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NA-50-1277

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NORTH AMERICAN AVIATION INC

ESTIMATED AERODYNAMIC CHARACTERISTICS

FOR

DESIGN OF THE

F-86E AIRPLANE

FC

File No. ——

Report No. NA-50-1277

NORTH AMERICAN AVIATION, INC.

ENGINEERING DEPARTMENT

ESTIMATED

AERODYNAMIC CHARACTERISTICS

FOR

DESIGN OF THE

F-86E AIRPLANE

PREPARED BY

Aerodynamics Group - Basic Data

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No. of Pages 82

Date 12-26-50

REVISIONS

DATE	REV. BY	PAGES AFFECTED	REMARKS

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INTRODUCTION

This report is a compilation of aerodynamic data for design of the F-86E airplane. The aerodynamic coefficients presented herein are based on wind tunnel tests conducted in the North American Aerodynamics Laboratory 7.75 x 11 foot low speed wind tunnel and in the high speed Southern California Cooperative Wind Tunnel. NACA experimental results are also utilized.

This report was prepared by F. T. Gardner and H. T. Downey under the supervision of W. E. Swanson.

W. E. Swanson
Basic Data Section

SUMMARY

Estimated aerodynamic characteristics of the F-86E airplane have been compiled herein for the purpose of furnishing a resume of design data. This report is in effect an appendix* to the aerodynamic report on the F-86A airplane since the principal difference between the F-86A and the F-86E which affects the aerodynamic characteristics is the incorporation of an all-movable horizontal tail.

The major portion of the information presented has been divided into sections of airplane longitudinal, lateral, and directional characteristics; the final sections are composed of fuel tank force data and slat load characteristics. Included in the longitudinal section are tail-off and tail-on lift and pitching moment, stabilizer and elevator effectiveness, stabilizer and elevator hinge moments, the effect of speed brakes, and the effect on airplane drag and pitching moment of the external under-wing fuel tanks. Lateral characteristics include the effect of aileron on lift, pitching moment and rolling moment. Aileron hinge moments and panel rolling moment complete the lateral section. The directional section consists of rudder hinge moment as a function of angle of yaw.

* For convenience the data of the F-86A airplane report (NA-48-814), which is applicable to both the F-86A and F-86E airplanes, have been reproduced herein such that the complete airplane characteristics of the F-86E are available in this one report.

DISCUSSION

GENERAL

The aerodynamic characteristics in this report have been presented as airplane coefficients which are defined by the nomenclature of Table II and by the dimensional data of Table I. This report is effectively an appendix to the aerodynamic characterisitcs report on the F-86A airplane, reference (a), since the principal aerodynamic difference between the F-86A and the F-86E is due to the difference in horizontal tails. The F-86E stabilizer serves as the primary longitudinal control and is operated by motion of the control column. The elevator is connected to the stabilizer by differential linkage so that the net effect is an all-moving horizontal tail. The F-86A stabilizer, however, is used only as a trimming device with the elevator acting in the conventional manner as the primary longitudinal control.

The data in this report are applicable only to a rigid airplane; therefore suitable modifications must be applied to include aero-elastic effects.

LONGITUDINAL CHARACTERISTICS

1. Tail-Off Lift, Drag, and Pitching Moment

Tail-off lift and pitching moment coefficients, slats closed, are presented in figure 4 for a Mach number range of M = .20 to 1.20. The effect of slats on lift and pitching moment is shown in figures 5 and 6 for the configurations of wing plus fuselage and wing in the presence of the fuselage. The tail-off drag polar, clean configuration, appears in figure 7 for M = .20 to M = 1.20. Figure 8 presents the drag of the fuselage in the presence of the wing, from which $C_{D_{W(B)}}$ can be calculated since $C_{D_{W(B)}} = C_{D_{W+B}} - C_{D_{B(W)}}$.

All tail-off data as listed above are reproduced from reference (a).

2. Tail-On Lift and Pitching Moment

Figure 9 presents tail-on lift and pitching moment for the Mach range of M = .20 to 1.20. These data are also reproduced from reference (a).

Pitching moment coefficients are taken about a center of gravity located at fuselage station 188.52

DISCUSSION

LONGITUDINAL CHARACTERISTICS

2. Tail-On Lift and Pitching Moment (Cont.)

(.25 M.A.C.), water plane -12.23, and buttock plane zero. It should be noted that tail-on pitching moment data are for a stabilizer setting of +1°.

Estimated limit trim lift coefficients versus Mach number for slat closed and open and for abrupt and gradual stalls are shown in figure 10. In figures 4 through 7 and 9 the limit lift coefficients for which data are shown are not correct for Mach numbers less than .60. The revised limit trim lift coefficients shown in figure 10 were used in the design of the airplane primarily because they were predicated upon flight test data of references (u) and (v).

3. Horizontal Tail Data

In addition to the difference already noted (General Discussion), the F-86E horizontal tail is designed with the elevator hinge line at the 72% chord element instead of the 67% chord element as it was for F-86A elevator. Moving the hinge line aft 5% of the horizontal tail chord reduced the elevator area but the nose of the elevator remained at essentially the same horizontal tail element thus the F-86E has an aerodynamic balance of the overhanging type. The static horn balance that was located near the tip of the horizontal tail has been removed and a new static balance, distributed internally along the nose of the aerodynamic balance, has been added. The trailing edge strip that was installed on the F-86A elevator has been removed from the F-86E. Figure 11 presents the rate of change of the elevator hinge moment coefficient with stabilizer deflection, $dC_{He}/d\delta_s$, versus Mach number. The variation of stabilizer hinge moment with elevator deflection, $C_{Hs}(\delta_e)$ is shown in figures 12 and 13. The rate of change of stabilizer hinge moment with stabilizer deflection, $dC_{Hs}/d\delta_s$, versus Mach number appears in figure 14. Figures 15 through 18 present the variation of stabilizer hinge moment with elevator deflection, $C_{Hs}(\delta_e)$. The data of figures 11 through 18 are based on references (e), (f), and (g).

Stabilizer effectiveness, figure 19, is based on references (e), (g), (l), and (m). Elevator effectiveness in the form of increments of airplane pitching moment at constant angles of attack due to elevator deflection, appears in figures

DISCUSSION

LONGITUDINAL CHARACTERISTICS

3. Horizontal Tail Data (Cont.)

20 through 22. These data are predicated on references (e), (g), (1), and (p). Figure 23 presents the stabilizer-elevator gearing curve. Inasmuch as the effectiveness of an all-movable horizontal tail is such that it requires a high degree of accuracy in manufacture and rigging that is difficult to produce, a tolerance of ±1° elevator deflection is shown.

4. Speed Brake Effects

Increments in airplane pitching moment and drag due to deflection of the fuselage speed brakes, figures 24 through 27, are reproduced from the F-86A report, reference (a). It should be noted that the maximum speed brake deflection for the F-86E is 50° (see table I).

5. External Wing Fuel Tank Effects

Figure 28 presents the estimated increment in drag of the airplane due to one 120 gallon external wing fuel tank with fin for zero airplane angle of attack. The variation of $d\Delta C_m/dC_L$ with Mach number is shown in figure 29. These data have resulted from an analysis of references (c), (d), (o), (r), (s), and (w). The location of the under-wing tank is at Buttock Plane 99.5.

LATERAL CHARACTERISTICS

Increments in lift, pitching moment, and rolling moment due to aileron deflection will be found in figures 31 through 44. Longitudinal and lateral center of pressure locations of the increment of wing load due to aileron deflection versus Mach number are presented in figure 30. The data of reference (b), (i), (l), and (m) were utilized in deriving the above information.

Aileron hinge moments, figures 45 and 46, are based on the data of references (i), (m), (q), and (a-2).

Panel rolling moment as a function of airplane angle of attack for the two configurations of wing plus fuselage and wing in the presence of the fuselage are reproduced from reference (a). Slats closed data appear in figure 47, while slats free data are given in figure 48.

DISCUSSION

LATERAL CHARACTERISTICS (Cont.)

For convenience, the average pressure coefficients measured in the aileron paddle balance chamber are included in this report in figures 49 through 52. These data are based on the information of references (i), (n), (o), (p), (q), (t), and (x).

DIRECTIONAL CHARACTERISTICS

The variation of rudder hinge moment due to both yaw and rudder deflection are presented at various Mach numbers in figures 53 and 54. Figure 55 presents the increment in rudder hinge moment due to angle of attack, throughout the range of yaw angles. These data are based on references (g) and (h).

TANK CHARACTERISTICS

Yaw data for the 120 gallon external wing fuel tank with large fin, located at Buttock Plane 99.5, are presented in figures 56 through 58. Tank normal force coefficient, C_N, and C_N x C.P. versus angle of yaw for various angles of attack and Mach numbers will be found in Figure 56.

Tank side force coefficient and the corresponding center of pressure versus angle of yaw for various airplane angles of attack and Mach number are presented in Figure 57. Figure 58 presents tank support fairing side force section data.

All tank data are predicated on the data of reference (j), (y), and (z).

SLAT LOAD CHARACTERISTICS

A table of retracted slat load characteristics at various Mach numbers and angles of attack is presented in figure 59. Included in this figure is a complete definition of the forces and moment arms involved.

The slat opening force coefficient, C_s, versus angle of attack for various Mach numbers is presented in figure 60.

All slat data are based on the tunnel tests of reference (k).

REFERENCES

(a) NA-48-814 "Estimated Aerodynamic Characteristics for Structural Design of XP-86 and P-86A Airplane", dated 21 July, 1948

(b) NA-48-835 "Estimated Aerodynamic Characteristics for Structural Design of the YF-93 Airplane", dated 25 October 1948

(c) NA-49-797 "Revised Performance Calculations for the Model F-86A Airplane", Appendix I, dated 31 October 1949

(d) NA-49-1045 "Estimated Aerodynamic Characteristics for Design of B-45 Airplane", dated 21 November 49

(e) NA-46-852 (NAAL-46) "Wind Tunnel Tests of a 0.23-Scale Model of the XP-86 Airplane with a 5 Aspect Ratio Sweptback Wing", dated 11 November 1946

(f) NA-46-969 (NAAL-55) "Wind Tunnel Tests of an 0.23-Scale Model of the XP-86 Airplane to Determine the Slats Open Flying Qualities", dated 15 October 1946

(g) NA-47-1043 (NAAL-84) "Wind Tunnel Tests to Determine the Low Speed Flying Qualities of a 0.20-Scale High Speed Model of the XP-86 Airplane", dated 26 October 1947

(h) NA-48-351 (NAAL-99) "Wind Tunnel Tests of a 0.20-Scale Model of the P-86B Airplane with an Enlarged Horizontal Tail and Revised Speed Brakes", dated 17 March 1948

(i) NA-49-467 (NAAL-142) "Wind Tunnel Tests to Determine the Stability and Fuselage Pressure Distribution of a 0.20-Scale Model of the F-93A Airplane"

(j) NA-49-1027 (NAAL-154) "Wind Tunnel Tests of a 1/3-Scale Semi-Span Model of the F-86A Airplane to Determine Force and Pressure Characteristics for Three 120 Gallon Wing Fuel Tanks", dated 16 November 1949

REFERENCES

(k) CWT-23 "Preliminary Report on High Speed Wind Tunnel Tests of a 1/3-Scale Half Model of the North American XP-86 Airplane", dated 23 September 1947

(l) CWT-38 "Preliminary Report on High Speed Wind Tunnel Tests on a 0.20-Scale Half Model of the P-86B Airplane", dated 20 January 1948 through 1 March 1948

(m) CWT-52 "Preliminary Report on Wind Tunnel Tests at Transonic Speed of Several Proposed 1/40-Scale Models of the North American F-86B and F-86C Airplanes", dated 19 November 1948

(n) CWT-54 "Preliminary Report on Additional High Speed Wind Tunnel Tests of an 0.08-Scale Model of the North American XAJ-1 Airplane", dated 6 August 1948

(o) CWT-98 "Report on Wind Tunnel Tests at High Speeds and High Reynolds Numbers of a 0.115-Scale Reflection-Plane Model of the North American XA2J-1, Phase 1 Airplane", dated 26 April 1949

(p) CWT-110 "Report on Wind Tunnel Tests at High Speeds and High Reynolds Numbers of a 1/5-Scale Refelction-Plane Model Incorporating Various Components of the North American F-86 and YF-93 Airplane", dated 12 August 1949

(q) CWT-130 "Report on Wind Tunnel Tests at High Speeds of a 1/5-Scale Reflection-Plane Model of the North American F-86 and YF-93 Airplane", dated 12 August 1949

(r) RM-L9J19 (NACA) "The Effect of Tip Tanks on the Rolling Characteristics at High Subsonic Mach Numbers of a Wing Having an Aspect Ratio of 3 with a Quarter-Chord Line Swept Back 35°", dated 17 January 1950

(s) RM-L9K25 "Experimental Investigation of Various External-Store Configurations on a Model of a Tailless Airplane with a Sweptback Wing", dated 19 January 1950

REFERENCES (Cont.)

(t) RM-L8H06 "Pressure Distributions Over a Wing-Fuselage Model at Mach Numbers of .4 to .99 and at 1.2", dated 3 November 1948

(u) RM-A8130 "The Effect of Change of Angle of Attack on the Maximum Lift Coefficient of a Pursuit Airplane", dated 6 May 1949

(v) CMR-A5G06 (NACA) "Effect of Mach and Reynolds Numbers on Maximum Lift Coefficient in Gradual and Abrupt Stalls", dated July 1945

(w) Technical Report F-TR-1188-IA(ATI No. 43187) "Compressibility Effects on Drag--Air Drag: Theoretical and Practical Data on Aerodynamic Drag"

(x) NACA-PC #5.36/5 "High Speed Wind Tunnel Tests of a 1/4 Scale Model of the XP-81 Airplane -- Aileron Hinge Moment and Balance Pressures", dated 25 January 1945

(y) TM-1194 (NACA) "Force and Pressure Distribution Measurements on Eight Fuselages"

(z) Archives Report No. 66/120 (German Report) "Three Component Measurements on 15 Cm. Shell Shapes 1 and 5"

(a-1) NA-50-928" Aerodynamic Dimensional Data for the F-86E Airplane (N.A.A. Model Designation NA-170)", dated 30 August 1950

(a-2) Flight Test Data, Flight 19, F-86A, No. 49-1067

TABLE I

AERODYNAMIC DIMENSIONAL DATA*

WING DATA

S_w	Total wing area (includes flaps, slats, and 49.92 ft.^{2} covered by the fuselage)	287.95 ft.^{2}
b_w	Span (horizontal)	37.12 ft.
AR_w	Aspect ratio	4.785
λ_w	Taper ratio $\frac{1}{1.949}$	.5131
Γ_w	Dihedral angle	3°00'
$\bar{c}_w$	Mean aerodynamic chord (wing sta.98.71) Fuselage sta. of .25 $\bar{c}_w$ (W.P.-25.63)	97.03 in. 188.52
φ_w	Sweepback of the 25% element(aerodynamic)	35°13'31.4"
i_r	Incidence of the root chord (sta.0)	+1°00'
i_t	Incidence of the tip chord (sta.220.8)	-1°00'
	Root airfoil(normal to 25% element)	NACA 0012-64 (modified)
	Tip airfoil(normal to 25% element)	NACA 0011-64 (modified)

* From Reference (a-1)

TABLE I (Cont.)

AERODYNAMIC DIMENSIONAL DATA

AILERON DATA (Data for one aileron)

Type		Flat Sided
S_a	Area (aft of aileron hinge line and including aileron tab)	16.36 ft^2
$S_a\bar{c}_a$	Area moment	26.49 ft^2
c_a/c_w	Ratio of aileron chord to wing chord (in streamline)	.3081
$\delta_{a_{max}}$	Aileron deflection, maximum	15°up,15°down
S_b	Balance area forward of the hinge line (including 50% of the fabric seal = .701 ft^2)	6.43 ft^2
c_b/c_a	Ratio balance chord to aileron chord	.4390

LEADING EDGE SLAT DATA (for one side only)

S_{sl}	Area, projected into wing ref. plane	17.72 ft^2
b_{sl}	Span (Wing Sta.54.09 to 209.33)	155.24 in.
C_{sl}	Chord (constant)	16.43 in.
δ_{sl}	Deflection	15°00'

HORIZONTAL TAIL

Type	Stabilizer adjustable from cockpit control column; elevator connected to stabilizer by differential linkage	
S_H	Total area (including 1.20 $ft.^2$ covered by vertical tail)	35.28 ft^2
b_H	Span	12.75 ft^2
AR_H	Aspect ratio	4.65
λ_H	Taper ratio	.450

TABLE I (Cont.)

AERODYNAMIC DIMENSIONAL DATA

HORIZONTAL TAIL (Cont.)

Γ_H	Dihedral angle	10°
$\bar{c}_H$	Mean aerodynamic chord (H.T.Sta.33.54) Fuselage station of .25 $\bar{c}_H$(W.P.20.70)	34.71 in. 406.01
φ_H	Sweepback of the 25% element	34°35'20"
$\frac{S_H}{S_W}$	Ratio horizontal tail area to wing area	.1225
	Airfoil Sections (Root and Tip, parallel to ℄)	NACA 0010-64
δ_s	Deflection of stabilizer with respect to the fuselage reference plane	10°down, 6°up
S_e	Area (excluding balance area forward of the hinge line)	8.62 ft^2
$S_e\bar{c}_e$	Area moment (normal to hinge line)	6.07 ft^3
c_e/c_H	Ratio of elevator chord to horizontal tail chord	.2800
δ_e	Deflection maximum (measured with respect to horizontal stabilizer chord plane and normal to elevator hinge line)	20°54'up 8°20'down

VERTICAL TAIL DATA

S_V	Area (including .92 ft.^{2} blanketed by the fuselage and excluding 3.96 ft.2 dorsal fin)	33.44 ft.^{2}
AR_V	Aspect ratio	1.74
λ_V	Taper ratio	.362
$\bar{c}_V$	Mean aerodynamic chord (V.T.Sta.37.87)	55.99 in.
	Fuselage station of 25 c_V(W.P.54.59)	385.78
φ_V	Sweepback of 25% element	35°

TABLE I (Cont.)

AERODYNAMIC DIMENSIONAL DATA

VERTICAL TAIL DATA

	Airfoil (parallel to fuselage reference plane, constant)	NACA 0011(10) -64 modified
S_r	Area (including tab but excluding rudder balance forward of hinge line)	8.12 ft^2
$S_r\bar{c}_r$	Area moment	9.72 ft^3
δ_r	Deflection, maximum	27.5°R, 27.5°L

SPEED BRAKE DATA

$\delta_{j_{max}}$	Speed brake deflection, maximum	50°
S_j	Area (surface area of one brake)	5.49 ft^2

TAPLE II

NOMENCLATURE

GENERAL NOMENCLATURE

M: Free stream Mach number = $\frac{V}{a}$

V: Average free stream velocity, ft./sec.

a: Velocity of sound in air, ft./sec.

α: Angle of attack of fuselage reference line relative to the free air stream, degrees

ψ: Angle of yaw of plane of symmetry relative to the free air stream, degrees

q: Incompressible dynamic pressure of free stream= $\frac{\rho V^2}{2}$

ρ: Mass density of air, slugs/ft^3

$\frac{p}{q}$: Difference between local static pressure and free stream static pressure divided by free stream incompressible dynamic pressure

S: Wing area projected in wing reference plane, ft.^{2}

S_{aft}: Area of movable surface aft of hinge line, ft.^{2}

$\bar{c}$: Mean aerodynamic chord, in.

$\bar{c}_{aft}$: Mean aerodynamic chord of movable surface, in.

b: Wing span, ft.

AIRPLANE NOMENCLATURE

W = Wing

B = Fuselage

S = Slats

S_f = Slats free

W(B) = Wing in the presence of fuselage, slats retracted

B(W) = Fuselage in presence of wing, slats retracted

H = Horizontal tail

V = Vertical tail

TABLE II

NOMENCLATURE (Cont.)

AIRPLANE COEFFICIENTS

C_L = Lift coefficient = $\frac{\text{Lift}}{qS}$

C_D = Drag coefficient = $\frac{\text{Drag}}{qS}$

C_m = Pitching coefficient = $\frac{\text{Pitching Moment}}{qS\bar{c}}$

C_{ℓ}' = Panel rolling moment coefficient (due to lift on one wing only) = $\frac{\text{Panel Rolling Moment}}{qSb}$

C_{ℓ} = Airplane rolling moment coefficient due to deflection of one aileron $\frac{\text{Airplane Rolling Moment}}{qSb}$

C_Y = Side force coefficient = $\frac{\text{Side Force}}{qS}$

MOVABLE SURFACES

C_H = Hinge moment, where subscript (without parenthesis) denotes movable surface = $\frac{\text{Hinge Moment}}{qS_{aft}\bar{c}_{aft}}$

$C_{He}(\delta_e)$ = Elevator hinge moment coefficient versus C_L for various elevator angles

$C_{HS}(\delta_e)$ = Stabilizer hinge moment coefficient versus C_L for various elevator angles

$\delta_{(\ )}$ = Angular deflection in plane normal to axis of rotation, where subscript indicates movable surface

TANK COEFFICIENTS

C_N = Normal force coefficient based on tank planview area = $\frac{\text{Normal Force}}{qS_{plan\ view}}$

C_{Y_F} = Support fairing section side force coefficient = $\frac{\text{Section Side Force}}{q\,c_{fairing}}$

C_Y = Tank Side Force Coefficient = $\frac{\text{Side Force}}{qS_{planview}}$

TABLE II

NOMENCLATURE (Cont.)

SUBSCRIPTS

a = Aileron

e = Elevator

s = Stabilizer

r = Rudder

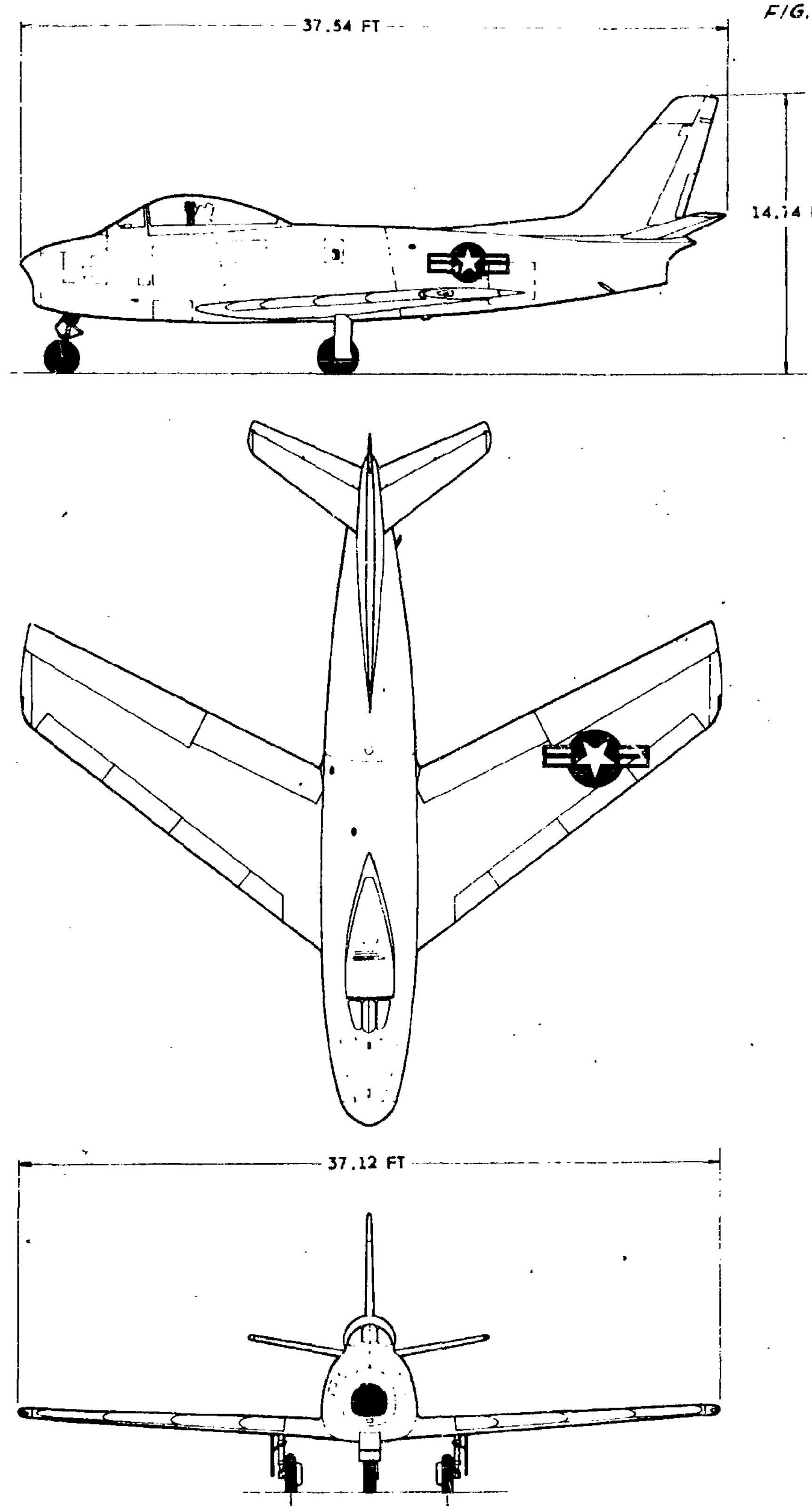
INDEX OF FIGURES

INDEX OF FIGURES (Cont.)

INDEX OF FIGURES (Cont.)

INDEX OF FIGURES (Cont.)

FIG. 1



F-86E

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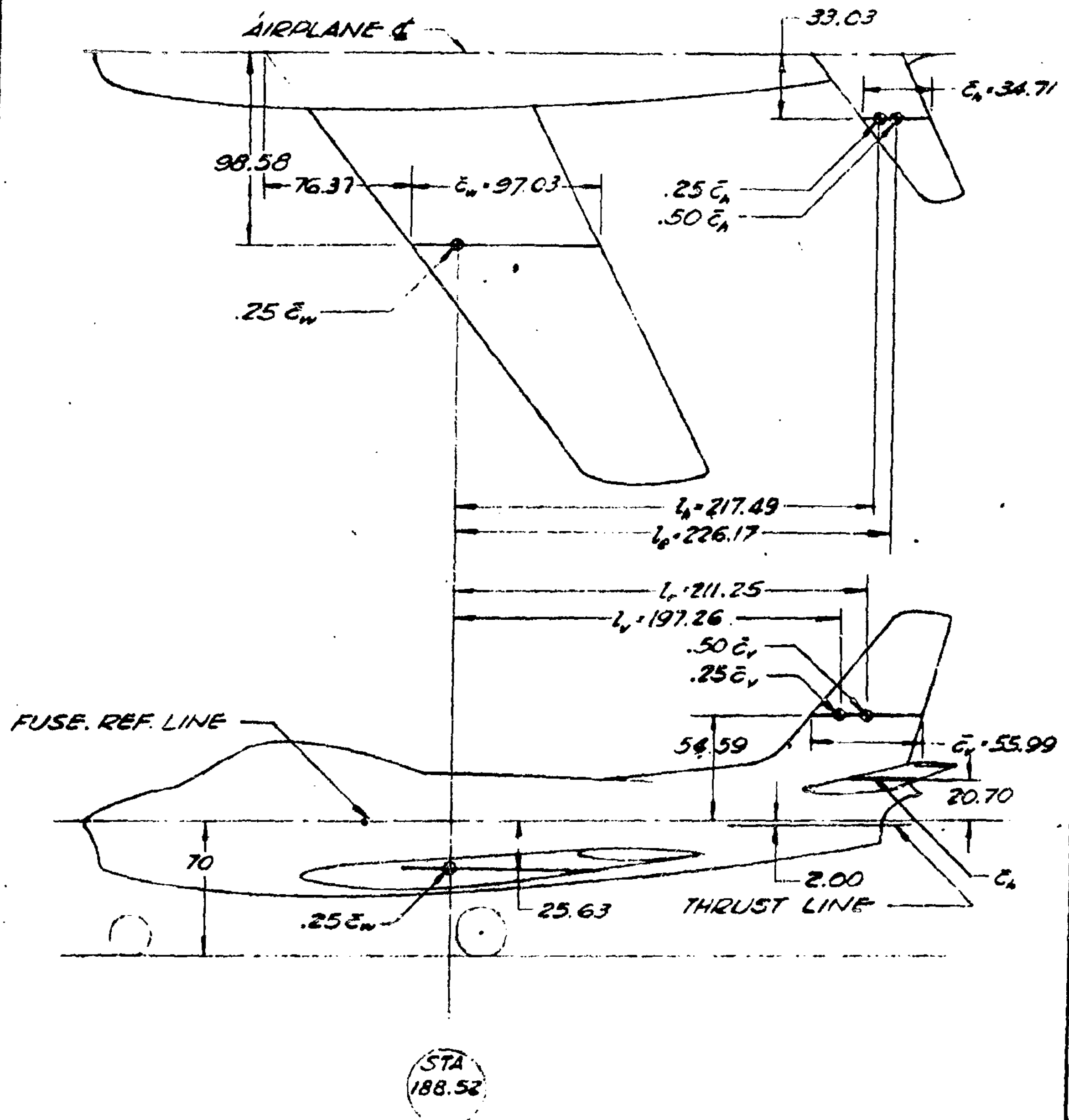
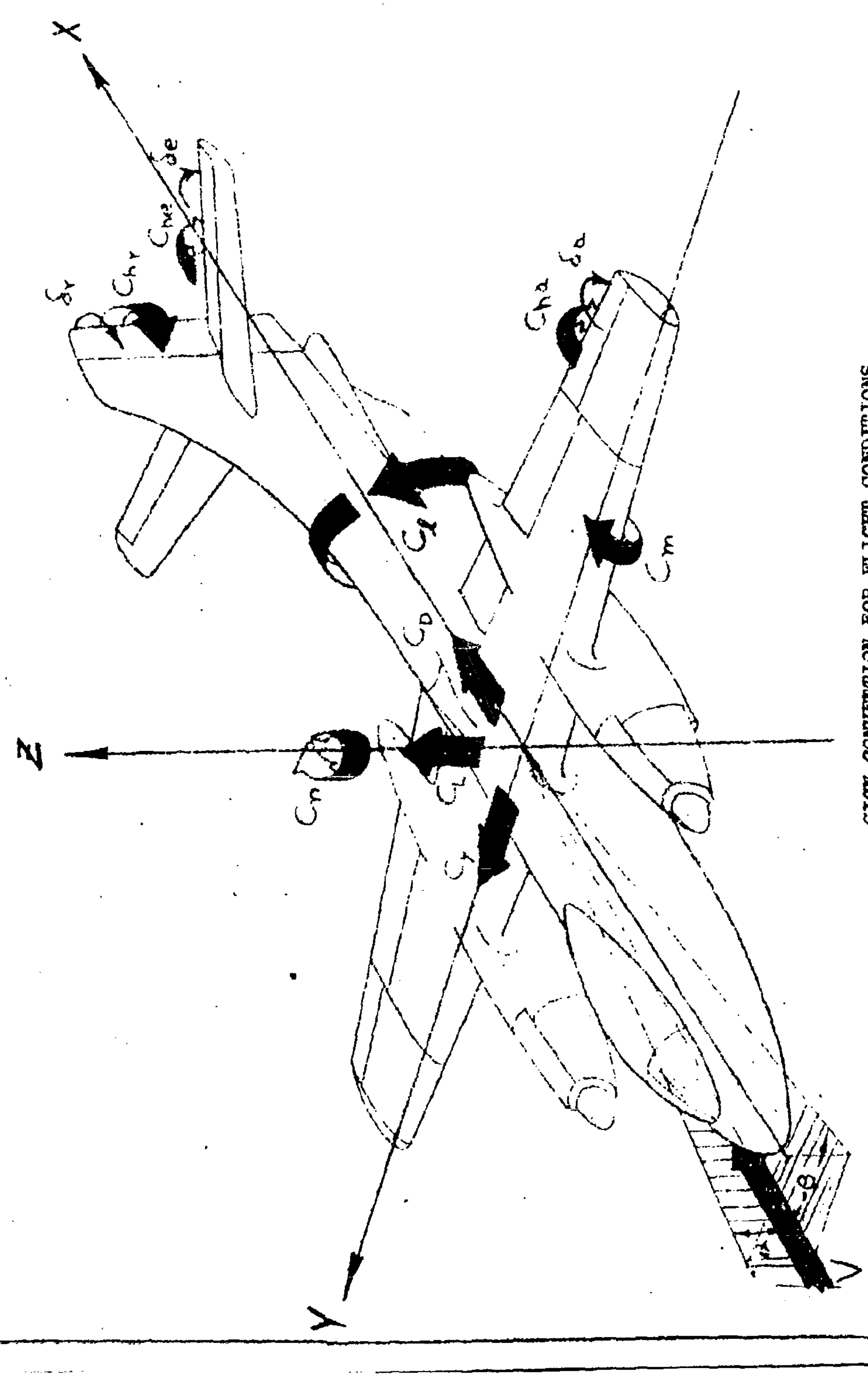
FIGURE NO. 2



ESTIMATED AERODYNAMIC CHARACTERISTICS

FIG. 3

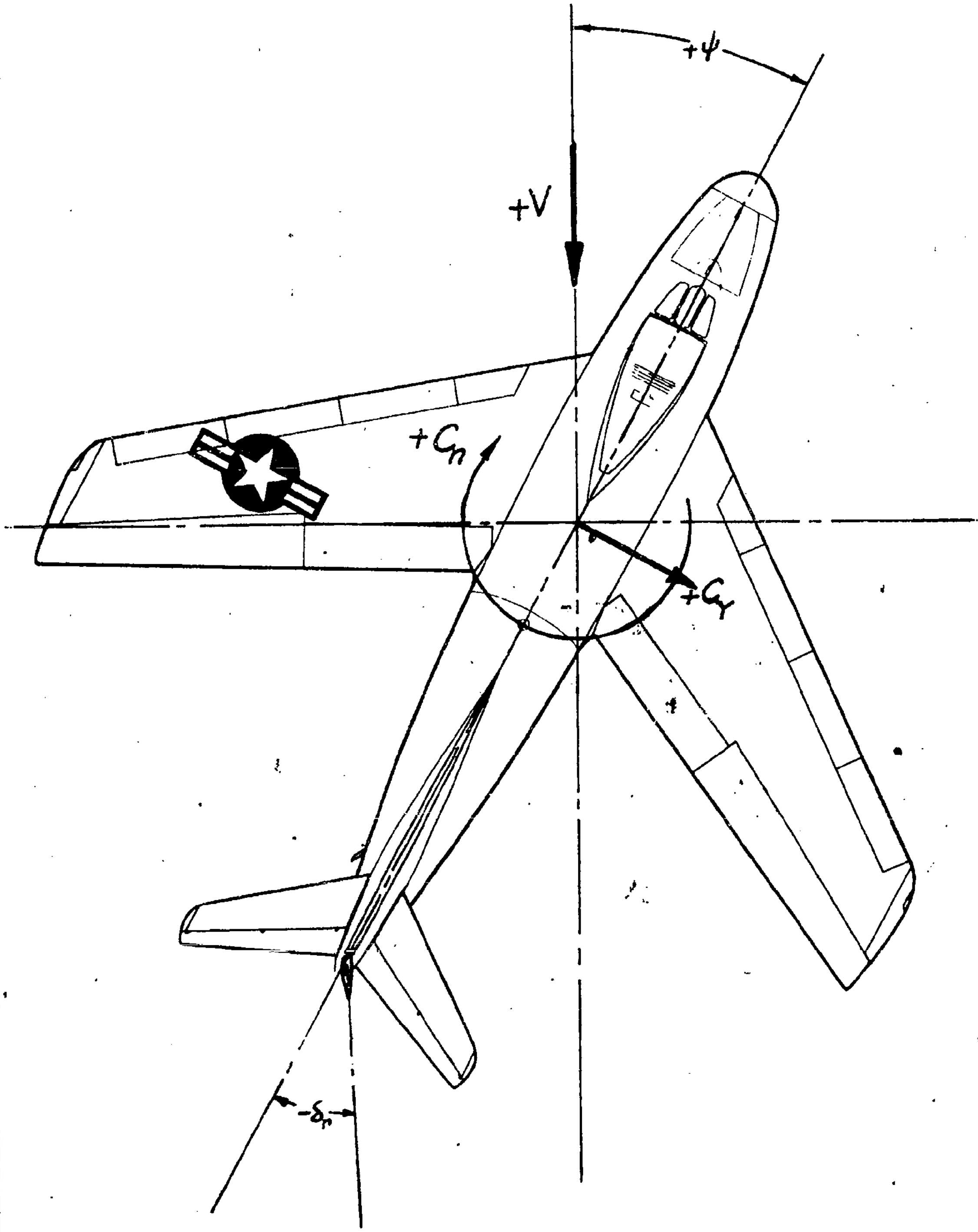


SIGN CONVENTION FOR FLIGHT CONDITIONS

Directions, angles, surface deflections, and coefficients are positive as shown.

FIG. 3a

SIGN CONVENTION
YAW CONDITION



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BASIC TAIL-OFF C
C_m & α_A VARI

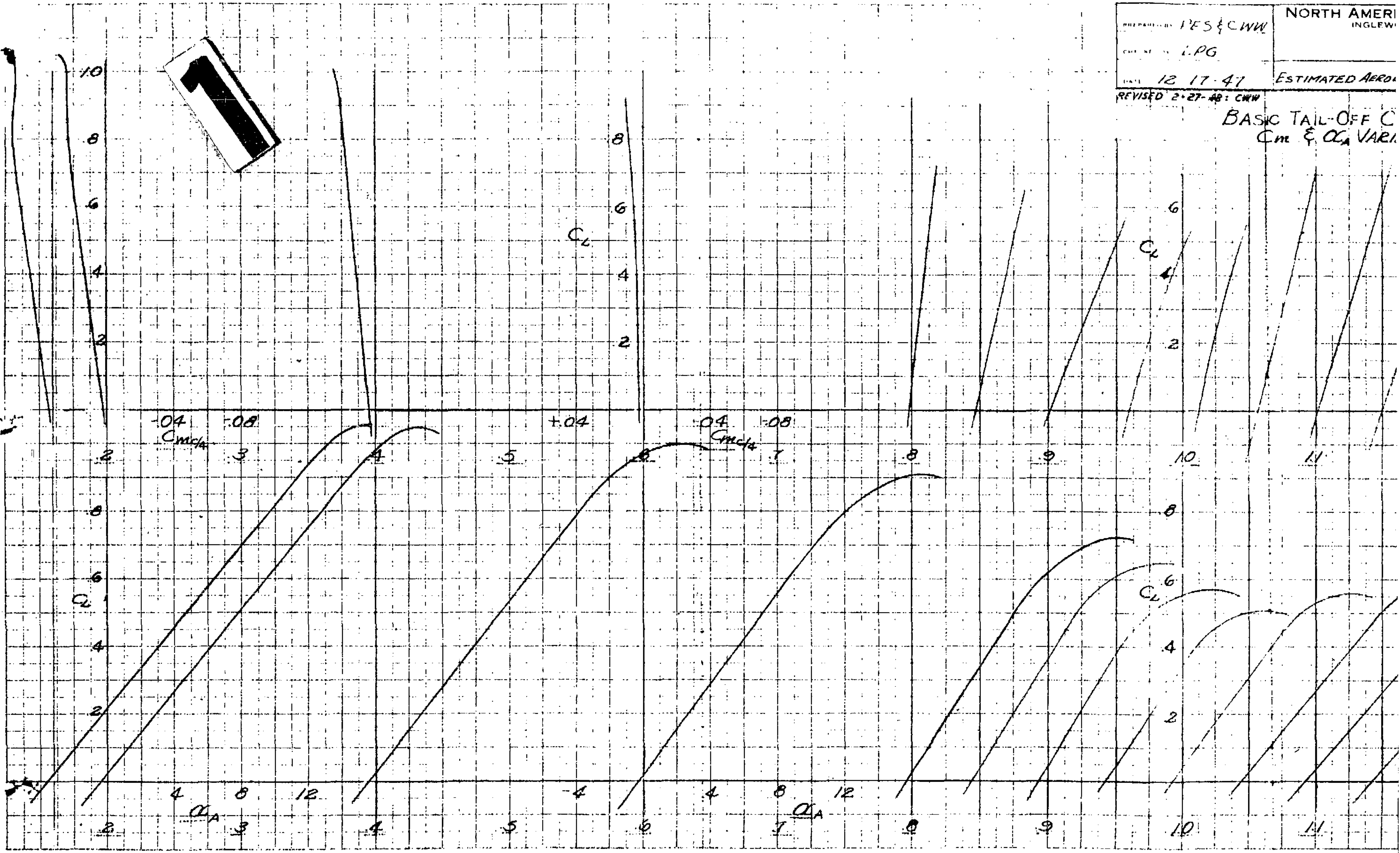

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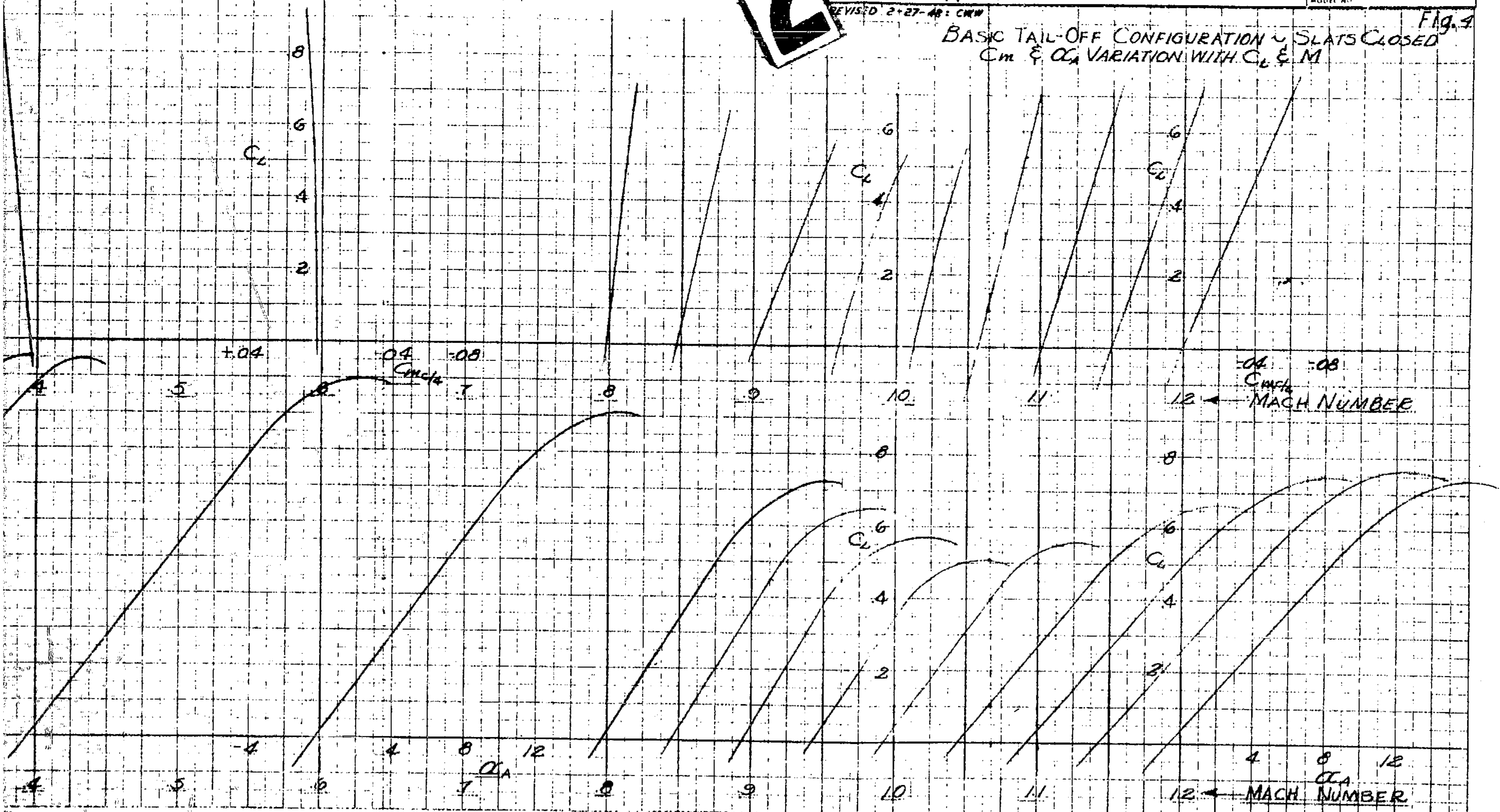
Fig. 4

BASIC TAIL-OFF CONFIGURATION ~ SLATS CLOSED

C_m & α_A VARIATION WITH C_L & M

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VARIATION OF
ATTACK –
WING PLUS FUSELAGE
WING IN PRESENCE OF
NOTE
C_L
α
MACH NUMBER

FORM ED-324

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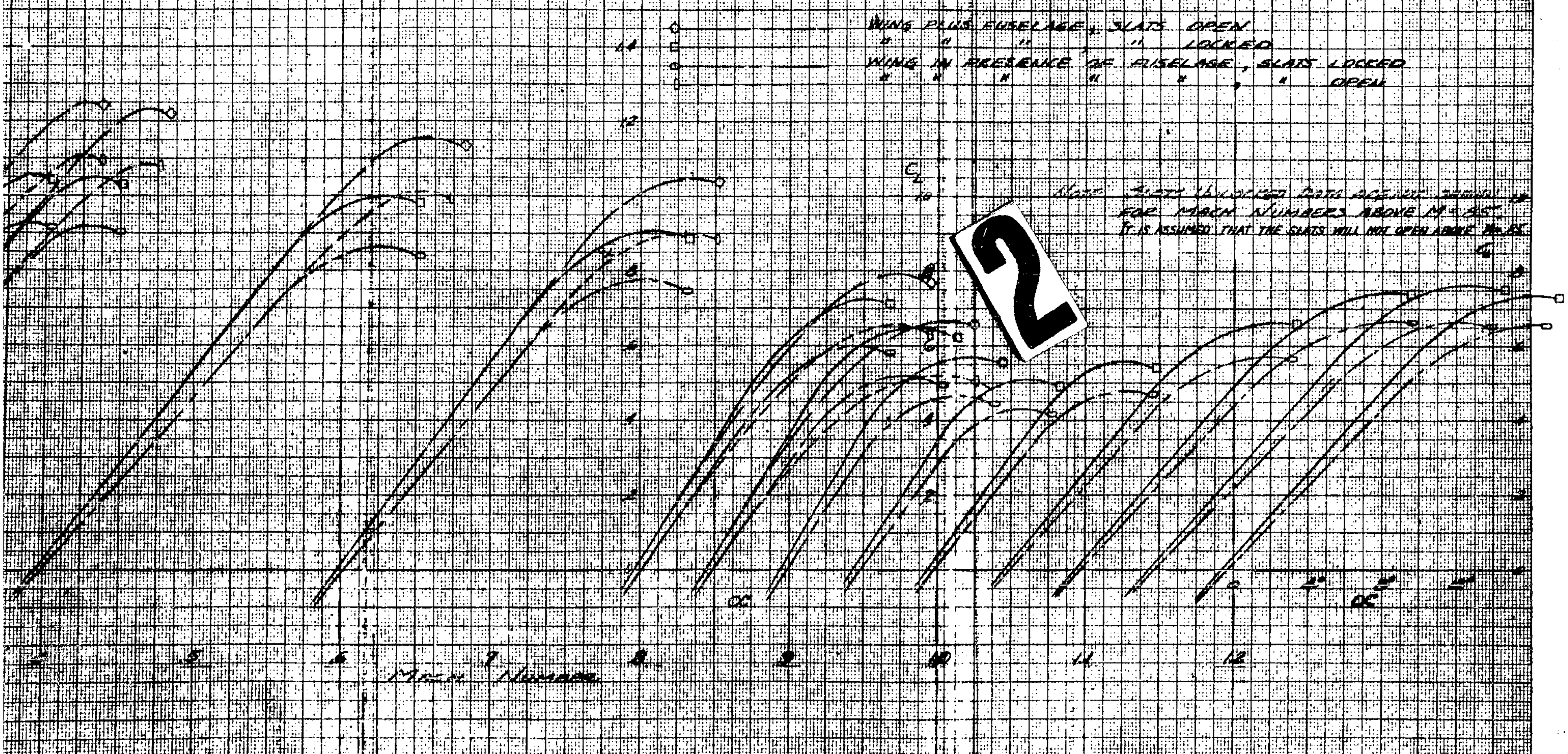
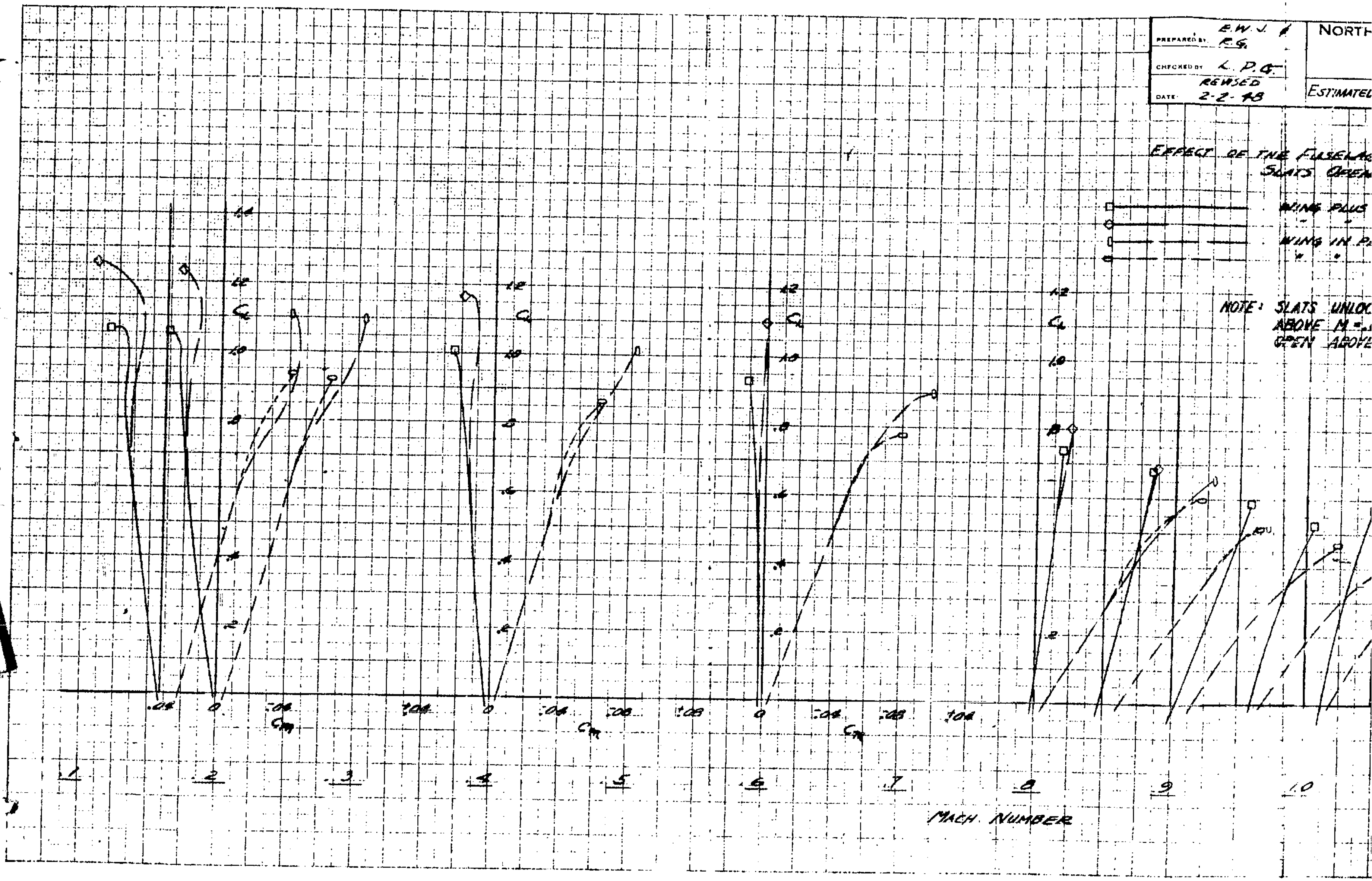
FIG. 5

VARIATION OF LIFT COEFFICIENT WITH ANGLE OF ATTACK – SLATS LOCKED (CLOSED) AND UNLOCKED

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REVISED
DATE 2-2-48
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ESTIMATED
EFFECT OF THE FUSELAG
SLATS OPEN
WING PLUS
WING IN P
NOTE: SLATS UNLOC
ABOVE M =
OPEN ABOVE
C_L
C_m
MACH NUMBER
.1
.2
.3
.4
.5
.6
.7
.8
.9
1.0

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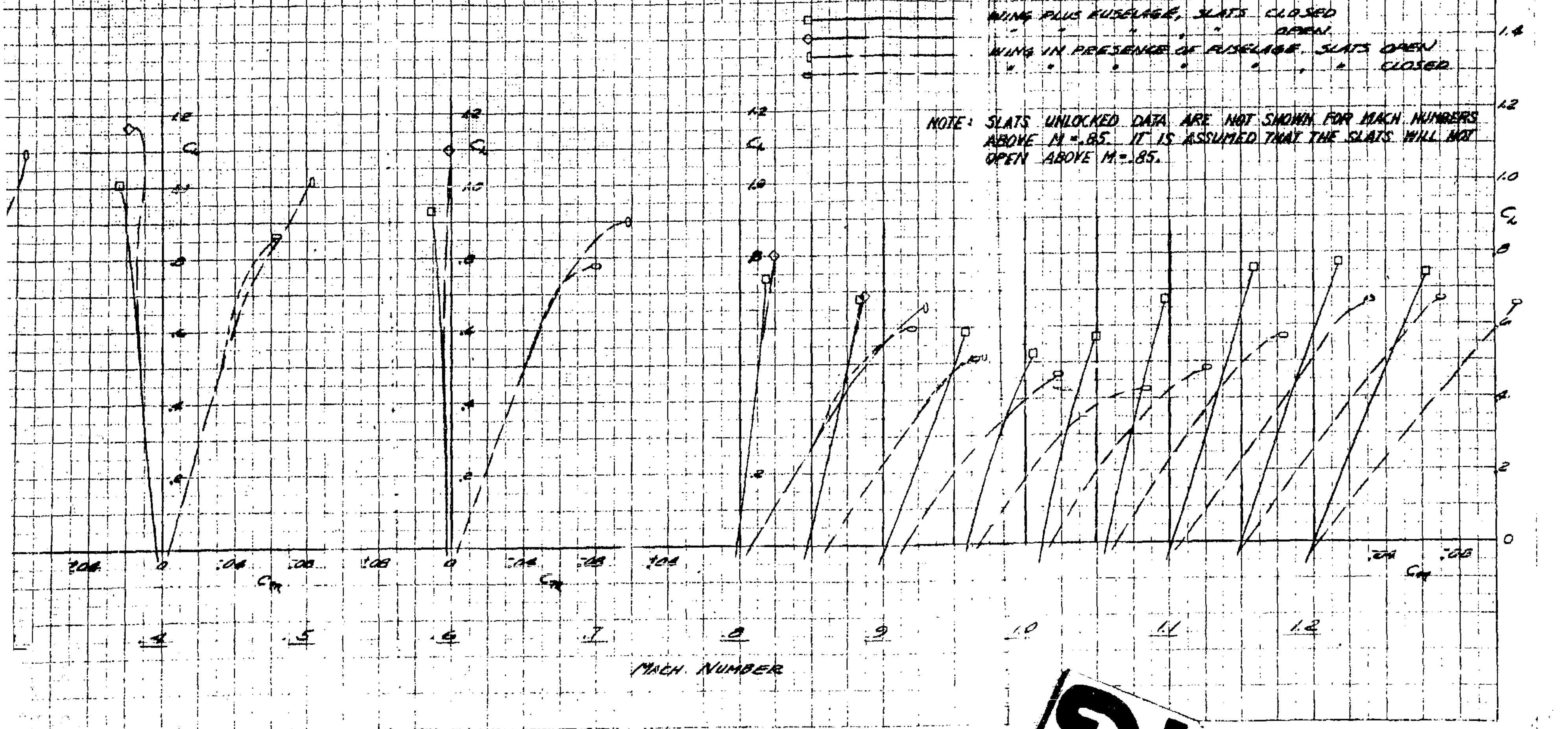
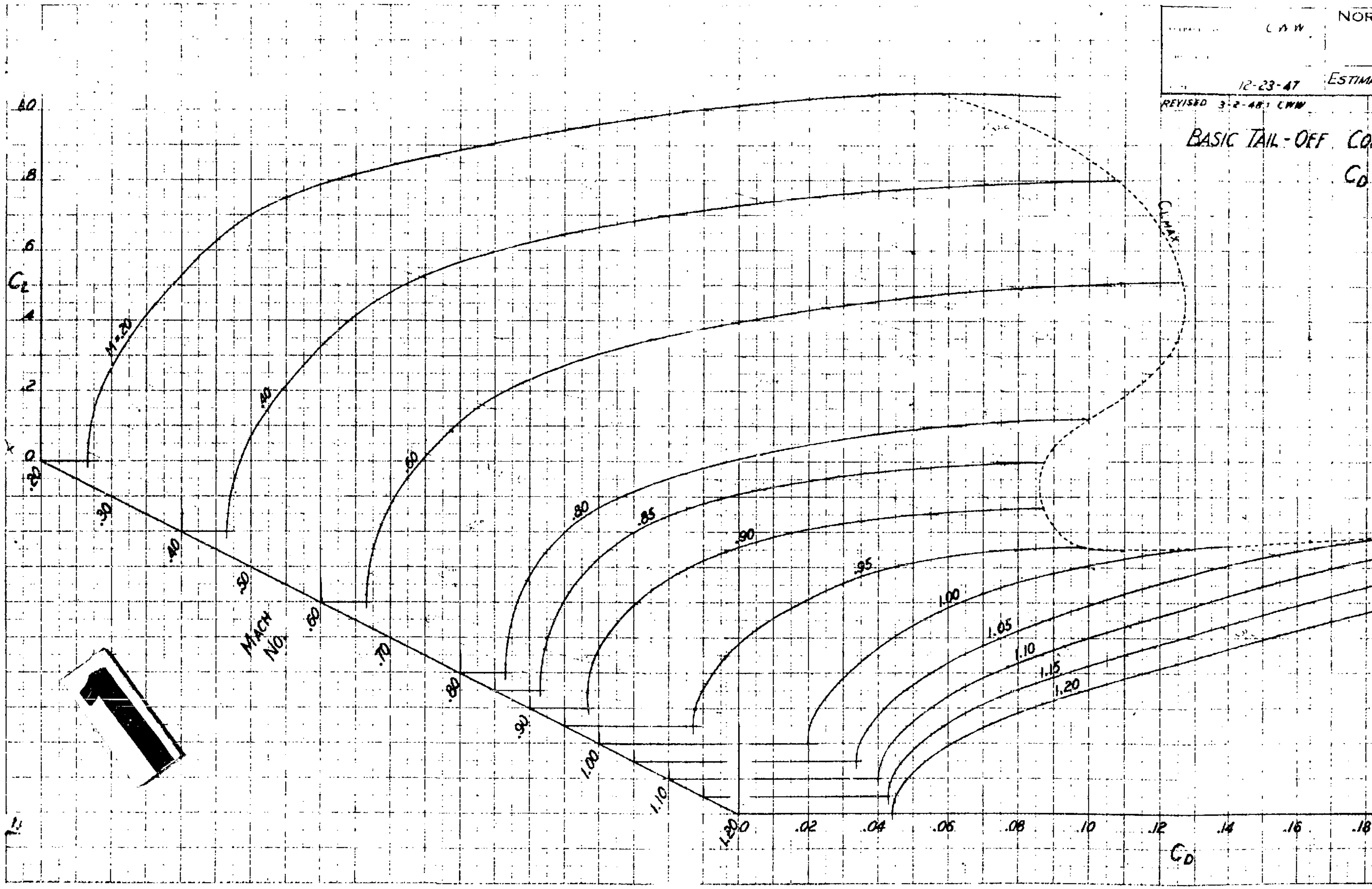
Fig. 6.

EFFECT OF THE FUSELAGE ON THE PITCHING MOMENT DATA
SLATS OPEN AND CLOSED

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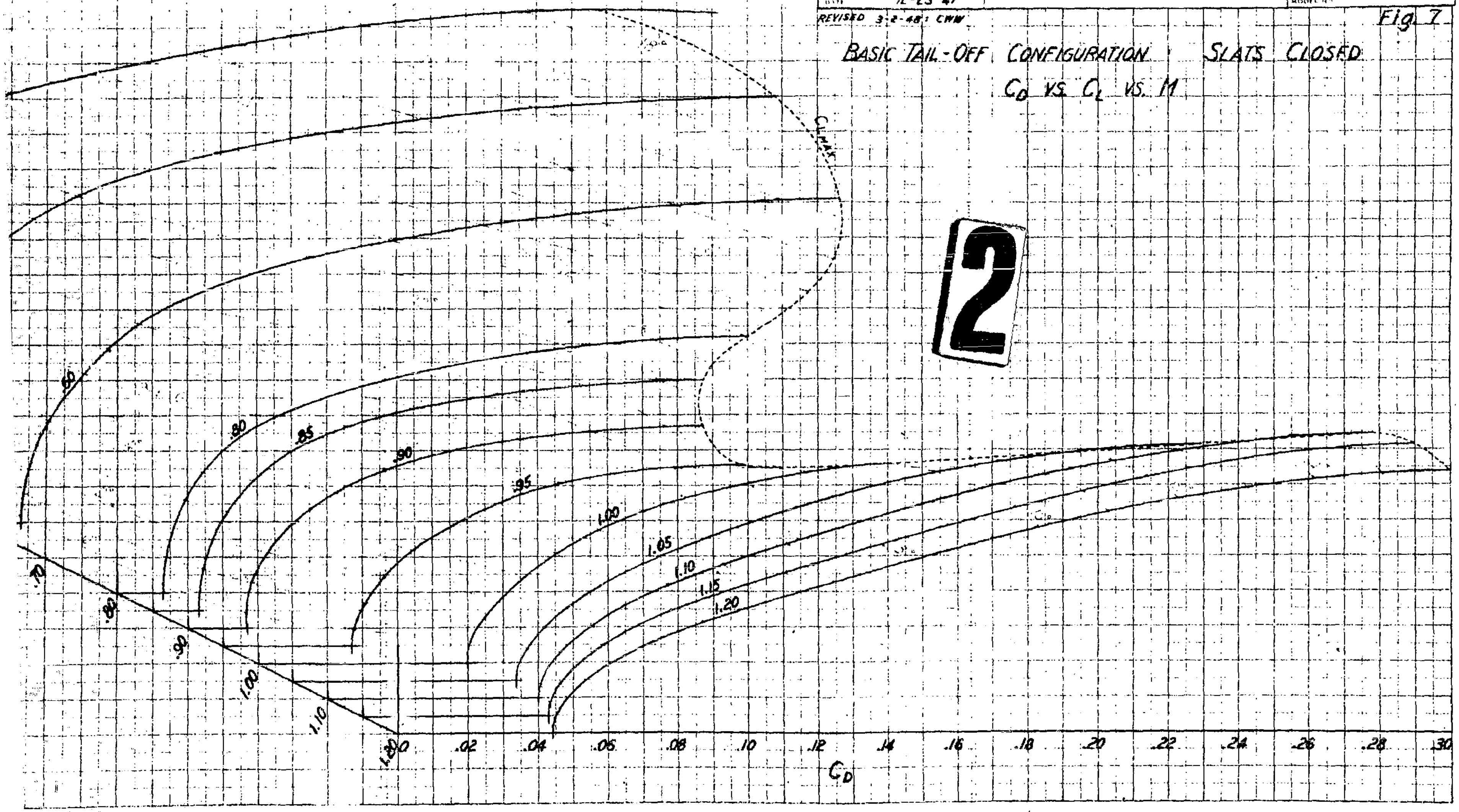
BASIC TAIL-OFF CO
C_D
$C_{L MAX}$
C_L
C_D
M=.20
.40
.60
.80
.85
.90
.95
1.00
1.05
1.10
1.15
1.20
MACH NO.
.30
.50
.70
1.20
0
.2
.4
.6
.8
1.0
.02
.04
.06
.08
.10
.12
.14
.16
.18

Fig. 7

BASIC TAIL-OFF CONFIGURATION SLATS CLOSED

C_D VS. C_L VS. M



2

FORM ED-148

NORTH AMERICAN AVIATION, INC.

PREPARED BY CWW

CHECKED BY

DATE 3-2-48

ESTIMATED AERODYNAMIC CHARACTERISTICS

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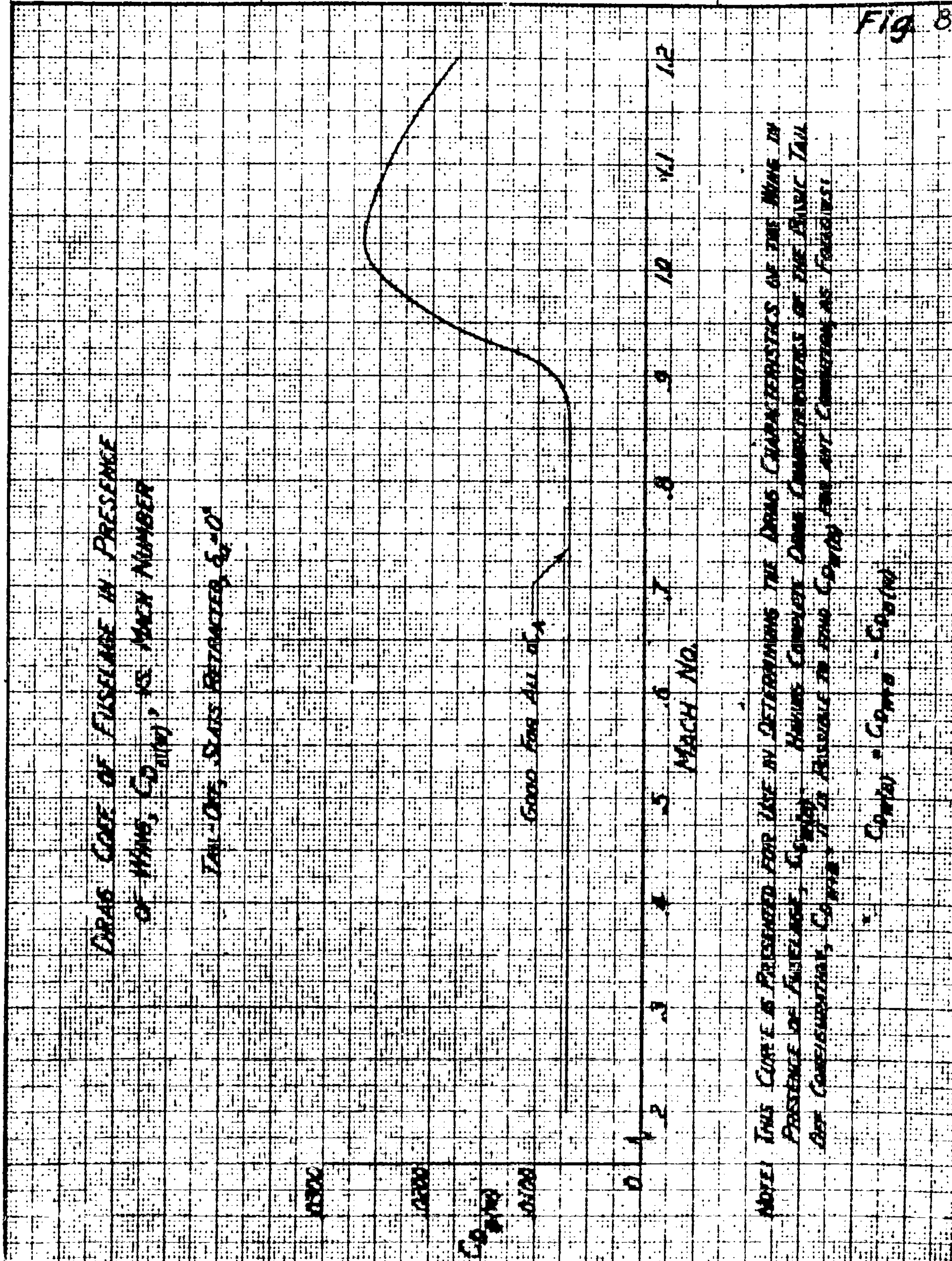
REPORT NO NA-50-1277

MODEL NO F-86E

Fig. 8



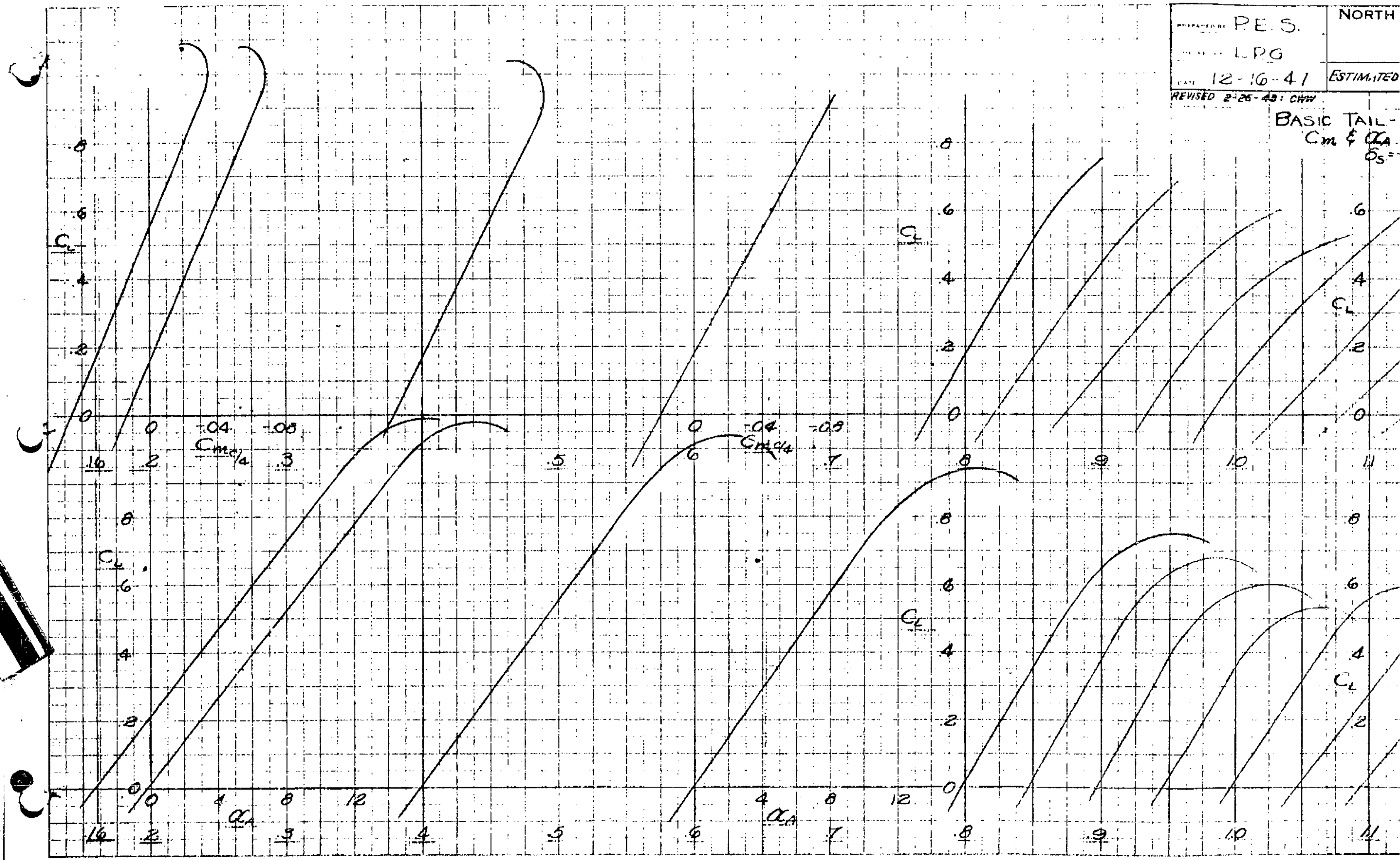
GALVANIZED NO. 1881

PREPARED BY P.E.S.
L.P.G.
DATE 12-16-41
REVISED 2-26-43: CHW

NORTH

ESTIMATED

BASIC TAIL-
C_m & α_A
δ_S=



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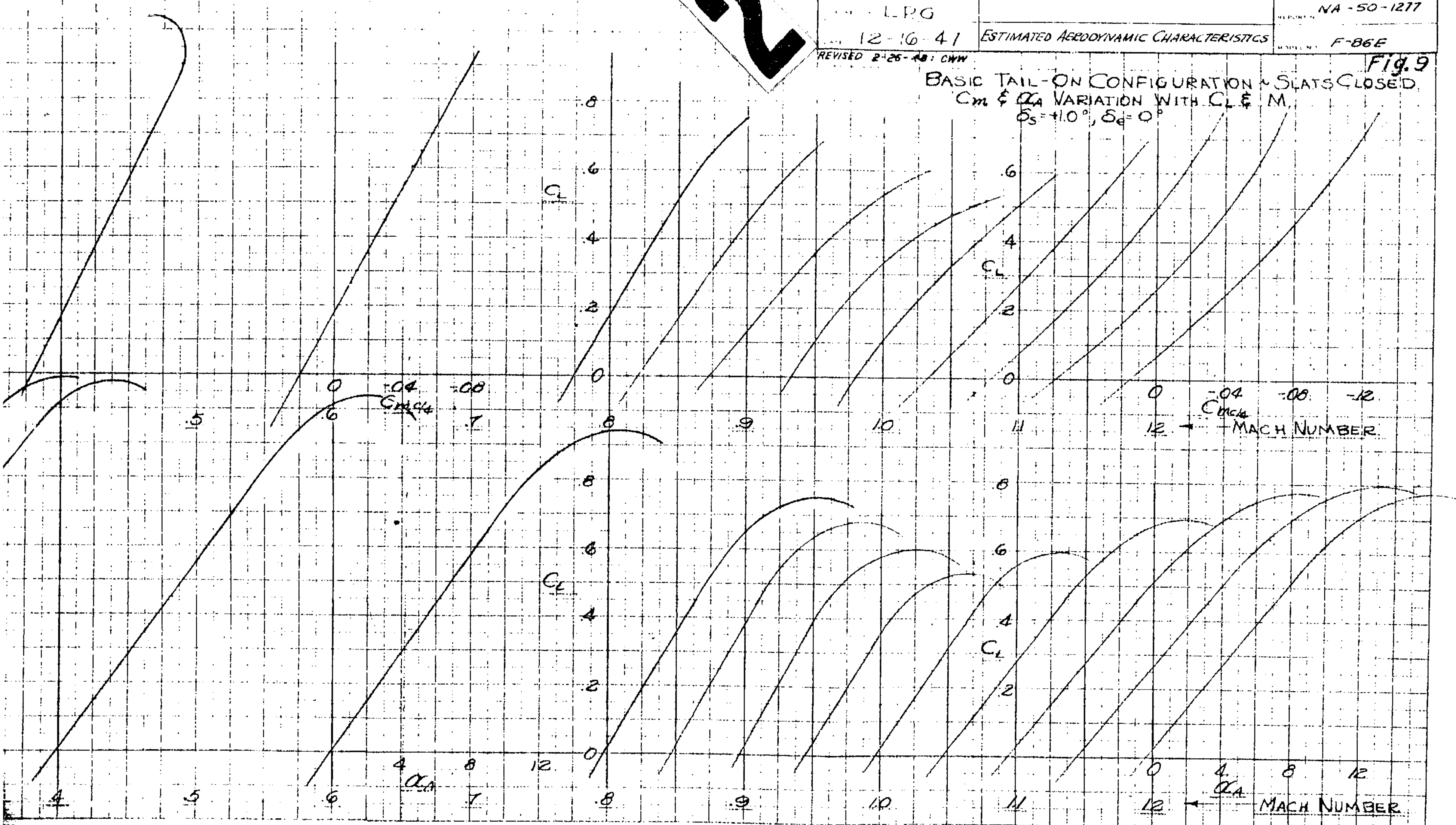
REVISED 2-26-48: CWW

Fig. 9

BASIC TAIL-ON CONFIGURATION ~ SLATS CLOSED
C_m & α_A VARIATION WITH C_L & M.
$\delta_s = +1.0°$, $\delta_e = 0°$



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DATE: 10-24-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO F-86A, F-86D, F-86E

FIG. 10

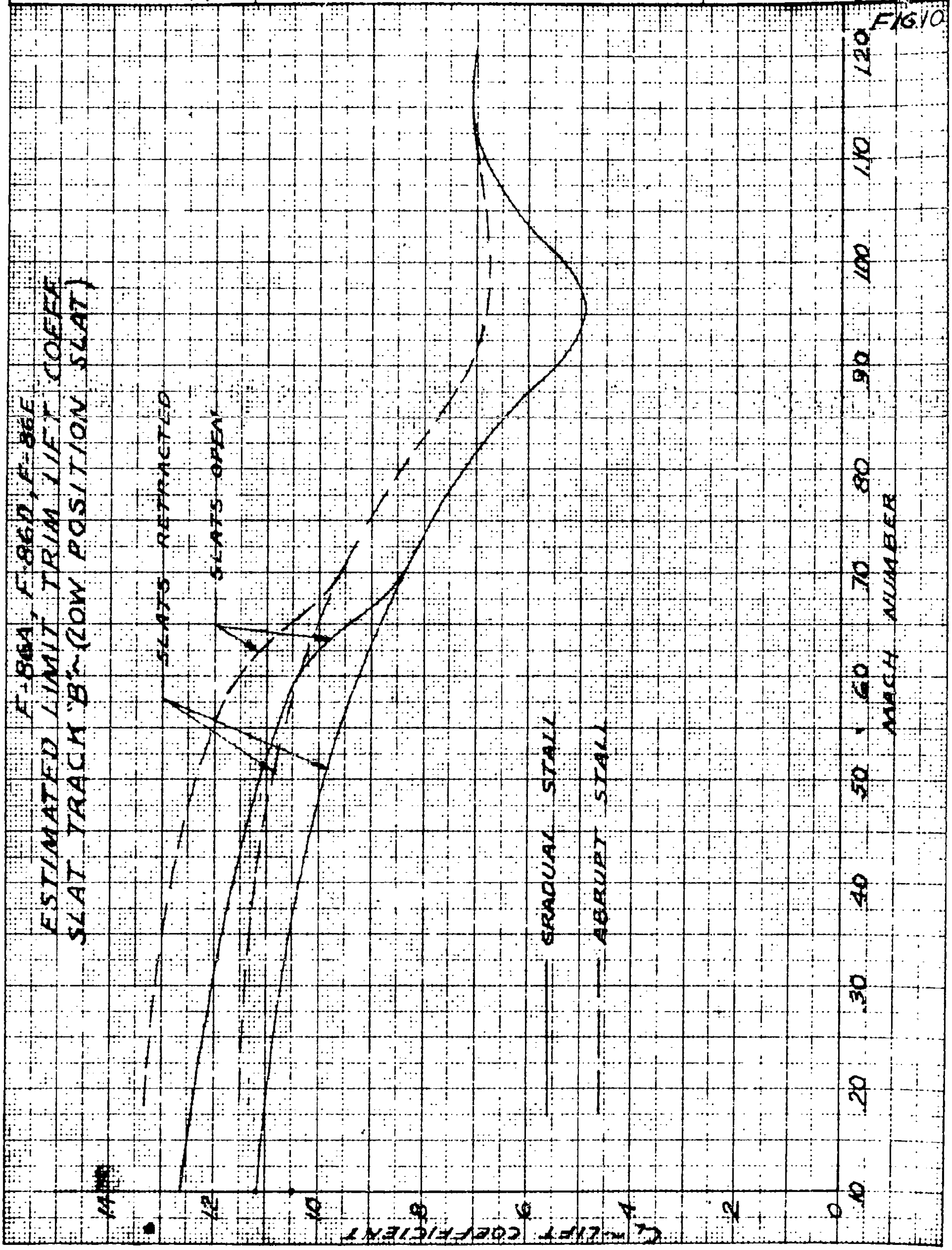

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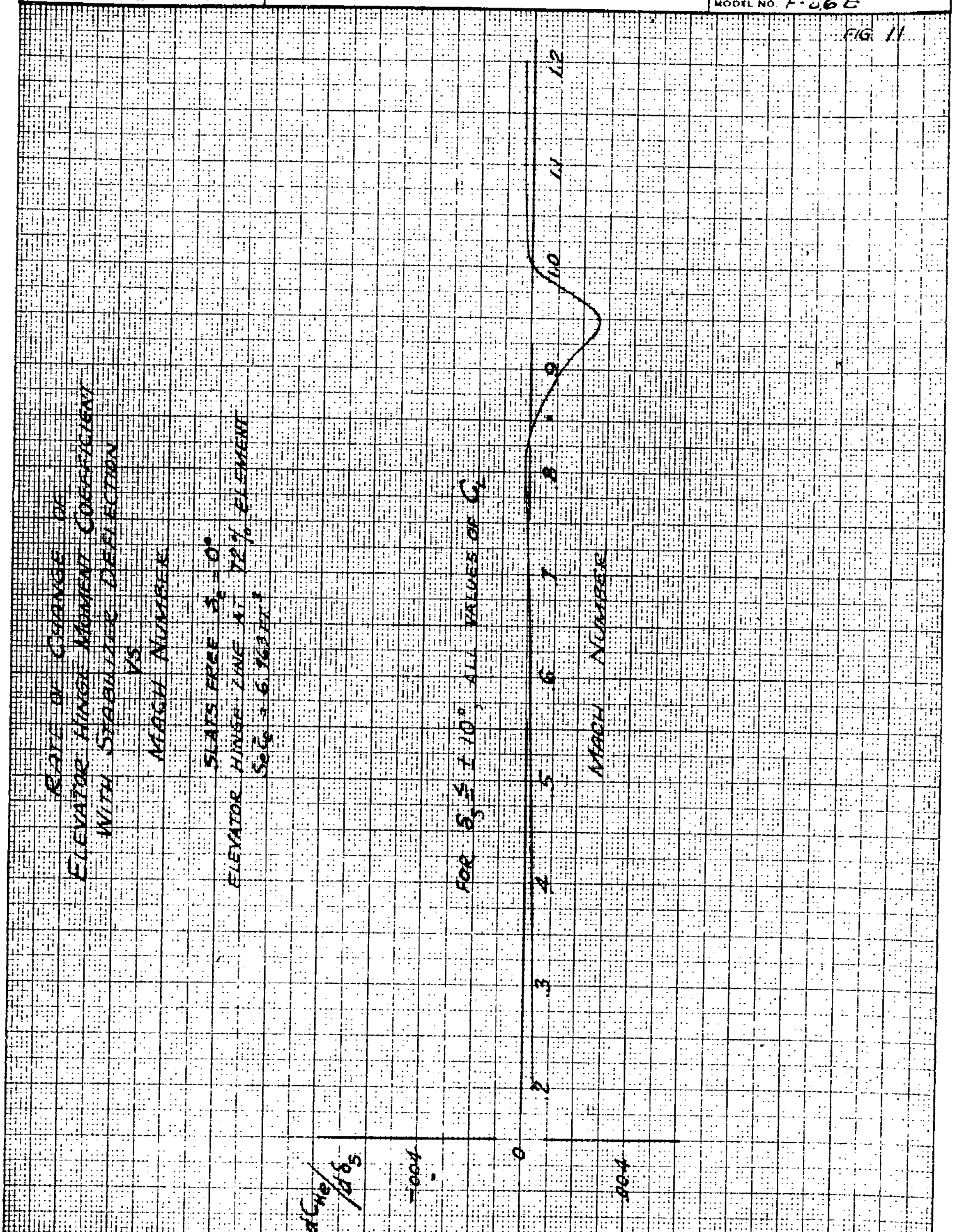
FIG. 11



PREPARED BY: HTC
CHECKED BY: FTG
DATE: 1-20-50

NORTH AMERICAN

ESTIMATED AERODYN

VARIATION OF ELEVATOR
WITH ELEVATOR DE

HINGE LINE AT 72%
SLATS FREE, δ_S =
$S_e \bar{c}_e = 6.563$ ft.^{3}

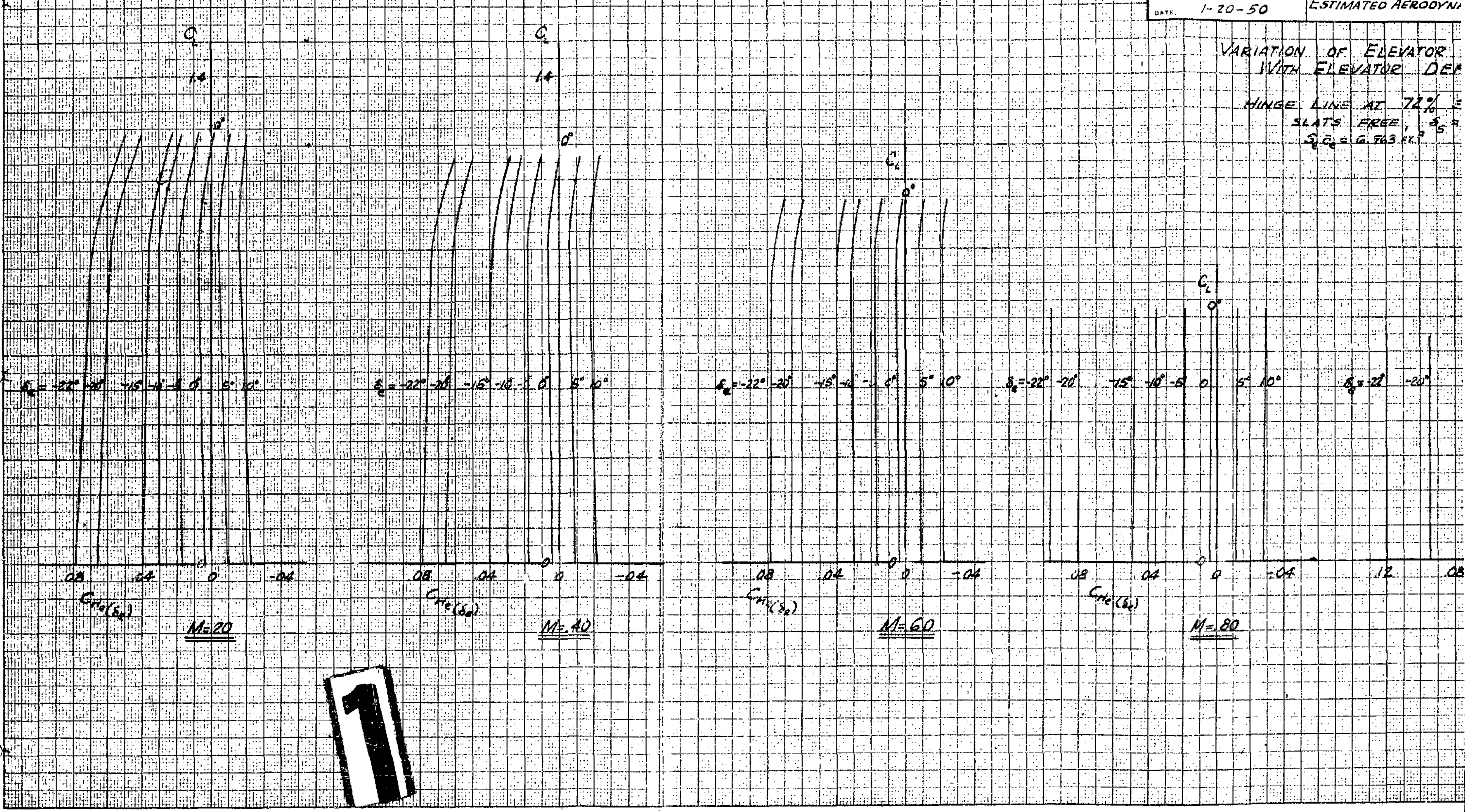
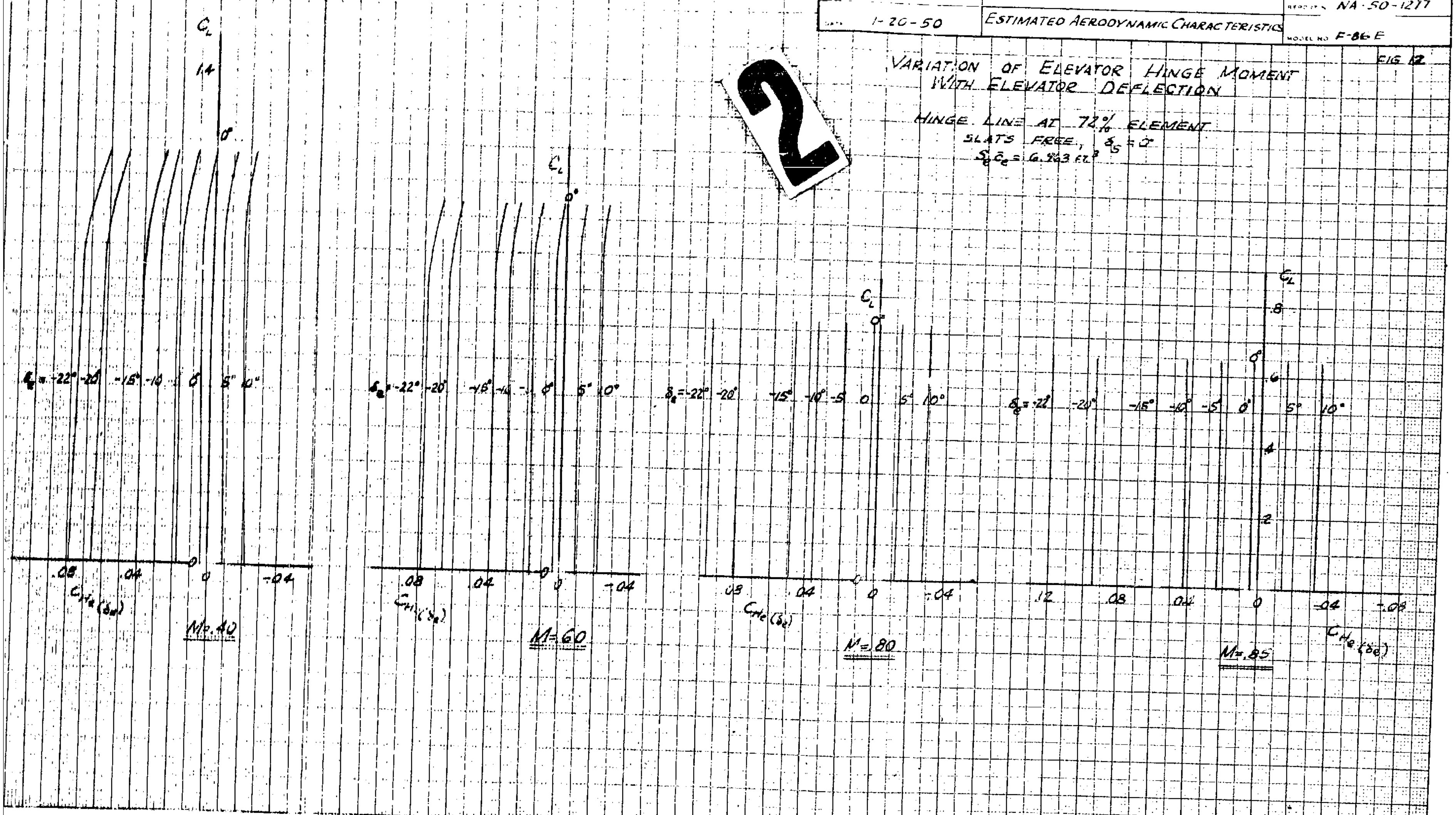


FIG 12

VARIATION OF ELEVATOR HINGE MOMENT WITH ELEVATOR DEFLECTION

HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_S = 0°$
$S_e \bar{c}_e = 6.963$ FT.^{3}



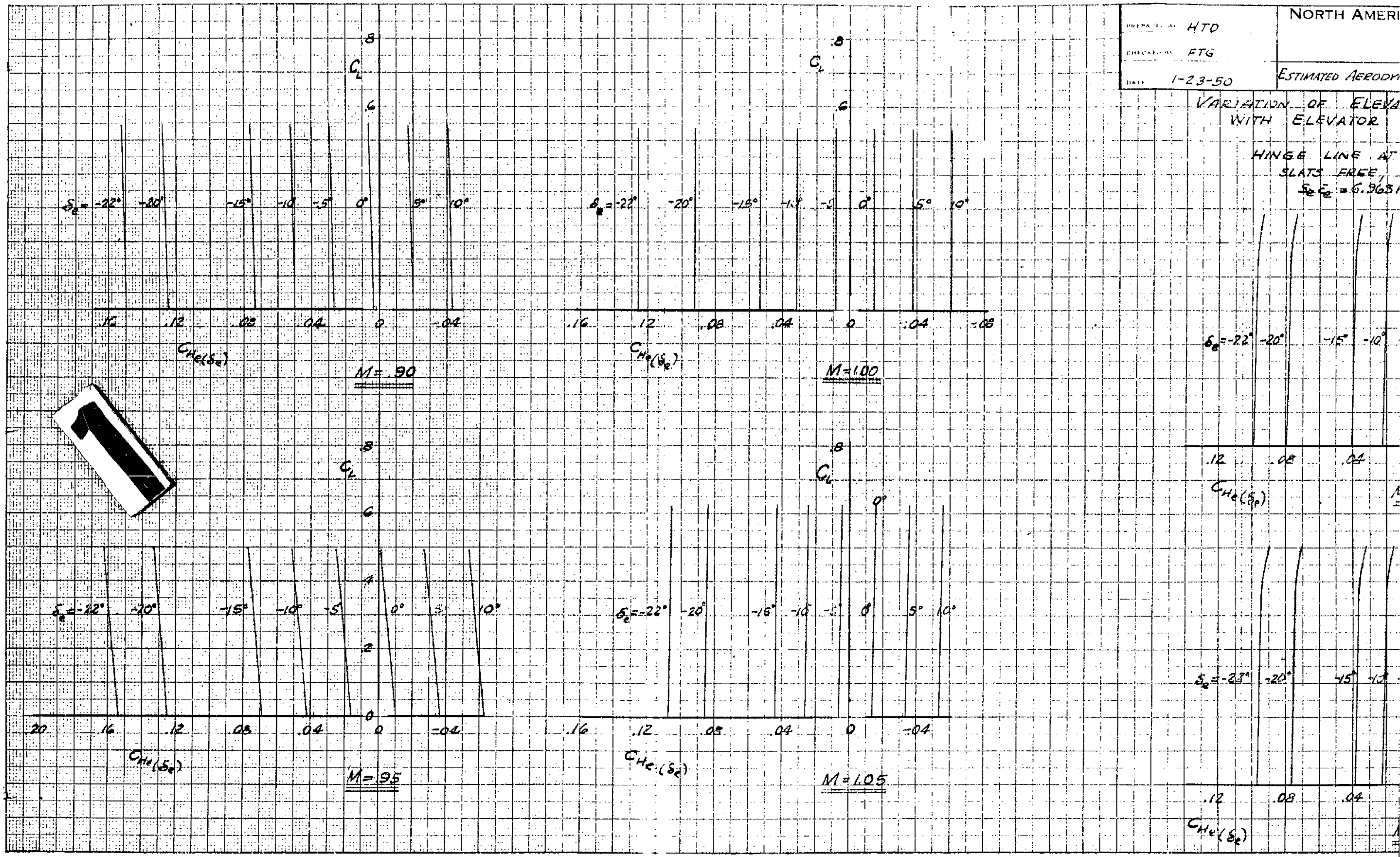
PREPARED BY HTO
CHECKED BY FTG
DATE 1-23-50

NORTH AMERI

ESTIMATED AERODY

VARIATION OF ELEVA
WITH ELEVATOR

HINGE LINE AT
SLATS FREE,
$S_e \bar{c}_e = 6.963$



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VARIATION OF ELEVATOR HINGE MOMENT WITH ELEVATOR DEFLECTION

FIG. 13

HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_s = 0°$
$S_e \bar{c}_e = 6.963\ FT^3$

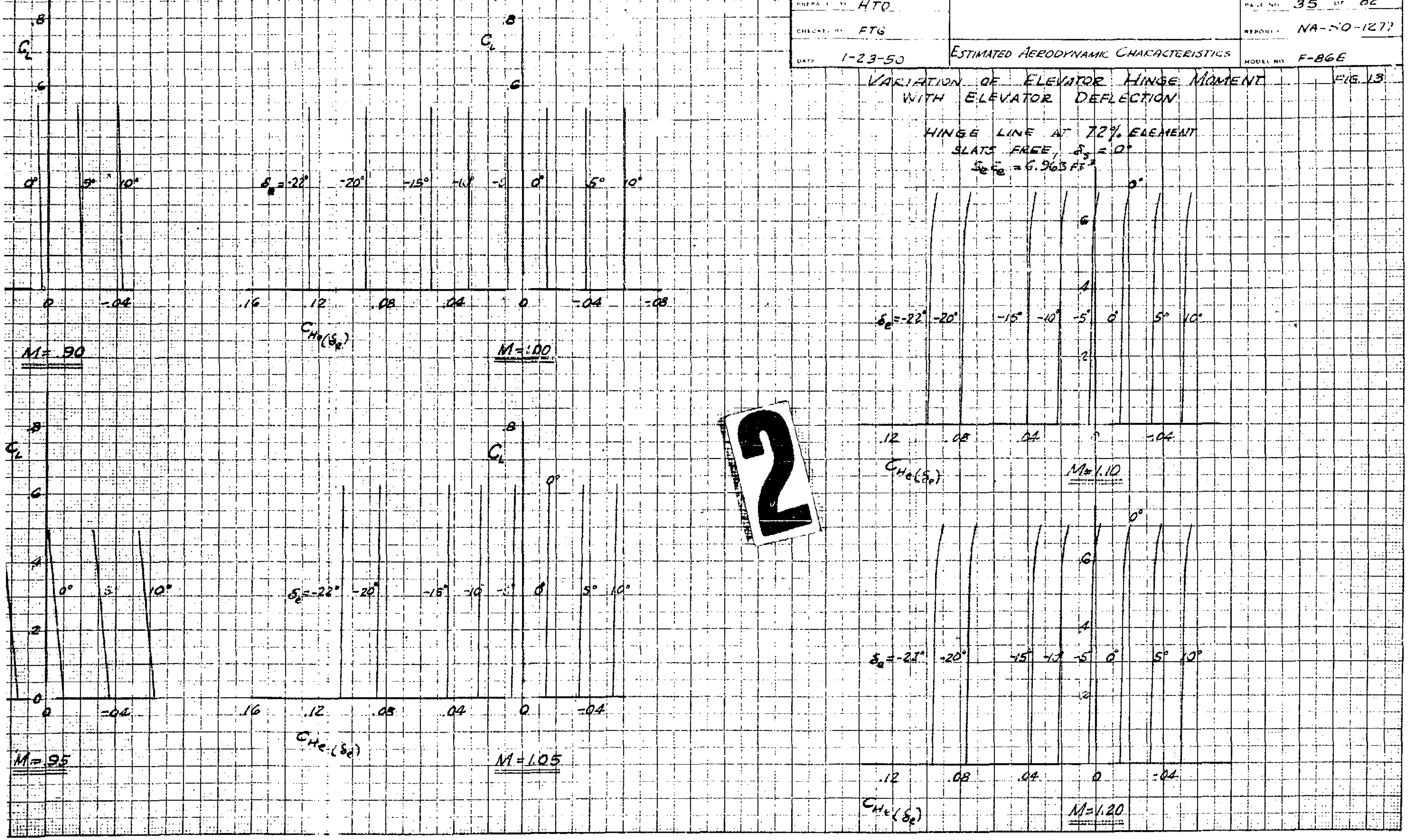

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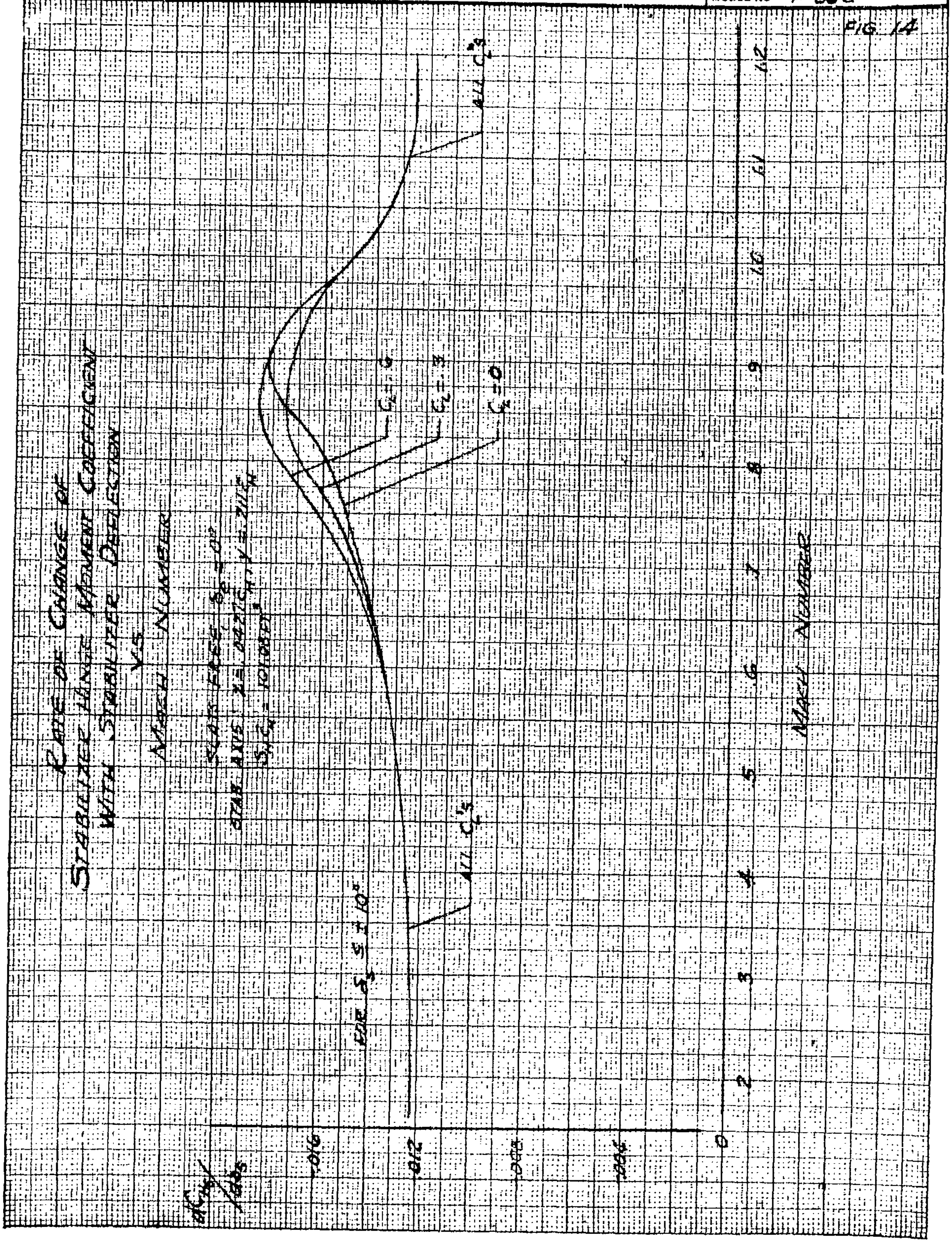
FIG. 14



195-L "ALBANENE" TRACING PAPER—K. & E. CO., N. Y.—REG.U.S. PAT.OFF.

PREPARED BY HTD

CHECKED BY FTG

DATE: 1-18-50

NORTH AMERI

ESTIMATED AERODY

VARIATION OF STABILIZ
WITH ELEVATOR

ELEVATOR HINGE LINE
SLATS FREE, δ_s = 0
$S_H \bar{c}_H$ = 10.08 FT.³

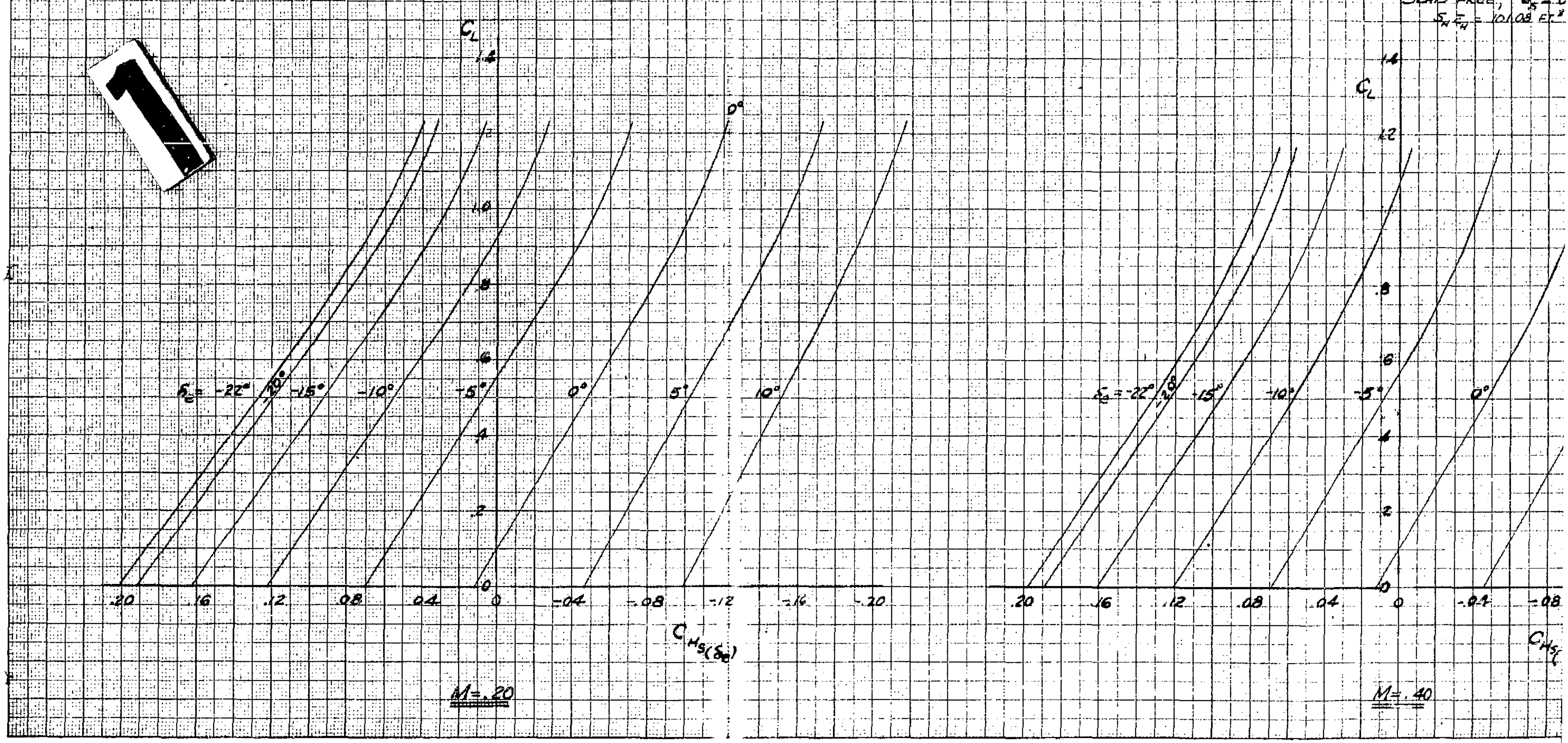
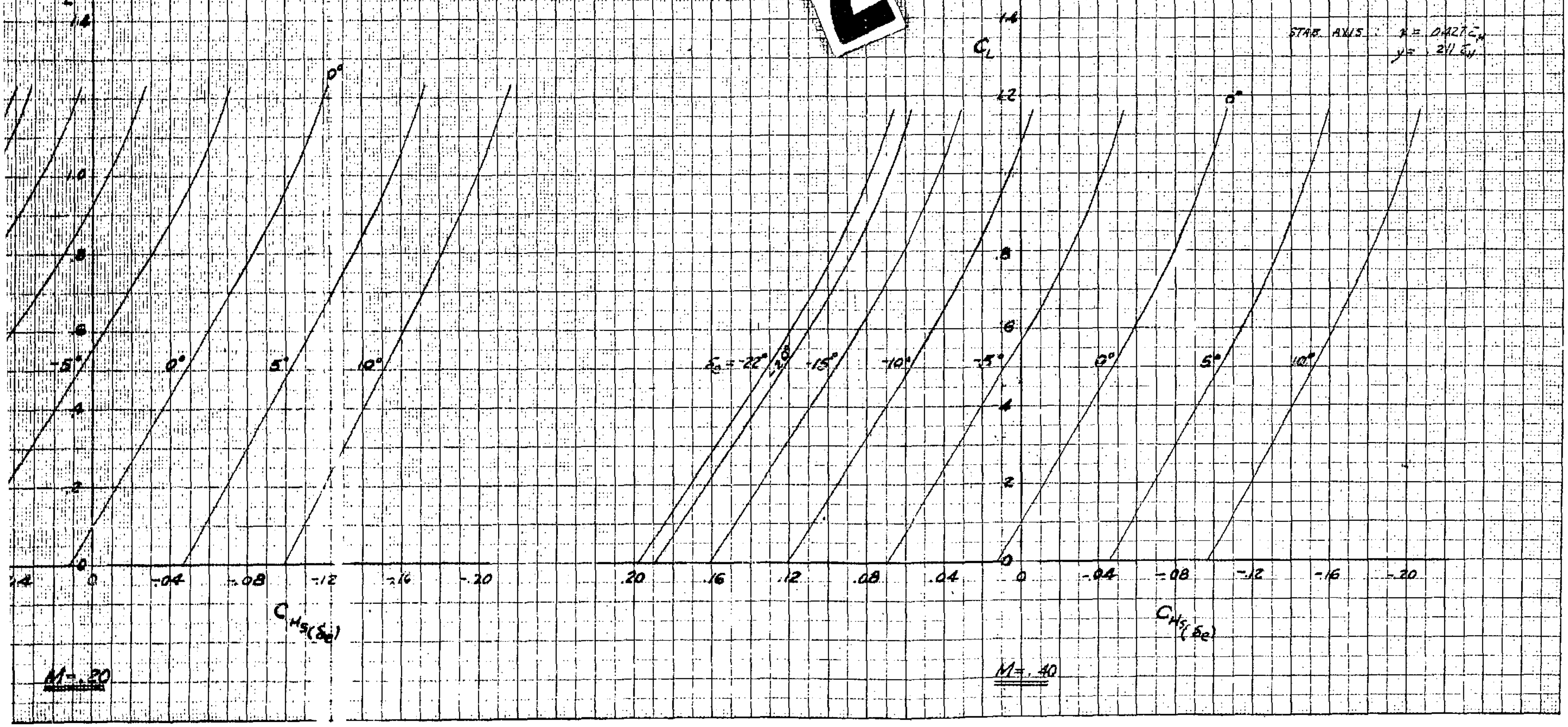


FIG. 15

VARIATION OF STABILIZER HINGE MOMENT WITH ELEVATOR DEFLECTION

ELEVATOR HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_s = 0°$
$S_H \bar{c}_H = 101.08$ FT^3



PREPARED BY HTO		NORTH AMERICAN A
CHECKED BY FTG		
DATE: 1-19-50		ESTIMATED AERODYNAMIC (

VARIATION OF STABILIZER
WITH ELEVATOR DE

ELEVATOR HINGE LINE AT 7
SLATS FREE, $\delta_S = 0°$
$S_H \bar{c}_H = 101.08$ FT^3

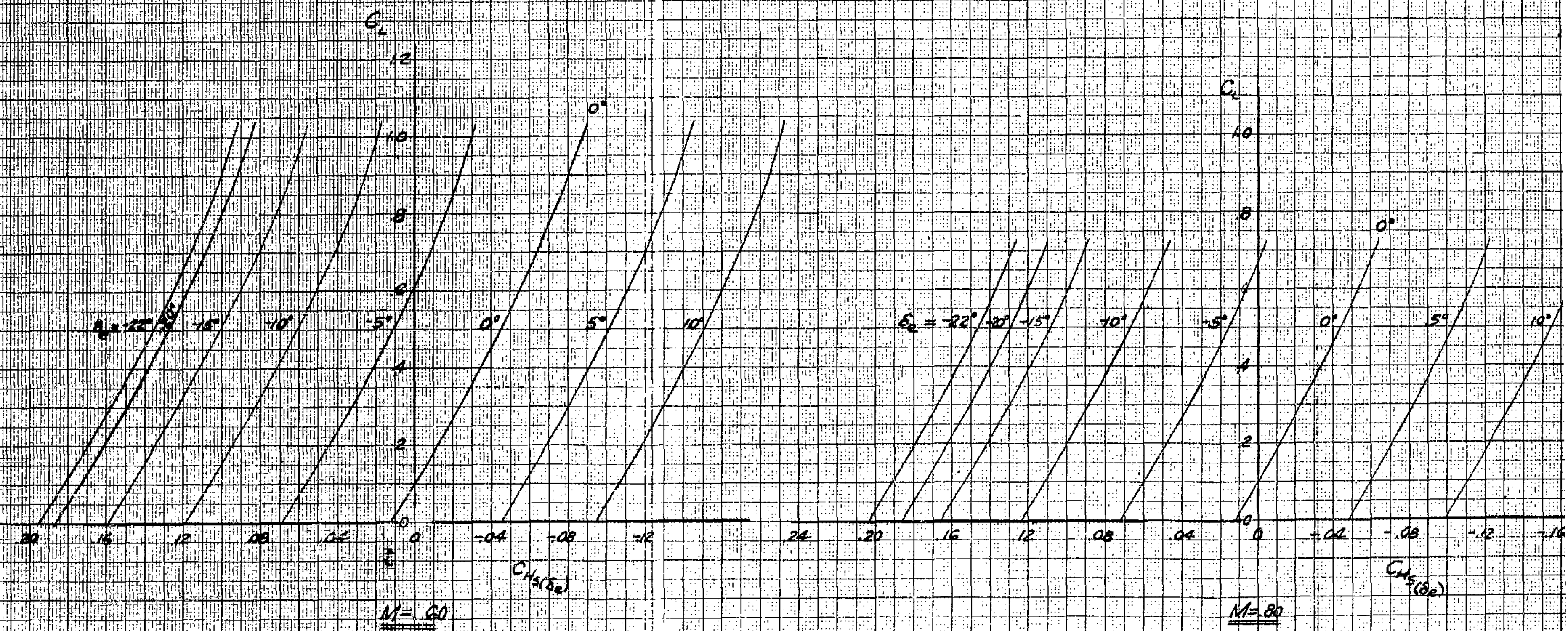
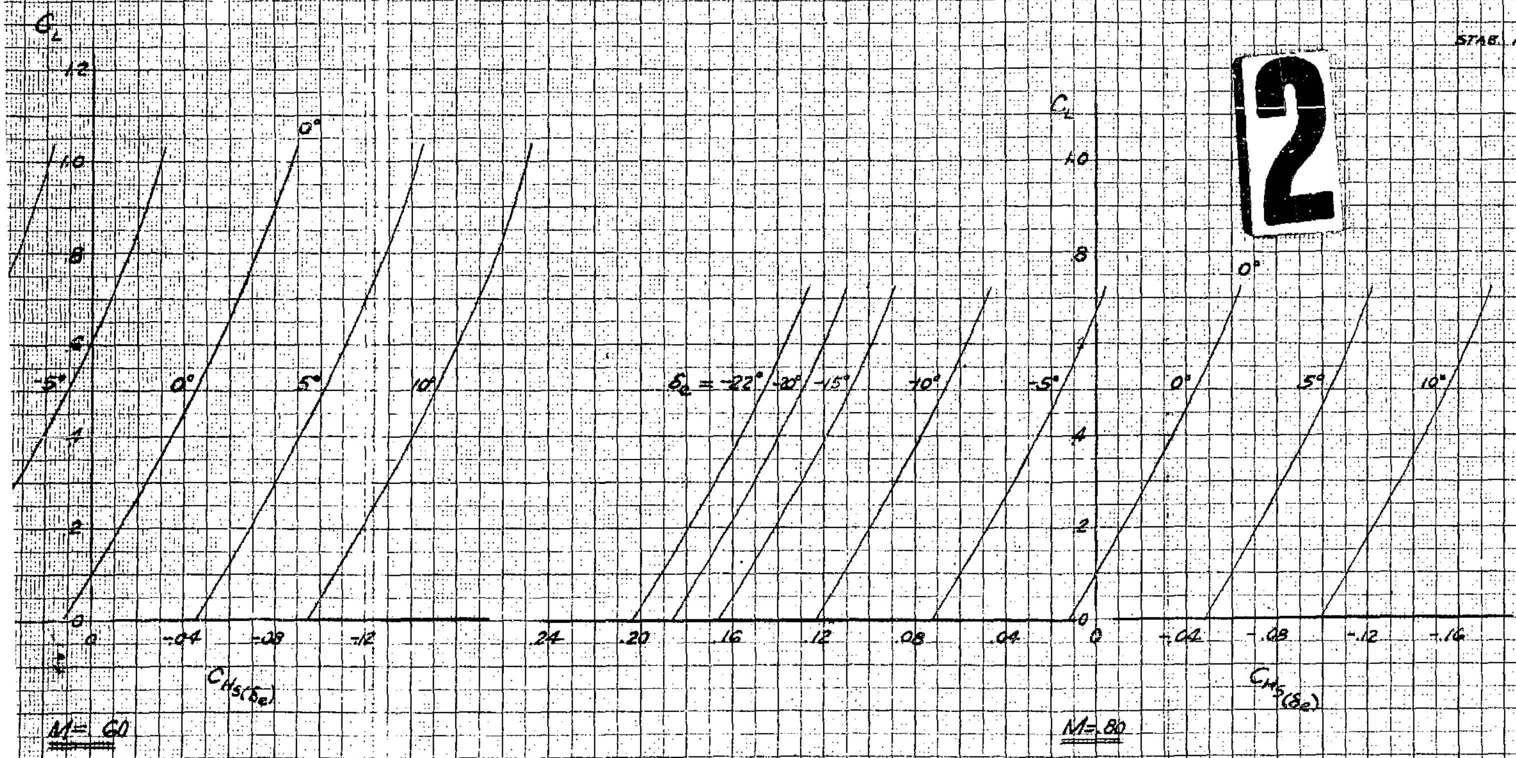


FIG. 16

VARIATION OF STABILIZER HINGE MOMENT WITH ELEVATOR DEFLECTION

ELEVATOR HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_S = 0°$
$S_H \bar{c}_H = 101.08\ FT^3$

STAB. AXIS: $x = .0427\ \bar{c}_H$
$y = .211\ \bar{c}_H$



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PREPARED BY HTO

CHECKED BY FTG

DATE: 1-19-50

ESTIMATED AERODYNAMIC

VARIATION OF STABILIZER
WITH ELEVATOR DEFL

ELEVATOR HINGE LINE AT 72
SLATS FREE, $\delta_s = 0$

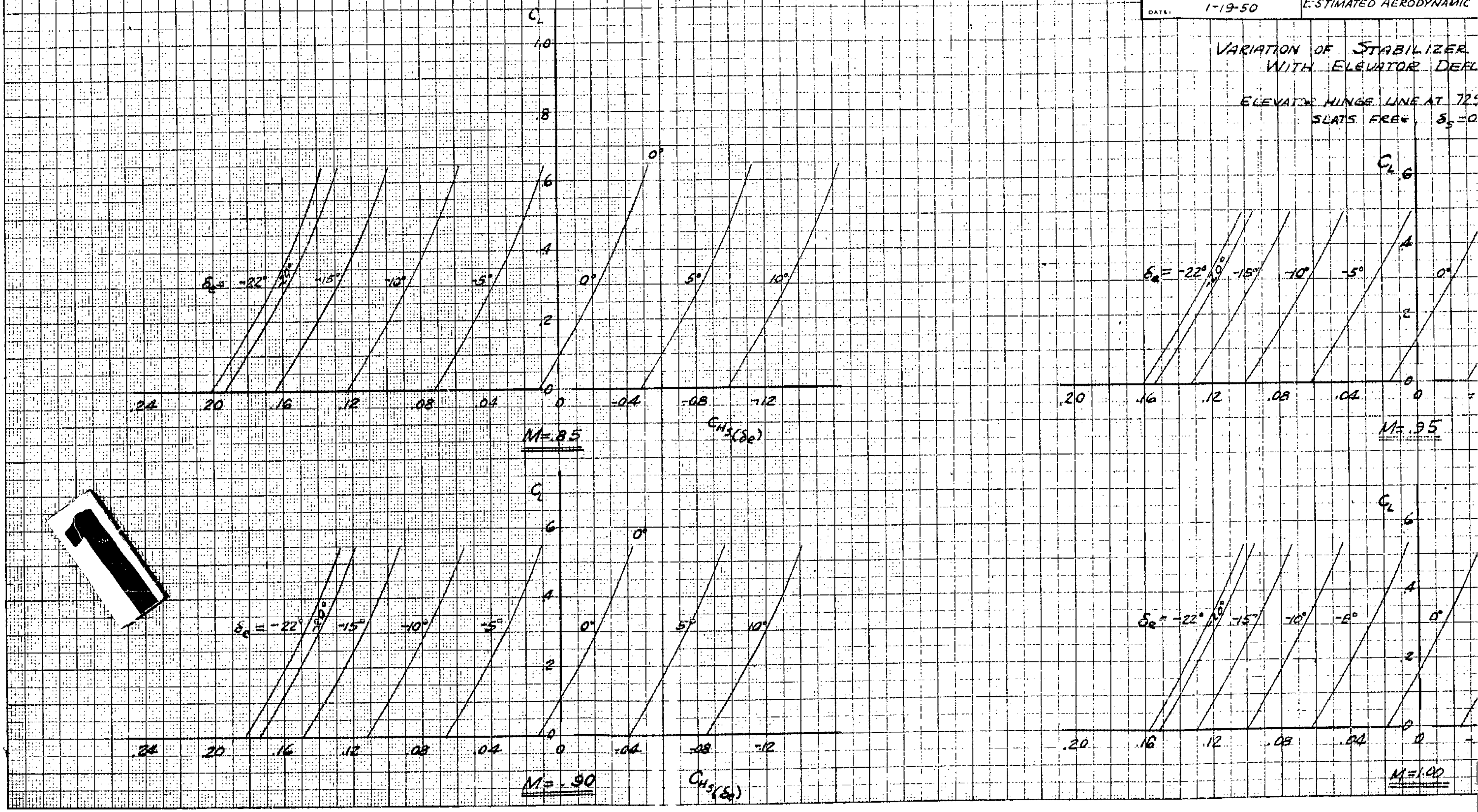

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FIG. 17

VARIATION OF STABILIZER HINGE MOMENT WITH ELEVATOR DEFLECTION

ELEVATOR HINGE LINE AT 72% ELEMENT

SLATS FREE, $\delta_s = 0°$

$S_H \bar{c}_H = 101.08\ FT^3$

STAB. AXIS:

$z = .0427\ \bar{c}_H$

$x = .211\ \bar{c}_H$

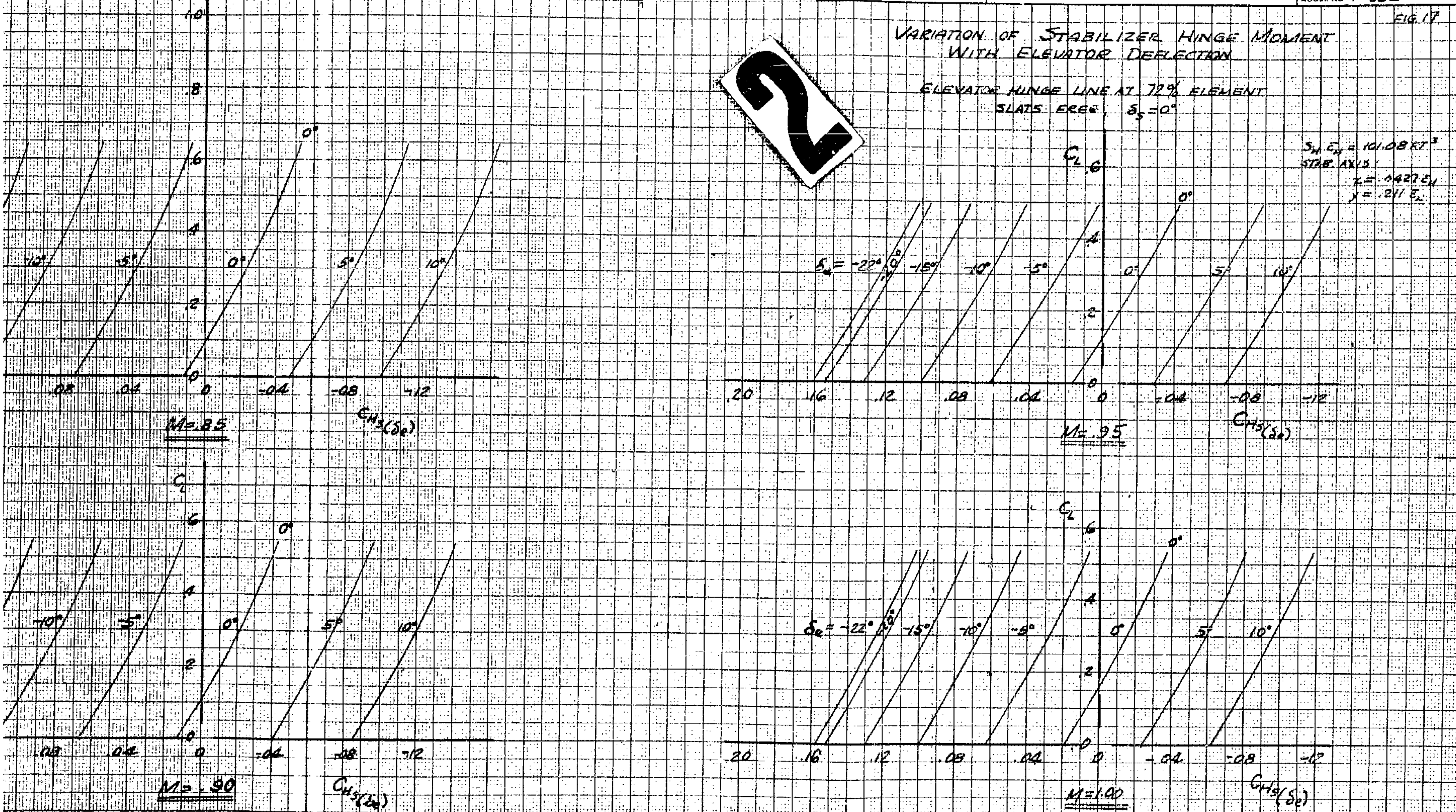

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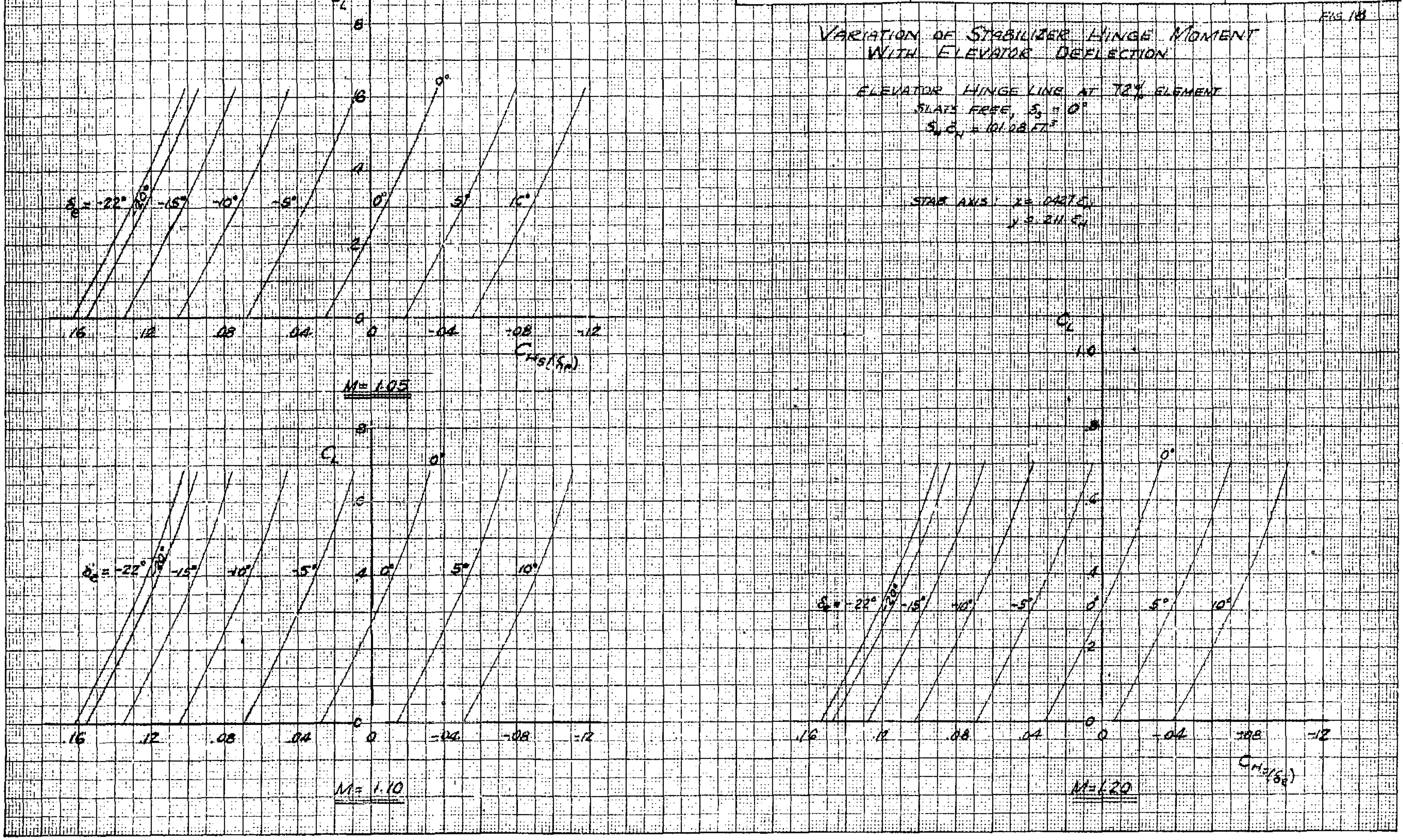
FIG. 18

VARIATION OF STABILIZER HINGE MOMENT
WITH ELEVATOR DEFLECTION

ELEVATOR HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_S = 0°$
$S_H \bar{c}_H = 101.08\ FT^3$

STAB. AXIS: $x = .0427\,\bar{c}_H$
$y = .211\,\bar{c}_H$



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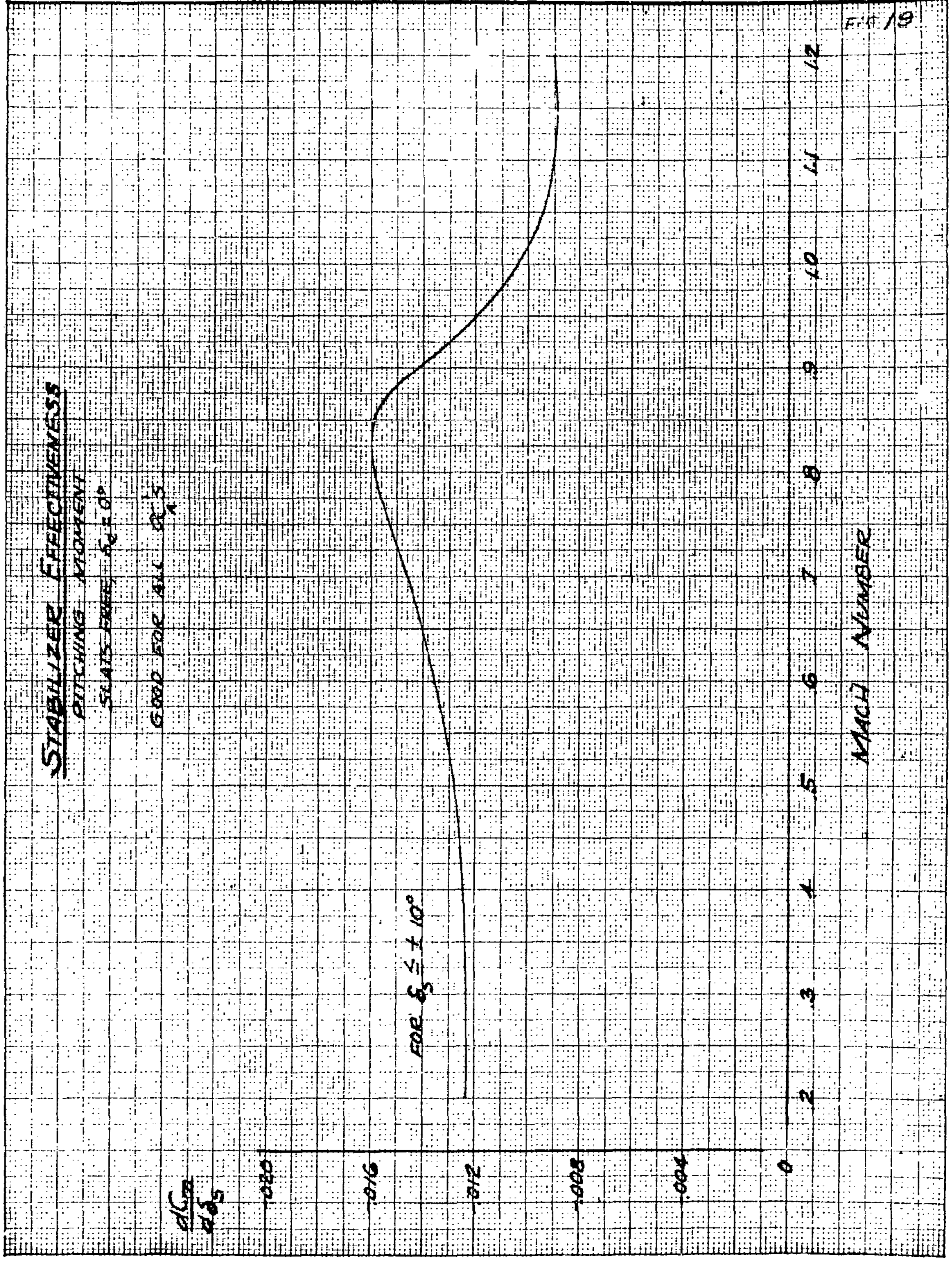

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CHECKED BY ETG	
DATE 1-20-50	ESTIMATED AERODYNAM

ELEVATOR E

PITCHING

HINGE LINE AT

SLATS FR

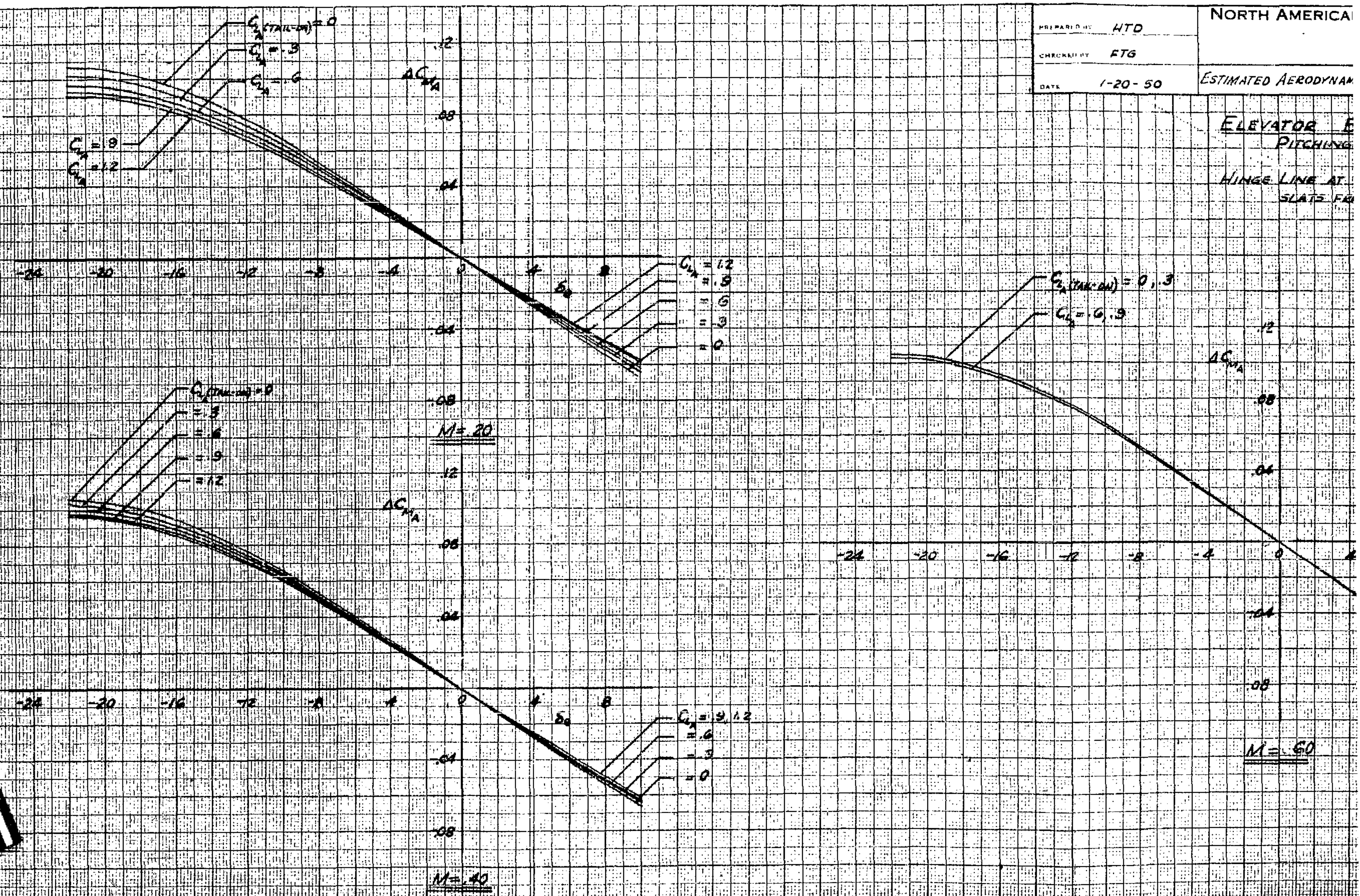

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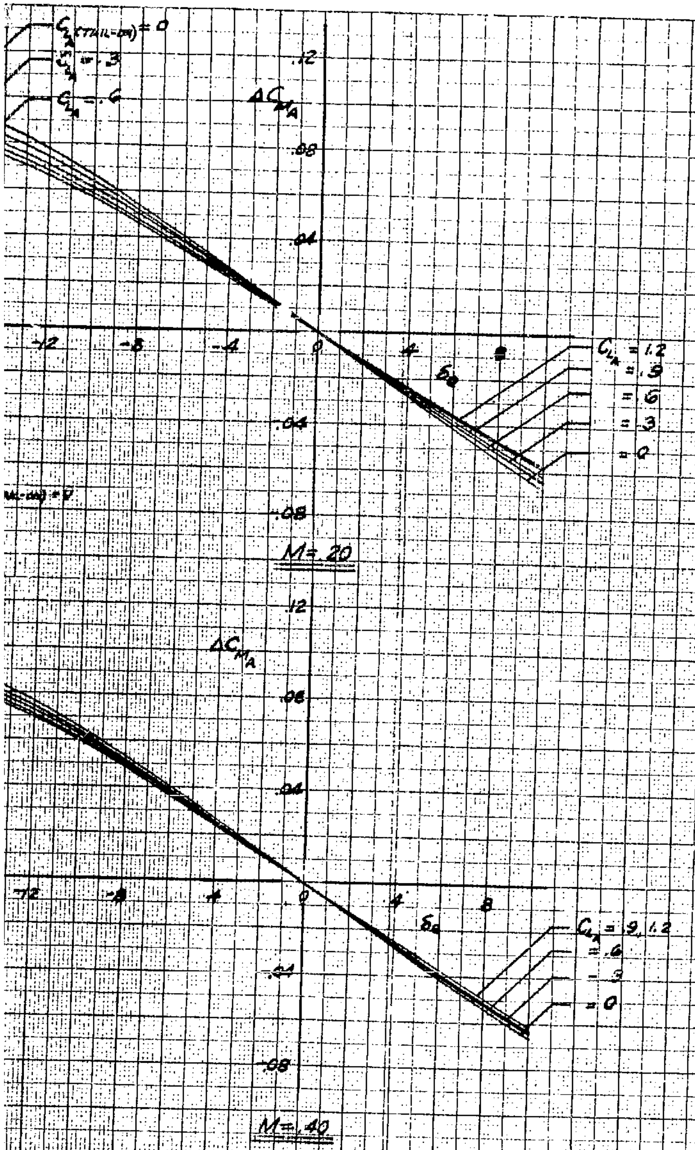
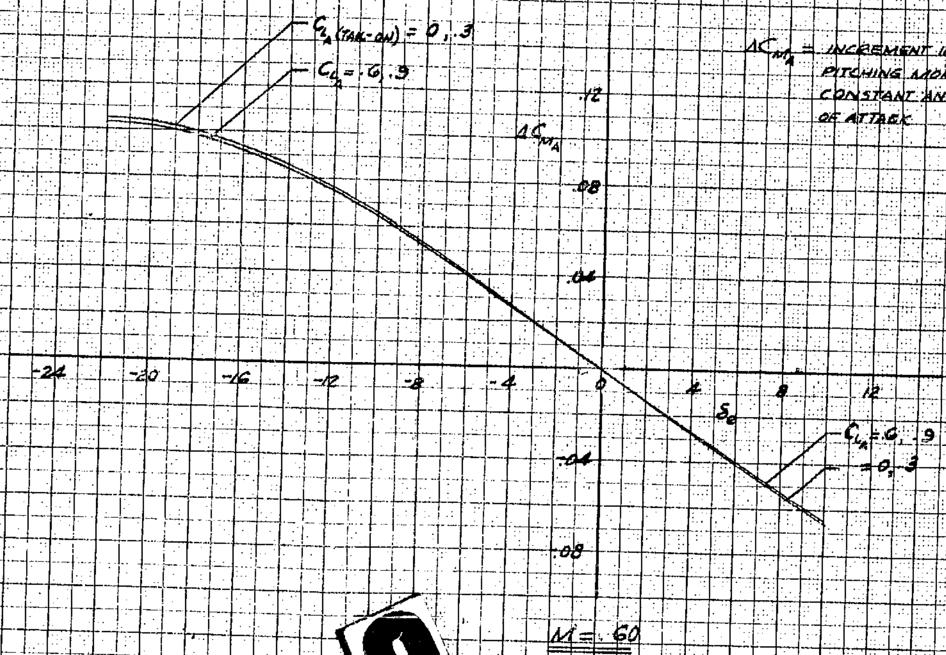
FIG. 20

ELEVATOR EFFECTIVENESS
PITCHING MOMENT

HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_S = 0°$

ΔC_{M_A} = INCREMENT IN AIRPLANE PITCHING MOMENT AT CONSTANT ANGLES OF ATTACK





PREPARED BY HTP
CHECKED BY FTG
DATE 1-20-50

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ESTIMATED AER

ELEVATOR
PITCH

HINGE LIN
SLAT

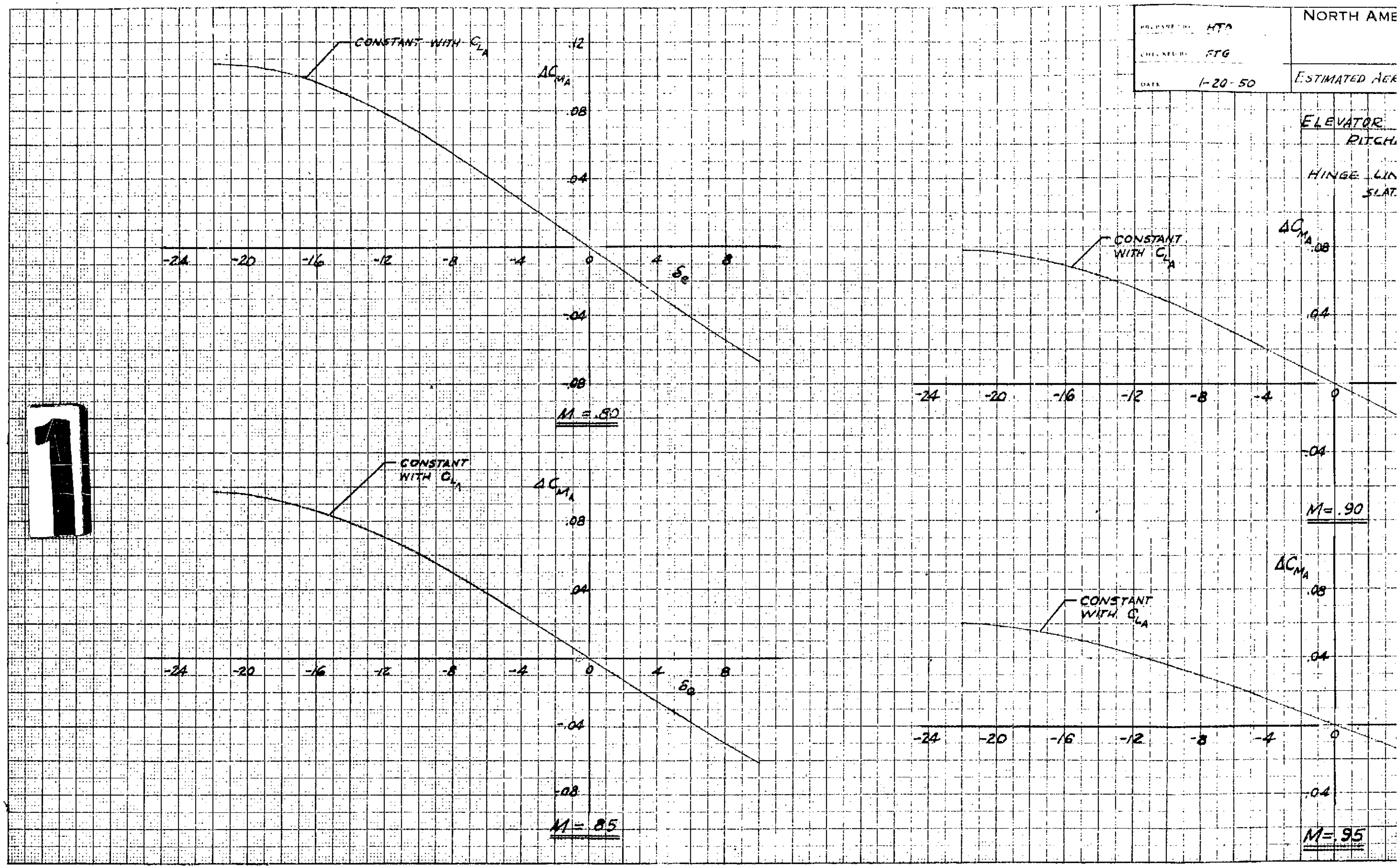

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FIG. 21

ELEVATOR EFFECTIVENESS
PITCHING MOMENT

HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_s = 0°$

ΔC_{M_A} = INCREMENT IN AIRPLANE PITCHING MOMENT AT CONSTANT ANGLES OF ATTACK

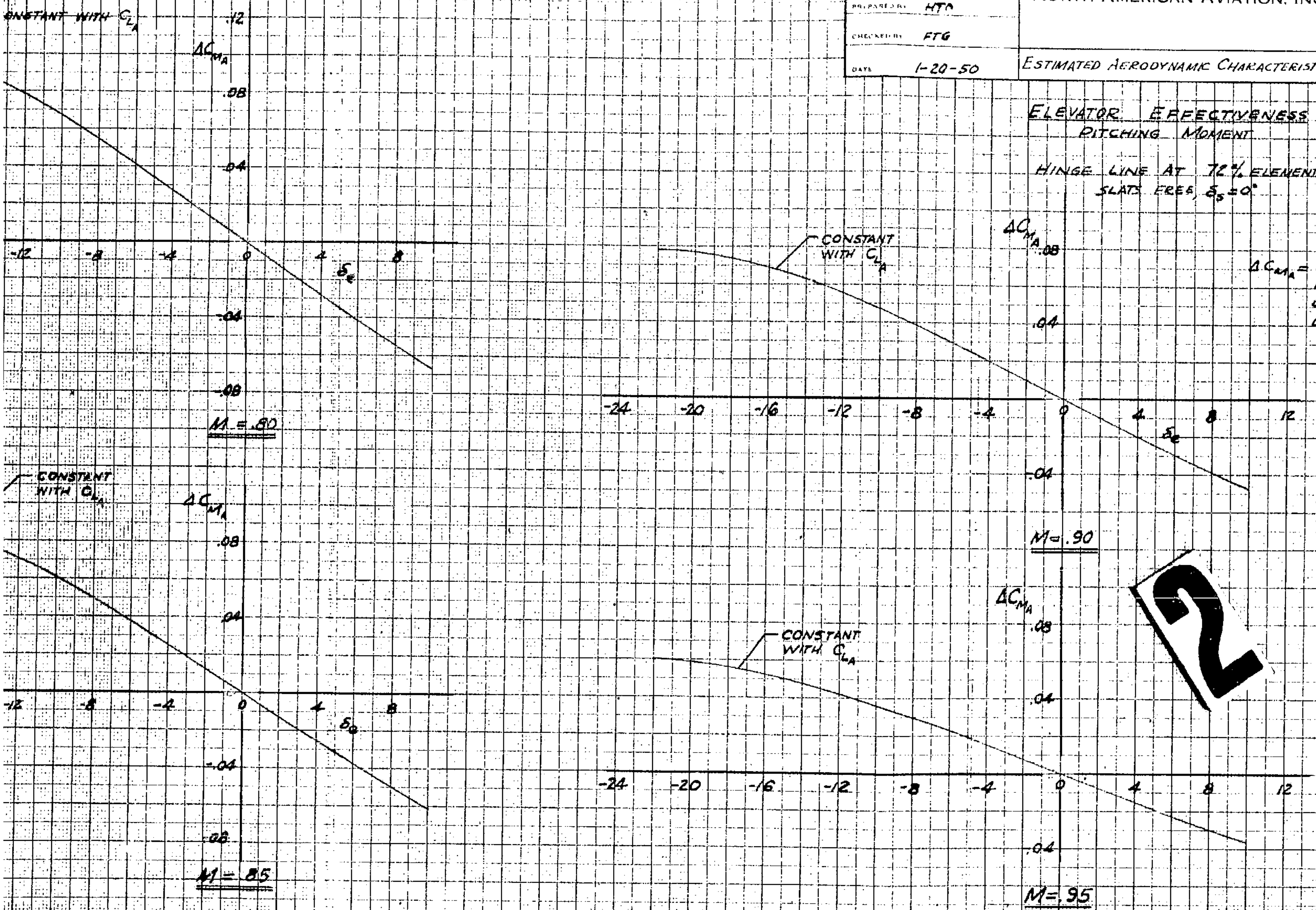

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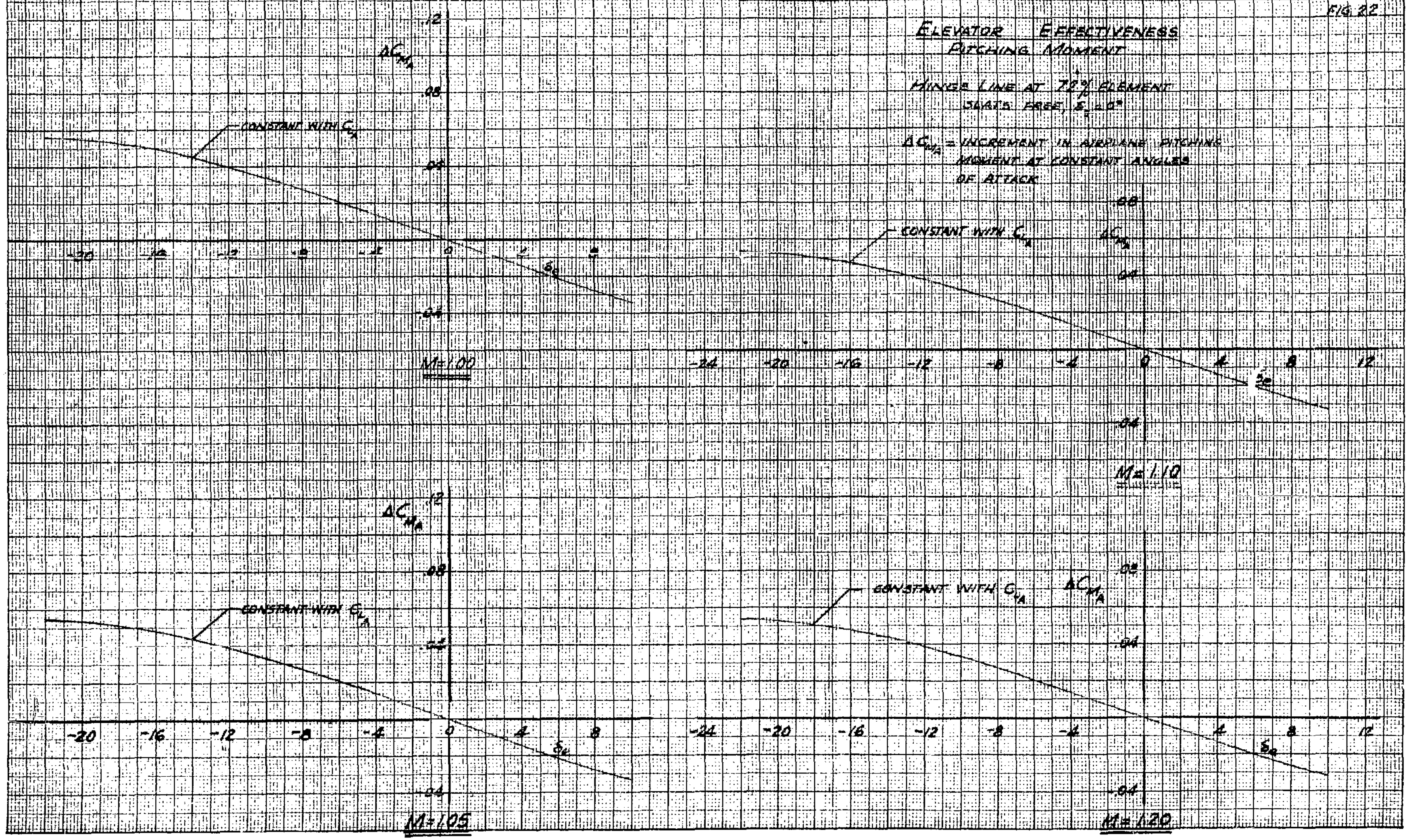
FIG. 22

ELEVATOR EFFECTIVENESS
PITCHING MOMENT

HINGE LINE AT 72% ELEMENT
SLATS FREE, $\delta_t = 0°$

ΔC_{M_A} = INCREMENT IN AIRPLANE PITCHING MOMENT AT CONSTANT ANGLES OF ATTACK



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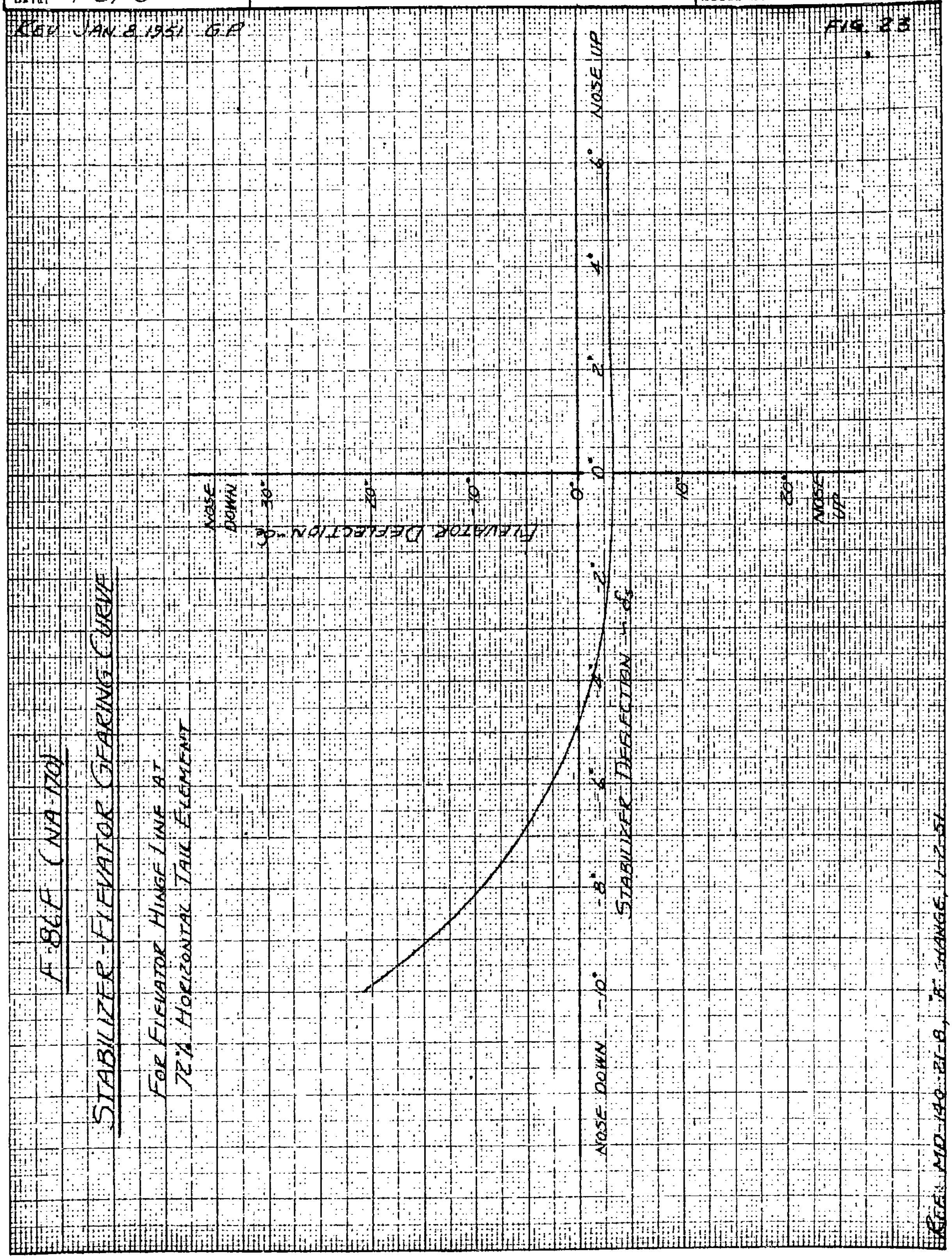
REV JAN 8 1951 G.P.

FIG. 23



PREPARED BY: PES
CHECKED BY: LPG
DATE: 2-11-48

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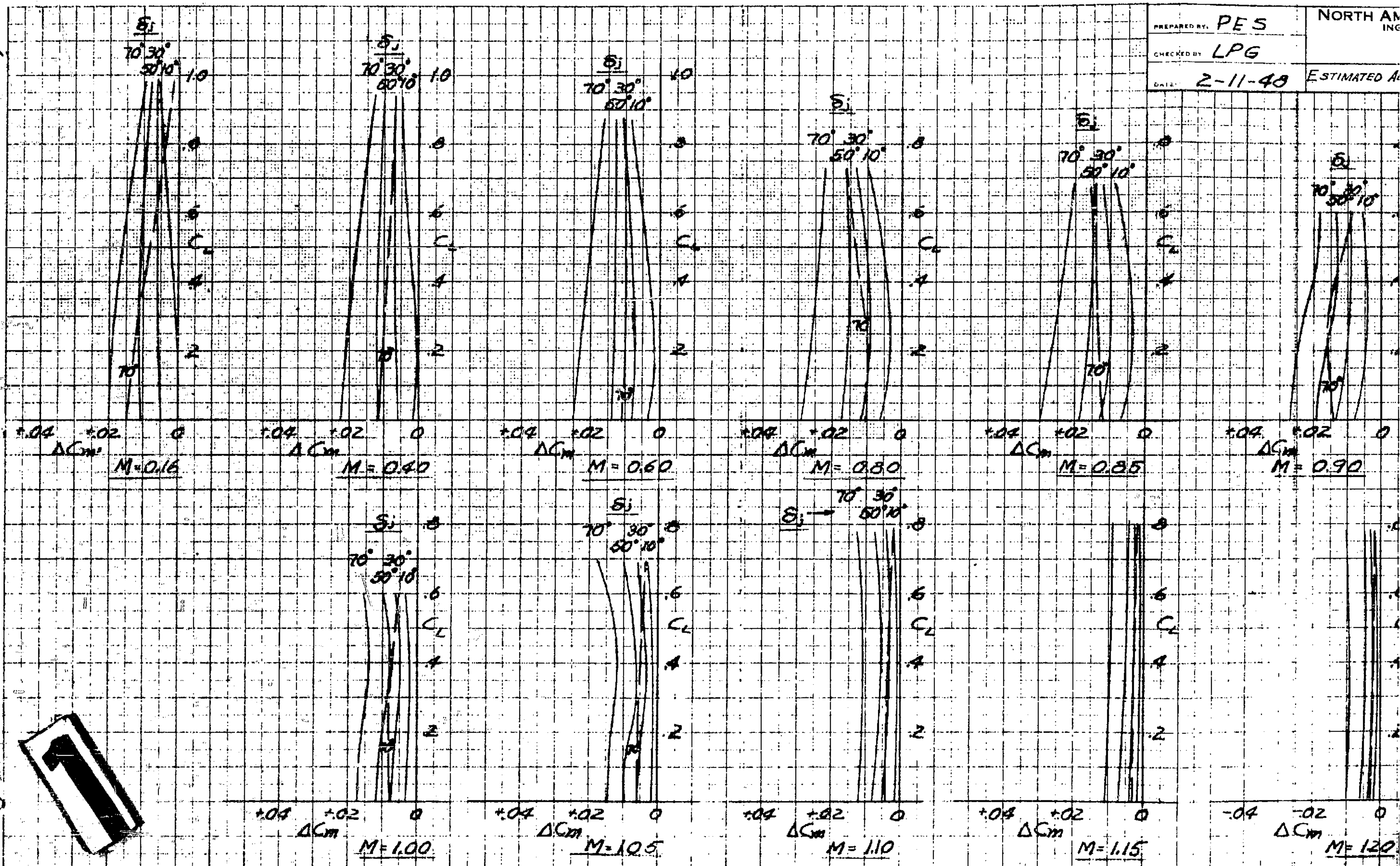
INC

ESTIMATED A[...]



PREPARED BY: PES | CHECKED BY: LPG | DATE: 2-11-48

NORTH AMERICAN AVIATION, INC.
INGLEWOOD, CALIFORNIA

ESTIMATED AERODYNAMIC CHARACTERISTICS

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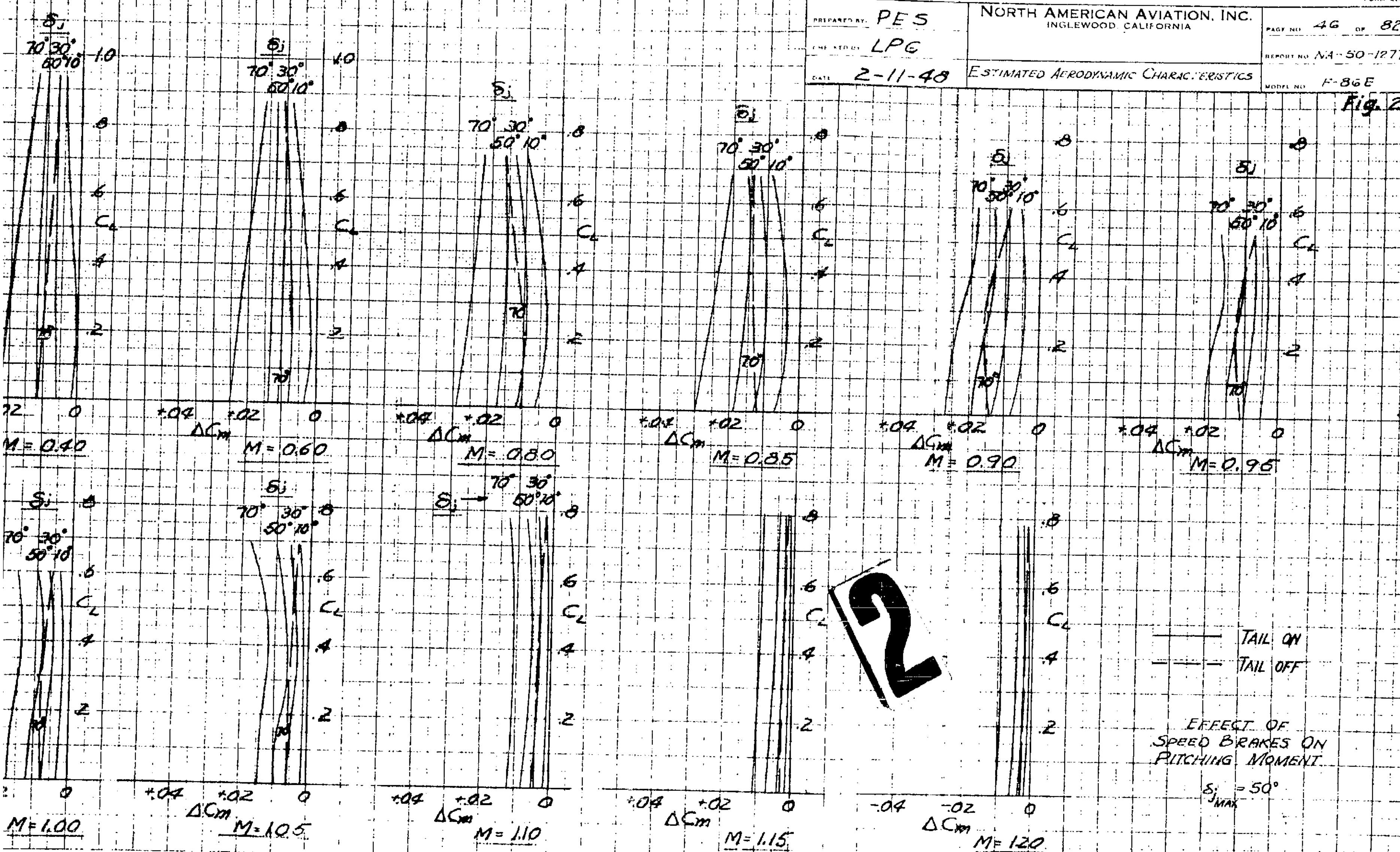
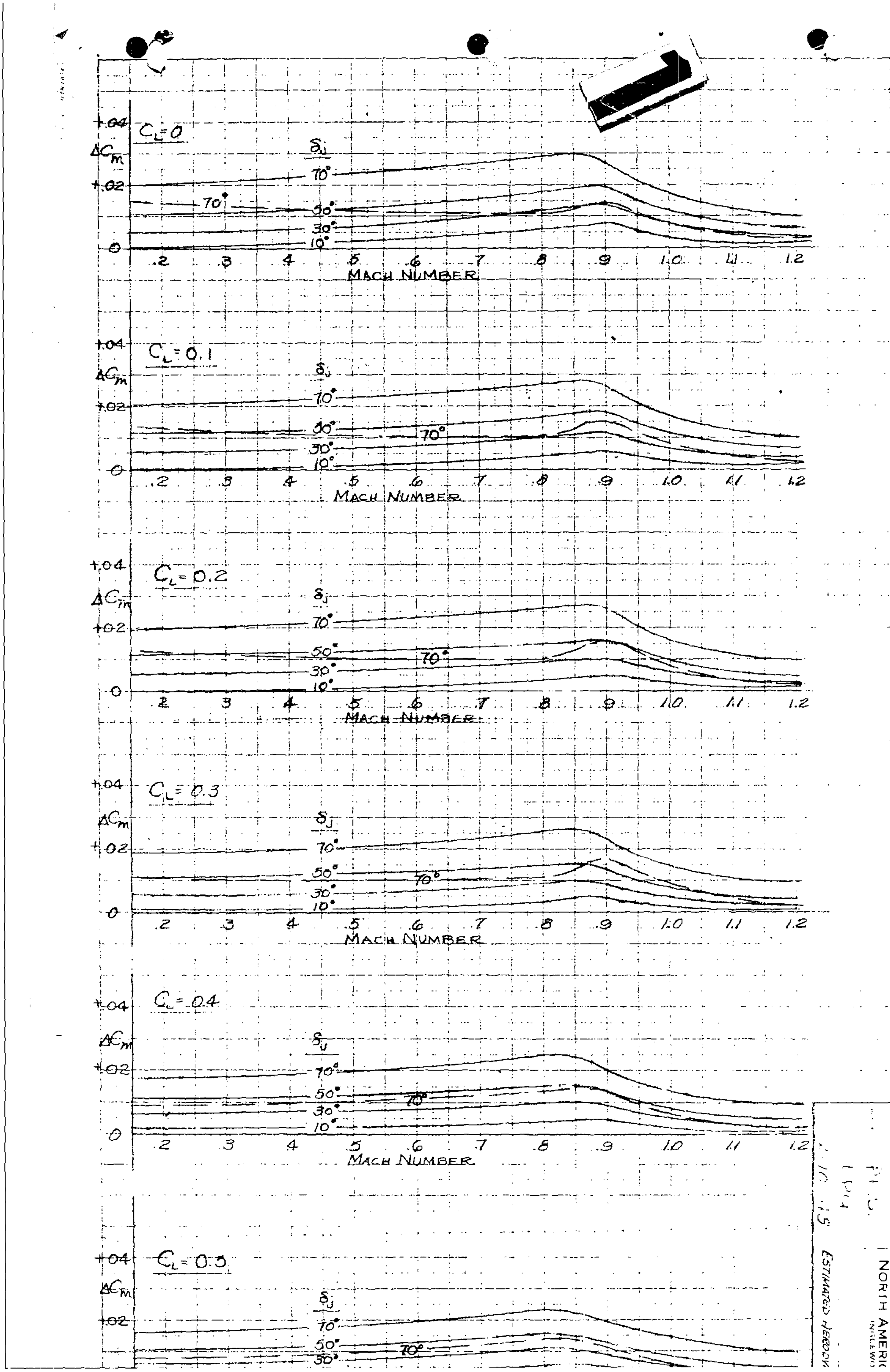


Fig. 24

EFFECT OF SPEED BRAKES ON PITCHING MOMENT

$\delta_{j_{MAX}} = 50°$



$C_L = 0$
$C_L = 0.1$
$C_L = 0.2$
$C_L = 0.3$
$C_L = 0.4$
$C_L = 0.5$
ΔC_m
δ_j
70°
50°
30°
10°
+.04
+.02
0
.2 .3 .4 .5 .6 .7 .8 .9 1.0 1.1 1.2
MACH NUMBER
NORTH AMERIC
ESTIMATED AERODY

P.E.S. L.P.G. 2-10-48	NORTH AMERICAN AVIATION, INC. INGLEWOOD CALIFORNIA	Page 47 of 82
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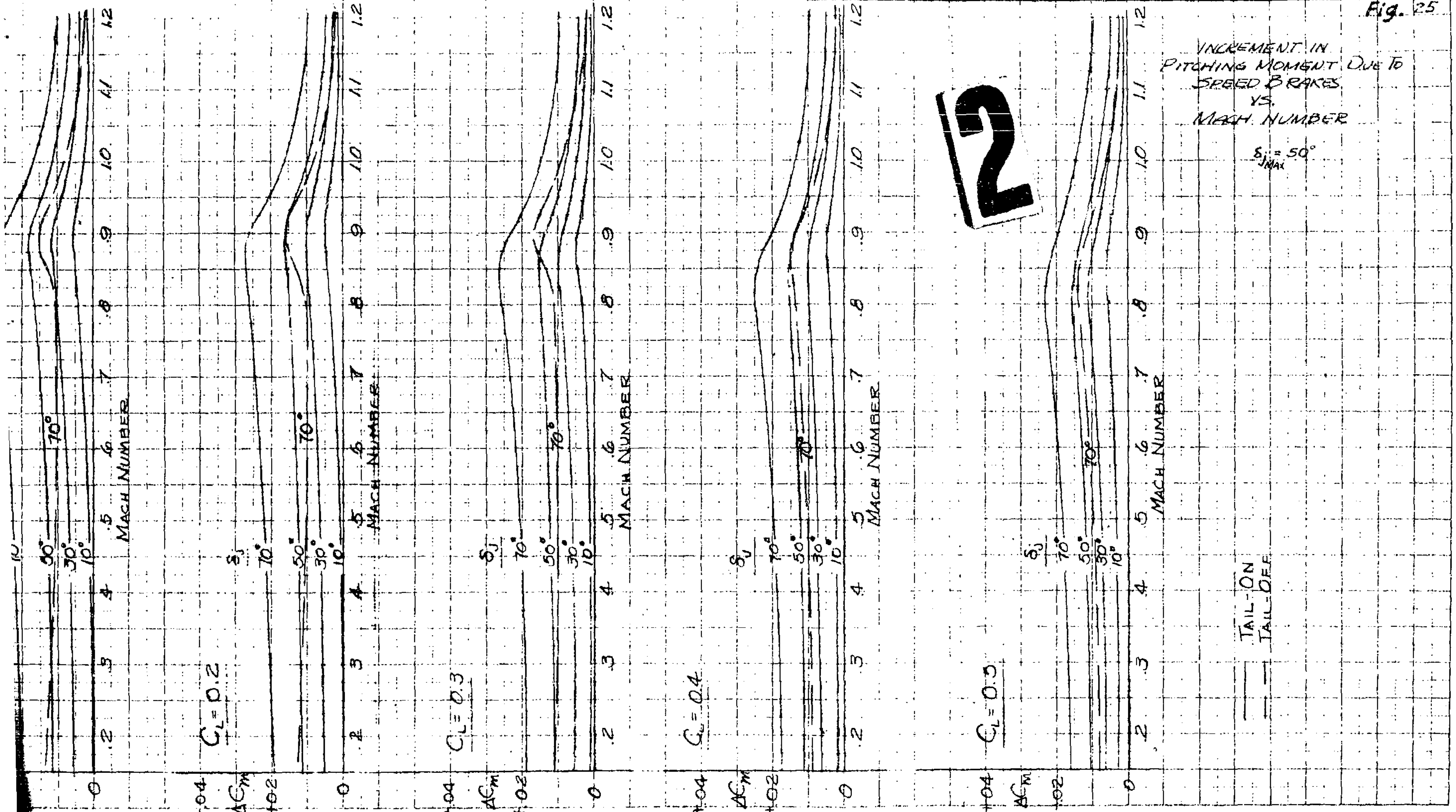
		F-86E

Fig. 25

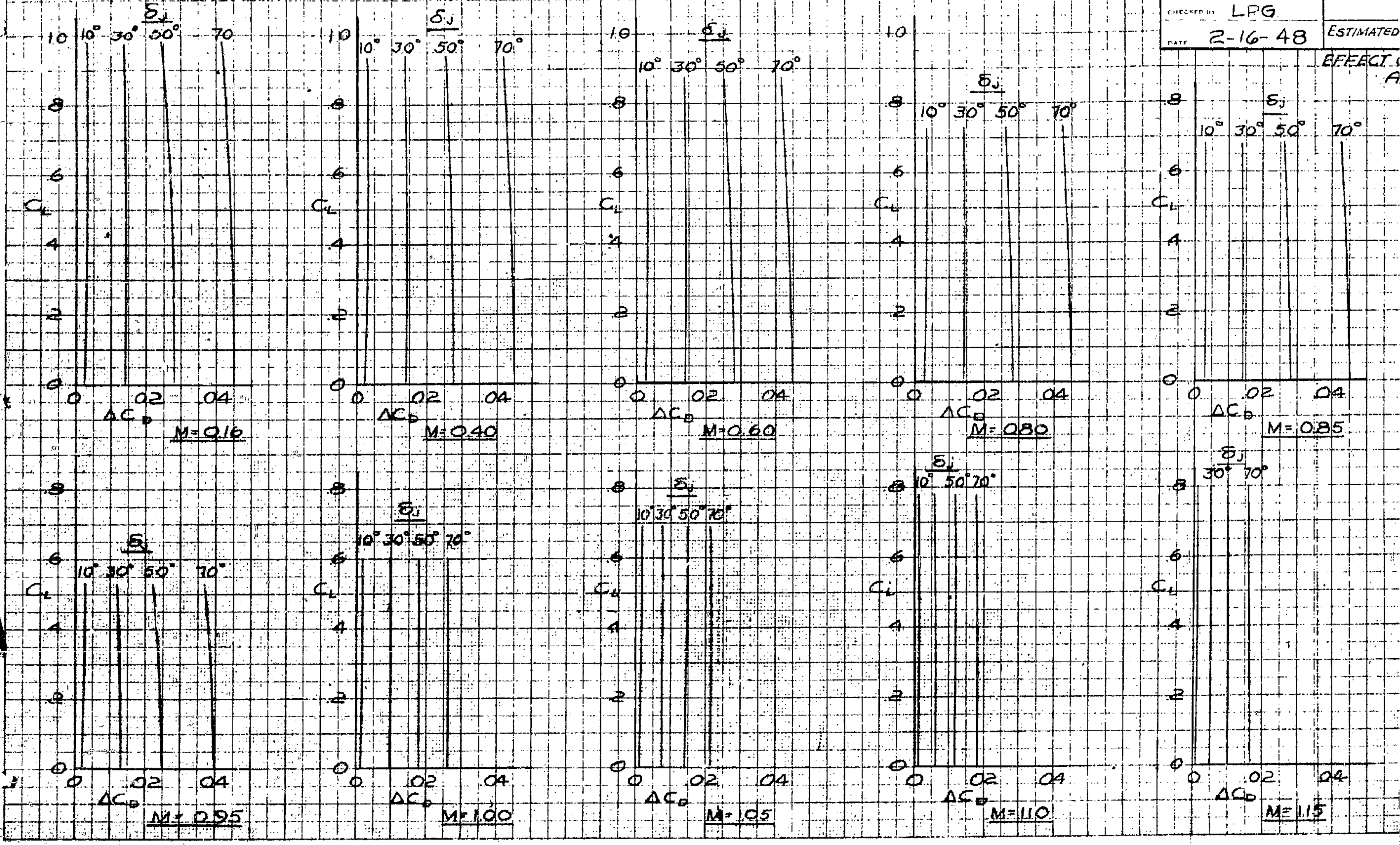
INCREMENT IN PITCHING MOMENT DUE TO SPEED BRAKES VS. MACH NUMBER

$\delta_{J_{MAX}} = 50°$



PREPARED BY PES.	NORTH
CHECKED BY LPG	
DATE 2-16-48	ESTIMATED

EFFECT ...
A...



NORTH AMERICAN AVIATION, INC.
INGLEWOOD, CALIFORNIA

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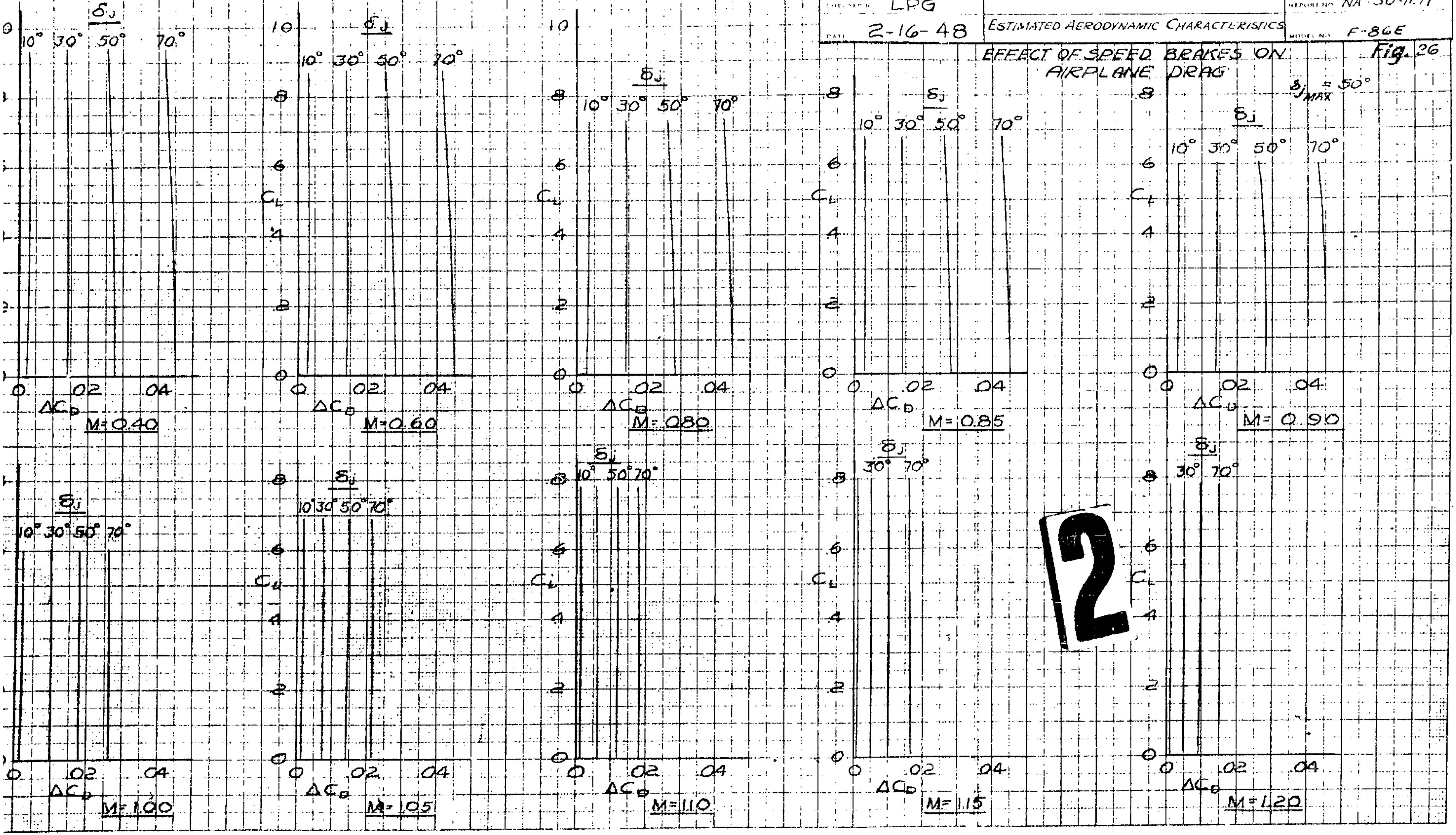
EFFECT OF SPEED BRAKES ON AIRPLANE DRAG

Fig. 26



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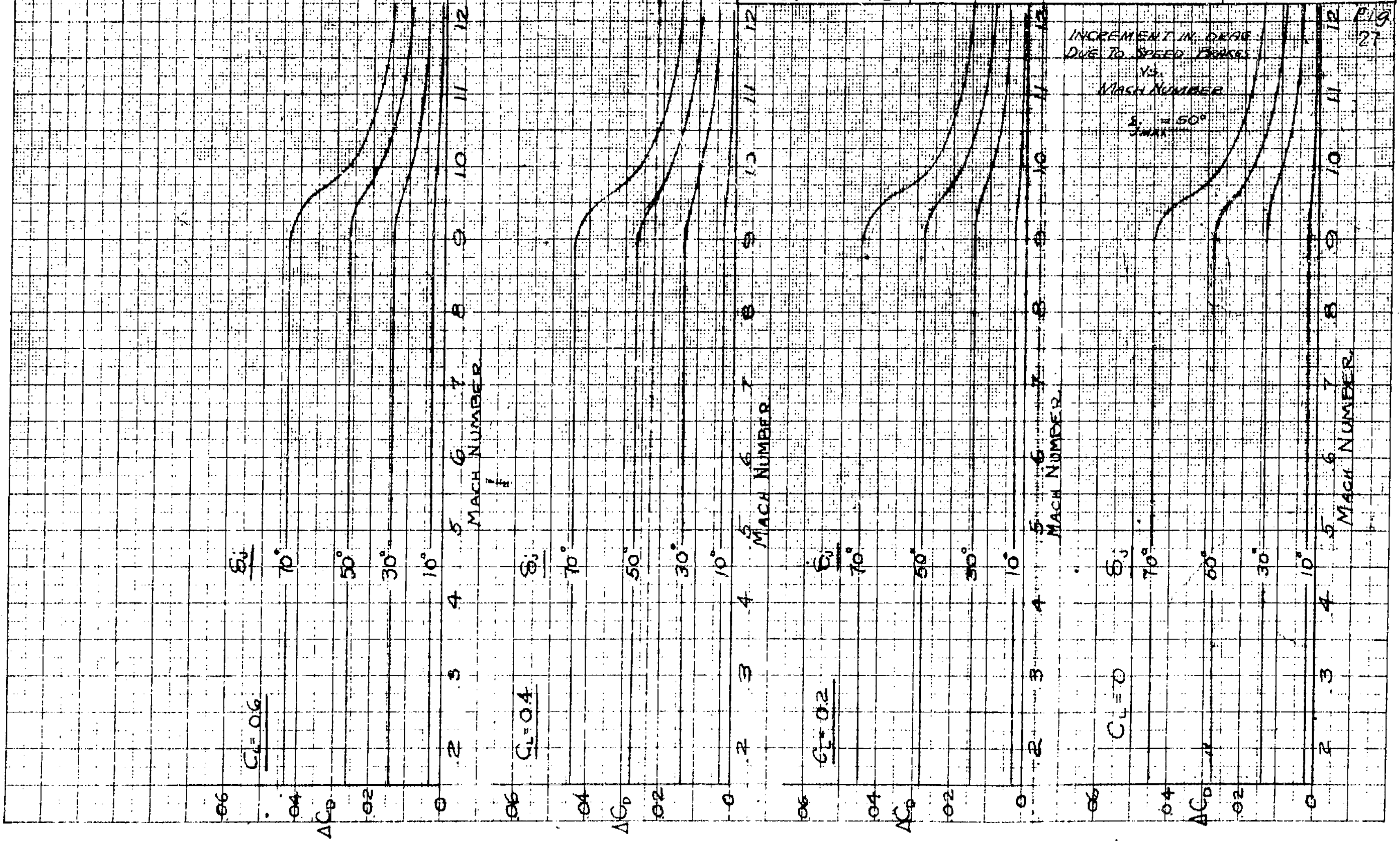

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FIG. 28

F-86E

ESTIMATED INCREMENT OF DRAG COEFFICIENT DUE TO ONE 120 GAL. EXTERNAL FUEL TANK WITH FIN

$\alpha = 0°$

$\Delta C_{D_{TANK}} = \Delta D / qS$ WHERE: ΔD = DRAG INCREMENT

S = WING AREA = 288 SQ. FT.

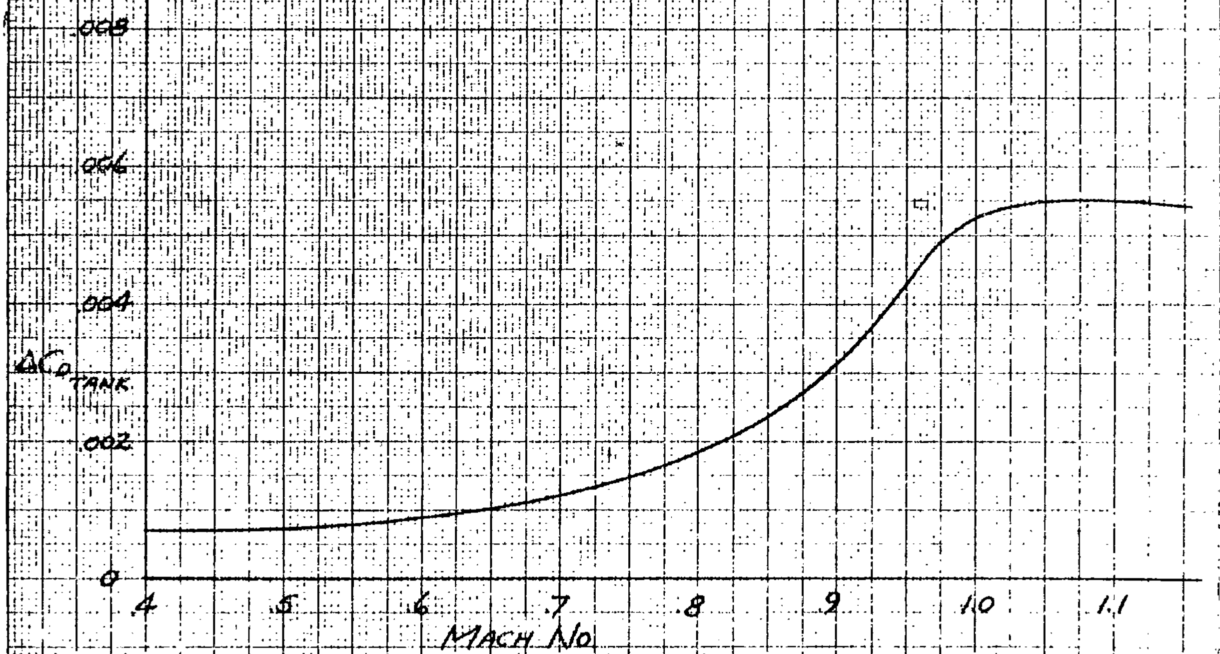

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FIG. 29

F-86E

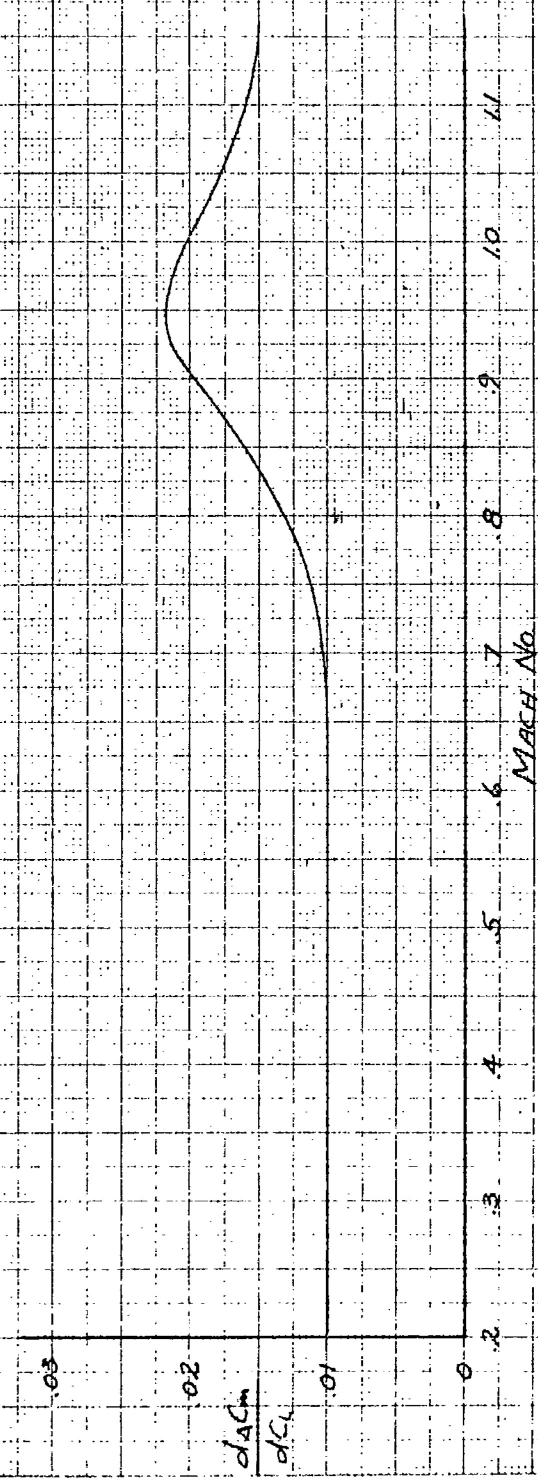
ESTIMATED VARIATION OF $\frac{d\Delta C_m}{dC_L}$ WITH MACH NO. DUE TO 120 GALLON EXTERNAL FUEL TANKS WITH FINS

$\Delta C_m = \frac{\Delta M}{q S \bar{c}_w}$ WHERE: ΔM = MOMENT INCREMENT DUE TO TWO TANKS

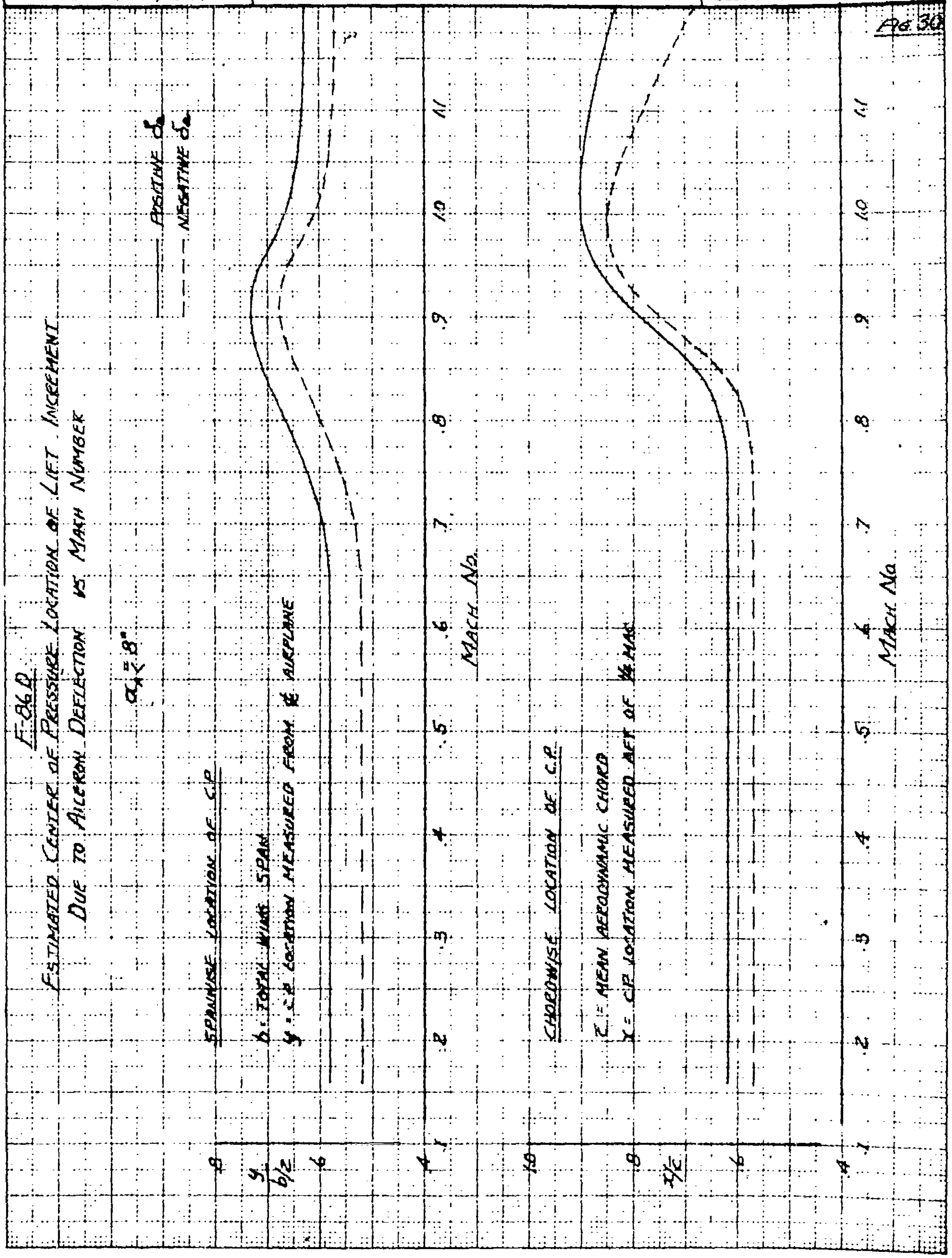
S = WING AREA

$\bar{c}_w$ = WING M.A.C.

$\Delta C_{m_{0\,TANK}} = 0$

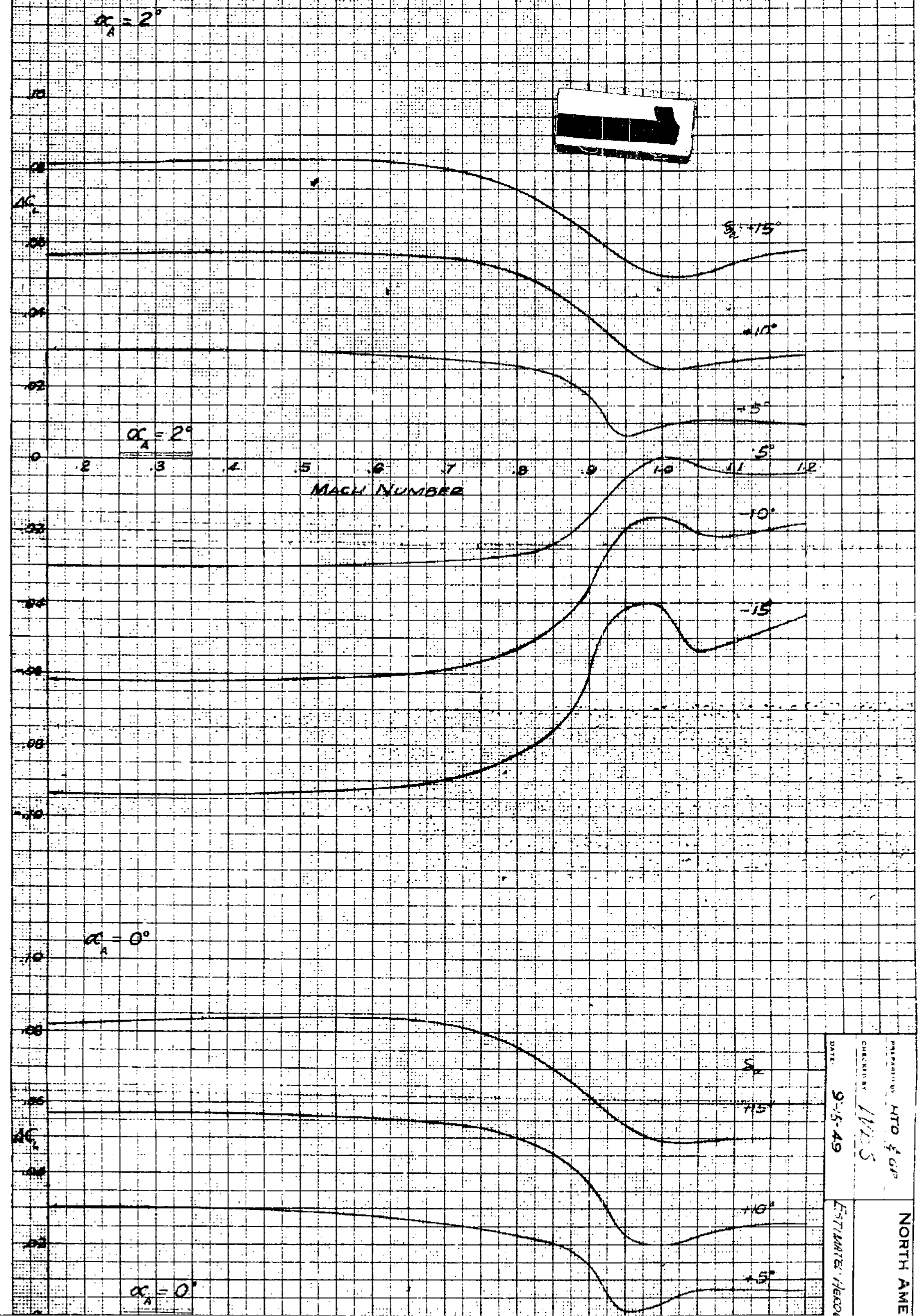


PREPARED BY: G.P	NORTH AMERICAN AVIATION, INC.	PAGE NO 52 OF 82
CHECKED BY: W.E.S.		REPORT NO NA-50-1277
DATE: SEPT 15, 1949	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO F-86E



ESTIMATED INCREMENT OF LIFT COEFFICIENT
DUE TO AILERON DEFLECTION
(ONE AILERON)

$\alpha_A = 0°$ & $\alpha_A = 2°$



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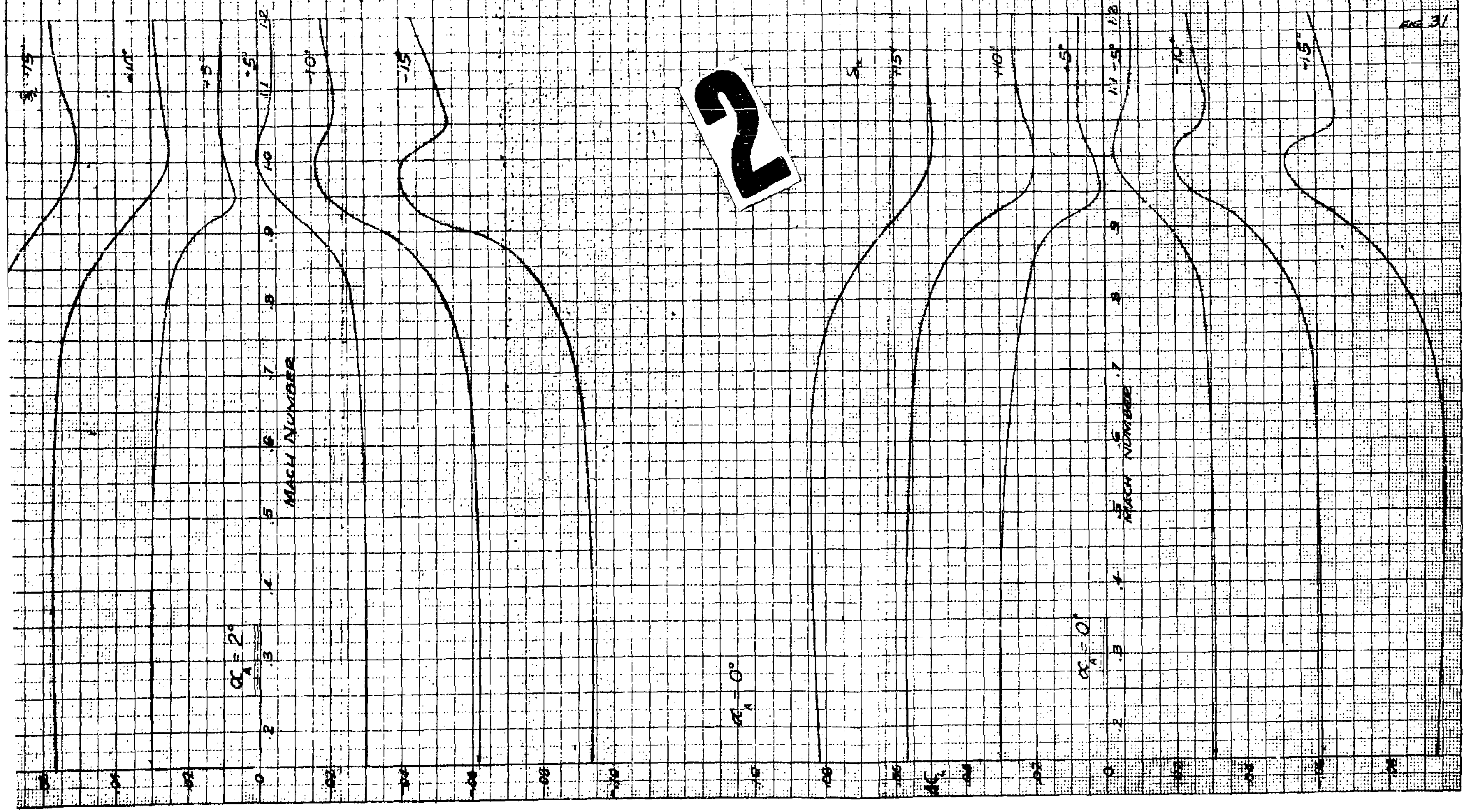
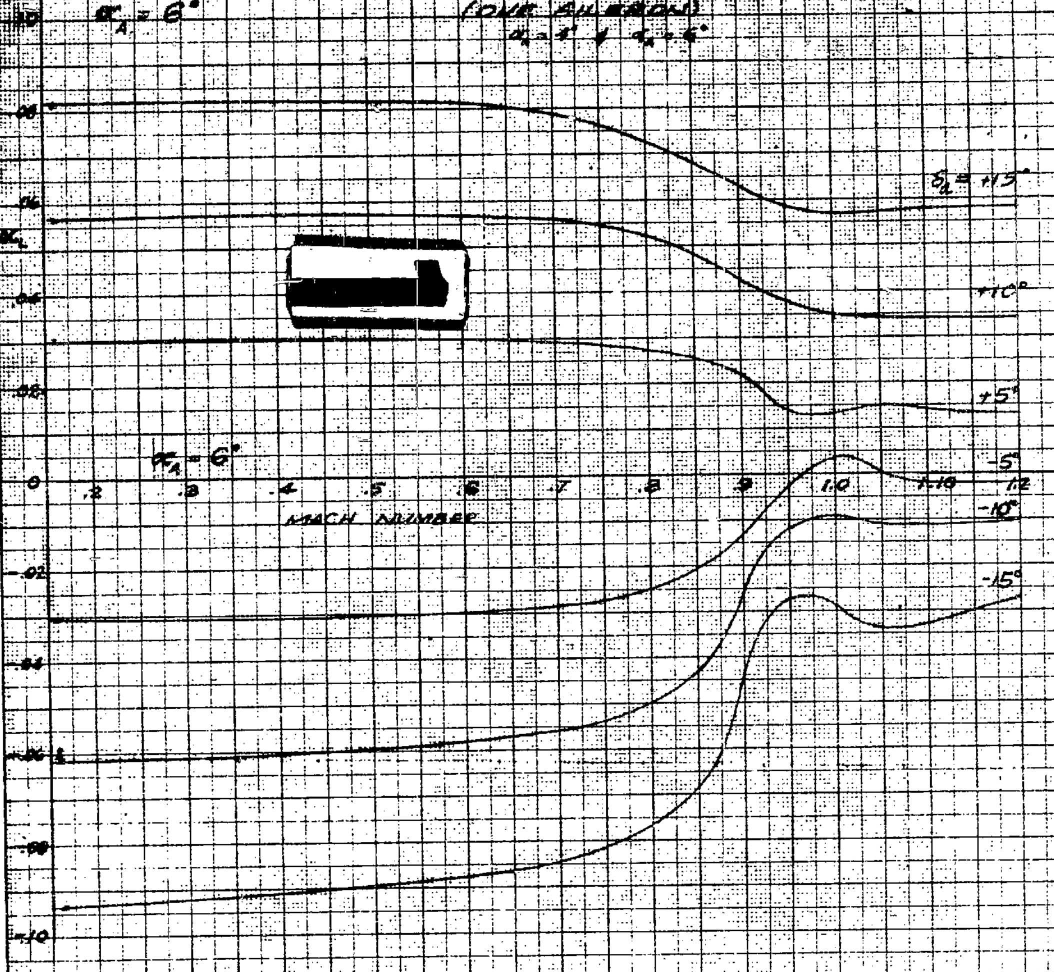
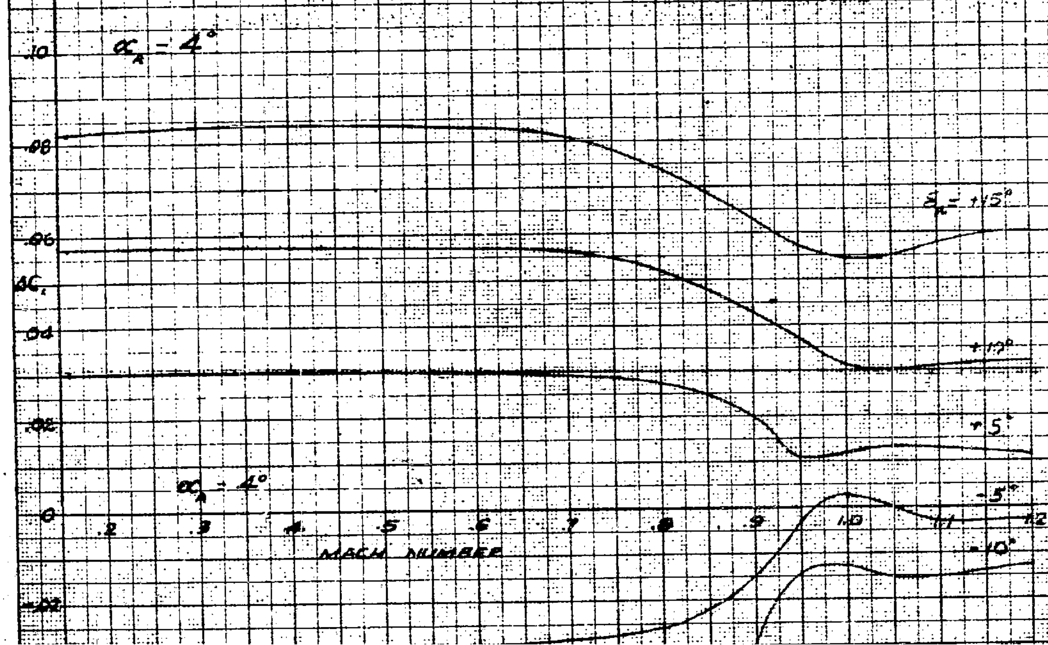


ESTIMATED INCREMENT OF LIFT COEFFICIENT
DUE TO AILERON DEFLECTION
(ONE AILERON)
$\alpha_A = 4°$ & $\alpha_A = 6°$





NORTH AMER[ICAN]
ESTIMATED AER[ODYNAMIC]
PREPARED BY HTD & GP
CHECKED BY WES
DATE 9-15-49

PREPARED BY HTD & GP	NORTH AMERICAN AVIATION, INC.		PAGE NO 54 OF 82
CHECKED BY WES			REPORT NO NA-50-4277
DATE 9-15-49	ESTIMATED AERODYNAMIC CHARACTERISTICS		MODEL NO F-86E

FIG. 32

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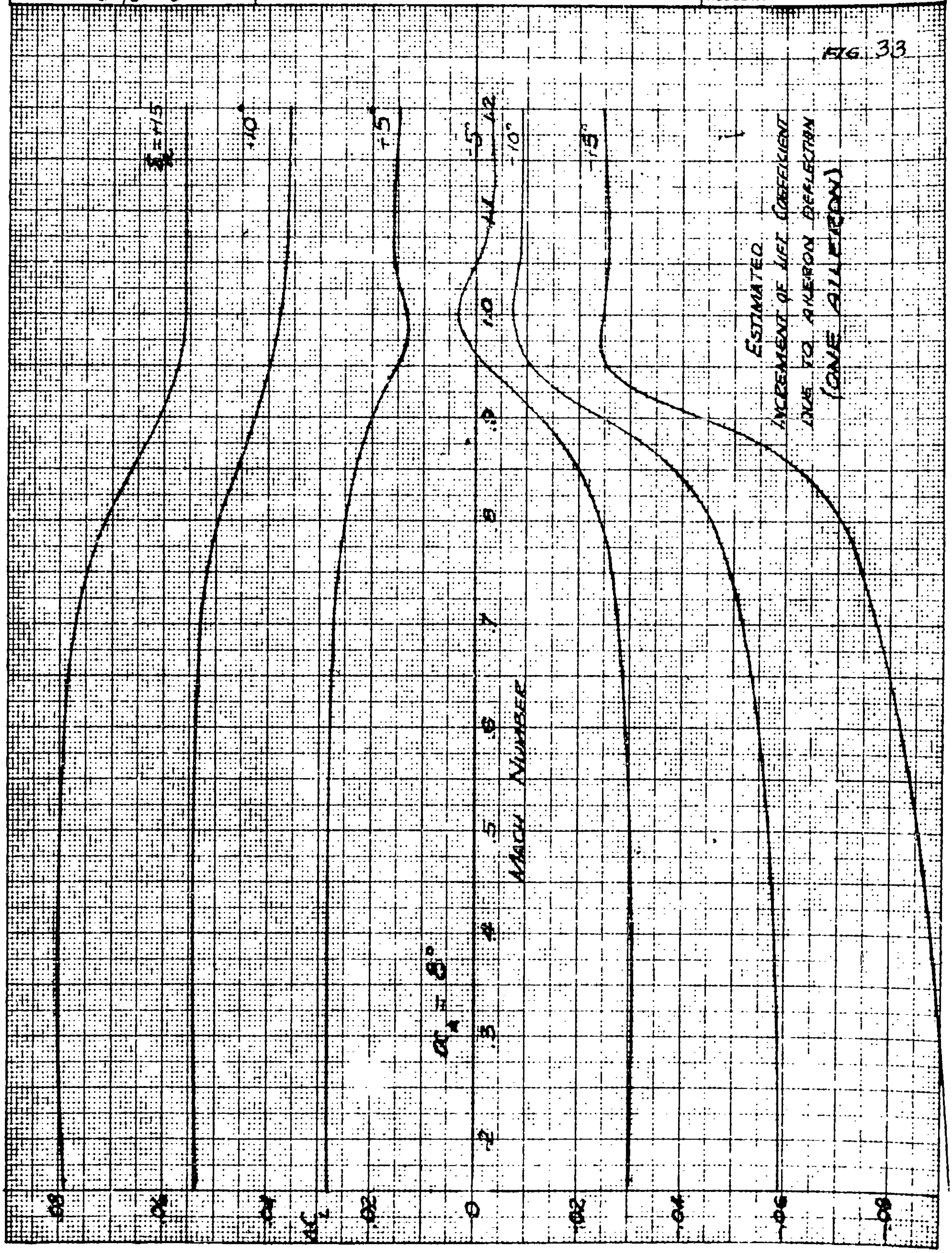
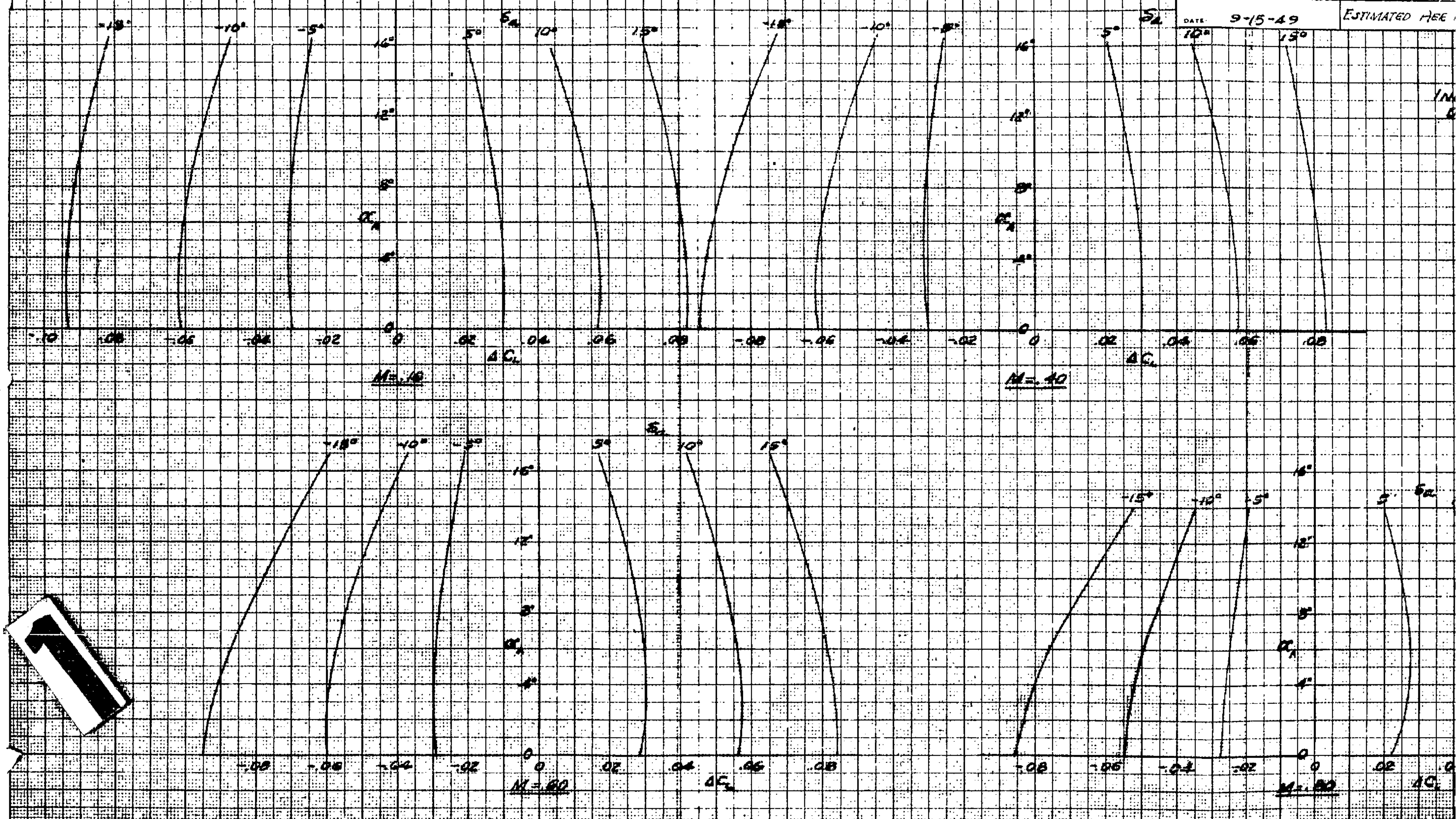
CHECKED BY WES		REPORT NO NA-50-1277
DATE 9-15-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO F-86E



PREPARED BY HTD & GF
CHECKED BY
DATE 9-15-49

NORTH AME

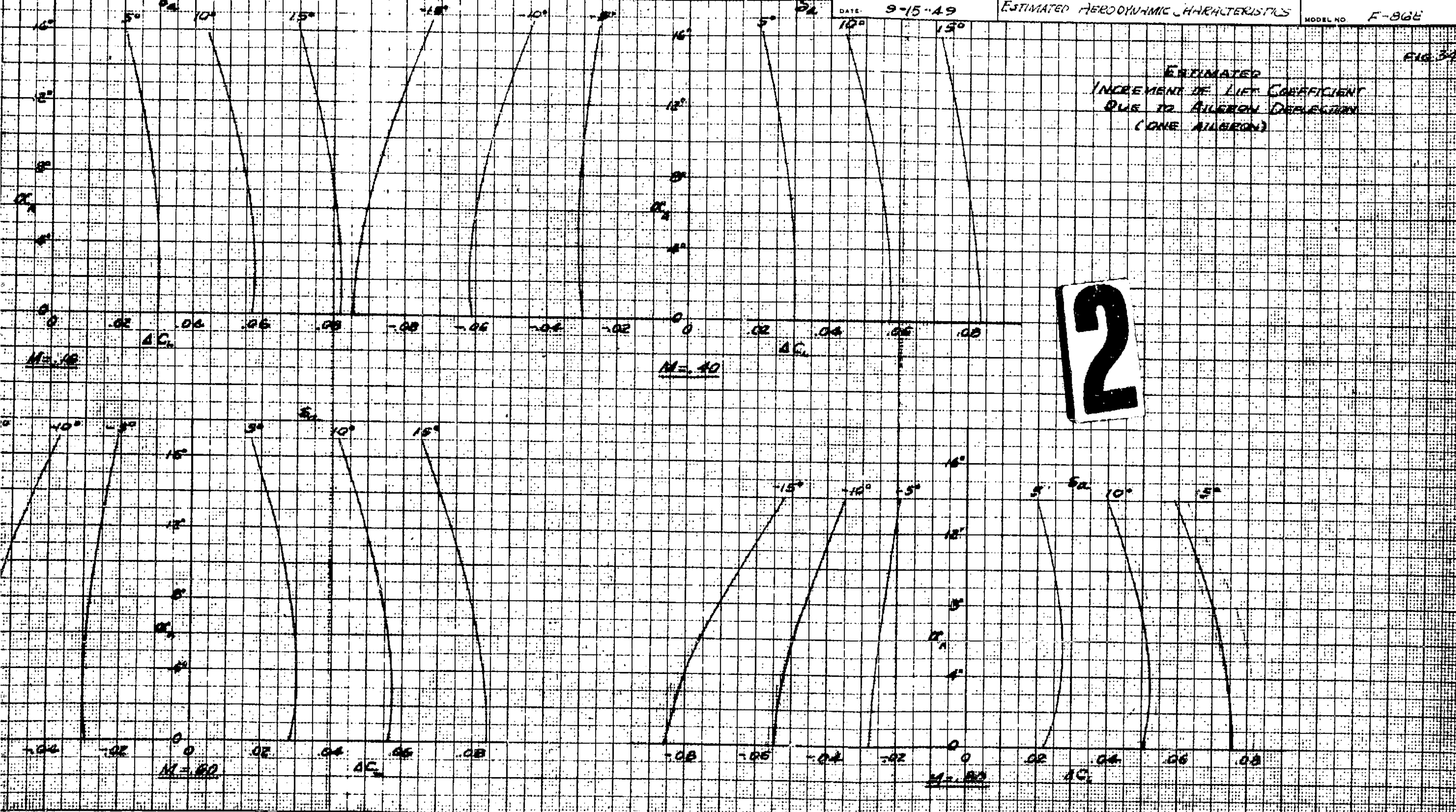
ESTIMATED AEE



PREPARED BY HTD & GP	NORTH AMERICAN AVIATION, INC.	PAGE NO. 56 OF 82	FORM ED-324 REV. 1-41
CHECKED BY		REPORT NO. NA-50-1277	
DATE: 9-15-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO. F-86E	

FIG. 34

ESTIMATED
INCREMENT OF LIFT COEFFICIENT
DUE TO AILERON DEFLECTION
(ONE AILERON)



NORTH AMER

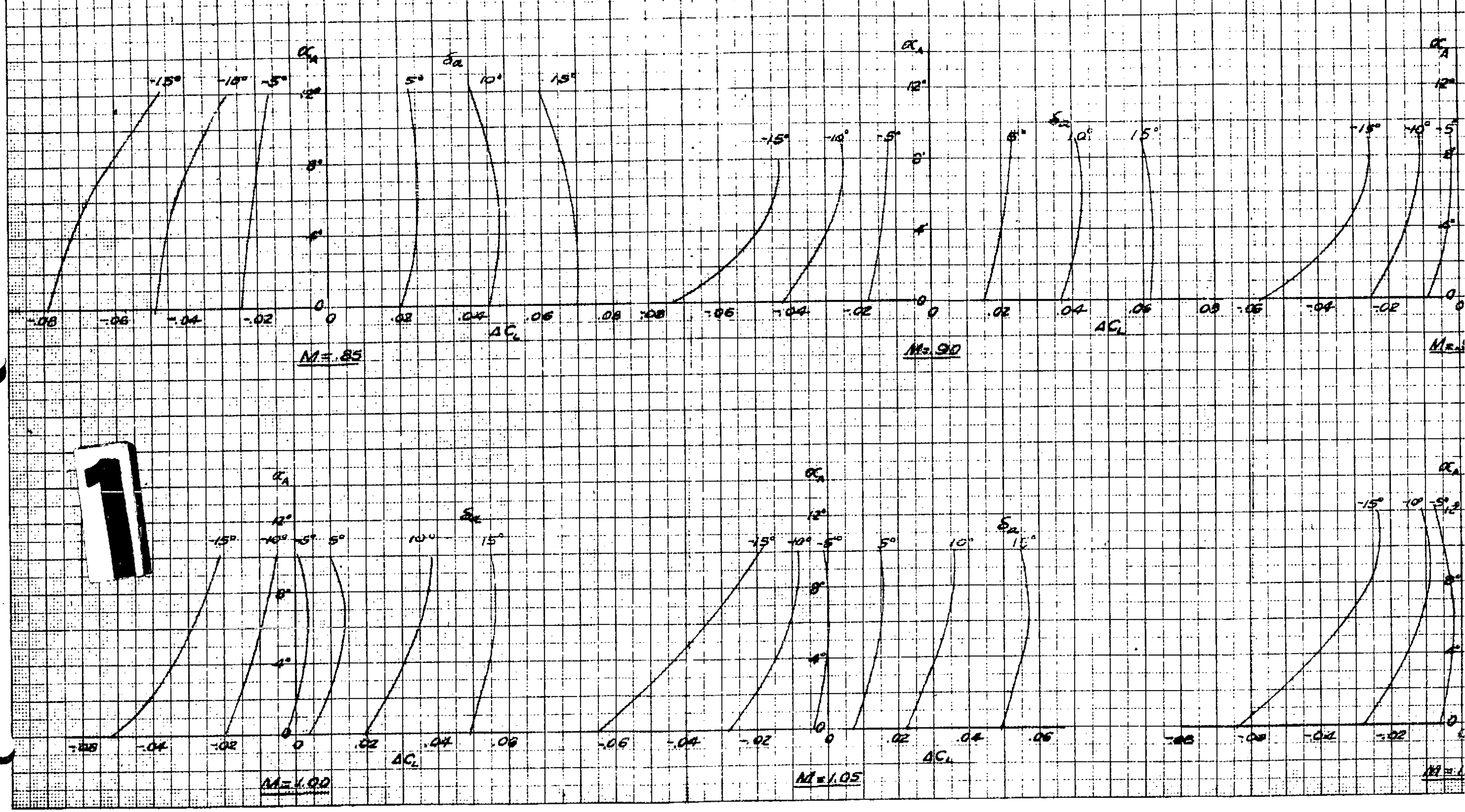
PREPARED BY: HTD & GP

CHECKED BY:

DATE: 9-15-49

ESTIMATED AERO

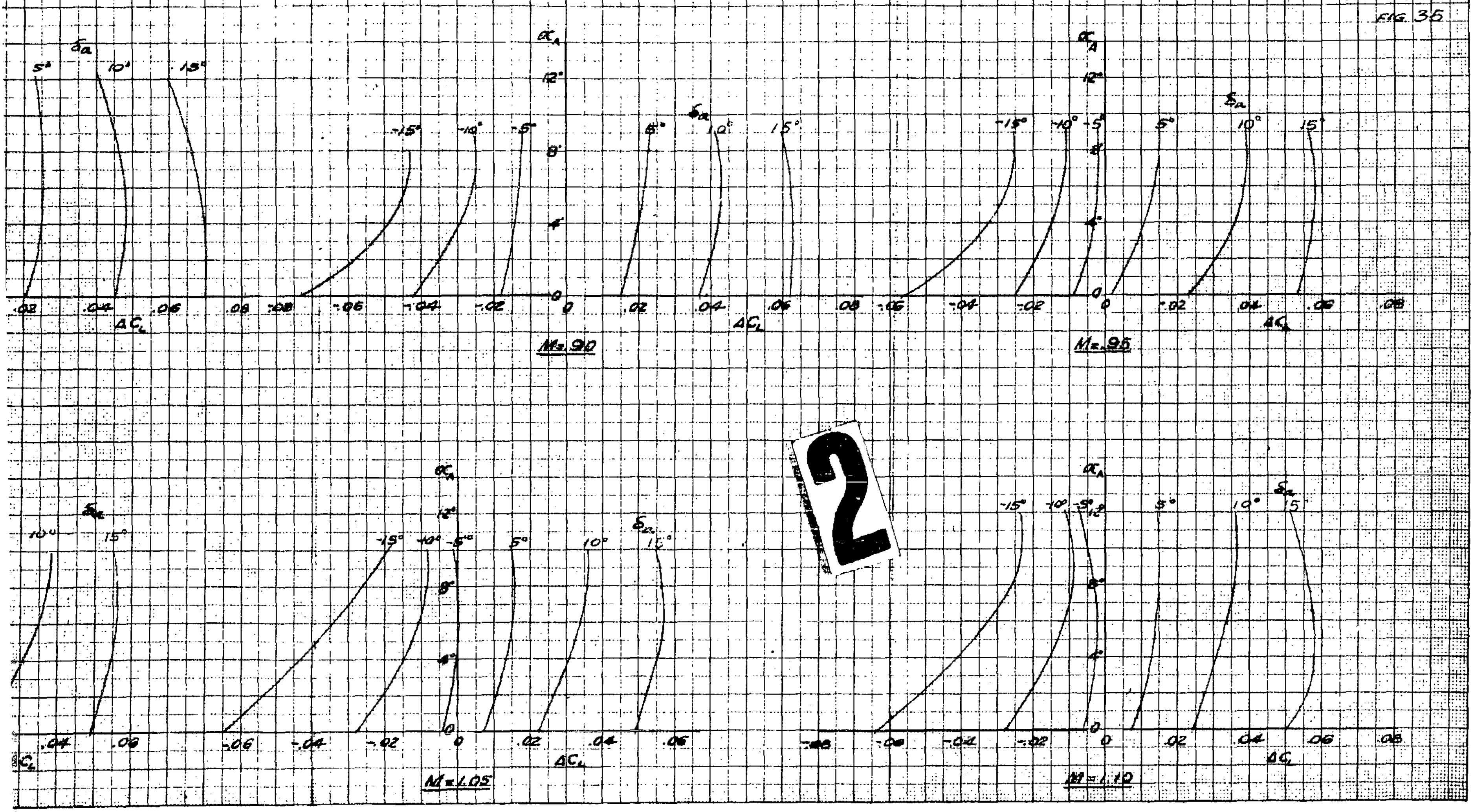
ESTIMATED INCREMENT OF LIFT COEFFICIENT
DUE TO AILERON DEFLECTION
(ONE AILERON)



PREPARED BY HTD & GP	NORTH AMERICAN AVIATION, INC.	PAGE NO. 57 OF 82	FORM ED-314 REV. 1-48
CHECKED BY		REPORT NO. NA-50-1277	
DATE 9-15-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO. F-86E	

ESTIMATED INCREMENT OF LIFT COEFFICIENT DUE TO AILERON DEFLECTION (ONE AILERON)

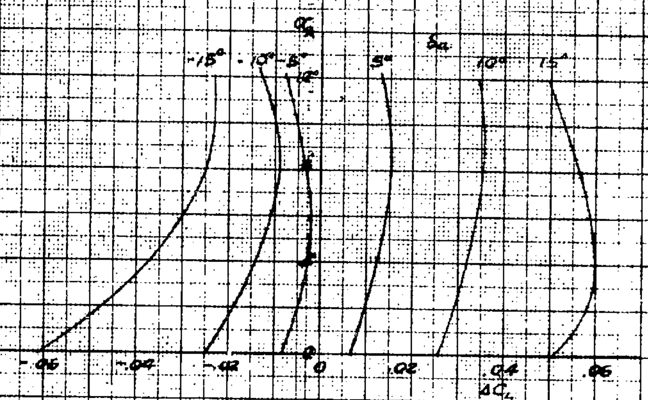
FIG. 35



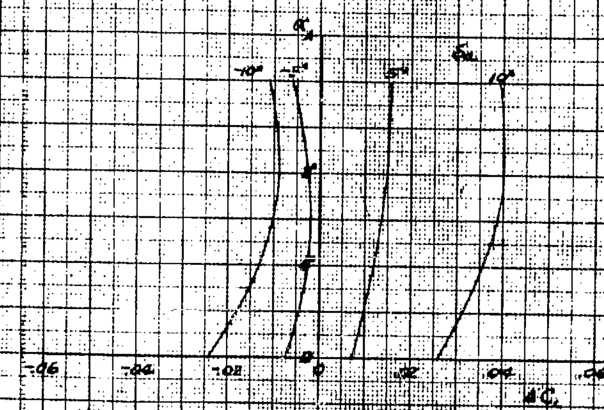
PREPARED BY HTO & GP	NORTH AMERICAN AVIATION, INC.	PAGE NO. 58 OF 82	FORM
CHECKED BY		REPORT NO. NA-50-1277	
DATE 9.16.49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO. F-86E	

FIG. 36

ESTIMATED
INCREMENT OF LIFT COEFFICIENT
DUE TO AILERON DEFLECTION
(ONE AILERON)



M = 1.15



M = 1.20

INCREMENT OF ROLLING MOMENT DUE TO AILERON DEFLECTION (LEFT AILERON)

PREPARED BY HTO & GP	NORTH AMERICAN AVIATION, INC.		PAGE NO. 59 OF 82
CHECKED BY			REPORT NO. NA-50-1277
DATE: 9-16-49	ESTIMATED AERODYNAMIC CHARACTERISTICS		MODEL NO. F-86E

FIG 37

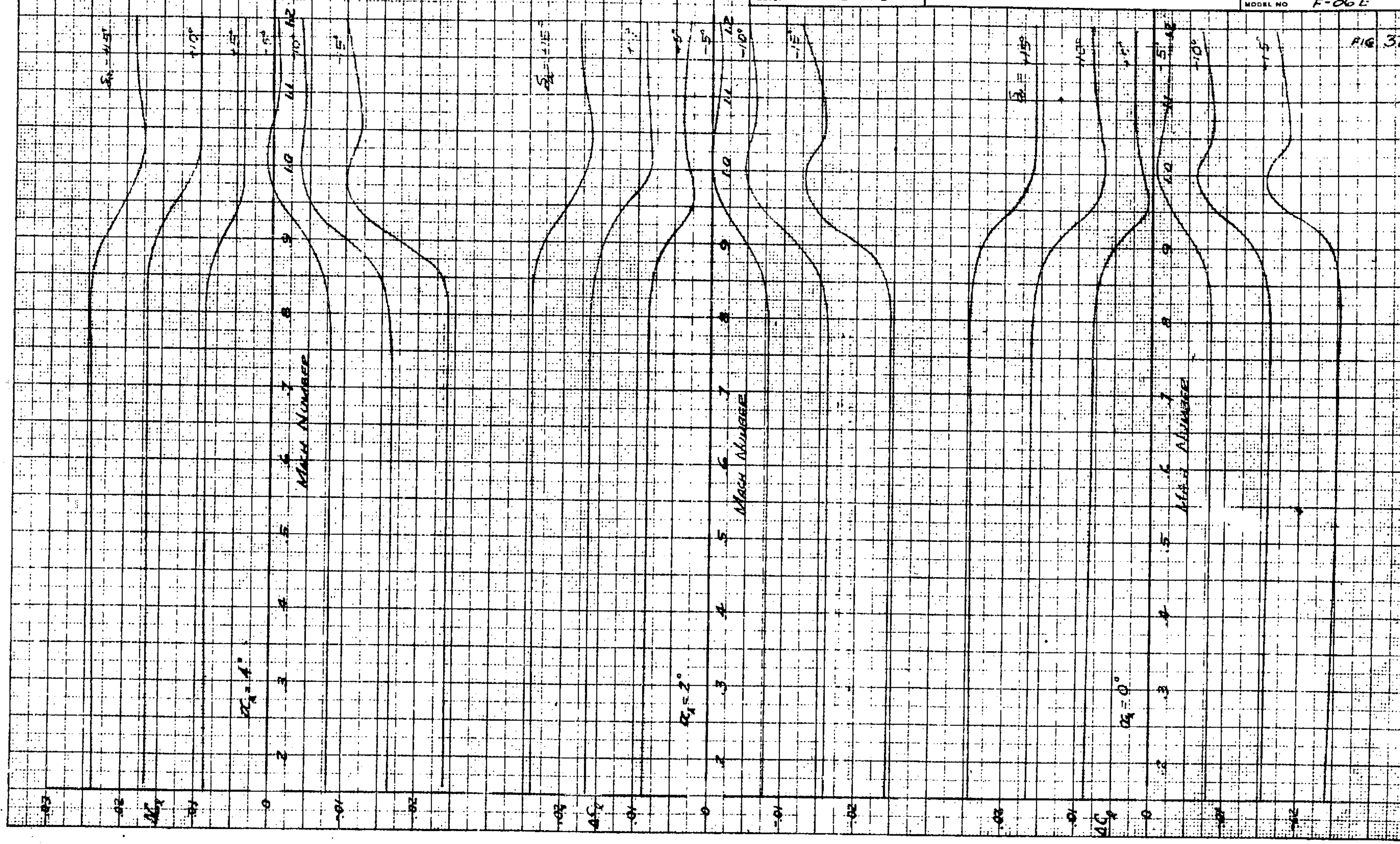
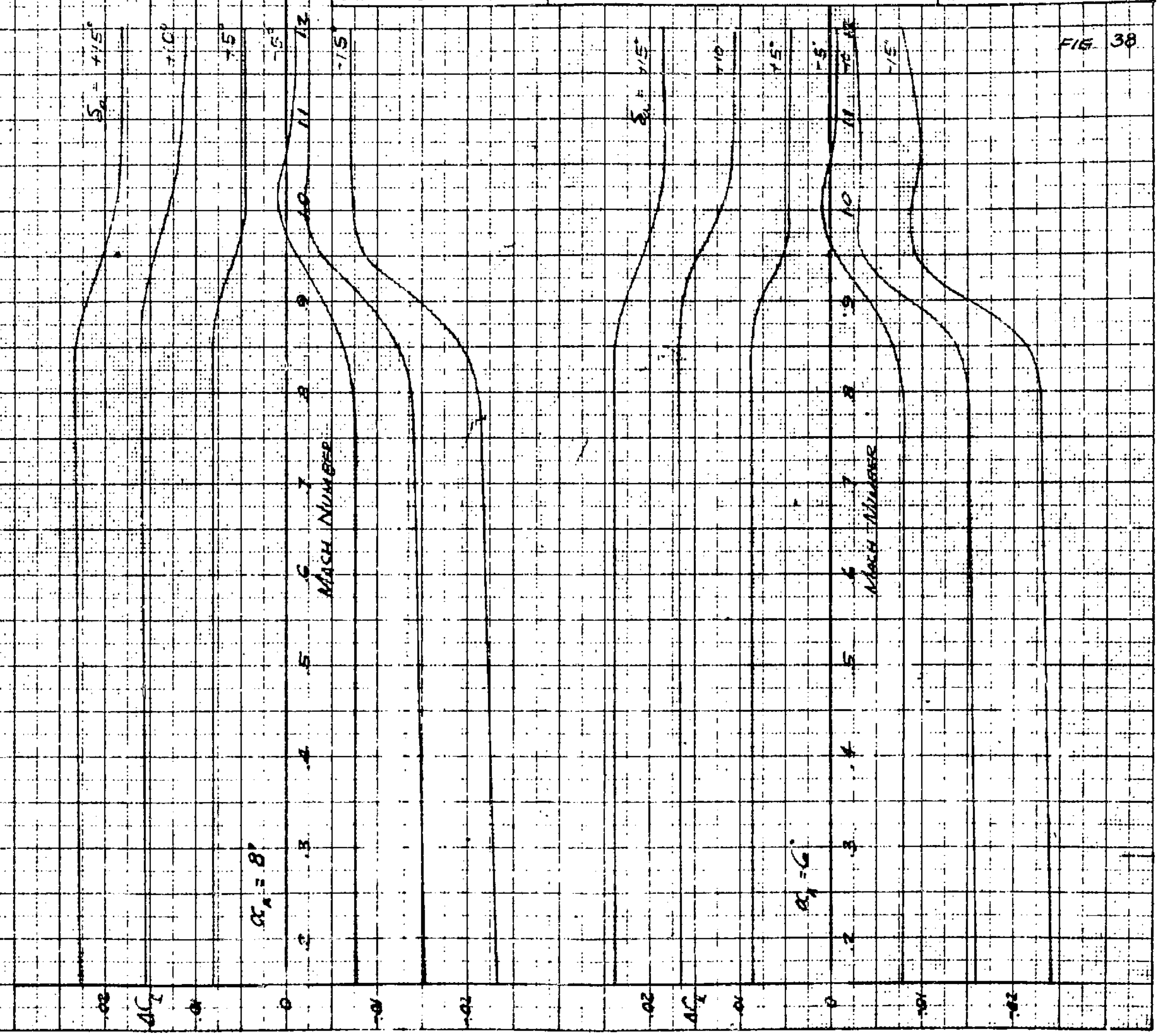


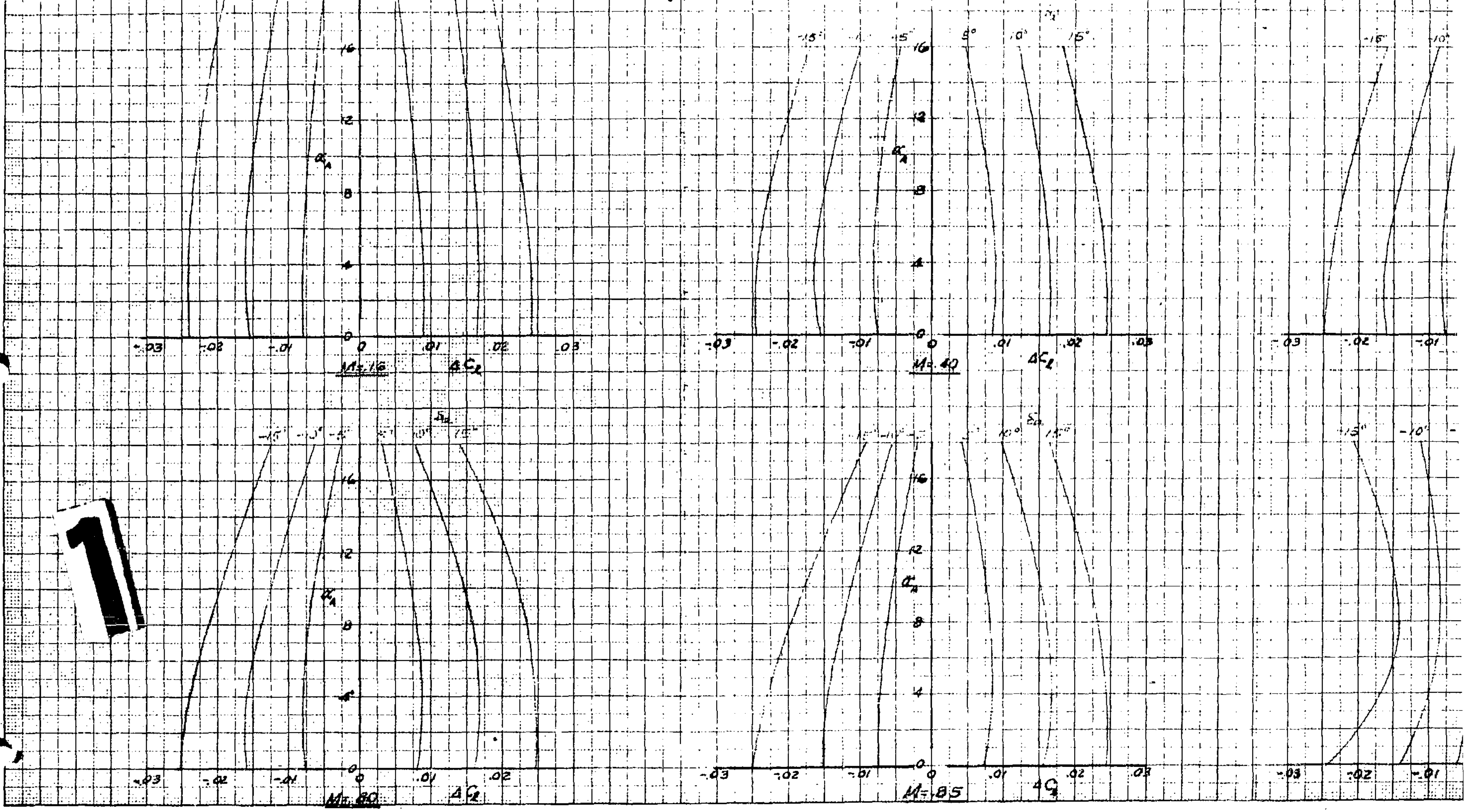
FIG. 38



INCREMENT OF
ROLLING MOMENT DUE TO
AILERON DEFLECTION
(LEFT AILERON)

INCREMENT OF
ROLLING MOMENT DUE TO
AILERON DEFLECTION
(LEFT AILERON)

HTD & GF	NORTH AM
DATE 9-16-49	ESTIMATED AERO

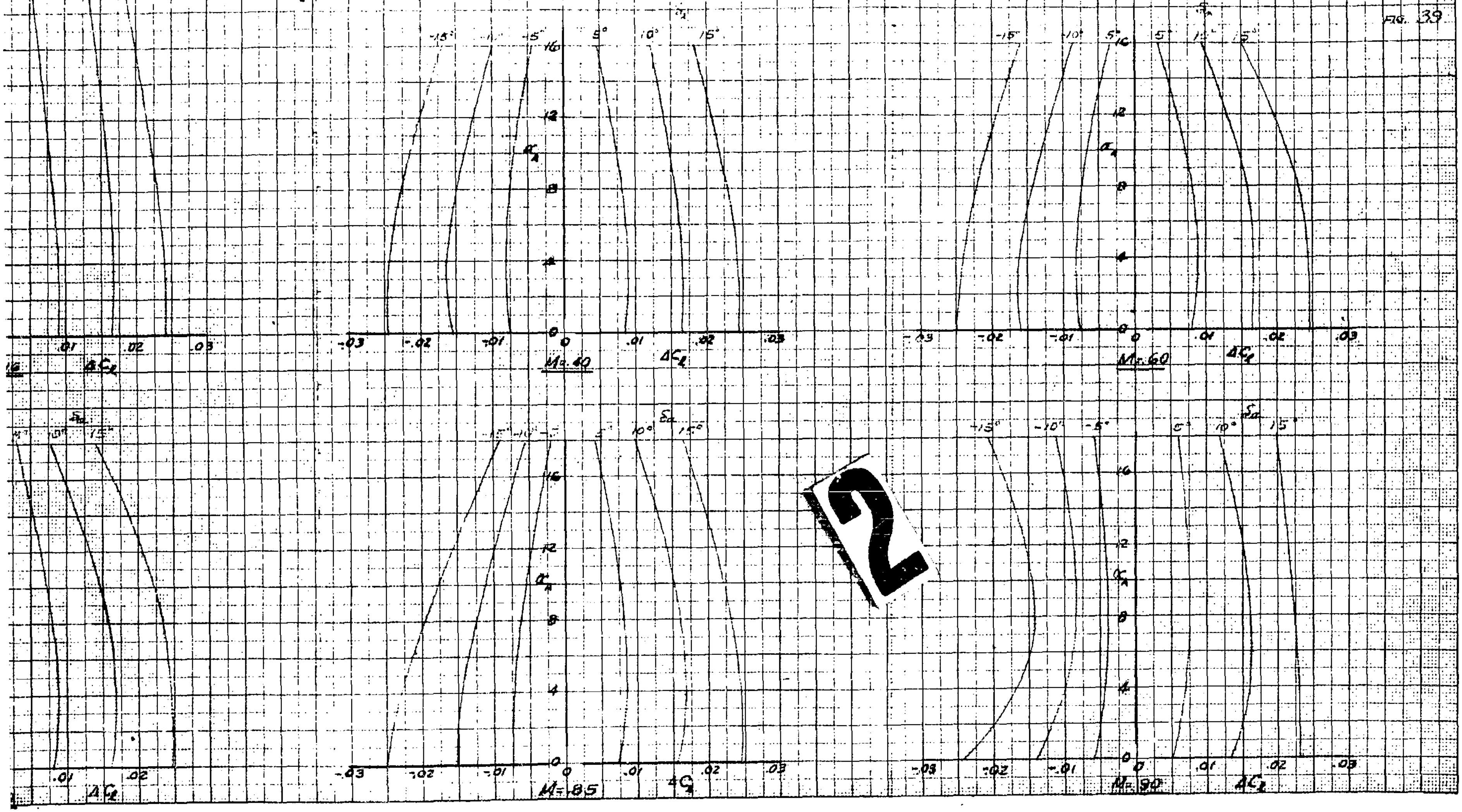


FORM 20-334 REV. 1-46

Drawn by: HTO & GP	NORTH AMERICAN AVIATION, INC.	Page No. 61 of 82
Checked by:		Report No. NA-50-1277
Date: 9-16-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	Model No. F-86E

INCREMENT OF ROLLING MOMENT DUE TO AILERON DEFLECTION (LEFT AILERON)

FIG. 39



INCREMENT OF
ROLLING MOMENT DUE TO
AILERON DEFLECTION
(LEFT AILERON)

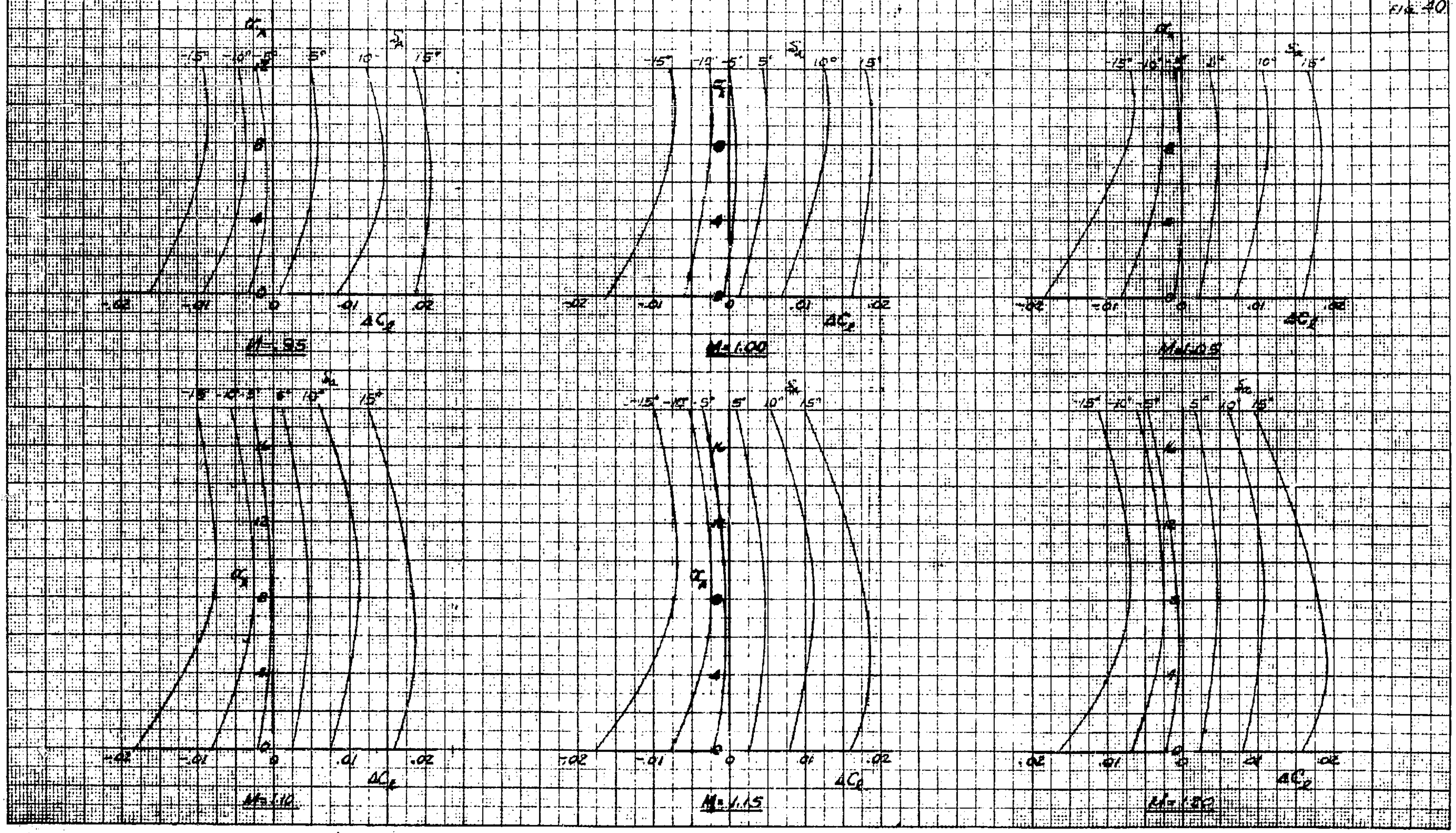
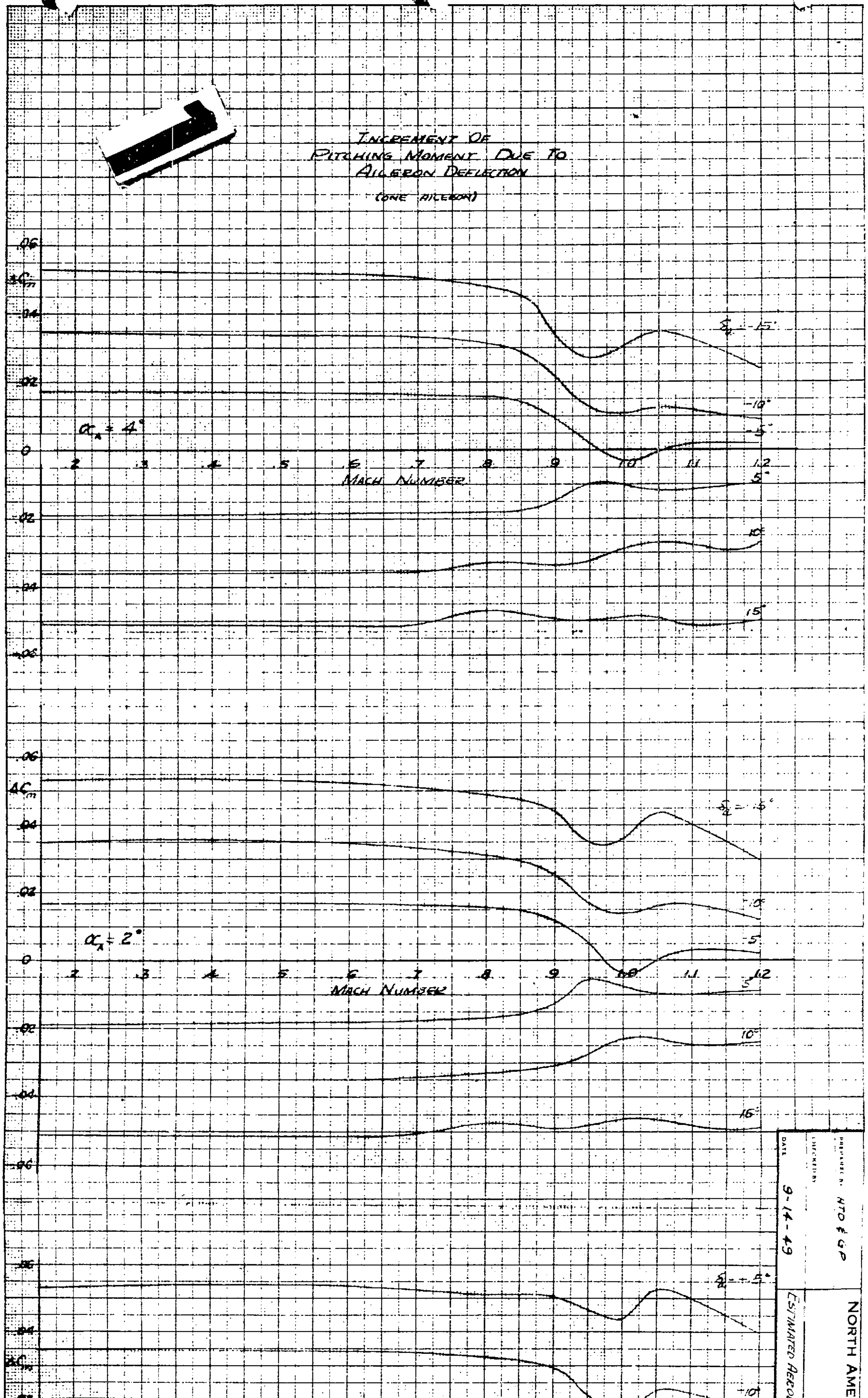
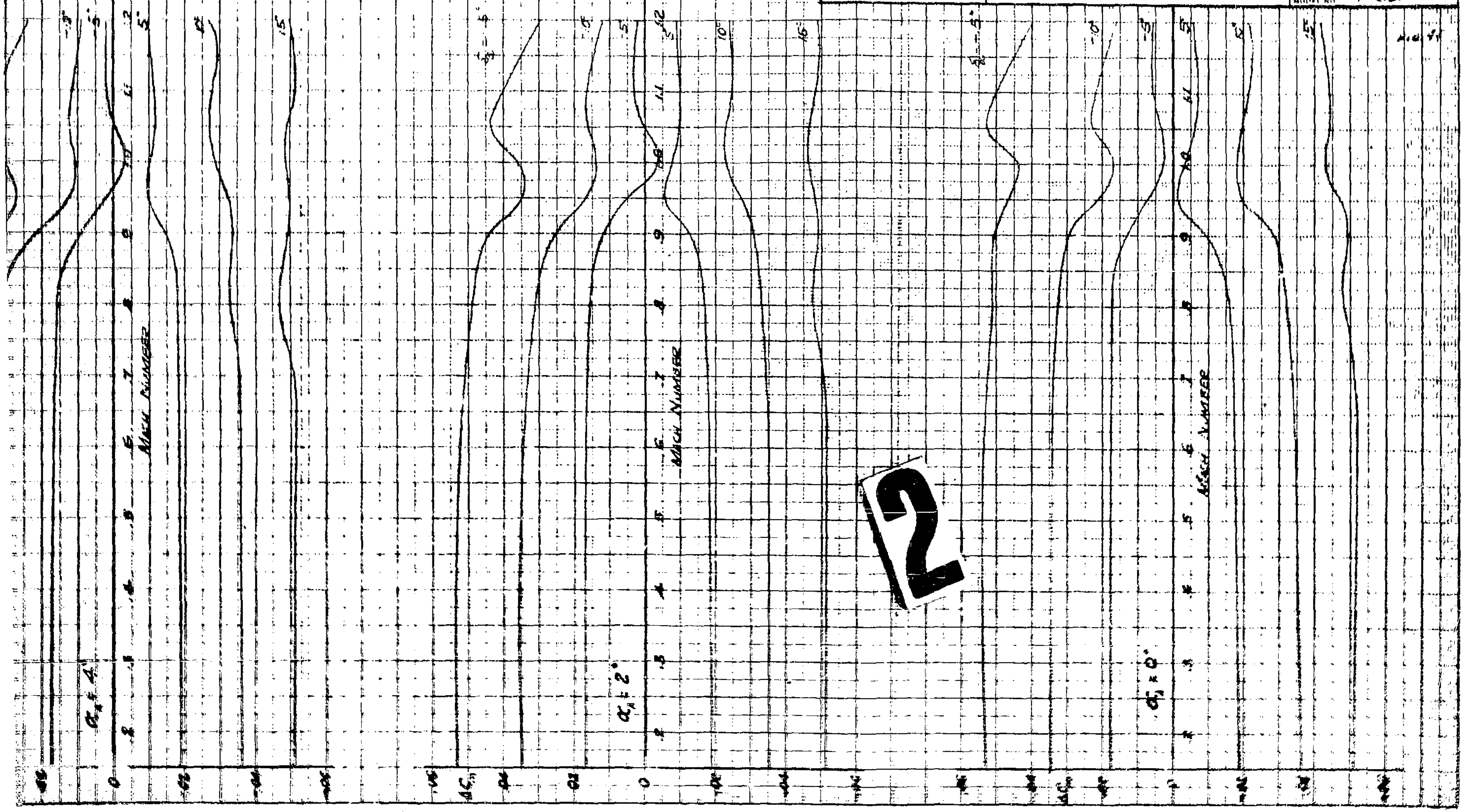


FIG. 40



Increment Of
Pitching Moment Due To
Aileron Deflection
(One Aileron)
$\alpha_x = 4°$
$\alpha_x = 2°$
Mach Number
ΔC_m
$\delta_a = 5°$
$\delta_a = 15°$
10°
15°
.2
.3
.4
.5
.6
.7
.8
.9
1.0
1.1
1.2
.02
.04
.06
0
NORTH AME
ESTIMATED AERO
PREPARED BY HTD & GP
CHECKED BY
DATE 9-14-49

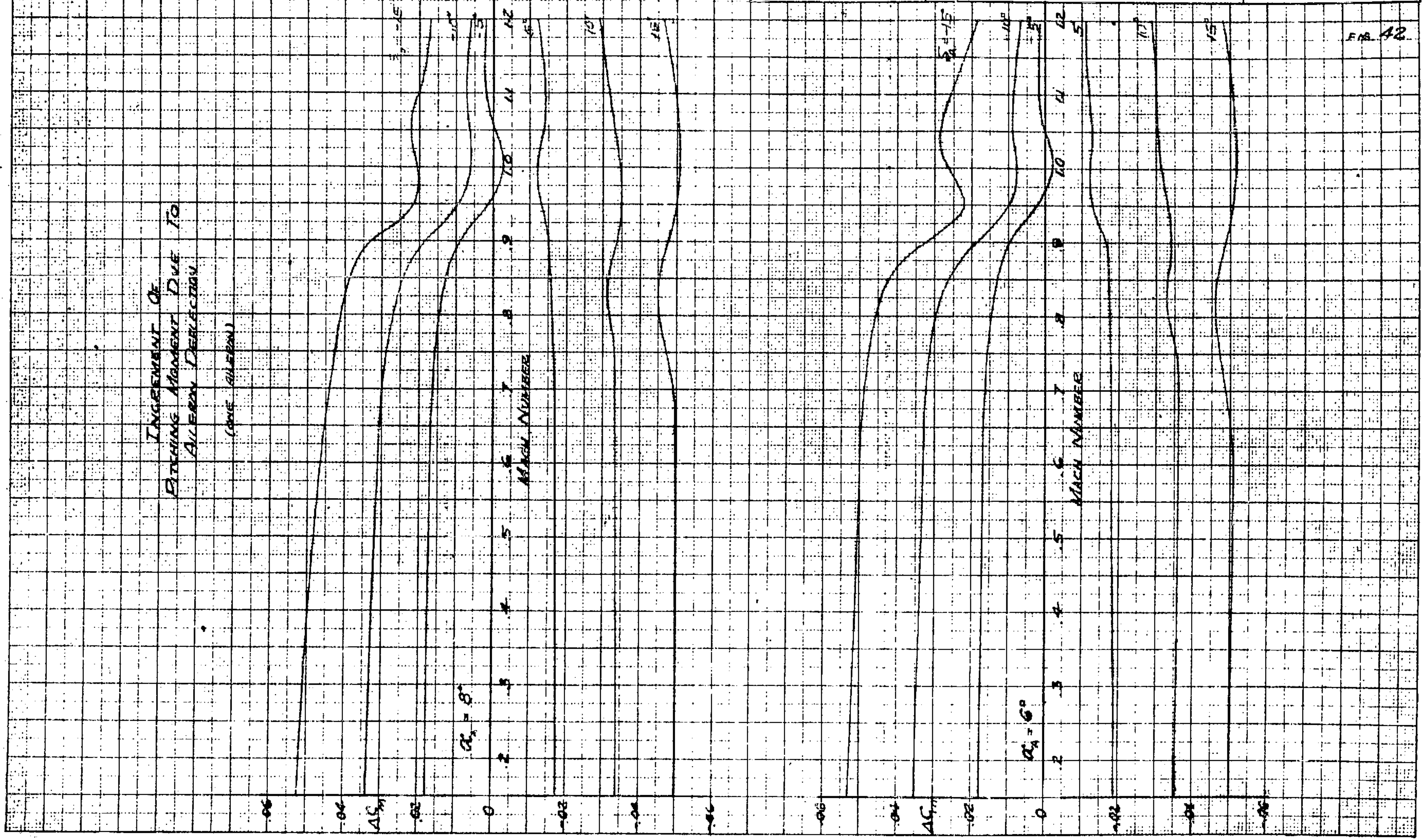
PREPARED BY HTD & GP	NORTH AMERICAN AVIATION, INC.
CHECKED BY	
DATE 9-14-49	ESTIMATED AERODYNAMICS CHARACTERISTICS
PAGE NO. [illegible]	REPORT NO. NA [illegible]
MODEL NO. F-86	



PREPARED BY: HTO & GP	NORTH AMERICAN AVIATION, INC.	PAGE NO 64 OF 82
CHECKED BY		REPORT NO NA-50-1277
DATE 9-14-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO F-86E

FIG. 42

INCREMENT OF PITCHING MOMENT DUE TO AILERON DEFLECTION (ONE AILERON)



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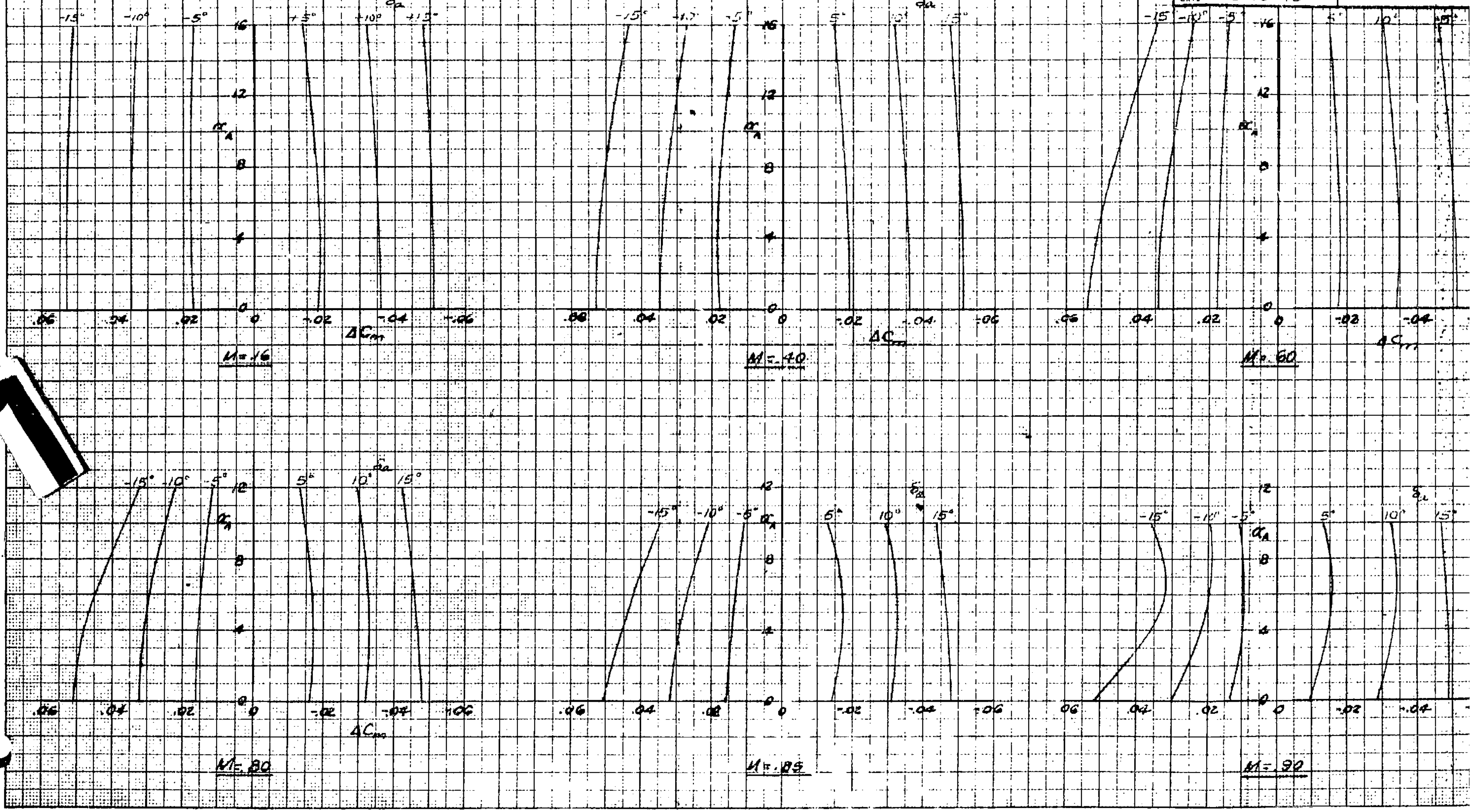
CHECKED BY

DATE 9-19-49

NORTH AMERIC

ESTIMATED AERODYN



PREPARED BY HTD & G.P	NORTH AMERICAN AVIATION, INC.	PAGE NO 65 OF 82
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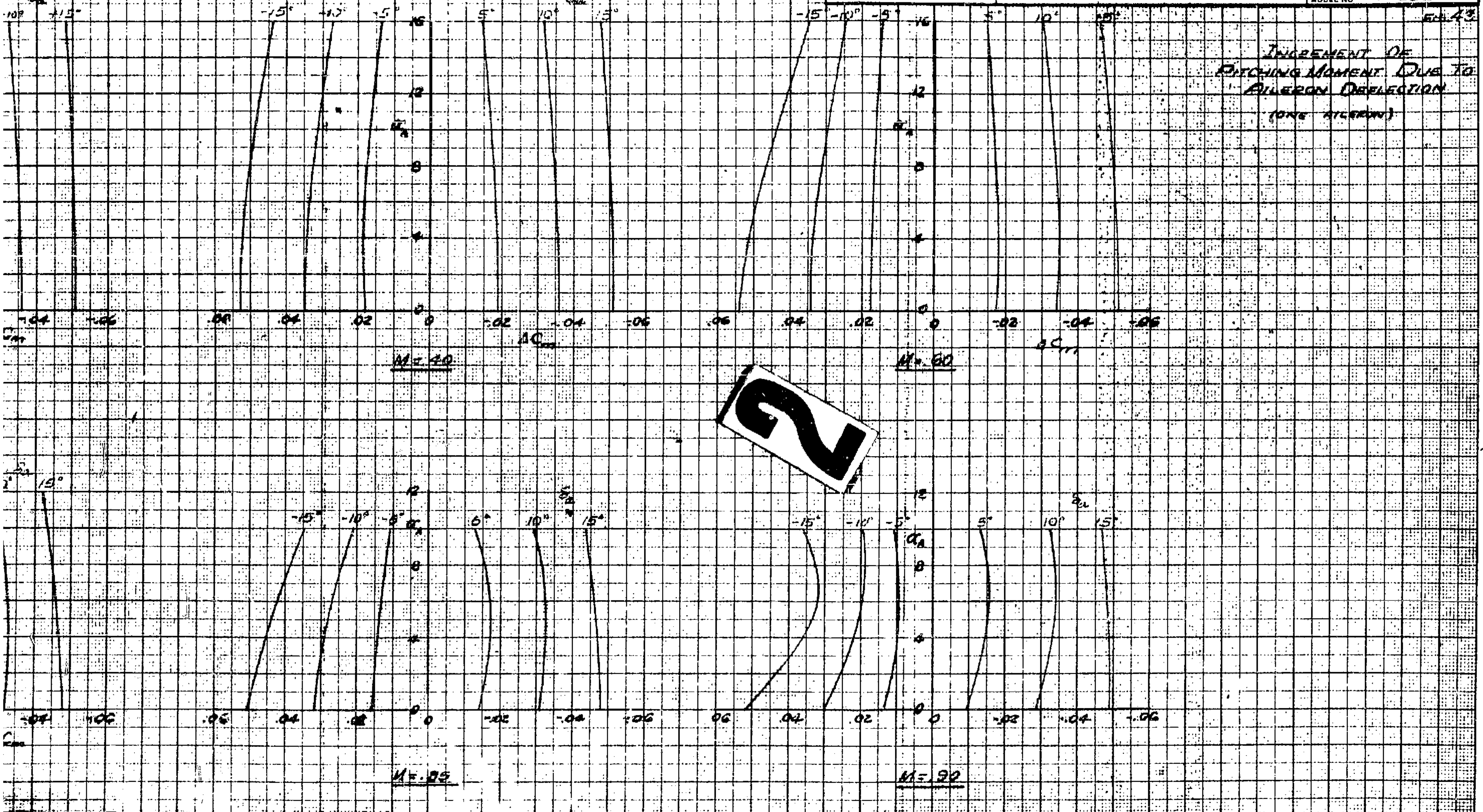
DATE 9-19-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO F-86E

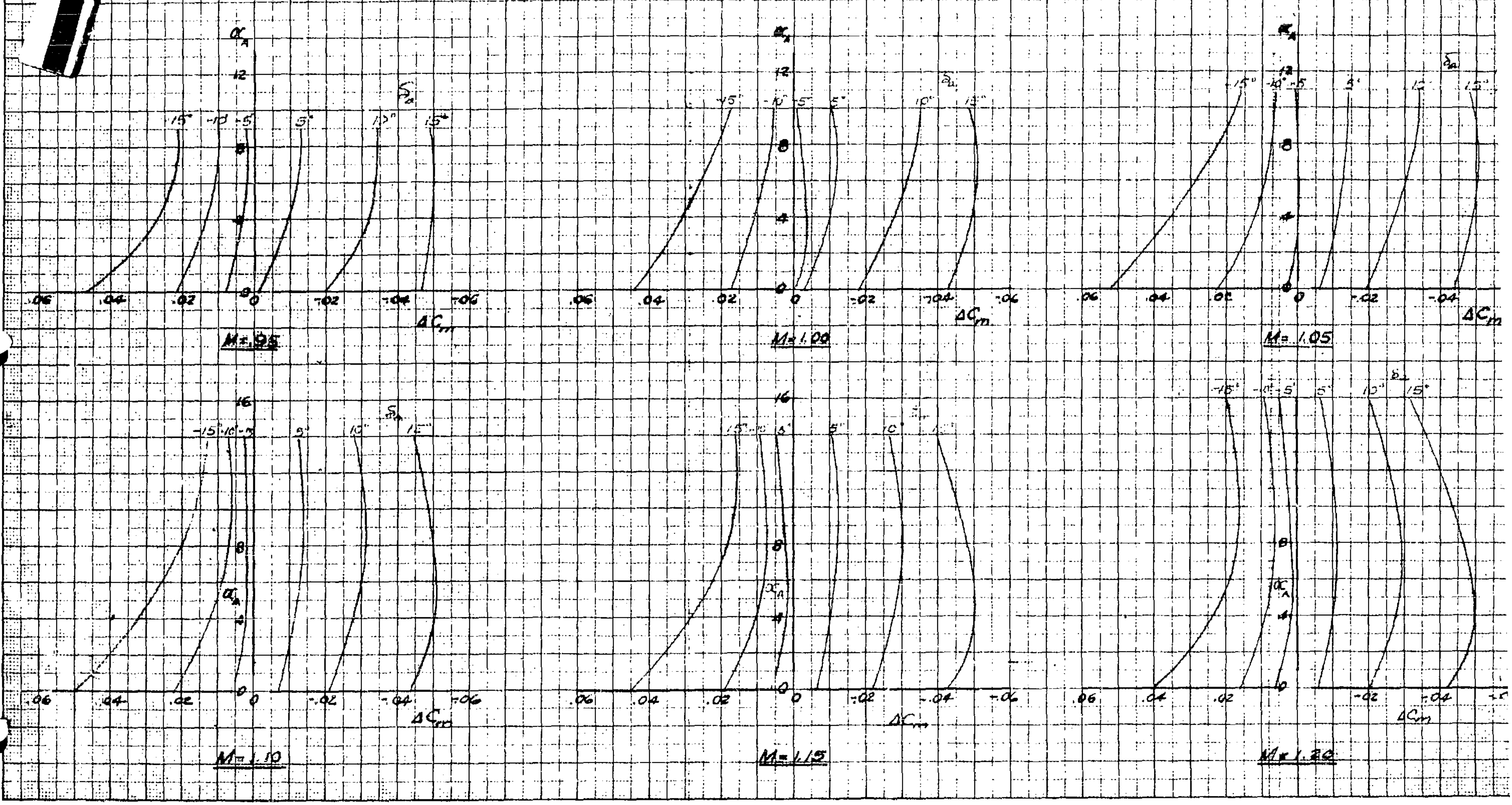
Fig. 43

INCREMENT OF PITCHING MOMENT DUE TO AILERON DEFLECTION

(ONE AILERON)



PREPARED BY HTD & GP		NORTH AMERI
CHECKED BY		
DATE 9-19-49		ESTIMATED AERODY

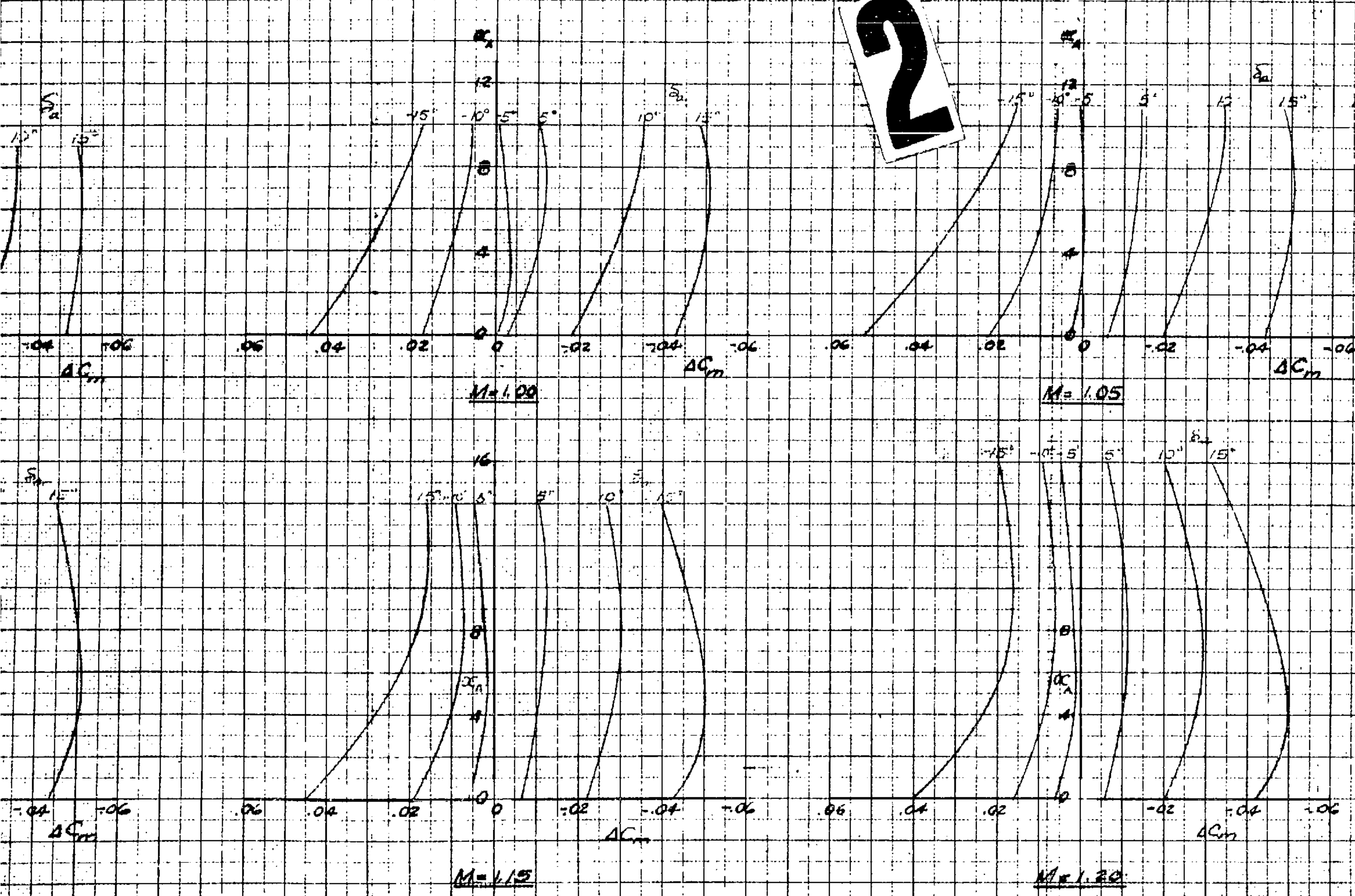


Prepared by: HTD & GD	NORTH AMERICAN AVIATION, INC.	Page No. 66 of 86
Checked by:		Report No. NA-50-1277
Date: 9-19-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	Model No. F-86E

FIG. 44

INCREMENT OF PITCHING MOMENT DUE TO AILERON DEFLECTION

(ONE AILERON)



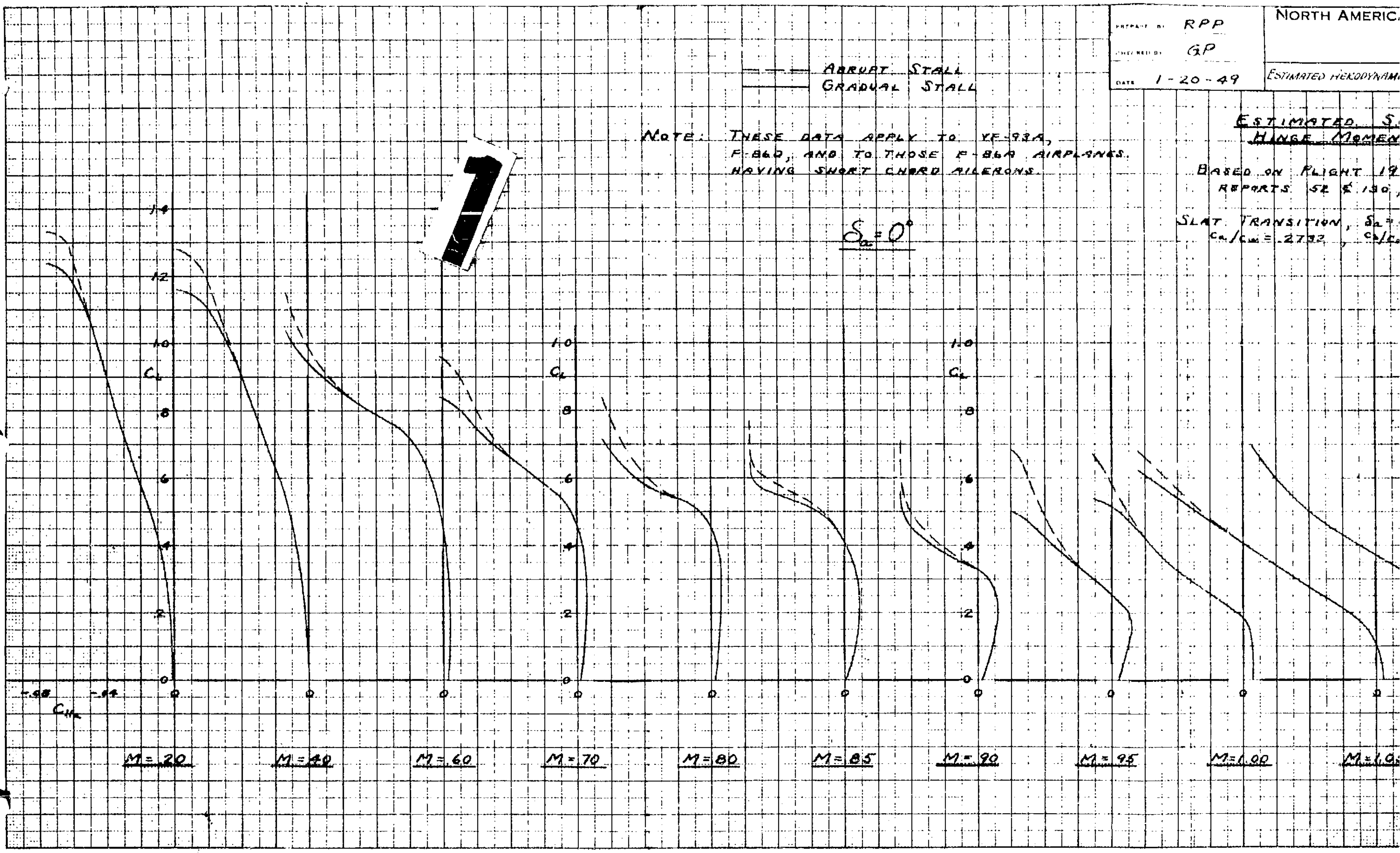

PREPARED BY RPP
CHECKED BY GP
DATE 1-20-49
NORTH AMERIC
ESTIMATED AERODYNAM
ESTIMATED S
HINGE MOMEN
BASED ON FLIGHT 19
REPORTS 52 & 130,
SLAT TRANSITION, δ_a =
c_a/c_w = .2732 , c_b/c_a
ABRUPT STALL
GRADUAL STALL
NOTE: THESE DATA APPLY TO YF-93A,
F-86D, AND TO THOSE F-86A AIRPLANES
HAVING SHORT CHORD AILERONS.
$\delta_a = 0°$
C_L
1.4
1.2
1.0
.8
.6
.4
.2
0
-.08
-.04
C_{H_a}
M = .20
M = .40
M = .60
M = .70
M = .80
M = .85
M = .90
M = .95
M = 1.00
M = 1.0

FIG. 45

— — — ABRUPT STALL
——— GRADUAL STALL

NOTE: THESE DATA APPLY TO YF-93A, F-86D, AND TO THOSE F-86A AIRPLANES HAVING SHORT CHORD AILERONS.

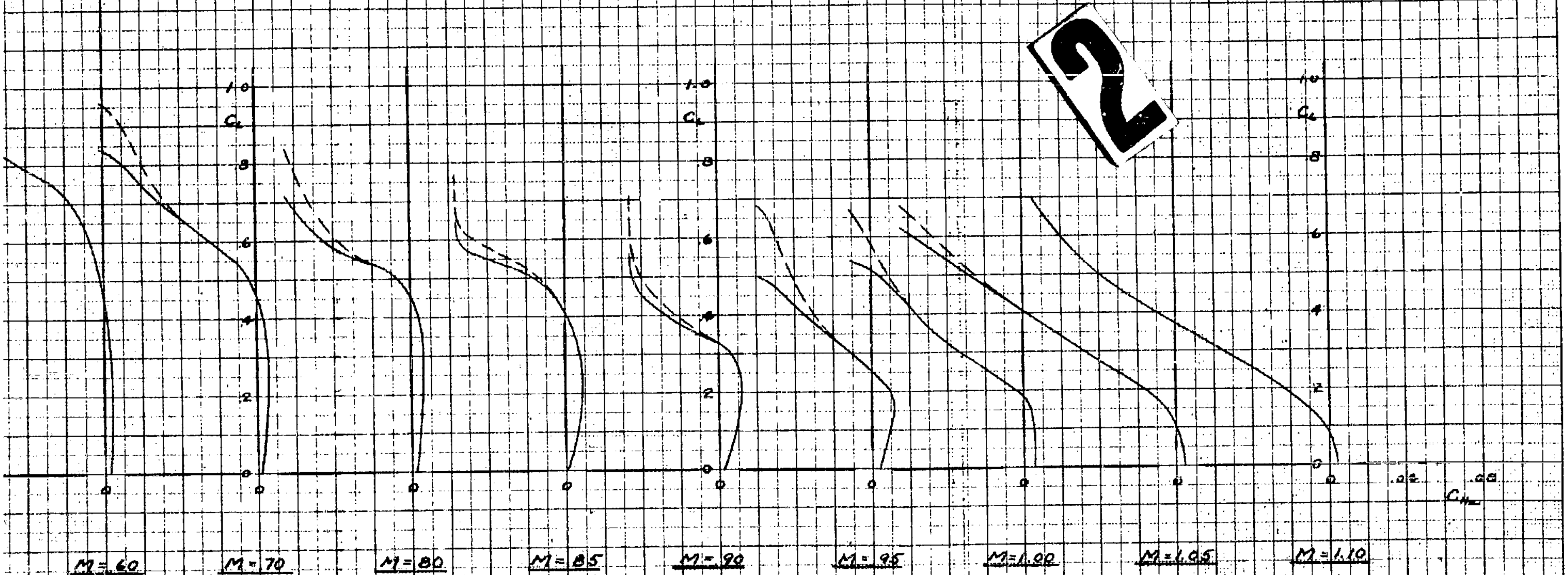
ESTIMATED SHORT CHORD AILERON HINGE MOMENT COEFFICIENTS

BASED ON FLIGHT 19 OF F-86A # 49-1067, CWT REPORTS 52 & 130, AND NAAL 142

SLAT TRANSITION, $\delta_a = 0°$, GRADUAL AND ABRUPT STALL

$c_a/c_w = .2732$, $c_b/c_a = .4390$, $S_a \bar{c}_a = 26.49$ FT.^{3}

$\delta_a = 0°$



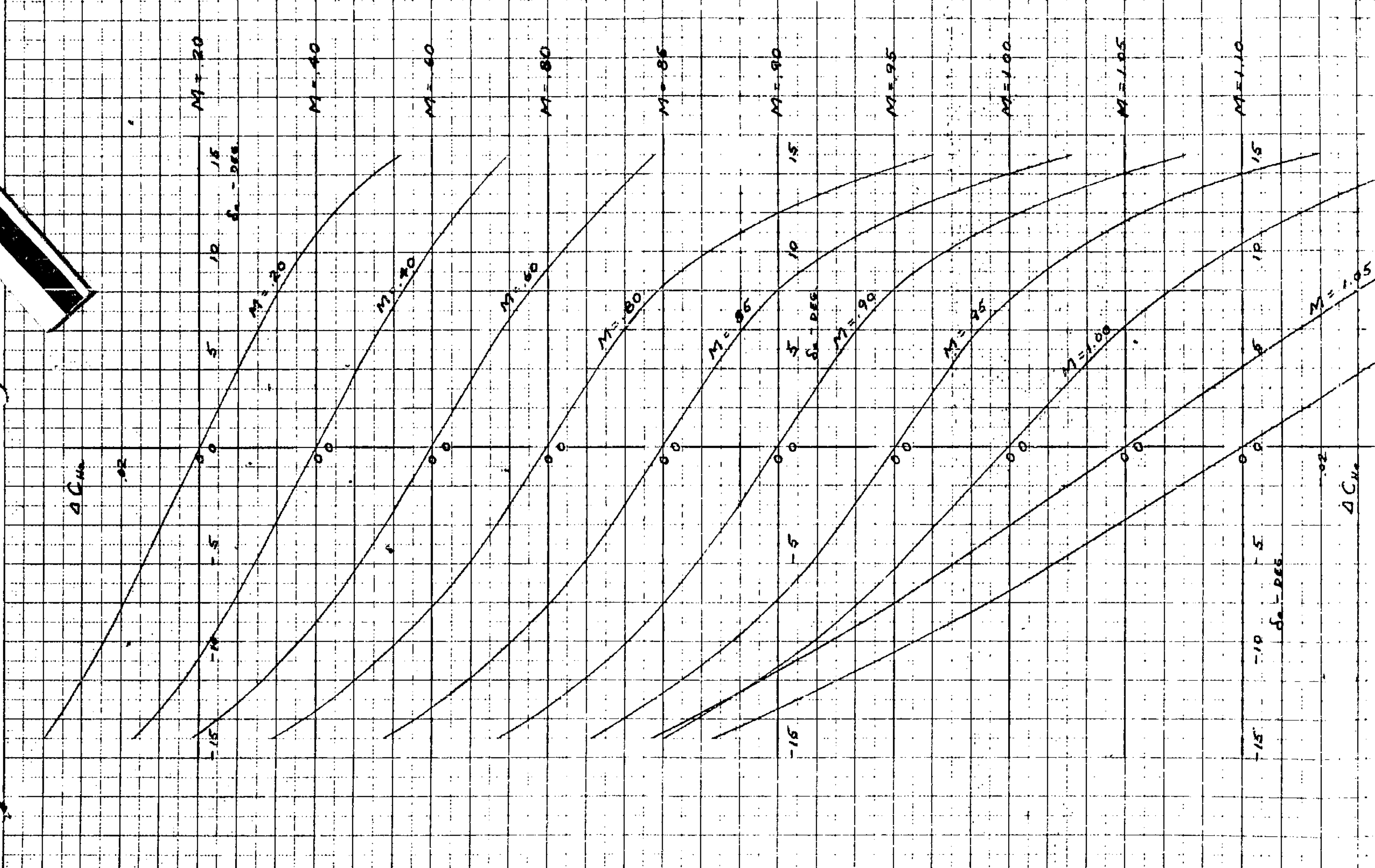
PREPARED BY RPP & GP

CHECKED BY

DATE 1-19-50

NORTH AMERICA[N]

ESTIMATED AERODYNAM[...]

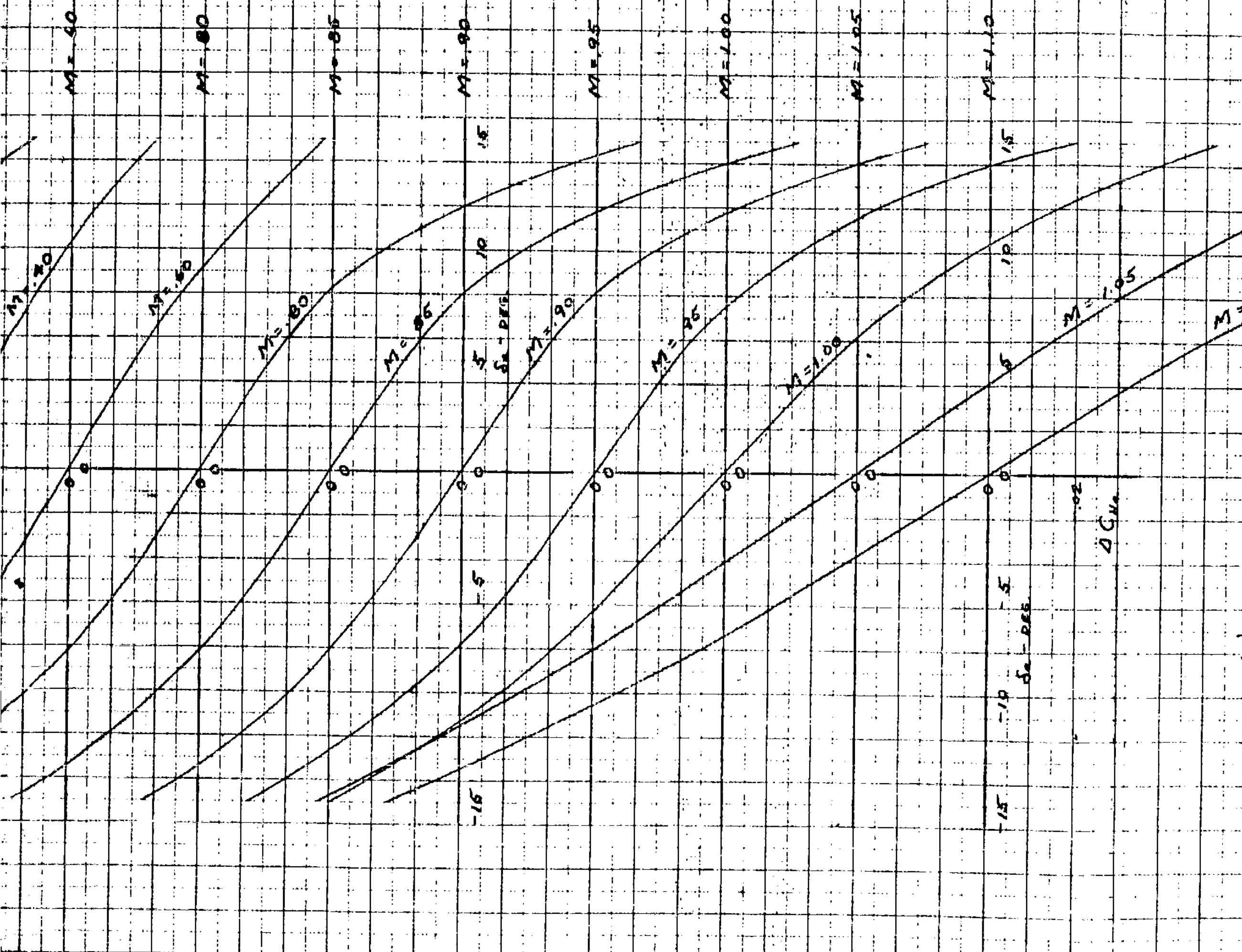


ESTIMATED [...]
CHORD AILER[ON ...]
COEFFICIENTS [...]
(FROM [...]

NOTE:- THESE [...]

THESE [...]
F-86D, [...]
HAVING [...]

Fig. 46



ESTIMATED INCREMENTS OF SHORT CHORD AILERON HINGE MOMENT COEFFICIENTS DUE TO AILERON DEFLECTION

(FROM FLIGHT TEST DATA)

NOTE:-

THESE DATA APPLY FOR ALL C_L'S.

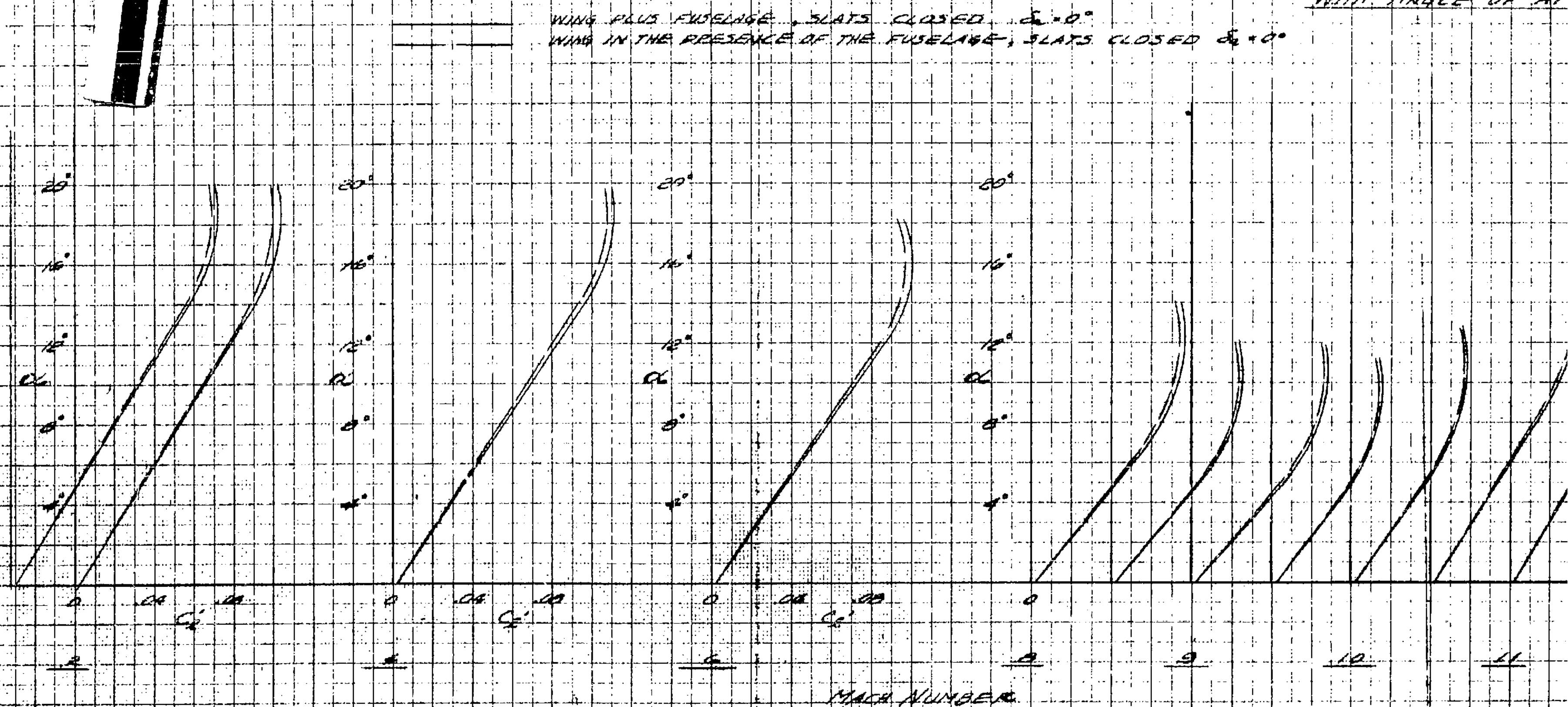
THESE DATA APPLY TO YF-93A, F-86D, AND TO THOSE F-86A AIRPLANES HAVING SHORT CHORD AILERONS.

E.W.J. | CAT | 1-7-43

NORTH AMERI
INGLEWO

ESTIMATED AEROD

THE VARIATION OF ROL
WITH ANGLE OF AT



PREPARED BY E.W.J.	NORTH AMERICAN AVIATION, INC. INGLEWOOD, CALIFORNIA	PAGE NO. 69 OF 86	
CHECKED BY L.H.G.		REPORT NO. NA-50-1211	
DATE 1-7-48	ESTIMATED AERODYNAMIC CHARACTERISTICS	F-86E MODEL NO.	

Fig. 47

THE VARIATION OF ROLLING MOMENT DUE TO LIFT WITH ANGLE OF ATTACK. (LIFT ON LEFT WING ONLY)

WING PLUS FUSELAGE, SLATS CLOSED $\delta_a = 0°$

WING IN THE PRESENCE OF THE FUSELAGE, SLATS CLOSED $\delta_a = 0°$

NORTH AMERIC[...]
INGLEWOO[...]

PREPARED BY LRS.
REVISED 5-4-48

ESTIMATED AERO[...]

THE VARIATION OF ROLLING MOME[...]
WITH ANGLE OF ATTACK, S[...]

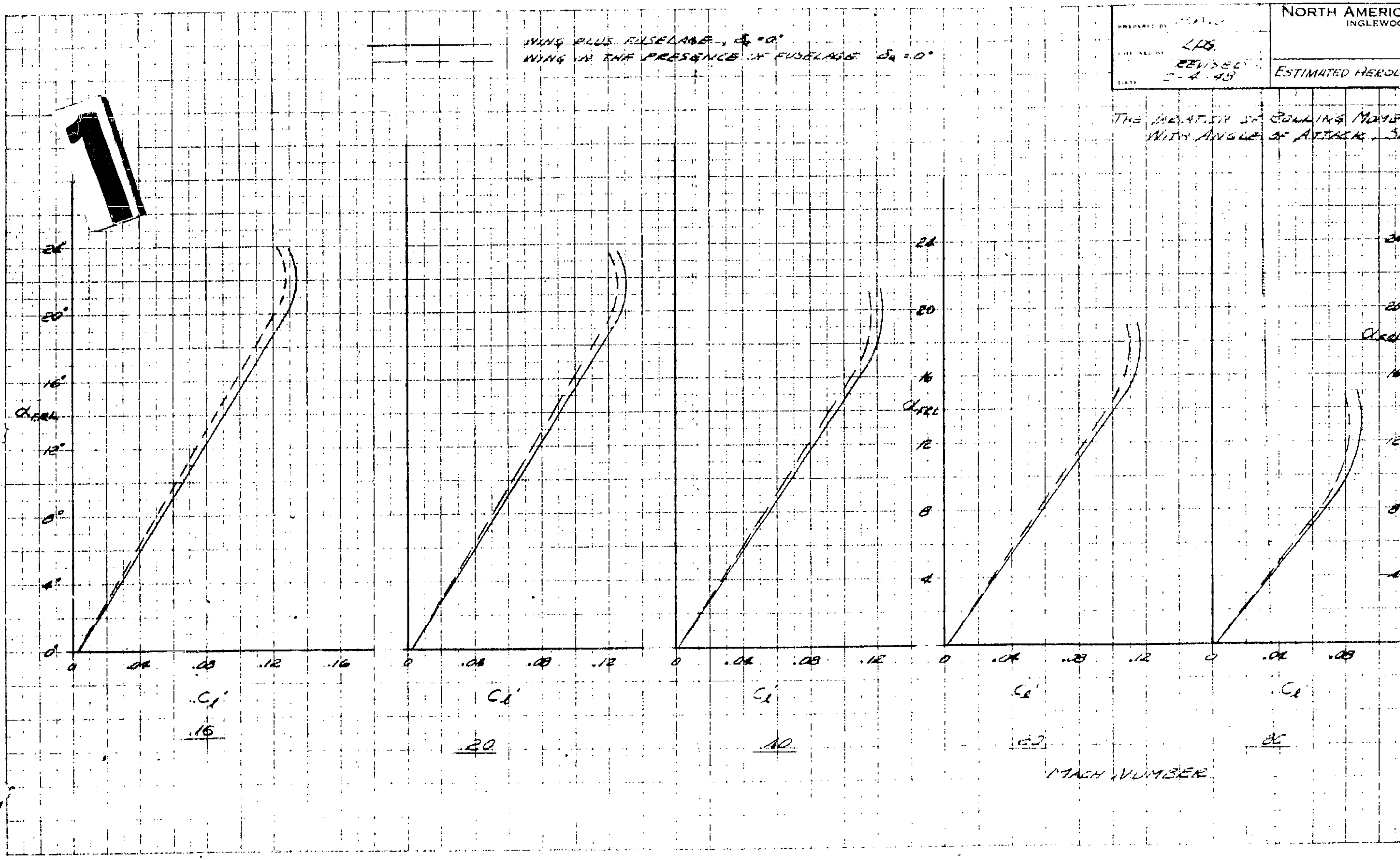
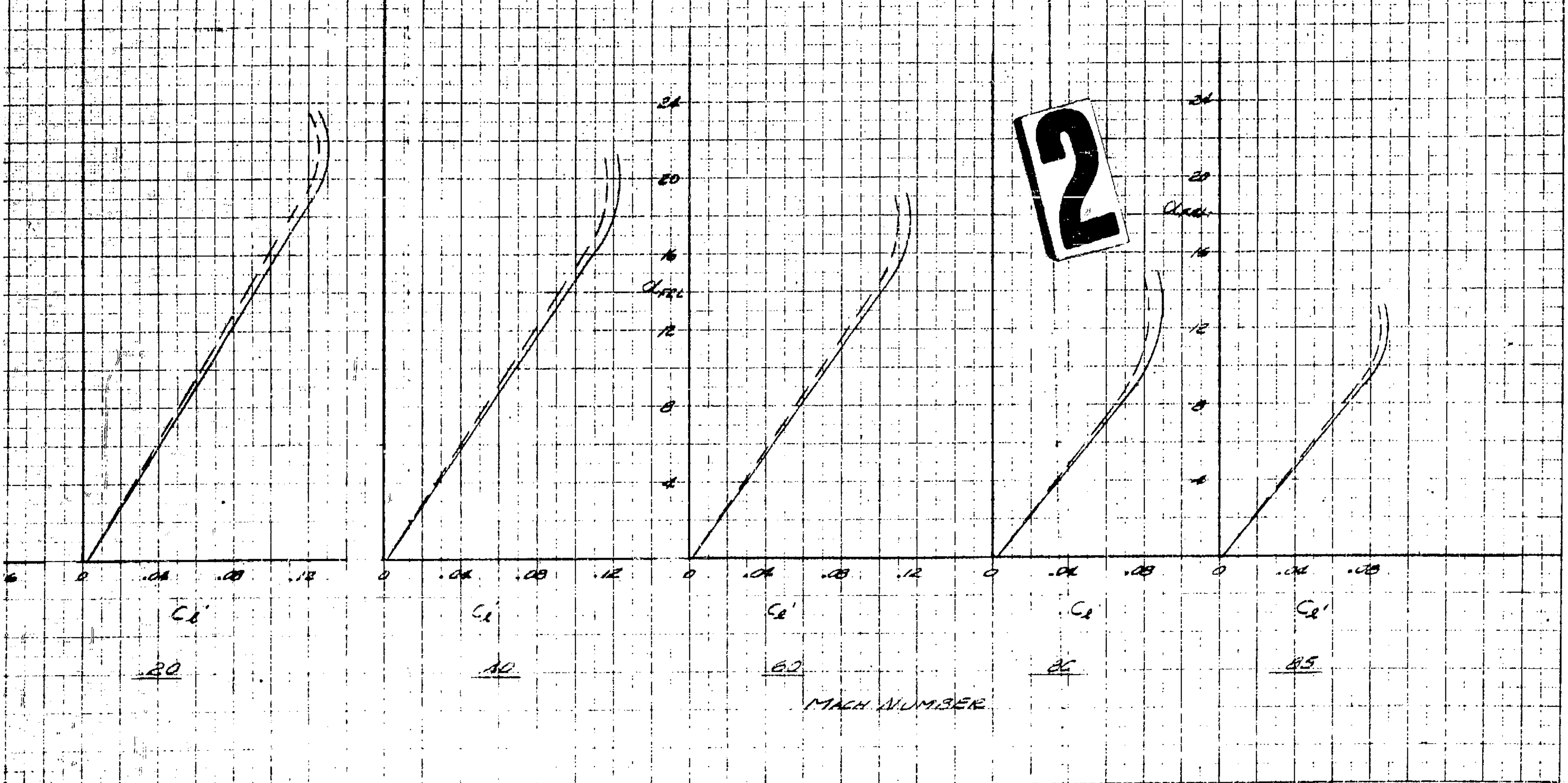


Fig. 48

THE VARIATION OF ROLLING MOMENT DUE TO LIFT ON LEFT WING WITH ANGLE OF ATTACK, SLATS OPEN

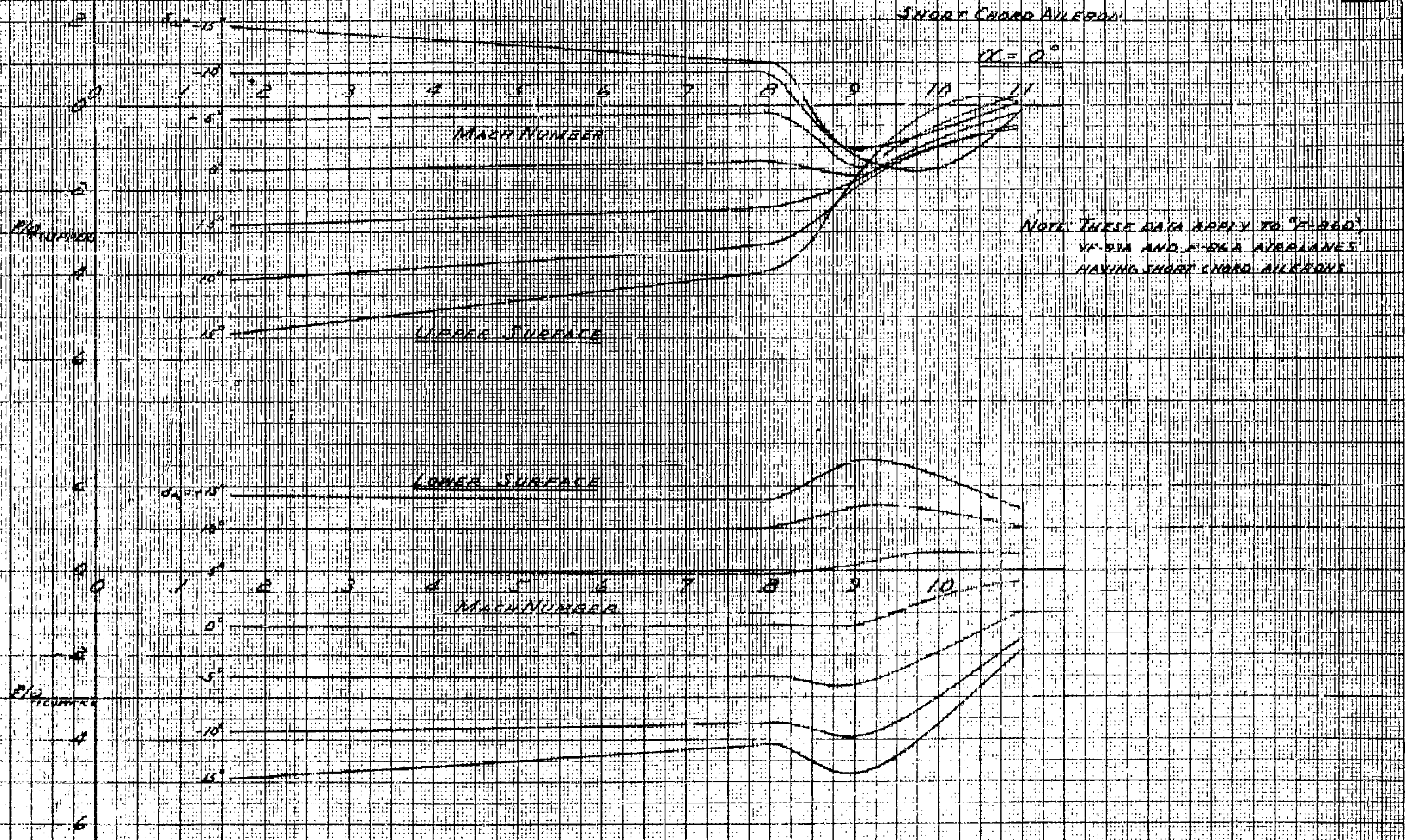
WING PLUS FUSELAGE, $\delta_a = 0°$
WING IN THE PRESENCE OF FUSELAGE $\delta_a = 0°$



PREPARED BY O/A	NORTH AMERICAN AVIATION, INC.		PAGE NO 71 OF 82
CHECKED BY G P			REPORT NO NA-50-1277
DATE 8-23-49	ESTIMATED AERODYNAMIC CHARACTERISTICS		MODEL NO F-86E

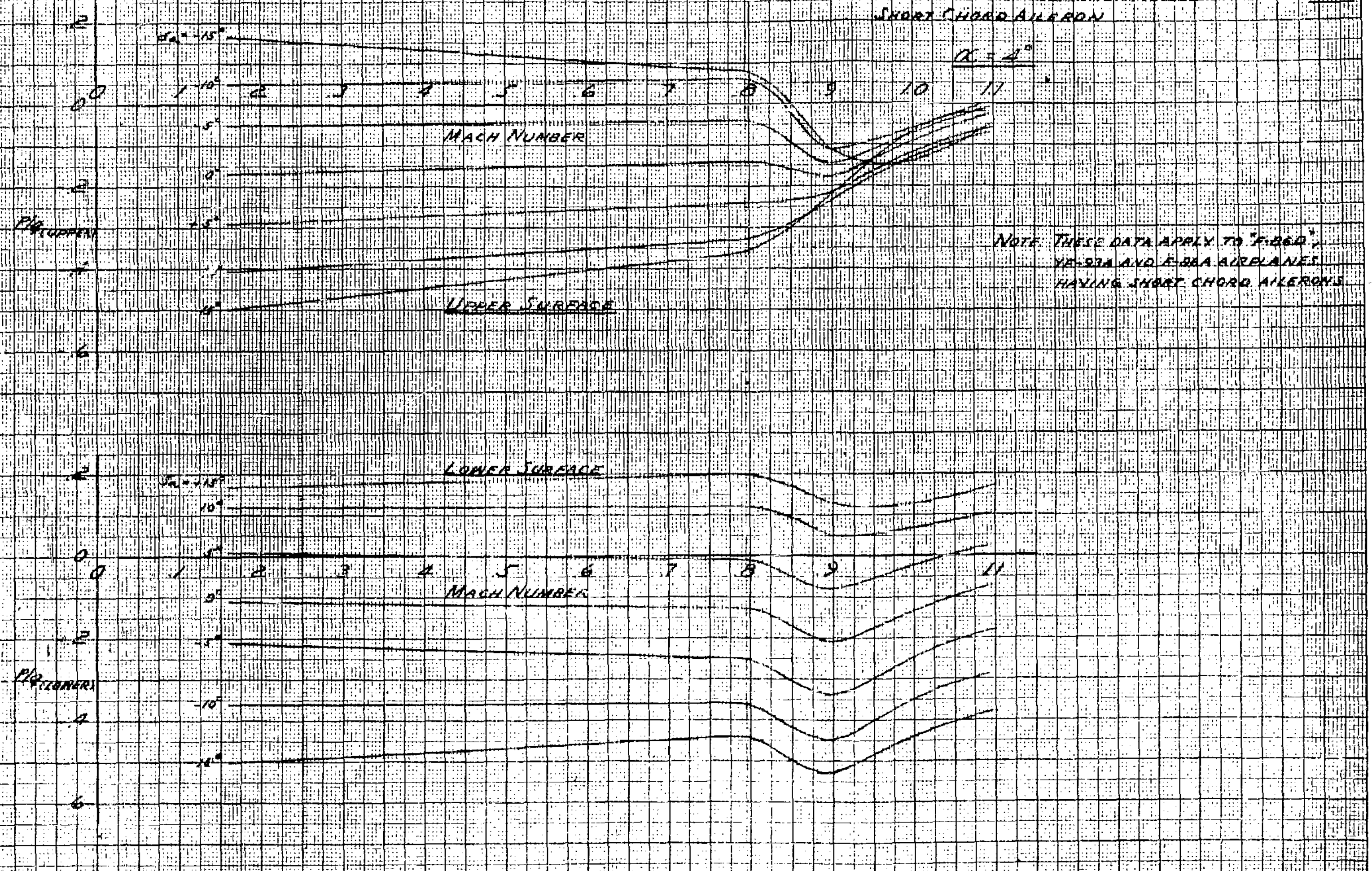
ESTIMATED AILERON PADDLE BALANCE CHAMBER AVERAGE PRESSURE COEFFICIENTS VS. MACH NUMBER SHORT CHORD AILERON

FIG 49



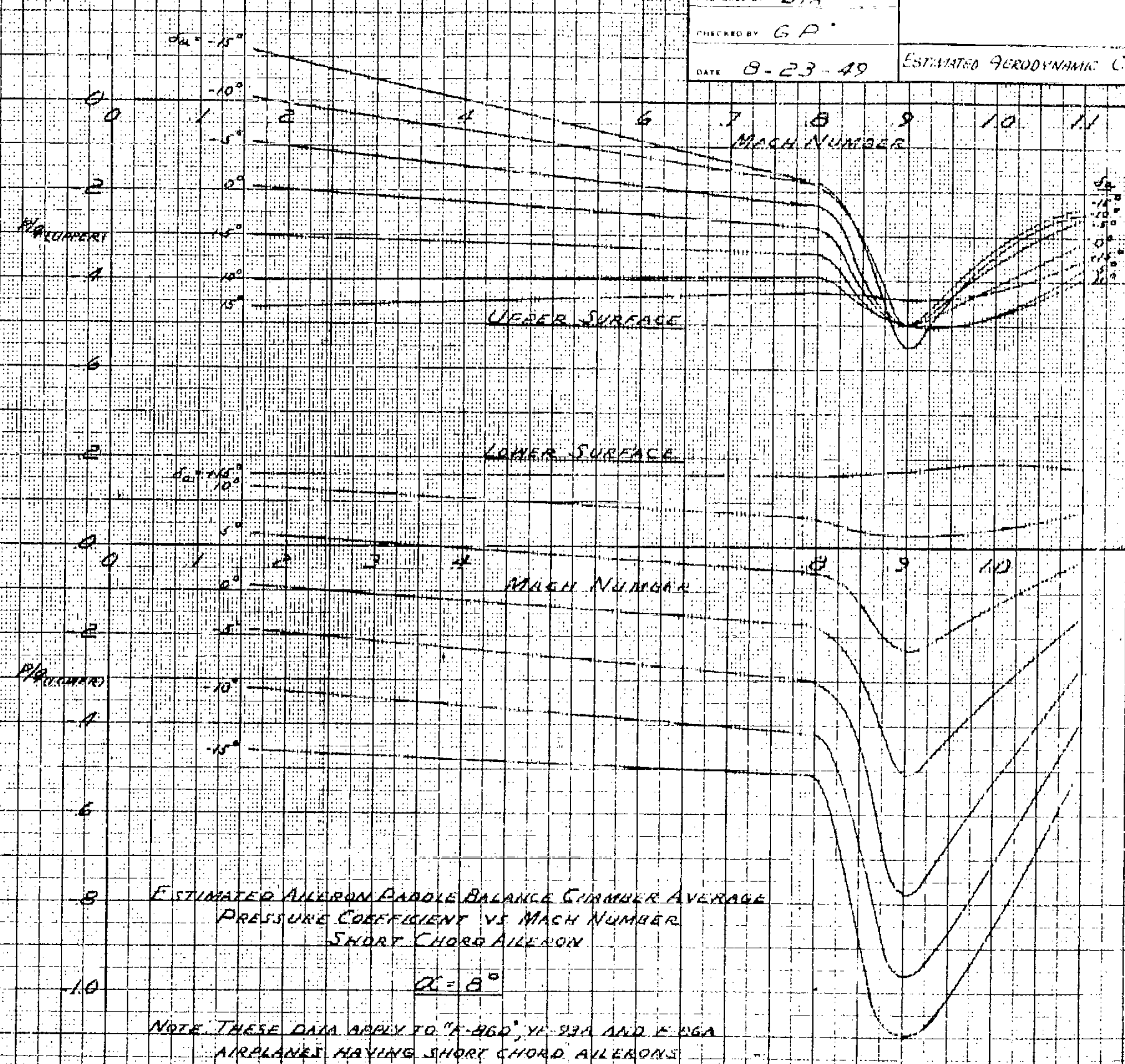
ESTIMATED AILERON PADDLE BALANCE CHAMBER AVERAGE PRESSURE COEFFICIENT VS MACH NUMBER
SHORT CHORD AILERON

Fig 50



PREPARED BY DJA	NORTH AMERICAN AVIATION, INC.		PAGE NO. 73 OF 82
CHECKED BY G.P.			REPORT NO. NA-50-1277
DATE 8-23-49	ESTIMATED AERODYNAMIC CHARACTERISTICS		MODEL F-86E

Fig. 51



ESTIMATED AILERON PADDLE BALANCE CHAMBER AVERAGE
PRESSURE COEFFICIENT VS MACH NUMBER
SHORT CHORD AILERON

$\alpha = 8°$

NOTE: THESE DATA APPLY TO "F-86D", YF-93A AND F-86A
AIRPLANES HAVING SHORT CHORD AILERONS

PREPARED BY: D J B

CHECKED BY: G. P.

DATE: 12-16-49

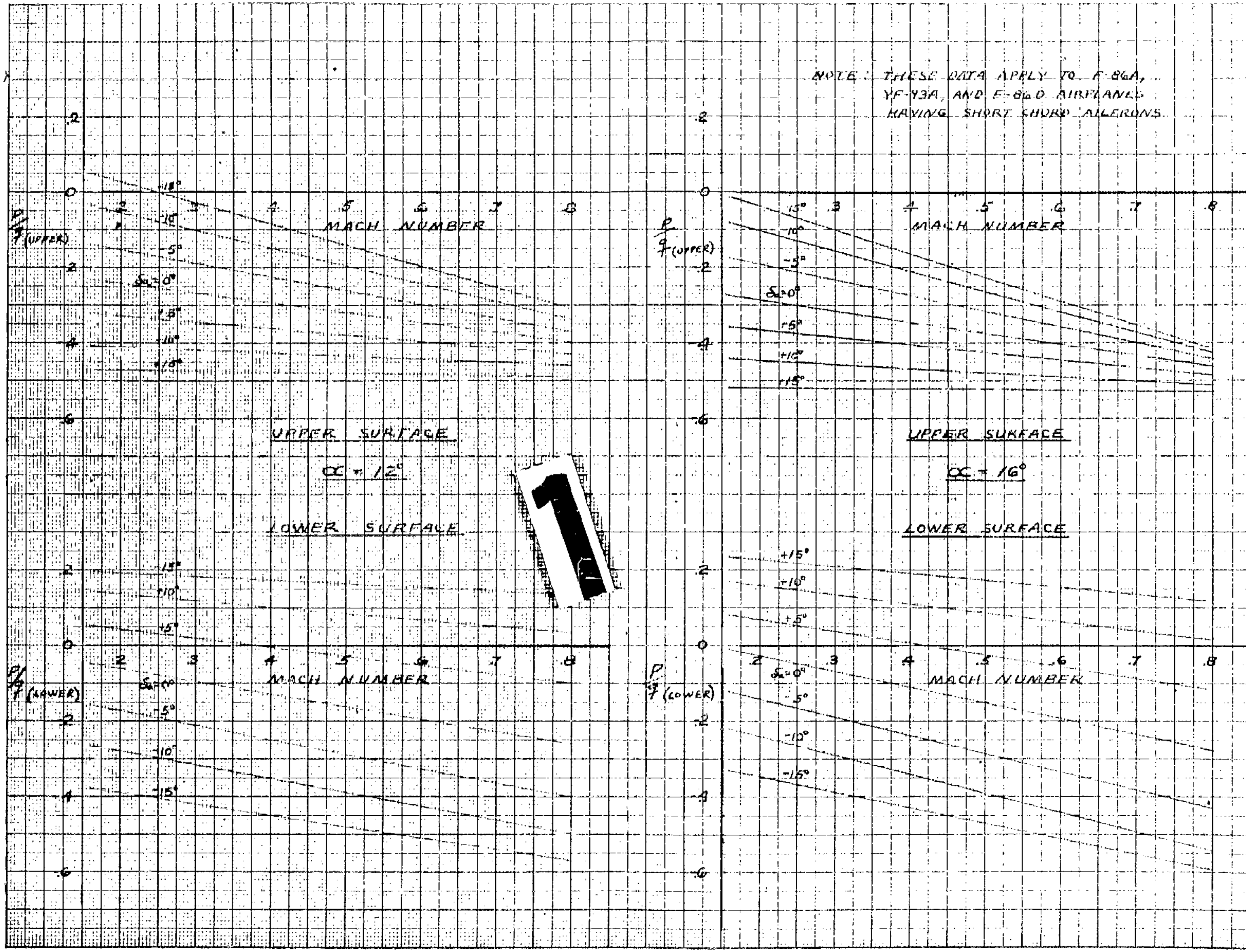
NORTH AMERIC

ESTIMATED AERODY

AILERON PADDLE

PRESSURE COEFFICI

SHORT

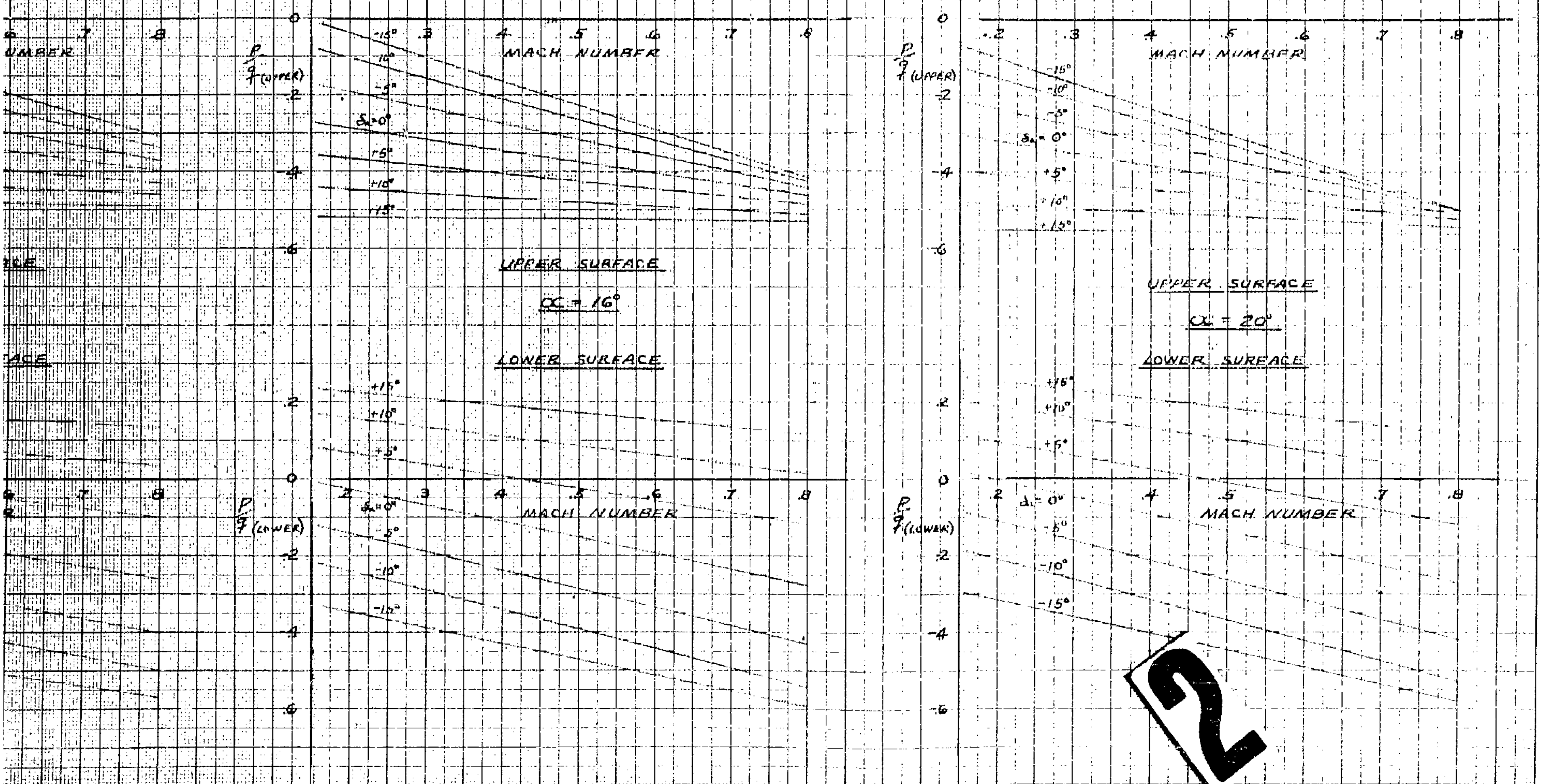


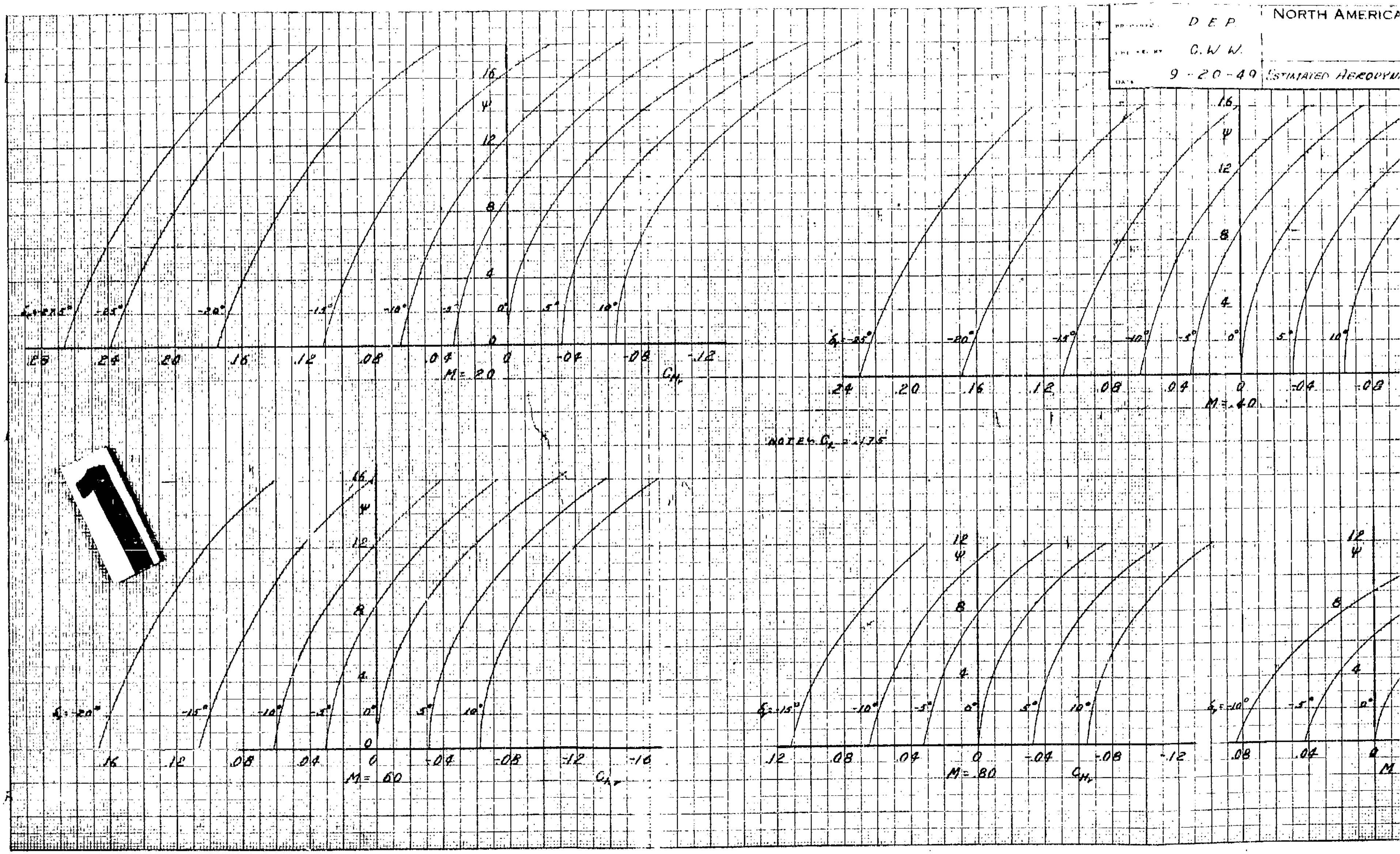
PREPARED BY: D J B	NORTH AMERICAN AVIATION, INC.		PAGE NO. 74 OF 82
CHECKED BY: G. P.			REPORT NO. NA-50-1271
DATE: 12-16-49	ESTIMATED AERODYNAMIC CHARACTERISTICS		MODEL NO. F-86E

NOTE: THESE DATA APPLY TO F-86A, YF-93A, AND F-86D AIRPLANES HAVING SHORT CHORD AILERONS.

AILERON PADDLE BALANCE CHAMBER AVERAGE PRESSURE COEFFICIENT VS. MACH NUMBER
SHORT CHORD AILERON

FIG 52



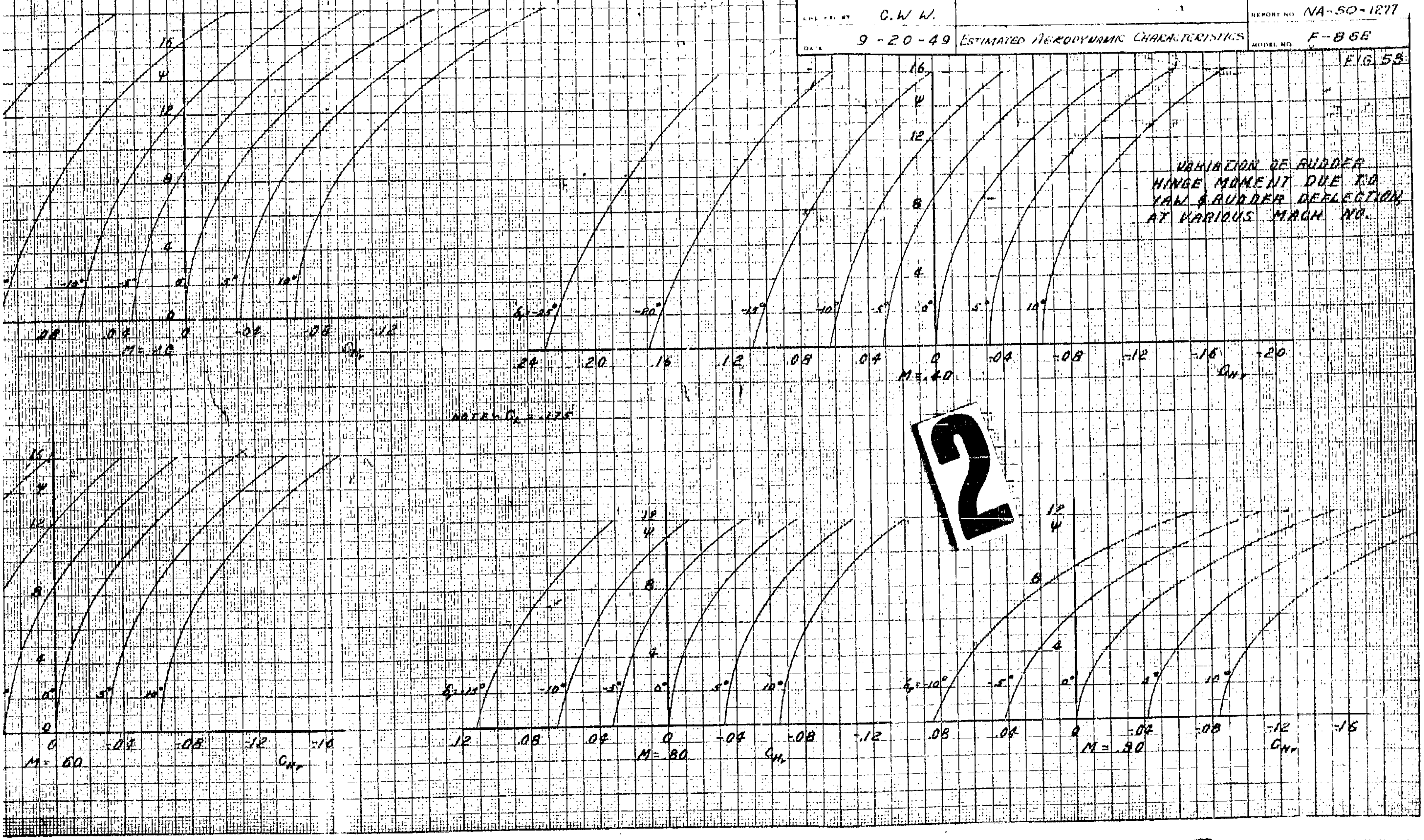


D E P
C. W. W.
9 - 20 - 49
NORTH AMERICA
ESTIMATED AERODYN
M = .20
M = .40
M = .60
M = .80
C_{H_v}
ψ
$\delta_r = -27.5°$
$\delta_r = -25°$
$\delta_r = -20°$
$\delta_r = -15°$
$\delta_r = -10°$
NOTE: C_L = .175

PREPARED BY	D. E. P.	NORTH AMERICAN AVIATION, INC.	PAGE NO. 75 OF 82
CHECKED BY	C. W. W.		REPORT NO. NA-50-1277
DATE	9-20-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO. F-86E

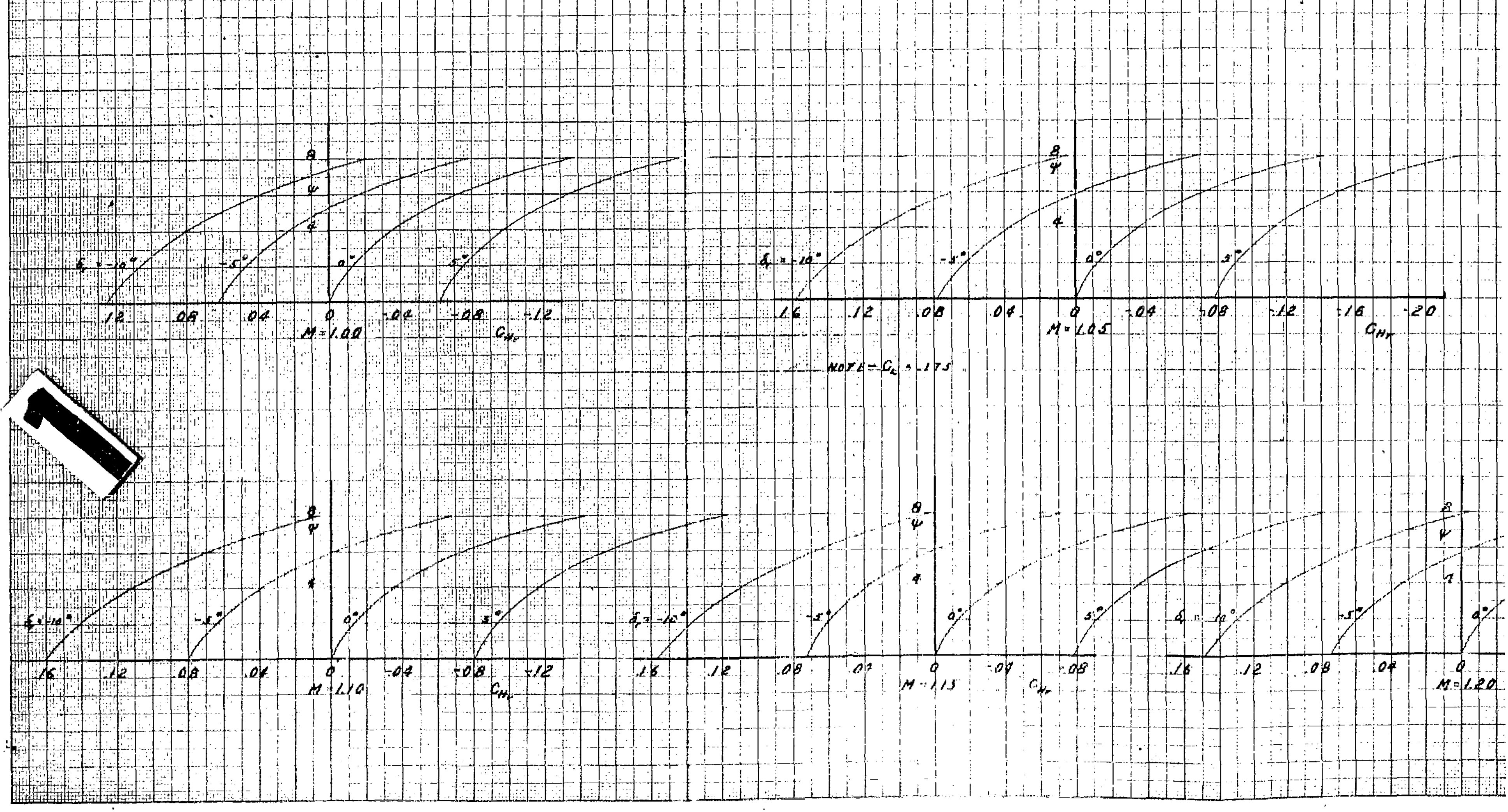
FIG. 53

VARIATION OF RUDDER HINGE MOMENT DUE TO YAW & RUDDER DEFLECTION AT VARIOUS MACH NO.



NORTH AMERICA

D.E.P.
C.W.W.
9-20-49
ESTIMATED AERODYNA



PREPARED BY: D.E.P.	NORTH AMERICAN AVIATION, INC.		PAGE NO. 76 OF 82
CHECKED BY: O.W.W.			REPORT NO. NA-50-1277
DATE: 9-20-49	ESTIMATED AERODYNAMIC CHARACTERISTICS		MODEL NO. F-86E

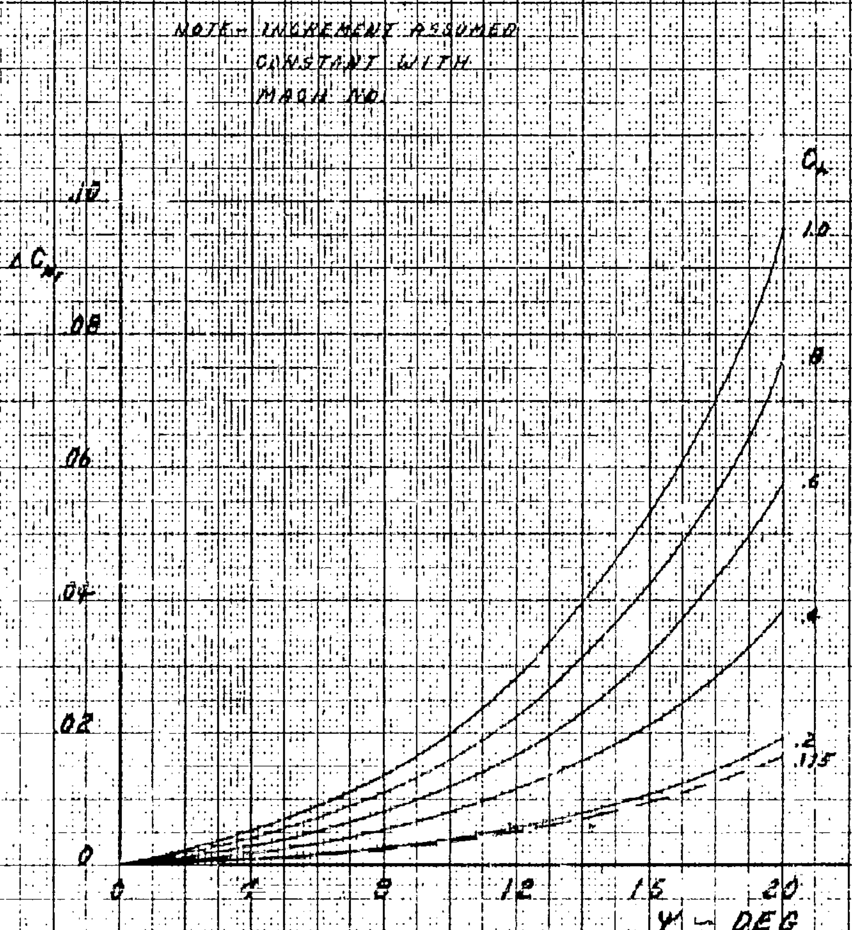
FIG. 54

VARIATION OF RUDDER HINGE MOMENT DUE TO YAW & RUDDER DEFLECTION AT VARIOUS MACH NO.

PREPARED BY D.E.P	NORTH AMERICAN AVIATION, INC.	PAGE NO. 77 OF 80	
CHECKED BY C.W.W.		REPORT NO. NA-50-1277	
DATE 9-19-49	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO. F-86E	

FIG 55

VARIATION OF INCREMENT IN RUDDER HINGE MOMENT DUE TO C_L WITH YAW



GP	NORTH AMERICAN AVIATION, INC.		78 of 82
WES			NA-50-1271
MAY 8, 1950	ESTIMATED AERODYNAMIC CHARACTERISTICS		F-86E

FIG. 56

F-86A

120 GAL EXTERNAL FUEL TANK WITH LARGE* FIN

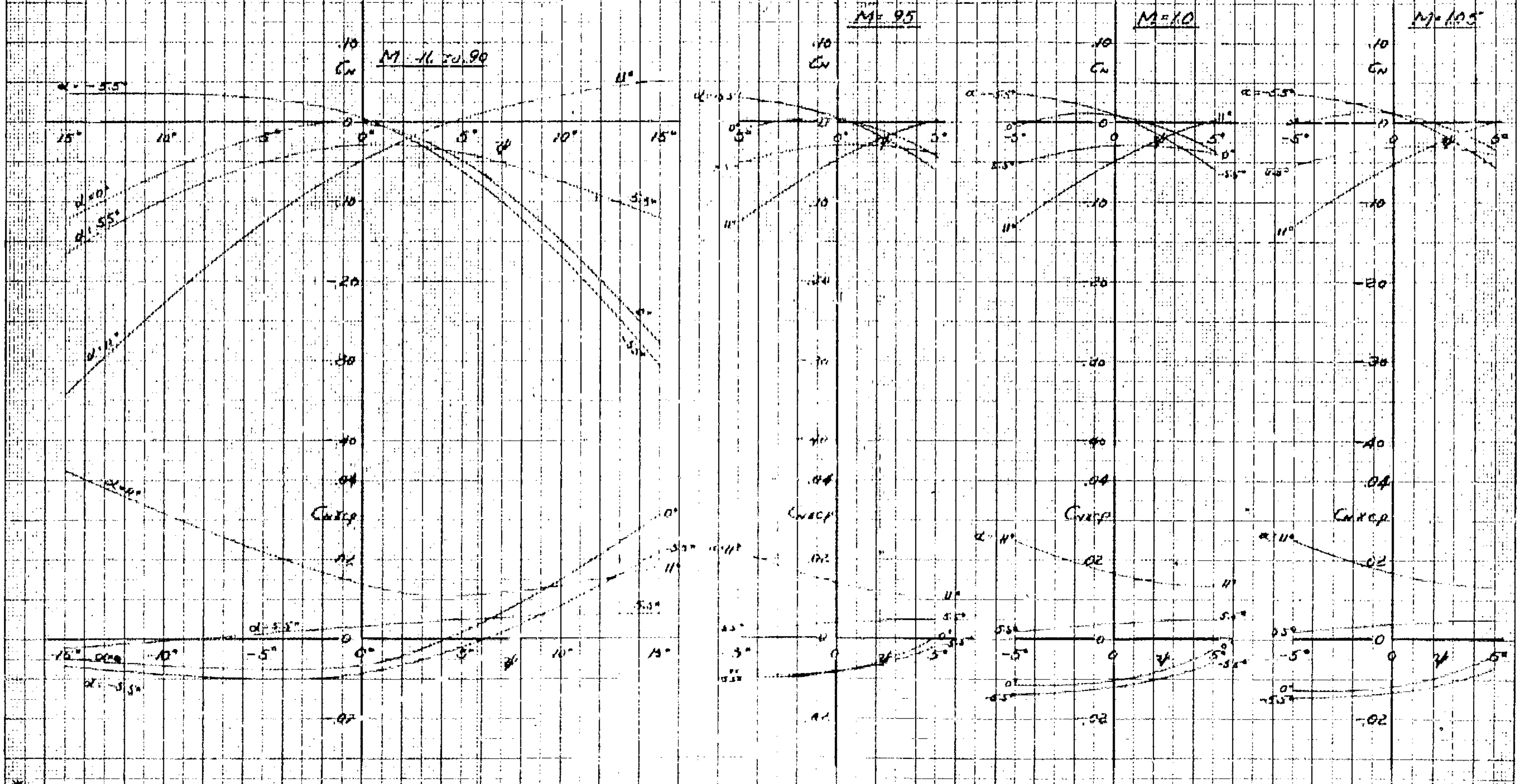
NORMAL FORCE COEFFICIENT AND CENTER OF PRESSURE

$C_N = N/qS_p$ WHERE: N = NORMAL FORCE, POSITIVE UP

S_p = PLAN VIEW AREA OF TANK = 16.0 SQ FT

C.P. = LOCATION OF CENTER OF PRESSURE FROM 42% TANK STA. IN TANK LENGTHS (POSITIVE = FWD OF 42%)

ψ = ANGLE OF YAW, α = AIRPLANE ANGLE OF ATTACK



* NOMINAL 600 SQ IN FIN WITH 17° CATHEDRAL

F-86A

120 Gal. External Fuel Tank with Large* Fin

SIDE FORCE COEFFICIENT AND CENTER OF PRESSURE

Left Wing Tank Only

Prepared	G.P.
Checked	WES
Date	MAY 9, 1950

NORTH AMERICAN AVIATION, INC.

Estimated Aerodynamic Characteristics

Page No.	79 of 82
Report No.	NA-50-1277
Model No.	F-86E

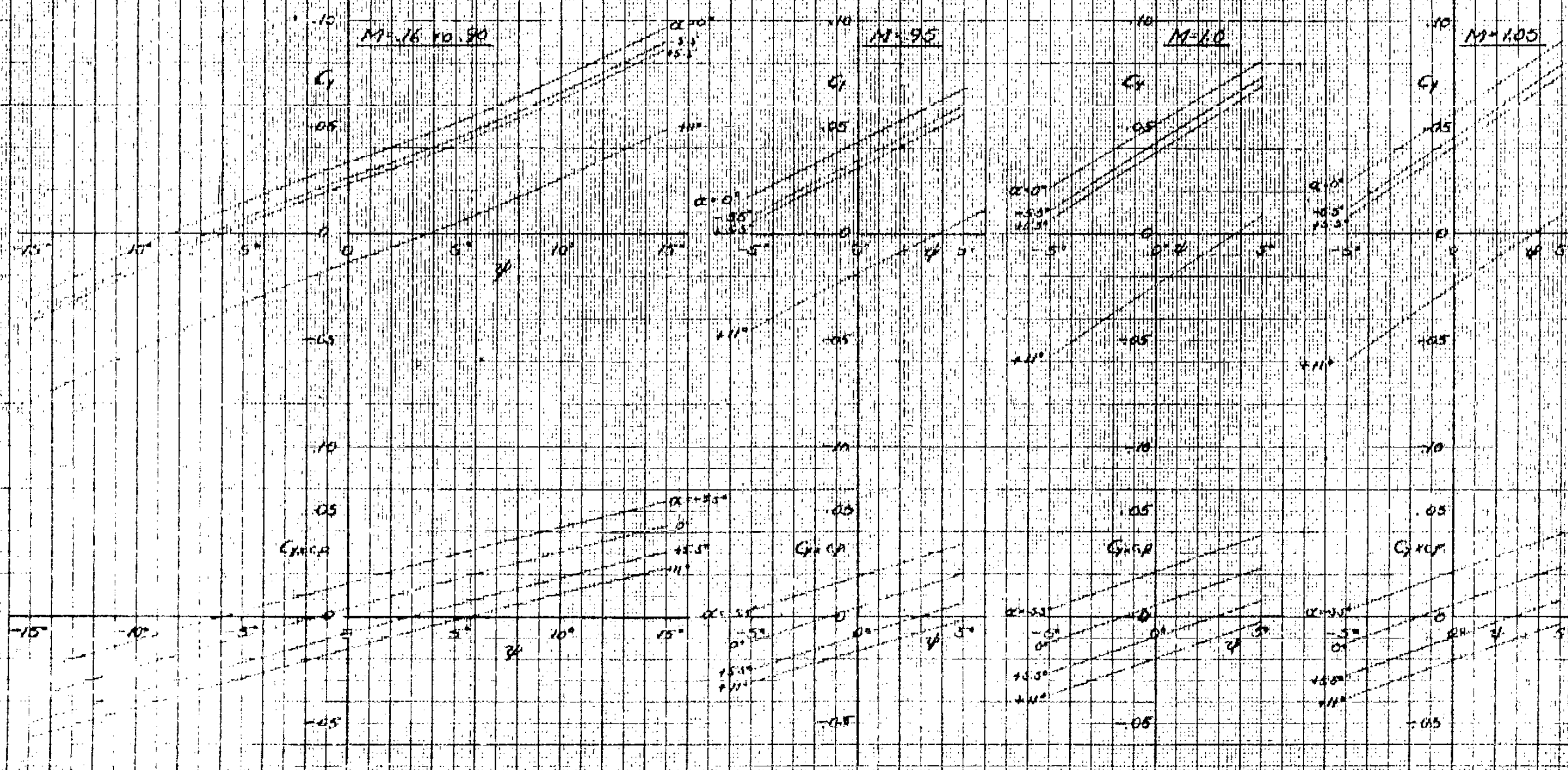
Fig 57

C_Y = Side Force Coefficient = $Y/q\,S_p$ where Y = Side Force, Positive to Right

S_p = Tank Plan View Area = 16.0 sq ft

C.P. = Location of Center of Pressure from 42% Tank Sta. in Tank Lengths (Positive Fwd of 42%)

ψ = Angle of Yaw, α = Airplane Angle of Attack



* Nominal 500 sq in fin with 17° cathedral

PREPARED BY GP	NORTH AMERICAN AVIATION, INC.	PAGE NO. 80 OF 82	
CHECKED BY W.E.S.		REPORT NO. NA 50-1271	
DATE MAY 11 1950	ESTIMATED AERODYNAMIC CHARACTERISTICS	MODEL NO. F-86E	

FIG. 60

F-86A
120 GAL EXTERNAL FUEL TANK SUPPORT FAIRING
SUPPORT FAIRING SIDE FORCE SECTION COEFFICIENT AND CENTER OF PRESSURE

LEFT WING TANK ONLY

C_{Y_F} = SECTION SIDE FORCE COEFFICIENT (POSITIVE TOWARD RIGHT) = $\frac{Y_F}{q C_F}$

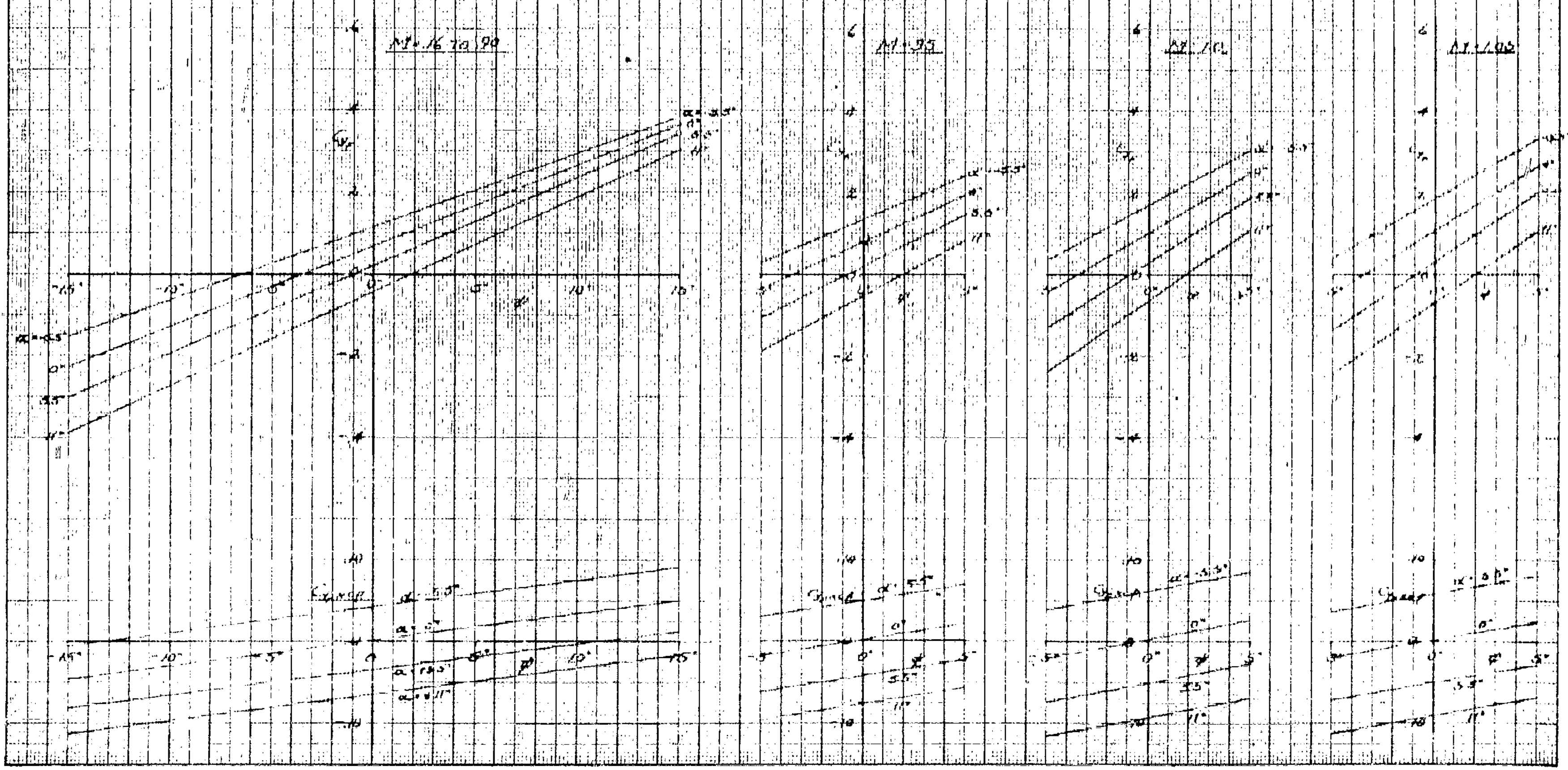
WHERE: Y_F = FAIRING SIDE FORCE (LB/FT) AT W.S. 36

C_F = FAIRING CHORD = 3.35 FT.

C.P. = LOCATION OF CENTER OF PRESSURE FROM 42% TANK STA (66.4% FAIRING STA) IN FAIRING CHORDS (POSITIVE FWD. OF 42% TANK STA)

ψ = ANGLE OF YAW

α = AIRPLANE ANGLE OF ATTACK



F-86 TYPE SLAT

TABLE OF RETRACTED SLAT LOAD CHARACTERISTICS AT VARIOUS MACH NO.S AND ANGLES OF ATTACK

		SLAT NO. 1				SLAT NO. 2				SLAT NO. 3			
M	α	C_n	X_n	C_c	Z_c	C_n	X_n	C_c	Z_c	C_n	X_n	C_c	Z_c
.300	2.1°	-.191	22.4	-.149	12.2	-.249	30.2	-.149	12.4	-.250	28.6	-.115	10.1
	0°	.148	45.6	-.330	-5.6	.128	53.0	-.402	-5.2	.077	48.2	-.430	-3.3
	2.1°	.435	46.0	0	30	.515	45.6	.152	35.8	.460	39.6	.090	37.6
	4.3°	.825	42.0	.166	32.5	.844	42.8	.290	19.4	.784	41.6	.192	18.2
	6.6°	1.281	41.3	.403	22.2	1.304	42.1	.500	14.4	1.360	38.2	.406	19.4
	8.7°	1.394	41.2	.486	19.5	1.350	41.4	.701	13.2	1.599	34.6	.530	12.2
.600	2.2°	-.193	26.0	-.165	3.9	-.226	27.5	-.152	9.0	-.253	29.5	-.127	9.5
	0°	.140	49.2	-.281	-3.7	.073	56.2	-.409	-1.3	.068	57.4	-.479	-1.3
	2.2°	[illegible]	4.9	.085	46.5	.640	43.4	.126	27.8	.607	41.2	.091	27.0
	4.4°	.943	42.4	.155	34.7	1.129	44.1	.326	18.0	1.032	42.5	.255	17.3
	6.5°	1.345	41.8	.390	23.6	1.578	47.6	.570	15.6	1.555	40.8	.450	16.5
	8.7°	1.911	41.0	.620	20.4	2.240	42.8	.835	18.4	2.026	40.6	.645	13.8
.801	2.2°	-.327	27.5	-.174	8.7	-.344	26.2	-.156	8.8	-.238	23.2	-.156	8.0
	0°	.162	52.1	-.401	-4.8	.142	53.1	-.478	-5.3	.124	48.8	-.438	-3.5
	2.5°	[illegible]	46.3	.201	46.3	.772	47.1	.135	27.8	.738	44.1	.130	24.2
	4.5°	.988	46.2	[illegible]	34.5	1.362	48.8	.342	19.9	1.352	45.8	.265	15.8
	6.7°	1.355	46.5	.366	28.5	1.485	52.1	.434	13.0	1.675	44.0	.346	10.4
	8.9°	1.645	46.6	.577	26.8	1.865	46.6	.581	12.1	1.665	44.9	.606	11.8
.851	0°	.172	52.2	-.434	-6.5	.238	52.8	-.676	-12.4	.296	52.7	-.655	-12.1
	2.3°	.553	48.4	.015	19.8	.700	49.8	.118	36.5	.866	49.8	.112	29.2
	4.5°	.913	46.6	.136	33	1.120	52.1	.276	21.6	1.252	49.8	.212	22.9
	6.7°	1.236	47.5	.228	31.8	1.507	54.2	.385	25.2	1.476	49.8	.235	20.6
	8.8°	1.463	48.2	.347	28.4	1.725	52.3	.482	19.6	1.590	48.6	.532	18.4
.885	0°	.140	57.8	-.114	-3.4	.116	60.7	-.698	-12.2	.142	61.0	-.868	-4.2
	2.3°	.814	49.0	.061	48.7	.378	52.1	.108	32.4	.383	51.0	.085	34.7
	4.5°	.835	47.5	.161	43.9	1.127	52.5	.238	25.5	1.105	52.2	.133	25.0
	6.7°	1.111	47.8	.181	34.0	1.391	52.5	.315	20.8	1.312	50.0	.228	22.1
	9.0°	1.381	48.5	.277	29.8	1.591	56.6	.379	20.0	1.420	48.4	.276	21.0
.903	-2.3°	-.132	25.0	-.162	8.1	-.138	26.0	-.124	6.6	-.132	20.0	-.156	5.6
	-0.1°	.165	58.7	-.488	-4.2	.302	54.0	-.677	-8.6	.210	51.3	-.467	-8.4
	2.5°	.457	47.2	[illegible]	-13.8	[illegible]	49.7	.162	43.8	.62	48.5	.155	43.4
	4.5°	.759	46.0	.081	52.5	1.125	53.3	.209	24.5	.988	46.9	.16	26.8
	6.4°	1.088	47.2	[illegible]	31.6	1.324	52.1	.342	21.5	1.225	40.7	.205	25.0

C_n = Force Coefficient Perpendicular to WRP, Positive Upward.
X_n = Distance of C.P. Aft of Slat L.E., Measured Parallel to WRP, Per Cent Slat Chord.
C_c = Force Coefficient Parallel to WRP, Positive Forward.
Z_c = Distance of C.P. Above WRP, Per Cent Slat Chord.

Note – Tabulated Data Result from Integration of Slat Pressure Distributions Obtained from Tests of 1/8 Scale Model, CWT Rep. # 23.

100% Slat Chord = 13 in. Full Scale.

$C_n, C_c = F/sq$, Where S = Slat Area Projected on WRP.
M = Test Mach Number.
α = Model Angle of Attack Tunnel Corrected.

NORTH AMERICAN AVIATION, INC.

Prepared by D.E.P. Checked by P.S.I. Date 6-20-50
Page No. 81 of 82 Report No. NA-50-1211 Model No. F-86E

FIG. 60

SLAT OPENING FORCE COEFFICIENT, C_S, VS ANGLE OF ATTACK FOR VARIOUS MACH NOS AND SLATS

SLATS FULLY RETRACTED

SLAT TRACK "B"

C_S CALCULATIONS BASED ON THE FOLLOWING SLAT ROLLER TRACK DIMENSIONS:

RADIUS, R_R 32.856 IN.
CENTER OF ROTATION
AFT OF L.E., X_R 15.800 IN.
BELOW WRP, Z_R 32.000 IN.

$$C_S = \frac{C_N(X_N - X_R) + C_C(Z_C + Z_R)}{R_R}$$

C_N, C_C, X_N, Z_C OBTAINED FROM PRESSURE DISTRIBUTION DATA OF 1/9 SCALE MODEL, CWT REP. #29

MACH NO.	SYMBOL
.300	○
.600	△
.801	□
.851	◇
.882	▽
.903	◁

$$C_S = \frac{F}{Sq} = f(\alpha)$$

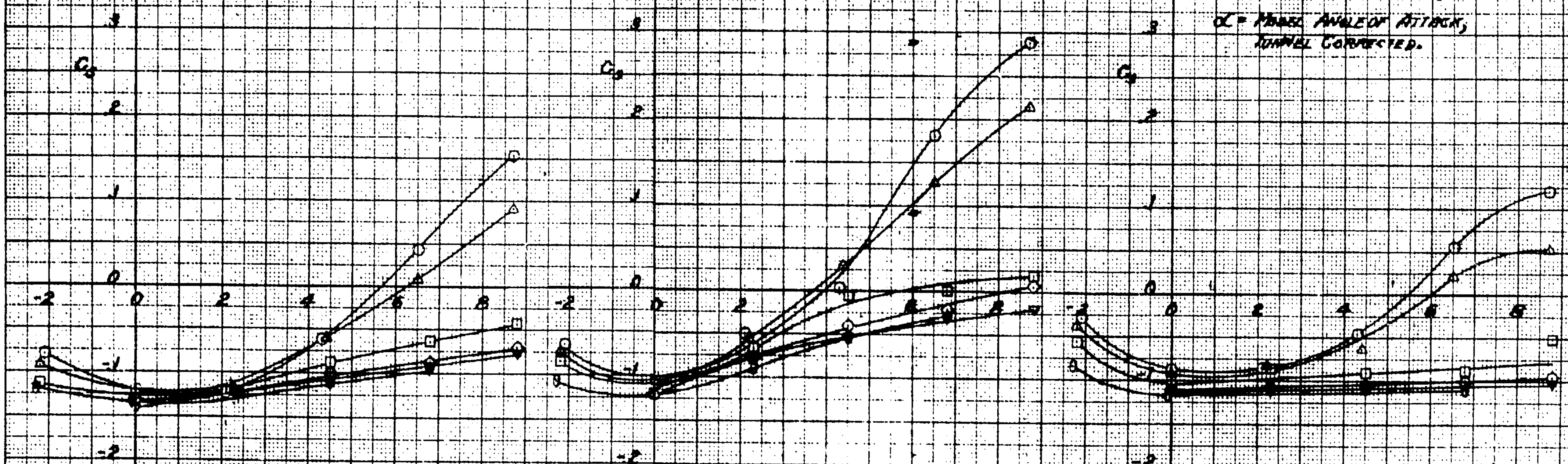
WHERE:

F = TOTAL FORCE ACTING TANGENTIALLY TO ℄ OF TRACK ROLLERS, LBS. (POSITIVE WHEN TENDING TO EXTEND SLAT)

S = TOTAL AREA OF SLAT AS PROJECTED IN WRP, FT.²

q = DYNAMIC PRESSURE, LBS/FT.²

α = MODEL ANGLE OF ATTACK, TUNNEL CORRECTED.



SLAT No. 1 SLAT No. 2 SLAT No. 3

AD 69271

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DEPARTMENT OF THE AIR FORCE
HEADQUARTERS AIR FORCE MATERIEL COMMAND
WRIGHT-PATTERSON AIR FORCE BASE OHIO

FEB 19 2002

MEMORANDUM FOR DTIC/OCQ (ZENA ROGERS)
8725 JOHN J. KINGMAN ROAD, SUITE 0944
FORT BELVOIR VA 22060-6218

FROM: AFMC CSO/SCOC
4225 Logistics Avenue, Room S132
Wright-Patterson AFB OH 45433-5714

SUBJECT: Technical Reports Cleared for Public Release

References: (a) HQ AFMC/PAX Memo, 26 Nov 01, Security and Policy Review, AFMC 01-242 (Atch 1)

(b) HQ AFMC/PAX Memo, 19 Dec 01, Security and Policy Review, AFMC 01-275 (Atch 2)

(c) HQ AFMC/PAX Memo, 17 Jan 02, Security and Policy Review, AFMC 02-005 (Atch 3)

1. Technical reports submitted in the attached references listed above are cleared for public release in accordance with AFI 35-101, 26 Jul 01, *Public Affairs Policies and Procedures*, Chapter 15 (Cases AFMC 01-242, AFMC 01-275, & AFMC 02-005).

2. Please direct further questions to Lezora U. Nobles, AFMC CSO/SCOC, DSN 787-8583.

Lezora U. Nobles

LEZORA U. NOBLES
AFMC STINFO Assistant
Directorate of Communications and Information

Attachments:
1. HQ AFMC/PAX Memo, 26 Nov 01
2. HQ AFMC/PAX Memo, 19 Dec 01
3. HQ AFMC/PAX Memo, 17 Jan 02

cc:
HQ AFMC/HO (Dr. William Elliott)

DEPARTMENT OF THE AIR FORCE
HEADQUARTERS AIR FORCE MATERIEL COMMAND
WRIGHT-PATTERSON AIR FORCE BASE OHIO

JAN 17 2002

MEMORANDUM FOR HQ AFMC/HO

FROM: HQ AFMC/PAX

SUBJECT: Security and Policy Review, AFMC 02-005

1. The reports listed in your attached letter were submitted for security and policy review IAW AFI 35-101, Chapter 15. They have been cleared for public release.

2. If you have any questions, please call me at 77828. Thanks.

James A. Morrow

JAMES A. MORROW
Security and Policy Review
Office of Public Affairs

Attachment:
Your Ltr 14 January 2002

14 January 2002

MEMORANDUM FOR: HQ AFMC/PAX
Attn: Jim Morrow

FROM: HQ AFMC/HO

SUBJECT: Releasability Reviews

1. Please conduct public releasability reviews for the following attached Defense Technical Information Center (DTIC) reports:

    a. *Flight Test Program for Model P-86 Airplane Class – Jet Propelled Fighter*, 2 December 1946; DTIC No. AD-B804 069.

    b. *Physiological Recognition of Strain in Flying Personnel: Eosinopenia in F-86 Combat Operations*, September 1953; DTIC No. AD- 020 375.

    c. *Phase IV Performance Test of the F-86F-40 Airplane Equipped with 6x3-inch Leading Edge Slats and 12-inch Extensions on the Wing Tips*, May 1956; DTIC No. AD- 096 084.

    d. *F-86E Thrust Augmentation Evaluation*, March 1957; DTIC No. AD- 118 703.

    e. *F-86E Thrust Augmentation Evaluation*, Appendix IV, March 1957; DTIC No. AD- 118 707.

    f. *A Means of Comparing Fighter Effectiveness in the Approach Phase*, October 1949; DTIC No. AD- 223 596.

    g. *War Emergency Thrust Augmentation for the J47 Engine in the F-86 Aircraft*, August 1955; DTIC No. AD- 095 757.

    h. *Operational Suitability Test of the F-86F Airplane*, 4 May 1953; DTIC No. AD-017 568.

    i. *Estimated Aerodynamic Characteristics for Design of the F-86E Airplane*, 26 December 1950; DTIC No. AD- 069 271.

    j. *Combat Suitability Test of F-86F-2 Aircraft with T-160 Guns*, August 1953; DTIC No. AD- 019 725.

2. These attachments have been requested by Dr. Kenneth P. Werrell, a private researcher.

3. The AFMC/HO point of contact for these reviews is Dr. William Elliott, who may be reached at extension 77476.

JOHN D. WEBER
Command Historian

10 Attachments:

a. DTIC No. AD-B804 069
b. DTIC No. AD- 020 375
c. DTIC No. AD- 096 084
d. DTIC No. AD- 118 703
e. DTIC No. AD- 118 707
f. DTIC No. AD- 223 596
g. DTIC No. AD- 095 757
h. DTIC No. AD- 017 568
i. DTIC No. AD- 069 271
j. DTIC No. AD- 019 725