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WADD TECHNICAL REPORT 60-56
PART II

**A COMPENDIUM OF THE
PROPERTIES OF MATERIALS
AT LOW TEMPERATURE (PHASE I)**

PART II. PROPERTIES OF SOLIDS

Victor J. Johnson, General Editor

*National Bureau of Standards
Cryogenic Engineering Laboratory*

OCTOBER 196

WRIGHT AIR DEVELOPMENT DIVISION



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**A COMPENDIUM OF THE
PROPERTIES OF MATERIALS
AT LOW TEMPERATURE (PHASE I)**

PART I. PROPERTIES OF SOLIDS

Victor J. Johnson, General Editor

*National Bureau of Standards
Cryogenic Engineering Laboratory*

OCTOBER 1960

Materials Central
Contract No. AF 33(616)-58-4
Project No. 7360

WRIGHT AIR DEVELOPMENT DIVISION
AIR RESEARCH AND DEVELOPMENT COMMAND
UNITED STATES AIR FORCE
WRIGHT-PATTERSON AIR FORCE BASE, OHIO

FOREWORD

This report was prepared by the National Bureau of Standards Cryogenic Engineering Laboratory under U. S. Air Force Contract No. 33(616)58-4. This contract was initiated under Project No. 8-(8-7360), "Thermophysical Properties of Cryogenic Materials", Task No. 73603. The work was administered under the direction of the Physics Laboratory, Directorate of Laboratories, Wright Air Development Division, with Mr. Paul W. Dimiduk acting as project engineer.

This report covers work conducted from January 1958 to March 1959.

The following members of the Cryogenic Engineering Laboratory Staff contributed to this phase of the compendium: D. B. Mann (task author for helium), Dr. F. E. E. Germann (task author for hydrogen), Dr. K. D. Timmerhaus* (task author for neon, nitrogen and carbon monoxide), John Macinko (task author for oxygen), D. A. Van Gundy, and W. J. Veigle (task authors for air), Dr. P. L. Barrick* (task author for argon), R. F. Robbins (task author for fluorine and methane), R. L. Powell (task author for thermal conductivity of solids), and Dr. R. J. Corruccini (task author for expansivity, specific heat and enthalpy of solids); R. B. Scott and E. H. Brown reviewed most of the data sheets, noted many inconsistencies and offered many suggestions for improving the validity and usefulness of the data; Dr. R. D. Goodwin planned the program for compiling the compendium and initiated work on it. (He also along with Dr. Corruccini, conferred with the sponsor (WADC) and Armour Research Foundation regarding the scope and arrangement of the compendium. The proposal and contract were evolved from this planning.) D. B. Chelton (literature searches for nitrogen and carbon monoxide); R. V. Smith** and R. B. Stewart*** (hydrogen literature searching); Dr. V. D. Arp and J. J. Gniewek compiled data on specific heat and enthalpy of solids; R. J. Rasmussen and B. D. Troyer, graduate students, assembled much of the data for typing and drafting of the data sheets; J. A. Brennan and J. R. Cahoon monitored completion of the data sheets and prepared check prints; W. W. Bulla and G. A. Reynolds drew most of the graphs; Genevieve Michela and Signe Hartley typed most of the data sheets; and D. E. Jordan assisted in final review and completion of the compendium. Many other staff members contributed to the compendium in numerous ways but it is difficult to name them all and identify their aid. The task was a huge one and all contributions were valuable.

Many others who were sent preliminary copies of this compilation contributed helpful suggestions and criticisms of the material which has materially improved the final presentation and its accuracy. The following is a partial list of such contribution: I. Simon and I. A. Black of A. D. Little Co., F. Din of British Oxygen Co., L. C. Matsch and staff of Linde Co., W. B. Mitchell of Convair Astronautics, T. I. Bell of British Royal Aircraft Establishment, Paul Hernandez of the University of California Radiation Laboratory, W. T. Ziegler of Georgia Institute of Technology, P. E. Liley of Purdue University, E. J. Dethke of National Cylinder Gas, W. E. Schaefer of Air Reduction Sales Co., and H. Ziebland of British Ministry of Aviation. Their help and the help of many others is gratefully acknowledged.

The efforts of Genevieve Michela in carefully supervising the many changes and corrections made throughout the compendium and preparing it for final publication are sincerely appreciated.

*Professor of Chemical Engineering, University of Colorado, employed part-time by the Cryogenic Engineering Laboratory.

**Assoc. Professor of Mechanical Engineering, Colorado State University, Fort Collins.

***Assoc. Professor of Mechanical Engineering, University of Colorado


ABSTRACT

This first phase of the Compendium covers ten properties of ten fluids (Part I), three properties of solids (Part II), and an extensive bibliography of references (Part III). Density, expansivity, thermal conductivity, specific heat and enthalpy, transition heats, phase equilibria, dielectric constants, adsorption, surface tension and viscosity for the solid, liquid and gas phases of helium, hydrogen, neon, nitrogen, oxygen, air, carbon monoxide, fluorine, argon and methane are given wherever adequate data could be collected. Thermal expansion, thermal conductivity and specific heat and enthalpy are given for a number of solids of interest in cryogenic engineering. Data sheets, primarily in graphic form, are presented from "best values" of data collected. The source of the material used, other references and tables of selected values with appropriate comments are furnished with each data sheet to document the data presented. Conversion tables and other helpful information are also included.

PUBLICATION REVIEW

This report has been reviewed and is approved.

FOR THE COMMANDER:



Jules I. Wittebort

JULES I. WITTEBORT
Chief, Thermophysics Branch
Physics Laboratory
Materials Central

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* General Contents only; detailed contents given at the beginning of each chapter.

** Code designation sequence used in lieu of page numbers to permit internal expansion.

NOTE TO USER

This volume is intended basically as a loose-leaf report for continuous expansion and revision as new and revised data sheets are produced. It has been bound as an economical means of assembly and distribution. It is also punched for standard three hole binders that are available from many commercial sources. A simple method of removing the bound cover and loosening the sheets is to shear off approximately 1/16" of the bound edge in an ordinary printers shear.

Manuscript released for publication August 1960 as a WADD Technical Report.

INTRODUCTION

A. General Introduction to Phase I of the Compilation Program

In the past ten years there has been a greatly accelerated growth of interest and activity in cryogenic engineering. From a few industrial applications such as the liquefaction of oxygen and from laboratory scale research at low temperatures, the activity has spread to nuclear reactors, controlled thermonuclear reactions, high altitude flight, missiles and rockets, the use of cryogenic fuels and oxidants, nuclear powered rockets, and transportation of liquefied gases; to name a few areas of application in this ever widening field.

As a result of the increased cryogenic activity, and the rigorous technical demands that often occur in new applications, it soon became apparent that a great deal more information and data on the properties of materials at low temperatures is needed by design engineers and physicists than is now readily available to them. The Wright Air Development Division of the U. S. Air Force, which is conducting and sponsoring a large amount of engineering development involving cryogenics, arranged with the National Bureau of Standards to undertake a program of collecting and compiling data on the thermophysical properties of materials used in low temperature applications. The program was started early in 1958 by the Cryogenic Engineering Laboratory Staff and this compendium presents the first phase of the work.

The scope of this first phase includes as extensive a literature search as was deemed practical and the correlation and presentation of data on ten specified properties of ten of the most common cryogenic fluids. It also includes three of the more pertinent properties of a number of solids used at low temperatures. The specified temperature range of primary interest was from near absolute zero to 110°K. Where desirable and practicable, however, data are included for temperatures up to near room temperature (300°K). Upon the selection and presentation of the "best values" found in the literature graphical presentation of the data is also made where practicable. It was stipulated that the metric system of units be

used for the primary coordinates of graphs and that "English" or engineering units also be shown as alternate coordinates to aid design engineers not accustomed to metric units.

The plan adopted for organizing the compendium embodied two basic features. One was a "loose-leaf" design allowing more data to be added as it became available. The other concerned the numbering scheme for arranging the data sheets. Considering that there are a limited number of properties of materials and almost an unlimited number of materials that might eventually be of interest, the primary arrangement was made by properties and a secondary order established for materials. Each data sheet then is made complete and somewhat independent of any of the other data sheets. Each is assigned a code number by property and material classification and placed in the compendium in a corresponding order.

The data sheets are designed in such a manner as to serve both the design engineer who needs preselected values suitable for direct use and the researcher who is interested in the nature of the data and how it was derived. The "best values", or what are considered to be the most probable values, have been plotted as a full page graph whenever practicable with no encumbering deviations or alternate values. This is intended primarily for the design engineer. As complete a documentation as feasible is given to support each graph and to aid those interested or in need of a more thorough evaluation of the data. This includes the source of the data, other references of merit, brief comments concerning the data and a tabulation of values selected from the source. Occasionally, alternate values from other references are tabulated also for comparison purposes. In most cases the values are given just as they appeared in the source and accordingly the units are not necessarily the same as used on the graph. By doing this, possible conversion errors were eliminated and the full significance of the values retained.

This first phase of the program was divided into a number of tasks for assignment to qualified senior staff members. The task break-down for the fluids was by material and so there were ten such tasks. The break-down for solids was made by property resulting in three additional tasks.

The person assigned a task is referred to as a "task author". It was the task author's responsibility to make as complete a literature search as practicable and record the scope of his search. He also selected "best values" from the references he found and made pertinent comments regarding the data. He then presented it to the "general editor" for preparation of the data sheets. Student aides from the University of Colorado (both graduates and undergraduates in engineering) were used extensively in preparing the detailed data sheets. They also assisted the senior staff members in identifying references in the literature search. The Cryogenic Data Center played an important role in actually obtaining documents for task authors. It also profited as a result of this assistance since the literature searches turned up nearly two thousand new references of interest in cryogenics.

Division of the work in the manner just described has both advantages and disadvantages over other arrangements. A major advantage is that use can be made of a great diversity of talent by seeking help from persons most familiar with the subject matter. On the other hand, these people are usually the ones that already have the greatest demands made on their time and so it is very difficult to achieve orderly progress of the work on a reasonable time schedule. A somewhat better arrangement from a scheduling standpoint might be to have about two experienced persons working full time instead of ten or more on a hit-and-miss basis. Two difficulties immediately become apparent. One is finding persons with broad enough experience to handle a wide cross section of subject matter as is represented in this work who would accept the tediousness of such a task for a year or more. The other is that no one or two persons can possess the general knowledge that is usually represented by a large number of persons each working in a somewhat specialized area. Present planning for the future phases of this work is to reach some kind of a compromise between the two plans, i.e. have at least one full time experienced person carrying the bulk of the search and correlation load but utilize numerous other staff members to review and criticize the data derived.

The next phase of the program (Phase II) is already well underway.

It covers the following additional properties for essentially the same materials as included in Phase I:

| | |
|--|---------|
| Compressibility Factor ($Z = PV/RT$)..... | 11.000* |
| Compressibility $\left[-\frac{1}{V} \left(\frac{dV}{dP} \right)_T \right]$ and | |
| Compressibility Coefficient $\left[-\frac{P}{V} \left(\frac{dV}{dP} \right)_T \right]$ | 12.000 |
| Thermal Conductivity Integrals $\left[\int_{T_0}^{T_1} \lambda dT \right]$ | 13.000 |
| Entropy (S)..... | 14.000 |
| Velocity of Sound..... | 15.000 |
| Solubility (2 component mixtures of liquids and gases)..... | 16.000 |
| Electrical Resistivities..... | 17.000 |
| Ferromagnetic Properties..... | 18.000 |

* This number represents the coding sequence.

It will be issued as a supplement to this first phase of the Compendium and will be arranged for uniform continuity. There also will, undoubtedly, be revisions and additions to the material issued here as inconsistencies and better data are discovered. Revised data sheets will be prepared and issued to supplant or supplement the current ones.

Comments on this compendium will be greatly appreciated. They should be sent to the Cryogenic Engineering Laboratory, attention of the general editor for the WADD Compendium. We would also appreciate being informed of any errors (typographical, or otherwise) that may be discovered and any new information that users may have that would enhance the value of this compilation.

B. Introduction to Part II

This Compendium is divided into three parts for convenience; Part I, Properties of Fluids; Part II, Properties of Solids; and Part III, Bibliography of References, Cross-Indexed.

The properties of solids included in this phase of the Compendium are: Thermal Expansion (2.000), Thermal Conductivity (3.000), and Specific Heat and Enthalpy (4.000). The solids covered are listed in the "Contents" for each property. (Code numbers for solids were grouped by classes as follows: .100 - Pure Metals; .200 - Non-Ferrous Alloys; .300 - Ferrous Alloys; .400 - Inorganic Compounds; and .500 - Organic Compounds.)

Data sheets are presented individually for each property and material combination that was found in the literature search. Property values for many materials of interest in the cryogenic engineering field and for certain temperature ranges are missing in the compilation. Such omission indicates that no information was found in the search and perhaps may be that no measurements have been made in those areas for those cases. Where information does exist but was not found in the search, it is planned that data sheets will be prepared as the information is received and added to this compilation. Likewise, where better information than now presented is developed or found, a revised data sheet will be prepared to replace the current one.

The graphical presentation of "best values" selected from data given in the literature is made on full-page graphs as far as practicable. Metric units are used for the primary coordinates, but "English" or engineering units are also given as alternate coordinates except in a few instances where the metric units are regularly used by engineers. (It might be noted that alternate use of calories and joules exists among some of the graphs. The joule is now the accepted metric unit of energy, but unfortunately some of the first graphs were prepared using calories and have not yet been redrawn.) Careful note should be made of the units used when picking values from a graph. Not only should the exact dimensions of the units be noted but also the magnitude of the unit. For instance, some units are given in watts, others in milliwatts or microwatts, etc. Also, occasionally there is

a note to "multiply by 10^{-3} " or "multiply value by 10^{-5} ", etc. For all instances, this means to multiply the numerical value taken from the graph by the number given. It has no direct reference to the size of the unit. For example, a value of 317 may be read from a graph that has a note to "multiply by 10^{-4} ". The actual value is .0317 of the units given. The curves on the graphs are often plotted for a limited temperature range because of the limitation of available data. It is dangerous to extrapolate such curves beyond the extent plotted because of transitions and other anomalies that frequently are present but not indicated.

Conversion tables of dimensional units pertinent to a particular property are given at the beginning of each property chapter. Other conversion tables of more general application have been included for users' convenience as appendixes.

C. Scope of Literature Searches

Specific literature searches were made by the task authors in an effort to survey as much of the published literature as possible on the thermo-physical properties of materials of interest in cryogenic engineering. The principal indexes and bibliography services used for searching out the desired literature were: Chemical Abstracts, Physics Abstracts, Engineering Index, Industrial Arts Index, ASME Seventy-Seven Year Index, Dissertation Abstracts, Bureau of Mines Bibliographies, and other published bibliographies. The usual procedure was to search the indexes of the various abstracts and note all items that might possibly pertain to the desired subject matter. A review of the actual abstracts of the referenced literature then indicated more conclusively whether the article was pertinent. Articles selected were then ordered from various library services and reviewed in full text. All articles that contained pertinent information were then listed in the applicable bibliography of references and considered in the selection of data. There is listed below the extent of the specific searches made for each task:

Thermal Expansion of Solids

a. Physical Abstracts

1898 thru 1957

- b. A.S.M. Review of Metal Literature 1944 thru 1956
- c. Metallurgical Abstracts 1931 thru 1956
- d. Chemical Abstracts 1948 thru 1956

Thermal Conductivity of Solids

- a. Chemical Abstracts: Volumes 1 thru 50 (1907 - 1956)
- b. Physics Abstracts: 1900 thru 1956
- c. Landolt-Bornstein Physikalischemische Tabellen, Edited by W. A. Roth and K. Scheel (Julius Springer, Berlin) 5th ed., vol. 2, 1923; 5th ed., 1st supplement, vol. 1, 1927; 5th ed., 2nd supplement, vol. 2, 1931; 5th ed., 3rd supplement, vol. 3, 1936.
- d. NBS Circular 556. Thermal Conductivity of Metals and Alloys at Low Temperatures; A Review of the Literature (1954)

Specific Heat and Enthalpy of Solids

- a. Bureau of Mines Bulletin 477, 1950 covers inorganic substances up to 1948.
- b. General Electric Company Research Laboratory Bulletin: The Heat Capacities of the Elements Below Room Temperature Compiled by C. A. Shiftman covers elements to 1952.
- c. Physics Abstracts: 1948 thru 1957
- d. Chemical Abstracts: 1948 thru 1956

In addition to the specific searches listed above, a considerable number of references were found from listings on file in the Data Center that had been acquired somewhat at random. Also, inasmuch as most of the searches were for all properties of a particular material, many of the articles covered several materials. These additional references were added to the bibliographies of the other materials covered and were used by task authors in their evaluation and selection of data. A third additional source of references was from the documents themselves. Selected documents frequently listed references of a broader coverage than the material presented in it, and thus provided a more extensive range of properties. As a result, the actual scope of the literature searching was much greater than indicated by the specific searches as listed.

THERMAL EXPANSION of CRYOGENIC SOLIDS

CONTENTS

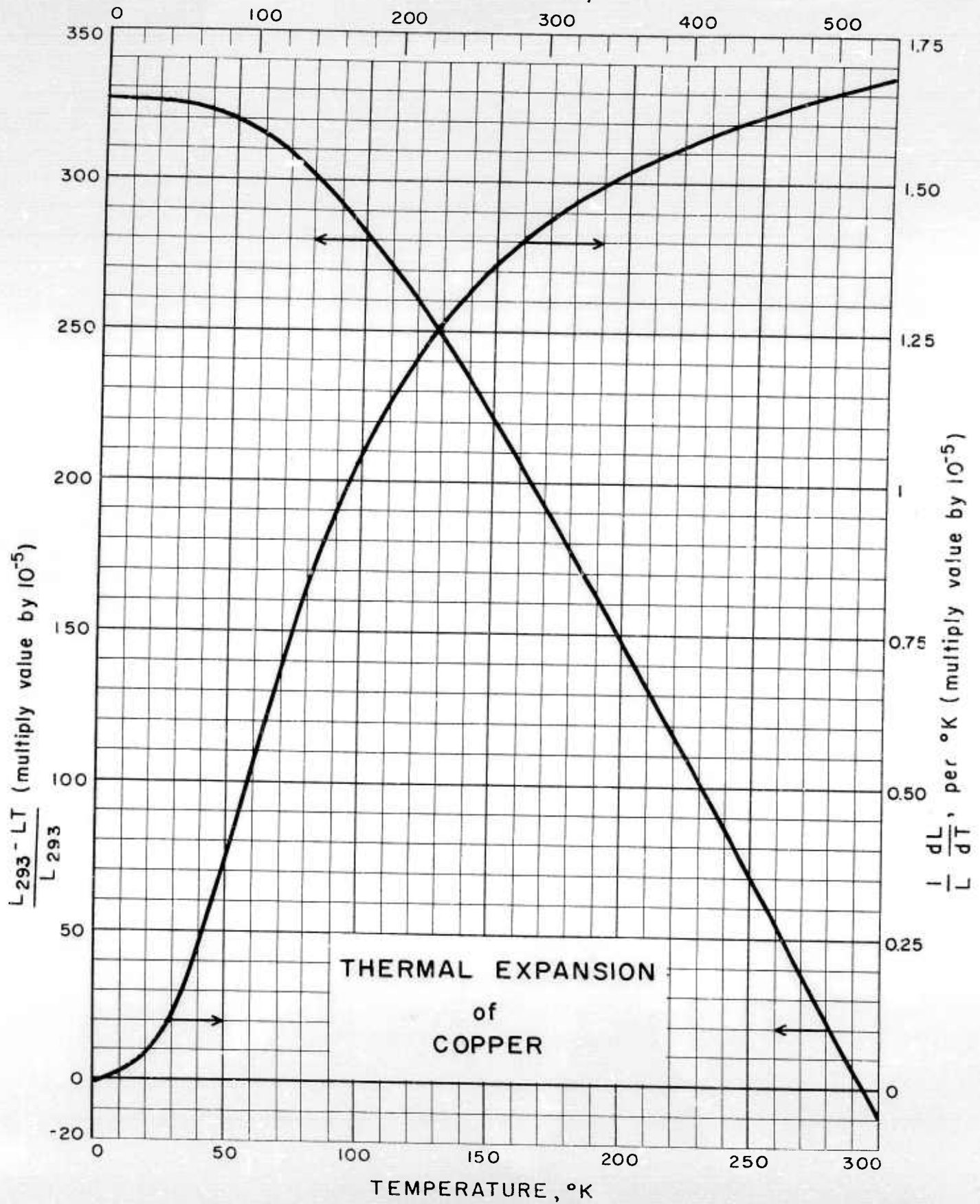
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| Thermal Expansion of L-Nickel..... | 2.181 |

Author's Note

Values of thermal expansion are given in the form of (a) total fractional expansion, $\frac{L_{293} - L_T}{L_{293}}$; and (b) by coefficient of expansion $\frac{1}{L} \frac{dL}{dT}$, change per unit length per °K. For example the total fractional expansion (or contraction) for copper for a temperature change from 293.15°K (20°C) to 50°K is .00321 in./in., i.e., a bar will be .00321 inches shorter at 50°K per inch of length than it was at 293.15°K. However, the coefficient of expansion for copper at 50°K is .00038 in./in.-°K, i.e. it will expand (or contract) .00038 inches per inch per °K temperature change from 50°K.

2.112-1

TEMPERATURE, °R



THERMAL EXPANSION
of
COPPER

THERMAL EXPANSION OF COPPER

Source of Data:

Rubin, T., Altman, H. W. and Johnston, H. L., J. Am. Chem. Soc. 76, 5289-93 (1954)

Other References:

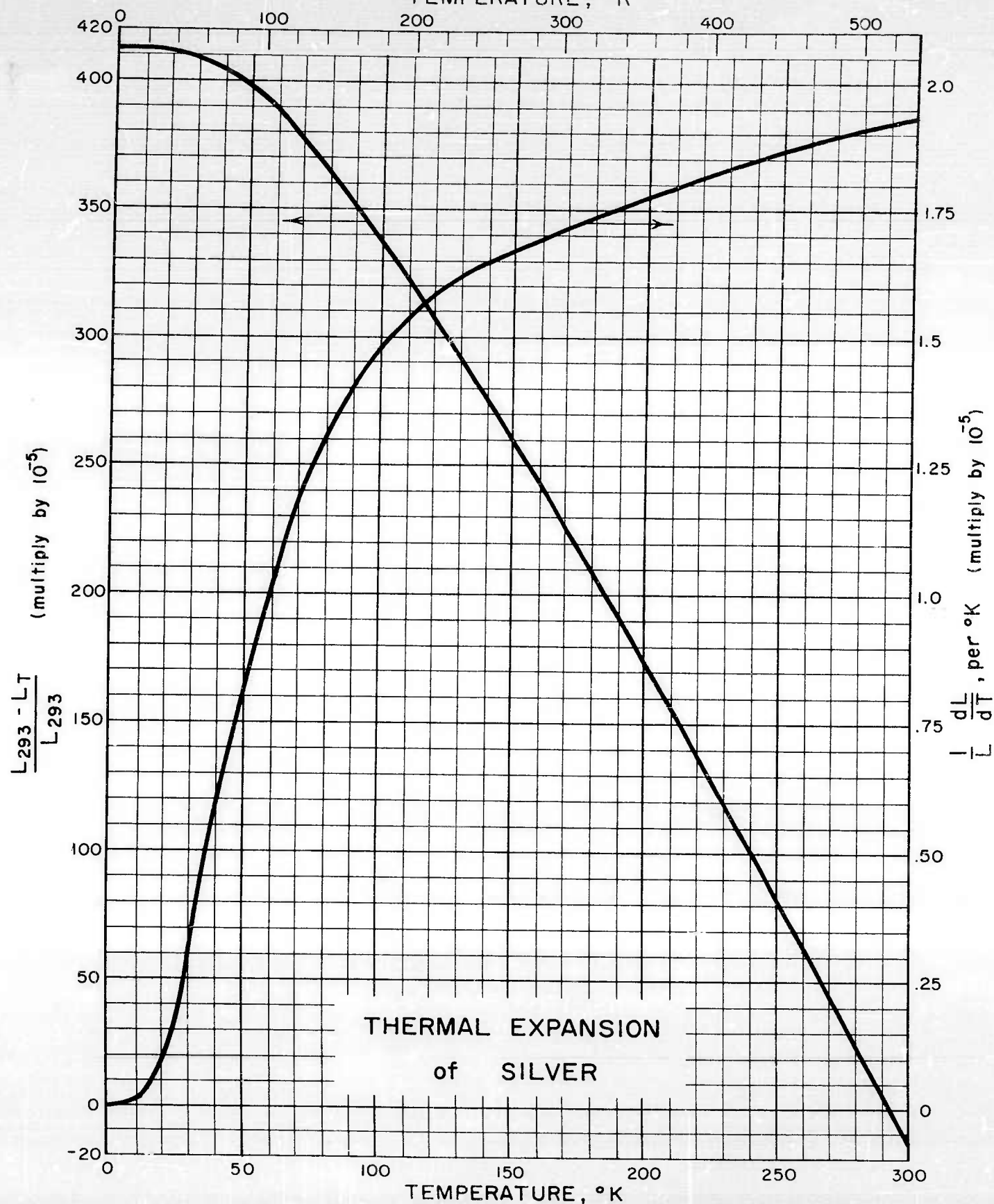
- Simmons, R. O. and Balluffi, R. W., Phys. Rev. 108, 278-80 (1957)
 Beenakker, J. J. M. and Swenson, C. A., Rev. Sci. Instr. 26, 1204 (1955)
 Bijl, D. and Pullan H., Physica 21, 285 (1955)
 Fraser, D. B. and Hollis-Hallet, A. C., Proc. 9th Intern. Congr. Refrig. 1, 1065 (1955)
 Nix, F. C. and MacNair, D., Phys. Rev. 60, 597-605 (1941)
 Aoyama, S. and Ito, T., Sci. Repts. Tohoku Univ. 27, 348-64 (1939)
 Adenstedt, H., Ann. Physik 26, 69-96 (1936)
 Simon, F. and Bergmann, R., Z. physik. Chem. 8, 255-80 (1930)
 Krupkowski, A. and De Haas, W. J., Commun. Phys. Lab. Univ. Leiden 194b (1928)
 Keesom, W. H., Van Agt, F. P. G. and Jansen, A. T. J., Proc. Acad. Sci. Amsterdam 29, 786-91 (1926)
 Buffington, R. M. and Latimer, W. M., J. Am. Chem. Soc. 48, 2305-19 (1926)
 Borelius, G. and Johansson, C. H., Ann. Physik 75, 23-36 (1924)
 Lindemann, C. L., Phys. Z. 12, 1197-99 (1911)
 Henning, F., Ann. Physik (4) 22, 631-39 (1907)
 Dorsey, H. G., Phys. Rev. 25, 88-102 (1907)

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$, per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$, per °K |
|-------------|---------------------------------|--------------------------------------|-------------|---------------------------------|--------------------------------------|
| 0 | 326×10^{-5} | 0 | 120 | 260×10^{-5} | 1.20×10^{-5} |
| 10 | 326 " | 0.004×10^{-5} | 140 | 235 " | 1.32 " |
| 20 | 326 " | .03 " | 160 | 208 " | 1.41 " |
| 30 | 325 " | .10 " | 180 | 179 " | 1.47 " |
| 40 | 324 " | .23 " | 200 | 149 " | 1.52 " |
| 50 | 321 " | .38 " | 220 | 118 " | 1.56 " |
| 60 | 316 " | .55 " | 240 | 87 " | 1.59 " |
| 70 | 310 " | .70 " | 260 | 55 " | 1.62 " |
| 80 | 302 " | .84 " | 273.15 | 33 " | 1.64 " |
| 90 | 293 " | .95 " | 280 | 22 " | 1.65 " |
| 100 | 283 " | 1.05 " | 293.15 | 0 " | 1.67 " |
| | | | 300 | -11 " | 1.68 " |

2.112-2

TEMPERATURE, °R



THERMAL EXPANSION
of SILVER

THERMAL EXPANSION of SILVER

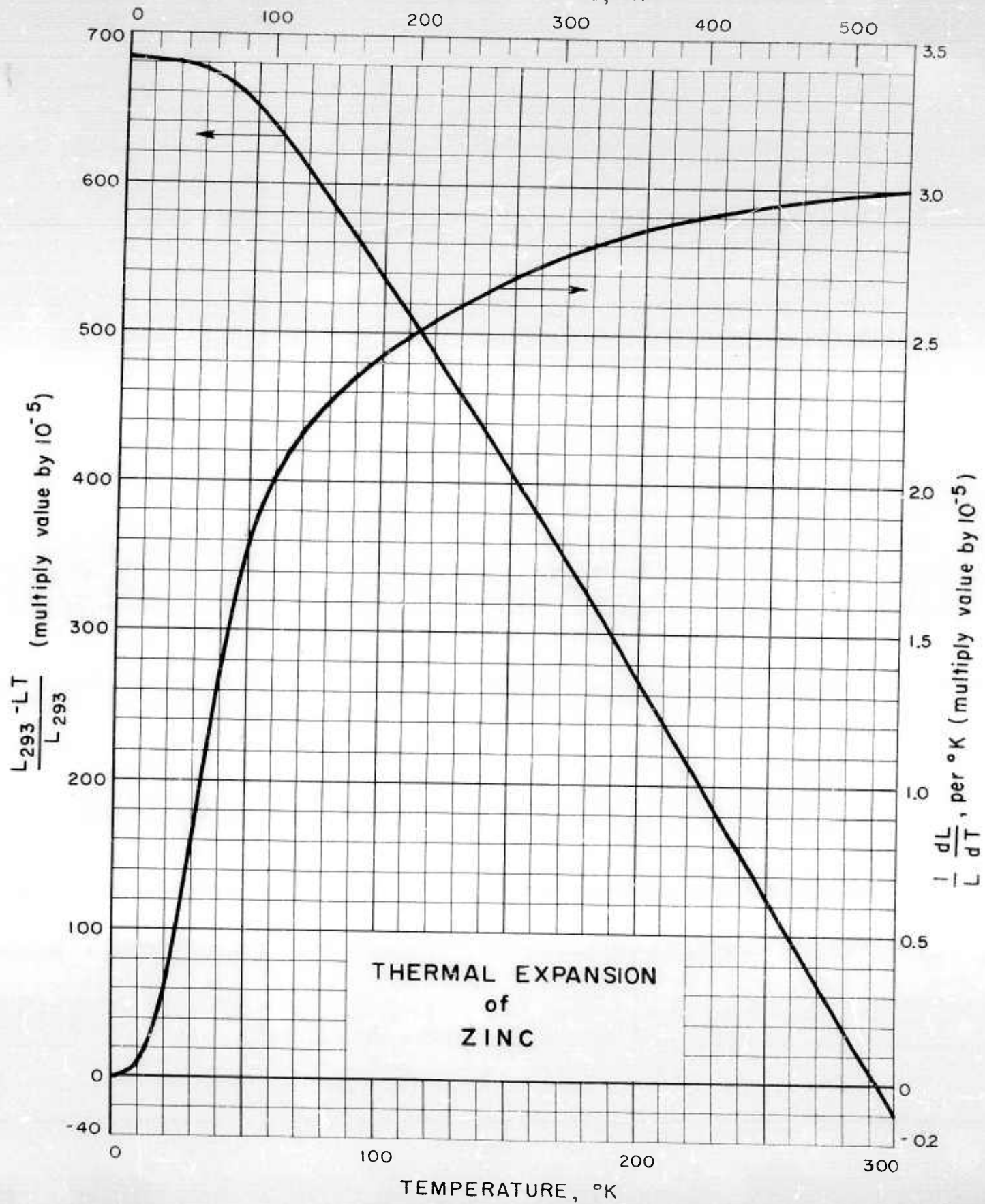
Sources of Data: Ebert 1928, Nix and MacNair 1942.

Other References: Ayres 1905, Buffington and Latimer 1926,
Dorsey 1907, Henning 1907, Keesom and
Jansen 1927, Lindemann 1911.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 413×10^{-5} | 0 | 120 | 308×10^{-5} | 1.59×10^{-5} |
| 10 | 413 " | 0.01×10^{-5} | 140 | 276 " | 1.65 " |
| 20 | 412 " | .1 " | 160 | 242 " | 1.69 " |
| 30 | 410 " | .3 " | 180 | 208 " | 1.73 " |
| 40 | 405 " | .6 " | 200 | 173 " | 1.77 " |
| 50 | 398 " | .8 " | 220 | 137 " | 1.81 " |
| 60 | 389 " | 1.0 " | 240 | 100 " | 1.85 " |
| 70 | 378 " | 1.2 " | 260 | 63 " | 1.88 " |
| 80 | 366 " | 1.3 " | 273 | 38 " | 1.90 " |
| 90 | 353 " | 1.36 " | 280 | 25 " | 1.90 " |
| 100 | 339 " | 1.46 " | 293 | 0 " | 1.91 " |
| | | | 300 | -13 " | 1.91 " |

TEMPERATURE, °R



THERMAL EXPANSION of ZINC

Source of Data:

Grüneisen, E. and Goens, E., Z. Physik. 29, 141 (1924)

Other References:

Dorsey, H. G., Phys. Rev. 27, 1 (1908)

Grüneisen, E., Ann. Physik. 33, 33 (1910)

Head, E. L. and Laquer, H. L., AECD-3706 (1952)

Lindemann, C. L., Physik. Z. 12, 1197-9 (1911)

McLennan, J. C. and Monkman, R. J., Trans. Roy. Soc. Can. III 23, 255-67 (1929)

Comments:

The data on zinc are discordant. The differences found among polycrystalline samples (Dorsey, Grüneisen, Head and Laquer, Lindemann) are attributable to the high degree of anisotropy of the zinc crystal which is shown by the data of Grüneisen and Goens in Table I. Evidently, appreciable preferred orientation is present in most polycrystalline zinc.

Table II has been derived from Table I and gives the average linear expansion. This is presumed to be representative of polycrystalline zinc that is without preferred orientation of crystallites. The expansion coefficients of Dorsey and of Head and Laquer are up to 20 per cent lower than those of Table II while those of Grüneisen and of Lindemann are less than one third as great. The expansions of various samples of polycrystalline zinc could conceivably cover a wide range of values between the limits set by the data of Table I.

Table I

Expansion Coefficients of Single Crystal Zinc
Parallel and Perpendicular to the Hexagonal Axis

| T ₂ °K | T ₁ °K | $\frac{1}{L_{293}} \times \frac{L_2 - L_1}{T_2 - T_1}$ | |
|----------------------|----------------------|--|-------------------------|
| | | | ⊥ |
| 293 | 253 | 6.43 x 10 ⁻⁵ | 1.25 x 10 ⁻⁵ |
| 253 | 213 | 6.51 " | 1.13 " |
| 213 | 173 | 6.54 " | 1.01 " |
| 173 | 133 | 6.56 " | .83 " |
| 133 | 93 | 6.44 " | + .50 " |
| 86 | 20 | 5.25 " | - .21 " |

THERMAL EXPANSION of ZINC (Cont.)

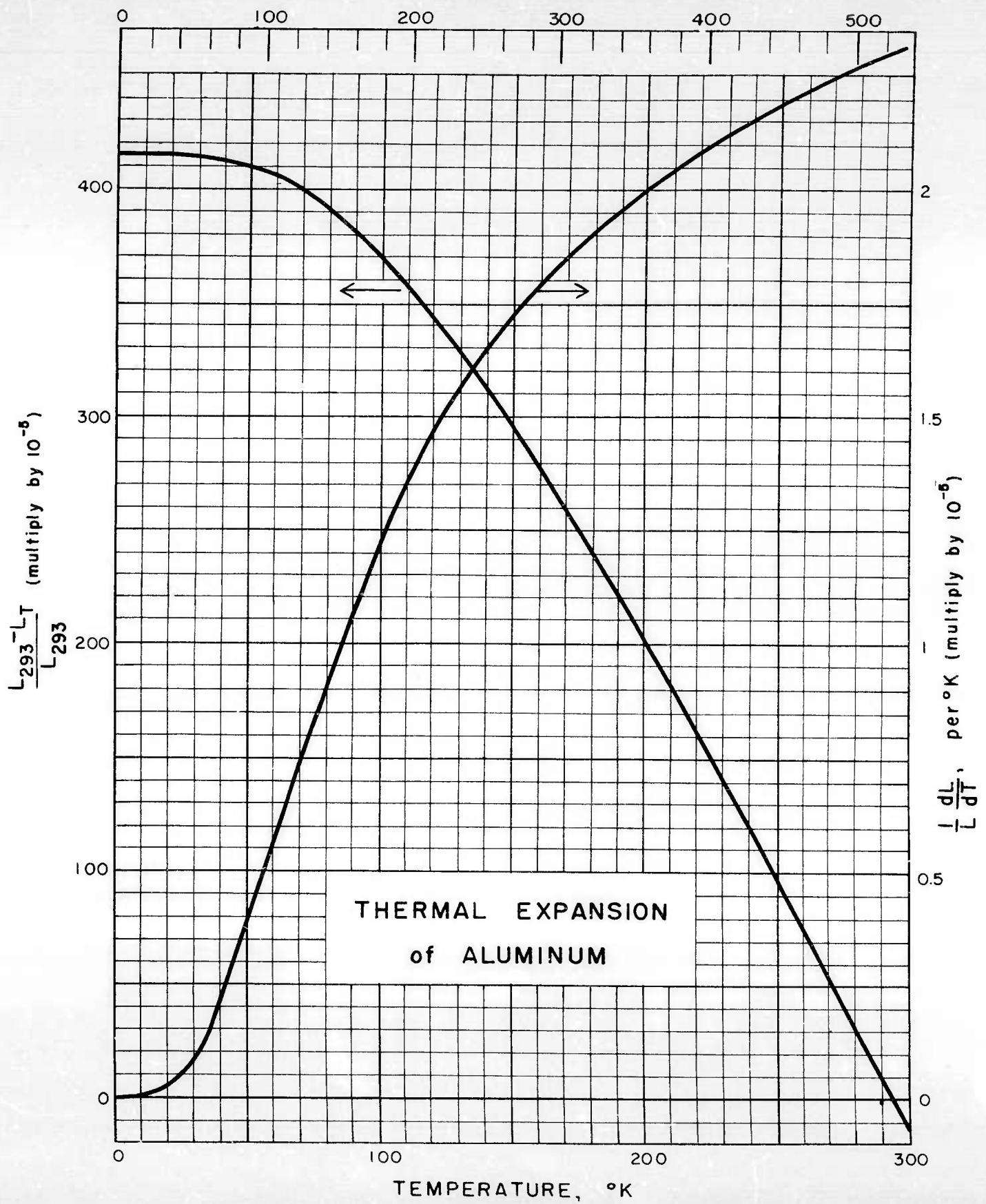
Table II

AVERAGE EXPANSION of ZINC*

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$, per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$, per °K |
|-------------|---------------------------------|--------------------------------------|-------------|---------------------------------|--------------------------------------|
| 0 | 683×10^{-5} | 0 | 120 | 492×10^{-5} | 2.53×10^{-5} |
| 10 | 683 " | $.03 \times 10^{-5}$ | 140 | 440 " | 2.63 " |
| 20 | 682 " | .3 " | 160 | 386 " | 2.73 " |
| 30 | 677 " | .8 " | 180 | 331 " | 2.81 " |
| 40 | 667 " | 1.3 " | 200 | 274 " | 2.87 " |
| 50 | 652 " | 1.7 " | 220 | 216 " | 2.91 " |
| 60 | 633 " | 2.1 " | 240 | 157 " | 2.94 " |
| 70 | 611 " | 2.2 " | 260 | 98 " | 2.96 " |
| 80 | 588 " | 2.3 " | 273 | 60 " | 2.97 " |
| 90 | 565 " | 2.36 " | 280 | 39 " | 2.98 " |
| 100 | 541 " | 2.42 " | 293 | 0 | 2.99 " |
| | | | 300 | -21 " | 3.00 " |

* Calculated on the basis: $\left(\frac{1}{L} \times \frac{dL}{dT}\right)_{av} = \left(\frac{1}{3L} \times \frac{dL}{dT}\right)_{||} + \left(\frac{2}{3L} \times \frac{dL}{dT}\right)_{\perp}$

TEMPERATURE, °R



THERMAL EXPANSION
of ALUMINUM

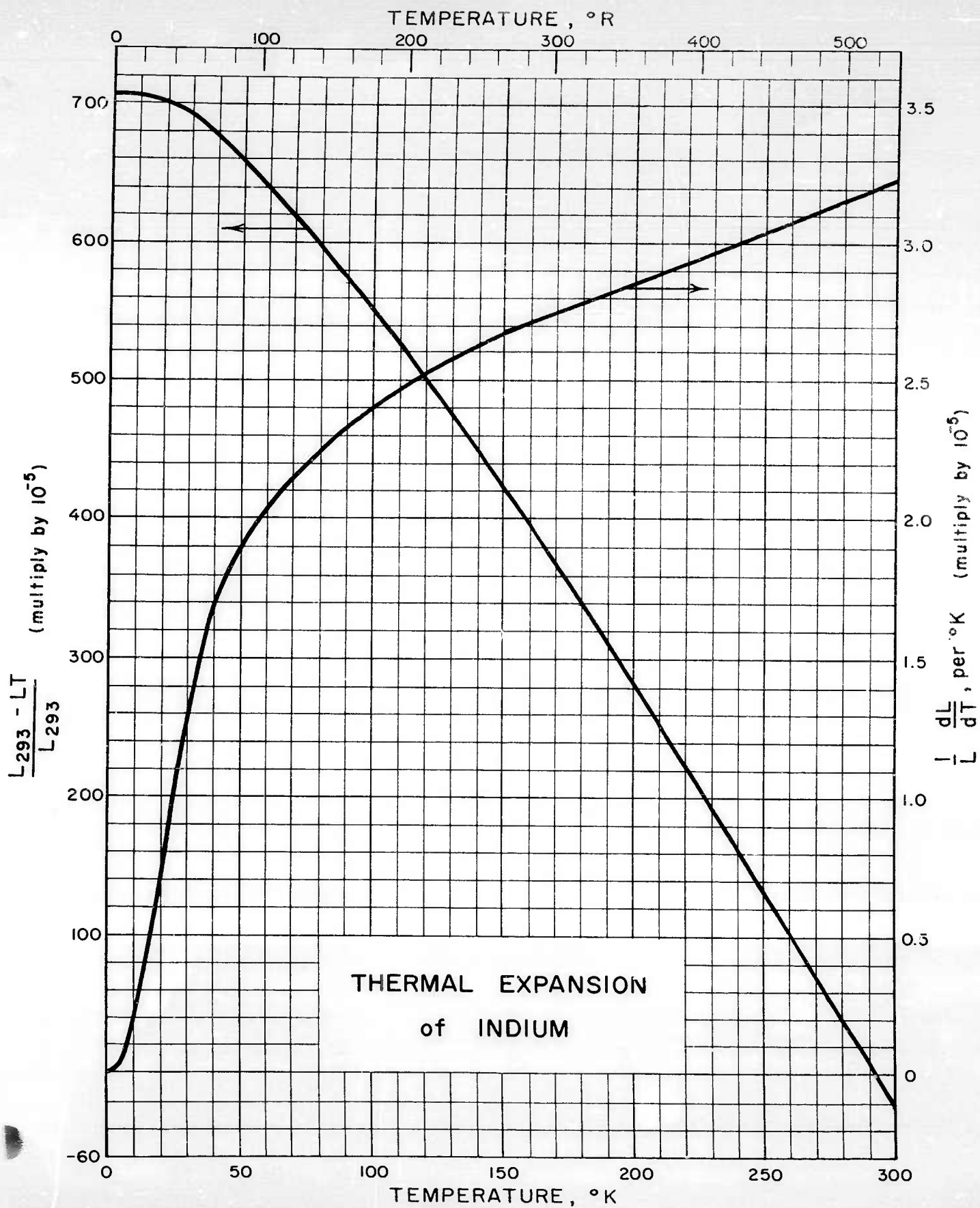
THERMAL EXPANSION of ALUMINUM

Source of Data: Altman, Rubin and Johnston 1954.

Other References: Ayres 1905, Bijl and Pullan 1955, Buffington and Latimer 1926, Ebert 1928, Gibbons 1958, Henning 1907, Hume-Rothery and Strawbridge 1947, Lindemann 1911, Nix and MacNair 1941.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 415×10^{-5} | 0 | 120 | 343×10^{-5} | 1.46×10^{-5} |
| 10 | 415 " | 0.005×10^{-5} | 140 | 312 " | 1.65 " |
| 20 | 415 " | .02 " | 160 | 277 " | 1.79 " |
| 30 | 414 " | .09 " | 180 | 240 " | 1.90 " |
| 40 | 413 " | .22 " | 200 | 201 " | 2.00 " |
| 50 | 410 " | .38 " | 220 | 160 " | 2.08 " |
| 60 | 405 " | .55 " | 240 | 118 " | 2.15 " |
| 70 | 399 " | .74 " | 260 | 75 " | 2.21 " |
| 80 | 391 " | .91 " | 273 | 45 " | 2.25 " |
| 90 | 381 " | 1.07 " | 280 | 30 " | 2.27 " |
| 100 | 370 " | 1.22 " | 293 | 0 " | 2.30 " |
| | | | 300 | -16 " | 2.32 " |



THERMAL EXPANSION of INDIUM

Source of Data: Swenson 1955

Other References: Hidnert and Blair 1943

Discussion: In the two investigations above, the experimental methods and sample purities were very similar. Yet the two points by Hidnert and Blair, $(L_{273} - L_{195}) / L_{273}$ and $(L_{273} - L_{83}) / L_{273}$, are respectively 7% and 4% less than Swenson's corresponding points. Swenson's data have been adopted solely because they include more points over a wider temperature range.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 706×10^{-5} | 0. | 120 | 500×10^{-5} | 2.52×10^{-5} |
| 10 | 706 " | 0.2×10^{-5} | 140 | 448 " | 2.63 " |
| 20 | 701 " | 0.7 " | 160 | 394 " | 2.72 " |
| 30 | 691 " | 1.3 " | 180 | 339 " | 2.79 " |
| 40 | 676 " | 1.7 " | 200 | 282 " | 2.86 " |
| 50 | 658 " | 1.91 " | 220 | 224 " | 2.93 " |
| 60 | 638 " | 2.04 " | 240 | 165 " | 3.01 " |
| 70 | 617 " | 2.15 " | 260 | 104 " | 3.08 " |
| 80 | 595 " | 2.24 " | 273 | 63 " | 3.13 " |
| 90 | 572 " | 2.32 " | 280 | 42 " | 3.15 " |
| 100 | 549 " | 2.39 " | 293 | 0 " | 3.20 " |
| | | | 300 | -22 | 3.22 " |

THERMAL EXPANSION of CARBON (GRAPHITE)

Sources of Data:

- Baskin, Y. and Meyer, L., Phys. Rev. 100, 544 (1955)
 Cohen, E. and Olie, J., Z. physik Chem. 71, 385-400 (1910)
 Dewar, J., Proc. Roy. Soc. (London) 70, 237-46 (1902)
 Erfling, H. D., Ann. Physik 34, 136-60 (1939)
 Walker, P. L., McKinstry, H. A. and Wright, C. C., Ind. Eng. Chem. 45, 1711 (1953)

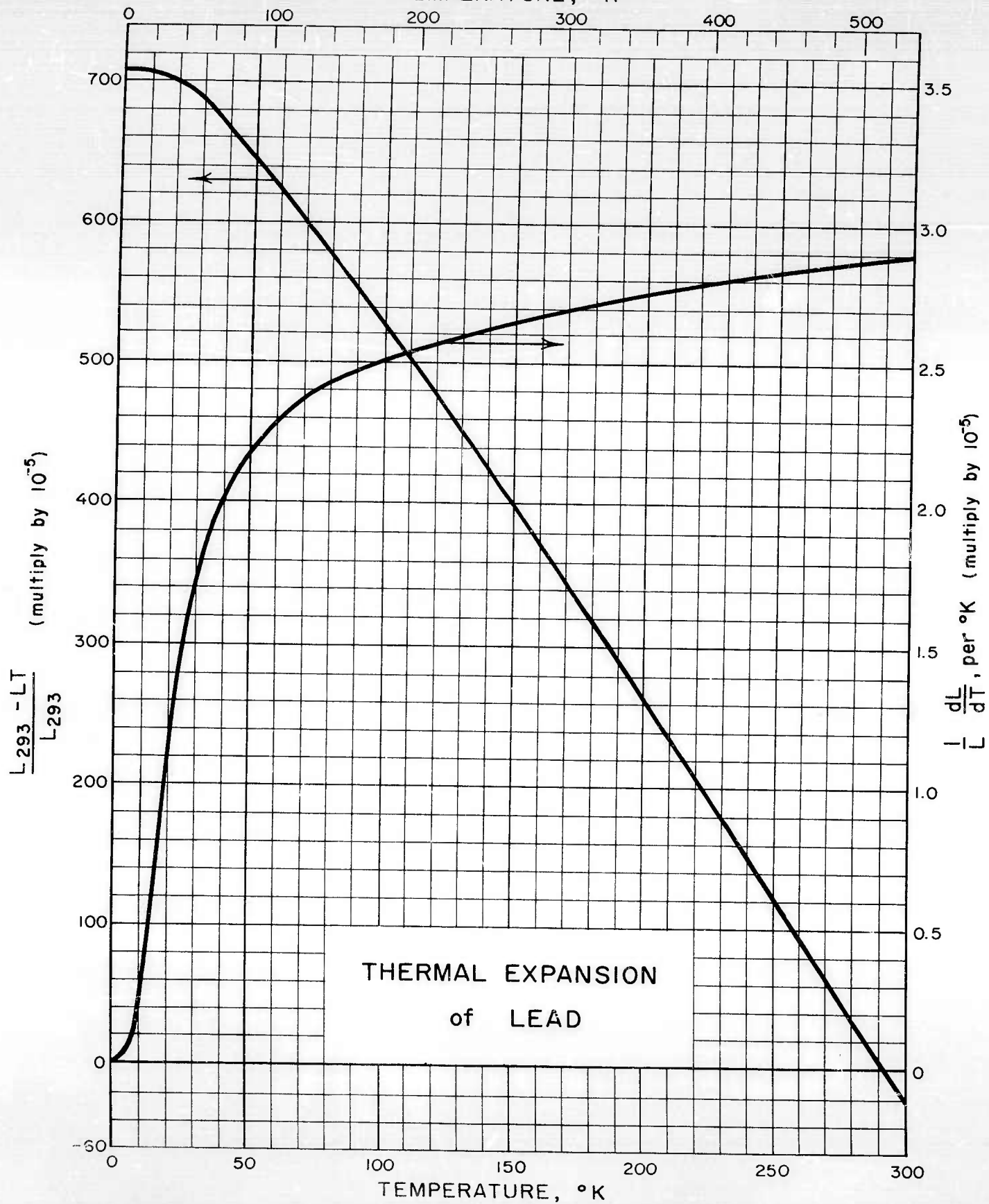
Comments:

The macroscopic thermal expansion of polycrystalline graphite has not been measured at low temperatures. Baskin and Meyer by x-ray methods obtained 28×10^{-6} for $\bar{\alpha}_c$, the mean expansion coefficient from 78° to 297°K in the c-direction (normal to the laminae) for polycrystalline artificial graphite. This result agrees closely with Walker et al who obtained the constant value 29×10^{-6} from high temperatures down to 77°K. Baskin and Meyer found the corresponding coefficient for the a-direction, $\bar{\alpha}_a$ (parallel to the laminae) to be zero within experimental error, as was $\bar{\alpha}_a$ in the interval, 4° to 78°K. With a single crystal the values $\bar{\alpha}_c = (22 \pm 1) \times 10^{-6}$ in the range 78° to 297°K, and $\bar{\alpha}_c = (7 \pm 3) \times 10^{-6}$ in the range 4.2° to 78°K, were obtained. Erfling determined precise values of α_a for a natural graphite ranging from 6.6×10^{-6} at room temperature to 2.3×10^{-6} at about 90°K. Cohen and Olie obtained a mean volume expansion coefficient for a natural graphite over the interval 110° to 295°K which when divided by 3 gives an average linear expansion coefficient of 6×10^{-6} . Dewar similarly obtained 24×10^{-6} in the interval 85° to 290°K.

From these discordant results we can estimate that a polycrystalline artificial graphite will probably have a mean α between room temperature and liquid air temperatures within a factor of two of the value 10×10^{-6} per °K. However much lower values for room temperature can be found in the literature

2.142-3

TEMPERATURE, °R



THERMAL EXPANSION
of LEAD

THERMAL EXPANSION of LEAD

Sources of Data: Dheer and Surange 1958, Ebert 1928, Nix and MacNair 1942, Olsen and Rohrer 1957.

Other References: Dorsey 1908, Gruneisen 1910, Head and Laquer 1952, Lindemann 1911, McLennan, Allen and Wilhelm 1931.

Discussion: Superconducting lead has a slightly greater volume and a slightly smaller expansion coefficient than normal lead according to data by Olsen and Rohrer covering the region from 1° to the transition temperature, 7.2°K. For example, the difference in expansion coefficients at 5°K is about 10%.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 708×10^{-5} | 0 | 120 | 477×10^{-5} | 2.56×10^{-5} |
| 5 | 708 " | 0.03×10^{-5} | 140 | 425 " | 2.63 " |
| 10 | 707 " | 0.32 " | 160 | 372 " | 2.68 " |
| 20 | 700 " | 1.1 " | 180 | 318 " | 2.72 " |
| 30 | 686 " | 1.7 " | 200 | 263 " | 2.75 " |
| 40 | 667 " | 2.0 " | 220 | 208 " | 2.78 " |
| 50 | 646 " | 2.2 " | 240 | 152 " | 2.82 " |
| 60 | 624 " | 2.3 " | 260 | 96 " | 2.85 " |
| 70 | 601 " | 2.4 " | 273 | 58 " | 2.88 " |
| 80 | 577 " | 2.4 " | 280 | 38 " | 2.89 " |
| 90 | 552 " | 2.5 " | 293 | 0 | 2.9 " |
| 100 | 528 " | 2.5 " | 300 | -20 | 2.9 " |

THERMAL EXPANSION of TIN (GRAY)

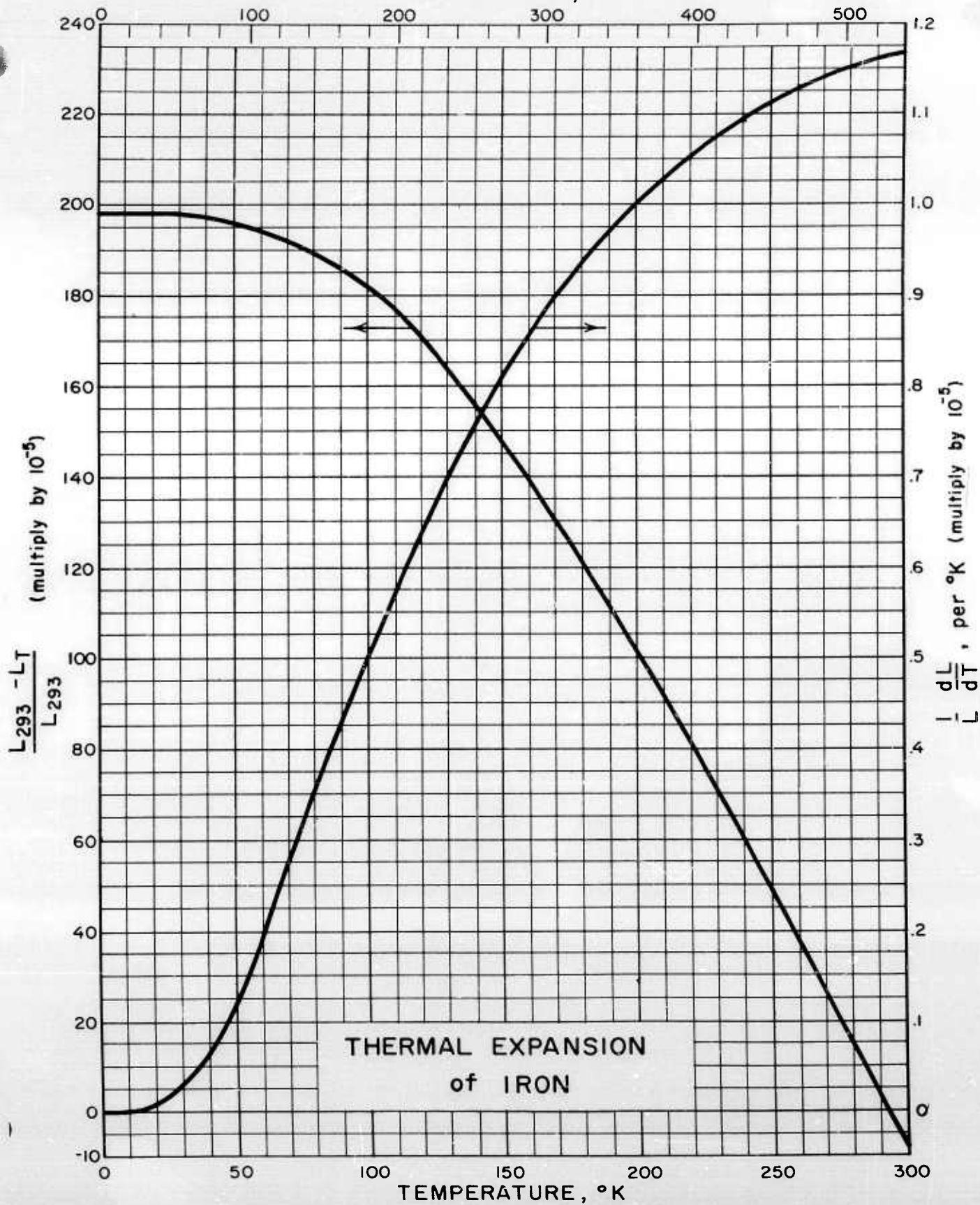
References: Thewlis and Davey 1954

Discussion: Gray tin is a brittle form with diamond-type lattice that is stable below 18°C. The ordinary ductile variety of tin (white tin) if pure may transform to gray tin at low ambient temperatures but is stabilized by the presence of impurities.

Data: The data cover the range -130 to +20°C and are represented by a constant expansion coefficient,

$$\frac{1}{L} \frac{dL}{dT} = 0.47 \times 10^{-5} \text{ per } ^\circ\text{C}.$$

TEMPERATURE, °R



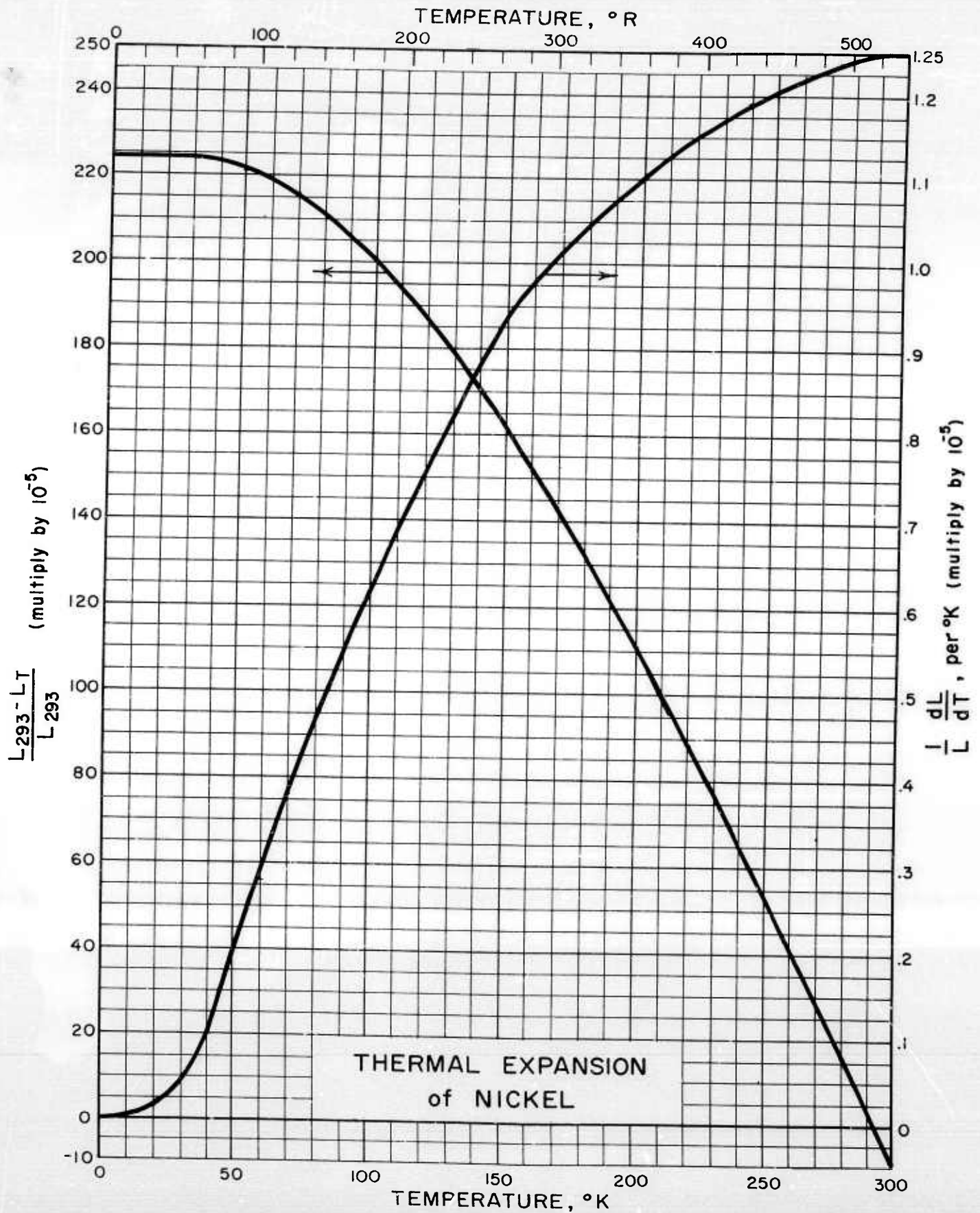
THERMAL EXPANSION of IRON

Sources of Data: Ebert 1928, Nix and MacNair 1941

Other References: Adenstedt 1936, Dorsey 1907, Simon and Bergmann 1930.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 198×10^{-5} | 0 | 140 | 156×10^{-5} | 0.76×10^{-5} |
| 20 | 198 " | 0.01×10^{-5} | 160 | 140 " | 0.86 " |
| 30 | 198 " | .03 " | 180 | 122 " | 0.94 " |
| 40 | 197 " | .07 " | 200 | 102 " | 1.00 " |
| 50 | 196 " | .13 " | 220 | 82 " | 1.05 " |
| 60 | 195 " | .20 " | 240 | 60 " | 1.09 " |
| 70 | 192 " | .28 " | 260 | 38 " | 1.13 " |
| 80 | 189 " | .35 " | 273 | 23 " | 1.14 " |
| 90 | 185 " | .42 " | 280 | 15 " | 1.15 " |
| 100 | 181 " | .49 " | 293 | 0 " | 1.16 " |
| 120 | 170 " | .63 " | 300 | -8 " | 1.17 " |



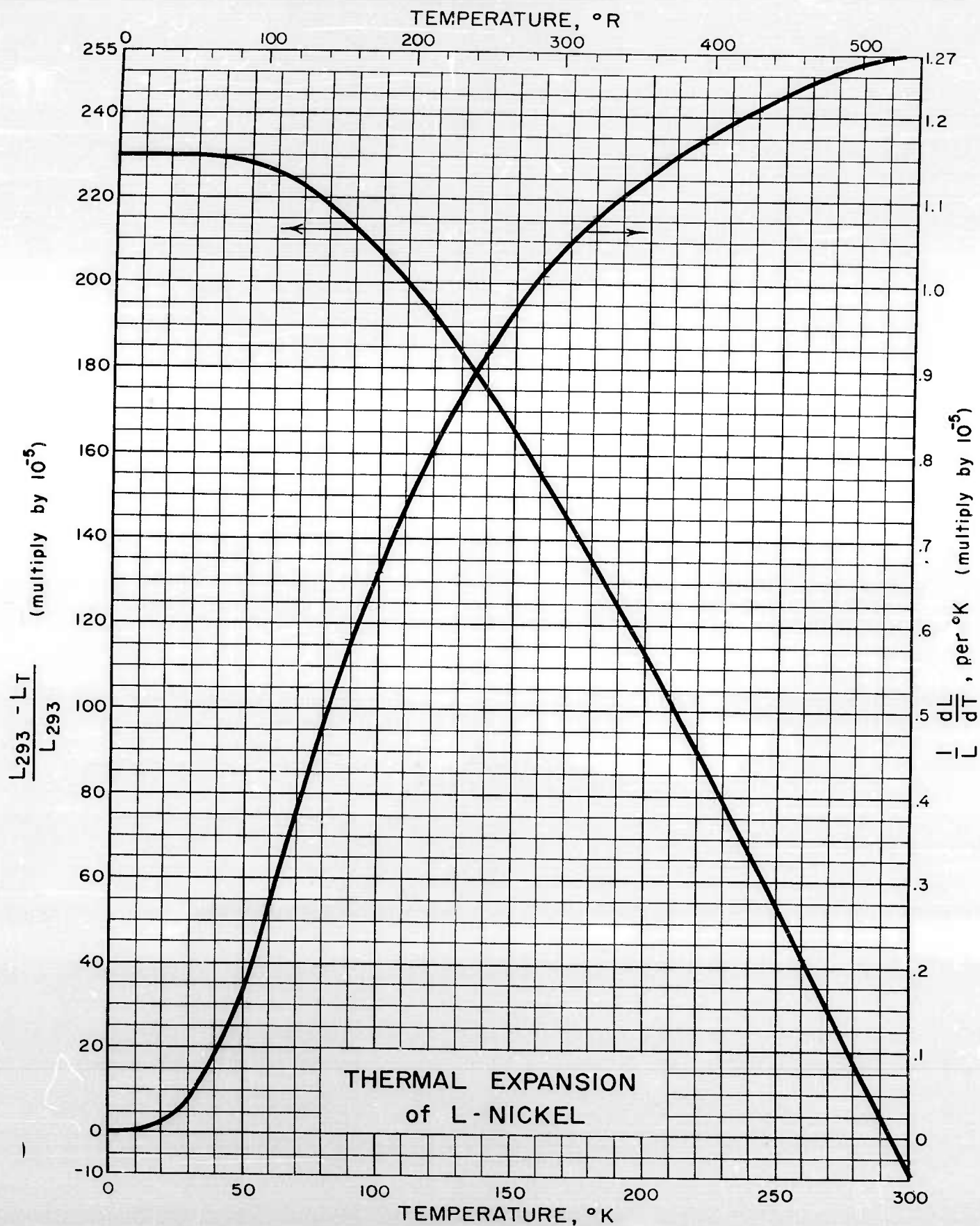
THERMAL EXPANSION of NICKEL

Sources of Data: Krupkowski and DeHaas 1928, Nix and MacNair 1941.

Other References: Adenstedt 1936, Altman, Rubin and Johnston 1954, Aoyama and Ito 1939, Disch 1921, Henning 1907, Simon and Bergmann 1930.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 224×10^{-5} | 0. | 140 | 171×10^{-5} | 0.88×10^{-5} |
| 20 | 224 " | 0.02×10^{-5} | 160 | 152 " | 0.98 " |
| 30 | 224 " | .05 " | 180 | 132 " | 1.05 " |
| 40 | 223 " | .10 " | 200 | 111 " | 1.10 " |
| 50 | 221 " | .19 " | 220 | 88 " | 1.15 " |
| 60 | 219 " | .28 " | 240 | 65 " | 1.19 " |
| 70 | 216 " | .38 " | 260 | 41 " | 1.22 " |
| 80 | 211 " | .47 " | 273 | 25 " | 1.23 " |
| 90 | 206 " | .55 " | 280 | 16 " | 1.24 " |
| 100 | 201 " | .61 " | 293 | 0 " | 1.25 " |
| 120 | 187 " | .75 " | 300 | -9 " | 1.25 " |



THERMAL EXPANSION of L-NICKEL

(International Nickel Co. low-carbon nickel, 99.6% pure)

Source of Data: Altman, Rubin and Johnston 1954.

Table of Selected Values

| Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K | Temp. °K | $\frac{L_{293} - L_T}{L_{293}}$ | $\frac{1}{L} \frac{dL}{dT}$ per °K |
|-------------|---------------------------------|---------------------------------------|-------------|---------------------------------|---------------------------------------|
| 0 | 230×10^{-5} | 0 | 140 | 175×10^{-5} | 0.92×10^{-5} |
| 20 | 230 " | $.01 \times 10^{-5}$ | 160 | 156 " | 1.01 " |
| 30 | 230 " | .04 " | 180 | 135 " | 1.08 " |
| 40 | 229 " | .09 " | 200 | 113 " | 1.13 " |
| 50 | 228 " | .17 " | 220 | 90 " | 1.17 " |
| 60 | 226 " | .27 " | 240 | 66 " | 1.21 " |
| 70 | 223 " | .38 " | 260 | 42 " | 1.24 " |
| 80 | 218 " | .48 " | 273 | 25 " | 1.26 " |
| 90 | 213 " | .58 " | 280 | 17 " | 1.27 " |
| 100 | 207 " | .66 " | 293 | 0 " | 1.28 " |
| 120 | 192 " | .80 " | 300 | -9 " | 1.29 " |

THERMAL CONDUCTIVITY of CRYOGENIC SOLIDS

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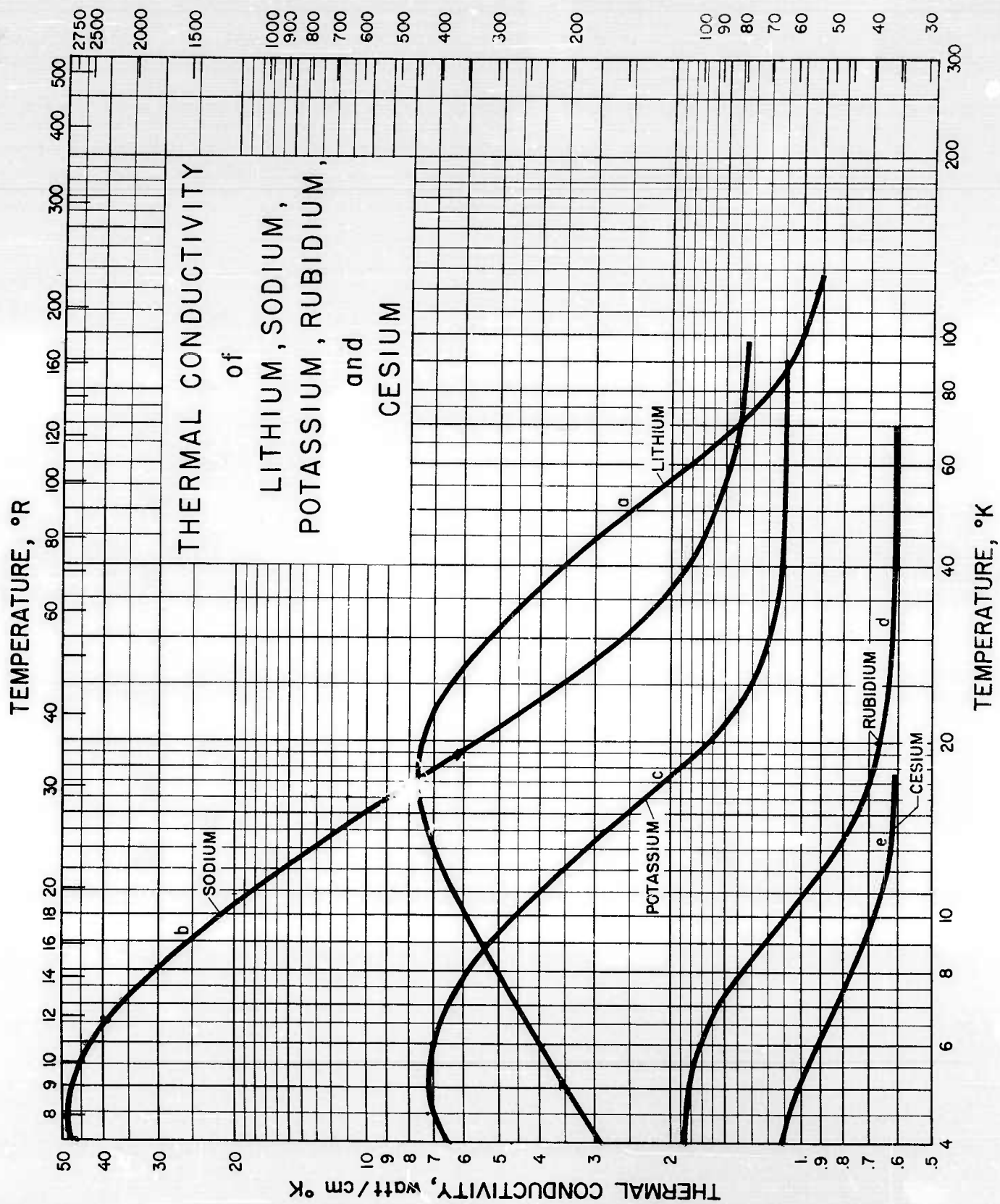
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| Thermal Conductivity of Coppers (various types)..... | 3.112-1 |
| Thermal Conductivity of Silver and Gold..... | 3.112-2 |
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| Thermal Conductivity of Lanthanum, Cerium, and Uranium..... | 3.131 |
| Thermal Conductivity of Aluminum, Gallium, Indium, and Thallium..... | 3.132 |
| Thermal Conductivity of Titanium, Zirconium, and Hafnium..... | 3.141 |
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| Thermal Conductivity of Tin and Lead..... | 3.142-3 |
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| Thermal Conductivity of Antimony and Bismuth..... | 3.152 |
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| Thermal Conductivity of Copper-Nickel and Silver Alloys..... | 3.212-2 |
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| Thermal Conductivity of Nickel Alloys..... | 3.281 |
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| Thermal Conductivity of Ferrous Alloys..... | 3.301 |
| Thermal Conductivity of Glasses and Plastics..... | 3.501 |

CONVERSION FACTORS for THERMAL CONDUCTIVITY

| | $\frac{\text{Watts cm}}{\text{cm}^2 \text{ } ^\circ\text{K}}$ | $\frac{\text{Watts in}}{\text{in}^2 \text{ } ^\circ\text{F}}$ | $\frac{\text{Cal cm}}{\text{sec cm}^2 \text{ } ^\circ\text{K}}$ | $\frac{\text{BTU in}}{\text{hr ft}^2 \text{ } ^\circ\text{F}}$ | $\frac{\text{BTU ft}}{\text{hr ft}^2 \text{ } ^\circ\text{F}}$ | $\frac{\text{BTU in}}{\text{sec in}^2 \text{ } ^\circ\text{F}}$ | $\frac{\text{BTU in}}{\text{hr in}^2 \text{ } ^\circ\text{F}}$ |
|--|---|---|---|--|--|---|--|
| $1 \frac{\text{Watts cm}}{\text{cm}^2 \text{ } ^\circ\text{K}} =$ | 1.000 | 1.411 | 0.2389 | 6.9340×10^2 | 57.79 | 1.338×10^{-3} | 4.816 |
| $1 \frac{\text{Watts in}}{\text{in}^2 \text{ } ^\circ\text{F}} =$ | 0.7087 | 1.000 | 0.1693 | 4.914×10^2 | 40.95 | 9.480×10^{-4} | 3.413 |
| $1 \frac{\text{Cal. cm}}{\text{sec cm}^2 \text{ } ^\circ\text{K}} =$ | 4.1858 | 5.907 | 1.000 | 2.9027×10^3 | 2.419×10^2 | 5.602×10^{-3} | 20.16 |
| $1 \frac{\text{BTU in}}{\text{hr ft}^2 \text{ } ^\circ\text{F}} =$ | 1.442×10^{-3} | 2.035×10^{-3} | 3.445×10^{-4} | 1.000 | 8.33×10^{-2} | 1.929×10^{-6} | 6.944×10^{-3} |
| $1 \frac{\text{BTU ft}}{\text{hr ft}^2 \text{ } ^\circ\text{F}} =$ | 1.730×10^{-2} | 2.442×10^{-2} | 4.135×10^{-3} | 12.000 | 1.000 | 2.315×10^{-5} | 8.333×10^{-2} |
| $1 \frac{\text{BTU in}}{\text{sec in}^2 \text{ } ^\circ\text{F}} =$ | 7.4738×10^2 | 1.0548×10^3 | 1.785×10^2 | 5.184×10^5 | 4.3191×10^4 | 1.000 | 3.600×10^3 |
| $1 \frac{\text{BTU in}}{\text{hr in}^2 \text{ } ^\circ\text{F}} =$ | 0.2076 | 0.2930 | 4.960×10^{-2} | 1.44×10^2 | 12.000 | 2.778×10^{-4} | 1.000 |

JRC/VJJ Issued: 10/7/59
Revised: 5/20/60

THERMAL CONDUCTIVITY, BTU / hr ft °R



THERMAL CONDUCTIVITY OF LITHIUM, SODIUM
POTASSIUM, RUBIDIUM, and CESIUM

- Source of Data:
- (a) D.K.C. MacDonald, G.K. White and S.B. Woods, Proc. Roy. Soc. (London) A235, 358-374 (1956).
 - (b) Same as (a); and R. Berman and D.K.C. MacDonald, Proc. Roy. Soc. (London) A209, 368-375 (1951).
 - (c) Same as (a).
 - (d) Same as (a).
 - (e) Same as (a).

- Comments:
- (a) Lithium; "high purity," melted and extruded into a stainless steel tube, (A.D. Mackay)
 - (b) Sodium; "exceptional purity" melted in vacuum and cast in glass, (Philips); and trace of silver, melted in vacuum and cast in glass, (Philips)
 - (c) Potassium; "high purity," melted in vacuum and cast in glass
 - (d) Rubidium; "high purity," melted in vacuum and cast in glass, (Mackay)
 - (e) Cesium; "high purity," melted in vacuum and cast in glass, (Mackay)

RLP Issued: 5/1/58
Revised: 3/1/59

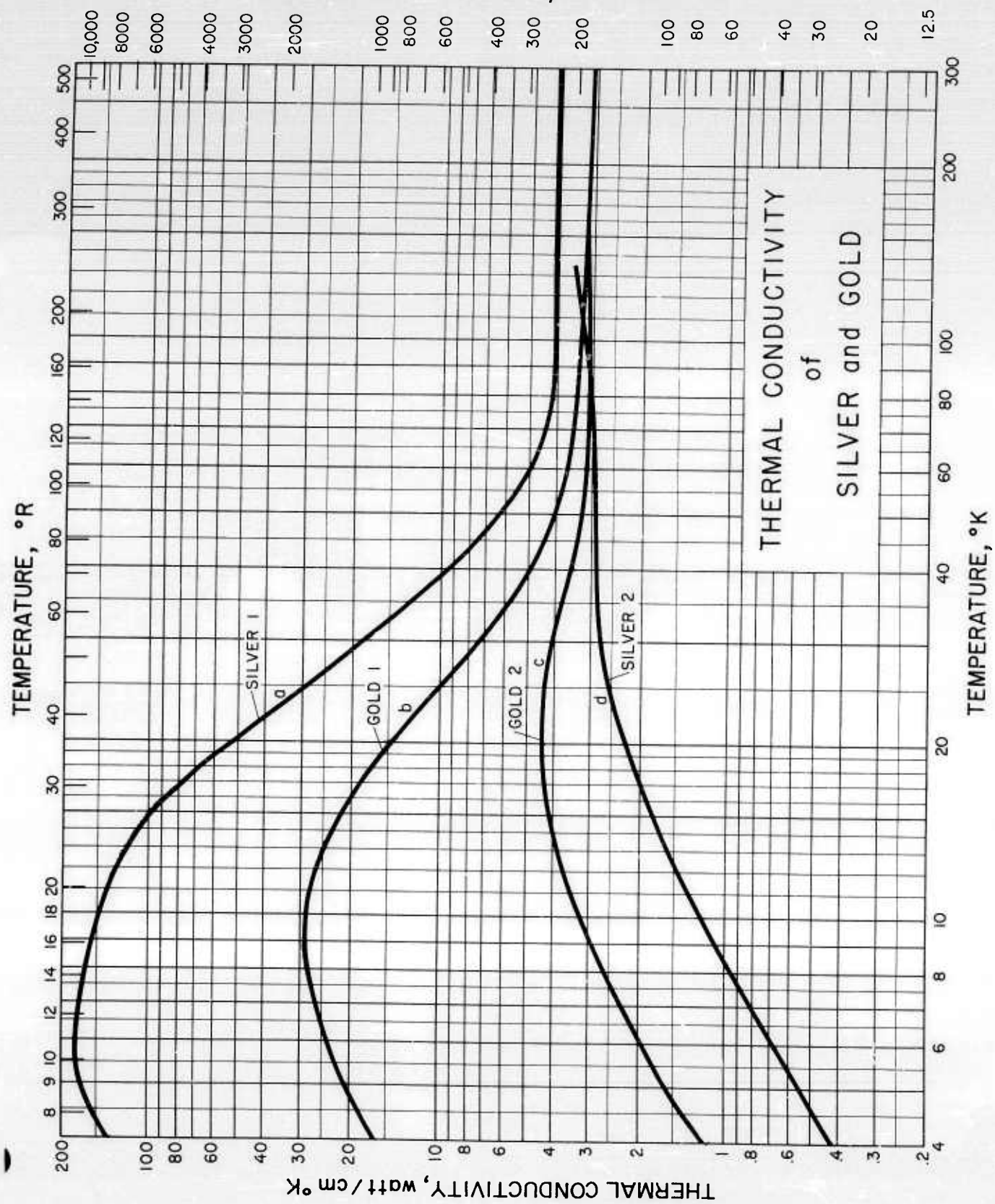
THERMAL CONDUCTIVITY
of COPPERS

- Source of Data:
- (a) R. L. Powell, H. M. Roder and W. J. Hall,
to be published
 - (b) R. L. Powell, H. M. Roder and W. M. Rogers,
J. Appl. Phys. 28, 1282-1288 (1957)
 - (c) Same as (b).
 - (d) R. W. Powers, D. Schwartz and H. L.
Johnston, TR 264-5, Cryogenics Laboratory,
Ohio State University (1951) 11 pp.
 - (e) R. L. Powell and D. O. Coffin, Rev. Sci.
Instr. 26, 516 (1955).
 - (f) Same as (b).

- Comments:
- (a) High Purity; 99.999% pure, annealed, (Am. Smelt
Ref.)
 - (b) Coalesced; 99.98% pure, annealed, (Phelps Dodge)
 - (c) Electrolytic Tough Pitch; 99.95% pure, annealed
 - (d) O.F.H.C.; 99.95% pure, annealed
 - (e) (Pb) Cu; 1% Pb, annealed
 - (f) (Te) Cu; 0.6% Te, annealed

RLP Issued: 5/1/58
Revised: 3/1/59

THERMAL CONDUCTIVITY, BTU/hr ft °R

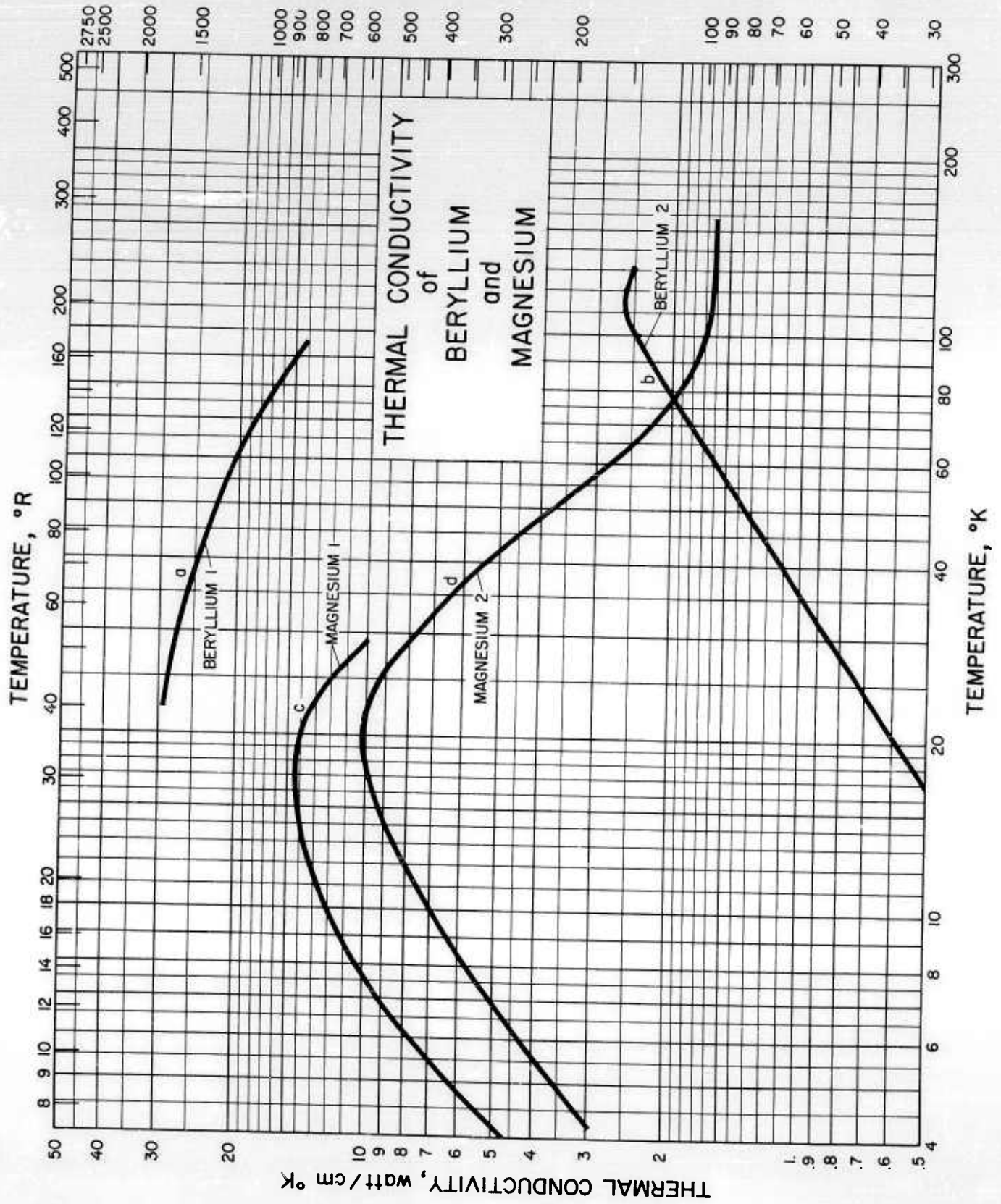


THERMAL CONDUCTIVITY
of SILVER and GOLD

- Source of Data: (a) G. K. White, Proc. Phys. Soc.
(London) A66, 844-845 (1953);
C. H. Lees, Phil. Trans. Roy. Soc.
(London) A208, 381-443 (1908)
- (b) G. K. White, Ibid. (a)
- (c) G. K. White, Proc. Phys. Soc.
(London) A66, 559-564 (1953);
W. Meissner, Ann. Physik 47,
1001-1058 (1915)
- (d) G. K. White, Ibid. (c)
- Comments: (a) Silver 1; 99.999% pure, annealed, and
99.9% pure (Johnson, Matthey)
- (b) Silver 2; 99.999% pure, drawn (Johnson, Matthey)
- (c) Gold 1; 99.999% pure, annealed (Johnson, Matthey),
99.999% pure, annealed (Mylius)
- (d) Gold 2; 99.9% pure, drawn, (Garrett)

RLP Issued: 5/1/58
Revised: 3/1/59

THERMAL CONDUCTIVITY, BTU / hr ft °K



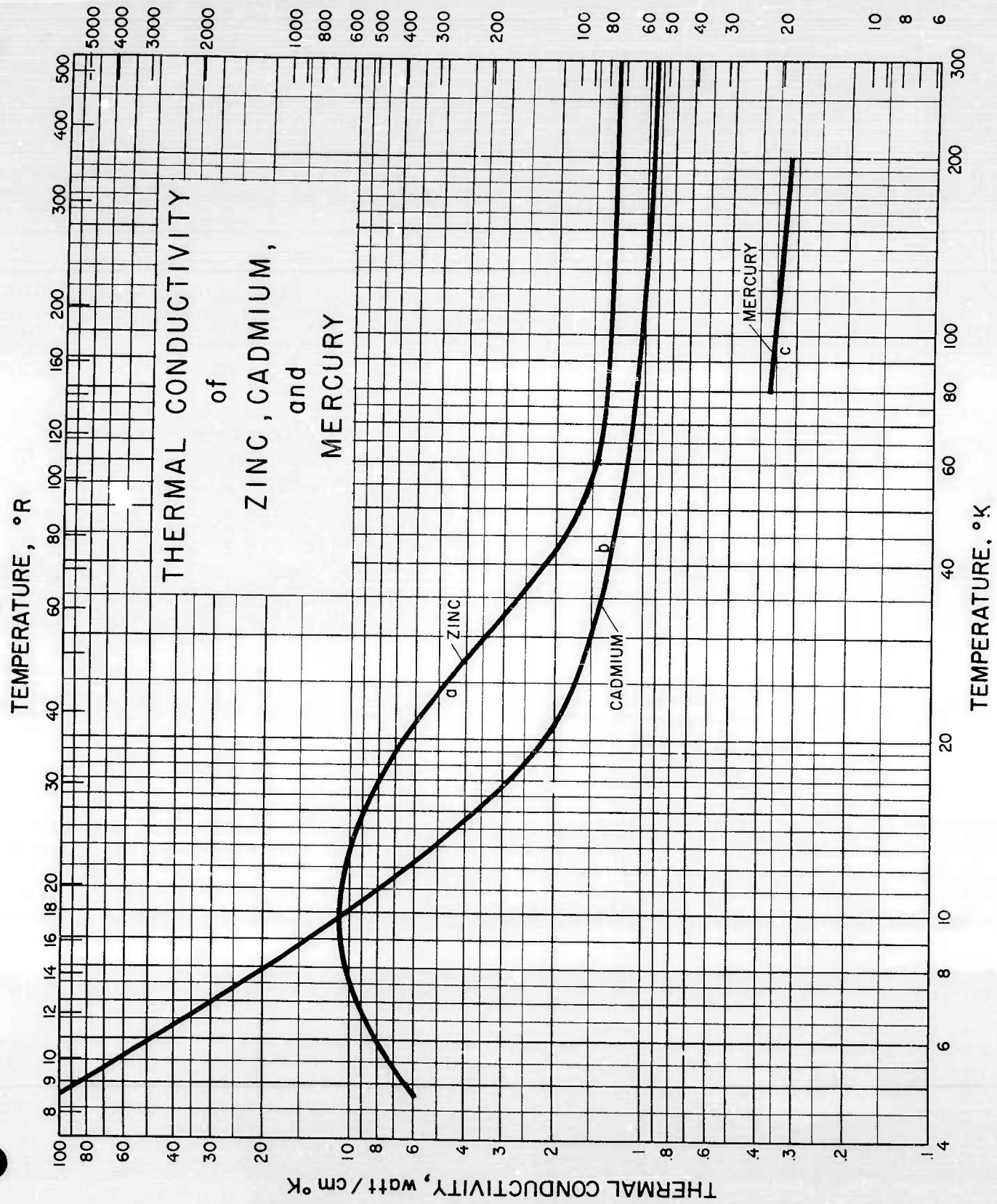
THERMAL CONDUCTIVITY of
BERYLLIUM and MAGNESIUM

- Source of Data: (a) H.-D. Erfling and E. Gruneisen, Ann. Physik 41, 89-99 (1942).
- (b) G.K. White and S.B. Woods, Can. J. Physics 33, 58-73 (1955).
- (c) W.R.G. Kemp, A.K. Sreedhar and G.K. White, Proc. Phys. Soc. (London) A66, 1077-1078 (1953).
- (d) Same as (c)

- Comments: (a) Beryllium-1; "high Purity" single crystal, (Degussa)
- (b) Beryllium-2; 2% magnesium, sintered rod, (Brush)
- (c) Magnesium-1; 99.98% pure, annealed in vacuum 3 hours at 350°C, (Johnson, Matthey)
- (d) Magnesium-2; 99.98% pure, cold drawn, (Johnson, Matthey)

RLP Issued: 5/1/58
Revised: 3/1/59

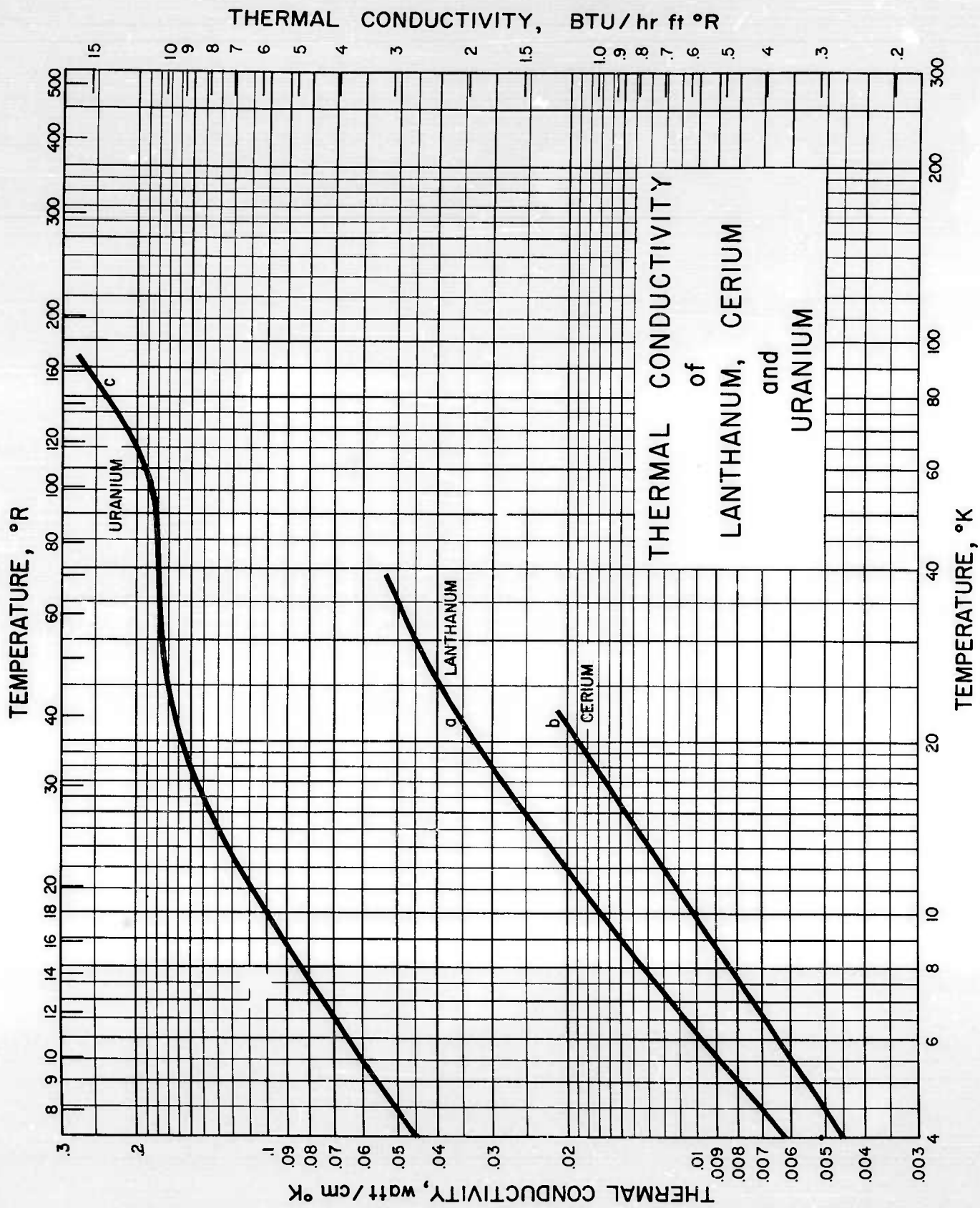
THERMAL CONDUCTIVITY, BTU / hr ft °R



THERMAL CONDUCTIVITY of
ZINC, CADMIUM, and MERCURY

- Source of Data:
- (a) H. M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955); C. C. Bidwell and E. J. Lewis, Phys. Rev. 33, 249-251 (1929).
 - (b) H. M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955); E. Goens and E. Gruneisen, Ann. Physik 14, 164-180 (1932).
 - (c) H. Reddemann, Ann. Physik 14, 139-163 (1932).
- Comments:
- (a) Zinc; 99.997% pure, single crystal, annealed, (Imperial Smelt); and 99.993 pure, single crystal
 - (b) Cadmium; 99.995% pure, single crystal, (Hilger); and "pure" single crystal, (Kahlbaum)
 - (c) Mercury; Average values for ten single crystals

RLP Issued: 5/1/58
Revised: 3/1/59



THERMAL CONDUCTIVITY of
LANTHANUM, CERIUM, and URANIUM

Source of Data: (a) H.M. Rosenberg, Phil. Trans. Roy.
Soc. (London) A247, 441-497 (1955).

(b) Same as (a).

(c) Same as (a).

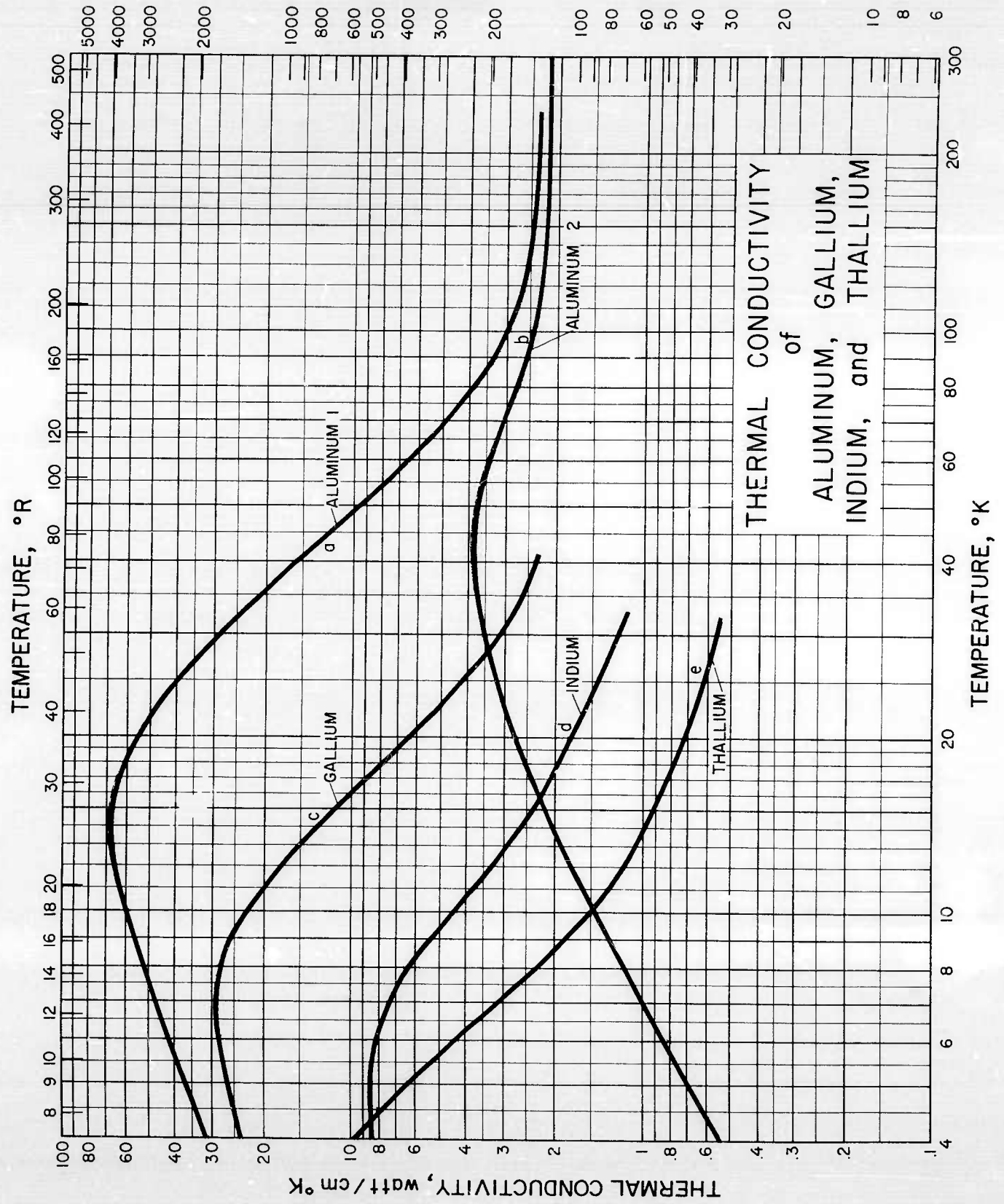
Comments: (a) Lanthanum; 99.94% pure

(b) Cerium; 99.6% pure

(c) Uranium; "Very high" purity

RLP Issued: 5/1/58
Revised: 3/1/59

THERMAL CONDUCTIVITY, BTU/hr ft °R

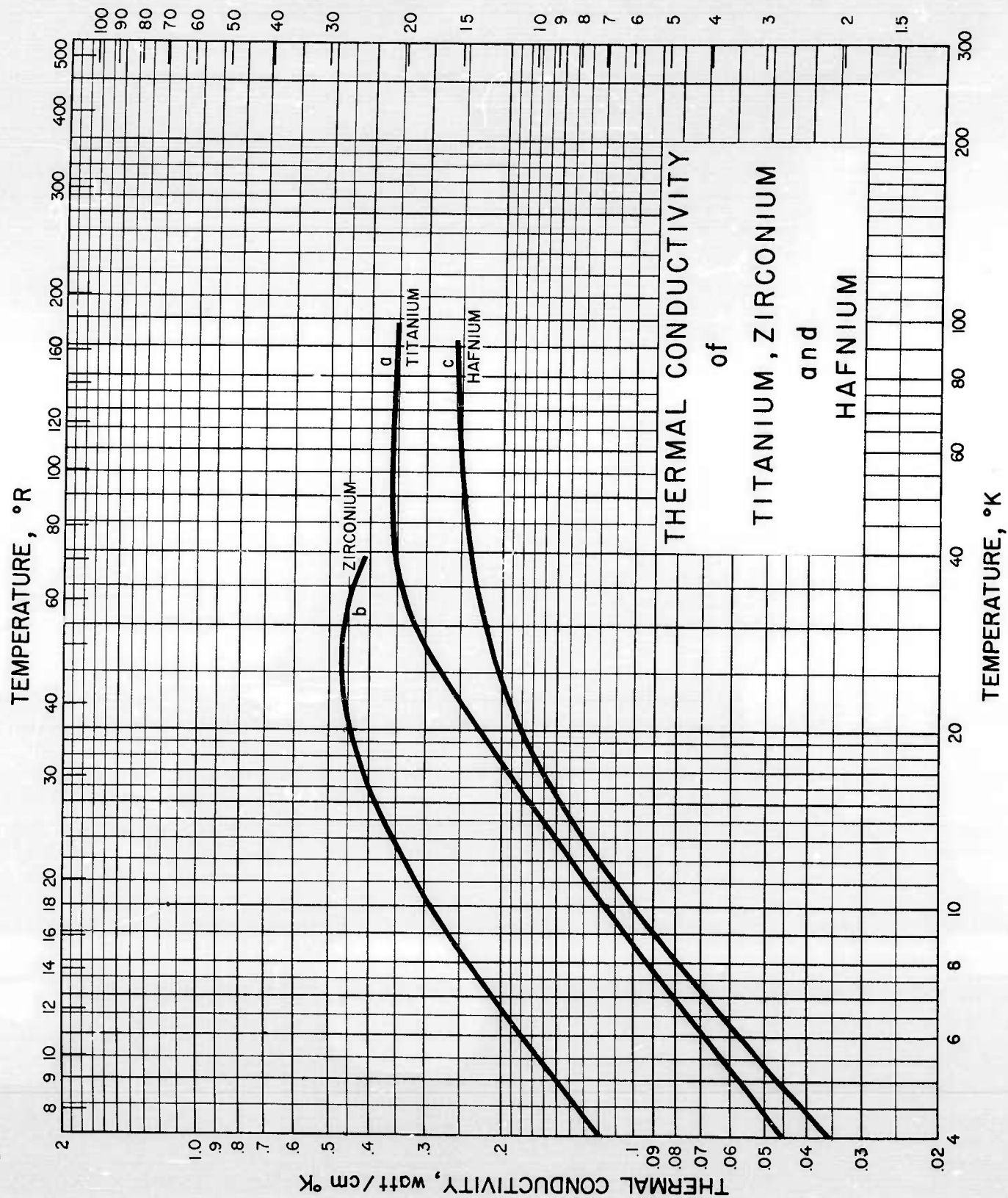


THERMAL CONDUCTIVITY of ALUMINUM,
GALLIUM, INDIUM, and THALLIUM

- Source of Data:
- (a) R. A. Andrews, R. T. Webber and D. A. Spohr, Phys. Rev. 84, 994-996 (1951); R. W. Powers, D. Schwartz, and H. L. Johnston, TR 264-5, Cryogenic Laboratory, Ohio State University 11 pp (1951).
 - (b) R. L. Powell, W. J. Hall and H. M. Roder, to be published.
 - (c) H. M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955).
 - (d) Same as (c)
 - (e) Same as (c)
- Comments:
- (a) Aluminum-1; 99.996% pure, single crystal (Alcoa) and 99.99% pure, cold drawn (Alcoa)
 - (b) Aluminum-2; 99% commercial pure, (Alcoa) drawn
 - (c) Gallium; Single crystal
 - (d) Indium; 99.993% pure, (Johnson, Matthey)
 - (e) Thallium; 99.99% pure, (Johnson, Matthey)

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THERMAL CONDUCTIVITY, BTU / hr ft °R



THERMAL CONDUCTIVITY of
TITANIUM, ZIRCONIUM, and HAFNIUM

Source of Data: (a) H.M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955)

(b) Same as (a)

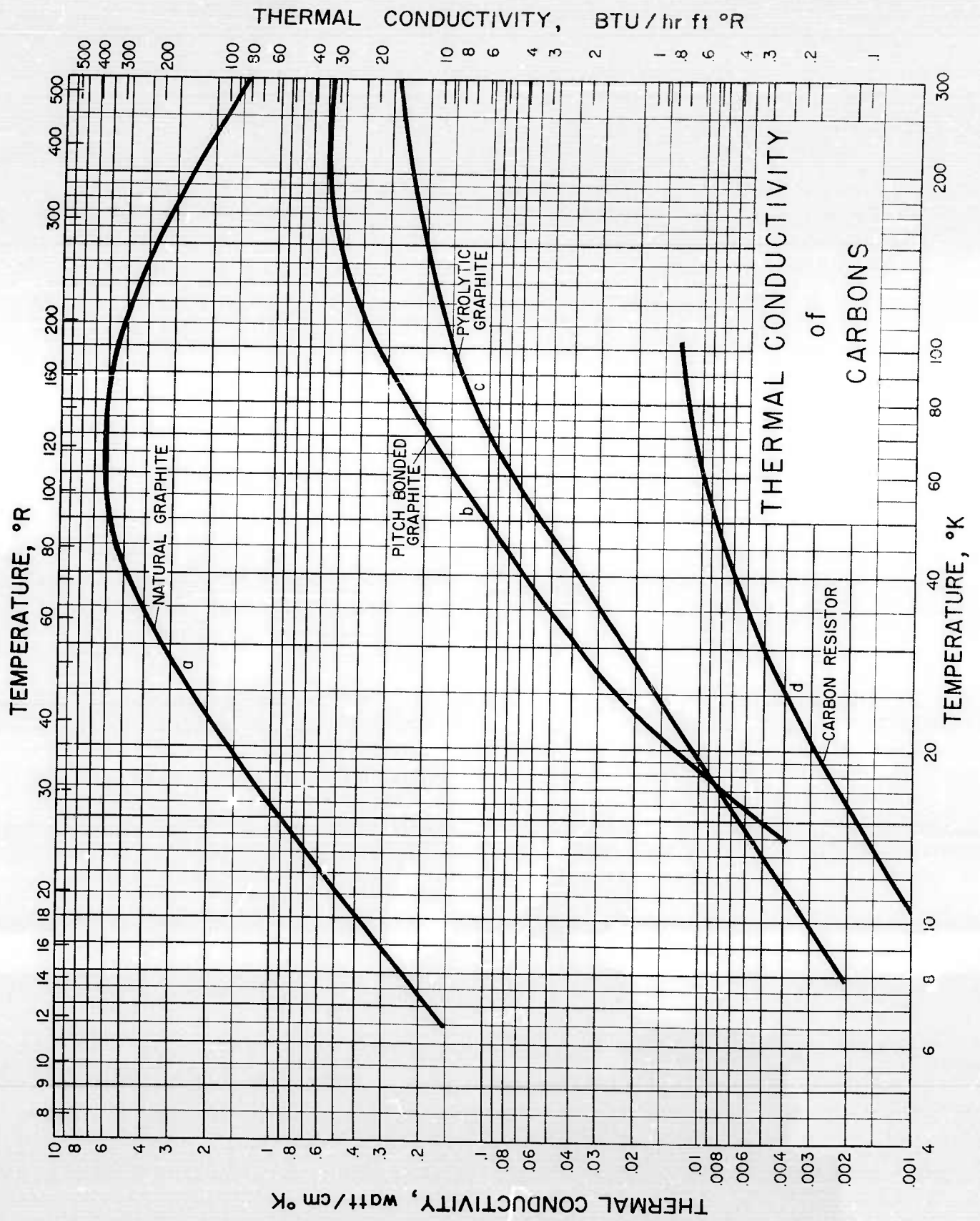
(c) G.K. White and S.B. Woods, Can. J. Physics 35, 892-900 (1957)

Comments: (a) Titanium; 99.99% pure, (Assoc. Elec. Industries) single crystal

(b) Zirconium; 98% pure, (Metropolitan Vickers)

(c) Hafnium: 1% Zr., (Foote Mineral)

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3.142-1

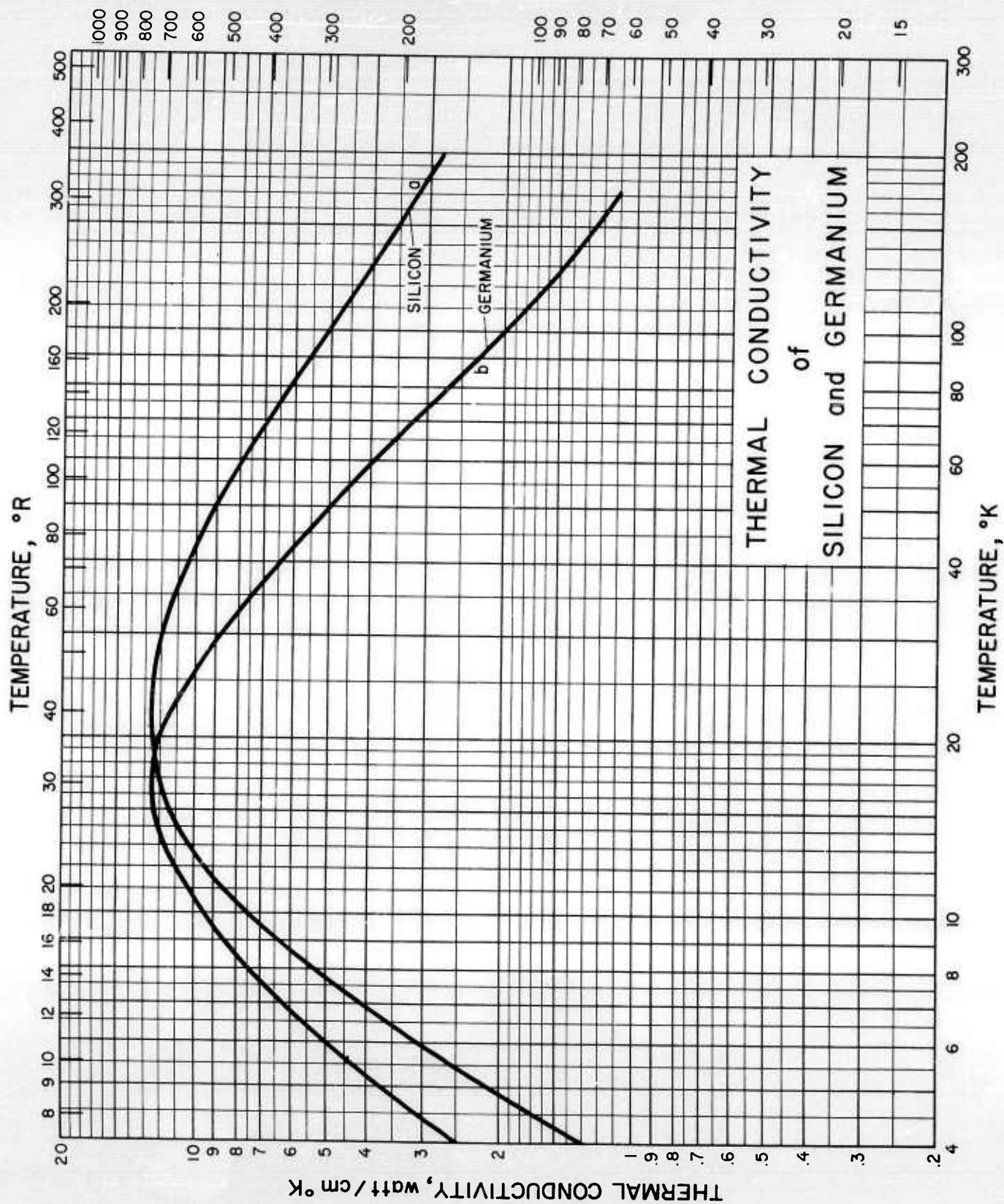
THERMAL CONDUCTIVITY
of CARBONS

- Source of Data: (a) W.W. Smith and N.S. Rasor, Phys. Rev.
104, 885 (1956)
- (b) Same as (a)
- (c) Same as (a)
- (d) R. Berman, Bull. Inst. Int. du Froid,
Annexe 1952-1 (1952)

- Comments: (a) Natural Graphite; National Carbon
- (b) Pitch Bonded Graphite; Type AGOT-KC
- (c) Pyrolytic Graphite; National Carbon
- (d) Carbon Resistor;

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THERMAL CONDUCTIVITY, BTU/hr ft °R



3.142-2

THERMAL CONDUCTIVITY of
SILICON and GERMANIUM

Source of Data: (a) G.K. White and S.B. Woods, Phys. Rev.
103, 569-571 (1956)

(b) Same as (a)

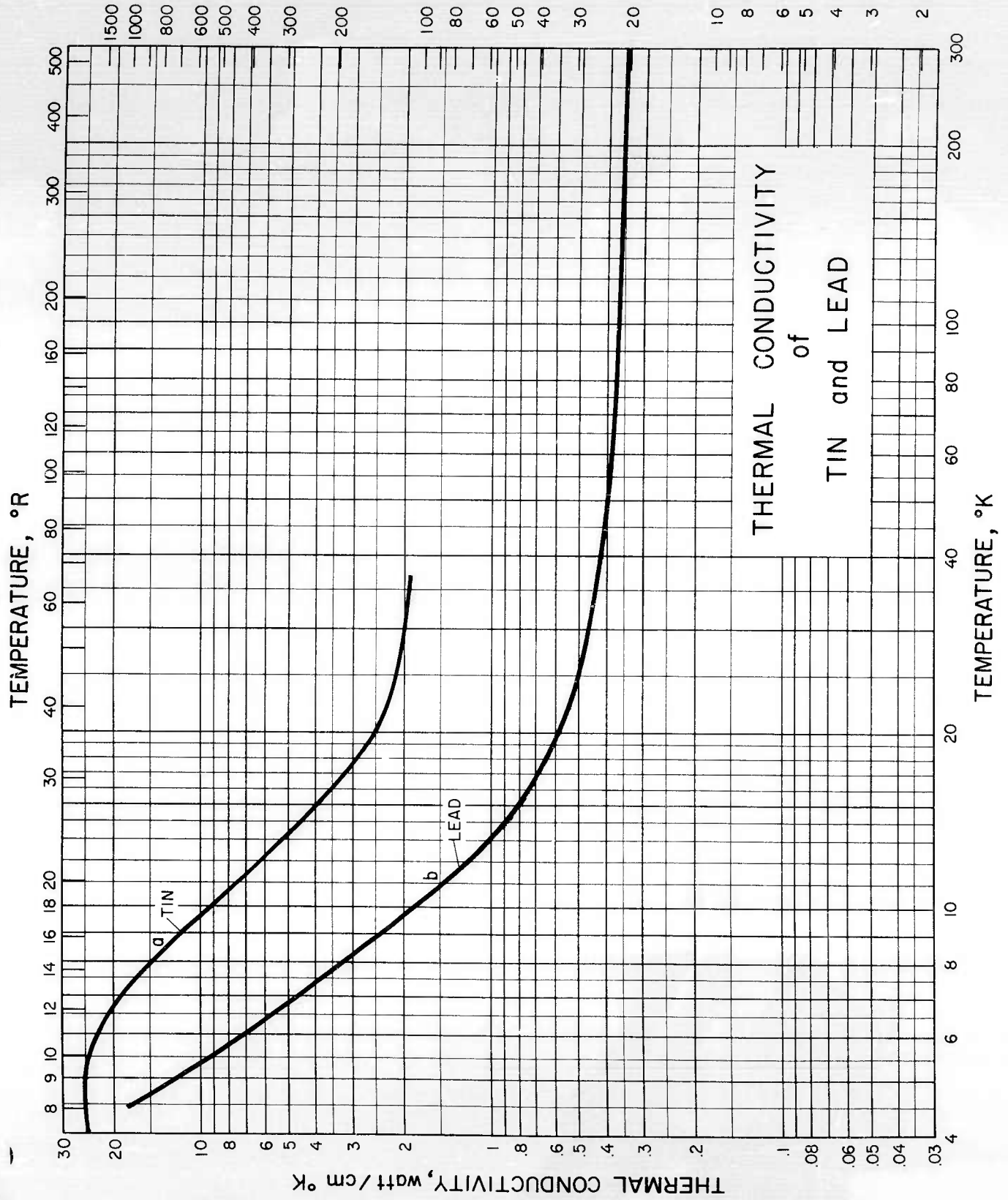
Comments: (a) Silicon; n-type single crystal

(b) Germanium; p-type

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3.142-3

THERMAL CONDUCTIVITY, BTU/hr ft °R



THERMAL CONDUCTIVITY
of TIN and LEAD

Source of Data: (a) H.M. Rosenberg, Phil. Trans. Roy. Soc.
(London) A247, 441-497 (1955)

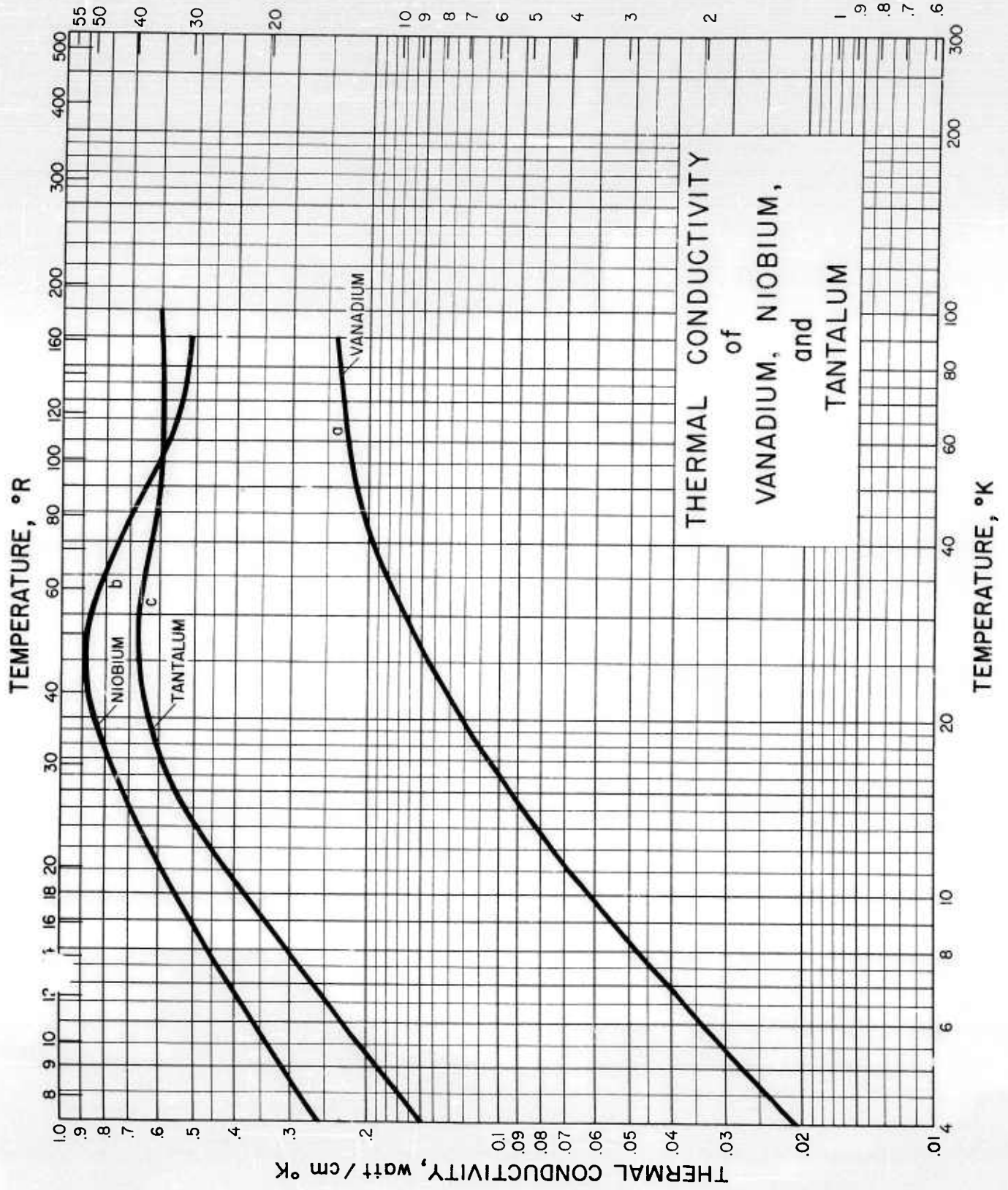
(b) Same as (a) and W. Meissner, Ann.
Physik 47, 1001-1058 (1915)

Comments: (a) Tin; 99.995% pure, single crystal, (Johnson,
Matthey)

(b) Lead; 99.998% pure, single crystal (Tadanac)
and 99.998% pure, cold drawn, (Kahlbaum)

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THERMAL CONDUCTIVITY, BTU / hr ft °R



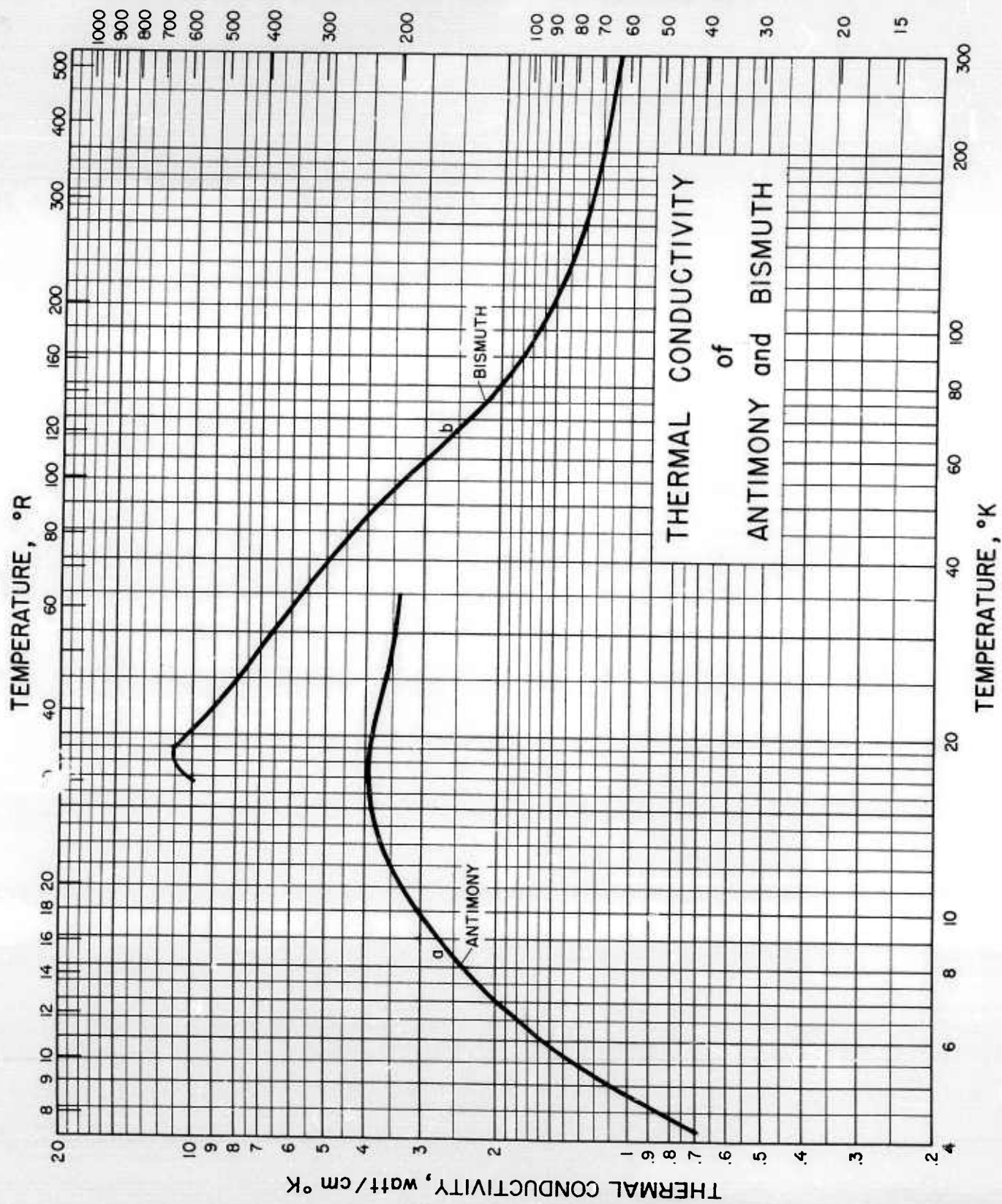
THERMAL CONDUCTIVITY of
VANADIUM, NIOBIUM, and TANTALUM

- Source of Data: (a) G. K. White and S. B. Woods, Can. J.
Physics 35, 892-900 (1957)
- (b) Same as (a)
- (c) H. M. Rosenberg, Phil. Trans. Roy. Soc.
(London) A247, 441-497 (1955)

- Comments: (a) Vanadium; 99.9% pure, (Electrometallurgical Co.)
- (b) Niobium; 99.9% pure, annealed in vacuum, (Fansteel
Metal)
- (c) Tantalum; 99.98% pure, (Johnson, Matthey)

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THERMAL CONDUCTIVITY, BTU/hr ft °R



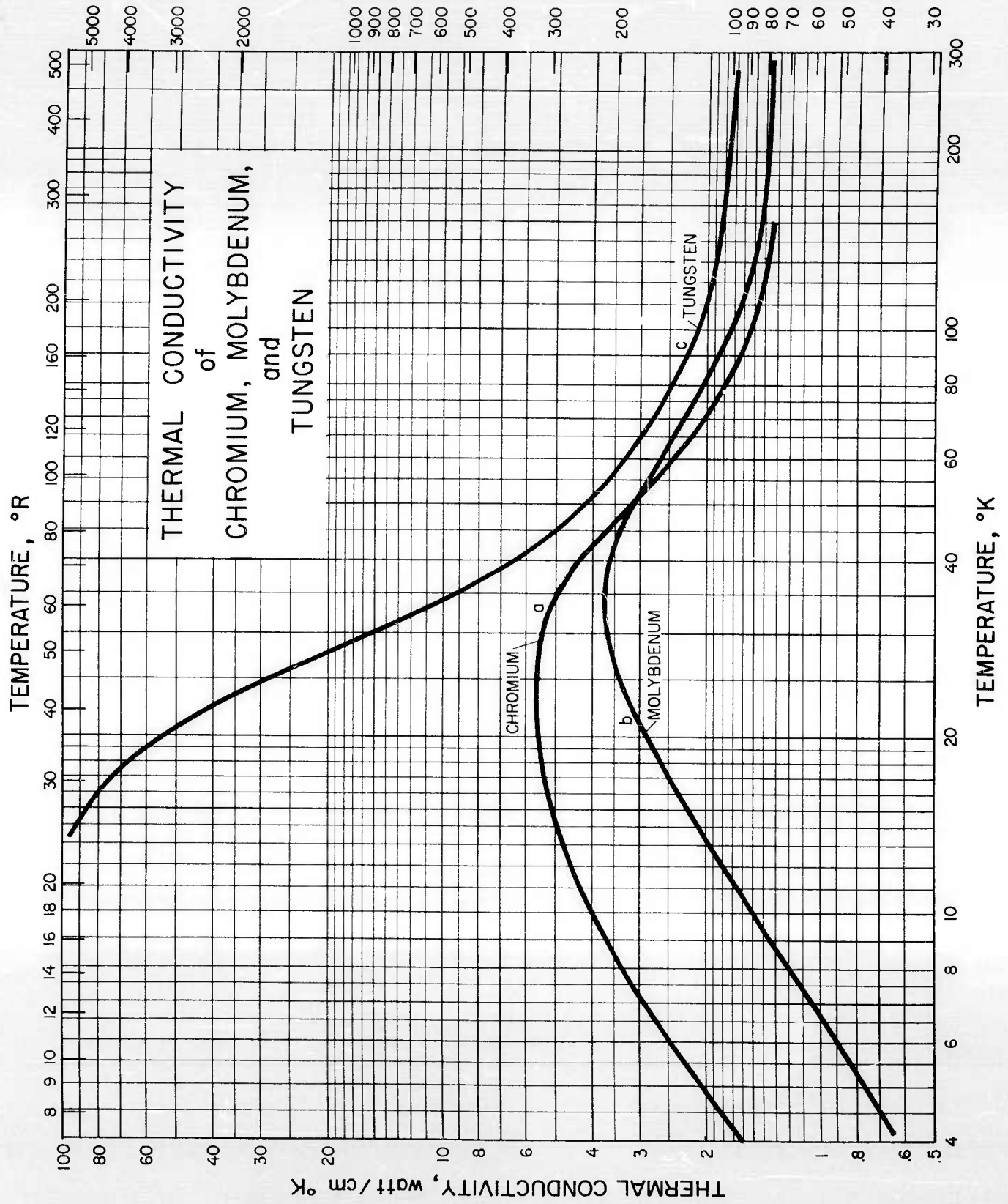
THERMAL CONDUCTIVITY of
ANTIMONY and BISMUTH

Source of Data: (a) H. M. Rosenberg, Phil. Trans. Roy. Soc.
(London) A247, 441-497 (1955)
A. Eucken and G. Gelhoff, Deutsch Physik
Gesell, 14, 169-182 (1912)
(b) W. J. deHaas and W. J. Capel, Physica 1,
929-934 (1934)
H. Reddemann, Ann. Physik 20, 441-448 (1934)

Comments: (a) Antimony; annealed, (Johnson, Matthey)
cold drawn (Kahlbaum)
(b) Bismuth; 99.995% pure, single crystal, (Hilger)
single crystal, (Kahlbaum)

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THERMAL CONDUCTIVITY, BTU/hr ft °R

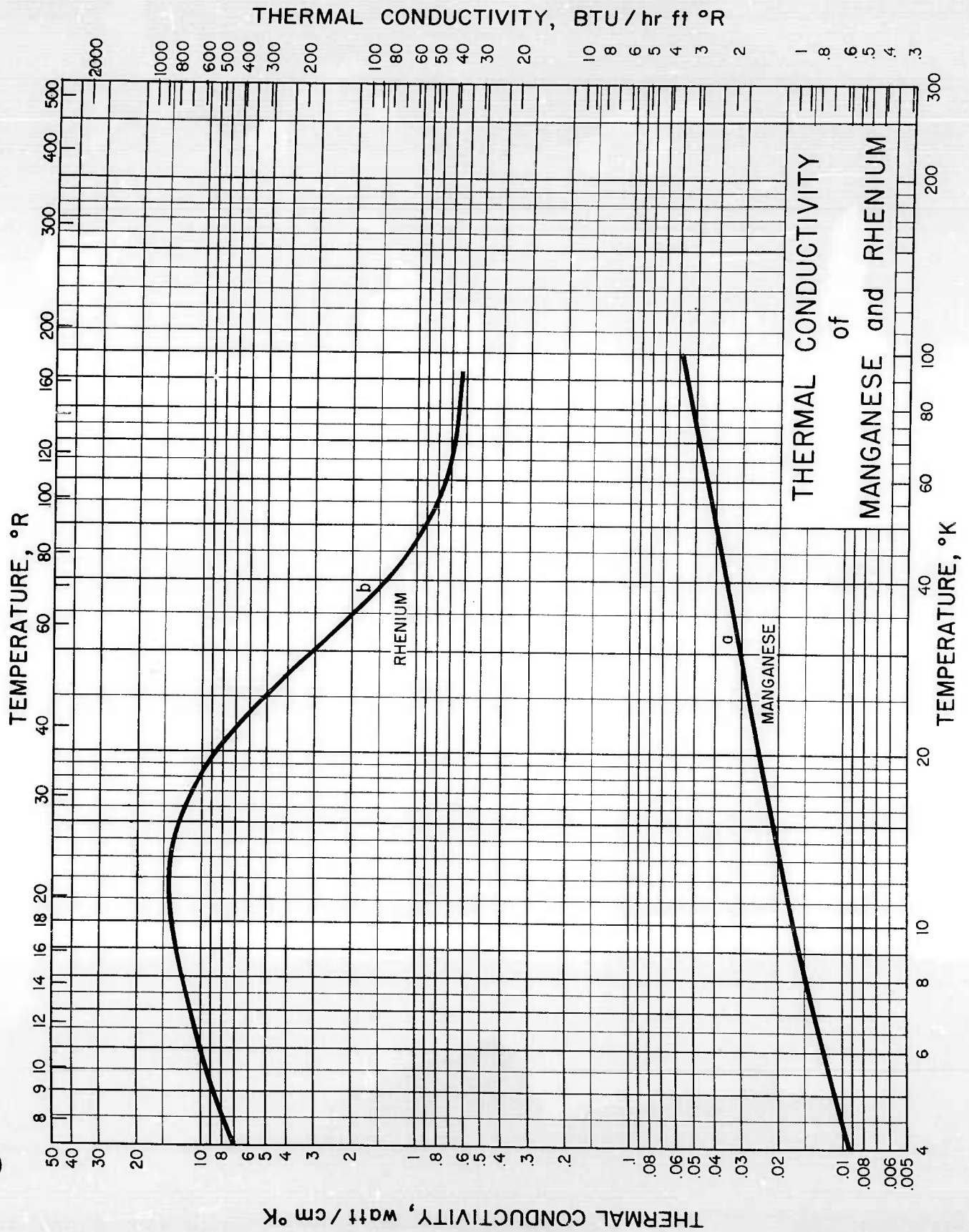


THERMAL CONDUCTIVITY OF CHROMIUM,
MOLYBDENUM, and TUNGSTEN

- Source of Data: (a) A.F.A. Harper, W.R.G. Kemp, P.G. Klemens, R.J. Tainsh, and G.K. White, Phil. Mag. 2, 577-583 (1957).
- (b). H.M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955); W.G. Kannaluk, Proc. Roy. Soc. (London) A141, 159-168 (1933)
- (c). W.J. deHaas and J. deNobel, Physica 5, 449-463 (1938)

- Comments: (a) Chromium: 99.998% pure, recrystallized.
- (b) Molybdenum: 99.95% pure and 99.8% pure
- (c) Tungsten: Philips, single crystal

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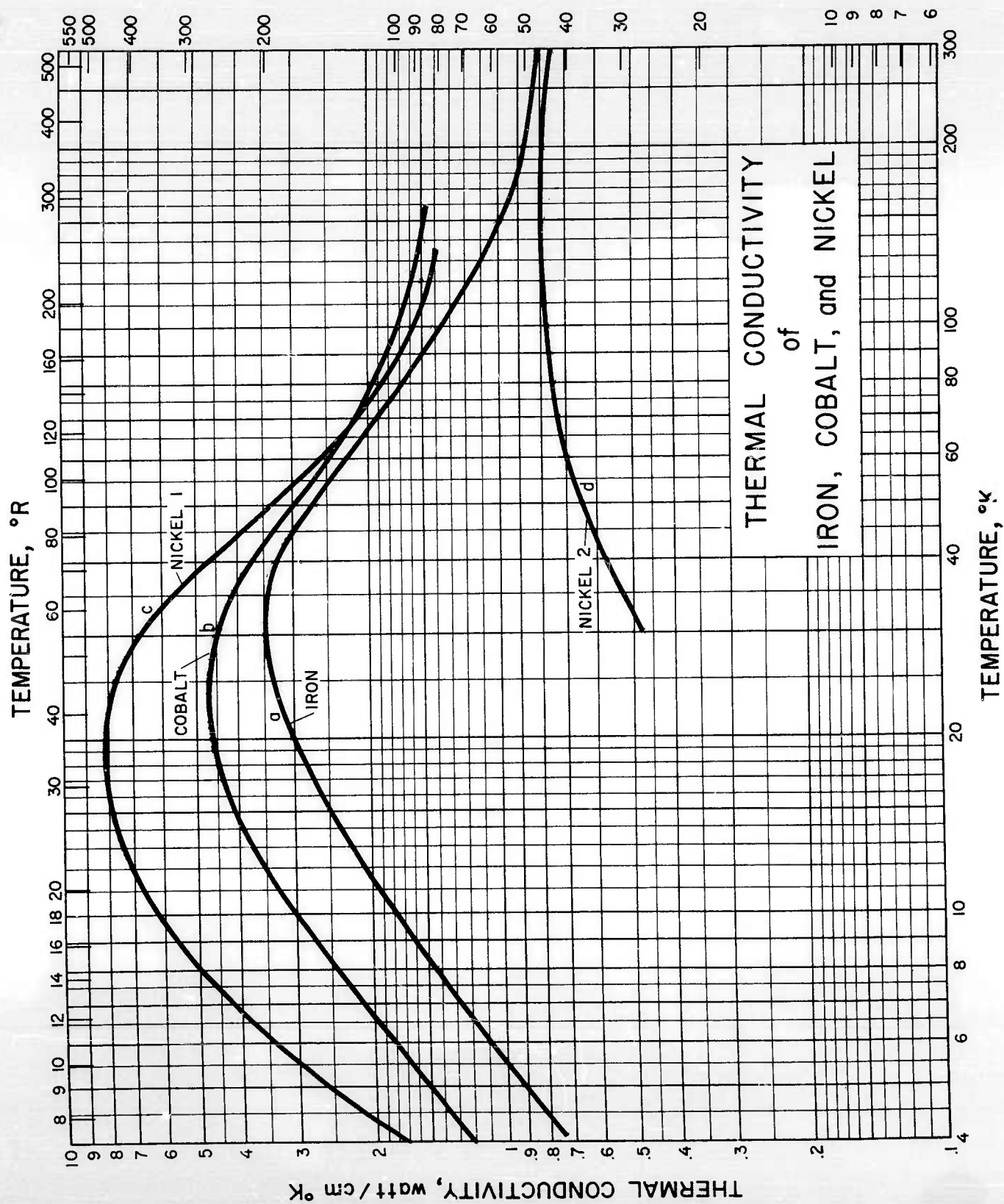
THERMAL CONDUCTIVITY of
MANGANESE and RHENIUM

Source of Data: (a) G. K. White and S. B. Woods, Can J. Physics
35, 346-348 (1957)
(b) G. K. White and S. B. Woods, Can J. Physics
35, 656-665 (1957)

Comments: (a) Manganese; 99.99% pure, α phase, annealed, (Johnson,
Matthey)
(b) Rhenium; 99.99% pure, zone melted.

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THERMAL CONDUCTIVITY, BTU/hr ft °R

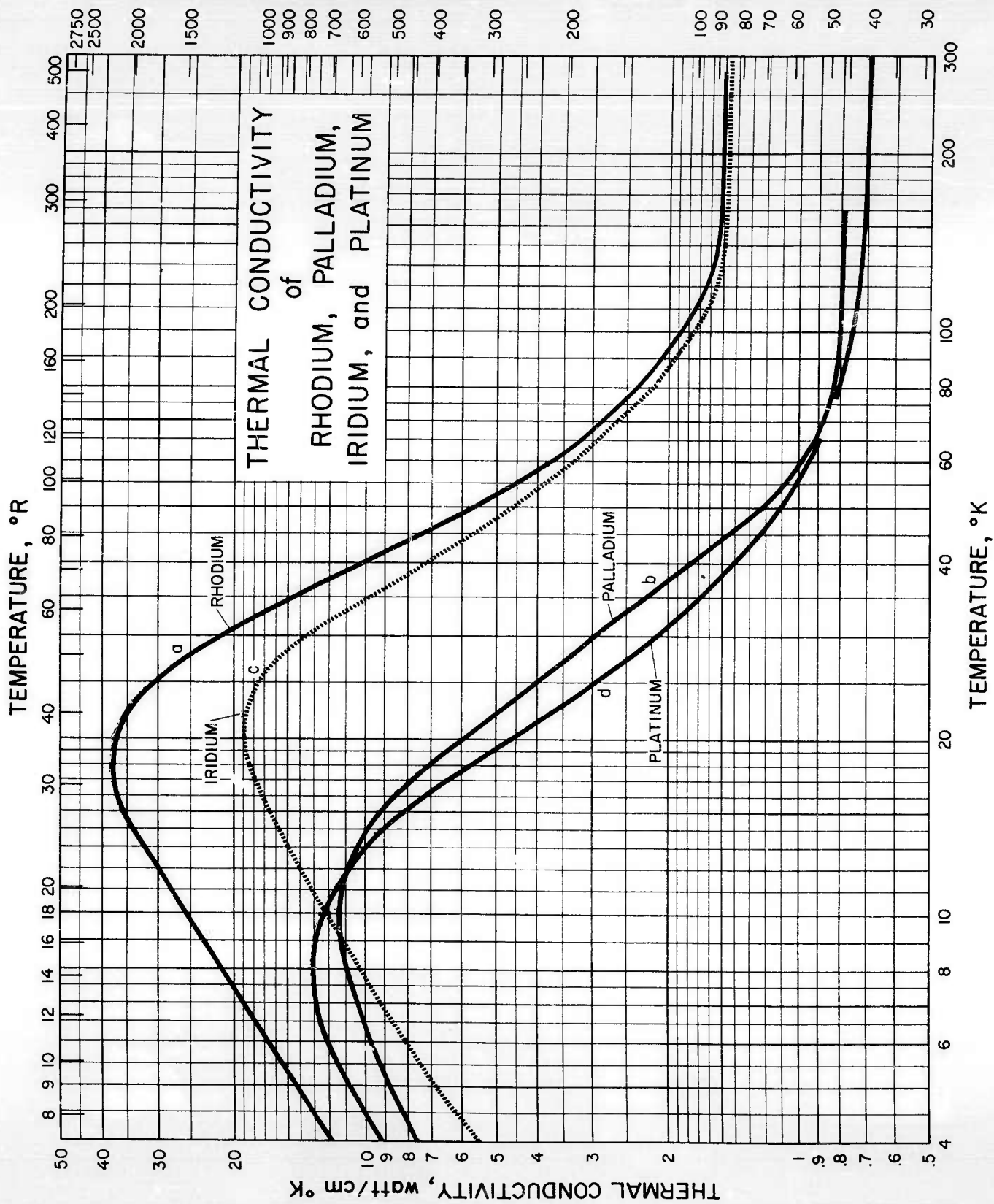


THERMAL CONDUCTIVITY of
IRON, COBALT, and NICKEL

- Source of Data:
- (a) H.M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955)
R.W. Powers, J.B. Ziegler and H.L. Johnston, TR 264-6, Cryogenics Laboratory, Ohio State University, 17 pp (1951)
 - (b) G.K. White and S.B. Woods, Can. J. Physics 35, 656-665 (1957)
 - (c) W.R.G. Kemp, P.G. Klemens, and G.K. White, Aust. J. Physics 9, 180-188 (1956)
 - (d) R.W. Powers, D. Schwartz and H.L. Johnston, TR 264-5, Cryogenic Laboratory, Ohio State University 11 pp (1951)
- Comments:
- (a) Iron; 99.99% pure, annealed, (Johnson, Matthey) and 99.99% pure, (Johnson, Matthey)
 - (b) Cobalt; 99.99% pure, annealed, Johnson, Matthey)
 - (c) Nickel-1; 99.99% pure, annealed, (Johnson, Matthey)
 - (d) Nickel-2; 99% pure (Int. Nickel)

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THERMAL CONDUCTIVITY, BTU / hr ft °R



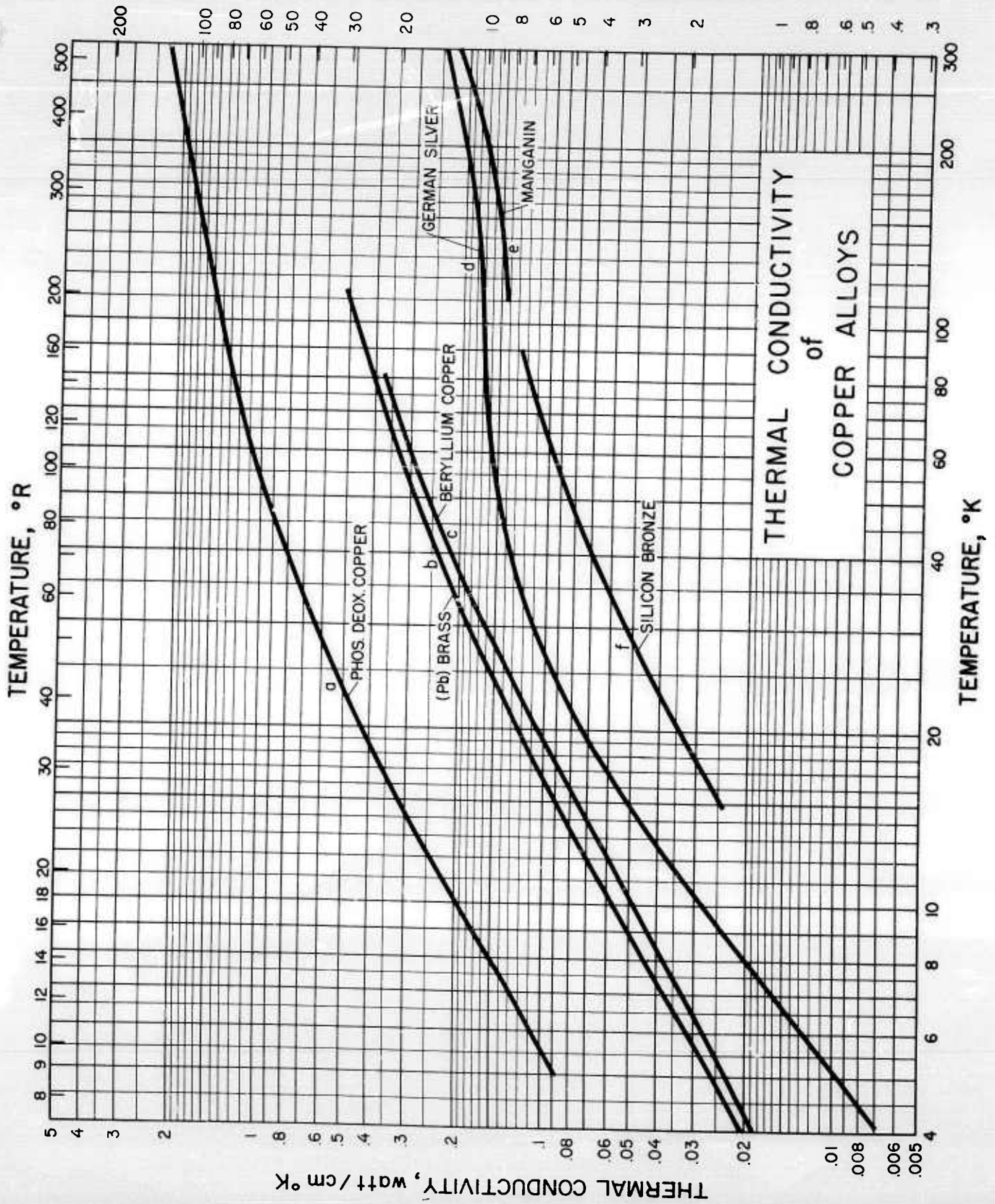
THERMAL CONDUCTIVITY OF RHODIUM,
PALLADIUM, IRIDIUM, AND PLATINUM

- Source of Data: (a) G.K. White and S.B. Woods, Can. J. Physics 35, 248-257 (1957); R.W. Powell and R.P. Tye, "Int. Conf. on Low Temp" Paris, Sept. 1955.
- (b) W.R.G. Kemp, P.G. Klemens, A.K. Sreedhar, and G.K. White, Phil. Mag. 46, 811-814 (1955).
- (c) H.M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955); R.W. Powell and R.P. Tye, "Int. Conf. on Low Temp" Paris, Sept. 1955.
- (d) H.M. Rosenberg, Phil. Trans. Roy. Soc. (London) A247, 441-497 (1955); W. Meissner, Ann. Physik 47, 1001-1058 (1915).

- Comments: (a) Rhodium; 99.99% pure, annealed, (Johnson, Matthey) and 99.9% pure, annealed, (Johnson, Matthey)
- (b) Palladium; 99.99% pure, annealed, (Johnson, Matthey)
- (c) Iridium; 99.995% pure, annealed, (Johnson, Matthey) and 99.9% pure, annealed, (Johnson, Matthey)
- (d) Platinum; 99.999% pure, annealed, (Johnson, Matthey), and "very pure", annealed (Heraeus).

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THERMAL CONDUCTIVITY, BTU/hr ft °R



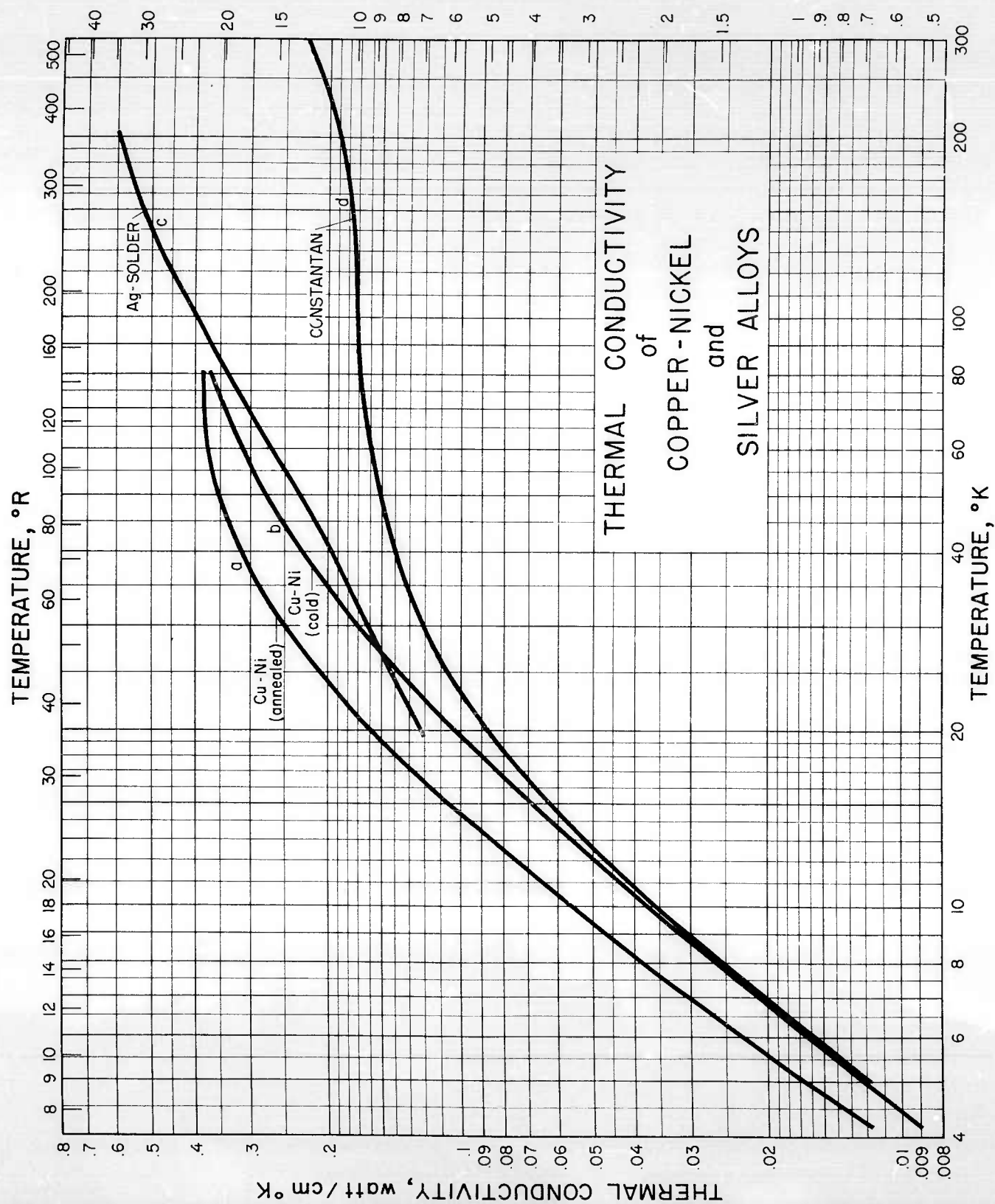
THERMAL CONDUCTIVITY
of COPPER ALLOYS

- Source of Data: (a) R. L. Powell, H. M. Roder, and W. M. Rogers,
J. Appl. Phys. 28, 1282-1288 (1957).
(b) Same as (a)
(c) R. Berman, E. L. Foster, H. M. Rosenberg,
Brit. J. Appl. Physics 6, 181-182 (1955).
(d) R. Berman, Phil. Mag. 42, 642-650 (1951);
C. H. Lees, Phil. Trans. Roy. Soc.
(London) A208, 381-443 (1908).
(e) C. H. Lees, Phil. Trans. Roy. Soc. (London)
A208, 381-443 (1908).
(f) Same as (a)

- Comments: (a) Phos. Deox. Copper; 0.027% P, 99% Cu,
Commercial hard temper.
(b) (Pb) Brass; 35.7% Zn, 3.27% Pb, 1% Sn, 60% Cu,
hard temper.
(c) Beryllium Copper; 2% Be, 98% Cu, held at 300 °C
for two hours.
(d) German Silver; 47% Cu, 41% Zn, 9% Ni, 2% Pb.;
~~and 62% Cu, 22% Zn, 15% Ni.~~
(e) Manganin; 84% Cu, 12% Mn, 4% Ni.
(f) Silicon Bronze; 3.15% Si, 1.13% Mn, 1% Zn,
94% Cu, hard temper.

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THERMAL CONDUCTIVITY, BTU/hr ft °R

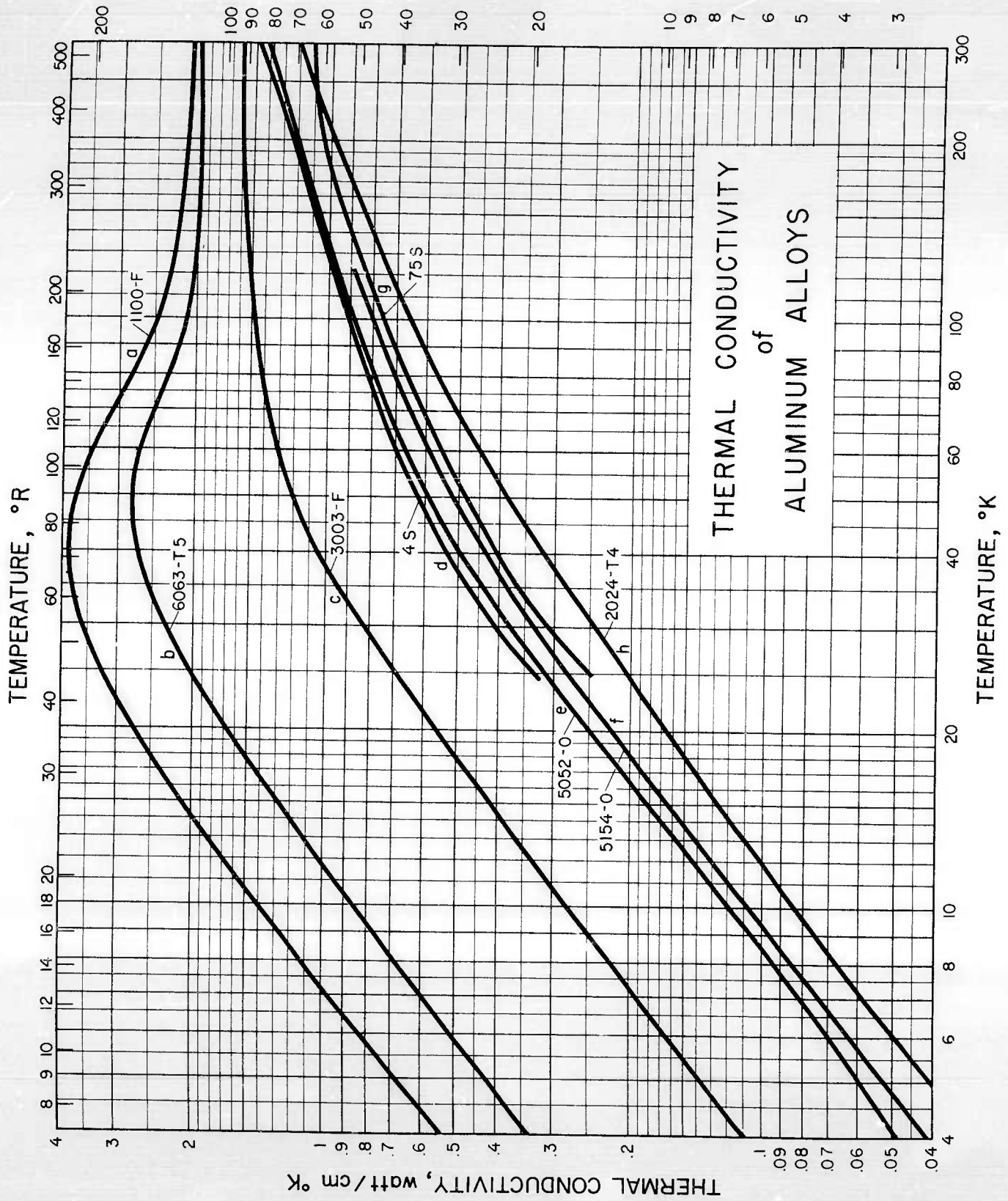


THERMAL CONDUCTIVITY of COPPER-NICKEL
and SILVER ALLOYS

- Source of Data:
- (a) I. Estermann and J. E. Zimmerman,
J. Appl. Phys. 23, 578-588 (1952)
 - (b) Same as (a).
 - (c) R. L. Powell, Unpublished (1953)
 - (d) R. Berman, Phil. Mag. 42, 642-650 (1951);
R. W. Powers, J. B. Zeigler and H. L
Johnston, TR 264-8, Ohio State Univ. (1951)
- Comments:
- (a) Cu-Ni (annealed); 90% Cu, 10% Ni; annealed
 - (b) Cu-Ni (cold); 90% Cu, 10% Ni; cold-worked
 - (c) Ag-Solder; 50% Ag, 15.5% Cu, 16.5% Zn, 18% Cd
 - (d) Constantan; 60% Cu, 40% Ni; and 55% Cu, 45% Ni.

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THERMAL CONDUCTIVITY, BTU/hr ft °R



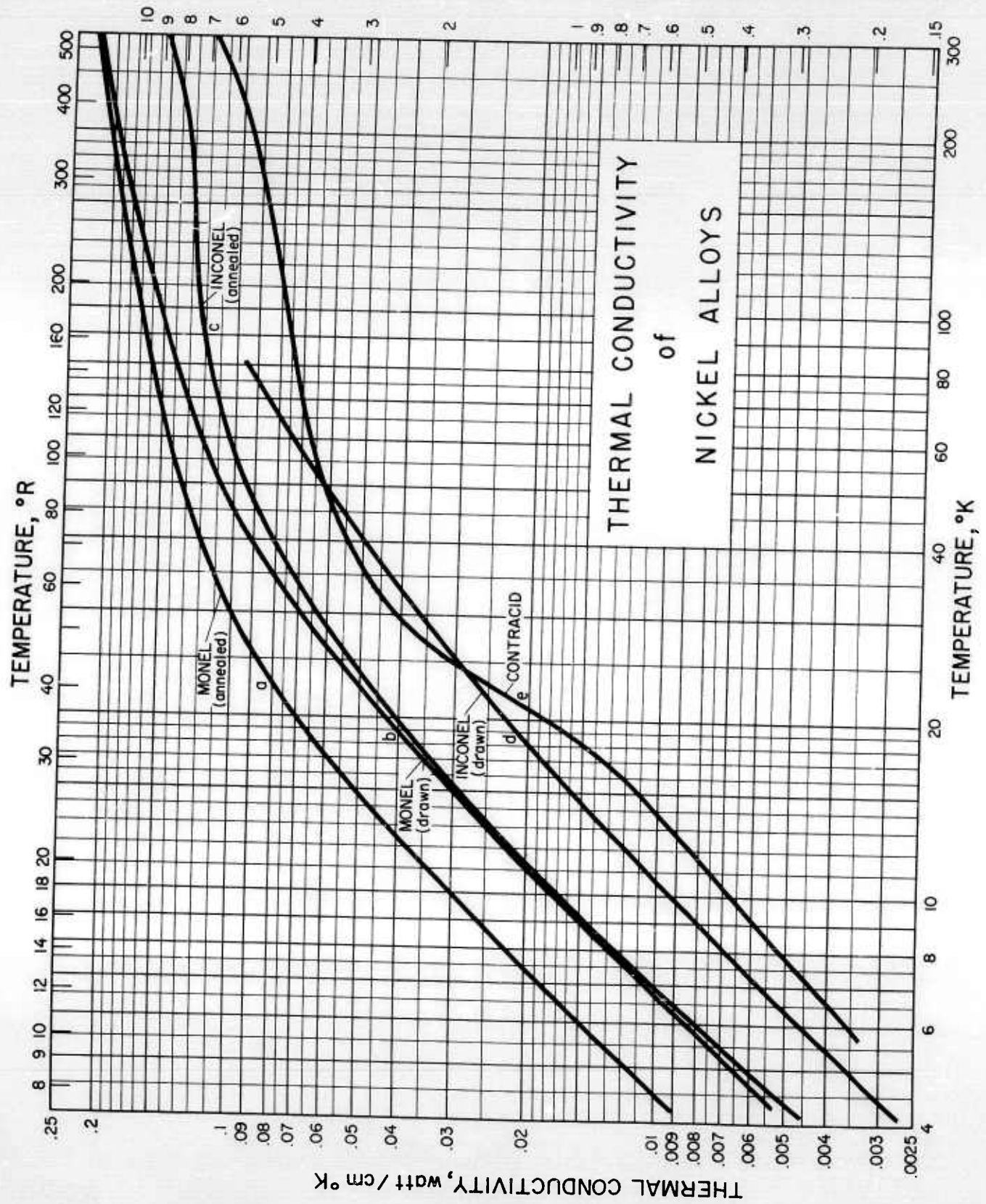
THERMAL CONDUCTIVITY
of ALUMINUM ALLOYS

- Source of Data: (a) R. L. Powell, W. J. Hall, and H. M. Roder,
to be published (1958)
- (b) Same as (a)
- (c) Same as (a)
- (d) R. W. Powers, J. B. Ziegler, and
H. L. Johnston, TR 264-7, Cryogenics
Laboratory, Ohio State University 10 pp. (1951)
- (e) Same as (a)
- (f) Same as (a)
- (g) Same as (d)
- (h) Same as (a)

- Comments: (a) 1100-F; Alcoa, 99% Al, as fabricated.
- (b) 6063-T5; Alcoa, 0.4% Si, 0.7% Mg, 98.5% Al, as
fabricated.
- (c) 3003-F; Alcoa, 1.2% Mn, 98.5% Al, as fabricated.
- (d) 4-S; 0.16% Cu, 1.02% Mg, 1.20% Mn, 0.52% Fe,
0.13% Si, 0.02% Cr, 0.02% Ti.
- (e) 5052-0; 0.25% Cr, 2.5% Mg, 97% Al, annealed.
- (f) 5154-0; 0.25% Cr, 3.5% Mg, 96% Al, annealed.
- (g) 75-S; 1.5% Cu, 5.5% Zn, 2.5% Mg, 0.2% Mn,
0.3% Cr.
- (h) 2024-T4; 0.6% Mn, 1.5% Mg, 4.5% Cu, 93% Al,
solution heat treated.

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THERMAL CONDUCTIVITY, BTU/hr ft °R



THERMAL CONDUCTIVITY
of NICKEL ALLOYS

- Source of Data: (a) I. Estermann and J.E. Zimmerman,
J. Appl. Phys. 23, 578-588 (1952);
R.W. Powers, J.B. Ziegler, and
H.L. Johnston, TR 264-8, Cryogenics
Laboratory, Ohio State University
(1951) 11 pp.
- (b) Same as (a).
- (c) Same as (a).
- (d) I. Estermann and J.E. Zimmerman,
J. Appl. Phys. 23, 578-588 (1952).
- (e) J. Karweil and K. Schafer, Ann.
Physik 36, 567-577 (1939); R.W.
Powers, J.B. Ziegler, and H.L.
Johnston, TR 264-8, Cryogenics
Laboratory, Ohio State University
(1951) 11 pp.

- Comments: (a) Monel; annealed; and 67%Ni, 30% Cu, 1.4%
Fe, 1.0%Mn, 0.15% C, 0.1% Si, 0.01% S,
hot-rolled
- (b) Monel; Hard-drawn; and 67% Ni, 30% Cu, 1.4%
Fe, 1.0% Mn, 0.15% C, 0.1% Si, 0.01% S,
Cold-rolled
- (c) Inconel; Annealed; and 80% Ni, 14% Cr, 6% Fe.
- (d) Inconel; Hard-drawn
- (e) Contracid; 60% Ni, 15% Cr, 16% Fe, 7% Mo;
and 60.05% Ni, 14.74% Cr, 15.82% Fe,
7.2% Mo, 2.14% Mn, 0.05% C.

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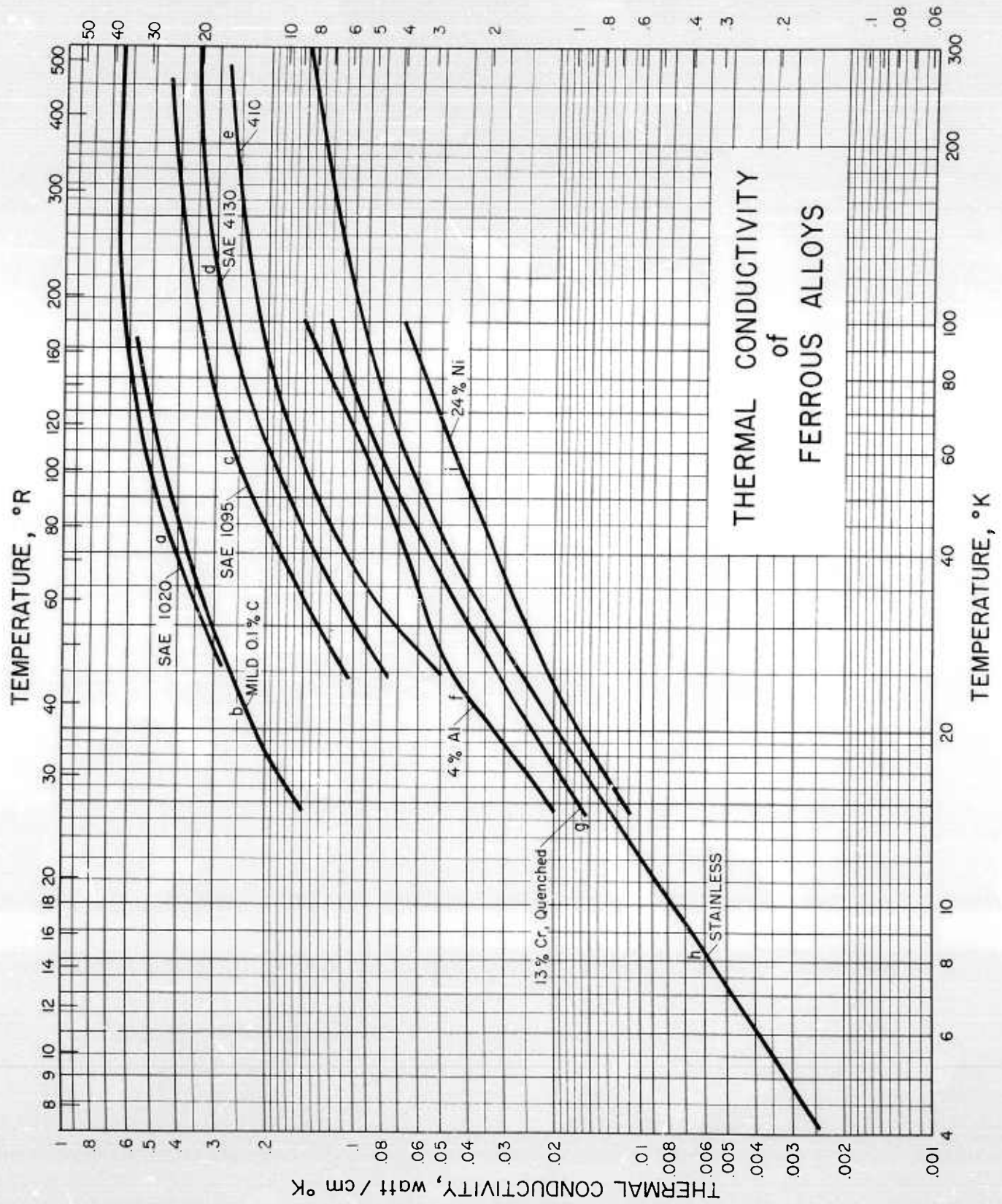
THERMAL CONDUCTIVITY of
MISCELLANEOUS ALLOYS

- Source of Data: (a) R. Berman, E. L. Foster, and H. M. Rosenberg
Brit. J. Appl. Physics 6, 181-182 (1955)
(b) H. Bremmer and W. J. deHaas,
Physica 3, 692-704 (1936).
(c) Same as (a)
(d) Same as (b)
(e) Same as (b)
(f) W. W. Tyler and A. C. Wilson
Knolls Atomic Power Laboratory Report 803,
41 pp. (1952)

- Comments: (a) Soft Solder; 60% Sn, 40% Pb
(b) Lead - 44% Tin; 56% Pb, 44% Sn
(c) Wood's Metal; 48% Pb, 13% Sn, 13% Cd
(d) Rose's Metal; 50% Bi, 25% Pb, 25% Sn
(e) Lead - 50% Indium; 50% In, 50% Pb
(f) Titanium; Rem - Cru, RC130-B, 4.7% Mn, 3.99% Al,
0.14% C.

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THERMAL CONDUCTIVITY, BTU / hr ft °R



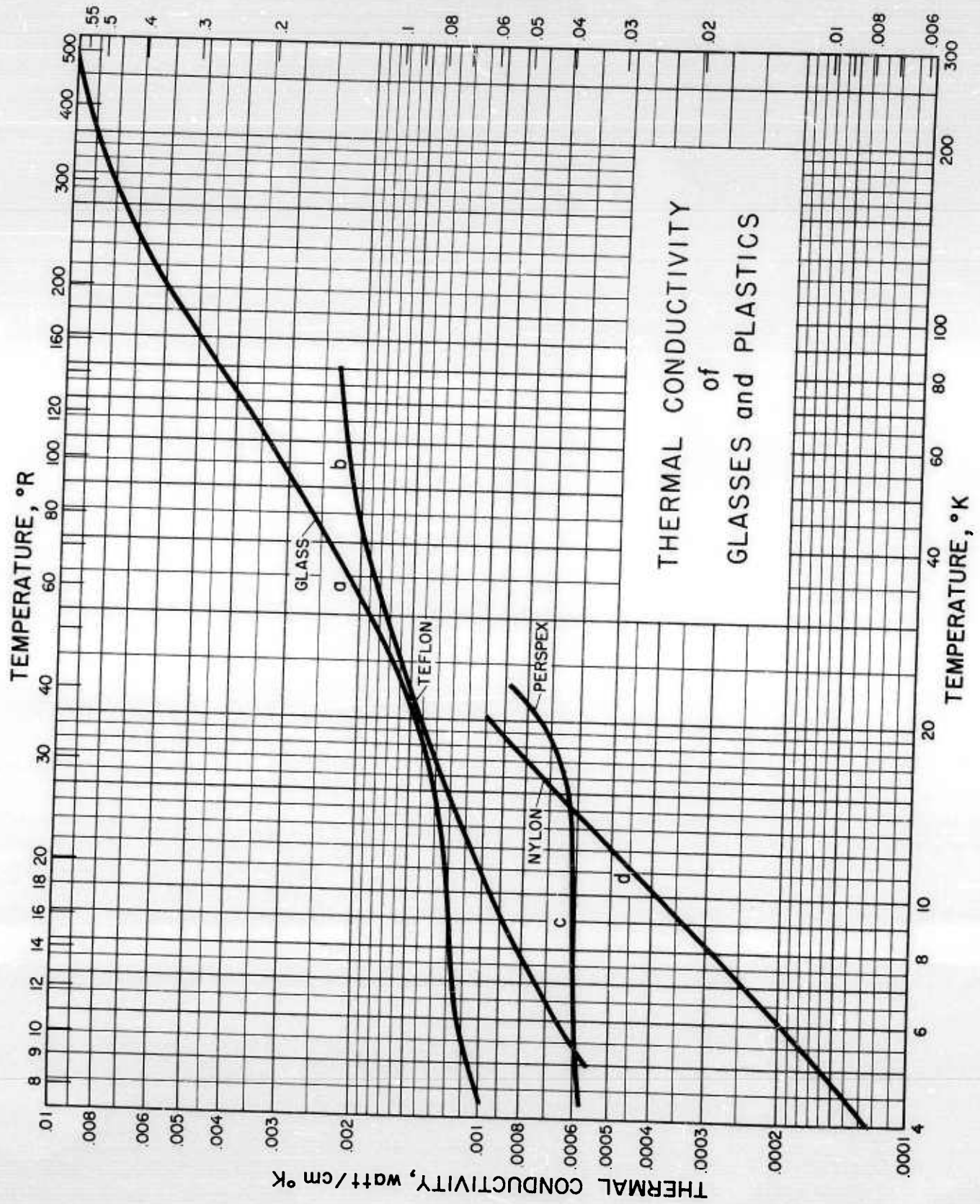
THERMAL CONDUCTIVITY
of FERROUS ALLOYS

- Source of Data: (a) R. W. Powers, J. B. Ziegler, and
H. L. Johnston, TR 264-6, Cryogenic
Laboratory, Ohio State University 17, (1951)
(b) J. deNobel, Physica 17, 551-562 (1951)
(c) Same as (a)
(d) Same as (a)
(e) Same as (a)
(f) Same as (b)
(g) Same as (b)
(h) R. L. Powell, and W. A. Blanpied,
NBS Circular 556, 68 pp. (1954)
(i) Same as (b)

- Comments: (a) SAE 1020; 0.33% Mn, 0.18% C, 0.014% Si.
(b) Mild 0.1% C; 0.14% C, 0.08% Si, 0.07% Mn;
heated to 800°C and furnace cooled.
(c) SAE 1095; 0.93% C, 0.34% Mn, 0.26% Si, 0.1% Ni,
Cr, 0.05% Mo.
(d) SAE 4130; 0.99% Cr, 0.52% Mn, 0.33% C, 0.2% Si,
Ni, and Mo.
(e) 410; 12.6% Cr, 0.36% Si, 0.32% Mn, 0.12% Ni,
0.09% C, 0.06% Cu, 0.03% N, 0.01% P.
(f) 4% Al; 4.11% Al, 0.13% Si, 0.08% Mn, 0.03% C,
0.01% Si, heated to 800°C and furnace cooled.
(g) 13% Cr; 13.5% Cr, 0.36% C, 0.22% Si, 0.13% Mn,
heated to 950°C, oil quenched, reheated to 450°C,
air-cooled.
(h) Stainless; average value for close curves of
types 303, 304, 316, 347, and "stainless" as
compiled in NBS Circular 556.
(i) 24% Ni; 24.30% Ni, 6.05% Mn, 1.18% C, heated
to 1050°C and water-quenched.

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THERMAL CONDUCTIVITY, BTU / hr ft °R



THERMAL CONDUCTIVITY OF
GLASSES and PLASTICS

- Source of Data: (a) R. L. Powell and W. A. Blanpied,
NBS Circular 556, 68 (1954)
(b) R. L. Powell, W. M. Rogers, and D. O. Coffin
J. Research NBS, 59, 349-355 (1957)
(c) R. Berman, E. L. Foster and H. M. Rosenberg
Brit. J. Appl. Physics 6, 181-182 (1955)
(d) R. Berman
Proc. Roy. Soc. (London) A208, 90-108 (1951)

- Comments: (a) Glass; average value of quartz, Pyrex, and boro-
silicate glasses.
(b) Teflon; extruded
(c) Nylon; Imperial Chem. Ind.; drawn monofilament.
(d) Perspex; An English organic glass thermo-plastic
similar to Lucite or Flexiglass.

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SPECIFIC HEAT and ENTHALPY of CRYOGENIC SOLIDS

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(continued)

SPECIFIC HEAT and ENTHALPY of CRYOGENIC SOLIDS (cont.)

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SPECIFIC HEAT, ENTHALPY of SODIUM

Sources of Data:

Eastman, E. D. and Rodebush, W. H., J. Am. Chem. Soc. 40, 489 (1918)

Roberts, L. M., Proc. Phys. Soc. (London) B70, 744 (1957)

Simon, F. and Zeidler, W., Z. physik. Chem. 123, 383 (1926)

Other References:

Dauphinee, T. M., Mac Donald, D. K. C. and Preston-Thomas, H., Proc. Roy. Soc. (London) A221, 267-276 (1954)

Griffiths, E. G. and Griffiths, E., Phil. Trans. Roy. Soc. London A214, 319 (1914); Proc. Roy. Soc. (London) A90, 557 (1914)

Gunther, P., Ann. phys. (4) 63, 476 (1920)

Koref, F., Ann. phys. (4) 36, 49 (1911)

Martin, D. L., Phys. Rev. Letters 1, 4-5 (1958)

Parkinson, D. H. and Quarrington, J. E., Proc. Phys. Soc. (London) A68, 762 (1955)

Pickard, G. L. and Simon, F., Proc. Phys. Soc. (London) 61, 1 (1948)

Rayne, J. A., Phys. Rev. 95, 1428 (1954)

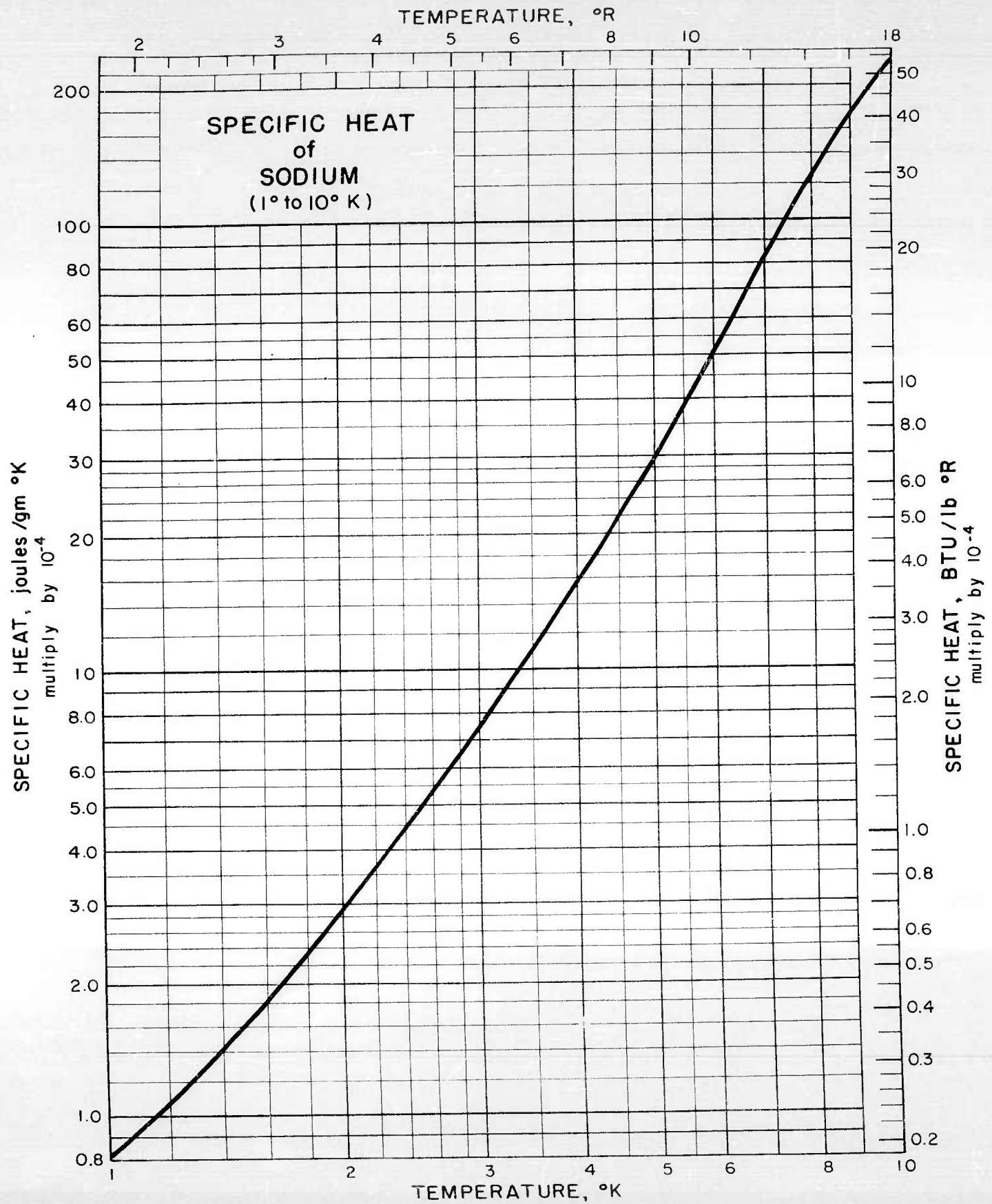
Comments:

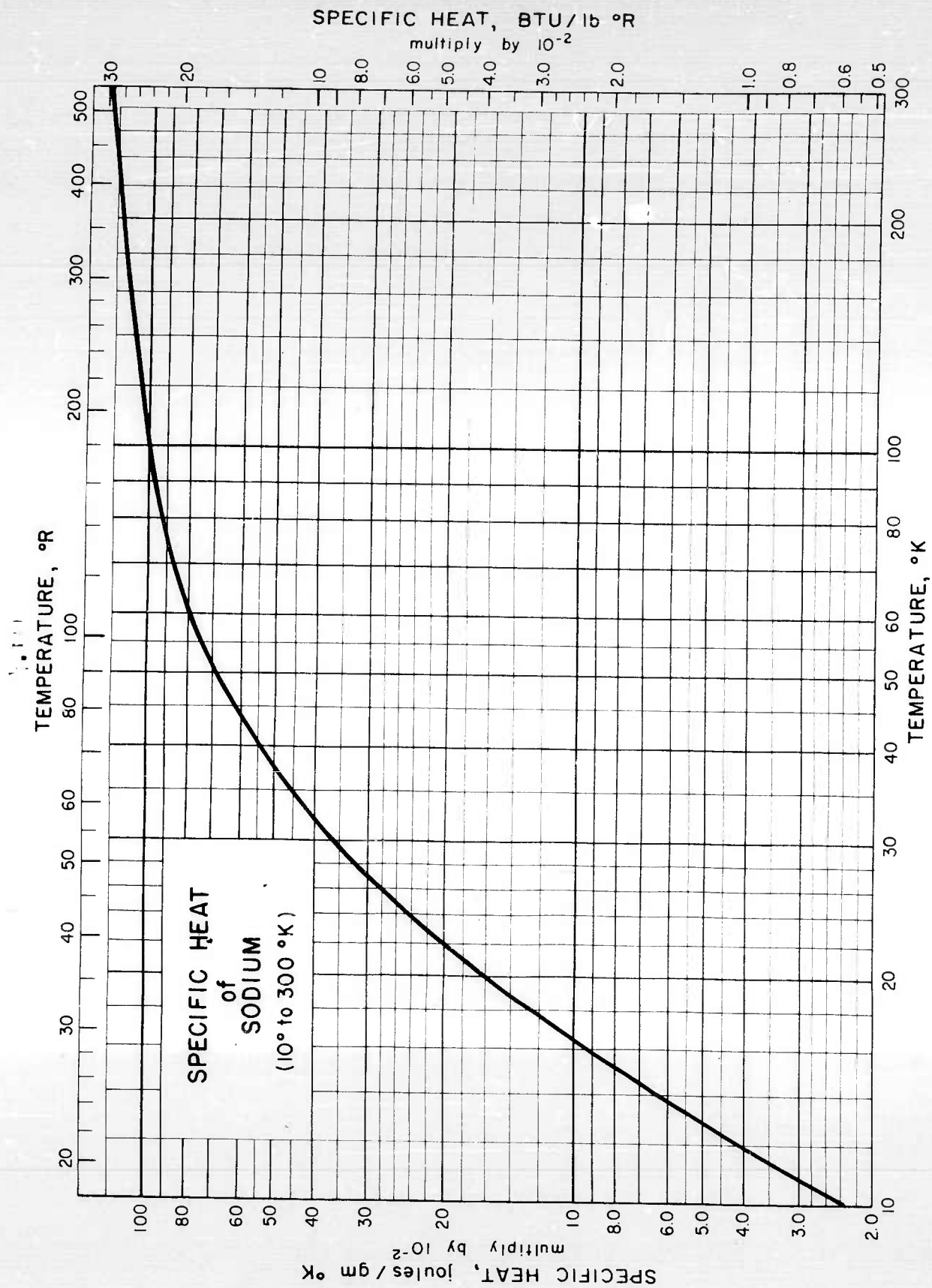
Barrett, C. S. (Acta Cryst 9, 671-7 [1956]), has shown that sodium on cooling below 36°K may transform to the extent of a few percent from the normal body centered cubic structure to a close-packed hexagonal structure. The transformation is of the martensite type and is prompted by cold work at low temperatures. The cph structure persisted to about 100°K on warming. Inasmuch as none of the calorimetric measurements on sodium were accompanied by crystallographic analysis, the tabulated data are to some degree ambiguous below 100°K.

Table of Selected Values

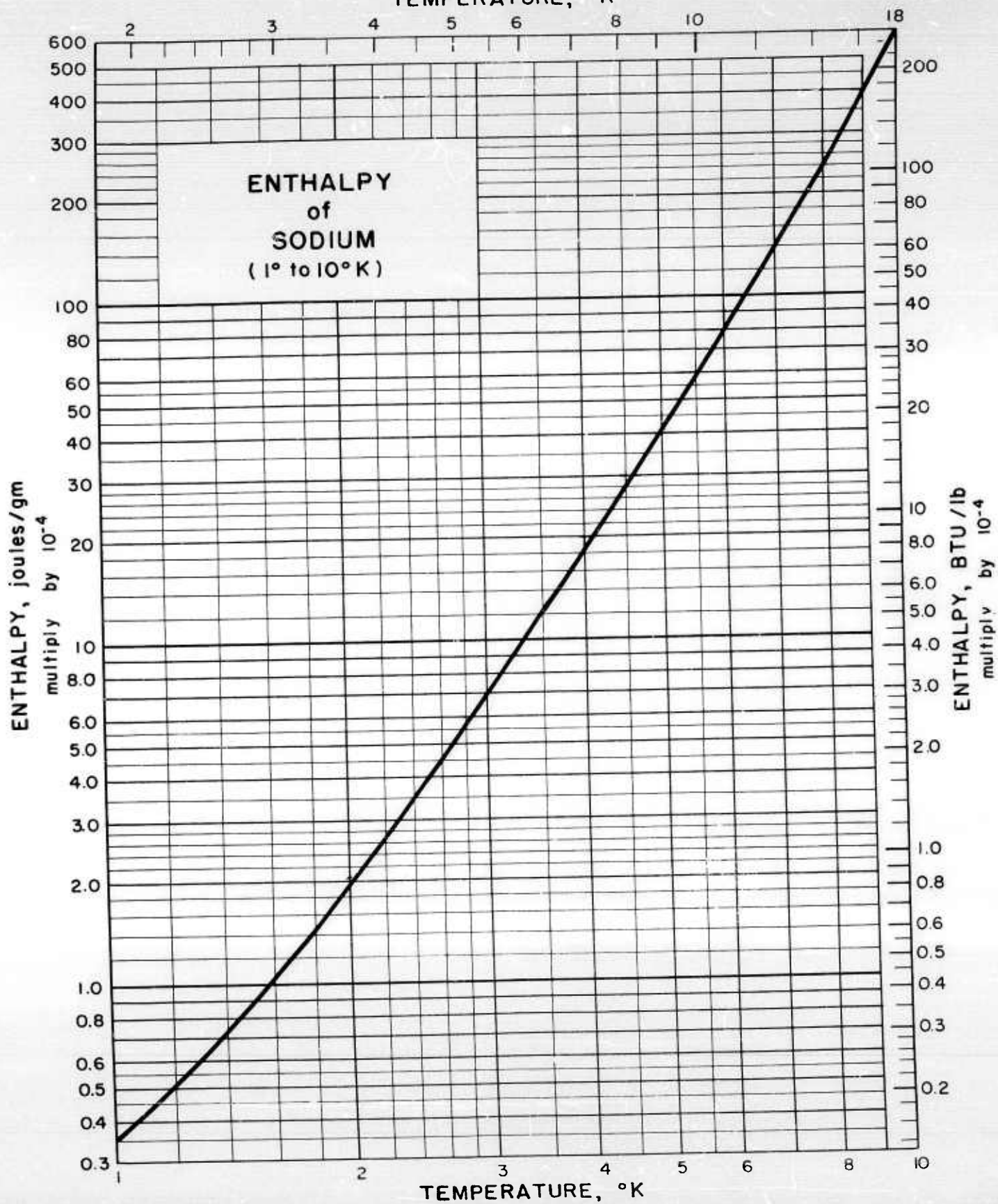
| Temp. °K | C _p j/gm°K | H j/gm | Temp. °K | C _p j/gm°K | H j/gm | Temp. °K | C _p j/gm°K | H j/gm |
|-------------|--------------------------|-----------|-------------|--------------------------|-----------|-------------|--------------------------|-----------|
| 1 | 0.000 081 | 0.000 035 | 18 | 0.124 | 0.597 | 120 | 1.03 | 78.0 |
| 2 | .000 289 | .000 204 | 20 | .155 | 0.875 | 140 | 1.06 | 98.9 |
| 3 | .000 76 | .000 70 | 25 | .259 | 1.90 | 160 | 1.09 | 120.5 |
| 4 | .001 60 | .001 84 | 30 | .364 | 3.45 | 180 | 1.12 | 142.6 |
| 5 | .002 98 | .004 08 | 40 | .544 | 8.03 | 200 | 1.14 | 165.2 |
| 6 | .005 1 | .008 1 | 50 | .695 | 14.2 | 220 | 1.16 | 188.2 |
| 8 | .012 2 | .024 7 | 60 | .793 | 21.7 | 240 | 1.18 | 211.6 |
| 10 | .023 8 | .060 2 | 70 | .86 | 30.0 | 260 | 1.20 | 235.4 |
| 12 | .039 7 | .123 | 80 | .91 | 38.9 | 280 | 1.22 | 259.6 |
| 14 | .063 | .225 | 90 | .95 | 48.2 | 300 | 1.24 | 284.2 |
| 16 | .093 | .380 | 100 | .98 | 57.9 | | | |

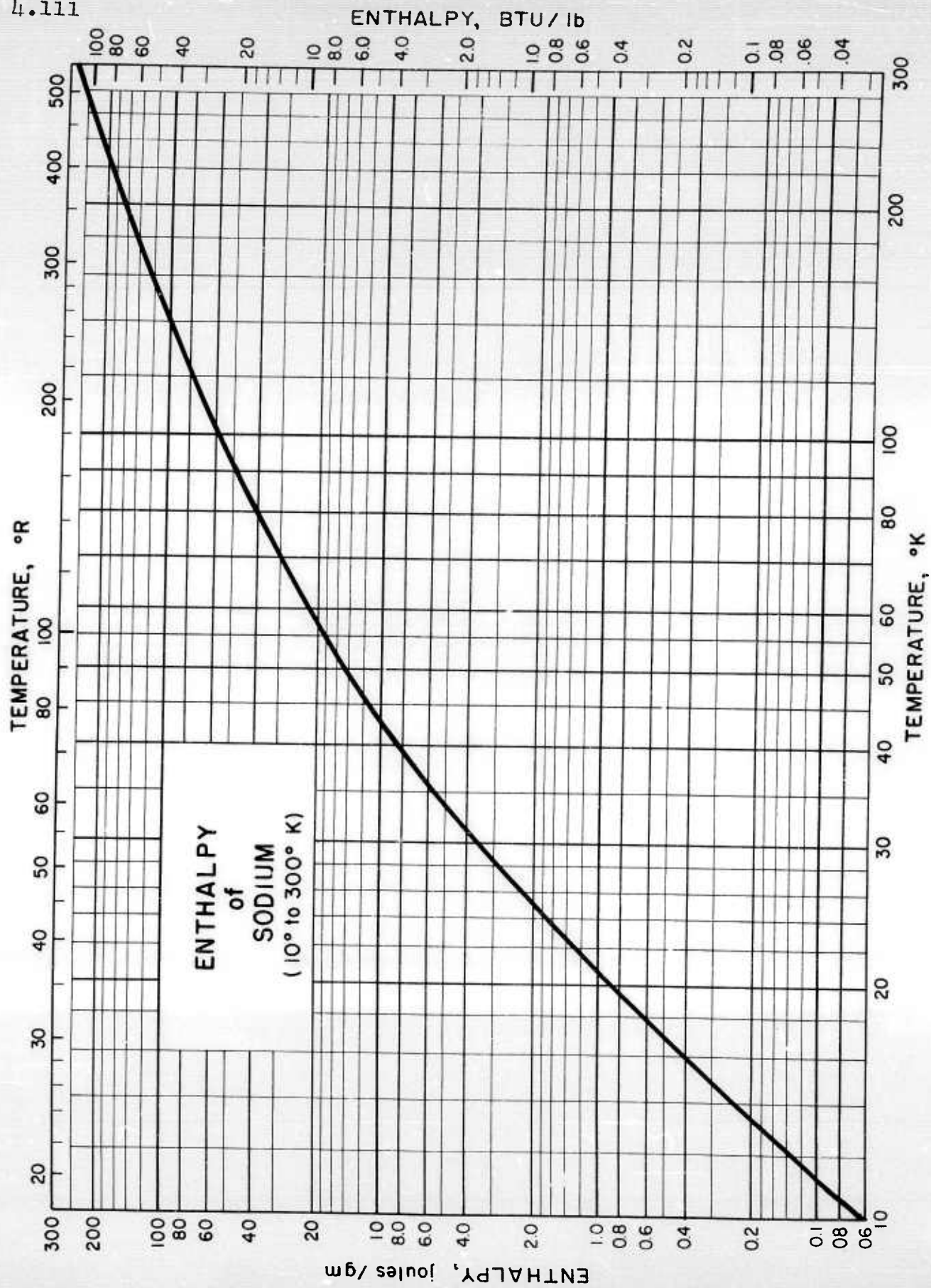
4.111





TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of COPPER
(1° to 10°K)

Sources of Data:

Corak, W. S., Garfunkel, M. P., Satterthwaite, C. B. and
Wexler, A., Phys. Rev. 98, 1699-1707 (1955)

Rayne, J. A., Australian J. Phys. 2, 189-97 (1956)

Other References:

Estermann, I., Friedberg, S. A., and Goldman, J. E., Phys. Rev.
87, 582 (1952)

Kok, J. A. and Keesom, W. H., Physica 3, 1035-45 (1936)

Phillips, N. E., Low Temperature Physics and Chemistry, Univ.
Wisconsin Press (1958) pp. 414-7

Comments:

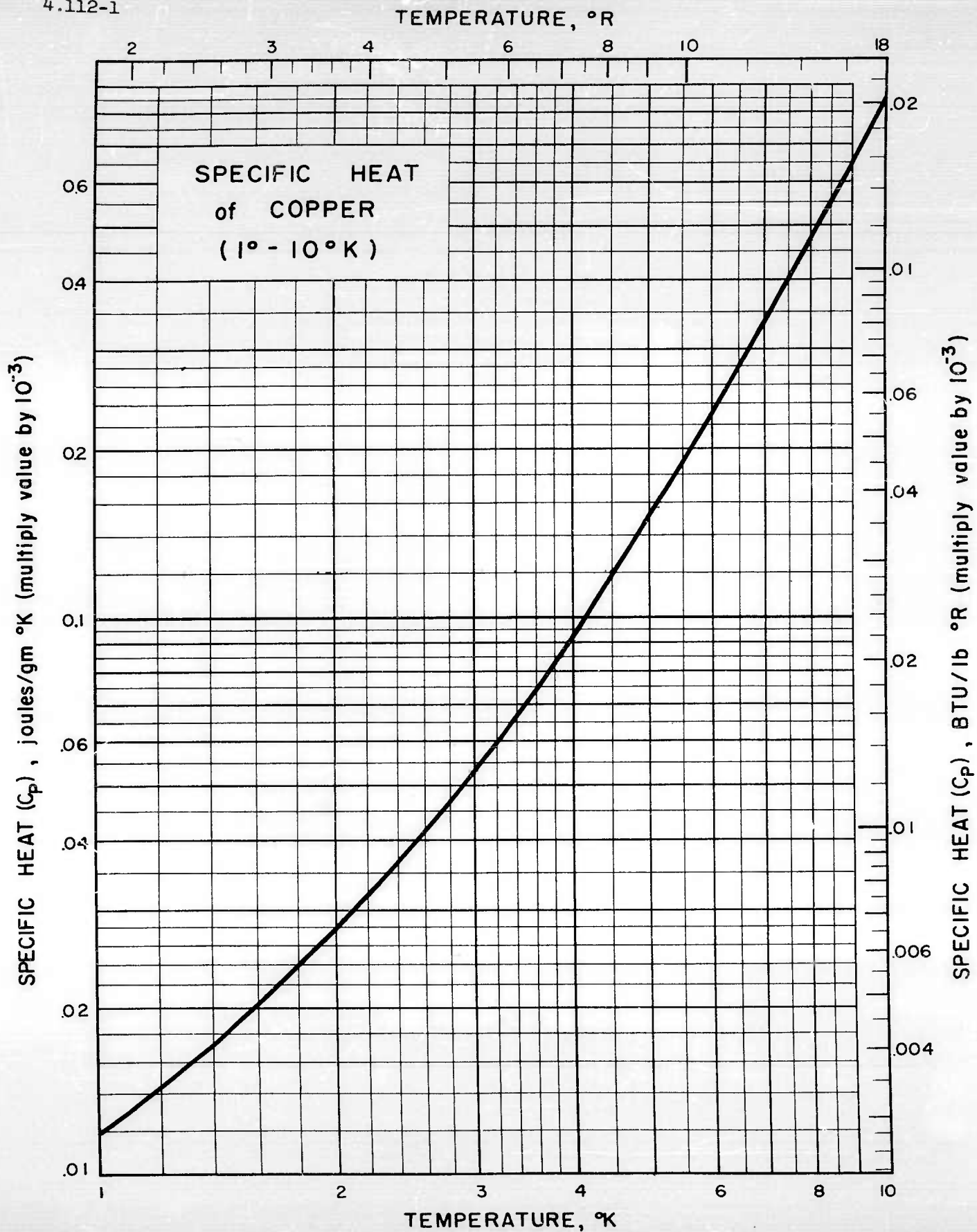
For the temperature range 0° to 10°K, the specific heat follows
the equation:

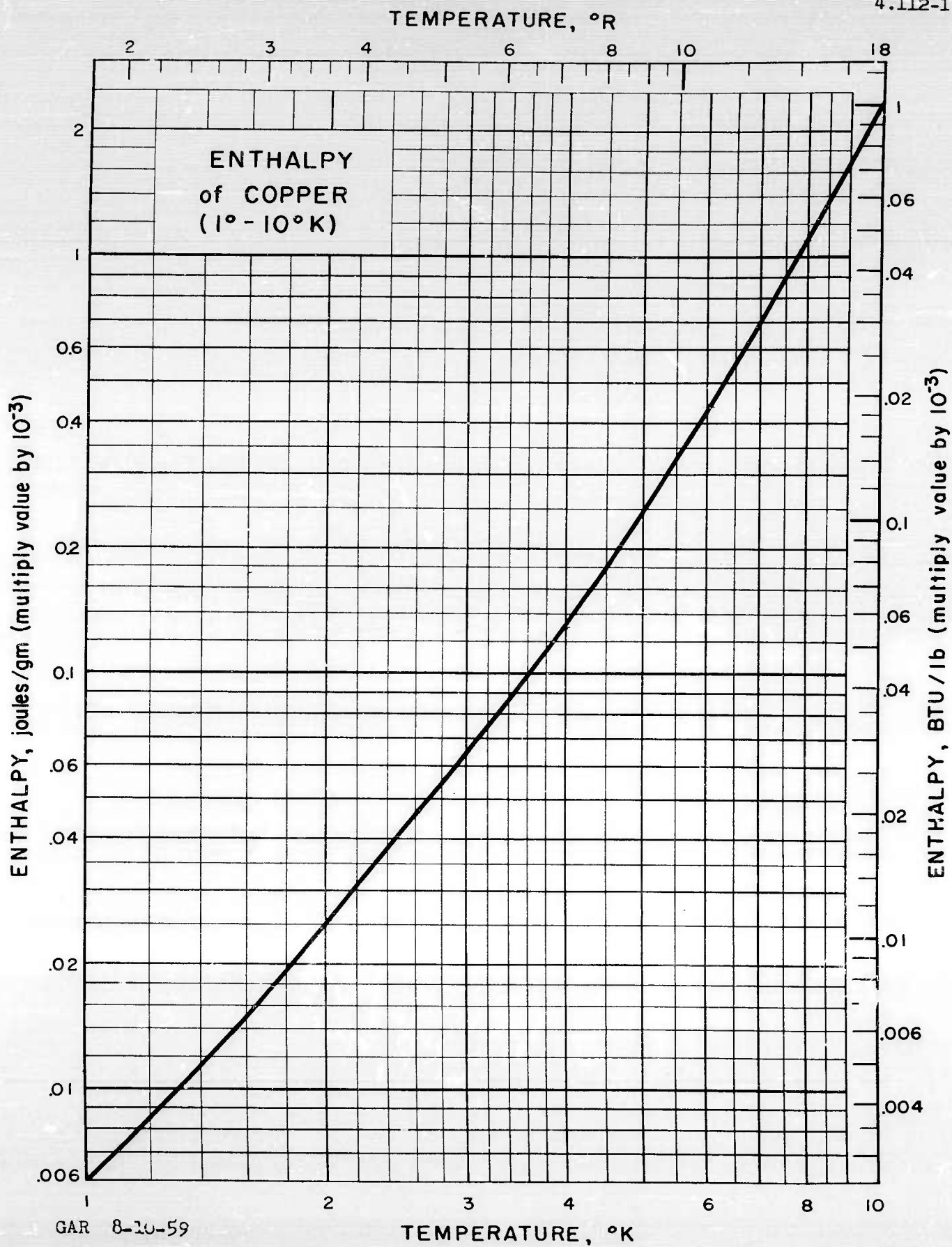
$$C_p = 10.8 \times 10^{-6} T + 30.6 \left[\frac{T}{344.5} \right]^3 \text{ j/gm-}^\circ\text{K}$$

Table of Selected Values

| Temp. °K | C _p j/gm-°K | H * j/gm |
|-------------|---------------------------|-------------|
| 1 | 0.000 012 | 0.000 006 |
| 2 | .000 028 | .000 025 |
| 3 | .000 053 | .000 064 |
| 4 | .000 091 | .000 13 |
| 6 | .000 23 | .000 44 |
| 8 | .000 47 | .001 12 |
| 10 | .000 86 | .002 4 |

$$* H = \int_0^T C_p dT$$





SPECIFIC HEAT, ENTHALPY of COPPER
(10° to 300°K)

Sources of Data:

Dockerty, S. M., Can. J. Research 15A, 59-66 (1937)

Other References:

Aoyama, S. and Kanda, E., J. Chem. Soc. Japan 62, 312-15 (1941)

Behn, U., Ann. Physik u. Chem. (3) 66, 237-44 (1898)

Bronson, H. L., Chisholm, H. M. and Dockerty, S. M., Can. J. Research 8, 282-303 (1933)

Eucken, A. and Werth, H., Z. anorg. allgem. Chem. 188, Schenck Festschrift, 152-72 (1930)

Giauque, W. F. and Meads, P. F., J. Am. Chem. Soc. 63, 1897-1901 (1941)

Keesom, W. H. and Onnes, H. K., Commun. Phys. Lab. Univ. Leiden No. 147a, 3 (1915)

Koref, F., Ann. Physik 36, 49-73 (1911)

Neimst, W., Sitzber. kgl. preuss. Akad. Wiss. 262 (1910)

Nernst, W., Sitzber, kgl. preuss. Akad. Wiss. 306 (1911)

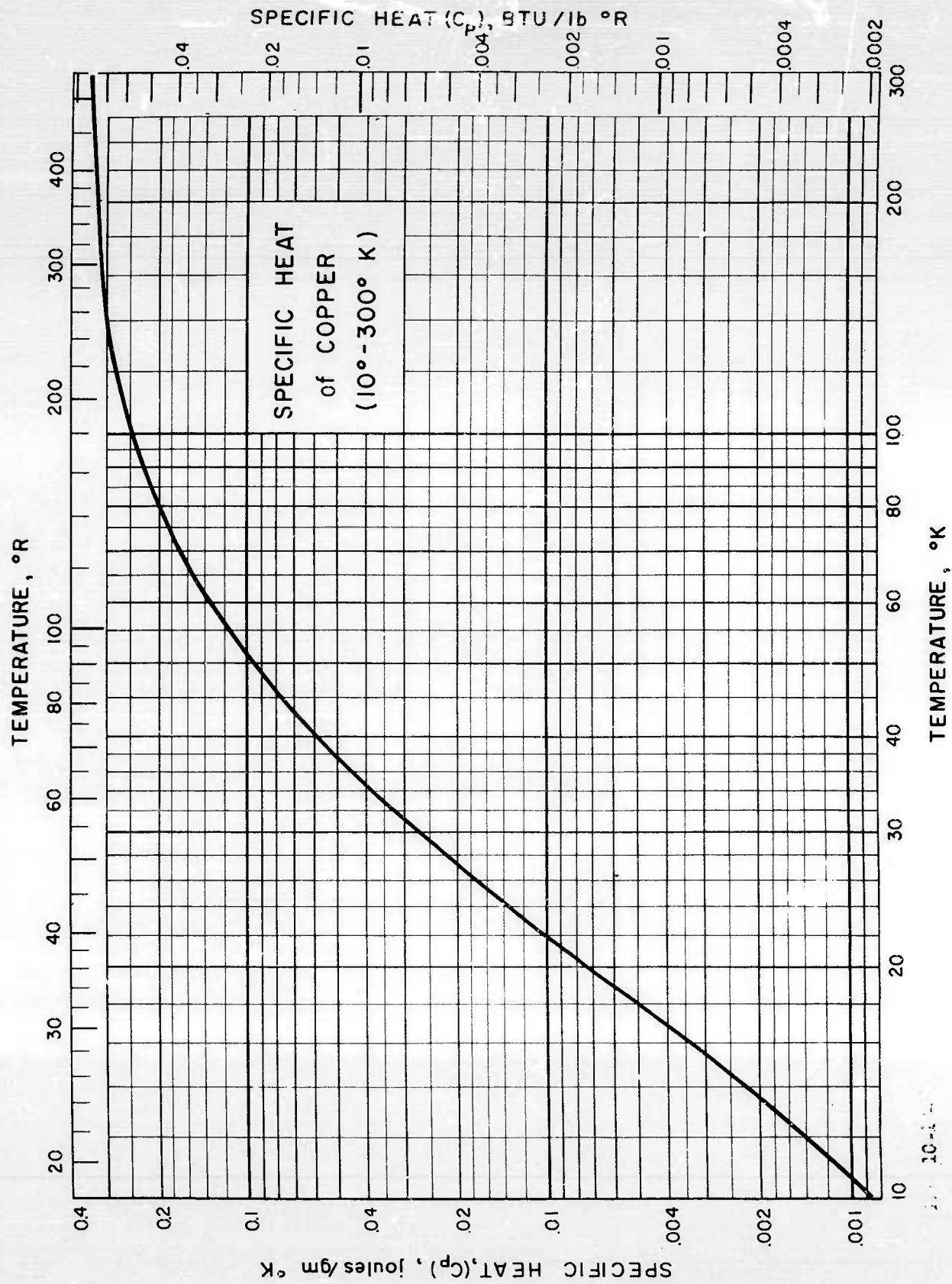
Nernst, W. and Lindemann, F. A., Z. Elektrochem. 17, 817 (1911)

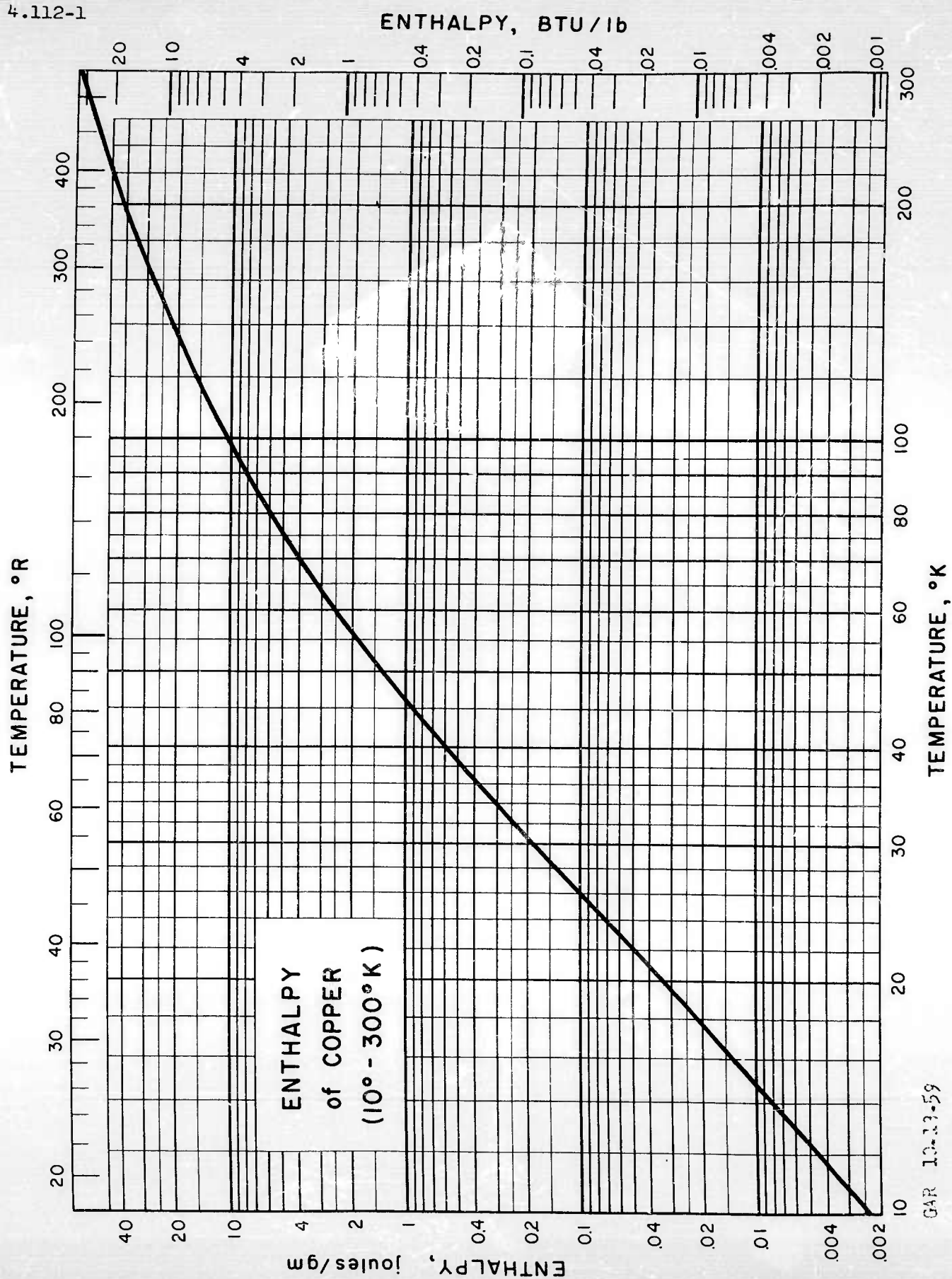
Schimpff, H., Z. physik. Chem. 71, 257 (1910)

Table of Selected Values

| Temp. °K | C _p j/gm-°K | H* j/gm | Temp. °K | C _p j/gm-°K | H* j/gm |
|-------------|---------------------------|------------|-------------|---------------------------|------------|
| 10 | 0.000 86 | 0.0024 | 100 | 0.254 | 10.6 |
| 15 | .002 7 | .0107 | 120 | .288 | 16.1 |
| 20 | .007 7 | .034 | 140 | .313 | 22.1 |
| 25 | .016 | .090 | 160 | .332 | 28.5 |
| 30 | .027 | .195 | 180 | .346 | 35.3 |
| 40 | .060 | .61 | 200 | .356 | 42.4 |
| 50 | .099 | 1.40 | 220 | .364 | 49.6 |
| 60 | .137 | 2.58 | 240 | .371 | 56.9 |
| 70 | .173 | 4.13 | 260 | .376 | 64.4 |
| 80 | .205 | 6.02 | 280 | .381 | 72.0 |
| 90 | .232 | 8.22 | 300 | .386 | 79.6 |

$$* H = \int_0^T C_p dT$$





SPECIFIC HEAT, ENTHALPY of GOLD

Sources of Data:

Corak, W. S., Garfunkel, M. P., Satterthwaite, C. B. and Wexler, A.,
Phys. Rev. 98, 1699 (1955)

Geballe, T. H. and Glauque, W. F., J. Am. Chem. Soc. 74, 2368-9 (1952)

Other References:

Clusius, K. and Harteck, P., Z. physik. Chem. 134, 243 (1928)

Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)

Comments:

For $0 < T \leq 15^\circ\text{K}$, the values for specific heat in the table of selected values below are given by the equation:

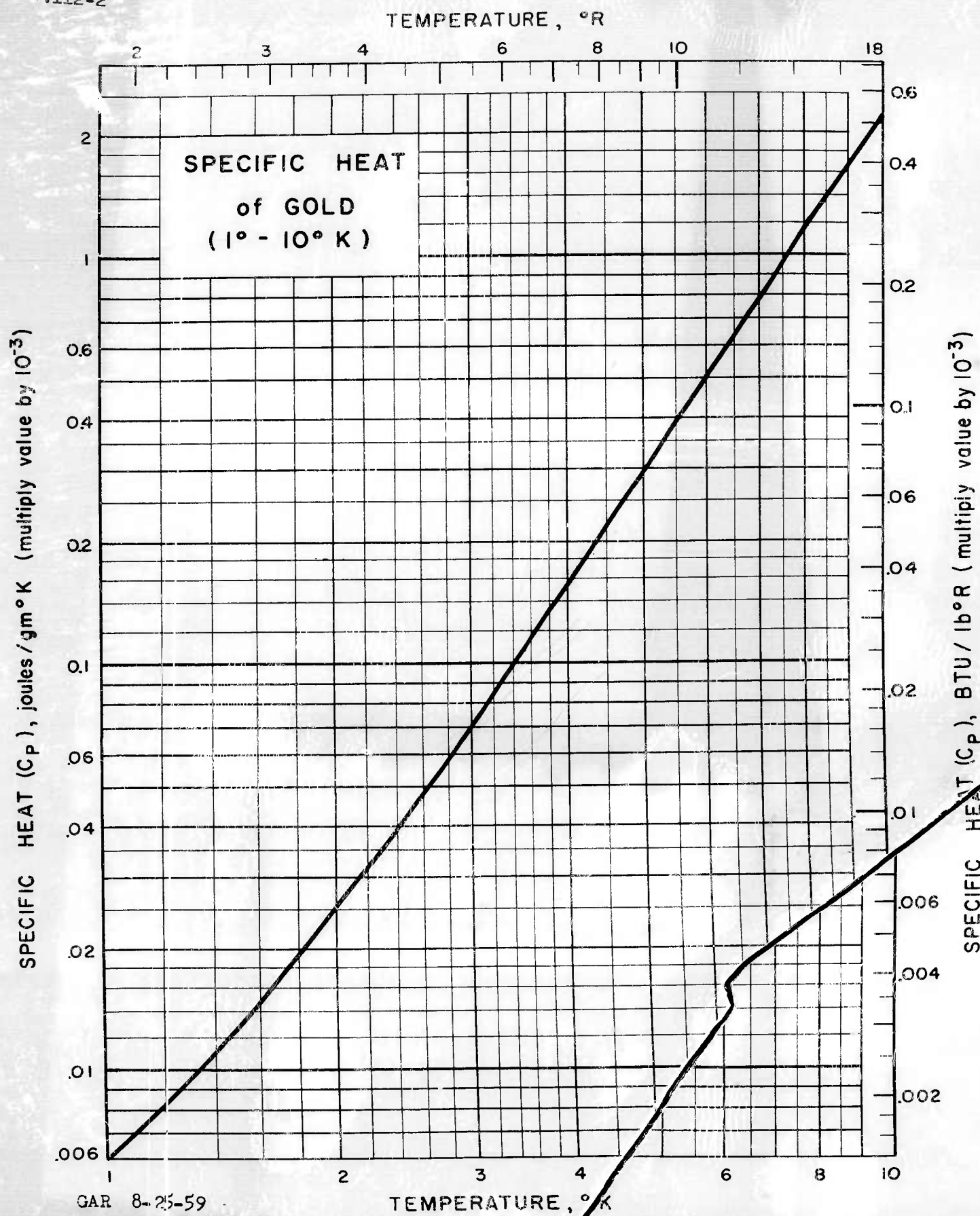
$$C_p = 9.86 (T/165)^3 + 3.75 \times 10^{-6} T \text{ j/gm-}^\circ\text{K}$$

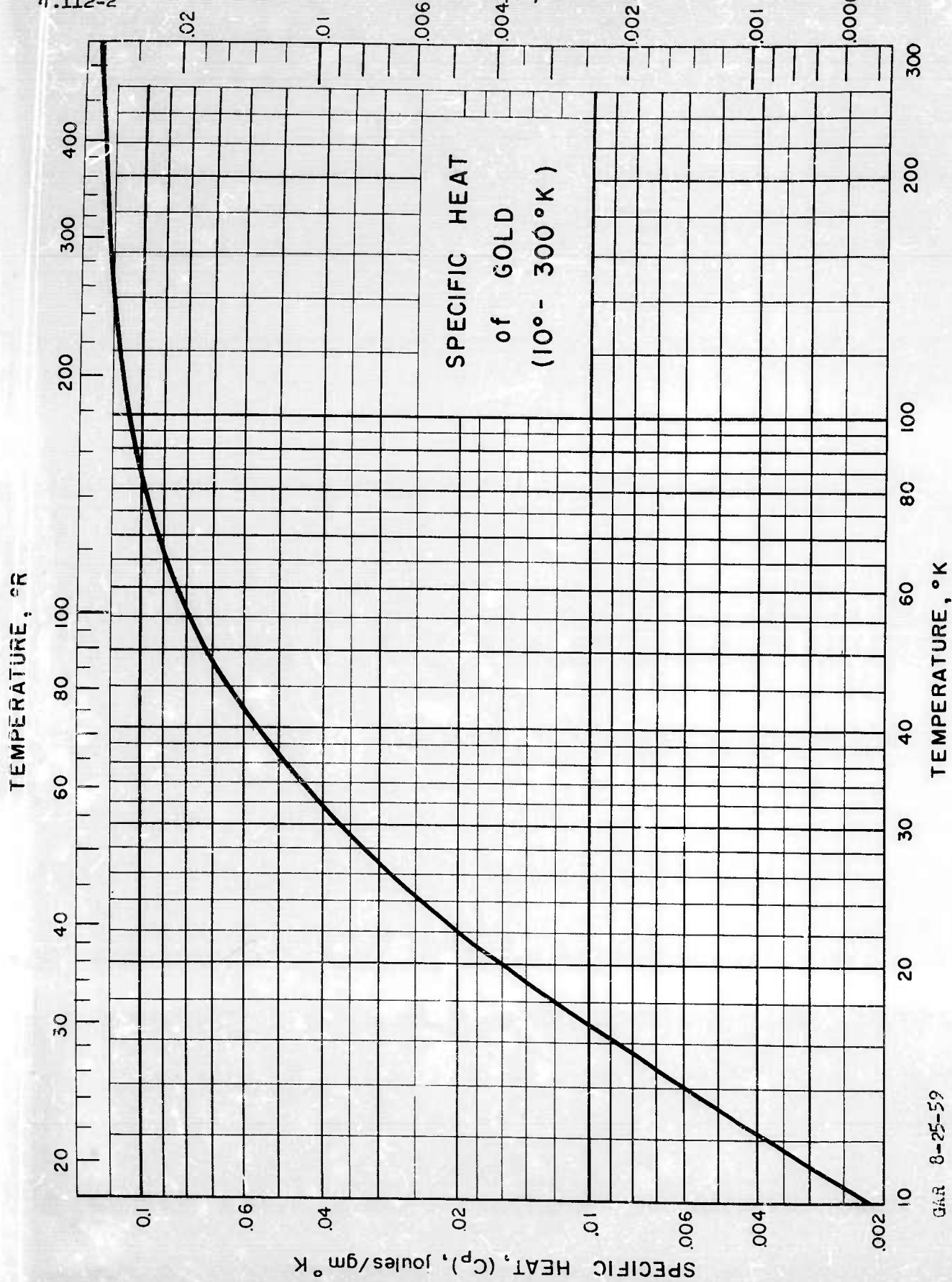
Table of Selected Values

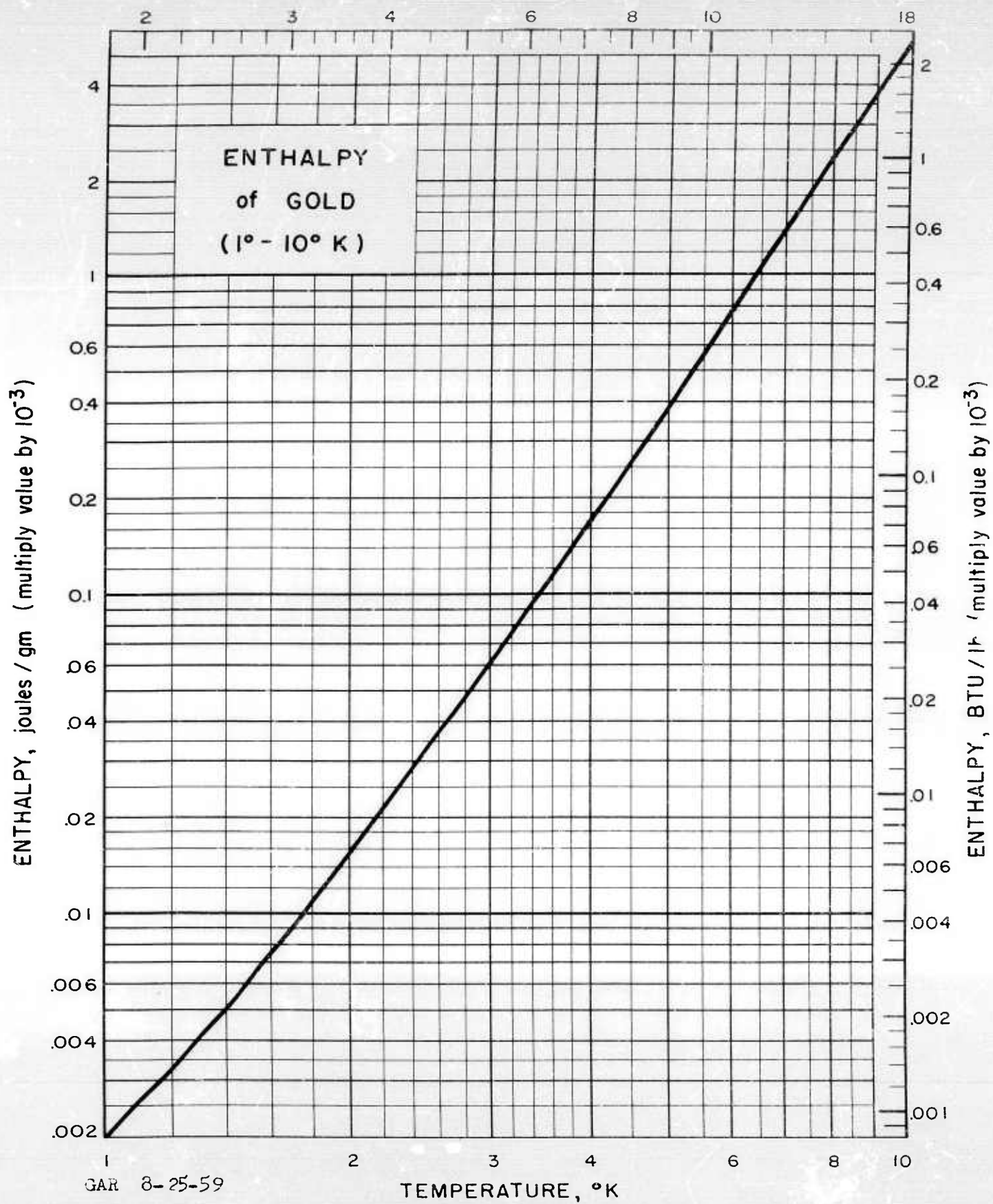
| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|-----------|-------------|------------------|-----------|
| 1 | 0.000 006 | 0.000 002 | 70 | 0.0928 | 3.14 |
| 2 | .000 025 | .000 016 | 80 | .0992 | 4.10 |
| 3 | .000 070 | .000 061 | 90 | .1043 | 5.12 |
| 4 | .000 16 | .000 17 | 100 | .1083 | 6.18 |
| 6 | .000 50 | .000 78 | 120 | .1137 | 8.41 |
| 8 | .001 2 | .002 4 | 140 | .1175 | 10.72 |
| 10 | .002 2 | .005 6 | 160 | .1202 | 13.10 |
| 15 | .007 4 | .028 | 180 | .1221 | 15.52 |
| 20 | .015 9 | .086 | 200 | .1235 | 17.98 |
| 25 | .026 3 | .191 | 220 | .1247 | 20.46 |
| 30 | .037 1 | .349 | 240 | .1257 | 22.96 |
| 40 | .057 2 | .821 | 260 | .1267 | 25.49 |
| 50 | .072 6 | 1.47 | 280 | .1276 | 28.03 |
| 60 | .084 2 | 2.25 | 300 | .1285 | 30.59 |

RJC/JJG Issued: 10-21-59

Revised: 5-20-60

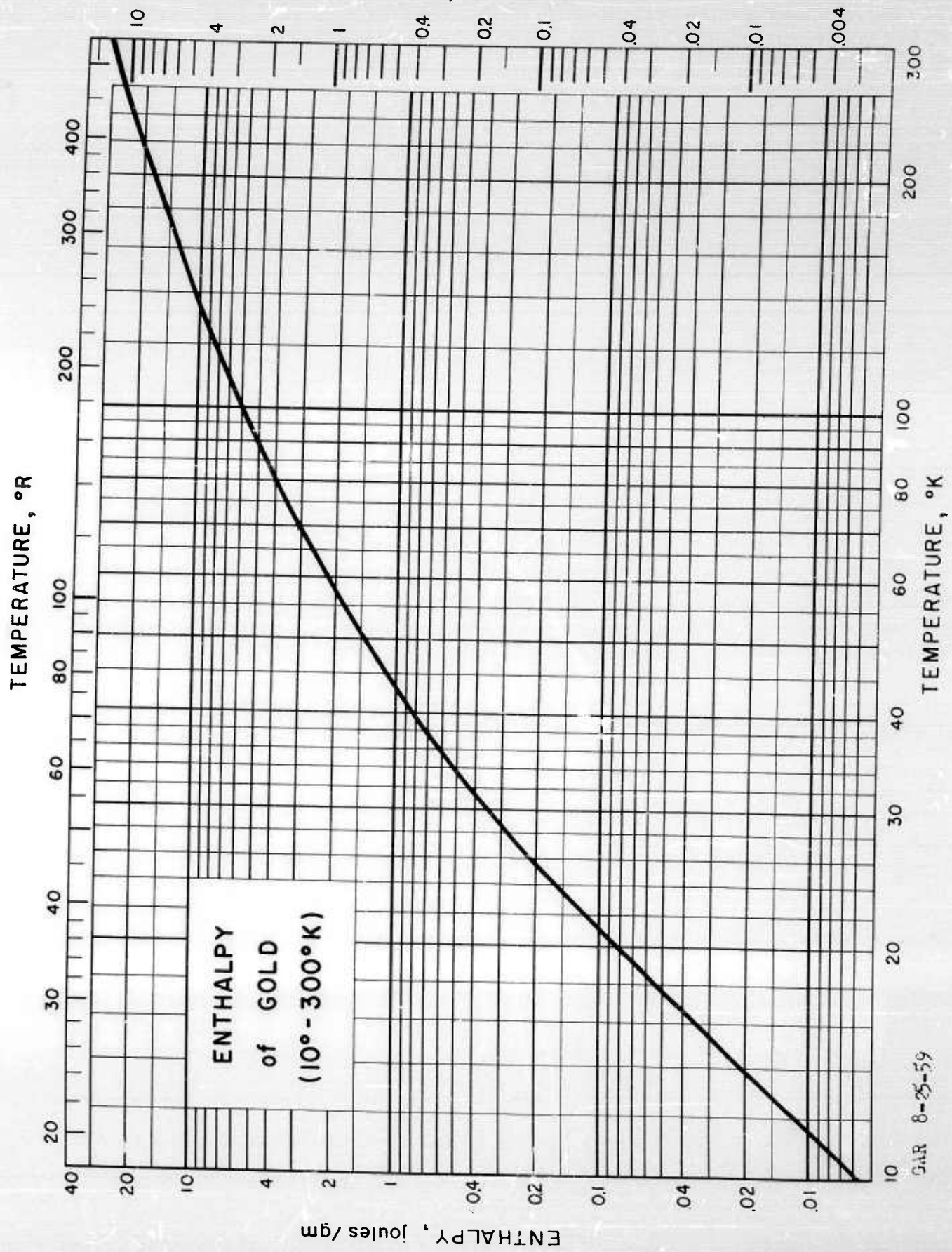






GAR 8-25-59

TEMPERATURE, °K



SPECIFIC HEAT, ENTHALPY of SILVER

Sources of Data:

Corak, W. S., Garfunkel, M. P., Satterthwaite, C. B. and Wexler, A.,
Phys. Rev. 98, 1699 (1955)
Meads, P. F., Forsythe, W. R. and Giaouque, W. F., J. Am. Chem. Soc. 63,
1902 (1941)

Other References:

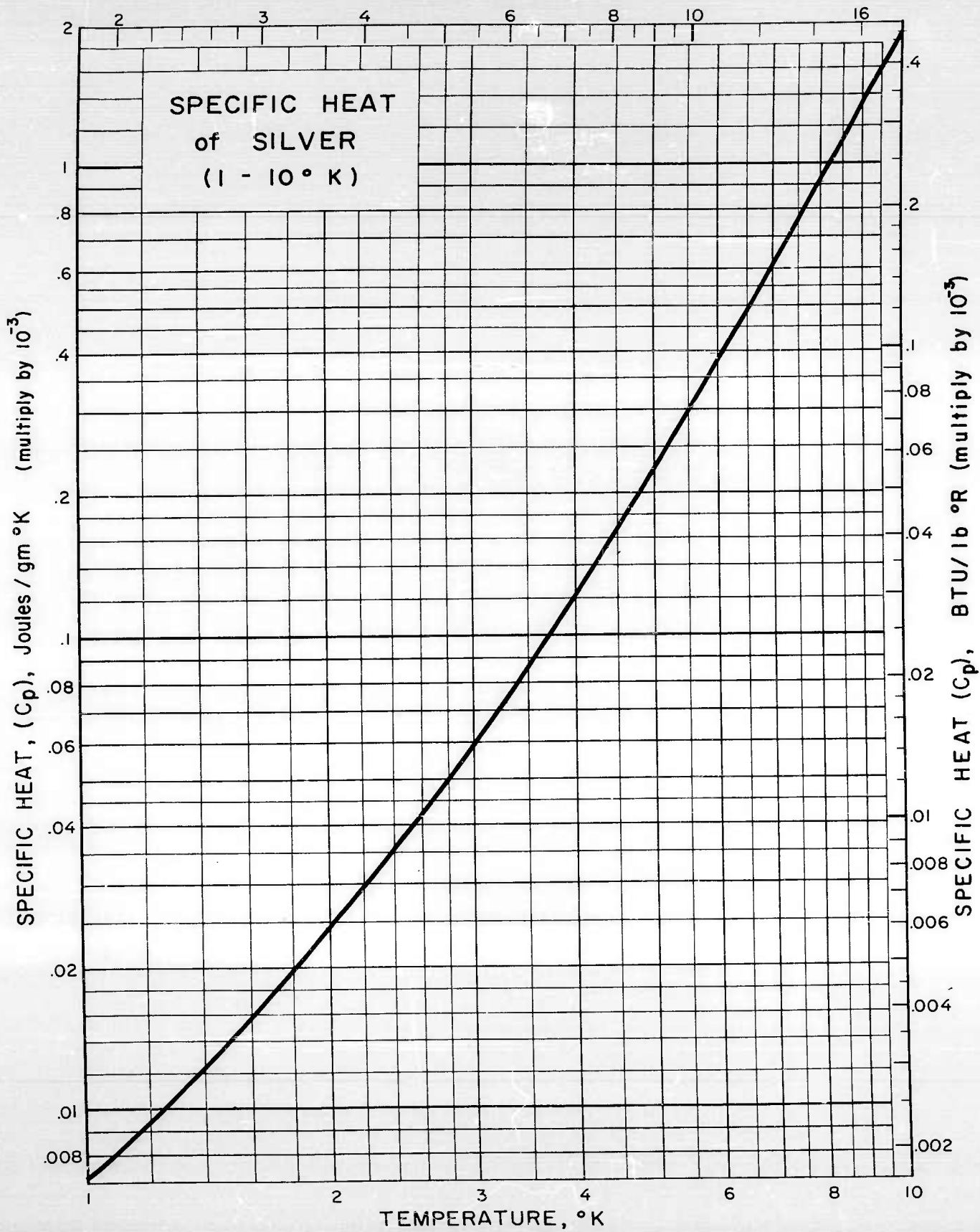
Barchall, H., Z. Electrochem. 17, 341 (1911)
Bronson, H. L. and Wilson, A. J. C., Can. J. Research, A14, 181 (1936)
Eucken, A., Clusius, K. and Weiteneck, H., Z. anorg. allgem. Chemie 203,
39 (1931)
Griffiths, E. G. and Griffiths, E., Proc. Roy. Soc. (London) A90, 557 (1914)
Keesom, W. H., Z. ges. Kalte-Ind. 40, 49 (1933)
Keesom, W. H., J. phys. radium (7) 5, 373 (1934)
Keesom, W. H. and Kok, J. A., Proc. Acad. Sci. Amsterdam 35, 301 (1932)
Keesom, W. H. and Kok, J. A., Physica 1, 770 (1934)
Keesom, W. H. and Pearlman, N., Phys. Rev. 98, 548 (1955)
Mendelschn, K. and Closs, J. O., Z. physik. Chem. B19, 291 (1932)
Nernst, W., Sitzber. kgl. preuss. Akad. Wiss. 262 (1910)
Nernst, W., Ann. Physik (4) 36, 395 (1911)
Nernst, W. and Lindemann, F. A., Sitzber. kgl. preuss. Akad. Wiss. 494 (1911)
Rayne, J. A., Phys. Rev. 95, 1428 (1954)
Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)
Tilden, W. A., Proc. Roy. Soc. (London) 71, 220 (1903)
Hoare, F. E. and Yates, L., Proc. Roy. Soc. (London) A240, 42 (1957)

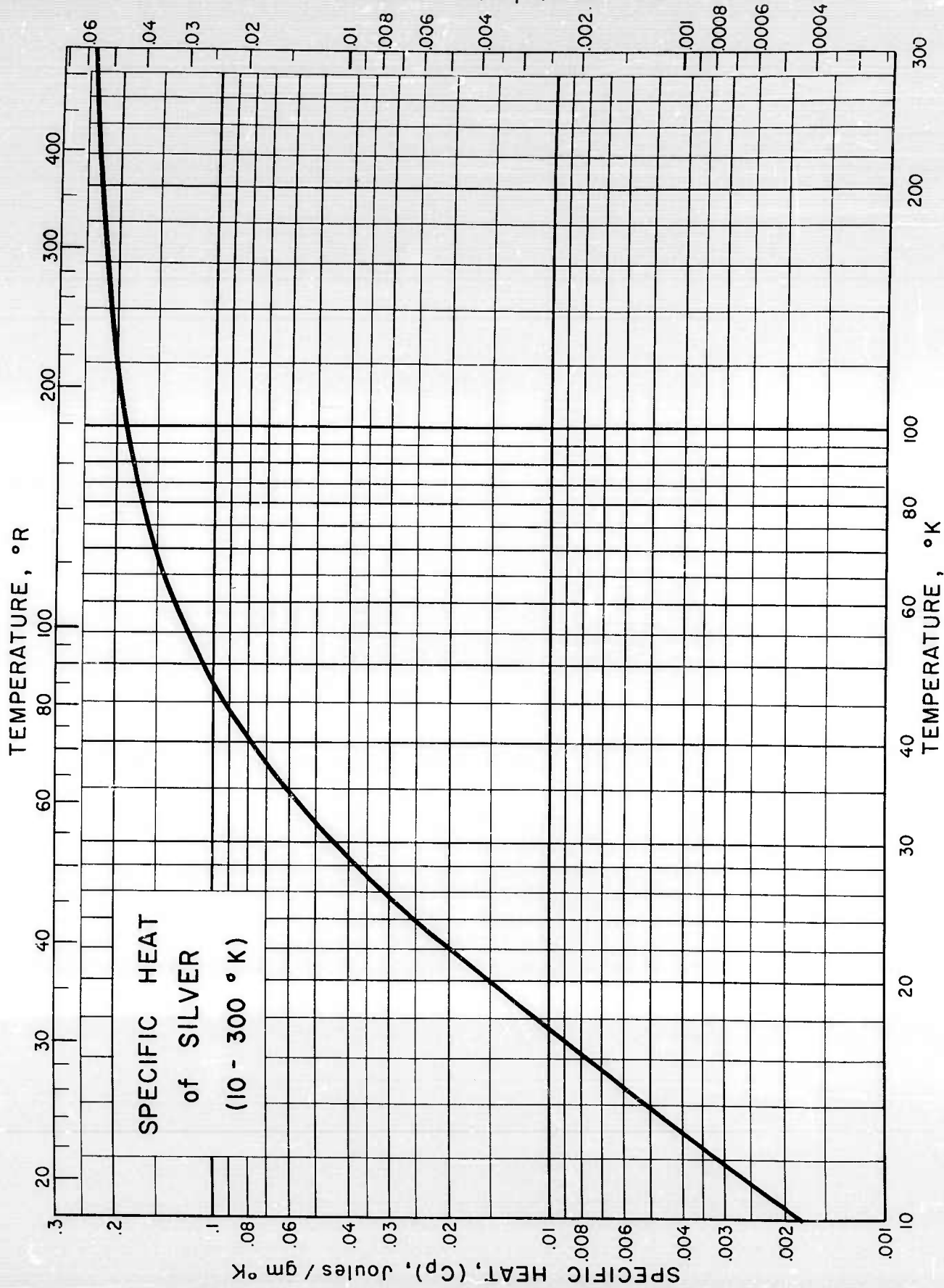
Table of Selected Values

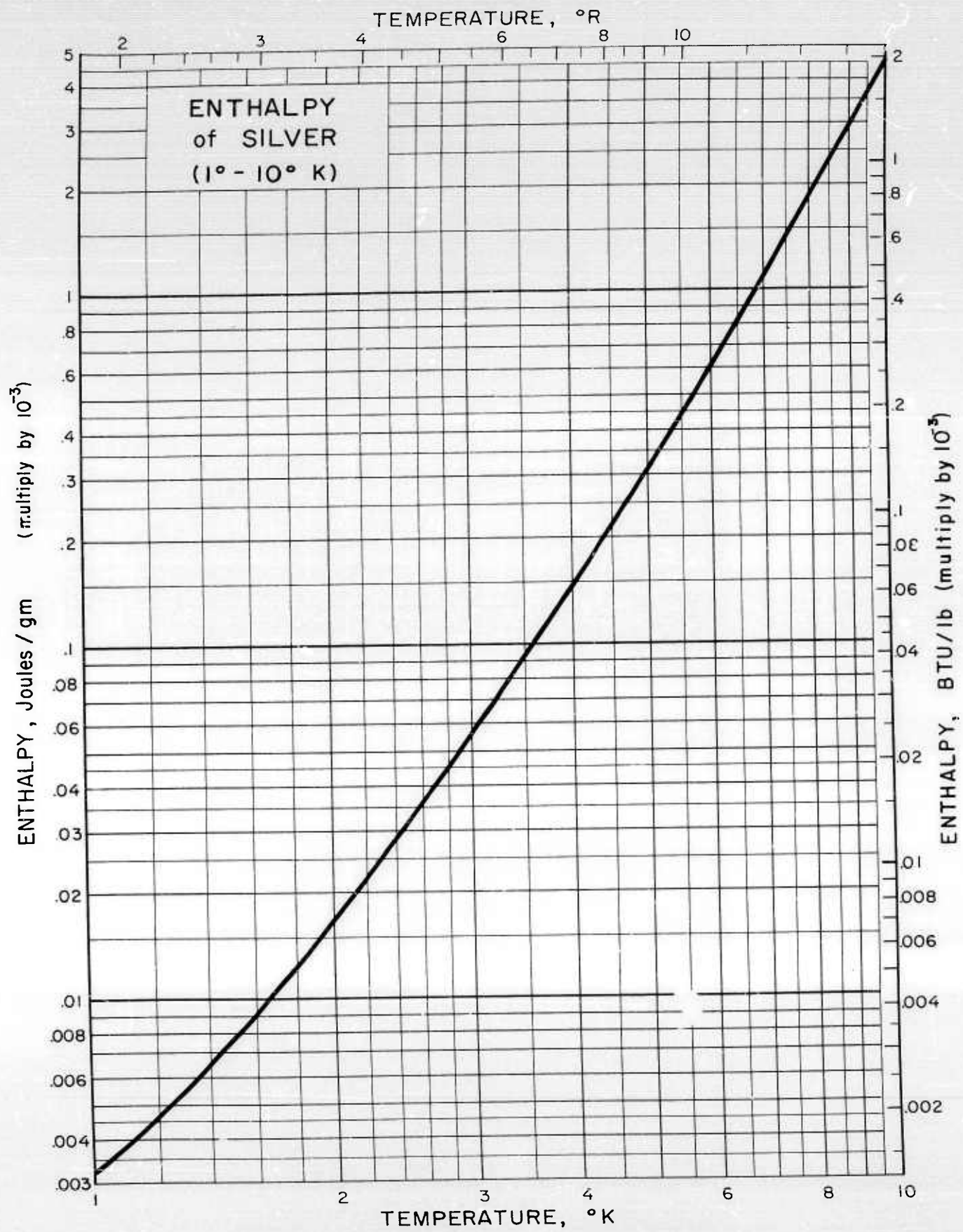
| T | Cp | H | T | Cp | H |
|----|------------|------------|-----|---------|-------|
| °K | j/gm-°K | j/gm | °K | j/gm-°K | j/gm |
| 1 | 0.000 0072 | 0.000 0032 | 70 | 0.151 | 4.54 |
| 2 | .000 0239 | .000 0176 | 80 | .166 | 6.13 |
| 3 | .000 0595 | .000 0574 | 90 | .177 | 7.85 |
| 4 | .000 124 | .000 146 | 100 | .187 | 9.67 |
| 6 | .000 39 | .000 62 | 120 | .200 | 13.55 |
| 8 | .000 91 | .001 87 | 140 | .209 | 17.65 |
| 10 | .001 8 | .004 52 | 160 | .216 | 21.91 |
| 15 | .006 4 | .023 3 | 180 | .221 | 26.29 |
| 20 | .015 5 | .076 | 200 | .225 | 30.75 |
| 25 | .028 7 | .185 | 220 | .228 | 35.28 |
| 30 | .044 2 | .368 | 240 | .231 | 39.86 |
| 40 | .078 | .979 | 260 | .234 | 44.50 |
| 50 | .108 | 1.91 | 280 | .235 | 49.20 |
| 60 | .133 | 3.12 | 300 | .236 | 53.91 |

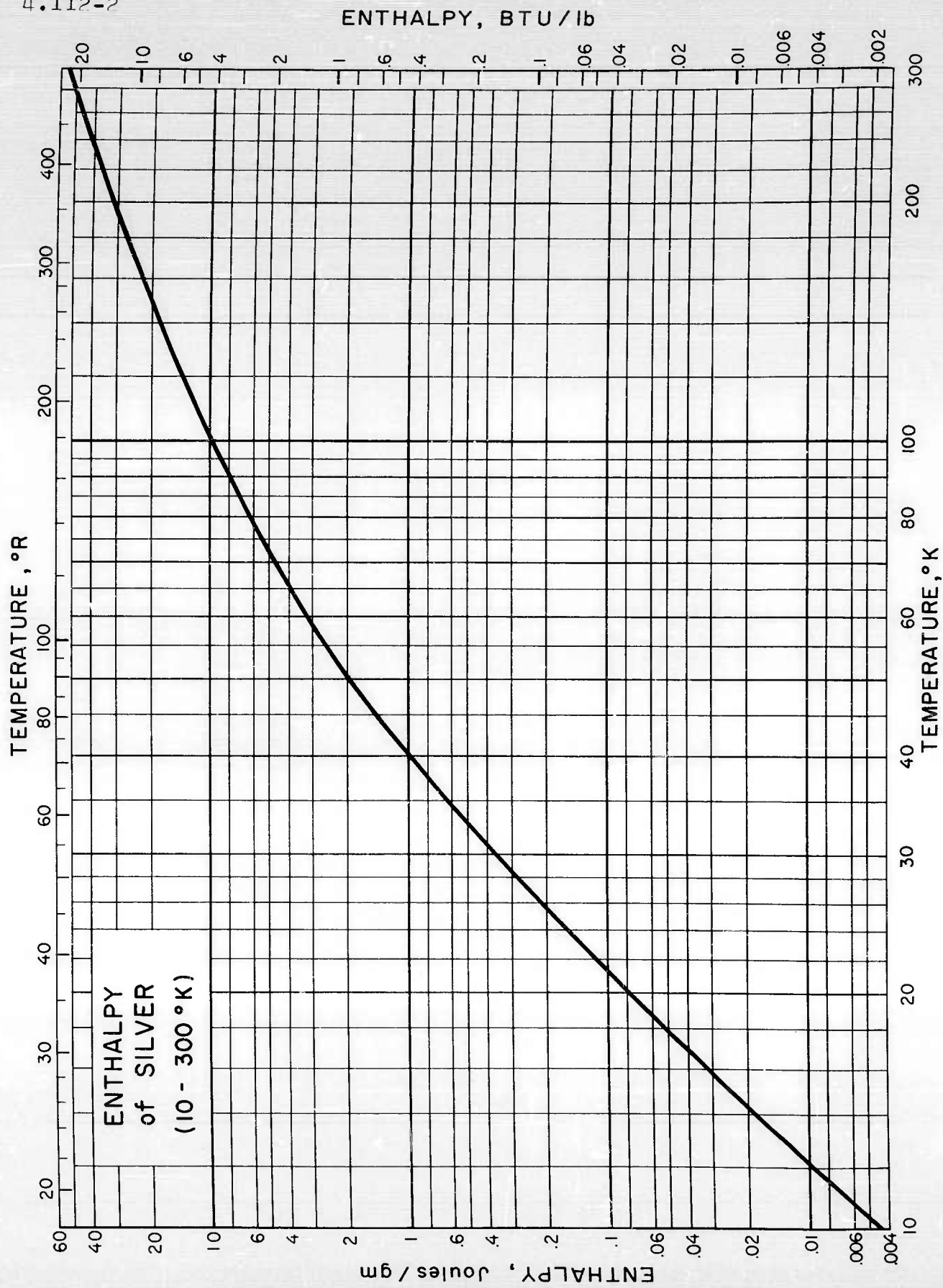
RJC Issued: 6-15-59
Revised: 5-20-60

TEMPERATURE, °R









SPECIFIC HEAT, ENTHALPY of BERYLLIUM

Source of Data:

Hill, R. W. and Smith, P. L., Phil. Mag. 44, 636-44 (1953)

Other References:

Cristescu, S. and Simon, F., Z. physik. Chem. B25, 273 (1934)

Kelley, K. K., U.S. Bur. Mines Bull. No. 476 (1949)

Lewis, E. J., Phys. Rev. (2) 34, 1575 (1929)

Simon, F. and Ruhemann, M., Z. physik. Chem. 129, 321 (1927)

Comments:

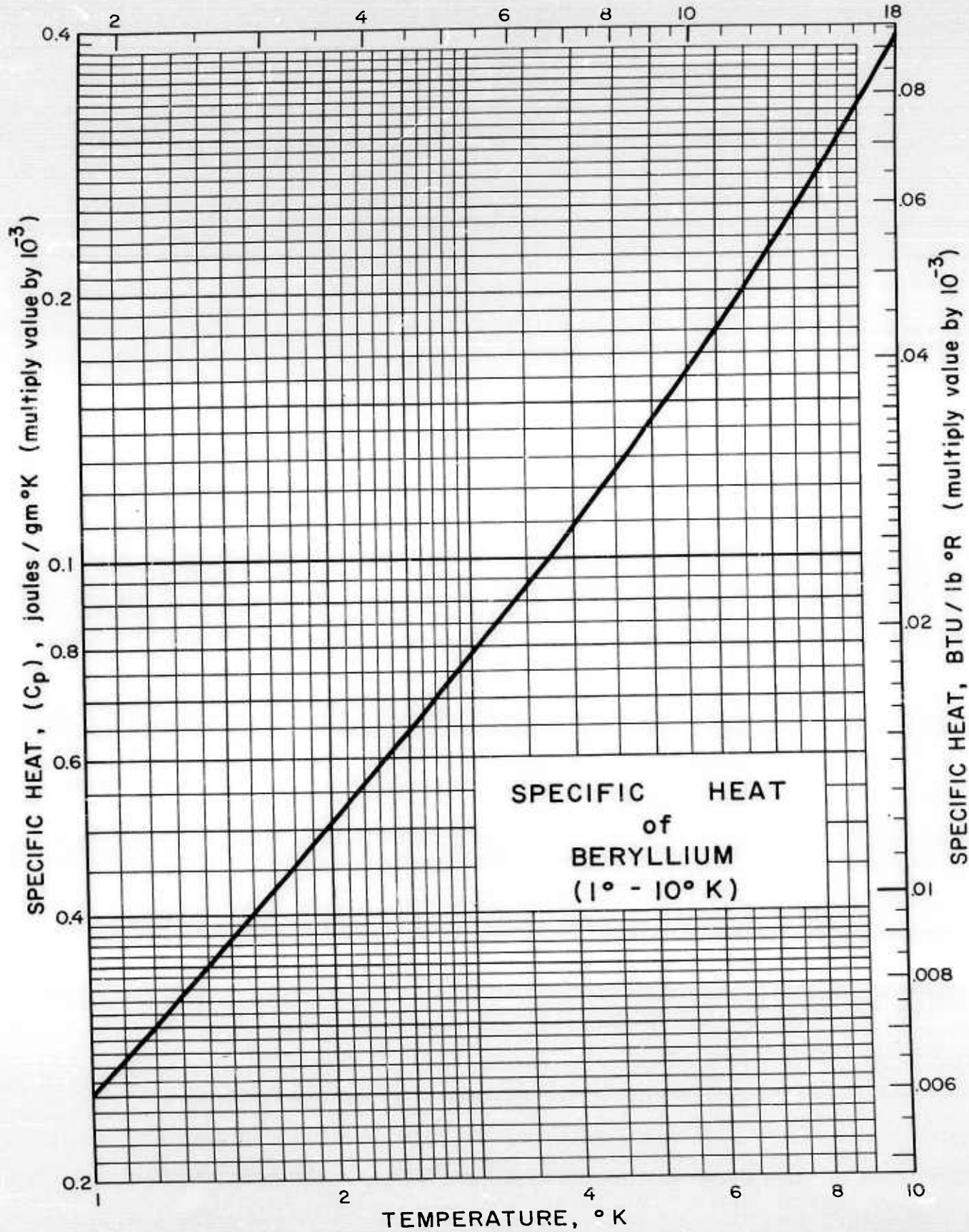
For the temperature range from 0° to 20°K, the specific heat C_p follows the equation:

$$C_p = (2.5 \pm 0.4) \times 10^{-5} T + 215.7 \left(\frac{T}{1160 \pm 5} \right)^3 \text{ j/gm-}^\circ\text{K}$$

Table of Selected Values

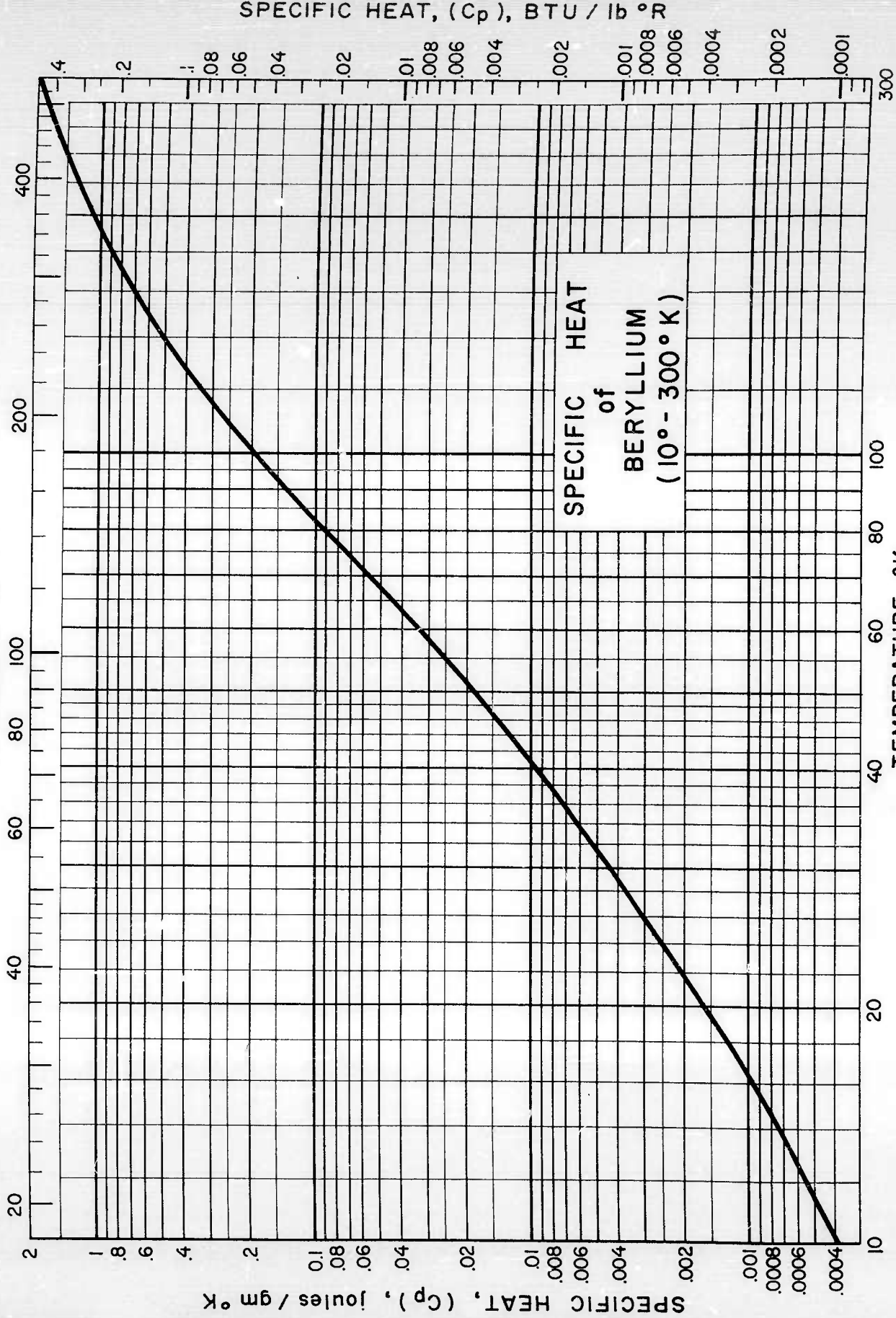
| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|-----------|-------------|------------------|-----------|
| 1 | 0.000 025 | 0.000 013 | 70 | 0.0562 | 0.971 |
| 2 | .000 051 | .000 051 | 80 | .0906 | 1.69 |
| 3 | .000 079 | .000 116 | 90 | .139 | 2.82 |
| 4 | .000 109 | .000 209 | 100 | .199 | 4.51 |
| 6 | .000 180 | .000 496 | 120 | .345 | 9.87 |
| 8 | .000 271 | .000 944 | 140 | .525 | 18.5 |
| 10 | .000 389 | .001 60 | 160 | .723 | 31.0 |
| 15 | .000 842 | .004 57 | 180 | .921 | 47.4 |
| 20 | .001 61 | .010 5 | 200 | 1.11 | 67.8 |
| 25 | .002 79 | .021 2 | 220 | 1.29 | 91.8 |
| 30 | .004 50 | .039 2 | 240 | 1.47 | 120 |
| 40 | .009 96 | .109 | 260 | 1.64 | 151 |
| 50 | .019 2 | .253 | 280 | 1.81 | 185 |
| 60 | .034 1 | .523 | 300 | 1.97 | 223 |

TEMPERATURE, °R

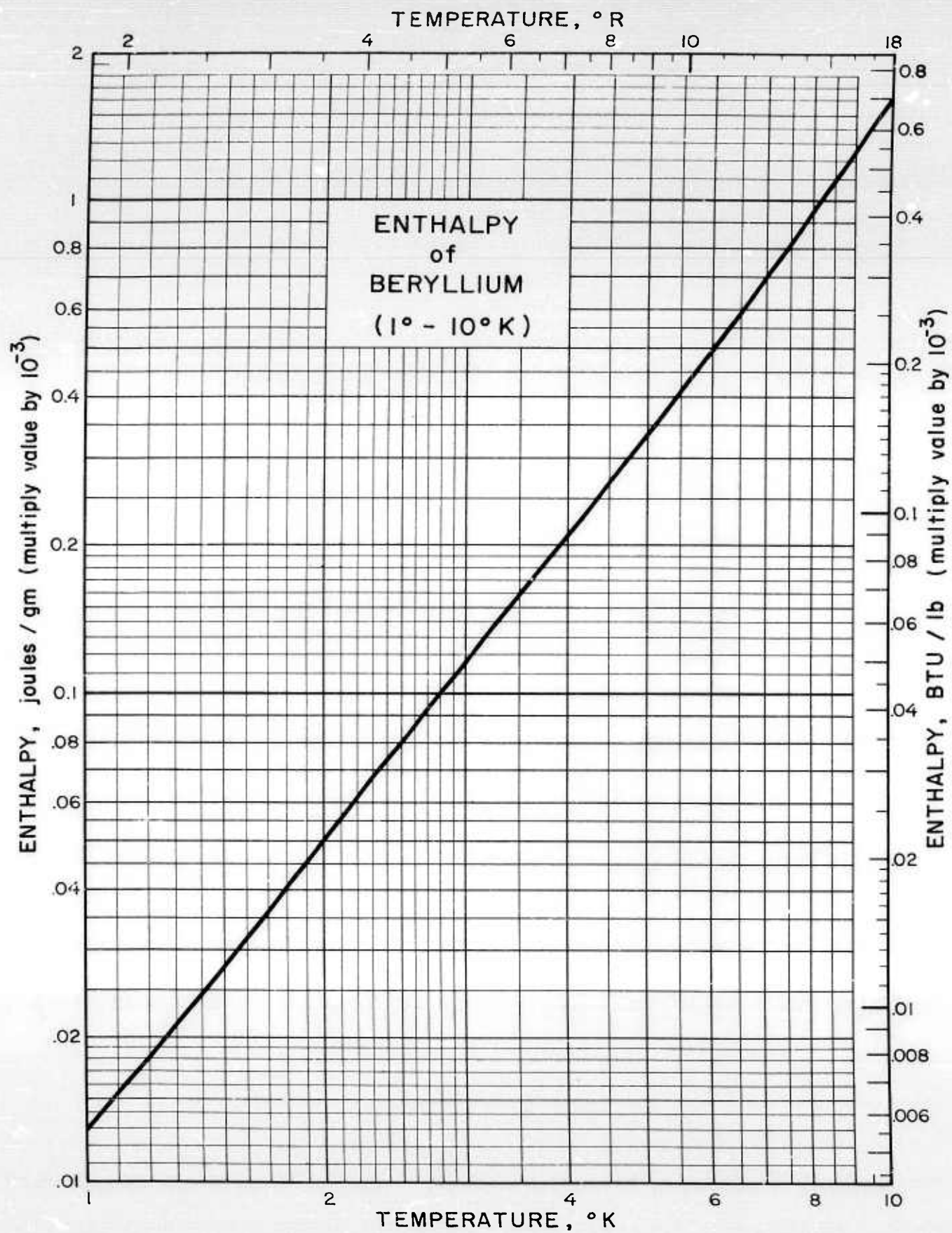


4.121

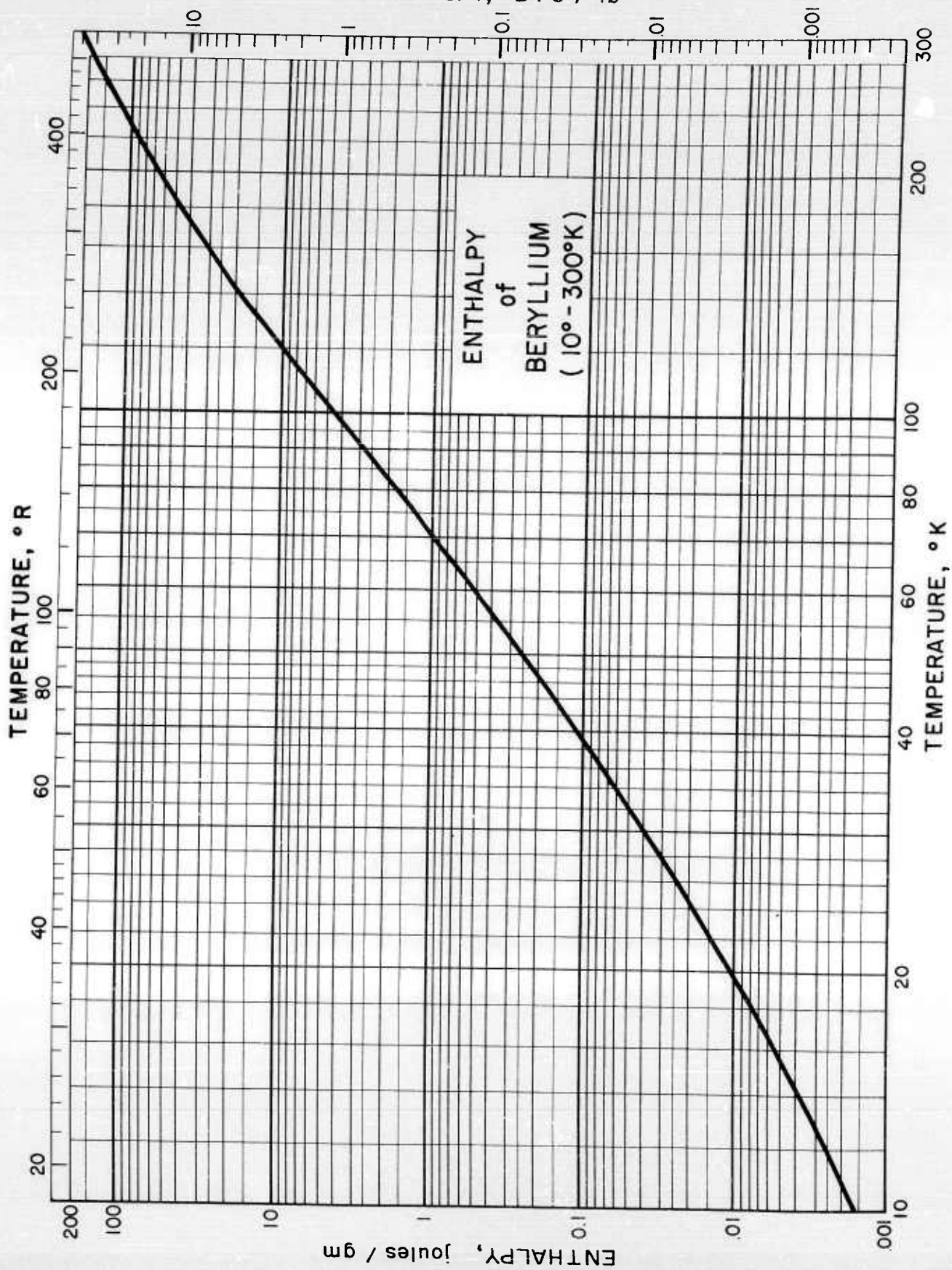
TEMPERATURE, °R



TEMPERATURE, °K



ENTHALPY, BTU / lb



SPECIFIC HEAT, ENTHALPY of MAGNESIUM

Sources of Data:

Craig, R. S., Krier, C. A., Coffey, L. W., Bates, E. A. and Wallace, W. E., J. Am. Chem. Soc. 76, 238 (1954)

Smith, P. L., Phil. Mag. (7) 46, 744 (1955)

Other References:

Clusius, K. and Vaughen, J. V., J. Am. Chem. Soc. 52, 4686 (1930)

Eastman, E. C. and Rodebush, W. H., J. Am. Chem. Soc. 40, 489 (1918)

Estermann, I., Friedberg, S. A. and Goldman, J. E., Phys. Rev. 87, 582 (1952)

Friedberg, S. A., Estermann, I. and Goldman, J. E., Phys. Rev. 85, 375-6 (1952)

Ewald, R., Ann. Physik (4) 44, 1213 (1914)

Nernst, W. and Schwers, F., Sitzber. kgl. preuss. Akad. Wiss. 355, (1914)

Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)

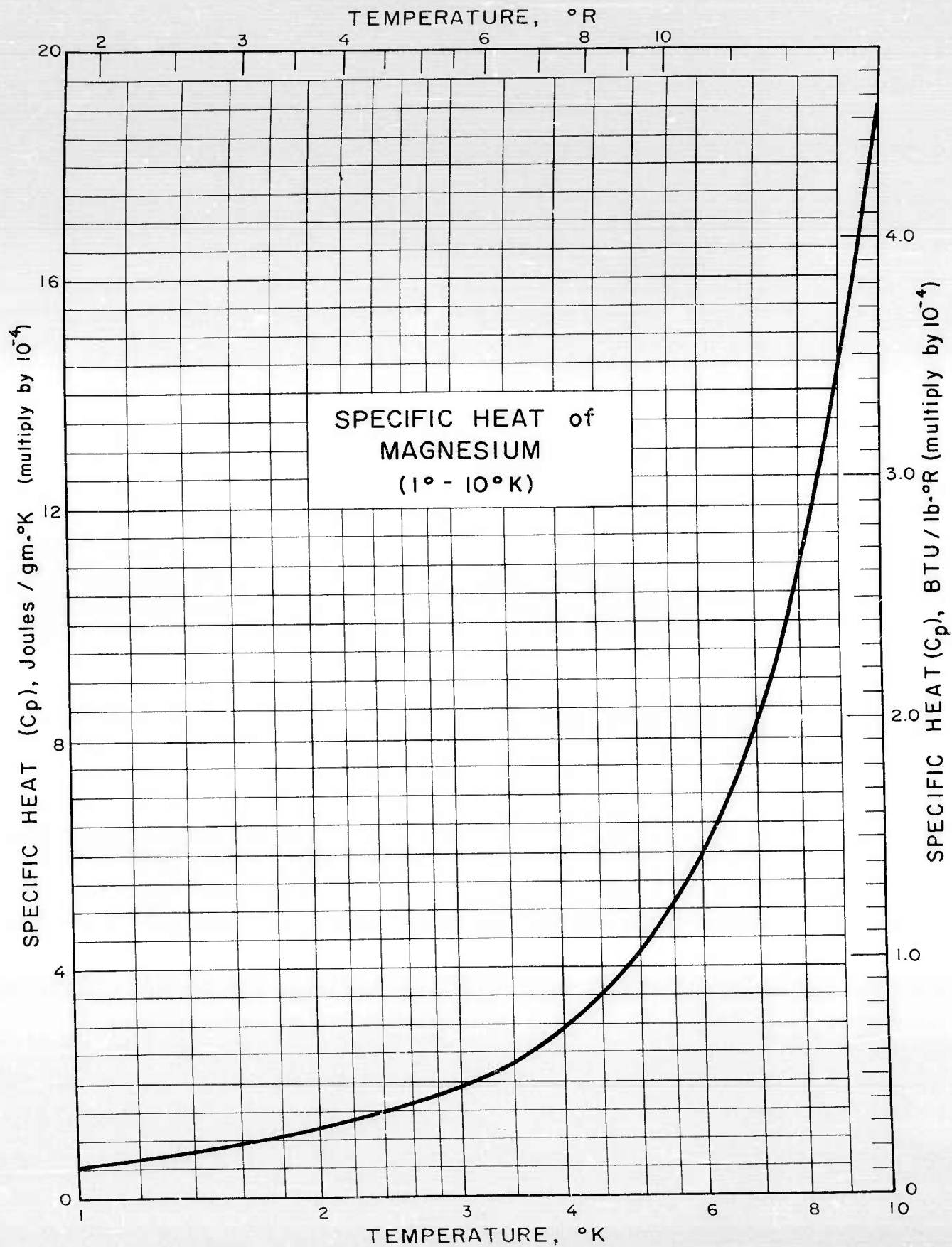
Table of Selected Values

| Temp. °K | C _p j/gm °K | H j/gm | Temp. °K | C _p j/gm °K | H j/g |
|-------------|---------------------------|-----------|-------------|---------------------------|----------|
| 1 | 0.000 055 | 0.000 027 | 70 | 0.430 | 9.9 |
| 2 | .000 117 | .000 112 | 80 | .513 | 14.6 |
| 3 | .000 19 | .000 26 | 90 | .586 | 20.1 |
| 4 | .000 29 | .000 50 | 100 | .646 | 26.3 |
| 6 | .000 59 | .001 36 | 120 | .741 | 40.2 |
| 8 | .001 08 | .003 00 | 140 | .812 | 55.8 |
| 10 | .001 9 | .005 9 | 160 | .862 | 72.5 |
| 15 | .005 8 | .023 7 | 180 | .901 | 90.2 |
| 20 | .015 | .074 | 200 | .932 | 108.5 |
| 25 | .032 | .189 | 220 | .955 | 127.4 |
| 30 | .059 | .415 | 240 | .975 | 146.7 |
| 35 | .095 | .795 | 260 | .992 | 166.4 |
| 40 | .138 | 1.37 | 280 | 1.007 | 186.4 |
| 50 | .235 | 3.23 | 300 | 1.021 | 206.7 |
| 60 | .336 | 6.10 | | | |

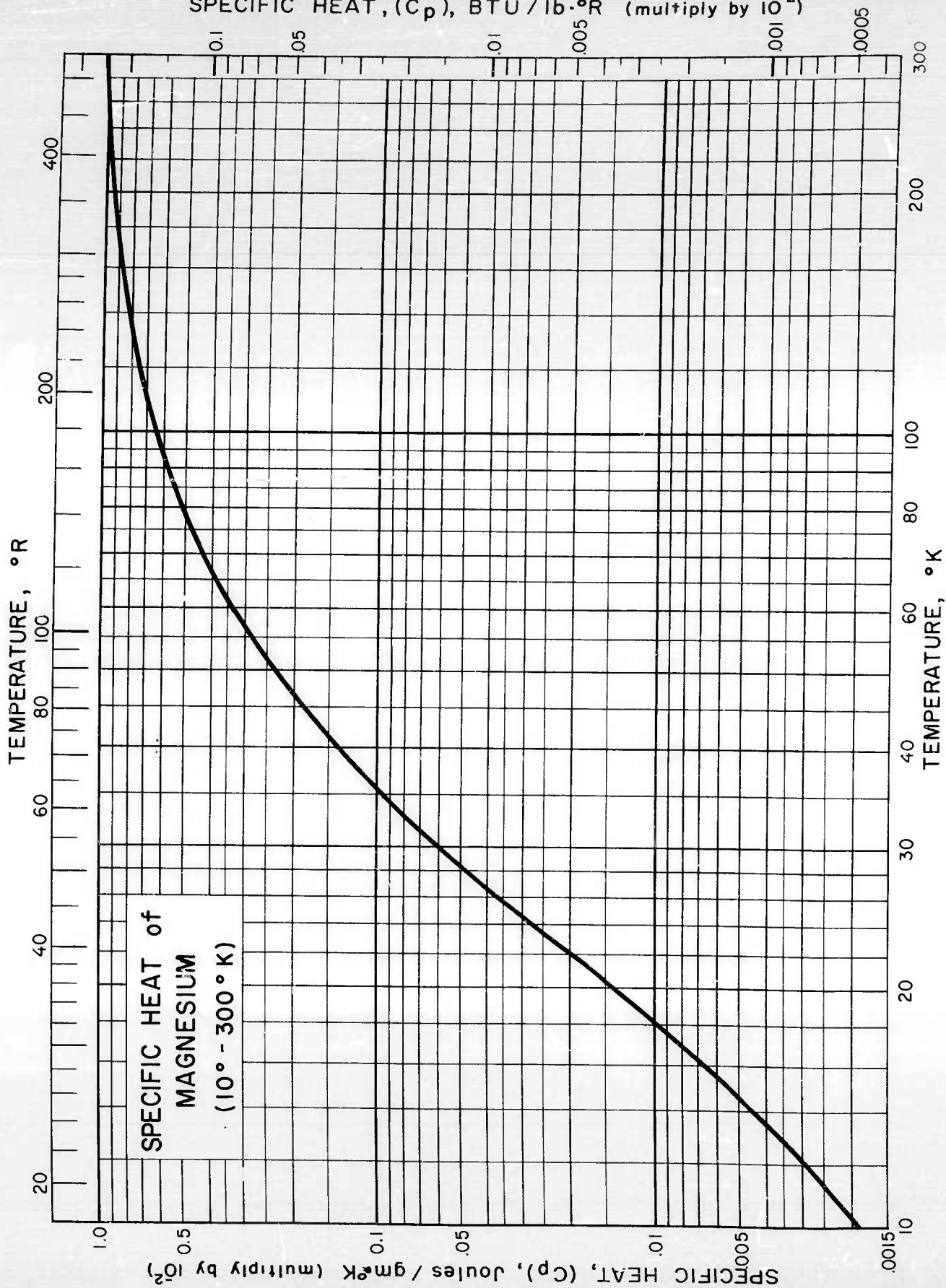
RJC Issued: 12-10-59

Revised: 5-20-60

L.121

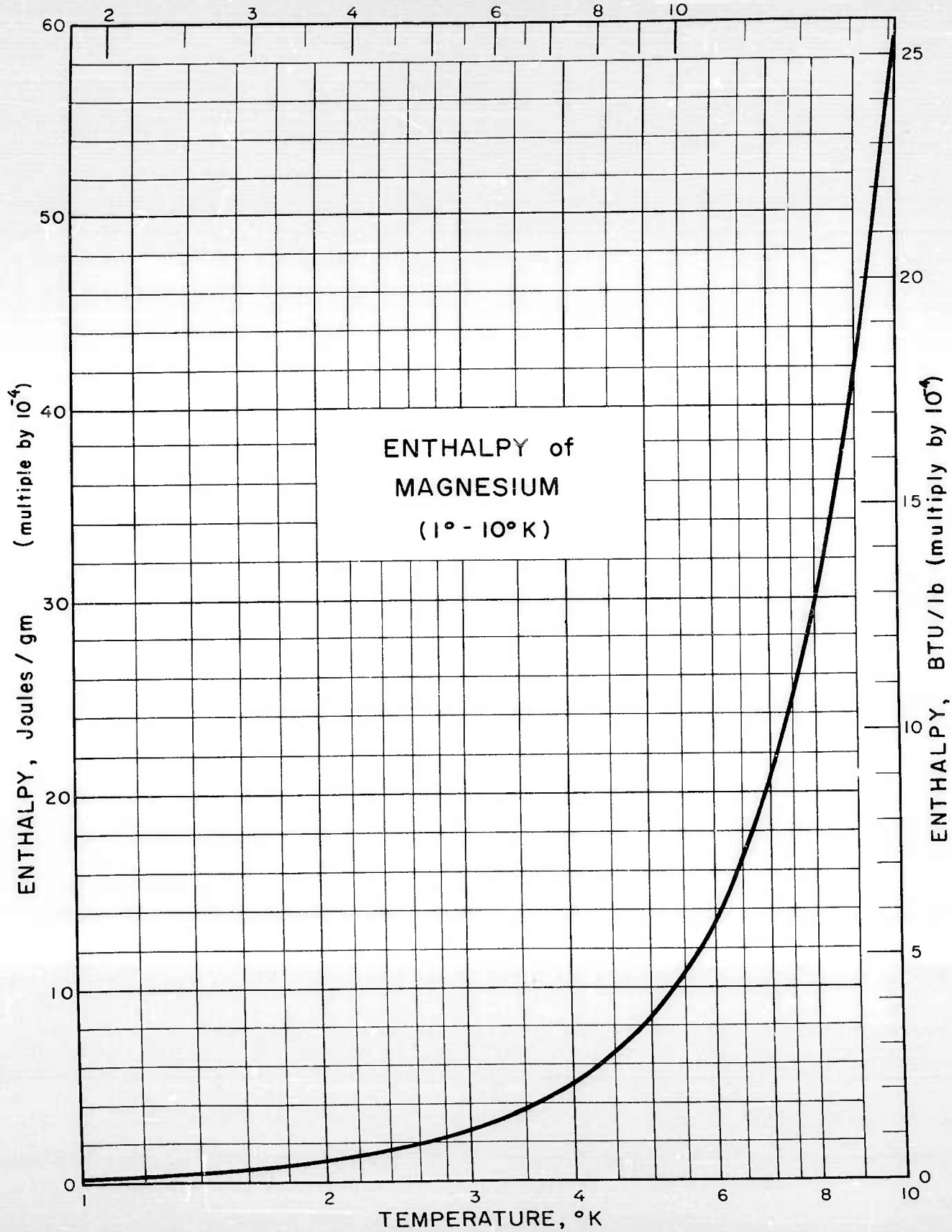


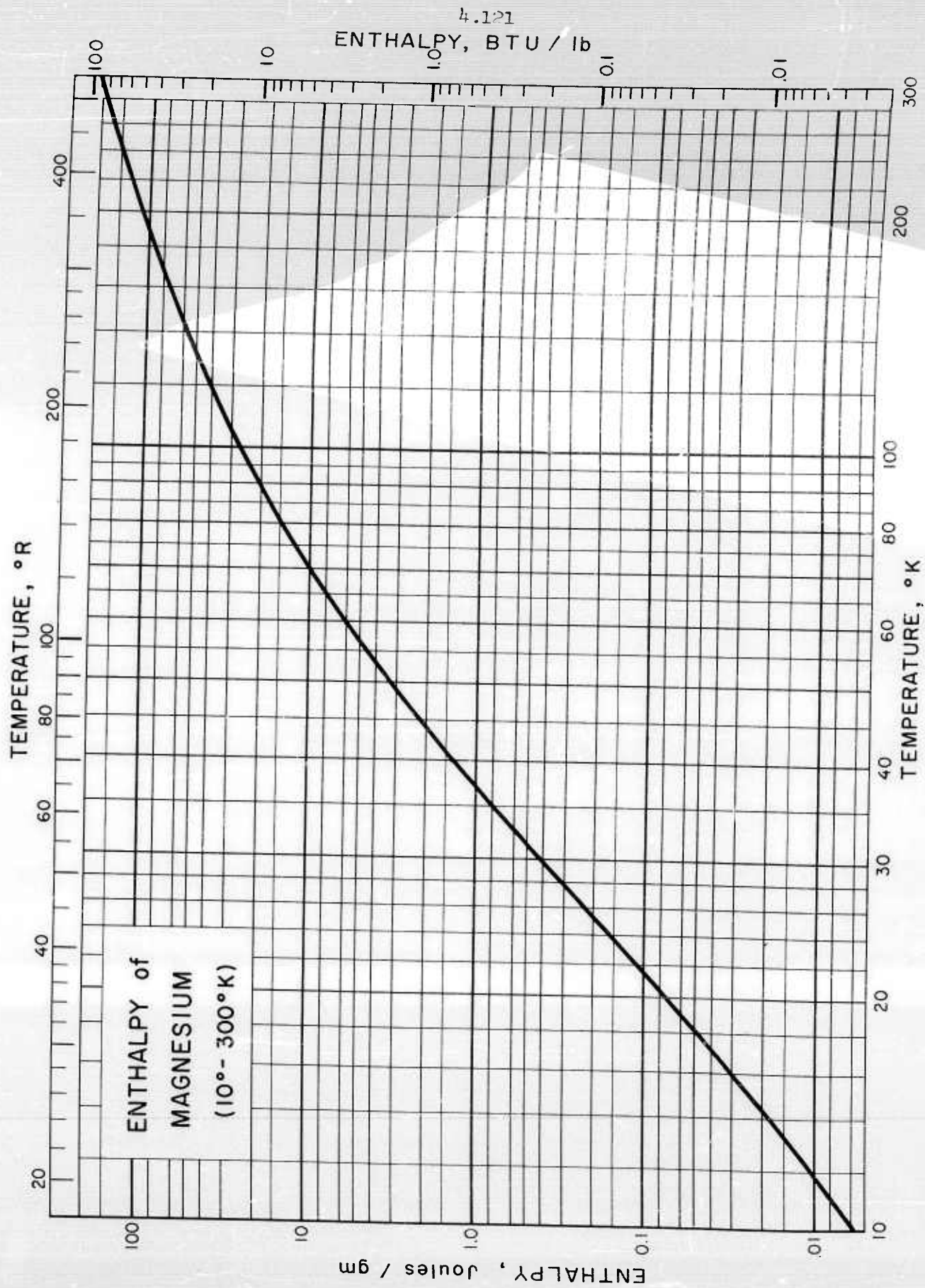
4.121
SPECIFIC HEAT, (C_p), BTU / lb·°R (multiply by 10^{-2})



4.121

TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of CADMIUM

Sources of Data:

- Bronson, H. L. and Wilson, A. J. C., Can. J. Research A14, 181 (1936)
 Craig, R. S., Krier, C. A., Coffey, L. W., Bates, E. A. and Wallace, W. E., J. Am. Chem. Soc. 76, 238 (1954)
 Smith, P. L., Conference de Physique des Basses Temperatures, Paris 281-3 (1955)

Other References:

- Barchall, H., Z. Elektrochem. 17, 341 (1911)
 Ewald, R., Ann. Physik. (4) 44, 1213 (1914)
 Lange, F. and Simon, F., Z. physik. Chem. 134, 374 (1928)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
 Rodebush, W. H., J. Am. Chem. Soc. 45, 1413 (1923)
 Samoïlov, B. N., Doklady Akad. Nauk. S.S.S.R. 86, 281-4 (1952)

Comments:

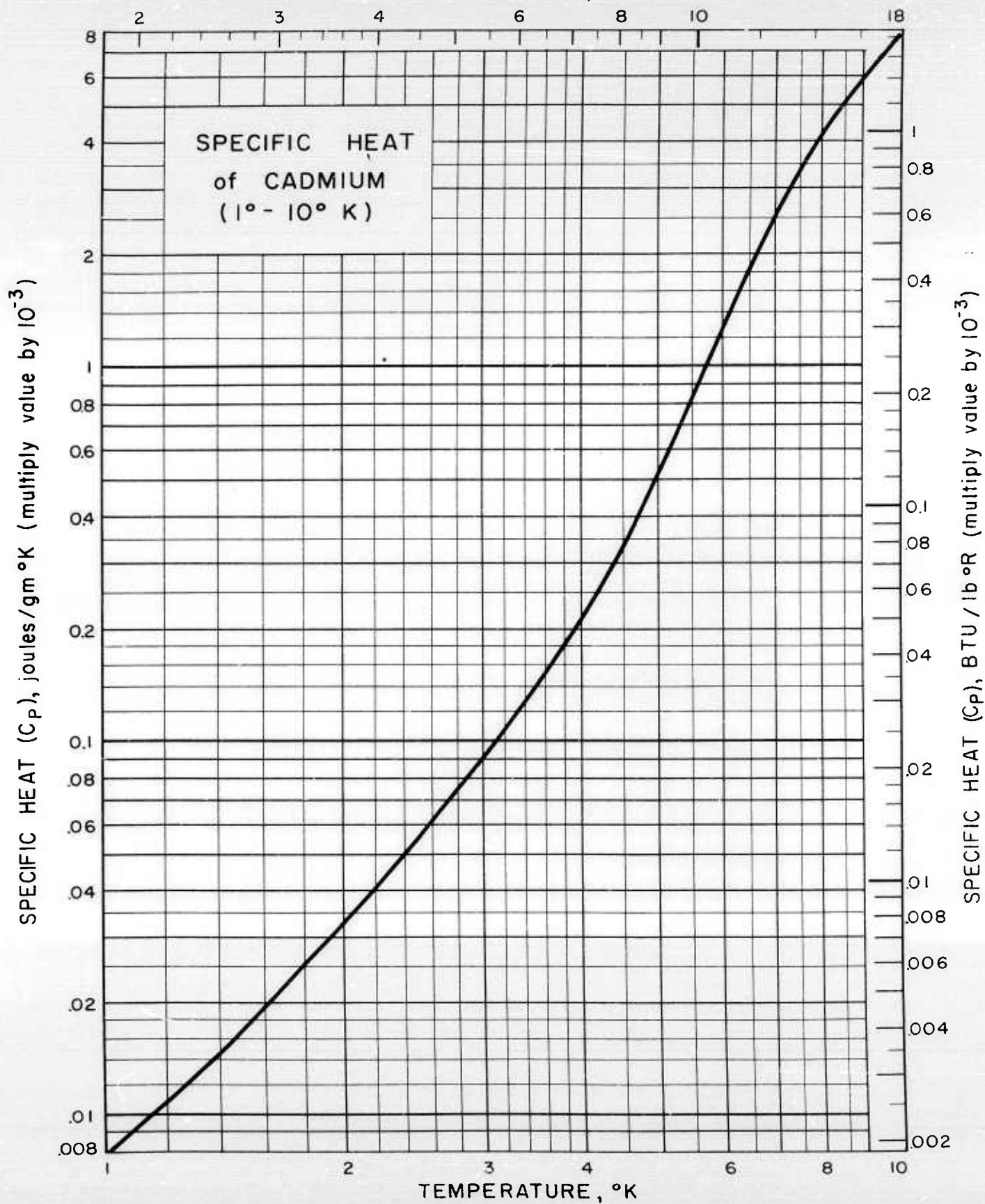
For $0 < T \leq 3^\circ\text{K}$

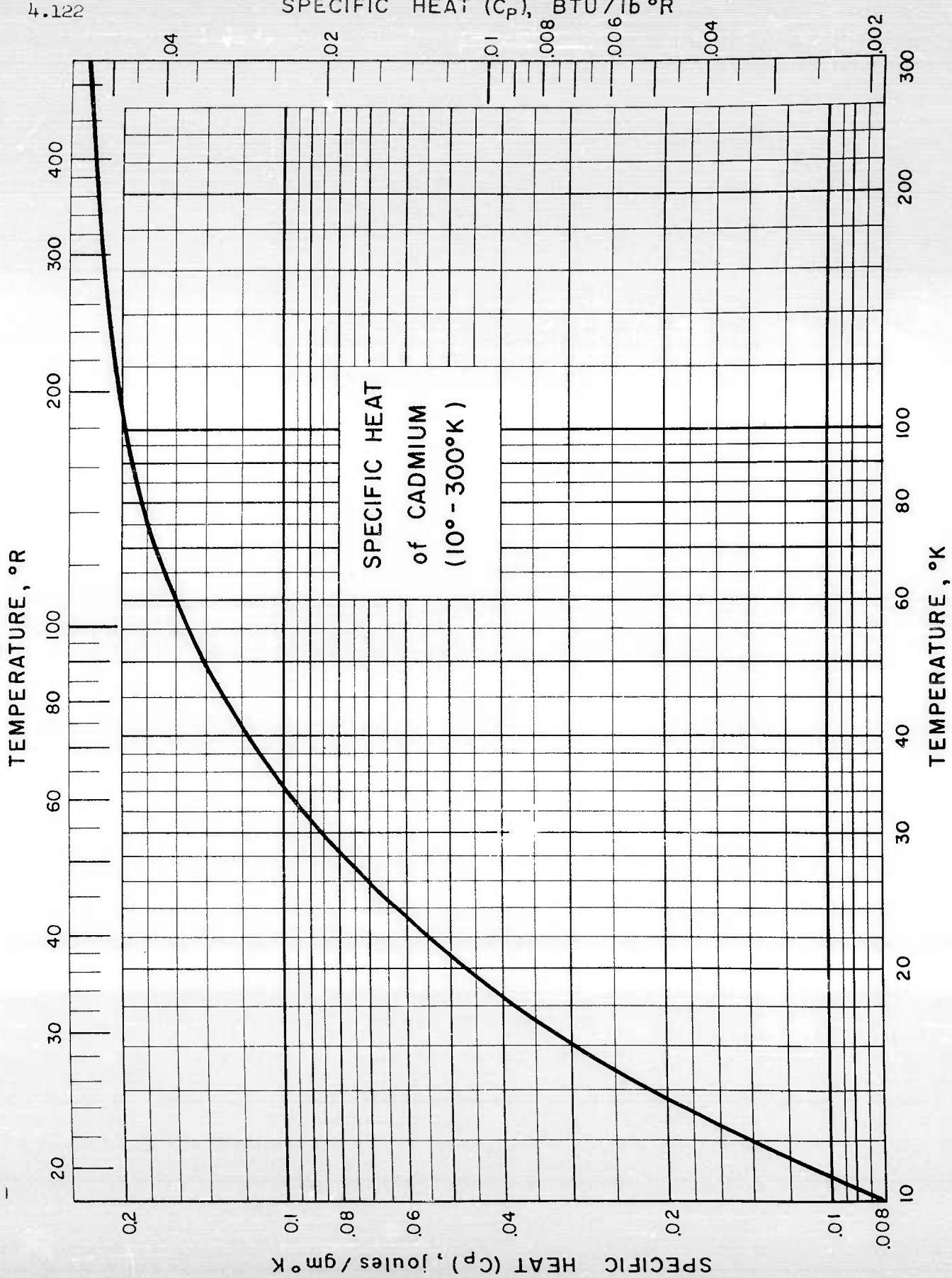
$$C_p = 17.3 (T/186)^3 \times 5.6 \times 10^{-6} T \text{ j/gm-}^\circ\text{K}$$

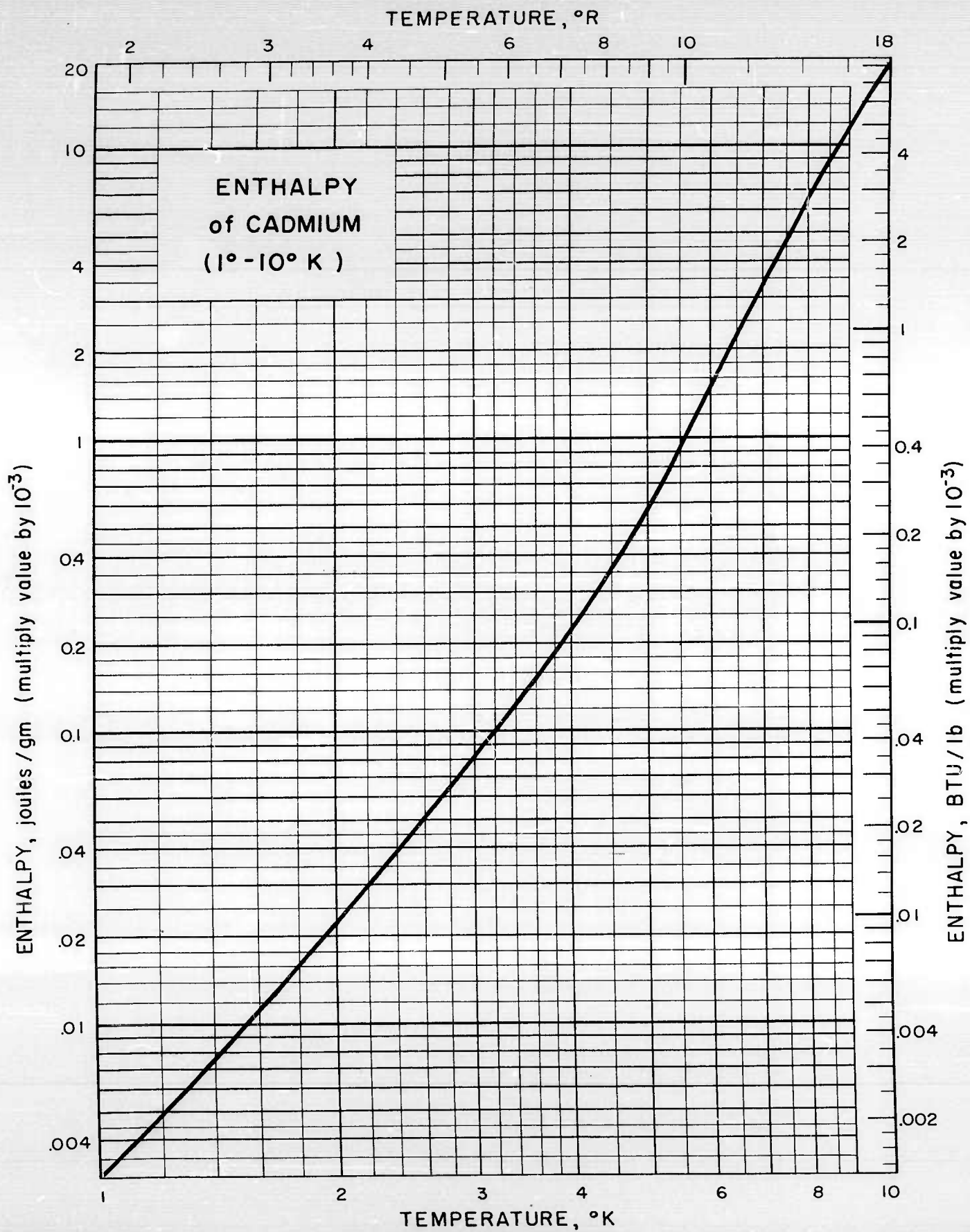
Table of Selected Values

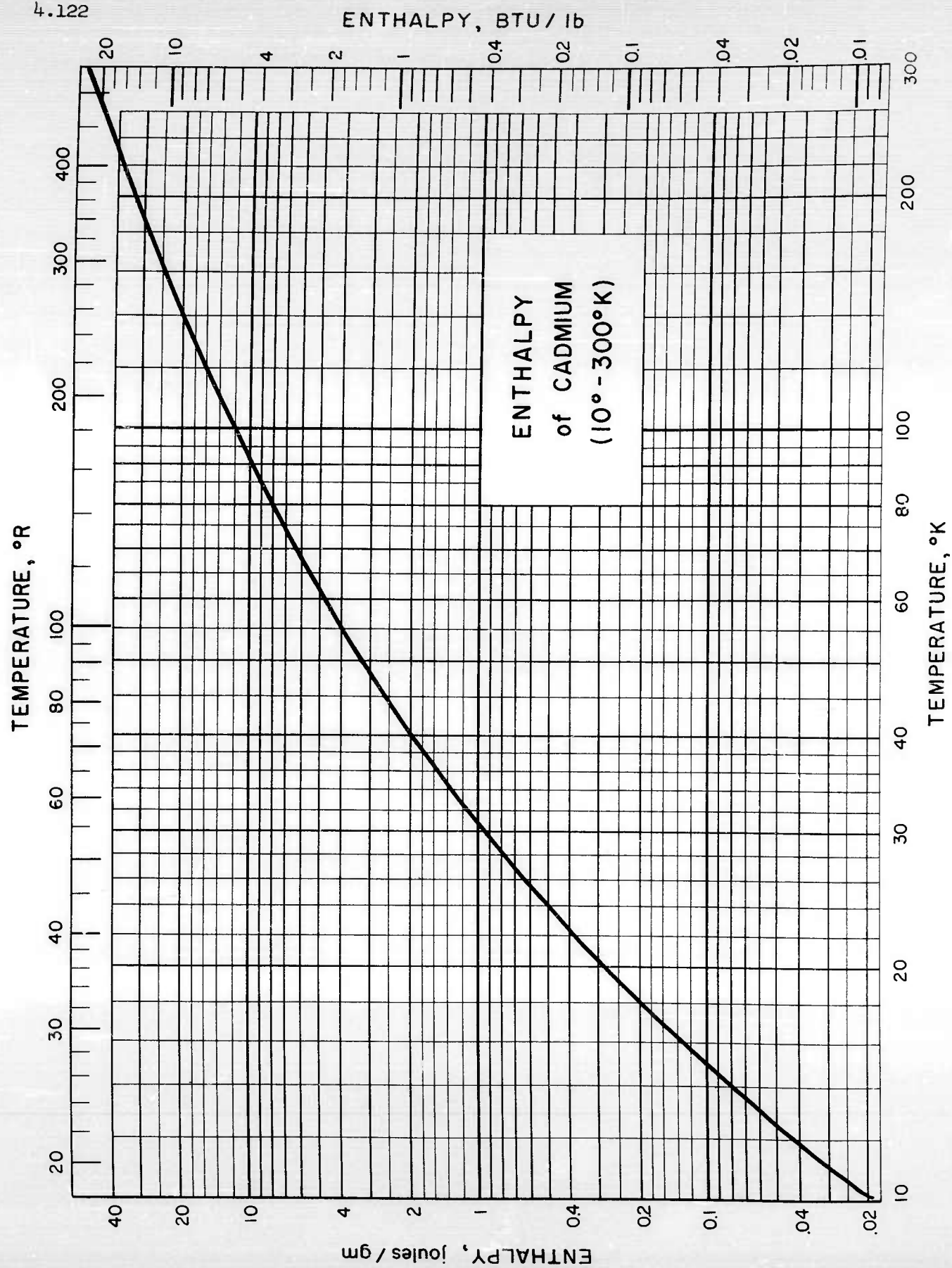
| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|-----------------------|-----------------------|-------------|------------------|-----------|
| 1 | $.008 \times 10^{-3}$ | $.003 \times 10^{-3}$ | 70 | .172 | 6.43 |
| 2 | .033 " | .022 " | 80 | .182 | 8.20 |
| 3 | .090 " | .082 " | 90 | .190 | 10.1 |
| 4 | .21 " | .22 " | 100 | .196 | 12.0 |
| 6 | 1.30 " | 1.5 " | 120 | .205 | 16.0 |
| 8 | 4.30 " | 7.0 " | 140 | .211 | 20.2 |
| 10 | 8.0 " | 19.0 " | 160 | .215 | 24.4 |
| 15 | .025 | .102 | 180 | .219 | 28.8 |
| 20 | .046 | .28 | 200 | .222 | 33.2 |
| 25 | .066 | .56 | 220 | .224 | 37.6 |
| 30 | .086 | .94 | 240 | .226 | 42.1 |
| 40 | .117 | 1.96 | 260 | .228 | 46.7 |
| 50 | .141 | 3.26 | 280 | .229 | 51.2 |
| 60 | .159 | 4.76 | 300 | .230 | 55.8 |

TEMPERATURE, °R









SPECIFIC HEAT, ENTHALPY of MERCURY

Sources of Data:

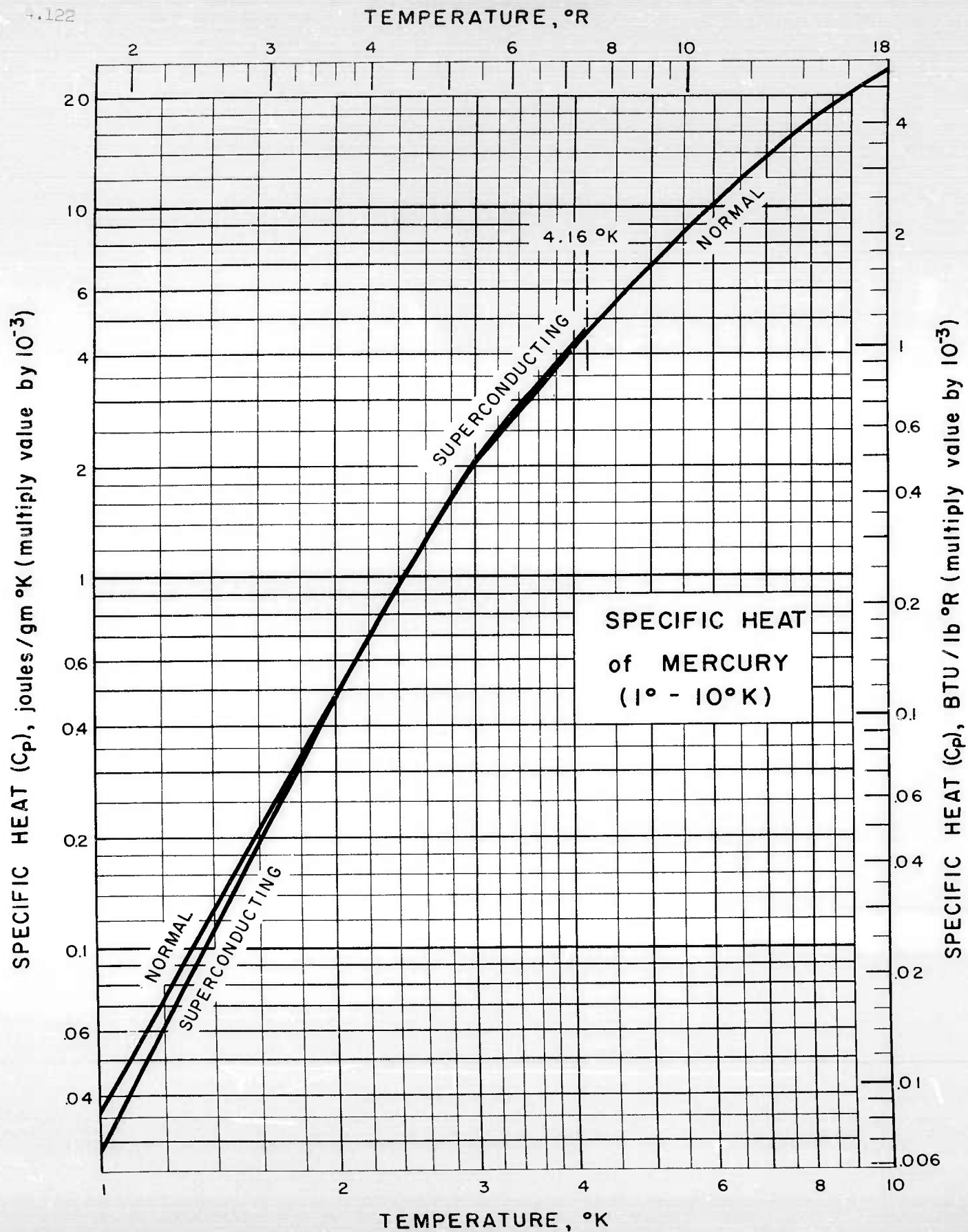
- Busey, R. H. and Giauque, W. F., J. Am. Chem. Soc. 75, 806-9 (1953)
 Misener, A. D., Proc. Roy. Soc. (London) A174, 262 (1940)
 Smith, P. L. and Wolcott, N. M., Phil. Mag. 1, 854-65 (1956)

Other References:

- Barchall, H., Z. Elektrochem. 17, 341 (1911)
 Carpenter, L. G. and Stoodley, L. G., Phil. Mag. (7) 10, 249-65 (1930)
 Koref, F., Ann. Physik 36, 49 (1911)
 Maxwell, E. and Lutes, O. S., Phys. Rev. 95, 333-8 (1954)
 Onnes, H. K. and Holst, G., Commun. Phys. Lab. Univ. Leiden No. 142c (1914)
 Pickard, G. L. and Simon, F., Proc. Phys. Soc. 61, 1-9 (1948)
 Pollitzer, F., Z. Elektrochem. 17, 5 (1911); Z. Elektrochem. 19, 513-18 (1913)
 Russel, A. S., Physik. Z. 13, 59 (1912)
 Simon, F., Ann. Physik 68, 241 (1922); Z. physik. Chem. 107, 279 (1923)

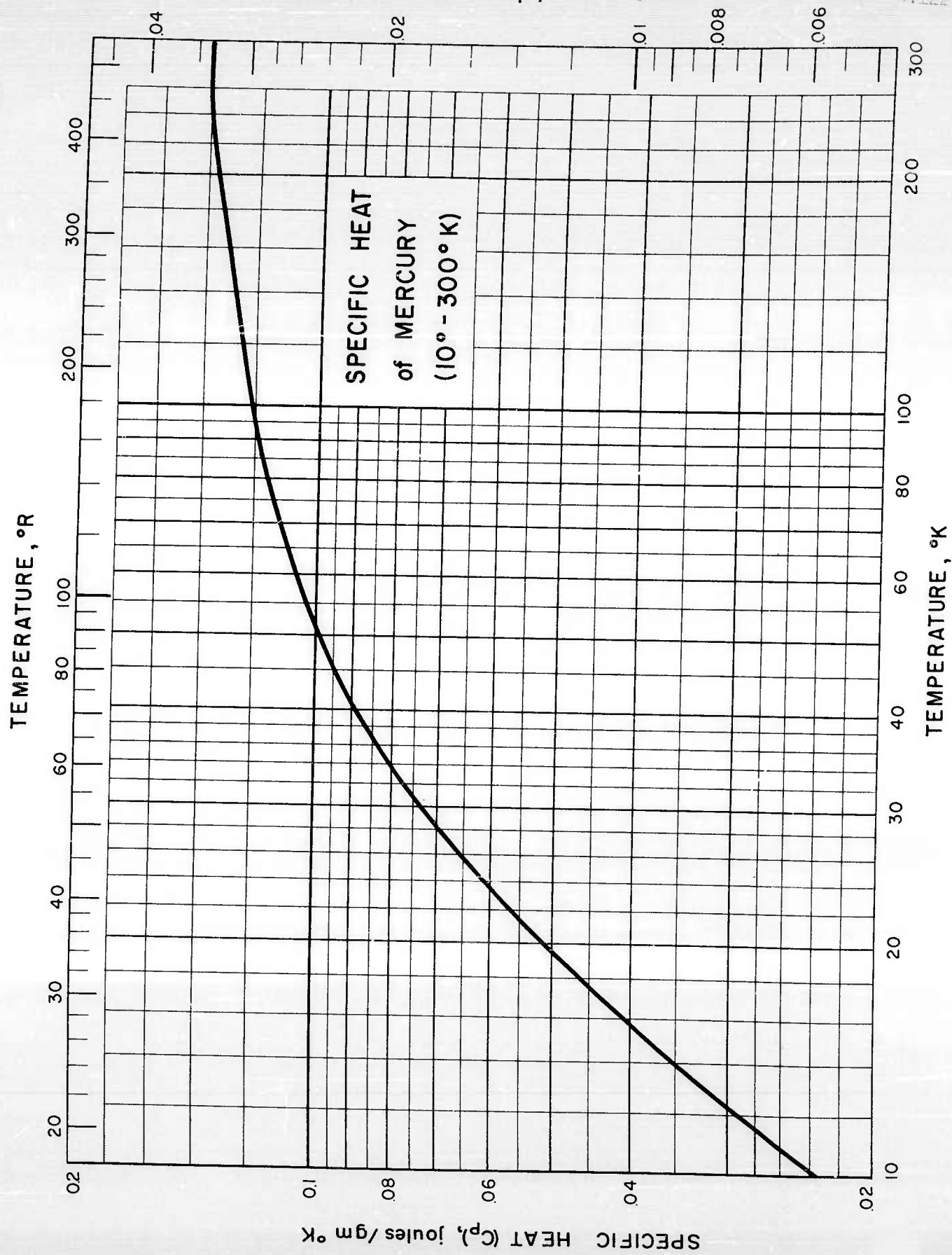
Table of Selected Values

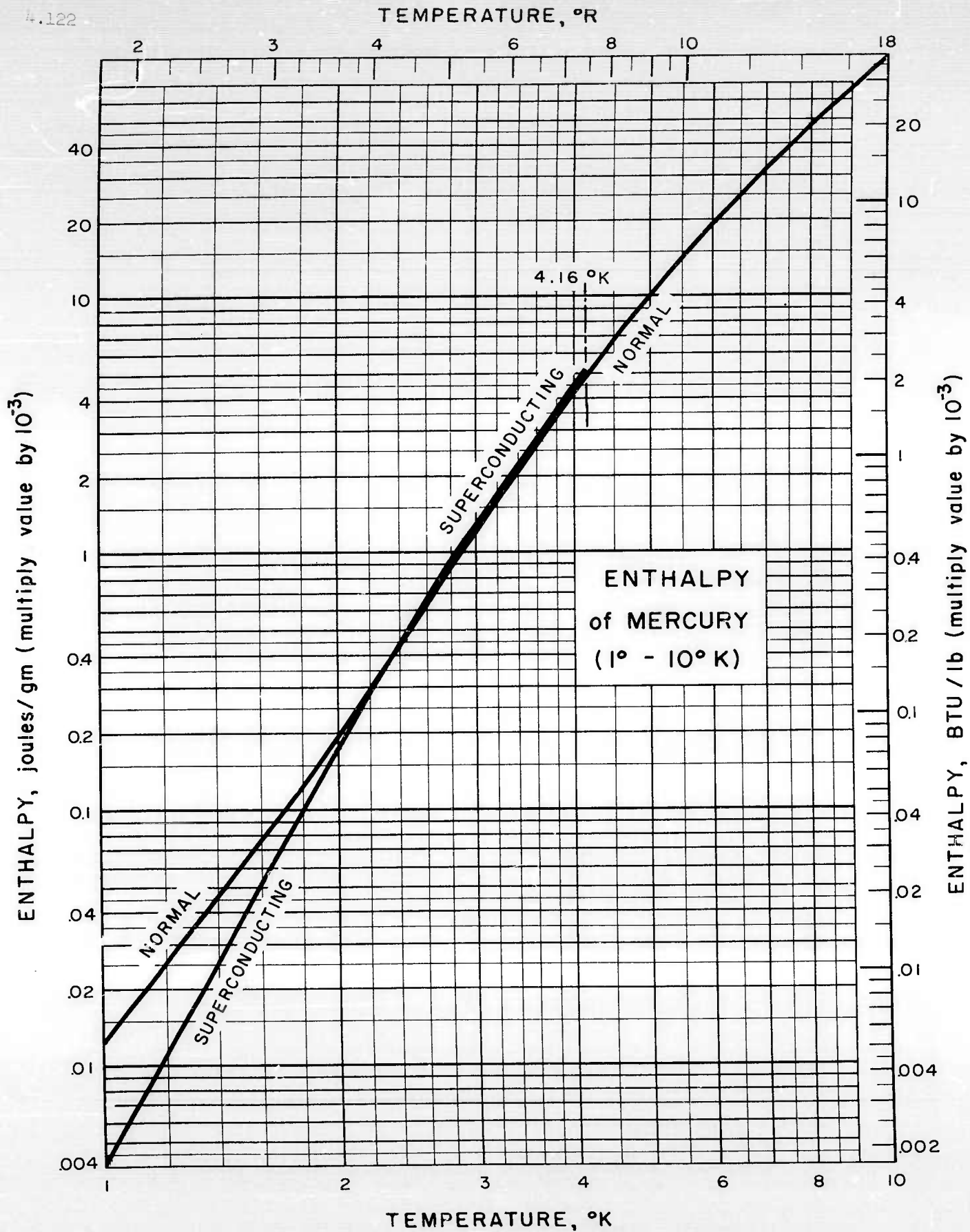
| Temp. °K | C _p , j/gm-°K | | H, j/gm | | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|--------------------------|------------------|------------|------------------|-----------------------|---------------------------|-----------|
| | normal | super-conducting | normal | super-conducting | | | |
| 1 | 0.000 036 | 0.000 029 | 0.000 0125 | 0.000 0042 | 70 | 0.112 | 4.99 |
| 2 | .000 480 | .000 480 | .000 184 | .000 175 | 80 | .116 | 6.13 |
| 3 | .002 07 | .002 09 | .001 37 | .001 38 | 90 | .118 | 7.30 |
| 4 | .004 09 | .004 17 | .004 38 | .004 45 | 100 | .121 | 8.50 |
| 4.16 | .004 63 | .004 71 | .005 07 | .005 16 | 120 | .125 | 11.0 |
| 6 | .010 9 | | .019 4 | | 140 | .128 | 13.5 |
| 8 | .017 5 | | .047 7 | | 160 | .130 | 16.1 |
| 10 | .023 5 | | .088 6 | | 180 | .133 | 18.7 |
| 15 | .038 0 | | .243 | | 200 | .136 | 21.4 |
| 20 | .051 5 | | .468 | | 220 | .139 | 24.1 |
| 25 | .063 3 | | .756 | | 234.3* [↑] S | .142 | 26.1 |
| 30 | .073 7 | | 1.10 | | 234.3* [↓] L | .142 | 37.6 |
| 40 | .089 5 | | 1.92 | | 240 | .142 | 38.4 |
| 50 | .099 3 | | 2.87 | | 260 | .141 | 41.2 |
| 60 | .107 | | 3.90 | | 280 | .140 | 44.0 |
| | | | | | 300 | .139 | 46.8 |

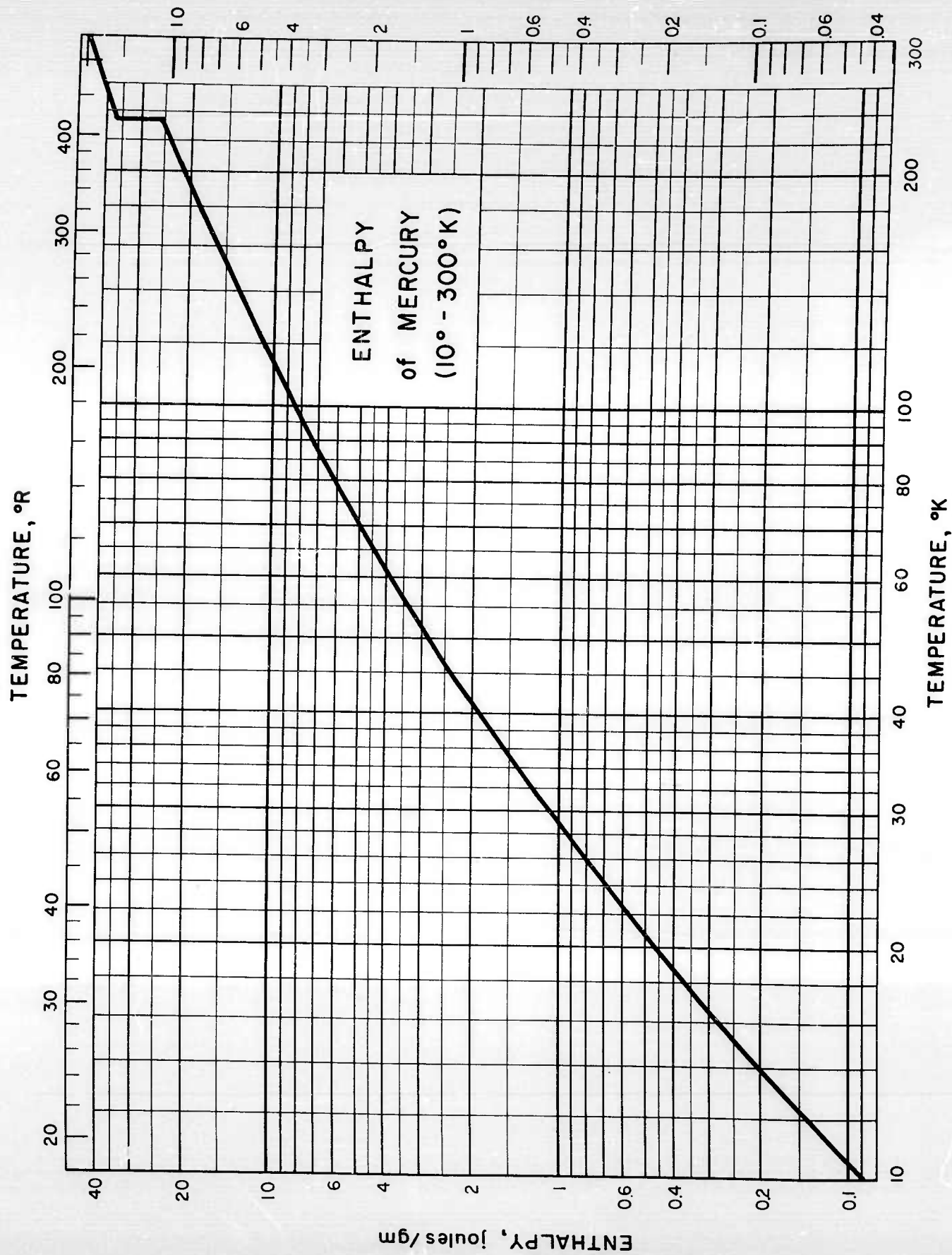


SPECIFIC HEAT (C_p), BTU / lb °R

4.122







SPECIFIC HEAT, ENTHALPY of ZINC

Sources of Data:

- Bronson, H. L. and Wilson, A. J. C., Can. J. Research A14, 181 (1936)
 Clusius, K. and Harteck, P., Z. physik. Chem. 134, 243 (1928)
 Silvidi, A. A. and Daunt, J. G., Phys. Rev. (2) 77, 125 (1950)
 Smith, P. L., Phil. Mag. 46, 744 (1955)

Other References:

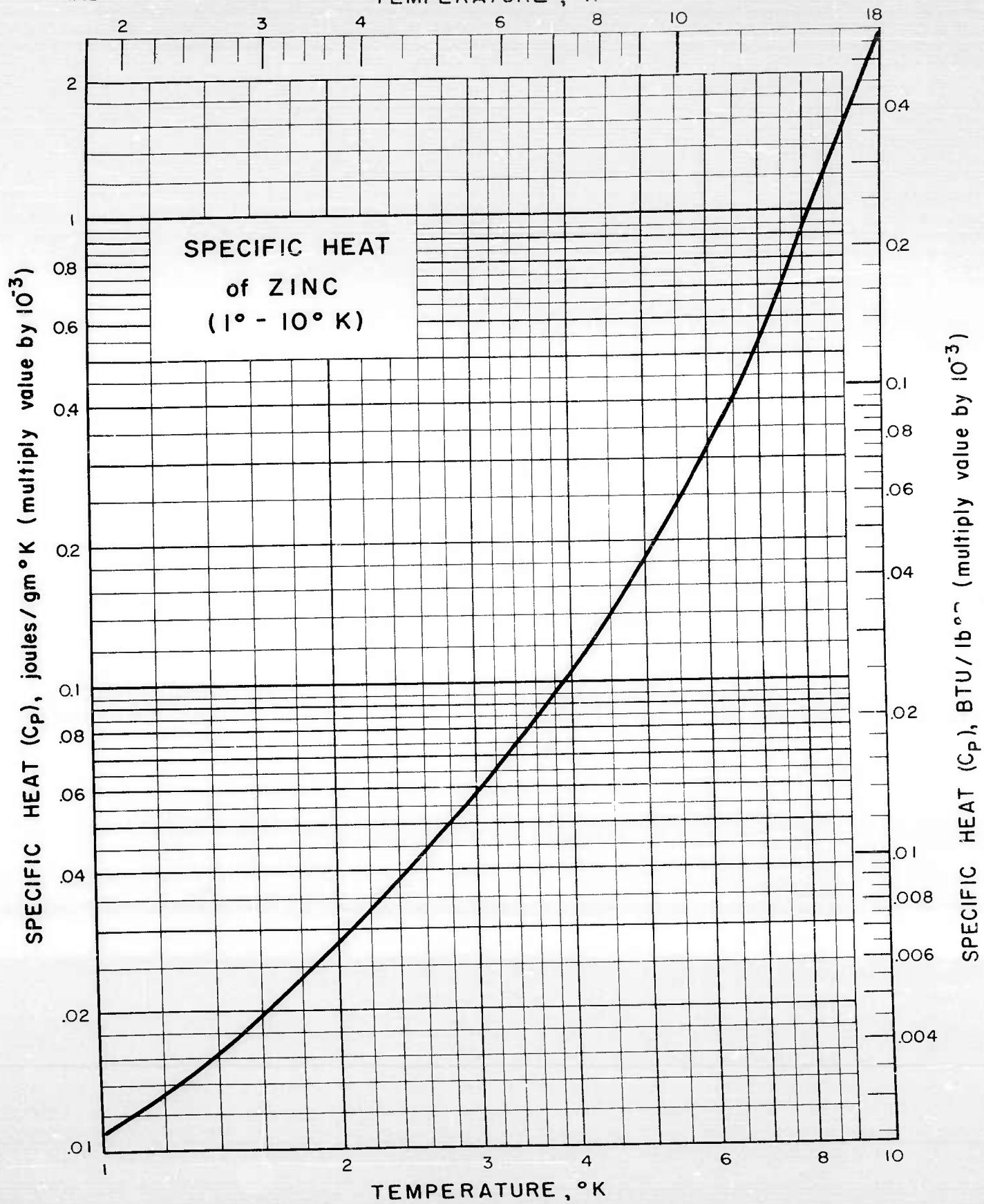
- Eucken, A. and Schwers, F., Verhandl. deut. physik. Ges. 15, 578 (1913)
 Ewald, R., Ann. Physik. (4) 44, 1213 (1914)
 Griffiths, E. G. and Griffiths, E., Phil. Trans. Roy. Soc. London A214, 319 (1914); Proc. Roy. Soc. (London) A90, 557 (1914)
 Keesom, W. H., Pontif. Acad. Sci. Novi Lyncaei, Sci. Nuncius Radiophonius 10, 5 (1932)
 Keesom, W. H. and Kok, J. A., Physica 1, 770 (1934); Proc. Acad. Sci. Amsterdam 37, 377 (1934)
 Keesom, W. H. and Van Den Ende, J. N., Commun. Kamerlingh Onnes Lab. Univ. Leiden 219b, 10 (1932); Proc. Acad. Sci. Amsterdam 35, 143 (1932)
 Koref, F., Ann. Physik. (4) 36, 49 (1911)
 Nernst, W., Ann. Physik (4) 36, 395 (1911); Sitzber. kgl. preuss. Akad. Wiss. 306 (1911)
 Pollitzer, F., Z. Elektrochem. 17, 15 (1911)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
 Schimpff, H., Z. physik. Chem. 71, 257 (1910)
 Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)

Comments:

For $0 < T \leq 6^\circ\text{K}$

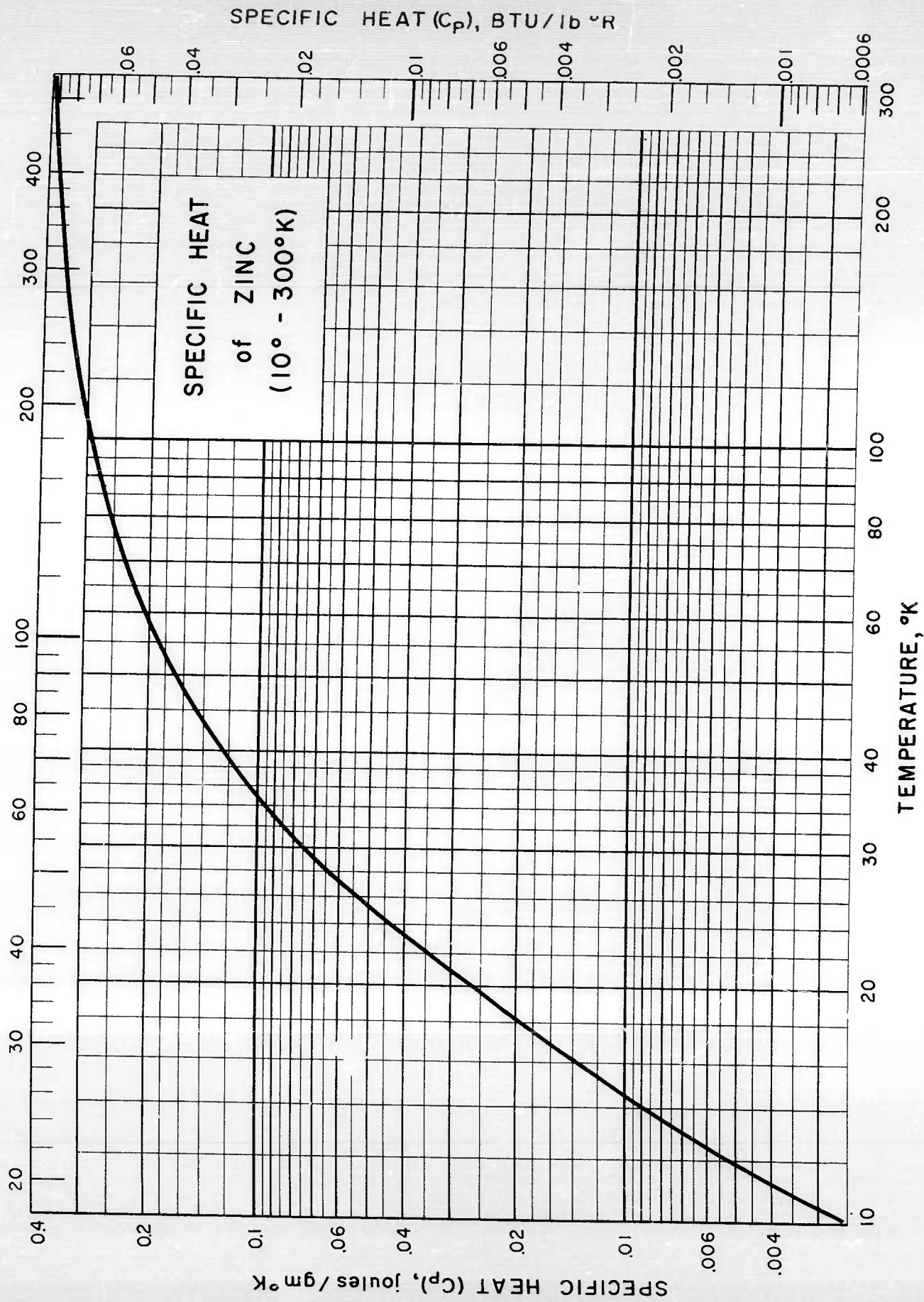
$$C_p = 29.7 (T/304)^3 + 9.8 \times 10^{-6} T \text{ j/gm-}^\circ\text{K}$$

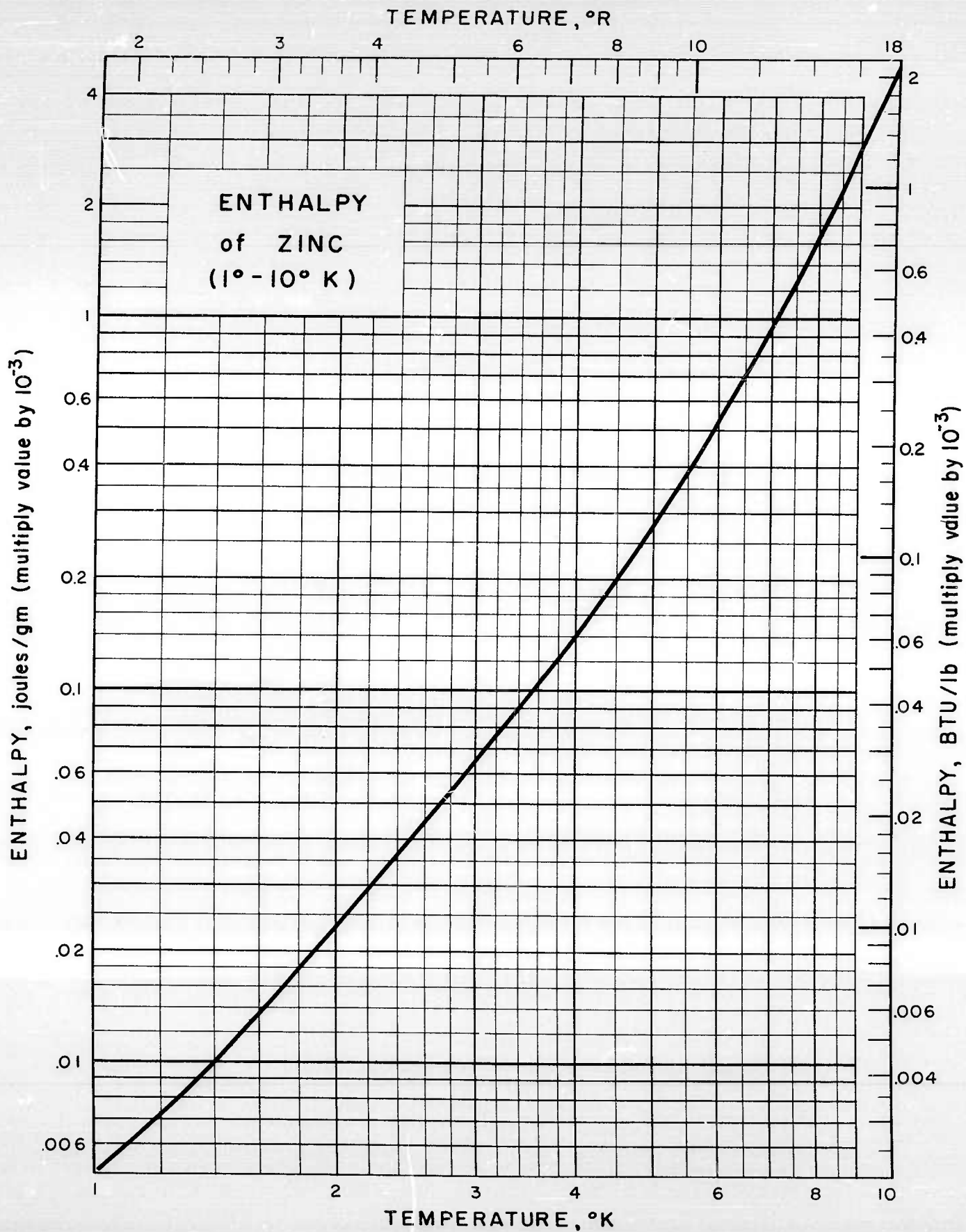
| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|-------------------------|-------------------------|-------------|------------------|-----------|
| 1 | .011 x 10 ⁻³ | .005 x 10 ⁻³ | 70 | .236 | 7.23 |
| 2 | .028 " | .023 " | 80 | .258 | 9.70 |
| 3 | .058 " | .065 " | 90 | .277 | 12.38 |
| 4 | .11 " | .14 " | 100 | .293 | 15.24 |
| 6 | .29 " | .53 " | 120 | .319 | 21.38 |
| 8 | .96 " | 1.6 " | 140 | .337 | 27.96 |
| 10 | 2.5 " | 5.0 " | 160 | .350 | 34.85 |
| 15 | .011 | .034 | 180 | .360 | 41.95 |
| 20 | .026 | .125 | 200 | .367 | 49.22 |
| 25 | .049 | .31 | 220 | .373 | 56.62 |
| 30 | .076 | .62 | 240 | .378 | 64.12 |
| 40 | .125 | 1.62 | 260 | .382 | 71.71 |
| 50 | .171 | 3.11 | 280 | .386 | 79.39 |
| 60 | .208 | 5.01 | 300 | .390 | 87.15 |



4.122

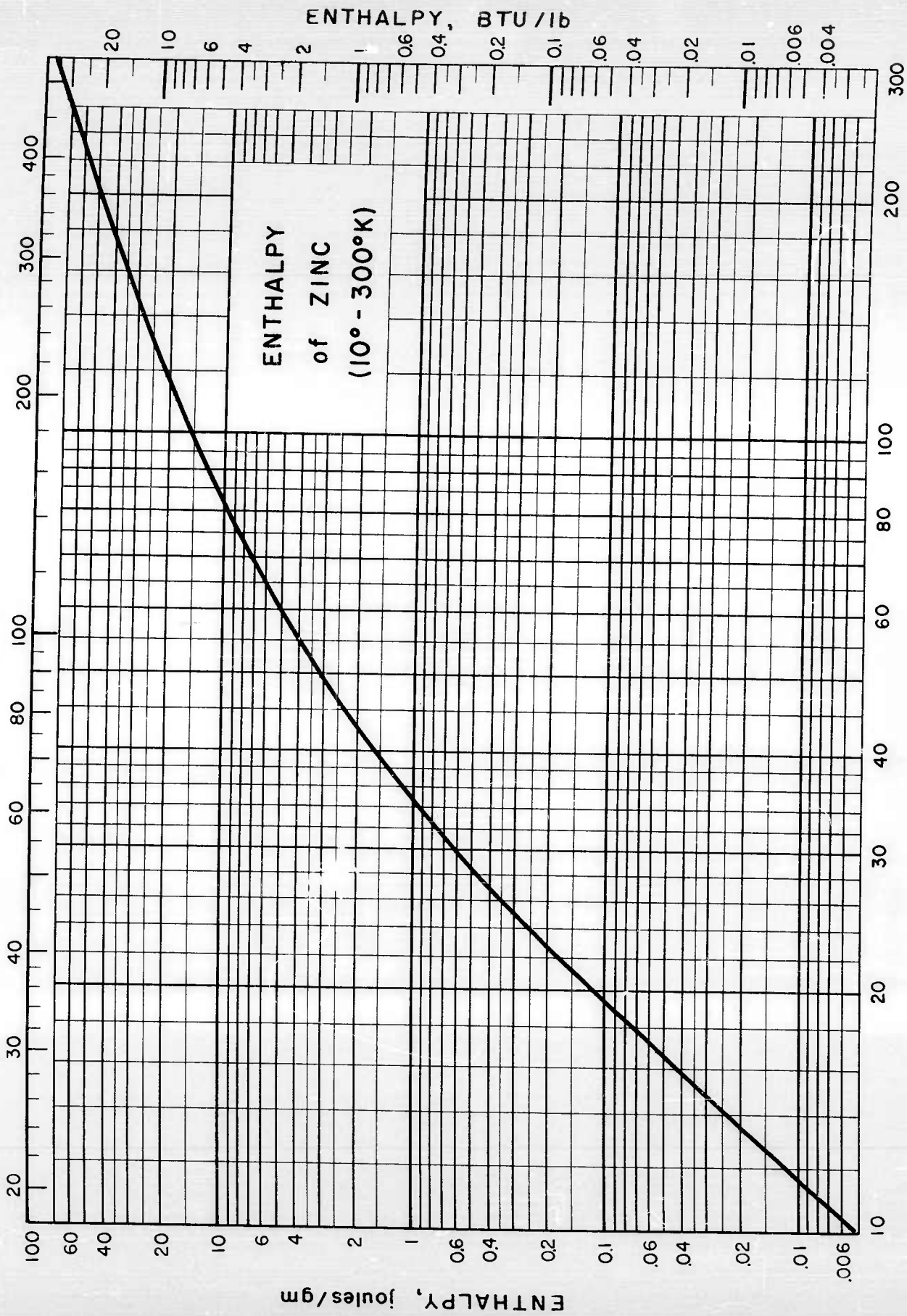
TEMPERATURE, °R





4.122

TEMPERATURE, °R



TEMPERATURE, °K

SPECIFIC HEAT, ENTHALPY of ALUMINUM

Sources of Data:

Glaue, W. F. and Meads, P. F., J. Am. Chem. Soc. 63, 1897-1901 (1941)
 Maier, C. G. and Anderson, C. T., J. Chem. Phys. 2, 513-27 (1934)
 Phillips, N. E., Low Temperature Physics and Chemistry, Univ. Wisconsin Press (1958)

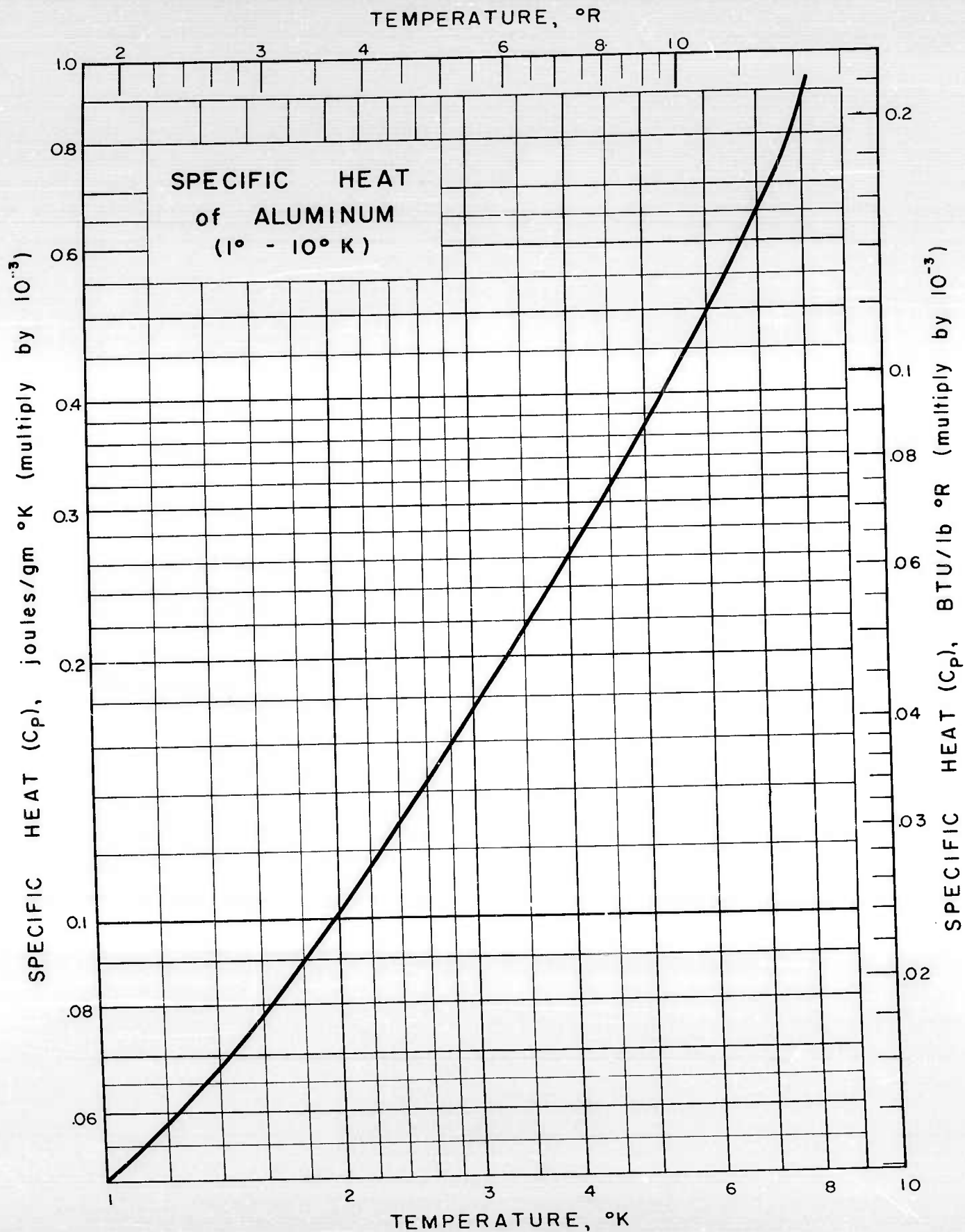
Other References:

Behn, U., Ann. Physik Beiblätter 25, 178 (1901)
 Goodman, B. B., Compt. rend. 244, 2899 (1957)
 Griffiths, E. G. and Griffiths, E., Phil. Trans. Roy. Soc. London A90, 557 (1914)
 Kok, J. A. and Keesom, W. H., Physica 4, 835 (1937)
 Koref, F., Ann. Physik (4) 36, 49 (1911)
 Nernst, W., Ann. Physik (4) 36, 395 (1911)
 Nernst, W. and Lindemann, F. A., Z. Elektrochem. 17, 817 (1911)
 Nernst, W. and Schwers, F., Sitzber. kgl. preuss. Akad. Wiss. 355 (1914)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
 Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)
 Tilden, W. A., Proc. Roy. Soc. (London) 71, 220 (1903)

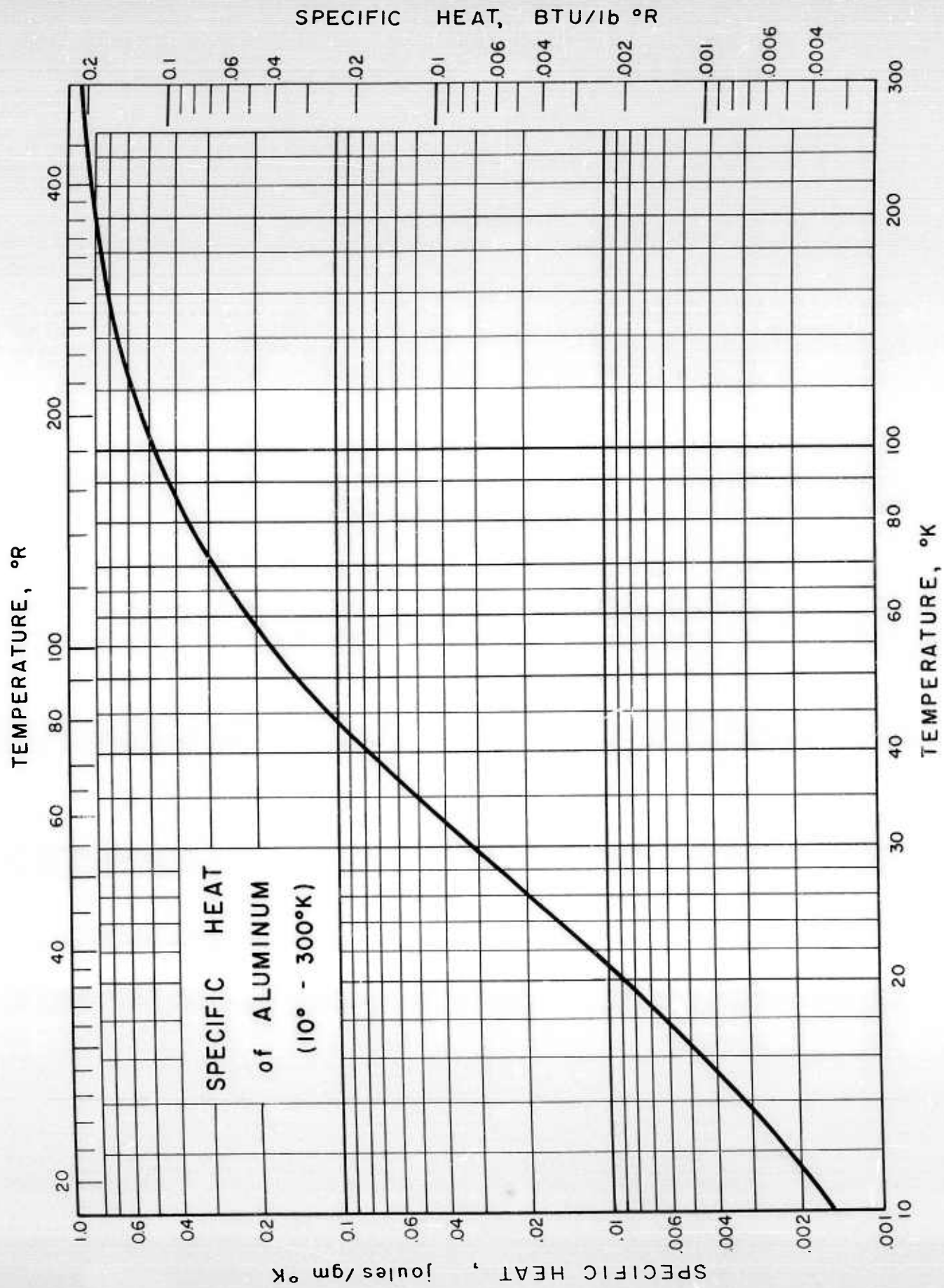
Table of Selected Values

| Temp. °K | C _p j/gm-°K | H j/gm | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|-------------|---------------------------|-----------|
| 1 | 0.000 10* | | 60 | 0.214 | 3.64 |
| 1 | .000 051 | 0.000 025 | 70 | .287 | 6.15 |
| 2 | .000 108 | .000 105 | 80 | .357 | 9.37 |
| 3 | .000 176 | .000 246 | 90 | .422 | 13.25 |
| 4 | .000 261 | .000 463 | 100 | .481 | 17.76 |
| 6 | .000 50 | .001 21 | 120 | .580 | 28.4 |
| 8 | .000 88 | .002 6 | 140 | .654 | 40.7 |
| 10 | .001 4 | .004 9 | 160 | .713 | 54.4 |
| 15 | .004 0 | .018 | 180 | .760 | 69.2 |
| 20 | .008 9 | .048 | 200 | .797 | 84.8 |
| 25 | .017 5 | .112 | 220 | .826 | 101.0 |
| 30 | .031 5 | .232 | 240 | .849 | 117.8 |
| 35 | .051 5 | .436 | 260 | .869 | 135.0 |
| 40 | .077 5 | .755 | 280 | .886 | 152.5 |
| 50 | .142 | 1.85 | 300 | .902 | 170.4 |

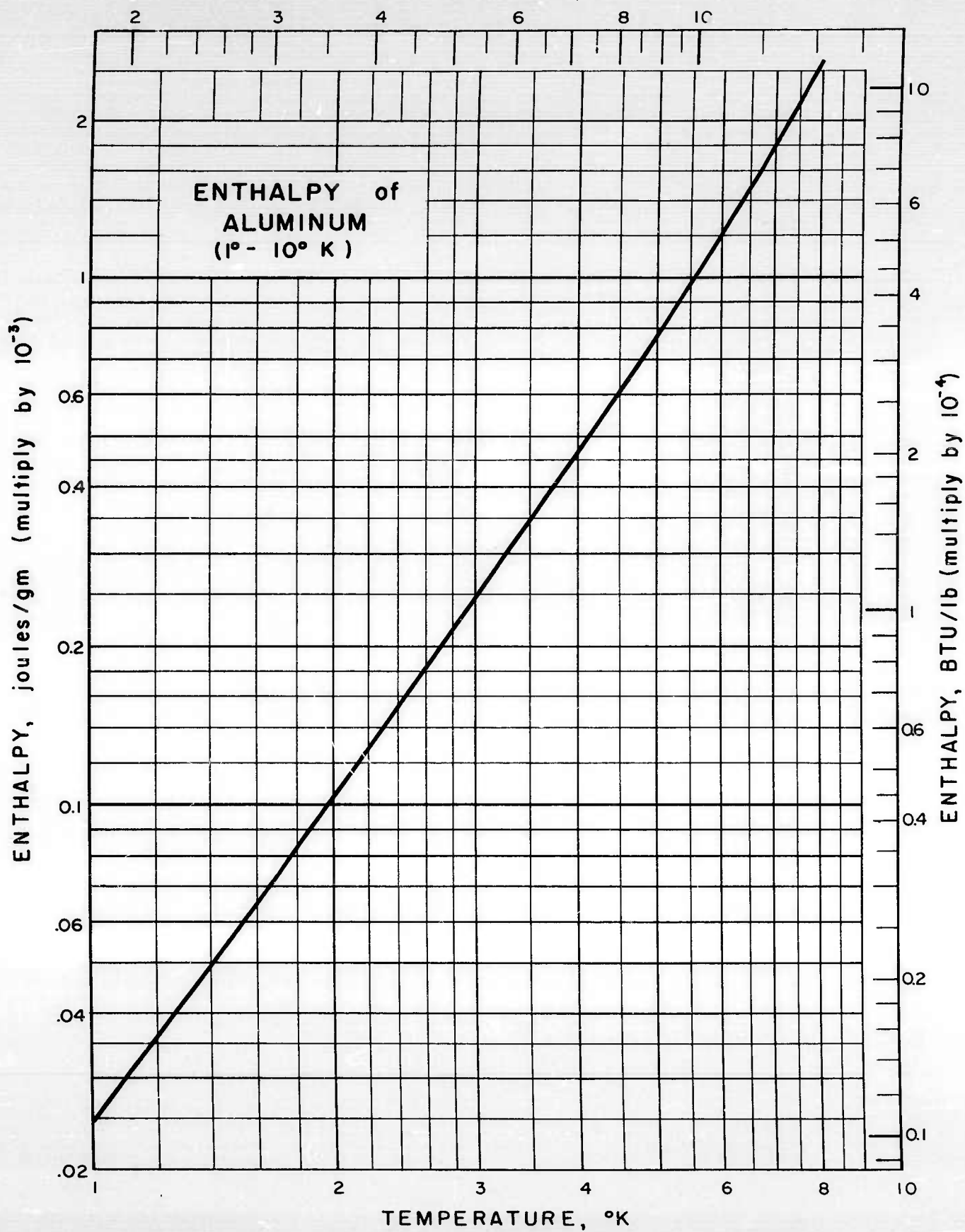
* Superconducting

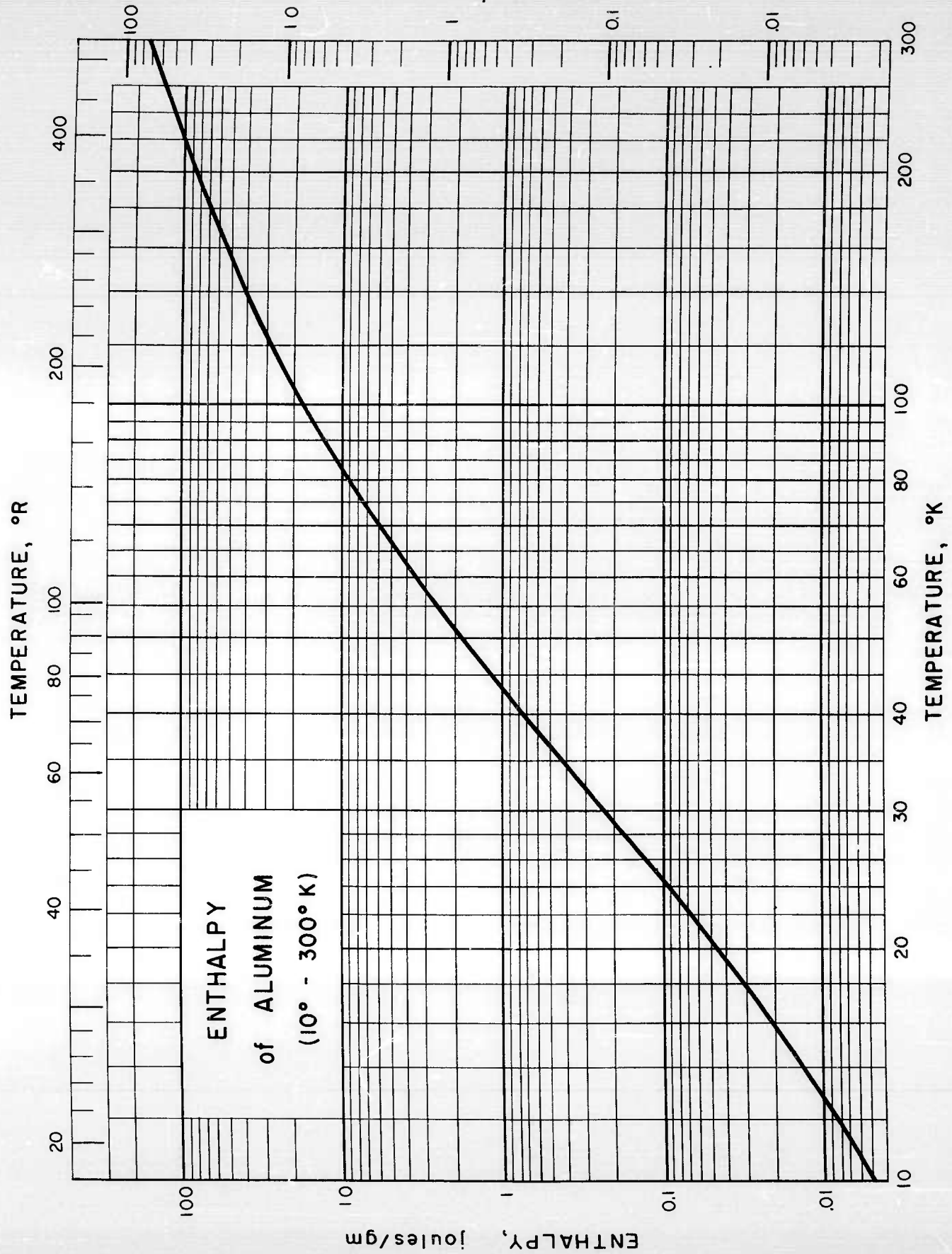


4.132



TEMPERATURE, °R





SPECIFIC HEAT and ENTHALPY of INDIUM

Sources of Data:Clement, J. R. and Quirmell, E. H., Phys. Rev. 92, 258 (1953)Clusius, K. and Schachinger, L., Z. Naturforsch. A7, 185 (1952)Other References:Clement, J. R. and Quinnell, E. H., Nat. Bur. Standards Circ. 519, 89 (1952) and Phys. Rev. 79, 1028 (1950)

Table of Selected Values

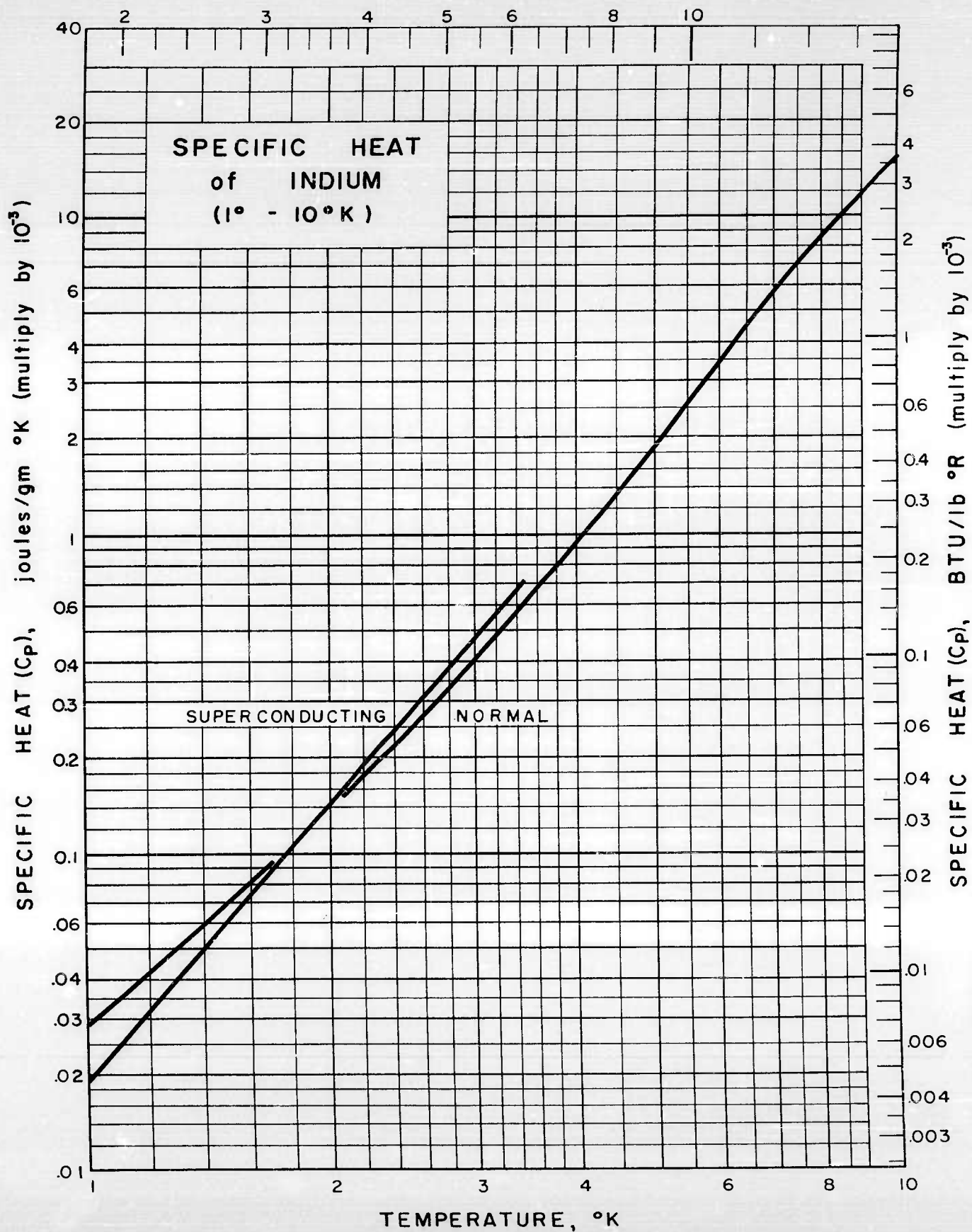
| T °K | Cp j/gm-°K | H j/gm | T °K | Cp j/gm-°K | H j/gm |
|---------|---------------|-----------|---------|---------------|-----------|
| 1 | 0.000 029 | 0.000 011 | 60 | 0.176 | 5.73 |
| 1 | .000 019* | .000 006* | 70 | .186 | 7.53 |
| 2 | .000 138 | .000 085 | 80 | .193 | 9.42 |
| 2 | .000 141* | .000 073* | 90 | .198 | 11.38 |
| 3 | .000 410 | .000 341 | 100 | .203 | 13.39 |
| 3 | .000 464* | .000 357* | 120 | .211 | 17.53 |
| 3.40** | .000 584 | .000 537 | 140 | .217 | 21.81 |
| 3.40 | .000 669* | .000 581* | 160 | .220 | 26.18 |
| 4 | .000 95 | .000 99 | 180 | .223 | 30.61 |
| 6 | .003 59 | .005 20 | 200 | .225 | 35.08 |
| 8 | .008 55 | .017 0 | 220 | .227 | 39.59 |
| 10 | .015 5 | .040 8 | 240 | .229 | 44.14 |
| 15 | .036 7 | .170 | 260 | .230 | 48.72 |
| 20 | .060 8 | .413 | 280 | .232 | 53.34 |
| 25 | .085 7 | .778 | 300 | .233 | 58.0 |
| 30 | .108 | 1.265 | | | |
| 40 | .141 | 2.52 | | | |
| 50 | .162 | 4.04 | | | |

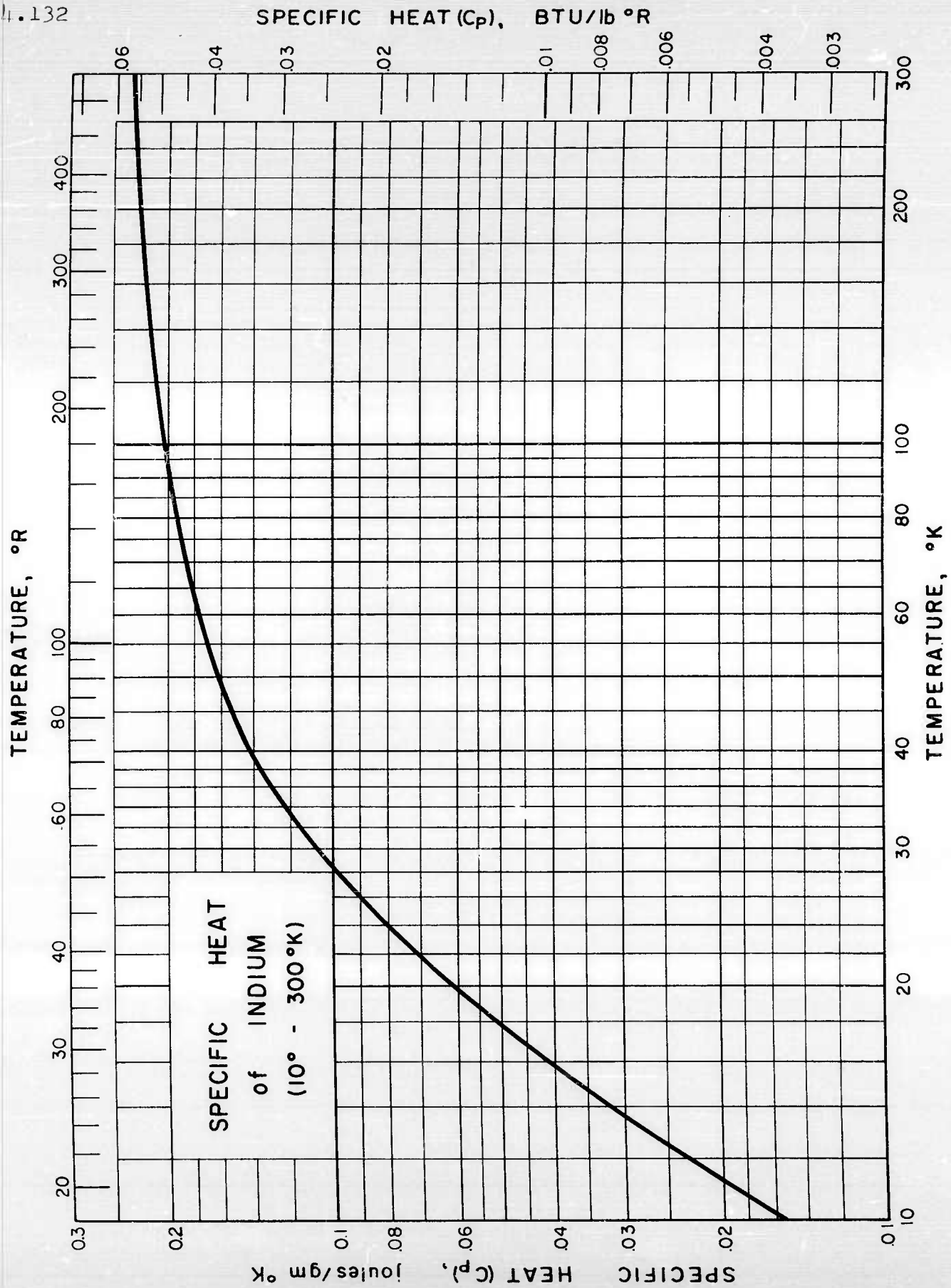
* Superconducting

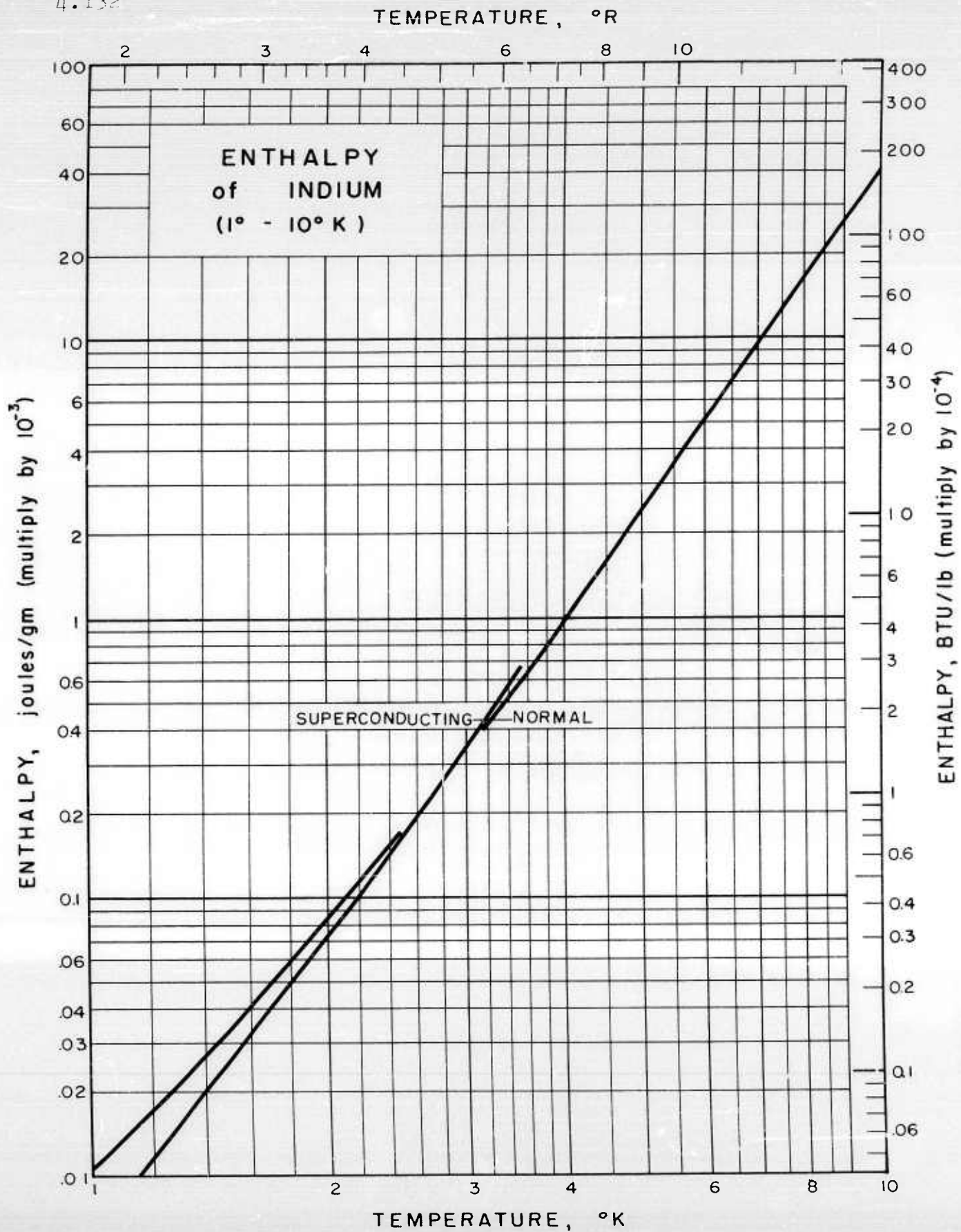
** Superconducting transition temperature

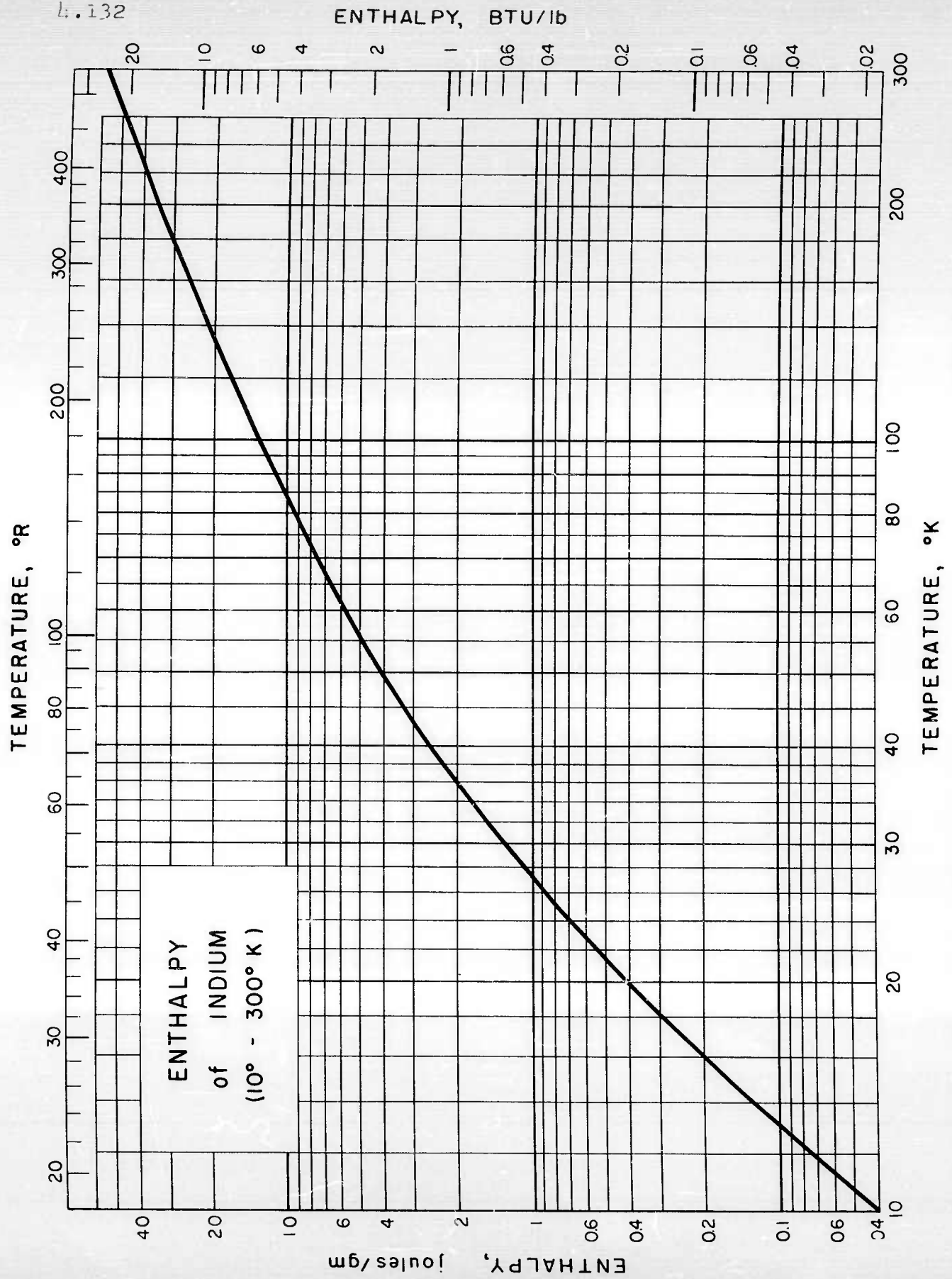
RJC Issued: 6-11-59

Revised: 5-20-60









SPECIFIC HEAT, ENTHALPY of TITANIUM

Sources of Data:

Aven, M. H., Craig, R. S., Waite, T. R. and Wallace, W. E.,
Phys. Rev. 102, 1263 (1956)

Kothen, C. W. and Johnston, H. L., J. Am. Chem. Soc. 75, 3101
(1953)

Wolcott, N. M., Conf. de Physique des Basses Temperatures, Paris
(1955)

Other References:

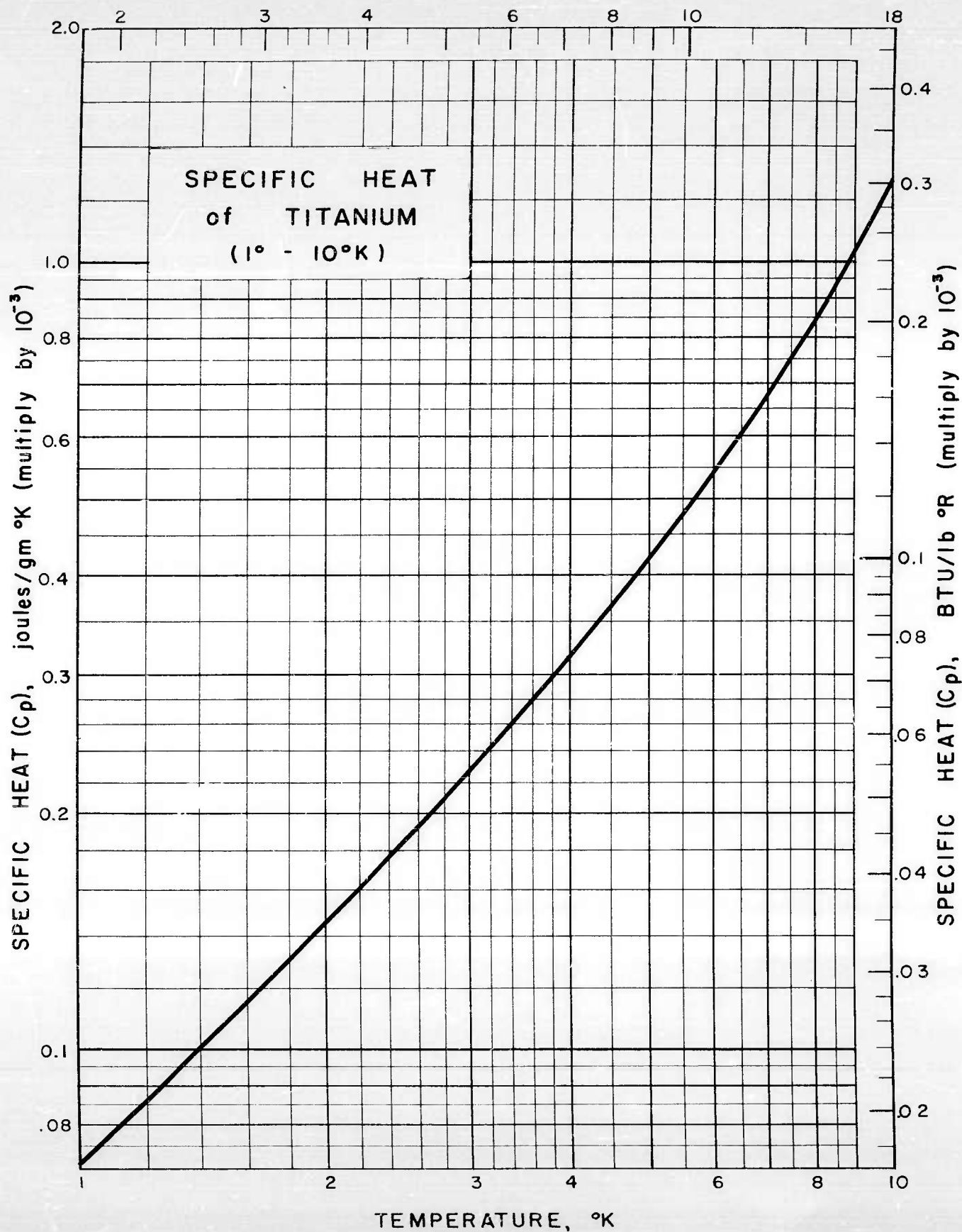
Estermann, I., Friedberg, S. A. and Goldman, J. E., Phys. Rev.
87, 582 (1952)

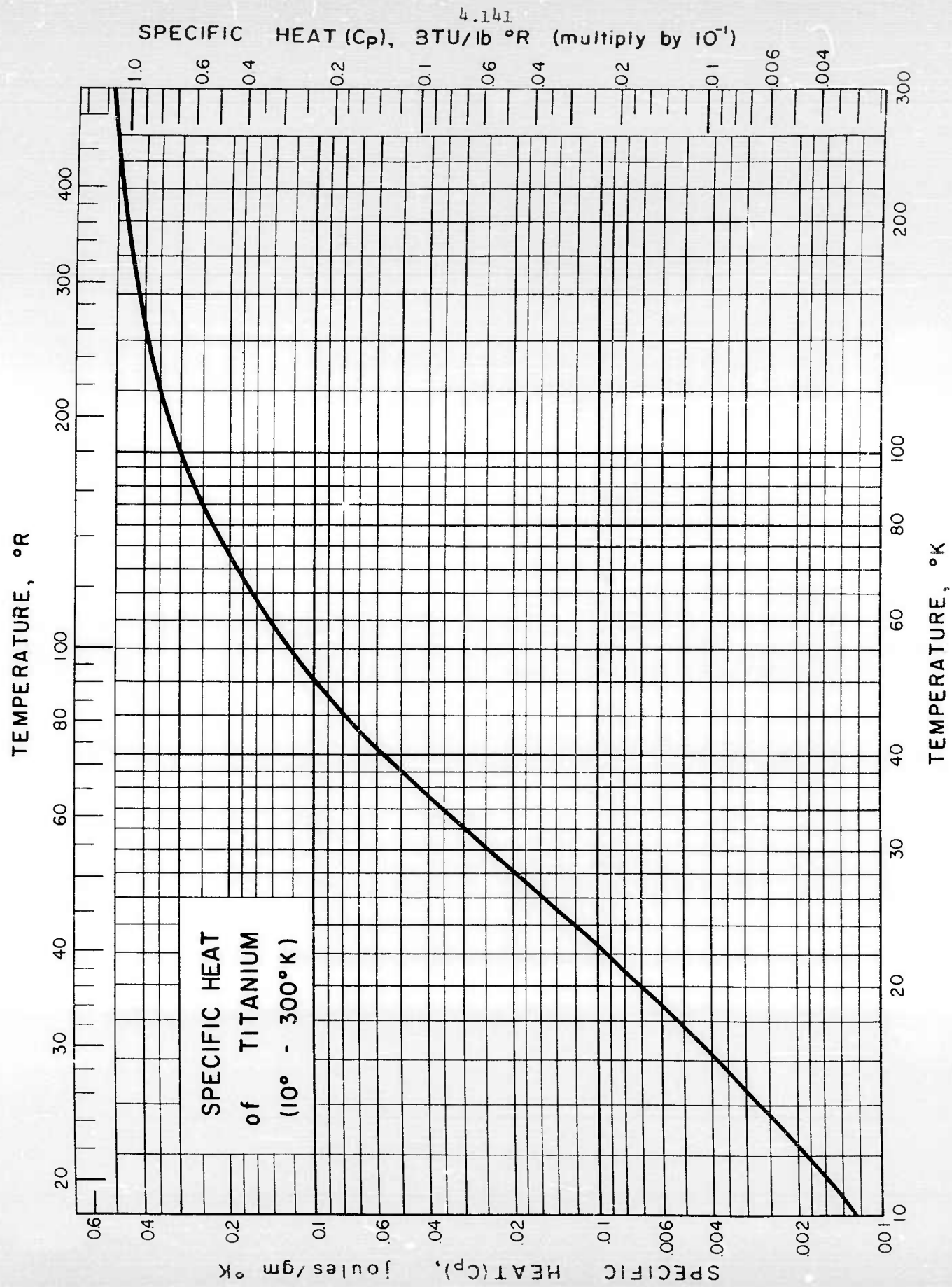
Kelley, K. K., Ind. Eng. Chem. 36, 865 (1944)

Table of Selected Values

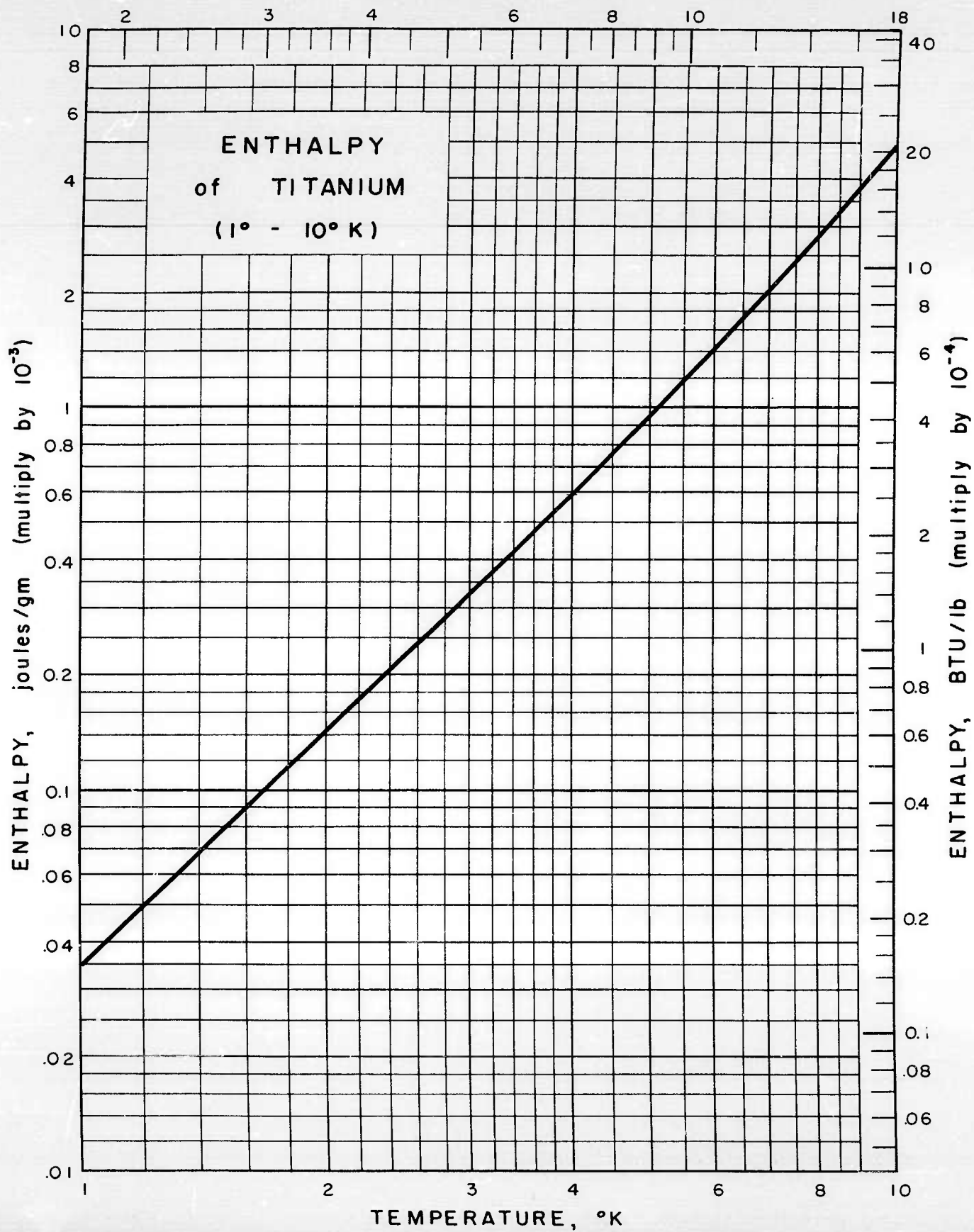
| Temp. °K | C _p j/gm-°K | H j/gm | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|-------------|---------------------------|-----------|
| 1 | 0.000 071 | 0.000 035 | 70 | 0.189 | 4.27 |
| 2 | .000 146 | .000 143 | 80 | .230 | 6.37 |
| 3 | .000 226 | .000 329 | 90 | .267 | 8.86 |
| 4 | .000 317 | .000 599 | 100 | .300 | 11.69 |
| 6 | .000 54 | .001 45 | 120 | .352 | 18.24 |
| 8 | .000 84 | .002 81 | 140 | .391 | 25.69 |
| 10 | .001 26 | .004 89 | 160 | .422 | 33.84 |
| 15 | .003 3 | .015 6 | 180 | .446 | 42.54 |
| 20 | .007 0 | .040 | 200 | .465 | 51.66 |
| 25 | .013 4 | .090 | 220 | .480 | 61.11 |
| 30 | .024 5 | .182 | 240 | .493 | 70.84 |
| 40 | .057 1 | .581 | 260 | .504 | 80.82 |
| 50 | .099 2 | 1.358 | 280 | .514 | 91.01 |
| 60 | .146 7 | 2.592 | 300 | .522 | 101.39 |

4.141
TEMPERATURE, °R

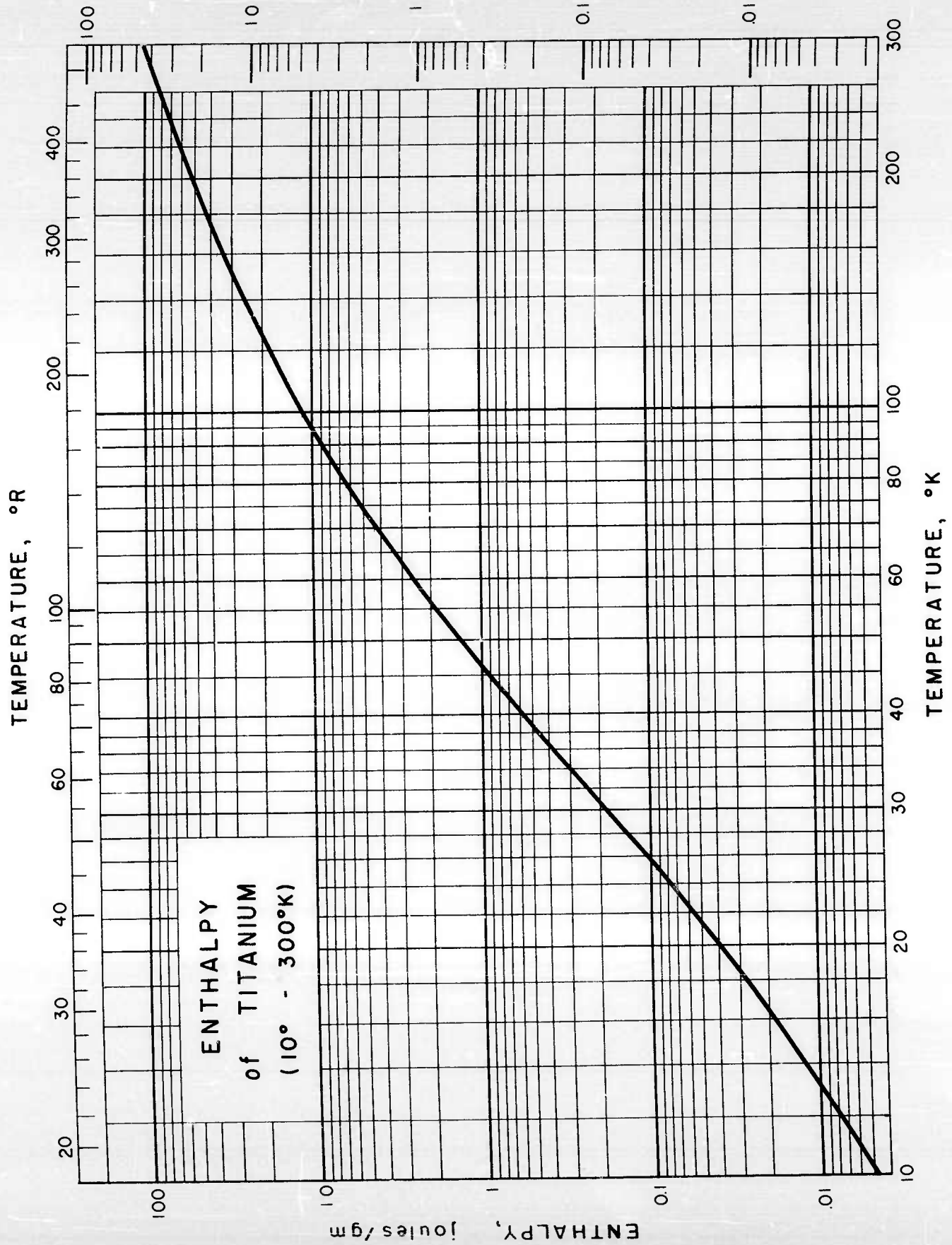




4.141
TEMPERATURE, °R



4.141
ENTHALPY, BTU/lb



SPECIFIC HEAT, ENTHALPY of ACTIVATED CHARCOAL

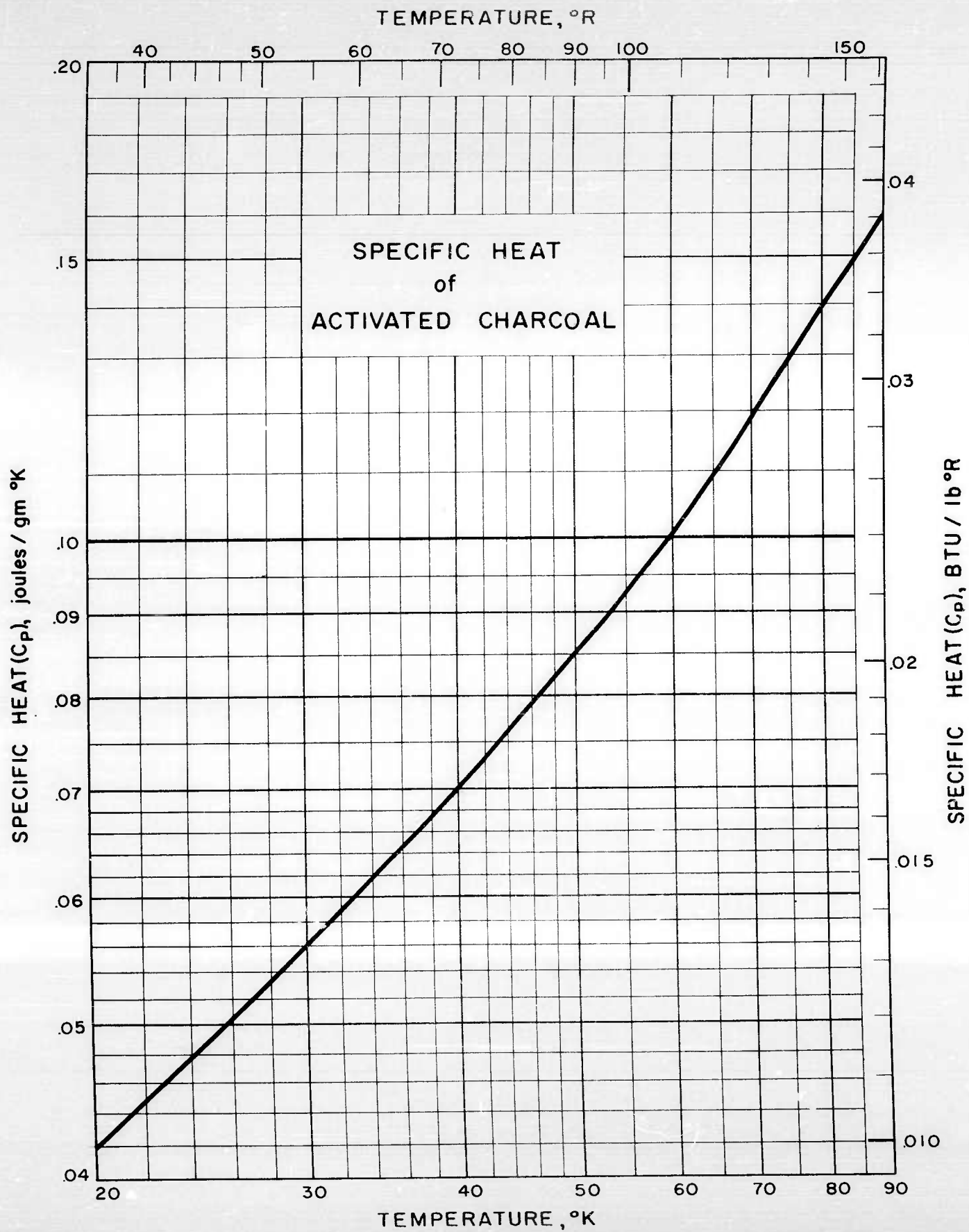
Source of Data:Simon, F. and Swain, R. C., Z. physik. Chem. B28, 189-98 (1935)Comments:

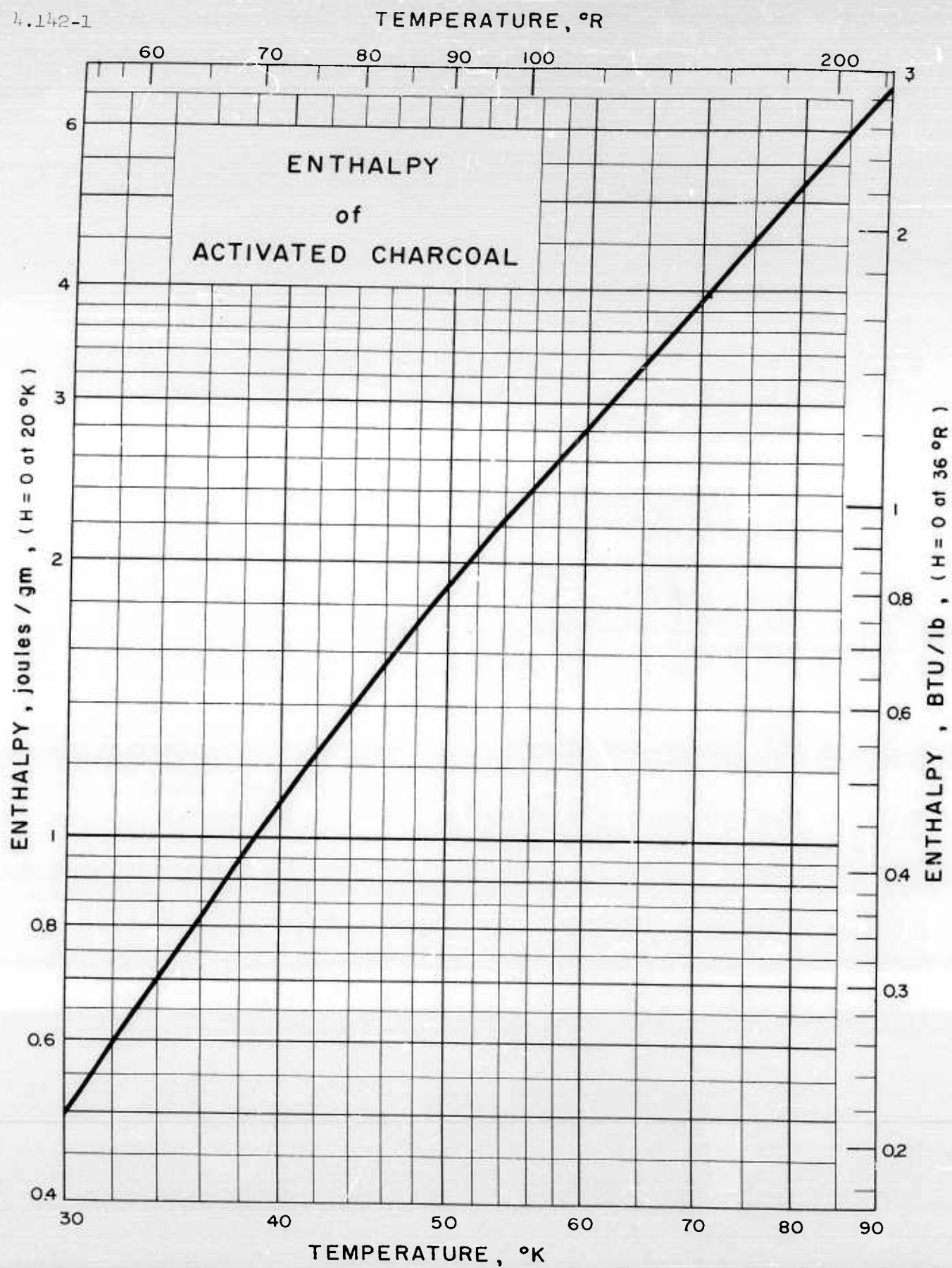
The values in the table below do not represent precise measurements and were made on a sample not fully characterized. The values are much higher than those for graphite. Since activated charcoal varies in structure and area, one may infer that the specific heat might also vary considerably from sample to sample.

Table of Selected Values

| Temp. °K | C _p j/gm-°K | H-H ₂ O j/gm |
|-------------|---------------------------|----------------------------|
| 20 | 0.042 | |
| 30 | .056 | 0.49 |
| 40 | .070 | 1.1 |
| 50 | .087 | 1.9 |
| 60 | .10 | 2.8 |
| 70 | .12 | 3.9 |
| 80 | .14 | 5.2 |
| 90 | .16 | 6.7 |

JJG/JRC Issued: 9/2/59
Revised: 1/20/60





SPECIFIC HEAT, ENTHALPY of CARBON (GRAPHITE)

Sources of Data:Keesom, P. H. and Pearlman, N.; Phys. Rev. 99, 1119-24 (1955)De Sorbo, W. and Tyler, W., J. Chem. Phys. 21, 1660-3 (1953)Other References:Bergenlid, V., Hill, R. W., Webb, F. J. and Wilks, J., Phil. Mag. 45, 851-4 (1954)Dewar, J., Proc. Roy. Soc. (London) A76, 325 (1904)

Ewald, R., Ann. phys. (4) 1213 (1914)

Jacobs, C. J. and Parks, G. S., J. Am. Chem. Soc. 56, 1513 (1934)Koref, F., Ann. Phys. (4) 36, 49 (1911)Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)Comments:For $0 < T < 2^\circ\text{K}$

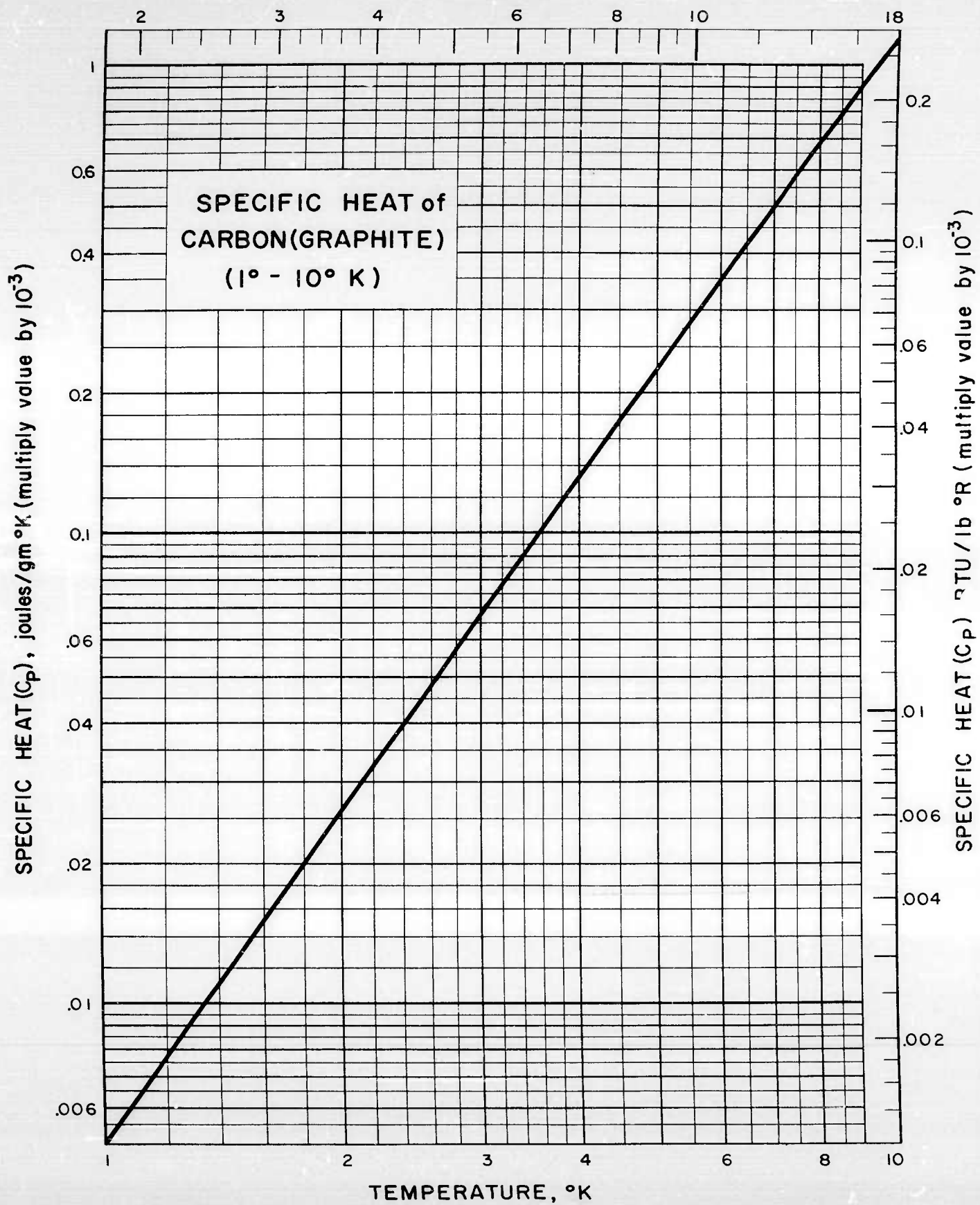
$$C_p = 162 (T/391)^3 + 2.6 \times 10^{-6} T \text{ j/gm-}^\circ\text{K}$$

| Temp. °K | C _p j/gm-°K | H j/gm | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|-------------|---------------------------|-----------|
| 1 | .000 005 | .000 002 | 70 | .077 | 1.87 |
| 2 | .000 027 | .000 016 | 80 | .097 | 2.74 |
| 3 | .000 070 | .000 062 | 90 | .118 | 3.81 |
| 4 | .000 144 | .000 168 | 100 | .140 | 5.10 |
| 6 | .000 33 | .000 61 | 120 | .188 | 8.37 |
| 8 | .000 64 | .001 56 | 140 | .240 | 12.65 |
| 10 | .001 14 | .003 3 | 160 | .296 | 18.0 |
| 15 | .003 3 | .014 2 | 180 | .355 | 24.5 |
| 20 | .006 3 | .038 | 200 | .414 | 32.2 |
| 25 | .010 3 | .079 | 220 | .474 | 41.1 |
| 30 | .015 5 | .143 | 240 | .535 | 51.2 |
| 40 | .027 | .36 | 260 | .595 | 62.5 |
| 50 | .042 | .70 | 280 | .656 | 75.0 |
| 60 | .058 | 1.20 | 300 | .716 | 88.7 |

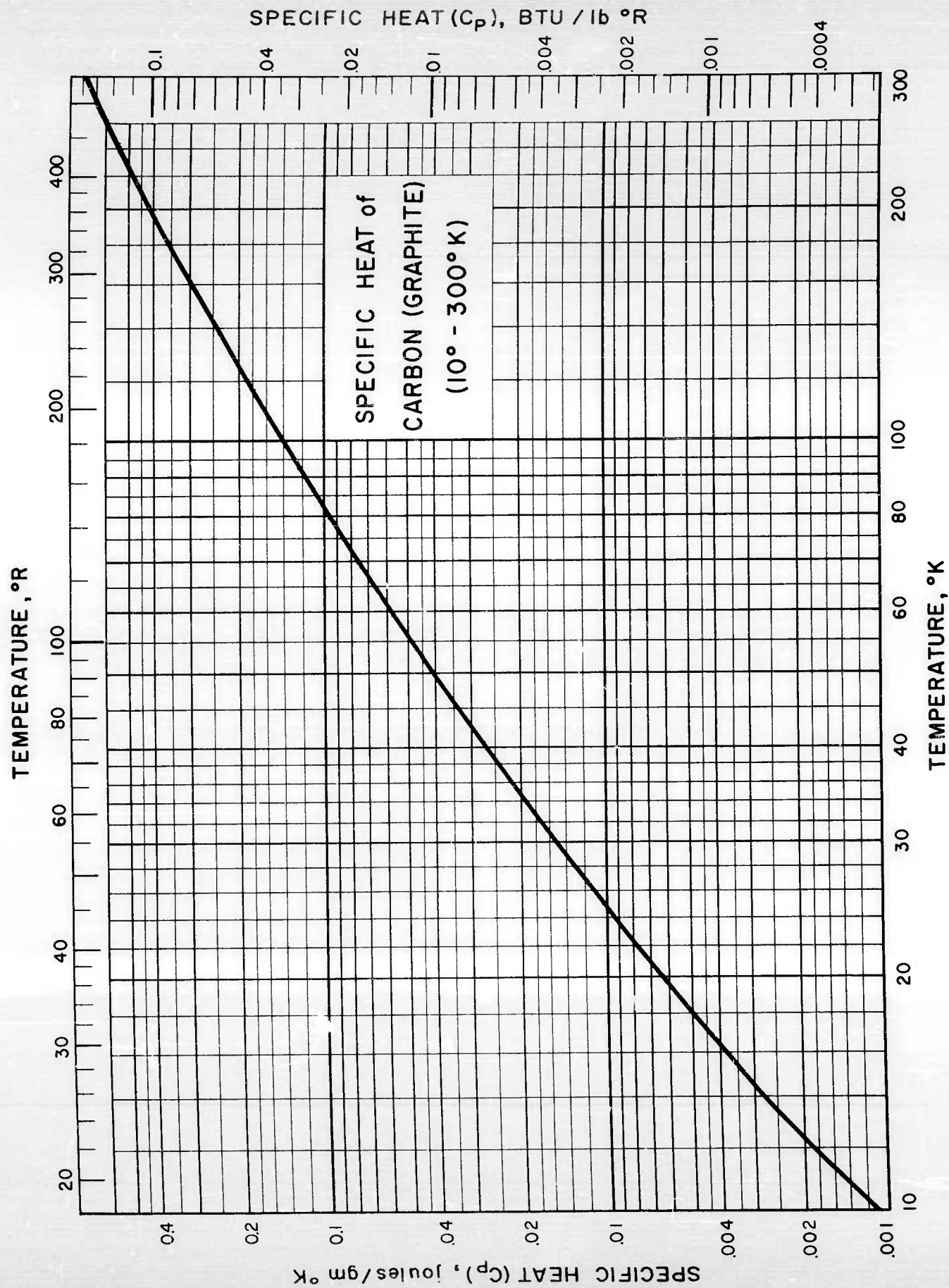
RJC/JJG Issued: 12-16-59
Revised: 5-20-60

4.142-1

TEMPERATURE, °R

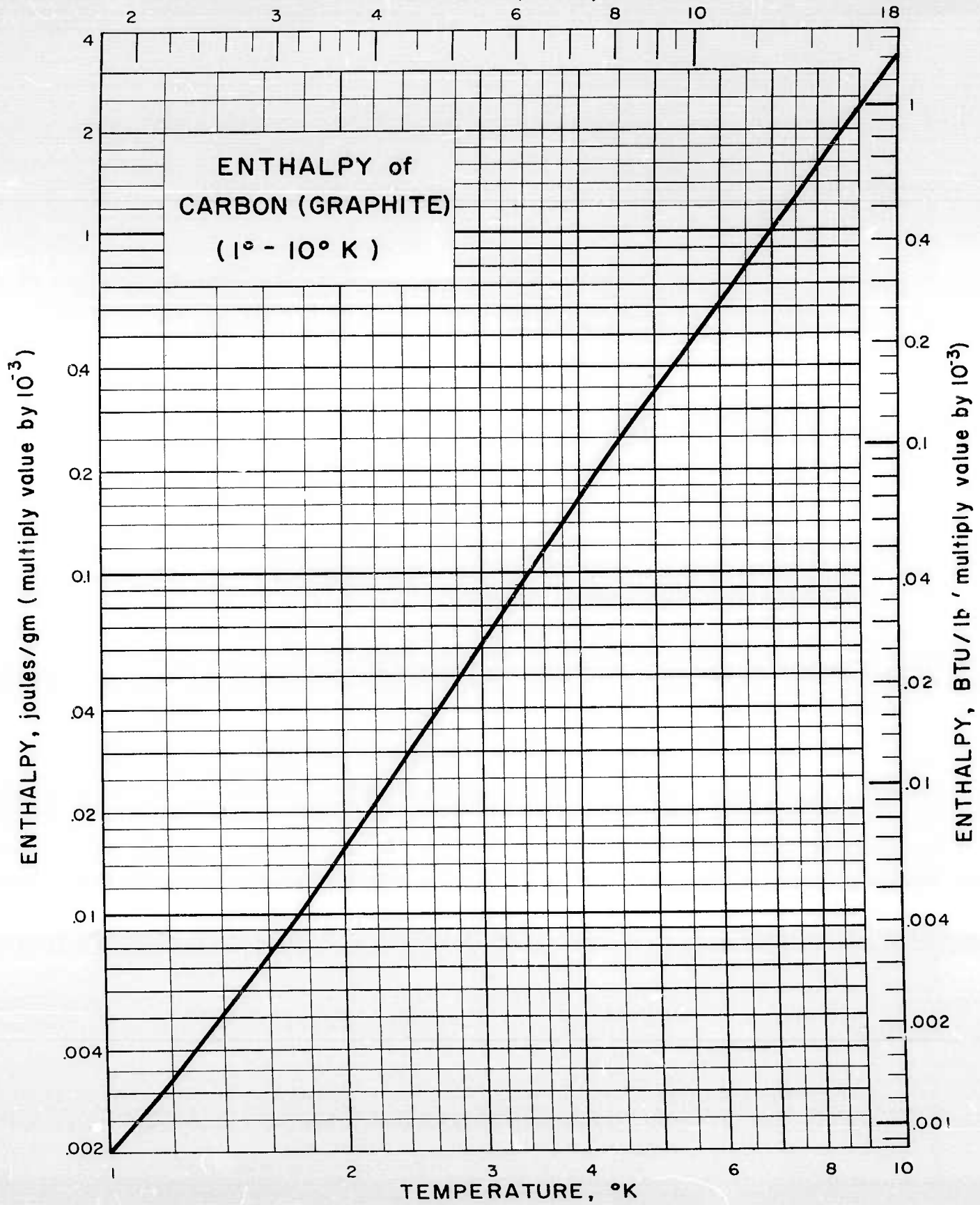


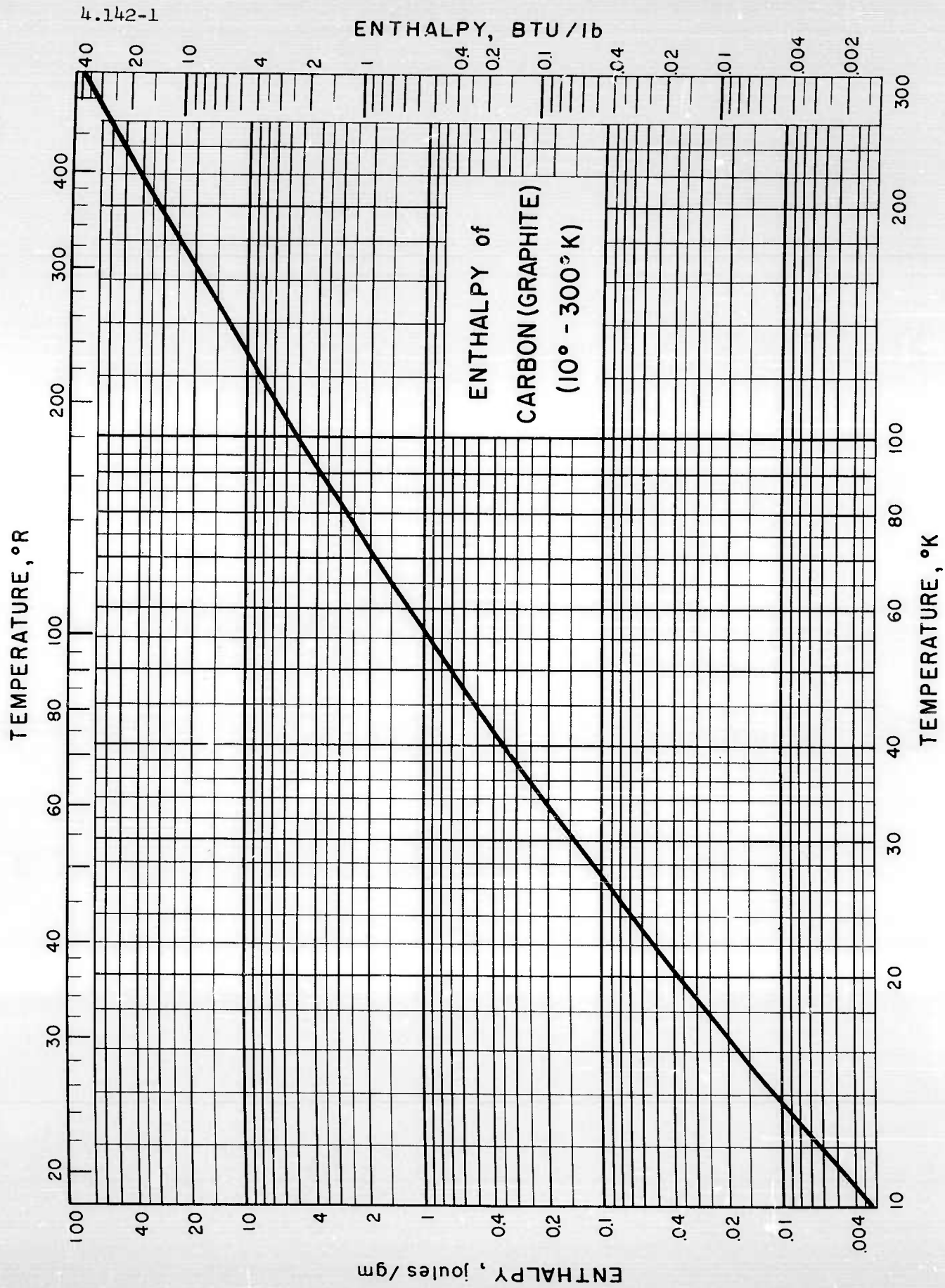
4.142-1



4.142-1

TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of DIAMOND

Sources of Data:

- Burk, D. L. and Friedberg, S. A., Phys. Rev. 111, 1275-82 (1958)
 Desnoyers, J. E. and Morrison, J. A., Phil. Mag. 3, 42-8 (1958)
 De Sorbo, W., J. Chem. Phys. 21, 876 (1953)

Other References:

- Berman, R. and Poulter, J., J. Chem. Phys. 21, 1906-7 (1953)
 Nernst, W., Ann. Physik. 36, 395-439 (1911)
 Nernst, W. and Lindemann, F. A., Z. Elektrochem. 17, 817-27 (1911)
 Pitzer, K. S., J. Chem. Phys. 6, 68-70 (1938)
 Robertson, R., Fox, J. J. and Martin, A. E., Proc. Roy. Soc. (London) A157, 579-94 (1936)

Comments:

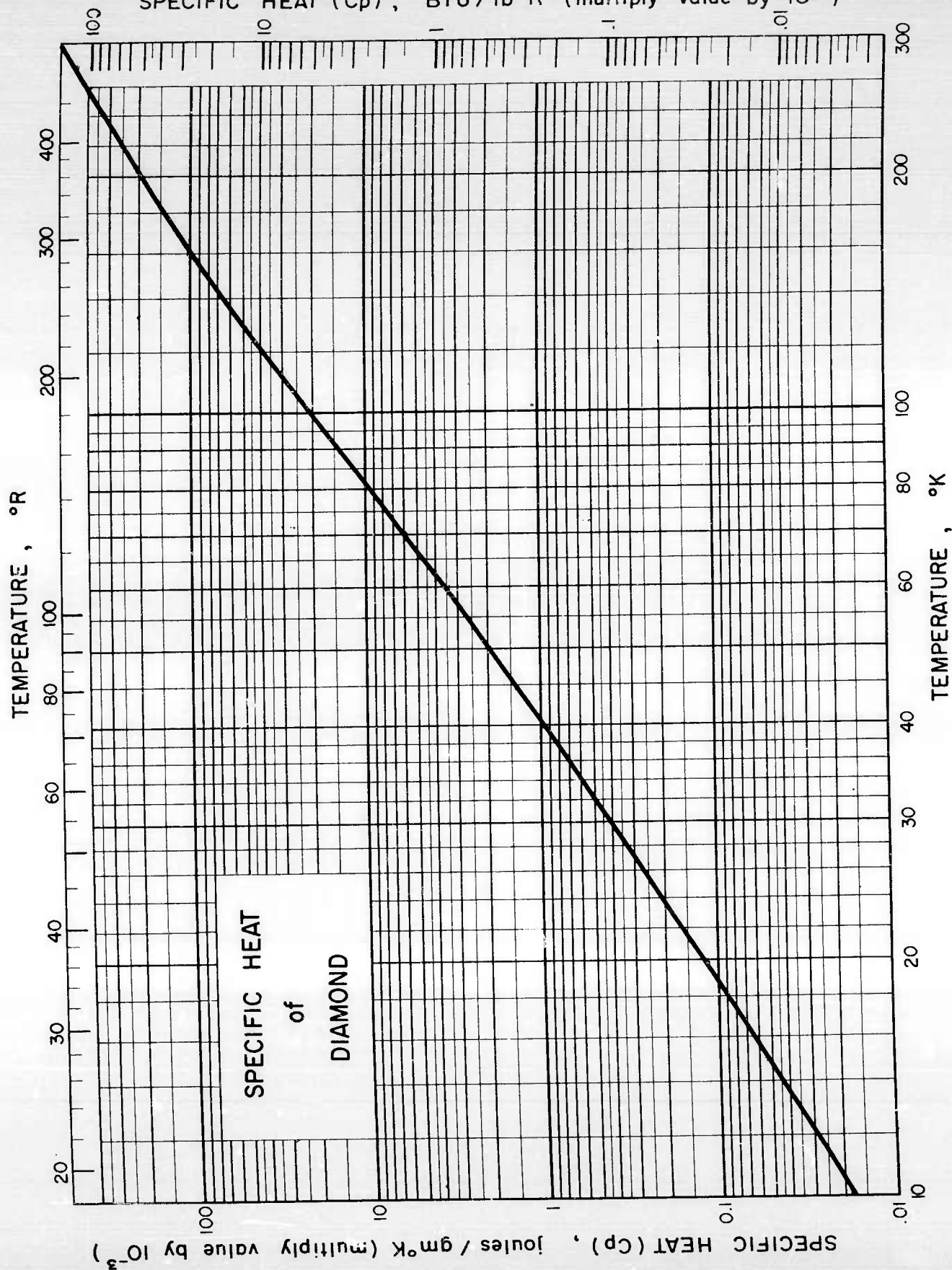
C_p values are without regard to ratio of Type I to Type II crystals used as sample.

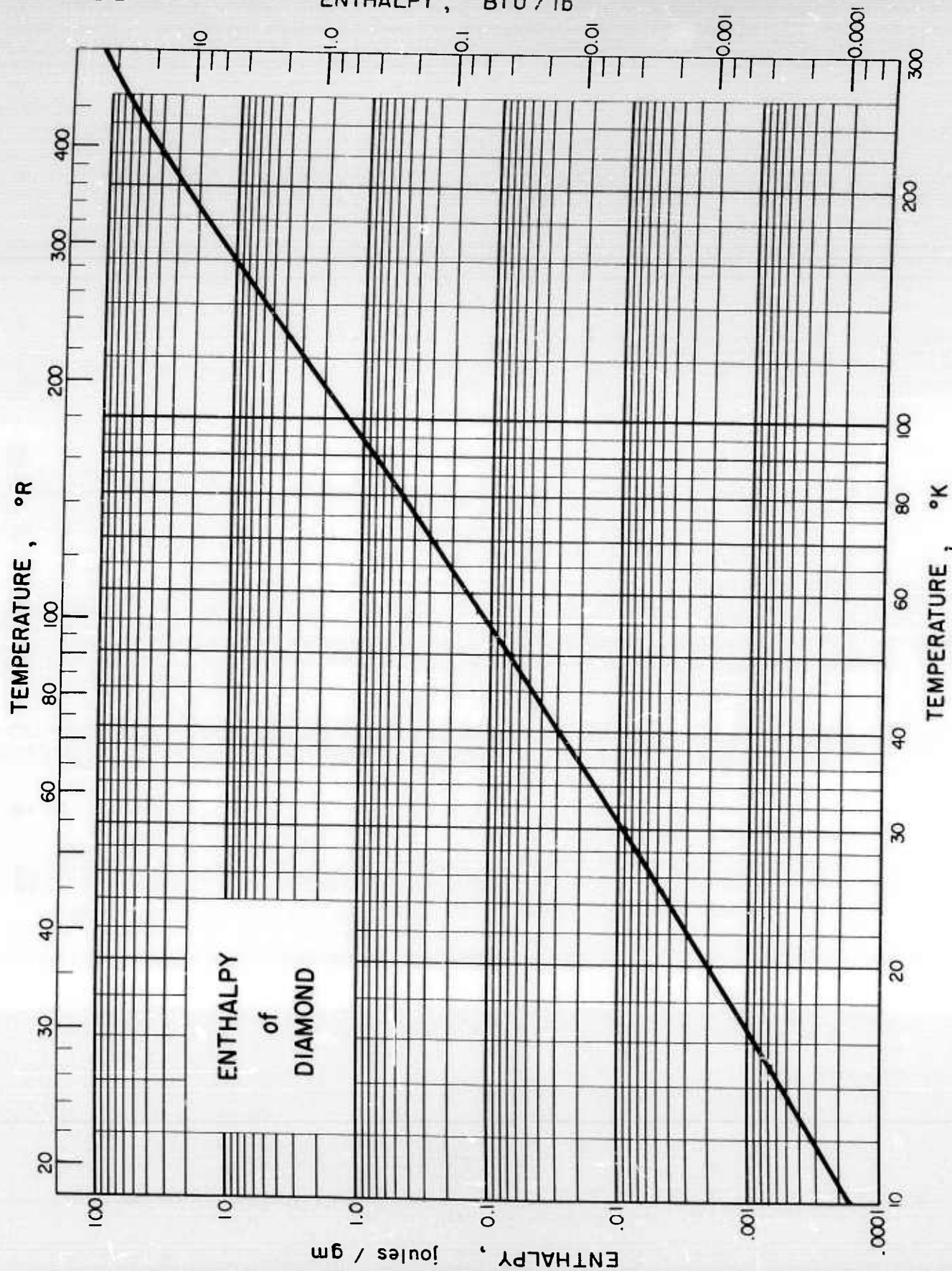
The Debye Temperature at 0°K, θ_0 , used in theoretical calculations of specific heats near 0°K, for diamond = 2100 ± 140 .

Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|-----------|-------------|------------------|-----------|
| 10 | 0.000 018 | 0.000 17 | 100 | 0.0204 | 1.31 |
| 15 | .000 053 | .000 66 | 120 | .0390 | 2.97 |
| 20 | .000 122 | .001 87 | 140 | .0658 | 5.94 |
| 25 | .000 235 | .004 38 | 160 | .102 | 10.7 |
| 30 | .000 404 | .008 87 | 180 | .145 | 17.8 |
| 40 | .000 979 | .027 8 | 200 | .195 | 27.5 |
| 50 | .001 95 | .068 8 | 220 | .252 | 40.3 |
| 60 | .003 41 | .144 | 240 | .314 | 56.6 |
| 70 | .005 92 | .276 | 260 | .380 | 76.5 |
| 80 | .009 34 | .489 | 280 | .447 | 100 |
| 90 | .014 0 | .821 | 300 | .518 | 128 |

RJC/JJG/VDA Issued: 10-13-59
 Revised: 5-20-60

SPECIFIC HEAT (C_p), BTU/lb $^{\circ}$ R (multiply value by 10^{-3})



SPECIFIC HEAT and ENTHALPY of VITREOUS SILICA
(Silica Glass, Quartz Glass)

Sources of Data:

- Simon, F., Ann. Physik (4) 68, 241-80 (1922)
 Simon, F. and Lange, F., Z. physik. 38, 227-36 (1926)
 Westrum, E. F., data reproduced in Lord, R. C. and Morrow,
 J. C., J. Chem. Phys. 26, 230 (1957)

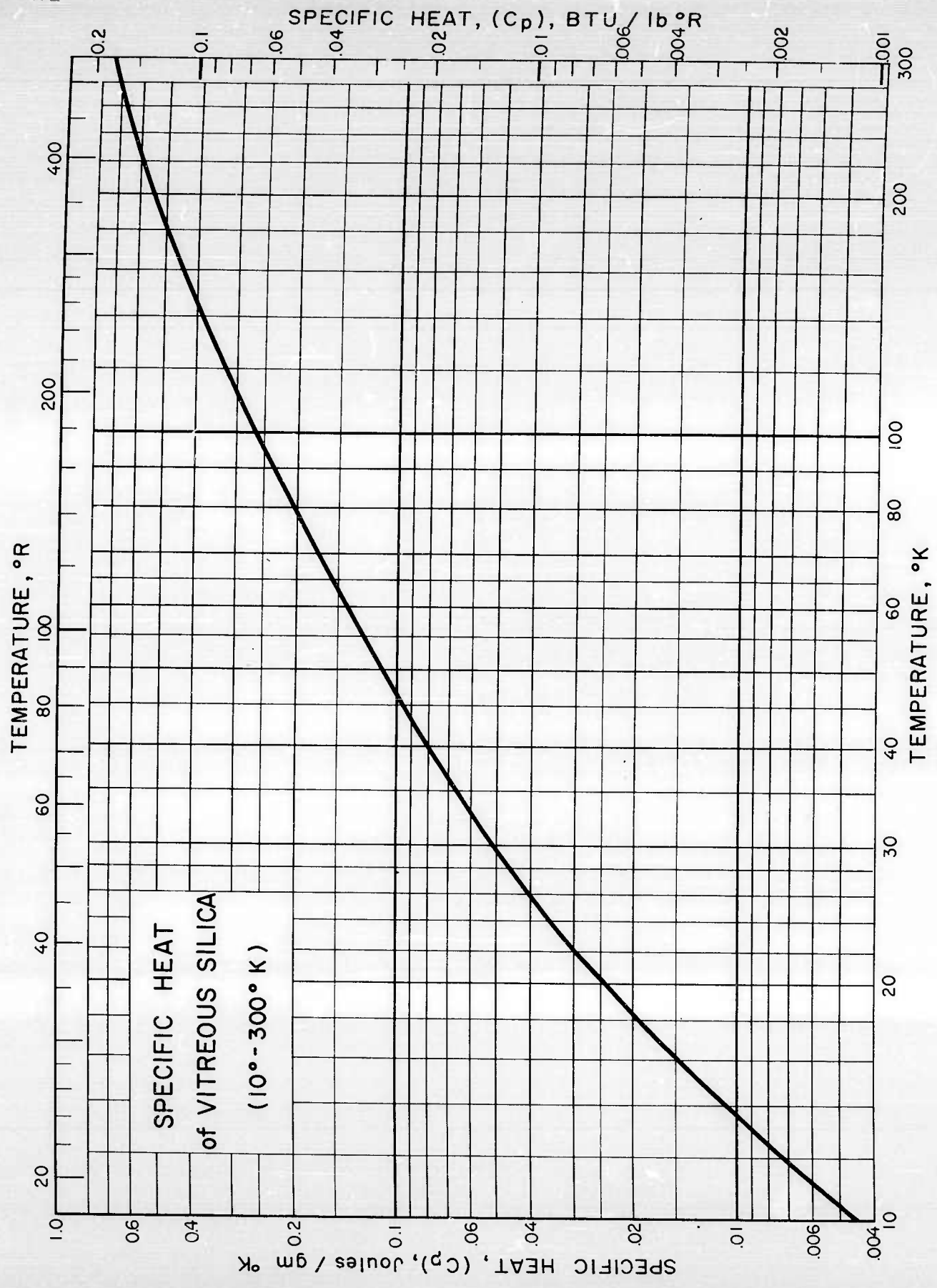
Other References:

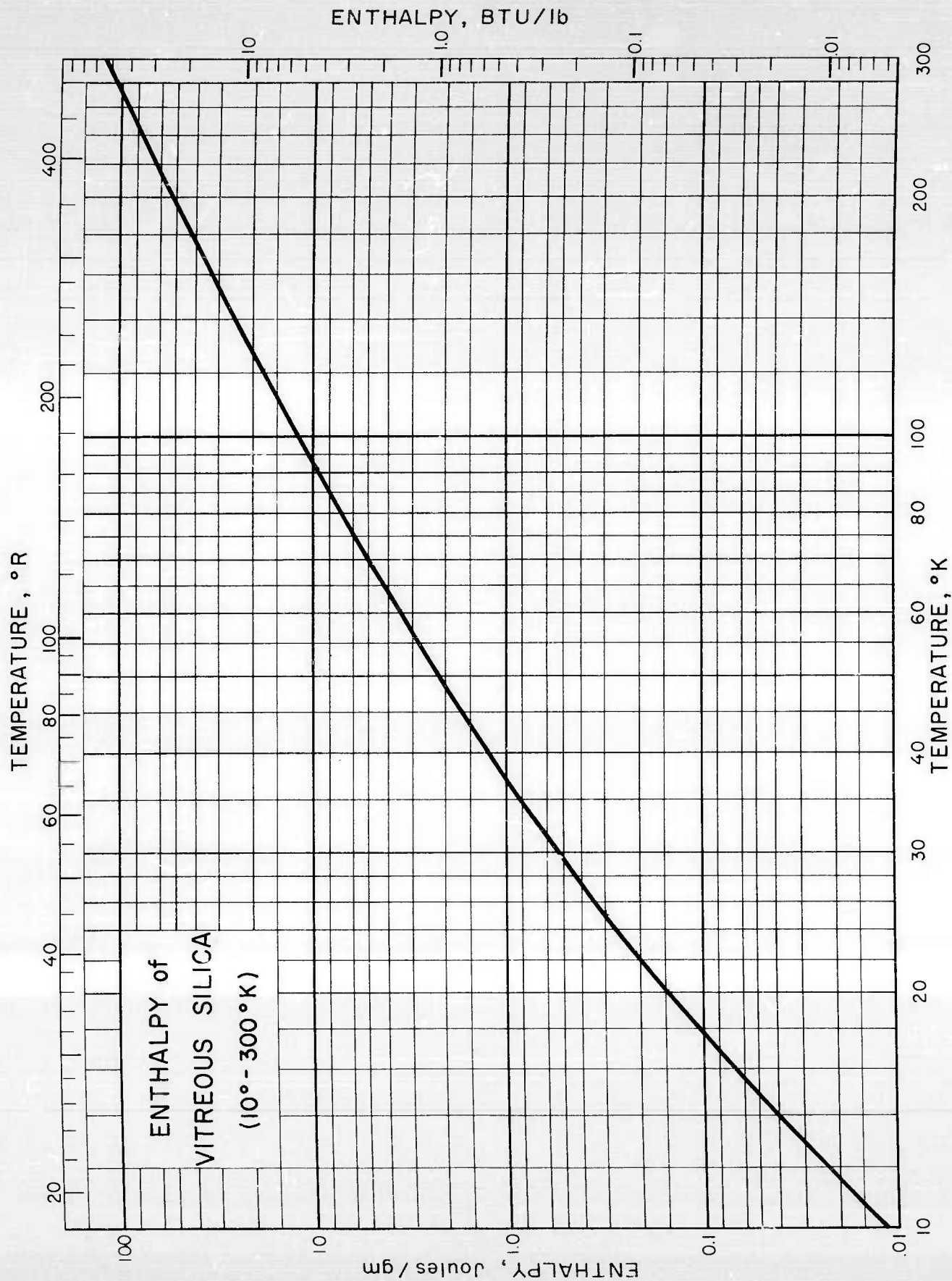
- Nernst, W., Sitzber. kgl. preuss. Akad. Wiss., 306 (1911)

Table of Selected Values

| Temp. °K | C _p j/gm-°K | H j/gm | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|-------------|---------------------------|-----------|
| 10 | 0.0045 | 0.011 | 100 | 0.268 | 11.57 |
| 15 | .0126 | 0.052 | 120 | .331 | 17.56 |
| 20 | .0244 | 0.143 | 140 | .391 | 24.77 |
| 25 | .0379 | 0.299 | 160 | .446 | 33.14 |
| 30 | .0519 | 0.524 | 180 | .497 | 42.6 |
| 40 | .0808 | 1.186 | 200 | .544 | 53.0 |
| 50 | .111 | 2.15 | 220 | .588 | 64.3 |
| 60 | .141 | 3.41 | 240 | .629 | 76.5 |
| 70 | .172 | 4.97 | 260 | .668 | 89.5 |
| 80 | .204 | 6.85 | 280 | .704 | 103.2 |
| 90 | .236 | 9.05 | 300 | .738 | 117.6 |

RJC Issued: 6/15/59
 Revised: 5/20/60





SPECIFIC HEAT and ENTHALPY of LEAD

Sources of Data:

- Horowitz, M., Silvidi, A. A., Malaker, S. F. and Daunt, J. G.,
Phys. Rev. 88, 1182 (1952)
- Meads, P. F., Forsythe, W. R. and Glauque, W. F., J. Am. Chem. Soc.
63, 1902 (1941)

Other References:

- Behn, U., Ann. Physik (3) 66, 237 (1898)
- Bronson, H. L. and Wilson, A. J. C., Can. J. Research A14, 181
(1936)
- Clement, J. R. and Quinnell, E. H., Phys. Rev. 85, 502 (1952)
- Dolacek, R. L., Conf. de Physique des Basses Temperatures, Paris
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- Eucken, A. and Schwers, F., Verhandl. deut. physik. Ges. 15, 578
(1913)
- Griffiths, E. G. and Griffiths, E., Proc. Roy. Soc. (London) A90,
557 (1914)
- Keesom, W. H. and Andrews, D. H., Commun. Kamerlingh Onnes Lab.
Univ. Leiden 17, No. 185a, (1924)
- Keesom, W. H. and Onnes, H. K., Commun. Kamerlingh Onnes Lab. Univ.
Leiden No. 143, (1913-14) and Verslag Koninkl. Akad. Wetenschap.
Amsterdam 23, 798-812 (1914)
- Keesom, W. H. and Van den Ende, J. N., Physik. Z. 29, 896 (1928)
- Keesom, W. H. and Van den Ende, J. N., Commun. Kamerlingh Onnes
Lab. Univ. Leiden No. 203d, 25 (1930) and Proc. Acad. Sci.
Amsterdam 33, 243 (1930)
- Keesom, W. H. and Van den Ende, J. N., Commun. Kamerlingh Onnes
Lab. Univ. Leiden No. 213c, (1931) and Proc. Acad. Sci. Amsterdam
34, 210 (1931)
- Koref, F., Ann. Physik (4) 36, 49 (1911)
- Mendelssohn, N. and Simon, F., Z. physik. Chem. B16, 72 (1932)
- Nernst, W., Sitzber. klg. preuss. Akad. Wiss., 262 (1910)

(continued)

SPECIFIC HEAT and ENTHALPY of LEAD (Cont.)

Other References (Cont.)

Nernst, W. Sitzber. kgl. preuss. Akad. Wiss., 306 (1911)

Nernst, W. and Lindemann, F. A., Sitzber. kgl. preuss. Akad. Wiss., 494 (1911)

Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)

Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)

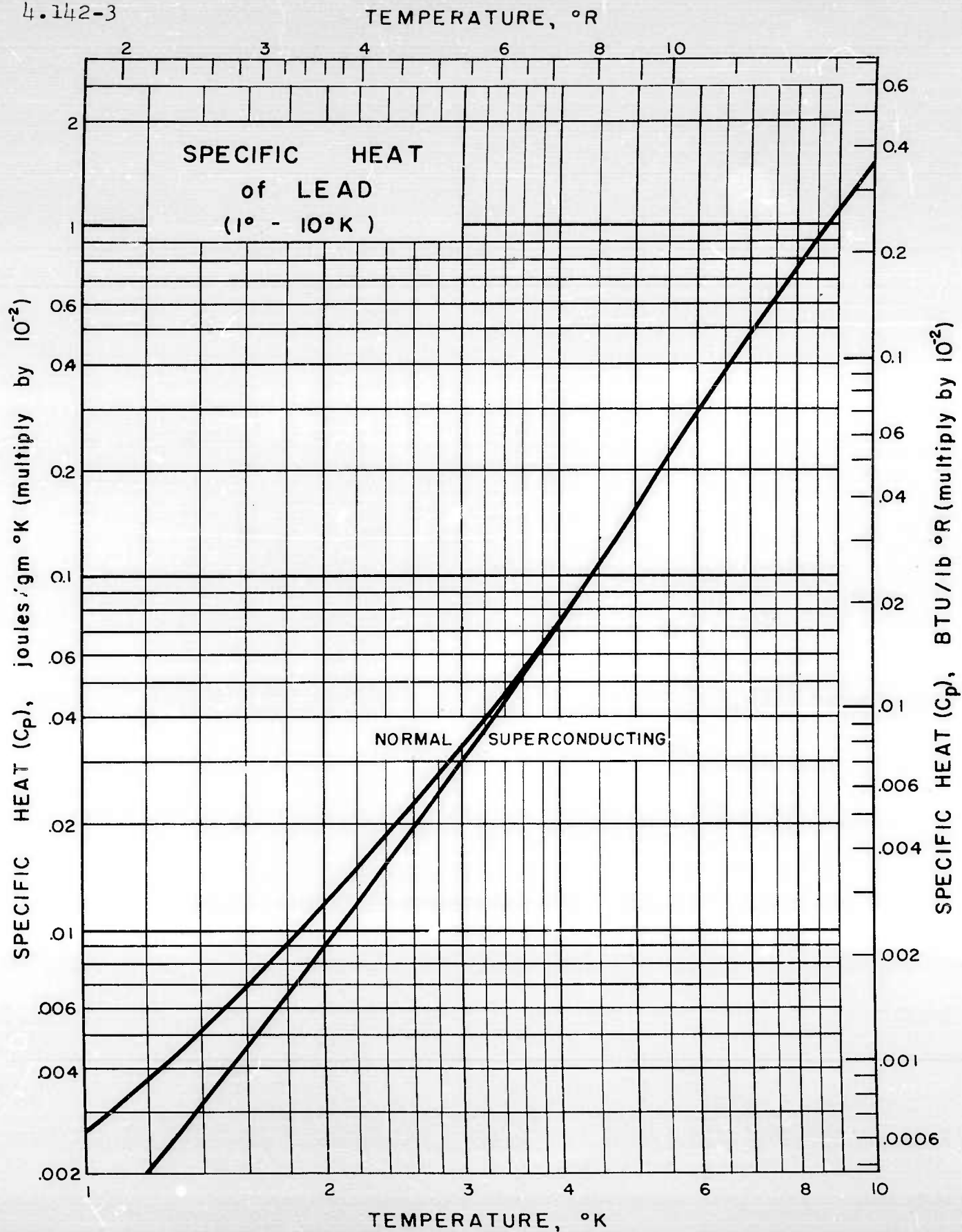
Simon, F., Z. physik. Chem. 110, 572 (1924)

Table of Selected Values

| T °K | C _p , j/gm °K | | H, j/gm | | T °K | C _p j/gm °K Normal | H j/gm Normal |
|---------|--------------------------|---------------------|-----------|---------------------|---------|-------------------------------------|---------------------|
| | Normal | Super Conducting | Normal | Super Conducting | | | |
| 1 | 0.000 026 | 0.000 012 | 0.000 010 | 0.000 003 | 50 | 0.103 | 2.91 |
| 2 | .000 12 | .000 09 | .000 07 | .000 05 | 60 | .108 | 3.97 |
| 3 | .000 33 | .000 31 | .000 28 | .000 23 | 70 | .112 | 5.07 |
| 4 | .000 7 | .000 7 | .000 8 | .000 7 | 80 | .114 | 6.20 |
| 5 | .001 5 | .001 5 | .001 8 | .001 8 | 90 | .116 | 7.35 |
| 6 | .002 9 | .003 0 | .003 9 | .004 0 | 100 | .118 | 8.53 |
| 7 | .004 8 | .005 0 | .008 | .008 | 120 | .120 | 10.91 |
| 8 | .007 3 | | .014 | | 140 | .121 | 13.32 |
| 10 | .013 7 | | .034 | | 160 | .123 | 15.76 |
| 15 | .033 5 | | .150 | | 180 | .124 | 18.22 |
| 20 | .053 1 | | .368 | | 200 | .125 | 20.71 |
| 25 | .068 1 | | .672 | | 220 | .126 | 23.21 |
| 30 | .079 6 | | 1.042 | | 240 | .127 | 25.73 |
| 35 | .088 2 | | 1.462 | | 260 | .128 | 28.28 |
| 40 | .094 4 | | 1.920 | | 280 | .129 | 30.85 |
| 45 | .099 1 | | 2.405 | | 300 | .130 | 33.43 |

RJC Issued: 6-15-59

4.142-3

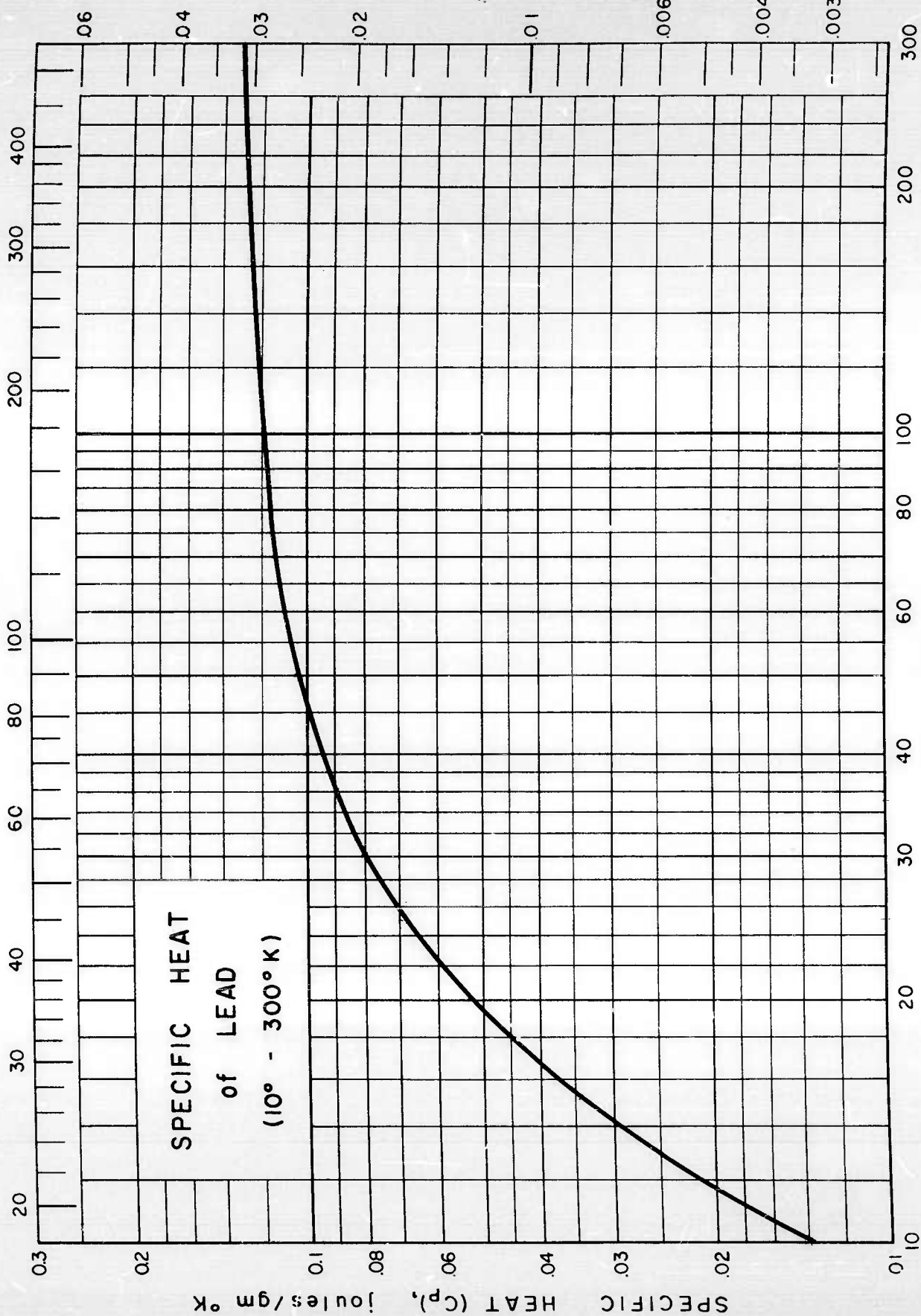


4.142-3

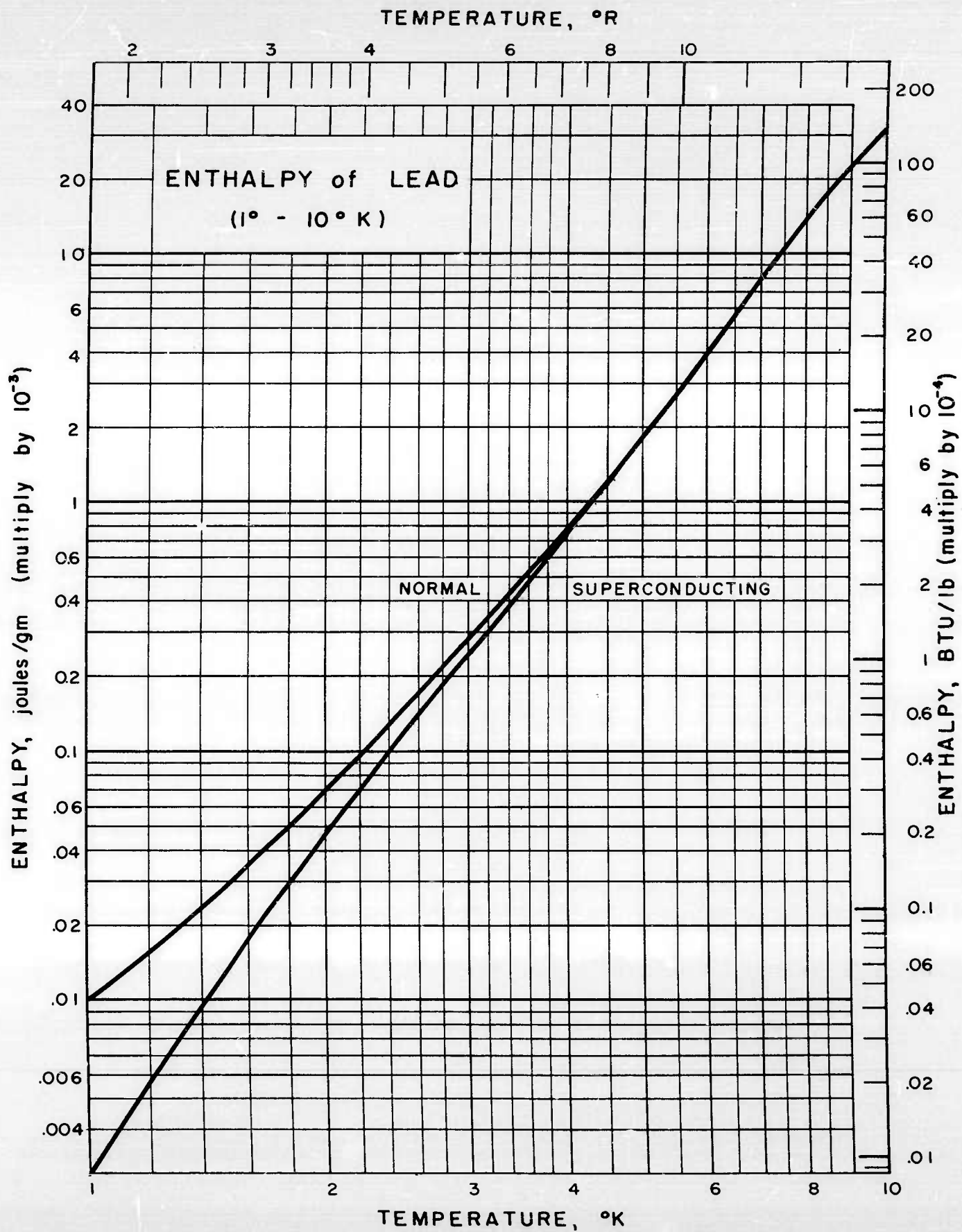
SPECIFIC HEAT (C_p), BTU/lb °R

TEMPERATURE, °R

TEMPERATURE, °K

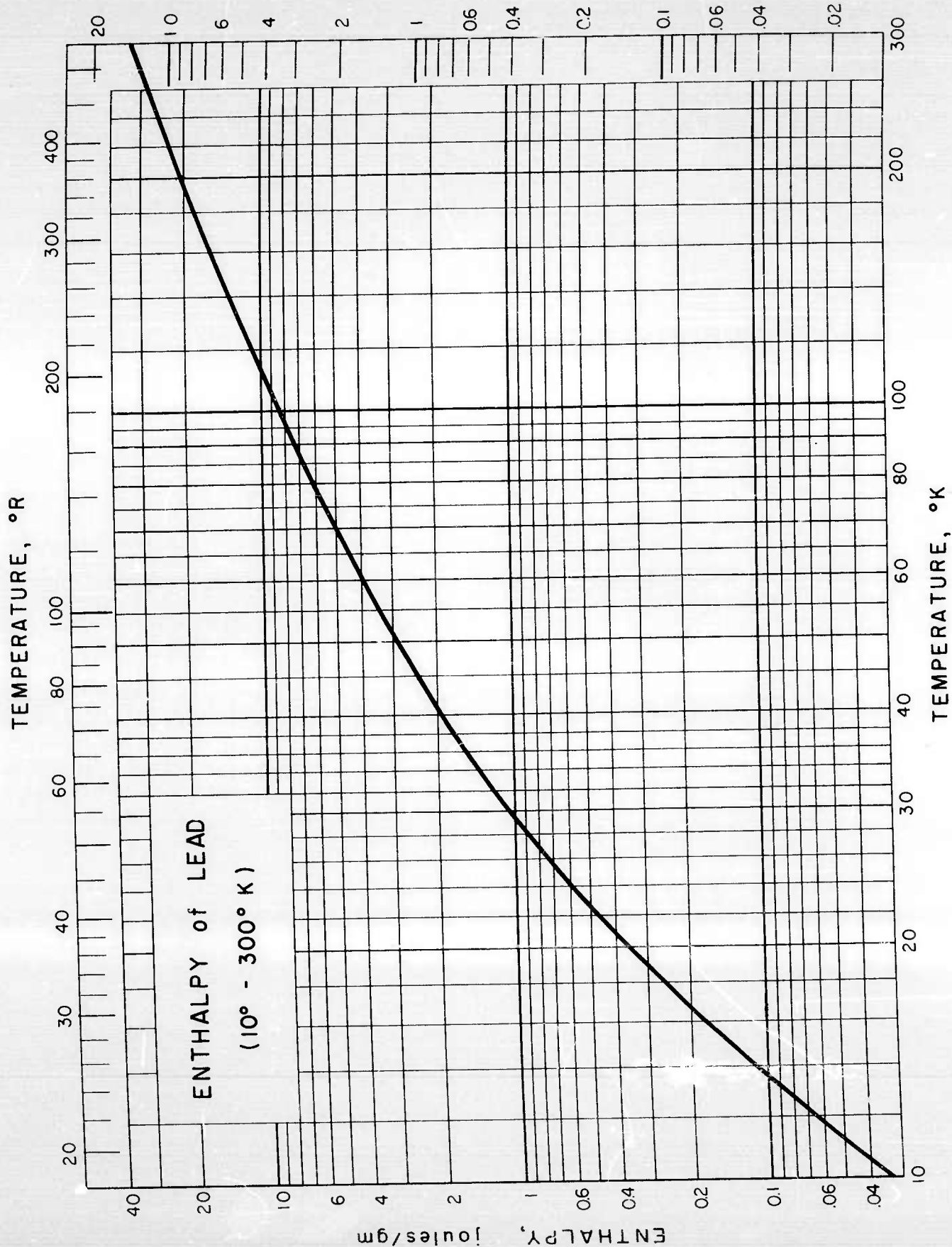


4.142-3



4.142-3

ENTHALPY, BTU/lb



SPECIFIC HEAT, ENTHALPY of TIN (white)

Sources of Data:

- Corak, W. S. and Satterwaite, C. B., Phys. Rev. 102, 662 (1956)
 Goodman, B. B., Compt. rend. 244, 2899 (1957)
 Keesom, W. H. and Van den Ende, J. N., Proc. Acad. Sci. Amsterdam 35,
 143 (1932)
 Lange, F., Z. physik. Chem. 110, 343 (1924)
 Rodebush, W. H., J. Am. Chem. Soc. 45, 1413 (1923)

Other References:

- Brönsted, J. N., Z. physik. Chem. 88, 479 (1914)
 Keesom, W. H. and Kok, J. A., Proc. Acad. Sci. Amsterdam 35, 743 (1932)
 Keesom, W. H. and Van Laer, P. H., Physica 3, 371 (1936)
 Keesom, W. H. and Van Laer, P. H., Physica 4, 487 (1937)
 Keesom, W. H. and Van Laer, P. H., Physica 5, 133 (1938)
 Ramanathan, K. G. and Srinivasan, T. M., Phil. Mag. 46, 338 (1955)
 Richards, T. W. and Jackson, R. G., Z. physik. Chem. 70, 414 (1910)
 Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)

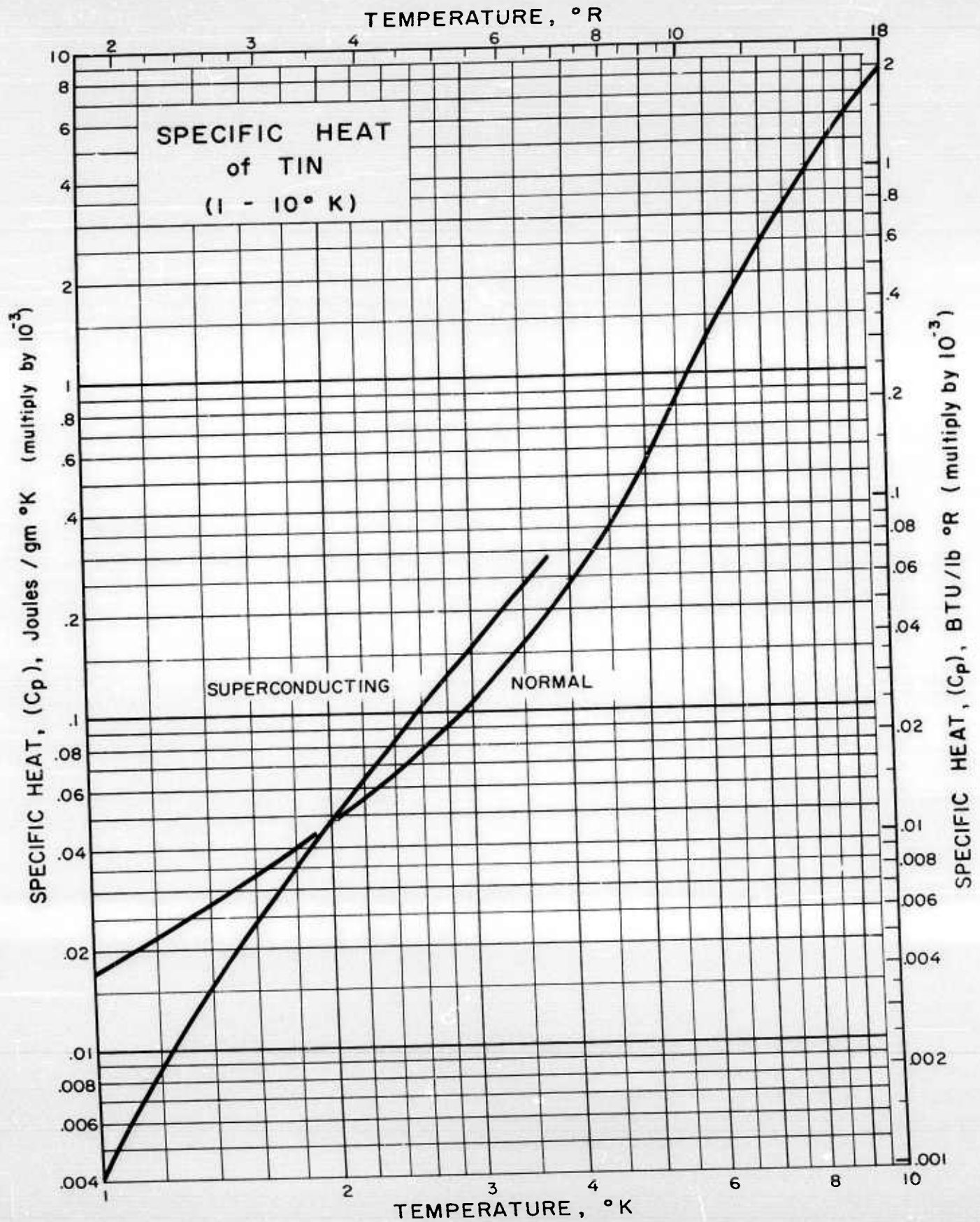
Table of Selected Values

| Temp. °K | C _p , j/gm-°K | | H, j/gm | | Temp. °K | C _p , j/gm-°K | H, j/gm |
|-------------|--------------------------|----------------------|------------|----------------------|-------------|--------------------------|---------|
| | Normal | Super- conducting | Normal | Super- conducting | | | |
| 1 | 0.000 0170 | 0.000 0041 | 0.000 0079 | 0.000 0009 | 60 | 0.148 | 4.33 |
| 2 | .000 047 | .000 048 | .000 0383 | .000 0228 | 70 | .162 | 5.88 |
| 3 | .000 109 | .000 151 | .000 113 | .000 116 | 80 | .173 | 7.55 |
| *3.72 | .000 198 | .000 285 | .000 221 | .000 270 | 90 | .182 | 9.33 |
| 4 | .000 245 | | .000 283 | | 100 | .189 | 11.18 |
| 5 | .000 54 | | .000 65 | | 120 | .198 | 15.05 |
| 6 | .001 27 | | .001 51 | | 140 | .204 | 19.1 |
| 8 | .004 2 | | .006 8 | | 160 | .208 | 23.2 |
| 10 | .008 1 | | .019 0 | | 180 | .212 | 27.4 |
| 15 | .022 6 | | .093 | | 200 | .214 | 31.7 |
| 20 | .040 | | .251 | | 220 | .216 | 36.0 |
| 25 | .058 | | .498 | | 240 | .218 | 40.3 |
| 30 | .076 | | .834 | | 260 | .220 | 44.7 |
| 40 | .106 | | 1.75 | | 280 | .221 | 49.1 |
| 50 | .130 | | 2.93 | | 300 | .222 | 53.6 |

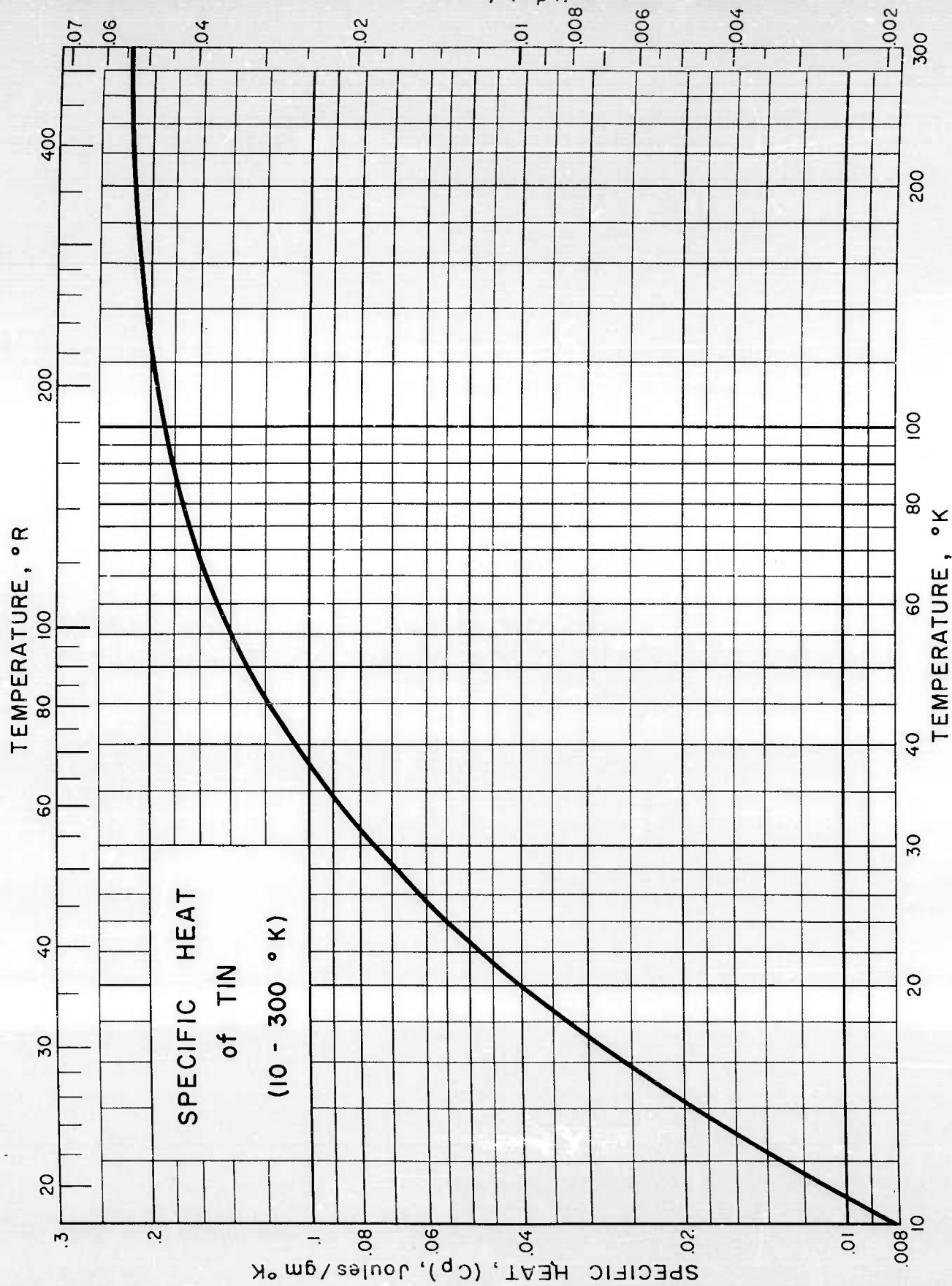
* Superconducting transition temperature

RJC Issued: 6-5-59
 Revised: 5-20-60

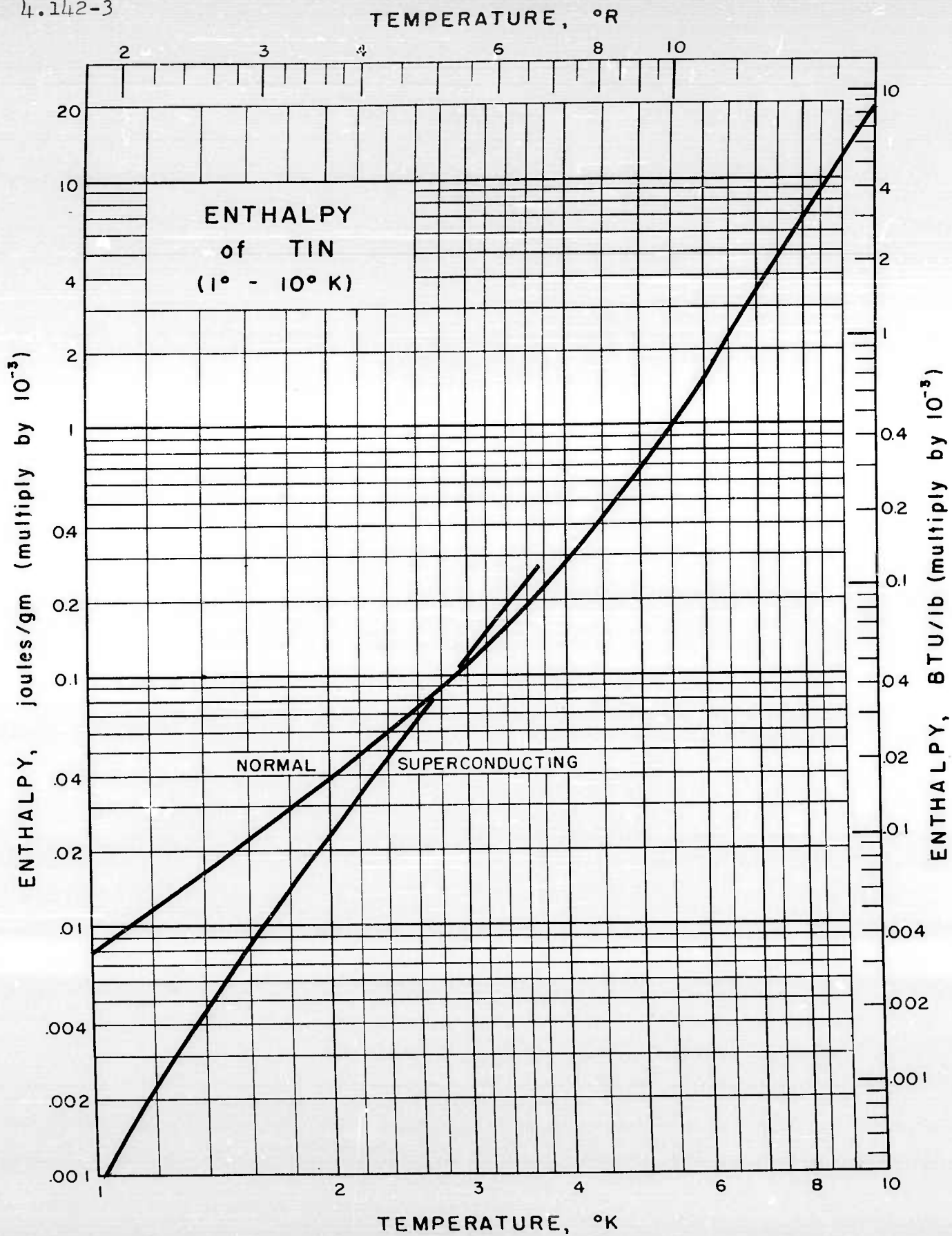
4.142-3



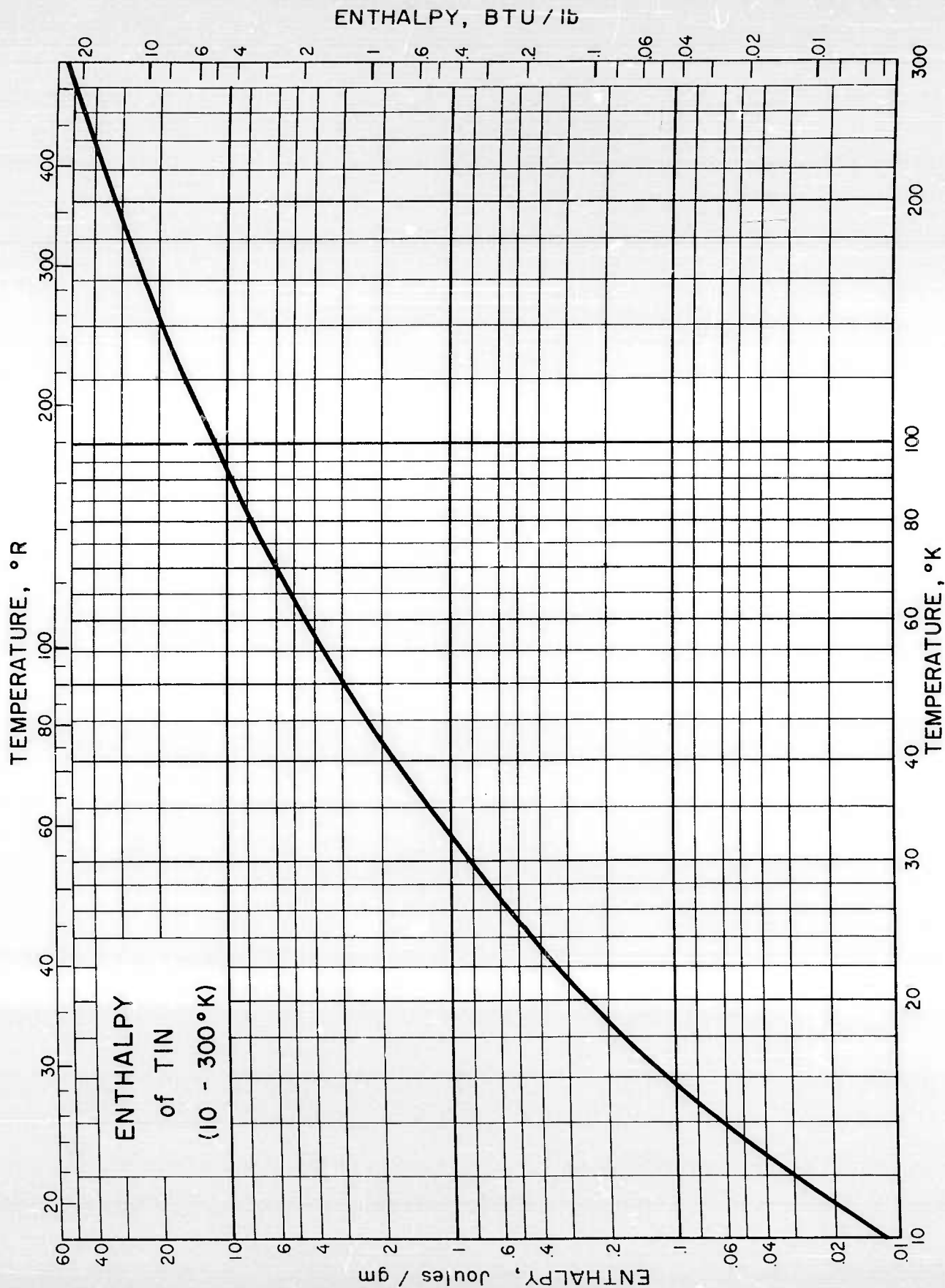
4.142-3

SPECIFIC HEAT, (C_p), BTU / lb °R

4.142-3



4.142-3



SPECIFIC HEAT, ENTHALPY of NIOBIUM

Source of Data:

Chou, C., White, P. and Johnston, H. L., Phys. Rev. 109, 788-796 (1958)

Other References:

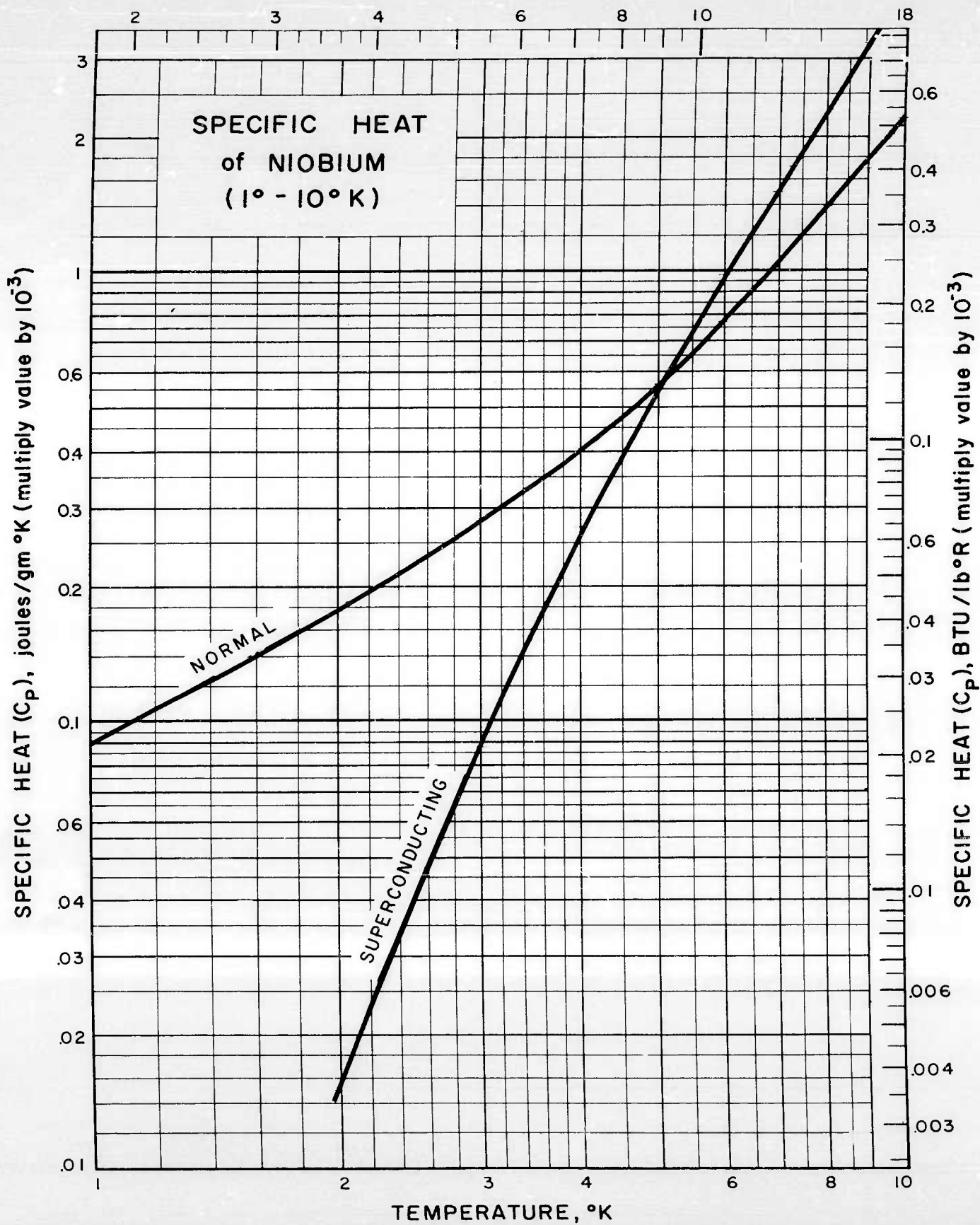
Brown, A., Zemansky, M. W. and Boorse, H. A., Phys. Rev. 86, 134 (1952)

Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)

Comments:

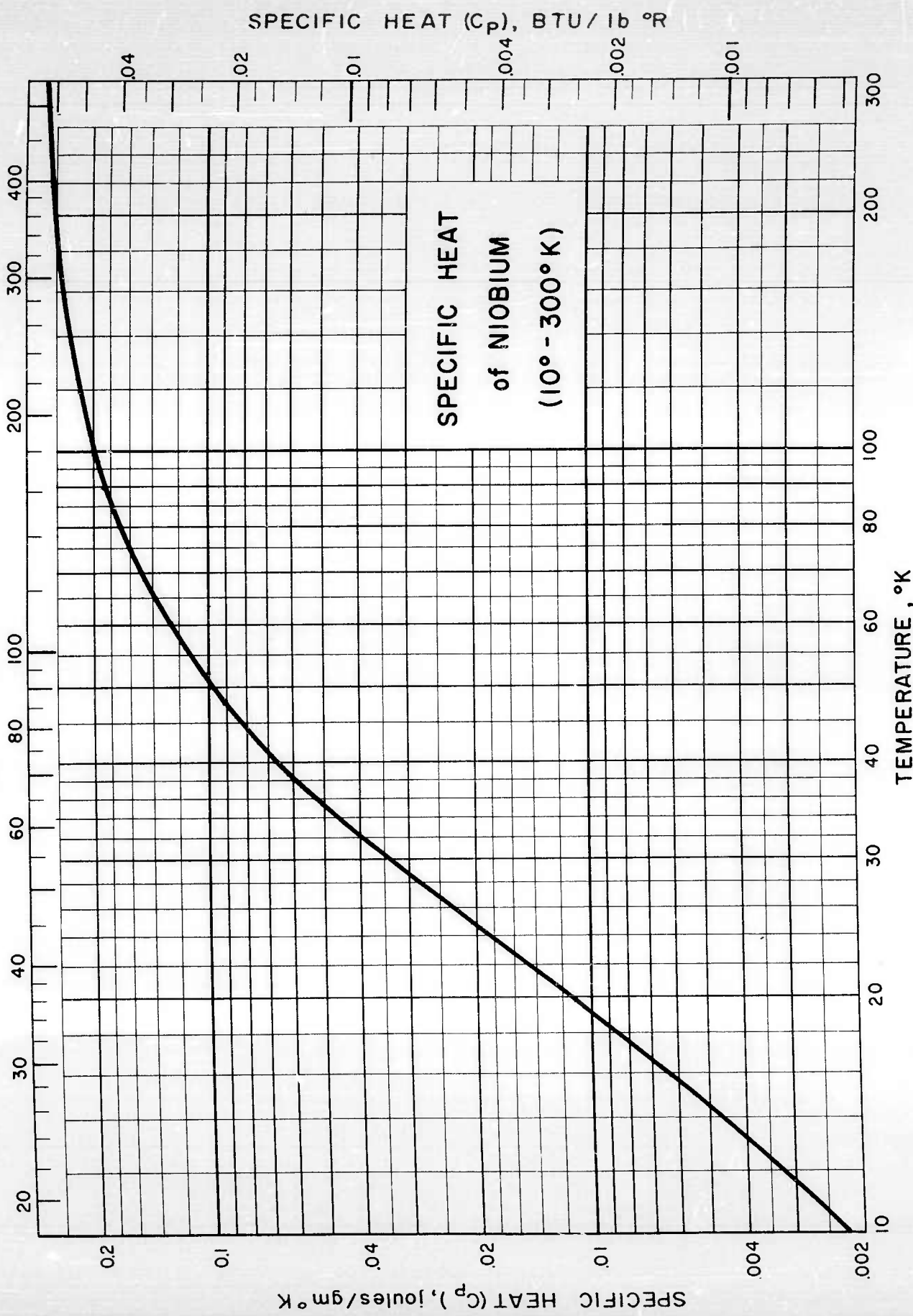
The data of Chou, White and Johnston cover the range, 1.5° to 30°K while the compilation of Kelley (1949) gives best values for room temperature and above. Between 30° and room temperature no modern experimental data are to be found. The values in this region given here are estimates. While the accuracy at 2 to 30° and at 300°K is of order 1%, the estimated values between 30° and 300°K are more uncertain and may be in error by as much as 10% in the region 40° to 100°K.

| Temp. °K | C _p joules/gram-°K | | H joules/gram | | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|-------------------------------|------------------------|-----------------------|------------------------|-------------|------------------------|--------|
| | Normal | Supercond. | Normal | Supercond. | | Normal | Normal |
| 1 | .09 x10 ⁻³ | | .04 x10 ⁻³ | | 60 | .127 | 2.76 |
| 2 | .18 " | .015 x10 ⁻³ | .17 " | .005 x10 ⁻³ | 70 | .152 | 4.2 |
| 3 | .28 " | .088 " | .40 " | .049 " | 80 | .173 | 5.8 |
| 4 | .40 " | .27 " | .73 " | .22 " | 90 | .189 | 7.6 |
| 5 | .56 " | .56 " | 1.20 " | .62 " | 100 | .202 | 9.6 |
| 6 | .77 " | .98 " | 1.86 " | 1.38 " | 120 | .221 | 13.8 |
| 7 | 1.02 " | 1.5 " | 2.75 " | 2.6 " | 140 | .234 | 18.3 |
| 8 | 1.4 " | 2.3 " | 3.93 " | 4.5 " | 160 | .243 | 23.1 |
| 9 | 1.7 " | 3.2 " | 5.5 " | 7.2 " | 180 | .249 | 28.0 |
| 10 | 2.2 " | | 7.4 " | | 200 | .254 | 33.1 |
| 15 | .0055 | | .026 | | 220 | .258 | 38.2 |
| 20 | .0113 | | .066 | | 240 | .261 | 43.4 |
| 25 | .021 | | .145 | | 260 | .264 | 48.6 |
| 30 | .035 | | .28 | | 280 | .266 | 53.9 |
| 40 | .068 | | .80 | | 300 | .268 | 59.2 |
| 50 | .099 | | 1.63 | | | | |



4.151

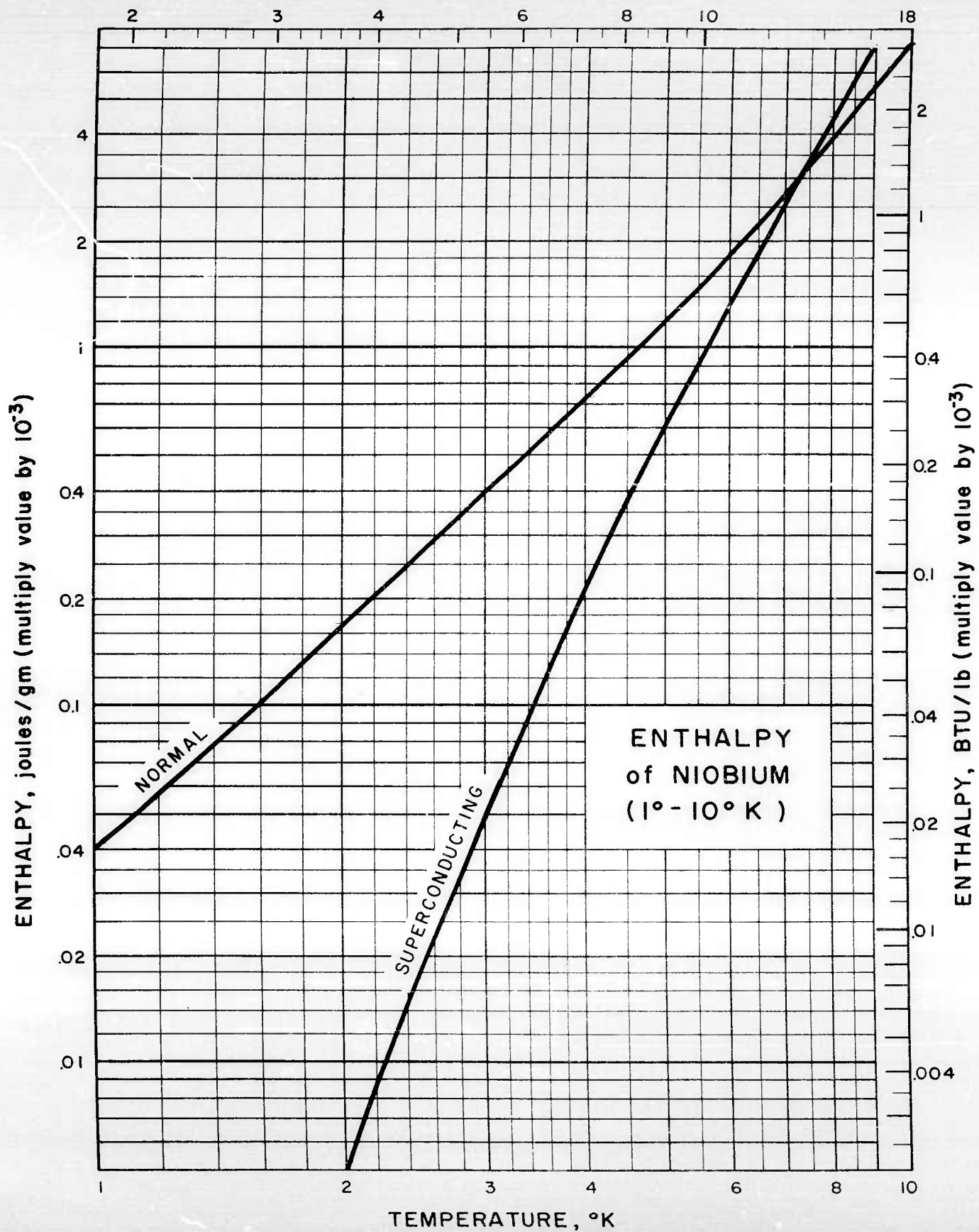
TEMPERATURE, °R



TEMPERATURE, °K

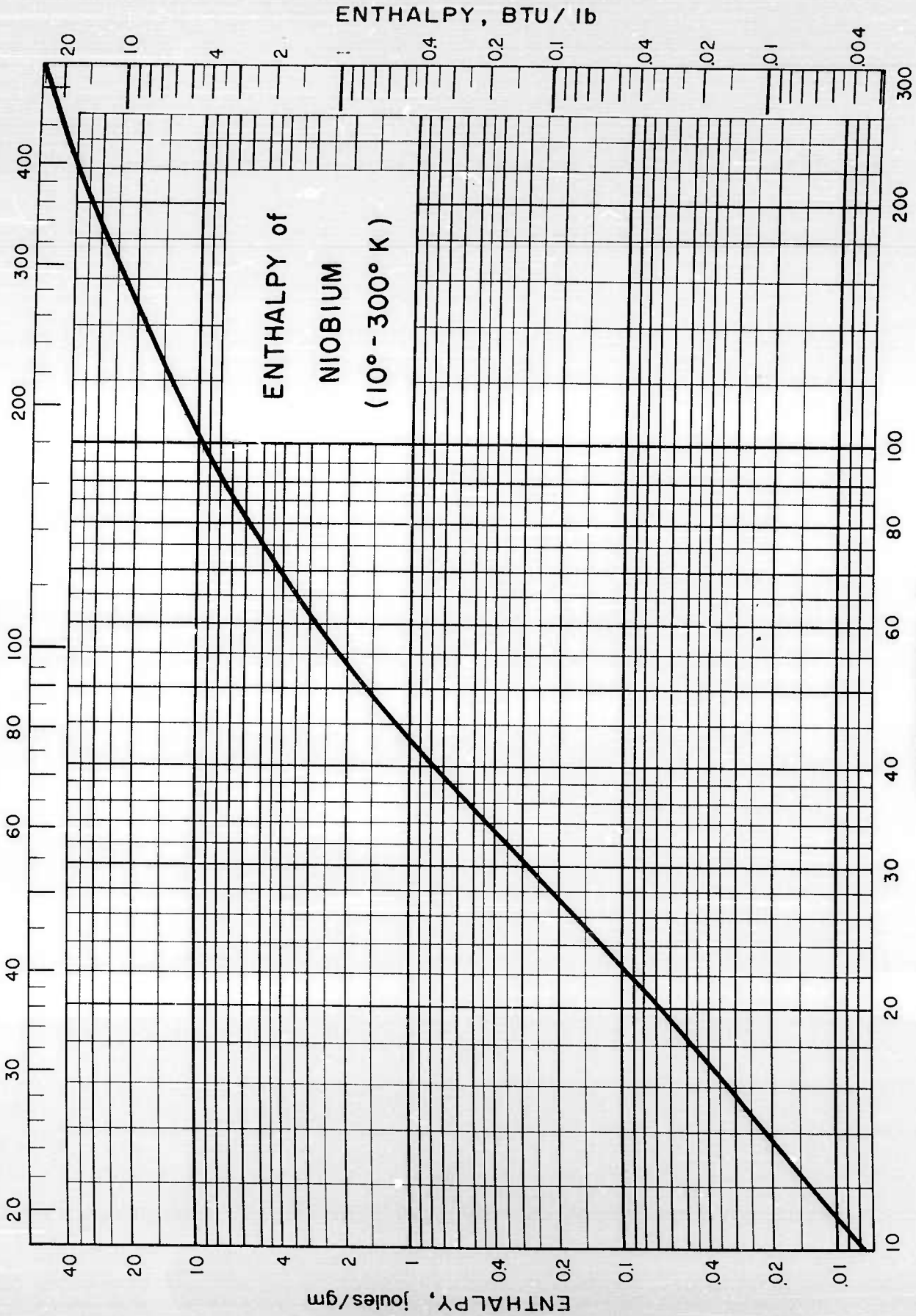
4.151

TEMPERATURE, °R



4.151

TEMPERATURE, °R



SPECIFIC HEAT, ENTHALPY of TANTALUM

Sources of Data:Kelley, K. K., J. Chem. Phys. 8, 316-22 (1940)White, D., Chou, C. and Johnston, H. L., Phys. Rev. 109, 797-802 (1958)Other References:Clusius, K. and Losa, G. L., Z. Naturforsch. 10A, 939-43 (1955)Desirant, M., Rept. Intern. Conf. Fundamental Particles and Low Temp. 2, 124 (1947)Keesom, W. H. and Desirant, M., Physica 8, 273 (1941)Mendlesohn, K., Nature 148, 316 (1941)

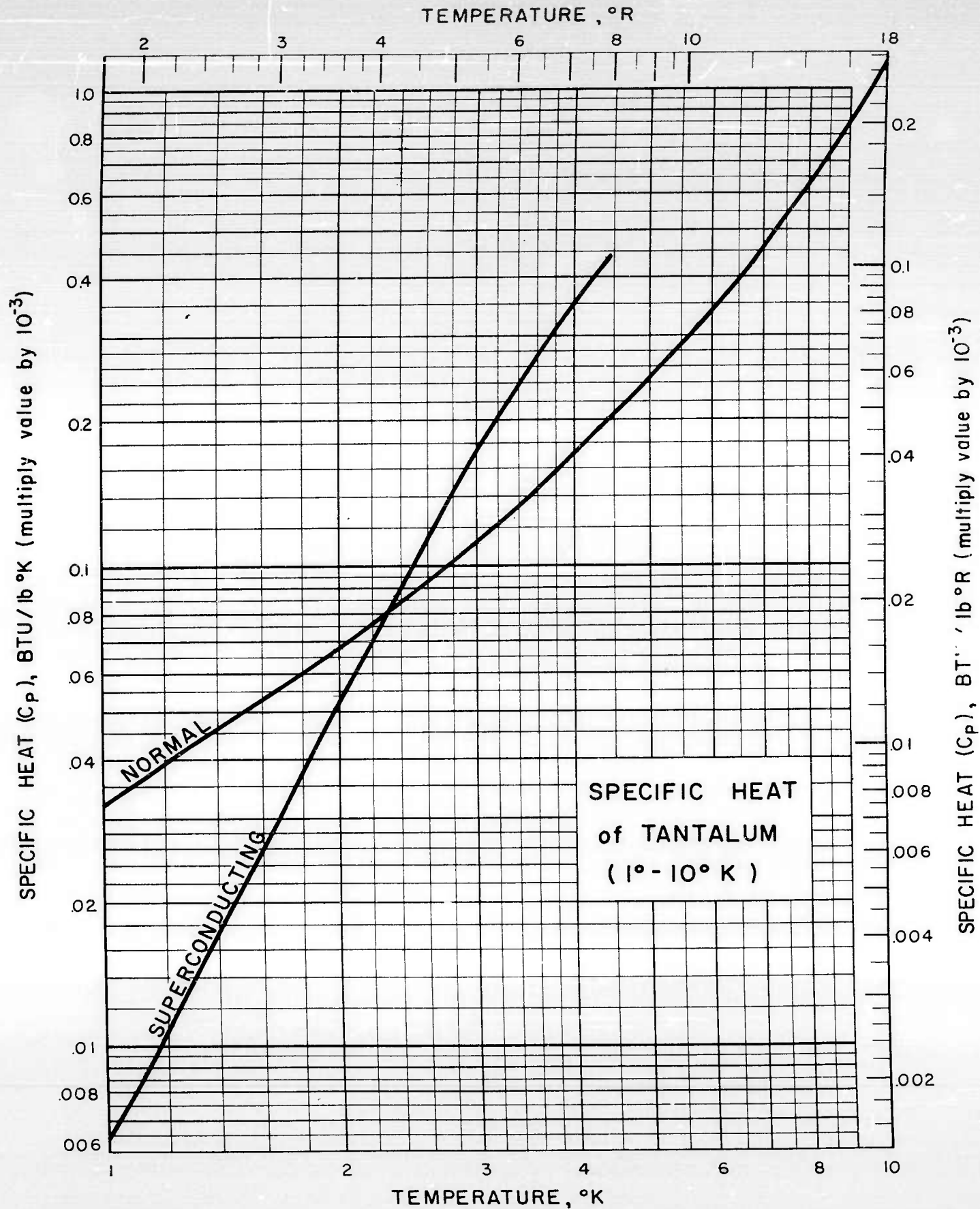
Wolcott, N. M., Conf. Physique Bases Temp., Paris (1955)

Worley, R. D., Zemansky, M. W. and Boorse, H. A., Phys. Rev. 91, 1567-8 (1953); Phys. Rev. 99, 447-58 (1955)Comments:For temperatures less than 4°K, the normal specific heat C_p follows the equation:

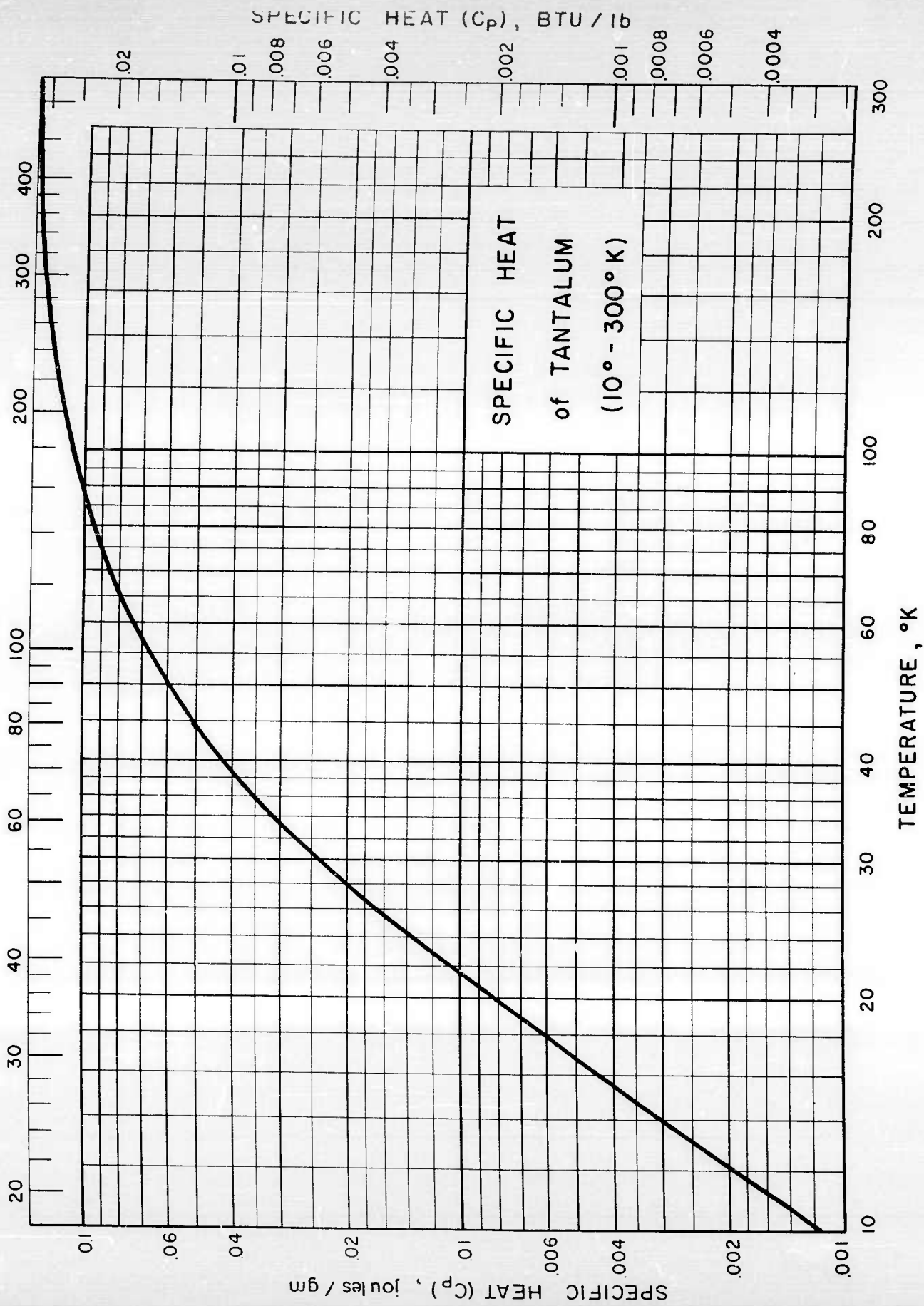
$$C_p = (31.7 \pm 0.9) \times 10^{-6} T + 10.74 \left(\frac{T}{248 \pm 6} \right)^3 \text{ j/gm-}^\circ\text{K}$$

Table of Selected Values

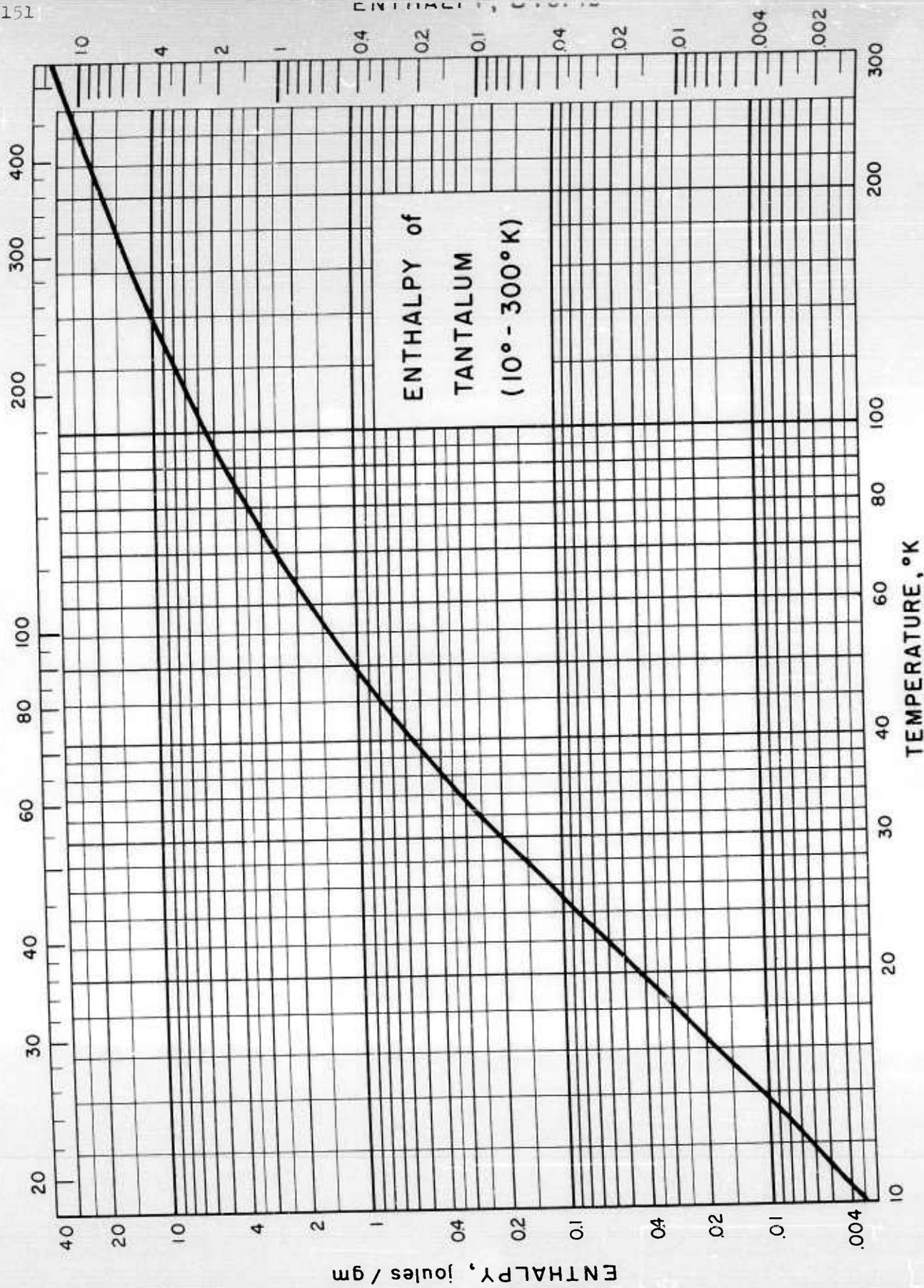
| Temp. °K | C_p , j/gm-°K | | H, j/gm | | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|-----------------|------------------|-----------|------------------|-------------|------------------|-----------|
| | normal | super-conducting | normal | super-conducting | | | |
| 1 | 0.000 032 | 0.000 0063 | 0.000 016 | 0.000 0021 | 70 | 0.0879 | 2.56 |
| 2 | .000 068 | .000 054 | .000 065 | .000 026 | 80 | .0976 | 3.49 |
| 3 | .000 112 | .000 178 | .000 155 | .000 138 | 90 | .105 | 4.50 |
| 4 | .000 171 | .000 352 | .000 295 | .000 400 | 100 | .111 | 5.58 |
| 4.39 | .000 201 | .000 433 | .000 368 | .000 553 | 120 | .119 | 7.88 |
| 6 | .000 333 | | .000 776 | | 140 | .125 | 10.4 |
| 8 | .000 648 | | .001 73 | | 160 | .128 | 12.9 |
| 10 | .001 17 | | .003 52 | | 180 | .131 | 15.5 |
| 15 | .003 60 | | .014 5 | | 200 | .134 | 18.1 |
| 20 | .008 23 | | .043 2 | | 220 | .136 | 20.8 |
| 25 | .015 3 | | .102 | | 240 | .137 | 23.6 |
| 30 | .024 0 | | .202 | | 260 | .138 | 26.3 |
| 40 | .043 0 | | .540 | | 280 | .139 | 29.1 |
| 50 | .060 4 | | 1.06 | | 300 | .140 | 31.9 |
| 60 | .075 4 | | 1.74 | | | | |

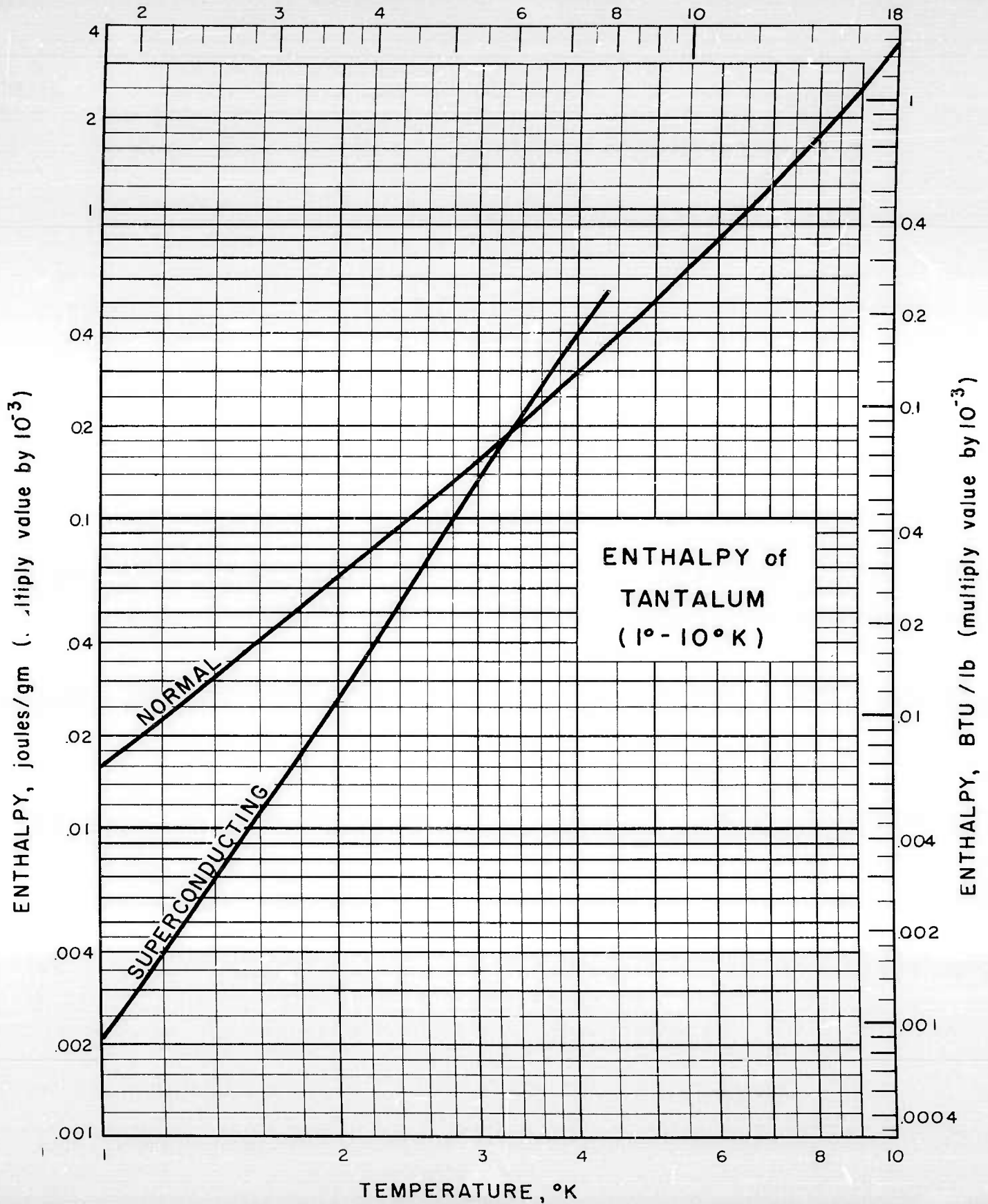


4.151
TEMPERATURE, °R



TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of BISMUTH

Sources of Data:

- Anderson, C. T., J. Am. Chem. Soc. 52, 2720 (1930)
 Armstrong, L. D. and Grayson-Smith, H., Can. J. Research A27, 9 (1949)
 Bronson, H. L. and MacHattie, L. E., Can. J. Research A16, 177 (1938)
 Kalinkina, I. V. and Strelkov, P. G., Zhur. Eksptl. i Teoret. Fiz. 34,
 616-21 (1958)
 Keesom, P. H. and Pearlman, N., Phys. Rev. 96, 897-902 (1954)
 Keesom, W. H. and Van Den Ende, J. N., Commun. Phys. Lab. Univ. Leiden
 No. 213c (1931)

Other References:

- Ramanathan, K. G. and Srinivasan, T. M., Phil. Mag. 46, 338 (1955)

Comments:

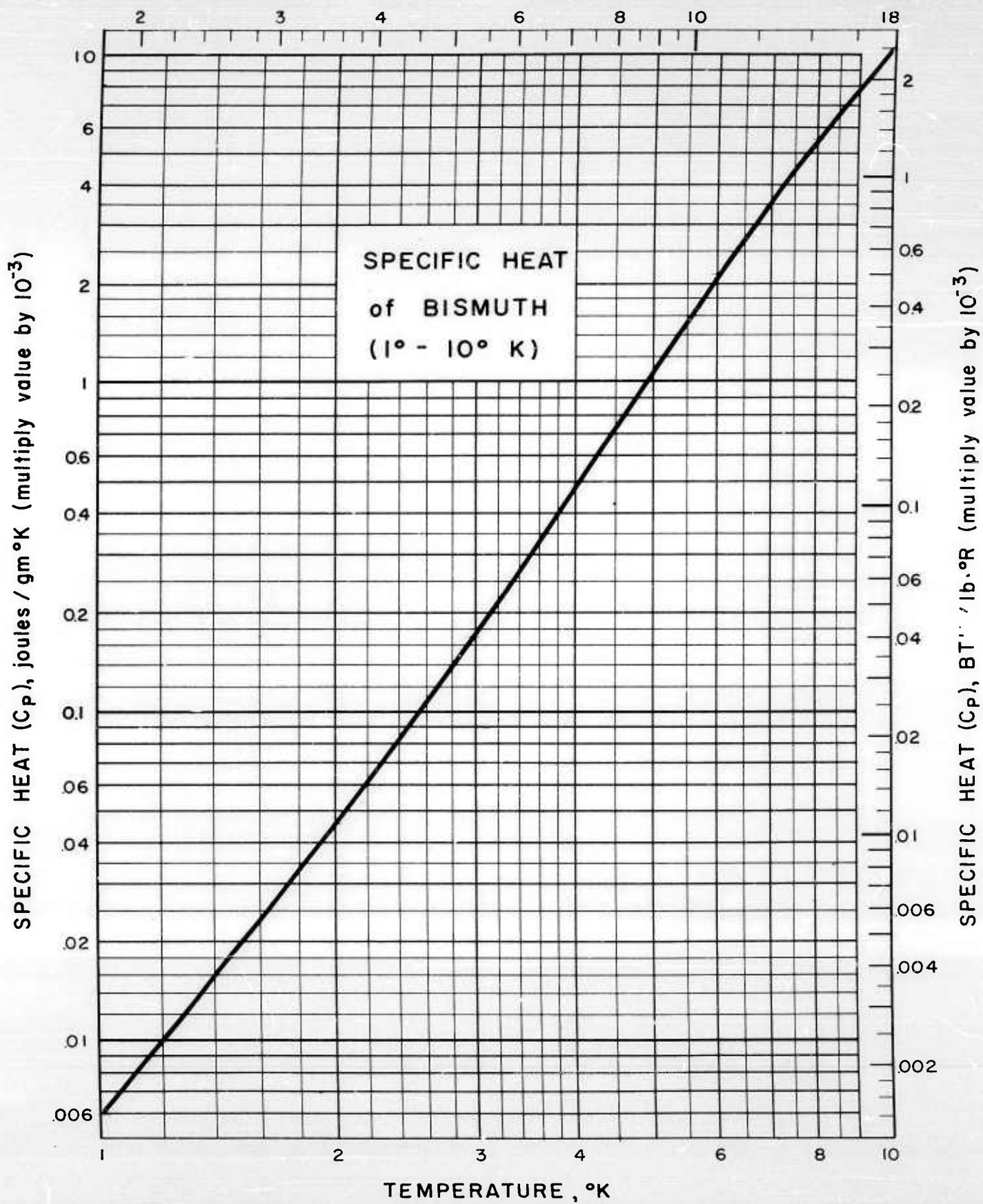
In the temperature range from 0° to 2°K, the specific heat C_p follows the equation:

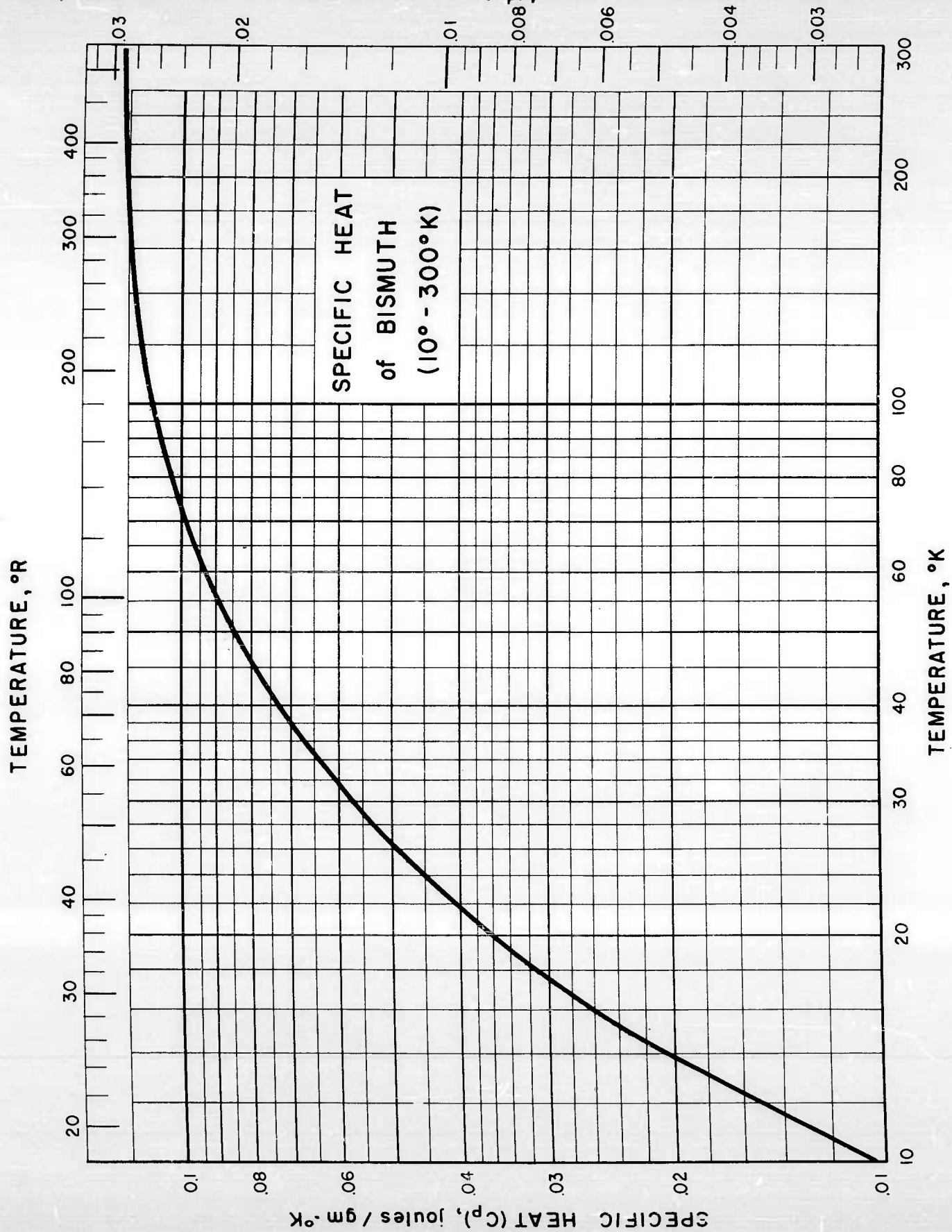
$$C_p = (3.2 \pm 0.2) \times 10^{-7} T + 9.303 \left(\frac{T}{118 \pm 1} \right)^3 \text{ j/gm-}^\circ\text{K}$$

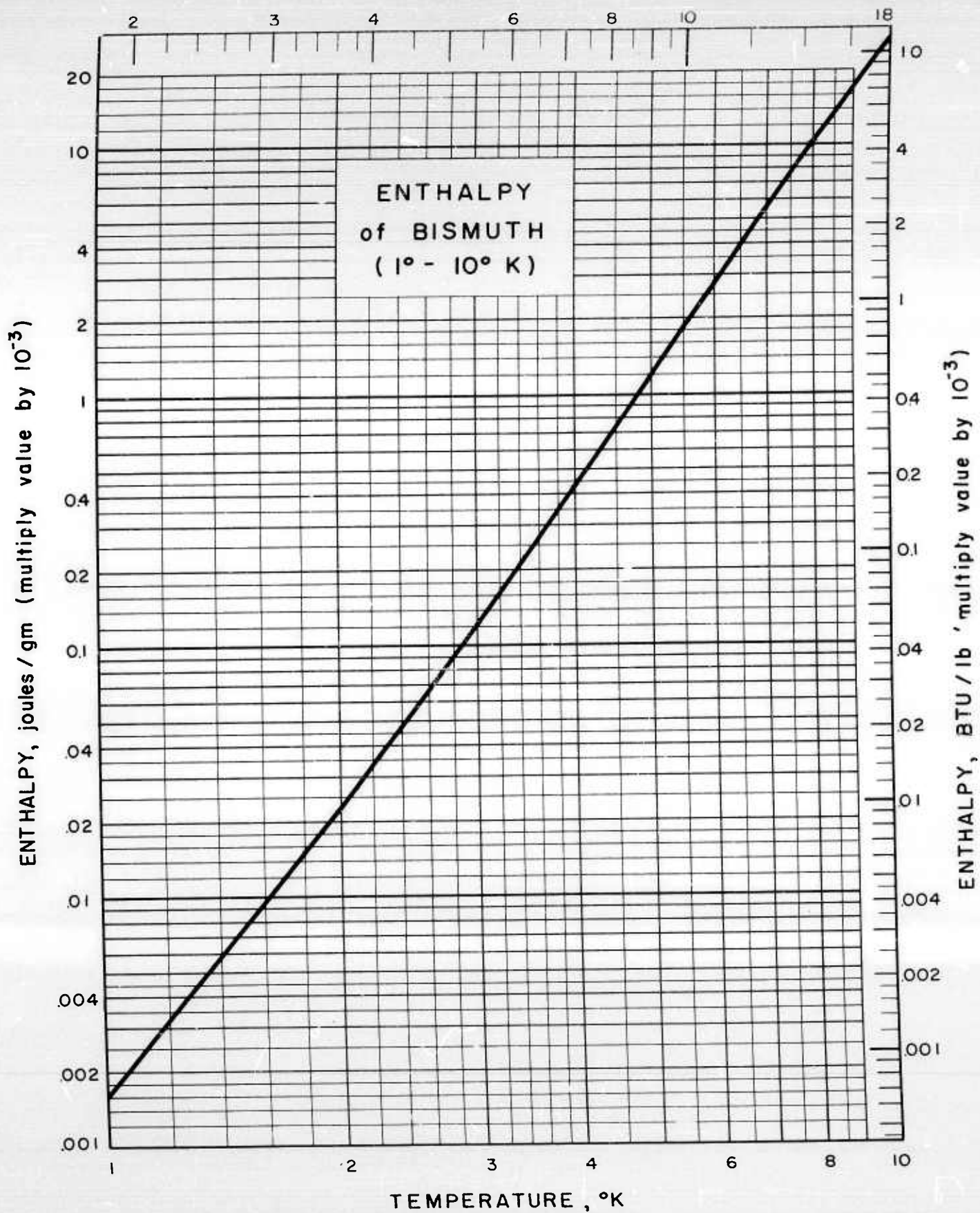
Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|-------------|-------------|------------------|-----------|
| 1 | 0.000 00598 | 0.000 00158 | 70 | 0.100 | 4.03 |
| 2 | .000 0461 | .000 0233 | 80 | .105 | 5.05 |
| 3 | .000 170 | .000 123 | 90 | .108 | 6.12 |
| 4 | .000 493 | .000 432 | 100 | .111 | 7.21 |
| 6 | .002 14 | .002 88 | 120 | .114 | 9.45 |
| 8 | .005 47 | .010 2 | 140 | .116 | 11.8 |
| 10 | .010 4 | .025 9 | 160 | .118 | 14.1 |
| 15 | .023 8 | .111 | 180 | .119 | 16.5 |
| 20 | .036 3 | .262 | 200 | .120 | 18.9 |
| 25 | .047 7 | .472 | 220 | .121 | 21.3 |
| 30 | .057 2 | .734 | 240 | .122 | 23.7 |
| 40 | .072 7 | 1.38 | 260 | .122 | 26.2 |
| 50 | .084 6 | 2.17 | 280 | .123 | 28.6 |
| 60 | .093 5 | 3.06 | 300 | .124 | 31.1 |

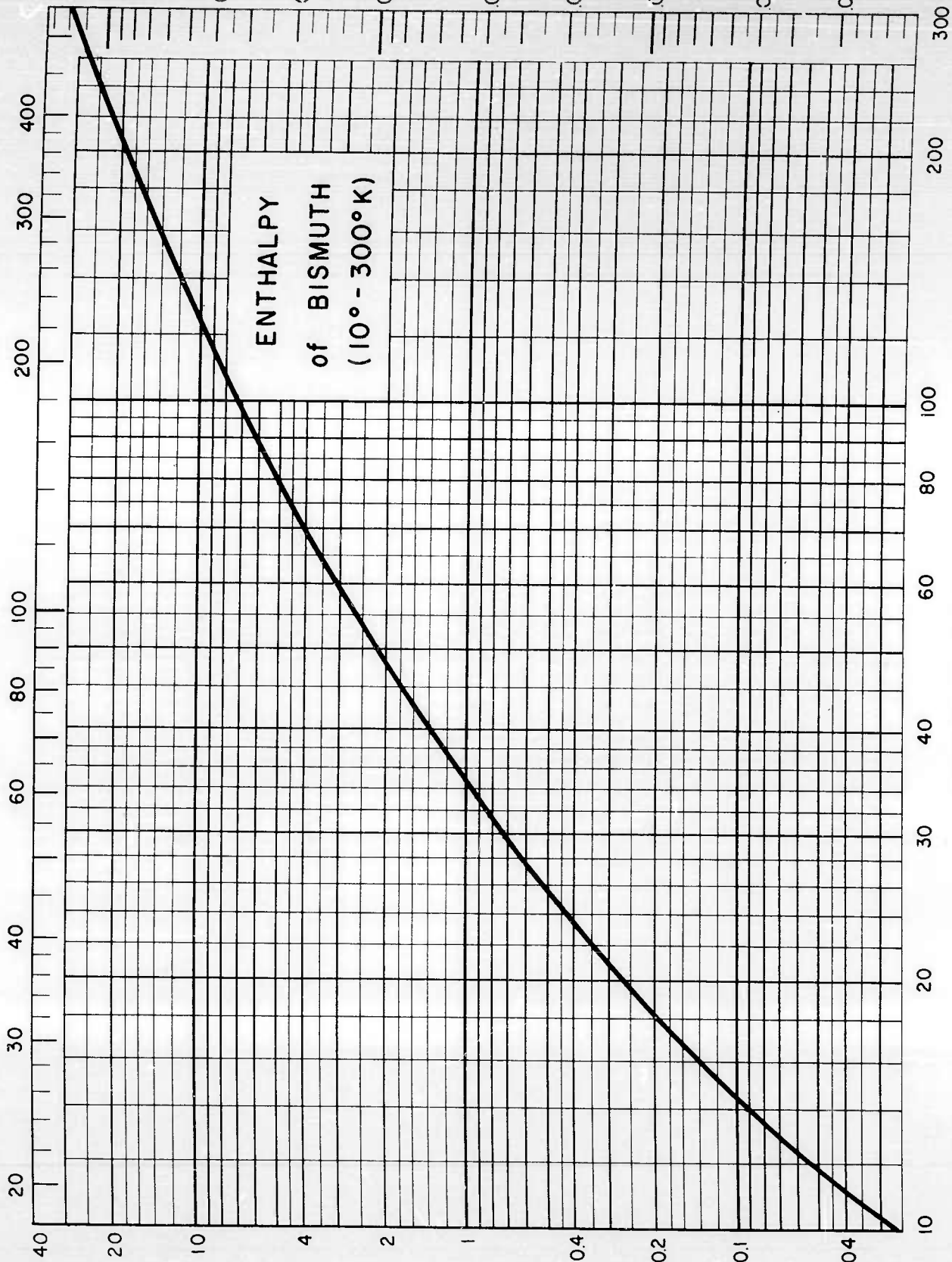
JJG/JRC Issued: 10-19-59
 Revised: 5-20-60



SPECIFIC HEAT (C_p), BTU/lb·°R



TEMPERATURE, °R



ENTHALPY, joules/gm

ENTHALPY
of BISMUTH
(10° - 300°K)

ENTHALPY, BTU/lb

TEMPERATURE, °K

SPECIFIC HEAT, ENTHALPY of CHROMIUM

Sources of Data:

- Anderson, C. T., J. Am. Chem. Soc. 59, 488-91 (1937)
 Rayne, J. A. and Kemp, W. R. G., Phil. Mag. (8) 1, 918-25 (1956)
 Wolcott, N. M., Conf. Physique Basses Temp., Paris (1955)

Other References:

- Adler, F. W., Ann. Physik. Beiblätter 27, 330 (1903)
 Estermann, I., Friedberg, S. A. and Goldman, J. E., Phys. Rev. 87, 582-8 (1952)
 Forch, C. and Nordmeyer, P., Ann. Physik. (4) 20, 423 (1906)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
 Simon, F. and Ruhemann, M., Z. physik. Chem. 129, 321 (1927)
 Weertman, J. R., Burk, D. and Goldman, J. E., Phys. Rev. 86, 628 (1952)
 Friedberg, S. A., Estermann, I. and Goldman, J. E., Phys. Rev. 85, 375 (1952)

Comments:

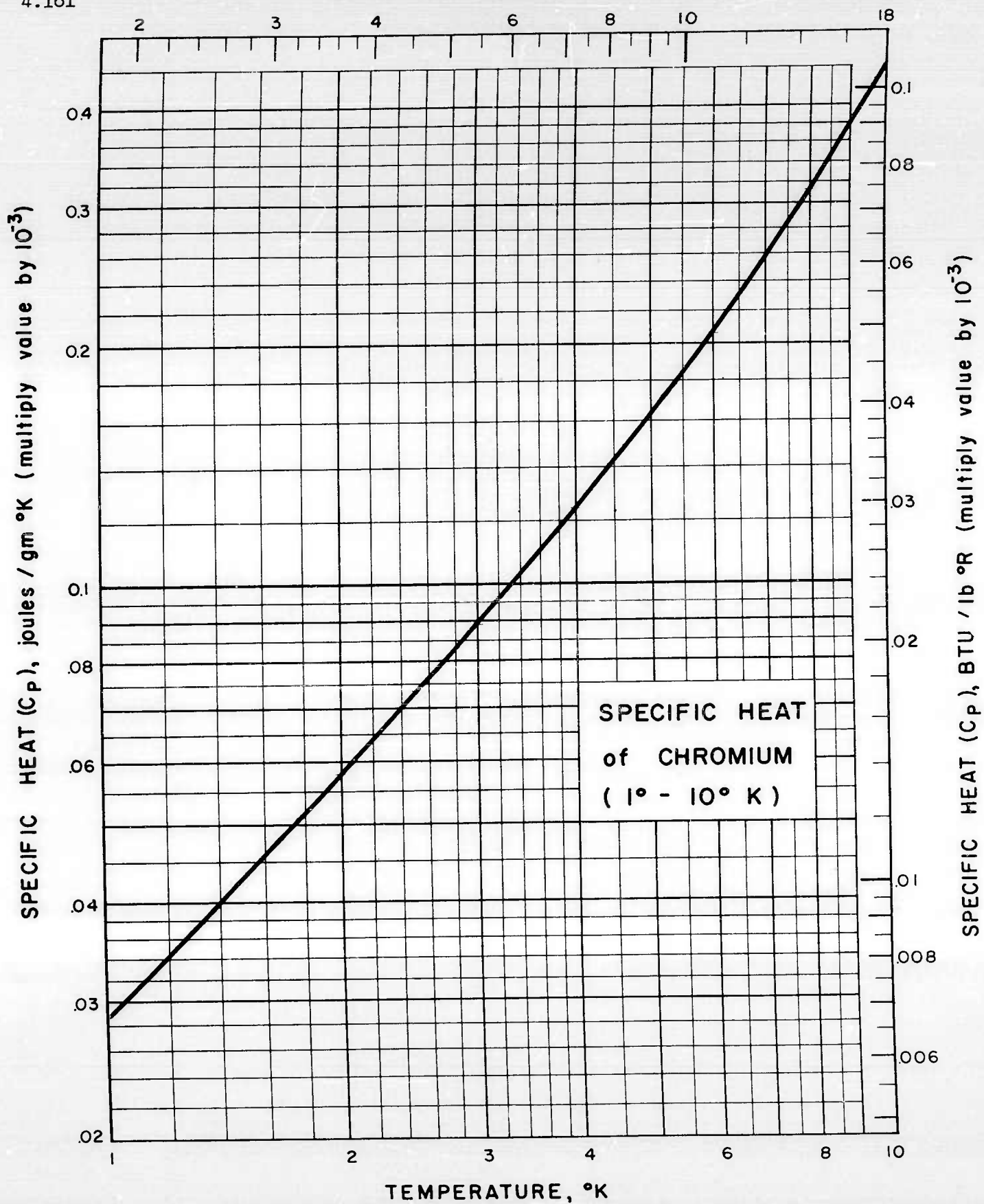
For temperatures from 0° to 4°K, the specific heat C_p follows the equation:

$$C_p = (2.83 \pm 0.12) \times 10^{-5} T + 37.39 \left(\frac{T}{610 \pm 30} \right)^3 \text{ j/gm-}^\circ\text{K}$$

Table of Selected Values

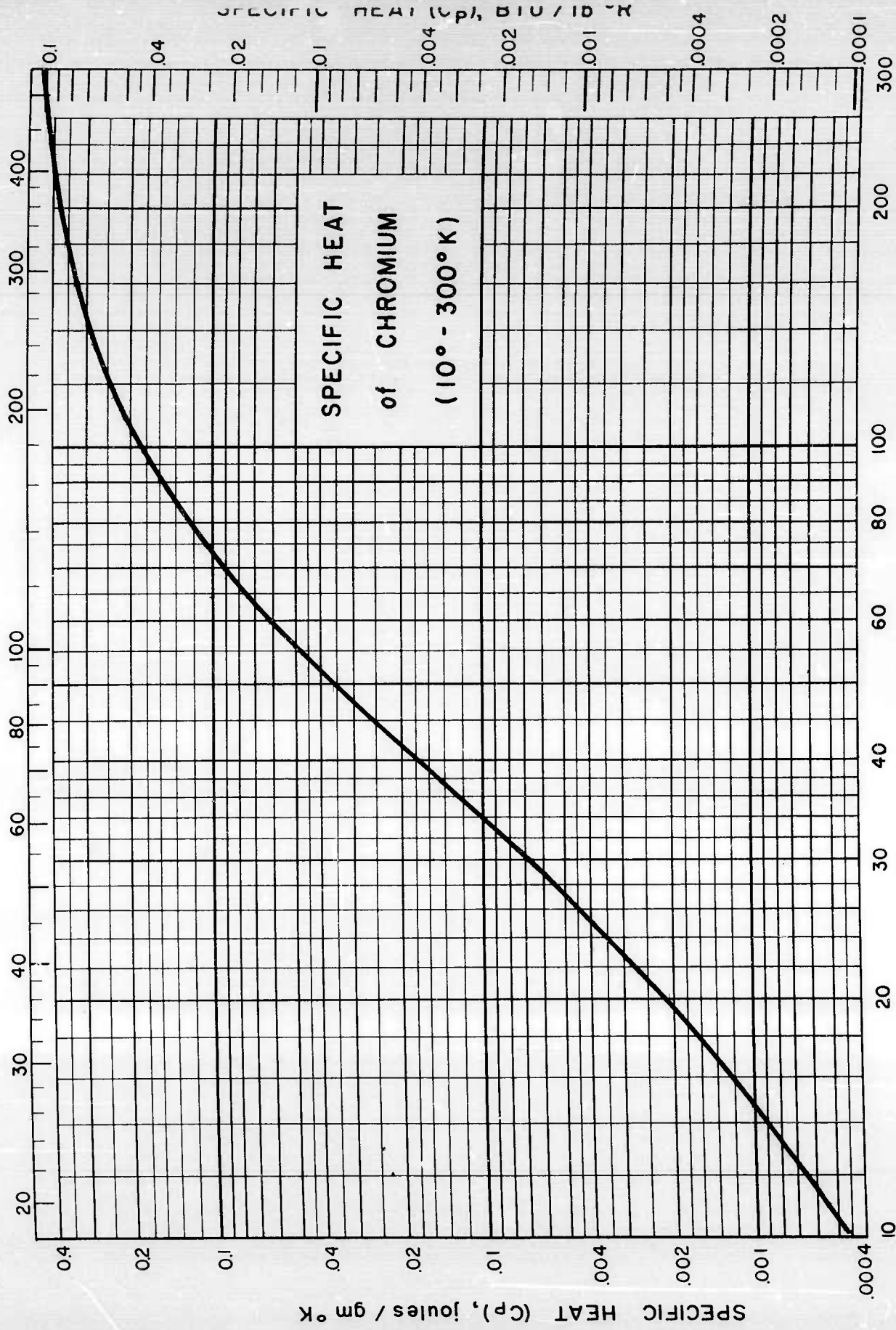
| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|------------|-------------|------------------|-----------|
| 1 | 0.000 0285 | 0.000 0142 | 70 | 0.093 | 1.68 |
| 2 | .000 058 | .000 0573 | 80 | .127 | 2.77 |
| 3 | .000 089 | .000 131 | 90 | .161 | 4.21 |
| 4 | .000 124 | .000 237 | 100 | .193 | 5.98 |
| 6 | .000 206 | .000 567 | 120 | .249 | 10.4 |
| 8 | .000 312 | .001 07 | 140 | .296 | 15.9 |
| 10 | .000 451 | .001 82 | 160 | .332 | 22.2 |
| 15 | .001 02 | .005 28 | 180 | .361 | 29.1 |
| 20 | .002 10 | .012 8 | 200 | .385 | 36.6 |
| 25 | .003 92 | .027 4 | 220 | .404 | 44.5 |
| 30 | .006 83 | .053 2 | 240 | .419 | 52.7 |
| 40 | .017 1 | .163 | 260 | .431 | 61.2 |
| 50 | .035 8 | .421 | 280 | .441 | 70.0 |
| 60 | .062 1 | .904 | 300 | .450 | 78.9 |

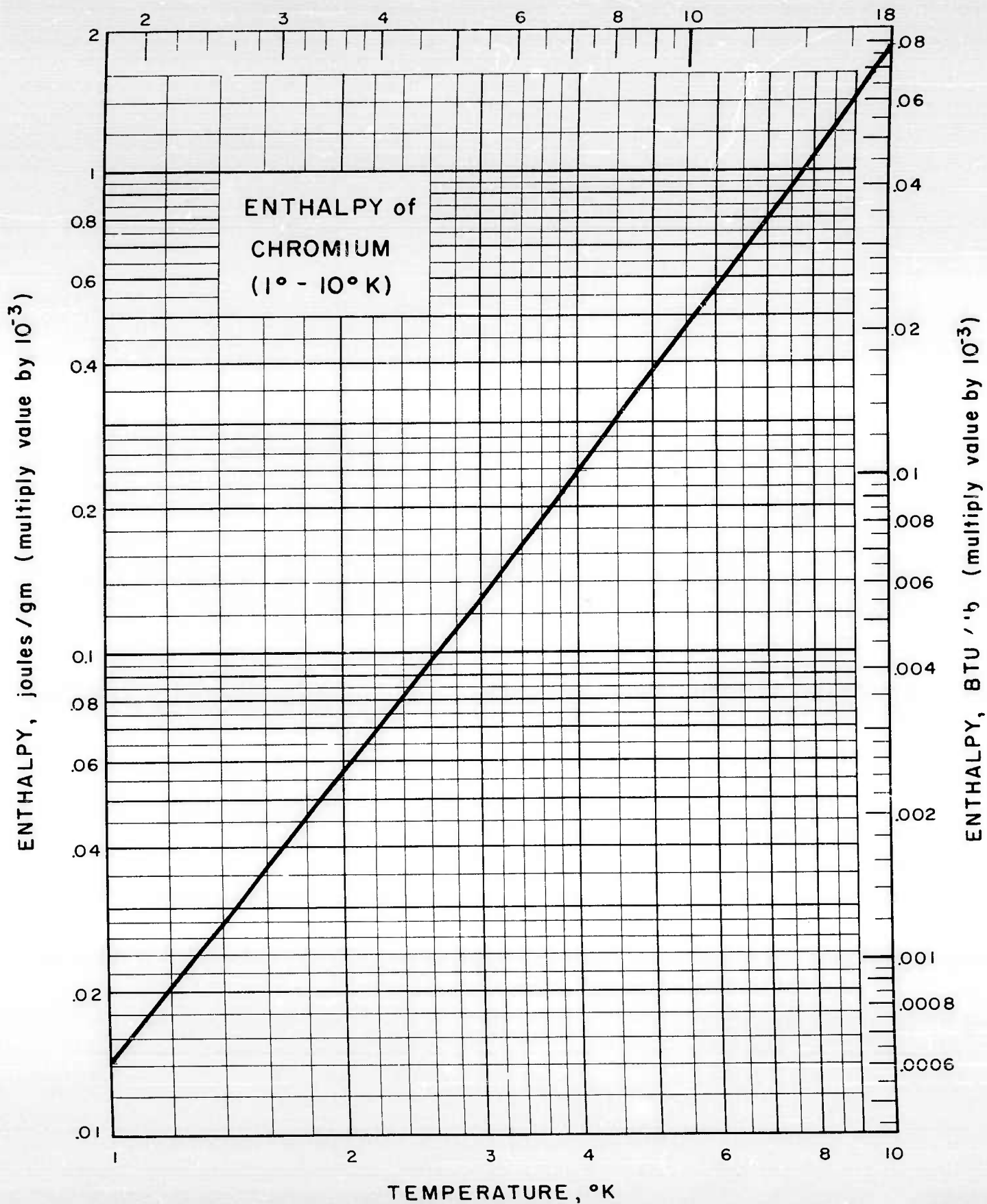
RJC Issued: 12-18-59
 Revised: 5-20-60

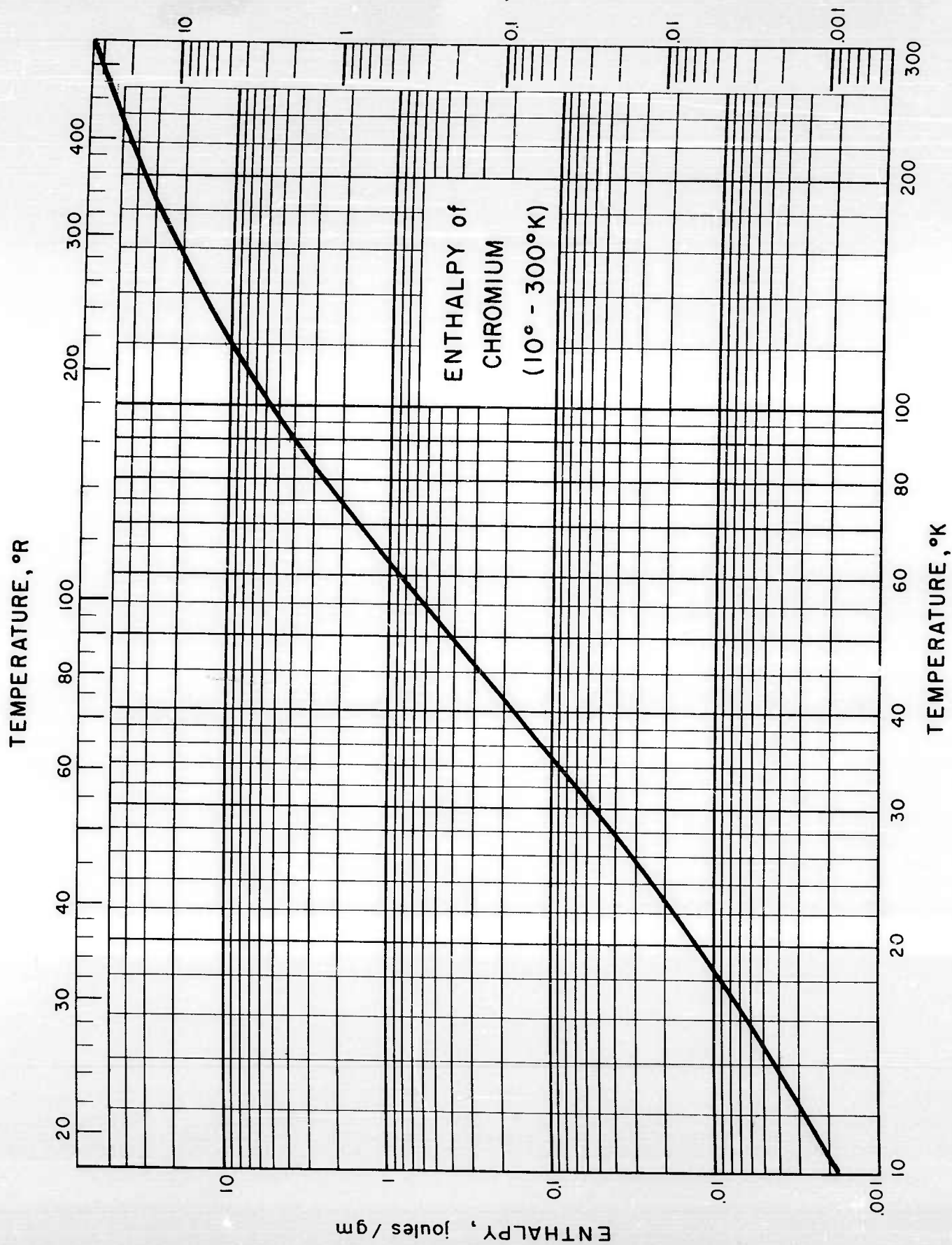


4.161

TEMPERATURE, °R







SPECIFIC HEAT, ENTHALPY of MOLYBDENUM

Sources of Data:Horowitz, M. and Daurt, J. G., Phys. Rev. 91, 1099-1106 (1953)Rayne, J. A., Phys. Rev. 95, 1428-34 (1954)Simon, F. and Zeidler, W., Z. physik. Chem. 123, 383-404 (1926)Other References:Cooper, D. and Longstroeth, G., Phys. Rev. 33, 243-8 (1929)Comments:For the temperature range from 0° to 4°K, the specific heat C_p follows the equation:

$$C_p = (2.27 \pm 0.1) \times 10^{-5} T + 20.26 \left(\frac{T}{430 \pm 15} \right)^3 \text{ j/gm-}^\circ\text{K}$$

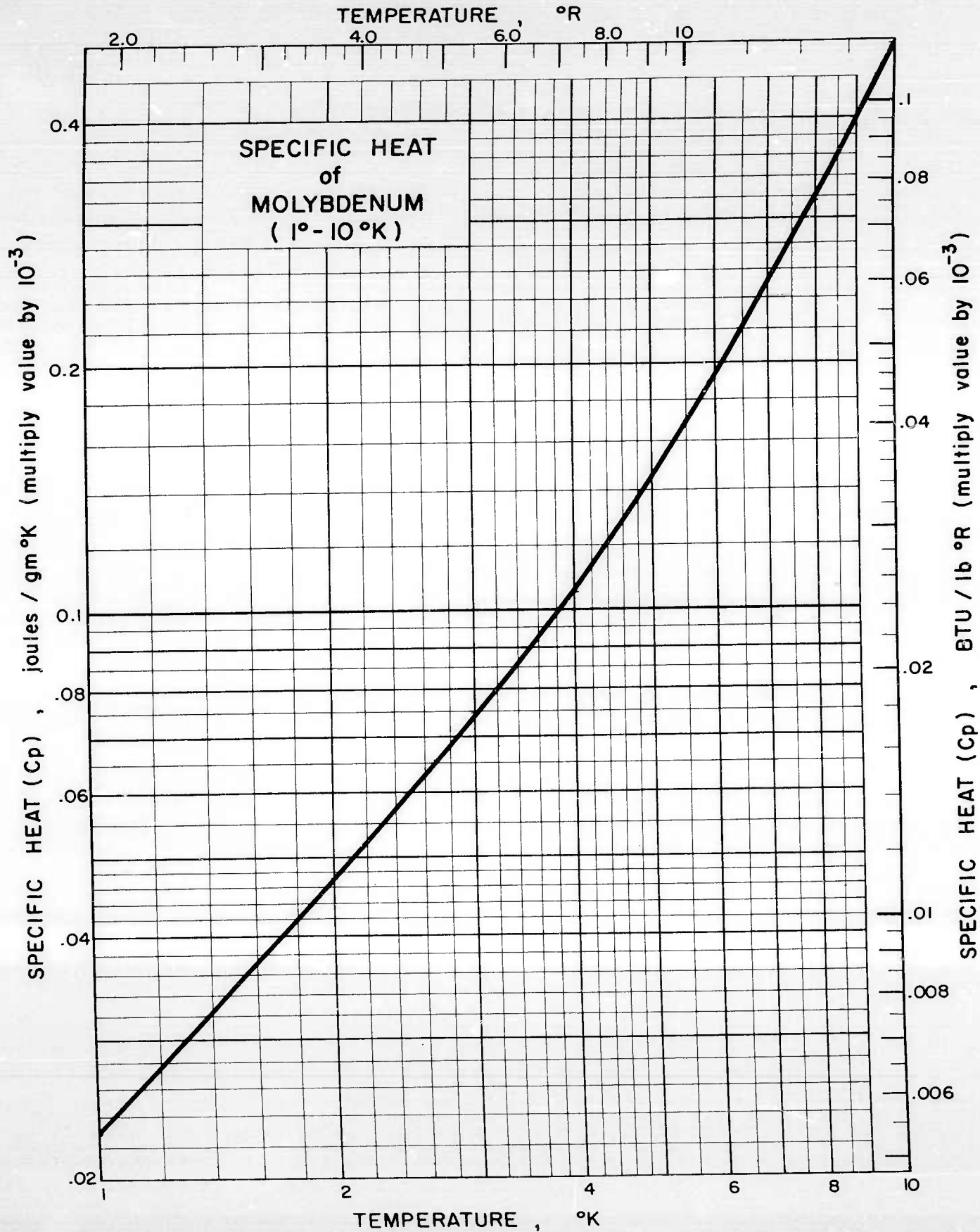
Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|------------|-------------|------------------|-----------|
| 1 | 0.000 0229 | 0.000 0105 | 70 | 0.0838 | 1.80 |
| 2 | .000 0472 | .000 0445 | 80 | .104 | 2.74 |
| 3 | .000 0745 | .000 105 | 90 | .123 | 3.88 |
| 4 | .000 106 | .000 194 | 100 | .139 | 5.20 |
| 6 | .000 191 | .000 484 | 120 | .168 | 8.27 |
| 8 | .000 317 | .000 981 | 140 | .187 | 11.8 |
| 10 | .000 498 | .001 78 | 160 | .202 | 15.7 |
| 15 | .001 31 | .006 10 | 180 | .213 | 19.9 |
| 20 | .002 87 | .016 1 | 200 | .222 | 24.2 |
| 25 | .005 77 | .037 4 | 220 | .229 | 28.7 |
| 30 | .009 60 | .072 9 | 240 | .236 | 33.4 |
| 40 | .023 6 | .232 | 260 | .240 | 38.1 |
| 50 | .041 0 | .554 | 280 | .243 | 43.0 |
| 60 | .061 9 | 1.07 | 300 | .246 | 47.9 |

RJC/JJG/VDA Issued: 12-18-59

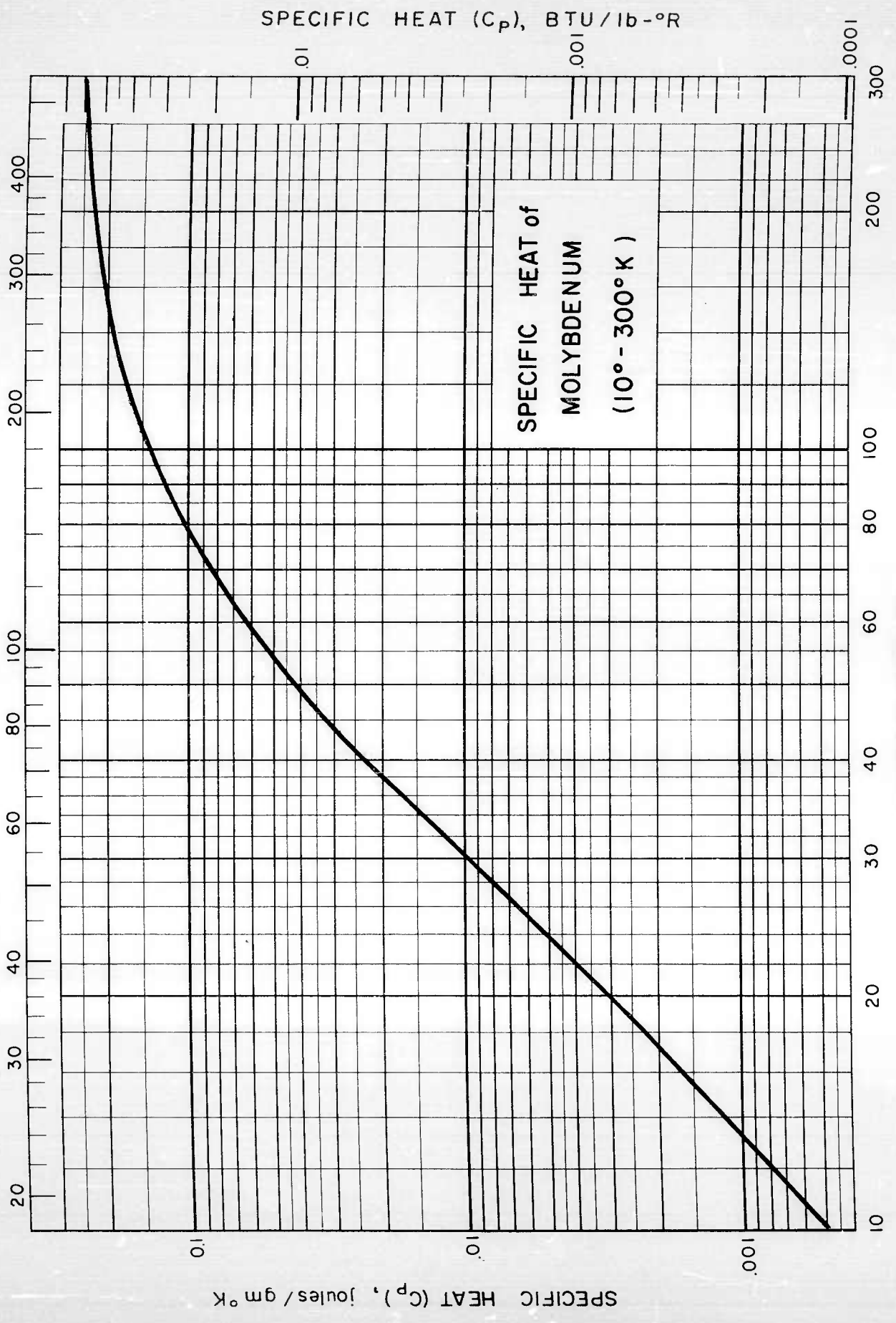
Revised: 5-20-60

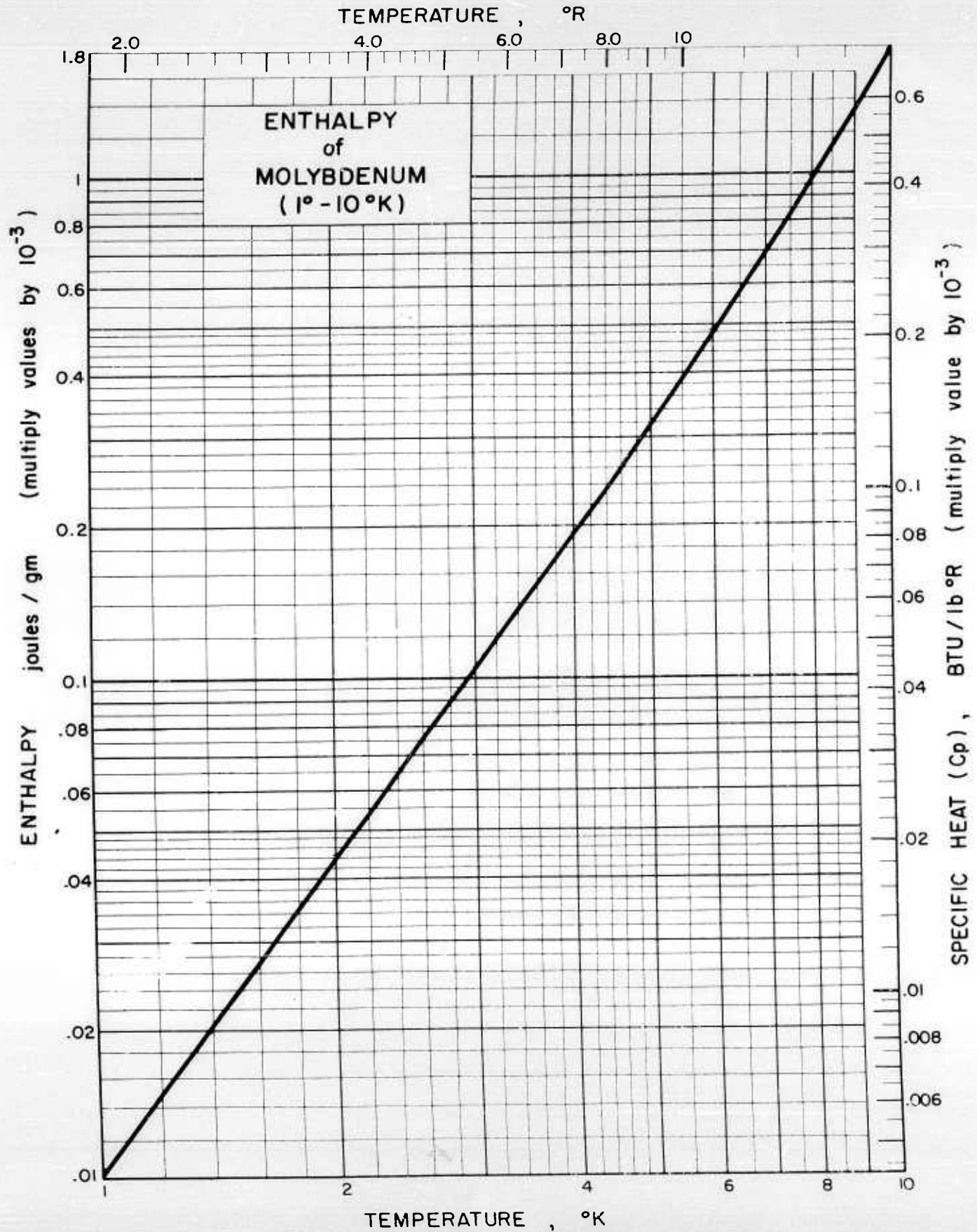
4.161



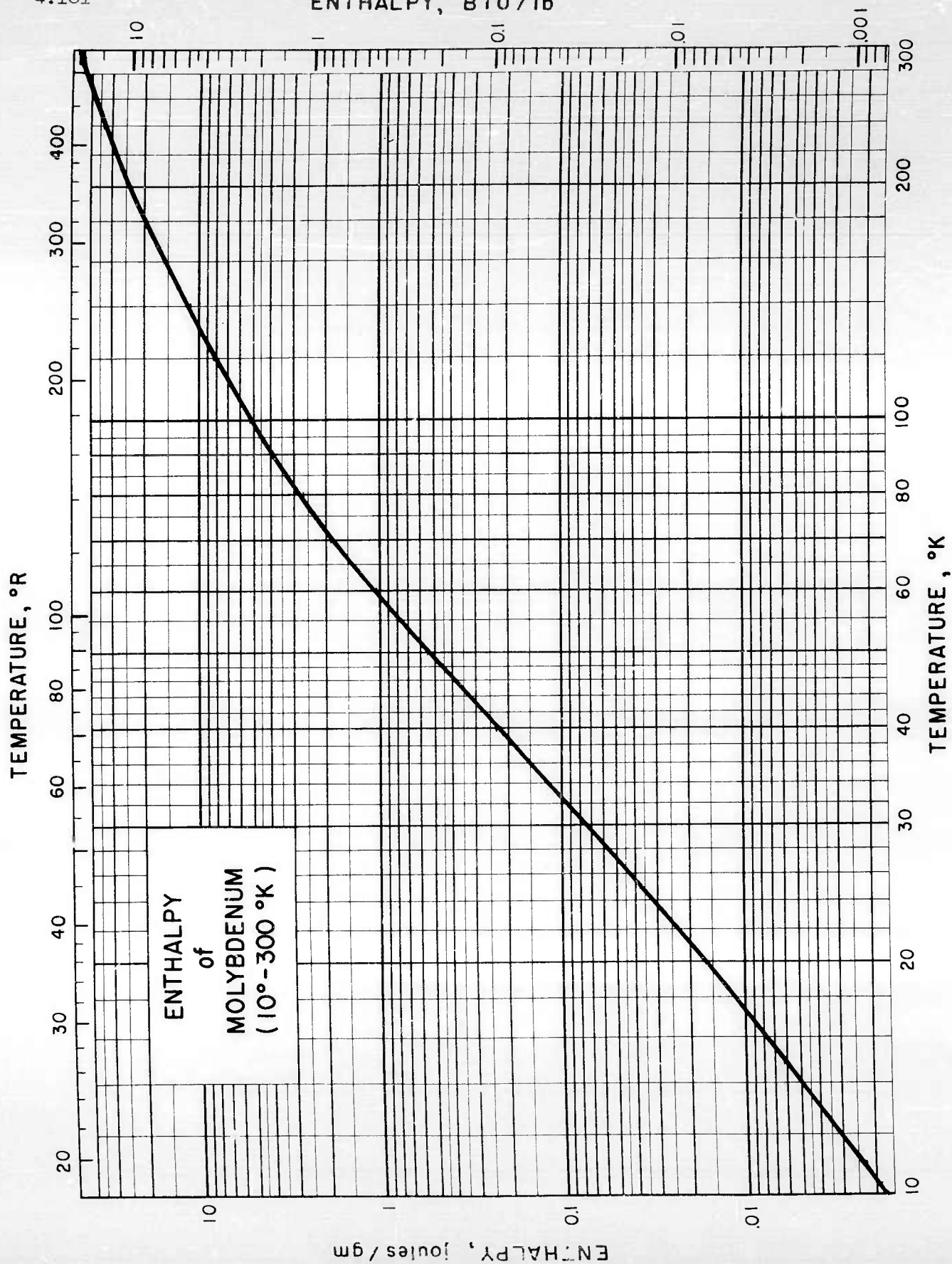
4.161

TEMPERATURE, °R





ENTHALPY, BTU/lb



SPECIFIC HEAT, ENTHALPY of TUNGSTEN

Sources of Data:

- Horowitz, M. and Daunt, J. G., Phys. Rev. 91, 1099-1106 (1953)
 Lange, F., Z. physik. Chem. 110, 343 (1924)
 Rayne, J. A., Phys. Rev. 95, 1428 (1954)
 Wolcott, N. M., Conf. Physique Basses Temp. Paris (1955)

Other References:

- Bronson, H. L., Chisholm, H. M. and Dockerty, S. M., Can. J. Research 8, 282 (1933)
 Silvidi, A. A. and Daunt, J. G., Phys. Rev. (2) 77, 125-9 (1950)
 Zwikker, C. and Schmidt, G., Physik. Z. 52, 668-77 (1928)

Comments:

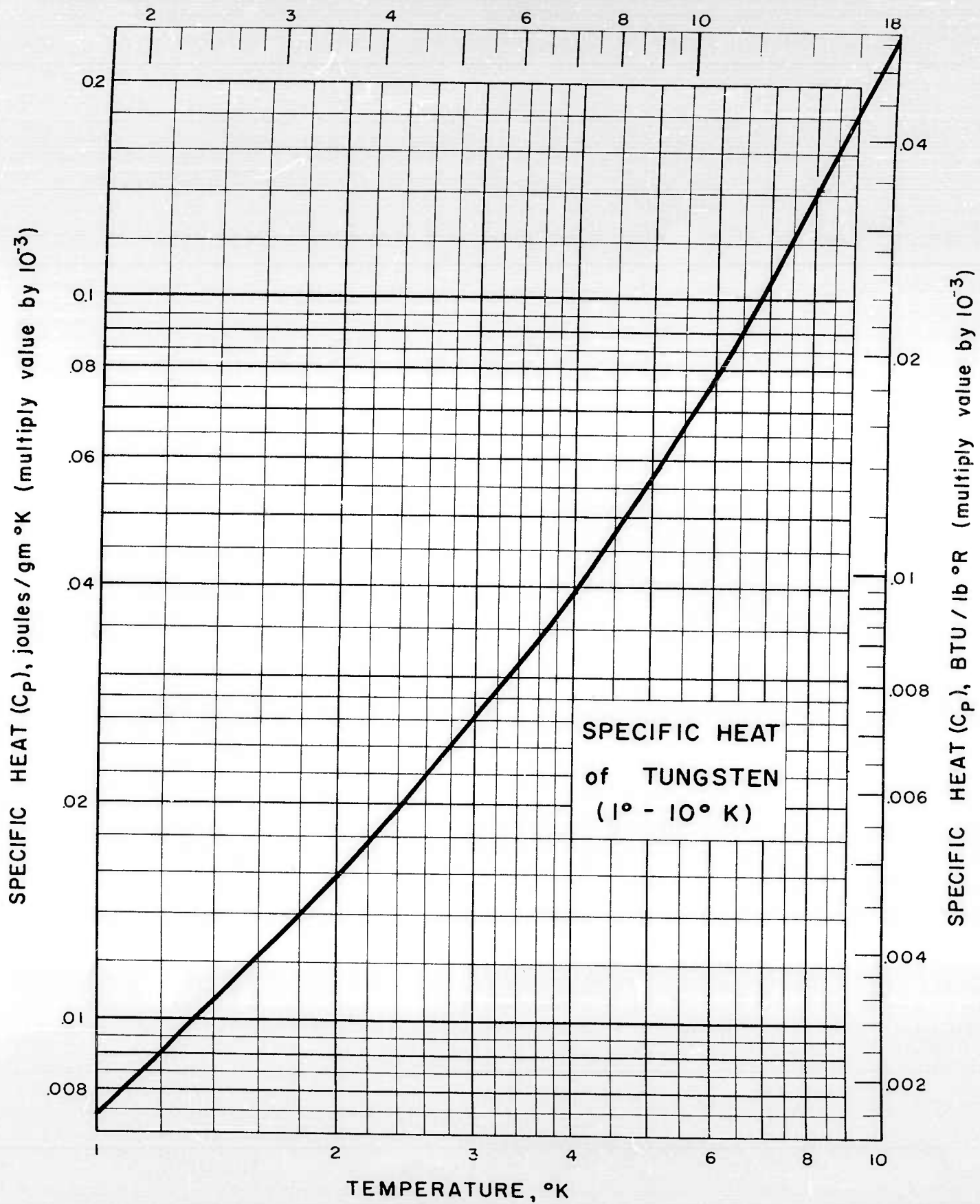
For the temperature range from 0° to 4°K the specific heat C_p follows the equation:

$$C_p = (7.3 \pm 1) \times 10^{-6} T + 10.6 \left(\frac{T}{405 \pm 20} \right)^3 \text{ j/gm-}^\circ\text{K}$$

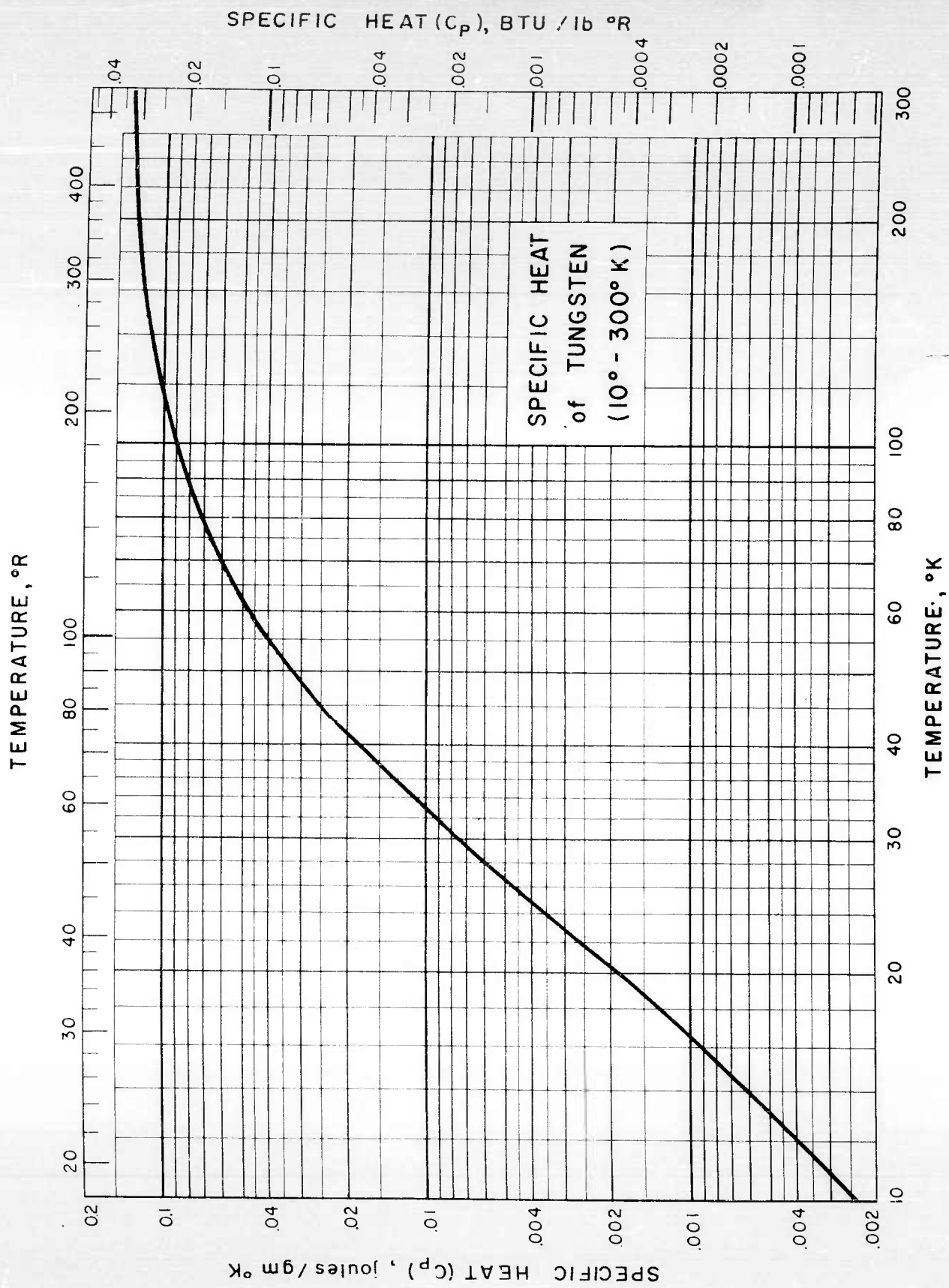
Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|------------|-------------|------------------|-----------|
| 1 | 0.000 0074 | 0.000 0037 | 70 | 0.0605 | 1.39 |
| 2 | .000 0158 | .000 0152 | 80 | .0715 | 2.05 |
| 3 | .000 0262 | .000 0360 | 90 | .0810 | 2.81 |
| 4 | .000 0393 | .000 0685 | 100 | .0888 | 3.66 |
| 6 | .000 0783 | .000 182 | 120 | .101 | 5.57 |
| 8 | .000 141 | .000 396 | 140 | .110 | 7.68 |
| 10 | .000 234 | .000 765 | 160 | .117 | 9.95 |
| 15 | .000 725 | .002 97 | 180 | .122 | 12.3 |
| 20 | .001 89 | .009 27 | 200 | .125 | 14.8 |
| 25 | .004 21 | .023 7 | 220 | .128 | 17.4 |
| 30 | .007 83 | .053 4 | 240 | .130 | 20.0 |
| 40 | .018 4 | .181 | 260 | .132 | 22.6 |
| 50 | .033 2 | .436 | 280 | .134 | 25.3 |
| 60 | .048 3 | .843 | 300 | .136 | 28.0 |

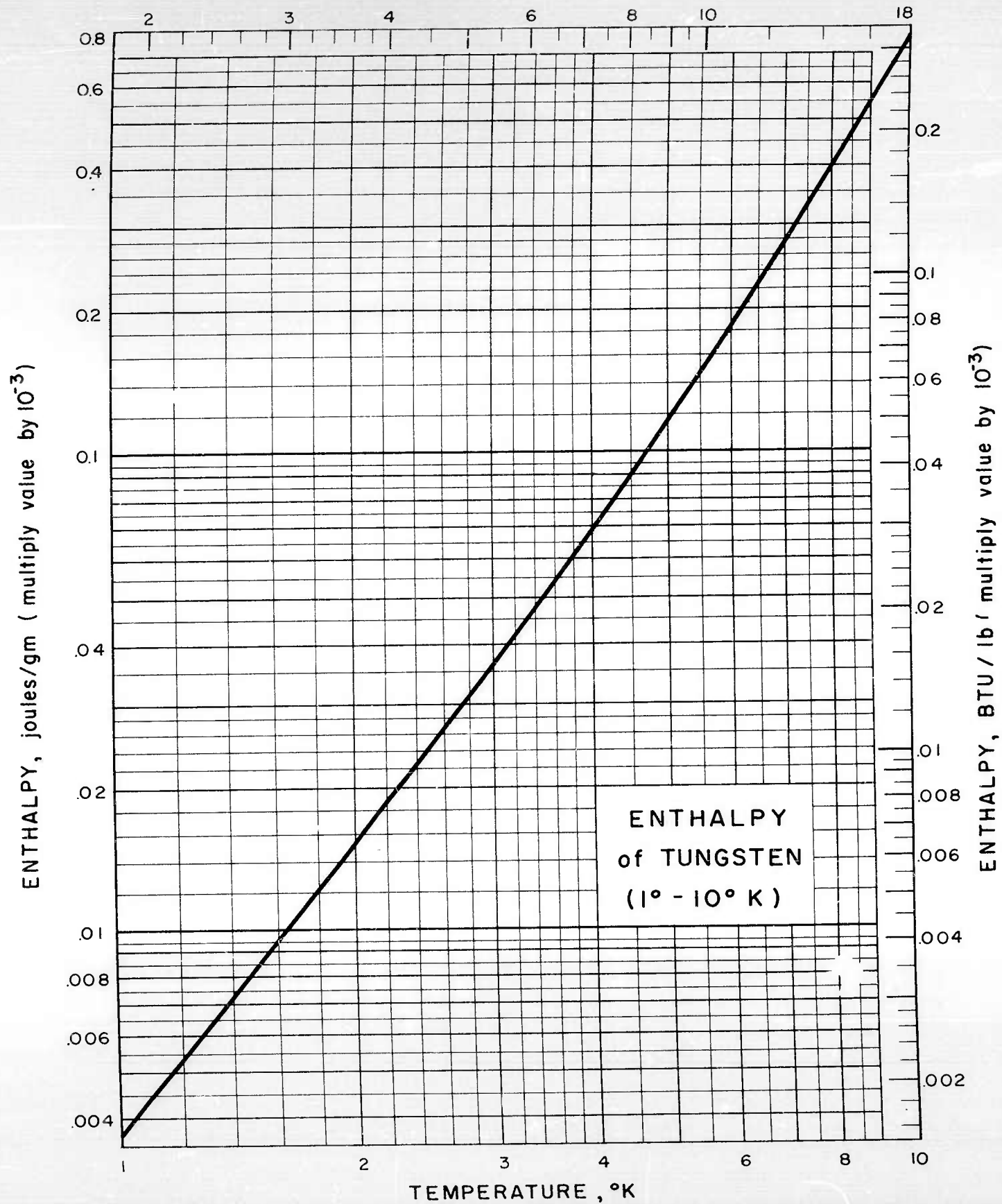
RJC/JJG Issued: 12-18-59
 Revised: 5-20-60



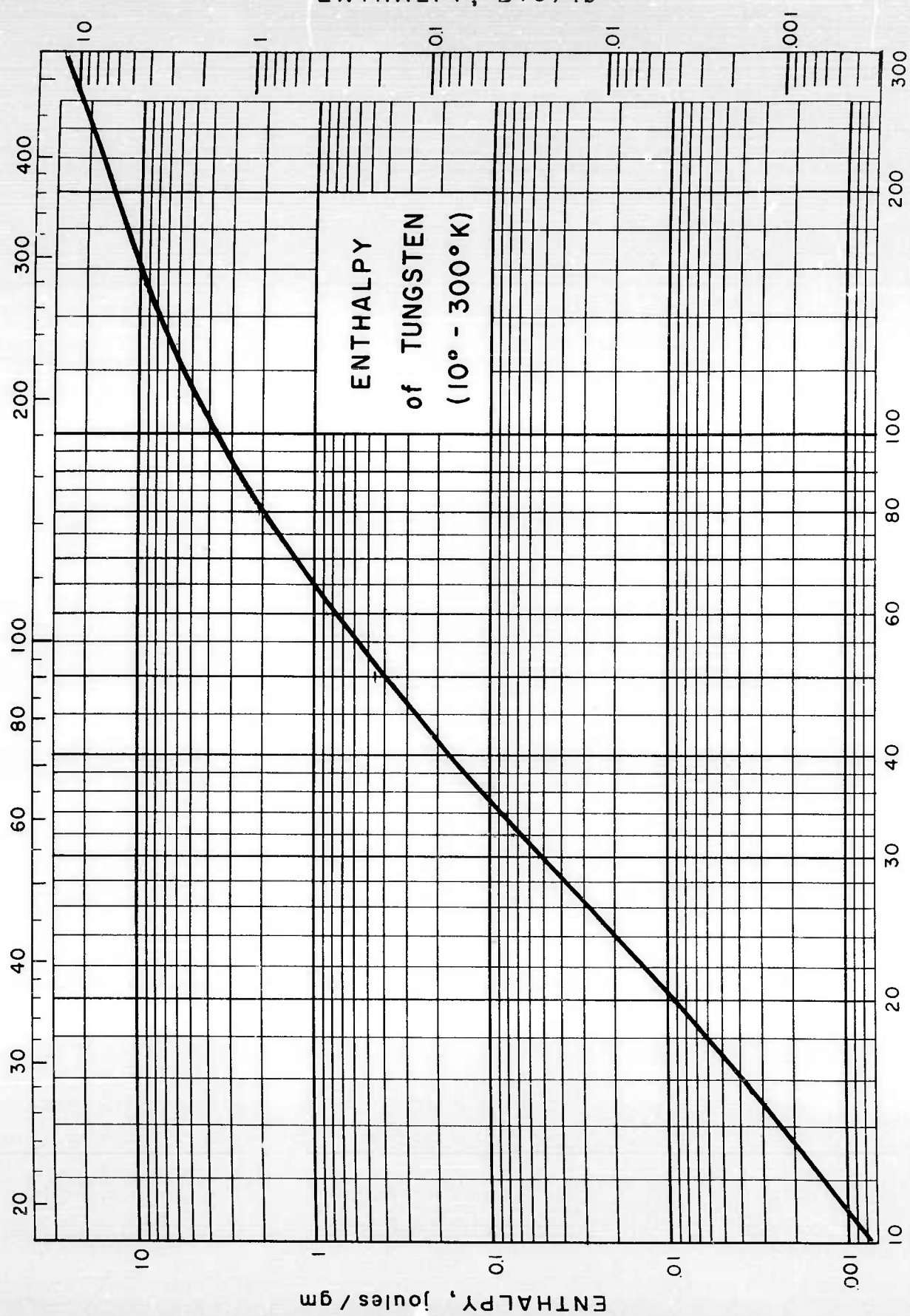
SPECIFIC HEAT
of TUNGSTEN
(1° - 10° K)



TEMPERATURE, °R



TEMPERATURE, °R



ENTHALPY, joules / gm

TEMPERATURE, °K

Sources of Data:

Booth, G. L., Hoare, F. E., and Murphy, B. T., Proc. Phys. Soc. (London) 68B, 830 (1955)

Guthrie, G., Friedberg, S. A., and Goldman, J. E., Phys. Rev. 98, 1181 (1955)

Shomate, E. H., J. Chem. Phys. 13, 326 (1945)

Other References:

Armstrong, L. D., and Grayson-Smith, H., Can. J. Research A27, 9 (1949)

Elson, R. G., Grayson-Smith, H., and Wilhelm, J. O., Can. J. Research A18, 83 (1940)

Kelley, K. K., J. Am. Chem. Soc. 61, 203 (1939)

Richards, T. W., and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)

Wolcott, N. M., Conf. Phys. basses temp. (1955)

Comments:

α Mn is stable at all temperatures up to about 730°C. A small peak in C_p is found centering at 95°K which is due to an antiferromagnetic transition (Neel point). The data of Armstrong and Grayson-Smith, Elson, Grayson-Smith and Wilhelm, and Wolcott in the region up to 20°K form a self-consistent set that is 20 to 30% higher than the data of Booth, Hoare and Murphy, and Guthrie, Friedberg and Goldman. The latter have been adopted because these authors present more conclusive evidence of the chemical and phase purity of their samples.

Table of Selected Values

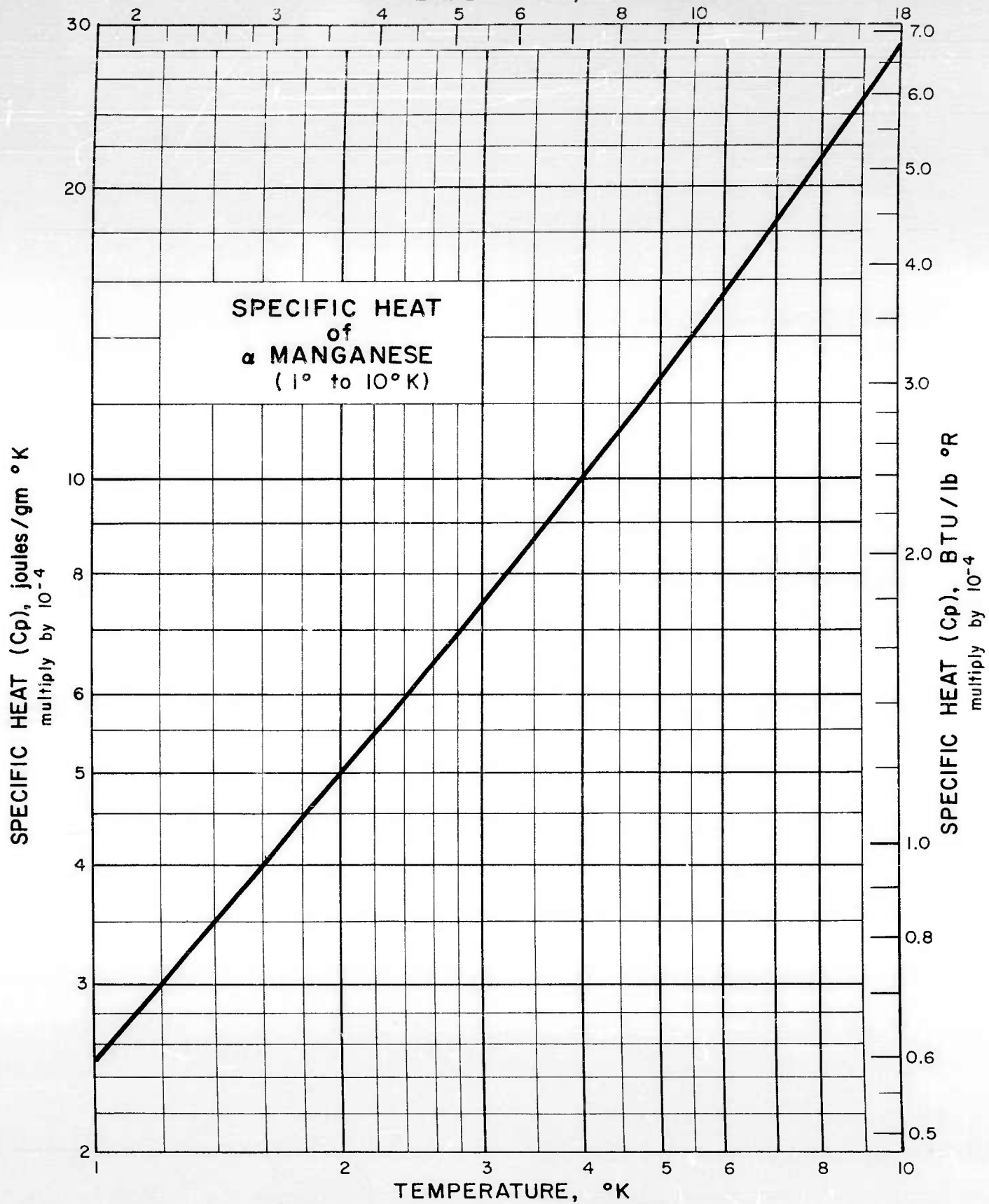
| T | C _p | H | T | C _p | H |
|----|----------------|----------|-----|----------------|-------|
| °K | j/g-deg K | j/g | °K | j/g-deg K | j/g |
| 1 | 0.000 25 | 0.000 13 | 70 | 0.171 | 3.82 |
| 2 | .000 50 | .000 50 | 80 | .214 | 5.75 |
| 3 | .000 75 | .001 12 | 90 | .257 | 8.11 |
| 4 | .001 01 | .002 01 | 95 | .273* | 9.44 |
| 6 | .001 56 | .004 6 | 100 | .267 | 10.79 |
| 8 | .002 16 | .008 3 | 120 | .312 | 16.6 |
| 10 | .002 82 | .013 3 | 140 | .349 | 23.2 |
| 15 | .005 2 | .032 7 | 160 | .379 | 30.5 |
| 20 | .009 0 | .067 | 180 | .402 | 38.3 |
| 25 | .014 7 | .126 | 200 | .420 | 46.5 |
| 30 | .023 | .219 | 220 | .435 | 55.1 |
| 40 | .050 | .57 | 240 | .448 | 63.9 |
| 50 | .087 | 1.25 | 260 | .460 | 73.0 |
| 60 | .129 | 2.32 | 280 | .470 | 82.3 |
| | | | 300 | .480 | 91.8 |

*Peak due to antiferromagnetic transition.

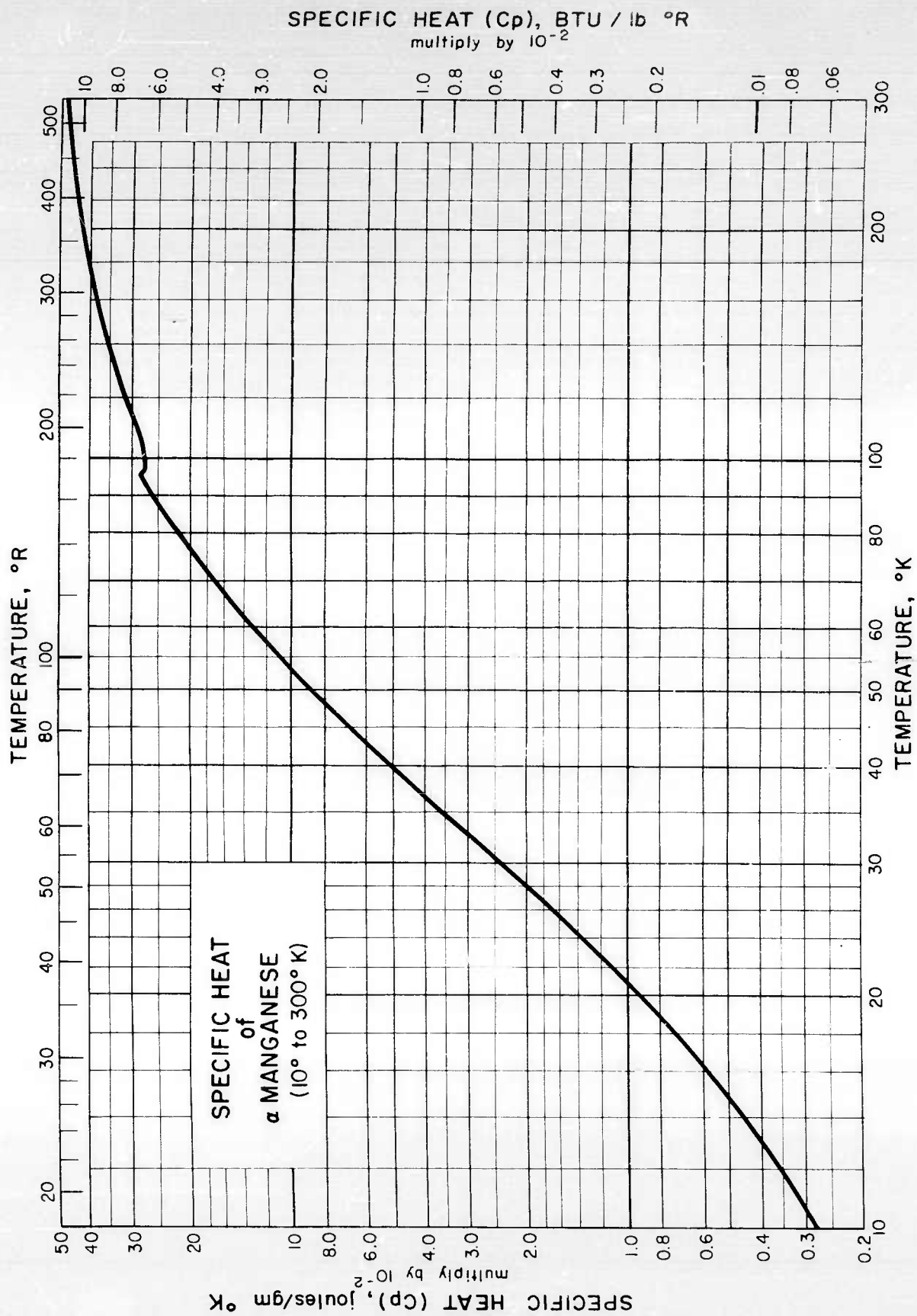
RJC Issued: 6-5-59

Revised: 5-20-60

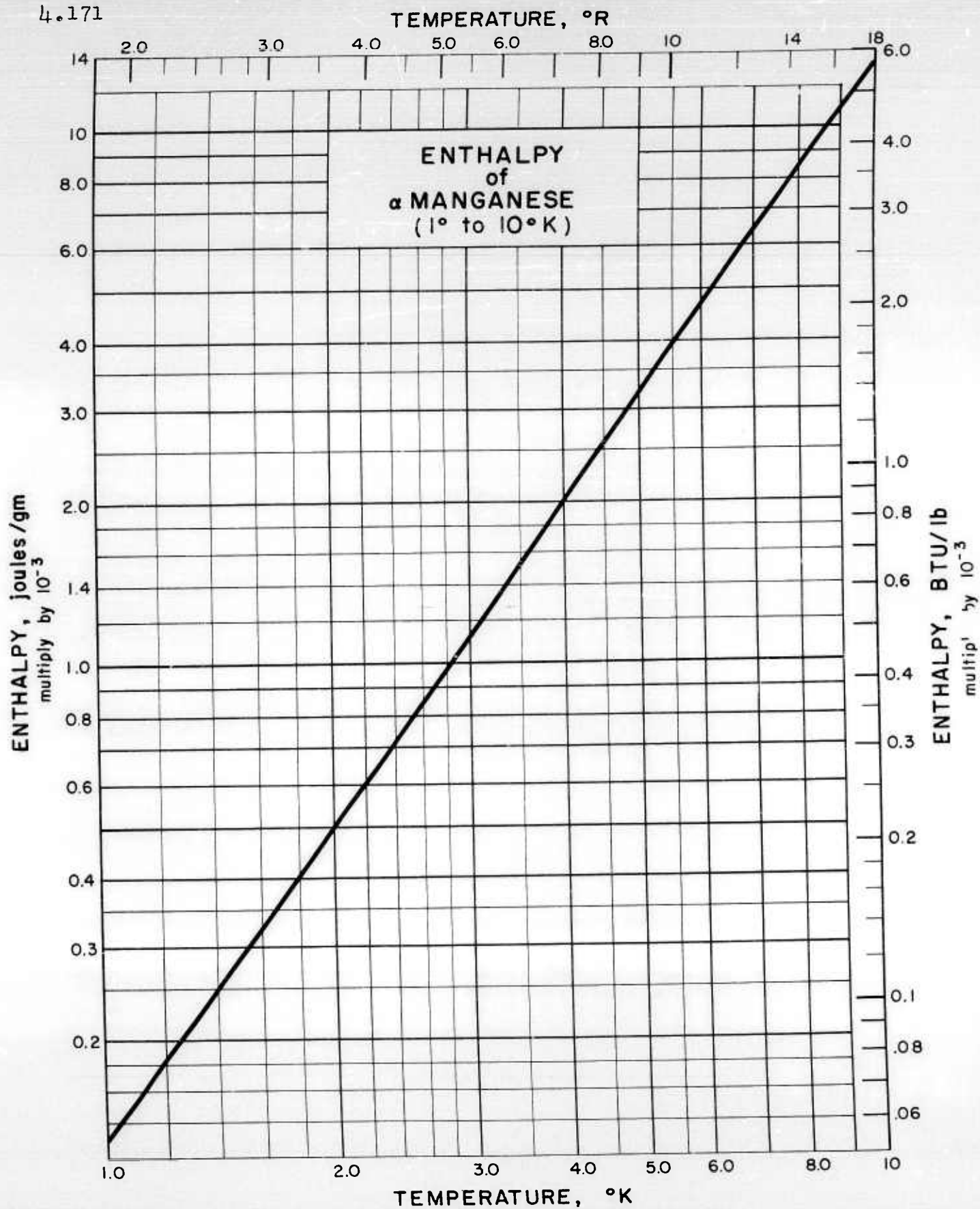
TEMPERATURE, °R



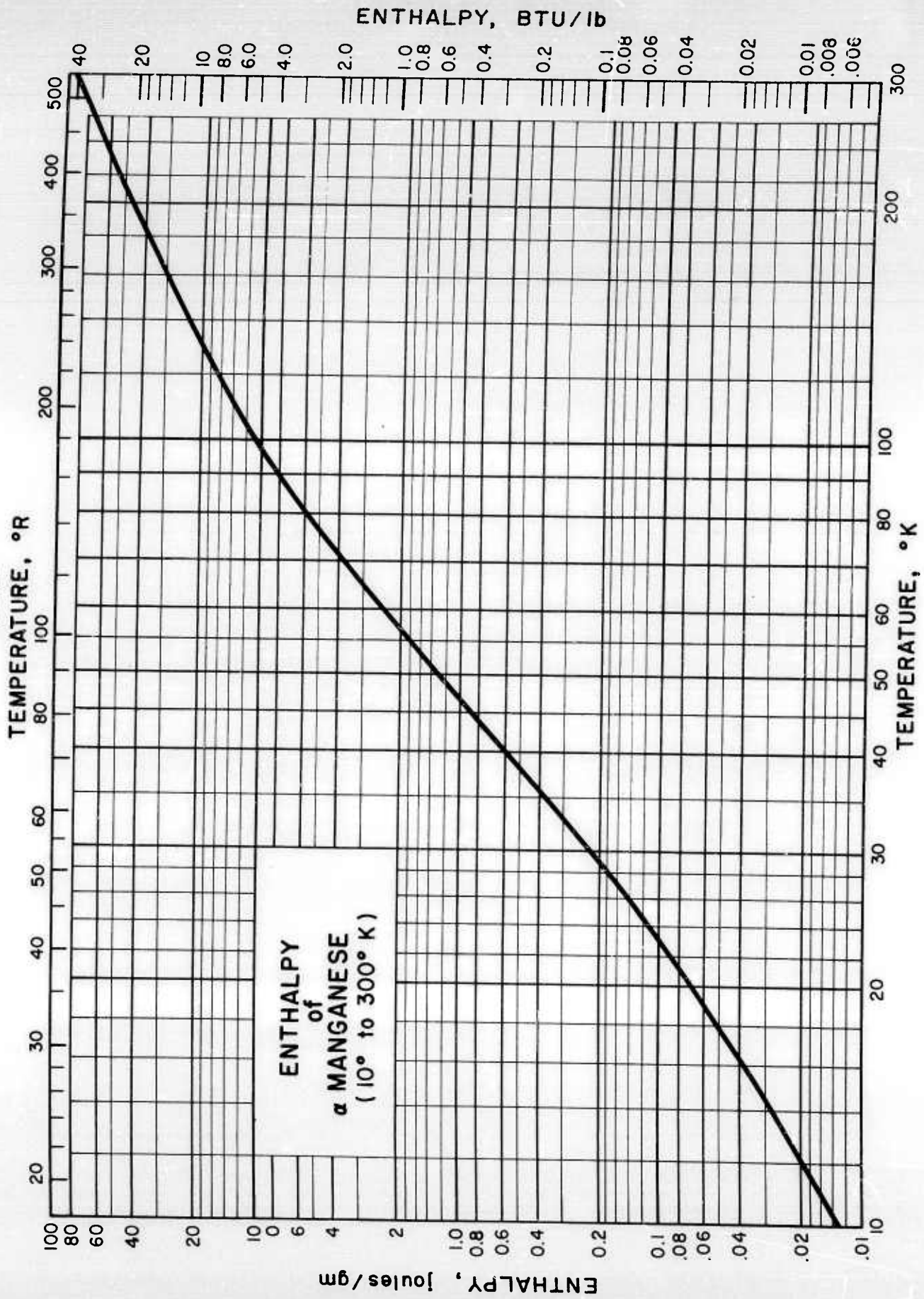
..171



4.171



4.171



SPECIFIC HEAT of MANGANESE, β FORMSource of Data:

Booth, G. L., Hoare, F. E., and Murphy, B. T., Proc. Phys. Soc. (London)
68B, 830 (1955)

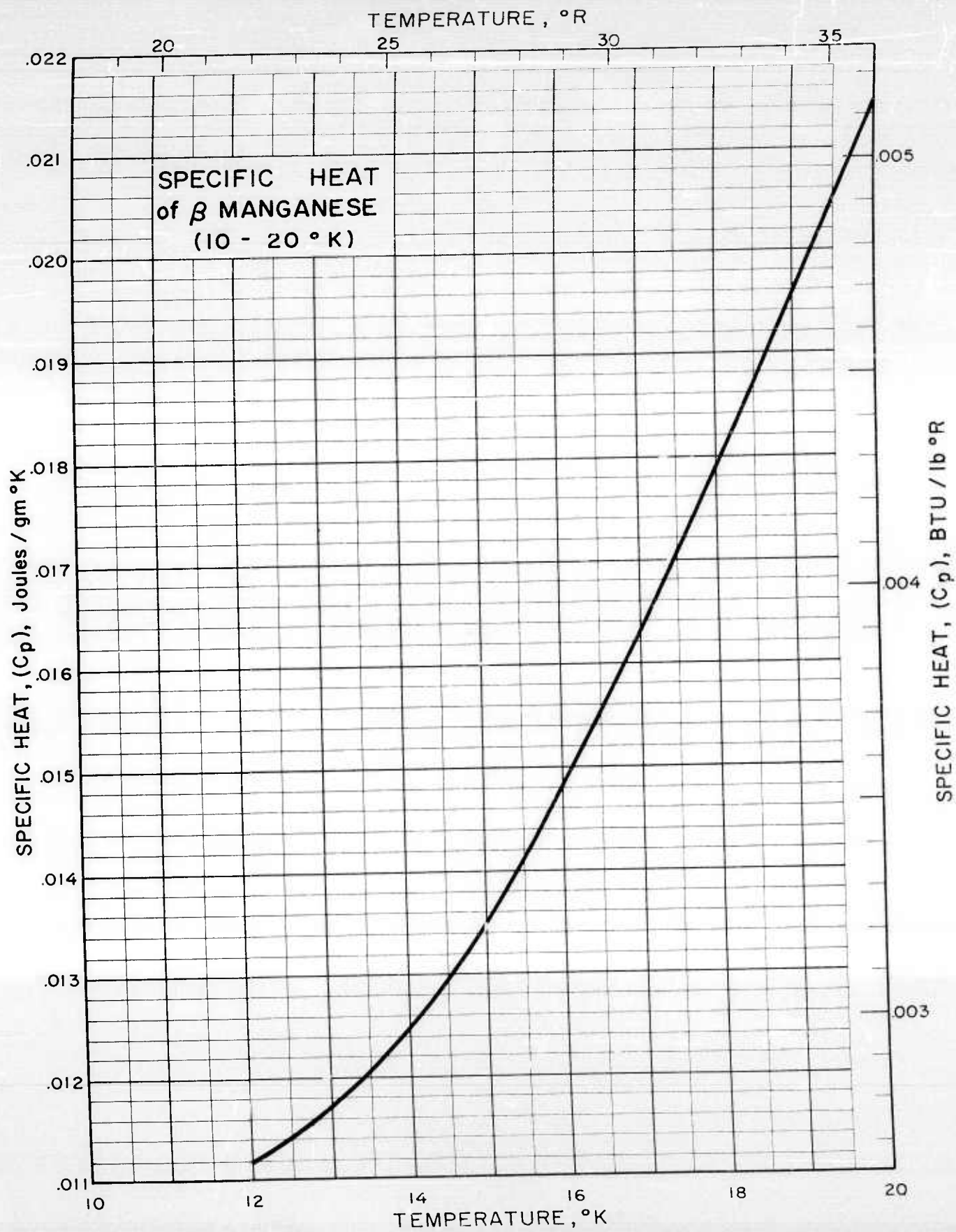
Comments:

β Mn is stable between about 730°C and 1100°C. The sample of Booth, Hoare and Murphy was produced by heating ordinary (α) manganese to 1120°C in argon, then quenching in water.

Table of Selected Values

| T °K | Cp j/gm-°K |
|---------|---------------|
| 12 | 0.0112 |
| 13 | .0117 |
| 14 | .0125 |
| 15 | .0135 |
| 16 | .0148 |
| 17 | .0163 |
| 18 | .0179 |
| 19 | .0196 |
| 20 | .0214 |

RJC Issued: 6-15-59

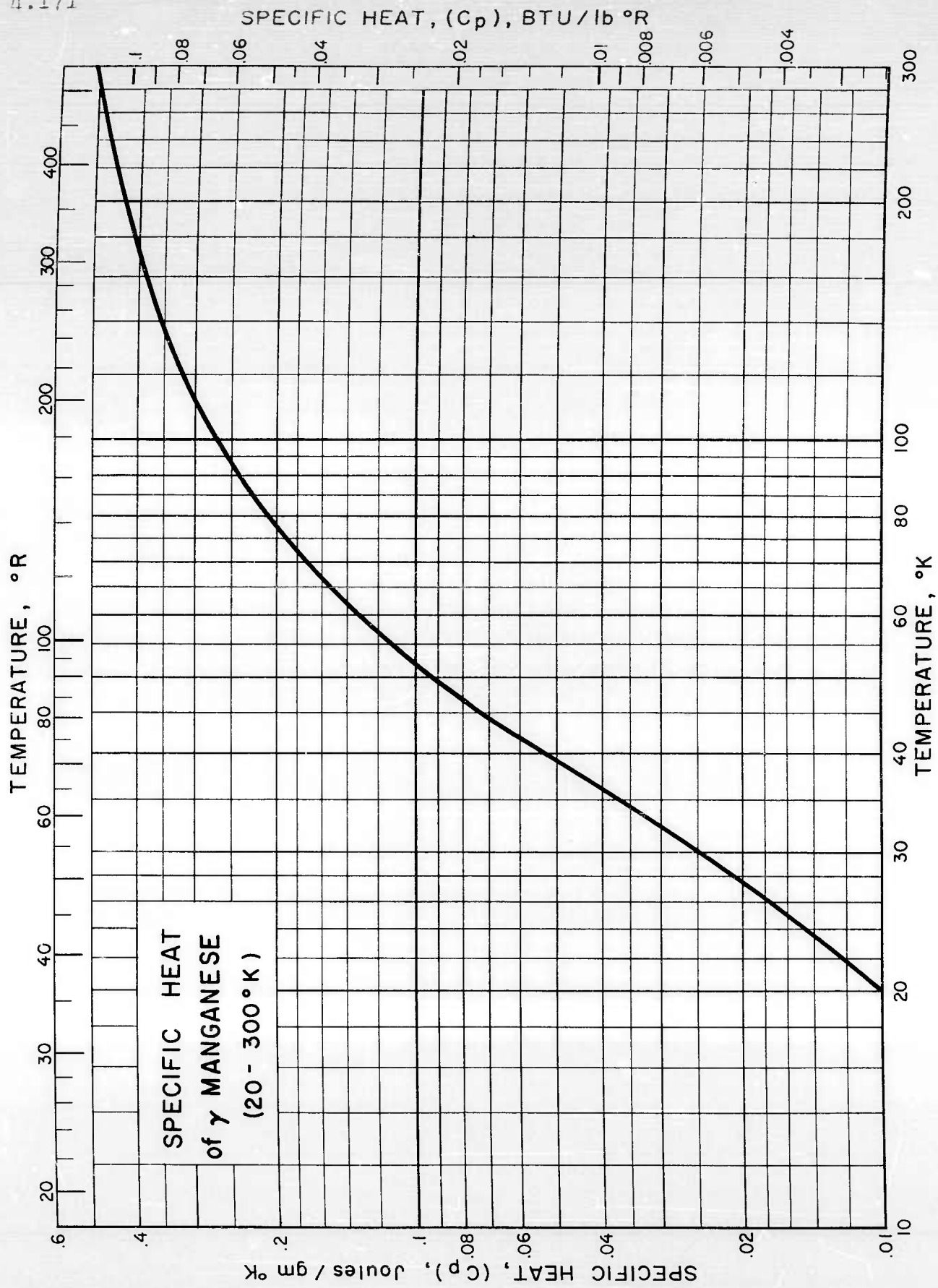


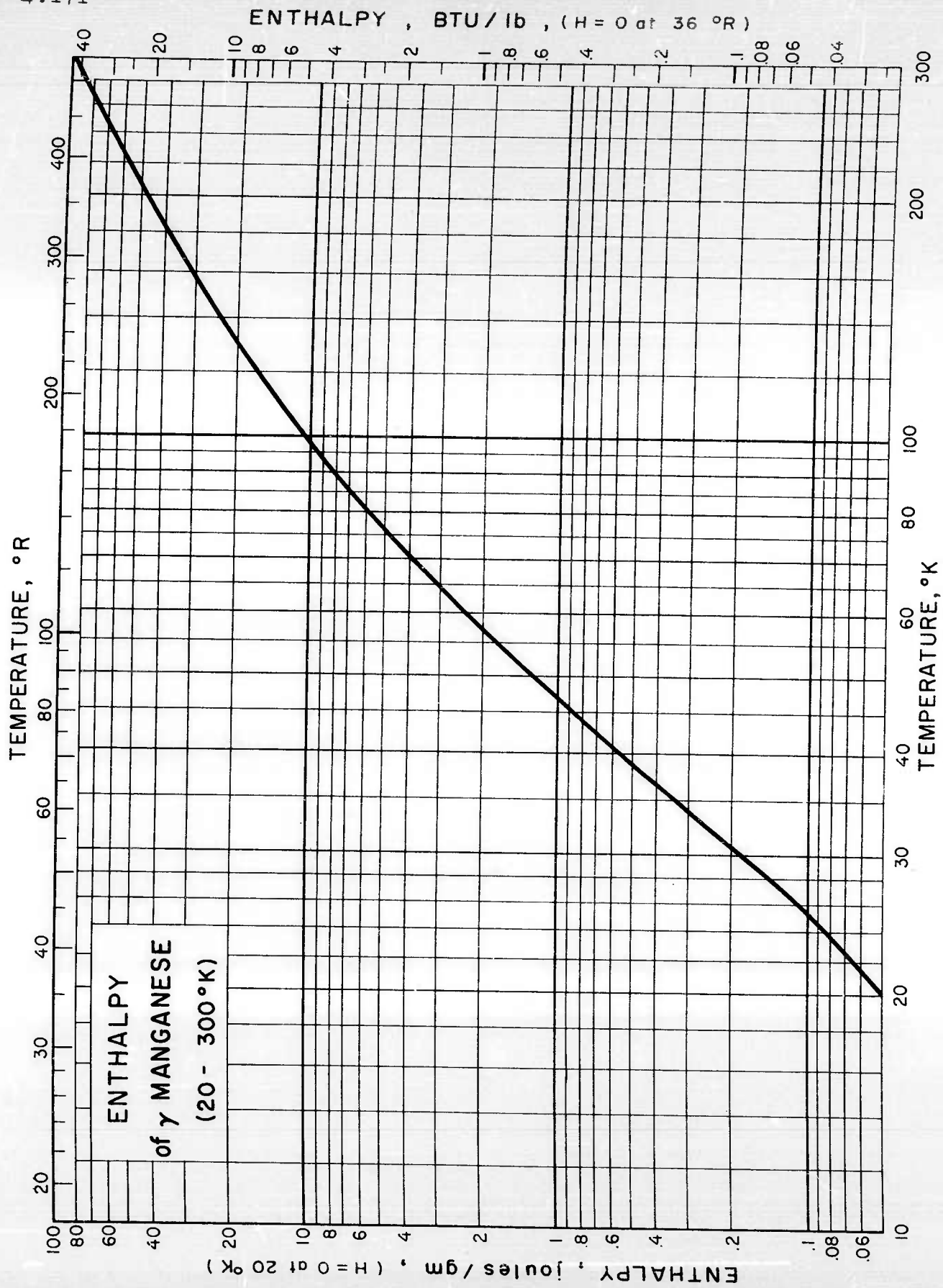
SPECIFIC HEAT, ENTHALPY of MANGANESE: γ FORMSource of Data:Shomate, C. H., J. Chem. Phys. 13, 326 (1945)Comments:

γ Mn is a ductile form that is stable between about 1100° and 1135°C when pure. It is often found as a separate phase in manganese alloys. The sample measured by Shomate was produced by electrolytic deposition.

Table of Selected Values

| T °K | Cp j/gm-°K | H j/gm | T °K | Cp j/gm-°K | H j/gm |
|---------|---------------|-----------|---------|---------------|-----------|
| 20 | 0.01 | 0.05 | 120 | 0.318 | 16.5 |
| 30 | .025 | 0.19 | 140 | .356 | 23.3 |
| 40 | .053 | 0.55 | 160 | .386 | 30.7 |
| 50 | .092 | 1.27 | 180 | .410 | 38.6 |
| 60 | .133 | 2.39 | 200 | .430 | 47.0 |
| 70 | .172 | 3.92 | 220 | .447 | 55.8 |
| 80 | .208 | 5.82 | 240 | .463 | 64.9 |
| 90 | .240 | 8.06 | 260 | .477 | 74.3 |
| 100 | .270 | 10.61 | 280 | .490 | 84.0 |
| | | | 300 | .503 | 93.9 |





SPECIFIC HEAT and ENTHALPY of α -IRONSources of Data:

- Duyckaerts, G., Physica 6, 401-8 (1939)
 Keesom, W. H. and Kurrelmayer, B., Physica 6, 633 (1939)
 Kelley, K. K., J. Chem. Phys. 11, 16-8 (1943)

Other References:

- Austin, J. B., Ind. Eng. Chem. 24, 1225 (1932)
 Behn, U., Ann. Physik (3) 66, 237 (1898)
 Duyckaerts, G., Mem. soc. roy. sci. Liege 6, 193 (1945)
 Eucken, A. and Werth, H., Z. anorg. u. allgem. Chem. 188, 152 (1930)
 Griffiths, E. G. and Griffiths, E., Phil. Trans. Roy. Soc. London A214, 319 (1914) and Proc. Roy. Soc. (London) A90, 557 (1914)
 Gunther, P., Ann. Physik (4) 51, 828 (1916)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
 Rodebush, W. H. and Michalek, J. C., J. Am. Chem. Soc. 47, 2117 (1925)
 Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)
 Simon, F., Z. angew. Chem. 41, 1113 (1928)
 Simon, F. and Swain, R. C., Z. physik. Chem. B28, 189 (1935)

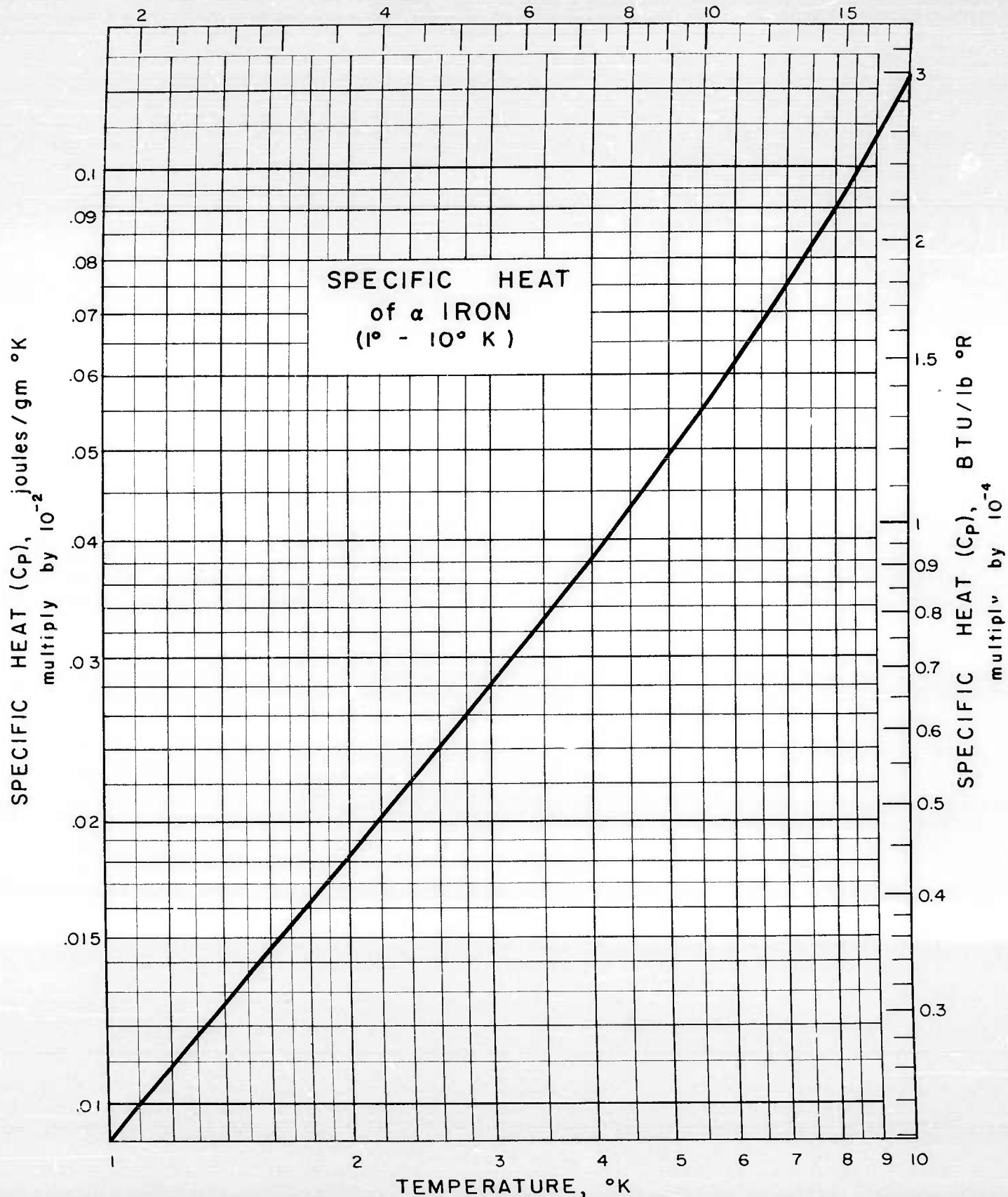
Comments:

α -Iron is the form that is stable up to the Curie point at 760°C. It has a body-centered cubic lattice.

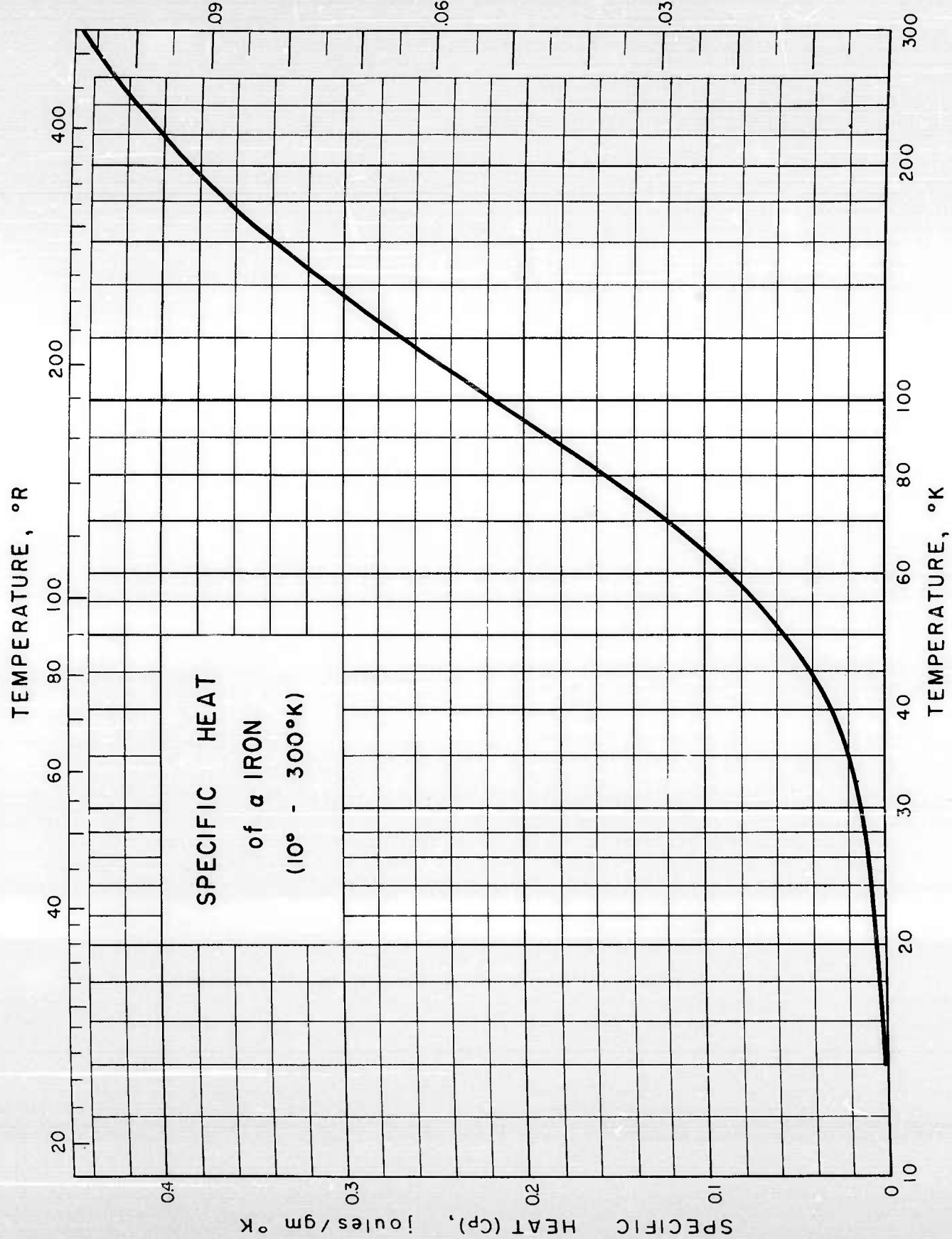
| T °K | C _p j/gm-°K | H j/gm | T °K | C _p j/gm-°K | H j/gm |
|---------|---------------------------|-----------|---------|---------------------------|-----------|
| 1 | 0.000 090 | 0.000 045 | 70 | 0.121 | 2.46 |
| 2 | .000 183 | .000 181 | 80 | .154 | 3.84 |
| 3 | .000 279 | .000 412 | 90 | .186 | 5.55 |
| 4 | .000 382 | .000 742 | 100 | .216 | 7.56 |
| 6 | .000 615 | .001 73 | 120 | .267 | 12.40 |
| 8 | .000 90 | .003 23 | 140 | .307 | 18.16 |
| 10 | .001 24 | .005 37 | 160 | .339 | 24.63 |
| 15 | .002 49 | .014 5 | 180 | .364 | 31.67 |
| 20 | .004 5 | .031 6 | 200 | .384 | 39.2 |
| 25 | .007 5 | .061 | 220 | .401 | 47.0 |
| 30 | .012 4 | .110 | 240 | .415 | 55.2 |
| 40 | .029 | .31 | 260 | .428 | 63.6 |
| 50 | .055 | .73 | 280 | .439 | 72.3 |
| 60 | .087 | 1.43 | 300 | .447 | 81.1 |

4.181

TEMPERATURE, °R

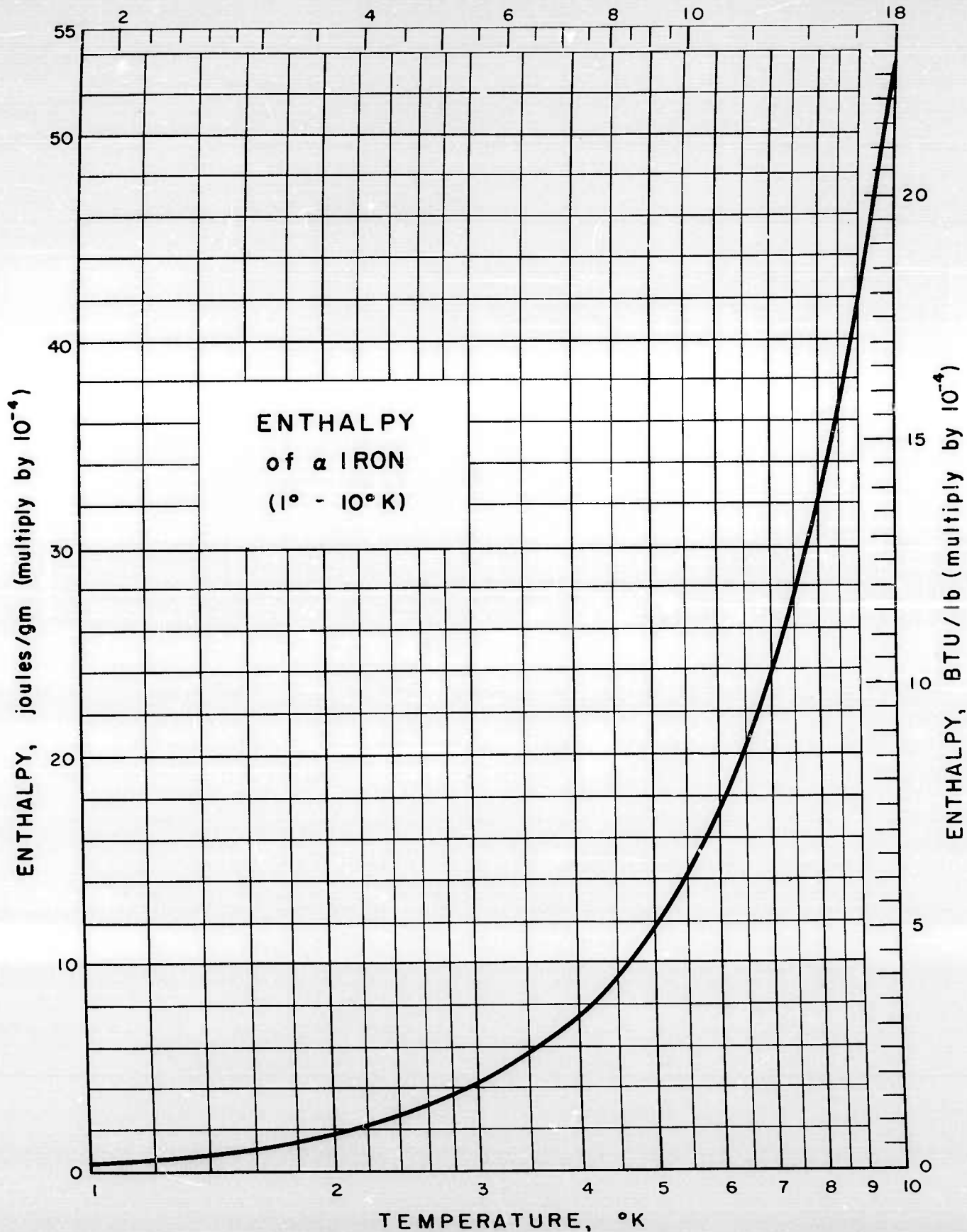


4.181
SPECIFIC HEAT (C_p), BTU/lb °R



4.181

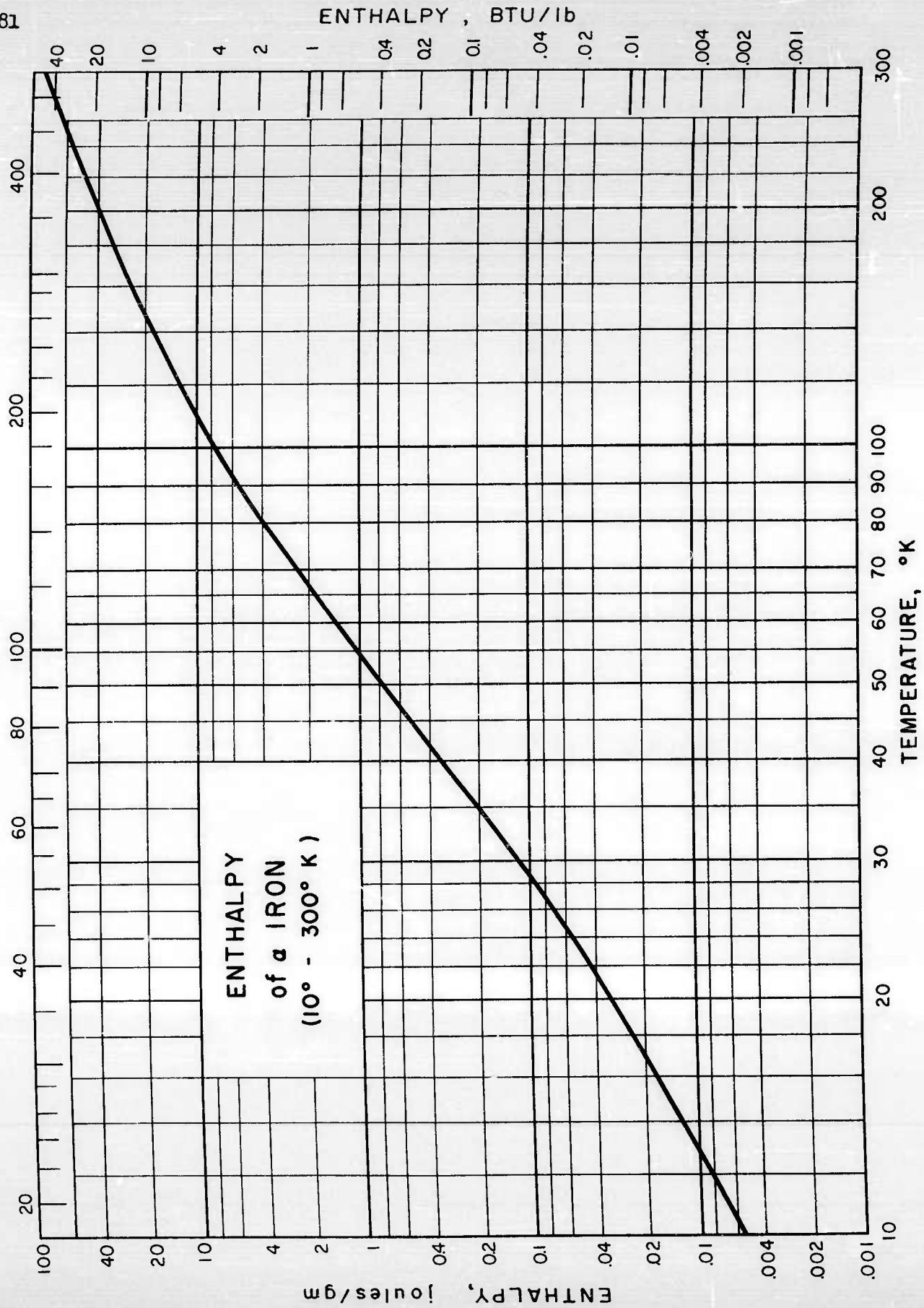
TEMPERATURE, °R



4.181

4.181

TEMPERATURE, °R



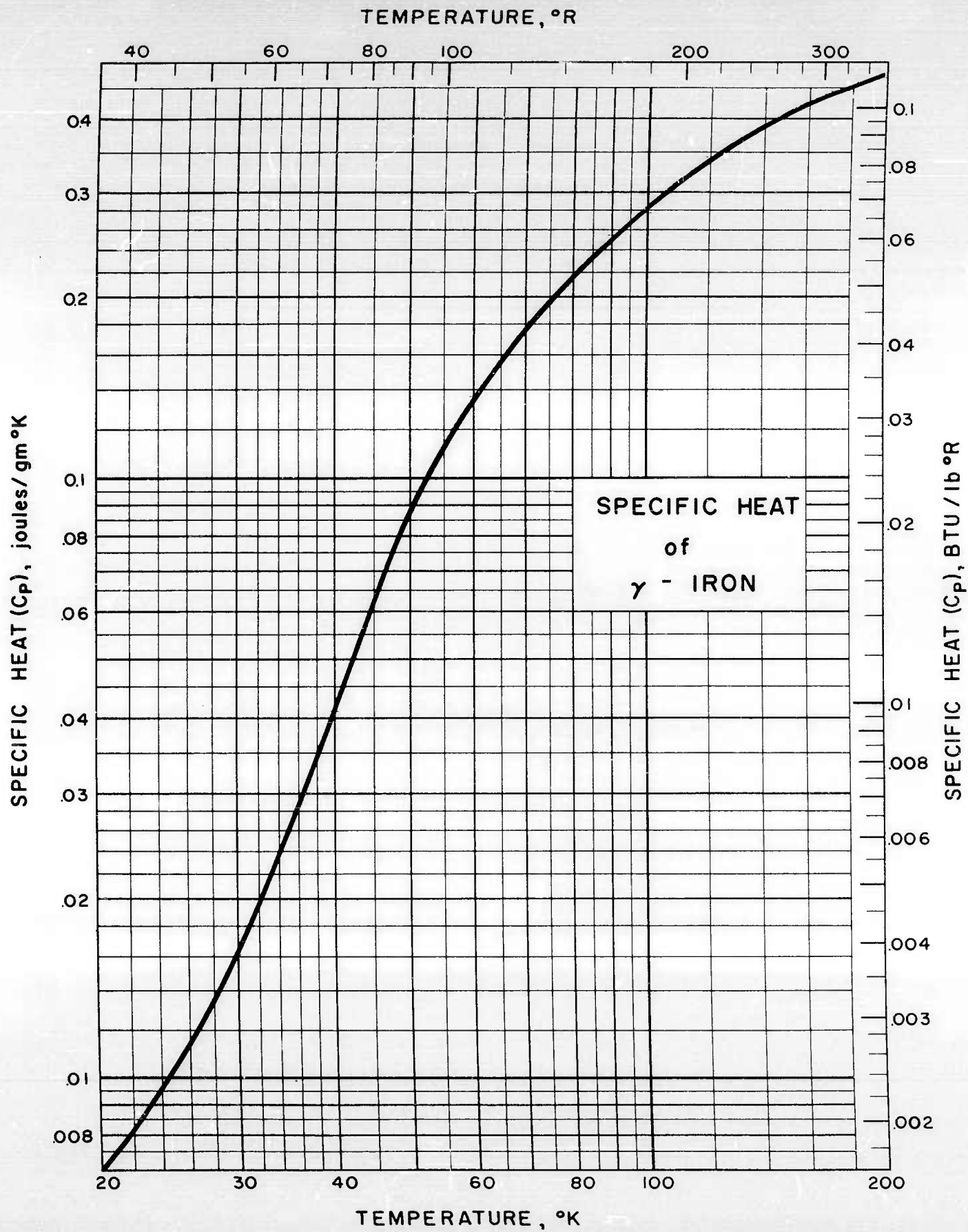
SPECIFIC HEAT, ENTHALPY of γ - IRONSources of Data:

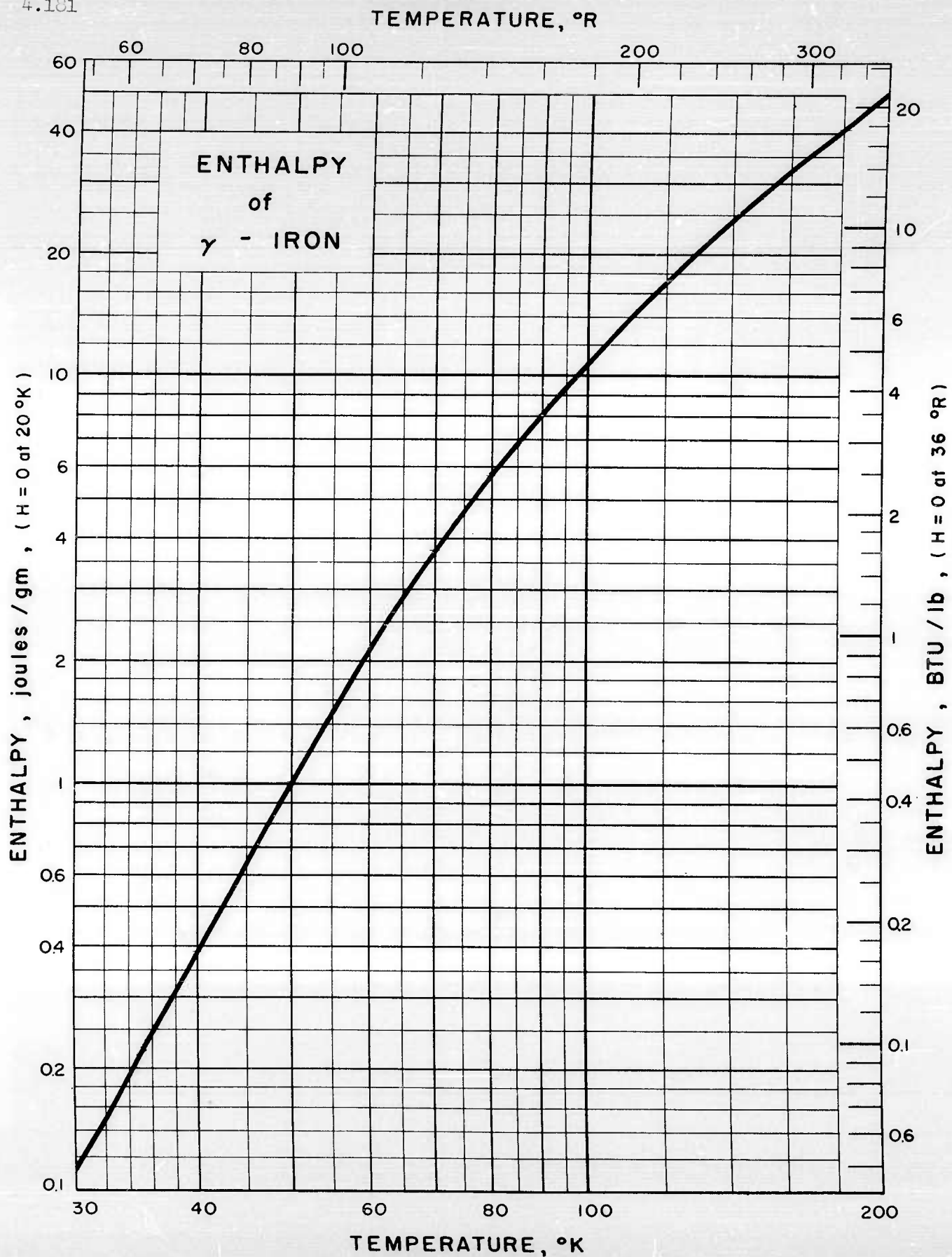
Eucken A. and Werth, H., Z. anorg. u. allgem. Chem. 188, 152-72 (1930).

Comments:

The values of specific heat for pure γ iron were calculated by Eucken and Werth by application of the Kopp-Neumann principle to their specific heat measurements on a 30% Mn-Fe alloy and 19.4% Mn-Fe alloy. In view of this procedure, the values tabulated below should be regarded as an approximation only.

| T °K | C _p j/gm-°K | H-H ₂₀ j/gm |
|---------|---------------------------|---------------------------|
| 20 | 0.007 | |
| 30 | .016 | 0.11 |
| 40 | .041 | 0.39 |
| 50 | .090 | 1.02 |
| 60 | .137 | 2.16 |
| 70 | .180 | 3.75 |
| 80 | .218 | 5.74 |
| 90 | .255 | 8.1 ₁ |
| 100 | .288 | 10.8 |
| 120 | .345 | 17.1 |
| 140 | .389 | 24.4 |
| 160 | .427 | 32.6 |
| 180 | .450 | 41.4 |
| 200 | .470 | 50.6 |





Sources of Data:

- Busey, R. H. and Giaugue, W. F., J. Am. Chem. Soc. 74, 3157-8 (1952)
 Keesom, W. H. and Clark, C. W., Physica 2, 513-20 (1935)
 Rayne, J. A. and Kemp, W. R. G., Phil. Mag. (8) 1, 918 (1956)

Other References:

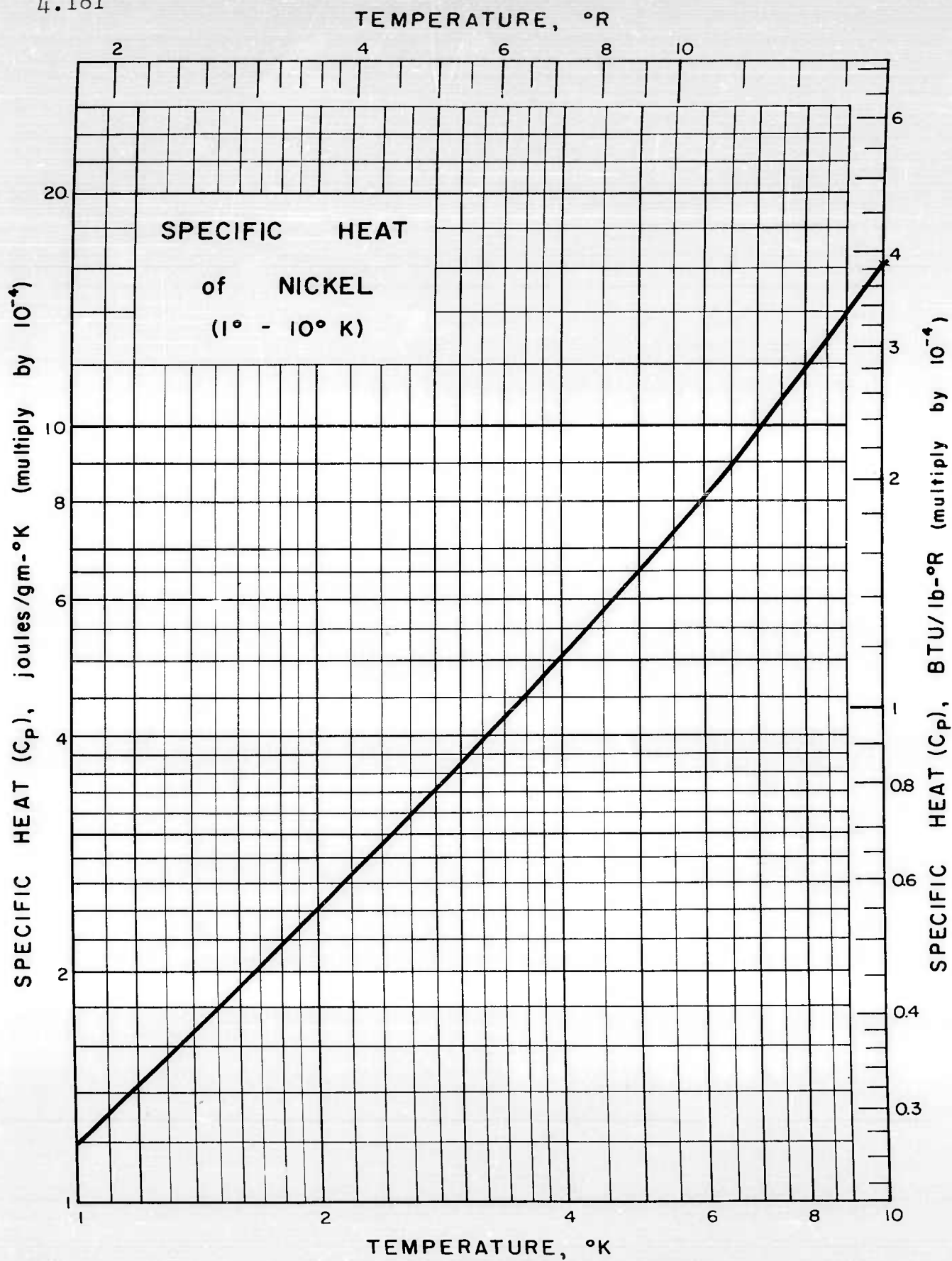
- Aoyama, S. and Kanda, E., J. Chem. Soc. Japan 62, 312-5 (1941)
 Behn, U., Ann. Physik (3) 66, 237 (1898)
 Bronson, H. L. and Wilson, A. J. C., Can. J. Research A14, 181 (1936)
 Clusius, K. and Goldman, J., Z. physik. Chem. B31, 256 (1936)
 Duyckaerts, G., Mem. soc. roy. sci. Liege 6, 193 (1945)
 Eucken, A. and Werth, H., Z. anorg. u. allgem. Chem. 188, 152 (1930)
 Grew, K. E., Proc. Roy. Soc. (London) A145, 509 (1934)
 Keesom, W. H. and Kok, J. A., 7th Cong. intern. froid. 1st Comm. intern. Rapports et Commun., 156 (1936)
 Lapp, E., Ann. Physik. 12, 442 (1929)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)
 Rodebush, W. H. and Michalek, J. C., J. Am. Chem. Soc. 47, 2117 (1925)
 Schmitz, H. E., Proc. Roy. Soc. (London) 72, 177 (1903)
 Simon, F. and Ruheman, M., Z. physik. Chem. 129, 321 (1927)
 Tilden, W. A., Phil. Trans. Roy. Soc. London A194, 233 (1900); Proc. Roy. Soc. (London) 66, 244 (1900)

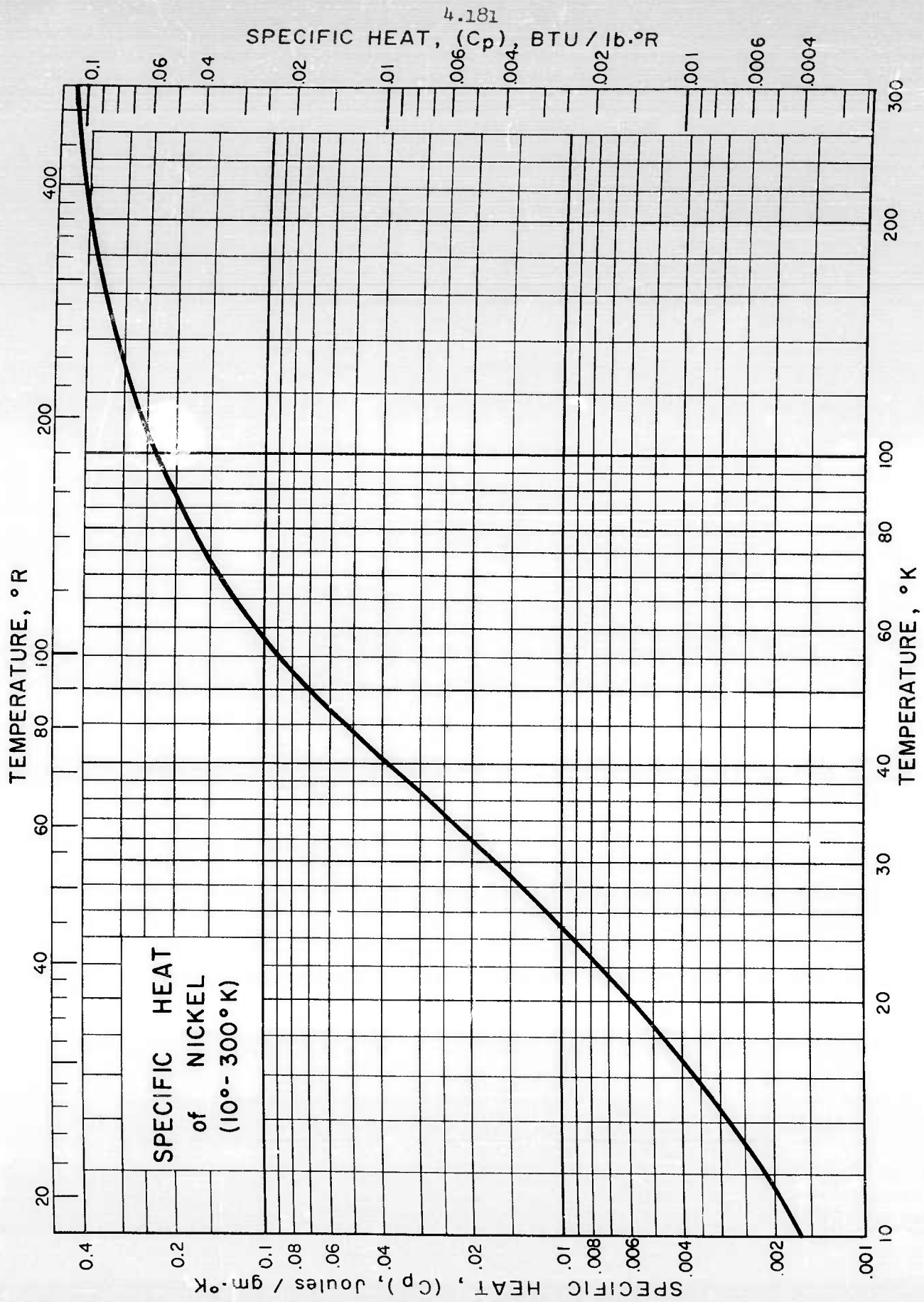
Table of Selected Values

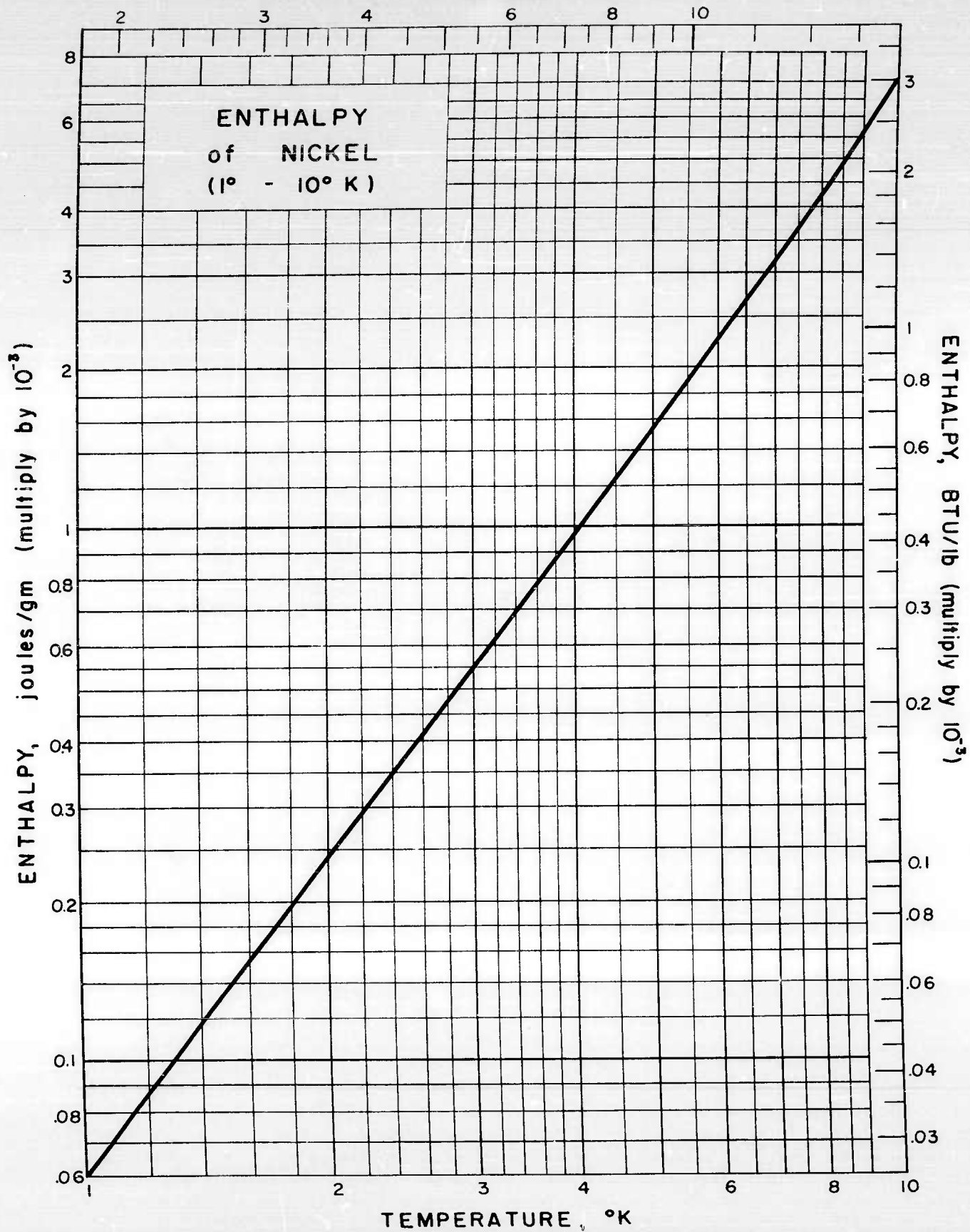
| T °K | C _p j/gm-°K | H j/gm | T °K | C _p j/gm-°K | H j/gm |
|---------|---------------------------|-----------|---------|---------------------------|-----------|
| 1 | 0.000 120 | 0.000 060 | 70 | 0.139 | 3.00 |
| 2 | .000 242 | .000 241 | 80 | .173 | 4.56 |
| 3 | .000 369 | .000 546 | 90 | .204 | 6.45 |
| 4 | .000 503 | .000 98 | 100 | .232 | 8.63 |
| 6 | .000 82 | .002 28 | 120 | .278 | 13.76 |
| 8 | .001 19 | .004 28 | 140 | .314 | 19.70 |
| 10 | .001 62 | .007 1 | 160 | .342 | 26.28 |
| 15 | .003 1 | .018 5 | 180 | .365 | 33.35 |
| 20 | .005 8 | .041 | 200 | .383 | 40.82 |
| 25 | .010 1 | .079 | 220 | .397 | 48.6 |
| 30 | .016 7 | .145 | 240 | .410 | 56.7 |
| 40 | .038 1 | .413 | 260 | .422 | 65.0 |
| 50 | .068 2 | .937 | 280 | .433 | 73.6 |
| 60 | .103 | 1.79 | 300 | .445 | 82.4 |

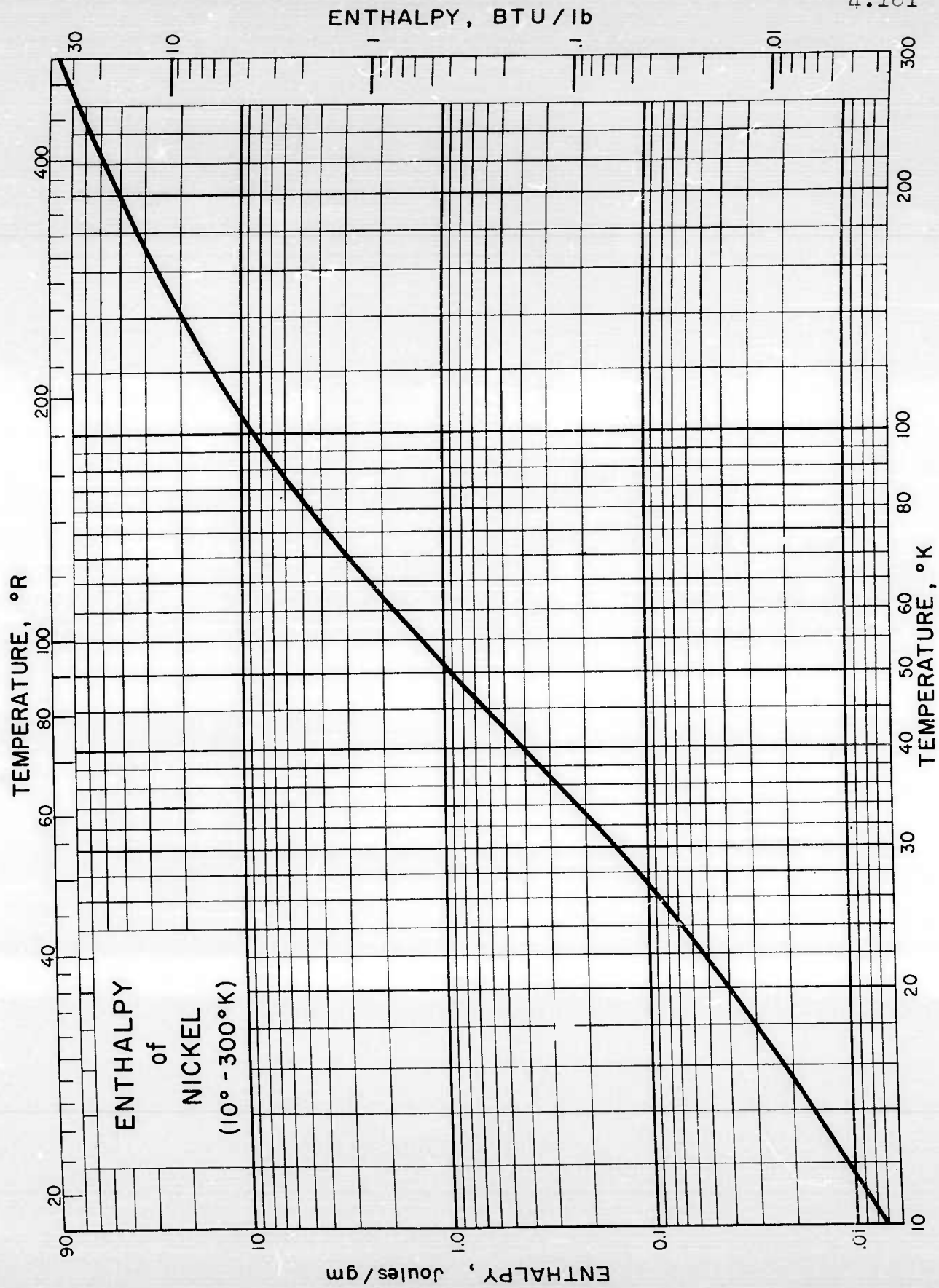
RJC Issued: 12-18-59

Revised: 5-20-60









SPECIFIC HEAT, ENTHALPY of PALLADIUM

Sources of Data:

- Clusius, K. and Schachinger, L., Z. Naturforsch. 2a, 90-7 (1947)
 Hoare, F. E. and Yates, B., Proc. Roy. Soc. (London) A240, 42-53, (1957)
 Pickard, G. L. and Simon, F., Proc. Phys. Soc. (London) 61, 1-9, (1948)
 Rayne, J. A., Phys. Rev. 95, 1428 (1954)

Other References:

- Behn, U., Ann. Physik 66, 237 (1898)
 Pickard, G. L., Nature 138, 123 (1936)
 Richards, T. W. and Jackson, F. G., Z. physik. Chem. 70, 414 (1910)

Comments:

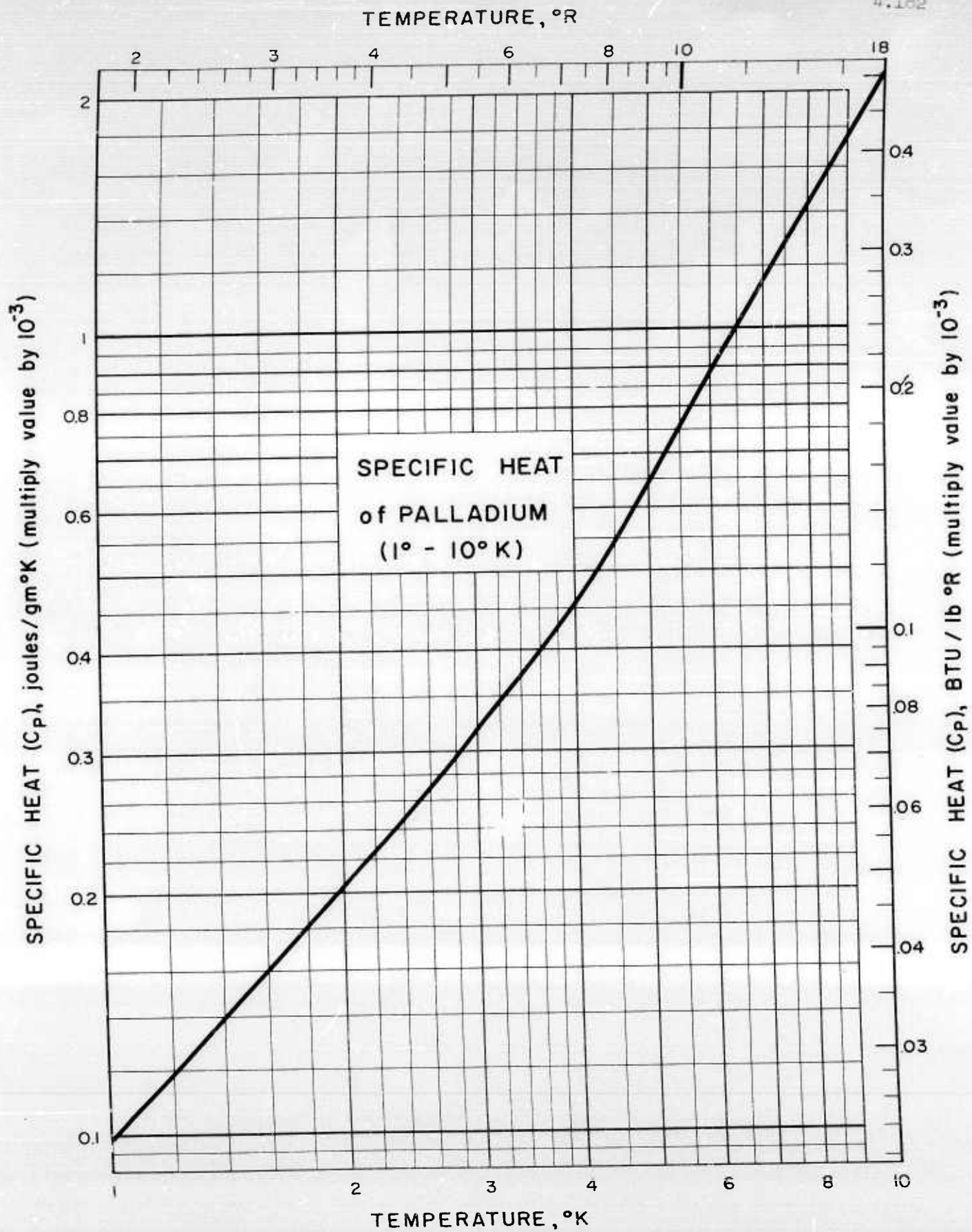
For the range from 0° to 4°K, the specific heat C_p follows the equation:

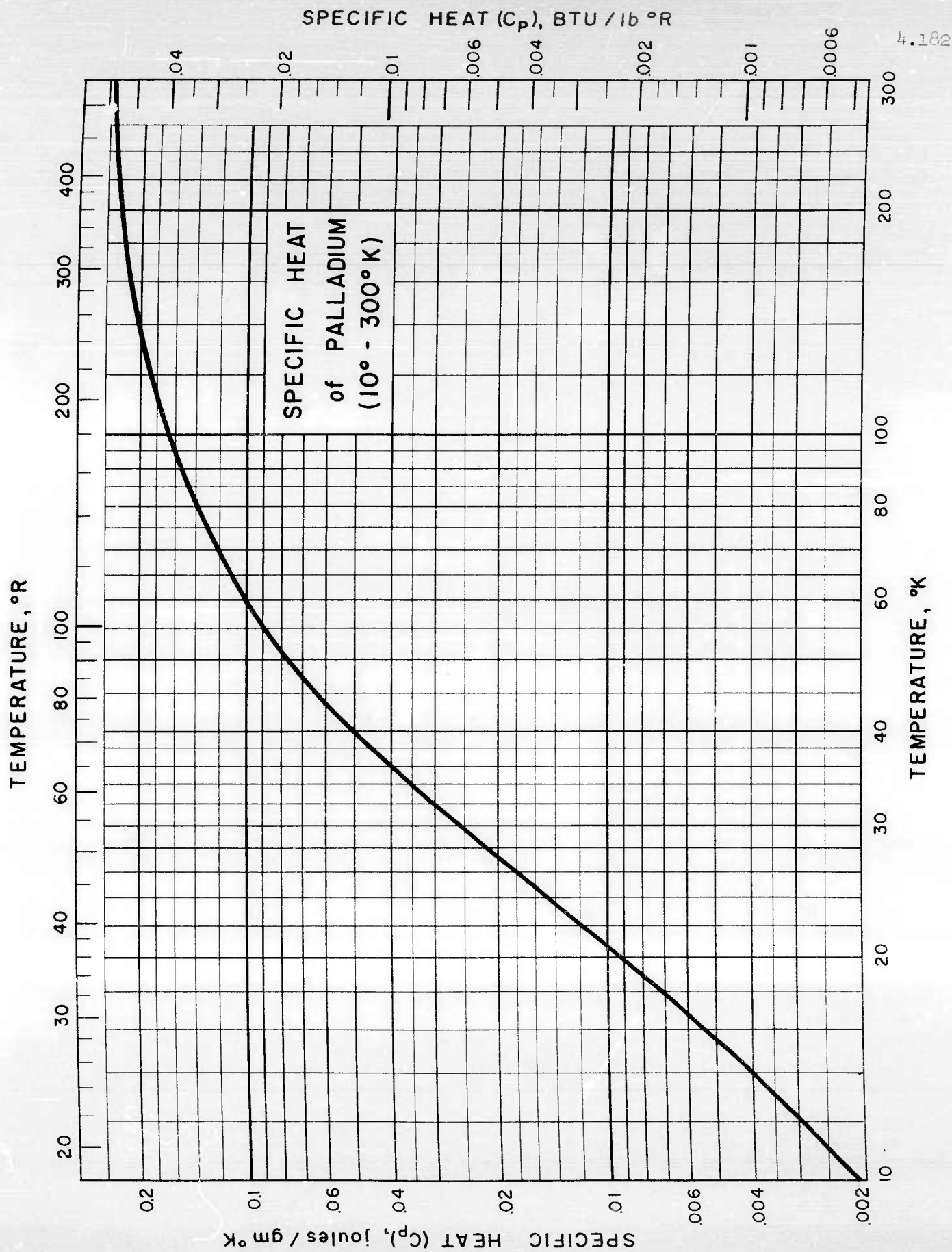
$$C_p = (9.8 \pm 0.8) \times 10^{-5} T + 18.22 \left(\frac{T}{274 \pm 3} \right)^3 \text{ j/gm-}^\circ\text{K}$$

Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|------------|-------------|------------------|-----------|
| 1 | 0.000 099 | 0.000 0493 | 70 | 0.122 | 3.26 |
| 2 | .000 203 | .000 200 | 80 | .139 | 4.56 |
| 3 | .000 318 | .000 459 | 90 | .154 | 6.03 |
| 4 | .000 447 | .000 840 | 100 | .167 | 7.63 |
| 6 | .000 891 | .002 31 | 120 | .188 | 11.2 |
| 8 | .001 41 | .004 60 | 140 | .202 | 15.1 |
| 10 | .002 10 | .008 07 | 160 | .213 | 19.2 |
| 15 | .004 71 | .024 5 | 180 | .221 | 23.6 |
| 20 | .009 22 | .058 6 | 200 | .227 | 28.1 |
| 25 | .016 0 | .120 | 220 | .232 | 32.6 |
| 30 | .025 8 | .223 | 240 | .236 | 37.3 |
| 40 | .050 7 | .600 | 260 | .239 | 42.1 |
| 50 | .077 7 | 1.24 | 280 | .241 | 46.9 |
| 60 | .101 | 2.14 | 300 | .243 | 51.7 |

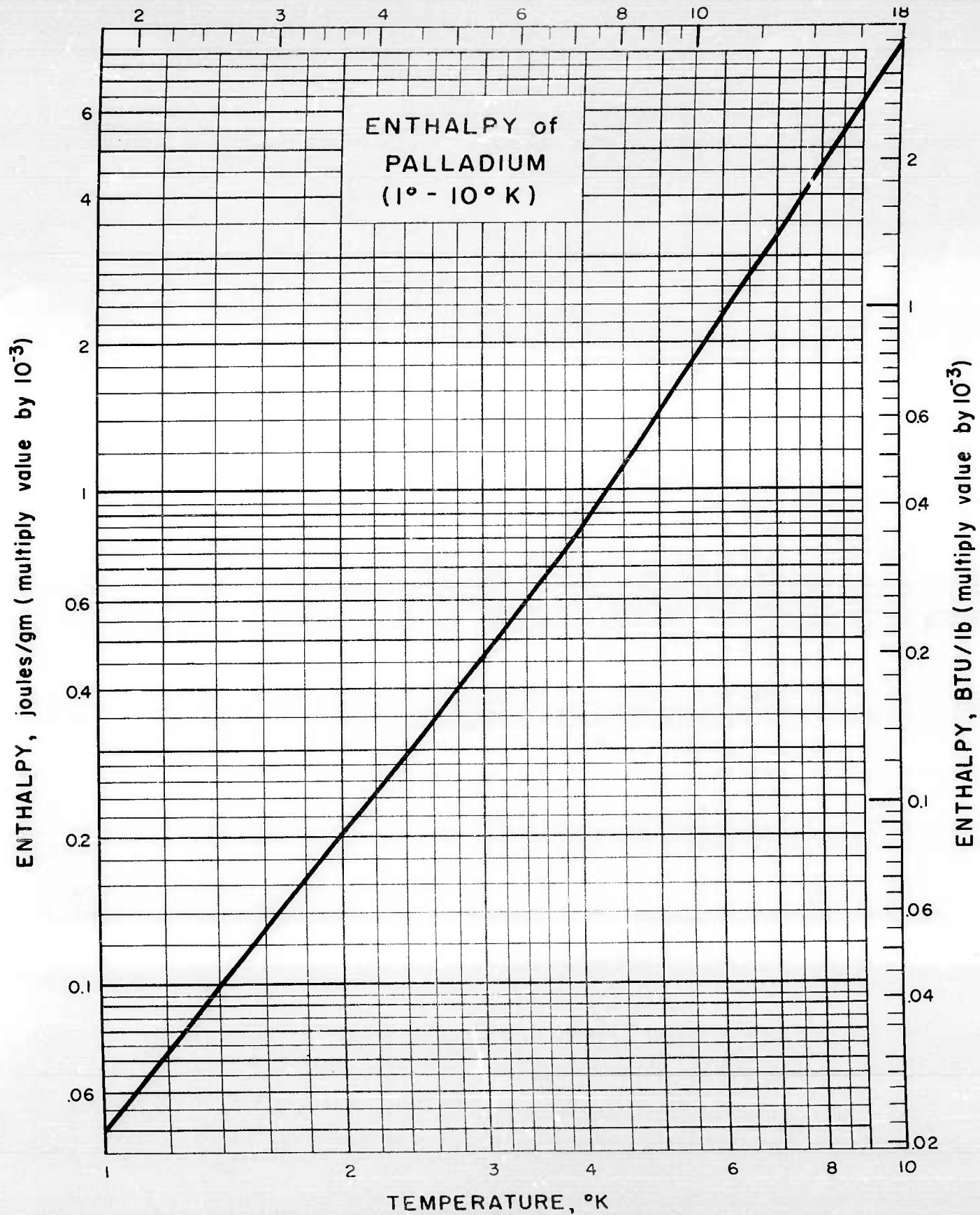
RJC/JJG Issued: 12-18-59

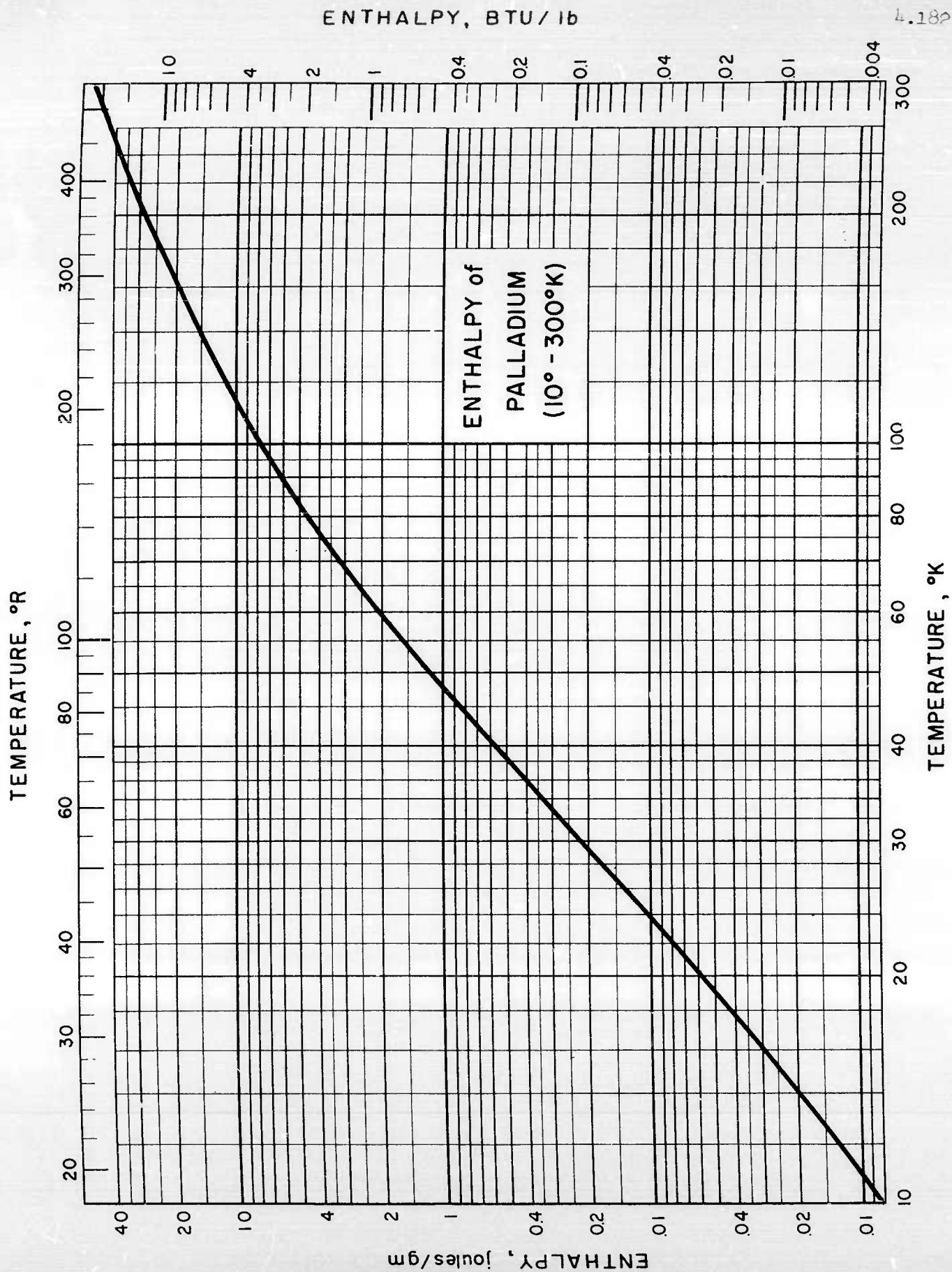




TEMPERATURE, °R

4.182





SPECIFIC HEAT, ENTHALPY of PLATINUM

Sources of Data:

- Kok, J. A. and Keesom, W. H., *Physica* 3, 1035-45 (1936)
 Ramanathan, K. G. and Srinivasan, T. M., *Proc. Indian Acad. Sci.*
49, 55-60 (1959)
 Simon, F. and Zeidler, W., *Z. physik. Chem.* 123, 383 (1926)

Other References:

- Behn, U., *Ann. Physik.* 66, 237 (1898)
 Rayne, J. A., *Phys. Rev.* 95, 1428 (1954)
 Richards, T. W. and Jackson, F. G., *Z. physik. Chem.* 70, 414 (1910)
 Tilden, W. A., *Proc. Roy. Soc. (London)* A71, 220 (1903); *Ann. Physik.*
Beiblätter 27, 557 (1903)

Comments:

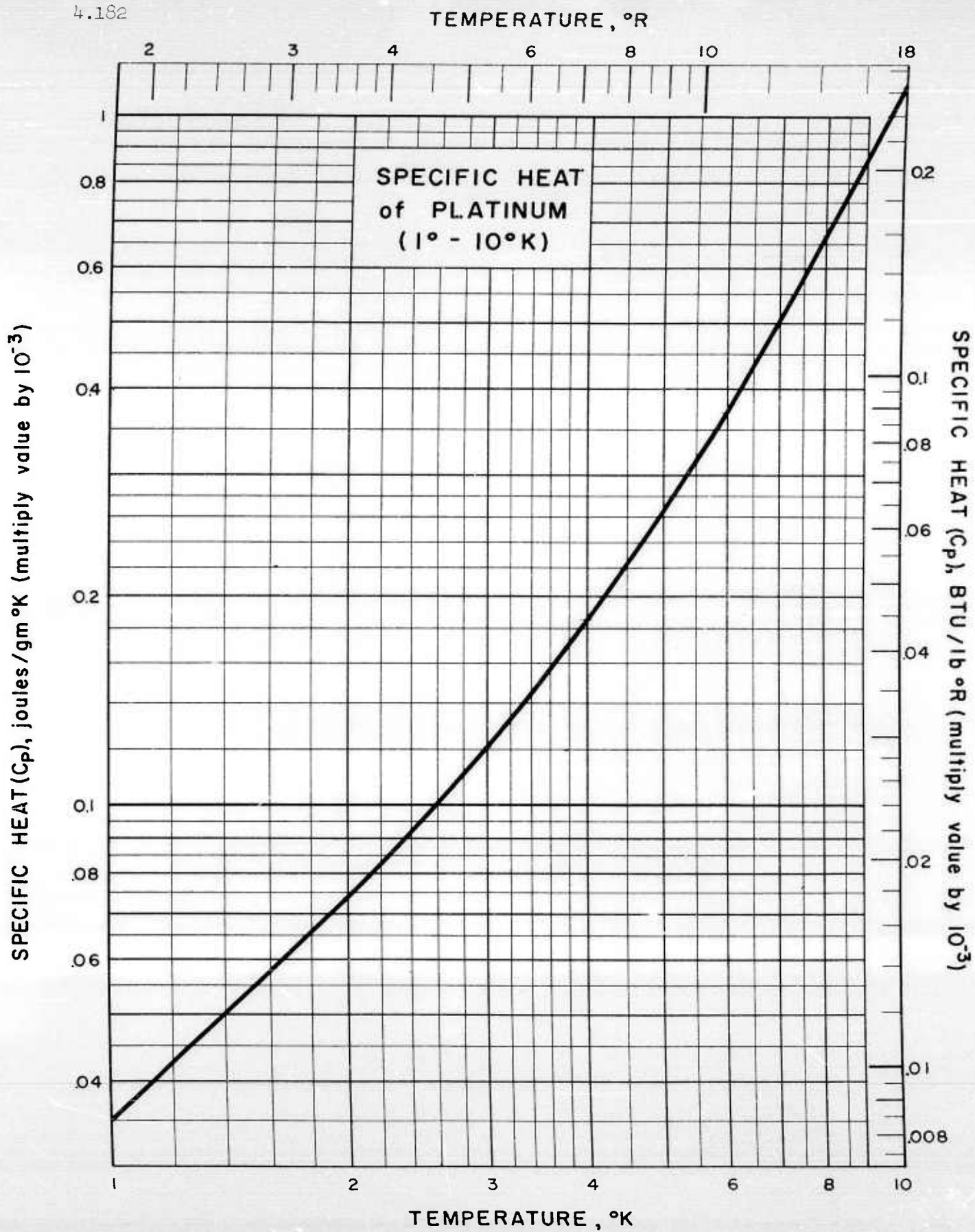
For the temperature range from 0° to 3°K, the specific heat C_p follows the equation:

$$C_p = (3.41 \pm 0.02) \times 10^{-5} T + 9.96 \left(\frac{T}{240 \pm 5} \right)^3 \text{ j/gm-}^\circ\text{K}$$

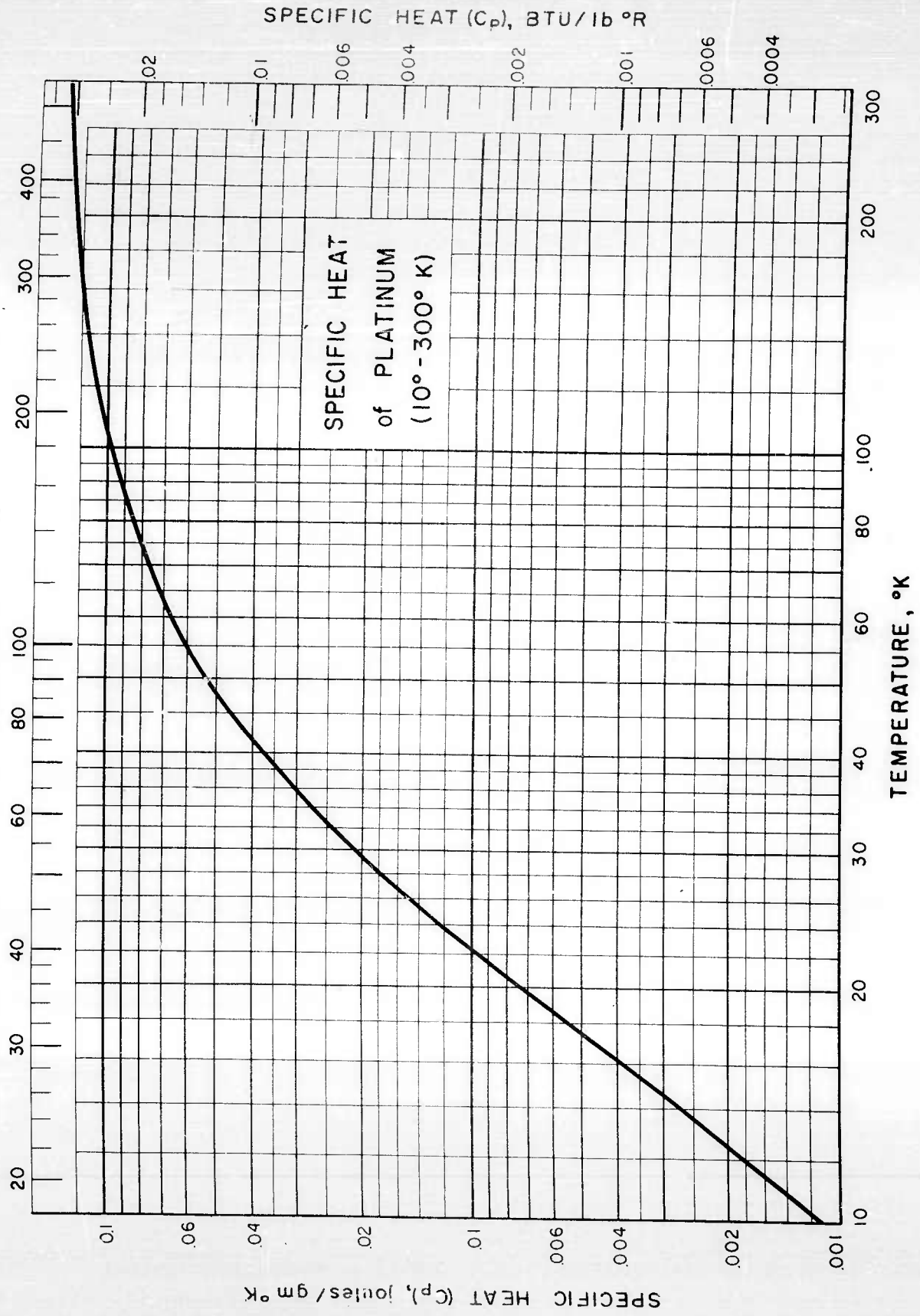
Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|------------|-------------|------------------|-----------|
| 1 | 0.000 035 | 0.000 0175 | 70 | 0.079 | 2.29 |
| 2 | .000 074 | .000 071 | 80 | .088 | 3.12 |
| 3 | .000 122 | .000 168 | 90 | .094 | 4.02 |
| 4 | .000 186 | .000 320 | 100 | .100 | 5.01 |
| 6 | .000 37 | .000 85 | 120 | .109 | 7.10 |
| 8 | .000 67 | .001 88 | 140 | .116 | 9.37 |
| 10 | .001 12 | .003 65 | 160 | .121 | 11.8 |
| 15 | .003 3 | .013 5 | 180 | .125 | 14.2 |
| 20 | .007 4 | .039 5 | 200 | .127 | 16.7 |
| 25 | .013 7 | .092 | 220 | .129 | 19.3 |
| 30 | .021 2 | .182 | 240 | .130 | 21.9 |
| 40 | .038 | .48 | 260 | .131 | 24.5 |
| 50 | .055 | .95 | 280 | .132 | 27.1 |
| 60 | .068 | 1.56 | 300 | .133 | 29.8 |

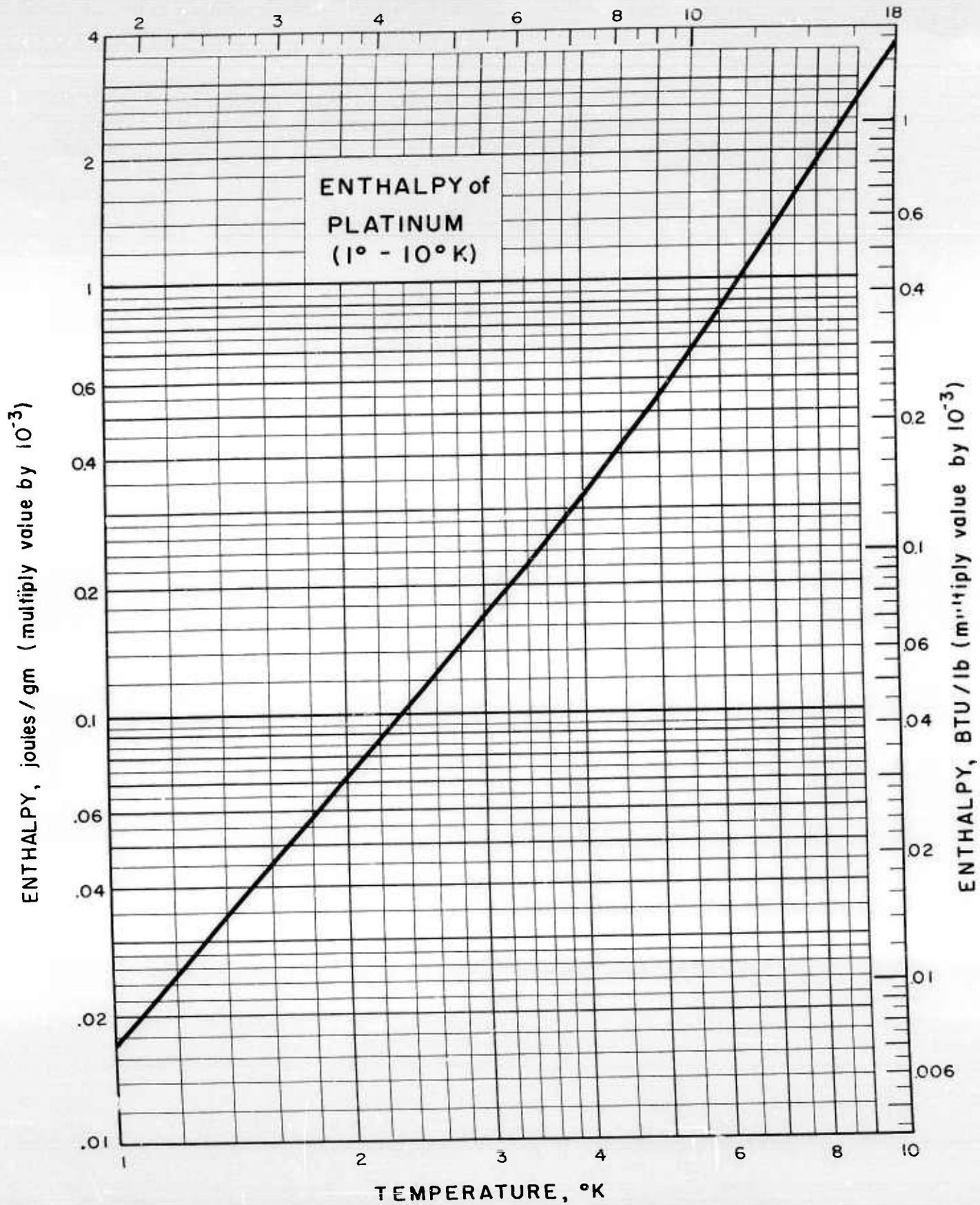
RJC/JJG Issued: 12-18-59
 Revised: 5-20-60

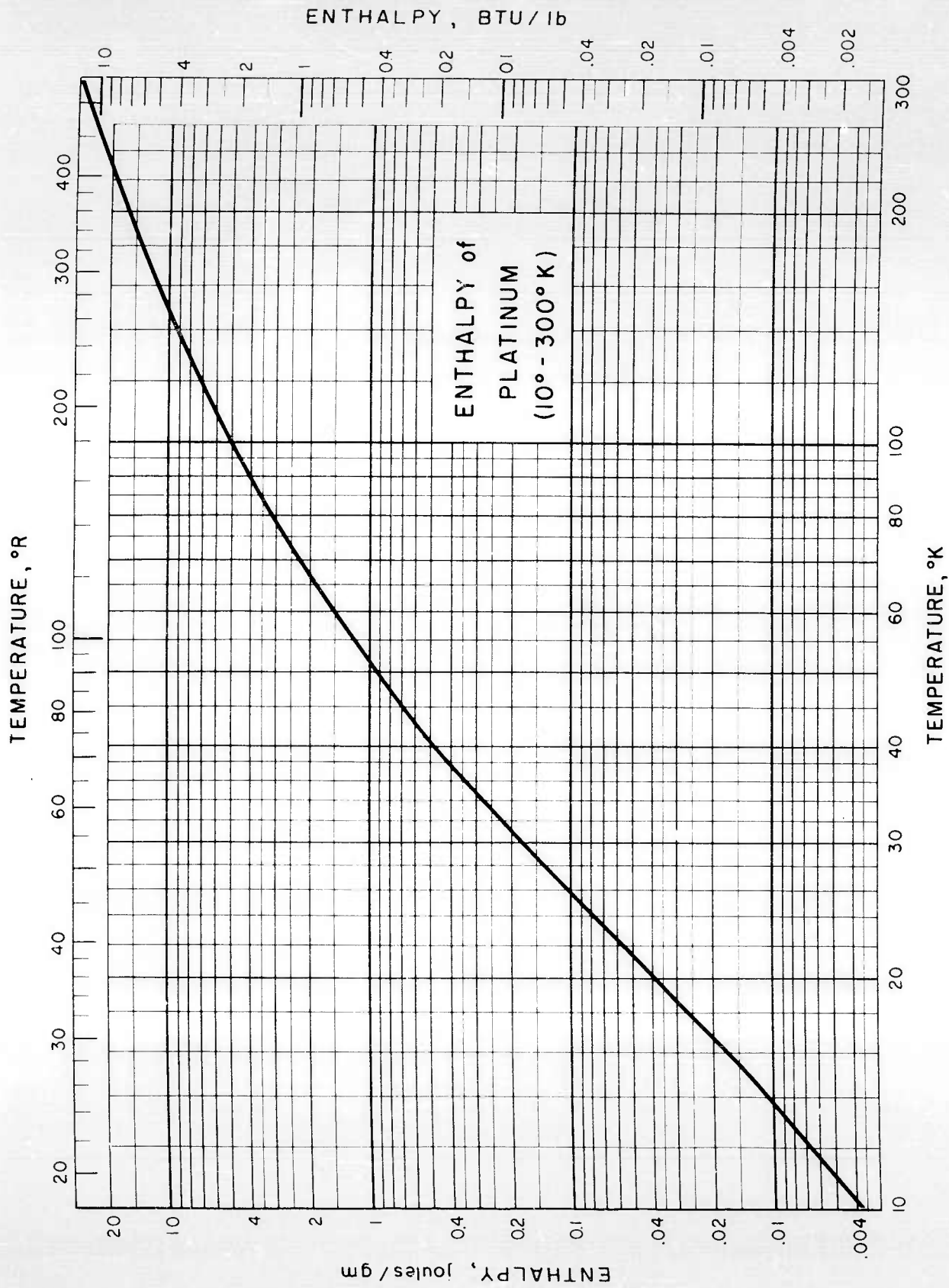


TEMPERATURE, °R



TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of RHODIUM

Source of Data:Clusius, K., and Losa, C. G., Z. Naturforsch. 10A, 545 (1955)

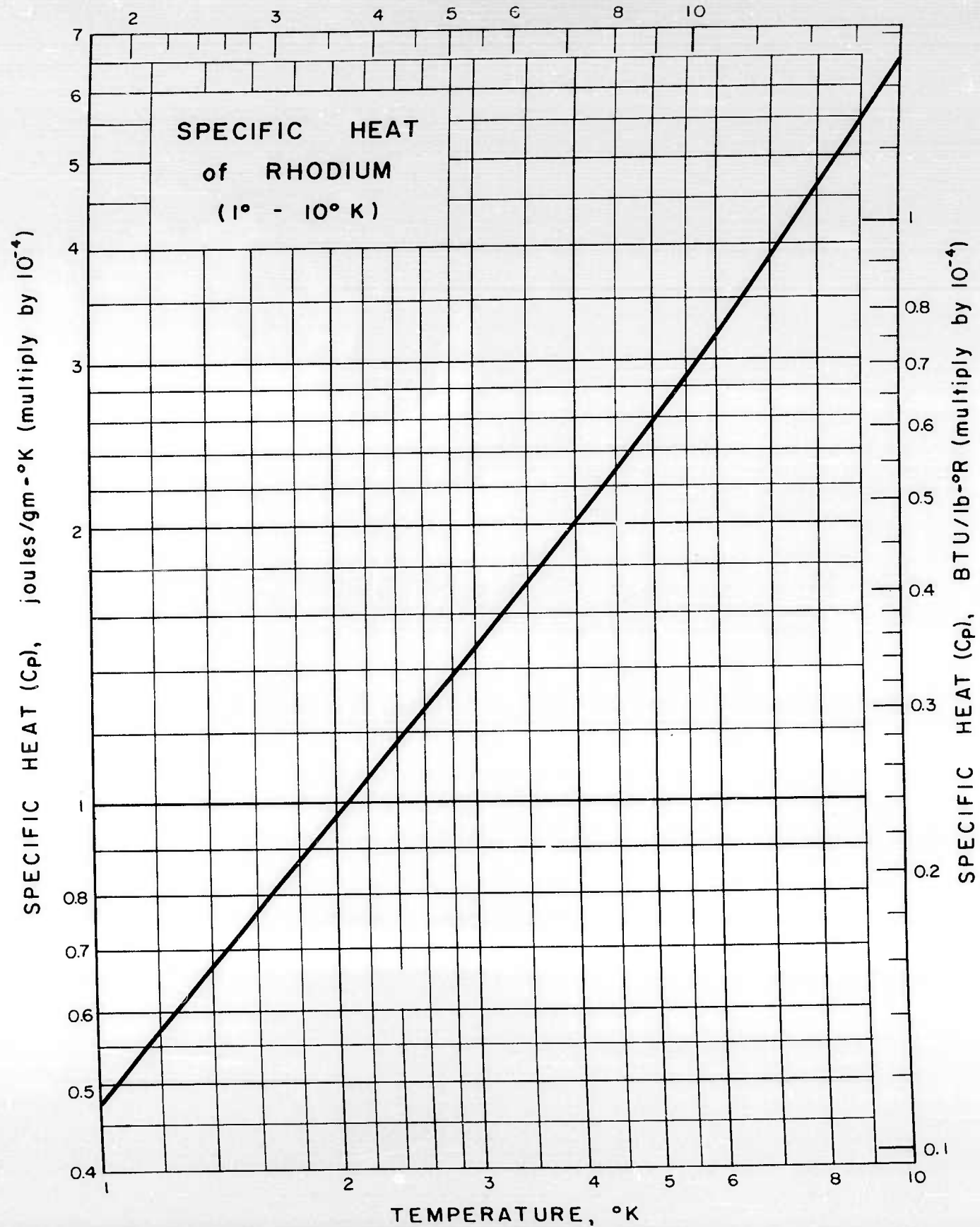
Wolcott, N. M., Conf. Phys. basses Temp. (1955)

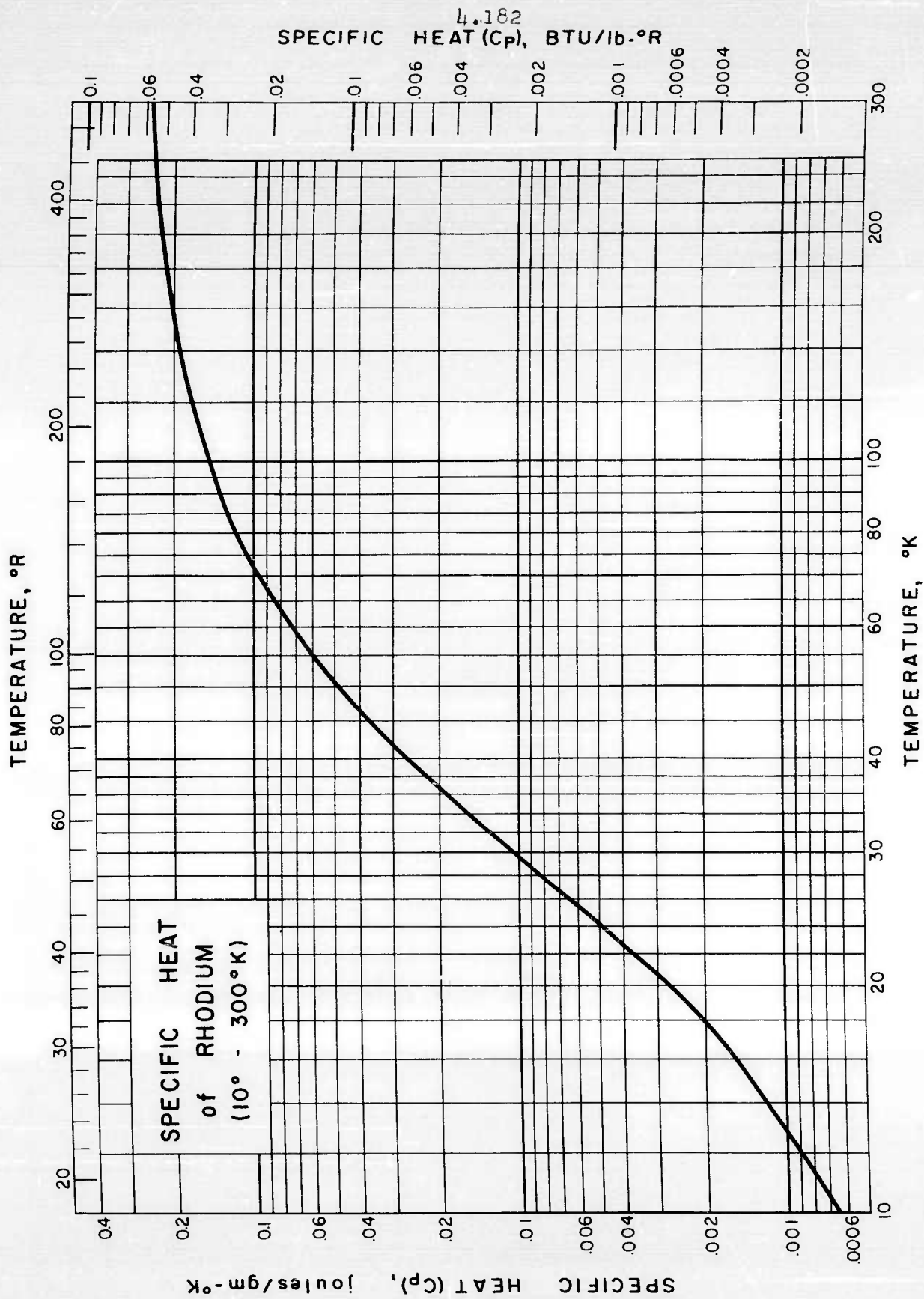
Table of Selected Values

| T °K | Cp j/gm-°K | H j/gm | T °K | Cp j/gm-°K | H j/gm |
|---------|---------------|-----------|---------|---------------|-----------|
| 1 | 0.000 048 | 0.000 024 | 70 | 0.094 | 2.07 |
| 2 | .000 097 | .000 096 | 80 | .114 | 3.11 |
| 3 | .000 147 | .000 218 | 90 | .132 | 4.34 |
| 4 | .000 201 | .000 392 | 100 | .147 | 5.74 |
| 6 | .000 32 | .000 91 | 120 | .171 | 8.93 |
| 8 | .000 47 | .001 70 | 140 | .189 | 12.54 |
| 10 | .000 65 | .002 81 | 160 | .202 | 16.46 |
| 15 | .001 35 | .007 65 | 180 | .212 | 20.60 |
| 20 | .002 71 | .017 4 | 200 | .220 | 24.92 |
| 25 | .005 61 | .037 3 | 220 | .226 | 29.38 |
| 30 | .010 6 | .077 1 | 240 | .232 | 33.96 |
| 40 | .026 6 | .256 | 260 | .236 | 38.63 |
| 50 | .048 9 | .633 | 280 | .240 | 43.38 |
| 60 | .072 4 | 1.238 | 300 | .243 | 48.2 |

RJC/jrc Issued: 6-5-59

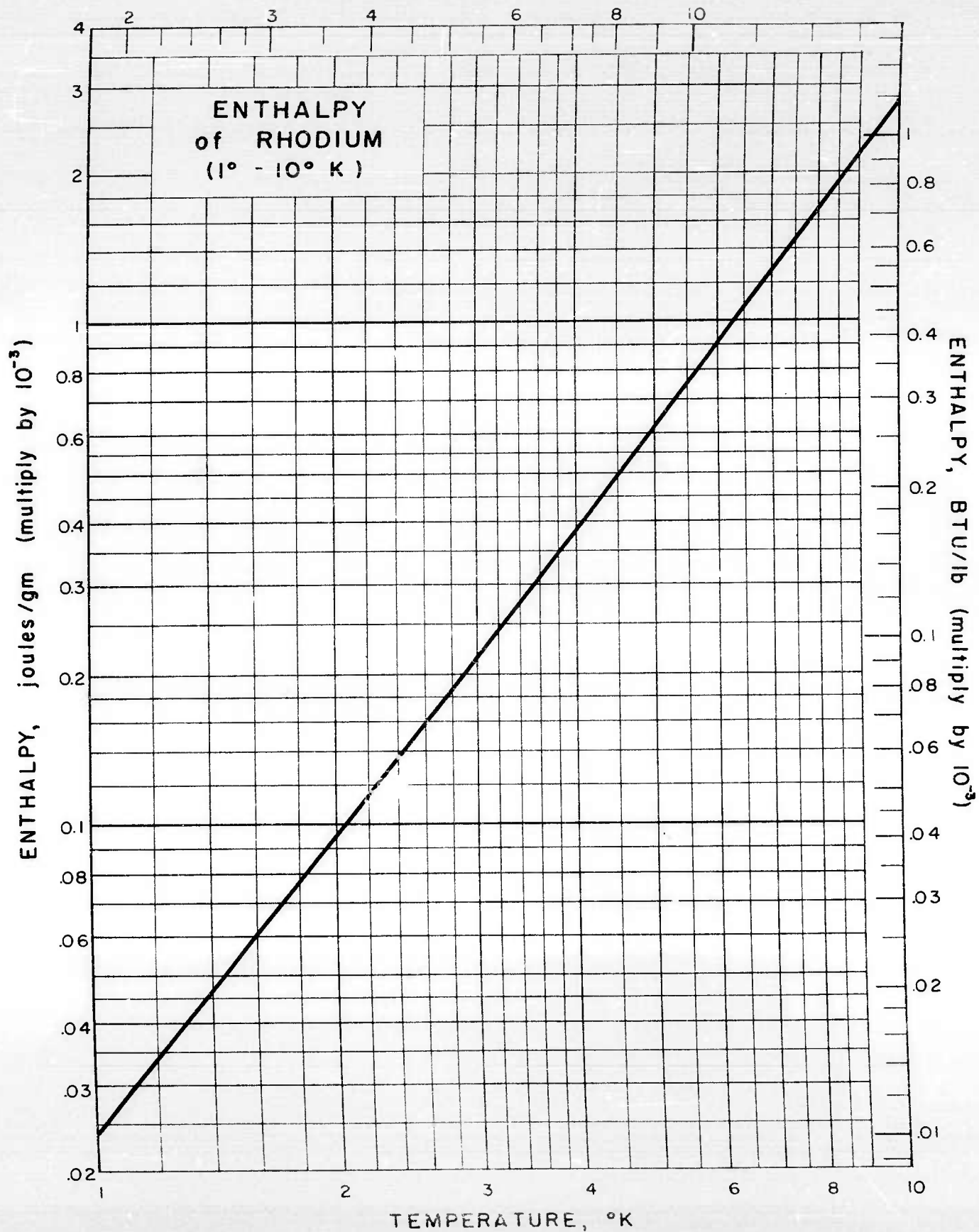
TEMPERATURE, °R

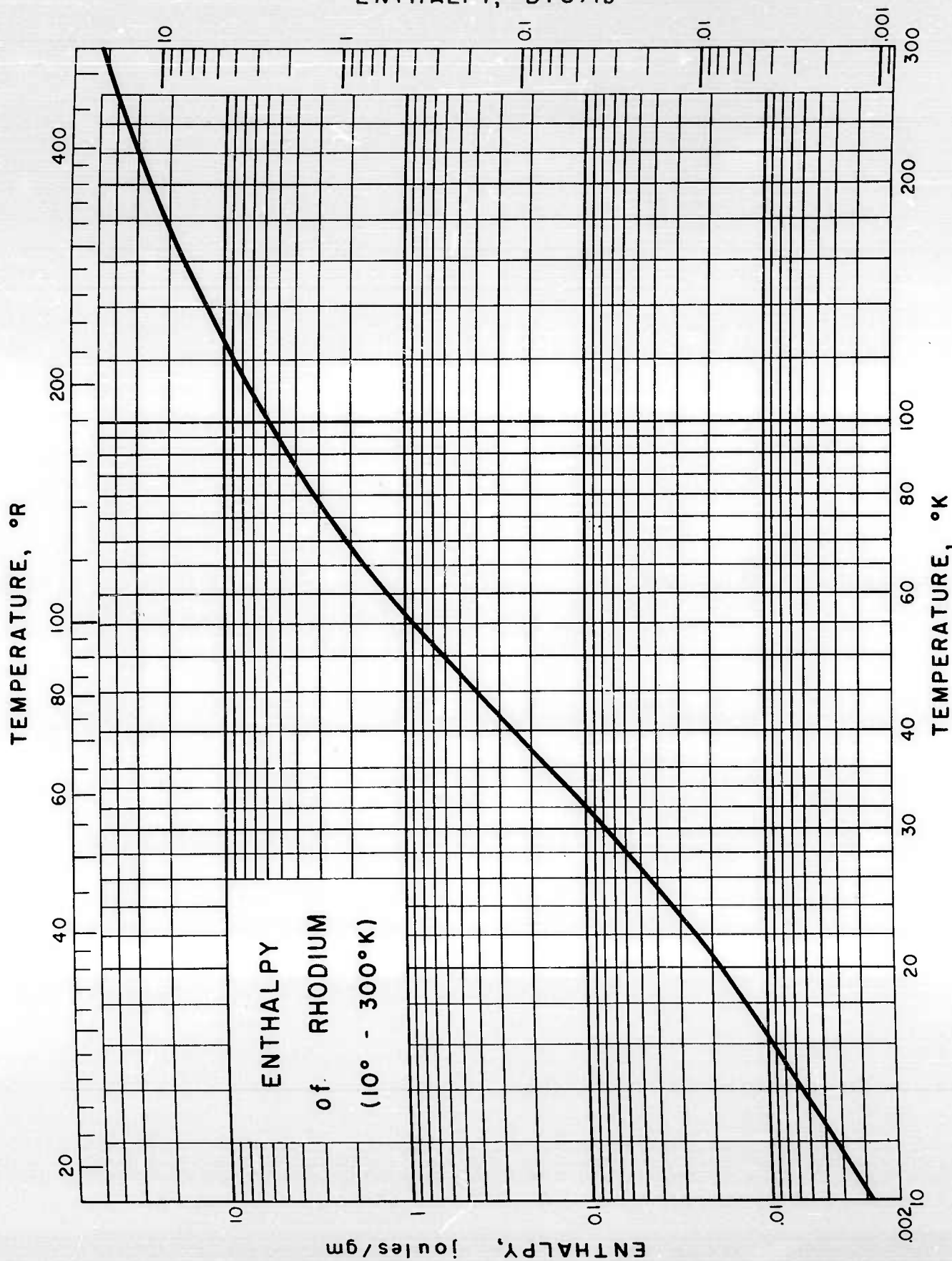




4.162

TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of WOOD'S METAL

(Sn, 12.5%; Cd, 12.5%; Pb, 25%; Bi, 50%)

Source of Data:

Parkinson, D. H. and Quarrington, J. E., Brit. J. Appl. Phys. 5, 219-20 (1954)

Comments:

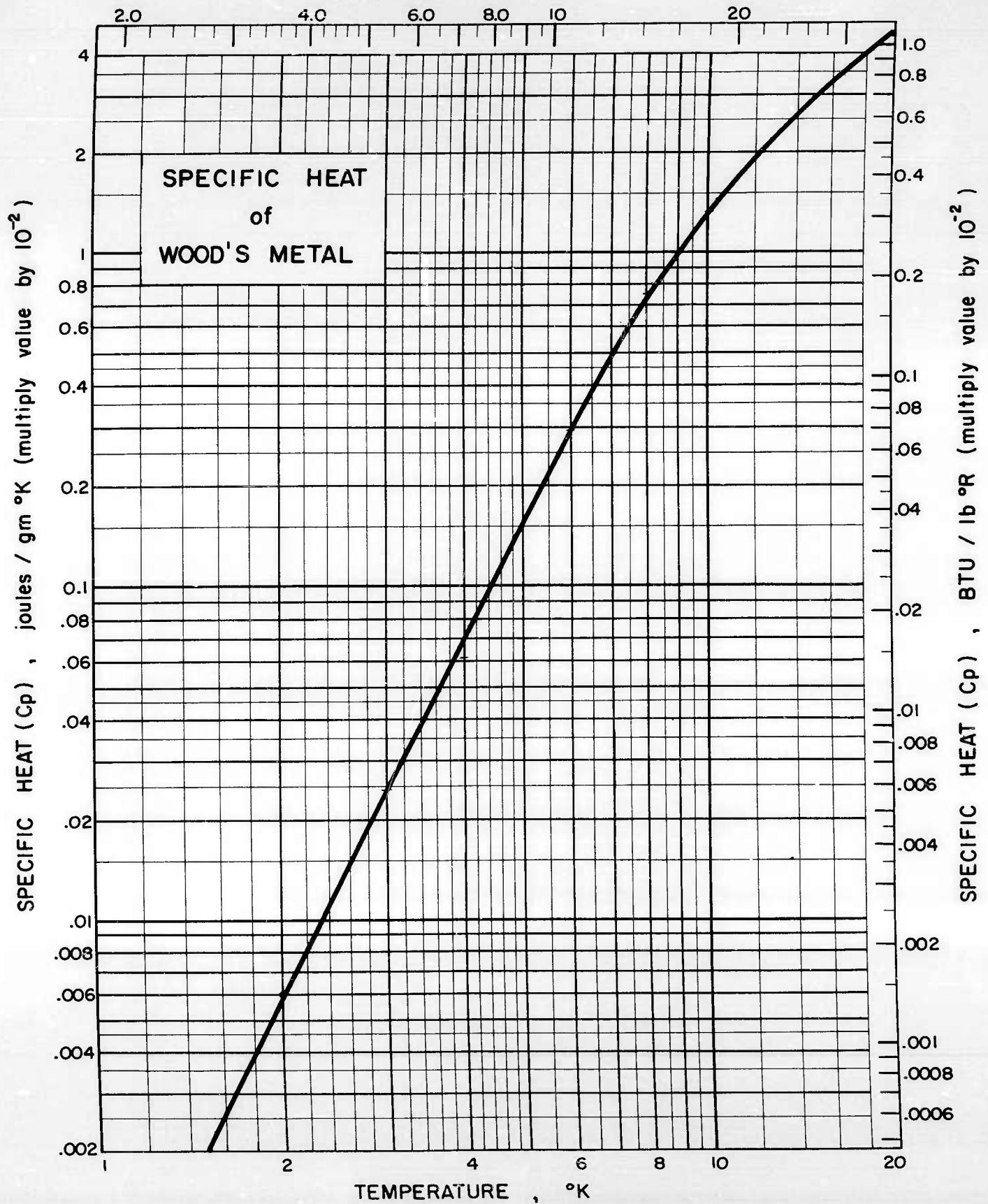
There was slight evidence of a superconducting transition at approximately 4.8°K. Tabulated values below 6°K are from measurements made in the superconducting state.

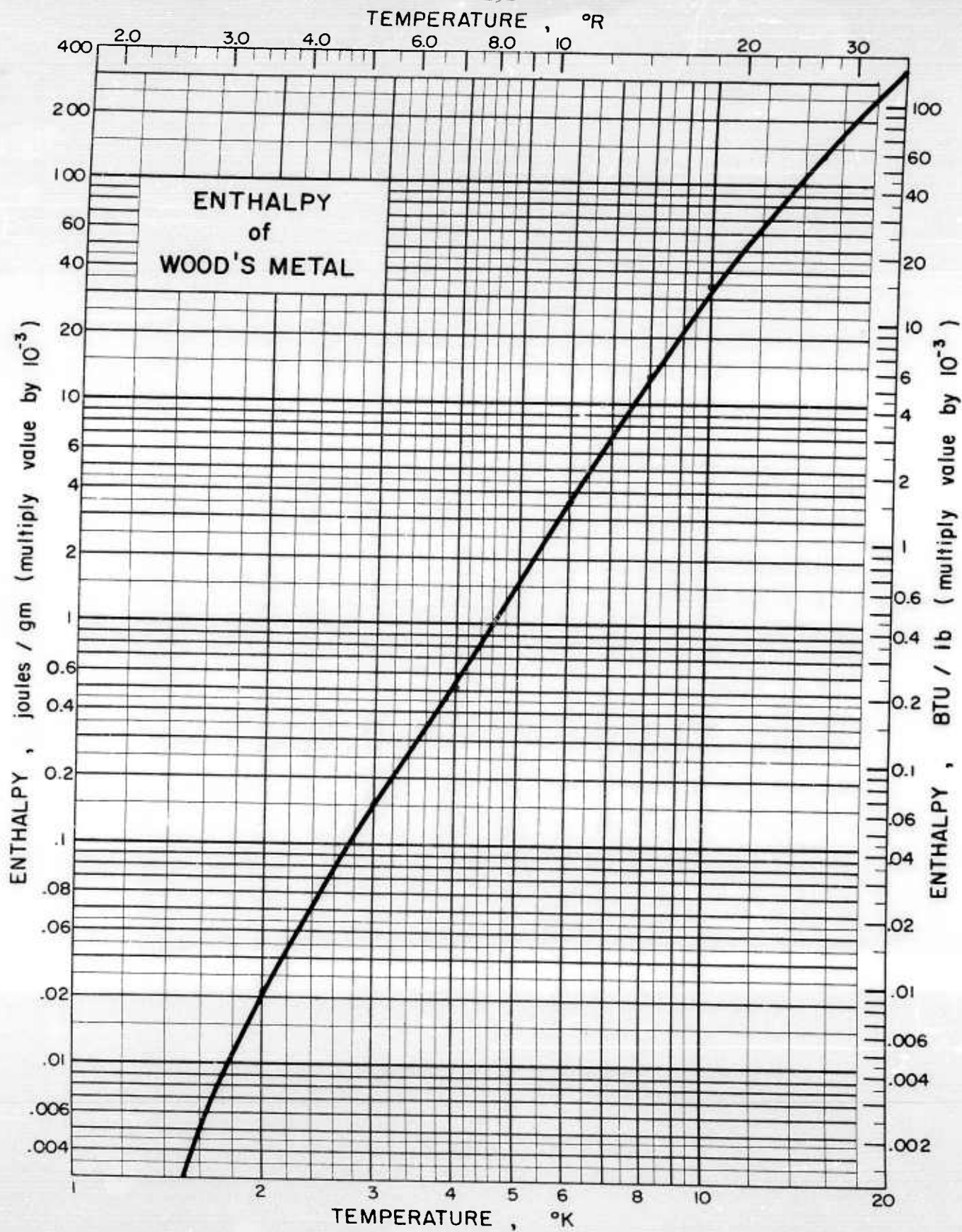
Table of Selected Values

| Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|
| 1.5 | 0.000 02 | 0.000 003 |
| 2 | .000 06 | .000 022 |
| 3 | .000 24 | .000 154 |
| 4 | .000 62 | .000 516 |
| 6 | .002 9 | .003 57 |
| 8 | .007 6 | .013 8 |
| 10 | .013 4 | .034 7 |
| 15 | .029 7 | .142 |
| 20 | .046 0 | .331 |

4.252

TEMPERATURE, °R





SPECIFIC HEAT, ENTHALPY of ARALDITE

(TYPE I)

Source of Data:

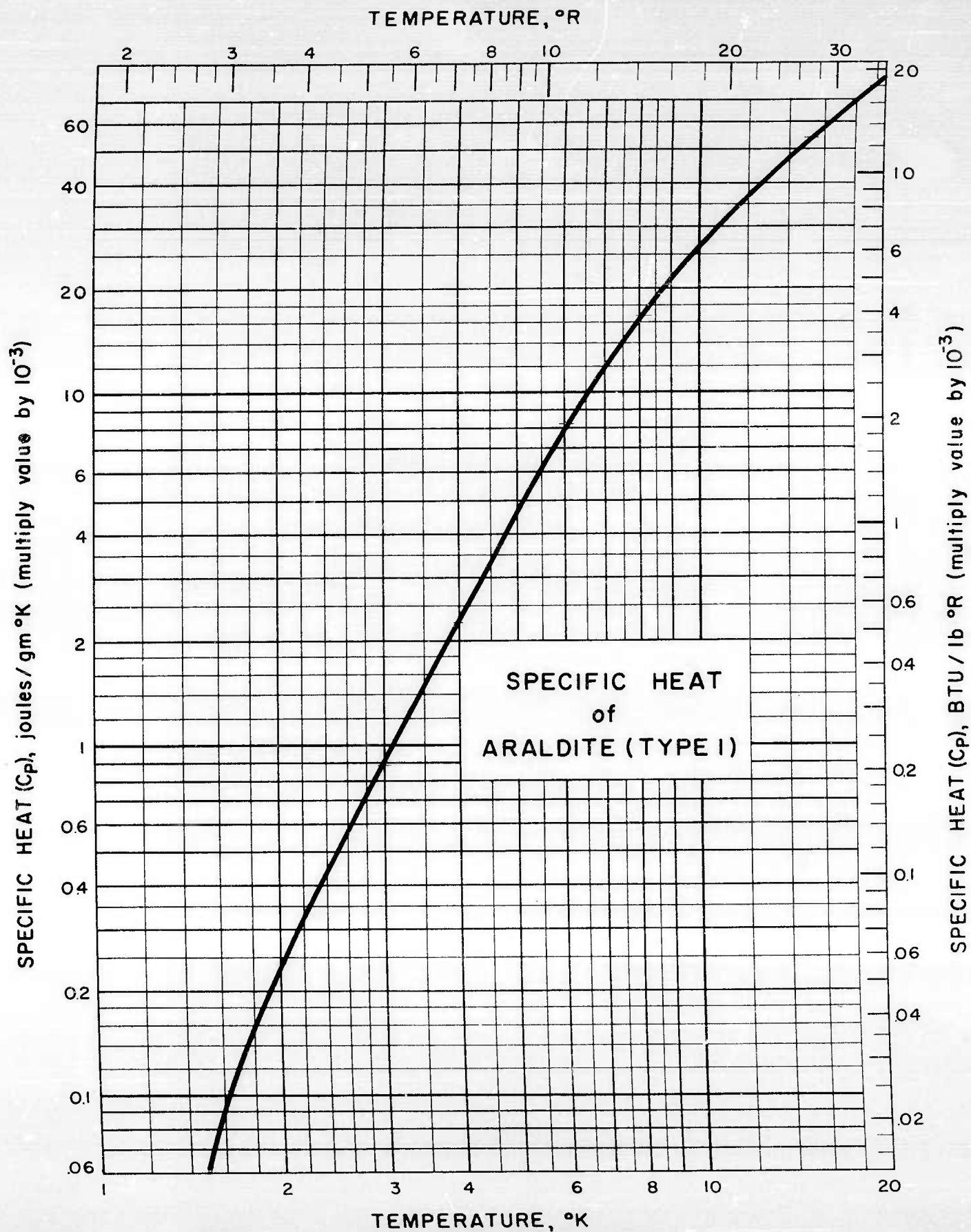
Parkinson, D. H. and Quarrington, J. E., Brit. J. Appl. Phys. 5, 219-20 (1954)

Comments:

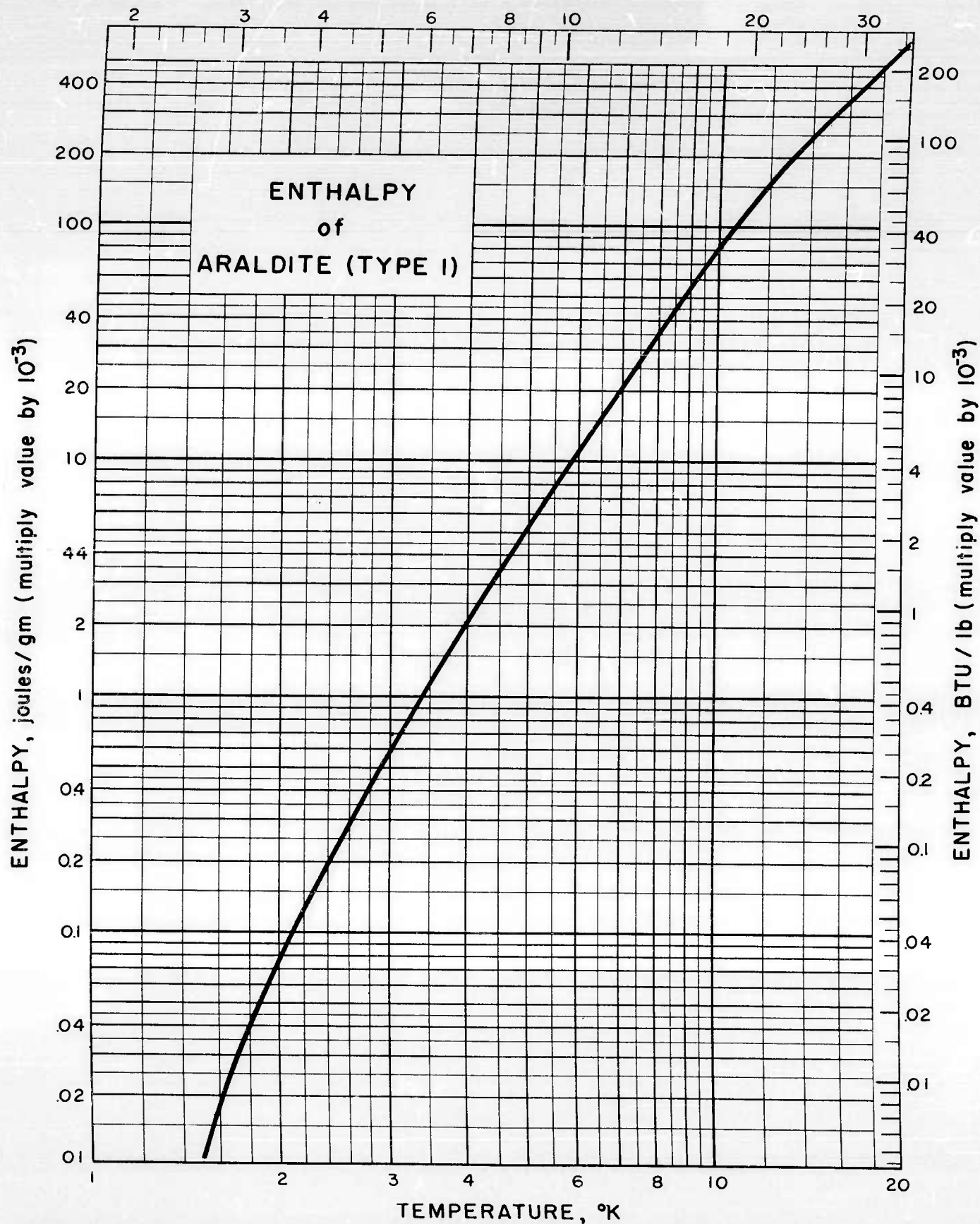
Sample prepared according to manufacturer's directions.

Table of Selected Values

| Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|
| 1.5 | 0.000 06 | 0.000 01 |
| 2 | .000 24 | .000 08 |
| 3 | .000 89 | .000 60 |
| 4 | .002 25 | .002 10 |
| 6 | .008 2 | .011 7 |
| 8 | .016 9 | .036 7 |
| 10 | .027 2 | .080 7 |
| 15 | .054 2 | .284 |
| 20 | .081 1 | .623 |



TEMPERATURE, °R



SPECIFIC HEAT, ENTHALPY of PYREX

Source of Data:

Smith, P. L. and Wolcott, N. M., Phil. Mag. 1, 854-65 (1956)

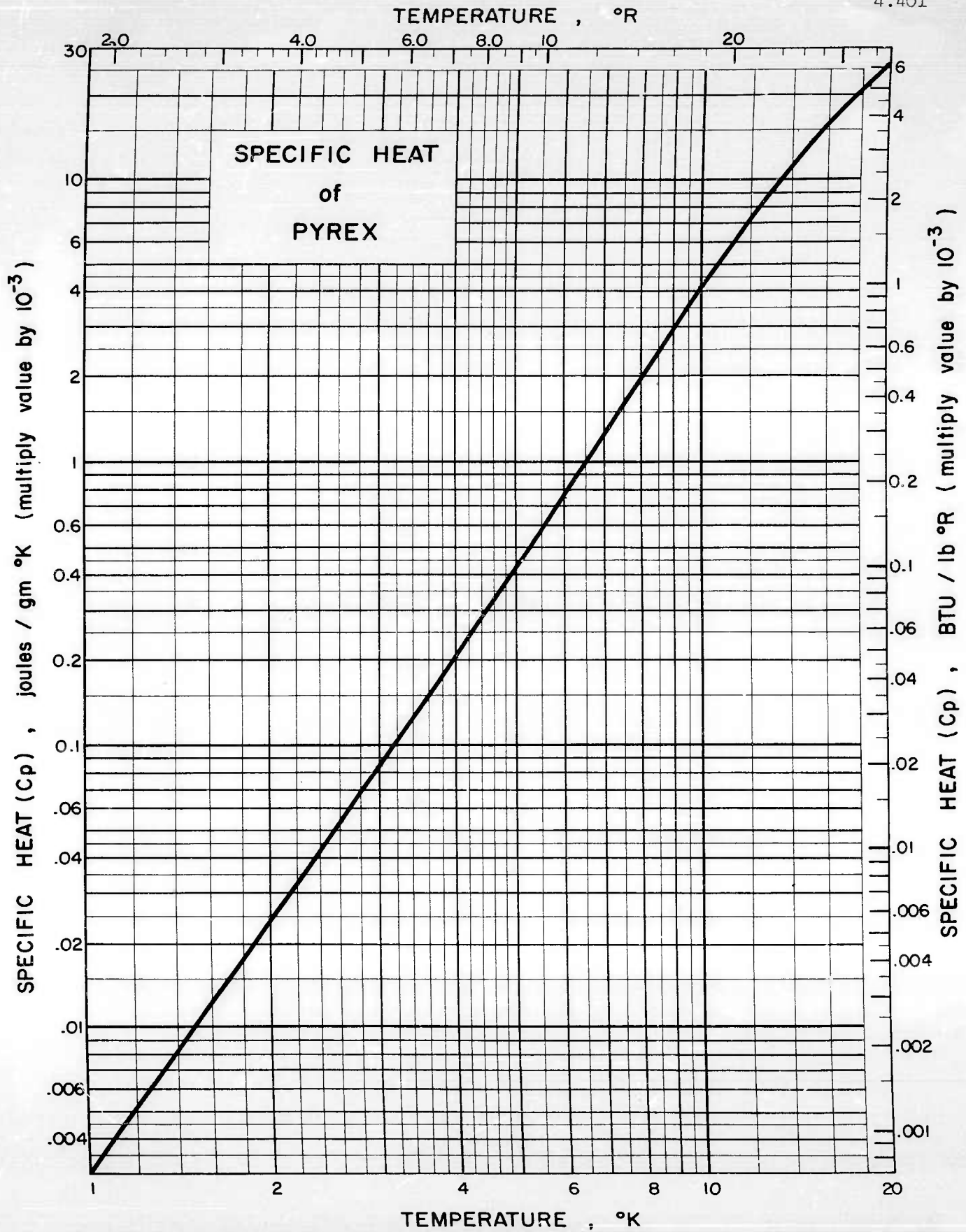
Comments:

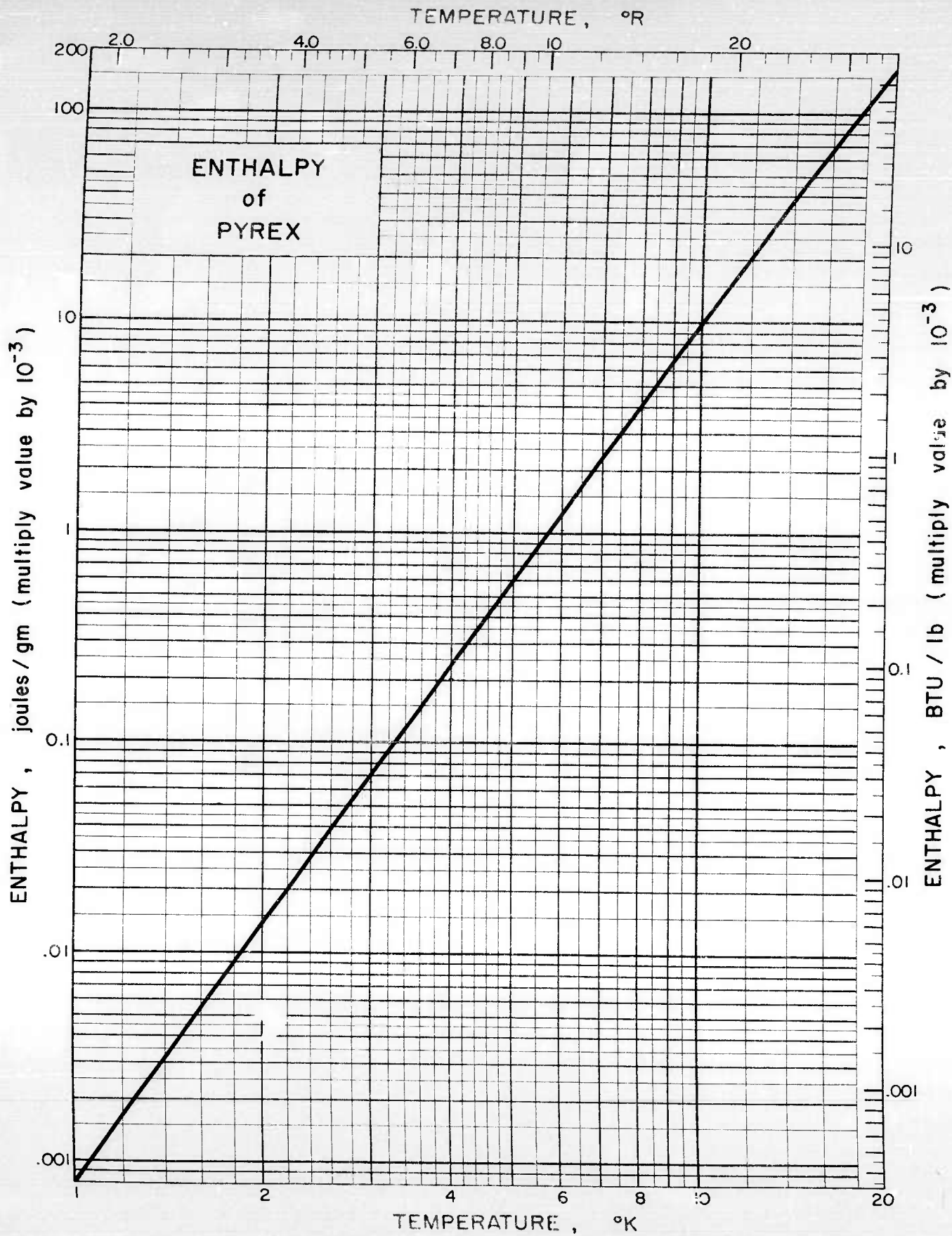
The values for C_p at temperatures less than 5°K can be expressed by the formula:

$$C_p = (3.14 \times 10^{-6})T^3 \text{ j/gm-}^\circ\text{K}$$

Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|------------|
| 1 | 0.000 0031 | 0.000 0008 |
| 2 | .000 025 | .000 013 |
| 3 | .000 084 | .000 064 |
| 4 | .000 201 | .000 201 |
| 6 | .000 753 | .001 04 |
| 8 | .002 09 | .003 94 |
| 10 | .004 19 | .010 0 |
| 15 | .013 7 | .052 5 |
| 20 | .027 4 | .154 |



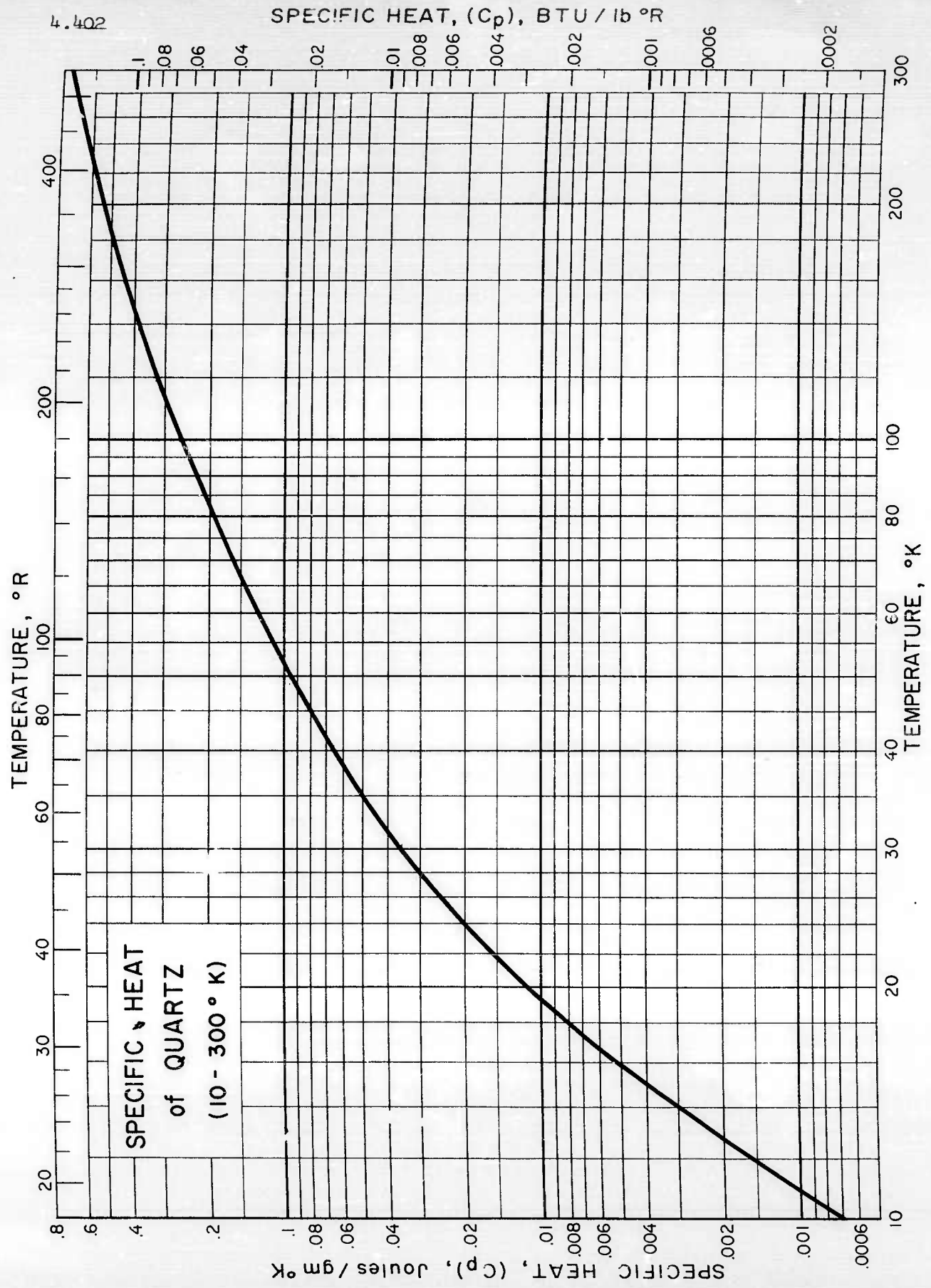


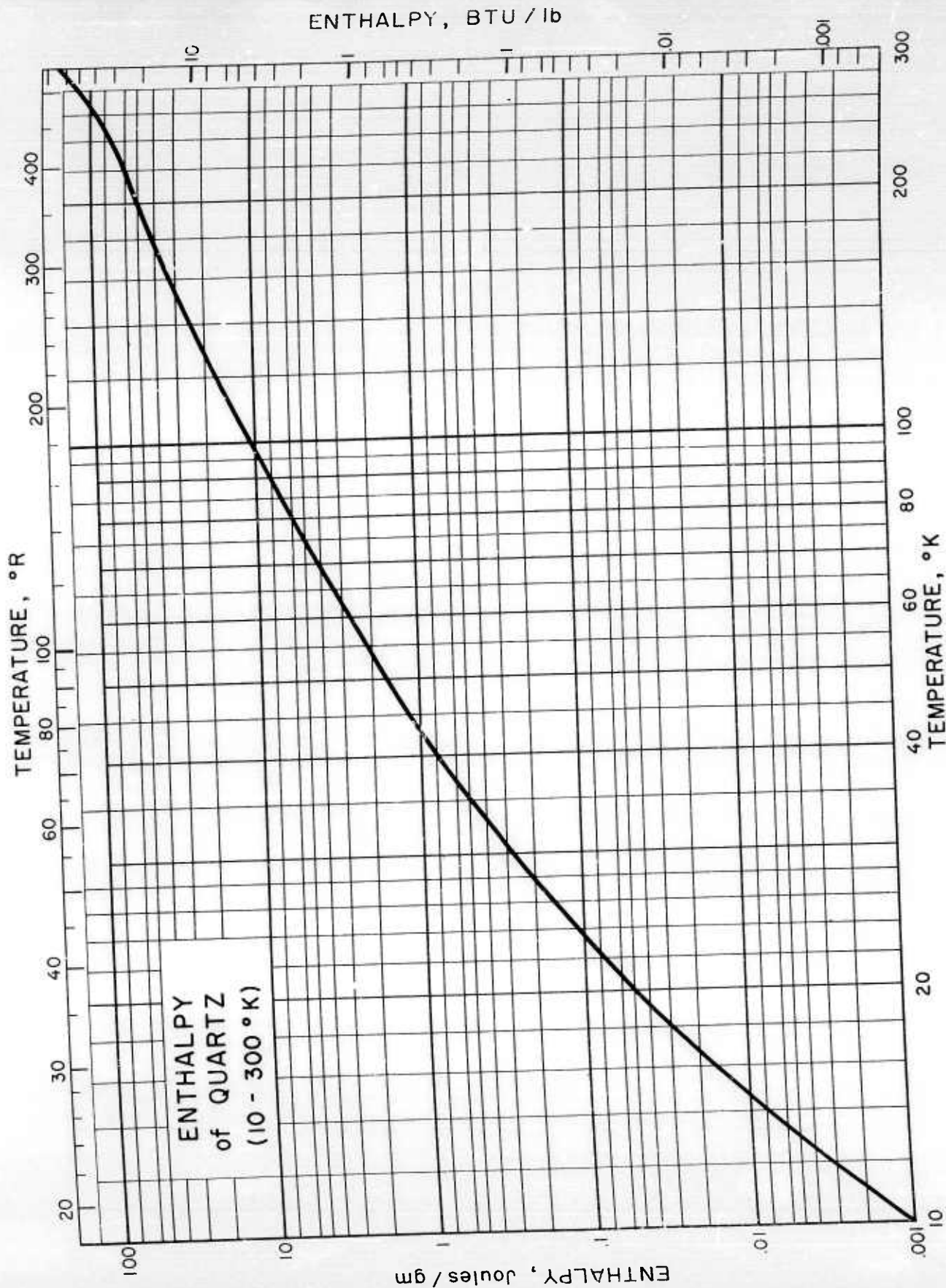
SPECIFIC HEAT and ENTHALPY of QUARTZ

Sources of Data:Anderson, C. T., J. Am. Chem. Soc. 58, 568 (1936)Westrum, E. F.; data reproduced in Lord, R.C. and Morrow, J. C., J. Chem. Phys. 26, 230 (1957)Other References:Gunther, P., Z. anorg. u allgem. Chem. 116, 71 (1921)Nernst, W., Ann. Physik (4) 36, 395 (1911)

Table of Selected Values

| T °K | Cp j/gm-°K | H j/gm | T °K | Cp j/gm-°K | H j/gm |
|---------|---------------|-----------|---------|---------------|-----------|
| 10 | 0.0007 | 0.001 | 100 | 0.261 | 10.51 |
| 15 | .0040 | 0.012 | 120 | .325 | 16.37 |
| 20 | .0113 | 0.049 | 140 | .385 | 23.48 |
| 25 | .0221 | 0.131 | 160 | .441 | 31.75 |
| 30 | .0353 | 0.273 | 180 | .494 | 41.1 |
| 40 | .0653 | 0.773 | 200 | .543 | 51.5 |
| 50 | .0969 | 1.583 | 220 | .588 | 62.8 |
| 60 | .129 | 2.71 | 240 | .631 | 75.0 |
| 70 | .162 | 4.17 | 260 | .671 | 88.0 |
| 80 | .195 | 5.95 | 280 | .709 | 101.8 |
| 90 | .228 | 8.07 | 300 | .745 | 116.4 |





SPECIFIC HEAT, ENTHALPY of ICE

Sources of Data:

Giauque, W. F. and Stout, J. W., J. Am. Chem. Soc. 58, 1144 (1936)

Simon, F., unpublished (1923). Data reproduced in Giauque and Stout (see above).

Other References:

Barnes, W. H. and Maas, O., Can. J. Research 3, 205 (1930)

Duyckaerts, G., Mem. soc. roy. sci. Liege 6, 325 (1945)

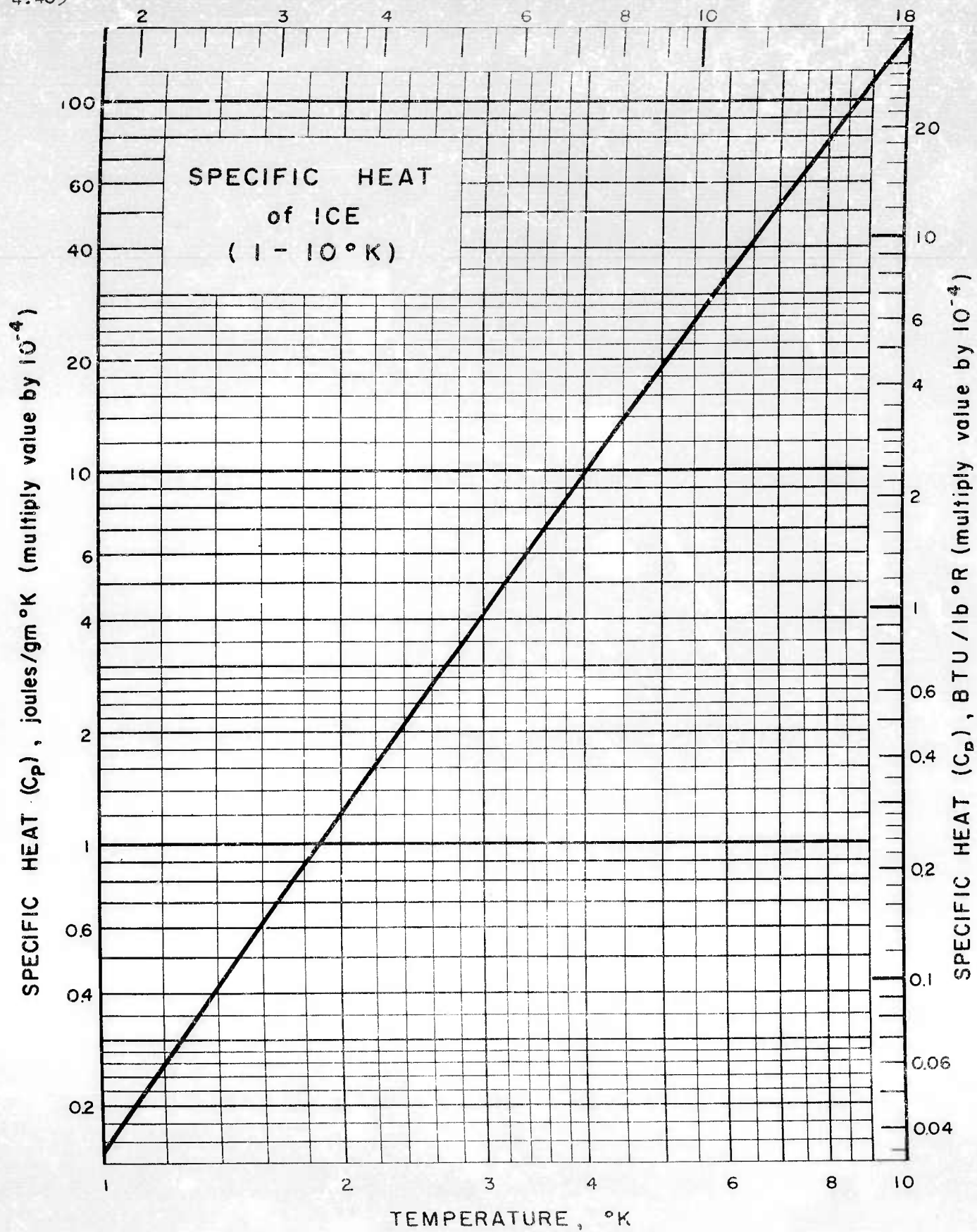
Nernst, W., Ann. physik, ser. 4, 36, 395 (1911)

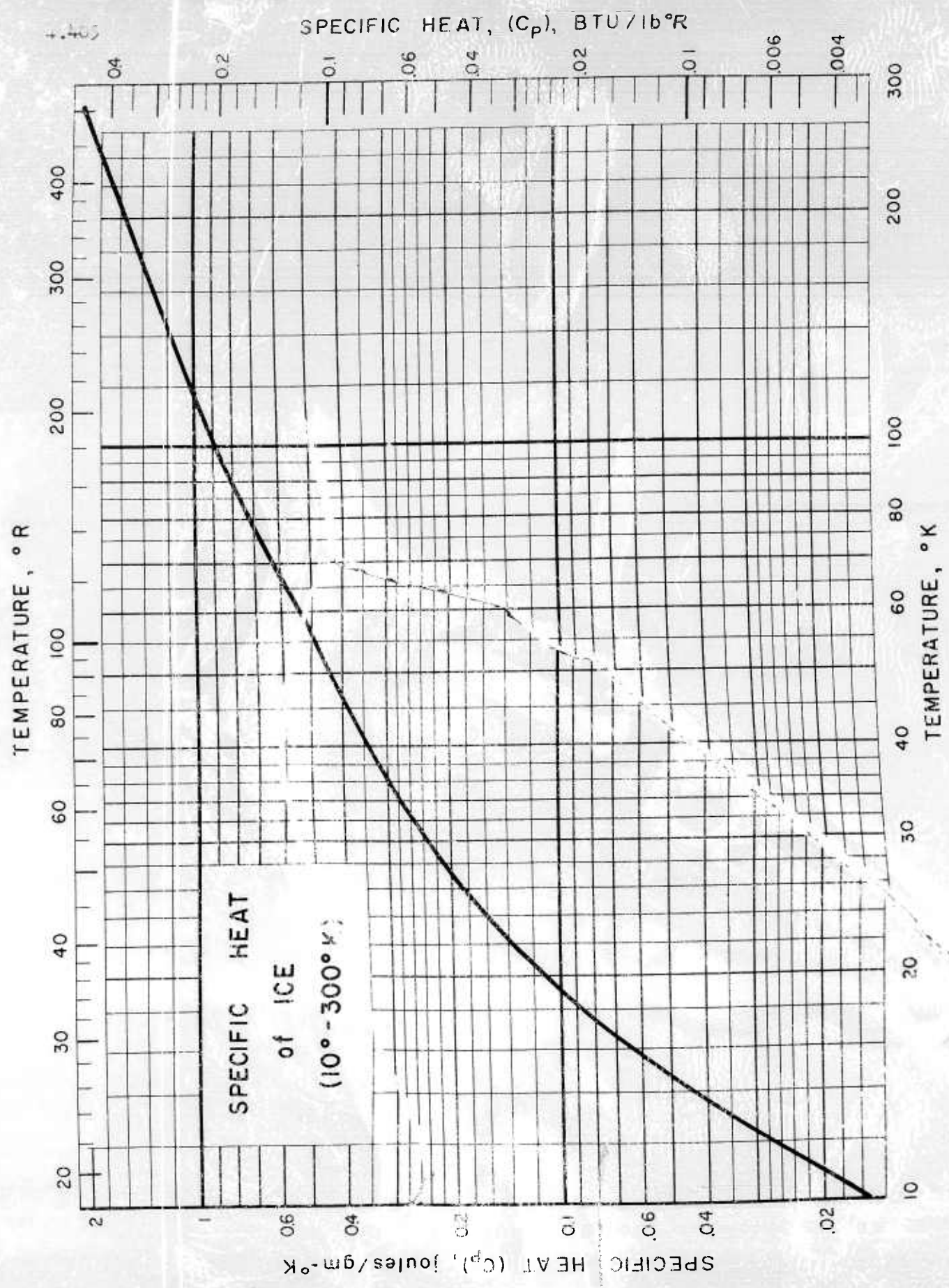
Pollitzer, F., Z. Elektrochem. 19, 513 (1913)

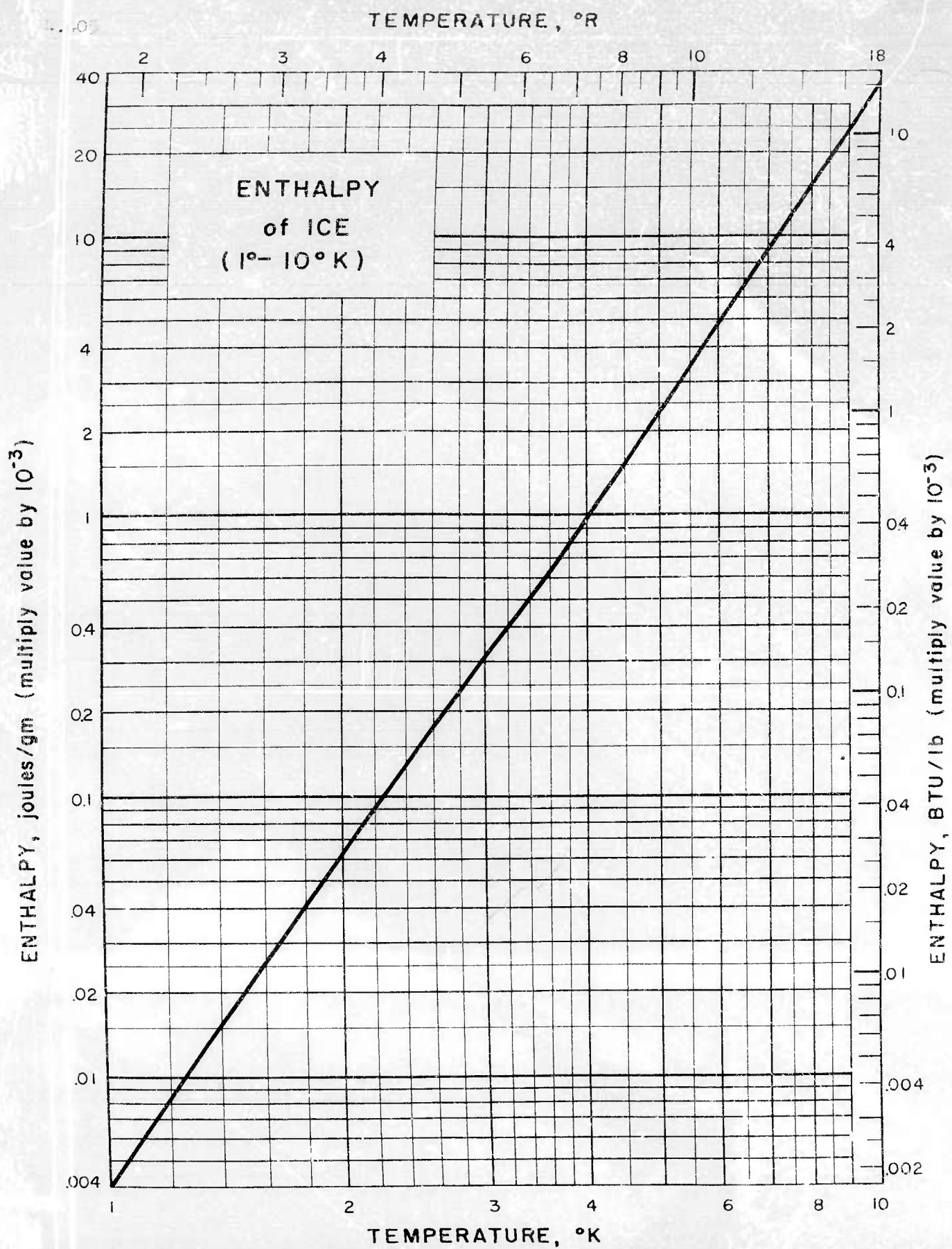
Table of Selected Values

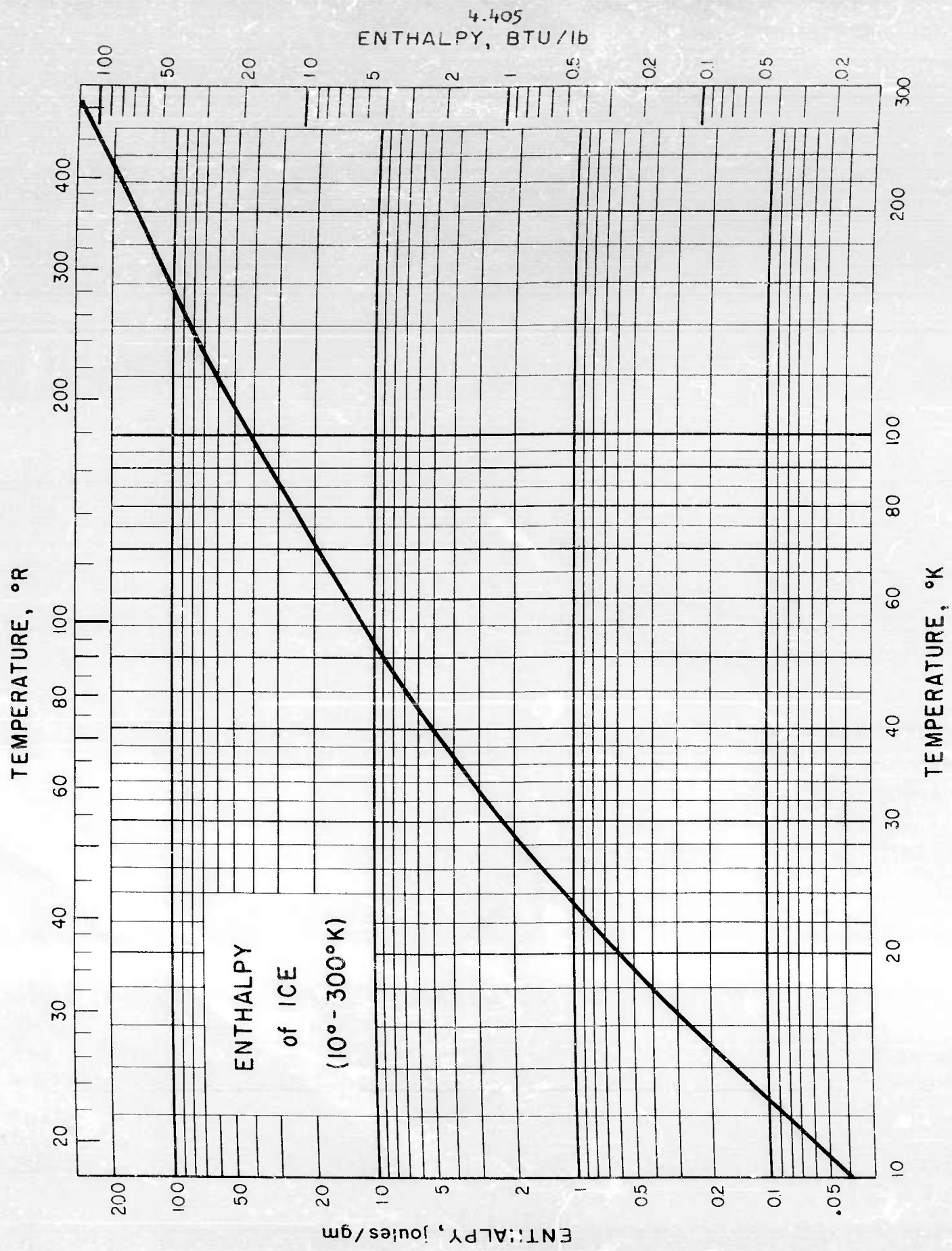
| Temp. °K | C _p j/gm-°K | H j/gm | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|-------------|---------------------------|-----------|
| 1 | 0.000 015 | 0.000 004 | 60 | 0.535 | 13.97 |
| 2 | 0.000 12 | 0.000 061 | 70 | 0.627 | 19.78 |
| 3 | 0.000 41 | 0.000 31 | 80 | 0.716 | 26.49 |
| 4 | 0.000 98 | 0.000 98 | 90 | 0.801 | 34.06 |
| 6 | 0.003 3 | 0.004 9 | 100 | 0.882 | 42.47 |
| 8 | 0.007 8 | 0.015 6 | 120 | 1.03 | 61.6 |
| 10 | 0.015 2 | 0.038 | 140 | 1.16 | 83.5 |
| 12 | 0.026 5 | 0.079 | 160 | 1.29 | 108.0 |
| 14 | 0.043 | 0.148 | 180 | 1.43 | 135.2 |
| 16 | 0.065 | 0.255 | 200 | 1.57 | 165.1 |
| 18 | 0.090 | 0.410 | 220 | 1.72 | 197.9 |
| 20 | 0.114 | 0.615 | 240 | 1.86 | 233.7 |
| 30 | 0.229 | 2.33 | 260 | 2.01 | 272.4 |
| 40 | 0.340 | 5.18 | 270 | 2.08 | 292.8 |
| 50 | 0.440 | 9.09 | 273.15 | 2.10 | 299.4 |

RJC Issued: 12-18-59









SPECIFIC HEAT, ENTHALPY of MgO

Source of Data:

Giauque, W. R. and Archibald, R. C., J. Am. Chem. Soc. 59, 561 (1937)

Other References:

Gunther, P., Ann. phys. 51, 838 (1916)

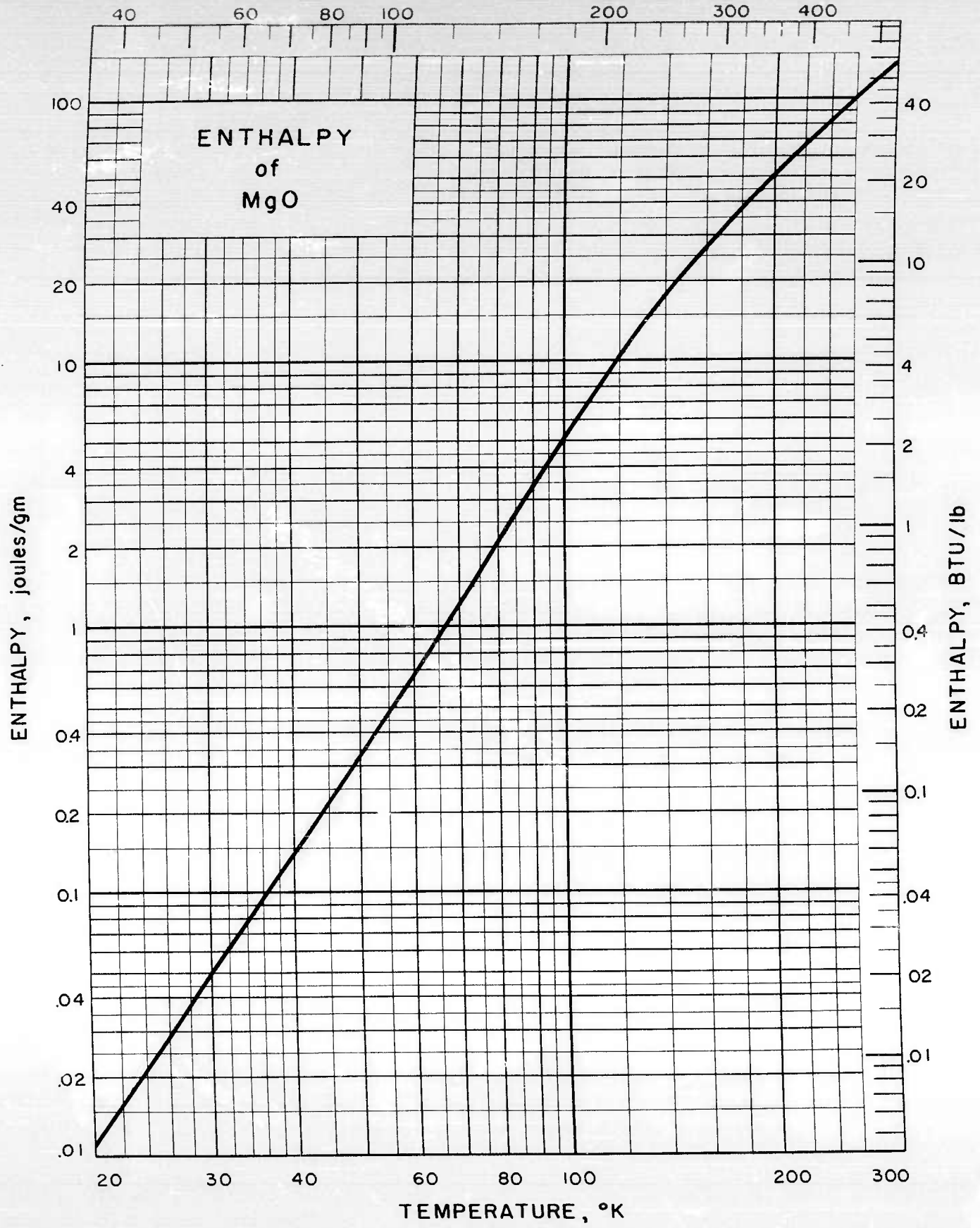
Parks, G. S. and Kelley, K. K., J. Phys. Chem. 30, 47 (1926)

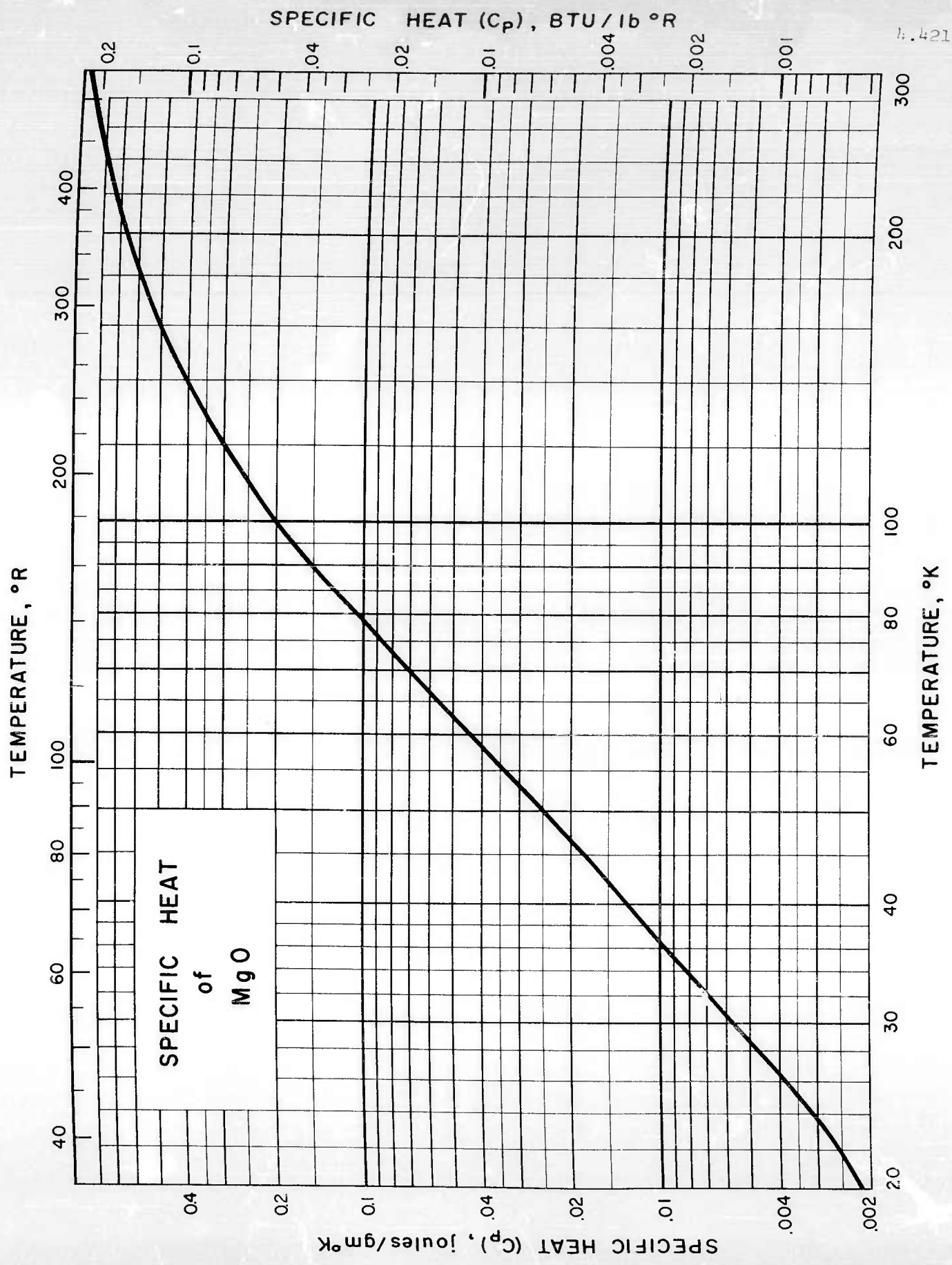
Comments:

The data of Parks and Kelley are believed to be the most representative of bulk crystalline MgO but unfortunately do not extend below 94°K. Accordingly we have used the more complete data of Giauque and Archibald, even though they were obtained using a fine powder sample and appear to be too high on that account. The extra specific heat due to the surface can be estimated by comparison with the data of Parks and Kelley and also by fitting the data below 70°K (approx. $\theta_0/12$) with the expression $C = aT^2 + bT^3$, in which the first term gives the surface contribution [Keesom and Pearlman, Handbuch der Physik XIV, 332-3 (1956)]. If this interpretation is correct one finds that the surface term amounts to about one-third of the total specific heat at 20°, about 5% at 100°, and is negligible at 300°K.

| Temp. °K | C_p j/gm-°K | H j/gm | Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|-----------|-------------|------------------|-----------|
| 20 | 0.0022 | 0.011 | 100 | 0.208 | 5.31 |
| 25 | .0036 | .025 | 120 | .312 | 10.5 |
| 30 | .0059 | .048 | 140 | .42 | 17.8 |
| 35 | .0090 | .084 | 160 | .51 | 27.0 |
| 40 | .0131 | .139 | 180 | .60 | 38.1 |
| 45 | .0182 | .217 | 200 | .68 | 50.9 |
| 50 | .0243 | .322 | 220 | .74 | 65.1 |
| 60 | .041 | .64 | 240 | .80 | 80.6 |
| 70 | .073 | 1.20 | 260 | .85 | 97.2 |
| 80 | .113 | 2.13 | 280 | .90 | 114.7 |
| 90 | .159 | 3.48 | 300 | .94 | 133.1 |

RJC/JJG Issued: 10-21-59
Revised: 5/20/60





SPECIFIC HEAT AND ENTHALPY OF
GR-S (BUNA S) RUBBER (1-3 BUTADIENE, 25 WT. % STYRENE)

Source of Data:

Rands, R. D. Jr., Ferguson, W. T. and Prather, J. L., J. Research
Natl. Bur. Standards 33, 63-70 (1944)

Comments:

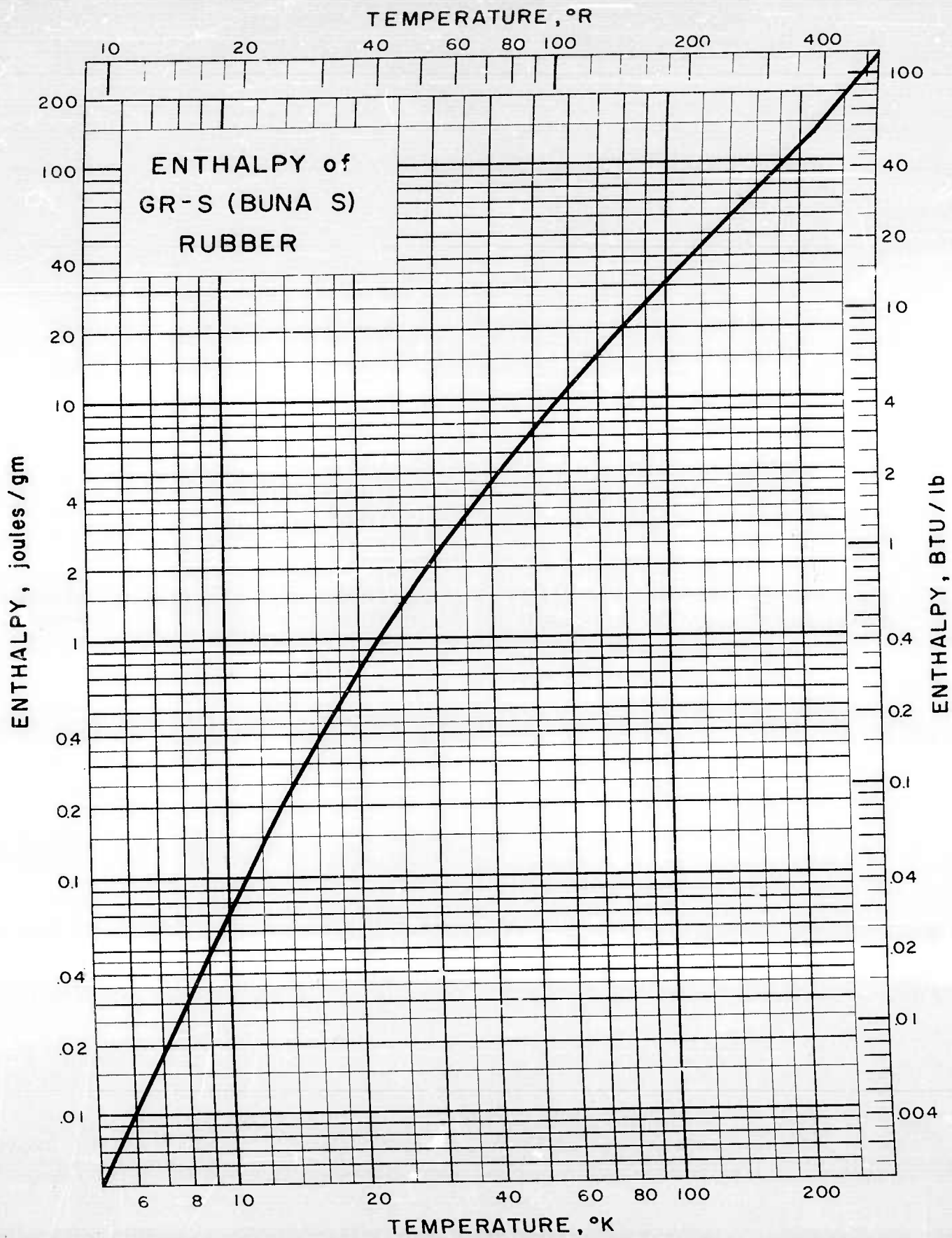
A second-order transition which indicates a change of slope occurs
at about 212 °K. Hysteresis occurs in the region immediately below
this transition.

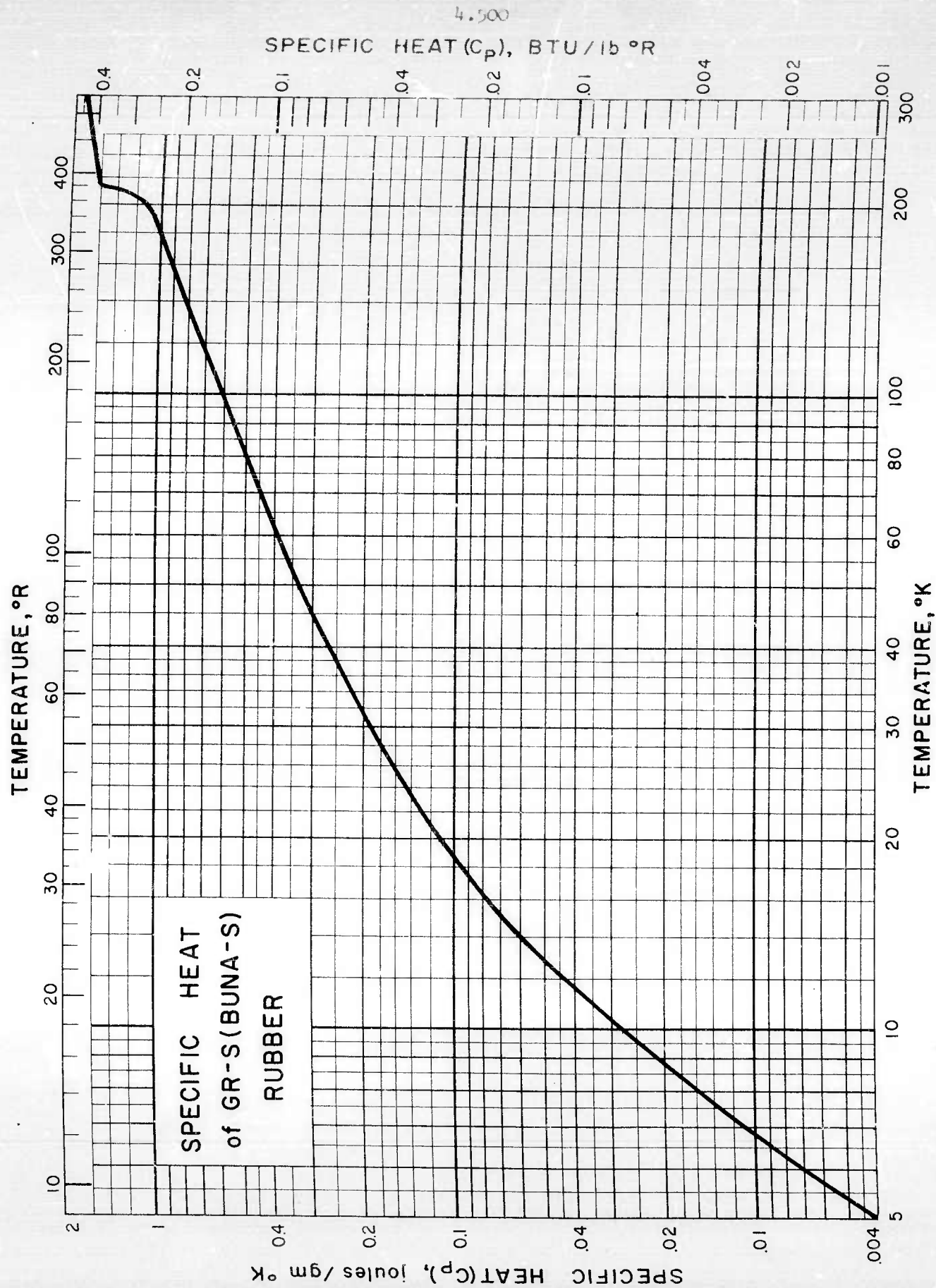
Table of Selected Values

| Temp. °K | C _p j/gm-°K | H j/gm | Temp. °K | C _p j/gm-°K | H j/gm |
|-------------|---------------------------|-----------|-------------|---------------------------|-----------|
| 5 | 0.004 | 0.005 | 120 | 0.711 | 45.0 |
| 10 | .028 | .07 | 140 | .811 | 60.2 |
| 15 | .070 | .31 | 160 | .911 | 77.4 |
| 20 | .113 | .77 | 180 | 1.01 | 96.7 |
| 25 | .155 | 1.44 | 200 | 1.12 | 118.0 |
| 30 | .196 | 2.32 | 210 | 1.34 | 130.0 |
| 40 | .272 | 4.66 | 212 | 1.66 | 133.3 |
| 50 | .338 | 7.72 | 220 | 1.68 | 146.1 |
| 60 | .399 | 11.40 | 240 | 1.73 | 180.1 |
| 70 | .455 | 15.68 | 260 | 1.78 | 215.2 |
| 80 | .509 | 20.50 | 280 | 1.84 | 251.4 |
| 90 | .562 | 25.86 | 300 | 1.90 | 288.7 |
| 100 | .612 | 31.74 | | | |

R. /JJG Issued: 10-21-59

4.500





SPECIFIC HEAT and ENTHALPY of NATURAL
RUBBER HYDROCARBON (Amorphous)

Source of Data:

Bekkedahl, N., and Matheson, H. J., Research Nat. Bur. Standards 15, 503 (1934)

Comments:

These data apply to pure hydrocarbon polymer extracted from latex. Commercial natural rubber differs from this by containing various additives and having been vulcanized. No low-temperature data for vulcanized rubber have been found, and the data on this sheet are presented as being the closest available approximation thereto. A second-order transformation (glass transformation) occurs at about 200°K. The data in this region are the least applicable to other forms of rubber since the temperature and shape of the transition in C_p will be rather strongly affected by vulcanization and additives.

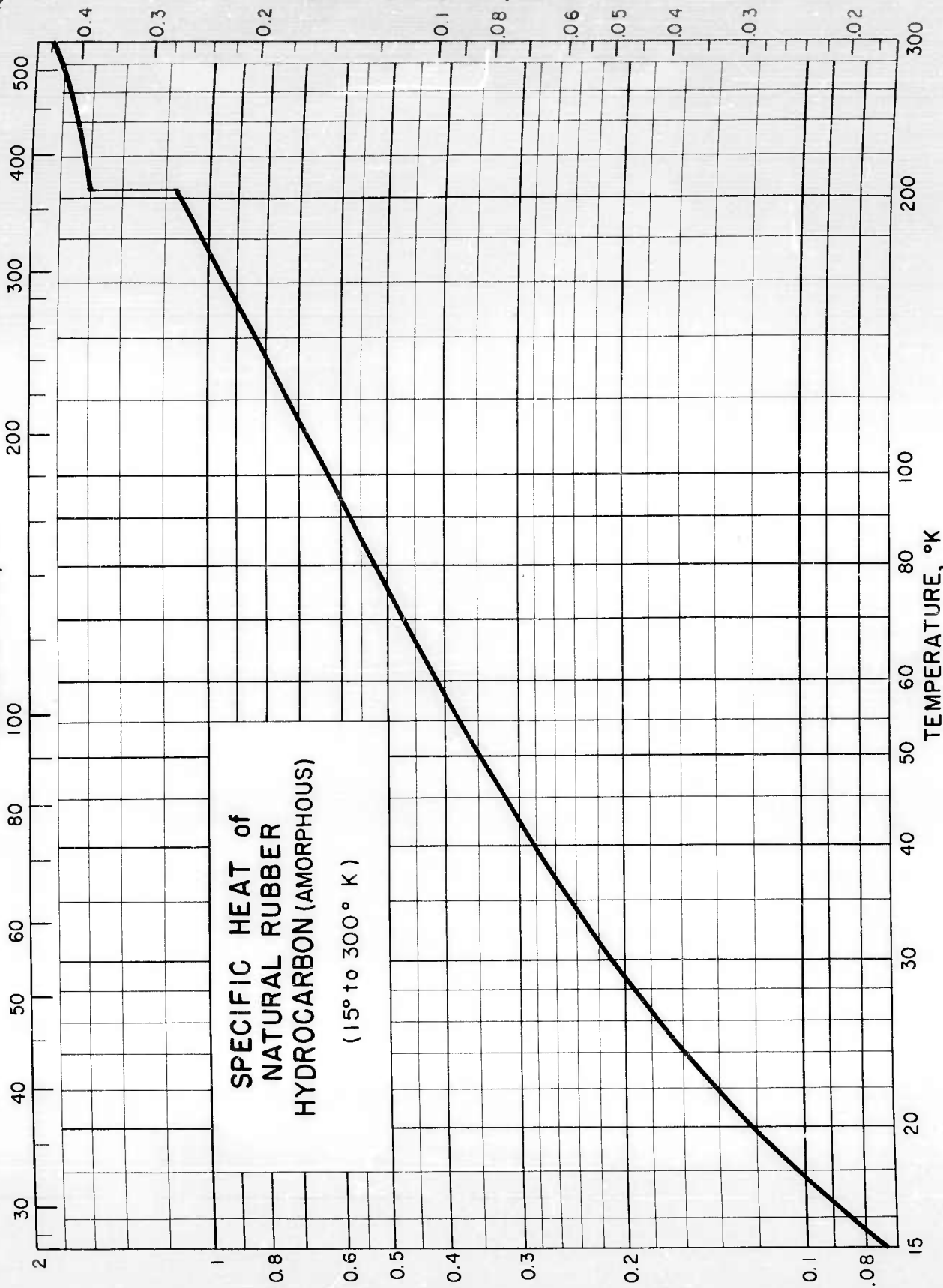
Table of Selected Values

| T | C_p | H | T | C_p | H |
|-----|---------|-------|------|---------|-------|
| °K | j/gm-°K | j/gm | °K | j/gm-°K | j/gm |
| 15 | 0.073 | 0.32 | 180 | 1.03 | 100.7 |
| 20 | .117 | 0.80 | 190 | 1.08 | |
| 30 | .204 | 2.41 | 195 | 1.10 | |
| 40 | .282 | 4.84 | 200* | 1.44 | |
| 50 | .352 | 8.01 | 205 | 1.60 | |
| 60 | .418 | 11.87 | 210 | 1.61 | |
| 70 | .480 | 16.36 | 220 | 1.64 | 155.0 |
| 80 | .537 | 21.45 | 240 | 1.70 | 188.4 |
| 90 | .596 | 27.12 | 260 | 1.75 | 222.9 |
| 100 | .646 | 33.34 | 280 | 1.81 | 258.4 |
| 120 | .75 | 47.3 | 290 | 1.84 | 276.6 |
| 140 | .84 | 63.2 | 300 | 1.89 | 295.3 |
| 160 | .94 | 81.0 | | | |

* Second-order transition

4.502

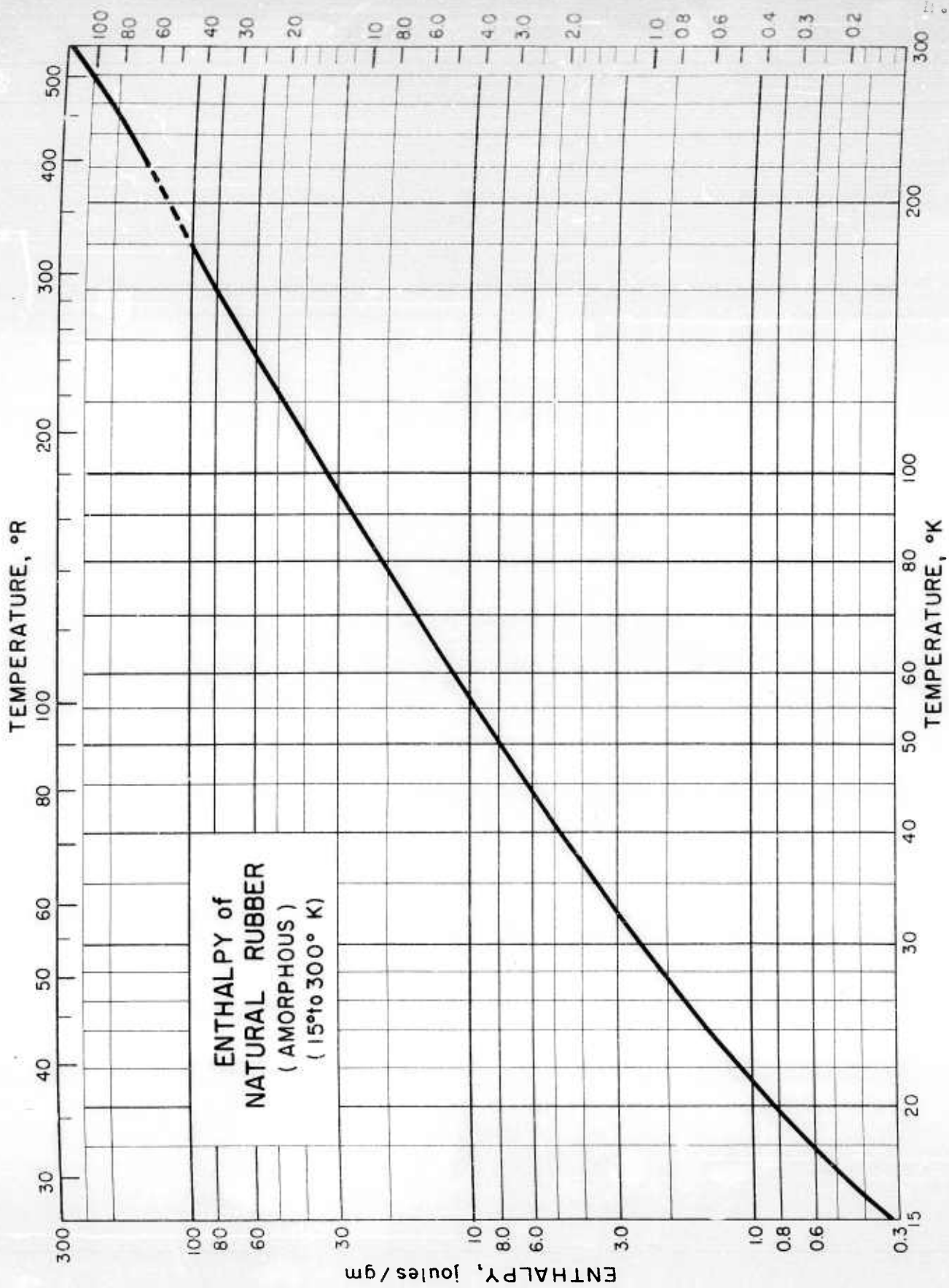
TEMPERATURE, °R



SPECIFIC HEAT OF
NATURAL RUBBER
HYDROCARBON (AMORPHOUS)
(15° to 300° K)

SPECIFIC HEAT, joules / gm -°K

TEMPERATURE, °K



SPECIFIC HEAT and ENTHALPY of TEFLON (MOLDED)

Source of Data:

Furukawa, G. T., McCoskey, R. E. and King, G. J., J. Research Natl. Bur. Standards 49, 273 (1952)

Other References:

Noer, R. J., Dempsey, C. W. and Gordon, J. E., Bull. Am. Phys. Soc. 4, 108 (1959)

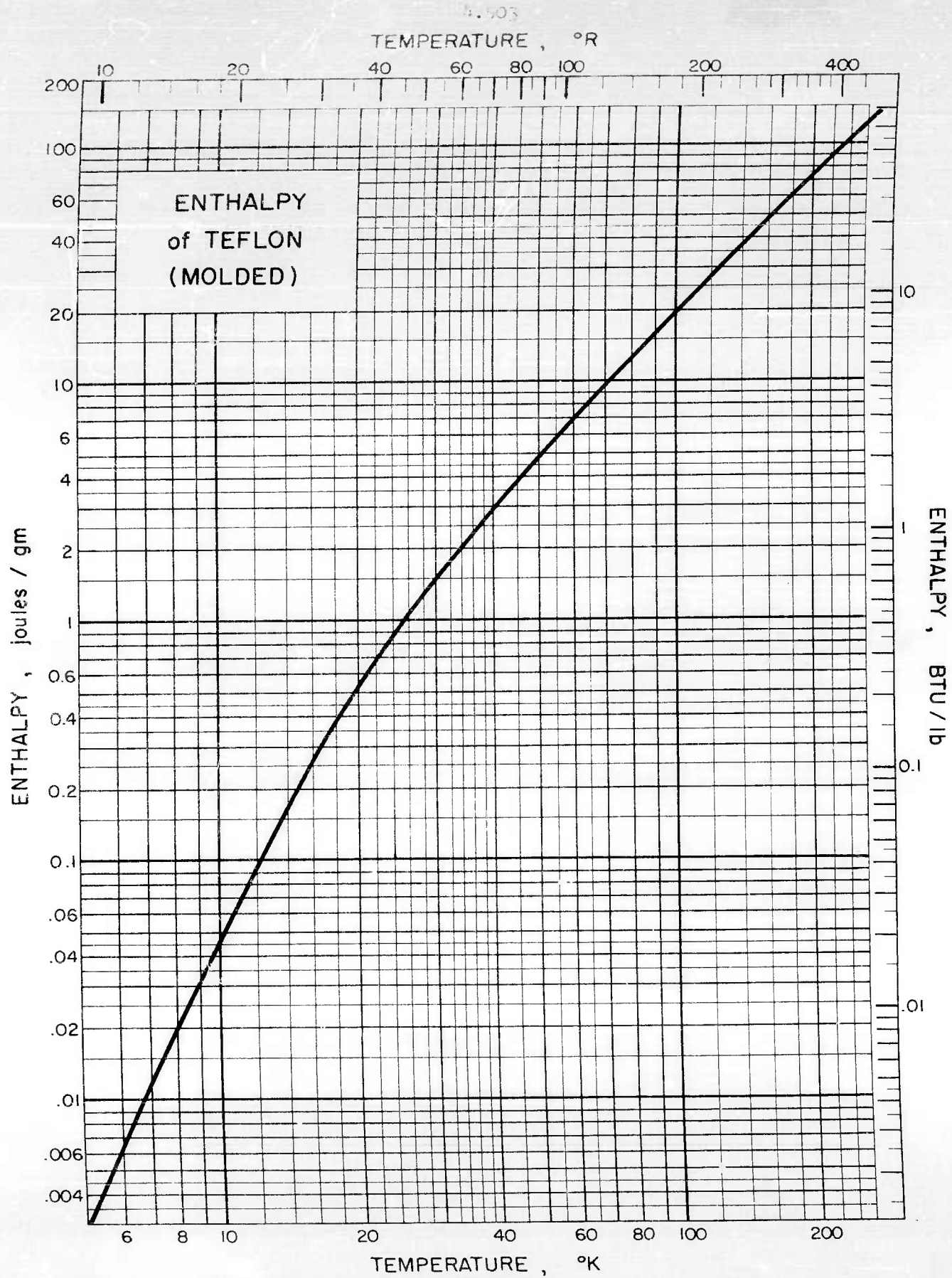
Comments:

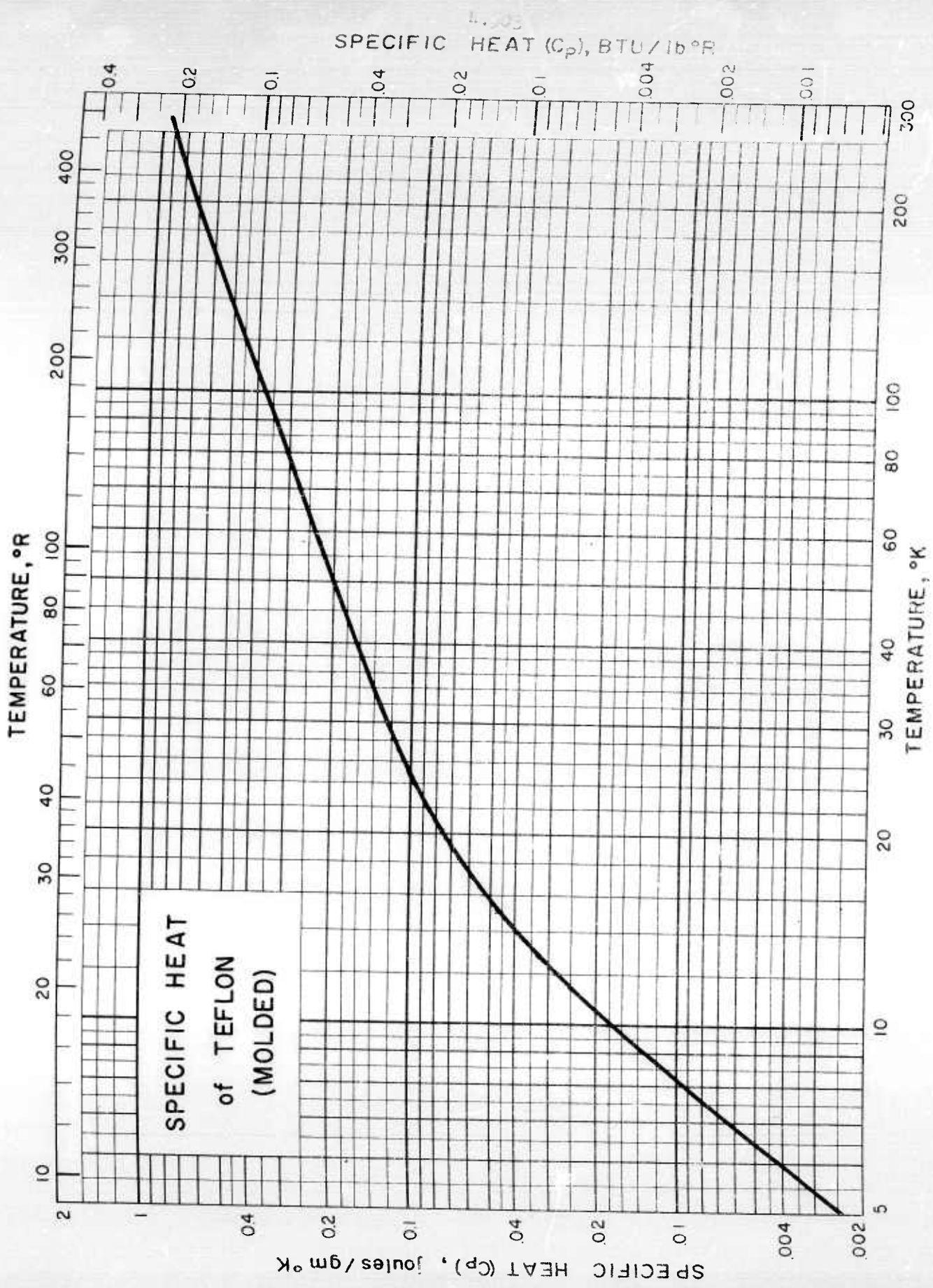
The above reference (Furukawa, et al.), also gives data on molded and annealed, molded and quenched, and powdered teflon. The effects of heat treatment do not exceed 3% and are not significant below 150°K. The data indicate a second-order transition at about 160°K and two first-order transitions between 280°K and 310°K. Thermal hysteresis occurs in these regions. Because of this effect, data are not presented for the region 280°K to 310°K. Specific heat values at 5°K and 10°K were obtained through computation involving the Debye temperature, θ_0 values extrapolated from the 15-30°K range.

Noer, et al. report an approximate formula for the specific heat of teflon between 1.4°K and 4.2°K which is not in good agreement with the extrapolated value of Furukawa, et al. tabulated below. Their approximate formula is given as

$$C \cong 4 \times 10^{-5} T^3 \text{ j/gm-}^\circ\text{K}$$

| Temp. °K | C _p j/gm°K | H j/gm | Temp. °K | C _p j/gm°K | H j/gm |
|-------------|--------------------------|-----------|-------------|--------------------------|-----------|
| 5 | 0.0024 | 0.003 | 100 | 0.386 | 19.51 |
| 10 | .018 | 0.047 | 120 | 0.457 | 27.9 |
| 15 | .048 | 0.21 | 140 | 0.525 | 37.7 |
| 20 | .076 | 0.52 | 160 | 0.598 | 49.0 |
| 25 | .102 | 0.97 | 180 | 0.677 | 61.7 |
| 30 | .125 | 1.54 | 200 | 0.741 | 75.9 |
| 40 | .165 | 2.99 | 220 | 0.798 | 91.3 |
| 50 | .202 | 4.83 | 240 | 0.853 | 107.8 |
| 60 | .238 | 7.02 | 260 | 0.193 | 125.5 |
| 70 | .274 | 9.59 | 280 | 1.01 | 144.6 |
| 80 | .312 | 12.52 | 310 | 1.02 | 179.3 |
| 90 | .350 | 15.83 | | | |





SPECIFIC HEAT, ENTHALPY of POLYETHYLENE

Source of Data:

Sochava, I. V. and Trapeznikova, O. N., Sov. Phys. Doklady 2,
164-6 (1957).

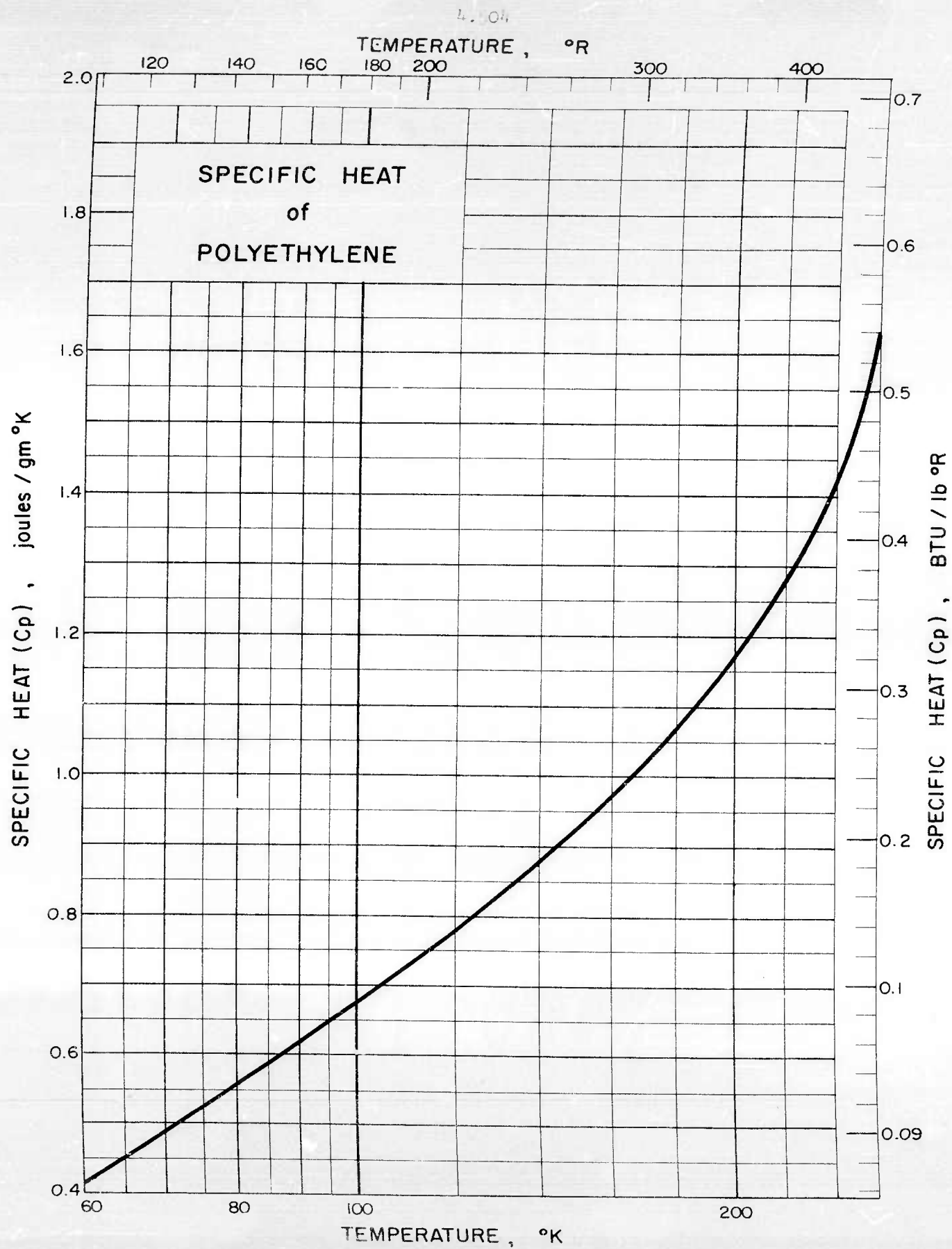
Comments:

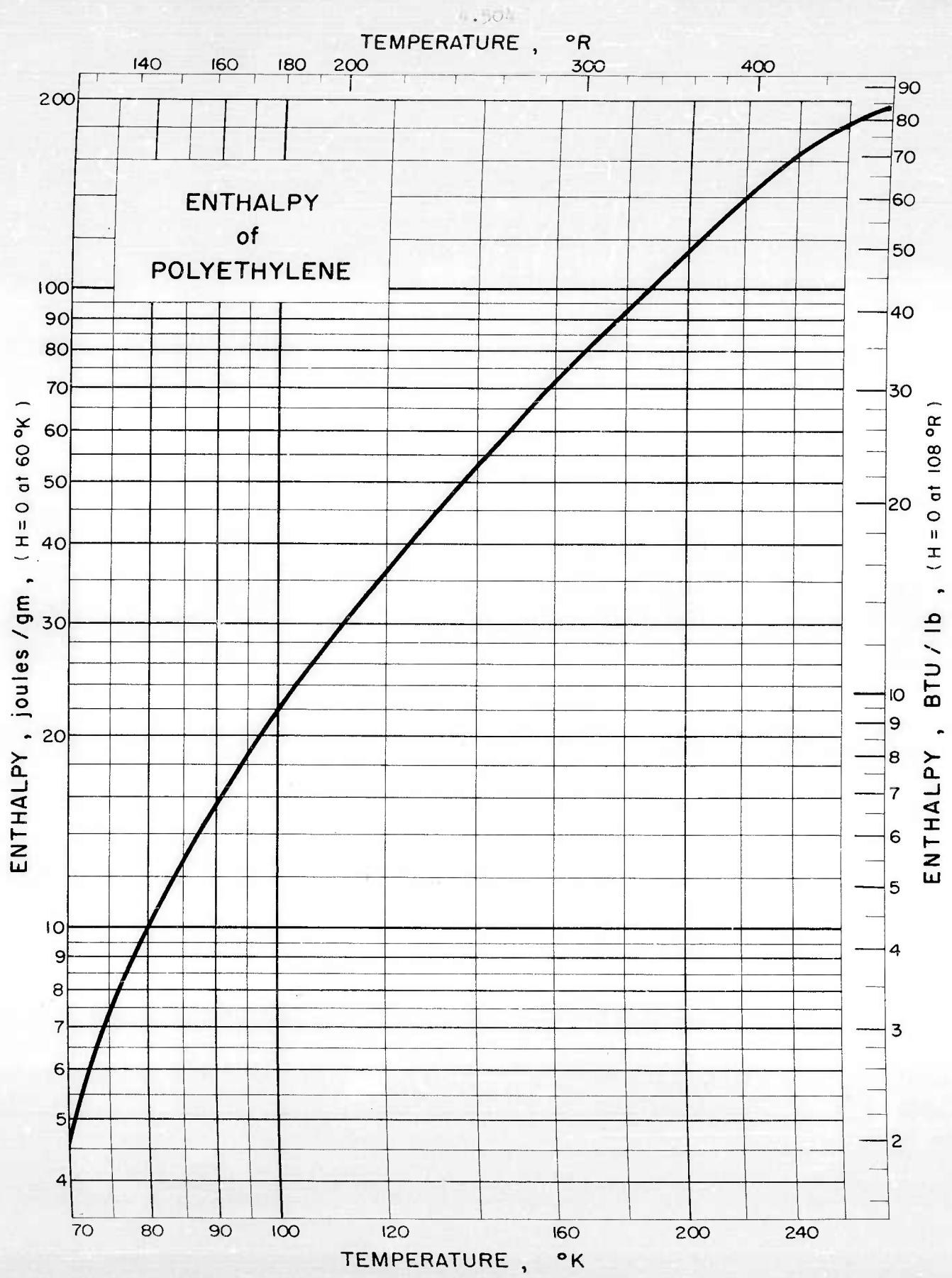
Since no specific heat measurements existed below 60°K, enthalpy values are given referenced to this temperature.

Table of Selected Values

| T °K | C _p j/gm-°K | H-H ₆₀ j/gm |
|---------|---------------------------|---------------------------|
| 60 | 0.418 | |
| 70 | .496 | 4.57 |
| 80 | .561 | 9.84 |
| 90 | .619 | 15.7 |
| 100 | .676 | 22.2 |
| 120 | .778 | 36.8 |
| 140 | .872 | 53.2 |
| 160 | .971 | 71.7 |
| 180 | 1.07 | 92.1 |
| 200 | 1.17 | 114 |
| 220 | 1.28 | 139 |
| 240 | 1.43 | 166 |
| 260 | 1.63 | 196 |

$$H - H_{60} = \int_{60}^T C_p dT$$





SPECIFIC HEAT, ENTHALPY of BAKELITE VARNISH
(Formite Bakelite Varnish V11105)

Source of Data:

Hill, R. W. and Smith, P. L., Phil. Mag. 44, 636-44 (1953)

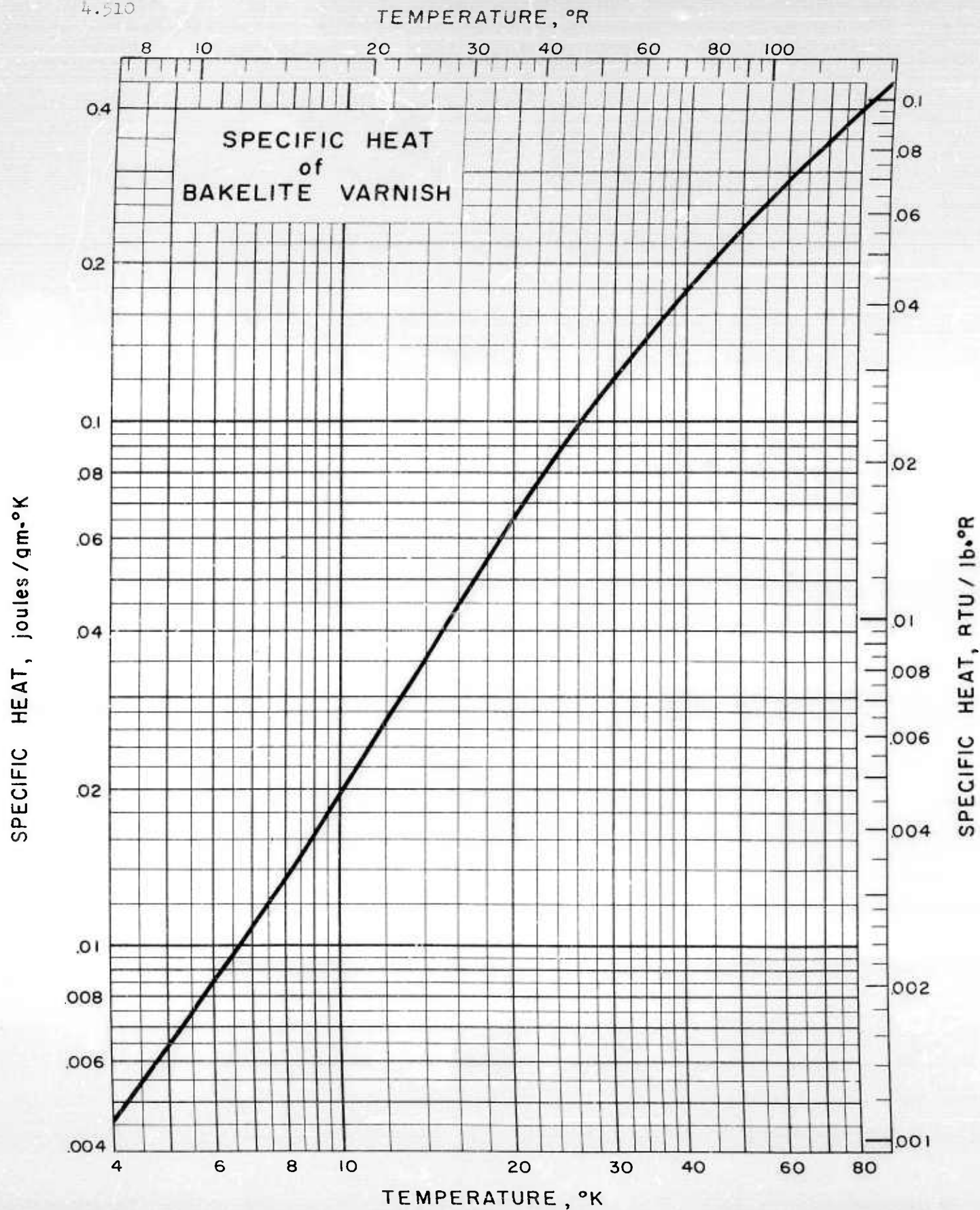
Comments:

Values tabulated below are smoothed values from the original data of Hill and Smith and may vary up to 3% from their work.

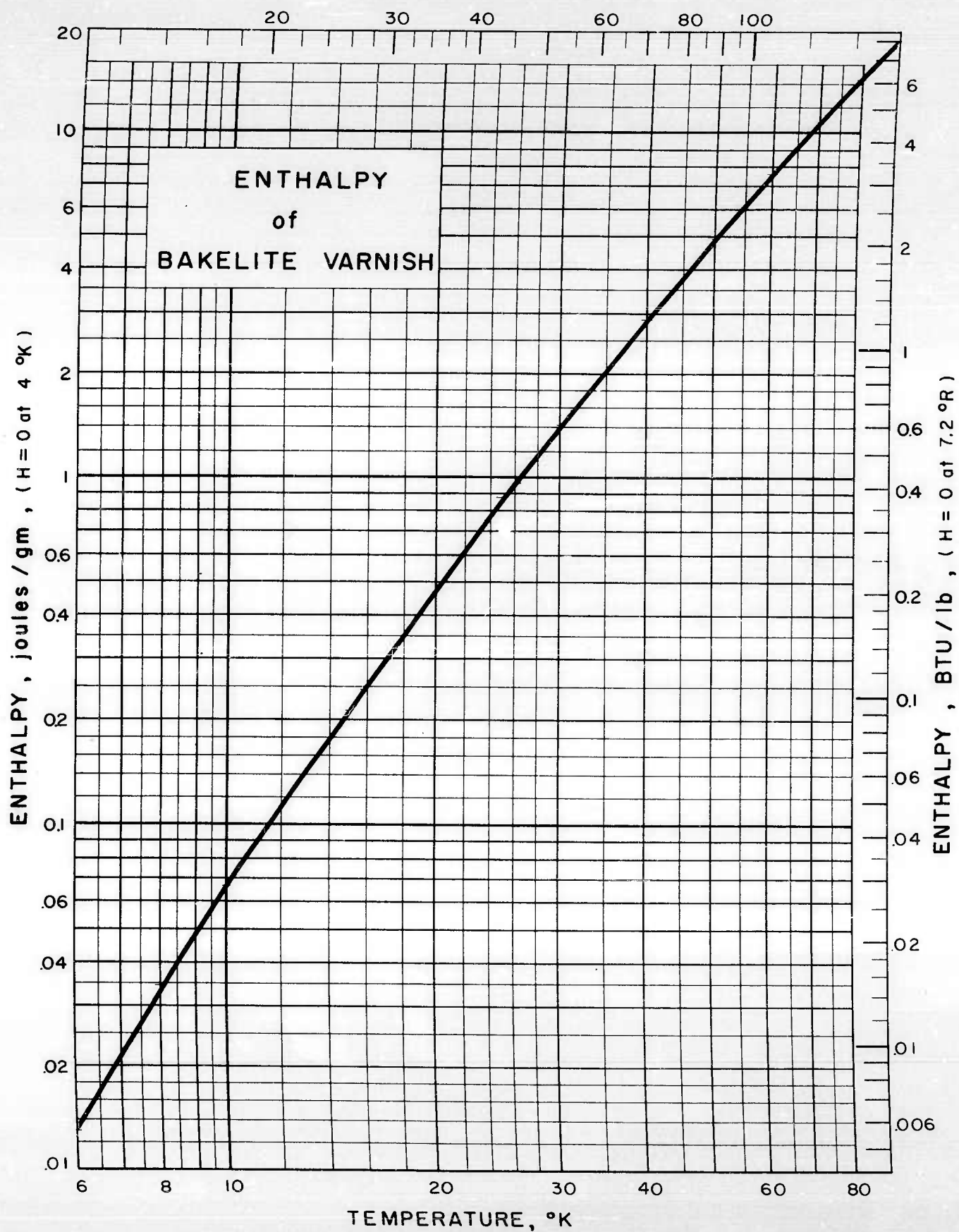
The sample was prepared by baking on an aluminum foil according to the manufacturer's specifications.

Table of Selected Values

| Temp. °K | C_p j/gm-°K | H-H ₄ j/gm |
|-------------|------------------|--------------------------|
| 4 | 0.0046 | |
| 6 | .0086 | 0.0130 |
| 8 | .0134 | .0347 |
| 10 | .0192 | .0672 |
| 15 | .0418 | .216 |
| 20 | .0667 | .487 |
| 25 | .093 | .886 |
| 30 | .121 | 1.42 |
| 40 | .179 | 2.91 |
| 50 | .237 | 4.99 |
| 60 | .293 | 7.64 |
| 70 | .347 | 10.8 |
| 80 | .400 | 14.6 |
| 90 | .449 | 18.8 |



TEMPERATURE, °R



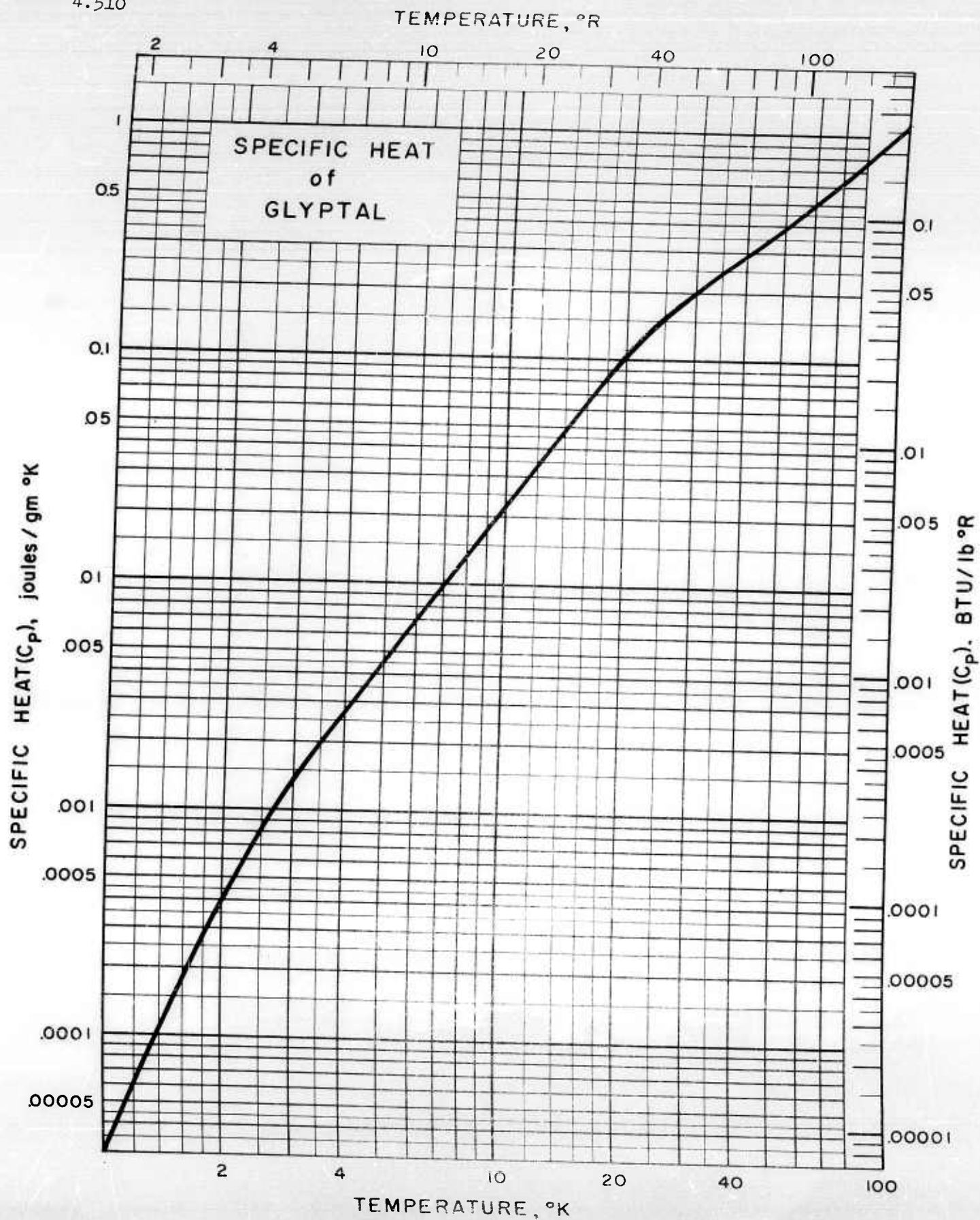
SPECIFIC HEAT, ENTHALPY of GLYPTAL

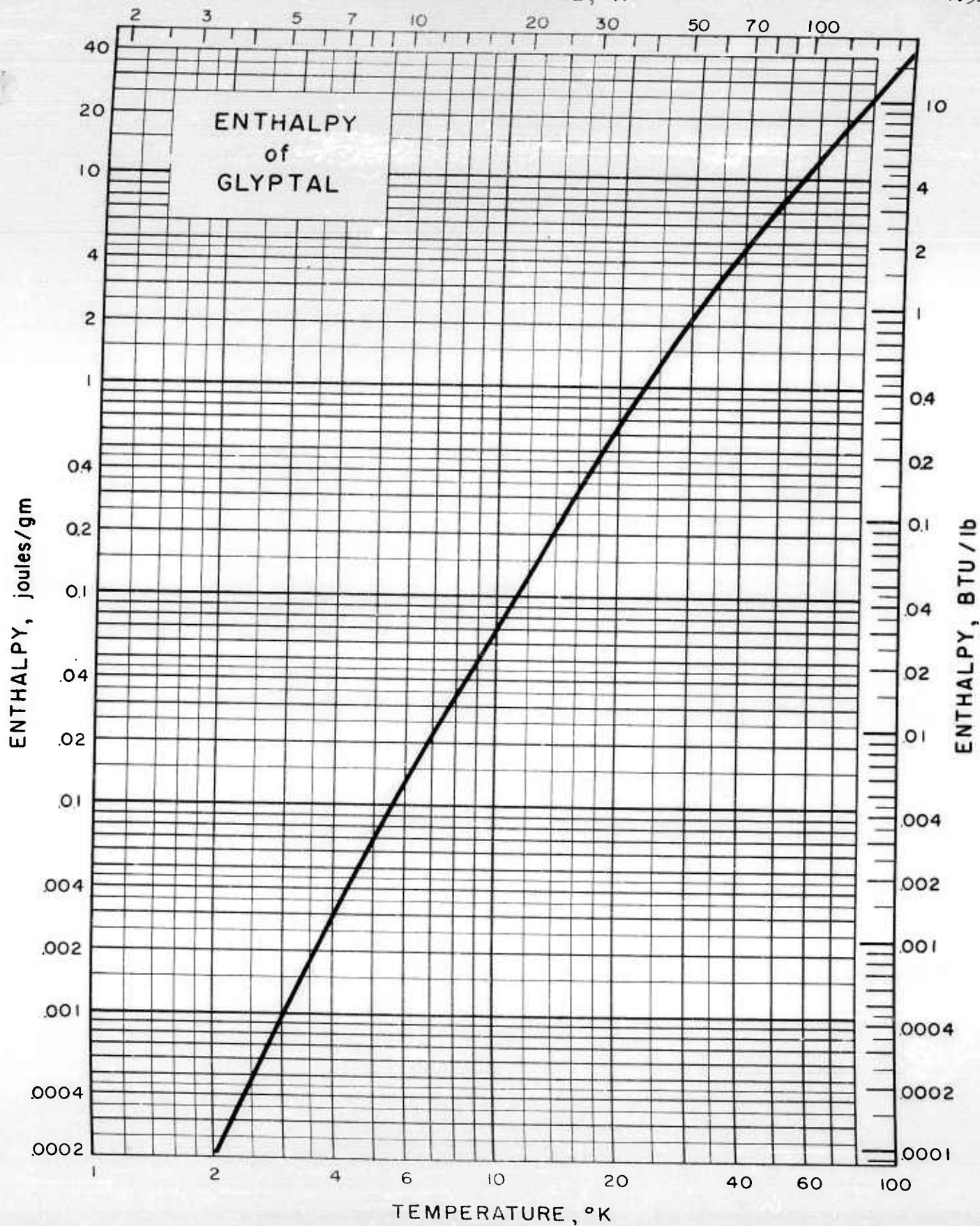
Sources of Data:Keesom, P. H. and Seidel, G., Phys. Rev. 113, 33-9 (1959)Pearlman, N. and Keesom, P. H., Phys. Rev. 88, 398-405 (1952)Comments:

Pearlman and Keesom present the specific heat below 15°K by the approximate empirical relation $C \approx 2.2 \times 10^{-4}T^2$ j/gm-°K. Keesom and Seidel give the expression $C \approx 2.7 \times 10^{-5}T^3$ for representing the specific heat between 1.3° and 4.2°K. The values tabulated below are a graphical average of the two since both results claim no better than 20% accuracy, the former equation being based on measurements at 4°K and 10°K only.

Table of Selected Values

| Temp. °K | C_p j/gm-°K | H j/gm |
|-------------|------------------|-----------|
| 1 | 0.000 03 | 0.000 007 |
| 2 | .000 4 | .000 2 |
| 3 | .001 4 | .001 0 |
| 4 | .002 6 | .003 0 |
| 6 | .007 3 | .013 |
| 8 | .014 | .034 |
| 10 | .022 | .070 |
| 15 | .057 | .26 |
| 20 | .11 | .67 |
| 25 | .16 | 1.3 |
| 30 | .20 | 2.2 |
| 40 | .29 | 4.7 |
| 50 | .38 | 8.1 |
| 60 | .49 | 12 |
| 70 | .62 | 18 |
| 80 | .79 | 25 |
| 90 | .97 | 34 |
| 100 | 1.15 | 44 |





SPECIFIC HEAT, ENTHALPY of POLYVINYL ALCOHOL

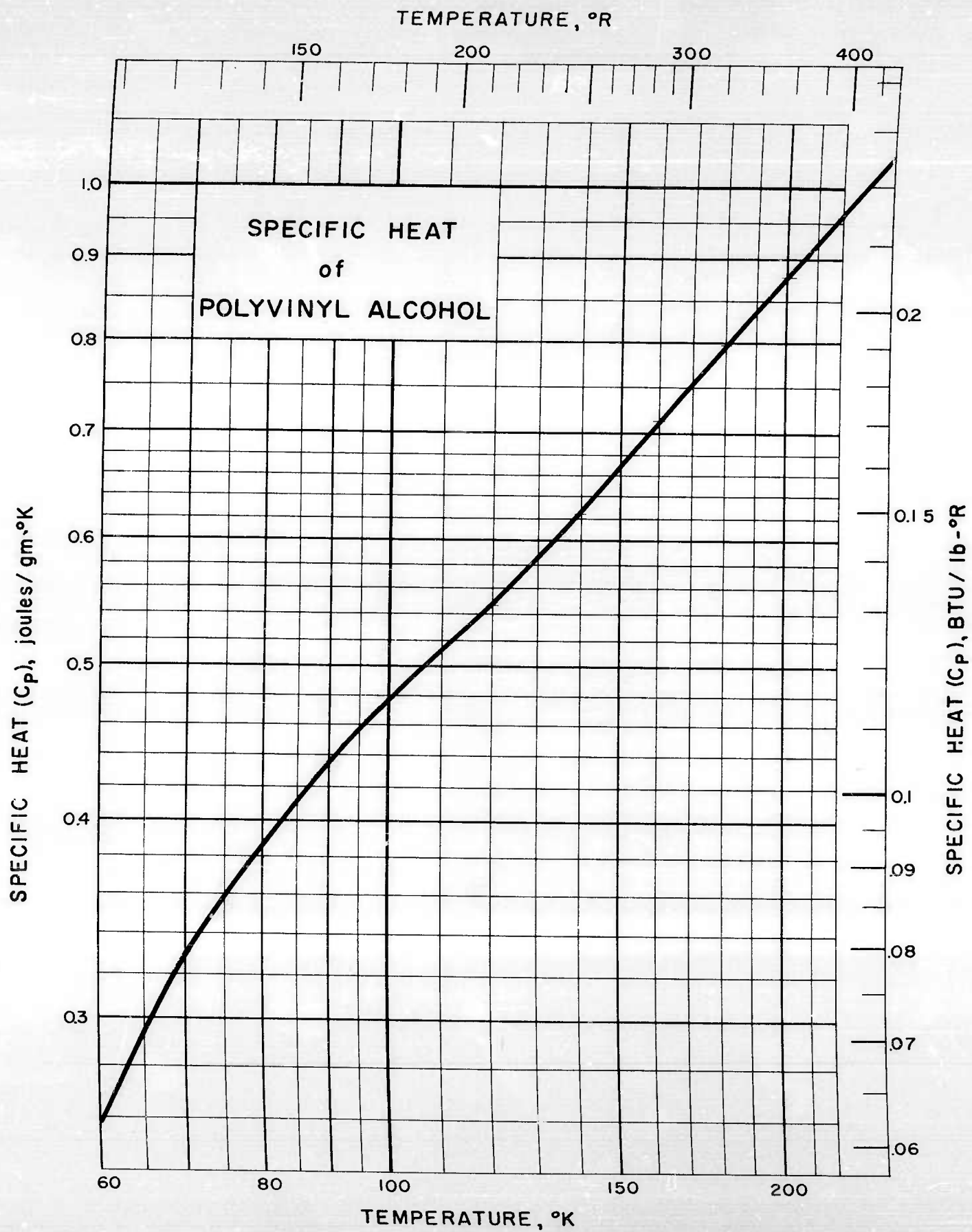
Source of Data:

Sochava, I. V. and Trapeznikova, O. N., Soviet Phys. Doklady
 2, 164-6 (1957)

Table of Selected Values

| Temp. °K | C _p j/gm-°K | H - H ₆₀ j/gm |
|-------------|---------------------------|-----------------------------|
| 60 | 0.257 | |
| 70 | .331 | 2.95 |
| 80 | .388 | 6.55 |
| 90 | .436 | 10.7 |
| 100 | .478 | 15.3 |
| 120 | .546 | 25.5 |
| 140 | .624 | 37.2 |
| 160 | .713 | 50.5 |
| 180 | .798 | 65.7 |
| 200 | .879 | 82.4 |
| 220 | .959 | 101 |
| 240 | 1.05 | 121 |

RJC/JJG/JRC Issued: 12-18-59
 Revised: 5-20-60

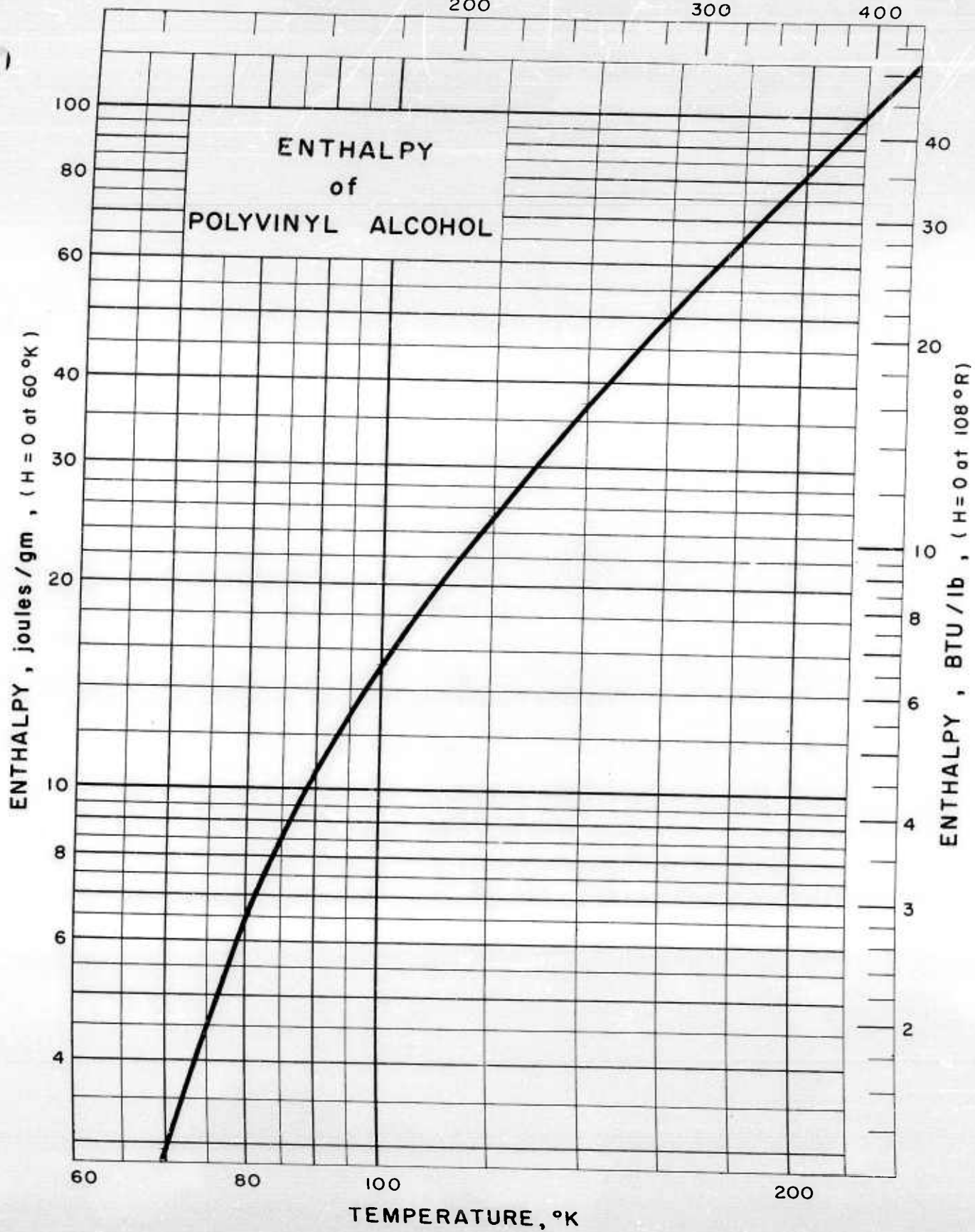


TEMPERATURE, °R

200

300

400



APPENDIXES

TEMPERATURE INTERCONVERSION TABLE

CONVERSION FACTORS FOR UNITS OF LENGTH

CONVERSION FACTORS FOR UNITS OF AREA

CONVERSION FACTORS FOR UNITS OF VOLUME

CONVERSION FACTORS FOR UNITS OF MASS

CONVERSION FACTORS FOR UNITS OF PRESSURE

CONVERSION FACTORS FOR UNITS OF ENERGY

DATA SHEET AUTHOR IDENTIFICATION BY INITIALS

APPENDIX

Temperature Interconversion Table
(0 to 200°K)

| °K | °C | °F | °R | °K | °C | °F | °R |
|-------|---------|---------|--------|--------|---------|---------|--------|
| 0. | -273.16 | -459.69 | 0. | 100. | -173.16 | -279.69 | 180. |
| 3.16 | -270. | -454.00 | 5.69 | 103.16 | -170. | -274.00 | 185.69 |
| 5.38 | -267.78 | -450. | 9.69 | 105.38 | -167.78 | -270. | 189.69 |
| 5.55 | -267.61 | -449.69 | 10. | 105.56 | -167.60 | -269.69 | 190. |
| 10. | -263.16 | -441.69 | 18.00 | 110. | -163.16 | -261.69 | 198.00 |
| 10.94 | -262.22 | -440. | 19.69 | 110.96 | -162.20 | -260. | 199.69 |
| 11.11 | -262.05 | -439.69 | 20. | 111.11 | -162.05 | -259.69 | 200. |
| 13.16 | -260. | -436.00 | 23.69 | 113.16 | -160. | -256.00 | 203.69 |
| 16.49 | -256.67 | -430. | 29.69 | 116.49 | -156.67 | -250. | 209.69 |
| 16.67 | -256.49 | -429.69 | 30. | 116.67 | -156.49 | -249.69 | 210. |
| 20. | -253.16 | -423.69 | 36.00 | 120. | -153.16 | -243.69 | 216.00 |
| 22.05 | -251.11 | -420. | 39.69 | 122.05 | -151.11 | -240. | 219.69 |
| 22.22 | -250.94 | -419.69 | 40. | 122.22 | -150.94 | -239.69 | 220. |
| 23.16 | -250. | -418.00 | 41.69 | 123.16 | -150. | -238.00 | 221.69 |
| 27.60 | -245.56 | -410. | 49.69 | 127.60 | -145.56 | -230. | 229.69 |
| 27.78 | -245.38 | -409.69 | 50. | 127.78 | -145.38 | -229.69 | 230. |
| 30. | -243.16 | -405.69 | 54.00 | 130. | -143.16 | -225.69 | 234.00 |
| 33.16 | -240. | -400. | 59.69 | 133.16 | -140. | -220. | 239.69 |
| 33.33 | -239.83 | -399.69 | 60. | 133.33 | -139.83 | -219.69 | 240. |
| 38.72 | -234.44 | -390. | 69.69 | 138.72 | -134.44 | -210. | 249.69 |
| 38.89 | -234.27 | -389.69 | 70. | 138.89 | -134.27 | -209.69 | 250. |
| 40. | -233.16 | -387.69 | 72.00 | 140. | -133.16 | -207.69 | 252.00 |
| 43.16 | -230. | -382.00 | 77.69 | 143.16 | -130. | -202.00 | 257.69 |
| 44.27 | -228.89 | -380. | 79.69 | 144.27 | -128.89 | -200. | 259.69 |
| 44.44 | -228.72 | -379.69 | 80. | 144.44 | -128.62 | -199.69 | 260. |
| 49.83 | -223.33 | -370. | 89.69 | 149.83 | -123.33 | -190. | 269.69 |
| 50. | -223.16 | -369.69 | 90. | 150. | -123.16 | -189.69 | 270. |
| 53.16 | -220. | -364.00 | 95.69 | 153.16 | -120. | -184.00 | 275.69 |
| 55.38 | -217.78 | -360. | 99.69 | 155.38 | -117.78 | -180. | 279.69 |
| 55.56 | -217.60 | -359.69 | 100. | 155.56 | -117.60 | -179.69 | 280. |
| 60. | -213.16 | -351.69 | 108.00 | 160. | -113.16 | -171.69 | 288.00 |
| 60.94 | -212.22 | -350. | 109.69 | 160.94 | -112.22 | -170. | 289.69 |
| 61.11 | -212.05 | -349.69 | 110. | 161.11 | -112.05 | -169.69 | 290. |
| 63.16 | -210. | -346.00 | 113.69 | 163.16 | -110. | -166.00 | 293.69 |
| 66.49 | -206.67 | -340. | 119.69 | 166.49 | -106.67 | -160. | 299.69 |
| 66.67 | -206.49 | -339.69 | 120. | 166.67 | -106.49 | -159.69 | 300. |
| 70. | -203.16 | -333.69 | 126.00 | 170. | -103.16 | -153.69 | 306.00 |
| 72.05 | -201.11 | -330. | 129.69 | 172.05 | -101.11 | -150. | 309.69 |
| 72.22 | -200.94 | -329.69 | 130. | 172.22 | -100.94 | -149.69 | 310. |
| 73.16 | -200. | -328.00 | 131.69 | 173.16 | -100. | -148.00 | 311.69 |
| 77.60 | -195.56 | -320. | 139.69 | 177.60 | -95.56 | -140. | 319.69 |
| 77.78 | -195.38 | -319.69 | 140. | 177.78 | -95.38 | -139.69 | 320. |
| 80. | -193.16 | -315.69 | 144.00 | 180. | -93.16 | -135.69 | 324.00 |
| 83.16 | -190. | -310. | 149.69 | 183.16 | -90. | -130. | 329.69 |
| 83.33 | -189.83 | -309.69 | 150. | 183.33 | -89.83 | -129.69 | 330. |
| 88.72 | -184.44 | -300. | 159.69 | 188.72 | -84.44 | -120. | 339.69 |
| 88.89 | -184.27 | -299.69 | 160. | 188.89 | -84.27 | -119.69 | 340. |
| 90. | -183.16 | -297.69 | 162.00 | 190. | -83.16 | -117.69 | 342.00 |
| 93.16 | -180. | -292.00 | 167.69 | 193.16 | -80. | -112.00 | 347.69 |
| 94.27 | -178.89 | -290. | 169.69 | 194.27 | -78.89 | -110. | 349.69 |
| 94.44 | -178.72 | -289.69 | 170. | 194.44 | -78.72 | -109.69 | 350. |
| 99.83 | -173.33 | -280. | 179.69 | 199.83 | -73.33 | -100. | 359.69 |
| 100. | -173.16 | -279.69 | 180. | 200. | -73.16 | -99.69 | 360. |

| °K | °R |
|----|-------|
| °C | °F |
| 1 | 1.8 |
| 2 | 3.6 |
| 3 | 5.4 |
| 4 | 7.2 |
| 5 | 9.0 |
| 6 | 10.8 |
| 7 | 12.6 |
| 8 | 14.4 |
| 9 | 16.2 |
| 10 | 18.0 |
| °R | °K |
| °F | °C |
| 1 | 0.56 |
| 2 | 1.11 |
| 3 | 1.67 |
| 4 | 2.22 |
| 5 | 2.78 |
| 6 | 3.33 |
| 7 | 3.89 |
| 8 | 4.44 |
| 9 | 5.00 |
| 10 | 5.56 |
| 11 | 6.11 |
| 12 | 6.67 |
| 13 | 7.22 |
| 14 | 7.78 |
| 15 | 8.33 |
| 16 | 8.89 |
| 17 | 9.44 |
| 18 | 10.00 |

APPENDIX

Temperature Interconversion Table
(200 to 400°K)

| °K | °C | °F | °R | °K | °C | °F | °R |
|--------|--------|--------|--------|--------|--------|--------|--------|
| 200. | -73.16 | -99.69 | 360. | 300. | 26.84 | 80.31 | 540. |
| 203.16 | -70. | -94.00 | 365.69 | 303.16 | 30. | 86.00 | 545.69 |
| 205.38 | -67.78 | -90. | 369.69 | 305.38 | 32.22 | 90. | 549.69 |
| 205.56 | -67.60 | -89.99 | 370. | 305.56 | 32.40 | 90.31 | 550. |
| 210. | -63.16 | -81.69 | 378.00 | 310. | 36.84 | 98.31 | 558.00 |
| 210.94 | -62.22 | -80. | 379.69 | 310.94 | 37.78 | 100. | 559.69 |
| 211.11 | -62.05 | -79.69 | 380. | 311.11 | 37.95 | 100.31 | 560. |
| 213.16 | -60. | -76.00 | 383.69 | 313.16 | 40. | 104.00 | 563.69 |
| 216.41 | -56.67 | -70. | 389.69 | 316.41 | 43.33 | 110. | 569.69 |
| 216.67 | -56.49 | -69.69 | 390. | 316.67 | 43.51 | 110.31 | 570. |
| 220. | -53.16 | -63.69 | 396.00 | 320. | 46.84 | 116.31 | 576.00 |
| 222.05 | -51.11 | -60. | 399.69 | 322.05 | 48.89 | 120. | 579.69 |
| 222.22 | -50.94 | -59.69 | 400. | 322.22 | 49.06 | 120.31 | 580. |
| 223.16 | -50. | -58.00 | 401.69 | 323.16 | 50. | 122.00 | 581.69 |
| 227.60 | -45.56 | -50. | 409.69 | 327.60 | 54.44 | 130. | 589.69 |
| 227.78 | -45.38 | -49.69 | 410. | 327.78 | 54.62 | 130.31 | 590. |
| 230. | -43.16 | -45.69 | 414.00 | 330. | 56.84 | 134.31 | 594.00 |
| 233.16 | -40. | -40. | 419.69 | 333.16 | 60. | 140. | 599.69 |
| 233.33 | -39.83 | -39.69 | 420. | 333.33 | 60.17 | 140.31 | 600. |
| 238.72 | -34.44 | -30. | 429.69 | 338.72 | 65.56 | 150. | 609.69 |
| 238.89 | -34.27 | -29.69 | 430. | 338.89 | 65.73 | 150.31 | 610. |
| 240. | -33.16 | -27.69 | 432.00 | 340. | 66.84 | 152.31 | 612.00 |
| 243.16 | -30. | -22.00 | 437.69 | 343.16 | 70. | 158.00 | 617.69 |
| 244.27 | -28.89 | -20. | 439.69 | 344.27 | 71.11 | 160. | 619.69 |
| 244.44 | -28.72 | -19.69 | 440. | 344.44 | 71.28 | 160.31 | 620. |
| 249.83 | -23.33 | -10. | 449.69 | 349.83 | 76.67 | 170. | 629.69 |
| 250. | -23.16 | -9.69 | 450. | 350. | 76.84 | 170.31 | 630. |
| 253.16 | -20. | -4.00 | 455.69 | 353.16 | 80. | 176.00 | 635.69 |
| 255.38 | -17.78 | 0. | 459.69 | 355.38 | 82.22 | 180. | 639.69 |
| 255.56 | -17.60 | +31 | 460. | 355.56 | 82.40 | 180.31 | 640. |
| 260. | -13.16 | +8.31 | 468.00 | 360. | 86.84 | 188.31 | 648.00 |
| 260.94 | -12.22 | 10. | 469.69 | 360.94 | 87.78 | 190. | 649.69 |
| 261.11 | -12.05 | 10.31 | 470. | 361.11 | 87.95 | 190.31 | 650. |
| 263.16 | -10. | 14.00 | 473.69 | 363.16 | 90. | 194.00 | 653.69 |
| 266.49 | -6.67 | 20. | 479.69 | 366.49 | 93.33 | 200. | 659.69 |
| 266.67 | -6.49 | 20.31 | 480. | 366.67 | 93.51 | 200.31 | 660. |
| 270. | -3.16 | 26.31 | 486.00 | 370. | 96.84 | 206.31 | 666.00 |
| 272.05 | -1.11 | 30. | 489.69 | 372.05 | 98.89 | 210. | 669.69 |
| 272.22 | -.94 | 30.31 | 490. | 372.22 | 99.06 | 210.31 | 670. |
| 273.16 | 0. | 32.00 | 491.69 | 373.16 | 100. | 212.00 | 671.69 |
| 277.60 | +4.44 | 40. | 499.69 | 377.60 | 104.44 | 220. | 679.69 |
| 277.78 | 4.62 | 40.31 | 500. | 377.78 | 104.62 | 220.31 | 680. |
| 280. | 6.84 | 44.31 | 504.00 | 380. | 106.84 | 224.31 | 684.00 |
| 283.16 | 10. | 50. | 509.69 | 383.16 | 110. | 230. | 689.69 |
| 283.33 | 10.17 | 50.31 | 510. | 383.33 | 110.17 | 230.31 | 690. |
| 288.72 | 15.56 | 60. | 519.69 | 388.72 | 115.56 | 240. | 699.69 |
| 288.89 | 15.73 | 60.31 | 520. | 388.89 | 115.73 | 240.31 | 700. |
| 290. | 16.84 | 62.31 | 522.00 | 390. | 116.84 | 242.31 | 702.00 |
| 293.16 | 20. | 68.00 | 527.69 | 393.16 | 120. | 248.00 | 707.69 |
| 294.27 | 21.11 | 70. | 529.69 | 394.27 | 121.11 | 250. | 709.69 |
| 294.44 | 21.28 | 70.31 | 530. | 394.44 | 121.28 | 250.31 | 710. |
| 299.83 | 26.67 | 80. | 539.69 | 399.83 | 126.67 | 260. | 719.69 |
| 300. | 26.84 | 80.31 | 540. | 400. | 126.84 | 260.31 | 720. |

| °K | °R |
|----|-------|
| °C | °F |
| 1 | 1.8 |
| 2 | 3.6 |
| 3 | 5.4 |
| 4 | 7.2 |
| 5 | 9.0 |
| 6 | 10.8 |
| 7 | 12.6 |
| 8 | 14.4 |
| 9 | 16.2 |
| 10 | 18.0 |
| °R | °K |
| °F | °C |
| 1 | 0.56 |
| 2 | 1.11 |
| 3 | 1.67 |
| 4 | 2.22 |
| 5 | 2.78 |
| 6 | 3.33 |
| 7 | 3.89 |
| 8 | 4.44 |
| 9 | 5.00 |
| 10 | 5.56 |
| 11 | 6.11 |
| 12 | 6.67 |
| 13 | 7.22 |
| 14 | 7.78 |
| 15 | 8.33 |
| 16 | 8.89 |
| 17 | 9.44 |
| 18 | 10.00 |

APPENDIX

Conversion Factors
for
Units of Length and Area

CONVERSION FACTORS FOR UNITS OF LENGTH

| Multiply by appropriate entry to obtain → ↓ | cm | mm | μ | $m\mu$ | Å |
|---|-------------------|-----------|-----------|-----------|------------|
| | 1 Centimeter (cm) | 1 | 10 | 10^4 | 10^7 |
| 1 Millimeter (mm) | 10^{-1} | 1 | 10^3 | 10^6 | 10^7 |
| 1 Micron (μ) | 10^{-4} | 10^{-3} | 1 | 10^3 | 10^4 |
| 1 Millimicron ($m\mu$) | 10^{-7} | 10^{-6} | 10^{-3} | 1 | 10 |
| 1 Angstrom Unit (Å) | 10^{-8} | 10^{-7} | 10^{-4} | 10^{-1} | 1 |

CONVERSION FACTORS FOR UNITS OF LENGTH - Cont.

| Multiply by appropriate entry to obtain → ↓ | cm | m | in | ft | yd |
|---|-----------|-------------|-------|-------------|-------------|
| | 1 cm | 1 | 0.01 | 0.3937 | 0.032808333 |
| 1 m | 100. | 1 | 39.37 | 3.2808333 | 1.0936111 |
| 1 in | 2.5400051 | 0.025400051 | 1 | 0.083333333 | 0.027777778 |
| 1 ft | 30.480061 | 0.30480061 | 12. | 1 | 0.33333333 |
| 1 yd | 91.440183 | 0.91440183 | 36. | 3. | 1 |

CONVERSION FACTORS FOR UNITS OF AREA

| Multiply by appropriate entry to obtain → ↓ | cm^2 | m^2 | sq in | sq ft | sq yd |
|---|-----------------|----------------------------|-----------|----------------------------|----------------------------|
| | 1 cm^2 | 1 | 10^{-4} | 0.15499969 | 1.0763867×10^{-3} |
| 1 m^2 | 10^4 | 1 | 1549.9969 | 10.763867 | 1.1959853 |
| 1 sq in | 6.4516258 | 6.4516258×10^{-4} | 1 | 6.9444444×10^{-3} | 7.7160494×10^{-4} |
| 1 sq ft | 929.03412 | 0.092903412 | 144. | 1 | 0.11111111 |
| 1 sq yd | 8361.3070 | 0.83613070 | 1296. | 9. | 1 |

APPENDIX

Conversion Factors

CONVERSION FACTORS FOR UNITS OF VOLUME

| Multiply by appropriate entry to obtain ↓ 1 cm ³ | ml | liter | gal |
|--|-------------------|-----------------------------|------------------------------|
| | 1 cm ³ | 0.9999720 | 0.9999720 x 10 ⁻³ |
| 1 cu in | 16.38670 | 1.638670 x 10 ⁻² | 4.3290043 x 10 ⁻³ |
| 1 cu ft | 28316.22 | 28.31622 | 7.4805195 |
| 1 ml | 1 | 0.001 | 2.641779 x 10 ⁻⁴ |
| 1 liter | 1000. | 1 | 0.2641779 |
| 1 gal | 3785.329 | 3.785329 | 1 |

CONVERSION FACTORS FOR UNITS OF VOLUME - Cont.

| Multiply by appropriate entry to obtain ↓ 1 cm ³ | cm ³ | cu in | cu ft |
|--|-------------------|------------|------------------------------|
| | 1 cm ³ | 1 | 0.061023378 |
| 1 cu in | 16.387162 | 1 | 5.7870370 x 10 ⁻⁴ |
| 1 cu ft | 28317.017 | 1728. | 1 |
| 1 ml | 1.000028 | 0.06102509 | 3.531544 x 10 ⁻⁵ |
| 1 liter | 1000.028 | 61.02509 | 0.03531544 |
| 1 gal | 3785.4345 | 231. | 0.13368056 |

APPENDIX

Conversion Factors

CONVERSION FACTORS FOR UNITS OF MASS

| Multiply by appropriate entry to obtain → | g | kg | lb | metric ton | ton |
|--|-----------|------------|----------------------------|----------------------------|----------------------------|
| 1 g | 1 | 10^{-3} | 2.2046223×10^{-3} | 10^{-6} | 1.1023112×10^{-6} |
| 1 kg | 10^3 | 1 | 2.2046223 | 10^{-3} | 1.1023112×10^{-3} |
| 1 lb | 453.59243 | 0.45359243 | 1 | 4.5359243×10^{-4} | 0.0005 |
| 1 metric ton | 10^6 | 10^3 | 2204.6223 | 1 | 1.1023112 |
| 1 ton | 907184.86 | 907.18486 | 2000. | 0.90718486 | 1 |

APPENDIX

Conversion Factors
for
Units of Pressure

CONVERSION FACTORS FOR UNITS OF PRESSURE

| Multiply by appropriate entry to obtain → 1 dyne/cm ² | dyne/cm ² | bar | atm | kg(wt)/cm ² | mm Hg | in Hg | lb(wt)/sq in |
|---|----------------------|---------------------------------|---------------------------------|---------------------------------|---------------------------------|--------------------------------|--------------------------------|
| | | 1 | 10 ⁻⁶ | 0.9869233 x 10 ⁻⁶ | 1.0197162 x 10 ⁻⁶ | 7.500617 x 10 ⁻⁴ | 2.952993 x 10 ⁻⁵ |
| 1 bar | 10 ⁶ | 1 | 0.9869233 | 1.0197162 | 750.0617 | 29.52993 | 14.503830 |
| 1 atm | 1013250. | 1.013250 | 1 | 1.0332275 | 760. | 29.92120 | 14.696006 |
| 1 kg(wt)/cm ² | 980665. | 0.980665 | 0.9678411 | 1 | 735.5592 | 28.95897 | 14.223398 |
| 1 mm Hg | 1333.2237 | 1.3332237 x 10 ⁻³ | 1.3157895 x 10 ⁻³ | 1.3595098 x 10 ⁻³ | 1 | 0.03937 | 0.019336850 |
| 1 in Hg | 33863.95 | 0.03386395 | 0.03342112 | 0.03453162 | 25.40005 | 1 | 0.4911570 |
| 1 lb(wt)/sq in | 68947.31 | 0.06894731 | 0.06804570 | 0.07030669 | 51.71473 | 2.036009 | 1 |

APPENDIX

Conversion Factors
for
Units of Energy

CONVERSION FACTORS FOR UNITS OF ENERGY

| Multiply by appropriate entry to obtain → | g mass (energy equiv) | abs. joule | int. joule | cal | I. T. cal | BTU | int. kilowatt -hr |
|---|------------------------------|----------------------------|----------------------------|----------------------------|----------------------------|-----------------------------|-----------------------------|
| 1 g mass (energy equiv) | 1 | 8.98656 x 10 ¹³ | 8.98508 x 10 ¹³ | 2.14784 x 10 ¹³ | 2.14644 x 10 ¹³ | 8.51775 x 10 ¹⁰ | 2.49586 x 10 ⁷ |
| 1 abs. joule | 1.112772 x 10 ⁻¹⁴ | 1 | 0.999835 | 0.239006 | 0.238849 | 0.947831 x 10 ⁻³ | 2.77732 x 10 ⁻⁷ |
| 1 int. joule | 1.112956 x 10 ⁻¹⁴ | 1.000165 | 1 | 0.239045 | 0.238889 | 0.947988 x 10 ⁻³ | 2.777778 x 10 ⁻⁷ |
| 1 cal | 4.65584 x 10 ⁻¹⁴ | 4.1840 | 4.1833 | 1 | 0.999346 | 3.96573 x 10 ⁻³ | 1.162030 x 10 ⁻⁶ |
| 1 I. T. cal | 4.65888 x 10 ⁻¹⁴ | 4.18674 | 4.18605 | 1.000654 | 1 | 3.96832 x 10 ⁻³ | 1.162791 x 10 ⁻⁶ |
| 1 BTU | 1.174019 x 10 ⁻¹¹ | 1055.040 | 1054.866 | 252.161 | 251.996 | 1 | 2.93018 x 10 ⁻⁴ |
| 1 int. kilowatt-hr | 4.00664 x 10 ⁻⁸ | 3,600,594. | 3,600,000. | 860,563. | 860,000. | 3412.76 | 1 |
| 1 horsepower-hr | 2.98727 x 10 ⁻⁸ | 2,684,525. | 2,684,082. | 641,617. | 641,197. | 2544.48 | 0.745578 |
| 1 ft-lb(wt) | 1.508720 x 10 ⁻¹⁴ | 1.355821 | 1.355597 | 0.324049 | 0.323837 | 1.285089 x 10 ⁻³ | 3.76555 x 10 ⁻⁷ |
| 1 cu ft - lb(wt)/sq in | 2.17256 x 10 ⁻¹² | 195.2382 | 195.2060 | 46.6630 | 46.6325 | 0.1850529 | 5.42239 x 10 ⁻⁵ |
| 1 liter-atm | 1.127548 x 10 ⁻¹² | 101.3278 | 101.3111 | 24.2179 | 24.2021 | 0.0960417 | 2.81420 x 10 ⁻⁵ |

APPENDIX

Conversion Factors

CONVERSION FACTORS FOR UNITS OF ENERGY - Cont.

| Multiply by appropriate entry to obtain → | ft-lb(wt) | cu ft- lb(wt)/sq in. | liter-atm | horsepower -hr |
|--|-----------------------------|-----------------------------|------------------------------|------------------------------|
| 1 g mass(energy equiv) | 6.62814 $\times 10^{13}$ | 4.60287 $\times 10^{11}$ | 8.86880 $\times 10^{11}$ | 3.34754 $\times 10^7$ |
| 1 abs. joule | 0.737561 | 5.12195 $\times 10^{-3}$ | 9.86896 $\times 10^{-3}$ | 3.72505 $\times 10^{-7}$ |
| 1 int. joule | 0.737682 | 5.12279 $\times 10^{-3}$ | 9.87058 $\times 10^{-3}$ | 3.72567 $\times 10^{-7}$ |
| 1 cal | 3.08595 | 2.14302 $\times 10^{-2}$ | 4.12917 $\times 10^{-2}$ | 1.558562 $\times 10^{-6}$ |
| 1 I. T. cal | 3.08797 | 2.14443 $\times 10^{-2}$ | 4.13187 $\times 10^{-2}$ | 1.559562 $\times 10^{-6}$ |
| 1 BTU | 778.156 | 5.40386 | 10.41215 | 3.93008 $\times 10^{-4}$ |
| 1 int. kilowatt-hr | 2,655,656. | 18442.06 | 35534.1 | 1.341241 |
| 1 horsepower-hr | 1,980,000. | 13750. | 26493.5 | 1 |
| 1 ft-lb(wt) | 1 | 6.94444 $\times 10^{-3}$ | 1.338054 $\times 10^{-2}$ | 5.05051 $\times 10^{-7}$ |
| 1 cu ft - lb(wt)/sq in | 144. | 1 | 1.926797 | 7.27273 $\times 10^{-5}$ |
| 1 liter-atm | 74.7354 | 5.18996 | 1 | 3.77452 $\times 10^{-5}$ |

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