

UNCLASSIFIED

AD 274 107

*Reproduced
by the*

**ARMED SERVICES TECHNICAL INFORMATION AGENCY
ARLINGTON HALL STATION
ARLINGTON 12, VIRGINIA**



UNCLASSIFIED

NOTICE: When government or other drawings, specifications or other data are used for any purpose other than in connection with a definitely related government procurement operation, the U. S. Government thereby incurs no responsibility, nor any obligation whatsoever; and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use or sell any patented invention that may in any way be related thereto.

274 107

AFOSR 2304

DESLIP IN ALUMINUM
SINGLE CRYSTAL SPECIMENS
(Terminal Report)

by

Robert B. Pond

Eleanor Harrison

The Johns Hopkins University

January 1962

SOLID STATE SCIENCES DIVISION
AIR FORCE OFFICE OF SCIENTIFIC RESEARCH
ARDC

Washington 25, D. C.

Contract No. AF 49 (638)-509

Qualified requestors may obtain copies of this report from the ASTIA Document Service Center, Arlington Hall Station, Arlington 12, Va. Department of Defense contractors must be established for ASTIA services, or have their 'need-to-know' certified by the cognizant military agency of their project or contract.

ABSTRACT

By the technique of interferometric cinemicrography which was developed on this contract deslip in aluminum single crystals was observed as a result of reversing the stress. An explanation of the phenomenon is presented.

The technique is also used to evaluate the effects of temperature over the range -150°F to $+225^{\circ}\text{F}$, on the velocity of slip.

Unslip of a band during continuing deformation was observed and an explanation of the phenomenon is presented.

INTRODUCTION

Investigations of the plastic deformation of metals can be divided into three general areas by considering the physical scale the investigations incorporate. These three groups are a) the submicroscopic, b) the microscopic, and c) the macroscopic. Investigations of the submicroscopic type are concerned with the basic structure, dislocations and other imperfections and their behavior under plastic deformation. Such investigations have been principally concerned with static tests although in recent years dynamic observations have been accomplished. Investigations of the macroscopic type are concerned with geometric shape of the specimen, strain rate effects, stress-strain relationships, strain wave propagation, and so forth. Such investigations comprise the bulk of the efforts so far expended in the general field and have involved both static and dynamic observations. Investigations of the microscopic type are concerned with crystal class and orientations, grain boundary effects, slip bands, deformation bands, twins and so forth. Such investigations, although numerous, have been principally carried out by static observations. Dynamic observations of the microscopic behavior of a metal being plastically deformed have been reported by Chen and Pond (1), Becker and Haasen (2), Haasen and Siems (3) and Pond and Harrison (4). Because of the scarcity of such dynamic observations an array of data in excess of the amount necessary to present this report is included so the

scientific community can have access to it.

The technique of interferometric cinemicrography (5) which was developed under this contract was used in the documentation hereafter presented.

SPECIMEN PREPARATION

All specimens used in these investigations were cast aluminum single crystals $1/8$ inch x $1/8$ inch square in cross section by $1-3/8$ inches long in gauge length and were produced from research purity (99.99% pure) aluminum by a modified Bridgman process. This process which was described by Chen and Pond (1) was used to produce 108 crystals simultaneously from the same melt. By gating from the foot of each crystal to a common seed large numbers of crystals having the same orientation and purity were produced.

Each crystal was ground flat, etched, thermally homogenized and, finally, electrolytically polished in methyl alcohol and nitric acid (2/1). The crystallographic orientations were determined by the Laue X-ray back-reflection method. From this data the side of the crystal was selected on which the maximum surface upheaval would result from primary slip. This side of the crystal was used for microscopic observation. The orientations relative to the specimen axis or stress axis are presented in Fig. 1-A for the specimens used in the deslip experiments and in Fig. 1-B for the temperature experiments.

METHOD OF TESTING AND DEVELOPING DATA

After each crystal was prepared and immediately before it was tested the interference mirror was attached to the selected side. The crystal was then placed in the micro tensile machine on the microscope as previously described (1) and in the case of the deslip experiments it was first compressed and then extended, the interval of time between the reversal being controlled. In all other cases the specimen was simply extended. During deformation the motion picture record was made of the changes occurring in the interference pattern. The camera speed was 12 frames per second. The minimum vertical resolution by the interference pattern was $100 \text{ \AA}$ and the minimum lateral resolution of the microscope was .0022 mm.

High temperature runs were accomplished by encapsulating the specimen on the three sides not used for observation in a small Nichrome heater. Low temperature runs were accomplished by packing crushed dry ice around the specimen and grips. The interference mirror and the objective lens were kept free by means of an aluminum foil shield which was wrapped around the objective tube and the specimen at the point of observation. In both cases the temperature was determined by means of a thermocouple situated on the specimen.

Following each successful run the film was developed and that portion of the film was printed which depicted the phenomenon from the beginning of slip on the first slip band until sufficient

slip bands had appeared so that the field became confused. These prints were analyzed by measuring the average "elevation factor" for each line at many different times (or at many different strain intervals). The "elevation factor" is defined as the ratio of the extent of displacement of an interference fringe to the distance between fringes and is that factor which, when multiplied by $1/\cos \theta$ (where θ is the angle between the normal to the observation plane and the slip direction) and multiplied by the half wave length of the radiation used, equals to the resolved shear or extent of slip in the slip direction. An illustration of a resulting plot is given in Figs. 2, 3, 4. From such a plot the velocity of slip can be determined for each slip band at any time or extent of strain desired.

PRESENTATION OF RESULTS

This investigation was conducted in two parts. The first part was concerned with endeavors to deslip aluminum. The second part was concerned with temperature effects on the velocity of slip. In order to prevent confusion the results will be presented and discussed independently.

1. Deslip

A summary tabulation of the data developed during these investigations is not revealing since it is awkward to insert in such a tabulation the juxtaposition of the slip lines. The data is therefore presented in two forms. Figs. 6, 7, 8 and 9 illustrate

a) the relative spatial positions of the array of slip bands by ordinate intercepts, b) the time during which slip occurred on each band by the abscissa interval of the cross-hatched area, c) the velocity of slip by the height of the cross-hatched area, d) the extent of slip by the area of the cross-hatched area, e) the time of compressive load cessation by noting as Reversal, f) the interval of time after compression before tensile extension.

It can be noted in Fig. 6 that after maintaining a compressive stress on the specimen 9-1-5 for 5.58 seconds the load was removed and after a wait of 38.2 seconds a tensile stress was applied which resulted in deslipping on the compressive bands C_1 , C_2 , C_3 , and C_4 .

Deslip was not observed on every slip band nor was deslip observed in every specimen. In most instances the tensile bands developed were interspersed between the compressive bands. This resulted in extrusions and metallurgical notches. So that the extent of such notches and extrusions can be appreciated the results of the reversed stress are presented in time-distance extent of gliding plots in Figs. 10, 11, 12, and 13. The profiles herein presented are the physical surfaces of the observation surface as seen in the plane containing the stress axis and the slip directions.

Although such plots delineate the juxtaposition of tensile and compressive slip bands the history of deslip is not adequately presented. Fig. 14 illustrates similar profiles taken at various time intervals for specimen 9-1-5. The extent of compressive slip,

deslip, and tensile slip on the same band is easily observed in this plot.

No correlation could be made between deslip and any other factor such as a) orientation, b) extent of slip, c) velocity of slip, rapidity of stress reversal, etc.

2. Temperature Effects

The specimens used in these tests are identified with a three part index, i.e. 39-3-16. The first number (39) identifies the heat or the gang of crystals simultaneously produced. The second number (3) identifies the orientation, and the last number (16) identifies the specific specimen. Interferometric cinemicrographic tests were performed at the three temperature levels, approximately -150°F, room temperature and approximately 225°F.

Tables 1 thru 9 present the data illustrating the chronological appearance of the slip bands, the extent of slip, and the velocity of slip. The slip line number frequently contains a subscript number which indicates whether the shear referred to is the first, second, etc., shear observed on this band. A better understanding of this multiple movement on the same band can be had by studying Fig. 2. The slopes of the lines in Fig. 2 are the velocities of slip. These same velocities are presented in bar graph form in Fig. 16.

During some of the high temperature extensions some slip bands seemed to partially disappear. This phenomenon is hereafter referred to as "Unslip" and is illustrated in Fig. 15. At the end

of these specific runs the load was maintained constant for a period of time and photographs taken before unloading. Fig. 15 shows further unslip on one band during this interval. Fig. 5 at room temperature and Fig. 2 at low temperature indicate no unslip.

All of the data from these investigations has not been presented. The reason for these omissions is one of the following: a) picture out of focus, b) insufficient fringes in the field to allow accurate measurement, or c) fringes too fuzzy to allow precise measurement.

DISCUSSION OF RESULTS

1. Deslip

The time records of slip developed have all shown the velocity of slip to be a constant with no acceleration or deceleration apparent. This fact led to the supposition that strain hardening on the slip band is cataclysmic and requires some finite period of time. It was further supposed that if the stress could be reversed within this period of time it should be possible to deslip the material.

The current investigations have not shown this time dependence to exist. Fig. 6 illustrates the fact that a slip band may cease to be active after about two seconds (line C1) and yet it can be deslipped after a wait of 41 seconds.

The evidence that an aluminum single crystal can be deslipped is not to be doubted. Yet it was not possible to deslip all of the

active slip bands in the specimens in which deslip was observed. It also proved to be impossible to detect any deslip in the records from some specimens. Efforts were made to correlate the tendency to deslip with orientation and extent of compressive strain without success. The deslip phenomenon can be explained by lattice bending as is discussed under temperature effects.

2. Temperature Effects

The slip velocities observed at the various temperatures follow the law previously presented (4)

$$V = K \dot{\epsilon} \left(\frac{\sigma^2}{2Ef} \right)$$

where K is a constant presently not understood but probably related to dislocation density

$\dot{\epsilon}$ - Strain rate

σ - Elastic Limit stress

E - Elastic modulus in direction of stress axis

f - frequency of coactive slip bands

The elastic limit stress change over the temperature range varies from 124 gm/mm² at the low temperature to 92 gm/mm² at the high temperature as the Elastic Modulus changes from 9 x 10⁶ gm/mm² at the low temperature to 6 x 10⁶ gm/mm² at the high temperature. The $\frac{\sigma^2}{2E}$ factor therefore varies from 8.5 x 10⁻⁴ to 7.0 x 10⁻⁴. The distance between coactive slip bands (1/f) on the other hand is observed to vary between 5 and 100 microns.

Since these tests were performed at approximately the same strain rate it would be expected that the velocity of slip could

change by two orders of magnitude as a function of the frequency of coactive slip bands alone. It would also be expected that the elastic resilience would not affect the velocity to any noticeable extent. In general the low temperature slip velocities are observed to have higher values than those obtained in the high temperature tests. The distance between the coactive bands can be greater in the low temperature tests than in the high temperature tests. This is necessarily a qualitative statement in view of the fact that the coactive band frequency can change by an order of magnitude in one specimen at a given temperature.

One of the most unexpected observations of this investigation is that of unslip. An explanation of this may be found by consideration of Fig. 17. If a total slip band does not become active at one time, one of two possible configurations must exist. Either the lattice between the slip planes must be bent as illustrated or one end of the crystal must twist about the specimen axis relative to the other end. In the case where the dislocation loops penetrate the surface in the center of the specimen the twisting is not possible and lattice bending must occur. If this lattice bending is of an elastic type, it is possible that a slip band becoming active in its close proximity can relieve the load and elastic restitution can occur or unslipping can occur as a result of released elastic strains.

It is also speculated that this bent lattice concept can explain the deslip when the stress is purposefully reversed. Since the elastic bending will provide an incremental and highly directed additive stress to the reversed stress, the bands which would deslip would only be those which were associated with lattice bending.

CONCLUSIONS

1. It is possible to deslip aluminum single crystals with reversed stresses.
2. The deslip phenomenon is not dependent on time, extent of strain, or orientation, but may be dependent on lattice bending.
3. The velocity of slip in the temperature range between -150°F and 225°F is relatively unaffected by the mechanical property changes.
4. The velocities of slip in the afore mentioned temperature range are primarily dependent on the frequency of co-active slip bands.
5. It is possible for a slip band to unslip or partially restore itself to its original configuration without a stress reversal or while slip is continuing on other bands.
6. Unslip can be explained by lattice bending of the elastic type.

ACKNOWLEDGMENT

The authors wish to acknowledge and express their gratitude for the efforts of Mr. Carol Mobley. His careful measurements and dedicated efforts have reduced a myriad of photomicrographs to a sensible array of data.

TABLE 1
 A1 39-3-12
 +77°F
 12 frames/sec.

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear(Δ)</u>	<u>Glide Time (Seconds)</u>	<u>Time from Beginning of Run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity Δ/sec</u>
1 ₁	.130	418				
2 ₁	.160	515				
3 ₁	.057	184	Lines in at beginning of run			
4 ₁	.135	434				
5 ₁	.027	87				
4 ₁	.045	145	.25	1.00		580
6 ₂	.040	129	.42	1.08	.08	307
4 ₁	.017	55	.10	1.50	.42	550
4 ₃	.013	42	.08	2.00	.50	525
5 ₄	.020	64	.18	2.82	.82	355
4 ₂	.015	48	.09	3.08	.26	533
6 ₅	.055	177	.42	4.65	1.57	422
5 ₂	.020	64	.17	4.75	.10	376
7 ₃	.035	113	1.00	10.00	5.25	113
8 ₁	.030	97	.25	10.90	.90	388
6 ₁	.040	129	.80	15.05	4.15	161
8 ₃	.022	71	.23	16.42	1.37	309
6 ₂	.037	119	.36	16.82	.40	331
8 ₄	.078	251	.65	17.70	.88	386
6 ₃	.028	90	.15	18.42	.72	600
7 ₅	.030	97	.22	19.08	.66	441
8 ₂	.025	81	.15	19.25	.17	540
7 ₄	.030	97	.18	19.92	.67	539
2 ₃	.030	97	.15	22.50	2.58	647
5 ₂	.040	129	.65	22.52	.02	198
6 ₄	.022	71	.25	24.25	1.73	284
6 ₇	.033	106	.32	24.75	.50	331

TABLE 2
 A1 39-6-1
 +77°F
 12 frames/sec.

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear A</u>	<u>Glide Time(sec)</u>	<u>Time from Beginning of run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity A/sec</u>
1 ₁	.495	2145				
2 ₁	.225	977				
3 ₁	.252	1093	Lines in at beginning of run			
4 ₁	.125	543				
5 ₁	.295	1281	1.15	7.0		1114
1 ₁	.070	304	0.40	7.60	0.60	760
6 ₂	.135	586	1.35	7.90	0.30	434
5 ₁	.105	456	0.50	9.55	1.65	912
6 ₂	.162	703	0.50	9.63	0.08	1406
3 ₂	.038	165	0.15	10.15	0.52	1100
3 ₂	.030	130.3	0.12	10.50	0.35	1086
6 ₃	.068	295	0.30	10.52	0.02	984
3 ₄	.060	260.5	0.15	11.60	1.08	1735

TABLE 3
 Al 39-3-16
 +235-225°F
 12 frames/sec.

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear(A)</u>	<u>Glide Time (Seconds)</u>	<u>Time from Beginning of Run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity A/sec</u>
1 ₁	.168	541				
2 ₁	.040	129				
3 ₁	.030	97				
4 ₁	.075	242				
5 ₁	.108	348				
6 ₁	.025	81				
7 ₁	.045	145				
6 ₁	.040	129	.25	7.17		516
2 ₂	.160	515	.50	8.17	1.00	1030
2 ₂	.058	187	.25	9.07	.90	748
6 ₃	.040	129	.30	9.50	.43	430
2 ₃	.042	135	.28	10.35	.85	482
7 ₂	.090	290	.23	10.85	.50	1260
3 ₂	.202	651	.42	13.43	2.58	1550
7 ₃	.105	338	.70	13.80	.37	483

Lines in at beginning of run

TABLE 4
 A1 39-6-7
 230-225°F
 12 frames/sec

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear(Å)</u>	<u>Glide Time (Seconds)</u>	<u>Time from Beginning of Run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity Å/sec</u>
1 ₁	.517	2245	Lines in at beginning of run			
2 ₁	.385	1670				
3 ₁	.200	867	0.33	1.67		2625
4 ₁	.300	1302	1.04	3.78	2.11	1252
5 ₁	.095	412	0.50	4.15	0.37	824
2 ₁	-.107	-464	0.45	4.30	0.15	1032
3 ₁	-.040	-174	0.15	5.45	1.15	1160
3 ₂	-.035	-152	0.15	5.92	0.47	1013
2 ₂	.040	174	0.25	6.00	0.08	696
3 ₃	-.020	-87	0.13	6.35	0.35	669
2 ₃	.036	156	0.15	6.52	0.17	1040
3 ₄	-.030	-130	0.17	6.93	0.41	765
5 ₁	-.028	-122	0.15	7.50	0.57	814
3 ₅	-.025	-108	0.17	7.83	0.33	635
6 ₁	.062	269	0.15	8.10	0.27	1793
5 ₂	-.022	-95	0.20	8.68	0.58	475
3 ₆	-.020	-87	0.08	9.00	0.32	1088
6 ₂	.038	165	0.28	9.22	0.22	589
2 ₄	.052	226	0.20	9.30	0.08	1130
2 ₅	.068	295	0.27	10.15	0.85	1093
5 ₃	-.025	-108	0.17	11.25	1.10	635
5 ₄	-.020	-87	0.25	12.18	0.93	348
2 ₆	.054	234	0.30	13.05	0.87	780
7 ₁	.143	621	0.68	15.07	2.02	914
2 ₇	.074	321	0.27	16.00	0.93	1188
7 ₂	.102	442	0.50	17.38	1.38	884
6 ₃	.120	521	0.38	17.42	0.04	1371
2 ₈	.093	403	0.35	19.40	1.98	1152
7 ₃	.047	204	0.15	20.65	1.25	1360
4 ₂	.055	239	0.32	20.95	0.30	747
6 ₄	.085	369	0.33	22.10	1.15	1119
8 ₁	.050	217	0.35	26.40	4.30	620

TABLE 5
 A1 39-6-5
 230°F-225°F
 12 frames/sec.

<u>Line</u>	<u>Ratio</u>	<u>Shear</u>		<u>Time from beginning of run(sec)</u>	<u>Time between lines(sec)</u>	<u>Velocity A/sec</u>
		<u>°</u> <u>A</u> <u>Resolved</u>	<u>Glide</u> <u>Time(sec)</u>			
1 ₁	.212	919				
2 ₁	.280	1214				
3 ₁	.072	312				
4 ₁	.048	208				
5 ₁	.045	195				
2 ₂	.035	152	0.30	0.17		507
6 ₂	.050	217	0.20	0.72	.55	1084
4 ₂	.057	247	0.17	0.75	.03	1452
3 ₂	.173	750	0.23	0.77	.02	3260
7 ₂	.040	173	0.28	0.82	.05	618
6 ₂	.105	456	0.35	1.92	1.10	1301
1 ₂	.085	369	0.31	1.97	.05	1190
4 ₃	.115	498	0.25	2.00	.03	1992
8 ₃	.075	325	0.65	2.10	.10	500
5 ₂	.155	672	0.50	2.25	.15	1344
3 ₃	.085	369	0.25	2.43	.18	1476
4 ₄	.135	586	0.30	2.52	.09	1951
7 ₂	.028	121	0.15	2.62	.10	807
5 ₃	.033	143	0.15	3.67	1.05	954
6 ₃	.065	282	0.25	3.75	.08	1128
1 ₃	.058	252	0.13	3.87	.12	1939
3 ₄	.065	282	0.30	3.95	.08	940
6 ₄	.030	130	0.10	5.45	1.50	1300
9 ₁	.042	182	0.30	5.55	.10	607
1 ₄	.120	511	0.23	5.80	.25	2262
3 ₅	.030	130	0.15	5.92	.12	867
6 ₅	.050	217	0.17	6.00	.08	1276
5 ₄	.092	399	0.47	6.10	.10	849
10 ₁	.190	824	0.38	8.52	2.42	2165
5 ₅	.128	555	0.28	8.52	0.00	1982
11 ₁	.093	403	0.27	8.55	.03	1493
12 ₁	.045	195	0.15	8.85	.30	1300
6 ₆	.060	260	0.25	9.10	.25	1040
11 ₂	.152	659	0.30	10.00	.90	2195
13 ₁	.045	195	0.15	10.03	.03	1300
12 ₂	.048	208	0.13	10.12	.09	1600
10 ₂	.055	239	0.20	10.50	.38	1195
12 ₃	.067	291	0.30	10.52	.02	970
11 ₃	.040	173	0.19	10.73	.21	911
6 ₇	.108	468	0.25	10.75	.02	1872
11 ₄	.107	464	0.48	11.20	.45	968
13 ₂	.080	347	0.40	11.35	.15	868

Lines in at beginning of run

TABLE 5 (Continued)

<u>Line</u>	<u>Ratio</u>	Shear • <u>A</u> <u>Resolved</u>	<u>Glide</u> <u>Time(sec)</u>	<u>Time from</u> <u>beginning</u> <u>of run(sec)</u>	<u>Time</u> <u>between</u> <u>lines(sec)</u>	<u>Velocity</u> <u>A/sec</u>
14 ₁	.160	694	0.55	11.68	.33	1261
6 ₁	.097	421	0.34	11.93	.25	1238
10 ₃	.187	811	0.33	12.05	.12	2455
15 ₁	.155	672	0.20	12.15	.10	3360
16 ₁	.048	208	0.15	12.92	.77	1387
10 ₄	.088	382	0.45	13.00	.08	848
15 ₂	.033	143	0.30	13.20	.20	477
17 ₁	.080	347	0.28	13.22	.02	1239
18 ₁	.045	195	0.23	13.32	.10	848
19 ₁	.036	156	0.15	13.43	.11	1040
19 ₂	.086	373	0.37	13.93	.50	1008
16 ₂	.104	451	0.31	14.52	.59	1453
17 ₂	.165	716	0.22	14.60	.08	3250
9 ₂	.053	230	0.25	14.75	.15	920

TABLE 6
 A1 39-3-13
 -120°F
 12 frames/sec

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear A</u>	<u>Glide Time(sec)</u>	<u>Time from Beginning of run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity A/sec</u>
1 ₁	.150	483				
2 ₁	.070	226				
3 ₁	.040	129				
4 ₁	.260	837	.75	1.25		1116
5 ₁	.020	64.4	.18	1.50	.25	358
6 ₁	.043	138	.15	1.75	.25	920
7 ₁	.110	354	.55	2.05	.30	644
8 ₁	.100	322	.50	2.75	.70	644
6 ₂	.017	55	.08	3.92	1.17	688
7 ₂	.060	193	.12	4.13	.21	1610
8 ₂	.053	171	.25	4.75	.62	684
6 ₃	.035	113	.20	5.17	.42	565
9 ₁	.027	87	.18	6.57	1.40	483
8 ₃	.082	264	.25	6.75	.18	1056
8 ₄	.045	145	.20	7.55	.80	725
9 ₂	.070	226	.35	8.60	1.05	646
10 ₁	.170	547	.78	9.72	1.12	702
5 ₂	.070	226	.45	9.80	.08	502
11 ₁	.220	709	.75	9.85	.05	945
12 ₁	.025	80.5	.05	9.87	.02	1610
13 ₁	.165	532	.80	9.95	.08	665
12 ₂	.155	499	.35	10.15	.20	1427
14 ₁	.100	322	.58	10.17	.02	555
15 ₁	.047	151	.20	10.32	.15	755
10 ₂	.105	338	.30	10.70	.38	1127
11 ₂	.050	161	.18	10.82	.12	895
13 ₂	.055	177	.25	12.00	1.18	708
5 ₃	.022	71	.13	12.07	.07	546
15 ₂	.028	90.3	.23	12.07	.00	393
14 ₂	.058	187	.40	12.10	.03	467
14 ₃	.030	97	.18	12.82	.72	539
14 ₄	.030	97	.17	13.25	.43	570

Lines in at beginning of run

TABLE 7
 A1 60-39-9-1
 -158°F
 32 frames/sec.

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear A</u>	<u>Glide Time(sec)</u>	<u>Time from Beginning of run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity A/sec</u>
1 ₁	.03	130	Lines in at beginning of run			
2 ₁	.185	803				
1 ₂	.245	1063	.09	0.88	0.88	11815
3 ₂	.055	238	.125	0.94	0.06	1903
4 ₁	.285	1237	.08	4.56	3.62	15470
2 ₂	.030	130	.13	4.57	0.01	1000
5 ₂	.035	152	.045	4.585	0.015	3375
3 ₂	.150	651	.045	4.59	0.005	14450
6 ₁	.030	130	.06	4.615	0.025	2165
7 ₁	.512	2220	.075	6.06	1.445	29600
8 ₁	.030	130	.04	6.075	0.015	3250
9 ₁	.165	716	.075	6.12	0.045	9545
1 ₃	.060	260	.075	6.32	0.20	3465
9 ₂	.140	607	.10	6.75	0.43	6070

TABLE 8
 A1 39-9-3
 -190°F
 32 frames/sec

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear(Å)</u>	<u>Glide Time (Seconds)</u>	<u>Time from Beginning of Run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity Å/sec</u>
1 ₁	.242	1050	.105	.21		10000
2 ₁	.190	824	.045	.28	.07	18310
3 ₁	.107	464	.025	.315	.035	18580
3 ₂	.173	751	.13	.78	.465	5775
2 ₂	.077	334	.05	.80	.02	6685
4 ₂	.378	1640	.05	.85	.05	32800
5-6 ₁	.360	1562	.16	1.50	.65	9760
5-6 ₂	.141	612	.12	2.12	.62	5100
3 ₃	.042	182	.035	2.65	.53	5200
5-6 ₃	.125	542	.075	2.775	.125	7235
2 ₃	.043	187	.045	2.825	.050	4160
7 ₃	.200	868	.11	2.85	.025	7890
2 ₄	.030	130	.035	3.34	.49	3715
7 ₂	.073	317	.04	3.35	.01	7925
8 ₁	.232	1007	.08	3.40	.05	12590
3 ₄	.058	252	.02	3.41	.01	12600
8 ₄	.100	434	.065	4.065	.655	6685
8 ₂	.268	1162	.10	4.80	.735	11620
3 ₅	.060	261	.035	4.95	.15	7460
9 ₅	.177	768	.14	5.39	.44	5485
8 ₁	.110	477	.03	5.45	.06	15910
3 ₆	.047	204	.065	5.50	.05	3140
10 ₁	.055	239	.06	5.50	.00	3980
10 ₂	.055	239	.065	7.025	1.525	3680

TABLE 9
 A1 39-2-3
 -155°F
 32 frames/sec

<u>Line</u>	<u>Ratio</u>	<u>Resolved Shear A</u>	<u>Glide Time (sec)</u>	<u>Time from Beginning of Run(sec)</u>	<u>Time between Lines(sec)</u>	<u>Velocity A/Sec</u>
1 ₁	.126	1328				
2 ₁	.080	843	Lines in at beginning of run			
3 ₁	.040	421				
4 ₁	.357	3760				
3 ₁	.160	1687	.07	.23		24100
5 ₁	.215	2265	.09	.31	0.08	25200
5 ₂	.077	812	.07	.44	0.13	11600
2 ₂	.020	211	.04	.50	0.06	5275
5 ₃	.041	432	.025	.80	0.30	17290
5 ₄	.034	358	.035	1.98	1.18	10220
6 ₁	.205	2160	.09	2.11	0.13	24000
6 ₂	.045	474	.14	2.84	0.73	3385
6 ₃	.057	601	.10	7.09	4.25	6010

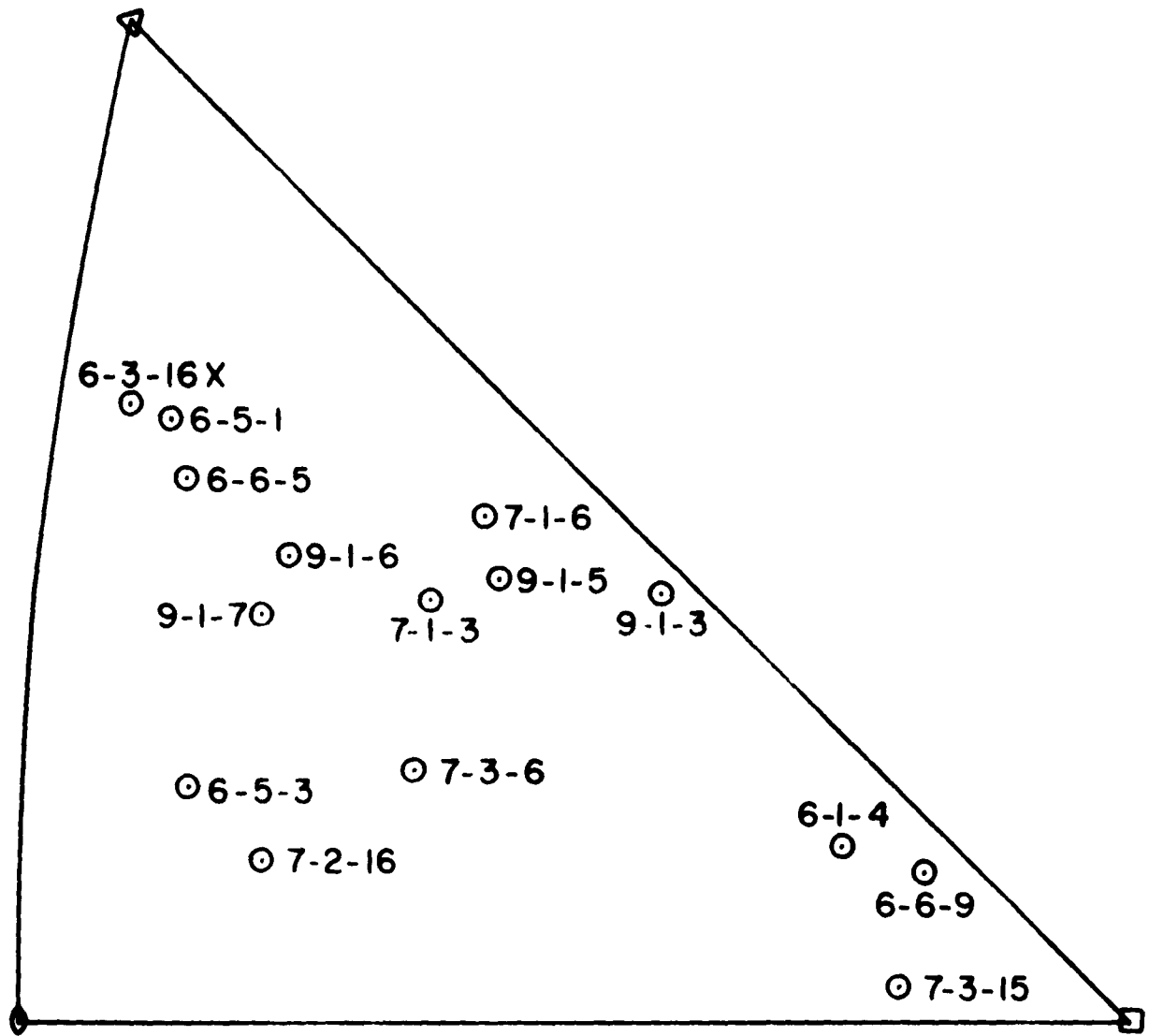


Figure 1a

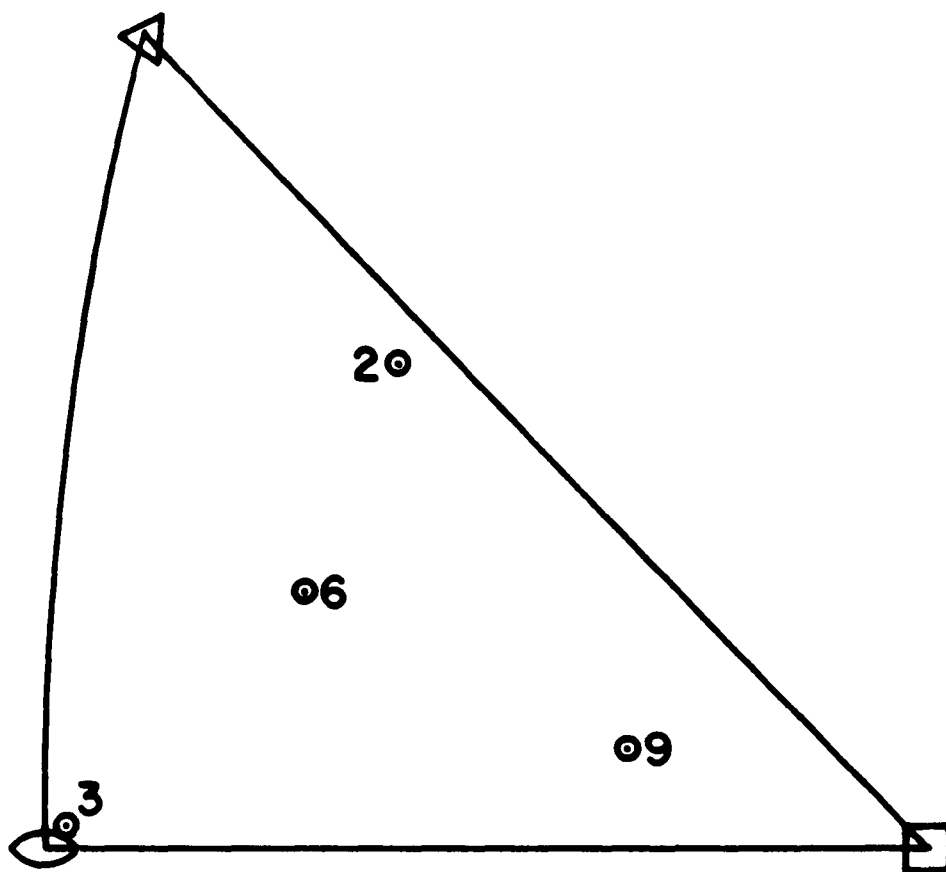


FIG. 1b

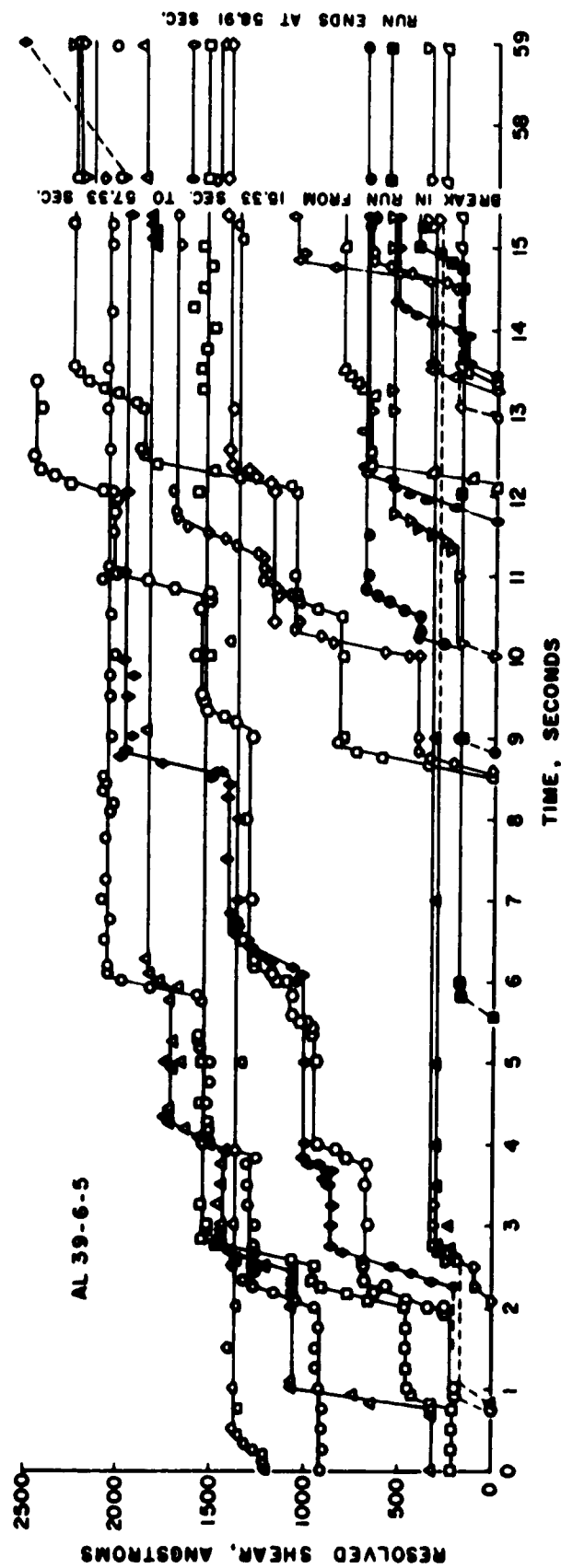


FIG. 2

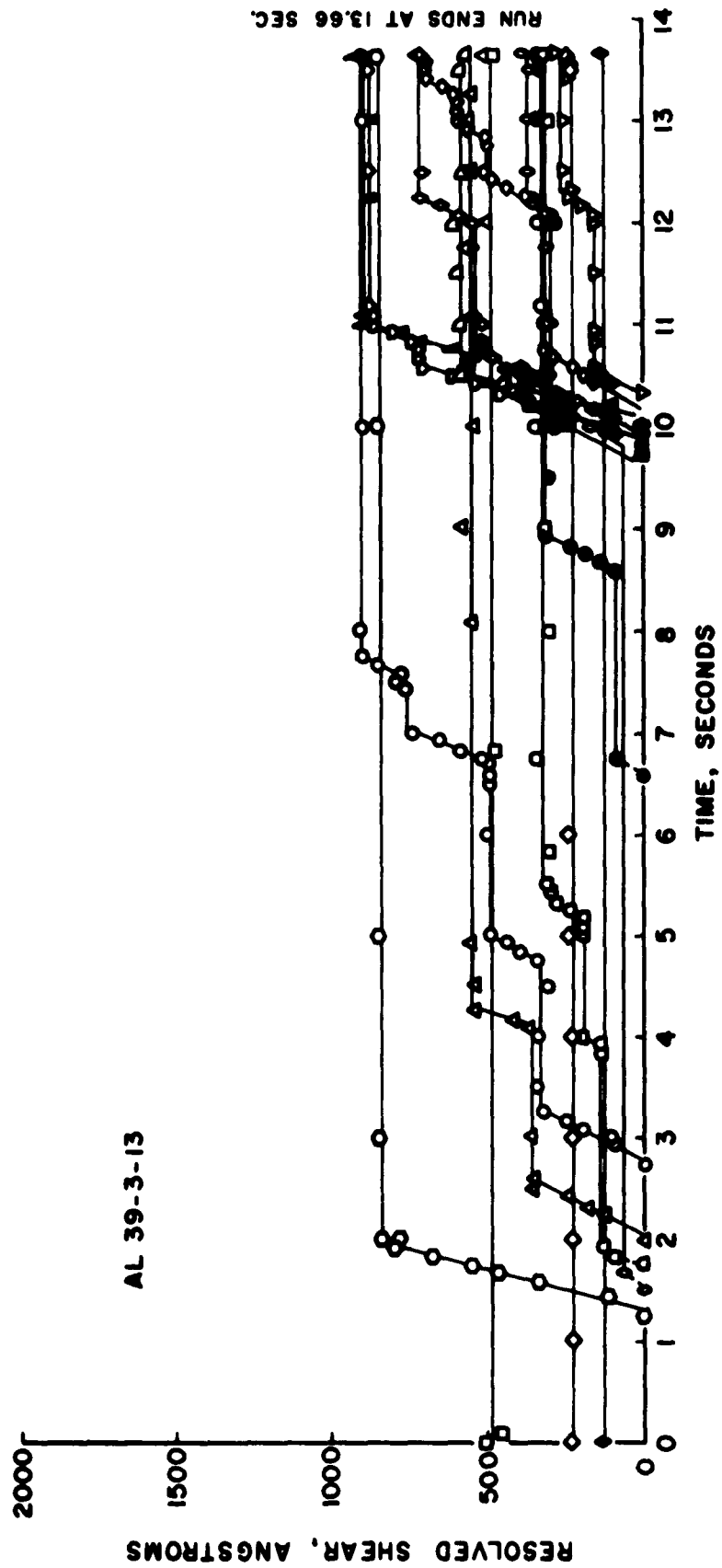


FIG. 3

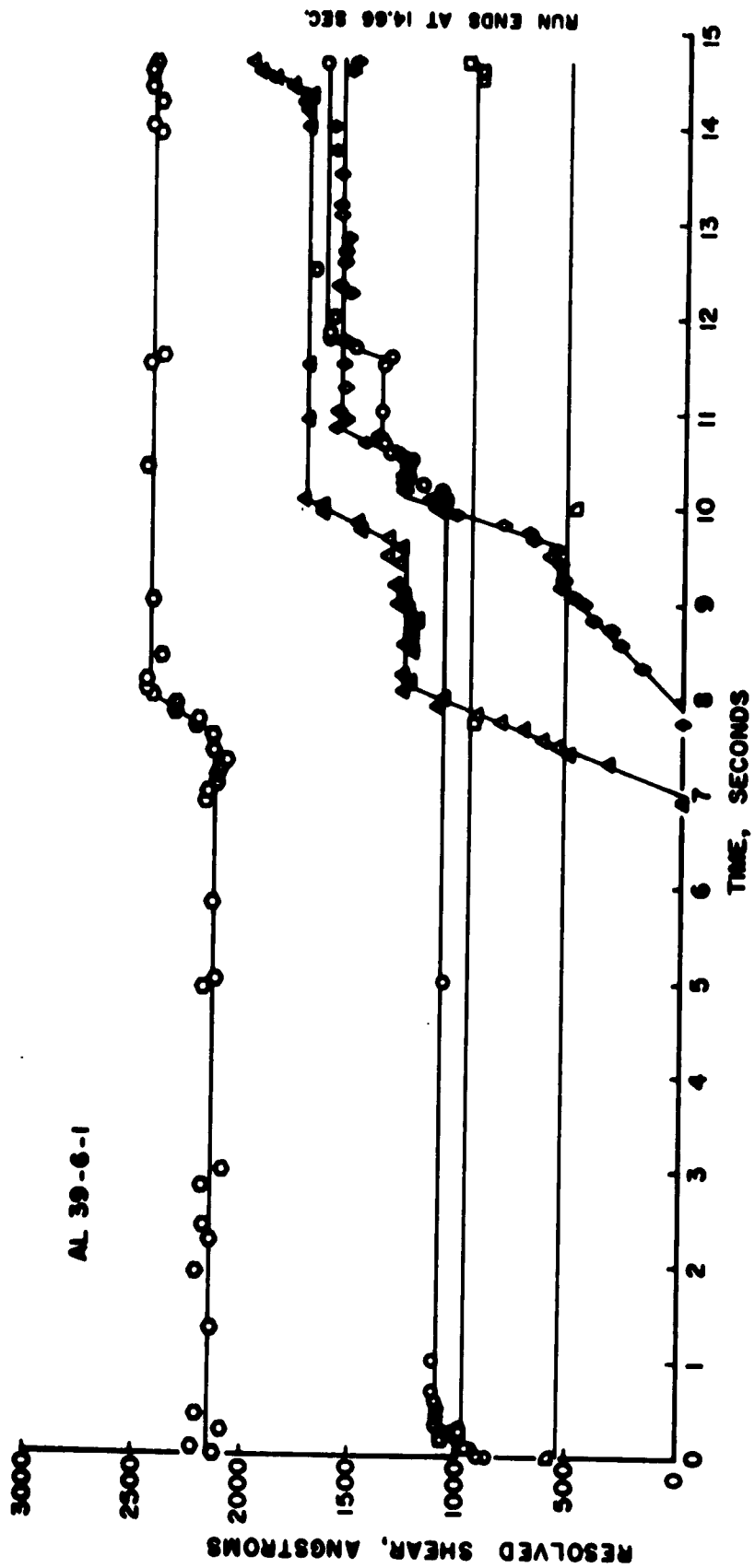
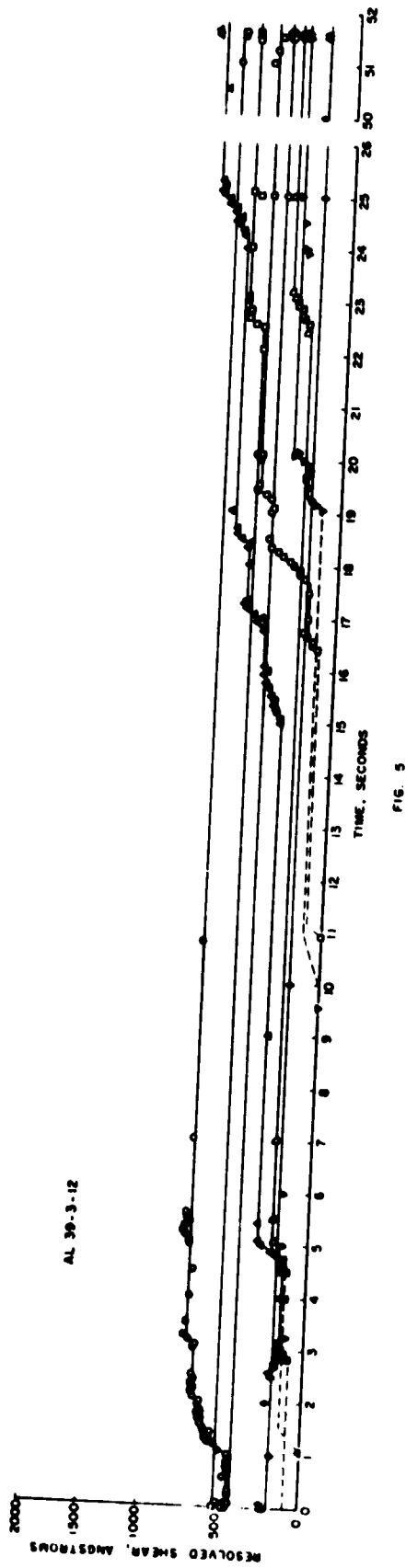
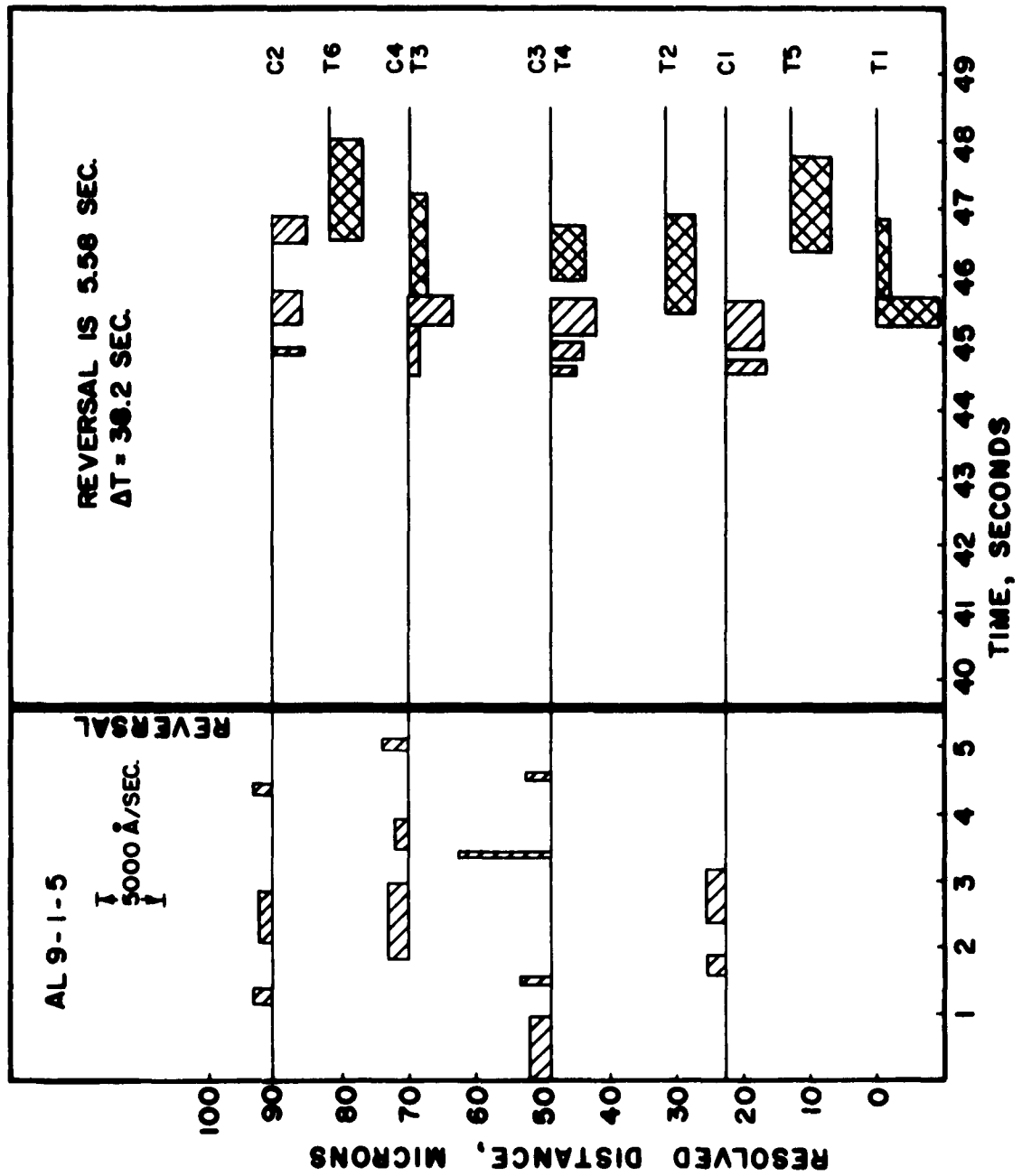


FIG. 4





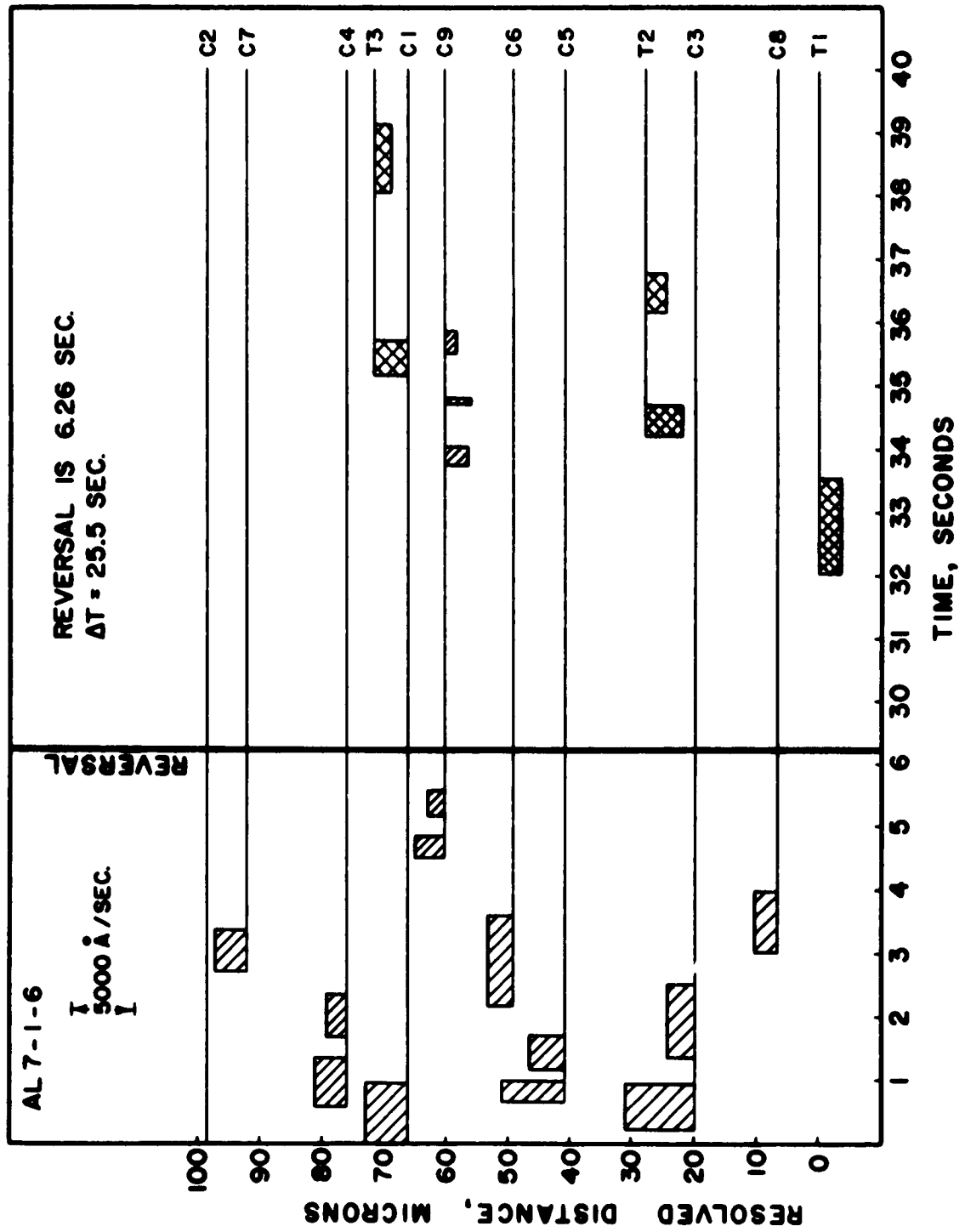


FIG. 7

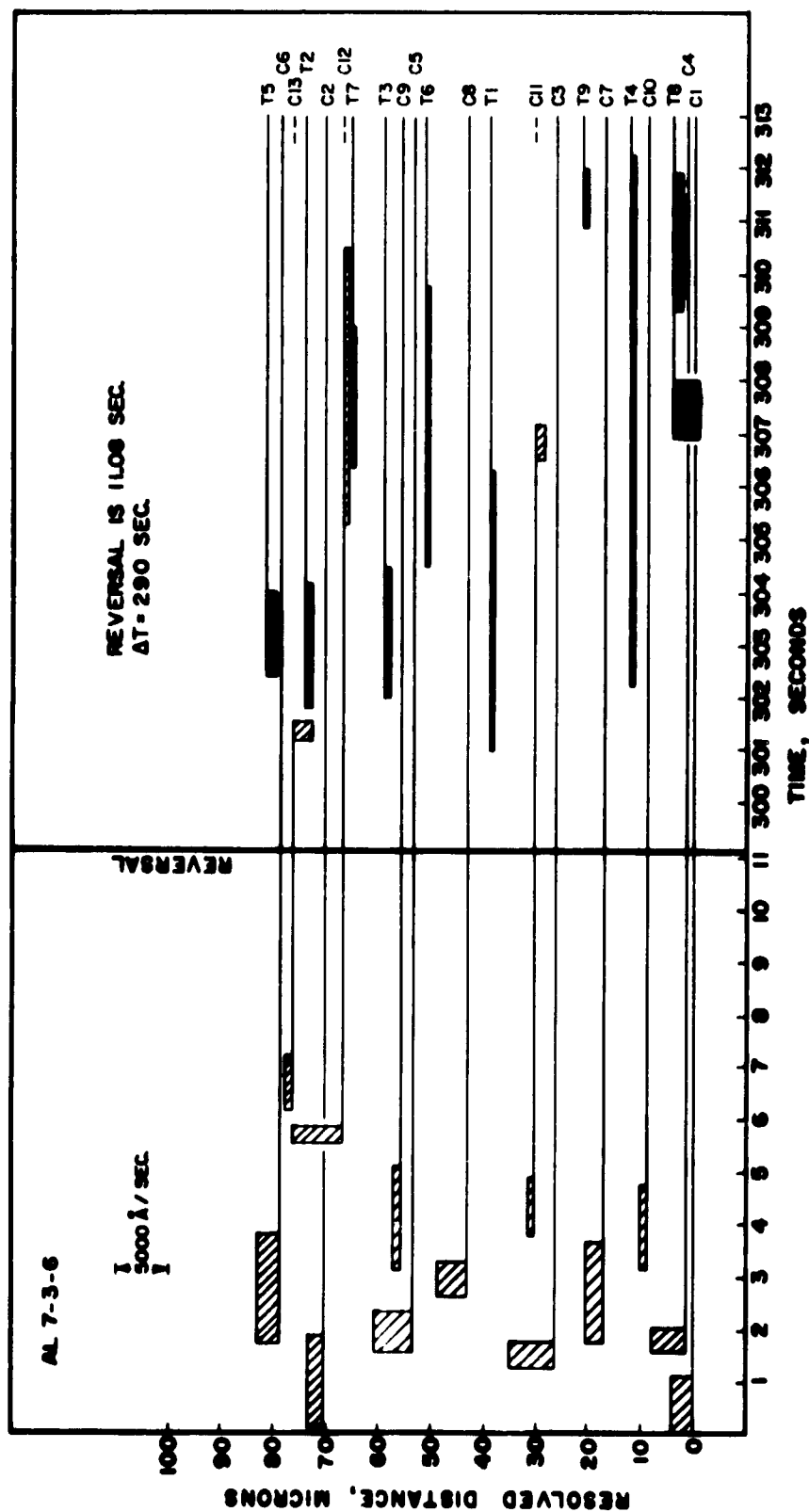


FIG. 8

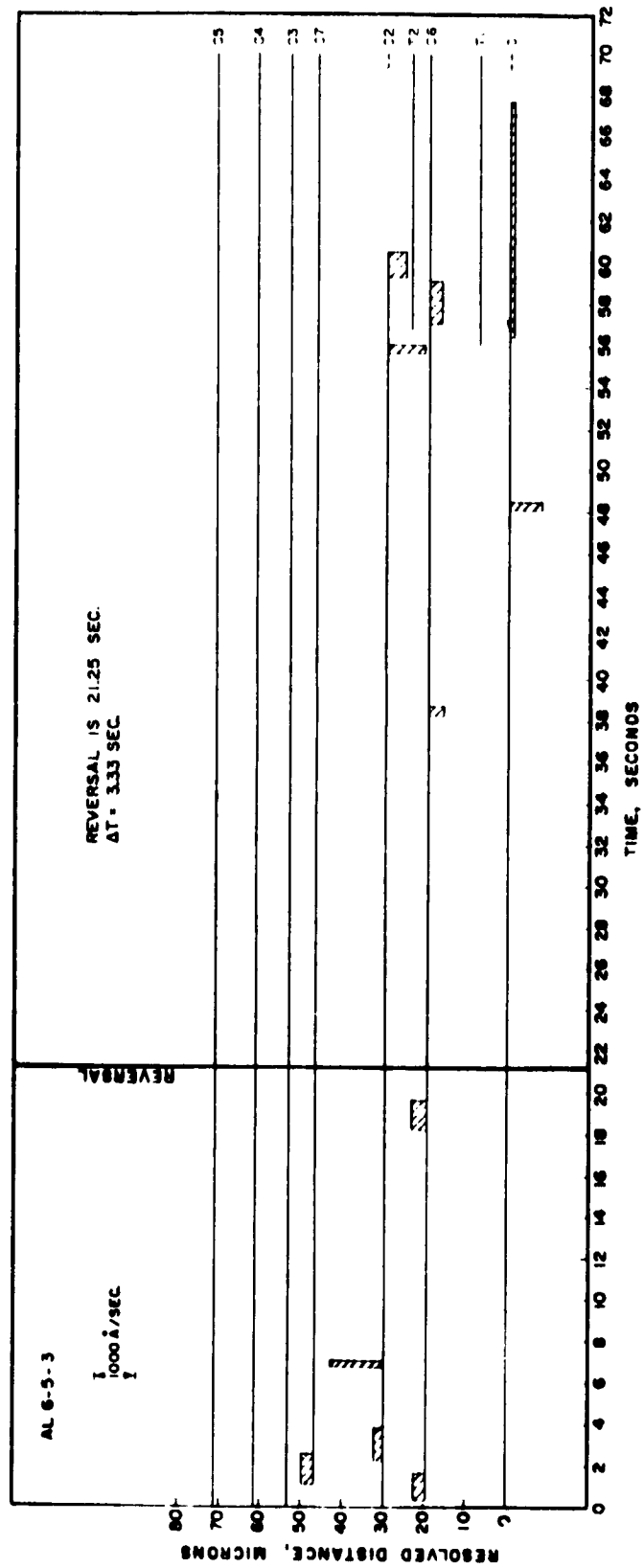


FIG. 9

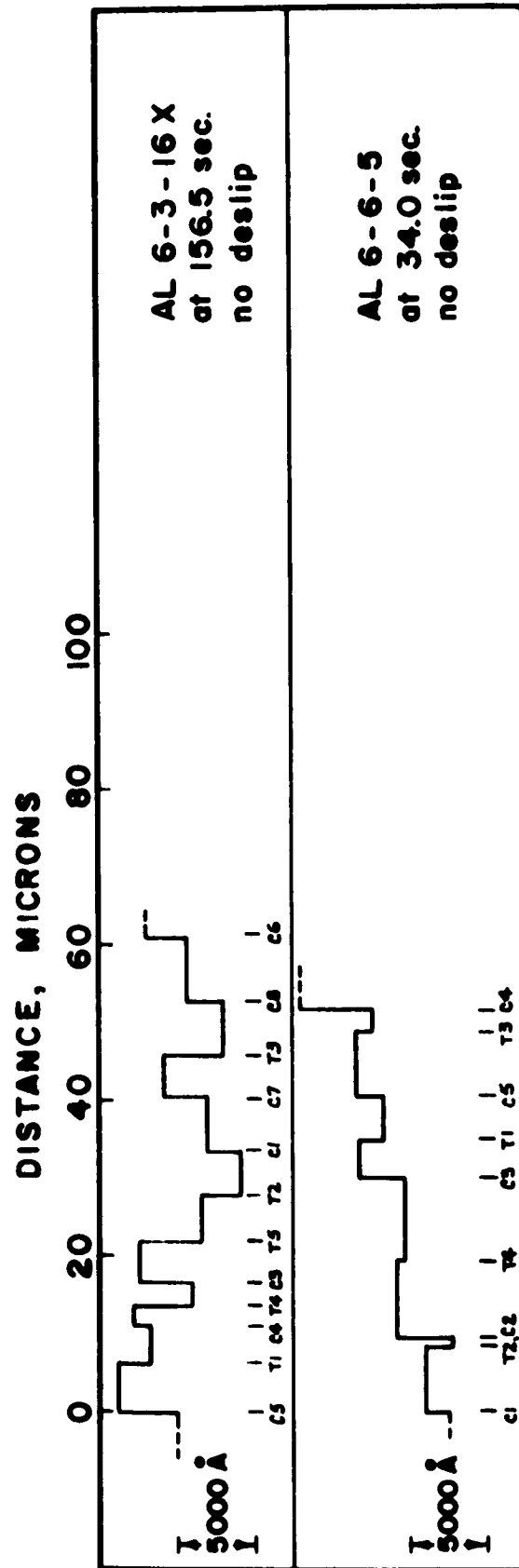


FIG. 10

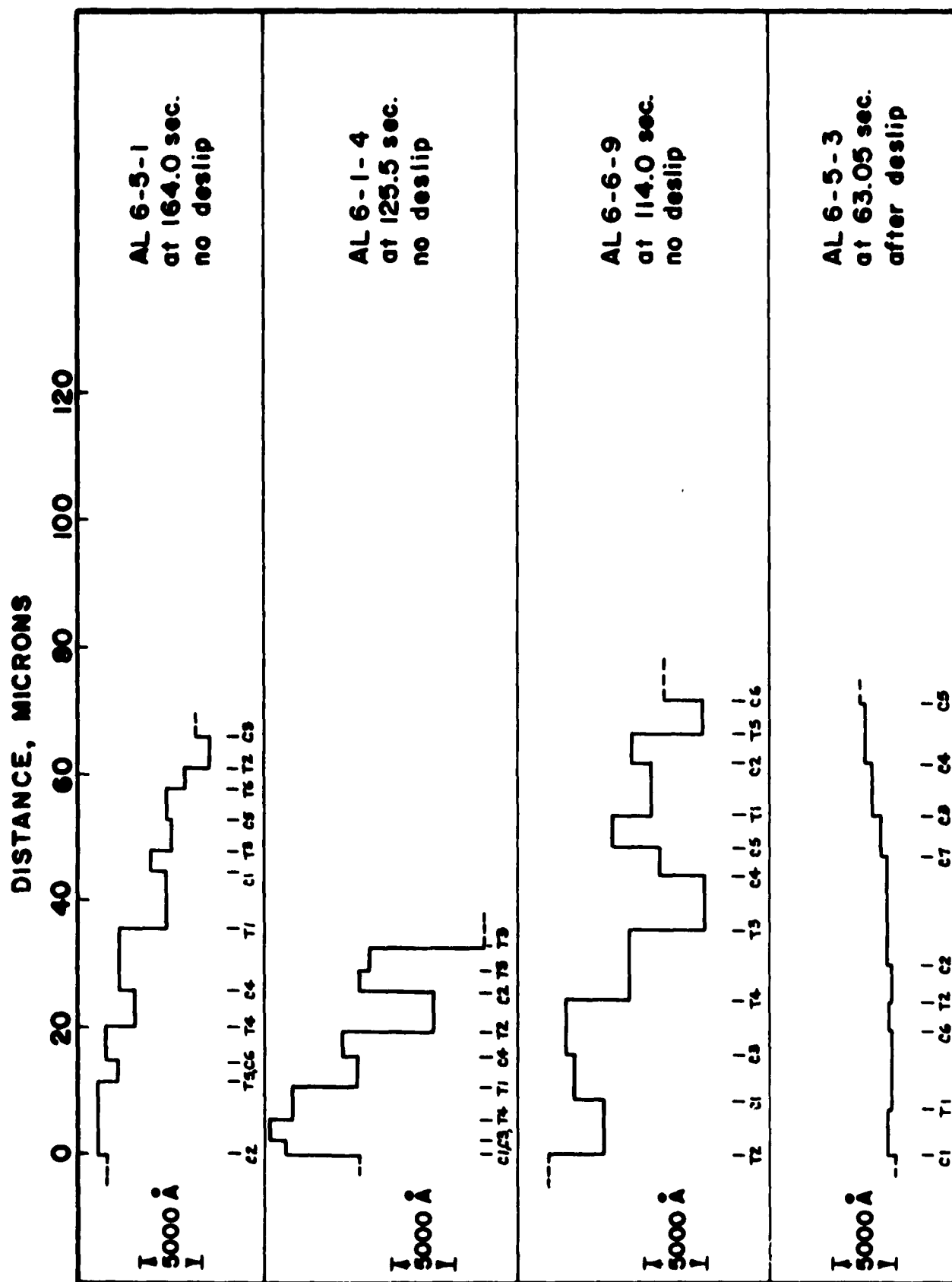


FIG. 11

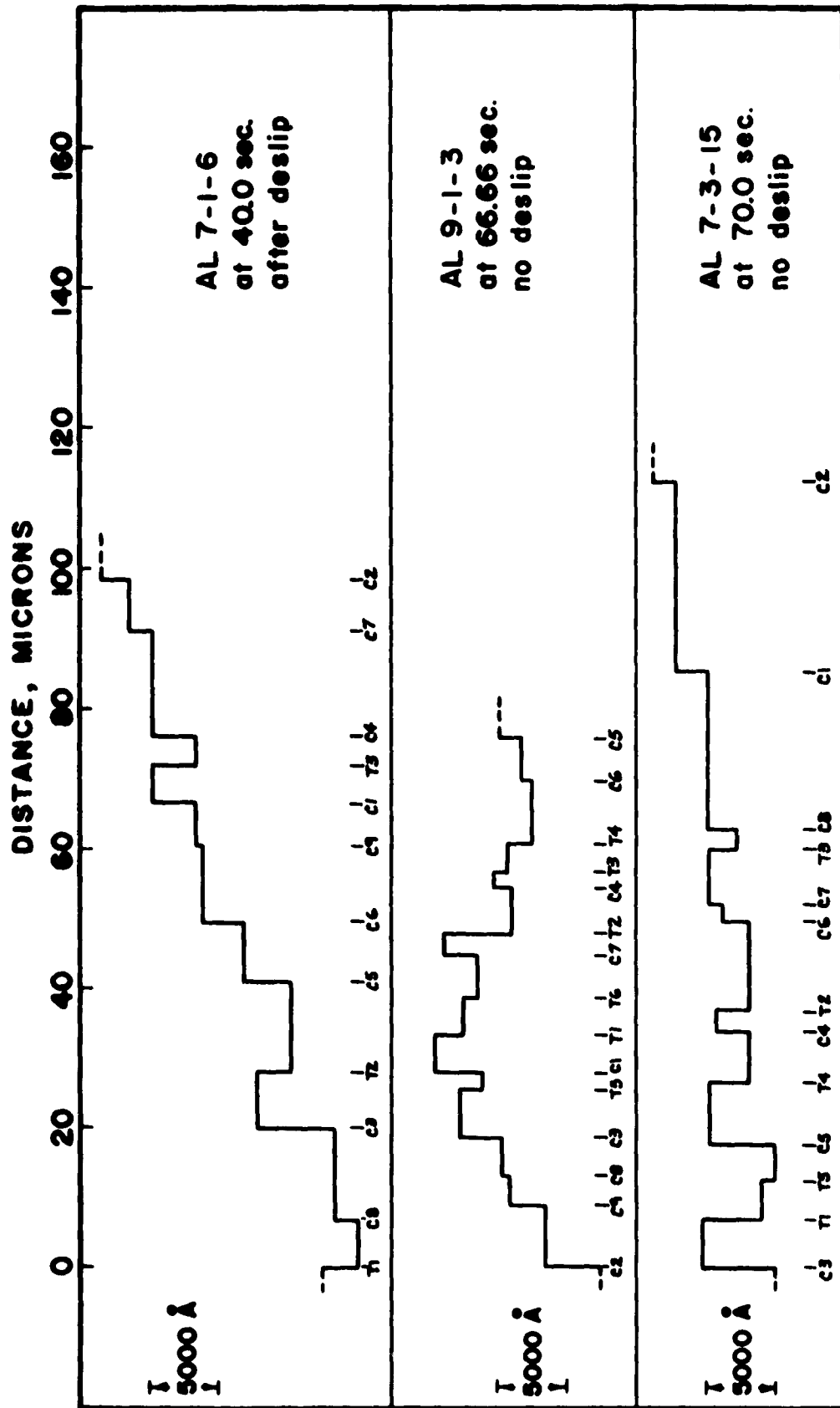
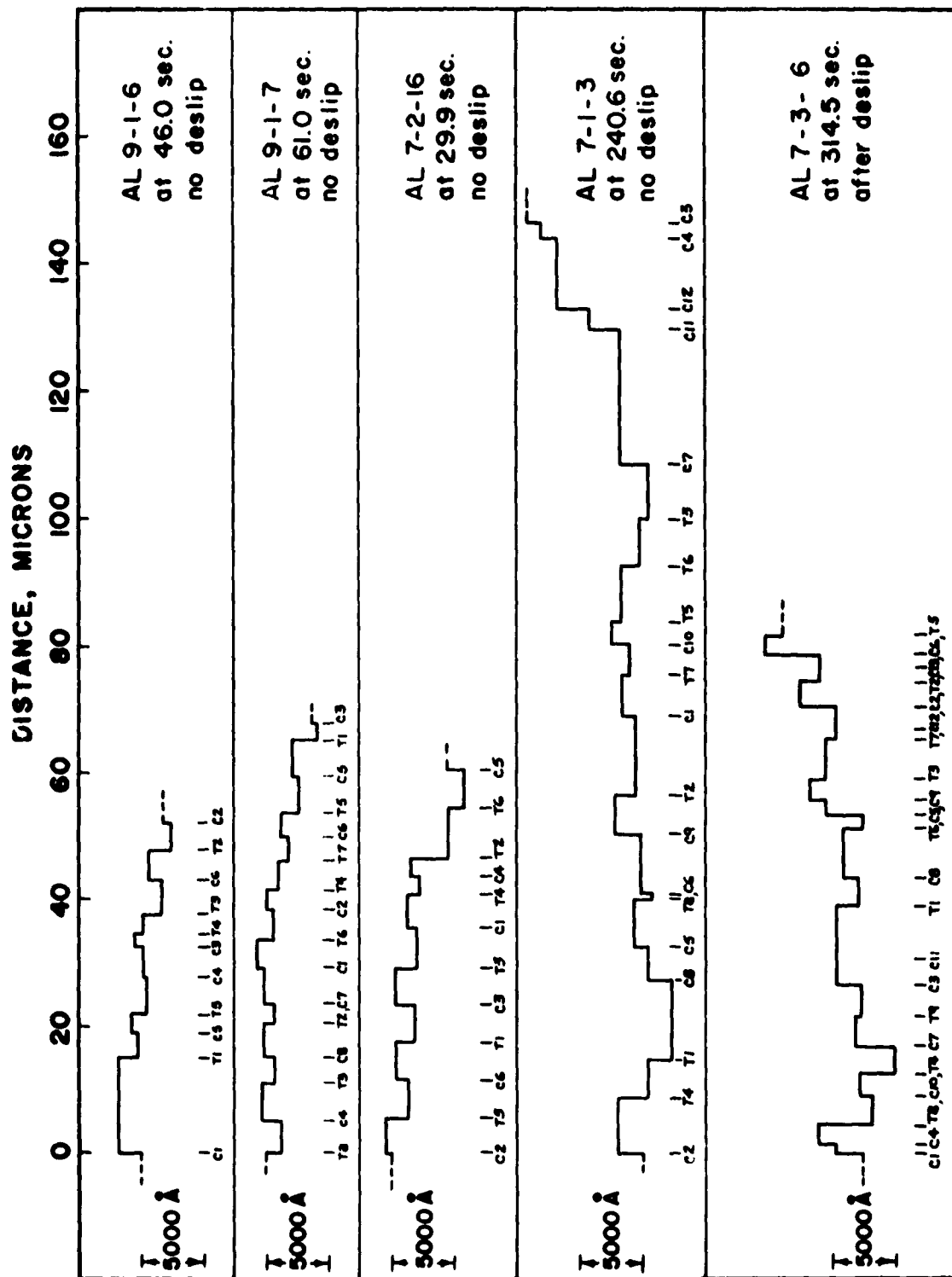


FIG. 12



AL 9-1-5

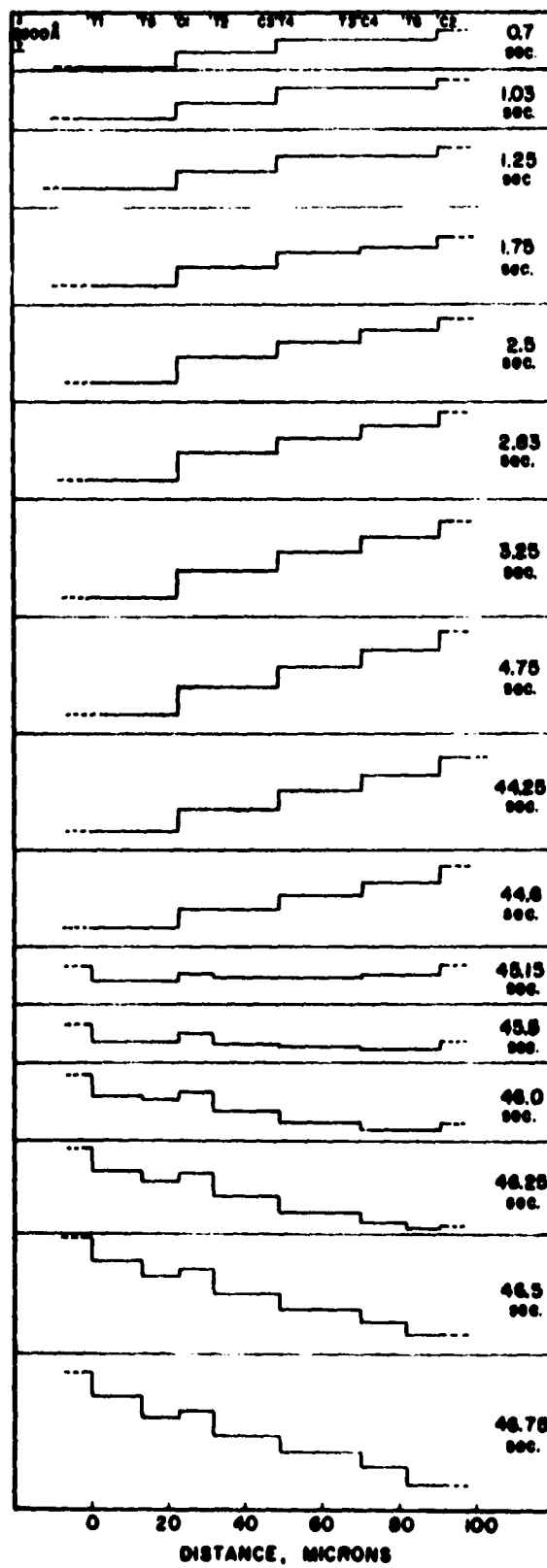


FIG. 14

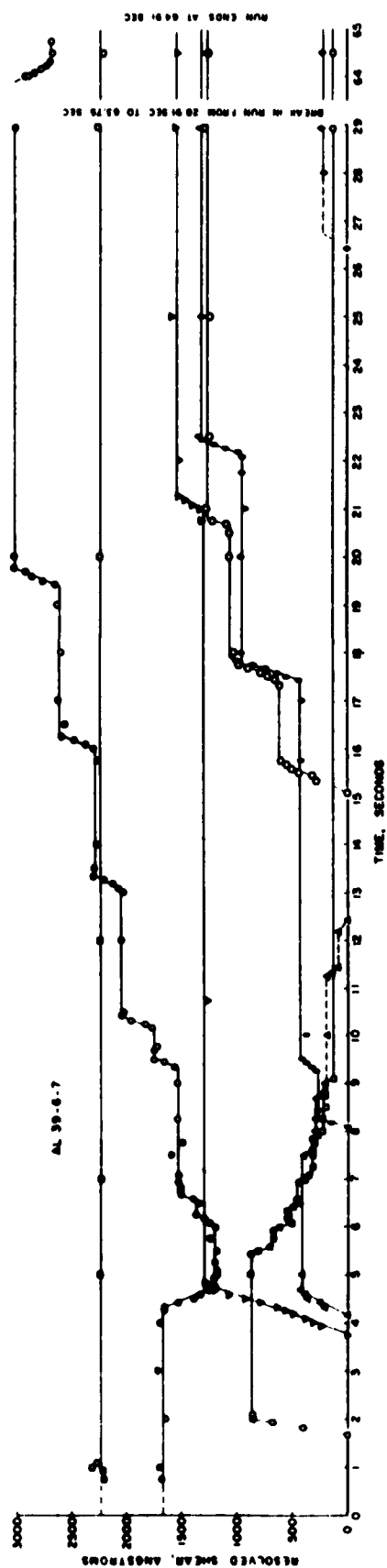
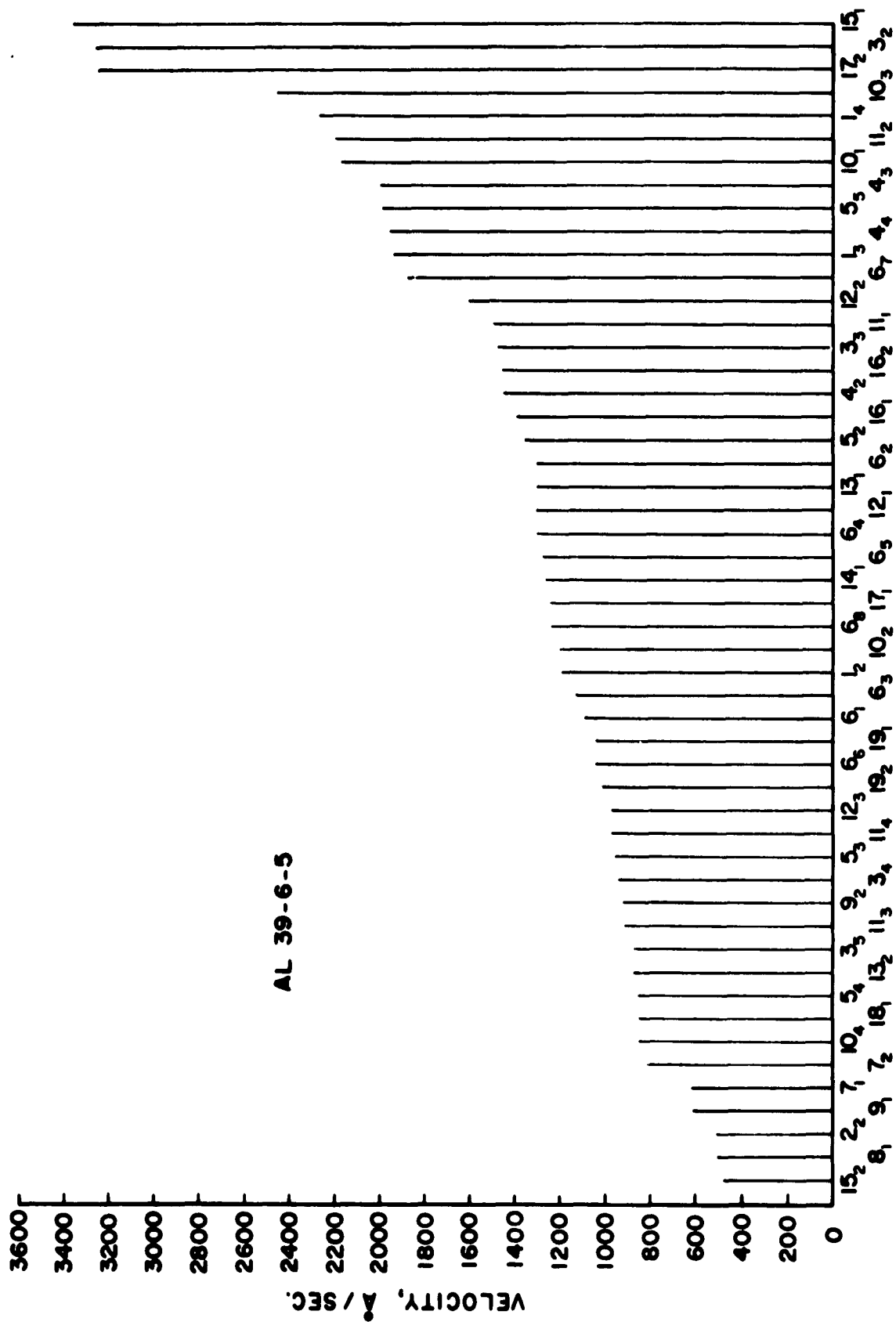
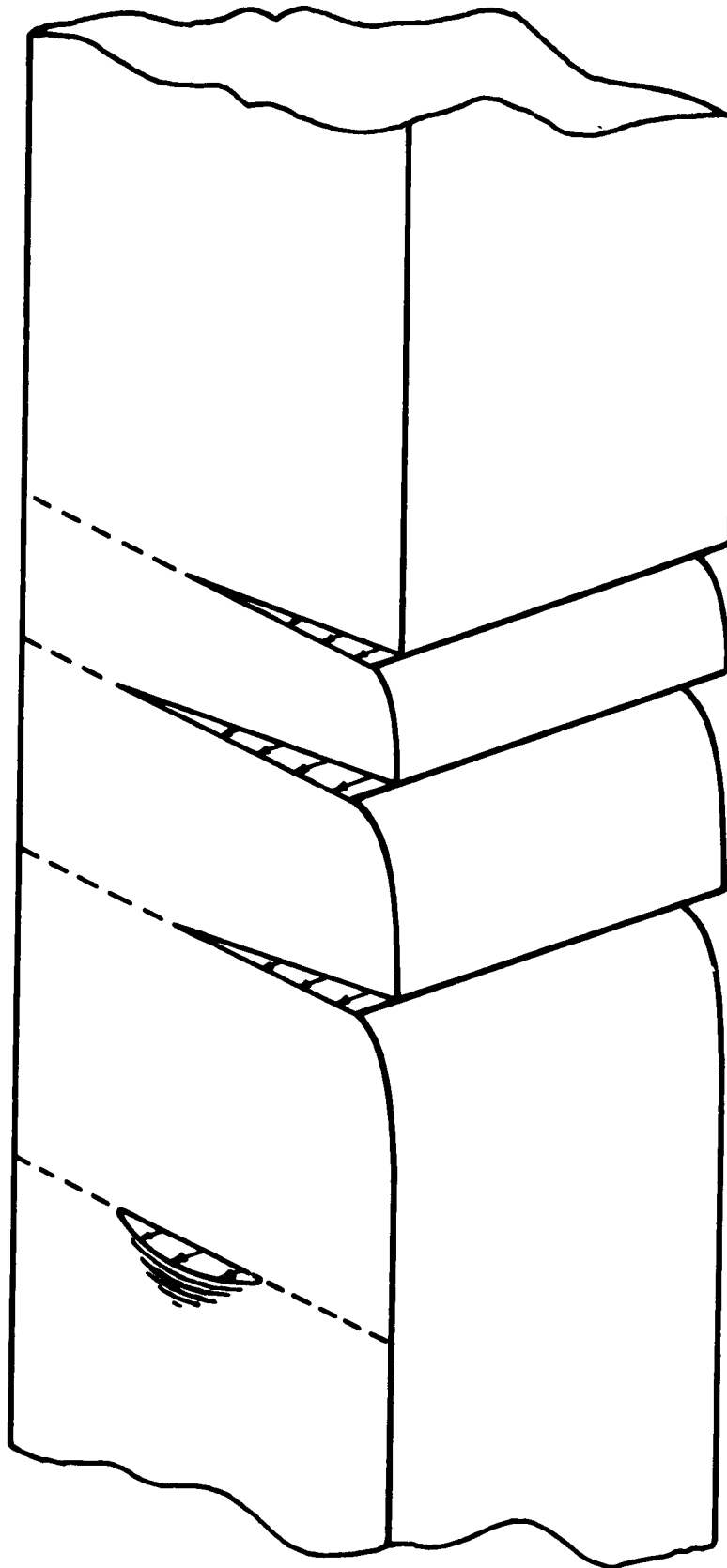


FIG. 15



LINE NUMBER

FIGURE 15

**FIGURE 17**

BIBLIOGRAPHY

1. N. K. Chen, R. B. Pond: "Dynamic Formation of Slip Bands in Aluminum," Trans. AIME Oct. 1952 p. 1085-1092.
2. R. Becker, P. Haasen: "Kinematographie Von Gleitlinien Auf Al.-Einkristallen" Acta Met 1 (1953) 325.
3. P. Haasen, R. Siems: "Wachstum Von Gleitlinien Auf Einkristallen Aus Aluminum Und Zink" Z Metallkunde, Vol. 48 (1957), p. 315-326.
4. R. B. Pond, E. Harrison: "Slip Velocities in Several Metals as Measured by Interferometric Cinemicrography" ASTIA Document No. AD 162 153, August 1958.
5. R. B. Pond, E. Harrison: "Cinemicrographic Recording of Multiple Interferometric Fringes during Plastic Deformation of Single Crystals," Review of Scientific Instruments, Vol. 28 (1957), p. 574.

DISTRIBUTION LIST FOR TECHNICAL NOTES AND TECHNICAL REPORTS

SOLID STATE SCIENCES DIVISION

1 March 1961

<u>AGENCY</u>	<u>NUMBER OF COPIES</u>
Air Force Office of Scientific Research ATTN: Solid State Sciences Division Wash. 25, DC	3
Air Force Office of Scientific Research ATTN: Technical Library (SRGL) Wash. 25, DC	2
ASTIA (TIPCn) Arlington Hall Station Arlington 12, Va.	10
ARDC(RDRS) Andrews AFB Wash. 25, DC	1
EOAFRD ARDC 47 Cantersteen Brussels, Belgium	1
HQ USAF(AFDRT) Wash. 25, DC	1
ARL (Technical Library) Bldg. 450 Wright-Patterson AFB, Ohio	1
WADD(WWAD) Wright-Patterson AFB, Ohio	1
WADD (Metals & Ceramics Lab) Materials Central Wright-Patterson AFB, Ohio	
WADD (Physics Lab) Materials Central Wright-Patterson AFB, Ohio	1
WADD (Materials Information Branch) Materials Central Wright-Patterson AFB, Ohio	1
Institute of Technology (AU) Library MCLI-LIB, Bldg. 125, Area B Wright-Patterson AFB, Ohio	1

ARL (Metallurgy) AFRD Wright-Patterson AFB, Ohio	1
ARL (Physics, Solid State) AFRD Wright-Patterson AFB, Ohio	1
AFOSR (SRLTL) Holloman AFB, New Mexico	1
AFCRL (CRRELA) Laurence G. Hanscom Field, Bedford, Mass.	1
AFFTC (FTCTL) Edwards AFB, California	1
AEDC (AEOIM) Arnold Air Force Station, Tennessee	1
AFSWC (SWOI) Kirtland AFB, New Mexico	1
Commander Army Rocket & Guided Missile Agency ATTN: ORDXR-OTL Redstone Arsenal, Alabama	2
Office of the Chief of Research and Development Department of the Army ATTN: Scientific Information Washington 25, D. C.	1
Army Research Office (Durham) ATTN: CRD-AA-IP Box CM, Duke Station Durham, North Carolina	1
Commanding Officer Ordnance Materials Research Office (ATTN: PS&C Div.) Watertown Arsenal Watertown 72, Massachusetts	1
Commanding Officer Watertown Arsenal ATTN: Watertown Arsenal Labs, Tech Reports Section Watertown 72, Massachusetts	1
Commander Signal Corps Engineering Laboratory ATTN: SIGFM/EL-ROP Fort Monmouth, New Jersey	1

Director US Naval Research Laboratory ATTN: Library Wash. 25, DC	1
Department of the Navy Office of Naval Research ATTN: Code 423 ATTN: Code 421 Wash. 25, DC	2
Officer in Charge Office of Naval Research Navy No. 100 Fleet Post Office New York, New York	1
Commanding Officer Naval Radiological Defense Laboratory San Francisco Naval Shipyard San Francisco 24, California	1
Dr. D. F. Bleil Associate Technical Director for Research US Naval Ordnance Lab White Oak, Silver Spring, Maryland	1
National Aeronautics & Space Agency ATTN: Library 1520 H St., N. W. Wash. 25, DC	1
Ames Research Center (NASA) ATTN: Tech Library Moffett Field, California	1
High Speed Flight Station (NASA) ATTN: Tech Library Edwards AFB, California	1
Langley Research Center (NASA) ATTN: Tech. Library Langley AFB, Virginia	1
Lewis Research Center (NASA) ATTN: Tech Library 21000 Brookpark Road Cleveland 35, Ohio	1
Wallops Station (NASA) ATTN: Tech Library Wallops Island, Virginia	1

Division of Research US Atomic Energy Commission Division Office Washington 25, D. C.	1
US Atomic Energy Commission Library Branch Tech Information Div., ORE P.O. Box #E Oak Ridge, Tennessee	1
Major John Radcliffe ANP Office US Atomic Energy Commission Washington 25, D. C.	1
Oak Ridge National Laboratory ATTN: Central Files Post Office Box P Oak Ridge, Tennessee	1
Brookhaven National Laboratory ATTN: Research Laboratory Upton, Long Island, New York	1
Argonne National Laboratory ATTN: Librarian 9700 South Cass Avenue Argonne, Illinois	1
Document Custodian Los Alamos Scientific Laboratory P. O. Box 1663 Los Alamos, New Mexico	1
Ames Laboratory Iowa State College P. O. Box 14A, Station A Ames, Iowa	1
Knolls Atomic Power Laboratory ATTN: Document Librarian P.O. Box 1072 Schenectady, New York	1
National Science Foundation 1901 Constitution Avenue., N. W. Washington 25, D. C.	1
National Bureau of Standards Library Room 203, Northwest Building Washington 25, D. C.	1

Director Office of Technical Services Department of Commerce Technical Reports Branch Washington 25, DC	1
Chairman Canadian Joint Staff (DRB/DSIS) 2450 Massachusetts Avenue, N. W. Washington, DC	1
Defense Research Member Canadian Joint Staff ATTN: Mr. H. C. Oatway Director of Engineering Research Defense Research Board Ottawa, Canada	1
Institute of the Aeronautical Sciences ATTN: Librarian 2 East 64th Street New York 21, New York	1
RAND Corporation 1700 Main Street Santa Monica, California	2