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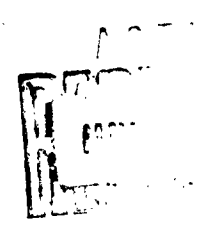
ANALYSIS OF CRITERION RELATIONSHIPS FOR LIQUIDS BOILING IN TUBES

UTOCHENIE KRITERIAL'NYKH ZAVISIMOSTEI PRI KIPENII ZHIDKOSTEI
V TRUBAKH

IZV. VYSSH. UCHEBN. ZAVEDENII, ENERGETIKA, (5), 108-114, 1959, U.S.S.R.

By

I.I.Sagan'



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Analysis of criterion relationships for
liquids boiling in tubes

I.I. Sagan'

Izv. Vyssh. Uchebn. Zavedenii, Energetika, (5), 108-114, 1959, USSR

The boiling process is a complex process which has as yet not been fully studied. Owing to the great complexity of the heat transfer process in boiling, there are as yet no firmly established criteria and consequently no universally accepted relationships which could be used for all cases of boiling liquids and solutions in the absence of experimental data.

For generalising experimental data relating to boiling a number of criterion equations have been put forward. The better known of these are the equations of S.S. Kutateladze (1), G.N. Kruzhilin (2), M.A. Kichigin - N.Y. Tobilevich (3) and V.I. Tolubinskii (4).

The equations of V.I. Tolubinskii and those of M.A. Kichigin - N.Y. Tobilevich are the result of vast experimental material relating to the heat transfer process in boiling water and various solutions in tubes. In the resolution of the Science Session of the Commission on High Pressure Steam Research of the Academy of Science of the USSR and the Institute of Thermoenergetics of the Academy of Science of the Ukrainian SSR, made in 1951, it was pointed out that the formulae of M.A. Kichigin - N.Y. Tobilevich and those of V.I. Tolubinskii have certain practical advantages in comparison with the others. It was mentioned that until further special research is undertaken, it was impossible to express any decisive preference for the one or the other system. In generalising our experimental data, therefore, relating to the boiling process in highly concentrated sugar solutions in tubes, we used only the criterial equations of M.A. Kichigin - N.Y. Tobilevich and V.I. Tolubinsky.

The M.A. Kichigin - N.Y. Tobilevich equation

$$Nu = 3.25 \times 10^{-4} Pe^{0.6} Ga^{0.125} Kp^{0.7} \quad (1)$$

is recommended by authors for calculating evaporators and condensers.

The V.I. Tolubinskii equation

$$Nu = 54k^{0.6} Pr^{-0.3} \quad (2)$$

is recommended by the authors for determining the heat transfer coefficient α_p for horizontal and vertical evaporators.

Up to recent times there were no experimental data available relating to the heat transfer in the boiling process of highly concentrated sugar solutions, in tubes of large diameters, with optimum levels of the boiling liquid. For these conditions the validity of the above mentioned criterion relationships (1) and (2) have not yet been proved. For this reason we have carried out a special experimental investigation into the heat transfer in highly concentrated boiling sugar solutions, using a single tube evaporator with natural circulation and interchangeable steel heating tubes of 159/150, 95/87 and 57/48 mm in diameter, installed at the Grivan Sugar factory. The content of dry substances was varied from 0 to 86%, with the pressure varying from 0.4 to 1 atm. abs and the heat flow q varying from 5 to 90 thousand kcal/m².h., with a depth of immersion of the heating surface of up to 200%. In addition the kinematic viscosity in the experiments varied from 0.295×10^{-6} to 215×10^{-6} m²/sec

i.e. about 730 times and the Pr number varied from 1.72 to 1540 i.e. about 900 times.

In determining the relationship between the similarity criteria in heat transfer to boiling liquids, it is important to determine experimentally the effect of the separate physical properties of the boiling liquid on the heat transfer coefficient α_2 . The difficulty, however, is that as one of the properties changes the other properties vary as well.

The effect of viscosity on the heat transfer coefficient can be determined from the experimental data, obtained in the course of the investigation. The properties relating to the vapour phase (γ , ν) hardly vary. The physical constants σ , λ , c and γ for sugar solutions vary comparatively little. The main factor affecting the heat exchange process is the viscosity, which varies within wide limits (table 1) and, in fact, the viscosity is the basic factor determining the quantitative value of the non-dimensional criterion of the physical parameters i.e. Prandtl's number Pr.

Table 1 Some physical constants at $p = 0.4 \text{ atm. abs.}$

Name of constant	Units	Concentration in %		±%
		0	86	
Surface tension	kg/m	0.63×10^{-2}	0.759×10^{-2}	+ 20
Coefficient of thermal conductivity	$\frac{\text{kcal}}{\text{m} \cdot \text{h} \cdot \text{degree}}$	0.581	0.455	- 21
Specific gravity	kg/m^3	972	1394	+ 43
Thermal capacity	$\frac{\text{kcal}}{\text{kg} \cdot \text{degree}}$	1.0	0.633	- 36
Coefficient of kinematic viscosity	m^2/sec	0.376×10^{-6}	215×10^{-6}	+ 57000
Prandtl number	-	2.2	1540	+ 70000

On the basis of the then existing experimental data it was only possible to make an approximate assessment of the effect of viscosity on the heat transfer coefficient α_2 in a boiling liquid and, therefore, also only an approximate evaluation of the Ga power index in the M.A. Kichigin - N.Y. Tobilevich equation or the Pr index in the V.I. Tolubinskii equation, since the experiments were carried out in a narrow range of viscosity changes. For instance, in V.I. Tolubinskii's experiments the Pr number varied only from 1.7 to 100 and in N.Y. Tobilevich's experiments it varied from 0.7 to 170.

Comparing the experimental results of different authors, we observe different values for the power index of the Pr number. In the case of convective heat exchange in a non-boiling liquid the Pr index, in calculation formulae, is of the order of 0.33 to 0.43(5). In criterial equations relating to the heat transfer in boiling the Pr power index varies from + 0.21 [L.S. Sterman (6)] to - 0.5 [G.N. Kruzhilin (7)].

The relationship of the heat transfer coefficient α_2 to the coefficient of kinematic viscosity ν is shown in fig. 1. In this figure the results of our experiments are compared with the data of N.Y. Tobilevich (3), according to which $\alpha_2 \sim \nu^{-0.25}$. In our case $\alpha_2 \sim \nu^{-0.2}$ at atmospheric pressure and $\alpha_2 \sim \nu^{-0.18}$ at a pressure of 0.4 atm abs. According to V.I. Tolubinskii (4)

$\alpha_2 \sim \nu^{-0.3}$, whereas according to V.D. Popov (8) $\alpha_2 \sim \nu^{0.23}$ and according to A.F. Sorokin (9) $\alpha_2 \sim \nu^{0.4}$ to -0.5 .

Fig.1. Relationship of the heat transfer coefficient α_2 to the viscosity coefficient ν .

- 1 - the author's experiments, $p = 0.4$ atm.abs., $q = 40 \times 10^3$ kcal/m².h.
- 2 - N.Y. Tobilevich's experiments, $p = 1.0$ atm.abs., $q = 10 \times 10^3$ kcal/m².h.
- 3 - the author's experiments, $p = 1.0$ atm.abs., $q = 10 \times 10^3$ kcal/m².h.

Analysing the curves of fig.1, we can conclude that in the transfer of heat to boiling sugar solutions at a pressure $p < 1$ atm.abs. the ratio of α_2 to ν decreases slightly.

Taking into account the results obtained by plotting the relationship $\alpha_2 = f(\nu)$, we carried out a comparative approximation correction of the M.A. Kichigin - N.Y. Tobilevich and the V.I. Tolubinskii criterial equations, based on our experimental data. In doing so, we did not necessarily aim at obtaining a relationship valid only for working conditions specific to vacuum condensers and evaporators employed in the sugar industry, although it would be possible to do that. What we had in mind is to maintain or rather widen the sphere of applicability of these generalised relationships to a wider range of values, embracing a number of liquids with differing physical properties and boiling in a wider range of pressure variations.

The corrected or refined criterion relationship of M.A. Kichigin - N.Y. Tobilevich $\frac{Nu}{Ga^{0.09} K_p^{0.77}} = f(Pr)$, based on our experimental data, is

shown in fig.2. Although the tested sugar solutions differ considerably in their physical properties, nevertheless the experimental points appear to be grouped quite satisfactorily along the mean criterion line with a scatter of $\pm 15\%$. If the same data are generalised to the M.A. Kichigin - N.Y. Tobilevich criterion system without altering the power indices, then the scatter of the points relative to the mean line exceeds +49 and -28%.

Fig.2. Generalisation of the author's experimental data with the corrected M.A. Kichigin - N.Y. Tobilevich criterion relationship

Table in figure 2

Liquid	Sugar content %	P atm.abs.	Outside diameter d mm	Notation
Water	0	1.0	48	○
"	0	1.0	87	⊙
"	0	0.4	87	⊙
Sugar solution	60	1.0	48	⊙
" "	60	1.0	87	⊙
" "	60	1.0	150	⊙
" "	60	0.4	48	⊙
" "	60	0.4	87	⊙

With a view to confirming the validity of the corrected M.A. Kichigin - N.Y. Tobilevich equation for a wider range of liquids, extensive experimental material was used drawn from different authors. The generalisation of these experimental results, relating to boiling liquids widely differing in their physical properties, is shown in the same coordinates

$\frac{Nu}{Ga^{0.09} Kp^{0.77}} = f(Pe)$ in fig.3. The scatter of the experimental points

relative to the mean line is within the limits of $\pm 15\%$. The result of generalising all the above experimental data, including our own, can be expressed by a corrected, non-dimensional equation of the following type

$$Nu = 2.71 \times 10^{-4} Pe^{0.6} Ga^{0.09} Kp^{0.77}$$

which, after converting, will take the following form

$$\alpha_2 = 2.71 \times 10^{-4} \frac{g^{0.09} \lambda^{0.4} c^{0.6} p^{0.77} \gamma^{0.28}}{n^{0.6} \gamma''^{0.6} \sigma^{0.45} \nu^{0.18}} q^{0.6} \left[\frac{\text{kcal}}{\text{m}^2 \cdot \text{h} \cdot \text{degree}} \right]$$

In this formula, in view of the narrow range of pressure variations and since $\gamma > \gamma''$, it was assumed that $\gamma - \gamma'' = \gamma$, in order to simplify the calculations.

Fig.3. Generalisation of the experimental results of other authors with the corrected M.A. Kichigin - N.Y. Tobilevich criterion relationship

Table in fig.3.

Author	Liquid	Sugar content %	P atm.abs.	Notation
N.Y. Tobilevich	NaCl solution	20	1.0	①
"	Water	0	1.0	②
"	Sugar solution	25	1.0	③
"	" "	30	1.0	④
"	" "	47	1.0	⑤
"	" "	60	1.0	⑥
"	" "	65	0.2	⑦
Y.I. Tolubinskii	Water	0	0.7	⑧
"	"	0	0.4	⑨
N.Y. Tobilevich	Sugar solution	25	1.46	⑩
N.G. Yampol'skii	" "	65	0.24	⑪
A.G. Bondar'	NaOH solution	5	1.0	⑫
"	" "	20	1.0	⑬
"	" "	40	0.62	⑭
R.Y. Ladiev	NH ₄ NO ₃ solution	10	1.0	⑮
"	" "	40	1.0	⑯
"	" "	60	1.0	⑰

It follows from the above that the corrected M.A. Kichigin - N.Y. Tobilevich criterion formula satisfactorily generalises the experimental data relating to a large group of substances and is valid for rather a wide range of variations of the basic factors affecting the heat transfer process in boiling liquids.

The corrected or refined criterion system shows rather less scatter of the experimental points, relative to the concentration, than the previous one. However, for other liquids it cannot be considered reliable and would require additional verification for conditions not applying to the generalised experiments.

The V.I. Tolubinskii criterion equation has attracted considerable interest owing to its simple form. Fig.4 shows the generalisation of the author's experimental data with the V.I. Tolubinskii corrected criterion relationship $NuPr^{0.2} = f(K)$. The experimental points are distributed along the mean line with a scatter of $\pm 20\%$. If the same data are generalised to the criterion system with the Pr power index taken as 0.3, then the deviation of the points from the mean line will exceed +56 and -36%. Generalisation of experimental results of other authors to the V.I. Tolubinskii refined criterion system, has shown that the deviation of the points from the mean line amounts to -17 and +30%.

Fig.4. Generalisation of the author's experimental data with the corrected V.I. Tolubinskii criterion relationship

Table in fig.4.

Liquid	Sugar content %	P atm.abs.	d mm	Notation
Water	0	1.0	87	⊙
"	0	1.0	48	●
"	0	0.4	87	⊙
Sugar solution	60	1.0	150	●
" "	60	1.0	87	⊙
" "	60	0.4	150	⊙
" "	60	0.4	87	●
" "	60	0.4	48	●
" "	75	1.0	150	⊙

The result of generalising all the experimental data can be expressed by a corrected non-dimensional equation of the following type

$$NuPr^{0.2} = 41.3K^{0.5}$$

or

$$\alpha_2 = 1.4 \frac{1.2 \gamma^{0.3} \mu^{0.06}}{n^{0.6} \gamma_0^{0.66} c^{0.2} d^{0.5} \nu^{0.2}} q^{0.6} \left[\frac{\text{kcal}}{\text{m}^2 \cdot \text{h} \cdot \text{degree}} \right]$$

When comparing the generalised results of the two criterion systems, we see that a greater deviation of the experimental points from the mean line is obtained when using V.I. Tolubinskii's criterion equation. The greater deviation of the experimental data, from the line corresponding to this criterion equation, is probably due to an inaccurate evaluation of d_0U , since experimental information relating to the value of this term for different liquids and pressures is as yet somewhat scanty. Both the author and V.I. Tolubinskii have used values of d_0U relating to water at pressures of 1 to 5 atm.abs., carbon tetrachloride, sodium chloride solutions and glycerine at atmospheric pressure. As far as other liquids are concerned, there are as yet no experimental data available for them relating to the d_0U value for atmospheric or any other pressures. In order to develop further, therefore, the given criterion system, it will be necessary to carry out special

preliminary experiments for ascertaining the true values of d_0U for various liquids and pressures.

Conclusions

1. A study was made of the heat exchange process in boiling highly concentrated sugar solutions with natural circulation and interchangeable heating tubes of 159/150, 95/87 and 57/48 mm in diameter, the sugar content being 0,60,75,82 and 86%, the pressure varying from 0.4 to 1.0 atm.abs. with a depth of immersion of the heating surface of up to 200%.

2. The experiments, carried out for a sufficiently wide range of variations of kinematic viscosities ν (from 0.295×10^{-6} to 215×10^{-6} m²/sec), allowed of ascertaining the effect of the viscosity on the heat transfer coefficient α_2 and of determining the values of the Ga and Pr power indices in the M.A. Kichigin-N.Y. Tobilevich and in the V.I. Tolubinskii criterial systems.

3. The new experimental data made it possible to obtain a corrected criterion equation for the M.A. Kichigin-N.Y. Tobilevich system

$$Nu = 2.71 \times 10^{-4} Pe^{0.6} Ga^{0.09} Kp^{0.77}$$

and a corrected criterion formula for the V.I. Tolubinskii system

$$NuPr^{0.2} = 41.3 K^{0.6}$$

and to extend the applicable range of these formulae for Prandtl numbers ranging from 0.7 to 1540.

4. Since the M.A. Kichigin-N.Y. Tobilevich corrected criterion system yields a smaller error in generalising experimental data relating to a large group of experimental substances and is valid in a wide variational range of factors affecting the heat transfer in boiling liquids, its application should be given preference, at least at the present stage of progress, in the study of the heat exchange processes in boiling.

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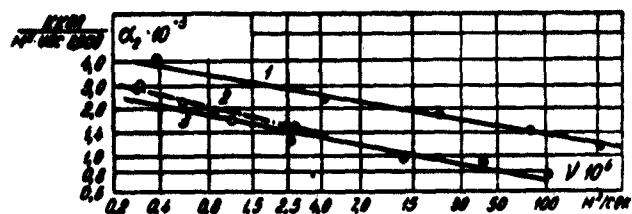


Рис. 1. Зависимость коэффициента теплоотдачи α_2 от коэффициента кинематической вязкости ν ;

1 — опыты автора, $p = 0.4$ атм, $q = 40 \cdot 10^3$ ккал/м²·час;
2 — Н. Ю. Тобилевича, $p = 1.0$ атм, $q = 10 \cdot 10^3$ ккал/м²·час;
3 — автора, $p = 1.0$ атм, $q = 10 \cdot 10^3$ ккал/м²·час

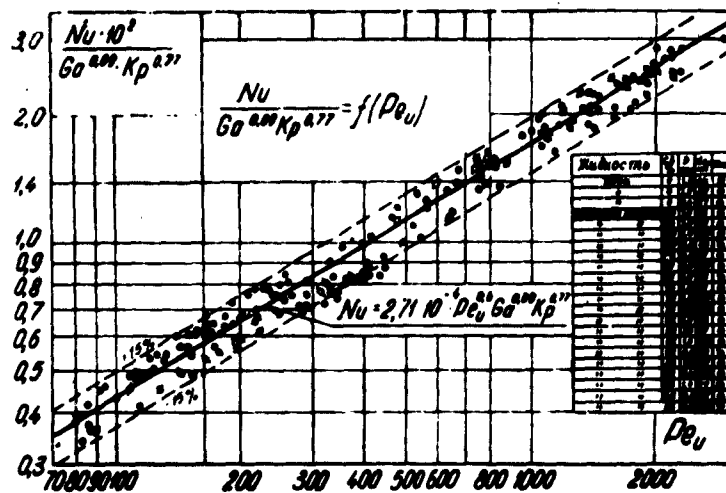


Рис. 2. Обобщение опытных данных автора в уточненной критериальной зависимости М. А. Кичигина — Н. Ю. Тобилевича

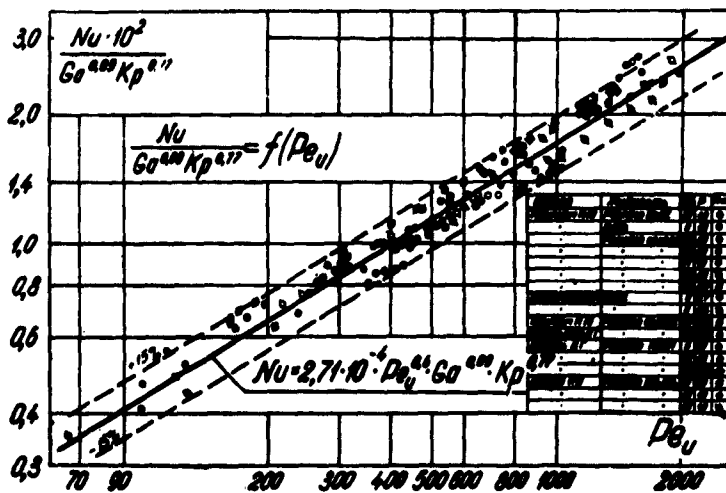


Рис. 3. Обобщение опытных данных других исследователей в уточненной критериальной зависимости М. А. Кичигина — Н. Ю. Тобилевича

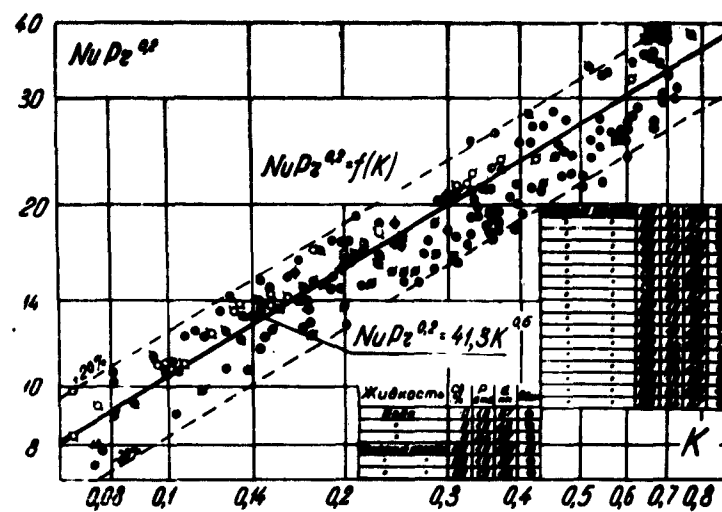


Рис. 4. Обобщение опытных данных автора в уточненной критериальной зависимости В. И. Толубинского

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