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ONR ltr, 4 May 1977

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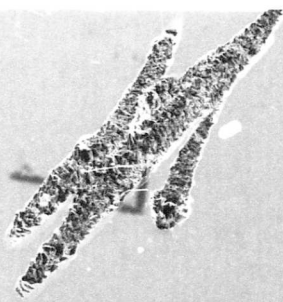
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HUGHES TOOL COMPANY · AIRCRAFT DIVISION
Culver City, California

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HTC-AD 65-15

Volume III

APPENDIXES G AND H

SUMMARY TECHNICAL REPORT
ROTOR/WING CONCEPT STUDY

September 1965

Prepared by Robert E. Head

Contract Number: Nonr-4588(00)
Authority: NR 212-162/12-8-64



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HUGHES TOOL COMPANY -- AIRCRAFT DIVISION
Culver City, California

FOREWORD

This report presents the results of whirlstand and wind tunnel tests of a one-sixth scale model of the Rotor/Wing high-speed VTOL aircraft. The main body of the report presented as Volume I, discusses highlights of the test results, includes a discussion of the application of the test results to full-scale, and describes the characteristics of such an aircraft. Volume II, which includes Appendixes A through F, contains detailed analyses and test data from the model research program. Volume III, which includes Appendixes G and H, contains a collection of the detailed drawings of the model and the stress analysis used in the design.

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APPENDIX H - STRUCTURAL ANALYSIS	III-26

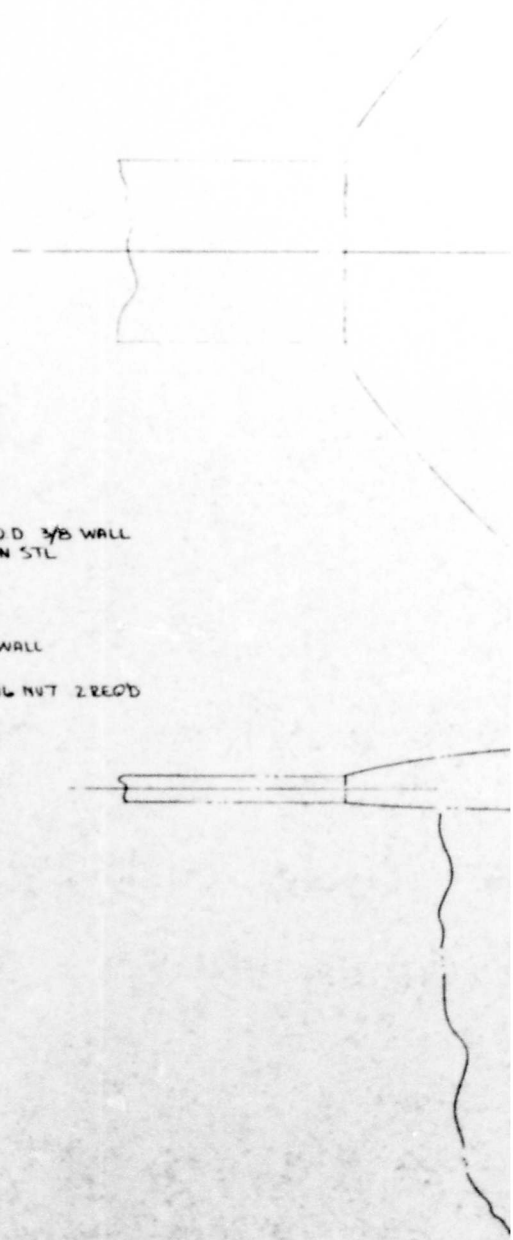
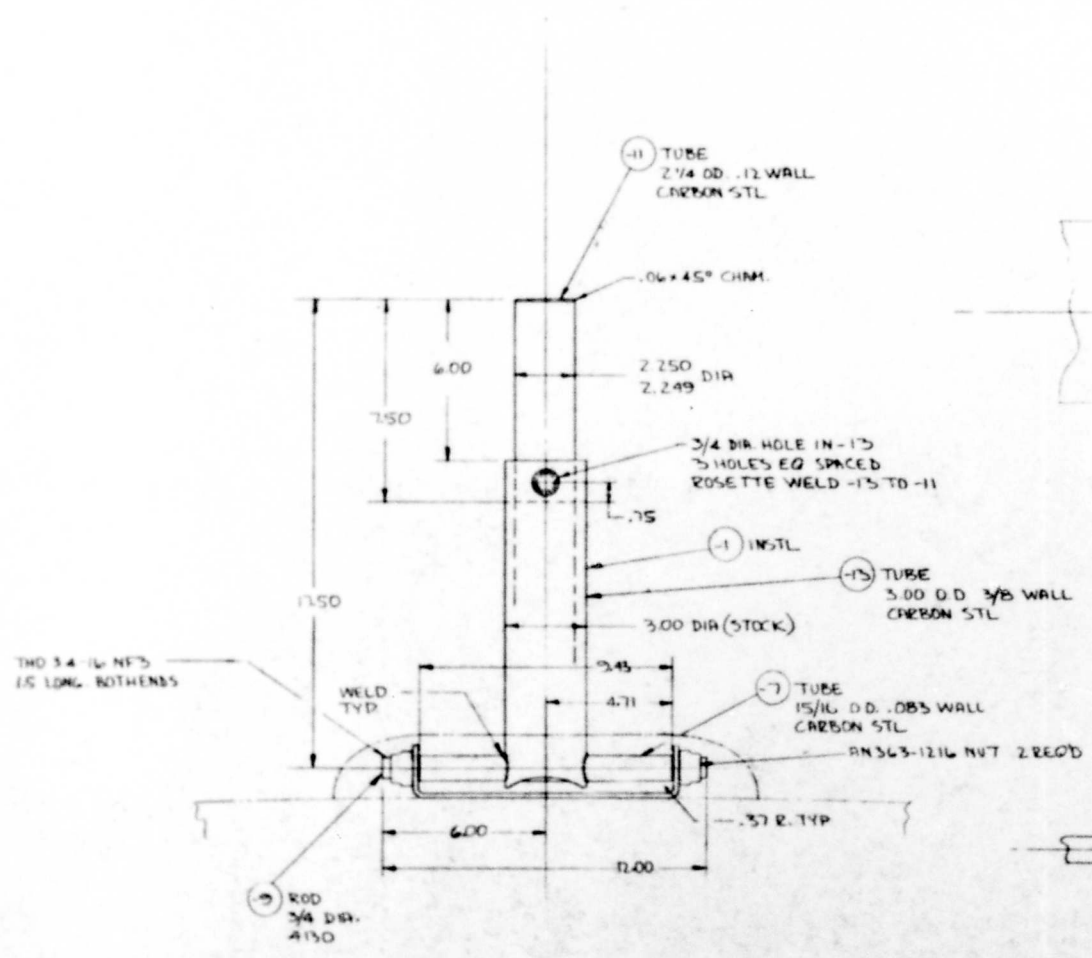
APPENDIX G
ROTOR/WING MODEL DRAWINGS

APPENDIX G
ROTOR/WING MODEL DRAWINGS

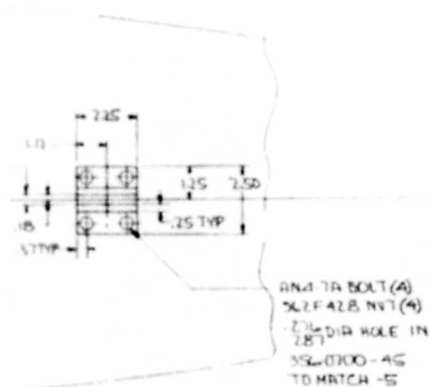
This Appendix includes the layout drawings for the major components of the model, and the detail drawings for the actual components. The basic layout drawings for the model may be seen in Volume I as Figures 9, 10, and 11. Drawings included herein are:

<u>Drawing Number</u>	<u>Sheet</u>	<u>Title</u>
356-0602	1	Mast Assembly
356-0603	1	Image Strut Assembly
356-0700	1, 2	Fuselage
356-0800	1, 2	Empennage*
356-0801	1, 2	Empennage
356-0900	1, 2	Rotor
356-0902	1	Spoiler
356-0903	1	Empennage
356-1000	1, 2, 3	Controls
356-1001	1	Swashplate
356-1002	1	Swashplate
356-1003	1	Swashplate
356-1005	1	Swashplate
356-1006	1	Swashplate
356-1100	1, 2	Propulsion System
356-1501	1	Tachometer

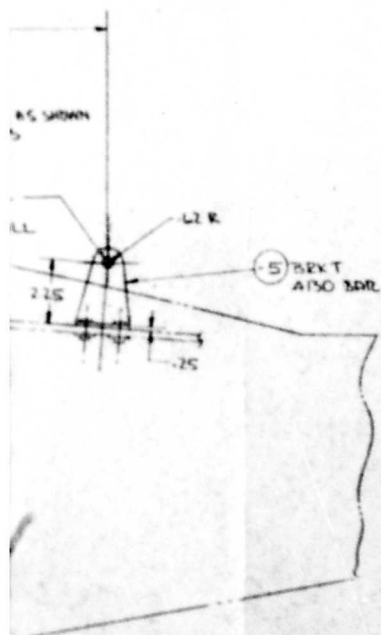
*An engine nacelle was included in the drawing, but it was not constructed.



REVISIONS				
REV	E.O.S.	DESCRIPTION	DATE	APP'D



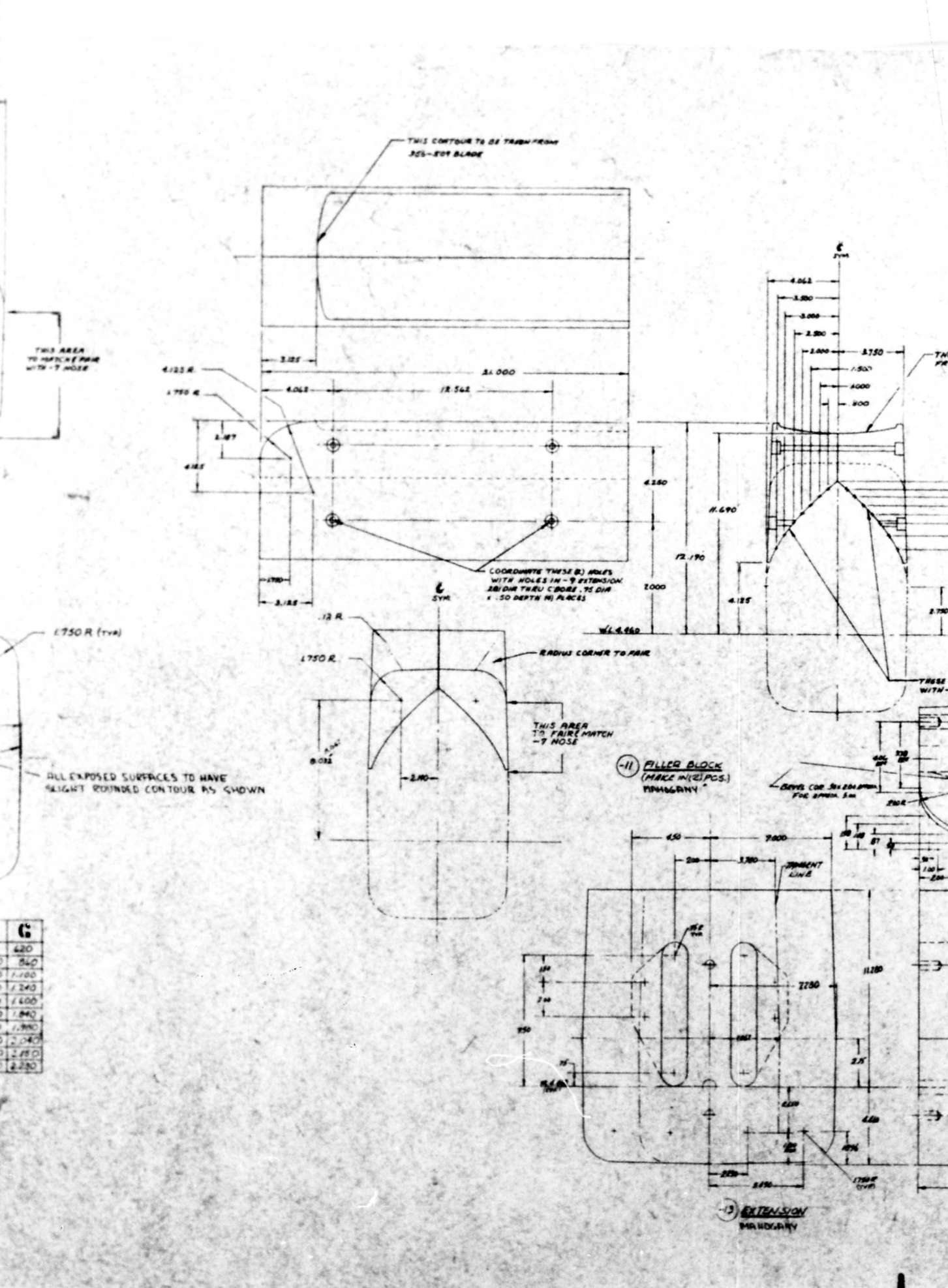
6.
TINY



356-0603

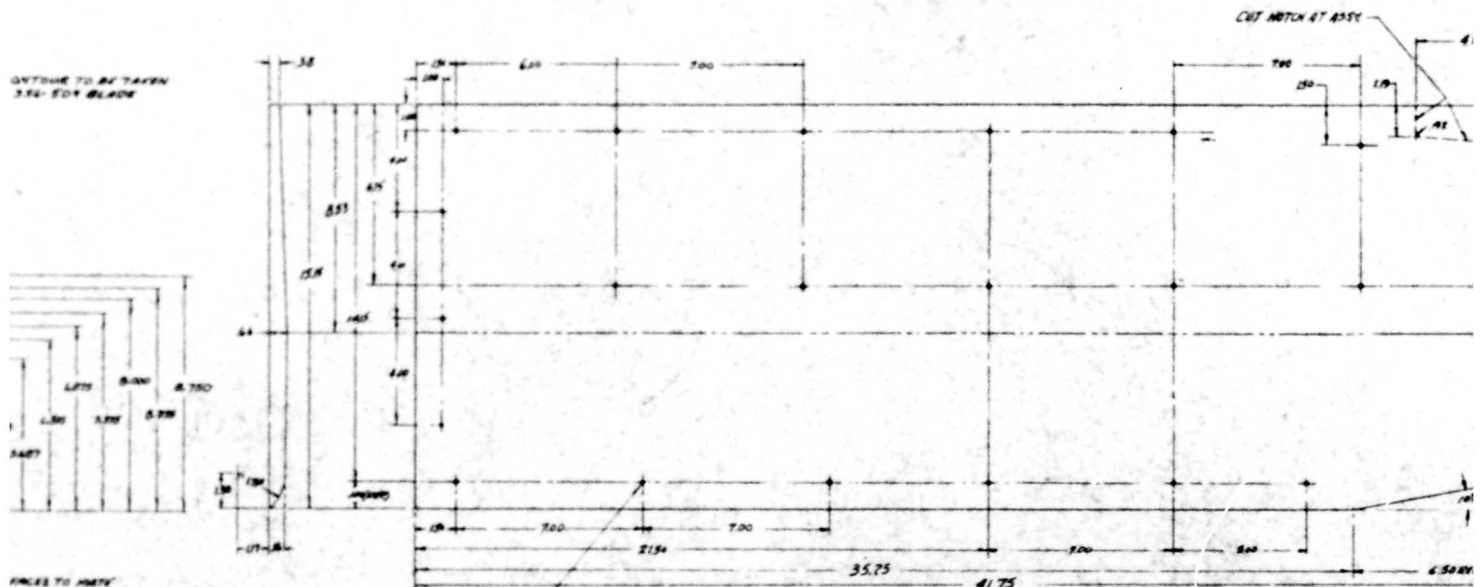
REV	E.O.S.	DESCRIPTION	DATE	APP'D

IMAGE MAST ASSY/1
 ONE ROTOR WING
 WIND TUNNEL MODEL
 356-0603
 06/03



G
0.420
0.540
0.7100
0.7240
0.7400
0.7800
0.7900
0.8040
0.8150
0.8300

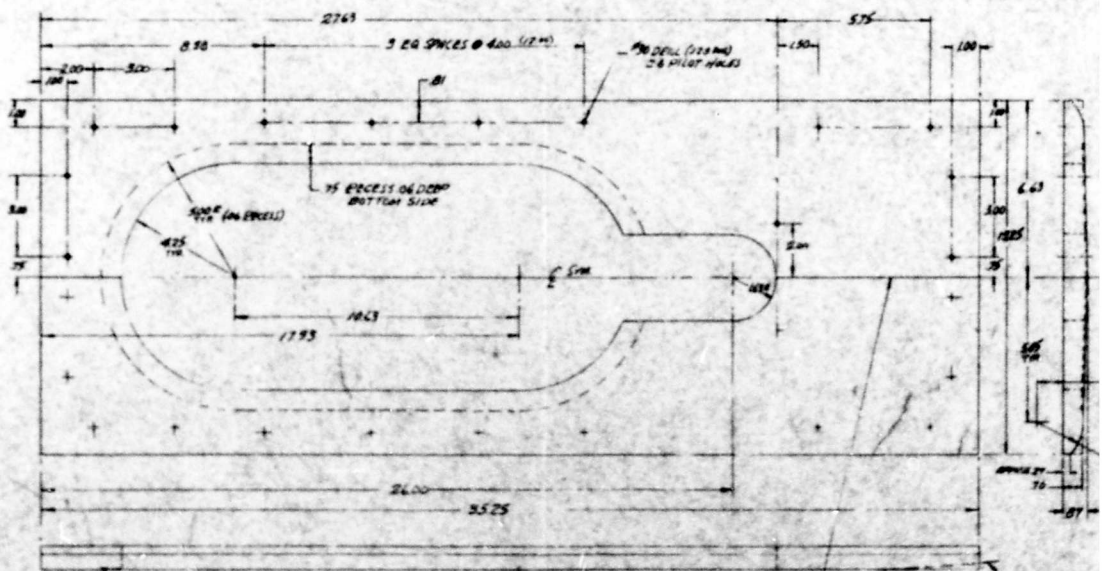
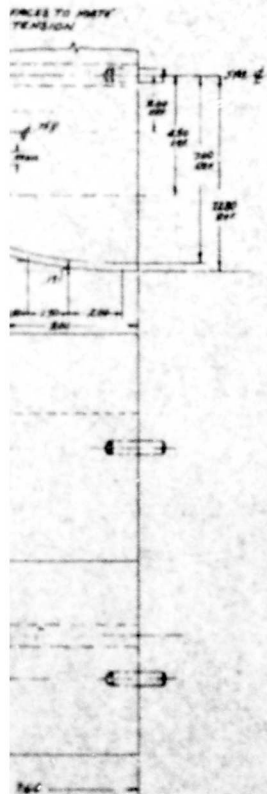
OUTLINE TO BE TAKEN
3.74 - FWD BLADE



1/2" DEEL (125 DIA)
23 PILOT HOLES

(17) SIDE PANEL - FWD. LH. SAGAW

(18) RH OPPOSITE
MAHOGANI



(15) BOTTOM (MADE IN U.S.A.) BUTT OF
FWD
MAHOGANI

FRAMED LH
BOTTOM 3/4
7.65 888 A
(APPROX. 80)

REVISIONS				
REV	DATE	DESCRIPTION	BY	CHK

TAP - #4-11
#1 - 25

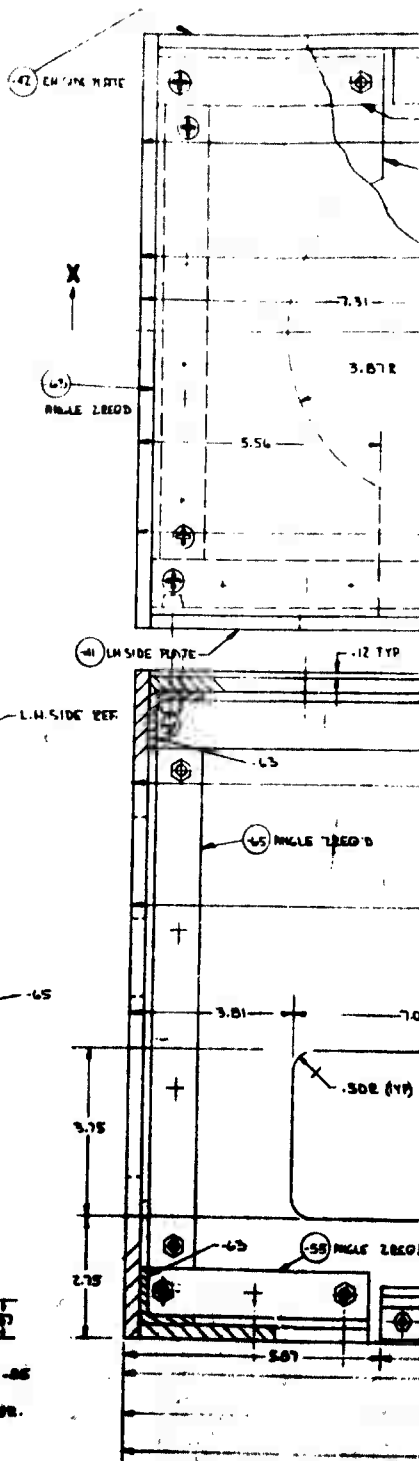
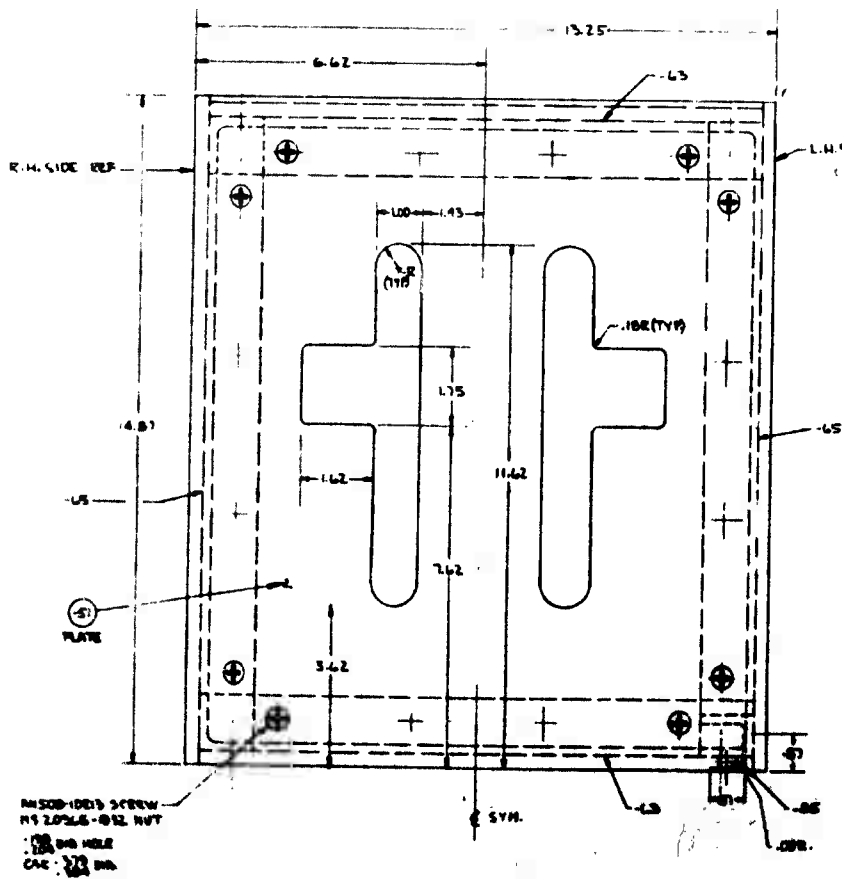
Support

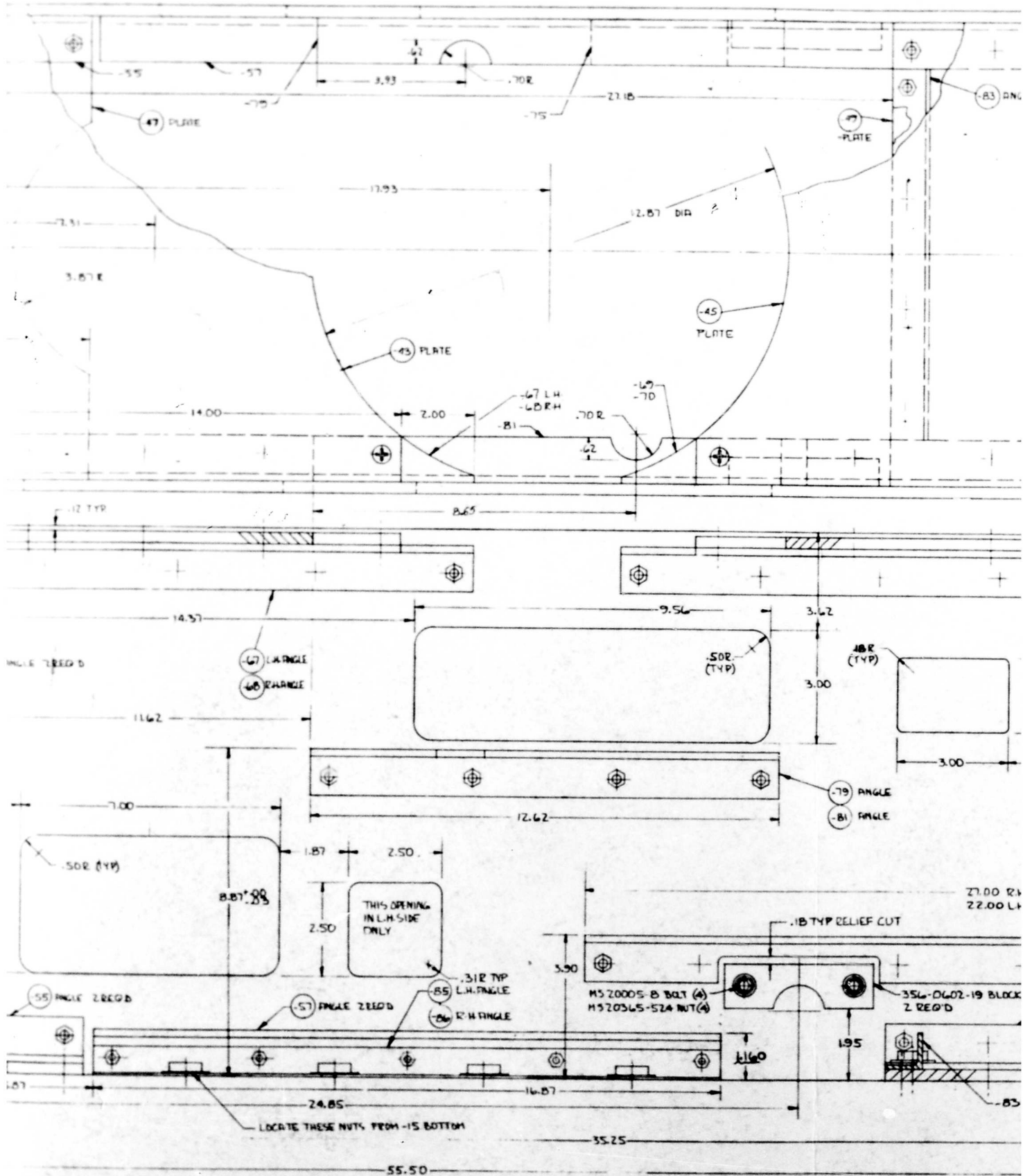


35L-0700

REV	DATE	DESCRIPTION	BY	CHK

MUST ASSEY USED IN APPLICATION	QTY 0000	PART NAME PART NO PART QTY PART UNIT	DRAWN CHECKED APPR DATE	FUSELAGE - FAR UTILITY WING WIND TUNNEL MODEL	35L-0700
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SECTION X-X

REV	DATE

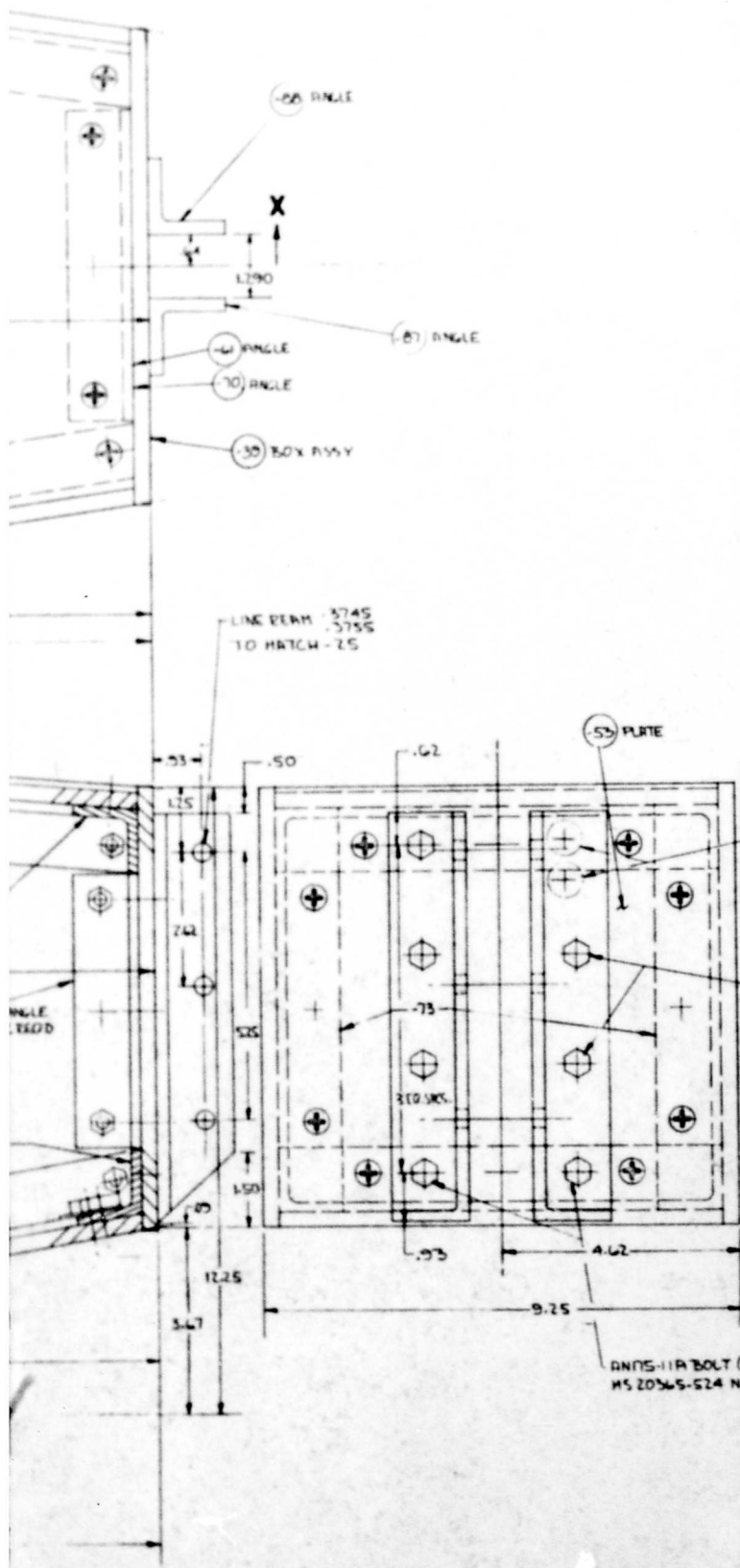
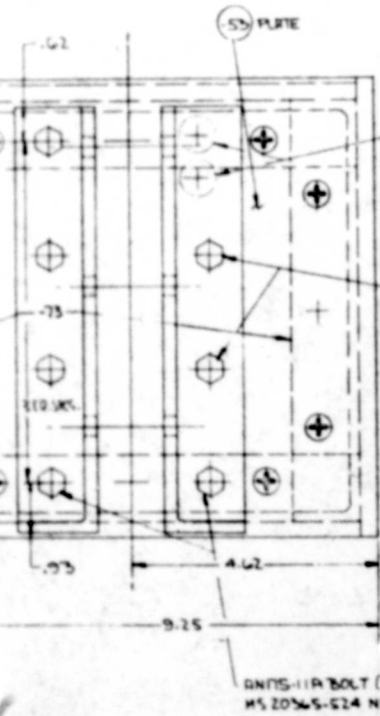


PLATE MAT (EXCEPT -51-53) 3/16 2024-T4.
 -51-53 PLATE 5/16 2024-T4.
 ALL ANGLES (EXCEPT -83-B5-B6-87-88)
 ARE 3/16 x 1/4 x 1/4 2024-T4.
 -83 ANGLE IS 1/8 x 1 x 1 2024-T4.
 -B5-B6 ANGLE MADE OF .06 2024-O. HT TO T4.
 -87-88 ANGLE: 1/4 x 1/2 x 1/2 2024-T4

REV	DATE	BY	CHKD

REVISIONS					
REV	Q.D.	DESCRIPTION	APP'D	DATE	INITIALS

(B) ANGLE



DRN175-10A BOLT (4)

DRN175-11A BOLT (5)
MS 20% S-524 NUT (7)

PLATE MAT (EXCEPT -51-53) 3/16 2024-T4.
 -51-53 PLATE 3/16 2024-T4.
 ALL ANGLES (EXCEPT -B3-B5-B6-B7-B8)
 FREE 3/16 x 1/4 x 1/4 2024-T4.
 -B3 ANGLE 1/8 x 1 x 1 2024-T4.
 -B5-B6 ANGLE MADE OF .06 2024-O. HT TO T4.
 -B7-B8 ANGLE: 1/4 x 1/2 x 1 1/2 2024-T4

356-0700

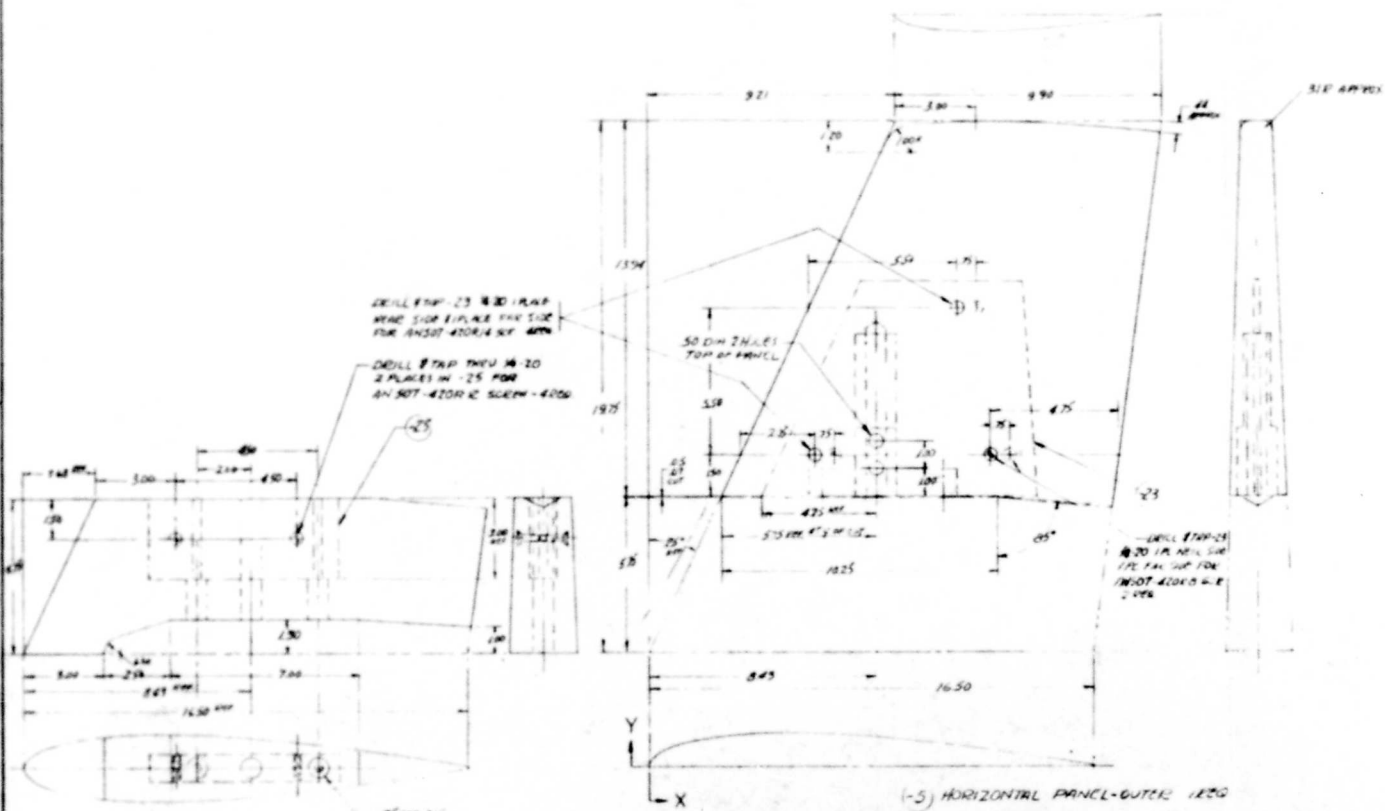
FUSELAGE - ONR MOTOR-WING WIND TUNNEL MODEL				356-0700	
REV	Q.D.	DESCRIPTION	APP'D	DATE	INITIALS

D

C

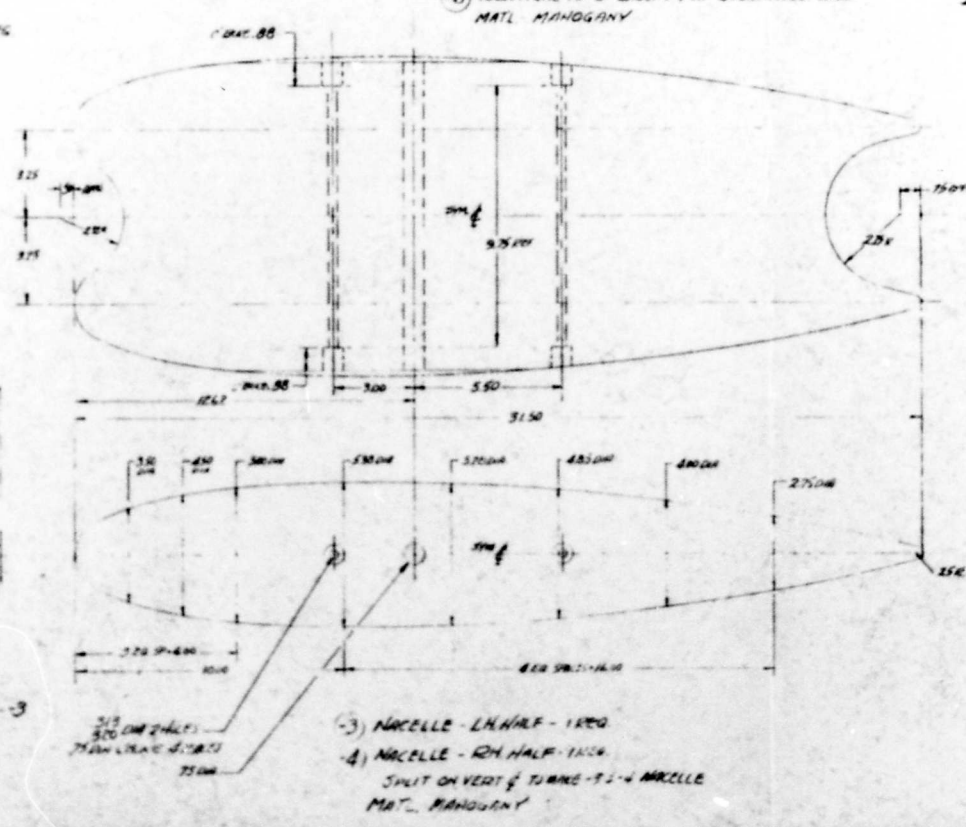
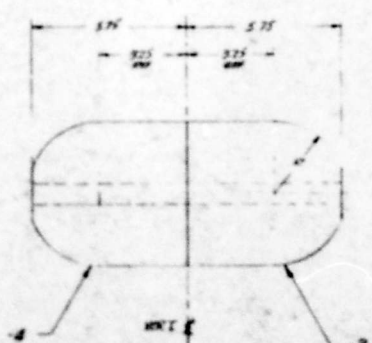
B

A



(7) HORIZONTAL PANEL-INSIDE - 1/2 IN
MATERIAL MANOGANY

(-5) HORIZONTAL PANEL-OUTSIDE - 1/2 IN
(-6) IDENTICAL TO -5 EXCEPT FOR SIDE FLANGES - 1/2 IN
MATERIAL MANOGANY

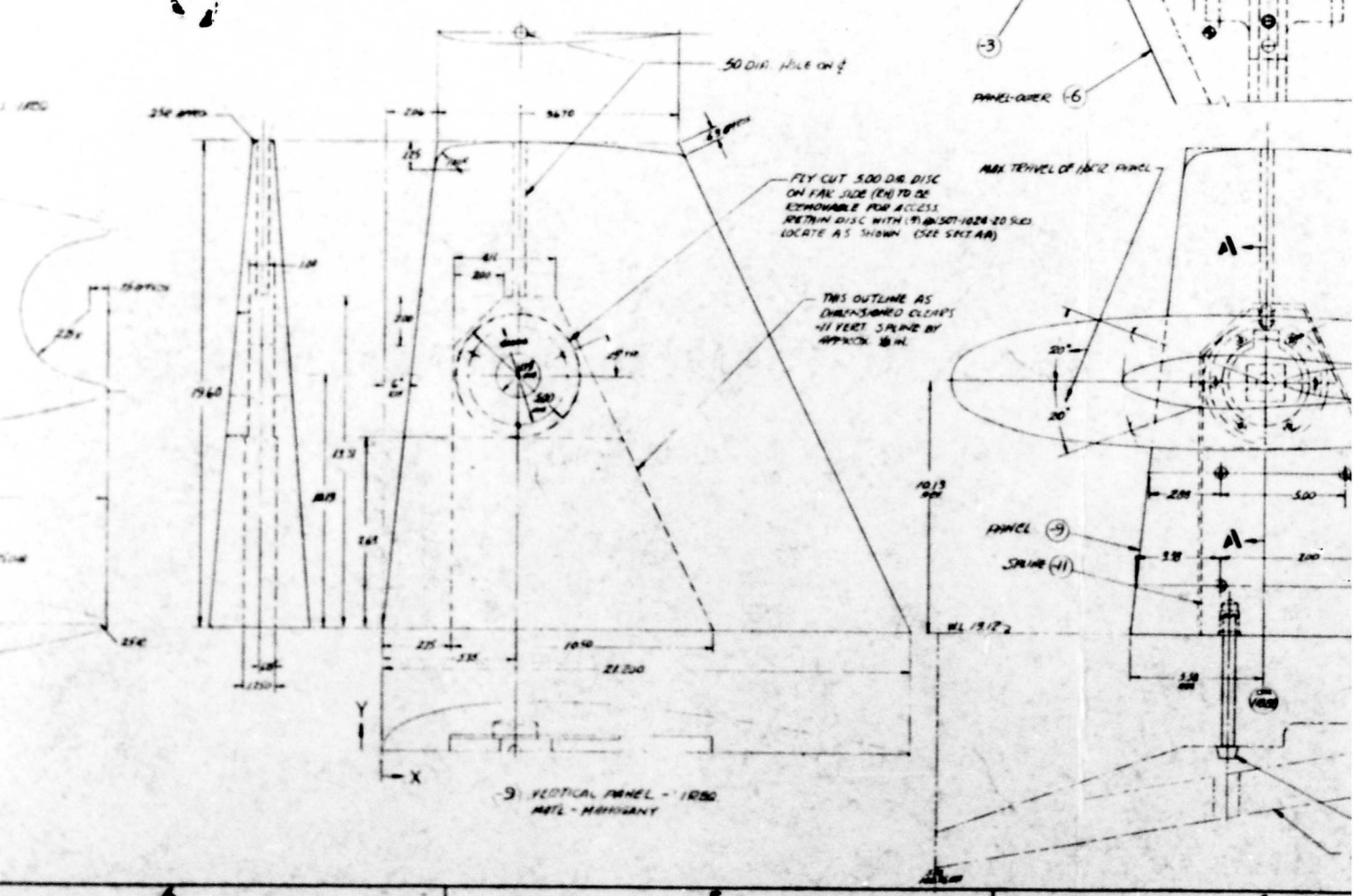
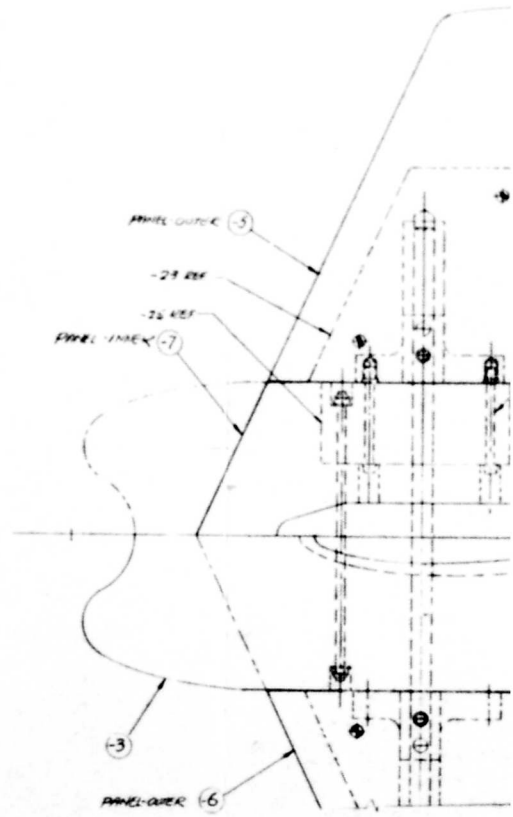


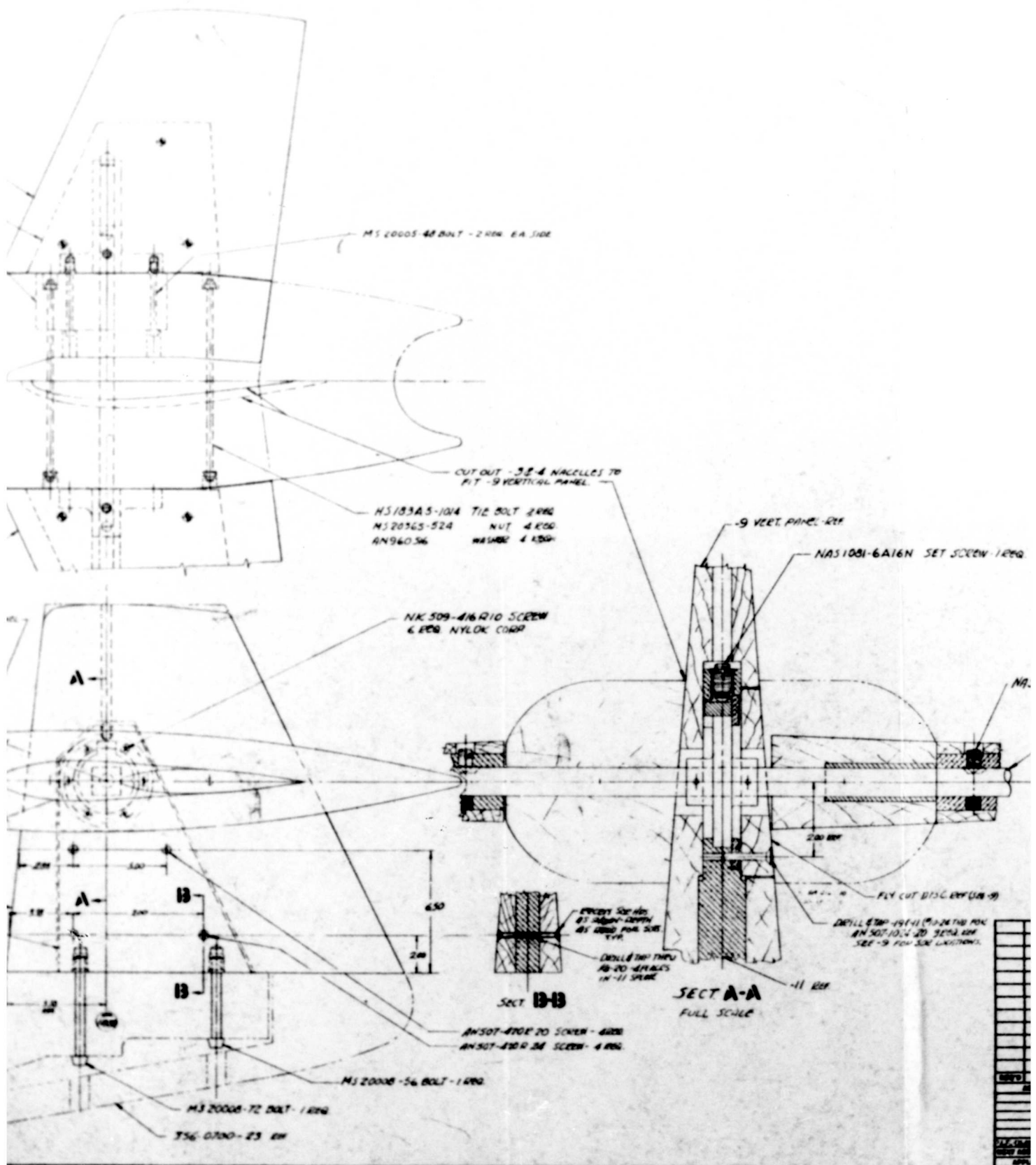
(-3) NACELLE - LH HALF - 1/2 IN
(-4) NACELLE - RH HALF - 1/2 IN
SPLIT ON VERT & TURNING - 1/2 IN NACELLE
MATERIAL MANOGANY

ORDINANCES

HORIZONTAL SURFACE					
ABOUT D.A. 80			TIP (1-8-20)		
AREA 0018		AREA 0012			
X	Y	X	Y	X	Y
O	O	O	O	O	O
175	306	288	307	187	
27	512	370	247	189	
37	821	341	491	251	
47	1138	364	741	414	
57	1450	360	990	459	
67	1767	109	481	329	
77	2080	21	980	340	
87	2397	221	2407	399	
97	2710	132	190	394	
107	3027	176	360	376	
117	3340	103	610	374	
127	3657	34	360	431	
137	3970	70	690	361	
147	4287	247	30	241	
157	4600	230	270	184	
167	4917	43	1401	07	
177	5230	278	390	203	
187	5547	277	27	17	

VERTICAL SURFACE					
ABOUT 0-2128			TIP (1-8-20)		
AREA 0019		AREA 0009			
X	Y	X	Y	X	Y
O	O	O	O	O	O
125	245	674	221	197	
229	330	877	242	190	
333	1068	1195	484	258	
437	1590	1410	725	301	
541	2109	1571	967	319	
645	2630	1785	1251	382	
749	3140	1924	1514	414	
853	3650	1996	2408	491	
957	4160	204	290	485	
1061	4670	947	360	411	
1165	5180	177	480	384	
1269	5690	351	560	351	
1373	6200	231	639	244	
1477	6710	82	776	90	
1581	7220	458	870	105	
1685	7730	249	367	030	
1789	8240	245	640	210	
1893	8750				





MS 2000S 4R BOLT - 2 REQ. EA. SIDE

CUT OUT - 3/8" X 4" NACELLES TO FIT - 9 VERTICAL PANEL

H5183A5-1014 TIE BOLT 2 REQ
MS 2016S-524 NUT 4 REQ
AN940.36 WASHER 4 REQ

NK 509-416 R10 SCREW 6 REQ NYLON CORR

9 VERT. PANEL - REF

NAS1001-6A16N SET SCREW 12 REQ

A

NA

6.50

FLY CUT DISC. ENF (ON 9)

DRILL 6.75 DIA (6.75-26 TAP FOR AN 507-10, 20, 30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150, 160, 170, 180, 190, 200, 210, 220, 230, 240, 250, 260, 270, 280, 290, 300, 310, 320, 330, 340, 350, 360, 370, 380, 390, 400, 410, 420, 430, 440, 450, 460, 470, 480, 490, 500, 510, 520, 530, 540, 550, 560, 570, 580, 590, 600, 610, 620, 630, 640, 650, 660, 670, 680, 690, 700, 710, 720, 730, 740, 750, 760, 770, 780, 790, 800, 810, 820, 830, 840, 850, 860, 870, 880, 890, 900, 910, 920, 930, 940, 950, 960, 970, 980, 990, 1000

EXCEPT SIZE AND BT 2000-DEPTH AS SHOWN FOR THIS TYPE

DRILL 6.75 DIA (6.75-26 TAP FOR AN 507-10, 20, 30, 40, 50, 60, 70, 80, 90, 100, 110, 120, 130, 140, 150, 160, 170, 180, 190, 200, 210, 220, 230, 240, 250, 260, 270, 280, 290, 300, 310, 320, 330, 340, 350, 360, 370, 380, 390, 400, 410, 420, 430, 440, 450, 460, 470, 480, 490, 500, 510, 520, 530, 540, 550, 560, 570, 580, 590, 600, 610, 620, 630, 640, 650, 660, 670, 680, 690, 700, 710, 720, 730, 740, 750, 760, 770, 780, 790, 800, 810, 820, 830, 840, 850, 860, 870, 880, 890, 900, 910, 920, 930, 940, 950, 960, 970, 980, 990, 1000

SECT B-B

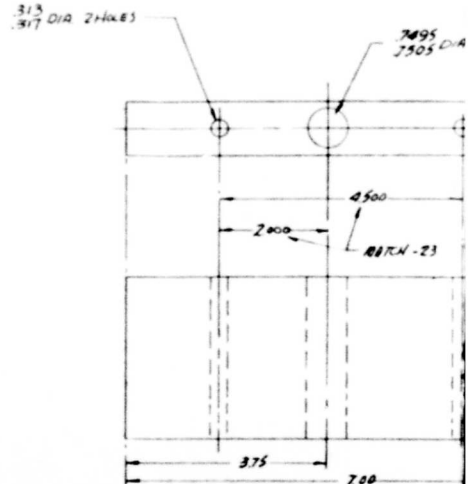
SECT A-A
FULL SCALE

AN507-410R 20 SCREW - 4 REQ
AN507-410R 36 SCREW - 4 REQ

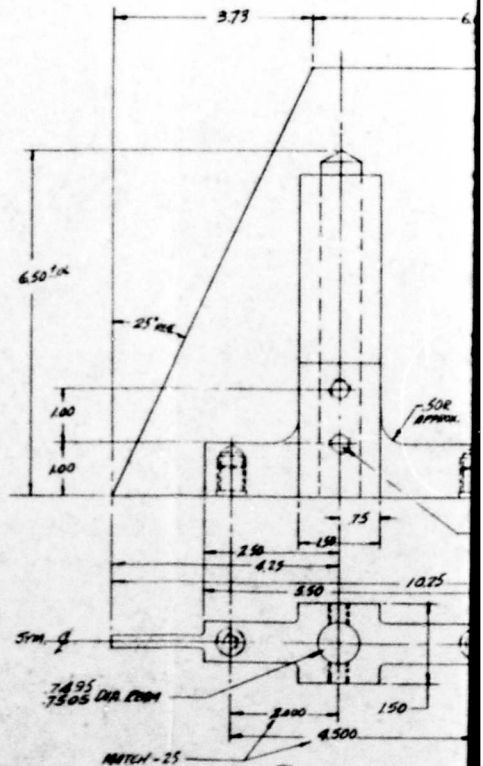
MS 2000S - 5/16" BOLT - 1 REQ

H5 2000S-72 BOLT - 1 REQ

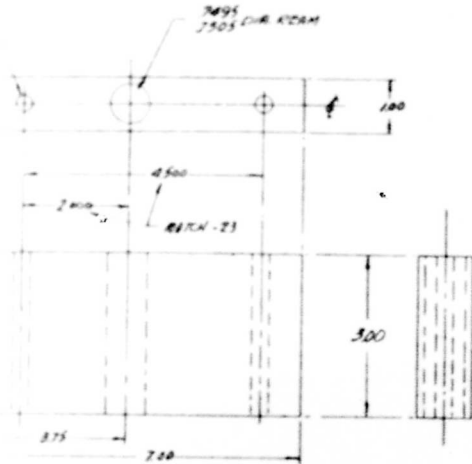
T56 0700-23 IN



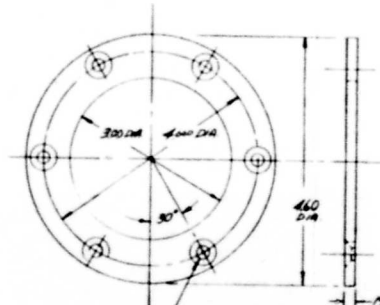
(25) HORIZ SPLINE-INNER 2
MFL-2024 T4 ALUM PL



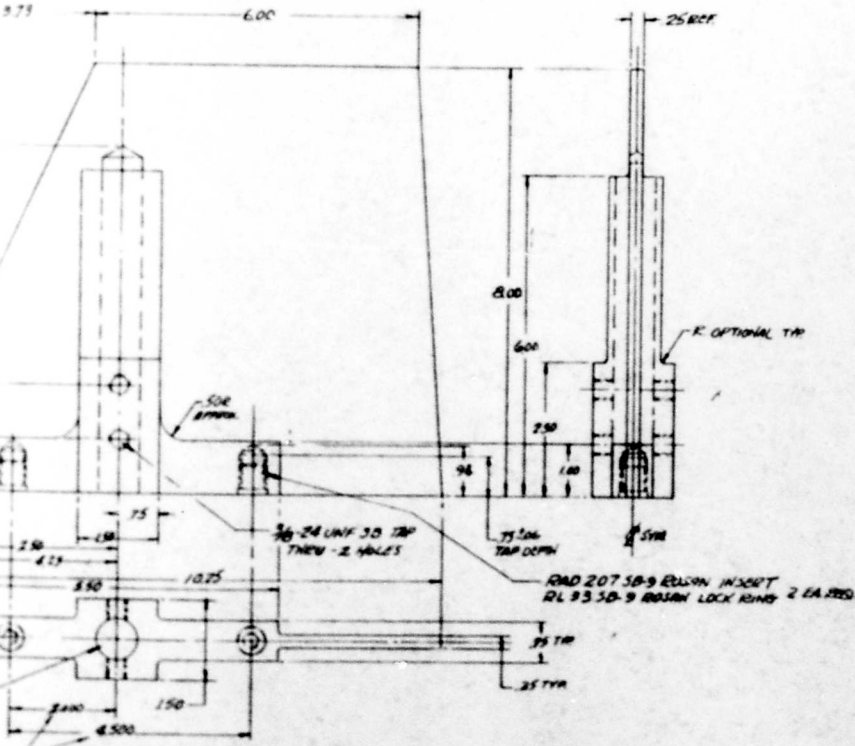
(25) HORIZONTAL SPLINE
MFL-2024 T4 AL



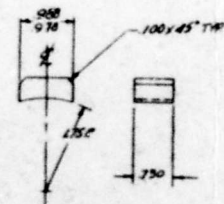
-25 HORIZ SPLINE INNER 2 REQ
MFL-2024 T4 ALUM PLATE



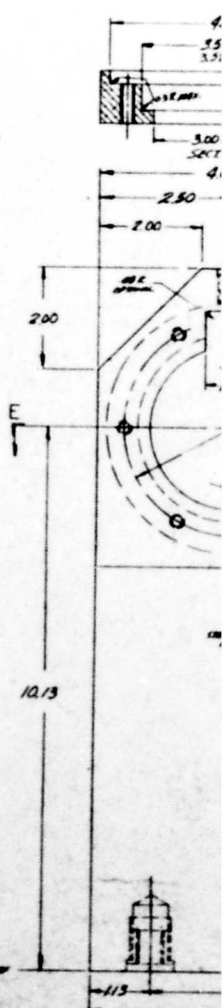
-19 RETAINER 1 REQ
MFL-1907R 2024-T3 ALUM. SHT



-23 HORIZONTAL SPLINE 2 REQ
MFL-2024 T4 ALUM PLATE



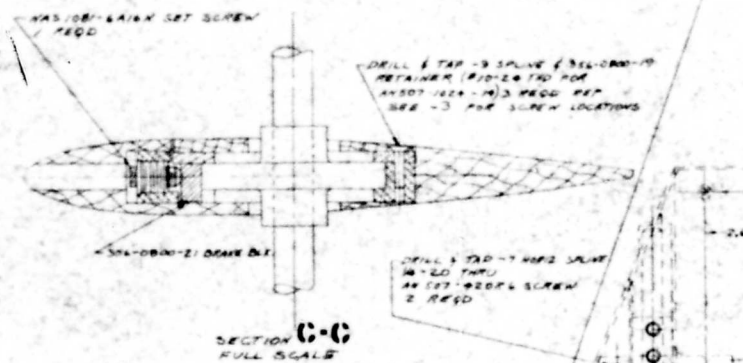
-21 DEVICE BLOCK 1 REQ
MFL-4130 OR 1025 STEEL BAR



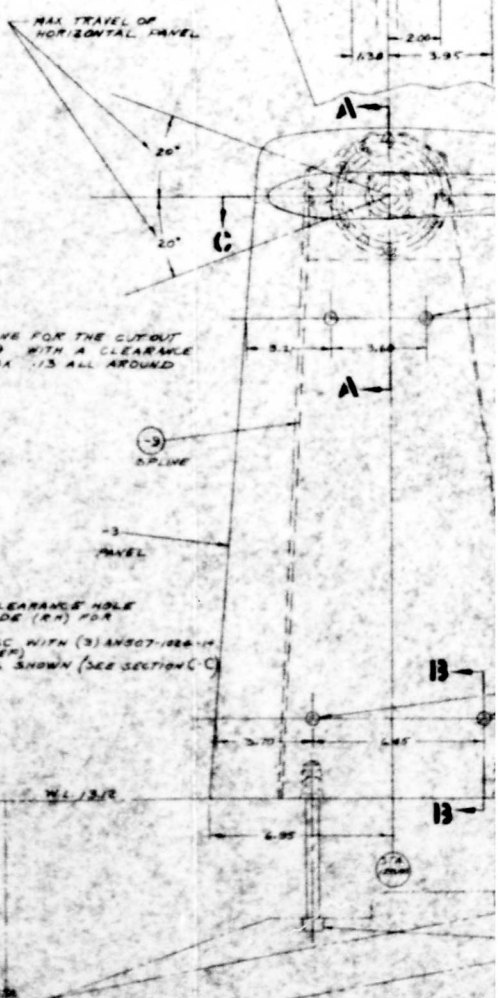
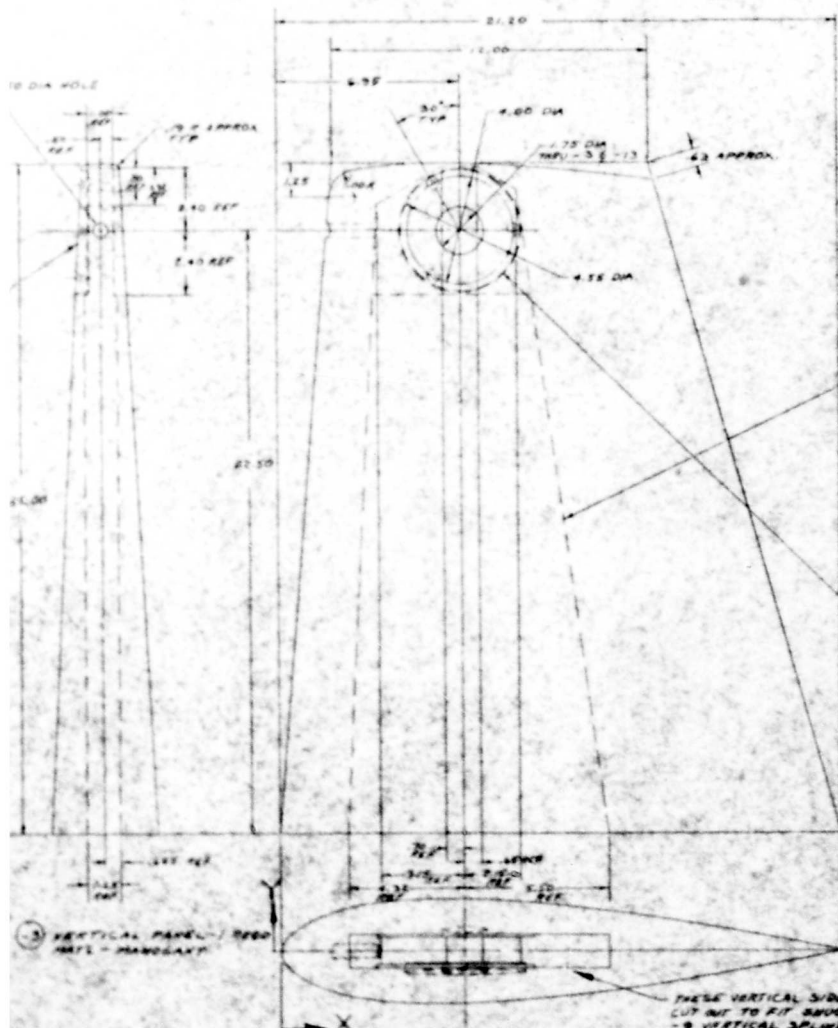
ORDINATES

HORIZONTAL SURFACE			
X	Y	X	Y
11	10	100	100
12	20	100	100
13	30	100	100
14	40	100	100
15	50	100	100
16	60	100	100
17	70	100	100
18	80	100	100
19	90	100	100
20	100	100	100
21	110	100	100
22	120	100	100
23	130	100	100
24	140	100	100
25	150	100	100
26	160	100	100
27	170	100	100
28	180	100	100
29	190	100	100
30	200	100	100
31	210	100	100
32	220	100	100
33	230	100	100
34	240	100	100
35	250	100	100
36	260	100	100
37	270	100	100
38	280	100	100
39	290	100	100
40	300	100	100
41	310	100	100
42	320	100	100
43	330	100	100
44	340	100	100
45	350	100	100
46	360	100	100
47	370	100	100
48	380	100	100
49	390	100	100
50	400	100	100
51	410	100	100
52	420	100	100
53	430	100	100
54	440	100	100
55	450	100	100
56	460	100	100
57	470	100	100
58	480	100	100
59	490	100	100
60	500	100	100
61	510	100	100
62	520	100	100
63	530	100	100
64	540	100	100
65	550	100	100
66	560	100	100
67	570	100	100
68	580	100	100
69	590	100	100
70	600	100	100
71	610	100	100
72	620	100	100
73	630	100	100
74	640	100	100
75	650	100	100
76	660	100	100
77	670	100	100
78	680	100	100
79	690	100	100
80	700	100	100
81	710	100	100
82	720	100	100
83	730	100	100
84	740	100	100
85	750	100	100
86	760	100	100
87	770	100	100
88	780	100	100
89	790	100	100
90	800	100	100
91	810	100	100
92	820	100	100
93	830	100	100
94	840	100	100
95	850	100	100
96	860	100	100
97	870	100	100
98	880	100	100
99	890	100	100
100	900	100	100

VERTICAL SURFACE			
X	Y	X	Y
11	10	100	100
12	20	100	100
13	30	100	100
14	40	100	100
15	50	100	100
16	60	100	100
17	70	100	100
18	80	100	100
19	90	100	100
20	100	100	100
21	110	100	100
22	120	100	100
23	130	100	100
24	140	100	100
25	150	100	100
26	160	100	100
27	170	100	100
28	180	100	100
29	190	100	100
30	200	100	100
31	210	100	100
32	220	100	100
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59	490	100	100
60	500	100	100
61	510	100	100
62	520	100	100
63	530	100	100
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68	580	100	100
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74	640	100	100
75	650	100	100
76	660	100	100
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89	790	100	100
90	800	100	100
91	810	100	100
92	820	100	100
93	830	100	100
94	840	100	100
95	850	100	100
96	860	100	100
97	870	100	100
98	880	100	100
99	890	100	100
100	900	100	100



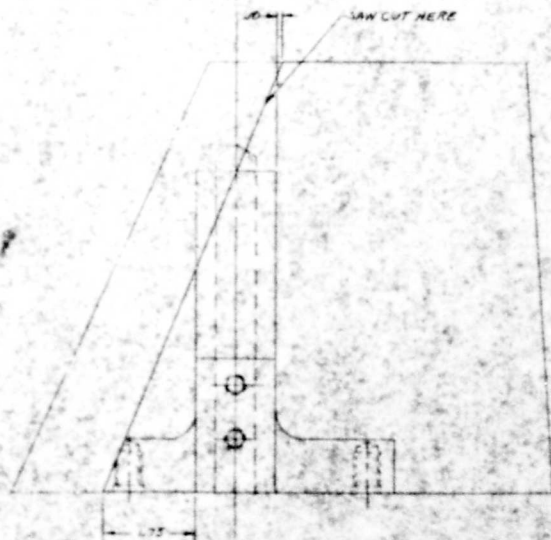
SECTION C-C
FULL SCALE



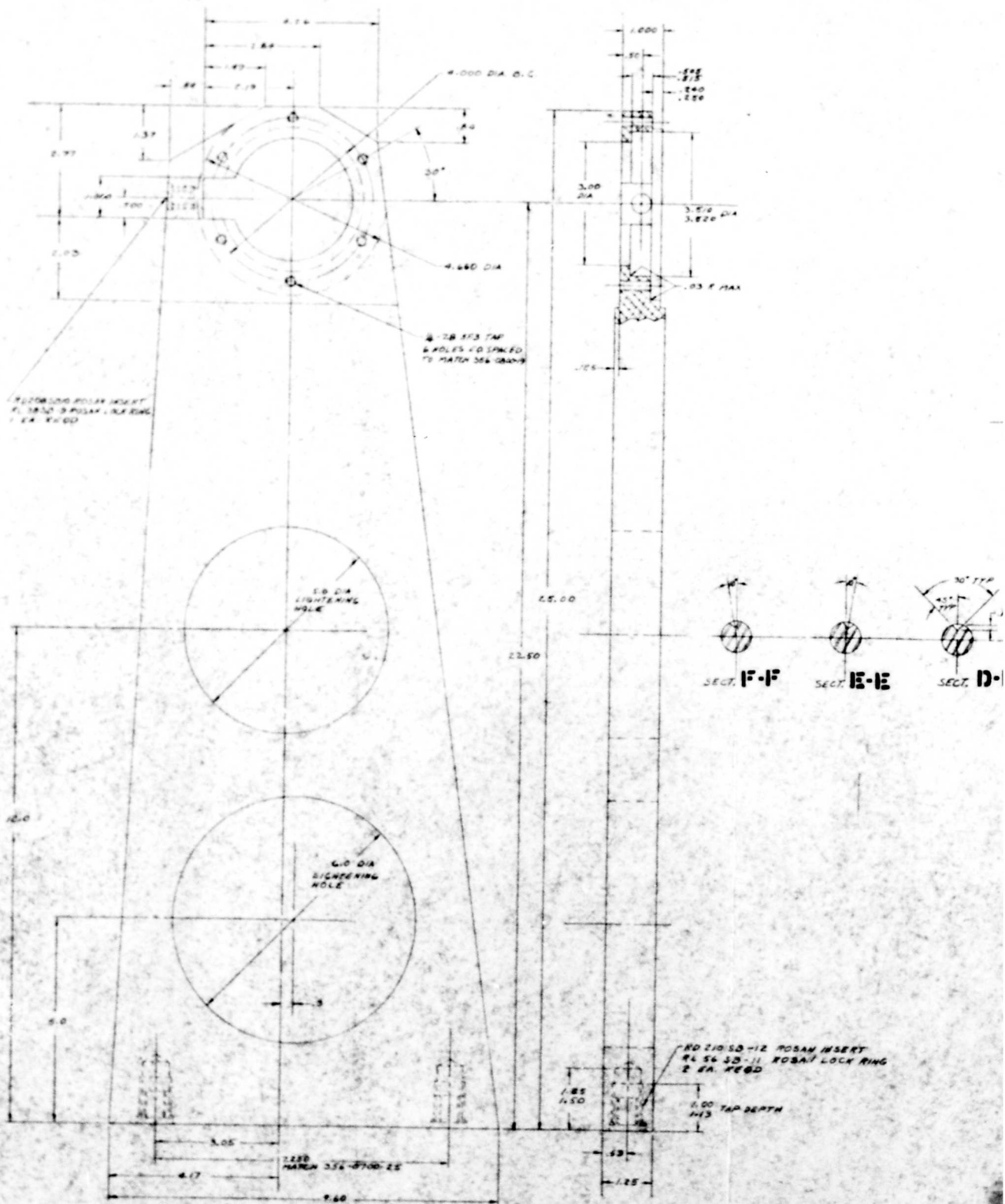
THIS OUTLINE FOR THE CUT OUT TO FIT -9 WITH A CLEARANCE OF APPROX .13 ALL AROUND

FLY CUT CLEARANCE HOLE ON MAX SIDE (RM) FOR -13 DISC RETAIN DISC WITH (3) ANSOT-1884-14 SCREWS (REF) LOCATE AS SHOWN (SEE SECTION C)

THESE VERTICAL SIDE SURFACES OF CUT OUT TO FIT ROUGHLY AGAINST -9 VERTICAL SPLINE



① HORIZONTAL SPLINE & R500
MAKE FROM 356-0800-23 HORIZ. SPLINE

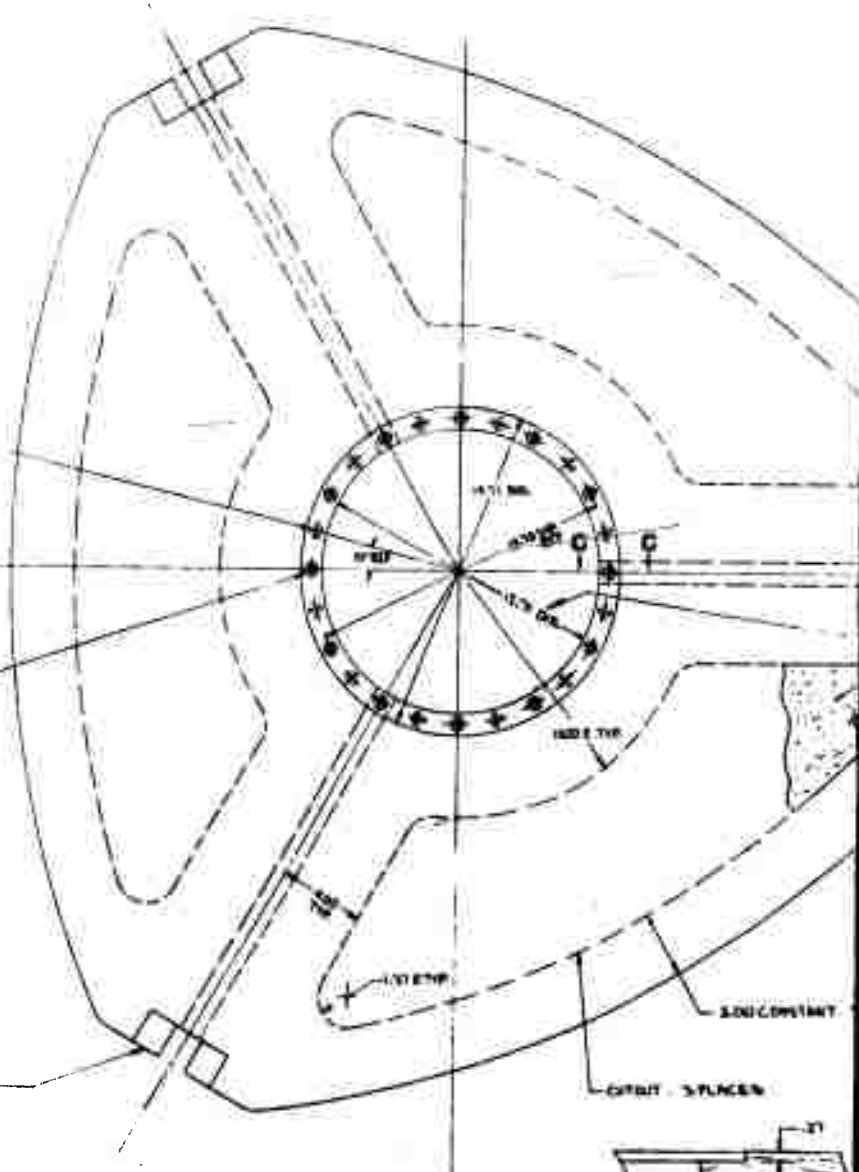


⑨ VERTICAL SPLINE 1 Pcsd
MATL - 2024 TH ALUM PLATE

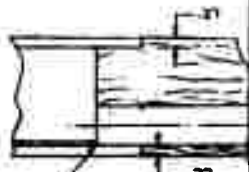
ROSKN WASLET P/N 746 SB-KL
 ROSKIN LOCKING PIN 5510 SB-D
 11 EACH REQD TO MATCH -11 HUB
 LOCKING TO BE 05 BELOW SURFACE.
 RETAIN HUB WITH LOCTITE SERBANT

ROSKIN WASLET P/N 746 SB-KL
 ROSKIN LOCKING PIN 5510 SB-D
 11 EACH REQD TO MATCH -15 PLATE
 LOCKING TO BE 05 BELOW SURFACE.
 RETAIN HUB WITH LOCTITE SERBANT

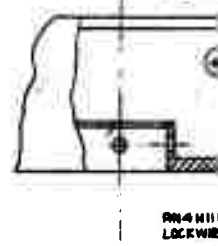
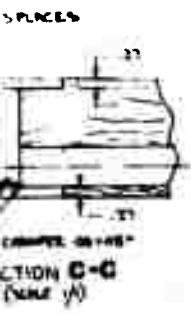
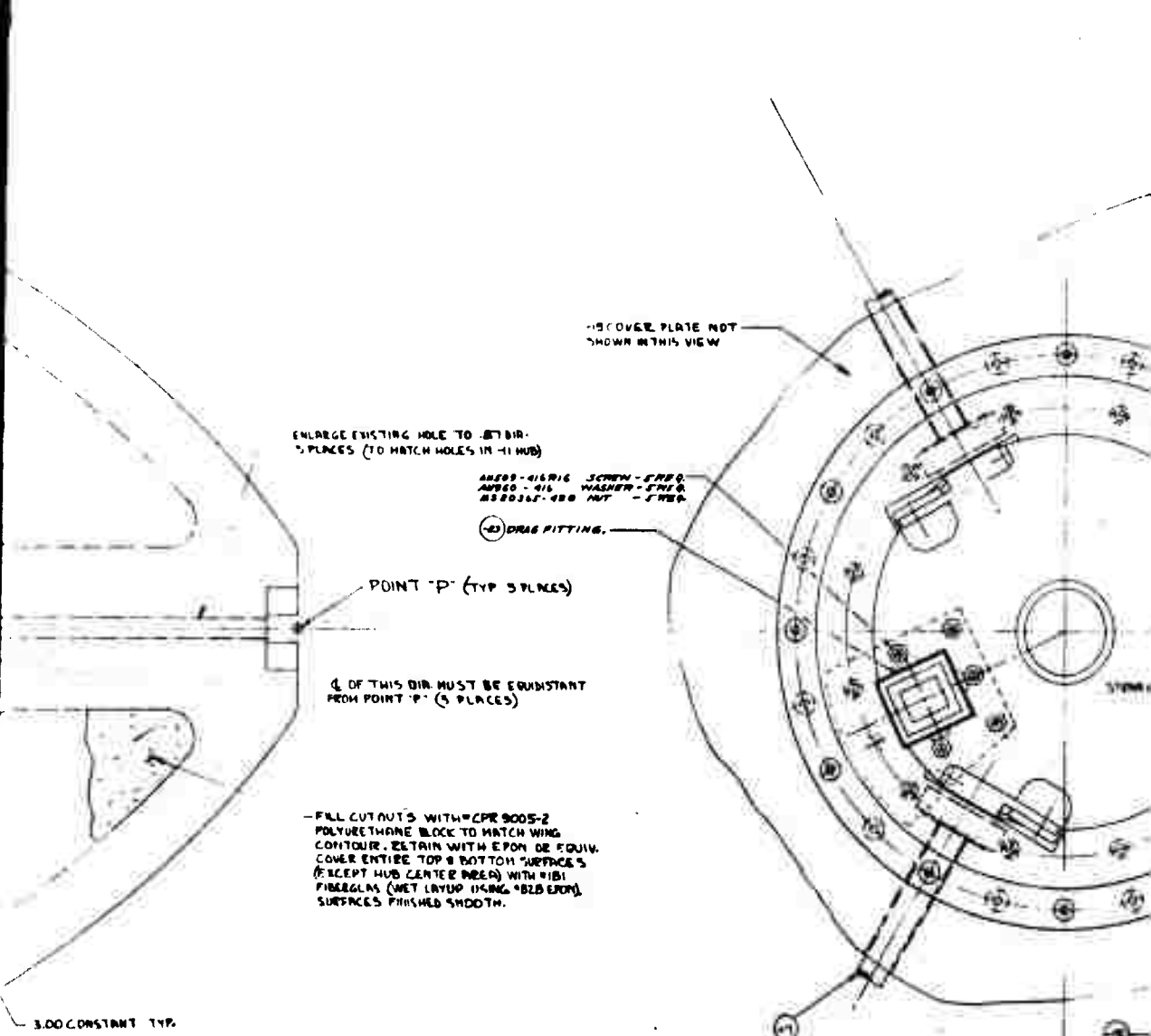
CUTOUT TO SUIT - 9
 3 PLACES AS SHOWN
 IN VIEW A-A

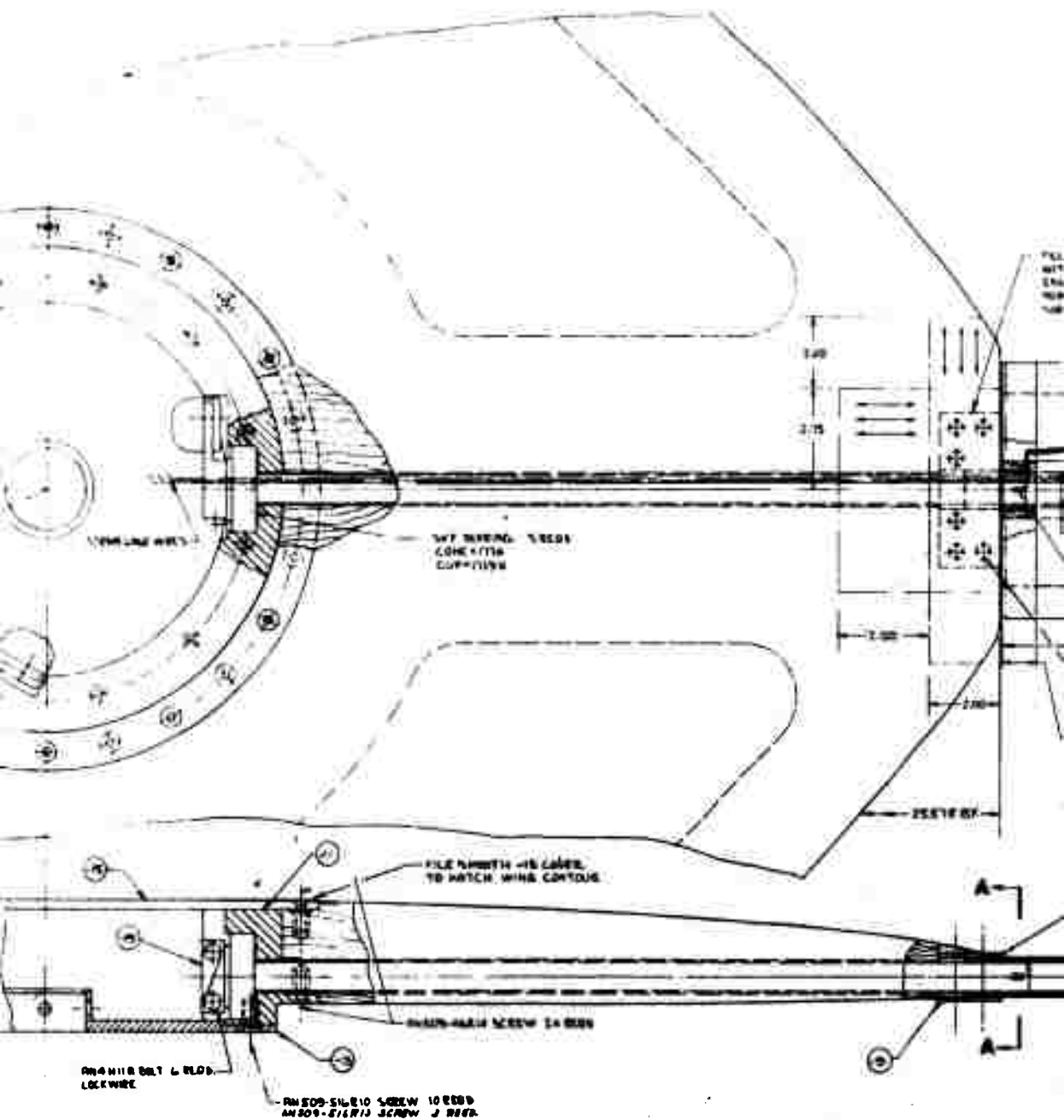


⑤ WING
 (MAKE FROM 35L-0103)
 (SCALE 1/1)



CHAMFER .05 ± .05"
 SECTION C-C
 (SCALE 1/1)





FILL CAVITY WITH EPON 828 FUSION
WITH WING CON TOUR
ENVELOPE FIBER WITH #81 FIBERGLAS
POURED WITH EPON 828
SURFACE SANDED SMOOTH

T TAPERED LENGTH INDICATED

NR5 184-3-6 STUD 6 RPD

356-0106-11 NUT 6 RPD

WIRE TIE BAR IN SHORT SPAN ONLY

1/4" 1/8" BT

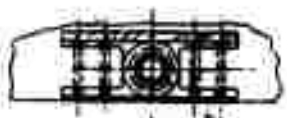
STIFFEN ANGLE NARROW TO 1/4" 1/8"

DESIGN OR 1/4" 1/8" 1/8" 1/8"

1/8" SHORT SPAN CUT FROM BLADE
FILL KEEP AS BECS WITH FIBERGLAS CLOTH TO
MAINTAIN BLADE ORIGINAL SPAN.
BOND SHORT SPAN TO BLADE BY WRAPPING
WITH #81 FIBERGLAS CLOTH + #828 EPON
(FOR 5 BLADES)

29 BLADE (S)
MADE FROM 356-0204-505

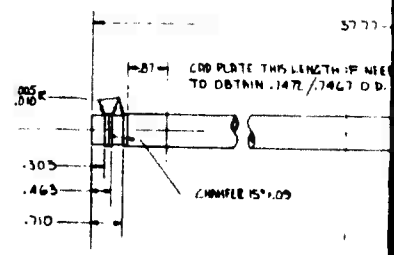
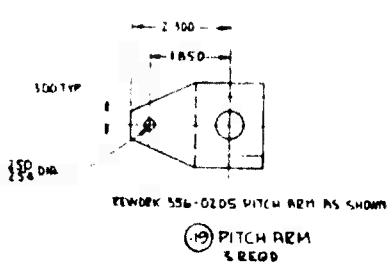
25.578 BT



VIEW A-A

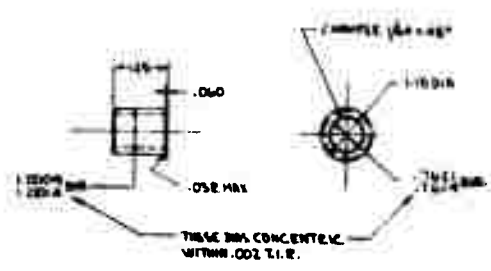
1. DIAMETERS MARKED (C) TO BE CON
WITHIN .002 T.I.E.
NOTES:

5777

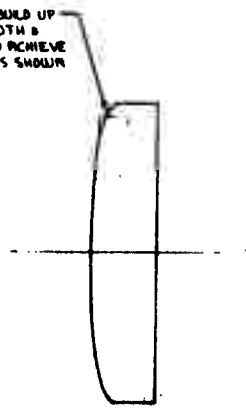


REWORK 75

REMOVE EXPOSED TUBE & BUILD UP WITH #18 FIBERGLAS CLOTH & EPOX BLD OR EQUAL TO ACHIEVE SYMMETRICAL SHAPE AS SHOWN



(7) BUSHING
3 REQ'S
MATERIAL OF OLITE BRONZE



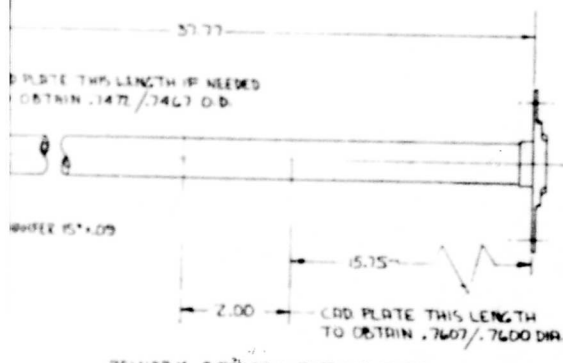
356-0206-505 TIP
REWORK AS INDICATED

(21) BLADE TIP
3 REQS

DRILL .190 DIA
CSK 100* .375
6 PLACES

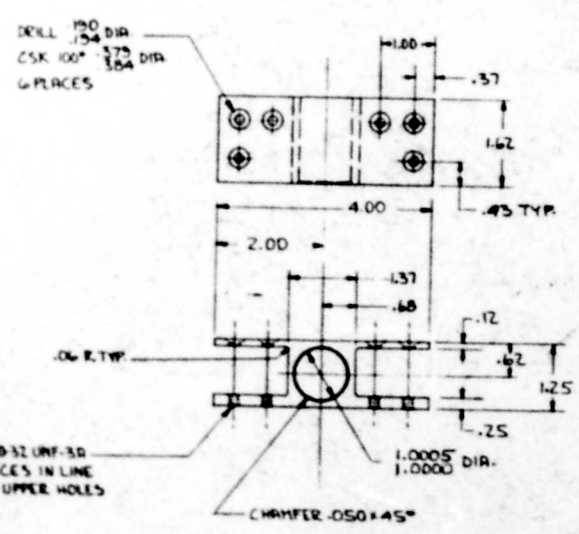
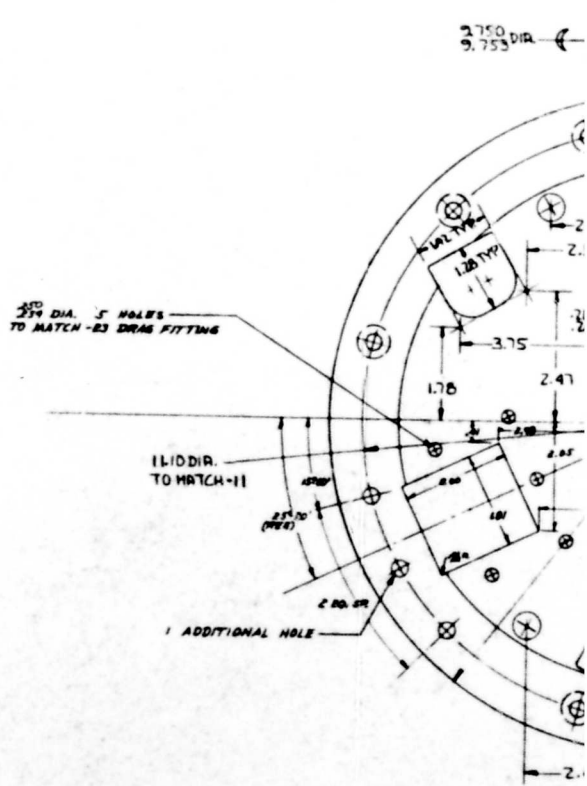
.06 RTYP

TIP @ 12 O'Clock
6 PLACES IN LINE
WITH UPPER HOLES



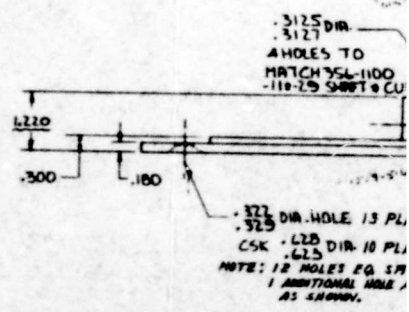
REWORK 3/50 OZ II RETAINER TUBE

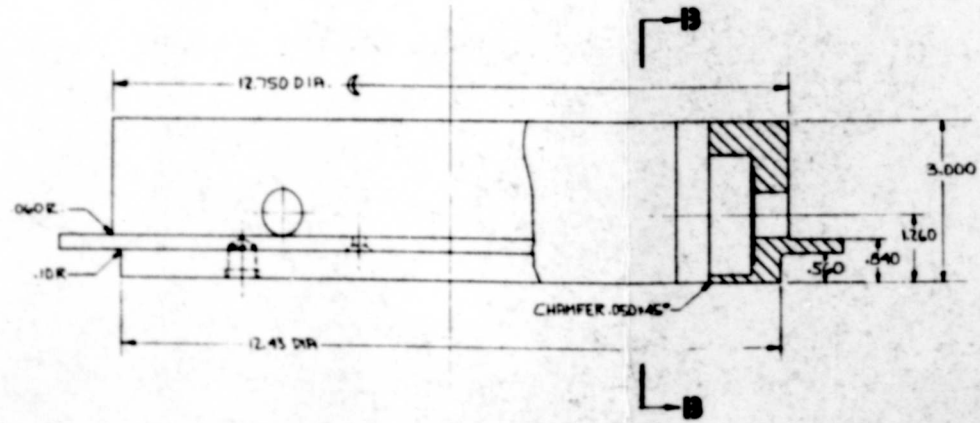
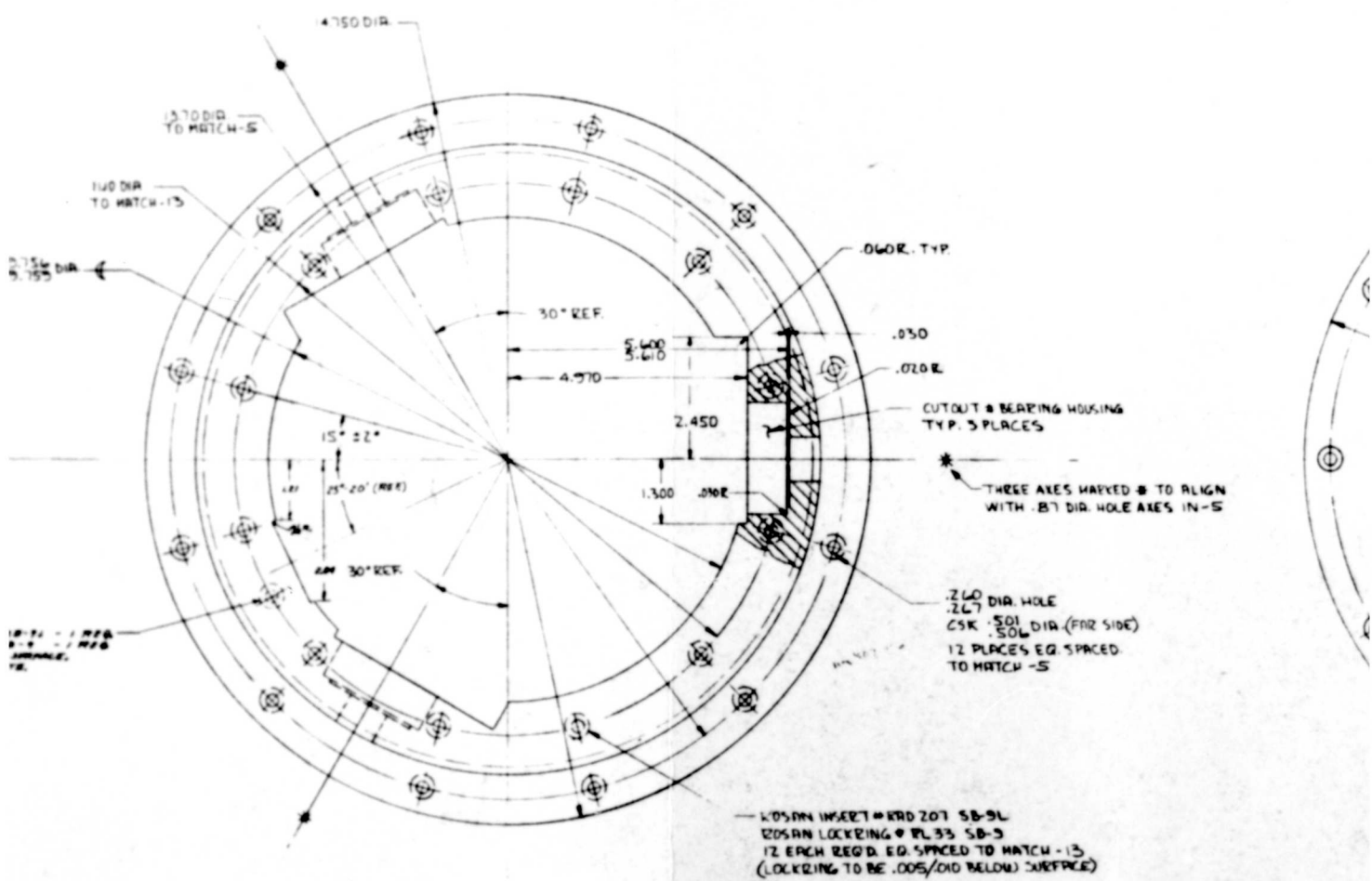
(47) SPARE
3 RECD



TAP 10-32 UNF-30
6 PLACES IN LINE
WITH UPPER HOLES

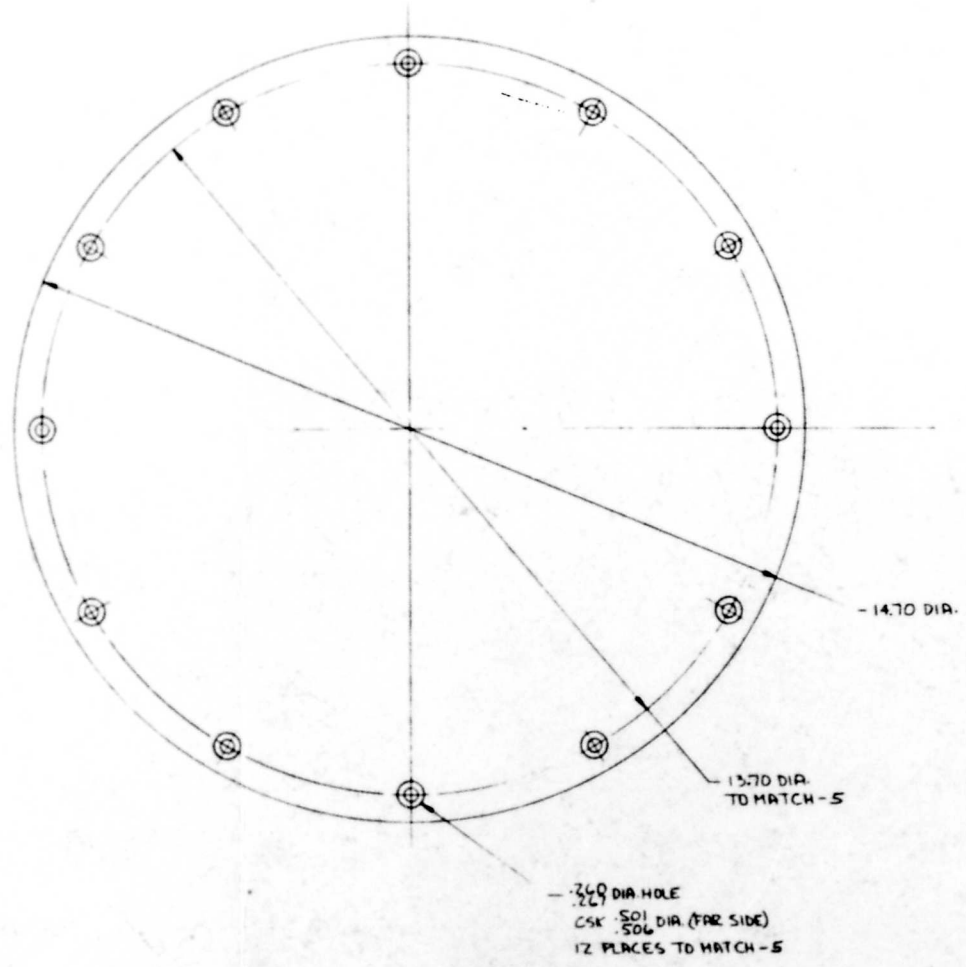
(9) HOUSING
PART OF 2024-T4
3 RECD





(11) HUB
 MAKE OF 202A-T4

REVISIONS					
REV	DATE	DESCRIPTION	BY	APP'D	DATE



RING HOUSING IS
 AXES MARKED TO ALIGN
 .87 DIA. HOLE AXES IN-5

HOLE
 DIA. (FAR SIDE)
 EQ SPACED
 -5

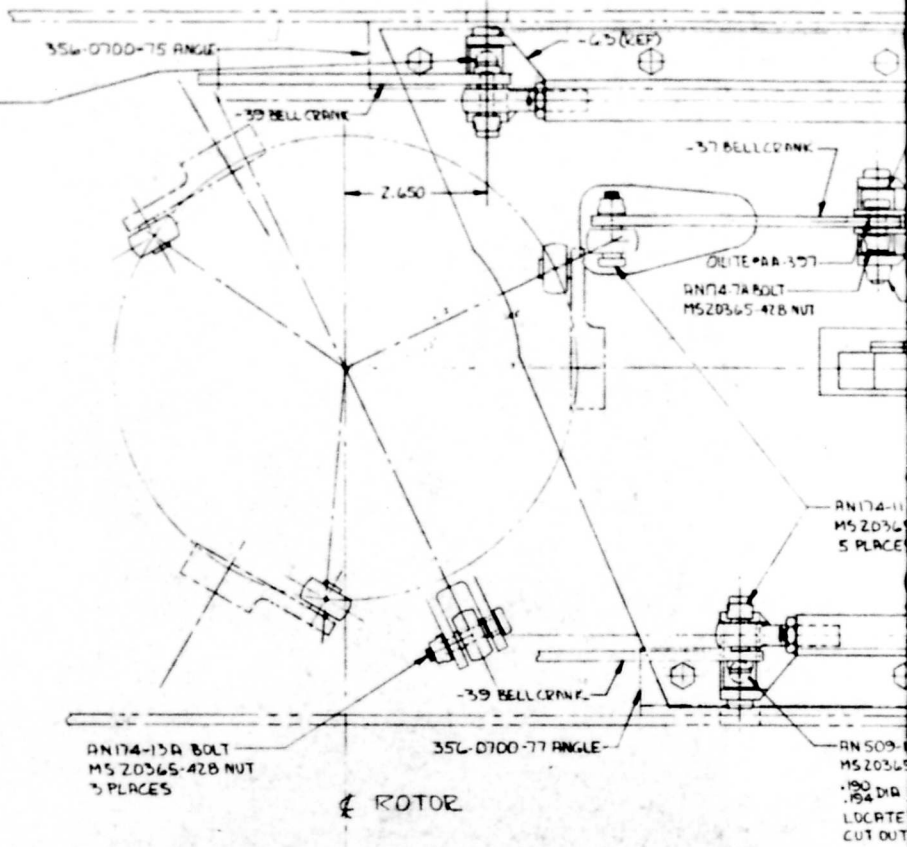
12H - 12
 SURFACE

15 COVER PLATE
 MAKE OF 2024-T4

356-0900

BEST COPY USED ON		APPROVED BY		DATE		ROTOR - ONE ROTOR-WING WIND TUNNEL MODEL		356-0900 2024	

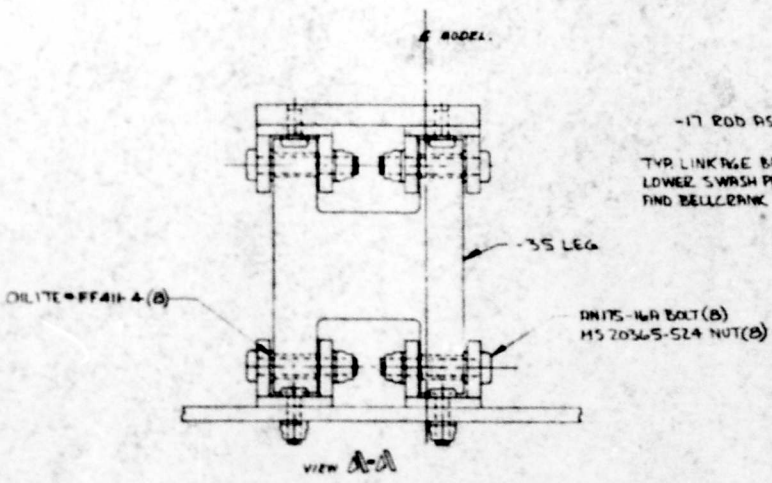
AN509-16R14 SCREW
MS 20365-1052 NUT
.190 DIA. IN 356-0700-75 ANGLE
.194 LOCATE FROM -63 BRET.
CUT OUT ANGLE TO CLEAR
ADJACENT NUTS



-19 ROD ASSY
TYP. LINKAGE BETWEEN
UPPER SWASH PLATE
AND BLADE PITCH ARM

-17 ROD ASSY
TYP. LINKAGE BETWEEN
LOWER SWASH PLATE
AND BELL CRANK

AN174-12 BOLT (L)
AN 310-4 NUT (L)
AN 381-2-10 COTTER (L)

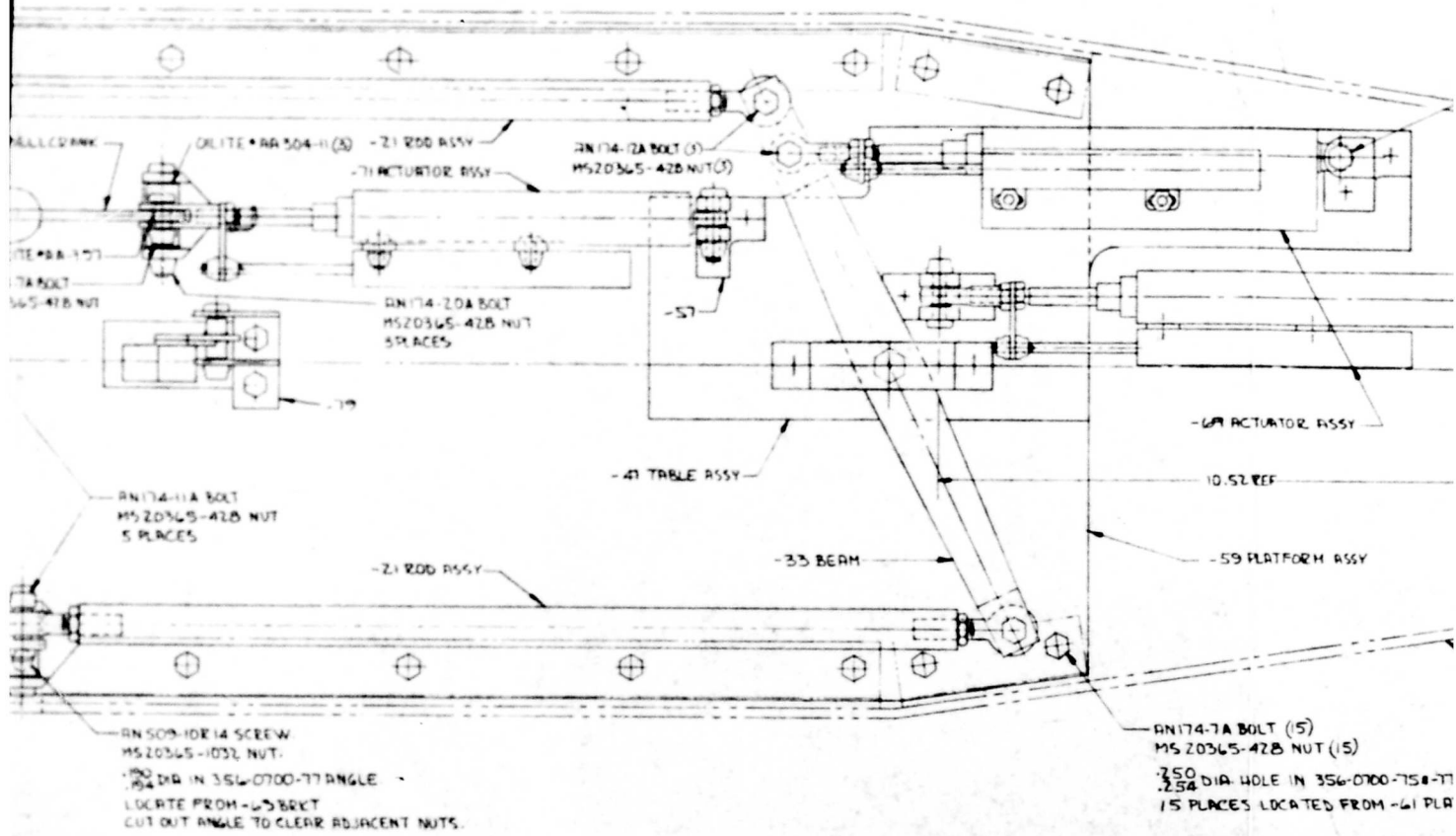


356-0602 MAST (REF)

6

5

4



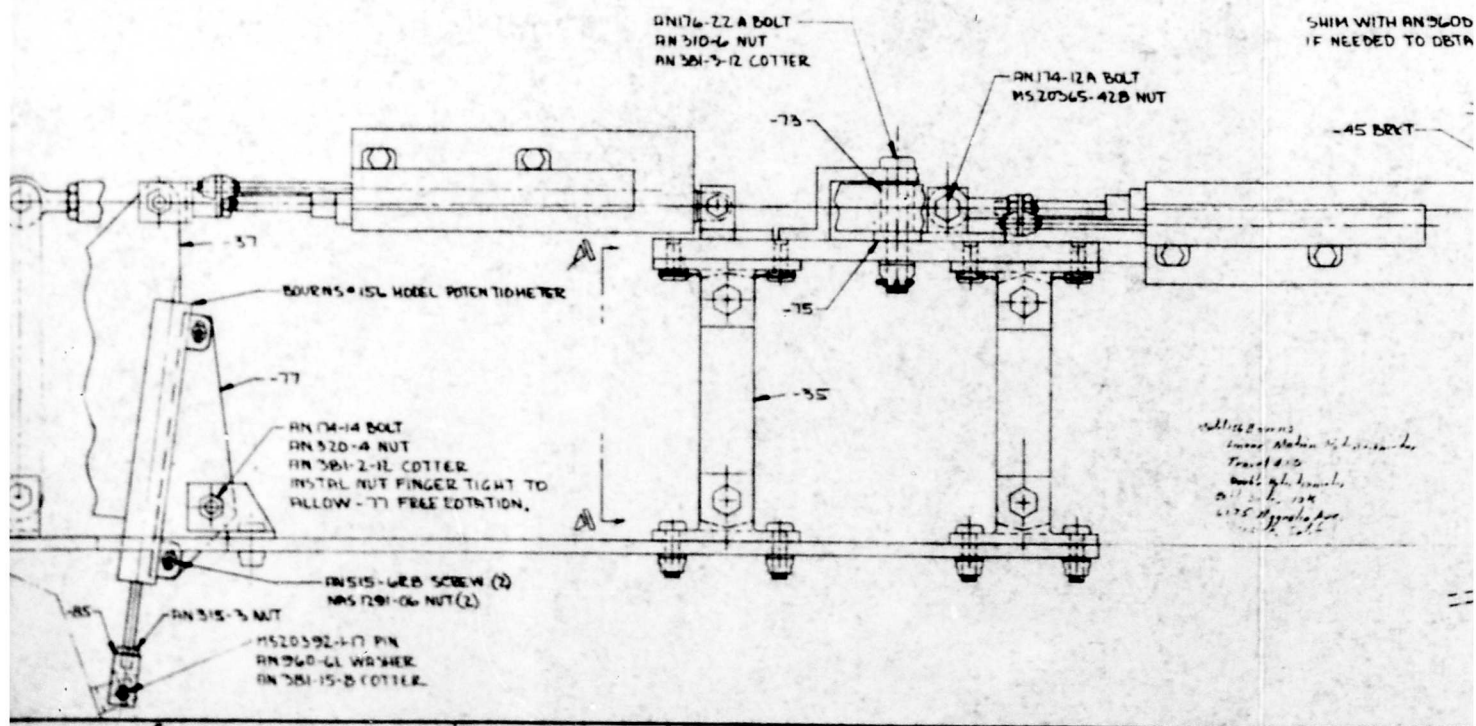
1900-10 PITCH ARM REF

ALL CONTROLS SHOWN
IN NEUTRAL POSITION
(0° CYCLIC, 0° COLLECTIVE)

1/2 BOLT (6)
3/4 NUT (6)
1/2-10 COTTER (4)

P. 1040

SHIM WITH AN 9606
IF NEEDED TO OBTAIN

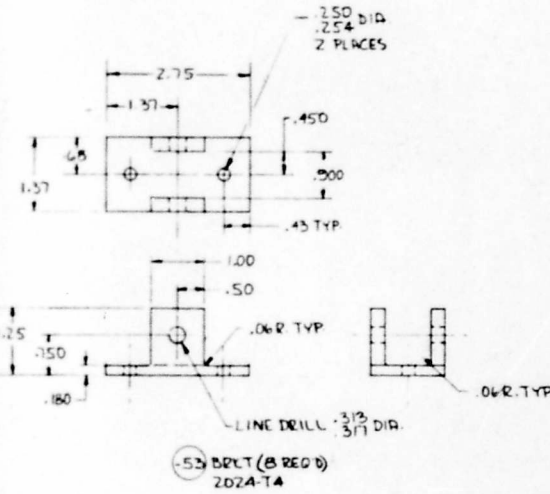


all Bourns
control potentiometers
part # ISL
model # ISL
part # 1291-06
MS 1291-06
AN 515-3 NUT

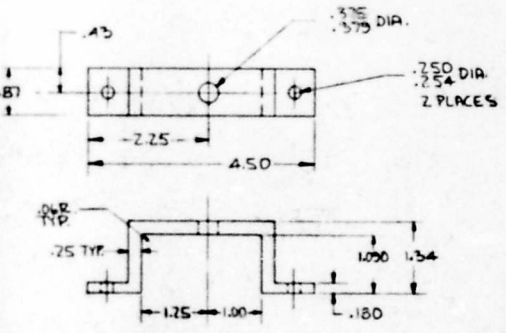
6

5

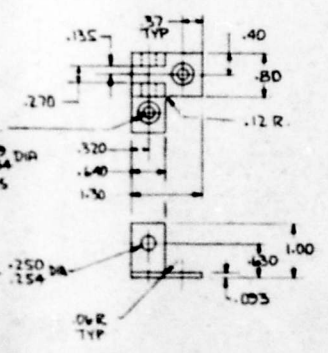
4



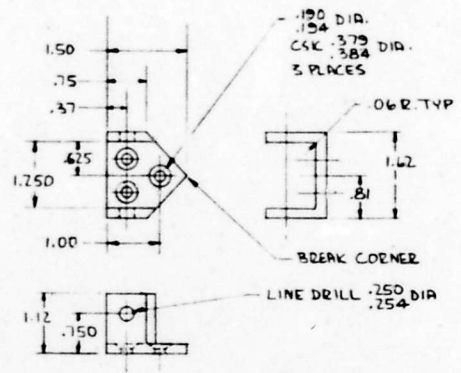
(53) BRKT (S REG D)
202A-T4



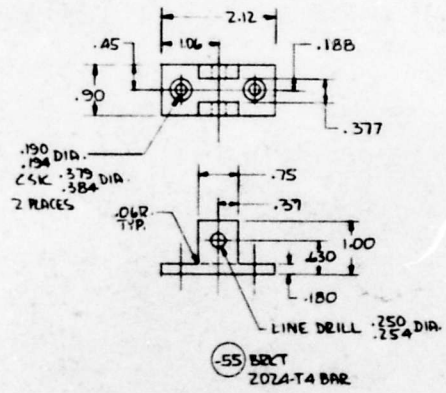
(51) BRKT
4130 BAR



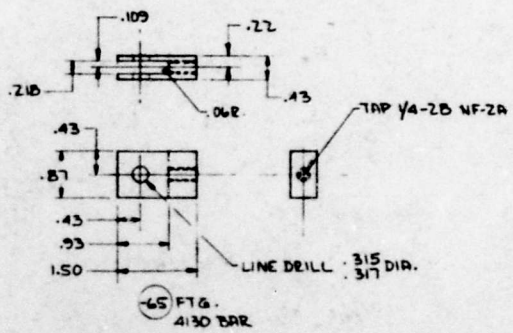
(57) BRKT
202A-T4 BAR



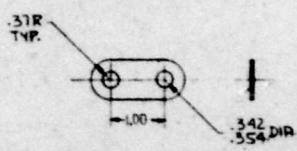
(62) BRKT (S REG D)
202A-T4 BAR



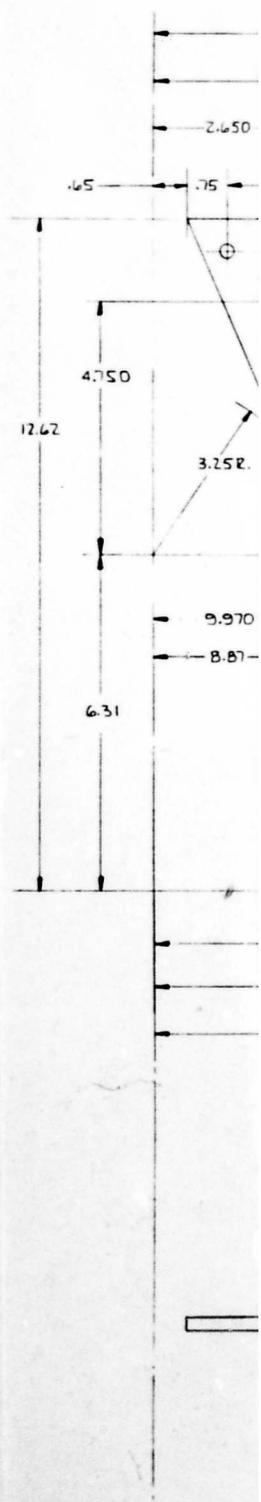
(55) BRKT
202A-T4 BAR

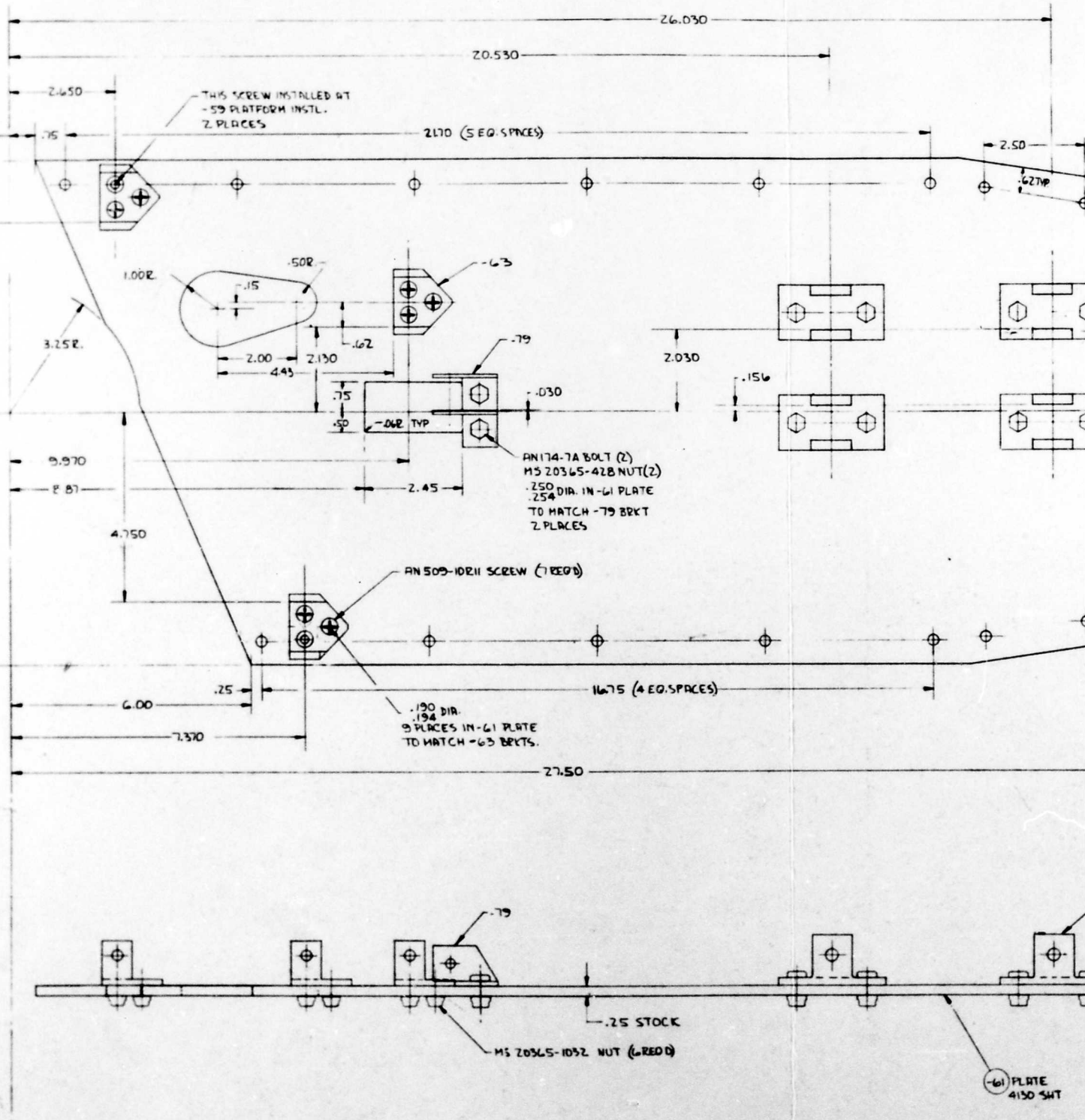


(65) FTG.
4130 BAR

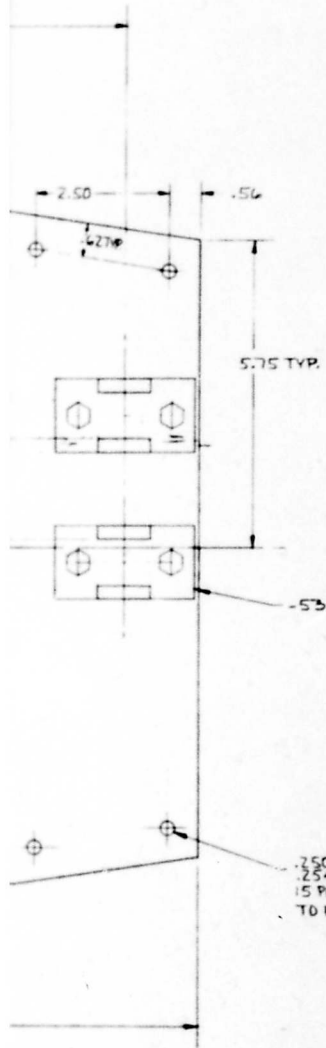


(67) LINK (S REG D)
4130 SHT.



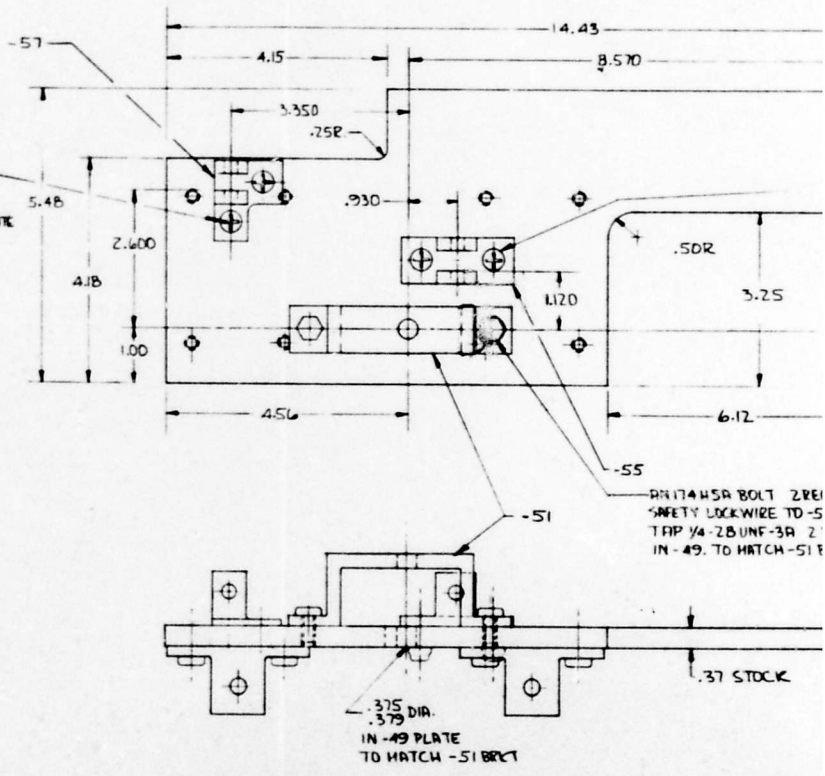


PLATFORM ASSY

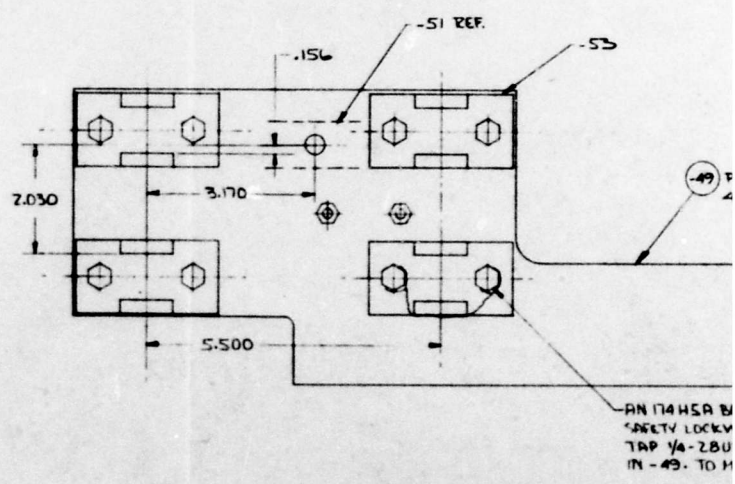


Ø 2.50 DIA.
 15 PLACES
 TO MATCH 356-0700-75-T1 ANGLES

NK 509-10R7 SCREW
 (Z. RED D)
 (NYLOK CORP.)
 TAP 10S2 UNF-3A IN -49 PLATE
 TO MATCH -57 BRKT.
 2 PLACES.



AN 174 H5A BOLT 2 REI
 SAFETY LOCKWIRE TO -5
 TAP 1/4-28 UNF-3A 2"
 IN -49. TO MATCH -51 F



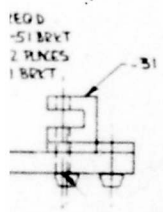
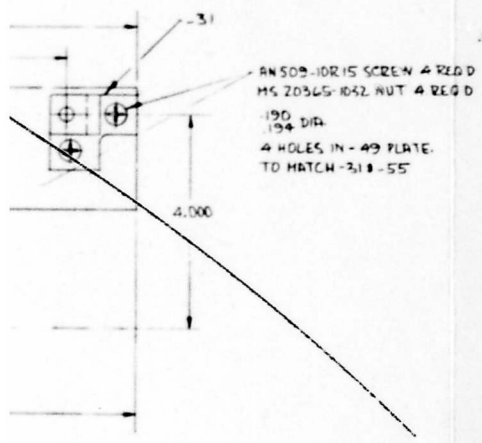
AN 174-7A BOLT (B REG D)
 Ø 2.50 DIA.
 .754
 8 HOLES IN -61 TO MATCH -53 BRKT

MS 20065-42B NUT (B REG D)

AN 174 H5A B
 SAFETY LOCKW
 TAP 1/4-28 U
 IN -49. TO M

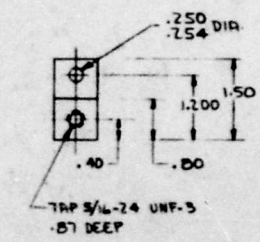
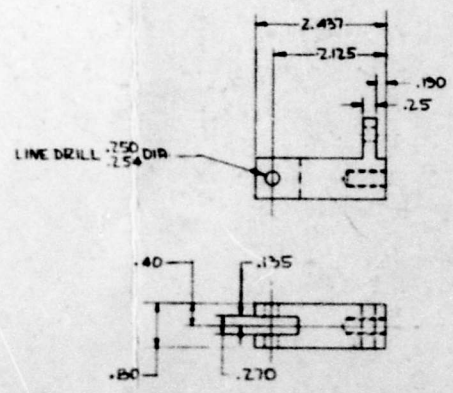
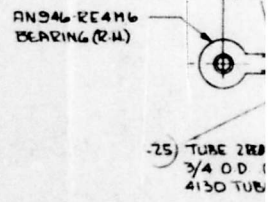
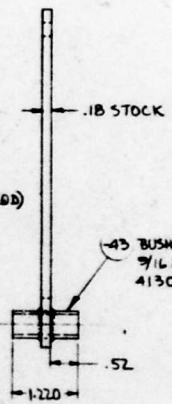
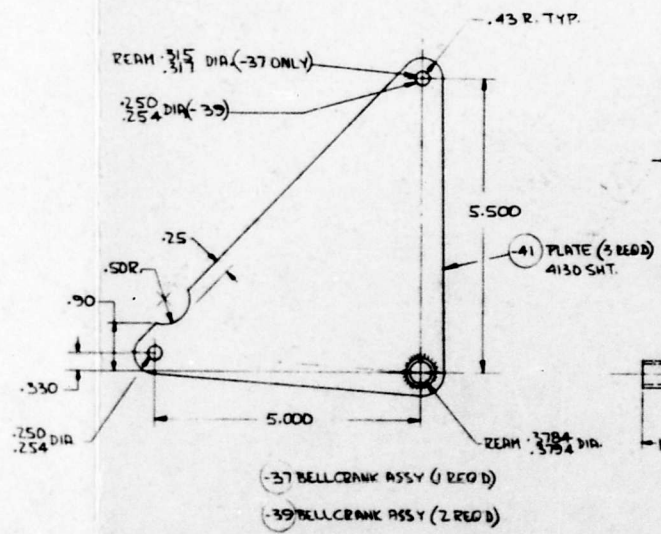
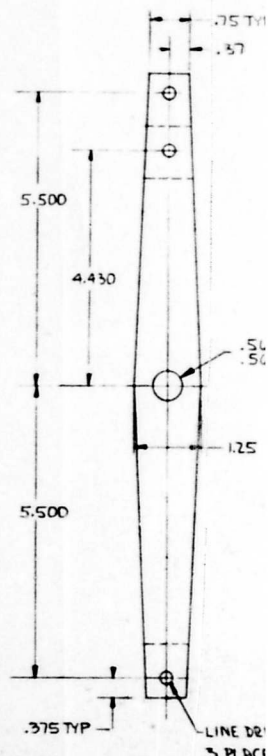
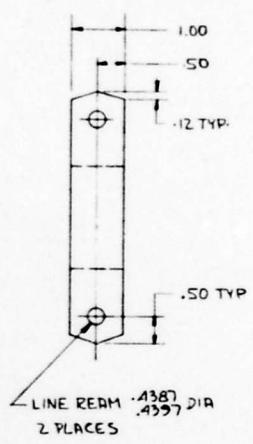
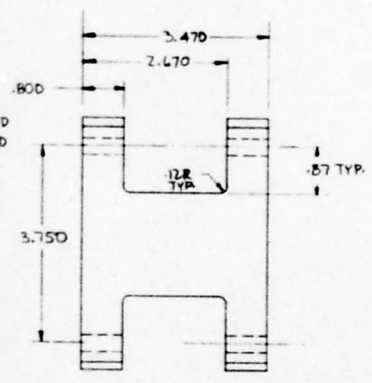
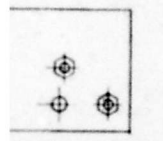
PLATE
 .1150 SWT

(47) TABLE ASSY

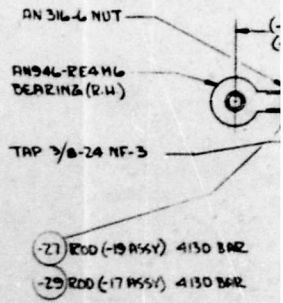


.750 DIA IN -49 PLATE
TO MATCH -31

PLATE
4130 SHT

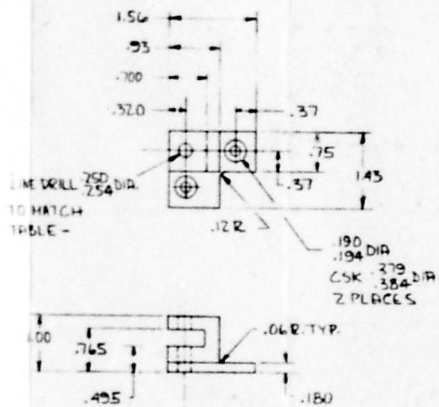


-45 BRKT
4130 BAR

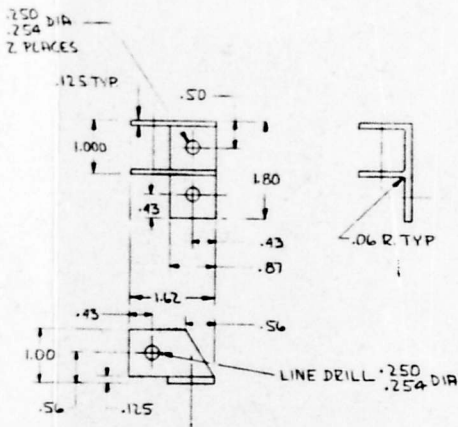


-27 ROD (-19 ASSY) 4130 BAR
-29 ROD (-17 ASSY) 4130 BAR

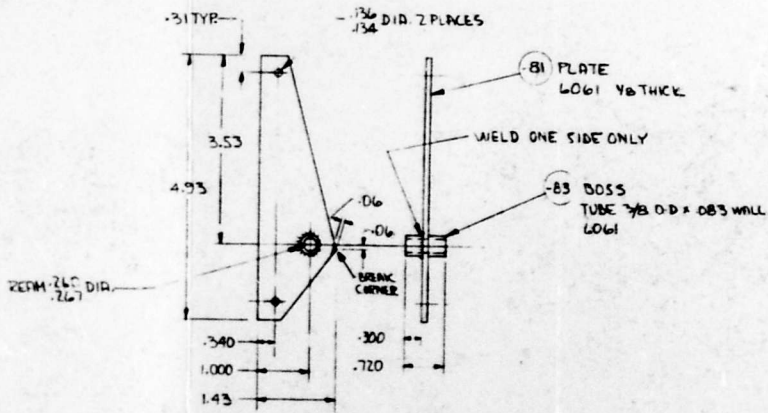
REVISIONS					
SYM	E.O.S.	DESCRIPTION	DRWN	APP'D	DATE



31 BRKT
2024-T4 BAR

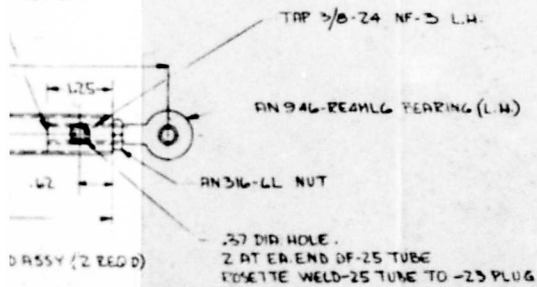


79 BRKT
2024-T4 BAR

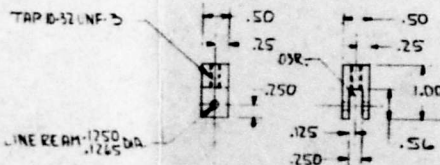


77 BRKT ASSY

PLUG 2280 D
4130 BAR



AN 316-LL NUT
AN 946-RE4H16 BEARING (L.H.)



85 FORK
1020 BAR

356-1000

AP 3/8-24 NF-3 LH.

CONTROL- WING ROTOR WING WIND TUNNEL MODEL		356-1000	
REV	DATE	BY	CHKD

35L-0700 FINE STRUCT. (REF.)

35L-1100 PROPULSION SYSTEM (REF.)

-17 ROD ASSY. (REF.)

-9 DRAG ROD ASSY. (REF.)

N5626-3-4-790 BUSHING - 1 REQ.
 NAS46474-23 BOLT - 1 REQ.
 AN310-A NUT - 1 REQ.
 AN960-416 WASHER - 1 REQ.
 AN381-R-12 COTTER PIN - 1 REQ.
 TORQUE 90-100 IN. LB.

N5626-3-4-250 BUSHING - 1 REQ.
 NAS46474-17 BOLT - 1 REQ.
 AN310-A NUT - 1 REQ.
 AN960-416 WASHER - 1 REQ.
 AN381-R-12 COTTER PIN - 1 REQ.
 TORQUE 90-100 IN. LB.

AN960-416 WASHER (REF.)
 .375 DIA.

35L-1100 PROPULSION SYSTEM (REF.)

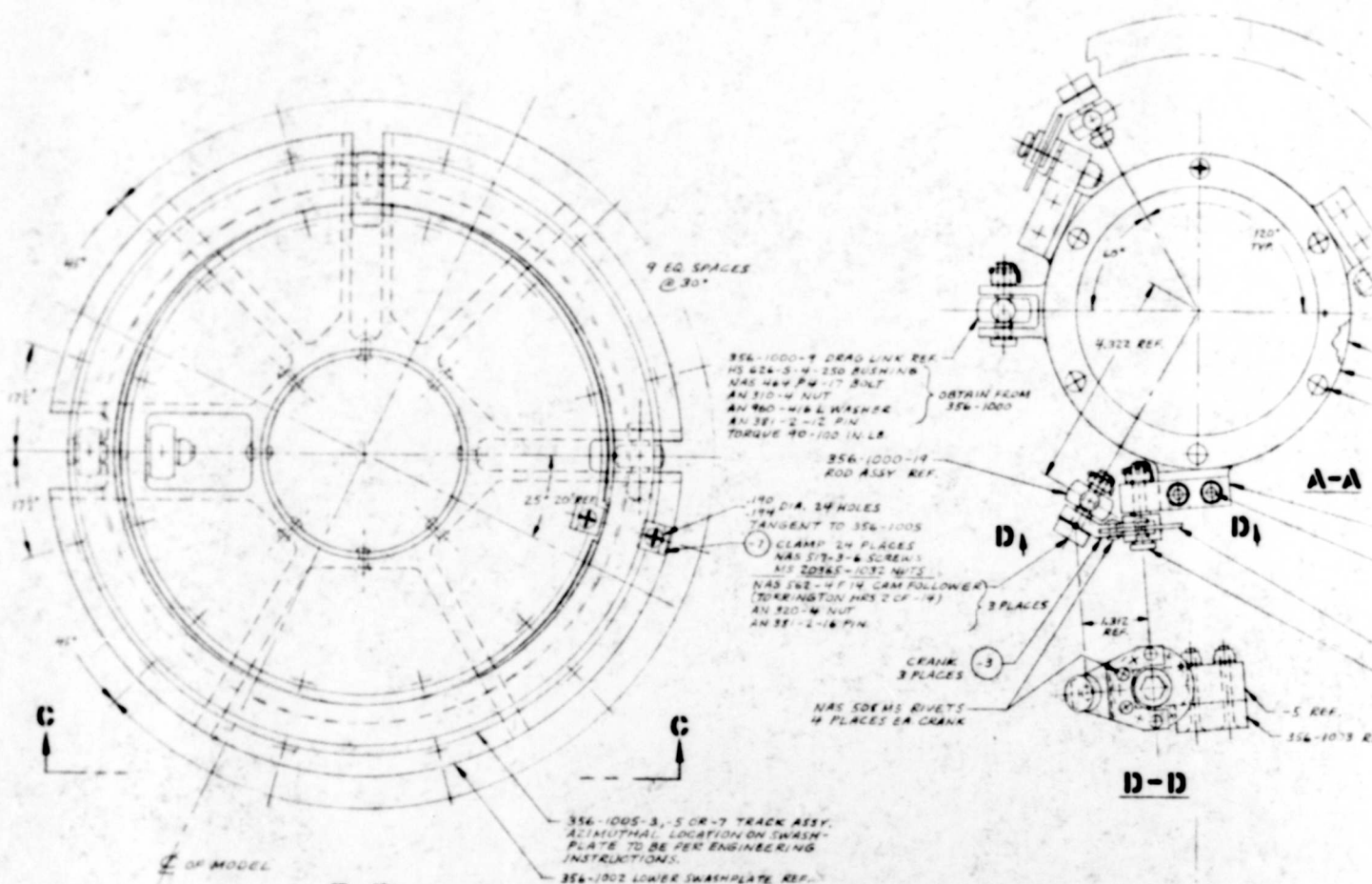
Ø HVB.

Ø ROTARY BLADE.

Ø UPPER SWASH PLATE.

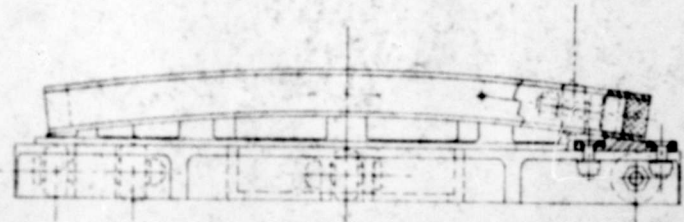
Ø LOWER SWASH PLATE (REF.)

SECT. 13-13

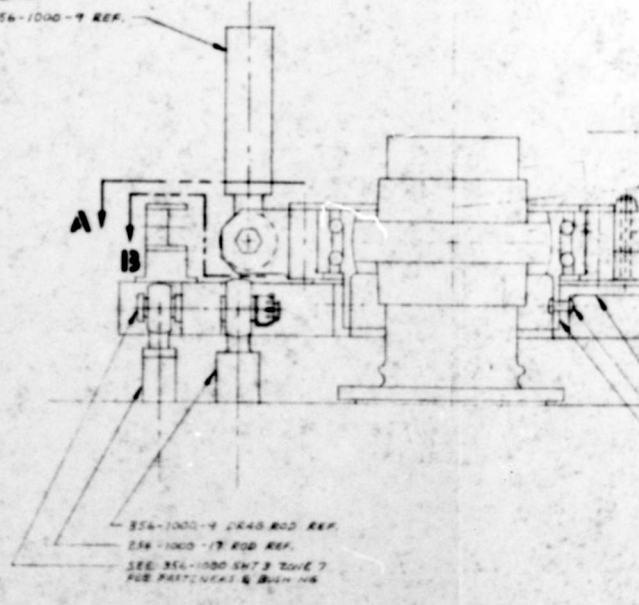


B-B

D-D



C-C



A-A

8

7

6

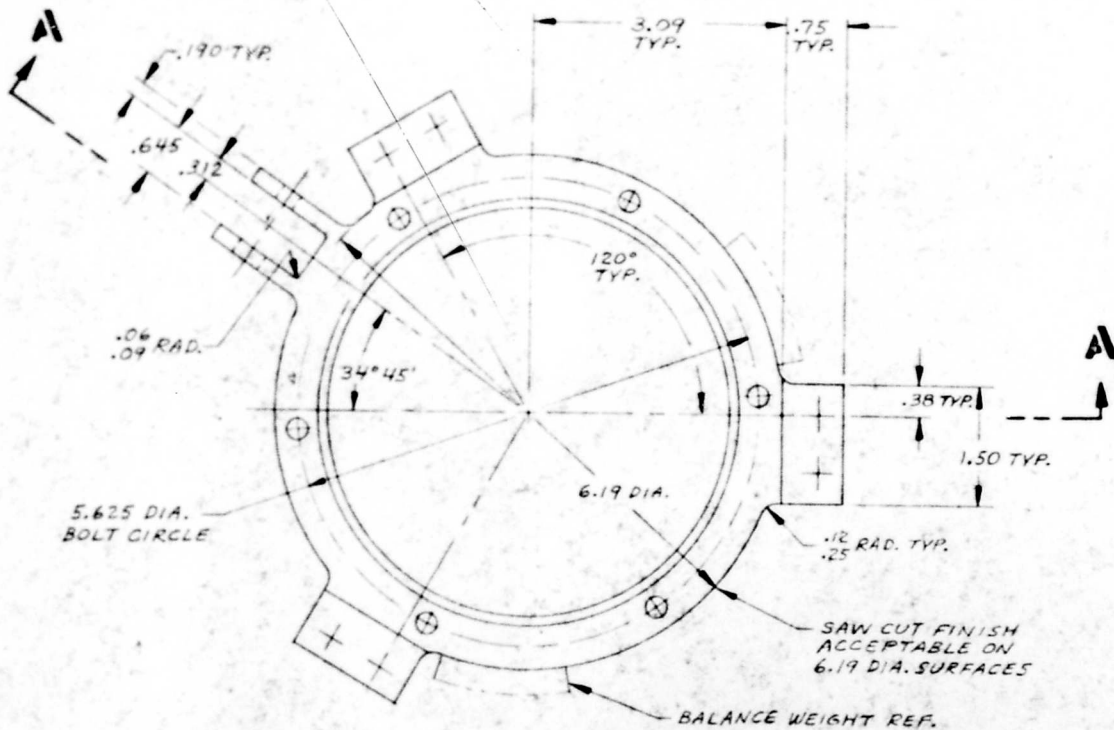
5

D

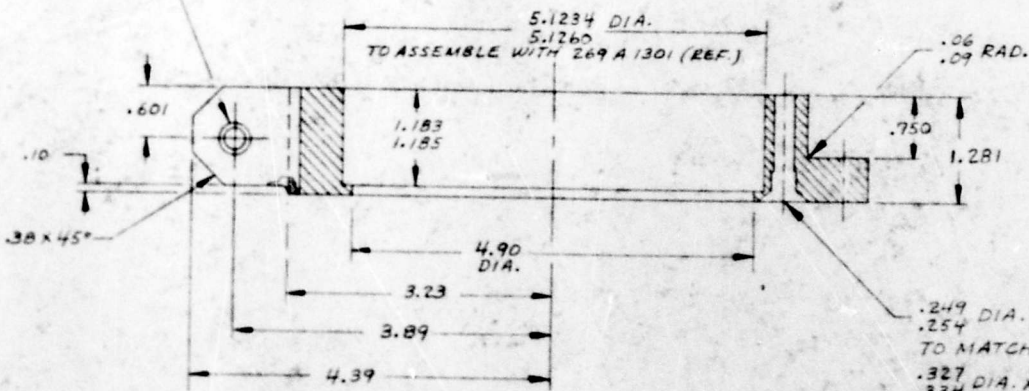
C

B

A



.3745
.3755 DIA. HOLE NEAR SIDE
.2495
.2505 DIA. HOLE FAR SIDE } IN LINE

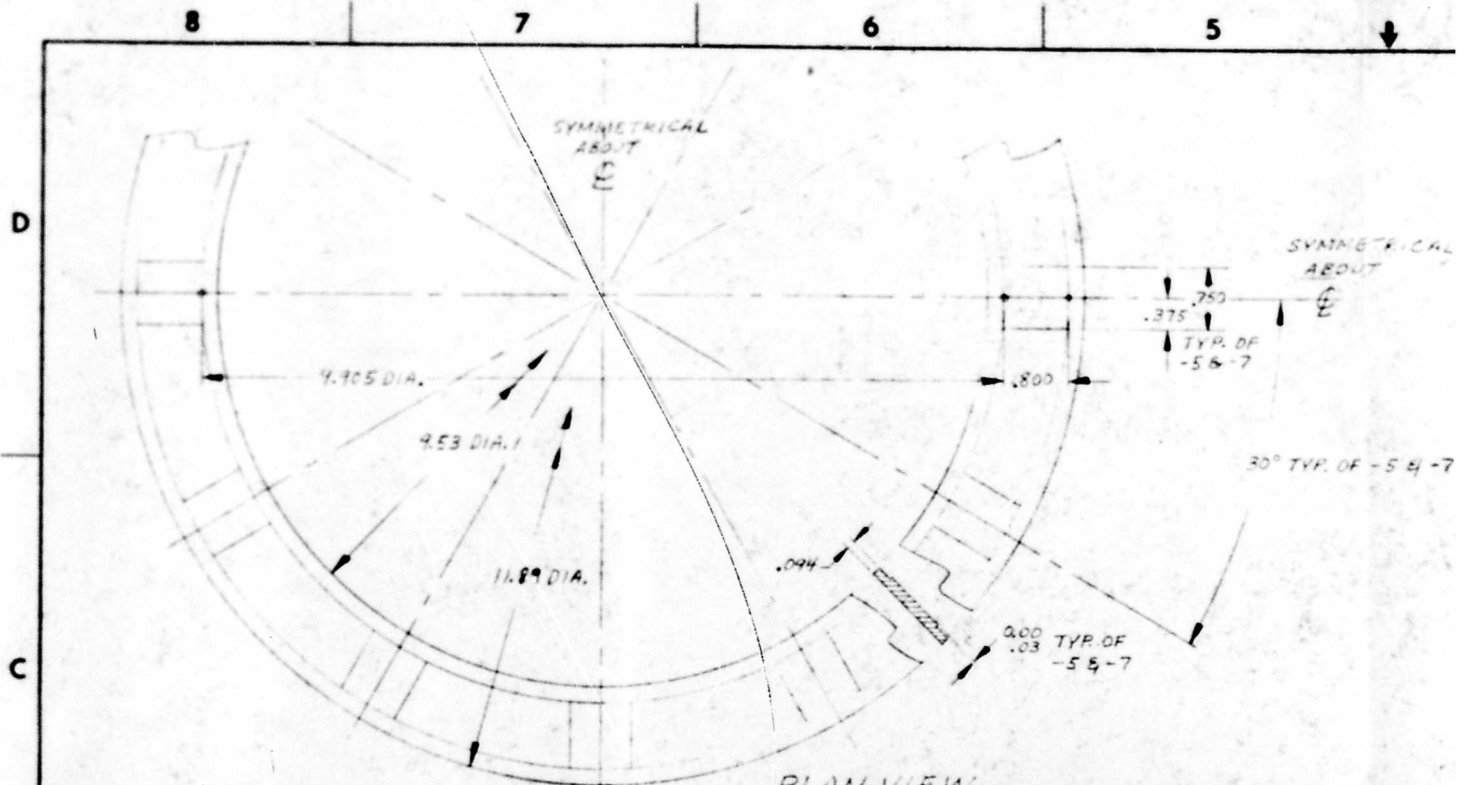


A-A

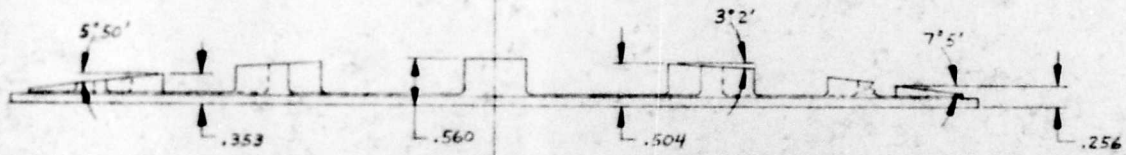
2. ¹²⁵ MACH. FINISH ALL OVER

① MATERIAL AVAILABLE FROM 4TCAD STOCK, ACCT # 10513

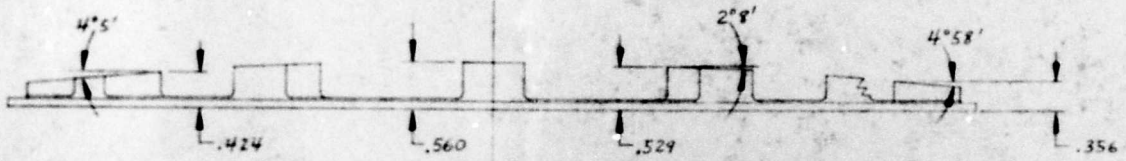
NOTE: UNLESS SPECIFIED OTHERWISE



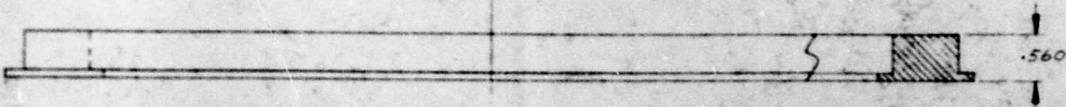
PLAN VIEW
TYP. OF -3,-5,-7
EXCEPT AS NOTED



DETAIL -7 (FOR ±3.5° TRACK)



DETAIL -5 (FOR ±2.5° TRACK)



DETAIL -3

1.125 MACH. FINISH ALL OVER
NOTE:

4 | 3 | 2 | 1

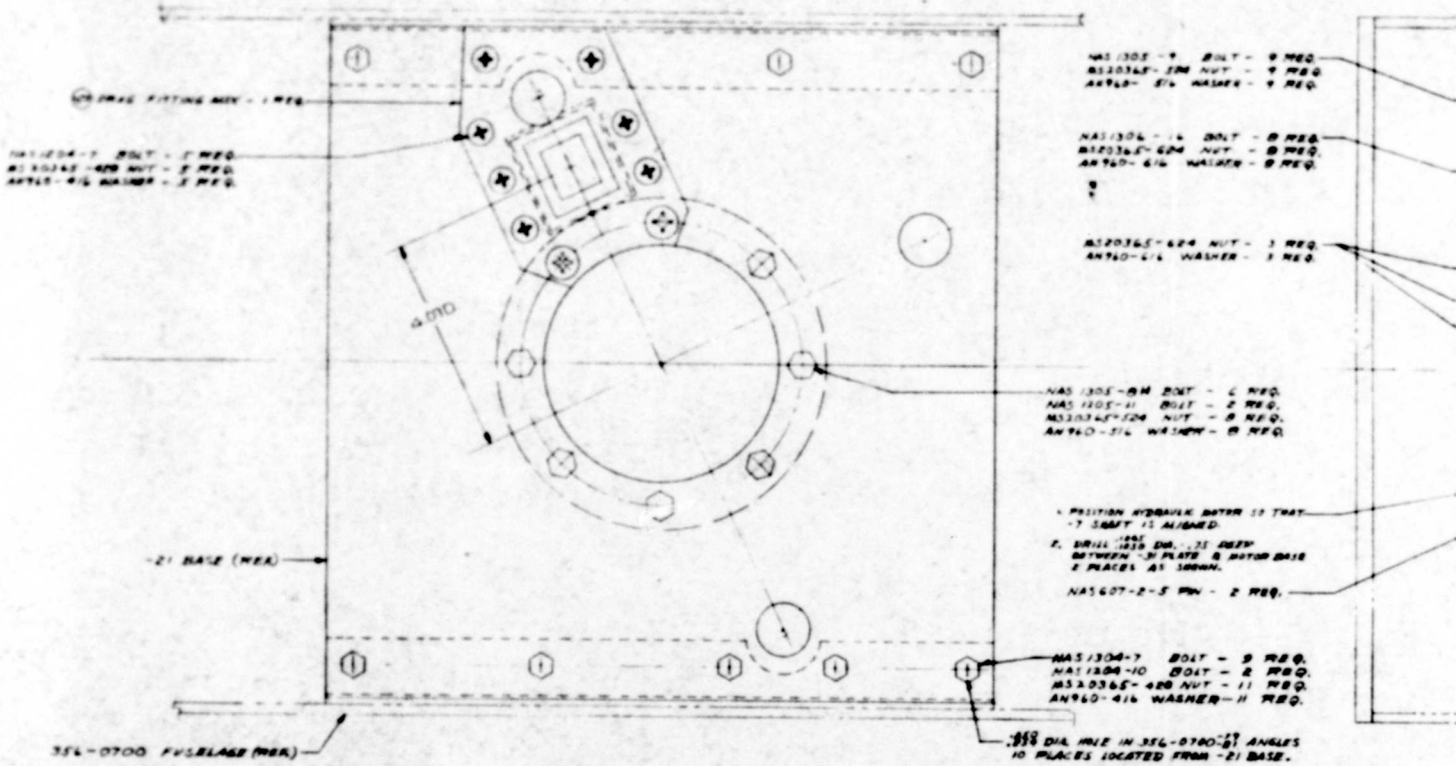
EFFECTIVE	REVISIONS					
	ON	ZONE	LT	DESCRIPTION	DATE	APPROV'D DATE

INDUSTRIAL
 100-54-7

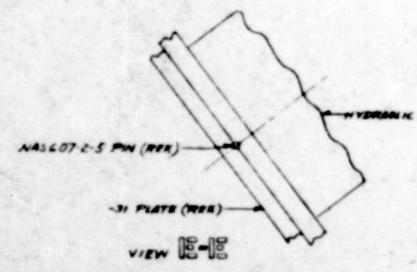
356-1006

PART NO.	NAME	SIZE	DESCRIPTION	SPECIFICATION	ZONE
-7	RING	3/4 x 12.5 DIA	STL PLATE	A137101B, C1116 OR ASTM-A-7	
-5	RING	3/4 x 12.5 DIA	STL PLATE		
-3	RING	3/4 x 12.5 DIA	STL PLATE		

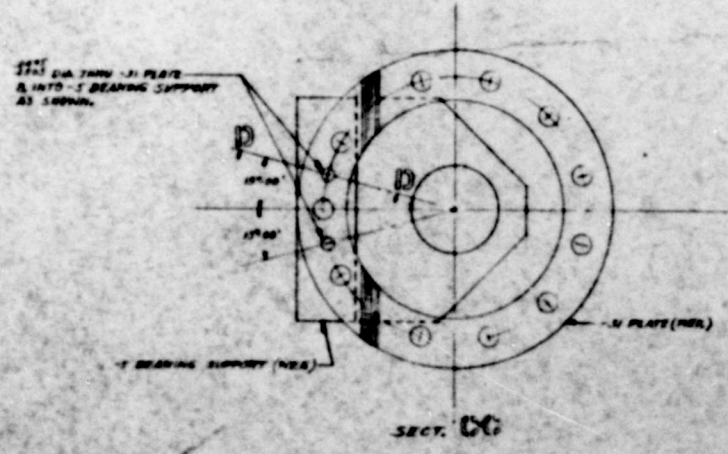
UNLESS OTHERWISE SPECIFIED DIMENSIONS ARE IN INCHES DECIMALS TO THIRDS 3 PLACE DECIMALS & 0.01 2 PLACE DECIMALS & 0.05				CONTRACT NO. DWRN O. FLOWE 15476		HUGHES TOOL COMPANY AIRCRAFT DIVISION CULVER CITY, CALIFORNIA	
MATERIAL AND PROCESS 11(9) 1(6) 1(9) 1(6) 1(3) 1(3)				LIST OF MATERIAL DRG TITLE RING-CAM TRACK MOUNT, ONR ROTOR/WING WIND TUNNEL MODEL		DRG NO. 356-1006	
FROM THIS APPLICATION QTY REQD				H/CAD APPROVAL APPROVAL		SIZE CODE IDENT NO. D 02731	
				SCALE 1/1		SHEET	



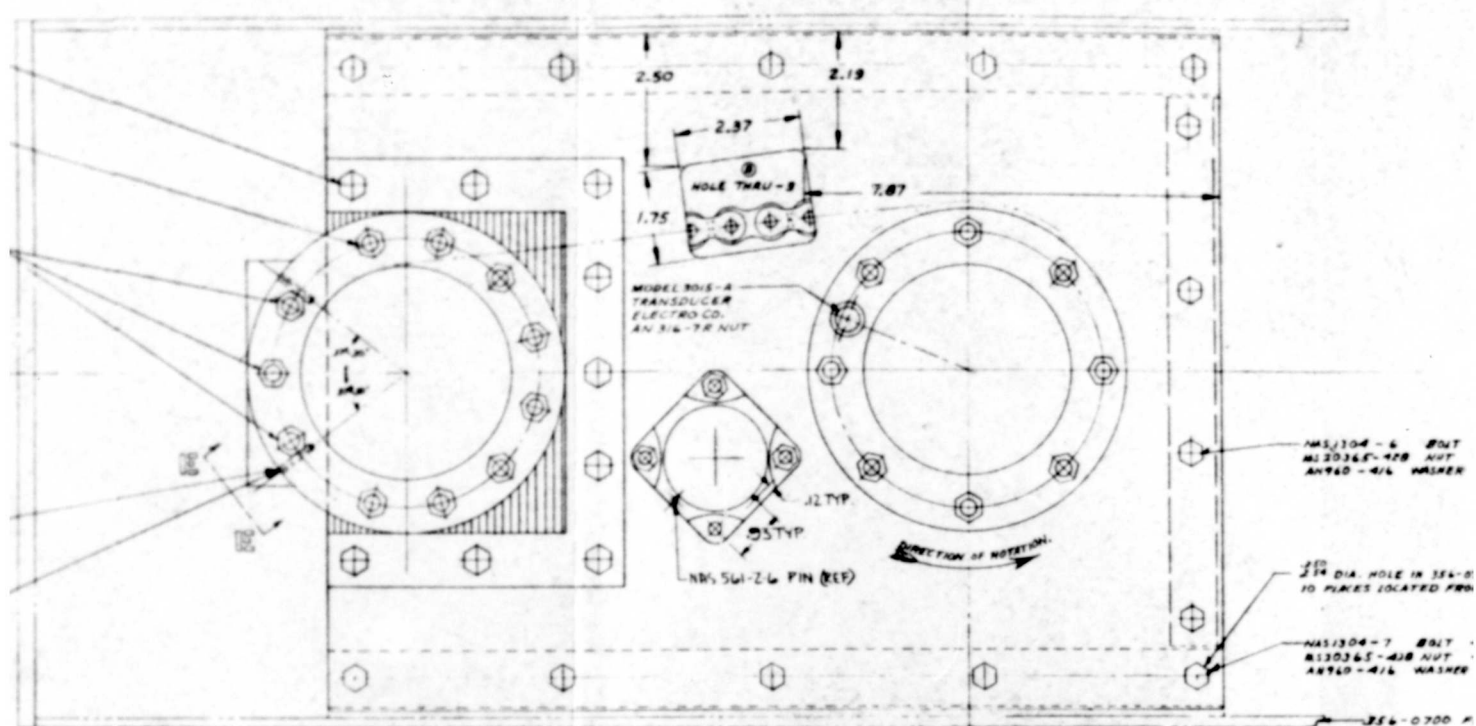
VIEW A-A



HYDRAULIC MOTOR
 VICEE'S #MF40-50B-50Y-4
 (FLANGE REVISED TO HAVE 24 BOLT)

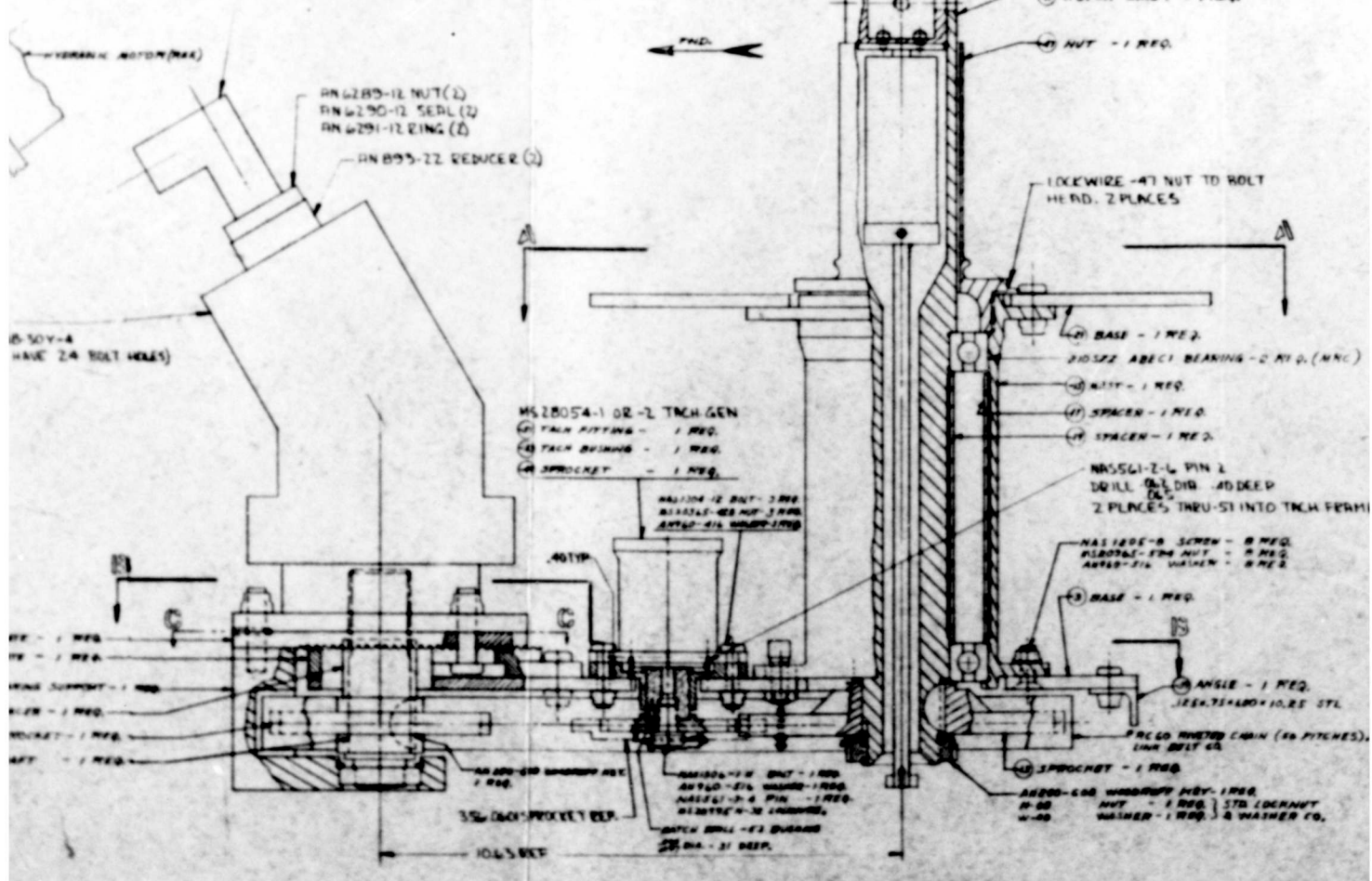


- ① PLATE - 1 REQ.
- ② PLATE - 1 REQ.
- ③ BEARING SUPPORT - 1 REQ.
- ④ SPACER - 1 REQ.
- ⑤ SPROCKET - 1 REQ.
- ⑥ SHAFT - 1 REQ.



VIEW B-B

MS 2190B-12 ELBOW (2)



REVISIONS					
REV	DATE	DESCRIPTION	BY	APP'D	DATE
A		STURVED FIG. AT MOTION			
		STURVED 154. DRAW SPOCKET REF			
B		ADDED BUSHES HOLE IN B BRIS			
		FOR STURVED AND V LINE			

WAS-104-6 NUT - 4 REQ.
 WAS-104-7 NUT - 4 REQ.
 WAS-104-8 WASHER - 4 REQ.

1/8" DIA. HOLE IN 356-0700 - 17 ANGLES
 IS PLATE ISOLATED FROM -3 MALE.

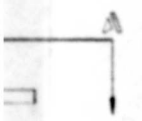
WAS-104-7 NUT - 10 REQ.
 WAS-104-8 NUT - 10 REQ.
 WAS-104-9 WASHER - 10 REQ.

356-0700 FUSELAGE (MKA)

- 1 REQ.

- 1 REQ.

T TO HOLT



BEARING - 2 AT Q. (MKA)

V.2
 W.2

VIN 2
 IS ADDED
 NEW-S1 INTO TNA FERRE

WAS-104-6 NUT - 4 REQ.
 WAS-104-7 NUT - 4 REQ.
 WAS-104-8 NUT - 4 REQ.

ANGLE - 1 REQ.
 WAS-104-10 NUT 17L

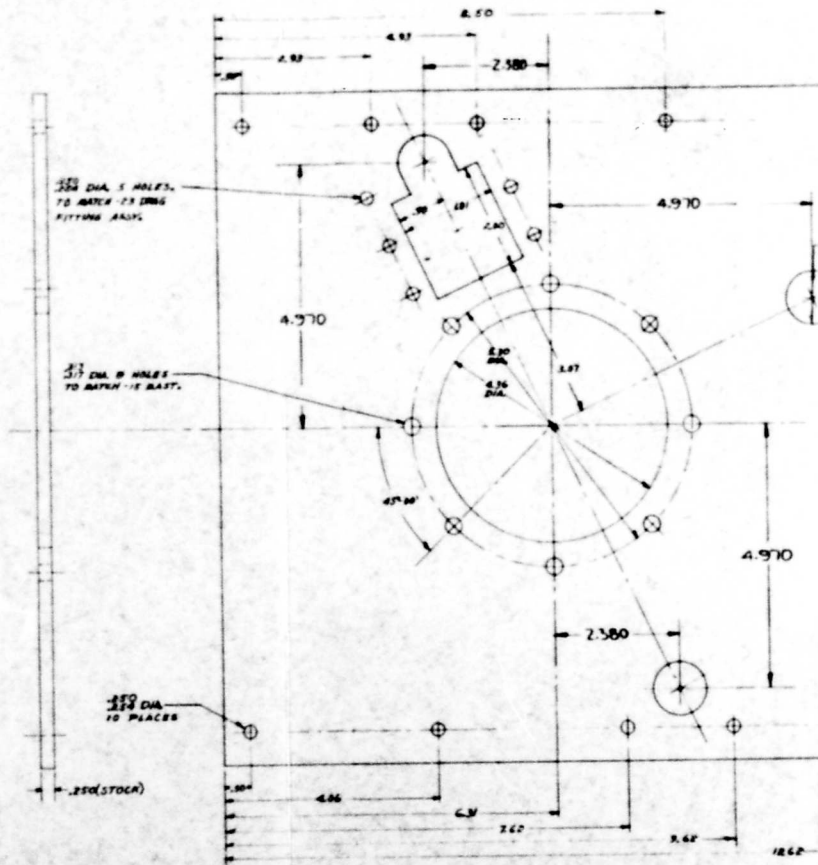
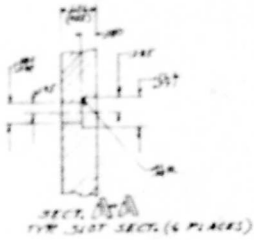
WASHER (1/4" (16 PITCHES)) 1 REQ.
 17L 0L

WAS-104-6 NUT - 4 REQ.
 WAS-104-7 NUT - 4 REQ.
 WAS-104-8 WASHER CO.

356-1100
 B

RELEASE FOR FABRICATION 10-19-69
 KEV W 1064

PROPULSION SYSTEM									
356-1100									



DETAIL -21 BASE
.850x13.00x1.00 4130 ST2. SMT
MIL-S-18729 COND. A

26 BUSHINGS - 1 REQ.
.850 x 1.50 x .125 DILITE BRONZE.
MIL-B-5687 TYPE I, CORR. A.

27 HOUSING - 1 REQ.
.850 x 4.00 x 6.00 4130 ST1W
MIL-S-6758 COND. A

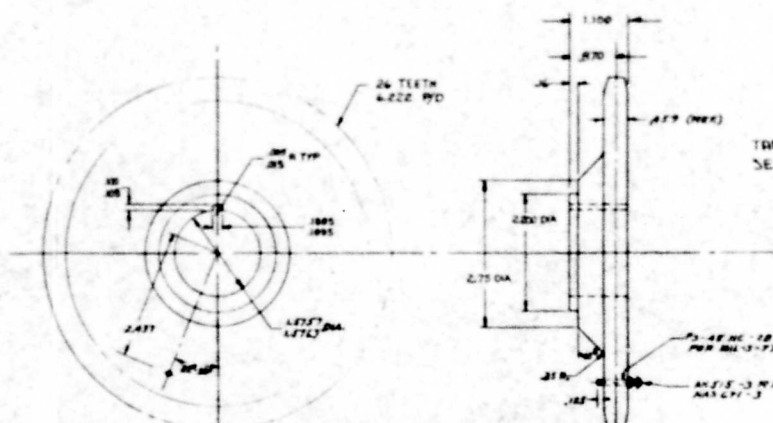
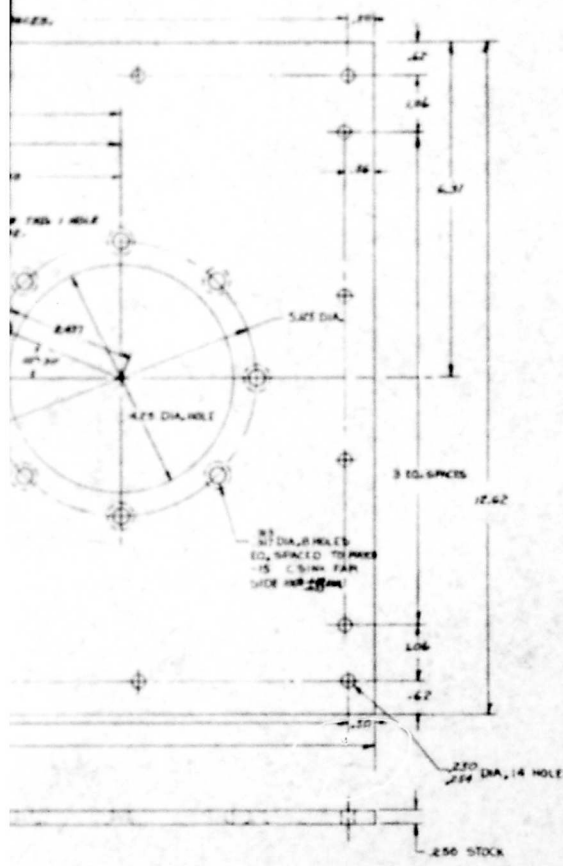
3/32 DIA. 2 HOLES
1/16" x 3/32" DIA. CSK.
TO MATCH -21 BASE.

.010 CORNER R. TYP.
IN -27

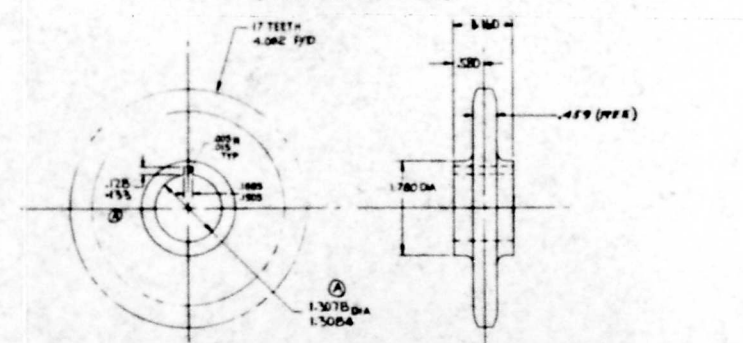
CHAMFER .030 x 45° TYP.
-25 CORNERS

3/32 DIA. 2 HOLES
1/16" x 3/32" DIA. CSK.
TO MATCH -11 BRG.

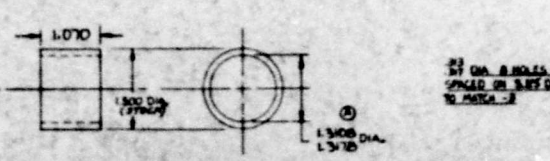
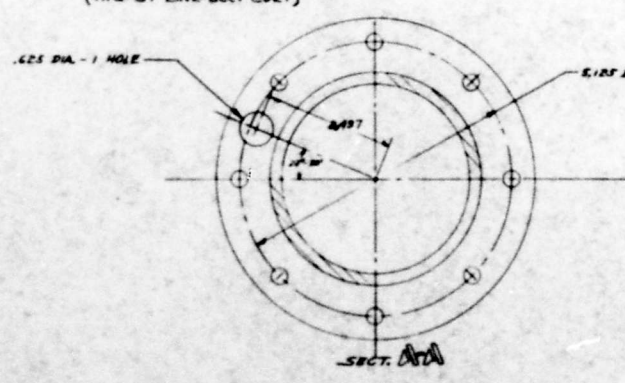
DETAIL -23 BRG FITTING ASSY.
CONSISTS OF -25 BUSHING & -27 HOUSING.



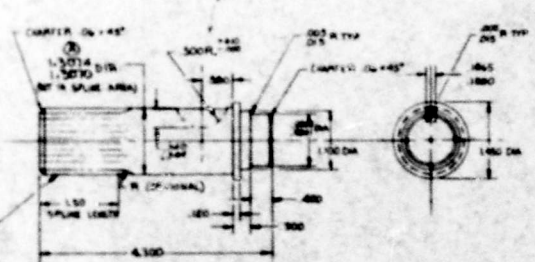
DETAIL -13 SPROCKET
 MAKE FROM SAE 1040 STEEL (THRU HARDENING) (45-50 ROCKWELL)
 (MFG BY LINK-BELT CORP)



DETAIL -41 SPROCKET
 MAKE FROM SAE 1040 STEEL (THRU HARDENING) (45-50 ROCKWELL)
 (MFG BY LINK-BELT CORP)

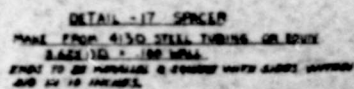
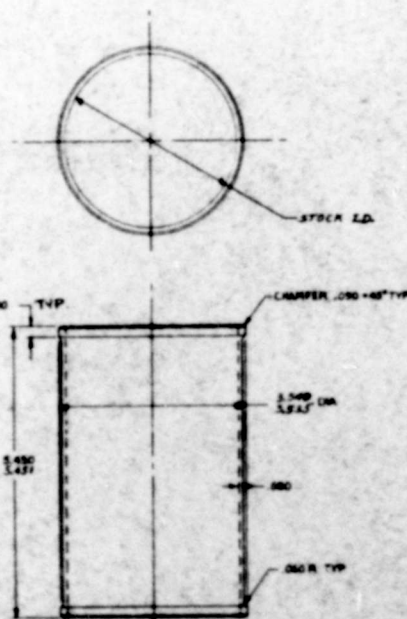
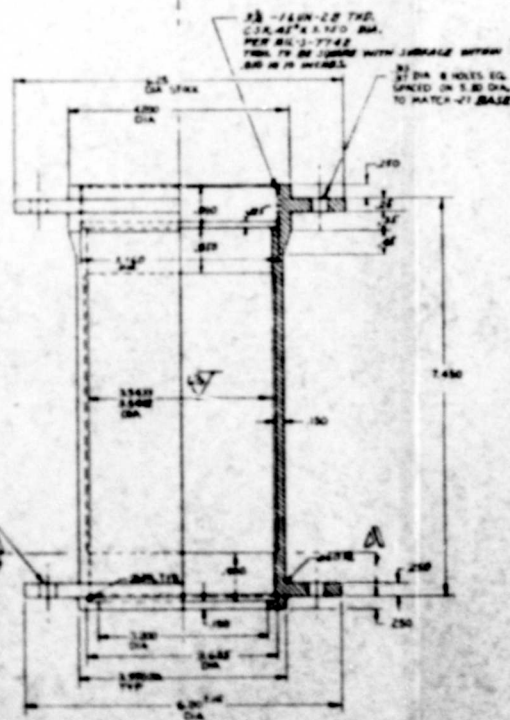
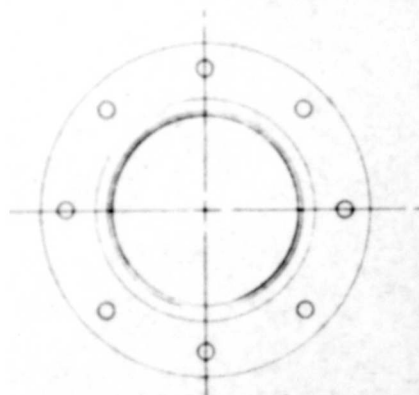
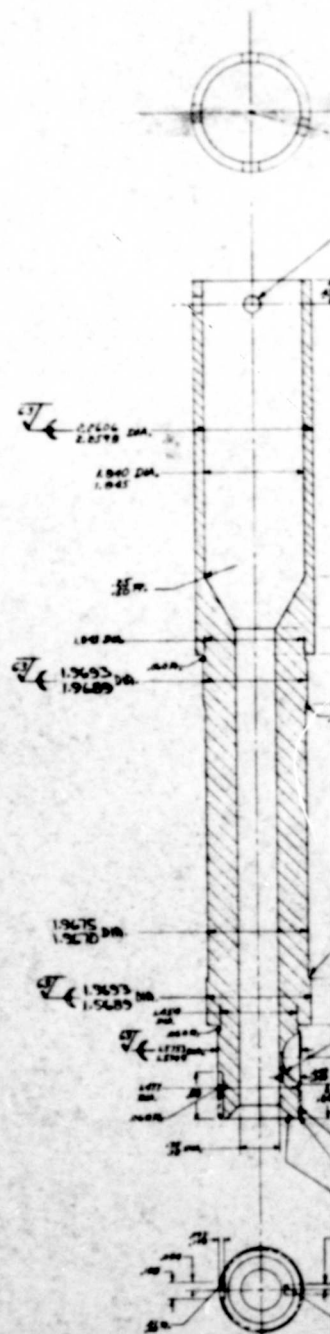
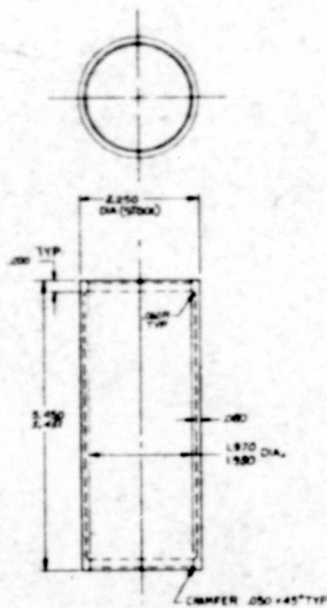
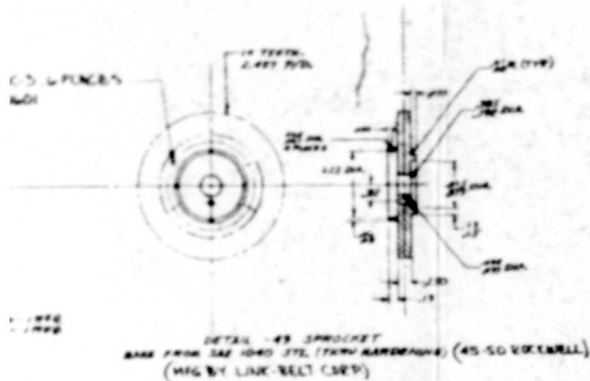


DETAIL -9 SPACER
 MAKE FROM BAR STEEL 4130 MIL-S-6788 COND.F4



DETAIL -7 SHAFT
 MAKE FROM BAR STEEL 4130 MIL-S-6788 COND.D3
 HEAT TREAT TO 115,000 PSI

10-1-1968
 MD-1-100
 4130-4.30

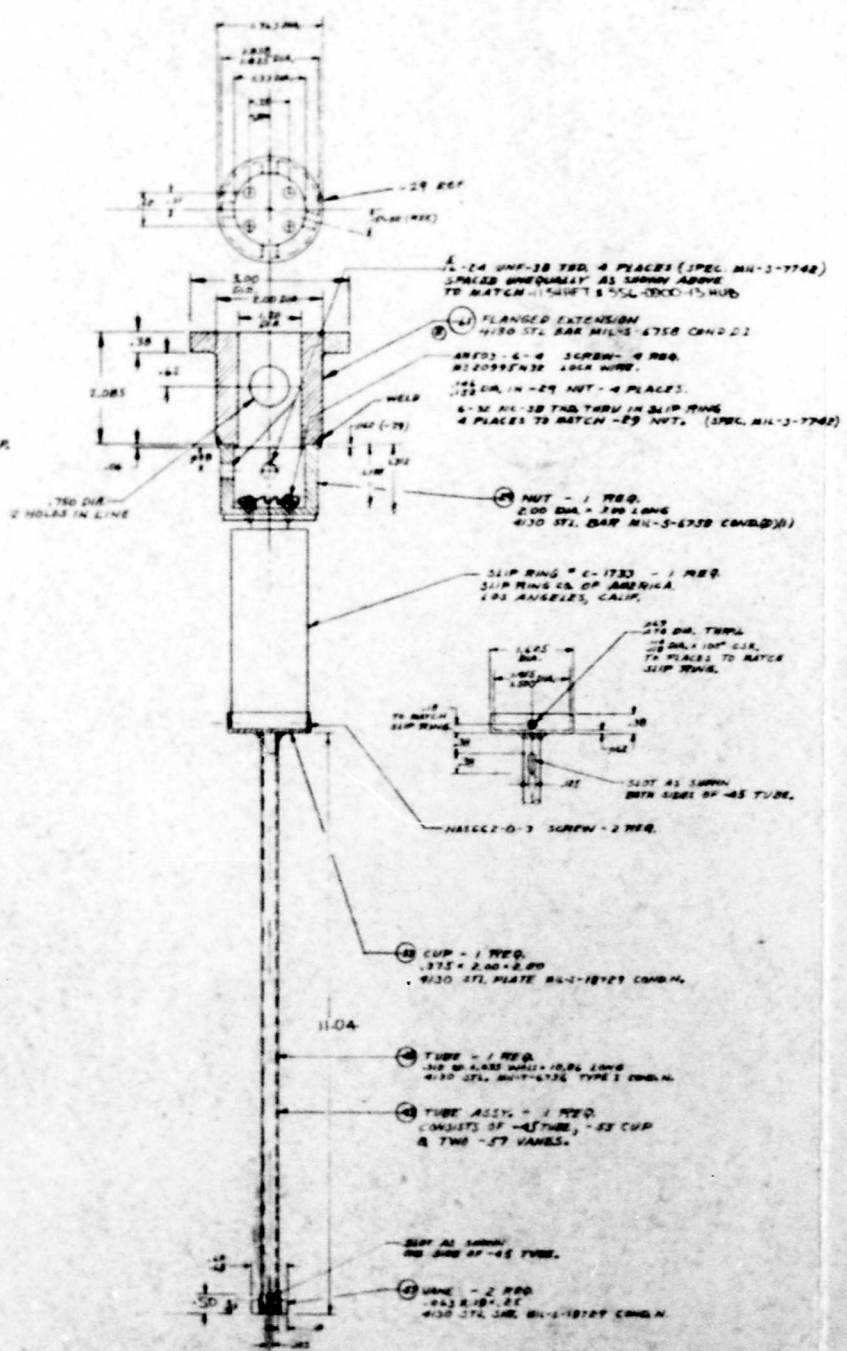


24 UNF-38 THD. 4 PLACES (SPEC. MIL-S-7742)
SPACED UNIFORMLY AS SHOWN ABOVE
TO MATCH -15 SHEET & 55L-0000-15 HUB

24 UNF-38 THD. 4 PLACES (SPEC. MIL-S-7742)
SPACED UNIFORMLY AS SHOWN ABOVE
TO MATCH -15 SHEET & 55L-0000-15 HUB

BREAK CORNERS
1/8" (MIN.)
1/16" (MIN.)

FROM FITTING,
1/32" STL. BAR
10" L. X 4"
IF AS SHOWN



DETAIL -35 SLIP RING ASSY - CONSISTS OF
-43 TUBE ASSY, C-1733 SLIP RING
& -29 NUT.

APPENDIX H
STRUCTURAL ANALYSIS

APPENDIX H
STRUCTURAL ANALYSIS

The structural analysis for the Rotor/Wing wind tunnel model is presented in this Appendix. Throughout the analysis, a factor of safety of five has been used.

The maximum loads expected are:

	<u>Wing</u>	<u>Tail</u>	<u>Model Minus Tail</u>
Lift	363	254	- -
Drag	157	- -	242
Side force	- -	73	25
Pitching, steady	260	- -	- -
Moment, alternating	<u>+30</u>	- -	- -
Rolling, steady	87	- -	- -
Moment, alternating	<u>+30</u>	- -	- -
Yawing moment	- -	347	43

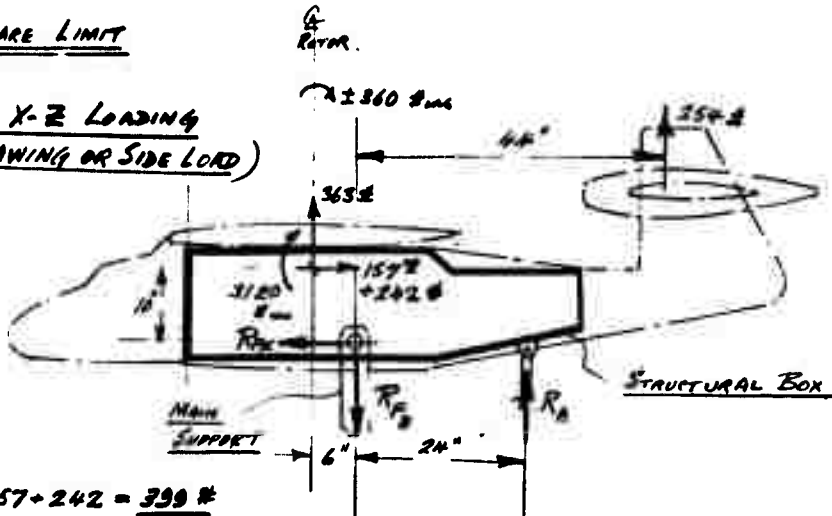
Forces in pounds; moments in foot-pounds

WIND TUNNEL MODEL

CG Location is on ϕ of rotor 10" above load point

LOADS ARE LIMIT

i) MAX X-Z LOADING
(NO YAWING OR SIDE LOAD)



$$R_{FX} = 157 + 242 = \underline{399 \#}$$

$$R_A = \frac{3120 + (363 \times 6) + (399 \times 10) - (254 \times 44)}{24} \pm \frac{360}{24}$$

$$= \underline{79 \# \pm 15 \#} \quad \therefore R_{FZ} = 363 - 79 + 254 = \underline{538 \# \pm 15 \#}$$

ii) MAX XY LOADING
(+ 1/2 VALUES OF X-Z LOADS ABOVE)

$$R_1 = 100 + \frac{516 - (25 \times 6) + (73 \times 51)}{12} = \underline{441 \#}$$

$$R_Y = 73 + 25 = \underline{98 \#}$$

$$\therefore R_2 = 441 - 200 = \underline{241 \#}$$

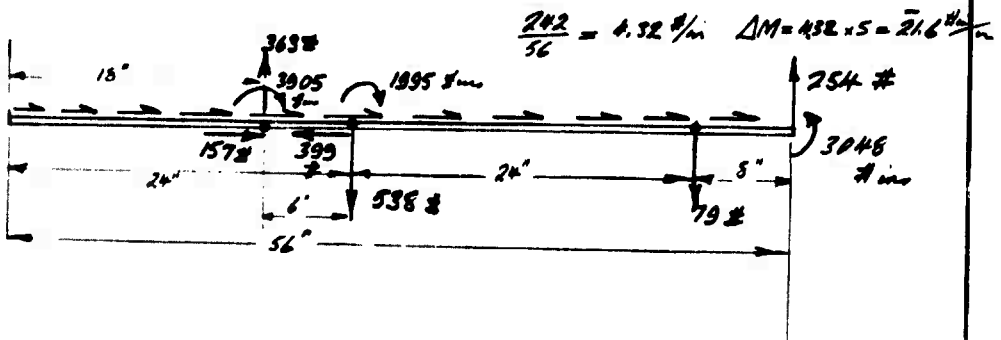


WIND TUNNEL MODEL

VERTICAL BMS ON STRUCTURAL BOX — LIMIT LOADS

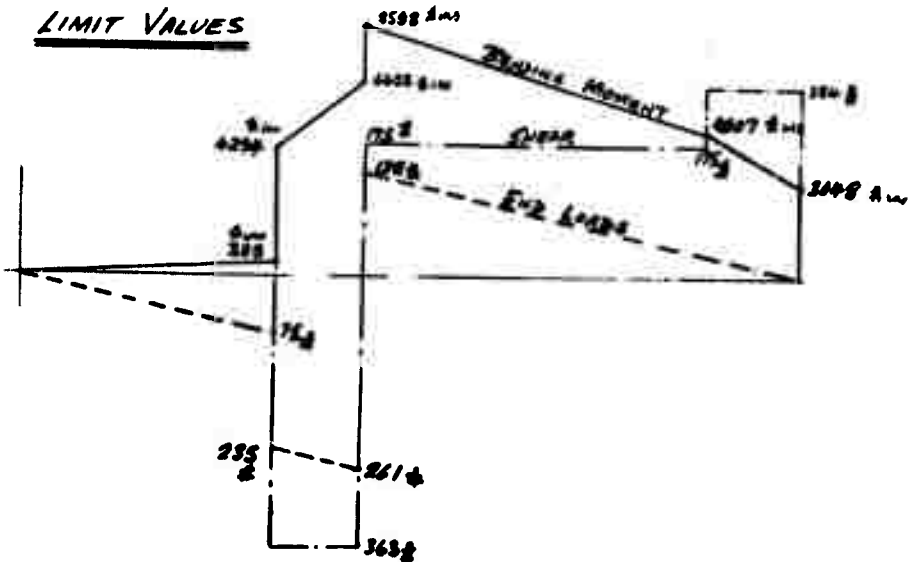
Assumptions: —

- i) 363 # LIFT + 3120 # in applied as concentrated loads on shaft
- ii) 399 # DRAG applied as a concentrated 157 # and 242 # as a uniform load (5' above N. Axis.)
- iii) Take out the cyclic load until later



VERTICAL BMS SHEARS & END LOADS

LIMIT VALUES

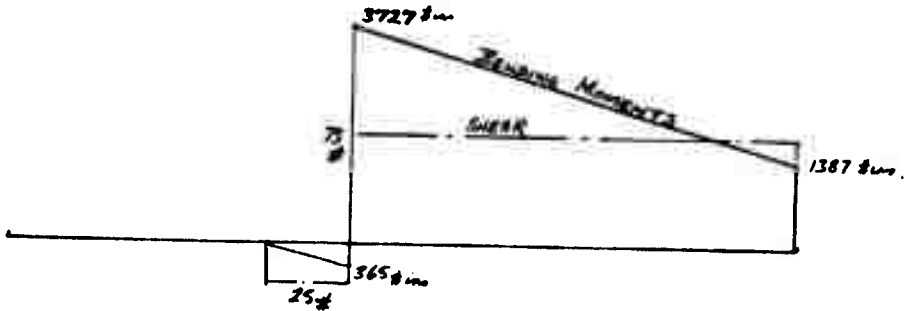
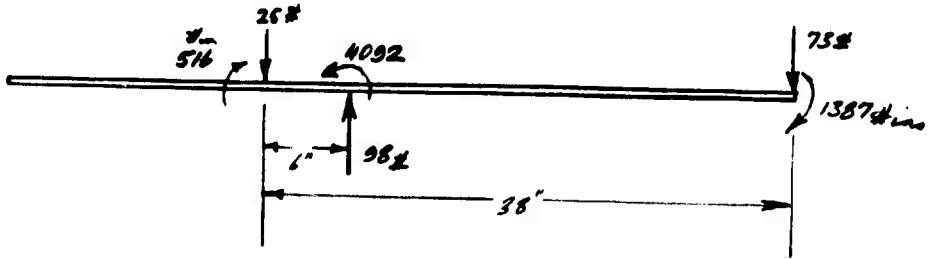


WIND TUNNEL MODEL

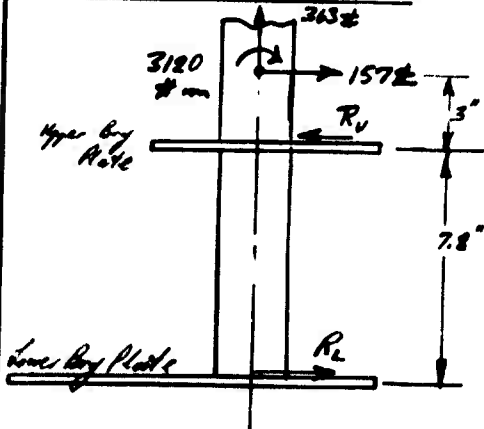
HORIZONTAL BMs ON STRUCTURAL BOX

(APPLIED AT SAME TIME AS $\frac{1}{2}$ MAX. VERTICAL)

LIMIT LOADS



SHAFT BEARING REACTIONS — DUE TO WING LOADS



$$\begin{aligned}
 R_u &= 157 \times \frac{10.8}{7.8} + \frac{3120}{7.8} \\
 &= \underline{618 \#} \\
 R_L &= \underline{360 \#}
 \end{aligned}
 \left. \vphantom{\begin{aligned} R_u \\ R_L \end{aligned}} \right\} \underline{\underline{LIMIT LOADS}}$$

WIND TUNNEL MODEL

SECTION @ MAX. VERTICAL B.M.

$$M = 8,600 \text{ kg. ins. (LIMIT)}$$

$$\text{ULT. FACTOR} = 5.0$$

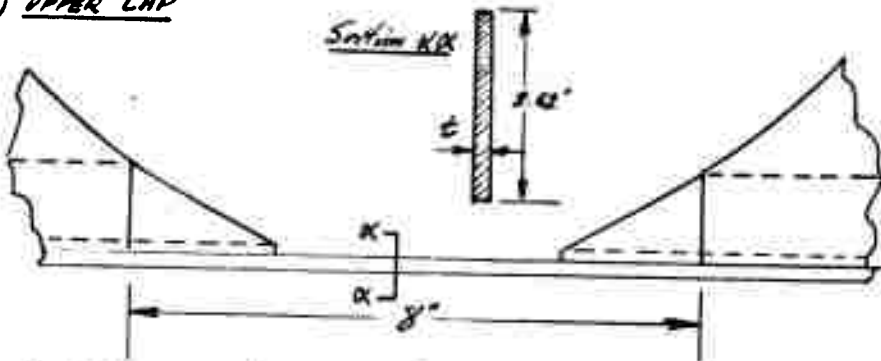
$$= 17,200 \text{ " " (ULT.)}$$

TAKE AS A COUPLE $h = 12"$

$$\frac{M}{h} = 3,580 \text{ lbs.}$$

THIS IS TOTAL (IS FOR 2 SIDES) $\therefore P = 1790 \text{ lbs./side}$

a) UPPER CAP



$$L = 8" \quad \rho = \frac{t}{\pi R} = .183t$$

$$\text{MATE} = 24\text{ST.} \quad A = 2.62t$$

$$\text{TRY } t = .312 \quad \rho = .09 \quad \frac{1}{\rho} = 89 \quad f_c = 12,000 \frac{\text{psi}}{\text{in}^2} \quad A = .815 \text{ in}^2$$

$$\frac{P}{A} = \frac{1790}{.815} = 2,190 \frac{\text{psi}}{\text{in}^2} \quad \text{M.S. HIGH}$$

$$\text{TRY } t = .25" \quad \rho = .072 \quad \frac{1}{\rho} = 111 \quad f_c = 7,500 \frac{\text{psi}}{\text{in}^2} \quad A = .656$$

$$\frac{P}{A} = \frac{1790}{.656} = 2730 \frac{\text{psi}}{\text{in}^2} \quad \text{M.S.} > 1.0$$

$$\text{TRY } t = .187 \quad \rho = .054 \quad \frac{1}{\rho} = 148 \quad I = \frac{2.62 \times .187^3}{12} = .00143$$

$$P = \frac{\pi^2 EI}{L^2} = \frac{3.14^2 \times 14,300}{8 \times 8} = 2,200 \text{ lbs} \quad \text{M.S. } + .23$$

b) LOWER CAP

THIS IS OK by examination, as the lower plate of the shaft support stabilizes it

✓

WIND TUNNEL MODEL

END PLATE ON TAIL ATTACH

VIEW LOCKING DOWN

LOADS SHOWN ARE ULTIMATE

$$\begin{aligned} \text{APPROX MAX BM} &= \frac{6840 + (.75 \times 438)}{2} \\ &= 3585 \text{ #in} \end{aligned}$$

$$f = \frac{M}{Z} \quad Z = \frac{bt^2}{6} = t^2$$

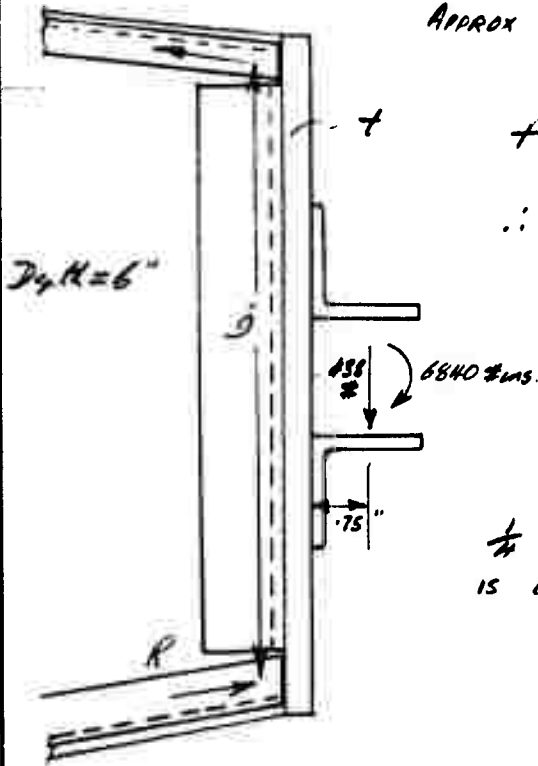
$$\therefore f = \frac{M}{t^2}$$

$$\text{Allowable } f_m = 56,000$$

$$t^2 = \frac{3585}{56,000} = .064$$

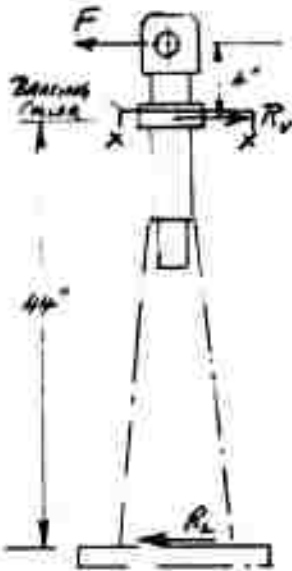
$$t = .252''$$

$\frac{1}{4}''$ will be OK as the analysis is conservative.



WIND TUNNEL MODEL

MOUNTING MAST & BRACING



$F =$ APPLIED LOAD FROM MODEL

$$R_v = \frac{48}{44} F = 1.09 F$$

$$R_L = .09 F$$

Max. BM ON SECTION XX

CASE (i) $F_x = 399 \#$ (LIMIT)

$F_y = 0$ $T_0 = 0$

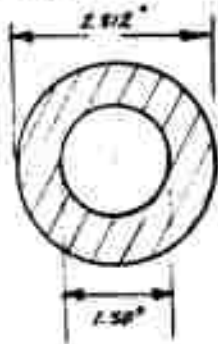
$M = 399 \times 4 = \underline{1596 \# \text{ IN.}} \text{ LIMIT}$

CASE (ii) $F_x = 200 \#$ (LIMIT)

$F_y = 98 \#$ (LIMIT) $T_0 = 4092 \# \text{ IN.}$ (LIMIT)

$M = \sqrt{200^2 + 98^2} \times 4 = \underline{893 \# \text{ IN.}} \text{ LIMIT}$

SECTION XX



$$I_1 = 2.1783$$

$$I_2 = \frac{.3313}{1.8470}$$

$$I_P = 2 \times 1.847 = \underline{3.694 \text{ in}^4}$$

$$Z_{\text{BENDING}} = \frac{1.847}{1.406} = \underline{1.312 \text{ in}^3}$$

$$Z_{\text{TENSION}} = \frac{3.694}{1.406} = \underline{2.625 \text{ in}^3}$$

Case (i) $f_b = \frac{5 \times 1596}{1.312} = \underline{6,100 \#/\text{in}^2}$

$f_{Tn} = 90,000 \#/\text{in}^2$ M.S. HIGH

Case (ii) $f_b = \underline{3410 \#/\text{in}^2}$

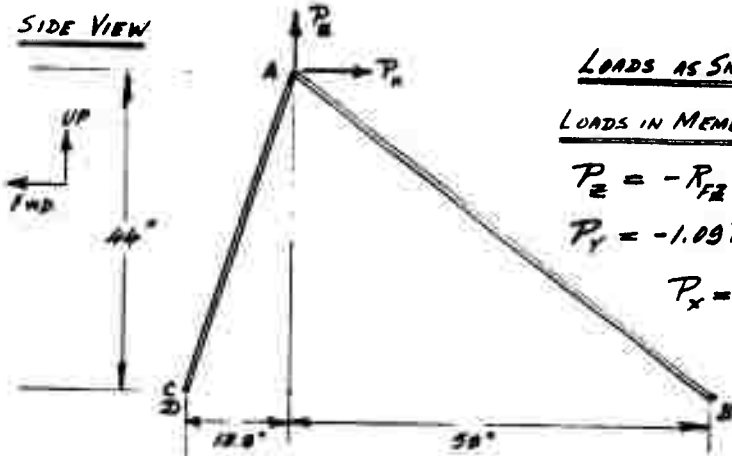
$f_s = \frac{5 \times 4092}{2.625} = \underline{7,800 \#/\text{in}^2}$

COMBINED M.S. HIGH

WIND TUNNEL MODEL

MOUNTING MAST & BRACING

SIDE VIEW



LOADS AS SHOWN ARE +VE

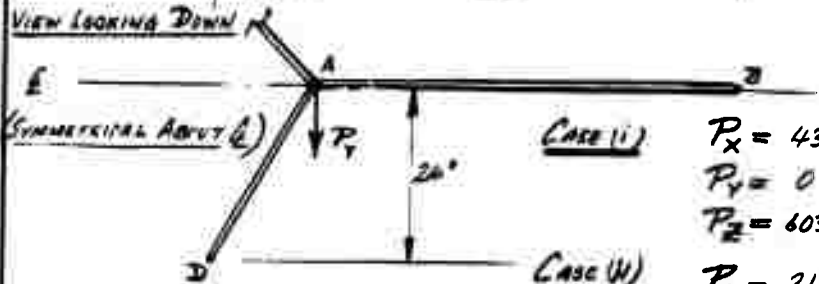
LOADS IN MEMBERS - TENSION = +VE

$$P_z = -R_{Fz} \text{ (PAGE 1)}$$

$$P_y = -1.09 R_{Fy}$$

$$P_x = -1.09 R_{Fx}$$

VIEW LOOKING DOWN



CASE (I)

$$P_x = 435 \#$$

$$P_y = 0$$

$$P_z = 603 \#$$

LIMIT LOADS

CASE (II)

$$P_x = 218 \#$$

$$P_y = 108 \#$$

$$P_z = 302 \#$$

LIMIT LOADS

GEOMETRY & DIRECTION COSINES.

MEMBER	x	y	z	x ²	y ²	z ²	L ²	L	cos X	cos Y	cos Z	Σ l ² (INCH ²)
AB	59	0	44	3481	0	1936	5417	73.60	.8016	0	.5978	.9999
AC	13.9	24	44	193	576	1936	2705	52.01	.2672	.4614	.8460	10000
AD	13.9	24	44	193	576	1936	2705	52.01	.2672	.4614	.8460	10000

a) X LOADS.

$$P_x + .8016 P_{AB} - .2672 P_{AD} - .2672 P_{AC} = 0 \quad \text{--- } \textcircled{1}$$

$$\& P_{AC} = P_{AD} \quad \therefore .5978 P_{AB} = -2(.846) P_{AC} \quad P_{AB} = -2.83 P_{AC}$$

$$\text{PUTTING THIS IN } \textcircled{1} \quad P_x - 2.265 P_{AC} - .5344 P_{AC} = 0$$

WIND TUNNEL MODEL

X LOADS - Cont'd

$$2.799 P_{AC} = P_x$$

$$P_{AC} = \underline{.357 P_x}$$

$$P_{AD} = \underline{.357 P_x}$$

THEN $P_{AB} = \underline{-1.010 P_x}$

b) Y LOADS

$$-.4614 P_{AC} + .4614 P_{AD} + P_y = 0$$

$$P_{AC} = -P_{AD}$$

$$\therefore .9228 P_{AD} = -P_y$$

$$P_{AD} = \underline{-1.083 P_y}$$

$$\underline{P_{AB} = 0}$$

$$P_{AC} = \underline{+1.083 P_y}$$

c) Z LOADS

$$P_z - .5978 P_{AB} - .8460 P_{AD} - .8460 P_{AC} = 0$$

$$P_{AD} = P_{AC}$$

$$.8016 P_{AB} = 2(.2672) P_{AD} \quad P_{AB} = .666 P_{AD}$$

THEN $P_z - .398 P_{AD} - .846 P_{AD} - .846 P_{AD} = 0$

$$P_z = 2.090 P_{AD}$$

$$P_{AD} = \underline{.478 P_z}$$

$$P_{AC} = \underline{.478 P_z}$$

$$P_{AB} = \underline{.318 P_z}$$

TOTALS

$$P_{AB} = -1.010 P_x + (0) P_y + .318 P_z$$

$$P_{AC} = +.357 P_x + 1.083 P_y + .478 P_z$$

$$P_{AD} = +.357 P_x - 1.083 P_y + .478 P_z$$

CASE	$\frac{-1.010}{P_x}$	$\frac{0}{P_y}$	$\frac{+.318}{P_z}$	P_{AB}	$\frac{+.357}{P_x}$	$\frac{+1.083}{P_y}$	$\frac{+.478}{P_z}$	P_{AC}	$\frac{+.357}{P_x}$	$\frac{-1.083}{P_y}$	$\frac{+.478}{P_z}$	P_{AD}
(i) $P_x = 435$ $P_y = 0$ $P_z = 603$	-439	0	+192	-247	+155	0	+288	+343	+155	0	+288	+443
(ii) $P_x = 215$ $P_y = 105$ $P_z = 302$	-220	0	+96	-124	+78	+117	+144	+339	+78	-117	+144	+105

THESE ARE ALL LIMIT LOADS

WIND TUNNEL MODEL

LOADING — CONTROL SYSTEM

ONE BLADE — TORQUE AT FEATHERING APM

$$T_0 = 110 \pm 110 \text{ lbs. in.}$$

(NOTE:— THIS VALUE WAS GIVEN BY BOB HEAD & IS A MAX. VALUE. FOR DEFLECTION STUDY AND ALSO FOR FATIGUE ANALYSIS THIS FIGURE WILL BE USED WITHOUT ANY FACTORS. HOWEVER, FOR THE ULTIMATE STRENGTH A FACTOR OF FIVE WILL BE USED)

Feathering Arm radius $r = 1.85''$

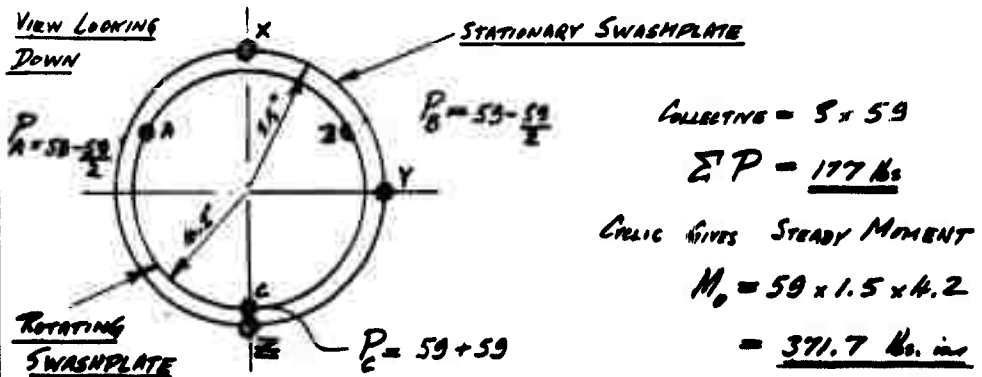
Loads in rods to rotating swashplate:—

$$P_1 = \frac{110 \pm 110}{1.85} = \underline{59 \pm 59 \text{ lbs. (FATIGUE)}}$$

$$\& P_1 = \frac{220 \times 5}{1.85} = \underline{595 \text{ lbs. (ULTIMATE)}}$$

Loads through swashplates:—

a) Consider lined up with the lateral arms



THEN $P_x = \frac{177}{2} - \frac{371.7}{11} = 54.7 \pm$ Similarly $P_z = 122.3 \pm$
 & of course $P_y = 0$

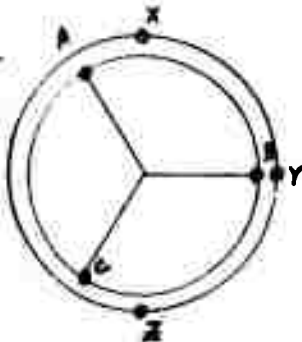
WIND TUNNEL MODEL

Cont'd

a) $P_z = \text{CRITICAL LOAD} = 5 \times 122.8 = \underline{612 \text{ lbs. ULT.}}$

b) Considered head up with long tubular arm.

VIEW FROM
ABOVE



$$P_A = 59 - 59/2$$

$$P_B = 59 + 59$$

$$P_C = 59 - 59/2$$

$$\Sigma P = 177$$

$$M_o = 371.7 \text{ #in}$$

$$P_x = P_z = \frac{177}{2} = 88.5 \text{ #}$$

$$P_y = \frac{371.7}{5.5} = 67.6 \text{ #. (LIMIT)} = \underline{\underline{338 \text{ lbs (ULT)}}$$

IT CAN BE SEEN FROM THE FOREGOING THAT THE LOADS USED FOR PRELIMINARY ANALYSIS (PAGES 1-6) ARE CONSERVATIVE

WIND TUNNEL MODEL

STIFFNESS CONSTANTS FOR BLADE SPAR TUBE AND FOR CONTROL SYSTEM

BLADE SPAR TUBE IS $\frac{3}{4}$ " $\frac{1}{2}$ " x .120" WALL - STEEL

FLEXURAL STIFFNESS PER UNIT LENGTH = CONSTANT EI

$$EI = \underline{366,000 \text{ lbs. in}^2}$$

TORSIONAL STIFFNESS PER UNIT LENGTH = CONSTANT GJ

$$GJ = \underline{292,800 \text{ lbs. in}^2}$$

SPRING CONSTANT OF CONTROL SYSTEM:-

AT PITCH ARM $K = \underline{54,300 \text{ lbs. in per radian}}$

(THE ABOVE IS THE ELASTIC DEFLECTION ONLY,

NO ACCOUNT IS TAKEN OF SLOP IN SYSTEM)

NOTE:- 68% OF THE DEFLECTION TAKES PLACE IN THE NON-ROTATING PART OF THE CONTROL SYSTEM, THE REMAINING 32% BEING IN THE ROTATING PART.

MOMENT OF INERTIA OF CONTROL SYSTEM

$$I_{\text{TOTAL}} = \underline{.003871 \text{ SLUGS. FT}^2}$$

$$\text{ROTATING SYSTEM } I = \underline{.001793 \text{ SLUGS. FT}^2}$$

$$\text{NON-ROTATING SYSTEM } I = \underline{.002078 \text{ SLUGS. FT}^2}$$

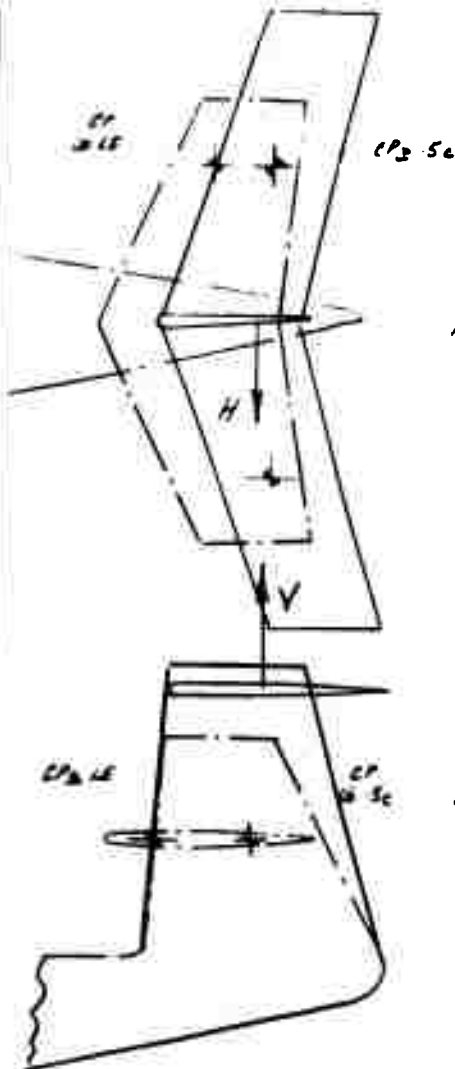
WIND TUNNEL MODEL

REVISED EMPENNAGE

PREVIOUS EMPENNAGE SHOWN SOLID

DOTTED

LOADS WILL BE RATED UP AS
FEN AREAS



OLD HORIZ WAS 3.61 ft²
NEW HORIZ IS 4.17 ft²

$$\therefore \text{FACTOR} = 1.15$$

MAX LIFT OR DOWN LOAD ON TAIL

$$= 254 \times 1.15 = \underline{292 \#} \quad (\text{LIMIT})$$

OLD VERT WAS 2.10 ft²
NEW VERT IS 2.88 ft²

$$\therefore \text{FACTOR} = 1.37$$

MAX SIDE LOAD ON TAIL

$$= 1.37 \times 73 = \underline{100 \#} \quad (\text{LIMIT})$$

CENTERS OF PRESSURE ARE AS MARKED.

ULTIMATE LOAD FACTOR = 3.0

$$V = 3 \times 292 = \underline{876 \#} \quad (\text{ULT})$$

$$\& H = \underline{300 \#}$$

CONSERVATIVELY, WITH SIDE LOAD TAKE ROLLING MOMENT ON HORIZ SURFACE, AS FOLLOWS:-

$$\text{SYMM. COMPONENT} = \frac{2}{3} V \quad \text{ASYMM. COMP.} = \frac{1}{3} V$$

WIND TUNNEL MODEL

CONTINUED WIND SPEED $V = 554 \text{ *}$ $\frac{V}{2} = \underline{292 \text{ *}/\text{SIDE}}$ (ULTIMATE)

$\therefore \text{HLS} = 292 + 146 = 438 \text{ * (VLT)}$

$\text{LLS} = 292 - 146 = 146 \text{ * (VLT)}$

HORIZONTAL SURFACE:

CRITICAL CASE IS UN-SYMM WITH CPD SC $\text{HLS} = 438 \text{ * (VLT)}$

MISSING SIDEWIND LEADING IS UN-SYMM (CONSERVATIVE)

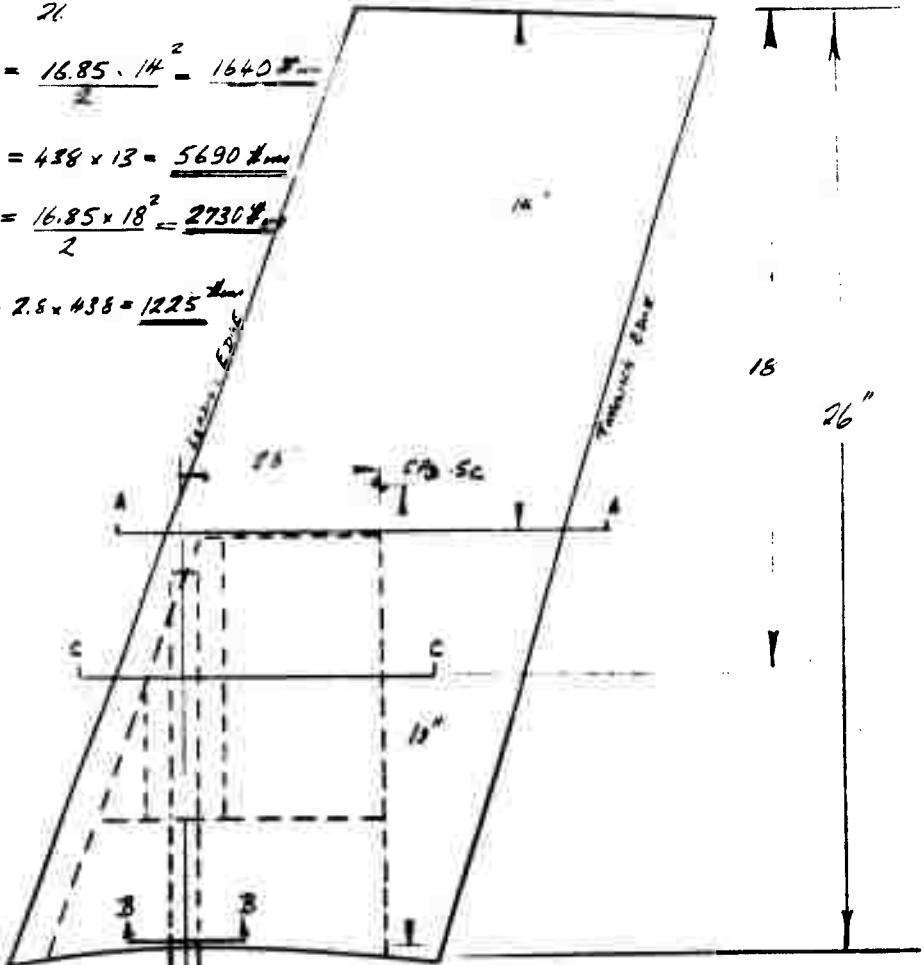
$w = \frac{438}{26} = 16.85 \text{ *}/\text{m}$

$M_{AA} = \frac{16.85 \cdot 14^2}{2} = 1640 \text{ *}$

$M_{BB} = 438 \times 13 = 5690 \text{ *}$

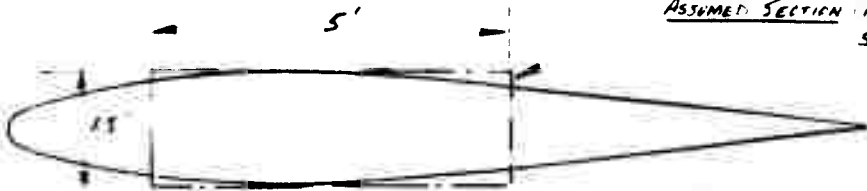
$M_{CC} = \frac{16.85 \times 18^2}{2} = 2730 \text{ *}$

$T_{0 \text{ BB}} = 2.5 \times 438 = 1095 \text{ *}$



WIND TUNNEL MODEL

SECTION AA



ASSUMED SECTION (FOR SIMPLICITY)

$$M_{AA} = 1640 \text{ #in.}$$

$$Z = \frac{5 \times 1.5^2}{6} = 1.875$$

$$\frac{M}{Z} = \frac{875 \text{ #in.}^2}{1}$$

M.S. HIGH

MANCANY

SECTION BB



$$Z_{\text{BENDING}} = .0413 \text{ in.}^3$$

$$Z_{\text{TORSION}} = .0526 \text{ in.}^3$$

$$M = 5636 \text{ #in.}$$

$$T_0 = 1225 \text{ #in.}$$

$$\frac{M}{Z} = 138,000 \text{ #in.}^2$$

$$\frac{T_0}{Z} = 14,800 \text{ #in.}^2$$

4130 STEEL
 $f_u = 21,000 \text{ #in.}^2$

Allowable Stress
 (Plastic Bending)

$$f_{\text{bending}} = 16,000 \text{ #in.}^2$$

$$f_s = 52,000$$

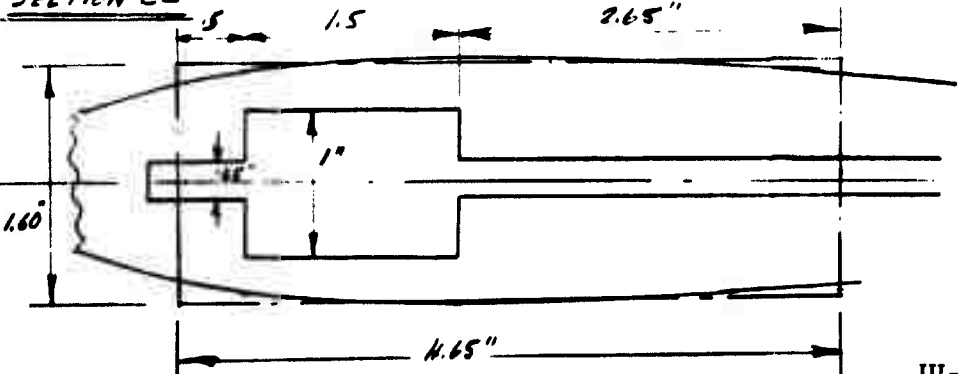
$$R_B = .852$$

$$R_s = .285$$

$$M.S. = \frac{1}{\sqrt{R_B^2 + R_s^2}} - 1 = \frac{1}{\sqrt{.725 + .0815}} - 1$$

M.S. + .10

SECTION CC



WIND TUNNEL MODEL

SECTION CC - CONT'D

$$N.G. \bar{I}_{AA} = \frac{(1.60^3 \times 4.15) - (25^3 \times 3.15) - (1^3 \times 1.5)}{12}$$

$$= \frac{1810 - 105 - 1.5}{12} = \frac{17.45}{12} = 1.45 \text{ m}^4$$

$$Z = \frac{1.45}{.81} = 1.81 \text{ m}^3$$

$$\frac{M}{Z} = \frac{2730}{1.81} = 1500 \text{ #/m}^2$$

M.S. HIGH

VERTICAL SURFACE
(ULTIMATE LOADS)

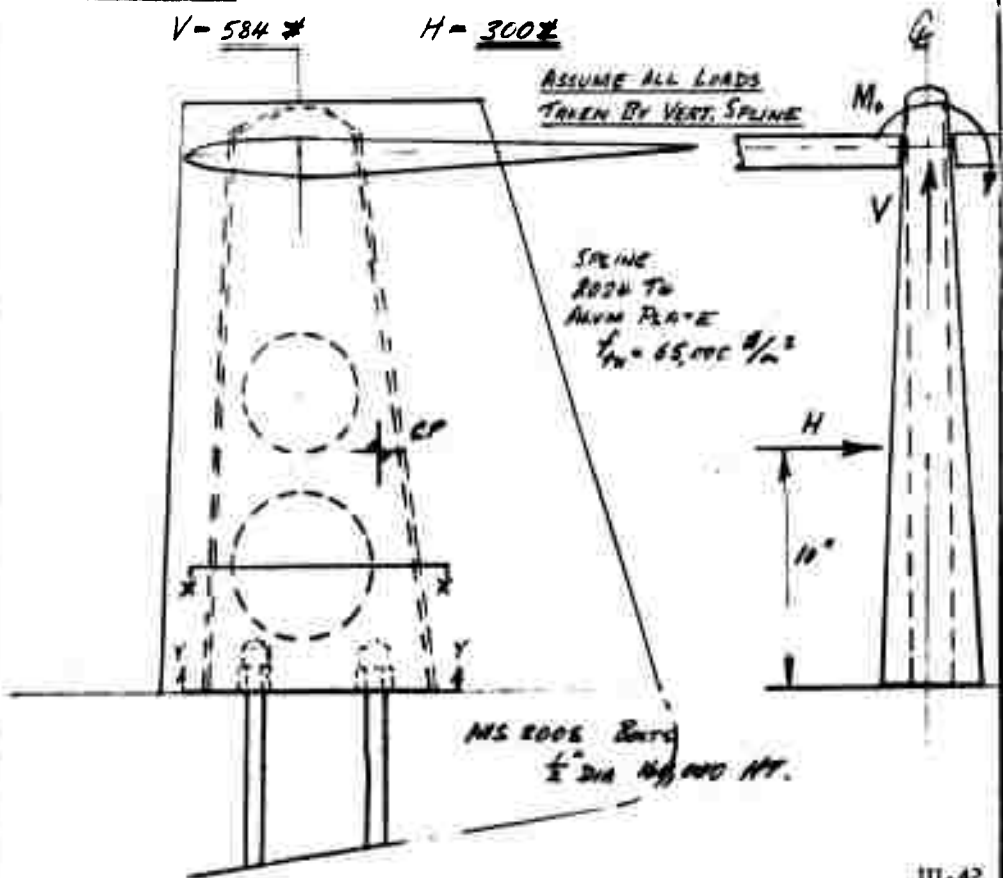
$M_o = \text{ROLLING MOMENT (SEE PAGES 1 \& 2)}$
 $= 146 \times 27 = 3950 \text{ #/m}$

$V = 584 \text{ #}$

$H = 300 \text{ #}$

ASSUME ALL LOADS
TAKEN BY VERT. SPLINE

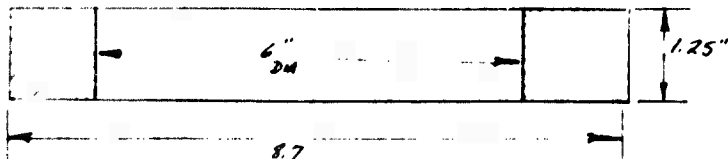
SPLINE
RIGID TO
AVOID PLATE
 $f_{cr} = 65,000 \text{ #/m}^2$



WIND TUNNEL MODEL

SECTION XX

$$Z = \frac{2.7 \times 1.25^2}{6} = .703 \text{ m}^3 \quad A = 3.38 \text{ m}^2$$



$$M_{xx} = M_o + 4.8 \times 800 = 3950 + 1440 = 5390 \text{ #in}$$

$$M/Z = 7660 \text{ #/m}^2$$

$$V/A = 172 \text{ #/m}^2$$

M.S. HIGH

SECTION YV (IN ATTEN BELTS)

1/2" DIA BELTS

$$Z = .00307 \text{ m}^3$$

$$A = .196 \text{ m}^2$$

$$M = 3950 - (10 \times 300) = 6950 \text{ #in}$$

$$V = 584 \text{ #}$$

THE MOMENT IS REACTED BY A COUPLE
BETWEEN BELT & BEARING SURFACE

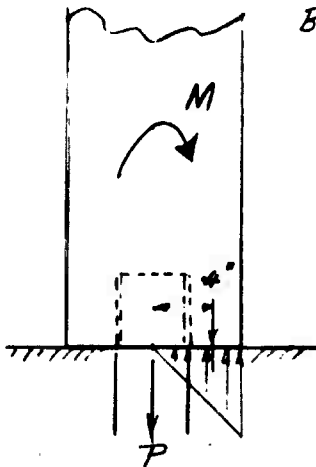
$$P = \frac{6950}{.40} = 17,300 \text{ #} \quad (8,650 \text{ #/BELT})$$

BELT IS GOOD FOR 28,400 #

M.S. HIGH

$$f_{brg} = \frac{8650}{.6 \times 1.0} \times 2 = 28,800 \text{ #/m}^2$$

M.S. HIGH



WIND TUNNEL MODEL

CONTINUED

THE FOREGOING COMPLETES THE STRUCTURAL ANALYSIS OF THE NEW EMPENNAGE & ATTACHMENTS

CHECK ON OVER-ALL FUSELAGE STRENGTH:-

PREVIOUS ULTIMATE FACTOR USED WAS 5.0 THIS IS ON THE HIGH SIDE, AND 3.0 WOULD BE MORE APPROPRIATE.

MAX BM (V.I.T) WAS DUE TO TAIL LOAD OF 254 # (NOW 292 #) LIMIT

M.S. WAS +.23 (BASED ON ULT FACTOR 5.0)

$$\text{NEW M.S.} = 1.23 \times \frac{5.0}{3.0} \times \frac{254}{392} = 1.33 \quad \frac{\text{M.S.} + .33}{(\text{BASED ON ULT FACTOR} = 3.0)}$$

BY EXAMINATION, & COMPARISON WITH THE PREVIOUS ANALYSIS, REST OF STRUCTURE HAS ADEQUATE STRENGTH

Unclassified

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DOCUMENT CONTROL DATA - R&D		
<i>(Security classification of title, body of abstract and indexing annotation must be entered when the overall report is classified)</i>		
1. ORIGINATING ACTIVITY (Corporate author) Hughes Tool Company - Aircraft Division Culver City, California		2a. REPORT SECURITY CLASSIFICATION Unclassified
		2b. GROUP X
3. REPORT TITLE SUMMARY TECHNICAL REPORT, ROTOR/WING CONCEPT STUDY (Volumes I, II, and III)		
4. DESCRIPTIVE NOTES (Type of report and inclusive dates) Summary Report		
5. AUTHOR(S) (Last name, first name, initial) Head, Robert E.		
6. REPORT DATE September 1965	7a. TOTAL NO. OF PAGES	7b. NO. OF REFS 9
8a. CONTRACT OR GRANT NO. Nonr-4588(00)	9a. ORIGINATOR'S REPORT NUMBER(S) HTC-AD 65-15	
b. PROJECT NO. NR-212-162/12-8-64	9b. OTHER REPORT NO(S) (Any other numbers that may be assigned this report) ---	
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11. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY U. S. Navy, Office of Naval Research and Bureau of Naval Weapons	
13. ABSTRACT Research work including wind tunnel and whirl test of the Rotor/Wing is described. The Rotor/Wing is a dual-purpose lifting device that is a rotor with an unusually large hub. It acts as a tip-jet powered helicopter for low-speed flight and stops in flight to become a tapered and sweptback low-aspect ratio wing for cruise. Stopping the rotor in flight removes the speed limitations of the helicopter rotor and permits flight speeds up to 500 knots. Research work was supported by the U. S. Navy Office of Naval Research and Bureau of Naval Weapons. Three series of wind tunnel tests demonstrated that the powered-rotor and autorotating-rotor characteristics are similar to those of a high-performance helicopter; that the stopped-rotor characteristics are similar to a conventional low-aspect ratio wing with sweep and taper, and maximum lift/drag ratios of 12 or more should be achievable for full-scale aircraft; and that conversion from stopped- to running- rotor and vice versa is a simple and straightforward procedure.		

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KEY WORDS	LINK A		LINK R		LINK C	
	ROLE	WT	ROLE	A	ROLE	WT
Rotor Wing Stopped-rotor Conversion Helicopter Wind tunnel test						

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