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# USAAVLABS TECHNICAL REPORT 68-22B

# IN-FLIGHT MEASUREMENT AND CORRELATION WITH THEORY OF BLADE AIRLOADS AND RESPONSES ON THE XH-51A COMPOUND HELICOPTER ROTOR

## VOLUME II
## MEASUREMENT AND DATA REDUCTION OF AIRLOADS AND STRUCTURAL LOADS APPENDIXES V THROUGH IX

By

E. A. Bartsch

May 1968

U. S. ARMY AVIATION MATERIEL LABORATORIES
FORT EUSTIS, VIRGINIA

CONTRACT DA 44-177-AMC-357(T)
LOCKHEED-CALIFORNIA COMPANY
BURBANK, CALIFORNIA

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DEPARTMENT OF THE ARMY
U. S. ARMY AVIATION MATERIEL LABORATORIES
FORT EUSTIS, VIRGINIA 23604

Under Army contract, the Lockheed Aircraft Corporation has conducted an investigation of blade aerodynamic pressures and strains and other associated flight characteristics on an XH-51A compound helicopter. The flight tests and theoretical analyses which were performed during the program were monitored by Army personnel, and the final report has been reviewed to ensure basic technical accuracy.

This report is published for the dissemination of information and the stimulation of further research.

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May 1968

# IN-FLIGHT MEASUREMENT AND CORRELATION WITH THEORY OF BLADE AIRLOADS AND RESPONSES ON THE XH-51A COMPOUND HELICOPTER ROTOR

LR 21072

## VOLUME II
## MEASUREMENT AND DATA REDUCTION OF AIRLOADS AND STRUCTURAL LOADS APPENDIXES V THROUGH IX

By

E. A. Bartsch

Prepared by

Lockheed-California Company
Burbank, California

for

U. S. ARMY AVIATION MATERIEL LABORATORIES
FORT EUSTIS, VIRGINIA

This document has been approved for public release and sale; its distribution is unlimited.

## ABSTRACT

This report presents the results of a two-phase research program consisting of (1) in-flight measurement of aerodynamic pressures and structural loads on a compound, rigid-rotor helicopter and (2) correlation of these data with theoretical results.

Flight test data obtained in Phase I and recorded on an oscillograph were read on an oscillograph reading machine and were processed in an automatic data reduction program. This data processing consisted of integration of the pressure data to obtain the distribution of aerodynamic lift and pitching moments over the rotor blade, as functions of azimuth position. Airload and structural load data were harmonically analyzed.

Output of the data reduction program was used in Phase II as input to the correlation program. The measured airloads were used to compute the theoretical bending and torsion responses of the blade. The measured torsion moments were used in the theoretical prediction of the airloads. The results of the applied theories are compared with the flight measurements.

## FOREWORD

This report describes a two-phase research program consisting of (1) flight test measurements of helicopter rotor blade structural loads and aerodynamic pressures and (2) correlation of these measurements with data obtained from current theories. This research program was conducted by the Lockheed-California Company under Contract DA 44-177-AMC-357(T) to the U.S. Army Aviation Materiel Laboratories (USAAVLABS), Fort Eustis, Virginia.

The research program was performed during the period from June 1966 to October 1967. Technical monitoring of the project for USAAVLABS was by W. E. Nettles.

The report covering the program is presented in three volumes. Volume I is entitled "Measurement and Data Reduction of Airloads and Structural Loads". It contains the main body of the report plus Appendixes I through IV. Volume II contains Appendixes V through IX, with all flight test data in tabular form. The correlation of the measured airloads and structural loads with theoretical data is covered in Volume III, "Theoretical Prediction of Airloads and Structural Loads and Correlation with Flight Test Measurements".

The Lockheed program was under the technical direction of A. W. Turner and W. E. Spreuer, engineering managers, and J. E. Sweers, project leader. The test pilot was R. Goudey. Additional Lockheed personnel associated with the program included W. H. Foulke and R. A. Berry, flight test; C. J. Buzzetti, E. A. Bartsch, S. H. Lomax, and T. H. Oglesby, structural flight measurement; R. H. Cook and R. G. Murison, instrumentation; R. D. Baker and W. C. Weddle, data processing; R. E. Donham and D. H. Janda, rotary wing dynamics; C. H. Ranschau, programming; and R. P. Beal, editor.

Appreciation is due USAAVLABS for their help in providing assistance and advice in planning and executing the entire research program.

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## DIFFERENTIAL PRESSURE - DYNAMIC COMPONENTS

The dynamic components of the differential pressure (in psi) interpolated for 72 data points per cycle are presented in this appendix. Data of all instrumented span and chord stations are tabulated for the 20 test conditions selected for full analysis.

The corresponding static components of the 46 stations are listed in Appendix VI.

Abbreviations used in the heading are:

| | |
|---|---|
| CNTR No. | counter number |
| TCN | test condition number |
| C.R. | computer run |
| AZ | azimuth position |
| DEG | degrees |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 538 TCN= 1. C.R.= 53.1

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.950 | 10.400 | DEG. |
| 0. | 0.06 | 0.03 | 0.03 | -0.00 | 0. |
| 5. | 0.03 | 0.02 | 0.02 | -0.01 | 5. |
| 10. | 0.01 | 0.01 | 0.01 | -0.01 | 10. |
| 15. | 0.01 | 0.00 | 0.00 | -0.00 | 15. |
| 20. | 0.02 | -0.00 | -0.00 | -0.01 | 20. |
| 25. | -0.00 | -0.01 | -0.01 | -0.01 | 25. |
| 30. | -0.03 | -0.02 | -0.02 | -0.02 | 30. |
| 35. | -0.07 | -0.04 | -0.03 | -0.02 | 35. |
| 40. | -0.08 | -0.05 | -0.03 | -0.01 | 40. |
| 45. | -0.05 | -0.04 | -0.04 | -0.01 | 45. |
| 50. | -0.08 | -0.04 | -0.03 | -0.01 | 50. |
| 55. | -0.12 | -0.05 | -0.03 | -0.02 | 55. |
| 60. | -0.12 | -0.06 | -0.03 | -0.01 | 60. |
| 65. | -0.06 | -0.05 | -0.02 | -0.01 | 65. |
| 70. | 0.01 | -0.02 | -0.02 | -0.01 | 70. |
| 75. | 0.04 | 0.00 | -0.01 | -0.01 | 75. |
| 80. | 0.05 | 0.01 | -0.01 | -0.01 | 80. |
| 85. | 0.04 | 0.01 | -0.01 | -0.01 | 85. |
| 90. | 0.02 | -0.00 | -0.01 | -0.01 | 90. |
| 95. | 0.01 | -0.01 | -0.02 | -0.00 | 95. |
| 100. | -0.00 | -0.03 | -0.02 | 0.00 | 100. |
| 105. | -0.01 | -0.04 | -0.03 | 0.00 | 105. |
| 110. | -0.03 | -0.05 | -0.03 | -0.00 | 110. |
| 115. | -0.05 | -0.05 | -0.03 | 0.00 | 115. |
| 120. | -0.06 | -0.05 | -0.02 | 0.01 | 120. |
| 125. | -0.06 | -0.04 | -0.02 | 0.01 | 125. |
| 130. | -0.06 | -0.04 | -0.02 | 0.00 | 130. |
| 135. | -0.05 | -0.03 | -0.02 | 0.00 | 135. |
| 140. | -0.04 | -0.03 | -0.02 | 0.00 | 140. |
| 145. | -0.03 | -0.02 | -0.02 | 0.00 | 145. |
| 150. | -0.01 | -0.01 | -0.02 | -0.00 | 150. |
| 155. | 0.01 | -0.01 | -0.01 | -0.00 | 155. |
| 160. | 0.03 | 0.00 | 0.00 | 0.00 | 160. |
| 165. | 0.05 | 0.01 | 0.01 | 0.01 | 165. |
| 170. | 0.07 | 0.02 | 0.01 | 0.02 | 170. |
| 175. | 0.08 | 0.03 | 0.02 | 0.02 | 175. |
| 180. | 0.08 | 0.04 | 0.02 | 0.02 | 180. |
| 185. | 0.07 | 0.03 | 0.02 | 0.02 | 185. |
| 190. | 0.06 | 0.02 | 0.01 | 0.02 | 190. |
| 195. | 0.05 | -0.00 | 0.01 | 0.03 | 195. |
| 200. | 0.03 | -0.02 | 0.01 | 0.03 | 200. |
| 205. | 0.01 | -0.02 | 0.00 | 0.02 | 205. |
| 210. | -0.00 | -0.02 | -0.00 | 0.01 | 210. |
| 215. | -0.02 | -0.02 | -0.01 | 0.00 | 215. |
| 220. | -0.03 | -0.02 | -0.01 | 0.00 | 220. |
| 225. | -0.04 | -0.01 | -0.02 | 0.01 | 225. |
| 230. | -0.04 | -0.01 | -0.02 | 0.01 | 230. |
| 235. | -0.03 | -0.01 | -0.02 | 0.01 | 235. |
| 240. | -0.01 | -0.01 | -0.01 | 0.01 | 240. |
| 245. | -0.02 | -0.01 | -0.00 | 0.01 | 245. |
| 250. | -0.04 | -0.01 | 0.00 | 0.01 | 250. |
| 255. | -0.05 | -0.01 | 0.01 | 0.01 | 255. |
| 260. | -0.04 | 0.00 | 0.01 | 0.01 | 260. |
| 265. | -0.03 | 0.01 | 0.02 | 0.01 | 265. |
| 270. | -0.02 | 0.02 | 0.02 | 0.01 | 270. |
| 275. | -0.01 | 0.02 | 0.02 | 0.01 | 275. |
| 280. | -0.00 | 0.02 | 0.02 | 0.01 | 280. |
| 285. | 0.00 | 0.02 | 0.01 | 0.00 | 285. |
| 290. | 0.01 | 0.02 | 0.01 | -0.02 | 290. |
| 295. | 0.01 | 0.02 | 0.01 | -0.03 | 295. |
| 300. | 0.02 | 0.03 | 0.01 | 0.01 | 300. |
| 305. | 0.01 | 0.04 | 0.01 | -0.01 | 305. |
| 310. | 0.00 | 0.04 | 0.01 | -0.02 | 310. |
| 315. | -0.00 | 0.05 | 0.02 | -0.02 | 315. |
| 320. | -0.00 | 0.04 | 0.02 | -0.02 | 320. |
| 325. | 0.00 | 0.04 | 0.03 | -0.01 | 325. |
| 330. | 0.02 | 0.04 | 0.04 | -0.01 | 330. |
| 335. | 0.05 | 0.06 | 0.04 | -0.00 | 335. |
| 340. | 0.09 | 0.07 | 0.05 | -0.00 | 340. |
| 345. | 0.12 | 0.08 | 0.05 | -0.00 | 345. |
| 350. | 0.12 | 0.07 | 0.05 | 0.00 | 350. |
| 355. | 0.10 | 0.05 | 0.04 | 0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST .02 CNTR NO. 538 TCN= 1. C.R.= 53.1

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.435 | 1.040 | 1.950 | 2.995 | 4.550 | 7.150 | .0.400 | DEG. |
| 0. | 0.14 | 0.11 | 0.07 | 0.05 | 0.04 | 0.02 | 0.02 | 0. |
| 5. | 0.14 | 0.10 | 0.07 | 0.04 | 0.03 | 0.02 | 0.02 | 5. |
| 10. | 0.13 | 0.09 | 0.06 | 0.03 | 0.02 | 0.02 | 0.01 | 10. |
| 15. | 0.12 | 0.09 | 0.05 | 0.03 | 0.02 | 0.02 | 0.01 | 15. |
| 20. | 0.12 | 0.08 | 0.05 | 0.03 | 0.01 | 0.01 | 0.02 | 20. |
| 25. | 0.12 | 0.08 | 0.04 | 0.03 | 0.02 | 0.02 | 0.01 | 25. |
| 30. | 0.11 | 0.08 | 0.04 | 0.03 | 0.02 | 0.01 | 0.01 | 30. |
| 35. | 0.11 | 0.07 | 0.04 | 0.02 | 0.02 | 0.01 | 0.01 | 35. |
| 40. | 0.09 | 0.07 | 0.04 | 0.01 | 0.02 | 0.01 | 0.01 | 40. |
| 45. | 0.07 | 0.06 | 0.03 | 0.01 | 0.01 | 0.00 | 0.00 | 45. |
| 50. | 0.06 | 0.05 | 0.03 | 0.00 | 0.01 | 0.00 | 0.00 | 50. |
| 55. | 0.05 | 0.04 | 0.02 | -0.00 | 0.00 | -0.00 | 0.01 | 55. |
| 60. | 0.04 | 0.03 | 0.01 | -0.01 | 0.00 | -0.00 | 0.01 | 60. |
| 65. | 0.03 | 0.01 | -0.01 | -0.01 | 0.01 | -0.00 | 0.01 | 65. |
| 70. | 0.02 | -0.00 | -0.02 | -0.02 | 0.01 | -0.01 | 0.01 | 70. |
| 75. | 0.02 | -0.01 | -0.03 | -0.02 | 0.02 | -0.00 | 0.01 | 75. |
| 80. | 0.01 | -0.03 | -0.04 | -0.02 | 0.02 | -0.00 | 0.01 | 80. |
| 85. | 0.00 | -0.04 | -0.04 | -0.03 | 0.01 | -0.00 | 0.01 | 85. |
| 90. | -0.02 | -0.05 | -0.04 | -0.03 | -0.00 | -0.00 | 0.00 | 90. |
| 95. | -0.04 | -0.04 | -0.04 | -0.03 | -0.01 | -0.01 | -0.00 | 95. |
| 100. | -0.06 | -0.07 | -0.05 | -0.04 | -0.02 | -0.01 | -0.01 | 100. |
| 105. | -0.09 | -0.08 | -0.05 | -0.04 | -0.02 | -0.01 | -0.01 | 105. |
| 110. | -0.11 | -0.09 | -0.06 | -0.04 | -0.02 | -0.01 | -0.01 | 110. |
| 115. | -0.13 | -0.09 | -0.07 | -0.04 | -0.02 | -0.01 | -0.01 | 115. |
| 120. | -0.14 | -0.09 | -0.07 | -0.03 | -0.03 | -0.01 | -0.01 | 120. |
| 125. | -0.14 | -0.09 | -0.08 | -0.03 | -0.03 | -0.01 | -0.01 | 125. |
| 130. | -0.14 | -0.10 | -0.08 | -0.03 | -0.03 | -0.01 | -0.02 | 130. |
| 135. | -0.13 | -0.10 | -0.08 | -0.03 | -0.03 | -0.01 | -0.02 | 135. |
| 140. | -0.12 | -0.09 | -0.08 | -0.03 | -0.02 | -0.01 | -0.01 | 140. |
| 145. | -0.10 | -0.09 | -0.07 | -0.03 | -0.02 | -0.01 | -0.01 | 145. |
| 150. | -0.08 | -0.07 | -0.06 | -0.03 | -0.03 | -0.01 | -0.01 | 150. |
| 155. | -0.05 | -0.05 | -0.05 | -0.02 | -0.02 | -0.01 | -0.01 | 155. |
| 160. | -0.02 | -0.02 | -0.02 | -0.01 | -0.01 | -0.01 | -0.00 | 160. |
| 165. | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | -0.00 | -0.00 | 165. |
| 170. | 0.04 | 0.04 | 0.03 | 0.02 | 0.02 | 0.00 | -0.01 | 170. |
| 175. | 0.07 | 0.06 | 0.04 | 0.02 | 0.02 | 0.01 | -0.01 | 175. |
| 180. | 0.07 | 0.06 | 0.05 | 0.03 | 0.02 | 0.01 | -0.02 | 180. |
| 185. | 0.06 | 0.05 | 0.05 | 0.02 | 0.02 | 0.01 | -0.02 | 185. |
| 190. | 0.03 | 0.04 | 0.04 | 0.01 | 0.01 | 0.01 | -0.02 | 192. |
| 195. | -0.00 | 0.02 | 0.01 | 0.00 | -0.01 | 0.01 | -0.02 | 195. |
| 200. | -0.05 | 0.00 | -0.01 | -0.01 | -0.02 | 0.00 | -0.02 | 200. |
| 205. | -0.09 | -0.03 | -0.03 | -0.02 | -0.04 | -0.00 | -0.03 | 205. |
| 210. | -0.12 | -0.06 | -0.05 | -0.03 | -0.04 | -0.01 | -0.03 | 210. |
| 215. | -0.13 | -0.08 | -0.05 | -0.04 | -0.05 | -0.02 | -0.02 | 215. |
| 220. | -0.14 | -0.09 | -0.05 | -0.05 | -0.05 | -0.02 | -0.01 | 220. |
| 225. | -0.14 | -0.09 | -0.06 | -0.05 | -0.04 | -0.02 | -0.02 | 225. |
| 230. | -0.13 | -0.09 | -0.06 | -0.05 | -0.04 | -0.02 | -0.02 | 230. |
| 235. | -0.12 | -0.09 | -0.05 | -0.05 | -0.04 | -0.02 | -0.02 | 235. |
| 240. | -0.11 | -0.09 | -0.05 | -0.05 | -0.04 | -0.01 | -0.02 | 240. |
| 245. | -0.10 | -0.09 | -0.05 | -0.04 | -0.04 | -0.02 | -0.01 | 245. |
| 250. | -0.09 | -0.09 | -0.04 | -0.04 | -0.03 | -0.02 | -0.01 | 250. |
| 255. | -0.08 | -0.08 | -0.03 | -0.02 | -0.03 | -0.01 | -0.01 | 255. |
| 260. | -0.07 | -0.07 | -0.02 | -0.01 | -0.02 | 0.00 | -0.01 | 260. |
| 265. | -0.04 | -0.04 | -0.01 | 0.00 | -0.02 | 0.01 | -0.00 | 265. |
| 270. | -0.04 | -0.05 | -0.00 | 0.01 | 0.01 | 0.01 | 0.01 | 270. |
| 275. | -0.03 | -0.03 | 0.01 | 0.01 | 0.01 | 0.01 | 0.01 | 275. |
| 280. | -0.01 | -0.02 | 0.01 | 0.02 | 0.01 | 0.01 | 0.01 | 280. |
| 285. | 0.00 | -0.00 | 0.02 | 0.02 | 0.01 | 0.01 | 0.01 | 285. |
| 290. | 0.01 | 0.02 | 0.03 | 0.02 | 0.02 | 0.01 | 0.01 | 290. |
| 295. | 0.02 | 0.03 | 0.03 | 0.03 | 0.02 | 0.01 | 0.01 | 295. |
| 300. | 0.03 | 0.04 | 0.04 | 0.03 | 0.02 | 0.01 | 0.01 | 300. |
| 305. | 0.04 | 0.05 | 0.04 | 0.03 | 0.02 | 0.01 | 0.01 | 305. |
| 310. | 0.05 | 0.06 | 0.05 | 0.03 | 0.02 | 0.01 | 0.01 | 310. |
| 315. | 0.07 | 0.06 | 0.05 | 0.03 | 0.02 | 0.01 | 0.02 | 315. |
| 320. | 0.08 | 0.07 | 0.06 | 0.03 | 0.02 | 0.01 | 0.02 | 320. |
| 325. | 0.10 | 0.07 | 0.06 | 0.03 | 0.02 | 0.00 | 0.01 | 325. |
| 330. | 0.12 | 0.09 | 0.07 | 0.04 | 0.01 | 0.00 | 0.01 | 330. |
| 335. | 0.13 | 0.11 | 0.07 | 0.04 | 0.02 | 0.00 | 0.01 | 335. |
| 340. | 0.14 | 0.13 | 0.08 | 0.05 | 0.02 | 0.00 | 0.01 | 340. |
| 345. | 0.14 | 0.13 | 0.09 | 0.06 | 0.03 | 0.01 | 0.02 | 345. |
| 350. | 0.15 | 0.13 | 0.09 | 0.06 | 0.05 | 0.02 | 0.02 | 350. |
| 355. | 0.15 | 0.12 | 0.08 | 0.06 | 0.05 | 0.03 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-502 CNTR NO. 530 YCN= 1. C.R.= 53.1

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.940 | 4.550 | 7.153 | 10.400 | DEG. |
| 0. | 0.33 | 0.28 | 0.18 | 0.13 | 0.12 | 0.07 | 0.01 | 0. |
| 5. | 0.32 | 0.25 | 0.16 | 0.17 | 0.11 | 0.06 | 0.01 | 5. |
| 10. | 0.32 | 0.23 | 0.15 | 0.14 | 0.10 | 0.05 | 0.00 | 10. |
| 15. | 0.31 | 0.22 | 0.14 | 0.13 | 0.09 | 0.04 | 0.00 | 15. |
| 20. | 0.30 | 0.21 | 0.13 | 0.11 | 0.09 | 0.04 | 0.00 | 20. |
| 25. | 0.28 | 0.21 | 0.11 | 0.10 | 0.09 | 0.04 | 0.00 | 25. |
| 30. | 0.27 | 0.19 | 0.10 | 0.09 | 0.08 | 0.03 | 0.00 | 30. |
| 35. | 0.26 | 0.16 | 0.19 | 0.08 | 0.08 | 0.03 | 0.00 | 35. |
| 40. | 0.25 | 0.14 | 0.09 | 0.07 | 0.08 | 0.02 | 0.00 | 40. |
| 45. | 0.25 | 0.12 | 0.09 | 0.07 | 0.07 | 0.02 | 0.00 | 45. |
| 50. | 0.24 | 0.10 | 0.09 | 0.06 | 0.06 | 0.02 | 0.00 | 50. |
| 55. | 0.22 | 0.08 | 0.08 | 0.05 | 0.06 | 0.01 | 0.00 | 55. |
| 60. | 0.20 | 0.06 | 0.07 | 0.04 | 0.05 | 0.01 | 0.00 | 60. |
| 65. | 0.18 | 0.00 | 0.06 | 0.02 | 0.04 | 0.00 | 0.00 | 65. |
| 70. | 0.15 | -0.04 | 0.05 | 0.01 | 0.03 | -0.00 | 0.00 | 70. |
| 75. | 0.12 | -0.05 | 0.03 | -0.00 | 0.03 | -0.00 | 0.00 | 75. |
| 80. | 0.10 | -0.05 | 0.02 | -0.02 | 0.02 | -0.01 | 0.00 | 80. |
| 85. | 0.09 | -0.04 | 0.00 | -0.02 | 0.01 | -0.01 | 0.00 | 85. |
| 90. | 0.08 | -0.04 | -0.01 | -0.03 | 0.01 | -0 | 0.00 | 90. |
| 95. | 0.06 | -0.07 | -0.02 | -0.03 | -0.00 | -0.02 | -0.00 | 95. |
| 100. | 0.02 | -0.09 | -0.03 | -0.04 | -0.01 | -0.02 | -0.00 | 100. |
| 105. | -0.03 | -0.12 | -0.06 | -0.05 | -0.03 | -0.03 | -0.00 | 105. |
| 110. | -0.07 | -0.13 | -0.06 | -0.06 | -0.03 | -0.04 | -0.00 | 110. |
| 115. | -0.11 | -0.13 | -0.09 | -0.07 | -0.04 | -0.04 | -0.01 | 115. |
| 120. | -0.15 | -0.14 | -0.11 | -0.09 | -0.05 | -0.05 | -0.01 | 120. |
| 125. | -0.19 | -0.15 | -0.14 | -0.11 | -0.06 | -0.05 | -0.01 | 125. |
| 130. | -0.22 | -0.16 | -0.15 | -0.12 | -0.07 | -0.05 | -0.01 | 130. |
| 135. | -0.24 | -0.17 | -0.16 | -0.12 | -0.07 | -0.05 | -0.01 | 135. |
| 140. | -0.24 | -0.18 | -0.16 | -0.12 | -0.08 | -0.04 | -0.00 | 140. |
| 145. | -0.24 | -0.19 | -0.16 | -0.12 | -0.08 | -0.04 | -0.00 | 145. |
| 150. | -0.23 | -0.19 | -0.15 | -0.11 | -0.07 | -0.04 | -0.00 | 150. |
| 155. | -0.22 | -0.18 | -0.14 | -0.11 | -0.07 | -0.04 | -0.00 | 155. |
| 160. | -0.21 | -0.16 | -0.15 | -0.10 | -0.07 | -0.04 | -0.00 | 160. |
| 165. | -0.20 | -0.14 | -0.13 | -0.09 | -0.06 | -0.03 | -0.00 | 165. |
| 170. | -0.19 | -0.12 | -0.13 | -0.08 | -0.05 | -0.03 | 0.00 | 170. |
| 175. | -0.18 | -0.12 | -0.11 | -0.08 | -0.05 | -0.02 | 0.00 | 175. |
| 180. | -0.17 | -0.12 | -0.10 | -0.07 | -0.05 | -0.02 | 0.00 | 180. |
| 185. | -0.16 | -0.13 | -0.09 | -0.07 | -0.05 | -0.02 | 0.00 | 185. |
| 190. | -0.17 | -0.15 | -0.09 | -0.07 | -0.05 | -0.02 | 0.00 | 190. |
| 195. | -0.19 | -0.17 | -0.09 | -0.07 | -0.05 | -0.02 | -0.00 | 195. |
| 200. | -0.21 | -0.20 | -0.09 | -0.08 | -0.06 | -0.02 | -0.00 | 200. |
| 205. | -0.23 | -0.21 | -0.10 | -0.09 | -0.06 | -0.03 | -0.01 | 205. |
| 210. | -0.25 | -0.21 | -0.11 | -0.10 | -0.07 | -0.03 | -0.01 | 210. |
| 215. | -0.27 | -0.21 | -0.13 | -0.10 | -0.08 | -0.03 | -0.01 | 215. |
| 220. | -0.29 | -0.21 | -0.14 | -0.11 | -0.08 | -0.03 | -0.01 | 220. |
| 225. | -0.29 | -0.21 | -0.14 | -0.11 | -0.08 | -0.03 | -0.01 | 225. |
| 230. | -0.28 | -0.20 | -0.14 | -0.11 | -0.08 | -0.03 | -0.01 | 230. |
| 235. | -0.26 | -0.19 | -0.12 | -0.10 | -0.07 | -0.02 | -0.01 | 235. |
| 240. | -0.24 | -0.17 | -0.11 | -0.09 | -0.07 | -0.02 | -0.01 | 240. |
| 245. | -0.22 | -0.14 | -0.09 | -0.08 | -0.07 | -0.02 | -0.01 | 245. |
| 250. | -0.19 | -0.10 | -0.08 | -0.07 | -0.07 | -0.02 | -0.01 | 250. |
| 255. | -0.16 | -0.07 | -0.06 | -0.06 | -0.06 | -0.01 | -0.01 | 255. |
| 260. | -0.13 | -0.03 | -0.04 | -0.05 | -0.06 | -0.01 | -0.00 | 260. |
| 265. | -0.11 | -0.01 | -0.02 | -0.04 | -0.05 | -0.01 | -0.00 | 265. |
| 270. | -0.08 | 0.02 | 0.01 | -0.01 | -0.04 | -0.00 | 0.00 | 270. |
| 275. | -0.05 | 0.04 | 0.02 | 0.02 | -0.03 | 0.00 | 0.00 | 275. |
| 280. | -0.03 | 0.06 | 0.03 | 0.03 | -0.02 | 0.01 | 0.00 | 280. |
| 285. | -0.00 | 0.09 | 0.04 | 0.04 | -0.01 | 0.01 | 0.00 | 285. |
| 290. | 0.02 | 0.12 | 0.06 | 0.05 | -0.00 | 0.02 | 0.00 | 290. |
| 295. | 0.04 | 0.13 | 0.08 | 0.06 | 0.01 | 0.02 | 0.00 | 295. |
| 300. | 0.04 | 0.11 | 0.10 | 0.07 | 0.02 | 0.02 | 0.00 | 300. |
| 305. | 0.04 | 0.10 | 0.11 | 0.08 | 0.04 | 0.02 | 0.00 | 305. |
| 310. | 0.11 | 0.12 | 0.12 | 0.10 | 0.06 | 0.03 | 0.00 | 310. |
| 315. | 0.13 | 0.15 | 0.12 | 0.11 | 0.07 | 0.03 | 0.01 | 315. |
| 320. | 0.15 | 0.19 | 0.13 | 0.12 | 0.07 | 0.03 | 0.01 | 320. |
| 325. | 0.17 | 0.22 | 0.15 | 0.12 | 0.08 | 0.04 | 0.01 | 325. |
| 330. | 0.20 | 0.25 | 0.15 | 0.13 | 0.08 | 0.04 | 0.01 | 330. |
| 335. | 0.23 | 0.28 | 0.17 | 0.14 | 0.08 | 0.05 | 0.00 | 335. |
| 340. | 0.26 | 0.31 | 0.19 | 0.14 | 0.08 | 0.06 | 0.00 | 340. |
| 345. | 0.28 | 0.33 | 0.20 | 0.15 | 0.09 | 0.06 | 0.01 | 345. |
| 350. | 0.32 | 0.33 | 0.21 | 0.17 | 0.11 | 0.07 | 0.01 | 350. |
| 355. | 0.34 | 0.31 | 0.19 | 0.18 | 0.13 | 0.07 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 538 TCN= 1. C.R.= 53.1

DIFFERENTIAL PRESSURES

SPAN STATION 193.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 5.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.42 | 0.32 | 0.35 | 0.22 | 0.20 | 0.10 | 0.04 | 0. |
| 5. | 0.40 | 0.29 | 0.31 | 0.18 | 0.18 | 0.09 | 0.04 | 5. |
| 10. | 0.35 | 0.28 | 0.28 | 0.15 | 0.16 | 0.09 | 0.03 | 10. |
| 15. | 0.40 | 0.27 | 0.26 | 0.14 | 0.14 | 0.08 | 0.03 | 15. |
| 20. | 0.41 | 0.26 | 0.25 | 0.14 | 0.14 | 0.07 | 0.03 | 20. |
| 25. | 0.37 | 0.26 | 0.24 | 0.15 | 0.13 | 0.06 | 0.02 | 25. |
| 30. | 0.36 | 0.23 | 0.23 | 0.14 | 0.12 | 0.05 | 0.02 | 30. |
| 35. | 0.35 | 0.18 | 0.20 | 0.13 | 0.11 | 0.03 | 0.02 | 35. |
| 40. | 0.32 | 0.14 | 0.17 | 0.12 | 0.10 | 0.02 | 0.01 | 40. |
| 45. | 0.31 | 0.17 | 0.14 | 0.11 | 0.09 | 0.02 | 0.01 | 45. |
| 50. | 0.31 | 0.23 | 0.11 | 0.11 | 0.08 | 0.02 | 0.01 | 50. |
| 55. | 0.30 | 0.23 | 0.08 | 0.10 | 0.07 | 0.01 | 0.01 | 55. |
| 60. | 0.29 | 0.22 | 0.05 | 0.10 | 0.06 | 0.01 | 0.00 | 60. |
| 65. | 0.27 | 0.21 | 0.02 | 0.09 | 0.06 | -0.00 | -0.00 | 65. |
| 70. | 0.24 | 0.19 | -0.02 | 0.08 | 0.05 | -0.01 | -0.01 | 70. |
| 75. | 0.18 | 0.17 | -0.05 | 0.07 | 0.03 | -0.01 | -0.01 | 75. |
| 80. | 0.12 | 0.15 | -0.07 | 0.05 | 0.02 | -0.02 | -0.01 | 80. |
| 85. | 0.04 | 0.07 | -0.09 | 0.03 | 0.01 | -0.02 | -0.01 | 85. |
| 90. | -0.03 | -0.01 | -0.11 | 0.01 | -0.01 | -0.03 | -0.01 | 90. |
| 95. | -0.08 | -0.04 | -0.12 | -0.01 | -0.02 | -0.04 | -0.01 | 95. |
| 100. | -0.12 | -0.04 | -0.14 | -0.03 | -0.04 | -0.04 | -0.02 | 100. |
| 105. | -0.16 | -0.03 | -0.17 | -0.05 | -0.05 | -0.05 | -0.02 | 105. |
| 110. | -0.21 | -0.04 | -0.19 | -0.08 | -0.07 | -0.06 | -0.02 | 110. |
| 115. | -0.26 | -0.10 | -0.21 | -0.10 | -0.08 | -0.07 | -0.03 | 115. |
| 120. | -0.31 | -0.15 | -0.22 | -0.11 | -0.09 | -0.07 | -0.03 | 120. |
| 125. | -0.36 | -0.19 | -0.23 | -0.12 | -0.11 | -0.07 | -0.03 | 125. |
| 130. | -0.41 | -0.22 | -0.23 | -0.13 | -0.12 | -0.08 | -0.03 | 130. |
| 135. | -0.44 | -0.23 | -0.22 | -0.14 | -0.13 | -0.08 | -0.03 | 135. |
| 140. | -0.46 | -0.23 | -0.21 | -0.15 | -0.14 | -0.07 | -0.03 | 140. |
| 145. | -0.45 | -0.23 | -0.21 | -0.16 | -0.13 | -0.07 | -0.03 | 145. |
| 150. | -0.45 | -0.24 | -0.20 | -0.16 | -0.12 | -0.06 | -0.02 | 150. |
| 155. | -0.49 | -0.23 | -0.19 | -0.16 | -0.11 | -0.06 | -0.02 | 155. |
| 160. | -0.52 | -0.22 | -0.18 | -0.16 | -0.11 | -0.07 | -0.02 | 160. |
| 165. | -0.49 | -0.19 | -0.16 | -0.16 | -0.12 | -0.06 | -0.02 | 165. |
| 170. | -0.45 | -0.15 | -0.14 | -0.15 | -0.12 | -0.05 | -0.02 | 170. |
| 175. | -0.35 | -0.09 | -0.11 | -0.12 | -0.11 | -0.04 | -0.02 | 175. |
| 180. | -0.29 | -0.04 | -0.10 | -0.08 | -0.09 | -0.03 | -0.02 | 180. |
| 185. | -0.25 | -0.03 | -0.10 | -0.07 | -0.07 | -0.03 | -0.02 | 185. |
| 190. | -0.24 | -0.08 | -0.10 | -0.08 | -0.07 | -0.03 | -0.02 | 190. |
| 195. | -0.29 | -0.17 | -0.12 | -0.11 | -0.08 | -0.04 | -0.02 | 195. |
| 200. | -0.35 | -0.16 | -0.14 | -0.13 | -0.09 | -0.04 | -0.02 | 200. |
| 205. | -0.39 | -0.17 | -0.14 | -0.13 | -0.10 | -0.04 | -0.02 | 205. |
| 210. | -0.42 | -0.21 | -0.17 | -0.13 | -0.11 | -0.04 | -0.02 | 210. |
| 215. | -0.43 | -0.24 | -0.17 | -0.13 | -0.12 | -0.04 | -0.02 | 215. |
| 220. | -0.40 | -0.23 | -0.17 | -0.13 | -0.12 | -0.04 | -0.01 | 220. |
| 225. | -0.34 | -0.22 | -0.16 | -0.12 | -0.12 | -0.03 | -0.01 | 225. |
| 230. | -0.30 | -0.20 | -0.14 | -0.12 | -0.11 | -0.02 | -0.01 | 230. |
| 235. | -0.27 | -0.17 | -0.11 | -0.11 | -0.10 | -0.02 | -0.00 | 235. |
| 240. | -0.25 | -0.15 | -0.09 | -0.10 | -0.09 | -0.02 | -0.00 | 240. |
| 245. | -0.22 | -0.14 | -0.07 | -0.10 | -0.07 | -0.01 | -0.00 | 245. |
| 250. | -0.18 | -0.13 | -0.06 | -0.09 | -0.06 | -0.01 | -0.01 | 250. |
| 255. | -0.13 | -0.13 | -0.05 | -0.07 | -0.05 | -0.00 | -0.00 | 255. |
| 260. | -0.09 | -0.12 | -0.04 | -0.06 | -0.04 | -0.00 | -0.00 | 260. |
| 265. | -0.07 | -0.07 | -0.04 | -0.05 | -0.04 | 0.00 | 0.00 | 265. |
| 270. | -0.04 | -0.00 | -0.02 | -0.03 | -0.03 | 0.01 | 0.01 | 270. |
| 275. | -0.02 | -0.11 | -0.03 | -0.02 | -0.03 | 0.02 | 0.01 | 275. |
| 280. | -0.01 | -0.12 | 0.02 | -0.00 | -0.02 | 0.02 | 0.01 | 280. |
| 285. | 0.01 | -0.10 | 0.04 | 0.01 | -0.01 | 0.02 | 0.01 | 285. |
| 290. | 0.03 | -0.07 | 0.05 | 0.02 | 0.01 | 0.03 | 0.01 | 290. |
| 295. | 0.04 | -0.04 | 0.07 | 0.03 | 0.02 | 0.03 | 0.02 | 295. |
| 300. | 0.09 | -0.05 | 0.08 | 0.04 | 0.04 | 0.04 | 0.02 | 300. |
| 305. | 0.13 | -0.03 | 0.10 | 0.05 | 0.05 | 0.04 | 0.02 | 305. |
| 310. | 0.18 | -0.01 | 0.11 | 0.06 | 0.07 | 0.05 | 0.02 | 310. |
| 315. | 0.24 | 0.04 | 0.13 | 0.08 | 0.09 | 0.05 | 0.02 | 315. |
| 320. | 0.33 | 0.13 | 0.16 | 0.10 | 0.11 | 0.06 | 0.02 | 320. |
| 325. | 0.40 | 0.19 | 0.18 | 0.13 | 0.12 | 0.07 | 0.03 | 325. |
| 330. | 0.45 | 0.21 | 0.21 | 0.16 | 0.14 | 0.08 | 0.03 | 330. |
| 335. | 0.50 | 0.23 | 0.25 | 0.19 | 0.16 | 0.08 | 0.03 | 335. |
| 340. | 0.55 | 0.28 | 0.30 | 0.21 | 0.17 | 0.08 | 0.03 | 340. |
| 345. | 0.60 | 0.34 | 0.34 | 0.22 | 0.18 | 0.09 | 0.04 | 345. |
| 350. | 0.64 | 0.38 | 0.37 | 0.23 | 0.20 | 0.09 | 0.04 | 350. |
| 355. | 0.64 | 0.34 | 0.37 | 0.23 | 0.20 | 0.09 | 0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 538 TCN= 1. C.R.= 53.1

DIFFERENTIAL PRESSURES

SPAN STATION 170.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.695 | 1.345 | 1.958 | 2.990 | 4.958 | 7.138 | 10.488 | DEG. |
| 0. | 0.78 | 0.55 | 0.41 | 0.25 | 0.19 | 0.10 | 0.03 | 0. |
| 5. | 0.77 | 0.54 | 0.40 | 0.23 | 0.19 | 0.09 | 0.03 | 5. |
| 10. | 0.76 | 0.53 | 0.38 | 0.21 | 0.18 | 0.09 | 0.03 | 10. |
| 15. | 0.72 | 0.51 | 0.37 | 0.20 | 0.17 | 0.08 | 0.03 | 15. |
| 20. | 0.67 | 0.48 | 0.35 | 0.20 | 0.16 | 0.07 | 0.02 | 20. |
| 25. | 0.61 | 0.44 | 0.33 | 0.19 | 0.14 | 0.06 | 0.01 | 25. |
| 30. | 0.54 | 0.40 | 0.31 | 0.16 | 0.12 | 0.05 | 0.01 | 30. |
| 35. | 0.48 | 0.36 | 0.28 | 0.14 | 0.10 | 0.04 | 0.00 | 35. |
| 40. | 0.43 | 0.33 | 0.24 | 0.11 | 0.08 | 0.04 | 0.00 | 40. |
| 45. | 0.41 | 0.30 | 0.21 | 0.10 | 0.06 | 0.03 | -0.00 | 45. |
| 50. | 0.38 | 0.28 | 0.19 | 0.09 | 0.05 | 0.03 | -0.00 | 50. |
| 55. | 0.36 | 0.26 | 0.18 | 0.08 | 0.05 | 0.03 | -0.01 | 55. |
| 60. | 0.34 | 0.24 | 0.17 | 0.07 | 0.04 | 0.02 | -0.01 | 60. |
| 65. | 0.32 | 0.22 | 0.15 | 0.06 | 0.02 | 0.02 | -0.01 | 65. |
| 70. | 0.27 | 0.20 | 0.13 | 0.04 | 0.01 | 0.01 | -0.01 | 70. |
| 75. | 0.22 | 0.16 | 0.10 | 0.02 | -0.01 | 0.01 | -0.01 | 75. |
| 80. | 0.16 | 0.12 | 0.07 | 0.01 | -0.02 | 0.01 | -0.01 | 80. |
| 85. | 0.10 | 0.07 | 0.03 | -0.01 | -0.03 | -0.00 | -0.01 | 85. |
| 90. | 0.04 | 0.03 | -0.01 | -0.03 | -0.05 | -0.01 | -0.01 | 90. |
| 95. | -0.02 | -0.01 | -0.04 | -0.05 | -0.06 | -0.03 | -0.02 | 95. |
| 100. | -0.06 | -0.05 | -0.10 | -0.07 | -0.07 | -0.04 | -0.02 | 100. |
| 105. | -0.10 | -0.10 | -0.13 | -0.09 | -0.08 | -0.05 | -0.03 | 105. |
| 110. | -0.15 | -0.16 | -0.15 | -0.12 | -0.09 | -0.06 | -0.03 | 110. |
| 115. | -0.24 | -0.18 | -0.18 | -0.14 | -0.11 | -0.06 | -0.03 | 115. |
| 120. | -0.32 | -0.22 | -0.21 | -0.16 | -0.12 | -0.07 | -0.03 | 120. |
| 125. | -0.38 | -0.27 | -0.24 | -0.17 | -0.14 | -0.08 | -0.03 | 125. |
| 130. | -0.42 | -0.32 | -0.28 | -0.18 | -0.15 | -0.08 | -0.03 | 130. |
| 135. | -0.47 | -0.35 | -0.31 | -0.18 | -0.16 | -0.08 | -0.03 | 135. |
| 140. | -0.53 | -0.39 | -0.33 | -0.18 | -0.17 | -0.09 | -0.03 | 140. |
| 145. | -0.57 | -0.42 | -0.35 | -0.18 | -0.17 | -0.08 | -0.03 | 145. |
| 150. | -0.61 | -0.45 | -0.36 | -0.19 | -0.17 | -0.08 | -0.03 | 150. |
| 155. | -0.65 | -0.47 | -0.37 | -0.19 | -0.17 | -0.08 | -0.02 | 155. |
| 160. | -0.68 | -0.49 | -0.36 | -0.19 | -0.16 | -0.08 | -0.02 | 160. |
| 165. | -0.69 | -0.49 | -0.35 | -0.18 | -0.15 | -0.08 | -0.02 | 165. |
| 170. | -0.67 | -0.47 | -0.33 | -0.18 | -0.13 | -0.08 | -0.02 | 170. |
| 175. | -0.59 | -0.44 | -0.31 | -0.18 | -0.11 | -0.07 | -0.01 | 175. |
| 180. | -0.53 | -0.41 | -0.30 | -0.18 | -0.10 | -0.06 | -0.01 | 180. |
| 185. | -0.51 | -0.39 | -0.29 | -0.18 | -0.08 | -0.05 | -0.01 | 185. |
| 190. | -0.51 | -0.38 | -0.28 | -0.17 | -0.08 | -0.04 | -0.01 | 190. |
| 195. | -0.50 | -0.36 | -0.27 | -0.17 | -0.08 | -0.04 | -0.00 | 195. |
| 200. | -0.50 | -0.35 | -0.26 | -0.15 | -0.08 | -0.03 | -0.00 | 200. |
| 205. | -0.49 | -0.34 | -0.26 | -0.14 | -0.08 | -0.04 | -0.00 | 205. |
| 210. | -0.49 | -0.32 | -0.25 | -0.13 | -0.09 | -0.04 | -0.01 | 210. |
| 215. | -0.49 | -0.31 | -0.24 | -0.12 | -0.09 | -0.05 | -0.01 | 215. |
| 220. | -0.49 | -0.30 | -0.22 | -0.11 | -0.09 | -0.05 | -0.01 | 220. |
| 225. | -0.47 | -0.29 | -0.21 | -0.10 | -0.09 | -0.04 | -0.01 | 225. |
| 230. | -0.44 | -0.28 | -0.19 | -0.09 | -0.09 | -0.04 | -0.01 | 230. |
| 235. | -0.40 | -0.27 | -0.17 | -0.09 | -0.08 | -0.03 | -0.00 | 235. |
| 240. | -0.37 | -0.26 | -0.15 | -0.08 | -0.08 | -0.02 | -0.00 | 240. |
| 245. | -0.34 | -0.24 | -0.13 | -0.08 | -0.07 | -0.01 | 0.00 | 245. |
| 250. | -0.30 | -0.21 | -0.11 | -0.07 | -0.05 | -0.01 | 0.00 | 250. |
| 255. | -0.26 | -0.18 | -0.09 | -0.06 | -0.04 | -0.00 | 0.01 | 255. |
| 260. | -0.20 | -0.14 | -0.07 | -0.04 | -0.03 | 0.00 | 0.01 | 260. |
| 265. | -0.15 | -0.10 | -0.05 | -0.03 | -0.02 | 0.01 | 0.01 | 265. |
| 270. | -0.10 | -0.06 | -0.03 | -0.01 | -0.01 | 0.01 | 0.01 | 270. |
| 275. | -0.07 | -0.03 | -0.01 | 0.00 | -0.00 | 0.01 | 0.01 | 275. |
| 280. | -0.04 | -0.00 | 0.01 | 0.02 | 0.02 | 0.02 | 0.01 | 280. |
| 285. | 0.02 | 0.03 | 0.03 | 0.03 | 0.04 | 0.02 | 0.01 | 285. |
| 290. | 0.08 | 0.06 | 0.05 | 0.04 | 0.07 | 0.03 | 0.01 | 290. |
| 295. | 0.13 | 0.09 | 0.07 | 0.05 | 0.08 | 0.03 | 0.01 | 295. |
| 300. | 0.14 | 0.11 | 0.09 | 0.06 | 0.09 | 0.03 | 0.02 | 300. |
| 305. | 0.16 | 0.14 | 0.11 | 0.08 | 0.10 | 0.04 | 0.02 | 305. |
| 310. | 0.25 | 0.20 | 0.14 | 0.11 | 0.11 | 0.04 | 0.02 | 310. |
| 315. | 0.37 | 0.27 | 0.20 | 0.15 | 0.13 | 0.05 | 0.02 | 315. |
| 320. | 0.48 | 0.33 | 0.27 | 0.18 | 0.15 | 0.06 | 0.03 | 320. |
| 325. | 0.58 | 0.38 | 0.33 | 0.20 | 0.17 | 0.07 | 0.03 | 325. |
| 330. | 0.64 | 0.41 | 0.37 | 0.22 | 0.18 | 0.08 | 0.03 | 330. |
| 335. | 0.67 | 0.44 | 0.39 | 0.25 | 0.19 | 0.08 | 0.03 | 335. |
| 340. | 0.69 | 0.47 | 0.43 | 0.27 | 0.19 | 0.09 | 0.03 | 340. |
| 345. | 0.73 | 0.50 | 0.41 | 0.28 | 0.19 | 0.10 | 0.03 | 345. |
| 350. | 0.76 | 0.53 | 0.45 | 0.28 | 0.19 | 0.10 | 0.03 | 350. |
| 355. | 0.79 | 0.54 | 0.43 | 0.27 | 0.19 | 0.10 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST•502 CNTR NO. 939 TCN• 1. C.R.• 93.1

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.445 | 1.540 | 1.950 | 2.990 | 4.550 | 7.153 | 10.400 | DEG. |
| 0. | 0.81 | 0.58 | 0.35 | 0.22 | 0.16 | 0.01 | 0.01 | 0. |
| 5. | 0.79 | 0.56 | 0.34 | 0.2C | 0.15 | 0.00 | 0.01 | 5. |
| 10. | 0.77 | 0.54 | 0.33 | 0.19 | 0.15 | 0.00 | 0.01 | 10. |
| 15. | 0.76 | 0.51 | 0.32 | 0.17 | 0.16 | 0.00 | 0.01 | 15. |
| 20. | 0.74 | 0.48 | 0.31 | 0.12 | 0.16 | -0.01 | -0.01 | 20. |
| 25. | 0.72 | 0.45 | 0.28 | 0.00 | 0.16 | -0.02 | -0.01 | 25. |
| 30. | 0.69 | 0.43 | 0.25 | 0.06 | 0.15 | -0.03 | -0.02 | 30. |
| 35. | 0.63 | 0.40 | 0.22 | 0.04 | 0.14 | -0.04 | -0.02 | 35. |
| 40. | 0.56 | 0.36 | 0.17 | 0.04 | 0.14 | -0.05 | -0.02 | 40. |
| 45. | 0.49 | 0.31 | 0.14 | 0.04 | 0.13 | -0.07 | -0.02 | 45. |
| 50. | 0.42 | 0.25 | 0.12 | 0.02 | 0.13 | -0.07 | -0.02 | 50. |
| 55. | 0.39 | 0.19 | 0.10 | 0.01 | 0.13 | -0.05 | -0.02 | 55. |
| 60. | 0.38 | 0.16 | 0.08 | -0.01 | 0.13 | -0.05 | -0.03 | 60. |
| 65. | 0.38 | 0.15 | 0.07 | -0.02 | 0.11 | -0.05 | -0.03 | 65. |
| 70. | 0.34 | 0.14 | 0.06 | -0.04 | 0.09 | -0.06 | -0.03 | 70. |
| 75. | 0.28 | 0.12 | 0.04 | -0.05 | 0.06 | -0.06 | -0.03 | 75. |
| 80. | 0.21 | 0.08 | 0.02 | -0.06 | 0.04 | -0.06 | -0.03 | 80. |
| 85. | 0.14 | 0.04 | -0.00 | -0.00 | 0.02 | -0.06 | -0.04 | 85. |
| 90. | 0.06 | -0.00 | -0.03 | -0.09 | -0.00 | -0.06 | -0.04 | 90. |
| 95. | -0.01 | -0.05 | -0.07 | -0.1C | -0.02 | -0.06 | -0.04 | 95. |
| 100. | -0.06 | -0.09 | -0.13 | -0.12 | -0.03 | -0.06 | -0.03 | 100. |
| 105. | -0.15 | -0.14 | -0.19 | -0.14 | -0.05 | -0.06 | -0.03 | 105. |
| 110. | -0.21 | -0.20 | -0.24 | -0.17 | -0.07 | -0.07 | -0.03 | 110. |
| 115. | -0.32 | -0.24 | -0.27 | -0.20 | -0.09 | -0.07 | -0.03 | 115. |
| 120. | -0.42 | -0.34 | -0.30 | -0.22 | -0.11 | -0.07 | -0.02 | 120. |
| 125. | -0.53 | -0.43 | -0.32 | -0.24 | -0.13 | -0.07 | -0.02 | 125. |
| 130. | -0.64 | -0.51 | -0.34 | -0.25 | -0.14 | -0.07 | -0.02 | 130. |
| 135. | -0.74 | -0.57 | -0.35 | -0.25 | -0.15 | -0.06 | -0.01 | 135. |
| 140. | -0.83 | -0.60 | -0.36 | -0.26 | -0.15 | -0.06 | -0.01 | 140. |
| 145. | -0.90 | -0.60 | -0.37 | -0.23 | -0.15 | -0.05 | -0.00 | 145. |
| 150. | -0.96 | -0.57 | -0.36 | -0.23 | -0.15 | -0.04 | 0.01 | 150. |
| 155. | -0.05 | -C.52 | -0.34 | -C.23 | -0.15 | -0.03 | 0.01 | 155. |
| 160. | -0.0C | -C.51 | -0.32 | -0.22 | -0.14 | -0.02 | 0.00 | 160. |
| 165. | -0.07 | -0.59 | -0.33 | -C.20 | -0.13 | -0.01 | -0.00 | 165. |
| 170. | -0.96 | -0.05 | -0.34 | -C.16 | -0.12 | 0.01 | 0.00 | 170. |
| 175. | -1.02 | -C.66 | -0.34 | -0.11 | -0.11 | 0.04 | C.02 | 175. |
| 180. | -0.97 | -0.6C | -C.27 | -0.06 | -0.09 | 0.07 | 0.03 | 180. |
| 185. | -0.04 | -C.44 | -0.18 | -0.03 | -0.06 | 0.08 | C.03 | 185. |
| 190. | -0.60 | -C.35 | -0.11 | -C.01 | -0.04 | 0.08 | 0.01 | 190. |
| 195. | -0.55 | -0.30 | -0.09 | C.01 | -0.03 | 0.07 | -0.00 | 195. |
| 200. | -0.48 | -0.28 | -0.08 | 0.01 | -0.03 | 0.05 | -0.01 | 200. |
| 205. | -0.45 | -0.27 | -0.08 | 0.01 | -0.04 | 0.04 | -0.0C | 205. |
| 210. | -0.44 | -0.27 | -0.08 | -0.00 | -0.05 | 0.05 | -0.00 | 210. |
| 215. | -0.43 | -0.26 | -0.10 | -0.01 | -0.06 | 0.03 | -0.01 | 215. |
| 220. | -0.42 | -0.25 | -0.10 | -C.02 | -0.06 | 0.02 | 0.00 | 220. |
| 225. | -0.38 | -0.24 | -0.10 | -0.02 | -0.06 | 0.03 | 0.01 | 225. |
| 230. | -0.35 | -0.24 | -0.10 | -0.02 | -0.05 | 0.05 | 0.01 | 230. |
| 235. | -0.35 | -C.23 | -0.10 | -0.02 | -0.05 | 0.04 | 0.01 | 235. |
| 240. | -0.32 | -0.21 | -0.09 | -0.02 | -0.05 | 0.04 | 0.02 | 240. |
| 245. | -0.28 | -0.16 | -0.07 | -0.02 | -0.05 | 0.05 | 0.03 | 245. |
| 250. | -0.08 | -0.00 | -0.05 | -0.00 | -0.05 | 0.05 | 0.03 | 250. |
| 255. | -0.00 | -0.01 | -0.03 | 0.02 | -0.05 | 0.06 | 0.03 | 255. |
| 260. | -0.1C | 0.02 | -0.02 | 0.04 | -0.05 | 0.06 | 0.03 | 260. |
| 265. | -0.09 | 0.02 | -0.00 | 0.05 | -0.05 | 0.06 | 0.03 | 265. |
| 270. | -0.00 | 0.01 | 0.01 | 0.04 | -0.04 | 0.07 | 0.04 | 270. |
| 275. | -0.00 | -0.02 | 0.02 | 0.04 | -0.07 | 0.07 | 0.04 | 275. |
| 280. | -0.07 | -0.07 | 0.02 | 0.04 | -0.08 | 0.07 | 0.04 | 280. |
| 285. | -0.06 | -0.07 | 0.02 | 0.03 | -0.08 | 0.07 | 0.05 | 285. |
| 290. | -0.03 | 0.02 | 0.05 | 0.04 | -0.08 | 0.06 | 0.05 | 290. |
| 295. | 0.36 | 0.26 | 0.15 | 0.11 | -0.05 | 0.04 | 0.03 | 295. |
| 300. | 0.44 | 0.32 | 0.18 | 0.13 | -0.02 | -0.00 | 0.00 | 300. |
| 305. | 0.4C | 0.23 | 0.13 | 0.11 | -0.02 | -0.01 | -0.00 | 305. |
| 310. | 0.47 | 0.30 | 0.17 | 0.11 | -0.03 | 0.01 | 0.00 | 310. |
| 315. | 0.53 | 0.39 | 0.22 | 0.12 | -0.03 | 0.03 | 0.01 | 315. |
| 320. | 0.58 | 0.43 | 0.22 | 0.14 | -0.00 | 0.02 | 0.00 | 320. |
| 325. | 0.65 | 0.47 | 0.23 | 0.10 | 0.00 | 0.01 | 0.01 | 325. |
| 330. | 0.76 | 0.55 | 0.29 | 0.23 | 0.10 | 0.01 | 0.01 | 330. |
| 335. | 0.83 | 0.59 | 0.34 | 0.25 | 0.19 | 0.02 | 0.00 | 335. |
| 340. | 0.80 | 0.59 | 0.33 | 0.24 | 0.18 | 0.02 | 0.00 | 340. |
| 345. | 0.80 | 0.57 | 0.33 | 0.22 | 0.17 | 0.01 | 0.01 | 345. |
| 350. | 0.82 | 0.58 | 0.37 | 0.23 | 0.16 | 0.01 | 0.01 | 350. |
| 355. | 0.83 | 0.59 | 0.36 | 0.24 | 0.16 | 0.01 | 0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 538 TCN= 1. C.R.= 53.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.435 | 1.040 | 1.950 | 2.990 | 4.999 | 7.150 | 10.400 | DEG. |
| 0. | -1.98 | -0.86 | -0.52 | -C.38 | -0.28 | -0.09 | 0.00 | 0. |
| 5. | -1.93 | -0.84 | -0.53 | -C.38 | -0.21 | -0.09 | -0.00 | 5. |
| 10. | -1.84 | -0.78 | -0.53 | -C.38 | -0.22 | -0.09 | 0.00 | 10. |
| 15. | -1.74 | -0.77 | -0.52 | -0.37 | -0.22 | -0.09 | -0.01 | 15. |
| 20. | -1.77 | -0.83 | -0.51 | -0.37 | -0.21 | -0.10 | -0.03 | 20. |
| 25. | -1.79 | -0.85 | -C.51 | -0.38 | -0.21 | -0.12 | -0.04 | 25. |
| 30. | -1.79 | -0.85 | -0.52 | -0.39 | -0.21 | -0.13 | -0.04 | 30. |
| 35. | -1.81 | -0.84 | -0.54 | -0.41 | -0.21 | -0.14 | -0.05 | 35. |
| 40. | -1.86 | -0.91 | -0.56 | -0.42 | -0.23 | -0.14 | -0.05 | 40. |
| 45. | -2.06 | -0.96 | -0.59 | -0.43 | -0.23 | -0.14 | -0.05 | 45. |
| 50. | -2.02 | -0.91 | -0.59 | -0.42 | -0.23 | -0.13 | -0.05 | 50. |
| 55. | -1.98 | -0.81 | -0.55 | -0.41 | -0.23 | -0.12 | -0.05 | 55. |
| 60. | -1.72 | -0.70 | -0.50 | -0.39 | -0.22 | -0.12 | -0.05 | 60. |
| 65. | -1.58 | -0.61 | -0.45 | -0.36 | -0.20 | -0.12 | -0.05 | 65. |
| 70. | -1.56 | -0.63 | -0.43 | -0.34 | -0.20 | -0.11 | -0.06 | 70. |
| 75. | -1.41 | -0.64 | -0.42 | -0.32 | -0.1* | -0.13 | -0.06 | 75. |
| 80. | -1.3C | -0.56 | -0.41 | -0.30 | -0.18 | -0.13 | -0.06 | 80. |
| 85. | -1.25 | -0.46 | -0.36 | -0.28 | -0.17 | -0.15 | -0.06 | 85. |
| 90. | -1.2E | -0.39 | -0.30 | -0.24 | -0.15 | -0.12 | -0.06 | 90. |
| 95. | -1.11 | -0.37 | -0.24 | -0.20 | -0.13 | -0.11 | -0.06 | 95. |
| 100. | -0.92 | -0.29 | -0.19 | -0.15 | -0.11 | -0.10 | -0.06 | 100. |
| 105. | -0.68 | -0.14 | -0.15 | -0.20 | -0.09 | -0.09 | -0.06 | 105. |
| 110. | -0.50 | 0.00 | -0.07 | -0.03 | -0.07 | -0.08 | -0.06 | 110. |
| 115. | -0.33 | 0.09 | -0.00 | 0.01 | -0.06 | -0.07 | -0.06 | 115. |
| 120. | -0.2C | 0.15 | 0.04 | C.03 | -0.05 | -0.06 | -0.06 | 120. |
| 125. | -0.18 | 0.15 | 0.05 | C.04 | -0.03 | -0.05 | -0.05 | 125. |
| 130. | -0.03 | 0.18 | 0.06 | 0.05 | -0.02 | -0.04 | -0.04 | 130. |
| 135. | 0.17 | 0.28 | 0.11 | 0.07 | 0.00 | -0.03 | -0.03 | 135. |
| 140. | 0.27 | 0.37 | 0.17 | 0.09 | 0.02 | -0.02 | -0.02 | 140. |
| 145. | 0.34 | 0.45 | 0.22 | 0.12 | 0.04 | -0.01 | -0.01 | 145. |
| 150. | 0.52 | 0.49 | 0.27 | C.14 | 0.07 | 0.00 | -0.00 | 150. |
| 155. | 0.68 | 0.45 | 0.26 | C.16 | 0.08 | 0.01 | -0.00 | 155. |
| 160. | 0.66 | C.42 | 0.25 | 0.17 | 0.10 | 0.02 | -0.00 | 160. |
| 165. | 0.92 | 0.44 | 0.28 | 0.19 | 0.12 | 0.04 | 0.01 | 165. |
| 170. | 1.20 | 0.57 | 0.38 | 0.27 | 0.14 | 0.06 | 0.01 | 170. |
| 175. | 2.34 | 0.75 | 0.47 | C.36 | 0.17 | 0.08 | 0.02 | 175. |
| 180. | 2.95 | 0.87 | 0.53 | C.41 | 0.22 | 0.10 | 0.03 | 180. |
| 185. | 2.78 | 0.95 | 0.56 | 0.44 | 0.25 | 0.11 | 0.04 | 185. |
| 190. | 2.83 | 0.94 | 0.59 | 0.45 | 0.25 | 0.13 | 0.05 | 190. |
| 195. | 2.77 | 0.89 | 0.60 | 0.45 | 0.25 | 0.13 | 0.05 | 195. |
| 200. | 2.69 | 0.83 | 0.60 | 0.45 | 0.26 | 0.14 | 0.05 | 200. |
| 205. | 2.74 | 0.79 | 0.59 | 0.44 | 0.25 | 0.14 | 0.05 | 205. |
| 210. | 2.58 | 0.80 | 0.58 | C.43 | 0.25 | 0.14 | 0.04 | 210. |
| 215. | 2.2C | 0.80 | 0.56 | 0.41 | 0.24 | 0.14 | 0.04 | 215. |
| 220. | 2.20 | C.76 | 0.53 | 0.39 | 0.23 | 0.14 | 0.04 | 220. |
| 225. | 1.75 | 0.72 | 0.49 | 0.38 | 0.22 | 0.14 | 0.05 | 225. |
| 230. | 1.57 | 0.72 | 0.47 | 0.38 | 0.21 | 0.15 | 0.05 | 230. |
| 235. | 1.91 | 0.74 | 0.50 | 0.38 | 0.22 | 0.15 | 0.05 | 235. |
| 240. | 2.04 | C.77 | 0.53 | C.39 | 0.22 | 0.15 | 0.05 | 240. |
| 245. | 1.81 | 0.79 | 0.53 | 0.39 | 0.23 | 0.16 | 0.06 | 245. |
| 250. | 1.73 | 0.80 | 0.53 | 0.39 | 0.24 | 0.16 | 0.06 | 250. |
| 255. | 1.83 | 0.81 | 0.53 | 0.39 | 0.24 | 0.16 | 0.06 | 255. |
| 260. | 1.84 | 0.81 | 0.54 | C.40 | 0.25 | 0.17 | 0.06 | 260. |
| 265. | 1.96 | C.81 | 0.55 | C.40 | 0.25 | 0.17 | 0.07 | 265. |
| 270. | 2.00 | 0.77 | 0.56 | 0.41 | 0.26 | 0.17 | 0.07 | 270. |
| 275. | 1.91 | 0.77 | 0.60 | 0.42 | 0.26 | 0.16 | 0.07 | 275. |
| 280. | 2.09 | 0.83 | 0.66 | 0.43 | 0.26 | 0.16 | 0.07 | 280. |
| 285. | 2.32 | C.80 | 0.63 | 0.44 | 0.27 | 0.16 | 0.07 | 285. |
| 290. | 1.62 | 0.59 | 0.36 | 0.3C | 0.21 | 0.11 | 0.06 | 290. |
| 295. | 0.48 | 0.36 | 0.13 | C.04 | 0.04 | 0.01 | 0.01 | 295. |
| 300. | -0.77 | -0.15 | -0.10 | -0.17 | -0.09 | -0.07 | -0.02 | 300. |
| 305. | -1.55 | -0.66 | -0.36 | -C.25 | -0.13 | -0.07 | C.00 | 305. |
| 310. | -1.40 | -0.58 | -0.28 | -0.23 | -0.12 | -0.02 | 0.01 | 310. |
| 315. | -1.52 | -C.64 | -0.42 | -C.29 | -0.13 | -0.03 | C.00 | 315. |
| 320. | -1.05 | -0.00 | -0.56 | -0.35 | -0.18 | -0.05 | -0.00 | 320. |
| 325. | -1.94 | -0.87 | -0.53 | -0.35 | -0.19 | -0.04 | 0.00 | 325. |
| 330. | -1.87 | -0.71 | -0.48 | -0.33 | -0.17 | -0.04 | C.00 | 330. |
| 335. | -1.73 | -0.73 | -0.46 | -0.31 | -0.16 | -0.05 | -0.01 | 335. |
| 340. | -1.76 | -C.00 | -0.48 | -0.33 | -0.17 | -0.07 | -0.01 | 340. |
| 345. | -1.06 | -0.86 | -0.52 | -0.36 | -0.18 | -0.00 | -C.01 | 345. |
| 350. | -1.89 | -0.85 | -0.51 | -0.36 | -0.19 | -0.00 | 0.00 | 350. |
| 355. | -1.90 | -0.84 | -0.51 | -C.36 | -0.19 | -0.00 | 0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 5r3 ICN= 4. C.R.= 37.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.435 | 1.952 | 4.550 | 10.400 | DEG. |
| 0. | -0.02 | -0.02 | 0.10 | -0.01 | 0. |
| 5. | -0.03 | 0.04 | 0.21 | 0.02 | 5. |
| 10. | -0.04 | 0.01 | 0.13 | 0.05 | 10. |
| 15. | 0.01 | 0.01 | 0.09 | 0.03 | 15. |
| 20. | 0.00 | 0.05 | 0.09 | 0.01 | 20. |
| 25. | 0.19 | 0.09 | 0.07 | 0.02 | 25. |
| 30. | 0.27 | 0.12 | 0.04 | 0.02 | 30. |
| 35. | 0.28 | 0.10 | 0.01 | 0.03 | 35. |
| 40. | 0.26 | 0.05 | -0.00 | 0.03 | 40. |
| 45. | 0.20 | 0.00 | 0.01 | 0.02 | 45. |
| 50. | 0.12 | -0.02 | 0.05 | 0.02 | 50. |
| 55. | 0.07 | 0.02 | 0.09 | 0.01 | 55. |
| 60. | 0.13 | 0.05 | 0.09 | 0.01 | 60. |
| 65. | 0.14 | 0.04 | 0.05 | 0.02 | 65. |
| 70. | 0.08 | 0.04 | 0.02 | 0.02 | 70. |
| 75. | 0.14 | 0.07 | 0.04 | 0.02 | 75. |
| 80. | 0.23 | 0.10 | 0.07 | 0.02 | 80. |
| 85. | 0.27 | 0.14 | 0.08 | 0.01 | 85. |
| 90. | 0.16 | 0.13 | 0.05 | 0.01 | 90. |
| 95. | 0.09 | 0.11 | 0.03 | 0.00 | 95. |
| 100. | 0.09 | 0.09 | 0.03 | 0.00 | 100. |
| 105. | 0.10 | 0.08 | 0.03 | 0.00 | 105. |
| 110. | 0.07 | 0.08 | 0.03 | 0.00 | 110. |
| 115. | 0.11 | 0.09 | 0.03 | 0.01 | 115. |
| 120. | 0.20 | 0.09 | 0.02 | 0.01 | 120. |
| 125. | 0.14 | 0.08 | 0.01 | -0.00 | 125. |
| 130. | 0.05 | 0.08 | -0.00 | -0.01 | 130. |
| 135. | 0.05 | 0.07 | -0.00 | -0.01 | 135. |
| 140. | 0.07 | 0.06 | 0.00 | -0.01 | 140. |
| 145. | 0.02 | 0.03 | -0.01 | -0.01 | 145. |
| 150. | -0.04 | 0.01 | -0.02 | -0.01 | 150. |
| 155. | -0.07 | -0.01 | -0.02 | -0.02 | 155. |
| 160. | -0.03 | -0.01 | -0.01 | -0.03 | 160. |
| 165. | 0.02 | -0.03 | 0.00 | 0.02 | 165. |
| 170. | 0.04 | 0.01 | 0.00 | 0.03 | 170. |
| 175. | 0.01 | 0.02 | 0.00 | 0.03 | 175. |
| 180. | -0.01 | 0.01 | -0.00 | 0.02 | 180. |
| 185. | -0.02 | 0.00 | 0.00 | 0.01 | 185. |
| 190. | -0.03 | -0.01 | 0.01 | 0.01 | 190. |
| 195. | -0.04 | -0.02 | 0.01 | 0.02 | 195. |
| 200. | -0.07 | -0.03 | 0.00 | 0.02 | 200. |
| 205. | -0.10 | -0.05 | -0.01 | 0.02 | 205. |
| 210. | -0.10 | -0.04 | -0.03 | 0.01 | 210. |
| 215. | -0.03 | -0.04 | -0.04 | 0.01 | 215. |
| 220. | 0.04 | -0.04 | -0.04 | 0.01 | 220. |
| 225. | 0.02 | -0.04 | -0.04 | 0.01 | 225. |
| 230. | -0.05 | -0.03 | -0.03 | 0.01 | 230. |
| 235. | -0.09 | -0.03 | -0.02 | 0.00 | 235. |
| 240. | -0.08 | -0.03 | -0.02 | -0.00 | 240. |
| 245. | -0.07 | -0.03 | -0.03 | -0.01 | 245. |
| 250. | -0.12 | -0.04 | -0.04 | -0.01 | 250. |
| 255. | -0.19 | -0.07 | -0.05 | -0.02 | 255. |
| 260. | -0.25 | -0.10 | -0.04 | -0.02 | 260. |
| 265. | -0.21 | -0.09 | -0.04 | -0.02 | 265. |
| 270. | -0.19 | -0.07 | -0.03 | -0.02 | 270. |
| 275. | -0.08 | -0.04 | -0.03 | -0.02 | 275. |
| 280. | -0.08 | -0.04 | -0.05 | -0.02 | 280. |
| 285. | -0.13 | -0.07 | -0.07 | -0.03 | 285. |
| 290. | -0.19 | -0.10 | -0.08 | -0.04 | 290. |
| 295. | -0.25 | -0.13 | -0.08 | -0.04 | 295. |
| 300. | -0.27 | -0.12 | -0.07 | -0.05 | 300. |
| 305. | -0.22 | -0.11 | -0.07 | -0.05 | 305. |
| 310. | -0.15 | -0.09 | -0.06 | -0.04 | 310. |
| 315. | -0.10 | -0.07 | -0.06 | -0.04 | 315. |
| 320. | -0.07 | -0.06 | -0.05 | -0.03 | 320. |
| 325. | -0.06 | -0.05 | -0.05 | -0.03 | 325. |
| 330. | -0.06 | -0.04 | -0.06 | -0.03 | 330. |
| 335. | -0.06 | -0.03 | -0.07 | -0.03 | 335. |
| 340. | -0.06 | -0.03 | -0.07 | -0.02 | 340. |
| 345. | -0.06 | -0.04 | -0.06 | -0.01 | 345. |
| 350. | -0.06 | -0.06 | -0.06 | -0.00 | 350. |
| 355. | -0.06 | -0.11 | -0.02 | 0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 563 TCN= 4. C.R.= 57.9

DIFFERENTIAL PRESSURES

SPAN STATION 74.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.240 | 1.950 | 2.990 | 4.550 | 7.150 | 10.493 | DEG. |
| 0. | 0.14 | 0.07 | 0.06 | 0.04 | -0.02 | 0.01 | 0.01 | 0. |
| 5. | 0.18 | 0.18 | 0.15 | 0.08 | 0.00 | 0.04 | 0.03 | 5. |
| 10. | 0.20 | 0.19 | 0.17 | 0.10 | 0.03 | 0.04 | 0.03 | 10. |
| 15. | 0.26 | 0.22 | 0.19 | 0.12 | 0.06 | 0.05 | 0.03 | 15. |
| 20. | 0.36 | 0.30 | 0.23 | 0.16 | 0.09 | 0.06 | 0.03 | 20. |
| 25. | 0.44 | 0.34 | 0.27 | 0.18 | 0.11 | 0.07 | 0.03 | 25. |
| 30. | 0.58 | 0.43 | 0.30 | 0.20 | 0.11 | 0.07 | 0.04 | 30. |
| 35. | 0.65 | 0.44 | 0.31 | 0.21 | 0.11 | 0.07 | 0.04 | 35. |
| 40. | 0.62 | 0.41 | 0.30 | 0.19 | 0.11 | 0.06 | 0.03 | 40. |
| 45. | 0.50 | 0.33 | 0.24 | 0.17 | 0.11 | 0.05 | 0.03 | 45. |
| 50. | 0.29 | 0.19 | 0.18 | 0.14 | 0.10 | 0.04 | 0.03 | 50. |
| 55. | 0.19 | 0.17 | 0.16 | 0.12 | 0.10 | 0.05 | 0.04 | 55. |
| 60. | 0.27 | 0.20 | 0.16 | 0.11 | 0.08 | 0.05 | 0.04 | 60. |
| 65. | 0.24 | 0.19 | 0.17 | 0.11 | 0.08 | 0.05 | 0.03 | 65. |
| 70. | 0.24 | 0.20 | 0.17 | 0.12 | 0.08 | 0.05 | 0.02 | 70. |
| 75. | 0.33 | 0.23 | 0.16 | 0.12 | 0.09 | 0.04 | 0.03 | 75. |
| 80. | 0.31 | 0.20 | 0.15 | 0.09 | 0.09 | 0.04 | 0.03 | 80. |
| 85. | 0.19 | 0.14 | 0.13 | 0.05 | 0.08 | 0.03 | 0.01 | 85. |
| 90. | 0.13 | 0.11 | 0.10 | 0.05 | 0.08 | 0.03 | 0.00 | 90. |
| 95. | 0.13 | 0.10 | 0.07 | 0.05 | 0.07 | 0.03 | -0.00 | 95. |
| 100. | 0.11 | 0.09 | 0.05 | 0.05 | 0.07 | 0.02 | -0.00 | 100. |
| 105. | 0.10 | 0.08 | 0.04 | 0.04 | 0.06 | 0.02 | -0.00 | 105. |
| 110. | 0.08 | 0.08 | 0.04 | 0.03 | 0.06 | 0.02 | -0.01 | 110. |
| 115. | 0.07 | 0.07 | 0.04 | 0.02 | 0.05 | 0.01 | -0.01 | 115. |
| 120. | 0.08 | 0.06 | 0.04 | 0.01 | 0.04 | 0.01 | -0.02 | 120. |
| 125. | 0.08 | 0.05 | 0.03 | -0.00 | 0.04 | 0.00 | -0.02 | 125. |
| 130. | 0.07 | 0.05 | 0.03 | -0.01 | 0.03 | -0.00 | -0.02 | 130. |
| 135. | 0.04 | 0.04 | 0.02 | -0.01 | 0.03 | -0.00 | -0.02 | 135. |
| 140. | 0.01 | 0.03 | 0.02 | -0.01 | 0.03 | -0.01 | -0.02 | 140. |
| 145. | -0.01 | 0.03 | 0.01 | -0.01 | 0.02 | -0.01 | -0.02 | 145. |
| 150. | -0.02 | 0.02 | -0.00 | -0.01 | 0.02 | -0.01 | -0.02 | 150. |
| 155. | -0.02 | 0.02 | -0.02 | -0.01 | 0.02 | -0.01 | -0.01 | 155. |
| 160. | -0.01 | 0.02 | -0.02 | -0.00 | 0.03 | 0.00 | -0.01 | 160. |
| 165. | 0.01 | 0.02 | -0.02 | 0.00 | 0.04 | 0.01 | -0.01 | 165. |
| 170. | 0.04 | 0.03 | -0.01 | 0.02 | 0.05 | 0.02 | -0.00 | 170. |
| 175. | 0.06 | 0.05 | 0.01 | 0.03 | 0.06 | 0.02 | -0.00 | 175. |
| 180. | 0.09 | 0.07 | 0.03 | 0.05 | 0.07 | 0.02 | -0.00 | 180. |
| 185. | 0.09 | 0.08 | 0.04 | 0.04 | 0.07 | 0.02 | -0.00 | 185. |
| 190. | 0.07 | 0.07 | 0.05 | 0.03 | 0.06 | 0.02 | -0.00 | 190. |
| 195. | 0.03 | 0.05 | 0.03 | 0.01 | 0.04 | 0.01 | -0.00 | 195. |
| 200. | -0.02 | 0.02 | 0.01 | -0.01 | 0.03 | 0.00 | -0.01 | 200. |
| 205. | -0.06 | -0.02 | -0.02 | -0.03 | 0.01 | -0.01 | -0.02 | 205. |
| 210. | -0.11 | -0.07 | -0.05 | -0.04 | -0.01 | -0.02 | -0.02 | 210. |
| 215. | -0.17 | -0.11 | -0.08 | -0.06 | -0.03 | -0.02 | -0.03 | 215. |
| 220. | -0.24 | -0.15 | -0.11 | -0.07 | -0.05 | -0.03 | -0.03 | 220. |
| 225. | -0.27 | -0.17 | -0.13 | -0.08 | -0.06 | -0.03 | -0.03 | 225. |
| 230. | -0.24 | -0.18 | -0.13 | -0.10 | -0.06 | -0.03 | -0.03 | 230. |
| 235. | -0.22 | -0.16 | -0.13 | -0.11 | -0.06 | -0.03 | -0.03 | 235. |
| 240. | -0.21 | -0.17 | -0.13 | -0.10 | -0.06 | -0.03 | -0.03 | 240. |
| 245. | -0.21 | -0.16 | -0.12 | -0.10 | -0.07 | -0.04 | -0.02 | 245. |
| 250. | -0.21 | -0.15 | -0.12 | -0.09 | -0.07 | -0.03 | -0.02 | 250. |
| 255. | -0.21 | -0.15 | -0.11 | -0.09 | -0.07 | -0.03 | -0.02 | 255. |
| 260. | -0.21 | -0.15 | -0.11 | -0.09 | -0.07 | -0.03 | -0.02 | 260. |
| 265. | -0.21 | -0.16 | -0.11 | -0.08 | -0.07 | -0.04 | -0.01 | 265. |
| 270. | -0.22 | -0.16 | -0.11 | -0.08 | -0.07 | -0.04 | -0.01 | 270. |
| 275. | -0.22 | -0.17 | -0.12 | -0.08 | -0.07 | -0.04 | -0.01 | 275. |
| 280. | -0.22 | -0.18 | -0.13 | -0.08 | -0.08 | -0.04 | -0.01 | 280. |
| 285. | -0.22 | -0.19 | -0.13 | -0.08 | -0.08 | -0.04 | -0.01 | 285. |
| 290. | -0.22 | -0.19 | -0.13 | -0.08 | -0.09 | -0.04 | -0.00 | 290. |
| 295. | -0.23 | -0.19 | -0.13 | -0.08 | -0.09 | -0.04 | -0.00 | 295. |
| 300. | -0.24 | -0.20 | -0.12 | -0.08 | -0.09 | -0.04 | -0.00 | 300. |
| 305. | -0.24 | -0.20 | -0.12 | -0.07 | -0.09 | -0.04 | -0.00 | 305. |
| 310. | -0.25 | -0.20 | -0.13 | -0.07 | -0.09 | -0.04 | -0.00 | 310. |
| 315. | -0.25 | -0.21 | -0.15 | -0.07 | -0.10 | -0.04 | 0.00 | 315. |
| 320. | -0.27 | -0.21 | -0.16 | -0.08 | -0.11 | -0.04 | 0.00 | 320. |
| 325. | -0.30 | -0.21 | -0.17 | -0.09 | -0.12 | -0.04 | 0.00 | 325. |
| 330. | -0.31 | -0.22 | -0.18 | -0.10 | -0.13 | -0.04 | -0.00 | 330. |
| 335. | -0.30 | -0.23 | -0.19 | -0.12 | -0.13 | -0.04 | -0.00 | 335. |
| 340. | -0.31 | -0.27 | -0.18 | -0.13 | -0.14 | -0.05 | -0.00 | 340. |
| 345. | -0.38 | -0.31 | -0.20 | -0.13 | -0.14 | -0.05 | 0.00 | 345. |
| 350. | -0.43 | -0.32 | -0.21 | -0.14 | -0.15 | -0.04 | 0.00 | 350. |
| 355. | -0.37 | -0.27 | -0.19 | -0.14 | -0.13 | -0.04 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 563 TCN= 4. C.R.= 37.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | AZ |
|---|---|---|---|---|---|---|---|
| DEG. | 2.455 | 1.040 | 1.959 | 2.990 | 4.550 | 7.153 | 10.400 | DEG. |
| 0. | 0.14 | 0.13 | 0.07 | 0.09 | 0.05 | 0.03 | 0.02 | 0. |
| 5. | 0.24 | 0.2C | 0.15 | 0.15 | 0.08 | 0.05 | 0.02 | 5. |
| 10. | 0.30 | C.26 | 0.20 | 0.17 | 0.11 | 0.06 | 0.01 | 10. |
| 15. | 0.36 | 0.30 | 0.21 | 0.17 | 0.13 | 0.06 | 0.02 | 15. |
| 20. | 0.38 | 0.34 | 0.21 | 0.17 | 0.14 | 0.07 | 0.03 | 20. |
| 25. | 0.42 | 0.39 | 0.26 | 0.20 | 0.16 | 0.09 | 0.04 | 25. |
| 30. | 0.43 | 0.49 | 0.38 | 0.28 | 0.20 | 0.10 | 0.04 | 30. |
| 35. | 0.84 | 0.58 | 0.44 | 0.33 | 0.24 | 0.11 | 0.04 | 35. |
| 40. | 0.84 | 0.57 | 0.40 | 0.32 | 0.23 | 0.11 | 0.03 | 40. |
| 45. | 0.72 | 0.51 | 0.32 | 0.28 | 0.19 | 0.10 | C.04 | 45. |
| 50. | 0.53 | C.41 | 0.25 | 0.22 | 0.16 | 0.09 | 0.03 | 50. |
| 55. | 0.36 | C.31 | 0.21 | C.16 | 0.14 | 0.07 | 0.02 | 55. |
| 60. | 0.34 | 0.26 | 0.20 | 0.14 | 0.12 | 0.06 | 0.02 | 60. |
| 65. | 0.35 | C.26 | 0.20 | 0.15 | C.12 | 0.06 | 0.02 | 65. |
| 70. | 0.35 | 0.28 | 0.20 | 0.16 | C.13 | 0.06 | 0.02 | 70. |
| 75. | 0.33 | C.28 | 0.19 | 0.15 | 0.12 | 0.06 | 0.02 | 75. |
| 80. | 0.29 | 0.25 | 0.17 | 0.13 | 0.11 | 0.05 | C.02 | 80. |
| 85. | 0.26 | 0.21 | 0.14 | 0.11 | 0.09 | 0.04 | 0.02 | 85. |
| 90. | 0.23 | 0.17 | 0.11 | 0.09 | 0.08 | 0.03 | 0.01 | 90. |
| 95. | 0.20 | C.15 | 0.09 | 0.07 | 0.07 | 0.02 | 0.01 | 95. |
| 100. | 0.15 | 0.13 | 0.07 | 0.05 | 0.06 | 0.01 | 0.00 | 100. |
| 105. | 0.10 | 0.12 | 0.05 | 0.03 | 0.05 | 0.00 | -C.00 | 105. |
| 110. | 0.06 | C.10 | 0.04 | 0.01 | 0.03 | -0.01 | -0.01 | 110. |
| 115. | 0.04 | 0.08 | 0.02 | -0.00 | 0.02 | -0.02 | -0.01 | 115. |
| 120. | 0.04 | 0.04 | 0.01 | -0.01 | 0.01 | -0.02 | -0.01 | 120. |
| 125. | 0.04 | -0.02 | -0.02 | -0.02 | -0.00 | -0.03 | -0.01 | 125. |
| 130. | -0.04 | -0.06 | -0.04 | -0.04 | -0.01 | -0.03 | -0.01 | 130. |
| 135. | -0.11 | -0.11 | -0.06 | -0.07 | -0.02 | -0.03 | -0.01 | 135. |
| 140. | -0.13 | -0.12 | -0.08 | -0.09 | -0.04 | -0.03 | -0.01 | 140. |
| 145. | -0.13 | -0.12 | -0.10 | -0.09 | -0.05 | -0.03 | -0.01 | 145. |
| 150. | -0.13 | -0.13 | -0.11 | -0.10 | -0.05 | -0.03 | -0.01 | 150. |
| 155. | -0.15 | -0.15 | -0.11 | -0.10 | -0.05 | -0.03 | -0.01 | 155. |
| 160. | -0.17 | -0.16 | -0.12 | -0.10 | -0.05 | -0.03 | -0.01 | 160. |
| 165. | -0.18 | -0.16 | -0.12 | -0.10 | -0.05 | -0.03 | -0.01 | 165. |
| 170. | -0.18 | -0.15 | -0.12 | -0.10 | -0.06 | -0.02 | -0.01 | 170. |
| 175. | -0.18 | -0.14 | -0.12 | -0.09 | -0.06 | -0.02 | -0.01 | 175. |
| 180. | -0.18 | -0.15 | -0.12 | -0.08 | -0.05 | -0.02 | -0.00 | 180. |
| 185. | -0.19 | -0.17 | -0.12 | -0.07 | -0.04 | -0.03 | -0.01 | 185. |
| 190. | -0.21 | -0.19 | -0.13 | -0.08 | -0.05 | -0.03 | -0.01 | 190. |
| 195. | -0.23 | -0.20 | -0.14 | -0.10 | -0.06 | -0.03 | -0.01 | 195. |
| 200. | -0.24 | -0.21 | -0.15 | -0.11 | -0.07 | -0.04 | -0.01 | 200. |
| 205. | -0.24 | -0.21 | -0.15 | -0.11 | -0.07 | -0.03 | -0.01 | 205. |
| 210. | -0.20 | -0.21 | -0.14 | -0.10 | -0.07 | -0.03 | -0.01 | 210. |
| 215. | -0.18 | -0.21 | -0.13 | -0.09 | -0.07 | -0.03 | -0.01 | 215. |
| 220. | -0.22 | -0.22 | -0.12 | -0.10 | -0.08 | -0.03 | -0.01 | 220. |
| 225. | -0.26 | -0.22 | -0.11 | -0.11 | -0.09 | -0.03 | -0.01 | 225. |
| 230. | -0.31 | -0.23 | -0.13 | -0.12 | -0.09 | -0.03 | -0.01 | 230. |
| 235. | -0.30 | -0.23 | -0.14 | -0.13 | -0.09 | -0.03 | -0.01 | 235. |
| 240. | -0.27 | -0.24 | -0.16 | -0.13 | -0.09 | -0.04 | -0.01 | 240. |
| 245. | -0.25 | -0.24 | -0.17 | -0.12 | -0.08 | -0.04 | -0.01 | 245. |
| 250. | -0.27 | -0.24 | -0.17 | -0.11 | -0.09 | -0.04 | -0.02 | 250. |
| 255. | -0.30 | -0.24 | -0.16 | -0.10 | -0.10 | -0.05 | -0.02 | 255. |
| 260. | -0.32 | -0.23 | -0.16 | -0.11 | -0.10 | -0.05 | -0.02 | 260. |
| 265. | -0.29 | -0.22 | -0.15 | -0.11 | -0.10 | -0.04 | -0.02 | 265. |
| 270. | -0.25 | -0.21 | -0.13 | -0.11 | -0.09 | -0.04 | -0.01 | 270. |
| 275. | -0.23 | -0.20 | -0.11 | -0.10 | -0.08 | -0.03 | -0.01 | 275. |
| 280. | -0.25 | -0.18 | -0.10 | -0.09 | -0.08 | -0.03 | -0.01 | 280. |
| 285. | -0.28 | -0.16 | -0.10 | -0.08 | -0.08 | -0.03 | -0.01 | 285. |
| 290. | -0.28 | -0.15 | -0.09 | -0.08 | -0.08 | -0.03 | -0.00 | 290. |
| 295. | -0.25 | -0.14 | -0.08 | -0.07 | -0.08 | -0.03 | -0.01 | 295. |
| 300. | -0.21 | -0.14 | -0.07 | -0.07 | -0.08 | -0.03 | -0.01 | 300. |
| 305. | -0.18 | -0.12 | -0.06 | -0.06 | -0.07 | -0.03 | -0.01 | 305. |
| 310. | -0.16 | -0.08 | -0.05 | -0.04 | -0.06 | -0.03 | -0.01 | 310. |
| 315. | -0.13 | -0.03 | -0.03 | -0.03 | -0.05 | -0.02 | -0.00 | 315. |
| 320. | -0.10 | -0.01 | -0.02 | -0.02 | -0.03 | -0.01 | -0.00 | 320. |
| 325. | -0.07 | -0.00 | -0.01 | -0.01 | -0.02 | -0.00 | -0.00 | 325. |
| 330. | -0.04 | -0.01 | -0.01 | 0.00 | -0.01 | 0.00 | -0.00 | 330. |
| 335. | -0.04 | -0.02 | -0.01 | 0.01 | -0.04 | 0.00 | -0.00 | 335. |
| 340. | -0.05 | -0.05 | -0.02 | 0.00 | -0.05 | -0.01 | -0.00 | 340. |
| 345. | -0.06 | -0.07 | -0.03 | -0.02 | -0.05 | -0.01 | -0.01 | 345. |
| 350. | -0.07 | -0.06 | -0.07 | -0.03 | -0.04 | -0.01 | -0.01 | 350. |
| 355. | -0.04 | 0.01 | -0.04 | -0.02 | 0.00 | 0.01 | 0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 563 TC№ 4. C.R.= 37.0

DIFFERENTIAL PRESSURES

SPAN STATION 193.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.52 | 0.27 | 0.22 | 0.14 | 0.12 | 0.09 | 0.03 | 0. |
| 5. | 0.60 | 0.37 | 0.32 | 0.19 | 0.16 | 0.13 | 0.04 | 5. |
| 10. | 0.80 | 0.47 | 0.40 | 0.24 | 0.18 | 0.11 | 0.04 | 10. |
| 15. | 0.86 | 0.53 | 0.42 | 0.27 | 0.20 | 0.10 | 0.04 | 15. |
| 20. | 0.89 | 0.56 | 0.42 | 0.27 | 0.21 | 0.09 | 0.04 | 20. |
| 25. | 0.86 | 0.54 | 0.40 | 0.26 | 0.20 | 0.10 | 0.03 | 25. |
| 30. | 0.78 | 0.47 | 0.39 | 0.25 | 0.19 | 0.10 | 0.03 | 30. |
| 35. | 0.70 | 0.42 | 0.37 | 0.25 | 0.18 | 0.09 | 0.03 | 35. |
| 40. | 0.64 | 0.42 | 0.35 | 0.24 | 0.16 | 0.07 | 0.02 | 40. |
| 45. | 0.58 | 0.39 | 0.33 | 0.24 | 0.15 | 0.06 | 0.02 | 45. |
| 50. | 0.56 | 0.37 | 0.30 | 0.23 | 0.15 | 0.06 | 0.03 | 50. |
| 55. | 0.56 | 0.35 | 0.29 | 0.24 | 0.15 | 0.06 | 0.03 | 55. |
| 60. | 0.55 | 0.36 | 0.27 | 0.24 | 0.16 | 0.06 | 0.03 | 60. |
| 65. | 0.52 | 0.37 | 0.25 | 0.24 | 0.15 | 0.05 | 0.03 | 65. |
| 70. | 0.46 | 0.36 | 0.23 | 0.22 | 0.14 | 0.05 | 0.03 | 70. |
| 75. | 0.39 | 0.32 | 0.22 | 0.18 | 0.13 | 0.04 | 0.03 | 75. |
| 80. | 0.36 | 0.27 | 0.22 | 0.13 | 0.11 | 0.03 | 0.02 | 80. |
| 85. | 0.33 | 0.26 | 0.19 | 0.11 | 0.10 | 0.02 | 0.02 | 85. |
| 90. | 0.30 | 0.27 | 0.17 | 0.10 | 0.09 | 0.02 | 0.01 | 90. |
| 95. | 0.27 | 0.27 | 0.16 | 0.10 | 0.08 | 0.01 | 0.01 | 95. |
| 100. | 0.23 | 0.25 | 0.15 | 0.10 | 0.07 | 0.01 | 0.00 | 100. |
| 105. | 0.24 | 0.23 | 0.15 | 0.10 | 0.06 | 0.00 | -0.00 | 105. |
| 110. | 0.24 | 0.22 | 0.14 | 0.10 | 0.05 | -0.00 | -0.01 | 110. |
| 115. | 0.24 | 0.21 | 0.13 | 0.09 | 0.03 | -0.01 | -0.01 | 115. |
| 120. | 0.12 | 0.17 | 0.11 | 0.08 | 0.02 | -0.02 | -0.01 | 120. |
| 125. | -0.04 | 0.08 | 0.05 | 0.03 | 0.00 | -0.04 | -0.01 | 125. |
| 130. | -0.20 | -0.02 | -0.03 | -0.04 | -0.03 | -0.05 | -0.02 | 130. |
| 135. | -0.34 | -0.13 | -0.11 | -0.10 | -0.06 | -0.06 | -0.01 | 135. |
| 140. | -0.44 | -0.22 | -0.16 | -0.13 | -0.09 | -0.06 | -0.01 | 140. |
| 145. | -0.45 | -0.22 | -0.19 | -0.12 | -0.11 | -0.07 | -0.01 | 145. |
| 150. | -0.36 | -0.14 | -0.10 | -0.09 | -0.08 | -0.06 | -0.01 | 150. |
| 155. | -0.29 | -0.08 | -0.06 | -0.06 | -0.06 | -0.06 | -0.01 | 155. |
| 160. | -0.37 | -0.14 | -0.16 | -0.08 | -0.06 | -0.05 | -0.02 | 160. |
| 165. | -0.46 | -0.22 | -0.18 | -0.10 | -0.09 | -0.06 | -0.02 | 165. |
| 170. | -0.51 | -0.28 | -0.22 | -0.13 | -0.11 | -0.07 | -0.03 | 170. |
| 175. | -0.56 | -0.30 | -0.25 | -0.15 | -0.12 | -0.07 | -0.02 | 175. |
| 180. | -0.58 | -0.31 | -0.28 | -0.16 | -0.12 | -0.07 | -0.02 | 180. |
| 185. | -0.61 | -0.34 | -0.30 | -0.17 | -0.13 | -0.07 | -0.02 | 185. |
| 190. | -0.62 | -0.36 | -0.32 | -0.18 | -0.13 | -0.07 | -0.02 | 190. |
| 195. | -0.64 | -0.38 | -0.34 | -0.19 | -0.14 | -0.08 | -0.03 | 195. |
| 200. | -0.64 | -0.38 | -0.34 | -0.20 | -0.15 | -0.08 | -0.03 | 200. |
| 205. | -0.66 | -0.37 | -0.33 | -0.21 | -0.15 | -0.08 | -0.03 | 205. |
| 210. | -0.66 | -0.38 | -0.32 | -0.21 | -0.15 | -0.08 | -0.03 | 210. |
| 215. | -0.71 | -0.43 | -0.31 | -0.22 | -0.16 | -0.07 | -0.03 | 215. |
| 220. | -0.68 | -0.46 | -0.29 | -0.22 | -0.17 | -0.07 | -0.03 | 220. |
| 225. | -0.63 | -0.41 | -0.27 | -0.22 | -0.16 | -0.06 | -0.02 | 225. |
| 230. | -0.58 | -0.35 | -0.25 | -0.21 | -0.15 | -0.06 | -0.02 | 230. |
| 235. | -0.47 | -0.30 | -0.22 | -0.19 | -0.12 | -0.05 | -0.03 | 235. |
| 240. | -0.36 | -0.28 | -0.20 | -0.16 | -0.10 | -0.04 | -0.03 | 240. |
| 245. | -0.30 | -0.27 | -0.19 | -0.14 | -0.09 | -0.03 | -0.02 | 245. |
| 250. | -0.28 | -0.26 | -0.17 | -0.13 | -0.08 | -0.02 | -0.02 | 250. |
| 255. | -0.29 | -0.26 | -0.15 | -0.12 | -0.08 | -0.02 | -0.02 | 255. |
| 260. | -0.30 | -0.26 | -0.15 | -0.12 | -0.09 | -0.01 | -0.01 | 260. |
| 265. | -0.31 | -0.26 | -0.16 | -0.11 | -0.09 | -0.01 | -0.01 | 265. |
| 270. | -0.32 | -0.26 | -0.17 | -0.11 | -0.09 | -0.02 | -0.01 | 270. |
| 275. | -0.30 | -0.24 | -0.17 | -0.11 | -0.09 | -0.02 | -0.01 | 275. |
| 280. | -0.21 | -0.20 | -0.13 | -0.10 | -0.07 | -0.02 | -0.01 | 280. |
| 285. | -0.10 | -0.13 | -0.09 | -0.09 | -0.06 | -0.01 | -0.01 | 285. |
| 290. | -0.10 | -0.11 | -0.07 | -0.08 | -0.03 | 0.00 | -0.00 | 290. |
| 295. | -0.13 | -0.13 | -0.08 | -0.07 | -0.02 | 0.01 | 0.00 | 295. |
| 300. | -0.12 | -0.14 | -0.10 | -0.06 | -0.02 | 0.01 | 0.00 | 300. |
| 305. | -0.10 | -0.12 | -0.10 | -0.06 | -0.02 | 0.02 | 0.00 | 305. |
| 310. | -0.05 | -0.09 | -0.06 | -0.05 | -0.01 | 0.02 | 0.00 | 310. |
| 315. | 0.03 | -0.05 | -0.03 | -0.04 | -0.00 | 0.02 | 0.00 | 315. |
| 320. | 0.13 | -0.01 | 0.04 | -0.01 | 0.01 | 0.03 | 0.00 | 320. |
| 325. | 0.23 | 0.02 | 0.06 | 0.02 | 0.02 | 0.03 | 0.00 | 325. |
| 330. | 0.26 | 0.05 | 0.07 | 0.04 | 0.02 | 0.03 | 0.00 | 330. |
| 335. | 0.26 | 0.06 | 0.06 | 0.04 | 0.02 | 0.03 | 0.01 | 335. |
| 340. | 0.25 | 0.05 | 0.05 | 0.03 | 0.02 | 0.04 | 0.01 | 340. |
| 345. | 0.25 | 0.05 | 0.06 | 0.03 | 0.02 | 0.04 | 0.01 | 345. |
| 350. | 0.49 | 0.10 | 0.10 | 0.05 | 0.03 | 0.04 | 0.02 | 350. |
| 355. | 0.50 | 0.17 | 0.15 | 0.08 | 0.06 | 0.06 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 563 TCN= 4. C.R.= 37.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.455 | 1.240 | 1.950 | 2.990 | 4.550 | 7.159 | 10.400 | DEG. |
| 0. | 0.58 | 0.44 | 0.31 | 0.18 | 0.15 | 0.09 | 0.03 | 0. |
| 5. | 0.72 | 0.55 | 0.37 | 0.25 | 0.19 | 0.13 | 0.04 | 5. |
| 10. | 0.77 | 0.62 | 0.42 | 0.30 | 0.22 | 0.13 | 0.05 | 10. |
| 15. | 0.71 | 0.61 | 0.40 | 0.30 | 0.21 | 0.11 | 0.04 | 15. |
| 20. | 0.61 | 0.58 | 0.35 | 0.28 | 0.18 | 0.09 | 0.03 | 20. |
| 25. | 0.59 | 0.56 | 0.32 | 0.24 | 0.17 | 0.07 | 0.03 | 25. |
| 30. | 0.62 | 0.54 | 0.32 | 0.24 | 0.17 | 0.07 | 0.03 | 30. |
| 35. | 0.65 | 0.53 | 0.32 | 0.23 | 0.17 | 0.07 | 0.02 | 35. |
| 40. | 0.65 | 0.52 | 0.32 | 0.22 | 0.16 | 0.07 | 0.02 | 40. |
| 45. | 0.63 | 0.50 | 0.31 | 0.21 | 0.16 | 0.07 | 0.01 | 45. |
| 50. | 0.59 | 0.49 | 0.29 | 0.19 | 0.14 | 0.06 | 0.01 | 50. |
| 55. | 0.54 | 0.46 | 0.26 | 0.16 | 0.12 | 0.05 | 0.01 | 55. |
| 60. | 0.46 | 0.42 | 0.23 | 0.13 | 0.10 | 0.04 | 0.01 | 60. |
| 65. | 0.38 | 0.34 | 0.18 | 0.11 | 0.07 | 0.03 | 0.01 | 65. |
| 70. | 0.30 | 0.25 | 0.14 | 0.08 | 0.05 | 0.03 | 0.01 | 70. |
| 75. | 0.22 | 0.17 | 0.10 | 0.06 | 0.03 | 0.02 | 0.00 | 75. |
| 80. | 0.14 | 0.12 | 0.07 | 0.05 | 0.02 | 0.01 | 0.00 | 80. |
| 85. | 0.09 | 0.09 | 0.04 | 0.03 | 0.01 | 0.01 | -0.00 | 85. |
| 90. | 0.08 | 0.06 | 0.03 | 0.03 | 0.01 | 0.00 | -0.00 | 90. |
| 95. | 0.09 | 0.04 | 0.03 | 0.02 | 0.01 | 0.00 | -0.00 | 95. |
| 100. | 0.10 | 0.01 | 0.03 | 0.02 | 0.01 | 0.00 | -0.00 | 100. |
| 105. | 0.10 | -0.02 | 0.02 | 0.01 | 0.01 | 0.00 | -0.01 | 105. |
| 110. | 0.08 | -0.05 | -0.01 | -0.00 | -0.01 | -0.01 | -0.01 | 110. |
| 115. | 0.02 | -0.08 | -0.04 | -0.02 | -0.03 | -0.02 | -0.01 | 115. |
| 120. | -0.04 | -0.11 | -0.08 | -0.05 | -0.05 | -0.03 | -0.02 | 120. |
| 125. | -0.10 | -0.17 | -0.12 | -0.09 | -0.08 | -0.04 | -0.02 | 125. |
| 130. | -0.29 | -0.24 | -0.16 | -0.12 | -0.11 | -0.05 | -0.03 | 130. |
| 135. | -0.41 | -0.33 | -0.20 | -0.15 | -0.15 | -0.07 | -0.03 | 135. |
| 140. | -0.58 | -0.44 | -0.23 | -0.17 | -0.18 | -0.09 | -0.03 | 140. |
| 145. | -0.67 | -0.53 | -0.29 | -0.18 | -0.19 | -0.10 | -0.03 | 145. |
| 150. | -0.64 | -0.58 | -0.35 | -0.19 | -0.19 | -0.10 | -0.03 | 150. |
| 155. | -0.53 | -0.38 | -0.29 | -0.19 | -0.11 | -0.08 | -0.02 | 155. |
| 160. | -0.36 | -0.32 | -0.22 | -0.18 | -0.09 | -0.06 | -0.01 | 160. |
| 165. | -0.33 | -0.32 | -0.19 | -0.16 | -0.10 | -0.06 | -0.01 | 165. |
| 170. | -0.39 | -0.33 | -0.21 | -0.15 | -0.11 | -0.06 | -0.02 | 170. |
| 175. | -0.41 | -0.32 | -0.23 | -0.13 | -0.12 | -0.06 | -0.02 | 175. |
| 180. | -0.38 | -0.31 | -0.22 | -0.13 | -0.10 | -0.04 | -0.02 | 180. |
| 185. | -0.40 | -0.33 | -0.21 | -0.14 | -0.10 | -0.06 | -0.02 | 185. |
| 190. | -0.47 | -0.37 | -0.23 | -0.15 | -0.11 | -0.06 | -0.02 | 190. |
| 195. | -0.51 | -0.40 | -0.25 | -0.17 | -0.12 | -0.06 | -0.02 | 195. |
| 200. | -0.46 | -0.42 | -0.25 | -0.18 | -0.11 | -0.06 | -0.02 | 200. |
| 205. | -0.44 | -0.40 | -0.24 | -0.16 | -0.10 | -0.06 | -0.02 | 205. |
| 210. | -0.41 | -0.30 | -0.22 | -0.12 | -0.08 | -0.06 | -0.02 | 210. |
| 215 | -0.28 | -0.18 | -0.15 | -0.11 | -0.06 | -0.05 | -0.02 | 215. |
| 220 | -0.29 | -0.22 | -0.15 | -0.11 | -0.06 | -0.04 | -0.01 | 220. |
| 225 | -0.46 | -0.34 | -0.23 | -0.12 | -0.12 | -0.04 | -0.01 | 225. |
| 230. | -0.56 | -0.39 | -0.27 | -0.12 | -0.13 | -0.04 | -0.00 | 230. |
| 235. | -0.39 | -0.34 | -0.22 | -0.12 | -0.11 | -0.04 | 0.02 | 235. |
| 240. | -0.28 | -0.29 | -0.16 | -0.12 | -0.09 | -0.03 | 0.00 | 240. |
| 245. | -0.27 | -0.26 | -0.16 | -0.10 | -0.06 | -0.02 | 0.01 | 245. |
| 250. | -0.20 | -0.23 | -0.12 | -0.08 | -0.04 | -0.01 | 0.01 | 250. |
| 255. | -0.25 | -0.18 | -0.09 | -0.07 | -0.03 | -0.00 | 0.01 | 255. |
| 260. | -0.21 | -0.13 | -0.06 | -0.06 | -0.02 | -0.00 | 0.01 | 260. |
| 265. | -0.19 | -0.14 | -0.06 | -0.07 | -0.02 | -0.00 | 0.01 | 265. |
| 270. | -0.21 | -0.16 | -0.07 | -0.08 | -0.03 | -0.01 | 0.00 | 270. |
| 275. | -0.23 | -0.17 | -0.07 | -0.06 | -0.04 | -0.01 | 0.00 | 275. |
| 280. | -0.23 | -0.16 | -0.08 | -0.04 | -0.04 | -0.02 | -0.00 | 280. |
| 285. | -0.28 | -0.13 | -0.06 | -0.01 | -0.04 | -0.01 | -0.00 | 285. |
| 290. | -0.10 | -0.06 | -0.01 | 0.02 | -0.03 | -0.00 | 0.03 | 290. |
| 295. | -0.00 | 0.02 | 0.04 | 0.03 | 0.00 | 0.01 | 0.00 | 295. |
| 300. | 0.08 | 0.07 | 0.08 | 0.03 | 0.05 | 0.03 | 0.01 | 300. |
| 305. | 0.11 | 0.10 | 0.09 | 0.04 | 0.06 | 0.03 | 0.01 | 305. |
| 310. | 0.09 | 0.10 | 0.08 | 0.04 | 0.05 | 0.03 | 0.01 | 310. |
| 315. | 0.09 | 0.09 | 0.08 | 0.04 | 0.04 | 0.03 | 0.01 | 315. |
| 320. | 0.14 | 0.10 | 0.08 | 0.05 | 0.05 | 0.02 | 0.00 | 320. |
| 325. | 0.23 | 0.15 | 0.10 | 0.06 | 0.05 | 0.02 | -0.00 | 325. |
| 330. | 0.30 | 0.20 | 0.12 | 0.07 | 0.05 | 0.03 | -0.01 | 330. |
| 335. | 0.32 | 0.22 | 0.13 | 0.06 | 0.05 | 0.03 | -0.01 | 335. |
| 340. | 0.31 | 0.24 | 0.14 | 0.06 | 0.05 | 0.03 | -0.00 | 340. |
| 345. | 0.31 | 0.25 | 0.15 | 0.06 | 0.07 | 0.04 | 0.00 | 345. |
| 350. | 0.29 | 0.27 | 0.18 | 0.08 | 0.09 | 0.05 | 0.01 | 350. |
| 355. | 0.37 | 0.34 | 0.24 | 0.12 | 0.12 | 0.07 | 0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 563 TCN= 4. C.R.= 37.0

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ DEG. | CHORD STATION 0.455 | 1.040 | 1.959 | 2.990 | 4.550 | 7.150 | 10.400 | AZ DEG. |
|---|---|---|---|---|---|---|---|---|
| 0. | 0.39 | 0.29 | 0.23 | 0.16 | 0.07 | 0.05 | 0.03 | 0. |
| 5. | 0.46 | 0.41 | 0.39 | 0.30 | 0.18 | 0.08 | 0.05 | 5. |
| 10. | 0.47 | 0.48 | 0.41 | 0.31 | 0.19 | 0.08 | 0.04 | 10. |
| 15. | 0.44 | 0.39 | 0.33 | 0.24 | 0.13 | 0.06 | 0.03 | 15. |
| 20. | 0.39 | 0.27 | 0.23 | 0.17 | 0.12 | 0.03 | 0.02 | 20. |
| 25. | 0.32 | 0.23 | 0.21 | 0.16 | 0.12 | 0.03 | 0.02 | 25. |
| 30. | 0.29 | 0.24 | 0.19 | 0.16 | 0.14 | 0.03 | 0.02 | 30. |
| 35. | 0.33 | 0.26 | 0.18 | 0.16 | 0.15 | 0.03 | 0.02 | 35. |
| 40. | 0.36 | 0.26 | 0.19 | 0.14 | 0.17 | 0.03 | 0.01 | 40. |
| 45. | 0.36 | 0.25 | 0.19 | 0.12 | 0.14 | 0.03 | 0.01 | 45. |
| 50. | 0.31 | 0.23 | 0.19 | 0.09 | 0.18 | 0.02 | 0.01 | 50. |
| 55. | 0.17 | 0.18 | 0.18 | 0.06 | 0.16 | 0.01 | 0.00 | 55. |
| 60. | 0.04 | 0.09 | 0.15 | 0.03 | 0.15 | -0.00 | -0.00 | 60. |
| 65. | -0.06 | 0.00 | 0.11 | 0.00 | 0.14 | -0.02 | -0.00 | 65. |
| 70. | -0.14 | -0.09 | 0.06 | -0.03 | 0.13 | -0.03 | -0.01 | 70. |
| 75. | -0.27 | -0.17 | 0.02 | -0.05 | 0.11 | -0.04 | -0.01 | 75. |
| 80. | -0.35 | -0.23 | -0.02 | -0.07 | 0.10 | -0.05 | -0.01 | 80. |
| 85. | -0.39 | -0.25 | -0.07 | -0.08 | 0.09 | -0.05 | -0.01 | 85. |
| 90. | -0.39 | -0.24 | -0.10 | -0.09 | 0.07 | -0.04 | -0.01 | 90. |
| 95. | -0.40 | -0.21 | -0.13 | -0.09 | 0.05 | -0.03 | -0.01 | 95. |
| 100. | -0.40 | -0.18 | -0.14 | -0.10 | 0.04 | -0.03 | -0.01 | 100. |
| 105. | -0.40 | -0.18 | -0.15 | -0.10 | 0.02 | -0.03 | -0.01 | 105. |
| 110. | -0.40 | -0.19 | -0.16 | -0.17 | -0.00 | -0.04 | -0.02 | 110. |
| 115. | -0.42 | -0.21 | -0.18 | -0.12 | -0.32 | -0.05 | -0.02 | 115. |
| 120. | -0.49 | -0.25 | -0.20 | -0.17 | -0.04 | -0.05 | -0.03 | 120. |
| 125. | -0.57 | -0.31 | -0.23 | -0.17 | -0.07 | -0.06 | -0.03 | 125. |
| 130. | -0.56 | -0.41 | -0.27 | -0.17 | -0.09 | -0.06 | -0.03 | 130. |
| 135. | -0.74 | -0.52 | -0.34 | -0.22 | -0.13 | -0.07 | -0.04 | 135. |
| 140. | -0.97 | -0.62 | -0.41 | -0.29 | -0.17 | -0.07 | -0.04 | 140. |
| 145. | -1.03 | -0.66 | -0.48 | -0.33 | -0.18 | -0.07 | -0.04 | 145. |
| 150. | -1.05 | -0.57 | -0.47 | -0.32 | -0.15 | -0.06 | -0.03 | 150. |
| 155. | -0.46 | -0.42 | -0.29 | -0.21 | -0.09 | -0.06 | -0.02 | 155. |
| 160. | -0.38 | -0.28 | -0.10 | -0.10 | -0.04 | -0.05 | -0.02 | 160. |
| 165. | -0.29 | -0.19 | -0.05 | -0.09 | -0.02 | -0.04 | -0.02 | 165. |
| 170. | -0.78 | -0.15 | -0.07 | -0.10 | -0.00 | -0.03 | -0.02 | 170. |
| 175. | -0.27 | -0.13 | -0.10 | -0.10 | -0.01 | -0.04 | -0.02 | 175. |
| 180. | -0.11 | -0.11 | -0.08 | -0.09 | -0.02 | -0.03 | -0.02 | 180. |
| 185. | -0.11 | -0.13 | -0.10 | -0.08 | -0.04 | -0.03 | -0.02 | 185. |
| 190. | -0.33 | -0.22 | -0.14 | -0.08 | -0.04 | -0.03 | -0.02 | 190. |
| 195. | -0.13 | -0.07 | -0.12 | -0.08 | -0.04 | -0.02 | -0.01 | 195. |
| 200. | 0.18 | 0.09 | -0.03 | -0.07 | -0.01 | -0.01 | -0.01 | 200. |
| 205. | 0.03 | -0.00 | -0.05 | -0.03 | -0.01 | -0.02 | -0.01 | 205. |
| 210. | 0.09 | 0.09 | 0.02 | 0.05 | 0.00 | 0.02 | -0.01 | 210. |
| 215. | 0.45 | 0.30 | 0.18 | 0.15 | 0.04 | 0.04 | -0.00 | 215. |
| 220. | 0.38 | 0.22 | 0.15 | 0.12 | 0.06 | 0.03 | 0.00 | 220. |
| 225. | 0.12 | -0.01 | 0.02 | -0.00 | 0.03 | 0.02 | 0.00 | 225. |
| 230. | 0.03 | -0.05 | -0.01 | -0.04 | -0.01 | 0.02 | 0.00 | 230. |
| 235. | 0.12 | 0.02 | 0.01 | 0.00 | -0.02 | 0.02 | 0.00 | 235. |
| 240. | 0.33 | 0.17 | 0.08 | 0.07 | -0.02 | 0.02 | 0.00 | 240. |
| 245. | 0.48 | 0.30 | 0.15 | 0.12 | -0.01 | 0.03 | 0.01 | 245. |
| 250. | 0.57 | 0.37 | 0.20 | 0.13 | 0.03 | 0.03 | 0.01 | 250. |
| 255. | 0.00 | 0.41 | 0.23 | 0.13 | 0.05 | 0.04 | 0.01 | 255. |
| 260. | 0.77 | 0.38 | 0.21 | 0.13 | 0.05 | 0.04 | 0.01 | 260. |
| 265. | 0.60 | 0.28 | 0.13 | 0.12 | 0.04 | 0.03 | 0.01 | 265. |
| 270. | 0.28 | 0.11 | 0.05 | 0.04 | -0.02 | 0.01 | 0.00 | 270. |
| 275. | 0.06 | -0.05 | -0.03 | -0.02 | -0.00 | -0.01 | -0.00 | 275. |
| 280. | 0.05 | -0.01 | -0.02 | 0.01 | -0.00 | 0.01 | 0.01 | 280. |
| 285. | 0.11 | 0.10 | 0.07 | 0.00 | -0.06 | 0.03 | 0.01 | 285. |
| 290. | 0.15 | 0.09 | 0.08 | 0.00 | -0.05 | 0.03 | 0.01 | 290. |
| 295. | 0.19 | 0.00 | 0.06 | 0.00 | -0.07 | 0.05 | 0.01 | 295. |
| 300. | 0.28 | 0.09 | 0.01 | 0.00 | -0.00 | 0.06 | 0.02 | 300. |
| 305. | 0.24 | 0.07 | -0.02 | 0.05 | -0.11 | 0.03 | 0.02 | 305. |
| 310. | 0.15 | 0.03 | -0.00 | 0.02 | -0.12 | 0.03 | 0.02 | 310. |
| 315. | 0.06 | -0.01 | -0.04 | 0.02 | -0.13 | 0.03 | 0.02 | 315. |
| 320. | 0.05 | -0.00 | -0.04 | 0.04 | -0.13 | 0.03 | 0.01 | 320. |
| 325. | 0.09 | 0.03 | -0.06 | 0.03 | -0.13 | 0.02 | 0.01 | 325. |
| 330. | 0.12 | 0.04 | -0.07 | 0.01 | -0.13 | 0.02 | 0.01 | 330. |
| 335. | 0.14 | 0.04 | -0.07 | -0.01 | -0.13 | 0.02 | 0.01 | 335. |
| 340. | 0.09 | 0.06 | -0.06 | -0.01 | -0.13 | 0.01 | 0.01 | 340. |
| 345. | -0.01 | -0.02 | -0.04 | -0.01 | -0.13 | 0.01 | 0.01 | 345. |
| 350. | -0.02 | 0.02 | 0.00 | 0.01 | -0.11 | 0.00 | 0.02 | 350. |
| 355. | 0.15 | 0.15 | 0.09 | 0.05 | -0.07 | 0.02 | 0.03 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-498 CNTR NO. 563 TCN= 4. C.R.= 37.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.655 | 1.340 | 1.950 | 2.990 | 4.550 | 7.139 | 10.400 | DEG. |
| 0. | -0.73 | -0.16 | -0.09 | -0.08 | -0.05 | -0.00 | 0.02 | 0. |
| 5. | -0.17 | 0.21 | 0.10 | 0.08 | 0.07 | 0.02 | 0.02 | 5. |
| 10. | -0.29 | 0.17 | 0.01 | 0.09 | 0.10 | 0.02 | 0.02 | 10. |
| 15. | -0.59 | -0.05 | -0.04 | 0.02 | 0.09 | 0.00 | 0.01 | 15. |
| 20. | -0.69 | -0.10 | -0.09 | -0.06 | 0.03 | -0.01 | 0.02 | 20. |
| 25. | -0.75 | -0.12 | -0.09 | -0.07 | 0.01 | -0.00 | -0.01 | 25. |
| 30. | -0.73 | -0.10 | -0.08 | -0.06 | 0.00 | 0.00 | -0.01 | 30. |
| 35. | -0.66 | -0.06 | -0.06 | -0.05 | -0.01 | -0.01 | -0.02 | 35. |
| 40. | -0.57 | -0.03 | -0.04 | -0.03 | -0.02 | -0.01 | -0.02 | 40. |
| 45. | -0.48 | -0.02 | -0.07 | -0.01 | -0.04 | -0.02 | -0.03 | 45. |
| 50. | -0.52 | -0.04 | -0.11 | -0.00 | -0.05 | -0.04 | -0.03 | 50. |
| 55. | -0.73 | -0.10 | -0.15 | -0.04 | -0.07 | -0.05 | -0.03 | 55. |
| 60. | -0.94 | -0.17 | -0.21 | -0.12 | -0.08 | -0.04 | -0.03 | 60. |
| 65. | -1.03 | -0.25 | -0.26 | -0.18 | -0.10 | -0.06 | -0.03 | 65. |
| 70. | -1.09 | -0.31 | -0.29 | -0.18 | -0.11 | -0.07 | -0.03 | 70. |
| 75. | -1.22 | -0.36 | -0.31 | -0.19 | -0.11 | -0.07 | -0.04 | 75. |
| 80. | -1.36 | -0.41 | -0.34 | -0.23 | -0.12 | -0.08 | -0.04 | 80. |
| 85. | -1.33 | -0.43 | -0.35 | -0.24 | -0.12 | -0.06 | -0.04 | 85. |
| 90. | -1.07 | -0.37 | -0.33 | -0.22 | -0.11 | -0.06 | -0.03 | 90. |
| 95. | -0.83 | -0.26 | -0.24 | -0.18 | -0.10 | -0.06 | -0.03 | 95. |
| 100. | -0.93 | -0.23 | -0.19 | -0.16 | -0.08 | -0.07 | -0.04 | 100. |
| 105. | 1.08 | -0.26 | -0.20 | -0.14 | -0.06 | -0.07 | -0.04 | 105. |
| 110. | -1.24 | -0.31 | -0.22 | -0.14 | -0.06 | -0.07 | -0.04 | 110. |
| 115. | -0.94 | -0.28 | -0.21 | -0.14 | -0.06 | -0.07 | -0.04 | 115. |
| 120. | -0.86 | -0.24 | -0.23 | -0.14 | -0.06 | -0.07 | -0.05 | 120. |
| 125. | -0.89 | -0.21 | -0.20 | -0.15 | -0.07 | -0.08 | -0.05 | 125. |
| 130. | -0.98 | -0.22 | -0.27 | -0.18 | -0.08 | -0.09 | -0.05 | 130. |
| 135. | -1.18 | -0.34 | -0.33 | -0.23 | -0.09 | -0.10 | -0.05 | 135. |
| 140. | -1.30 | -0.42 | -0.35 | -0.25 | -0.11 | -0.11 | -0.05 | 140. |
| 145. | -1.25 | -0.38 | -0.31 | -0.18 | -0.11 | -0.08 | -0.04 | 145. |
| 150. | -0.96 | -0.23 | -0.19 | -0.09 | -0.10 | -0.05 | -0.03 | 150. |
| 155. | -0.91 | -0.11 | -0.02 | -0.05 | -0.08 | -0.01 | -0.03 | 155. |
| 160. | -0.38 | 0.02 | 0.03 | -0.02 | -0.04 | -0.01 | -0.02 | 160. |
| 165. | -0.24 | 0.11 | 0.02 | 0.05 | -0.01 | -0.03 | -0.02 | 165. |
| 170. | 0.10 | 0.15 | 0.07 | 0.06 | 0.01 | -0.00 | -0.01 | 170. |
| 175. | -0.10 | 0.15 | 0.04 | 0.04 | 0.03 | 0.01 | -0.01 | 175. |
| 180. | -0.10 | 0.06 | 0.02 | -0.00 | 0.03 | -0.01 | -0.01 | 180. |
| 185. | -0.38 | -0.06 | -0.05 | -0.04 | 0.01 | -0.01 | -0.01 | 185. |
| 190. | -0.79 | -0.08 | -0.15 | -0.06 | -0.02 | 0.03 | -0.01 | 190. |
| 195. | -0.81 | -0.03 | -0.01 | -0.05 | -0.02 | 0.01 | -0.00 | 195. |
| 200. | -0.53 | 0.04 | 0.10 | 0.04 | 0.01 | -0.00 | 0.01 | 200. |
| 205. | 0.03 | 0.09 | -0.02 | 0.05 | 0.05 | 0.01 | 0.01 | 205. |
| 210. | 0.97 | 0.20 | 0.20 | 0.11 | 0.09 | 0.04 | 0.03 | 210. |
| 215. | 2.13 | 0.42 | 0.47 | 0.32 | 0.12 | 0.09 | 0.05 | 215. |
| 220. | 2.70 | 0.61 | 0.48 | 0.41 | 0.15 | 0.11 | 0.04 | 220. |
| 225. | 2.63 | 0.46 | 0.43 | 0.38 | 0.19 | 0.12 | 0.04 | 225. |
| 230. | 2.45 | 0.48 | 0.40 | 0.31 | 0.20 | 0.12 | 0.05 | 230. |
| 235. | 2.46 | 0.50 | 0.44 | 0.29 | 0.21 | 0.12 | 0.05 | 235. |
| 240. | 2.54 | 0.50 | 0.52 | 0.32 | 0.21 | 0.13 | 0.06 | 240. |
| 245. | 2.64 | 0.49 | 0.57 | 0.35 | 0.21 | 0.13 | 0.06 | 245. |
| 250. | 2.63 | 0.48 | 0.59 | 0.37 | 0.21 | 0.13 | 0.04 | 250. |
| 255. | 2.66 | 0.52 | 0.58 | 0.38 | 0.20 | 0.13 | 0.04 | 255. |
| 260. | 2.87 | 0.54 | 0.55 | 0.37 | 0.20 | 0.13 | 0.04 | 260. |
| 265. | 3.11 | 0.44 | 0.49 | 0.35 | 0.19 | 0.11 | 0.05 | 265. |
| 270. | 1.67 | 0.35 | 0.37 | 0.30 | 0.16 | 0.07 | 0.03 | 270. |
| 275. | 0.55 | 0.34 | 0.18 | 0.24 | 0.09 | 0.02 | 0.01 | 275. |
| 280. | 0.84 | 0.36 | 0.16 | 0.19 | 0.05 | 0.04 | 0.02 | 280. |
| 285. | 1.71 | 0.35 | 0.30 | 0.15 | 0.06 | 0.07 | 0.04 | 285. |
| 290. | 1.44 | 0.30 | 0.32 | 0.15 | 0.09 | 0.08 | 0.05 | 290. |
| 295. | 1.67 | 0.35 | 0.25 | 0.14 | 0.07 | 0.07 | 0.05 | 295. |
| 300. | 1.05 | 0.28 | 0.13 | 0.09 | 0.03 | 0.05 | 0.04 | 300. |
| 305. | -0.43 | 0.04 | -0.02 | -0.07 | -0.02 | 0.03 | 0.03 | 305. |
| 310. | -0.65 | -0.13 | -0.08 | -0.12 | -0.05 | 0.01 | 0.02 | 310. |
| 315. | -0.47 | -0.14 | -0.02 | -0.13 | -0.06 | 0.00 | 0.01 | 315. |
| 320. | -0.24 | -0.14 | -0.09 | -0.12 | -0.06 | -0.00 | 0.00 | 320. |
| 325. | -0.45 | -0.16 | -0.15 | -0.14 | -0.06 | -0.01 | -0.00 | 325. |
| 330. | -0.68 | -0.19 | -0.19 | -0.17 | -0.09 | -0.02 | -0.01 | 330. |
| 335. | -0.80 | -0.25 | -0.21 | -0.19 | -0.12 | -0.03 | -0.01 | 335. |
| 340. | -0.92 | -0.33 | -0.25 | -0.20 | -0.15 | -0.04 | -0.01 | 340. |
| 345. | -1.07 | -0.39 | -0.27 | -0.20 | -0.15 | -0.04 | -0.00 | 345. |
| 350. | -1.13 | -0.40 | -0.27 | -0.19 | -0.14 | -0.03 | 0.01 | 350. |
| 355. | -1.03 | -0.36 | -0.27 | -0.16 | -0.12 | -0.02 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 394 TCN= 5. C.P.= 90.1

DIFFERENTIAL PRESSURES

SPAN STATION 92.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.950 | 10.400 | DEG. |
| 0. | 0.13 | 0.08 | 0.12 | -0.00 | 0. |
| 5. | 0.20 | 0.10 | 0.07 | 0.01 | 5. |
| 10. | 0.17 | 0.08 | 0.05 | 0.01 | 10. |
| 15. | 0.19 | 0.08 | 0.05 | 0.00 | 15. |
| 20. | 0.26 | 0.13 | 0.06 | -0.00 | 20. |
| 25. | 0.11 | 0.09 | 0.07 | -0.00 | 25. |
| 30. | 0.00 | 0.03 | 0.07 | -0.00 | 30. |
| 35. | 0.13 | 0.07 | 0.06 | 0.00 | 35. |
| 40. | 0.13 | 0.09 | 0.06 | -0.00 | 40. |
| 45. | 0.06 | 0.05 | 0.05 | -0.01 | 45. |
| 50. | 0.14 | 0.07 | 0.05 | -0.00 | 50. |
| 55. | 0.16 | 0.09 | 0.05 | 0.01 | 55. |
| 60. | 0.21 | 0.09 | 0.05 | 0.01 | 60. |
| 65. | 0.13 | 0.08 | 0.03 | 0.00 | 65. |
| 70. | 0.03 | 0.05 | 0.02 | -0.00 | 70. |
| 75. | 0.13 | 0.05 | 0.04 | -0.00 | 75. |
| 80. | 0.19 | 0.06 | 0.04 | -0.00 | 80. |
| 85. | 0.12 | 0.05 | 0.02 | 0.00 | 85. |
| 90. | -0.05 | 0.01 | -0.01 | 0.00 | 90. |
| 95. | -0.21 | -0.05 | -0.03 | 0.00 | 95. |
| 100. | -0.16 | -0.06 | -0.00 | 0.00 | 100. |
| 105. | 0.13 | 0.02 | 0.04 | 0.01 | 105. |
| 110. | 0.24 | 0.06 | 0.03 | 0.02 | 110. |
| 115. | 0.09 | 0.02 | 0.02 | 0.02 | 115. |
| 120. | -0.02 | -0.02 | 0.01 | 0.01 | 120. |
| 125. | -0.08 | -0.03 | -0.00 | 0.00 | 125. |
| 130. | -0.06 | -0.03 | 0.00 | 0.01 | 130. |
| 135. | 0.04 | 0.00 | 0.02 | 0.02 | 135. |
| 140. | 0.15 | 0.03 | 0.03 | 0.02 | 140. |
| 145. | 0.21 | 0.05 | 0.04 | 0.01 | 145. |
| 150. | 0.17 | 0.07 | 0.03 | 0.00 | 150. |
| 155. | 0.15 | 0.09 | 0.03 | 0.01 | 155. |
| 160. | 0.17 | 0.05 | 0.03 | 0.01 | 160. |
| 165. | 0.20 | 0.08 | 0.04 | 0.01 | 165. |
| 170. | 0.21 | 0.08 | 0.04 | 0.01 | 170. |
| 175. | 0.22 | 0.08 | 0.03 | 0.01 | 175. |
| 180. | 0.20 | 0.08 | 0.03 | 0.00 | 180. |
| 185. | 0.17 | 0.07 | 0.02 | 0.00 | 185. |
| 190. | 0.13 | 0.06 | 0.01 | 0.00 | 190. |
| 195. | 0.09 | 0.04 | 0.01 | 0.01 | 195. |
| 200. | 0.05 | 0.02 | 0.00 | 0.01 | 200. |
| 205. | 0.01 | -0.00 | -0.01 | 0.01 | 205. |
| 210. | -0.03 | -0.02 | -0.01 | 0.01 | 210. |
| 215. | -0.08 | -0.04 | -0.02 | 0.00 | 215. |
| 220. | -0.13 | -0.05 | -0.03 | -0.00 | 220. |
| 225. | -0.18 | -0.07 | -0.04 | -0.01 | 225. |
| 230. | -0.21 | -0.08 | -0.05 | -0.01 | 230. |
| 235. | -0.23 | -0.08 | -0.06 | -0.01 | 235. |
| 240. | -0.25 | -0.09 | -0.07 | -0.01 | 240. |
| 245. | -0.27 | -0.10 | -0.08 | -0.00 | 245. |
| 250. | -0.29 | -0.11 | -0.08 | 0.00 | 250. |
| 255. | -0.30 | -0.12 | -0.09 | 0.00 | 255. |
| 260. | -0.30 | -0.13 | -0.09 | 0.00 | 260. |
| 265. | -0.29 | -0.13 | -0.09 | 0.00 | 265. |
| 270. | -0.28 | -0.13 | -0.09 | 0.00 | 270. |
| 275. | -0.29 | -0.14 | -0.09 | -0.00 | 275. |
| 280. | -0.30 | -0.13 | -0.08 | -0.01 | 280. |
| 285. | -0.30 | -0.13 | -0.08 | -0.01 | 285. |
| 290. | -0.26 | -0.12 | -0.08 | -0.01 | 290. |
| 295. | -0.21 | -0.11 | -0.07 | -0.01 | 295. |
| 300. | -0.17 | -0.10 | -0.06 | -0.01 | 300. |
| 305. | -0.13 | -0.09 | -0.06 | -0.01 | 305. |
| 310. | -0.11 | -0.08 | -0.05 | -0.01 | 310. |
| 315. | -0.10 | -0.07 | -0.04 | -0.01 | 315. |
| 320. | -0.09 | -0.07 | -0.04 | -0.02 | 320. |
| 325. | -0.07 | -0.05 | -0.03 | -0.02 | 325. |
| 330. | -0.04 | -0.03 | -0.02 | -0.02 | 330. |
| 335. | 0.04 | -0.00 | -0.01 | -0.02 | 335. |
| 340. | 0.11 | 0.02 | 0.01 | -0.02 | 340. |
| 345. | 0.13 | 0.04 | 0.02 | -0.01 | 345. |
| 350. | 0.07 | 0.03 | 0.03 | -0.00 | 350. |
| 355. | 0.04 | 0.00 | 0.07 | -0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=532 CNTR NO. 354 TCN= 5. C.R.= 50.1

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.26 | 0.18 | 0.14 | 0.11 | 0.07 | 0.05 | 0.02 | 0. |
| 5. | 0.32 | 0.22 | 0.17 | 0.12 | 0.09 | 0.04 | 0.02 | 5. |
| 10. | 0.32 | 0.24 | 0.17 | 0.13 | 0.08 | 0.05 | 0.01 | 10. |
| 15. | 0.24 | 0.20 | 0.15 | 0.12 | 0.08 | 0.05 | 0.01 | 15. |
| 20. | 0.09 | 0.09 | 0.05 | 0.08 | 0.08 | 0.04 | 0.01 | 20. |
| 25. | 0.05 | 0.12 | 0.07 | 0.08 | 0.11 | 0.04 | 0.01 | 25. |
| 30. | 0.27 | 0.22 | 0.14 | 0.14 | 0.13 | 0.07 | 0.02 | 30. |
| 35. | 0.35 | 0.21 | 0.15 | 0.12 | 0.11 | 0.05 | 0.01 | 35. |
| 40. | 0.29 | 0.19 | 0.10 | 0.07 | 0.07 | 0.03 | -0.00 | 40. |
| 45. | 0.24 | 0.17 | 0.08 | 0.05 | 0.06 | 0.02 | 0.02 | 45. |
| 50. | 0.24 | 0.15 | 0.06 | 0.04 | 0.05 | 0.01 | 0.05 | 50. |
| 55. | 0.23 | 0.12 | 0.04 | 0.04 | 0.05 | 0.00 | 0.05 | 55. |
| 60. | 0.10 | 0.08 | 0.03 | 0.03 | 0.03 | -0.01 | 0.05 | 60. |
| 65. | 0.02 | 0.04 | 0.02 | 0.01 | 0.03 | -0.01 | 0.04 | 65. |
| 70. | 0.14 | 0.09 | 0.03 | 0.03 | 0.08 | 0.03 | 0.06 | 70. |
| 75. | 0.21 | 0.15 | 0.03 | 0.06 | 0.10 | 0.01 | 0.08 | 75. |
| 80. | 0.17 | 0.06 | 0.00 | 0.02 | 0.07 | -0.00 | 0.07 | 80. |
| 85. | -0.09 | -0.08 | -0.07 | -0.06 | 0.04 | -0.02 | 0.05 | 85. |
| 90. | -0.24 | -0.09 | -0.08 | -0.04 | 0.04 | -0.02 | 0.06 | 90. |
| 95. | 0.15 | 0.09 | 0.04 | 0.03 | 0.05 | 0.00 | 0.07 | 95. |
| 100. | 0.09 | 0.05 | -0.01 | 0.01 | 0.05 | -0.01 | 0.04 | 100. |
| 105. | -0.10 | -0.08 | -0.09 | -0.03 | 0.02 | -0.01 | 0.01 | 105. |
| 110. | -0.21 | -0.13 | -0.11 | -0.03 | 0.02 | -0.01 | 0.04 | 110. |
| 115. | -0.00 | 0.01 | -0.01 | -0.01 | 0.03 | -0.03 | 0.05 | 115. |
| 120. | 0.18 | 0.09 | 0.07 | 0.05 | 0.05 | 0.01 | 0.05 | 120. |
| 125. | 0.17 | 0.09 | 0.05 | 0.07 | 0.05 | 0.01 | 0.04 | 125. |
| 130. | 0.05 | 0.03 | 0.02 | 0.04 | 0.05 | 0.01 | 0.04 | 130. |
| 135. | -0.01 | 0.01 | 0.02 | 0.02 | 0.03 | 0.01 | 0.05 | 135. |
| 140. | -0.31 | 0.02 | 0.04 | 0.02 | 0.03 | 0.01 | 0.05 | 140. |
| 145. | 0.02 | 0.05 | 0.06 | 0.03 | 0.04 | 0.02 | 0.04 | 145. |
| 150. | 0.09 | 0.10 | 0.08 | 0.05 | 0.05 | 0.02 | 0.03 | 150. |
| 155. | 0.18 | 0.16 | 0.11 | 0.06 | 0.06 | 0.03 | 0.02 | 155. |
| 160. | 0.31 | 0.23 | 0.15 | 0.08 | 0.06 | 0.02 | 0.02 | 160. |
| 165. | 0.42 | 0.30 | 0.18 | 0.09 | 0.07 | 0.02 | 0.03 | 165. |
| 170. | 0.48 | 0.34 | 0.20 | 0.10 | 0.08 | 0.02 | 0.03 | 170. |
| 175. | 0.47 | 0.34 | 0.20 | 0.10 | 0.09 | 0.02 | 0.01 | 175. |
| 180. | 0.41 | 0.29 | 0.19 | 0.10 | 0.08 | 0.03 | 0.00 | 180. |
| 185. | 0.33 | 0.24 | 0.17 | 0.09 | 0.07 | 0.03 | -0.00 | 185. |
| 190. | 0.25 | 0.19 | 0.14 | 0.07 | 0.05 | 0.03 | -0.01 | 190. |
| 195. | 0.17 | 0.13 | 0.11 | 0.06 | 0.03 | 0.03 | -0.02 | 195. |
| 200. | 0.08 | 0.08 | 0.08 | 0.04 | 0.00 | 0.02 | -0.03 | 200. |
| 205. | 0.01 | 0.03 | 0.04 | 0.02 | -0.02 | 0.01 | -0.03 | 205. |
| 210. | -0.05 | -0.02 | -0.01 | -0.01 | -0.04 | -0.03 | -0.03 | 210. |
| 215. | -0.10 | -0.06 | -0.04 | -0.03 | -0.05 | -0.01 | -0.04 | 215. |
| 220. | -0.14 | -0.09 | -0.06 | -0.04 | -0.07 | -0.02 | -0.05 | 220. |
| 225. | -0.16 | -0.11 | -0.07 | -0.06 | -0.08 | -0.02 | -0.05 | 225. |
| 230. | -0.16 | -0.12 | -0.07 | -0.07 | -0.10 | -0.03 | -0.05 | 230. |
| 235. | -0.16 | -0.12 | -0.08 | -0.07 | -0.11 | -0.03 | -0.05 | 235. |
| 240. | -0.20 | -0.14 | -0.09 | -0.07 | -0.11 | -0.04 | -0.05 | 240. |
| 245. | -0.29 | -0.20 | -0.10 | -0.09 | -0.12 | -0.04 | -0.06 | 245. |
| 250. | -0.37 | -0.26 | -0.13 | -0.13 | -0.12 | -0.04 | -0.06 | 250. |
| 255. | -0.42 | -0.31 | -0.18 | -0.16 | -0.13 | -0.04 | -0.06 | 255. |
| 260. | -0.44 | -0.33 | -0.22 | -0.17 | -0.13 | -0.04 | -0.05 | 260. |
| 265. | -0.45 | -0.34 | -0.23 | -0.16 | -0.13 | -0.04 | -0.05 | 265. |
| 270. | -0.47 | -0.35 | -0.22 | -0.15 | -0.13 | -0.04 | -0.05 | 270. |
| 275. | -0.47 | -0.35 | -0.20 | -0.15 | -0.12 | -0.04 | -0.05 | 275. |
| 280. | -0.45 | -0.34 | -0.19 | -0.13 | -0.11 | -0.04 | -0.05 | 280. |
| 285. | -0.38 | -0.31 | -0.18 | -0.10 | -0.10 | -0.04 | -0.05 | 285. |
| 290. | -0.21 | -0.19 | -0.13 | -0.08 | -0.09 | -0.04 | -0.04 | 290. |
| 295. | -0.07 | -0.07 | -0.08 | -0.07 | -0.09 | -0.05 | -0.04 | 295. |
| 300. | -0.29 | -0.19 | -0.12 | -0.08 | -0.09 | -0.05 | -0.05 | 300. |
| 305. | -0.47 | -0.31 | -0.18 | -0.14 | -0.10 | -0.05 | -0.05 | 305. |
| 310. | -0.52 | -0.35 | -0.20 | -0.17 | -0.11 | -0.06 | -0.05 | 310. |
| 315. | -0.46 | -0.31 | -0.20 | -0.15 | -0.11 | -0.05 | -0.05 | 315. |
| 320. | -0.34 | -0.23 | -0.16 | -0.11 | -0.09 | -0.04 | -0.04 | 320. |
| 325. | -0.18 | -0.16 | -0.12 | -0.07 | -0.07 | -0.03 | -0.03 | 325. |
| 330. | -0.10 | -0.09 | -0.05 | -0.03 | -0.05 | -0.01 | -0.02 | 330. |
| 335. | -0.03 | -0.03 | -0.01 | 0.01 | -0.03 | 0.01 | -0.01 | 335. |
| 340. | 0.08 | 0.04 | 0.04 | 0.04 | -0.01 | 0.03 | -0.00 | 340. |
| 345. | 0.15 | 0.09 | 0.07 | 0.06 | 0.02 | 0.04 | 0.00 | 345. |
| 350. | 0.19 | 0.09 | 0.10 | 0.06 | 0.03 | 0.04 | 0.00 | 350. |
| 355. | 0.19 | 0.12 | 0.10 | 0.07 | 0.03 | 0.04 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 354 TCN= 5. C.R.= 90.1

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.65 | 0.48 | 0.35 | 0.29 | 0.20 | 0.10 | 0.04 | 0. |
| 5. | 0.52 | 0.37 | 0.31 | 0.26 | 0.20 | 0.09 | 0.04 | 5. |
| 10. | 0.49 | 0.30 | 0.24 | 0.22 | 0.18 | 0.09 | 0.03 | 10. |
| 15. | 0.44 | 0.26 | 0.20 | 0.16 | 0.15 | 0.07 | 0.02 | 15. |
| 20. | 0.38 | 0.21 | 0.18 | 0.15 | 0.13 | 0.04 | 0.01 | 20. |
| 25. | 0.37 | 0.17 | 0.15 | 0.14 | 0.12 | 0.03 | 0.01 | 25. |
| 30. | 0.29 | 0.16 | 0.13 | 0.11 | 0.11 | 0.01 | -0.01 | 30. |
| 35. | 0.32 | 0.16 | 0.11 | 0.09 | 0.10 | -0.00 | -0.02 | 35. |
| 40. | 0.31 | 0.17 | 0.09 | 0.08 | 0.10 | -0.00 | -0.02 | 40. |
| 45. | 0.30 | 0.16 | 0.08 | 0.07 | 0.09 | -0.02 | -0.03 | 45. |
| 50. | 0.33 | 0.14 | 0.07 | 0.06 | 0.08 | -0.04 | -0.04 | 50. |
| 55. | 0.35 | 0.11 | 0.04 | 0.04 | 0.08 | -0.04 | -0.04 | 55. |
| 60. | 0.27 | 0.08 | -0.00 | 0.00 | 0.07 | -0.05 | -0.05 | 60. |
| 65. | 0.27 | 0.05 | 0.00 | -0.01 | 0.05 | -0.06 | -0.05 | 65. |
| 70. | 0.26 | 0.01 | 0.01 | -0.00 | 0.05 | -0.04 | -0.04 | 70. |
| 75. | 0.09 | -0.08 | -0.08 | -0.06 | 0.03 | -0.06 | -0.05 | 75. |
| 80. | 0.00 | -0.09 | -0.08 | -0.08 | 0.03 | -0.05 | -0.04 | 80. |
| 85. | 0.18 | -0.00 | -0.04 | -0.06 | 0.00 | -0.04 | -0.03 | 85. |
| 90. | -0.11 | -0.22 | -0.18 | -0.15 | 0.02 | -0.05 | -0.04 | 90. |
| 95. | -0.16 | -0.25 | -0.17 | -0.12 | -0.01 | -0.05 | -0.03 | 95. |
| 100. | 0.15 | -0.04 | -0.04 | -0.04 | 0.03 | -0.04 | -0.02 | 100. |
| 105. | 0.14 | -0.02 | -0.03 | -0.04 | 0.04 | -0.04 | -0.03 | 105. |
| 110. | -0.07 | -0.20 | -0.14 | -0.12 | 0.02 | -0.04 | -0.03 | 110. |
| 115. | -0.09 | -0.19 | -0.10 | -0.08 | 0.02 | -0.02 | -0.01 | 115. |
| 120. | 0.12 | -0.03 | -0.03 | -0.02 | 0.04 | -0.00 | -0.01 | 120. |
| 125. | 0.18 | 0.01 | 0.01 | -0.02 | 0.04 | -0.02 | -0.01 | 125. |
| 130. | 0.01 | -0.01 | -0.04 | -0.03 | 0.02 | -0.02 | -0.02 | 130. |
| 135. | -0.00 | -0.05 | -0.05 | -0.04 | 0.01 | -0.01 | -0.01 | 135. |
| 140. | -0.09 | -0.04 | -0.04 | -0.04 | 0.02 | 0.00 | -0.01 | 140. |
| 145. | -0.04 | -0.01 | -0.02 | -0.03 | 0.03 | 0.01 | 0.00 | 145. |
| 150. | -0.02 | 0.03 | 0.01 | -0.01 | 0.04 | 0.02 | 0.02 | 150. |
| 155. | 0.05 | 0.08 | 0.04 | 0.03 | 0.05 | 0.02 | 0.02 | 155. |
| 160. | 0.14 | 0.11 | 0.08 | 0.06 | 0.06 | 0.02 | 0.02 | 160. |
| 165. | 0.19 | 0.13 | 0.12 | 0.08 | 0.04 | 0.04 | 0.01 | 165. |
| 170. | 0.26 | 0.19 | 0.16 | 0.10 | 0.07 | 0.04 | 0.01 | 170. |
| 175. | 0.30 | 0.24 | 0.17 | 0.12 | 0.07 | 0.04 | 0.02 | 175. |
| 180. | 0.41 | 0.34 | 0.18 | 0.12 | 0.07 | 0.04 | 0.02 | 180. |
| 185. | 0.38 | 0.33 | 0.18 | 0.11 | 0.06 | 0.03 | 0.01 | 185. |
| 190. | 0.28 | 0.31 | 0.18 | 0.12 | 0.04 | 0.03 | 0.01 | 190. |
| 195. | 0.25 | 0.27 | 0.17 | 0.11 | 0.00 | 0.02 | 0.00 | 195. |
| 200. | 0.22 | 0.23 | 0.13 | 0.09 | -0.02 | 0.01 | 0.00 | 200. |
| 205. | 0.12 | 0.19 | 0.07 | 0.04 | -0.04 | -0.00 | 0.00 | 205. |
| 210. | 0.04 | 0.13 | 0.04 | 0.01 | -0.05 | -0.00 | 0.01 | 210. |
| 215. | -0.05 | 0.02 | 0.03 | -0.01 | -0.06 | 0.00 | 0.00 | 215. |
| 220. | -0.19 | -0.10 | -0.04 | -0.02 | -0.07 | 0.01 | 0.00 | 220. |
| 225. | -0.39 | -0.18 | -0.11 | -0.06 | -0.09 | 0.02 | 0.01 | 225. |
| 230. | -0.58 | -0.25 | -0.16 | -0.11 | -0.10 | 0.02 | 0.03 | 230. |
| 235. | -0.64 | -0.31 | -0.20 | -0.15 | -0.12 | 0.01 | 0.03 | 235. |
| 240. | -0.64 | -0.34 | -0.22 | -0.17 | -0.14 | 0.01 | 0.03 | 240. |
| 245. | -0.62 | -0.35 | -0.23 | -0.17 | -0.16 | 0.00 | 0.02 | 245. |
| 250. | -0.64 | -0.33 | -0.23 | -0.16 | -0.17 | -0.01 | 0.01 | 250. |
| 255. | -0.60 | -0.30 | -0.20 | -0.13 | -0.16 | -0.02 | 0.01 | 255. |
| 260. | -0.30 | -0.25 | -0.08 | -0.11 | -0.14 | -0.02 | 0.01 | 260. |
| 265. | -0.07 | -0.08 | -0.03 | -0.09 | -0.12 | -0.02 | 0.00 | 265. |
| 270. | -0.44 | -0.29 | -0.15 | -0.13 | -0.16 | -0.05 | -0.01 | 270. |
| 275. | -0.77 | -0.54 | -0.30 | -0.25 | -0.23 | -0.07 | -0.02 | 275. |
| 280. | -0.86 | -0.52 | -0.36 | -0.26 | -0.23 | -0.08 | -0.01 | 280. |
| 285. | -0.76 | -0.44 | -0.31 | -0.21 | -0.22 | -0.06 | -0.01 | 285. |
| 290. | -0.60 | -0.32 | -0.24 | -0.15 | -0.20 | -0.05 | -0.00 | 290. |
| 295. | -0.47 | -0.26 | -0.16 | -0.11 | -0.16 | -0.04 | -0.01 | 295. |
| 300. | -0.52 | -0.37 | -0.24 | -0.19 | -0.18 | -0.06 | -0.03 | 300. |
| 305. | -0.65 | -0.39 | -0.28 | -0.21 | -0.21 | -0.07 | -0.01 | 305. |
| 310. | -0.59 | -0.30 | -0.23 | -0.17 | -0.17 | -0.05 | 0.00 | 310. |
| 315. | -0.40 | -0.12 | -0.15 | -0.09 | -0.12 | -0.02 | 0.01 | 315. |
| 320. | -0.12 | -0.02 | -0.00 | -0.02 | -0.06 | 0.01 | 0.02 | 320. |
| 325. | 0.05 | -0.09 | 0.04 | 0.04 | -0.01 | 0.02 | 0.01 | 325. |
| 330. | -0.00 | -0.19 | 0.01 | 0.04 | -0.01 | 0.02 | 0.01 | 330. |
| 335. | 0.12 | 0.16 | 0.09 | 0.09 | 0.05 | 0.05 | 0.04 | 335. |
| 340. | 0.37 | 0.34 | 0.21 | 0.19 | 0.13 | 0.08 | 0.05 | 340. |
| 345. | 0.59 | 0.44 | 0.33 | 0.26 | 0.17 | 0.10 | 0.05 | 345. |
| 350. | 0.64 | 0.52 | 0.38 | 0.29 | 0.19 | 0.11 | 0.05 | 350. |
| 355. | 0.69 | 0.52 | 0.37 | 0.30 | 0.20 | 0.12 | 0.04 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 354 TCN= 5. C.R.= 50.1

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 1.22 | 0.73 | 0.49 | 0.31 | 0.24 | 0.14 | 0.05 | 0. |
| 5. | 1.03 | 0.92 | 0.35 | 0.22 | 0.20 | 0.12 | 0.04 | 5. |
| 10. | 0.61 | 0.41 | 0.23 | 0.16 | 0.15 | 0.09 | 0.03 | 10. |
| 15. | 0.49 | 0.45 | 0.16 | 0.14 | 0.12 | 0.05 | 0.03 | 15. |
| 20. | 0.35 | 0.48 | 0.11 | 0.09 | 0.09 | 0.03 | 0.02 | 20. |
| 25. | 0.26 | 0.47 | 0.06 | 0.04 | 0.07 | 0.00 | -0.00 | 25. |
| 30. | 0.20 | 0.43 | 0.02 | 0.03 | 0.04 | -0.02 | -0.01 | 30. |
| 35. | 0.17 | 0.39 | -0.00 | 0.05 | 0.02 | -0.03 | -0.01 | 35. |
| 40. | 0.12 | 0.39 | -0.03 | 0.06 | 0.02 | -0.05 | -0.02 | 40. |
| 45. | 0.09 | 0.40 | -0.06 | 0.07 | 0.03 | -0.07 | -0.03 | 45. |
| 50. | 0.06 | 0.38 | -0.07 | 0.07 | 0.04 | -0.07 | -0.04 | 50. |
| 55. | 0.01 | 0.30 | -0.06 | 0.06 | 0.05 | -0.08 | -0.05 | 55. |
| 60. | -0.07 | 0.16 | -0.07 | 0.05 | 0.05 | -0.09 | -0.06 | 60. |
| 65. | -0.18 | -0.03 | -0.12 | 0.04 | 0.05 | -0.10 | -0.07 | 65. |
| 70. | -0.25 | -0.21 | -0.19 | 0.02 | 0.04 | -0.12 | -0.07 | 70. |
| 75. | -0.40 | -0.33 | -0.29 | -0.01 | -0.01 | -0.15 | -0.07 | 75. |
| 80. | -0.81 | -0.55 | -0.35 | -0.07 | -0.05 | -0.17 | -0.07 | 80. |
| 85. | -0.56 | -0.47 | -0.24 | -0.06 | -0.02 | -0.14 | -0.06 | 85. |
| 90. | -0.43 | -0.37 | -0.23 | -0.02 | -0.01 | -0.13 | -0.06 | 90. |
| 95. | -0.84 | -0.59 | -0.35 | -0.07 | -0.04 | -0.14 | -0.05 | 95. |
| 100. | -0.48 | -0.44 | -0.24 | 0.01 | -0.01 | -0.11 | -0.04 | 100. |
| 105. | -0.22 | -0.21 | -0.06 | 0.06 | 0.03 | -0.09 | -0.05 | 105. |
| 110. | -0.40 | -0.28 | -0.09 | 0.05 | 0.04 | -0.08 | -0.03 | 110. |
| 115. | -0.55 | -0.36 | -0.14 | 0.05 | 0.02 | -0.05 | -0.03 | 115. |
| 120. | -0.35 | -0.22 | -0.12 | 0.06 | 0.02 | -0.05 | -0.03 | 120. |
| 125. | 0.00 | -0.05 | -0.07 | 0.08 | 0.03 | -0.06 | -0.03 | 125. |
| 130. | 0.13 | -0.05 | -0.03 | 0.07 | 0.02 | -0.08 | -0.05 | 130. |
| 135. | -0.06 | -0.17 | -0.06 | 0.05 | 0.02 | -0.08 | -0.05 | 135. |
| 140. | -0.16 | -0.25 | -0.08 | 0.03 | 0.02 | -0.07 | -0.03 | 140. |
| 145. | -0.09 | -0.18 | -0.08 | 0.03 | 0.03 | -0.05 | -0.02 | 145. |
| 150. | 0.09 | -0.07 | -0.05 | 0.05 | 0.05 | -0.04 | -0.01 | 150. |
| 155. | 0.18 | -0.03 | -0.00 | 0.07 | 0.07 | -0.02 | -0.00 | 155. |
| 160. | 0.21 | 0.04 | 0.03 | 0.09 | 0.08 | -0.01 | -0.00 | 160. |
| 165. | 0.19 | 0.17 | 0.06 | 0.11 | 0.08 | 0.01 | 0.00 | 165. |
| 170. | 0.18 | 0.40 | 0.09 | 0.13 | 0.08 | 0.04 | 0.02 | 170. |
| 175. | 0.15 | 0.53 | 0.13 | 0.12 | 0.08 | 0.05 | 0.03 | 175. |
| 180. | 0.12 | 0.48 | 0.15 | 0.09 | 0.08 | 0.06 | 0.03 | 180. |
| 185. | 0.09 | 0.36 | 0.14 | 0.08 | 0.06 | 0.05 | 0.02 | 185. |
| 190. | 0.06 | 0.25 | 0.12 | 0.09 | 0.04 | 0.07 | 0.03 | 190. |
| 195. | 0.02 | 0.16 | 0.10 | 0.09 | 0.01 | 0.07 | 0.03 | 195. |
| 200. | -0.01 | 0.28 | 0.09 | 0.05 | -0.01 | 0.05 | 0.03 | 200. |
| 205. | -0.05 | 0.44 | 0.08 | 0.02 | -0.03 | 0.05 | 0.03 | 205. |
| 210. | -0.09 | 0.55 | 0.08 | -0.02 | -0.04 | 0.04 | 0.02 | 210. |
| 215. | -0.11 | 0.36 | 0.08 | -0.05 | -0.05 | 0.04 | 0.03 | 215. |
| 220. | -0.14 | 0.04 | 0.06 | -0.07 | -0.05 | 0.05 | 0.03 | 220. |
| 225. | -0.19 | -0.76 | 0.02 | -0.09 | -0.06 | 0.04 | 0.03 | 225. |
| 230. | -0.23 | -0.34 | -0.03 | -0.12 | -0.07 | 0.04 | 0.04 | 230. |
| 235. | -0.24 | -0.33 | -0.06 | -0.12 | -0.08 | 0.05 | 0.04 | 2[illegible]. |
| 240. | -0.17 | -0.26 | -0.01 | -0.08 | -0.08 | 0.06 | 0.04 | 24[illegible]. |
| 245. | -0.03 | -0.15 | 0.04 | -0.04 | -0.06 | 0.06 | 0.04 | 245. |
| 250. | 0.31 | 0.07 | 0.11 | 0.01 | -0.03 | 0.07 | 0.04 | 250. |
| 255. | [illegible]7 | 0.12 | 0.12 | -0.03 | -0.04 | 0.04 | 0.02 | 255. |
| 260. | -0.49 | -0.36 | -0.16 | -0.19 | -0.13 | 0.03 | 0.00 | 260. |
| 265. | -0.80 | -0.71 | -0.25 | -0.32 | -0.22 | -0.00 | -0.00 | 265. |
| 270. | -0.83 | -0.73 | -0.27 | -0.34 | -0.26 | -0.04 | -0.01 | 270. |
| 275. | -0.61 | -0.58 | -0.28 | -0.30 | -0.24 | -0.05 | -0.02 | 275. |
| 280. | -0.51 | -0.56 | -0.13 | -0.27 | -0.20 | -0.04 | -0.02 | 280. |
| 285. | -0.62 | -0.52 | -0.20 | -0.29 | -0.22 | -0.03 | -0.02 | 285. |
| 290. | -0.73 | -0.69 | -0.27 | -0.33 | -0.25 | -0.05 | -0.03 | 290. |
| 295. | -0.74 | -0.71 | -0.25 | -0.35 | -0.25 | -0.05 | -0.02 | 295. |
| 300. | -0.66 | -0.62 | -0.23 | -0.32 | -0.22 | -0.03 | -0.01 | 300. |
| 305. | -0.54 | -0.52 | -0.23 | -0.27 | -0.17 | -0.02 | -0.01 | 305. |
| 310. | -0.41 | -0.44 | -0.19 | -0.23 | -0.13 | -0.01 | 0.01 | 310. |
| 315. | -0.23 | -0.34 | -0.08 | -0.19 | -0.09 | 0.02 | 0.03 | 315. |
| 320. | 0.01 | -0.20 | 0.02 | -0.10 | -0.04 | 0.05 | 0.04 | 320. |
| 325. | 0.27 | -0.02 | 0.11 | -0.00 | 0.00 | 0.08 | 0.05 | 325. |
| 330. | 0.55 | 0.22 | 0.21 | 0.07 | 0.05 | 0.11 | 0.06 | 330. |
| 335. | 0.80 | 0.43 | 0.31 | 0.14 | 0.11 | 0.13 | 0.06 | 335. |
| 340. | 1.03 | 0.52 | 0.45 | 0.24 | 0.18 | 0.15 | 0.06 | 340. |
| 345. | 1.47 | 0.77 | 0.58 | 0.34 | 0.24 | 0.19 | 0.07 | 345. |
| 350. | 1.62 | 0.93 | 0.56 | 0.33 | 0.26 | 0.17 | 0.06 | 350. |
| 355. | 1.38 | 0.70 | 0.46 | 0.33 | 0.26 | 0.14 | 0.04 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 394 TCN= 5. C.R.= 50.1

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.950 | 7.150 | 10.400 | DEG. |
| 0. | 0.69 | 0.50 | 0.33 | 0.21 | 0.18 | 0.09 | 0.03 | 0. |
| 5. | 0.52 | 0.44 | 0.25 | 0.16 | 0.13 | 0.06 | 0.02 | 5. |
| 10. | 0.36 | 0.35 | 0.19 | 0.12 | 0.07 | 0.02 | 0.01 | 10. |
| 15. | 0.17 | 0.19 | 0.02 | 0.09 | -0.01 | -0.01 | 0.00 | 15. |
| 20. | -0.04 | 0.01 | -0.12 | 0.01 | -0.08 | -0.05 | -0.01 | 20. |
| 25. | -0.26 | -0.17 | -0.25 | -0.06 | -0.12 | -0.08 | -0.01 | 25. |
| 30. | -0.39 | -0.29 | -0.33 | -0.18 | -0.16 | -0.10 | -0.02 | 30. |
| 35. | -0.46 | -0.36 | -0.37 | -0.15 | -0.19 | -0.11 | -0.02 | 35. |
| 40. | -0.49 | -0.42 | -0.39 | -0.18 | -0.2. | -0.11 | -0.03 | 40. |
| 45. | -0.52 | -0.47 | -0.39 | -0.21 | -0.23 | -0.12 | -0.03 | 45. |
| 50. | -0.54 | -0.51 | -0.41 | -0.22 | -0.25 | -0.13 | -0.03 | 50. |
| 55. | -0.59 | -0.45 | -0.45 | -0.23 | -0.26 | -0.14 | -0.02 | 55. |
| 60. | -0.46 | -0.49 | -0.50 | -0.24 | -0.27 | -0.16 | -0.03 | 60. |
| 65. | -0.74 | -0.62 | -0.55 | -0.26 | -0.29 | -0.17 | -0.04 | 65. |
| 70. | -0.83 | -0.65 | -0.61 | -0.31 | -0.31 | -0.19 | -0.05 | 70. |
| 75. | -0.88 | -0.69 | -0.62 | -0.35 | -0.35 | -0.21 | -0.06 | 75. |
| 80. | -1.22 | -0.89 | -0.69 | -0.36 | -0.39 | -0.21 | -0.05 | 80. |
| 85. | -1.38 | -0.92 | -0.82 | -0.39 | -0.41 | -0.19 | -0.04 | 85. |
| 90. | -0.84 | -0.49 | -0.57 | -0.32 | -0.30 | -0.12 | -0.03 | 90. |
| 95. | -0.87 | -0.64 | -0.56 | -0.26 | -0.23 | -0.11 | -0.01 | 95. |
| 100. | -0.88 | -0.65 | -0.47 | -0.23 | -0.22 | -0.08 | 0.00 | 100. |
| 105. | -0.45 | -0.31 | -0.29 | -0.19 | -0.16 | -0.07 | 0.01 | 105. |
| 110. | -0.27 | -0.34 | -0.25 | -0.17 | -0.13 | -0.07 | -0.01 | 110. |
| 115. | -0.61 | -0.54 | -0.34 | -0.17 | -0.14 | -0.09 | -0.01 | 115. |
| 120. | -0.76 | -0.56 | -0.40 | -0.17 | -0.16 | -0.09 | -0.02 | 120. |
| 125. | -0.66 | -0.51 | -0.38 | -0.18 | -0.15 | -0.04 | -0.02 | 125. |
| 130. | -0.40 | -0.42 | -0.28 | -0.13 | -0.13 | -0.04 | -0.02 | 130. |
| 135. | -0.07 | -0.31 | -0.15 | -0.08 | -0.10 | -0.04 | -0.02 | 135. |
| 140. | 0.23 | -0.18 | -0.02 | -0.02 | -0.09 | -0.03 | -0.02 | 140. |
| 145. | 0.43 | -0.03 | 0.09 | 0.01 | -0.01 | -0.02 | -0.02 | 145. |
| 150. | 0.52 | 0.1 | 0.16 | 0.03 | 0.03 | 0.00 | -0.01 | 150. |
| 155. | 0.57 | 0.. | 0.21 | 0.04 | 0.06 | 0.03 | -0.01 | 155. |
| 160. | 0.59 | 0.25 | 0.24 | 0.05 | 0.09 | 0.05 | -0.00 | 160. |
| 165. | 0.59 | 0.30 | 0.26 | 0.06 | 0.12 | 0.09 | 0.01 | 165. |
| 170. | 0.60 | 0.34 | 0.28 | 0.08 | 0.14 | 0.09 | 0.01 | 170. |
| 175. | 0.60 | 0.37 | 0.29 | 0.10 | 0.16 | 0.10 | 0.01 | 175. |
| 180. | 0.62 | 0.41 | 0.30 | 0.12 | 0.17 | 0.11 | 0.02 | 180. |
| 185. | 0.65 | 0.44 | 0.32 | 0.14 | 0.18 | 0.11 | 0.02 | 185. |
| 190. | 0.69 | 0.48 | 0.34 | 0.16 | 0.18 | 0.11 | 0.02 | 190. |
| 195. | 0.73 | 0.51 | 0.41 | 0.17 | 0.18 | 0.11 | 0.02 | 195. |
| 200. | 0.75 | 0.54 | 0.44 | 0.18 | 0.20 | 0.11 | 0.02 | 200. |
| 205. | 0.77 | 0.47 | 0.45 | 0.17 | 0.21 | 0.11 | 0.02 | 205. |
| 210. | 0.77 | 0.59 | 0.45 | 0.17 | 0.22 | 0.11 | 0.01 | 210. |
| 215. | 0.78 | 0.60 | 0.46 | 0.19 | 0.24 | 0.11 | 0.01 | 215. |
| 220. | 0.85 | 0.63 | 0.51 | 0.22 | 0.26 | 0.12 | 0.01 | 220. |
| 225. | 0.97 | 0.70 | 0.56 | 0.26 | 0.27 | 0.12 | 0.01 | 225. |
| 230. | 1.09 | 0.75 | 0.61 | 0.28 | 0.27 | 0.12 | 0.01 | 230. |
| 235. | 1.12 | 0.80 | 0.63 | 0.29 | 0.25 | 0.11 | 0.01 | 235. |
| 240. | 0.97 | 0.73 | 0.54 | 0.25 | 0.21 | 0.11 | 0.01 | 240. |
| 245. | 0.59 | 0.50 | 0.41 | 0.18 | 0.17 | 0.11 | 0.02 | 245. |
| 250. | 0.03 | 0.24 | 0.20 | 0.13 | 0.15 | 0.12 | 0.04 | 250. |
| 255. | -0.25 | 0.11 | 0.08 | 0.10 | 0.13 | 0.13 | 0.05 | 255. |
| 260. | -0.24 | 0.11 | 0.10 | 0.10 | 0.14 | 0.12 | 0.05 | 260. |
| 265. | 0.04 | 0.21 | 0.21 | 0.17 | 0.16 | 0.11 | 0.04 | 265. |
| 270. | 0.34 | 0.29 | 0.35 | 0.18 | 0.18 | 0.07 | 0.03 | 270. |
| 275. | -0.14 | 0.04 | 0.13 | 0.06 | 0.05 | -0.04 | 0.01 | 275. |
| 280. | -1.09 | -0.39 | -0.30 | -0.11 | -0.12 | -0.10 | -0.02 | 280. |
| 285. | -1.16 | -0.49 | -0.45 | -0.22 | -0.19 | -0.11 | -0.02 | 285. |
| 290. | -0.97 | -0.42 | -0.37 | -0.25 | -0.21 | -0.11 | -0.01 | 290. |
| 295. | -0.84 | -0.44 | -0.30 | -0.23 | -0.19 | -0.11 | -0.02 | 295. |
| 300. | -0.79 | -0.43 | -0.27 | -0.17 | -0.16 | -0.13 | -0.02 | 300. |
| 305. | -0.75 | -0.37 | -0.24 | -0.14 | -0.12 | -0.08 | -0.02 | 305. |
| 310. | -0.58 | -0.28 | -0.17 | -0.09 | -0.07 | -0.05 | -0.02 | 310. |
| 315. | -0.35 | -0.18 | -0.07 | -0.04 | -0.01 | -0.02 | -0.01 | 315. |
| 320. | -0.13 | -0.06 | 0.02 | 0.04 | 0.05 | 0.02 | 0.01 | 320. |
| 325. | 0.10 | 0.06 | 0.13 | 0.12 | 0.11 | 0.09 | 0.02 | 325. |
| 330. | 0.34 | 0.20 | 0.25 | 0.19 | 0.17 | 0.08 | 0.02 | 330. |
| 335. | 0.55 | 0.36 | 0.37 | 0.23 | 0.22 | 0.11 | 0.03 | 335. |
| 340. | 0.75 | 0.49 | 0.43 | 0.27 | 0.26 | 0.13 | 0.04 | 340. |
| 345. | 0.88 | 0.56 | 0.47 | 0.29 | 0.27 | 0.14 | 0.04 | 345. |
| 350. | 0.94 | 0.60 | 0.48 | 0.29 | 0.26 | 0.13 | 0.04 | 350. |
| 355. | 0.86 | 0.59 | 0.43 | 0.29 | 0.23 | 0.12 | 0.03 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 454 TCN= 9. C.R.= 0.1

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.57 | 0.48 | 0.44 | 0.32 | 0.10 | 0.11 | 0.03 | 0. |
| 5. | 0.63 | 0.42 | 0.31 | 0.22 | 0.09 | 0.07 | 0.02 | 5. |
| 10. | 0.37 | 0.23 | 0.15 | 0.12 | 0.07 | 0.03 | 0.01 | 10. |
| 15. | 0.10 | -0.00 | -0.01 | -0.00 | 0.03 | -0.02 | -0.01 | 15. |
| 20. | -0.20 | -0.26 | -0.17 | -0.12 | -0.01 | -0.05 | -0.03 | 20. |
| 25. | -0.49 | -0.44 | -0.29 | -0.21 | -0.04 | -0.09 | -0.03 | 25. |
| 30. | -0.67 | -0.57 | -0.38 | -0.28 | -0.07 | -0.11 | -0.04 | 30. |
| 35. | -0.79 | -0.65 | -0.43 | -0.32 | -0.06 | -0.13 | -0.04 | 35. |
| 40. | -0.85 | -0.68 | -0.46 | -0.34 | -0.05 | -0.14 | -0.04 | 40. |
| 45. | -0.89 | -0.69 | -0.47 | -0.34 | 0.01 | -0.15 | -0.03 | 45. |
| 50. | -0.93 | -0.72 | -0.50 | -0.37 | 0.01 | -0.17 | -0.05 | 50. |
| 55. | -1.00 | -0.76 | -0.52 | -0.39 | 0.00 | -0.19 | -0.07 | 55. |
| 60. | -1.10 | -0.82 | -0.56 | -0.44 | -0.01 | -0.22 | -0.09 | 60. |
| 65. | -1.19 | -0.86 | -0.60 | -0.50 | -0.02 | -0.25 | -0.10 | 65. |
| 70. | -1.28 | -0.95 | -0.65 | -0.58 | -0.05 | -0.29 | -0.10 | 70. |
| 75. | -1.53 | -1.18 | -0.79 | -0.64 | -0.11 | -0.30 | -0.12 | 75. |
| 80. | -1.84 | -1.44 | -0.90 | -0.65 | -0.12 | -0.33 | -0.11 | 80. |
| 85. | -1.48 | -0.96 | -0.71 | -0.47 | -0.01 | -0.25 | -0.09 | 85. |
| 90. | -1.54 | -0.94 | -0.53 | -0.32 | 0.07 | -0.15 | -0.06 | 90. |
| 95. | -0.80 | -0.44 | -0.37 | -0.26 | 0.17 | -0.13 | -0.03 | 95. |
| 100. | -0.26 | -0.11 | -0.10 | -0.14 | 0.26 | -0.12 | -0.04 | 100. |
| 105. | -0.43 | 1.38 | -0.08 | -0.11 | 0.29 | -0.12 | -0.04 | 105. |
| 110. | -0.14 | -0.43 | -0.15 | -0.12 | 0.29 | -0.09 | -0.02 | 110. |
| 115. | -0.37 | -0.18 | -0.09 | -0.10 | 0.27 | -0.07 | -0.02 | 115. |
| 120. | 0.02 | 0.09 | 0.07 | -0.07 | 0.24 | -0.08 | -0.04 | 120. |
| 125. | 0.31 | 0.23 | 0.10 | -0.04 | 0.22 | -0.12 | -0.07 | 125. |
| 130. | 0.28 | 0.23 | 0.07 | -0.06 | 0.21 | -0.12 | -0.06 | 130. |
| 135. | 0.14 | 0.16 | 0.04 | -0.07 | 0.20 | -0.09 | -0.04 | 135. |
| 140. | 0.08 | 0.10 | 0.03 | -0.08 | 0.19 | -0.07 | -0.03 | 140. |
| 145. | 0.05 | 0.06 | 0.02 | -0.08 | 0.18 | -0.04 | -0.02 | 145. |
| 150. | 0.02 | 0.03 | 0.02 | -0.08 | 0.17 | -0.02 | -0.01 | 150. |
| 155. | 0.00 | 0.02 | 0.02 | -0.07 | 0.16 | -0.00 | -0.00 | 155. |
| 160. | 0.03 | 0.02 | 0.03 | -0.06 | 0.14 | 0.01 | 0.01 | 160. |
| 165. | 0.09 | 0.05 | 0.05 | -0.03 | 0.13 | 0.02 | 0.01 | 165. |
| 170. | 0.13 | 0.08 | 0.07 | -0.00 | 0.12 | 0.03 | 0.02 | 170. |
| 175. | 0.17 | 0.13 | 0.11 | 0.03 | 0.11 | 0.04 | 0.02 | 175. |
| 180. | 0.24 | 0.18 | 0.16 | 0.06 | 0.10 | 0.05 | 0.03 | 180. |
| 185. | 0.35 | 0.24 | 0.20 | 0.09 | 0.09 | 0.05 | 0.02 | 185. |
| 190. | 0.43 | 0.29 | 0.23 | 0.12 | 0.08 | 0.06 | 0.02 | 190. |
| 195. | 0.48 | 0.33 | 0.23 | 0.14 | 0.08 | 0.08 | 0.03 | 195. |
| 200. | 0.52 | 0.36 | 0.26 | 0.16 | 0.08 | 0.09 | 0.03 | 200. |
| 205. | 0.56 | 0.40 | 0.26 | 0.17 | 0.09 | 0.09 | 0.03 | 205. |
| 210. | 0.61 | 0.45 | 0.29 | 0.19 | -0.02 | 0.10 | 0.03 | 210. |
| 215. | 0.65 | 0.50 | 0.31 | 0.22 | -0.03 | 0.11 | 0.03 | 215. |
| 220. | 0.69 | 0.54 | 0.34 | 0.26 | -0.02 | 0.12 | 0.04 | 220. |
| 225. | 0.77 | 0.62 | 0.37 | 0.31 | -0.01 | 0.14 | 0.05 | 225. |
| 230. | 0.89 | 0.70 | 0.40 | 0.34 | 0.01 | 0.15 | 0.06 | 230. |
| 235. | 1.10 | 0.92 | 0.45 | 0.42 | 0.04 | 0.17 | 0.06 | 235. |
| 240. | 1.38 | 0.95 | 0.57 | 0.48 | 0.08 | 0.18 | 0.06 | 240. |
| 245. | 1.71 | 1.09 | 0.70 | 0.54 | 0.09 | 0.19 | 0.07 | 245. |
| 250. | 1.91 | 1.23 | 0.75 | 0.57 | 0.08 | 0.19 | 0.06 | 250. |
| 255. | 1.77 | 1.15 | 0.69 | 0.50 | 0.06 | 0.18 | 0.05 | 255. |
| 260. | 1.20 | 0.75 | 0.50 | 0.39 | 0.04 | 0.19 | 0.04 | 260. |
| 265. | 0.20 | 0.23 | 0.25 | 0.27 | -0.01 | 0.21 | 0.04 | 265. |
| 270. | -0.04 | 0.05 | 0.09 | 0.20 | -0.07 | 0.19 | 0.11 | 270. |
| 275. | 0.00 | 0.12 | 0.17 | 0.20 | -0.14 | 0.14 | 0.08 | 275. |
| 280. | -0.21 | -0.20 | -0.08 | 0.04 | -0.29 | 0.07 | 0.03 | 280. |
| 285. | -0.94 | -0.67 | -0.39 | -0.22 | -0.44 | 0.00 | -0.00 | 285. |
| 290. | -1.15 | -0.87 | -0.52 | -0.30 | -0.56 | -0.05 | -0.02 | 290. |
| 295. | -1.17 | -0.88 | -0.54 | -0.30 | -0.59 | -0.08 | -0.03 | 295. |
| 300. | -1.05 | -0.77 | -0.50 | -0.28 | -0.57 | -0.08 | -0.03 | 300. |
| 305. | -0.84 | -0.56 | -0.40 | -0.20 | -0.51 | -0.06 | -0.02 | 305. |
| 310. | -0.58 | -0.31 | -0.27 | -0.12 | -0.41 | -0.01 | -0.00 | 310. |
| 315. | -0.31 | -0.09 | -0.14 | -0.03 | -0.32 | 0.03 | 0.01 | 315. |
| 320. | 0.00 | 0.06 | -0.00 | 0.08 | -0.22 | 0.06 | 0.03 | 320. |
| 325. | 0.29 | 0.21 | 0.14 | 0.18 | -0.13 | 0.09 | 0.04 | 325. |
| 330. | 0.55 | 0.39 | 0.28 | 0.26 | -0.05 | 0.12 | 0.05 | 330. |
| 335. | 0.81 | 0.57 | 0.39 | 0.32 | 0.01 | 0.15 | 0.05 | 335. |
| 340. | 1.03 | 0.75 | 0.48 | 0.36 | 0.05 | 0.16 | 0.06 | 340. |
| 345. | 1.14 | 0.85 | 0.54 | 0.40 | 0.08 | 0.15 | 0.05 | 345. |
| 350. | 1.14 | 0.83 | 0.55 | 0.42 | 0.10 | 0.16 | 0.06 | 350. |
| 355. | 1.04 | 0.72 | 0.51 | 0.38 | 0.10 | 0.15 | 0.05 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST•502 CNTR NO. 154 TCH• 5. C.R.• 50.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.93 | 0.54 | 0.37 | 0.24 | 0.14 | 0.06 | -0.00 | 0. |
| 5. | 0.90 | 0.34 | 0.24 | 0.15 | 0.07 | 0.03 | -0.02 | 5. |
| 10. | 0.18 | 0.16 | 0.10 | 0.03 | -0.01 | -0.03 | -0.03 | 10. |
| 15. | -0.06 | -0.02 | -0.06 | -0.09 | -0.07 | -0.05 | -0.04 | 15. |
| 20. | -0.41 | -0.22 | -0.22 | -0.20 | -0.13 | -0.10 | -0.06 | 20. |
| 25. | -0.79 | -0.43 | -0.35 | -0.28 | -0.17 | -0.14 | -0.07 | 25. |
| 30. | -0.94 | -0.56 | -0.41 | -0.33 | -0.20 | -0.17 | -0.08 | 30. |
| 35. | -0.97 | -0.62 | -0.45 | -0.37 | -0.22 | -0.19 | -0.08 | 35. |
| 40. | -1.02 | -0.66 | -0.45 | -0.38 | -0.23 | -0.21 | -0.08 | 40. |
| 45. | -1.10 | -0.69 | -0.53 | -0.40 | -0.23 | -0.23 | -0.08 | 45. |
| 50. | -1.19 | -0.73 | -0.57 | -0.41 | -0.23 | -0.24 | -0.09 | 50. |
| 55. | -1.31 | -0.77 | -0.60 | -0.44 | -0.24 | -0.25 | -0.10 | 55. |
| 60. | -1.45 | -0.83 | -0.64 | -0.49 | -0.26 | -0.28 | -0.11 | 60. |
| 65. | -1.63 | -0.93 | -0.71 | -0.62 | -0.31 | -0.31 | -0.12 | 65. |
| 70. | -1.82 | -1.17 | -0.82 | -0.74 | -0.34 | -0.34 | -0.13 | 70. |
| 75. | -2.13 | -1.45 | -1.03 | -0.77 | -0.36 | -0.34 | -0.14 | 75. |
| 80. | -2.08 | -1.28 | -0.87 | -0.61 | -0.30 | -0.28 | -0.11 | 80. |
| 85. | -1.35 | -0.69 | -0.39 | -0.33 | -0.15 | -0.20 | -0.07 | 85. |
| 90. | -0.04 | -0.01 | 0.04 | -0.04 | -0.03 | -0.13 | -0.05 | 90. |
| 95. | 0.13 | 0.24 | 0.15 | 0.10 | 0.04 | -0.10 | -0.05 | 95. |
| 100. | 0.18 | 0.24 | 0.17 | 0.12 | 0.08 | -0.10 | -0.05 | 100. |
| 105. | 0.57 | 0.53 | 0.25 | 0.10 | 0.08 | -0.11 | -0.05 | 105. |
| 110. | 0.93 | 0.57 | 0.32 | 0.08 | 0.07 | -0.13 | -0.06 | 110. |
| 115. | 0.45 | 0.37 | 0.21 | 0.03 | 0.05 | -0.14 | -0.07 | 115. |
| 120. | 0.03 | 0.11 | 0.05 | -0.02 | 0.01 | -0.13 | -0.07 | 120. |
| 125. | -0.26 | -0.09 | -0.09 | -0.08 | -0.02 | -0.13 | -0.07 | 125. |
| 130. | -0.39 | -0.22 | -0.18 | -0.14 | -0.06 | -0.13 | -0.07 | 130. |
| 135. | -0.43 | -0.28 | -0.21 | -0.17 | -0.08 | -0.13 | -0.06 | 135. |
| 140. | -0.46 | -0.30 | -0.21 | -0.17 | -0.09 | -0.11 | -0.05 | 140. |
| 145. | -0.48 | -0.30 | -0.21 | -0.17 | -0.09 | -0.10 | -0.04 | 145. |
| 150. | -0.46 | -0.31 | -0.21 | -0.15 | -0.08 | -0.09 | -0.03 | 150. |
| 155. | -0.47 | -0.31 | -0.20 | -0.13 | -0.06 | -0.07 | -0.02 | 155. |
| 160. | -0.46 | -0.28 | -0.18 | -0.10 | -0.05 | -0.04 | -0.00 | 160. |
| 165. | -0.41 | -0.24 | -0.16 | -0.06 | -0.02 | -0.03 | 0.01 | 165. |
| 170. | -0.30 | -0.19 | -0.13 | -0.03 | -0.00 | -0.02 | 0.02 | 170. |
| 175. | -0.15 | -0.12 | -0.10 | 0.00 | 0.02 | 0.00 | 0.02 | 175. |
| 180. | -0.05 | -0.05 | -0.05 | 0.03 | 0.04 | 0.02 | 0.03 | 180. |
| 185. | 0.03 | 0.02 | 0.03 | 0.05 | 0.06 | 0.04 | 0.04 | 185. |
| 190. | 0.15 | 0.10 | 0.09 | 0.07 | 0.07 | 0.05 | 0.04 | 190. |
| 195. | 0.26 | 0.17 | 0.11 | 0.09 | 0.07 | 0.09 | 0.05 | 195. |
| 200. | 0.31 | 0.21 | 0.12 | 0.12 | 0.08 | 0.08 | 0.05 | 200. |
| 205. | 0.34 | 0.22 | 0.12 | 0.13 | 0.08 | 0.09 | 0.05 | 205. |
| 210. | 0.38 | 0.23 | 0.13 | 0.15 | 0.08 | 0.09 | 0.05 | 210. |
| 215. | 0.44 | 0.23 | 0.15 | 0.16 | 0.09 | 0.10 | 0.05 | 215. |
| 220. | 0.47 | 0.23 | 0.18 | 0.18 | 0.09 | 0.12 | 0.05 | 220. |
| 225. | 0.49 | 0.25 | 0.22 | 0.20 | 0.11 | 0.14 | 0.06 | 225. |
| 230. | 0.58 | 0.30 | 0.29 | 0.23 | 0.14 | 0.15 | 0.06 | 230. |
| 235. | 0.76 | 0.39 | 0.34 | 0.28 | 0.17 | 0.18 | 0.07 | 235. |
| 240. | 1.01 | 0.54 | 0.45 | 0.37 | 0.22 | 0.21 | 0.09 | 240. |
| 245. | 1.33 | 0.74 | 0.56 | 0.48 | 0.27 | 0.25 | 0.10 | 245. |
| 250. | 1.73 | 1.01 | 0.72 | 0.58 | 0.32 | 0.28 | 0.11 | 250. |
| 255. | 2.09 | 1.26 | 0.86 | 0.66 | 0.36 | 0.30 | 0.11 | 255. |
| 260. | 2.46 | 1.49 | 0.97 | 0.71 | 0.37 | 0.29 | 0.10 | 260. |
| 265. | 2.66 | 1.48 | 0.97 | 0.70 | 0.35 | 0.27 | 0.10 | 265. |
| 270. | 2.29 | 1.16 | 0.82 | 0.60 | 0.31 | 0.27 | 0.09 | 270. |
| 275. | 1.25 | 0.71 | 0.55 | 0.50 | 0.27 | 0.29 | 0.10 | 275. |
| 280. | 0.28 | 0.25 | 0.34 | 0.36 | 0.21 | 0.23 | 0.12 | 280. |
| 285. | -0.19 | -0.34 | 0.00 | 0.04 | 0.06 | 0.18 | 0.10 | 285. |
| 290. | -1.22 | -0.88 | -0.44 | -0.24 | -0.14 | 0.05 | 0.07 | 290. |
| 295. | -1.72 | -1.09 | -0.68 | -0.41 | -0.27 | -0.01 | 0.03 | 295. |
| 300. | -1.57 | -1.02 | -0.69 | -0.46 | -0.31 | -0.04 | 0.01 | 300. |
| 305. | -1.13 | -0.74 | -0.52 | -0.30 | -0.29 | -0.01 | 0.01 | 305. |
| 310. | -0.53 | -0.39 | -0.31 | -0.17 | -0.20 | 0.04 | 0.02 | 310. |
| 315. | -0.15 | -0.14 | -0.09 | -0.08 | -0.10 | 0.07 | 0.03 | 315. |
| 320. | 0.20 | 0.09 | 0.07 | -0.00 | -0.04 | 0.09 | 0.04 | 320. |
| 325. | 0.60 | 0.29 | 0.18 | 0.07 | 0.01 | 0.14 | 0.05 | 325. |
| 330. | 0.59 | 0.46 | 0.27 | 0.16 | 0.07 | 0.13 | 0.05 | 330. |
| 335. | 0.12 | 0.60 | 0.28 | 0.24 | 0.13 | 0.15 | 0.04 | 335. |
| 340. | 0.58 | 0.70 | 0.46 | 0.32 | 0.18 | 0.15 | 0.04 | 340. |
| 345. | 1.35 | 0.75 | 0.52 | 0.37 | 0.20 | 0.15 | 0.04 | 345. |
| 350. | 1.35 | 0.74 | 0.53 | 0.35 | 0.20 | 0.13 | 0.03 | 350. |
| 355. | 1.18 | 0.68 | 0.47 | 0.29 | 0.18 | 0.10 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 306 TCN= 8. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.550 | 10.400 | DEG. |
| 0. | -0.11 | -0.05 | -0.02 | -0.01 | 0. |
| 5. | -0.16 | -0.07 | 0.03 | -0.02 | 5. |
| 10. | -0.18 | -0.09 | -0.01 | -0.03 | 10. |
| 15. | -0.20 | -0.09 | -0.02 | -0.03 | 15. |
| 20. | -0.09 | -0.04 | 0.01 | -0.01 | 20. |
| 25. | 0.16 | 0.09 | 0.08 | 0.00 | 25. |
| 30. | 0.37 | 0.21 | 0.12 | -0.00 | 30. |
| 35. | 0.22 | 0.11 | 0.07 | -0.01 | 35. |
| 40. | -0.00 | -0.02 | 0.02 | -0.00 | 40. |
| 45. | -0.05 | -0.06 | 0.01 | 0.00 | 45. |
| 50. | 0.02 | -0.02 | 0.02 | 0.01 | 50. |
| 55. | 0.06 | 0.02 | 0.02 | 0.01 | 55. |
| 60. | 0.04 | -0.00 | 0.01 | 0.02 | 60. |
| 65. | -0.01 | -0.03 | 0.00 | 0.02 | 65. |
| 70. | -0.08 | -0.06 | -0.01 | 0.01 | 70. |
| 75. | -0.14 | -0.06 | -0.01 | 0.02 | 75. |
| 80. | -0.17 | -0.07 | -0.01 | 0.03 | 80. |
| 85. | -0.17 | -0.07 | -0.01 | 0.03 | 85. |
| 90. | -0.14 | -0.06 | -0.01 | 0.02 | 90. |
| 95. | -0.09 | -0.04 | 0.01 | 0.03 | 95. |
| 100. | -0.02 | -0.03 | 0.03 | 0.06 | 100. |
| 105. | 0.06 | -0.00 | 0.05 | 0.07 | 105. |
| 110. | 0.13 | 0.03 | 0.08 | 0.07 | 110. |
| 115. | 0.21 | 0.07 | 0.11 | 0.06 | 115. |
| 120. | 0.30 | 0.12 | 0.13 | 0.06 | 120. |
| 125. | 0.37 | 0.16 | 0.15 | 0.07 | 125. |
| 130. | 0.44 | 0.20 | 0.16 | 0.07 | 130. |
| 135. | 0.49 | 0.23 | 0.16 | 0.07 | 135. |
| 140. | 0.52 | 0.24 | 0.16 | 0.06 | 140. |
| 145. | 0.52 | 0.25 | 0.16 | 0.05 | 145. |
| 150. | 0.52 | 0.27 | 0.16 | 0.05 | 150. |
| 155. | 0.59 | 0.29 | 0.17 | 0.05 | 155. |
| 160. | 0.75 | 0.33 | 0.19 | 0.05 | 160. |
| 165. | 0.88 | 0.41 | 0.22 | 0.05 | 165. |
| 170. | 0.95 | 0.47 | 0.25 | 0.05 | 170. |
| 175. | 0.89 | 0.44 | 0.24 | 0.05 | 175. |
| 180. | 0.76 | 0.37 | 0.21 | 0.05 | 180. |
| 185. | 0.59 | 0.27 | 0.17 | 0.06 | 185. |
| 190. | 0.43 | 0.20 | 0.12 | 0.04 | 190. |
| 195. | 0.27 | 0.13 | 0.07 | 0.02 | 195. |
| 200. | 0.13 | 0.06 | 0.01 | 0.02 | 200. |
| 205. | 0.01 | -0.01 | -0.05 | 0.02 | 205. |
| 210. | -0.09 | -0.07 | -0.08 | 0.01 | 210. |
| 215. | -0.18 | -0.11 | -0.10 | -0.01 | 215. |
| 220. | -0.26 | -0.13 | -0.11 | -0.02 | 220. |
| 225. | -0.30 | -0.13 | -0.12 | -0.03 | 225. |
| 230. | -0.32 | -0.14 | -0.13 | -0.03 | 230. |
| 235. | -0.34 | -0.15 | -0.14 | -0.02 | 235. |
| 240. | -0.34 | -0.15 | -0.14 | -0.02 | 240. |
| 245. | -0.33 | -0.15 | -0.14 | -0.03 | 245. |
| 250. | -0.32 | -0.15 | -0.14 | -0.03 | 250. |
| 255. | -0.30 | -0.15 | -0.13 | -0.03 | 255. |
| 260. | -0.30 | -0.15 | -0.13 | -0.02 | 260. |
| 265. | -0.30 | -0.16 | -0.12 | -0.02 | 265. |
| 270. | -0.30 | -0.16 | -0.12 | -0.03 | 270. |
| 275. | -0.30 | -0.16 | -0.11 | -0.05 | 275. |
| 280. | -0.30 | -0.16 | -0.11 | -0.07 | 280. |
| 285. | -0.31 | -0.15 | -0.11 | -0.08 | 285. |
| 290. | -0.32 | -0.14 | -0.12 | -0.09 | 290. |
| 295. | -0.33 | -0.12 | -0.11 | -0.09 | 295. |
| 300. | -0.33 | -0.11 | -0.11 | -0.09 | 300. |
| 305. | -0.31 | -0.11 | -0.10 | -0.08 | 305. |
| 310. | -0.28 | -0.10 | -0.08 | -0.06 | 310. |
| 315. | -0.26 | -0.11 | -0.07 | -0.04 | 315. |
| 320. | -0.30 | -0.14 | -0.07 | -0.04 | 320. |
| 325. | -0.35 | -0.16 | -0.09 | -0.05 | 325. |
| 330. | -0.38 | -0.17 | -0.10 | -0.05 | 330. |
| 335. | -0.34 | -0.15 | -0.11 | -0.04 | 335. |
| 340. | -0.5. | -0.13 | -0.10 | -0.03 | 340. |
| 345. | -0.36 | -0.11 | -0.10 | -0.02 | 345. |
| 350. | -0.36 | -0.13 | -0.09 | -0.03 | 350. |
| 355. | -0.24 | -0.10 | -0.08 | -0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-502 CNTR NO. 306 TCN= 0. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.190 | 10.400 | DEG. |
| 0. | -0.55 | -0.38 | -0.26 | -0.16 | -0.13 | -0.07 | 0.03 | 0. |
| 5. | -0.50 | -0.32 | -0.26 | -0.17 | -0.13 | -0.08 | 0.02 | 5. |
| 10. | -0.33 | -0.18 | -0.10 | -0.16 | -0.09 | -0.08 | 0.01 | 10. |
| 15. | -0.07 | -0.05 | -0.11 | -0.10 | -0.03 | -0.06 | 0.02 | 15. |
| 20. | 0.09 | 0.04 | -0.00 | -0.03 | 0.02 | -0.04 | 0.02 | 20. |
| 25. | 0.15 | 0.09 | 0.02 | -0.00 | 0.03 | -0.03 | 0.01 | 25. |
| 30. | 0.20 | 0.12 | 0.03 | 0.02 | 0.05 | -0.02 | -0.00 | 30. |
| 35. | 0.26 | 0.16 | 0.06 | 0.03 | 0.06 | -0.01 | -0.00 | 35. |
| 40. | 0.33 | 0.21 | 0.09 | 0.05 | 0.07 | -0.00 | -0.01 | 40. |
| 45. | 0.37 | 0.22 | 0.09 | 0.05 | 0.07 | -0.01 | -0.02 | 45. |
| 50. | 0.33 | 0.19 | 0.06 | 0.04 | 0.07 | -0.02 | -0.04 | 50. |
| 55. | 0.24 | 0.14 | 0.02 | 0.02 | 0.07 | -0.03 | -0.04 | 55. |
| 60. | 0.11 | 0.06 | -0.02 | -0.01 | 0.06 | -0.04 | -0.04 | 60. |
| 65. | -0.01 | -0.01 | -0.08 | -0.04 | 0.06 | -0.05 | -0.04 | 65. |
| 70. | -0.12 | -0.08 | -0.13 | -0.07 | 0.06 | -0.07 | -0.04 | 70. |
| 75. | -0.21 | -0.13 | -0.18 | -0.08 | 0.05 | -0.07 | -0.04 | 75. |
| 80. | -0.26 | -0.16 | -0.20 | -0.09 | 0.04 | -0.07 | -0.04 | 80. |
| 85. | -0.26 | -0.16 | -0.20 | -0.07 | 0.07 | -0.06 | -0.04 | 85. |
| 90. | -0.23 | -0.15 | -0.18 | -0.05 | 0.11 | -0.06 | -0.03 | 90. |
| 95. | -0.17 | -0.13 | -0.14 | -0.02 | 0.13 | -0.04 | -0.03 | 95. |
| 100. | -0.10 | -0.08 | -0.10 | 0.02 | 0.14 | -0.01 | -0.02 | 100. |
| 105. | -0.01 | -0.02 | -0.05 | 0.06 | 0.15 | 0.01 | -0.00 | 105. |
| 110. | 0.10 | 0.07 | 0.01 | 0.10 | 0.16 | 0.03 | -0.00 | 110. |
| 115. | 0.22 | 0.16 | 0.07 | 0.14 | 0.18 | 0.05 | -0.00 | 115. |
| 120. | 0.32 | 0.24 | 0.13 | 0.17 | 0.21 | 0.06 | 0.01 | 120. |
| 125. | 0.44 | 0.31 | 0.20 | 0.20 | 0.23 | 0.07 | 0.01 | 125. |
| 130. | 0.50 | 0.43 | 0.28 | 0.23 | 0.24 | 0.09 | 0.01 | 130. |
| 135. | 0.76 | 0.55 | 0.36 | 0.26 | 0.26 | 0.11 | 0.01 | 135. |
| 140. | 0.92 | 0.69 | 0.44 | 0.29 | 0.28 | 0.13 | 0.01 | 140. |
| 145. | 1.06 | 0.78 | 0.50 | 0.31 | 0.30 | 0.13 | 0.01 | 145. |
| 150. | 1.16 | 0.84 | 0.54 | 0.34 | 0.31 | 0.13 | 0.01 | 150. |
| 155. | 1.25 | 0.89 | 0.58 | 0.36 | 0.31 | 0.14 | 0.01 | 155. |
| 160. | 1.33 | 0.92 | 0.64 | 0.39 | 0.31 | 0.15 | 0.01 | 160. |
| 165. | 1.39 | 0.95 | 0.68 | 0.41 | 0.31 | 0.17 | 0.02 | 165. |
| 170. | 1.40 | 0.96 | 0.69 | 0.44 | 0.30 | 0.19 | 0.04 | 170. |
| 175. | 1.34 | 0.93 | 0.67 | 0.44 | 0.29 | 0.20 | 0.06 | 175. |
| 180. | 1.23 | 0.85 | 0.63 | 0.42 | 0.27 | 0.20 | 0.06 | 180. |
| 185. | 1.07 | 0.72 | 0.56 | 0.38 | 0.22 | 0.18 | 0.05 | 185. |
| 190. | 0.87 | 0.55 | 0.46 | 0.32 | 0.17 | 0.14 | 0.05 | 190. |
| 195. | 0.66 | 0.41 | 0.34 | 0.24 | 0.11 | 0.11 | 0.04 | 195. |
| 200. | 0.44 | 0.28 | 0.23 | 0.17 | 0.04 | 0.08 | 0.03 | 200. |
| 205. | 0.22 | 0.16 | 0.15 | 0.10 | -0.02 | 0.05 | 0.01 | 205. |
| 210. | 0.05 | 0.03 | 0.07 | 0.04 | -0.07 | 0.02 | -0.00 | 210. |
| 215. | -0.09 | -0.08 | 0.00 | -0.02 | -0.10 | -0.00 | -0.02 | 215. |
| 220. | -0.21 | -0.17 | -0.06 | -0.07 | -0.13 | -0.03 | -0.03 | 220. |
| 225. | -0.31 | -0.23 | -0.11 | -0.11 | -0.15 | -0.05 | -0.03 | 225. |
| 230. | -0.41 | -0.28 | -0.15 | -0.15 | -0.18 | -0.06 | -0.02 | 230. |
| 235. | -0.49 | -0.33 | -0.19 | -0.17 | -0.20 | -0.07 | -0.02 | 235. |
| 240. | -0.55 | -0.37 | -0.21 | -0.19 | -0.21 | -0.07 | -0.04 | 240. |
| 245. | -0.59 | -0.40 | -0.24 | -0.19 | -0.22 | -0.07 | -0.04 | 245. |
| 250. | -0.62 | -0.43 | -0.25 | -0.20 | -0.22 | -0.07 | -0.03 | 250. |
| 255. | -0.64 | -0.44 | -0.27 | -0.20 | -0.22 | -0.07 | -0.02 | 255. |
| 260. | -0.65 | -0.47 | -0.28 | -0.20 | -0.22 | -0.07 | -0.02 | 260. |
| 265. | -0.67 | -0.48 | -0.28 | -0.19 | -0.22 | -0.06 | -0.02 | 265. |
| 270. | -0.68 | -0.47 | -0.29 | -0.19 | -0.23 | -0.06 | -0.02 | 270. |
| 275. | -0.69 | -0.47 | -0.29 | -0.20 | -0.23 | -0.07 | -0.02 | 275. |
| 280. | -0.71 | -0.47 | -0.29 | -0.21 | -0.23 | -0.08 | -0.02 | 280. |
| 285. | -0.72 | -0.47 | -0.30 | -0.21 | -0.23 | -0.08 | -0.02 | 285. |
| 290. | -0.72 | -0.47 | -0.30 | -0.22 | -0.23 | -0.08 | -0.02 | 290. |
| 295. | -0.72 | -0.46 | -0.30 | -0.23 | -0.23 | -0.09 | -0.02 | 295. |
| 300. | -0.72 | -0.46 | -0.29 | -0.23 | -0.22 | -0.09 | -0.02 | 300. |
| 305. | -0.70 | -0.45 | -0.29 | -0.23 | -0.21 | -0.08 | -0.00 | 305. |
| 310. | -0.68 | -0.44 | -0.28 | -0.21 | -0.20 | -0.06 | 0.01 | 310. |
| 315. | -0.64 | -0.42 | -0.26 | -0.19 | -0.20 | -0.05 | 0.02 | 315. |
| 320. | -0.59 | -0.40 | -0.24 | -0.18 | -0.19 | -0.04 | 0.02 | 320. |
| 325. | -0.54 | -0.37 | -0.22 | -0.16 | -0.17 | -0.03 | 0.03 | 325. |
| 330. | -0.49 | -0.34 | -0.20 | -0.14 | -0.14 | -0.02 | 0.04 | 330. |
| 335. | -0.44 | -0.32 | -0.17 | -0.12 | -0.11 | -0.00 | 0.05 | 335. |
| 340. | -0.40 | -0.30 | -0.16 | -0.11 | -0.11 | -0.00 | 0.05 | 340. |
| 345. | -0.42 | -0.33 | -0.17 | -0.11 | -0.11 | -0.01 | 0.04 | 345. |
| 350. | -0.47 | -0.38 | -0.21 | -0.14 | -0.12 | -0.03 | 0.03 | 350. |
| 355. | -0.52 | -0.42 | -0.24 | -0.17 | -0.12 | -0.04 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 306 TCN= 8. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.27 | 0.17 | 0.18 | 0.14 | 0.06 | 0.04 | 0.01 | 0. |
| 5. | 0.33 | 0.22 | 0.20 | 0.15 | 0.08 | 0.04 | 0.00 | 5. |
| 10. | 0.49 | 0.28 | 0.25 | 0.20 | 0.11 | 0.05 | 0.00 | 10. |
| 15. | 0.57 | 0.36 | 0.24 | 0.22 | 0.14 | 0.03 | -0.01 | 15. |
| 20. | 0.63 | 0.35 | 0.28 | 0.22 | 0.14 | 0.03 | -0.02 | 20. |
| 25. | 0.70 | 0.33 | 0.30 | 0.22 | 0.16 | 0.03 | -0.02 | 25. |
| 30. | 0.79 | 0.44 | 0.34 | 0.24 | 0.21 | 0.02 | -0.03 | 30. |
| 35. | 0.84 | 0.51 | 0.38 | 0.25 | 0.24 | 0.00 | -0.04 | 35. |
| 40. | 0.89 | 0.50 | 0.36 | 0.23 | 0.25 | -0.01 | -0.05 | 40. |
| 45. | 0.85 | 0.43 | 0.31 | 0.19 | 0.24 | -0.03 | -0.06 | 45. |
| 50. | 0.77 | 0.31 | 0.20 | 0.12 | 0.21 | -0.06 | -0.08 | 50. |
| 55. | 0.62 | 0.14 | 0.06 | 0.01 | 0.16 | -0.10 | -0.09 | 55. |
| 60. | 0.33 | -0.03 | -0.09 | -0.10 | 0.10 | -0.12 | -0.09 | 60. |
| 65. | 0.03 | -0.19 | -0.24 | -0.20 | 0.04 | 0.14 | -0.10 | 65. |
| 70. | -0.19 | -0.38 | -0.37 | -0.30 | -0.02 | -0.17 | -0.10 | 70. |
| 75. | -0.36 | -0.57 | -0.46 | -0.36 | -0.07 | -0.17 | -0.10 | 75. |
| 80. | -0.47 | -0.66 | -0.50 | -0.39 | -0.09 | -0.17 | -0.09 | 80. |
| 85. | -0.52 | -0.66 | -0.51 | -0.40 | -0.09 | -0.16 | -0.08 | 85. |
| 90. | -0.51 | -0.63 | -0.48 | -0.39 | -0.08 | -0.17 | -0.08 | 90. |
| 95. | -0.46 | -0.60 | -0.45 | -0.35 | -0.06 | -0.15 | -0.07 | 95. |
| 100. | -0.37 | -0.53 | -0.39 | -0.30 | -0.05 | -0.13 | -0.06 | 100. |
| 105. | -0.20 | -0.39 | -0.29 | -0.23 | -0.03 | -0.09 | -0.05 | 105. |
| 110. | 0.02 | -0.20 | -0.14 | -0.13 | 0.05 | -0.06 | -0.04 | 110. |
| 115. | 0.23 | 0.00 | -0.03 | -0.04 | 0.12 | -0.03 | -0.02 | 115. |
| 120. | 0.37 | 0.19 | 0.04 | 0.01 | 0.15 | -0.01 | -0.01 | 120. |
| 125. | 0.46 | 0.30 | 0.07 | 0.05 | 0.17 | 0.02 | 0.01 | 125. |
| 130. | 0.52 | 0.29 | 0.10 | 0.09 | 0.19 | 0.04 | 0.02 | 130. |
| 135. | 0.56 | 0.34 | 0.14 | 0.13 | 0.20 | 0.06 | 0.03 | 135. |
| 140. | 0.66 | 0.56 | 0.20 | 0.17 | 0.22 | 0.07 | 0.04 | 140. |
| 145. | 0.72 | 0.61 | 0.25 | 0.20 | 0.23 | 0.09 | 0.06 | 145. |
| 150. | 0.76 | 0.58 | 0.31 | 0.22 | 0.24 | 0.10 | 0.06 | 150. |
| 155. | 0.77 | 0.54 | 0.35 | 0.25 | 0.25 | 0.12 | 0.06 | 155. |
| 160. | 0.75 | 0.51 | 0.38 | 0.28 | 0.26 | 0.13 | 0.07 | 160. |
| 165. | 0.72 | 0.54 | 0.41 | 0.30 | 0.25 | 0.15 | 0.08 | 165. |
| 170. | 0.70 | 0.60 | 0.42 | 0.31 | 0.26 | 0.18 | 0.10 | 170. |
| 175. | 0.68 | 0.61 | 0.44 | 0.35 | 0.29 | 0.16 | 0.07 | 175. |
| 180. | 0.70 | 0.64 | 0.48 | 0.38 | 0.23 | 0.13 | 0.04 | 180. |
| 185. | 0.85 | 0.72 | 0.51 | 0.38 | 0.20 | 0.17 | 0.07 | 185. |
| 190. | 1.06 | 0.84 | 0.63 | 0.47 | 0.28 | 0.21 | 0.09 | 190. |
| 195. | 1.18 | 0.92 | 0.66 | 0.49 | 0.26 | 0.21 | 0.10 | 195. |
| 200. | 1.00 | 0.81 | 0.59 | 0.42 | 0.21 | 0.18 | 0.10 | 200. |
| 205. | 0.72 | 0.64 | 0.47 | 0.33 | 0.14 | 0.16 | 0.09 | 205. |
| 210. | 0.51 | 0.49 | 0.36 | 0.27 | 0.11 | 0.15 | 0.08 | 210. |
| 215. | 0.30 | 0.34 | 0.26 | 0.21 | 0.06 | 0.14 | 0.08 | 215. |
| 220. | 0.10 | 0.21 | 0.18 | 0.15 | 0.02 | 0.12 | 0.07 | 220. |
| 225. | -0.08 | 0.08 | 0.10 | 0.08 | -0.02 | 0.10 | 0.07 | 225. |
| 230. | -0.27 | -0.05 | -0.00 | 0.00 | -0.06 | 0.07 | 0.06 | 230. |
| 235. | -0.44 | -0.17 | -0.10 | -0.07 | -0.12 | 0.04 | 0.05 | 234. |
| 240. | -0.65 | -0.29 | -0.20 | -0.14 | -0.19 | 0.01 | 0.03 | 240. |
| 245. | -0.80 | -0.40 | -0.28 | -0.21 | -0.26 | -0.03 | 0.01 | 245. |
| 250. | -0.93 | -0.51 | -0.34 | -0.25 | -0.31 | -0.07 | -0.02 | 250. |
| 255. | -1.02 | -0.59 | -0.38 | -0.28 | -0.34 | -0.10 | -0.04 | 255. |
| 260. | -1.10 | -0.66 | -0.42 | -0.30 | -0.35 | -0.11 | -0.04 | 260. |
| 265. | -1.16 | -0.69 | -0.44 | -0.32 | -0.36 | -0.11 | -0.03 | 265. |
| 270. | -1.20 | -0.70 | -0.45 | -0.33 | -0.37 | -0.11 | -0.03 | 270. |
| 275. | -1.23 | -0.69 | -0.46 | -0.34 | -0.38 | -0.11 | -0.03 | 275. |
| 280. | -1.23 | -0.68 | -0.47 | -0.35 | -0.38 | -0.11 | -0.03 | 280. |
| 285. | -1.21 | -0.68 | -0.47 | -0.35 | -0.38 | -0.11 | -0.03 | 285. |
| 290. | -1.19 | -0.68 | -0.46 | -0.35 | -0.36 | -0.11 | -0.02 | 290. |
| 295. | -1.15 | -0.68 | -0.45 | -0.33 | -0.35 | -0.09 | -0.02 | 295. |
| 300. | -1.10 | -0.66 | -0.44 | -0.31 | -0.33 | -0.08 | -0.01 | 300. |
| 305. | -1.04 | -0.63 | -0.41 | -0.28 | -0.32 | -0.07 | -0.01 | 305. |
| 310. | -0.96 | -0.58 | -0.37 | -0.24 | -0.30 | -0.07 | -0.01 | 310. |
| 315. | -0.84 | -0.52 | -0.32 | -0.19 | -0.27 | -0.05 | -0.01 | 315. |
| 320. | -0.71 | -0.43 | -0.26 | -0.14 | -0.23 | -0.04 | -0.01 | 320. |
| 325. | -0.57 | -0.33 | -0.18 | -0.09 | -0.19 | -0.02 | 0.00 | 325. |
| 330. | -0.45 | -0.22 | -0.11 | -0.04 | -0.14 | -0.01 | 0.01 | 330. |
| 335. | -0.32 | -0.11 | -0.04 | 0.00 | -0.09 | 0.01 | 0.01 | 335. |
| 340. | -0.13 | -0.01 | 0.03 | 0.04 | -0.05 | 0.03 | 0.01 | 340. |
| 345. | 0.05 | 0.08 | 0.11 | 0.10 | -0.01 | 0.04 | 0.02 | 345. |
| 350. | 0.18 | 0.17 | 0.17 | 0.14 | 0.02 | 0.05 | 0.02 | 350. |
| 355. | 0.28 | 0.19 | 0.18 | 0.12 | 0.04 | 0.04 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 306 ICN= 0. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.950 | 7.150 | 10.400 | DEG. |
| 0. | 0.98 | 0.58 | 0.40 | 0.20 | 0.18 | 0.13 | 0.07 | 0. |
| 5. | 0.97 | 0.62 | 0.36 | 0.22 | 0.19 | 0.11 | 0.07 | 5. |
| 10. | 0.94 | 0.64 | 0.34 | 0.23 | 0.20 | 0.13 | 0.06 | 10. |
| 15. | 0.91 | 0.62 | 0.33 | 0.23 | 0.19 | 0.09 | 0.06 | 15. |
| 20. | 0.92 | 0.59 | 0.34 | 0.27 | 0.18 | 0.07 | 0.04 | 20. |
| 25. | 0.96 | 0.48 | 0.35 | 0.32 | 0.18 | 0.05 | 0.03 | 25. |
| 30. | 1.03 | 0.66 | 0.37 | 0.35 | 0.19 | 0.06 | 0.00 | 30. |
| 35. | 1.07 | 0.76 | 0.39 | 0.39 | 0.20 | 0.04 | -0.01 | 35. |
| 40. | 1.02 | 0.74 | 0.40 | 0.36 | 0.20 | 0.02 | -0.01 | 40. |
| 45. | 0.88 | 0.69 | 0.36 | 0.34 | 0.16 | -0.04 | -0.03 | 45. |
| 50. | 0.61 | 0.51 | 0.23 | 0.24 | 0.10 | -0.09 | -0.06 | 50. |
| 55. | 0.21 | 0.27 | 0.02 | 0.16 | 0.02 | -0.15 | -0.08 | 55. |
| 60. | -0.25 | -0.03 | -0.24 | 0.03 | -0.07 | -0.21 | -0.09 | 60. |
| 65. | -0.70 | -0.40 | -0.49 | -0.14 | -0.15 | -0.27 | -0.12 | 65. |
| 70. | -1.16 | -0.73 | -0.69 | -0.25 | -0.23 | -0.31 | -0.13 | 70. |
| 75. | -1.59 | -0.97 | -0.84 | -0.33 | -0.27 | -0.36 | -0.13 | 75. |
| 80. | -1.90 | -1.10 | -0.95 | -0.39 | -0.30 | -0.40 | -0.13 | 80. |
| 85. | -2.06 | -1.19 | -1.07 | -0.45 | -0.31 | -0.41 | -0.13 | 85. |
| 90. | -2.05 | -1.18 | -1.04 | -0.44 | -0.30 | -0.40 | -0.13 | 90. |
| 95. | -1.88 | -0.94 | -0.91 | -0.36 | -0.27 | -0.35 | -0.12 | 95. |
| 100. | -1.66 | -0.74 | -0.78 | -0.27 | -0.23 | -0.30 | -0.11 | 100. |
| 105. | -1.46 | -0.57 | -0.70 | -0.19 | -0.20 | -0.25 | -0.10 | 105. |
| 110. | -1.31 | -0.44 | -0.62 | -0.15 | -0.17 | -0.25 | -0.10 | 110. |
| 115. | -1.22 | -0.33 | -0.55 | -0.14 | -0.13 | -0.22 | -0.09 | 115. |
| 120. | -1.19 | -0.38 | -0.55 | -0.12 | -0.07 | -0.19 | -0.06 | 120. |
| 125. | -1.19 | -0.36 | -0.45 | -0.01 | -0.02 | -0.12 | -0.03 | 125. |
| 130. | -0.89 | 0.12 | -0.12 | 0.19 | 0.10 | -0.05 | -0.01 | 130. |
| 135. | 0.63 | 0.76 | 0.33 | 0.42 | 0.25 | -0.00 | -0.00 | 135. |
| 140. | 1.31 | 1.07 | 0.61 | 0.57 | 0.39 | 0.07 | 0.03 | 140. |
| 145. | 1.50 | 1.13 | 0.73 | 0.65 | 0.50 | 0.14 | 0.07 | 145. |
| 150. | 1.56 | 1.09 | 0.79 | 0.68 | 0.59 | 0.20 | 0.10 | 150. |
| 155. | 1.74 | 1.11 | 0.85 | 0.74 | 0.63 | 0.24 | 0.11 | 155. |
| 160. | 1.88 | 1.17 | 0.90 | 0.77 | 0.62 | 0.24 | 0.11 | 160. |
| 165. | 1.89 | 1.25 | 0.92 | 0.76 | 0.58 | 0.27 | 0.11 | 165. |
| 170. | 1.85 | 1.25 | 0.91 | 0.70 | 0.53 | 0.27 | 0.09 | 170. |
| 175. | 1.75 | 1.13 | 0.85 | 0.63 | 0.44 | 0.25 | 0.07 | 175. |
| 180. | 1.58 | 0.96 | 0.75 | 0.55 | 0.35 | 0.21 | 0.05 | 180. |
| 185. | 1.33 | 0.79 | 0.64 | 0.46 | 0.28 | 0.19 | 0.04 | 185. |
| 190. | 1.04 | 0.61 | 0.50 | 0.34 | 0.18 | 0.15 | 0.04 | 190. |
| 195. | 0.74 | 0.44 | 0.39 | 0.22 | 0.12 | 0.13 | 0.03 | 195. |
| 200. | 0.49 | 0.26 | 0.26 | 0.13 | 0.08 | 0.12 | 0.04 | 200. |
| 205. | 0.29 | 0.07 | 0.17 | 0.06 | 0.06 | 0.11 | 0.04 | 205. |
| 210. | 0.12 | -0.07 | 0.10 | 0.01 | 0.01 | 0.10 | 0.05 | 210. |
| 215. | 0.00 | -0.13 | 0.03 | -0.04 | -0.02 | 0.09 | 0.04 | 215. |
| 220. | -0.08 | -0.19 | -0.01 | -0.07 | -0.03 | 0.09 | 0.06 | 220. |
| 225. | -0.14 | -0.22 | -0.04 | -0.11 | -0.02 | 0.09 | 0.06 | 225. |
| 230. | -0.19 | -0.24 | -0.05 | -0.14 | -0.05 | 0.09 | 0.06 | 230. |
| 235. | -0.22 | -0.29 | -0.08 | -0.17 | -0.08 | 0.09 | 0.05 | 235. |
| 240. | -0.25 | -0.29 | -0.05 | -0.20 | -0.10 | 0.09 | 0.04 | 240. |
| 245. | -0.26 | -0.29 | -0.04 | -0.23 | -0.13 | 0.09 | 0.03 | 245. |
| 250. | -0.29 | -0.29 | -0.04 | -0.27 | -0.16 | 0.05 | 0.01 | 250. |
| 255. | -0.38 | -0.34 | -0.07 | -0.31 | -0.20 | 0.05 | -0.01 | 255. |
| 260. | -0.54 | -0.49 | -0.15 | -0.37 | -0.26 | 0.02 | -0.03 | 260. |
| 265. | -0.79 | -0.68 | -0.25 | -0.46 | -0.34 | -0.03 | -0.05 | 265. |
| 270. | -1.05 | -0.87 | -0.38 | -0.55 | -0.40 | -0.07 | -0.07 | 270. |
| 275. | -1.29 | -1.03 | -0.50 | -0.62 | -0.45 | -0.10 | -0.08 | 275. |
| 280. | -1.37 | -1.12 | -0.54 | -0.65 | -0.48 | -0.11 | -0.07 | 280. |
| 285. | -1.37 | -1.14 | -0.53 | -0.65 | -0.49 | -0.11 | -0.06 | 285. |
| 290. | -1.33 | -1.11 | -0.50 | -0.64 | -0.46 | -0.09 | -0.04 | 290. |
| 295. | -1.23 | -1.03 | -0.48 | -0.67 | -0.42 | -0.08 | -0.02 | 295. |
| 300. | -1.11 | -0.92 | -0.44 | -0.58 | -0.36 | -0.05 | -0.01 | 300. |
| 305. | -0.94 | -0.82 | -0.38 | -0.52 | -0.31 | -0.03 | 0.00 | 305. |
| 310. | -0.74 | -0.71 | -0.31 | -0.45 | -0.25 | 0.00 | 0.01 | 310. |
| 315. | -0.51 | -0.56 | -0.23 | -0.37 | -0.20 | 0.03 | 0.02 | 315. |
| 320. | -0.25 | -0.37 | -0.15 | -0.28 | -0.15 | 0.05 | 0.03 | 320. |
| 325. | 0.05 | -0.18 | -0.07 | -0.20 | -0.10 | 0.09 | 0.04 | 325. |
| 330. | 0.27 | 0.02 | 0.03 | -0.12 | -0.03 | 0.10 | 0.04 | 330. |
| 335. | 0.52 | 0.21 | 0.18 | -0.02 | 0.02 | 0.12 | 0.04 | 335. |
| 340. | 0.79 | 0.36 | 0.30 | 0.08 | 0.08 | 0.13 | 0.05 | 340. |
| 345. | 0.97 | 0.50 | 0.38 | 0.17 | 0.12 | 0.14 | 0.05 | 345. |
| 350. | 1.05 | 0.57 | 0.41 | 0.19 | 0.16 | 0.15 | 0.07 | 350. |
| 355. | 1.00 | 0.57 | 0.42 | 0.19 | 0.18 | 0.15 | 0.08 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 306 TCN= 8. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 1.79 | 1.18 | 0.79 | 0.53 | 0.45 | 0.21 | 0.06 | 0. |
| 5. | 1.51 | 0.98 | 0.63 | 0.46 | 0.37 | 0.19 | 0.05 | 5. |
| 10. | 1.31 | 0.81 | 0.50 | 0.38 | 0.31 | 0.15 | 0.05 | 10. |
| 15. | 1.12 | 0.67 | 0.39 | 0.32 | 0.25 | 0.12 | 0.05 | 15. |
| 20. | 0.99 | 0.57 | 0.33 | 0.28 | 0.19 | 0.10 | 0.05 | 20. |
| 25. | 0.93 | 0.51 | 0.32 | 0.27 | 0.16 | 0.09 | 0.04 | 25. |
| 30. | 0.92 | 0.52 | 0.36 | 0.25 | 0.17 | 0.10 | 0.04 | 30. |
| 35. | 0.96 | 0.51 | 0.39 | 0.24 | 0.20 | 0.10 | 0.04 | 35. |
| 40. | 0.95 | 0.45 | 0.39 | 0.24 | 0.20 | 0.07 | 0.03 | 40. |
| 45. | 0.81 | 0.32 | 0.36 | 0.22 | 0.17 | 0.02 | 0.01 | 45. |
| 50. | 0.54 | 0.18 | 0.27 | 0.15 | 0.09 | -0.04 | -0.01 | 50. |
| 55. | 0.16 | -0.07 | 0.02 | 0.02 | -0.11 | -0.09 | -0.03 | 55. |
| 60. | -0.29 | -0.39 | -0.31 | -0.16 | -0.27 | -0.13 | -0.05 | 60. |
| 65. | -0.86 | -0.75 | -0.56 | -0.35 | -0.46 | -0.20 | -0.08 | 65. |
| 70. | -1.42 | -1.14 | -0.89 | -0.52 | -0.61 | -0.35 | -0.09 | 70. |
| 75. | -1.83 | -1.43 | -1.24 | -0.67 | -0.74 | -0.41 | -0.10 | 75. |
| 80. | -2.17 | -1.56 | -1.49 | -0.79 | -0.83 | -0.44 | -0.10 | 80. |
| 85. | -2.38 | -1.54 | -1.58 | -0.83 | -0.85 | -0.44 | -0.09 | 85. |
| 90. | -2.46 | -1.57 | -1.61 | -0.82 | -0.84 | -0.41 | -0.08 | 90. |
| 95. | -2.47 | -1.60 | -1.60 | -0.80 | -0.78 | -0.35 | -0.05 | 95. |
| 100. | -2.42 | -1.55 | -1.51 | -0.75 | -0.67 | -0.29 | -0.04 | 100. |
| 105. | -1.76 | -1.16 | -1.09 | -0.59 | -0.52 | -0.23 | -0.05 | 105. |
| 110. | -0.92 | -0.86 | -0.66 | -0.42 | -0.35 | -0.18 | -0.05 | 110. |
| 115. | -0.58 | -0.77 | -0.45 | -0.36 | -0.27 | -0.14 | -0.03 | 115. |
| 120. | -0.51 | -0.81 | -0.39 | -0.33 | -0.24 | -0.10 | -0.02 | 120. |
| 125. | -0.54 | -0.74 | -0.40 | -0.31 | -0.21 | -0.07 | -0.02 | 125. |
| 130. | -0.51 | -0.64 | -0.39 | -0.29 | -0.18 | -0.04 | -0.02 | 130. |
| 135. | -0.37 | -0.52 | -0.29 | -0.25 | -0.15 | -0.00 | -0.02 | 135. |
| 140. | -0.19 | -0.40 | -0.18 | -0.19 | -0.10 | 0.04 | -0.01 | 140. |
| 145. | -0.01 | -0.26 | -0.08 | -0.13 | -0.05 | 0.07 | 0.00 | 145. |
| 150. | 0.18 | -0.11 | 0.03 | -0.07 | 0.02 | 0.10 | 0.02 | 150. |
| 155. | 0.40 | 0.06 | 0.15 | -0.01 | 0.10 | 0.14 | 0.03 | 155. |
| 160. | 0.62 | 0.22 | 0.26 | 0.06 | 0.16 | 0.17 | 0.03 | 160. |
| 165. | 0.81 | 0.37 | 0.33 | 0.12 | 0.21 | 0.18 | 0.04 | 165. |
| 170. | 0.93 | 0.48 | 0.39 | 0.16 | 0.23 | 0.18 | 0.04 | 170. |
| 175. | 0.97 | 0.55 | 0.41 | 0.17 | 0.24 | 0.15 | 0.04 | 175. |
| 180. | 0.89 | 0.55 | 0.38 | 0.16 | 0.22 | 0.14 | 0.03 | 180. |
| 185. | 0.73 | 0.49 | 0.31 | 0.14 | 0.18 | 0.11 | 0.02 | 185. |
| 190. | 0.52 | 0.38 | 0.22 | 0.11 | 0.13 | 0.09 | 0.01 | 190. |
| 195. | 0.29 | 0.20 | 0.14 | 0.07 | 0.09 | 0.04 | 0.01 | 195. |
| 200. | 0.10 | 0.20 | 0.06 | 0.03 | 0.05 | 0.03 | 0.00 | 200. |
| 205. | -0.06 | 0.11 | 0.02 | 0.00 | 0.03 | 0.02 | -0.00 | 205. |
| 210. | -0.19 | 0.03 | -0.01 | -0.02 | 0.01 | 0.01 | -0.01 | 210. |
| 215. | -0.29 | -0.03 | -0.04 | -0.03 | -0.01 | 0.03 | -0.02 | 215. |
| 220. | -0.34 | -0.06 | -0.05 | -0.04 | -0.01 | -0.00 | -0.01 | 220. |
| 225. | -0.37 | -0.07 | -0.05 | -0.04 | -0.01 | 0.00 | -0.00 | 225. |
| 230. | -0.59 | -0.07 | -0.02 | -0.03 | -0.01 | 0.01 | -0.00 | 230. |
| 235. | -0.87 | -0.04 | 0.02 | -0.02 | 0.01 | 0.02 | -0.00 | 235. |
| 240. | -1.00 | -0.01 | 0.07 | 0.01 | 0.03 | 0.02 | 0.00 | 240. |
| 245. | -0.61 | 0.04 | 0.11 | 0.04 | 0.05 | 0.03 | 0.00 | 245. |
| 250. | -0.19 | 0.08 | 0.15 | 0.07 | 0.08 | 0.03 | 0.01 | 250. |
| 255. | -0.09 | 0.12 | 0.19 | 0.10 | 0.10 | 0.02 | 0.01 | 255. |
| 260. | -0.10 | 0.17 | 0.22 | 0.11 | 0.12 | 0.00 | 0.01 | 260. |
| 265. | -0.09 | 0.20 | 0.24 | 0.13 | 0.12 | -0.00 | 0.01 | 265. |
| 270. | -0.15 | 0.17 | 0.22 | 0.14 | 0.09 | -0.03 | -0.00 | 270. |
| 275. | -0.32 | 0.05 | 0.13 | 0.08 | 0.03 | -0.02 | -0.01 | 275. |
| 280. | -0.58 | -0.10 | -0.04 | -0.03 | -0.05 | -0.06 | -0.02 | 280. |
| 285. | -0.78 | -0.23 | -0.20 | -0.09 | -0.11 | -0.10 | -0.04 | 285. |
| 290. | -0.83 | -0.28 | -0.27 | -0.10 | -0.12 | -0.11 | -0.04 | 290. |
| 295. | -0.74 | -0.27 | -0.21 | -0.09 | -0.10 | -0.09 | -0.03 | 295. |
| 300. | -0.56 | -0.21 | -0.13 | -0.06 | -0.05 | -0.05 | -0.02 | 300. |
| 305. | -0.36 | -0.11 | -0.02 | 0.01 | 0.01 | -0.02 | -0.00 | 305. |
| 310. | -0.10 | 0.02 | 0.12 | 0.08 | 0.08 | 0.02 | 0.01 | 310. |
| 315. | 0.21 | 0.18 | 0.2. | 0.16 | 0.16 | 0.05 | 0.02 | 315. |
| 320. | 0.56 | 0.35 | 0.39 | 0.23 | 0.24 | 0.11 | 0.03 | 320. |
| 325. | 0.90 | 0.35 | 0.54 | 0.31 | 0.32 | 0.15 | 0.03 | 325. |
| 330. | 1.24 | 0.79 | 0.73 | 0.41 | 0.40 | 0.18 | 0.04 | 330. |
| 335. | 1.58 | 1.03 | 0.89 | 0.50 | 0.49 | 0.23 | 0.05 | 335. |
| 340. | 1.88 | 1.22 | 1.01 | 0.57 | 0.55 | 0.26 | 0.06 | 340. |
| 345. | 2.03 | 1.32 | 1.06 | 0.61 | 0.58 | 0.27 | 0.06 | 345. |
| 350. | 2.07 | 1.34 | 1.03 | 0.61 | 0.56 | 0.26 | 0.05 | 350. |
| 355. | 1.98 | 1.29 | 0.92 | 0.59 | 0.50 | 0 | 0.05 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 306 TCN= 8. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 3.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 2.52 | 1.65 | 1.09 | 0.75 | 0.41 | 0.27 | 0.09 | 0. |
| 5. | 1.89 | 1.36 | 0.94 | 0.61 | 0.46 | 0.22 | 0.09 | 5. |
| 10. | 1.50 | 1.12 | 0.74 | 0.51 | 0.48 | 0.19 | 0.08 | 10. |
| 15. | 1.26 | 0.89 | 0.62 | 0.42 | 0.49 | 0.13 | 0.07 | 15. |
| 20. | 1.00 | 0.73 | 0.52 | 0.32 | 0.50 | 0.09 | 0.05 | 20. |
| 25. | 0.85 | 0.64 | 0.47 | 0.30 | 0.51 | 0.04 | 0.03 | 25. |
| 30. | 0.80 | 0.69 | 0.51 | 0.31 | 0.56 | 0.03 | 0.03 | 30. |
| 35. | 0.77 | 0.67 | 0.47 | 0.33 | 0.60 | 0.02 | 0.01 | 35. |
| 40. | 0.69 | 0.60 | 0.40 | 0.33 | 0.57 | -0.00 | -0.02 | 40. |
| 45. | 0.51 | 0.43 | 0.27 | 0.28 | 0.49 | -0.04 | -0.04 | 45. |
| 50. | 0.23 | 0.19 | 0.06 | 0.16 | 0.37 | -0.11 | -0.07 | 50. |
| 55. | -0.14 | -0.12 | 0.24 | -0.09 | 0.26 | -0.21 | -0.11 | 55. |
| 60. | -0.72 | -0.55 | -0.10 | -0.36 | 0.12 | -0.30 | -0.14 | 60. |
| 65. | -1.28 | -1.05 | -0.52 | -0.63 | -0.11 | -0.38 | -0.17 | 65. |
| 70. | -1.92 | -1.55 | -0.96 | -0.92 | -0.42 | -0.45 | -0.19 | 70. |
| 75. | -2.50 | -1.97 | -1.33 | -1.12 | -0.62 | -0.52 | -0.20 | 75. |
| 80. | -2.92 | -2.27 | -1.59 | -1.29 | -0.69 | -0.55 | -0.20 | 80. |
| 85. | -3.24 | -2.56 | -1.75 | -1.39 | -0.67 | -0.55 | -0.17 | 85. |
| 90. | -3.51 | -2.70 | -1.77 | -1.35 | -0.58 | -0.50 | -0.14 | 90. |
| 95. | -3.13 | -2.28 | -1.39 | -1.08 | -0.48 | -0.41 | -0.12 | 95. |
| 100. | -2.24 | -1.51 | -0.92 | -0.93 | -0.37 | -0.35 | -0.13 | 100. |
| 105. | -1.83 | -1.23 | -0.70 | -0.69 | -0.29 | -0.34 | -0.13 | 105. |
| 110. | -1.77 | -1.19 | -0.67 | -0.65 | -0.14 | -0.31 | -0.11 | 110. |
| 115. | -1.80 | -1.21 | -0.67 | -0.65 | -0.10 | -0.28 | -0.09 | 115. |
| 120. | -1.74 | -1.21 | -0.65 | -0.62 | -0.09 | -0.25 | -0.07 | 120. |
| 125. | -1.60 | -1.08 | -0.63 | -0.56 | -0.10 | -0.22 | -0.06 | 125. |
| 130. | -1.42 | -0.97 | -0.56 | -0.49 | -0.11 | -0.19 | -0.05 | 130. |
| 135. | -1.21 | -0.68 | -0.47 | -0.43 | -0.08 | -0.15 | -0.03 | 135. |
| 140. | -0.98 | -0.54 | -0.37 | -0.36 | -0.04 | -0.11 | -0.02 | 140. |
| 145. | -0.74 | -0.39 | -0.26 | -0.27 | 0.00 | -0.07 | 0.00 | 145. |
| 150. | -0.49 | -0.23 | -0.15 | -0.16 | 0.05 | -0.01 | 0.02 | 150. |
| 155. | -0.21 | -0.04 | -0.02 | -0.05 | 0.09 | 0.04 | 0.04 | 155. |
| 160. | 0.07 | 0.14 | 0.11 | 0.06 | 0.09 | 0.09 | 0.05 | 160. |
| 165. | 0.34 | 0.31 | 0.27 | 0.14 | 0.12 | 0.12 | 0.06 | 165. |
| 170. | 0.55 | 0.44 | 0.28 | 0.20 | 0.18 | 0.13 | 0.06 | 170. |
| 175. | 0.67 | 0.50 | 0.30 | 0.22 | 0.22 | 0.13 | 0.05 | 175. |
| 180. | 0.70 | 0.47 | 0.28 | 0.20 | 0.20 | 0.11 | 0.04 | 180. |
| 185. | 0.62 | 0.39 | 0.23 | 0.16 | 0.14 | 0.10 | 0.04 | 185. |
| 190. | 0.47 | 0.28 | 0.15 | 0.11 | 0.06 | 0.08 | 0.03 | 190. |
| 195. | 0.30 | 0.16 | 0.06 | 0.06 | -0.02 | 0.07 | 0.02 | 195. |
| 200. | 0.11 | 0.04 | -0.02 | 0.04 | -0.10 | 0.05 | 0.02 | 200. |
| 205. | -0.06 | -0.05 | -0.10 | 0.03 | -0.16 | 0.05 | 0.02 | 205. |
| 210. | -0.18 | -0.12 | -0.14 | -0.01 | -0.21 | 0.05 | 0.01 | 210. |
| 215. | -0.28 | -0.17 | -0.18 | -0.05 | -0.26 | 0.05 | 0.01 | 215. |
| 220. | -0.34 | -0.20 | -0.21 | -0.06 | -0.30 | 0.05 | 0.02 | 220. |
| 225. | -0.36 | -0.20 | -0.22 | -0.06 | -0.32 | 0.06 | 0.03 | 225. |
| 230. | -0.32 | -0.17 | -0.21 | -0.04 | -0.32 | 0.07 | 0.03 | 230. |
| 235. | -0.26 | -0.12 | -0.18 | 0.00 | -0.31 | 0.08 | 0.04 | 235. |
| 240. | -0.16 | 0.06 | -0.14 | 0.04 | -0.29 | 0.10 | 0.04 | 240. |
| 245. | -0.01 | 0.01 | -0.10 | 0.09 | -0.28 | 0.11 | 0.04 | 245. |
| 250. | 0.12 | 0.08 | -0.05 | 0.13 | -0.27 | 0.11 | 0.04 | 250. |
| 255. | 0.18 | 0.14 | -0.01 | 0.17 | -0.26 | 0.11 | 0.03 | 255. |
| 260. | -0.02 | 0.20 | 0.04 | 0.20 | -0.26 | 0.11 | 0.02 | 260. |
| 265. | -0.25 | 0.25 | 0.08 | 0.22 | -0.26 | 0.11 | 0.02 | 265. |
| 270. | -0.05 | 0.27 | 0.11 | 0.24 | -0.25 | 0.13 | 0.03 | 270. |
| 275. | 0.34 | 0.24 | 0.12 | 0.23 | -0.25 | 0.13 | 0.03 | 275. |
| 280. | 0.15 | 0.06 | 0.01 | 0.14 | -0.26 | 0.09 | 0.01 | 280. |
| 285. | -0.14 | -0.14 | -0.14 | 0.03 | -0.32 | 0.05 | -0.01 | 285. |
| 290. | -0.32 | -0.27 | -0.24 | -0.04 | -0.36 | 0.04 | -0.02 | 290. |
| 295. | -0.33 | -0.24 | -0.23 | -0.03 | -0.30 | 0.05 | 0.00 | 295. |
| 300. | -0.17 | -0.10 | -0.15 | 0.03 | -0.20 | 0.08 | 0.02 | 300. |
| 305. | 0.11 | 0.11 | -0.01 | 0.13 | -0.09 | 0.11 | 0.04 | 305. |
| 310. | 0.44 | 0.38 | 0.13 | 0.24 | 0.01 | 0.15 | 0.06 | 310. |
| 315. | 0.80 | 0.64 | 0.29 | 0.37 | 0.12 | 0.19 | 0.07 | 315. |
| 320. | 1.20 | 0.90 | 0.46 | 0.50 | 0.24 | 0.22 | 0.07 | 320. |
| 325. | 1.63 | 1.15 | 0.69 | 0.64 | 0.36 | 0.26 | 0.08 | 325. |
| 330. | 2.08 | 1.41 | 0.90 | 0.76 | 0.47 | 0.30 | 0.10 | 330. |
| 335. | 2.59 | 1.67 | 1.09 | 0.87 | 0.45 | 0.32 | 0.11 | 335. |
| 340. | 3.08 | 1.92 | 1.22 | 0.95 | 0.57 | 0.34 | 0.12 | 340. |
| 345. | 3.43 | 2.03 | 1.29 | 0.97 | 0.51 | 0.34 | 0.12 | 345. |
| 350. | 3.49 | 1.98 | 1.26 | 0.92 | 0.40 | 0.31 | 0.10 | 350. |
| 355. | 3.16 | 1.82 | 1.16 | 0.84 | 0.34 | 0.29 | 0.09 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 306 TCN= R. C.R.= 48.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 3.48 | 1.42 | 0.84 | 0.64 | 0.37 | 0.20 | 0.01 | 0. |
| 5. | 2.13 | 1.32 | 0.65 | 0.42 | 0.30 | 0.15 | -0.02 | 5. |
| 10. | 1.38 | 1.04 | 0.48 | 0.38 | 0.25 | 0.11 | -0.03 | 10. |
| 15. | 1.02 | 0.42 | 0.32 | 0.27 | 0.21 | 0.04 | -0.03 | 15. |
| 20. | 0.84 | 0.68 | 0.24 | 0.22 | 0.19 | -0.01 | -0.04 | 20. |
| 25. | 0.66 | 0.62 | 0.24 | 0.22 | 0.19 | -0.05 | -0.07 | 25. |
| 30. | 0.58 | 0.60 | 0.22 | 0.25 | 0.20 | -0.07 | -0.08 | 30. |
| 35. | 0.57 | 0.62 | 0.32 | 0.24 | 0.21 | -0.09 | -0.09 | 35. |
| 40. | 0.49 | 0.66 | 0.61 | 0.24 | 0.20 | -0.14 | -0.12 | 40. |
| 45. | 0.25 | 0.64 | 1.09 | 0.16 | 0.14 | -0.22 | -0.15 | 45. |
| 50. | -0.10 | 0.45 | 1.43 | 0.03 | 0.34 | -0.30 | -0.17 | 50. |
| 55. | -0.54 | 0.06 | 1.43 | -0.13 | -0.09 | -0.37 | -0.19 | 55. |
| 60. | -1.11 | -0.41 | 1.13 | -0.32 | -0.23 | -0.45 | -0.22 | 60. |
| 65. | -1.79 | -0.93 | 0.56 | -0.52 | -0.37 | -0.49 | -0.22 | 65. |
| 70. | -2.48 | -1.42 | -0.19 | -0.78 | -0.49 | -0.59 | -0.23 | 70. |
| 75. | -3.09 | -1.91 | -0.95 | -1.02 | -0.58 | -0.63 | -0.24 | 75. |
| 80. | -3.60 | -2.34 | -1.50 | -1.15 | -0.63 | -0.62 | -0.21 | 80. |
| 85. | -3.70 | -2.33 | -1.41 | -1.05 | -0.57 | -0.59 | -0.18 | 85. |
| 90. | -2.95 | -1.77 | -0.76 | -0.86 | -0.48 | -0.53 | -0.16 | 90. |
| 95. | -2.56 | -1.44 | -0.27 | -0.73 | -0.40 | -0.47 | -0.14 | 95. |
| 100. | -2.57 | -1.42 | -0.30 | -0.73 | -0.35 | -0.44 | -0.13 | 100. |
| 105. | -2.67 | -1.47 | -0.58 | -0.73 | -0.33 | -0.41 | -0.14 | 105. |
| 110. | -2.65 | -1.41 | -0.85 | -0.73 | -0.31 | -0.39 | -0.11 | 110. |
| 115. | -2.57 | -1.51 | -1.04 | -0.70 | -0.30 | -0.35 | -0.06 | 115. |
| 120. | -2.43 | -1.40 | -1.06 | -0.65 | -0.27 | -0.34 | -0.03 | 120. |
| 125. | -2.24 | -1.24 | -0.98 | -0.59 | -0.27 | -0.32 | -0.03 | 125. |
| 130. | -2.01 | -1.09 | -0.86 | -0.53 | -0.23 | -0.29 | -0.02 | 130. |
| 135. | -1.75 | -0.95 | -0.79 | -0.44 | -0.19 | -0.24 | 0.00 | 135. |
| 140. | -1.50 | -0.80 | -0.70 | -0.41 | -0.15 | -0.19 | 0.03 | 140. |
| 145. | -1.27 | -0.64 | -0.59 | -0.33 | -0.10 | -0.13 | 0.03 | 145. |
| 150. | -1.02 | -0.46 | -0.47 | -0.23 | -0.05 | -0.08 | 0.01 | 150. |
| 155. | -0.72 | -0.28 | -0.35 | -0.13 | 0.01 | -0.07 | 0.02 | 155. |
| 160. | -0.39 | -0.10 | -0.24 | -0.02 | 0.06 | 0.03 | 0.04 | 160. |
| 165. | -0.09 | 0.06 | -0.14 | 0.08 | 0.10 | 0.09 | 0.06 | 165. |
| 170. | 0.15 | 0.19 | -0.05 | 0.15 | 0.13 | 0.11 | 0.08 | 170. |
| 175. | 0.30 | 0.26 | 0.00 | 0.17 | 0.15 | 0.13 | 0.08 | 175. |
| 180. | 0.36 | 0.26 | 0.00 | 0.17 | 0.14 | 0.13 | 0.07 | 180. |
| 185. | 0.35 | 0.22 | -0.04 | 0.15 | 0.11 | 0.13 | 0.06 | 185. |
| 190. | 0.27 | 0.15 | -0.10 | 0.12 | 0.08 | 0.14 | 0.06 | 190. |
| 195. | 0.15 | 0.07 | -0.15 | 0.08 | 0.05 | 0.13 | 0.06 | 195. |
| 200. | 0.01 | -0.03 | -0.21 | 0.03 | 0.01 | 0.13 | 0.06 | 200. |
| 205. | -0.15 | -0.12 | -0.27 | -0.01 | -0.02 | 0.12 | 0.07 | 205. |
| 210. | -0.29 | -0.21 | -0.31 | -0.04 | -0.05 | 0.12 | 0.05 | 210. |
| 215. | -0.41 | -0.29 | -0.35 | -0.06 | -0.07 | 0.11 | 0.05 | 215. |
| 220. | -0.46 | -0.36 | -0.36 | -0.06 | -0.08 | 0.12 | 0.06 | 220. |
| 225. | -0.47 | -0.36 | -0.34 | -0.05 | -0.08 | 0.14 | 0.08 | 225. |
| 230. | -0.41 | -0.32 | -0.34 | -0.04 | -0.07 | 0.16 | 0.08 | 230. |
| 235. | -0.32 | -0.26 | -0.30 | -0.01 | -0.04 | 0.17 | 0.09 | 235. |
| 240. | -0.19 | -0.17 | -0.25 | 0.02 | -0.04 | 0.22 | 0.10 | 240. |
| 245. | -0.05 | -0.08 | -0.19 | 0.04 | -0.02 | 0.24 | 0.11 | 245. |
| 250. | 0.10 | 0.01 | -0.12 | 0.10 | -0.00 | 0.25 | 0.11 | 250. |
| 255. | 0.25 | 0.10 | -0.06 | 0.16 | 0.01 | 0.25 | 0.11 | 255. |
| 260. | 0.40 | 0.17 | 0.00 | 0.21 | 0.03 | 0.25 | 0.12 | 260. |
| 265. | 0.53 | 0.24 | 0.06 | 0.24 | 0.05 | 0.27 | 0.12 | 265. |
| 270. | 0.63 | 0.32 | 0.11 | 0.26 | 0.07 | 0.29 | 0.11 | 270. |
| 275. | 0.70 | 0.41 | 0.13 | 0.29 | 0.08 | 0.29 | 0.11 | 275. |
| 280. | 0.63 | 0.40 | 0.12 | 0.27 | 0.08 | 0.25 | 0.10 | 280. |
| 285. | 0.39 | 0.26 | -0.01 | 0.16 | 0.01 | 0.7 | 0.08 | 285. |
| 290. | 0.04 | 0.08 | -0.13 | 0.07 | -0.05 | 0.14 | 0.06 | 290. |
| 295. | -0.04 | -0.04 | -0.18 | 0.02 | -0.08 | 0.15 | 0.05 | 295. |
| 300. | 0.13 | 0.06 | -0.13 | 0.06 | -0.05 | 0.17 | 0.05 | 300. |
| 305. | 0.48 | 0.27 | -0.01 | 0.14 | 0.01 | 0.19 | 0.07 | 305. |
| 310. | 0.89 | 0.52 | 0.14 | 0.27 | 0.08 | 0.23 | 0.08 | 310. |
| 315. | 1.33 | 0.80 | 0.32 | 0.39 | 0.16 | 0.27 | 0.08 | 315. |
| 320. | 1.75 | 1.08 | 0.51 | 0.51 | 0.25 | 0.33 | 0.08 | 320. |
| 325. | 2.19 | 1.35 | 0.70 | 0.63 | 0.34 | 0.32 | 0.08 | 325. |
| 330. | 2.78 | 1.61 | 0.85 | 0.76 | 0.42 | 0.35 | 0.08 | 330. |
| 335. | 3.57 | 1.84 | 1.03 | 0.86 | 0.47 | 0.37 | 0.08 | 335. |
| 340. | 4.48 | 2.00 | 1.12 | 0.92 | 0.50 | 0.36 | 0.08 | 340. |
| 345. | 4.92 | 2.03 | 1.15 | 0.92 | 0.49 | 0.33 | 0.06 | 345. |
| 350. | 4.87 | 1.97 | 1.10 | 0.85 | 0.44 | 0.29 | 0.03 | 350. |
| 355. | 4.56 | 1.84 | 1.00 | 0.75 | 0.42 | 0.25 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=504 CNTR NO. 269 ICN= 11. C.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.550 | 10.400 | DEG. |
| 0. | -0.32 | -0.14 | -0.06 | -0.02 | 0. |
| 5. | -0.13 | -0.09 | -0.03 | -0.01 | 5. |
| 10. | -0.07 | -0.04 | -0.01 | -0.01 | 10. |
| 15. | 0.03 | 0.01 | 0.01 | 0.00 | 15. |
| 20. | 0.19 | 0.06 | 0.03 | 0.01 | 20. |
| 25. | 0.24 | 0.09 | 0.04 | -0.01 | 25. |
| 30. | 0.15 | 0.03 | 0.02 | -0.03 | 30. |
| 35. | 0.02 | 0.02 | 0.01 | -0.02 | 35. |
| 40. | 0.18 | 0.06 | 0.05 | -0.01 | 40. |
| 45. | 0.19 | 0.08 | 0.08 | 0.00 | 45. |
| 50. | 0.15 | 0.05 | 0.07 | 0.01 | 50. |
| 55. | 0.18 | 0.04 | 0.05 | 0.01 | 55. |
| 60. | 0.18 | 0.05 | 0.04 | 0.01 | 60. |
| 65. | 0.13 | 0.04 | 0.02 | 0.00 | 65. |
| 70. | 0.07 | -0.01 | -0.02 | 0.00 | 70. |
| 75. | -0.21 | -0.06 | -0.04 | 0.01 | 75. |
| 80. | 0.11 | 0.01 | 0.03 | 0.02 | 80. |
| 85. | 0.41 | 0.19 | 0.10 | 0.02 | 85. |
| 90. | 0.30 | 0.13 | 0.06 | 0.02 | 90. |
| 95. | 0.20 | 0.06 | 0.04 | 0.01 | 95. |
| 100. | 0.17 | 0.04 | 0.03 | 0.02 | 100. |
| 105. | 0.15 | 0.02 | 0.03 | 0.03 | 105. |
| 110. | 0.13 | -0.01 | 0.04 | 0.03 | 110. |
| 115. | 0.04 | -0.01 | 0.06 | 0.03 | 115. |
| 120. | 0.08 | 0.05 | 0.07 | 0.03 | 120. |
| 125. | 0.39 | 0.17 | 0.10 | 0.03 | 125. |
| 130. | 0.60 | 0.26 | 0.13 | 0.03 | 130. |
| 135. | 0.63 | 0.29 | 0.14 | 0.03 | 135. |
| 140. | 0.55 | 0.29 | 0.14 | 0.02 | 140. |
| 145. | 0.53 | 0.27 | 0.14 | 0.02 | 145. |
| 150. | 0.56 | 0.24 | 0.13 | 0.02 | 150. |
| 155. | 0.58 | 0.24 | 0.12 | 0.02 | 155. |
| 160. | 0.57 | 0.24 | 0.12 | 0.02 | 160. |
| 165. | 0.55 | 0.24 | 0.12 | 0.02 | 165. |
| 170. | 0.52 | 0.23 | 0.12 | 0.02 | 170. |
| 175. | 0.47 | 0.22 | 0.11 | 0.02 | 175. |
| 180. | 0.41 | 0.20 | 0.10 | 0.01 | 180. |
| 185. | 0.34 | 0.18 | 0.09 | 0.01 | 185. |
| 190. | 0.27 | 0.16 | 0.08 | 0.02 | 190. |
| 195. | 0.21 | 0.12 | 0.06 | 0.02 | 195. |
| 200. | 0.14 | 0.07 | 0.04 | 0.03 | 200. |
| 205. | 0.07 | 0.03 | 0.02 | 0.03 | 205. |
| 210. | -0.00 | -0.01 | -0.01 | 0.03 | 210. |
| 215. | -0.08 | -0.04 | -0.03 | 0.02 | 215. |
| 220. | -0.15 | -0.06 | -0.05 | 0.01 | 220. |
| 225. | -0.22 | -0.08 | -0.07 | -0.01 | 225. |
| 230. | -0.28 | -0.10 | -0.08 | -0.01 | 230. |
| 235. | -0.34 | -0.11 | -0.09 | -0.01 | 235. |
| 240. | -0.38 | -0.12 | -0.10 | -0.00 | 240. |
| 245. | -0.39 | -0.. | -0.10 | -0.01 | 245. |
| 250. | -0.37 | -0.14 | -0.10 | -0.01 | 250. |
| 255. | -0.35 | -0.14 | -0.10 | -0.01 | 255. |
| 260. | -0.35 | -0.14 | -0.10 | -0.01 | 260. |
| 265. | -0.36 | -0.13 | -0.10 | -0.00 | 265. |
| 270. | -0.38 | -0.13 | -0.09 | -0.00 | 270. |
| 275. | -0.39 | -0.12 | -0.09 | -0.01 | 275. |
| 280. | -0.40 | -0.13 | -0.09 | -0.02 | 280. |
| 285. | -0.41 | -0.14 | -0.09 | -0.02 | 285. |
| 290. | -0.41 | -0.15 | -0.09 | -0.02 | 290. |
| 295. | -0.41 | -0.16 | -0.09 | -0.02 | 295. |
| 300. | -0.40 | -0.17 | -0.09 | -0.03 | 300. |
| 305. | -0.39 | -0.17 | -0.09 | -0.04 | 305. |
| 310. | -0.37 | -0.18 | -0.09 | -0.04 | 310. |
| 315. | -0.34 | -0.18 | -0.09 | -0.04 | 315. |
| 320. | -0.32 | -0.18 | -0.09 | -0.04 | 320. |
| 325. | -0.32 | -0.18 | -0.10 | -0.05 | 325. |
| 330. | -0.33 | -0.18 | -0.10 | -0.06 | 330. |
| 335. | -0.34 | -0.19 | -0.10 | -0.06 | 335. |
| 340. | -0.36 | -0.19 | -0.09 | -0.03 | 340. |
| 345. | -0.36 | -0.18 | -0.08 | -0.02 | 345. |
| 350. | -0.36 | -0.16 | -0.07 | -0.02 | 350. |
| 355. | -0.36 | -0.15 | -0.06 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=504 CNTR NO. 269 TCN= 11. C.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 13.400 | DEG. |
| 0. | -0.20 | -0.16 | -0.10 | -0.06 | -0.04 | -0.01 | -0.02 | 0. |
| 5. | -0.19 | -0.24 | -0.16 | -0.08 | -0.02 | -0.02 | -0.02 | 5. |
| 10. | -0.43 | -0.28 | -0.19 | -0.09 | -0.01 | -0.02 | -0.03 | 10. |
| 15. | -0.13 | -0.10 | -0.11 | -0.05 | -0.01 | -0.03 | -0.02 | 15. |
| 20. | 0.26 | 0.12 | 0.03 | 0.02 | 0.01 | -0.01 | -0.02 | 20. |
| 25. | 0.22 | 0.16 | 0.12 | 0.06 | 0.02 | 0.02 | -0.02 | 25. |
| 30. | 0.04 | 0.04 | 0.08 | 0.04 | 0.06 | 0.01 | -0.02 | 30. |
| 35. | 0.05 | 0.07 | 0.01 | 0.00 | 0.07 | 0.00 | -0.02 | 35. |
| 40. | 0.13 | 0.13 | 0.02 | 0.00 | 0.07 | -0.01 | -0.01 | 40. |
| 45. | 0.18 | 0.14 | 0.04 | 0.01 | 0.07 | -0.01 | 0.01 | 45. |
| 50. | 0.20 | 0.15 | 0.06 | 0.02 | 0.07 | -0.01 | 0.03 | 50. |
| 55. | 0.22 | 0.15 | 0.08 | 0.04 | 0.07 | -0.01 | 0.05 | 55. |
| 60. | 0.21 | 0.14 | 0.07 | 0.05 | 0.08 | -0.00 | 0.04 | 60. |
| 65. | 0.15 | 0.10 | -0.00 | 0.04 | 0.09 | 0.00 | 0.07 | 65. |
| 70. | -0.00 | -0.02 | -0.07 | -0.02 | 0.09 | -0.01 | 0.07 | 70. |
| 75. | 0.01 | 0.10 | 0.08 | 0.04 | 0.15 | -0.01 | 0.07 | 75. |
| 80. | 0.35 | 0.31 | 0.17 | 0.15 | 0.20 | 0.03 | 0.09 | 80. |
| 85. | 0.35 | 0.25 | 0.16 | 0.11 | 0.20 | 0.01 | 0.08 | 85. |
| 90. | 0.20 | 0.17 | 0.10 | 0.09 | 0.17 | 0.01 | 0.11 | 90. |
| 95. | 0.16 | 0.10 | 0.00 | 0.09 | 0.15 | 0.00 | 0.11 | 95. |
| 100. | 0.03 | -0.05 | -0.07 | 0.02 | 0.13 | -0.01 | 0.07 | 100. |
| 105. | -0.16 | -0.01 | -0.05 | 0.05 | 0.13 | 0.01 | 0.07 | 105. |
| 110. | 0.32 | 0.29 | 0.20 | 0.16 | 0.17 | 0.04 | 0.11 | 110. |
| 115. | 0.72 | 0.51 | 0.33 | 0.24 | 0.21 | 0.07 | 0.13 | 115. |
| 120. | 0.68 | 0.50 | 0.32 | 0.27 | 0.22 | 0.08 | 0.13 | 120. |
| 125. | 0.55 | 0.43 | 0.29 | 0.27 | 0.23 | 0.08 | 0.13 | 125. |
| 130. | 0.57 | 0.44 | 0.29 | 0.24 | 0.22 | 0.08 | 0.14 | 130. |
| 135. | 0.59 | 0.46 | 0.30 | 0.21 | 0.21 | 0.07 | 0.15 | 135. |
| 140. | 0.56 | 0.45 | 0.30 | 0.19 | 0.19 | 0.07 | 0.14 | 140. |
| 145. | 0.54 | 0.43 | 0.28 | 0.17 | 0.17 | 0.07 | 0.12 | 145. |
| 150. | 0.52 | 0.42 | 0.28 | 0.18 | 0.17 | 0.07 | 0.12 | 150. |
| 155. | 0.55 | 0.43 | 0.31 | 0.20 | 0.17 | 0.08 | 0.13 | 155. |
| 160. | 0.65 | 0.50 | 0.37 | 0.24 | 0.18 | 0.09 | 0.12 | 160. |
| 165. | 0.88 | 0.67 | 0.46 | 0.29 | 0.21 | 0.10 | 0.09 | 165. |
| 170. | 1.11 | 0.80 | 0.54 | 0.33 | 0.23 | 0.11 | 0.09 | 170. |
| 175. | 1.21 | 0.83 | 0.58 | 0.35 | 0.23 | 0.12 | 0.09 | 175. |
| 180. | 1.13 | 0.77 | 0.56 | 0.35 | 0.22 | 0.13 | 0.07 | 180. |
| 185. | 0.96 | 0.63 | 0.50 | 0.32 | 0.19 | 0.13 | 0.05 | 185. |
| 190. | 0.78 | 0.51 | 0.41 | 0.27 | 0.15 | 0.12 | 0.02 | 190. |
| 195. | 0.59 | 0.40 | 0.31 | 0.21 | 0.10 | 0.10 | -0.01 | 195. |
| 200. | 0.41 | 0.29 | 0.22 | 0.16 | 0.05 | 0.08 | -0.03 | 200. |
| 205. | 0.26 | 0.18 | 0.13 | 0.10 | -0.00 | 0.06 | -0.05 | 205. |
| 210. | 0.11 | 0.07 | 0.06 | 0.05 | -0.04 | 0.04 | -0.06 | 210. |
| 215. | -0.01 | -0.03 | -0.00 | 0.00 | -0.06 | 0.02 | -0.07 | 215. |
| 220. | -0.13 | -0.12 | -0.06 | -0.05 | -0.08 | -0.01 | -0.07 | 220. |
| 225. | -0.23 | -0.20 | -0.10 | -0.09 | -0.11 | -0.03 | -0.08 | 225. |
| 230. | -0.32 | -0.26 | -0.15 | -0.13 | -0.15 | -0.05 | -0.09 | 230. |
| 235. | -0.40 | -0.32 | -0.19 | -0.17 | -0.19 | -0.06 | -0.10 | 235. |
| 240. | -0.46 | -0.36 | -0.22 | -0.19 | -0.21 | -0.06 | -0.10 | 240. |
| 245. | -0.52 | -0.39 | -0.25 | -0.21 | -0.22 | -0.07 | -0.10 | 245. |
| 250. | -0.56 | -0.41 | -0.27 | -0.21 | -0.23 | -0.07 | -0.10 | 250. |
| 255. | -0.59 | -0.42 | -0.28 | -0.21 | -0.23 | -0.07 | -0.10 | 255. |
| 260. | -0.60 | -0.43 | -0.28 | -0.20 | -0.23 | -0.07 | -0.09 | 260. |
| 265. | -0.59 | -0.42 | -0.28 | -0.20 | -0.22 | -0.07 | -0.09 | 265. |
| 270. | -0.58 | -0.42 | -0.28 | -0.19 | -0.21 | -0.06 | -0.09 | 270. |
| 275. | -0.58 | -0.41 | -0.28 | -0.19 | -0.20 | -0.06 | -0.08 | 275. |
| 280. | -0.62 | -0.41 | -0.29 | -0.20 | -0.19 | -0.06 | -0.08 | 280. |
| 285. | -0.67 | -0.48 | -0.30 | -0.21 | -0.19 | -0.06 | -0.09 | 285. |
| 290. | -0.72 | -0.54 | -0.34 | -0.24 | -0.22 | -0.08 | -0.09 | 290. |
| 295. | -0.74 | -0.59 | -0.38 | -0.28 | -0.26 | -0.09 | -0.08 | 295. |
| 300. | -0.82 | -0.64 | -0.40 | -0.30 | -0.26 | -0.10 | -0.09 | 300. |
| 305. | -0.83 | -0.59 | -0.40 | -0.30 | -0.25 | -0.11 | -0.10 | 305. |
| 310. | -0.82 | -0.58 | -0.39 | -0.29 | -0.25 | -0.11 | -0.11 | 310. |
| 315. | -0.79 | -0.57 | -0.38 | -0.28 | -0.25 | -0.12 | -0.11 | 315. |
| 320. | -0.74 | -0.54 | -0.35 | -0.26 | -0.23 | -0.11 | -0.10 | 320. |
| 325. | -0.68 | -0.48 | -0.32 | -0.23 | -0.19 | -0.07 | -0.08 | 325. |
| 330. | -0.59 | -0.41 | -0.27 | -0.19 | -0.15 | -0.05 | -0.06 | 330. |
| 335. | -0.49 | -0.34 | -0.23 | -0.16 | -0.13 | -0.04 | -0.05 | 335. |
| 340. | -0.39 | -0.30 | -0.19 | -0.12 | -0.12 | -0.03 | -0.05 | 340. |
| 345. | -0.31 | -0.27 | -0.15 | -0.10 | -0.10 | -0.03 | -0.05 | 345. |
| 350. | -0.28 | -0.24 | -0.13 | -0.09 | -0.08 | -0.02 | -0.04 | 350. |
| 355. | -0.20 | -0.20 | -0.11 | -0.07 | -0.06 | -0.01 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-504 CNTR NO. 269 TCN= 11. C.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.39 | 0.28 | 0.24 | 0.20 | 0.11 | 0.07 | 0.02 | 0. |
| 5. | 0.28 | 0.21 | 0.19 | 0.19 | 0.12 | 0.06 | 0.03 | 5. |
| 10. | 0.31 | 0.28 | 0.22 | 0.17 | 0.12 | 0.05 | 0.02 | 10. |
| 15. | 0.35 | 0.24 | 0.18 | 0.14 | 0.12 | 0.04 | 0.01 | 15. |
| 20. | 0.35 | 0.17 | 0.13 | 0.13 | 0.11 | 0.04 | 0.01 | 20. |
| 25. | 0.37 | 0.17 | 0.13 | 0.13 | 0.11 | 0.03 | -0.01 | 25. |
| 30. | 0.42 | 0.21 | 0.15 | 0.13 | 0.11 | 0.02 | -0.02 | 30. |
| 35. | 0.49 | 0.29 | 0.18 | 0.14 | 0.13 | 0.00 | -0.04 | 35. |
| 40. | 0.56 | 0.28 | 0.20 | 0.15 | 0.17 | -0.01 | -0.05 | 40. |
| 45. | 0.63 | 0.30 | 0.22 | 0.15 | 0.19 | -0.02 | -0.05 | 45. |
| 50. | 0.65 | 0.32 | 0.21 | 0.14 | 0.20 | -0.03 | -0.06 | 50. |
| 55. | 0.63 | 0.31 | 0.19 | 0.12 | 0.19 | -0.04 | -0.06 | 55. |
| 60. | 0.55 | 0.22 | 0.13 | 0.07 | 0.16 | -0.06 | -0.07 | 60. |
| 65. | 0.45 | 0.10 | 0.08 | 0.01 | 0.15 | -0.08 | -0.07 | 65. |
| 70. | 0.43 | 0.09 | 0.09 | 0.05 | 0.17 | -0.05 | -0.04 | 70. |
| 75. | 0.53 | 0.21 | 0.11 | 0.09 | 0.19 | -0.03 | -0.03 | 75. |
| 80. | 0.45 | 0.08 | 0.00 | 0.03 | 0.17 | -0.05 | -0.04 | 80. |
| 85. | 0.21 | -0.13 | -0.16 | -0.11 | 0.09 | -0.07 | -0.05 | 85. |
| 90. | -0.26 | -0.28 | -0.16 | -0.12 | 0.07 | -0.06 | -0.05 | 90. |
| 95. | 0.53 | 0.21 | 0.05 | 0.07 | 0.17 | -0.02 | -0.02 | 95. |
| 100. | 0.64 | 0.21 | 0.13 | 0.11 | 0.22 | -0.01 | -0.02 | 100. |
| 105. | 0.50 | 0.12 | 0.09 | 0.04 | 0.19 | -0.01 | -0.02 | 105. |
| 110. | 0.37 | 0.04 | 0.00 | 0.00 | 0.15 | -0.01 | -0.02 | 110. |
| 115. | 0.20 | 0.01 | -0.03 | -0.02 | 0.14 | -0.01 | -0.03 | 115. |
| 120. | 0.11 | 0.05 | 0.03 | -0.01 | 0.16 | 0.02 | -0.01 | 120. |
| 125. | 0.51 | 0.11 | 0.23 | 0.16 | 0.19 | 0.04 | 0.00 | 125. |
| 130. | 1.00 | 0.67 | 0.32 | 0.24 | 0.22 | 0.04 | 0.01 | 130. |
| 135. | 0.99 | 0.59 | 0.37 | 0.25 | 0.24 | 0.06 | 0.02 | 135. |
| 140. | 0.60 | 0.50 | 0.34 | 0.22 | 0.25 | 0.08 | 0.03 | 140. |
| 145. | 0.51 | 0.46 | 0.31 | 0.21 | 0.25 | 0.09 | 0.04 | 145. |
| 150. | 0.63 | 0.49 | 0.31 | 0.22 | 0.24 | 0.09 | 0.05 | 150. |
| 155. | 0.70 | 0.52 | 0.33 | 0.23 | 0.23 | 0.09 | 0.05 | 155. |
| 160. | 0.71 | 0.54 | 0.35 | 0.24 | 0.23 | 0.09 | 0.05 | 160. |
| 165. | 0.70 | 0.54 | 0.37 | 0.24 | 0.22 | 0.10 | 0.06 | 165. |
| 170. | 0.68 | 0.53 | 0.37 | 0.24 | 0.21 | 0.10 | 0.06 | 170. |
| 175. | 0.63 | 0.50 | 0.37 | 0.24 | 0.18 | 0.10 | 0.05 | 175. |
| 180. | 0.54 | 0.44 | 0.34 | 0.22 | 0.15 | 0.10 | 0.05 | 180. |
| 185. | 0.42 | 0.35 | 0.27 | 0.20 | 0.11 | 0.09 | 0.05 | 185. |
| 190. | 0.28 | 0.25 | 0.20 | 0.16 | 0.07 | 0.08 | 0.04 | 190. |
| 195. | 0.13 | 0.13 | 0.13 | 0.10 | 0.02 | 0.06 | 0.04 | 195. |
| 200. | -0.03 | 0.02 | 0.05 | 0.04 | -0.02 | 0.05 | 0.04 | 200. |
| 205. | -0.18 | -0.05 | -0.01 | -0.01 | -0.05 | 0.04 | 0.04 | 205. |
| 210. | -0.33 | -0.10 | -0.08 | -0.05 | -0.09 | 0.04 | 0.03 | 210. |
| 215. | -0.45 | -0.16 | -0.14 | -0.08 | -0.12 | 0.03 | 0.04 | 215. |
| 220. | -0.54 | -0.22 | -0.18 | -0.11 | -0.14 | 0.02 | 0.04 | 220. |
| 225. | -0.62 | -0.28 | -0.21 | -0.14 | -0.16 | 0.02 | 0.04 | 225. |
| 230. | -0.65 | -0.32 | -0.23 | -0.16 | -0.18 | 0.01 | 0.04 | 230. |
| 235. | -0.67 | -0.34 | -0.24 | -0.17 | -0.20 | -0.00 | 0.03 | 235. |
| 240. | -0.69 | -0.37 | -0.26 | -0.18 | -0.22 | -0.01 | 0.02 | 240. |
| 245. | -0.74 | -0.40 | -0.29 | -0.20 | -0.24 | -0.03 | 0.01 | 245. |
| 250. | -0.80 | -0.43 | -0.31 | -0.22 | -0.26 | -0.05 | 0.01 | 250. |
| 255. | -0.86 | -0.48 | -0.34 | -0.24 | -0.28 | -0.06 | -0.00 | 255. |
| 260. | -0.90 | -0.52 | -0.36 | -0.26 | -0.30 | -0.07 | -0.01 | 260. |
| 265. | -0.93 | -0.57 | -0.37 | -0.28 | -0.32 | -0.09 | -0.02 | 265. |
| 270. | -0.94 | -1.60 | -0.38 | -0.29 | -0.33 | -0.09 | -0.03 | 270. |
| 275. | -0.96 | -0.56 | -0.38 | -0.29 | -0.34 | -0.09 | -0.03 | 275. |
| 280. | -0.81 | -0.47 | -0.33 | -0.29 | -0.33 | -0.08 | -0.02 | 280. |
| 285. | -0.80 | -0.47 | -0.26 | -0.25 | -0.29 | -0.08 | -0.02 | 285. |
| 290. | -1.12 | -0.68 | -0.44 | -0.32 | -0.36 | -0.10 | -0.04 | 290. |
| 295. | -1.39 | -0.90 | -0.59 | -0.42 | -0.43 | -0.14 | -0.06 | 295. |
| 300. | -1.38 | -0.93 | -0.63 | -0.44 | -0.44 | -0.15 | -0.06 | 300. |
| 305. | -1.19 | -0.79 | -0.58 | -0.41 | -0.40 | -0.14 | -0.04 | 305. |
| 310. | -1.00 | -0.65 | -0.47 | -0.35 | -0.34 | -0.11 | -0.03 | 310. |
| 315. | -0.82 | -0.54 | -0.38 | -0.27 | -0.29 | -0.08 | -0.02 | 315. |
| 320. | -0.66 | -0.42 | -0.31 | -0.19 | -0.24 | -0.06 | -0.01 | 320. |
| 325. | -0.51 | -0.29 | -0.22 | -0.12 | -0.19 | -0.04 | -0.00 | 325. |
| 330. | -0.34 | -0.16 | -0.09 | -0.07 | -0.13 | -0.01 | 0.00 | 330. |
| 335. | -0.15 | -0.02 | 0.04 | -0.01 | -0.08 | 0.02 | 0.01 | 335. |
| 340. | 0.03 | 0.11 | 0.14 | 0.07 | -0.02 | 0.05 | 0.01 | 340. |
| 345. | 0.28 | 0.29 | 0.21 | 0.15 | 0.04 | 0.07 | 0.02 | 345. |
| 350. | 0.46 | 0.39 | 0.27 | 0.21 | 0.09 | 0.08 | 0.03 | 350. |
| 355. | 0.47 | 0.35 | 0.28 | 0.22 | 0.11 | 0.08 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=504 CNTR NO. 269 MW= 11. C.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.85 | 0.43 | 0.32 | 0.20 | 0.14 | 0.14 | 0.08 | 0. |
| 5. | 0.67 | 0.36 | 0.25 | 0.17 | 0.12 | 0.11 | 0.07 | 5. |
| 10. | 0.44 | 0.24 | 0.16 | 0.11 | 0.11 | 0.07 | 0.06 | 10. |
| 15. | 0.23 | 0.12 | 0.06 | 0.03 | 0.10 | 0.04 | 0.04 | 15. |
| 20. | 0.11 | 0.19 | 0.01 | -0.00 | 0.09 | 0.01 | 0.02 | 20. |
| 25. | 0.13 | 0.33 | -0.01 | 0.02 | 0.07 | -0.00 | 0.01 | 25. |
| 30. | 0.22 | 0.44 | 0.00 | 0.06 | 0.06 | -0.01 | -0.00 | 30. |
| 35. | 0.29 | 0.55 | 0.02 | 0.09 | 0.05 | -0.02 | -0.02 | 35. |
| 40. | 0.35 | 0.64 | 0.03 | 0.12 | 0.05 | -0.03 | -0.02 | 40. |
| 45. | 0.37 | 0.67 | 0.04 | 0.14 | 0.04 | -0.03 | -0.02 | 45. |
| 50. | 0.34 | 0.58 | 0.03 | 0.16 | 0.04 | -0.05 | -0.02 | 50. |
| 55. | 0.24 | 0.30 | 0.01 | 0.17 | 0.02 | -0.08 | -0.04 | 55. |
| 60. | 0.06 | 0.05 | -0.04 | 0.14 | -0.01 | -0.12 | -0.06 | 60. |
| 65. | -0.16 | -0.10 | -0.10 | 0.08 | -0.04 | -0.14 | -0.07 | 65. |
| 70. | -0.23 | -0.20 | -0.18 | 0.03 | -0.05 | -0.15 | -0.07 | 70. |
| 75. | -0.49 | -0.44 | -0.32 | -0.01 | -0.04 | -0.17 | -0.07 | 75. |
| 80. | -1.01 | -0.57 | -0.46 | -0.03 | -0.01 | -0.19 | -0.06 | 80. |
| 85. | -0.60 | -0.33 | -0.39 | 0.04 | 0.02 | -0.17 | -0.06 | 85. |
| 90. | -0.69 | -0.36 | -0.37 | 0.04 | -0.00 | -0.20 | -0.07 | 90. |
| 95. | -1.24 | -0.74 | -0.55 | -0.06 | -0.04 | -0.22 | -0.07 | 95. |
| 100. | -1.40 | -0.86 | -0.50 | -0.10 | -0.04 | -0.18 | -0.05 | 100. |
| 105. | -0.57 | -0.39 | -0.17 | 0.11 | 0.03 | -0.11 | -0.04 | 105. |
| 110. | 0.02 | 0.19 | -0.04 | 0.20 | 0.08 | -0.08 | -0.04 | 110. |
| 115. | -0.21 | 0.32 | -0.02 | 0.24 | 0.10 | -0.07 | -0.04 | 115. |
| 120. | -0.38 | 0.16 | -0.02 | 0.24 | 0.10 | -0.07 | -0.04 | 120. |
| 125. | -0.36 | -0.11 | -0.06 | 0.21 | 0.09 | -0.06 | -0.03 | 125. |
| 130. | -0.31 | -0.17 | -0.11 | 0.18 | 0.11 | -0.05 | -0.01 | 130. |
| 135. | -0.39 | -0.20 | -0.15 | 0.16 | 0.13 | -0.03 | -0.00 | 135. |
| 140. | -0.39 | -0.19 | -0.12 | 0.17 | 0.17 | -0.00 | 0.00 | 140. |
| 145. | -0.24 | -0.08 | 0.05 | 0.24 | 0.23 | 0.04 | 0.01 | 145. |
| 150. | 0.37 | 0.20 | 0.30 | 0.38 | 0.30 | 0.08 | 0.01 | 150. |
| 155. | 1.18 | 0.86 | 0.54 | 0.50 | 0.36 | 0.09 | 0.01 | 155. |
| 160. | 1.73 | 1.54 | 0.68 | 0.57 | 0.41 | 0.10 | 0.02 | 160. |
| 165. | 1.82 | 1.56 | 0.74 | 0.60 | 0.44 | 0.13 | 0.03 | 165. |
| 170. | 1.79 | 1.41 | 0.77 | 0.61 | 0.44 | 0.16 | 0.04 | 170. |
| 175. | 1.68 | 1.21 | 0.77 | 0.59 | 0.42 | 0.18 | 0.05 | 175. |
| 180. | 1.53 | 1.06 | 0.74 | 0.57 | 0.38 | 0.18 | 0.05 | 180. |
| 185. | 1.38 | 0.96 | 0.68 | 0.52 | 0.33 | 0.17 | 0.04 | 185. |
| 190. | 1.22 | 0.84 | 0.58 | 0.44 | 0.27 | 0.15 | 0.03 | 190. |
| 195. | 1.05 | 0.68 | 0.48 | 0.30 | 0.19 | 0.13 | 0.03 | 195. |
| 200. | 0.85 | 0.46 | 0.38 | 0.15 | 0.12 | 0.11 | 0.03 | 200. |
| 205. | 0.61 | 0.28 | 0.30 | 0.05 | 0.05 | 0.10 | 0.03 | 205. |
| 210. | 0.39 | 0.18 | 0.24 | -0.02 | 0.03 | 0.09 | 0.03 | 210. |
| 215. | 0.28 | 0.11 | 0.18 | -0.07 | 0.01 | 0.08 | 0.04 | 215. |
| 220. | 0.25 | 0.05 | 0.14 | -0.11 | 0.01 | 0.09 | 0.05 | 220. |
| 225. | 0.25 | 0.03 | 0.11 | -0.13 | 0.01 | 0.09 | 0.06 | 225. |
| 230. | 0.29 | 0.05 | 0.09 | -0.12 | 0.01 | 0.09 | 0.05 | 230. |
| 235. | 0.35 | 0.11 | 0.08 | -0.11 | 0.00 | 0.08 | 0.05 | 235. |
| 240. | 0.41 | 0.15 | 0.07 | -0.11 | -0.02 | 0.07 | 0.04 | 240. |
| 245. | 0.35 | 0.06 | 0.03 | -0.13 | -0.06 | 0.03 | 0.02 | 245. |
| 250. | -0.26 | -0.30 | -0.11 | -0.22 | -0.15 | 0.01 | -0.00 | 250. |
| 255. | -1.11 | -0.85 | -0.40 | -0.44 | -0.25 | -0.01 | -0.01 | 255. |
| 260. | -1.44 | -1.12 | -0.54 | -0.57 | -0.37 | -0.06 | -0.02 | 260. |
| 265. | -1.39 | -1.12 | -0.57 | -0.59 | -0.45 | -0.09 | -0.02 | 265. |
| 270. | -1.36 | -1.06 | -0.57 | -0.61 | -0.48 | -0.12 | -0.03 | 270. |
| 275. | -1.37 | -1.08 | -0.55 | -0.62 | -0.49 | -0.13 | -0.07 | 275. |
| 280. | -1.36 | -1.09 | -0.55 | -0.61 | -0.48 | -0.13 | -0.07 | 280. |
| 285. | -1.33 | -1.10 | -0.56 | -0.61 | -0.45 | -0.12 | -0.06 | 285. |
| 290. | -1.35 | -1.13 | -0.62 | -0.62 | -0.45 | -0.11 | -0.06 | 290. |
| 295. | -1.53 | -1.21 | -0.68 | -0.66 | -0.46 | -0.13 | -0.06 | 295. |
| 300. | -1.61 | -1.25 | -0.68 | -0.70 | -0.47 | -0.14 | -0.06 | 300. |
| 305. | -1.43 | -1.15 | -0.60 | -0.65 | -0.44 | -0.12 | -0.02 | 305. |
| 310. | -1.16 | -0.99 | -0.47 | -0.56 | -0.37 | -0.08 | -0.01 | 310. |
| 315. | -0.84 | -0.80 | -0.30 | -0.51 | -0.29 | -0.05 | 0.00 | 315. |
| 320. | -0.63 | -0.55 | -0.12 | -0.41 | -0.19 | 0.00 | 0.02 | 320. |
| 325. | -0.03 | -0.17 | 0.03 | -0.13 | -0.10 | 0.06 | 0.04 | 325. |
| 330. | 0.59 | 0.26 | 0.16 | 0.03 | -0.04 | 0.08 | 0.04 | 330. |
| 335. | 0.62 | 0.28 | 0.26 | 0.07 | -0.01 | 0.09 | 0.03 | 335. |
| 340. | 0.72 | 0.33 | 0.34 | 0.11 | 0.04 | 0.13 | 0.04 | 340. |
| 345. | 0.89 | 0.47 | 0.41 | 0.20 | 0.13 | 0.17 | 0.07 | 345. |
| 350. | 0.99 | 0.54 | 0.45 | 0.25 | 0.19 | 0.19 | 0.09 | 350. |
| 355. | 0.97 | 0.50 | 0.40 | 0.24 | 0.18 | 0.18 | 0.09 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=504 CNTR NO. 269 TCN= 11. G.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 1.39 | 0.91 | 0.65 | 0.45 | 0.36 | 0.18 | 0.06 | 0. |
| 5. | 1.26 | 0.82 | 0.58 | 0.41 | 0.29 | 0.16 | 0.06 | 5. |
| 10. | 0.98 | 0.62 | 0.42 | 0.33 | 0.21 | 0.11 | 0.05 | 10. |
| 15. | 0.61 | 0.37 | 0.22 | 0.21 | 0.11 | 0.05 | 0.04 | 15. |
| 20. | 0.27 | 0.15 | 0.03 | 0.11 | 0.03 | 0.00 | 0.03 | 20. |
| 25. | 0.10 | 0.00 | -0.06 | 0.06 | -0.01 | -0.01 | 0.01 | 25. |
| 30. | 0.04 | -0.03 | -0.08 | 0.03 | -0.03 | -0.02 | 0.01 | 30. |
| 35. | 0.06 | -0.01 | -0.08 | 0.01 | -0.02 | -0.02 | 0.01 | 35. |
| 40. | 0.10 | -0.01 | -0.05 | 0.00 | -0.02 | -0.02 | 0.01 | 40. |
| 45. | 0.13 | -0.02 | -0.04 | -0.00 | -0.02 | -0.02 | 0.01 | 45. |
| 50. | 0.11 | -0.07 | -0.04 | -0.02 | -0.04 | -0.04 | -0.00 | 50. |
| 55. | 0.03 | -0.14 | -0.07 | -0.06 | -0.08 | -0.06 | -0.02 | 55. |
| 60. | -0.09 | -0.21 | -0.13 | -0.11 | -0.12 | -0.10 | -0.02 | 60. |
| 65. | -0.26 | -0.26 | -0.24 | -0.17 | -0.18 | -0.13 | -0.02 | 65. |
| 70. | -0.55 | -0.43 | -0.40 | -0.23 | -0.24 | -0.16 | -0.05 | 70. |
| 75. | -0.72 | -0.65 | -0.50 | -0.29 | -0.31 | -0.20 | -0.07 | 75. |
| 80. | -0.80 | -0.77 | -0.68 | -0.36 | -0.41 | -0.22 | -0.08 | 80. |
| 85. | -1.63 | -1.37 | -1.01 | -0.46 | -0.44 | -0.22 | -0.07 | 85. |
| 90. | -1.27 | -0.96 | -0.62 | -0.41 | -0.35 | -0.18 | -0.04 | 90. |
| 95. | -0.90 | -0.59 | -0.34 | -0.28 | -0.25 | -0.14 | -0.02 | 95. |
| 100. | -0.70 | -0.82 | -0.45 | -0.28 | -0.22 | -0.10 | 0.00 | 100. |
| 105. | -1.08 | -0.90 | -0.59 | -0.31 | -0.21 | -0.07 | 0.01 | 105. |
| 110. | -1.16 | -0.88 | -0.53 | -0.24 | -0.17 | -0.05 | 0.01 | 110. |
| 115. | -0.50 | -0.43 | -0.17 | -0.16 | -0.06 | -0.03 | -0.00 | 115. |
| 120. | 0.42 | 0.18 | 0.22 | 0.00 | 0.04 | -0.01 | -0.01 | 120. |
| 125. | 1.31 | 0.43 | 0.38 | 0.07 | 0.09 | -0.01 | -0.02 | 125. |
| 130. | 1.03 | 0.30 | 0.18 | 0.04 | 0.09 | 0.01 | -0.02 | 130. |
| 135. | 0.58 | 0.21 | 0.17 | -0.02 | 0.04 | 0.05 | -0.01 | 135. |
| 140. | 0.39 | 0.14 | 0.10 | -0.04 | 0.05 | 0.00 | -0.00 | 140. |
| 145. | 0.30 | 0.11 | 0.07 | -0.04 | 0.03 | 0.11 | 0.00 | 145. |
| 150. | 0.24 | 0.10 | 0.05 | -0.03 | 0.02 | 0.12 | 0.00 | 150. |
| 155. | 0.24 | 0.10 | 0.05 | -0.02 | 0.01 | 0.10 | 0.00 | 155. |
| 160. | 0.25 | 0.11 | 0.05 | -0.02 | 0.03 | 0.09 | 0.01 | 160. |
| 165. | 0.27 | 0.14 | 0.06 | -0.00 | 0.04 | 0.10 | 0.01 | 165. |
| 170. | 0.31 | 0.17 | 0.10 | 0.01 | 0.08 | 0.12 | 0.02 | 170. |
| 175. | 0.36 | 0.24 | 0.15 | 0.04 | 0.11 | 0.13 | 0.02 | 175. |
| 180. | 0.43 | 0.30 | 0.17 | 0.07 | 0.13 | 0.12 | 0.02 | 180. |
| 185. | 0.46 | 0.32 | 0.15 | 0.09 | 0.12 | 0.10 | 0.02 | 185. |
| 190. | 0.40 | 0.28 | 0.13 | 0.09 | 0.10 | 0.07 | 0.01 | 190. |
| 195. | 0.29 | 0.22 | 0.11 | 0.07 | 0.06 | 0.04 | 0.01 | 195. |
| 200. | 0.15 | 0.15 | 0.07 | 0.05 | 0.03 | 0.01 | 0.00 | 200. |
| 205. | -0.01 | 0.08 | 0.01 | 0.01 | -0.01 | -0.01 | -0.01 | 205. |
| 210. | -0.16 | 0.02 | -0.04 | -0.02 | -0.05 | -0.02 | -0.01 | 210. |
| 215. | -0.29 | -0.03 | -0.07 | -0.04 | -0.06 | -0.02 | -0.01 | 215. |
| 220. | -0.37 | -0.07 | -0.08 | -0.06 | -0.07 | -0.02 | -0.01 | 220. |
| 225. | -0.39 | -0.09 | -0.08 | -0.07 | -0.06 | -0.01 | -0.01 | 225. |
| 230. | -0.36 | -0.07 | -0.06 | -0.06 | -0.03 | -0.00 | -0.00 | 230. |
| 235. | -0.31 | -0.03 | -0.01 | -0.02 | 0.01 | 0.01 | 0.01 | 235. |
| 240. | -0.21 | 0.04 | 0.06 | 0.02 | 0.05 | 0.03 | 0.01 | 240. |
| 245. | -0.08 | 0.14 | 0.18 | 0.07 | 0.09 | 0.04 | 0.02 | 245. |
| 250. | 0.12 | 0.26 | 0.31 | 0.11 | 0.14 | 0.06 | 0.02 | 250. |
| 255. | 0.33 | 0.40 | 0.48 | 0.16 | 0.23 | 0.08 | 0.02 | 255. |
| 260. | 0.59 | 0.64 | 0.49 | 0.23 | 0.26 | 0.07 | 0.02 | 260. |
| 265. | 0.63 | 0.67 | 0.53 | 0.22 | 0.18 | 0.03 | 0.01 | 265. |
| 270. | 0.93 | 0.25 | 0.17 | 0.06 | -0.01 | -0.03 | -0.00 | 270. |
| 275. | -1.38 | -0.62 | -0.40 | -0.18 | -0.24 | -0.12 | -0.02 | 275. |
| 280. | -1.58 | -0.78 | -0.64 | -0.32 | -0.33 | -0.18 | -0.03 | 280. |
| 285. | -1.35 | -0.70 | -0.66 | -0.31 | -0.33 | -0.19 | -0.04 | 285. |
| 290. | -1.22 | -0.62 | -0.55 | -0.27 | -0.28 | -0.18 | -0.04 | 290. |
| 295. | -1.17 | -0.57 | -0.49 | -0.24 | -0.22 | -0.16 | -0.75 | 295. |
| 300. | -1.16 | -0.55 | -0.46 | -0.21 | -0.19 | -0.14 | -0.04 | 300. |
| 305. | -1.07 | -0.50 | -0.39 | -0.18 | -0.15 | -0.13 | -0.03 | 305. |
| 310. | -0.85 | -0.35 | -0.28 | -0.11 | -0.09 | -0.09 | -0.02 | 310. |
| 315. | -0.55 | -0.15 | -0.13 | -0.02 | -0.01 | -0.04 | -0.01 | 315. |
| 320. | -0.20 | 0.04 | 0.05 | 0.07 | 0.06 | 0.01 | 0.00 | 320. |
| 325. | 0.18 | 0.19 | 0.23 | 0.15 | 0.12 | 0.06 | 0.01 | 325. |
| 330. | 0.56 | 0.35 | 0.36 | 0.22 | 0.19 | 0.09 | 0.02 | 330. |
| 335. | 0.91 | 0.57 | 0.49 | 0.30 | 0.26 | 0.13 | 0.02 | 335. |
| 340. | 1.22 | 0.79 | 0.65 | 0.39 | 0.36 | 0.18 | 0.04 | 340. |
| 345. | 1.46 | 0.93 | 0.74 | 0.46 | 0.48 | 0.21 | 0.05 | 345. |
| 350. | 1.54 | 0.99 | 0.77 | 0.49 | 0.41 | 0.20 | 0.06 | 350. |
| 355. | 1.42 | 0.98 | 0.72 | 0.48 | 0.40 | 0.19 | 0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=50+ CNTR NO. 269 TCN= 11. C.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 1.94 | 1.39 | 0.90 | 0.66 | 0.27 | 0.23 | 0.07 | 0. |
| 5. | 1.67 | 1.11 | 0.79 | 0.53 | 0.24 | 0.19 | 0.06 | 5. |
| 10. | 1.14 | 0.74 | 0.58 | 0.37 | 0.21 | 0.13 | 0.04 | 10. |
| 15. | 0.69 | 0.41 | 0.36 | 0.20 | 0.20 | 0.06 | 0.03 | 15. |
| 20. | 0.34 | 0.20 | 0.19 | 0.09 | 0.2. | 0.00 | 0.01 | 20. |
| 25. | -0.03 | 0.05 | 0.08 | 0.02 | 0.21 | -0.03 | 0.01 | 25. |
| 30. | -0.14 | -0.04 | 0.02 | -0.01 | 0.24 | -0.03 | 0.00 | 30. |
| 35. | -0.13 | -0.08 | 0.01 | -0.01 | 0.24 | -0.03 | 0.00 | 35. |
| 40. | -0.13 | -0.09 | 0.03 | -0.00 | 0.26 | -0.03 | -0.01 | 40. |
| 45. | -0.11 | -0.10 | 0.07 | 0.00 | 0.29 | -0.05 | -0.02 | 45. |
| 50. | -0.11 | -0.12 | 0.09 | -0.01 | 0.31 | -0.08 | -0.04 | 50. |
| 55. | -0.16 | -0.20 | 0.09 | -0.05 | 0.31 | -0.13 | -0.05 | 55. |
| 60. | -0.31 | -0.32 | 0.02 | -0.13 | 0.27 | -0.18 | -0.06 | 60. |
| 65. | -0.64 | -0.53 | -0.10 | -0.23 | 0.20 | -0.23 | -0.08 | 65. |
| 70. | -0.95 | -0.80 | -0.29 | -0.35 | 0.08 | -0.28 | -0.12 | 70. |
| 75. | -1.23 | -1.08 | -0.48 | -0.53 | -0.08 | -0.32 | -0.14 | 75. |
| 80. | -1.87 | -1.49 | -0.73 | -0.68 | -0.16 | -0.33 | -0.14 | 80. |
| 85. | -1.58 | -1.22 | -0.92 | -0.52 | -0.14 | -0.30 | -0.12 | 85. |
| 90. | -1.10 | -0.91 | -0.44 | -0.39 | -0.10 | -0.27 | -0.11 | 90. |
| 95. | -1.66 | -1.29 | -0.52 | -0.39 | -0.19 | -0.22 | -0.08 | 95. |
| 100. | -1.83 | -1.07 | -0.42 | -0.30 | -0.06 | -0.16 | -0.03 | 100. |
| 105. | -0.72 | -0.05 | 0.12 | -0.11 | 0.19 | -0.11 | -0.01 | 105. |
| 110. | 0.49 | 0.47 | 0.61 | 0.11 | 0.31 | -0.13 | -0.06 | 110. |
| 115. | 0.84 | 0.33 | 0.64 | 0.21 | 0.30 | -0.12 | -0.08 | 115. |
| 120. | 0.60 | 0.07 | 0.44 | 0.16 | 0.33 | -0.09 | -0.05 | 120. |
| 125. | 0.86 | -0.06 | 0.23 | 0.05 | 0.39 | -0.08 | -0.03 | 125. |
| 130. | -0.13 | -0.13 | 0.06 | -0.05 | 0.37 | -0.08 | -0.02 | 130. |
| 135. | -0.25 | -0.22 | -0.08 | -0.14 | 0.31 | -0.08 | -0.03 | 135. |
| 140. | -0.34 | -0.27 | -0.14 | -0.19 | 0.24 | -0.07 | -0.01 | 140. |
| 145. | -0.37 | -0.28 | -0.17 | -0.19 | 0.19 | -0.07 | -0.00 | 145. |
| 150. | -0.36 | -0.26 | -0.18 | -0.18 | 0.16 | -0.06 | -0.00 | 150. |
| 155. | -0.33 | -0.23 | -0.19 | -0.20 | 0.14 | -0.05 | -0.00 | 155. |
| 160. | -0.30 | -0.20 | -0.17 | -0.21 | 0.13 | -0.03 | 0.01 | 160. |
| 165. | -0.23 | -0.17 | -0.14 | -0.20 | 0.12 | -0.01 | 0.03 | 165. |
| 170. | -0.10 | -0.12 | -0.09 | -0.14 | 0.12 | 0.02 | 0.03 | 170. |
| 175. | 0.09 | -0.04 | -0.05 | -0.07 | 0.11 | 0.04 | 0.03 | 175. |
| 180. | 0.21 | 0.04 | -0.01 | -0.01 | 0.10 | 0.07 | 0.03 | 180. |
| 185. | 0.26 | 0.07 | 0.02 | 0.02 | 0.08 | 0.07 | 0.03 | 185. |
| 190. | 0.26 | 0.06 | 0.01 | 0.01 | 0.05 | 0.06 | 0.03 | 190. |
| 195. | 0.20 | 0.04 | -0.01 | -0.02 | 0.00 | 0.05 | 0.01 | 195. |
| 200. | 0.08 | 0.01 | -0.06 | -0.06 | -0.06 | 0.03 | -0.00 | 200. |
| 205. | -0.07 | -0.02 | -0.13 | -0.09 | -0.13 | 0.02 | -0.01 | 205. |
| 210. | -0.22 | -0.08 | -0.21 | -0.12 | -0.19 | 0.01 | 0.00 | 210. |
| 215. | -0.33 | -0.18 | -0.27 | -0.15 | -0.24 | 0.01 | 0.00 | 215. |
| 220. | -0.38 | -0.27 | -0.30 | -0.16 | -0.28 | 0.02 | 0.00 | 220. |
| 225. | -0.38 | -0.30 | -0.31 | -0.15 | -0.29 | 0.03 | 0.01 | 225. |
| 230. | -0.35 | -0.26 | -0.30 | -0.10 | -0.29 | 0.04 | 0.02 | 230. |
| 235. | -0.28 | -0.19 | -0.26 | -0.04 | -0.28 | 0.05 | 0.03 | 235. |
| 240. | -0.17 | -0.09 | -0.20 | -0.01 | -0.26 | 0.06 | 0.03 | 240. |
| 245. | -0.03 | 0.04 | -0.13 | 0.05 | -0.25 | 0.07 | 0.04 | 245. |
| 250. | 0.14 | 0.19 | -0.05 | 0.12 | -0.22 | 0.10 | 0.04 | 250. |
| 255. | 0.41 | 0.36 | 0.05 | 0.20 | -0.20 | 0.14 | 0.05 | 255. |
| 260. | 0.70 | 0.63 | 0.22 | 0.30 | -0.13 | 0.18 | 0.05 | 260. |
| 265. | 0.99 | 1.01 | 0.38 | 0.38 | -0.07 | 0.19 | 0.06 | 265. |
| 270. | 1.27 | 1.06 | 0.45 | 0.42 | -0.00 | 0.17 | 0.05 | 270. |
| 275. | 1.05 | 0.42 | 0.07 | 0.21 | -0.23 | 0.10 | 0.01 | 275. |
| 280. | -1.19 | -0.92 | -0.53 | -0.21 | -0.43 | -0.03 | -0.04 | 280. |
| 285. | 1.51 | -1.08 | -0.85 | -0.42 | -0.63 | -0.09 | -0.05 | 285. |
| 290. | -1.30 | -0.93 | -0.74 | -0.39 | -0.64 | -0.09 | -0.03 | 290. |
| 295. | -1.04 | -0.64 | -0.56 | -0.32 | -0.61 | -0.07 | -0.02 | 295. |
| 300. | -0.89 | -0.52 | -0.52 | -0.24 | -0.54 | -0.03 | -0.01 | 300. |
| 305. | -0.77 | -0.38 | -0.48 | -0.17 | -0.47 | 0.00 | -0.00 | 305. |
| 310. | -0.51 | -0.19 | -0.33 | -0.10 | -0.38 | 0.03 | 0.01 | 310. |
| 315. | -0.17 | 0.08 | -0.16 | -0.02 | -0.29 | 0.06 | 0.03 | 315. |
| 320. | 0.24 | 0.36 | 0.03 | 0.11 | -0.19 | 0.10 | 0.04 | 320. |
| 325. | 0.61 | 0.61 | 0.21 | 0.25 | -0.09 | 0.14 | 0.05 | 325. |
| 330. | 0.90 | 0.86 | 0.39 | 0.39 | 0.02 | 0.18 | 0.06 | 330. |
| 335. | 1.48 | 1.15 | 0.56 | 0.50 | 0.11 | 0.21 | 0.08 | 335. |
| 340. | 1.95 | 1.38 | 0.71 | 0.59 | 0.28 | 0.24 | 0.09 | 340. |
| 345. | 2.14 | 1.51 | 0.83 | 0.67 | 0.25 | 0.27 | 0.09 | 345. |
| 350. | 2.19 | 1.48 | 0.91 | 0.71 | 0.28 | 0.28 | 0.09 | 350. |
| 355. | 2.01 | 1.42 | 0.93 | 0.71 | 0.28 | 0.26 | 0.08 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=504 CNTR NO. 269 TCN= 11. C.R.= 62.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 2.39 | 1.26 | 0.76 | 0.49 | 0.31 | 0.20 | 0.06 | 0. |
| 5. | 1.69 | 0.98 | 0.54 | 0.31 | 0.22 | 0.13 | 0.03 | 5. |
| 10. | 1.07 | 0.67 | 0.32 | 0.14 | 0.14 | 0.06 | 0.02 | 10. |
| 15. | 0.60 | 0.40 | 0.14 | -0.01 | 0.07 | -0.00 | 0.00 | 15. |
| 20. | 0.25 | 0.17 | -0.01 | -0.11 | 0.03 | -0.04 | -0.02 | 20. |
| 25. | -0.01 | 0.01 | -0.10 | -0.17 | 0.00 | -0.09 | -0.03 | 25. |
| 30. | -0.20 | -0.09 | -0.11 | -0.20 | -0.01 | -0.11 | -0.05 | 30. |
| 35. | -0.27 | -0.11 | -0.09 | -0.17 | -0.01 | -0.13 | -0.07 | 35. |
| 40. | -0.29 | -0.10 | -0.07 | -0.13 | -0.01 | -0.15 | -0.10 | 40. |
| 45. | -0.29 | -0.08 | -0.05 | -0.09 | -0.02 | -0.17 | -0.12 | 45. |
| 50. | -0.31 | -0.08 | -0.02 | -0.07 | -0.03 | -0.21 | -0.12 | 50. |
| 55. | -0.40 | -0.13 | 0.01 | -0.10 | -0.06 | -0.26 | -0.12 | 55. |
| 60. | -0.60 | -0.28 | -0.03 | -0.17 | -0.13 | -0.32 | -0.14 | 60. |
| 65. | -1.00 | -0.48 | -0.15 | -0.28 | -0.19 | -0.40 | -0.15 | 65. |
| 70. | -1.49 | -0.83 | -0.43 | -0.48 | -0.25 | -0.45 | -0.19 | 70. |
| 75. | -1.98 | -1.32 | -0.75 | -0.48 | -0.28 | -0.47 | -0.21 | 75. |
| 80. | -2.12 | -1.25 | -0.83 | -0.47 | -0.26 | -0.46 | -0.21 | 80. |
| 85. | -1.82 | -1.08 | -0.64 | -0.36 | -0.21 | -0.45 | -0.18 | 85. |
| 90. | -2.03 | -1.06 | -0.36 | -0.19 | -0.13 | -0.33 | -0.12 | 90. |
| 95. | -0.84 | 0.08 | 0.13 | 0.08 | -0.05 | -0.25 | -0.06 | 95. |
| 100. | 0.75 | 1.98 | 1.15 | 0.21 | 0.04 | -0.21 | -0.10 | 100. |
| 105. | 0.35 | 1.91 | 1.76 | 0.24 | 0.10 | -0.16 | -0.12 | 105. |
| 110. | -0.07 | 0.70 | 1.03 | 0.17 | 0.11 | -0.13 | -0.11 | 110. |
| 115. | -3.50 | -0.07 | 0.55 | 0.06 | 0.10 | -0.13 | -0.10 | 115. |
| 120. | -3.71 | -0.26 | 0.13 | -0.03 | 0.07 | -0.15 | -0.08 | 120. |
| 125. | -0.84 | -0.35 | -0.13 | -0.12 | 0.04 | -0.18 | -0.05 | 125. |
| 130. | -0.92 | -0.39 | -0.24 | -0.18 | -0.00 | -0.17 | -0.03 | 130. |
| 135. | -0.96 | -0.47 | -0.31 | -0.21 | -0.04 | -0.17 | -0.03 | 135. |
| 140. | -0.98 | -0.52 | -0.35 | -0.23 | -0.07 | -0.16 | -0.02 | 140. |
| 145. | -0.98 | -0.56 | -0.39 | -0.24 | -0.09 | -0.14 | -0.01 | 145. |
| 150. | -0.97 | -0.59 | -0.41 | -0.24 | -0.10 | -0.13 | 0.01 | 150. |
| 155. | -0.93 | -0.59 | -0.42 | -0.24 | -0.09 | -0.11 | 0.02 | 155. |
| 160. | -0.84 | -0.56 | -0.42 | -0.24 | -0.08 | -0.09 | 0.02 | 160. |
| 165. | -0.72 | -0.47 | -0.40 | -0.19 | -0.06 | -0.04 | 0.03 | 165. |
| 170. | -0.51 | -0.35 | -0.35 | -0.13 | -0.04 | 0.00 | 0.04 | 170. |
| 175. | -0.31 | -0.23 | -0.27 | -0.07 | -0.01 | 0.05 | 0.04 | 175. |
| 180. | -0.15 | -0.13 | -0.18 | -0.02 | 0.03 | 0.08 | 0.04 | 180. |
| 185. | -0.03 | -0.07 | -0.12 | 0.01 | 0.04 | 0.10 | 0.05 | 185. |
| 190. | 0.04 | -0.04 | -0.12 | 0.04 | 0.04 | 0.10 | 0.05 | 190. |
| 195. | 0.05 | -0.14 | -0.14 | 0.03 | 0.03 | 0.09 | 0.05 | 195. |
| 200. | 0.02 | -0.21 | -0.18 | 0.00 | 0.01 | 0.07 | 0.04 | 200. |
| 205. | -0.05 | -0.29 | -0.23 | -0.04 | -0.02 | 0.07 | 0.05 | 205. |
| 210. | -0.17 | -0.36 | -0.28 | -0.09 | -0.05 | 0.07 | 0.05 | 210. |
| 215. | -0.30 | -0.43 | -0.33 | -0.12 | -0.07 | 0.07 | 0.04 | 215. |
| 220. | -0.38 | -0.48 | -0.36 | -0.15 | -0.10 | 0.08 | 0.05 | 220. |
| 225. | -0.41 | -0.48 | -0.37 | -0.14 | -0.11 | 0.08 | 0.06 | 225. |
| 230. | -0.37 | -0.43 | -0.35 | -0.12 | -0.11 | 0.10 | 0.07 | 230. |
| 235. | -0.25 | -0.35 | -0.30 | -0.08 | -0.10 | 0.12 | 0.08 | 235. |
| 240. | -0.10 | -0.25 | -0.24 | -0.03 | -0.07 | 0.14 | 0.09 | 240. |
| 245. | 0.07 | -0.15 | 0.17 | 0.04 | -0.04 | 0.18 | 0.10 | 245. |
| 250. | 0.24 | -0.05 | 0.09 | 0.11 | -0.01 | 0.21 | 0.11 | 250. |
| 255. | 0.44 | 0.08 | 0.00 | 0.19 | 0.03 | 0.24 | 0.11 | 255. |
| 260. | 0.66 | 0.26 | 0.13 | 0.28 | 0.07 | 0.27 | 0.12 | 260. |
| 265. | 0.91 | 0.46 | 0.29 | 0.37 | 0.14 | 0.30 | 0.12 | 265. |
| 270. | 1.24 | 0.83 | 0.49 | 0.47 | 0.18 | 0.33 | 0.13 | 270. |
| 275. | 1.69 | 1.07 | 0.65 | 0.54 | 0.21 | 0.33 | 0.13 | 275. |
| 280. | 1.64 | 0.56 | 0.32 | 0.27 | 0.08 | 0.28 | 0.10 | 280. |
| 285. | -0.63 | -0.48 | -0.40 | -0.20 | -0.20 | 0.11 | 0.01 | 285. |
| 290. | -1.40 | -1.08 | -0.74 | -0.39 | -0.33 | 0.02 | -0.03 | 290. |
| 295. | -1.20 | -0.91 | -0.68 | -0.37 | -0.28 | 0.02 | 0.01 | 295. |
| 300. | -0.71 | -0.59 | -0.50 | -0.26 | -0.24 | 0.03 | 0.03 | 300. |
| 305. | -0.29 | -0.34 | -0.39 | -0.13 | -0.19 | 0.07 | 0.03 | 305. |
| 310. | -0.06 | -0.21 | -0.26 | -0.04 | -0.11 | 0.11 | 0.03 | 310. |
| 315. | -0.07 | 0.03 | -0.07 | 0.02 | -0.02 | 0.14 | 0.03 | 315. |
| 320. | 0.23 | 0.29 | 0.14 | 0.12 | 0.07 | 0.18 | 0.04 | 320. |
| 325. | 1.38 | 0.56 | 0.31 | 0.29 | 0.14 | 0.22 | 0.05 | 325. |
| 330. | 1.66 | 0.84 | 0.47 | 0.42 | 0.20 | 0.24 | 0.05 | 330. |
| 335. | 2.10 | 1.09 | 0.63 | 0.50 | 0.26 | 0.26 | 0.06 | 335. |
| 340. | 2.52 | 1.28 | 0.78 | 0.59 | 0.33 | 0.28 | 0.07 | 340. |
| 345. | 2.78 | 1.42 | 0.90 | 0.65 | 0.39 | 0.31 | 0.09 | 345. |
| 350. | 2.97 | 1.49 | 0.96 | 0.65 | 0.41 | 0.30 | 0.10 | 350. |
| 355. | 2.88 | 1.43 | 0.87 | 0.60 | 0.37 | 0.24 | 0.08 | 355. |

DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=505 CNTR NO. 354 ICN= 16. C.R.= 66.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.990 | 4.550 | 10.400 | DEG. |
| 0. | 0.03 | 0.01 | -0.02 | -0.00 | 0. |
| 5. | 0.04 | 0.03 | 0.00 | -0.00 | 5. |
| 10. | 0.22 | 0.09 | 0.03 | -0.00 | 10. |
| 15. | 0.36 | 0.14 | 0.05 | -0.01 | 15. |
| 20. | 0.28 | 0.12 | 0.05 | -0.01 | 20. |
| 25. | 0.20 | 0.09 | 0.03 | -0.01 | 25. |
| 30. | 0.17 | 0.07 | 0.00 | -0.02 | 30. |
| 35. | 0.19 | 0.07 | -0.01 | -0.02 | 35. |
| 40. | 0.24 | 0.08 | 0.00 | -0.02 | 40. |
| 45. | 0.25 | 0.07 | 0.02 | -0.03 | 45. |
| 50. | 0.22 | 0.04 | 0.02 | -0.02 | 50. |
| 55. | 0.20 | 0.06 | 0.02 | -0.02 | 55. |
| 60. | 0.24 | 0.11 | 0.05 | -0.01 | 60. |
| 65. | 0.31 | 0.13 | 0.07 | -0.01 | 65. |
| 70. | 0.37 | 0.14 | 0.08 | -0.01 | 70. |
| 75. | 0.34 | 0.13 | 0.07 | -0.00 | 75. |
| 80. | 0.30 | 0.12 | 0.06 | 0.00 | 80. |
| 85. | 0.25 | 0.11 | 0.06 | -0.00 | 85. |
| 90. | 0.25 | 0.11 | 0.05 | -0.01 | 90. |
| 95. | 0.25 | 0.11 | 0.05 | -0.01 | 95. |
| 100. | 0.26 | 0.11 | 0.05 | 0.00 | 100. |
| 105. | 0.27 | 0.11 | 0.05 | 0.01 | 105. |
| 110. | 0.27 | 0.11 | 0.05 | 0.00 | 110. |
| 115. | 0.26 | 0.11 | 0.05 | 0.00 | 115. |
| 120. | 0.24 | 0.10 | 0.05 | -0.00 | 120. |
| 125. | 0.23 | 0.09 | 0.05 | 0.01 | 125. |
| 130. | 0.21 | 0.08 | 0.05 | 0.01 | 130. |
| 135. | 0.19 | 0.06 | 0.05 | 0.01 | 135. |
| 140. | 0.17 | 0.05 | 0.04 | 0.01 | 140. |
| 145. | 0.14 | 0.05 | 0.03 | 0.01 | 145. |
| 150. | 0.12 | 0.04 | 0.03 | 0.01 | 150. |
| 155. | 0.10 | 0.04 | 0.03 | 0.02 | 155. |
| 160. | 0.09 | 0.04 | 0.03 | 0.02 | 160. |
| 165. | 0.09 | 0.03 | 0.02 | 0.02 | 165. |
| 170. | 0.09 | 0.02 | 0.02 | 0.01 | 170. |
| 175. | 0.09 | 0.02 | 0.02 | 0.01 | 175. |
| 180. | 0.09 | 0.02 | 0.02 | 0.02 | 180. |
| 185. | 0.09 | 0.03 | 0.02 | 0.02 | 185. |
| 190. | 0.09 | 0.04 | 0.02 | 0.01 | 190. |
| 195. | 0.08 | 0.05 | 0.02 | 0.01 | 195. |
| 200. | 0.07 | 0.06 | 0.02 | 0.00 | 200. |
| 205. | 0.06 | 0.05 | 0.02 | 0.01 | 205. |
| 210. | 0.05 | 0.05 | 0.02 | 0.02 | 210. |
| 215. | 0.01 | 0.03 | 0.01 | 0.01 | 215. |
| 220. | -0.03 | 0.01 | 0.00 | 0.00 | 220. |
| 225. | -0.07 | -0.00 | -0.01 | -0.00 | 225. |
| 230. | -0.11 | -0.01 | -0.02 | -0.00 | 230. |
| 235. | -0.15 | -0.03 | -0.03 | 0.00 | 235. |
| 240. | -0.19 | -0.05 | -0.04 | 0.00 | 240. |
| 245. | -0.21 | -0.07 | -0.05 | 0.00 | 245. |
| 250. | -0.23 | -0.09 | -0.06 | 0.00 | 250. |
| 255. | -0.25 | -0.09 | -0.05 | 0.00 | 255. |
| 260. | -0.26 | -0.10 | -0.07 | 0.00 | 260. |
| 265. | -0.28 | -0.11 | -0.07 | -0.00 | 265. |
| 270. | -0.30 | -0.13 | -0.07 | -0.01 | 270. |
| 275. | -0.33 | -0.15 | -0.07 | -0.01 | 275. |
| 280. | -0.36 | -0.17 | -0.06 | -0.01 | 280. |
| 285. | -0.38 | -0.18 | -0.05 | -0.01 | 285. |
| 290. | -0.38 | -0.18 | -0.07 | -0.00 | 290. |
| 295. | -0.39 | -0.17 | -0.09 | -0.00 | 295. |
| 300. | -0.42 | -0.16 | -0.09 | -0.00 | 300. |
| 305. | -0.52 | -0.15 | -0.08 | -0.01 | 305. |
| 310. | -0.52 | -0.15 | -0.07 | -0.00 | 310. |
| 315. | -0.47 | -0.15 | -0.08 | 0.00 | 315. |
| 320. | -0.46 | -0.17 | -0.06 | 0.01 | 320. |
| 325. | -0.44 | -0.19 | -0.03 | 0.00 | 325. |
| 330. | -0.41 | -0.17 | -0.02 | -0.01 | 330. |
| 335. | -0.35 | -0.13 | -0.03 | -0.01 | 335. |
| 340. | -0.28 | -0.12 | -0.04 | -0.00 | 340. |
| 345. | -0.19 | -0.13 | -0.04 | -0.00 | 345. |
| 350. | -0.10 | -0.12 | -0.04 | -0.00 | 350. |
| 355. | -0.02 | -0.07 | -0.05 | -0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-505 CNTR NO. 354 TCN= 16. C..L.= 66.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | | | C.J.R.D STATION | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.199 | 10.400 | DEG. |
| 0. | -0.09 | -0.08 | -0.10 | -0.06 | -0.05 | -0.03 | -0.04 | 0. |
| 5. | 0.07 | 0.02 | -0.01 | 0.00 | -0.01 | -0.01 | -0.04 | 5. |
| 10. | 0.13 | 0.09 | 0.03 | 0.04 | 0.02 | 0.00 | -0.03 | 10. |
| 15. | 0.14 | 0.11 | 0.04 | 0.03 | 0.03 | 0.00 | -0.02 | 15. |
| 20. | 0.18 | 0.10 | 0.09 | 0.02 | 0.03 | -0.01 | 0.00 | 20. |
| 25. | 0.12 | 0.04 | 0.01 | -0.00 | 0.02 | -0.01 | 0.01 | 25. |
| 30. | 0.04 | 0.05 | -0.03 | -0.01 | 0.01 | -0.02 | 0.03 | 30. |
| 35. | 0.11 | 0.11 | 0.01 | 0.02 | 0.03 | -0.01 | 0.04 | 35. |
| 40. | 0.17 | 0.10 | 0.09 | 0.03 | 0.05 | -0. 0 | 0.05 | 40. |
| 45. | 0.08 | 0.01 | -0.01 | 0.01 | 0.03 | -0.01 | 0.05 | 45. |
| 50. | -0.02 | -0.01 | -0.05 | -0.00 | 0.01 | -0.01 | 0.04 | 50. |
| 55. | -0.03 | -0.00 | -0.04 | -0.01 | 0.00 | -0.02 | 0.04 | 55. |
| 60. | -0.01 | -0.00 | -0.02 | -0.01 | 0.01 | -0.02 | 0.03 | 60. |
| 65. | 0.00 | 0.00 | -0.02 | -0.01 | 0.02 | -0.02 | 0.03 | 65. |
| 70. | 0.02 | 0.02 | -0.02 | -0.00 | 0.02 | -0.01 | 0.04 | 70. |
| 75. | 0.05 | 0.05 | 0.00 | 0.01 | 0.03 | -0.00 | 0.05 | 75. |
| 80. | 0.10 | 0.09 | 0.03 | 0.05 | 0.04 | 0.00 | 0.05 | 80. |
| 85. | 0.16 | 0.12 | 0.07 | 0.07 | 0.06 | 0.01 | 0.05 | 85. |
| 90. | 0.21 | 0.14 | 0.08 | 0.08 | 0.07 | 0.01 | 0.05 | 90. |
| 95. | 0.23 | 0.16 | 0.09 | 0.08 | 0.08 | 0.02 | 0.07 | 95. |
| 100. | 0.24 | 0.18 | 0.10 | 0.09 | 0.09 | 0.02 | 0.07 | 100. |
| 105. | 0.25 | 0.18 | 0.11 | 0.09 | 0.09 | 0.02 | 0.07 | 105. |
| 110. | 0.26 | 0.18 | 0.13 | 0.09 | 0.09 | 0.02 | 0.06 | 110. |
| 115. | 0.26 | 0.18 | 0.13 | 0.09 | 0.09 | 0.02 | 0.05 | 115. |
| 120. | 0.25 | 0.17 | 0.13 | 0.08 | 0.08 | 0.02 | 0.04 | 120. |
| 125. | 0.24 | 0.16 | 0.11 | 0.07 | 0.07 | 0.02 | 0.03 | 125. |
| 130. | 0.22 | 0.15 | 0.10 | 0.06 | 0.06 | 0.02 | 0.04 | 130. |
| 135. | 0.20 | 0.14 | 0.09 | 0.06 | 0.06 | 0.02 | 0.05 | 135. |
| 140. | 0.17 | 0.13 | 0.08 | 0.05 | 0.07 | 0.02 | 0.05 | 140. |
| 145. | 0.15 | 0.12 | 0.07 | 0.05 | 0.07 | 0.02 | 0.05 | 145. |
| 150. | 0.14 | 0.11 | 0.07 | 0.05 | 0.06 | 0.01 | 0.05 | 150. |
| 155. | 0.14 | 0.11 | 0.06 | 0.06 | 0.05 | 0.01 | 0.04 | 155. |
| 160. | 0.14 | 0.10 | 0.07 | 0.06 | 0.04 | 0.02 | 0.03 | 160. |
| 165. | 0.14 | 0.10 | 0.07 | 0.06 | 0.04 | 0.02 | 0.03 | 165. |
| 170. | 0.15 | 0.10 | 0.08 | 0.07 | 0.05 | 0.03 | 0.04 | 170. |
| 175. | 0.16 | 0.11 | 0.09 | 0.07 | 0.06 | 0.03 | 0.04 | 175. |
| 180. | 0.18 | 0.12 | 0.1 | 0.07 | 0.07 | 0.03 | 0.03 | 180. |
| 185. | 0.20 | 0.14 | 0.11 | 0.07 | 0.07 | 0.03 | 0.02 | 185. |
| 190. | 0.21 | 0.15 | 0.12 | 0.07 | 0.07 | 0.03 | 0.01 | 190. |
| 195. | 0.21 | 0.15 | 0.12 | 0.08 | 0.07 | 0.03 | 0.01 | 195. |
| 200. | 0.20 | 0.15 | 0.13 | 0.08 | 0.07 | 0.03 | 0.01 | 200. |
| 205. | 0.18 | 0.14 | 0.12 | 0.08 | 0.05 | 0.03 | 0.00 | 205. |
| 210. | 0.16 | 0.12 | 0.11 | 0.07 | 0.04 | 0.03 | -0.01 | 210. |
| 215. | 0.12 | 0.10 | 0.09 | 0.06 | 0.02 | 0.03 | -0.02 | 215. |
| 220. | 0.09 | 0.08 | 0.07 | 0.04 | 0.02 | 0.03 | -0.03 | 220. |
| 225. | 0.05 | 0.05 | 0.05 | 0.02 | 0.01 | 0.02 | -0.03 | 225. |
| 230. | 0.00 | 0.02 | 0.03 | 0.01 | -0.00 | 0.02 | -0.03 | 230. |
| 235. | -0.04 | -0.01 | 0.01 | -0.01 | -0.02 | 0.01 | -0.03 | 235. |
| 240. | -0.09 | -0.04 | -0.01 | -0.03 | -0.04 | 0.00 | -0.03 | 240 |
| 245. | -0.12 | -0.07 | -0.03 | -0.04 | -0.04 | -0.00 | -0.04 | 245. |
| 250. | -0.15 | -0.10 | -0.05 | -0.05 | -0.07 | -0.00 | -0.04 | 250. |
| 255. | -0.18 | -0.13 | -0.06 | -0.06 | -0.08 | -0.01 | -0.04 | 255. |
| 260. | -0.20 | -0.16 | -0.07 | -0.07 | -0.08 | -0.01 | -0.05 | 260. |
| 265. | -0.22 | -0.17 | -0.08 | -0.07 | -0.08 | -0.01 | -0.05 | 265. |
| 270. | -0.24 | -0.18 | -0.09 | -0.07 | -0.08 | -0.01 | -0.05 | 270. |
| 275. | -0.25 | -0.18 | -0.10 | -0.08 | -0.08 | -0.01 | -0.05 | 275. |
| 280. | -0.27 | -0.19 | -0.11 | -0.08 | -0.08 | -0.01 | -0.05 | 280. |
| 285. | -0.28 | -0.19 | -0.11 | -0.08 | -0.08 | -0.02 | -0.05 | 285. |
| 290. | -0.30 | -0.21 | -0.12 | -0.09 | -0.08 | -0.02 | -0.05 | 290. |
| 29 | -0.31 | -0.22 | -0.12 | -0.10 | -0.08 | -0.02 | -0.05 | 295. |
| 300. | -0.31 | -0.24 | -0.12 | -0.10 | -0.08 | -0.02 | -0.05 | 300. |
| 305. | -0.33 | -0.25 | -0.13 | -0.11 | -0.09 | -0.02 | -0.05 | 305. |
| 3 . | -0.34 | -0.24 | -0.14 | -0.11 | -0.09 | -0.03 | -0.03 | 310. |
| 315. | -0.34 | -0.23 | -0.14 | -0.11 | -0.10 | -0.03 | -0.05 | 315. |
| 320. | -0.31 | -0.20 | -0.12 | -0.10 | -0.09 | -0.03 | -0.05 | 320. |
| 325. | -0.20 | -0.15 | -0.09 | -0.08 | -0.08 | -0.02 | -0.05 | 325. |
| 330. | -0.13 | -0.12 | -0.06 | -0.06 | -0.07 | -0.02 | -0.04 | 330. |
| 335. | -0.20 | -0.16 | -0.10 | -0.08 | -0.08 | -0.02 | -0.04 | 335. |
| 340. | -0.35 | -0.24 | -0.17 | -0.12 | -0.10 | -0.04 | -0.06 | 340. |
| 345. | -0.47 | -0.33 | -0.21 | -0.14 | -0.11 | -0.05 | -0.07 | 345. |
| 350. | -0.47 | -0.35 | -0.24 | -0.17 | -0.14 | -0.06 | -0.08 | 350. |
| 355. | -0.29 | -0.23 | -0.19 | -0.13 | -0.11 | -0.05 | -0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-505 CNTR NO. 354 TCH= 16. C.R.= 66.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.16 | -0.11 | -0.10 | -0.05 | -0.06 | -0.02 | -0.01 | 0. |
| 5. | -0.07 | -0.10 | -0.04 | -0.01 | -0.03 | -0.01 | -0.00 | 5. |
| 10. | 0.05 | 0.03 | 0.01 | 0.01 | 0.01 | -0.02 | -0.01 | 10. |
| 15. | -0.09 | -0.08 | -0.05 | -0.03 | 0.01 | -0.04 | -0.01 | 15. |
| 20. | -0.16 | -0.12 | -0.08 | -0.07 | -0.01 | -0.04 | -0.02 | 20. |
| 25. | -0.10 | -0.07 | -0.06 | -0.05 | -0.02 | -0.04 | -0.03 | 25. |
| 30. | -0.13 | -0.12 | -0.09 | -0.06 | -0.03 | -0.05 | -0.0 | 30. |
| 35. | -0.18 | -0.17 | -0.12 | -0.08 | -0.04 | -0.05 | -0.0 | 35. |
| 40. | -0.18 | -0.14 | -0.13 | -0.10 | -0.05 | -0.05 | -0.03 | 40. |
| 45. | -0.15 | -0.13 | -0.13 | -0.12 | -0.05 | -0.06 | -0.04 | 45. |
| 50. | -0.09 | -0.21 | -0.14 | -0.12 | -0.05 | -0.08 | -0.04 | 50. |
| 55. | -0.04 | -0.19 | -0.14 | -0.11 | -0.05 | -0.07 | -0.05 | 55. |
| 60. | 0.01 | -0.12 | -0.12 | -0.09 | -0.04 | -0.06 | -0.04 | 60. |
| 65. | 0.06 | -0.04 | -0.08 | -0.06 | -0.03 | -0.05 | -0.03 | 65. |
| 70. | 0.11 | -0.01 | -0.04 | -0.03 | -0.02 | -0.04 | -0.03 | 70. |
| 75. | 0.16 | 0.02 | 0.01 | 0.00 | -0.00 | -0.04 | -0.03 | 75. |
| 80. | 0.21 | 0.06 | 0.04 | 0.03 | 0.02 | -0.03 | -0.03 | 80. |
| 85. | 0.28 | 0.11 | 0.07 | 0.05 | 0.04 | -0.02 | -0.03 | 85. |
| 90. | 0.34 | 0.15 | 0.09 | 0.06 | 0.06 | -0.02 | -0.02 | 90. |
| 95. | 0.40 | 0.18 | 0.11 | 0.06 | 0.07 | -0.01 | -0.01 | 95. |
| 100. | 0.43 | 0.19 | 0.12 | 0.06 | 0.09 | -0.01 | -0.02 | 100. |
| 105. | 0.43 | 0.20 | 0.12 | 0.07 | 0.10 | -0.01 | -0.02 | 105. |
| 110. | 0.42 | 0.19 | 0.12 | 0.07 | 0.10 | -0.02 | -0.02 | 110. |
| 115. | 0.39 | 0.17 | 0.12 | 0.06 | 0.10 | -0.02 | -0.02 | 115. |
| 120. | 0.33 | 0.14 | 0.11 | 0.06 | 0.10 | -0.01 | -0.01 | 120. |
| 125. | 0.27 | 0.11 | 0.09 | 0.05 | 0.09 | -0.00 | -0.01 | 125. |
| 130. | 0.22 | 0.09 | 0.08 | 0.05 | 0.08 | 0.00 | -0.01 | 130. |
| 135. | 0.18 | 0.08 | 0.06 | 0.04 | 0.06 | 0.00 | -0.01 | 135. |
| 140. | 0.16 | 0.06 | 0.04 | 0.02 | 0.05 | 0.00 | -0.01 | 140. |
| 145. | 0.14 | 0.05 | 0.02 | 0.01 | 0.04 | -0.00 | -0.01 | 145. |
| 150. | 0.12 | 0.04 | 0.01 | -0.00 | 0.03 | -0.00 | -0.01 | 150. |
| 155. | 0.11 | 0.03 | 0.01 | -0.00 | 0.03 | 0.00 | -0.01 | 155. |
| 160. | 0.11 | 0.04 | 0.00 | -0.00 | 0.03 | 0.00 | -0.01 | 160. |
| 165. | 0.11 | 0.06 | 0.01 | 0.01 | 0.03 | 0.01 | -0.00 | 165. |
| 170. | 0.11 | 0.08 | 0.02 | 0.02 | 0.04 | 0.01 | 0.01 | 170. |
| 175. | 0.11 | 0.10 | 0.03 | 0.03 | 0.04 | 0.02 | 0.01 | 175. |
| 180. | 0.12 | 0.12 | 0.05 | 0.04 | 0.06 | 0.03 | 0.02 | 180. |
| 185. | 0.13 | 0.14 | 0.07 | 0.05 | 0.07 | 0.04 | 0.02 | 185. |
| 190. | 0.14 | 0.15 | 0.09 | 0.06 | 0.07 | 0.04 | 0.02 | 190. |
| 195. | 0.14 | 0.16 | 0.10 | 0.07 | 0.08 | 0.05 | 0.03 | 195. |
| 200. | 0.15 | 0.16 | 0.12 | 0.07 | 0.08 | 0.05 | 0.03 | 200. |
| 205. | 0.14 | 0.15 | 0.12 | 0.08 | 0.07 | 0.05 | 0.03 | 205. |
| 210. | 0.13 | 0.14 | 0.11 | 0.08 | 0.06 | 0.05 | 0.03 | 210. |
| 215. | 0.11 | 0.13 | 0.10 | 0.08 | 0.05 | 0.05 | 0.03 | 215. |
| 220. | 0.08 | 0.11 | 0.09 | 0.07 | 0.04 | 0.04 | 0.03 | 220. |
| 225. | 0.03 | 0.09 | 0.07 | 0.06 | 0.02 | 0.04 | 0.04 | 225. |
| 230. | -0.01 | 0.07 | 0.06 | 0.06 | 0.01 | 0.04 | 0.03 | 230. |
| 235. | -0.05 | 0.05 | 0.05 | 0.04 | -0.01 | 0.03 | 0.03 | 235. |
| 240. | -0.09 | 0.03 | 0.04 | 0.03 | -0.02 | 0.03 | 0.02 | 240. |
| 245. | -0.12 | 0.01 | 0.02 | 0.02 | -0.03 | 0.03 | 0.02 | 245. |
| 250. | -0.15 | -0.01 | 0.01 | 0.01 | -0.03 | 0.03 | 0.02 | 250. |
| 255. | -0.17 | -0.03 | 0.00 | -0.00 | -0.04 | 0.03 | 0.03 | 255. |
| 260. | -0.19 | -0.04 | -0.02 | -0.00 | -0.04 | 0.03 | 0.02 | 260. |
| 265. | -0.20 | -0.05 | -0.01 | -0.00 | -0.04 | 0.03 | 0.02 | 265. |
| 270. | -0.21 | -0.05 | -0.01 | -0.01 | -0.04 | 0.03 | 0.02 | 270. |
| 275. | -0.20 | -0.05 | -0.01 | -0.00 | -0.04 | 0.03 | 0.02 | 275. |
| 280. | -0.20 | -0.05 | -0.01 | -0.00 | -0.04 | 0.03 | 0.03 | 280. |
| 285. | -0.19 | -0.05 | -0.01 | 0.00 | -0.04 | 0.03 | 0.03 | 285. |
| 290. | -0.19 | -0.04 | -0.01 | 0.00 | -0.04 | 0.03 | 0.02 | 290. |
| 295. | -0.17 | -0.02 | -0.00 | 0.01 | -0.05 | 0.02 | 0.01 | 295. |
| 300. | -0.16 | -0.01 | 0.00 | 0.02 | -0.05 | 0.02 | 0.01 | 300. |
| 305. | -0.16 | -0.01 | -0.00 | 0.00 | -0.05 | 0.02 | 0.01 | 305. |
| 310. | -0.17 | -0.03 | -0.01 | -0.01 | -0.05 | 0.02 | 0.01 | 310. |
| 315. | -0.21 | -0.01 | -0.03 | -0.02 | -0.05 | 0.01 | 0.01 | 315. |
| 320. | -0.26 | -0.13 | -0.06 | -0.05 | -0.06 | 0.00 | 0.01 | 320. |
| 325. | -0.31 | -0.18 | -0.10 | -0.06 | -0.07 | -0.00 | 0.01 | 325. |
| 330. | -0.37 | -0.24 | -0.13 | -0.08 | -0.08 | -0.01 | 0.00 | 330. |
| 335. | -0.39 | -0.27 | -0.16 | -0.10 | -0.10 | -0.02 | -0.00 | 335. |
| 340. | -0.34 | -0.23 | -0.17 | -0.10 | -0.10 | -0.02 | -0.00 | 340. |
| 345. | -0.25 | -0.13 | -0.13 | -0.07 | -0.09 | -0.01 | -0.00 | 345. |
| 350. | -0.16 | -0.07 | -0.09 | -0.05 | -0.08 | -0.01 | -0.01 | 350. |
| 355. | -0.14 | -0.19 | -0.10 | -0.04 | -0.07 | -0.04 | -0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-305 CNTR NO. 354 TCN= 16. C.R.= 66.0

DIFFERENTIAL PRESSURES

SPAN STATION 193.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.958 | 2.990 | 4.590 | 7.150 | 10.400 | DEG. |
| 0. | -0.19 | -0.30 | -0.11 | -0.12 | -0.09 | -0.01 | -0.01 | 0. |
| 5. | -0.52 | -0.45 | -0.18 | -0.12 | -0.07 | -0.01 | 0.01 | 5. |
| 10. | -0.25 | -0.17 | -0.14 | -0.00 | -0.06 | -0.01 | 0.00 | 10. |
| 15. | -0.16 | -0.09 | -0.06 | -0.07 | -0.06 | -0.03 | -0.02 | 15. |
| 20. | -0.20 | -0.09 | -0.07 | -0.10 | -0.04 | -0.04 | -0.02 | 20. |
| 25. | -0.18 | -0.04 | -0.00 | -0.07 | -0.05 | -0.04 | -0.03 | 25. |
| 30. | -0.27 | -0.05 | -0.11 | -0.00 | -0.04 | -0.05 | -0.03 | 30. |
| 35. | -0.36 | -0.10 | -0.13 | -0.11 | -0.05 | -0.05 | -0.03 | 35. |
| 40. | -0.32 | -0.15 | -0.15 | 0.11 | -0.06 | -0.07 | -0.03 | 40. |
| 45. | -0.19 | -0.09 | -0.16 | -0.10 | -0.07 | -0.00 | -0.03 | 45. |
| 50. | -0.14 | -0.00 | -0.17 | -0.08 | -0.06 | -0.09 | -0.04 | 50. |
| 55. | -0.12 | 0.09 | -0.17 | -0.05 | -0.04 | -0.09 | -0.04 | 55. |
| 60. | -0.12 | 0.06 | -0.14 | -0.04 | -0.02 | -0.08 | -0.03 | 60. |
| 65. | -0.09 | 0.10 | -0.09 | -0.03 | 0.00 | -0.07 | -0.03 | 65. |
| 70. | -0.05 | 0.14 | -0.05 | -0.01 | 0.03 | -0.06 | -0.03 | 70. |
| 75. | 0.04 | 0.17 | -0.00 | 0.02 | 0.05 | -0.05 | -0.02 | 75. |
| 80. | 0.10 | 0.20 | 0.03 | 0.04 | 0.07 | -0.04 | -0.02 | 80. |
| 85. | 0.15 | 0.24 | 0.06 | 0.10 | 0.09 | -0.03 | -0.02 | 85. |
| 90. | 0.19 | 0.29 | 0.07 | 0.13 | 0.10 | -0.04 | -0.02 | 90. |
| 95. | 0.22 | 0.31 | 0.09 | 0.14 | 0.11 | -0.04 | -0.02 | 95. |
| 100. | 0.23 | 0.34 | 0.10 | 0.15 | 0.11 | -0.04 | -0.03 | 100. |
| 105. | 0.23 | 0.37 | 0.10 | 0.15 | 0.11 | -0.05 | -0.03 | 105. |
| 110. | 0.22 | 0.38 | 0.10 | 0.15 | 0.11 | -0.05 | -0.03 | 110. |
| 115. | 0.20 | 0.32 | 0.10 | 0.15 | 0.11 | -0.05 | -0.02 | 115. |
| 120. | 0.17 | 0.26 | 0.08 | 0.14 | 0.11 | -0.05 | -0.02 | 120. |
| 125. | 0.12 | 0.21 | 0.05 | 0.13 | 0.11 | -0.04 | -0.01 | 125. |
| 130. | 0.06 | 0.18 | 0.03 | 0.11 | 0.09 | -0.04 | -0.01 | 130. |
| 135. | 0.01 | 0.14 | -0.00 | 0.09 | 0.08 | -0.04 | -0.01 | 135. |
| 140. | -0.02 | 0.15 | -0.03 | 0.07 | 0.07 | -0.03 | -0.01 | 140. |
| 145. | -0.10 | 0.15 | -0.06 | 0.05 | 0.06 | -0.03 | -0.02 | 145. |
| 150. | -0.14 | 0.11 | -0.08 | 0.00 | 0.04 | -0.03 | -0.03 | 150. |
| 155. | -0.18 | 0.05 | -0.09 | 0.02 | 0.02 | -0.03 | -0.03 | 155. |
| 160. | -0.20 | 0.00 | -0.10 | 0.02 | -0.00 | -0.03 | -0.03 | 160. |
| 165. | -0.21 | -0.01 | -0.10 | 0.01 | -0.01 | -0.03 | -0.02 | 165. |
| 170. | -0.21 | 0.07 | -0.10 | 0.00 | -0.01 | -0.03 | -0.02 | 170. |
| 175. | -0.20 | 0.10 | -0.09 | -0.02 | -0.01 | -0.04 | -0.01 | 175. |
| 180. | -0.18 | 0.23 | -0.08 | -0.03 | -0.00 | -0.03 | -0.01 | 180. |
| 185. | -0.16 | 0.23 | -0.06 | -0.02 | 0.00 | -0.02 | -0.00 | 185. |
| 190. | -0.12 | 0.23 | -0.04 | -0.00 | 0.01 | -0.00 | 0.01 | 190. |
| 195. | -0.07 | 0.22 | -0.02 | 0.01 | 0.02 | 0.01 | 0.01 | 195. |
| 200. | -0.01 | 0.21 | 0.01 | 0.03 | 0.02 | 0.02 | 0.02 | 200. |
| 205. | 0.04 | 0.19 | 0.03 | 0.04 | 0.03 | 0.04 | 0.02 | 205. |
| 210. | 0.08 | 0.15 | 0.05 | 0.05 | 0.03 | 0.04 | 0.02 | 210. |
| 215. | 0.09 | 0.10 | 0.07 | 0.05 | 0.02 | 0.05 | 0.02 | 215. |
| 220. | 0.10 | 0.03 | 0.06 | 0.05 | 0.01 | 0.05 | 0.02 | 220. |
| 225. | 0.11 | -0.04 | 0.06 | 0.04 | -0.00 | 0.05 | 0.02 | 225. |
| 230. | 0.11 | -0.09 | 0.06 | 0.03 | -0.01 | 0.04 | 0.02 | 230. |
| 235. | 0.12 | -0.12 | 0.08 | 0.02 | -0.01 | 0.06 | 0.02 | 235. |
| 240. | 0.12 | -0.12 | 0.08 | 0.02 | -0.01 | 0.06 | 0.02 | 240. |
| 245. | 0.11 | -0.12 | 0.08 | 0.00 | -0.02 | 0.06 | 0.02 | 245. |
| 250. | 0.09 | -0.13 | 0.07 | -0.01 | -0.02 | 0.07 | 0.03 | 250. |
| 255. | 0.08 | -0.15 | 0.06 | -0.05 | -0.03 | 0.07 | 0.03 | 255. |
| 260. | 0.07 | -0.16 | 0.06 | -0.04 | -0.03 | 0.07 | 0.03 | 260. |
| 265. | 0.07 | -0.19 | 0.04 | -0.05 | -0.02 | 0.07 | 0.03 | 265. |
| 270. | 0.07 | -0.19 | 0.04 | -0.02 | -0.04 | 0.07 | 0.03 | 270. |
| 275. | 0.09 | -0.20 | 0.10 | -0.01 | -0.05 | 0.07 | 0.03 | 275. |
| 280. | 0.11 | -0.19 | 0.10 | -0.01 | -0.03 | 0.07 | 0.03 | 280. |
| 285. | 0.13 | -0.19 | 0.10 | -0.01 | -0.02 | 0.07 | 0.03 | 285. |
| 290. | 0.14 | -0.19 | 0.09 | -0.01 | -0.02 | 0.08 | 0.03 | 290. |
| 295. | 0.15 | -0.18 | 0.09 | -0.02 | -0.02 | 0.08 | 0.03 | 295. |
| 300. | 0.16 | -0.18 | 0.08 | -0.02 | -0.02 | 0.08 | 0.03 | 300. |
| 305. | 0.16 | -0.18 | 0.08 | -0.02 | -0.02 | 0.08 | 0.03 | 305. |
| 310. | 0.15 | -0.18 | 0.07 | -0.02 | -0.02 | 0.07 | 0.03 | 310. |
| 315. | 0.14 | -0.18 | 0.06 | -0.01 | -0.03 | 0.07 | 0.03 | 315. |
| 320. | 0.12 | -0.18 | 0.05 | -0.01 | -0.04 | 0.06 | 0.03 | 320. |
| 325. | 0.09 | -0.17 | 0.04 | -0.01 | -0.05 | 0.06 | 0.02 | 325. |
| 330. | 0.06 | -0.19 | 0.03 | -0.04 | -0.06 | 0.05 | 0.02 | 330. |
| 335. | 0.03 | -0.23 | 0.02 | -0.07 | -0.06 | 0.04 | 0.02 | 335. |
| 340. | 0.04 | -0.24 | 0.01 | -0.08 | -0.06 | 0.03 | 0.02 | 340. |
| 345. | 0.18 | -0.19 | -0.01 | -0.08 | -0.06 | 0.05 | 0.02 | 345. |
| 350. | 0.09 | -0.16 | -0.05 | -0.09 | -0.06 | 0.02 | 0.01 | 350. |
| 355. | -0.01 | -0.18 | -0.06 | -0.10 | -0.07 | -0.06 | -0.00 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-505 CNTR NO. 354 TCM= 16. C.R.= 64.0

DIFFERENTIAL PRESSURES

SPAN STATION 170.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.959 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.24 | -0.20 | -0.10 | -0.05 | -0.05 | -0.03 | -0.00 | 0. |
| 5. | -0.19 | -0.16 | -0.10 | -0.05 | -0.05 | -0.02 | 0.00 | 5. |
| 10. | -0.09 | -0.08 | -0.11 | -0.05 | -0.06 | -0.03 | 0.00 | 10. |
| 15. | -0.10 | -0.14 | -0.17 | -0.09 | -0.09 | -0.04 | 0.00 | 15. |
| 20. | -0.36 | -0.24 | -0.25 | -0.07 | -0.14 | -0.07 | -0.01 | 20. |
| 25. | -0.47 | -0.33 | -0.32 | -0.10 | -0.10 | -0.10 | -0.02 | 25. |
| 30. | -0.46 | -0.31 | -0.33 | -0.13 | -0.17 | -0.10 | -0.02 | 30. |
| 35. | -0.38 | -0.26 | -0.27 | -0.13 | -0.15 | -0.09 | -0.02 | 35. |
| 40. | -0.29 | -0.20 | -0.20 | -0.11 | -0.13 | -0.08 | -0.02 | 40. |
| 45. | -0.14 | -0.10 | -0.17 | -0.11 | -0.12 | -0.09 | -0.02 | 45. |
| 50. | -0.14 | -0.20 | -0.20 | -0.11 | -0.13 | -0.10 | -0.02 | 50. |
| 55. | -0.17 | -0.21 | -0.23 | -0.12 | -0.14 | -0.10 | -0.02 | 55. |
| 60. | -0.17 | -0.21 | -0.23 | -0.12 | -0.13 | -0.09 | -0.02 | 60. |
| 65. | -0.13 | -0.18 | -0.19 | -0.11 | -0.11 | -0.08 | -0.02 | 65. |
| 70. | -0.06 | -0.14 | -0.14 | -0.09 | -0.09 | -0.07 | -0.02 | 70. |
| 75. | 0.02 | -0.09 | -0.08 | -0.07 | -0.06 | -0.05 | -0.01 | 75. |
| 80. | 0.10 | -0.05 | -0.04 | -0.05 | -0.03 | -0.03 | -0.01 | 80. |
| 85. | 0.18 | -0.01 | 0.03 | -0.04 | -0.01 | -0.02 | -0.01 | 85. |
| 90. | 0.22 | 0.02 | 0.04 | -0.02 | 0.01 | -0.00 | -0.00 | 90. |
| 95. | 0.24 | 0.05 | 0.06 | -0.01 | 0.02 | 0.00 | -0.00 | 95. |
| 100. | 0.24 | 0.06 | 0.07 | 0.02 | 0.03 | 0.01 | -0.00 | 100. |
| 105. | 0.24 | 0.07 | 0.07 | [illegible] | 0.03 | 0.01 | 0.00 | 105. |
| 110. | 0.23 | 0.06 | 0.06 | 0 | 0.03 | 0.01 | 0.00 | 110. |
| 115. | 0.22 | 0.05 | 0.05 | 0 | 0.02 | 0.00 | 0.01 | 115. |
| 120. | 0.18 | -0.01 | 0.01 | 0 | -0.01 | -0.01 | 0.01 | 120. |
| 125. | 0.12 | -0.06 | -0.03 | 0.04 | -0.03 | -0.02 | 0.01 | 125. |
| 130. | 0.05 | -0.11 | -0.08 | -0.01 | -0.06 | -0.03 | 0.00 | 130. |
| 135. | -0.02 | -0.15 | -0.14 | -0.06 | -0.08 | -0.03 | -0.01 | 135. |
| 140. | -0.10 | -0.18 | -0.18 | -0.09 | -0.10 | -0.05 | -0.02 | 140. |
| 145. | -0.17 | -0.21 | -0.22 | -0.10 | -0.11 | -0.05 | -0.02 | 145. |
| 150. | -0.23 | -0.24 | -0.25 | -0.11 | -0.12 | -0.06 | -0.02 | 150. |
| 155. | -0.28 | -0.26 | -0.27 | -0.11 | -0.13 | -0.07 | -0.03 | 155. |
| 160. | -0.31 | -0.28 | -0.29 | -0.12 | -0.14 | -0.07 | -0.03 | 160. |
| 165. | -0.33 | -0.29 | -0.29 | -0.14 | -0.15 | -0.08 | -0.03 | 165. |
| 170. | -0.34 | -0.29 | -0.28 | -0.13 | -0.15 | -0.07 | -0.03 | 170. |
| 175. | -0.34 | -0.28 | -0.26 | -0.13 | -0.14 | -0.06 | -0.02 | 175. |
| 180. | -0.33 | -0.26 | -0.24 | -0.09 | -0.13 | -0.05 | -0.02 | 180. |
| 185. | -0.31 | -0.23 | -0.21 | -0.07 | -0.11 | -0.04 | -0.02 | 185. |
| 190. | -0.27 | -0.19 | -0.17 | -0.06 | -0.08 | -0.04 | -0.01 | 190. |
| 195. | -0.21 | -0.15 | -0.13 | -0.06 | -0.05 | -0.02 | -0.01 | 195. |
| 200. | -0.14 | -0.10 | -0.08 | -0.04 | -0.02 | -0.00 | -0.01 | 200. |
| 205. | -0.06 | -0.05 | -0.02 | -0.01 | 0.01 | 0.02 | -0.00 | 205. |
| 210. | 0.02 | -0.00 | 0.04 | 0.02 | 0.04 | 0.03 | 0.00 | 210. |
| 215. | 0.08 | 0.05 | 0.10 | 0.04 | 0.06 | 0.04 | 0.01 | 215. |
| 220. | 0.14 | 0.10 | 0.16 | 0.05 | 0.09 | 0.05 | 0.01 | 220. |
| 225. | 0.18 | 0.14 | 0.19 | 0.06 | 0.11 | 0.06 | 0.01 | 225. |
| 230. | 0.22 | 0.19 | 0.22 | 0.07 | 0.12 | 0.06 | 0.01 | 230. |
| 235. | 0.24 | 0.22 | 0.25 | 0.08 | 0.14 | 0.07 | 0.01 | 235. |
| 240. | 0.26 | 0.26 | 0.27 | 0.09 | 0.15 | 0.07 | 0.02 | 240. |
| 245. | 0.27 | 0.28 | 0.28 | 0.11 | 0.16 | 0.08 | 0.02 | 245. |
| 250. | 0.27 | 0.30 | 0.29 | 0.12 | 0.17 | 0.08 | 0.02 | 250. |
| 255. | 0.27 | 0.32 | 0.31 | 0.13 | 0.18 | 0.09 | 0.03 | 255. |
| 260. | 0.26 | 0.33 | 0.32 | 0.14 | 0.19 | 0.11 | 0.03 | 260. |
| 265. | 0.25 | 0.34 | 0.32 | 0.14 | 0.18 | 0.11 | 0.03 | 265. |
| 270. | 0.25 | 0.34 | 0.33 | 0.15 | 0.18 | 0.10 | 0.03 | 270. |
| 275. | 0.25 | 0.34 | 0.33 | 0.15 | 0.17 | 0.09 | 0.03 | 275. |
| 280. | 0.26 | 0.34 | 0.32 | 0.15 | 0.17 | 0.09 | 0.03 | 280. |
| 285. | 0.26 | 0.34 | 0.31 | 0.15 | 0.17 | 0.10 | 0.03 | 285. |
| 290. | 0.27 | 0.34 | 0.30 | 0.15 | 0.16 | 0.10 | 0.03 | 290. |
| 295. | 0.27 | 0.35 | 0.28 | 0.14 | 0.16 | 0.10 | 0.02 | 295. |
| 300. | 0.26 | 0.32 | 0.26 | 0.14 | 0.15 | 0.09 | 0.02 | 300. |
| 305. | 0.22 | 0.30 | 0.24 | 0.13 | 0.13 | 0.08 | 0.02 | 305. |
| 310. | 0.19 | 0.28 | 0.22 | 0.12 | 0.11 | 0.07 | 0.02 | 310. |
| 315. | 0.15 | 0.24 | 0.19 | 0.10 | 0.10 | 0.06 | 0.02 | 315. |
| 320. | 0.14 | 0.23 | 0.17 | 0.07 | 0.09 | 0.05 | 0.02 | 320. |
| 325. | 0.12 | 0.20 | 0.14 | 0.05 | 0.08 | 0.04 | 0.01 | 325. |
| 330. | 0.11 | 0.16 | 0.10 | 0.04 | 0.07 | 0.03 | 0.01 | 330. |
| 335. | 0.04 | 0.09 | 0.07 | 0.03 | 0.05 | 0.04 | 0.01 | 335. |
| 340. | -0.00 | 0.01 | 0.03 | 0.04 | 0.02 | 0.02 | 0.00 | 340. |
| 345. | -0.14 | -0.05 | -0.01 | 0.00 | -0.02 | -0.00 | -0.00 | 345. |
| 350. | -0.14 | -0.00 | -0.05 | -0.03 | -0.04 | -0.02 | -0.00 | 350. |
| 355. | -0.11 | -0.04 | -0.00 | -0.05 | -0.05 | -0.03 | -0.00 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-505 CNTR NO. 354 TCN= 16. C.R.= 66.3

DIFFERENTIAL PRESSURES

SPAN STATION 189.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.45 | -0.29 | -0.21 | -0.10 | -0.23 | -0.02 | -0.00 | 0. |
| 5. | -0.47 | -0.27 | -0.16 | -0.05 | -0.14 | -0.01 | -0.0: | 5. |
| 10. | -0.35 | -0.18 | -0.10 | -0.01 | -0.09 | -0.01 | -0.01 | 10. |
| 15. | -0.16 | -0.10 | -0.04 | -0.00 | -0.04 | -0.02 | -0.01 | 15. |
| 20. | -0.22 | -0.25 | -0.08 | -0.08 | -0.06 | -0.04 | -0.02 | 20. |
| 25. | -0.45 | -0.37 | -0.23 | -0.20 | -0.11 | -0.07 | -0.04 | 25. |
| 30. | -0.60 | -0.46 | -0.30 | -0.26 | -0.13 | -0.10 | -0.05 | 30. |
| 35. | -0.65 | -0.39 | -0.25 | -0.21 | -0.12 | -0.08 | -0.04 | 35. |
| 40. | -0.50 | -0.26 | -0.18 | -0.13 | -0.09 | -0.06 | -0.04 | 40. |
| 45. | -0.31 | -0.24 | -0.20 | -0.11 | -0.07 | -0.07 | -0.04 | 45. |
| 50. | -0.27 | -0.26 | -0.24 | -0.15 | -0.06 | -0.09 | -0.05 | 50. |
| 55. | -0.28 | -0.26 | -0.27 | -0.20 | -0.04 | -0.10 | -0.05 | 55. |
| 60. | -0.30 | -0.22 | -0.25 | -0.21 | -0.02 | -0.10 | -0.04 | 60. |
| 65. | -0.25 | -0.17 | -0.19 | -0.18 | 0.02 | -0.10 | -0.04 | 65. |
| 70. | -0.15 | -0.10 | -0.12 | -0.13 | 0.07 | -0.09 | -0.04 | 70. |
| 75. | -0.04 | -0.02 | -0.05 | -0.07 | 0.13 | -0.07 | -0.04 | 75. |
| 80. | 0.07 | 0.06 | 0.02 | -0.01 | 0.17 | -0.05 | -0.02 | 80. |
| 85. | 0.16 | 0.13 | 0.08 | 0.02 | 0.22 | -0.04 | -0.02 | 85. |
| 90. | 0.24 | 0.17 | 0.13 | 0.05 | 0.26 | -0.03 | -0.02 | 90. |
| 95. | 0.30 | 0.20 | 0.16 | 0.08 | 0.29 | -0.03 | -0.02 | 95. |
| 100. | 0.33 | 0.21 | 0.17 | 0.09 | 0.33 | -0.03 | -0.01 | 100. |
| 105. | 0.31 | 0.20 | 0.17 | 0.08 | 0.36 | -0.04 | -0.01 | 105. |
| 110. | 0.27 | 0.17 | 0.15 | 0.07 | 0.38 | -0.05 | -0.01 | 110. |
| 115. | 0.21 | 0.12 | 0.11 | 0.05 | 0.39 | -0.06 | -0.01 | 115. |
| 120. | 0.14 | 0. 7 | 0.06 | 0.02 | 0.38 | -0.07 | -0.01 | 120. |
| 125. | 0.05 | -0.00 | 0.01 | -0.01 | 0.36 | -0.08 | -0.02 | 125. |
| 130. | -0.05 | -0.08 | -0.05 | -0.05 | 0.33 | -0.08 | -0.03 | 130. |
| 135. | -0.14 | -0.17 | -0.10 | -0.09 | 0.28 | -0.09 | -0.04 | 135. |
| 140. | -0.23 | -0.26 | -0.15 | -0.13 | 0.22 | -0.10 | -0.04 | 140. |
| 145. | -0.33 | -0.35 | -0.20 | -0.17 | 0.15 | -0.10 | -0.04 | 145. |
| 150. | -0.42 | -0.43 | -0.24 | -0.21 | 0.08 | -0.10 | -0.04 | 150. |
| 155. | -0.50 | -0.50 | -0.28 | -0.24 | 0.02 | -0.11 | -0.04 | 155. |
| 160. | -0.57 | -0.55 | -0.31 | -0.25 | -0.01 | -0.11 | -0.05 | 160. |
| 165. | -0.63 | -0.58 | -0.33 | -0.26 | -0.05 | -0.11 | -0.04 | 165. |
| 170. | -0.68 | -0.59 | -0.34 | -0.26 | -0.07 | -0.10 | -0.04 | 170. |
| 175. | -0.69 | -0.59 | -0.34 | -0.26 | -0.09 | -0.09 | -0.03 | 175. |
| 180. | -0.66 | -0.56 | -0.32 | -0.23 | -0.10 | -0.08 | -0.03 | 180. |
| 185. | -0.62 | -0.52 | -0.29 | -0.21 | -0.11 | -0.07 | -0.02 | 185. |
| 190. | -0.55 | -0.45 | -0.24 | -0.17 | -0.12 | -0.05 | -0.01 | 190. |
| 195. | -0.47 | -0.37 | -0.19 | -0.13 | -0.12 | -0.03 | -0.01 | 195. |
| 200. | -0.36 | -0.26 | -0.13 | -0.09 | -0.11 | -0.01 | -0.00 | 200. |
| 205. | -0.24 | -0.14 | -0.06 | -0.05 | -0.09 | 0.02 | 0.00 | 205. |
| 210. | -0.11 | -0.02 | 0.02 | -0.01 | -0.06 | 0.03 | 0.01 | 210. |
| 215. | 0.02 | 0.10 | 0.09 | 0.04 | -0.00 | 0.05 | 0.01 | 215. |
| 220. | 0.15 | 0.21 | 0.16 | 0.08 | -0.05 | 0.06 | 0.02 | 220. |
| 225. | 0.25 | 0.28 | 0.22 | 0.12 | -0.04 | 0.07 | 0.02 | 225. |
| 230. | 0.34 | 0.35 | 0.26 | 0.15 | -0.04 | 0.06 | 0.03 | 230. |
| 235. | 0.42 | 0.40 | 0.29 | 0.18 | -0.04 | 0.09 | 0.04 | 235. |
| 240. | 0.49 | 0.44 | 0.32 | 0.21 | -0.04 | 0.11 | 0.04 | 240. |
| 245. | 0.54 | 0.48 | 0.34 | 0.23 | -0.03 | 0.12 | 0.04 | 245. |
| 250. | 0.58 | 0.50 | 0.35 | 0.24 | -0.02 | 0.12 | 0.04 | 250. |
| 255. | 0.61 | 0.52 | 0.36 | 0.26 | -0.01 | 0.13 | 0.05 | 255. |
| 260. | 0.63 | 0.53 | 0.36 | 0.27 | 0.00 | 0.14 | 0.06 | 260. |
| 265. | 0.64 | 0.53 | 0.36 | 0.27 | 0.02 | 0.14 | 0.06 | 265. |
| 270. | 0.64 | 0.53 | 0.35 | 0.27 | 0.04 | 0.14 | 0.06 | 270. |
| 275. | 0.63 | 0.52 | 0.33 | 0.27 | 0.04 | 0.14 | 0.06 | 275. |
| 280. | 0.61 | 0.50 | 0.32 | 0.27 | 0.00 | 0.14 | 0.06 | 280. |
| 285. | 0.59 | 0.48 | 0.30 | 0.26 | -0.05 | 0.14 | 0.06 | 285. |
| 290. | 0.56 | 0.46 | 0.27 | 0.25 | -0.07 | 0.13 | 0.06 | 290. |
| 295. | 0.54 | 0.43 | 0.25 | 0.24 | -0.07 | 0.12 | 0.06 | 295. |
| 300. | 0.54 | 0.40 | 0.23 | 0.22 | -0.06 | 0.12 | 0.05 | 300. |
| 305. | 0.53 | 0.37 | 0.21 | 0.20 | -0.05 | 0.11 | 0.04 | 305. |
| 310. | 0.49 | 0.33 | 0.18 | 0.18 | -0.07 | 0.10 | 0.03 | 310. |
| 315. | 0.41 | 0.28 | 0.15 | 0.16 | -0.09 | 0.09 | 0.03 | 315. |
| 320. | 0.29 | 0.23 | 0.12 | 0.13 | -0.11 | 0.08 | 0.03 | 320. |
| 325. | 0.21 | 0.18 | 0.08 | 0.10 | -0.14 | 0.08 | 0.03 | 325. |
| 330. | 0.19 | 0.11 | 0.04 | 0.06 | -0.16 | 0.07 | 0.03 | 330. |
| 335. | 0.13 | 0.04 | -0.01 | 0.03 | -0.19 | 0.06 | 0.02 | 335. |
| 340. | 0.01 | -0.02 | -0.06 | -0.01 | -0.21 | 0.03 | 0.02 | 340. |
| 345. | -0.12 | -0.05 | -0.13 | -0.04 | -0.23 | 0.02 | 0.02 | 345. |
| 350. | -0.16 | -0.03 | -0.14 | -0.07 | -0.25 | 0.0 | -.02 | 350. |
| 355. | -0.17 | -0.10 | -0.11 | -0.09 | -0.2. | 0.00 | 1 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=505 CNTR NO. 354 TCN= 16. C R.= 66.9

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.40 | -0.33 | -0.23 | -0.18 | -0.10 | -0.02 | 0.01 | 0. |
| 5. | -0.50 | -0.26 | -0.14 | -0.15 | -0.07 | -0.03 | -0.00 | 5. |
| 10. | -0.36 | -0.20 | -0.10 | -0.12 | -0.05 | -0.04 | -0.02 | 10. |
| 15. | -0.31 | -0.18 | -0.11 | -0.13 | -0.05 | -0.06 | -0.02 | 15. |
| 20. | -0.45 | -0.29 | -0.20 | -0.17 | -0.11 | -0.08 | -0.03 | 20. |
| 25. | -0.65 | -0.41 | -0.32 | -0.26 | -0.16 | -0.10 | -0.04 | 25. |
| 30. | -0.67 | -0.38 | -0.32 | -0.17 | -0.15 | -0.10 | -0.05 | 30. |
| 35. | -0.57 | -0.29 | -0.24 | -0.13 | -0.11 | -0.09 | -0.05 | 35. |
| 40. | -0.37 | -0.18 | -0.15 | -0.10 | -0.08 | -0.07 | -0.04 | 40. |
| 45. | -0.21 | -0.15 | -0.14 | -0.12 | -0.09 | -0.08 | -0.05 | 45. |
| 50. | -0.19 | -0.19 | -0.18 | -0.15 | -0.10 | -0.10 | -0.05 | 50. |
| 55. | -0.23 | -0.23 | -0.21 | -0.18 | -0.11 | -0.12 | -0.06 | 55. |
| 60. | -0.28 | -0.28 | -0.28 | -0.17 | -0.10 | -0.12 | -0.06 | 60. |
| 65. | -0.20 | -0.11 | -0.15 | -0.13 | -0.08 | -0.11 | -0.05 | 65. |
| 70. | -0.10 | -0.02 | -0.09 | -0.07 | -0.06 | -0.11 | -0.05 | 70. |
| 75. | 0.02 | 0.06 | -0.01 | -0.01 | -0.03 | -0.10 | -0.05 | 75. |
| 80. | 0.13 | 0.13 | 0.06 | 0.05 | 0.01 | -0.10 | -0.05 | 80. |
| 85. | 0.24 | 0.20 | 0.13 | 0.09 | 0.05 | -0.09 | -0.05 | 85. |
| 90. | 0.33 | 0.27 | 0.19 | 0.13 | 0.08 | -0.09 | -0.05 | 90. |
| 95. | 0.41 | 0.33 | 0.22 | 0.15 | 0.11 | -0.09 | -0.05 | 95. |
| 100. | 0.46 | 0.36 | 0.24 | 0.16 | 0.12 | -0.11 | -0.06 | 100. |
| 105. | 0.46 | 0.36 | 0.24 | 0.16 | 0.12 | -0.12 | -0.06 | 105. |
| 110. | 0.40 | 0.33 | 0.21 | 0.10 | 0.12 | -0.11 | -0.01 | 110. |
| 115. | 0.30 | 0.27 | 0.16 | 0.06 | 0.10 | -0.09 | -0.01 | 115. |
| 120. | 0.16 | 0.19 | 0.09 | 0.01 | 0.08 | -0.06 | -0.03 | 120. |
| 125. | 0.02 | 0.08 | 0.02 | -0.03 | 0.04 | -0.04 | -0.02 | 125. |
| 130. | -0.12 | -0.04 | -0.06 | -0.08 | 0.01 | -0.05 | -0.02 | 130. |
| 135. | -0.28 | -0.16 | -0.12 | -0.12 | -0.03 | -0.06 | -0.03 | 135. |
| 140. | -0.42 | -0.28 | -0.18 | -0.16 | -0.06 | -0.07 | -0.04 | 140. |
| 145. | -0.56 | -0.36 | -0.24 | -0.19 | -0.09 | -0.09 | -0.04 | 145. |
| 150. | -0.69 | -0.43 | -0.30 | -0.23 | -0.11 | -0.10 | -0.04 | 150. |
| 155. | -0.79 | -0.48 | -0.35 | -0.26 | -0.12 | -0.11 | -0.04 | 155. |
| 160. | -0.87 | -0.53 | -0.39 | -0.29 | -0.13 | -0.11 | -0.03 | 160. |
| 165. | -0.92 | -0.56 | -0.43 | 0.31 | -0.14 | -0.11 | -0.04 | 165. |
| 170. | -0.94 | -0.60 | -0.45 | -0.32 | -0.14 | -0.11 | -0.03 | 170. |
| 175. | -0.92 | -0.62 | -0.44 | -0.30 | -0.14 | -0.10 | -0.01 | 175. |
| 180. | -0.87 | -0.61 | -0.42 | -0.27 | -0.13 | -0.08 | -0.01 | 180. |
| 185. | -0.80 | -0.57 | -0.38 | -0.24 | -0.11 | -0.06 | -0.01 | 185. |
| 190. | -0.70 | -0.47 | -0.33 | -0.20 | -0.09 | -0.04 | -0.00 | 190. |
| 195. | -0.59 | -0.36 | -0.27 | -0.15 | -0.07 | -0.02 | 0.01 | 195. |
| 200. | -0.46 | -0.24 | -0.21 | -0.11 | -0.05 | -0.00 | 0.02 | 200. |
| 205. | -0.33 | -0.15 | -0.14 | -0.06 | -0.03 | 0.02 | 0.03 | 205. |
| 210. | -0.18 | -0.06 | -0.06 | -0.02 | -0.01 | 0.04 | 0.03 | 210. |
| 215. | -0.04 | 0.03 | 0.01 | 0.03 | 0.01 | 0.06 | 0.03 | 215. |
| 220. | 0.09 | 0.10 | 0.08 | 0.08 | 0.03 | 0.08 | 0.04 | 220. |
| 225. | 0.21 | 0.17 | 0.15 | 0.12 | 0.05 | 0.10 | 0.04 | 225. |
| 230. | 0.33 | 0.23 | 0.19 | 0.16 | 0.06 | 0.12 | 0.05 | 230. |
| 235. | 0.44 | 0.29 | 0.24 | 0.20 | 0.08 | 0.14 | 0.05 | 235. |
| 240. | 0.54 | 0.33 | 0.27 | 0.23 | 0.09 | 0.16 | 0.06 | 240. |
| 245. | 0.64 | 0.38 | 0.31 | 0.26 | 0.11 | 0.17 | 0.05 | 245. |
| 250. | 0.77 | 0.43 | 0.34 | 0.28 | 0.12 | 0.18 | 0.06 | 250. |
| 255. | 0.86 | 0.48 | 0.37 | 0.30 | 0.13 | 0.19 | 0.07 | 255. |
| 260. | 0.93 | 0.54 | 0.40 | 0.31 | 0.14 | 0.19 | 0.08 | 260. |
| 265. | 0.95 | 0.59 | 0.43 | 0.32 | 0.15 | 0.19 | 0.09 | 265. |
| 270. | 0.95 | 0.62 | 0.44 | 0.32 | 0.16 | 0.18 | 0.09 | 270. |
| 275. | 0.93 | 0.62 | 0.44 | 0.31 | 0.16 | 0.17 | 0.0? | 275. |
| 280. | 0.90 | 0.59 | 0.43 | 0.30 | 0.16 | 0.16 | 0.05 | 280. |
| 285. | 0.87 | 0.55 | 0.41 | 0.28 | 0.14 | 0.16 | 0.05 | 285. |
| 290. | 0.83 | 0.50 | 0.38 | 0.26 | 0.13 | 0.15 | 0.06 | 290. |
| 295. | 0.78 | 0.44 | 0.33 | 0.24 | 0.14 | 0.14 | 0.05 | 295. |
| 300. | 0.71 | 0.38 | 0.31 | 0.22 | 0.13 | 0.14 | 0.04 | 300. |
| 305. | 0.63 | 0.32 | 0.27 | 0.19 | 0.11 | 0.13 | 0.04 | 305. |
| 310. | 0.55 | 0.26 | 0.23 | 0.16 | 0.09 | 0.12 | 0.03 | 310. |
| 315. | 0.45 | 0.20 | 0.18 | 0.14 | 0.07 | 0.10 | 0.03 | 315. |
| 320. | 0.35 | 0.13 | 0.14 | 0.11 | 0.05 | 0.08 | 0.02 | 320. |
| 325. | 0.24 | 0.07 | 0.09 | 0.08 | 0.02 | 0.05 | 0.02 | 325. |
| 330. | 0.14 | 0.01 | 0.05 | 0.05 | -0.00 | 0.03 | 0.02 | 330. |
| 335. | 0.03 | -0.05 | 0.00 | 0.01 | -0.03 | 0.03 | 0.01 | 335. |
| 340. | -0.08 | -0.11 | -0.05 | -0.03 | -0.05 | 0.02 | 0.01 | 340. |
| 345. | -0.16 | -0.16 | -0.09 | -0.06 | -0.07 | 0.02 | 0.01 | 345. |
| 350. | -0.24 | -0.25 | 0.15 | -0.10 | -0.08 | 0.01 | 0.02 | 350. |
| 355. | -0.42 | -0.30 | -0.23 | -0.15 | -0.10 | 0.00 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 351 TCN= 19. C.R.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.550 | 13.400 | DEG. |
| 0. | 0.11 | 0.07 | 0.05 | -0.00 | 0. |
| 5. | 0.10 | 0.07 | 0.04 | -0.00 | 5. |
| 10. | 0.11 | 0.05 | 0.04 | -0.00 | 10. |
| 15. | 0.15 | 0.08 | 0.04 | -0.00 | 15. |
| 20. | 0.19 | 0.12 | 0.07 | -0.01 | 20. |
| 25. | 0.23 | 0.13 | 0.08 | -0.01 | 25. |
| 30. | 0.27 | 0.11 | 0.06 | -0.01 | 30. |
| 35. | 0.21 | 0.08 | 0.04 | -0.01 | 35. |
| 40. | 0.12 | 0.06 | 0.02 | -0.01 | 40. |
| 45. | 0.13 | 0.07 | 0.03 | -0.01 | 45. |
| 50. | 0.14 | 0.06 | 0.04 | -0.01 | 50. |
| 55. | 0.09 | 0.03 | 0.03 | -0.01 | 55. |
| 60. | 0.01 | 0.02 | 0.02 | -0.01 | 60. |
| 65. | 0.02 | 0.03 | 0.02 | -0.01 | 65. |
| 70. | 0.07 | 0.03 | 0.02 | -0.01 | 70. |
| 75. | 0.03 | 0.02 | 0.01 | -0.01 | 75. |
| 80. | 0.02 | 0.00 | 0.00 | -0.01 | 80. |
| 85. | 0.02 | -0.02 | -0.01 | -0.00 | 85. |
| 90. | -0.03 | -0.03 | -0.02 | -0.01 | 90. |
| 95. | -0.04 | -0.02 | -0.02 | -0.01 | 95. |
| 100. | 0.02 | -0.01 | -0.02 | -0.01 | 100. |
| 105. | 0.04 | -0.04 | -0.02 | -0.00 | 105. |
| 110. | 0.01 | -0.04 | -0.03 | 0.00 | 110. |
| 115. | -0.03 | -0.07 | -0.03 | 0.01 | 115. |
| 120. | -0.07 | -0.07 | -0.04 | 0.00 | 120. |
| 125. | -0.09 | -0.07 | -0.04 | -0.01 | 125. |
| 130. | -0.11 | -0.06 | -0.04 | -0.01 | 130. |
| 135. | -0.11 | -0.09 | -0.04 | -0.01 | 135. |
| 140. | -0.10 | -0.06 | -0.04 | 0.00 | 140. |
| 145. | -0.08 | -0.05 | -0.03 | 0.01 | 145. |
| 150. | -0.06 | -0.04 | -0.03 | 0.00 | 150. |
| 155. | -0.02 | -0.03 | -0.02 | 0.00 | 155. |
| 160. | 0.01 | -0.01 | -0.01 | 0.01 | 160. |
| 165. | 0.04 | 0.00 | 0.01 | 0.01 | 165. |
| 170. | 0.06 | 0.02 | 0.02 | 0.02 | 170. |
| 175. | 0.08 | 0.03 | 0.02 | 0.02 | 175. |
| 180. | 0.08 | 0.03 | 0.01 | 0.01 | 180. |
| 185. | 0.07 | 0.05 | 0.01 | 0.01 | 185. |
| 190. | 0.05 | 0.02 | 0.01 | 0.02 | 190. |
| 195. | 0.02 | 0.01 | 0.00 | 0.01 | 195. |
| 200. | -0.01 | -0.00 | -0.01 | 0.00 | 200. |
| 205. | -0.05 | -0.01 | -0.02 | 0.03 | 205. |
| 210. | -0.08 | -0.02 | -0.03 | 0.02 | 210. |
| 215. | -0.11 | -0.03 | -0.04 | 0.01 | 215. |
| 220. | -0.14 | -0.04 | -0.04 | 0.01 | 220. |
| 225. | -0.16 | -0.05 | -0.04 | 0.01 | 225. |
| 230. | -0.18 | -0.06 | -0.04 | 0.01 | 230. |
| 235. | -0.19 | -0.06 | -0.04 | 0.00 | 235. |
| 240. | -0.20 | -0.07 | -0.04 | -0.00 | 240. |
| 245. | -0.19 | -0.07 | -0.04 | 0.00 | 245. |
| 250. | -0.19 | -0.07 | -0.04 | 0.01 | 250. |
| 255. | -0.17 | -0.07 | -0.03 | 0.01 | 255. |
| 260. | -0.16 | -0.07 | -0.0. | 0.01 | 260. |
| 265. | -0.14 | -0.06 | -0.02 | 0.01 | 265. |
| 270. | -0.12 | -0.05 | -0.02 | 0.01 | 270. |
| 275. | -0.11 | -0.05 | -0.02 | 0.01 | 275. |
| 280. | -0.09 | -0.04 | -0.02 | 0.01 | 280. |
| 285. | -0.08 | -0.03 | -0.02 | 0.00 | 285. |
| 290. | -0.06 | -0.02 | -0.02 | 0.00 | 290. |
| 295. | -0.05 | -0.02 | -0.02 | -0.00 | 295. |
| 300. | -0.04 | -0.01 | -0.02 | -0.01 | 300. |
| 305. | -0.02 | 0.00 | -0.02 | -0.01 | 305. |
| 310. | -0.01 | 0.01 | -0.01 | -0.01 | 310. |
| 315. | 0.01 | 0.02 | 0.00 | -0.01 | 315. |
| 320. | 0.02 | 0.03 | 0.02 | -0.01 | 320. |
| 325. | 0.04 | 0.03 | 0.03 | -0.01 | 325. |
| 330. | 0.07 | 0.04 | 0.04 | -0.01 | 330. |
| 335. | 0.09 | 0.06 | 0.05 | -0.01 | 335. |
| 340. | 0.12 | 0.07 | 0.05 | -0.01 | 340. |
| 345. | 0.14 | 0.07 | 0.05 | -0.01 | 345. |
| 350 | 0.14 | 0.07 | 0.05 | -0.01 | 350. |
| 355. | 0.13 | 0.07 | 0.05 | -0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNFR NO. 351 TCN= 19. C.P.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.350 | 7.150 | 10.400 | DEG. |
| 0. | 0.28 | 0.20 | 0.16 | 0.09 | 0.06 | 0.06 | 0.04 | 0. |
| 5. | 0.25 | 0.18 | 0.13 | 0.08 | 0.05 | 0.05 | 0.04 | 5. |
| 10. | 0.21 | 0.14 | 0.10 | 0.06 | 0.04 | 0.04 | 0.03 | 10. |
| 15. | 0.14 | 0.09 | 0.07 | 0.04 | 0.02 | 0.03 | 0.02 | 15. |
| 20. | 0.07 | 0.05 | 0.05 | 0.02 | 0.02 | 0.02 | 0.02 | 20. |
| 25. | 0.05 | 0.05 | 0.04 | 0.02 | 0.02 | 0.02 | 0.02 | 25. |
| 30. | 0.07 | 0.06 | 0.03 | 0.03 | 0.02 | 0.01 | 0.02 | 30. |
| 35. | 0.09 | 0.06 | 0.03 | 0.03 | 0.02 | 0.01 | 0.01 | 35. |
| 40. | 0.12 | 0.06 | 0.04 | 0.03 | 0.03 | 0.01 | 0.01 | 40. |
| 45. | 0.14 | 0.09 | 0.05 | 0.03 | 0.03 | 0.01 | 0.02 | 45. |
| 50. | 0.17 | 0.12 | 0.06 | 0.04 | 0.04 | 0.01 | 0.03 | 50. |
| 55. | 0.19 | 0.14 | 0.08 | 0.04 | 0.05 | 0.02 | 0.04 | 55. |
| 60. | 0.20 | 0.15 | 0.08 | 0.05 | 0.05 | 0.02 | 0.03 | 60. |
| 65. | 0.19 | 0.15 | 0.07 | 0.04 | 0.06 | 0.01 | 0.03 | 65. |
| 70. | 0.16 | 0.14 | 0.08 | 0.04 | 0.06 | 0.01 | 0.02 | 70. |
| 75. | 0.13 | 0.11 | 0.06 | 0.03 | 0.06 | 0.01 | 0.01 | 75. |
| 80. | 0.09 | 0.07 | 0.03 | 0.02 | 0.05 | 0.00 | 0.01 | 80. |
| 85. | 0.05 | 0.04 | 0.01 | 0.02 | 0.04 | -0.00 | 0.01 | 85. |
| 90. | 0.02 | 0.01 | -0.01 | 0.02 | 0.03 | -0.01 | 0.02 | 90. |
| 95. | -0.01 | -0.02 | -0.02 | 0.01 | 0.02 | -0.01 | 0.02 | 95. |
| 100. | -0.04 | -0.04 | -0.04 | -0.01 | 0.01 | -0.01 | 0.01 | 100. |
| 105. | -0.07 | -0.07 | -0.05 | -0.03 | 0.00 | -0.02 | 0.01 | 105. |
| 110. | -0.10 | -0.09 | -0.06 | -0.03 | -0.01 | -0.02 | -0.00 | 110. |
| 115. | -0.13 | -0.11 | -0.07 | -0.04 | -0.01 | -0.02 | -0.01 | 115. |
| 120. | -0.15 | -0.12 | -0.09 | -0.04 | -0.02 | -0.03 | -0.02 | 120. |
| 125. | -0.17 | -0.13 | -0.10 | -0.05 | -0.03 | -0.03 | -0.02 | 125. |
| 130. | -0.18 | -0.13 | -0.10 | -0.06 | -0.05 | -0.03 | -0.02 | 130. |
| 135. | -0.19 | -0.13 | -0.11 | -0.07 | -0.06 | -0.03 | -0.02 | 135. |
| 140. | -0.19 | -0.14 | -0.12 | -0.07 | -0.06 | -0.04 | -0.03 | 140. |
| 145. | -0.18 | -0.13 | -0.09 | -0.08 | -0.05 | -0.04 | -0.03 | 145. |
| 150. | -0.15 | -0.11 | -0.08 | -0.07 | -0.04 | -0.04 | -0.02 | 150. |
| 155. | -0.11 | -0.07 | -0.06 | -0.06 | -0.03 | -0.03 | -0.02 | 155. |
| 160. | -0.05 | -0.02 | -0.04 | -0.04 | -0.02 | -0.02 | -0.01 | 160. |
| 165. | 0.01 | 0.02 | -0.02 | -0.01 | -0.01 | -0.02 | -0.01 | 165. |
| 170. | 0.06 | 0.04 | 0.01 | 0.01 | -0.00 | -0.01 | -0.01 | 170. |
| 175. | 0.09 | 0.06 | 0.03 | 0.02 | 0.01 | -0.00 | -0.01 | 175. |
| 180. | 0.09 | 0.06 | 0.05 | 0.03 | 0.02 | 0.01 | -0.01 | 180. |
| 185. | 0.07 | 0.04 | 0.04 | 0.04 | 0.02 | 0.01 | -0.01 | 185. |
| 190. | 0.03 | 0.01 | 0.02 | 0.04 | 0.00 | 0.01 | -0.02 | 190. |
| 195. | -0.03 | -0.03 | -0.01 | 0.02 | -0.02 | 0.00 | -0.02 | 195. |
| 200. | -0.08 | -0.06 | -0.04 | -0.00 | -0.04 | -0.01 | -0.03 | 200. |
| 205. | -0.12 | -0.09 | -0.06 | -0.03 | -0.04 | -0.01 | -0.03 | 205. |
| 210. | -0.16 | -0.12 | -0.09 | -0.04 | -0.05 | -0.02 | -0.03 | 210. |
| 215. | -0.20 | -0.15 | -0.11 | -0.06 | -0.06 | -0.02 | -0.03 | 215. |
| 220. | -0.24 | -0.18 | -0.13 | -0.08 | -0.06 | -0.03 | -0.03 | 220. |
| 225. | -0.28 | -0.21 | -0.15 | -0.09 | -0.07 | -0.03 | -0.03 | 225. |
| 230. | -0.31 | -0.22 | -0.15 | -0.10 | -0.08 | -0.04 | -0.03 | 230. |
| 235. | -0.33 | -0.23 | -0.16 | -0.11 | -0.08 | -0.03 | -0.03 | 235. |
| 240. | -0.34 | -0.22 | -0.15 | -0.11 | -0.08 | -0.03 | -0.03 | 240. |
| 245. | -0.33 | -0.22 | -0.14 | -0.10 | -0.09 | -0.03 | -0.02 | 245. |
| 250. | -0.29 | -0.21 | -0.12 | -0.08 | -0.09 | -0.03 | -0.02 | 250. |
| 255. | -0.24 | -0.17 | -0.09 | -0.07 | -0.06 | -0.02 | -0.02 | 255. |
| 260. | -0.20 | -0.14 | -0.08 | -0.07 | -0.05 | -0.02 | -0.01 | 260. |
| 265. | -0.25 | -0.16 | -0.10 | -0.07 | -0.04 | -0.01 | -0.01 | 265. |
| 270. | -0.25 | -0.16 | -0.10 | -0.07 | -0.04 | -0.01 | -0.01 | 270. |
| 275. | -0.15 | -0.08 | -0.07 | -0.04 | -0.04 | -0.01 | -0.01 | 275. |
| 280. | -0.02 | -0.02 | -0.03 | -0.01 | -0.03 | -0.01 | -0.01 | 280. |
| 285. | 0.04 | 0.03 | -0.00 | 0.00 | -0.01 | -0.00 | -0.01 | 285. |
| 290. | 0.06 | 0.05 | 0.02 | 0.02 | -0.00 | 0.00 | -0.01 | 290. |
| 295. | 0.06 | 0.06 | 0.04 | 0.02 | 0.01 | 0.01 | -0.00 | 295. |
| 300. | 0.08 | 0.06 | 0.05 | 0.02 | 0.01 | 0.01 | 0.00 | 300. |
| 305. | 0.10 | 0.06 | 0.06 | 0.02 | 0.02 | 0.01 | -0.00 | 305. |
| 310. | 0.11 | 0.06 | 0.06 | 0.02 | 0.02 | 0.00 | -0.00 | 310. |
| 315. | 0.13 | 0.09 | 0.07 | 0.02 | 0.02 | 0.01 | 0.01 | 315. |
| 320. | 0.15 | 0.11 | 0.09 | 0.04 | 0.03 | 0.03 | 0.01 | 320. |
| 325. | 0.17 | 0.14 | 0.12 | 0.08 | 0.04 | 0.04 | 0.02 | 325. |
| 330. | 0.21 | 0.16 | 0.14 | 0.11 | 0.05 | 0.04 | 0.03 | 330. |
| 335. | 0.26 | 0.18 | 0.16 | 0.11 | 0.07 | 0.04 | 0.02 | 335. |
| 340. | 0.29 | 0.19 | 0.17 | 0.11 | 0.08 | 0.04 | 0.03 | 340. |
| 345. | 0.31 | 0.22 | 0.18 | 0.11 | 0.09 | 0.04 | 0.04 | 345. |
| 350. | 0.31 | 0.23 | 0.18 | 0.11 | 0.08 | 0.05 | 0.04 | 350. |
| 355. | 0.30 | 0.22 | 0.18 | 0.10 | 0.07 | 0.06 | 0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST•503 CNTR NO. 351 TCN• 19. C.J.• 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.953 | 2.990 | 4.559 | 7.150 | 10.400 | DEG. |
| 0. | 0.61 | 0.43 | 0.32 | 0.27 | 0.19 | 0.10 | 0.04 | 0. |
| 5. | 0.57 | 0.40 | 0.29 | 0.24 | 0.17 | 0.09 | 0.03 | 5. |
| 10. | 0.53 | 0.37 | 0.27 | 0.22 | 0.15 | 0.08 | 0.03 | 10. |
| 15. | 0.50 | 0.36 | 0.26 | 0.21 | 0.14 | 0.07 | 0.03 | 15. |
| 20. | 0.49 | 0.36 | 0.24 | 0.20 | 0.13 | 0.06 | 0.02 | 20. |
| 25. | 0.51 | 0.37 | 0.24 | 0.19 | 0.13 | 0.06 | 0.02 | 25. |
| 30. | 0.54 | 0.37 | 0.24 | 0.18 | 0.13 | 0.05 | 0.02 | 30. |
| 35. | 0.55 | 0.37 | 0.25 | 0.18 | 0.13 | 0.06 | 0.02 | 35. |
| 40. | 0.55 | 0.36 | 0.26 | 0.18 | 0.13 | 0.06 | 0.02 | 40. |
| 45. | 0.53 | 0.36 | 0.25 | 0.18 | 0.13 | 0.06 | 0.01 | 45. |
| 50. | 0.51 | 0.36 | 0.24 | 0.16 | 0.13 | 0.05 | 0.01 | 50. |
| 55. | 0.48 | 0.34 | 0.21 | 0.14 | 0.12 | 0.03 | 0.01 | 55. |
| 60. | 0.43 | 0.30 | 0.18 | 0.12 | 0.11 | 0.02 | 0.00 | 60. |
| 65. | 0.38 | 0.25 | 0.15 | 0.11 | 0.10 | 0.01 | -0.01 | 65. |
| 70. | 0.32 | 0.19 | 0.11 | 0.09 | 0.08 | 0.00 | -0.01 | 70. |
| 75. | 0.24 | 0.14 | 0.07 | 0.07 | 0.06 | -0.01 | -0.01 | 75. |
| 80. | 0.14 | 0.09 | 0.03 | 0.04 | 0.04 | -0.01 | -0.01 | 80. |
| 85. | 0.04 | -0.00 | -0.01 | 0.01 | 0.02 | -0.02 | -0.01 | 85. |
| 90. | -0.04 | -0.09 | -0.04 | -0.02 | -0.00 | -0.04 | -0.02 | 90. |
| 95. | -0.07 | -0.14 | -0.07 | -0.06 | -0.02 | -0.05 | -0.03 | 95. |
| 100. | -0.10 | -0.17 | -0.09 | -0.06 | -0.04 | -0.05 | -0.03 | 100. |
| 105. | -0.12 | -0.18 | -0.12 | -0.11 | -0.06 | -0.06 | -0.03 | 105. |
| 110. | -0.16 | -0.21 | -0.15 | -0.13 | -0.07 | -0.06 | -0.03 | 110. |
| 115. | -0.21 | -0.25 | -0.18 | -0.14 | -0.09 | -0.07 | -0.04 | 115. |
| 120. | -0.26 | -0.29 | -0.20 | -0.16 | -0.10 | -0.07 | -0.04 | 120. |
| 125. | -0.29 | -0.32 | -0.22 | -0.18 | -0.11 | -0.07 | -0.04 | 125. |
| 130. | -0.31 | -0.33 | -0.22 | -0.20 | -0.12 | -0.07 | -0.03 | 130. |
| 135. | -0.33 | -0.32 | -0.21 | -0.20 | -0.12 | -0.07 | -0.03 | 135. |
| 140. | -0.34 | -0.30 | -0.21 | -0.20 | -0.12 | -0.07 | -0.03 | 140. |
| 145. | -0.35 | -0.27 | -0.20 | -0.20 | -0.12 | -0.07 | -0.03 | 145. |
| 150. | -0.35 | -0.25 | -0.19 | -0.19 | -0.12 | -0.06 | -0.03 | 150. |
| 155 | -0.34 | -0.24 | -0.19 | -0.19 | -0.12 | -0.06 | -0.03 | 155. |
| 160. | -0.32 | -0.23 | -0.18 | -0.18 | -0.11 | -0.06 | -0.02 | 160. |
| 165. | -0.30 | -0.23 | -0.17 | -0.17 | -0.10 | -0.05 | -0.02 | 165. |
| 170. | -0.28 | -0.23 | -0.16 | -0.14 | -0.09 | -0.04 | -0.02 | 170. |
| 175. | -0.27 | -0.23 | -0.15 | -0.11 | -0.08 | -0.04 | -0.02 | 175. |
| 180. | -0.27 | -0.24 | -0.14 | -0.10 | -0.08 | -0.04 | -0.02 | 180. |
| 185. | -0.28 | -0.25 | -0.13 | -0.11 | -0.08 | -0.05 | -0.02 | 185. |
| 190. | -0.30 | -0.26 | -0.15 | -0.12 | -0.09 | -0.05 | -0.02 | 190. |
| 195. | -0.33 | -0.27 | -0.17 | -0.14 | -0.10 | -0.05 | -0.02 | 195. |
| 200. | -0.36 | -0.28 | -0.20 | -0.15 | -0.11 | -0.05 | -0.02 | 200. |
| 205. | -0.40 | -0.29 | -0.22 | -0.16 | -0.12 | -0.05 | -0.02 | 205. |
| 210. | -0.45 | -0.30 | -0.23 | -0.16 | -0.12 | -0.05 | -0.01 | 210. |
| 215. | -0.49 | -0.32 | -0.24 | -0.17 | -0.12 | -0.04 | -0.01 | 215. |
| 220. | -0.53 | -0.34 | -0.25 | -0.18 | -0.13 | -0.04 | -0.01 | 220. |
| 225. | -0.56 | -0.35 | -0.26 | -0.18 | -0.13 | -0.04 | -0.01 | 225. |
| 230. | -0.59 | -0.36 | -0.27 | -0.19 | -0.14 | -0.04 | -0.01 | 230. |
| 235. | -0.61 | -0.38 | -0.27 | -0.19 | -0.14 | -0.04 | -0.00 | 235. |
| 240. | -0.62 | -0.39 | -0.27 | -0.19 | -0.14 | -0.04 | -0.00 | 240. |
| 245. | -0.62 | -0.39 | -0.27 | -0.19 | -0.14 | -0.04 | -0.01 | 245. |
| 250. | -0.62 | -0.38 | -0.27 | -0.18 | -0.14 | -0.04 | -0.01 | 250. |
| 255. | -0.58 | -0.35 | -0.26 | -0.18 | -0.14 | -0.03 | -0.01 | 255. |
| 260. | -0.49 | -0.30 | -0.24 | -0.16 | -0.13 | -0.03 | -0.00 | 260. |
| 265. | -0.37 | -0.25 | -0.19 | -0.13 | -0.10 | -0.04 | 0.00 | 265. |
| 270. | -0.28 | -0.21 | -0.11 | -0.09 | -0.07 | -0.03 | -0.01 | 270. |
| 275. | -0.24 | -0.17 | -0.05 | -0.05 | -0.06 | -0.02 | -0.01 | 275. |
| 280. | -0.23 | -0.13 | -0.04 | -0.03 | -0.05 | -0.00 | -0.00 | 280. |
| 285. | -0.21 | -0.10 | -0.04 | -0.02 | -0.03 | 0.01 | 0.00 | 285. |
| 290. | -0.10 | -0.05 | -0.00 | 0.01 | -0.00 | 0.01 | 0.02 | 290. |
| 295. | 0.06 | 0.04 | 0.08 | 0.05 | 0.03 | 0.02 | 0.02 | 295. |
| 300. | 0.21 | 0.19 | 0.16 | 0.11 | 0.06 | 0.04 | 0.02 | 300. |
| 305. | 0.34 | 0.37 | 0.22 | 0.12 | 0.09 | 0.06 | 0.03 | 305. |
| 310. | 0.44 | 0.42 | 0.26 | 0.21 | 0.11 | 0.09 | 0.04 | 310. |
| 315. | 0.43 | 0.43 | 0.28 | 0.23 | 0.14 | .10 | 0.04 | 315. |
| 320. | 0.42 | 0.40 | 0.29 | 0.24 | 0.15 | 0.10 | 0.04 | 320. |
| 325. | 0.45 | 0.40 | 0.29 | 0.24 | 0.16 | 0.09 | 0.04 | 325. |
| 330. | 0.50 | 0.42 | 0.31 | 0.25 | 0.17 | 0.09 | 0.03 | 330. |
| 335. | 0.54 | 0.45 | 0.33 | 0.27 | 0.18 | 0.10 | 0.03 | 335. |
| 340. | 0.62 | 0.48 | 0.35 | 0.28 | 0.19 | 0.10 | 0.04 | 340. |
| 345. | 0.66 | 0.51 | 0.36 | 0.30 | 0.20 | 0.11 | 0.05 | 345. |
| 350. | 0.69 | 0.53 | 0.36 | 0.30 | 0.21 | 0.12 | 0.05 | 350. |
| 355. | 0.67 | 0.56 | 0.34 | 0.29 | 0.21 | 0.11 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 351 TLN= 19. C.R.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 1.07 | 0.54 | 0.48 | 0.32 | 0.25 | 0.16 | 0.07 | 0. |
| 5. | 0.99 | 0.48 | 0.45 | 0.29 | 0.25 | 0.16 | 0.07 | 5. |
| 10. | 0.91 | 0.43 | 0.41 | 0.27 | 0.24 | 0.15 | 0.06 | 10. |
| 15. | 0.87 | 0.43 | 0.37 | 0.26 | 0.23 | 0.13 | 0.06 | 15. |
| 20. | 0.84 | 0.45 | 0.34 | 0.26 | 0.22 | 0.13 | 0.06 | 20. |
| 25. | 0.83 | 0.48 | 0.31 | 0.26 | 0.22 | 0.12 | 0.05 | 25. |
| 30. | 0.83 | 0.48 | 0.30 | 0.26 | 0.21 | 0.11 | 0.05 | 30. |
| 35. | 0.80 | 0.48 | 0.29 | 0.25 | 0.20 | 0.10 | 0.04 | 35. |
| 40. | 0.73 | 0.48 | 0.29 | 0.24 | 0.20 | 0.09 | 0.04 | 40. |
| 45. | 0.67 | 0.48 | 0.28 | 0.23 | 0.19 | 0.08 | 0.03 | 45. |
| 50. | 0.63 | 0.51 | 0.27 | 0.22 | 0.18 | 0.06 | 0.03 | 50. |
| 55. | 0.58 | 0.53 | 0.24 | 0.21 | 0.16 | 0.05 | 0.01 | 55. |
| 60. | 0.50 | 0.50 | 0.19 | 0.19 | 0.15 | 0.03 | 0.00 | 60. |
| 65. | 0.37 | 0.42 | 0.11 | 0.16 | 0.13 | 0.00 | -0.01 | 65. |
| 70. | 0.21 | 0.3. | 0.02 | 0.10 | 0.10 | -0.02 | -0.01 | 70. |
| 75. | 0.02 | 0.20 | -0.06 | 0.04 | 0.07 | -0.05 | -0.02 | 75. |
| 80. | -0.14 | 0.08 | -0.11 | -0.02 | 0.04 | -0.08 | -0.03 | 80. |
| 85. | -0.27 | -.04 | -0.16 | -0.06 | -0.00 | -0.10 | -0.04 | 85. |
| 90. | -0.39 | -0.15 | -0.20 | -0.07 | -0.04 | -0.11 | -0.04 | 90. |
| 95. | -0.49 | -0.23 | -0.27 | -0.09 | -0.07 | -0.12 | -0.05 | 95. |
| 100. | -0.56 | -0.26 | -0.32 | -0.13 | -0.08 | -0.12 | -0.05 | 100. |
| 105. | -0.59 | -0.27 | -0.31 | -0.16 | -0.09 | -0.13 | -0.05 | 105. |
| 110. | -0.56 | -0.26 | -0.27 | -0.15 | -0.09 | -0.12 | -0.05 | 110. |
| 115. | -0.51 | -0.25 | -0.27 | -0.13 | -0.10 | -0.11 | -0.05 | 115. |
| 120. | -0.56 | -0.26 | -0.29 | -0.15 | -0.14 | -0.11 | -0.05 | 120. |
| 125. | -0.68 | -0.31 | -0.31 | -0.20 | -0.17 | -0.12 | -0.05 | 125. |
| 130. | -0.68 | -0.31 | -0.31 | -0.20 | -0.16 | -0.12 | -0.05 | 130. |
| 135. | -0.61 | -0.22 | -0.30 | -0.18 | -0.12 | -0.12 | -0.05 | 135. |
| 140. | -0.52 | -0.15 | -0.28 | -0.16 | -0.11 | -0.10 | -0.05 | 140. |
| 145. | -0.52 | -0.12 | -0.26 | -0.16 | -0.12 | -0.10 | -0.04 | 145. |
| 150. | -0.53 | -0.12 | -0.25 | -0.17 | -0.14 | -0.10 | -0.04 | 150. |
| 155. | -0.55 | -0.12 | -0.24 | -0.18 | -0.14 | -0.10 | -0.04 | 155. |
| 160. | -0.58 | -0.13 | -0.24 | -0.18 | -0.14 | -0.09 | -0.04 | 160. |
| 165. | -0.60 | -0.12 | -0.23 | -0.18 | -0.14 | -0.08 | -0.03 | 165. |
| 170. | -0.60 | -0.11 | -0.23 | -0.17 | -0.15 | -0.08 | -0.03 | 170. |
| 175. | -0.54 | -0.11 | -0.22 | -0.17 | -0.14 | -0.08 | -0.03 | 175. |
| 180. | -0.47 | -0.10 | -0.20 | -0.16 | -0.12 | -0.07 | -0.03 | 180. |
| 185. | -0.45 | -0.09 | -0.17 | -0.15 | -0.11 | -0.05 | -0.03 | 185. |
| 190. | -0.46 | -0.10 | -0.15 | -0.15 | -0.12 | -0.05 | -0.03 | 190. |
| 195. | -0.49 | -0.15 | -0.15 | -0.14 | -0.14 | -0.05 | -0.03 | 195. |
| 200. | -0.52 | -0.21 | -0.17 | -0.14 | -0.14 | -0.06 | -0.03 | 200. |
| 205. | -0.51 | -0.20 | -0.19 | -0.14 | -0.13 | -0.06 | -0.02 | 205. |
| 210. | -0.47 | -0.21 | -0.21 | -0.14 | -0.13 | -0.05 | -0.02 | 210. |
| 215. | -0.47 | -0.25 | -0.22 | -0.15 | -0.14 | -0.05 | -0.01 | 215. |
| 220. | -0.50 | -0.31 | -0.23 | -0.17 | -0.15 | -0.05 | -0.01 | 220. |
| 225. | -0.55 | -0.37 | -0.25 | -0.19 | -0.17 | -0.05 | -0.01 | 225. |
| 230. | -0.60 | -0.45 | -0.27 | -0.21 | -0.18 | -0.05 | -0.01 | 230. |
| 235. | -0.64 | -0.53 | -0.29 | -0.22 | -0.18 | -0.06 | -0.01 | 235. |
| 240. | -0.67 | -0.56 | -0.30 | -0.24 | -0.18 | -0.06 | -0.01 | 240. |
| 245. | -0.66 | -0.56 | -0.29 | -0.24 | -0.20 | -0.05 | -0.01 | 245. |
| 250. | -0.71 | -0.64 | -0.29 | -0.25 | -0.22 | -0.05 | -0.01 | 250. |
| 255. | -0.85 | -0.64 | -0.29 | -0.26 | -0.20 | -0.05 | -0.01 | 255. |
| 260. | -0.60 | -0.52 | -0.26 | -0.19 | -0.15 | -0.03 | -0.02 | 260. |
| 265. | -0.25 | -0.35 | -0.14 | -0.10 | -0.11 | -0.02 | -0.02 | 265. |
| 270. | -0.13 | -0.33 | 0.03 | -0.11 | -0.11 | -0.01 | -0.02 | 270. |
| 275. | -0.10 | -0.44 | -0.07 | -0.14 | -0.14 | -0.01 | -0.02 | 275. |
| 280. | -0.36 | -0.45 | -0.12 | -0.13 | -0.13 | -0.02 | -0.02 | 280. |
| 285. | -0.23 | -0.34 | -0.18 | -0.11 | -0.10 | -0.01 | -0.01 | 285. |
| 290. | -0.11 | -0.26 | -0.02 | -0.09 | -0.05 | 0.01 | -0.01 | 290. |
| 295. | 0.02 | -0.20 | 0.06 | -0.05 | 0.01 | 0.03 | 0.00 | 295. |
| 300. | 0.21 | -0.08 | 0.15 | 0.04 | 0.07 | 0.05 | 0.02 | 300. |
| 305. | 0.43 | 0.12 | 0.24 | 0.15 | 0.12 | 0.08 | 0.03 | 305. |
| 310. | 0.65 | 0.27 | 0.31 | 0.21 | 0.16 | 0.12 | 0.05 | 310. |
| 315. | 0.78 | 0.33 | 0.37 | 0.25 | 0.19 | 0.14 | 0.07 | 315. |
| 320. | 0.85 | 0.37 | 0.42 | 0.26 | 0.20 | 0.15 | 0.07 | 320. |
| 325. | 0.94 | 0.39 | 0.45 | 0.27 | 0.21 | 0.15 | 0.07 | 325. |
| 330. | 1.01 | 0.43 | 0.48 | 0.30 | 0.22 | 0.16 | 0.07 | 330. |
| 335. | 1.08 | 0.50 | 0.50 | 0.35 | 0.25 | 0.17 | 0.07 | 335. |
| 340. | 1.14 | 0.56 | 0.53 | 0.36 | 0.26 | 0.17 | 0.07 | 340. |
| 345. | 1.17 | 0.56 | 0.55 | 0.35 | 0.26 | 0.17 | 0.07 | 345. |
| 350. | 1.18 | 0.56 | 0.54 | 0.34 | 0.25 | 0.17 | 0.07 | 350. |
| 355. | 1.14 | 0.56 | 0.52 | 0.33 | 0.25 | 0.17 | 0.07 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=533 CNTR NO. 351 TCN= 19. C.R.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.89 | 0.69 | 0.46 | 0.25 | 0.16 | 0.09 | 0.02 | 0. |
| 5. | 0.81 | 0.63 | 0.43 | 0.22 | 0.13 | 0.08 | 0.02 | 5. |
| 10. | 0.75 | 0.58 | 0.38 | 0.19 | 0.11 | 0.07 | 0.01 | 10. |
| 15. | 0.66 | 0.52 | 0.31 | 0.15 | 0.10 | 0.06 | 0.00 | 15. |
| 20. | 0.56 | 0.44 | 0.22 | 0.11 | 0.08 | 0.04 | -0.00 | 20. |
| 25. | 0.49 | 0.37 | 0.18 | 0.09 | 0.07 | 0.03 | -0.00 | 25. |
| 30. | 0.43 | 0.33 | 0.17 | 0.08 | 0.05 | 0.02 | -0.00 | 30. |
| 35. | 0.40 | 0.29 | 0.16 | 0.08 | 0.04 | 0.02 | -0.00 | 35. |
| 40. | 0.38 | 0.26 | 0.15 | 0.07 | 0.02 | 0.01 | -0.01 | 40. |
| 45. | 0.36 | 0.23 | 0.13 | 0.05 | -0.00 | 0.00 | -0.01 | 45. |
| 50. | 0.34 | 0.18 | 0.10 | 0.04 | -0.02 | -0.01 | -0.02 | 50. |
| 55. | 0.28 | 0.13 | 0.04 | 0.02 | -0.04 | -0.02 | -0.01 | 55. |
| 60. | 0.12 | 0.05 | -0.02 | -0.02 | -0.05 | -0.04 | -0.01 | 60. |
| 65. | -0.06 | -0.09 | -0.09 | -0.06 | -0.07 | -0.07 | -0.02 | 65. |
| 70. | -0.14 | -0.16 | -0.15 | -0.10 | -0.09 | -0.06 | -0.03 | 70. |
| 75. | -0.28 | -0.25 | -0.23 | -0.15 | -0.12 | -0.09 | -0.04 | 75. |
| 80. | -0.46 | -0.36 | -0.36 | -0.20 | -0.19 | -0.14 | -0.04 | 80. |
| 85. | -0.64 | -0.49 | -0.46 | -0.26 | -0.26 | -0.17 | -0.05 | 85. |
| 90. | -0.85 | -0.63 | -0.57 | -0.31 | -0.32 | -0.19 | -0.05 | 90. |
| 95. | -1.02 | -0.76 | -0.64 | -0.35 | -0.36 | -0.20 | -0.06 | 95. |
| 100. | -1.14 | -0.86 | -0.71 | -0.38 | -0.39 | -0.21 | -0.06 | 100. |
| 105. | -1.19 | -0.92 | -0.73 | -0.38 | -0.38 | -0.20 | -0.05 | 105. |
| 110. | -1.16 | -0.98 | -0.72 | -0.36 | -0.35 | -0.17 | -0.05 | 110. |
| 115. | -1.07 | -0.98 | -0.83 | -0.32 | -0.29 | -0.12 | -0.03 | 115. |
| 120. | -0.78 | -0.84 | -0.66 | -0.25 | -0.18 | -0.07 | -0.01 | 120. |
| 125. | -0.32 | -0.45 | -0.19 | -0.16 | -0.10 | -0.04 | -0.01 | 125. |
| 130. | -0.03 | -0.24 | -0.15 | -0.11 | -0.06 | -0.04 | -0.03 | 130. |
| 135. | -0.06 | -0.19 | -0.13 | -0.10 | -0.05 | -0.04 | -0.03 | 135. |
| 140. | -0.16 | -0.19 | -0.14 | -0.12 | -0.05 | -0.05 | -0.03 | 140. |
| 145. | -0.16 | -0.18 | -0.14 | -0.12 | -0.04 | -0.03 | -0.02 | 145. |
| 150. | -0.12 | -0.12 | -0.10 | -0.10 | -0.02 | -0.01 | -0.01 | 150. |
| 155. | 0.02 | 0.01 | -0.00 | -0.04 | 0.06 | 0.02 | -0.00 | 155. |
| 160. | 0.37 | 0.22 | 0.22 | 0.09 | 0.16 | 0.07 | 0.01 | 160. |
| 165. | 0.83 | 0.62 | 0.54 | 0.20 | 0.25 | 0.13 | 0.03 | 165. |
| 170. | 1.33 | 0.83 | 0.71 | 0.26 | 0.32 | 0.16 | 0.04 | 170. |
| 175. | 1.18 | 0.83 | 0.69 | 0.30 | 0.36 | 0.16 | 0.04 | 175. |
| 180. | 1.39 | 0.99 | 0.76 | 0.34 | 0.38 | 0.18 | 0.04 | 180. |
| 185. | 1.60 | 1.10 | 0.81 | 0.37 | 0.37 | 0.18 | 0.05 | 185. |
| 190. | 1.32 | 0.83 | 0.59 | 0.27 | 0.32 | 0.20 | 0.04 | 190. |
| 195. | 0.21 | 0.32 | 0.18 | 0.13 | 0.20 | 0.15 | 0.04 | 195. |
| 200. | -0.69 | -0.12 | -0.17 | 0.00 | 0.06 | 0.06 | 0.03 | 200. |
| 205. | -0.90 | -0.35 | -0.32 | -0.09 | -0.07 | 0.03 | 0.02 | 205. |
| 210. | -0.90 | -0.50 | -0.37 | -0.15 | -0.11 | -0.00 | 0.01 | 210. |
| 215. | -1.00 | -0.61 | -0.42 | -0.18 | -0.13 | -0.01 | 0.00 | 215. |
| 220. | -1.06 | -0.66 | -0.44 | -0.19 | -0.12 | -0.00 | 0.01 | 220. |
| 225. | -1.04 | -0.65 | -0.41 | -0.17 | -0.11 | 0.01 | 0.02 | 225. |
| 230. | -0.95 | -0.63 | -0.38 | -0.15 | -0.12 | 0.01 | 0.03 | 230. |
| 235. | -0.89 | -0.60 | -0.36 | -0.17 | -0.16 | -0.02 | 0.02 | 235. |
| 240. | -0.89 | -0.60 | -0.36 | -0.19 | -0.19 | -0.05 | 0.01 | 240. |
| 245. | -0.97 | -0.61 | -0.38 | -0.20 | -0.19 | -0.08 | -0.01 | 245. |
| 250. | -1.02 | -0.55 | -0.35 | -0.16 | -0.16 | -0.09 | -0.01 | 250. |
| 255. | -0.52 | 0.37 | -0.23 | -0.12 | -0.14 | -0.07 | -0.01 | 255. |
| 260. | -0.39 | -0.34 | -0.18 | -0.11 | -0.12 | -0.04 | -0.01 | 260. |
| 265. | -0.38 | -0.34 | -0.19 | -0.10 | -0.11 | -0.04 | -0.01 | 265. |
| 270. | -0.42 | -0.33 | -0.20 | -0.09 | -0.09 | -0.05 | -0.01 | 270. |
| 275. | -0.43 | -0.32 | -0.21 | -0.08 | -0.07 | -0.06 | -0.01 | 275. |
| 280. | -0.39 | -0.29 | -0.18 | -0.06 | -0.06 | -0.06 | -0.00 | 280. |
| 285. | -0.29 | -0.19 | -0.11 | -0.02 | -0.03 | -0.04 | -0.00 | 285. |
| 290. | -0.15 | -0.06 | -0.01 | 0.02 | 0.01 | -0.03 | 0.00 | 290. |
| 295. | -0.03 | 0.04 | 0.09 | 0.06 | 0.06 | -0.01 | 0.01 | 295. |
| 300. | 0.06 | 0.10 | 0.14 | 0.09 | 0.10 | 0.00 | 0.01 | 300. |
| 305. | 0.15 | 0.15 | 0.19 | 0.12 | 0.13 | 0.02 | 0.01 | 305. |
| 310. | 0.30 | 0.25 | 0.26 | 0.16 | 0.15 | 0.04 | 0.02 | 310. |
| 315. | 0.44 | 0.38 | 0.35 | 0.20 | 0.16 | 0.06 | 0.02 | 315. |
| 320. | 0.65 | 0.50 | 0.45 | 0.23 | 0.18 | 0.08 | 0.02 | 320. |
| 325. | 0.74 | 0.59 | 0.50 | 0.25 | 0.19 | 0.09 | 0.02 | 325. |
| 330. | 0.81 | 0.66 | 0.51 | 0.27 | 0.19 | 0.10 | 0.02 | 330. |
| 335. | 0.87 | 0.70 | 0.52 | 0.28 | 0.20 | 0.10 | 0.02 | 335. |
| 340. | 0.93 | 0.72 | 0.52 | 0.29 | 0.20 | 0.10 | 0.02 | 340. |
| 345. | 0.96 | 0.74 | 0.52 | 0.29 | 0.20 | 0.10 | 0.03 | 345. |
| 350. | 1.50 | 0.76 | 0.52 | 0.29 | 0.21 | 0.10 | 0.03 | 350. |
| 355. | 0.98 | 0.74 | 0.50 | 0.28 | 0.20 | 0.10 | 0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-503 CNFR NO. 351 TCN= 19. C.R.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.170 | 10.490 | DEG. |
| 0. | 0.07 | 0.11 | 0.06 | 0.03 | -0.11 | -0.02 | -0.02 | 0. |
| 5. | -0.02 | 0.05 | 0.05 | 0.01 | -0.12 | -0.04 | -0.03 | 5. |
| 10. | -0.12 | 0.01 | 0.00 | -0.03 | -0.13 | -0.06 | -0.0 | 10. |
| 15. | -0.24 | -0.06 | -0.08 | -0.08 | -0.14 | -0.08 | -0.04 | 15. |
| 20. | -0.37 | -0.16 | -0.17 | -0.14 | -0.15 | -0.10 | -0.05 | 20. |
| 25. | -0.48 | -0.25 | -0.25 | -0.20 | -0.14 | -0.11 | -0.06 | 25. |
| 30. | -0.55 | -0.30 | -0.31 | -0.24 | -0.13 | -0.12 | -0.06 | 30. |
| 35. | -0.58 | -0.33 | -0.33 | -0.25 | -0.12 | -0.13 | -0.06 | 35. |
| 40. | -0.60 | -0.36 | -0.34 | -0.26 | -0.10 | -0.15 | -0.06 | 40. |
| 45. | -0.65 | -0.39 | -0.35 | -0.26 | -0.08 | -0.17 | -0.07 | 45. |
| 50. | -0.71 | -0.44 | -0.37 | -0.27 | -0.06 | -0.19 | -0.07 | 50. |
| 55. | -0.79 | -0.50 | -0.41 | -0.29 | -0.05 | -0.20 | -0.08 | 55. |
| 60. | -0.88 | -0.58 | -0.46 | -0.33 | -0.07 | -0.20 | -0.08 | 60. |
| 65. | -0.96 | -0.68 | -0.49 | -0.38 | -0.09 | -0.20 | -0.09 | 65. |
| 70. | -1.01 | -0.81 | -0.50 | -0.41 | -0.11 | -0.20 | -0.09 | 70. |
| 75. | -1.10 | -0.96 | -0.53 | -0.44 | -0.13 | -0.20 | -0.10 | 75. |
| 80. | -1.25 | -1.11 | -0.58 | -0.49 | -0.15 | -0.23 | -0.11 | 80. |
| 85. | -1.49 | -1.25 | -0.71 | -0.59 | -0.15 | -0.27 | -0.12 | 85. |
| 90. | -1.69 | -1.40 | -0.90 | -0.71 | -0.15 | -0.29 | -0.11 | 90. |
| 95. | -1.11 | -1.67 | -1.03 | -0.90 | -0.20 | -0.29 | -0.11 | 95. |
| 100. | -2.43 | -1.78 | -1.08 | -0.81 | -0.25 | -0.27 | -0.09 | 100. |
| 105. | -1.94 | -1.49 | -0.85 | -0.67 | -0.25 | -0.21 | -0.07 | 105. |
| 110. | -1.24 | -0.94 | -0.67 | -0.42 | -0.18 | -0.14 | -0.06 | 110. |
| 115. | -0.69 | -0.32 | -0.19 | -0.19 | -0.07 | -0.05 | -0.04 | 115. |
| 120. | -0.09 | 0.03 | 0.03 | -0.02 | 0.09 | 0.02 | -0.01 | 120. |
| 125. | 0.15 | 0.30 | 0.29 | 0.13 | 0.26 | 0.05 | 0.01 | 125. |
| 130. | 0.73 | -0.29 | 0.03 | 0.11 | 0.29 | 0.05 | 0.04 | 130. |
| 135. | -1.33 | -0.42 | -0.15 | -0.08 | 0.21 | 0.06 | 0.05 | 135. |
| 140. | -1.11 | -0.42 | -0.15 | -0.07 | 0.22 | 0.08 | 0.07 | 140. |
| 145. | -0.68 | 0.01 | -0.03 | 0.04 | 0.26 | 0.13 | 0.11 | 145. |
| 150. | -0.33 | 0.30 | 0.15 | 0.15 | 0.33 | 0.19 | 0.14 | 150. |
| 155. | 0.33 | 0.51 | 0.32 | 0.19 | 0.39 | 0.21 | 0.15 | 155. |
| 160. | 0.24 | 0.51 | 0.39 | 0.25 | 0.44 | 0.22 | 0.15 | 160. |
| 165. | 0.46 | 0.49 | 0.41 | 0.38 | 0.48 | 0.23 | 0.15 | 165. |
| 170. | 0.87 | 0.73 | 0.53 | 0.50 | 0.49 | 0.24 | 0.15 | 170. |
| 175. | 1.35 | 0.94 | 0.67 | 0.54 | 0.48 | 0.25 | 0.14 | 175. |
| 180. | 1.96 | 0.87 | 0.67 | 0.54 | 0.46 | 0.27 | 0.15 | 180. |
| 185. | 0.83 | 0.82 | 0.64 | 0.53 | 0.44 | 0.29 | 0.17 | 185. |
| 190. | 1.17 | 1.08 | 0.73 | 0.56 | 0.40 | 0.27 | 0.17 | 190. |
| 195. | 2.62 | 1.53 | 0.86 | 0.57 | 0.34 | 0.21 | 0.11 | 195. |
| 200. | 4.26 | 1.92 | 1.01 | 0.56 | 0.25 | 0.11 | -0.00 | 200. |
| 205. | 4.92 | 2.19 | 1.05 | 0.49 | 0.17 | 0.05 | -0.07 | 205. |
| 210. | 4.74 | 2.11 | 1.03 | 0.51 | 0.16 | 0.04 | -0.07 | 210. |
| 215. | 4.27 | 2.00 | 1.02 | 0.57 | 0.18 | 0.05 | -0.07 | 215. |
| 220. | 3.69 | 1.80 | 1.01 | 0.60 | 0.22 | 0.08 | -0.07 | 220. |
| 225. | 2.64 | 1.56 | 0.96 | 0.60 | 0.26 | 0.11 | -0.04 | 225. |
| 230. | 2.20 | 1.35 | 0.88 | 0.54 | 0.25 | 0.14 | 0.01 | 230. |
| 235. | 1.20 | 0.96 | 0.71 | 0.34 | 0.16 | 0.15 | 0.03 | 235. |
| 240. | -0.23 | -0.06 | 0.09 | 0.10 | -0.09 | 0.12 | 0.05 | 240. |
| 245. | -1.70 | -0.82 | -0.35 | -0.06 | -0.29 | 0.1 | 0.04 | 245. |
| 250. | -2.07 | -1.10 | -0.50 | -0.32 | -0.36 | 05 | 0.02 | 250. |
| 255. | -1.65 | -1.01 | -0.45 | -0.20 | -0.21 | 0.01 | 0.03 | 255. |
| 260. | -0.53 | -0.05 | -0.12 | 0.10 | -0.04 | 0.15 | 0.08 | 260. |
| 265. | -0.42 | 0.10 | -0.01 | 0.30 | 0.01 | 0.24 | 0.12 | 265. |
| 270. | -0.90 | -0.47 | -0.20 | 0.11 | -0.15 | 0.14 | 0.10 | 270. |
| 275. | -0.89 | -0.43 | -0.36 | -0.16 | -0.29 | 0.01 | 0.03 | 275. |
| 280. | -0.82 | -0.57 | -0.39 | -0.26 | -0.34 | -0.07 | -0.02 | 280. |
| 285. | -0.72 | -0.44 | -0.26 | -0.25 | -0.30 | -0.06 | -0.02 | 285. |
| 290. | -0.63 | -0.37 | -0.20 | -0.16 | -0.27 | -0.03 | -0.02 | 290. |
| 295. | -0.53 | -0.33 | -0.21 | -0.10 | -0.26 | -0.02 | -0.02 | 295. |
| 300. | -0.56 | -0.32 | -0.23 | -0.05 | -0.25 | -0.01 | -0.01 | 300. |
| 305. | -0.48 | -0.28 | -0.19 | -0.02 | -0.20 | -0.00 | -0.01 | 305. |
| 310. | -0.37 | -0.18 | -0.12 | 0.01 | -0.15 | 0.00 | -0.00 | 310. |
| 315. | 0.18 | -0.07 | -0.03 | 0.03 | -0.12 | 0.00 | -0.01 | 315. |
| 320. | 0.09 | 0.03 | 0.04 | 0.04 | -0.11 | 0.01 | -0.01 | 320. |
| 325. | 0.06 | 0.12 | 0.07 | 0.05 | -0.10 | 0.01 | -0.00 | 325. |
| 330. | 0.12 | 0.19 | 0.08 | 0.06 | -0.10 | 0.01 | -0.00 | 330. |
| 335. | 0.18 | 0.24 | 0.09 | 0.06 | -0.09 | 0.00 | -0.01 | 335. |
| 340. | 0.23 | 0.27 | 0.12 | 0.09 | -0.09 | -0.00 | -0.02 | 340. |
| 345. | 0.25 | 0.29 | 0.13 | 0.12 | -0.08 | -0.01 | -0.02 | 345. |
| 350. | 0.23 | 0.28 | 0.14 | 0.12 | -0.09 | -0.01 | -0.02 | 350. |
| 355. | 0.16 | 0.22 | 0.11 | 0.08 | -0.10 | -0.02 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 551 TCN= 19. C.R.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.048 | 1.958 | 2.998 | 4.598 | 7.196 | 10.480 | DEG. |
| 0. | -2.00 | -0.83 | -0.50 | -0.37 | -0.23 | -0.11 | -0.02 | 0. |
| 5. | -2.13 | -0.91 | -0.57 | -0.41 | -0.26 | -0.12 | -0.02 | 5. |
| 10. | -2.17 | -0.98 | -0.64 | -0.45 | -0.29 | -0.14 | -0.03 | 10. |
| 15. | -2.41 | -1.06 | -0.72 | -0.49 | -0.31 | -0.16 | -0.04 | 15. |
| 20. | -2.54 | -1.13 | -0.79 | -0.52 | -0.33 | -0.18 | -0.06 | 20. |
| 25. | -2.64 | -1.20 | -0.83 | -0.56 | -0.35 | -0.20 | -0.07 | 25. |
| 30. | -2.73 | -1.28 | -0.85 | -0.59 | -0.36 | -0.20 | -0.07 | 30. |
| 35. | -2.71 | -1.3C | -0.84 | -0.59 | -0.36 | -0.20 | -0.06 | 35. |
| 40. | -2.59 | -1.16 | -0.80 | -0.55 | -0.34 | -0.20 | -0.07 | 40. |
| 45. | -2.58 | -1.16 | -0.76 | -0.54 | -0.34 | -0.21 | -0.07 | 45. |
| 50. | -2.69 | -1.31 | -0.86 | -0.60 | -0.35 | -0.22 | -0.08 | 50. |
| 55. | -2.76 | -1.34 | -0.89 | -0.64 | -0.36 | -0.24 | -0.08 | 55. |
| 60. | -2.72 | -1.29 | -0.84 | -0.62 | -0.38 | -0.23 | -0.08 | 60. |
| 65. | -2.51 | -1.17 | -0.78 | -0.56 | -0.36 | -0.22 | -0.08 | 65. |
| 70. | -2.42 | -1.07 | -0.55 | -0.64 | -0.24 | -0.20 | -0.07 | 70. |
| 75. | -1.99 | -1.70 | -0.665 | -0.35 | -0.24 | -0.18 | -0.58 | 75. |
| 80. | -2.06 | -0.68 | -0.49 | -0.43 | -0.26 | -0.20 | -0.09 | 80. |
| 85. | -2.45 | -0.89 | -0.66 | -0.53 | -0.29 | -0.24 | -0.10 | 85. |
| 90. | -2.81 | -1.13 | -0.79 | -0.57 | -0.32 | -0.27 | -0.10 | 90. |
| 95. | -3.01 | -1.17 | -0.66 | -0.49 | -0.27 | -0.25 | -0.11 | 95. |
| 100. | -2.64 | -0.25 | -0.28 | -0.20 | -0.15 | -0.20 | -0.06 | 100. |
| 105. | 2.20 | 0.51 | 0.21 | -0.02 | -0.05 | -0.12 | -0.05 | 105. |
| 110. | 1.51 | 0.64 | 0.33 | 0.05 | 0.02 | -0.05 | -0.02 | 110. |
| 115. | 1.49 | 0.64 | 0.34 | 0.20 | 0.08 | -0.00 | -0.01 | 115. |
| 120. | 2.22 | 0.92 | 0.48 | 0.32 | 0.13 | 0.02 | -0.01 | 120. |
| 125. | 2.97 | 1.12 | 0.66 | 0.38 | 0.18 | 0.03 | -0.02 | 125. |
| 130. | 3.34 | 1.28 | 0.73 | 0.43 | 0.22 | 0.03 | -0.03 | 130. |
| 135. | 3.36 | 1.34 | 1.76 | 0.45 | 0.24 | 0.02 | -0.04 | 135. |
| 140. | 3.32 | 1.25 | 1.76 | 0.47 | 0.25 | 0.02 | -0.04 | 140. |
| 145. | 3.26 | 1.16 | 0.73 | 0.47 | 0.26 | 0.04 | -0.03 | 145. |
| 150. | 3.22 | 1.14 | 0.71 | 0.47 | 0.26 | 0.07 | -0.02 | 150. |
| 155. | 3.20 | 1.11 | 0.70 | 0.45 | 0.26 | 0.08 | -0.02 | 155. |
| 160. | 3.09 | 1.02 | 0.65 | 0.44 | 0.25 | 0.08 | -0.00 | 160. |
| 165. | 2.89 | 0.89 | 0.61 | 0.42 | 0.23 | 0.09 | 0.00 | 165. |
| 170. | 2.68 | 0.85 | 0.59 | 0.40 | 0.21 | 0.10 | 0.01 | 170. |
| 175. | 2.63 | 0.88 | 0.57 | 0.40 | 0.22 | 0.12 | 0.03 | 175. |
| 180. | 2.79 | 0.92 | 0.58 | 0.42 | 0.25 | 0.14 | 0.05 | 180. |
| 185. | 2.92 | 0.96 | 0.60 | 0.44 | 0.27 | 0.17 | 0.05 | 185. |
| 190. | 3.06 | 0.99 | 0.63 | 0.47 | 0.29 | 0.18 | 0.05 | 190. |
| 195. | 3.08 | 0.98 | 0.66 | 0.49 | 0.30 | 0.19 | 0.06 | 195. |
| 200. | 2.72 | 0.96 | 0.67 | 0.50 | 0.31 | 0.19 | 0.07 | 200. |
| 205. | 2.18 | 0.92 | 0.64 | 0.48 | 0.31 | 0.19 | 0.07 | 205. |
| 210. | 1.63 | 0.85 | 0.59 | 0.45 | 0.30 | 0.18 | 0.07 | 210. |
| 215. | 1.12 | 0.73 | 0.51 | 0.41 | 0.28 | 0.16 | 0.06 | 215. |
| 220. | 0.58 | 0.57 | 0.44 | 0.36 | 0.25 | 0.14 | 0.04 | 220. |
| 225. | 0.21 | 0.49 | 0.44 | 0.32 | 0.24 | 0.14 | 0.09 | 225. |
| 230. | 0.30 | 0.49 | 0.48 | 0.33 | 0.25 | 0.19 | 0.09 | 230. |
| 235. | 0.79 | 0.62 | 0.45 | 0.38 | 0.27 | 0.21 | 0.10 | 235. |
| 240. | 1.75 | 0.80 | 0.52 | 0.43 | 0.27 | 0.21 | 0.10 | 240. |
| 245. | 2.63 | 0.94 | 0.58 | 0.42 | 0.25 | 0.15 | 0.06 | 245. |
| 250. | 2.88 | 1.02 | 0.62 | 0.42 | 0.22 | 0.11 | 0.02 | 250. |
| 255. | 2.97 | 0.98 | 0.62 | 0.43 | 0.20 | 0.14 | 0.01 | 255. |
| 260. | 2.95 | 0.84 | 0.57 | 0.42 | 0.23 | 0.18 | 0.05 | 260. |
| 265. | 1.27 | 0.68 | 0.48 | 0.42 | 0.24 | 0.21 | 0.08 | 265. |
| 270. | 0.22 | 0.48 | 0.35 | 0.18 | 0.20 | 0.20 | 0.13 | 270. |
| 275. | -0.22 | 0.09 | 0.17 | 0.24 | 0.12 | 0.16 | 0.09 | 275. |
| 280. | -0.94 | -0.20 | -0.03 | 0.01 | 0.04 | 0.13 | 0.07 | 280. |
| 285. | -0.97 | -0.18 | -0.11 | -0.07 | -0.00 | 0.08 | 0.04 | 285. |
| 290. | -1.20 | -0.33 | -0.23 | -0.09 | -0.04 | 0.04 | 0.04 | 290. |
| 295. | -1.39 | -0.43 | -0.23 | -0.14 | -0.07 | 0.00 | 0.05 | 295. |
| 300. | -1.23 | -0.32 | -0.19 | -0.10 | -0.07 | 0.06 | 0.05 | 300. |
| 305. | -1.55 | -0.49 | -0.35 | -0.23 | -0.07 | -0.01 | 0.03 | 305. |
| 310. | -1.60 | -0.38 | -0.24 | -0.11 | -0.08 | 0.02 | 0.03 | 310. |
| 315. | -1.25 | -0.36 | -0.21 | -0.12 | -0.08 | 0.02 | 0.02 | 315. |
| 320. | -1.65 | -0.54 | -0.35 | -0.21 | -0.10 | 0.01 | 0.01 | 320. |
| 325. | -1.80 | -0.71 | -0.41 | -0.26 | -0.13 | 0.00 | 0.01 | 325. |
| 330. | -1.80 | -0.70 | -0.43 | -0.28 | -0.14 | -0.02 | 0.00 | 330. |
| 335. | -1.72 | -0.65 | -0.41 | -0.28 | -0.16 | -0.05 | -0.01 | 335. |
| 340. | -1.70 | -0.63 | -0.42 | -0.26 | -0.17 | -0.04 | -0.01 | 340. |
| 345. | -1.70 | -0.63 | -0.41 | -0.27 | -0.17 | -0.05 | -0.01 | 345. |
| 350. | -1.74 | -0.66 | -0.40 | -0.29 | -0.18 | -0.07 | 0.01 | 350. |
| 355. | -1.85 | -0.74 | -0.43 | -0.33 | -0.20 | -0.09 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 494 TCN= 21. C.R.= 36.3

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ DEG. | CHORD STATION 0.492 | 1.992 | 4.250 | 10.498 | AZ DEG. |
|---|---|---|---|---|---|
| 0. | -0.05 | -0.03 | -0.01 | 0.01 | 0. |
| 5. | -0.00 | 0.02 | 0.05 | 0.01 | 5. |
| 10. | 0.00 | 0.04 | 0.04 | 0.01 | 10. |
| 15. | 0.16 | 0.06 | 0.07 | 0.02 | 15. |
| 20. | 0.17 | 0.07 | 0.05 | 0.02 | 20. |
| 25. | 0.13 | 0.06 | 0.05 | 0.01 | 25. |
| 30. | 0.05 | 0.03 | 0.01 | -0.00 | 30. |
| 35. | -0.05 | 0.03 | 0.01 | 0.00 | 35. |
| 40. | -0.10 | 0.04 | 0.03 | 0.00 | 40. |
| 45. | -0.14 | 0.05 | 0.03 | 0.01 | 45. |
| 50. | -0.14 | -0.00 | -0.00 | 0.00 | 50. |
| 55. | -0.05 | -0.05 | -0.01 | 0.01 | 55. |
| 60. | 0.00 | -0.04 | 0.01 | 0.02 | 60. |
| 65. | 0.12 | -0.04 | 0.04 | 0.01 | 65. |
| 70. | 0.11 | -0.03 | 0.04 | -0.00 | 70. |
| 75. | 0.00 | -0.01 | 0.01 | -0.01 | 75. |
| 80. | 0.00 | 0.02 | 0.01 | -0.00 | 80. |
| 85. | 0.00 | 0.05 | 0.01 | 0.00 | 85. |
| 90. | 0.12 | 0.05 | 0.01 | -0.00 | 90. |
| 95. | 0.14 | 0.06 | 0.02 | -0.01 | 95. |
| 100. | 0.15 | 0.06 | 0.03 | -0.01 | 100. |
| 105. | 0.16 | 0.06 | 0.03 | -0.00 | 105. |
| 110. | 0.16 | 0.05 | 0.04 | 0.01 | 110. |
| 115. | 0.16 | 0.06 | 0.04 | 0.01 | 115. |
| 120. | 0.16 | 0.06 | 0.05 | 0.01 | 120. |
| 125. | 0.17 | 0.06 | 0.05 | 0.01 | 125. |
| 130. | 0.18 | 0.07 | 0.05 | 0.00 | 130. |
| 135. | 0.18 | 0.07 | 0.05 | 0.00 | 135. |
| 140. | 0.19 | 0.07 | 0.05 | -0.00 | 140. |
| 145. | 0.20 | 0.07 | 0.05 | -0.01 | 145. |
| 150. | 0.21 | 0.07 | 0.05 | -0.01 | 150. |
| 155. | 0.22 | 0.08 | 0.05 | -0.00 | 155. |
| 160. | 0.23 | 0.10 | 0.05 | 0.00 | 160. |
| 165. | 0.24 | 0.11 | 0.06 | 0.00 | 165. |
| 170. | 0.25 | 0.12 | 0.06 | 0.00 | 170. |
| 175. | 0.25 | 0.13 | 0.07 | 0.00 | 175. |
| 180. | 0.25 | 0.13 | 0.07 | 0.00 | 180. |
| 185. | 0.25 | 0.13 | 0.08 | 0.00 | 185. |
| 190. | 0.24 | 0.12 | 0.07 | 0.00 | 190. |
| 195. | 0.22 | 0.11 | 0.07 | 0.00 | 195. |
| 200. | 0.20 | 0.10 | 0.06 | -0.01 | 200. |
| 205. | 0.17 | 0.08 | 0.05 | 0.01 | 205. |
| 210. | 0.13 | 0.06 | 0.03 | 0.01 | 210. |
| 215. | 0.08 | 0.04 | 0.01 | 0.01 | 215. |
| 220. | 0.01 | 0.02 | -0.00 | 0.00 | 220. |
| 225. | -0.05 | -0.00 | -0.01 | -0.01 | 225. |
| 230. | -0.09 | -0.02 | -0.02 | -0.01 | 230. |
| 235. | -0.12 | -0.04 | -0.03 | -0.01 | 235. |
| 240. | -0.15 | -0.05 | -0.03 | -0.00 | 240. |
| 245. | -0.16 | -0.06 | -0.04 | -0.00 | 245. |
| 250. | -0.17 | -0.07 | -0.05 | -0.01 | 250. |
| 255. | -0.19 | -0.08 | -0.05 | -0.01 | 255. |
| 260. | -0.21 | -0.10 | -0.06 | -0.01 | 260. |
| 265. | -0.23 | -0.12 | -0.07 | 0.00 | 265. |
| 270. | -0.25 | -0.12 | -0.07 | 0.01 | 270. |
| 275. | -0.27 | -0.13 | -0.08 | 0.00 | 275. |
| 280. | -0.29 | -0.13 | -0.08 | -0.01 | 280. |
| 285. | -0.30 | -0.13 | -0.08 | -0.01 | 285. |
| 290. | -0.30 | -0.13 | -0.09 | -0.00 | 290. |
| 295. | -0.31 | -0.13 | -0.09 | -0.00 | 295. |
| 300. | -0.31 | -0.12 | -0.09 | -0.01 | 300. |
| 305. | -0.30 | -0.12 | -0.09 | -0.01 | 305. |
| 310. | -0.28 | -0.11 | -0.09 | -0.02 | 310. |
| 315. | -0.27 | -0.10 | -0.08 | -0.01 | 315. |
| 320. | -0.25 | -0.11 | -0.08 | -0.01 | 320. |
| 325. | -0.22 | -0.11 | -0.08 | -0.01 | 325. |
| 330. | -0.20 | -0.11 | -0.07 | -0.01 | 330. |
| 335. | -0.16 | -0.10 | -0.06 | -0.02 | 335. |
| 340. | -0.17 | -0.10 | -0.05 | -0.01 | 340. |
| 345. | -0.11 | -0.08 | -0.04 | 0.00 | 345. |
| 350. | -0.14 | -0.06 | -0.03 | 0.01 | 350. |
| 355. | -0.14 | -0.03 | -0.02 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-[illegible] CNTR NO. [illegible] TCM= 21. C.R.= 30.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.001 | 1.953 | 2.998 | 4.598 | 7.153 | 19.400 | DEG. |
| 0. | 0.10 | 0.06 | 0.04 | 0.04 | 0.03 | 0.03 | -0.01 | 0. |
| 5. | 0.09 | -0.01 | 0.02 | 0.03 | 0.02 | 0.02 | -0.02 | 5. |
| 10. | -0.11 | -0.02 | -0.04 | -0.00 | 0.01 | 0.01 | -0.03 | 10. |
| 15. | -0.01 | 0.03 | 0.01 | 0.01 | 0.02 | 0.02 | -0.02 | 15. |
| 20. | 0.11 | 0.15 | 0.07 | 0.04 | 0.04 | 0.02 | -0.00 | 20. |
| 25. | 0.12 | 0.17 | 0.09 | 0.06 | 0.06 | 0.02 | 0.00 | 25. |
| 30. | 0.10 | 0.15 | 0.08 | 0.07 | 0.06 | 0.01 | 0.00 | 30. |
| 35. | 0.07 | 0.04 | 0.01 | 0.04 | 0.05 | 0.03 | -0.01 | 35. |
| 40. | -0.07 | -0.08 | -0.06 | -0.01 | 0.04 | -0.00 | -0.02 | 40. |
| 45. | -0.20 | -0.07 | -0.04 | -0.01 | 0.03 | -0.03 | -0.02 | 45. |
| 50. | -0.00 | 0.00 | 0.00 | 0.01 | 0.03 | 0.00 | -0.02 | 50. |
| 55. | 0.01 | -0.01 | -0.03 | 0.02 | 0.03 | -0.00 | -0.03 | 55. |
| 60. | -0.04 | -0.05 | -0.05 | -0.00 | 0.03 | -0.01 | -0.03 | 60. |
| 65. | -0.08 | -0.06 | -0.04 | -0.02 | 0.03 | -0.02 | -0.01 | 65. |
| 70. | -0.09 | -0.05 | -0.03 | -0.02 | 0.03 | -0.02 | -0.03 | 70. |
| 75. | -0.08 | -0.04 | -0.02 | -0.02 | 0.03 | -0.02 | 0.04 | 75. |
| 80. | -0.07 | -0.01 | -0.01 | -0.02 | 0.03 | -0.02 | 0.04 | 80. |
| 85. | 0.00 | 0.01 | -0.00 | -0.01 | 0.03 | -0.02 | 0.04 | 85. |
| 90. | 0.05 | 0.04 | 0.00 | 0.00 | 0.04 | -0.02 | 0.04 | 90. |
| 95. | 0.07 | 0.07 | 0.02 | 0.02 | 0.04 | -0.02 | 0.04 | 95. |
| 100. | 0.07 | 0.10 | 0.03 | 0.03 | 0.04 | -0.02 | 0.04 | 100. |
| 105. | 0.12 | 0.13 | 0.04 | 0.04 | 0.04 | -0.02 | 0.07 | 105. |
| 110. | 0.18 | 0.15 | 0.05 | 0.05 | 0.04 | -0.02 | 0.06 | 110. |
| 115. | 0.21 | 0.17 | 0.07 | 0.06 | 0.05 | -0.01 | 0.06 | 115. |
| 120. | 0.24 | 0.18 | 0.08 | 0.07 | 0.07 | 0.01 | 0.07 | 120. |
| 125. | 0.25 | 0.19 | 0.09 | 0.07 | 0.08 | 0.01 | 0.08 | 125. |
| 130. | 0.24 | 0.19 | 0.10 | 0.07 | 0.09 | 0.02 | 0.08 | 130. |
| 135. | 0.24 | 0.19 | 0.10 | 0.08 | 0.10 | 0.02 | 0.08 | 135. |
| 140. | 0.24 | 0.19 | 0.11 | 0.08 | 0.10 | 0.02 | 0.07 | 140. |
| 145. | 0.27 | 0.20 | 0.11 | 0.09 | 0.10 | 0.02 | 0.06 | 145. |
| 150. | 0.30 | 0.21 | 0.11 | 0.09 | 0.10 | 0.02 | 0.07 | 150. |
| 155. | 0.32 | 0.22 | 0.13 | 0.09 | 0.10 | 0.02 | 0.08 | 155. |
| 160. | 0.35 | 0.24 | 0.15 | 0.10 | 0.11 | 0.02 | 0.08 | 160. |
| 165. | 0.36 | 0.26 | 0.17 | 0.11 | 0.12 | 0.03 | 0.07 | 165. |
| 170. | 0.39 | 0.28 | 0.19 | 0.12 | 0.12 | 0.04 | 0.07 | 170. |
| 175. | 0.40 | 0.29 | 0.21 | 0.13 | 0.13 | 0.05 | 0.07 | 175. |
| 180. | 0.40 | 0.28 | 0.22 | 0.13 | 0.13 | 0.06 | 0.06 | 180. |
| 185. | 0.39 | 0.26 | 0.23 | 0.13 | 0.12 | 0.06 | 0.05 | 185. |
| 190. | 0.36 | 0.24 | 0.22 | 0.13 | 0.11 | 0.06 | 0.05 | 190. |
| 195. | 0.32 | 0.21 | 0.20 | 0.12 | 0.10 | 0.06 | 0.02 | 195. |
| 200. | 0.28 | 0.19 | 0.17 | 0.11 | 0.08 | 0.05 | 0.01 | 200. |
| 205. | 0.23 | 0.16 | 0.14 | 0.09 | 0.05 | 0.05 | -0.00 | 205. |
| 210. | 0.16 | 0.15 | 0.12 | 0.07 | 0.02 | 0.04 | -0.01 | 210. |
| 215. | 0.12 | 0.13 | 0.06 | 0.04 | -0.01 | 0.03 | -0.02 | 215. |
| 220. | 0.07 | 0.09 | 0.03 | 0.02 | -0.03 | 0.02 | -0.03 | 220. |
| 225. | 0.01 | 0.02 | 0.01 | -0.01 | -0.04 | 0.01 | -0.03 | 225. |
| 230. | -0.04 | -0.04 | -0.02 | -0.02 | -0.04 | -0.03 | -0.04 | 230. |
| 235. | -0.09 | -0.08 | -0.04 | -0.04 | -0.05 | -0.01 | -0.04 | 235. |
| 240. | -0.13 | -0.11 | -0.06 | -0.06 | -0.06 | -0.01 | -0.04 | 240. |
| 245. | -0.17 | -0.14 | -0.08 | -0.07 | -0.07 | -0.02 | -0.05 | 245. |
| 250. | -0.21 | -0.17 | -0.10 | -0.08 | -0.08 | -0.02 | -0.05 | 250. |
| 255. | -0.24 | -0.19 | -0.10 | -0.09 | -0.09 | -0.03 | -0.05 | 255. |
| 260. | -0.27 | -0.21 | -0.11 | -0.10 | -0.11 | -0.03 | -0.05 | 260. |
| 265. | -0.28 | -0.23 | -0.13 | -0.10 | -0.12 | -0.03 | -0.05 | 265. |
| 270. | -0.33 | -0.26 | -0.15 | -0.11 | -0.13 | -0.03 | -0.05 | 270. |
| 275. | -0.34 | -0.28 | -0.17 | -0.12 | -0.13 | -0.03 | -0.05 | 275. |
| 280. | -0.38 | -0.29 | -0.17 | -0.13 | -0.14 | -0.03 | -0.05 | 280. |
| 285. | -0.39 | -0.31 | -0.20 | -0.14 | -0.15 | -0.03 | -0.05 | 285. |
| 290. | -0.40 | -0.32 | -0.21 | -0.15 | -0.15 | -0.04 | -0.05 | 290. |
| 295. | -0.40 | -0.32 | -0.21 | -0.15 | -0.15 | -0.04 | -0.06 | 295. |
| 300. | -0.40 | -0.32 | -0.21 | -0.15 | -0.15 | -0.04 | -0.06 | 300. |
| 305. | -0.39 | -0.31 | -0.21 | -0.14 | -0.15 | -0.04 | -0.06 | 305. |
| 310. | -0.39 | -0.30 | -0.19 | -0.14 | -0.14 | -0.04 | -0.06 | 310. |
| 315. | -0.38 | -0.27 | -0.18 | -0.13 | -0.13 | -0.04 | -0.06 | 315. |
| 320. | -0.35 | -0.24 | -0.16 | -0.11 | -0.12 | -0.03 | -0.06 | 320. |
| 325. | -0.31 | -0.21 | -0.13 | -0.10 | -0.11 | -0.03 | -0.05 | 325. |
| 330. | -0.24 | -0.17 | -0.10 | -0.08 | -0.10 | -0.02 | -0.05 | 330. |
| 335. | -0.16 | -0.15 | -0.08 | -0.06 | -0.09 | -0.01 | -0.05 | 335. |
| 340. | -0.10 | -0.14 | -0.07 | -0.04 | -0.07 | -0.00 | -0.05 | 340. |
| 345. | -0.06 | -0.13 | -0.05 | -0.02 | -0.05 | 0.01 | -0.03 | 345. |
| 350. | -0.04 | -0.09 | -0.02 | -0.01 | -0.03 | 0.02 | -0.02 | 350. |
| 355. | -0.02 | -0.03 | 0.01 | -0.01 | 0.01 | 0.02 | -0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 496 TCN= 21. ' R.= 36.9

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.457 | 1.340 | 1.932 | 2.990 | 4.550 | 7.153 | 10.498 | DEG. |
| 0. | 0.17 | 0.11 | 0.11 | 0.11 | 0.09 | 0.06 | 0.02 | 0. |
| 5. | 0.29 | 0.15 | 0.13 | 0.13 | 0.10 | 0.04 | 0.03 | 5. |
| 10. | 0.39 | 0.26 | 0.17 | 0.14 | 0.11 | 0.04 | 0.02 | 10. |
| 15. | 0.27 | 0.23 | 0.11 | 0.10 | 0.09 | 0.03 | 0.01 | 15. |
| 20. | 0.05 | 0.12 | 0.00 | 0.06 | 0.05 | 0.02 | 0.00 | 20. |
| 25. | -0.17 | 0.00 | -0.06 | 0.00 | 0.01 | 0.02 | 0.01 | 25. |
| 30. | -0.16 | -0.10 | -0.08 | -0.01 | 0.02 | 0.02 | 0.01 | 30. |
| 35. | -0.13 | -0.11 | -0.08 | -0.02 | 0.02 | -0.00 | -0.01 | 35. |
| 40. | -0.05 | -0.08 | -0.06 | -0.02 | 0.02 | -0.02 | -0.01 | 40. |
| 45. | 0.02 | -0.04 | -0.04 | -0.01 | 0.02 | -0.03 | -0.01 | 45. |
| 50. | 0.08 | -0.03 | -0.02 | -0.00 | 0.01 | -0.03 | -0.02 | 50. |
| 55. | 0.08 | -0.03 | -0.01 | -0.01 | 0.03 | -0.03 | -0.03 | 55. |
| 60. | 0.04 | -0.04 | -0.01 | -0.02 | 0.03 | -0.04 | -0.04 | 60. |
| 65. | 0.02 | -0.05 | -0.03 | -0.03 | 0.02 | -0.04 | -0.04 | 65. |
| 70. | 0.01 | -0.06 | -0.03 | -0.05 | 0.01 | -0.04 | -0.04 | 70. |
| 75. | 0.03 | -0.08 | -0.07 | -0.07 | -0.00 | -0.05 | -0.04 | 75. |
| 80. | 0.07 | -0.10 | -0.09 | -0.09 | -0.01 | -0.06 | -0.05 | 80. |
| 85. | 0.11 | -0.11 | -0.10 | -0.10 | -0.02 | -0.07 | -0.05 | 85. |
| 90. | 0.11 | -0.11 | -0.13 | -0.11 | -0.02 | -0.08 | -0.05 | 90. |
| 95. | 0.09 | -0.09 | -0.09 | -0.10 | -0.01 | -0.08 | -0.05 | 95. |
| 100. | 0.14 | -0.05 | -0.07 | -0.09 | -0.02 | -0.08 | -0.05 | 100. |
| 105. | 0.20 | -0.02 | -0.04 | -0.07 | 0.01 | -0.08 | -0.05 | 105. |
| 110. | 0.20 | 0.01 | -0.01 | -0.04 | 0.02 | -0.07 | -0.05 | 110. |
| 115. | 0.31 | 0.08 | 0.02 | -0.02 | 0.03 | -0.05 | -0.04 | 115. |
| 120. | 0.34 | 0.11 | 0.05 | -0.00 | 0.04 | -0.04 | -0.03 | 120. |
| 125. | 0.34 | 0.11 | 0.06 | -0.01 | 0.05 | -0.03 | -0.02 | 125. |
| 130. | 0.32 | 0.10 | 0.06 | -0.02 | 0.05 | -0.02 | -0.02 | 130. |
| 135. | 0.29 | 0.08 | 0.05 | -0.04 | 0.04 | -0.02 | -0.02 | 135. |
| 140. | 0.27 | 0.08 | 0.03 | 0.05 | 0.04 | -0.01 | -0.02 | 140. |
| 145. | 0.28 | 0.09 | 0.09 | 0.02 | 0.04 | -0.01 | -0.02 | 145. |
| 150. | 0.26 | 0.11 | 0.06 | 0.03 | 0.07 | -0.01 | -0.01 | 150. |
| 155. | 0.26 | 0.14 | 0.08 | 0.04 | 0.06 | -0.01 | 0.00 | 155. |
| 160. | 0.26 | 0.16 | 0.10 | 0.05 | 0.09 | 0.01 | 0.01 | 160. |
| 165. | 0.27 | 0.19 | 0.12 | 0.06 | 0.10 | 0.03 | 0.01 | 165. |
| 170. | 0.28 | 0.22 | 0.13 | 0.08 | 0.11 | 0.04 | 0.01 | 170. |
| 175. | 0.29 | 0.25 | 0.14 | 0.09 | 0.11 | 0.05 | 0.03 | 175. |
| 180. | 0.30 | 0.26 | 0.15 | 0.11 | 0.11 | 0.05 | 0.03 | 180. |
| 185. | 0.29 | 0.27 | 0.16 | 0.12 | 0.10 | 0.04 | 0.03 | 185. |
| 190. | 0.28 | 0.26 | 0.16 | 0.12 | 0.09 | 0.04 | 0.03 | 190. |
| 195. | 0.25 | 0.25 | 0.15 | 0.12 | 0.08 | 0.04 | 0.03 | 195. |
| 200. | 0.21 | 0.22 | 0.14 | 0.11 | 0.05 | 0.03 | 0.03 | 200. |
| 205. | 0.16 | 0.20 | 0.12 | 0.10 | 0.04 | 0.03 | 0.03 | 205. |
| 210. | 0.10 | 0.17 | 0.11 | 0.08 | 0.02 | 0.04 | 0.03 | 210. |
| 215. | 0.04 | 0.13 | 0.09 | 0.07 | 0.01 | 0.04 | 0.03 | 215. |
| 220. | -0.02 | 0.10 | 0.07 | 0.06 | -0.02 | 0.03 | 0.03 | 220. |
| 225. | -0.06 | 0.06 | 0.04 | 0.04 | -0.01 | 0.03 | 0.03 | 225. |
| 230. | -0.07 | 0.03 | 0.04 | 0.03 | -0.02 | 0.03 | 0.03 | 230. |
| 235. | -0.11 | -0.01 | 0.02 | 0.01 | -0.03 | 0.03 | 0.03 | 235. |
| 240. | -0.10 | -0.04 | -0.00 | -0.00 | -0.04 | 0.02 | 0.03 | 240. |
| 245. | -0.13 | -0.06 | -0.03 | -0.02 | -0.04 | 0.02 | 0.02 | 245. |
| 250. | -0.12 | -0.12 | -0.05 | -0.03 | -0.04 | 0.01 | 0.01 | 250. |
| 255. | -0.11 | -0.16 | -0.08 | -0.05 | -0.10 | 0.00 | 0.01 | 255. |
| 260. | -0.07 | -0.20 | -0.11 | -0.07 | -0.11 | -0.00 | 0.01 | 260. |
| 265. | -0.08 | -0.23 | -0.14 | -0.09 | -0.12 | -0.01 | 0.01 | 265. |
| 270. | -0.07 | -0.25 | -0.16 | -0.10 | -0.13 | -0.02 | 0.01 | 270. |
| 275. | -0.07 | -0.25 | -0.16 | -0.11 | -0.14 | -0.02 | 0.01 | 275. |
| 280. | -0.08 | -0.26 | -0.16 | -0.11 | -0.14 | -0.02 | 0.01 | 280. |
| 285. | -0.11 | -0.28 | -0.19 | -0.11 | -0.14 | -0.02 | 0.01 | 285. |
| 290. | -0.12 | -0.30 | -0.17 | -0.11 | -0.14 | -0.02 | 0.00 | 290. |
| 295. | -0.08 | -0.30 | -0.16 | -0.10 | -0.14 | -0.02 | 0.00 | 295. |
| 300. | -0.03 | -0.29 | -0.16 | -0.11 | -0.14 | -0.02 | 0.00 | 300. |
| 305. | -0.02 | -0.27 | -0.16 | -0.11 | -0.13 | -0.01 | 0.00 | 305. |
| 310. | -0.01 | -0.27 | -0.15 | -0.10 | -0.12 | -0.01 | 0.00 | 310. |
| 315. | -0.00 | -0.27 | -0.14 | -0.10 | -0.11 | 0.00 | 0.01 | 315. |
| 320. | -0.02 | -0.22 | -0.11 | -0.05 | -0.11 | 0.01 | 0.01 | 320. |
| 325. | -0.02 | -0.15 | -0.06 | -0.02 | -0.08 | 0.02 | 0.01 | 325. |
| 330. | -0.01 | -0.07 | -0.01 | 0.01 | -0.05 | 0.03 | 0.01 | 330. |
| 335. | -0.05 | -0.06 | 0.04 | 0.03 | -0.01 | 0.03 | 0.01 | 335. |
| 340. | 0.01 | 0.06 | 0.06 | 0.05 | 0.02 | 0.03 | 0.02 | 340. |
| 345. | 0.05 | 0.13 | 0.12 | 0.08 | 0.04 | 0.04 | 0.02 | 345. |
| 350. | 0.09 | 0.17 | 0.14 | 0.10 | 0.05 | 0.04 | 0.01 | 350. |
| 355. | 0.13 | 0.17 | 0.14 | 0.11 | 0.06 | 0.04 | 0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 DATA NO. 494 TCH= 21. C.R.= 16.9

DIFFERENTIAL PRESSURES

SPAN STATION 153.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.422 | 1.246 | 1.950 | 2.997 | 4.550 | 7.122 | 10.490 | DEG. |
| 0. | 0.10 | 0.40 | 0.17 | 0.07 | 0.09 | 0.01 | 0.04 | 0. |
| 5. | 0.23 | 0.32 | 0.08 | 0.07 | 0.06 | 0.05 | 0.02 | 5. |
| 10. | 0.10 | 0.29 | 0.05 | 0.07 | 0.04 | 0.03 | 0.02 | 10. |
| 15. | 0.05 | 0.25 | 0.03 | 0.03 | 0.02 | 0.02 | 0.01 | 15. |
| 20. | -0.15 | 0.16 | -0.02 | -0.06 | -0.03 | -0.01 | 0.01 | 20. |
| 25. | -0.25 | 0.07 | -0.08 | -0.09 | -0.02 | -0.03 | -0.01 | 25. |
| 30. | -0.26 | 0.00 | -0.10 | -0.11 | -0.02 | -0.05 | -0.02 | 30. |
| 35. | -0.26 | -0.03 | -0.12 | -0.09 | -0.03 | -0.06 | -0.02 | 35. |
| 40. | -0.23 | 0.01 | -0.13 | -0.08 | -0.02 | -0.06 | -0.02 | 40. |
| 45. | -0.21 | 0.06 | -0.13 | -0.07 | -0.02 | -0.06 | -0.03 | 45. |
| 50. | -0.22 | 0.11 | -0.12 | -0.05 | -0.00 | -0.06 | -0.04 | 50. |
| 55. | -0.23 | 0.06 | -0.11 | -0.04 | 0.01 | -0.06 | -0.04 | 55. |
| 60. | -0.26 | -0.02 | -0.11 | -0.02 | 0.02 | -0.06 | -0.04 | 60. |
| 65. | -0.29 | -0.10 | -0.12 | -0.02 | 0.03 | -0.07 | -0.04 | 65. |
| 70. | -0.32 | -0.19 | -0.12 | -0.03 | 0.01 | -0.06 | -0.04 | 70. |
| 75. | -0.34 | -0.27 | -0.14 | -0.05 | -0.02 | -0.10 | -0.05 | 75. |
| 80. | -0.36 | -0.32 | -0.17 | -0.07 | -0.04 | -0.11 | -0.05 | 80. |
| 85. | -0.35 | -0.32 | -0.20 | -0.07 | -0.05 | -0.13 | -0.05 | 85. |
| 90. | -0.29 | -0.28 | -0.21 | -0.04 | -0.04 | -0.14 | -0.04 | 90. |
| 95. | -0.20 | -0.22 | -0.19 | -0.00 | -0.04 | -0.15 | -0.04 | 95. |
| 100. | -0.10 | -0.15 | -0.14 | 0.03 | -0.05 | -0.14 | -0.03 | 100. |
| 105. | -0.00 | -0.08 | -0.08 | 0.06 | -0.03 | -0.12 | -0.00 | 105. |
| 110. | 0.08 | -0.02 | -0.02 | 0.08 | -0.01 | -0.10 | -0.03 | 110. |
| 115. | 0.15 | 0.03 | 0.03 | 0.10 | 0.00 | -0.08 | -0.04 | 115. |
| 120. | 0.20 | 0.06 | 0.06 | 0.11 | 0.01 | -0.07 | -0.03 | 120. |
| 125. | 0.22 | 0.06 | 0.08 | 0.12 | 0.01 | -0.06 | -0.03 | 125. |
| 130. | 0.20 | 0.05 | 0.06 | 0.12 | 0.01 | -0.06 | -0.03 | 130. |
| 135. | 0.16 | 0.03 | 0.03 | 0.12 | 0.02 | -0.05 | -0.04 | 135. |
| 140. | 0.10 | 0.00 | 0.02 | 0.11 | 0.02 | -0.05 | -0.03 | 140. |
| 145. | 0.05 | -0.02 | 0.01 | 0.10 | 0.03 | -0.04 | -0.03 | 145. |
| 150. | 0.01 | -0.05 | 0.01 | 0.09 | 0.04 | -0.04 | -0.02 | 150. |
| 155. | -0.01 | -0.08 | 0.01 | 0.07 | 0.05 | -0.03 | -0.02 | 155. |
| 160. | -0.01 | -0.07 | 0.01 | 0.06 | 0.07 | -0.02 | -0.01 | 160. |
| 165. | 0.01 | 0.02 | 0.01 | 0.05 | 0.09 | -0.01 | -0.00 | 165. |
| 170. | 0.04 | 0.10 | 0.03 | 0.10 | 0.11 | 0.02 | 0.00 | 170. |
| 175. | 0.12 | 0.33 | 0.06 | 0.11 | 0.11 | 0.01 | 0.01 | 175. |
| 180. | 0.18 | 0.49 | 0.09 | 0.12 | 0.12 | 0.03 | 0.02 | 180. |
| 185. | 0.22 | 0.53 | 0.13 | 0.13 | 0.12 | 0.05 | 0.02 | 185. |
| 190. | 0.25 | 0.50 | 0.15 | 0.13 | 0.12 | 0.05 | 0.03 | 190. |
| 195. | 0.26 | 0.43 | 0.15 | 0.14 | 0.12 | 0.04 | 0.03 | 195. |
| 200. | 0.26 | 0.33 | 0.16 | 0.14 | 0.11 | 0.07 | 0.03 | 200. |
| 205. | 0.27 | 0.26 | 0.16 | 0.13 | 0.10 | 0.07 | 0.03 | 205. |
| 210. | 0.27 | 0.21 | 0.16 | 0.12 | 0.08 | 0.09 | 0.03 | 210. |
| 215. | 0.25 | 0.16 | 0.16 | 0.10 | 0.06 | 0.08 | 0.03 | 215. |
| 220. | 0.20 | 0.10 | 0.15 | 0.09 | 0.04 | 0.07 | 0.03 | 220. |
| 225. | 0.15 | 0.05 | 0.13 | 0.06 | 0.01 | 0.07 | 0.03 | 225. |
| 230. | 0.10 | -0.00 | 0.11 | 0.04 | -0.01 | 0.07 | 0.03 | 230. |
| 235. | 0.05 | -0.05 | 0.09 | 0.01 | -0.03 | 0.07 | 0.03 | 235. |
| 240. | 0.02 | -0.10 | 0.06 | -0.01 | -0.04 | 0.07 | 0.03 | 240. |
| 245. | -0.01 | -0.13 | 0.02 | -0.03 | -0.05 | 0.06 | 0.03 | 245. |
| 250. | -0.02 | -0.14 | -0.01 | -0.04 | -0.05 | 0.04 | 0.03 | 250. |
| 255. | 0.01 | -0.13 | -0.00 | -0.04 | -0.05 | 0.04 | 0.03 | 255. |
| 260. | 0.05 | -0.11 | 0.02 | -0.03 | -0.04 | 0.05 | 0.02 | 260. |
| 265. | 0.03 | -0.17 | 0.07 | -0.00 | -0.07 | 0.04 | 0.02 | 265. |
| 270. | -0.05 | -0.24 | 0.03 | -0.01 | -0.09 | 0.03 | 0.02 | 270. |
| 275. | -0.19 | -0.31 | -0.00 | -0.03 | -0.12 | 0.02 | 0.01 | 275. |
| 280. | -0.26 | -0.35 | -0.07 | -0.06 | -0.13 | 0.02 | 0.01 | 280. |
| 285. | -0.23 | -0.36 | -0.06 | -0.07 | -0.13 | 0.02 | 0.01 | 285. |
| 290. | -0.11 | -0.30 | -0.11 | -0.10 | -0.14 | 0.01 | 0.01 | 290. |
| 295. | -0.17 | -0.30 | -0.12 | -0.07 | -0.14 | 0.02 | 0.01 | 295. |
| 300. | -0.28 | -0.31 | -0.19 | -0.07 | -0.12 | 0.03 | 0.01 | 300. |
| 305. | -0.22 | -0.28 | -0.09 | -0.07 | -0.10 | 0.03 | 0.02 | 305. |
| 310. | -0.31 | -0.29 | -0.11 | -0.09 | -0.10 | 0.03 | 0.02 | 310. |
| 315. | -0.25 | -0.29 | -0.10 | -0.09 | -0.09 | 0.03 | 0.02 | 315. |
| 320. | -0.09 | -0.19 | -0.07 | -0.10 | -0.07 | 0.04 | 0.01 | 320. |
| 325. | 0.03 | -0.08 | -0.03 | -0.10 | -0.06 | 0.05 | 0.03 | 325. |
| 330. | 0.02 | -0.04 | -0.00 | -0.07 | -0.01 | 0.05 | 0.02 | 330. |
| 335. | 0.09 | -0.03 | 0.01 | -0.06 | 0.01 | 0.06 | 0.03 | 335. |
| 340. | 0.20 | 0.04 | 0.03 | -0.04 | 0.03 | 0.08 | 0.03 | 340. |
| 345. | 0.08 | 0.24 | 0.14 | 0.04 | 0.07 | 0.09 | 0.04 | 345. |
| 350. | 0.03 | 0.26 | 0.24 | 0.11 | 0.10 | 0.13 | 0.04 | 350. |
| 355. | 0.05 | 0.41 | 0.26 | 0.13 | 0.11 | 0.09 | 0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-498 CNTR NO. 494 TCN= 21. C.R.= 36.8

DIFFERENTIAL PRESSURES

SPAN STATION 170.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.493 | 1.042 | 1.993 | 2.993 | 4.993 | 7.159 | 10.489 | DEG. |
| 0. | 0.20 | 0.07 | 0.16 | 0.14 | 0.10 | 0.05 | 0.02 | 0. |
| 5. | 0.00 | 0.09 | 0.04 | 0.10 | 0.04 | 0.01 | 0.01 | 5. |
| 10. | -0.12 | 0.04 | -0.07 | 0.06 | -0.03 | -0.02 | -0.00 | 10. |
| 15. | -0.15 | -0.09 | -0.07 | 0.03 | -0.03 | -0.05 | -0.01 | 15. |
| 20. | -0.33 | -0.21 | -0.13 | -0.04 | -0.07 | -0.07 | -0.02 | 20. |
| 25. | -0.40 | -0.24 | -0.27 | -0.13 | -0.15 | -0.09 | -0.03 | 25. |
| 30. | -0.40 | -0.29 | -0.32 | -0.17 | -0.16 | -0.09 | -0.03 | 30. |
| 35. | -0.47 | -0.26 | -0.33 | -0.17 | -0.14 | -0.12 | -0.03 | 35. |
| 40. | -0.48 | -0.24 | -0.35 | -0.16 | -0.15 | -0.11 | -0.02 | 40. |
| 45. | -0.52 | -0.25 | -0.37 | -0.15 | -0.15 | -0.11 | -0.02 | 45. |
| 50. | -0.59 | -0.23 | -0.38 | -0.16 | -0.16 | -0.13 | -0.02 | 50. |
| 55. | -0.61 | -0.23 | -0.39 | -0.13 | -0.14 | -0.10 | -0.02 | 55. |
| 60. | -0.62 | -0.23 | -0.36 | -0.13 | -0.14 | -0.10 | -0.02 | 60. |
| 65. | -0.61 | -0.22 | -0.40 | -0.14 | -0.13 | -0.09 | -0.02 | 65. |
| 70. | -0.56 | -0.20 | -0.39 | -0.10 | -0.15 | -0.13 | -0.02 | 70. |
| 75. | -0.48 | -0.19 | -0.39 | -0.22 | -0.17 | -0.11 | -0.03 | 75. |
| 80. | -0.39 | -0.17 | -0.38 | -0.25 | -0.21 | -0.11 | -0.03 | 80. |
| 85. | -0.33 | -0.18 | -0.37 | -0.25 | -0.23 | -0.13 | -0.03 | 85. |
| 90. | -0.31 | -0.19 | -0.35 | -0.24 | -0.22 | -0.12 | -0.03 | 90. |
| 95. | -0.25 | -0.16 | -0.31 | -0.21 | -0.19 | -0.09 | -0.02 | 95. |
| 100. | -0.14 | -0.09 | -0.26 | -0.18 | -0.16 | -0.07 | -0.03 | 100. |
| 105. | -0.02 | -0.04 | -0.20 | -0.14 | -0.12 | -0.05 | 0.01 | 105. |
| 110. | 0.05 | -0.04 | -0.15 | -0.11 | -0.08 | -0.04 | 0.02 | 110. |
| 115. | 0.08 | -0.05 | -0.12 | -0.08 | -0.04 | -0.03 | 0.01 | 115. |
| 120. | 0.09 | -0.06 | -0.10 | -0.06 | -0.05 | -0.02 | -0.00 | 120. |
| 125. | 0.04 | -0.06 | -0.09 | -0.06 | -0.05 | -0.01 | -0.01 | 125. |
| 130. | 0.06 | -0.06 | -0.09 | -0.06 | -0.05 | -0.01 | -0.01 | 130. |
| 135. | 0.05 | -0.06 | -0.09 | -0.07 | -0.06 | -0.01 | -0.03 | 135. |
| 140. | 0.06 | -0.09 | -0.10 | -0.09 | -0.07 | -0.02 | -0.01 | 140. |
| 145. | 0.01 | -0.08 | -0.11 | -0.09 | -0.07 | -0.03 | -0.01 | 145. |
| 150. | -0.02 | -0.06 | -0.12 | -0.10 | -0.07 | -0.03 | -0.01 | 150. |
| 155. | -0.05 | -0.06 | -0.12 | -0.11 | -0.07 | -0.02 | -0.01 | 155. |
| 160. | -0.07 | -0.05 | -0.12 | -0.11 | -0.07 | -0.02 | -0.01 | 160. |
| 165. | -0.07 | -0.04 | -0.11 | -0.10 | -0.08 | -0.01 | -0.01 | 165. |
| 170. | -0.06 | -0.02 | -0.07 | -0.08 | -0.07 | 0.00 | -0.01 | 170. |
| 175. | 0.01 | 0.01 | -0.02 | -0.06 | -0.04 | 0.01 | -0.00 | 175. |
| 180. | 0.00 | 0.05 | 0.04 | -0.02 | 0.01 | 0.03 | 0.00 | 180. |
| 185. | 0.17 | 0.09 | 0.09 | 0.02 | 0.06 | 0.04 | 0.00 | 185. |
| 190. | 0.26 | 0.12 | 0.14 | 0.07 | 0.09 | 0.06 | 0.01 | 190. |
| 195. | 0.34 | 0.16 | 0.19 | 0.10 | 0.11 | 0.07 | 0.01 | 195. |
| 200. | 0.43 | 0.19 | 0.22 | 0.12 | 0.12 | 0.08 | 0.01 | 200. |
| 205. | 0.47 | 0.22 | 0.26 | 0.13 | 0.13 | 0.09 | 0.01 | 205. |
| 210. | 0.49 | 0.23 | 0.31 | 0.15 | 0.14 | 0.09 | 0.01 | 210. |
| 215. | 0.51 | 0.24 | 0.35 | 0.15 | 0.14 | 0.09 | 0.01 | 215. |
| 220. | 0.53 | 0.25 | 0.38 | 0.16 | 0.15 | 0.09 | 0.01 | 220. |
| 225. | 0.54 | 0.24 | 0.43 | 0.16 | 0.15 | 0.09 | 0.01 | 225. |
| 230. | 0.57 | 0.22 | 0.41 | 0.17 | 0.16 | 0.09 | 0.01 | 230. |
| 235. | 0.57 | 0.20 | 0.41 | 0.19 | 0.16 | 0.09 | 0.01 | 235. |
| 240. | 0.55 | 0.18 | 0.40 | 0.21 | 0.17 | 0.09 | 0.02 | 240. |
| 245. | 0.40 | 0.16 | 0.39 | 0.22 | 0.17 | 0.09 | 0.02 | 245. |
| 250. | 0.40 | 0.13 | 0.35 | 0.20 | 0.17 | 0.09 | 0.02 | 250. |
| 255. | 0.30 | 0.10 | 0.31 | 0.17 | 0.16 | 0.09 | 0.02 | 255. |
| 260. | 0.28 | 0.09 | 0.27 | 0.15 | 0.15 | 0.09 | 0.03 | 260. |
| 265. | 0.12 | 0.08 | 0.25 | 0.13 | 0.14 | 0.10 | 0.03 | 265. |
| 270. | 0.13 | 0.10 | 0.24 | 0.12 | 0.13 | 0.07 | 0.03 | 270. |
| 275. | 0.14 | 0.12 | 0.21 | 0.11 | 0.11 | 0.05 | 0.02 | 275. |
| 280. | 0.11 | 0.11 | 0.16 | 0.10 | 0.10 | 0.04 | 0.02 | 280. |
| 285. | -0.02 | 0.09 | 0.12 | 0.06 | 0.09 | 0.01 | 0.01 | 285. |
| 290. | -0.11 | 0.07 | 0.09 | 0.04 | 0.08 | 0.02 | 0.01 | 290. |
| 295. | -0.18 | 0.07 | 0.09 | 0.05 | 0.09 | 0.02 | 0.00 | 295. |
| 300. | -0.07 | 0.07 | 0.12 | 0.11 | 0.09 | 0.04 | 0.00 | 300. |
| 305. | -0.10 | 0.02 | 0.09 | 0.07 | 0.07 | 0.03 | -0.00 | 305. |
| 310. | -0.25 | 0.02 | -0.05 | -0.01 | -0.00 | -0.03 | -0.00 | 310. |
| 315. | -0.14 | 0.03 | -0.03 | 0.07 | -0.01 | 0.00 | -0.00 | 315. |
| 320. | -0.03 | 0.02 | 0.10 | 0.05 | 0.02 | 0.01 | 0.00 | 320. |
| 325. | -0.10 | 0.01 | 0.02 | 0.04 | -0.01 | -0.03 | 0.00 | 325. |
| 330. | -0.11 | 0.01 | 0.01 | 0.04 | -0.02 | 0.01 | -0.03 | 330. |
| 335. | 0.10 | 0.05 | 0.13 | 0.09 | 0.05 | 0.03 | 0.00 | 335. |
| 340. | 0.28 | 0.09 | 0.24 | 0.13 | 0.11 | 0.05 | 0.01 | 340. |
| 345. | 0.27 | 0.12 | 0.25 | 0.13 | 0.12 | 0.06 | 0.01 | 345. |
| 350. | 0.29 | 0.13 | 0.22 | 0.13 | 0.11 | 0.07 | 0.01 | 350. |
| 355. | 0.33 | 0.11 | 0.20 | 0.14 | 0.11 | 0.07 | 0.0. | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 DATA NO. 494 TCN= 21. C.G.= 36.0

DIFFERENTIAL PRESSURES

SPAN STATION 100.0

| AC | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.695 | 1.346 | 1.999 | 3.998 | 4.994 | 7.150 | 10.420 | DEG. |
| 0. | 3.36 | 0.24 | 0.17 | 0.19 | 0.03 | 0.98 | 0.02 | 0. |
| 5. | -3.01 | 0.00 | 0.04 | 0.00 | 0.03 | 0.35 | 0.01 | 5. |
| 10. | -3.37 | -0.19 | -0.08 | -0.05 | -0.02 | 0.01 | 0.00 | 10. |
| 15. | -3.56 | -0.39 | -0.16 | -0.11 | -0.00 | -0.33 | -0.01 | 15. |
| 20. | -3.68 | -0.52 | -0.27 | -0.16 | -0.10 | -0.56 | -0.04 | 20. |
| 25. | -3.79 | -0.58 | -0.37 | -0.20 | -0.20 | -0.98 | -0.04 | 25. |
| 30. | -3.77 | -0.57 | -0.38 | -0.24 | -0.07 | -0.13 | -0.03 | 30. |
| 35. | -0.67 | -0.53 | -0.34 | -0.28 | -0.05 | -0.11 | -0.03 | 35. |
| 40. | -3.70 | -0.54 | -0.33 | -0.26 | -0.23 | -0.11 | -0.04 | 40. |
| 45. | -3.81 | -0.56 | -0.33 | -0.24 | -0.21 | -0.11 | -0.04 | 45. |
| 50. | -3.85 | -0.59 | -0.34 | -0.25 | 0.01 | -0.11 | -0.04 | 50. |
| 55. | -0.86 | -0.60 | -0.34 | -0.23 | 0.02 | -0.13 | -0.04 | 55. |
| 60. | -3.83 | -0.56 | -0.34 | -0.23 | 0.04 | -0.13 | -0.04 | 60. |
| 65. | -3.76 | -0.53 | -0.32 | -0.23 | 0.04 | -0.11 | -0.04 | 65. |
| 70. | -3.67 | -0.50 | -0.30 | -0.24 | 0.04 | -0.12 | -0.04 | 70. |
| 75. | -0.33 | -0.47 | -0.31 | -0.25 | -0.30 | -0.14 | -0.04 | 75. |
| 80. | -3.61 | -0.43 | -0.33 | -0.28 | -0.01 | -0.16 | -0.04 | 80. |
| 85. | -0.39 | -0.38 | -0.34 | -0.29 | 0.01 | -0.17 | -0.04 | 85. |
| 90. | -0.38 | -0.31 | -0.29 | -0.27 | 0.39 | -0.17 | -0.04 | 90. |
| 95. | -0.29 | -0.24 | -0.21 | -0.22 | 0.22 | -0.15 | -0.03 | 95. |
| 100. | -0.19 | -0.15 | -0.12 | -0.13 | 0.26 | -0.13 | -0.02 | 100. |
| 105. | -0.17 | -0.07 | -0.04 | -0.00 | 0.27 | -0.11 | -0.02 | 105. |
| 110. | -0.13 | 0.00 | 0.05 | 0.07 | 0.31 | -0.09 | -0.01 | 110. |
| 115. | 0.31 | 0.08 | 0.13 | 0.09 | 0.34 | -0.08 | -0.01 | 115. |
| 120. | 0.19 | 0.15 | 0.19 | 0.14 | 0.35 | -0.07 | -0.01 | 120. |
| 125. | 0.19 | 0.19 | 0.16 | 0.04 | 0.32 | -0.06 | -0.01 | 125. |
| 130. | 0.17 | 0.13 | 0.12 | 0.04 | 0.28 | -0.06 | -0.01 | 130. |
| 135. | 0.08 | 0.04 | 0.09 | 0.06 | 0.23 | -0.07 | -0.01 | 135. |
| 140. | -0.03 | -0.04 | -0.03 | -0.10 | 0.17 | -0.07 | -0.01 | 140. |
| 145. | -0.20 | -0.19 | -0.13 | -0.14 | 0.11 | -0.07 | -0.01 | 145. |
| 150. | -0.35 | -0.23 | -0.18 | -0.18 | 0.06 | -0.07 | -0.01 | 150. |
| 155. | -0.46 | -0.28 | -0.20 | -0.21 | 0.03 | -0.07 | -0.02 | 155. |
| 160. | -0.51 | -0.34 | -0.22 | -0.23 | 0.01 | -0.06 | -0.02 | 160. |
| 165. | -0.51 | -0.36 | -0.23 | -0.23 | 0.00 | -0.05 | -0.01 | 165. |
| 170. | -0.46 | -0.34 | -0.21 | -0.21 | 0.00 | -0.04 | -0.01 | 170. |
| 175. | -0.37 | -0.29 | -0.18 | -0.18 | 0.01 | -0.03 | -0.00 | 175. |
| 180. | -0.26 | -0.14 | -0.14 | -0.13 | 0.02 | -0.01 | 0.00 | 180. |
| 185. | -0.13 | -0.03 | -0.08 | -0.07 | 0.02 | 0.01 | 0.01 | 185. |
| 190. | 0.01 | 0.07 | 0.01 | -0.00 | 0.02 | 0.04 | 0.01 | 190. |
| 195. | 0.14 | 0.17 | 0.11 | 0.05 | 0.02 | 0.05 | 0.02 | 195. |
| 200. | 0.23 | 0.24 | 0.20 | 0.10 | -0.00 | 0.06 | 0.02 | 200. |
| 205. | 0.31 | 0.28 | 0.26 | 0.13 | -0.03 | 0.07 | 0.02 | 205. |
| 210. | 0.36 | 0.31 | 0.25 | 0.14 | -0.06 | 0.07 | 0.02 | 210. |
| 215. | 0.40 | 0.33 | 0.25 | 0.15 | -0.07 | 0.08 | 0.02 | 215. |
| 220. | 0.45 | 0.34 | 0.25 | 0.17 | -0.08 | 0.08 | 0.02 | 220. |
| 225. | 0.47 | 0.38 | 0.25 | 0.19 | -0.08 | 0.09 | 0.02 | 225. |
| 230. | 0.51 | 0.42 | 0.28 | 0.22 | -0.08 | 0.11 | 0.03 | 230. |
| 235. | 0.57 | 0.48 | 0.29 | 0.24 | -0.08 | 0.12 | 0.03 | 235. |
| 240. | 0.70 | 0.58 | 0.33 | 0.27 | -0.07 | 0.13 | 0.03 | 240. |
| 245. | 0.86 | 0.67 | 0.41 | 0.30 | -0.06 | 0.13 | 0.04 | 245. |
| 250. | 0.98 | 0.74 | 0.46 | 0.33 | -0.04 | 0.14 | 0.04 | 250. |
| 255. | 1.03 | 0.76 | 0.46 | 0.35 | -0.02 | 0.14 | 0.04 | 255. |
| 260. | 0.98 | 0.69 | 0.38 | 0.37 | -0.00 | 0.14 | 0.04 | 260. |
| 265. | 0.72 | 0.50 | 0.28 | 0.39 | -0.02 | 0.13 | 0.03 | 265. |
| 270. | 0.60 | 0.41 | 0.23 | 0.38 | -0.01 | 0.12 | 0.03 | 270. |
| 275. | 0.54 | 0.34 | 0.21 | 0.23 | -0.11 | 0.11 | 0.04 | 275. |
| 280. | 0.49 | 0.27 | 0.19 | 0.18 | -0.15 | 0.10 | 0.03 | 280. |
| 285. | 0.41 | 0.23 | 0.15 | 0.16 | -0.17 | 0.09 | 0.03 | 285. |
| 290. | 0.32 | 0.20 | 0.12 | 0.15 | -0.17 | 0.09 | 0.03 | 290. |
| 295. | 0.28 | 0.21 | 0.08 | 0.15 | -0.15 | 0.12 | 0.03 | 295. |
| 300. | 0.31 | 0.19 | 0.14 | 0.19 | -0.14 | 0.19 | 0.03 | 300. |
| 305. | 0.25 | 0.05 | 0.11 | 0.19 | -0.15 | 0.28 | 0.03 | 305. |
| 310. | -0.13 | -0.14 | -0.06 | 0.01 | -0.25 | 0.03 | 0.02 | 310. |
| 315. | 0.11 | 0.02 | -0.01 | 0.04 | -0.19 | 0.05 | 0.02 | 315. |
| 320. | 0.10 | -0.03 | -0.04 | 0.00 | -0.10 | 0.04 | 0.01 | 320. |
| 325. | -0.07 | -0.06 | -0.04 | 0.01 | -0.21 | 0.01 | 0.01 | 325. |
| 330. | 0.16 | 0.15 | 0.09 | 0.07 | -0.13 | 0.09 | 0.02 | 330. |
| 335. | 0.40 | 0.31 | 0.19 | 0.16 | -0.06 | 0.17 | 0.02 | 335. |
| 340. | 0.49 | 0.25 | 0.15 | 0.17 | -0.05 | 0.07 | 0.02 | 340. |
| 345. | 0.55 | 0.19 | 0.13 | 0.16 | -0.04 | 0.07 | 0.02 | 345. |
| 350. | 0.39 | 0.20 | 0.14 | 0.15 | -0.02 | 0.07 | 0.03 | 350. |
| 355. | 0.43 | 0.25 | 0.18 | 0.17 | 0.01 | 0.08 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 494 TCN= 21. C.R.= 36.0

DIFFERENTIAL PRESSURES

SPAN STATION 149.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.455 | 1.240 | 1.959 | 2.990 | 4.550 | 7.152 | 10.490 | DEG. |
| 0. | 0.35 | 0.23 | 0.16 | 0.09 | 0.04 | 0.05 | 0.01 | 0. |
| 5. | 0.05 | 0.04 | 0.05 | -0.05 | -0.02 | 0.02 | -0.00 | 5. |
| 10. | -0.32 | -0.14 | -0.10 | -0.14 | -0.08 | -0.02 | -0.01 | 10. |
| 15. | -0.56 | -0.28 | -0.21 | -0.18 | -0.11 | -0.06 | -0.02 | 15. |
| 20. | -0.66 | -0.43 | -0.29 | -0.23 | -0.12 | -0.09 | -0.04 | 20. |
| 25. | -0.77 | -0.57 | -0.35 | -0.29 | -0.13 | -0.11 | -0.05 | 25. |
| 30. | -0.85 | -0.62 | -0.38 | -0.31 | -0.15 | -0.13 | -0.06 | 30. |
| 35. | -0.86 | -0.57 | -0.40 | -0.32 | -0.16 | -0.11 | -0.05 | 35. |
| 40. | -0.81 | -0.50 | -0.41 | -0.31 | -0.15 | -0.11 | -0.05 | 40. |
| 45. | -0.84 | -0.51 | -0.41 | -0.29 | -0.13 | -0.12 | -0.05 | 45. |
| 50. | -0.42 | -0.52 | -0.43 | -0.28 | -0.11 | -0.11 | -0.05 | 50. |
| 55. | -0.99 | -0.54 | -0.38 | -0.26 | -0.09 | -0.11 | -0.05 | 55. |
| 60. | -0.93 | -0.45 | -0.34 | -0.25 | -0.08 | -0.11 | -0.05 | 60. |
| 65. | -0.88 | -0.36 | -0.34 | -0.24 | -0.10 | -0.11 | -0.05 | 65. |
| 70. | -0.36 | -0.24 | -0.31 | -0.23 | 0.13 | -0.12 | -0.06 | 70. |
| 75. | -0.26 | -0.36 | -0.29 | -0.23 | -0.15 | -0.15 | -0.06 | 75. |
| 80. | -0.24 | -0.05 | -0.27 | -0.23 | -0.14 | -0.10 | -0.07 | 80. |
| 85. | -0.25 | -0.62 | -0.24 | -0.22 | -0.11 | -0.17 | -0.06 | 85. |
| 90. | -0.26 | -0.43 | -0.19 | -0.17 | -0.08 | -0.15 | -0.06 | 90. |
| 95. | -0.24 | -0.21 | -0.11 | -0.09 | -0.04 | -0.12 | -0.05 | 95. |
| 100. | -0.36 | -0.09 | -0.01 | -0.01 | 0.00 | -0.17 | -0.04 | 100. |
| 105. | 0.14 | 0.14 | 0.08 | 0.06 | 0.04 | -0.13 | -0.03 | 105. |
| 110. | 0.26 | 0.41 | 0.16 | 0.12 | 0.08 | -0.09 | -0.02 | 110. |
| 115. | 0.28 | 0.44 | 0.21 | 0.14 | 0.12 | -0.06 | -0.02 | 115. |
| 120. | 0.23 | 0.38 | 0.17 | 0.10 | 0.11 | -0.09 | -0.03 | 120. |
| 125. | 0.13 | 0.29 | 0.18 | 0.04 | 0.09 | -0.13 | -0.04 | 125. |
| 130. | -0.01 | 0.17 | 0.03 | -0.03 | 0.06 | -0.15 | -0.04 | 130. |
| 135. | -0.18 | 0.02 | -0.10 | -0.10 | 0.02 | -0.13 | -0.04 | 135. |
| 140. | -0.25 | -0.13 | -0.10 | -0.10 | -0.01 | -0.11 | -0.03 | 140. |
| 145. | -0.32 | -0.31 | -0.27 | -0.22 | -0.05 | -0.12 | -0.03 | 145. |
| 150. | -0.44 | -0.43 | -0.33 | -0.26 | -0.08 | -0.12 | -0.02 | 150. |
| 155. | -0.77 | -0.50 | -0.37 | -0.28 | -0.11 | -0.12 | -0.02 | 155. |
| 160. | -0.83 | -0.54 | -0.39 | -0.29 | -0.12 | -0.10 | -0.01 | 160. |
| 165. | -0.83 | -0.54 | -0.38 | -0.28 | -0.12 | -0.09 | -0.01 | 165. |
| 170. | -0.77 | -0.51 | -0.36 | -0.25 | -0.10 | -0.07 | 0.00 | 170. |
| 175. | -0.66 | -0.45 | -0.32 | -0.21 | -0.06 | -0.04 | 0.01 | 175. |
| 180. | -0.52 | -0.34 | -0.25 | -0.15 | -0.02 | -0.02 | 0.02 | 180. |
| 185. | -0.35 | -0.24 | -0.17 | -0.09 | 0.02 | 0.01 | 0.02 | 185. |
| 190. | -0.18 | -0.15 | -0.10 | -0.03 | 0.05 | 0.03 | 0.03 | 190. |
| 195. | -0.04 | -0.05 | -0.05 | 0.02 | 0.06 | 0.05 | 0.04 | 195. |
| 200. | 0.03 | 0.02 | 0.00 | 0.07 | 0.07 | 0.06 | 0.04 | 200. |
| 205. | 0.06 | 0.04 | 0.04 | 0.11 | 0.07 | 0.07 | 0.04 | 205. |
| 210. | 0.12 | 0.06 | 0.08 | 0.12 | 0.07 | 0.08 | 0.04 | 210. |
| 215. | 0.19 | 0.08 | 0.11 | 0.12 | 0.07 | 0.09 | 0.04 | 215. |
| 220. | 0.24 | 0.14 | 0.14 | 0.13 | 0.07 | 0.09 | 0.04 | 220. |
| 225. | 0.34 | 0.21 | 0.17 | 0.13 | 0.06 | 0.09 | 0.04 | 225. |
| 230. | 0.44 | 0.26 | 0.20 | 0.14 | 0.07 | 0.11 | 0.04 | 230. |
| 235. | 0.53 | 0.30 | 0.23 | 0.16 | 0.07 | 0.12 | 0.05 | 235. |
| 240. | 0.64 | 0.35 | 0.27 | 0.21 | 0.08 | 0.13 | 0.05 | 240. |
| 245. | 0.74 | 0.41 | 0.32 | 0.26 | 0.11 | 0.15 | 0.06 | 245. |
| 250. | 0.86 | 0.51 | 0.39 | 0.32 | 0.15 | 0.16 | 0.06 | 250. |
| 255. | 1.00 | 0.62 | 0.49 | 0.39 | 0.17 | 0.17 | 0.06 | 255. |
| 260. | 1.12 | 0.76 | 0.57 | 0.45 | 0.19 | 0.18 | 0.06 | 260. |
| 265. | 1.35 | 0.87 | 0.64 | 0.49 | 0.18 | 0.18 | 0.06 | 265. |
| 270. | 1.21 | 0.90 | 0.62 | 0.46 | 0.17 | 0.16 | 0.06 | 270. |
| 275. | 0.97 | 0.62 | 0.55 | 0.39 | 0.14 | 0.16 | 0.06 | 275. |
| 280. | 0.81 | 0.51 | 0.44 | 0.31 | 0.11 | 0.16 | 0.06 | 280. |
| 285. | 0.71 | 0.47 | 0.39 | 0.26 | 0.08 | 0.17 | 0.06 | 285. |
| 290. | 0.65 | 0.44 | 0.38 | 0.23 | 0.09 | 0.17 | 0.05 | 290. |
| 295. | 0.59 | 0.41 | 0.36 | 0.23 | 0.10 | 0.18 | 0.04 | 295. |
| 300. | 0.62 | 0.34 | 0.33 | 0.28 | 0.09 | 0.15 | 0.03 | 300. |
| 305. | 0.44 | 0.26 | 0.23 | 0.17 | 0.04 | 0.09 | 0.02 | 305. |
| 310. | -0.11 | -0.03 | -0.06 | -0.01 | -0.07 | 0.03 | 0.01 | 310. |
| 315. | 0.29 | 0.12 | 0.08 | 0.06 | -0.03 | 0.06 | 0.01 | 315. |
| 320. | -0.03 | -0.01 | -0.03 | -0.03 | -0.09 | 0.04 | 0.00 | 320. |
| 325. | 0.00 | -0.00 | -0.04 | 0.00 | -0.07 | 0.03 | 0.01 | 325. |
| 330. | 0.42 | 0.31 | 0.16 | 0.17 | 0.02 | 0.06 | 0.02 | 330. |
| 335. | 0.47 | 0.32 | 0.18 | 0.13 | 0.02 | 0.06 | 0.01 | 335. |
| 340. | 0.27 | 0.18 | 0.10 | 0.06 | -0.01 | 0.04 | 0.01 | 340. |
| 345. | 0.22 | 0.17 | 0.11 | 0.08 | -0.01 | 0.04 | 0.01 | 345. |
| 350. | 0.34 | 0.28 | 0.16 | 0.07 | 0.03 | 0.05 | 0.01 | 350. |
| 355. | 0.44 | 0.32 | 0.19 | 0.12 | 0.05 | 0.06 | 0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=901 CNTR NO. 346 TC= 23. C.R.= 42.C

DIFFERENTIAL PRESSURES

SPAN STATION 92.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.425 | 1.950 | 4.250 | 10.400 | DEG. |
| 0. | -0.37 | -0.16 | -0.07 | 0.00 | 0. |
| 5. | -0.39 | -0.24 | -0.11 | -0.01 | 5. |
| 10. | -0.44 | -0.30 | -0.08 | -0.02 | 10. |
| 15. | -0.42 | -0.21 | -0.09 | -0.01 | 15. |
| 20. | -0.38 | -0.13 | -0.07 | -0.01 | 20. |
| 25. | -0.28 | -0.14 | -0.06 | -0.02 | 25. |
| 30. | -0.29 | -0.14 | -0.07 | -0.03 | 30. |
| 35. | -0.16 | -0.13 | -0.06 | -0.03 | 35. |
| 40. | -0.01 | -0.11 | -0.05 | -0.03 | 40. |
| 45. | -0.07 | -0.09 | -0.05 | -0.04 | 45. |
| 50. | -0.06 | -0.10 | -0.05 | -0.04 | 50. |
| 55. | -0.02 | -0.07 | -0.05 | -0.04 | 55. |
| 60. | 0.03 | -0.07 | -0.05 | -0.03 | 60. |
| 65. | 0.09 | -0.06 | -0.05 | -0.03 | 65. |
| 70. | 0.12 | -0.06 | -0.03 | -0.03 | 70. |
| 75. | 0.14 | -0.04 | -0.01 | -0.03 | 75. |
| 80. | 0.17 | -0.03 | -0.00 | -0.03 | 80. |
| 85. | 0.21 | 0.00 | 0.01 | -0.02 | 85. |
| 90. | 0.25 | 0.05 | 0.01 | -0.03 | 90. |
| 95. | 0.29 | 0.10 | 0.03 | -0.03 | 95. |
| 100. | 0.35 | 0.15 | 0.05 | -0.02 | 100. |
| 105. | 0.41 | 0.17 | 0.08 | -0.02 | 105. |
| 110. | 0.49 | 0.19 | 0.11 | -0.01 | 110. |
| 115. | 0.53 | 0.20 | 0.13 | 0.00 | 115. |
| 120. | 0.57 | 0.21 | 0.15 | 0.01 | 120. |
| 125. | 0.60 | 0.23 | 0.16 | 0.01 | 125. |
| 130. | 0.63 | 0.24 | 0.16 | 0.01 | 130. |
| 135. | 0.65 | 0.26 | 0.18 | 0.03 | 135. |
| 140. | 0.67 | 0.28 | 0.18 | 0.04 | 140. |
| 145. | 0.69 | 0.30 | 0.18 | 0.03 | 145. |
| 150. | 0.70 | 0.32 | 0.18 | 0.03 | 150. |
| 155. | 0.71 | 0.34 | 0.19 | 0.02 | 155. |
| 160. | 0.72 | 0.35 | 0.19 | 0.03 | 160. |
| 165. | 0.72 | 0.35 | 0.19 | 0.03 | 165. |
| 170. | 0.72 | 0.35 | 0.19 | 0.03 | 170. |
| 175. | 0.71 | 0.34 | 0.18 | 0.03 | 175. |
| 180. | 0.67 | 0.33 | 0.17 | 0.03 | 180. |
| 185. | 0.58 | 0.30 | 0.16 | 0.03 | 185. |
| 190. | 0.48 | 0.27 | 0.15 | 0.03 | 190. |
| 195. | 0.36 | 0.24 | 0.12 | 0.03 | 195. |
| 200. | 0.25 | 0.19 | 0.08 | 0.03 | 200. |
| 205. | 0.16 | 0.13 | 0.04 | 0.02 | 205. |
| 210. | 0.03 | 0.06 | -0.00 | 0.01 | 210. |
| 215. | -0.09 | 0.01 | -0.03 | 0.02 | 215. |
| 220. | -0.18 | -0.04 | -0.04 | 0.02 | 220. |
| 225. | -0.25 | -0.08 | -0.06 | 0.01 | 225. |
| 230. | -0.28 | -0.11 | -0.07 | 0.01 | 230. |
| 235. | -0.27 | -0.12 | -0.08 | 0.01 | 235. |
| 240. | -0.29 | -0.1. | -0.08 | .01 | 240. |
| 245. | -0.34 | -0.14 | -0.08 | 0.02 | 245. |
| 250. | -0.39 | -0.15 | -0.09 | 0.01 | 250. |
| 255. | -0.40 | -0.15 | -0.09 | 0.00 | 255. |
| 260. | -0.40 | -0.15 | -0.10 | 0.00 | 260. |
| 265. | -0.39 | -0.15 | -0.10 | 0.00 | 265. |
| 270. | -0.38 | -0.15 | -0.10 | 0.00 | 270. |
| 275. | -0.39 | -0.15 | -0.10 | -0.00 | 275. |
| 280. | -0.39 | -0.15 | -0.10 | -0.01 | 280. |
| 285. | -0.39 | -0.15 | -0.10 | -0.01 | 285. |
| 290. | -0.40 | -0.14 | -0.10 | -0.01 | 290. |
| 295. | -0.40 | -0.14 | -0.10 | -0.00 | 295. |
| 300. | -0.40 | -0.14 | -0.09 | -0.00 | 300. |
| 305. | -0.41 | -0.14 | -0.09 | -0.00 | 305. |
| 310. | -0.41 | -0.14 | -0.09 | -0.00 | 310. |
| 315. | -0.41 | -0.14 | -0.09 | -0.00 | 315. |
| 320. | -0.41 | -0.14 | -0.09 | 0.00 | 320. |
| 325. | -0.40 | -0.14 | -0.08 | 0.00 | 325. |
| 330. | -0.42 | -0.15 | -0.08 | -0.00 | 330. |
| 335. | -0.43 | -0.15 | -0.09 | -0.00 | 335. |
| 340. | -0.39 | -0.15 | -0.08 | -0.00 | 340. |
| 345. | -0.36 | -0.14 | -0.07 | 0.00 | 345. |
| 350. | -0.37 | -0.15 | -0.06 | 0.00 | 350. |
| 355. | -0.42 | -0.18 | -0.07 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-501 CNTR NO. 346 TCM= 23. C.R.= 42.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.959 | 2.990 | 4.590 | 7.150 | 13.490 | DEG. |
| 0. | -1.06 | -0.81 | -0.56 | -0.34 | -0.23 | -0.13 | -0.09 | 0. |
| 5. | -0.89 | -0.56 | -0.40 | -0.25 | -0.20 | -0.09 | -0.08 | 5. |
| 10. | -0.78 | -0.51 | -0.39 | -0.24 | -0.16 | -0.08 | -0.09 | 10. |
| 15. | -0.66 | -0.48 | -0.32 | -0.23 | -0.14 | -0.06 | -0.08 | 15. |
| 20. | -0.63 | -0.44 | -0.31 | -0.23 | -0.13 | -0.08 | -0.07 | 20. |
| 25. | -0.48 | -0.41 | -0.29 | -0.21 | -0.12 | -0.07 | -0.07 | 25. |
| 30. | -0.33 | -0.31 | -0.24 | -0.19 | -0.10 | -0.07 | -0.06 | 30. |
| 35. | -0.26 | -0.20 | -0.20 | -0.17 | -0.09 | -0.07 | -0.05 | 35. |
| 40. | -0.20 | -0.16 | -0.16 | -0.16 | -0.07 | -0.07 | -0.02 | 40. |
| 45. | -0.10 | -0.13 | -0.17 | -0.15 | -0.06 | -0.07 | 0.02 | 45. |
| 50. | -0.02 | -0.12 | -0.14 | -0.13 | -0.06 | -0.07 | 0.04 | 50. |
| 55. | 0.01 | -0.10 | -0.13 | -0.12 | -0.05 | -0.07 | 0.04 | 55. |
| 60. | 0.02 | -0.08 | -0.12 | -0.10 | -0.02 | -0.07 | 0.04 | 60. |
| 65. | 0.04 | -0.06 | -0.11 | -0.07 | -0.01 | -0.07 | 0.04 | 65. |
| 70. | 0.07 | -0.02 | -0.09 | -0.04 | 0.01 | -0.07 | 0.04 | 70. |
| 75. | 0.12 | 0.02 | -0.07 | -0.00 | 0.04 | -0.06 | 0.04 | 75. |
| 80. | 0.18 | 0.07 | -0.05 | 0.03 | 0.07 | -0.05 | 0.02 | 80. |
| 85. | 0.26 | 0.11 | -0.02 | 0.07 | 0.11 | -0.04 | 0.00 | 85. |
| 90. | 0.36 | 0.16 | 0.04 | 0.12 | 0.14 | -0.02 | 0.00 | 90. |
| 95. | 0.45 | 0.22 | 0.11 | 0.15 | 0.16 | -0.02 | 0.01 | 95. |
| 100. | 0.51 | 0.30 | 0.16 | 0.16 | 0.18 | -0.01 | 0.05 | 100. |
| 105. | 0.55 | 0.36 | 0.18 | 0.19 | 0.19 | 0.01 | 0.10 | 105. |
| 110. | 0.58 | 0.40 | 0.19 | 0.22 | 0.19 | 0.02 | 0.12 | 110. |
| 115. | 0.61 | 0.42 | 0.21 | 0.26 | 0.20 | 0.06 | 0.13 | 115. |
| 120. | 0.63 | 0.44 | 0.23 | 0.28 | 0.23 | 0.07 | 0.14 | 120. |
| 125. | 0.66 | 0.47 | 0.25 | 0.29 | 0.25 | 0.07 | 0.15 | 125. |
| 130. | 0.70 | 0.49 | 0.27 | 0.30 | 0.26 | 0.07 | 0.15 | 130. |
| 135. | 0.75 | 0.51 | 0.29 | 0.32 | 0.26 | 0.09 | 0.15 | 135. |
| 140. | 0.80 | 0.54 | 0.32 | 0.34 | 0.27 | 0.10 | 0.16 | 140. |
| 145. | 0.85 | 0.58 | 0.36 | 0.34 | 0.28 | 0.11 | 0.17 | 145. |
| 150. | 0.88 | 0.61 | 0.41 | 0.34 | 0.28 | 0.12 | 0.18 | 150. |
| 155. | 0.94 | 0.65 | 0.44 | 0.34 | 0.28 | 0.12 | 0.19 | 155. |
| 160. | 1.04 | 0.82 | 0.47 | 0.35 | 0.28 | 0.13 | 0.19 | 160. |
| 165. | 1.16 | 0.74 | 0.52 | 0.37 | 0.28 | 0.13 | 0.18 | 165. |
| 170. | 1.29 | 0.81 | 0.61 | 0.38 | 0.28 | 0.14 | 0.16 | 170. |
| 175. | 1.34 | 0.86 | 0.65 | 0.40 | 0.28 | 0.15 | 0.14 | 175. |
| 180. | 1.32 | 0.87 | 0.66 | 0.40 | 0.28 | 0.16 | 0.13 | 180. |
| 185. | 1.25 | 0.86 | 0.64 | 0.40 | 0.27 | 0.17 | 0.12 | 185. |
| 190. | 1.14 | 0.82 | 0.59 | 0.38 | 0.26 | 0.16 | 0.09 | 190. |
| 195. | 0.98 | 0.75 | 0.54 | 0.35 | 0.21 | 0.15 | 0.05 | 195. |
| 200. | 0.88 | 0.65 | 0.46 | 0.31 | 0.15 | 0.13 | 0.01 | 200. |
| 205. | 0.62 | 0.53 | 0.33 | 0.24 | 0.10 | 0.09 | -0.01 | 205. |
| 210. | 0.43 | 0.40 | 0.21 | 0.17 | 0.05 | 0.07 | -0.03 | 210. |
| 215. | 0.24 | 0.27 | 0.17 | 0.10 | 0.01 | 0.05 | -0.05 | 215. |
| 220. | 0.07 | 0.14 | 0.12 | 0.04 | -0.02 | 0.04 | -0.06 | 220. |
| 225. | -0.00 | 0.04 | 0.04 | 0.00 | -0.04 | 0.02 | -0.07 | 225. |
| 230. | -0.10 | -0.05 | -0.04 | -0.04 | -0.07 | 0.01 | -0.08 | 230. |
| 235. | -0.20 | -0.13 | -0.06 | -0.08 | -0.09 | 0.00 | -0.08 | 235. |
| 240. | -0.35 | -0.19 | -0.11 | -0.12 | -0.12 | -0.01 | -0.08 | 240. |
| 245. | -0.43 | -0.25 | -0.14 | -0.16 | -0.13 | -0.02 | -0.09 | 245. |
| 250. | -0.50 | -0.30 | -0.17 | -0.18 | -0.14 | -0.03 | -0.09 | 250. |
| 255. | -0.56 | -0.34 | -0.19 | -0.19 | -0.16 | -0.04 | -0.09 | 255. |
| 260. | -0.60 | -0.38 | -0.20 | -0.19 | -0.17 | -0.04 | -0.09 | 260. |
| 265. | -0.62 | -0.41 | -0.21 | -0.19 | -0.18 | -0.04 | -0.09 | 265. |
| 270. | -0.64 | -0.42 | -0.20 | -0.19 | -0.19 | -0.05 | -0.10 | 270. |
| 275. | -0.64 | -0.43 | -0.19 | -0.19 | -0.19 | -0.05 | -0.10 | 275. |
| 280. | -0.65 | -0.43 | -0.19 | -0.19 | -0.18 | -0.05 | -0.10 | 280. |
| 285. | -0.64 | -0.41 | -0.19 | -0.18 | -0.17 | -0.05 | -0.09 | 285. |
| 290. | -0.60 | -0.41 | -0.20 | -0.17 | -0.17 | -0.05 | -0.09 | 290. |
| 295. | -0.70 | -0.44 | -0.22 | -0.18 | -0.16 | -0.05 | -0.10 | 295. |
| 300. | -0.71 | -0.46 | -0.23 | -0.21 | -0.16 | -0.05 | -0.10 | 300. |
| 305. | -0.69 | -0.45 | -0.23 | -0.22 | -0.17 | -0.04 | -0.09 | 305. |
| 310. | -0.66 | -0.44 | -0.23 | -0.21 | -0.18 | -0.04 | -0.09 | 310. |
| 315. | -0.64 | -0.42 | -0.23 | -0.20 | -0.19 | -0.04 | -0.09 | 315. |
| 320. | -0.63 | -0.42 | -0.23 | -0.20 | -0.18 | -0.04 | -0.09 | 320. |
| 325. | -0.64 | -0.40 | -0.24 | -0.20 | -0.18 | -0.04 | -0.09 | 325. |
| 330. | -0.67 | -0.41 | -0.26 | -0.21 | -0.17 | -0.05 | -0.09 | 330. |
| 335. | -0.70 | -0.51 | -0.29 | -0.22 | -0.17 | -0.05 | -0.09 | 335. |
| 340. | -0.71 | -0.49 | -0.29 | -0.22 | -0.18 | -0.06 | -0.10 | 340. |
| 345. | -0.62 | -0.51 | -0.32 | -0.25 | -0.19 | -0.07 | -0.10 | 345. |
| 350. | -0.96 | -0.59 | -0.37 | -0.28 | -0.21 | -0.08 | -0.11 | 350. |
| 355. | -1.39 | -0.72 | -0.46 | -0.31 | -0.22 | -0.08 | -0.11 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=501 CNTR NO. 346 TCN= 23. C.R.= 42.3

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.240 | 1.950 | 2.990 | 4.550 | 7.150 | 10.480 | DEG. |
| 0. | -0.42 | -0.42 | -0.29 | -0.19 | -0.19 | -0.11 | -0.05 | 0. |
| 5. | -0.41 | -0.37 | -0.36 | -0.24 | -0.25 | -0.13 | -0.06 | 5. |
| 10. | -0.40 | -0.45 | -0.45 | -0.27 | -0.25 | -0.14 | -0.06 | 10. |
| 15. | -0.73 | -0.40 | -0.39 | -0.24 | -0.25 | -0.13 | -0.07 | 15. |
| 20. | -0.53 | -0.44 | -0.36 | -0.19 | -0.14 | -0.11 | -0.06 | 20. |
| 25. | -0.41 | -0.34 | -0.25 | -0.18 | -0.09 | -0.11 | -0.07 | 25. |
| 30. | -0.26 | -0.24 | -0.23 | -0.15 | -0.14 | -0.12 | -0.07 | 30. |
| 35. | -0.07 | -0.15 | -0.21 | -0.11 | 0.22 | -0.11 | -0.06 | 35. |
| 40. | 0.09 | -0.07 | -0.15 | -0.11 | 0.26 | -0.11 | -0.06 | 40. |
| 45. | 0.19 | -0.00 | -0.10 | -0.10 | 0.28 | -0.10 | -0.07 | 45. |
| 50. | 0.31 | 0.05 | -0.01 | -0.04 | 0.08 | -0.13 | -0.07 | 50. |
| 55. | 0.36 | 0.10 | 0.04 | 0.01 | 0.11 | -0.13 | -0.07 | 55. |
| 60. | 0.38 | 0.14 | 0.07 | 0.03 | 0.13 | -0.09 | -0.07 | 60. |
| 65. | 0.39 | 0.18 | 0.08 | 0.04 | 0.14 | -0.09 | -0.06 | 65. |
| 70. | 0.39 | 0.21 | 0.08 | 0.05 | 0.15 | -0.08 | -0.06 | 70. |
| 75. | 0.39 | 0.20 | 0.07 | 0.04 | 0.15 | -0.08 | -0.06 | 75. |
| 80. | 0.39 | 0.19 | 0.06 | 0.04 | 0.15 | -0.07 | -0.06 | 80. |
| 85. | 0.39 | 0.18 | 0.06 | 0.03 | 0.15 | -0.06 | -0.05 | 85. |
| 90. | 0.37 | 0.16 | 0.06 | 0.03 | 0.15 | -0.03 | -0.06 | 90. |
| 95. | 0.35 | 0.13 | 0.06 | 0.02 | 0.14 | -0.05 | -0.05 | 95. |
| 100. | 0.33 | 0.10 | 0.08 | 0.02 | 0.14 | -0.07 | -0.05 | 100. |
| 105. | 0.33 | 0.09 | 0.09 | 0.02 | 0.13 | -0.06 | -0.05 | 105. |
| 110. | 0.33 | 0.08 | 0.09 | 0.01 | 0.13 | -0.06 | -0.05 | 110. |
| 115. | 0.31 | 0.09 | 0.06 | 0.01 | 0.13 | -0.03 | -0.05 | 115. |
| 120. | 0.30 | 0.11 | 0.07 | 0.01 | 0.14 | -0.02 | -0.04 | 120. |
| 125. | 0.48 | 0.13 | 0.08 | 0.01 | 0.14 | -0.02 | -0.03 | 125. |
| 130. | 0.46 | 0.15 | 0.10 | 0.02 | 0.14 | -0.01 | -0.01 | 130. |
| 135. | 0.46 | 0.17 | 0.10 | 0.02 | 0.14 | -0.00 | 0.00 | 135. |
| 140. | 0.48 | 0.20 | 0.09 | 0.03 | 0.15 | 0.01 | 0.00 | 140. |
| 145. | 0.50 | 0.23 | 0.11 | 0.04 | 0.15 | 0.02 | 0.01 | 145. |
| 150. | 0.53 | 0.27 | 0.13 | 0.07 | 0.15 | 0.03 | 0.03 | 150. |
| 155. | 0.56 | 0.32 | 0.17 | 0.10 | 0.15 | 0.06 | 0.05 | 155. |
| 160 | 0.60 | 0.38 | 0.21 | 0.14 | 0.16 | 0.08 | 0.04 | 160. |
| 165. | 0.64 | 0.44 | 0.26 | 0.18 | 0.17 | 0.11 | 0.05 | 165. |
| 170. | 0.69 | 0.50 | 0.31 | 0.23 | 0.18 | 0.13 | 0.06 | 170. |
| 175. | 0.74 | 0.55 | 0.35 | 0.27 | 0.19 | 0.14 | 0.07 | 175. |
| 180. | 0.78 | 0.59 | 0.40 | 0.30 | 0.21 | 0.14 | 0.08 | 180. |
| 185. | 0.80 | 0.62 | 0.43 | 0.33 | 0.21 | 0.15 | 0.09 | 185. |
| 190. | 0.78 | 0.62 | 0.44 | 0.33 | 0.21 | 0.16 | 0.09 | 190. |
| 195. | 0.72 | 0.60 | 0.43 | 0.32 | 0.20 | 0.16 | 0.08 | 195. |
| 200. | 0.64 | 0.56 | 0.42 | 0.31 | 0.17 | 0.15 | 0.08 | 200. |
| 205. | 0.54 | 0.51 | 0.39 | 0.29 | 0.14 | 0.14 | 0.08 | 205. |
| 210. | 0.39 | 0.44 | 0.33 | 0.26 | 0.11 | 0.12 | 0.07 | 210. |
| 215. | 0.22 | 0.36 | 0.26 | 0.20 | 0.07 | 0.11 | 0.06 | 215. |
| 220. | 0.09 | 0.27 | 0.19 | 0.15 | 0.04 | 0.10 | 0.06 | 220. |
| 225. | -0.01 | 0.19 | 0.14 | 0.10 | -0.00 | 0.09 | 0.05 | 225. |
| 230. | -0.12 | 0.11 | 0.11 | 0.07 | -0.04 | 0.08 | 0.05 | 230. |
| 235. | -0.24 | 0.04 | 0.09 | 0.04 | -0.07 | 0.07 | 0.06 | 235. |
| 240. | -0.34 | -0.01 | 0.07 | 0.02 | -0.10 | 0.07 | 0.06 | 240. |
| 245. | -0.42 | -0.07 | 0.05 | -0.00 | -0.12 | 0.06 | 0.06 | 245. |
| 250. | -0.49 | -0.11 | 0.02 | -0.02 | -0.13 | 0.06 | 0.05 | 250. |
| 255. | -0.54 | -0.13 | -0.04 | -0.04 | -0.14 | 0.05 | 0.05 | 255. |
| 260. | -0.58 | -0.14 | -0.11 | -0.06 | -0.15 | 0.04 | 0.04 | 260. |
| 265. | -0.62 | -0.16 | -0.16 | -0.07 | -0.16 | 0.03 | 0.02 | 265. |
| 270. | -0.65 | -0.20 | -0.18 | -0.09 | -0.17 | 0.02 | 0.01 | 270. |
| 275. | -0.68 | -0.23 | -0.19 | -0.10 | -0.17 | 0.02 | 0.02 | 275. |
| 280. | -0.70 | -0.27 | -0.19 | -0.11 | -0.18 | 0.02 | 0.02 | 280. |
| 285. | -0.71 | -0.31 | -0.19 | -0.12 | -0.19 | 0.01 | 0.01 | 285. |
| 290. | -0.72 | -0.34 | -0.19 | -0.12 | -0.19 | 0.01 | 0.01 | 290. |
| 295. | -0.72 | -0.37 | -0.20 | -0.13 | -0.20 | 0.00 | 0.01 | 295. |
| 300. | -0.72 | -0.38 | -0.20 | -0.13 | -0.20 | -0.02 | 0.01 | 300. |
| 305. | -0.71 | -0.39 | -0.20 | -0.13 | -0.19 | -0.02 | 0.01 | 305. |
| 310. | -0.70 | -0.39 | -0.20 | -0.14 | -0.19 | -0.02 | 0.01 | 310. |
| 315. | -0.69 | -0.40 | -0.20 | -0.14 | -0.19 | -0.01 | 0.01 | 315. |
| 320. | -0.69 | -0.40 | -0.20 | -0.14 | -0.19 | -0.01 | 0.01 | 320. |
| 325. | -0.69 | -0.40 | -0.21 | -0.14 | -0.18 | -0.01 | 0.01 | 325. |
| 330. | -0.67 | -0.39 | -0.21 | -0.13 | -0.18 | -0.01 | 0.01 | 330. |
| 335. | -0.63 | -0.40 | -0.21 | -0.13 | -0.17 | -0.02 | 0.01 | 335. |
| 340. | -0.57 | -0.39 | -0.20 | -0.12 | -0.16 | -0.03 | 0.00 | 340. |
| 345. | -0.47 | -0.31 | -0.17 | -0.09 | -0.14 | -0.02 | -0.01 | 345. |
| 350. | -0.40 | -0.23 | -0.12 | -0.08 | -0.13 | -0.02 | -0.01 | 350. |
| 355. | -0.36 | -0.17 | -0.25 | -0.16 | -0.16 | -0.05 | -0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=501 CNTR NO. 346 TCN= 23. C.R.= 42.9

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.190 | 10.400 | DEG. |
| 0. | -0.36 | -0.25 | -0.27 | -0.21 | -0.11 | -0.30 | -0.01 | 0. |
| 5. | -0.40 | -0.25 | -0.28 | -0.20 | -0.12 | -0.36 | -0.01 | 5. |
| 10. | -0.36 | -0.23 | -0.24 | -0.19 | -0.09 | -0.06 | -0.01 | 10. |
| 15. | -0.29 | -0.27 | -0.23 | -0.18 | -0.08 | -0.37 | -0.01 | 15. |
| 20. | -0.29 | -0.30 | -0.26 | -0.19 | -0.09 | -0.10 | -0.02 | 20. |
| 25. | -0.16 | -0.23 | -0.21 | -0.16 | -0.07 | -0.37 | -0.01 | 25. |
| 30. | 0.05 | -0.09 | -0.16 | -0.11 | -0.05 | -0.06 | -0.01 | 30. |
| 35. | 0.27 | 0.05 | -0.07 | -0.04 | -0.04 | -0.04 | -0.03 | 35. |
| 40. | 0.42 | 0.20 | 0.03 | 0.04 | 0.00 | -0.37 | -0.02 | 40. |
| 45. | 0.54 | 0.33 | 0.12 | 0.12 | 0.06 | -0.05 | -0.01 | 45. |
| 50. | 0.68 | 0.44 | 0.19 | 0.18 | 0.09 | -0.04 | -0.02 | 50. |
| 55. | 0.76 | 0.52 | 0.23 | 0.24 | 0.12 | -0.03 | -0.02 | 55. |
| 60. | 0.78 | 0.58 | 0.25 | 0.29 | 0.14 | -0.02 | -0.01 | 60. |
| 65. | 0.78 | 0.62 | 0.26 | 0.34 | 0.15 | -0.01 | -0.01 | 65. |
| 70. | 0.76 | 0.62 | 0.25 | 0.38 | 0.18 | -0.01 | -0.02 | 70. |
| 75. | 0.71 | 0.60 | 0.24 | 0.40 | 0.24 | -0.03 | -0.02 | 75. |
| 80. | 0.59 | 0.56 | 0.22 | 0.45 | 0.27 | -0.01 | -0.02 | 80. |
| 85. | 0.44 | 0.49 | 0.18 | 0.38 | 0.28 | -0.06 | -0.03 | 85. |
| 90. | 0.31 | 0.40 | 0.14 | 0.36 | 0.19 | -0.09 | -0.03 | 90. |
| 95. | 0.19 | 0.35 | 0.09 | 0.33 | 0.17 | -0.12 | -0.03 | 95. |
| 100. | 0.09 | 0.32 | 0.04 | 0.29 | 0.15 | -0.13 | -0.03 | 100. |
| 105. | 0.00 | 0.30 | -0.04 | 0.25 | 0.12 | -0.13 | -0.04 | 105. |
| 110. | -0.06 | 0.27 | -0.12 | 0.21 | 0.10 | -0.12 | -0.04 | 110. |
| 115. | -0.12 | 0.26 | -0.19 | 0.19 | 0.08 | -0.11 | -0.04 | 115. |
| 120. | -0.21 | 0.25 | -0.22 | 0.17 | 0.06 | -0.12 | -0.03 | 120. |
| 125. | -0.31 | 0.23 | -0.24 | 0.13 | 0.02 | -0.14 | -0.04 | 125. |
| 130. | -0.42 | 0.16 | -0.27 | 0.07 | -0.02 | -0.15 | -0.05 | 130. |
| 135. | -0.51 | -0.01 | -0.34 | -0.00 | -0.05 | -0.16 | -0.00 | 135. |
| 140. | -0.62 | -0.18 | -0.40 | -0.05 | -0.06 | -0.16 | -0.07 | 140. |
| 145. | -0.66 | -0.22 | -0.39 | -0.08 | -0.06 | -0.15 | -0.06 | 145. |
| 150. | -0.67 | -0.21 | -0.39 | -0.09 | -0.05 | -0.13 | -0.04 | 150. |
| 155. | -0.61 | -0.20 | -0.36 | -0.08 | -0.04 | -0.14 | -0.03 | 155. |
| 160. | -0.50 | -0.16 | -0.31 | -0.05 | -0.01 | -0.08 | -0.03 | 160. |
| 165. | -0.36 | -0.12 | -0.23 | -0.01 | -0.01 | -0.06 | -0.02 | 165. |
| 170. | -0.17 | -0.07 | -0.14 | 0.02 | 0.01 | -0.03 | -0.02 | 170. |
| 175. | -0.06 | -0.03 | -0.02 | 0.06 | 0.04 | 0.02 | -0.01 | 175. |
| 180. | 0.14 | 0.01 | 0.09 | 0.10 | 0.10 | 0.05 | -0.00 | 180. |
| 185. | 0.24 | 0.03 | 0.16 | 0.13 | 0.14 | 0.06 | 0.00 | 185. |
| 190. | 0.32 | 0.05 | 0.20 | 0.16 | 0.14 | 0.07 | 0.01 | 190. |
| 195. | 0.35 | 0.06 | 0.22 | 0.17 | 0.13 | 0.08 | 0.01 | 195. |
| 200. | 0.35 | 0.07 | 0.23 | 0.17 | 0.10 | 0.09 | 0.02 | 200. |
| 205. | 0.32 | 0.07 | 0.23 | 0.14 | 0.08 | 0.10 | 0.03 | 205. |
| 210. | 0.28 | 0.06 | 0.23 | 0.11 | 0.04 | 0.10 | 0.03 | 210. |
| 215. | 0.24 | 0.04 | 0.21 | 0.08 | 0.01 | 0.09 | 0.02 | 215. |
| 220. | 0.19 | 0.01 | 0.20 | 0.05 | 0.01 | 0.09 | 0.02 | 220. |
| 225. | 0.13 | -0.03 | 0.18 | 0.02 | -0.01 | 0.09 | 0.03 | 225. |
| 230. | 0.08 | -0.06 | 0.15 | -0.03 | -0.03 | 0.08 | 0.03 | 230. |
| 235. | -0.01 | -0.10 | 0.12 | -0.00 | -0.04 | 0.09 | 0.03 | 235. |
| 240. | -0.06 | -0.13 | 0.10 | -0.12 | -0.05 | 0.09 | 0.03 | 240. |
| 245. | -0.09 | -0.16 | 0.13 | -0.14 | -0.05 | 0.10 | 0.03 | 245. |
| 250. | -0.10 | -0.18 | 0.11 | -0.15 | -0.06 | 0.09 | 0.04 | 250. |
| 255. | -0.09 | -0.17 | 0.11 | -0.16 | -0.06 | 0.10 | 0.04 | 255. |
| 260. | -0.07 | -0.17 | 0.12 | -0.18 | -0.06 | 0.10 | 0.04 | 260. |
| 265. | -0.06 | -0.16 | 0.13 | -0.19 | -0.07 | 0.11 | 0.04 | 265. |
| 270. | -0.05 | -0.15 | 0.13 | -0.17 | -0.07 | 0.10 | 0.04 | 270. |
| 275. | -0.06 | -0.15 | 0.13 | -0.15 | -0.08 | 0.10 | 0.04 | 275. |
| 280. | -0.08 | -0.15 | 0.13 | -0.14 | -0.09 | 0.10 | 0.04 | 280. |
| 285. | -0.09 | -0.17 | 0.13 | -0.15 | -0.09 | 0.10 | 0.04 | 285. |
| 290. | -0.10 | -0.19 | 0.12 | -0.16 | -0.10 | 0.10 | 0.04 | 290. |
| 295. | -0.10 | -0.21 | 0.10 | -0.17 | -0.10 | 0.09 | 0.04 | 295. |
| 300. | -0.10 | -0.21 | 0.09 | -0.18 | -0.10 | 0.09 | 0.04 | 300. |
| 305. | -0.10 | -0.20 | 0.08 | -0.18 | -0.10 | 0.09 | 0.04 | 305. |
| 310. | -0.10 | -0.19 | 0.08 | -0.18 | -0.10 | 0.09 | 0.04 | 310. |
| 315. | -0.10 | -0.20 | 0.07 | -0.17 | -0.09 | 0.09 | 0.04 | 315. |
| 320. | -0.10 | -0.22 | 0.05 | -0.17 | -0.09 | 0.08 | 0.04 | 320. |
| 325. | -0.13 | -0.25 | 0.02 | -0.17 | -0.09 | 0.07 | 0.04 | 325. |
| 330. | -0.19 | -0.27 | -0.07 | -0.20 | -0.09 | 0.06 | 0.04 | 330. |
| 335. | -0.25 | -0.29 | -0.15 | -0.23 | -0.10 | 0.04 | 0.05 | 335. |
| 340. | -0.29 | -0.32 | -0.19 | -0.24 | -0.11 | 0.02 | 0.02 | 340. |
| 345. | -0.28 | -0.31 | -0.20 | -0.24 | -0.14 | -0.03 | 0.01 | 345. |
| 350. | -0.23 | -0.27 | -0.16 | -0.21 | -0.12 | -0.00 | 0.03 | 350. |
| 355. | -0.15 | -0.18 | -0.13 | -0.14 | -0.08 | -0.02 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=501 CNTR NO. 346 TC= 23. C.R.= 42.3

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.344 | 1.953 | 2.997 | 4.550 | 7.153 | 10.430 | DEG. |
| 0. | 0.18 | 0.20 | 0.18 | 0.12 | 0.06 | -0.33 | 0.01 | 0. |
| 5. | -0.19 | -0.11 | 0.03 | 0.09 | 0.01 | -0.31 | 0.01 | 5. |
| 10. | -0.04 | 0.08 | 0.12 | 0.08 | 0.03 | -0.34 | 0.00 | 10. |
| 15. | -0.10 | 0.09 | 0.09 | 0.08 | 0.01 | -0.35 | -0.00 | 15. |
| 20. | -0.04 | 0.07 | 0.07 | 0.07 | 0.01 | -0.34 | -0.01 | 20. |
| 25. | 0.22 | 0.27 | 0.27 | 0.06 | 0.01 | -0.33 | 0.00 | 25. |
| 30. | 0.32 | 0.10 | 0.18 | 0.05 | 0.01 | -0.33 | 0.00 | 30. |
| 35. | 0.47 | 0.17 | 0.11 | 0.05 | 0.02 | -0.32 | 0.00 | 35. |
| 40. | 0.58 | 0.28 | 0.15 | 0.06 | 0.04 | -0.32 | 0.01 | 40. |
| 45. | 0.65 | 0.42 | 0.22 | 0.08 | 0.06 | -0.03 | 0.02 | 45. |
| 50. | 0.72 | 0.51 | 0.30 | 0.11 | 0.08 | 0.17 | 0.03 | 50. |
| 55. | 0.84 | 0.57 | 0.38 | 0.13 | 0.10 | 0.38 | 0.03 | 55. |
| 60. | 0.95 | 0.59 | 0.42 | 0.15 | 0.11 | 0.39 | 0.03 | 60. |
| 65. | 1.01 | 0.60 | 0.44 | 0.16 | 0.11 | 0.39 | 0.03 | 65. |
| 70. | 1.09 | 0.57 | 0.43 | 0.15 | 0.11 | 0.38 | 0.03 | 70. |
| 75. | 0.93 | 0.64 | 0.40 | 0.12 | 0.09 | 0.35 | 0.02 | 75. |
| 80. | 0.81 | 0.74 | 0.34 | 0.10 | 0.07 | 0.31 | 0.02 | 80. |
| 85. | 0.62 | 0.67 | 0.29 | 0.06 | 0.02 | -0.02 | 0.01 | 85. |
| 90. | 0.36 | -0.07 | 0.14 | 0.02 | -0.03 | -0.04 | 0.01 | 90. |
| 95. | 0.07 | -0.23 | -0.12 | -0.07 | -0.08 | -0.08 | 0.01 | 95. |
| 100. | -0.23 | -0.42 | -0.29 | -0.18 | -0.16 | -0.11 | 0.01 | 100. |
| 105. | -0.50 | -0.66 | -0.47 | -0.29 | -0.26 | -0.14 | 0.00 | 105. |
| 110. | -0.75 | -0.98 | -0.63 | -0.38 | -0.35 | -0.16 | -0.01 | 110. |
| 115. | -0.99 | -1.21 | -0.77 | -0.44 | -0.42 | -0.15 | -0.03 | 115. |
| 120. | -1.19 | -1.36 | -0.89 | -0.50 | -0.44 | -0.13 | -0.04 | 120. |
| 125. | -1.31 | -1.43 | -0.98 | -0.55 | -0.44 | -0.10 | -0.05 | 125. |
| 130. | -1.37 | -1.46 | -1.03 | -0.58 | -0.45 | -0.09 | -0.05 | 130. |
| 135. | -1.39 | -1.49 | -1.05 | -0.60 | -0.46 | -0.21 | -0.05 | 135. |
| 140. | -1.40 | -1.50 | -1.04 | -0.60 | -0.47 | -0.21 | -0.04 | 140. |
| 145. | -1.41 | -1.44 | -1.03 | -0.59 | -0.46 | -0.20 | -0.04 | 145. |
| 150. | -1.39 | -1.28 | -0.92 | -0.57 | -0.45 | -0.18 | -0.04 | 150. |
| 155. | -1.31 | -1.07 | -0.82 | -0.54 | -0.42 | -0.15 | -0.04 | 155. |
| 160. | -1.15 | -0.96 | -0.72 | -0.50 | -0.38 | -0.12 | -0.04 | 160. |
| 165. | -0.98 | -0.76 | -0.62 | -0.46 | -0.32 | -0.13 | -0.03 | 165. |
| 170. | -0.82 | -0.62 | -0.52 | -0.40 | -0.26 | -0.07 | -0.03 | 170. |
| 175. | -0.65 | -0.48 | -0.39 | -0.33 | -0.19 | -0.06 | -0.02 | 175. |
| 180. | -0.47 | -0.34 | -0.26 | -0.26 | -0.11 | -0.12 | -0.02 | 180. |
| 185. | -0.29 | -0.19 | -0.14 | -0.19 | -0.04 | -0.03 | -0.01 | 185. |
| 190. | -0.14 | -0.04 | -0.04 | -0.13 | 0.01 | 0.01 | -0.01 | 190. |
| 195. | -0.01 | 0.07 | 0.03 | -0.07 | 0.04 | 0.05 | -0.00 | 195. |
| 200. | 0.08 | 0.13 | 0.09 | -0.03 | 0.05 | 0.05 | -0.00 | 200. |
| 205. | 0.13 | 0.17 | 0.15 | 0.01 | 0.07 | 0.05 | -0.00 | 205. |
| 210. | 0.13 | 0.23 | 0.21 | 0.03 | 0.08 | 0.05 | 0.00 | 210. |
| 215. | 0.12 | 0.27 | 0.25 | 0.05 | 0.09 | 0.05 | 0.00 | 215. |
| 220. | 0.09 | 0.29 | 0.27 | 0.06 | 0.09 | 0.05 | -0.00 | 220. |
| 225. | 0.06 | 0.28 | 0.27 | 0.07 | 0.09 | 0.05 | -0.00 | 225. |
| 230. | 0.05 | 0.27 | 0.19 | 0.09 | 0.10 | 0.06 | -0.01 | 230. |
| 235. | 0.05 | 0.25 | 0.08 | 0.10 | 0.10 | 0.06 | -0.01 | 235. |
| 240. | 0.03 | 0.24 | 0.00 | 0.11 | 0.10 | 0.06 | -0.00 | 240. |
| 245. | 0.04 | 0.26 | -0.12 | 0.13 | 0.11 | 0.05 | -0.00 | 245. |
| 250. | 0.07 | 0.34 | 0.04 | 0.14 | 0.12 | 0.05 | 0.00 | 250. |
| 255. | 0.13 | 0.41 | 0.24 | 0.15 | 0.14 | 0.06 | 0.01 | 255. |
| 260. | 0.20 | 0.46 | 0.43 | 0.17 | 0.16 | 0.07 | 0.01 | 260. |
| 265. | 0.28 | 0.49 | 0.48 | 0.19 | 0.17 | 0.08 | 0.01 | 265. |
| 270. | 0.34 | 0.53 | 0.46 | 0.21 | 0.19 | 0.09 | 0.01 | 270. |
| 275. | 0.38 | 0.57 | 0.46 | 0.22 | 0.19 | 0.10 | 0.01 | 275. |
| 280. | 0.39 | 0.60 | 0.45 | 0.24 | 0.21 | 0.11 | 0.01 | 280. |
| 285. | 0.39 | 0.59 | 0.44 | 0.25 | 0.23 | 0.13 | 0.01 | 285. |
| 290. | 0.37 | 0.56 | 0.42 | 0.26 | 0.23 | 0.13 | 0.01 | 290. |
| 295. | 0.35 | 0.53 | 0.40 | 0.27 | 0.23 | 0.13 | 0.01 | 295. |
| 300. | 0.34 | 0.52 | 0.38 | 0.27 | 0.22 | 0.13 | 0.01 | 300. |
| 305. | 0.35 | 0.50 | 0.38 | 0.27 | 0.22 | 0.13 | 0.01 | 305. |
| 310. | 0.37 | 0.49 | 0.38 | 0.27 | 0.22 | 0.13 | 0.01 | 310. |
| 315. | 0.39 | 0.49 | 0.37 | 0.26 | 0.22 | 0.13 | 0.01 | 315. |
| 320. | 0.41 | 0.48 | 0.36 | 0.26 | 0.22 | 0.13 | 0.01 | 320. |
| 325. | 0.41 | 0.47 | 0.33 | 0.25 | 0.22 | 0.13 | 0.01 | 325. |
| 330. | 0.41 | 0.45 | 0.29 | 0.25 | 0.21 | 0.13 | 0.01 | 330. |
| 335. | 0.38 | 0.43 | 0.25 | 0.25 | 0.20 | 0.12 | 0.01 | 335. |
| 340. | 0.35 | 0.43 | 0.21 | 0.25 | 0.19 | 0.11 | 0.02 | 340. |
| 345. | 0.34 | 0.41 | 0.17 | 0.24 | 0.19 | 0.10 | 0.02 | 345. |
| 350. | 0.34 | 0.37 | 0.15 | 0.25 | 0.18 | 0.10 | 0.02 | 350. |
| 355. | 0.64 | 0.48 | 0.15 | 0.07 | 0.16 | 0.09 | 0.01 | 355. |

TEXT NOT REPRODUCIBLE

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=901 CNTR NO. 346 YCN= 23. Q.R.= 42.9

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.362 | 1.959 | 2.990 | 4.552 | 7.157 | 13.402 | DEG. |
| 0. | 0.20 | 0.15 | 0.15 | 0.18 | 0.08 | 0.33 | 0.02 | 0. |
| 5. | 0.24 | 0.19 | 0.18 | 0.21 | 0.08 | 0.36 | 0.03 | 5. |
| 10. | 0.19 | 0.14 | 0.15 | 0.15 | 0.12 | 0.31 | 0.02 | 10. |
| 15. | 0.14 | 0.13 | 0.12 | 0.12 | 0.17 | 0.27 | 0.01 | 15. |
| 20. | 0.16 | 0.14 | 0.13 | 0.12 | 0.21 | -0.13 | 0.02 | 20. |
| 25. | 0.23 | 0.16 | 0.13 | 0.13 | 0.22 | -0.31 | 0.01 | 25. |
| 30. | 0.32 | 0.20 | 0.12 | 0.13 | 0.22 | -0.32 | -0.00 | 30. |
| 35. | 0.44 | 0.25 | 0.16 | 0.12 | 0.24 | -0.32 | 0.01 | 35. |
| 40. | 0.59 | 0.31 | 0.22 | 0.13 | 0.25 | -0.31 | 0.01 | 40. |
| 45. | 0.75 | 0.39 | 0.29 | 0.19 | 0.27 | 0.32 | 0.01 | 45. |
| 50. | 0.92 | 0.50 | 0.39 | 0.25 | 0.03 | 0.35 | 0.02 | 50. |
| 55. | 1.10 | 0.67 | 0.47 | 0.28 | 0.44 | 0.35 | 0.02 | 55. |
| 60. | 1.22 | 0.75 | 0.56 | 0.29 | 0.48 | 0.36 | 0.02 | 60. |
| 65. | 1.01 | 0.71 | 0.57 | 0.29 | 0.57 | 0.33 | 0.02 | 65. |
| 70. | 0.99 | 0.65 | 0.54 | 0.26 | 0.50 | 0.32 | 0.00 | 70. |
| 75. | 0.85 | 0.56 | 0.49 | 0.23 | 0.56 | -0.33 | -0.02 | 75. |
| 80. | 0.55 | 0.44 | 0.42 | 0.14 | 0.21 | -0.35 | -0.03 | 80. |
| 85. | 0.30 | 0.30 | 0.29 | 0.01 | 0.17 | -0.13 | -0.04 | 85. |
| 90. | 0.30 | 0.19 | 0.09 | -0.20 | 0.15 | -0.14 | -0.05 | 90. |
| 95. | -0.51 | -0.26 | -0.19 | -0.19 | 0.09 | -0.21 | -0.07 | 95. |
| 100. | -0.87 | -0.45 | -0.57 | -0.52 | 0.06 | -0.24 | -0.07 | 100. |
| 105. | -1.22 | -0.96 | -0.87 | -0.83 | 0.04 | -0.26 | -0.07 | 105. |
| 110. | -1.55 | -1.22 | -0.96 | -0.74 | -0.03 | -0.27 | -0.08 | 110. |
| 115. | -1.64 | -1.38 | -1.42 | -0.83 | -0.11 | -0.28 | -0.09 | 115. |
| 120. | -1.78 | -1.50 | -1.11 | -0.90 | -0.16 | -0.29 | -0.09 | 120. |
| 125. | -1.87 | -1.57 | -1.17 | -0.94 | -0.20 | -0.29 | -0.09 | 125. |
| 130. | -1.94 | -1.60 | -1.22 | -1.05 | -0.24 | -0.29 | -0.09 | 130. |
| 135. | -1.98 | -1.61 | -1.19 | -0.95 | -0.28 | -0.29 | -0.09 | 135. |
| 140. | -1.99 | -1.60 | -1.17 | -0.93 | -0.31 | -0.28 | -0.08 | 140. |
| 145. | -1.96 | -1.55 | -1.12 | -0.90 | -0.33 | -0.27 | -0.08 | 145. |
| 150. | -1.88 | -1.46 | -1.07 | -0.86 | -0.34 | -0.25 | -0.08 | 150. |
| 155. | -1.75 | -1.33 | -1.01 | -0.81 | -0.33 | -0.24 | -0.07 | 155. |
| 160. | -1.58 | -1.18 | -0.95 | -0.74 | -0.32 | -0.22 | -0.06 | 160. |
| 165. | -1.37 | -1.03 | -0.86 | -0.65 | -0.29 | -0.19 | -0.06 | 165. |
| 170. | -1.15 | -0.89 | -0.75 | -0.55 | -0.26 | -0.16 | -0.05 | 170. |
| 175. | -0.94 | -0.74 | -0.61 | -0.44 | -0.22 | -0.12 | -0.02 | 175. |
| 180. | -0.74 | -0.64 | -0.46 | -0.32 | -0.19 | -0.09 | -0.01 | 180. |
| 185. | -0.54 | -0.46 | -0.33 | -0.21 | -0.15 | -0.06 | -0.01 | 185. |
| 190. | -0.35 | -0.33 | -0.22 | -0.13 | -0.13 | -0.03 | 0.00 | 190. |
| 195. | -0.18 | -0.21 | -0.12 | -0.06 | -0.11 | -0.01 | 0.01 | 195. |
| 200. | -0.06 | -0.10 | -0.05 | -0.01 | -0.13 | 0.03 | 0.01 | 200. |
| 205. | 0.02 | 0.01 | 0.01 | 0.04 | -0.09 | 0.06 | 0.01 | 205. |
| 210. | 0.07 | 0.11 | 0.06 | 0.09 | -0.07 | 0.09 | 0.01 | 210. |
| 215. | 0.11 | 0.15 | 0.10 | 0.12 | -0.06 | 0.10 | 0.01 | 215. |
| 220. | 0.13 | 0.18 | 0.13 | 0.12 | -0.05 | 0.06 | 0.01 | 220. |
| 225. | 0.14 | 0.19 | 0.15 | 0.13 | -0.06 | 0.06 | 0.01 | 225. |
| 230. | 0.14 | 0.22 | 0.17 | 0.13 | -0.08 | 0.07 | 0.01 | 230. |
| 235. | 0.14 | 0.24 | 0.18 | 0.14 | -0.11 | 0.08 | 0.02 | 235. |
| 240. | 0.17 | 0.25 | 0.19 | 0.20 | -0.13 | 0.08 | 0.02 | 240. |
| 245. | 0.22 | 0.25 | 0.22 | 0.23 | -0.14 | 0.09 | 0.03 | 245. |
| 250. | 0.26 | 0.26 | 0.25 | 0.26 | -0.14 | 0.11 | 0.03 | 250. |
| 255. | 0.32 | 0.29 | 0.26 | 0.28 | -0.14 | 0.11 | 0.04 | 255. |
| 260. | 0.40 | 0.36 | 0.33 | 0.29 | -0.13 | 0.16 | 0.04 | 260. |
| 265. | 0.51 | 0.48 | 0.37 | 0.32 | -0.12 | 0.17 | 0.04 | 265. |
| 270. | 0.65 | 0.60 | 0.41 | 0.38 | -0.11 | 0.19 | 0.04 | 270. |
| 275. | 0.79 | 0.69 | 0.46 | 0.47 | -0.07 | 0.19 | 0.04 | 275. |
| 280. | 0.92 | 0.75 | 0.50 | 0.50 | -0.04 | 0.19 | 0.04 | 280. |
| 285. | 0.99 | 0.78 | 0.53 | 0.49 | -0.02 | 0.19 | 0.04 | 285. |
| 290. | 0.93 | 0.79 | 0.54 | 0.47 | -0.01 | 0.19 | 0.04 | 290. |
| 295. | 0.87 | 0.77 | 0.54 | 0.46 | -0.02 | 0.19 | 0.04 | 295. |
| 300. | 0.85 | 0.73 | 0.52 | 0.45 | -0.02 | 0.19 | 0.04 | 300. |
| 305. | 0.85 | 0.72 | 0.51 | 0.46 | -0.03 | 0.19 | 0.04 | 305. |
| 310. | 0.85 | 0.69 | 0.51 | 0.46 | -0.02 | 0.18 | 0.04 | 310. |
| 315. | 0.85 | 0.69 | 0.51 | 0.45 | -0.02 | 0.19 | 0.04 | 315. |
| 320. | 0.86 | 0.68 | 0.51 | 0.46 | -0.01 | 0.19 | 0.05 | 320. |
| 325. | 0.86 | 0.68 | 0.51 | 0.44 | -0.01 | 0.18 | 0.05 | 325. |
| 330. | 0.87 | 0.68 | 0.51 | 0.46 | -0.01 | 0.19 | 0.06 | 330. |
| 335. | 0.88 | 0.68 | 0.53 | 0.45 | 0.00 | 0.18 | 0.06 | 335. |
| 340. | 0.93 | 0.76 | 0.54 | 0.45 | 0.03 | 0.14 | 0.06 | 340. |
| 345. | 1.02 | 0.84 | 0.54 | 0.46 | 0.07 | 0.17 | 0.06 | 345. |
| 350. | 0.93 | 0.73 | 0.52 | 0.45 | 0.09 | 0.16 | 0.06 | 350. |
| 355. | 0.46 | 0.31 | 0.47 | 0.33 | 0.09 | 0.19 | 0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=501 CNTR NO. 346 TCN= 23. C.R.= 42.3

DIFFERENTIAL PRESSURE

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.948 | 1.957 | 2.995 | 4.553 | 7.152 | 13.430 | DEG. |
| 0. | 0.02 | 0.27 | 0.17 | 0.11 | 0.07 | 0.07 | -0.02 | 0. |
| 5. | 0.53 | 0.43 | 0.32 | 0.17 | 0.15 | 0.15 | -0.01 | 5. |
| 10. | 0.35 | 0.24 | 0.19 | 0.13 | 0.08 | 0.05 | -0.03 | 10. |
| 15. | 0.20 | 0.22 | 0.14 | 0.08 | 0.05 | 0.02 | -0.04 | 15. |
| 20. | 0.28 | 0.27 | 0.14 | 0.08 | 0.05 | -0.01 | -0.04 | 20. |
| 25. | 0.25 | 0.28 | 0.16 | 0.07 | 0.05 | -0.04 | -0.04 | 25. |
| 30. | 0.34 | 0.30 | 0.17 | 0.05 | 0.06 | -0.05 | -0.05 | 30. |
| 35. | 0.44 | 0.33 | 0.23 | 0.17 | 0.07 | -0.07 | -0.05 | 35. |
| 40. | 0.50 | 0.35 | 0.26 | 0.11 | 0.09 | -0.06 | -0.05 | 40. |
| 45. | 0.58 | 0.41 | 0.33 | 0.16 | 0.12 | -0.06 | -0.05 | 45. |
| 50. | 0.78 | 0.91 | 0.41 | 0.21 | 0.16 | -0.06 | -0.05 | 50. |
| 55. | 0.87 | 0.67 | 0.53 | 0.25 | 0.19 | -0.07 | -0.05 | 55. |
| 60. | 0.99 | 0.75 | 0.61 | 0.28 | 0.21 | -0.09 | -0.05 | 60. |
| 65. | 0.98 | 0.75 | 0.60 | 0.28 | 0.22 | -0.11 | -0.05 | 65. |
| 70. | 0.88 | 0.72 | 0.52 | 0.27 | 0.23 | -0.14 | -0.06 | 70. |
| 75. | 0.76 | 0.63 | 0.38 | 0.22 | 0.22 | -0.17 | -0.08 | 75. |
| 80. | 0.43 | 0.30 | 0.18 | 0.09 | 0.17 | -0.21 | -0.09 | 80. |
| 85. | 0.27 | 0.25 | -0.09 | -0.07 | 0.08 | -0.25 | -0.10 | 85. |
| 90. | -0.40 | -0.22 | -0.38 | -0.22 | -0.03 | -0.26 | -0.10 | 90. |
| 95. | -0.93 | -0.68 | -0.83 | -0.36 | -0.11 | -0.29 | -0.09 | 95. |
| 100. | -1.36 | -0.80 | -0.95 | -0.39 | -0.18 | -0.30 | -0.08 | 100. |
| 105. | -1.56 | -1.04 | -1.08 | -0.42 | -0.24 | -0.31 | -0.09 | 105. |
| 110. | -1.77 | -1.33 | -1.14 | -0.43 | -0.28 | -0.31 | -0.10 | 110. |
| 115. | -1.95 | -1.52 | -1.17 | -0.42 | -0.32 | -0.32 | -0.09 | 115. |
| 120. | -2.10 | -1.59 | -1.23 | -0.37 | -0.34 | -0.33 | -0.09 | 120. |
| 125. | -2.24 | -1.58 | -1.22 | -0.36 | -0.36 | -0.34 | -0.08 | 125. |
| 130. | -2.31 | -1.58 | -1.22 | -0.34 | -0.37 | -0.35 | -0.07 | 130. |
| 135. | -2.25 | -1.58 | -1.18 | -0.29 | -0.37 | -0.36 | -0.06 | 135. |
| 140. | -2.19 | -1.37 | -1.14 | -0.07 | -0.38 | -0.36 | -0.05 | 140. |
| 145. | -2.16 | -1.55 | -1.23 | -0.04 | -0.37 | -0.32 | -0.05 | 145. |
| 150. | -2.12 | -1.58 | -1.23 | -0.05 | -0.36 | -0.29 | -0.06 | 150. |
| 155. | -2.01 | -1.42 | -1.15 | -0.75 | -0.36 | -0.27 | -0.06 | 155. |
| 160. | -1.77 | -1.27 | -1.05 | -0.69 | -0.35 | -0.24 | -0.06 | 160. |
| 165. | -1.52 | -1.08 | -0.87 | -0.62 | -0.33 | -0.21 | -0.05 | 165. |
| 170. | -1.34 | -0.91 | -0.69 | -0.54 | -0.31 | -0.15 | -0.04 | 170. |
| 175. | -1.17 | -0.83 | -0.55 | -0.45 | -0.29 | -0.10 | -0.02 | 175. |
| 180. | -0.99 | -0.75 | -0.38 | -0.37 | -0.25 | -0.03 | -0.00 | 180. |
| 185. | -0.73 | -0.63 | -0.28 | -0.27 | -0.22 | -0.03 | 0.01 | 185. |
| 190. | -0.47 | -0.41 | -0.19 | -0.18 | -0.18 | 0.02 | 0.02 | 190. |
| 195. | -0.25 | -0.19 | -0.12 | -0.11 | -0.13 | 0.03 | 0.03 | 195. |
| 200. | -0.16 | -0.02 | -0.03 | -0.04 | -0.08 | 0.03 | 0.04 | 200. |
| 205. | -0.10 | 0.11 | 0.04 | -0.01 | -0.03 | 0.04 | 0.04 | 205. |
| 210. | -0.04 | 0.17 | 0.13 | 0.01 | 0.01 | 0.06 | 0.04 | 210. |
| 215. | 0.05 | 0.19 | 0.19 | 0.03 | 0.04 | 0.08 | 0.05 | 215. |
| 220. | 0.10 | 0.18 | 0.16 | 0.05 | 0.04 | 0.09 | 0.05 | 220. |
| 225. | 0.12 | 0.17 | 0.15 | 0.04 | 0.05 | 0.11 | 0.05 | 225. |
| 230. | 0.12 | 0.17 | 0.15 | 0.10 | 0.05 | 0.11 | 0.05 | 230. |
| 235. | 0.14 | 0.19 | 0.17 | 0.13 | 0.05 | 0.15 | 0.07 | 235. |
| 240. | 0.21 | 0.22 | 0.23 | 0.16 | 0.06 | 0.16 | 0.07 | 240. |
| 245. | 0.31 | 0.26 | 0.30 | 0.18 | 0.07 | 0.19 | 0.08 | 245. |
| 250. | 0.39 | 0.31 | 0.37 | 0.21 | 0.09 | 0.19 | 0.09 | 250. |
| 255. | 0.44 | 0.36 | 0.44 | 0.24 | 0.11 | 0.21 | 0.09 | 255. |
| 260. | 0.57 | 0.42 | 0.48 | 0.29 | 0.13 | 0.24 | 0.10 | 260. |
| 265. | 0.81 | 0.46 | 0.52 | 0.35 | 0.15 | 0.24 | 0.10 | 265. |
| 270. | 1.03 | 0.50 | 0.55 | 0.41 | 0.16 | 0.26 | 0.10 | 270. |
| 275. | 1.09 | 0.56 | 0.57 | 0.49 | 0.16 | 0.27 | 0.09 | 275. |
| 280. | 1.18 | 0.65 | 0.59 | 0.54 | 0.16 | 0.28 | 0.09 | 280. |
| 285. | 1.27 | 0.74 | 0.61 | 0.59 | 0.18 | 0.29 | 0.09 | 285. |
| 290. | 1.33 | 0.80 | 0.61 | 0.57 | 0.19 | 0.28 | 0.08 | 290. |
| 295. | 1.29 | 0.80 | 0.62 | 0.54 | 0.18 | 0.29 | 0.08 | 295. |
| 300. | 1.23 | 0.78 | 0.61 | 0.52 | 0.16 | 0.27 | 0.07 | 300. |
| 305. | 1.17 | 0.75 | 0.61 | 0.51 | 0.16 | 0.26 | 0.07 | 305. |
| 310. | 1.15 | 0.74 | 0.60 | 0.50 | 0.16 | 0.25 | 0.07 | 310. |
| 315. | 1.15 | 0.73 | 0.59 | 0.50 | 0.17 | 0.24 | 0.06 | 315. |
| 320. | 1.16 | 0.72 | 0.59 | 0.50 | 0.19 | 0.24 | 0.06 | 320. |
| 325. | 1.17 | 0.73 | 0.59 | 0.50 | 0.20 | 0.24 | 0.06 | 325. |
| 330. | 1.18 | 0.74 | 0.58 | 0.53 | 0.20 | 0.24 | 0.06 | 330. |
| 335. | 1.23 | 0.76 | 0.60 | 0.58 | 0.20 | 0.23 | 0.05 | 335. |
| 340. | 1.20 | 0.78 | 0.62 | 0.62 | 0.19 | 0.24 | 0.05 | 340. |
| 345. | 1.39 | 0.90 | 0.62 | 0.59 | 0.20 | 0.24 | 0.06 | 345. |
| 350. | 1.47 | 0.86 | 0.77 | 0.62 | 0.19 | 0.18 | 0.04 | 350. |
| 355. | 0.00 | 0.58 | 0.41 | 0.11 | 0.18 | 0.13 | -0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 184 TC= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

SPAN STATION 92.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.[illegible] | 4.550 | 10.400 | DEG. |
| 0. | -1.18 | -0.53 | -0.29 | 0.00 | 0. |
| 5. | -1.21 | -0.55 | -0.29 | 0.02 | 5. |
| 10. | -1.63 | -0.29 | -0.05 | 0.04 | 10. |
| 15. | -2.34 | -0.02 | 0.21 | 0.06 | 15. |
| 20. | -2.33 | 0.01 | -0.23 | 0.01 | 20. |
| 25. | -2.15 | -2.13 | -0.07 | -0.21 | 25. |
| 30. | -2.44 | -0.23 | -0.10 | 0.01 | 30. |
| 35. | -1.94 | -0.22 | -0.08 | 0.04 | 35. |
| 40. | -1.42 | -0.15 | -0.05 | 0.03 | 40. |
| 45. | -1.38 | -0.12 | -0.05 | 0.00 | 45. |
| 50. | -1.25 | -0.13 | -0.06 | -0.01 | 50. |
| 55. | -1.07 | -0.[illegible]7 | -0.04 | 0.00 | 55. |
| 60. | 0.01 | -0.02 | -0.01 | 0.00 | 60. |
| 65. | 0.01 | 0.01 | -0.01 | -0.01 | 65. |
| 70. | 0.21 | 0.00 | -0.01 | -0.03 | 70. |
| 75. | 0.03 | -0.02 | -0.01 | -0.02 | 75. |
| 80. | 0.00 | -0.02 | 0.01 | -0.01 | 80. |
| 85. | 0.18 | 0.02 | 0.04 | 0.00 | 85. |
| 90. | 0.01 | 0.00 | 0.00 | 0.00 | 90. |
| 95. | 0.45 | 0.14 | 0.11 | 0.00 | 95. |
| 100. | 0.90 | 0.21 | 0.17 | 0.01 | 100. |
| 105. | 0.73 | 0.27 | 0.24 | 0.03 | 105. |
| 110. | 0.41 | 0.32 | 0.27 | 0.05 | 110. |
| 115. | 0.08 | 0.38 | 0.29 | 0.05 | 115. |
| 120. | 0.04 | 0.43 | 0.31 | 0.06 | 120. |
| 125. | 0.09 | 0.47 | 0.33 | 0.06 | 125. |
| 130. | 1.05 | 0.50 | 0.35 | 0.06 | 130. |
| 135. | 1.10 | 0.53 | 0.36 | 0.07 | 135. |
| 140. | 1.15 | 0.55 | 0.37 | 0.07 | 140. |
| 145. | 1.20 | 0.56 | 0.37 | 0.07 | 145. |
| 150. | 1.24 | 0.56 | 0.36 | 0.06 | 150. |
| 155. | 1.26 | 0.56 | 0.34 | 0.05 | 155. |
| 160. | 1.24 | 0.55 | 0.34 | 0.05 | 160. |
| 165. | 1.17 | 0.52 | 0.32 | 0.04 | 165. |
| 170. | 1.06 | 0.47 | 0.[illegible] | 0.03 | 170. |
| 175. | 0.9[illegible] | 0.42 | 0.22 | 0.02 | 175. |
| 180. | 0.72 | 0.31 | 0.16 | 0.01 | 180. |
| 185. | 0.51 | 0.18 | 0.10 | 0.[illegible] | 185. |
| 190. | 0.24 | 0.04 | 0.04 | 0.00 | 190. |
| 195. | 0.02 | -0.09 | -0.01 | 0.01 | 195. |
| 200. | -0.09 | -0.18 | -0.06 | 0.01 | 200. |
| 205. | -0.20 | -0.22 | -0.13 | 0.02 | 205. |
| 210. | -0.35 | -0.24 | -0.14 | 0.[illegible] | 210. |
| 215. | -0.41 | -0.24 | -0.16 | -0.03 | 215. |
| 220. | -0.42 | -0.24 | -0.17 | -0.01 | 220. |
| 225. | -0.44 | -0.24 | -0.18 | -0.02 | 225. |
| 230. | -0.44 | -0.24 | -0.18 | -0.03 | 230. |
| 235. | -0.44 | -0.24 | -0.18 | -0.03 | 235. |
| 240. | -0.43 | -0.23 | -0.18 | -0.03 | 240. |
| 245. | -0.42 | -0.22 | -0.17 | -0.04 | 245. |
| 250. | -0.41 | -0.21 | -0.16 | -0.05 | 250. |
| 255. | -0.39 | -0.21 | -0.16 | -0.06 | 255. |
| 260. | -0.38 | -0.20 | -0.15 | -0.07 | 260. |
| 265. | -0.39 | -0.18 | -0.15 | -0.07 | 265. |
| 270. | -0.39 | -0.14 | -0.14 | -0.06 | 270. |
| 275. | -0.39 | -0.10 | -0.14 | -0.06 | 275. |
| 280. | -0.40 | -0.07 | -0.14 | -0.05 | 280. |
| 285. | -0.40 | -0.04 | -0.13 | -0.07 | 285. |
| 290. | -0.40 | -0.01 | -0.11 | -0.09 | 290. |
| 295. | -0.36 | 0.01 | -0.09 | -0.08 | 295. |
| 300. | -0.33 | 0.02 | -0.10 | -0.07 | 300. |
| 305. | -0.31 | 0.01 | -0.10 | -0.06 | 305. |
| 310. | -0.31 | -0.03 | -0.08 | -0.06 | 310. |
| 315. | -0.31 | -0.03 | -0.07 | -0.05 | 315. |
| 320. | -0.35 | -0.04 | -0.07 | -0.02 | 320. |
| 325. | -0.41 | -0.15 | -0.09 | 0.02 | 325. |
| 330. | -0.51 | -0.24 | -0.12 | 0.02 | 330. |
| 335. | -0.60 | -0.31 | -0.14 | 0.01 | 335. |
| 340. | -0.65 | -0.34 | -0.15 | 0.01 | 340. |
| 345. | -0.63 | -0.29 | -0.14 | 0.01 | 345. |
| 350. | -0.59 | -0.32 | -0.13 | 0.01 | 350. |
| 355. | -0.09 | -0.42 | -0.21 | 0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 184 YCN= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

SPAN STATION 79.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 18.400 | DEG. |
| 0. | -1.58 | -1.12 | -0.54 | -0.56 | -0.39 | -3.18 | -0.37 | 0. |
| 5. | -1.83 | -1.42 | -0.57 | -0.63 | -0.45 | -3.19 | -0.06 | 5. |
| 10. | -1.34 | -1.07 | -0.58 | -0.45 | -0.30 | -0.12 | 0.01 | 10. |
| 15. | -1.23 | -0.98 | -0.67 | -0.42 | -0.25 | -3.10 | 0.02 | 15. |
| 20. | -1.13 | -0.85 | -0.62 | -0.36 | -0.23 | -3.12 | -0.01 | 20. |
| 25. | -1.05 | -0.87 | -0.63 | -0.36 | -0.22 | -3.13 | -0.03 | 25. |
| 30. | -0.65 | -0.59 | -0.45 | -0.26 | -0.17 | -0.10 | -0.02 | 30. |
| 35. | -0.41 | -0.37 | -0.33 | -0.16 | -0.11 | -0.10 | -0.02 | 35. |
| 40. | -0.29 | -0.24 | -0.28 | -0.14 | -0.10 | -0.11 | -0.03 | 40. |
| 45. | -0.22 | -0.19 | -0.26 | -0.13 | -0.08 | -0.10 | -0.03 | 45. |
| 50. | -0.17 | -0.19 | -0.25 | -0.12 | -0.75 | -3.13 | -0.02 | 50. |
| 55. | -0.13 | -0.16 | -0.25 | -0.11 | -0.21 | -3.15 | -0.03 | 55. |
| 60. | -0.08 | -0.14 | -0.24 | -0.10 | -0.02 | -3.10 | -0.22 | 60. |
| 65. | -0.02 | -0.11 | -0.22 | -0.09 | -0.02 | -0.11 | -0.04 | 65. |
| 70. | 0.06 | -0.07 | -0.19 | -0.04 | -0.01 | -0.11 | -0.05 | 70. |
| 75. | 0.11 | -0.00 | -0.14 | -0.02 | 0.03 | -3.11 | -0.03 | 75. |
| 80. | 0.18 | 0.07 | -0.08 | 0.04 | 0.09 | -3.08 | -0.02 | 80. |
| 85. | 0.29 | 0.16 | -0.00 | 0.16 | 0.15 | -3.06 | -0.21 | 85. |
| 90. | 0.42 | 0.25 | 0.08 | 0.16 | 0.21 | -0.05 | 0.33 | 90. |
| 95. | 0.53 | 0.33 | 0.14 | 0.22 | 0.26 | -0.03 | -0.00 | 95. |
| 100. | 0.63 | 0.42 | 0.21 | 0.26 | 0.29 | -0.01 | 0.00 | 100. |
| 105. | 0.73 | 0.50 | 0.26 | 0.28 | 0.31 | 0.02 | 0.02 | 105. |
| 110. | 0.84 | 0.59 | 0.32 | 0.32 | 0.34 | 0.04 | 0.03 | 110. |
| 115. | 0.97 | 0.67 | 0.38 | 0.38 | 0.39 | 0.06 | 0.24 | 115. |
| 120. | 1.09 | 0.77 | 0.45 | 0.44 | 0.44 | 0.13 | 0.05 | 120. |
| 125. | 1.20 | 0.86 | 0.52 | 0.47 | 0.47 | 0.14 | 0.06 | 125. |
| 130. | 1.29 | 0.94 | 0.59 | 0.47 | 0.47 | 0.16 | 0.08 | 130. |
| 135. | 1.38 | 1.04 | 0.66 | 0.51 | 0.46 | 0.16 | 0.08 | 135. |
| 140. | 1.47 | 1.12 | 0.73 | 0.53 | 0.47 | 0.18 | 0.08 | 140. |
| 145. | 1.53 | 1.18 | 0.79 | 0.56 | 0.48 | 0.22 | 0.28 | 145. |
| 150. | 1.65 | 1.24 | 0.84 | 0.55 | 0.50 | 0.20 | 0.37 | 150. |
| 155. | 1.77 | 1.32 | 0.93 | 0.56 | 0.51 | 0.21 | 0.09 | 155. |
| 160. | 1.89 | 1.41 | 0.98 | 0.61 | 0.51 | 0.23 | 0.09 | 160. |
| 165. | 1.99 | 1.47 | 1.03 | 0.66 | 0.50 | 0.24 | 0.10 | 165. |
| 170. | 2.05 | 1.48 | 1.06 | 0.68 | 0.48 | 0.26 | 0.10 | 170. |
| 175. | 1.95 | 1.48 | 1.03 | 0.66 | 0.44 | 0.26 | 0.09 | 175. |
| 180. | 1.71 | 1.28 | 0.94 | 0.59 | 0.38 | 0.24 | 0.08 | 180. |
| 185. | 1.38 | 1.09 | 0.80 | 0.49 | 0.35 | 0.21 | 0.07 | 185. |
| 190. | 1.03 | 0.83 | 0.62 | 0.36 | 0.29 | 0.18 | 0.06 | 190. |
| 195. | 0.68 | 0.56 | 0.43 | 0.23 | 0.18 | 0.13 | 0.03 | 195. |
| 200. | 0.33 | 0.31 | 0.25 | 0.11 | 0.02 | 0.07 | 0.00 | 200. |
| 205. | 0.02 | 0.13 | 0.10 | 0.03 | -0.04 | 0.05 | -0.01 | 205. |
| 210. | -0.16 | -0.03 | -0.03 | -0.03 | -0.08 | 0.01 | -0.01 | 210. |
| 215. | -0.34 | -0.15 | -0.11 | -0.07 | -0.12 | -0.01 | -0.01 | 215. |
| 220. | -0.48 | -0.25 | -0.16 | -0.14 | -0.16 | -0.02 | -0.03 | 220. |
| 225. | -0.56 | -0.33 | -0.19 | -0.18 | -0.19 | -0.03 | -0.04 | 225. |
| 230. | -0.56 | -0.38 | -0.24 | -0.21 | -0.21 | -0.04 | -0.03 | 230. |
| 235. | -0.55 | -0.42 | -0.27 | -0.23 | -0.22 | -0.05 | -0.03 | 235. |
| 240. | -0.59 | -0.45 | -0.29 | -0.23 | -0.24 | -0.06 | -0.04 | 240. |
| 245. | -0.66 | -0.47 | -0.29 | -0.24 | -0.25 | -0.07 | -0.04 | 245. |
| 250. | -0.69 | -0.48 | -0.29 | -0.24 | -0.26 | -3.07 | -0.05 | 250. |
| 255. | -0.71 | -0.49 | -0.29 | -0.23 | -0.26 | -0.07 | -0.05 | 255. |
| 260. | -0.73 | -0.50 | -0.29 | -0.23 | -0.26 | -0.06 | -0.05 | 260. |
| 265. | -0.74 | -0.50 | -0.29 | -0.23 | -0.26 | -0.07 | -0.06 | 265. |
| 270. | -0.75 | -0.50 | -0.29 | -0.23 | -0.26 | -0.06 | -0.06 | 270. |
| 275. | -0.75 | -0.50 | -0.29 | -0.23 | -0.26 | -0.06 | -0.05 | 275. |
| 280. | -0.75 | -0.50 | -0.29 | -0.23 | -0.24 | -3.05 | -0.05 | 280. |
| 285. | -0.74 | -0.50 | -0.29 | -0.23 | -0.23 | -0.05 | -0.05 | 285. |
| 290. | -0.74 | -0.50 | -0.28 | -0.23 | -0.22 | -3.04 | -0.04 | 290. |
| 295. | -0.73 | -0.50 | -0.28 | -0.23 | -0.22 | -0.04 | -0.02 | 295. |
| 300. | -0.71 | -0.51 | -0.28 | -0.23 | -0.23 | -3.04 | -0.02 | 300. |
| 305. | -0.70 | -0.51 | -0.28 | -0.23 | -0.23 | -3.03 | -0.03 | 305. |
| 310. | -0.69 | -0.51 | -0.28 | -0.23 | -0.21 | -3.02 | -0.02 | 310. |
| 315. | -0.68 | -0.51 | -0.29 | -0.23 | -0.19 | -0.02 | -0.01 | 315. |
| 320. | -0.69 | -0.50 | -0.29 | -0.23 | -0.18 | -0.02 | -0.00 | 320. |
| 325. | -0.68 | -0.48 | -0.29 | -0.22 | -0.19 | -0.02 | -0.01 | 325. |
| 330. | -0.69 | -0.46 | -0.30 | -0.22 | -0.21 | -0.03 | -0.01 | 330. |
| 335. | -0.66 | -0.47 | -0.32 | -0.22 | -0.21 | -0.03 | -0.01 | 335. |
| 340. | -0.73 | -0.50 | -0.34 | -0.24 | -0.21 | -0.04 | -0.01 | 340. |
| 345. | -0.59 | -0.39 | -0.24 | -0.18 | -0.17 | -0.03 | 0.02 | 345. |
| 350. | -0.37 | -0.24 | -0.14 | -0.11 | -0.14 | -0.02 | 0.03 | 350. |
| 355. | -0.79 | -0.52 | -0.33 | -0.31 | -0.23 | -0.08 | -0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-496 CNTR NO. 184 TCN= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

| AZ | SPAN STATION 119.7 CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -1.28 | -0.95 | -0.64 | -0.46 | -0.39 | -0.17 | -0.05 | 0. |
| 5. | -1.35 | -0.87 | -0.60 | -0.44 | -0.36 | -0.15 | -0.05 | 5. |
| 10. | -1.09 | -0.75 | -0.51 | -0.43 | -0.28 | -0.14 | -0.06 | 10. |
| 15. | -0.84 | -0.69 | -0.48 | -0.35 | -0.21 | -0.14 | -0.08 | 15. |
| 20. | -0.79 | -0.70 | -0.47 | -0.34 | -0.17 | -0.11 | -0.10 | 20. |
| 25. | -0.65 | -0.50 | -0.29 | -0.27 | -0.07 | -0.10 | -0.10 | 25. |
| 30. | -0.99 | -0.23 | -0.11 | -0.16 | 0.05 | -0.13 | -0.09 | 30. |
| 35. | 0.21 | -0.05 | 0.03 | -0.04 | 0.17 | -0.19 | -0.13 | 35. |
| 40. | 0.47 | 0.08 | 0.10 | 0.04 | 0.26 | -0.08 | -0.09 | 40. |
| 45. | 0.67 | 0.19 | 0.15 | 0.09 | 0.34 | -0.06 | -0.08 | 45. |
| 50. | 0.81 | 0.28 | 0.19 | 0.12 | 0.40 | -0.08 | -0.10 | 50. |
| 55. | 0.92 | 0.34 | 0.24 | 0.16 | 0.47 | -0.07 | -0.11 | 55. |
| 60. | 1.00 | 0.37 | 0.27 | 0.15 | 0.52 | -0.07 | -0.10 | 60. |
| 65. | 1.02 | 0.39 | 0.27 | 0.17 | 0.51 | -0.08 | -0.13 | 65. |
| 70. | 1.00 | 0.41 | 0.25 | 0.18 | 0.47 | -0.05 | -0.09 | 70. |
| 75. | 1.02 | 0.42 | 0.21 | 0.17 | 0.40 | -0.05 | -0.08 | 75. |
| 80. | 0.98 | 0.36 | 0.16 | 0.13 | 0.32 | -0.06 | -0.09 | 80. |
| 85. | 0.87 | 0.36 | 0.09 | 0.09 | 0.25 | -0.03 | -0.09 | 85. |
| 90. | 0.83 | 0.27 | 0.09 | 0.07 | 0.27 | -0.00 | -0.08 | 90. |
| 95. | 0.85 | 0.31 | 0.12 | 0.05 | 0.31 | -0.00 | -0.07 | 95. |
| 100. | 0.89 | 0.37 | 0.15 | 0.09 | 0.33 | -0.07 | -0.06 | 100. |
| 105. | 0.93 | 0.40 | 0.14 | 0.11 | 0.32 | -0.06 | -0.06 | 105. |
| 110. | 0.96 | 0.41 | 0.15 | 0.13 | 0.31 | -0.02 | -0.05 | 110. |
| 115. | 0.99 | 0.44 | 0.16 | 0.15 | 0.29 | -0.01 | -0.05 | 115. |
| 120. | 0.99 | 0.51 | 0.20 | 0.16 | 0.29 | -0.01 | -0.04 | 120. |
| 125. | 0.91 | 0.49 | 0.17 | 0.13 | 0.28 | -0.00 | -0.02 | 125. |
| 130. | 0.76 | 0.43 | 0.14 | 0.09 | 0.24 | 0.00 | -0.01 | 130. |
| 135. | 0.71 | 0.35 | 0.14 | 0.07 | 0.20 | 0.01 | 0.00 | 135. |
| 140. | 0.60 | 0.30 | 0.14 | 0.06 | 0.17 | 0.01 | 0.01 | 140. |
| 145. | 0.54 | 0.30 | 0.14 | 0.08 | 0.14 | 0.02 | 0.01 | 145. |
| 150. | 0.60 | 0.40 | 0.18 | 0.11 | 0.14 | 0.04 | 0.02 | 150. |
| 155. | 0.79 | 0.55 | 0.28 | 0.16 | 0.16 | 0.07 | 0.04 | 155. |
| 160. | 0.98 | 0.72 | 0.41 | 0.24 | 0.20 | 0.11 | 0.06 | 160. |
| 165. | 1.12 | 0.85 | 0.52 | 0.34 | 0.23 | 0.16 | 0.08 | 165. |
| 170. | 1.28 | 0.98 | 0.61 | 0.42 | 0.26 | 0.21 | 0.10 | 170. |
| 175. | 1.22 | 1.06 | 0.67 | 0.46 | 0.27 | 0.24 | 0.11 | 175. |
| 180. | 1.16 | 1.05 | 0.70 | 0.48 | 0.27 | 0.25 | 0.12 | 180. |
| 185. | 1.03 | 0.96 | 0.68 | 0.50 | 0.25 | 0.25 | 0.13 | 185. |
| 190. | 0.87 | 0.84 | 0.62 | 0.44 | 0.20 | 0.23 | 0.12 | 190. |
| 195. | 0.67 | 0.69 | 0.49 | 0.37 | 0.15 | 0.19 | 0.10 | 195. |
| 200. | 0.45 | 0.53 | 0.37 | 0.30 | 0.08 | 0.16 | 0.08 | 200. |
| 205. | 0.21 | 0.37 | 0.27 | 0.23 | 0.03 | 0.14 | 0.07 | 205. |
| 210. | -0.01 | 0.22 | 0.17 | 0.14 | -0.03 | 0.11 | 0.06 | 210. |
| 215. | -0.18 | 0.10 | 0.09 | 0.06 | -0.08 | 0.09 | 0.06 | 215. |
| 220. | -0.32 | -0.00 | 0.02 | 0.01 | -0.12 | 0.07 | 0.07 | 220. |
| 225. | -0.43 | -0.11 | -0.03 | -0.03 | -0.17 | 0.05 | 0.06 | 225. |
| 230. | -0.53 | -0.18 | -0.08 | -0.05 | -0.21 | 0.04 | 0.06 | 230. |
| 235. | -0.61 | -0.25 | -0.11 | -0.07 | -0.24 | 0.03 | 0.06 | 235. |
| 240. | -0.65 | -0.31 | -0.14 | -0.09 | -0.27 | 0.03 | 0.06 | 240. |
| 245. | -0.68 | -0.34 | -0.16 | -0.11 | -0.29 | 0.02 | 0.05 | 245. |
| 250. | -0.74 | -0.37 | -0.18 | -0.12 | -0.30 | 0.02 | 0.04 | 250. |
| 255. | -0.82 | -0.39 | -0.19 | -0.13 | -0.30 | 0.01 | 0.04 | 255. |
| 260. | -0.82 | -0.40 | -0.20 | -0.14 | -0.31 | 0.01 | 0.04 | 260. |
| 265. | -0.83 | -0.40 | -0.21 | -0.14 | -0.31 | 0.01 | 0.03 | 265. |
| 270. | -0.83 | -0.41 | -0.22 | -0.15 | -0.31 | 0.00 | 0.04 | 270. |
| 275. | -0.83 | -0.41 | -0.22 | -0.15 | -0.32 | 0.00 | 0.04 | 275. |
| 280. | -0.83 | -0.41 | -0.23 | -0.15 | -0.32 | 0.01 | 0.04 | 280. |
| 285. | -0.83 | -0.41 | -0.23 | -0.15 | -0.32 | 0.02 | 0.04 | 285. |
| 290. | -0.82 | -0.39 | -0.23 | -0.15 | -0.32 | 0.03 | 0.04 | 290. |
| 295. | -0.80 | -0.39 | -0.22 | -0.15 | -0.31 | 0.03 | 0.04 | 295. |
| 300. | -0.78 | -0.38 | -0.21 | -0.15 | -0.30 | 0.03 | 0.04 | 300. |
| 305. | -0.77 | -0.37 | -0.20 | -0.11 | -0.29 | 0.01 | 0.05 | 305. |
| 310. | -0.76 | -0.32 | -0.16 | -0.08 | -0.28 | 0.00 | 0.05 | 310. |
| 315. | -0.74 | -0.31 | -0.13 | -0.07 | -0.26 | -0.01 | 0.03 | 315. |
| 320. | -0.68 | -0.33 | -0.14 | -0.09 | -0.25 | -0.03 | 0.03 | 320. |
| 325. | -0.77 | -0.48 | -0.21 | -0.13 | -0.25 | -0.04 | 0.03 | 325. |
| 330. | -0.99 | -0.66 | -0.36 | -0.20 | -0.27 | -0.05 | 0.02 | 330. |
| 335. | -1.14 | -0.74 | -0.45 | -0.27 | -0.31 | -0.07 | -0.00 | 335. |
| 340. | -1.08 | -0.71 | -0.44 | -0.25 | -0.31 | -0.09 | -0.02 | 340. |
| 345. | -1.16 | -0.73 | -0.48 | -0.30 | -0.30 | -0.11 | -0.03 | 345. |
| 350. | -1.43 | -0.94 | -0.56 | -0.38 | -0.33 | -0.14 | -0.05 | 350. |
| 355. | -1.55 | -1.14 | -0.75 | -0.45 | -0.39 | -0.16 | -0.06 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

.EST=496 CNTR NO. 184 TCM= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.998 | 2.990 | 4.558 | 7.193 | 10.460 | DEG. |
| 0. | -0.92 | -0.88 | -0.55 | -0.40 | -0.33 | -0.00 | -0.03 | 0. |
| 5. | -1.05 | -0.91 | -0.63 | -0.54 | -0.35 | -0.14 | -0.04 | 5. |
| 10. | -0.71 | -0.65 | -0.44 | -0.42 | -0.26 | -0.19 | -0.04 | 10. |
| 15. | -0.26 | -0.16 | -0.25 | -0.21 | -0.11 | -0.10 | -0.04 | 15. |
| 20. | -0.06 | -0.02 | -0.23 | -0.05 | -0.05 | -0.14 | -0.02 | 20. |
| 25. | -0.01 | 0.02 | -0.17 | -0.02 | -0.02 | -0.11 | -0.03 | 25. |
| 30. | 0.31 | 0.23 | -0.04 | 0.09 | 0.06 | -0.08 | -0.03 | 30. |
| 35. | 0.69 | 0.51 | 0.18 | 0.23 | 0.14 | -0.04 | -0.01 | 35. |
| 40. | 1.04 | 0.81 | 0.25 | 0.38 | 0.23 | -0.05 | 0.02 | 40. |
| 45. | 1.29 | 1.03 | 0.39 | 0.54 | 0.31 | -0.02 | 0.03 | 45. |
| 50. | 1.46 | 1.15 | 0.50 | 0.68 | 0.40 | -0.00 | 0.02 | 50. |
| 55. | 1.44 | 1.19 | 0.57 | 0.77 | 0.44 | 0.01 | 0.05 | 55. |
| 60. | 1.49 | 1.29 | 0.62 | 0.81 | 0.47 | 0.00 | 0.02 | 60. |
| 65. | 1.46 | 1.30 | 0.63 | 0.83 | 0.48 | -0.01 | 0.02 | 65. |
| 70. | 1.29 | 1.20 | 0.60 | 0.84 | 0.49 | -0.03 | 0.05 | 70. |
| 75. | 1.08 | 1.14 | 0.51 | 0.84 | 0.49 | -0.05 | -0.02 | 75. |
| 80. | 0.89 | 0.89 | 0.49 | 0.81 | 0.48 | -0.04 | -0.01 | 80. |
| 85. | 0.74 | 0.70 | 0.29 | 0.79 | 0.44 | -0.13 | -0.02 | 85. |
| 90. | 0.61 | 0.60 | 0.28 | 0.74 | 0.36 | -0.17 | -0.07 | 90. |
| 95. | 0.47 | 0.53 | 0.09 | 0.65 | 0.28 | -0.22 | -0.08 | 95. |
| 100. | 0.34 | 0.47 | -0.05 | 0.53 | 0.19 | -0.21 | -0.08 | 100. |
| 105. | 0.07 | 0.36 | -0.25 | 0.37 | 0.07 | -0.23 | -0.09 | 105. |
| 110. | -0.44 | -0.02 | -0.57 | 0.12 | -0.07 | -0.29 | -0.11 | 110. |
| 115. | -1.15 | -0.76 | -0.98 | -0.17 | -0.22 | -0.32 | -0.12 | 115. |
| 120. | -1.71 | -1.13 | -1.26 | -0.35 | -0.31 | -0.35 | -0.12 | 120. |
| 125. | -1.80 | -1.26 | -1.27 | -0.41 | -0.30 | -0.35 | -0.11 | 125. |
| 130. | -1.72 | -1.06 | -1.14 | -0.39 | -0.26 | -0.33 | -0.10 | 130. |
| 135. | -1.55 | -1.06 | -0.97 | -0.32 | -0.20 | -0.29 | -0.11 | 135. |
| 140. | -1.32 | -0.99 | -0.82 | -0.24 | -0.13 | -0.24 | -0.10 | 140. |
| 145. | -1.00 | -0.61 | -0.64 | -0.17 | -0.07 | -0.20 | -0.07 | 145. |
| 150. | -0.84 | -0.21 | -0.46 | -0.10 | -0.04 | -0.15 | -0.07 | 150. |
| 155. | -0.58 | 0.03 | -0.27 | -0.02 | -0.04 | -0.13 | -0.07 | 155. |
| 160. | -0.32 | 0.10 | -0.10 | 0.07 | 0.04 | -0.05 | -0.05 | 160. |
| 165. | -0.07 | 0.26 | 0.05 | 0.14 | 0.14 | 0.05 | -0.01 | 165. |
| 170. | 0.17 | 0.29 | 0.19 | 0.21 | 0.23 | 0.05 | -0.01 | 170. |
| 175. | 0.37 | 0.32 | 0.31 | 0.24 | 0.26 | 0.09 | 0.01 | 175. |
| 180. | 0.53 | 0.37 | 0.39 | 0.27 | 0.25 | 0.13 | 0.01 | 180. |
| 185. | 0.43 | 0.41 | 0.45 | 0.28 | 0.23 | 0.14 | 0.03 | 185. |
| 190. | 0.68 | 0.48 | 0.49 | 0.27 | 0.20 | 0.18 | 0.05 | 190. |
| 195. | 0.66 | 0.52 | 0.48 | 0.22 | 0.16 | 0.18 | 0.06 | 195. |
| 200. | 0.59 | 0.56 | 0.45 | 0.14 | 0.11 | 0.14 | 0.04 | 200. |
| 205. | 0.48 | 0.58 | 0.40 | 0.06 | 0.05 | 0.15 | 0.03 | 205. |
| 210. | 0.36 | 0.19 | 0.34 | -0.01 | -0.00 | 0.13 | 0.03 | 210. |
| 215. | 0.23 | 0.02 | 0.28 | -0.08 | -0.05 | 0.12 | 0.03 | 215. |
| 220. | 0.11 | -0.11 | 0.22 | -0.14 | -0.09 | 0.11 | 0.03 | 220. |
| 225. | 0.01 | -0.19 | 0.17 | -0.19 | -0.11 | 0.11 | 0.03 | 225. |
| 230. | -0.07 | -0.24 | 0.14 | -0.22 | -0.13 | 0.11 | 0.04 | 230. |
| 235. | -0.13 | -0.27 | 0.12 | -0.25 | -0.14 | 0.12 | 0.04 | 235 |
| 240. | -0.18 | -0.30 | 0.11 | -0.27 | -0.14 | 0.13 | 0.04 | 240. |
| 245. | -0.22 | -0.32 | 0.10 | -0.29 | -0.15 | 0.13 | 0.05 | 245. |
| 250. | -0.24 | -0.33 | 0.10 | -0.32 | -0.15 | 0.12 | 0.05 | 250. |
| 255. | -0.25 | -0.34 | 0.10 | -0.33 | -0.17 | 0.12 | 0.05 | 255. |
| 260. | -0.25 | -0.34 | 0.10 | -0.34 | -0.18 | 0.12 | 0.05 | 260. |
| 265. | -0.24 | -0.34 | 0.10 | -0.34 | -0.19 | 0.12 | 0.05 | 265. |
| 270. | -0.24 | -0.35 | 0.10 | -0.34 | -0.19 | 0.12 | 0.05 | 270. |
| 275. | -0.24 | -0.36 | 0.10 | -0.34 | -0.19 | 0.12 | 0.05 | 275. |
| 280. | -0.23 | -0.36 | 0.10 | -0.35 | -0.19 | 0.12 | 0.05 | 280. |
| 285. | -0.20 | -0.35 | 0.10 | -0.36 | -0.18 | 0.12 | 0.06 | 285. |
| 290. | -0.15 | -0.32 | 0.10 | -0.35 | -0.17 | 0.12 | 0.06 | 290. |
| 295. | -0.09 | -0.26 | 0.11 | -0.34 | -0.16 | 0.13 | 0.06 | 295. |
| 300. | -0.03 | -0.21 | 0.12 | -0.30 | -0.15 | 0.14 | 0.06 | 300. |
| 305. | 0.01 | -0.18 | 0.14 | -0.26 | -0.14 | 0.13 | 0.07 | 305. |
| 310. | 0.04 | -0.16 | 0.15 | -0.23 | -0.13 | 0.13 | 0.08 | 310. |
| 315. | 0.06 | -0.15 | 0.15 | -0.22 | -0.11 | 0.14 | 0.07 | 315. |
| 320. | 0.03 | -0.18 | 0.12 | -0.21 | -0.08 | 0.13 | 0.06 | 320. |
| 325. | 0.01 | -0.21 | 0.09 | -0.22 | -0.10 | 0.11 | 0.06 | 325. |
| 330. | 0.01 | -0.22 | 0.07 | -0.22 | -0.11 | 0.10 | 0.05 | 330. |
| 335. | 0.10 | -0.19 | 0.07 | -0.22 | -0.09 | 0.09 | 0.05 | 335. |
| 340. | 0.36 | -0.04 | 0.16 | -0.19 | -0.07 | 0.09 | 0.04 | 340. |
| 345. | 0.01 | -0.16 | 0.12 | -0.23 | -0.13 | 0.09 | 0.03 | 345. |
| 350. | -0.99 | -0.63 | -0.35 | -0.41 | -0.24 | 0.12 | -0.01 | 350. |
| 355. | -1.12 | -0.80 | -0.48 | -0.46 | -0.30 | 0.14 | -0.04 | 355. |

## LIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 194 TCN= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.046 | 1.950 | 2.99C | 4.55C | 7.150 | 10.40C | DEG. |
| 0. | 0.28 | C.17 | 0.13 | C.21 | -C.07 | -C.03 | -C.17 | 0. |
| 5. | 0.09 | -C.27 | -0.21 | -0.02 | -0.28 | -0.12 | -C.02 | 5. |
| 10. | 0.28 | -C.44 | -0.33 | -1.02 | -0.26 | -0.15 | -C.03 | 10. |
| 15. | 0.20 | -C.21 | -0.21 | C.04 | -0.16 | -0.14 | -C.02 | 15. |
| 20. | 0.40 | 0.57 | 0.64 | C.19 | -0.03 | -0.06 | -C.01 | 20. |
| 25. | 0.62 | C.32 | 0.22 | 0.27 | C.13 | 0.00 | 0.00 | 25. |
| 30. | 0.73 | C.52 | 0.34 | 0.34 | 0.23 | 0.05 | 0.02 | 30. |
| 35. | 0.81 | 0.68 | 0.40 | C.46 | 0.28 | 0.06 | 0.03 | 35. |
| 40. | 0.92 | 0.80 | 0.46 | C.47 | 0.33 | 0.07 | C.03 | 40. |
| 45. | 1.04 | C.89 | 0.55 | 0.53 | 0.41 | 0.10 | 0.03 | 45. |
| 50. | 1.14 | 0.97 | 0.66 | C.59 | C.49 | 0.14 | 0.05 | 50. |
| 55. | 1.19 | 1.01 | 0.74 | 0.63 | 0.56 | 0.16 | C.07 | 55. |
| 60. | 1.16 | C.94 | 0.69 | 0.44 | 0.60 | C.15 | C.06 | 60. |
| 65. | 1.06 | C.78 | 0.52 | 0.62 | 0.61 | 0.12 | C.05 | 65. |
| 70. | 0.99 | 0.57 | 0.29 | 0.52 | 0.57 | 0.08 | C.03 | 70. |
| 75. | 0.68 | C.30 | 0.04 | C.49 | 0.53 | 0.02 | 0.04 | 75. |
| 80. | 0.43 | 0.00 | -0.17 | 0.67 | C.46 | -0.05 | 0.02 | 80. |
| 85. | 0.21 | -0.33 | -0.31 | C.75 | C.29 | -0.12 | -C.01 | 85. |
| 90. | -0.00 | -0.72 | -0.55 | C.51 | 0.03 | -0.22 | -C.04 | 93. |
| 95. | -0.43 | -1.16 | -0.81 | -C.5C | -0.16 | -0.30 | -C.03 | 95. |
| 100. | -1.15 | -1.71 | -1.37 | -1.4C | -0.25 | -0.30 | -C.03 | 100. |
| 105. | -1.97 | -2.27 | -1.76 | -1.81 | -0.29 | -0.29 | -0.03 | 105. |
| 110. | -2.45 | -2.82 | -1.96 | -1.9C | -0.32 | -0.31 | -0.03 | 110. |
| 115. | -2.57 | -3.23 | -2.07 | -2.11 | -0.39 | -0.34 | -C.03 | 115. |
| 120. | -2.66 | -3.36 | -2.17 | -1.94 | -0.48 | -0.36 | -0.04 | 120. |
| 125. | -2.74 | -3.32 | -2.29 | -1.46 | -0.60 | -0.37 | -0.05 | 125. |
| 130. | -2.83 | -3.18 | -2.37 | -1.11 | -0.63 | -0.37 | -0.06 | 130. |
| 135. | -2.82 | -2.94 | -2.29 | -1.0C | -0.60 | -0.36 | -0.05 | 135. |
| 140. | -2.64 | -2.63 | -2.08 | -1.0C | -0.55 | -0.33 | -0.04 | 140. |
| 145. | -2.35 | -2.25 | -1.65 | -0.99 | -0.48 | -0.29 | -0.03 | 145. |
| 150. | -1.99 | -1.83 | -1.28 | -0.74 | -0.40 | -0.23 | -C.02 | 150. |
| 155. | -1.59 | -1.39 | -0.98 | -0.63 | -0.33 | -0.18 | -0.01 | 155. |
| 160. | -1.19 | -1.00 | -0.71 | -0.48 | -0.24 | -0.13 | 0.00 | 160. |
| 165. | -0.81 | -0.68 | -0.47 | -0.37 | -0.16 | -0.09 | 0.01 | 165. |
| 170. | -0.47 | -C.39 | -0.26 | -0.26 | -0.08 | -0.05 | 0.01 | 170. |
| 175. | -0.22 | -C.13 | -0.07 | -0.14 | -0.00 | -0.00 | 0.02 | 175. |
| 180. | -0.02 | 0.10 | 0.11 | -0.03 | 0.05 | 0.04 | 0.02 | 180. |
| 185. | 0.18 | 0.31 | 0.27 | C.05 | 0.07 | 0.07 | C.04 | 185. |
| 190. | 0.39 | 0.48 | 0.38 | C. 1 | 0.08 | 0.08 | 0.04 | 190. |
| 195. | 0.49 | 0.59 | 0.45 | C.14 | 0.08 | 0.09 | 0.04 | 195. |
| 200. | 0.52 | 0.65 | 0.49 | C.17 | 0.07 | 0.09 | 0.03 | 200. |
| 205. | 0.52 | C.69 | 0.51 | 0.17 | 0.06 | 0.08 | 0.03 | 205. |
| 210. | 0.49 | C.70 | 0.51 | C.18 | 0.03 | 0.07 | 0.02 | 210. |
| 215. | 0.45 | C.7C | 0.50 | C.17 | -C.00 | 0.07 | 0.02 | 215. |
| 220. | 0.42 | 0.68 | 0.49 | C.16 | -0.03 | 0.07 | C.02 | 220. |
| 225. | 0.38 | C.67 | 0.48 | C.16 | -0.05 | 0.07 | 0.02 | 225. |
| 230. | 0.34 | C.67 | 0.47 | 0.16 | -0.07 | 0.07 | 0.02 | 230. |
| 235. | 0.29 | 0.67 | 0.48 | 0.17 | -0.07 | 0.08 | C.02 | 235. |
| 240. | 0.28 | 0.68 | 0.50 | C.17 | -0.07 | 0.10 | 0.02 | 240. |
| 245. | 0.29 | C.69 | 0.53 | C.18 | -0.06 | 0.11 | 0.02 | 245. |
| 250. | 0.33 | C.72 | 0.56 | 0.20 | -C.05 | 0.11 | 0.02 | 250. |
| 255. | 0.38 | 0.74 | 0.59 | 0.21 | -0.05 | 0.12 | 0.02 | 255. |
| 260. | 0.44 | 0.77 | 0.61 | 0.23 | -0.03 | 0.12 | 0.02 | 260. |
| 265. | 0.47 | C.79 | 0.63 | 0.25 | -0.02 | 0.13 | 0.02 | 265. |
| 270. | 0.48 | 0.81 | 0.64 | 0.27 | -0.01 | 0.14 | C.02 | 270. |
| 275. | 0.49 | 0.84 | 0.66 | 0.28 | 0.01 | 0.14 | 0.02 | 275. |
| 280. | 0.51 | 0.88 | 0.68 | C.3C | 0.02 | 0.15 | 0.02 | 280. |
| 285. | 0.54 | 0.93 | 0.71 | 0.31 | C.03 | 0.16 | 0.02 | 285. |
| 290. | 0.59 | C.99 | 0.73 | 0.33 | 0.04 | 0.16 | 0.02 | 290. |
| 295. | 0.67 | 1.02 | 0.77 | 0.36 | 0.05 | 0.17 | 0.02 | 295. |
| 300. | 0.75 | 1.06 | 0.81 | 0.40 | 0.06 | 0.18 | 0.02 | 300. |
| 305. | 0.82 | 1.09 | 0.84 | C.44 | 0.07 | 0.18 | 0.02 | 305. |
| 310. | 0.88 | 1.16 | 0.86 | 0.47 | 0.08 | 0.18 | 0.02 | 310. |
| 315. | 0.88 | 1.22 | 0.86 | C.48 | 0.09 | 0.18 | 0.02 | 315. |
| 320. | 0.86 | 1.18 | 0.85 | C.49 | 0.12 | 0.17 | 0.03 | 320. |
| 325. | 0.82 | 1.04 | 0.74 | C.48 | 0.14 | 0.16 | 0.04 | 325. |
| 330. | 0.76 | 0.88 | 0.67 | 0.47 | 0.14 | 0.14 | 0.02 | 330. |
| 335. | 0.67 | 0.79 | 0.61 | 0.41 | 0.09 | 0.12 | 0.02 | 335. |
| 340. | 0.58 | 0.76 | 0.57 | 0.37 | 0.05 | 0.11 | 0.02 | 340. |
| 345. | 0.62 | C.84 | 0.58 | 0.35 | C.00 | 0.11 | -0.05 | 345. |
| 350. | 0.74 | 0.85 | 0.62 | 0.44 | 0.14 | 0.10 | -0.16 | 350. |
| 355. | 0.69 | 0.98 | 0.44 | C.48 | 0.09 | 0.13 | -0.25 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-0494 CNTR NO. 184 TC%= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

SPAN STATION 100.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.25 | 0.40 | 0.34 | 0.36 | 0.30 | 0.34 | 0.02 | 0. |
| 5. | -0.45 | -0.23 | -0.32 | -0.01 | 0.17 | -0.09 | -0.01 | 5. |
| 10. | -0.57 | -0.50 | -0.36 | -0.04 | 0.12 | -0.11 | -0.01 | 10. |
| 15. | -0.33 | -0.36 | -0.25 | 0.06 | 0.19 | -0.08 | 0.00 | 15. |
| 20. | 0.05 | -0.02 | -0.05 | 0.21 | 0.32 | -0.03 | 0.01 | 20. |
| 25. | 0.40 | 0.28 | 0.18 | 0.34 | 0.43 | 0.02 | 0.00 | 25. |
| 30. | 0.48 | 0.53 | 0.36 | 0.39 | 0.50 | 0.05 | 0.06 | 30. |
| 35. | 1.16 | 0.76 | 0.45 | 0.39 | 0.51 | 0.03 | 0.06 | 35. |
| 40. | 1.28 | 0.92 | 0.52 | 0.43 | 0.54 | 0.00 | 0.05 | 40. |
| 45. | 1.35 | 1.03 | 0.57 | 0.47 | 0.62 | 0.02 | 0.05 | 45. |
| 50. | 1.37 | 1.07 | 0.70 | 0.51 | 0.78 | 0.06 | 0.05 | 50. |
| 55. | 1.33 | 1.04 | 1.01 | 0.55 | 0.94 | 0.08 | 0.06 | 55. |
| 60. | 1.28 | 0.92 | 1.34 | 0.75 | 1.02 | 0.06 | 0.06 | 60. |
| 65. | 0.99 | 0.75 | 1.52 | 1.03 | 1.02 | -0.01 | -0.03 | 65. |
| 70. | 0.75 | 0.58 | 1.47 | 0.81 | 0.96 | -0.08 | -0.03 | 70. |
| 75. | 0.49 | 0.40 | 1.29 | 0.29 | 0.81 | -0.16 | -0.02 | 75. |
| 80. | 0.23 | 0.18 | 1.14 | -0.17 | 0.66 | -0.26 | -0.06 | 80. |
| 85. | 0.11 | -0.04 | 0.95 | -0.37 | 0.91 | -0.38 | -0.10 | 85. |
| 90. | -0.63 | -0.50 | 0.76 | -0.66 | 0.11 | -0.39 | -0.06 | 90. |
| 95. | -1.57 | -1.20 | -0.36 | -1.18 | -1.31 | -0.27 | -0.03 | 95. |
| 100. | -2.11 | -1.83 | -1.35 | -1.47 | -2.56 | -0.19 | -0.02 | 100. |
| 105. | -2.31 | -2.29 | -1.66 | -1.84 | -3.06 | -0.12 | -0.01 | 105. |
| 110. | -2.52 | -2.52 | -1.75 | -2.38 | -3.03 | -0.11 | -0.02 | 110. |
| 115. | -2.71 | -2.76 | -1.86 | -2.71 | -2.58 | -0.15 | -0.02 | 115. |
| 120. | -2.99 | -2.97 | -2.12 | -2.91 | -1.38 | -0.23 | -0.02 | 120. |
| 125. | -3.04 | -3.10 | -2.30 | -3.08 | -0.20 | -0.32 | -0.04 | 125. |
| 130. | -3.12 | -3.11 | -2.52 | -2.62 | -0.07 | -0.38 | -0.06 | 130. |
| 135. | -3.09 | -3.00 | -2.55 | -1.72 | -0.29 | -0.38 | -0.06 | 135. |
| 140. | -2.98 | -2.74 | -2.41 | -1.17 | -0.42 | -0.35 | -0.06 | 140. |
| 145. | -2.76 | -2.36 | -2.15 | -1.03 | -0.44 | -0.31 | -0.06 | 145. |
| 150. | -2.40 | -1.95 | -1.80 | -0.92 | -0.39 | -0.26 | -0.06 | 150. |
| 155. | -1.97 | -1.57 | -1.40 | -0.68 | -0.29 | -0.21 | -0.04 | 155. |
| 160. | -1.51 | -1.19 | -1.00 | -0.44 | -0.16 | -0.16 | -0.04 | 160. |
| 165. | -1.14 | -0.85 | -0.73 | -0.35 | -0.05 | -0.11 | -0.03 | 165. |
| 170. | -0.81 | -0.54 | -0.50 | -0.19 | 0.05 | -0.06 | -0.02 | 170. |
| 175. | -0.58 | -0.26 | -0.31 | -0.05 | 0.10 | -0.01 | -0.02 | 175. |
| 180. | -0.10 | -0.01 | -0.16 | 0.08 | 0.13 | 0.03 | -0.01 | 180. |
| 185. | 0.12 | 0.21 | 0.02 | 0.21 | 0.18 | 0.06 | -0.00 | 185. |
| 190. | 0.35 | 0.40 | 0.09 | 0.30 | 0.12 | 0.06 | -0.01 | 190. |
| 195. | 0.40 | 0.54 | 0.17 | 0.34 | 0.13 | 0.13 | -0.01 | 195. |
| 200. | 0.54 | 0.62 | 0.24 | 0.35 | 0.13 | 0.10 | -0.01 | 200. |
| 205. | 0.54 | 0.63 | 0.29 | 0.37 | 0.13 | 0.10 | -0.01 | 205. |
| 210. | 0.51 | 0.61 | 0.31 | 0.39 | 0.11 | 0.10 | -0.02 | 210. |
| 215. | 0.46 | 0.57 | 0.32 | 0.40 | 0.08 | 0.10 | -0.03 | 215. |
| 220. | 0.43 | 0.55 | 0.32 | 0.41 | 0.05 | 0.09 | -0.02 | 220. |
| 225. | 0.41 | 0.54 | 0.31 | 0.43 | 0.03 | 0.09 | -0.01 | 225. |
| 230. | 0.41 | 0.54 | 0.30 | 0.45 | 0.02 | 0.10 | -0.00 | 230. |
| 235. | 0.43 | 0.54 | 0.29 | 0.46 | 0.02 | 0.11 | -0.01 | 235. |
| 240. | 0.45 | 0.55 | 0.30 | 0.48 | 0.01 | 0.11 | -0.01 | 240. |
| 245. | 0.48 | 0.56 | 0.31 | 0.50 | 0.01 | 0.12 | -0.00 | 245. |
| 250. | 0.52 | 0.58 | 0.33 | 0.51 | 0.01 | 0.12 | 0.00 | 250. |
| 255. | 0.56 | 0.61 | 0.35 | 0.53 | 0.01 | 0.13 | 0.00 | 255. |
| 260. | 0.61 | 0.65 | 0.37 | 0.55 | 0.01 | 0.14 | 0.01 | 260. |
| 265. | 0.66 | 0.70 | 0.38 | 0.55 | 0.01 | 0.14 | 0.01 | 265. |
| 270. | 0.71 | 0.76 | 0.39 | 0.56 | 0.02 | 0.14 | 0.01 | 270. |
| 275. | 0.78 | 0.82 | 0.41 | 0.60 | 0.03 | 0.15 | 0.01 | 275. |
| 280. | 0.87 | 0.87 | 0.43 | 0.63 | 0.05 | 0.16 | 0.01 | 280. |
| 285. | 0.97 | 0.92 | 0.47 | 0.66 | 0.07 | 0.17 | 0.01 | 285. |
| 290. | 1.06 | 0.97 | 0.51 | 0.69 | 0.10 | 0.17 | 0.02 | 290. |
| 295. | 1.14 | 1.01 | 0.58 | 0.72 | 0.13 | 0.18 | 0.02 | 295. |
| 300. | 1.21 | 1.06 | 0.65 | 0.75 | 0.17 | 0.18 | 0.02 | 300. |
| 305. | 1.27 | 1.10 | 0.72 | 0.76 | 0.21 | 0.19 | 0.03 | 305. |
| 310. | 1.30 | 1.13 | 0.74 | 0.77 | 0.26 | 0.20 | 0.04 | 310. |
| 315. | 1.32 | 1.14 | 0.75 | 0.76 | 0.32 | 0.20 | 0.04 | 315. |
| 320. | 1.30 | 1.12 | 0.73 | 0.75 | 0.37 | 0.20 | 0.04 | 320. |
| 325. | 1.25 | 1.07 | 0.70 | 0.72 | 0.41 | 0.19 | 0.04 | 325. |
| 330. | 1.17 | 1.00 | 0.64 | 0.68 | 0.44 | 0.17 | 0.03 | 330. |
| 335. | 1.08 | 0.87 | 0.57 | 0.61 | 0.44 | 0.15 | 0.04 | 335. |
| 340. | 0.87 | 0.75 | 0.52 | 0.56 | 0.27 | 0.14 | 0.04 | 340. |
| 345. | 1.01 | 0.74 | 0.51 | 0.55 | 0.22 | 0.13 | 0.04 | 345. |
| 350. | 1.34 | 1.09 | 0.67 | 0.69 | 0.25 | 0.18 | 0.36 | 350. |
| 355. | 1.13 | 1.19 | 0.73 | 0.66 | 0.20 | 0.16 | 0.07 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 184 TCN= 25. C.R.= 22.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.959 | 2.990 | 4.550 | 7.159 | 10.400 | DEG. |
| 0. | 3.55 | C.58 | 0.19 | C.28 | 0.28 | 0.01 | -0.03 | 0. |
| 5. | -3.52 | -0.02 | -0.3C | -C.05 | 0.02 | -0.30 | -0.05 | 5. |
| 10. | -3.72 | -0.23 | -0.44 | -C.15 | -0.32 | -0.12 | -0.36 | 10. |
| 15. | -0.37 | -C.11 | -0.32 | -G.07 | G.04 | -3.11 | -0.05 | 15. |
| 20. | 0.26 | 0.16 | -0.C8 | L.09 | 0.14 | -0.00 | -0.04 | 20. |
| 25. | 3.62 | 0.42 | 0.13 | 0.26 | 0.23 | -0.05 | -0.02 | 25. |
| 30. | 3.78 | 0.65 | 0.23 | 0.20 | G.29 | -0.05 | -C.02 | 30. |
| 35. | 1.22 | 0.82 | 0.21 | 0.30 | 0.34 | -0.08 | -0.03 | 35. |
| 40. | 1.66 | 0.92 | 0.23 | 0.32 | 0.42 | -0.13 | -0.03 | 40. |
| 45. | 1.64 | 0.97 | 3.68 | 0.31 | 0.48 | -0.12 | -0.32 | 45. |
| 50. | 1.55 | 0.96 | 1.21 | 0.64 | 0.53 | -0.15 | -0.33 | 50. |
| 55. | 1.58 | C.9C | 1.53 | 1.03 | G.55 | -0.20 | -0.04 | 55. |
| 60. | 1.53 | C.8C | 1.45 | 1.52 | 0.47 | -0.28 | -0.06 | 60. |
| 65. | 1.30 | 0.68 | 1.26 | 1.63 | 0.01 | -0.37 | -0.06 | 65. |
| 70. | 1.02 | 0.50 | 1.10 | 1.35 | 1.34 | -0.46 | -0.05 | 70. |
| 75. | 0.85 | 0.30 | 0.99 | G.57 | 1.76 | -1.53 | -0.04 | 75. |
| 80. | 0.40 | -0.05 | 0.87 | -0.13 | 1.03 | -0.53 | -0.08 | 80. |
| 85. | -0.45 | -0.78 | 0.54 | -G.68 | 0.23 | -0.41 | -0.04 | 85. |
| 90. | -1.28 | -1.39 | 0.01 | -C.92 | -0.52 | -0.23 | 0.06 | 90. |
| 95. | -1.75 | -1.79 | -0.40 | -1.31 | -0.77 | 3.01 | 0.08 | 95. |
| 100. | -1.99 | -2.01 | -0.57 | -1.49 | -2.20 | 0.18 | 0.09 | 100. |
| 105. | -2.21 | -2.11 | -0.79 | -1.54 | -3.08 | 3.25 | 0.11 | 105. |
| 110. | -2.39 | -2.24 | -0.91 | -1.73 | -3.25 | 0.17 | 0.09 | 110. |
| 115. | -2.58 | -2.34 | -1.22 | -2.05 | -3.15 | -0.01 | 0.09 | 115. |
| 120. | -2.75 | -2.42 | -1.62 | -2.58 | -2.88 | -0.10 | 0.09 | 120. |
| 125. | -2.87 | -2.51 | -2.62 | -2.91 | -1.31 | -0.32 | 0.65 | 125. |
| 130. | -2.94 | -2.58 | -2.23 | -3.02 | -0.15 | -0.43 | 6.81 | 130. |
| 135. | -2.93 | -2.59 | -2.28 | -2.85 | -0.04 | -0.59 | -0.32 | 135. |
| 140. | -2.82 | -2.51 | -2.39 | -1.52 | -0.12 | -0.48 | -0.04 | 140. |
| 147. | -2.57 | -2.33 | -2.24 | -C.85 | -C.35 | -3.44 | -0.03 | 145. |
| 150. | -2.25 | -2.00 | -1.87 | -C.00 | -0.35 | -0.37 | -0.03 | 150. |
| 155. | -1.9C | -1.74 | -1.55 | -C.78 | -0.38 | -3.30 | -0.02 | 155. |
| 160. | -1.57 | -1.39 | -1.23 | -0.6C | -0.22 | -0.25 | -0.00 | 160. |
| 165. | -1.24 | -1.02 | -0.92 | -0.4 | 0.12 | -0.19 | 0.02 | 165. |
| 170. | -0.91 | -C.69 | -0.66 | -G.24 | -0.04 | -0.14 | 0.01 | 170. |
| 175. | -0.58 | -0.44 | -0.42 | -C.14 | C.02 | -0.09 | 0.50 | 175. |
| 180. | -3.26 | -C.25 | -0.22 | -C.01 | 0.37 | -0.02 | 0.01 | 180. |
| 185. | 0.02 | -C.04 | -3.06 | 0.12 | 0.12 | 3.03 | 0.31 | 185. |
| 190. | 3.25 | 0.21 | 0.16 | 0.23 | 0.16 | 0.05 | 0.31 | 193. |
| 195. | 0.40 | 0.41 | 3.12 | C.31 | 0.19 | 0.06 | -0.00 | 195. |
| 200. | 0.44 | 0.46 | 0.16 | 0.34 | 0.20 | 0.08 | -0.00 | 200. |
| 205. | 3.44 | 0.42 | 0.19 | 0.35 | 0.20 | 0.10 | -0.00 | 205. |
| 210. | 0.37 | 0.43 | 0.21 | 0.35 | 0.20 | 0.11 | -0.00 | 210. |
| 215. | 0.29 | 0.45 | 0.23 | 0.37 | 0.2C | 0.11 | 0.30 | 215. |
| 220. | 0.21 | 0.46 | 0.24 | C.39 | 0.2C | 0.12 | 0.30 | 220. |
| 225. | 0.19 | C.48 | 0.25 | 0.40 | 0.20 | 0.10 | 0.00 | 225. |
| 230. | 0.20 | 0.51 | 0.26 | C.41 | 0.19 | 0.10 | 0.01 | 230. |
| 235. | 0.24 | C.55 | 0.27 | C.43 | 0.19 | 0.21 | 0.01 | 235. |
| 240. | 0.28 | 0.59 | 0.28 | C.44 | 0.19 | 0.21 | 0.01 | 240. |
| 245. | 0.34 | C.64 | 0.30 | C.47 | 0.19 | 0.22 | 0.31 | 245. |
| 250. | 0.40 | C.69 | 0.32 | C.51 | 0.19 | 0.22 | 0.01 | 252 |
| 255. | 0.46 | C.72 | 0.34 | 0.54 | 0.20 | 0.23 | C.30 | 255. |
| 260. | 0.53 | C.76 | 0.36 | 0.56 | 0.22 | 0.25 | C.00 | 260. |
| 265. | 0.60 | C.79 | 0.39 | C.57 | 0.24 | 0.26 | 0.01 | 265. |
| 270. | 0.68 | 0.83 | 0.43 | 0.59 | 0.26 | 0.27 | 0.02 | 270. |
| 275. | 0.77 | C.87 | 0.47 | 0.6C | 0.28 | 0.28 | 0.03 | 275. |
| 280. | 0.87 | C.91 | 0.51 | 0.61 | 0.30 | C.29 | 0.03 | 280. |
| 285. | 0.94 | 0.96 | 0.54 | C.62 | 0.32 | 0.29 | C.02 | 285. |
| 290. | 1.07 | 1.01 | 0.59 | 0.64 | 0.34 | C.29 | 0.02 | 290. |
| 295. | 1.18 | 1.07 | 0.63 | C.66 | 0.35 | 0.29 | C.02 | 295. |
| 300. | 1.26 | 1.12 | 0.66 | G.71 | 0.37 | 0.29 | 0.02 | 300. |
| 305. | 1.31 | 1.17 | 0.68 | 0.74 | 0.37 | 0.29 | C.31 | 305. |
| 310. | 1.31 | 1.20 | 0 69 | C.75 | 0.38 | 0.29 | 0.00 | 313. |
| 315. | 1.29 | 1.18 | 0.68 | 0.74 | 0.39 | 0.28 | 0.00 | 315. |
| 320. | 1.3C | 1.20 | 0.67 | C.71 | 0.41 | 0.27 | 0.00 | 320. |
| 325. | 1.27 | 1.17 | 0.67 | G.68 | 0.41 | 0.26 | -0.00 | 325. |
| 330. | 1.18 | 1.10 | 0.60 | 0.64 | 0.36 | 0.24 | -0.01 | 330. |
| 335. | 0.87 | C.91 | 0.49 | C.56 | 0.30 | 0.21 | -0.01 | 335. |
| 340. | 0.60 | 0.78 | 0.41 | C.48 | 0.28 | 0.19 | -0.02 | 340. |
| 345. | 0.81 | 0.76 | 0.37 | 0.45 | 0.33 | 0.16 | -0.02 | 345. |
| 350. | 1.24 | 1.04 | 0.37 | 0.44 | 0.52 | 0.13 | -0.00 | 350. |
| 355. | 1.30 | 1.17 | 0.55 | 0.62 | 0.55 | 0.11 | -0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=404 CNTR NO. 264 TCN= 26. C.R.= 11.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.550 | 10.400 | DEG. |
| 0. | -0.00 | -0.41 | -0.29 | 0.03 | 0. |
| 5. | -0.48 | -0.22 | -0.17 | 0.14 | 5. |
| 10. | -0.74 | -0.21 | -0.02 | 0.09 | 10. |
| 15. | -0.86 | -0.40 | -0.10 | 0.98 | 15. |
| 20. | -0.62 | -0.30 | -0.11 | 0.07 | 20. |
| 25. | -0.57 | -0.16 | -0.04 | 0.07 | 25. |
| 30. | -0.46 | -0.29 | -0.07 | 0.03 | 30. |
| 35. | -0.00 | -0.40 | -0.22 | -0.03 | 35. |
| 40. | -1.04 | -0.52 | -0.24 | 0.02 | 40. |
| 45. | -0.05 | -0.41 | -0.19 | 0.02 | 45. |
| 50. | -0.54 | -0.26 | -0.09 | 0.03 | 50. |
| 55. | -0.23 | -0.02 | 0.00 | 0.04 | 55. |
| 60. | -0.04 | 0.05 | 0.05 | 0.03 | 60. |
| 65. | 0.93 | 0.69 | 0.07 | 0.01 | 65. |
| 70. | -0.X | 0.04 | 0.05 | 0.01 | 70. |
| 75. | -0.07 | -0.05 | 0.02 | 0.01 | 75. |
| 80. | -0.11 | -0.0% | 0.01 | 0.00 | 80. |
| 85. | -2.07 | -0.07 | 0.01 | -0.00 | 85. |
| 90. | 0.06 | -0.02 | 0.05 | 0.00 | 90. |
| 95. | 0.23 | 0.06 | 0.09 | 0.02 | 95. |
| 100. | 0.40 | 0.16 | 0.15 | 0.05 | 100. |
| 105. | 0.58 | 0.27 | 0.22 | 0.06 | 105. |
| 110. | 0.76 | 0.39 | 0.28 | 0.07 | 110. |
| 115. | 0.94 | 0.50 | 0.35 | 0.07 | 115. |
| 120. | 1.10 | 0.60 | 0.40 | 0.08 | 120. |
| 125. | 1.25 | 0.69 | 0.44 | 0.10 | 125. |
| 130. | 1.38 | 0.76 | 0.47 | 0.10 | 130. |
| 135. | 1.47 | 0.76 | 0.48 | 0.11 | 135. |
| 140. | 1.53 | 0.79 | 0.49 | 0.11 | 140. |
| 145. | 1.56 | 0.79 | 0.48 | 0.11 | 145. |
| 150. | 1.56 | 0.79 | 0.46 | 0.10 | 150. |
| 155. | 1.54 | 0.78 | 0.44 | 0.11 | 155. |
| 160. | 1.49 | 0.66 | 0.41 | 0.10 | 160. |
| 165. | 1.40 | 0.62 | 0.37 | 0.08 | 165. |
| 170. | 1.28 | 0.55 | 0.32 | 0.06 | 170. |
| 175. | 1.11 | 0.47 | 0.26 | 0.04 | 175. |
| 180. | 0.85 | 0.34 | 0.19 | 0.03 | 180. |
| 185. | 0.54 | 0.19 | 0.12 | 0.02 | 185. |
| 190. | 0.27 | 0.09 | 0.04 | 0.01 | 190. |
| 195. | 0.03 | -0.10 | -0.05 | 0.00 | 195. |
| 200. | -0.14 | -0.23 | -0.13 | -0.00 | 200. |
| 205. | -0.28 | -0.32 | -0.21 | -0.01 | 205. |
| 210. | -0.37 | -0.34 | -0.24 | -0.01 | 210. |
| 215. | -0.42 | -0.34 | -0.26 | -0.01 | 215. |
| 220. | -0.44 | -0.30 | -0.26 | -0.03 | 220. |
| 225. | -0.44 | -0.28 | -0.25 | -0.05 | 225. |
| 230. | -0.41 | -0.26 | -0.24 | -0.07 | 230. |
| 235. | -0.38 | -0.24 | -0.23 | -0.09 | 235. |
| 240. | -0.34 | -0.22 | -0.21 | -0.10 | 240. |
| 245 | -0.33 | -0.20 | -0.20 | -0.10 | 245. |
| 250. | -0.35 | -0.19 | -0.19 | -0.11 | 250. |
| 255. | -0.35 | -0.18 | -0.19 | -0.11 | 255. |
| 260. | -0.35 | -0.17 | -0.18 | -0.11 | 260. |
| 265. | -0.34 | -0.16 | -0.18 | -0.11 | 265. |
| 270. | -0.34 | -0.15 | -0.17 | -0.11 | 270. |
| 275. | -0.36 | -0.14 | -0.16 | -0.11 | 275. |
| 280. | -0.36 | -0.13 | -0.16 | -0.11 | 280. |
| 285. | -0.36 | -0.12 | -0.15 | -0.12 | 285. |
| 290. | -0.36 | -0.11 | -0.14 | -0.14 | 290. |
| 295. | -0.36 | -0.10 | -0.13 | -0.16 | 295. |
| 300. | -0.37 | -0.10 | -0.11 | -0.14 | 300. |
| 305. | -0.38 | -0.08 | -0.08 | -0.15 | 305. |
| 310. | -0.39 | -0.06 | -0.07 | -0.14 | 310. |
| 315. | -0.39 | -0.05 | -0.06 | -0.11 | 315. |
| 320. | -0.39 | -0.05 | -0.05 | -0.07 | 320. |
| 325. | -0.39 | -0.07 | -0.04 | -0.02 | 325. |
| 330. | -0.42 | -0.12 | -0.06 | 0.03 | 330. |
| 335. | -0.49 | -0.16 | -0.06 | 0.05 | 335. |
| 340. | -0.44 | -0.17 | -0.06 | 0.04 | 340. |
| 345. | -0.71 | -0.33 | -0.14 | 0.02 | 345. |
| 350. | -0.72 | -0.48 | -0.23 | 0.04 | 350. |
| 355. | -0.75 | -0.36 | -0.27 | 0.08 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-494 CNTR NO. 264 TCN= 26. C.R.= 11.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.930 | 2.990 | 4.550 | 7.150 | 10.480 | DEG. |
| 0. | -1.65 | -1.18 | -0.85 | -0.60 | -0.45 | -0.16 | -0.03 | 0. |
| 5. | -2.10 | -1.73 | -1.14 | -0.80 | -0.52 | -0.25 | -0.08 | 5. |
| 10. | -1.78 | -1.33 | -0.79 | -0.51 | -0.27 | -0.08 | 0.03 | 10. |
| 15. | -0.89 | -0.61 | -0.34 | -0.20 | -0.04 | 0.10 | 0.16 | 15. |
| 20. | -0.09 | -0.72 | -0.52 | -0.32 | -0.16 | 0.01 | 0.09 | 20. |
| 25. | -1.26 | -0.97 | -0.74 | -0.44 | -0.29 | -0.11 | 0.02 | 25. |
| 30. | -1.17 | -0.91 | -0.67 | -0.38 | -0.27 | -0.17 | -0.00 | 30. |
| 35. | -0.82 | -0.69 | -0.54 | -0.28 | -0.16 | -0.15 | -0.03 | 35. |
| 40. | -0.69 | -0.55 | -0.49 | -0.23 | -0.08 | -0.15 | -0.02 | 40. |
| 45. | -0.59 | -0.44 | -0.43 | -0.18 | -0.03 | -0.12 | 0.01 | 45. |
| 50. | -0.48 | -0.31 | -0.33 | -0.12 | -0.02 | -0.10 | 0.01 | 50. |
| 55. | -0.17 | -0.18 | -0.25 | -0.07 | -0.02 | -0.10 | -0.00 | 55. |
| 60. | -0.05 | -0.10 | -0.22 | -0.07 | -0.04 | -0.11 | -0.02 | 60. |
| 65. | 0.00 | -0.10 | -0.24 | -0.10 | -0.05 | -0.14 | -0.03 | 65. |
| 70. | 0.01 | -0.12 | -0.28 | -0.10 | -0.05 | -0.17 | -0.04 | 70. |
| 75. | -0.01 | -0.14 | -0.27 | -0.09 | -0.02 | -0.17 | -0.04 | 75. |
| 80. | -0.03 | -0.14 | -0.24 | -0.07 | 0.00 | -0.15 | -0.01 | 80. |
| 85. | -0.01 | -0.11 | -0.19 | -0.04 | 0.14 | -0.13 | -0.01 | 85. |
| 90. | 0.07 | -0.05 | -0.14 | -0.02 | 0.19 | -0.13 | -0.01 | 90. |
| 95. | 0.20 | 0.05 | -0.07 | 0.07 | 0.19 | -0.11 | 0.01 | 95. |
| 100. | 0.40 | 0.19 | 0.06 | 0.16 | 0.25 | -0.06 | 0.01 | 100. |
| 105. | 0.46 | 0.39 | 0.21 | 0.27 | 0.32 | -0.01 | 0.03 | 105. |
| 110. | 0.46 | 0.42 | 0.37 | 0.37 | 0.40 | 0.03 | 0.07 | 110. |
| 115. | 1.22 | 0.94 | 0.59 | 0.46 | 0.47 | 0.07 | 0.00 | 115. |
| 120. | 1.45 | 1.04 | 0.71 | 0.54 | 0.53 | 0.13 | 0.09 | 120. |
| 125. | 1.64 | 1.26 | 0.83 | 0.60 | 0.58 | 0.17 | 0.12 | 125. |
| 130. | 1.80 | 1.38 | 0.91 | 0.64 | 0.61 | 0.20 | 0.13 | 130. |
| 135. | 1.90 | 1.46 | 0.96 | 0.66 | 0.62 | 0.21 | 0.12 | 135. |
| 140. | 1.95 | 1.50 | 0.97 | 0.65 | 0.61 | 0.20 | 0.11 | 140. |
| 145. | 1.93 | 1.47 | 0.96 | 0.62 | 0.57 | 0.20 | 0.12 | 145. |
| 150. | 1.83 | 1.40 | 0.91 | 0.59 | 0.51 | 0.18 | 0.11 | 150. |
| 155. | 1.71 | 1.31 | 0.99 | 0.55 | 0.49 | 0.16 | 0.13 | 155. |
| 160. | 1.63 | 1.24 | 0.81 | 0.53 | 0.42 | 0.17 | 0.13 | 160. |
| 165. | 1.76 | 1.32 | 0.89 | 0.57 | 0.46 | 0.20 | 0.11 | 165. |
| 170. | 1.90 | 1.41 | 0.90 | 0.66 | 0.50 | 0.24 | 0.13 | 170. |
| 175. | 2.00 | 1.44 | 1.05 | 0.69 | 0.52 | 0.27 | 0.14 | 175. |
| 180. | 1.90 | 1.38 | 1.03 | 0.66 | 0.48 | 0.28 | 0.14 | 180. |
| 185. | 1.61 | 1.22 | 0.93 | 0.55 | 0.38 | 0.26 | 0.13 | 185. |
| 190. | 1.23 | 0.95 | 0.72 | 0.40 | 0.24 | 0.22 | 0.10 | 190. |
| 195. | 0.82 | 0.62 | 0.45 | 0.24 | 0.10 | 0.17 | 0.07 | 195. |
| 200. | 0.42 | 0.29 | 0.21 | 0.10 | -0.04 | 0.10 | 0.03 | 200. |
| 205. | 0.04 | 0.00 | 0.04 | -0.03 | -0.19 | 0.04 | 0.01 | 205. |
| 210. | -0.26 | -0.13 | -0.08 | -0.12 | -0.18 | -0.01 | -0.01 | 210. |
| 215. | -0.47 | -0.28 | -0.17 | -0.17 | -0.21 | -0.03 | -0.01 | 215. |
| 220. | -0.58 | -0.39 | -0.22 | -0.21 | -0.22 | -0.04 | -0.02 | 220. |
| 225. | -0.49 | -0.47 | -0.25 | -0.23 | -0.24 | -0.05 | -0.03 | 225. |
| 230. | -0.37 | -0.31 | -0.27 | -0.25 | -0.26 | -0.06 | -0.04 | 230. |
| 235. | -0.44 | -0.32 | -0.27 | -0.25 | -0.27 | -0.07 | -0.02 | 235. |
| 240. | -0.48 | -0.38 | -0.27 | -0.25 | -0.27 | -0.07 | -0.00 | 240. |
| 245. | -0.44 | -0.47 | -0.25 | -0.24 | -0.27 | -0.06 | -0.07 | 245. |
| 250. | -0.42 | -0.42 | -0.23 | -0.24 | -0.27 | -0.06 | -0.07 | 250. |
| 255. | -0.40 | -0.40 | -0.21 | -0.23 | -0.27 | -0.06 | -0.08 | 255. |
| 260. | -0.39 | -0.39 | -0.19 | -0.22 | -0.26 | -0.06 | -0.09 | 260. |
| 265. | -0.39 | -0.39 | -0.17 | -0.21 | -0.25 | -0.06 | -0.11 | 265. |
| 270. | -0.39 | -0.39 | -0.16 | -0.20 | -0.25 | -0.07 | -0.11 | 270. |
| 275. | -0.39 | -0.39 | -0.16 | -0.19 | -0.25 | -0.06 | -0.11 | 275. |
| 280. | -0.39 | -0.39 | -0.17 | -0.18 | -0.24 | -0.06 | -0.11 | 280. |
| 285. | -0.39 | -0.39 | -0.17 | -0.17 | -0.24 | -0.06 | -0.10 | 285. |
| 290. | -0.40 | -0.39 | -0.18 | -0.16 | -0.24 | -0.06 | -0.13 | 290. |
| 295. | -0.40 | -0.39 | -0.19 | -0.16 | -0.24 | -0.05 | -0.19 | 295. |
| 300. | -0.42 | -0.38 | -0.18 | -0.15 | -0.24 | -0.03 | -0.22 | 300. |
| 305. | -0.44 | -0.38 | -0.18 | -0.15 | -0.23 | -0.01 | -0.20 | 305. |
| 310. | -0.45 | -0.38 | -0.18 | -0.15 | -0.22 | 0.01 | -0.15 | 310. |
| 315. | -0.46 | -0.38 | -0.19 | -0.15 | -0.20 | 0.00 | -0.09 | 315. |
| 320. | -0.46 | -0.38 | -0.20 | -0.16 | -0.19 | -0.01 | -0.07 | 320. |
| 325. | -0.46 | -0.38 | -0.23 | -0.18 | -0.17 | 0.01 | -0.05 | 325. |
| 330. | -0.48 | -0.39 | -0.29 | -0.15 | -0.15 | 0.01 | -0.03 | 330. |
| 335. | -0.45 | -0.43 | -0.32 | -0.18 | -0.17 | 0.01 | 0.03 | 335. |
| 340. | -0.75 | -0.50 | -0.34 | -0.27 | -0.23 | -0.00 | 0.01 | 340. |
| 345. | -0.48 | -0.47 | -0.29 | -0.25 | -0.24 | 0.01 | 0.01 | 345. |
| 350. | -0.61 | -0.48 | -0.26 | -0.22 | -0.21 | -0.01 | 0.02 | 350. |
| 355. | -1.03 | -0.88 | -0.37 | -0.31 | -0.30 | -0.03 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-494 CNTR NO. 264 TAN- 26. C.R.- 11.0

DIFFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.940 | 4.550 | 7.150 | 10.480 | DEG. |
| 0. | -1.01 | -1.31 | -0.77 | -0.95 | -0.49 | -0.15 | -0.03 | 0. |
| 5. | -2.21 | -1.66 | -1.01 | -0.88 | -0.53 | -0.27 | -0.09 | 5. |
| 10. | -2.23 | -1.72 | -1.09 | -0.86 | -0.52 | -0.33 | -0.14 | 10. |
| 15. | -1.87 | -1.52 | -0.99 | -0.69 | -0.48 | -0.32 | -0.17 | 15. |
| 20. | -1.26 | -1.14 | -0.72 | -0.49 | -0.28 | -0.25 | -0.16 | 20. |
| 25. | -0.62 | -0.69 | -0.37 | -0.23 | -0.01 | -0.17 | -0.12 | 25. |
| 30. | -0.11 | -0.26 | -0.04 | -0.02 | 0.19 | -0.10 | -0.10 | 30. |
| 35. | 0.18 | -0.02 | -0.01 | 0.08 | 0.33 | -0.09 | -0.10 | 35. |
| 40. | 0.25 | 0.03 | 0.02 | 0.10 | 0.43 | -0.07 | -0.09 | 40. |
| 45. | 0.35 | 0.14 | 0.15 | 0.18 | 0.48 | -0.03 | -0.08 | 45. |
| 50. | 0.37 | 0.33 | 0.28 | 0.25 | 0.39 | -0.05 | -0.10 | 50. |
| 55. | 1.27 | 0.46 | 0.33 | 0.24 | 0.31 | -0.09 | -0.14 | 55. |
| 60. | 1.39 | 0.58 | 0.27 | 0.20 | 0.37 | -0.11 | -0.15 | 60. |
| 65. | 1.39 | 0.48 | 0.25 | 0.21 | 0.44 | -0.11 | -0.13 | 65. |
| 70. | 1.28 | 0.41 | 0.24 | 0.21 | 0.50 | -0.11 | -0.12 | 70. |
| 75. | 1.08 | 0.26 | 0.11 | 0.13 | 0.42 | -0.15 | -0.14 | 75. |
| 80. | 0.83 | 0.06 | -0.07 | 0.01 | 0.31 | -0.19 | -0.14 | 80. |
| 85. | 0.65 | -0.04 | -0.19 | -0.06 | 0.25 | -0.15 | -0.11 | 85. |
| 90. | 0.77 | 0.11 | -0.11 | 0.02 | 0.29 | -0.12 | -0.09 | 90. |
| 95. | 1.04 | 0.36 | 0.05 | 0.14 | 0.37 | -0.11 | -0.07 | 95. |
| 100. | 1.37 | 0.63 | 0.22 | 0.27 | 0.44 | -0.07 | -0.06 | 100. |
| 105. | 1.46 | 0.88 | 0.37 | 0.39 | 0.49 | -0.02 | -0.06 | 105. |
| 110. | 1.88 | 1.09 | 0.50 | 0.47 | 0.53 | 0.01 | -0.05 | 110. |
| 115. | 2.00 | 1.22 | 0.59 | 0.48 | 0.52 | 0.02 | -0.04 | 115. |
| 120. | 1.97 | 1.28 | 0.58 | 0.46 | 0.42 | -0.02 | -0.03 | 120. |
| 125. | 1.41 | 0.71 | 0.28 | 0.11 | 0.26 | -0.06 | -0.04 | 125. |
| 130. | 0.34 | -0.09 | -0.21 | -0.17 | 0.10 | -0.06 | -0.02 | 130. |
| 135. | -0.23 | -0.33 | -0.42 | -0.21 | 0.03 | -0.06 | -0.02 | 135. |
| 140. | -0.03 | -0.17 | -0.30 | -0.14 | 0.00 | -0.07 | -0.03 | 140. |
| 145. | 0.15 | -0.05 | -0.22 | -0.12 | -0.01 | -0.09 | -0.03 | 145. |
| 150. | 0.33 | -0.04 | -0.18 | -0.10 | -0.01 | -0.06 | -0.00 | 150. |
| 155. | 0.17 | 0.05 | -0.08 | -0.02 | 0.02 | 0.01 | 0.02 | 155. |
| 160. | 0.34 | 0.23 | 0.07 | 0.00 | 0.05 | 0.04 | 0.02 | 160. |
| 165. | 0.56 | 0.43 | 0.23 | 0.10 | 0.11 | 0.10 | 0.05 | 165. |
| 170. | 0.77 | 0.65 | 0.38 | 0.28 | 0.17 | 0.14 | 0.09 | 170. |
| 175. | 0.95 | 0.84 | 0.51 | 0.36 | 0.23 | 0.19 | 0.12 | 175. |
| 180. | 1.06 | 0.96 | 0.61 | 0.41 | 0.25 | 0.23 | 0.14 | 180. |
| 185. | 1.06 | 0.99 | 0.67 | 0.39 | 0.22 | 0.27 | 0.15 | 185. |
| 190. | 0.93 | 0.92 | 0.65 | 0.34 | 0.17 | 0.29 | 0.14 | 190. |
| 195. | 0.72 | 0.77 | 0.56 | 0.27 | 0.10 | 0.25 | 0.13 | 195. |
| 200. | 0.49 | 0.59 | 0.42 | 0.20 | 0.02 | 0.23 | 0.13 | 200. |
| 205. | 0.25 | 0.39 | 0.31 | 0.13 | -0.00 | 0.15 | 0.08 | 205. |
| 210. | 0.01 | 0.21 | 0.20 | 0.06 | -0.13 | 0.12 | 0.07 | 210. |
| 215. | -0.19 | 0.08 | 0.10 | 0.01 | -0.16 | 0.10 | 0.07 | 215. |
| 220. | -0.34 | 0.01 | 0.05 | -0.02 | -0.18 | 0.05 | 0.08 | 220. |
| 225. | -0.45 | -0.04 | 0.02 | -0.04 | -0.19 | 0.06 | 0.08 | 225. |
| 230. | -0.54 | -0.11 | 0.00 | -0.06 | -0.22 | 0.07 | 0.08 | 230. |
| 235. | -0.66 | -0.17 | -0.02 | -0.07 | -0.24 | 0.07 | 0.07 | 235. |
| 240. | -0.65 | -0.21 | -0.04 | -0.09 | -0.26 | 0.06 | 0.06 | 240. |
| 245. | -0.69 | -0.23 | -0.05 | -0.10 | -0.27 | 0.06 | 0.05 | 245. |
| 250. | -0.71 | -0.24 | -0.07 | -0.11 | -0.28 | 0.06 | 0.05 | 250. |
| 255. | -0.73 | -0.24 | -0.08 | -0.11 | -0.28 | 0.06 | 0.06 | 255. |
| 260. | -0.73 | -0.24 | -0.08 | -0.11 | -0.27 | 0.06 | 0.06 | 260. |
| 265. | -0.74 | -0.24 | -0.08 | -0.11 | -0.26 | 0.06 | 0.07 | 265. |
| 270. | -0.74 | -0.24 | -0.08 | -0.10 | -0.25 | 0.06 | 0.07 | 270. |
| 275. | -0.75 | -0.24 | -0.08 | -0.09 | -0.24 | 0.06 | 0.07 | 275. |
| 280. | -0.75 | -0.24 | -0.08 | -0.09 | -0.23 | 0.07 | 0.08 | 280. |
| 285. | -0.75 | -0.25 | -0.08 | -0.08 | -0.22 | 0.07 | 0.08 | 285. |
| 290. | -0.75 | -0.25 | -0.08 | -0.08 | -0.22 | 0.07 | 0.08 | 290. |
| 295. | -0.74 | -0.25 | -0.08 | -0.08 | -0.22 | 0.06 | 0.07 | 295. |
| 300. | -0.75 | -0.26 | -0.09 | -0.08 | -0.23 | 0.06 | 0.06 | 300. |
| 305. | -0.78 | -0.28 | -0.09 | -0.08 | -0.23 | 0.06 | 0.05 | 305. |
| 310. | -0.79 | -0.30 | -0.10 | -0.07 | -0.23 | 0.05 | 0.06 | 310. |
| 315. | -0.80 | -0.31 | -0.10 | -0.07 | -0.23 | 0.05 | 0.05 | 315. |
| 320. | -0.79 | -0.32 | -0.10 | -0.07 | -0.23 | 0.04 | 0.05 | 320. |
| 325. | -0.76 | -0.31 | -0.09 | -0.06 | -0.22 | 0.03 | 0.05 | 325. |
| 330. | -0.71 | -0.29 | -0.08 | -0.05 | -0.22 | 0.02 | 0.03 | 330. |
| 335. | -0.64 | -0.27 | -0.07 | -0.04 | -0.21 | 0.02 | 0.02 | 335. |
| 340. | -0.53 | -0.24 | -0.04 | -0.04 | -0.20 | 0.02 | 0.01 | 340. |
| 345. | -0.47 | -0.21 | -0.01 | -0.02 | -0.20 | 0.01 | 0.01 | 345. |
| 350. | -0.63 | -0.33 | -0.18 | -0.04 | -0.21 | -0.01 | -0.00 | 350. |
| 355. | -1.07 | -0.48 | -0.34 | -0.14 | -0.29 | -0.07 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 264 TCN= 26. C.R.= 11.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.77 | -0.63 | -0.37 | -0.90 | -0.29 | -0.06 | -0.00 | 0. |
| 5. | -0.26 | -0.26 | -0.22 | -0.33 | -0.21 | -0.12 | -0.02 | 5. |
| 10. | -0.11 | -0.29 | -0.30 | -0.31 | -0.20 | -0.10 | -0.02 | 10. |
| 15. | -0.61 | -0.63 | -0.55 | -0.40 | -0.26 | -0.13 | -0.02 | 15. |
| 20. | -0.63 | -0.66 | -0.58 | -0.33 | -0.24 | -0.17 | -0.04 | 20. |
| 25. | -0.14 | -0.28 | -0.34 | -0.11 | -0.09 | -0.11 | -0.05 | 25. |
| 30. | 0.54 | 0.19 | -0.01 | 0.17 | 0.09 | -0.04 | -0.02 | 30. |
| 35. | 1.07 | 0.66 | 0.26 | 0.44 | 0.26 | 0.02 | 0.04 | 35. |
| 40. | 1.43 | 0.99 | 0.44 | 0.61 | 0.36 | 0.05 | 0.03 | 40. |
| 45. | 1.76 | 1.14 | 0.50 | 0.71 | 0.39 | 0.00 | 0.00 | 45. |
| 50. | 1.91 | 1.28 | 0.53 | 0.82 | 0.44 | -0.02 | -0.00 | 50. |
| 55. | 1.89 | 1.41 | 0.61 | 0.92 | 0.52 | 0.01 | 0.01 | 55. |
| 60. | 1.75 | 1.48 | 0.65 | 1.02 | 0.59 | 0.02 | 0.03 | 60. |
| 65. | 1.51 | 1.38 | 0.62 | 1.04 | 0.59 | -0.03 | 0.00 | 65. |
| 70. | 1.20 | 1.11 | 0.48 | 0.95 | 0.51 | -0.11 | -0.04 | 70. |
| 75. | 0.86 | 0.86 | 0.24 | 0.92 | 0.46 | -0.15 | -0.06 | 75. |
| 80. | 0.64 | 0.70 | 0.02 | 0.97 | 0.47 | -0.17 | -0.06 | 80. |
| 85. | 0.51 | 0.62 | -0.11 | 0.95 | 0.38 | -0.23 | -0.08 | 85. |
| 90. | 0.51 | 0.65 | -0.15 | 0.84 | 0.35 | -0.29 | -0.09 | 90. |
| 95. | 0.62 | 0.80 | -0.07 | 1.00 | 0.36 | -0.32 | -0.09 | 95. |
| 100. | 1.01 | 1.12 | 0.10 | 0.91 | 0.21 | -0.26 | -0.07 | 100. |
| 105. | 0.20 | 0.67 | -0.35 | 0.20 | 0.07 | -0.23 | -0.06 | 105. |
| 110. | -0.01 | -0.17 | -1.12 | -0.00 | -0.02 | -0.25 | -0.07 | 110. |
| 115. | -1.17 | -0.52 | -1.34 | -0.12 | -0.08 | -0.30 | -0.10 | 115. |
| 120. | -1.11 | -0.52 | -1.37 | -0.18 | -0.13 | -0.33 | -0.13 | 120. |
| 125. | -1.28 | -0.60 | -1.30 | -0.26 | -0.20 | -0.33 | -0.12 | 125. |
| 130. | -1.51 | -0.80 | -1.24 | -0.33 | -0.26 | -0.33 | -0.14 | 130. |
| 135. | -1.70 | -1.07 | -1.22 | -0.40 | -0.28 | -0.35 | -0.15 | 135. |
| 140. | -1.82 | -1.16 | -1.19 | -0.45 | -0.27 | -0.33 | -0.15 | 140. |
| 145. | -1.83 | -1.19 | -1.60 | -0.46 | -0.24 | -0.30 | -0.14 | 145. |
| 150. | -1.76 | -1.21 | -0.89 | -0.43 | -0.23 | -0.25 | -0.12 | 150. |
| 155. | -1.57 | -1.11 | -0.78 | -0.32 | -0.22 | -0.21 | -0.10 | 155. |
| 160. | -1.27 | -0.88 | -0.58 | -0.21 | -0.14 | -0.15 | -0.09 | 160. |
| 165. | -0.92 | -0.52 | -0.29 | -0.10 | -0.01 | -0.07 | -0.07 | 165. |
| 170. | -0.53 | -0.07 | -0.07 | -0.01 | 0.15 | 0.01 | -0.02 | 170. |
| 175. | -0.15 | 0.25 | 0.13 | 0.09 | 0.28 | 0.07 | 0.02 | 175. |
| 180. | 0.18 | 0.31 | 0.32 | 0.16 | 0.35 | 0.12 | 0.01 | 180. |
| 185. | 0.45 | 0.33 | 0.46 | 0.21 | 0.38 | 0.14 | 0.01 | 185. |
| 190. | 0.59 | 0.36 | 0.57 | 0.21 | 0.21 | 0.15 | 0.02 | 190. |
| 195. | 0.64 | 0.36 | 0.62 | 0.17 | 0.15 | 0.17 | 0.03 | 195. |
| 200. | 0.63 | 0.32 | 0.62 | 0.12 | 0.10 | 0.19 | 0.03 | 200. |
| 205. | 0.57 | 0.26 | 0.59 | 0.08 | 0.06 | 0.19 | 0.03 | 205. |
| 210. | 0.47 | 0.20 | 0.53 | 0.04 | 0.02 | 0.18 | 0.05 | 210. |
| 215. | 0.36 | 0.14 | 0.45 | -0.01 | -0.01 | 0.18 | 0.05 | 215. |
| 220. | 0.24 | 0.07 | 0.40 | -0.04 | -0.04 | 0.17 | 0.05 | 220. |
| 225. | 0.16 | -0.01 | 0.37 | -0.16 | -0.07 | 0.17 | 0.05 | 225. |
| 230. | 0.10 | -0.07 | 0.35 | -0.20 | -0.09 | 0.18 | 0.05 | 230. |
| 235. | 0.05 | -0.09 | 0.34 | -0.22 | -0.11 | 0.18 | 0.04 | 235. |
| 240. | 0.02 | -0.10 | 0.33 | -0.23 | -0.12 | 0.17 | 0.04 | 240. |
| 245. | -0.02 | -0.13 | 0.32 | -0.25 | -0.13 | 0.16 | 0.04 | 245. |
| 250. | -0.05 | -0.15 | 0.31 | -0.27 | -0.14 | 0.18 | 0.05 | 250. |
| 255. | -0.08 | -0.18 | 0.31 | -0.30 | -0.16 | 0.18 | 0.05 | 255. |
| 260. | -0.10 | -0.21 | 0.31 | -0.31 | -0.17 | 0.18 | 0.06 | 260. |
| 265. | -0.11 | -0.21 | 0.30 | -0.32 | -0.17 | 0.18 | 0.06 | 265. |
| 270. | -0.11 | -0.21 | 0.29 | -0.33 | -0.18 | 0.18 | 0.07 | 270. |
| 275. | -0.11 | -0.20 | 0.28 | -0.33 | -0.18 | 0.18 | 0.07 | 275. |
| 280. | -0.10 | -0.19 | 0.28 | -0.33 | -0.17 | 0.19 | 0.08 | 280. |
| 285. | -0.09 | -0.19 | 0.27 | -0.32 | -0.17 | 0.20 | 0.09 | 285. |
| 290. | -0.07 | -0.19 | 0.26 | -0.31 | -0.16 | 0.21 | 0.10 | 290. |
| 295. | -0.05 | -0.18 | 0.28 | -0.30 | -0.14 | 0.21 | 0.10 | 295. |
| 300. | -0.02 | -0.14 | 0.30 | -0.29 | -0.13 | 0.21 | 0.10 | 300. |
| 305. | 0.02 | -0.10 | 0.31 | -0.28 | -0.12 | 0.20 | 0.10 | 305. |
| 310. | 0.05 | -0.07 | 0.32 | -0.28 | -0.12 | 0.19 | 0.09 | 310. |
| 315. | 0.08 | -0.05 | 0.31 | -0.27 | -0.12 | 0.18 | 0.09 | 315. |
| 320. | 0.12 | -0.04 | 0.28 | -0.28 | -0.14 | 0.16 | 0.07 | 320. |
| 325. | 0.10 | -0.11 | 0.23 | -0.29 | -0.16 | 0.14 | 0.06 | 325. |
| 330. | -0.09 | -0.23 | 0.15 | -0.32 | -0.19 | 0.11 | 0.06 | 330. |
| 335. | -0.34 | -0.36 | 0.02 | -0.40 | -0.23 | 0.07 | 0.04 | 335. |
| 340. | -0.46 | -0.45 | -0.10 | -0.48 | -0.27 | 0.02 | 0.02 | 340. |
| 345. | -0.36 | -0.43 | -0.15 | -0.48 | -0.26 | 0.98 | 0.01 | 345. |
| 350. | -0.14 | -0.26 | -0.04 | -0.34 | -0.22 | 0.02 | 0.02 | 350. |
| 355. | -0.00 | -0.14 | -0.03 | -0.37 | -0.18 | 0.02 | 0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 264 TCM= 26. C.R.= 11.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.955 | 2.990 | 4.590 | 7.150 | 10.400 | DEG. |
| 0. | -0.72 | -0.22 | -0.38 | -0.06 | -0.27 | -0.13 | -0.06 | 0. |
| 5. | -0.43 | -0.02 | -0.07 | 0.06 | -0.11 | -0.08 | -0.04 | 5. |
| 10. | -0.53 | -0.17 | -0.02 | 0.09 | -0.01 | -0.03 | -0.04 | 10. |
| 15. | -0.41 | -0.13 | -0.07 | 0.08 | -0.03 | -0.01 | -0.05 | 15. |
| 20. | -0.38 | -0.18 | -0.14 | 0.07 | -0.02 | 0.01 | -0.04 | 20. |
| 25. | -0.14 | -0.03 | -0.08 | 0.16 | 0.10 | 0.03 | -0.01 | 25. |
| 30. | 0.34 | 0.37 | 0.16 | 0.32 | 0.28 | 0.05 | 0.02 | 30. |
| 35. | 1.01 | 0.73 | 0.37 | 0.44 | 0.44 | 0.09 | 0.04 | 35. |
| 40. | 1.28 | 0.83 | 0.38 | 0.49 | 0.54 | 0.14 | 0.04 | 40. |
| 45. | 1.32 | 0.91 | 0.43 | 0.52 | 0.64 | 0.18 | 0.05 | 45. |
| 50. | 1.40 | 1.05 | 0.46 | 0.54 | 0.80 | 0.22 | 0.05 | 50. |
| 55. | 1.36 | 0.96 | 0.43 | 0.60 | 0.90 | 0.22 | 0.04 | 55. |
| 60. | 1.22 | 0.78 | 0.34 | 1.02 | 0.95 | 0.19 | 0.02 | 60. |
| 65. | 1.04 | 0.42 | 0.66 | 1.09 | 1.05 | 0.13 | 0.00 | 65. |
| 70. | 0.85 | 0.21 | 0.64 | 0.83 | 1.29 | -0.30 | -0.03 | 70. |
| 75. | 0.67 | 0.22 | 0.63 | 0.51 | 1.41 | -0.25 | -0.05 | 75. |
| 80. | 0.57 | 0.28 | 0.70 | 0.34 | 0.90 | -0.39 | -0.06 | 80. |
| 85. | 0.41 | -0.03 | 0.22 | 0.34 | 0.66 | -0.39 | -0.06 | 85. |
| 90. | -0.11 | -0.48 | -0.60 | 0.14 | 0.31 | -0.54 | -0.04 | 90. |
| 95. | -0.90 | -1.61 | -1.21 | -1.21 | -0.22 | -0.82 | 0.05 | 95. |
| 100. | -1.34 | -2.40 | -1.48 | -0.42 | -0.50 | -1.04 | 0.11 | 100. |
| 105. | -1.30 | -2.47 | -1.45 | -0.46 | -0.41 | -0.91 | 0.13 | 105. |
| 110. | -1.15 | -2.29 | -1.32 | -0.48 | -0.19 | -0.51 | 0.10 | 110. |
| 115. | -1.00 | -2.04 | -1.33 | -0.32 | -0.20 | -0.13 | 0.07 | 115. |
| 120. | -1.14 | -2.07 | -1.44 | -0.54 | -1.55 | 0.16 | 0.04 | 120. |
| 125. | -1.42 | -2.22 | -1.59 | -0.77 | -3.29 | 0.29 | 0.01 | 125. |
| 130. | -1.86 | -2.47 | -1.79 | -1.00 | -2.04 | 0.12 | -0.02 | 130. |
| 135. | -2.32 | -2.93 | -2.12 | -2.50 | -0.52 | -0.09 | -0.04 | 135. |
| 140. | -2.69 | -3.39 | -2.51 | -2.20 | 0.01 | -0.24 | -0.05 | 140. |
| 145. | -2.97 | -3.66 | -2.72 | -1.44 | -0.45 | -0.36 | -0.05 | 145. |
| 150. | -2.92 | -3.48 | -2.55 | -1.00 | -0.63 | -0.33 | -0.05 | 150. |
| 155. | -2.99 | -2.75 | -1.97 | -1.07 | -0.63 | -0.28 | -0.04 | 155. |
| 160. | -2.19 | -2.07 | -1.51 | -0.97 | -0.54 | -0.25 | -0.03 | 160. |
| 165. | -1.71 | -1.47 | -1.13 | -0.78 | -0.38 | -0.20 | -0.02 | 165. |
| 170. | -1.18 | -0.92 | -0.79 | -0.57 | -0.22 | -0.13 | -0.00 | 170. |
| 175. | -0.65 | -0.46 | -0.48 | -0.38 | -0.11 | -0.06 | 0.01 | 175. |
| 180. | -0.17 | -0.07 | -0.21 | -0.21 | -0.02 | 0.00 | 0.02 | 180. |
| 185. | 0.19 | 0.26 | 0.04 | -0.05 | 0.06 | 0.05 | 0.03 | 185. |
| 190. | 0.46 | 0.53 | 0.26 | 0.04 | 0.11 | 0.10 | 0.03 | 190. |
| 195. | 0.64 | 0.72 | 0.44 | 0.18 | 0.14 | 0.13 | 0.03 | 195. |
| 200. | 0.73 | 0.87 | 0.56 | 0.33 | 0.14 | 0.15 | 0.03 | 200. |
| 205. | 0.75 | 0.96 | 0.63 | 0.44 | 0.13 | 0.15 | 0.02 | 205. |
| 210. | 0.75 | 1.01 | 0.67 | 0.48 | 0.11 | 0.15 | 0.02 | 210. |
| 215. | 0.72 | 1.03 | 0.70 | 0.49 | 0.08 | 0.14 | 0.01 | 215. |
| 220. | 0.67 | 1.05 | 0.73 | 0.50 | 0.07 | 0.13 | 0.01 | 220. |
| 225. | 0.62 | 1.01 | 0.73 | 0.51 | 0.07 | 0.13 | 0.01 | 225. |
| 230. | 0.62 | 0.99 | 0.76 | 0.52 | 0.06 | 0.14 | 0.01 | 230. |
| 235. | 0.62 | 1.00 | 0.77 | 0.54 | 0.06 | 0.17 | 0.00 | 235. |
| 240. | 0.63 | 1.02 | 0.78 | 0.55 | 0.06 | 0.18 | 0.00 | 240. |
| 245. | 0.65 | 1.04 | 0.78 | 0.57 | 0.05 | 0.19 | 0.00 | 245. |
| 250. | 0.66 | 1.06 | 0.78 | 0.58 | 0.04 | 0.19 | -0.00 | 250. |
| 255. | 0.69 | 1.08 | 0.79 | 0.59 | 0.04 | 0.19 | -0.00 | 255. |
| 260. | 0.71 | 1.09 | 0.79 | 0.59 | 0.03 | 0.19 | -0.00 | 260. |
| 265. | 0.71 | 1.10 | 0.80 | 0.59 | 0.03 | 0.19 | -0.01 | 265. |
| 270. | 0.72 | 1.11 | 0.80 | 0.59 | 0.03 | 0.19 | -0.01 | 270. |
| 275. | 0.72 | 1.12 | 0.81 | 0.58 | 0.04 | 0.20 | -0.01 | 275. |
| 280. | 0.73 | 1.13 | 0.81 | 0.58 | 0.05 | 0.21 | -0.01 | 280. |
| 285. | 0.73 | 1.14 | 0.82 | 0.51 | 0.06 | 0.21 | -0.01 | 285. |
| 290. | 0.74 | 1.17 | 0.83 | 0.32 | 0.07 | 0.22 | -0.00 | 290. |
| 295. | 0.75 | 1.19 | 0.83 | 0.34 | 0.08 | 0.22 | -0.00 | 295. |
| 300. | 0.76 | 1.22 | 0.84 | 0.35 | 0.09 | 0.22 | -0.00 | 300. |
| 305. | 0.77 | 1.23 | 0.84 | 0.37 | 0.11 | 0.22 | 0.00 | 305. |
| 310. | 0.79 | 1.23 | 0.84 | 0.38 | 0.12 | 0.22 | 0.01 | 310. |
| 315. | 0.81 | 1.21 | 0.83 | 0.40 | 0.12 | 0.21 | 0.01 | 315. |
| 320. | 0.85 | 1.17 | 0.82 | 0.41 | 0.13 | 0.19 | 0.00 | 320. |
| 325. | 0.91 | 1.12 | 0.81 | 0.42 | 0.14 | 0.17 | -0.00 | 325. |
| 330. | 0.80 | 1.04 | 0.77 | 0.40 | 0.13 | 0.15 | -0.01 | 330. |
| 335. | 0.62 | 0.94 | 0.68 | 0.37 | 0.10 | 0.12 | -0.01 | 335. |
| 340. | 0.36 | 0.78 | 0.49 | 0.32 | 0.02 | 0.09 | -0.02 | 340. |
| 345. | 0.01 | 0.53 | 0.29 | 0.22 | -0.07 | 0.03 | -0.04 | 345. |
| 350. | -0.32 | 0.25 | 0.13 | 0.11 | -0.12 | -0.03 | -0.06 | 350. |
| 355. | -0.51 | -0.02 | -0.02 | -0.02 | -0.13 | -0.08 | -0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST•494 CNTR NO. 264 TCR• 26. C.R.• 11.8

DIFFERENTIAL PRESSURES

SPAN STATION 109.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.99 | -0.67 | -0.64 | -0.10 | -0.09 | 0.06 | -0.02 | 0. |
| 5. | -0.17 | -0.16 | 0.11 | 0.00 | 0.14 | 0.11 | 0.01 | 5. |
| 10. | 0.07 | -0.19 | 0.09 | 0.21 | 0.28 | 0.16 | 0.02 | 10. |
| 15. | -0.26 | -0.44 | -0.32 | 0.02 | 0.17 | 0.09 | -0.00 | 15. |
| 20. | -0.22 | -0.40 | -0.34 | 0.01 | 0.16 | 0.09 | 0.01 | 20. |
| 25. | 0.11 | -0.19 | -0.21 | 0.11 | 0.27 | 0.17 | 0.03 | 25. |
| 30. | 0.00 | 0.53 | 0.06 | 0.75 | 0.44 | 0.23 | 0.00 | 30. |
| 35. | 1.01 | 0.74 | 0.39 | 0.44 | 0.61 | 0.24 | 0.04 | 35. |
| 40. | 1.20 | 0.74 | 0.74 | 0.48 | 0.84 | 0.28 | 0.07 | 40. |
| 45. | 1.40 | 0.96 | 1.19 | 0.40 | 1.00 | 0.28 | 0.09 | 45. |
| 50. | 1.62 | 1.11 | 1.96 | 0.67 | 1.25 | 0.24 | 0.07 | 50. |
| 55. | 1.58 | 1.01 | 1.93 | 0.95 | 1.23 | 0.18 | 0.03 | 55. |
| 60. | 1.40 | 0.83 | 1.38 | 0.77 | 1.79 | 0.07 | -0.02 | 60. |
| 65. | 1.13 | 0.69 | 1.54 | 0.32 | 1.79 | -0.07 | -0.05 | 65. |
| 70. | 0.95 | 0.56 | 1.05 | -0.03 | 1.02 | -0.22 | -0.10 | 70. |
| 75. | 0.74 | 0.56 | 1.06 | -0.09 | 0.78 | -0.34 | -0.11 | 75. |
| 80. | 0.63 | 0.38 | 1.49 | -0.00 | 0.73 | -0.62 | -0.11 | 80. |
| 85. | -0.39 | -0.39 | 0.00 | -0.13 | 0.24 | -1.49 | -0.03 | 85. |
| 90. | -0.80 | -1.19 | 0.33 | -0.95 | -0.38 | -2.00 | 0.07 | 90. |
| 95. | -1.40 | -1.95 | -0.05 | -0.95 | -0.77 | -2.49 | 0.05 | 95. |
| 100. | -1.45 | -1.67 | -0.13 | -0.93 | -0.75 | -1.27 | -0.04 | 100. |
| 105. | -1.27 | -1.62 | -0.28 | -0.88 | -0.62 | -0.94 | 0.01 | 105. |
| 110. | -1.22 | -1.65 | -0.26 | -0.79 | -0.61 | -0.86 | 0.13 | 110. |
| 115. | -1.28 | -1.69 | -0.46 | -0.75 | -0.50 | -1.03 | 0.25 | 115. |
| 120. | -1.59 | -1.74 | -0.75 | -0.75 | -0.82 | -0.96 | 0.29 | 120. |
| 125. | -1.36 | -1.87 | -1.04 | -1.04 | -1.00 | -0.49 | 0.22 | 125. |
| 130. | -1.82 | -2.20 | -1.44 | -1.75 | -2.98 | 0.29 | 0.11 | 130. |
| 135. | -2.37 | -2.55 | -1.85 | -2.51 | -2.93 | 0.54 | 0.02 | 135. |
| 140. | -2.98 | -2.87 | -2.36 | -3.08 | -1.16 | 0.17 | -0.05 | 140. |
| 145. | -3.29 | -3.16 | -2.76 | -3.23 | -0.21 | -0.18 | -0.10 | 145. |
| 150. | -3.48 | -3.18 | -2.77 | -2.98 | -0.54 | -0.22 | -0.11 | 150. |
| 155. | -3.22 | -2.76 | -2.44 | -2.33 | -0.95 | -0.16 | -0.10 | 155. |
| 160. | -2.62 | -2.15 | -1.98 | -1.62 | -0.53 | -0.00 | -0.07 | 160. |
| 165. | -2.28 | -1.95 | -1.58 | -0.92 | -0.48 | -0.00 | -0.00 | 165. |
| 170. | -1.69 | -0.98 | -1.17 | -0.49 | -0.24 | 0.07 | -0.07 | 170. |
| 175. | -1.09 | -0.47 | -0.79 | -0.22 | -0.14 | 0.14 | -0.05 | 175. |
| 180. | -0.94 | -0.10 | -0.48 | -0.01 | -0.05 | 0.19 | -0.03 | 180. |
| 185. | -0.12 | 0.20 | -0.24 | 0.17 | 0.22 | 0.23 | -0.03 | 185. |
| 190. | 0.22 | 0.44 | -0.04 | 0.36 | 0.37 | 0.27 | -0.03 | 190. |
| 195. | 0.46 | 0.60 | 0.11 | 0.48 | 0.48 | 0.29 | -0.03 | 195. |
| 200. | 0.63 | 0.82 | 0.21 | 0.47 | 0.48 | 0.30 | -0.04 | 200. |
| 205. | 0.73 | 0.88 | 0.28 | 0.51 | 0.46 | 0.30 | -0.04 | 205. |
| 210. | 0.75 | 0.89 | 0.28 | 0.54 | 0.45 | 0.30 | -0.04 | 210. |
| 215. | 0.73 | 0.90 | 0.27 | 0.54 | 0.44 | 0.30 | -0.04 | 215. |
| 220. | 0.70 | 0.91 | 0.25 | 0.54 | 0.34 | 0.30 | -0.03 | 220. |
| 225. | 0.70 | 0.92 | 0.24 | 0.59 | 0.33 | 0.31 | -0.02 | 225. |
| 230. | 0.71 | 0.92 | 0.27 | 0.60 | 0.32 | 0.31 | -0.02 | 230. |
| 235. | 0.73 | 0.92 | 0.30 | 0.62 | 0.32 | 0.32 | -0.02 | 235. |
| 240. | 0.75 | 0.93 | 0.33 | 0.65 | 0.31 | 0.34 | -0.02 | 240. |
| 245. | 0.79 | 0.95 | 0.36 | 0.67 | 0.31 | 0.35 | -0.02 | 245. |
| 250. | 0.82 | 0.97 | 0.37 | 0.69 | 0.31 | 0.35 | -0.02 | 250. |
| 255. | 0.84 | 0.99 | 0.37 | 0.70 | 0.31 | 0.35 | -0.02 | 255. |
| 260. | 0.84 | 1.00 | 0.38 | 0.70 | 0.31 | 0.35 | -0.02 | 260. |
| 265. | 0.83 | 1.01 | 0.38 | 0.71 | 0.32 | 0.35 | -0.02 | 265. |
| 270. | 0.80 | 1.02 | 0.38 | 0.71 | 0.32 | 0.35 | -0.02 | 270. |
| 275. | 0.82 | 1.03 | 0.38 | 0.71 | 0.33 | 0.36 | -0.01 | 275. |
| 280. | 0.84 | 1.03 | 0.38 | 0.71 | 0.34 | 0.36 | -0.01 | 280. |
| 285. | 0.87 | 1.04 | 0.39 | 0.73 | 0.35 | 0.37 | -0.00 | 285. |
| 290. | 0.91 | 1.06 | 0.40 | 0.75 | 0.36 | 0.37 | 0.00 | 290. |
| 295. | 0.94 | 1.08 | 0.41 | 0.77 | 0.37 | 0.38 | 0.01 | 295. |
| 300. | 1.02 | 1.10 | 0.43 | 0.78 | 0.39 | 0.38 | 0.01 | 300. |
| 305. | 1.08 | 1.12 | 0.45 | 0.78 | 0.10 | 0.38 | 0.01 | 305. |
| 310. | 1.13 | 1.12 | 0.46 | 0.78 | 0.11 | 0.38 | 0.01 | 310. |
| 315. | 1.15 | 1.12 | 0.47 | 0.77 | 0.12 | 0.37 | 0.00 | 315. |
| 320. | 1.16 | 1.10 | 0.48 | 0.75 | 0.12 | 0.36 | 0.01 | 320. |
| 325. | 1.12 | 1.06 | 0.47 | 0.72 | 0.11 | 0.35 | 0.02 | 325. |
| 330. | 1.03 | 0.96 | 0.43 | 0.69 | 0.10 | 0.34 | 0.02 | 330. |
| 335. | 0.86 | 0.83 | 0.35 | 0.65 | ...08 | 0.32 | 0.02 | 335. |
| 340. | 0.61 | 0.62 | 0.21 | 0.57 | 0.07 | 0.28 | 0.00 | 340. |
| 345. | 0.25 | 0.16 | 0.06 | 0.36 | 0.04 | 0.24 | -0.02 | 345. |
| 350. | -0.24 | -0.23 | -0.27 | 0.17 | 0.01 | 0.18 | -0.04 | 350. |
| 355. | -0.36 | -0.28 | -0.29 | 0.13 | -0.00 | 0.12 | -0.04 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 264 TCN= 26. C.R.= 11.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.480 | DEG. |
| 0. | -1.22 | -0.60 | -0.78 | -0.35 | -0.13 | -0.03 | -0.05 | 0. |
| 5. | -1.42 | -0.98 | -0.69 | -0.29 | -0.03 | -0.02 | -0.03 | 5. |
| 10. | -0.83 | -0.83 | -0.39 | -0.00 | 0.04 | -0.02 | -0.04 | 10. |
| 15. | 0.09 | -0.25 | -0.34 | -0.20 | 0.02 | -0.08 | -0.05 | 15. |
| 20. | -0.13 | -0.38 | -0.61 | -0.17 | 0.02 | -0.11 | -0.05 | 20. |
| 25. | -0.01 | -0.05 | -0.34 | 0.00 | 0.11 | -0.05 | -0.02 | 25. |
| 30. | 0.56 | 0.33 | -0.18 | 0.04 | 0.25 | 0.01 | 0.02 | 30. |
| 35. | 1.03 | 0.67 | 0.03 | 0.16 | 0.48 | 0.05 | 0.04 | 35. |
| 40. | 1.34 | 0.96 | 0.60 | 0.51 | 0.75 | 0.04 | 0.04 | 40. |
| 45. | 1.66 | 0.72 | 1.15 | 1.24 | 0.98 | -0.25 | 0.04 | 45. |
| 50. | 2.03 | 0.86 | 1.48 | 2.06 | 0.88 | -0.19 | 0.03 | 50. |
| 55. | 2.09 | 0.96 | 1.48 | 1.41 | 1.22 | -0.33 | 0.02 | 55. |
| 60. | 1.93 | 0.89 | 1.27 | 0.64 | 1.23 | -0.32 | -0.04 | 60. |
| 65. | 1.66 | 0.77 | 1.23 | 0.22 | 0.79 | -0.09 | -0.14 | 65. |
| 70. | 1.58 | 0.78 | 1.29 | 0.12 | 0.52 | -0.33 | -0.14 | 70. |
| 75. | 1.39 | 0.67 | 1.22 | 0.02 | 0.41 | -1.59 | -0.04 | 75. |
| 80. | 0.78 | -0.12 | 0.72 | -0.41 | 0.21 | -2.34 | 0.12 | 80. |
| 85. | -0.22 | -1.14 | 0.21 | -0.79 | -0.17 | -1.48 | -0.09 | 85. |
| 90. | -1.15 | -1.55 | -0.13 | -0.99 | -0.44 | -0.03 | -0.57 | 90. |
| 95. | -1.30 | -1.48 | -0.26 | -0.92 | -0.58 | -0.42 | -0.68 | 95. |
| 100. | -1.13 | -1.38 | -0.25 | -0.75 | -0.59 | 0.72 | -0.59 | 100. |
| 105. | -0.85 | -1.26 | -0.26 | -0.62 | -0.57 | 1.00 | -0.35 | 105. |
| 110. | -0.84 | -1.29 | -0.28 | -0.56 | -0.63 | 0.69 | 0.02 | 110. |
| 115. | -0.99 | -1.36 | -0.23 | -0.62 | -0.77 | -0.13 | 0.26 | 115. |
| 120. | -1.01 | -1.48 | -0.14 | -0.77 | -0.77 | -1.28 | 0.31 | 120. |
| 125. | -1.22 | -1.37 | -0.29 | -0.86 | -0.92 | -1.02 | 0.28 | 125. |
| 130. | -1.51 | -1.43 | -0.49 | -1.43 | -2.16 | -0.16 | 0.23 | 130. |
| 135. | -1.88 | -1.74 | -1.22 | -2.48 | -3.29 | 0.36 | 0.18 | 135. |
| 140. | -2.39 | -2.11 | -1.94 | -3.08 | -2.18 | -0.08 | 0.02 | 140. |
| 145. | -2.89 | -2.45 | -2.39 | -3.22 | -0.92 | -0.39 | -0.08 | 145. |
| 150. | -3.17 | -2.71 | -2.59 | -2.13 | -0.23 | -0.45 | -0.08 | 150. |
| 155. | -3.17 | -2.76 | -2.39 | -1.09 | -0.44 | -0.39 | 0.01 | 155. |
| 160. | -2.84 | -2.41 | -1.99 | -0.88 | -0.44 | -0.28 | 0.01 | 160. |
| 165. | -2.27 | -1.83 | -1.51 | -0.78 | -0.36 | -0.23 | 0.02 | 165. |
| 170. | -1.60 | -1.25 | -1.11 | -0.54 | -0.23 | -0.16 | 0.03 | 170. |
| 175. | -1.16 | -0.76 | -0.74 | -0.29 | -0.10 | -0.05 | 0.05 | 175. |
| 180. | -0.65 | -0.34 | -0.41 | -0.05 | 0.02 | 0.06 | 0.06 | 180. |
| 185. | -0.18 | -0.03 | -0.15 | 0.13 | 0.13 | 0.11 | 0.06 | 185. |
| 190. | 0.23 | 0.22 | 0.05 | 0.28 | 0.19 | 0.14 | 0.05 | 190. |
| 195. | 0.49 | 0.39 | 0.18 | 0.37 | 0.21 | 0.17 | 0.03 | 195. |
| 200. | 0.58 | 0.52 | 0.24 | 0.43 | 0.22 | 0.19 | 0.03 | 200. |
| 205. | 0.59 | 0.48 | 0.26 | 0.45 | 0.22 | 0.20 | 0.03 | 205. |
| 210. | 0.56 | 0.45 | 0.28 | 0.44 | 0.21 | 0.22 | 0.03 | 210. |
| 215. | 0.55 | 0.49 | 0.33 | 0.48 | 0.20 | 0.24 | 0.03 | 215. |
| 220. | 0.53 | 0.71 | 0.31 | 0.50 | 0.21 | 0.26 | 0.04 | 220. |
| 225. | 0.51 | 0.73 | 0.32 | 0.52 | 0.22 | 0.28 | 0.05 | 225. |
| 230. | 0.49 | 0.74 | 0.33 | 0.53 | 0.24 | 0.31 | 0.06 | 230. |
| 235. | 0.50 | 0.76 | 0.36 | 0.55 | 0.24 | 0.33 | 0.06 | 235. |
| 240. | 0.52 | 0.79 | 0.38 | 0.57 | 0.25 | 0.34 | 0.06 | 240. |
| 245. | 0.54 | 0.83 | 0.41 | 0.59 | 0.25 | 0.35 | 0.06 | 245. |
| 250. | 0.57 | 0.86 | 0.42 | 0.61 | 0.26 | 0.36 | 0.06 | 250. |
| 255. | 0.57 | 0.89 | 0.43 | 0.63 | 0.26 | 0.36 | 0.06 | 255. |
| 260. | 0.58 | 0.92 | 0.44 | 0.63 | 0.26 | 0.37 | 0.06 | 260. |
| 265. | 0.59 | 0.95 | 0.45 | 0.64 | 0.26 | 0.37 | 0.05 | 265. |
| 270. | 0.60 | 0.95 | 0.46 | 0.65 | 0.26 | 0.38 | 0.05 | 270. |
| 275. | 0.63 | 0.96 | 0.47 | 0.65 | 0.27 | 0.38 | 0.05 | 275. |
| 280. | 0.66 | 0.97 | 0.49 | 0.65 | 0.27 | 0.39 | 0.05 | 280. |
| 285. | 0.70 | 0.98 | 0.50 | 0.66 | 0.28 | 0.39 | 0.05 | 285. |
| 290. | 0.75 | 1.01 | 0.51 | 0.67 | 0.28 | 0.39 | 0.05 | 290. |
| 295. | 0.80 | 1.05 | 0.52 | 0.68 | 0.29 | 0.39 | 0.05 | 295. |
| 300. | 0.86 | 1.08 | 0.53 | 0.68 | 0.30 | 0.38 | 0.05 | 300. |
| 305. | 0.92 | 1.11 | 0.54 | 0.69 | 0.30 | 0.37 | 0.04 | 305. |
| 310. | 0.96 | 1.14 | 0.54 | 0.69 | 0.31 | 0.37 | 0.04 | 310. |
| 315. | 0.98 | 1.16 | 0.53 | 0.70 | 0.31 | 0.36 | 0.03 | 315. |
| 320. | 0.97 | 1.16 | 0.50 | 0.69 | 0.31 | 0.34 | 0.03 | 320. |
| 325. | 0.91 | 1.13 | 0.47 | 0.66 | 0.29 | 0.32 | 0.02 | 325. |
| 330. | 0.80 | 1.04 | 0.42 | 0.59 | 0.27 | 0.31 | 0.01 | 330. |
| 335. | 0.64 | 0.91 | 0.32 | 0.46 | 0.24 | 0.27 | -0.00 | 335. |
| 340. | 0.48 | 0.71 | 0.17 | 0.31 | 0.18 | 0.22 | -0.02 | 340. |
| 345. | 0.04 | 0.42 | -0.06 | 0.15 | 0.11 | 0.16 | -0.04 | 345. |
| 350. | -0.51 | -0.03 | -0.33 | -0.00 | 0.02 | 0.07 | -0.05 | 350. |
| 355. | -0.90 | -0.00 | -0.32 | -0.00 | -0.07 | 0.03 | -0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=990 CNTR NO. 450 TCN= 27. C.R.= 39.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.959 | 6.590 | 13.400 | DEG. |
| 0. | -0.82 | -0.40 | -0.30 | 0.06 | 0. |
| 5. | -0.89 | -0.29 | -0.10 | 0.06 | 5. |
| 10. | -0.87 | -0.24 | 0.03 | 0.07 | 10. |
| 15. | -0.67 | -0.19 | 0.04 | 0.04 | 15. |
| 20. | -0.64 | -0.18 | -0.05 | 0.02 | 20. |
| 25. | -1.16 | -0.45 | -0.17 | 0.02 | 25. |
| 30. | -1.45 | -0.66 | -0.26 | 0.03 | 30. |
| 35. | -1.30 | -0.66 | -0.28 | 0.03 | 35. |
| 40. | -1.09 | -0.54 | -0.23 | 0.01 | 40. |
| 45. | -0.83 | -0.41 | -0.1' | -0.04 | 45. |
| 50. | -0.55 | -0.25 | -0.0 | -0.03 | 50. |
| 55. | -0.28 | -0.09 | 0.05 | 0.01 | 55. |
| 60. | -0.14 | -0.04 | 0.09 | 0.02 | 60. |
| 65. | -0.11 | -0.04 | 0.09 | 0.00 | 65. |
| 70. | -0.13 | -0.12 | 0.05 | -0.01 | 70. |
| 75. | -0.18 | -0.16 | 0.02 | 0.00 | 75. |
| 80. | -0.21 | -0.19 | 0.01 | C.:1 | 80. |
| 85. | -0.15 | -0.18 | 0.01 | 0.01 | 85. |
| 90. | -0.04 | -0.14 | 0.03 | -0.01 | 90. |
| 95. | 0.18 | -0.07 | 0.07 | -0.01 | 95. |
| 100. | 0.47 | 0.07 | 0.14 | 0.02 | 100. |
| 105. | 0.79 | 0.27 | 0.23 | 0.04 | 105. |
| 110. | 1.02 | 0.44 | 0.31 | 0.06 | 110. |
| 115. | 1.13 | 0.54 | 0.36 | 0.06 | 115. |
| 120. | 1.18 | 0.59 | 0.39 | C.07 | 120. |
| 125. | 1.27 | 0.64 | 0.40 | 0.09 | 125. |
| 130. | 1.37 | 0.68 | 0.44 | 0.10 | 130. |
| 135. | 1.51 | C.73 | 0.48 | C.11 | 135. |
| 140. | 1.65 | 0.78 | 0.51 | 0.12 | 140. |
| 145. | 1.76 | 0.83 | 0.53 | 0.12 | 145. |
| 150. | 1.82 | 0.87 | 0.51 | C.11 | 150. |
| 155. | 1.81 | 0.86 | 0.47 | 0.10 | 155. |
| 160. | 1.72 | 0.80 | 0.42 | 0.08 | 160. |
| 165. | 1.57 | 0.70 | 0.34 | C.05 | 165. |
| 170. | 1.36 | 0.60 | 0.29 | 0.02 | 170. |
| 175. | 1.11 | 0.48 | 0.20 | -0.01 | 175. |
| 180. | 0.79 | 0.32 | 0.11 | -0.01 | 180. |
| 185. | 0.46 | 0.13 | 0.03 | -0.01 | 185. |
| 190. | 0.16 | -0.05 | -0.07 | -0.02 | 190. |
| 195. | -0.10 | -0.19 | -0.14 | -0.03 | 195. |
| 200. | -0.28 | -0.27 | -0.22 | -0.02 | 200. |
| 205. | -0.38 | -0.30 | -0.25 | -0.01 | 205. |
| 210. | -0.4: | -0.35 | -0.26 | -0.02 | 210. |
| 215. | -0.40 | -0.27 | -0.24 | -0.02 | 215. |
| 220. | -0.36 | -0.24 | -0.24 | -0.03 | 220. |
| 225. | -0.32 | -0.23 | -0.23 | -0.03 | 225. |
| 230. | -0.32 | -0.22 | -0.21 | -0.03 | 230. |
| 235. | -0.31 | -0.21 | -0.21 | -0.03 | 235. |
| 240. | -0.31 | -0.19 | -0.21 | -0.04 | 240. |
| 245. | -0.30 | -0.17 | -0.21 | -0.05 | 245. |
| 250. | -0.30 | -0.14 | -0.21 | -0.07 | 250. |
| 255. | -0.31 | -0.12 | -0.21 | -0.09 | 255. |
| 260. | -0.31 | -0.10 | -0.20 | -0.10 | 260. |
| 265. | -0.31 | -0.08 | -0.20 | -0.11 | 265. |
| 270. | -0.31 | -0.07 | -0.20 | -0.12 | 270. |
| 275. | -0.30 | -0.06 | -0.19 | -0.13 | 275. |
| 280. | -0.28 | -0.06 | -0.18 | -0.13 | 280. |
| 285. | -0.27 | -0.05 | -0.15 | -0.12 | 285. |
| 290. | -0.29 | -0.06 | -0.13 | -0.11 | 290. |
| 295. | -0.32 | -0.06 | -0.12 | -0.10 | 295. |
| 300. | -0.34 | -0.07 | -0.11 | -0.10 | 300. |
| 305. | -0.35 | -0.07 | -0.10 | -0.10 | 305. |
| 310. | -0.32 | -0.06 | -0.09 | -0.12 | 310. |
| 315. | -0.31 | -0.04 | -0.07 | -0.07 | 315. |
| 320. | -0.36 | -0.04 | -0.06 | -0.01 | 320. |
| 325. | -0.41 | -0.13 | -0.03 | 0.02 | 325. |
| 330. | -0.45 | -0.12 | -0.04 | 0.04 | 330. |
| 335. | -0.40 | -0.12 | -0.05 | 0.06 | 335. |
| 340. | -0.35 | -0.12 | -0.02 | 0.07 | 340. |
| 345. | -0.44 | -0.17 | -0.0: | 0.07 | 345. |
| 350. | -0.66 | -0.32 | -0.07 | 0.07 | 350. |
| 355. | -0.71 | -0.43 | -0.07 | 0.07 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-390 CNTR NO. 458 TCM= 27. C.R.= 39.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -2.34 | -1.52 | -0.91 | -0.64 | -0.40 | -0.15 | -0.02 | 0. |
| 5. | -1.98 | -1.00 | -0.69 | -0.45 | -0.31 | -0.05 | 0.02 | 5. |
| 10. | -1.16 | -0.80 | -0.58 | -0.37 | -0.22 | -0.06 | 0.09 | 10. |
| 15. | -0.93 | -0.75 | -0.51 | -0.33 | -0.20 | -0.05 | 0.06 | 15. |
| 20. | -1.00 | -0.87 | -0.65 | -0.43 | -0.29 | -0.13 | 0.00 | 20. |
| 25. | -1.32 | -1.05 | -0.87 | -0.58 | -0.31 | -0.18 | -0.01 | 25. |
| 30. | -1.25 | -0.99 | -0.81 | -0.48 | -0.28 | -0.19 | 0.00 | 30. |
| 35. | -1.08 | -0.85 | -0.72 | -0.45 | -0.24 | -0.16 | -0.02 | 35. |
| 40. | -0.98 | -0.87 | -0.68 | -0.46 | -0.18 | -0.18 | -0.04 | 40. |
| 45. | -0.71 | -0.54 | -0.58 | -0.31 | -0.13 | -0.14 | -0.03 | 45. |
| 50. | -0.56 | -0.44 | -0.44 | -0.27 | -0.12 | -0.13 | -0.00 | 50. |
| 55. | -0.48 | -0.36 | -0.42 | -0.26 | -0.12 | -0.12 | 0.00 | 55. |
| 60. | -0.22 | -0.31 | -0.39 | -0.21 | -0.09 | -0.13 | -0.01 | 60. |
| 65. | -0.07 | -0.28 | -0.34 | -0.17 | -0.05 | -0.14 | -0.02 | 65. |
| 70. | 0.04 | -0.25 | -0.26 | -0.10 | 0.01 | -0.14 | -0.03 | 70. |
| 75. | 0.09 | -0.24 | -0.21 | -0.02 | 0.00 | -0.14 | -0.02 | 75. |
| 80. | 0.01 | -0.24 | -0.24 | -0.03 | 0.12 | -0.13 | 0.00 | 80. |
| 85. | -0.03 | -0.23 | -0.28 | -0.04 | 0.11 | -0.15 | -0.00 | 85. |
| 90. | 0.07 | -0.15 | -0.24 | 0.01 | 0.13 | -0.13 | -0.01 | 90. |
| 95. | 0.30 | 0.04 | -0.11 | 0.10 | 0.28 | -0.13 | 0.00 | 95. |
| 100. | 0.90 | 0.28 | 0.04 | 0.21 | 0.27 | -0.05 | 0.01 | 100. |
| 105. | 0.90 | 0.51 | 0.18 | 0.32 | 0.33 | -0.02 | 0.03 | 105. |
| 110. | 1.17 | 0.67 | 0.38 | 0.41 | 0.42 | 0.22 | 0.04 | 110. |
| 115. | 1.20 | 0.80 | 0.42 | 0.48 | 0.38 | 0.05 | 0.07 | 115. |
| 120. | 1.38 | 0.91 | 0.55 | 0.53 | 0.55 | 0.19 | 0.11 | 120. |
| 125. | 1.57 | 1.03 | 0.68 | 0.57 | 0.58 | 0.24 | 0.14 | 125. |
| 130. | 1.76 | 1.14 | 0.79 | 0.62 | 0.58 | 0.19 | 0.14 | 130. |
| 135. | 1.91 | 1.22 | 0.87 | 0.68 | 0.55 | 0.21 | 0.14 | 135. |
| 140. | 2.02 | 1.26 | 0.93 | 0.69 | 0.55 | 0.22 | 0.14 | 140. |
| 145. | 2.08 | 1.37 | 0.96 | 0.64 | 0.55 | 0.22 | 0.13 | 145. |
| 150. | 2.03 | 1.34 | 0.95 | 0.62 | 0.56 | 0.22 | 0.13 | 150. |
| 155. | 2.14 | 1.41 | 1.09 | 0.66 | 0.57 | 0.24 | 0.13 | 155. |
| 160. | 2.30 | 1.61 | 1.11 | 0.73 | 0.59 | 0.24 | 0.14 | 160. |
| 165. | 2.57 | 1.76 | 1.24 | 0.81 | 0.61 | 0.22 | 0.19 | 165. |
| 170. | 2.59 | 1.82 | 1.30 | 0.83 | 0.60 | 0.20 | 0.19 | 170. |
| 175. | 2.39 | 1.77 | 1.28 | 0.78 | 0.57 | 0.17 | 0.15 | 175. |
| 180. | 2.03 | 1.59 | 1.17 | 0.67 | 0.49 | 0.14 | 0.15 | 180. |
| 185. | 1.53 | 1.25 | 0.94 | 0.51 | 0.36 | 0.12 | 0.12 | 185. |
| 190. | 0.96 | 0.85 | 0.62 | 0.35 | 0.17 | 0.10 | 0.08 | 190. |
| 195. | 0.43 | 0.47 | 0.34 | 0.15 | -0.00 | 0.00 | 0.04 | 195. |
| 200. | 0.01 | 0.17 | 0.14 | 0.01 | -0.11 | 0.05 | 0.01 | 200. |
| 205. | -0.20 | -0.06 | -0.01 | -0.07 | -0.19 | 0.04 | 0.00 | 205. |
| 210. | -0.42 | -0.23 | -0.10 | -0.12 | -0.14 | 0.03 | 0.01 | 210. |
| 215. | -0.40 | -0.35 | -0.15 | -0.15 | -0.14 | 0.02 | 0.01 | 215. |
| 220. | -0.51 | -0.41 | -0.18 | -0.17 | -0.20 | 0.00 | -0.00 | 220. |
| 225. | -0.63 | -0.43 | -0.20 | -0.20 | -0.22 | -0.01 | -0.02 | 225. |
| 230. | -0.69 | -0.42 | -0.21 | -0.21 | -0.23 | -0.03 | -0.03 | 230. |
| 235. | -0.71 | -0.46 | -0.21 | -0.22 | -0.25 | -0.05 | -0.05 | 235. |
| 240. | -0.70 | -0.38 | -0.20 | -0.22 | -0.26 | -0.06 | -0.07 | 240. |
| 245. | -0.67 | -0.36 | -0.20 | -0.22 | -0.27 | -0.06 | -0.08 | 245. |
| 250. | -0.63 | -0.33 | -0.20 | -0.22 | -0.27 | -0.06 | -0.10 | 250. |
| 255. | -0.61 | -0.32 | -0.19 | -0.21 | -0.27 | -0.07 | -0.11 | 255. |
| 260. | -0.60 | -0.34 | -0.18 | -0.20 | -0.26 | -0.08 | -0.12 | 260. |
| 265. | -0.60 | -0.37 | -0.16 | -0.17 | -0.25 | -0.07 | -0.13 | 265. |
| 270. | -0.59 | -0.37 | -0.13 | -0.15 | -0.23 | -0.05 | -0.14 | 270. |
| 275. | -0.59 | -0.37 | -0.12 | -0.15 | -0.22 | -0.04 | -0.15 | 275. |
| 280. | -0.60 | -0.36 | -0.11 | -0.15 | -0.22 | -0.04 | -0.15 | 280. |
| 285. | -0.61 | -0.35 | -0.11 | -0.15 | -0.21 | -0.04 | -0.15 | 285. |
| 290. | -0.62 | -0.34 | -0.12 | -0.16 | -0.21 | -0.03 | -0.14 | 290. |
| 295. | -0.63 | -0.33 | -0.13 | -0.16 | -0.21 | -0.02 | -0.17 | 295. |
| 300. | -0.64 | -0.32 | -0.14 | -0.16 | -0.22 | 0.00 | -0.18 | 300. |
| 305. | -0.64 | -0.31 | -0.15 | -0.16 | -0.22 | 0.02 | -0.16 | 305. |
| 310. | -0.64 | -0.28 | -0.17 | -0.16 | -0.22 | 0.02 | -0.14 | 310. |
| 315. | -0.64 | -0.24 | -0.18 | -0.16 | -0.22 | 0.02 | -0.15 | 315. |
| 320. | -0.63 | -0.29 | -0.18 | -0.17 | -0.20 | 0.02 | -0.13 | 320. |
| 325. | -0.63 | -0.34 | -0.18 | -0.16 | -0.19 | 0.02 | -0.07 | 325. |
| 330. | -0.63 | -0.35 | -0.18 | -0.16 | -0.17 | 0.03 | 0.03 | 330. |
| 335. | -0.64 | -0.33 | -0.16 | -0.16 | -0.13 | 0.05 | 0.09 | 335. |
| 340. | -0.70 | -0.35 | -0.17 | -0.18 | -0.06 | 0.08 | 0.10 | 340. |
| 345. | -0.72 | -0.43 | -0.26 | -0.20 | -0.10 | 0.09 | 0.12 | 345. |
| 350. | -1.29 | -0.77 | -0.33 | -0.40 | -0.36 | 0.01 | 0.04 | 350. |
| 355. | -1.80 | -1.06 | -0.65 | -0.63 | -0.52 | -0.16 | -0.09 | 355. |

TEXT NOT REPRODUCIBLE

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=900 CNTR NO. 458 TCN= 27. C.A.= 19.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.435 | 1.240 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -2.09 | -1.57 | -0.46 | -0.69 | -0.57 | -0.27 | -0.06 | 0. |
| 5. | -2.64 | -1.92 | -0.32 | -0.87 | -3.68 | -0.31 | -0.04 | 5. |
| 10. | -2.05 | -1.58 | -0.85 | -0.75 | -0.57 | -0.37 | -0.15 | 10. |
| 15. | -1.62 | -1.38 | -0.97 | -0.43 | -9.41 | -0.33 | -0.17 | 15. |
| 20. | -0.97 | -0.91 | -0.71 | -0.38 | -0.19 | -0.25 | -0.13 | 20. |
| 25. | -0.32 | -0.49 | -0.18 | -0.17 | 0.02 | -0.14 | -0.18 | 25. |
| 30. | 0.01 | -0.27 | -0.09 | -0.06 | 0.06 | -0.12 | -0.12 | 30. |
| 35. | 0.11 | -0.21 | -0.10 | -0.04 | 0.07 | -0.14 | -0.13 | 35. |
| 40. | 0.32 | -0.06 | -0.01 | 0.04 | 0.20 | -0.11 | -0.10 | 40. |
| 45. | 0.68 | 0.17 | 0.14 | 0.13 | 0.32 | -0.07 | -0.09 | 45. |
| 50. | 1.09 | 0.33 | 0.19 | 0.15 | 0.39 | -0.09 | -0.11 | 50. |
| 55. | 1.26 | 0.34 | 0.19 | 0.13 | 0.42 | -0.13 | -0.15 | 55. |
| 60. | 1.34 | 0.36 | 0.17 | 0.14 | 0.48 | -0.12 | -0.16 | 60. |
| 65. | 1.40 | 0.43 | 0.21 | 0.20 | 0.55 | -0.11 | -0.14 | 65. |
| 70. | 1.49 | 0.48 | 0.19 | 0.19 | 0.57 | -0.11 | -0.12 | 70. |
| 75. | 1.48 | 0.39 | 0.68 | 0.13 | 0.50 | -0.14 | -0.13 | 75. |
| 80. | 1.30 | 0.32 | 0.02 | 0.10 | 0.46 | -0.13 | -0.13 | 80. |
| 85. | 1.32 | 0.35 | 0.02 | 0.12 | 0.48 | -0.08 | -0.09 | 85. |
| 90. | 1.51 | 0.48 | 0.18 | 0.19 | 0.48 | -0.08 | -0.08 | 90. |
| 95. | 1.69 | 0.60 | 0.28 | 0.28 | 0.47 | -0.11 | -0.08 | 95. |
| 100. | 1.85 | 0.71 | 0.29 | 0.27 | 0.51 | -0.08 | -0.09 | 100. |
| 105. | 1.82 | 0.74 | 0.24 | 0.26 | 0.42 | -3.08 | -0.11 | 105. |
| 110. | 1.68 | 0.59 | 0.06 | 0.05 | 0.30 | -3.12 | -0.11 | 110. |
| 115. | 1.10 | 0.29 | -0.21 | -0.14 | 0.17 | -0.15 | -0.09 | 115. |
| 120. | 0.15 | -0.27 | -0.54 | -0.48 | 0.02 | -0.16 | -0.08 | 120. |
| 125. | -0.78 | -0.85 | -0.89 | -0.57 | -0.08 | -0.13 | -0.05 | 125. |
| 130. | -0.71 | -0.82 | -0.75 | -0.52 | -0.07 | -0.09 | -0.02 | 130. |
| 135. | -0.84 | -0.96 | -0.35 | -0.30 | 0.03 | -3.24 | -0.02 | 135. |
| 140. | 0.43 | 0.03 | -0.05 | -0.12 | 0.09 | -0.04 | -0.04 | 140. |
| 145. | 0.68 | 0.27 | 0.09 | -0.08 | 0.12 | -0.02 | -0.04 | 145. |
| 150. | 0.79 | 0.41 | 0.19 | 0.07 | 0.13 | 0.04 | -0.02 | 150. |
| 155. | 0.84 | 0.54 | 0.29 | 0.14 | 0.15 | 0.08 | 0.02 | 155. |
| 160. | 0.97 | 0.69 | 0.40 | 0.25 | 0.21 | 0.14 | 0.06 | 160. |
| 165. | 1.15 | 0.98 | 0.56 | 0.38 | 0.27 | 0.22 | 0.10 | 165. |
| 170. | 1.35 | 1.12 | 0.73 | 0.51 | 0.34 | 0.28 | 0.14 | 170. |
| 175. | 1.47 | 1.27 | 0.83 | 0.60 | 0.38 | 0.32 | 0.16 | 175. |
| 180. | 1.44 | 1.29 | 0.87 | 0.63 | 0.36 | 0.32 | 0.16 | 180. |
| 185. | 1.26 | 1.14 | 0.80 | 0.57 | 0.29 | 0.30 | 0.15 | 185. |
| 190. | 0.99 | 0.93 | 0.69 | 0.49 | 0.21 | 0.27 | 0.13 | 190. |
| 195. | 0.67 | 0.71 | 0.55 | 0.40 | 0.11 | 0.22 | 0.12 | 195. |
| 200. | 0.32 | 0.50 | 0.41 | 0.29 | -0.00 | 0.16 | 0.09 | 200. |
| 205. | -0.01 | 0.32 | 0.28 | 0.17 | -0.10 | 0.10 | 0.07 | 205. |
| 210. | -0.24 | 0.17 | 0.17 | 0.09 | -0.14 | 0.09 | 0.07 | 210. |
| 215. | -0.37 | 0.07 | 0.10 | 0.06 | -0.16 | 0.10 | 0.08 | 215. |
| 220. | -0.48 | 0.01 | 0.05 | 0.05 | -0.18 | 0.11 | 0.09 | 220. |
| 225. | -0.56 | -0.04 | 0.03 | 0.04 | -0.19 | 0.12 | 0.10 | 225. |
| 230. | -0.59 | -0.08 | 0.00 | 0.01 | -0.20 | 0.11 | 0.09 | 230. |
| 235. | -0.61 | -0.12 | -0.02 | -0.02 | -0.22 | 0.10 | 0.08 | 235. |
| 240. | -0.69 | -0.16 | -0.04 | -0.03 | -0.24 | 0.08 | 0.07 | 240. |
| 245. | -0.78 | -0.19 | -0.06 | -0.04 | -0.25 | 0.07 | 0.07 | 245. |
| 250. | -0.80 | -0.20 | -0.07 | -0.05 | -0.26 | 0.07 | 0.07 | 250. |
| 255. | -0.78 | -0.20 | -0.08 | -0.04 | -0.26 | 0.08 | 0.08 | 255. |
| 260. | -0.76 | -0.19 | -0.08 | -0.04 | -0.25 | 0.08 | 0.08 | 260. |
| 265. | -0.76 | -0.19 | -0.08 | -0.03 | -0.24 | 0.07 | 0.07 | 265. |
| 270. | -0.75 | -0.18 | -0.08 | -0.02 | -0.24 | 0.07 | 0.07 | 270. |
| 275. | -0.75 | -0.18 | -0.08 | -0.03 | -0.25 | 0.06 | 0.07 | 275. |
| 280. | -0.75 | -0.18 | -0.08 | -0.04 | -0.25 | 0.05 | 0.06 | 280. |
| 285. | -0.76 | -0.18 | -0.08 | -0.05 | -0.25 | 0.04 | 0.06 | 285. |
| 290. | -0.76 | -0.18 | -0.08 | -0.05 | -0.25 | 0.04 | 0.06 | 290. |
| 295. | -0.77 | -0.18 | -0.08 | -0.05 | -0.25 | 0.05 | 0.06 | 295. |
| 300. | -0.77 | -0.18 | -0.08 | -0.04 | -0.24 | 0.06 | 0.06 | 300. |
| 305. | -0.76 | -0.18 | -0.07 | -0.04 | -0.22 | 0.07 | 0.06 | 305. |
| 310. | -0.76 | -0.18 | -0.06 | -0.03 | -0.20 | 0.06 | 0.07 | 310. |
| 315. | -0.75 | -0.19 | -0.05 | -0.01 | -0.18 | 0.04 | 0.06 | 315. |
| 320. | -0.74 | -0.20 | -0.04 | -0.00 | -0.16 | 0.04 | 0.07 | 320. |
| 325. | -0.72 | -0.20 | -0.04 | 0.00 | -0.16 | 0.07 | 0.06 | 325. |
| 330. | -0.68 | -0.20 | -0.03 | 0.01 | -0.19 | 0.05 | 0.05 | 330. |
| 335. | -0.60 | -0.19 | -0.02 | -0.00 | -0.20 | 0.04 | 0.05 | 335. |
| 340. | -0.64 | -0.18 | -0.02 | 0.01 | -0.22 | 0.03 | 0.04 | 340. |
| 345. | -0.91 | -0.17 | -0.14 | -0.06 | -0.28 | -0.00 | 0.00 | 345. |
| 350. | -1.32 | -0.00 | -0.30 | -0.27 | -0.35 | -0.07 | -0.04 | 350. |
| 355. | -1.04 | -0.00 | -0.11 | -0.43 | -0.41 | -0.17 | -0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST•500 CNTR NO. 458 ICN• 27. C.R.• 39.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 3.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.153 | 10.430 | DEG. |
| 0. | -0.83 | -0.57 | -0.83 | -0.26 | -0.29 | -0.15 | -0.00 | 0. |
| 5. | -1.11 | -0.89 | -0.84 | -0.41 | -0.20 | -0.15 | -0.14 | 5. |
| 10. | -1.15 | -0.89 | -0.85 | -0.46 | -0.29 | -0.12 | -0.07 | 10. |
| 15. | -0.96 | -0.90 | -0.83 | -0.44 | -0.24 | -0.19 | -0.10 | 15. |
| 20. | -0.66 | -0.57 | -0.59 | -0.32 | -0.16 | -0.12 | -0.11 | 20. |
| 25. | -0.08 | -0.21 | -0.30 | -0.14 | 0.02 | -0.13 | -0.08 | 25. |
| 30. | 0.47 | 0.20 | 0.06 | 0.02 | 0.19 | -0.13 | -0.02 | 30. |
| 35. | 1.09 | 0.80 | 0.39 | 0.16 | 0.32 | 0.01 | 0.02 | 35. |
| 40. | 1.47 | 0.94 | 0.69 | 0.27 | 0.44 | 0.06 | 0.04 | 40. |
| 45. | 1.85 | 1.22 | 0.96 | 0.38 | 0.55 | 0.22 | 0.03 | 45. |
| 50. | 2.35 | 1.47 | 1.29 | 0.72 | 0.64 | 0.35 | 0.02 | 50. |
| 55. | 2.33 | 1.55 | 1.45 | 0.95 | 0.72 | 0.36 | 0.03 | 55. |
| 60. | 1.94 | 1.43 | 1.41 | 0.64 | 0.76 | 0.03 | 0.01 | 60. |
| 65. | 1.55 | 1.20 | 1.49 | 0.27 | 0.73 | -0.03 | -0.01 | 65. |
| 70. | 1.29 | 0.97 | 2.00 | 0.38 | 0.76 | -0.09 | -0.02 | 70. |
| 75. | 1.15 | 0.88 | 2.80 | -0.05 | 0.81 | -0.05 | -0.01 | 75. |
| 80. | 1.14 | 0.80 | 3.25 | -0.14 | 0.89 | -0.12 | -0.06 | 80. |
| 85. | 1.12 | 0.78 | 2.84 | -0.16 | 0.34 | -0.19 | -0.11 | 85. |
| 90. | 1.06 | 0.68 | 2.21 | -0.12 | 0.34 | -0.24 | -0.05 | 90. |
| 95. | 1.43 | 1.15 | 2.73 | -0.03 | 0.91 | -0.21 | -0.11 | 95. |
| 100. | 1.22 | 1.21 | 3.16 | -0.06 | -0.38 | -0.59 | -0.16 | 100. |
| 105. | -0.17 | -0.34 | 1.58 | -0.48 | -1.63 | -0.46 | -0.14 | 105. |
| 110. | -1.65 | -1.35 | -1.73 | -0.64 | -2.26 | -0.23 | -0.09 | 110. |
| 115. | -1.88 | -1.40 | -2.56 | -0.79 | -1.55 | -0.23 | -0.11 | 115. |
| 120. | -2.12 | -1.81 | -3.42 | -1.20 | -0.32 | -0.33 | -0.13 | 120. |
| 125. | -2.47 | -2.00 | -4.09 | -1.51 | 0.03 | -0.35 | -0.10 | 125. |
| 130. | -2.93 | -2.19 | -3.11 | -1.56 | -0.15 | -0.36 | -0.09 | 130. |
| 135. | -2.21 | -1.73 | -0.03 | -1.19 | -0.18 | -0.34 | -0.11 | 135. |
| 140. | -1.71 | -1.05 | -0.65 | -0.77 | -0.38 | -0.28 | -0.12 | 140. |
| 145. | -1.21 | -0.53 | 0.17 | -0.44 | 0.01 | -0.24 | -0.11 | 145. |
| 150. | -0.88 | -0.27 | 0.04 | -0.24 | 0.07 | -0.21 | -0.10 | 150. |
| 155. | -0.57 | -0.24 | 0.11 | -0.13 | 0.09 | -0.17 | -0.08 | 155. |
| 160. | -0.38 | -0.26 | 0.17 | -0.22 | 0.12 | -0.11 | -0.07 | 160. |
| 165. | -0.12 | -0.02 | 0.22 | 0.09 | 0.16 | -0.04 | -0.05 | 165. |
| 170. | 0.38 | 0.36 | 0.30 | 0.18 | 0.22 | 0.02 | -0.02 | 170. |
| 175. | 0.82 | 0.66 | 0.36 | 0.28 | 0.36 | 0.17 | 0.00 | 175. |
| 180. | 1.12 | 0.79 | 0.42 | 0.38 | 0.38 | 0.12 | 0.02 | 180. |
| 185. | 1.03 | 0.77 | 0.47 | 0.45 | 0.40 | 0.16 | 0.03 | 185. |
| 190. | 0.81 | 0.69 | 0.47 | 0.49 | 0.41 | 0.18 | 0.05 | 190. |
| 195. | 0.66 | 0.63 | 0.60 | 0.49 | 0.23 | 0.19 | 0.05 | 195. |
| 200. | 0.56 | 0.53 | 0.50 | 0.46 | 0.16 | 0.19 | 0.04 | 200. |
| 205. | 0.46 | 0.40 | 0.17 | 0.42 | 0.08 | 0.17 | 0.03 | 205. |
| 210. | 0.33 | 0.25 | 0.01 | 0.36 | 0.01 | 0.14 | 0.02 | 210. |
| 215. | 0.18 | 0.12 | -0.13 | 0.31 | -0.05 | 0.12 | -0.00 | 215. |
| 220. | 0.03 | 0.02 | -0.21 | 0.27 | -0.09 | 0.12 | -0.02 | 220. |
| 225. | -0.08 | -0.04 | -0.26 | 0.25 | -0.10 | 0.13 | 0.02 | 225. |
| 230. | -0.16 | -0.08 | -0.35 | 0.24 | -0.09 | 0.15 | 0.04 | 230. |
| 235. | -0.20 | -0.09 | -0.32 | 0.23 | -0.08 | 0.18 | 0.06 | 235. |
| 240. | -0.20 | -0.09 | -0.31 | 0.22 | -0.08 | 0.19 | 0.08 | 240. |
| 245. | -0.19 | -0.08 | -0.34 | 0.21 | -0.08 | 0.20 | 0.09 | 245. |
| 250. | -0.19 | -0.07 | -0.34 | 0.19 | -0.08 | 0.21 | 0.10 | 250. |
| 255. | -0.19 | -0.08 | -0.36 | 0.18 | -0.10 | 0.23 | 0.09 | 255. |
| 260. | -0.20 | -0.12 | -0.38 | 0.18 | -0.13 | 0.19 | 0.08 | 260. |
| 265. | -0.22 | -0.16 | -0.41 | 0.19 | -0.15 | 0.15 | 0.07 | 265. |
| 270. | -0.23 | -0.18 | -0.44 | 0.19 | -0.17 | 0.14 | 0.07 | 270. |
| 275. | -0.25 | -0.18 | -0.46 | 0.20 | -0.18 | 0.17 | 0.06 | 275. |
| 280. | -0.27 | -0.17 | -0.47 | 0.21 | -0.17 | 0.16 | 0.05 | 280. |
| 285. | -0.28 | -0.15 | -0.47 | 0.21 | -0.15 | 0.16 | 0.06 | 285. |
| 290. | -0.26 | -0.14 | -0.47 | 0.21 | -0.14 | 0.17 | 0.07 | 290. |
| 295. | -0.23 | -0.13 | -0.48 | 0.21 | -0.14 | 0.17 | 0.07 | 295. |
| 300. | -0.20 | -0.12 | -0.48 | 0.20 | -0.14 | 0.16 | 0.07 | 300. |
| 305. | -0.16 | -0.12 | -0.49 | 0.19 | -0.12 | 0.16 | 0.07 | 305. |
| 310. | -0.13 | -0.11 | -0.51 | 0.17 | -0.10 | 0.16 | 0.08 | 310. |
| 315. | -0.10 | -0.12 | -0.52 | 0.14 | -0.10 | 0.16 | 0.09 | 315. |
| 320. | -0.27 | -0.20 | -0.55 | 0.08 | -0.13 | 0.15 | 0.09 | 320. |
| 325. | -0.39 | -0.32 | -0.63 | 0.04 | -0.16 | 0.12 | 0.08 | 325. |
| 330. | -0.43 | -0.39 | -0.67 | 0.02 | -0.17 | 0.09 | 0.07 | 330. |
| 335. | -0.32 | -0.36 | -0.64 | 0.04 | -0.16 | 0.07 | 0.05 | 335. |
| 340. | -0.24 | -0.18 | -0.44 | 0.09 | -0.11 | 0.07 | 0.05 | 340. |
| 345. | 0.38 | 0.12 | -0.19 | 0.21 | -0.01 | 0.11 | 0.07 | 345. |
| 350. | 0.57 | 0.36 | -0.05 | 0.29 | 0.05 | 0.15 | 0.08 | 350. |
| 355. | -0.32 | 0.02 | -0.38 | 0.09 | -0.07 | 0.10 | 0.05 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=SUC CNTR NO. 458 TCN= 27. C.R.= 39.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.20 | 0.38 | 0.01 | 0.05 | 0.07 | -0.01 | 0.02 | 0. |
| 5. | -0.55 | -0.03 | -0.37 | -0.10 | -0.39 | -0.38 | 0.00 | 5. |
| 10. | -0.91 | -0.50 | -0.65 | -0.31 | -0.24 | -0.16 | -0.01 | 10. |
| 15. | -0.70 | -0.53 | -0.64 | -0.43 | -0.28 | -0.21 | 0.00 | 15. |
| 20. | -0.43 | -0.35 | -0.59 | -0.33 | -0.24 | -0.19 | 0.00 | 20. |
| 25. | -0.11 | -0.05 | -0.43 | -0.17 | -0.09 | -0.09 | 0.04 | 25. |
| 30. | 0.47 | 0.31 | -0.12 | 0.04 | 0.07 | 0.02 | 0.08 | 30. |
| 35. | 1.00 | 0.62 | 0.19 | 0.16 | 0.21 | 0.11 | 0.11 | 35. |
| 40. | 1.43 | 0.78 | 0.44 | 0.26 | 0.35 | 0.21 | 0.14 | 40. |
| 45. | 1.74 | 0.76 | 0.58 | 0.41 | 0.50 | 0.31 | 0.16 | 45. |
| 50. | 1.91 | 0.66 | 0.80 | 0.93 | 0.71 | 0.37 | 0.15 | 50. |
| 55. | 1.95 | 0.68 | 1.11 | 1.40 | 0.91 | 0.32 | 0.10 | 55. |
| 60. | 1.78 | 0.64 | 1.16 | 1.52 | 1.36 | 0.23 | 0.06 | 60. |
| 65. | 1.52 | 0.35 | 0.93 | 1.16 | 1.75 | 0.19 | 0.05 | 65. |
| 70. | 1.46 | -0.04 | 0.82 | 0.69 | 1.33 | 0.03 | -0.05 | 70. |
| 75. | 1.43 | -0.31 | 0.82 | 0.62 | 0.69 | -0.16 | -0.13 | 75. |
| 80. | 0.41 | -0.51 | 0.03 | 0.46 | 0.19 | -0.66 | -0.00 | 80. |
| 85. | 0.42 | -0.75 | -0.42 | 0.53 | 0.17 | 0.25 | -0.06 | 85. |
| 90. | 0.73 | -1.34 | -0.57 | 0.51 | -0.03 | -1.05 | -0.12 | 90. |
| 95. | -0.17 | -1.77 | -0.96 | 0.16 | -0.49 | -1.01 | -0.12 | 95. |
| 100. | -0.75 | -2.04 | -1.12 | -0.19 | -0.82 | -0.71 | -0.23 | 100. |
| 105. | -0.92 | -2.20 | -1.15 | -0.55 | -0.99 | -0.89 | -0.35 | 105. |
| 110. | -1.05 | -2.34 | -1.13 | -0.87 | -1.10 | -0.97 | -0.38 | 110. |
| 115. | -1.33 | -2.51 | -1.08 | -1.08 | -1.23 | 0.51 | -0.27 | 115. |
| 120. | -1.57 | -2.63 | -1.10 | -1.16 | -1.47 | -0.72 | -0.06 | 120. |
| 125. | -1.68 | -2.66 | -1.15 | -0.98 | -1.50 | -1.32 | 0.21 | 125. |
| 130. | -1.66 | -2.58 | -1.28 | -1.04 | -2.72 | -0.49 | 0.26 | 130. |
| 135. | -1.58 | -2.47 | -1.32 | -1.64 | -4.22 | 0.29 | 0.14 | 135. |
| 140. | -1.67 | -2.51 | -1.42 | -2.41 | -2.23 | 0.66 | 0.03 | 140. |
| 145. | -1.78 | -2.49 | -2.11 | -2.02 | -0.08 | 3.17 | -0.01 | 145. |
| 150. | -1.71 | -2.24 | -2.13 | -1.08 | -0.16 | -0.36 | -0.02 | 150. |
| 155. | -1.49 | -1.75 | -1.69 | -0.85 | -0.39 | -0.39 | -0.01 | 155. |
| 160. | -1.23 | -1.07 | -1.31 | -0.86 | -0.42 | -0.01 | 0.00 | 160. |
| 165. | -0.99 | -0.96 | -0.97 | -0.70 | -0.29 | 0.03 | -0.01 | 165. |
| 170. | -0.72 | -0.26 | -0.70 | -0.66 | -0.14 | 0.05 | -0.01 | 170. |
| 175. | -0.44 | -0.07 | -0.47 | -0.55 | -0.33 | 0.39 | 0.01 | 175. |
| 180. | -0.17 | 0.18 | -0.22 | -0.34 | 0.07 | 0.14 | 0.02 | 180. |
| 185. | 0.05 | 0.46 | 0.01 | -0.19 | 0.15 | 0.19 | 0.03 | 185. |
| 190. | 0.23 | 0.70 | 0.21 | -0.05 | 0.22 | 0.21 | 0.03 | 190. |
| 195. | 0.41 | 0.87 | 0.36 | 0.07 | 0.27 | 0.22 | 0.03 | 195. |
| 200. | 0.52 | 0.98 | 0.47 | 0.15 | 0.30 | 0.22 | 0.02 | 200. |
| 205. | 0.53 | 1.03 | 0.51 | 0.20 | 0.32 | 0.20 | 0.01 | 205. |
| 210. | 0.48 | 1.03 | 0.52 | 0.22 | 0.32 | 0.16 | -0.00 | 210. |
| 215. | 0.39 | 1.00 | 0.49 | 0.22 | 0.29 | 0.15 | -0.01 | 215. |
| 220. | 0.27 | 0.94 | 0.47 | 0.22 | 0.26 | 0.14 | -0.02 | 220. |
| 225. | 0.17 | 0.89 | 0.44 | 0.23 | 0.24 | 0.12 | -0.02 | 225. |
| 230. | 0.11 | 0.86 | 0.47 | 0.25 | 0.27 | 0.12 | -0.02 | 230. |
| 235. | 0.09 | 0.86 | 0.51 | 0.27 | 0.31 | 0.14 | -0.01 | 235. |
| 240. | 0.10 | 0.88 | 0.56 | 0.28 | 0.34 | 0.15 | 0.00 | 240. |
| 245. | 0.10 | 0.91 | 0.60 | 0.32 | 0.36 | 0.17 | 0.01 | 245. |
| 250. | 0.11 | 0.95 | 0.63 | 0.31 | 0.37 | 0.18 | 0.01 | 250. |
| 255. | 0.12 | 0.99 | 0.66 | 0.33 | 0.38 | 0.18 | 0.01 | 255. |
| 260. | 0.13 | 1.01 | 0.68 | 0.34 | 0.38 | 0.17 | 0.01 | 260. |
| 265. | 0.15 | 1.02 | 0.69 | 0.36 | 0.38 | 0.16 | 0.01 | 265. |
| 270. | 0.15 | 1.02 | 0.70 | 0.37 | 0.37 | 0.16 | 0.01 | 270. |
| 275. | 0.16 | 1.03 | 0.70 | 0.39 | 0.37 | 0.16 | 0.01 | 275. |
| 280. | 0.17 | 1.04 | 0.71 | 0.40 | 0.38 | 0.16 | 0.00 | 280. |
| 285. | 0.18 | 1.05 | 0.71 | 0.40 | 0.38 | 0.17 | 0.00 | 285. |
| 290. | 0.21 | 1.06 | 0.71 | 0.40 | 0.38 | 0.17 | 0.00 | 290. |
| 295. | 0.24 | 1.06 | 0.71 | 0.40 | 0.38 | 0.16 | 0.00 | 295. |
| 300. | 0.27 | 1.06 | 0.73 | 0.39 | 0.37 | 0.16 | 0.00 | 300. |
| 305. | 0.29 | 1.02 | 0.67 | 0.38 | 0.37 | 0.15 | 0.01 | 305. |
| 310. | 0.29 | 0.98 | 0.63 | 0.37 | 0.36 | 0.15 | 0.01 | 310. |
| 315. | 0.30 | 0.97 | 0.60 | 0.36 | 0.35 | 0.16 | 0.01 | 315. |
| 320. | 0.35 | 1.01 | 0.59 | 0.37 | 0.36 | 0.16 | 0.02 | 320. |
| 325. | 0.43 | 1.02 | 0.58 | 0.38 | 0.36 | 0.16 | 0.02 | 325. |
| 330. | 0.39 | 0.95 | 0.53 | 0.35 | 0.33 | 0.14 | 0.02 | 330. |
| 335. | 0.12 | 0.70 | 0.42 | 0.25 | 0.24 | 0.10 | 0.02 | 335. |
| 340. | -0.18 | 0.44 | 0.21 | 0.14 | 0.15 | 0.03 | 0.01 | 340. |
| 345. | -0.24 | 0.17 | 0.07 | 0.09 | 0.09 | -0.02 | 0.01 | 345. |
| 350. | 0.12 | 0.51 | 0.23 | 0.18 | 0.16 | -0.01 | 0.01 | 350. |
| 355. | 0.37 | 0.55 | 0.31 | 0.22 | 0.16 | 0.01 | -0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-990 CNTR NO. 458 TCN= 27. C.R.= 39.0

DIFFERENTIAL PRESSURES

SPAN STATION 149.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.04C | 1.95C | 2.990 | 4.590 | 7.150 | 10.40C | DEG. |
| 0. | -3.66 | -0.65 | -0.24 | 0.06 | 0.01 | -3.05 | 0.05 | 0. |
| 5. | -3.92 | -C.72 | -0.24 | 0.01 | 0.02 | -3.14 | 0.07 | 5. |
| 10. | -0.56 | -0.8C | -0.39 | -0.11 | -0.03 | -3.13 | 0.37 | 10. |
| 15. | -0.48 | -C.90 | -3.49 | -C.21 | -0.1C | -3.18 | 0.36 | 15. |
| 20. | -0.41 | -0.95 | -3.47 | -3.27 | -0.09 | -0.22 | C.01 | 20. |
| 25. | -0.16 | -C.76 | -0.32 | -C.13 | C.37 | -0.17 | 0.C1 | 25. |
| 30. | 0.43 | -0.45 | 0.13 | 0.15 | 0.32 | -3.05 | 0.68 | 3C. |
| 35. | 1.07 | -3.2C | 0.56 | 0.32 | 0.60 | 3.03 | C.12 | 35. |
| 40. | 1.53 | 0.19 | 0.06 | C.33 | 0.86 | 0.04 | 0.13 | 4C. |
| 45. | 1.85 | 0.94 | 0.98 | 0.59 | 1.16 | 0.11 | 0.16 | 45. |
| 50. | 2.07 | 1.63 | 1.C3 | 1.50 | 1.42 | 0.12 | 0.13 | 50. |
| 55. | 2.16 | 1.94 | 1.10 | 1.69 | 2.24 | -0.37 | 0.06 | 55. |
| 60. | 1.97 | 1.88 | 1.C2 | 1.77 | 2.42 | -0.42 | -0.02 | 6C. |
| 65. | 1.66 | 1.55 | 0.79 | C.56 | 1.56 | -3.47 | -C.11 | 65. |
| 70. | 1.54 | 1.38 | 0.85 | 0.55 | 0.95 | 0.13 | -0.21 | 7C. |
| 75. | 1.1C | 1.15 | 0.2C | -C.06 | 0.68 | -C.04 | -C.25 | 75. |
| 80. | -0.05 | C.75 | -0.24 | -0.57 | 0.33 | -0.85 | -0.63 | 8C. |
| 85. | 0.36 | 1.07 | 0.C8 | -0.15 | 0.16 | -0.48 | -0.02 | 85. |
| 90. | -0.46 | 0.79 | -0.65 | -0.33 | -0.27 | -3.43 | -0.2: | 9C. |
| 95. | -0.93 | 0.20 | -3.92 | -0.71 | -0.47 | -3.73 | -0.39 | 95. |
| 100. | -1.09 | -0.06 | -1.06 | -C.89 | -0.61 | -1.12 | -0.39 | 10C. |
| 105. | -1.32 | -0.46 | -1.19 | -C.99 | -0.79 | -1.11 | -C.24 | 105. |
| 110. | -1.67 | -C.92 | -1.28 | -1.21 | -9.88 | -0.17 | -0.22 | 11C. |
| 115. | -2.02 | -1.37 | -1.64 | -1.53 | -1.04 | 1.99 | -0.27 | 115. |
| 120. | -2.23 | -1.60 | -1.94 | -1.74 | -1.22 | 2.79 | -0.49 | 12C. |
| 125. | -2.26 | -1.74 | -1.96 | -1.73 | -1.12 | 1.28 | -C.94 | 125. |
| 130. | -2.11 | -1.58 | -1.88 | -1.56 | -0.93 | -3.68 | -0.32 | 13C. |
| 135. | -1.91 | -1.31 | -1.60 | -1.44 | -1.02 | -1.31 | 0.40 | 135. |
| 140. | -1.79 | -1.43 | -1.58 | -2.07 | -3.12 | -0.24 | 0.39 | 14C. |
| 145. | -1.93 | -1.94 | -1.79 | -3.26 | -1.68 | 3.48 | 0.13 | 145. |
| 150. | -2.11 | -2.31 | -1.85 | -2.33 | 0.02 | -3.16 | -0.05 | 15C. |
| 155. | -1.93 | -2.29 | -1.46 | -1.14 | -0.06 | -0.37 | -0.C8 | 155. |
| 160. | -1.48 | -1.97 | -1.21 | -C.78 | -0.22 | -0.34 | -C.07 | 16C. |
| 165. | -1.56 | -1.45 | -0.92 | -C.66 | -0.24 | -3.23 | -0.05 | 165. |
| 170. | -1.17 | -1.02 | -0.61 | -0.48 | -0.17 | -0.18 | -0.04 | 17C. |
| 175. | -3.77 | -0.66 | -0.36 | -0.29 | -0.78 | -3.13 | -0.83 | 175. |
| 180. | -0.42 | -3.35 | -0.15 | -0.10 | 0.02 | -3.36 | -3.31 | 18C. |
| 185. | -2.09 | -3.06 | 3.37 | 0.08 | C.1C | -3.03 | C.31 | 185. |
| 190. | 3.23 | 0.18 | 0.26 | 0.23 | 0.13 | 0.95 | 0.62 | 19C. |
| 195. | 0.48 | 0.39 | 0.41 | C.33 | 0.15 | 0.98 | 0.62 | 195. |
| 200. | 0.63 | 0.53 | 0.52 | C.41 | 0.14 | 0.17 | 0.63 | 20C. |
| 205. | 0.7C | 0.57 | 0.58 | 0.44 | 0.13 | 0.13 | 0.62 | 205. |
| 210. | 0.7C | 0.56 | 0.60 | 0.45 | 0.10 | 0.17 | 0.61 | 210. |
| 215. | 0.64 | 0.52 | 0.58 | C.45 | 0.08 | 0.14 | 0.61 | 215. |
| 220. | 0.54 | C.47 | 0.54 | 0.44 | 0.05 | 0.09 | C.61 | 22C. |
| 225. | 0.45 | C.43 | 0.51 | 0.43 | 0.02 | 0.09 | 0.01 | 225. |
| 230. | 0.41 | 0.40 | 0.49 | 0.45 | -0.03 | 0.09 | C.01 | 23C. |
| 235. | 0.60 | 0.41 | 0.50 | 0.49 | -0.01 | 0.10 | 0.02 | 235. |
| 240. | 0.4C | 0.45 | 0.54 | 0.53 | 0.71 | 0.11 | 0.04 | 240. |
| 245. | 0.41 | 0.49 | 0.57 | 0.55 | 0.03 | 0.14 | 0.06 | 245. |
| 250. | 0.44 | 0.53 | 0.59 | 0.57 | 0.04 | 0.16 | 0.08 | 250. |
| 255. | 0.48 | 0.54 | 0.60 | 0.58 | 0.04 | 0.17 | 0.08 | 255. |
| 260. | 0.51 | 0.55 | 0.60 | 0.58 | 0.04 | 0.17 | 0.07 | 260. |
| 265. | 0.54 | 0.56 | 0.61 | 0.59 | 0.04 | 0.17 | 0.07 | 265. |
| 270. | 0.57 | 0.57 | 0.62 | 0.61 | C.03 | 0.17 | 0.06 | 270. |
| 275. | 0.59 | 0.59 | 0.64 | 0.63 | 0.04 | 0.17 | 0.07 | 275. |
| 280. | 0.62 | C.60 | 0.67 | 0.65 | 0.04 | 0.17 | 0.07 | 280. |
| 285. | 0.64 | 0.62 | 0.69 | 0.67 | 0.05 | 0.17 | 0.07 | 285. |
| 290. | 0.7C | 0.65 | 0.71 | C.69 | 0.06 | 0.17 | C.06 | 290. |
| 295. | 0.74 | 0.67 | 0.74 | 0.7C | 0.07 | 0.17 | 0.06 | 295. |
| 300. | 0.76 | 0.67 | 0.75 | C.71 | 0.07 | 0.17 | 0.07 | 300. |
| 305. | 0.78 | C.63 | 0.74 | 0.7C | 0.08 | 0.17 | C.08 | 305. |
| 310. | 0.78 | 0.58 | 0.69 | 0.68 | 0.09 | 0.17 | 0.08 | 310. |
| 315. | 0.76 | 0.55 | 0.65 | 0.67 | 0.11 | 0.16 | C.08 | 315. |
| 320. | 0.73 | 0.52 | 0.66 | C.70 | 0.12 | 0.16 | 0.09 | 320. |
| 325. | 0.77 | C.54 | 0.70 | 0.7. | 0.14 | 0.18 | 0.11 | 325. |
| 330. | 0.76 | 0.56 | 0.70 | 0.69 | 0.14 | 0.18 | 0.12 | 330. |
| 335. | 0.60 | C.45 | 0.62 | 0.59 | 0.11 | 0.14 | C.11 | 335. |
| 340. | 0.21 | 0.06 | 0.41 | 0.38 | 0.02 | 0.08 | C.09 | 340. |
| 345. | -3.28 | -0.34 | 0.00 | 0.23 | -0.00 | 0.00 | 0.06 | 345. |
| 350. | -3.90 | -0.51 | -0.C8 | C.16 | -0.07 | -3.05 | C.04 | 35C. |
| 355. | -0.93 | -0.90 | -0.10 | 0.15 | -0.09 | -0.07 | 0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-500 CNTR NO. 458 TC4= 27. C.R.= 39.5

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.993 | 2.990 | 4.550 | 7.159 | 10.480 | DEG. |
| 0. | -1.97 | -0.52 | -3.74 | -0.26 | -0.13 | -0.02 | -0.04 | 0. |
| 5. | -3.31 | -0.11 | -0.59 | -0.11 | -0.05 | -0.05 | -0.03 | 5. |
| 10. | -3.26 | -0.07 | -0.45 | -0.11 | 0.00 | -0.04 | -0.08 | 10. |
| 15. | -0.55 | -0.29 | -0.06 | -0.29 | -0.10 | -0.17 | -0.13 | 15. |
| 20. | -0.66 | -0.42 | -0.83 | -0.44 | -0.15 | -0.25 | -0.14 | 20. |
| 25. | -0.44 | -0.43 | -0.83 | -0.41 | -0.04 | -0.22 | -0.11 | 25. |
| 30. | 0.14 | -0.01 | -0.57 | -0.16 | 0.14 | -0.14 | -0.06 | 30. |
| 35. | 0.78 | 0.52 | -0.14 | 0.14 | 0.30 | -0.06 | -0.04 | 35. |
| 40. | 1.39 | 0.81 | 0.54 | 0.31 | 0.44 | -0.02 | -0.00 | 40. |
| 45. | 1.84 | 1.17 | 1.30 | 1.23 | 0.75 | -0.06 | -0.02 | 45. |
| 50. | 2.12 | 1.73 | 1.67 | 2.33 | 1.23 | -0.24 | -0.11 | 50. |
| 55. | 2.18 | 2.23 | 1.74 | 1.72 | 1.63 | -0.53 | -0.20 | 55. |
| 60. | 2.18 | 2.28 | 1.63 | 0.89 | 1.47 | -0.63 | -0.27 | 60. |
| 65. | 2.12 | 2.12 | 1.48 | 0.53 | 0.96 | -0.87 | -0.27 | 65. |
| 70. | 1.78 | 0.95 | 1.35 | 0.34 | 0.55 | -1.27 | -0.13 | 70. |
| 75. | -0.71 | -0.42 | 0.89 | -0.54 | 0.05 | -0.63 | 0.13 | 75. |
| 80. | -0.22 | -0.57 | 0.87 | -0.73 | -0.31 | -0.13 | 0.23 | 80. |
| 85. | -0.35 | -0.26 | 0.91 | -0.45 | 0.02 | -0.16 | -0.25 | 85. |
| 90. | -0.94 | -0.94 | 0.65 | -0.64 | -0.17 | -0.46 | -0.06 | 90. |
| 95. | -1.17 | -1.22 | 0.38 | -0.82 | -0.37 | -0.33 | 0.11 | 95. |
| 100. | -1.29 | -1.27 | 0.17 | -0.85 | -0.47 | 0.58 | 0.61 | 100. |
| 105. | -1.64 | -1.38 | -0.06 | -0.87 | -0.40 | 0.49 | 0.41 | 105. |
| 110. | -2.99 | -1.62 | -0.36 | -1.00 | -0.86 | 0.59 | 0.53 | 110. |
| 115. | -2.90 | -2.07 | -0.64 | -1.17 | -1.13 | 1.00 | 0.77 | 115. |
| 120. | -2.75 | -2.93 | -0.93 | -1.32 | -1.46 | 0.92 | -0.78 | 120. |
| 125. | -2.77 | -2.65 | -1.06 | -1.42 | -1.45 | -0.87 | -0.41 | 125. |
| 130. | -2.91 | -2.42 | -0.86 | -1.38 | -1.38 | -1.61 | -0.20 | 130. |
| 135. | -2.18 | -2.07 | -0.56 | -1.23 | -1.37 | -2.14 | 0.22 | 135. |
| 140. | -1.94 | -1.72 | -0.41 | -1.04 | -1.07 | -0.87 | 0.28 | 140. |
| 145. | -1.99 | -1.51 | -0.61 | -1.00 | -2.72 | 0.39 | 0.17 | 145. |
| 150. | -2.08 | -1.67 | -1.22 | -2.56 | -0.92 | 0.10 | -0.04 | 150. |
| 155. | -2.12 | -1.87 | -1.71 | -1.90 | -0.18 | -0.43 | -0.07 | 155. |
| 160. | -1.94 | -1.87 | -1.86 | -0.80 | -0.17 | -0.63 | -0.07 | 160. |
| 165. | -1.64 | -1.57 | -1.55 | -0.54 | -0.17 | -0.45 | -0.25 | 165. |
| 170. | -1.26 | -1.10 | -1.23 | -0.44 | -0.13 | -0.27 | -0.04 | 170. |
| 175. | -0.85 | -0.66 | -0.87 | -0.31 | -0.06 | -0.19 | -0.52 | 175. |
| 180. | -0.44 | -0.35 | -0.58 | -0.17 | 0.22 | -0.12 | 0.01 | 180. |
| 185. | -0.36 | -0.07 | -0.37 | -0.32 | 0.11 | -0.06 | 0.03 | 185. |
| 190. | 0.26 | 0.16 | -0.20 | 0.14 | 0.18 | 0.00 | 0.03 | 190. |
| 195. | 0.52 | 0.35 | -0.06 | 0.27 | 0.21 | 0.07 | 0.04 | 195. |
| 200. | 0.71 | 0.52 | 0.06 | 0.36 | 0.24 | 0.12 | 0.06 | 200. |
| 205. | 0.83 | 0.64 | 0.14 | 0.42 | 0.25 | 0.18 | 0.06 | 205. |
| 210. | 0.88 | 0.72 | 0.17 | 0.47 | 0.25 | 0.21 | 0.06 | 210. |
| 215. | 0.85 | 0.69 | 0.16 | 0.48 | 0.25 | 0.22 | 0.05 | 215. |
| 220. | 0.78 | 0.64 | 0.15 | 0.49 | 0.24 | 0.22 | 0.05 | 220. |
| 225. | 0.71 | 0.57 | 0.15 | 0.48 | 0.23 | 0.23 | 0.05 | 225. |
| 230. | 0.68 | 0.56 | 0.16 | 0.47 | 0.21 | 0.24 | 0.05 | 230. |
| 235. | 0.67 | 0.56 | 0.16 | 0.47 | 0.20 | 0.25 | 0.06 | 235. |
| 240. | 0.66 | 0.58 | 0.17 | 0.49 | 0.21 | 0.26 | 0.07 | 240. |
| 245. | 0.67 | 0.61 | 0.19 | 0.51 | 0.21 | 0.27 | 0.09 | 245. |
| 250. | 0.69 | 0.64 | 0.21 | 0.53 | 0.22 | 0.30 | 0.09 | 250. |
| 255. | 0.71 | 0.68 | 0.23 | 0.55 | 0.24 | 0.32 | 0.09 | 255. |
| 260. | 0.75 | 0.72 | 0.25 | 0.57 | 0.25 | 0.35 | 0.09 | 260. |
| 265. | 0.78 | 0.76 | 0.27 | 0.58 | 0.27 | 0.37 | 0.09 | 265. |
| 270. | 0.82 | 0.79 | 0.29 | 0.60 | 0.29 | 0.37 | 0.10 | 270. |
| 275. | 0.87 | 0.80 | 0.31 | 0.61 | 0.30 | 0.38 | 0.10 | 275. |
| 280. | 0.91 | 0.81 | 0.33 | 0.62 | 0.31 | 0.37 | 0.10 | 280. |
| 285. | 0.96 | 0.83 | 0.35 | 0.63 | 0.31 | 0.37 | 0.09 | 285. |
| 290. | 1.02 | 0.86 | 0.37 | 0.63 | 0.31 | 0.36 | 0.08 | 290. |
| 295. | 1.08 | 0.89 | 0.39 | 0.63 | 0.31 | 0.35 | 0.07 | 295. |
| 300. | 1.13 | 0.92 | 0.40 | 0.63 | 0.31 | 0.35 | 0.06 | 300. |
| 305. | 1.18 | 0.93 | 0.40 | 0.62 | 0.31 | 0.34 | 0.06 | 305. |
| 310. | 1.21 | 0.93 | 0.39 | 0.61 | 0.31 | 0.33 | 0.07 | 310. |
| 315. | 1.22 | 0.92 | 0.37 | 0.60 | 0.31 | 0.32 | 0.08 | 315. |
| 320. | 1.21 | 0.90 | 0.36 | 0.58 | 0.32 | 0.33 | 0.08 | 320. |
| 325. | 1.19 | 0.90 | 0.42 | 0.58 | 0.33 | 0.32 | 0.07 | 325. |
| 330. | 1.24 | 1.05 | 0.42 | 0.56 | 0.33 | 0.33 | 0.04 | 330. |
| 335. | 1.14 | 0.93 | 0.35 | 0.51 | 0.30 | 0.26 | 0.01 | 335. |
| 340. | 0.72 | 0.67 | 0.12 | 0.34 | 0.21 | 0.18 | -0.02 | 340. |
| 345. | 0.30 | 0.14 | -0.21 | 0.11 | 0.09 | 0.10 | -0.04 | 345. |
| 350. | -0.74 | -0.32 | -0.51 | -0.18 | -0.06 | 0.02 | -0.05 | 350. |
| 355. | -1.20 | -0.38 | -0.70 | -0.23 | -0.15 | -0.03 | -0.05 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=***  CNTR NO. 57C  YCN= 91.  C.G.= 40.0

DIFFERENTIAL PRESSURES

SPAN STATION *2.5

| AZ DEG. | 0.455 | UPPER STATION 1.500 | 4.*** | 10.400 | AZ DEG. |
|---|---|---|---|---|---|
| 0. | -0.72 | -0.27 | -0.17 | 0.08 | 0. |
| 5. | -0.73 | -0.19 | 0.07 | 0.07 | 5. |
| 10. | -0.70 | -0.30 | -0.05 | 0.09 | 10. |
| 15. | -0.36 | -0.11 | 0.07 | 0.08 | 15. |
| 20. | -0.71 | -0.17 | 0.00 | 0.10 | 20. |
| 25. | -1.08 | -0.69 | -0.14 | 0.04 | 25. |
| 30. | -1.09 | -0.63 | -0.20 | 0.02 | 30. |
| 35. | -0.91 | -0.61 | -0.14 | 0.02 | 35. |
| 40. | -0.90 | -0.38 | -0.13 | 0.01 | 40. |
| 45. | -0.77 | -0.34 | -0.13 | -0.01 | 45. |
| 50. | -0.68 | -0.33 | -0.07 | -0.02 | 50. |
| 55. | -0.58 | -0.44 | 0.05 | -0.01 | 55. |
| 60. | -0.76 | -0.11 | 0.05 | -0.01 | 60. |
| 65. | -0.31 | -0.17 | 0.07 | -0.01 | 65. |
| 70. | -0.27 | -0.20 | 0.07 | -0.01 | 70. |
| 75. | -0.17 | -0.19 | 0.03 | -0.02 | 75. |
| 80. | -0.04 | -0.15 | 0.03 | -0.02 | 80. |
| 85. | 0.07 | -0.12 | 0.04 | -0.03 | 85. |
| 90. | 0.25 | -0.07 | 0.07 | -0.03 | 90. |
| 95. | 0.47 | 0.10 | 0.14 | 0.00 | 95. |
| 100. | 0.74 | 0.29 | 0.27 | 0.02 | 100. |
| 105. | 0.94 | 0.49 | 0.36 | 0.02 | 105. |
| 110. | 1.04 | 0.60 | 0.37 | 0.03 | 110. |
| 115. | 1.07 | 0.64 | 0.38 | 0.04 | 115. |
| 120. | 1.04 | 0.66 | 0.36 | 0.04 | 120. |
| 125. | 1.04 | 0.67 | 0.37 | 0.06 | 125. |
| 130. | 1.10 | 0.68 | 0.38 | 0.08 | 130. |
| 135. | 1.27 | 0.64 | 0.40 | 0.07 | 135. |
| 140. | 1.37 | 0.60 | 0.42 | 0.09 | 140. |
| 145. | 1.33 | 0.56 | 0.47 | 0.10 | 145. |
| 150. | 1.69 | 0.77 | 0.46 | 0.08 | 150. |
| 155. | 1.66 | 0.78 | 0.42 | 0.06 | 155. |
| 160. | 1.61 | 0.76 | 0.37 | 0.04 | 160. |
| 165. | 1.48 | 0.64 | 0.30 | 0.02 | 165. |
| 170. | 1.25 | 0.52 | 0.25 | -0.01 | 170. |
| 175. | 0.91 | 0.36 | 0.14 | -0.03 | 175. |
| 180. | 0.55 | 0.19 | 0.05 | -0.03 | 180. |
| 185. | 0.20 | 0.01 | -0.04 | -0.03 | 185. |
| 190. | -0.08 | -0.15 | -0.14 | -0.04 | 190. |
| 195. | -0.27 | -0.23 | -0.19 | -0.04 | 195. |
| 200. | -0.36 | -0.24 | -0.23 | -0.02 | 200. |
| 205. | -0.32 | -0.22 | -0.25 | -0.02 | 205. |
| 210. | -0.29 | -0.22 | -0.24 | -0.03 | 210. |
| 215. | -0.28 | -0.22 | -0.23 | -0.03 | 215. |
| 220. | -0.27 | -0.21 | -0.22 | -0.02 | 220. |
| 225. | -0.27 | -0.19 | -0.20 | -0.00 | 225. |
| 230. | -0.28 | -0.17 | -0.19 | 0.00 | 230. |
| 235. | -0.29 | -0.17 | -0.19 | -0.01 | 235. |
| 240. | -0.30 | -0.17 | -0.19 | -0.02 | 240. |
| 245. | -0.31 | -0.16 | -0.19 | -0.04 | 245. |
| 250. | -0.32 | -0.17 | -0.20 | -0.04 | 250. |
| 255. | -0.32 | -0.19 | -0.20 | -0.07 | 255. |
| 260. | -0.32 | -0.21 | -0.21 | -0.08 | 260. |
| 265. | -0.31 | -0.21 | -0.20 | -0.10 | 265. |
| 270. | -0.31 | -0.21 | -0.19 | -0.11 | 270. |
| 275. | -0.30 | -0.20 | -0.16 | -0.11 | 275. |
| 280. | -0.29 | -0.19 | -0.15 | -0.10 | 280. |
| 285. | -0.29 | -0.18 | -0.13 | -0.09 | 285. |
| 290. | -0.31 | -0.17 | -0.10 | -0.10 | 290. |
| 295. | -0.34 | -0.17 | -0.09 | -0.08 | 295. |
| 300. | -0.35 | -0.17 | -0.08 | -0.09 | 300. |
| 305. | -0.35 | -0.19 | -0.08 | -0.10 | 305. |
| 310. | -0.35 | -0.21 | -0.07 | -0.06 | 310. |
| 315. | -0.36 | -0.20 | -0.07 | -0.01 | 315. |
| 320. | -0.40 | -0.20 | -0.07 | 0.03 | 320. |
| 325. | -0.25 | -0.04 | -0.07 | 0.05 | 325. |
| 330. | -0.23 | -0.07 | -0.01 | 0.07 | 330. |
| 335. | -0.40 | -0.15 | -0.05 | 0.06 | 335. |
| 340. | -0.49 | -0.21 | -0.05 | 0.05 | 340. |
| 345. | -0.52 | -0.24 | -0.09 | 0.05 | 345. |
| 350. | -0.54 | -0.29 | -0.14 | 0.06 | 350. |
| 355. | -0.70 | -0.34 | -0.23 | 0.04 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-500 RUN NO. 570 TCA= 91. C.G.= 40.0

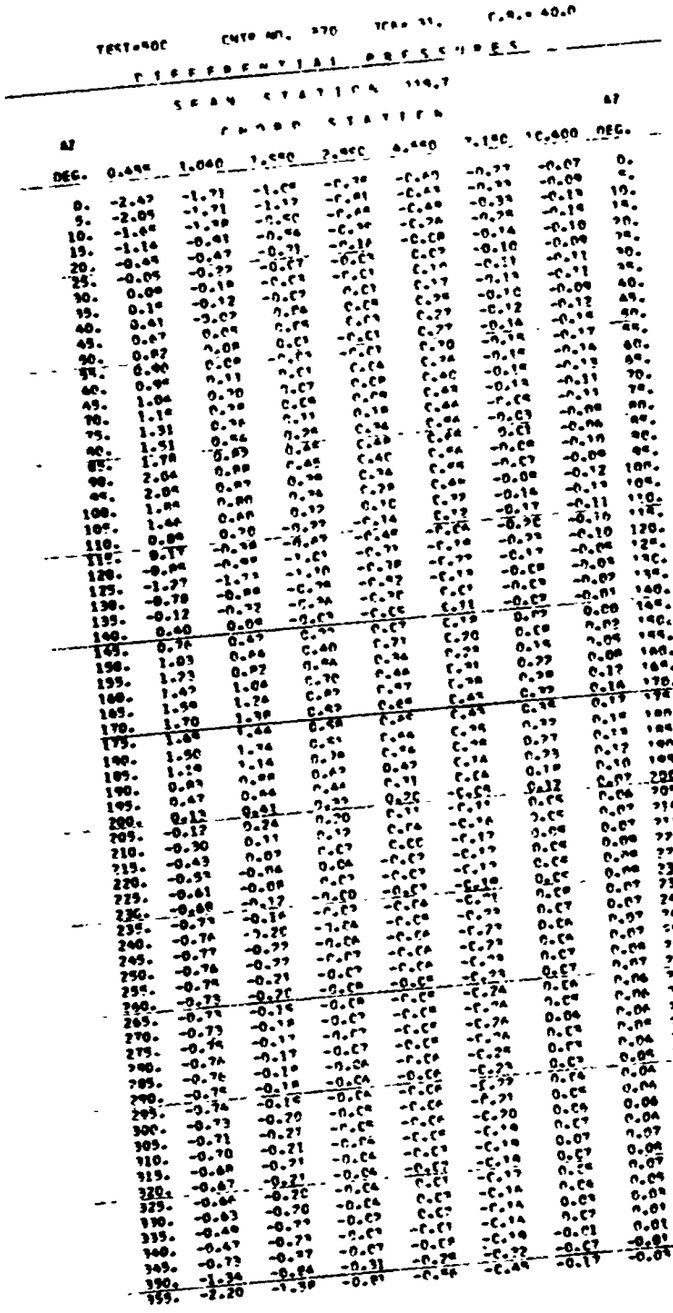
DIFFERENTIAL PRESSURES

SPAN STATION 70.0

| AZ DEG. | CHORD STATION 0.450 | 1.040 | 1.590 | 2.800 | 4.490 | 7.190 | 10.400 | AZ DEG. |
|---|---|---|---|---|---|---|---|---|
| 0. | -1.71 | -1.01 | -0.61 | -0.41 | -0.26 | -0.09 | -0.00 | 0. |
| 5. | -0.59 | -0.28 | -0.24 | -0.11 | -0.06 | 0.10 | 0.13 | 5. |
| 10. | -0.35 | -0.20 | -0.21 | -0.13 | -0.04 | 0.09 | 0.09 | 10. |
| 15. | -1.16 | -0.92 | -0.63 | -0.37 | -0.20 | -0.08 | 0.02 | 15. |
| 20. | -1.10 | -0.80 | -0.60 | -0.41 | -0.24 | -0.16 | -0.01 | 20. |
| 25. | -0.92 | -0.76 | -0.66 | -0.36 | -0.22 | -0.15 | 0.00 | 25. |
| 30. | -0.89 | -0.69 | -0.66 | -0.37 | -0.19 | -0.15 | -0.00 | 30. |
| 35. | -0.89 | -0.69 | -0.67 | -0.37 | -0.20 | -0.14 | -0.02 | 35. |
| 40. | -0.87 | -0.69 | -0.66 | -0.36 | -0.16 | -0.14 | -0.01 | 40. |
| 45. | -0.77 | -0.66 | -0.69 | -0.31 | -0.14 | -0.14 | -0.02 | 45. |
| 50. | -0.61 | -0.59 | -0.57 | -0.31 | -0.17 | -0.16 | -0.01 | 50. |
| 55. | -0.50 | -0.41 | -0.57 | -0.30 | -0.15 | -0.14 | -0.02 | 55. |
| 60. | -0.38 | -0.42 | -0.48 | -0.29 | -0.05 | -0.17 | -0.03 | 60. |
| 65. | -0.24 | -0.29 | -0.40 | -0.19 | -0.03 | -0.14 | -0.02 | 65. |
| 70. | -0.11 | -0.19 | -0.30 | -0.09 | 0.03 | -0.14 | -0.00 | 70. |
| 75. | 0.03 | -0.08 | -0.19 | -0.03 | 0.08 | -0.13 | -0.00 | 75. |
| 80. | 0.17 | 0.01 | -0.14 | 0.02 | 0.13 | -0.09 | 0.01 | 80. |
| 85. | 0.34 | 0.09 | -0.04 | 0.15 | 0.14 | -0.07 | -0.00 | 85. |
| 90. | 0.54 | 0.22 | 0.04 | 0.19 | 0.23 | -0.04 | 0.03 | 90. |
| 95. | 0.75 | 0.42 | 0.17 | 0.29 | 0.29 | -0.03 | 0.03 | 95. |
| 100. | 0.94 | 0.58 | 0.31 | 0.38 | 0.33 | 0.00 | 0.04 | 100. |
| 105. | 1.12 | 0.65 | 0.43 | 0.40 | 0.38 | 0.01 | 0.04 | 105. |
| 110. | 1.19 | 0.77 | 0.47 | 0.42 | 0.41 | 0.00 | 0.05 | 110. |
| 115. | 1.10 | 0.76 | 0.46 | 0.42 | 0.46 | 0.01 | 0.07 | 115. |
| 120. | 1.04 | 0.73 | 0.44 | 0.41 | 0.41 | 0.07 | 0.11 | 120. |
| 125. | 1.19 | 0.93 | 0.44 | 0.42 | 0.43 | 0.14 | 0.14 | 125. |
| 130. | 1.29 | 0.78 | 0.58 | 0.48 | 0.50 | 0.16 | 0.13 | 130. |
| 135. | 1.49 | 0.87 | 0.64 | 0.48 | 0.47 | 0.17 | 0.12 | 135. |
| 140. | 1.84 | 1.01 | 0.74 | 0.52 | 0.46 | 0.15 | 0.12 | 140. |
| 145. | 1.85 | 1.19 | 0.84 | 0.48 | 0.46 | 0.20 | 0.15 | 145. |
| 150. | 2.00 | 1.41 | 0.97 | 0.65 | 0.60 | 0.22 | 0.14 | 150. |
| 155. | 2.35 | 1.61 | 1.11 | 0.79 | 0.61 | 0.25 | 0.16 | 155. |
| 160. | 2.55 | 1.76 | 1.23 | 0.80 | 0.68 | 0.28 | 0.16 | 160. |
| 165. | 2.65 | 1.81 | 1.31 | 0.82 | 0.68 | 0.30 | 0.16 | 165. |
| 170. | 2.53 | 1.73 | 1.30 | 0.78 | 0.66 | 0.29 | 0.15 | 170. |
| 175. | 2.23 | 1.49 | 1.16 | 0.76 | 0.65 | 0.29 | 0.15 | 175. |
| 180. | 1.74 | 1.23 | 0.98 | 0.68 | 0.54 | 0.24 | 0.12 | 180. |
| 185. | 1.19 | 0.81 | 0.71 | 0.45 | 0.35 | 0.19 | 0.10 | 185. |
| 190. | 0.69 | 0.46 | 0.43 | 0.24 | 0.20 | 0.12 | 0.06 | 190. |
| 195. | 0.16 | 0.15 | 0.20 | 0.05 | -0.04 | 0.05 | 0.02 | 195. |
| 200. | -0.17 | 0.04 | 0.03 | -0.04 | -0.13 | 0.02 | 0.01 | 200. |
| 205. | -0.35 | -0.17 | -0.08 | -0.07 | -0.17 | 0.02 | 0.01 | 205. |
| 210. | -0.34 | -0.32 | -0.14 | -0.11 | -0.18 | 0.02 | 0.02 | 210. |
| 215. | -0.30 | -0.40 | -0.18 | -0.14 | -0.17 | 0.02 | 0.01 | 215. |
| 220. | -0.25 | -0.41 | -0.20 | -0.16 | -0.17 | 0.00 | -0.00 | 220. |
| 225. | -0.40 | -0.38 | -0.31 | -0.17 | -0.18 | -0.01 | -0.01 | 225. |
| 230. | -0.61 | -0.38 | -0.33 | -0.16 | -0.20 | -0.03 | -0.03 | 230. |
| 235. | -0.69 | -0.38 | -0.31 | -0.31 | -0.22 | -0.04 | -0.05 | 235. |
| 240. | -0.61 | -0.38 | -0.30 | -0.29 | -0.23 | -0.05 | -0.07 | 240. |
| 245. | -0.54 | -0.38 | -0.30 | -0.31 | -0.23 | -0.05 | -0.07 | 245. |
| 250. | -0.50 | -0.33 | -0.19 | -0.21 | -0.23 | -0.05 | -0.08 | 250. |
| 255. | -0.58 | -0.37 | -0.19 | -0.23 | -0.24 | -0.08 | -0.11 | 255. |
| 260. | -0.58 | -0.31 | -0.17 | -0.23 | -0.25 | -0.04 | -0.14 | 260. |
| 265. | -0.57 | -0.34 | -0.14 | -0.25 | -0.25 | -0.07 | -0.15 | 265. |
| 270. | -0.54 | -0.31 | -0.13 | -0.15 | -0.20 | -0.05 | -0.14 | 270. |
| 275. | -0.54 | -0.37 | -0.13 | -0.14 | -0.19 | -0.04 | -0.14 | 275. |
| 280. | -0.57 | -0.37 | -0.15 | -0.14 | -0.20 | -0.04 | -0.15 | 280. |
| 285. | -0.58 | -0.35 | -0.14 | -0.14 | -0.21 | -0.04 | -0.15 | 285. |
| 290. | -0.60 | -0.37 | -0.15 | -0.15 | -0.22 | -0.01 | -0.14 | 290. |
| 295. | -0.61 | -0.37 | -0.14 | -0.15 | -0.19 | 0.01 | -0.16 | 295. |
| 300. | -0.61 | -0.37 | -0.15 | -0.14 | -0.19 | 0.01 | -0.14 | 300. |
| 305. | -0.60 | -0.37 | -0.15 | -0.14 | -0.19 | 0.01 | -0.14 | 305. |
| 310. | -0.59 | -0.37 | -0.14 | -0.15 | -0.16 | 0.00 | -0.13 | 310. |
| 315. | -0.60 | -0.36 | -0.17 | -0.14 | -0.15 | 0.00 | -0.13 | 315. |
| 320. | -0.61 | -0.38 | -0.14 | -0.17 | -0.16 | 0.01 | -0.09 | 320. |
| 325. | -0.59 | -0.38 | -0.14 | -0.18 | -0.17 | 0.03 | -0.02 | 325. |
| 330. | -0.60 | -0.38 | -0.21 | -0.18 | -0.19 | 0.01 | 0.02 | 330. |
| 335. | -0.72 | -0.44 | -0.28 | -0.21 | -0.20 | -0.02 | 0.00 | 335. |
| 340. | -0.98 | -0.62 | -0.40 | -0.30 | -0.27 | -0.06 | -0.03 | 340. |
| 345. | -1.30 | -0.88 | -0.59 | -0.41 | -0.35 | -0.11 | -0.02 | 345. |
| 350. | -1.67 | -1.06 | -0.67 | -0.54 | -0.43 | -0.16 | -0.02 | 350. |
| 355. | -2.03 | -1.39 | -0.80 | -0.71 | -0.49 | -0.20 | -0.04 | 355. |

TEXT NOT REPRODUCIBLE

DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS



TEXT NOT REPRODUCIBLE

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-800 CNTR NO. 870 TCA- 31. C.R.- 40.0

DIFFERENTIAL PRESSURES

SPAN STATIC- 193.3

| AZ | SPAN STATICS | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.590 | 2.080 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.84 | -0.79 | -0.46 | -0.57 | -0.29 | -0.10 | -0.00 | 0. |
| 5. | -1.26 | -0.97 | -0.70 | -0.44 | -0.34 | -0.14 | -0.04 | 5. |
| 10. | -1.18 | -0.67 | -0.78 | -0.67 | -0.34 | -0.24 | -0.08 | 10. |
| 15. | -0.72 | -0.60 | -0.61 | -0.49 | -0.34 | -0.22 | -0.08 | 15. |
| 20. | -0.16 | -0.15 | -0.28 | -0.19 | -0.04 | -0.13 | -0.06 | 20. |
| 25. | 0.42 | 0.26 | 0.01 | 0.05 | 0.14 | -0.04 | -0.07 | 25. |
| 30. | 0.84 | 0.49 | 0.26 | 0.23 | 0.28 | 0.01 | 0.01 | 30. |
| 35. | 1.17 | 0.82 | 0.61 | 0.33 | 0.34 | 0.00 | 0.01 | 35. |
| 40. | 1.46 | 1.11 | 0.80 | 0.49 | 0.38 | -0.03 | -0.01 | 40. |
| 45. | 1.70 | 1.22 | 0.82 | 0.60 | 0.48 | -0.00 | 0.01 | 45. |
| 50. | 1.58 | 1.23 | 0.64 | 0.73 | 0.83 | -0.03 | 0.00 | 50. |
| 55. | 1.38 | 1.19 | 0.98 | 0.78 | 0.81 | -0.07 | -0.02 | 55. |
| 60. | 1.20 | 0.87 | 0.72 | 0.84 | 0.83 | -0.08 | -0.04 | 60. |
| 65. | 1.08 | 0.87 | 0.68 | 1.14 | 0.87 | -0.08 | -0.03 | 65. |
| 70. | 1.06 | 0.78 | -0.10 | 1.68 | 0.82 | -0.10 | -0.06 | 70. |
| 75. | 1.04 | 0.78 | -0.18 | 2.07 | 0.68 | -0.14 | -0.07 | 75. |
| 80. | 1.22 | 0.88 | -0.17 | 1.88 | 1.68 | -0.03 | -0.11 | 80. |
| 85. | 1.14 | 0.84 | -0.12 | 1.64 | 0.81 | -0.29 | -0.09 | 85. |
| 90. | 1.27 | 1.13 | 0.03 | 1.67 | 0.73 | -0.29 | -0.12 | 90. |
| 95. | 1.18 | 0.81 | 0.08 | 1.64 | 0.64 | -0.67 | -0.21 | 95. |
| 100. | 0.00 | -0.35 | -0.49 | 0.69 | 0.33 | -0.52 | -0.14 | 100. |
| 105. | -1.24 | -1.15 | -0.79 | -0.48 | -1.71 | -0.30 | -0.11 | 105. |
| 110. | -1.70 | -1.47 | -0.69 | -1.48 | -2.71 | -0.19 | -0.10 | 110. |
| 115. | -2.11 | -1.89 | -0.69 | -1.94 | -2.64 | -0.18 | -0.10 | 115. |
| 120. | -2.50 | -2.18 | -2.13 | -2.60 | -1.78 | -0.23 | -0.04 | 120. |
| 125. | -2.98 | -2.47 | -2.88 | -2.86 | -0.13 | -0.28 | -0.07 | 125. |
| 130. | -2.90 | -2.64 | -2.94 | -1.88 | -0.04 | -0.33 | -0.10 | 130. |
| 135. | -2.35 | -1.77 | -1.39 | -0.81 | -0.18 | -0.28 | -0.11 | 135. |
| 140. | -1.50 | -0.86 | -1.00 | -0.09 | -0.12 | -0.21 | -0.09 | 140. |
| 145. | -0.89 | -0.38 | -0.61 | 0.18 | 0.04 | -0.15 | -0.08 | 145. |
| 150. | -0.28 | 0.01 | -0.05 | 0.27 | 0.17 | -0.09 | -0.06 | 150. |
| 155. | 0.12 | 0.28 | 0.18 | 0.33 | 0.26 | -0.07 | -0.04 | 155. |
| 160. | 0.41 | 0.45 | 0.34 | 0.37 | 0.33 | 0.04 | -0.01 | 160. |
| 165. | 0.62 | 0.76 | 0.52 | 0.41 | 0.38 | 0.10 | 0.00 | 165. |
| 170. | 0.83 | 1.01 | 0.69 | 0.44 | 0.34 | 0.14 | 0.02 | 170. |
| 175. | 0.94 | 1.04 | 0.70 | 0.41 | 0.38 | 0.16 | 0.02 | 175. |
| 180. | 1.01 | 0.98 | 0.78 | 0.53 | 0.43 | 0.18 | 0.04 | 180. |
| 185. | 0.98 | 0.88 | 0.74 | 0.48 | 0.37 | 0.20 | 0.04 | 185. |
| 190. | 0.91 | 0.72 | 0.74 | 0.49 | 0.38 | 0.20 | 0.04 | 190. |
| 195. | 0.79 | 0.59 | 0.68 | 0.33 | 0.17 | 0.19 | 0.04 | 195. |
| 200. | 0.61 | 0.47 | 0.49 | 0.27 | 0.05 | 0.14 | 0.03 | 200. |
| 205. | 0.42 | 0.28 | 0.24 | 0.11 | 0.01 | 0.16 | 0.01 | 205. |
| 210. | 0.24 | 0.17 | 0.46 | 0.03 | -0.05 | 0.17 | -0.00 | 210. |
| 215. | 0.10 | 0.09 | 0.40 | -0.03 | -0.08 | 0.11 | -0.01 | 215. |
| 220. | -0.01 | 0.01 | 0.33 | -0.08 | -0.10 | 0.12 | 0.00 | 220. |
| 225. | -0.08 | -0.05 | 0.30 | -0.11 | -0.10 | 0.14 | 0.03 | 225. |
| 230. | -0.13 | -0.08 | 0.30 | -0.12 | -0.05 | 0.17 | 0.04 | 230. |
| 235. | -0.16 | -0.08 | 0.30 | -0.14 | -0.06 | 0.18 | 0.06 | 235. |
| 240. | -0.14 | -0.07 | 0.31 | -0.14 | -0.06 | 0.18 | 0.06 | 240. |
| 245. | -0.15 | -0.07 | 0.33 | -0.17 | -0.06 | 0.19 | 0.10 | 245. |
| 250. | -0.15 | -0.06 | 0.30 | -0.16 | -0.06 | 0.20 | 0.10 | 250. |
| 255. | -0.17 | -0.11 | 0.28 | -0.21 | -0.11 | 0.19 | 0.08 | 255. |
| 260. | -0.19 | -0.12 | 0.24 | -0.21 | -0.14 | 0.18 | 0.07 | 260. |
| 265. | -0.21 | -0.11 | 0.28 | -0.21 | -0.14 | 0.17 | 0.06 | 265. |
| 270. | -0.22 | -0.10 | 0.24 | -0.21 | -0.14 | 0.16 | 0.06 | 270. |
| 275. | -0.22 | -0.11 | 0.24 | -0.21 | -0.16 | 0.16 | 0.04 | 275. |
| 280. | -0.21 | -0.12 | 0.24 | -0.22 | -0.16 | 0.16 | 0.04 | 280. |
| 285. | -0.19 | -0.12 | 0.24 | -0.24 | -0.16 | 0.15 | 0.05 | 285. |
| 290. | -0.16 | -0.11 | 0.25 | -0.26 | -0.16 | 0.15 | 0.05 | 290. |
| 295. | -0.13 | -0.11 | 0.27 | -0.28 | -0.17 | 0.14 | 0.06 | 295. |
| 300. | -0.11 | -0.12 | 0.28 | -0.30 | -0.16 | 0.14 | 0.04 | 300. |
| 305. | -0.11 | -0.13 | 0.28 | -0.30 | -0.17 | 0.15 | 0.07 | 305. |
| 310. | -0.14 | -0.14 | 0.28 | -0.30 | -0.17 | 0.15 | 0.08 | 310. |
| 315. | -0.26 | -0.21 | 0.17 | -0.30 | -0.19 | 0.13 | 0.08 | 315. |
| 320. | -0.35 | -0.27 | 0.08 | -0.33 | -0.19 | 0.11 | 0.07 | 320. |
| 325. | -0.40 | -0.30 | 0.01 | -0.34 | -0.19 | 0.09 | 0.04 | 325. |
| 330. | -0.39 | -0.30 | -0.05 | -0.34 | -0.19 | 0.07 | 0.04 | 330. |
| 335. | -0.19 | -0.20 | -0.00 | -0.30 | -0.17 | 0.09 | 0.04 | 335. |
| 340. | 0.22 | 0.04 | 0.23 | -0.17 | -0.04 | 0.13 | 0.04 | 340. |
| 345. | 0.61 | 0.37 | 0.38 | -0.04 | 0.04 | 0.14 | 0.08 | 345. |
| 350. | 0.93 | 0.70 | 0.36 | -0.00 | 0.09 | 0.13 | 0.07 | 350. |
| 355. | -0.35 | -0.38 | -0.18 | -0.31 | -0.17 | 0.09 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-500 CNTR NO. 470 YCN= 91. C.R.= 40.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ DEG. | CHORD STATION 0.455 | 1.060 | 1.580 | 2.980 | 4.380 | 7.180 | 10.400 | AZ DEG. |
|---|---|---|---|---|---|---|---|---|
| 0. | -0.14 | 0.37 | 0.04 | 0.06 | 0.09 | -0.07 | 0.05 | 0. |
| 5. | 0.00 | 0.11 | -0.03 | -0.07 | 0.11 | -0.12 | 0.05 | 5. |
| 10. | -0.30 | -0.14 | -0.41 | -0.07 | -0.04 | -0.14 | 0.04 | 10. |
| 15. | -0.35 | -0.34 | -0.48 | -0.16 | -0.16 | -0.25 | 0.02 | 15. |
| 20. | -0.11 | -0.17 | -0.40 | -0.15 | -0.05 | -0.18 | 0.03 | 20. |
| 25. | 0.43 | 0.24 | -0.14 | -0.01 | 0.10 | -0.07 | 0.05 | 25. |
| 30. | 1.06 | 0.47 | 0.16 | 0.15 | 0.23 | 0.02 | 0.04 | 30. |
| 35. | 1.49 | 0.73 | 0.38 | 0.25 | 0.27 | 0.09 | 0.12 | 35. |
| 40. | 1.58 | 0.61 | 0.48 | 0.44 | 0.40 | 0.14 | 0.14 | 40. |
| 45. | 1.49 | 0.60 | 0.40 | 0.39 | 0.64 | 0.17 | 0.14 | 45. |
| 50. | 1.54 | 0.25 | 0.06 | 1.05 | 0.71 | 0.10 | 0.08 | 50. |
| 55. | 1.30 | 0.16 | 0.89 | 1.05 | 0.81 | -0.04 | 0.03 | 55. |
| 60. | 1.01 | -0.10 | 0.68 | 0.72 | 1.04 | -0.07 | 0.03 | 60. |
| 65. | 0.95 | -0.34 | 0.65 | 0.47 | 0.83 | -0.07 | 0.01 | 65. |
| 70. | 1.05 | -0.48 | 0.68 | 0.41 | 0.38 | -0.35 | -0.12 | 70. |
| 75. | 0.08 | -1.03 | -0.07 | 0.26 | -0.09 | -1.31 | -0.04 | 75. |
| 80. | 0.05 | -1.17 | -0.33 | 0.25 | -0.01 | -0.75 | 0.06 | 80. |
| 85. | 0.48 | -1.00 | 0.19 | 0.34 | 0.04 | -0.04 | -0.04 | 85. |
| 90. | -0.19 | -1.53 | 0.01 | 0.19 | -0.34 | -0.36 | -0.04 | 90. |
| 95. | -0.47 | -1.84 | -0.01 | -0.10 | -0.71 | -0.89 | -0.14 | 95. |
| 100. | -0.97 | -2.07 | -1.04 | -0.41 | -0.69 | -1.05 | -0.30 | 100. |
| 105. | -1.19 | -2.14 | -1.12 | -0.72 | -1.18 | 0.47 | -0.47 | 105. |
| 110. | -1.58 | -2.75 | -1.14 | -0.59 | -1.40 | 1.82 | -0.45 | 110. |
| 115. | -1.96 | -3.15 | -1.25 | -1.08 | -1.71 | 1.78 | -0.55 | 115. |
| 120. | -2.19 | -3.18 | -1.34 | -1.07 | -1.69 | 0.10 | -0.29 | 120. |
| 125. | -2.18 | -3.11 | -1.06 | -1.01 | -2.26 | -1.14 | 0.12 | 125. |
| 130. | -2.01 | -2.88 | -1.71 | -1.37 | -3.20 | -0.25 | 0.28 | 130. |
| 135. | -2.03 | -2.44 | -1.09 | -1.67 | -2.74 | 0.58 | 0.19 | 135. |
| 140. | -1.96 | -2.55 | -2.[illegible] | -2.08 | -0.66 | 0.22 | 0.07 | 140. |
| 145. | -1.52 | -2.08 | -[illegible] | -1.14 | 0.09 | -0.09 | 0.01 | 145. |
| 150. | -1.01 | -1.15 | -[illegible] | -0.69 | -0.15 | -0.07 | 0.00 | 150. |
| 155. | -0.59 | -0.63 | -0.63 | -0.37 | -0.19 | 0.03 | 0.01 | 155. |
| 160. | -0.27 | -0.19 | -0.60 | -0.32 | -0.09 | 0.05 | 0.02 | 160. |
| 165. | -0.03 | 0.15 | -0.35 | -0.24 | 0.04 | 0.05 | 0.02 | 165. |
| 170. | 0.15 | 0.38 | -0.15 | -0.24 | 0.15 | 0.08 | 0.03 | 170. |
| 175. | 0.32 | 0.47 | 0.09 | -0.14 | 0.22 | 0.12 | 0.04 | 175. |
| 180. | 0.44 | 0.74 | 0.17 | -0.04 | 0.27 | 0.13 | 0.04 | 180. |
| 185. | 0.51 | 0.88 | 0.28 | 0.07 | 0.31 | 0.13 | 0.03 | 185. |
| 190. | 0.53 | 0.98 | 0.36 | 0.09 | 0.33 | 0.13 | 0.03 | 190. |
| 195. | 0.52 | 1.01 | 0.40 | 0.12 | 0.34 | 0.13 | 0.03 | 195. |
| 200. | 0.47 | 1.01 | 0.41 | 0.13 | 0.34 | 0.10 | 0.03 | 200. |
| 205. | 0.40 | 0.98 | 0.40 | 0.17 | 0.32 | 0.07 | 0.02 | 205. |
| 210. | 0.32 | 0.87 | 0.38 | 0.19 | 0.31 | 0.05 | 0.01 | 210. |
| 215. | 0.23 | 0.84 | 0.37 | 0.18 | 0.29 | 0.03 | 0.00 | 215. |
| 220. | 0.16 | 0.80 | 0.36 | 0.17 | 0.29 | 0.02 | -0.00 | 220. |
| 225. | 0.10 | 0.84 | 0.41 | 0.19 | 0.28 | 0.02 | -0.00 | 225. |
| 230. | 0.10 | 0.87 | 0.45 | 0.19 | 0.29 | 0.02 | -0.00 | 230. |
| 235. | 0.11 | 0.86 | 0.50 | 0.21 | 0.31 | 0.04 | 0.00 | 235. |
| 240. | 0.14 | 0.91 | 0.54 | 0.22 | 0.34 | 0.05 | 0.01 | 240. |
| 245. | 0.16 | 0.96 | 0.56 | 0.24 | 0.36 | 0.08 | 0.02 | 245. |
| 250. | 0.16 | 0.97 | 1.00 | 0.24 | 0.38 | 0.09 | 0.02 | 250. |
| 255. | 0.16 | 0.98 | 0.99 | 0.27 | 0.38 | 0.07 | 0.03 | 255. |
| 260. | 0.16 | 0.97 | 0.99 | 0.28 | 0.40 | 0.06 | 0.03 | 260. |
| 265. | 0.16 | 0.98 | 0.98 | 0.29 | 0.40 | 0.06 | 0.03 | 265. |
| 270. | 0.16 | 0.98 | 0.97 | 0.30 | 0.39 | 0.06 | 0.03 | 270. |
| 275. | 0.19 | 0.98 | 0.97 | 0.31 | 0.39 | 0.04 | 0.02 | 275. |
| 280. | 0.19 | 0.99 | 0.98 | 0.31 | 0.38 | 0.05 | 0.02 | 280. |
| 285. | 0.21 | 0.99 | 0.99 | 0.31 | 0.37 | 0.05 | 0.02 | 285. |
| 290. | 0.22 | 0.99 | 0.99 | 0.31 | 0.36 | 0.05 | 0.02 | 290. |
| 295. | 0.23 | 0.99 | 0.98 | 0.31 | 0.35 | 0.05 | 0.02 | 295. |
| 300. | 0.23 | 0.99 | 0.96 | 0.32 | 0.35 | 0.04 | 0.02 | 300. |
| 305. | 0.24 | 0.98 | 0.96 | 0.32 | 0.36 | 0.04 | 0.02 | 305. |
| 310. | 0.24 | 0.97 | 0.96 | 0.31 | 0.36 | 0.04 | 0.03 | 310. |
| 315. | 0.23 | 0.96 | 0.95 | 0.30 | 0.36 | 0.04 | 0.04 | 315. |
| 320. | 0.23 | 0.93 | 0.93 | 0.29 | 0.33 | 0.03 | 0.04 | 320. |
| 325. | 0.24 | 0.90 | 0.90 | 0.28 | 0.29 | 0.00 | 0.03 | 325. |
| 330. | -0.01 | 0.76 | 0.79 | 0.21 | 0.21 | -0.03 | 0.03 | 330. |
| 335. | -0.26 | 0.56 | 0.31 | 0.12 | 0.13 | -0.08 | 0.02 | 335. |
| 340. | -0.10 | 0.57 | 0.09 | 0.15 | 0.19 | -0.10 | 0.03 | 340. |
| 345. | 0.40 | 0.69 | 0.37 | 0.27 | 0.27 | -0.04 | 0.05 | 345. |
| 350. | 0.50 | 0.87 | 0.38 | 0.29 | 0.26 | -0.04 | 0.04 | 350. |
| 355. | 0.26 | 0.61 | 0.19 | 0.20 | 0.24 | -0.09 | 0.04 | 355. |

TEXT NOT REPRODUCIBLE

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=40C  CNTR NO. 470  TCN= 31.  C.R.= 40.0

DIFFERENTIAL PRESSURES

SPAN STATION 195.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.640 | 2.440 | 4.450 | 7.140 | 10.400 | DEG. |
| 0. | 0.1[illegible] | 0.0[illegible] | -0.14 | 0.20 | 0.1[illegible] | -0.0[illegible] | 0.09 | 0. |
| 5. | 0.0[illegible] | -0.02 | -0.21 | 0.13 | 0.1[illegible] | -0.01 | 0.10 | 5. |
| 10. | -0.1[illegible] | -0.12 | -0.[illegible]0 | -0.00 | 0.1[illegible] | -0.10 | 0.04 | 10. |
| 1[illegible]. | -0.21 | -0.[illegible]1 | -0.[illegible]0 | -0.1[illegible] | 0.1[illegible] | -0.2[illegible] | 0.01 | 1[illegible]. |
| 20. | 0.1[illegible] | -0.1[illegible] | -0.4[illegible] | -0.[illegible]5 | 0.24 | -0.20 | 0.06 | 20. |
| 25. | 0.6[illegible] | 0.[illegible]1 | -0.1[illegible] | 0.1[illegible] | 0.44 | -0.10 | 0.07 | 25. |
| 30. | 1.2[illegible] | 0.[illegible]6 | 0.[illegible]0 | 0.3[illegible] | 0.6[illegible] | -0.0[illegible] | 0.08 | 30. |
| 35. | 1.61 | 0.[illegible]7 | 0.[illegible]8 | 0.[illegible]8 | 0.[illegible]4 | -0.0[illegible] | 0.11 | 35. |
| 40. | 1.72 | 0.47 | 1.20 | 0.66 | 1.16 | 0.01 | 0.10 | 40. |
| 45. | 1.8[illegible] | 0.7[illegible] | 1.47 | 1.[illegible]8 | 1.24 | -0.0[illegible] | 0.04 | 45. |
| 50. | 1.7[illegible] | 0.7[illegible] | 1.[illegible]6 | 1.[illegible]6 | 1.[illegible]4 | -0.[illegible]4 | -0.[illegible]5 | 50. |
| 55. | 1.[illegible]8 | 0.4[illegible] | 1.40 | 0.4[illegible] | 1.44 | -0.6[illegible] | -0.10 | 55. |
| 60. | 1.1[illegible] | 0.[illegible]5 | 1.1[illegible] | 0.2[illegible] | 0.7[illegible] | -0.4[illegible] | -0.1[illegible] | 60. |
| 65. | 1.0[illegible] | 0.41 | 1.[illegible]4 | 0.[illegible]3 | 0.[illegible]5 | 0.0[illegible] | -0.2[illegible] | 65. |
| 70. | -0.1[illegible] | -0.2[illegible] | 0.[illegible]8 | -0.[illegible]5 | 0.47 | -0.40 | -0.12 | 70. |
| 7[illegible]. | -0.44 | -0.64 | 0.[illegible]8 | -0.6[illegible] | -0.0[illegible] | -0.7[illegible] | 0.07 | 7[illegible]. |
| 80. | 0.05 | -0.[illegible]0 | 0.[illegible]7 | -0.[illegible]2 | -0.2[illegible] | -0.[illegible]5 | -0.10 | 80. |
| 8[illegible]. | -0.47 | -0.6[illegible] | 0.[illegible]1 | -0.[illegible]4 | -0.4[illegible] | -0.4[illegible] | -0.1[illegible] | 8[illegible]. |
| 90. | -0.7[illegible] | -0.[illegible]0 | 0.[illegible]7 | -0.6[illegible] | -0.6[illegible] | -0.4[illegible] | -0.27 | 90. |
| 9[illegible]. | -1.06 | -1.01 | 0.0[illegible] | -0.[illegible]7 | -0.[illegible]6 | -0.8[illegible] | -0.1[illegible] | 9[illegible]. |
| 100. | -1.4[illegible] | -1.1[illegible] | -0.[illegible]0 | -0.[illegible]0 | -0.[illegible]7 | -0.1[illegible] | -0.[illegible]4 | 100. |
| 10[illegible]. | -1.[illegible]8 | -1.[illegible]4 | -0.[illegible]7 | -1.[illegible]8 | -0.[illegible]4 | 0.[illegible]4 | 0.20 | 10[illegible]. |
| 110. | -2.32 | -2.[illegible]0 | -1.[illegible]4 | -1.[illegible]7 | -1.[illegible]2 | 1.[illegible]7 | 0.[illegible]6 | 110. |
| 11[illegible]. | -2.6[illegible] | -2.[illegible]7 | -1.[illegible]4 | -1.[illegible]5 | -1.[illegible]0 | 2.60 | -0.[illegible]9 | 11[illegible]. |
| 120. | -2.77 | -2.[illegible]7 | -1.[illegible]9 | -2.[illegible]0 | -1.[illegible]5 | 1.[illegible]8 | -0.[illegible]3 | 120. |
| 125. | -.[illegible]4 | -2.47 | -1.77 | -1.[illegible]7 | -1.[illegible]8 | 0.27 | -0.44 | 125. |
| 130. | -2.[illegible]8 | -2.1[illegible] | -1.[illegible]5 | -1.[illegible]6 | -1.[illegible]0 | -1.[illegible]5 | -0.01 | 130. |
| 135. | -2.12 | -1.[illegible]6 | -1.[illegible]5 | -1.[illegible]5 | -2.[illegible]0 | -0.4[illegible] | 0.[illegible]7 | 135. |
| 140. | -2.00 | -2.01 | -1.[illegible]4 | -2.[illegible]5 | -1.[illegible]2 | 0.[illegible]1 | 0.[illegible]0 | 140. |
| 145. | -1.[illegible]4 | -1.[illegible]6 | -1.[illegible]1 | -2.1[illegible] | -[illegible].[illegible]3 | -0.[illegible]9 | 0.01 | 145. |
| 150. | -1.67 | -1.[illegible]7 | -1.[illegible]7 | -[illegible].82 | [illegible].[illegible]2 | -0.[illegible]1 | -0.[illegible]6 | 150. |
| 155. | -1.1[illegible] | -0.[illegible]1 | -1.10 | -0.[illegible]7 | [illegible].[illegible]8 | -0.[illegible]8 | -0.[illegible]4 | 155. |
| 160. | -0.[illegible]6 | -0.40 | -0.[illegible]8 | -0.[illegible]9 | [illegible].[illegible]3 | -0.[illegible]7 | -0.01 | 160. |
| 165. | -0.[illegible]5 | -0.[illegible]5 | -0.40 | -0.[illegible]4 | [illegible].[illegible]8 | -0.14 | -0.[illegible]3 | 165. |
| 170. | 0.[illegible]4 | 0.[illegible]5 | -0.[illegible]7 | -0.[illegible]1 | [illegible].[illegible]4 | -0.[illegible]7 | -0.[illegible]3 | 170. |
| 175. | 0.[illegible]8 | 0.[illegible]7 | -0.[illegible]5 | 0.14 | [illegible].[illegible]1 | -0.[illegible]8 | -0.00 | 175. |
| 180. | 0.43 | 0.[illegible]0 | 0.[illegible]4 | 0.[illegible]7 | [illegible].[illegible]3 | -0.[illegible]3 | 0.00 | 180. |
| 185. | 0.[illegible]7 | 0.47 | 0.12 | 0.[illegible]6 | [illegible].[illegible]3 | -0.[illegible]3 | -0.01 | 185. |
| 190. | 0.[illegible]5 | 0.[illegible]1 | 0.[illegible]0 | 0.[illegible]0 | [illegible].[illegible]3 | -0.[illegible]3 | -0.00 | 190. |
| 195. | 0.[illegible]9 | 0.[illegible]6 | 0.[illegible]3 | 0.[illegible]2 | [illegible].[illegible]0 | -0.[illegible]1 | 0.[illegible] | 195. |
| 200. | 0.[illegible]9 | 0.[illegible]6 | 0.[illegible]3 | 0.[illegible]2 | [illegible].[illegible]4 | 0.[illegible]0 | 0.01 | 200. |
| 205. | 0.5[illegible] | 0.[illegible]3 | 0.[illegible]4 | 0.44 | [illegible].[illegible]2 | -0.[illegible]0 | -0.00 | 205. |
| 210. | 0.51 | 0.[illegible]1 | 0.[illegible]3 | 0.44 | [illegible].[illegible]0 | -0.[illegible]1 | -0.01 | 210. |
| 215. | 0.45 | 0.[illegible]8 | 0.[illegible]1 | 0.44 | [illegible].[illegible]7 | -0.[illegible]1 | -0.00 | 215. |
| 220. | 0.40 | 0.[illegible]4 | 0.[illegible]0 | 0.44 | [illegible].[illegible]5 | -0.[illegible]1 | 0.01 | 220. |
| 225. | 0.3[illegible] | 0.[illegible]4 | 0.[illegible]0 | 0.4[illegible] | [illegible].[illegible]3 | -0.[illegible]1 | -0.00 | 225. |
| 230. | 0.3[illegible] | 0.[illegible]3 | 0.[illegible]0 | 0.41 | [illegible].[illegible]2 | -0.[illegible]0 | 0.00 | 230. |
| 235. | 0.32 | 0.[illegible]0 | 0.[illegible]0 | 0.[illegible]0 | [illegible].[illegible]1 | 0.[illegible]1 | 0.[illegible]3 | 235. |
| 240. | 0.3[illegible] | 0.[illegible]1 | 0.[illegible]1 | 0.[illegible]2 | [illegible].[illegible]2 | 0.[illegible]4 | 0.[illegible]6 | 240. |
| 245. | 0.3[illegible] | 0.[illegible]0 | 0.[illegible]1 | 0.[illegible]1 | [illegible].[illegible]3 | 0.[illegible]7 | 0.[illegible]4 | 245. |
| 250. | 0.3[illegible] | 0.[illegible]1 | 0.[illegible]0 | 0.[illegible]4 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]6 | 250. |
| 255. | 0.4[illegible] | 0.[illegible]0 | 0.[illegible]1 | 0.[illegible]0 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]6 | 255. |
| 260. | 0.46 | 0.[illegible]1 | 0.[illegible]2 | 0.[illegible]1 | [illegible].[illegible]3 | 0.[illegible]7 | 0.[illegible]4 | 260. |
| 265. | 0.4[illegible] | 0.[illegible]3 | 0.[illegible]2 | 0.[illegible]0 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]5 | 265. |
| 270. | 0.51 | 0.[illegible]3 | 0.[illegible]4 | 0.40 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]5 | 270. |
| 275. | 0.54 | 0.[illegible]3 | 0.[illegible]4 | 0.[illegible]1 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]4 | 275. |
| 280. | 0.55 | 0.[illegible]4 | 0.[illegible]4 | 0.[illegible]1 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]3 | 280. |
| 285. | 0.56 | 0.[illegible]4 | 0.[illegible]3 | 0.[illegible]1 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]4 | 285. |
| 290. | 0.5[illegible] | 0.[illegible]3 | 0.[illegible]3 | 0.[illegible]1 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]4 | 290. |
| 295. | 0.61 | 0.[illegible]2 | 0.[illegible]4 | 0.[illegible]1 | [illegible].[illegible]5 | 0.[illegible]7 | 0.[illegible]4 | 295. |
| 300. | 0.6[illegible] | 0.[illegible]1 | 0.[illegible]3 | 0.[illegible]1 | [illegible].[illegible]0 | 0.[illegible]7 | 0.[illegible]5 | 300. |
| 305. | 0.6[illegible] | 0.[illegible]0 | 0.[illegible]3 | 0.[illegible]0 | [illegible].[illegible]2 | 0.[illegible]4 | 0.[illegible]7 | 305. |
| 310. | 0.6[illegible] | 0.[illegible]7 | 0.[illegible]4 | 0.[illegible]5 | [illegible].[illegible]4 | 0.[illegible]4 | 0.[illegible]8 | 310. |
| 315. | 0.6[illegible] | 0.[illegible]6 | 0.[illegible]4 | 0.[illegible]0 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]9 | 315. |
| 320. | 0.70 | 0.[illegible]9 | 0.[illegible]3 | 0.[illegible]0 | [illegible].[illegible]4 | 0.[illegible]7 | 0.[illegible]8 | 320. |
| 325. | 0.71 | 0.70 | 0.[illegible]7 | 0.[illegible]0 | [illegible].[illegible]4 | 0.[illegible]8 | 0.[illegible]7 | 325. |
| 330. | 0.52 | 0.47 | 0.[illegible]0 | 0.[illegible]4 | [illegible].[illegible]0 | 0.[illegible]2 | 0.07 | 330. |
| 335. | 0.0[illegible] | 0.17 | -0.[illegible]3 | 0.[illegible]3 | [illegible].[illegible]1 | -0.[illegible]4 | 0.[illegible]6 | 335. |
| 340. | -0.2[illegible] | -0.[illegible]5 | -0.[illegible]4 | 0.16 | [illegible].[illegible]5 | -0.[illegible]1 | 0.04 | 340. |
| 345. | -0.07 | 0.01 | -0.12 | 0.[illegible]7 | [illegible].[illegible]4 | -0.[illegible]9 | 0.04 | 345. |
| 350. | 0.08 | 0.[illegible]6 | -0.[illegible]7 | 0.[illegible]6 | [illegible].[illegible]0 | -0.[illegible]8 | 0.[illegible]3 | 350. |
| 355. | 0.04 | 0.[illegible]3 | -0.[illegible]5 | 0.[illegible]3 | [illegible].[illegible]7 | -0.[illegible]8 | 0.[illegible]8 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-500 CNTR NO. 970 YCH= 31. C.L.= 60.0

DIFFERENTIAL PRESSURES

SPAN STATION 100.0

| AZ | | | CHORD STATION | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| | .455 | 1.040 | | | | 7.140 | 10.400 | |
| DEG. | | | | | | | | DEG. |
| 0. | 0.01 | 0.14 | -0.30 | C.CC | C.13 | -0.07 | -0.05 | 0. |
| 5. | 1.17 | 0.84 | 0.17 | 0.44 | C.27 | 0.CC | -0.04 | 5. |
| 10. | 0.31 | 0.19 | -0.34 | C.29 | C.24 | -0.11 | -0.19 | 10. |
| 15. | -0.41 | -0.72 | -0.74 | -0.3C | C.C1 | -0.27 | -0.16 | 15. |
| 20. | -0.91 | -0.22 | -0.27 | -0.39 | C.C1 | -0.28 | -0.14 | 20. |
| 25. | 0.37 | 0.19 | -0.46 | -C.14 | C.16 | -0.19 | -0.10 | 25. |
| 30. | 1.17 | 0.74 | 0.28 | C.44 | -0.15 | -0.07 | 30. | |
| 35. | 1.45 | 1.27 | 1.19 | 1.02 | C.65 | -0.19 | -0.09 | 35. |
| 40. | 1.93 | 1.67 | 1.49 | 1.08 | C.70 | -0.24 | -0.17 | 40. |
| 45. | 1.99 | 1.87 | 1.48 | 1.38 | 1.11 | -0.15 | -0.25 | 45. |
| 50. | 1.74 | 1.74 | 1.49 | 1.CC | 1.27 | -0.00 | -0.28 | 50. |
| 55. | 1.28 | 1.35 | 1.35 | 0.99 | C.C3 | -0.03 | -0.28 | 55. |
| 60. | 1.15 | 1.14 | 1.32 | 0.9C | C.63 | -0.04 | -0.24 | 60. |
| 65. | 0.38 | 0.16 | 1.02 | -C.33 | C.70 | -0.41 | -0.16 | 65. |
| 70. | -1.36 | -1.06 | 0.42 | -1.C7 | -C.31 | -0.49 | -0.19 | 70. |
| 75. | -0.71 | -0.62 | 0.42 | -0.72 | -C.19 | -0.41 | -0.23 | 75. |
| 80. | -0.94 | -0.69 | 0.74 | -0.44 | -C.C3 | -0.41 | -0.06 | 80. |
| 85. | -0.91 | -0.85 | 0.44 | -0.69 | -C.17 | -0.45 | 0.27 | 85. |
| 90. | -1.00 | -1.04 | 0.40 | -0.67 | -0.78 | -0.84 | 0.42 | 90. |
| 95. | -1.17 | -1.12 | 0.11 | -0.72 | -0.96 | -0.72 | 0.82 | 95. |
| 100. | -1.71 | -1.33 | -0.21 | -0.89 | -0.98 | 0.48 | 0.70 | 100. |
| 105. | -2.31 | -1.97 | -0.94 | -1.11 | -C.CC | 1.47 | 1.08 | 105. |
| 110. | -2.79 | -2.72 | -0.67 | -1.48 | -1.20 | 2.16 | 0.74 | 110. |
| 115. | -3.11 | -3.01 | -1.30 | -1.84 | -1.09 | 1.64 | 0.04 | 115. |
| 120. | -3.22 | -3.00 | -1.47 | -2.00 | -1.60 | 1.38 | -0.48 | 120. |
| 125. | -3.01 | -2.77 | -1.40 | -1.87 | -1.02 | 1.34 | -0.89 | 125. |
| 130. | -2.69 | -2.48 | -1.09 | -1.56 | -1.08 | 0.84 | -0.42 | 130. |
| 135. | -2.28 | -2.00 | -0.62 | -1.48 | -1.89 | -1.14 | 0.16 | 135. |
| 140. | -1.94 | -1.41 | -0.43 | -2.14 | -2.32 | -0.94 | 0.78 | 140. |
| 145. | -1.88 | -1.46 | -1.28 | -2.18 | -1.20 | 0.14 | 0.11 | 145. |
| 150. | -1.79 | -1.49 | -1.49 | -0.87 | C.C3 | -0.25 | -0.08 | 150. |
| 155. | -1.49 | -1.07 | -1.28 | -0.C7 | -C.CA | -0.40 | -0.12 | 155. |
| 160. | -0.99 | -0.98 | -0.8C | 0.04 | -0.C3 | -0.34 | -0.07 | 160. |
| 165. | -0.48 | -0.79 | -0.54 | -C.C8 | C.11 | -0.23 | -0.04 | 165. |
| 170. | -0.10 | -0.09 | -0.31 | 0.07 | C.14 | -0.20 | -0.05 | 170. |
| 175. | 0.39 | 0.19 | -0.14 | C.14 | C.18 | -0.18 | -0.02 | 175. |
| 180. | 0.48 | 0.25 | -0.07 | C.27 | C.21 | -0.14 | -0.01 | 180. |
| 185. | 0.84 | 0.58 | -0.07 | C.39 | C.29 | -0.09 | -0.07 | 185. |
| 190. | 0.70 | 0.37 | 0.26 | C.34 | C.24 | -0.04 | -0.02 | 190. |
| 195. | 0.70 | 0.48 | 0.07 | 0.40 | C.25 | -0.CC | 0.00 | 195. |
| 200. | 0.69 | 0.52 | 0.10 | 0.44 | C.25 | 0.03 | 0.02 | 200. |
| 205. | 0.75 | 0.47 | 0.12 | 0.47 | C.2C | 0.04 | 0.01 | 205. |
| 210. | 0.74 | 0.41 | 0.13 | 0.48 | C.2C | 0.05 | 0.00 | 210. |
| 215. | 0.72 | 0.49 | 0.14 | 0.48 | C.24 | 0.04 | 0.01 | 215. |
| 220. | 0.68 | 0.41 | 0.14 | 0.49 | C.24 | 0.04 | 0.03 | 220. |
| 225. | 0.64 | 0.40 | 0.16 | 0.47 | C.23 | 0.07 | 0.03 | 225. |
| 230. | 0.62 | 0.44 | 0.15 | 0.46 | C.23 | 0.08 | 0.02 | 230. |
| 235. | 0.61 | 0.48 | 0.18 | 0.46 | C.23 | 0.10 | 0.04 | 235. |
| 240. | 0.61 | 0.46 | 0.14 | 0.44 | C.23 | 0.12 | 0.05 | 240. |
| 245. | 0.63 | 0.49 | 0.19 | 0.47 | C.24 | 0.14 | 0.04 | 245. |
| 250. | 0.66 | 0.48 | 0.18 | 0.48 | C.24 | 0.16 | 0.04 | 250. |
| 255. | 0.69 | 0.48 | 0.22 | 0.49 | C.25 | 0.18 | 0.04 | 255. |
| 260. | 0.73 | 0.52 | 0.24 | 0.51 | C.25 | 0.19 | 0.07 | 260. |
| 265. | 0.77 | 0.55 | 0.27 | C.54 | C.24 | 0.20 | 0.07 | 265. |
| 270. | 0.80 | 0.58 | 0.29 | C.54 | C.27 | 0.20 | 0.04 | 270. |
| 275. | 0.84 | 0.62 | 0.31 | C.58 | C.28 | 0.20 | 0.04 | 275. |
| 280. | 0.88 | 0.66 | 0.32 | 0.60 | C.28 | 0.20 | 0.04 | 280. |
| 285. | 0.92 | 0.67 | 0.32 | 0.63 | C.3C | 0.19 | 0.05 | 285. |
| 290. | 0.96 | 0.68 | 0.33 | C.60 | C.31 | 0.16 | 0.04 | 290. |
| 295. | 1.00 | 0.68 | 0.33 | 0.60 | C.31 | 0.16 | 0.03 | 295. |
| 300. | 1.02 | 0.67 | 0.31 | C.57 | C.29 | 0.15 | 0.03 | 300. |
| 305. | 1.07 | 0.66 | 0.30 | C.55 | C.26 | 0.14 | 0.04 | 305. |
| 310. | 1.06 | 0.67 | 0.27 | 0.54 | C.26 | 0.18 | 0.04 | 310. |
| 315. | 1.00 | 0.68 | 0.24 | 0.54 | C.26 | 0.17 | 0.04 | 315. |
| 320. | 1.03 | 0.64 | 0.24 | 0.47 | C.29 | 0.14 | 0.03 | 320. |
| 325. | 0.99 | 0.74 | 0.34 | 0.56 | C.28 | 0.17 | 0.03 | 325. |
| 330. | 0.84 | 0.61 | 0.17 | 0.60 | C.27 | 0.05 | -0.00 | 330. |
| 335. | 0.54 | 0.38 | -0.09 | 0.30 | C.19 | 0.04 | -0.04 | 335. |
| 340. | -0.12 | -0.06 | -0.37 | 0.04 | -.04 | -0.07 | -0.07 | 340. |
| 345. | -0.44 | -0.30 | -0.44 | -0.04 | -0.04 | -0.09 | -0.09 | 345. |
| 350. | -0.91 | -0.74 | -0.44 | -0.08 | -0.09 | -0.10 | -0.09 | 350. |
| 355. | -0.82 | -0.81 | -0.61 | -0.09 | -0.08 | -0.07 | -0.03 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 253 TCN= 33. C.R.= 32.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | | CHORD STATION | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.059 | 4.952 | 1.602 | DEG. |
| 0. | -0.04 | -0.41 | -0.28 | -0.01 | 0. |
| 5. | -0.14 | -0.31 | -0.21 | 0.02 | 5. |
| 10. | -0.34 | -0.16 | -0.13 | 0.03 | 10. |
| 15. | -0.16 | -0.05 | -0.07 | 0.02 | 15. |
| 20. | -0.07 | 0.01 | -0.08 | 0.00 | 20. |
| 25. | -0.13 | -0.04 | -0.11 | -0.02 | 25. |
| 30. | -0.35 | -0.15 | -0.15 | -0.03 | 30. |
| 35. | -0.42 | -0.17 | -0.12 | 0.00 | 35. |
| 40. | -0.28 | -0.13 | -0.09 | -0.00 | 40. |
| 45. | -0.11 | -0.07 | -0.12 | -0.02 | 45. |
| 50. | 0.00 | -0.04 | -0.12 | -0.02 | 50. |
| 55. | 0.07 | -0.02 | -0.09 | -0.02 | 55. |
| 60. | 0.11 | -0.01 | -0.07 | -0.02 | 60. |
| 65. | 0.12 | -0.01 | -0.06 | -0.02 | 65. |
| 70. | 0.12 | -0.01 | -0.06 | -0.03 | 70. |
| 75. | 0.12 | 0.01 | 0.00 | -0.03 | 75. |
| 80. | 0.16 | 0.04 | 0.02 | -0.03 | 80. |
| 85. | 0.22 | 0.07 | 0.05 | -0.02 | 85. |
| 90. | 0.30 | 0.10 | 0.10 | -0.01 | 90. |
| 95. | 0.40 | 0.14 | 0.12 | -0.01 | 95. |
| 100. | 0.51 | 0.19 | 0.14 | -0.01 | 100. |
| 105. | 0.61 | 0.25 | 0.17 | -0.01 | 105. |
| 110. | 0.72 | 0.29 | 0.20 | -0.00 | 110. |
| 115. | 0.77 | 0.32 | 0.24 | 0.02 | 115. |
| 120. | 0.81 | 0.34 | 0.28 | 0.02 | 120. |
| 125. | 0.82 | 0.37 | 0.31 | 0.02 | 125. |
| 130. | 0.83 | 0.39 | 0.32 | 0.03 | 130. |
| 135. | 0.84 | 0.41 | 0.32 | 0.03 | 135. |
| 140. | 0.87 | 0.43 | 0.33 | 0.04 | 140. |
| 145. | 0.89 | 0.44 | 0.35 | 0.04 | 145. |
| 150. | 0.92 | 0.45 | 0.37 | 0.04 | 150. |
| 155. | 0.93 | 0.45 | 0.39 | 0.03 | 155. |
| 160. | 0.92 | 0.43 | 0.40 | 0.02 | 160. |
| 165. | 0.87 | 0.41 | 0.41 | 0.03 | 165. |
| 170. | 0.86 | 0.37 | 0.42 | 0.03 | 170. |
| 175. | 0.88 | 0.32 | 0.43 | 0.02 | 175. |
| 180. | 0.93 | 0.25 | 0.35 | 0.00 | 180. |
| 185. | 0.95 | 0.15 | 0.29 | -0.00 | 185. |
| 190. | 0.97 | 0.06 | 0.22 | -0.01 | 190. |
| 195. | 1.00 | -0.02 | 0.13 | 0.00 | 195. |
| 200. | -0.11 | -0.03 | 0.08 | 0.00 | 200. |
| 205. | -0.14 | 0.01 | 0.03 | 0.01 | 205. |
| 210. | -0.27 | -0.03 | -0.02 | 0.01 | 210. |
| 215. | -0.33 | -0.09 | -0.07 | 0.01 | 215. |
| 220. | -0.36 | -0.14 | -0.10 | 0.01 | 220. |
| 225. | -0.37 | -0.16 | -0.13 | -0.00 | 225. |
| 230. | -0.36 | -0.17 | -0.15 | -0.01 | 230. |
| 235. | -0.34 | -0.17 | -0.17 | -0.01 | 235. |
| 240. | -0.32 | -0.17 | -0.18 | -0.01 | 240. |
| 245. | -0.32 | -0.17 | -0.18 | -0.00 | 245. |
| 250. | -0.32 | -0.16 | -0.18 | -0.00 | 250. |
| 255. | -0.33 | -0.15 | -0.18 | -0.01 | 255. |
| 260. | -0.33 | -0.15 | -0.18 | -0.01 | 260. |
| 265. | -0.33 | -0.15 | -0.18 | -0.01 | 265. |
| 270. | -0.34 | -0.14 | -0.18 | -0.01 | 270. |
| 275. | -0.34 | -0.14 | -0.18 | -0.01 | 275. |
| 280. | -0.35 | -0.14 | -0.18 | -0.01 | 280. |
| 285. | -0.35 | -0.14 | -0.17 | -0.01 | 285. |
| 290. | -0.36 | -0.14 | -0.16 | -0.01 | 290. |
| 295. | -0.36 | -0.14 | -0.15 | -0.01 | 295. |
| 300. | -0.34 | -0.14 | -0.14 | -0.01 | 300. |
| 305. | -0.31 | -0.14 | -0.14 | -0.01 | 305. |
| 310. | -0.28 | -0.14 | -0.13 | -0.01 | 310. |
| 315. | -0.27 | -0.14 | -0.13 | -0.01 | 315. |
| 320. | -0.29 | -0.15 | -0.14 | -0.01 | 320. |
| 325. | -0.33 | -0.17 | -0.16 | -0.01 | 325. |
| 330. | -0.42 | -0.21 | -0.18 | -0.01 | 330. |
| 335. | -0.54 | -0.25 | -0.18 | -0.00 | 335. |
| 340. | -0.54 | -0.27 | -0.16 | -0.00 | 340. |
| 345. | -0.64 | -0.28 | -0.16 | -0.00 | 345. |
| 350. | -0.79 | -0.30 | -0.19 | -0.00 | 350. |
| 355. | -0.78 | -0.30 | -0.24 | -0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-498 CNTR NO. 253 TCN= 33. C.R.= 32.2

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.090 | 1.992 | 2.992 | 4.350 | 7.150 | 12.420 | DEG. |
| 0. | -1.31 | -0.71 | -0.44 | -0.25 | -0.25 | -0.11 | -0.05 | 0. |
| 5. | -1.90 | -0.65 | -0.48 | -0.25 | -0.19 | -0.10 | -0.02 | 5. |
| 10. | -1.76 | -0.54 | -0.37 | -0.18 | -0.18 | -0.09 | -0.00 | 10. |
| 15. | -1.70 | -0.49 | -0.34 | -0.15 | -0.18 | -0.13 | -0.07 | 15. |
| 20. | -0.55 | -0.42 | -0.31 | -0.14 | -0.18 | -0.09 | -0.02 | 20. |
| 25. | -0.58 | -0.40 | -0.32 | -0.14 | -0.15 | -0.09 | -0.02 | 25. |
| 30. | -0.43 | -0.27 | -0.22 | -0.09 | -0.08 | -0.08 | -0.01 | 30. |
| 35. | -0.24 | -0.19 | -0.18 | -0.04 | -0.08 | -0.09 | -0.01 | 35. |
| 40. | -0.15 | -0.16 | -0.16 | -0.04 | -0.09 | -0.13 | -0.02 | 40. |
| 45. | -0.11 | -0.14 | -0.16 | -0.03 | -0.08 | -0.13 | -0.03 | 45. |
| 50. | -0.09 | -0.14 | -0.14 | -0.01 | -0.06 | -0.09 | -0.03 | 50. |
| 55. | -0.07 | -0.10 | -0.15 | 0.01 | -0.02 | -0.08 | -0.02 | 55. |
| 60. | -0.04 | -0.06 | -0.11 | 0.03 | -0.02 | -0.08 | -0.02 | 60. |
| 65. | -0.00 | -0.01 | -0.08 | 0.04 | -0.00 | -0.07 | -0.02 | 65. |
| 70. | 0.05 | 0.03 | -0.05 | 0.08 | 0.03 | -0.07 | -0.02 | 70. |
| 75. | 0.11 | 0.07 | -0.02 | 0.06 | 0.07 | -0.05 | -0.02 | 75. |
| 80. | 0.19 | 0.11 | 0.02 | 0.06 | 0.10 | -0.04 | -0.01 | 80. |
| 85. | 0.27 | 0.16 | 0.07 | 0.09 | 0.14 | -0.03 | 0.00 | 85. |
| 90. | 0.37 | 0.24 | 0.12 | 0.12 | 0.17 | -0.02 | 0.01 | 90. |
| 95. | 0.47 | 0.31 | 0.18 | 0.14 | 0.22 | -0.03 | 0.01 | 95. |
| 100. | 0.56 | 0.38 | 0.23 | 0.17 | 0.22 | 0.01 | 0.01 | 100. |
| 105. | 0.65 | 0.45 | 0.27 | 0.20 | 0.24 | 0.03 | 0.02 | 105. |
| 110. | 0.73 | 0.51 | 0.32 | 0.23 | 0.26 | 0.05 | 0.03 | 110. |
| 115. | 0.82 | 0.55 | 0.36 | 0.26 | 0.29 | 0.08 | 0.04 | 115. |
| 120. | 0.90 | 0.60 | 0.40 | 0.29 | 0.32 | 0.10 | 0.05 | 120. |
| 125. | 0.98 | 0.64 | 0.45 | 0.32 | 0.35 | 0.12 | 0.05 | 125. |
| 130. | 1.05 | 0.69 | 0.49 | 0.33 | 0.36 | 0.14 | 0.06 | 130. |
| 135. | 1.12 | 0.73 | 0.52 | 0.34 | 0.36 | 0.14 | 0.06 | 135. |
| 140. | 1.19 | 0.78 | 0.55 | 0.34 | 0.36 | 0.15 | 0.07 | 140. |
| 145. | 1.26 | 0.82 | 0.58 | 0.34 | 0.37 | 0.15 | 0.07 | 145. |
| 150. | 1.34 | 0.88 | 0.64 | 0.34 | 0.37 | 0.16 | 0.07 | 150. |
| 155. | 1.43 | 0.95 | 0.69 | 0.32 | 0.38 | 0.18 | 0.06 | 155. |
| 160. | 1.53 | 0.99 | 0.73 | 0.31 | 0.39 | 0.18 | 0.07 | 160. |
| 165. | 1.56 | 1.00 | 0.75 | 0.28 | 0.34 | 0.17 | 0.07 | 165. |
| 170. | 1.52 | 0.97 | 0.74 | 0.25 | 0.35 | 0.20 | 0.06 | 170. |
| 175. | 1.43 | 0.90 | 0.69 | 0.21 | 0.33 | 0.19 | 0.06 | 175. |
| 180. | 1.28 | 0.80 | 0.61 | 0.16 | 0.26 | 0.18 | 0.05 | 180. |
| 185. | 1.05 | 0.65 | 0.52 | 0.11 | 0.21 | 0.15 | 0.05 | 185. |
| 190. | 0.78 | 0.45 | 0.40 | 0.06 | 0.14 | 0.12 | 0.04 | 190. |
| 195. | 0.48 | 0.24 | 0.29 | -0.00 | 0.06 | 0.09 | 0.02 | 195. |
| 200. | 0.20 | 0.10 | 0.17 | -0.07 | -0.02 | 0.04 | 0.01 | 200. |
| 205. | -0.02 | -0.00 | 0.05 | -0.11 | -0.05 | 0.03 | -0.01 | 205. |
| 210. | -0.20 | -0.07 | -0.03 | -0.12 | -0.05 | 0.02 | 0.00 | 210. |
| 215. | -0.31 | -0.06 | -0.05 | -0.11 | -0.06 | 0.01 | 0.01 | 215. |
| 220. | -0.39 | -0.02 | -0.13 | -0.11 | -0.09 | -0.01 | -0.00 | 220. |
| 225. | -0.46 | 0.01 | -0.19 | -0.12 | -0.13 | -0.02 | -0.01 | 225. |
| 230. | -0.52 | -0.07 | -0.23 | -0.12 | -0.15 | -0.03 | -0.02 | 230. |
| 235. | -0.56 | -0.18 | -0.25 | -0.12 | -0.16 | -0.04 | -0.02 | 235. |
| 240. | -0.61 | -0.30 | -0.24 | -0.12 | -0.17 | -0.05 | -0.02 | 240. |
| 245. | -0.65 | -0.37 | -0.22 | -0.12 | -0.19 | -0.06 | -0.03 | 245. |
| 250. | -0.67 | -0.42 | -0.23 | -0.12 | -0.19 | -0.06 | -0.04 | 250. |
| 255. | -0.68 | -0.44 | -0.25 | -0.13 | -0.20 | -0.06 | -0.05 | 255. |
| 260. | -0.68 | -0.46 | -0.26 | -0.13 | -0.20 | -0.06 | -0.05 | 260. |
| 265. | -0.67 | -0.46 | -0.27 | -0.13 | -0.20 | -0.06 | -0.05 | 265. |
| 270. | -0.67 | -0.46 | -0.27 | -0.13 | -0.20 | -0.06 | -0.04 | 270. |
| 275. | -0.67 | -0.47 | -0.27 | -0.13 | -0.19 | -0.05 | -0.04 | 275. |
| 280. | -0.67 | -0.47 | -0.27 | -0.13 | -0.19 | -0.05 | -0.04 | 280. |
| 285. | -0.67 | -0.46 | -0.27 | -0.13 | -0.19 | -0.04 | -0.04 | 285. |
| 290. | -0.67 | -0.46 | -0.27 | -0.13 | -0.19 | -0.04 | -0.03 | 290. |
| 295. | -0.67 | -0.46 | -0.27 | -0.13 | -0.18 | -0.05 | -0.03 | 295. |
| 300. | -0.66 | -0.46 | -0.27 | -0.13 | -0.18 | -0.05 | -0.03 | 300. |
| 305. | -0.64 | -0.46 | -0.28 | -0.13 | -0.18 | -0.05 | -0.02 | 305. |
| 310. | -0.66 | -0.45 | -0.28 | -0.12 | -0.18 | -0.04 | -0.02 | 310. |
| 315. | -0.65 | -0.45 | -0.29 | -0.12 | -0.17 | -0.04 | -0.01 | 315. |
| 320. | -0.65 | -0.45 | -0.28 | -0.12 | -0.18 | -0.04 | -0.01 | 320. |
| 325. | -0.64 | -0.44 | -0.28 | -0.12 | -0.19 | -0.04 | -0.01 | 325. |
| 330. | -0.58 | -0.41 | -0.26 | -0.13 | -0.18 | -0.03 | -0.01 | 330. |
| 335. | -0.58 | -0.37 | -0.24 | -0.15 | -0.17 | -0.03 | -0.01 | 335. |
| 340. | -0.45 | -0.37 | -0.23 | -0.16 | -0.15 | -0.02 | -0.01 | 340. |
| 345. | -0.59 | -0.43 | -0.29 | -0.15 | -0.17 | -0.02 | -0.00 | 345. |
| 350. | -0.54 | -0.42 | -0.32 | -0.16 | -0.18 | -0.03 | 0.01 | 350. |
| 355. | -0.58 | -0.41 | -0.31 | -0.19 | -0.20 | -0.06 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNFR NO. 253 TCN= 33. C.R.= 32.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.042 | 1.955 | 2.990 | 4.552 | 7.150 | 10.490 | DEG. |
| 0. | -0.90 | -0.54 | -0.30 | -0.26 | -0.23 | -0.10 | -0.03 | 0. |
| 5. | -0.86 | -0.63 | -0.43 | -0.29 | -0.21 | -0.12 | -0.05 | 5. |
| 10. | -0.73 | -0.55 | -0.35 | -0.25 | -0.18 | -0.14 | -0.06 | 10. |
| 15. | -0.58 | -0.48 | -0.32 | -0.22 | -0.13 | -0.13 | -0.05 | 15. |
| 20. | -0.38 | -0.33 | -0.22 | -0.17 | -0.07 | -0.12 | -0.06 | 20. |
| 25. | -0.15 | -0.22 | -0.10 | -0.10 | -0.01 | -0.10 | -0.07 | 25. |
| 30. | 0.03 | -0.13 | -0.05 | -0.08 | 0.01 | -0.09 | -0.07 | 30. |
| 35. | 0.23 | -0.01 | -0.01 | -0.05 | 0.04 | -0.08 | -0.07 | 35. |
| 40. | 0.40 | 0.07 | 0.03 | 0.01 | 0.07 | -0.07 | -0.08 | 40. |
| 45. | 0.55 | 0.18 | 0.11 | 0.08 | 0.10 | -0.04 | -0.08 | 45. |
| 50. | 0.66 | 0.28 | 0.14 | 0.12 | 0.17 | -0.05 | -0.07 | 50. |
| 55. | 0.74 | 0.32 | 0.20 | 0.14 | 0.22 | -0.04 | -0.07 | 55. |
| 60. | 0.82 | 0.33 | 0.23 | 0.15 | 0.24 | -0.04 | -0.07 | 60. |
| 65. | 0.86 | 0.35 | 0.23 | 0.15 | 0.25 | -0.04 | -0.07 | 65. |
| 70. | 0.92 | 0.35 | 0.19 | 0.13 | 0.23 | -0.05 | -0.07 | 70. |
| 75. | 0.76 | 0.32 | 0.14 | 0.11 | 0.22 | -0.04 | -0.07 | 75. |
| 80. | 0.69 | 0.27 | 0.11 | 0.08 | 0.22 | -0.04 | -0.06 | 80. |
| 85. | 0.64 | 0.22 | 0.08 | 0.07 | 0.21 | -0.05 | -0.06 | 85. |
| 90. | 0.62 | 0.20 | 0.07 | 0.01 | 0.21 | -0.06 | -0.07 | 90. |
| 95. | 0.62 | 0.21 | 0.07 | 0.06 | 0.21 | -0.05 | -0.06 | 95. |
| 100. | 0.65 | 0.25 | 0.08 | 0.07 | 0.21 | -0.02 | -0.04 | 100. |
| 105. | 0.70 | 0.28 | 0.10 | 0.08 | 0.22 | 0.03 | -0.04 | 105. |
| 110. | 0.74 | 0.31 | 0.13 | 0.09 | 0.22 | 0.01 | -0.03 | 110. |
| 115. | 0.73 | 0.33 | 0.14 | 0.11 | 0.22 | 0.00 | -0.02 | 115. |
| 120. | 0.68 | 0.34 | 0.15 | 0.11 | 0.21 | 0.01 | -0.01 | 120. |
| 125. | 0.64 | 0.34 | 0.15 | 0.11 | 0.21 | 0.02 | 0.00 | 125. |
| 130. | 0.60 | 0.32 | 0.15 | 0.12 | 0.20 | 0.03 | 0.01 | 130. |
| 135. | 0.56 | 0.31 | 0.14 | 0.12 | 0.19 | 0.04 | 0.01 | 135. |
| 140. | 0.55 | 0.31 | 0.14 | 0.10 | 0.18 | 0.06 | 0.02 | 140. |
| 145. | 0.59 | 0.36 | 0.21 | 0.13 | 0.18 | 0.07 | 0.02 | 145. |
| 150. | 0.70 | 0.44 | 0.28 | 0.18 | 0.20 | 0.08 | 0.04 | 150. |
| 155. | 0.84 | 0.55 | 0.35 | 0.25 | 0.23 | 0.11 | 0.05 | 155. |
| 160. | 0.96 | 0.66 | 0.45 | 0.31 | 0.25 | 0.13 | 0.07 | 160. |
| 165. | 1.05 | 0.77 | 0.52 | 0.37 | 0.29 | 0.16 | 0.08 | 165. |
| 170. | 1.10 | 0.86 | 0.57 | 0.41 | 0.29 | 0.18 | 0.09 | 170. |
| 175. | 1.09 | 0.88 | 0.58 | 0.44 | 0.28 | 0.20 | 0.09 | 175. |
| 180. | 1.02 | 0.84 | 0.58 | 0.43 | 0.26 | 0.19 | 0.10 | 180. |
| 185. | 0.89 | 0.74 | 0.54 | 0.39 | 0.22 | 0.17 | 0.10 | 185. |
| 190. | 0.71 | 0.62 | 0.47 | 0.32 | 0.16 | 0.15 | 0.09 | 190. |
| 195. | 0.52 | 0.51 | 0.38 | 0.26 | 0.10 | 0.13 | 0.07 | 195. |
| 200. | 0.32 | 0.40 | 0.29 | 0.20 | 0.04 | 0.11 | 0.06 | 200. |
| 205. | 0.14 | 0.27 | 0.19 | 0.14 | -0.02 | 0.09 | 0.05 | 205. |
| 210. | -0.03 | 0.15 | 0.11 | 0.09 | -0.04 | 0.06 | 0.05 | 210. |
| 215. | -0.17 | 0.04 | 0.05 | 0.03 | -0.07 | 0.05 | 0.05 | 215. |
| 220. | -0.26 | -0.04 | -0.01 | -0.01 | -0.10 | 0.05 | 0.05 | 220. |
| 225. | -0.34 | -0.10 | -0.05 | -0.04 | -0.13 | 0.04 | 0.04 | 225. |
| 230. | -0.44 | -0.16 | -0.09 | -0.07 | -0.15 | 0.04 | 0.04 | 230. |
| 235. | -0.53 | -0.22 | -0.12 | -0.09 | -0.17 | 0.03 | 0.04 | 235. |
| 240. | -0.60 | -0.28 | -0.15 | -0.11 | -0.19 | 0.01 | 0.03 | 240. |
| 245. | -0.66 | -0.32 | -0.17 | -0.14 | -0.21 | -0.00 | 0.03 | 245. |
| 250. | -0.70 | -0.33 | -0.20 | -0.13 | -0.22 | -0.01 | 0.02 | 250. |
| 255. | -0.72 | -0.34 | -0.22 | -0.16 | -0.22 | -0.01 | 0.02 | 255. |
| 260. | -0.75 | -0.35 | -0.23 | -0.16 | -0.23 | -0.01 | 0.02 | 260. |
| 265. | -0.76 | -0.35 | -0.24 | -0.17 | -0.23 | -0.02 | 0.02 | 265. |
| 270. | -0.78 | -0.34 | -0.23 | -0.17 | -0.23 | -0.02 | 0.02 | 270. |
| 275. | -0.85 | -0.35 | -0.19 | -0.16 | -0.24 | -0.02 | 0.02 | 275. |
| 280. | -0.92 | -0.41 | -0.20 | -0.16 | -0.22 | -0.04 | 0.02 | 280. |
| 285. | -0.95 | -0.46 | -0.25 | -0.11 | -0.17 | -0.04 | 0.02 | 285. |
| 290. | -0.93 | -0.47 | -0.28 | -0.15 | -0.16 | -0.01 | 0.01 | 290. |
| 295. | -0.88 | -0.49 | -0.26 | -0.25 | -0.18 | 0.05 | 0.02 | 295. |
| 300. | -0.82 | -0.49 | -0.27 | -0.22 | -0.21 | 0.04 | 0.05 | 300. |
| 305. | -0.77 | -0.47 | -0.27 | -0.21 | -0.22 | -0.02 | 0.03 | 305. |
| 310. | -0.71 | -0.42 | -0.26 | -0.19 | -0.21 | -0.04 | 0.01 | 310. |
| 315. | -0.66 | -0.37 | -0.24 | -0.17 | -0.21 | -0.03 | 0.00 | 315. |
| 320. | -0.63 | -0.36 | -0.21 | -0.15 | -0.20 | -0.03 | 0.01 | 320. |
| 325. | -0.73 | -0.43 | -0.24 | -0.16 | -0.21 | -0.03 | 0.02 | 325. |
| 330. | -0.87 | -0.55 | -0.33 | -0.21 | -0.23 | -0.04 | 0.00 | 330. |
| 335. | -0.92 | -0.59 | -0.35 | -0.25 | -0.26 | -0.06 | -0.02 | 335. |
| 340. | -0.83 | -0.54 | -0.36 | -0.23 | -0.25 | -0.04 | -0.02 | 340. |
| 345. | -0.83 | -0.55 | -0.35 | -0.23 | -0.24 | -0.10 | -0.03 | 345. |
| 350. | -0.90 | -0.60 | -0.39 | -0.28 | -0.26 | -0.11 | -0.05 | 350. |
| 355. | -0.85 | -0.61 | -0.43 | -0.32 | -0.26 | -0.11 | -0.05 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 251 TC%= 33. Q.R.= 32.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.044 | 1.950 | 2.390 | 4.553 | 7.153 | 10.4.0 | DEG. |
| 0. | -1.35 | -0.76 | -0.40 | -1.49 | -0.25 | -0.13 | -0.03 | 0. |
| 5. | -0.13 | -0.16 | 0.05 | -0.32 | -0.08 | -0.05 | -0.01 | 5. |
| 10. | 0.02 | -0.07 | 0.03 | -0.25 | -0.06 | -0.07 | -0.03 | 10. |
| 15. | -0.13 | -0.17 | -0.07 | -0.20 | -0.08 | -0.07 | -0.02 | 15. |
| 20. | -0.04 | -0.08 | -0.01 | -0.15 | -0.03 | -0.07 | -0.02 | 20. |
| 25. | 0.18 | 0.06 | 0.09 | -0.10 | 0.05 | -0.06 | -0.02 | 25. |
| 30. | 0.41 | 0.23 | 0.12 | -0.07 | 0.07 | -0.07 | -0.02 | 30. |
| 35. | 0.62 | 0.45 | 0.24 | 0.06 | 0.13 | -0.05 | -0.02 | 35. |
| 40. | 0.81 | 0.68 | 0.39 | 0.21 | 0.22 | -0.07 | -0.01 | 40. |
| 45. | 0.96 | 0.86 | 0.52 | 0.35 | 0.28 | 0.01 | -0.03 | 45. |
| 50. | 1.05 | 0.93 | 0.61 | 0.46 | 0.33 | 0.02 | -0.06 | 50. |
| 55. | 1.07 | 0.95 | 0.66 | 0.50 | 0.34 | 0.02 | -0.0 | 55. |
| 60. | 1.02 | 0.91 | 0.68 | 0.52 | 0.34 | 0.03 | -0.01 | 60. |
| 65. | 0.93 | 0.82 | 0.64 | 0.49 | 0.33 | -0.01 | -0.02 | 65. |
| 70. | 0.73 | 0.71 | 0.53 | 0.42 | 0.33 | -0.02 | -0.02 | 70. |
| 75. | 0.55 | 0.58 | 0.43 | 0.40 | 0.32 | -0.04 | -0.03 | 75. |
| 80. | 0.42 | 0.44 | 0.32 | 0.36 | 0.29 | -0.06 | -0.04 | 80. |
| 85. | 0.29 | 0.31 | 0.24 | 0.30 | 0.23 | -0.11 | -0.05 | 85. |
| 90. | 0.14 | 0.16 | 0.16 | 0.23 | 0.17 | -0.16 | -0.07 | 90. |
| 95. | -0.03 | -0.01 | 0.06 | 0.13 | 0.11 | -0.17 | -0.07 | 95. |
| 100. | -0.22 | -0.19 | -0.06 | 0.03 | 0.06 | -0.17 | -0.07 | 100. |
| 105. | -0.42 | -0.33 | -0.21 | -0.09 | 0.02 | -0.18 | -0.07 | 105. |
| 110. | -0.65 | -0.47 | -0.37 | -0.22 | -0.08 | -0.21 | -0.08 | 110. |
| 115. | -0.94 | -0.66 | -0.51 | -0.28 | -0.11 | -0.23 | -0.09 | 115. |
| 120. | -1.13 | -0.79 | -0.60 | -0.32 | -0.16 | -0.23 | -0.08 | 120. |
| 125. | -1.14 | -0.80 | -0.61 | -0.32 | -0.17 | -0.23 | -0.08 | 125. |
| 130. | -1.00 | -0.75 | -0.55 | -0.30 | -0.15 | -0.21 | -0.07 | 130. |
| 135. | -0.99 | -0.62 | -0.45 | -0.27 | -0.12 | -0.19 | -0.06 | 135. |
| 140. | -0.83 | -0.44 | -0.34 | -0.22 | -0.07 | -0.15 | -0.04 | 140. |
| 145. | -0.64 | -0.24 | -0.21 | -0.15 | -0.02 | -0.12 | -0.04 | 145. |
| 150. | -0.45 | -0.04 | -0.08 | -0.08 | 0.02 | -0.07 | -0.03 | 150. |
| 155. | -0.22 | 0.19 | 0.06 | -0.01 | 0.06 | -0.03 | -0.01 | 155. |
| 160. | 0.04 | 0.33 | 0.19 | 0.06 | 0.07 | 0.01 | 0.00 | 160. |
| 165. | 0.28 | 0.39 | 0.32 | 0.12 | 0.11 | 0.04 | 0.01 | 165. |
| 170. | 0.46 | 0.43 | 0.39 | 0.17 | 0.21 | 0.07 | 0.03 | 170. |
| 175. | 0.56 | 0.43 | 0.44 | 0.21 | 0.23 | 0.13 | 0.03 | 175. |
| 180. | 0.61 | 0.43 | 0.47 | 0.22 | 0.22 | 0.12 | 0.04 | 180. |
| 185. | 0.61 | 0.41 | 0.46 | 0.22 | 0.18 | 0.13 | 0.04 | 185. |
| 190. | 0.58 | 0.38 | 0.42 | 0.20 | 0.15 | 0.13 | 0.04 | 190. |
| 195. | 0.52 | 0.35 | 0.35 | 0.19 | 0.11 | 0.13 | 0.04 | 195. |
| 200. | 0.43 | 0.28 | 0.27 | 0.16 | 0.04 | 0.12 | 0.03 | 200. |
| 205. | 0.32 | 0.18 | 0.20 | 0.13 | 0.03 | 0.11 | 0.03 | 205. |
| 210. | 0.20 | 0.07 | 0.12 | 0.09 | 0.00 | 0.10 | 0.03 | 210. |
| 215. | 0.09 | -0.02 | 0.05 | 0.05 | -0.03 | 0.10 | 0.03 | 215. |
| 220. | -0.01 | -0.09 | 0.01 | 0.03 | -0.07 | 0.09 | 0.03 | 220. |
| 225. | -0.08 | -0.13 | -0.04 | 0.02 | -0.10 | 0.09 | 0.03 | 225. |
| 230. | -0.14 | -0.14 | -0.10 | -0.02 | -0.11 | 0.09 | 0.04 | 230. |
| 235. | -0.18 | -0.16 | -0.15 | -0.03 | -0.12 | 0.09 | 0.04 | 235. |
| 240. | -0.21 | -0.23 | -0.20 | -0.05 | -0.11 | 0.09 | 0.04 | 240. |
| 245. | -0.24 | -0.26 | -0.24 | -0.06 | -0.15 | 0.08 | 0.04 | 245. |
| 250. | -0.26 | -0.28 | -0.25 | -0.08 | -0.16 | 0.08 | 0.04 | 250. |
| 255. | -0.28 | -0.29 | -0.25 | -0.10 | -0.17 | 0.04 | 0.03 | 255. |
| 260. | -0.28 | -0.28 | -0.25 | -0.11 | -0.17 | 0.09 | 0.03 | 260. |
| 265. | -0.28 | -0.28 | -0.25 | -0.13 | -0.17 | 0.07 | 0.03 | 265. |
| 270. | -0.28 | -0.28 | -0.23 | -0.13 | -0.16 | 0.07 | 0.02 | 270. |
| 275. | -0.27 | -0.27 | -0.22 | -0.13 | -0.15 | 0.07 | 0.02 | 275. |
| 280. | -0.25 | -0.26 | -0.22 | -0.13 | -0.15 | 0.07 | 0.02 | 280. |
| 285. | -0.22 | -0.23 | -0.22 | -0.11 | -0.17 | 0.08 | 0.03 | 285. |
| 290. | -0.19 | -0.20 | -0.21 | -0.09 | -0.13 | 0.09 | 0.03 | 290. |
| 295. | -0.12 | -0.18 | -0.20 | -0.05 | -0.11 | 0.09 | 0.04 | 295. |
| 300. | -0.05 | -0.15 | -0.17 | -0.02 | -0.09 | 0.10 | 0.04 | 300. |
| 305. | 0.01 | -0.11 | -0.15 | -0.01 | -0.09 | 0.10 | 0.04 | 305. |
| 310. | 0.04 | -0.08 | -0.13 | -0.02 | -0.09 | 0.09 | 0.05 | 310. |
| 315. | 0.04 | -0.07 | -0.12 | -0.03 | -0.09 | 0.09 | 0.05 | 315. |
| 320. | 0.04 | -0.08 | -0.12 | -0.03 | -0.09 | 0.09 | 0.04 | 320. |
| 325. | 0.02 | -0.09 | -0.11 | -0.03 | -0.09 | 0.09 | 0.04 | 325. |
| 330. | 0.03 | -0.10 | -0.05 | -0.01 | -0.10 | 0.09 | 0.04 | 330. |
| 335. | 0.12 | -0.06 | -0.01 | 0.03 | -0.09 | 0.08 | 0.04 | 335. |
| 340. | 0.36 | 0.04 | -0.04 | 0.02 | -0.04 | 0.06 | 0.04 | 340. |
| 345. | -0.02 | -0.04 | -0.21 | -0.12 | -0.07 | 0.01 | 0.01 | 345. |
| 350. | -0.54 | -0.49 | -0.43 | -0.31 | -0.20 | -0.05 | 0.01 | 350. |
| 355. | -0.95 | -0.54 | -0.45 | -0.34 | -0.27 | -0.08 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 259 ICN= 33. Q.P.= 32.9

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.342 | 1.953 | 2.996 | 4.550 | 7.153 | 10.433 | DEG. |
| 0. | -0.04 | 0.15 | 0.22 | 0.26 | -0.30 | -0.45 | 0.01 | 0. |
| 5. | -0.05 | -0.02 | -0.07 | 0.05 | -0.07 | -0.08 | 0.01 | 5. |
| 10. | 0.04 | -0.17 | -0.07 | 0.16 | -0.06 | -0.07 | 0.01 | 10. |
| 15. | 0.11 | 0.10 | 0.06 | 0.08 | 0.02 | -0.04 | 0.02 | 15. |
| 20. | 0.14 | 0.28 | 0.14 | 0.10 | 0.02 | -0.03 | 0.01 | 20. |
| 25. | 0.17 | 0.41 | 0.19 | 0.11 | 0.02 | -0.03 | 0.01 | 25. |
| 30. | 0.20 | 0.52 | 0.23 | 0.14 | 0.05 | -0.01 | 0.03 | 30. |
| 35. | 0.36 | 0.62 | 0.33 | 0.18 | 0.12 | 0.04 | 0.05 | 35. |
| 40. | 0.37 | 0.69 | 0.44 | 0.24 | 0.18 | 0.07 | 0.05 | 40. |
| 45. | 0.34 | 0.74 | 0.53 | 0.28 | 0.23 | 0.09 | 0.05 | 45. |
| 50. | 0.29 | 0.79 | 0.54 | 0.30 | 0.25 | 0.10 | 0.04 | 50. |
| 55. | 0.22 | 0.79 | 0.55 | 0.32 | 0.27 | 0.11 | 0.04 | 55. |
| 60. | 0.16 | 0.76 | 0.49 | 0.31 | 0.27 | 0.09 | 0.04 | 60. |
| 65. | 0.05 | 0.59 | 0.28 | 0.41 | 0.24 | 0.07 | 0.03 | 65. |
| 70. | -0.12 | 0.47 | 0.15 | 0.06 | 0.19 | 0.03 | 0.01 | 70. |
| 75. | -0.14 | 0.33 | -0.03 | 0.72 | 0.11 | -0.02 | 0.03 | 75. |
| 80. | -0.14 | 0.17 | -0.19 | 0.08 | -0.00 | -0.08 | -0.01 | 80. |
| 85. | -0.40 | -0.03 | -0.31 | 0.52 | -0.16 | -0.15 | -0.03 | 85. |
| 90. | -0.66 | -0.28 | -0.50 | 0.23 | -0.37 | -0.18 | -0.05 | 90. |
| 95. | -0.86 | -0.61 | -0.88 | -0.23 | -0.48 | -0.20 | -0.03 | 95. |
| 100. | -0.95 | -0.96 | -1.11 | -0.79 | -0.52 | -0.22 | -0.03 | 100. |
| 105. | -0.99 | -1.24 | -1.29 | -1.17 | -0.52 | -0.19 | -0.03 | 105. |
| 110. | -1.01 | -1.37 | -1.47 | -1.29 | -0.51 | -0.19 | -0.04 | 110. |
| 115. | -1.01 | -1.42 | -1.59 | -1.26 | -0.53 | -0.20 | -0.05 | 115. |
| 120. | -1.00 | -1.44 | -1.64 | -1.00 | -0.54 | -0.20 | -0.05 | 120. |
| 125. | -1.00 | -1.47 | -1.72 | -0.77 | -0.61 | -0.20 | -0.05 | 125. |
| 130. | -0.96 | -1.47 | -1.59 | -0.72 | -0.61 | -0.19 | -0.05 | 130. |
| 135. | -0.84 | -1.41 | -1.41 | -0.72 | -0.58 | -0.19 | -0.05 | 135. |
| 140. | -0.67 | -1.30 | -1.22 | -0.69 | -0.52 | -0.15 | -0.04 | 140. |
| 145. | -0.54 | -1.16 | -1.04 | -0.59 | -0.44 | -0.12 | -0.04 | 145. |
| 150. | -0.42 | -0.98 | -0.87 | -0.49 | -0.36 | -0.08 | -0.04 | 150. |
| 155. | -0.30 | -0.78 | -0.65 | -0.39 | -0.27 | -0.04 | -0.03 | 155. |
| 160. | -0.19 | -0.55 | -0.46 | -0.27 | -0.18 | -0.00 | -0.02 | 160. |
| 165. | -0.08 | -0.34 | -0.27 | -0.22 | -0.10 | 0.03 | -0.01 | 165. |
| 170. | 0.03 | -0.16 | -0.11 | -0.14 | -0.03 | 0.05 | -0.01 | 170. |
| 175. | 0.12 | -0.04 | 0.02 | -0.07 | 0.03 | 0.08 | -0.00 | 175. |
| 180. | 0.21 | 0.13 | 0.12 | -0.01 | 0.07 | 0.09 | -0.01 | 180. |
| 185. | 0.28 | 0.22 | 0.20 | 0.04 | 0.11 | 0.09 | 0.01 | 185. |
| 190. | 0.34 | 0.27 | 0.25 | 0.08 | 0.13 | 0.09 | 0.01 | 190. |
| 195. | 0.31 | 0.30 | 0.29 | 0.08 | 0.14 | 0.08 | 0.01 | 195. |
| 200. | 0.29 | 0.30 | 0.31 | 0.08 | 0.14 | 0.07 | 0.00 | 200. |
| 205. | 0.26 | 0.28 | 0.31 | 0.08 | 0.13 | 0.06 | -0.00 | 205. |
| 210. | 0.22 | 0.25 | 0.31 | 0.08 | 0.12 | 0.05 | -0.00 | 210. |
| 215. | 0.18 | 0.21 | 0.32 | 0.08 | 0.12 | 0.04 | -0.00 | 215. |
| 220. | 0.17 | 0.17 | 0.32 | 0.08 | 0.11 | 0.04 | -0.00 | 220. |
| 225. | 0.17 | 0.13 | 0.32 | 0.09 | 0.11 | 0.03 | -0.01 | 225. |
| 230. | 0.17 | 0.11 | 0.33 | 0.09 | 0.11 | 0.03 | -0.01 | 230. |
| 235. | 0.18 | 0.08 | 0.33 | 0.10 | 0.11 | 0.03 | -0.01 | 235. |
| 240. | 0.20 | 0.06 | 0.34 | 0.11 | 0.11 | 0.03 | -0.01 | 240. |
| 245. | 0.23 | 0.05 | 0.35 | 0.11 | 0.12 | 0.04 | -0.01 | 245. |
| 250. | 0.25 | 0.03 | 0.39 | 0.12 | 0.12 | 0.04 | -0.00 | 250. |
| 255. | 0.26 | 0.03 | 0.42 | 0.13 | 0.12 | 0.04 | 0.00 | 255. |
| 260. | 0.26 | 0.04 | 0.44 | 0.14 | 0.12 | 0.04 | 0.00 | 260. |
| 265. | 0.26 | 0.07 | 0.45 | 0.15 | 0.13 | 0.04 | 0.01 | 265. |
| 270. | 0.27 | 0.11 | 0.46 | 0.15 | 0.14 | 0.04 | 0.01 | 270. |
| 275. | 0.27 | 0.16 | 0.47 | 0.16 | 0.15 | 0.04 | 0.01 | 275. |
| 280. | 0.28 | 0.23 | 0.47 | 0.17 | 0.17 | 0.04 | 0.00 | 280. |
| 285. | 0.30 | 0.31 | 0.48 | 0.19 | 0.18 | 0.05 | 0.00 | 285. |
| 290. | 0.32 | 0.39 | 0.51 | 0.20 | 0.19 | 0.06 | 0.00 | 290. |
| 295. | 0.35 | 0.44 | 0.54 | 0.22 | 0.21 | 0.08 | 0.01 | 295. |
| 300. | 0.36 | 0.47 | 0.57 | 0.24 | 0.23 | 0.09 | 0.02 | 300. |
| 305. | 0.36 | 0.49 | 0.59 | 0.24 | 0.24 | 0.09 | 0.02 | 305. |
| 310. | 0.37 | 0.51 | 0.61 | 0.28 | 0.25 | 0.09 | 0.01 | 310. |
| 315. | 0.36 | 0.52 | 0.61 | 0.29 | 0.25 | 0.10 | 0.02 | 315. |
| 320. | 0.35 | 0.52 | 0.60 | 0.29 | 0.24 | 0.09 | 0.02 | 320. |
| 325. | 0.35 | 0.49 | 0.55 | 0.27 | 0.22 | 0.09 | 0.03 | 325. |
| 330. | 0.37 | 0.46 | 0.50 | 0.24 | 0.19 | 0.07 | 0.02 | 330. |
| 335. | 0.37 | 0.39 | 0.48 | 0.22 | 0.17 | 0.06 | 0.02 | 335. |
| 340. | 0.32 | 0.36 | 0.44 | 0.19 | 0.17 | 0.05 | 0.02 | 340. |
| 345. | 0.28 | 0.31 | 0.34 | 0.21 | 0.21 | 0.06 | 0.03 | 345. |
| 350. | 0.28 | 0.23 | 0.22 | 0.19 | 0.18 | 0.05 | 0.02 | 350. |
| 355. | -0.06 | 0.19 | 0.26 | 0.15 | 0.32 | 0.01 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 250 TCN= 33. C.R.= 32.7

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 3.495 | 1.340 | 1.959 | 2.992 | 4.550 | 7.151 | 10.400 | DEG. |
| 0. | 0.41 | 0.35 | 0.48 | 0.27 | 0.18 | 0.32 | 0.22 | 0. |
| 5. | 0.15 | 0.21 | -0.07 | 0.21 | 0.12 | -0.35 | 0.22 | 5. |
| 10. | -0.01 | 0.03 | -0.09 | 0.12 | 0.10 | -0.42 | 0.11 | 10. |
| 15. | 0.28 | 0.22 | 0.14 | 0.22 | 0.12 | 0.07 | 0.01 | 15. |
| 20. | 0.56 | 0.41 | 0.15 | 0.23 | 0.18 | 0.31 | 0.11 | 20. |
| 25. | 0.68 | 0.48 | 0.23 | 0.22 | 0.26 | -0.02 | 0.01 | 25. |
| 30. | 0.76 | 0.52 | 0.31 | 0.27 | 0.35 | -0.03 | 0.01 | 30. |
| 35. | 0.86 | 0.59 | 0.41 | 0.38 | 0.44 | -0.01 | 0.02 | 35. |
| 40. | 0.94 | 0.64 | 0.53 | 0.44 | 0.53 | 0.01 | 0.02 | 40. |
| 45. | 0.95 | 0.62 | 0.63 | 0.42 | 0.56 | 0.03 | 0.02 | 45. |
| 50. | 0.91 | 0.56 | 0.66 | 0.47 | 0.59 | 0.04 | 0.01 | 50. |
| 55. | 0.82 | 0.49 | 0.70 | 0.63 | 0.59 | 0.03 | -0.00 | 55. |
| 60. | 0.66 | 0.39 | 0.74 | 0.86 | 0.63 | -0.02 | -0.02 | 60. |
| 65. | 0.46 | 0.25 | 0.14 | 0.78 | 0.62 | -0.06 | -0.03 | 65. |
| 70. | 0.21 | 0.03 | 0.95 | 0.62 | 0.52 | -0.12 | -0.05 | 70. |
| 75. | -0.04 | -0.18 | 0.78 | -0.03 | 0.43 | -0.20 | -0.07 | 75. |
| 80. | -0.31 | -0.37 | 0.65 | -0.30 | 0.32 | -0.29 | -0.10 | 80. |
| 85. | -0.59 | -0.70 | 0.61 | -0.67 | 0.30 | -0.35 | -0.10 | 85. |
| 90. | -1.00 | -1.09 | -0.07 | -0.89 | 0.21 | -0.34 | -0.08 | 90. |
| 95. | -1.58 | -1.46 | -0.71 | -0.92 | -1.60 | -0.26 | -0.05 | 95. |
| 100. | -1.80 | -1.72 | -1.16 | -1.17 | -2.24 | -0.15 | -0.03 | 100. |
| 105. | -2.01 | -1.96 | -1.27 | -1.45 | -2.31 | -0.11 | -0.03 | 105. |
| 110. | -2.11 | -1.92 | -1.28 | -1.76 | -2.32 | -0.11 | -0.03 | 110. |
| 115. | -2.20 | -1.98 | -1.36 | -2.09 | -1.39 | -0.15 | -0.04 | 115. |
| 120. | -2.27 | -2.02 | -1.51 | -2.39 | -0.22 | -0.22 | -0.04 | 120. |
| 125. | -2.31 | -2.08 | -1.66 | -2.38 | -0.36 | -0.26 | -0.05 | 125. |
| 130. | -2.32 | -2.13 | -1.79 | -1.92 | -0.24 | -0.29 | -0.06 | 130. |
| 135. | -2.27 | -2.01 | -1.78 | -1.04 | -0.32 | -0.28 | -0.06 | 135. |
| 140. | -2.11 | -1.74 | -1.56 | -0.87 | -0.32 | -0.24 | -0.05 | 140. |
| 145. | -1.99 | -1.48 | -1.27 | -0.79 | -0.28 | -0.22 | -0.05 | 145. |
| 150. | -1.62 | -1.21 | -0.99 | -0.67 | -0.22 | -0.18 | -0.04 | 150. |
| 155. | -1.30 | -0.93 | -0.79 | -0.51 | -0.16 | -0.13 | -0.03 | 155. |
| 160. | -0.97 | -0.64 | -0.62 | -0.34 | -0.09 | -0.09 | -0.03 | 160. |
| 165. | -0.65 | -0.39 | -0.46 | -0.19 | -0.02 | -0.05 | -0.02 | 165. |
| 170. | -0.36 | -0.17 | -0.36 | -0.06 | 0.04 | -0.02 | -0.01 | 170. |
| 175. | -0.11 | 0.02 | -0.16 | 0.04 | 0.08 | 0.02 | -0.00 | 175. |
| 180. | 0.09 | 0.18 | -0.04 | 0.12 | 0.09 | 0.05 | 0.00 | 180. |
| 185. | 0.24 | 0.31 | 0.05 | 0.18 | 0.08 | 0.07 | 0.00 | 185. |
| 190. | 0.34 | 0.38 | 0.11 | 0.22 | 0.07 | 0.09 | 0.00 | 190. |
| 195. | 0.39 | 0.43 | 0.14 | 0.24 | 0.05 | 0.08 | 0.00 | 195. |
| 200. | 0.40 | 0.44 | 0.16 | 0.28 | 0.02 | 0.08 | 0.00 | 200. |
| 205. | 0.39 | 0.44 | 0.17 | 0.29 | 0.01 | 0.08 | 0.00 | 205. |
| 210. | 0.35 | 0.43 | 0.17 | 0.27 | 0.00 | 0.08 | 0.00 | 210. |
| 215. | 0.32 | 0.41 | 0.17 | 0.29 | -0.02 | 0.08 | 0.00 | 215. |
| 220. | 0.29 | 0.39 | 0.15 | 0.28 | -0.03 | 0.08 | 0.00 | 220. |
| 225. | 0.26 | 0.37 | 0.14 | 0.27 | -0.01 | 0.09 | 0.01 | 225. |
| 230. | 0.24 | 0.37 | 0.13 | 0.27 | -0.02 | 0.08 | 0.01 | 230. |
| 235. | 0.25 | 0.38 | 0.13 | 0.28 | -0.03 | 0.08 | 0.01 | 235. |
| 240. | 0.27 | 0.40 | 0.14 | 0.29 | -0.03 | 0.09 | 0.01 | 240. |
| 245. | 0.30 | 0.42 | 0.15 | 0.30 | -0.03 | 0.09 | 0.01 | 245. |
| 250. | 0.33 | 0.43 | 0.16 | 0.31 | -0.03 | 0.09 | 0.02 | 250. |
| 255. | 0.36 | 0.44 | 0.18 | 0.33 | -0.02 | 0.10 | 0.02 | 255. |
| 260. | 0.39 | 0.46 | 0.19 | 0.35 | -0.01 | 0.10 | 0.02 | 260. |
| 265. | 0.43 | 0.49 | 0.21 | 0.37 | -0.00 | 0.10 | 0.02 | 265. |
| 270. | 0.48 | 0.53 | 0.21 | 0.40 | 0.01 | 0.10 | 0.02 | 270. |
| 275. | 0.55 | 0.58 | 0.22 | 0.42 | 0.02 | 0.11 | 0.02 | 275. |
| 280. | 0.62 | 0.65 | 0.24 | 0.44 | 0.03 | 0.11 | 0.01 | 280. |
| 285. | 0.69 | 0.63 | 0.28 | 0.47 | 0.04 | 0.12 | 0.02 | 285. |
| 290 | 0.76 | 0.68 | 0.33 | 0.50 | 0.06 | 0.14 | 0.02 | 290. |
| 295. | 0.85 | 0.76 | 0.43 | 0.53 | 0.09 | 0.15 | 0.03 | 295. |
| 300. | 1.04 | 0.82 | 0.46 | 0.56 | 0.11 | 0.15 | 0.04 | 300. |
| 305. | 1.01 | 0.85 | 0.48 | 0.57 | 0.13 | 0.16 | 0.04 | 305. |
| 310. | 1.04 | 0.85 | 0.47 | 0.58 | 0.15 | 0.17 | 0.05 | 310. |
| 315. | 1.05 | 0.86 | 0.47 | 0.59 | 0.17 | 0.18 | 0.05 | 315. |
| 320. | 1.04 | 0.85 | 0.46 | 0.58 | 0.18 | 0.19 | 0.06 | 320. |
| 325. | 1.01 | 0.82 | 0.44 | 0.56 | 0.19 | 0.17 | 0.05 | 325. |
| 330. | 0.93 | 0.76 | 0.37 | 0.51 | 0.14 | 0.15 | 0.05 | 330. |
| 335. | 0.84 | 0.65 | 0.30 | 0.46 | 0.12 | 0.14 | 0.05 | 335. |
| 340. | 0.76 | 0.54 | 0.30 | 0.44 | 0.12 | 0.13 | 0.05 | 340. |
| 345. | 0.93 | 0.65 | 0.33 | 0.46 | 0.13 | 0.13 | 0.05 | 345. |
| 350. | 1.14 | 0.89 | 0.45 | 0.55 | 0.25 | 0.16 | 0.07 | 350. |
| 355. | 1.12 | 0.78 | 0.45 | 0.55 | 0.27 | 0.12 | 0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=498 CNTR NO. 251 TEN= 33. C.R.= 32.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.555 | 1.040 | 1.953 | 2.993 | 4.553 | 7.150 | 10.400 | DEG. |
| 0. | 0.67 | 0.49 | 0.47 | 0.13 | 0.13 | 0.02 | -0.02 | 0. |
| 5. | 0.42 | 0.40 | -0.01 | 0.08 | 0.12 | 0.01 | -0.02 | 5. |
| 10. | 0.14 | 0.22 | -0.11 | 0.06 | 0.08 | -0.01 | -0.03 | 10. |
| 15. | 0.44 | 0.39 | 0.12 | 0.17 | 0.14 | 0.01 | -0.01 | 15. |
| 20. | 0.77 | 0.56 | 0.28 | 0.15 | 0.14 | -0.04 | -0.04 | 20. |
| 25. | 0.84 | 0.61 | 0.29 | 0.14 | 0.14 | -0.07 | -0.05 | 25. |
| 30. | 0.84 | 0.65 | 0.29 | 0.20 | 0.19 | -0.06 | -0.04 | 30. |
| 35. | 0.86 | 0.72 | 0.26 | 0.20 | 0.27 | -0.04 | -0.03 | 35. |
| 40. | 0.93 | 0.77 | 0.74 | 0.32 | 0.32 | -0.04 | -0.03 | 40. |
| 45. | 0.92 | 0.77 | 1.28 | 0.41 | 0.35 | -0.06 | -0.03 | 45. |
| 50. | 0.84 | 0.76 | 1.47 | 0.41 | 0.35 | -0.11 | -0.04 | 50. |
| 55. | 0.72 | 0.69 | 1.33 | 0.05 | 0.19 | -0.15 | -0.07 | 55. |
| 60. | 0.53 | 0.62 | 1.14 | 1.00 | 0.32 | -0.21 | -0.08 | 60. |
| 65. | 0.30 | 0.49 | 1.01 | 1.02 | 1.07 | -0.28 | -0.09 | 65. |
| 70. | 0.06 | 0.24 | 0.87 | 0.55 | 1.28 | -0.36 | -0.10 | 70. |
| 75. | -0.24 | -0.04 | 0.69 | 0.04 | 0.99 | -0.42 | -0.12 | 75. |
| 80. | -0.46 | -0.42 | 0.44 | -0.32 | 0.37 | -0.42 | -0.12 | 80. |
| 85. | -1.15 | -0.91 | 0.17 | -0.73 | -0.12 | -0.34 | -0.09 | 85. |
| 90. | -1.61 | -1.38 | -0.12 | -1.26 | -0.43 | -0.17 | -0.03 | 90. |
| 95. | -1.92 | -1.67 | -0.43 | -1.15 | -0.60 | -0.01 | 0.00 | 95. |
| 100. | -2.14 | -1.84 | -0.64 | -1.20 | -1.03 | 0.09 | 0.03 | 100. |
| 105. | -2.29 | -1.94 | -0.69 | -1.27 | -1.07 | 0.14 | 0.04 | 105. |
| 110. | -2.39 | -2.01 | -0.73 | -1.36 | -2.35 | 0.13 | 0.02 | 110. |
| 115. | -2.44 | -2.07 | -0.85 | -1.56 | -2.49 | -0.01 | 0.02 | 115. |
| 120. | -2.49 | -2.10 | -1.23 | -1.85 | -1.53 | -0.16 | -0.00 | 120. |
| 125. | -2.53 | -2.12 | -1.61 | -2.12 | -0.35 | -0.26 | -0.03 | 125. |
| 130. | -2.57 | -2.10 | -1.78 | -2.13 | -0.03 | -0.31 | -0.03 | 130. |
| 135. | -2.53 | -2.02 | -1.79 | -1.63 | -0.17 | -0.32 | -0.05 | 135. |
| 140. | -2.39 | -1.86 | -1.73 | -0.75 | -0.28 | -0.33 | -0.05 | 140. |
| 145. | -2.17 | -1.64 | -1.53 | -0.59 | -0.28 | -0.27 | -0.04 | 145. |
| 150. | -1.90 | -1.38 | -1.26 | -0.62 | -0.22 | -0.22 | -0.03 | 150. |
| 155. | -1.59 | -1.10 | -1.02 | -0.53 | -0.17 | -0.16 | -0.01 | 155. |
| 160. | -1.26 | -0.85 | -0.83 | -0.46 | -0.12 | -0.11 | -0.00 | 160. |
| 165. | -0.88 | -0.61 | -0.63 | -0.26 | -0.06 | -0.09 | 0.01 | 165. |
| 170. | -0.52 | -0.37 | -0.44 | -0.12 | -0.01 | -0.05 | 0.02 | 170. |
| 175. | -0.27 | -0.16 | -0.29 | -0.01 | 0.04 | 0.03 | -0.02 | 175. |
| 180. | -0.05 | -0.01 | -0.17 | 0.08 | 0.07 | 0.04 | 0.02 | 180. |
| 185. | 0.16 | 0.11 | -0.08 | 0.19 | 0.09 | 0.05 | 0.02 | 185. |
| 190. | 0.31 | 0.21 | -0.07 | 0.16 | 0.10 | 0.05 | 0.03 | 190. |
| 195. | 0.37 | 0.27 | 0.00 | 0.19 | 0.11 | 0.05 | 0.03 | 195. |
| 200. | 0.37 | 0.29 | 0.02 | 0.21 | 0.11 | 0.06 | 0.02 | 200. |
| 205. | 0.37 | 0.30 | 0.04 | 0.22 | 0.12 | 0.06 | 0.02 | 205. |
| 210. | 0.36 | 0.32 | 0.05 | 0.23 | 0.12 | 0.06 | 0.02 | 210. |
| 215. | 0.35 | 0.32 | 0.07 | 0.24 | 0.12 | 0.06 | 0.02 | 215. |
| 220. | 0.35 | 0.32 | 0.08 | 0.24 | 0.11 | 0.06 | 0.03 | 220. |
| 225. | 0.35 | 0.32 | 0.09 | 0.25 | 0.11 | 0.10 | 0.03 | 225. |
| 230. | 0.34 | 0.32 | 0.09 | 0.25 | 0.10 | 0.12 | 0.03 | 230. |
| 235. | 0.34 | 0.33 | 0.09 | 0.28 | 0.10 | 0.13 | 0.03 | 235. |
| 240. | 0.35 | 0.34 | 0.09 | 0.30 | 0.10 | 0.13 | 0.04 | 240. |
| 245. | 0.39 | 0.36 | 0.11 | 0.33 | 0.11 | 0.14 | 0.04 | 245. |
| 250. | 0.44 | 0.38 | 0.14 | 0.35 | 0.11 | 0.14 | 0.04 | 250. |
| 255. | 0.50 | 0.42 | 0.16 | 0.36 | 0.11 | 0.15 | 0.04 | 255. |
| 260. | 0.54 | 0.47 | 0.17 | 0.36 | 0.11 | 0.15 | 0.04 | 260. |
| 265. | 0.58 | 0.51 | 0.19 | 0.37 | 0.12 | 0.16 | 0.04 | 265. |
| 270. | 0.62 | 0.56 | 0.21 | 0.38 | 0.13 | 0.17 | 0.04 | 270. |
| 275. | 0.67 | 0.61 | 0.22 | 0.39 | 0.14 | 0.17 | 0.04 | 275. |
| 280. | 0.74 | 0.65 | 0.25 | 0.42 | 0.15 | 0.17 | 0.04 | 280. |
| 285. | 0.83 | 0.69 | 0.29 | 0.45 | 0.16 | 0.18 | 0.03 | 285. |
| 290. | 0.95 | 0.75 | 0.36 | 0.55 | 0.18 | 0.18 | 0.03 | 290. |
| 295. | 1.08 | 0.87 | 0.42 | 0.54 | 0.19 | 0.19 | 0.04 | 295. |
| 300. | 1.20 | 0.94 | 0.47 | 0.55 | 0.20 | 0.19 | 0.04 | 300. |
| 305. | 1.30 | 0.93 | 0.48 | 0.56 | 0.22 | 0.19 | 0.04 | 305. |
| 310. | 1.36 | 0.93 | 0.48 | 0.56 | 0.23 | 0.19 | 0.04 | 310. |
| 315. | 1.38 | 0.94 | 0.46 | 0.56 | 0.25 | 0.18 | 0.04 | 315. |
| 320. | 1.39 | 0.93 | 0.44 | 0.57 | 0.26 | 0.17 | 0.05 | 320. |
| 325. | 1.35 | 0.87 | 0.44 | 0.50 | 0.27 | 0.17 | 0.04 | 325. |
| 330. | 1.24 | 0.80 | 0.49 | 0.45 | 0.24 | 0.16 | 0.02 | 330. |
| 335. | 1.09 | 0.72 | 0.31 | 0.39 | 0.20 | 0.15 | 0.02 | 335. |
| 340. | 0.94 | 0.65 | 0.25 | 0.34 | 0.18 | 0.12 | 0.02 | 340. |
| 345. | 1.30 | 0.72 | 0.31 | 0.36 | 0.21 | 0.13 | 0.02 | 345. |
| 350. | 1.48 | 0.98 | 0.48 | 0.5. | 0.26 | 0.14 | 0.03 | 350. |
| 355. | 1.62 | 1.10 | 0.53 | 0.43 | 0.24 | 0.11 | 0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=552 CNTR NO. 175 TCN= 36. C.R.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 92.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.550 | 13.650 | DEG. |
| 0. | -0.87 | -0.40 | -0.23 | -0.02 | 0. |
| 5. | -0.88 | -0.39 | -0.22 | -0.01 | 5. |
| 10. | -0.86 | -0.39 | -0.13 | 0.01 | 10. |
| 15. | -0.86 | -0.16 | -0.06 | 0.02 | 15. |
| 20. | -0.16 | -0.04 | -0.01 | -0.01 | 20. |
| 25. | 0.01 | -0.08 | -0.02 | -0.04 | 25. |
| 30. | -0.24 | -0.15 | -0.08 | -0.04 | 30. |
| 35. | -0.32 | -0.16 | -0.09 | -0.04 | 35. |
| 40. | -0.18 | -0.11 | -0.06 | -0.03 | 40. |
| 45. | -0.17 | -0.11 | -0.04 | -0.04 | 45. |
| 50. | -0.03 | -0.09 | -0.02 | -0.05 | 50. |
| 55. | 0.06 | -0.06 | 0.00 | -0.05 | 55. |
| 60. | 0.12 | -0.03 | 0.01 | -0.05 | 60. |
| 65. | 0.16 | -0.00 | 0.02 | -0.05 | 65. |
| 70. | 0.18 | 0.02 | 0.03 | -0.06 | 70. |
| 75. | 0.21 | 0.05 | 0.03 | -0.06 | 75. |
| 80. | 0.24 | 0.08 | 0.03 | -0.05 | 80. |
| 85. | 0.28 | 0.11 | 0.05 | -0.04 | 85. |
| 90. | 0.35 | 0.11 | 0.07 | -0.02 | 90. |
| 95. | 0.44 | 0.15 | 0.10 | -0.00 | 95. |
| 100. | 0.55 | 0.21 | 0.14 | 0.00 | 100. |
| 105. | 0.66 | 0.27 | 0.18 | 0.01 | 105. |
| 110. | 0.76 | 0.32 | 0.21 | 0.01 | 110. |
| 115. | 0.85 | 0.38 | 0.24 | 0.02 | 115. |
| 120. | 0.92 | 0.42 | 0.27 | 0.04 | 120. |
| 125. | 0.99 | 0.46 | 0.29 | 0.04 | 125. |
| 130. | 1.03 | 0.49 | 0.30 | 0.03 | 130. |
| 135. | 1.06 | 0.52 | 0.31 | 0.03 | 135. |
| 140. | 1.07 | 0.53 | 0.32 | 0.04 | 140. |
| 145. | 1.09 | 0.54 | 0.32 | 0.04 | 145. |
| 150. | 1.09 | 0.54 | 0.32 | 0.04 | 150. |
| 155. | 1.08 | 0.53 | 0.30 | 0.04 | 155. |
| 160. | 1.05 | 0.50 | 0.29 | 0.03 | 160. |
| 165. | 0.99 | 0.47 | 0.26 | 0.03 | 165. |
| 170. | 0.90 | 0.43 | 0.22 | 0.03 | 170. |
| 175. | 0.81 | 0.37 | 0.18 | 0.03 | 175. |
| 180. | 0.67 | 0.30 | 0.16 | 0.03 | 180. |
| 185. | 0.51 | 0.23 | 0.13 | 0.02 | 185. |
| 190. | 0.32 | 0.15 | 0.08 | 0.02 | 190. |
| 195. | 0.12 | 0.07 | 0.03 | 0.03 | 195. |
| 200. | -0.09 | -0.01 | -0.01 | 0.03 | 200. |
| 205. | -0.22 | -0.08 | -0.05 | 0.03 | 205. |
| 210. | -0.24 | -0.10 | -0.09 | 0.03 | 210. |
| 215. | -0.33 | -0.11 | -0.12 | 0.02 | 215. |
| 220. | -0.43 | -0.13 | -0.14 | 0.03 | 220. |
| 225. | -0.50 | -0.12 | -0.15 | 0.04 | 225. |
| 230. | -0.54 | -0.10 | -0.15 | 0.02 | 230. |
| 235. | -0.55 | -0.21 | -0.16 | 0.01 | 235. |
| 240. | -0.55 | -0.22 | -0.16 | -0.00 | 240. |
| 245. | -0.54 | -0.23 | -0.16 | 0.00 | 245. |
| 250. | -0.52 | -0.23 | -0.17 | 0.00 | 250. |
| 255 | -0.51 | -0.23 | -0.18 | -0.00 | 255. |
| 260. | -0.51 | -0.24 | -0.18 | -0.02 | 260. |
| 265. | -0.51 | -0.24 | -0.18 | -0.01 | 265. |
| 270. | -0.52 | -0.24 | -0.17 | -0.01 | 270. |
| 275. | -0.52 | -0.24 | -0.16 | -0.01 | 275. |
| 280. | -0.53 | -0.24 | -0.15 | -0.01 | 280. |
| 285. | -0.53 | -0.24 | -0.14 | -0.01 | 285. |
| 290. | -0.53 | -0.24 | -0.13 | -0.01 | 290. |
| 295. | -0.53 | -0.23 | -0.12 | -0.00 | 295. |
| 300. | -0.53 | -0.23 | -0.12 | -0.00 | 300. |
| 305. | -0.54 | -0.22 | -0.12 | -0.01 | 305. |
| 310. | -0.54 | -0.22 | -0.12 | -0.01 | 310. |
| 315. | -0.54 | -0.21 | -0.12 | -0.01 | 315. |
| 320. | -0.54 | -0.22 | -0.12 | -0.01 | 320. |
| 325. | -0.54 | -0.24 | -0.13 | -0.01 | 325. |
| 330. | -0.57 | -0.25 | -0.12 | -0.00 | 330. |
| 335. | -0.54 | -0.23 | -0.11 | -0.01 | 335. |
| 340. | -0.38 | -0.17 | -0.07 | -0.01 | 340. |
| 345. | -0.15 | -0.11 | -0.02 | -0.01 | 345. |
| 350. | -0.10 | -0.10 | -0.05 | -0.01 | 350. |
| 355. | -0.56 | -0.29 | -0.13 | -0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 175 TCN= 30. C.R.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.367 | 2.953 | 2.992 | 4.959 | 7.159 | 19.400 | DEG. |
| 0. | -1.34 | -0.98 | -0.71 | -0.65 | -0.32 | -0.16 | -0.05 | 0. |
| 5. | -1.14 | -0.82 | -0.63 | -0.56 | -0.25 | -0.13 | -0.04 | 5. |
| 10. | -0.89 | -0.67 | -0.62 | -0.57 | -0.17 | -0.11 | -0.01 | 10. |
| 15. | -0.25 | -0.13 | -0.20 | -0.14 | -0.11 | -0.08 | -0.01 | 15. |
| 20. | -0.15 | -0.26 | -0.22 | -0.14 | -0.10 | -0.11 | -0.05 | 20. |
| 25. | -0.50 | -0.38 | -0.30 | -0.23 | -0.13 | -0.10 | -0.04 | 25. |
| 30. | -0.51 | -0.35 | -0.27 | -0.21 | -0.13 | -0.09 | -0.02 | 30. |
| 35. | -0.27 | -0.21 | -0.23 | -0.19 | -0.08 | -0.08 | -0.01 | 35. |
| 40. | -0.11 | -0.09 | -0.18 | -0.13 | -0.05 | -0.06 | -0.02 | 40. |
| 45. | -0.01 | -0.05 | -0.15 | -0.10 | -0.01 | -0.06 | -0.03 | 45. |
| 50. | 0.04 | -0.03 | -0.12 | -0.07 | 0.01 | -0.04 | -0.03 | 50. |
| 55. | 0.07 | -0.01 | -0.11 | -0.06 | 0.05 | -0.08 | -0.02 | 55. |
| 60. | 0.08 | 0.02 | -0.09 | -0.04 | 0.09 | -0.08 | -0.02 | 60. |
| 65. | 0.11 | 0.05 | -0.08 | -0.01 | 0.10 | -0.07 | -0.02 | 65. |
| 70. | 0.19 | 0.12 | -0.05 | 0.02 | 0.13 | -0.06 | -0.01 | 70. |
| 75. | 0.00 | 0.20 | 0.03 | 0.06 | 0.17 | -0.04 | -0.01 | 75. |
| 80. | 0.42 | 0.28 | 0.07 | 0.10 | 0.22 | -0.03 | 0.00 | 80. |
| 85. | 0.54 | 0.35 | 0.14 | 0.15 | 0.26 | -0.01 | 0.01 | 85. |
| 90. | 0.64 | 0.42 | 0.19 | 0.19 | 0.29 | 0.03 | 0.01 | 90. |
| 95. | 0.73 | 0.48 | 0.25 | 0.23 | 0.32 | 0.02 | 0.02 | 95. |
| 100. | 0.81 | 0.54 | 0.31 | 0.26 | 0.34 | 0.05 | 0.02 | 100. |
| 105. | 0.90 | 0.60 | 0.35 | 0.29 | 0.37 | 0.07 | 0.02 | 105. |
| 110. | 1.00 | 0.66 | 0.42 | 0.31 | 0.38 | 0.08 | 0.03 | 110. |
| 115. | 1.09 | 0.72 | 0.46 | 0.33 | 0.40 | 0.10 | 0.04 | 115. |
| 120. | 1.16 | 0.77 | 0.48 | 0.34 | 0.41 | 0.11 | 0.04 | 120. |
| 125. | 1.22 | 0.83 | 0.52 | 0.41 | 0.42 | 0.12 | 0.05 | 125. |
| 130. | 1.27 | 0.89 | 0.57 | 0.43 | 0.42 | 0.15 | 0.05 | 130. |
| 135. | 1.33 | 0.94 | 0.62 | 0.46 | 0.43 | 0.18 | 0.06 | 135. |
| 140. | 1.42 | 0.99 | 0.67 | 0.48 | 0.43 | 0.19 | 0.07 | 140. |
| 145. | 1.41 | 1.04 | 0.72 | 0.51 | 0.43 | 0.23 | 0.07 | 145. |
| 150. | 1.49 | 1.09 | 0.76 | 0.52 | 0.42 | 0.20 | 0.07 | 150. |
| 155. | 1.56 | 1.13 | 0.80 | 0.54 | 0.42 | 0.21 | 0.07 | 155. |
| 160. | 1.74 | 1.17 | 0.82 | 0.54 | 0.41 | 0.22 | 0.07 | 160. |
| 165. | 1.79 | 1.19 | 0.84 | 0.54 | 0.39 | 0.23 | 0.08 | 165. |
| 170. | 1.79 | 1.18 | 0.84 | 0.53 | 0.37 | 0.23 | 0.08 | 170. |
| 175. | 1.70 | 1.12 | 0.82 | 0.51 | 0.33 | 0.23 | 0.07 | 175. |
| 180. | 1.59 | 1.03 | 0.72 | 0.48 | 0.28 | 0.22 | 0.07 | 180. |
| 185. | 1.35 | 0.89 | 0.62 | 0.45 | 0.23 | 0.19 | 0.06 | 185. |
| 190. | 1.10 | 0.73 | 0.51 | 0.40 | 0.18 | 0.16 | 0.05 | 190. |
| 195. | 0.84 | 0.55 | 0.43 | 0.33 | 0.12 | 0.12 | 0.02 | 195. |
| 200. | 0.56 | 0.37 | 0.30 | 0.24 | 0.06 | 0.09 | 0.01 | 200. |
| 205. | 0.32 | 0.19 | 0.19 | 0.19 | -0.01 | 0.05 | 0.00 | 205. |
| 210. | 0.11 | 0.03 | 0.10 | 0.14 | -0.06 | 0.02 | -0.03 | 210. |
| 215. | -0.08 | -0.09 | 0.01 | -0.02 | -0.10 | 0.00 | -0.03 | 215. |
| 220. | -0.27 | -0.18 | -0.05 | -0.06 | -0.13 | -0.01 | -0.01 | 220. |
| 225. | -0.45 | -0.26 | -0.12 | -0.10 | -0.16 | -0.02 | -0.02 | 225. |
| 230. | -0.59 | -0.26 | -0.14 | -0.13 | -0.21 | -0.03 | -0.03 | 230. |
| 235. | -0.66 | -0.25 | -0.13 | -0.16 | -0.25 | -0.04 | -0.04 | 235. |
| 240. | -0.71 | -0.29 | -0.12 | -0.19 | -0.28 | -0.06 | -0.03 | 240. |
| 245. | -0.78 | -0.37 | -0.11 | -0.20 | -0.30 | -0.07 | -0.03 | 245. |
| 250. | -0.80 | -0.45 | -0.15 | -0.21 | -0.31 | -0.08 | -0.03 | 250. |
| 255. | -0.93 | -0.53 | -0.11 | -0.23 | -0.32 | -0.09 | -0.03 | 255. |
| 260. | -2.93 | -0.60 | -0.17 | -0.18 | -0.31 | -0.09 | -0.02 | 260. |
| 265. | -0.94 | -0.64 | -0.26 | -0.18 | -0.28 | -0.09 | -0.02 | 265. |
| 270. | -0.97 | -0.66 | -0.38 | -0.21 | -0.26 | -0.08 | -0.02 | 270. |
| 275. | -0.98 | -0.67 | -0.44 | -0.24 | -0.25 | -0.07 | -0.02 | 275. |
| 280. | -0.98 | -0.68 | -0.47 | -0.27 | -0.25 | -0.06 | -0.03 | 280. |
| 285. | -0.97 | -0.67 | -0.47 | -0.28 | -0.25 | -0.05 | -0.03 | 285. |
| 290. | -0.96 | -0.67 | -0.45 | -0.29 | -0.26 | -0.05 | -0.03 | 290. |
| 295. | -0.94 | -0.66 | -0.42 | -0.31 | -0.26 | -0.05 | -0.03 | 295. |
| 300. | -0.94 | -0.65 | -0.43 | -0.31 | -0.26 | -0.05 | -0.03 | 300. |
| 305. | -0.94 | -0.65 | -0.43 | -0.31 | -0.26 | -0.07 | -0.03 | 305. |
| 310. | -0.94 | -0.65 | -0.43 | -0.31 | -0.26 | -0.07 | -0.03 | 310. |
| 315. | -0.95 | -0.65 | -0.43 | -0.31 | -0.25 | -0.07 | -0.03 | 315. |
| 320. | -0.95 | -0.66 | -0.43 | -0.32 | -0.25 | -0.07 | -0.02 | 320. |
| 325. | -0.97 | -0.67 | -0.43 | -0.31 | -0.25 | -0.07 | -0.02 | 325. |
| 330. | -0.92 | -0.66 | -0.42 | -0.31 | -0.25 | -0.07 | -0.02 | 330. |
| 335. | -0.95 | -0.65 | -0.42 | -0.32 | -0.24 | -0.08 | -0.02 | 335. |
| 340. | -1.01 | -0.69 | -0.45 | -0.33 | -0.24 | -0.08 | -0.03 | 340. |
| 345. | -1.13 | -0.80 | -0.54 | -0.37 | -0.27 | -0.09 | -0.03 | 345. |
| 350. | -1.30 | -0.98 | -0.68 | -0.47 | -0.34 | -0.11 | -0.04 | 350. |
| 355. | -1.79 | -1.24 | -0.85 | -0.59 | -0.43 | -0.17 | -0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 175 TCN= 36. C.R.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.153 | 10.493 | DEG. |
| 0. | -1.17 | -0.87 | -0.44 | -0.31 | -0.27 | -0.11 | -0.05 | 0. |
| 5. | -1.28 | -0.87 | -0.55 | -0.41 | -0.30 | -0.21 | -0.04 | 5. |
| 10. | -0.65 | -0.43 | -0.31 | -0.23 | -0.16 | -0.12 | -0.07 | 10. |
| 15. | -0.45 | -0.36 | -0.28 | -0.17 | -0.13 | -0.13 | -0.08 | 15. |
| 20. | -0.58 | -0.43 | -0.32 | -0.21 | -0.16 | -0.14 | -0.08 | 20. |
| 25. | -0.58 | -0.41 | -0.28 | -0.19 | -0.09 | -0.12 | -0.08 | 25. |
| 30. | -0.33 | -0.30 | -0.21 | -0.16 | -0.02 | -0.13 | -0.07 | 30. |
| 35. | -0.11 | -0.20 | -0.17 | -0.12 | 0.04 | -0.11 | -0.08 | 35. |
| 40. | 0.14 | -0.10 | -0.09 | -0.06 | 0.09 | -0.10 | -0.10 | 40. |
| 45. | 0.49 | 0.07 | 0.03 | 0.03 | 0.16 | -0.08 | -0.10 | 45. |
| 50. | 0.56 | 0.21 | 0.14 | 0.08 | 0.22 | -0.07 | -0.09 | 50. |
| 55. | 0.66 | 0.24 | 0.16 | 0.11 | 0.25 | -0.07 | -0.08 | 55. |
| 60. | 0.71 | 0.25 | 0.15 | 0.11 | 0.26 | -0.06 | -0.08 | 60. |
| 65. | 0.72 | 0.26 | 0.16 | 0.12 | 0.26 | -0.05 | -0.07 | 65. |
| 70. | 0.71 | 0.25 | 0.13 | 0.08 | 0.25 | -0.05 | -0.07 | 70. |
| 75. | 0.70 | 0.25 | 0.11 | 0.07 | 0.24 | -0.06 | -0.07 | 75. |
| 80. | 0.69 | 0.24 | 0.10 | 0.06 | 0.24 | -0.07 | -0.06 | 80. |
| 85. | 0.69 | 0.24 | 0.08 | 0.06 | 0.24 | -0.06 | -0.06 | 85. |
| 90. | 0.71 | 0.24 | 0.10 | 0.06 | 0.23 | -0.06 | -0.06 | 90. |
| 95. | 0.72 | 0.23 | 0.11 | 0.07 | 0.23 | -0.07 | -0.05 | 95. |
| 100. | 0.72 | 0.25 | 0.13 | 0.08 | 0.24 | -0.01 | -0.04 | 100. |
| 105. | 0.71 | 0.29 | 0.14 | 0.09 | 0.24 | 0.01 | -0.03 | 105. |
| 110. | 0.70 | 0.34 | 0.14 | 0.10 | 0.24 | 0.01 | -0.03 | 110. |
| 115. | 0.69 | 0.35 | 0.14 | 0.10 | 0.23 | 0.02 | -0.03 | 115. |
| 120. | 0.69 | 0.34 | 0.15 | 0.11 | 0.22 | 0.02 | -0.02 | 120. |
| 125. | 0.69 | 0.34 | 0.15 | 0.11 | 0.21 | 0.02 | 0.00 | 125. |
| 130. | 0.70 | 0.36 | 0.16 | 0.12 | 0.22 | 0.04 | 0.01 | 130. |
| 135. | 0.71 | 0.39 | 0.18 | 0.14 | 0.22 | 0.06 | 0.02 | 135. |
| 140. | 0.74 | 0.43 | 0.20 | 0.17 | 0.23 | 0.08 | 0.04 | 140. |
| 145. | 0.79 | 0.46 | 0.23 | 0.21 | 0.25 | 0.11 | 0.05 | 145. |
| 150. | 0.85 | 0.50 | 0.33 | 0.26 | 0.27 | 0.13 | 0.06 | 150. |
| 155. | 0.94 | 0.57 | 0.41 | 0.31 | 0.28 | 0.15 | 0.07 | 155. |
| 160. | 1.02 | 0.69 | 0.50 | 0.36 | 0.30 | 0.16 | 0.08 | 160. |
| 165. | 1.08 | 0.82 | 0.57 | 0.40 | 0.32 | 0.18 | 0.09 | 165. |
| 170. | 1.14 | 0.89 | 0.61 | 0.44 | 0.33 | 0.20 | 0.10 | 170. |
| 175. | 1.17 | 0.92 | 0.62 | 0.46 | 0.31 | 0.21 | 0.10 | 175. |
| 180. | 1.09 | 0.88 | 0.60 | 0.45 | 0.28 | 0.21 | 0.11 | 180. |
| 185. | 0.95 | 0.80 | 0.54 | 0.42 | 0.24 | 0.20 | 0.11 | 185. |
| 190. | 0.77 | 0.64 | 0.47 | 0.36 | 0.19 | 0.16 | 0.10 | 190. |
| 195. | 0.57 | 0.51 | 0.40 | 0.28 | 0.14 | 0.14 | 0.09 | 195. |
| 200. | 0.39 | 0.35 | 0.33 | 0.21 | 0.08 | 0.13 | 0.07 | 200. |
| 205. | 0.20 | 0.23 | 0.25 | 0.14 | 0.02 | 0.10 | 0.06 | 205. |
| 210. | 0.01 | 0.12 | 0.15 | 0.08 | -0.03 | 0.08 | 0.06 | 210. |
| 215. | -0.18 | 0.01 | 0.06 | 0.02 | -0.07 | 0.06 | 0.06 | 215. |
| 220. | -0.34 | -0.09 | -0.01 | -0.03 | -0.11 | 0.05 | 0.05 | 220. |
| 225. | -0.45 | -0.18 | -0.05 | -0.07 | -0.14 | 0.04 | 0.05 | 225. |
| 230. | -0.54 | -0.27 | -0.09 | -0.10 | -0.17 | 0.03 | 0.05 | 230. |
| 235. | -0.64 | -0.34 | -0.14 | -0.14 | -0.20 | 0.02 | 0.04 | 235. |
| 240. | -0.74 | -0.39 | -0.19 | -0.16 | -0.23 | 0.01 | 0.04 | 240. |
| 245. | -0.82 | -0.43 | -0.23 | -0.19 | -0.25 | -0.01 | 0.03 | 245. |
| 250. | -0.88 | -0.47 | -0.27 | -0.22 | -0.29 | -0.01 | 0.02 | 250. |
| 255. | -0.93 | -0.49 | -0.29 | -0.23 | -0.31 | -0.02 | 0.01 | 255. |
| 260. | -0.96 | -0.52 | -0.32 | -0.25 | -0.32 | -0.03 | 0.01 | 260. |
| 265. | -1.00 | -0.54 | -0.34 | -0.25 | -0.34 | -0.04 | 0.02 | 265. |
| 270. | -1.02 | -0.55 | -0.35 | -0.26 | -0.34 | -0.04 | 0.02 | 270. |
| 275. | -1.05 | -0.56 | -0.36 | -0.26 | -0.35 | -0.04 | 0.01 | 275. |
| 280. | -1.07 | -0.57 | -0.37 | -0.26 | -0.34 | -0.05 | 0.01 | 280. |
| 285. | -1.08 | -0.58 | -0.38 | -0.27 | -0.34 | -0.05 | 0.02 | 285. |
| 290. | -1.10 | -0.60 | -0.38 | -0.27 | -0.34 | -0.05 | 0.02 | 290. |
| 295. | -1.10 | -0.61 | -0.40 | -0.27 | -0.34 | -0.06 | 0.01 | 295. |
| 300. | -1.11 | -0.62 | -0.41 | -0.27 | -0.33 | -0.07 | -0.00 | 300. |
| 305. | -1.11 | -0.63 | -0.41 | -0.28 | -0.34 | -0.08 | -0.00 | 305. |
| 310. | -1.10 | -0.63 | -0.41 | -0.28 | -0.34 | -0.09 | -0.01 | 310. |
| 315. | -1.08 | -0.62 | -0.41 | -0.28 | -0.33 | -0.09 | -0.02 | 315. |
| 320. | -1.04 | -0.59 | -0.39 | -0.26 | -0.30 | -0.08 | -0.01 | 320. |
| 325. | -0.97 | -0.54 | -0.37 | -0.23 | -0.27 | -0.07 | -0.01 | 325. |
| 330. | -0.89 | -0.49 | -0.34 | -0.22 | -0.24 | -0.05 | -0.01 | 330. |
| 335. | -0.78 | -0.46 | -0.24 | -0.15 | -0.20 | -0.03 | -0.01 | 335. |
| 340. | -0.28 | -0.09 | -0.04 | 0.03 | -0.09 | 0.00 | 0.02 | 340. |
| 345. | 0.56 | 0.53 | 0.34 | 0.26 | 0.05 | 0.05 | 0.02 | 345. |
| 350. | 1.22 | 0.85 | 0.59 | 0.33 | 0.14 | 0.04 | -0.02 | 350. |
| 355. | 0.74 | 0.37 | 0.33 | 0.17 | 0.07 | -0.01 | -0.05 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=532 CNTR NO. 175 TCN= 36. C.R.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 15%.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.655 | 1.040 | 1.950 | 3.390 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.35 | -0.36 | -0.21 | -0.23 | -0.15 | -0.05 | -0.02 | 0. |
| 5. | -0.34 | -0.39 | -0.13 | -0.14 | -0.08 | -0.02 | -0.01 | 5. |
| 10. | -0.19 | -0.31 | -0.22 | -0.17 | -0.08 | -0.06 | -0.02 | 10. |
| 15. | -0.39 | -0.43 | -0.31 | -0.24 | -0.11 | -0.08 | -0.03 | 15. |
| 20. | -0.18 | -0.25 | -0.24 | -0.13 | -0.10 | -0.09 | -0.03 | 20. |
| 25. | 0.13 | -0.00 | -0.13 | -0.06 | -0.04 | -0.09 | -0.03 | 25. |
| 30. | 0.34 | 0.19 | -0.05 | 0.03 | 0.00 | -0.07 | -0.04 | 30. |
| 35. | 0.56 | 0.39 | 0.09 | 0.18 | 0.09 | -0.04 | -0.04 | 35. |
| 40. | 0.87 | 0.67 | 0.27 | 0.33 | 0.19 | -0.01 | -0.02 | 40. |
| 45. | 1.12 | 0.92 | 0.38 | 0.44 | 0.27 | 0.02 | -0.01 | 45. |
| 50. | 1.22 | 1.05 | 0.45 | 0.51 | 0.32 | 0.03 | -0.00 | 50. |
| 55. | 1.23 | 1.07 | 0.51 | 0.56 | 0.36 | 0.05 | 0.02 | 55. |
| 60. | 1.17 | 1.01 | 0.52 | 0.57 | 0.37 | 0.01 | 0.01 | 60. |
| 65. | 1.04 | 0.89 | 0.45 | 0.56 | 0.36 | -0.01 | -0.01 | 65. |
| 70. | 0.80 | 0.75 | 0.34 | 0.52 | 0.33 | -0.02 | -0.03 | 70. |
| 75. | 0.55 | 0.60 | 0.23 | 0.48 | 0.32 | -0.03 | -0.04 | 75. |
| 80. | 0.33 | 0.50 | 0.15 | 0.43 | 0.30 | -0.08 | -0.04 | 80. |
| 85. | 0.19 | 0.43 | 0.08 | 0.39 | 0.26 | -0.12 | -0.04 | 85. |
| 90. | 0.09 | 0.39 | 0.04 | 0.36 | 0.22 | -0.14 | -0.06 | 90. |
| 95. | 0.04 | 0.44 | 0.01 | 0.34 | 0.19 | -0.14 | -0.06 | 95. |
| 100. | -0.01 | 0.47 | 0.01 | 0.31 | 0.16 | -0.13 | -0.05 | 100. |
| 105. | -0.01 | 0.39 | -0.01 | 0.28 | 0.12 | -0.13 | -0.06 | 105. |
| 110. | -0.23 | 0.28 | -0.11 | 0.23 | 0.07 | -0.15 | -0.08 | 110. |
| 115. | -0.39 | 0.19 | -0.23 | 0.16 | 0.02 | -0.17 | -0.08 | 115. |
| 120. | -0.55 | 0.12 | -0.35 | 0.06 | -0.02 | -0.19 | -0.08 | 120. |
| 125. | -0.72 | -0.03 | -0.44 | -0.00 | -0.05 | -0.20 | -0.08 | 125. |
| 130. | -0.83 | -0.18 | -0.58 | -0.05 | -0.06 | -0.21 | -0.07 | 130. |
| 135. | -0.83 | -0.19 | -0.49 | -0.06 | -0.06 | -0.23 | -0.06 | 135. |
| 140. | -0.72 | -0.13 | -0.41 | -0.04 | -0.04 | -0.17 | -0.05 | 140. |
| 145. | -0.56 | -0.07 | -0.33 | -0.00 | -0.00 | -0.13 | -0.03 | 145. |
| 150. | -0.37 | 0.04 | -0.18 | 0.06 | 0.04 | -0.09 | -0.02 | 150. |
| 155. | -0.15 | 0.16 | -0.05 | 0.12 | 0.10 | -0.04 | -0.00 | 155. |
| 160. | 0.06 | 0.22 | 0.07 | 0.19 | 0.17 | -0.03 | 0.01 | 160. |
| 165. | 0.26 | 0.25 | 0.17 | 0.25 | 0.24 | 0.05 | 0.02 | 165. |
| 170. | 0.41 | 0.25 | 0.26 | 0.28 | 0.30 | 0.08 | 0.03 | 170. |
| 175. | 0.53 | 0.25 | 0.32 | 0.30 | 0.28 | 0.10 | 0.04 | 175. |
| 180. | 0.61 | 0.26 | 0.35 | 0.29 | 0.23 | 0.11 | 0.04 | 180. |
| 185. | 0.60 | 0.25 | 0.34 | 0.26 | 0.17 | 0.12 | 0.04 | 185. |
| 190. | 0.55 | 0.22 | 0.34 | 0.22 | 0.13 | 0.11 | 0.04 | 190. |
| 195. | 0.46 | 0.17 | 0.31 | 0.15 | 0.08 | 0.11 | 0.04 | 195. |
| 200. | 0.36 | 0.10 | 0.27 | 0.10 | 0.04 | 0.10 | 0.04 | 200. |
| 205. | 0.25 | 0.02 | 0.22 | 0.05 | 0.01 | 0.09 | 0.04 | 205. |
| 210. | 0.15 | -0.07 | 0.15 | -0.01 | -0.03 | 0.08 | 0.04 | 210. |
| 215. | 0.05 | -0.16 | 0.11 | -0.08 | -0.06 | 0.08 | 0.04 | 215. |
| 220. | -0.04 | -0.23 | 0.05 | -0.14 | -0.08 | 0.07 | 0.04 | 220. |
| 225. | -0.11 | -0.28 | 0.02 | -0.18 | -0.11 | 0.07 | 0.04 | 225. |
| 230. | -0.16 | -0.32 | -0.01 | -0.21 | -0.13 | 0.07 | 0.04 | 230. |
| 235. | -0.20 | -0.35 | -0.03 | -0.23 | -0.14 | 0.07 | 0.04 | 235. |
| 240. | -0.23 | -0.37 | -0.04 | -0.24 | -0.16 | 0.07 | 0.04 | 240. |
| 245. | -0.25 | -0.37 | -0.04 | -0.25 | -0.17 | 0.07 | 0.04 | 245. |
| 250. | -0.25 | -0.37 | -0.04 | -0.25 | -0.18 | 0.08 | 0.03 | 250. |
| 255. | -0.25 | -0.37 | -0.03 | -0.25 | -0.19 | 0.07 | 0.03 | 255. |
| 260. | -0.23 | -0.36 | -0.02 | -0.25 | -0.20 | 0.07 | 0.02 | 260. |
| 265. | -0.22 | -0.35 | -0.01 | -0.24 | -0.20 | 0.07 | 0.02 | 265. |
| 270. | -0.20 | -0.34 | -0.01 | -0.24 | -0.21 | 0.07 | 0.02 | 270. |
| 275. | -0.18 | -0.34 | -0.01 | -0.24 | -0.21 | 0.08 | 0.02 | 275. |
| 280. | -0.19 | -0.34 | -0.01 | -0.24 | -0.21 | 0.08 | 0.02 | 280. |
| 285. | -0.20 | -0.35 | -0.01 | -0.24 | -0.22 | 0.08 | 0.02 | 285. |
| 290. | -0.21 | -0.36 | -0.01 | -0.25 | -0.22 | 0.08 | 0.03 | 290. |
| 295. | -0.21 | -0.37 | -0.03 | -0.28 | -0.19 | 0.09 | 0.04 | 295. |
| 300. | -0.20 | -0.38 | -0.01 | -0.31 | -0.18 | 0.09 | 0.04 | 300. |
| 305. | -0.18 | -0.37 | -0.01 | -0.29 | -0.17 | 0.09 | 0.05 | 305. |
| 310. | -0.16 | -0.33 | -0.03 | -0.26 | -0.16 | 0.09 | 0.05 | 310. |
| 315. | -0.16 | -0.30 | -0.05 | -0.26 | -0.15 | 0.09 | 0.05 | 315. |
| 320. | -0.18 | -0.31 | -0.09 | -0.26 | -0.14 | 0.08 | 0.04 | 320. |
| 325. | -0.21 | -0.33 | -0.13 | -0.27 | -0.14 | 0.07 | 0.03 | 325. |
| 330. | -0.22 | -0.35 | -0.15 | -0.26 | -0.12 | 0.06 | 0.03 | 330. |
| 335. | -0.16 | -0.29 | -0.14 | -0.24 | -0.09 | 0.05 | 0.02 | 335. |
| 340. | -0.18 | -0.24 | -0.15 | -0.24 | -0.09 | 0.04 | 0.02 | 340. |
| 345. | -0.33 | -0.35 | -0.18 | -0.28 | -0.13 | 0.02 | -0.00 | 345. |
| 350. | -0.75 | -0.72 | -0.42 | -0.43 | -0.28 | -0.04 | -0.03 | 350. |
| 355. | -1.19 | -0.95 | -0.53 | -0.48 | -0.38 | -0.13 | -0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=522 CNTR NO. 175 TCM= 3c. C.R.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.450 | 1.040 | 1.950 | 2.990 | 4.950 | 7.150 | 10.430 | DEG. |
| 5. | 0.37 | 0.37 | 0.29 | 0.19 | 0.09 | 0.03 | 0.02 | 5. |
| 5. | -0.02 | 0.01 | -0.10 | 0.06 | -0.04 | -0.04 | 0.01 | 5. |
| 10. | -0.08 | -0.04 | -0.12 | 0.02 | -0.03 | -0.05 | 0.03 | 10. |
| 15. | 0.03 | 0.01 | -0.07 | 0.05 | -0.02 | -0.04 | 0.02 | 15. |
| 20. | 0.23 | 0.10 | 0.03 | 0.06 | -0.01 | -0.04 | 0.01 | 20. |
| 25. | 0.45 | 0.23 | 0.07 | 0.06 | -0.01 | -0.04 | 0.01 | 25. |
| 30. | 0.64 | 0.33 | 0.15 | 0.08 | 0.03 | -0.03 | 0.02 | 30. |
| 35. | 0.77 | 0.44 | 0.31 | 0.17 | 0.11 | 0.05 | 0.04 | 35. |
| 40. | 0.87 | 0.64 | 0.49 | 0.26 | 0.21 | 0.11 | 0.05 | 40. |
| 45. | 1.10 | 0.82 | 0.64 | 0.34 | 0.30 | 0.15 | 0.06 | 45. |
| 50. | 1.44 | 0.98 | 0.75 | 0.39 | 0.33 | 0.16 | 0.05 | 50. |
| 55. | 1.63 | 0.89 | 0.79 | 0.40 | 0.33 | 0.15 | 0.05 | 55. |
| 60. | 1.32 | 0.79 | 0.76 | 0.37 | 0.29 | 0.12 | 0.05 | 60. |
| 65. | 1.12 | 0.61 | 0.64 | 0.31 | 0.22 | 0.08 | 0.04 | 65. |
| 70. | 0.87 | 0.39 | 0.53 | 0.22 | 0.15 | 0.03 | 0.02 | 70. |
| 75. | 0.59 | 0.13 | 0.33 | 0.10 | 0.08 | -0.02 | -0.00 | 75. |
| 80. | 0.31 | -0.14 | -0.14 | -0.02 | -0.02 | -0.06 | -0.01 | 80. |
| 85. | 0.06 | -0.39 | -0.27 | -0.13 | -0.10 | -0.10 | -0.01 | 85. |
| 90. | -0.19 | -0.63 | -0.32 | -0.22 | -0.20 | -0.13 | -0.01 | 90. |
| 95. | -0.43 | -0.87 | -0.57 | -0.31 | -0.27 | -0.15 | -0.01 | 95. |
| 100. | -0.71 | -1.11 | -0.82 | -0.39 | -0.43 | -0.18 | -0.02 | 100. |
| 105. | -1.00 | -1.32 | -1.03 | -0.54 | -0.48 | -0.21 | -0.04 | 105. |
| 110. | -1.26 | -1.52 | -1.18 | -0.64 | -0.55 | -0.23 | -0.05 | 110. |
| 115. | -1.47 | -1.66 | -1.33 | -0.68 | -0.61 | -0.25 | -0.05 | 115. |
| 120. | -1.60 | -1.76 | -1.43 | -0.73 | -0.64 | -0.26 | -0.06 | 120. |
| 125. | -1.69 | -1.80 | -1.45 | -0.75 | -0.69 | -0.26 | -0.06 | 125. |
| 130. | -1.71 | -1.79 | -1.42 | -0.74 | -0.69 | -0.25 | -0.06 | 130. |
| 135. | -1.67 | -1.72 | -1.34 | -0.72 | -0.66 | -0.24 | -0.06 | 135. |
| 140. | -1.57 | -1.57 | -1.23 | -0.68 | -0.58 | -0.21 | -0.05 | 140. |
| 145. | -1.44 | -1.37 | -1.11 | -0.62 | -0.49 | -0.18 | -0.05 | 145. |
| 150. | -1.29 | -1.14 | -0.95 | -0.56 | -0.43 | -0.14 | -0.05 | 150. |
| 155. | -1.03 | -0.96 | -0.78 | -0.48 | -0.38 | -0.13 | -0.04 | 155. |
| 160. | -0.80 | -0.78 | -0.58 | -0.39 | -0.31 | -0.06 | -0.03 | 160. |
| 165. | -0.56 | -0.60 | -0.39 | -0.31 | -0.21 | -0.02 | -0.02 | 165. |
| 170. | -0.39 | -0.40 | -0.24 | -0.22 | -0.11 | 0.02 | -0.01 | 170. |
| 175. | -0.19 | -0.18 | -0.12 | -0.14 | -0.03 | 0.04 | -0.01 | 175. |
| 180. | -0.06 | 0.01 | -0.03 | -0.08 | 0.03 | 0.04 | -0.00 | 180. |
| 185. | 0.04 | 0.14 | 0.04 | -0.03 | 0.07 | 0.04 | -0.00 | 185. |
| 190. | 0.10 | 0.21 | 0.09 | 0.00 | 0.09 | 0.05 | -0.00 | 190. |
| 195. | 0.11 | 0.25 | 0.11 | 0.02 | 0.10 | 0.04 | -0.01 | 195. |
| 200. | 0.10 | 0.26 | 0.14 | 0.03 | 0.10 | 0.04 | -0.01 | 200. |
| 205. | 0.07 | 0.25 | 0.15 | 0.04 | 0.10 | 0.03 | -0.01 | 205. |
| 210. | 0.03 | 0.23 | 0.16 | 0.04 | 0.09 | 0.03 | -0.02 | 210. |
| 215. | -0.02 | 0.21 | 0.16 | 0.04 | 0.09 | 0.02 | -0.02 | 215. |
| 220. | -0.07 | 0.20 | 0.16 | 0.04 | 0.09 | 0.02 | -0.02 | 220. |
| 225. | -0.11 | 0.20 | 0.17 | 0.04 | 0.09 | 0.03 | -0.02 | 225. |
| 230. | -0.12 | 0.20 | 0.18 | 0.05 | 0.10 | 0.03 | -0.02 | 230. |
| 235. | -0.10 | 0.21 | 0.19 | 0.06 | 0.11 | 0.04 | -0.01 | 235. |
| 240. | -0.07 | 0.21 | 0.22 | 0.07 | 0.13 | 0.05 | -0.01 | 240. |
| 245. | -0.03 | 0.24 | 0.25 | 0.10 | 0.16 | 0.05 | 0.00 | 245. |
| 250. | 0.02 | 0.41 | 0.[illegible] | 0.14 | 0.19 | 0.06 | 0.00 | 250. |
| 255. | 0.08 | 0.47 | 0.47 | 0.18 | 0.22 | 0.06 | 0.01 | 255. |
| 260. | 0.14 | 0.52 | 0.53 | 0.22 | 0.23 | 0.07 | 0.01 | 260. |
| 265. | 0.20 | 0.54 | 0.47 | 0.25 | 0.23 | 0.07 | 0.01 | 265. |
| 270. | 0.25 | 0.60 | 0.51 | 0.26 | 0.24 | 0.08 | 0.01 | 270. |
| 275. | 0.31 | 0.63 | 0.53 | 0.27 | 0.25 | 0.09 | 0.02 | 275. |
| 280. | 0.37 | 0.65 | 0.53 | 0.28 | 0.26 | 0.10 | 0.02 | 280. |
| 285. | 0.42 | 0.64 | 0.53 | 0.29 | 0.27 | 0.10 | 0.02 | 285. |
| 290. | 0.46 | 0.60 | 0.51 | 0.29 | 0.27 | 0.11 | 0.02 | 290. |
| 295. | 0.43 | 0.65 | 0.49 | 0.30 | 0.25 | 0.12 | 0.02 | 295. |
| 300. | 0.40 | 0.62 | 0.47 | 0.29 | 0.23 | 0.10 | 0.02 | 300. |
| 305. | 0.40 | 0.60 | 0.45 | 0.29 | 0.23 | 0.10 | 0.02 | 305. |
| 310. | 0.42 | 0.61 | 0.44 | 0.28 | 0.24 | 0.10 | 0.02 | 310. |
| 315. | 0.45 | 0.63 | 0.44 | 0.28 | 0.25 | 0.11 | 0.03 | 315. |
| 320. | 0.48 | 0.63 | 0.44 | 0.28 | 0.25 | 0.11 | 0.03 | 320. |
| 325. | 0.44 | 0.59 | 0.42 | 0.28 | 0.24 | 0.11 | 0.03 | 325. |
| 330. | 0.43 | 0.52 | 0.36 | 0.28 | 0.22 | 0.09 | 0.03 | 330. |
| 335. | 0.32 | 0.43 | 0.29 | 0.27 | 0.18 | 0.06 | 0.03 | 335. |
| 340. | 0.26 | 0.31 | 0.22 | 0.24 | 0.13 | 0.04 | 0.02 | 340. |
| 345. | 0.26 | 0.27 | 0.18 | 0.22 | 0.13 | 0.04 | 0.02 | 345. |
| 350. | 0.35 | 0.27 | 0.23 | 0.22 | 0.13 | 0.04 | 0.03 | 350. |
| 355. | 0.37 | 0.46 | 0.23 | 0.22 | 0.12 | 0.05 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 175 TON= 35. C.G.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 189.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.957 | 2.393 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.48 | 0.35 | 0.30 | 0.29 | 0.17 | 0.09 | 0.04 | 0. |
| 5. | 0.13 | 0.21 | 0.16 | 0.18 | 0.11 | 0.02 | 0.01 | 5. |
| 10. | 0.13 | 0.18 | 0.14 | 0.14 | 0.19 | -0.01 | -0.01 | 10. |
| 15. | 0.27 | 0.22 | 0.16 | 0.13 | 0.25 | -0.01 | 0.00 | 15. |
| 20. | 0.42 | 0.31 | 0.18 | 0.11 | 0.29 | -0.03 | 0.01 | 20. |
| 25. | 0.58 | 0.40 | 0.24 | 0.12 | 0.33 | -0.05 | 0.01 | 25. |
| 30. | 0.78 | 0.52 | 0.35 | 0.19 | 0.43 | -0.05 | 0.01 | 30. |
| 35. | 0.99 | 0.69 | 0.50 | 0.30 | 0.54 | -0.02 | 0.01 | 35. |
| 40. | 1.18 | 0.88 | 0.72 | 0.44 | 0.64 | 0.03 | 0.03 | 40. |
| 45. | 1.33 | 1.04 | 0.93 | 0.56 | 0.67 | 0.08 | 0.05 | 45. |
| 50. | 1.41 | 1.15 | 1.08 | 0.62 | 0.67 | 0.10 | 0.03 | 50. |
| 55. | 1.39 | 1.11 | 1.15 | 0.64 | 0.61 | 0.08 | 0.01 | 55. |
| 60. | 1.24 | 0.89 | 1.19 | 0.55 | 0.56 | 0.04 | -0.00 | 60. |
| 65. | 1.00 | 0.66 | 1.13 | 0.41 | 0.56 | -0.01 | -0.02 | 65. |
| 70. | 0.63 | 0.39 | 0.93 | 0.26 | 0.64 | -0.13 | -0.05 | 70. |
| 75. | 0.22 | 0.08 | 0.62 | 0.10 | 0.28 | -0.16 | -0.08 | 75. |
| 80. | -0.16 | -0.25 | 0.25 | -0.09 | 0.17 | -0.23 | -0.10 | 80. |
| 85. | -0.50 | -0.58 | -0.16 | -0.35 | 0.06 | -0.30 | -0.11 | 85. |
| 90. | -0.83 | -0.83 | -0.56 | -0.62 | -0.03 | -0.35 | -0.10 | 90. |
| 95. | -1.19 | -1.07 | -0.87 | -0.86 | -0.13 | -0.36 | -0.09 | 95. |
| 100. | -1.57 | -1.30 | -1.12 | -1.05 | -0.21 | -0.36 | -0.10 | 100. |
| 105. | -1.90 | -1.54 | -1.33 | -1.15 | -0.30 | -0.37 | -0.11 | 105. |
| 110. | -2.14 | -1.76 | -1.48 | -1.21 | -0.37 | -0.38 | -0.11 | 110. |
| 115. | -2.31 | -1.93 | -1.59 | -1.26 | -0.41 | -0.39 | -0.12 | 115. |
| 120. | -2.42 | -2.00 | -1.65 | -1.28 | -0.42 | -0.40 | -0.10 | 120. |
| 125. | -2.47 | -2.00 | -1.67 | -1.27 | -0.41 | -0.39 | -0.10 | 125. |
| 130. | -2.47 | -1.93 | -1.65 | -1.23 | -0.40 | -0.37 | -0.10 | 130. |
| 135. | -2.47 | -1.84 | -1.58 | -1.17 | -0.39 | -0.34 | -0.09 | 135. |
| 140. | -2.41 | -1.72 | -1.48 | -1.08 | -0.38 | -0.30 | -0.08 | 140. |
| 145. | -2.28 | -1.56 | -1.33 | -0.99 | -0.36 | -0.26 | -0.06 | 145. |
| 150. | -2.10 | -1.34 | -1.14 | -0.86 | -0.32 | -0.22 | -0.05 | 150. |
| 155. | -1.88 | -1.04 | -0.91 | -0.72 | -0.26 | -0.17 | -0.04 | 155. |
| 160. | -1.24 | -0.75 | -0.69 | -0.55 | -0.20 | -0.13 | -0.02 | 160. |
| 165. | -1.01 | -0.54 | -0.50 | -0.38 | -0.15 | -0.08 | -0.01 | 165. |
| 170. | -0.72 | -0.40 | -0.36 | -0.25 | -0.12 | -0.04 | -0.00 | 170. |
| 175. | -0.42 | -0.29 | -0.24 | -0.16 | -0.09 | -0.01 | 0.00 | 175. |
| 180. | -0.23 | -0.19 | -0.15 | -0.08 | -0.11 | 0.02 | 0.01 | 180. |
| 185. | -0.10 | -0.10 | -0.07 | -0.02 | -0.13 | 0.04 | 0.01 | 185. |
| 190. | -0.02 | -0.03 | -0.01 | 0.03 | -0.14 | 0.05 | 0.01 | 190. |
| 195. | 0.03 | 0.03 | 0.03 | 0.06 | -0.14 | 0.06 | 0.01 | 195. |
| 200. | 0.05 | 0.08 | 0.05 | 0.07 | -0.13 | 0.07 | 0.01 | 200. |
| 205. | 0.06 | 0.10 | 0.05 | 0.08 | -0.13 | 0.08 | 0.01 | 205. |
| 210. | 0.06 | 0.10 | 0.04 | 0.09 | -0.14 | 0.08 | 0.01 | 210. |
| 215. | 0.05 | 0.10 | 0.03 | 0.11 | -0.17 | 0.08 | 0.01 | 215. |
| 220. | 0.05 | 0.09 | 0.01 | 0.13 | -0.19 | 0.09 | 0.01 | 220. |
| 225. | 0.06 | 0.08 | 0.02 | 0.15 | -0.21 | 0.09 | 0.02 | 225. |
| 230. | 0.08 | 0.10 | 0.04 | 0.17 | -0.22 | 0.12 | 0.02 | 230. |
| 235. | 0.12 | 0.14 | 0.06 | 0.18 | -0.22 | 0.11 | 0.03 | 235. |
| 240. | 0.18 | 0.18 | 0.09 | 0.19 | -0.22 | 0.13 | 0.04 | 240. |
| 245. | 0.25 | 0.24 | 0.13 | 0.21 | -0.20 | 0.14 | 0.04 | 245. |
| 250. | 0.34 | 0.30 | 0.19 | 0.26 | -0.18 | 0.15 | 0.04 | 250. |
| 255. | 0.48 | 0.38 | 0.25 | 0.34 | -0.16 | 0.17 | 0.04 | 255. |
| 260. | 0.66 | 0.48 | 0.31 | 0.41 | -0.14 | 0.18 | 0.04 | 260. |
| 265. | 0.71 | 0.54 | 0.38 | 0.45 | -0.13 | 0.19 | 0.04 | 265. |
| 270. | 0.82 | 0.63 | 0.45 | 0.48 | -0.13 | 0.20 | 0.05 | 270. |
| 275. | 0.91 | 0.70 | 0.52 | 0.49 | -0.12 | 0.21 | 0.05 | 275. |
| 280. | 0.98 | 0.74 | 0.55 | 0.50 | -0.07 | 0.22 | 0.05 | 280. |
| 285. | 1.01 | 0.76 | 0.56 | 0.51 | 0.01 | 0.23 | 0.05 | 285. |
| 290. | 1.01 | 0.75 | 0.52 | 0.51 | 0.07 | 0.22 | 0.05 | 290. |
| 295. | 0.97 | 0.74 | 0.51 | 0.48 | 0.11 | 0.21 | 0.05 | 295. |
| 300. | 0.92 | 0.73 | 0.51 | 0.47 | 0.13 | 0.19 | 0.05 | 300. |
| 305. | 0.89 | 0.72 | 0.51 | 0.46 | 0.15 | 0.19 | 0.05 | 305. |
| 310. | 0.94 | 0.73 | 0.51 | 0.48 | 0.20 | 0.20 | 0.06 | 310. |
| 315. | 1.00 | 0.76 | 0.54 | 0.51 | 0.24 | 0.21 | 0.06 | 315. |
| 320. | 1.08 | 0.80 | 0.56 | 0.53 | 0.25 | 0.22 | 0.07 | 320. |
| 325. | 1.08 | 0.79 | 0.55 | 0.54 | 0.24 | 0.22 | 0.07 | 325. |
| 330. | 1.03 | 0.74 | 0.53 | 0.52 | 0.21 | 0.21 | 0.07 | 330. |
| 335. | 0.86 | 0.67 | 0.43 | 0.44 | 0.13 | 0.18 | 0.06 | 335. |
| 340. | 0.77 | 0.58 | 0.39 | 0.38 | 0.03 | 0.16 | 0.05 | 340. |
| 345. | 0.84 | 0.60 | 0.41 | 0.39 | -0.01 | 0.16 | 0.06 | 345. |
| 350. | 1.01 | 0.76 | 0.41 | 0.49 | 0.11 | 0.18 | 0.07 | 350. |
| 355. | 1.00 | 0.77 | 0.38 | 0.51 | 0.20 | 0.18 | 0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 175 TCN= 16. C.R.= 44.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ DEG. | CHORD STATION 0.455 | 1.249 | 1.950 | 3.990 | 4.550 | 7.150 | 10.490 | AZ DEG. |
|---|---|---|---|---|---|---|---|---|
| 0. | 0.76 | 0.55 | 0.15 | 0.10 | 0.07 | 0.09 | -0.01 | 0. |
| 5. | 0.23 | 0.21 | -0.04 | 0.03 | 0.04 | 0.04 | -0.01 | 5. |
| 10. | 0.31 | 0.28 | -0.05 | 0.00 | 0.02 | 0.01 | -0.03 | 10. |
| 15. | 0.43 | 0.40 | 0.03 | -0.03 | 0.01 | -0.02 | -0.05 | 15. |
| 20. | 0.52 | 0.45 | 0.04 | -0.07 | 0.04 | -0.05 | -0.06 | 20. |
| 25. | 0.67 | 0.52 | 0.07 | -0.05 | 0.09 | -0.07 | -0.07 | 25. |
| 30. | 0.84 | 0.64 | 0.17 | 0.02 | 0.16 | -0.08 | -0.07 | 30. |
| 35. | 0.96 | 0.79 | 0.30 | 0.16 | 0.23 | -0.06 | -0.06 | 35. |
| 40. | 1.07 | 0.97 | 0.46 | 0.33 | 0.29 | -0.05 | -0.05 | 40. |
| 45. | 1.19 | 1.13 | 0.68 | 0.45 | 0.34 | -0.06 | -0.06 | 45. |
| 50. | 1.32 | 1.21 | 1.21 | 0.51 | 0.36 | -0.09 | -0.08 | 50. |
| 55. | 1.34 | 1.21 | 2.03 | 0.53 | 0.33 | -0.14 | -0.10 | 55. |
| 60. | 1.18 | 1.05 | 2.27 | 0.51 | 0.27 | -0.20 | -0.11 | 60. |
| 65. | 0.89 | 0.76 | 2.05 | 0.53 | 0.19 | -0.26 | -0.10 | 65. |
| 70. | 0.50 | 0.42 | 1.62 | 0.63 | 0.09 | -0.31 | -0.11 | 70. |
| 75. | 0.03 | 0.04 | 1.22 | 0.70 | -0.02 | -0.35 | -0.13 | 75. |
| 80. | -0.52 | -0.35 | 0.83 | 0.62 | -0.11 | -0.39 | -0.14 | 80. |
| 85. | -1.00 | -0.74 | 0.61 | 0.29 | -0.16 | -0.41 | -0.12 | 85. |
| 90. | -1.55 | -1.13 | 0.29 | -0.32 | -0.20 | -0.42 | -0.07 | 90. |
| 95. | -1.95 | -1.47 | -0.23 | -0.66 | -0.23 | -0.42 | -0.06 | 95. |
| 100. | -2.29 | -1.71 | -0.75 | -0.80 | -0.28 | -0.42 | -0.09 | 100. |
| 105. | -2.55 | -1.87 | -1.32 | -0.84 | -0.34 | -0.42 | -0.09 | 105. |
| 110. | -2.75 | -1.99 | -1.75 | -0.93 | -0.38 | -0.43 | -0.08 | 110. |
| 115. | -2.89 | -2.08 | -1.95 | -1.01 | -0.43 | -0.44 | -0.06 | 115. |
| 120. | -2.98 | -2.12 | -1.97 | -1.08 | -0.46 | -0.45 | -0.05 | 120. |
| 125. | -3.01 | -2.12 | -1.89 | -1.10 | -0.49 | -0.45 | -0.04 | 125. |
| 130. | -2.95 | -2.07 | -1.82 | -1.10 | -0.49 | -0.45 | -0.04 | 130. |
| 135. | -2.84 | -1.98 | -1.70 | -1.07 | -0.47 | -0.42 | -0.07 | 135. |
| 140. | -2.66 | -1.86 | -1.57 | -1.02 | -0.44 | -0.38 | -0.07 | 140. |
| 145. | -2.42 | -1.67 | -1.44 | -0.95 | -0.39 | -0.32 | -0.07 | 145. |
| 150. | -2.14 | -1.45 | -1.29 | -0.87 | -0.34 | -0.26 | -0.06 | 150. |
| 155. | -1.83 | -1.21 | -1.12 | -0.76 | -0.28 | -0.20 | -0.05 | 155. |
| 160. | -1.52 | -0.98 | -0.95 | -0.65 | -0.22 | -0.15 | -0.04 | 160. |
| 165. | -1.22 | -0.77 | -0.78 | -0.51 | -0.16 | -0.10 | -0.01 | 165. |
| 170. | -0.92 | -0.58 | -0.62 | -0.36 | -0.11 | -0.05 | 0.01 | 170. |
| 175. | -0.65 | -0.41 | -0.48 | -0.22 | -0.06 | -0.03 | 0.03 | 175. |
| 180. | -0.40 | -0.26 | -0.37 | -0.13 | -0.02 | 0.05 | 0.04 | 180. |
| 185. | -0.19 | -0.15 | -0.28 | -0.08 | -0.01 | 0.07 | 0.04 | 185. |
| 190. | -0.07 | -0.06 | -0.21 | -0.04 | -0.01 | 0.09 | 0.04 | 190. |
| 195. | -0.01 | -0.00 | -0.15 | -0.01 | -0.01 | 0.09 | 0.04 | 195. |
| 200. | 0.01 | 0.03 | -0.11 | 0.01 | -0.02 | 0.10 | 0.04 | 200. |
| 205. | 0.02 | 0.05 | -0.10 | 0.02 | -0.03 | 0.11 | 0.04 | 205. |
| 210. | 0.04 | 0.05 | -0.09 | 0.03 | -0.03 | 0.12 | 0.04 | 210. |
| 215. | 0.06 | 0.04 | -0.08 | 0.04 | -0.04 | 0.14 | 0.05 | 215. |
| 220. | 0.09 | 0.04 | -0.07 | 0.05 | -0.04 | 0.16 | 0.06 | 220. |
| 225. | 0.12 | 0.04 | -0.06 | 0.06 | -0.03 | 0.18 | 0.06 | 225. |
| 230. | 0.18 | 0.06 | -0.05 | 0.08 | -0.03 | 0.23 | 0.07 | 230. |
| 235. | 0.24 | 0.08 | -0.02 | 0.11 | -0.02 | 0.21 | 0.07 | 235. |
| 240. | 0.32 | 0.11 | 0.02 | 0.15 | -0.00 | 0.22 | 0.08 | 240. |
| 245. | 0.42 | 0.17 | 0.08 | 0.19 | 0.02 | 0.24 | 0.08 | 245. |
| 250. | 0.55 | 0.25 | 0.14 | 0.24 | 0.06 | 0.25 | 0.09 | 250. |
| 255. | 0.68 | 0.34 | 0.21 | 0.28 | 0.09 | 0.27 | 0.09 | 255. |
| 260. | 0.82 | 0.45 | 0.27 | 0.32 | 0.12 | 0.29 | 0.09 | 260. |
| 265. | 0.97 | 0.56 | 0.33 | 0.35 | 0.14 | 0.31 | 0.09 | 265. |
| 270. | 1.14 | 0.67 | 0.37 | 0.38 | 0.15 | 0.32 | 0.09 | 270. |
| 275. | 1.28 | 0.77 | 0.46 | 0.43 | 0.17 | 0.33 | 0.09 | 275. |
| 280. | 1.40 | 0.86 | 0.51 | 0.47 | 0.17 | 0.33 | 0.09 | 280. |
| 285. | 1.44 | 0.91 | 0.51 | 0.50 | 0.16 | 0.32 | 0.09 | 285. |
| 290. | 1.44 | 0.95 | 0.49 | 0.47 | 0.18 | 0.31 | 0.08 | 290. |
| 295. | 1.37 | 0.92 | 0.46 | 0.41 | 0.18 | 0.30 | 0.08 | 295. |
| 300. | 1.27 | 0.86 | 0.43 | 0.36 | 0.19 | 0.29 | 0.07 | 300. |
| 305. | 1.22 | 0.81 | 0.41 | 0.35 | 0.20 | 0.29 | 0.07 | 305. |
| 310. | 1.28 | 0.78 | 0.40 | 0.37 | 0.21 | 0.30 | 0.07 | 310. |
| 315. | 1.37 | 0.85 | 0.42 | 0.41 | 0.21 | 0.30 | 0.07 | 315. |
| 320. | 1.46 | 0.93 | 0.50 | 0.45 | 0.22 | 0.30 | 0.07 | 320. |
| 325. | 1.55 | 0.98 | 0.56 | 0.48 | 0.22 | 0.30 | 0.07 | 325. |
| 330. | 1.43 | 0.99 | 0.51 | 0.46 | 0.22 | 0.29 | 0.06 | 330. |
| 335. | 1.25 | 0.96 | 0.42 | 0.39 | 0.19 | 0.26 | 0.04 | 335. |
| 340. | 1.15 | 0.90 | 0.36 | 0.33 | 0.17 | 0.23 | 0.03 | 340. |
| 345. | 1.27 | 0.96 | 0.37 | 0.36 | 0.18 | 0.22 | 0.05 | 345. |
| 350. | 1.66 | 1.08 | 0.52 | 0.43 | 0.20 | 0.22 | 0.05 | 350. |
| 355. | 1.67 | 0.99 | 0.49 | 0.31 | 0.16 | 0.17 | 0.01 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=532 CNTR NO. 188 TCN= 37. C.R.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ DEG. | CHORD STATION 3.455 | 1.950 | 4.350 | 10.400 | AZ DEG. |
|---|---|---|---|---|---|
| 0. | -0.82 | -0.41 | -0.19 | -0.02 | 0. |
| 5. | -0.80 | -0.37 | -0.18 | -0.00 | 5. |
| 10. | -0.69 | -0.35 | -0.14 | 0.00 | 10. |
| 15. | -0.57 | -0.25 | -0.10 | -0.01 | 15. |
| 20. | -0.18 | -0.09 | -0.03 | -0.02 | 20. |
| 25. | 0.28 | 0.04 | 0.00 | -0.03 | 25. |
| 30. | 0.05 | -0.09 | -0.08 | -0.05 | 30. |
| 35. | -0.27 | -0.20 | -0.13 | -0.05 | 35. |
| 40. | -0.27 | -0.19 | -0.08 | -0.04 | 40. |
| 45. | -0.02 | -0.09 | -0.02 | -0.04 | 45. |
| 50. | 0.17 | 0.01 | 0.01 | -0.04 | 50. |
| 55. | 0.22 | 0.01 | 0.02 | -0.04 | 55. |
| 60. | 0.20 | 0.00 | 0.02 | -0.04 | 60. |
| 65. | 0.20 | 0.01 | 0.02 | -0.03 | 65. |
| 70. | 0.24 | 0.05 | 0.04 | -0.04 | 70. |
| 75. | 0.30 | 0.09 | 0.06 | -0.04 | 75. |
| 80. | 0.38 | 0.13 | 0.08 | -0.03 | 80. |
| 85. | 0.45 | 0.17 | 0.11 | -0.02 | 85. |
| 90. | 0.54 | 0.21 | 0.14 | -0.01 | 90. |
| 95. | 0.63 | 0.26 | 0.18 | -0.00 | 95. |
| 100. | 0.73 | 0.31 | 0.21 | 0.00 | 100. |
| 105. | 0.85 | 0.38 | 0.24 | 0.01 | 105. |
| 110. | 0.96 | 0.43 | 0.27 | 0.02 | 110. |
| 115. | 1.05 | 0.48 | 0.30 | 0.04 | 115. |
| 120. | 1.12 | 0.52 | 0.33 | 0.04 | 120. |
| 125. | 1.17 | 0.56 | 0.35 | 0.05 | 125. |
| 130. | 1.21 | 0.59 | 0.37 | 0.05 | 130. |
| 135. | 1.23 | 0.60 | 0.38 | 0.04 | 135. |
| 140. | 1.23 | 0.61 | 0.38 | 0.04 | 140. |
| 145. | 1.22 | 0.61 | 0.37 | 0.04 | 145. |
| 150. | 1.20 | 0.59 | 0.36 | 0.04 | 150. |
| 155. | 1.15 | 0.56 | 0.34 | 0.04 | 155. |
| 160. | 1.09 | 0.53 | 0.31 | 0.04 | 160. |
| 165. | 1.00 | 0.48 | 0.27 | 0.04 | 165. |
| 170. | 0.89 | 0.42 | 0.22 | 0.04 | 170. |
| 175. | 0.76 | 0.33 | 0.17 | 0.04 | 175. |
| 180. | 0.59 | 0.25 | 0.13 | 0.04 | 180. |
| 185. | 0.32 | 0.16 | 0.10 | 0.04 | 185. |
| 190. | 0.07 | 0.09 | 0.07 | 0.04 | 190. |
| 195. | -0.12 | 0.04 | 0.04 | 0.04 | 195. |
| 200. | -0.22 | 0.01 | -0.01 | 0.04 | 200. |
| 205. | -0.25 | 0.04 | -0.07 | 0.03 | 205. |
| 210. | -0.36 | 0.07 | -0.13 | 0.03 | 210. |
| 215. | -0.49 | 0.05 | -0.17 | 0.03 | 215. |
| 220. | -0.60 | -0.05 | -0.18 | 0.02 | 220. |
| 225. | -0.65 | -0.16 | -0.18 | 0.01 | 225. |
| 230. | -0.68 | -0.22 | -0.18 | 0.01 | 230. |
| 235. | -0.69 | -0.26 | -0.18 | -0.00 | 235. |
| 240. | -0.69 | -0.27 | -0.18 | -0.01 | 240. |
| 245. | -0.69 | -0.27 | -0.18 | -0.01 | 245. |
| 250. | -0.69 | -0.28 | -0.18 | -0.01 | 250. |
| 255. | -0.69 | -0.29 | -0.19 | -0.01 | 255. |
| 260. | -0.69 | -0.30 | -0.19 | -0.01 | 260. |
| 265. | -0.59 | -0.30 | -0.19 | -0.01 | 265. |
| 270. | -0.59 | -0.30 | -0.19 | -0.01 | 270. |
| 275. | -0.59 | -0.30 | -0.18 | -0.01 | 275. |
| 280. | -0.59 | -0.30 | -0.18 | -0.01 | 280. |
| 285. | -0.59 | -0.30 | -0.17 | -0.01 | 285. |
| 290. | -0.60 | -0.30 | -0.17 | -0.01 | 290. |
| 295. | -0.58 | -0.29 | -0.16 | -0.02 | 295. |
| 300. | -0.56 | -0.29 | -0.16 | -0.02 | 300. |
| 305. | -0.54 | -0.29 | -0.15 | -0.02 | 305. |
| 310. | -0.55 | -0.30 | -0.15 | -0.02 | 310. |
| 315. | -0.57 | -0.31 | -0.14 | -0.01 | 315. |
| 320. | -0.61 | -0.33 | -0.15 | -0.00 | 320. |
| 325. | -0.68 | -0.34 | -0.16 | -0.01 | 325. |
| 330. | -0.64 | -0.33 | -0.16 | -0.03 | 330. |
| 335. | -0.51 | -0.29 | -0.14 | -0.04 | 335. |
| 340. | -0.36 | -0.23 | -0.12 | -0.03 | 340. |
| 345 | -0.26 | -0.17 | -0.11 | -0.02 | 345. |
| 350. | -0.46 | -0.22 | -0.14 | -0.02 | 350. |
| 355. | -0.72 | -0.35 | -0.17 | -0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 188 TCN= 37. C.P.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.240 | 1.950 | 2.990 | 4.990 | 7.150 | 10.420 | DEG. |
| 0. | -0.89 | -0.69 | -0.52 | -0.34 | -0.26 | -0.14 | -0.02 | 0. |
| 5. | -0.88 | -0.55 | -0.47 | -0.32 | -0.22 | -0.15 | -0.05 | 5. |
| 10. | -0.87 | -0.49 | -0.46 | -0.31 | -0.20 | -0.14 | -0.02 | 10. |
| 15. | -0.85 | -0.57 | -0.48 | -0.33 | -0.21 | -0.15 | -0.04 | 15. |
| 20. | -0.82 | -0.57 | -0.46 | -0.32 | -0.20 | -0.14 | -0.04 | 20. |
| 25. | -0.83 | -0.47 | -0.39 | -0.28 | -0.15 | -0.13 | -0.04 | 25. |
| 30. | -0.38 | -0.29 | -0.29 | -0.21 | -0.10 | -0.11 | -0.02 | 30. |
| 35. | -0.20 | -0.16 | -0.24 | -0.17 | -0.09 | -0.11 | -0.03 | 35. |
| 40. | -0.09 | -0.09 | -0.21 | -0.14 | -0.05 | -0.10 | -0.04 | 40. |
| 45. | -0.02 | -0.03 | -0.17 | -0.11 | -0.00 | -0.09 | -0.04 | 45. |
| 50. | 0.04 | 0.01 | -0.15 | -0.09 | 0.04 | -0.09 | -0.03 | 50. |
| 55. | 0.10 | 0.05 | -0.13 | -0.06 | 0.05 | -0.08 | -0.03 | 55. |
| 60. | 0.14 | 0.07 | -0.03 | -0.03 | 0.07 | -0.07 | -0.02 | 60. |
| 65. | 0.26 | 0.13 | -0.01 | 0.01 | 0.12 | -0.05 | -0.02 | 65. |
| 70. | 0.37 | 0.22 | 0.05 | 0.05 | 0.18 | -0.03 | -0.00 | 70. |
| 75. | 0.49 | 0.32 | 0.12 | 0.10 | 0.21 | -0.02 | 0.00 | 75. |
| 80. | 0.61 | 0.41 | 0.18 | 0.15 | 0.24 | 0.02 | 0.05 | 80. |
| 85. | 0.73 | 0.49 | 0.25 | 0.20 | 0.29 | 0.03 | 0.06 | 85. |
| 90. | 0.84 | 0.57 | 0.31 | 0.25 | 0.34 | 0.05 | 0.02 | 90. |
| 95. | 0.98 | 0.65 | 0.38 | 0.29 | 0.38 | 0.07 | 0.03 | 95. |
| 100. | 1.10 | 0.73 | 0.44 | 0.34 | 0.41 | 0.09 | 0.04 | 100. |
| 105. | 1.20 | 0.82 | 0.49 | 0.39 | 0.43 | 0.10 | 0.04 | 105. |
| 110. | 1.29 | 0.89 | 0.55 | 0.43 | 0.43 | 0.12 | 0.04 | 110. |
| 115. | 1.37 | 0.91 | 0.60 | 0.47 | 0.44 | 0.13 | 0.04 | 115. |
| 120. | 1.45 | 0.94 | 0.64 | 0.50 | 0.46 | 0.15 | 0.05 | 120. |
| 125. | 1.52 | 1.02 | 0.69 | 0.53 | 0.47 | 0.18 | 0.06 | 125. |
| 130. | 1.58 | 1.10 | 0.73 | 0.54 | 0.47 | 0.20 | 0.08 | 130. |
| 135. | 1.64 | 1.14 | 0.76 | 0.55 | 0.47 | 0.21 | 0.08 | 135. |
| 140. | 1.72 | 1.16 | 0.79 | 0.55 | 0.46 | 0.22 | 0.07 | 140. |
| 145. | 1.79 | 1.18 | 0.82 | 0.55 | 0.44 | 0.22 | 0.07 | 145. |
| 150. | 1.85 | 1.21 | 0.84 | 0.56 | 0.43 | 0.23 | 0.08 | 150. |
| 155. | 1.89 | 1.25 | 0.85 | 0.56 | 0.42 | 0.23 | 0.08 | 155. |
| 160. | 1.90 | 1.26 | 0.87 | 0.56 | 0.41 | 0.24 | 0.08 | 160. |
| 165. | 1.86 | 1.25 | 0.87 | 0.56 | 0.39 | 0.24 | 0.08 | 165. |
| 170. | 1.76 | 1.19 | 0.84 | 0.55 | 0.36 | 0.24 | 0.07 | 170. |
| 175. | 1.63 | 1.10 | 0.78 | 0.51 | 0.33 | 0.23 | 0.07 | 175. |
| 180. | 1.45 | 0.97 | 0.69 | 0.45 | 0.28 | 0.21 | 0.06 | 180. |
| 185. | 1.22 | 0.80 | 0.59 | 0.38 | 0.21 | 0.17 | 0.05 | 185. |
| 190. | 0.95 | 0.62 | 0.45 | 0.30 | 0.15 | 0.14 | 0.03 | 190. |
| 195. | 0.67 | 0.42 | 0.32 | 0.21 | 0.09 | 0.10 | 0.02 | 195. |
| 200. | 0.39 | 0.23 | 0.19 | 0.12 | 0.03 | 0.07 | 0.01 | 200. |
| 205. | 0.15 | 0.06 | 0.08 | 0.03 | -0.02 | 0.04 | 0.00 | 205. |
| 210. | -0.08 | -0.06 | -0.00 | -0.02 | -0.06 | 0.02 | 0.00 | 210. |
| 215. | -0.30 | -0.15 | -0.05 | -0.08 | -0.10 | 0.00 | 0.00 | 215. |
| 220. | -0.52 | -0.19 | -0.05 | -0.11 | -0.15 | -0.01 | -0.00 | 220. |
| 225. | -0.70 | -0.19 | -0.01 | -0.12 | -0.20 | -0.03 | -0.02 | 225. |
| 230. | -0.71 | -0.23 | 0.05 | -0.12 | -0.26 | -0.04 | -0.02 | 230. |
| 235. | -0.77 | -0.35 | 0.06 | -0.10 | -0.30 | -0.06 | -0.01 | 235. |
| 240. | -0.87 | -0.47 | 0.02 | -0.04 | -0.33 | -0.09 | -0.00 | 240. |
| 245. | -0.99 | -0.56 | -0.08 | -0.04 | -0.34 | -0.10 | -0.01 | 245. |
| 250. | -1.07 | -0.64 | -0.23 | -0.07 | -0.30 | -0.10 | -0.02 | 250. |
| 255. | -1.12 | -0.71 | -0.36 | -0.12 | -0.25 | -0.09 | -0.02 | 255. |
| 260. | -1.14 | -0.76 | -0.45 | -0.26 | -0.22 | -0.07 | -0.02 | 260. |
| 265. | -1.18 | -0.80 | -0.50 | -0.40 | -0.22 | -0.06 | -0.03 | 265. |
| 270. | -1.18 | -0.81 | -0.52 | -0.34 | -0.24 | -0.07 | -0.04 | 270. |
| 275 | -1.18 | -0.81 | -0.52 | -0.35 | -0.28 | -0.07 | -0.05 | 275. |
| 280. | -1.16 | -0.80 | -0.52 | -0.35 | -0.28 | -0.07 | -0.05 | 280. |
| 285. | -1.14 | -0.78 | -0.52 | -0.36 | -0.29 | -0.07 | -0.05 | 285. |
| 290. | -1.13 | -0.77 | -0.52 | -0.37 | -0.30 | -0.07 | -0.04 | 290. |
| 295. | -1.11 | -0.76 | -0.52 | -0.38 | -0.32 | -0.09 | -0.04 | 295. |
| 300. | -1.09 | -0.75 | -0.52 | -0.37 | -0.33 | -0.10 | -0.04 | 300. |
| 305. | -1.08 | -0.74 | -0.51 | -0.37 | -0.32 | -0.10 | -0.04 | 305. |
| 310. | -1.07 | -0.72 | -0.51 | -0.37 | -0.30 | -0.10 | -0.04 | 310. |
| 315. | -1.06 | -0.72 | -0.49 | -0.36 | -0.29 | -0.09 | -0.04 | 315. |
| 320. | -1.05 | -0.71 | -0.47 | -0.35 | -0.28 | -0.09 | -0.03 | 320. |
| 325. | -1.02 | -0.71 | -0.47 | -0.35 | -0.28 | -0.09 | -0.02 | 325. |
| 330. | -0.98 | -0.73 | -0.48 | -0.35 | -0.28 | -0.09 | -0.02 | 330. |
| 335. | -1.01 | -0.77 | -0.51 | -0.36 | -0.27 | -0.09 | -0.02 | 335. |
| 340. | -1.13 | -0.83 | -0.55 | -0.37 | -0.28 | -0.10 | -0.03 | 340. |
| 345. | -1.33 | -0.95 | -0.64 | -0.41 | -0.33 | -0.12 | -0.05 | 345. |
| 350. | -1.45 | -1.05 | -0.73 | -0.47 | -0.36 | -0.15 | -0.06 | 350. |
| 355. | -1.13 | -0.74 | -0.56 | -0.38 | -0.27 | -0.12 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 188 TCN= 37. C.R.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.455 | 1.040 | 1.990 | 3.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -3.74 | -0.85 | -0.58 | -0.41 | -0.32 | -0.16 | -0.07 | 0. |
| 5. | -1.02 | -0.80 | -0.48 | -0.34 | -0.29 | -0.18 | -0.06 | 5. |
| 10. | -0.54 | -0.43 | -0.31 | -0.25 | -0.23 | -0.18 | -0.09 | 10. |
| 15. | -0.58 | -0.51 | -0.36 | -0.26 | -0.20 | -0.14 | -0.09 | 15. |
| 20. | -0.55 | -0.45 | -0.33 | -0.21 | -0.11 | -0.12 | -0.08 | 20. |
| 25. | -0.44 | -0.36 | -0.27 | -0.20 | -0.15 | -0.14 | -0.10 | 25. |
| 30. | -0.27 | -0.35 | -0.26 | -0.20 | -0.06 | -0.13 | -0.10 | 30. |
| 35. | -0.06 | -0.24 | -0.17 | -0.13 | 0.04 | -0.11 | -0.09 | 35. |
| 40. | 0.17 | -0.05 | -0.14 | -0.04 | 0.12 | -0.11 | -0.10 | 40. |
| 45. | 0.40 | 0.15 | 0.06 | 0.04 | 0.19 | -0.09 | -0.09 | 45. |
| 50. | 0.60 | 0.30 | 0.14 | 0.10 | 0.27 | -0.07 | -0.08 | 50. |
| 55. | 0.72 | 0.36 | 0.18 | 0.12 | 0.31 | -0.05 | -0.08 | 55. |
| 60. | 0.76 | 0.36 | 0.20 | 0.13 | 0.31 | -0.04 | -0.07 | 60. |
| 65. | 0.78 | 0.32 | 0.19 | 0.12 | 0.27 | -0.04 | -0.07 | 65. |
| 70. | 0.79 | 0.33 | 0.19 | 0.12 | 0.26 | -0.04 | -0.07 | 70. |
| 75. | 0.79 | 0.34 | 0.19 | 0.12 | 0.27 | -0.02 | -0.05 | 75. |
| 80. | 0.82 | 0.36 | 0.19 | 0.13 | 0.28 | 0.00 | -0.04 | 80. |
| 85. | 0.87 | 0.37 | 0.20 | 0.15 | 0.29 | -0.01 | -0.05 | 85. |
| 90. | 0.92 | 0.39 | 0.23 | 0.17 | 0.30 | -0.01 | -0.05 | 90. |
| 95. | 0.96 | 0.40 | 0.26 | 0.19 | 0.31 | 0.01 | -0.03 | 95. |
| 100. | 0.98 | 0.42 | 0.30 | 0.20 | 0.32 | 0.05 | -0.01 | 100. |
| 105. | 0.99 | 0.44 | 0.33 | 0.21 | 0.33 | 0.06 | -0.01 | 105. |
| 110. | 1.00 | 0.45 | 0.36 | 0.22 | 0.32 | 0.06 | -0.02 | 110. |
| 115. | 0.97 | 0.44 | 0.36 | 0.22 | 0.31 | 0.05 | -0.01 | 115. |
| 120. | 0.94 | 0.45 | 0.33 | 0.22 | 0.30 | 0.06 | 0.01 | 120. |
| 125. | 0.92 | 0.45 | 0.32 | 0.23 | 0.30 | 0.08 | 0.03 | 125. |
| 130. | 0.91 | 0.46 | 0.33 | 0.23 | 0.31 | 0.10 | 0.04 | 130. |
| 135. | 0.94 | 0.46 | 0.35 | 0.25 | 0.32 | 0.12 | 0.05 | 135. |
| 140. | 0.98 | 0.41 | 0.40 | 0.28 | 0.33 | 0.14 | 0.06 | 140. |
| 145. | 1.03 | 0.70 | 0.47 | 0.32 | 0.34 | 0.16 | 0.07 | 145. |
| 150. | 1.11 | 0.80 | 0.54 | 0.37 | 0.35 | 0.18 | 0.09 | 150. |
| 155. | 1.19 | 0.87 | 0.60 | 0.42 | 0.36 | 0.20 | 0.10 | 155. |
| 160. | 1.28 | 0.91 | 0.65 | 0.46 | 0.38 | 0.21 | 0.12 | 160. |
| 165. | 1.33 | 0.95 | 0.69 | 0.50 | 0.38 | 0.23 | 0.11 | 165. |
| 170. | 1.33 | 1.00 | 0.70 | 0.52 | 0.38 | 0.24 | 0.11 | 170. |
| 175. | 1.24 | 1.02 | 0.69 | 0.51 | 0.36 | 0.24 | 0.12 | 175. |
| 180. | 1.10 | 0.97 | 0.66 | 0.49 | 0.33 | 0.23 | 0.12 | 180. |
| 185. | 0.94 | 0.86 | 0.60 | 0.44 | 0.28 | 0.21 | 0.11 | 185. |
| 190. | 0.76 | 0.71 | 0.52 | 0.38 | 0.22 | 0.19 | 0.10 | 190. |
| 195. | 0.56 | 0.56 | 0.42 | 0.31 | 0.15 | 0.16 | 0.09 | 195. |
| 200. | 0.35 | 0.40 | 0.30 | 0.24 | 0.09 | 0.13 | 0.07 | 200. |
| 205. | 0.15 | 0.25 | 0.19 | 0.16 | 0.03 | 0.10 | 0.07 | 205. |
| 210. | -0.04 | 0.11 | 0.11 | 0.10 | -0.03 | 0.08 | 0.06 | 210. |
| 215. | -0.21 | 0.00 | 0.04 | 0.03 | -0.08 | 0.07 | 0.06 | 215. |
| 220. | -0.36 | -0.09 | -0.02 | -0.02 | -0.12 | 0.05 | 0.06 | 220. |
| 225. | -0.49 | -0.17 | -0.10 | -0.06 | -0.16 | 0.04 | 0.05 | 225. |
| 230. | -0.61 | -0.25 | -0.13 | -0.10 | -0.19 | 0.03 | 0.05 | 230. |
| 235. | -0.71 | -0.32 | -0.18 | -0.13 | -0.22 | 0.01 | 0.05 | 235. |
| 240. | -0.79 | -0.39 | -0.23 | -0.16 | -0.25 | -0.01 | 0.03 | 240. |
| 245. | -0.87 | -0.45 | -0.25 | -0.19 | -0.28 | -0.02 | 0.02 | 245. |
| 250. | -0.95 | -0.50 | -0.33 | -0.22 | -0.30 | -0.04 | 0.01 | 250. |
| 255. | -1.02 | -0.54 | -0.33 | -0.24 | -0.31 | -0.05 | 0.01 | 255. |
| 260. | -1.08 | -0.59 | -0.36 | -0.25 | -0.33 | -0.06 | 0.00 | 260. |
| 265. | -1.13 | -0.61 | -0.38 | -0.27 | -0.34 | -0.06 | 0.01 | 265. |
| 270. | -1.15 | -0.63 | -0.40 | -0.28 | -0.36 | -0.06 | 0.01 | 270. |
| 275. | -1.16 | -0.65 | -0.42 | -0.29 | -0.37 | -0.06 | 0.01 | 275. |
| 280. | -1.17 | -0.66 | -0.43 | -0.30 | -0.37 | -0.05 | 0.02 | 280. |
| 285. | -1.18 | -0.67 | -0.44 | -0.30 | -0.37 | -0.05 | 0.03 | 285. |
| 290. | -1.21 | -0.68 | -0.44 | -0.31 | -0.36 | -0.04 | 0.04 | 290. |
| 295. | -1.24 | -0.70 | -0.46 | -0.32 | -0.37 | -0.03 | 0.02 | 295. |
| 300. | -1.26 | -0.72 | -0.49 | -0.34 | -0.40 | -0.12 | -0.02 | 300. |
| 305. | -1.29 | -0.72 | -0.53 | -0.37 | -0.43 | -0.14 | -0.07 | 305. |
| 310. | -1.29 | -0.72 | -0.52 | -0.36 | -0.41 | -0.13 | -0.05 | 310. |
| 315. | -1.26 | -0.71 | -0.50 | -0.34 | -0.37 | -0.13 | -0.02 | 315. |
| 320. | -1.17 | -0.67 | -0.45 | -0.31 | -0.34 | -0.13 | -0.01 | 320. |
| 325. | -1.05 | -0.61 | -0.39 | -0.28 | -0.31 | -0.13 | -0.03 | 325. |
| 330. | -0.90 | -0.53 | -0.33 | -0.22 | -0.27 | -0.09 | -0.02 | 330. |
| 335. | -0.71 | -0.38 | -0.24 | -0.14 | -0.21 | -0.05 | -0.01 | 335. |
| 340. | -0.47 | -0.22 | -0.16 | -0.09 | -0.16 | -0.07 | -0.03 | 340. |
| 345. | -0.22 | -0.20 | -0.16 | -0.11 | -0.16 | -0.11 | -0.07 | 345. |
| 350. | -0.12 | -0.47 | -0.28 | -0.23 | -0.22 | -0.10 | -0.07 | 350. |
| 355. | -0.24 | -0.70 | -0.57 | -0.45 | -0.34 | -0.16 | -0.07 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 188 TC№ 37. C.P.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.157 | 10.422 | DEG. |
| 0. | -0.55 | -0.44 | -0.35 | -0.29 | -0.20 | -0.08 | -0.03 | 0. |
| 5. | -0.51 | -0.36 | -0.25 | -0.26 | -0.17 | -0.08 | -0.02 | 5. |
| 10. | -0.55 | -0.39 | -0.30 | -0.24 | -0.16 | -0.11 | -0.03 | 10. |
| 15. | -0.55 | -0.43 | -0.36 | -0.25 | -0.19 | -0.14 | -0.04 | 15. |
| 20. | -0.27 | -0.34 | -0.33 | -0.21 | -0.18 | -0.16 | -0.05 | 20. |
| 25. | -0.01 | -0.15 | -0.2[illegible] | -0.11 | -0.13 | -0.15 | -0.04 | 25. |
| 30. | 0.29 | 0.10 | -0.01 | 0.02 | -0.04 | -0.12 | -0.05 | 30. |
| 35. | 0.56 | 0.39 | 0.10 | 0.18 | 0.08 | -0.07 | -0.04 | 35. |
| 40. | 0.82 | 0.69 | 0.27 | 0.32 | 0.20 | -0.02 | -0.02 | 40. |
| 45. | 1.04 | 0.93 | 0.42 | 0.43 | 0.27 | 0.01 | -0.01 | 45. |
| 50. | 1.14 | 1.00 | 0.53 | 0.50 | 0.31 | 0.01 | -0.01 | 50. |
| 55. | 1.13 | 0.99 | 0.55 | 0.53 | 0.32 | 0.03 | -0.01 | 55. |
| 60. | 1.02 | 0.93 | 0.50 | 0.54 | 0.33 | -0.01 | -0.03 | 60. |
| 65. | 0.84 | 0.85 | 0.43 | 0.53 | 0.33 | -0.03 | -0.03 | 65. |
| 70. | 0.63 | 0.75 | 0.35 | 0.51 | 0.32 | -0.03 | -0.03 | 70. |
| 75. | 0.43 | 0.63 | 0.26 | 0.49 | 0.30 | -0.05 | -0.03 | 75. |
| 80. | 0.27 | 0.50 | 0.18 | 0.47 | 0.27 | -0.09 | -0.03 | 80. |
| 85. | 0.16 | 0.44 | 0.18 | 0.45 | 0.24 | -0.11 | -0.03 | 85. |
| 90. | 0.15 | 0.46 | 0.18 | 0.42 | 0.23 | -0.12 | -0.04 | 90. |
| 95. | 0.16 | 0.44 | 0.18 | 0.40 | 0.22 | -0.11 | -0.05 | 95. |
| 100. | 0.13 | 0.40 | 0.15 | 0.37 | 0.22 | -0.10 | -0.05 | 100. |
| 105. | 0.06 | 0.32 | 0.10 | 0.34 | 0.21 | -0.10 | -0.05 | 105. |
| 110. | -0.04 | 0.22 | 0.11 | 0.35 | 0.15 | -0.12 | -0.06 | 110. |
| 115. | -0.21 | 0.08 | -0.13 | 0.24 | 0.10 | -0.14 | -0.06 | 115. |
| 120. | -0.35 | 0.29 | -0.20 | 0.17 | 0.06 | -0.15 | -0.06 | 120. |
| 125. | -0.45 | 0.19 | -0.24 | 0.12 | 0.04 | -0.15 | -0.06 | 125. |
| 130. | -0.47 | 0.09 | -0.26 | 0.09 | 0.04 | -0.14 | -0.04 | 130. |
| 135. | -0.43 | 0.07 | -0.25 | 0.09 | 0.04 | -0.12 | -0.03 | 135. |
| 140. | -0.36 | 0.10 | -0.23 | 0.10 | 0.05 | -0.09 | -0.02 | 140. |
| 145. | -0.23 | 0.15 | -0.14 | 0.13 | 0.07 | -0.05 | 0.00 | 145. |
| 150. | -0.06 | 0.17 | -0.05 | 0.17 | 0.12 | -0.02 | 0.02 | 150. |
| 155. | 0.13 | 0.19 | 0.06 | 0.22 | 0.18 | 0.02 | 0.03 | 155. |
| 160. | 0.30 | 0.21 | 0.18 | 0.26 | 0.25 | 0.04 | 0.04 | 160. |
| 165. | 0.45 | 0.23 | 0.29 | 0.29 | 0.29 | 0.08 | 0.04 | 165. |
| 170. | 0.57 | 0.26 | 0.37 | 0.31 | 0.30 | 0.11 | 0.05 | 170. |
| 175. | 0.64 | 0.27 | 0.43 | 0.30 | 0.28 | 0.13 | 0.05 | 175. |
| 180. | 0.65 | 0.26 | 0.45 | 0.28 | 0.21 | 0.13 | 0.05 | 180. |
| 185. | 0.62 | 0.21 | 0.42 | 0.24 | 0.17 | 0.13 | 0.05 | 185. |
| 190. | 0.55 | 0.16 | 0.36 | 0.19 | 0.13 | 0.13 | 0.05 | 190. |
| 195. | 0.44 | 0.11 | 0.30 | 0.14 | 0.09 | 0.12 | 0.04 | 195. |
| 200. | 0.31 | 0.06 | 0.23 | 0.09 | 0.05 | 0.11 | 0.04 | 200. |
| 205. | 0.20 | -0.01 | 0.16 | 0.02 | 0.01 | 0.10 | 0.04 | 205. |
| 210. | 0.09 | -0.13 | 0.10 | -0.06 | -0.02 | 0.09 | 0.04 | 210. |
| 215. | -0.01 | -0.24 | 0.04 | -0.17 | -0.05 | 0.09 | 0.04 | 215. |
| 220. | -0.11 | -0.30 | -0.01 | -0.15 | -0.08 | 0.08 | 0.04 | 220. |
| 225. | -0.20 | -0.33 | -0.05 | -0.17 | -0.10 | 0.08 | 0.04 | 225. |
| 230. | -0.27 | -0.37 | -0.08 | -0.22 | -0.12 | 0.07 | 0.04 | 230. |
| 235. | -0.31 | -0.41 | -0.10 | -0.28 | -0.14 | 0.07 | 0.04 | 235. |
| 240. | -0.34 | -0.44 | -0.11 | -0.33 | -0.16 | 0.07 | 0.03 | 240. |
| 245. | -0.36 | -0.46 | -0.12 | -0.35 | -0.18 | 0.07 | 0.02 | 245. |
| 250. | -0.37 | -0.46 | -0.13 | -0.36 | -0.20 | 0.07 | 0.02 | 250. |
| 255. | -0.37 | -0.46 | -0.14 | -0.35 | -0.22 | 0.07 | 0.02 | 255. |
| 260. | -0.37 | -0.45 | -0.14 | -0.34 | -0.23 | 0.06 | 0.01 | 260. |
| 265. | -0.38 | -0.44 | -0.14 | -0.32 | -0.23 | 0.06 | 0.01 | 265. |
| 270. | -0.38 | -0.45 | -0.14 | -0.31 | -0.24 | 0.06 | 0.00 | 270. |
| 275. | -0.39 | -0.45 | -0.16 | -0.31 | -0.24 | 0.05 | 0.00 | 275. |
| 280. | -0.41 | -0.46 | -0.17 | -0.33 | -0.24 | 0.05 | 0.01 | 280. |
| 285. | -0.44 | -0.49 | -0.18 | -0.36 | -0.23 | 0.05 | 0.01 | 285. |
| 290. | -0.45 | -0.51 | -0.18 | -0.38 | -0.23 | 0.05 | 0.01 | 290. |
| 295. | -0.43 | -0.51 | -0.17 | -0.38 | -0.22 | 0.05 | 0.02 | 295. |
| 300. | -0.40 | -0.48 | -0.16 | -0.35 | -0.20 | 0.06 | 0.03 | 300. |
| 305. | -0.38 | -0.45 | -0.16 | -0.34 | -0.19 | 0.06 | 0.04 | 305. |
| 310. | -0.35 | -0.45 | -0.14 | -0.32 | -0.18 | 0.07 | 0.04 | 310. |
| 315. | -0.34 | -0.47 | -0.17 | -0.32 | -0.18 | 0.06 | 0.03 | 315. |
| 320. | -0.34 | -0.50 | -0.20 | -0.33 | -0.19 | 0.05 | 0.03 | 320. |
| 325. | -0.35 | -0.52 | -0.23 | -0.33 | -0.21 | 0.04 | 0.02 | 325. |
| 330. | -0.39 | -0.53 | -0.25 | -0.35 | -0.22 | 0.02 | 0.00 | 330. |
| 335. | -0.41 | -0.52 | -0.28 | -0.37 | -0.25 | -0.01 | -0.01 | 335. |
| 340. | -0.37 | -0.48 | -0.27 | -0.36 | -0.25 | -0.01 | -0.01 | 340. |
| 345. | -0.25 | -0.41 | -0.22 | -0.31 | -0.19 | 0.00 | 0.00 | 345. |
| 350. | 0.19 | -0.03 | -0.09 | -0.19 | -0.09 | 0.02 | 0.00 | 350. |
| 355. | 0.27 | 0.01 | -0.09 | -0.15 | -0.04 | -0.03 | -0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CYCR NO. 188 TCN= 37. C.R.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.240 | 1.950 | 2.990 | 4.550 | 7.153 | 10.405 | DEG. |
| 0. | -0.09 | -0.02 | -0.09 | 0.01 | -0.02 | -0.03 | 0.00 | 0. |
| 5. | -0.39 | -0.21 | -0.25 | -0.01 | -0.04 | -0.07 | 0.00 | 5. |
| 10. | -0.21 | -0.10 | -0.20 | -0.00 | -0.06 | -0.08 | -0.00 | 10. |
| 15. | 0.03 | -0.05 | -0.12 | -0.00 | -0.10 | -0.09 | -0.01 | 15. |
| 20. | 0.27 | -0.04 | -0.11 | -0.04 | -0.10 | -0.09 | -0.01 | 20. |
| 25. | 0.43 | 0.04 | -0.06 | -0.01 | -0.06 | -0.07 | 0.01 | 25. |
| 30. | 0.60 | 0.27 | 0.12 | 0.09 | 0.04 | 0.01 | 0.03 | 30. |
| 35. | 0.90 | 0.51 | 0.35 | 0.21 | 0.19 | 0.07 | 0.05 | 35. |
| 40. | 1.19 | 0.70 | 0.55 | 0.30 | 0.29 | 0.12 | 0.06 | 40. |
| 45. | 1.33 | 0.79 | 0.66 | 0.36 | 0.32 | 0.14 | 0.05 | 45. |
| 50. | 1.34 | 0.79 | 0.72 | 0.37 | 0.33 | 0.14 | 0.05 | 50. |
| 55. | 1.29 | 0.69 | 0.73 | 0.37 | 0.30 | 0.12 | 0.05 | 55. |
| 60. | 1.15 | 0.53 | 0.64 | 0.33 | 0.23 | 0.08 | 0.04 | 60. |
| 65. | 0.89 | 0.32 | 0.54 | 0.25 | 0.14 | 0.03 | 0.02 | 65. |
| 70. | 0.61 | 0.07 | 0.34 | 0.16 | 0.07 | -0.02 | 0.01 | 70. |
| 75. | 0.34 | -0.15 | 0.18 | 0.07 | 0.01 | -0.05 | -0.00 | 75. |
| 80. | 0.10 | -0.31 | 0.02 | -0.01 | -0.10 | -0.08 | -0.01 | 80. |
| 85. | -0.13 | -0.47 | -0.13 | -0.09 | -0.19 | -0.10 | -0.00 | 85. |
| 90. | -0.33 | -0.63 | -0.25 | -0.16 | -0.23 | -0.12 | 0.00 | 90. |
| 95. | -0.48 | -0.76 | -0.37 | -0.24 | -0.28 | -0.14 | -0.00 | 95. |
| 100. | -0.57 | -0.87 | -0.50 | -0.34 | -0.33 | -0.16 | -0.03 | 100. |
| 105. | -0.89 | -1.05 | -0.72 | -0.44 | -0.41 | -0.18 | -0.04 | 105. |
| 110. | -1.36 | -1.24 | -0.91 | -0.52 | -0.48 | -0.19 | -0.04 | 110. |
| 115. | -1.23 | -1.36 | -1.04 | -0.59 | -0.51 | -0.20 | -0.05 | 115. |
| 120. | -1.35 | -1.43 | -1.11 | -0.62 | -0.53 | -0.21 | -0.05 | 120. |
| 125. | -1.42 | -1.46 | -1.14 | -0.63 | -0.55 | -0.21 | -0.05 | 125. |
| 130. | -1.43 | -1.44 | -1.13 | -0.63 | -0.54 | -0.20 | -0.05 | 130. |
| 135. | -1.39 | -1.35 | -1.08 | -0.62 | -0.54 | -0.17 | -0.05 | 135. |
| 140. | -1.38 | -1.23 | -0.98 | -0.58 | -0.49 | -0.14 | -0.05 | 140. |
| 145. | -1.16 | -1.07 | -0.87 | -0.52 | -0.42 | -0.11 | -0.04 | 145. |
| 150. | -0.98 | -0.89 | -0.74 | -0.44 | -0.34 | -0.09 | -0.03 | 150. |
| 155. | -0.77 | -0.69 | -0.59 | -0.36 | -0.25 | -0.05 | -0.02 | 155. |
| 160. | -0.55 | -0.50 | -0.44 | -0.28 | -0.17 | -0.01 | -0.01 | 160. |
| 165. | -0.35 | -0.32 | -0.29 | -0.22 | -0.09 | 0.02 | -0.00 | 165. |
| 170. | -0.17 | -0.15 | -0.17 | -0.16 | -0.03 | 0.03 | 0.00 | 170. |
| 175. | -0.05 | -0.00 | -0.08 | -0.11 | 0.02 | 0.05 | 0.00 | 175. |
| 180. | 0.03 | 0.10 | -0.02 | -0.07 | 0.06 | 0.06 | 0.00 | 180. |
| 185. | 0.07 | 0.16 | 0.02 | -0.03 | 0.08 | 0.06 | 0.00 | 185. |
| 190. | 0.07 | 0.20 | 0.06 | -0.01 | 0.09 | 0.06 | -0.00 | 190. |
| 195. | 0.07 | 0.21 | 0.09 | 0.00 | 0.09 | 0.05 | -0.00 | 195. |
| 200. | 0.05 | 0.22 | 0.10 | 0.01 | 0.08 | 0.04 | -0.01 | 200. |
| 205. | 0.01 | 0.22 | 0.10 | 0.02 | 0.08 | 0.03 | -0.01 | 205. |
| 210. | -0.06 | 0.21 | 0.10 | 0.02 | 0.07 | 0.03 | -0.01 | 210. |
| 215. | -0.12 | 0.19 | 0.10 | 0.02 | 0.07 | 0.02 | -0.01 | 215. |
| 220. | -0.16 | 0.18 | 0.10 | 0.03 | 0.07 | 0.02 | -0.01 | 220. |
| 225. | -0.18 | 0.18 | 0.12 | 0.03 | 0.07 | 0.03 | -0.01 | 225. |
| 230. | -0.17 | 0.19 | 0.14 | 0.03 | 0.07 | 0.03 | -0.01 | 230. |
| 235. | -0.14 | 0.21 | 0.15 | 0.05 | 0.08 | 0.04 | -0.00 | 235. |
| 240. | -0.09 | 0.24 | 0.20 | 0.07 | 0.09 | 0.05 | -0.00 | 240. |
| 245. | -0.04 | 0.30 | 0.. | 0.12 | 0.12 | 0.05 | 0.00 | 245. |
| 250. | 0.03 | 0.36 | 0.32 | 0.18 | 0.14 | 0.06 | 0.00 | 250. |
| 255. | 0.11 | 0.42 | 0.37 | 0.23 | 0.17 | 0.06 | 0.01 | 255. |
| 260. | 0.19 | 0.47 | 0.42 | 0.25 | 0.18 | 0.06 | 0.01 | 260. |
| 265. | 0.26 | 0.52 | 0.41 | 0.26 | 0.19 | 0.07 | 0.00 | 265. |
| 270. | 0.30 | 0.57 | 0.41 | 0.25 | 0.20 | 0.07 | 0.00 | 270. |
| 275. | 0.33 | 0.61 | 0.39 | 0.25 | 0.21 | 0.08 | 0.00 | 275. |
| 280. | 0.32 | 0.61 | 0.37 | 0.23 | 0.22 | 0.08 | 0.00 | 280. |
| 285. | 0.29 | 0.58 | 0.36 | 0.23 | 0.22 | 0.08 | 0.01 | 285. |
| 290. | 0.26 | 0.5 | 0.35 | 0.23 | 0.22 | 0.08 | 0.01 | 290. |
| 295. | 0.26 | 0.51 | 0.34 | 0.23 | 0.20 | 0.08 | 0.01 | 295. |
| 300. | 0.29 | 0.51 | 0.35 | 0.24 | 0.19 | 0.08 | 0.01 | 300. |
| 305. | 0.34 | 0.53 | 0.37 | 0.25 | 0.20 | 0.08 | 0.01 | 305. |
| 310. | 0.43 | 0.57 | 0.41 | 0.25 | 0.21 | 0.10 | 0.02 | 310. |
| 315. | 0.51 | 0.61 | 0.44 | 0.28 | 0.24 | 0.11 | 0.03 | 315. |
| 320. | 0.55 | 0.62 | 0.43 | 0.29 | 0.25 | 0.11 | 0.03 | 320. |
| 325. | 0.51 | 0.56 | 0.38 | 0.28 | 0.23 | 0.10 | 0.03 | 325. |
| 330. | 0.41 | 0.44 | 0.31 | 0.23 | 0.18 | 0.08 | 0.02 | 330. |
| 335. | 0.25 | 0.30 | 0.19 | 0.17 | 0.12 | 0.04 | 0.01 | 335. |
| 340. | 0.20 | 0.24 | 0.09 | 0.16 | 0.09 | 0.03 | 0.01 | 340. |
| 345. | 0.37 | 0.32 | 0.15 | 0.16 | 0.11 | 0.03 | 0.01 | 345. |
| 350. | 0.34 | 0.32 | 0.15 | 0.13 | 0.06 | -0.00 | 0.00 | 350. |
| 355. | 0.06 | 0.14 | -0.06 | 0.04 | -0.02 | -0.00 | 0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=502 CNTR NO. 188 TCN= 37. C.P.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.046 | 1.552 | 2.990 | 4.990 | 7.150 | 10.430 | DEG. |
| 0. | 0.08 | 0.36 | 0.09 | 0.11 | 0.12 | 0.01 | 0.01 | 0. |
| 5. | 0.42 | 0.16 | -0.04 | 0.01 | 0.11 | -0.04 | -0.01 | 5. |
| 10. | 0.08 | 0.01 | -0.09 | 0.00 | 0.16 | -0.07 | -0.01 | 10. |
| 15. | 0.06 | 0.12 | -0.01 | 0.02 | 0.21 | -0.06 | 0.00 | 15. |
| 20. | 0.29 | 0.18 | -0.04 | -0.01 | 0.24 | -0.09 | -0.00 | 20. |
| 25. | 0.52 | 0.35 | 0.07 | 0.00 | 0.33 | -0.09 | -0.04 | 25. |
| 30. | 0.74 | 0.65 | 0.31 | 0.27 | 0.45 | -0.03 | 0.01 | 30. |
| 35. | 0.96 | 0.90 | 0.57 | 0.41 | 0.54 | 0.05 | 0.02 | 35. |
| 40. | 1.15 | 1.01 | 0.75 | 0.51 | 0.53 | 0.09 | 0.04 | 40. |
| 45. | 1.27 | 1.03 | 0.88 | 0.57 | 0.50 | 0.09 | 0.03 | 45. |
| 50. | 1.29 | 1.02 | 1.06 | 0.61 | 0.59 | 0.06 | -0.00 | 50. |
| 55. | 1.20 | 0.92 | 1.30 | 0.59 | 0.67 | 0.02 | -0.01 | 55. |
| 60. | 1.02 | 0.74 | 1.60 | 0.49 | 0.66 | -0.03 | -0.01 | 60. |
| 65. | 0.69 | 0.49 | 1.68 | 0.34 | 0.58 | -0.09 | -0.05 | 65. |
| 70. | 0.26 | 0.19 | 1.48 | 0.16 | 0.42 | -0.15 | -0.08 | 70. |
| 75. | -0.14 | -0.12 | 1.15 | -0.02 | 0.25 | -0.20 | -0.10 | 75. |
| 80. | -0.47 | -0.42 | 0.75 | -0.17 | 0.11 | -0.25 | -0.10 | 80. |
| 85. | -0.76 | -0.71 | 0.27 | -0.32 | 0.13 | -0.33 | -0.11 | 85. |
| 90. | -1.01 | -0.92 | -0.21 | -0.47 | 0.00 | -0.33 | -0.10 | 90. |
| 95. | -1.25 | -1.10 | -0.60 | -0.62 | -0.01 | -0.34 | -0.09 | 95. |
| 100. | -1.52 | -1.28 | -0.88 | -0.79 | -0.11 | -0.33 | -0.11 | 100. |
| 105. | -1.77 | -1.47 | -1.15 | -0.93 | -0.20 | -0.34 | -0.11 | 105. |
| 110. | -1.90 | -1.61 | -1.27 | -1.01 | -0.27 | -0.35 | -0.10 | 110. |
| 115. | -2.15 | -1.71 | -1.38 | -1.07 | -0.31 | -0.35 | -0.10 | 115. |
| 120. | -2.24 | -1.77 | -1.43 | -1.09 | -0.33 | -0.36 | -0.10 | 120. |
| 125. | -2.26 | -1.78 | -1.43 | -1.09 | -0.33 | -0.35 | -0.10 | 125. |
| 130. | -2.23 | -1.74 | -1.43 | -1.05 | -0.31 | -0.34 | -0.09 | 130. |
| 135. | -2.14 | -1.63 | -1.39 | -0.98 | -0.29 | -0.30 | -0.07 | 135. |
| 140. | -2.00 | -1.48 | -1.28 | -0.90 | -0.27 | -0.26 | -0.07 | 140. |
| 145. | -1.81 | -1.32 | -1.12 | -0.79 | -0.25 | -0.21 | -0.06 | 145. |
| 150. | -1.59 | -1.15 | -0.95 | -0.67 | -0.22 | -0.17 | -0.06 | 150. |
| 155. | -1.33 | -0.89 | -0.79 | -0.54 | -0.20 | -0.12 | -0.04 | 155. |
| 160. | -1.35 | -0.58 | -0.65 | -0.41 | -0.18 | -0.08 | -0.02 | 160. |
| 165. | -0.79 | -0.35 | -0.51 | -0.28 | -0.14 | -0.04 | -0.01 | 165. |
| 170. | -0.54 | -0.20 | -0.38 | -0.17 | -0.12 | -0.01 | 0.02 | 170. |
| 175. | -0.34 | -0.09 | -0.27 | -0.10 | -0.13 | 0.01 | 0.01 | 175. |
| 180. | -0.19 | -0.02 | -0.20 | -0.06 | -0.13 | 0.04 | 0.01 | 180. |
| 185. | -0.08 | 0.03 | -0.14 | -0.02 | -0.10 | 0.05 | 0.02 | 185. |
| 190. | -0.01 | 0.06 | -0.11 | 0.01 | -0.02 | 0.07 | 0.02 | 190. |
| 195 | 0.03 | 0.07 | -0.09 | 0.03 | -0.02 | 0.07 | 0.01 | 195. |
| 200. | 0.04 | 0.06 | -0.09 | 0.04 | -0.00 | 0.08 | 0.01 | 200. |
| 205. | 0.04 | 0.05 | -0.10 | 0.0 | -0.12 | 0.08 | 0.01 | 205. |
| 210. | 0.03 | 0.04 | -0.09 | 0.05 | -0.15 | 0.08 | 0.01 | 210. |
| 215. | 0.02 | 0.03 | -0.09 | 0.06 | -0.18 | 0.08 | 0.02 | 215. |
| 220. | 0.01 | 0.03 | -0.08 | 0.05 | -0.20 | 0.09 | 0.02 | 220. |
| 225. | 0.01 | 0.05 | -0.07 | 0.10 | -0.21 | 0.11 | 0.03 | 225. |
| 230. | 0.04 | 0.09 | -0.05 | 0.13 | -0.22 | 0.12 | 0.04 | 230. |
| 235. | 0.09 | 0.16 | -0.03 | 0.16 | -0.21 | 0.13 | 0.04 | 235. |
| 240. | 0.15 | 0.23 | 0.00 | 0.20 | -0.21 | 0.14 | 0.04 | 240. |
| 245. | 0.20 | 0.28 | 0.04 | 0.23 | -0.19 | 0.14 | 0.04 | 245. |
| 250. | 0.40 | 0.34 | 0.08 | 0.27 | -0.18 | 0.16 | 0.04 | 250. |
| 255. | 0.54 | 0.41 | 0.13 | 0.31 | -0.17 | 0.17 | 0.04 | 255. |
| 260. | 0.67 | 0.51 | 0.19 | 0.36 | -0.16 | 0.18 | 0.05 | 260. |
| 265. | 0.79 | 0.60 | 0.25 | 0.41 | -0.14 | 0.20 | 0.04 | 265. |
| 270. | 0.88 | 0.66 | 0.33 | 0.44 | -0.12 | 0.20 | 0.04 | 270. |
| 275. | 0.95 | 0.68 | 0.38 | 0.46 | -0.11 | 0.21 | 0.04 | 275. |
| 280. | 0.98 | 0.68 | 0.39 | 0.46 | -0.10 | 0.21 | 0.05 | 280. |
| 285. | 0.96 | 0.67 | 0.39 | 0.45 | -0.09 | 0.22 | 0.05 | 285. |
| 290. | 0.88 | 0.65 | 0.36 | 0.43 | -0.08 | 0.21 | 0.05 | 290. |
| 295. | 0.84 | 0.63 | 0.33 | 0.40 | -0.08 | 0.20 | 0.04 | 295. |
| 300. | 0.84 | 0.63 | 0.33 | 0.39 | -0.09 | 0.19 | 0.04 | 300. |
| 305. | 0.88 | 0.66 | 0.35 | 0.41 | -0.09 | 0.20 | 0.04 | 305. |
| 310. | 0.97 | 0.76 | 0.38 | 0.45 | -0.09 | 0.21 | 0.04 | 310. |
| 315. | 1.13 | 0.85 | 0.44 | 0.49 | -0.01 | 0.23 | 0.04 | 315. |
| 320. | 1.24 | 0.88 | 0.48 | 0.51 | 0.03 | 0.23 | 0.04 | 320. |
| 325. | 1.22 | 0.83 | 0.44 | 0.50 | 0.05 | 0.22 | 0.04 | 325. |
| 330. | 1.04 | 0.72 | 0.36 | 0.42 | 0.04 | 0.20 | 0.07 | 330. |
| 335. | 0.84 | 0.54 | 0.27 | 0.33 | 0.03 | 0.16 | 0.04 | 335. |
| 340. | 0.83 | 0.56 | 0.27 | 0.31 | 0.00 | 0.15 | 0.04 | 340. |
| 345. | 0.77 | 0.49 | 0.25 | 0.29 | 0.00 | 0.13 | 0.04 | 345. |
| 350. | 0.49 | 0.23 | 0.07 | 0.18 | 0.05 | 0.10 | 0.05 | 350. |
| 355. | 0.27 | 0.07 | -0.04 | 0.04 | 0.04 | 0.04 | 0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-502 CNTR NO. 188 TCN= 37. C.R.= 45.1

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.493 | 1.046 | 1.952 | 2.990 | 4.952 | 7.159 | 10.400 | DEG. |
| 0. | 0.83 | 0.50 | 0.01 | -0.02 | 0.04 | -0.01 | -0.04 | 0. |
| 5. | 0.58 | 0.46 | 0.04 | -0.05 | 0.04 | -0.03 | -0.05 | 5. |
| 10. | 0.17 | 0.25 | -0.25 | -0.17 | 0.01 | -0.03 | -0.07 | 10. |
| 15. | 0.15 | 0.19 | -0.25 | -0.21 | -0.01 | -0.04 | -0.06 | 15. |
| 20. | 0.40 | 0.32 | -0.16 | -0.17 | 0.02 | -0.10 | -0.08 | 20. |
| 25. | 0.48 | 0.52 | 0.03 | -0.06 | 0.08 | -0.09 | -0.10 | 25. |
| 30. | 0.91 | 0.73 | 0.31 | 0.12 | 0.19 | -0.05 | -0.07 | 30. |
| 35. | 1.07 | 0.90 | 0.44 | 0.28 | 0.27 | -0.04 | -0.06 | 35. |
| 40. | 1.17 | 1.01 | 0.80 | 0.38 | 0.34 | -0.04 | -0.06 | 40. |
| 45. | 1.25 | 1.10 | 1.52 | 0.42 | 0.37 | -0.06 | -0.07 | 45. |
| 50. | 1.26 | 1.14 | 2.12 | 0.44 | 0.35 | -0.10 | -0.10 | 50. |
| 55. | 1.12 | 1.09 | 2.22 | 0.44 | 0.29 | -0.17 | -0.11 | 55. |
| 60. | 0.77 | 0.87 | 1.98 | 0.60 | 0.20 | -0.24 | -0.09 | 60. |
| 65. | 0.34 | 0.58 | 1.68 | 0.90 | 0.09 | -0.29 | -0.10 | 65. |
| 70. | -0.13 | 0.26 | 1.35 | 1.05 | -0.01 | -0.34 | -0.13 | 70. |
| 75. | -0.56 | -0.09 | 1.02 | 0.93 | -0.10 | -0.39 | -0.15 | 75. |
| 80. | -0.95 | -0.43 | 0.70 | 0.78 | -0.16 | -0.41 | -0.14 | 80. |
| 85. | -1.29 | -0.75 | 0.41 | 0.61 | -0.19 | -0.41 | -0.12 | 85. |
| 90. | -1.60 | -1.05 | 0.18 | 0.41 | -0.18 | -0.40 | -0.09 | 90. |
| 95. | -1.90 | -1.31 | 0.01 | -0.12 | -0.19 | -0.40 | -0.10 | 95. |
| 100. | -2.19 | -1.54 | -0.18 | -0.72 | -0.23 | -0.39 | -0.12 | 100. |
| 105. | -2.44 | -1.72 | -0.61 | -0.98 | -0.27 | -0.40 | -0.11 | 105. |
| 110. | -2.64 | -1.85 | -1.27 | -0.96 | -0.32 | -0.40 | -0.07 | 110. |
| 115. | -2.75 | -1.93 | -1.70 | -0.98 | -0.36 | -0.42 | -0.06 | 115. |
| 120. | -2.79 | -1.96 | -1.72 | -1.02 | -0.39 | -0.43 | -0.05 | 120. |
| 125. | -2.80 | -1.94 | -1.69 | -1.05 | -0.41 | -0.42 | -0.03 | 125. |
| 130. | -2.76 | -1.87 | -1.61 | -1.04 | -0.41 | -0.39 | -0.02 | 130. |
| 135. | -2.63 | -1.76 | -1.52 | -1.00 | -0.40 | -0.36 | -0.05 | 135. |
| 140. | -2.41 | -1.61 | -1.47 | -0.92 | -0.38 | -0.32 | -0.06 | 140. |
| 145. | -2.16 | -1.44 | -1.30 | -0.83 | -0.35 | -0.27 | -0.06 | 145. |
| 150. | -1.90 | -1.27 | -1.17 | -0.74 | -0.31 | -0.22 | -0.04 | 150. |
| 155. | -1.62 | -1.08 | -1.04 | -0.64 | -0.26 | -0.17 | -0.02 | 155. |
| 160. | -1.35 | -0.90 | -0.88 | -0.53 | -0.20 | -0.11 | -0.01 | 160. |
| 165. | -1.07 | -0.68 | -0.72 | -0.40 | -0.13 | -0.06 | 0.01 | 165. |
| 170. | -0.78 | -0.49 | -0.58 | -0.29 | -0.08 | -0.01 | 0.03 | 170. |
| 175. | -0.53 | -0.35 | -0.47 | -0.23 | -0.04 | 0.04 | 0.04 | 175. |
| 180. | -0.33 | -0.23 | -0.38 | -0.18 | -0.05 | 0.08 | 0.06 | 180. |
| 185. | -0.19 | -0.16 | -0.31 | -0.15 | -0.05 | 0.12 | 0.06 | 185. |
| 190. | -0.12 | -0.11 | -0.26 | -0.12 | -0.03 | 0.13 | 0.06 | 190. |
| 195. | -0.07 | -0.08 | -0.24 | -0.10 | -0.02 | 0.14 | 0.06 | 195. |
| 200. | -0.05 | -0.06 | -0.24 | -0.09 | -0.01 | 0.15 | 0.06 | 200. |
| 205. | -0.04 | -0.04 | -0.24 | -0.07 | -0.01 | 0.15 | 0.06 | 205. |
| 210. | -0.03 | -0.03 | -0.23 | -0.06 | -0.02 | 0.15 | 0.06 | 210. |
| 215. | -0.02 | -0.03 | -0.21 | -0.06 | -0.03 | 0.17 | 0.06 | 215. |
| 220. | 0.01 | -0.01 | -0.19 | -0.05 | -0.03 | 0.18 | 0.07 | 220. |
| 225. | 0.04 | 0.01 | -0.14 | -0.03 | -0.02 | 0.23 | 0.07 | 225. |
| 230. | 0.11 | 0.03 | -0.12 | 0.01 | 0.05 | 0.21 | 0.08 | 230. |
| 235. | 0.21 | 0.08 | -0.08 | 0.06 | 0.03 | 0.23 | 0.10 | 235. |
| 240. | 0.33 | 0.14 | -0.02 | 0.11 | 0.09 | 0.24 | 0.11 | 240. |
| 245. | 0.46 | 0.24 | 0.02 | 0.15 | 0.07 | 0.26 | 0.10 | 245. |
| 250. | 0.62 | 0.36 | 0.08 | 0.19 | 0.09 | 0.27 | 0.10 | 250. |
| 255. | 0.78 | 0.48 | 0.14 | 0.23 | 0.10 | 0.29 | 0.10 | 255. |
| 260. | 0.94 | 0.60 | 0.21 | 0.27 | 0.11 | 0.31 | 0.10 | 260. |
| 265. | 1.11 | 0.71 | 0.27 | 0.31 | 0.13 | 0.32 | 0.10 | 265. |
| 270. | 1.26 | 0.80 | 0.33 | 0.35 | 0.15 | 0.32 | 0.10 | 270. |
| 275. | 1.37 | 0.85 | 0.39 | 0.38 | 0.... | 0.31 | 0.09 | 275. |
| 280. | 1.43 | 0.86 | 0.42 | 0.38 | 0.16 | 0.30 | 0.08 | 280. |
| 285. | 1.38 | 0.82 | 0.40 | 0.36 | 0.17 | 0.29 | 0.08 | 285. |
| 290. | 1.27 | 0.76 | 0.34 | 0.32 | 0.15 | 0.26 | 0.07 | 290. |
| 295. | 1.19 | 0.72 | 0.35 | 0.28 | 0.12 | 0.26 | 0.07 | 295. |
| 300. | 1.17 | 0.71 | 0.28 | 0.24 | 0.13 | 0.27 | 0.07 | 300. |
| 305. | 1.24 | 0.76 | 0.32 | 0.29 | 0.15 | 0.28 | 0.07 | 305. |
| 310. | 1.37 | 0.85 | 0.38 | 0.35 | 0.17 | 0.29 | 0.07 | 310. |
| 315. | 1.52 | 0.96 | 0.44 | 0.40 | 0.19 | 0.29 | 0.07 | 315. |
| 320. | 1.66 | 1.07 | 0.48 | 0.43 | 0.21 | 0.29 | 0.07 | 320. |
| 325. | 1.67 | 1.05 | 0.46 | 0.41 | 0.21 | 0.28 | 0.06 | 325. |
| 330. | 1.54 | 0.92 | 0.39 | 0.35 | 0.20 | 0.26 | 0.04 | 330. |
| 335. | 1.49 | 0.87 | 0.34 | 0.28 | 0.18 | 0.23 | 0.03 | 335. |
| 340. | 1.51 | 0.88 | 0.29 | 0.27 | 0.18 | 0.19 | 0.02 | 340. |
| 345. | 1.46 | 0.74 | 0.26 | 0.22 | 0.16 | 0.15 | 0.02 | 345. |
| 350. | 1.23 | 0.39 | 0.01 | 0.05 | 0.09 | 0.09 | 0.01 | 350. |
| 355. | 1.19 | 0.17 | -0.11 | -0.05 | -0.01 | -0.05 | -0.03 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 226 TCH= 39. C.R.= 8.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ DEG. | CHORD STATION 0.455 | 1.950 | 4.550 | 10.400 | AZ DEG. |
|---|---|---|---|---|---|
| 0. | -0.92 | -0.46 | -0.33 | 0.02 | 0. |
| 5. | -0.90 | -0.45 | -0.23 | 0.01 | 5. |
| 10. | -0.80 | -0.31 | -0.13 | 0.03 | 10. |
| 15. | -0.81 | -0.15 | -0.07 | 0.07 | 15. |
| 20. | -0.74 | -0.09 | -0.06 | 0.09 | 20. |
| 25. | -0.56 | -0.12 | -0.10 | 0.07 | 25. |
| 30. | -0.84 | -0.27 | -0.16 | 0.02 | 30. |
| 35. | -0.85 | -0.41 | -0.22 | -0.01 | 35. |
| 40. | -0.97 | -0.46 | -0.23 | -0.00 | 40. |
| 45. | -0.69 | -0.43 | -0.15 | 0.03 | 45. |
| 50. | -0.42 | -0.23 | -0.06 | 0.04 | 50. |
| 55. | -0.20 | -0.12 | 0.01 | 0.07 | 55. |
| 60. | -0.07 | -0.05 | 0.04 | 0.04 | 60. |
| 65. | -0.04 | -0.03 | 0.04 | 0.05 | 65. |
| 70. | -0.06 | -0.06 | 0.02 | -0.01 | 70. |
| 75. | -0.09 | -0.11 | -0.01 | -0.01 | 75. |
| 80. | -0.12 | -0.15 | -0.04 | -0.01 | 80. |
| 85. | -0.13 | -0.15 | -0.03 | -0.01 | 85. |
| 90. | -0.10 | -0.11 | 0.03 | -0.00 | 90. |
| 95. | 0.17 | -0.03 | 0.08 | 0.01 | 95. |
| 100. | 0.47 | 0.08 | 0.13 | 0.02 | 100. |
| 105. | 0.64 | 0.20 | 0.20 | 0.04 | 105. |
| 110. | 0.82 | 0.33 | 0.28 | 0.06 | 110. |
| 115. | 1.01 | 0.46 | 0.36 | 0.06 | 115. |
| 120. | 1.22 | 0.58 | 0.43 | 0.07 | 120. |
| 125. | 1.42 | 0.68 | 0.48 | 0.08 | 125. |
| 130. | 1.53 | 0.76 | 0.51 | 0.09 | 130. |
| 135. | 1.61 | 0.81 | 0.52 | 0.09 | 135. |
| 140. | 1.7. | 0.84 | 0.52 | 0.09 | 140. |
| 145. | 1.78 | 0.86 | 0.51 | 0.08 | 145. |
| 150. | 1.83 | 0.86 | 0.50 | 0.08 | 150. |
| 155. | 1.77 | 0.85 | 0.47 | 0.08 | 155. |
| 160. | 1.67 | 0.82 | 0.45 | 0.07 | 160. |
| 165. | 1.58 | 0.77 | 0.41 | 0.05 | 165. |
| 170. | 1.48 | 0.70 | 0.37 | 0.04 | 170. |
| 175. | 1.33 | 0.61 | 0.32 | 0.03 | 175. |
| 180. | 1.13 | 0.52 | 0.25 | 0.03 | 180. |
| 185. | 0.84 | 0.37 | 0.18 | 0.02 | 185. |
| 190. | 0.46 | 0.17 | 0.09 | 0.01 | 190. |
| 195. | 0.13 | -0.02 | -0.01 | 0.00 | 195. |
| 200. | -0.12 | -0.19 | -0.11 | -0.00 | 200. |
| 205. | -0.31 | -0.26 | -0.18 | -0.02 | 205. |
| 210. | -0.51 | -0.26 | -0.23 | -0.00 | 210. |
| 215. | -0.51 | -0.26 | -0.26 | -0.02 | 215. |
| 220. | -0.45 | -0.27 | -0.26 | -0.05 | 220. |
| 225. | -0.45 | -0.28 | -0.26 | -0.07 | 225. |
| 230. | -0.45 | -0.29 | -0.26 | -0.07 | 230. |
| 235. | -0.45 | -0.27 | -0.25 | -0.06 | 235. |
| 240. | -0.45 | -0.25 | -0.24 | -0.06 | 240. |
| 245. | -0.45 | -0.22 | -0.23 | -0.06 | 245. |
| 250. | -0.45 | -0.21 | -0.21 | -0.08 | 250. |
| 255. | -0.45 | -0.20 | -0.20 | -0.10 | 255. |
| 260. | -0.45 | -0.19 | -0.19 | -0.10 | 260. |
| 265. | -0.45 | -0.19 | -0.19 | -0.12 | 265. |
| 270. | -0.45 | -0.18 | -0.18 | -0.10 | 270. |
| 275. | -0.44 | -0.18 | -0.17 | -0.09 | 275. |
| 280. | -0.44 | -0.17 | -0.16 | -0.09 | 280. |
| 285. | -0.44 | -0.16 | -0.15 | -0.09 | 285. |
| 290. | -0.47 | -0.16 | -0.14 | -0.10 | 290. |
| 295. | -0.47 | -0.16 | -0.13 | -0.12 | 295. |
| 300. | -0.47 | -0.16 | -0.12 | -0.12 | 300. |
| 305. | -0.48 | -0.16 | -0.10 | -0.12 | 305. |
| 310. | -0.48 | -0.17 | -0.09 | -0.10 | 310. |
| 315. | -0.49 | -0.19 | -0.07 | -0.07 | 315. |
| 320. | -0.49 | -0.21 | -0.06 | -0.04 | 320. |
| 325. | -0.48 | -0.22 | -0.05 | -0.01 | 325. |
| 330. | -0.46 | -0.19 | -0.03 | 0.01 | 330. |
| 335. | -0.44 | -0.12 | -0.03 | 0.04 | 335. |
| 340. | -0.56 | -0.15 | -0.07 | 0.06 | 340. |
| 345. | -0.69 | -0.20 | -0.13 | 0.08 | 345. |
| 350. | -0.75 | -0.42 | -0.25 | 0.04 | 350. |
| 355. | -0.78 | -0.58 | -0.32 | 0.02 | 355. |

## DIFFERENTIAL PRFSSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 226 TCN= 39. C.A.= 8.7

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.990 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -1.30 | -0.43 | -0.02 | -0.41 | -0.30 | -0.13 | 0.01 | 0. |
| 5. | -1.65 | 1.13 | -1.00 | -0.68 | -0.43 | -0.16 | -0.00 | 5. |
| 10. | -1.11 | -1.58 | -0.98 | -0.60 | -0.47 | -0.14 | -0.00 | 10. |
| 15. | -0.59 | -1.06 | -0.68 | -0.42 | -0.39 | -0.08 | 0.05 | 15. |
| 20. | -0.47 | -0.85 | -0.29 | -0.23 | -0.24 | -0.04 | 0.08 | 20. |
| 25. | -0.96 | -0.43 | -0.44 | -0.45 | -0.21 | -0.12 | 0.04 | 25. |
| 30. | -1.49 | -0.97 | -0.86 | -0.49 | -0.33 | -0.17 | -0.01 | 30. |
| 35. | -1.34 | -1.12 | -0.72 | -0.38 | -0.32 | -0.17 | -0.02 | 35. |
| 40. | -0.94 | -0.86 | -0.53 | -0.25 | -0.21 | -0.14 | -0.02 | 40. |
| 45. | -0.58 | -0.60 | -0.41 | -0.19 | -0.11 | -0.11 | -0.01 | 45. |
| 50. | -0.33 | -0.44 | -0.36 | -0.15 | -0.08 | -0.11 | 0.00 | 50. |
| 55. | -0.18 | -0.31 | -0.33 | -0.13 | -0.09 | -0.12 | -0.01 | 55. |
| 60. | -0.11 | -0.24 | -0.31 | -0.13 | -0.08 | -0.13 | -0.02 | 60. |
| 65. | -0.09 | -0.21 | -0.30 | -0.14 | -0.08 | -0.17 | -0.05 | 65. |
| 70. | -0.09 | -0.19 | -0.30 | -0.14 | -0.08 | -0.18 | -0.06 | 70. |
| 75. | -0.11 | -0.19 | -0.30 | -0.11 | -0.07 | -0.18 | -0.05 | 75. |
| 80. | -0.13 | -0.20 | -0.28 | -0.09 | -0.03 | -0.17 | -0.03 | 80. |
| 85. | -0.11 | -0.19 | -0.24 | -0.05 | 0.03 | -0.14 | -0.01 | 85. |
| 90. | -0.03 | -0.14 | -0.16 | -0.00 | 0.15 | -0.12 | -0.01 | 90. |
| 95. | 0.12 | -0.04 | -0.04 | 0.07 | 0.17 | -0.10 | 0.00 | 95. |
| 100. | 0.33 | 0.11 | 0.03 | 0.19 | 0.23 | -0.06 | 0.02 | 100. |
| 105. | 0.61 | 0.30 | 0.18 | 0.33 | 0.30 | 0.01 | 0.03 | 105. |
| 110. | 0.92 | 0.52 | 0.42 | 0.45 | 0.39 | 0.06 | 0.05 | 110. |
| 115. | 1.23 | 0.76 | 0.60 | 0.55 | 0.44 | 0.11 | 0.07 | 115. |
| 120. | 1.51 | 1.01 | 0.77 | 0.62 | 0.50 | 0.17 | 0.09 | 120. |
| 125. | 1.77 | 1.23 | 0.93 | 0.67 | 0.65 | 0.21 | 0.12 | 125. |
| 130. | 1.97 | 1.41 | 1.08 | 0.76 | 0.70 | 0.24 | 0.13 | 130. |
| 135. | 2.09 | 1.53 | 1.17 | 0.73 | 0.71 | 0.26 | 0.12 | 135. |
| 140. | 2.12 | 1.60 | 1.13 | 0.74 | 0.70 | 0.25 | 0.11 | 140. |
| 145. | 2.12 | 1.63 | 1.10 | 0.73 | 0.67 | 0.24 | 0.11 | 145. |
| 150. | 2.09 | 1.62 | 1.09 | 0.71 | 0.63 | 0.23 | 0.11 | 150. |
| 155. | 2.05 | 1.59 | 1.07 | 0.69 | 0.58 | 0.22 | 0.11 | 155. |
| 160. | 2.08 | 1.56 | 1.09 | 0.71 | 0.53 | 0.23 | 0.12 | 160. |
| 165. | 2.16 | 1.59 | 1.14 | 0.74 | 0.53 | 0.25 | 0.13 | 165. |
| 170. | 2.30 | 1.62 | 1.19 | 0.77 | 0.56 | 0.28 | 0.14 | 170. |
| 175. | 2.29 | 1.65 | 1.21 | 0.78 | 0.56 | 0.31 | 0.15 | 175. |
| 180. | 2.11 | 1.61 | 1.16 | 0.73 | 0.53 | 0.31 | 0.14 | 180. |
| 185. | 1.80 | 1.47 | 1.03 | 0.64 | 0.47 | 0.29 | 0.12 | 185. |
| 190. | 1.39 | 1.19 | 0.82 | 0.50 | 0.37 | 0.25 | 0.09 | 190. |
| 195. | 0.90 | 0.83 | 0.53 | 0.29 | 0.24 | 0.19 | 0.07 | 195. |
| 200. | 0.37 | 0.52 | 0.27 | 0.08 | 0.10 | 0.11 | 0.04 | 200. |
| 205. | -0.04 | 0.30 | 0.08 | -0.04 | -0.00 | 0.04 | 0.02 | 205. |
| 210. | -0.31 | 0.12 | -0.08 | -0.11 | -0.08 | 0.01 | 0.00 | 210. |
| 215. | -0.48 | -0.05 | -0.20 | -0.16 | -0.14 | -0.02 | -0.01 | 215. |
| 220. | -0.59 | -0.23 | -0.28 | -0.20 | -0.19 | -0.04 | -0.03 | 220. |
| 225. | -0.66 | -0.37 | -0.31 | -0.24 | -0.23 | -0.06 | -0.05 | 225. |
| 230. | -0.73 | -0.47 | -0.32 | -0.27 | -0.26 | -0.08 | -0.05 | 230. |
| 235. | -0.80 | -0.54 | -0.34 | -0.29 | -0.29 | -0.09 | -0.06 | 235. |
| 240. | -0.84 | -0.57 | -0.34 | -0.30 | -0.30 | -0.09 | -0.07 | 240. |
| 245. | -0.85 | -0.57 | -0.34 | -0.29 | -0.31 | -0.10 | -0.09 | 245. |
| 250. | -0.85 | -0.57 | -0.33 | -0.29 | -0.32 | -0.09 | -0.10 | 250. |
| 255. | -0.83 | -0.57 | -0.31 | -0.29 | -0.32 | -0.09 | -0.10 | 255. |
| 260. | -0.81 | -0.56 | -0.30 | -0.30 | -0.31 | -0.09 | -0.11 | 260. |
| 265. | -0.81 | -0.55 | -0.29 | -0.28 | -0.30 | -0.09 | -0.11 | 265. |
| 270. | -0.81 | -0.54 | -0.28 | -0.26 | -0.28 | -0.08 | -0.11 | 270. |
| 275. | -0.81 | -0.52 | -0.27 | -0.25 | -0.26 | -0.07 | -0.10 | 275. |
| 280. | -0.81 | -0.51 | -0.27 | -0.25 | -0.25 | -0.07 | -0.10 | 280. |
| 285. | -0.81 | -0.51 | -0.28 | -0.25 | -0.26 | -0.07 | -0.10 | 285. |
| 290. | -0.81 | -0.51 | -0.28 | -0.25 | -0.27 | -0.07 | -0.09 | 290. |
| 295. | -0.82 | -0.51 | -0.29 | -0.25 | -0.28 | -0.05 | -0.08 | 295. |
| 300. | -0.82 | -0.51 | -0.29 | -0.25 | -0.28 | -0.03 | -0.15 | 300. |
| 305. | -0.83 | -0.52 | -0.29 | -0.25 | -0.26 | -0.03 | -0.11 | 305. |
| 310. | -0.83 | -0.51 | -0.29 | -0.24 | -0.25 | -0.02 | -0.11 | 310. |
| 315. | -0.83 | -0.49 | -0.28 | -0.24 | -0.23 | -0.01 | -0.10 | 315. |
| 320. | -0.82 | -0.48 | -0.26 | -0.23 | -0.22 | 0.01 | -0.08 | 320. |
| 325. | -0.80 | -0.46 | -0.26 | -0.22 | -0.21 | 0.02 | -0.04 | 325. |
| 330. | -0.78 | -0.46 | -0.26 | -0.21 | -0.19 | 0.02 | -0.01 | 330. |
| 335. | -0.81 | -0.50 | -0.28 | -0.21 | -0.17 | 0.01 | 0.03 | 335. |
| 340. | -0.87 | -0.59 | -0.31 | -0.23 | -0.19 | -0.02 | -0.00 | 340. |
| 345. | -0.94 | -0.68 | -0.42 | -0.28 | -0.24 | -0.06 | -0.03 | 345. |
| 350. | -0.96 | -0.94 | -0.25 | -0.22 | -0.24 | -0.06 | -0.03 | 350. |
| 355. | -1.39 | -0.25 | -0.21 | -0.18 | -0.18 | -0.09 | -0.0. | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 226 TCN= 39. C.R.= 8.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.360 | 1.950 | 2.990 | 4.550 | 7.159 | 10.430 | DEG. |
| 0. | -1.68 | -0.92 | -0.72 | -0.44 | -0.43 | -0.09 | -0.04 | 0. |
| 5. | -1.83 | -1.25 | -0.80 | -0.59 | -0.48 | -0.17 | -0.04 | 5. |
| 10. | -2.02 | -1.42 | -1.01 | -0.72 | -0.52 | -0.23 | -0.07 | 10. |
| 15. | -1.92 | -1.39 | -0.96 | -0.69 | -0.44 | -0.29 | -0.12 | 15. |
| 20. | -1.40 | -1.42 | -0.69 | -0.95 | -0.28 | -0.32 | -0.16 | 20. |
| 25. | -0.68 | -1.01 | -0.66 | -0.34 | -0.11 | -0.26 | -0.13 | 25. |
| 30. | -0.20 | -0.59 | 0.12 | -0.37 | 0.08 | -0.17 | -0.11 | 30. |
| 35. | 0.07 | -0.30 | 0.36 | 0.02 | 0.20 | -0.14 | -0.11 | 35. |
| 40. | 0.27 | -0.10 | 0.04 | 0.02 | 0.31 | -0.11 | -0.10 | 40. |
| 45. | 0.64 | 0.04 | 0.11 | 0.09 | 0.44 | -0.09 | -0.09 | 45. |
| 50. | 0.97 | 0.17 | 0.21 | 0.15 | 0.49 | -0.08 | -0.09 | 50. |
| 55. | 1.16 | 0.36 | 0.30 | 0.19 | 0.42 | -0.08 | -0.12 | 55. |
| 60. | 1.23 | 0.44 | 0.31 | 0.20 | 0.33 | -0.10 | -0.16 | 60. |
| 65. | 1.20 | 0.44 | 0.24 | 0.19 | 0.37 | -0.11 | -0.14 | 65. |
| 70. | 1.12 | 0.39 | 0.15 | 0.14 | 0.45 | -0.11 | -0.12 | 70. |
| 75. | 0.99 | 0.22 | 0.04 | 0.05 | 0.40 | -0.15 | -0.13 | 75. |
| 80. | 0.74 | 0.08 | -0.10 | -0.07 | 0.31 | -0.18 | -0.14 | 80. |
| 85. | 0.54 | -0.07 | -0.21 | -0.14 | 0.24 | -0.19 | -0.14 | 85. |
| 90. | 0.56 | -0.11 | -0.22 | -0.11 | 0.28 | -0.17 | -0.11 | 90. |
| 95. | 0.82 | 0.02 | -0.04 | -0.01 | 0.34 | -0.13 | -0.09 | 95. |
| 100. | 1.19 | 0.24 | 0.16 | 0.13 | 0.41 | -0.09 | -0.07 | 100. |
| 105. | 1.51 | 0.50 | 0.32 | 0.29 | 0.48 | -0.04 | -0.06 | 105. |
| 110. | 1.82 | 0.81 | 0.44 | 0.42 | 0.53 | -0.03 | -0.04 | 110. |
| 115. | 2.01 | 1.09 | 0.59 | 0.47 | 0.54 | 0.02 | -0.03 | 115. |
| 120. | 1.93 | 1.28 | 0.69 | 0.41 | 0.49 | 0.02 | -0.02 | 120. |
| 125. | 1.49 | 1.19 | 0.37 | 0.23 | 0.38 | 0.00 | -0.03 | 125. |
| 130. | 0.86 | 0.76 | 0.04 | 0.05 | 0.25 | -0.01 | -0.02 | 130. |
| 135. | 0.46 | 0.28 | -0.11 | -0.01 | 0.19 | -0.01 | -0.00 | 135. |
| 140. | 0.53 | 0.12 | -0.09 | 0.00 | 0.16 | -0.01 | 0.01 | 140. |
| 145. | 0.55 | 0.28 | 0.64 | 0.05 | 0.14 | -0.00 | 0.01 | 145. |
| 150. | 0.60 | 0.29 | 0.14 | 0.10 | 0.14 | 0.01 | 0.02 | 150. |
| 155. | 0.69 | 0.35 | 0.24 | 0.16 | 0.16 | 0.04 | 0.03 | 155. |
| 160. | 0.84 | 0.50 | 0.35 | 0.24 | 0.20 | 0.08 | 0.05 | 160. |
| 165. | 1.02 | 0.71 | 0.48 | 0.33 | 0.25 | 0.13 | 0.07 | 165. |
| 170. | 1.24 | 0.90 | 0.62 | 0.44 | 0.30 | 0.19 | 0.09 | 170. |
| 175. | 1.40 | 1.07 | 0.76 | 0.54 | 0.34 | 0.23 | 0.12 | 175. |
| 180. | 1.41 | 1.20 | 0.82 | 0.58 | 0.36 | 0.27 | 0.15 | 180. |
| 185. | 1.28 | 1.24 | 0.80 | 0.57 | 0.35 | 0.30 | 0.16 | 185. |
| 190. | 1.05 | 1.16 | 0.71 | 0.51 | 0.24 | 0.29 | 0.16 | 190. |
| 195. | 0.77 | 1.00 | 0.60 | 0.42 | 0.16 | 0.27 | 0.15 | 195. |
| 200. | 0.49 | 0.80 | 0.46 | 0.33 | 0.08 | 0.23 | 0.13 | 200. |
| 205. | 0.25 | 0.58 | 0.34 | 0.24 | 0.01 | 0.19 | 0.11 | 205. |
| 210. | 0.03 | 0.36 | 0.25 | 0.16 | -0.06 | 0.14 | 0.09 | 210. |
| 215. | -0.16 | 0.20 | 0.15 | 0.09 | -0.12 | 0.10 | 0.08 | 215. |
| 220. | -0.32 | 0.06 | 0.06 | 0.04 | -0.17 | 0.06 | 0.06 | 220. |
| 225. | -0.45 | -0.05 | -0.05 | -0.00 | -0.21 | 0.03 | 0.04 | 225. |
| 230. | -0.56 | -0.14 | -0.09 | -0.04 | -0.23 | 0.01 | 0.02 | 230. |
| 235. | -0.66 | -0.22 | -0.12 | -0.09 | -0.24 | 0.00 | 0.01 | 235. |
| 240. | -0.76 | -0.28 | -0.16 | -0.12 | -0.20 | -0.01 | 0.00 | 240. |
| 245. | -0.84 | -0.33 | -0.20 | -0.15 | -0.31 | -0.03 | 0.05 | 245. |
| 250. | -0.91 | -0.37 | -0.24 | -0.17 | -0.33 | 0.00 | 0.04 | 250. |
| 255. | -0.96 | -0.40 | -0.27 | -0.19 | -0.35 | 0.01 | 0.04 | 255. |
| 260. | -0.98 | -0.41 | -0.28 | -0.21 | -0.36 | 0.01 | 0.04 | 260. |
| 265. | -0.99 | -0.42 | -0.28 | -0.22 | -0.37 | 0.02 | 0.04 | 265. |
| 270. | -1.00 | -0.42 | -0.28 | -0.22 | -0.37 | 0.02 | 0.04 | 270. |
| 275. | -0.99 | -0.41 | -0.27 | -0.22 | -0.37 | 0.03 | 0.04 | 275. |
| 280. | -0.99 | -0.42 | -0.27 | -0.21 | -0.36 | 0.03 | 0.04 | 280. |
| 285. | -0.99 | -0.43 | -0.26 | -0.20 | -0.34 | 0.03 | 0.04 | 285. |
| 290. | -0.98 | -0.43 | -0.25 | -0.19 | -0.34 | 0.04 | 0.04 | 290. |
| 295. | -0.97 | -0.44 | -0.24 | -0.18 | -0.33 | 0.04 | 0.04 | 295. |
| 300. | -0.98 | -0.45 | -0.23 | -0.18 | -0.32 | 0.04 | 0.04 | 300. |
| 305. | -0.98 | -0.47 | -0.23 | -0.18 | -0.31 | 0.04 | 0.04 | 305. |
| 310. | -0.99 | -0.49 | -0.22 | -0.18 | -0.31 | 0.04 | 0.05 | 310. |
| 315. | -1.00 | -0.50 | -0.22 | -0.18 | -0.30 | 0.04 | 0.05 | 315. |
| 320. | -1.00 | -0.50 | -0.22 | -0.17 | -0.30 | 0.05 | 0.04 | 320. |
| 325. | -0.99 | -0.49 | -0.23 | -0.16 | -0.30 | 0.05 | 0.02 | 325. |
| 330. | -0.93 | -0.46 | -0.21 | -0.15 | -0.29 | 0.04 | 0.01 | 330. |
| 335. | -0.83 | -0.41 | -0.17 | -0.11 | -0.26 | 0.05 | -0.01 | 335. |
| 340. | -0.69 | -0.36 | -0.12 | -0.08 | -0.23 | 0.04 | -0.02 | 340. |
| 345. | -0.54 | -0.28 | -0.06 | -0.07 | -0.21 | 0.02 | -0.03 | 345. |
| 350. | -0.36 | -0.24 | -0.15 | -0.06 | -0.22 | 0.01 | -0.04 | 350. |
| 355. | -0.96 | -0.91 | -0.34 | -0.17 | -0.32 | -0.01 | -0.04 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 226 TCN= 39. C.R.= 8.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.140 | 10.400 | DEG. |
| 0. | -0.41 | -0.49 | -0.28 | -0.46 | -0.28 | -0.04 | -0.00 | 0. |
| 5. | -0.40 | -0.49 | -0.89 | -0.50 | -0.31 | -0.11 | -0.01 | 5. |
| 10. | -0.38 | -0.36 | -0.35 | -0.30 | -0.19 | -0.09 | -0.01 | 10. |
| 15. | -0.70 | -0.55 | -0.50 | -0.38 | -0.24 | -0.12 | -0.01 | 15. |
| 20. | -0.74 | -0.65 | -0.55 | -0.28 | -0.24 | -0.15 | -0.02 | 20. |
| 25. | -0.20 | -0.36 | -0.38 | -0.12 | -0.12 | -0.12 | -0.02 | 25. |
| 30. | 0.42 | 0.11 | -0.13 | 0.06 | 0.02 | -0.08 | -0.02 | 30. |
| 35. | 1.09 | 0.59 | 0.09 | 0.27 | 0.16 | -0.04 | -0.00 | 35. |
| 40. | 1.55 | 0.91 | 0.29 | 0.49 | 0.28 | -0.00 | 0.01 | 40. |
| 45. | 1.75 | 1.15 | 0.48 | 0.71 | 0.39 | 0.00 | 0.01 | 45. |
| 50. | 1.88 | 1.34 | 0.63 | 0.89 | 0.49 | -0.00 | 0.00 | 50. |
| 55. | 1.90 | 1.47 | 0.72 | 0.98 | 0.57 | 0.01 | -0.00 | 55. |
| 60. | 1.77 | 1.50 | 0.73 | 1.02 | 0.60 | 0.03 | 0.01 | 60. |
| 65. | 1.52 | 1.37 | 0.67 | 1.00 | 0.59 | -0.02 | 0.02 | 65. |
| 70. | 1.16 | 1.10 | 0.55 | 0.94 | 0.56 | -0.10 | -0.02 | 70. |
| 75. | 0.73 | 0.82 | 0.34 | 0.80 | 0.50 | -0.16 | -0.05 | 75. |
| 80. | 0.37 | 0.57 | 0.02 | 0.65 | 0.41 | -0.20 | -0.07 | 80. |
| 85. | 0.12 | 0.37 | -0.25 | 0.78 | 0.32 | -0.23 | -0.10 | 85. |
| 90. | -0.02 | 0.27 | -0.37 | 0.06 | 0.25 | -0.32 | -0.09 | 90. |
| 95. | -0.05 | 0.30 | -0.35 | 0.76 | 0.24 | -0.37 | -0.10 | 95. |
| 100. | 0.08 | 0.48 | -0.22 | 0.90 | 0.16 | -0.33 | -0.09 | 100. |
| 105. | 0.13 | 0.61 | -0.32 | 0.52 | 0.08 | -0.26 | -0.08 | 105. |
| 110. | -0.62 | 0.15 | -0.75 | 0.28 | 0.07 | -0.23 | -0.07 | 110. |
| 115. | -1.30 | -0.36 | -0.99 | 0.06 | 0.04 | -0.20 | -0.08 | 115. |
| 120. | -0.98 | -0.35 | -0.97 | 0.01 | -0.03 | -0.30 | -0.10 | 120. |
| 125. | -1.00 | -0.44 | -0.96 | -0.03 | -0.11 | -0.31 | -0.11 | 125. |
| 130. | -1.14 | -0.59 | -0.97 | -0.14 | -0.16 | -0.31 | -0.12 | 130. |
| 135. | -1.35 | -0.76 | -0.98 | -0.24 | -0.19 | -0.32 | -0.13 | 135. |
| 140. | -1.52 | -0.91 | -0.97 | -0.29 | -0.20 | -0.30 | -0.13 | 140. |
| 145. | -1.55 | -0.99 | -0.93 | -0.30 | -0.19 | -0.28 | -0.13 | 145. |
| 150. | -1.41 | -0.97 | -0.81 | -0.28 | -0.17 | -0.22 | -0.12 | 150. |
| 155. | -1.18 | -0.78 | -0.56 | -0.19 | -0.12 | -0.16 | -0.10 | 155. |
| 160. | -0.89 | -0.48 | -0.29 | -0.06 | -0.06 | -0.09 | -0.08 | 160. |
| 165. | -0.47 | -0.13 | -0.10 | 0.05 | 0.03 | 0.00 | -0.05 | 165. |
| 170. | -0.05 | 0.18 | 0.08 | 0.14 | 0.14 | 0.07 | -0.02 | 170. |
| 175. | 0.31 | 0.43 | 0.28 | 0.23 | 0.27 | 0.13 | 0.02 | 175. |
| 180. | 0.64 | 0.58 | 0.46 | 0.29 | 0.38 | 0.16 | 0.03 | 180. |
| 185. | 0.84 | 0.61 | 0.56 | 0.31 | 0.38 | 0.18 | 0.04 | 185. |
| 190. | 0.87 | 0.57 | 0.61 | 0.29 | 0.28 | 0.18 | 0.04 | 190. |
| 195. | 0.83 | 0.52 | 0.62 | 0.24 | 0.19 | 0.19 | 0.04 | 195. |
| 200. | 0.73 | 0.45 | 0.61 | 0.16 | 0.13 | 0.20 | 0.04 | 200. |
| 205. | 0.62 | 0.36 | 0.57 | 0.08 | 0.09 | 0.23 | 0.04 | 205. |
| 210. | 0.52 | 0.26 | 0.52 | 0.01 | 0.05 | 0.19 | 0.04 | 210. |
| 215. | 0.42 | 0.18 | 0.46 | -0.05 | 0.01 | 0.18 | 0.05 | 215. |
| 220. | 0.32 | 0.12 | 0.39 | -0.09 | -0.02 | 0.17 | 0.05 | 220. |
| 225. | 0.21 | 0.04 | 0.34 | -0.15 | -0.05 | 0.17 | 0.06 | 225. |
| 230. | 0.10 | -0.06 | 0.31 | -0.22 | -0.09 | 0.17 | 0.06 | 230. |
| 235. | 0.01 | -0.16 | 0.29 | -0.28 | -0.13 | 0.18 | 0.06 | 235. |
| 240. | -0.07 | -0.24 | 0.27 | -0.33 | -0.16 | 0.17 | 0.06 | 240. |
| 245. | -0.14 | -0.28 | 0.25 | -0.37 | -0.18 | 0.16 | 0.06 | 245. |
| 250. | -0.19 | -0.31 | 0.22 | -0.41 | -0.19 | 0.15 | 0.06 | 250. |
| 255. | -0.24 | -0.33 | 0.20 | -0.43 | -0.20 | 0.15 | 0.06 | 255. |
| 260. | -0.27 | -0.35 | 0.17 | -0.44 | -0.21 | 0.14 | 0.05 | 260. |
| 265. | -0.29 | -0.36 | 0.15 | -0.44 | -0.23 | 0.14 | 0.04 | 265. |
| 270. | -0.30 | -0.36 | 0.14 | -0.44 | -0.24 | 0.14 | 0.04 | 270. |
| 275. | -0.29 | -0.35 | 0.14 | -0.43 | -0.24 | 0.14 | 0.05 | 275. |
| 280. | -0.28 | -0.34 | 0.14 | -0.42 | -0.24 | 0.15 | 0.05 | 280. |
| 285. | -0.25 | -0.32 | 0.15 | -0.40 | -0.23 | 0.16 | 0.06 | 285. |
| 290. | -0.21 | -0.29 | 0.16 | -0.38 | -0.21 | 0.17 | 0.06 | 290. |
| 295. | -0.16 | -0.27 | 0.18 | -0.36 | -0.19 | 0.18 | 0.07 | 295. |
| 300. | -0.10 | -0.24 | 0.20 | -0.34 | -0.17 | 0.19 | 0.08 | 300. |
| 305. | -0.07 | -0.21 | 0.22 | -0.33 | -0.15 | 0.19 | 0.09 | 305. |
| 310. | 0.01 | -0.18 | 0.23 | -0.32 | -0.13 | 0.19 | 0.10 | 310. |
| 315. | 0.06 | -0.14 | 0.24 | -0.31 | -0.12 | 0.18 | 0.09 | 315. |
| 320. | 0.10 | -0.11 | 0.24 | -0.29 | -0.12 | 0.17 | 0.07 | 320. |
| 325. | 0.18 | -0.06 | 0.22 | -0.28 | -0.13 | 0.15 | 0.07 | 325. |
| 330. | 0.14 | -0.05 | 0.15 | -0.36 | -0.16 | 0.12 | 0.06 | 330. |
| 335. | -0.31 | -0.37 | 0.02 | -0.47 | -0.23 | 0.07 | 0.04 | 335. |
| 340. | -0.60 | -0.66 | -0.22 | -0.54 | -0.30 | 0.02 | 0.03 | 340. |
| 345. | -0.63 | -0.70 | -0.26 | -0.51 | -0.33 | -0.02 | 0.01 | 345. |
| 350. | -0.43 | -0.54 | -0.16 | -0.45 | -0.25 | -0.01 | -0.00 | 350. |
| 355. | -0.27 | -0.32 | 0.28 | -0.40 | -0.21 | 0.01 | -0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 226 TCN= 39. C.R.= 0.0

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.28 | 0.14 | -0.11 | 0.07 | -0.16 | -0.06 | -0.04 | 0. |
| 5. | -0.19 | 0.14 | -0.12 | 0.09 | -0.14 | -0.01 | -0.02 | 5. |
| 10. | -0.43 | 0.00 | -0.16 | 0.07 | -0.13 | -0.04 | -0.02 | 10. |
| 15. | -0.40 | -0.17 | -0.25 | 0.03 | -0.12 | -0.10 | -0.03 | 15. |
| 20. | -0.46 | -0.20 | -0.23 | 0.03 | -0.02 | -0.10 | -0.02 | 20. |
| 25. | -0.33 | 0.07 | -0.13 | 0.10 | 0.11 | -0.02 | -0.01 | 25. |
| 30. | 0.65 | 0.58 | 0.15 | 0.29 | 0.23 | 0.04 | 0.01 | 30. |
| 35. | 1.10 | 0.86 | 0.27 | 0.42 | 0.34 | 0.06 | 0.03 | 35. |
| 40. | 1.14 | 0.96 | 0.33 | 0.49 | 0.46 | 0.13 | 0.04 | 40. |
| 45. | 1.27 | 0.98 | 0.39 | 0.50 | 0.59 | 0.18 | 0.06 | 45. |
| 50. | 1.33 | 1.04 | 0.49 | 0.53 | 0.77 | 0.25 | 0.07 | 50. |
| 55. | 1.36 | 1.07 | 0.60 | 0.78 | 0.88 | 0.27 | 0.07 | 55. |
| 60. | 1.29 | 0.83 | 0.79 | 1.13 | 0.88 | 0.23 | 0.05 | 60. |
| 65. | 1.07 | 0.60 | 0.80 | 1.11 | 1.08 | 0.15 | 0.02 | 65. |
| 70. | 0.72 | 0.31 | 0.52 | 0.77 | 1.61 | 0.07 | -0.02 | 70. |
| 75. | 0.35 | -0.01 | 0.32 | 0.33 | 1.76 | -0.10 | -0.07 | 75. |
| 80. | 0.00 | -0.43 | 0.31 | 0.13 | 1.19 | -0.45 | -0.10 | 80. |
| 85. | -0.28 | -0.99 | 0.12 | 0.10 | 0.69 | -0.58 | -0.12 | 85. |
| 90. | -0.69 | -1.55 | -0.31 | 0.08 | 0.21 | -0.64 | -0.11 | 90. |
| 95. | -1.28 | -2.06 | -0.90 | -0.20 | -0.22 | -0.82 | -0.01 | 95. |
| 100. | -1.78 | -2.50 | -1.26 | -0.55 | -0.65 | -1.11 | 0.11 | 100. |
| 105. | -1.78 | -2.61 | -1.25 | -0.61 | -0.86 | -1.01 | 0.13 | 105. |
| 110. | -1.56 | -2.43 | -1.03 | -0.67 | -0.59 | -0.62 | 0.10 | 110. |
| 115. | -1.35 | -2.27 | -0.89 | -0.71 | -0.53 | -0.12 | 0.07 | 115. |
| 120. | -1.36 | -2.31 | -0.92 | -0.62 | -0.65 | 0.16 | 0.03 | 120. |
| 125. | -1.54 | -2.42 | -1.07 | -0.72 | -2.56 | 0.22 | 0.01 | 125. |
| 130. | -1.72 | -2.47 | -1.28 | -1.29 | -2.15 | 0.39 | -0.01 | 130. |
| 135. | -2.06 | -2.72 | -1.83 | -2.24 | -0.26 | -0.12 | -0.05 | 135. |
| 140. | -2.57 | -3.34 | -2.49 | -2.03 | -0.78 | -0.29 | -0.06 | 140. |
| 145. | -2.81 | -3.46 | -2.63 | -1.31 | -0.50 | -0.34 | -0.06 | 145. |
| 150. | -2.73 | -2.96 | -2.37 | -1.01 | -0.62 | -0.31 | -0.05 | 150. |
| 155. | -2.40 | -2.19 | -1.85 | -0.91 | -0.58 | -0.26 | -0.04 | 155. |
| 160. | -2.01 | -1.69 | -1.40 | -0.85 | -0.65 | -0.20 | -0.02 | 160. |
| 165. | -1.56 | -1.34 | -1.11 | -0.66 | -0.33 | -0.13 | -0.00 | 165. |
| 170. | -1.00 | -0.95 | -0.85 | -0.47 | -0.21 | -0.06 | 0.02 | 170. |
| 175. | -0.53 | -0.35 | -0.37 | -0.35 | -0.29 | -0.01 | 0.03 | 175. |
| 180. | -0.09 | 0.12 | -0.06 | -0.23 | -0.00 | 0.07 | 0.04 | 180. |
| 185. | 0.30 | 0.47 | 0.14 | -0.05 | 0.06 | 0.11 | 0.04 | 185. |
| 190. | 0.60 | 0.76 | 0.29 | 0.13 | 0.11 | 0.13 | 0.04 | 190. |
| 195. | 0.77 | 0.93 | 0.42 | 0.21 | 0.12 | 0.14 | 0.03 | 195. |
| 200. | 0.81 | 0.98 | 0.51 | 0.22 | 0.11 | 0.14 | 0.03 | 200. |
| 205. | 0.72 | 0.96 | 0.54 | 0.21 | 0.09 | 0.14 | 0.02 | 205. |
| 210. | 0.63 | 0.97 | 0.54 | 0.17 | 0.06 | 0.13 | 0.02 | 210. |
| 215. | 0.57 | 0.97 | 0.54 | 0.15 | 0.03 | 0.13 | 0.01 | 215. |
| 220. | 0.52 | 0.96 | 0.54 | 0.16 | 0.01 | 0.14 | 0.00 | 220. |
| 225. | 0.49 | 0.95 | 0.55 | 0.17 | -0.01 | 0.14 | 0.00 | 225. |
| 230. | 0.48 | 0.94 | 0.55 | 0.18 | -0.02 | 0.15 | -0.00 | 230. |
| 235. | 0.50 | 0.92 | 0.54 | 0.18 | -0.03 | 0.16 | -0.00 | 235. |
| 240. | 0.53 | 0.93 | 0.55 | 0.19 | -0.03 | 0.17 | -0.01 | 240. |
| 245. | 0.56 | 0.94 | 0.56 | 0.19 | -0.04 | 0.18 | -0.01 | 245. |
| 250. | 0.57 | 0.95 | 0.56 | 0.20 | -0.04 | 0.18 | -0.01 | 250. |
| 255. | 0.55 | 0.96 | 0.57 | 0.20 | -0.04 | 0.18 | -0.02 | 255. |
| 260. | 0.53 | 0.97 | 0.58 | 0.21 | -0.04 | 0.19 | -0.02 | 260. |
| 265. | 0.52 | 0.98 | 0.58 | 0.21 | -0.05 | 0.19 | -0.02 | 265. |
| 270. | 0.53 | 0.99 | 0.57 | 0.22 | -0.05 | 0.19 | -0.02 | 270. |
| 275. | 0.54 | 0.99 | 0.56 | 0.23 | -0.06 | 0.18 | -0.02 | 275. |
| 280. | 0.57 | 1.00 | 0.55 | 0.24 | -0.07 | 0.18 | -0.02 | 280. |
| 285. | 0.60 | 1.02 | 0.58 | 0.25 | -0.01 | 0.19 | -0.01 | 285. |
| 290. | 0.65 | 1.04 | 0.64 | 0.27 | 0.01 | 0.20 | -0.00 | 290. |
| 295. | 0.71 | 1.06 | 0.71 | 0.29 | 0.03 | 0.21 | 0.00 | 295. |
| 300. | 0.77 | 1.11 | 0.76 | 0.31 | 0.05 | 0.22 | 0.01 | 300. |
| 305. | 0.83 | 1.16 | 0.78 | 0.34 | 0.06 | 0.23 | 0.01 | 305. |
| 310. | 0.87 | 1.21 | 0.79 | 0.36 | 0.08 | 0.23 | 0.02 | 310. |
| 315. | 0.90 | 1.25 | 0.79 | 0.40 | 0.10 | 0.23 | 0.02 | 315. |
| 320. | 0.91 | 1.27 | 0.79 | 0.44 | 0.15 | 0.23 | 0.01 | 320. |
| 325. | 0.92 | 1.27 | 0.79 | 0.46 | 0.18 | 0.22 | 0.00 | 325. |
| 330. | 0.90 | 1.25 | 0.77 | 0.46 | 0.18 | 0.21 | -0.00 | 330. |
| 335. | 0.87 | 1.22 | 0.72 | 0.43 | 0.16 | 0.19 | -0.00 | 335. |
| 340. | 0.85 | 1.13 | 0.67 | 0.38 | 0.08 | 0.16 | -0.00 | 340. |
| 345. | 0.96 | 0.75 | 0.44 | 0.24 | -0.03 | 0.09 | -0.02 | 345. |
| 350. | 0.77 | 0.31 | -0.02 | 0.05 | -0.14 | -0.00 | -0.04 | 350. |
| 355. | 0.95 | 0.08 | 0.65 | 0.07 | -0.18 | -0.06 | -0.05 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 226 TCN= 39. C.R.= 8.0

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 15.400 | DEG. |
| 0. | -0.46 | -0.27 | -0.42 | -0.01 | -0.11 | 0.19 | -0.03 | 0. |
| 5. | -0.16 | 0.05 | -0.26 | 0.08 | 0.12 | 0.29 | 0.01 | 5. |
| 10. | -0.29 | -0.10 | -0.25 | 0.11 | 0.15 | 0.29 | 0.03 | 10. |
| 15. | -0.14 | -0.07 | -0.22 | 0.05 | 0.19 | 0.14 | 0.01 | 15. |
| 20. | -0.12 | -0.18 | -0.31 | -0.01 | 0.09 | 0.13 | 0.01 | 20. |
| 25. | 0.28 | 0.17 | -0.08 | 0.11 | 0.15 | 0.19 | 0.04 | 25. |
| 30. | 0.97 | 0.57 | 0.21 | 0.22 | 0.23 | 0.22 | 0.07 | 30. |
| 35. | 1.29 | 0.81 | 0.37 | 0.29 | 0.40 | 0.22 | 0.07 | 35. |
| 40. | 1.36 | 0.85 | 0.70 | 0.31 | 0.66 | 0.24 | 0.06 | 40. |
| 45. | 1.39 | 0.92 | 1.15 | 0.41 | 0.95 | 0.29 | 0.08 | 45. |
| 50. | 1.55 | 0.99 | 1.48 | 0.69 | 1.16 | 0.31 | 0.09 | 50. |
| 55. | 1.50 | 0.94 | 1.73 | 1.21 | 1.28 | 0.27 | 0.07 | 55. |
| 60. | 1.32 | 0.81 | 1.65 | 1.29 | 1.92 | 0.17 | 0.02 | 60. |
| 65. | 1.06 | 0.62 | 1.37 | 0.64 | 2.36 | 0.07 | -0.06 | 65. |
| 70. | 0.76 | 0.40 | 1.21 | 0.06 | 1.68 | -0.19 | -0.14 | 70. |
| 75. | 0.45 | 0.15 | 1.15 | -0.21 | 0.88 | -0.29 | -0.20 | 75. |
| 80. | 0.12 | -0.15 | 1.13 | -0.27 | 0.62 | -0.37 | -0.21 | 80. |
| 85. | -0.31 | -0.58 | 0.95 | -0.29 | -0.19 | -0.96 | -0.17 | 85. |
| 90. | -1.14 | -1.41 | 0.42 | -0.51 | -0.52 | -3.30 | -0.04 | 90. |
| 95. | -1.95 | -2.14 | -0.18 | -0.93 | -0.89 | -3.78 | 0.06 | 95. |
| 100. | -1.97 | -2.20 | -0.56 | -1.16 | -0.89 | -2.44 | -0.02 | 100. |
| 105. | -1.86 | -2.07 | -0.61 | -1.15 | -0.83 | -1.29 | -0.03 | 105. |
| 110. | -1.73 | -1.93 | -0.54 | -1.04 | -0.76 | -0.61 | 0.12 | 110. |
| 115. | -1.70 | -1.93 | -0.63 | -0.98 | -0.63 | -0.72 | 0.26 | 115. |
| 120. | -1.72 | -1.98 | -0.79 | -1.00 | -0.59 | -0.85 | 0.27 | 120. |
| 125. | -1.79 | -2.03 | -0.92 | -1.13 | -0.77 | -0.84 | 0.20 | 125. |
| 130. | -1.99 | -2.16 | -1.14 | -1.09 | -1.46 | 0.35 | 0.12 | 130. |
| 135. | -2.38 | -2.41 | -1.60 | -1.87 | -2.91 | 0.50 | 0.03 | 135. |
| 140. | -2.82 | -2.72 | -2.29 | -2.94 | -4.51 | 0.33 | -0.04 | 140. |
| 145. | -3.12 | -3.08 | -2.77 | -3.25 | -5.21 | -0.16 | -0.08 | 145. |
| 150. | -3.26 | -3.13 | -2.81 | -2.35 | -0.33 | -0.23 | -0.10 | 150. |
| 155. | -3.17 | -2.71 | -2.50 | -1.31 | -0.67 | -0.14 | -0.10 | 155. |
| 160. | -2.77 | -2.18 | -2.11 | -0.94 | -0.45 | -0.07 | -0.08 | 160. |
| 165. | -2.17 | -1.63 | -1.65 | -0.77 | -0.35 | 0.02 | -0.05 | 165. |
| 170. | -1.50 | -0.99 | -0.98 | -0.61 | -0.20 | 0.10 | -0.04 | 170. |
| 175. | -0.85 | -0.35 | -0.60 | -0.34 | -0.09 | 0.17 | -0.03 | 175. |
| 180. | -0.26 | 0.09 | -0.36 | -0.08 | 0.08 | 0.24 | -0.01 | 180. |
| 185. | 0.17 | 0.41 | -0.09 | 0.13 | 0.14 | 0.28 | -0.01 | 185. |
| 190. | 0.47 | 0.63 | 0.11 | 0.29 | 0.12 | 0.29 | -0.02 | 190. |
| 195. | 0.67 | 0.77 | 0.17 | 0.36 | 0.06 | 0.30 | -0.02 | 195. |
| 200. | 0.75 | 0.83 | 0.18 | 0.40 | 0.04 | 0.31 | -0.03 | 200. |
| 205. | 0.74 | 0.83 | 0.20 | 0.42 | 0.02 | 0.30 | -0.03 | 205. |
| 210. | 0.68 | 0.82 | 0.20 | 0.43 | 0.02 | 0.29 | -0.04 | 210. |
| 215. | 0.60 | 0.79 | 0.20 | 0.43 | 0.01 | 0.29 | -0.03 | 215. |
| 220. | 0.57 | 0.75 | 0.20 | 0.42 | 0.01 | 0.30 | -0.03 | 220. |
| 225. | 0.57 | 0.74 | 0.20 | 0.44 | -0.01 | 0.31 | -0.02 | 225. |
| 230. | 0.58 | 0.74 | 0.21 | 0.46 | -0.02 | 0.31 | -0.02 | 230. |
| 235. | 0.60 | 0.75 | 0.22 | 0.48 | -0.04 | 0.32 | -0.01 | 235. |
| 240. | 0.63 | 0.76 | 0.23 | 0.50 | -0.05 | 0.33 | -0.01 | 240. |
| 245. | 0.66 | 0.79 | 0.25 | 0.53 | -0.05 | 0.35 | -0.01 | 245. |
| 250. | 0.69 | 0.82 | 0.28 | 0.55 | -0.05 | 0.35 | -0.01 | 250. |
| 255. | 0.71 | 0.86 | 0.31 | 0.56 | -0.05 | 0.34 | -0.01 | 255. |
| 260. | 0.73 | 0.89 | 0.33 | 0.57 | -0.04 | 0.34 | -0.02 | 260. |
| 265. | 0.75 | 0.91 | 0.35 | 0.58 | -0.03 | 0.33 | -0.02 | 265. |
| 270. | 0.7 | 0.93 | 0.35 | 0.59 | -0 | 0.33 | -0.02 | 270. |
| 275. | 0.77 | 0.94 | 0.36 | 0.60 | -0. | 0.34 | -0.02 | 275. |
| 280. | 0.78 | 0.96 | 0.37 | 0.61 | 0.01 | 0.35 | -0.01 | 280. |
| 285. | 0.81 | 0.98 | 0.39 | 0.62 | 0.02 | 0.36 | -0.00 | 285. |
| 290. | 0.86 | 1.01 | 0.41 | 0.64 | 0.03 | 0.37 | 0.00 | 290. |
| 295. | 0.93 | 1.05 | 0.45 | 0.66 | 0.04 | 0.38 | 0.01 | 295. |
| 300. | 1.03 | 1.09 | 0.49 | 0.68 | 0.07 | 0.39 | 0.02 | 300. |
| 305. | 1.15 | 1.16 | 0.54 | 0.71 | 0.09 | 0.40 | 0.02 | 305. |
| 310. | 1.26 | 1.24 | 0.58 | 0.73 | 0.11 | 0.40 | 0.02 | 310. |
| 315. | 1.34 | 1.30 | 0.62 | 0.76 | 0.13 | 0.41 | 0.03 | 315. |
| 320. | 1.38 | 1.33 | 0.65 | 0.76 | 0.13 | 0.41 | 0.03 | 320. |
| 325. | 1.39 | 1.32 | 0.65 | 0.75 | 0.13 | 0.40 | 0.03 | 325. |
| 330. | 1.33 | 1.27 | 0.63 | 0.72 | 0.12 | 0.40 | 0.04 | 330. |
| 335. | 1.23 | 1.20 | 0.55 | 0.69 | 0.10 | 0.39 | 0.04 | 335. |
| 340. | 1.25 | 1.30 | 0.47 | 0.70 | 0.06 | 0.37 | 0.03 | 340. |
| 345. | 1.05 | 0.88 | 0.37 | 0.62 | -0.00 | 0.33 | 0.02 | 345. |
| 350. | 0.17 | 0.10 | 0.03 | 0.34 | -0.06 | 0.27 | -0.01 | 350. |
| 355. | -0.40 | -0.21 | -0.30 | 0.10 | -0.15 | 0.14 | -0.04 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-404 CNFG NO. 226 TCM= 39. C.R.= 0.3

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.990 | 7.190 | 10.400 | DEG. |
| 0. | -0.73 | -0.75 | -0.67 | -0.31 | -0.16 | -0.12 | -0.03 | 0. |
| 5. | -0.21 | 0.12 | -0.36 | 0.04 | -0.01 | -0.07 | 0.00 | 5. |
| 10. | 0.11 | 0.30 | -0.16 | 0.04 | 0.00 | -0.04 | 0.01 | 10. |
| 15. | -0.11 | 0.28 | -0.34 | -0.12 | 0.04 | -0.14 | -0.02 | 15. |
| 20. | -0.29 | -0.10 | -0.42 | -0.14 | 0.02 | -0.15 | -0.02 | 20. |
| 25. | -0.03 | 0.17 | -0.24 | 0.00 | 0.00 | -0.12 | -0.00 | 25. |
| 30. | 0.66 | 0.44 | -0.14 | 0.09 | 0.19 | -0.11 | 0.02 | 30. |
| 35. | 1.25 | 0.60 | -0.71 | 0.01 | 0.28 | -0.13 | 0.03 | 35. |
| 40. | 1.45 | 0.66 | 0.48 | 0.23 | 0.40 | -0.11 | 0.03 | 40. |
| 45. | 1.44 | 0.65 | 1.14 | 0.97 | 0.57 | -0.10 | 0.03 | 45. |
| 50. | 1.35 | 0.88 | 1.34 | 1.00 | 0.46 | -0.19 | 0.02 | 50. |
| 55. | 1.44 | 0.96 | 1.32 | 2.30 | 1.56 | -0.26 | -0.01 | 55. |
| 60. | 1.05 | 1.05 | 1.19 | 1.50 | 1.06 | -0.40 | -0.06 | 60. |
| 65. | 1.52 | 0.98 | 1.12 | 0.94 | 1.29 | -0.30 | -0.10 | 65. |
| 70. | 1.30 | 0.78 | 1.04 | 0.28 | 0.96 | 0.19 | -0.27 | 70. |
| 75. | 0.98 | 0.27 | 0.95 | -0.18 | 0.57 | -0.22 | -0.20 | 75. |
| 80. | 0.34 | -0.27 | 0.78 | -0.34 | 0.22 | -1.34 | -0.04 | 80. |
| 85. | -0.43 | -0.98 | 0.34 | -0.66 | -0.18 | -2.37 | 0.02 | 85. |
| 90. | -1.09 | -1.66 | -0.15 | -1.19 | -0.94 | -1.32 | -0.22 | 90. |
| 95. | -1.81 | -1.98 | -0.45 | -1.38 | -0.69 | -0.58 | -0.51 | 95. |
| 100. | -1.88 | -1.88 | -0.49 | -1.17 | -0.74 | -0.02 | -0.67 | 100. |
| 105. | -1.68 | -1.72 | -0.44 | -0.99 | -0.76 | 1.05 | -0.45 | 105. |
| 110. | -1.51 | -1.39 | -0.44 | -0.84 | -0.77 | 1.46 | -0.11 | 110. |
| 115. | -1.44 | -1.37 | -0.44 | -0.88 | -0.80 | 1.43 | 0.12 | 115. |
| 120. | -1.47 | -1.50 | -0.53 | -0.86 | -0.88 | 0.23 | 0.27 | 120. |
| 125. | -1.57 | -1.99 | -2.03 | -0.97 | -0.92 | -1.14 | 0.33 | 125. |
| 130. | -1.77 | -1.62 | -0.63 | -1.12 | -1.32 | -0.57 | 0.20 | 130. |
| 135. | -2.04 | -1.78 | -0.48 | -1.44 | -2.57 | 0.18 | 0.10 | 135. |
| 140. | -2.37 | -2.10 | -1.42 | -2.86 | -2.73 | -2.80 | 0.06 | 140. |
| 145. | -2.69 | -2.44 | -2.85 | -3.17 | -0.88 | -0.41 | 0.02 | 145. |
| 150. | -2.91 | -2.75 | -2.41 | -2.99 | -0.35 | -0.53 | 0.01 | 150. |
| 155. | -2.96 | -2.88 | -2.46 | -1.19 | -0.41 | -0.46 | 0.01 | 155. |
| 160. | -2.78 | -2.59 | -2.14 | -0.88 | -0.49 | -0.38 | 0.02 | 160. |
| 165. | -2.22 | -2.08 | -1.64 | -0.87 | -0.37 | -0.38 | 0.03 | 165. |
| 170. | -1.51 | -1.41 | -1.12 | -0.68 | -0.23 | -0.24 | 0.03 | 170. |
| 175. | -0.91 | -0.82 | -0.78 | -0.38 | -0.18 | -0.17 | 0.03 | 175. |
| 180. | -0.44 | -0.39 | -0.43 | -0.08 | 0.31 | -0.07 | 0.06 | 180. |
| 185. | 0.05 | -0.08 | -0.22 | 0.17 | 0.09 | 0.02 | 0.07 | 185. |
| 190. | 0.39 | 0.24 | -0.01 | 0.28 | 0.15 | 0.08 | 0.05 | 190. |
| 195. | 0.59 | 0.47 | 0.12 | 0.35 | 0.19 | 0.10 | 0.04 | 195. |
| 200. | 0.67 | 0.60 | 0.18 | 0.36 | 0.22 | 0.10 | 0.03 | 200. |
| 205. | 0.65 | 0.65 | 0.20 | 0.40 | 0.21 | 0.11 | 0.03 | 205. |
| 210. | 0.58 | 0.66 | 0.21 | 0.41 | 0.19 | 0.11 | 0.03 | 210. |
| 215. | 0.48 | 0.64 | 0.21 | 0.41 | 0.16 | 0.12 | 0.03 | 215. |
| 220. | 0.41 | 0.64 | 0.20 | 0.41 | 0.13 | 0.14 | 0.03 | 220. |
| 225. | 0.36 | 0.67 | 0.20 | 0.41 | 0.12 | 0.18 | 0.04 | 225. |
| 230. | 0.34 | 0.70 | 0.24 | 0.43 | 0.13 | 0.21 | 0.04 | 230. |
| 235. | 0.34 | 0.72 | 0.27 | 0.46 | 0.13 | 0.25 | 0.05 | 235. |
| 240. | 0.36 | 0.75 | 0.31 | 0.48 | 0.15 | 0.25 | 0.05 | 240. |
| 245. | 0.40 | 0.77 | 0.34 | 0.50 | 0.16 | 0.26 | 0.05 | 245. |
| 250. | 0.44 | 0.79 | 0.37 | 0.51 | 0.18 | 0.27 | 0.05 | 250. |
| 255. | 0.49 | 0.80 | 0.39 | 0.52 | 0.19 | 0.28 | 0.05 | 255. |
| 260. | 0.55 | 0.82 | 0.39 | 0.52 | 0.20 | 0.28 | 0.05 | 260. |
| 265. | 0.60 | 0.85 | 0.40 | 0.53 | 0.20 | 0.29 | 0.05 | 265. |
| 270. | 0.64 | 0.89 | 0.40 | 0.53 | 0.21 | 0.29 | 0.04 | 270. |
| 275. | 0.66 | 0.91 | 0.40 | 0.54 | 0.21 | 0.29 | 0.04 | 275. |
| 280. | 0.68 | 0.94 | 0.40 | 0.54 | 0.22 | 0.30 | 0.04 | 280. |
| 285. | 0.72 | 0.97 | 0.41 | 0.56 | 0.22 | 0.30 | 0.04 | 285. |
| 290. | 0.78 | 1.01 | 0.45 | 0.60 | 0.23 | 0.33 | 0.05 | 290. |
| 295. | 0.86 | 1.05 | 0.49 | 0.62 | 0.25 | 0.32 | 0.05 | 295. |
| 300. | 0.96 | 1.10 | 0.53 | 0.64 | 0.26 | 0.30 | 0.05 | 300. |
| 305. | 1.06 | 1.15 | 0.56 | 0.65 | 0.29 | 0.31 | 0.04 | 305. |
| 310. | 1.19 | 1.20 | 0.58 | 0.66 | 0.27 | 0.31 | 0.04 | 310. |
| 315. | 1.26 | 1.23 | 0.59 | 0.70 | 0.29 | 0.31 | 0.04 | 315. |
| 320. | 1.34 | 1.25 | 0.61 | 0.71 | 0.30 | 0.31 | 0.03 | 320. |
| 325. | 1.33 | 1.24 | 0.62 | 0.71 | 0.31 | 0.30 | 0.03 | 325. |
| 330. | 1.23 | 1.23 | 0.61 | 0.68 | 0.32 | 0.29 | 0.02 | 330. |
| 335. | 1.11 | 1.17 | 0.65 | 0.63 | 0.31 | 0.26 | 0.01 | 335. |
| 340. | 1.10 | 1.17 | 0.62 | 0.57 | 0.30 | 0.22 | -0.00 | 340. |
| 345. | 0.92 | 1.03 | 0.44 | 0.52 | 0.26 | 0.19 | -0.02 | 345. |
| 350. | 0.32 | 0.50 | 0.00 | 0.21 | 0.11 | 0.11 | -0.03 | 350. |
| 355. | -0.01 | -0.08 | -0.21 | -0.13 | -0.08 | -0.05 | -0.03 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=497 CNTR NO. 256 TCN= 40. C.R.= 25.9

DIFFERENTIAL PRESSURE

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 2.499 | 1.936 | 4.550 | 12.480 | DEG. |
| 0. | -0.04 | -0.23 | 0.05 | -0.37 | 0. |
| 5. | -0.34 | -0.29 | 0.09 | -0.31 | 5. |
| 10. | -0.02 | -0.26 | 0.12 | -0.04 | 10. |
| 15. | -1.16 | -0.44 | 0.11 | -0.10 | 15. |
| 20. | -1.01 | -0.37 | 0.04 | -0.11 | 20. |
| 25. | -0.70 | -0.33 | 0.03 | -0.30 | 25. |
| 30. | -0.04 | -0.29 | 0.04 | -0.08 | 30. |
| 35. | -0.04 | -0.39 | 0.02 | -0.12 | 35. |
| 40. | -0.02 | -0.48 | 0.02 | -0.09 | 40. |
| 45. | -0.46 | -0.21 | 0.04 | -0.04 | 45. |
| 50. | -0.08 | -0.09 | 0.21 | -0.01 | 50. |
| 55. | 0.09 | -0.12 | -0.03 | 0.01 | 55. |
| 60. | 0.12 | -0.03 | -0.04 | 0.01 | 60. |
| 65. | 0.04 | -0.13 | -0.08 | -0.00 | 65. |
| 70. | -0.07 | -0.15 | -0.09 | -0.01 | 70. |
| 75. | -0.08 | -0.15 | -0.08 | -0.01 | 75. |
| 80. | -0.02 | -0.12 | -0.07 | 0.01 | 80. |
| 85. | 0.03 | -0.06 | -0.03 | 0.02 | 85. |
| 90. | 0.17 | 0.02 | -0.01 | 0.02 | 90. |
| 95. | 0.30 | 0.12 | 0.03 | 0.03 | 95. |
| 100. | 0.03 | 0.25 | 0.05 | 0.13 | 100. |
| 105. | 0.08 | 0.38 | 0.07 | 0.18 | 105. |
| 110. | 1.16 | 0.57 | 0.11 | 0.22 | 110. |
| 115. | 1.29 | 0.64 | 0.16 | 0.25 | 115. |
| 120. | 1.45 | 0.75 | 0.18 | 0.28 | 120. |
| 125. | 1.58 | 0.83 | 0.18 | 0.29 | 125. |
| 130. | 1.66 | 0.88 | 0.18 | 0.30 | 130. |
| 135. | 1.77 | 0.92 | 0.18 | 0.31 | 135. |
| 140. | 1.82 | 0.95 | 0.19 | 0.31 | 140. |
| 145. | 1.86 | 0.97 | 0.19 | 0.32 | 145. |
| 150. | 1.81 | 0.89 | 0.18 | 0.28 | 150. |
| 155. | 1.75 | 0.84 | 0.16 | 0.27 | 155. |
| 160. | 1.65 | 0.78 | 0.15 | 0.25 | 160. |
| 165. | 1.51 | 0.71 | 0.15 | 0.22 | 165. |
| 170. | 1.32 | 0.63 | 0.15 | 0.19 | 170. |
| 175. | 1.07 | 0.51 | 0.12 | 0.14 | 175. |
| 180. | 0.76 | 0.33 | 0.09 | 0.10 | 180. |
| 185. | 0.27 | 0.12 | 0.06 | 0.05 | 185. |
| 190. | -0.18 | -0.06 | 0.05 | -0.00 | 190. |
| 195. | -0.11 | -0.17 | 0.04 | -0.05 | 195. |
| 200. | -0.33 | -0.17 | 0.03 | -0.11 | 200. |
| 205. | -0.40 | -0.25 | 0.01 | -0.15 | 205. |
| 210. | -0.32 | -0.27 | -0.03 | -0.16 | 210. |
| 215. | -0.40 | -0.31 | -0.07 | -0.16 | 215. |
| 220. | -0.40 | -0.31 | -0.10 | -0.15 | 220. |
| 225. | -0.47 | -0.30 | -0.12 | -0.15 | 225. |
| 230. | -0.44 | -0.27 | -0.13 | -0.14 | 230. |
| 235. | -0.46 | -0.25 | -0.13 | -0.13 | 235. |
| 240. | -0.46 | -0.23 | -0.14 | -0.13 | 240. |
| 245. | -0.44 | -0.22 | -0.14 | -0.12 | 245. |
| 250. | -0.44 | -0.21 | -0.15 | -0.11 | 250. |
| 255. | -0.47 | -0.20 | -0.15 | -0.11 | 255. |
| 260. | -0.48 | -0.20 | -0.15 | -0.11 | 260. |
| 265. | -0.49 | -0.20 | -0.14 | -0.10 | 265. |
| 270. | -0.50 | -0.20 | -0.13 | -0.10 | 270. |
| 275. | -0.51 | -0.19 | -0.13 | -0.10 | 275. |
| 280. | -0.51 | -0.19 | -0.14 | -0.10 | 280. |
| 285. | -0.52 | -0.19 | -0.16 | -0.10 | 285. |
| 290. | -0.52 | -0.19 | -0.21 | -0.09 | 290. |
| 295. | -0.53 | -0.18 | -0.24 | -0.07 | 295. |
| 300. | -0.50 | -0.16 | -0.21 | -0.04 | 300. |
| 305. | -0.50 | -0.15 | -0.15 | -0.03 | 305. |
| 310. | -0.01 | -0.12 | -0.14 | -0.05 | 310. |
| 315. | -0.01 | -0.17 | -0.09 | -0.05 | 315. |
| 320. | -0.36 | -0.29 | 0.00 | -0.03 | 320. |
| 325. | -0.37 | -0.12 | 0.10 | 0.02 | 325. |
| 330. | -0.21 | -0.04 | 0.15 | 0.04 | 330. |
| 335. | -0.07 | -0.13 | 0.26 | -0.02 | 335. |
| 340. | -0.04 | -0.52 | -0.03 | -0.13 | 340. |
| 345. | -0.07 | -0.68 | -0.02 | -0.23 | 345. |
| 350. | -0.08 | -0.68 | -0.01 | -0.25 | 350. |
| 355. | -1.03 | -0.53 | -0.02 | -0.25 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=447 CWG NO. 256 ICA= 4C. C.G.= 25.%

DIFFERENTIAL PRESSURES

SPAN STATION 70.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.455 | 1.046 | 1.957 | [illegible] | 4.959 | 7.153 | 10.460 | DEG. |
| 0. | -2.19 | -1.53 | -3.99 | -C.67 | -0.53 | -3.21 | -0.03 | 0. |
| 5. | -2.01 | -1.19 | -3.83 | -C.52 | -0.36 | -3.12 | 0.00 | 5. |
| 10. | -1.96 | -0.74 | -3.54 | -0.36 | -0.16 | -3.11 | 0.11 | 10. |
| 15. | -3.4 | -0.34 | -3.71 | -0.39 | -0.19 | -0.01 | 0.13 | 15. |
| 20. | -3.66 | -0.5[illegible] | -3.42 | -0.34 | -0.20 | -3.11 | 0.32 | 20. |
| 25. | -1.28 | -1.02 | -3.74 | -0.42 | -0.19 | -3.18 | -[illegible].04 | 25. |
| 30. | -1.39 | -0.89 | -0.78 | -[illegible].65 | -[illegible].31 | -3.23 | -0.03 | 30. |
| 35. | -0.84 | -0.56 | -3.57 | -0.3[illegible] | -3.20 | -3.16 | -0.02 | 35. |
| 40. | -0.46 | -0.31 | -0.38 | -0.20 | -0.11 | -3.12 | -0.09 | 40. |
| 45. | -0.21 | -0.17 | [illegible].29 | -[illegible].14 | -0.07 | -3.11 | -[illegible].[illegible] | 45. |
| 50. | -0.08 | -0.11 | -0.26 | -0.11 | -0.04 | -3.13 | -0.02 | 50. |
| 55. | -0.04 | -[illegible].31 | -0.27 | -[illegible].11 | -0.07 | -3.15 | -0.04 | 55. |
| 60. | -0.05 | -0.11 | -0.26 | -0.12 | -3.07 | -3.17 | -0.05 | 60. |
| 65. | -0.09 | -[illegible].13 | -0.24 | -[illegible].12 | -3.06 | -3.14 | -[illegible].04 | 65. |
| 70. | -0.14 | -0.15 | -[illegible].25 | -[illegible].12 | -3.11 | -[illegible].17 | -0.02 | 70. |
| 75. | -0.17 | -0.13 | -[illegible].23 | -0.10 | 0.04 | -3.14 | -0.02 | 75. |
| 80. | -0.15 | -[illegible].07 | -0.21 | -[illegible].07 | 0.15 | -3.15 | -0.01 | 80. |
| 85. | -0.05 | 0.0[illegible] | -0.16 | -0.03 | 0.16 | -3.14 | -[illegible].01 | 85. |
| 90. | 0.12 | [illegible].18 | -[illegible].[illegible] | [illegible].04 | 0.19 | -3.12 | -0.03 | 90. |
| 95. | 0.32 | 0.2[illegible] | 0.17 | 0.13 | 0.24 | -[illegible].[illegible]7 | 0.01 | 95. |
| 100. | 0.58 | 0.44 | 0.25 | 0.25 | 0.33 | -[illegible].[illegible]3 | 0.04 | 100. |
| 105. | 0.80 | 0.74 | 0.45 | 0.38 | 0.45 | 0.36 | 0.06 | 105. |
| 110. | 1.24 | 0.99 | [illegible].63 | [illegible].51 | 0.56 | 0.12 | 0.09 | 110. |
| 115. | 1.50 | 1.23 | 0.79 | [illegible].62 | [illegible].64 | 0.17 | 0.11 | 115. |
| 120. | 1.89 | 1.43 | 0.97 | [illegible].7[illegible] | 0.76 | 0.23 | 0.12 | 120. |
| 125. | 2.12 | 1.55 | 1.12 | [illegible].76 | 0.76 | 0.25 | 0.14 | 125. |
| 130. | 2.30 | 1.62 | 1.19 | [illegible].79 | 0.75 | [illegible].28 | 0.16 | 130. |
| 135. | 2.42 | [illegible].66 | 1.14 | [illegible].79 | 0.74 | 0.24 | 0.15 | 135. |
| 140. | 2.46 | 1.68 | 1.17 | [illegible].74 | [illegible].73 | 0.27 | 0.15 | 140. |
| 145. | 2.45 | 1.67 | 1.16 | [illegible].77 | [illegible].65 | [illegible].26 | [illegible].14 | 145. |
| 150. | 2.44 | 1.66 | 1.14 | [illegible].76 | [illegible].61 | [illegible].25 | [illegible].12 | 150. |
| 155. | 2.51 | 1.68 | 1.15 | [illegible].77 | [illegible].60 | [illegible].24 | [illegible].13 | 155. |
| 160. | 2.56 | 1.72 | 1.19 | [illegible].80 | [illegible].61 | [illegible].29 | [illegible].13 | 160. |
| 165. | 2.58 | 1.73 | 1.22 | [illegible].82 | [illegible].61 | [illegible].31 | [illegible].14 | 165. |
| 170. | [illegible].67 | 1.68 | 1.22 | [illegible].81 | [illegible].[illegible]5 | [illegible].33 | [illegible].14 | 170. |
| 175. | 2.77 | 1.54 | [illegible].17 | [illegible].76 | [illegible].56 | [illegible].33 | [illegible].14 | 175. |
| 180. | 1.96 | 1.28 | [illegible].16 | [illegible].64 | [illegible].47 | [illegible].33 | [illegible].13 | 180. |
| 185. | 1.52 | [illegible].93 | [illegible].04 | [illegible].52 | [illegible].34 | [illegible].25 | [illegible].11 | 185. |
| 190. | 1.00 | [illegible].54 | [illegible].94 | [illegible].35 | [illegible].22 | [illegible].19 | [illegible].09 | 190. |
| 195. | [illegible].47 | [illegible].29 | [illegible].31 | [illegible].19 | [illegible].[illegible]6 | [illegible].12 | [illegible].08 | 195. |
| 200. | [illegible].08 | [illegible].18 | [illegible].19 | [illegible].14 | -[illegible].[illegible]0 | [illegible].15 | [illegible].02 | 200. |
| 205. | -0.35 | [illegible].11 | -[illegible].17 | -[illegible].06 | -0.17 | [illegible].[illegible]1 | -0.03 | 205. |
| 210. | -0.52 | -[illegible].05 | -[illegible].[illegible]3 | -[illegible].13 | -0.22 | -[illegible].[illegible]2 | -[illegible].02 | 210. |
| 215. | -0.64 | -[illegible].29 | -[illegible].29 | -[illegible].19 | -[illegible].25 | -[illegible].[illegible]5 | -[illegible].[illegible]2 | 215. |
| 220. | -1.68 | -[illegible].4[illegible] | -[illegible].35 | -[illegible].24 | -[illegible].29 | -[illegible].[illegible]7 | -[illegible].03 | 220. |
| 225. | -1.78 | -[illegible].5[illegible] | -[illegible].39 | -[illegible].2[illegible] | -[illegible].32 | -[illegible].[illegible]9 | -[illegible].05 | 225. |
| 230. | -0.85 | -[illegible].61 | -[illegible].44 | -[illegible].31 | -[illegible].36 | -[illegible].[illegible]3 | -[illegible].06 | 230. |
| 235. | -0.[illegible] | -[illegible].[illegible] | -[illegible].[illegible] | -0.32 | -[illegible].34 | -[illegible].[illegible] | -[illegible].09 | 235. |
| 240. | -[illegible].92 | -[illegible].66 | -[illegible].39 | -[illegible].31 | -[illegible].35 | -[illegible].[illegible]2 | -[illegible].[illegible] | 240. |
| 245. | -[illegible].92 | -[illegible].66 | -[illegible].39 | -[illegible].[illegible]3 | -[illegible].36 | -[illegible].11 | -[illegible].[illegible] | 245. |
| 250. | -[illegible].91 | -[illegible].65 | -[illegible].36 | -[illegible].[illegible]5 | -[illegible].[illegible]7 | -[illegible].11 | -[illegible].11 | 250. |
| 255. | -[illegible].89 | -[illegible].6[illegible] | -[illegible].33 | -[illegible].29 | -[illegible].[illegible]7 | -[illegible].1[illegible] | -[illegible].12 | 255. |
| 260. | -[illegible].87 | -[illegible].61 | -[illegible].32 | -[illegible].29 | -[illegible].[illegible]6 | -[illegible].13 | -[illegible].[illegible]7 | 260. |
| 265. | -[illegible].87 | -[illegible].6[illegible] | -[illegible].31 | -[illegible].28 | -[illegible].34 | -[illegible].[illegible]9 | -[illegible].12 | 265. |
| 270. | -[illegible].87 | -[illegible].58 | -[illegible].31 | -[illegible].28 | -[illegible].32 | -[illegible].[illegible]9 | -[illegible].11 | 270. |
| 275. | -[illegible].87 | -[illegible].58 | -[illegible].31 | -[illegible].28 | -[illegible].33 | -[illegible].[illegible]9 | -[illegible].11 | 275. |
| 280. | -[illegible].87 | -[illegible].58 | -[illegible].31 | -[illegible].27 | -[illegible].[illegible]8 | -[illegible].[illegible]3 | -[illegible].12 | 280. |
| 285. | -[illegible].87 | -[illegible].59 | -[illegible].31 | -[illegible].27 | -[illegible].26 | -[illegible].[illegible]9 | -[illegible].11 | 285. |
| 290. | -[illegible].87 | -[illegible].6[illegible] | -[illegible].31 | -[illegible].27 | -[illegible].24 | -[illegible].[illegible]8 | -[illegible].13 | 290. |
| 295. | -[illegible].87 | -[illegible].61 | -[illegible].31 | -[illegible].27 | -[illegible].23 | -[illegible].[illegible]6 | -[illegible].12 | 295. |
| 300. | -[illegible].87 | -[illegible].62 | -[illegible].32 | -[illegible].27 | -[illegible].22 | -[illegible].[illegible]5 | -[illegible].14 | 300. |
| 305. | -[illegible].87 | -[illegible].63 | -[illegible].32 | -[illegible].27 | -[illegible].22 | -[illegible].[illegible]3 | -[illegible].15 | 305. |
| 310. | -[illegible].87 | -[illegible].64 | -[illegible].32 | -[illegible].26 | -[illegible].22 | -[illegible].[illegible]1 | -[illegible].14 | 310. |
| 315. | -[illegible].87 | -[illegible].63 | -[illegible].33 | -[illegible].25 | -[illegible].22 | -[illegible].[illegible]0 | -[illegible].12 | 315. |
| 320. | -[illegible].87 | -[illegible].62 | -[illegible].33 | -[illegible].23 | -[illegible].22 | [illegible].[illegible]3 | -[illegible].[illegible]7 | 320. |
| 325. | -[illegible].[illegible]4 | -[illegible].[illegible]1 | -[illegible].32 | -[illegible].21 | -[illegible].21 | -[illegible].[illegible]1 | -[illegible].[illegible]1 | 325. |
| 330. | -[illegible].[illegible]4 | -[illegible].[illegible]1 | -[illegible].32 | -[illegible].21 | -[illegible].22 | [illegible].[illegible]8 | [illegible].[illegible]3 | 330. |
| 335. | -[illegible].[illegible]8 | -[illegible].[illegible]5 | -[illegible].[illegible]8 | -[illegible].25 | -[illegible].24 | -[illegible].[illegible]2 | [illegible].[illegible]2 | 335. |
| 340. | -[illegible].[illegible]4 | -[illegible].[illegible]4 | -[illegible].[illegible]4 | -[illegible].[illegible]9 | -[illegible].[illegible]7 | -[illegible].[illegible]7 | -[illegible].[illegible]2 | 340. |
| 345. | -[illegible].87 | -[illegible].67 | -[illegible].41 | -[illegible].31 | -[illegible].28 | -[illegible].[illegible]5 | -[illegible].[illegible]2 | 345. |
| 350. | -[illegible].92 | -[illegible].[illegible]5 | -[illegible].[illegible]6 | -[illegible].37 | -[illegible].33 | -[illegible].[illegible]6 | [illegible].[illegible]1 | 350. |
| 355. | -[illegible].[illegible]0 | -[illegible].[illegible]4 | -[illegible].[illegible]4 | -[illegible].[illegible]4 | -[illegible].[illegible]4 | -[illegible].[illegible]9 | -[illegible].[illegible]3 | 355. |

TEXT NOT REPRODUCIBLE

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-497 CETA NO. 256 TCNO 4C. C.G.= 29.9

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.000 | 1.959 | 2.990 | 4.999 | 7.153 | 10.400 | DEG. |
| 0. | -1.04 | -1.27 | -0.82 | -0.54 | -0.45 | -0.18 | -0.05 | 0. |
| 5. | -1.00 | -1.28 | -0.87 | -0.61 | -0.41 | -0.23 | -0.08 | 5. |
| 10. | -1.05 | -1.32 | -0.82 | -0.57 | -0.37 | -0.24 | -0.13 | 10. |
| 15. | -1.41 | -1.35 | -0.57 | -0.43 | -0.23 | -0.22 | -0.16 | 15. |
| 20. | -0.75 | -1.17 | -0.31 | -0.27 | -0.07 | -0.15 | -0.12 | 20. |
| 25. | -0.20 | -0.52 | -0.19 | -0.11 | 0.07 | -0.12 | -0.09 | 25. |
| 30. | 0.15 | 0.02 | 0.03 | -0.07 | 0.18 | -0.13 | -0.16 | 30. |
| 35. | 0.51 | 0.10 | 0.03 | 0.07 | 0.28 | -0.19 | -0.10 | 35. |
| 40. | 0.83 | 0.26 | 0.17 | 0.17 | 0.38 | -0.08 | -0.12 | 40. |
| 45. | 1.10 | 0.48 | 0.29 | 0.20 | 0.48 | -0.07 | -0.11 | 45. |
| 50. | 1.30 | 0.59 | 0.36 | 0.27 | 0.48 | -0.06 | -0.13 | 50. |
| 55. | 1.43 | 0.62 | 0.40 | 0.34 | 0.41 | -0.08 | -0.14 | 55. |
| 60. | 1.46 | 0.54 | 0.33 | 0.26 | 0.34 | -0.10 | -0.13 | 60. |
| 65. | 1.33 | 0.41 | 0.21 | 0.17 | 0.49 | -0.11 | -0.13 | 65. |
| 70. | 1.13 | 0.25 | 0.14 | 0.09 | 0.43 | -0.14 | -0.14 | 70. |
| 75. | 0.90 | 0.10 | -0.02 | -0.03 | 0.35 | -0.16 | -0.15 | 75. |
| 80. | 0.71 | -0.02 | -0.22 | -0.11 | 0.29 | -0.17 | -0.14 | 80. |
| 85. | 0.61 | -0.07 | -0.24 | -0.12 | 0.26 | -0.16 | -0.11 | 85. |
| 90 | 0.77 | 0.04 | -0.14 | -0.04 | 0.31 | -0.12 | -0.09 | 90. |
| 95. | 1.03 | 0.27 | 0.04 | 0.08 | 0.39 | -0.05 | -0.06 | 95. |
| 100. | 1.30 | 0.62 | 0.33 | 0.26 | 0.46 | 0.02 | -0.05 | 100. |
| 105. | 1.60 | 0.88 | 0.60 | 0.38 | 0.51 | 0.03 | -0.06 | 105. |
| 110. | 1.83 | 1.03 | 0.65 | 0.42 | 0.52 | 0.01 | -0.05 | 110. |
| 115. | 1.75 | 0.99 | 0.51 | 0.37 | 0.47 | 0.02 | -0.03 | 115. |
| 120. | 1.52 | 0.76 | 0.37 | 0.27 | 0.30 | 0.01 | -0.02 | 120. |
| 125. | 1.17 | 0.53 | 0.13 | 0.13 | 0.30 | 0.01 | -0.01 | 125. |
| 130. | 0.80 | 0.29 | 0.04 | 0.03 | 0.22 | 0.01 | 0.00 | 130. |
| 135. | 0.65 | 0.25 | 0.05 | 0.02 | 0.19 | 0.02 | 0.01 | 135. |
| 140. | 0.71 | 0.32 | 0.12 | 0.05 | 0.19 | 0.04 | 0.01 | 140. |
| 145. | 0.76 | 0.45 | 0.23 | 0.12 | 0.21 | 0.05 | 0.03 | 145. |
| 150. | 0.95 | 0.59 | 0.31 | 0.21 | 0.24 | 0.11 | 0.06 | 150. |
| 155. | 1.03 | 0.75 | 0.43 | 0.27 | 0.27 | 0.15 | 0.09 | 155. |
| 160. | 1.23 | 0.91 | 0.59 | 0.42 | 0.30 | 0.23 | 0.10 | 160. |
| 165. | 1.47 | 1.06 | 0.69 | 0.46 | 0.34 | 0.25 | 0.11 | 165. |
| 170. | 1.52 | 1.16 | 0.80 | 0.58 | 0.36 | 0.29 | 0.13 | 170. |
| 175. | 1.53 | 1.25 | 0.87 | 0.63 | 0.36 | 0.31 | 0.15 | 175. |
| 180. | 1.49 | 1.19 | 0.85 | 0.61 | 0.33 | 0.31 | 0.16 | 180. |
| 185. | 1.24 | 1.05 | 0.74 | 0.53 | 0.27 | 0.24 | 0.15 | 185. |
| 190. | 0.96 | 0.88 | 0.61 | 0.44 | 0.18 | 0.24 | 0.14 | 190. |
| 195. | 0.87 | 0.85 | 0.57 | 0.34 | 0.20 | 0.23 | 0.12 | 195. |
| 200. | 0.89 | 0.84 | 0.57 | 0.23 | 0.21 | 0.16 | 0.10 | 200. |
| 205. | 0.92 | 0.80 | 0.55 | 0.16 | -0.39 | 0.12 | 0.09 | 205. |
| 210. | -0.21 | 0.11 | 0.14 | 0.07 | -0.14 | 0.13 | 0.08 | 210. |
| 215. | -0.40 | -0.02 | 0.05 | 0.01 | -0.18 | 0.08 | 0.08 | 215. |
| 220. | -0.56 | -0.11 | -0.04 | -0.05 | -0.21 | 0.07 | 0.08 | 220. |
| 225. | -0.69 | -0.19 | -0.11 | -0.09 | -0.25 | 0.05 | 0.07 | 225. |
| 230. | -0.81 | -0.26 | -0.19 | -0.13 | -0.28 | 0.02 | 0.06 | 230. |
| 235. | -0.92 | -0.34 | -0.23 | -0.16 | -0.32 | 0.00 | 0.05 | 235. |
| 240. | -1.00 | -0.41 | -0.29 | -0.19 | -0.34 | -0.02 | 0.04 | 240. |
| 245. | -1.09 | -0.47 | -0.31 | -0.22 | -0.37 | -0.03 | 0.03 | 245. |
| 250. | -1.16 | -0.49 | -0.34 | -0.25 | -0.39 | -0.03 | 0.02 | 250. |
| 255. | -1.17 | -0.49 | -0.35 | -0.26 | -0.41 | -0.04 | 0.02 | 255. |
| 260. | -1.15 | -0.48 | -0.35 | -0.26 | -0.41 | -0.04 | 0.02 | 260. |
| 265. | -1.12 | -0.47 | -0.35 | -0.26 | -0.40 | -0.03 | 0.03 | 265. |
| 270. | -1.13 | -0.47 | -0.34 | -0.25 | -0.39 | -0.03 | 0.04 | 270. |
| 275. | -1.13 | -0.49 | -0.33 | -0.24 | -0.38 | -0.02 | 0.04 | 275. |
| 280. | -1.14 | -0.51 | -0.32 | -0.23 | -0.38 | -0.01 | 0.04 | 280. |
| 285. | -1.16 | -0.53 | -0.31 | -0.23 | -0.37 | -0.00 | 0.05 | 285. |
| 290. | -1.17 | -0.54 | -0.31 | -0.22 | -0.37 | 0.00 | 0.05 | 290. |
| 295. | -1.18 | -0.55 | -0.31 | -0.22 | -0.36 | 0.01 | 0.05 | 295. |
| 300. | -1.19 | -0.56 | -0.31 | -0.22 | -0.36 | 0.01 | 0.06 | 300. |
| 305. | -1.19 | -0.56 | -0.31 | -0.21 | -0.36 | 0.01 | 0.06 | 305. |
| 310. | -1.18 | -0.55 | -0.30 | -0.21 | -0.35 | 0.01 | 0.06 | 310. |
| 315. | -1.15 | -0.55 | -0.28 | -0.20 | -0.35 | -0.01 | 0.05 | 315. |
| 320. | -1.12 | -0.54 | -0.25 | -0.20 | -0.33 | -0.01 | 0.05 | 320. |
| 325. | -1.01 | -0.50 | -0.22 | -0.18 | -0.32 | -0.02 | 0.03 | 325. |
| 330. | -0.91 | -0.44 | -0.18 | -0.16 | -0.29 | -0.02 | 0.02 | 330. |
| 335. | -0.75 | -0.33 | -0.15 | -0.10 | -0.26 | -0.01 | 0.02 | 335. |
| 340. | -0.58 | -0.23 | -0.10 | -0.07 | -0.22 | -0.01 | 0.01 | 340. |
| 345. | -0.44 | -0.15 | -0.13 | -0.10 | -0.23 | -0.01 | -0.00 | 345. |
| 350. | -0.11 | -0.53 | -0.32 | -0.24 | -0.31 | -0.08 | -0.05 | 350. |
| 355. | -1.04 | -1.27 | -0.77 | -0.55 | -0.49 | -0.16 | -0.08 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-497 CWTR NO. 256 TCM= 48. C.R.= 25.8

DIFFERENTIAL PRESSURES

SPAN STATION 193.3

| AZ | CHORD STATION | | | | | | AZ |
|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.840 | 1.959 | 2.990 | 4.230 | 7.150 | 10.430 | DEG. |
| 0. | -0.33 | -0.25 | -0.44 | -0.30 | 0.0 | -0.07 | -0.02 | 0. |
| 5. | -0.63 | -0.07 | -0.37 | -0.46 | 0.0 | -0.13 | -0.02 | 5. |
| 10. | -1.92 | -0.69 | -0.81 | -0.57 | 0.0 | -0.15 | -0.02 | 10. |
| 15. | -0.37 | -0.98 | -0.86 | -0.43 | 0.0 | -0.12 | -0.02 | 15. |
| 20. | 0.99 | -0.81 | -0.94 | -0.21 | 0.0 | -0.07 | -0.01 | 20. |
| 25. | 1.18 | 0.41 | -0.26 | 0.02 | 0.0 | -0.05 | 0.00 | 25. |
| 30. | 1.45 | 0.76 | -0.16 | 0.26 | 0.0 | 0.02 | 0.01 | 30. |
| 35. | 1.72 | 1.00 | 0.30 | 0.53 | 0.0 | 0.04 | 0.00 | 35. |
| 40. | 1.99 | 1.40 | 0.05 | 0.77 | 0.0 | 0.07 | 0.00 | 40. |
| 45. | 2.17 | 1.63 | 1.02 | 0.94 | 0.0 | 0.07 | 0.01 | 45. |
| 50. | 2.20 | 1.73 | 1.09 | 1.03 | 0.0 | 0.10 | 0.02 | 50. |
| 55. | 2.09 | 1.69 | 1.07 | 1.04 | 0.0 | 0.12 | 0.03 | 55. |
| 60. | 1.79 | 1.51 | 0.94 | 1.04 | 0.0 | 0.06 | 0.02 | 60. |
| 65. | 1.41 | 1.28 | 0.74 | 0.98 | 0.0 | -0.04 | -0.03 | 65. |
| 70. | 1.98 | 1.04 | 0.47 | 0.88 | 0.0 | -0.13 | -0.05 | 70. |
| 75. | 0.59 | 0.74 | 0.14 | 0.74 | 0.0 | -0.19 | -0.04 | 75. |
| 80. | 0.19 | 0.41 | -0.17 | 0.61 | 0.0 | -0.25 | -0.03 | 80. |
| 85. | -0.12 | 0.15 | -0.39 | 0.55 | 0.0 | -0.32 | -0.05 | 85. |
| 90. | -0.24 | 0.02 | -0.48 | 0.60 | 0.0 | -0.34 | -0.00 | 90. |
| 95. | -0.15 | 0.05 | -0.41 | 0.69 | 0.0 | -0.30 | -0.01 | 95. |
| 100. | -0.22 | -0.09 | -0.33 | 0.54 | 0.0 | -0.24 | -0.09 | 100. |
| 105. | -0.91 | -0.39 | -0.42 | 0.24 | 0.0 | -0.21 | -0.08 | 105. |
| 110. | -0.84 | -0.57 | -0.59 | 0.27 | 0.0 | -0.26 | -0.13 | 110. |
| 115. | -0.97 | -0.64 | -0.74 | -0.05 | 0.0 | -0.31 | -0.12 | 115. |
| 120. | -1.03 | -0.72 | -0.85 | -0.12 | 0.0 | -0.32 | -0.12 | 120. |
| 125. | -1.22 | -0.80 | -0.92 | -0.18 | 0.0 | -0.32 | -0.12 | 125. |
| 130. | -1.39 | -1.00 | -0.96 | -0.26 | 0.0 | -0.32 | -0.13 | 130. |
| 135. | -1.52 | -1.06 | -0.96 | -0.32 | 0.0 | -0.30 | -0.13 | 135. |
| 140. | -1.56 | -1.06 | -0.90 | -0.31 | 0.0 | -0.26 | -0.11 | 140. |
| 145. | -1.43 | -0.95 | -0.76 | -0.25 | 0.0 | -0.23 | -0.09 | 145. |
| 150. | -1.15 | -0.73 | -0.52 | -0.15 | 0.0 | -0.13 | -0.06 | 150. |
| 155. | -0.78 | -0.34 | -0.27 | -0.02 | 0.0 | -0.06 | -0.03 | 155. |
| 160. | -0.37 | 0.31 | -0.02 | 0.11 | 0.0 | 0.01 | -0.00 | 160. |
| 165. | 0.05 | 0.59 | 0.22 | 0.22 | 0.0 | 0.07 | 0.02 | 165. |
| 170. | 0.39 | 0.69 | 0.40 | 0.30 | 0.0 | 0.12 | 0.02 | 170. |
| 175. | 0.62 | 0.84 | 0.53 | 0.35 | 0.0 | 0.15 | 0.02 | 175. |
| 180. | 0.72 | 0.90 | 0.62 | 0.35 | 0.0 | 0.17 | 0.02 | 180. |
| 185. | 0.74 | 0.91 | 0.63 | 0.31 | 0.0 | 0.17 | 0.02 | 185. |
| 190. | 0.70 | 0.84 | 0.61 | 0.29 | 0.0 | 0.16 | 0.02 | 190. |
| 195. | 0.62 | 0.79 | 0.55 | 0.19 | 0.0 | 0.15 | 0.02 | 195. |
| 200. | 0.52 | 0.73 | 0.49 | 0.12 | 0.0 | 0.14 | 0.03 | 200. |
| 205. | 0.41 | 0.26 | 0.45 | 0.05 | 0.0 | 0.17 | 0.04 | 205. |
| 210. | 0.31 | 0.17 | 0.41 | -0.01 | 0.0 | 0.17 | 0.05 | 210. |
| 215. | 0.21 | 0.08 | 0.37 | -0.07 | 0.0 | 0.17 | 0.06 | 215. |
| 220. | 0.13 | -0.01 | 0.33 | -0.11 | 0.0 | 0.17 | 0.06 | 220. |
| 225. | 0.05 | -0.09 | 0.33 | -0.14 | 0.0 | 0.17 | 0.06 | 225. |
| 230. | -0.02 | -0.15 | 0.27 | -0.17 | 0.0 | 0.16 | 0.05 | 230. |
| 235. | -0.10 | -0.19 | 0.26 | -0.22 | 0.0 | 0.15 | 0.05 | 235. |
| 240. | -0.19 | -0.22 | 0.21 | -0.26 | 0.0 | 0.14 | 0.04 | 240. |
| 245. | -0.27 | -0.26 | 0.18 | -0.31 | 0.0 | 0.13 | 0.03 | 245. |
| 250. | -0.35 | -0.30 | 0.15 | -0.36 | 0.0 | 0.12 | 0.03 | 250. |
| 255. | -0.40 | -0.35 | 0.11 | -0.40 | 0.0 | 0.11 | 0.02 | 255. |
| 260. | -0.43 | -0.39 | 0.08 | -0.44 | 0.0 | 0.10 | 0.02 | 260. |
| 265. | -0.44 | -0.42 | 0.05 | -0.45 | 0.0 | 0.10 | 0.02 | 265. |
| 270. | -0.44 | -0.44 | 0.03 | -0.45 | 0.0 | 0.11 | 0.03 | 270. |
| 275. | -0.51 | -0.45 | 0.02 | -0.44 | 0.0 | 0.11 | 0.04 | 275. |
| 280. | -0.51 | -0.44 | 0.02 | -0.43 | 0.0 | 0.12 | 0.05 | 280. |
| 285. | -0.47 | -0.42 | 0.04 | -0.41 | 0.0 | 0.14 | 0.07 | 285. |
| 290. | -0.41 | -0.37 | 0.06 | -0.39 | 0.0 | 0.16 | 0.09 | 290. |
| 295. | -0.33 | -0.32 | 0.08 | -0.37 | 0.0 | 0.16 | 0.10 | 295. |
| 300. | -0.24 | -0.26 | 0.11 | -0.33 | 0.0 | 0.17 | 0.10 | 300. |
| 305. | -0.15 | -0.20 | 0.16 | -0.29 | 0.0 | 0.16 | 0.10 | 305. |
| 310. | -0.06 | -0.15 | 0.20 | -0.26 | 0.0 | 0.15 | 0.09 | 310. |
| 315. | 0.02 | -0.12 | 0.21 | -0.25 | 0.0 | 0.14 | 0.08 | 315. |
| 320. | 0.10 | -0.12 | 0.19 | -0.29 | 0.0 | 0.13 | 0.06 | 320. |
| 325. | 0.06 | -0.22 | 0.08 | -0.39 | 0.0 | 0.11 | 0.03 | 325. |
| 330. | -0.04 | -0.40 | -0.12 | -0.44 | 0.0 | 0.05 | 0.04 | 330. |
| 335. | -0.07 | -0.62 | -0.28 | -0.53 | 0.0 | -0.09 | 0.02 | 335. |
| 340. | -0.17 | -0.58 | -0.26 | -0.55 | 0.0 | -0.03 | -0.01 | 340. |
| 345. | -0.27 | -0.39 | -0.14 | -0.44 | 0.0 | -0.01 | -0.01 | 345. |
| 350. | -0.23 | -0.40 | -0.18 | -0.45 | 0.0 | -0.01 | -0.01 | 350. |
| 355. | -0.42 | -0.42 | -0.25 | -0.49 | 0.0 | -0.04 | -0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-497 CNTR NO. 296 TCM= 48. C.G.= 25.3

DIFFERENTIAL PRESSURES

SPAN STATION 178.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 2.499 | 1.248 | 1.998 | 2.998 | 4.550 | 7.199 | 10.498 | DEG. |
| 0. | -0.28 | -0.01 | -0.16 | -0.93 | -0.96 | -0.06 | -0.02 | 0. |
| 5. | -0.03 | 0.11 | -0.09 | 0.32 | -0.01 | -0.04 | 0.01 | 5. |
| 10. | -0.09 | -0.05 | -0.15 | -0.33 | -0.37 | -0.06 | -0.00 | 10. |
| 15. | 0.07 | 0.04 | -0.11 | -0.02 | -0.05 | -0.04 | 0.01 | 15. |
| 20. | 0.57 | 0.29 | 0.10 | 0.07 | 0.07 | -0.01 | 0.03 | 20. |
| 25. | 1.06 | 0.44 | 0.25 | 0.19 | 0.14 | 0.05 | 0.04 | 25. |
| 30. | 1.49 | 0.55 | 0.44 | 0.32 | 0.23 | 0.13 | 0.06 | 30. |
| 35. | 1.75 | 0.65 | 0.71 | 0.48 | 0.38 | 0.22 | 0.09 | 35. |
| 40. | 1.93 | 0.74 | 0.87 | 0.65 | 0.54 | 0.31 | 0.13 | 40. |
| 45. | 2.05 | 0.74 | 0.91 | 0.80 | 0.71 | 0.38 | 0.13 | 45. |
| 50. | 2.01 | 0.57 | 1.16 | 1.01 | 0.79 | 0.43 | 0.11 | 50. |
| 55. | 1.82 | 0.31 | 1.47 | 1.48 | 0.81 | 0.35 | 0.08 | 55. |
| 60. | 1.55 | 0.05 | 1.69 | 1.19 | 1.18 | 0.26 | 0.04 | 60. |
| 65. | 1.22 | -0.17 | 1.66 | 0.91 | 1.43 | 0.11 | -0.01 | 65. |
| 70. | 0.85 | -0.39 | 1.03 | 0.43 | 1.58 | -0.17 | -0.06 | 70. |
| 75. | 0.47 | -0.59 | 0.24 | 0.36 | 0.95 | -0.44 | -0.10 | 75. |
| 80. | 0.05 | -0.78 | -0.51 | 0.15 | 0.36 | -0.54 | -0.11 | 80. |
| 85. | -0.48 | -0.96 | -1.01 | 0.11 | -0.53 | -0.73 | -0.08 | 85. |
| 90. | -0.96 | -1.12 | -1.24 | -0.16 | -0.92 | -0.96 | 0.03 | 90. |
| 95. | -1.26 | -1.23 | -1.26 | -0.43 | -1.13 | -1.19 | 0.18 | 95. |
| 100. | -1.38 | -1.21 | -1.14 | -0.65 | -1.23 | -1.38 | 0.12 | 100. |
| 105. | -1.17 | -1.11 | -1.02 | -0.63 | -1.09 | -0.62 | 0.10 | 105. |
| 110. | -1.02 | -1.07 | -1.08 | -0.63 | -1.06 | -0.12 | 0.06 | 110. |
| 115. | -1.06 | -1.08 | -1.24 | -0.67 | -1.28 | 0.22 | 0.03 | 115. |
| 120. | -1.18 | -1.13 | -1.19 | -0.85 | -2.93 | 0.29 | -0.00 | 120. |
| 125. | -1.42 | -1.23 | -1.59 | -1.44 | -2.57 | 0.18 | -0.03 | 125. |
| 130. | -1.81 | -1.36 | -2.15 | -2.16 | -0.78 | -0.22 | -0.05 | 130. |
| 135. | -2.19 | -1.50 | -2.65 | -2.18 | -0.38 | -3.16 | -0.07 | 135. |
| 140. | -2.41 | -1.48 | -2.72 | -1.63 | -0.28 | -0.21 | -0.07 | 140. |
| 145. | -2.61 | -1.33 | -2.67 | -1.18 | -0.01 | -3.25 | -0.06 | 145. |
| 150. | -2.19 | -1.11 | -2.63 | -1.09 | -0.72 | -0.15 | -0.03 | 150. |
| 155. | -1.87 | -0.84 | -1.84 | -0.92 | -0.53 | -0.08 | -0.03 | 155. |
| 160. | -1.98 | -0.56 | -1.25 | -0.72 | -0.37 | -2.01 | -0.02 | 160. |
| 165. | -1.87 | -0.33 | -0.88 | -3.92 | -0.22 | 0.06 | -0.00 | 165. |
| 170. | -0.94 | -0.11 | -0.53 | -0.37 | -0.07 | 0.12 | 0.01 | 170. |
| 175. | -0.87 | 0.08 | -0.24 | -0.23 | 0.03 | 0.15 | 0.02 | 175. |
| 180. | 0.17 | 0.24 | 0.03 | -0.13 | 0.11 | 0.16 | 0.02 | 180. |
| 185. | 0.31 | 0.36 | 0.17 | -0.25 | 0.16 | 0.17 | 0.01 | 185. |
| 190. | 0.41 | 0.45 | 0.29 | 0.31 | 0.19 | 0.16 | 0.01 | 190. |
| 195. | 0.45 | 0.44 | 0.37 | 0.36 | 0.19 | 0.15 | -0.00 | 195. |
| 200. | 0.44 | 0.41 | 0.42 | 0.09 | 0.20 | 0.14 | -0.01 | 200. |
| 205. | 0.40 | 0.39 | 0.45 | 0.12 | 0.19 | 0.13 | -0.02 | 205. |
| 210. | 0.32 | 0.42 | 0.45 | 0.13 | 0.20 | 0.13 | -0.01 | 210. |
| 215. | 0.25 | 0.47 | 0.45 | 0.15 | 0.20 | 0.13 | -0.01 | 215. |
| 220. | 0.23 | 0.49 | 0.47 | 0.17 | 0.21 | 0.13 | -0.01 | 220. |
| 225. | 0.21 | 0.50 | 0.48 | 0.18 | 0.22 | 0.13 | -0.01 | 225. |
| 230. | 0.19 | 0.50 | 0.50 | 0.20 | 0.23 | 0.13 | -0.01 | 230. |
| 235. | 0.19 | 0.50 | 0.53 | 0.21 | 0.24 | 0.13 | -0.01 | 235. |
| 240. | 0.18 | 0.49 | 0.50 | 0.23 | 0.25 | 0.13 | -0.01 | 240. |
| 245. | 0.18 | 0.48 | 0.61 | 0.23 | 0.25 | 0.12 | -0.02 | 245. |
| 250. | 0.18 | 0.48 | 0.63 | 0.24 | 0.25 | 0.13 | -0.02 | 250. |
| 255. | 0.18 | 0.47 | 0.63 | 0.25 | 0.25 | 0.09 | -0.03 | 255. |
| 260. | 0.16 | 0.47 | 0.63 | 0.24 | 0.25 | 0.09 | -0.03 | 260. |
| 265. | 0.14 | 0.47 | 0.61 | 0.24 | 0.25 | 0.09 | -0.04 | 265. |
| 270. | 0.14 | 0.47 | 0.60 | 0.25 | 0.25 | 0.09 | -0.04 | 270. |
| 275. | 0.14 | 0.47 | 0.59 | 0.25 | 0.25 | 0.10 | -0.04 | 275. |
| 280. | 0.16 | 0.48 | 0.59 | 0.26 | 0.26 | 0.11 | -0.03 | 280. |
| 285. | 0.19 | 0.49 | 0.60 | 0.28 | 0.27 | 0.13 | -0.02 | 285. |
| 290. | 0.25 | 0.50 | 0.62 | 0.31 | 0.28 | 0.14 | -0.01 | 290. |
| 295. | 0.32 | 0.52 | 0.64 | 0.34 | 0.30 | 0.15 | -0.00 | 295. |
| 300. | 0.40 | 0.55 | 0.66 | 0.37 | 0.31 | 0.16 | 0.01 | 300. |
| 305. | 0.50 | 0.57 | 0.69 | 0.38 | 0.32 | 0.16 | 0.01 | 305. |
| 310. | 0.60 | 0.59 | 0.71 | 0.39 | 0.34 | 0.16 | 0.01 | 310. |
| 315. | 0.68 | 0.61 | 0.72 | 0.40 | 0.34 | 0.17 | 0.01 | 315. |
| 320. | 0.74 | 0.62 | 0.72 | 0.40 | 0.34 | 0.16 | 0.01 | 320. |
| 325. | 0.76 | 0.63 | 0.73 | 0.41 | 0.34 | 0.16 | 0.01 | 325. |
| 330. | 0.77 | 0.58 | 0.86 | 0.43 | 0.32 | 0.15 | 0.01 | 330. |
| 335. | 0.58 | 0.45 | 0.65 | 0.38 | 0.26 | -0.01 | -0.00 | 335. |
| 340. | 0.09 | 0.25 | 0.19 | 0.18 | 0.12 | -0.37 | -0.02 | 340. |
| 345. | -0.44 | 0.12 | -0.15 | -0.04 | -0.06 | -0.12 | -0.04 | 345. |
| 350. | -0.74 | 0.10 | -0.28 | -0.14 | -0.15 | -0.13 | -0.05 | 350. |
| 355. | -0.83 | -0.16 | -0.28 | -0.18 | -0.13 | -0.16 | -0.05 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=497 UNIT NO. 256 TC%= 46. C.R.= 25.3

DIFFERENTIAL PRESSURES

SPAN STATION 149.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.995 | 4.559 | 7.159 | 13.450 | DEG. |
| 0. | -3.30 | -0.04 | -3.23 | 0.20 | 0.98 | 0.17 | 0.03 | 0. |
| 5. | 0.35 | 0.43 | 0.23 | 0.36 | 0.35 | 0.25 | 0.05 | 5. |
| 10. | 0.36 | 0.30 | 0.19 | 0.28 | 0.36 | 0.23 | 0.04 | 10. |
| 15. | 0.33 | 0.24 | 0.11 | 0.20 | 0.37 | 0.18 | 0.04 | 15. |
| 20. | 0.27 | 0.54 | 0.11 | 0.26 | 0.44 | 0.18 | 0.05 | 20. |
| 25. | 1.29 | 0.84 | 0.32 | 0.38 | 0.45 | 0.18 | 0.07 | 25. |
| 30. | 1.61 | 1.02 | 0.65 | 0.55 | 0.64 | 0.24 | 0.09 | 30. |
| 35. | 1.92 | 1.19 | 1.05 | 0.80 | 0.93 | 0.41 | 0.11 | 35. |
| 40. | 2.02 | 1.30 | 1.02 | 0.99 | 1.20 | 0.37 | 0.12 | 40. |
| 45. | 2.13 | 1.31 | 2.12 | 1.43 | 1.37 | 0.36 | 0.11 | 45. |
| 50. | 2.04 | 1.11 | 2.32 | 2.16 | 1.52 | 0.28 | 0.07 | 50. |
| 55. | 1.78 | 0.83 | 2.05 | 1.78 | 2.28 | 0.13 | 0.01 | 55. |
| 60. | 1.47 | 0.62 | 1.61 | 1.03 | 2.73 | -0.35 | -0.07 | 60. |
| 65. | 1.06 | 0.38 | 1.22 | 0.29 | 2.20 | -0.17 | -0.15 | 65. |
| 70. | 0.51 | 0.05 | 1.11 | -0.20 | 1.26 | -0.18 | -0.23 | 70. |
| 75. | -0.19 | -0.38 | 1.04 | -0.66 | 0.69 | -0.10 | -0.25 | 75. |
| 80. | -0.93 | -0.85 | 0.69 | -0.72 | -0.35 | -0.07 | -0.19 | 80. |
| 85. | -1.57 | -1.34 | 0.17 | -0.98 | -0.54 | -0.76 | -0.10 | 85. |
| 90. | -2.14 | -1.76 | -0.25 | -1.17 | -1.01 | -0.59 | 0.03 | 90. |
| 95. | -2.44 | -1.90 | -0.53 | -1.28 | -1.03 | -2.79 | 0.23 | 95. |
| 100. | -2.45 | -1.87 | -0.62 | -1.26 | -0.86 | -1.47 | 0.02 | 100. |
| 105. | -2.31 | -1.80 | -0.62 | -1.18 | -0.82 | -0.45 | 0.07 | 105. |
| 110. | -2.12 | -1.43 | -0.69 | -1.17 | -0.78 | -0.56 | 0.18 | 110. |
| 115. | -2.30 | -1.87 | -0.92 | -1.29 | -0.68 | -0.83 | 0.25 | 115. |
| 120. | -2.12 | -1.89 | -1.26 | -1.39 | -0.81 | -0.55 | 0.22 | 120. |
| 125. | -2.25 | -1.97 | -1.11 | -1.49 | -2.36 | -0.15 | 0.13 | 125. |
| 130. | -2.51 | -2.16 | -1.49 | -2.36 | -2.93 | 0.45 | 0.04 | 130. |
| 135. | -2.91 | -2.33 | -2.16 | -3.30 | -1.42 | 0.19 | -0.05 | 135. |
| 140. | -3.22 | -2.93 | -2.62 | -3.38 | -0.38 | -0.10 | -0.19 | 140. |
| 145. | -3.36 | -2.93 | -2.72 | -1.97 | -0.21 | -0.23 | -0.19 | 145. |
| 150. | -3.25 | -2.62 | -2.42 | -1.25 | -0.56 | -0.18 | -0.20 | 150. |
| 155. | -2.91 | -2.10 | -1.97 | -1.93 | -0.51 | -0.10 | -0.07 | 155. |
| 160. | -2.35 | -1.56 | -1.51 | -0.80 | -0.39 | -0.31 | -0.05 | 160. |
| 165. | -1.70 | -1.02 | -1.16 | -0.59 | -0.25 | 0.37 | -0.03 | 165. |
| 170. | -1.06 | -0.53 | -0.70 | -0.28 | -0.12 | 0.15 | -0.02 | 170. |
| 175. | -0.48 | -0.12 | -0.45 | -0.06 | 0.00 | 0.21 | -0.02 | 175. |
| 180. | -0.10 | 0.22 | -0.17 | 0.12 | 0.16 | 0.24 | -0.02 | 180. |
| 185. | 0.33 | 0.47 | 0.13 | 0.23 | 0.26 | 0.25 | -0.03 | 185. |
| 190. | 0.51 | 0.63 | 0.45 | 0.29 | 0.33 | 0.26 | -0.04 | 190. |
| 195. | 0.60 | 0.69 | 0.49 | 0.32 | 0.31 | 0.25 | -0.05 | 195. |
| 200. | 0.60 | 0.67 | 0.12 | 0.33 | -0.01 | 0.24 | -0.05 | 200. |
| 205. | 0.56 | 0.62 | 0.13 | 0.33 | -0.03 | 0.26 | -0.05 | 205. |
| 210. | 0.53 | 0.62 | 0.13 | 0.33 | -0.05 | 0.27 | -0.04 | 210. |
| 215. | 0.54 | 0.63 | 0.12 | 0.34 | -0.06 | 0.29 | -0.03 | 215. |
| 220. | 0.56 | 0.64 | 0.12 | 0.35 | -0.07 | 0.30 | -0.02 | 220. |
| 225. | 0.59 | 0.66 | 0.14 | 0.36 | -0.08 | 0.31 | -0.02 | 225. |
| 230. | 0.60 | 0.67 | 0.16 | 0.39 | -0.08 | 0.31 | -0.01 | 230. |
| 235. | 0.62 | 0.69 | 0.19 | 0.43 | -0.08 | 0.31 | -0.01 | 235. |
| 240. | 0.64 | 0.72 | 0.19 | 0.47 | -0.09 | 0.31 | -0.01 | 240. |
| 245. | 0.67 | 0.74 | 0.20 | 0.50 | -0.09 | 0.31 | -0.02 | 245. |
| 250. | 0.71 | 0.77 | 0.22 | 0.53 | -0.09 | 0.32 | -0.03 | 250. |
| 255. | 0.75 | 0.79 | 0.20 | 0.53 | -0.10 | 0.32 | -0.03 | 255. |
| 260. | 0.76 | 0.79 | 0.22 | 0.53 | -0.10 | 0.32 | -0.03 | 260. |
| 265. | 0.77 | 0.79 | 0.23 | 0.53 | -0.10 | 0.32 | -0.03 | 265. |
| 270. | 0.78 | 0.80 | 0.21 | 0.52 | -0.09 | 0.32 | -0.03 | 270. |
| 275. | 0.79 | 0.81 | 0.23 | 0.53 | -0.09 | 0.33 | -0.02 | 275. |
| 280. | 0.80 | 0.84 | 0.26 | 0.53 | -0.08 | 0.33 | -0.01 | 280. |
| 285. | 0.81 | 0.87 | 0.29 | 0.55 | -0.07 | 0.32 | 0.00 | 285. |
| 290. | 0.86 | 0.92 | 0.33 | 0.59 | -0.06 | 0.34 | 0.01 | 290. |
| 295. | 0.95 | 0.99 | 0.39 | 0.64 | -0.03 | 0.34 | 0.02 | 295. |
| 300. | 1.10 | 1.07 | 0.46 | 0.68 | 0.03 | 0.34 | 0.03 | 300. |
| 305. | 1.26 | 1.13 | 0.51 | 0.71 | 0.20 | 0.33 | 0.03 | 305. |
| 310. | 1.38 | 1.18 | 0.55 | 0.74 | 0.29 | 0.33 | 0.04 | 310. |
| 315. | 1.47 | 1.22 | 0.58 | 0.75 | 0.33 | 0.33 | 0.04 | 315. |
| 320. | 1.54 | 1.19 | 0.59 | 0.77 | 0.31 | 0.33 | 0.04 | 320. |
| 325. | 1.58 | 1.16 | 0.54 | 0.77 | 0.32 | 0.33 | 0.04 | 325. |
| 330. | 1.55 | 1.12 | 0.47 | 0.75 | 0.30 | 0.33 | 0.04 | 330. |
| 335. | 1.45 | 1.07 | 0.43 | 0.70 | 0.31 | 0.32 | 0.04 | 335. |
| 340. | 1.39 | 0.89 | 0.25 | 0.54 | 0.31 | 0.31 | 0.02 | 340. |
| 345. | 0.91 | 0.86 | -0.19 | 0.23 | -0.31 | 0.30 | -0.01 | 345. |
| 350. | -0.36 | -0.47 | -0.66 | 0.01 | -0.28 | 0.29 | -0.04 | 350. |
| 355. | -0.67 | -0.71 | -0.82 | 0.01 | -0.16 | 0.30 | -0.03 | 355. |

TEXT NOT REPRODUCIBLE

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=497 CNTR NO. 256 TCP= 40. C.R.= 25.9

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 3.455 | 1.040 | 1.957 | 2.390 | 4.552 | 7.159 | 13.434 | DEG |
| 0. | -3.47 | -3.20 | -3.47 | -3.12 | -0.76 | -3.37 | -0.03 | 0. |
| 5. | 3.71 | 2.53 | 3.65 | 0.24 | 0.17 | 3.36 | 0.30 | 5. |
| 10. | 0.57 | 0.32 | -0.15 | 0.13 | 0.14 | -0.11 | -0.01 | 10. |
| 15. | 0.52 | 0.53 | -0.19 | 0.05 | 0.12 | -0.10 | -0.03 | 15. |
| 20. | 3.93 | 0.06 | -3.11 | 0.12 | 0.16 | -0.13 | -0.03 | 20. |
| 25. | 1.37 | 1.05 | 0.19 | 0.24 | 0.26 | -0.13 | -0.01 | 25. |
| 30. | 1.71 | 1.10 | 0.06 | 0.39 | 0.44 | -0.14 | 0.04 | 30. |
| 35. | 1.96 | 1.23 | 1.36 | 0.49 | 0.58 | -0.13 | 0.09 | 35. |
| 40. | 2.12 | 1.55 | 1.03 | 1.45 | 0.64 | -0.15 | 0.09 | 40. |
| 45. | 2.19 | 1.99 | 1.92 | 2.36 | 0.91 | -0.17 | 0.03 | 45. |
| 50. | 2.11 | 2.26 | 1.71 | 2.52 | 1.37 | -0.19 | 0.05 | 50. |
| 55. | 1.84 | 2.07 | 1.48 | 2.33 | 2.20 | -0.51 | -0.14 | 55. |
| 60. | 1.47 | 1.65 | 1.29 | 1.84 | 1.58 | -0.31 | -0.23 | 60. |
| 65. | 1.02 | 1.16 | 1.24 | 0.33 | 1.39 | 0.39 | -0.29 | 65. |
| 70. | 0.43 | 0.67 | 1.12 | -0.21 | 0.63 | 0.13 | -0.27 | 70. |
| 75. | -0.39 | -0.23 | 0.74 | -0.52 | 0.16 | -0.39 | -0.12 | 75. |
| 80. | -1.26 | -1.34 | 0.29 | -1.07 | -0.24 | -1.03 | 0.02 | 80. |
| 85. | -2.31 | -1.93 | -0.16 | -1.32 | -0.55 | -0.96 | -0.29 | 85. |
| 90. | -2.54 | -2.14 | -0.35 | -1.41 | -0.73 | 0.12 | -0.35 | 90. |
| 95. | -2.60 | -2.17 | -0.41 | -1.36 | -0.76 | 1.16 | -0.01 | 95. |
| 100. | -2.49 | -2.09 | -0.45 | -1.22 | -0.76 | 1.28 | -0.47 | 100. |
| 105. | -2.42 | -1.95 | -0.49 | -1.13 | -0.77 | 1.43 | -0.14 | 105. |
| 110. | -2.36 | -1.48 | -0.48 | -1.07 | -0.82 | 1.13 | 0.24 | 110. |
| 115. | -2.34 | -1.86 | -0.43 | -1.03 | -0.93 | -0.42 | 0.32 | 115. |
| 120. | -2.37 | -1.87 | -0.38 | -0.97 | -1.15 | -1.19 | 0.33 | 120. |
| 125. | -2.44 | -1.92 | -0.43 | -1.14 | -1.39 | -0.65 | 0.27 | 125. |
| 130. | -2.75 | -2.02 | -0.61 | -1.69 | -2.30 | 2.32 | 0.15 | 130. |
| 135. | -3.47 | -2.22 | -1.14 | -2.61 | -2.68 | 3.39 | 0.08 | 135. |
| 140. | -3.97 | -2.49 | -2.11 | -3.08 | -1.11 | -0.29 | 0.09 | 140. |
| 145. | -3.57 | -2.75 | -2.58 | -2.54 | -0.95 | -3.55 | 0.09 | 145. |
| 150. | -3.53 | -2.83 | -2.56 | -1.24 | -0.42 | -2.57 | 0.07 | 150. |
| 155. | -3.19 | -2.55 | -2.22 | -0.95 | -0.45 | -0.46 | 0.04 | 155. |
| 160. | -2.70 | -2.09 | -1.77 | -0.81 | -0.43 | -1.39 | 0.03 | 160. |
| 165. | -2.14 | -1.54 | -1.34 | -0.69 | -0.31 | -2.33 | 0.05 | 165. |
| 170. | -1.52 | -0.98 | -0.95 | -0.44 | -0.15 | -0.22 | 0.07 | 170. |
| 175. | -0.41 | -0.53 | -0.01 | -0.20 | -0.14 | -0.14 | 0.08 | 175. |
| 180. | -0.17 | -0.17 | -0.34 | -0.14 | 0.03 | -0.38 | 0.08 | 180. |
| 185. | 0.27 | 0.09 | -0.14 | 0.07 | 0.08 | -0.14 | 0.07 | 185. |
| 190. | 0.49 | 0.27 | -0.02 | 0.14 | 0.11 | -0.31 | 0.06 | 190. |
| 195. | 0.55 | 0.37 | -0.03 | 0.20 | 0.11 | 0.71 | 0.04 | 195. |
| 200. | 0.56 | 0.42 | -0.03 | 0.24 | 0.10 | 0.72 | 0.03 | 200. |
| 205. | 0.56 | 0.43 | -0.02 | 0.27 | 0.08 | 0.70 | 0.03 | 205. |
| 210. | 0.54 | 0.40 | -0.03 | 0.30 | 0.10 | 0.36 | 0.02 | 210. |
| 215. | 0.51 | 0.37 | 0.01 | 0.32 | 0.09 | 0.04 | 0.02 | 215. |
| 220. | 0.50 | 0.36 | 0.04 | 0.34 | 0.09 | 0.13 | 0.03 | 220. |
| 225. | 0.54 | 0.37 | 0.06 | 0.36 | 0.10 | 0.12 | 0.03 | 225. |
| 230. | 0.61 | 0.41 | 0.06 | 0.37 | 0.11 | 0.14 | 0.03 | 230. |
| 235. | 0.69 | 0.45 | 0.13 | 0.38 | 0.12 | 0.17 | 0.04 | 235. |
| 240. | 0.73 | 0.51 | 0.19 | 0.41 | 0.12 | 0.19 | 0.04 | 240. |
| 245. | 0.76 | 0.56 | 0.25 | 0.44 | 0.13 | 0.23 | 0.05 | 245. |
| 250. | 0.78 | 0.61 | 0.26 | 0.46 | 0.13 | 0.21 | 0.05 | 250. |
| 255. | 0.80 | 0.65 | 0.26 | 0.48 | 0.13 | 0.21 | 0.06 | 255. |
| 260. | 0.82 | 0.66 | 0.21 | 0.49 | 0.13 | 0.20 | 0.06 | 260. |
| 265. | 0.85 | 0.67 | 0.21 | 0.50 | 0.13 | 0.19 | 0.06 | 265. |
| 270. | 0.88 | 0.69 | 0.22 | 0.51 | 0.14 | 0.19 | 0.07 | 270. |
| 275. | 0.93 | 0.71 | 0.25 | 0.51 | 0.15 | 0.20 | 0.07 | 275. |
| 280. | 0.97 | 0.75 | 0.27 | 0.52 | 0.16 | 0.20 | 0.07 | 280. |
| 285. | 1.07 | 0.85 | 0.31 | 0.55 | 0.19 | 0.21 | 0.07 | 285. |
| 290. | 1.17 | 0.98 | 0.35 | 0.57 | 0.19 | 0.22 | 0.07 | 290. |
| 295. | 1.29 | 0.97 | 0.39 | 0.59 | 0.21 | 0.22 | 0.07 | 295. |
| 300. | 1.42 | 1.08 | 0.45 | 0.62 | 0.23 | 0.23 | 0.07 | 300. |
| 305. | 1.55 | 1.12 | 0.50 | 0.66 | 0.25 | 0.24 | 0.07 | 305. |
| 310. | 1.69 | 1.16 | 0.54 | 0.69 | 0.27 | 0.24 | 0.07 | 310. |
| 315. | 1.81 | 1.19 | 0.57 | 0.72 | 0.29 | 0.25 | 0.07 | 315. |
| 320. | 1.87 | 1.24 | 0.58 | 0.72 | 0.31 | 0.24 | 0.06 | 320. |
| 325. | 1.87 | 1.27 | 0.55 | 0.65 | 0.31 | 0.24 | 0.05 | 325. |
| 330. | 1.75 | 1.22 | 0.50 | 0.57 | 0.31 | 0.22 | 0.04 | 330. |
| 335. | 1.59 | 1.01 | 0.43 | 0.48 | 0.28 | 0.19 | 0.02 | 335. |
| 340. | 1.48 | 0.94 | 0.39 | 0.44 | 0.26 | 0.18 | -0.01 | 340. |
| 345. | 0.58 | 0.58 | 0.03 | 0.24 | 0.06 | 0.03 | -0.03 | 345. |
| 350. | -0.24 | -0.05 | -0.40 | -0.16 | -0.07 | -0.11 | -0.05 | 350. |
| 355. | -0.06 | -0.26 | -0.53 | -0.21 | -0.15 | -0.29 | -0.07 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-503 CNTR NO. 163 TCN= 46. C.R.= 56.0

DIFFERENTIAL PRESSURES

SPAN STATION 52.5

| AZ | CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.499 | 1.990 | 4.990 | 10.403 | DEG. |
| 0. | -1.07 | -0.48 | -0.26 | 0.00 | 0. |
| 5. | -1.01 | -0.43 | -0.18 | 0.04 | 5. |
| 10. | -0.65 | -0.30 | -0.08 | 0.04 | 10. |
| 15. | -0.38 | -0.20 | -0.03 | 0.05 | 15. |
| 20. | -0.18 | -0.12 | -0.07 | 0.02 | 20. |
| 25. | -0.21 | -0.09 | -0.05 | -0.01 | 25. |
| 30. | -0.58 | -0.21 | -0.08 | 0.00 | 30. |
| 35. | -0.62 | -0.27 | -0.06 | 0.01 | 35. |
| 40. | -0.33 | -0.13 | -0.03 | -0.01 | 40. |
| 45. | -0.23 | -0.11 | -0.03 | -0.02 | 45. |
| 50. | -0.20 | -0.13 | -0.05 | -0.03 | 50. |
| 55. | -0.12 | -0.12 | -0.03 | -0.03 | 55. |
| 60. | -0.03 | -0.08 | 0.01 | -0.03 | 60. |
| 65. | 0.01 | -0.07 | 0.01 | -0.03 | 65. |
| 70. | -0.01 | -0.07 | -0.00 | -0.05 | 70. |
| 75. | -0.03 | -0.07 | -0.01 | -0.06 | 75. |
| 80. | -0.01 | -0.05 | 0.01 | -0.05 | 80. |
| 85. | 0.10 | -0.01 | 0.04 | -0.04 | 85. |
| 90. | 0.26 | 0.06 | 0.08 | -0.03 | 90. |
| 95. | 0.42 | 0.15 | 0.14 | -0.02 | 95. |
| 100. | 0.50 | 0.24 | 0.20 | -0.01 | 100. |
| 105. | 0.73 | 0.32 | 0.24 | 0.00 | 105. |
| 110. | 0.84 | 0.40 | 0.29 | 0.02 | 110. |
| 115. | 0.98 | 0.47 | 0.32 | 0.03 | 115. |
| 120. | 1.07 | 0.54 | 0.36 | 0.04 | 120. |
| 125. | 1.15 | 0.58 | 0.38 | 0.04 | 125. |
| 130. | 1.20 | 0.62 | 0.36 | 0.03 | 130. |
| 135. | 1.24 | 0.64 | 0.32 | 0.02 | 135. |
| 140. | 1.27 | 0.66 | 0.30 | 0.00 | 140. |
| 145. | 1.33 | 0.67 | 0.29 | 0.00 | 145. |
| 150. | 1.38 | 0.68 | 0.34 | 0.00 | 150. |
| 155. | 1.41 | 0.68 | 0.38 | 0.00 | 155. |
| 160. | 1.40 | 0.67 | 0.40 | 0.00 | 160. |
| 165. | 1.34 | 0.64 | 0.39 | 0.00 | 165. |
| 170. | 1.24 | 0.57 | 0.33 | 0.01 | 170. |
| 175. | 1.08 | 0.47 | 0.29 | 0.03 | 175. |
| 180. | 0.87 | 0.36 | 0.22 | 0.04 | 180. |
| 185. | 0.62 | 0.24 | 0.15 | 0.03 | 185. |
| 190. | 0.34 | 0.09 | 0.08 | 0.03 | 190. |
| 195. | 0.06 | -0.04 | -0.00 | 0.02 | 195. |
| 200. | -0.12 | -0.11 | -0.07 | 0.01 | 200. |
| 205. | -0.25 | -0.11 | -0.12 | 0.01 | 205. |
| 210. | -0.39 | -0.08 | -0.16 | 0.01 | 210. |
| 215. | -0.52 | -0.12 | -0.18 | 0.01 | 215. |
| 220. | -0.58 | -0.19 | -0.20 | -0.00 | 220. |
| 225. | -0.60 | -0.23 | -0.21 | -0.02 | 225. |
| 230. | -0.59 | -0.24 | -0.22 | -0.03 | 230. |
| 235. | -0.55 | -0.25 | -0.22 | -0.04 | 235. |
| 240. | -0.50 | -0.25 | -0.22 | -0.04 | 240. |
| 245. | -0.46 | -0.25 | -0.21 | -0.04 | 245. |
| 250. | -0.46 | -0.24 | -0.20 | -0.04 | 250. |
| 255. | -0.46 | -0.23 | -0.20 | -0.04 | 255. |
| 260. | -0.46 | -0.22 | -0.19 | -0.04 | 260. |
| 265. | -0.47 | -0.22 | -0.18 | -0.04 | 265. |
| 270. | -0.47 | -0.21 | -0.17 | -0.04 | 270. |
| 275. | -0.47 | -0.21 | -0.17 | -0.04 | 275. |
| 280. | -0.48 | -0.21 | -0.16 | -0.04 | 280. |
| 285. | -0.48 | -0.21 | -0.16 | -0.04 | 285. |
| 290. | -0.48 | -0.20 | -0.15 | -0.05 | 290. |
| 295. | -0.49 | -0.20 | -0.14 | -0.05 | 295. |
| 300. | -0.49 | -0.20 | -0.14 | -0.04 | 300. |
| 305. | -0.49 | -0.19 | -0.13 | -0.04 | 305. |
| 310. | -0.48 | -0.18 | -0.12 | -0.03 | 310. |
| 315. | -0.45 | -0.16 | -0.12 | -0.02 | 315. |
| 320. | -0.42 | -0.18 | -0.11 | -0.01 | 320. |
| 325. | -0.42 | -0.19 | -0.11 | 0.02 | 325. |
| 330. | -0.44 | -0.20 | -0.11 | 0.02 | 330. |
| 335. | -0.49 | -0.22 | -0.10 | 0.01 | 335. |
| 340. | -0.61 | -0.28 | -0.09 | 0.02 | 340. |
| 345. | -0.57 | -0.21 | -0.08 | 0.03 | 345. |
| 350. | -0.48 | -0.30 | -0.09 | 0.04 | 350. |
| 355. | -0.75 | -0.38 | -0.19 | 0.02 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 163 TCN= 46. C.R.= 56.7

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -1.48 | -1.09 | -0.86 | -0.65 | -0.37 | -0.19 | -0.05 | 0. |
| 5. | -1.60 | -1.28 | -0.83 | -0.57 | -0.38 | -0.20 | -0.04 | 5. |
| 10. | -1.13 | -0.88 | -0.59 | -0.38 | -0.29 | -0.14 | -0.01 | 10. |
| 15. | -0.86 | -0.65 | -0.42 | -0.21 | -0.18 | -0.12 | -0.03 | 15. |
| 20. | -0.47 | -0.43 | -0.33 | -0.24 | -0.13 | -0.10 | -0.03 | 20. |
| 25. | -0.73 | -0.54 | -0.45 | -0.31 | -0.16 | -0.14 | -0.04 | 25. |
| 30. | -0.83 | -0.56 | -0.49 | -0.31 | -0.12 | -0.12 | -0.02 | 30. |
| 35. | -0.55 | -0.43 | -0.38 | -0.22 | -0.06 | -0.09 | -0.01 | 35. |
| 40. | -0.31 | -0.32 | -0.33 | -0.19 | -0.05 | -0.11 | -0.04 | 40. |
| 45. | -0.19 | -0.26 | -0.27 | -0.18 | -0.04 | -0.11 | -0.04 | 45. |
| 50. | -0.14 | -0.21 | -0.27 | -0.18 | -0.02 | -0.10 | -0.03 | 50. |
| 55. | -0.12 | -0.18 | -0.27 | -0.16 | 0.01 | -0.10 | -0.03 | 55. |
| 60. | -0.12 | -0.15 | -0.25 | -0.14 | 0.02 | -0.11 | -0.03 | 60. |
| 65. | -0.08 | -0.12 | -0.20 | -0.11 | 0.03 | -0.11 | -0.04 | 65. |
| 70. | -0.01 | -0.06 | -0.14 | -0.07 | 0.06 | -0.10 | -0.04 | 70. |
| 75. | 0.08 | -0.06 | -0.08 | -0.03 | 0.09 | -0.09 | -0.03 | 75. |
| 80. | 0.20 | 0.07 | -0.02 | 0.02 | 0.13 | -0.07 | -0.02 | 80. |
| 85. | 0.34 | 0.17 | 0.04 | 0.09 | 0.18 | -0.05 | -0.01 | 85. |
| 90. | 0.49 | 0.28 | 0.12 | 0.17 | 0.23 | -0.02 | 0.00 | 90. |
| 95. | 0.65 | 0.40 | 0.21 | 0.24 | 0.28 | -0.00 | 0.01 | 95. |
| 100. | 0.82 | 0.50 | 0.31 | 0.30 | 0.32 | 0.02 | 0.02 | 100. |
| 105. | 0.99 | 0.61 | 0.40 | 0.36 | 0.35 | 0.04 | 0.03 | 105. |
| 110. | 1.15 | 0.71 | 0.48 | 0.41 | 0.36 | 0.07 | 0.04 | 110. |
| 115. | 1.30 | 0.81 | 0.56 | 0.45 | 0.41 | 0.15 | 0.06 | 115. |
| 120. | 1.44 | 0.90 | 0.63 | 0.49 | 0.44 | 0.12 | 0.07 | 120. |
| 125. | 1.56 | 0.99 | 0.69 | 0.53 | 0.46 | 0.14 | 0.08 | 125. |
| 130. | 1.68 | 1.06 | 0.75 | 0.55 | 0.48 | 0.16 | 0.09 | 130. |
| 135. | 1.78 | 1.13 | 0.81 | 0.57 | 0.49 | 0.18 | 0.09 | 135. |
| 140. | 1.89 | 1.18 | 0.87 | 0.59 | 0.50 | 0.21 | 0.10 | 140. |
| 145. | 1.99 | 1.25 | 0.93 | 0.61 | 0.52 | 0.23 | 0.10 | 145. |
| 150. | 2.08 | 1.32 | 0.98 | 0.64 | 0.53 | 0.25 | 0.10 | 150. |
| 155. | 2.16 | 1.39 | 1.04 | 0.66 | 0.55 | 0.27 | 0.11 | 155. |
| 160. | 2.21 | 1.44 | 1.08 | 0.69 | 0.55 | 0.28 | 0.11 | 160. |
| 165. | 2.25 | 1.51 | 1.11 | 0.71 | 0.56 | 0.29 | 0.11 | 165. |
| 170. | 2.28 | 1.50 | 1.11 | 0.73 | 0.51 | 0.29 | 0.11 | 170. |
| 175. | 2.08 | 1.42 | 1.05 | 0.72 | 0.47 | 0.29 | 0.11 | 175. |
| 180. | 1.88 | 1.28 | 0.95 | 0.65 | 0.41 | 0.28 | 0.10 | 180. |
| 185. | 1.58 | 1.05 | 0.83 | 0.54 | 0.33 | 0.24 | 0.09 | 185. |
| 190. | 1.22 | 0.79 | 0.68 | 0.42 | 0.23 | 0.19 | 0.06 | 190. |
| 195. | 0.83 | 0.53 | 0.51 | 0.28 | 0.13 | 0.13 | 0.04 | 195. |
| 200. | 0.44 | 0.28 | 0.31 | 0.17 | 0.06 | 0.08 | 0.01 | 200. |
| 205. | 0.09 | 0.15 | 0.12 | 0.07 | -0.03 | 0.05 | 0.01 | 205. |
| 210. | -0.22 | -0.02 | -0.03 | -0.01 | -0.09 | 0.03 | 0.01 | 210. |
| 215. | -0.44 | -0.06 | -0.12 | -0.07 | -0.15 | 0.00 | 0.01 | 215. |
| 220. | -0.54 | -0.03 | -0.19 | -0.13 | -0.20 | -0.02 | -0.01 | 220. |
| 225. | -0.62 | -0.01 | -0.25 | -0.17 | -0.23 | -0.04 | -0.02 | 225. |
| 230. | -0.64 | -0.11 | -0.30 | -0.21 | -0.24 | -0.05 | -0.03 | 230. |
| 235. | -0.75 | -0.24 | -0.32 | -0.23 | -0.25 | -0.06 | -0.04 | 235. |
| 240. | -0.84 | -0.34 | -0.32 | -0.25 | -0.27 | -0.07 | -0.04 | 240. |
| 245. | -0.92 | -0.44 | -0.33 | -0.26 | -0.29 | -0.08 | -0.05 | 245. |
| 250. | -0.94 | -0.54 | -0.34 | -0.27 | -0.30 | -0.08 | -0.05 | 250. |
| 255. | -0.94 | -0.59 | -0.36 | -0.28 | -0.31 | -0.08 | -0.06 | 255. |
| 260. | -0.94 | -0.62 | -0.37 | -0.29 | -0.31 | -0.09 | -0.07 | 260. |
| 265. | -0.94 | -0.63 | -0.37 | -0.29 | -0.31 | -0.09 | -0.07 | 265. |
| 270. | -0.93 | -0.63 | -0.37 | -0.30 | -0.30 | -0.09 | -0.07 | 270. |
| 275. | -0.93 | -0.62 | -0.37 | -0.30 | -0.30 | -0.09 | -0.08 | 275. |
| 280. | -0.93 | -0.61 | -0.36 | -0.30 | -0.30 | -0.08 | -0.07 | 280. |
| 285. | -0.93 | -0.61 | -0.36 | -0.29 | -0.29 | -0.08 | -0.07 | 285. |
| 290. | -0.94 | -0.61 | -0.36 | -0.29 | -0.29 | -0.08 | -0.06 | 290. |
| 295. | -0.94 | -0.61 | -0.36 | -0.29 | -0.29 | -0.08 | -0.05 | 295. |
| 300. | -0.94 | -0.61 | -0.36 | -0.29 | -0.29 | -0.07 | -0.04 | 300. |
| 305. | -0.95 | -0.61 | -0.36 | -0.28 | -0.29 | -0.07 | -0.03 | 305. |
| 310. | -0.95 | -0.61 | -0.35 | -0.28 | -0.27 | -0.05 | -0.03 | 310. |
| 315. | -0.95 | -0.61 | -0.35 | -0.26 | -0.25 | -0.05 | -0.02 | 315. |
| 320. | -0.95 | -0.60 | -0.35 | -0.24 | -0.24 | -0.05 | -0.02 | 320. |
| 325. | -0.98 | -0.59 | -0.35 | -0.23 | -0.23 | -0.05 | -0.01 | 325. |
| 330. | -0.86 | -0.56 | -0.34 | -0.23 | -0.24 | -0.04 | -0.02 | 330. |
| 335. | -0.84 | -0.56 | -0.35 | -0.24 | -0.24 | -0.04 | -0.03 | 335. |
| 340. | -0.94 | -0.64 | -0.39 | -0.26 | -0.23 | -0.05 | -0.03 | 340. |
| 345. | -1.14 | -0.78 | -0.44 | -0.33 | -0.23 | -0.07 | -0.02 | 345. |
| 350. | -1.39 | -1.01 | -0.56 | -0.38 | -0.26 | -0.07 | -0.01 | 350. |
| 355. | -1.56 | -1.12 | -0.74 | -0.51 | -0.34 | -0.12 | -0.04 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-503 CNTR NO. 163 TCN= 46. C.A.= 56.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -1.50 | -1.14 | -0.72 | -0.49 | -0.41 | -0.18 | -0.07 | 0. |
| 5. | -1.45 | -1.31 | -0.79 | -0.55 | -0.44 | -0.20 | -0.07 | 5. |
| 10. | -1.13 | -0.84 | -0.60 | -0.39 | -0.28 | -0.17 | -0.06 | 10. |
| 15. | -2.76 | -0.62 | -0.41 | -0.26 | -0.19 | -0.17 | -0.10 | 15. |
| 20. | -0.77 | -0.64 | -0.43 | -0.25 | -0.14 | -0.19 | -0.13 | 20. |
| 25. | -0.60 | -0.56 | -0.33 | -0.24 | -0.09 | -0.19 | -0.10 | 25. |
| 30. | -0.36 | -0.39 | -0.22 | -0.18 | -0.01 | -0.17 | -0.11 | 30. |
| 35. | -0.18 | -0.22 | -0.16 | -0.14 | 0.08 | -0.14 | -0.10 | 35. |
| 40. | 0.30 | -0.06 | -0.08 | -0.06 | 0.18 | -0.11 | -0.09 | 40. |
| 45. | 0.61 | 0.10 | 0.03 | 0.03 | 0.30 | -0.08 | -0.11 | 45. |
| 50. | 0.79 | 0.24 | 0.11 | 0.04 | 0.35 | -0.10 | -0.12 | 50. |
| 55. | 0.87 | 0.26 | 0.16 | 0.12 | 0.34 | -0.09 | -0.11 | 55. |
| 60. | 0.96 | 0.29 | 0.21 | 0.15 | 0.29 | -0.06 | -0.09 | 60. |
| 65. | 1.00 | 0.41 | 0.25 | 0.18 | 0.18 | -0.06 | -0.08 | 65. |
| 70. | 1.14 | 0.48 | 0.25 | 0.17 | 0.12 | -0.07 | -0.09 | 70. |
| 75. | 1.10 | 0.44 | 0.21 | 0.13 | 0.02 | -0.07 | -0.09 | 75. |
| 80. | 1.05 | 0.36 | 0.18 | 0.12 | 0.01 | -0.06 | -0.08 | 80. |
| 85. | 1.01 | 0.36 | 0.16 | 0.12 | 0.01 | -0.05 | -0.07 | 85. |
| 90. | 1.01 | 0.36 | 0.15 | 0.11 | 0.03 | -0.06 | -0.08 | 90. |
| 95. | 1.02 | 0.36 | 0.17 | 0.11 | 0.05 | -0.06 | -0.07 | 95. |
| 100. | 1.06 | 0.36 | 0.20 | 0.12 | 0.07 | -0.03 | -0.04 | 100. |
| 105. | 1.14 | 0.44 | 0.25 | 0.18 | 0.08 | 0.01 | -0.03 | 105. |
| 110. | 1.23 | 0.61 | 0.31 | 0.22 | 0.08 | 0.04 | -0.04 | 110. |
| 115. | 1.30 | 0.69 | 0.36 | 0.24 | 0.07 | 0.04 | -0.03 | 115. |
| 120. | 1.31 | 0.73 | 0.37 | 0.24 | 0.06 | 0.04 | -0.01 | 120. |
| 125. | 1.28 | 0.71 | 0.35 | 0.24 | 0.04 | 0.06 | 0.01 | 125. |
| 130. | 1.21 | 0.67 | 0.33 | 0.23 | 0.03 | 0.07 | 0.02 | 130. |
| 135. | 1.12 | 0.63 | 0.33 | 0.22 | 0.01 | 0.08 | 0.03 | 135. |
| 140. | 1.07 | 0.61 | 0.34 | 0.22 | 0.29 | 0.09 | 0.03 | 140. |
| 145. | 1.07 | 0.64 | 0.37 | 0.24 | 0.28 | 0.10 | 0.04 | 145. |
| 150. | 1.17 | 0.76 | 0.43 | 0.30 | 0.31 | 0.12 | 0.07 | 150. |
| 155. | 1.27 | 0.90 | 0.53 | 0.36 | 0.33 | 0.16 | 0.08 | 155. |
| 160. | 1.41 | 1.04 | 0.64 | 0.43 | 0.37 | 0.20 | 0.10 | 160. |
| 165. | 1.53 | 1.13 | 0.74 | 0.51 | 0.39 | 0.23 | 0.11 | 165. |
| 170. | 1.64 | 1.20 | 0.81 | 0.56 | 0.41 | 0.26 | 0.12 | 170. |
| 175. | 1.69 | 1.27 | 0.85 | 0.61 | 0.41 | 0.27 | 0.12 | 175. |
| 180. | 1.67 | 1.27 | 0.84 | 0.59 | 0.39 | 0.27 | 0.13 | 180. |
| 185. | 1.23 | 1.15 | 0.77 | 0.55 | 0.34 | 0.27 | 0.14 | 185. |
| 190. | 0.96 | 0.97 | 0.67 | 0.47 | 0.27 | 0.25 | 0.13 | 190. |
| 195. | 0.77 | 0.78 | 0.55 | 0.38 | 0.18 | 0.21 | 0.11 | 195. |
| 200. | 0.56 | 0.58 | 0.43 | 0.29 | 0.09 | 0.17 | 0.09 | 200. |
| 205. | 0.23 | 0.39 | 0.31 | 0.21 | -0.01 | 0.13 | 0.08 | 205. |
| 210. | -0.00 | 0.22 | 0.19 | 0.12 | -0.07 | 0.13 | 0.07 | 210. |
| 215. | -0.27 | 0.06 | 0.09 | 0.06 | -0.11 | 0.08 | 0.06 | 215. |
| 220. | -0.38 | -0.09 | -0.03 | 0.00 | -0.14 | 0.06 | 0.05 | 220. |
| 225. | -0.52 | -0.18 | -0.18 | -0.04 | -0.18 | 0.04 | 0.05 | 225. |
| 230. | -0.64 | -0.26 | -0.14 | -0.08 | -0.22 | 0.03 | 0.05 | 230. |
| 235. | -0.77 | -0.32 | -0.19 | -0.12 | -0.26 | 0.02 | 0.05 | 235. |
| 240. | -0.87 | -0.38 | -0.22 | -0.16 | -0.29 | 0.01 | 0.04 | 240. |
| 245. | -0.95 | -0.44 | -0.26 | -0.19 | -0.32 | -0.00 | 0.03 | 245. |
| 250. | -1.02 | -0.49 | -0.29 | -0.22 | -0.33 | -0.02 | 0.02 | 250. |
| 255. | -1.06 | -0.53 | -0.32 | -0.23 | -0.34 | -0.03 | 0.02 | 255. |
| 260. | -1.09 | -0.55 | -0.34 | -0.24 | -0.35 | -0.03 | 0.02 | 260. |
| 265. | -1.11 | -0.57 | -0.34 | -0.24 | -0.35 | -0.04 | 0.02 | 265. |
| 270 | -1.13 | -0.58 | -0.35 | -0.23 | -0.35 | -0.04 | 0.02 | 270. |
| 275 | -1.14 | -0.58 | -0.34 | -0.23 | -0.35 | -0.04 | 0.02 | 275. |
| 280. | -1.14 | -0.58 | -0.34 | -0.23 | -0.33 | -0.04 | 0.02 | 280. |
| 285. | -1.14 | -0.58 | -0.34 | -0.23 | -0.31 | -0.04 | 0.02 | 285. |
| 290. | -1.14 | -0.57 | -0.35 | -0.23 | -0.29 | -0.03 | 0.02 | 290. |
| 295. | -1.13 | -0.58 | -0.35 | -0.23 | -0.30 | 0.00 | 0.02 | 295. |
| 300. | -1.11 | -0.58 | -0.35 | -0.24 | -0.34 | 0.03 | 0.04 | 300. |
| 305. | -1.09 | -0.58 | -0.35 | -0.24 | -0.35 | 0.00 | 0.07 | 305. |
| 310. | -0.98 | -0.57 | -0.35 | -0.24 | -0.36 | -0.04 | 0.04 | 310. |
| 315. | -0.91 | -0.54 | -0.34 | -0.22 | -0.34 | -0.04 | 0.00 | 315. |
| 320. | -0.90 | -0.51 | -0.30 | -0.21 | -0.32 | -0.04 | 0.01 | 320. |
| 325. | -0.99 | -0.56 | -0.30 | -0.22 | -0.30 | -0.03 | 0.02 | 325. |
| 330. | -1.20 | -0.68 | -0.38 | -0.27 | -0.31 | -0.04 | 0.00 | 330. |
| 335. | -1.35 | -0.82 | -0.46 | -0.33 | -0.35 | -0.07 | -0.03 | 335. |
| 340. | -1.35 | -0.86 | -0.51 | -0.36 | -0.36 | -0.10 | -0.04 | 340. |
| 345. | -1.29 | -0.83 | -0.50 | -0.35 | -0.35 | -0.13 | -0.05 | 345. |
| 350. | -1.35 | -0.87 | -0.53 | -0.39 | -0.36 | -0.15 | -0.06 | 350. |
| 355. | -1.44 | -0.98 | -0.60 | -0.41 | -0.40 | -0.17 | -0.07 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 163 TCN= 46. C.R.= 50.3

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.190 | 10.480 | DEG. |
| 0. | -1.96 | -1.38 | -0.79 | -0.67 | -0.46 | -0.18 | -0.06 | 0. |
| 5. | -1.46 | -1.19 | -0.81 | -0.59 | -0.33 | -0.16 | -0.05 | 5. |
| 10. | -1.07 | -0.89 | -0.63 | -0.51 | -0.26 | -0.16 | -0.04 | 10. |
| 15. | -0.69 | -0.42 | -0.32 | -0.42 | -0.27 | -0.19 | -0.06 | 15. |
| 20. | -0.44 | -0.46 | -0.48 | -0.32 | -0.21 | -0.18 | -0.07 | 20. |
| 25. | -0.16 | -0.20 | -0.32 | -0.20 | -0.09 | -0.14 | -0.05 | 25. |
| 30. | 0.10 | 0.10 | -0.15 | -0.08 | 0.02 | -0.10 | -0.03 | 30. |
| 35. | 0.55 | 0.41 | -0.02 | 0.08 | 0.11 | -0.09 | -0.01 | 35. |
| 40. | 0.88 | 0.75 | 0.11 | 0.25 | 0.18 | -0.07 | -0.01 | 40. |
| 45. | 1.16 | 0.97 | 0.31 | 0.44 | 0.29 | -0.01 | -0.01 | 45. |
| 50. | 1.36 | 1.15 | 0.49 | 0.58 | 0.43 | 0.05 | 0.01 | 50. |
| 55. | 1.48 | 1.29 | 0.62 | 0.66 | 0.48 | 0.06 | 0.02 | 55. |
| 60. | 1.51 | 1.32 | 0.68 | 0.72 | 0.50 | 0.04 | 0.01 | 60. |
| 65. | 1.42 | 1.21 | 0.69 | 0.77 | 0.50 | 0.02 | 0.00 | 65. |
| 70. | 1.24 | 1.08 | 0.64 | 0.79 | 0.50 | 0.01 | 0.00 | 70. |
| 75. | 1.03 | 0.96 | 0.57 | 0.80 | 0.51 | 0.00 | -0.01 | 75. |
| 80. | 0.82 | 0.79 | 0.49 | 0.78 | 0.51 | -0.02 | -0.02 | 80. |
| 85. | 0.61 | 0.61 | 0.39 | 0.73 | 0.45 | -0.07 | -0.04 | 85. |
| 90. | 0.42 | 0.47 | 0.29 | 0.66 | 0.38 | -0.15 | -0.07 | 90. |
| 95. | 0.26 | 0.42 | 0.20 | 0.57 | 0.31 | -0.18 | -0.08 | 95. |
| 100. | 0.09 | 0.36 | 0.10 | 0.47 | 0.25 | -0.17 | -0.07 | 100. |
| 105. | -0.05 | 0.26 | -0.05 | 0.35 | 0.16 | -0.18 | -0.08 | 105. |
| 110. | -0.32 | 0.05 | -0.25 | 0.21 | 0.06 | -0.22 | -0.09 | 110. |
| 115. | -0.73 | -0.30 | -0.51 | 0.06 | -0.02 | -0.25 | -0.10 | 115. |
| 120. | -1.02 | -0.65 | -0.69 | -0.04 | -0.08 | -0.26 | -0.09 | 120. |
| 125. | -1.17 | -0.85 | -0.74 | -0.10 | -0.12 | -0.27 | -0.09 | 125. |
| 130. | -1.15 | -0.82 | -0.74 | -0.13 | -0.12 | -0.26 | -0.09 | 130. |
| 135. | -1.03 | -0.88 | -0.67 | -0.12 | -0.09 | -0.23 | -0.08 | 135. |
| 140. | -0.84 | -0.59 | -0.56 | -0.07 | -0.04 | -0.19 | -0.07 | 140. |
| 145. | -0.61 | -0.23 | -0.42 | 0.00 | 0.02 | -0.14 | -0.06 | 145. |
| 150. | -0.35 | 0.14 | -0.25 | 0.05 | 0.06 | -0.09 | -0.04 | 150. |
| 155. | -0.08 | 0.34 | -0.06 | 0.10 | 0.09 | -0.04 | -0.02 | 155. |
| 160. | 0.19 | 0.45 | 0.10 | 0.26 | 0.12 | 0.01 | 0.00 | 160. |
| 165. | 0.45 | 0.58 | 0.24 | 0.33 | 0.19 | 0.06 | 0.02 | 165. |
| 170. | 0.67 | 0.68 | 0.37 | 0.37 | 0.20 | 0.09 | 0.03 | 170. |
| 175. | 0.84 | 0.71 | 0.48 | 0.40 | 0.25 | 0.13 | 0.04 | 175. |
| 180. | 0.92 | 0.69 | 0.55 | 0.39 | 0.24 | 0.16 | 0.05 | 180. |
| 185. | 0.92 | 0.59 | 0.57 | 0.36 | 0.20 | 0.18 | 0.05 | 185. |
| 190. | 0.86 | 0.56 | 0.55 | 0.31 | 0.24 | 0.18 | 0.05 | 190. |
| 195. | 0.75 | 0.60 | 0.51 | 0.25 | 0.17 | 0.17 | 0.05 | 195. |
| 200. | 0.61 | 0.56 | 0.44 | 0.18 | 0.11 | 0.16 | 0.05 | 200. |
| 205. | 0.46 | 0.37 | 0.36 | 0.10 | 0.04 | 0.14 | 0.04 | 205. |
| 210. | 0.31 | 0.15 | 0.27 | 0.02 | -0.01 | 0.13 | 0.04 | 210. |
| 215. | 0.16 | -0.03 | 0.19 | -0.05 | -0.06 | 0.12 | 0.04 | 215. |
| 220. | 0.02 | -0.17 | 0.12 | -0.12 | -0.10 | 0.11 | 0.03 | 220. |
| 225. | -0.10 | -0.23 | 0.06 | -0.19 | -0.13 | 0.10 | 0.03 | 225. |
| 230. | -0.19 | -0.26 | 0.01 | -0.24 | -0.16 | 0.09 | 0.03 | 230. |
| 235. | -0.25 | -0.31 | -0.03 | -0.28 | -0.19 | 0.09 | 0.04 | 235. |
| 240. | -0.31 | -0.36 | -0.06 | -0.31 | -0.21 | 0.09 | 0.04 | 240. |
| 245. | -0.36 | -0.41 | -0.07 | -0.34 | -0.23 | 0.09 | 0.04 | 245. |
| 250. | -0.41 | -0.43 | -0.07 | -0.36 | -0.25 | 0.09 | 0.03 | 250. |
| 255. | -0.44 | -0.43 | -0.06 | -0.37 | -0.26 | 0.09 | 0.03 | 255. |
| 260. | -0.47 | -0.43 | -0.06 | -0.39 | -0.27 | 0.08 | 0.03 | 260. |
| 265. | -0.48 | -0.44 | -0.06 | -0.39 | -0.27 | 0.08 | 0.03 | 265. |
| 270. | -0.48 | -0.44 | -0.06 | -0.39 | -0.27 | 0.08 | 0.02 | 270. |
| 275. | -0.47 | -0.44 | -0.06 | -0.39 | -0.27 | 0.09 | 0.02 | 275. |
| 280. | -0.46 | -0.43 | -0.06 | -0.39 | -0.27 | 0.09 | 0.02 | 280. |
| 285. | -0.43 | -0.42 | -0.07 | -0.39 | -0.27 | 0.10 | 0.02 | 285. |
| 290. | -0.38 | -0.40 | -0.07 | -0.37 | -0.26 | 0.10 | 0.03 | 290. |
| 295. | -0.31 | -0.38 | -0.07 | -0.35 | -0.24 | 0.11 | 0.04 | 295. |
| 300. | -0.23 | -0.34 | -0.05 | -0.32 | -0.22 | 0.11 | 0.05 | 300. |
| 305. | -0.16 | -0.29 | -0.00 | -0.31 | -0.19 | 0.11 | 0.06 | 305. |
| 310. | -0.11 | -0.25 | 0.04 | -0.30 | -0.17 | 0.11 | 0.06 | 310. |
| 315. | -0.07 | -0.23 | 0.04 | -0.29 | -0.15 | 0.11 | 0.06 | 315. |
| 320. | -0.04 | -0.22 | 0.02 | -0.28 | -0.15 | 0.10 | 0.06 | 320. |
| 325. | 0.00 | -0.23 | -0.01 | -0.26 | -0.15 | 0.10 | 0.05 | 325. |
| 330. | -0.07 | -0.24 | -0.03 | -0.24 | -0.15 | 0.09 | 0.05 | 330. |
| 335. | -0.02 | -0.21 | -0.04 | -0.24 | -0.16 | 0.09 | 0.05 | 335. |
| 340. | 0.15 | -0.11 | -0.01 | -0.23 | -0.15 | 0.08 | 0.05 | 340. |
| 345. | 0.26 | -0.02 | 0.04 | -0.18 | -0.07 | 0.04 | 0.03 | 345. |
| 350. | -0.47 | -0.62 | -0.33 | -0.37 | -0.22 | -0.03 | 0.00 | 350. |
| 355. | -1.02 | -0.97 | -0.57 | -0.54 | -0.40 | -0.11 | -0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 163 TCN= 46. C.A.= 54.0

DIFFERENTIAL PRESSURES

SPAN STATION 170.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.042 | 1.954 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.04 | 0.24 | 0.00 | 0.07 | 0.04 | -0.02 | -0.00 | 0. |
| 5. | -0.57 | -0.31 | -0.24 | -0.10 | -0.17 | -0.12 | -0.01 | 5. |
| 10. | -0.44 | -0.43 | -0.39 | -0.18 | -0.26 | -0.16 | -0.51 | 10. |
| 15. | -0.32 | -0.33 | -0.38 | -0.17 | -0.25 | -0.10 | -0.02 | 15. |
| 20. | -0.27 | -0.17 | -0.22 | -0.12 | -0.18 | -0.12 | -0.01 | 20. |
| 25. | 0.17 | 0.09 | -0.02 | -0.06 | -0.00 | -0.05 | 0.02 | 25. |
| 30. | 0.50 | 0.22 | 0.14 | 0.01 | -0.01 | -0.02 | 0.04 | 30. |
| 35. | 0.98 | 0.47 | 0.29 | 0.08 | 0.08 | 0.02 | 0.05 | 35. |
| 40. | 1.13 | 0.69 | 0.48 | 0.16 | 0.18 | 0.10 | 0.06 | 40. |
| 45. | 1.31 | 0.85 | 0.71 | 0.27 | 0.29 | 0.16 | 0.08 | 45. |
| 50. | 1.45 | 0.88 | 0.90 | 0.38 | 0.39 | 0.20 | 0.10 | 50. |
| 55. | 1.54 | 0.79 | 0.94 | 0.43 | 0.45 | 0.22 | 0.09 | 55. |
| 60. | 1.51 | 0.65 | 0.83 | 0.53 | 0.47 | 0.20 | 0.07 | 60. |
| 65. | 1.32 | 0.43 | 0.64 | 0.88 | 0.44 | 0.16 | 0.05 | 65. |
| 70. | 1.10 | 0.18 | 0.49 | 1.13 | 0.38 | 0.11 | 0.04 | 70. |
| 75. | 0.90 | -0.00 | 0.35 | 1.28 | 0.29 | 0.06 | 0.02 | 75. |
| 80. | 0.69 | -0.31 | 0.16 | 1.21 | 0.18 | -0.05 | -0.00 | 80. |
| 85. | 0.46 | -0.53 | -0.16 | 1.02 | -0.00 | -0.13 | -0.03 | 85. |
| 90. | 0.16 | -0.76 | -0.48 | 0.86 | -0.24 | -0.22 | -0.05 | 90. |
| 95. | -0.32 | -1.14 | -0.76 | 0.41 | -0.51 | -0.27 | -0.05 | 95. |
| 100. | -0.87 | -1.62 | -1.06 | -0.35 | -0.66 | -0.28 | -0.04 | 100. |
| 105. | -1.35 | -2.04 | -1.36 | -1.09 | -0.67 | -0.27 | -0.04 | 105. |
| 110. | -1.68 | -2.27 | -1.63 | -1.67 | -0.63 | -0.25 | -0.04 | 110. |
| 115. | -1.73 | -2.39 | -1.68 | -1.80 | -0.57 | -0.24 | -0.04 | 115. |
| 120. | -1.88 | -2.43 | -2.09 | -1.48 | -0.01 | -0.24 | -0.05 | 120. |
| 125. | -1.88 | -2.41 | -2.09 | -1.15 | -0.60 | -0.25 | -0.06 | 125. |
| 130. | -1.89 | -2.33 | -1.93 | -1.04 | -0.75 | -0.26 | -0.06 | 130. |
| 135. | -1.88 | -2.13 | -1.73 | -1.00 | -0.77 | -0.25 | -0.06 | 135. |
| 140. | -1.76 | -1.89 | -1.58 | -1.00 | -0.74 | -0.20 | -0.05 | 140. |
| 145. | -1.57 | -1.59 | -1.28 | -0.87 | -0.64 | -0.16 | -0.05 | 145. |
| 150. | -1.31 | -1.28 | -1.06 | -0.72 | -0.51 | -0.11 | -0.04 | 150. |
| 155. | -1.02 | -0.96 | -0.84 | -0.60 | -0.40 | -0.07 | -0.03 | 155. |
| 160. | -0.78 | -0.65 | -0.62 | -0.49 | -0.28 | -0.02 | -0.02 | 160. |
| 165. | -0.39 | -0.33 | -0.39 | -0.39 | -0.16 | 0.03 | -0.01 | 165. |
| 170. | -0.18 | -0.07 | -0.19 | -0.26 | -0.04 | 0.07 | 0.00 | 170. |
| 175. | 0.14 | 0.19 | -0.01 | -0.10 | 0.04 | 0.11 | 0.01 | 175. |
| 180. | 0.30 | 0.39 | 0.12 | -0.00 | 0.11 | 0.13 | 0.02 | 180. |
| 185. | 0.48 | 0.54 | 0.22 | -0.01 | 0.15 | 0.13 | 0.02 | 185. |
| 190. | 0.43 | 0.62 | 0.30 | 0.03 | 0.17 | 0.12 | 0.02 | 190. |
| 195. | 0.42 | 0.65 | 0.34 | 0.05 | 0.17 | 0.11 | 0.01 | 195. |
| 200. | 0.38 | 0.64 | 0.35 | 0.07 | 0.16 | 0.09 | 0.00 | 200. |
| 205. | 0.32 | 0.61 | 0.35 | 0.08 | 0.15 | 0.08 | -0.00 | 205. |
| 210. | 0.23 | 0.54 | 0.34 | 0.09 | 0.14 | 0.06 | -0.00 | 210. |
| 215. | 0.12 | 0.51 | 0.34 | 0.10 | 0.13 | 0.05 | -0.00 | 215. |
| 220. | 0.03 | 0.49 | 0.33 | 0.10 | 0.12 | 0.04 | -0.00 | 220. |
| 225. | -0.03 | 0.47 | 0.32 | 0.09 | 0.11 | 0.03 | -0.01 | 225. |
| 230. | -0.06 | 0.46 | 0.32 | 0.09 | 0.10 | 0.03 | -0.02 | 230. |
| 235. | -0.08 | 0.45 | 0.32 | 0.08 | 0.10 | 0.03 | -0.02 | 235. |
| 240. | -0.09 | 0.45 | 0.34 | 0.08 | 0.10 | 0.03 | -0.02 | 240. |
| 245. | -0.10 | 0.46 | 0.37 | 0.09 | 0.11 | 0.04 | -0.02 | 245. |
| 250. | -0.09 | 0.48 | 0.40 | 0.11 | 0.13 | 0.04 | -0.02 | 250. |
| 255. | -0.07 | 0.50 | 0.43 | 0.13 | 0.15 | 0.05 | -0.01 | 255. |
| 260. | -0.05 | 0.54 | 0.46 | 0.16 | 0.16 | 0.05 | -0.01 | 260. |
| 265. | -0.02 | 0.57 | 0.49 | 0.18 | 0.17 | 0.05 | -0.01 | 265. |
| 270. | 0.02 | 0.60 | 0.51 | 0.20 | 0.18 | 0.06 | -0.00 | 270. |
| 275. | 0.05 | 0.64 | 0.52 | 0.21 | 0.19 | 0.06 | -0.00 | 275. |
| 280. | 0.08 | 0.67 | 0.54 | 0.23 | 0.20 | 0.06 | 0.00 | 280. |
| 285. | 0.13 | 0.71 | 0.56 | 0.24 | 0.21 | 0.07 | 0.00 | 285. |
| 290. | 0.20 | 0.76 | 0.58 | 0.26 | 0.23 | 0.07 | 0.01 | 290. |
| 295. | 0.27 | 0.78 | 0.60 | 0.27 | 0.25 | 0.08 | 0.01 | 295. |
| 300. | 0.39 | 0.82 | 0.63 | 0.29 | 0.27 | 0.09 | 0.01 | 300. |
| 305. | 0.48 | 0.86 | 0.65 | 0.30 | 0.28 | 0.10 | 0.01 | 305. |
| 310. | 0.54 | 0.90 | 0.68 | 0.33 | 0.29 | 0.11 | 0.02 | 310. |
| 315. | 0.59 | 0.92 | 0.69 | 0.35 | 0.30 | 0.12 | 0.02 | 315. |
| 320. | 0.62 | 0.92 | 0.68 | 0.36 | 0.29 | 0.12 | 0.02 | 320. |
| 325. | 0.60 | 0.87 | 0.65 | 0.35 | 0.28 | 0.10 | 0.02 | 325. |
| 330. | 0.51 | 0.78 | 0.59 | 0.30 | 0.26 | 0.08 | 0.02 | 330. |
| 335. | 0.43 | 0.68 | 0.51 | 0.25 | 0.22 | 0.06 | 0.01 | 335. |
| 340. | 0.40 | 0.61 | 0.44 | 0.22 | 0.19 | 0.05 | 0.01 | 340. |
| 345. | 0.46 | 0.63 | 0.47 | 0.23 | 0.22 | 0.06 | 0.02 | 345. |
| 350. | 0.52 | 0.68 | 0.49 | 0.22 | 0.20 | 0.05 | 0.02 | 350. |
| 355. | 0.46 | 0.59 | 0.37 | 0.17 | 0.10 | -0.00 | 0.00 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=503 CNTR NO. 163 TCM= 46. C.R.= 56.0

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.548 | 1.950 | 2.900 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | 0.66 | 0.51 | 0.28 | 0.36 | 0.05 | 0.09 | 0.04 | 0. |
| 5. | -0.52 | -0.50 | -0.44 | -0.10 | -0.05 | -0.06 | -0.00 | 5. |
| 10. | -0.02 | -0.76 | -0.64 | -0.27 | -0.13 | -0.12 | -0.01 | 10. |
| 15. | -0.50 | -0.44 | -0.44 | -0.16 | -0.14 | -0.00 | -0.00 | 15. |
| 20. | 0.01 | 0.07 | -0.21 | 0.03 | -0.02 | -0.03 | 0.02 | 20. |
| 25. | 0.47 | 0.46 | -0.03 | 0.09 | 0.16 | 0.00 | 0.04 | 25. |
| 30. | 0.01 | 0.64 | 0.14 | 0.16 | 0.33 | -0.02 | 0.03 | 30. |
| 35. | 1.05 | 0.79 | 0.35 | 0.32 | 0.51 | -0.01 | 0.03 | 35. |
| 40. | 1.26 | 0.99 | 0.60 | 0.49 | 0.67 | 0.03 | 0.04 | 40. |
| 45. | 1.43 | 1.11 | 0.90 | 0.61 | 0.82 | 0.07 | [illegible] | [illegible] |
| 50. | 1.48 | 1.13 | 1.48 | 0.76 | 0.94 | 0.10 | [illegible] | [illegible] |
| 55. | 1.44 | 1.14 | 1.92 | 1.04 | 1.02 | 0.10 | [illegible] | 55. |
| 60. | 1.37 | 1.06 | 1.99 | 1.31 | 1.00 | 0.04 | -0.00 | 60. |
| 65. | 1.17 | 0.83 | 1.78 | 1.31 | 0.85 | -0.06 | -0.03 | 65. |
| 70. | 0.87 | 0.53 | 1.49 | 0.95 | 0.69 | -0.14 | -0.05 | 70. |
| 75. | 0.59 | 0.22 | 1.22 | 0.48 | 1.21 | -0.28 | -0.09 | 75. |
| 80. | 0.27 | -0.05 | 1.06 | 0.83 | 1.05 | -0.39 | -0.14 | 80. |
| 85. | -0.15 | -0.28 | 0.88 | -0.24 | 2.19 | -0.52 | -0.17 | 85. |
| 90. | -0.67 | -0.86 | 0.38 | -0.55 | 1.75 | -0.57 | -0.14 | 90. |
| 95. | -1.32 | -1.47 | -0.24 | -0.92 | 0.25 | -0.45 | -0.10 | 95. |
| 100. | -1.76 | -1.85 | -0.86 | -1.19 | -1.70 | -0.35 | -0.08 | 100. |
| 105. | -1.96 | -2.04 | -1.31 | -1.46 | -2.96 | -0.25 | -0.07 | 105. |
| 110. | -2.12 | -2.16 | -1.56 | -1.81 | -3.81 | -0.21 | -0.05 | 110. |
| 115. | -2.25 | -2.27 | -1.63 | -2.33 | -1.72 | -0.22 | -0.05 | 115. |
| 120. | -2.35 | -2.35 | -1.69 | -2.82 | -0.43 | -0.30 | -0.06 | 120. |
| 125. | -2.44 | -2.44 | -2.00 | -3.03 | -0.21 | -0.37 | -0.07 | 125. |
| 130. | -2.49 | -2.47 | -2.25 | -2.56 | -0.29 | -0.48 | -0.08 | 130. |
| 135. | -2.47 | -2.38 | -2.38 | -1.73 | -0.43 | -0.48 | -0.09 | 135. |
| 140. | -2.36 | -2.28 | -2.18 | -1.14 | -0.48 | -0.35 | -0.08 | 140. |
| 145. | -2.12 | -1.93 | -1.76 | -1.05 | -0.44 | -0.28 | -0.07 | 145. |
| 150. | -1.82 | -1.61 | -1.45 | -0.90 | -0.36 | -0.24 | -0.06 | 150. |
| 155. | -1.49 | -1.26 | -1.15 | -0.73 | -0.27 | -0.20 | -0.05 | 155. |
| 160. | -1.13 | -0.91 | -0.84 | -0.53 | -0.18 | -0.14 | -0.04 | 160. |
| 165. | -0.78 | -0.54 | -0.61 | -0.33 | -0.09 | -0.08 | -0.02 | 165. |
| 170. | -0.43 | -0.21 | -0.38 | -0.15 | -0.02 | -0.02 | -0.00 | 170. |
| 175. | -0.12 | 0.03 | -0.18 | -0.01 | 0.01 | 0.04 | 0.01 | 175. |
| 180. | 0.14 | 0.21 | -0.03 | 0.19 | 0.01 | 0.08 | 0.01 | 180. |
| 185. | 0.32 | 0.32 | 0.07 | 0.18 | -0.01 | 0.10 | 0.01 | 185. |
| 190. | 0.42 | 0.39 | 0.12 | 0.23 | -0.02 | 0.12 | 0.01 | 190. |
| 195. | 0.45 | 0.42 | 0.13 | 0.27 | -0.04 | 0.13 | 0.01 | 195. |
| 200. | 0.41 | 0.43 | 0.14 | 0.28 | -0.06 | 0.13 | 0.01 | 200. |
| 205. | 0.34 | 0.42 | 0.13 | 0.29 | -0.08 | 0.13 | -0.00 | 205. |
| 210. | 0.27 | 0.38 | 0.11 | 0.29 | -0.10 | 0.13 | -0.00 | 210. |
| 215. | 0.22 | 0.34 | 0.09 | 0.28 | -0.13 | 0.12 | 0.01 | 215. |
| 220. | 0.18 | 0.33 | 0.07 | 0.28 | -0.15 | 0.12 | 0.01 | 220. |
| 225. | 0.15 | 0.33 | 0.06 | 0.27 | -0.17 | 0.12 | 0.01 | 225. |
| 230. | 0.13 | 0.33 | 0.05 | 0.27 | -0.19 | 0.13 | 0.01 | 230. |
| 235. | 0.13 | 0.35 | 0.06 | 0.28 | -0.21 | 0.13 | 0.01 | 235. |
| 240. | 0.14 | 0.37 | 0.08 | 0.31 | -0.23 | 0.14 | 0.02 | 240. |
| 245. | 0.17 | 0.39 | 0.10 | 0.34 | -0.21 | 0.14 | 0.02 | 245. |
| 250. | 0.21 | 0.41 | 0.12 | 0.38 | -0.19 | 0.15 | 0.03 | 250. |
| 255. | 0.26 | 0.44 | 0.14 | 0.42 | -0.18 | 0.16 | 0.03 | 255. |
| 260. | 0.31 | 0.48 | 0.17 | 0.45 | -0.17 | 0.17 | 0.03 | 260. |
| 265. | 0.38 | 0.53 | 0.20 | 0.48 | -0.16 | 0.18 | 0.03 | 265. |
| 270. | 0.45 | 0.58 | 0.24 | 0.51 | -0.16 | 0.19 | 0.03 | 270. |
| 275. | 0.52 | 0.63 | 0.28 | 0.53 | -0.14 | 0.20 | 0.03 | 275. |
| 280. | 0.58 | 0.68 | 0.33 | 0.55 | -0.12 | 0.21 | 0.04 | 280. |
| 285. | 0.64 | 0.72 | 0.39 | 0.57 | -0.10 | 0.21 | 0.04 | 285. |
| 290. | 0.70 | 0.76 | 0.45 | 0.60 | -0.07 | 0.21 | 0.03 | 290. |
| 295. | 0.80 | 0.82 | 0.50 | 0.62 | -0.03 | 0.21 | 0.04 | 295. |
| 300. | 0.91 | 0.91 | 0.54 | 0.65 | 0.01 | 0.22 | 0.05 | 300. |
| 305. | 1.00 | 0.99 | 0.57 | 0.68 | 0.05 | 0.23 | 0.06 | 305. |
| 310. | 1.04 | 1.04 | 0.58 | 0.70 | 0.10 | 0.25 | 0.07 | 310. |
| 315. | 1.06 | 1.05 | 0.59 | 0.71 | 0.16 | 0.25 | 0.07 | 315. |
| 320. | 1.08 | 1.05 | 0.59 | 0.71 | 0.22 | 0.25 | 0.07 | 320. |
| 325. | 1.10 | 1.06 | 0.56 | 0.69 | 0.25 | 0.24 | 0.07 | 325. |
| 330. | 1.02 | 0.89 | 0.50 | 0.64 | 0.23 | 0.21 | 0.07 | 330. |
| 335. | 0.86 | 0.70 | 0.42 | 0.57 | 0.18 | 0.19 | 0.06 | 335. |
| 340. | 0.73 | 0.68 | 0.34 | 0.49 | 0.10 | 0.18 | 0.07 | 340. |
| 345. | 0.71 | 0.64 | 0.30 | 0.48 | 0.03 | 0.18 | 0.07 | 345. |
| 350. | 0.73 | 0.67 | 0.30 | 0.48 | -0.02 | 0.17 | 0.07 | 350. |
| 355. | 0.66 | 0.75 | 0.34 | 0.48 | -0.02 | 0.15 | 0.06 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=533 CNTR NO. 163 TCH= 46. C.R.= 56.0

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.435 | 1.040 | 1.950 | 2.990 | 4.350 | 7.190 | 10.460 | DEG. |
| 0. | 1.04 | 0.04 | 0.09 | 0.15 | 0.08 | 0.07 | -0.05 | 0. |
| 5. | -0.52 | -0.21 | -0.40 | -0.27 | -0.11 | -0.04 | -0.07 | 5. |
| 10. | -0.96 | -0.56 | -0.71 | -0.38 | -0.17 | -0.10 | -0.07 | 10. |
| 15. | -0.48 | -0.28 | -0.53 | -0.23 | -0.09 | -0.06 | -0.06 | 15. |
| 20. | 3.25 | 0.15 | -0.23 | -0.07 | 0.01 | -0.05 | -0.05 | 20. |
| 25. | 0.69 | 0.48 | -0.08 | 0.05 | 0.09 | -0.07 | -0.05 | 25. |
| 30. | 0.90 | 0.68 | 0.82 | 0.12 | 0.19 | -0.09 | -0.06 | 30. |
| 35. | 1.17 | 0.86 | 0.28 | 0.29 | 0.21 | -0.08 | -0.07 | 35. |
| 40. | 1.38 | 1.04 | 1.02 | 0.43 | 0.42 | -0.07 | -0.06 | 40. |
| 45. | 1.51 | 1.14 | 1.01 | 0.60 | 0.49 | -0.09 | -0.06 | 45. |
| 50. | 1.57 | 1.18 | 2.05 | 1.22 | 0.52 | -0.15 | -0.06 | 50. |
| 55. | 1.52 | 1.32 | 2.03 | 1.74 | 0.37 | -0.24 | -0.10 | 55. |
| 60. | 1.34 | 1.36 | 1.82 | 1.65 | 0.49 | -0.36 | -0.15 | 60. |
| 65. | 1.06 | 1.15 | 1.53 | 1.73 | 1.18 | -0.47 | -0.17 | 65. |
| 70. | 0.72 | 0.81 | 1.35 | 1.54 | 1.92 | -0.54 | -0.15 | 70. |
| 75. | 0.32 | 0.40 | 1.14 | 0.97 | 1.69 | -0.69 | -0.16 | 75. |
| 80. | -5.23 | -0.18 | 0.87 | 6.11 | 0.97 | -0.78 | -0.22 | 80. |
| 85. | -0.89 | -0.69 | 0.55 | -0.41 | 0.38 | -0.69 | -0.20 | 85. |
| 90. | -1.53 | -1.28 | 0.21 | -0.81 | -0.08 | -0.44 | -0.12 | 90. |
| 95. | -2.06 | -1.77 | -0.89 | -1.18 | -0.44 | -0.16 | -0.05 | 95. |
| 100. | -2.41 | -2.03 | -0.34 | -1.38 | -0.61 | 0.02 | -0.03 | 100. |
| 105. | -2.64 | -2.17 | -0.54 | -1.45 | -1.22 | 0.11 | -0.04 | 105. |
| 110. | -2.81 | -2.27 | -0.64 | -1.46 | -2.54 | 0.19 | -0.01 | 110. |
| 115. | -2.93 | -2.33 | -0.71 | -1.81 | -3.18 | -0.02 | 0.02 | 115. |
| 120. | -3.01 | -2.36 | -0.87 | -2.13 | -2.58 | -0.19 | 0.03 | 120. |
| 125. | -3.06 | -2.38 | -1.24 | -2.56 | -0.94 | -0.37 | 0.03 | 125. |
| 130. | -3.10 | -2.43 | -1.82 | -2.83 | -0.14 | -0.44 | -0.03 | 130. |
| 135. | -3.07 | -2.44 | -2.13 | -2.18 | -0.16 | -0.48 | -0.06 | 135. |
| 140. | -2.99 | -2.38 | -2.14 | -1.21 | -0.38 | -0.44 | -0.07 | 140. |
| 145. | -2.61 | -2.05 | -1.93 | -0.70 | -0.38 | -0.38 | -0.06 | 145. |
| 150. | -2.27 | -1.74 | -1.61 | -0.67 | -0.37 | -0.32 | -0.05 | 150. |
| 155. | -1.88 | -1.49 | -1.32 | -0.74 | -0.32 | -0.26 | -0.02 | 155. |
| 160. | -1.58 | -1.20 | -1.04 | -0.56 | -0.23 | -0.19 | 0.00 | 160. |
| 165. | -1.13 | -0.73 | -0.88 | -0.34 | -0.14 | -0.13 | 0.02 | 165. |
| 170. | -0.75 | -0.44 | -0.48 | -0.20 | -0.06 | -0.07 | 0.04 | 170. |
| 175. | -0.37 | -0.19 | -0.42 | -0.07 | 0.00 | -0.02 | 0.05 | 175. |
| 180. | -0.04 | 0.01 | -0.28 | 0.03 | 0.05 | 0.03 | 0.04 | 180. |
| 185. | 0.18 | 0.16 | -0.18 | 0.09 | 0.07 | 0.04 | 0.04 | 185. |
| 190. | 0.32 | 0.25 | -0.11 | 0.14 | 0.09 | 0.00 | 0.05 | 190. |
| 195. | 0.39 | 0.29 | -0.08 | 0.17 | 0.10 | 0.10 | 0.04 | 195. |
| 200. | 0.48 | 0.30 | -0.07 | 0.18 | 0 | 0.11 | 0.05 | 200. |
| 205. | 0.37 | 0.31 | -0.08 | 0.18 | 0.07 | 0.12 | 0.04 | 205. |
| 210. | 0.31 | 0.30 | -0.08 | 0.18 | 0.06 | 0.13 | 0.05 | 210. |
| 215. | 0.27 | 0.28 | -0.09 | 0.19 | 0.04 | 0.14 | 0.06 | 215. |
| 220. | 0.25 | 0.27 | -0.09 | 0.19 | 0.04 | 0.16 | 0.06 | 220. |
| 225. | 0.26 | 0.26 | 0.09 | 0.18 | 0.04 | 0.18 | 0.06 | 225. |
| 230. | 0.28 | 0.27 | -0.07 | 0.2 | 0.05 | 0.21 | 0.06 | 230. |
| 235. | 0.31 | 0.29 | -0.05 | 0.24 | 0.05 | 0.23 | 0.07 | 235. |
| 240. | 0.34 | 0.32 | -0.01 | 0.26 | 0.06 | 0.25 | 0.08 | 240. |
| 245. | 0.42 | 0.37 | 0.02 | 0.29 | 0.07 | 0.26 | 0.08 | 245. |
| 250. | 0.50 | 0.41 | 0.06 | 0.32 | 0.07 | 0.28 | 0.08 | 250. |
| 255. | 0.58 | 0.46 | 0.10 | 0.35 | 0.08 | 0.28 | 0.08 | 255. |
| 260. | 0.68 | 0.52 | 0.15 | 0.38 | 0.09 | 0.29 | 0.08 | 260. |
| 265. | 0.77 | 0.58 | 0.17 | 0.40 | 0.11 | 0.30 | 0.09 | 265. |
| 270. | 0.87 | 0.63 | 0.22 | 0.43 | 0.12 | 0.30 | 0.09 | 270. |
| 275. | 0.97 | 0.69 | 0.26 | 0.46 | 0.14 | 0.30 | 0.09 | 275. |
| 280. | 1.08 | 0.76 | 0.30 | 0.48 | 0.15 | 0.30 | 0.10 | 280. |
| 285. | 1.19 | 0.83 | 0.34 | 0.50 | 0.17 | 0.31 | 0.09 | 285. |
| 290. | 1.30 | 0.90 | 0.39 | 0.52 | 0.19 | 0.31 | 0.08 | 290. |
| 295. | 1.40 | 0.97 | 0.42 | 0.54 | 0.21 | 0.32 | 0.08 | 295. |
| 300. | 1.48 | 1.04 | 0.46 | 0.56 | 0.23 | 0.32 | 0.06 | 300. |
| 305. | 1.54 | 1.08 | 0.48 | 0.57 | 0.24 | 0.32 | 0.06 | 305. |
| 310. | 1.57 | 1.11 | 0.48 | 0.59 | 0.26 | 0.32 | 0.07 | 310. |
| 315. | 1.62 | 1.13 | 0.48 | 0.59 | 0.27 | 0.31 | 0.07 | 315. |
| 320. | 1.64 | 1.15 | 0.47 | 0.58 | 0.28 | 0.31 | 0.06 | 320. |
| 325. | 1.60 | 1.13 | 0.45 | 0.57 | 0.29 | 0.29 | 0.05 | 325. |
| 330. | 1.47 | 1.06 | 0.41 | 0.53 | 0.27 | 0.28 | 0.04 | 330. |
| 335. | 1.22 | 0.89 | 0.31 | 0.46 | 0.23 | 0.26 | 0.03 | 335. |
| 340. | 1.03 | 0.72 | 0.22 | 0.38 | 0.18 | 0.24 | 0.02 | 340. |
| 345. | 0.93 | 0.64 | 0.18 | 0.34 | 0.13 | 0.20 | 0.02 | 345. |
| 350. | 0.97 | 0.71 | 0.23 | 0.34 | 0.13 | 0.16 | 0.56 | 350. |
| 355. | 1.15 | 0.85 | 0.27 | 0.37 | 0.22 | 0.18 | 0.31 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 256 TCN= 50. C.R.= 10.5

DIFFERENTIAL PRESSURES

| AZ | SPAN STATION 92.5 CHORD STATION | | | | AZ |
|---|---|---|---|---|---|
| DEG. | 0.455 | 1.950 | 4.550 | 10.400 | DEG. |
| 0. | -0.93 | -0.41 | -0.34 | 0.05 | 0. |
| 5. | -0.84 | -0.29 | -0.23 | 0.11 | 5. |
| 10. | -0.96 | -0.35 | -0.12 | 0.07 | 10. |
| 15. | -0.78 | -0.21 | -0.02 | 0.01 | 15. |
| 20. | -0.58 | -0.16 | 0.01 | 0.04 | 20. |
| 25. | -0.83 | -0.17 | -0.15 | 0.03 | 25. |
| 30. | -0.93 | -0.51 | -0.26 | -0.01 | 30. |
| 35. | -0.92 | -0.59 | -0.23 | -0.02 | 35. |
| 40. | -0.79 | -0.37 | -0.17 | -0.00 | 40. |
| 45. | -0.51 | -0.18 | -0.10 | 0.01 | 45. |
| 50. | -0.25 | -0.06 | -0.04 | 0.02 | 50. |
| 55. | -0.06 | -0.01 | 0.01 | 0.02 | 55. |
| 60. | 0.04 | -0.00 | 0.02 | 0.01 | 60. |
| 65. | -0.01 | -0.02 | 0.01 | 0.01 | 65. |
| 70. | -0.09 | -0.05 | -0.00 | -0.00 | 70. |
| 75. | -0.11 | -0.07 | -0.01 | -0.01 | 75. |
| 80. | -0.08 | -0.07 | -0.00 | -0.01 | 80. |
| 85. | 0.00 | -0.03 | 0.02 | -0.01 | 85. |
| 90. | 0.17 | 0.03 | 0.06 | -0.00 | 90. |
| 95. | 0.37 | 0.14 | 0.13 | 0.01 | 95. |
| 100. | 0.59 | 0.28 | 0.20 | .03 | 100. |
| 105. | 0.81 | 0.42 | 0.28 | .04 | 105. |
| 110. | 1.02 | 0.55 | 0.36 | 0.06 | 110. |
| 115. | 1.22 | 0.66 | 0.43 | 0.07 | 115. |
| 120. | 1.40 | 0.76 | 0.50 | 0.08 | 120. |
| 125. | 1.54 | 0.83 | 0.54 | 0.09 | 125. |
| 130. | 1.69 | 0.88 | 0.56 | 0.10 | 130. |
| 135. | 1.79 | 0.91 | 0.57 | 0.10 | 135. |
| 140. | 1.87 | 0.92 | 0.57 | 0.10 | 140. |
| 145. | 1.91 | 0.91 | 0.56 | 0.10 | 145. |
| 150. | 1.90 | 0.87 | 0.53 | 0.09 | 150. |
| 155. | 1.84 | 0.83 | 0.48 | 0.08 | 155. |
| 160. | 1.73 | 0.77 | 0.44 | 0.08 | 160. |
| 165. | 1.59 | 0.70 | 0.41 | 0.07 | 165. |
| 170. | 1.41 | 0.61 | 0.35 | 0.06 | 170. |
| 175. | 1.22 | 0.47 | 0.28 | 0.04 | 175. |
| 180. | 0.92 | 0.28 | 0.20 | 0.02 | 180. |
| 185. | 0.49 | 0.10 | 0.12 | 0.02 | 185. |
| 190. | 0.14 | -0.10 | 0.02 | 0.01 | 190. |
| 195. | -0.11 | -0.23 | -0.08 | 0.01 | 195. |
| 200. | -0.35 | -0.23 | -0.17 | -0.00 | 200. |
| 205. | -0.55 | -0.23 | -0.23 | -0.01 | 205. |
| 210. | -0.68 | -0.26 | -0.27 | -0.02 | 210. |
| 215. | -0.56 | -0.33 | -0.31 | -0.04 | 215. |
| 220. | -0.50 | -0.34 | -0.32 | -0.06 | 220. |
| 225. | -0.49 | -0.32 | -0.31 | -0.08 | 225. |
| 230. | -0.5C | -0.32 | -0.30 | -0.09 | 230. |
| 235. | -0.50 | -0.28 | -0.29 | -0.08 | 235. |
| 240. | -0.5C | -0.27 | -0.27 | -0.08 | 240. |
| 245. | -0.48 | -0.25 | -0.25 | -0.08 | 245. |
| 250. | -0.47 | -0.24 | -0.24 | -0.09 | 250. |
| 255. | -0.47 | -0.23 | -0.22 | -0.10 | 255. |
| 260. | -0.48 | -0.22 | -0.21 | -0.10 | 260. |
| 265. | -0.5C | -0.22 | -0.21 | -0.10 | 265. |
| 270. | -0.52 | -0.22 | -0.20 | -0.10 | 270. |
| 275. | -0.54 | -0.22 | -0.19 | -0.10 | 275. |
| 280. | -0.55 | -0.21 | -0.18 | -0.11 | 280. |
| 285. | -0.53 | -0.20 | -0.16 | -0.11 | 285. |
| 290. | -0.51 | -0.19 | -0.17 | -0.10 | 290. |
| 295. | -0.53 | -0.19 | -0.13 | -0.10 | 295. |
| 300. | -0.54 | -0.18 | -0.13 | -0.13 | 300. |
| 305. | -0.54 | -0.19 | -0.12 | -0.12 | 305. |
| 310. | -0.53 | -0.22 | -0.10 | -0.09 | 310. |
| 315. | -0.52 | -0.24 | -0.07 | -0.05 | 315. |
| 320. | -0.52 | -0.24 | -0.05 | -0.00 | 320. |
| 325. | -0.51 | -0.18 | -0.04 | 0.04 | 325. |
| 330. | -0.38 | -0.12 | -0.05 | 0.07 | 330. |
| 335. | -0.48 | -0.17 | -0.06 | 0.08 | 335. |
| 340. | -0.48 | -0.27 | -0.08 | 0.04 | 340. |
| 345. | -0.47 | -0.38 | -0.11 | 0.01 | 345. |
| 350. | -0.77 | -0.35 | -0.10 | 0.04 | 350. |
| 355. | -0.87 | -0.49 | -0.28 | 0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=404 CNTR NO. 256 TCN= 50. C.R.= 10.0

DIFFERENTIAL PRESSURES

SPAN STATION 79.8

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 3.495 | 1.048 | 1.955 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 5. | -2.48 | -1.00 | -1.25 | -0.82 | -0.58 | -0.27 | -0.12 | 0. |
| 5. | -2.42 | -1.03 | -1.23 | -0.73 | -0.51 | -0.15 | 0.01 | 5. |
| 10. | -1.73 | -1.20 | -0.92 | -0.44 | -0.35 | -0.19 | 0.08 | 10. |
| 15. | -0.83 | -0.79 | -0.58 | -0.36 | -0.28 | -0.11 | 0.03 | 15. |
| 20. | -0.97 | -0.82 | -0.63 | -0.38 | -0.29 | -0.13 | -0.03 | 20. |
| 25. | -1.11 | -0.92 | -0.69 | -0.44 | -0.31 | -0.16 | -0.01 | 25. |
| 30. | -1.12 | -0.90 | -0.68 | -0.37 | -0.29 | -0.14 | 0.00 | 30. |
| 35. | -1.01 | -0.77 | -0.61 | -0.31 | -0.21 | -0.15 | -0.01 | 35. |
| 40. | -0.76 | -0.56 | -0.48 | -0.22 | -0.10 | -0.12 | -0.01 | 40. |
| 45. | -0.45 | -0.37 | -0.37 | -0.14 | -0.03 | -0.09 | 0.00 | 45. |
| 50. | -0.17 | -0.23 | -0.29 | -0.08 | -0.03 | -0.10 | 0.00 | 50. |
| 55. | -0.05 | -0.17 | -0.26 | -0.07 | -0.05 | -0.11 | -0.01 | 55. |
| 60. | 0.00 | -0.13 | -0.26 | -0.08 | -0.07 | -0.13 | -0.03 | 60. |
| 65. | 0.02 | -0.11 | -0.27 | -0.10 | -0.05 | -0.15 | -0.04 | 65. |
| 70. | 0.01 | -0.09 | -0.26 | -0.09 | -0.01 | -0.16 | -0.04 | 70. |
| 75. | 0.01 | -0.08 | -0.22 | -0.08 | 0.05 | -0.15 | -0.02 | 75. |
| 80. | 0.03 | -0.06 | -0.17 | -0.02 | 0.11 | -0.13 | -0.01 | 80. |
| 85. | 0.10 | -0.01 | -0.10 | 0.05 | 0.17 | -0.11 | 0.06 | 85. |
| 90. | 0.23 | 0.08 | -0.01 | 0.12 | 0.23 | -0.09 | 0.01 | 90. |
| 95. | 0.44 | 0.23 | 0.11 | 0.21 | 0.30 | -0.06 | 0.22 | 95. |
| 100. | 0.73 | 0.44 | 0.28 | 0.32 | 0.37 | -0.01 | 0.04 | 100. |
| 105. | 1.03 | 0.69 | 0.46 | 0.44 | 0.44 | 0.04 | 0.06 | 105. |
| 110. | 1.32 | 0.92 | 0.63 | 0.55 | 0.54 | 0.09 | 0.07 | 110. |
| 115. | 1.60 | 1.13 | 0.79 | 0.65 | 0.62 | 0.15 | 0.08 | 115. |
| 120. | 1.85 | 1.34 | 0.96 | 0.72 | 0.69 | 0.21 | 0.11 | 120. |
| 125. | 2.08 | 1.54 | 1.06 | 0.76 | 0.74 | 0.25 | 0.14 | 125. |
| 130. | 2.25 | 1.69 | 1.14 | 0.79 | 0.75 | 0.27 | 0.15 | 130. |
| 135. | 2.32 | 1.75 | 1.17 | 0.80 | 0.72 | 0.28 | 0.15 | 135. |
| 140. | 2.31 | 1.77 | 1.18 | 0.78 | 0.67 | 0.27 | 0.14 | 140. |
| 145. | 2.24 | 1.74 | 1.16 | 0.75 | 0.63 | 0.26 | 0.13 | 145. |
| 150. | 2.19 | 1.70 | 1.13 | 0.72 | 0.58 | 0.25 | 0.12 | 150. |
| 155. | 2.10 | 1.65 | 1.12 | 0.71 | 0.56 | 0.25 | 0.12 | 155. |
| 160. | 2.20 | 1.65 | 1.17 | 0.73 | 0.55 | 0.26 | 0.13 | 160. |
| 165. | 2.34 | 1.68 | 1.21 | 0.76 | 0.55 | 0.28 | 0.14 | 165. |
| 170. | 2.36 | 1.69 | 1.22 | 0.78 | 0.57 | 0.30 | 0.15 | 170. |
| 175. | 2.28 | 1.64 | 1.20 | 0.74 | 0.57 | 0.32 | 0.15 | 175. |
| 180. | 2.50 | 1.92 | 1.11 | 0.65 | 0.52 | 0.31 | 0.15 | 180. |
| 185. | 1.58 | 1.28 | 0.92 | 0.53 | 0.38 | 0.28 | 0.13 | 185. |
| 190. | 1.00 | 0.91 | 0.69 | 0.38 | 0.22 | 0.22 | 0.10 | 190. |
| 195. | 0.57 | 0.53 | 0.35 | 0.22 | 0.08 | 0.14 | 0.06 | 195. |
| 200. | 0.11 | 0.32 | 0.17 | 0.05 | -0.04 | 0.08 | 0.03 | 200. |
| 205. | -0.22 | 0.13 | -0.09 | -0.10 | -0.13 | 0.03 | 0.01 | 205. |
| 210. | -0.42 | -0.04 | -0.19 | -0.18 | -0.19 | -0.01 | 0.03 | 210. |
| 215. | -0.52 | -0.24 | -0.25 | -0.22 | -0.23 | -0.05 | -0.01 | 215. |
| 220. | -0.56 | -0.43 | -0.30 | -0.27 | -0.26 | -0.06 | -0.02 | 220. |
| 225. | -0.60 | -0.53 | -0.34 | -0.30 | -0.29 | -0.08 | -0.04 | 225. |
| 230. | -0.78 | -0.57 | -0.36 | -0.33 | -0.31 | -0.09 | -0.05 | 230. |
| 235. | -0.82 | -0.60 | -0.37 | -0.33 | -0.32 | -0.10 | -0.06 | 235. |
| 240. | -0.85 | -0.60 | -0.36 | -0.32 | -0.33 | -0.09 | -0.07 | 240. |
| 245. | -0.84 | -0.61 | -0.35 | -0.30 | -0.33 | -0.09 | -0.08 | 245. |
| 250. | -0.85 | -0.61 | -0.34 | -0.29 | -0.33 | -0.09 | -0.09 | 250. |
| 255. | -0.83 | -0.60 | -0.33 | -0.29 | -0.33 | -0.09 | -0.10 | 255. |
| 260. | -0.82 | -0.59 | -0.32 | -0.29 | -0.31 | -0.09 | -0.10 | 260. |
| 265. | -0.81 | -0.58 | -0.31 | -0.28 | -0.30 | -0.09 | -0.11 | 265. |
| 270. | -0.81 | -0.57 | -0.30 | -0.26 | -0.29 | -0.08 | -0.11 | 270. |
| 275. | -0.81 | -0.56 | -0.29 | -0.26 | -0.27 | -0.07 | -0.10 | 275. |
| 280. | -0.82 | -0.56 | -0.28 | -0.25 | -0.27 | -0.07 | -0.10 | 280. |
| 285. | -0.81 | -0.57 | -0.28 | -0.26 | -0.28 | -0.08 | -0.10 | 285. |
| 290. | -0.81 | -0.57 | -0.28 | -0.27 | -0.28 | -0.07 | -0.09 | 290. |
| 295. | -0.82 | -0.57 | -0.28 | -0.26 | -0.27 | -0.08 | -0.11 | 295. |
| 300. | -0.82 | -0.58 | -0.28 | -0.25 | -0.25 | -0.08 | -0.14 | 300. |
| 305. | -0.82 | -0.58 | -0.26 | -0.24 | -0.23 | -0.01 | -0.14 | 305. |
| 310. | -0.82 | -0.58 | -0.24 | -0.23 | -0.22 | 0.00 | -0.12 | 310. |
| 315. | -0.81 | -0.55 | -0.23 | -0.21 | -0.21 | 0.01 | -0.10 | 315. |
| 320. | -0.81 | -0.52 | -0.22 | -0.20 | -0.20 | 0.02 | -0.07 | 320. |
| 325. | -0.79 | -0.48 | -0.23 | -0.20 | -0.18 | 0.01 | -0.01 | 325. |
| 330. | -0.76 | -0.43 | -0.26 | -0.21 | -0.17 | 0.02 | 0.03 | 330. |
| 335. | -0.78 | -0.45 | -0.31 | -0.23 | -0.20 | -0.02 | 0.03 | 335. |
| 340. | -0.83 | -0.65 | -0.39 | -0.28 | -0.24 | -0.11 | -0.05 | 340. |
| 345. | -0.73 | -0.61 | -0.47 | -0.36 | -0.28 | -0.09 | -0.04 | 345. |
| 350. | -0.92 | -0.79 | -0.59 | -0.45 | -0.42 | -0.15 | -0.10 | 350. |
| 355. | -1.48 | -1.27 | -0.83 | -0.54 | -0.52 | -0.27 | -0.17 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 256 TCN= 90. C.R.= 10.0

DIFFERENTIAL PRESSURES

SPAN STATION 119.7

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -2.06 | -1.45 | -0.80 | -0.44 | -0.50 | -0.17 | -0.03 | 0. |
| 5. | -2.20 | -1.78 | -1.05 | -0.82 | -0.58 | -0.25 | -0.08 | 5. |
| 10. | -2.15 | -1.73 | -1.10 | -0.81 | -0.59 | -0.35 | -0.15 | 10. |
| 15. | -1.91 | -1.52 | -0.98 | -0.72 | -0.48 | -0.34 | -0.19 | 15. |
| 20. | -1.22 | -1.12 | -0.71 | -0.52 | -0.28 | -0.20 | -0.. | 20. |
| 25. | -0.54 | -0.61 | -0.35 | -0.24 | -0.08 | -0.12 | -0.11 | 25. |
| 30. | -0.13 | -0.23 | -0.09 | -0.09 | 0.01 | -0.04 | -0.12 | 30. |
| 35. | 0.11 | 0.01 | 0.06 | 0.02 | 0.06 | -0.05 | -0.09 | 35. |
| 40. | 0.44 | 0.16 | 0.16 | 0.08 | 0.11 | -0.08 | -0.08 | 40. |
| 45. | 0.83 | 0.26 | 0.23 | 0.13 | 0.23 | -0.04 | -0.10 | 45. |
| 50. | 1.12 | 0.34 | 0.35 | 0.18 | 0.37 | -0.09 | -0.13 | 50. |
| 55. | 1.23 | 0.39 | 0.36 | 0.21 | 0.45 | -0.09 | -0.15 | 55. |
| 60. | 1.22 | 0.40 | 0.30 | 0.20 | 0.49 | -0.10 | -0.14 | 60. |
| 65. | 1.14 | 0.37 | 0.22 | 0.15 | 0.48 | -0.11 | -0.13 | 65. |
| 70. | 1.00 | 0.26 | 0.08 | 0.09 | 0.45 | -0.15 | -0.14 | 70. |
| 75. | 0.83 | 0.08 | -0.06 | 0.01 | 0.40 | -0.17 | -0.15 | 75. |
| 80. | 0.64 | -0.03 | -0.16 | -0.07 | 0.35 | -0.15 | -0.13 | 80. |
| 85. | 0.65 | -0.02 | -0.14 | -0.08 | 0.32 | -0.11 | -0.11 | 85. |
| 90. | 0.85 | 0.11 | -0.03 | 0.01 | 0.36 | -0.07 | -0.09 | 90. |
| 95. | 1.19 | 0.40 | 0.18 | 0.15 | 0.43 | -0.05 | -0.07 | 95. |
| 100. | 1.59 | 0.77 | 0.42 | 0.32 | 0.54 | -0.02 | -0.05 | 100. |
| 105. | 1.95 | 1.15 | 0.61 | 0.44 | 0.62 | -0.02 | -0.04 | 105. |
| 110. | 2.14 | 1.30 | 0.67 | 0.53 | 0.64 | 0.01 | -0.04 | 110. |
| 115. | 2.16 | 1.37 | 0.68 | 0.54 | 0.58 | 0.01 | -0.04 | 115. |
| 120. | 1.99 | 1.25 | 0.57 | 0.44 | 0.46 | 0.01 | -0.04 | 120. |
| 125. | 1.38 | 0.82 | 0.26 | 0.15 | 0.35 | 0.00 | -0.01 | 125. |
| 130. | 0.57 | 0.32 | 0.00 | 0.02 | 0.26 | -0.01 | 0.00 | 130. |
| 135. | 0.53 | 0.17 | -0.05 | -0.01 | 0.20 | -0.02 | 0.01 | 135. |
| 140. | 0.62 | 0.24 | -0.04 | 0.02 | 0.18 | -0.02 | 0.01 | 140. |
| 145. | 0.61 | 0.32 | 0.12 | 0.07 | 0.18 | 0.00 | 0.02 | 145. |
| 150. | 0.62 | 0.44 | 0.13 | 0.13 | 0.18 | 0.05 | 0.03 | 150. |
| 155. | 0.77 | 0.56 | 0.26 | 0.20 | 0.20 | 0.11 | 0.06 | 155. |
| 160. | 0.99 | 0.75 | 0.40 | 0.30 | 0.22 | 0.16 | 0.08 | 160. |
| 165. | 1.19 | 0.94 | 0.53 | 0.41 | 0.25 | 0.20 | 0.09 | 165. |
| 170. | 1.34 | 1.10 | 0.64 | 0.49 | 0.29 | 0.23 | 0.12 | 170. |
| 175. | 1.44 | 1.21 | 0.77 | 0.55 | 0.33 | 0.27 | 0.14 | 175. |
| 180. | 1.37 | 1.23 | 0.84 | 0.58 | 0.33 | 0.29 | 0.15 | 180. |
| 185. | 1.29 | 1.15 | 0.81 | 0.54 | 0.29 | 0.29 | 0.15 | 185. |
| 190. | 0.80 | 1.01 | 0.66 | 0.47 | 0.22 | 0.27 | 0.14 | 190. |
| 195. | 0.59 | 0.80 | 0.51 | 0.39 | 0.13 | 0.23 | 0.12 | 195. |
| 200. | 0.38 | 0.56 | 0.39 | 0.30 | 0.03 | 0.17 | 0.10 | 200. |
| 205. | 0.16 | 0.34 | 0.28 | 0.21 | -0.05 | 0.10 | 0.09 | 205. |
| 210. | -0.20 | 0.15 | 0.18 | 0.12 | -0.13 | 0.07 | 0.08 | 210. |
| 215. | -0.31 | -0.01 | 0.09 | 0.06 | -0.17 | 0.06 | 0.07 | 215. |
| 220. | -0.45 | -0.11 | 0.01 | -0.00 | -0.21 | 0.05 | 0.07 | 220. |
| 225. | -0.55 | -0.18 | -0.06 | -0.05 | -0.23 | 0.04 | 0.07 | 225. |
| 230. | -0.64 | -0.24 | -0.11 | -0.10 | -0.26 | 0.02 | 0.07 | 230. |
| 235. | -0.77 | -0.32 | -0.15 | -0.13 | -0.29 | 0.01 | 0.05 | 235. |
| 240. | -0.88 | -0.40 | -0.19 | -0.16 | -0.31 | 0.01 | 0.03 | 240. |
| 245. | -0.96 | -0.47 | -0.23 | -0.18 | -0.33 | 0.00 | 0.03 | 245. |
| 250. | -1.01 | -0.49 | -0.26 | -0.20 | -0.35 | -0.02 | 0.03 | 250. |
| 255. | -1.05 | -0.50 | -0.26 | -0.21 | -0.35 | -0.01 | 0.03 | 255. |
| 260. | -1.04 | -0.50 | -0.29 | -0.21 | -0.35 | -0.01 | 0.04 | 260. |
| 265. | -1.02 | -0.49 | -0.29 | -0.22 | -0.35 | -0.01 | 0.05 | 265. |
| 270. | -0.99 | -0.48 | -0.29 | -0.22 | -0.35 | -0.00 | 0.04 | 270. |
| 275. | -0.99 | -0.47 | -0.29 | -0.22 | -0.34 | 0.00 | 0.05 | 275. |
| 280. | -1.02 | -0.47 | -0.28 | -0.21 | -0.34 | 0.01 | 0.06 | 280. |
| 285. | -1.03 | -0.48 | -0.28 | -0.21 | -0.33 | 0.02 | 0.06 | 285. |
| 290. | -1.03 | -0.49 | -0.25 | -0.21 | -0.32 | 0.03 | 0.06 | 290. |
| 295. | -1.03 | -0.50 | -0.24 | -0.21 | -0.32 | 0.03 | 0.05 | 295. |
| 300. | -1.02 | -0.50 | -0.24 | -0.20 | -0.32 | 0.04 | 0.05 | 300. |
| 305. | -1.02 | -0.50 | -0.25 | -0.20 | -0.32 | 0.04 | 0.05 | 305. |
| 310. | -1.01 | -0.51 | -0.26 | -0.19 | -0.31 | 0.04 | 0.06 | 310. |
| 315. | -1.00 | -0.51 | -0.26 | -0.19 | -0.31 | 0.03 | 0.06 | 315. |
| 320. | -0.95 | -0.52 | -0.24 | -0.17 | -0.30 | 0.03 | 0.05 | 320. |
| 325. | -0.89 | -0.50 | -0.22 | -0.16 | -0.27 | 0.03 | 0.04 | 325. |
| 330. | -0.80 | -0.43 | -0.18 | -0.14 | -0.20 | 0.03 | 0.03 | 330. |
| 335. | -0.69 | -0.33 | -0.10 | -0.07 | -0.15 | 0.03 | 0.02 | 335. |
| 340. | -0.55 | -0.26 | -0.05 | -0.04 | -0.13 | 0.04 | 0.02 | 340. |
| 345. | -0.51 | -0.27 | -0.06 | -0.06 | -0.15 | 0.02 | 0.01 | 345. |
| 350. | -0.69 | -0.41 | -0.17 | -0.10 | -0.25 | -0.02 | -0.01 | 350. |
| 355. | -1.31 | -0.92 | -0.49 | -0.28 | -0.38 | -0.12 | -0.02 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 256 TCN= 50. C.R.= 10.0

DIFFERENTIAL PRESSURES

SPAN STATION 153.3

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.67 | -0.61 | -0.32 | -0.56 | -0.29 | -0.03 | -0.32 | 5. |
| 5. | -0.17 | -0.20 | -0.15 | -0.36 | -0.10 | 0.07 | 0.02 | 5. |
| 10. | -0.83 | -0.44 | -0.46 | -0.45 | -0.27 | -0.06 | -0.01 | 10. |
| 15. | -1.14 | -0.95 | -0.76 | -0.55 | -0.39 | -0.21 | -0.05 | 15. |
| 20. | -0.79 | -0.71 | -0.66 | -0.44 | -0.29 | -0.24 | -0.07 | 20. |
| 25. | -0.17 | -0.24 | -0.32 | -0.21 | -0.13 | -0.10 | -0.04 | 25. |
| 30. | 0.56 | 0.26 | 0.12 | 0.05 | 0.03 | -0.10 | 0.01 | 30. |
| 35. | 1.24 | 0.69 | 0.25 | 0.31 | 0.18 | -0.03 | 0.01 | 35. |
| 40. | 1.68 | 1.02 | 0.33 | 0.51 | 0.32 | -0.02 | 0.00 | 40. |
| 45. | 1.86 | 1.26 | 0.50 | 0.77 | 0.44 | -0.05 | 0.02 | 45. |
| 50. | 1.94 | 1.41 | 0.66 | 0.92 | 0.53 | 0.01 | 0.03 | 50. |
| 55. | 1.86 | 1.47 | 0.74 | 1.03 | 0.59 | 0.03 | 0.03 | 55. |
| 60. | 1.65 | 1.43 | 0.73 | 1.07 | 0.61 | 0.01 | 0.02 | 60. |
| 65. | 1.28 | 1.25 | 0.64 | 1.06 | 0.60 | -0.04 | -0.02 | 65. |
| 70. | 0.86 | 0.92 | 0.48 | 0.98 | 0.55 | -0.12 | -0.05 | 70. |
| 75. | 0.50 | 0.65 | 0.21 | 0.91 | 0.46 | -0.17 | -0.07 | 75. |
| 80. | 0.26 | 0.46 | -0.06 | 0.85 | 0.42 | -0.19 | -0.08 | 80. |
| 85. | 0.15 | 0.37 | -0.24 | 0.80 | 0.36 | -0.20 | -0.09 | 85. |
| 90. | 0.17 | 0.44 | -0.33 | 0.84 | 0.30 | -0.32 | -0.09 | 90. |
| 95. | 0.29 | 0.63 | -0.23 | 1.00 | 0.35 | -0.32 | -0.08 | 95. |
| 100. | 0.40 | 0.87 | -0.17 | 1.11 | 0.18 | -0.29 | -0.07 | 100. |
| 105. | -0.12 | 0.29 | -0.35 | 0.64 | 0.12 | -0.23 | -0.07 | 105. |
| 110. | -0.70 | -0.10 | -0.67 | 0.27 | 0.10 | -0.23 | -0.08 | 110. |
| 115. | -0.81 | -0.22 | -0.83 | 0.09 | 0.06 | -0.27 | -0.10 | 115. |
| 120. | -0.76 | -0.23 | -0.90 | 0.02 | -0.01 | -0.29 | -0.11 | 120. |
| 125. | -0.90 | -0.40 | -0.96 | -0.04 | -0.09 | -0.33 | -0.13 | 125. |
| 130. | -1.12 | -0.64 | -0.99 | -0.17 | -0.16 | -0.38 | -0.13 | 130. |
| 135. | -1.35 | -0.86 | -0.98 | -0.25 | -0.21 | -0.38 | -0.14 | 135. |
| 140. | -1.49 | -0.93 | -0.94 | -0.28 | -0.22 | -0.28 | -0.14 | 140. |
| 145. | -1.46 | -0.92 | -0.85 | -0.28 | -0.18 | -0.25 | -0.12 | 145. |
| 150. | -1.29 | -0.85 | -0.72 | -0.24 | -0.12 | -0.21 | -0.13 | 150. |
| 155. | -0.95 | -0.59 | -0.52 | -0.16 | -0.04 | -0.15 | -0.08 | 155. |
| 160. | -0.53 | -0.14 | -0.29 | -0.05 | 0.05 | -0.07 | -0.05 | 160. |
| 165. | -0.11 | 0.24 | -0.05 | 0.07 | 0.10 | 0.02 | -0.02 | 165. |
| 170. | 0.20 | 0.48 | 0.19 | 0.17 | 0.31 | 0.13 | 0.01 | 170. |
| 175. | 0.40 | 0.57 | 0.41 | 0.25 | 0.42 | 0.15 | 0.03 | 175. |
| 180. | 0.80 | 0.98 | 0.56 | 0.29 | 0.42 | 0.18 | 0.03 | 180. |
| 185. | 0.91 | 0.94 | 0.65 | 0.31 | 0.34 | 0.19 | 0.02 | 185. |
| 190. | 0.92 | 0.89 | 0.68 | 0.28 | 0.24 | 0.19 | 0.02 | 190. |
| 195. | 0.84 | 0.86 | 0.67 | 0.23 | 0.15 | 0.21 | 0.02 | 195. |
| 200. | 0.71 | 0.80 | 0.62 | 0.15 | 0.10 | 0.21 | 0.03 | 200. |
| 205. | 0.56 | 0.71 | 0.54 | 0.07 | 0.06 | 0.19 | 0.03 | 205. |
| 210. | 0.40 | 0.59 | 0.45 | -0.02 | 0.04 | 0.19 | 0.04 | 210. |
| 215. | 0.27 | 0.47 | 0.41 | -0.09 | 0.01 | 0.18 | 0.04 | 215. |
| 220. | 0.17 | -0.02 | 0.37 | -0.16 | -0.04 | 0.17 | 0.04 | 220. |
| 225. | 0.08 | -0.11 | 0.33 | -0.21 | -0.08 | 0.17 | 0.05 | 225. |
| 230. | 0.00 | -0.20 | 0.29 | -0.26 | -0.12 | 0.17 | 0.05 | 230. |
| 235. | -0.08 | -0.28 | 0.25 | -0.30 | -0.15 | 0.17 | 0.05 | 235. |
| 240. | -0.15 | -0.31 | 0.21 | -0.34 | -0.18 | 0.16 | 0.05 | 240. |
| 245. | -0.21 | -0.32 | 0.17 | -0.38 | -0.21 | 0.15 | 0.05 | 245. |
| 250. | -0.25 | -0.33 | 0.14 | -0.41 | -0.23 | 0.14 | 0.05 | 250. |
| 255. | -0.29 | -0.35 | 0.11 | -0.44 | -0.25 | 0.14 | 0.05 | 255. |
| 260. | -0.32 | -0.39 | 0.08 | -0.44 | -0.28 | 0.13 | 0.05 | 260. |
| 265. | -0.34 | -0.43 | 0.06 | -0.40 | -0.29 | 0.13 | 0.05 | 265. |
| 270. | -0.36 | -0.44 | 0.05 | -0.50 | -0.30 | 0.13 | 0.05 | 270. |
| 275. | -0.37 | -0.43 | 0.05 | -0.51 | -0.29 | 0.13 | 0.05 | 275. |
| 280. | -0.36 | -0.41 | 0.06 | -0.50 | -0.27 | 0.14 | 0.04 | 280. |
| 285. | -0.34 | -0.38 | 0.07 | -0.49 | -0.24 | 0.15 | 0.03 | 285. |
| 290. | -0.30 | -0.34 | 0.09 | -0.47 | -0.22 | 0.17 | 0.02 | 290. |
| 295. | -0.26 | -0.30 | 0.11 | -0.43 | -0.21 | 0.19 | 0.00 | 295. |
| 300. | -0.19 | -0.26 | 0.15 | -0.39 | -0.19 | 0.19 | 0.00 | 300. |
| 305. | -0.12 | -0.18 | 0.18 | -0.36 | -0.16 | 0.18 | 0.00 | 305. |
| 310. | -0.03 | -0.08 | 0.21 | -0.34 | -0.16 | 0.18 | 0.00 | 310. |
| 315. | 0.12 | -0.03 | 0.22 | -0.33 | -0.16 | 0.17 | 0.00 | 315. |
| 320. | 0.18 | -0.04 | 0.23 | -0.32 | -0.16 | 0.16 | 0.00 | 320. |
| 325. | 0.00 | -0.10 | 0.19 | -0.32 | -0.18 | 0.14 | 0.00 | 325. |
| 330. | -0.24 | -0.44 | 0.05 | -0.39 | -0.23 | 0.10 | 0.00 | 330. |
| 335. | -0.59 | -0.60 | -0.12 | -0.51 | -0.29 | 0.03 | -0.01 | 335. |
| 340. | -0.64 | -0.62 | -0.25 | -0.59 | -0.33 | -0.02 | 0.01 | 340. |
| 345. | -0.41 | -0.47 | -0.15 | -0.52 | -0.31 | -0.02 | -0.00 | 345. |
| 350. | -0.08 | -0.28 | -0.03 | -0.38 | -0.25 | 0.00 | -0.01 | 350. |
| 355. | -0.16 | -0.49 | -0.10 | -0.39 | -0.24 | -0.03 | -0.01 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 256 TCN= 90. C.R.= 10.0

DIFFERENTIAL PRESSURES

SPAN STATION 170.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -0.39 | -0.42 | -0.18 | -0.08 | -0.23 | -0.13 | -0.05 | 0. |
| 5. | -1.04 | -0.90 | -0.26 | -0.11 | -0.29 | -0.12 | -0.04 | 5. |
| 10. | -0.80 | -0.57 | -0.35 | -0.07 | -0.23 | -0.13 | -0.05 | 10. |
| 15. | -0.75 | -0.32 | -0.31 | -0.06 | -0.19 | -0.15 | -0.05 | 15. |
| 20. | -0.68 | -0.24 | -0.22 | -0.04 | -0.10 | -0.11 | -0.04 | 20. |
| 25. | 0.07 | 0.02 | -0.10 | 0.00 | 0.04 | -0.06 | -0.01 | 25. |
| 30. | 0.66 | 0.45 | 0.01 | 0.20 | 0.22 | 0.02 | 0.01 | 30. |
| 35. | 1.01 | 0.72 | 0.15 | 0.29 | 0.36 | 0.07 | 0.03 | 35. |
| 40. | 1.20 | 0.92 | 0.39 | 0.40 | 0.52 | 0.15 | 0.05 | 40. |
| 45. | 1.27 | 1.00 | 0.64 | 0.55 | 0.74 | 0.23 | 0.08 | 45. |
| 50. | 1.32 | 1.04 | 0.87 | 0.70 | 0.91 | 0.28 | 0.09 | 50. |
| 55. | 1.31 | 1.00 | 1.02 | 1.00 | 1.02 | 0.28 | 0.07 | 55. |
| 60. | 1.15 | 0.99 | 1.04 | 1.20 | 0.98 | 0.21 | 0.04 | 60. |
| 65. | 0.90 | 0.18 | 0.79 | 0.89 | 1.42 | 0.11 | 0.00 | 65. |
| 70. | 0.59 | -0.02 | 0.48 | 0.50 | 1.05 | -0.04 | -0.04 | 70. |
| 75. | 0.27 | -0.06 | 0.19 | 0.24 | 1.67 | -0.28 | -0.08 | 75. |
| 80. | -0.02 | -0.08 | 0.42 | 0.14 | 1.02 | -0.48 | -0.11 | 80. |
| 85. | -0.13 | -0.56 | 0.06 | 2.00 | 0.54 | -0.57 | -0.11 | 85. |
| 90. | -0.54 | -1.04 | -0.47 | -0.08 | 0.11 | -0.65 | -0.07 | 90. |
| 95. | -1.36 | -1.50 | -0.93 | -0.33 | -0.33 | -0.44 | 0.01 | 95. |
| 100. | -1.59 | -1.81 | -1.15 | -0.50 | -0.56 | -1.05 | 0.09 | 100. |
| 105. | -1.53 | -1.98 | -1.09 | -0.57 | -0.55 | -0.83 | 0.13 | 105. |
| 110. | -1.48 | -1.97 | -0.86 | -0.60 | -0.49 | -0.46 | 0.12 | 110. |
| 115. | -1.33 | -1.94 | -0.86 | -0.64 | -0.47 | -0.27 | 0.05 | 115. |
| 120. | -1.34 | -2.08 | -1.24 | -0.73 | -1.05 | 0.23 | -0.01 | 120. |
| 125. | -1.49 | -2.36 | -1.66 | -0.90 | -2.74 | 0.15 | -0.02 | 125. |
| 130. | -1.77 | -2.69 | -2.06 | -1.03 | -1.44 | 0.02 | -0.02 | 130. |
| 135. | -2.22 | -3.02 | -2.40 | -1.11 | 0.00 | -0.18 | -0.03 | 135. |
| 140. | -2.62 | -3.27 | -2.62 | -1.15 | -0.21 | -0.30 | -0.05 | 140. |
| 145. | -2.89 | -3.26 | -2.65 | -1.19 | -0.61 | -0.33 | -0.03 | 145. |
| 150. | -2.54 | -3.00 | -2.33 | -1.09 | -0.61 | -0.30 | -0.04 | 150. |
| 155. | -2.21 | -2.55 | -1.92 | -1.00 | -0.52 | -0.23 | -0.02 | 155. |
| 160. | -1.76 | -1.93 | -1.55 | -0.84 | -0.39 | -0.16 | -0.00 | 160. |
| 165. | -1.23 | -1.26 | -1.15 | -0.65 | -0.27 | -0.09 | 0.01 | 165. |
| 170. | -0.65 | -0.66 | -0.71 | -0.47 | -0.15 | -0.02 | 0.03 | 170. |
| 175. | -0.11 | -0.10 | -0.27 | -0.30 | -0.05 | 0.04 | 0.04 | 175. |
| 180. | 0.31 | 0.27 | 0.11 | -0.14 | 0.04 | 0.12 | 0.04 | 180. |
| 185. | 0.63 | 0.57 | 0.34 | -0.02 | 0.10 | 0.14 | 0.04 | 185. |
| 190. | 0.84 | 0.78 | 0.49 | 0.07 | 0.13 | 0.15 | 0.04 | 190. |
| 195. | 0.92 | 0.90 | 0.56 | 0.13 | 0.12 | 0.16 | 0.03 | 195. |
| 200. | 0.90 | 0.96 | 0.60 | 0.16 | 0.09 | 0.16 | 0.01 | 200. |
| 205. | 0.82 | 0.96 | 0.61 | 0.18 | 0.04 | 0.16 | -0.01 | 205. |
| 210. | 0.74 | 0.94 | 0.62 | 0.18 | 0.02 | 0.16 | 0.01 | 210. |
| 215. | 0.69 | 0.95 | 0.62 | 0.17 | 0.01 | 0.15 | 0.02 | 215. |
| 220. | 0.63 | 0.96 | 0.62 | 0.15 | -0.00 | 0.16 | 0.02 | 220. |
| 225. | 0.57 | 0.97 | 0.61 | 0.15 | -0.01 | 0.16 | 0.02 | 225. |
| 230. | 0.54 | 0.97 | 0.60 | 0.15 | -0.01 | 0.16 | 0.02 | 230. |
| 235. | 0.52 | 0.97 | 0.61 | 0.16 | 0.00 | 0.18 | 0.01 | 235. |
| 240. | 0.51 | 0.98 | 0.62 | 0.17 | -0.00 | 0.19 | 0.01 | 240. |
| 245. | 0.51 | 0.98 | 0.63 | 0.17 | -0.01 | 0.19 | 0.00 | 245. |
| 250. | 0.51 | 0.98 | 0.64 | 0.18 | -0.01 | 0.19 | -0.01 | 250. |
| 255. | 0.52 | 0.99 | 0.64 | 0.17 | -0.10 | 0.18 | -0.01 | 255. |
| 260. | 0.53 | 0.99 | 0.63 | 0.17 | -0.11 | 0.18 | -0.01 | 260. |
| 265. | 0.53 | 1.00 | 0.63 | 0.17 | -0.11 | 0.18 | -0.01 | 265. |
| 270. | 0.54 | 1.01 | 0.62 | 0.17 | -0.10 | 0.18 | -0.01 | 270. |
| 275. | 0.55 | 1.02 | 0.63 | 0.19 | -0.08 | 0.18 | -0.01 | 275. |
| 280. | 0.57 | 1.03 | 0.65 | 0.21 | -0.06 | 0.19 | -0.01 | 280. |
| 285. | 0.60 | 1.05 | 0.67 | 0.23 | -0.05 | 0.20 | -0.01 | 285. |
| 290. | 0.64 | 1.07 | 0.70 | 0.26 | -0.03 | 0.21 | -0.00 | 290. |
| 295. | 0.70 | 1.12 | 0.73 | 0.29 | -0.00 | 0.22 | 0.01 | 295. |
| 300. | 0.76 | 1.17 | 0.76 | 0.33 | 0.02 | 0.23 | 0.01 | 300. |
| 305. | 0.81 | 1.21 | 0.80 | 0.36 | 0.05 | 0.24 | 0.02 | 305. |
| 310. | 0.85 | 1.24 | 0.82 | 0.39 | 0.07 | 0.24 | 0.02 | 310. |
| 315. | 0.87 | 1.25 | 0.82 | 0.42 | 0.10 | 0.24 | 0.02 | 315. |
| 320. | 0.88 | 1.32 | 0.81 | 0.44 | 0.12 | 0.23 | 0.02 | 320. |
| 325. | 1.18 | 1.40 | 0.79 | 0.43 | 0.13 | 0.22 | 0.01 | 325. |
| 330. | 1.46 | 1.49 | 0.82 | 0.39 | 0.12 | 0.21 | 0.00 | 330. |
| 335. | 1.43 | 1.36 | 0.81 | 0.32 | 0.09 | 0.18 | -0.01 | 335. |
| 340. | 0.81 | 1.02 | 0.59 | 0.22 | 0.01 | 0.11 | -0.03 | 340. |
| 345. | -0.24 | 0.31 | 0.22 | 0.11 | -0.10 | 0.02 | -0.05 | 345. |
| 350. | -0.59 | -0.06 | -0.12 | 0.00 | -0.24 | -0.07 | -0.07 | 350. |
| 355. | -0.84 | -0.20 | -0.27 | -0.08 | -0.22 | -0.11 | -0.07 | 355. |

## DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST-494 CNTR NO. 256 TCN= 5C. C.R.= 10.0

DIFFERENTIAL PRESSURES

SPAN STATION 189.0

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.495 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 10.430 | DEG. |
| 5. | -0.66 | -0.45 | -0.60 | -0.09 | 0.02 | 0.25 | -0.03 | 5. |
| 5. | -0.64 | -0.39 | -0.54 | -0.06 | 0.02 | 0.10 | 0.01 | 5. |
| 10. | -0.49 | -0.41 | -0.51 | -0.11 | 0.02 | 0.27 | -0.01 | 10. |
| 15. | -0.52 | -0.44 | -0.47 | -0.14 | 0.06 | 0.23 | -0.01 | 15. |
| 20. | -0.36 | -0.22 | -0.43 | -0.05 | 0.10 | 0.30 | 0.01 | 20. |
| 25. | 0.28 | 0.18 | -0.13 | 0.16 | 0.17 | 0.14 | 0.04 | 25. |
| 30. | 0.04 | 0.49 | 0.15 | 0.23 | 0.31 | 0.16 | 0.06 | 30. |
| 35. | 1.19 | 0.74 | 0.41 | 0.33 | 0.50 | 0.20 | 0.08 | 35. |
| 40. | 1.36 | 0.91 | 0.87 | 0.39 | 0.06 | 0.25 | 0.05 | 40. |
| 45. | 1.52 | 1.01 | 1.48 | 0.64 | 1.12 | 0.29 | 0.08 | 45. |
| 50. | 1.66 | 1.03 | 1.83 | 1.19 | 1.26 | 0.33 | 0.09 | 50. |
| 55. | 1.54 | 0.97 | 1.78 | 1.47 | 1.65 | 0.25 | 0.03 | 55. |
| 60. | 1.38 | 0.83 | 1.55 | 0.95 | 2.26 | 0.13 | -0.02 | 60. |
| 65. | 1.20 | 0.63 | 1.34 | 0.29 | 2.19 | -0.17 | -0.09 | 65. |
| 70. | 0.75 | 0.48 | 1.19 | -0.11 | 1.39 | -0.28 | -0.18 | 70. |
| 75. | 0.39 | 0.12 | 1.13 | -0.10 | 0.73 | -0.27 | -0.23 | 75. |
| 80. | -0.01 | -0.19 | 1.12 | -0.21 | 0.55 | -0.34 | -0.21 | 80. |
| 85. | -0.02 | -0.03 | 0.74 | -0.42 | 0.09 | -0.44 | -0.03 | 85. |
| 90. | -1.45 | -1.44 | 0.17 | -0.81 | -0.64 | -0.84 | 0.04 | 90. |
| 95. | -1.83 | -1.94 | -0.16 | -1.03 | -0.91 | -0.95 | 0.04 | 95. |
| 100. | -1.81 | -2.13 | -0.29 | -1.09 | -0.85 | -1.47 | -0.01 | 100. |
| 105. | -1.78 | -2.08 | -0.37 | -1.03 | -0.80 | -0.85 | -0.01 | 105. |
| 110. | -1.64 | -1.96 | -0.45 | -1.01 | -0.72 | -0.59 | 0.18 | 110. |
| 115. | -1.43 | -1.99 | -0.62 | -1.02 | -0.66 | -0.76 | 0.22 | 115. |
| 120. | -1.72 | -1.98 | -0.75 | -1.08 | -0.69 | -0.72 | 0.24 | 120. |
| 125. | -1.84 | -2.05 | -0.85 | -1.15 | -0.67 | -0.32 | 0.16 | 125. |
| 130. | -1.97 | -2.17 | -1.08 | -1.30 | -2.96 | 0.38 | 0.08 | 130. |
| 135. | -2.31 | -2.38 | -1.57 | -2.05 | -2.33 | 0.35 | 0.05 | 135. |
| 140. | -2.78 | -2.76 | -2.28 | -3.28 | -0.67 | 0.97 | -0.07 | 140. |
| 145. | -3.10 | -3.02 | -2.79 | -2.85 | -0.18 | -0.18 | -0.09 | 145. |
| 150. | -3.17 | -2.88 | -2.64 | -1.38 | -0.39 | -0.21 | -0.09 | 150. |
| 155. | -2.94 | -2.36 | -2.22 | -1.11 | -0.47 | -0.13 | -0.00 | 155. |
| 160. | -2.58 | -1.66 | -1.62 | -0.80 | -0.48 | -0.25 | -0.06 | 160. |
| 165. | -1.91 | -1.18 | -1.19 | -0.65 | -0.38 | 0.34 | -0.05 | 165. |
| 170. | -1.26 | -0.50 | -0.84 | -0.39 | -0.18 | 0.12 | -0.03 | 170. |
| 175. | -0.62 | -0.13 | -0.45 | -0.14 | -0.06 | 0.18 | -0.01 | 175. |
| 180. | -0.05 | 0.28 | -0.13 | 0.09 | 0.05 | 0.24 | -0.01 | 180. |
| 185. | 0.40 | 0.58 | 0.10 | 0.27 | 0.11 | 0.27 | -0.01 | 185. |
| 190. | 0.69 | 0.73 | 0.21 | 0.39 | 0.12 | 0.28 | -0.01 | 190. |
| 195. | 0.77 | 0.80 | 0.24 | 0.42 | 0.09 | 0.29 | -0.03 | 195. |
| 200. | 0.76 | 0.84 | 0.25 | 0.40 | 0.04 | 0.28 | -0.04 | 200. |
| 205. | 0.75 | 0.84 | 0.23 | 0.41 | -0.01 | 0.28 | -0.04 | 205. |
| 210. | 0.71 | 0.81 | 0.21 | 0.42 | -0.06 | 0.28 | -0.03 | 210. |
| 215. | 0.66 | 0.78 | 0.18 | 0.44 | -0.10 | 0.28 | -0.02 | 215. |
| 220. | 0.63 | 0.76 | 0.18 | 0.46 | -0.11 | 0.28 | -0.02 | 220. |
| 225. | 0.62 | 0.75 | 0.18 | 0.47 | -0.10 | 0.29 | -0.01 | 225. |
| 230. | 0.64 | 0.78 | 0.19 | 0.49 | -0.08 | 0.30 | -0.01 | 230. |
| 235. | 0.68 | 0.82 | 0.20 | 0.51 | -0.07 | 0.31 | -0.01 | 235. |
| 240. | 0.73 | 0.88 | 0.21 | 0.54 | -0.07 | 0.32 | -0.00 | 240. |
| 245. | 0.76 | 0.90 | 0.23 | 0.56 | -0.07 | 0.32 | -0.00 | 245. |
| 250. | 0.77 | 0.92 | 0.24 | 0.57 | -0.08 | 0.32 | -0.01 | 250. |
| 255. | 0.76 | 0.92 | 0.25 | 0.58 | -0.08 | 0.32 | -0.01 | 255. |
| 260. | 0.76 | 0.90 | 0.26 | 0.58 | -0.08 | 0.31 | -0.02 | 260. |
| 265. | 0.76 | 0.89 | 0.28 | 0.59 | -0.08 | 0.31 | -0.01 | 265. |
| 270. | 0.77 | 0.90 | 0.29 | 0.58 | -0.07 | 0.31 | -0.01 | 270. |
| 275. | 0.79 | 0.92 | 0.30 | 0.58 | -0.07 | 0.31 | -0.01 | 275. |
| 280. | 0.82 | 0.95 | 0.32 | 0.59 | -0.06 | 0.32 | -0.01 | 280. |
| 285. | 0.86 | 0.98 | 0.34 | 0.60 | -0.05 | 0.34 | -0.00 | 285. |
| 290. | 0.92 | 1.03 | 0.36 | 0.61 | -0.03 | 0.35 | 0.01 | 290. |
| 295. | 0.99 | 1.09 | 0.38 | 0.63 | -0.02 | 0.36 | 0.02 | 295. |
| 300. | 1.07 | 1.17 | 0.41 | 0.66 | 0.00 | 0.37 | 0.03 | 300. |
| 305. | 1.14 | 1.23 | 0.44 | 0.72 | 0.03 | 0.38 | 0.03 | 305. |
| 310. | 1.21 | 1.26 | 0.50 | 0.75 | 0.06 | 0.38 | 0.03 | 310. |
| 315. | 1.29 | 1.23 | 0.53 | 0.77 | 0.10 | 0.38 | 0.03 | 315. |
| 320. | 1.39 | 1.19 | 0.56 | 0.79 | 0.13 | 0.38 | 0.04 | 320. |
| 325. | 1.43 | 1.18 | 0.58 | 0.80 | 0.15 | 0.38 | 0.04 | 325. |
| 330. | 1.36 | 1.19 | 0.57 | 0.79 | 0.15 | 0.37 | 0.05 | 330. |
| 335. | 1.35 | 1.11 | 0.53 | 0.72 | 0.15 | 0.36 | 0.04 | 335. |
| 340. | 1.28 | 0.93 | 0.44 | 0.56 | 0.14 | 0.32 | 0.02 | 340. |
| 345. | 0.46 | 0.34 | 0.03 | 0.30 | 0.09 | 0.24 | -0.01 | 345. |
| 350. | -0.47 | -0.26 | -0.45 | 0.06 | 0.04 | 0.13 | -0.04 | 350. |
| 355. | -0.91 | -0.58 | -0.65 | -0.11 | 0.01 | 0.05 | -0.05 | 355. |

# DIFFERENTIAL PRESSURE -- DYNAMIC COMPONENTS

TEST=494 CNTR NO. 256 TCN= 50. C.R.= 15.9

DIFFERENTIAL PRESSURES

SPAN STATION 199.5

| AZ | CHORD STATION | | | | | | | AZ |
|---|---|---|---|---|---|---|---|---|
| DEG. | 0.455 | 1.340 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 | DEG. |
| 0. | -1.30 | -0.57 | -0.75 | -0.23 | -0.18 | -0.11 | -0.05 | 0. |
| 5. | 1.32 | -0.06 | -0.23 | -0.02 | -0.06 | -0.07 | -0.04 | 5. |
| 10. | -0.42 | -0.42 | -0.58 | -0.28 | -0.06 | -0.11 | -0.03 | 10. |
| 15. | -0.60 | -0.42 | -0.64 | -0.22 | -0.09 | -0.17 | -0.03 | 15. |
| 20. | -0.54 | -0.25 | -0.51 | -0.16 | -0.06 | -0.17 | -0.03 | 20. |
| 25. | 0.27 | 0.03 | -0.30 | -0.04 | 0.06 | -0.12 | -0.01 | 25. |
| 30. | 0.04 | 0.37 | -0.18 | -1.99 | 0.18 | -0.13 | 0.03 | 30. |
| 35. | 1.27 | 0.58 | 0.17 | -3.01 | 0.34 | -0.08 | 0.07 | 35. |
| 40. | 1.47 | 0.70 | 0.91 | -3.36 | 0.54 | -0.07 | 0.05 | 40. |
| 45. | 1.64 | 0.78 | 1.40 | 2.11 | 0.74 | -0.13 | 0.02 | 45. |
| 50. | 1.7 | 0.95 | 1.42 | 2.46 | 1.26 | -0.23 | -0.01 | 50. |
| 55. | 1.81 | 1.08 | 1.22 | 2.22 | 1.83 | -0.35 | -0.04 | 55. |
| 60. | 1.64 | 1.07 | 1.11 | 1.17 | 1.56 | -0.41 | -0.13 | 60. |
| 65. | 1.98 | 0.84 | 1.04 | 0.46 | 1.16 | -0.04 | -0.25 | 65. |
| 70. | 1.10 | 0.45 | 1.06 | 0.26 | 0.81 | 0.55 | -0.29 | 70. |
| 75. | 0.67 | 0.17 | 0.96 | -0.06 | 0.65 | -0.87 | -0.31 | 75. |
| 80. | -0.07 | -0.47 | 0.57 | -0.43 | 0.08 | -2.15 | -0.35 | 80. |
| 85. | -0.94 | -1.31 | -0.06 | -0.89 | -0.32 | -1.92 | -0.48 | 85. |
| 90. | -1.43 | -1.68 | -0.41 | -1.11 | -0.58 | -0.88 | -0.52 | 90. |
| 95. | -1.70 | -1.70 | -0.45 | -1.09 | -0.70 | -0.56 | -0.63 | 95. |
| 100. | -1.61 | -1.64 | -0.47 | -0.96 | -0.74 | 0.15 | -0.38 | 100. |
| 105. | -1.47 | -1.57 | -0.45 | -0.80 | -0.76 | 0.71 | -0.19 | 105. |
| 110. | -1.41 | -1.52 | -0.44 | -0.71 | -0.78 | 0.99 | 0.00 | 110. |
| 115. | -1.37 | -1.51 | -0.48 | -0.71 | -0.85 | 0.68 | 0.28 | 115. |
| 120. | -1.39 | -1.52 | -0.55 | -0.76 | -0.97 | -0.85 | 0.36 | 120. |
| 125. | -1.48 | -1.56 | -0.63 | -0.88 | -1.15 | -0.75 | 0.27 | 125. |
| 130. | -1.66 | -1.68 | -0.53 | -1.19 | -1.37 | -0.12 | 0.19 | 130. |
| 135. | -1.97 | -1.93 | -0.77 | -1.97 | -3.14 | 0.21 | 0.12 | 135. |
| 140. | -2.32 | -2.24 | -1.61 | -2.99 | -2.37 | -3.87 | 0.07 | 140. |
| 145. | -2.79 | -2.51 | -2.13 | -2.80 | -0.54 | -3.54 | 0.02 | 145. |
| 150. | -2.91 | -2.66 | -2.44 | -2.06 | -0.23 | -0.51 | 0.01 | 150. |
| 155. | -2.74 | -2.62 | -2.31 | -1.05 | -0.46 | -0.41 | 0.03 | 155. |
| 160. | -2.52 | -2.32 | -1.99 | -0.66 | -0.42 | -0.31 | 0.05 | 160. |
| 165. | -2.15 | -1.41 | -1.39 | -0.50 | -0.27 | -0.23 | 0.06 | 165. |
| 170. | -1.18 | -0.87 | -0.95 | -0.37 | -0.11 | -0.18 | 0.07 | 170. |
| 175. | -0.56 | -0.37 | -0.60 | -0.07 | 0.04 | -0.08 | 0.07 | 175. |
| 180. | -0.11 | 0.14 | -0.29 | 0.15 | 0.13 | 0.23 | 0.08 | 180. |
| 185. | 0.33 | 0.39 | 0.01 | 0.31 | 0.16 | 0.08 | 0.09 | 185. |
| 190. | 0.57 | 0.52 | 0.18 | 0.41 | 0.17 | 0.11 | 0.08 | 190. |
| 195. | 0.64 | 0.62 | 0.23 | 0.44 | 0.17 | 0.12 | 0.06 | 195. |
| 200. | 0.62 | 0.67 | 0.26 | 0.44 | 0.17 | 0.13 | 0.05 | 200. |
| 205. | 0.55 | 0.68 | 0.27 | 0.44 | 0.16 | 0.13 | 0.05 | 205. |
| 210. | 0.48 | 0.67 | 0.27 | 0.47 | 0.15 | 0.14 | 0.05 | 210. |
| 215. | 0.45 | 0.64 | 0.25 | 0.51 | 0.15 | 0.17 | 0.06 | 215. |
| 220. | 0.42 | 0.63 | 0.23 | 0.54 | 0.14 | 0.19 | 0.06 | 220. |
| 225. | 0.40 | 0.64 | 0.24 | 0.55 | 0.15 | 0.23 | 0.07 | 225. |
| 230. | 0.39 | 0.66 | 0.25 | 0.56 | 0.16 | 0.25 | 0.07 | 230. |
| 235. | 0.39 | 0.68 | 0.26 | 0.56 | 0.17 | 0.28 | 0.07 | 235. |
| 240. | 0.39 | 0.70 | 0.27 | 0.56 | 0.18 | 0.30 | 0.08 | 240. |
| 245. | 0.41 | 0.73 | 0.30 | 0.57 | 0.19 | 0.31 | 0.07 | 245. |
| 250. | 0.43 | 0.77 | 0.32 | 0.58 | 0.19 | 0.31 | 0.07 | 250. |
| 255. | 0.46 | 0.80 | 0.35 | 0.59 | 0.19 | 0.31 | 0.06 | 255. |
| 260. | 0.49 | 0.84 | 0.37 | 0.60 | 0.19 | 0.31 | 0.06 | 260. |
| 265. | 0.52 | 0.87 | 0.40 | 0.61 | 0.19 | 0.32 | 0.06 | 265. |
| 270. | 0.52 | 0.89 | 0.41 | 0.61 | 0.19 | 0.32 | 0.07 | 270. |
| 275. | 0.52 | 0.91 | 0.43 | 0.62 | 0.20 | 0.33 | 0.06 | 275. |
| 280. | 0.54 | 0.92 | 0.44 | 0.63 | 0.20 | 0.33 | 0.06 | 280. |
| 285. | 0.58 | 0.94 | 0.46 | 0.65 | 0.21 | 0.33 | 0.06 | 285. |
| 290. | 0.68 | 0.97 | 0.50 | 0.68 | 0.22 | 0.33 | 0.06 | 290. |
| 295. | 0.82 | 1.01 | 0.54 | 0.72 | 0.24 | 0.33 | 0.06 | 295. |
| 300. | 0.96 | 1.05 | 0.58 | 0.75 | 0.26 | 0.33 | 0.06 | 300. |
| 305. | 1.10 | 1.10 | 0.62 | 0.78 | 0.27 | 0.34 | 0.06 | 305. |
| 310. | 1.22 | 1.16 | 0.66 | 0.79 | 0.29 | 0.34 | 0.06 | 310. |
| 315. | 1.32 | 1.20 | 0.68 | 0.79 | 0.30 | 0.34 | 0.06 | 315. |
| 320. | 1.39 | 1.22 | 0.68 | 0.78 | 0.31 | 0.33 | 0.05 | 320. |
| 325. | 1.41 | 1.23 | 0.66 | 0.77 | 0.32 | 0.32 | 0.05 | 325. |
| 330. | 1.38 | 1.20 | 0.62 | 0.74 | 0.33 | 0.30 | 0.04 | 330. |
| 335. | 1.24 | 1.14 | 0.60 | 0.68 | 0.33 | 0.31 | 0.02 | 335. |
| 340. | 1.08 | 1.00 | 0.53 | 0.59 | 0.31 | 0.32 | 0.01 | 340. |
| 345. | 0.69 | 0.67 | 0.27 | 0.43 | 0.13 | 0.25 | -0.01 | 345. |
| 350. | -0.38 | -0.06 | -0.25 | 0.08 | -0.05 | 0.02 | -0.03 | 350. |
| 355. | -1.42 | -0.79 | -0.79 | -2.27 | -0.11 | -0.09 | -0.03 | 355. |

## APPENDIX VI

## DIFFERENTIAL PRESSURE - STATIC COMPONENTS

This appendix contains the static components of the differential pressure (in psi) for the 46 instrumented span and chord stations of the blade. Tabulated are data for the 20 selected test conditions.

The corresponding dynamic components are presented in Appendix V.

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=501 CNTR NO. 538 TCN=01 C.R. = 53.1

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.441 | | 0.276 | | 0.135 | | 0.009 |
| 79.8 | 1.006 | 0.756 | 0.545 | 0.358 | 0.285 | 0.174 | 0.058 |
| 119.7 | 1.667 | 1.270 | 0.878 | 0.651 | 0.441 | 0.225 | 0.126 |
| 153.3 | 2.621 | 2.069 | 1.241 | 0.828 | 0.567 | 0.414 | 0.159 |
| 178.5 | 2.921 | 2.323 | 1.656 | 1.059 | 0.891 | 0.523 | 0.122 |
| 189.0 | 3.685 | 2.905 | 2.091 | 1.369 | 0.858 | 0.575 | 0.191 |
| 199.5 | 6.975 | 4.208 | 2.730 | 2.006 | 1.193 | 0.635 | 0.177 |

TEST=498 CNTR NO. 363 TCN=04 C.R. = 37.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.649 | | 0.348 | | 0.199 | | -0.027 |
| 79.8 | 1.298 | 0.976 | 0.686 | 0.417 | 0.313 | 0.188 | 0.081 |
| 119.7 | 2.375 | 1.847 | 1.319 | 0.967 | 0.621 | 0.345 | 0.147 |
| 153.3 | 3.999 | 2.511 | 2.064 | 1.335 | 0.882 | 0.596 | 0.219 |
| 178.5 | 4.613 | 2.693 | 2.367 | 1.794 | 1.262 | 0.793 | 0.193 |
| 189.0 | 6.319 | 4.508 | 2.967 | 2.057 | 1.536 | 0.772 | 0.264 |
| 199.5 | 7.990 | 4.795 | 3.198 | 2.450 | 1.423 | 0.726 | 0.235 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=502 CNTR NO. 354 TCN=05 C.R. = 50.1

| SPAN STA. | CHORD STATION 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
|---|---|---|---|---|---|---|---|
| 92.5 | 0.347 | | 0.179 | | 0.188 | | 0.190 |
| 79.8 | 0.977 | 0.625 | 0.381 | 0.224 | 0.367 | 0.121 | 0.129 |
| 119.7 | 1.950 | 1.165 | 0.816 | 0.621 | 0.530 | 0.176 | 0.033 |
| 153.3 | 2.559 | 2.051 | 1.221 | 1.083 | 0.738 | 0.290 | 0.110 |
| 178.5 | 3.307 | 1.983 | 1.261 | 1.158 | 0.727 | 0.477 | 0.021 |
| 189.0 | 3.489 | 2.410 | 1.461 | 1.074 | 1.256 | 0.364 | 0.165 |
| 199.5 | 3.560 | 2.468 | 1.642 | 1.170 | 0.815 | 0.236 | 0.043 |

TEST=502 CNTR NO. 306 TCN=08 C.R. = 48.1

| SPAN STA. | CHORD STATION 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
|---|---|---|---|---|---|---|---|
| 92.5 | 0.159 | | 0.095 | | 0.124 | | 0.046 |
| 79.8 | 0.725 | 0.403 | 0.293 | 0.237 | 0.273 | 0.086 | 0.070 |
| 119.7 | 1.877 | 1.201 | 0.813 | 0.593 | 0.526 | 0.165 | 0.051 |
| 153.3 | 3.225 | 2.360 | 1.411 | 1.303 | 0.804 | 0.350 | 0.132 |
| 178.5 | 3.883 | 2.427 | 1.630 | 1.303 | 0.915 | 0.575 | -0.123 |
| 189.0 | 4.199 | 2.983 | 2.060 | 1.300 | 1.344 | 0.441 | 0.177 |
| 199.5 | 4.503 | 3.115 | 2.177 | 1.574 | 1.013 | 0.318 | 0.087 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=504 CNTR NO. 269 TCN=11 C.R. = 62.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.423 | | 0.288 | | 0.285 | | 0.121 |
| 79.8 | 1.206 | 0.774 | 0.570 | 0.490 | 0.410 | 0.150 | 0.443 |
| 119.7 | 2.350 | 1.739 | 1.106 | 0.821 | 0.733 | 0.248 | 0.088 |
| 153.3 | 3.669 | 2.742 | 1.866 | 1.613 | 1.012 | 0.479 | 0.236 |
| 178.5 | 4.267 | 2.925 | 1.925 | 1.556 | 1.039 | 0.451 | -0.162 |
| 189.0 | 4.602 | 3.256 | 2.395 | 1.549 | 1.504 | 0.472 | 0.211 |
| 199.5 | 4.471 | 3.390 | 2.316 | 1.699 | 1.151 | 0.390 | 0.103 |

TEST=505 CNTR NO. 354 TCN=16 C.R. = 66.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.741 | | 0.434 | | 0.246 | | -0.181 |
| 79.8 | 1.589 | 1.072 | 0.891 | 0.591 | 0.301 | 0.166 | 0.148 |
| 119.7 | 1.999 | 1.672 | 1.059 | 0.843 | 0.651 | 0.311 | 0.116 |
| 153.3 | 2.681 | 1.864 | 1.164 | 1.059 | 0.322 | 0.398 | 0.192 |
| 178.5 | 2.394 | 1.598 | 1.192 | 0.788 | 0.594 | 0.368 | -0.425 |
| 189.0 | 2.296 | 1.814 | 1.248 | 0.767 | 0.342 | 0.234 | 0.058 |
| 199.5 | 2.188 | 1.424 | 0.984 | 0.748 | 0.361 | 0.239 | -0.064 |

## DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=503 CNTR NO. 351 TCN=19 C.R. = 60.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.420 | | 0.216 | | 0.116 | | -0.042 |
| 79.8 | 0.950 | 0.608 | 0.532 | 0.357 | 0.159 | 0.136 | 0.057 |
| 119.7 | 1.529 | 1.155 | 0.838 | 0.613 | 0.421 | 0.213 | 0.085 |
| 153.3 | 2.670 | 1.980 | 1.212 | 0.883 | 0.510 | 0.414 | 0.146 |
| 178.5 | 3.001 | 2.526 | 1.653 | 1.028 | 0.885 | 0.565 | 0.085 |
| 189.0 | 4.686 | 3.299 | 2.475 | 1.526 | 1.016 | 0.618 | 0.230 |
| 199.5 | 7.216 | 4.253 | 2.747 | 1.987 | 1.093 | 0.596 | 0.129 |

TEST=498 CNTR NO. 494 TCN=21 C.R. = 36.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.674 | | 0.402 | | 0.201 | | -0.097 |
| 79.8 | 1.239 | 0.908 | 0.810 | 0.616 | 0.237 | 0.221 | 0.147 |
| 119.7 | 1.787 | 1.601 | 1.096 | 0.771 | 0.525 | 0.270 | 0.145 |
| 153.3 | 2.599 | 1.523 | 1.324 | 0.846 | 0.654 | 0.393 | 0.170 |
| 178.5 | 2.390 | 1.471 | 1.229 | 0.978 | 0.698 | 0.449 | 0.226 |
| 189.0 | 2.912 | 2.081 | 1.379 | 0.747 | 0.949 | 0.364 | 0.134 |
| 199.5 | 2.819 | 1.892 | 1.170 | 0.931 | 0.591 | 0.248 | 0.085 |

## DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=501 CNTR NO. 346 TCN=23 C.R. = 42.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.258 | | 0.138 | | 0.119 | | 0.098 |
| 79.8 | 0.850 | 0.551 | 0.349 | 0.292 | 0.316 | 0.108 | 0.151 |
| 119.7 | 1.554 | 0.988 | 0.591 | 0.446 | 0.425 | 0.079 | 0.020 |
| 153.3 | 1.535 | 1.223 | 0.483 | 0.608 | 0.462 | 0.098 | 0.023 |
| 178.5 | 1.293 | 0.687 | 0.262 | 0.314 | 0.143 | 0.166 | -0.205 |
| 189.0 | 1.180 | 0.608 | 0.429 | 0.224 | 0.531 | 0.059 | 0.026 |
| 199.5 | 0.984 | 0.589 | 0.363 | 0.256 | 0.184 | -0.100 | -0.031 |

TEST=494 CNTR NO. 184 TCN=25 C.R. = 22.1

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.415 | | 0.225 | | 0.129 | | 0.053 |
| 79.8 | 0.747 | 0.510 | 0.334 | 0.262 | 0.278 | 0.087 | 0.057 |
| 119.7 | 1.168 | 0.628 | 0.352 | 0.236 | 0.356 | 0.032 | -0.032 |
| 153.3 | 0.855 | 0.773 | 0.173 | 0.568 | 0.318 | -0.045 | -0.031 |
| 178.5 | 0.405 | -0.119 | -0.144 | 0.094 | 0.271 | 0.002 | 0.008 |
| 189.0 | 0.326 | -0.023 | 0.091 | -0.166 | 0.294 | -0.002 | 0.029 |
| 199.5 | 0.635 | 0.013 | 0.192 | -0.109 | 0.049 | -0.084 | 0.037 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=494 CNTR NO. 264 TCN=26 C.R. = 11.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.345 | | 0.104 | | 0.067 | | 0.013 |
| 79.8 | 0.673 | 0.441 | 0.152 | 0.121 | 0.235 | 0.024 | -0.022 |
| 119.7 | 0.762 | 0.280 | 0.056 | 0.032 | 0.097 | 0.040 | -0.005 |
| 159.3 | 0.216 | 0.202 | -0.213 | 0.331 | 0.142 | -0.182 | -0.103 |
| 178.5 | -0.303 | -0.719 | -0.497 | -0.161 | 0.005 | -0.176 | 0.284 |
| 189.0 | -0.376 | -0.657 | -0.175 | -0.496 | 0.124 | -0.291 | 0.013 |
| 199.9 | 0.025 | -0.314 | -0.064 | -0.472 | -0.093 | -0.273 | -0.055 |

TEST=500 CNTR NO. 458 TCN=27 C.R. = 39.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.232 | | -0.007 | | 0.080 | | -0.060 |
| 79.8 | 0.584 | 0.305 | 0.048 | -0.047 | 0.207 | -0.026 | -0.030 |
| 119.7 | 0.708 | -0.051 | -0.106 | -0.054 | 0.152 | -0.112 | -0.139 |
| 159.3 | 0.032 | -0.015 | 0.510 | -0.548 | -0.050 | -0.231 | -0.116 |
| 178.5 | -0.020 | -0.879 | -0.589 | -0.372 | -0.424 | -0.224 | 0.271 |
| 189.0 | -0.464 | -0.570 | -0.919 | -0.668 | -0.110 | -0.193 | -0.075 |
| 199.5 | -0.473 | -0.684 | -0.074 | -0.535 | -0.227 | -0.294 | -0.199 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=500 CNTR NO. 570 TCN=31 C.R. = 40.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.295 | | 0.077 | | 0.056 | | -0.046 |
| 79.8 | 0.627 | 0.358 | 0.140 | 0.125 | 0.191 | 0.014 | 0.002 |
| 119.7 | 0.777 | 0.150 | 0.040 | 0.048 | 0.205 | -0.065 | -0.004 |
| 153.3 | 0.169 | 0.101 | -0.437 | 0.182 | 0.112 | -0.172 | -0.085 |
| 178.5 | 0.032 | -0.714 | -0.376 | -0.168 | -0.388 | -0.077 | 0.219 |
| 189.0 | -0.250 | -0.554 | -0.363 | -0.493 | -0.076 | -0.052 | -0.040 |
| 199.5 | -0.241 | -0.373 | 0.054 | -0.445 | -0.183 | -0.123 | -0.077 |

TEST=498 CNTR NO. 250 TCN=33 C.R. = 32.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.316 | | 0.197 | | 0.193 | | 0.004 |
| 79.8 | 0.762 | 0.437 | 0.259 | 0.163 | 0.221 | 0.061 | 0.033 |
| 119.7 | 1.166 | 0.686 | 0.394 | 0.309 | 0.312 | 0.063 | -0.011 |
| 153.3 | 1.051 | 0.887 | 0.195 | 0.610 | 0.323 | 0.034 | -0.038 |
| 178.5 | 1.058 | 0.623 | 0.206 | 0.311 | 0.170 | 0.114 | 0.041 |
| 189.0 | 0.932 | 0.474 | 0.443 | 0.151 | 0.321 | 0.084 | 0.033 |
| 199.5 | 1.056 | 0.641 | 0.598 | 0.246 | 0.233 | 0.045 | 0.008 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=502 CNTR NO. 175 TCN=36 C.R. = 44.1

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.348 | | C.172 | | 0.167 | | -0.372 |
| 79.8 | 1.010 | 0.654 | 0.619 | 0.537 | 0.214 | 0.149 | 0.086 |
| 119.7 | 1.835 | 1.226 | C.837 | C.564 | 0.450 | 0.117 | 0.042 |
| 153.3 | 1.944 | 1.465 | C.601 | 0.735 | C.496 | 0.118 | 0.035 |
| 178.5 | 1.754 | 0.772 | C.532 | 0.358 | C.262 | 0.208 | -0.200 |
| 189.0 | 1.669 | C.918 | 0.628 | 0.140 | 0.616 | 0.061 | 0.041 |
| 199.5 | 1.574 | 1.067 | C.698 | 0.454 | 0.346 | -0.383 | -0.106 |

TEST=502 CNTR NO. 188 TCN=37 C.R. = 45.1

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.486 | | C.264 | | 0.213 | | -0.052 |
| 79.8 | 1.228 | 0.808 | 0.738 | 0.623 | 0.286 | 0.168 | 0.104 |
| 119.7 | 2.209 | 1.488 | 1.019 | 0.702 | C.552 | 0.168 | 0.064 |
| 153.3 | 2.618 | 1.938 | 0.946 | 0.988 | 0.665 | 0.220 | 0.077 |
| 178.5 | 2.425 | 1.278 | 0.904 | 0.622 | 0.463 | 0.316 | -0.174 |
| 189.0 | 2.358 | 1.535 | 1.155 | 0.464 | C.819 | 0.152 | 0.078 |
| 199.5 | 2.277 | 1.643 | 1.152 | 0.801 | 0.514 | 0.020 | -0.076 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=494 CNTR NO. 226 TCN=39 C.R. = 08.0

| SPAN STA. | CHORD STATION 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
|---|---|---|---|---|---|---|---|
| 52.5 | 0.371 | | 0.104 | | 0.066 | | -0.012 |
| 79.8 | 0.803 | 0.566 | 0.285 | 0.282 | 0.273 | 0.076 | 0.030 |
| 119.7 | 0.903 | 0.436 | 0.227 | 0.124 | 0.198 | -0.006 | -0.050 |
| 153.3 | 0.506 | 0.414 | -0.052 | 0.415 | 0.285 | -0.122 | -0.060 |
| 178.5 | -0.142 | -0.595 | -0.216 | 0.008 | 0.175 | -0.079 | 0.274 |
| 189.0 | 0.111 | -0.458 | 0.054 | -0.264 | 0.283 | -0.199 | 0.033 |
| 199.5 | 0.302 | -0.219 | 0.149 | -0.242 | 0.011 | -0.118 | 0.033 |

TEST=497 CNTR NO. 256 TCN=40 C.R. = 25.0

| SPAN STA. | CHORD STATION 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
|---|---|---|---|---|---|---|---|
| 52.5 | 0.282 | | 0.052 | | 0.657 | | -0.376 |
| 79.8 | 0.865 | 0.500 | 0.221 | 0.143 | 0.227 | 0.031 | -0.024 |
| 119.7 | 0.913 | 0.224 | 0.104 | 0.117 | 0.216 | -0.023 | -0.095 |
| 153.3 | 0.491 | 0.373 | -0.204 | 0.297 | 0.0 | -0.109 | -0.093 |
| 178.5 | 0.524 | 0.467 | -0.251 | -0.054 | -0.167 | -0.070 | 0.329 |
| 189.0 | 0.070 | -0.321 | -0.098 | -0.326 | 0.017 | -0.254 | 0.033 |
| 199.5 | 0.067 | -0.130 | 0.242 | -0.305 | -0.124 | -0.157 | -0.091 |

DIFFERENTIAL PRESSURE -- STATIC COMPONENTS

TEST=503 CNTR NO. 163 TCN=46 C.R. = 56.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.326 | | 0.165 | | 0.173 | | -0.048 |
| 79.8 | 0.960 | 0.560 | 0.455 | 0.406 | 0.201 | 0.097 | 0.063 |
| 119.7 | 1.376 | 0.832 | 0.482 | 0.310 | 0.343 | 0.029 | -0.014 |
| 153.3 | 1.295 | 0.905 | 0.343 | 0.597 | 0.322 | 0.022 | 0.002 |
| 178.5 | 1.149 | 0.293 | 0.199 | 0.256 | 0.127 | 0.093 | -0.047 |
| 189.0 | 0.922 | 0.475 | 0.398 | -0.025 | 0.349 | -0.028 | 0.027 |
| 199.5 | 0.878 | 0.526 | 0.582 | 0.198 | 0.220 | -0.099 | -0.142 |

TEST=494 CNTR NO. 256 TCN=50 C.R. = 19.0

| SPAN | CHORD STATION | | | | | | |
|---|---|---|---|---|---|---|---|
| STA. | 0.455 | 1.040 | 1.950 | 2.990 | 4.550 | 7.150 | 10.400 |
| 52.5 | 0.546 | | 0.237 | | 0.141 | | 0.033 |
| 79.8 | 0.930 | 0.645 | 0.287 | 0.193 | 0.205 | 0.040 | -0.008 |
| 119.7 | 1.132 | 0.536 | 0.277 | 0.225 | 0.203 | 0.084 | 0.014 |
| 153.3 | 0.741 | 0.593 | 0.159 | 0.583 | 0.298 | -0.116 | -0.067 |
| 178.5 | 0.267 | -0.316 | -0.199 | 0.074 | 0.181 | -0.116 | 0.294 |
| 189.0 | 0.094 | -0.242 | 0.081 | -0.264 | 0.271 | -0.222 | 0.033 |
| 199.5 | 0.568 | -0.002 | 0.155 | -0.289 | 0.093 | -0.140 | -0.068 |

## APPENDIX VII

## BLADE LOADS - DYNAMIC AND STATIC COMPONENTS

The dynamic and static components of the integrated blade loads (in pounds per inch) are presented in this appendix for the seven instrumented span stations. These data are the result of the integration of the differential pressure along the chord. The dynamic components of the airload distribution are listed in the upper portion of the tables for 72 azimuth positions, while the static components are shown on the bottom line. Blade loads are presented for all 49 test conditions, including those to be partially analyzed.

# BLADE LOADS

TEST 502 CNTR NO. 538 T.C.No. 01 C.R. 55.1

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.26 | 0.55 | 1.30 | 2.10 | 2.43 | 2.01 | -3.55 | 0.0 |
| 5.00 | 0.10 | 0.48 | 1.18 | 1.93 | 2.34 | 1.90 | -3.62 | 5.00 |
| 10.00 | 0.02 | 0.41 | 1.07 | 1.74 | 2.26 | 1.84 | -3.51 | 10.00 |
| 15.00 | 0.02 | 0.37 | 1.00 | 1.63 | 2.16 | 1.79 | -3.46 | 15.00 |
| 20.00 | -0.03 | 0.36 | 0.95 | 1.48 | 2.02 | 1.65 | -3.62 | 20.00 |
| 25.00 | -0.14 | 0.35 | 0.90 | 1.39 | 1.83 | 1.46 | -3.74 | 25.00 |
| 30.00 | -0.26 | 0.32 | 0.83 | 1.29 | 1.60 | 1.31 | -3.79 | 30.00 |
| 35.00 | -0.36 | 0.29 | 0.76 | 1.12 | 1.38 | 1.17 | -3.89 | 35.00 |
| 40.00 | -0.37 | 0.24 | 0.70 | 0.97 | 1.20 | 0.99 | -4.08 | 40.00 |
| 45.00 | -0.35 | 0.19 | 0.65 | 0.90 | 1.05 | 0.79 | -4.25 | 45.00 |
| 50.00 | -0.40 | 0.13 | 0.60 | 0.86 | 0.94 | 0.66 | -4.17 | 50.00 |
| 55.00 | -0.45 | 0.10 | 0.53 | 0.79 | 0.85 | 0.58 | -3.93 | 55.00 |
| 60.00 | -0.42 | 0.08 | 0.43 | 0.70 | 0.78 | 0.52 | -3.63 | 60.00 |
| 65.00 | -0.29 | 0.06 | 0.32 | 0.58 | 0.69 | 0.42 | -3.38 | 65.00 |
| 70.00 | -0.14 | 0.03 | 0.22 | 0.45 | 0.55 | 0.27 | -3.34 | 70.00 |
| 75.00 | -0.05 | 0.02 | 0.14 | 0.30 | 0.38 | 0.10 | -3.23 | 75.00 |
| 80.00 | -0.03 | 0.00 | 0.08 | 0.13 | 0.20 | -0.05 | -3.02 | 80.00 |
| 85.00 | -0.06 | -0.05 | 0.02 | -0.07 | 0.01 | -0.21 | -2.78 | 85.00 |
| 90.00 | -0.09 | -0.12 | -0.04 | -0.26 | -0.18 | -0.39 | -2.53 | 90.00 |
| 95.00 | -0.10 | -0.20 | -0.12 | -0.41 | -0.39 | -0.56 | -2.28 | 95.00 |
| 100.00 | -0.14 | -0.27 | -0.21 | -0.54 | -0.59 | -0.76 | -1.91 | 100.00 |
| 105.00 | -0.20 | -0.31 | -0.30 | -0.69 | -0.78 | -0.96 | -1.45 | 105.00 |
| 110.00 | -0.24 | -0.36 | -0.47 | -0.85 | -0.97 | -1.18 | -1.02 | 110.00 |
| 115.00 | -0.23 | -0.36 | -0.37 | -1.03 | -1.16 | -1.41 | -0.67 | 115.00 |
| 120.00 | -0.21 | -0.34 | -0.69 | -1.18 | -1.36 | -1.63 | -0.42 | 120.00 |
| 125.00 | -0.20 | -0.44 | -0.76 | -1.33 | -1.53 | -1.84 | -0.32 | 125.00 |
| 130.00 | -0.22 | -0.45 | -0.86 | -1.41 | -1.67 | -2.00 | -0.08 | 130.00 |
| 135.00 | -0.19 | -0.44 | -0.89 | -1.47 | -1.79 | -2.11 | 0.28 | 135.00 |
| 140.00 | -0.18 | -0.41 | -0.90 | -1.49 | -1.88 | -2.17 | 0.63 | 140.00 |
| 145.00 | -0.15 | -0.38 | -0.89 | -1.44 | -1.97 | -2.18 | 0.92 | 145.00 |
| 150.00 | -0.12 | -0.33 | -0.88 | -1.40 | -2.02 | -2.09 | 1.33 | 150.00 |
| 155.00 | -0.04 | -0.24 | -0.84 | -1.39 | -2.06 | -1.96 | 1.45 | 155.00 |
| 160.00 | 0.05 | -0.11 | -0.79 | -1.41 | -2.06 | -1.87 | 1.35 | 160.00 |
| 165.00 | 0.16 | 0.03 | -0.72 | -1.35 | -2.02 | -1.93 | 1.61 | 165.00 |
| 170.00 | 0.26 | 0.13 | -0.65 | -1.21 | -1.91 | -1.91 | 2.46 | 170.00 |
| 175.00 | 0.31 | 0.19 | -0.58 | -1.00 | -1.75 | -1.71 | 3.50 | 175.00 |
| 180.00 | 0.32 | 0.20 | -0.53 | -0.79 | -1.60 | -1.33 | 4.24 | 180.00 |
| 185.00 | 0.29 | 0.17 | -0.51 | -0.68 | -1.49 | -0.95 | 4.66 | 185.00 |
| 190.00 | 0.26 | 0.13 | -0.53 | -0.75 | -1.42 | -0.68 | 4.81 | 190.00 |
| 195.00 | 0.24 | -0.05 | -0.60 | -0.92 | -1.36 | -0.56 | 4.77 | 195.00 |
| 200.00 | 0.18 | -0.19 | -0.68 | -1.06 | -1.31 | -0.53 | 4.68 | 200.00 |
| 205.00 | 0.10 | -0.34 | -0.76 | -1.12 | -1.30 | -0.51 | 4.65 | 205.00 |
| 210.00 | -0.02 | -0.43 | -0.82 | -1.20 | -1.29 | -0.58 | 4.49 | 210.00 |
| 215.00 | -0.17 | -0.47 | -0.87 | -1.24 | -1.29 | -0.67 | 4.16 | 215.00 |
| 220.00 | -0.10 | -0.47 | -0.91 | -1.19 | -1.25 | -0.66 | 4.08 | 220.00 |
| 225.00 | -0.11 | -0.48 | -0.92 | -1.14 | -1.19 | -0.59 | 3.71 | 225.00 |
| 230.00 | -0.09 | -0.49 | -0.99 | -0.95 | -1.12 | -0.53 | 3.55 | 230.00 |
| 235.00 | -0.06 | -0.49 | -0.83 | -0.83 | -1.03 | -0.51 | 3.87 | 235.00 |
| 240.00 | -0.03 | -0.47 | -0.75 | -0.73 | -0.93 | -0.41 | 4.04 | 240.00 |
| 245.00 | -0.03 | -0.42 | -0.67 | -0.66 | -0.81 | -0.23 | 3.94 | 245.00 |
| 250.00 | -0.02 | -0.37 | -0.59 | -0.58 | -0.67 | -0.04 | 3.94 | 250.00 |
| 255.00 | 0.02 | -0.29 | -0.50 | -0.49 | -0.53 | 0.17 | 4.09 | 255.00 |
| 260.00 | 0.07 | -0.19 | -0.40 | -0.37 | -0.39 | 0.14 | 4.09 | 260.00 |
| 265.00 | 0.11 | -0.08 | -0.28 | -0.25 | -0.25 | 0.18 | 4.21 | 265.00 |
| 270.00 | 0.13 | 0.02 | -0.15 | -0.16 | -0.12 | 0.21 | 4.24 | 270.00 |
| 275.00 | 0.13 | 0.08 | -0.03 | -0.09 | 0.01 | 0.20 | 4.22 | 275.00 |
| 280.00 | 0.13 | 0.12 | 0.07 | -0.01 | 0.14 | 0.13 | 4.47 | 280.00 |
| 285.00 | 0.12 | 0.14 | 0.17 | 0.07 | 0.31 | 0.12 | 4.59 | 285.00 |
| 290.00 | 0.01 | 0.18 | 0.24 | 0.18 | 0.47 | 0.27 | 3.22 | 290.00 |
| 295.00 | -0.05 | 0.21 | 0.33 | 0.28 | 0.60 | 0.81 | 0.91 | 295.00 |
| 300.00 | 0.17 | 0.23 | 0.42 | 0.43 | 0.69 | 0.83 | -1.50 | 300.00 |
| 305.00 | 0.08 | 0.24 | 0.51 | 0.52 | 0.80 | 0.60 | -2.61 | 305.00 |
| 310.00 | 0.05 | 0.26 | 0.61 | 0.65 | 1.02 | 0.82 | -2.19 | 310.00 |
| 315.00 | 0.05 | 0.30 | 0.69 | 0.84 | 1.33 | 1.04 | -2.01 | 315.00 |
| 320.00 | 0.08 | 0.32 | 0.76 | 1.00 | 1.64 | 1.15 | -3.43 | 320.00 |
| 325.00 | 0.14 | 0.33 | 0.84 | 1.31 | 1.92 | 1.46 | -3.43 | 325.00 |
| 330.00 | 0.23 | 0.34 | 0.92 | 1.51 | 2.07 | 1.92 | -3.14 | 330.00 |
| 335.00 | 0.34 | 0.37 | 1.00 | 1.67 | 2.19 | 2.13 | -3.04 | 335.00 |
| 340.00 | 0.44 | 0.42 | 1.08 | 1.86 | 2.27 | 2.05 | -3.25 | 340.00 |
| 345.00 | 0.49 | 0.51 | 1.18 | 2.04 | 2.37 | 1.98 | -3.48 | 345.00 |
| 350.00 | 0.47 | 0.61 | 1.32 | 2.15 | 2.46 | 2.04 | -3.47 | 350.00 |
| 355.00 | 0.36 | 0.62 | 1.38 | 2.17 | 2.48 | 2.08 | -3.45 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.58 | 3.52 | 5.79 | 8.48 | 10.44 | 12.51 | 17.98 | |

# TEXT NOT REPRODUCIBLE

## BLADE LOADS

TEST 497 CNTR NO. 596 T.C.No. 02 C.R. 31

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 197.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | 0.68 | [illegible] | [illegible] | [illegible] | 1.92 | 0.71 | -2.35 | 0.0 |
| 5.00 | 0.81 | [illegible] | [illegible] | [illegible] | 1.79 | 0.84 | -2.61 | 5.00 |
| 10.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 10.00 |
| 15.00 | 0.87 | [illegible] | [illegible] | [illegible] | 1.69 | 0.92 | -2.63 | 15.00 |
| 20.00 | 0.86 | [illegible] | [illegible] | [illegible] | 1.54 | 0.89 | -2.56 | 20.00 |
| 25.00 | 0.98 | [illegible] | [illegible] | [illegible] | 1.60 | 0.82 | -2.39 | 25.00 |
| 30.00 | 0.97 | [illegible] | [illegible] | [illegible] | 1.49 | 0.74 | -2.49 | 30.00 |
| 35.00 | 0.84 | [illegible] | [illegible] | [illegible] | 1.36 | 0.68 | -2.47 | 35.00 |
| 40.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 40.00 |
| 45.00 | 0.80 | [illegible] | [illegible] | 1.67 | 1.14 | 0.48 | -2.78 | 45.00 |
| 50.00 | 0.66 | [illegible] | [illegible] | [illegible] | 0.99 | 0.30 | -2.81 | 50.00 |
| 55.00 | 0.97 | [illegible] | [illegible] | [illegible] | 0.80 | 0.07 | -2.29 | 55.00 |
| 60.00 | 0.05 | [illegible] | [illegible] | [illegible] | 0.40 | -0.17 | -2.47 | 60.00 |
| 65.00 | -0.03 | [illegible] | [illegible] | [illegible] | 0.19 | -0.41 | -2.37 | 65.00 |
| 70.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 70.00 |
| 75.00 | 0.26 | [illegible] | [illegible] | [illegible] | -0.09 | -0.87 | -2.69 | 75.00 |
| 80.00 | 0.36 | [illegible] | [illegible] | [illegible] | -0.21 | -0.99 | -2.64 | 80.00 |
| 85.00 | 0.09 | [illegible] | [illegible] | [illegible] | -0.36 | -1.13 | -2.98 | 85.00 |
| 90.00 | 0.10 | [illegible] | [illegible] | [illegible] | -0.49 | -1.26 | -3.46 | 90.00 |
| 95.00 | 0.05 | [illegible] | [illegible] | [illegible] | -0.60 | -1.36 | -3.26 | 95.00 |
| 100.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 100.00 |
| 105.00 | 0.11 | [illegible] | [illegible] | -0.09 | -0.79 | -1.40 | -2.67 | 105.00 |
| 110.00 | 0.25 | [illegible] | [illegible] | -0.20 | -0.89 | -1.37 | -2.17 | 110.00 |
| 115.00 | 0.24 | [illegible] | -0.07 | -0.99 | -0.90 | -1.42 | -1.89 | 115.00 |
| 120.00 | 0.30 | [illegible] | -0.17 | -0.69 | -1.02 | -1.50 | -1.91 | 120.00 |
| 125.00 | 0.19 | [illegible] | -0.24 | -0.99 | -1.17 | -1.58 | -1.79 | 125.00 |
| 130.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 130.00 |
| 135.00 | 0.02 | [illegible] | -0.44 | -0.91 | -1.27 | -1.64 | -1.96 | 135.00 |
| 140.00 | -0.07 | [illegible] | -0.55 | -1.11 | -1.35 | -1.62 | -1.95 | 140.00 |
| 145.00 | -0.14 | [illegible] | -0.66 | -1.27 | -1.49 | -1.67 | -1.14 | 145.00 |
| 150.00 | -0.14 | [illegible] | -0.76 | -1.30 | -1.51 | -1.50 | -1.09 | 150.00 |
| 155.00 | -0.07 | -0.04 | -0.75 | -1.35 | -1.55 | -1.44 | -0.97 | 155.00 |
| 160.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 160.00 |
| 165.00 | 0.11 | [illegible] | -0.60 | -1.04 | -1.46 | -1.01 | -0.87 | 165.00 |
| 170.00 | 0.18 | [illegible] | -0.75 | -1.08 | -1.45 | -0.88 | -0.95 | 170.00 |
| 175.00 | 0.24 | [illegible] | -0.81 | -1.02 | -1.49 | -0.87 | -0.75 | 175.00 |
| 180.00 | 0.27 | [illegible] | -0.66 | -1.08 | -1.35 | -0.88 | 0.46 | 180.00 |
| 185.00 | 0.22 | [illegible] | -0.61 | -1.44 | -1.80 | -1.24 | 2.56 | 185.00 |
| 190.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 190.00 |
| 195.00 | 0.12 | -0.04 | -1.04 | -1.76 | -1.60 | -2.13 | 7.87 | 195.00 |
| 200.00 | 0.11 | -0.14 | -1.10 | -1.71 | -1.75 | -1.83 | 7.80 | 200.00 |
| 205.00 | 0.04 | -0.26 | -1.19 | -1.66 | -1.66 | -0.84 | 7.47 | 205.00 |
| 210.00 | -0.10 | -0.36 | -1.25 | -1.10 | -1.67 | 0.47 | 7.71 | 210.00 |
| 215.00 | -0.26 | -0.48 | -1.33 | -1.51 | -1.61 | 1.45 | 7.47 | 215.00 |
| 220.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 220.00 |
| 225.00 | -0.41 | -0.63 | -1.33 | -1.46 | -0.77 | 0.76 | 4.87 | 225.00 |
| 230.00 | -0.41 | -0.72 | -1.04 | -1.26 | -0.49 | 0.44 | 3.87 | 230.00 |
| 235.00 | -0.49 | -0.82 | -1.00 | -1.16 | -0.34 | 0.91 | 2.23 | 235.00 |
| 240.00 | -0.47 | -0.89 | -0.97 | -1.00 | -0.27 | 1.00 | 2.19 | 240.00 |
| 245.00 | -0.45 | -0.83 | -0.99 | -1.01 | -0.36 | 1.18 | 2.19 | 245.00 |
| 250.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 250.00 |
| 255.00 | -0.43 | -0.79 | -0.91 | -0.76 | 0.19 | 1.21 | 2.20 | 255.00 |
| 260.00 | -0.42 | -0.77 | -0.77 | -0.49 | 0.21 | 1.19 | 2.20 | 260.00 |
| 265.00 | -0.43 | -0.76 | -0.66 | -0.48 | 0.25 | 1.06 | 2.14 | 265.00 |
| 270.00 | -0.43 | -0.68 | -0.61 | -0.44 | 0.29 | 0.96 | 2.06 | 270.00 |
| 275.00 | -0.42 | -0.66 | -0.67 | -0.44 | 0.33 | 0.87 | 2.01 | 275.00 |
| 280.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 280.00 |
| 285.00 | -0.43 | -0.67 | -0.65 | -0.54 | 0.48 | 0.78 | 1.74 | 285.00 |
| 290.00 | -0.42 | -0.66 | -0.56 | -0.71 | 0.58 | 0.81 | 1.66 | 290.00 |
| 295.00 | -0.42 | -0.55 | -0.57 | -0.83 | 0.68 | 0.84 | 1.71 | 295.00 |
| 300.00 | -0.45 | -0.77 | 0.09 | 0.14 | 0.72 | 0.89 | 0.98 | 300.00 |
| 305.00 | -0.44 | -0.69 | 0.15 | 0.32 | 0.78 | 0.91 | 0.76 | 305.00 |
| 310.00 | -0.34 | -0.57 | 0.34 | 0.69 | 0.88 | 0.90 | 0.55 | 310.00 |
| 315.00 | -0.38 | 0.70 | 0.69 | 0.74 | 0.87 | 0.91 | 0.65 | 315.00 |
| 320.00 | -0.17 | 0.73 | 0.65 | 0.64 | 0.88 | 0.95 | 0.61 | 320.00 |
| 325.00 | 0.07 | 0.92 | 0.86 | 1.19 | 1.20 | 1.06 | 0.94 | 325.00 |
| 330.00 | 0.26 | 0.99 | 0.64 | 1.33 | 1.33 | 1.01 | -0.09 | 330.00 |
| 335.00 | 0.47 | 0.96 | 1.09 | 1.46 | 1.45 | 1.04 | -0.78 | 335.00 |
| 340.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 340.00 |
| 345.00 | 0.81 | [illegible] | 1.29 | 1.69 | 1.83 | 1.24 | -1.48 | 345.00 |
| 350.00 | 0.98 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 350.00 |
| 355.00 | 0.97 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | |

# BLADE LOADS

TEST 497 CNTR NO. 545 T.C.NO. 03 C.R. 30

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | 0.83 | [illegible] | [illegible] | 1.71 | 1.49 | [illegible] | -1.44 | 0.0 |
| 5.00 | 0.17 | [illegible] | 1.19 | 1.82 | 1.51 | [illegible] | -1.45 | 5.00 |
| 10.00 | -0.10 | [illegible] | 1.00 | 1.73 | 1.48 | [illegible] | -1.51 | 10.00 |
| 15.00 | -0.02 | [illegible] | [illegible] | 1.49 | 1.47 | [illegible] | -1.57 | 15.00 |
| 20.00 | -0.04 | [illegible] | [illegible] | 1.38 | 1.34 | [illegible] | -1.61 | 20.00 |
| 25.00 | [illegible] | [illegible] | [illegible] | 1.49 | 1.34 | [illegible] | -1.61 | 25.00 |
| 30.00 | [illegible] | [illegible] | [illegible] | 1.49 | 1.39 | [illegible] | -1.60 | 30.00 |
| 35.00 | [illegible] | [illegible] | [illegible] | 1.49 | 1.49 | [illegible] | -1.58 | 35.00 |
| 40.00 | [illegible] | [illegible] | [illegible] | 1.49 | 1.49 | [illegible] | -1.55 | 40.00 |
| 45.00 | [illegible] | [illegible] | [illegible] | 1.73 | 1.58 | [illegible] | -1.47 | 45.00 |
| 50.00 | [illegible] | [illegible] | [illegible] | 1.68 | 1.54 | [illegible] | -1.49 | 50.00 |
| 55.00 | -0.12 | -[illegible] | [illegible] | 1.69 | 1.69 | [illegible] | -1.74 | 55.00 |
| 60.00 | -0.47 | -[illegible] | [illegible] | 1.49 | [illegible] | [illegible] | -1.88 | 60.00 |
| 65.00 | -0.88 | -[illegible] | [illegible] | 1.18 | [illegible] | [illegible] | -2.08 | 65.00 |
| 70.00 | -0.42 | [illegible] | [illegible] | [illegible] | [illegible] | -[illegible] | -2.27 | 70.00 |
| 75.00 | -0.36 | [illegible] | [illegible] | [illegible] | [illegible] | -[illegible] | -2.37 | 75.00 |
| 80.00 | -[illegible] | [illegible] | [illegible] | [illegible] | -[illegible] | -[illegible] | -2.40 | 80.00 |
| 85.00 | -0.14 | [illegible] | [illegible] | [illegible] | -[illegible] | -[illegible] | -2.35 | 85.00 |
| 90.00 | -0.07 | [illegible] | [illegible] | [illegible] | -[illegible] | -[illegible] | -2.41 | 90.00 |
| 95.00 | [illegible] | [illegible] | [illegible] | [illegible] | -[illegible] | -[illegible] | -2.46 | 95.00 |
| 100.00 | [illegible] | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.02 | -2.21 | 100.00 |
| 105.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -1.90 | 105.00 |
| 110.00 | [illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -1.84 | 110.00 |
| 115.00 | [illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -1.69 | 115.00 |
| 120.00 | -0.17 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -1.74 | -1.69 | 120.00 |
| 125.00 | -0.13 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -1.36 | -1.58 | 125.00 |
| 130.00 | -0.05 | [illegible] | -[illegible] | -[illegible] | -1.10 | -1.56 | -1.64 | 130.00 |
| 135.00 | [illegible] | -[illegible] | -[illegible] | -[illegible] | -1.27 | -1.75 | -1.79 | 135.00 |
| 140.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.40 | -1.68 | -1.80 | 140.00 |
| 145.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.42 | -1.66 | -1.69 | 145.00 |
| 150.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.40 | -1.03 | -1.82 | 150.00 |
| 155.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.48 | -2.02 | -1.76 | 155.00 |
| 160.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.44 | -1.88 | -1.69 | 160.00 |
| 165.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.62 | -1.83 | -1.82 | 165.00 |
| 170.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.60 | -1.89 | -1.80 | 170.00 |
| 175.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.64 | -1.74 | -1.90 | 175.00 |
| 180.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.49 | -1.64 | -1.81 | 180.00 |
| 185.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.25 | -1.62 | -0.20 | 185.00 |
| 190.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.21 | -1.74 | 1.00 | 190.00 |
| 195.00 | [illegible] | [illegible] | -[illegible] | -[illegible] | -1.22 | -1.90 | 2.20 | 195.00 |
| 200.00 | [illegible] | -[illegible] | -[illegible] | -[illegible] | -1.29 | -[illegible] | 2.69 | 200.00 |
| 205.00 | [illegible] | -[illegible] | -[illegible] | -[illegible] | -1.13 | -[illegible] | 2.39 | 205.00 |
| 210.00 | -[illegible] | [illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 1.97 | 210.00 |
| 215.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 1.58 | 215.00 |
| 220.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 1.60 | 220.00 |
| 225.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 2.01 | 225.00 |
| 230.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 2.74 | 230.00 |
| 235.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 3.49 | 235.00 |
| 240.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 3.97 | 240.00 |
| 245.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 4.06 | 245.00 |
| 250.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 3.49 | 250.00 |
| 255.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 2.74 | 255.00 |
| 260.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | 2.22 | 260.00 |
| 265.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | [illegible] | 2.20 | 265.00 |
| 270.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | [illegible] | 2.89 | 270.00 |
| 275.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | [illegible] | 4.77 | 275.00 |
| 280.00 | -[illegible] | -[illegible] | -[illegible] | -[illegible] | [illegible] | [illegible] | 6.44 | 280.00 |
| 285.00 | -[illegible] | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | 8.44 | 285.00 |
| 290.00 | -[illegible] | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | 9.10 | 290.00 |
| 295.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 8.73 | 295.00 |
| 300.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 8.27 | 300.00 |
| 305.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 8.76 | 305.00 |
| 310.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 8.79 | 310.00 |
| 315.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 9.99 | 315.00 |
| 320.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 9.04 | 320.00 |
| 325.00 | -[illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 8.64 | 325.00 |
| 330.00 | [illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | -0.09 | 330.00 |
| 335.00 | [illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | -0.99 | 335.00 |
| 340.00 | [illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | -0.90 | 340.00 |
| 345.00 | [illegible] | -[illegible] | [illegible] | [illegible] | [illegible] | [illegible] | -1.16 | 345.00 |
| 350.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | -1.32 | 350.00 |
| 355.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | -1.56 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| 360.00 | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | [illegible] | 360.00 |

# BLADE LOADS

TEST 498 CNTR NO. 563 T.C.No. 04 C.R. 37

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.9 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | 0.33 | 0.31 | 0.64 | 1.57 | 1.82 | 1.29 | -0.84 | 0.0 |
| 5.00 | 1.12 | 0.86 | 1.03 | 2.12 | 2.59 | 2.13 | 0.01 | 5.00 |
| 10.00 | 0.85 | 0.94 | 1.25 | 2.44 | 2.77 | 2.24 | 0.43 | 10.00 |
| 15.00 | 0.58 | 1.04 | 1.40 | 2.57 | 2.61 | 1.78 | -0.24 | 15.00 |
| 20.00 | 0.62 | 1.35 | 1.57 | 2.63 | 2.28 | 1.34 | -0.63 | 20.00 |
| 25.00 | 0.73 | 1.62 | 1.81 | 2.54 | 2.11 | 1.22 | -0.75 | 25.00 |
| 30.00 | 0.77 | 1.84 | 2.39 | 2.38 | 2.08 | 1.21 | -0.75 | 30.00 |
| 35.00 | 0.65 | 1.88 | 2.60 | 2.18 | 2.07 | 1.27 | -0.71 | 35.00 |
| 40.00 | 0.46 | 1.78 | 2.78 | 2.01 | 2.01 | 1.30 | -0.66 | 40.00 |
| 45.00 | 0.36 | 1.52 | 2.37 | 1.89 | 1.93 | 1.29 | -0.67 | 45.00 |
| 50.00 | 0.48 | 1.13 | 1.89 | 1.83 | 1.79 | 1.17 | -0.82 | 50.00 |
| 55.00 | 0.57 | 1.03 | 1.45 | 1.83 | 1.61 | 0.92 | -1.14 | 55.00 |
| 60.00 | 0.66 | 1.09 | 1.29 | 1.82 | 1.38 | 0.60 | -1.57 | 60.00 |
| 65.00 | 0.54 | 1.01 | 1.29 | 1.75 | 1.11 | 0.31 | -1.87 | 65.00 |
| 70.00 | 0.36 | 1.02 | 1.36 | 1.61 | 0.83 | 0.24 | -2.06 | 70.00 |
| 75.00 | 0.55 | 1.15 | 1.29 | 1.41 | 0.57 | -0.23 | -2.27 | 75.00 |
| 80.00 | 0.84 | 1.92 | 1.15 | 1.22 | 0.38 | -0.65 | -2.65 | 80.00 |
| 85.00 | 0.91 | 0.74 | 0.96 | 1.79 | 0.24 | -0.58 | -2.41 | 85.00 |
| 90.00 | 0.65 | 0.58 | 0.80 | 0.99 | 0.19 | -0.63 | -2.09 | 90.00 |
| 95.00 | 0.48 | 0.52 | 0.66 | 0.99 | 0.17 | -0.65 | -1.71 | 95.00 |
| 100.00 | 0.41 | 0.48 | 0.51 | 0.80 | 0.14 | -0.68 | -1.67 | 100.00 |
| 105.00 | 0.40 | 0.41 | 0.34 | 0.74 | 0.07 | -0.76 | -1.76 | 105.00 |
| 110.00 | 0.39 | 0.33 | 0.18 | 0.67 | -0.08 | -0.89 | -1.79 | 110.00 |
| 115.00 | 0.44 | 0.27 | 0.05 | 0.57 | -0.27 | -1.04 | -1.66 | 115.00 |
| 120.00 | 0.48 | 0.28 | -0.04 | 0.36 | -0.53 | -1.24 | -1.62 | 120.00 |
| 125.00 | 0.38 | 0.14 | -0.13 | -0.01 | -0.83 | -1.45 | -1.66 | 125.00 |
| 130.00 | 0.12 | 0.18 | -0.29 | -0.47 | -1.14 | -1.64 | -1.71 | 130.00 |
| 135.00 | 0.11 | 0.06 | -0.47 | -0.98 | -1.51 | -2.18 | -2.31 | 135.00 |
| 140.00 | 0.12 | 0.00 | -0.58 | -1.23 | -1.99 | -2.56 | -2.51 | 140.00 |
| 145.00 | 0.03 | -0.04 | -0.63 | -1.25 | -2.25 | -2.77 | -2.25 | 145.00 |
| 150.00 | -0.14 | -0.06 | -0.65 | -1.03 | -2.04 | -2.53 | -1.82 | 150.00 |
| 155.00 | -0.29 | -0.25 | -0.68 | -0.87 | -1.68 | -1.75 | -0.81 | 155.00 |
| 160.00 | -0.12 | 0.01 | -0.78 | -0.99 | -1.32 | -1.31 | -0.46 | 160.00 |
| 165.00 | 0.13 | 0.18 | -0.76 | -1.24 | -1.27 | -0.73 | -0.17 | 165.00 |
| 170.00 | 0.25 | 0.21 | -0.69 | -1.40 | -1.36 | -0.65 | 0.37 | 170.00 |
| 175.00 | 0.22 | 0.33 | -0.66 | -1.58 | -1.39 | -0.69 | 0.20 | 175.00 |
| 180.00 | 0.14 | 0.41 | -0.64 | -1.64 | -1.30 | -0.54 | 0.04 | 180.00 |
| 185.00 | 0.07 | 0.42 | -0.65 | -1.71 | -1.31 | -0.58 | -0.44 | 185.00 |
| 190.00 | 0.05 | 0.34 | -0.73 | -1.80 | -1.44 | -0.85 | -0.90 | 190.00 |
| 195.00 | 0.03 | 0.20 | -0.83 | -1.93 | -1.58 | -0.93 | -0.64 | 195.00 |
| 200.00 | -0.02 | 0.09 | -0.90 | -1.96 | -1.54 | -0.80 | -0.13 | 200.00 |
| 205.00 | -0.10 | -0.16 | -0.89 | -1.95 | -1.47 | -0.15 | 0.26 | 205.00 |
| 210.00 | -0.22 | -0.38 | -0.83 | -1.97 | -1.26 | 0.25 | 1.55 | 210.00 |
| 215.00 | -0.24 | -0.59 | -0.79 | -2.03 | -0.92 | 1.12 | 3.61 | 215.00 |
| 220.00 | -0.15 | -0.76 | -0.84 | -2.08 | -0.93 | 0.92 | 4.52 | 220.00 |
| 225.00 | -0.18 | -0.85 | -0.92 | -1.98 | -1.32 | 0.22 | 3.85 | 225.00 |
| 230.00 | -0.22 | -0.86 | -0.98 | -1.72 | -1.47 | -0.07 | 3.71 | 230.00 |
| 235.00 | -0.23 | -0.85 | -1.00 | -1.50 | -1.24 | 0.11 | 3.80 | 235.00 |
| 240.00 | -0.29 | -0.85 | -0.99 | -1.33 | -0.94 | 0.54 | 4.00 | 240.00 |
| 245.00 | -0.27 | -0.84 | -1.00 | -1.13 | -0.80 | 0.91 | 4.15 | 245.00 |
| 250.00 | -0.40 | -0.82 | -1.04 | -1.03 | -0.67 | 1.18 | 4.17 | 250.00 |
| 255.00 | -0.66 | -0.80 | -1.09 | -0.99 | -0.51 | 1.47 | 4.20 | 255.00 |
| 260.00 | -0.70 | -0.77 | -1.12 | -0.99 | -0.39 | 1.43 | 4.31 | 260.00 |
| 265.00 | -0.61 | -0.76 | -1.05 | -0.99 | -0.40 | 1.18 | 4.24 | 265.00 |
| 270.00 | -0.47 | -0.78 | -0.96 | -1.30 | -0.48 | 0.34 | 2.74 | 270.00 |
| 275.00 | -0.36 | -0.81 | -0.86 | -0.98 | -0.54 | -0.27 | 1.37 | 275.00 |
| 280.00 | -0.47 | -0.82 | -0.81 | -0.77 | -0.55 | -0.15 | 1.52 | 280.00 |
| 285.00 | -0.71 | -0.83 | -0.78 | -0.53 | -0.43 | 0.29 | 2.37 | 285.00 |
| 290.00 | -0.92 | -0.84 | -0.75 | -0.37 | -0.16 | 0.34 | 2.27 | 290.00 |
| 295.00 | -1.04 | -0.84 | -0.72 | -0.35 | 0.15 | 0.37 | 2.36 | 295.00 |
| 300.00 | -1.04 | -0.81 | -0.69 | -0.34 | 0.43 | 0.40 | 1.90 | 300.00 |
| 305.00 | -0.95 | -0.81 | -0.62 | -0.30 | 0.53 | 0.18 | -0.17 | 305.00 |
| 310.00 | -0.83 | -0.84 | -0.53 | -0.19 | 0.49 | -0.31 | -0.78 | 310.00 |
| 315.00 | -0.69 | -0.87 | -0.36 | 0.01 | 0.44 | -0.12 | -0.69 | 315.00 |
| 320.00 | -0.57 | -0.92 | -0.22 | 0.22 | 0.50 | -0.13 | -0.63 | 320.00 |
| 325.00 | -0.51 | -1.00 | -0.13 | 0.39 | 0.62 | -0.13 | -0.93 | 325.00 |
| 330.00 | -0.52 | -1.07 | -0.11 | 0.47 | 0.71 | -0.15 | -1.30 | 330.00 |
| 335.00 | -0.29 | -1.13 | -0.15 | 0.48 | 0.74 | -0.17 | -1.57 | 335.00 |
| 340.00 | -0.56 | -1.19 | -0.22 | 0.44 | 0.79 | -0.25 | -1.81 | 340.00 |
| 345.00 | -0.46 | -1.29 | -0.30 | 0.49 | 0.87 | -0.31 | -1.97 | 345.00 |
| 350.00 | -0.36 | -1.28 | -0.34 | 0.71 | 1.04 | -0.17 | -1.93 | 350.00 |
| 355.00 | -0.34 | -0.91 | -0.06 | 1.00 | 1.39 | 0.33 | -1.69 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 2.02 | 4.28 | 8.31 | 12.58 | 15.23 | 19.51 | 21.06 | |

# BLADE LOADS

TEST 502 CNTR NO. 354 T.C.No. 05 C.R. 50.1

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.81 | 0.96 | 2.35 | 3.35 | 2.15 | 2.47 | 2.15 | 0.0 |
| 5.00 | 0.74 | 1.09 | 2.09 | 2.81 | 1.63 | 1.78 | 1.18 | 5.00 |
| 10.00 | 0.60 | 1.10 | 1.85 | 1.84 | 1.04 | 0.98 | 0.23 | 10.00 |
| 15.00 | 0.57 | 0.95 | 1.47 | 1.53 | 0.30 | 0.02 | -0.69 | 15.00 |
| 20.00 | 0.74 | 0.62 | 1.23 | 1.14 | -0.46 | -0.90 | -1.68 | 20.00 |
| 25.00 | 0.30 | 0.57 | 1.08 | 0.75 | -1.12 | -1.64 | -2.56 | 25.00 |
| 30.00 | 0.37 | 1.20 | 0.93 | 0.46 | -1.59 | -2.18 | -3.06 | 30.00 |
| 35.00 | 0.54 | 1.09 | 0.72 | 0.31 | -1.90 | -2.46 | -3.32 | 35.00 |
| 40.00 | 0.52 | 0.75 | 0.66 | 0.20 | -2.12 | -2.51 | -3.48 | 40.00 |
| 45.00 | 0.39 | 0.67 | 0.54 | 0.10 | -2.28 | -2.53 | -3.66 | 45.00 |
| 50.00 | 0.47 | 0.69 | 0.41 | 0.02 | -2.41 | -2.70 | -3.89 | 50.00 |
| 55.00 | 0.58 | 0.66 | 0.34 | -0.09 | -2.57 | -3.00 | -4.19 | 55.00 |
| 60.00 | 0.64 | 0.41 | 0.09 | -0.25 | -2.79 | -3.37 | -4.55 | 60.00 |
| 65.00 | 0.49 | 0.25 | 0.00 | -0.59 | -3.08 | -3.70 | -5.19 | 65.00 |
| 70.00 | 0.21 | 0.65 | 0.04 | -0.95 | -3.40 | -4.11 | -5.97 | 70.00 |
| 75.00 | 0.37 | 0.90 | -0.40 | -1.48 | -3.67 | -4.94 | -6.59 | 75.00 |
| 80.00 | 0.46 | 0.60 | -0.41 | -2.20 | -4.24 | -5.45 | -5.79 | 80.00 |
| 85.00 | 0.32 | -0.01 | 0.00 | -1.69 | -4.36 | -3.99 | -3.33 | 85.00 |
| 90.00 | -0.05 | -0.08 | -0.81 | -1.43 | -2.95 | -3.14 | -0.63 | 90.00 |
| 95.00 | -0.60 | 0.64 | -0.44 | -2.08 | -2.77 | -1.60 | 0.17 | 95.00 |
| 100.00 | -0.25 | 0.35 | -0.13 | -1.33 | -2.49 | -0.39 | 0.32 | 100.00 |
| 105.00 | 0.40 | -0.18 | -0.13 | -0.68 | -1.51 | -0.49 | 0.87 | 105.00 |
| 110.00 | 0.62 | -0.23 | -0.59 | -0.76 | -1.38 | -0.77 | 1.06 | 110.00 |
| 115.00 | 0.32 | 0.26 | -0.40 | -0.94 | -1.08 | -0.30 | 0.34 | 115.00 |
| 120.00 | 0.02 | 0.44 | 0.07 | -0.64 | -2.08 | 0.27 | -0.46 | 120.00 |
| 125.00 | -0.13 | 0.63 | 0.11 | -0.16 | -1.91 | 0.36 | -1.10 | 125.00 |
| 130.00 | -0.03 | 0.41 | -0.14 | -0.25 | -1.46 | 0.31 | -1.52 | 130.00 |
| 135.00 | 0.23 | 0.33 | -0.23 | -0.94 | -0.85 | 0.20 | -1.64 | 135.00 |
| 140.00 | 0.44 | 0.36 | -0.18 | -0.58 | -0.30 | 0.18 | -1.62 | 140.00 |
| 145.00 | 0.52 | 0.43 | -0.02 | -0.34 | 0.23 | 0.21 | -1.57 | 145.00 |
| 150.00 | 0.47 | 0.55 | 0.21 | 0.01 | 0.63 | 0.25 | -1.46 | 150.00 |
| 155.00 | 0.46 | 0.71 | 0.42 | 0.27 | 0.95 | 0.30 | -1.28 | 155.00 |
| 160.00 | 0.52 | 0.90 | 0.60 | 0.48 | 1.23 | 0.38 | -1.04 | 160.00 |
| 165.00 | 0.58 | 1.13 | 0.74 | 0.69 | 1.45 | 0.49 | -0.79 | 165.00 |
| 170.00 | 0.58 | 1.24 | 0.92 | 0.95 | 1.62 | 0.61 | -0.49 | 170.00 |
| 175.00 | 0.54 | 1.18 | 1.11 | 1.11 | 1.76 | 0.78 | -0.15 | 175.00 |
| 180.00 | 0.46 | 1.06 | 1.19 | 1.04 | 1.89 | 1.00 | 0.18 | 180.00 |
| 185.00 | 0.38 | 0.90 | 1.10 | 0.90 | 2.00 | 1.17 | 0.51 | 185.00 |
| 190.00 | 0.30 | 0.70 | 0.90 | 0.78 | 2.13 | 1.29 | 0.82 | 190.00 |
| 195.00 | 0.21 | 0.44 | 0.73 | 0.63 | 2.25 | 1.45 | 1.08 | 195.00 |
| 200.00 | 0.12 | 0.17 | 0.91 | 0.58 | 2.34 | 1.56 | 1.22 | 200.00 |
| 205.00 | 0.02 | -0.05 | 0.23 | 0.56 | 2.40 | 1.58 | 1.29 | 205.00 |
| 210.00 | -0.10 | -0.26 | 0.04 | 0.54 | 2.45 | 1.58 | 1.36 | 210.00 |
| 215.00 | -0.23 | -0.48 | -0.13 | 0.33 | 2.56 | 1.71 | 1.47 | 215.00 |
| 220.00 | -0.36 | -0.66 | -0.40 | 0.03 | 2.74 | 1.96 | 1.61 | 220.00 |
| 225.00 | -0.51 | -0.76 | -0.69 | -0.28 | 3.00 | 2.26 | 1.81 | 225.00 |
| 230.00 | -0.63 | -0.81 | -0.97 | -0.46 | 3.18 | 2.59 | 2.14 | 230.00 |
| 235.00 | -0.73 | -0.86 | -1.19 | -0.47 | 3.19 | 3.04 | 2.65 | 235.00 |
| 240.00 | -0.79 | -0.96 | -1.32 | -0.28 | 2.84 | 3.67 | 3.34 | 240.00 |
| 245.00 | -0.82 | -1.16 | -1.40 | 0.06 | 2.13 | 4.27 | 4.22 | 245.00 |
| 250.00 | -0.85 | -1.34 | -1.47 | 0.66 | 1.32 | 4.50 | 5.20 | 250.00 |
| 255.00 | -0.88 | -1.48 | -1.40 | 0.54 | 0.95 | 4.12 | 6.00 | 255.00 |
| 260.00 | -0.89 | -1.56 | -0.94 | -0.91 | 0.97 | 3.15 | 6.43 | 260.00 |
| 265.00 | -0.89 | -1.57 | -0.91 | -2.26 | 1.38 | 1.91 | 6.54 | 265.00 |
| 270.00 | -0.91 | -1.56 | -1.33 | -2.55 | 1.69 | 1.08 | 5.66 | 270.00 |
| 275.00 | -0.94 | -1.52 | -2.30 | -2.15 | 0.18 | 0.82 | 4.28 | 275.00 |
| 280.00 | -0.95 | -1.44 | -2.43 | -1.81 | -2.06 | -0.67 | 2.81 | 280.00 |
| 285.00 | -0.93 | -1.27 | -2.11 | -2.07 | -2.62 | -2.82 | 0.72 | 285.00 |
| 290.00 | -0.87 | -0.96 | -1.66 | -2.50 | -2.43 | -3.75 | -2.12 | 290.00 |
| 295.00 | -0.78 | -0.74 | -1.32 | -2.50 | -2.24 | -4.02 | -3.67 | 295.00 |
| 300.00 | -0.69 | -1.08 | -1.90 | -2.14 | -2.03 | -3.71 | -3.81 | 300.00 |
| 305.00 | -0.61 | -1.49 | -1.98 | -1.79 | -1.78 | -3.00 | -2.80 | 305.00 |
| 310.00 | -0.55 | -1.62 | -1.56 | -1.33 | -1.23 | -2.02 | -1.41 | 310.00 |
| 315.00 | -0.51 | -1.51 | -0.91 | -0.73 | -0.58 | -1.03 | -0.31 | 315.00 |
| 320.00 | -0.47 | -1.18 | -0.18 | -0.08 | 0.13 | -0.11 | 0.58 | 320.00 |
| 325.00 | -0.41 | -0.79 | 0.12 | 0.66 | 0.83 | 0.79 | 1.39 | 325.00 |
| 330.00 | -0.30 | -0.44 | 0.03 | 1.44 | 1.52 | 1.62 | 1.88 | 330.00 |
| 335.00 | -0.13 | -0.12 | 0.76 | 2.14 | 2.16 | 2.35 | 1.93 | 335.00 |
| 340.00 | 0.08 | 0.21 | 1.65 | 2.87 | 2.67 | 2.90 | 2.67 | 340.00 |
| 345.00 | 0.25 | 0.47 | 2.23 | 3.06 | 2.94 | 3.23 | 3.41 | 345.00 |
| 350.00 | 0.30 | 0.57 | 2.47 | 4.02 | 2.99 | 3.28 | 3.33 | 350.00 |
| 355.00 | 0.46 | 0.60 | 2.50 | 3.35 | 2.70 | 3.00 | 2.86 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.53 | 3.40 | 5.56 | 8.62 | 9.31 | 11.31 | 9.90 | |

# BLADE LOADS

TEST 502 CNTR NO. 327 T.C.N. 06 C.R. 49.1

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.11 | C.1[illegible] | 1.62 | 3.31 | 2.82 | 3.29 | 2.70 | 0.0 |
| 5.00 | -0.17 | [illegible] | 1.[illegible] | 2.67 | 1.39 | 1.82 | 0.97 | 5.00 |
| 10.00 | -0.08 | C.[illegible] | 1.44 | 2.15 | 0.68 | 0.85 | 0.02 | 10.00 |
| 15.00 | 0.0C | C.[illegible] | 1.22 | 1.7C | -0.07 | C.03 | -0.91 | 15.00 |
| 20.00 | 0.24 | 1.C4 | 1.C3 | 1.23 | -C.70 | -0.61 | -1.76 | 20.00 |
| 25.00 | 0.4C | C.64 | C.56 | C.9C | -1.13 | -1.38 | -2.34 | 25.00 |
| 30.00 | 0.3C | C.32 | C.52 | 0.65 | -1.61 | -1.95 | -2.63 | 30.00 |
| 35.00 | 0.34 | C.22 | C.[illegible] | 0.56 | -1.51 | -2.14 | -2.70 | 35.00 |
| 40.00 | 0.34 | C.37 | C.62 | C.52 | -1.56 | -1.78 | -2.72 | 40.00 |
| 45.00 | 0.4C | C.69 | C.7[illegible] | C.48 | -1.59 | -1.32 | -2.73 | 45.00 |
| 50.00 | 0.37 | C.74 | C.63 | C.2[illegible] | -1.78 | -1.66 | -2.97 | 50.00 |
| 55.00 | 0.37 | C.7[illegible] | C.48 | 0.01 | -2.14 | -2.23 | -3.46 | 55.00 |
| 60.00 | 0.3[illegible] | C.6[illegible] | C.2[illegible] | -0.37 | -2.47 | -2.78 | -4.03 | 60.00 |
| 65.00 | 0.27 | C.7C | C.C2 | -C.71 | -2.97 | -3.39 | -4.72 | 65.00 |
| 70.00 | 0.32 | C.72 | -C.1C | -1.14 | -3.39 | -4.15 | -5.63 | 70.00 |
| 75.00 | 0.2[illegible] | C.6[illegible] | -C.3[illegible] | -1.48 | -4.05 | -4.27 | -6.12 | 75.00 |
| 80.00 | 0.32 | C.5[illegible] | -C.[illegible] | -1.8C | -3.86 | -5.05 | -4.05 | 80.00 |
| 85.00 | 0.3C | C.4C | -C.7[illegible] | -2.56 | -4.17 | -4.71 | -2.61 | 85.00 |
| 90.00 | 0.2[illegible] | C.21 | -C.3[illegible] | -2.5[illegible] | -4.48 | -2.88 | -2.48 | 90.00 |
| 95.00 | 0.14 | -C.CE | -C.[illegible] | -1.[illegible] | -3.39 | -2.61 | -1.27 | 95.00 |
| 100.00 | 0.0C | C.44 | -1.23 | -1.[illegible] | -2.6[illegible] | -3.11 | -0.37 | 100.00 |
| 105.00 | -0.1[illegible] | 1.C[illegible] | -1.2[illegible] | -2.C[illegible] | -3.07 | -2.63 | -0.7[illegible] | 105.00 |
| 110.00 | -0.C[illegible] | C.[illegible]C | -C.3[illegible] | -2.1[illegible] | -3.41 | -1.7[illegible] | -1.4[illegible] | 110.00 |
| 115.00 | 0.[illegible]7 | C.7[illegible] | C.C7 | -1.44 | -3.36 | -C.93 | -2.1[illegible] | 115.00 |
| 120.00 | 1.0[illegible] | C.[illegible]7 | -C.1C | -0.91 | -2.42 | -0.6[illegible] | -2.51 | 120.00 |
| 125.00 | 0.8[illegible] | C.3[illegible] | -C.3[illegible] | -C.[illegible]C | -1.07 | -0.81 | -2.66 | 125.00 |
| 130.00 | 0.61 | C.3[illegible] | -C.[illegible] | -C.[illegible] | -0.[illegible] | -1.01 | -2.7[illegible] | 130.00 |
| 135.00 | 0.5[illegible] | C.[illegible]1 | -C.[illegible]1 | -C.[illegible]7 | -0.48 | -0.98 | -2.6[illegible] | 135.00 |
| 140.00 | 0.5[illegible] | 1.34 | -C.41 | -0.7C | -0.21 | -0.93 | -2.62 | 140.00 |
| 145.00 | 0.[illegible]C | 1.[illegible]5 | -C.C2 | -C.3[illegible] | -0.09 | -0.93 | -2.48 | 145.00 |
| 150.00 | C.[illegible]1 | 1.[illegible]C | C.[illegible]4 | -0.12 | -0.0C | -0.87 | -2.21 | 150.00 |
| 155.00 | 0.[illegible]4 | 1.24 | 1.1[illegible] | 0.03 | 0.[illegible]9 | -C.[illegible]9 | -1.[illegible] | 155.00 |
| 160.00 | 0.7C | 1.3[illegible] | 1.45 | C.2C | 0.42 | -0.42 | -1.33 | 160.00 |
| 165.00 | 0.[illegible]C | 1.37 | 1.[illegible] | C.47 | 0.71 | -0.07 | -0.85 | 165.00 |
| 170.00 | 1.0C | 1.45 | 1.31 | C.8[illegible] | 1.09 | 0.32 | -0.40 | 170.00 |
| 175.00 | 1.0[illegible] | 1.4[illegible] | 1.28 | 1.2[illegible] | 1.44 | 0.68 | 0.02 | 175.00 |
| 180.00 | 1.C2 | 1.3[illegible] | 1.27 | 1.61 | 1.73 | 1.01 | 0.42 | 180.00 |
| 185.00 | 0.9[illegible] | 1.2[illegible] | 1.21 | 1.87 | 1.[illegible]8 | 1.30 | 0.78 | 185.00 |
| 190.00 | 0.[illegible]8 | 1.C[illegible] | 1.C7 | 2.0C | 1.[illegible]5 | 1.41 | 1.06 | 190.00 |
| 195.00 | 0.7[illegible] | C.74 | C.[illegible]4 | 1.93 | 1.92 | 1.38 | 1.20 | 195.00 |
| 200.00 | 0.[illegible]7 | C.4[illegible] | C.[illegible]2 | 1.64 | 1.84 | 1.33 | 1.24 | 200.00 |
| 205.00 | 0.32 | C.2C | C.[illegible]4 | 1.2[illegible] | 1.7[illegible] | 1.21 | 1.2[illegible] | 205.00 |
| 210.00 | 0.07 | C.CC | C.14 | 0.[illegible]7 | 1.75 | 1.[illegible]8 | 1.24 | 210.00 |
| 215.00 | -0.12 | -C.2[illegible] | -C.C[illegible] | 0.35 | 1.77 | C.[illegible]9 | 1.24 | 215.00 |
| 220.00 | -0.3C | -C.4[illegible] | -C.16 | -C.11 | 1.87 | 1.03 | 1.[illegible] | 220.00 |
| 225.00 | -0.4[illegible] | -C.71 | -C.2C | -C.[illegible]1 | [illegible].09 | 1.1[illegible] | 1.3[illegible] | 225.00 |
| 230.00 | -0.[illegible]1 | -C.[illegible]C | -C.23 | -C.74 | 2.48 | 1.43 | 1.62 | 230.00 |
| 235.00 | -0.7[illegible] | -1.C4 | -C.24 | -C.84 | 3.01 | 1.94 | 2.00 | 235.00 |
| 240.00 | -0.[illegible]* | -1.17 | -C.2[illegible] | -0.83 | 3.[illegible]4 | 2.65 | 2.60 | 240.00 |
| 245.00 | -0.8[illegible] | -1.21 | -C.23 | -C.[illegible]1 | 3.83 | 3.51 | 3.42 | 245.00 |
| 250.00 | -0.87 | -1.[illegible] | -C.[illegible] | -C.7[illegible] | 3.[illegible] | 4.43 | 4.3[illegible] | 250.00 |
| 255.00 | -0.[illegible]2 | -1.[illegible]C | -1.14 | -C.67 | 2.18 | 5.15 | 5.34 | 255.00 |
| 260.00 | -[illegible] | -1.[illegible]1 | -1.[illegible]0 | -C.[illegible] | 0.21 | 4.90 | 6.30 | 260.00 |
| 265.00 | -0.[illegible]2 | -1.[illegible]4 | -2.22 | -0.6C | -0.72 | [illegible].27 | 6.[illegible] | 265.00 |
| 270.00 | -0.[illegible]E | -1.[illegible]E | -2.[illegible]5 | -0.7[illegible] | -[illegible].92 | -0.26 | 6.51 | 270.00 |
| 275.00 | -0.80 | -1.[illegible]2 | -2.C[illegible] | -1.04 | -0.84 | -2.45 | 5.14 | 275.00 |
| 280.00 | -0.77 | -1.[illegible]C | -2.C[illegible] | -2.55 | -1.04 | -2.84 | -0.97 | 280.00 |
| 285.00 | -0.7[illegible] | -C.[illegible]2 | -2.C2 | -2.7C | -1.[illegible]8 | -2.[illegible] | -3.34 | 285.00 |
| 290.00 | -0.7[illegible] | -C.[illegible]7 | -1.[illegible]5 | -2.62 | -2.02 | -3.04 | -3.[illegible] | 290.00 |
| 295.00 | -0.77 | -1.[illegible] | -1.[illegible]4 | -2.44 | -1.97 | -2.[illegible] | -3.04 | 295.00 |
| 300.00 | -0.7[illegible] | -1.[illegible]7 | -2.CC | -2.23 | -1.65 | -2.32 | -1.52 | 300.00 |
| 305.00 | -0.[illegible]1 | -2.C2 | -1.[illegible]6 | -1.[illegible]1 | -1.15 | -1.[illegible]6 | -0.2[illegible] | 305.00 |
| 310.00 | -0.[illegible]C | -1.[illegible]1 | -1.[illegible]E | -1.23 | -0.51 | -0.[illegible]3 | 0.62 | 310.00 |
| 315.00 | -0.[illegible]5 | -1.7[illegible] | -1.14 | -C.[illegible]4 | 0.2[illegible] | C.31 | 1.47 | 315.00 |
| 320.00 | -0.[illegible]7 | -1.[illegible]E | -C.[illegible]8 | C.15 | 1.05 | 1.36 | 2.31 | 320.00 |
| 325.00 | -0.[illegible]C | -1.[illegible]7 | -C.1[illegible] | C.[illegible]4 | 1.87 | 2.36 | 3.12 | 325.00 |
| 330.00 | -0.7[illegible] | -1.1[illegible] | C.[illegible]6 | 1.7[illegible] | 2.64 | 3.24 | [illegible].90 | 330.00 |
| 335.00 | -0.[illegible] | -C.[illegible]7 | 1.[illegible]3 | 2.49 | [illegible].33 | [illegible].03 | 4.57 | 335.00 |
| 340.00 | -0.[illegible]7 | -C.[illegible]7 | 1.[illegible]C | 3.1[illegible] | 3.87 | 4.69 | [illegible].08 | 340.00 |
| 345.00 | -0.38 | -C.24 | 1.[illegible]1 | 3.74 | 4.26 | 5.14 | [illegible].28 | 345.00 |
| 350.00 | 0.3[illegible] | C.2[illegible] | 1.[illegible]7 | 4.C[illegible] | 4.63 | 5.29 | [illegible].[illegible]1 | 350.00 |
| 355.00 | 0.77 | C.[illegible]E | 1.[illegible]7 | [illegible].[illegible]7 | 4.30 | 5.01 | [illegible].[illegible]2 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.47 | [illegible].[illegible]E | [illegible].22 | [illegible].1[illegible] | [illegible].22 | [illegible]1.07 | [illegible].[illegible]4 | |

TEXT NOT REPRODUCIBLE

BLADE LOADS

TEST 504 CNTR NO. 257 T.C.N. 07 C.R. 61

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.98 | -0.49 | 1.63 | 2.98 | 3.67 | 3.05 | 4.44 | 0.0 |
| 5.00 | -0.62 | -0.06 | 1.26 | 1.44 | 2.05 | 1.88 | 3.23 | 5.00 |
| 10.00 | -0.21 | -0.09 | 1.11 | 1.38 | 1.00 | 0.66 | 1.78 | 10.00 |
| 15.00 | -0.10 | -0.06 | 0.93 | 0.85 | 1.11 | 1.39 | 0.48 | 15.00 |
| 20.00 | -0.37 | -0.23 | 0.88 | 0.70 | 0.76 | 0.99 | -0.97 | 20.00 |
| 25.00 | -0.71 | -0.35 | 0.63 | 0.46 | -0.10 | -0.09 | -1.70 | 25.00 |
| 30.00 | -0.94 | -0.53 | 0.55 | 0.48 | -0.49 | -0.94 | -1.69 | 30.00 |
| 35.00 | -0.98 | 0.18 | 1.04 | 0.94 | -0.69 | -0.40 | -1.89 | 35.00 |
| 40.00 | 0.05 | 0.75 | 1.44 | 0.69 | -0.44 | -0.41 | -1.98 | 40.00 |
| 45.00 | 0.17 | 0.34 | 0.95 | 0.22 | -0.67 | -0.44 | -2.15 | 45.00 |
| 50.00 | 0.17 | 0.48 | 0.83 | -0.05 | -0.83 | -0.41 | -2.47 | 50.00 |
| 55.00 | 0.05 | 0.88 | 0.44 | -0.91 | -1.37 | -1.11 | -2.90 | 55.00 |
| 60.00 | 0.04 | 0.97 | 0.37 | -1.09 | -2.08 | -1.87 | -3.69 | 60.00 |
| 65.00 | 0.02 | 0.48 | -0.06 | -1.68 | -2.92 | -3.02 | -4.98 | 65.00 |
| 70.00 | -0.05 | 0.38 | -0.25 | -2.34 | -3.80 | -4.19 | -6.56 | 70.00 |
| 75.00 | -0.07 | 0.33 | -0.69 | -2.78 | -4.61 | -5.11 | -8.75 | 75.00 |
| 80.00 | -0.05 | 0.26 | -0.47 | -2.96 | -4.96 | -5.96 | -9.69 | 80.00 |
| 85.00 | -0.05 | 0.20 | -0.16 | -2.79 | -4.70 | -5.97 | -9.99 | 85.00 |
| 90.00 | -0.03 | 0.16 | -0.25 | -2.56 | -4.01 | -7.48 | -8.47 | 90.00 |
| 95.00 | 0.03 | 0.03 | -1.15 | -3.56 | -5.58 | -7.94 | -9.99 | 95.00 |
| 100.00 | 0.07 | 0.05 | -0.46 | -3.64 | -4.94 | -6.48 | -2.05 | 100.00 |
| 105.00 | 0.07 | 0.33 | -0.56 | -2.65 | -4.71 | -4.07 | -2.17 | 105.00 |
| 110.00 | 0.10 | 0.30 | -0.64 | -2.39 | -3.68 | -2.15 | -2.90 | 110.00 |
| 115.00 | 0.14 | 1.21 | -0.69 | -2.09 | -4.25 | -1.49 | -3.44 | 115.00 |
| 120.00 | 0.47 | 1.38 | -0.98 | -1.67 | -2.19 | -1.74 | -3.84 | 120.00 |
| 125.00 | 0.82 | 1.41 | -0.65 | -2.00 | -2.00 | -1.84 | -3.71 | 125.00 |
| 130.00 | 0.89 | 1.98 | 0.91 | -1.46 | -2.48 | -1.79 | -3.68 | 130.00 |
| 135.00 | 1.10 | 1.82 | 1.29 | -1.09 | -2.05 | -1.71 | -3.96 | 135.00 |
| 140.00 | 1.46 | 1.62 | 1.46 | -1.30 | -2.07 | -1.68 | -3.92 | 140.00 |
| 145.00 | 1.46 | 1.28 | 1.43 | -1.07 | -2.09 | -1.99 | -2.97 | 145.00 |
| 150.00 | 1.40 | 1.07 | 1.49 | -0.95 | -2.01 | -1.39 | -2.97 | 150.00 |
| 155.00 | 1.36 | | 1.63 | 1.41 | -0.10 | -1.09 | -2.12 | 155.00 |
| 160.00 | 1.09 | 1.17 | 1.78 | 2.48 | 0.19 | -0.76 | -1.29 | 160.00 |
| 165.00 | 1.91 | 2.13 | 2.06 | 4.41 | 0.46 | -0.29 | -1.05 | 165.00 |
| 170.00 | 2.07 | 2.49 | 2.36 | 5.08 | 1.07 | 0.31 | -0.40 | 170.00 |
| 175.00 | 1.94 | 2.36 | 2.36 | 5.16 | 1.30 | 0.99 | 0.07 | 175.00 |
| 180.00 | 1.42 | 2.00 | 2.01 | 4.09 | 1.09 | 1.23 | 0.82 | 180.00 |
| 185.00 | 1.24 | 2.68 | 1.72 | 4.69 | 1.79 | 1.39 | 0.80 | 185.00 |
| 190.00 | 1.04 | 2.91 | 1.79 | 4.06 | 1.67 | 1.36 | 0.69 | 190.00 |
| 195.00 | 0.81 | 1.35 | 1.68 | 3.98 | 1.68 | 1.11 | 1.00 | 195.00 |
| 200.00 | 0.98 | 1.24 | 0.43 | 3.14 | 1.23 | 0.99 | 0.99 | 200.00 |
| 205.00 | 0.31 | 0.76 | 0.09 | 2.48 | 0.96 | 0.62 | 0.83 | 205.00 |
| 210.00 | -0.02 | 0.99 | -0.29 | 2.37 | 0.79 | 0.37 | 0.70 | 210.00 |
| 215.00 | -0.37 | -0.03 | -0.68 | 2.11 | 0.44 | 0.17 | 0.66 | 215.00 |
| 220.00 | -0.69 | -0.78 | -0.78 | 2.00 | 0.66 | 0.09 | 0.66 | 220.00 |
| 225.00 | -0.82 | -0.65 | -0.75 | 1.69 | 0.90 | 0.02 | 0.61 | 225.00 |
| 230.00 | -0.66 | -0.66 | -0.85 | 1.77 | 0.84 | 0.10 | 0.78 | 230.00 |
| 235.00 | -0.81 | -1.16 | -0.47 | 1.76 | 0.87 | 0.68 | 1.10 | 235.00 |
| 240.00 | -0.87 | -1.78 | -1.07 | 0.90 | 1.28 | 0.90 | 1.98 | 240.00 |
| 245.00 | -0.76 | -1.63 | -1.38 | -1.04 | 1.73 | 1.60 | 2.06 | 245.00 |
| 250.00 | -0.71 | -1.66 | -1.78 | -2.74 | 2.68 | 1.89 | 2.70 | 250.00 |
| 255.00 | -0.71 | -1.70 | -1.40 | -2.66 | 3.07 | 2.62 | 3.38 | 255.00 |
| 260.00 | -0.72 | -1.73 | -1.88 | -2.60 | 2.86 | 3.23 | 4.09 | 260.00 |
| 265.00 | -0.74 | -1.68 | -1.37 | -2.86 | 1.79 | 3.84 | 4.74 | 265.00 |
| 270.00 | -0.71 | -1.68 | -1.68 | -2.67 | 0.12 | 2.40 | 4.34 | 270.00 |
| 275.00 | -0.65 | -1.70 | -1.68 | -2.75 | -0.84 | 0.41 | 4.00 | 275.00 |
| 280.00 | -0.69 | -1.78 | -2.05 | -2.84 | -1.24 | -1.72 | 2.64 | 280.00 |
| 285.00 | -0.66 | -1.68 | -2.17 | -2.88 | -1.18 | -1.76 | 0.98 | 285.00 |
| 290.00 | -0.70 | -1.87 | -2.20 | -2.61 | -1.09 | -1.88 | -0.65 | 290.00 |
| 295.00 | -0.65 | -1.88 | -2.18 | -2.63 | -0.89 | -1.68 | -0.67 | 295.00 |
| 300.00 | -0.67 | -1.85 | -2.10 | -2.77 | -0.99 | -1.20 | -0.07 | 300.00 |
| 305.00 | -0.66 | -1.88 | -1.64 | -2.38 | -0.11 | -0.95 | 0.73 | 305.00 |
| 310.00 | -0.67 | -1.84 | -1.67 | -1.76 | 0.65 | 0.24 | 1.67 | 310.00 |
| 315.00 | -0.82 | -1.74 | -1.78 | -1.09 | 1.03 | 1.30 | 2.44 | 315.00 |
| 320.00 | -0.54 | -1.58 | -0.76 | -0.29 | 1.84 | 2.62 | 3.61 | 320.00 |
| 325.00 | -0.43 | -1.93 | -0.78 | 0.41 | 2.81 | 3.70 | 4.83 | 325.00 |
| 330.00 | -0.84 | -1.11 | 0.31 | 1.46 | 3.64 | 4.45 | 5.74 | 330.00 |
| 335.00 | -0.67 | -0.64 | 0.60 | 2.27 | 4.37 | 5.31 | 6.00 | 335.00 |
| 340.00 | -0.46 | -0.74 | 1.68 | 2.68 | 4.82 | 4.00 | 7.65 | 340.00 |
| 345.00 | -0.09 | -0.87 | 1.65 | 3.69 | 4.25 | 4.65 | 6.78 | 345.00 |
| 350.00 | 0.11 | -0.66 | 1.74 | 3.92 | 4.93 | 4.93 | 4.60 | 350.00 |
| 355.00 | -0.78 | -0.29 | 1.78 | 3.17 | 4.92 | 4.09 | 4.86 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.19 | 4.96 | 6.27 | 10.45 | 5.78 | 12.49 | 11.99 | |

# BLADE LOADS

TEST 902 CNTR NO. 906 T.C.No. 08 C.R. 48.1

SPAN STATION

| DEG | 52.[illegible] | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.37 | -1.49 | 0.89 | 2.74 | 5.26 | 6.85 | 6.57 | 0.0 |
| 5.00 | -0.22 | -1.44 | 1.04 | 2.73 | 4.44 | 5.88 | 4.73 | 5.00 |
| 10.00 | -0.53 | -1.09 | 1.36 | 2.68 | 3.72 | 5.07 | 3.40 | 10.00 |
| 15.00 | -0.60 | -1.47 | 1.57 | 2.57 | 3.09 | 4.35 | 2.43 | 15.00 |
| 20.00 | -0.15 | 0.05 | 1.62 | 2.44 | 2.62 | 3.64 | 1.82 | 20.00 |
| 25.00 | 0.66 | 0.22 | 1.70 | 2.47 | 2.40 | 3.31 | 1.49 | 25.00 |
| 30.00 | 1.29 | 0.33 | 1.99 | 2.92 | 2.45 | 3.38 | 1.32 | 30.00 |
| 35.00 | 0.68 | 0.50 | 2.08 | 2.65 | 2.54 | 3.42 | 1.34 | 35.00 |
| 40.00 | 0.03 | 0.65 | 1.98 | 2.57 | 2.37 | 3.12 | 1.29 | 40.00 |
| 45.00 | -0.13 | 0.62 | 1.68 | 2.00 | 1.84 | 2.41 | 1.04 | 45.00 |
| 50.00 | 0.11 | 0.46 | 1.15 | 1.09 | 0.91 | 1.21 | 0.33 | 50.00 |
| 55.00 | 0.24 | 0.25 | 0.41 | -0.11 | -0.49 | -0.40 | -1.05 | 55.00 |
| 60.00 | 0.18 | -0.01 | -0.42 | -1.44 | -2.78 | -2.45 | -2.94 | 60.00 |
| 65.00 | 0.02 | -0.31 | -1.73 | -2.88 | -4.20 | -4.81 | -5.10 | 65.00 |
| 70.00 | -0.12 | -0.56 | -1.92 | -4.11 | -5.97 | -7.38 | -7.44 | 70.00 |
| 75.00 | -0.19 | -0.75 | -2.43 | -5.05 | -7.43 | -9.33 | -9.55 | 75.00 |
| 80.00 | -0.20 | -0.81 | -2.65 | -5.75 | -8.41 | -10.55 | -10.89 | 80.00 |
| 85.00 | -0.21 | -0.70 | -2.70 | -6.16 | -8.68 | -11.09 | -10.41 | 85.00 |
| 90.00 | -0.16 | -0.52 | -2.61 | -6.02 | -8.53 | -10.89 | -8.21 | 90.00 |
| 95.00 | 0.05 | -0.29 | -2.35 | -5.27 | -8.21 | -9.11 | -6.71 | 95.00 |
| 100.00 | 0.39 | 0.02 | -1.99 | -4.46 | -7.57 | -8.02 | -6.45 | 100.00 |
| 105.00 | 0.67 | 0.35 | -1.41 | -3.84 | -6.78 | -6.62 | -6.68 | 105.00 |
| 110.00 | 0.92 | 0.67 | -0.60 | -3.42 | -6.07 | -6.07 | -6.79 | 110.00 | 
| 115.00 | 1.17 | 1.02 | 0.19 | -2.98 | -5.88 | -6.01 | -6.59 | 115.00 |
| 120.00 | 1.44 | 1.35 | 0.74 | -2.65 | -5.54 | -6.60 | -6.17 | 120.00 |
| 125.00 | 1.69 | 1.72 | 1.14 | -1.98 | -5.33 | -6.20 | -5.67 | 125.00 |
| 130.00 | 1.88 | 2.10 | 1.40 | -0.39 | -5.07 | -5.67 | -5.02 | 130.00 |
| 135.00 | 1.97 | 2.52 | 1.69 | 2.32 | -1.57 | -3.02 | -4.29 | 135.00 |
| 140.00 | 1.98 | 2.93 | 2.12 | 4.17 | -0.96 | -2.31 | -3.49 | 140.00 |
| 145.00 | 1.94 | 3.23 | 2.79 | 5.15 | -0.30 | -1.55 | -2.79 | 145.00 |
| 150.00 | 1.97 | 3.46 | 2.94 | 5.68 | 0.37 | -0.70 | -2.04 | 150.00 |
| 155.00 | 2.12 | 3.63 | 2.87 | 6.18 | 1.14 | 0.20 | -1.14 | 155.00 |
| 160.00 | 2.44 | 3.86 | 2.80 | 6.47 | 1.84 | 0.97 | -0.21 | 160.00 |
| 165.00 | 2.89 | 4.05 | 2.93 | 6.48 | 2.37 | 1.66 | 0.64 | 165.00 |
| 170.00 | 3.16 | 4.18 | 3.13 | 6.15 | 2.69 | 2.19 | 1.23 | 170.00 |
| 175.00 | 3.02 | 4.18 | 3.16 | 5.53 | 2.78 | 2.42 | 1.56 | 175.00 |
| 180.00 | 2.65 | 3.94 | 2.90 | 4.74 | 2.55 | 2.27 | 1.57 | 180.00 |
| 185.00 | 2.14 | 3.40 | 3.23 | 3.88 | 2.11 | 1.84 | 1.39 | 185.00 |
| 190.00 | 1.43 | 2.76 | 4.03 | 2.99 | 1.56 | 1.25 | 1.11 | 190.00 |
| 195.00 | 0.92 | 2.07 | 4.24 | 2.19 | 0.98 | 0.65 | 0.79 | 195.00 |
| 200.00 | 0.37 | 1.35 | 3.69 | 1.57 | 0.49 | 0.12 | 0.45 | 200.00 |
| 205.00 | -0.13 | 0.66 | 2.94 | 1.05 | 0.18 | -0.30 | 0.08 | 205.00 |
| 210.00 | -0.54 | 0.06 | 2.37 | 0.60 | -0.12 | -0.69 | -0.30 | 210.00 |
| 215.00 | -0.86 | -0.44 | 1.72 | 0.30 | -0.35 | -0.98 | -0.55 | 215.00 |
| 220.00 | -1.09 | -0.87 | 1.17 | 0.15 | -0.43 | -1.14 | -0.60 | 220.00 |
| 225.00 | -1.23 | -1.19 | 0.64 | 0.01 | -0.43 | -1.16 | -0.52 | 225.00 |
| 230.00 | -1.29 | -1.46 | 0.03 | -0.17 | -0.49 | -1.03 | -0.31 | 230.00 |
| 235.00 | -1.30 | -1.68 | -0.64 | -0.36 | -0.55 | -0.80 | 0.00 | 235.00 |
| 240.00 | -1.33 | -1.89 | -1.32 | -0.51 | -0.43 | -0.51 | 0.38 | 240.00 |
| 245.00 | -1.36 | -2.01 | -2.04 | -0.64 | -0.03 | -0.18 | 0.78 | 245.00 |
| 250.00 | -1.37 | -2.03 | -2.45 | -0.94 | 0.44 | 0.07 | 1.18 | 250.00 |
| 255.00 | -1.33 | -2.03 | -3.06 | -1.33 | 0.64 | 0.22 | 1.54 | 255.00 |
| 260.00 | -1.27 | -2.05 | -3.27 | -1.97 | 0.71 | 0.19 | 1.85 | 260.00 |
| 265.00 | -1.23 | -2.06 | -3.36 | -2.85 | 0.76 | 0.15 | 2.14 | 265.00 |
| 270.00 | -1.27 | -2.08 | -3.47 | -3.76 | 0.60 | 0.44 | 2.42 | 270.00 |
| 275.00 | -1.36 | -2.11 | -3.51 | -4.44 | -0.01 | 0.67 | 2.63 | 275.00 |
| 280.00 | -1.47 | -2.16 | -3.52 | -4.75 | -0.91 | 0.02 | 2.41 | 280.00 |
| 285.00 | -1.44 | -2.19 | -3.49 | -4.72 | -1.64 | -0.91 | 1.57 | 285.00 |
| 290.00 | -1.57 | -2.22 | -3.40 | -4.44 | -1.84 | -1.45 | 0.61 | 290.00 |
| 295.00 | -1.56 | -2.23 | -3.26 | -4.05 | -1.57 | -1.22 | 0.25 | 295.00 |
| 300.00 | -1.49 | -2.18 | -3.09 | -3.59 | -1.03 | -0.49 | 0.62 | 300.00 |
| 305.00 | -1.34 | -2.06 | -2.99 | -3.04 | -0.35 | 0.41 | 1.48 | 305.00 |
| 310.00 | -1.12 | -1.88 | -2.85 | -2.41 | 0.42 | 1.60 | 2.55 | 310.00 |
| 315.00 | -0.98 | -1.77 | -2.32 | -1.70 | 1.29 | 2.75 | 3.67 | 315.00 |
| 320.00 | -1.09 | -1.64 | -1.91 | -0.99 | 2.21 | 3.98 | 4.77 | 320.00 |
| 325.00 | -1.28 | -1.43 | -1.43 | -0.29 | 3.15 | 5.26 | 5.86 | 325.00 |
| 330.00 | -1.41 | -1.15 | -0.94 | 0.42 | 4.16 | 6.49 | 7.04 | 330.00 |
| 335.00 | -1.31 | -0.95 | -0.49 | 1.10 | 5.17 | 7.62 | 8.19 | 335.00 |
| 340.00 | -1.14 | -0.87 | -0.02 | 1.91 | 5.97 | 8.48 | 9.11 | 340.00 |
| 345.00 | -1.10 | -0.98 | 0.46 | 2.43 | 6.35 | 8.76 | 9.27 | 345.00 |
| 350.00 | -1.13 | -1.19 | 0.79 | 2.79 | 6.26 | 8.27 | 8.91 | 350.00 |
| 355.00 | -1.16 | -1.39 | 0.92 | 2.82 | 5.85 | 7.40 | 8.05 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.14 | 2.47 | 5.27 | 10.15 | 10.71 | 13.52 | 12.82 | |

# BLADE LOADS

TEST 498 CNTR NO. 404 T.C.No. 09 C.R. 34

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.20 | 0.29 | 1.71 | 4.38 | 2.82 | 3.47 | 3.45 | 0.0 |
| 5.00 | 0.27 | 0.31 | 1.48 | 4.04 | 2.19 | 2.99 | 2.98 | 5.00 |
| 10.00 | 0.30 | 0.30 | 1.31 | 3.28 | 1.19 | 2.10 | 2.01 | 10.00 |
| 15.00 | 0.33 | 0.59 | 1.22 | 2.25 | 0.39 | 1.14 | 0.81 | 15.00 |
| 20.00 | 0.42 | 0.61 | 1.21 | 1.53 | 0.00 | 0.32 | -0.39 | 20.00 |
| 25.00 | 0.37 | 0.62 | 1.28 | 1.26 | -0.27 | -0.33 | -1.31 | 25.00 |
| 30.00 | 0.22 | 0.59 | 1.11 | 1.32 | -0.49 | -0.76 | -1.86 | 30.00 |
| 35.00 | 0.11 | 0.72 | 0.89 | 0.94 | -0.64 | -0.89 | -2.03 | 35.00 |
| 40.00 | 0.12 | 1.29 | 1.07 | 1.31 | -0.69 | -0.78 | -1.98 | 40.00 |
| 45.00 | 0.37 | 1.47 | 1.35 | 1.15 | -0.61 | -0.54 | -1.81 | 45.00 |
| 50.00 | 0.89 | 1.14 | 1.50 | 1.39 | -0.44 | -0.31 | -1.62 | 50.00 |
| 55.00 | 0.95 | 0.85 | 1.46 | 1.62 | -0.29 | -0.16 | -1.93 | 55.00 |
| 60.00 | 0.86 | 0.74 | 1.39 | 1.71 | -0.28 | -0.20 | -1.68 | 60.00 |
| 65.00 | 0.79 | 1.49 | 1.33 | 1.62 | -0.50 | -0.57 | -2.18 | 65.00 |
| 70.00 | 0.70 | 1.87 | 1.15 | 1.38 | -0.92 | -1.35 | -3.24 | 70.00 |
| 75.00 | 0.72 | 1.53 | 0.91 | 0.99 | -1.53 | -2.38 | -4.61 | 75.00 |
| 80.00 | 0.51 | 0.75 | 0.65 | 0.41 | -2.34 | -3.52 | -6.04 | 80.00 |
| 85.00 | -0.09 | 0.79 | 1.11 | -0.32 | -3.28 | -4.49 | -6.72 | 85.00 |
| 90.00 | 0.39 | 1.76 | 0.28 | -0.85 | -4.05 | -4.94 | -6.18 | 90.00 |
| 95.00 | 1.35 | 1.32 | -0.55 | -1.43 | -3.57 | -4.13 | -2.41 | 95.00 |
| 100.00 | 1.37 | 0.63 | 1.72 | -2.93 | -4.09 | -1.31 | 2.45 | 100.00 |
| 105.00 | 0.46 | 0.16 | 1.36 | -1.69 | -2.32 | 2.44 | 4.58 | 105.00 |
| 110.00 | 0.10 | 0.93 | 0.14 | 0.28 | 1.23 | 2.92 | 5.79 | 110.00 |
| 115.00 | 0.07 | 1.46 | -0.72 | -0.35 | 1.75 | 2.87 | 7.21 | 115.00 |
| 120.00 | 0.46 | 1.98 | 1.16 | -0.33 | 1.04 | 3.85 | 7.10 | 120.00 |
| 125.00 | 0.85 | 1.37 | 1.85 | 1.19 | 0.56 | 5.30 | 5.45 | 125.00 |
| 130.00 | 1.13 | 1.23 | 1.70 | 2.31 | 1.26 | 5.84 | 3.27 | 130.00 |
| 135.00 | 1.22 | 1.26 | 1.30 | 1.86 | 2.28 | 5.32 | 2.01 | 135.00 |
| 140.00 | 1.15 | 1.51 | 1.20 | 1.33 | 2.93 | 3.86 | 1.59 | 140.00 |
| 145.00 | 1.04 | 1.76 | 0.94 | 1.22 | 3.05 | 3.25 | 0.84 | 145.00 |
| 150.00 | 1.01 | 1.97 | 1.17 | 1.21 | 2.89 | 2.46 | 0.08 | 150.00 |
| 155.00 | 0.96 | 1.93 | 1.48 | 1.33 | 2.59 | 1.89 | -0.46 | 155.00 |
| 160.00 | 0.92 | 1.66 | 1.73 | 1.38 | 2.27 | 1.41 | -0.79 | 160.00 |
| 165.00 | 0.93 | 1.41 | 1.83 | 1.45 | 2.09 | 1.33 | -0.95 | 165.00 |
| 170.00 | 0.96 | 1.25 | 1.73 | 1.52 | 1.98 | 0.72 | -0.98 | 170.00 |
| 175.00 | 1.00 | 1.19 | 1.42 | 1.58 | 1.98 | 0.52 | -0.92 | 175.00 |
| 180.00 | 1.01 | 1.14 | 1.01 | 1.64 | 1.79 | 0.49 | -0.76 | 180.00 |
| 185.00 | 0.98 | 1.17 | 0.59 | 1.67 | 1.73 | 0.51 | -0.54 | 185.00 |
| 190.00 | 0.92 | 1.03 | 0.28 | .54 | 1.68 | 0.52 | -0.37 | 190.00 |
| 195.00 | 0.84 | 0.86 | 0.08 | 1.25 | 1.49 | 0.42 | -0.29 | 195.00 |
| 200.00 | 0.71 | 0.39 | -0.39 | 0.91 | 1.11 | 0.27 | -0.37 | 200.00 |
| 205.00 | 0.48 | 0.15 | -0.56 | 0.48 | 0.69 | -0.41 | -0.56 | 205.00 |
| 210.00 | 0.18 | -0.09 | -0.48 | -0.08 | 0.29 | -0.84 | -0.85 | 210.00 |
| 215.00 | -0.11 | -0.32 | -1.09 | -0.84 | 0.02 | -1.20 | -1.05 | 215.00 |
| 220.00 | -0.31 | -0.58 | -1.27 | -1.38 | -0.15 | -1.44 | -1.29 | 220.00 |
| 225.00 | -0.51 | -0.86 | -1.35 | -1.35 | -0.19 | -1.58 | -1.45 | 225.00 |
| 230.00 | -0.76 | -1.17 | -1.31 | -1.51 | -0.10 | -1.57 | -1.49 | 230.00 |
| 235.00 | -0.96 | -1.39 | -1.22 | -1.60 | 0.14 | -1.34 | -1.33 | 235.00 |
| 240.00 | -1.14 | -1.52 | -1.12 | -1.64 | 0.51 | -0.91 | -0.92 | 240.00 |
| 245.00 | -1.23 | -1.62 | -1.11 | -1.73 | 1.01 | -0.32 | -0.30 | 245.00 |
| 250.00 | -1.27 | -1.77 | -1.23 | -1.94 | 1.47 | 0.55 | 0.39 | 250.00 |
| 255.00 | -1.30 | -1.96 | -1.49 | -2.20 | 1.55 | 1.43 | 1.25 | 255.00 |
| 260.00 | -1.32 | -2.07 | -2.01 | -2.49 | 0.94 | 2.13 | 2.17 | 260.00 |
| 265.00 | -1.33 | -2.03 | -2.58 | -2.17 | 0.01 | 2.16 | 3.12 | 265.00 |
| 270.00 | -1.31 | -1.97 | -2.96 | -1.54 | -0.94 | 1.34 | 3.91 | 270.00 |
| 275.00 | -1.28 | -1.99 | -3.19 | -1.70 | -1.56 | -0.18 | 3.93 | 275.00 |
| 280.00 | -1.25 | -1.99 | -3.22 | -1.87 | -1.23 | -2.44 | 2.62 | 280.00 |
| 285.00 | -1.25 | -1.95 | -2.79 | -0.35 | -1.31 | -1.96 | 0.86 | 285.00 |
| 290.00 | -1.28 | -2.01 | -2.68 | -4.37 | -3.63 | -2.41 | -0.16 | 290.00 |
| 295.00 | -1.32 | -2.13 | -2.57 | -5.05 | -5.36 | -4.78 | -1.78 | 295.00 |
| 300.00 | -1.35 | -2.30 | -3.44 | -5.82 | -6.84 | -6.00 | -3.84 | 300.00 |
| 305.00 | -1.37 | -2.42 | -3.57 | -6.21 | -6.97 | -6.59 | -4.53 | 305.00 |
| 310.00 | -1.36 | -2.36 | -3.46 | -6.07 | -6.49 | -6.62 | -4.09 | 310.00 |
| 315.00 | -1.33 | -2.19 | -2.52 | -5.22 | -5.48 | -5.52 | -3.05 | 315.00 |
| 320.00 | -1.27 | -1.99 | -1.49 | -3.01 | -3.12 | -3.41 | -1.77 | 320.00 |
| 325.00 | -1.24 | -1.86 | -0.36 | -1.48 | -1.19 | -1.26 | -0.63 | 325.00 |
| 330.00 | -1.25 | -1.79 | -0.07 | -1.13 | -0.16 | -0.14 | 0.39 | 330.00 |
| 335.00 | -1.27 | -1.87 | -0.41 | 0.05 | 1.16 | 0.71 | 1.29 | 335.00 |
| 340.00 | -1.28 | -1.83 | 0.51 | 1.39 | 2.28 | 1.33 | 2.08 | 340.00 |
| 345.00 | -1.23 | -1.93 | 1.11 | 2.09 | 2.16 | 2.53 | 2.73 | 345.00 |
| 350.00 | -1.15 | -1.14 | 1.71 | 3.58 | 2.28 | 2.78 | 3.10 | 350.00 |
| 355.00 | 0.21 | -1.20 | 2.00 | 3.92 | 2.76 | 3.35 | 3.28 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.95 | 4.59 | 8.03 | 12.22 | 12.66 | 16.18 | 14.92 | |

# BLADE LOADS

TEST 498 CNTR NO. 419 T.C.No. 10 C.R. 35

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | 0.14 | 0.68 | 1.67 | 3.35 | 2.49 | 2.74 | 2.63 | 0.0 |
| 5.00 | 0.01 | 0.71 | 1.41 | 2.55 | 1.39 | 1.64 | 1.31 | 5.00 |
| 10.00 | -0.17 | 1.11 | 1.24 | 1.76 | 0.52 | 0.59 | 0.10 | 10.00 |
| 15.00 | 0.04 | 1.43 | 1.21 | 1.29 | -0.02 | -0.20 | -0.79 | 15.00 |
| 20.00 | 0.49 | 1.19 | 1.14 | 1.09 | -0.42 | -0.73 | -1.44 | 20.00 |
| 25.00 | 0.71 | 0.73 | 0.99 | 1.15 | -0.64 | -1.02 | -1.86 | 25.00 |
| 30.00 | 0.62 | 0.52 | 1.03 | 1.25 | -0.74 | -1.05 | -2.07 | 30.00 |
| 35.00 | 0.42 | 0.86 | 1.21 | 1.32 | -0.73 | -0.96 | -2.14 | 35.00 |
| 40.00 | 0.29 | 1.43 | 1.36 | 1.46 | -0.71 | -0.87 | -2.15 | 40.00 |
| 45.00 | 0.29 | 1.16 | 1.37 | 1.51 | -0.74 | -0.89 | -2.19 | 45.00 |
| 50.00 | 0.32 | 0.87 | 1.33 | 1.40 | -0.83 | -1.07 | -2.41 | 50.00 |
| 55.00 | 0.41 | 1.07 | 1.20 | 1.21 | -1.07 | -1.55 | -3.02 | 55.00 |
| 60.00 | 0.58 | 1.52 | 1.06 | 0.95 | -1.45 | -2.33 | -4.05 | 60.00 |
| 65.00 | 0.59 | 1.44 | 0.92 | 0.54 | -2.06 | -3.23 | -5.43 | 65.00 |
| 70.00 | 0.37 | 0.97 | 0.75 | 0.06 | -2.78 | -4.22 | -6.94 | 70.00 |
| 75.00 | 0.04 | 0.43 | 0.48 | -0.44 | -3.45 | -5.13 | -7.83 | 75.00 |
| 80.00 | -0.28 | 0.76 | -0.05 | -0.97 | -3.77 | -5.85 | -7.25 | 80.00 |
| 85.00 | 0.17 | 1.46 | -0.53 | -1.54 | -3.72 | -5.48 | -3.00 | 85.00 |
| 90.00 | 0.99 | 1.14 | 0.24 | -2.02 | -3.91 | -2.23 | 2.90 | 90.00 |
| 95.00 | 0.92 | 0.52 | 1.49 | -0.16 | -2.67 | 1.78 | 4.60 | 95.00 |
| 100.00 | 0.52 | 0.13 | 3.70 | 1.07 | 0.22 | 2.43 | 5.60 | 100.00 |
| 105.00 | 0.29 | 1.31 | -0.32 | 0.37 | 1.90 | 2.16 | 6.67 | 105.00 |
| 110.00 | 0.23 | 1.93 | 0.53 | -0.37 | 0.81 | 3.37 | 5.24 | 110.00 |
| 115.00 | 0.28 | 1.76 | 1.81 | 0.68 | 0.53 | 4.86 | 4.66 | 115.00 |
| 120.00 | 0.78 | 1.26 | 1.83 | 2.18 | 0.80 | 5.82 | 3.46 | 120.00 |
| 125.00 | 1.44 | 0.96 | 1.19 | 2.51 | 1.76 | 5.33 | 2.58 | 125.00 |
| 130.00 | 1.53 | 0.91 | 0.77 | 2.03 | 2.45 | 4.25 | 1.78 | 130.00 |
| 135.00 | 1.28 | 1.02 | 0.58 | 1.59 | 2.63 | 3.27 | 0.94 | 135.00 |
| 140.00 | 1.03 | 1.10 | 0.54 | 1.24 | 2.45 | 2.42 | 0.19 | 140.00 |
| 145.00 | 0.80 | 1.54 | 0.67 | 1.06 | 2.14 | 1.68 | -0.58 | 145.00 |
| 150.00 | 0.75 | 1.65 | 0.97 | 1.05 | 1.76 | 1.02 | -0.98 | 150.00 |
| 155.00 | 0.70 | 1.44 | 1.28 | 1.34 | 1.56 | 0.53 | -1.18 | 155.00 |
| 160.00 | 0.65 | 1.18 | 1.44 | 1.37 | 1.42 | 0.31 | -1.22 | 160.00 |
| 165.00 | 0.61 | 0.99 | 1.45 | 1.12 | 1.33 | 0.26 | -1.13 | 165.00 |
| 170.00 | 0.63 | 0.92 | 1.29 | 1.15 | 1.34 | 0.29 | -0.92 | 170.00 |
| 175.00 | 0.67 | 0.94 | 1.02 | 1.14 | 1.39 | 0.34 | -0.61 | 175.00 |
| 180.00 | 0.71 | 0.67 | 0.67 | 1.04 | 1.42 | 0.39 | -0.33 | 180.00 |
| 185.00 | 0.68 | 0.45 | 0.31 | 0.79 | 1.33 | 0.36 | -0.17 | 185.00 |
| 190.00 | 0.60 | 0.21 | -0.01 | 0.44 | 1.11 | 0.24 | -0.10 | 190.00 |
| 195.00 | 0.49 | -0.02 | -0.29 | 0.05 | 0.83 | 0.01 | -0.15 | 195.00 |
| 200.00 | 0.37 | -0.24 | -0.53 | -0.35 | 0.60 | -0.27 | -0.35 | 200.00 |
| 205.00 | 0.25 | -0.44 | -0.73 | -0.79 | 0.42 | -0.53 | -0.59 | 205.00 |
| 210.00 | 0.06 | -0.63 | -0.86 | -1.16 | 0.29 | -0.76 | -0.79 | 210.00 |
| 215.00 | -0.17 | -0.84 | -0.90 | -1.40 | 0.23 | -0.94 | -0.92 | 215.00 |
| 220.00 | -0.40 | -1.07 | -0.89 | -1.47 | 0.25 | -1.02 | -0.91 | 220.00 |
| 225.00 | -0.58 | -1.30 | -0.84 | -1.35 | 0.46 | -0.90 | -0.80 | 225.00 |
| 230.00 | -0.68 | -1.49 | -0.81 | -1.05 | 0.73 | -0.61 | -0.59 | 230.00 |
| 235.00 | -0.76 | -1.66 | -0.89 | -1.02 | 0.94 | -0.14 | -0.24 | 235.00 |
| 240.00 | -0.83 | -1.77 | -1.21 | -1.05 | 1.11 | 0.50 | 0.29 | 240.00 |
| 245.00 | -0.89 | -1.86 | -1.60 | -1.33 | 1.20 | 1.23 | 0.79 | 245.00 |
| 250.00 | -0.92 | -1.91 | -2.03 | -1.79 | 0.53 | 1.99 | 1.74 | 250.00 |
| 255.00 | -0.91 | -1.87 | -2.39 | -1.65 | -0.39 | 2.39 | 2.78 | 255.00 |
| 260.00 | -0.89 | -1.76 | -2.65 | -1.14 | -0.95 | 1.97 | 3.71 | 260.00 |
| 265.00 | -0.88 | -1.66 | -2.81 | -1.38 | -1.34 | 0.44 | 4.14 | 265.00 |
| 270.00 | -0.91 | -1.61 | -2.78 | -3.13 | -1.30 | -1.25 | 3.64 | 270.00 |
| 275.00 | -0.95 | -1.71 | -2.34 | -4.41 | -1.06 | -2.06 | 2.12 | 275.00 |
| 280.00 | -0.99 | -1.87 | -1.91 | -4.65 | -1.08 | -2.51 | -0.20 | 280.00 |
| 285.00 | -1.01 | -2.05 | -2.46 | -3.47 | -3.43 | -3.67 | -1.91 | 285.00 |
| 290.00 | -1.03 | -2.16 | -3.40 | -3.34 | -3.88 | -4.77 | -3.13 | 290.00 |
| 295.00 | -1.07 | -2.18 | -3.46 | -3.69 | -3.45 | -5.06 | -4.14 | 295.00 |
| 300.00 | -1.10 | -2.13 | -2.96 | -3.85 | -2.98 | -4.53 | -3.96 | 300.00 |
| 305.00 | -1.10 | -2.07 | -2.40 | -3.29 | -2.34 | -3.78 | -3.02 | 305.00 |
| 310.00 | -1.01 | -2.03 | -1.44 | -2.30 | -1.73 | -2.69 | -1.92 | 310.00 |
| 315.00 | -0.92 | -1.95 | -0.70 | -1.53 | -1.37 | -1.53 | -0.84 | 315.00 |
| 320.00 | -0.88 | -1.76 | -1.01 | -0.76 | -0.33 | -0.56 | 0.21 | 320.00 |
| 325.00 | -0.89 | -1.36 | -0.94 | 0.11 | 0.46 | 0.50 | 1.15 | 325.00 |
| 330.00 | -0.78 | -0.84 | -0.10 | 1.10 | 1.22 | 1.55 | 2.03 | 330.00 |
| 335.00 | -0.69 | -0.29 | 0.82 | 2.19 | 1.87 | 2.53 | 2.85 | 335.00 |
| 340.00 | -0.48 | 0.18 | 1.57 | 3.47 | 2.47 | 3.35 | 3.42 | 340.00 |
| 345.00 | -0.43 | 0.42 | 2.11 | 3.78 | 3.10 | 3.91 | 3.90 | 345.00 |
| 350.00 | -0.26 | 0.79 | 2.40 | 3.71 | 3.59 | 4.15 | 4.28 | 350.00 |
| 355.00 | -0.03 | 1.08 | 2.16 | 3.60 | 3.52 | 3.73 | 3.88 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 2.99 | 4.41 | 7.67 | 11.75 | 11.71 | 15.61 | 14.23 | |

# BLADE LOADS

TEST 504 CNTR NO. 269 T.C.No. 11 C.R. 62

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.89 | -0.64 | 1.47 | 2.44 | 4.30 | 5.53 | 5.32 | 0.0 |
| 5.00 | -0.48 | -0.72 | 1.28 | 2.00 | 3.81 | 4.64 | 3.77 | 5.00 |
| 10.00 | -0.20 | -0.97 | 1.31 | 1.42 | 2.87 | 3.31 | 2.26 | 10.00 |
| 15.00 | 0.08 | -0.92 | 1.18 | 0.83 | 1.67 | 2.07 | 1.00 | 15.00 |
| 20.00 | 0.45 | 0.24 | 1.05 | 0.50 | 0.84 | 1.19 | 0.63 | 20.00 |
| 25.00 | 0.53 | 0.53 | 0.97 | 0.53 | 0.06 | 0.56 | -0.63 | 25.00 |
| 30.00 | 0.18 | 0.27 | 0.97 | 0.61 | -0.14 | 0.32 | -1.03 | 30.00 |
| 35.00 | -0.01 | 0.17 | 1.05 | 0.68 | -0.10 | 0.33 | -1.21 | 35.00 |
| 40.00 | 0.47 | 0.31 | 1.17 | 0.77 | -0.04 | 0.36 | -1.28 | 40.00 |
| 45.00 | 0.69 | 0.45 | 1.25 | 0.81 | -0.06 | 0.35 | -1.33 | 45.00 |
| 50.00 | 0.61 | 0.56 | 1.25 | 0.69 | -0.24 | 0.28 | -1.45 | 50.00 |
| 55.00 | 0.57 | 0.70 | 1.11 | 0.24 | -0.62 | -0.32 | -1.77 | 55.00 |
| 60.00 | 0.50 | 0.77 | 0.74 | -0.35 | -1.06 | -0.64 | -2.52 | 60.00 |
| 65.00 | 0.33 | 0.69 | 0.37 | -0.89 | -1.65 | -1.66 | -3.58 | 65.00 |
| 70.00 | -0.03 | 0.32 | 0.60 | -1.23 | -2.50 | -2.93 | -5.08 | 70.00 |
| 75.00 | -0.45 | 0.77 | 1.01 | -1.80 | -3.27 | -4.28 | -6.45 | 75.00 |
| 80.00 | 0.37 | 1.67 | 0.56 | -2.36 | -4.01 | -5.79 | -6.15 | 80.00 |
| 85.00 | 1.36 | 1.49 | -0.38 | -1.61 | -5.45 | -4.67 | -5.26 | 85.00 |
| 90.00 | 0.92 | 1.29 | -0.83 | -1.83 | -4.08 | -3.89 | -4.37 | 90.00 |
| 95.00 | 0.56 | 1.03 | 0.94 | -2.94 | -2.41 | -4.35 | -1.27 | 95.00 |
| 100.00 | 0.48 | 0.49 | 1.31 | -2.97 | -2.57 | -3.46 | 1.26 | 100.00 |
| 105.00 | 0.47 | 0.47 | 0.92 | -1.10 | -3.00 | -0.43 | 4.76 | 105.00 |
| 110.00 | 0.45 | 1.70 | 0.52 | 0.12 | -2.72 | 1.55 | 1.16 | 110.00 |
| 115.00 | 0.42 | 2.01 | 0.32 | 0.25 | -1.18 | 1.76 | -0.29 | 115.00 |
| 120.00 | 0.65 | 2.06 | 0.51 | 0.02 | 0.90 | 1.24 | -1.11 | 120.00 |
| 125.00 | 1.29 | 2.52 | 1.38 | -0.16 | 1.76 | 0.85 | -1.68 | 125.00 |
| 130.00 | 1.80 | 2.51 | 2.01 | -0.17 | 1.43 | 0.37 | -1.94 | 130.00 |
| 135.00 | 1.91 | 2.49 | 2.59 | -0.17 | 0.95 | -0.15 | -2.18 | 135.00 |
| 140.00 | 1.70 | 2.35 | 2.29 | 0.08 | 0.74 | -0.48 | -2.35 | 140.00 |
| 145.00 | 1.71 | 2.23 | 2.20 | 0.79 | 0.65 | -0.59 | -2.35 | 145.00 |
| 150.00 | 1.64 | 2.18 | 2.31 | 2.08 | 0.61 | -0.65 | -2.32 | 150.00 |
| 155.00 | 1.66 | 2.30 | 2.38 | 3.69 | 0.57 | -0.64 | -2.24 | 155.00 |
| 160.00 | 1.65 | 2.56 | 2.45 | 4.96 | 0.61 | -0.53 | -2.03 | 160.00 |
| 165.00 | 1.61 | 2.98 | 2.51 | 5.31 | 0.77 | -0.28 | -1.59 | 165.00 |
| 170.00 | 1.54 | 3.40 | 2.48 | 5.34 | 1.61 | 0.09 | -1.04 | 170.00 |
| 175.00 | 1.44 | 3.58 | 2.32 | 5.11 | 1.29 | 0.41 | -0.48 | 175.00 |
| 180.00 | 1.30 | 3.42 | 2.06 | 4.78 | 1.45 | 0.67 | 0.03 | 180.00 |
| 185.00 | 1.15 | 2.95 | 1.70 | 4.30 | 1.41 | 0.75 | 0.36 | 185.00 |
| 190.00 | 0.98 | 2.34 | 1.26 | 3.68 | 1.16 | 0.63 | 0.43 | 190.00 |
| 195.00 | 0.82 | 1.70 | 0.86 | 2.93 | 0.83 | 0.31 | 0.30 | 195.00 |
| 200.00 | 0.60 | 1.10 | 0.35 | 2.14 | 0.42 | -0.13 | 0.07 | 200.00 |
| 205.00 | 0.34 | 0.54 | -0.17 | 1.48 | 0.62 | -0.57 | -0.16 | 205.00 |
| 210.00 | 0.08 | 0.04 | -0.43 | 1.01 | -0.34 | -0.96 | -0.48 | 210.00 |
| 215.00 | -0.19 | -0.17 | -0.71 | 0.76 | -0.39 | -1.30 | -0.78 | 215.00 |
| 220.00 | -0.45 | -0.76 | -0.96 | 0.65 | -0.70 | -1.51 | -0.95 | 220.00 |
| 225.00 | -0.69 | -1.14 | -1.17 | 0.62 | -0.67 | -1.49 | -0.97 | 225.00 |
| 230.00 | -0.85 | -1.51 | -1.34 | 0.63 | -0.49 | -1.32 | -0.79 | 230.00 |
| 235.00 | -0.97 | -1.82 | -1.52 | 0.65 | -0.18 | -1.06 | -0.42 | 235.00 |
| 240.00 | -1.05 | -2.05 | -1.70 | 0.58 | 0.21 | -0.72 | 0.06 | 240.00 |
| 245.00 | -1.11 | -2.19 | -1.91 | 0.12 | 0.68 | -0.30 | 0.56 | 245.00 |
| 250.00 | -1.13 | -2.28 | -2.15 | -1.10 | 1.24 | 0.23 | 1.11 | 250.00 |
| 255.00 | -1.11 | -2.31 | -2.40 | -2.95 | 1.86 | 0.94 | 1.73 | 255.00 |
| 260.00 | -1.08 | -2.29 | -2.63 | -4.09 | 2.49 | 1.88 | 2.43 | 260.00 |
| 265.00 | -1.04 | -2.24 | -2.82 | -4.42 | 2.20 | 2.76 | 3.24 | 265.00 |
| 270.00 | -1.04 | -2.16 | -2.95 | -4.61 | 0.30 | 3.04 | 4.14 | 270.00 |
| 275.00 | -1.06 | -2.09 | -2.94 | -4.74 | -2.93 | 1.15 | 5.05 | 275.00 |
| 280.00 | -1.11 | -2.11 | -2.64 | -4.70 | -3.95 | -3.47 | 3.44 | 280.00 |
| 285.00 | -1.14 | -2.28 | -2.43 | -4.61 | -3.80 | -5.00 | -1.93 | 285.00 |
| 290.00 | -1.17 | -2.58 | -3.34 | -4.65 | -3.41 | -4.57 | -3.74 | 290.00 |
| 295.00 | -1.20 | -2.79 | -4.31 | -5.01 | -3.05 | -3.79 | -3.15 | 295.00 |
| 300.00 | -1.25 | -2.92 | -4.40 | -5.13 | -2.84 | -3.13 | -2.05 | 300.00 |
| 305.00 | -1.29 | -2.97 | -3.88 | -4.58 | -2.49 | -2.54 | -1.13 | 305.00 |
| 310.00 | -1.28 | -2.98 | -3.25 | -3.76 | -1.74 | -1.67 | -0.35 | 310.00 |
| 315.00 | -1.27 | -2.93 | -2.64 | -2.87 | -0.77 | -0.61 | 0.40 | 315.00 |
| 320.00 | -1.27 | -2.79 | -2.02 | -1.82 | 0.22 | 0.54 | 1.44 | 320.00 |
| 325.00 | -1.34 | -2.34 | -1.45 | -0.18 | 1.11 | 1.70 | 3.09 | 325.00 |
| 330.00 | -1.39 | -1.87 | -0.85 | 1.33 | 1.96 | 2.83 | 4.01 | 330.00 |
| 335.00 | -1.34 | -1.55 | -0.22 | 1.31 | 2.91 | 4.11 | 4.93 | 335.00 |
| 340.00 | -1.26 | -1.34 | 0.42 | 1.79 | 3.94 | 5.17 | 5.87 | 340.00 |
| 345.00 | -1.18 | -1.17 | 1.11 | 2.60 | 4.59 | 5.80 | 6.62 | 345.00 |
| 350.00 | -1.38 | -0.99 | 1.63 | 3.06 | 4.80 | 6.01 | 6.92 | 350.00 |
| 355.00 | -1.01 | -0.76 | 1.70 | 2.92 | 4.58 | 5.83 | 6.57 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.87 | 4.55 | 7.63 | 12.74 | 12.27 | 15.15 | 13.88 | |

# TEXT NOT REPRODUCIBLE

## BLADE LOADS

TEST 504 CNTR NO. 278 T.C.N. 12 C.R. 63

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.90 | +0.63 | 1.71 | 2.15 | 3.87 | 3.96 | 3.41 | 0.0 |
| 5.00 | -0.23 | -1.11 | 0.96 | 1.38 | 2.27 | 2.77 | 1.78 | 5.00 |
| 10.00 | -0.00 | -1.04 | 0.57 | 0.98 | 1.15 | 1.35 | 0.28 | 10.00 |
| 15.00 | -0.21 | -0.68 | 0.44 | 0.18 | 0.14 | 0.19 | -2.74 | 15.00 |
| 20.00 | -0.01 | -0.20 | 0.41 | -0.37 | -0.53 | -0.57 | -1.52 | 20.00 |
| 25.00 | 0.58 | -0.06 | 0.38 | -0.50 | -0.92 | -0.96 | -2.11 | 25.00 |
| 30.00 | 0.92 | 0.01 | 0.48 | -0.45 | -1.10 | -1.07 | -2.47 | 30.00 |
| 35.00 | -0.09 | 0.01 | 0.48 | -0.32 | -1.15 | -1.01 | -2.57 | 35.00 |
| 40.00 | -0.26 | 0.09 | 0.44 | -0.22 | -1.12 | -0.93 | -2.57 | 40.00 |
| 45.00 | -0.82 | 0.23 | 0.75 | -0.22 | -1.10 | -0.90 | -2.99 | 45.00 |
| 50.00 | 0.10 | 0.37 | 0.70 | -0.34 | -1.19 | -1.02 | -2.78 | 50.00 |
| 55.00 | 0.04 | 0.48 | 0.98 | -0.58 | -1.42 | -1.33 | -3.27 | 55.00 |
| 60.00 | -0.00 | 0.49 | 0.21 | -0.99 | -1.90 | -1.97 | -4.00 | 60.00 |
| 65.00 | -0.09 | 0.32 | 0.00 | -1.48 | -2.61 | -2.93 | -5.18 | 65.00 |
| 70.00 | -0.34 | 0.14 | 0.28 | -2.00 | -3.47 | -4.41 | -6.93 | 70.00 |
| 75.00 | -0.5. | 0.00 | 0.20 | -2.63 | -4.05 | -5.01 | -7.82 | 75.00 |
| 80.00 | -0.07 | 1.40 | -0.34 | -2.71 | -5.15 | -5.67 | -5.65 | 80.00 |
| 85.00 | 0.99 | 1.14 | -1.27 | -2.30 | -5.70 | -4.34 | -5.09 | 85.00 |
| 90.00 | 0.95 | 0.00 | -0.05 | -2.78 | -3.55 | -4.57 | -2.39 | 90.00 |
| 95.00 | 0.57 | 0.71 | 0.76 | -3.55 | -2.79 | -4.00 | 0.41 | 95.00 |
| 100.00 | 0.39 | 0.43 | 1.02 | -2.02 | -3.36 | -2.05 | 1.46 | 100.00 |
| 105.00 | 0.41 | 0.64 | 0.00 | -0.01 | -3.38 | 0.25 | 0.67 | 105.00 |
| 110.00 | 0.46 | 1.03 | 0.21 | -0.00 | -2.58 | 1.00 | -0.33 | 110.00 |
| 115.00 | 0.58 | 2.00 | 0.02 | -0.07 | -0.54 | 1.77 | -0.99 | 115.00 |
| 120.00 | 0.76 | 2.00 | 0.35 | -0.25 | 1.38 | 0.87 | -1.47 | 120.00 |
| 125.00 | 1.14 | 2.41 | 1.57 | -0.29 | 1.07 | 0.34 | -1.75 | 125.00 |
| 130.00 | 1.41 | 2.31 | 2.44 | -0.20 | 1.62 | 0.11 | -1.90 | 130.00 |
| 135.00 | 1.00 | 2.27 | 2.43 | -0.15 | 1.14 | -0.87 | -2.05 | 135.00 |
| 140.00 | 1.00 | 2.20 | 2.25 | 0.20 | 0.76 | -0.26 | -2.00 | 140.00 |
| 145.00 | 1.75 | 2.17 | 2.29 | 1.09 | 0.63 | -0.39 | -2.02 | 145.00 |
| 150.00 | 1.78 | 2.20 | 2.37 | 2.34 | 0.65 | -0.40 | -1.87 | 150.00 |
| 155.00 | 1.66 | 2.20 | 2.42 | 3.03 | 0.69 | -0.26 | -1.61 | 155.00 |
| 160.00 | 1.64 | 2.43 | 2.46 | 4.00 | 0.83 | -0.02 | -1.24 | 160.00 |
| 165.00 | 1.60 | 2.71 | 2.47 | 5.34 | 1.09 | 0.34 | -0.00 | 165.00 |
| 170.00 | 1.53 | 3.07 | 2.70 | 5.42 | 1.41 | 0.77 | -0.32 | 170.00 |
| 175.00 | 1.42 | 3.27 | 2.15 | 5.70 | 1.67 | 1.02 | 0.17 | 175.00 |
| 180.00 | 1.20 | 3.11 | 1.05 | 4.00 | 1.70 | 1.11 | 0.56 | 180.00 |
| 185.00 | 1.11 | 2.66 | 1.48 | 4.43 | 1.73 | 1.06 | 0.79 | 185.00 |
| 190.00 | 0.90 | 2.11 | 1.06 | 3.01 | 1.44 | 0.85 | 0.82 | 190.00 |
| 195.00 | 0.64 | 1.54 | 0.64 | 3.15 | 1.09 | 0.52 | 0.70 | 195.00 |
| 200.00 | 0.38 | 1.00 | 0.23 | 2.59 | 0.70 | 0.20 | 0.43 | 200.00 |
| 205.00 | 0.14 | 0.51 | -0.14 | 1.98 | 0.38 | -0.11 | 0.12 | 205.00 |
| 210.00 | -0.03 | 0.03 | -0.40 | 1.52 | 0.16 | -0.34 | -0.10 | 210.00 |
| 215.00 | -0.22 | -0.38 | -0.80 | 1.38 | -0.03 | -0.57 | -0.22 | 215.00 |
| 220.00 | -0.38 | -0.74 | -1.02 | 1.27 | -0.12 | -0.66 | -0.23 | 220.00 |
| 225.00 | -0.56 | -1.00 | -1.19 | 1.27 | -0.06 | -0.67 | -0.12 | 225.00 |
| 230.00 | -0.72 | -1.37 | -1.32 | 1.28 | 0.15 | -0.58 | 0.11 | 230.00 |
| 235.00 | -0.82 | -1.60 | -1.47 | 1.13 | 0.49 | -0.20 | 0.45 | 235.00 |
| 240.00 | -0.88 | -1.78 | -1.64 | 0.55 | 0.92 | 0.24 | 0.88 | 240.00 |
| 245.00 | -0.92 | -1.91 | -1.82 | -0.65 | 1.48 | 0.65 | 1.39 | 245.00 |
| 250.00 | -0.99 | -1.99 | -2.03 | -2.03 | 1.95 | 1.19 | 1.99 | 250.00 |
| 255.00 | -1.04 | -1.99 | -2.25 | -3.05 | 2.53 | 1.94 | 2.69 | 255.00 |
| 260.00 | -1.05 | -1.91 | -2.44 | -4.01 | 2.47 | 3.03 | 3.54 | 260.00 |
| 265.00 | -1.02 | -1.81 | -2.59 | -3.90 | 2.05 | 3.68 | 4.45 | 265.00 |
| 270.00 | -0.99 | -1.81 | -2.65 | -4.04 | -1.24 | 2.55 | 5.05 | 270.00 |
| 275.00 | -0.99 | -2.01 | -2.54 | -4.07 | -5.14 | -0.78 | 4.39 | 275.00 |
| 280.00 | -1.01 | -2.20 | -2.47 | -4.00 | -3.20 | -4.38 | 1.73 | 280.00 |
| 285.00 | -1.03 | -2.51 | -2.99 | -4.16 | -3.44 | -4.31 | -2.06 | 285.00 |
| 290.00 | -1.04 | -2.66 | -3.74 | -4.32 | -2.75 | -3.35 | -2.62 | 290.00 |
| 295.00 | -1.09 | -2.71 | -3.91 | -4.37 | -2.44 | -2.39 | -1.72 | 295.00 |
| 300.00 | -1.07 | -2.67 | -3.91 | -4.01 | -1.98 | -1.99 | -0.76 | 300.00 |
| 305.00 | -1.10 | -2.55 | -2.97 | -3.34 | -1.35 | -1.33 | 0.12 | 305.00 |
| 310.00 | -1.14 | -2.44 | -2.44 | -2.59 | -0.68 | -0.51 | 0.97 | 310.00 |
| 315.00 | -1.24 | -2.27 | -1.92 | -1.80 | 0.26 | 0.58 | 1.95 | 315.00 |
| 320.00 | -1.34 | -2.05 | -1.35 | -0.82 | 1.17 | 1.58 | 2.98 | 320.00 |
| 325.00 | -1.31 | -1.73 | -0.81 | 0.11 | 2.15 | 2.51 | 3.91 | 325.00 |
| 330.00 | -1.06 | -1.40 | -0.12 | 0.71 | 3.04 | 4.02 | 4.78 | 330.00 |
| 335.00 | -0.76 | -1.12 | 1.11 | 1.60 | 3.82 | 5.03 | 5.00 | 335.00 |
| 340.00 | -0.73 | -0.91 | 2.18 | 2.68 | 4.44 | 5.75 | 6.29 | 340.00 |
| 345.00 | -0.78 | -0.75 | 2.93 | 3.44 | 4.72 | 6.01 | 6.78 | 345.00 |
| 350.00 | -0.40 | -0.60 | 2.62 | 4.01 | 4.42 | 5.59 | 6.37 | 350.00 |
| 355.00 | -0.40 | -0.52 | 2.48 | 3.85 | 3.71 | 4.73 | 4.78 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.14 | 4.88 | 7.10 | 11.03 | 11.42 | 14.24 | 12.88 | |

# BLADE LOADS

TEST 504 CNTR NO. 911 T.C.No. 13 C.R. 64

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.77 | -C.74 | 1.C1 | 3.2[illegible] | 3.62 | 4.[illegible]9 | 4.71 | 0.0 |
| 5.00 | -0.27 | -C.6[illegible] | C.59 | 1.86 | 2.58 | 3.[illegible] | 2.91 | 5.00 |
| 10.00 | 0.12 | -C.6[illegible] | 1.C7 | 0.8[illegible] | 1.58 | 2.65 | 1.37 | 10.00 |
| 15.00 | 0.20 | -C.C6 | 1.25 | C.6C | 0.88 | 1.60 | 0.31 | 15.00 |
| 20.00 | -0.1[illegible] | C.3[illegible] | 1.2C | C.65 | 0.69 | 1.06 | -0.34 | 20.00 |
| 25.00 | -0.3[illegible] | C.3[illegible] | 1.1C | C.7[illegible] | 0.36 | 0.84 | -0.66 | 25.00 |
| 30.00 | 0.24 | C.3[illegible] | 1.C4 | C.74 | 0.37 | 0.74 | -0.86 | 30.00 |
| 35.00 | 0.6[illegible] | C.5C | 1.C8 | 0.66 | 0.43 | 0.72 | -0.99 | 35.00 |
| 40.00 | 0.67 | C.6[illegible] | 1.1[illegible] | C.52 | 0.39 | C.73 | -1.13 | 40.00 |
| 45.00 | 0.4[illegible] | C.66 | 1.2[illegible] | C.5C | 0.19 | 0.[illegible]1 | -1.34 | 45.00 |
| 50.00 | 0.3[illegible] | C.61 | 1.11 | C.33 | -0.73 | 0.07 | -1.[illegible]8 | 50.00 |
| 55.00 | 0.2[illegible] | C.42 | C.72 | -C.66 | -0.80 | -0.49 | -2.92 | 55.00 |
| 60.00 | 0.07 | C.C7 | -C.14 | -1.C[illegible] | -1.67 | -1.[illegible]7 | -3.40 | 60.00 |
| 65.00 | -0.[illegible] | -C.12 | C.61 | -1.1C | -3.17 | -3.[illegible]5 | -4.75 | 65.00 |
| 70.00 | -0.02 | 1.1[illegible] | C.[illegible]2 | -2.45 | -3.68 | -[illegible].01 | -6.75 | 70.00 |
| 75.00 | 1.1[illegible] | 1.4C | C.1C | -3.4[illegible] | -4.08 | -4.1[illegible] | -7.36 | 75.00 |
| 80.00 | 1.0[illegible] | C.71 | -1.C[illegible] | -[illegible].47 | -4.0[illegible] | -4.54 | -[illegible].82 | 80.00 |
| 85.00 | [illegible].[illegible]7 | C.6[illegible] | -C.[illegible]6 | -2.5C | -[illegible].01 | -[illegible].07 | -[illegible].80 | 85.00 |
| 90.00 | 0.47 | C.[illegible]7 | C.4[illegible] | -3.66 | -[illegible].[illegible]9 | -[illegible].54 | -3.[illegible]8 | 90.00 |
| 95.00 | 0.3[illegible] | C.1[illegible] | C.[illegible]C | -3.6[illegible] | -[illegible].[illegible]1 | -5.41 | -1.34 | 95.00 |
| 100.00 | 0.31 | C.[illegible]6 | C.[illegible]5 | -2.02 | -3.72 | -2.7[illegible] | 0.11 | 100.00 |
| 105.00 | 0.22 | 1.[illegible]5 | C.1C | -C.7[illegible] | -3.[illegible]9 | -0.[illegible]8 | -0.C7 | 105.00 |
| 110.00 | 0.4C | 2.14 | -C.1C | -C.7[illegible] | -2.35 | C.[illegible]9 | -1.17 | 110.00 |
| 115.00 | 1.[illegible]7 | 2.C[illegible] | C.[illegible]7 | -1.C1 | -0.[illegible]9 | -0.70 | -2.28 | 115.00 |
| 120.00 | [illegible].[illegible] | 2.23 | [illegible].64 | -[illegible].02 | C.41 | -0.[illegible]3 | -3.08 | 120.00 |
| 125.00 | 2.0[illegible] | 2.34 | 2.1[illegible] | -1.11 | 0.32 | -1.12 | -[illegible].38 | 125.00 |
| 130.00 | 1.9[illegible] | 2.2[illegible] | 2.C6 | -1.21 | -0.05 | -1.37 | -[illegible].[illegible]9 | 130.00 |
| 135.00 | 1.[illegible]8 | 2.1[illegible] | 1.74 | -C.84 | -0.20 | -1.[illegible]3 | -[illegible].[illegible]7 | 135.00 |
| 140.00 | 2.0[illegible] | 2.C[illegible] | 1.[illegible]1 | C.24 | -C.17 | -1.41 | -[illegible].41 | 140.00 |
| 145.00 | 2.02 | 2.C1 | [illegible].1C | 2.C[illegible] | -0.10 | -1.[illegible]8 | -3.2C | 145.00 |
| 150.00 | 1.94 | 2.2[illegible] | 2.24 | [illegible].[illegible]8 | -0.0[illegible] | -1.[illegible]3 | -2.[illegible]5 | 150.00 |
| 155.00 | 1.94 | 2.52 | 2.[illegible]4 | 4.6C | 0.1[illegible] | -C.[illegible]0 | -2.44 | 155.00 |
| 160.00 | 1.84 | [illegible].[illegible]8 | [illegible].4[illegible] | 5.12 | 0.52 | -C.4C | -1.[illegible]8 | 160.00 |
| 165.00 | 1.74 | [illegible].[illegible]5 | 2.[illegible]4 | 4.17 | 0.[illegible]0 | -C.12 | -1.42 | 165.00 |
| 170.00 | 1.[illegible]8 | [illegible].[illegible]2 | [illegible].[illegible]4 | 4.[illegible]A | 1.2[illegible] | C.3[illegible] | -0.76 | 170.00 |
| 175.00 | 1.5[illegible] | [illegible].4[illegible] | 2.[illegible]8 | 4.61 | 1.47 | 0.7[illegible] | -0.11 | 175.00 |
| 180.00 | 1.4[illegible] | [illegible].1[illegible] | [illegible].14 | 4.[illegible]7 | 1.[illegible]7 | C.[illegible]4 | 0.[illegible]7 | 180.00 |
| 185.00 | 1.3[illegible] | 2.[illegible]C | 1.[illegible]C | [illegible].[illegible]A | 1.46 | 0.[illegible]7 | 0.61 | 185.00 |
| 190.00 | 1.1[illegible] | 1.[illegible]8 | 1.[illegible]1 | [illegible].2C | 1.15 | C.[illegible]9 | 0.[illegible]7 | 190.00 |
| 195.00 | 0.[illegible]1 | 1.[illegible]A | C.[illegible]3 | 2.4[illegible] | 0.76 | [illegible].17 | 0.54 | 195.00 |
| 200.00 | 0.[illegible]4 | 0.77 | C.44 | 1.7[illegible] | 0.35 | -0.27 | 0.29 | 200.00 |
| 205.00 | 0.1C | C.27 | C.12 | 1.21 | 0.00 | -0.[illegible]9 | -0.[illegible]4 | 205.00 |
| 210.00 | -0.2[illegible] | -C.27 | -C.2C | C.[illegible]1 | -0.27 | -1.01 | -0.37 | 210.00 |
| 215.00 | -0.4[illegible] | -C.7[illegible] | -C.4[illegible] | 0.42 | -0.44 | -1.70 | -0.[illegible]6 | 215.00 |
| 220.00 | -[illegible].[illegible]8 | -1.17 | -C.7[illegible] | 0.5[illegible] | -0.[illegible]6 | -1.74 | -[illegible].60 | 220.00 |
| 225.00 | -0.9C | -1.[illegible]C | -1.CC | C.52 | -0.32 | -1.10 | -0.[illegible]5 | 225.00 |
| 230.00 | -1.01 | -1.7[illegible] | -1.24 | C.[illegible]8 | -0.06 | -0.[illegible]1 | -0.1[illegible] | 230.00 |
| 235.00 | -1.[illegible]8 | -1.[illegible]4 | -[illegible].[illegible]1 | C.74 | 0.30 | -0.44 | 0.27 | 235.00 |
| 240.00 | -1.17 | -2.17 | -1.[illegible]C | C.6[illegible] | 0.74 | -0.01 | 0.76 | 240.00 |
| 245.00 | -1.[illegible]4 | -2.2[illegible] | -[illegible].C6 | 0.0[illegible] | 1.27 | C.[illegible]9 | 1.3[illegible] | 245.00 |
| 250.00 | -1.[illegible]C | -2.3[illegible] | -2.31 | -1.[illegible]5 | 1.[illegible]7 | C.[illegible]9 | 1.[illegible]3 | 250.00 |
| 255.00 | -1.[illegible]1 | -2.4[illegible] | -[illegible].[illegible]1 | -3.21 | [illegible].[illegible]5 | 1.[illegible]5 | [illegible].[illegible]7 | 255.00 |
| 260.00 | -1.[illegible]8 | -2.4[illegible] | -[illegible].[illegible]9 | -4.45 | 3.07 | 2.3[illegible] | 3.28 | 260.00 |
| 265.00 | -1.[illegible]3 | -2.[illegible]1 | -[illegible].[illegible]8 | -4.[illegible]5 | 1.[illegible]7 | [illegible].[illegible]7 | 4.41 | 265.00 |
| 270.00 | -1.[illegible]3 | -2.[illegible]3 | -[illegible].24 | -4.[illegible]A | -0.41 | [illegible].[illegible]0 | 5.77 | 270.00 |
| 275.00 | -1.2[illegible] | -2.[illegible]7 | -[illegible].[illegible]0 | -4.[illegible]6 | -[illegible].13 | -0.70 | 5.50 | 275.00 |
| 280.00 | -1.[illegible]4 | -2.41 | -[illegible].11 | -4.[illegible]5 | -3.[illegible]8 | -[illegible].[illegible]0 | 1.[illegible]3 | 280.00 |
| 285.00 | -1.41 | -2.3[illegible] | -[illegible].2[illegible] | -4.2[illegible] | -3.50 | -4.[illegible]5 | -2.52 | 285.00 |
| 290.00 | -1.4[illegible] | -2.[illegible]4 | -2.1C | -4.05 | -2.64 | -[illegible].[illegible]9 | -[illegible].5C | 290.00 |
| 295.00 | -1.4[illegible] | -2.4[illegible] | -[illegible].[illegible]4 | -4.4C | -1.[illegible]8 | -2.[illegible]3 | -2.[illegible]8 | 295.00 |
| 300.00 | -1.[illegible]8 | -2.[illegible]4 | -4.12 | -4.[illegible]8 | -1.[illegible]7 | -1.A1 | -0.42 | 300.00 |
| 305.00 | -1.2[illegible] | -2.[illegible]8 | -[illegible].81 | -4.11 | -1.60 | -0.[illegible]3 | 0.47 | 305.00 |
| 310.00 | -1.24 | -2.[illegible]5 | -[illegible].C4 | -[illegible].[illegible]7 | -0.62 | C.3[illegible] | 1.[illegible]7 | 310.00 |
| 315.00 | -1.2[illegible] | -2.[illegible]4 | -2.23 | -1.[illegible]7 | 0.[illegible]4 | 1.A[illegible] | 2.[illegible]8 | 315.00 |
| 320.00 | -1.[illegible]2 | -2.[illegible]2 | -[illegible].[illegible]6 | -C.[illegible]3 | 1.[illegible]7 | [illegible].05 | [illegible].63 | 320.00 |
| 325.00 | -1.[illegible]4 | -1.[illegible]8 | -C.[illegible]7 | C.42 | [illegible].21 | 4.23 | 4.[illegible]2 | 325.00 |
| 330.00 | -1.[illegible]3 | -1.[illegible]C | -C.[illegible]A | 2.14 | 3.23 | 4.[illegible]7 | 5.70 | 330.00 |
| 335.00 | -1.34 | -1.C2 | C.3C | [illegible].58 | 3.84 | 5.65 | 6.[illegible]9 | 335.00 |
| 340.00 | -1.14 | -C.[illegible]7 | [illegible].[illegible]5 | 4.[illegible]5 | 4.85 | A.43 | 7.[illegible]3 | 340.00 |
| 345.00 | -0.[illegible]7 | -C.[illegible]3 | [illegible].[illegible]4 | [illegible].[illegible]8 | [illegible].37 | 6.A[illegible] | 7.74 | 345.00 |
| 350.00 | -1.14 | -C.26 | [illegible].[illegible]9 | [illegible].[illegible]C | [illegible].12 | 6.40 | 7.57 | 350.00 |
| 355.00 | -1.[illegible]9 | -C.[illegible]4 | [illegible].[illegible]9 | 4.91 | 4.50 | [illegible].[illegible]5 | 6.41 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.[illegible] | [illegible].[illegible] | 7.[illegible]C | 13.2[illegible] | 12.35 | 15.64 | 14.42 | |

TEXT NOT REPRODUCIBLE

## BLADE LOADS

TEST 904 CNTR NO. 529 T.C.N. 14 C.R. 65

SPAN STATION

| DEG | 32.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -0.77 | -0.76 | 1.65 | 2.56 | 2.11 | 2.40 | 4.74 | 0.0 |
| 5.00 | -0.85 | 0.06 | 1.33 | 1.76 | 0.93 | 2.84 | 3.06 | 5.00 |
| 10.00 | -0.74 | 0.28 | 1.47 | 1.61 | 0.46 | 1.65 | 1.93 | 10.00 |
| 15.00 | 0.07 | -0.33 | 0.92 | 1.69 | 1.96 | 1.83 | 0.82 | 15.00 |
| 20.00 | 0.66 | -0.13 | 0.65 | 0.67 | 1.69 | 2.24 | 0.46 | 20.00 |
| 25.00 | 0.51 | 0.83 | 1.69 | 1.05 | 1.19 | 1.05 | 0.13 | 25.00 |
| 30.00 | 0.89 | 0.10 | 0.30 | 2.25 | 1.40 | 1.44 | -0.45 | 30.00 |
| 35.00 | 0.54 | -0.22 | 1.25 | 2.30 | 1.57 | 1.80 | -1.46 | 35.00 |
| 40.00 | 0.80 | 0.65 | 0.65 | 0.84 | 0.74 | 1.46 | -0.36 | 40.00 |
| 45.00 | 0.22 | 1.08 | 2.28 | 1.25 | 0.48 | 2.44 | -0.82 | 45.00 |
| 50.00 | 0.76 | 1.30 | 1.44 | 1.34 | -0.27 | -0.61 | -1.01 | 50.00 |
| 55.00 | 0.64 | 1.03 | 0.35 | -0.04 | -1.37 | -0.10 | -1.36 | 55.00 |
| 60.00 | 0.47 | 0.40 | -0.30 | -0.44 | -0.60 | -1.47 | -0.44 | 60.00 |
| 65.00 | 0.05 | 0.99 | 1.76 | 0.13 | -0.83 | -2.03 | -2.81 | 65.00 |
| 70.00 | 0.96 | 1.28 | 1.64 | -2.69 | -2.66 | -2.41 | -0.37 | 70.00 |
| 75.00 | 0.66 | 1.28 | 0.60 | -3.11 | -3.92 | -4.85 | -4.02 | 75.00 |
| 80.00 | 0.84 | 1.05 | -0.85 | -1.91 | -0.97 | -4.71 | -2.09 | 80.00 |
| 85.00 | 0.65 | 1.11 | 0.25 | -1.86 | -3.04 | -2.62 | -1.69 | 85.00 |
| 90.00 | 0.67 | 0.80 | 1.47 | -3.69 | -2.18 | -3.78 | 0.44 | 90.00 |
| 95.00 | 0.75 | 1.54 | 1.00 | -1.71 | -2.48 | -1.97 | 1.80 | 95.00 |
| 100.00 | 1.12 | 0.23 | 0.31 | -0.18 | -2.56 | 0.80 | 3.09 | 100.00 |
| 105.00 | 1.08 | 2.09 | 1.42 | -0.76 | -0.89 | 2.37 | 3.16 | 105.00 |
| 110.00 | 1.87 | 2.65 | 1.05 | -1.56 | 0.91 | 2.21 | -0.07 | 110.00 |
| 115.00 | 2.21 | 2.46 | 1.84 | -1.17 | 1.35 | 0.88 | -1.83 | 115.00 |
| 120.00 | 2.34 | 2.84 | 2.69 | -1.07 | 1.47 | 0.11 | -2.38 | 120.00 |
| 125.00 | 2.21 | 2.87 | 2.01 | -0.46 | 1.20 | -0.36 | -2.01 | 125.00 |
| 130.00 | 2.05 | 2.62 | 1.67 | -0.04 | 0.89 | -0.62 | -2.36 | 130.00 |
| 135.00 | 2.24 | 2.39 | 1.61 | 0.81 | 0.64 | -0.77 | -1.65 | 135.00 |
| 140.00 | 2.15 | 2.68 | 1.36 | 2.16 | 0.76 | -1.12 | -2.69 | 140.00 |
| 145.00 | 1.64 | 2.69 | 1.55 | 3.06 | 0.12 | -1.71 | -2.65 | 145.00 |
| 150.00 | 2.04 | 2.84 | 2.07 | 4.46 | 0.10 | -1.19 | -2.28 | 150.00 |
| 155.00 | 2.02 | 2.14 | 2.18 | 4.72 | 0.31 | -1.13 | -2.07 | 155.00 |
| 160.00 | 1.69 | 2.38 | 2.19 | 4.74 | 0.38 | -0.64 | -2.65 | 160.00 |
| 165.00 | 2.01 | 2.46 | 2.14 | 4.47 | 0.27 | -0.65 | -2.14 | 165.00 |
| 170.00 | 1.62 | 2.45 | 2.63 | 4.36 | 0.66 | -0.95 | -2.69 | 170.00 |
| 175.00 | 1.66 | 2.17 | 2.38 | 3.76 | 0.74 | -0.13 | -1.71 | 175.00 |
| 180.00 | 1.92 | 2.66 | 2.71 | 3.17 | 0.46 | -0.13 | -0.87 | 180.00 |
| 185.00 | 1.78 | 2.64 | 2.46 | 2.63 | 0.29 | -0.46 | -0.65 | 185.00 |
| 190.00 | 0.85 | 2.40 | 2.69 | 1.80 | -0.19 | -0.90 | -1.00 | 190.00 |
| 195.00 | 0.44 | 0.16 | 0.66 | 1.13 | -0.65 | -1.73 | -1.17 | 195.00 |
| 200.00 | 0.05 | 0.28 | 0.29 | 0.47 | -0.70 | -1.65 | -1.44 | 200.00 |
| 205.00 | -0.29 | -0.15 | -0.14 | 0.35 | -1.00 | -1.87 | -1.44 | 205.00 |
| 210.00 | -0.46 | -0.68 | -0.44 | 0.06 | -1.24 | -1.96 | -1.74 | 210.00 |
| 215.00 | -0.65 | -1.20 | -0.76 | -0.16 | -1.73 | -1.87 | -1.67 | 215.00 |
| 220.00 | -0.65 | -1.04 | -1.00 | -0.14 | -1.90 | -1.80 | -1.43 | 220.00 |
| 225.00 | -1.11 | -1.39 | -1.35 | -0.32 | -1.85 | -1.66 | -1.15 | 225.00 |
| 230.00 | -1.25 | -2.00 | -1.68 | -0.14 | -1.83 | -1.98 | -1.76 | 230.00 |
| 235.00 | -1.46 | -2.31 | -1.69 | -0.36 | -1.14 | -1.90 | -0.92 | 235.00 |
| 240.00 | -1.41 | -2.01 | -2.20 | -0.69 | 0.24 | -1.68 | 0.22 | 240.00 |
| 245.00 | -1.30 | -2.49 | -2.66 | -1.73 | 1.60 | 0.74 | 0.80 | 245.00 |
| 250.00 | -1.57 | -2.70 | -2.64 | -1.65 | 1.84 | 1.06 | 1.67 | 250.00 |
| 255.00 | -1.82 | -2.70 | -2.26 | -4.17 | 1.89 | 1.26 | 2.19 | 255.00 |
| 260.00 | -1.96 | -2.71 | -2.68 | -4.11 | 1.70 | 2.77 | 3.65 | 260.00 |
| 265.00 | -1.96 | -2.75 | -2.84 | -5.66 | 1.64 | 1.62 | 4.47 | 265.00 |
| 270.00 | -1.89 | -2.67 | -2.65 | -5.46 | 1.01 | -0.65 | 4.14 | 270.00 |
| 275.00 | -1.67 | -2.63 | -2.24 | -5.63 | -0.33 | -2.61 | 1.63 | 275.00 |
| 280.00 | -1.74 | -2.63 | -2.58 | -5.80 | -2.00 | -4.09 | -1.65 | 280.00 |
| 285.00 | -1.76 | -2.72 | -2.63 | -5.66 | -2.78 | -3.90 | -2.62 | 285.00 |
| 290.00 | -1.69 | -2.71 | -2.67 | -4.76 | -2.69 | -3.71 | -0.78 | 290.00 |
| 295.00 | -1.57 | -2.69 | -2.71 | -5.63 | -2.70 | -2.94 | -0.28 | 295.00 |
| 300.00 | -1.57 | -2.61 | -2.61 | -5.63 | -2.83 | -4.08 | -2.73 | 300.00 |
| 305.00 | -1.57 | -2.63 | -2.64 | -4.71 | -2.09 | -2.24 | -1.37 | 305.00 |
| 310.00 | -1.54 | -2.57 | -2.16 | -3.66 | -0.67 | -0.63 | 1.24 | 310.00 |
| 315.00 | -1.66 | -2.62 | -2.46 | -3.63 | 2.02 | 2.66 | 3.77 | 315.00 |
| 320.00 | -1.68 | -2.68 | -1.85 | -0.27 | 3.70 | 3.61 | 3.77 | 320.00 |
| 325.00 | -1.64 | -1.67 | -1.79 | 1.35 | 3.86 | 3.61 | 3.64 | 325.00 |
| 330.00 | -1.87 | -1.30 | -0.73 | 3.66 | 3.84 | 3.47 | 4.20 | 330.00 |
| 335.00 | -1.77 | -0.63 | 0.20 | 3.25 | 4.71 | 4.85 | 3.08 | 335.00 |
| 340.00 | -1.68 | -0.44 | 1.16 | 3.42 | 5.67 | 5.91 | 3.66 | 340.00 |
| 345.00 | -1.87 | 0.15 | 1.66 | 4.65 | 5.23 | 7.21 | 3.78 | 345.00 |
| 350.00 | -1.25 | 0.74 | 1.91 | 5.16 | 4.93 | 6.91 | 4.44 | 350.00 |
| 355.00 | -1.00 | 0.20 | 1.29 | 4.27 | 3.96 | 4.46 | 4.25 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 2.69 | 0.05 | 0.36 | 14.77 | 15.18 | 15.63 | 17.98 | |

# BLADE LOADS

TEST 494 CNTR NO. 958 T.C.No. 15 C.R. 67

SPAN STATION

| DEG | 52.9 | 79.8 | 119.7 | 159.9 | 178.9 | 189.8 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -1.09 | 0.07 | 1.64 | 1.64 | 2.81 | 3.85 | 4.05 | 0.0 |
| 5.00 | -0.83 | -0.06 | 1.35 | 0.92 | 1.68 | 2.50 | 2.86 | 5.00 |
| 10.00 | -0.77 | 0.19 | 1.15 | 1.48 | 2.83 | 1.99 | 0.42 | 10.00 |
| 15.00 | -0.25 | 0.43 | 0.64 | 2.72 | 4.10 | 5.11 | 1.69 | 15.00 |
| 20.00 | 0.09 | 0.38 | 1.37 | 1.48 | 4.47 | 6.34 | 4.23 | 20.00 |
| 25.00 | 0.46 | 0.09 | 2.38 | 1.08 | 2.22 | 3.38 | 3.22 | 25.00 |
| 30.00 | 1.78 | 0.24 | 2.33 | 3.61 | 2.04 | 2.25 | 0.11 | 30.00 |
| 35.00 | 1.28 | 0.43 | 1.83 | 4.25 | 4.67 | 4.00 | 1.86 | 35.00 |
| 40.00 | 0.85 | 0.74 | 0.21 | 1.78 | 2.75 | 3.12 | 1.65 | 40.00 |
| 45.00 | 0.61 | 1.19 | 1.32 | 0.99 | 0.90 | 1.44 | -0.07 | 45.00 |
| 50.00 | 0.93 | 1.28 | 2.45 | 2.93 | 1.93 | 1.08 | -1.06 | 50.00 |
| 55.00 | 0.70 | 1.31 | 1.65 | 0.94 | -1.79 | -2.12 | -2.84 | 55.00 |
| 60.00 | 0.85 | 1.07 | 0.64 | -1.37 | -1.27 | -0.21 | -2.84 | 60.00 |
| 65.00 | 0.63 | 1.07 | 0.75 | 0.21 | -2.67 | -3.16 | -3.85 | 65.00 |
| 70.00 | 0.65 | 1.36 | 2.04 | -1.71 | -3.84 | -3.77 | -2.93 | 70.00 |
| 75.00 | 1.11 | 1.87 | 1.25 | -2.36 | -2.40 | -3.10 | -3.21 | 75.00 |
| 80.00 | 1.21 | 1.94 | 0.41 | -0.48 | -3.82 | -1.46 | -0.75 | 80.00 |
| 85.00 | 1.19 | 1.76 | 0.84 | -0.76 | -3.84 | -0.93 | 0.06 | 85.00 |
| 90.00 | 1.12 | 1.93 | 1.84 | -2.01 | -1.77 | -1.35 | 0.85 | 90.00 |
| 95.00 | 1.35 | 1.78 | 1.28 | -1.50 | -2.29 | -1.34 | 1.95 | 95.00 |
| 100.00 | 1.07 | 2.32 | 0.84 | 0.01 | -2.60 | 1.22 | 2.60 | 100.00 |
| 105.00 | 1.56 | 2.71 | 1.07 | 0.16 | -1.75 | 2.07 | 1.86 | 105.00 |
| 110.00 | 2.12 | 3.18 | 1.72 | -0.66 | -0.19 | 2.89 | 0.86 | 110.00 |
| 115.00 | 2.34 | 3.15 | 1.84 | -0.62 | 1.84 | 1.81 | -0.02 | 115.00 |
| 120.00 | 2.69 | 3.04 | 2.74 | -0.67 | 2.84 | 1.83 | -0.97 | 120.00 |
| 125.00 | 2.81 | 2.65 | 2.44 | -0.07 | 2.81 | 1.74 | -1.36 | 125.00 |
| 130.00 | 2.79 | 2.38 | 2.04 | 0.84 | 2.50 | 0.47 | -2.16 | 130.00 |
| 135.00 | 2.67 | 2.68 | 1.88 | 1.93 | 1.87 | -0.14 | -2.66 | 135.00 |
| 140.00 | 2.69 | 3.27 | 1.84 | 2.37 | 0.98 | -0.65 | -2.88 | 140.00 |
| 145.00 | 3.07 | 3.81 | 1.80 | 3.47 | 0.81 | -1.13 | -3.24 | 145.00 |
| 150.00 | 2.90 | 3.93 | 1.67 | 4.14 | 0.12 | -1.42 | -3.46 | 150.00 |
| 155.00 | 2.61 | 3.56 | 2.23 | 4.17 | -0.18 | -1.66 | -3.52 | 155.00 |
| 160.00 | 2.91 | 3.69 | 2.28 | 4.16 | -0.66 | -1.86 | -3.41 | 160.00 |
| 165.00 | 2.92 | 3.97 | 2.38 | 3.88 | -0.67 | -2.09 | -3.28 | 165.00 |
| 170.00 | 2.82 | 3.96 | 2.63 | 3.46 | -0.99 | -2.03 | -3.14 | 170.00 |
| 175.00 | 1.65 | 3.26 | 1.83 | 2.84 | -0.79 | -2.09 | -2.98 | 175.00 |
| 180.00 | 1.79 | 2.70 | 1.87 | 2.65 | -0.99 | -2.16 | -2.80 | 180.00 |
| 185.00 | 1.44 | 2.68 | 1.38 | 2.68 | -1.14 | -2.37 | -2.66 | 185.00 |
| 190.00 | 1.22 | 2.65 | 1.64 | 2.86 | -1.40 | -2.63 | -2.51 | 190.00 |
| 195.00 | 0.85 | 2.00 | 0.87 | 1.00 | -1.85 | -2.77 | -2.60 | 195.00 |
| 200.00 | 0.79 | 2.09 | 0.33 | 0.99 | -1.64 | -2.87 | -2.68 | 200.00 |
| 205.00 | 0.69 | 2.05 | 0.81 | 0.86 | -1.82 | -2.89 | -2.77 | 205.00 |
| 210.00 | -0.21 | -0.46 | -0.34 | -0.35 | -2.10 | -2.99 | -2.84 | 210.00 |
| 215.00 | -0.46 | -1.04 | -0.84 | -0.82 | -2.23 | -3.42 | -2.94 | 215.00 |
| 220.00 | -0.69 | -1.06 | -0.87 | -0.84 | -2.14 | -3.27 | -2.76 | 220.00 |
| 225.00 | -1.75 | -1.83 | -1.30 | -0.83 | -1.90 | -2.98 | -2.41 | 225.00 |
| 230.00 | -1.98 | -2.00 | -1.96 | -0.87 | -1.87 | -2.86 | -1.98 | 230.00 |
| 235.00 | -1.66 | -2.01 | -1.81 | -0.84 | -1.98 | -2.68 | -1.44 | 235.00 |
| 240.00 | -1.69 | -2.21 | -2.05 | -0.88 | -0.83 | -1.93 | -0.81 | 240.00 |
| 245.00 | -1.75 | -2.35 | -2.05 | -1.48 | -0.19 | -0.94 | -0.19 | 245.00 |
| 250.00 | -1.84 | -2.02 | -2.01 | -2.48 | 0.11 | -0.46 | 0.69 | 250.00 |
| 255.00 | -1.72 | -2.69 | -2.32 | -3.54 | 0.90 | -0.09 | 1.00 | 255.00 |
| 260.00 | -1.69 | -2.07 | -2.69 | -4.44 | 0.14 | 0.47 | 1.47 | 260.00 |
| 265.00 | -2.00 | -2.21 | -2.89 | -4.68 | -1.36 | 0.89 | 2.37 | 265.00 |
| 270.00 | -2.09 | -2.08 | -2.98 | -4.51 | -2.76 | -0.09 | 2.66 | 270.00 |
| 275.00 | -2.05 | -2.51 | -2.64 | -4.01 | -4.81 | -2.47 | 1.76 | 275.00 |
| 280.00 | -2.14 | -2.09 | -2.31 | -4.41 | -4.84 | -4.41 | -0.94 | 280.00 |
| 285.00 | -2.19 | -4.04 | -2.97 | -4.47 | -4.42 | -4.23 | -2.60 | 285.00 |
| 290.00 | -2.15 | -4.24 | -2.76 | -4.74 | -3.74 | -3.13 | -1.90 | 290.00 |
| 295.00 | -2.30 | -4.44 | -2.95 | -4.81 | -1.76 | -0.89 | 1.79 | 295.00 |
| 300.00 | -2.20 | -4.03 | -2.42 | -3.61 | -2.96 | -2.42 | -0.94 | 300.00 |
| 305.00 | -2.16 | -4.23 | -2.76 | -4.08 | -2.90 | -2.84 | -2.42 | 305.00 |
| 310.00 | -2.11 | -4.09 | -2.80 | -3.65 | -1.68 | -1.22 | -0.01 | 310.00 |
| 315.00 | -1.99 | -3.47 | -2.34 | -1.60 | 1.76 | 3.83 | 4.78 | 315.00 |
| 320.00 | -1.64 | -2.17 | -0.80 | -0.01 | 4.44 | 6.16 | 7.60 | 320.00 |
| 325.00 | -2.10 | -2.04 | -1.71 | 1.69 | 3.81 | 1.25 | 1.20 | 325.00 |
| 330.00 | -2.27 | -1.61 | -0.65 | 3.58 | 2.76 | 1.81 | 3.12 | 330.00 |
| 335.00 | -2.28 | -1.69 | -0.10 | 3.82 | 3.97 | 4.66 | 5.86 | 335.00 |
| 340.00 | -2.20 | -0.68 | 0.76 | 3.84 | 4.23 | 6.91 | 7.18 | 340.00 |
| 345.00 | -2.00 | -0.46 | 1.35 | 2.96 | 4.17 | 7.31 | 7.87 | 345.00 |
| 350.00 | -1.85 | 0.07 | 1.72 | 3.68 | 4.00 | 6.71 | 7.98 | 350.00 |
| 355.00 | -1.61 | 0.09 | 1.18 | 2.94 | 4.28 | 4.23 | 6.68 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 2.84 | 4.57 | 10.91 | 17.48 | 19.79 | 22.27 | 21.24 | |

# BLADE LOADS

TEST 505 CNTR NO. 354 T.C.No. 16 C.R. 66

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 149.3 | 178.9 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.88 | -0.65 | -0.59 | -0.84 | -0.88 | -1.44 | -1.33 | 0.0 |
| 5.00 | 0.12 | -0.13 | -0.28 | -1.17 | -0.59 | -1.16 | -1.11 | 5.00 |
| 10.00 | 0.52 | 0.16 | 0.03 | -0.69 | -0.47 | -0.73 | -0.92 | 10.00 |
| 15.00 | 0.79 | 0.28 | -0.34 | -0.63 | -0.77 | -0.63 | -0.98 | 15.00 |
| 20.00 | 0.63 | 0.34 | -0.58 | -0.71 | -1.26 | -0.81 | -1.51 | 20.00 |
| 25.00 | 0.44 | 0.18 | -0.51 | -0.64 | -1.71 | -1.63 | -2.09 | 25.00 |
| 30.00 | 0.21 | 0.10 | -0.65 | -0.73 | -1.76 | -2.00 | -2.09 | 30.00 |
| 35.00 | 0.11 | 0.37 | -0.88 | -0.93 | -1.52 | -1.86 | -1.66 | 35.00 |
| 40.00 | 0.29 | 0.53 | -0.84 | -1.02 | -1.22 | -1.37 | -1.17 | 40.00 |
| 45.00 | 0.31 | 0.38 | -0.90 | -0.97 | -1.09 | -1.28 | -1.18 | 45.00 |
| 50.00 | 0.23 | 0.07 | -0.94 | -0.87 | -1.18 | -1.34 | -1.20 | 50.00 |
| 55.00 | 0.33 | 0.01 | -0.86 | -0.74 | -1.78 | -1.43 | -1.51 | 55.00 |
| 60.00 | 0.59 | 0.02 | -0.69 | -0.58 | -1.76 | -1.33 | -1.48 | 60.00 |
| 65.00 | 0.82 | 0.07 | -0.44 | -0.38 | -1.07 | -1.03 | -1.21 | 65.00 |
| 70.00 | 0.91 | 0.19 | -0.25 | -0.15 | -0.82 | -0.64 | -0.86 | 70.00 |
| 75.00 | 0.89 | 0.35 | -0.08 | 0.04 | -0.54 | -0.28 | -0.91 | 75.00 |
| 80.00 | 0.81 | 0.52 | 0.18 | 0.24 | -0.28 | 0.26 | -0.13 | 80.00 |
| 85.00 | 0.68 | 0.67 | 0.32 | 0.42 | -0.03 | 0.63 | 0.22 | 85.00 |
| 90.00 | 0.63 | 0.82 | 0.54 | 0.58 | 0.17 | 0.91 | 0.52 | 90.00 |
| 95.00 | 0.65 | 0.94 | 0.68 | 0.67 | 0.38 | 1.12 | 0.73 | 95.00 |
| 100.00 | 0.69 | 1.02 | 0.75 | 0.70 | 0.59 | 1.26 | 0.79 | 100.00 |
| 105.00 | 0.75 | 1.05 | 0.76 | 0.70 | 0.64 | 1.31 | 0.78 | 105.00 |
| 110.00 | 0.73 | 1.02 | 0.74 | 0.69 | 0.63 | 1.26 | 0.75 | 110.00 |
| 115.00 | 0.69 | 0.98 | 0.71 | 0.66 | 0.55 | 1.11 | 0.58 | 115.00 |
| 120.00 | 0.66 | 0.87 | 0.67 | 0.60 | 0.22 | 0.89 | 0.25 | 120.00 |
| 125.00 | 0.66 | 0.79 | 0.60 | 0.49 | -0.02 | 0.58 | -0.06 | 125.00 |
| 130.00 | 0.64 | 0.75 | 0.51 | 0.35 | -0.33 | 0.24 | -0.44 | 130.00 |
| 135.00 | 0.56 | 0.76 | 0.41 | 0.20 | -0.62 | -0.16 | -0.89 | 135.00 |
| 140.00 | 0.46 | 0.77 | 0.32 | 0.11 | -0.86 | -0.54 | -1.34 | 140.00 |
| 145.00 | 0.40 | 0.73 | 0.24 | -0.03 | -1.05 | -0.93 | -1.72 | 145.00 |
| 150.00 | 0.38 | 0.67 | 0.17 | -0.19 | -1.22 | -1.30 | -2.02 | 150.00 |
| 155.00 | 0.38 | 0.59 | 0.15 | -0.35 | -1.35 | -1.69 | -2.25 | 155.00 |
| 160.00 | 0.37 | 0.55 | 0.17 | -0.46 | -1.44 | -1.89 | -2.43 | 160.00 |
| 165.00 | 0.34 | 0.59 | 0.22 | -0.48 | -1.53 | -2.04 | -2.57 | 165.00 |
| 170.00 | 0.31 | 0.68 | 0.32 | -0.41 | -1.54 | -2.11 | -2.60 | 170.00 |
| 175.00 | 0.30 | 0.76 | 0.43 | -0.28 | -1.48 | -2.11 | -2.49 | 175.00 |
| 180.00 | 0.31 | 0.75 | 0.52 | -0.16 | -1.23 | -2.01 | -2.31 | 180.00 |
| 185.00 | 0.33 | 0.73 | 0.62 | -0.04 | -1.07 | -1.85 | -2.06 | 185.00 |
| 190.00 | 0.32 | 0.73 | 0.73 | 0.09 | -0.90 | -1.61 | -1.73 | 190.00 |
| 195.00 | 0.31 | 0.75 | 0.80 | 0.24 | -0.67 | -1.30 | -1.31 | 195.00 |
| 200.00 | 0.31 | 0.75 | 0.82 | 0.38 | -0.39 | -0.94 | -0.87 | 200.00 |
| 205.00 | 0.33 | 0.67 | 0.81 | 0.45 | -0.06 | -0.53 | -0.45 | 205.00 |
| 210.00 | 0.31 | 0.53 | 0.76 | 0.52 | 0.27 | -0.13 | -0.04 | 210.00 |
| 215.00 | 0.19 | 0.37 | 0.69 | 0.51 | 0.53 | 0.25 | 0.34 | 215.00 |
| 220.00 | 0.03 | 0.25 | 0.61 | 0.45 | 0.75 | 0.60 | 0.73 | 220.00 |
| 225.00 | -0.11 | 0.13 | 0.51 | 0.39 | 0.92 | 0.88 | 1.10 | 225.00 |
| 230.00 | -0.22 | -0.01 | 0.40 | 0.34 | 1.07 | 1.14 | 1.42 | 230.00 |
| 235.00 | -0.32 | -0.10 | 0.27 | 0.31 | 1.20 | 1.37 | 1.72 | 235.00 |
| 240.00 | -0.44 | -0.35 | 0.14 | 0.29 | 1.32 | 1.56 | 1.99 | 240.00 |
| 245.00 | -0.54 | -0.50 | 0.04 | 0.27 | 1.43 | 1.78 | 2.23 | 245.00 |
| 250.00 | -0.62 | -0.62 | 0.00 | 0.22 | 1.53 | 1.84 | 2.44 | 250.00 |
| 255.00 | -0.68 | -0.71 | -0.04 | 0.19 | 1.62 | 1.97 | 2.70 | 255.00 |
| 260.00 | -0.73 | -0.78 | -0.09 | 0.17 | 1.69 | 2.07 | 2.93 | 260.00 |
| 265.00 | -0.79 | -0.83 | -0.13 | 0.17 | 1.78 | 2.15 | 3.04 | 265.00 |
| 270.00 | -0.87 | -0.86 | -0.14 | 0.18 | 1.84 | 2.17 | 3.07 | 270.00 |
| 275.00 | -0.95 | -0.87 | -0.13 | 0.20 | 1.83 | 2.13 | 2.98 | 275.00 |
| 280.00 | -0.98 | -0.89 | -0.11 | 0.24 | 1.83 | 2.01 | 2.83 | 280.00 |
| 285.00 | -0.97 | -0.93 | -0.12 | 0.28 | 1.84 | 1.81 | 2.78 | 285.00 |
| 290.00 | -1.01 | -0.98 | -0.13 | 0.32 | 1.83 | 1.68 | 2.58 | 290.00 |
| 295.00 | -1.18 | -1.03 | -0.13 | 0.34 | 1.58 | 1.58 | 2.30 | 295.00 |
| 300.00 | -1.15 | -1.06 | -0.12 | 0.33 | 1.49 | 1.51 | 2.14 | 300.00 |
| 305.00 | -1.15 | -1.13 | -0.14 | 0.30 | 1.34 | 1.39 | 1.88 | 305.00 |
| 310.00 | -1.12 | -1.13 | -0.19 | 0.26 | 1.16 | 1.19 | 1.61 | 310.00 |
| 315.00 | -1.05 | -1.13 | -0.30 | 0.22 | 1.02 | 0.97 | 1.31 | 315.00 |
| 320.00 | -0.97 | -1.00 | -0.47 | 0.17 | 0.90 | 0.72 | 1.00 | 320.00 |
| 325.00 | -0.93 | -0.86 | -0.64 | 0.09 | 0.79 | 0.48 | 0.68 | 325.00 |
| 330.00 | -0.84 | -0.67 | -0.87 | -0.04 | 0.67 | 0.23 | 0.37 | 330.00 |
| 335.00 | -0.74 | -0.34 | -1.04 | -0.28 | 0.47 | -0.03 | 0.05 | 335.00 |
| 340.00 | -0.77 | -1.22 | -0.98 | -0.24 | 0.14 | -0.42 | -0.23 | 340.00 |
| 345.00 | -0.67 | -1.63 | -0.72 | -0.18 | -0.19 | -0.72 | -0.46 | 345.00 |
| 350.00 | -0.53 | -1.79 | -0.56 | -0.24 | -0.39 | -0.86 | -0.71 | 350.00 |
| 355.00 | -0.41 | -1.31 | -0.78 | -0.48 | -0.47 | -1.93 | -1.04 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.65 | 9.87 | 7.39 | 0.11 | 5.34 | 6.65 | 5.49 | |

# BLADE LOADS

TEST 503 CNTR NO. 907 T.C.N. 17 C.R. 59

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 179.5 | 189.8 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -1.92 | -1.68 | -1.10 | -0.95 | 0.67 | 0.79 | 0.77 | 0.0 |
| 5.00 | -0.64 | -1.72 | -1.13 | -2.52 | -0.12 | 0.58 | -0.05 | 5.00 |
| 10.00 | -0.88 | -1.65 | -1.29 | -2.13 | -1.78 | -0.46 | -1.19 | 10.00 |
| 15.00 | -0.83 | -1.63 | -2.20 | -2.48 | -2.24 | -1.58 | -2.05 | 15.00 |
| 20.00 | -0.83 | -1.76 | -2.38 | -2.51 | -2.70 | -2.32 | -2.40 | 20.00 |
| 25.00 | -0.83 | -1.77 | -2.48 | -2.67 | -2.66 | -2.07 | -2.26 | 25.00 |
| 30.00 | -0.76 | -1.61 | -2.27 | -2.59 | -2.18 | -1.31 | -1.81 | 30.00 |
| 35.00 | -0.76 | -1.47 | -2.06 | -1.67 | -1.42 | -0.91 | -1.12 | 35.00 |
| 40.00 | -0.61 | -1.16 | -1.98 | -1.16 | -0.64 | 0.24 | -0.44 | 40.00 |
| 45.00 | -0.41 | -0.98 | -1.63 | -0.89 | -0.98 | 0.82 | 0.05 | 45.00 |
| 50.00 | -0.19 | -0.71 | -0.94 | -0.07 | 0.27 | 1.25 | 0.37 | 50.00 |
| 55.00 | -0.09 | -0.44 | -0.29 | 0.21 | 0.95 | 1.45 | 0.46 | 55.00 |
| 60.00 | -0.03 | -0.16 | -0.04 | 0.34 | 0.96 | 1.40 | 0.39 | 60.00 |
| 65.00 | -0.00 | 0.11 | 0.15 | 0.36 | 0.22 | 1.10 | 0.06 | 65.00 |
| 70.00 | 0.04 | 0.36 | 0.24 | 0.29 | -0.00 | 0.69 | -0.28 | 70.00 |
| 75.00 | 0.27 | 0.60 | 0.36 | 0.29 | -0.90 | 0.27 | -0.75 | 75.00 |
| 80.00 | 0.40 | 0.84 | 0.46 | 0.15 | -0.96 | -0.17 | -1.17 | 80.00 |
| 85.00 | 0.61 | 1.08 | 0.46 | 0.19 | -0.72 | -0.59 | -1.50 | 85.00 |
| 90.00 | 0.87 | 1.34 | 0.78 | 0.19 | -0.77 | -0.81 | -1.77 | 90.00 |
| 95.00 | 1.07 | 1.63 | 0.61 | 0.16 | -0.87 | -1.00 | -1.98 | 95.00 |
| 100.00 | 1.22 | 1.69 | 1.06 | 0.26 | -1.06 | -1.42 | -2.46 | 100.00 |
| 105.00 | 1.42 | 2.12 | 1.12 | 0.27 | -1.96 | -2.06 | -2.66 | 105.00 |
| 110.00 | 1.61 | 2.27 | 1.13 | 0.19 | -1.74 | -2.69 | -3.49 | 110.00 |
| 115.00 | 1.74 | 2.38 | 1.04 | -0.05 | -2.15 | -3.08 | -3.99 | 115.00 |
| 120.00 | 1.88 | 2.37 | 0.68 | -0.30 | -2.90 | -3.91 | -4.38 | 120.00 |
| 125.00 | 1.69 | 2.48 | 0.46 | -0.92 | -2.99 | -3.88 | -4.66 | 125.00 |
| 130.00 | 1.66 | 2.08 | 1.05 | -0.91 | -3.57 | -4.14 | -4.82 | 130.00 |
| 135.00 | 2.04 | 2.46 | 1.05 | -0.87 | -3.84 | -4.39 | -5.07 | 135.00 |
| 140.00 | 2.08 | 2.63 | 1.19 | -0.46 | -3.68 | -4.48 | -4.14 | 140.00 |
| 145.00 | 2.04 | 2.68 | 1.24 | -0.41 | -3.84 | -4.82 | -4.12 | 144.00 |
| 150.00 | 1.66 | 2.39 | 1.27 | -0.69 | -3.68 | -4.62 | -4.01 | 150.00 |
| 155.00 | 1.84 | 2.36 | 1.46 | -0.68 | -3.28 | -4.19 | -4.77 | 155.00 |
| 160.00 | 1.61 | 2.22 | 1.36 | -0.19 | -2.84 | -3.76 | -4.36 | 160.00 |
| 165.00 | 1.89 | 2.60 | 2.02 | 0.14 | -2.66 | -3.36 | -4.09 | 165.00 |
| 170.00 | 1.81 | 2.65 | 2.23 | 0.41 | -2.09 | -2.79 | -3.94 | 170.00 |
| 175.00 | 1.66 | 2.36 | 2.36 | 0.76 | -1.81 | -2.17 | -2.66 | 175.00 |
| 180.00 | 1.47 | 2.46 | 2.46 | 1.06 | -1.00 | -1.54 | -1.82 | 180.00 |
| 185.00 | 1.36 | 2.31 | 2.47 | 1.39 | -0.40 | -0.94 | -1.29 | 185.00 |
| 190.00 | 1.15 | 2.22 | 2.39 | 1.48 | -0.04 | -0.49 | -0.81 | 190.00 |
| 195.00 | 0.69 | 1.66 | 2.19 | 1.69 | 0.28 | -0.04 | -0.09 | 195.00 |
| 200.00 | 0.34 | 1.23 | 1.84 | 1.39 | 0.64 | 0.22 | 0.32 | 200.00 |
| 205.00 | 0.02 | 1.01 | 1.56 | 1.32 | 0.94 | 0.48 | 0.72 | 205.00 |
| 210.00 | -0.32 | 0.71 | 1.26 | 1.38 | 0.94 | 0.66 | 1.01 | 210.00 |
| 215.00 | -0.26 | 0.36 | 0.68 | 1.16 | 1.06 | 0.91 | 1.24 | 215.00 |
| 220.00 | -0.12 | 0.26 | 0.36 | 1.06 | 1.19 | 0.66 | 1.06 | 220.00 |
| 225.00 | 0.07 | -0.28 | 0.46 | 1.09 | 1.34 | 1.05 | 1.05 | 225.00 |
| 230.00 | -0.17 | -0.47 | 0.46 | 0.98 | 1.36 | 1.29 | 1.07 | 230.00 |
| 235.00 | -0.47 | -0.69 | 0.20 | 0.84 | 1.30 | 1.48 | 0.19 | 235.00 |
| 240.00 | -0.82 | -0.86 | -0.69 | 0.74 | 0.84 | 1.70 | 0.49 | 240.00 |
| 245.00 | -1.01 | -1.07 | -0.76 | 0.47 | 0.27 | 0.05 | 0.74 | 245.00 |
| 250.00 | -1.12 | -1.21 | -0.6 | 0.21 | 0.45 | 0.50 | 0.17 | 250.00 |
| 255.00 | -1.19 | -1.22 | -0.96 | 0.06 | 0.07 | 0.04 | 0.00 | 255.00 |
| 260.00 | -1.19 | -1.26 | -0.64 | 0.28 | 0.42 | 0.04 | 0.04 | 260.00 |
| 265.00 | -1.19 | -1.26 | -0.57 | 0.29 | 0.06 | 0.04 | 0.16 | 265.00 |
| 270.00 | -1.14 | -1.16 | -0.47 | 0.16 | 0.30 | 0.00 | 0.20 | 270.00 |
| 275.00 | -1.17 | -1.03 | -0.66 | 0.12 | 0.19 | 0.29 | 0.29 | 275.00 |
| 280.00 | -1.27 | -1.28 | -0.78 | 0.28 | 0.06 | 0.48 | 0.06 | 280.00 |
| 285.00 | -1.36 | -1.43 | -1.08 | 0.06 | 0.09 | 0.49 | 0.03 | 285.00 |
| 290.00 | -1.27 | -1.46 | -1.11 | 0.07 | 0.07 | 0.27 | 0.00 | 290.00 |
| 295.00 | -1.33 | -1.39 | -1.16 | 0.03 | 0.08 | 0.33 | 0.03 | 295.00 |
| 300.00 | -1.21 | -1.30 | -1.16 | 0.09 | 0.09 | 0.30 | 0.06 | 300.00 |
| 305.00 | -1.19 | -1.46 | -1.17 | 0.07 | 0.09 | 0.30 | 0.05 | 305.00 |
| 310.00 | -1.28 | -1.33 | -1.18 | 0.19 | 0.17 | 0.30 | 0.18 | 310.00 |
| 315.00 | -1.41 | -1.33 | -1.21 | 0.21 | 0.29 | 0.40 | 0.24 | 315.00 |
| 320.00 | -1.33 | -1.46 | -1.26 | 0.27 | 0.27 | 0.47 | 0.26 | 320.00 |
| 325.00 | -1.46 | -1.46 | -1.31 | 0.36 | 0.12 | 0.42 | 0.16 | 325.00 |
| 330.00 | -1.46 | -1.36 | -1.33 | 0.26 | 0.07 | 0.28 | 0.09 | 330.00 |
| 335.00 | -1.49 | -1.42 | -1.32 | 0.22 | 0.47 | 0.06 | 0.41 | 335.00 |
| 340.00 | -1.35 | -1.48 | -1.16 | 0.29 | 0.48 | 0.33 | 0.31 | 340.00 |
| 345.00 | -1.33 | -1.36 | -1.06 | 0.44 | 0.40 | 0.41 | 0.19 | 345.00 |
| 350.00 | -1.18 | -1.43 | -1.42 | 0.58 | 0.81 | 0.83 | 0.48 | 350.00 |
| 355.00 | -1.32 | -1.39 | -1.49 | 0.56 | 0.60 | 0.39 | 0.79 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.10 | 0.00 | 0.04 | 0.14 | 0.20 | 0.34 | 0.69 | |

# BLADE LOADS

TEST 502 CNTR NO. 417 T.C.N. 18 C.R. 52

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.12 | C.6S | 2.C9 | 3.0E | 2.11 | -1.04 | -2.74 | 0.0 |
| 5.00 | -0.33 | C.41 | 1.74 | 2.62 | 1.63 | -1.67 | -3.57 | 5.00 |
| 10.00 | 0.05 | C.3P | 1.61 | 2.3E | 1.28 | -2.14 | -4.13 | 10.00 |
| 15.00 | 0.42 | C.5C | 1.4P | 2.1P | 1.01 | -2.47 | -4.43 | 15.00 |
| 20.00 | 0.77 | 1.0E | 1.2S | 2.13 | 0.72 | -2.75 | -4.5P | 20.00 |
| 25.00 | 0.93 | 1.5P | 1.15 | 2.15 | 0.51 | -3.04 | -4.8S | 25.00 |
| 30.00 | 0.84 | 1.24 | 1.2P | 2.11 | 0.42 | -3.24 | -5.17 | 30.00 |
| 35.00 | 0.70 | C.7C | 1.33 | 1.9S | 0.34 | -3.38 | -5.40 | 35.00 |
| 40.00 | 0.5E | C.47 | 1.44 | 1.93 | 0.18 | -3.45 | -5.53 | 40.00 |
| 45.00 | 0.37 | C.5E | 1.5P | 2.00 | -0.02 | -3.55 | -5.6P | 45.00 |
| 50.00 | 0.28 | C.7E | 1.6C | 1.9S | -0.24 | -3.67 | -5.91 | 50.00 |
| 55.00 | 0.27 | C.7C | 1.9E | 1.71 | -0.47 | -3.74 | -5.97 | 55.00 |
| 60.00 | 0.17 | C.4S | 1.27 | 1.34 | -0.71 | -3.75 | -5.91 | 60.00 |
| 65.00 | 0.22 | C.5E | C.93 | C.94 | -1.09 | -3.86 | -5.25 | 65.00 |
| 70.00 | 0.3S | C.67 | C.65 | C.53 | -1.52 | -4.40 | -5.46 | 70.00 |
| 75.00 | 0.23 | C.6C | C.4S | C.09 | -1.94 | -5.04 | -6.50 | 75.00 |
| 80.00 | -0.06 | C.42 | C.21 | -C.43 | -2.34 | -5.59 | -7.04 | 80.00 |
| 85.00 | -0.0P | C.7P | C.C7 | -C.7S | -2.80 | -6.23 | -7.44 | 85.00 |
| 90.00 | 0.05 | C.15 | -C.17 | -C.55 | -3.11 | -7.13 | -8.12 | 90.00 |
| 95.00 | 0.15 | C.1E | -C.36 | -0.32 | -3.03 | -7.49 | -8.79 | 95.00 |
| 100.00 | 0.0S | C.CE | -C.52 | -0.7E | -3.04 | -7.90 | -9.49 | 100.00 |
| 105.0C | -0.01 | -C.CP | -C.6A | -1.43 | -2.49 | -6.57 | -2.64 | 105.00 |
| 110.00 | -0.06 | -0.23 | -C.83 | -2.02 | -2.83 | -6.57 | -2.50 | 110.00 |
| 115.00 | -0.07 | -C.3S | -C.56 | -2.06 | -3.93 | -4.12 | -1.34 | 115.00 |
| 120.00 | -0.17 | -C.42 | -1.C4 | -2.01 | -3.90 | -4.67 | 0.72 | 120.00 |
| 125.00 | -0.3C | -C.4E | -1.11 | -2.03 | -3.78 | -3.50 | 1.59 | 125.00 |
| 130.00 | -0.34 | -C.52 | -1.21 | -2.03 | -3.3E | -3.49 | 2.99 | 130.00 |
| 135.00 | -0.27 | -C.44 | -1.2P | -1.9S | -2.90 | -2.35 | 4.55 | 135.00 |
| 140.00 | -0.28 | -C.57 | -1.3P | -1.84 | -2.96 | 2.18 | 5.27 | 140.00 |
| 145.00 | -0.2P | -C.57 | -1.37 | -1.57 | -3.15 | 6.35 | 5.24 | 145.00 |
| 150.00 | -0.1P | -0.5P | -1.42 | -1.37 | -2.89 | 8.15 | 4.72 | 150.00 |
| 155.00 | -0.22 | -C.5C | -1.5E | -1.4S | -1.9P | 9.74 | 4.30 | 155.0C |
| 160.00 | -0.2P | -C.1S | -1.0P | -1.71 | -0.55 | 8.48 | 4.50 | 160.00 |
| 165.00 | -0.1S | ..12 | -1.52 | -1.47 | 0.83 | 7.48 | 5.02 | 16P.00 |
| 170.00 | -0.00 | C.31 | -1.66 | -1.42 | 0.65 | 5.96 | 4.22 | 170.00 |
| 175.00 | 0.01 | C.37 | -1.37 | -1.6C | -0.18 | 6.66 | 7.03 | 175.00 |
| 180.00 | -0.17 | C.3C | -1.1S | -1.54 | 0.58 | 9.20 | 7.47 | 180.00 |
| 185.00 | -0.2C | C.1E | -1.CE | -1.54 | 0.51 | 9.64 | 7.97 | 185.00 |
| 190.00 | -0.2C | -C.CP | -1.3A | -1.9P | -0.17 | 9.42 | 7.75 | 190.00 |
| 195.00 | -0.21 | -C.22 | -1.7S | -2.0S | 0.21 | 8.72 | 7.29 | 195.00 |
| 200.00 | -0.3S | -C.5S | -2.C7 | -2.6A | 1.50 | 8.09 | 6.33 | 200.00 |
| 205.00 | -0.5E | -C.7S | -2.2A | -3.17 | 2.08 | 7.45 | 5.7A | 205.00 |
| 210.00 | -0.6C | -C.9P | -2.2E | -3.16 | 4.12 | 7.49 | 6.04 | 210.00 |
| 215.00 | -0.54 | -1.11 | -1.9P | -2.7C | 5.18 | 8.53 | 6.5S | 215.00 |
| 220.00 | -0.42 | -1.1S | -1.72 | -2.41 | 5.47 | 8.80 | 6.94 | 220.00 |
| 225.00 | -0.4S | -1.2P | -1.7S | -1.9C | 4.14 | 8.56 | 6.62 | 225.00 |
| 230.00 | -0.4P | -1.2P | -1.7E | -1.3S | 1.4A | 8.09 | 6.63 | 230.00 |
| 235.00 | -0.6E | -1.2E | -1.6A | -1.77 | -1.16 | 7.4A | 6.16 | 235.00 |
| 240.00 | -0.64 | -1.1E | -1.5A | -2.14 | -2.50 | 0.8A | 7.09 | 240.00 |
| 245.00 | -0.9S | -1.0S | -1.2E | -1.8P | -2.2A | -0.6S | 1.70 | 245.00 |
| 250.00 | -0.91 | -1.01 | -C.8A | -1.61 | -1.69 | -1.72 | 1.05 | 250.00 |
| 255.00 | -0.47 | -C.5S | -C.5A | -1.2P | -1.16 | -2.43 | 1.58 | 255.00 |
| 260.00 | -0.3S | -C.02 | -C.5E | -0.92 | -0.7S | -2.71 | 0.82 | 260.00 |
| 265.00 | -0.2A | -C.72 | -C.5E | -C.6A | -0.63 | -2.56 | -0.12 | 265.00 |
| 270.00 | -0.1S | -C.62 | -C.3S | -C.1A | -0.04 | -2.13 | -0.33 | 270.00 |
| 275.00 | -0.13 | -C.4P | -C.2A | -0.02 | 0.34 | -1.75 | -0.38 | 275.00 |
| 280.00 | -0.17 | -C.2S | -C.CA | 0.1S | 0.48 | -1.75 | -0.59 | 280.00 |
| 285.00 | -0.1P | -C.1C | C.23 | 0.3S | 0.51 | -1.64 | -0.81 | 285.00 |
| 290.00 | -0.1A | -C.CC | C.53 | C.5P | 0.68 | -1.32 | -0.35 | 290.00 |
| 295.00 | -0.12 | C.CA | C.4A | C.82 | 0.9A | -0.91 | 0.49 | 295.00 |
| 300.00 | -0.07 | C.CS | 1.3A | 1.17 | 1.47 | -0.40 | 0.97 | 300.00 |
| 305.00 | 0.01 | C.1E | 1.57 | 1.61 | 1.61 | -0.0A | -0.05 | 305.00 |
| 310.00 | 0.0P | C.2S | 1.67 | 2.0E | 1.85 | -0.65 | -0.65 | 310.00 |
| 315.00 | 0.17 | C.3A | 1.6A | 2.3S | 2.09 | -0.40 | -0.97 | 315.00 |
| 320.00 | 0.2E | C.4A | 1.7S | 2.6C | 2.32 | -0.36 | -0.9E | 320.00 |
| 325.00 | 0.3A | C.5A | 1.67 | 2.87 | 2.46 | -0.31 | -1.04 | 325.00 |
| 330.00 | 0.42 | C.6A | 2.C2 | 3.C2 | 2.53 | -0.25 | -1.09 | 330.00 |
| 335.00 | 0.47 | C.7E | 2.1S | 3.1S | 2.60 | -0.10 | -1.07 | 335.00 |
| 340.00 | 0.5E | C.91 | 2.32 | 3.27 | 2.81 | 0.07 | -0.96 | 340.00 |
| 345.00 | 0.75 | 1.11 | 2.4A | 3.4E | 3.01 | 0.23 | -0.8A | 345.00 |
| 350.00 | 0.9P | 1.1P | 2.4P | 3.61 | 3.11 | 0.16 | -1.07 | 350.00 |
| 355.00 | 0.97 | C.91 | 2.3A | 3.4S | 2.80 | -0.33 | -1.69 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.00 | 3.7A | 5.62 | 8.3C | 11.24 | 15.19 | 16.0A | |

# BLADE LOADS

TEST 503 CNTR NO. 391 T.C.N. 19 C.R. 60

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.9 | 178.5 | 189.0 | 199.+ | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.43 | 1.05 | 2.24 | 3.25 | 2.56 | -0.18 | -3.77 | 0.0 |
| 5.00 | 0.38 | 0.95 | 2.02 | 3.05 | 2.20 | -0.60 | -4.17 | 5.00 |
| 10.00 | 0.38 | 0.89 | 1.84 | 2.83 | 2.04 | -0.68 | -4.57 | 10.00 |
| 15.00 | 0.55 | 0.66 | 1.71 | 2.69 | 1.69 | -1.38 | -4.99 | 15.00 |
| 20.00 | 0.69 | 0.32 | 1.63 | 2.60 | 1.34 | -1.51 | -5.39 | 20.00 |
| 25.00 | 0.74 | 0.30 | 1.61 | 2.54 | 1.12 | -1.84 | -5.73 | 25.00 |
| 30.00 | 0.67 | 0.32 | 1.61 | 2.48 | 0.90 | -2.02 | -5.96 | 30.00 |
| 35.00 | 0.45 | 0.32 | 1.65 | 2.38 | 0.87 | -2.09 | -5.91 | 35.00 |
| 40.00 | 0.24 | 0.34 | 1.62 | 2.24 | 0.73 | -2.16 | -5.61 | 40.00 |
| 45.00 | 0.33 | 0.43 | 1.59 | 2.11 | 0.56 | -2.26 | -5.59 | 45.00 |
| 50.00 | 0.38 | 0.55 | 1.52 | 1.99 | 0.36 | -2.39 | -6.02 | 50.00 |
| 55.00 | 0.24 | 0.63 | 1.36 | 1.83 | 0.14 | -2.59 | -6.28 | 55.00 |
| 60.00 | 0.10 | 0.67 | 1.16 | 1.52 | -0.19 | -2.85 | -5.99 | 60.00 |
| 65.00 | 0.11 | 0.63 | 0.94 | 1.18 | -0.62 | -3.13 | -5.38 | 65.00 |
| 70.00 | 0.17 | 0.54 | 0.73 | 0.83 | -0.98 | -3.39 | -4.76 | 70.00 |
| 75.00 | 0.09 | 0.43 | 0.51 | 0.06 | -1.44 | -3.70 | -4.04 | 75.00 |
| 80.00 | 0.01 | 0.33 | 0.25 | -0.39 | -2.11 | -4.16 | -4.33 | 80.00 |
| 85.00 | -0.08 | 0.24 | -0.05 | -0.84 | -2.78 | -4.82 | -5.29 | 85.00 |
| 90.00 | -0.17 | 0.16 | -0.32 | -1.21 | -3.39 | -5.52 | -6.05 | 90.00 |
| 95.00 | -0.22 | 0.05 | -0.52 | -1.51 | -3.87 | -6.23 | -6.25 | 95.00 |
| 100.00 | -0.15 | -0.07 | -0.68 | -1.72 | -4.18 | -6.60 | -5.47 | 100.00 |
| 105.00 | -0.15 | -0.20 | -0.83 | -1.80 | -4.24 | -5.44 | 1.46 | 105.00 |
| 110.00 | -0.20 | -0.31 | -1.01 | -1.73 | -4.06 | -5.50 | 1.68 | 110.00 |
| 115.00 | -0.26 | -0.43 | -1.18 | -1.68 | -3.72 | -1.55 | 2.21 | 115.00 |
| 120.00 | -0.35 | -0.51 | -1.33 | -1.65 | -2.75 | 0.21 | 3.36 | 120.00 |
| 125.00 | -0.43 | -0.58 | -1.42 | -2.14 | -1.28 | 1.55 | 4.36 | 125.00 |
| 130.00 | -0.48 | -0.65 | -1.47 | -2.15 | -0.88 | 0.38 | 4.87 | 130.00 |
| 135.00 | -0.45 | -0.72 | -1.50 | -1.84 | -0.78 | -0.79 | 4.96 | 135.00 |
| 140.00 | -0.38 | -0.76 | -1.48 | -1.62 | -0.84 | -0.32 | 4.94 | 140.00 |
| 145.00 | -0.29 | -0.72 | -1.45 | -1.59 | -0.76 | 0.94 | 4.93 | 145.00 |
| 150.00 | -0.23 | -0.62 | -1.48 | -1.62 | -0.49 | 2.30 | 4.96 | 150.00 |
| 155.00 | -0.15 | -0.46 | -1.54 | -1.65 | 0.17 | 3.12 | 4.96 | 155.00 |
| 160.00 | -0.01 | -0.28 | -1.26 | -1.62 | 1.32 | 3.91 | 4.78 | 160.00 |
| 165.00 | 0.14 | -0.13 | -1.17 | -1.60 | 2.60 | 3.79 | 4.49 | 165.00 |
| 170.00 | 0.27 | 0.01 | -1.08 | -1.58 | 3.89 | 4.56 | 4.29 | 170.00 |
| 175.00 | 0.31 | 0.12 | -1.00 | -1.91 | 3.81 | 5.00 | 4.42 | 175.00 |
| 180.00 | 0.27 | 0.20 | -0.99 | -1.35 | 4.31 | 4.92 | 4.74 | 180.00 |
| 185.00 | 0.23 | 0.19 | -1.04 | -1.22 | 4.61 | 4.80 | 5.03 | 185.00 |
| 190.00 | 0.22 | 0.06 | -1.11 | -1.23 | 3.81 | 5.20 | 5.30 | 190.00 |
| 195.00 | 0.20 | -0.15 | -1.20 | -1.34 | 1.68 | 6.17 | 5.45 | 195.00 |
| 200.00 | 0.13 | -0.34 | -1.28 | -1.43 | -0.30 | 6.80 | 5.26 | 200.00 |
| 205.00 | -0.02 | -0.48 | -1.35 | -1.39 | -1.31 | 6.88 | 4.83 | 205.00 |
| 210.00 | -0.17 | -0.60 | -1.40 | -1.36 | -1.75 | 6.62 | 4.29 | 210.00 |
| 215.00 | -0.28 | -0.72 | -1.45 | -1.41 | -2.06 | 6.56 | 3.69 | 215.00 |
| 220.00 | -0.34 | -0.84 | -1.52 | -1.53 | -2.11 | 6.01 | 3.03 | 220.00 |
| 225.00 | -0.39 | -0.95 | -1.59 | -1.67 | -1.94 | 5.34 | 2.55 | 225.00 |
| 230.00 | -0.43 | -1.02 | -1.62 | -1.93 | -1.81 | 4.96 | 2.73 | 230.00 |
| 235.00 | -0.49 | -1.06 | -1.64 | -1.98 | -1.94 | 3.49 | 3.42 | 235.00 |
| 240.00 | -0.52 | -1.05 | -1.65 | -2.05 | -2.18 | 0.23 | 4.32 | 240.00 |
| 245.00 | -0.50 | -1.01 | -1.65 | -2.05 | -2.39 | -2.89 | 4.81 | 245.00 |
| 250.00 | -0.44 | -0.93 | -1.65 | -2.22 | -2.15 | -3.99 | 4.68 | 250.00 |
| 255.00 | -0.39 | -0.73 | -1.57 | -2.28 | -1.94 | -2.97 | 4.71 | 255.00 |
| 260.00 | -0.34 | -0.59 | -1.39 | -1.77 | -1.25 | 0.21 | 4.60 | 260.00 |
| 265.00 | -0.30 | -0.63 | -1.12 | -1.04 | -1.18 | 1.23 | 3.76 | 265.00 |
| 270.00 | -0.26 | -0.62 | -0.84 | -0.75 | -1.22 | -0.69 | 2.58 | 270.00 |
| 275.00 | -0.23 | -0.45 | -0.62 | -1.15 | -1.18 | -2.16 | 1.63 | 275.00 |
| 280.00 | -0.20 | -0.28 | -0.45 | -1.24 | -1.02 | -2.72 | -0.19 | 280.00 |
| 285.00 | -0.19 | -0.04 | -0.30 | -0.89 | -0.67 | -2.30 | -0.59 | 285.00 |
| 290.00 | -0.17 | 0.08 | -0.00 | -0.47 | -0.18 | -1.87 | -1.27 | 290.00 |
| 295.00 | -0.17 | 0.18 | 0.42 | -0.05 | 0.29 | -1.66 | -1.37 | 295.00 |
| 300.00 | -0.16 | 0.23 | 0.90 | 0.61 | 0.61 | -1.55 | -1.17 | 300.00 |
| 305.00 | -0.15 | 0.23 | 1.38 | 1.37 | 0.93 | -1.25 | -2.14 | 305.00 |
| 310.00 | -0.11 | 0.26 | 1.74 | 2.07 | 1.32 | -0.62 | -1.35 | 310.00 |
| 315.00 | -0.03 | 0.36 | 1.97 | 2.49 | 1.79 | -0.25 | -1.92 | 315.00 |
| 320.00 | 0.08 | 0.52 | 1.90 | 2.69 | 2.21 | -0.11 | -2.29 | 320.00 |
| 325.00 | 0.20 | 0.70 | 1.65 | 2.82 | 2.48 | 0.02 | -2.73 | 325.00 |
| 330.00 | 0.28 | 0.84 | 2.00 | 3.02 | 2.64 | 0.12 | -2.89 | 330.00 |
| 335.00 | 0.34 | 0.95 | 2.14 | 3.31 | 2.75 | 0.18 | -2.87 | 335.00 |
| 340.00 | 0.38 | 1.05 | 2.32 | 3.46 | 2.83 | 0.33 | -2.87 | 340.00 |
| 345.00 | 0.41 | 1.12 | 2.49 | 3.47 | 2.88 | 0.36 | -2.91 | 345.00 |
| 350.00 | 0.44 | 1.18 | 2.55 | 3.44 | 2.93 | 0.33 | -3.07 | 350.00 |
| 355.00 | 0.44 | 1.15 | 2.48 | 3.37 | 2.86 | 0.12 | -3.38 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.09 | 2.90 | 5.30 | 8.34 | 10.97 | 14.66 | 17.64 | |

# BLADE LOADS

TEST 497 CNTR NO. 494 T.C.N. 20 C.R. 29

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 159.9 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.51 | 1.87 | 2.45 | 3.38 | 2.55 | -0.12 | -3.17 | 0.0 |
| 5.00 | 0.55 | 1.21 | 2.65 | 3.14 | 2.37 | -0.78 | -3.94 | 5.00 |
| 10.00 | 0.50 | 1.25 | 2.50 | 2.88 | 2.05 | -1.25 | -4.49 | 10.00 |
| 15.00 | 0.42 | 1.09 | 2.27 | 2.71 | 1.74 | -1.62 | -4.88 | 15.00 |
| 20.00 | 0.34 | 0.88 | 2.11 | 2.67 | 1.44 | -2.03 | -5.14 | 20.00 |
| 25.00 | 0.29 | 0.72 | 2.07 | 2.69 | 1.23 | -2.23 | -5.23 | 25.00 |
| 30.00 | 0.40 | 0.63 | 2.02 | 2.75 | 1.12 | -2.23 | -5.21 | 30.00 |
| 35.00 | 0.56 | 0.62 | 1.95 | 2.71 | 1.11 | -2.17 | -5.13 | 35.00 |
| 40.00 | 0.65 | 0.67 | 1.83 | 2.65 | 1.16 | -2.17 | -5.04 | 40.00 |
| 45.00 | 0.25 | 0.71 | 1.61 | 2.43 | 1.04 | -2.14 | -4.93 | 45.00 |
| 50.00 | 0.18 | 0.71 | 1.36 | 2.10 | 0.84 | -2.15 | -4.86 | 50.00 |
| 55.00 | 0.29 | 0.67 | 1.09 | 1.68 | 0.48 | -2.34 | -4.94 | 55.00 |
| 60.00 | 0.44 | 0.55 | 0.80 | 1.11 | -0.08 | -2.85 | -5.30 | 60.00 |
| 65.00 | 0.51 | 0.42 | 0.50 | 0.43 | -0.71 | -3.55 | -5.78 | 65.00 |
| 70.00 | 0.48 | 0.31 | 0.18 | -0.20 | -1.36 | -4.33 | -6.27 | 70.00 |
| 75.00 | 0.35 | 0.22 | -0.18 | -0.99 | -2.11 | -5.22 | -6.86 | 75.00 |
| 80.00 | 0.25 | 0.15 | -0.54 | -1.66 | -2.89 | -6.26 | -5.65 | 80.00 |
| 85.00 | 0.22 | 0.19 | -0.86 | -2.33 | -3.64 | -7.25 | -4.15 | 85.00 |
| 90.00 | 0.16 | 0.04 | -1.10 | -2.44 | -4.34 | -7.84 | -2.72 | 90.00 |
| 95.00 | 0.07 | -0.36 | -1.20 | -2.82 | -4.68 | -8.21 | -1.49 | 95.00 |
| 100.00 | -0.01 | -0.17 | -1.22 | -2.77 | -4.88 | -8.29 | -0.32 | 100.00 |
| 105.00 | -0.02 | -0.25 | -1.23 | -2.24 | -4.22 | -6.85 | 1.06 | 105.00 |
| 110.00 | -0.31 | -0.31 | -1.22 | -1.75 | -3.45 | -4.17 | 2.20 | 110.00 |
| 115.00 | 0.32 | -0.32 | -1.22 | -1.45 | -2.76 | -2.31 | 2.17 | 115.00 |
| 120.00 | 0.04 | -0.30 | -1.25 | -1.36 | -2.44 | -2.68 | 2.06 | 120.00 |
| 125.00 | 0.06 | -0.25 | -1.27 | -1.38 | -2.38 | -1.18 | 1.33 | 125.00 |
| 130.00 | 0.06 | -0.25 | -1.28 | -1.44 | -2.38 | 1.55 | 0.66 | 130.00 |
| 135.00 | 0.04 | -0.31 | -1.26 | -1.53 | -2.07 | 3.82 | 1.01 | 135.00 |
| 140.00 | 0.02 | -0.34 | -1.23 | -1.62 | -1.65 | 4.39 | 1.38 | 140.00 |
| 145.00 | -0.01 | -0.34 | -1.17 | -1.60 | -1.19 | 4.13 | 1.54 | 145.00 |
| 150.00 | -0.02 | -0.26 | -1.07 | -1.50 | -0.91 | 3.92 | 1.54 | 150.00 |
| 155.00 | 0.05 | -0.15 | -0.96 | -1.39 | -0.78 | 4.00 | 1.51 | 155.00 |
| 160.00 | 0.22 | -0.06 | -0.96 | -1.24 | -0.79 | 4.28 | 1.60 | 160.00 |
| 165.00 | 0.41 | 0.04 | -0.83 | -1.17 | -0.93 | 4.69 | 1.91 | 165.00 |
| 170.00 | 0.51 | 0.16 | -0.83 | -1.13 | -0.30 | 5.09 | 2.43 | 170.00 |
| 175.00 | 0.50 | 0.26 | -0.86 | -1.09 | -0.06 | 5.53 | 3.01 | 175.00 |
| 180.00 | 0.45 | 0.32 | -0.92 | -1.06 | 0.13 | 6.03 | 3.50 | 180.00 |
| 185.00 | 0.38 | 0.24 | -1.00 | -1.03 | 0.18 | 6.35 | 3.74 | 185.00 |
| 190.00 | 0.33 | 0.09 | -1.09 | -1.02 | -0.01 | 6.32 | 3.52 | 190.00 |
| 195.00 | 0.23 | -0.12 | -1.17 | -1.03 | -0.29 | 6.16 | 3.23 | 195.00 |
| 200.00 | 0.06 | -0.33 | -1.24 | -1.11 | -0.52 | 5.98 | 3.13 | 200.00 |
| 205.00 | -0.15 | -0.47 | -1.31 | -1.31 | -0.56 | 5.63 | 3.26 | 205.00 |
| 210.00 | -0.33 | -0.49 | -1.35 | -1.69 | -0.72 | 4.99 | 3.69 | 210.00 |
| 215.00 | -0.47 | -0.44 | -1.36 | -2.00 | -0.83 | 4.24 | 4.32 | 215.00 |
| 220.00 | -0.56 | -0.26 | -1.35 | -1.98 | -1.07 | 3.62 | 4.92 | 220.00 |
| 225.00 | -0.62 | -0.06 | -1.33 | -1.93 | -1.26 | 3.23 | 4.21 | 225.00 |
| 230.00 | -0.66 | -0.10 | -1.29 | -2.03 | -1.24 | 2.35 | 4.43 | 230.00 |
| 235.00 | -0.68 | -0.09 | -1.24 | -2.15 | -0.58 | 1.23 | 4.82 | 235.00 |
| 240.00 | -0.69 | -0.14 | -1.19 | -2.20 | -0.18 | 0.35 | 5.16 | 240.00 |
| 245.00 | -0.68 | -0.09 | -1.13 | -2.19 | -0.43 | -0.17 | 4.56 | 245.00 |
| 250.00 | -0.66 | -0.02 | -1.07 | -2.12 | -0.71 | -0.97 | 5.67 | 250.00 |
| 255.00 | -0.63 | -0.05 | -1.01 | -1.96 | -0.72 | -1.95 | 3.34 | 255.00 |
| 260.00 | -0.60 | -0.04 | -0.96 | -1.75 | -0.81 | -2.17 | 5.48 | 260.00 |
| 265.00 | -0.56 | -0.09 | -0.88 | -1.44 | -0.95 | -2.53 | 6.99 | 265.00 |
| 270.00 | -0.53 | -0.04 | -0.79 | -1.24 | -0.84 | -1.76 | 5.21 | 270.00 |
| 275.00 | -0.51 | -0.59 | -0.71 | -0.95 | -0.10 | -1.04 | 2.67 | 275.00 |
| 280.00 | -0.48 | -0.51 | -0.60 | -0.58 | 0.34 | -1.02 | 0.75 | 280.00 |
| 285.00 | -0.47 | -0.44 | -0.44 | -0.24 | 0.69 | -1.22 | -0.29 | 285.00 |
| 290.00 | -0.45 | -0.44 | -0.24 | 0.02 | 1.08 | -1.16 | -0.59 | 290.00 |
| 295.00 | -0.46 | -0.45 | 0.05 | 0.39 | 1.50 | -0.83 | -0.46 | 295.00 |
| 300.00 | -0.45 | -0.41 | 0.38 | 0.96 | 1.92 | -0.48 | -0.00 | 300.00 |
| 305.00 | -0.43 | -0.29 | 0.74 | 1.58 | 2.31 | -0.04 | -0.02 | 305.00 |
| 310.00 | -0.38 | -0.12 | 1.10 | 2.13 | 2.66 | 0.11 | -1.03 | 310.00 |
| 315.00 | -0.29 | 0.09 | 1.45 | 2.47 | 3.00 | 0.24 | -1.83 | 315.00 |
| 320.00 | -0.18 | 0.27 | 1.74 | 2.83 | 3.33 | 0.55 | -1.83 | 320.00 |
| 325.00 | -0.06 | 0.44 | 1.96 | 3.08 | 3.65 | 0.93 | -1.50 | 325.00 |
| 330.00 | 0.05 | 0.60 | 2.05 | 3.32 | 3.93 | 1.24 | -1.16 | 330.00 |
| 335.00 | 0.14 | 0.72 | 2.11 | 3.48 | 4.13 | 1.48 | -1.04 | 335.00 |
| 340.00 | 0.21 | 0.86 | 2.13 | 3.57 | 4.21 | 1.54 | -1.04 | 340.00 |
| 345.00 | 0.27 | 0.99 | 2.12 | 3.52 | 4.11 | 1.42 | -1.18 | 345.00 |
| 350.00 | 0.33 | 1.08 | 2.16 | 3.63 | 3.89 | 1.23 | -1.55 | 350.00 |
| 355.00 | 0.41 | 1.37 | 2.29 | 3.55 | 3.48 | 0.52 | -2.24 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.28 | 2.99 | 4.30 | 7.33 | 9.31 | 14.52 | 15.89 | |

# BLADE LOADS

TEST 498 CNTR NO. 496 T.C.No. 21 C.R. 36

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -0.03 | 0.35 | 0.82 | 1.41 | 1.61 | 1.18 | 0.91 | 0.0 |
| 5.00 | 0.17 | 0.05 | 1.03 | 0.90 | 0.43 | 0.39 | 0.06 | 5.00 |
| 10.00 | 0.40 | -0.18 | 1.22 | 0.60 | -0.17 | -0.54 | -0.85 | 10.00 |
| 15.00 | 0.58 | 0.13 | 0.89 | 0.37 | -0.41 | -1.27 | -1.46 | 15.00 |
| 20.00 | 0.62 | 0.44 | 0.34 | -0.07 | -0.95 | -1.82 | -1.95 | 20.00 |
| 25.00 | 0.42 | 0.54 | -0.01 | -0.46 | -1.71 | -2.13 | -2.43 | 25.00 |
| 30.00 | 0.15 | 0.56 | -0.18 | -0.66 | -1.83 | -2.13 | -2.69 | 30.00 |
| 35.00 | 0.09 | 0.27 | -0.25 | -0.70 | -1.73 | -2.00 | -2.69 | 35.00 |
| 40.00 | 0.16 | -0.19 | -0.22 | -0.66 | -1.74 | -2.01 | -2.58 | 40.00 |
| 45.00 | 0.13 | -0.25 | -0.12 | -0.69 | -1.75 | -2.06 | -2.47 | 45.00 |
| 50.00 | -0.15 | -0.04 | -0.08 | -0.54 | -1.76 | -2.05 | -2.46 | 50.00 |
| 55.00 | -0.13 | -0.06 | -0.11 | -0.53 | -1.71 | -2.01 | -2.42 | 55.00 |
| 60.00 | 0.16 | -0.19 | -0.20 | -0.55 | -1.69 | -1.91 | -2.25 | 60.00 |
| 65.00 | 0.26 | -0.17 | -0.29 | -0.66 | -1.71 | -1.84 | -1.99 | 65.00 |
| 70.00 | 0.22 | -0.07 | -0.30 | -0.87 | -1.79 | -1.85 | -1.82 | 70.00 |
| 75.00 | 0.13 | 0.03 | -0.48 | -1.11 | -1.89 | -1.86 | -1.95 | 75.00 |
| 80.00 | 0.13 | 0.08 | -0.46 | -1.31 | -1.98 | -1.95 | -2.11 | 80.00 |
| 85.00 | 0.22 | 0.15 | -0.44 | -1.39 | -2.01 | -1.92 | -1.99 | 85.00 |
| 90.00 | 0.27 | 0.25 | -0.30 | -1.39 | -1.88 | -1.46 | -1.64 | 90.00 |
| 95.00 | 0.30 | 0.39 | -0.62 | -1.26 | -1.59 | -0.83 | -1.14 | 95.00 |
| 100.00 | 0.33 | 0.49 | -0.49 | -0.99 | -1.17 | -0.36 | -0.54 | 100.00 |
| 105.00 | 0.40 | 0.54 | -0.35 | -0.64 | -0.76 | -0.05 | 0.07 | 105.00 |
| 110.00 | 0.47 | 0.62 | -0.17 | -0.36 | -0.46 | 0.29 | 0.58 | 110.00 |
| 115.00 | 0.51 | 0.73 | 0.05 | -0.08 | -0.35 | 0.62 | 0.72 | 115.00 |
| 120.00 | 0.53 | 0.85 | 0.25 | 0.09 | -0.32 | 0.85 | 0.56 | 120.00 |
| 125.00 | 0.54 | 0.97 | 0.32 | 0.16 | -0.32 | 0.86 | 0.22 | 125.00 |
| 130.00 | 0.54 | 1.04 | 0.32 | 0.14 | -0.34 | 0.65 | -0.18 | 130.00 |
| 135.00 | 0.52 | 1.06 | 0.31 | 0.08 | -0.38 | 0.28 | -0.67 | 135.00 |
| 140.00 | 0.50 | 1.04 | 0.33 | 0.03 | -0.44 | -0.14 | -1.16 | 140.00 |
| 145.00 | 0.49 | 1.04 | 0.36 | -0.01 | -0.51 | -0.57 | -1.61 | 145.00 |
| 150.00 | 0.50 | 1.11 | 0.44 | -0.02 | -0.56 | -0.92 | -1.96 | 150.00 |
| 155.00 | 0.56 | 1.21 | 0.56 | 0.02 | -0.59 | -1.17 | -2.19 | 155.00 |
| 160.00 | 0.64 | 1.29 | 0.72 | 0.12 | -0.58 | -1.30 | -2.27 | 160.00 |
| 165.00 | 0.72 | 1.34 | 0.87 | 0.33 | -0.52 | -1.29 | -2.21 | 165.00 |
| 170.00 | 0.77 | 1.43 | 1.00 | 0.53 | -0.37 | -1.15 | -1.97 | 170.00 |
| 175.00 | 0.80 | 1.51 | 1.12 | 0.80 | -0.12 | -0.89 | -1.56 | 175.00 |
| 180.00 | 0.81 | 1.52 | 1.20 | 1.06 | 0.20 | -0.54 | -1.07 | 180.00 |
| 185.00 | 0.82 | 1.44 | 1.19 | 1.22 | 0.56 | -0.15 | -0.54 | 185.00 |
| 190.00 | 0.78 | 1.36 | 1.14 | 1.29 | 0.87 | 0.24 | -0.07 | 190.00 |
| 195.00 | 0.74 | 1.17 | 1.06 | 1.29 | 1.13 | 0.63 | 0.33 | 195.00 |
| 200.00 | 0.66 | 0.94 | 0.94 | 1.24 | 1.31 | 0.90 | 0.59 | 200.00 |
| 205.00 | 0.56 | 0.74 | 0.80 | 1.22 | 1.45 | 1.00 | 0.75 | 205.00 |
| 210.00 | 0.42 | 0.51 | 0.69 | 1.15 | 1.55 | 1.05 | 0.86 | 210.00 |
| 215.00 | 0.26 | 0.28 | 0.59 | 1.02 | 1.62 | 1.07 | 0.97 | 215.00 |
| 220.00 | 0.04 | 0.04 | 0.39 | 0.86 | 1.68 | 1.12 | 1.11 | 220.00 |
| 225.00 | -0.15 | -0.15 | 0.28 | 0.67 | 1.72 | 1.20 | 1.27 | 225.00 |
| 230.00 | -0.29 | -0.33 | 0.17 | 0.49 | 1.75 | 1.36 | 1.47 | 230.00 |
| 235.00 | -0.37 | -0.48 | 0.05 | 0.33 | 1.78 | 1.56 | 1.70 | 235.00 |
| 240.00 | -0.41 | -0.63 | -0.09 | 0.19 | 1.79 | 1.85 | 1.96 | 240.00 |
| 245.00 | -0.45 | -0.77 | -0.30 | 0.09 | 1.74 | 2.20 | 2.28 | 245.00 |
| 250.00 | -0.49 | -0.89 | -0.52 | -0.01 | 1.62 | 2.47 | 2.68 | 250.00 |
| 255.00 | -0.65 | -0.99 | -0.71 | -0.12 | 1.47 | 2.60 | 3.14 | 255.00 |
| 260.00 | -0.73 | -1.08 | -0.89 | -0.32 | 1.30 | 2.41 | 3.66 | 260.00 |
| 265.00 | -0.79 | -1.17 | -1.02 | -0.11 | 1.16 | 2.03 | 3.90 | 265.00 |
| 270.00 | -0.74 | -1.26 | -1.11 | -0.36 | 1.08 | 1.66 | 3.66 | 270.00 |
| 275.00 | -0.82 | -1.34 | -1.15 | -0.71 | 0.99 | 1.28 | 3.14 | 275.00 |
| 280.00 | -0.93 | -1.41 | -1.19 | -0.87 | 0.83 | 0.98 | 2.67 | 280.00 |
| 285.00 | -0.96 | -1.49 | -1.23 | -0.89 | 0.56 | 0.74 | 2.37 | 285.00 |
| 290.00 | -0.95 | -1.53 | -1.25 | -1.03 | 0.38 | 0.59 | 2.25 | 290.00 |
| 295.00 | -0.94 | -1.55 | -1.21 | -1.07 | 0.43 | 0.62 | 2.16 | 295.00 |
| 300.00 | -0.96 | -1.55 | -1.15 | -0.84 | 0.58 | 0.77 | 2.05 | 300.00 |
| 305.00 | -0.99 | -1.52 | -1.04 | -0.71 | 0.35 | 0.52 | 1.24 | 305.00 |
| 310.00 | -0.97 | -1.47 | -1.04 | -0.46 | -0.23 | -0.55 | -0.22 | 310.00 |
| 315.00 | -0.96 | -1.39 | -0.93 | -0.75 | -0.10 | -0.10 | 0.58 | 315.00 |
| 320.00 | -0.83 | -1.28 | -0.71 | -0.37 | 0.20 | -0.20 | -0.19 | 320.00 |
| 325.00 | -0.81 | -1.13 | -0.44 | -0.03 | -0.05 | -0.53 | -0.01 | 325.00 |
| 330.00 | -0.77 | -0.96 | -0.14 | 0.14 | -0.03 | 0.33 | 1.15 | 330.00 |
| 335.00 | -0.69 | -0.83 | 0.14 | 0.20 | 0.54 | 1.08 | 1.13 | 335.00 |
| 340.00 | -0.55 | -0.63 | 0.39 | 0.03 | 1.05 | 0.99 | 0.81 | 340.00 |
| 345.00 | -0.41 | -0.42 | 0.56 | 1.24 | 1.13 | 0.84 | 0.53 | 345.00 |
| 350.00 | -0.31 | -0.21 | 0.69 | 1.71 | 1.37 | 1.05 | 0.92 | 350.00 |
| 355.00 | -0.23 | 0.01 | 0.80 | 1.91 | 1.41 | 1.20 | 1.17 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.77 | 4.69 | 6.84 | 8.35 | 8.66 | 9.39 | 7.90 | |

# BLADE LOADS

TEST 502 CNTR NO. 383 T.C.No. 22 C.R. 51

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | 0.95 | 1.65 | 2.62 | 3.88 | 4.45 | 5.11 | 3.61 | 0.0 |
| 5.00 | 1.08 | 1.91 | 2.85 | 3.78 | 4.28 | 4.62 | 2.73 | 5.00 |
| 10.00 | 1.13 | 2.00 | 2.90 | 3.85 | 3.80 | 3.59 | 1.64 | 10.00 |
| 15.00 | 1.05 | 2.07 | 2.76 | 3.33 | 3.13 | 2.50 | 0.30 | 15.00 |
| 20.00 | 1.18 | 2.21 | 2.80 | 2.95 | 2.21 | 1.28 | -1.04 | 20.00 |
| 25.00 | 1.35 | 2.40 | 2.65 | 2.65 | 1.23 | 0.07 | -2.22 | 25.00 |
| 30.00 | 1.43 | 2.59 | 2.61 | 1.91 | 0.33 | -0.99 | -2.84 | 30.00 |
| 35.00 | 1.37 | 2.45 | 2.01 | 1.71 | -0.33 | -1.65 | -3.15 | 35.00 |
| 40.00 | 1.20 | 2.17 | 2.47 | 1.71 | -0.66 | -1.95 | -3.20 | 40.00 |
| 45.00 | 0.95 | 1.81 | 2.20 | 1.56 | -0.76 | -1.99 | -3.22 | 45.00 |
| 50.00 | 0.71 | 1.65 | 2.41 | 1.24 | -0.81 | -2.09 | -3.56 | 50.00 |
| 55.00 | 0.60 | 1.75 | 2.19 | 1.12 | -1.05 | -2.51 | -4.43 | 55.00 |
| 60.00 | 0.65 | 1.75 | 1.82 | 1.06 | -1.54 | -3.48 | -6.03 | 60.00 |
| 65.00 | 0.52 | 1.57 | 1.34 | 0.65 | -2.46 | -5.01 | -8.16 | 65.00 |
| 70.00 | 0.28 | 1.25 | 0.67 | 0.01 | -3.68 | -6.99 | -10.27 | 70.00 |
| 75.00 | 0.14 | 1.24 | 0.61 | -0.72 | -5.08 | -9.12 | -11.19 | 75.00 |
| 80.00 | 0.48 | 1.11 | 0.29 | -1.40 | -6.50 | -10.45 | -9.63 | 80.00 |
| 85.00 | 0.38 | 0.86 | -0.09 | -2.50 | -7.70 | -10.46 | -5.89 | 85.00 |
| 90.00 | 0.24 | 0.60 | -0.44 | -3.53 | -8.52 | -9.10 | -0.20 | 90.00 |
| 95.00 | 0.18 | 0.28 | -0.87 | -4.57 | -9.01 | -7.26 | 4.72 | 95.00 |
| 100.00 | 0.23 | 0.06 | -1.34 | -5.65 | -9.06 | -4.61 | 9.11 | 100.00 |
| 105.00 | 0.13 | -0.17 | -1.85 | -6.70 | -8.78 | -0.88 | 11.67 | 105.00 |
| 110.00 | -0.11 | -0.49 | -2.50 | -7.75 | -8.40 | 3.39 | 11.09 | 110.00 |
| 115.00 | -0.28 | -0.58 | -2.86 | -7.96 | -8.50 | 7.40 | 9.43 | 115.00 |
| 120.00 | -0.19 | -0.60 | -2.75 | -8.07 | -9.67 | 11.7 | 8.05 | 120.00 |
| 125.00 | -0.00 | -0.50 | -1.54 | -7.95 | -10.91 | -0.13 | -0.74 | 125.00 |
| 130.00 | -0.10 | -1.49 | -0.01 | -6.64 | -10.15 | -10.55 | -11.66 | 130.00 |
| 135.00 | -0.35 | -1.82 | 0.96 | -4.08 | -8.88 | -11.14 | -12.22 | 135.00 |
| 140.00 | -0.50 | -1.65 | -0.65 | 0.73 | -11.41 | -11.53 | -12.58 | 140.00 |
| 145.00 | -0.58 | -1.36 | -1.64 | 0.44 | -11.78 | -11.78 | -12.71 | 145.00 |
| 150.00 | -0.64 | -1.20 | -1.70 | 0.21 | -12.00 | -11.78 | -12.56 | 150.00 |
| 155.00 | -0.62 | -0.86 | -1.14 | 0.27 | -12.02 | -11.66 | -12.12 | 155.00 |
| 160.00 | -0.62 | -0.51 | -1.05 | 0.46 | -11.82 | -11.34 | -11.61 | 160.00 |
| 165.00 | -0.65 | -1.31 | -1.43 | 0.57 | -11.63 | -10.87 | -11.06 | 165.00 |
| 170.00 | -0.67 | -1.54 | -1.52 | 0.70 | -10.88 | -10.33 | -10.47 | 170.00 |
| 175.00 | -0.68 | -1.65 | -1.69 | 0.85 | -10.36 | 0.12 | 0.10 | 175.00 |
| 180.00 | -0.57 | -0.66 | -1.54 | 1.02 | -10.04 | 0.41 | 0.44 | 180.00 |
| 185.00 | -0.22 | -0.81 | -1.15 | 1.14 | 0.00 | 0.30 | 0.47 | 185.00 |
| 190.00 | -0.08 | -0.65 | -1.00 | 1.01 | -10.04 | 0.21 | 0.89 | 190.00 |
| 195.00 | -0.21 | -0.78 | -1.16 | 0.93 | -10.13 | 0.11 | 0.84 | 195.00 |
| 200.00 | -0.45 | -0.93 | -0.60 | 1.01 | -10.14 | 0.08 | 0.74 | 200.00 |
| 205.00 | -0.47 | -0.70 | -0.36 | 1.08 | -10.04 | 0.14 | 0.66 | 205.00 |
| 210.00 | -0.38 | -0.15 | -0.54 | 1.14 | 0.11 | 0.33 | 0.69 | 210.00 |
| 215.00 | -0.43 | -0.36 | -1.14 | 1.27 | 0.28 | 0.51 | 0.67 | 215.00 |
| 220.00 | -0.53 | -0.69 | -0.81 | 1.51 | 0.34 | 0.49 | 0.62 | 220.00 |
| 225.00 | -0.60 | -0.96 | -0.57 | 1.65 | 0.45 | 0.43 | 0.61 | 225.00 |
| 230.00 | -0.72 | -1.20 | -1.07 | 1.70 | 0.75 | 0.52 | 0.65 | 230.00 |
| 235.00 | -0.80 | -1.11 | -0.13 | 2.14 | 1.18 | 0.76 | 0.75 | 235.00 |
| 240.00 | -0.86 | -0.98 | 0.87 | 2.74 | 2.08 | 1.33 | 1.33 | 240.00 |
| 245.00 | -0.82 | -1.01 | 1.74 | 3.01 | 3.16 | 2.78 | 2.25 | 245.00 |
| 250.00 | -0.67 | -0.93 | 1.27 | 3.84 | 4.45 | 3.40 | 3.28 | 250.00 |
| 255.00 | -0.43 | -0.88 | 0.26 | 1.40 | 5.63 | 4.68 | 4.27 | 255.00 |
| 260.00 | -0.18 | -1.00 | -1.05 | -0.43 | 6.60 | 5.17 | 5.24 | 260.00 |
| 265.00 | 0.15 | -1.07 | -1.80 | -2.54 | 7.25 | 7.44 | 6.16 | 265.00 |
| 270.00 | 0.35 | -0.51 | -2.14 | -3.84 | 6.98 | 8.28 | 6.87 | 270.00 |
| 275.00 | 0.28 | -0.75 | -2.19 | -4.55 | 6.84 | 7.96 | 7.52 | 275.00 |
| 280.00 | -0.03 | -0.73 | -2.00 | -4.97 | 1.20 | 5.96 | 7.58 | 280.00 |
| 285.00 | -0.27 | -0.77 | -1.70 | -5.17 | -2.20 | 2.40 | 6.37 | 285.00 |
| 290.00 | -0.44 | -0.65 | -1.38 | -5.03 | -4.86 | -1.67 | 4.38 | 290.00 |
| 295.00 | -0.55 | -0.69 | -1.06 | -4.81 | -6.61 | -3.44 | 2.01 | 295.00 |
| 300.00 | -0.62 | -0.54 | -0.81 | -4.49 | -7.20 | -4.44 | -0.59 | 300.00 |
| 305.00 | -0.62 | -0.66 | -0.67 | -3.84 | -6.78 | -4.65 | -2.85 | 305.00 |
| 310.00 | -0.55 | -0.55 | -0.80 | -3.07 | -6.46 | -4.19 | -4.71 | 310.00 |
| 315.00 | -0.46 | -0.71 | -0.25 | -2.21 | -5.65 | -3.91 | -6.54 | 315.00 |
| 320.00 | -0.36 | -0.27 | 0.05 | -1.38 | -4.88 | -3.24 | -7.07 | 320.00 |
| 325.00 | -0.24 | -0.14 | 0.31 | -0.36 | -0.12 | -0.88 | -0.59 | 325.00 |
| 330.00 | -0.24 | 0.10 | 0.69 | 0.57 | 1.36 | 1.20 | 1.43 | 330.00 |
| 335.00 | 0.18 | 0.37 | 1.02 | 1.45 | 2.59 | 2.60 | 2.79 | 335.00 |
| 340.00 | 0.27 | 0.45 | 1.41 | 2.33 | 3.46 | 4.12 | 3.74 | 340.00 |
| 345.00 | 0.25 | 0.75 | 2.05 | 3.07 | 4.24 | 4.85 | 4.29 | 345.00 |
| 350.00 | 0.50 | 1.04 | 2.76 | 3.58 | 4.77 | 5.47 | 4.67 | 350.00 |
| 355.00 | 0.75 | 1.36 | 2.89 | 3.87 | 4.87 | 5.44 | 4.74 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.11 | 3.36 | 5.69 | 8.74 | 11.01 | 11.85 | 12.06 | |

# BLADE LOADS

TEST 501 CNTR NO. 944 T.C.No. 29 C.R. 42

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -0.99 | -3.34 | -2.18 | -1.29 | 0.57 | 0.91 | 0.78 | 0.0 |
| 5.00 | -1.55 | -2.57 | -2.76 | -1.43 | -0.05 | 1.13 | 1.06 | 5.00 |
| 10.00 | -1.64 | -2.37 | -3.10 | -1.21 | 0.21 | 0.99 | 0.94 | 10.00 |
| 15.00 | -1.28 | -2.18 | -2.68 | -1.24 | 0.06 | 0.89 | 0.58 | 15.00 |
| 20.00 | -0.88 | -2.09 | -2.09 | -1.41 | 0.09 | 1.01 | 0.49 | 20.00 |
| 25.00 | -0.92 | -1.89 | -1.75 | -1.04 | 0.29 | 1.07 | 0.45 | 25.00 |
| 30.00 | -1.00 | -1.57 | -1.43 | -1.01 | 0.37 | 1.09 | 0.47 | 30.00 |
| 35.00 | -1.01 | -1.29 | -0.96 | -0.31 | 0.60 | 1.32 | 0.61 | 35.00 |
| 40.00 | -0.62 | -1.05 | -0.62 | 0.25 | 0.94 | 1.70 | 0.83 | 40.00 |
| 45.00 | -0.08 | -0.74 | -0.41 | 0.84 | 1.34 | 2.27 | 1.13 | 45.00 |
| 50.00 | -0.65 | -0.53 | -0.12 | 1.24 | 1.75 | 2.84 | 1.51 | 50.00 |
| 55.00 | -0.60 | -0.47 | 0.24 | 1.54 | 2.08 | 3.17 | 1.94 | 55.00 |
| 60.00 | -0.51 | -0.39 | 0.44 | 1.79 | 2.27 | 3.41 | 2.19 | 60.00 |
| 65.00 | -0.41 | -0.25 | 0.54 | 1.94 | 2.34 | 3.58 | 2.16 | 65.00 |
| 70.00 | -0.29 | -0.08 | 0.66 | 2.00 | 2.24 | 3.21 | 1.99 | 70.00 |
| 75.00 | -0.18 | 0.11 | 0.59 | 2.13 | 1.92 | 2.67 | 1.34 | 75.00 |
| 80.00 | -0.05 | 0.27 | 0.61 | 2.03 | 1.40 | 1.54 | 0.41 | 80.00 |
| 85.00 | 0.11 | 0.81 | 0.70 | 1.47 | 0.76 | 0.68 | -0.84 | 85.00 |
| 90.00 | 0.26 | 1.08 | 0.66 | 1.12 | 0.07 | -0.38 | -2.23 | 90.00 |
| 95.00 | 0.44 | 1.13 | 0.57 | 0.81 | -0.57 | -1.78 | -3.59 | 95.00 |
| 100.00 | 0.72 | 1.47 | 0.52 | 0.61 | -1.53 | -3.02 | -4.55 | 100.00 |
| 105.00 | 0.99 | 1.85 | 0.53 | 0.21 | -2.56 | -3.99 | -5.30 | 105.00 |
| 110.00 | 1.26 | 2.09 | 0.55 | 0.08 | -3.52 | -4.85 | -6.01 | 110.00 |
| 115.00 | 1.48 | 2.32 | 0.58 | -0.10 | -4.30 | -5.48 | -6.47 | 115.00 |
| 120.00 | 1.44 | 2.54 | 0.62 | -0.32 | -4.86 | -5.93 | -6.79 | 120.00 |
| 125.00 | 1.73 | 2.69 | 0.68 | -0.54 | -5.21 | -6.25 | -6.99 | 125.00 |
| 130.00 | 1.86 | 2.79 | 0.76 | -0.96 | -5.41 | -6.45 | -7.15 | 130.00 |
| 135.00 | 2.03 | 2.94 | 0.89 | -1.50 | -5.50 | -6.55 | -6.97 | 135.00 |
| 140.00 | 2.17 | 3.13 | 0.96 | -1.83 | -5.51 | -6.54 | -6.82 | 140.00 |
| 145.00 | 2.19 | 3.31 | 1.09 | -1.81 | -5.41 | -6.41 | -6.73 | 145.00 |
| 150.00 | 2.21 | 3.47 | 1.33 | -1.79 | -5.11 | -6.16 | -6.49 | 150.00 |
| 155.00 | 2.27 | 3.61 | 1.59 | -1.69 | -4.81 | -5.77 | -6.17 | 155.00 |
| 160.00 | 2.35 | 3.65 | 1.81 | -1.19 | -4.55 | -5.28 | -5.62 | 160.00 |
| 165.00 | 2.38 | 3.92 | 2.09 | -0.81 | -3.94 | -4.69 | -4.90 | 165.00 |
| 170.00 | 2.36 | 4.12 | 2.38 | -0.39 | -2.86 | -3.98 | -4.14 | 170.00 |
| 175.00 | 2.29 | 4.22 | 2.65 | 0.14 | -2.19 | -3.21 | -3.44 | 175.00 |
| 180.00 | 2.18 | 4.19 | 2.87 | 0.64 | -1.52 | -2.48 | -2.73 | 180.00 |
| 185.00 | 2.03 | 4.07 | 3.01 | 0.97 | -0.84 | -1.82 | -2.03 | 185.00 |
| 190.00 | 1.76 | 3.76 | 3.04 | 1.17 | -0.26 | 1.21 | -1.32 | 190.00 |
| 195.00 | 1.47 | 3.21 | 2.93 | 1.27 | 0.17 | -0.68 | -0.67 | 195.00 |
| 200.00 | 1.10 | 2.57 | 2.72 | 1.27 | 0.44 | -0.28 | -0.17 | 200.00 |
| 205.00 | 0.65 | 1.84 | 2.43 | 1.20 | 0.64 | 0.03 | 0.21 | 205.00 |
| 210.00 | 0.21 | 1.19 | 2.02 | 1.07 | 0.80 | 0.27 | 0.53 | 210.00 |
| 215.00 | -0.10 | 0.64 | 1.54 | 0.93 | 0.89 | 0.45 | 0.77 | 215.00 |
| 220.00 | -0.36 | 0.15 | 1.11 | 0.73 | 0.89 | 0.56 | 0.93 | 220.00 |
| 225.00 | -0.57 | -0.30 | 0.81 | 0.56 | 0.86 | 0.61 | 1.02 | 225.00 |
| 230.00 | -0.71 | -0.68 | 0.50 | 0.35 | 0.77 | 0.64 | 1.13 | 230.00 |
| 235.00 | -0.77 | -0.99 | 0.22 | 0.19 | 0.68 | 0.62 | 1.31 | 235.00 |
| 240.00 | -0.82 | -1.24 | -0.02 | 0.06 | 0.62 | 0.71 | 1.56 | 240.00 |
| 245.00 | -0.98 | -1.49 | -0.22 | -0.02 | 0.67 | 0.83 | 1.85 | 245.00 |
| 250.00 | -0.97 | -1.73 | -0.41 | -0.03 | 0.89 | 1.02 | 2.14 | 250.00 |
| 255.00 | -1.06 | -1.85 | -0.69 | 0.02 | 1.24 | 1.21 | 2.43 | 255.00 |
| 260.00 | -1.10 | -1.95 | -0.82 | 0.03 | 1.66 | 1.46 | 2.75 | 260.00 |
| 265.00 | -1.10 | -2.03 | -1.02 | 0.09 | 1.86 | 1.78 | 3.12 | 265.00 |
| 270.00 | -1.09 | -2.09 | -1.17 | 0.04 | 1.98 | 2.16 | 3.47 | 270.00 |
| 275.00 | -1.12 | -2.11 | -1.23 | 0.05 | 2.09 | 2.53 | 3.71 | 275.00 |
| 280.00 | -1.15 | -2.16 | -1.33 | 0.01 | 2.18 | 2.81 | 3.86 | 280.00 |
| 285.00 | -1.15 | -2.21 | -1.42 | -0.04 | 2.21 | 2.97 | 4.20 | 285.00 |
| 290.00 | -1.13 | -2.06 | -1.47 | -0.10 | 2.16 | 2.97 | 4.27 | 290.00 |
| 295.00 | -1.13 | -2.09 | -1.53 | -0.15 | 2.12 | 2.87 | 4.15 | 295.00 |
| 300.00 | -1.07 | -2.14 | -1.59 | -0.17 | 2.07 | 2.78 | 3.98 | 300.00 |
| 305.00 | -1.07 | -2.15 | -1.60 | -0.17 | 2.06 | 2.74 | 3.84 | 305.00 |
| 310.00 | -1.07 | -2.12 | -1.60 | -0.17 | 2.10 | 2.72 | 3.79 | 310.00 |
| 315.00 | -1.04 | -2.07 | -1.59 | -0.18 | 2.07 | 2.73 | 3.77 | 315.00 |
| 320.00 | -1.01 | -2.06 | -1.57 | -0.21 | 2.05 | 2.76 | 3.77 | 320.00 |
| 325.00 | -1.01 | -2.05 | -1.55 | -0.32 | 2.01 | 2.79 | 3.79 | 325.00 |
| 330.00 | -1.04 | -2.10 | -1.54 | -0.54 | 1.93 | 2.82 | 3.80 | 330.00 |
| 335.00 | -1.11 | -2.24 | -1.51 | -0.90 | 1.82 | 2.89 | 3.93 | 335.00 |
| 340.00 | -0.99 | -2.31 | -1.45 | -1.33 | 1.73 | 3.21 | 4.06 | 340.00 |
| 345.00 | -0.75 | -2.54 | -1.25 | -1.19 | 1.65 | 3.24 | 4.24 | 345.00 |
| 350.00 | -0.77 | -2.91 | -1.64 | -1.33 | 1.95 | 3.68 | 3.94 | 350.00 |
| 355.00 | -1.03 | -3.19 | -1.72 | -1.75 | 2.22 | 2.00 | 1.91 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 1.91 | 3.24 | 4.18 | 4.57 | 2.03 | 1.41 | 1.80 | |

# BLADE LOADS

TEST 502 CNTR NO. 169 T.C.No. 24 C.R. 43

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.34 | -3.81 | -3.09 | -1.64 | 0.12 | 1.12 | 0.68 | 0.0 |
| 5.00 | -2.10 | -3.36 | -3.32 | -2.67 | -2.00 | 0.79 | -0.81 | 5.00 |
| 10.00 | -1.37 | -2.38 | -3.10 | -2.67 | -0.45 | 0.77 | -0.37 | 10.00 |
| 15.00 | -0.85 | -2.00 | -2.36 | -2.15 | -0.62 | 0.74 | -0.44 | 15.00 |
| 20.00 | -0.36 | -2.00 | -1.90 | -1.34 | -0.30 | 0.98 | -0.11 | 20.00 |
| 25.00 | -1.14 | -2.04 | -1.57 | -0.66 | 0.04 | 1.24 | -0.07 | 25.00 |
| 30.00 | -1.72 | -1.19 | -1.23 | -0.19 | 0.26 | 1.39 | 0.03 | 30.00 |
| 35.00 | -1.14 | -0.85 | -0.65 | 0.42 | 0.86 | 1.91 | 0.58 | 35.00 |
| 40.00 | -0.65 | -0.74 | -0.52 | 1.14 | 1.60 | 2.48 | 1.28 | 40.00 |
| 45.00 | -0.53 | -0.67 | -0.09 | 1.81 | 2.25 | 3.03 | 1.76 | 45.00 |
| 50.00 | -0.44 | -0.69 | 0.39 | 2.36 | 2.74 | 3.40 | 2.15 | 50.00 |
| 55.00 | -0.34 | -0.69 | 0.79 | 2.95 | 2.94 | 3.43 | 2.57 | 55.00 |
| 60.00 | -0.29 | -0.57 | 0.85 | 2.70 | 2.85 | 3.62 | 2.45 | 60.00 |
| 65.00 | -0.22 | -0.29 | 0.76 | 2.67 | 2.53 | 3.28 | 2.61 | 65.00 |
| 70.00 | -0.11 | 0.17 | 0.68 | 2.37 | 1.96 | 2.46 | 1.59 | 70.00 |
| 75.00 | 0.02 | 0.48 | 0.73 | 1.96 | 1.05 | 1.19 | 0.27 | 75.00 |
| 80.00 | 0.16 | 0.67 | 0.69 | 1.41 | 0.03 | -0.38 | -1.43 | 80.00 |
| 85.00 | 0.33 | 1.23 | 0.68 | 0.81 | -1.07 | -2.12 | -3.29 | 85.00 |
| 90.00 | 0.48 | 1.63 | 0.51 | 0.32 | -2.14 | -3.95 | -5.20 | 90.00 |
| 95.00 | 0.62 | 1.85 | 0.52 | 0.15 | -3.40 | -5.39 | -6.62 | 95.00 |
| 100.00 | 1.25 | 2.12 | 0.65 | -0.05 | -4.70 | -6.68 | -7.93 | 100.00 |
| 105.00 | 1.64 | 2.30 | 0.76 | -0.44 | -5.86 | -7.73 | -8.11 | 105.00 |
| 110.00 | 1.91 | 2.47 | 0.85 | -0.84 | -6.66 | -8.48 | -8.64 | 110.00 |
| 115.00 | 2.14 | 2.65 | 1.00 | -1.43 | -7.14 | -8.83 | -9.00 | 115.00 |
| 120.00 | 2.35 | 2.94 | 1.17 | -2.07 | -7.31 | -8.88 | -9.04 | 120.00 |
| 125.00 | 2.54 | 3.29 | 1.33 | -2.61 | -7.24 | -8.67 | -8.91 | 125.00 |
| 130.00 | 2.73 | 3.48 | 1.47 | -2.81 | -6.97 | -8.21 | -8.42 | 130.00 |
| 135.00 | 2.87 | 3.69 | 1.69 | -2.56 | -6.51 | -7.54 | -8.13 | 135.00 |
| 140.00 | 2.92 | 3.89 | 1.90 | -2.06 | -5.89 | -6.76 | -7.37 | 140.00 |
| 145.00 | 2.96 | 4.09 | 2.14 | -1.52 | -5.09 | -5.92 | -6.50 | 145.00 |
| 150.00 | 3.07 | 4.32 | 2.44 | -0.89 | -4.19 | -5.04 | -5.61 | 150.00 |
| 155.00 | 3.04 | 4.57 | 2.77 | -0.16 | -3.28 | -4.13 | -4.65 | 155.00 |
| 160.00 | 2.91 | 4.75 | 3.12 | 0.50 | -2.42 | -3.23 | -3.69 | 160.00 |
| 165.00 | 2.69 | 4.92 | 3.50 | 1.12 | -1.61 | -2.37 | -2.75 | 165.00 |
| 170.00 | 2.38 | 4.84 | 3.82 | 1.55 | -0.84 | -1.55 | -1.87 | 170.00 |
| 175.00 | 2.06 | 4.92 | 3.91 | 1.81 | -0.20 | -0.82 | -1.02 | 175.00 |
| 180.00 | 1.79 | 4.00 | 3.78 | 1.93 | 0.35 | -0.20 | -0.25 | 180.00 |
| 185.00 | 1.33 | 3.74 | 3.42 | 1.91 | 0.71 | 0.30 | 0.37 | 185.00 |
| 190.00 | 0.77 | 2.98 | 2.84 | 1.75 | 0.95 | 0.71 | 0.78 | 190.00 |
| 195.00 | 0.27 | 1.77 | 2.24 | 1.49 | 1.09 | 1.00 | 1.00 | 195.00 |
| 200.00 | -0.15 | 1.06 | 1.57 | 1.25 | 1.14 | 1.10 | 1.16 | 200.00 |
| 205.00 | -0.49 | 0.65 | 1.07 | 0.98 | 1.13 | 1.06 | 1.24 | 205.00 |
| 210.00 | -0.70 | 0.01 | 0.70 | 0.60 | 1.09 | 0.99 | 1.27 | 210.00 |
| 215.00 | -0.82 | -0.38 | 0.32 | 0.31 | 1.05 | 0.89 | 1.31 | 215.00 |
| 220.00 | -0.91 | -0.70 | -0.04 | 0.15 | 1.04 | 0.96 | 1.38 | 220.00 |
| 225.00 | -1.02 | -0.95 | -0.34 | 0.14 | 1.04 | 0.86 | 1.40 | 225.00 |
| 230.00 | -1.11 | -1.28 | -0.84 | -0.05 | 1.16 | 0.88 | 1.64 | 230.00 |
| 235.00 | -1.20 | -1.45 | -0.79 | -0.16 | 1.27 | 0.95 | 1.84 | 235.00 |
| 240.00 | -1.29 | -1.67 | -0.94 | -0.17 | 1.28 | 1.38 | 2.10 | 240.00 |
| 245.00 | -1.27 | -1.77 | -1.10 | -0.21 | 1.49 | 1.31 | 2.44 | 245.00 |
| 250.00 | -1.31 | -1.80 | -1.23 | -0.24 | 1.76 | 1.41 | 2.75 | 250.00 |
| 255.00 | -1.28 | -1.79 | -1.23 | -0.22 | 2.02 | 1.65 | 3.07 | 255.00 |
| 260.00 | -1.22 | -1.80 | -1.42 | -0.14 | 2.25 | 2.30 | 3.44 | 260.00 |
| 265.00 | -1.19 | -1.84 | -1.47 | -0.07 | 2.45 | 2.61 | 3.80 | 265.00 |
| 270.00 | -1.22 | -1.85 | -1.48 | -0.02 | 2.65 | 2.92 | 4.14 | 270.00 |
| 275.00 | -1.24 | -1.85 | -1.45 | -0.01 | 2.87 | 3.20 | 4.45 | 275.00 |
| 280.00 | -1.15 | -1.80 | -1.46 | -0.04 | 3.01 | 3.41 | 4.67 | 280.00 |
| 285.00 | -1.05 | -1.85 | -1.44 | -0.05 | 3.01 | 3.51 | 4.78 | 285.00 |
| 290.00 | -1.05 | -1.84 | -1.49 | -0.11 | 2.95 | 3.48 | 4.64 | 290.00 |
| 295.00 | -1.12 | -1.87 | -1.71 | -0.10 | 2.87 | 3.35 | 4.36 | 295.00 |
| 300.00 | -1.17 | -1.87 | -1.76 | -0.04 | 2.74 | 3.20 | 4.06 | 300.00 |
| 305.00 | -1.15 | -1.89 | -1.79 | -0.03 | 2.66 | 3.14 | 4.00 | 305.00 |
| 310.00 | -1.15 | -2.03 | -1.76 | -0.14 | 2.65 | 3.19 | 4.07 | 310.00 |
| 315.00 | -1.04 | -2.04 | -1.74 | -0.15 | 2.63 | 3.21 | 4.15 | 315.00 |
| 320.00 | -0.96 | -2.07 | -1.71 | -0.25 | 2.52 | 3.21 | 4.15 | 320.00 |
| 325.00 | -1.00 | -2.06 | -1.61 | -0.37 | 2.29 | 3.15 | 4.11 | 325.00 |
| 330.00 | -1.21 | -2.04 | -1.39 | -0.57 | 1.94 | 2.94 | 4.04 | 330.00 |
| 335.00 | -0.91 | -2.16 | -0.89 | -0.75 | 1.45 | 2.60 | 3.78 | 335.00 |
| 340.00 | -0.49 | -2.44 | -0.37 | -0.87 | 0.87 | 1.99 | 3.31 | 340.00 |
| 345.00 | -0.40 | -2.51 | -0.07 | -0.81 | 0.07 | 2.51 | 2.36 | 345.00 |
| 350.00 | -0.39 | -2.56 | -1.55 | -0.40 | 1.42 | 2.97 | 3.48 | 350.00 |
| 355.00 | -1.20 | -2.96 | -2.24 | -0.42 | 0.99 | 2.26 | 3.01 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.47 | 0.91 | 0.47 | 0.21 | 0.90 | 2.00 | 1.15 | |

# BLADE LOADS

TEST 494 CNTR NO. 184 T.C.N. 25 C.R. 22

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -3.39 | -4.75 | -4.27 | -3.28 | -0.15 | 1.99 | 1.67 | 0.0 |
| 5.00 | -3.3. | -5.35 | -4.12 | -3.95 | -1.37 | -0.59 | -1.09 | 5.00 |
| 10.00 | -1.17 | -3.90 | -3.59 | -3.27 | -1.73 | -1.19 | -1.82 | 10.00 |
| 15.00 | -2.55 | -3.48 | -3.07 | -1.64 | -0.96 | -0.41 | -1.12 | 15.00 |
| 20.00 | -0.10 | -3.32 | -2.97 | -0.73 | 0.35 | 0.90 | 0.29 | 20.00 |
| 25.00 | -0.73 | -3.30 | -2.05 | -0.61 | 1.49 | 2.29 | 1.46 | 25.00 |
| 30.00 | -1.26 | -2.35 | -0.97 | 0.27 | 2.34 | 3.35 | 2.05 | 30.00 |
| 35.00 | -1.02 | -1.66 | -0.13 | 1.42 | 2.81 | 3.72 | 2.48 | 35.00 |
| 40.00 | -0.70 | -1.45 | 0.59 | 2.44 | 3.26 | 3.98 | 3.01 | 40.00 |
| 45.00 | -0.81 | -1.26 | 1.18 | 3.43 | 3.87 | 4.48 | 3.69 | 45.00 |
| 50.00 | -0.74 | -1.11 | 1.47 | 4.37 | 4.39 | 5.12 | 4.38 | 50.00 |
| 55.00 | -0.36 | -1.04 | 1.78 | 4.61 | 4.97 | 5.89 | 4.99 | 55.00 |
| 60.00 | -0.07 | -0.89 | 2.07 | 4.70 | 4.92 | 6.28 | 4.94 | 60.00 |
| 65.00 | -0.09 | -0.85 | 2.09 | 4.89 | 4.41 | 6.21 | 4.72 | 65.00 |
| 70.00 | -0.20 | -0.77 | 2.09 | 4.47 | 3.55 | 5.25 | 4.37 | 70.00 |
| 75.00 | -0.17 | -0.42 | 1.93 | 3.96 | 2.69 | 4.57 | 4.07 | 75.00 |
| 80.00 | 0.06 | 0.09 | 1.48 | 3.58 | 1.94 | 1.76 | 1.53 | 80.00 |
| 85.00 | 0.43 | 0.59 | 1.65 | 2.72 | 0.78 | 1.22 | -1.44 | 85.00 |
| 90.00 | 0.81 | 1.09 | 1.66 | 2.08 | -0.99 | -1.88 | -4.46 | 90.00 |
| 95.00 | 1.19 | 1.53 | 1.28 | 1.31 | -3.67 | -7.53 | -9.83 | 95.00 |
| 100.00 | 1.79 | 1.88 | 1.50 | 0.72 | -6.37 | -12.30 | -8.88 | 100.00 |
| 105.00 | 2.45 | 2.28 | 1.65 | -0.37 | -8.31 | -14.43 | -11.63 | 105.00 |
| 110.00 | 2.87 | 2.68 | 1.75 | -2.33 | -9.51 | -15.36 | -12.94 | 110.00 |
| 115.00 | 3.16 | 3.20 | 1.86 | -4.23 | -10.35 | -15.19 | -14.07 | 115.00 |
| 120.00 | 3.40 | 3.71 | 1.98 | -5.72 | -10.72 | -13.62 | -14.91 | 120.00 |
| 125.00 | 3.61 | 4.18 | 1.91 | -5.83 | -10.69 | -11.68 | -12.92 | 125.00 |
| 130.00 | 3.82 | 4.53 | 1.64 | -5.36 | -10.43 | -11.28 | -11.12 | 130.00 |
| 135.00 | 4.04 | 4.76 | 1.49 | -4.83 | -9.95 | -10.76 | -11.00 | 135.00 |
| 140.00 | 4.16 | 5.03 | 1.37 | -4.32 | -9.15 | -9.88 | -9.59 | 140.00 |
| 145.00 | 4.18 | 5.27 | 1.24 | -2.95 | -7.88 | -8.97 | -8.72 | 145.00 |
| 150.00 | 4.15 | 5.52 | 1.54 | -2.31 | -6.43 | -7.75 | -7.75 | 150.00 |
| 155.00 | 4.06 | 5.79 | 2.12 | -1.24 | -5.02 | -6.04 | -6.60 | 155.00 |
| 160.00 | 3.99 | 6.08 | 2.83 | -0.32 | -3.71 | -4.42 | -5.16 | 160.00 |
| 165.00 | 3.82 | 6.35 | 3.53 | 0.58 | -2.51 | -3.02 | -3.73 | 165.00 |
| 170.00 | 3.37 | 6.46 | 4.12 | 1.35 | -1.40 | -1.77 | -2.53 | 170.00 |
| 175.00 | 2.71 | 6.18 | 4.50 | 1.97 | -0.42 | -0.76 | -1.48 | 175.00 |
| 180.00 | 1.03 | 5.52 | 4.59 | 2.27 | 0.43 | 0.17 | -0.44 | 180.00 |
| 185.00 | 1.29 | 4.61 | 4.37 | 2.55 | 1.12 | 0.90 | 0.47 | 185.00 |
| 190.00 | 0.52 | 3.48 | 3.80 | 2.72 | 1.64 | 1.42 | 1.18 | 190.00 |
| 195.00 | -0.16 | 2.22 | 3.05 | 2.59 | 1.92 | 1.78 | 1.63 | 195.00 |
| 200.00 | -0.66 | 1.09 | 2.31 | 2.19 | 1.89 | 1.98 | 1.86 | 200.00 |
| 205.00 | -1.05 | 0.22 | 1.57 | 1.74 | 1.87 | 2.00 | 1.95 | 205.00 |
| 210.00 | -1.39 | -0.49 | 0.93 | 1.16 | 1.87 | 1.94 | 1.92 | 210.00 |
| 215.00 | -1.58 | -0.91 | 0.38 | 0.66 | 1.72 | 1.89 | 1.90 | 215.00 |
| 220.00 | -1.70 | -1.35 | -0.07 | 0.25 | 1.59 | 1.74 | 1.90 | 220.00 |
| 225.00 | -1.79 | -1.67 | -0.47 | -0.36 | 1.49 | 1.73 | 2.02 | 225.00 |
| 230.00 | -1.85 | -1.85 | -0.81 | -0.17 | 1.43 | 1.76 | 2.16 | 230.00 |
| 235.00 | -1.83 | -1.93 | -1.07 | -0.28 | 1.42 | 1.76 | 2.27 | 235.00 |
| 240.00 | -1.73 | -2.01 | -1.28 | -0.35 | 1.48 | 1.83 | 2.38 | 240.00 |
| 245.00 | -1.80 | -2.26 | -1.46 | -0.44 | 1.57 | 1.95 | 2.52 | 245.00 |
| 250.00 | -1.78 | -2.33 | -1.60 | -0.51 | 1.76 | 2.14 | 2.69 | 250.00 |
| 255.00 | -1.77 | -2.36 | -1.73 | -0.54 | 1.86 | 2.30 | 2.85 | 255.00 |
| 260.00 | -1.77 | -2.38 | -1.76 | -0.59 | 1.99 | 2.29 | 3.05 | 260.00 |
| 265.00 | -1.71 | -2.41 | -1.77 | -0.61 | 2.11 | 2.41 | 3.28 | 265.00 |
| 270.00 | -1.80 | -2.42 | -1.82 | -0.62 | 2.21 | 2.52 | 3.55 | 270.00 |
| 275.00 | -1.49 | -2.39 | -1.87 | -0.63 | 2.31 | 2.71 | 3.80 | 275.00 |
| 280.00 | -1.43 | -2.31 | -1.87 | -0.62 | 2.44 | 2.93 | 4.01 | 280.00 |
| 285.00 | -1.42 | -2.24 | -1.85 | -0.57 | 2.58 | 3.21 | 4.21 | 285.00 |
| 290.00 | -1.41 | -2.16 | -1.80 | -0.46 | 2.75 | 3.52 | 4.46 | 290.00 |
| 295.00 | -1.21 | -2.11 | -1.72 | -0.30 | 2.96 | 3.81 | 4.68 | 295.00 |
| 300.00 | -1.09 | -2.12 | -1.66 | -0.11 | 3.17 | 4.08 | 4.88 | 300.00 |
| 305.00 | -1.22 | -2.11 | -1.58 | -0.03 | 3.35 | 4.28 | 4.99 | 305.00 |
| 310.00 | -0.97 | -2.02 | -1.49 | 0.19 | 3.50 | 4.63 | 5.01 | 310.00 |
| 315.00 | -0.94 | -1.91 | -1.49 | 0.18 | 3.59 | 4.78 | 4.98 | 315.00 |
| 320.00 | -0.89 | -1.87 | -1.53 | 0.13 | 3.57 | 4.83 | 4.96 | 320.00 |
| 325.00 | -0.97 | -1.89 | -1.53 | -0.05 | 3.43 | 4.77 | 4.83 | 325.00 |
| 330.00 | -1.36 | -1.93 | -1.46 | -0.17 | 3.10 | 4.56 | 4.33 | 330.00 |
| 335.00 | -1.84 | -1.94 | -1.99 | -0.37 | 2.66 | 4.07 | 3.59 | 335.00 |
| 340.00 | -1.95 | -2.09 | -2.46 | -0.36 | 2.38 | 3.66 | 3.05 | 340.00 |
| 345.00 | -1.72 | -1.96 | -3.22 | -0.33 | 2.28 | 3.39 | 3.12 | 345.00 |
| 350.00 | -1.63 | -1.97 | -3.39 | -1.96 | 2.24 | 4.46 | 4.05 | 350.00 |
| 355.00 | -2.56 | -2.35 | -4.72 | -2.84 | 1.65 | 4.66 | 4.55 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 1.68 | 2.[illegible] | 2.65 | 2.52 | 0.81 | 0.86 | 0.50 | |

# BLADE LOADS

TEST 494 CNTR NO. 264 T.C.No. 26 Code 11

SPAN STATION

| DEG | 52.5 | 79.6 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.74 | -5.08 | -5.29 | -2.78 | -2.21 | -2.00 | -2.97 | 0.0 |
| 5.00 | -1.38 | -7.02 | -7.02 | -1.78 | -0.92 | 0.60 | -2.58 | 5.00 |
| 10.00 | 0.71 | -6.29 | -7.46 | -1.89 | -0.67 | 1.16 | -0.65 | 10.00 |
| 15.00 | -1.56 | -5.84 | -6.75 | -2.91 | -0.63 | -0.06 | -1.23 | 15.00 |
| 20.00 | -1.28 | -2.01 | -4.89 | -3.91 | -0.58 | -0.14 | -1.56 | 20.00 |
| 25.00 | -0.68 | -3.67 | -2.40 | -1.43 | 0.26 | 1.26 | -0.33 | 25.00 |
| 30.00 | -1.16 | -3.66 | -0.47 | 0.73 | 1.88 | 3.32 | 1.20 | 30.00 |
| 35.00 | -2.73 | -2.77 | 0.36 | 2.78 | 3.49 | 4.44 | 2.65 | 35.00 |
| 40.00 | -2.92 | -2.24 | 0.82 | 3.94 | 4.13 | 5.56 | 4.49 | 40.00 |
| 45.00 | -2.27 | -1.77 | 1.61 | 4.32 | 4.74 | 6.08 | 6.30 | 45.00 |
| 50.00 | -1.19 | -1.22 | 1.92 | 4.69 | 5.39 | 8.12 | 7.48 | 50.00 |
| 55.00 | -0.06 | -0.90 | 1.82 | 5.30 | 5.61 | 7.94 | 7.09 | 55.00 |
| 60.00 | 0.42 | -0.84 | 1.89 | 5.67 | 5.85 | 8.23 | 5.72 | 60.00 |
| 65.00 | 0.56 | -1.02 | 2.15 | 5.23 | 5.66 | 6.85 | 4.18 | 65.00 |
| 70.00 | 0.35 | -1.19 | 2.13 | 3.99 | 5.14 | 3.99 | 2.00 | 70.00 |
| 75.00 | 0.02 | -1.09 | 1.30 | 3.03 | 4.17 | 2.89 | -0.86 | 75.00 |
| 80.00 | -0.19 | -0.67 | 0.31 | 2.49 | 2.63 | 1.61 | -4.80 | 80.00 |
| 85.00 | -0.14 | -0.36 | -0.04 | 1.79 | 0.99 | -3.57 | -6.52 | 85.00 |
| 90.00 | 0.24 | -0.16 | 0.59 | 1.32 | -1.84 | -10.20 | -8.52 | 90.00 |
| 95.00 | 0.87 | 0.37 | 1.52 | 1.83 | -5.69 | -11.42 | -8.17 | 95.00 |
| 100.00 | 1.63 | 1.11 | 2.58 | 2.18 | -7.98 | -9.47 | -6.44 | 100.00 |
| 105.00 | 2.38 | 2.07 | 3.51 | -0.17 | -7.31 | -7.16 | -2.33 | 105.00 |
| 110.00 | 3.08 | 3.14 | 4.22 | -2.79 | -5.90 | -6.28 | -1.89 | 110.00 |
| 115.00 | 3.75 | 4.10 | 4.59 | -3.91 | -4.91 | -6.67 | -3.60 | 115.00 |
| 120.00 | 4.41 | 5.01 | 4.11 | -4.28 | -7.11 | -5.25 | -6.72 | 120.00 |
| 125.00 | 4.95 | 5.77 | 2.16 | -4.69 | -11.58 | -7.41 | -6.78 | 125.00 |
| 130.00 | 5.33 | 6.29 | -0.21 | -5.22 | -11.31 | -11.92 | -8.97 | 130.00 |
| 135.00 | 5.54 | 6.50 | -1.20 | -5.71 | -10.17 | -13.42 | -12.93 | 135.00 |
| 140.00 | 5.62 | 6.49 | -0.86 | -5.82 | -10.05 | -12.48 | -13.87 | 140.00 |
| 145.00 | 5.59 | 6.34 | -0.62 | -5.55 | -11.06 | -12.16 | -12.83 | 145.00 |
| 150.00 | 5.49 | 5.92 | -0.39 | -5.12 | -10.61 | -12.55 | -10.74 | 150.00 |
| 155.00 | 5.31 | 5.44 | 0.20 | -4.42 | -9.24 | -11.41 | -9.87 | 155.00 |
| 160.00 | 5.02 | 5.21 | 0.93 | -3.33 | -7.67 | -9.08 | -8.30 | 160.00 |
| 165.00 | 4.57 | 5.72 | 1.87 | -1.88 | -5.71 | -6.54 | -6.64 | 165.00 |
| 170.00 | 3.99 | 6.32 | 2.83 | -0.20 | -3.75 | -4.22 | -4.62 | 170.00 |
| 175.00 | 3.31 | 6.73 | 3.68 | 1.24 | -2.05 | -2.26 | -2.58 | 175.00 |
| 180.00 | 2.45 | 6.43 | 4.22 | 2.00 | -0.56 | -0.94 | -0.73 | 180.00 |
| 185.00 | 1.51 | 5.56 | 4.33 | 2.35 | 0.65 | 0.60 | 0.67 | 185.00 |
| 190.00 | 0.56 | 4.22 | 4.01 | 2.40 | 1.61 | 1.48 | 1.67 | 190.00 |
| 195.00 | -0.37 | 2.66 | 3.25 | 2.31 | 2.27 | 2.13 | 2.31 | 195.00 |
| 200.00 | -1.21 | 1.13 | 2.34 | 2.27 | 2.62 | 2.53 | 2.64 | 200.00 |
| 205.00 | -1.83 | -0.59 | 1.43 | 2.04 | 2.76 | 2.72 | 2.76 | 205.00 |
| 210.00 | -2.13 | -0.94 | 0.65 | 1.74 | 2.78 | 2.76 | 2.83 | 210.00 |
| 215.00 | -2.27 | -1.46 | 0.17 | 1.41 | 2.79 | 2.77 | 2.93 | 215.00 |
| 220. | -2.33 | -1.78 | -0.13 | 1.06 | 2.68 | 2.76 | 3.08 | 220.00 |
| 225.00 | -2.37 | -2.02 | -0.35 | 0.74 | 2.65 | 2.80 | 3.22 | 225.00 |
| 230.00 | -2.37 | -2.22 | -0.57 | 0.53 | 2.67 | 2.87 | 3.35 | 230.00 |
| 235.00 | -2.29 | -2.36 | -0.80 | 0.42 | 2.72 | 2.97 | 3.49 | 235.00 |
| 240.00 | -2.20 | -2.41 | -1.00 | 0.33 | 2.77 | 3.08 | 3.64 | 240.00 |
| 245.00 | -2.17 | -2.39 | -1.13 | 0.30 | 2.82 | 3.19 | 3.76 | 245.00 |
| 250.00 | -2.13 | -2.29 | -1.18 | 0.21 | 2.86 | 3.26 | 3.87 | 250.00 |
| 255.00 | -2.11 | -2.24 | -1.18 | 0.12 | 2.89 | 3.30 | 3.93 | 255.00 |
| 260.00 | -2.07 | -2.26 | -1.16 | 0.06 | 2.90 | 3.32 | 3.97 | 260.00 |
| 265.00 | -2.04 | -2.28 | -1.13 | 0.03 | 2.91 | 3.32 | 3.99 | 265.00 |
| 270.00 | -2.00 | -2.26 | -1.09 | 0.01 | 2.93 | 3.35 | 4.04 | 270.00 |
| 275.00 | -1.94 | -2.23 | -1.03 | 0.04 | 2.97 | 3.41 | 4.14 | 275.00 |
| 280.00 | -1.89 | -2.20 | -0.96 | 0.13 | 3.03 | 3.50 | 4.19 | 280.00 |
| 285.00 | -1.87 | -2.14 | -0.95 | 0.25 | 3.10 | 3.62 | 4.27 | 285.00 |
| 290.00 | -1.94 | -2.24 | -0.95 | 0.29 | 3.10 | 3.75 | 4.35 | 290.00 |
| 295.00 | -1.95 | -2.44 | -0.99 | 0.40 | 3.27 | 3.90 | 4.44 | 295.00 |
| 300.00 | -1.78 | -2.49 | -1.06 | 0.49 | 3.36 | 4.05 | 4.52 | 300.00 |
| 305.00 | -1.70 | -2.34 | -1.12 | 0.49 | 3.44 | 4.16 | 4.59 | 305.00 |
| 310.00 | -1.54 | -2.08 | -1.16 | 0.52 | 3.50 | 4.27 | 4.62 | 310.00 |
| 315.00 | -1.34 | -1.88 | -1.20 | 0.47 | 3.51 | 4.26 | 4.60 | 315.00 |
| 320.00 | -1.09 | -1.79 | -1.23 | 0.31 | 3.49 | 4.23 | 4.49 | 320.00 |
| 325.00 | -0.75 | -1.65 | -1.22 | 0.05 | 3.41 | 4.12 | 4.26 | 325.00 |
| 330.00 | -0.63 | -1.49 | -1.17 | -0.36 | 3.17 | 3.87 | 3.85 | 330.00 |
| 335.00 | -0.56 | -1.52 | -1.16 | -1.12 | 2.67 | 3.42 | 3.16 | 335.00 |
| 340.00 | -0.76 | 2.01 | -1.01 | -1.83 | 1.77 | 2.63 | 2.20 | 340.00 |
| 345.00 | -1.81 | -1.88 | -0.92 | -1.80 | 0.61 | 1.35 | 0.90 | 345.00 |
| 350.00 | -2.[illegible] | -1.71 | -1.38 | -1.09 | -0.33 | -0.06 | -0.67 | 350.00 |
| 355.00 | -2.[illegible] | -2.[illegible] | -2.08 | -1.33 | -1.32 | -0.74 | -0.92 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.89 | 1.61 | 1.11 | -0.33 | -0.75 | -1.85 | -2.50 | |

# BLADE LOADS

TEST 900 CNTR NO. 458 T.C.N. 27 C.R. 39

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.56 | -5.93 | -6.14 | -2.90 | 0.43 | -1.02 | -2.62 | 0.0 |
| 5.00 | -1.48 | -3.78 | -7.23 | -3.82 | -1.25 | -0.84 | -1.12 | 5.00 |
| 10.00 | -0.74 | -2.73 | -7.16 | -4.34 | -2.95 | -1.48 | -1.18 | 10.00 |
| 15.00 | -3.46 | -2.46 | -6.28 | -3.73 | -3.05 | -2.08 | -2.73 | 15.00 |
| 20.00 | -1.04 | -3.46 | -4.03 | -2.85 | -2.51 | -2.36 | -3.57 | 20.00 |
| 25.00 | -2.59 | -4.30 | -1.58 | -1.24 | -0.99 | -1.24 | -2.97 | 25.00 |
| 30.00 | -3.62 | -4.07 | -0.94 | 0.65 | 1.01 | 1.15 | -0.89 | 30.00 |
| 35.00 | -3.54 | -3.69 | -0.95 | 2.55 | 2.70 | 3.33 | 1.36 | 35.00 |
| 40.00 | -3.01 | -3.20 | 0.0 | 3.95 | 4.15 | 4.94 | 3.44 | 40.00 |
| 45.00 | -2.47 | -2.55 | 1.15 | 4.96 | 5.32 | 7.13 | 6.31 | 45.00 |
| 50.00 | -1.45 | -2.09 | 1.44 | 5.94 | 6.75 | 9.46 | 8.91 | 50.00 |
| 55.00 | -0.16 | -1.90 | 1.40 | 6.47 | 7.84 | 11.13 | 8.42 | 55.00 |
| 60.00 | 0.35 | -1.59 | 1.75 | 6.63 | 8.40 | 9.37 | 6.51 | 60.00 |
| 65.00 | 0.19 | -1.32 | 2.23 | 5.24 | 7.92 | 5.28 | 3.98 | 65.00 |
| 70.00 | -0.15 | -0.99 | 2.41 | 5.33 | 5.42 | 5.18 | 0.33 | 70.00 |
| 75.00 | -0.36 | -0.58 | 1.84 | 5.63 | 2.86 | 0.60 | -1.78 | 75.00 |
| 80.00 | -0.43 | -0.50 | 1.57 | 5.67 | -0.91 | -2.62 | -0.70 | 80.00 |
| 85.00 | -0.57 | -0.58 | 1.44 | 3.11 | 0.77 | -0.24 | -1.43 | 85.00 |
| 90.00 | -0.21 | -0.35 | 2.35 | 3.27 | -3.45 | -3.25 | -3.38 | 90.00 |
| 95.00 | 0.30 | 0.47 | 2.59 | 5.45 | -6.13 | -6.60 | -2.74 | 95.00 |
| 100.00 | 1.31 | 1.43 | 3.10 | 1.59 | -7.69 | -8.65 | -0.02 | 100.00 |
| 105.00 | 2.53 | 2.39 | 2.66 | -5.05 | -9.69 | -8.93 | -1.85 | 105.00 |
| 110.00 | 3.48 | 3.19 | 1.59 | -10.58 | -10.80 | -7.59 | -2.64 | 110.00 |
| 115.00 | 4.02 | 3.97 | 0.34 | -10.40 | -7.28 | -3.88 | -5.68 | 115.00 |
| 120.00 | 4.36 | 4.92 | -1.72 | -9.42 | -10.70 | -3.87 | -9.78 | 120.00 |
| 125.00 | 4.67 | 5.84 | -3.38 | -10.34 | -11.34 | -7.91 | -13.78 | 125.00 |
| 130.00 | 5.06 | 5.99 | -2.85 | -9.79 | -11.79 | -10.20 | -14.23 | 130.00 |
| 135.00 | 5.56 | 6.16 | -1.02 | -6.60 | -14.03 | -11.74 | -13.13 | 135.00 |
| 140.00 | 5.93 | 6.41 | 0.08 | -4.31 | -10.21 | -12.65 | -9.84 | 140.00 |
| 145.00 | 6.21 | 6.44 | 0.05 | -2.71 | -7.10 | -10.42 | -9.61 | 145.00 |
| 150.00 | 6.19 | 6.36 | 1.48 | -1.78 | -6.66 | -8.17 | -8.92 | 150.00 |
| 155.00 | 5.93 | 6.65 | 2.00 | -1.18 | -5.97 | -7.07 | -8.09 | 155.00 |
| 160.00 | 5.45 | 7.25 | 2.94 | -0.55 | -4.85 | -6.36 | -7.67 | 160.00 |
| 165.00 | 4.73 | 7.73 | 4.03 | 0.32 | -3.53 | -5.14 | -6.19 | 165.00 |
| 170.00 | 3.79 | 7.82 | 5.09 | 1.53 | -2.33 | -3.73 | -4.50 | 170.00 |
| 175.00 | 2.80 | 7.42 | 5.76 | 2.84 | -1.17 | -2.36 | -2.90 | 175.00 |
| 180.00 | 1.81 | 6.49 | 5.80 | 3.48 | 0.09 | -0.97 | -1.94 | 180.00 |
| 185.00 | 0.78 | 5.05 | 5.17 | 3.74 | 1.03 | 0.32 | -0.30 | 185.00 |
| 190.00 | -0.38 | 3.24 | 4.28 | 3.49 | 1.91 | 1.30 | 0.79 | 190.00 |
| 195.00 | -1.35 | 1.46 | 3.23 | 3.11 | 2.59 | 2.04 | 1.70 | 195.00 |
| 200.00 | -1.87 | 0.15 | 2.42 | 2.62 | 2.98 | 2.91 | 2.46 | 200.00 |
| 205.00 | -2.11 | -0.54 | 0.96 | 2.02 | 3.06 | 2.63 | 2.98 | 205.00 |
| 210.00 | -2.20 | -0.90 | 0.39 | 1.32 | 2.93 | 2.53 | 3.21 | 210.00 |
| 215.00 | -2.15 | -1.15 | 0.12 | 0.68 | 2.66 | 2.37 | 3.19 | 215.00 |
| 220.00 | -2.04 | -1.49 | -0.03 | 0.29 | 2.36 | 2.15 | 3.08 | 220.00 |
| 225.00 | -1.94 | -1.78 | -0.14 | 0.17 | 2.13 | 1.95 | 2.95 | 225.00 |
| 230.00 | -1.85 | -1.99 | -0.31 | 0.20 | 2.19 | 1.86 | 2.91 | 230.00 |
| 235.00 | -1.80 | -2.13 | -0.54 | 0.29 | 2.40 | 1.97 | 2.95 | 235.00 |
| 240.00 | -1.78 | -2.21 | -0.79 | 0.37 | 2.65 | 2.21 | 3.07 | 240.00 |
| 245.00 | -1.81 | -2.26 | -0.98 | 0.43 | 2.84 | 2.50 | 3.24 | 245.00 |
| 250.00 | -1.88 | -2.27 | -1.11 | 0.45 | 2.97 | 2.72 | 3.42 | 250.00 |
| 255.00 | -1.94 | -2.29 | -0.96 | 0.33 | 3.06 | 2.80 | 3.61 | 255.00 |
| 260.00 | -1.94 | -2.32 | -0.88 | 0.12 | 3.11 | 2.84 | 3.81 | 260.00 |
| 265.00 | -1.93 | -2.29 | -0.88 | -0.03 | 3.13 | 2.87 | 4.00 | 265.00 |
| 270.00 | -1.94 | -2.18 | -0.91 | -0.13 | 3.13 | 2.91 | 4.16 | 270.00 |
| 275.00 | -1.95 | -2.14 | -0.95 | -0.25 | 3.16 | 2.99 | 4.28 | 275.00 |
| 280.00 | -1.95 | -2.13 | -1.00 | -0.27 | 3.19 | 3.10 | 4.36 | 280.00 |
| 285.00 | -1.72 | -2.11 | -1.08 | -0.18 | 3.27 | 3.19 | 4.39 | 285.00 |
| 290.00 | -1.54 | -2.06 | -1.09 | -0.10 | 3.25 | 3.28 | 4.42 | 290.00 |
| 295.00 | -1.49 | -2.15 | -1.06 | -0.07 | 3.26 | 3.38 | 4.44 | 295.00 |
| 300.00 | -1.49 | -2.17 | -0.99 | -0.05 | 3.24 | 3.46 | 4.47 | 300.00 |
| 305.00 | -1.49 | -2.06 | -0.89 | -0.02 | 3.19 | 3.45 | 4.48 | 305.00 |
| 310.00 | -1.47 | -1.97 | -0.76 | 0.07 | 3.11 | 3.39 | 4.47 | 310.00 |
| 315.00 | -1.09 | -1.96 | -0.65 | 0.04 | 3.06 | 3.36 | 4.43 | 315.00 |
| 320.00 | -0.74 | -1.91 | -0.62 | -0.01 | 3.27 | 3.40 | 4.43 | 320.00 |
| 325.00 | -0.62 | -1.89 | -0.68 | -0.03 | 3.27 | 3.53 | 4.51 | 325.00 |
| 330.00 | -0.61 | -1.27 | -0.77 | -1.11 | 3.00 | 3.66 | 4.41 | 330.00 |
| 335.00 | -0.47 | -1.03 | -0.73 | -1.05 | 2.09 | 3.08 | 3.83 | 335.00 |
| 340.00 | -0.26 | -0.83 | -0.89 | -0.35 | 1.04 | 1.01 | 2.43 | 340.00 |
| 345.00 | -0.62 | -1.01 | -1.77 | 0.04 | 0.49 | 0.09 | 0.32 | 345.00 |
| 350.00 | -1.09 | -3.06 | -3.65 | 1.78 | 1.14 | -0.75 | -1.80 | 350.00 |
| 355.00 | -1.40 | -5.49 | -4.89 | -0.14 | 1.95 | -0.84 | -2.80 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.26 | 0.99 | -0.14 | -1.13 | -2.09 | -3.47 | -3.40 | |

# BLADE LOADS

TEST 497 CNTR NO. 418 T.C.No. 28 C.R. 26

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -2.35 | -3.75 | -3.61 | -4.59 | 0.73 | 4.41 | 2.65 | 3.[illegible] |
| 5.00 | -3.26 | -4.76 | -4.56 | -3.27 | -0.98 | 1.80 | 0.31 | [illegible] |
| 10.00 | -2.76 | -4.53 | -4.29 | -2.67 | -1.82 | 0.14 | -0.23 | 10.00 |
| 15.00 | -1.44 | -3.32 | -3.93 | -2.05 | -1.78 | -0.10 | -0.62 | 15.00 |
| 20.00 | -0.65 | -2.73 | -3.65 | -1.64 | -0.42 | 0.78 | 0.01 | 20.00 |
| 25.00 | 0.18 | -3.09 | -2.90 | -1.42 | 0.11 | 1.54 | 0.88 | 25.00 |
| 30.00 | -0.32 | -2.96 | -1.89 | -0.57 | 0.73 | 2.26 | 1.22 | 30.00 |
| 35.00 | -1.12 | -2.37 | -0.96 | 0.66 | 1.58 | 2.94 | 1.67 | 35.00 |
| 40.00 | -0.69 | -1.76 | -0.06 | 1.66 | 2.71 | 3.91 | 2.20 | 40.00 |
| 45.00 | -0.39 | -1.36 | 0.36 | 2.46 | 2.64 | 3.95 | 2.91 | 45.00 |
| 50.00 | -0.49 | -1.07 | 0.64 | 3.23 | 3.02 | 4.31 | 3.70 | 50.00 |
| 55.00 | -0.44 | -0.87 | 0.98 | 3.80 | 3.43 | 4.67 | 4.38 | 55.00 |
| 60.00 | -0.29 | -0.75 | 1.34 | 4.27 | 3.77 | 4.91 | 4.84 | 60.00 |
| 65.00 | -0.20 | -0.71 | 1.60 | 4.63 | 3.81 | 4.62 | 5.46 | 65.00 |
| 70.00 | -0.21 | -0.67 | 1.71 | 4.37 | 3.48 | 4.27 | 5.15 | 70.00 |
| 75.00 | -0.07 | -0.57 | 1.47 | 4.14 | 3.05 | 4.03 | 5.03 | 75.00 |
| 80.00 | 0.03 | -0.32 | 1.28 | 3.97 | 2.33 | 4.76 | 5.79 | 80.00 |
| 85.00 | 0.01 | 0.06 | 1.00 | 3.68 | 1.46 | 3.39 | -1.09 | 85.00 |
| 90.00 | 0.11 | 0.47 | 0.86 | 2.96 | 0.08 | 0.06 | -3.71 | 90.00 |
| 95.00 | 0.63 | 0.96 | 0.93 | 2.27 | -2.12 | -4.61 | -5.32 | 95.00 |
| 100.00 | 0.87 | 1.43 | 1.28 | 1.42 | -5.23 | -8.41 | -6.45 | 100.00 |
| 105.00 | 1.39 | 1.42 | 1.62 | 0.91 | -7.47 | -10.97 | -6.94 | 105.00 |
| 110.00 | 1.89 | 2.20 | 1.85 | 0.05 | -8.00 | -12.33 | -7.09 | 110.00 |
| 115.00 | 2.29 | 2.59 | 2.06 | .75 | -7.82 | -12.97 | -8.42 | 115.00 |
| 120.00 | 2.59 | 3.09 | 2.20 | .93 | -7.70 | -12.96 | -11.64 | 120.00 |
| 125.00 | 2.84 | 3.59 | 2.08 | 1.77 | -8.29 | -12.70 | -13.16 | 125.00 |
| 130.00 | 3.08 | 4.00 | 1.77 | -4.05 | -8.43 | -11.73 | -12.49 | 130.00 |
| 135.00 | 3.32 | 4.24 | 1.38 | -4.13 | -8.45 | -10.33 | -10.89 | 135.00 |
| 140.00 | 3.48 | 4.43 | 0.93 | -3.65 | -8.14 | -9.51 | -10.13 | 140.00 |
| 145.00 | 3.56 | 4.62 | 0.68 | -3.02 | -7.54 | -8.69 | -9.21 | 145.00 |
| 150.00 | 3.68 | 4.83 | 0.99 | -2.31 | -6.56 | -7.72 | -8.14 | 150.00 |
| 155.00 | 3.81 | 5.09 | 1.41 | -1.60 | -5.22 | -6.41 | -6.93 | 155.00 |
| 160.00 | 3.87 | 5.10 | 2.36 | -0.41 | -3.85 | -4.89 | -5.48 | 160.00 |
| 165.00 | 3.81 | 5.61 | 3.12 | 0.91 | -2.57 | -3.69 | -3.85 | 165.00 |
| 170.00 | 3.63 | 5.99 | 3.76 | 1.28 | -1.45 | -2.37 | -2.90 | 170.00 |
| 175.00 | 3.32 | 5.99 | 4.22 | 1.92 | -0.58 | -0.93 | -1.83 | 175.00 |
| 180.00 | 2.90 | 4.72 | 4.38 | 2.34 | 0.23 | 0.06 | -0.38 | 180.00 |
| 185.00 | 2.35 | 5.19 | 4.18 | 2.59 | 0.89 | 0.82 | 0.35 | 185.00 |
| 190.00 | 1.56 | 4.31 | 3.72 | 2.44 | 1.43 | 1.36 | 0.98 | 190.00 |
| 195.00 | 0.68 | 3.27 | 3.11 | 2.16 | 1.74 | 1.71 | 1.42 | 195.00 |
| 200.00 | -0.09 | 2.17 | 2.37 | 1.77 | 1.86 | 1.84 | 1.57 | 200.00 |
| 205.00 | -0.55 | 1.13 | 1.63 | 1.27 | 1.85 | 1.84 | 1.71 | 205.00 |
| 210.00 | -0.87 | 0.23 | 0.94 | 1.44 | 1.80 | 1.76 | 1.79 | 210.00 |
| 215.00 | -1.13 | -0.38 | 0.40 | 1.42 | 1.73 | 1.67 | 1.83 | 215.00 |
| 220.00 | -1.36 | -0.74 | 0.02 | 0.92 | 1.66 | 1.58 | 1.86 | 220.00 |
| 225.00 | -1.50 | -1.05 | -0.22 | 0.16 | 1.61 | 1.67 | 1.99 | 225.00 |
| 230.00 | -1.56 | -1.33 | -0.44 | -0.12 | 1.59 | 1.67 | 1.96 | 230.00 |
| 235.00 | -1.58 | -1.56 | -0.65 | -0.44 | 1.58 | 1.61 | 2.05 | 235.00 |
| 240.00 | -1.59 | -1.72 | -0.84 | -0.69 | 1.60 | 1.62 | 2.17 | 240.00 |
| 245.00 | -1.59 | -1.89 | -1.02 | -0.87 | 1.62 | 1.51 | 2.30 | 245.00 |
| 250.00 | -1.60 | -2.00 | -1.23 | -0.92 | 1.67 | 1.61 | 2.44 | 250.00 |
| 255.00 | -1.61 | -2.04 | -1.38 | -0.85 | 1.74 | 1.72 | 2.57 | 255.00 |
| 260.00 | -1.57 | -2.12 | -1.47 | -0.66 | 1.81 | 1.82 | 2.69 | 260.00 |
| 265.00 | -1.53 | -2.17 | -1.54 | -0.47 | 1.89 | 1.93 | 2.82 | 265.00 |
| 270.00 | -1.56 | -2.14 | -1.47 | -0.72 | 1.97 | 2.02 | 2.90 | 270.00 |
| 275.00 | -1.59 | -2.16 | -1.37 | -0.92 | 2.05 | 2.13 | 2.98 | 275.00 |
| 280.00 | -1.55 | -2.09 | -1.36 | -0.89 | 2.14 | 2.25 | 3.09 | 280.00 |
| 283.00 | -1.42 | -2.02 | -1.32 | -0.91 | 2.23 | 2.40 | 3.27 | 283.00 |
| 290.00 | -1.30 | -1.97 | -1.48 | -0.82 | 2.34 | 2.58 | 3.34 | 290.00 |
| 295.00 | -1.27 | -1.96 | -1.42 | -0.73 | 2.46 | 2.81 | 3.55 | 295.00 |
| 300.00 | -1.40 | -1.96 | -1.37 | -0.55 | 2.60 | 3.08 | 3.79 | 300.00 |
| 305.00 | -1.38 | -1.93 | -1.31 | -0.41 | 2.74 | 3.36 | 4.08 | 305.00 |
| 310.00 | -1.29 | -1.85 | -1.20 | -0.27 | 2.87 | 3.61 | 4.24 | 310.00 |
| 315.00 | -1.25 | -1.79 | -1.34 | -0.18 | 2.95 | 3.78 | 4.43 | 315.00 |
| 320.00 | -1.21 | -1.78 | -1.44 | -0.16 | 2.96 | 3.83 | 4.24 | 320.00 |
| 325.00 | -1.13 | -1.73 | -1.77 | -0.22 | 2.96 | 3.88 | 4.05 | 325.00 |
| 330.00 | -1.08 | -1.44 | 2.19 | -0.29 | 2.82 | 3.64 | 3.68 | 330.00 |
| 335.00 | -1.10 | -1.58 | -2.51 | -0.32 | 2.31 | 3.13 | 3.13 | 335.00 |
| 340.00 | -1.18 | -1.76 | -2.48 | -0.15 | 2.07 | 2.79 | 2.80 | 340.00 |
| 345.00 | -1.25 | -2.13 | -2.21 | -0.57 | 2.06 | 2.73 | 2.44 | 345.00 |
| 350.00 | -1.10 | -2.39 | -2.09 | -1.04 | 2.13 | 2.84 | 2.34 | 350.00 |
| 355.00 | -1.04 | -2.73 | -2.43 | -1.75 | 1.56 | 2.36 | 2.12 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 1.17 | 1.97 | 2.00 | 1.99 | 0.09 | 0.14 | -0.01 | |

# BLADE LOADS

TEST 497 CNTR NO. 373 T.C.-. 29 C.R. 27

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.19 | -4.88 | -5.77 | -2.01 | -0.24 | 0.92 | -0.80 | 0.0 |
| 5.00 | -1.53 | -2.76 | -7.18 | -1.08 | 0.40 | 0.85 | 0.35 | 5.33 |
| 10.00 | -1.01 | -0.73 | -7.36 | -2.44 | -3.63 | 0.10 | -0.36 | 10.33 |
| 15.00 | -0.64 | -1.55 | -6.03 | -3.63 | -1.16 | -0.98 | -1.58 | 15.33 |
| 20.00 | -1.25 | -3.31 | -3.76 | -2.88 | -0.98 | -0.23 | -1.34 | 20.00 |
| 25.00 | -1.88 | -3.04 | -1.70 | -1.25 | 0.21 | 1.24 | -0.39 | 25.00 |
| 30.00 | -1.94 | -3.60 | -0.43 | 0.65 | 1.54 | 2.64 | 0.91 | 30.00 |
| 35.00 | -2.21 | -2.80 | 0.73 | 2.18 | 2.44 | 3.41 | 1.82 | 35.33 |
| 40.00 | -2.01 | -1.92 | 0.66 | 3.21 | 3.73 | 4.35 | 3.73 | 43.33 |
| 45.00 | -1.14 | -1.25 | 1.55 | 3.96 | 3.98 | 5.70 | 5.81 | 45.00 |
| 50.00 | -0.13 | -0.14 | 2.05 | 4.55 | 4.46 | 6.66 | 6.36 | 50.00 |
| 55.00 | 0.42 | -0.73 | 2.03 | 4.09 | 4.63 | 6.99 | 5.49 | 55.00 |
| 60.00 | 0.43 | -0.78 | 1.97 | 5.71 | 4.92 | 6.60 | 4.48 | 60.00 |
| 65.00 | 0.17 | -0.96 | 1.91 | 6.62 | 5.11 | 5.98 | 3.79 | 65.33 |
| 70.00 | -0.08 | -1.02 | 1.42 | 3.76 | 3.84 | 2.79 | 0.00 | 70.33 |
| 75.00 | -0.31 | -0.93 | 0.65 | 1.11 | 1.48 | 0.89 | -3.55 | 75.33 |
| 80.00 | -0.18 | -0.71 | 0.40 | 2.95 | 1.34 | -3.00 | -4.19 | 80.00 |
| 85.00 | -0.15 | -0.62 | 0.48 | 3.66 | 0.17 | -6.80 | -5.68 | 85.00 |
| 90.00 | 0.24 | 0.08 | 1.09 | 4.46 | -6.06 | -6.53 | -7.29 | 90.00 |
| 95.00 | 0.89 | 0.79 | 1.93 | 5.61 | -11.33 | -9.66 | -5.32 | 95.33 |
| 100.00 | 1.60 | 1.60 | 2.91 | 4.65 | -10.61 | -8.99 | -2.19 | 100.33 |
| 105.00 | 2.31 | 2.54 | 3.67 | -1.10 | -7.66 | -2.44 | 0.14 | 105.00 |
| 110.00 | 2.99 | 3.45 | 3.96 | -4.12 | -5.67 | 0.50 | 0.73 | 110.00 |
| 115.00 | 3.59 | 4.35 | 3.90 | -4.18 | -5.41 | -2.84 | -3.57 | 115.00 |
| 120.00 | 4.09 | 5.17 | 3.05 | -3.91 | -5.67 | -6.65 | -3.66 | 120.00 |
| 125.00 | 4.48 | 5.77 | -0.19 | -4.25 | -8.59 | -7.95 | -7.58 | 125.33 |
| 130.00 | 4.77 | 6.07 | -1.27 | -4.89 | -10.72 | -8.99 | -8.05 | 130.33 |
| 135.00 | 4.96 | 6.13 | -1.04 | -5.06 | -8.65 | -12.68 | -10.70 | 135.00 |
| 140.00 | 5.08 | 5.99 | -0.43 | -4.71 | -7.87 | -11.82 | -12.29 | 140.00 |
| 145.00 | 5.09 | 5.69 | -0.17 | -4.14 | -7.82 | -10.42 | -11.15 | 145.00 |
| 150.00 | 4.97 | 5.39 | 0.23 | -3.39 | -7.30 | -9.24 | -9.89 | 150.00 |
| 155.00 | 4.71 | 4.91 | 0.88 | -2.67 | -5.98 | -8.28 | -8.93 | 155.33 |
| 160.00 | 4.32 | 5.34 | 1.71 | -1.63 | -4.63 | -6.80 | -7.66 | 160.33 |
| 165.00 | 3.82 | 5.97 | 2.61 | -0.55 | -3.12 | -4.87 | -5.45 | 165.00 |
| 170.00 | 3.20 | 6.36 | 3.51 | 0.27 | -1.70 | -3.11 | -3.60 | 170.00 |
| 175.00 | 2.49 | 6.20 | 4.17 | 0.96 | -0.50 | -1.54 | -1.94 | 175.00 |
| 180.00 | 1.72 | 5.58 | 4.37 | 1.73 | 0.62 | -0.14 | -0.57 | 180.00 |
| 185.00 | 0.90 | 4.68 | 4.03 | 2.21 | 1.48 | 1.03 | 0.59 | 185.33 |
| 190.00 | -0.24 | 3.91 | 3.33 | 2.19 | 2.13 | 1.79 | 1.29 | 190.33 |
| 195.00 | -1.11 | 3.27 | 2.49 | 1.99 | 2.51 | 2.14 | 1.86 | 195.00 |
| 200.00 | -1.62 | 2.12 | 1.63 | 1.74 | 2.65 | 2.23 | 2.27 | 200.00 |
| 205.00 | -1.92 | -0.46 | 0.89 | 1.47 | 2.66 | 2.25 | 2.40 | 205.00 |
| 210.00 | -2.11 | -1.14 | 0.36 | 1.08 | 2.65 | 2.27 | 2.47 | 210.00 |
| 215.00 | -2.21 | -1.42 | 0.04 | 0.78 | 2.60 | 2.29 | 2.52 | 215.00 |
| 220.00 | -2.15 | -1.43 | -0.19 | 0.57 | 2.57 | 2.29 | 2.60 | 220.00 |
| 225.00 | -1.97 | -1.49 | -0.25 | 0.46 | 2.60 | 2.29 | 2.70 | 225.00 |
| 230.00 | -1.79 | -2.10 | -0.44 | 0.30 | 2.68 | 2.37 | 2.82 | 230.00 |
| 235.00 | -1.62 | -2.19 | -0.68 | 0.19 | 2.80 | 2.49 | 2.93 | 235.00 |
| 240.00 | -1.55 | -2.20 | -0.93 | 0.00 | 2.91 | 2.63 | 3.01 | 240.00 |
| 245.00 | -1.55 | -2.15 | -1.11 | -0.12 | 2.94 | 2.71 | 3.11 | 245.00 |
| 250.00 | -1.56 | -2.10 | -1.18 | -0.31 | 2.86 | 2.73 | 3.22 | 250.00 |
| 255.00 | -1.55 | -2.09 | -1.16 | -0.49 | 2.92 | 2.71 | 3.34 | 255.00 |
| 260.00 | -1.55 | -2.06 | -1.12 | -0.59 | 2.85 | 2.67 | 3.44 | 260.00 |
| 265.00 | -1.58 | -2.02 | -1.06 | -0.62 | 2.79 | 2.66 | 3.50 | 265.00 |
| 270.00 | -1.66 | -1.99 | -1.01 | -0.62 | 2.80 | 2.71 | 3.54 | 270.00 |
| 275.00 | -1.73 | -2.00 | -0.98 | -0.63 | 2.86 | 2.80 | 3.61 | 275.00 |
| 280.00 | -1.71 | -2.04 | -0.96 | -0.57 | 2.85 | 2.88 | 3.62 | 280.00 |
| 285.00 | -1.66 | -2.11 | -0.96 | -0.43 | 2.85 | 2.85 | 3.64 | 285.00 |
| 290.00 | -1.65 | -2.16 | -0.95 | -0.27 | 2.82 | 2.84 | 3.73 | 290.00 |
| 295.00 | -1.64 | -2.18 | -0.95 | -0.21 | 2.87 | 2.93 | 3.78 | 295.00 |
| 300.00 | -1.52 | -2.14 | -0.93 | -0.20 | 2.93 | 2.99 | 3.79 | 300.00 |
| 305.00 | -1.38 | -2.03 | -0.91 | -0.15 | 2.98 | 2.96 | 3.83 | 305.00 |
| 310.00 | -1.35 | -1.97 | -0.91 | -0.17 | 2.99 | 2.97 | 3.86 | 310.00 |
| 315.00 | -1.05 | -1.91 | -0.91 | -0.11 | 3.27 | 3.03 | 3.88 | 315.00 |
| 320.00 | -0.72 | -1.94 | -0.90 | -0.57 | 3.21 | 3.03 | 3.83 | 320.00 |
| 325.00 | -0.61 | -1.79 | -0.86 | -1.00 | 3.01 | 3.02 | 3.71 | 325.00 |
| 330.00 | -0.81 | -1.49 | -0.78 | -1.50 | 2.57 | 3.22 | 3.95 | 330.00 |
| 335.00 | -0.89 | -1.36 | -0.53 | -1.74 | 1.79 | 2.57 | 2.61 | 335.00 |
| 340.00 | -0.81 | -1.30 | -0.48 | -1.53 | 0.65 | 1.26 | 1.31 | 340.00 |
| 345.00 | -0.95 | -2.14 | -0.89 | -0.43 | -0.26 | -0.35 | -0.48 | 345.00 |
| 350.00 | -1.62 | -3.65 | -1.70 | -0.29 | -0.93 | -1.74 | -2.14 | 350.00 |
| 355.00 | -2.42 | -5.14 | -3.27 | -1.34 | -1.69 | -2.38 | -3.04 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.48 | 1.01 | 0.39 | -0.48 | -1.18 | .96 | -2.72 | |

# BLADE LOADS

TEST 497 CNTR NO. 394 T.C.N. 30 C.R. 28

SPAN STATION

| DEG | 52.0 | 79.8 | 119.7 | 159.5 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -2.51 | -9.13 | -6.63 | -3.63 | -0.44 | 0.27 | -1.11 | 0.0 |
| 5.00 | -1.7[illegible] | -2.78 | -7.44 | -4.88 | -0.29 | 0.67 | -0.95 | 5.00 |
| 10.00 | -2.01 | -0.59 | -7.13 | -5.36 | -0.95 | -0.53 | -1.74 | 10.00 |
| 15.00 | -1.99 | -1.46 | -5.87 | -4.52 | -1.92 | -1.67 | -2.76 | 15.00 |
| 20.00 | -0.98 | -3.42 | -3.90 | -3.56 | -2.14 | -1.92 | -3.24 | 20.00 |
| 25.00 | -0.73 | -4.39 | -1.99 | -1.98 | -0.87 | -0.77 | -2.29 | 25.00 |
| 30.00 | -1.79 | -3.81 | -0.97 | -0.01 | 0.71 | 1.01 | -0.67 | 30.00 |
| 35.00 | -2.46 | -3.05 | -0.72 | 1.73 | 2.00 | 2.72 | 1.49 | 35.00 |
| 40.00 | -1.93 | -2.43 | -0.18 | 3.52 | 3.04 | 4.26 | 4.02 | 40.00 |
| 45.00 | -1.06 | -1.47 | 0.78 | 3.95 | 3.72 | 5.49 | 5.41 | 45.00 |
| 50.00 | -0.41 | -1.46 | 1.43 | 4.59 | 4.23 | 6.37 | 5.42 | 50.00 |
| 55.00 | -0.07 | -1.27 | 1.58 | 4.83 | 4.52 | 6.78 | 4.93 | 55.00 |
| 60.00 | -0.01 | -1.16 | 1.72 | 4.59 | 4.88 | 4.93 | 4.88 | 60.00 |
| 65.00 | -0.05 | -0.93 | 1.96 | 4.15 | 4.82 | 3.78 | 2.25 | 65.00 |
| 70.00 | -0.10 | -0.65 | 1.78 | 4.06 | 3.40 | 2.30 | -1.26 | 70.00 |
| 75.00 | -0.14 | -0.42 | 1.32 | 5.29 | 0.83 | 0.39 | -0.01 | 75.00 |
| 80.00 | -0.14 | -0.43 | 1.05 | 6.96 | 0.68 | -0.13 | -1.13 | 80.00 |
| 85.00 | 0.03 | -0.44 | 1.30 | 7.83 | -0.45 | -1.98 | -4.76 | 85.00 |
| 90.00 | 0.44 | -0.04 | 1.67 | 7.34 | -7.41 | -5.46 | -5.76 | 90.00 |
| 95.00 | 1.10 | 0.71 | 2.25 | 7.64 | -7.84 | -7.46 | -3.80 | 95.00 |
| 100.00 | 1.76 | 1.64 | 2.98 | 4.68 | -6.56 | -6.33 | -1.15 | 100.00 |
| 105.00 | 2.38 | 2.65 | 3.42 | -0.21 | -5.64 | -3.38 | 0.22 | 105.00 |
| 110.00 | 3.01 | 3.51 | 3.24 | -4.91 | -4.85 | -0.87 | -1.07 | 110.00 |
| 115.00 | 3.71 | 4.23 | 2.46 | -7.07 | -6.89 | -0.88 | -3.10 | 115.00 |
| 120.00 | 4.27 | 4.84 | 0.93 | -9.44 | -8.24 | -2.56 | -4.40 | 120.00 |
| 125.00 | 4.61 | 5.34 | -0.95 | -6.77 | -7.26 | -0.17 | -3.93 | 125.00 |
| 130.00 | 4.83 | 5.69 | -1.83 | -4.85 | -10.93 | -9.66 | -8.64 | 130.00 |
| 135.00 | 4.[illegible] | 5.84 | -1.21 | -3.88 | -9.67 | -11.61 | -9.74 | 135.00 |
| 140.00 | 5.15 | 5.79 | -0.41 | -3.42 | -7.33 | -11.83 | -10.90 | 140.00 |
| 145.00 | 5.23 | 5.45 | 0.[illegible] | -3.48 | -6.51 | -10.35 | -11.10 | 145.00 |
| 150.00 | 5.12 | 5.14 | 0.47 | -3.04 | -5.86 | -8.47 | -9.24 | 150.00 |
| 155.00 | 4.79 | 5.24 | 1.01 | -2.32 | -5.42 | -7.45 | -8.10 | 155.00 |
| 160.00 | 4.26 | 5.77 | 1.85 | -1.32 | -4.42 | -6.47 | -6.52 | 160.00 |
| 165.00 | 3.64 | 6.71 | 2.76 | -0.03 | -3.21 | -4.95 | -5.41 | 165.00 |
| 170.00 | 2.97 | 8.56 | 3.72 | 0.32 | -1.94 | -3.25 | -3.89 | 170.00 |
| 175.00 | 2.25 | 5.32 | 4.47 | 1.22 | -0.72 | -1.69 | -2.25 | 175.00 |
| 180.00 | 1.47 | 5.65 | 4.65 | 2.32 | 0.40 | -0.37 | -0.83 | 180.00 |
| 185.00 | 0.44 | 4.30 | 4.30 | 2.44 | 1.22 | 0.62 | 0.28 | 185.00 |
| 190.00 | -0.58 | 2.61 | 3.61 | 2.33 | 1.95 | 1.46 | 1.15 | 190.00 |
| 195.00 | -1.29 | 1.23 | 2.63 | 2.02 | 2.46 | 1.93 | 1.74 | 195.00 |
| 200.00 | -1.66 | -0.33 | 1.66 | 1.70 | 2.69 | 2.17 | 2.11 | 200.00 |
| 205.00 | -1.85 | -0.69 | 0.84 | 1.28 | 2.72 | 2.20 | 2.33 | 205.00 |
| 210.00 | -2.02 | -1.06 | 0.39 | 0.78 | 2.63 | 2.13 | 2.44 | 210.00 |
| 215.00 | -2.10 | -1.24 | 0.08 | 0.29 | 2.53 | 2.06 | 2.52 | 215.00 |
| 220.00 | -1.97 | -1.47 | -0.13 | 0.04 | 2.49 | 1.98 | 2.54 | 220.00 |
| 225.00 | -1.92 | -1.69 | -0.26 | 0.00 | 2.49 | 1.97 | 2.60 | 225.00 |
| 230.00 | -1.67 | -1.91 | -0.39 | 0.00 | 2.39 | 2.02 | 2.67 | 230.00 |
| 235.00 | -1.58 | -2.07 | -0.53 | 0.00 | 2.48 | 2.13 | 2.77 | 235.00 |
| 240.00 | -1.56 | -2.13 | -0.67 | -0.31 | 2.59 | 2.25 | 2.86 | 240.00 |
| 245.00 | -1.53 | -2.12 | -0.80 | -0.32 | 2.71 | 2.36 | 2.96 | 245.00 |
| 250.00 | -1.54 | -2.13 | -0.82 | -0.32 | 2.79 | 2.41 | 3.08 | 250.00 |
| 255.00 | -1.56 | -2.11 | -0.78 | -0.15 | 2.85 | 2.48 | 3.21 | 255.00 |
| 260.00 | -1.53 | -2.09 | -0.73 | -0.24 | 2.87 | 2.55 | 3.33 | 260.00 |
| 265.00 | -1.53 | -2.09 | -0.72 | -0.27 | 2.90 | 2.62 | 3.46 | 265.00 |
| 270.00 | -1.52 | -1.99 | -0.72 | -0.32 | 2.93 | 2.69 | 3.59 | 270.00 |
| 275.00 | -1.52 | -1.99 | -0.72 | -0.34 | 2.98 | 2.78 | 3.70 | 275.00 |
| 280.00 | -1.[illegible] | -1.97 | -0.75 | -0.39 | 3.03 | 2.87 | 3.77 | 280.00 |
| 285.00 | -1.39 | -1.87 | -0.78 | -0.33 | 3.08 | 2.94 | 3.84 | 285.00 |
| 290.00 | -1.30 | -1.83 | -0.77 | -0.25 | 3.13 | 3.00 | 3.89 | 290.00 |
| 295.00 | -1.31 | -2.05 | -0.75 | -0.24 | 3.17 | 3.10 | 3.93 | 295.00 |
| 300.00 | -1.31 | -2.16 | -0.72 | -0.22 | 3.20 | 3.22 | 3.97 | 300.00 |
| 305.00 | -1.19 | -2.62 | -0.69 | -0.21 | 3.20 | 3.34 | 4.04 | 305.00 |
| 310.00 | -1.21 | -1.89 | -0.66 | -0.25 | 3.16 | 3.38 | 4.07 | 310.00 |
| 315.00 | -1.14 | -1.67 | -0.61 | -0.31 | 3.07 | 3.45 | 4.04 | 315.00 |
| 320.00 | -0.83 | -1.45 | -0.58 | -0.45 | 2.95 | 3.52 | 3.93 | 320.00 |
| 325.00 | -0.43 | -1.26 | -0.55 | -0.36 | 2.73 | 3.43 | 3.69 | 325.00 |
| 330.00 | -0.16 | -1.20 | -0.48 | -1.25 | 2.28 | 3.29 | 3.17 | 330.00 |
| 335.00 | -0.16 | -1.70 | -0.43 | -1.69 | 1.54 | 2.33 | 2.36 | 335.00 |
| 340.00 | -0.46 | -2.19 | -0.49 | -2.02 | 0.71 | 1.11 | 1.17 | 340.00 |
| 345.00 | -0.75 | -1.92 | -0.93 | 0.19 | 0.20 | -0.14 | -0.23 | 345.00 |
| 350.00 | -1.01 | -2.73 | -2.28 | 0.56 | 0.00 | -0.96 | -1.43 | 350.00 |
| 355.00 | -4.54 | -4.35 | -4.31 | -0.33 | -0.52 | -0.84 | -1.99 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 0.77 | 1.54 | 0.67 | -2.14 | -0.88 | -7.08 | -1.98 | |

# BLADE LOADS

TEST 500 CNTR NO. 570 T.C.N. 31 C.R. 40

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -1.83 | -4.07 | -7.77 | -9.17 | 0.48 | 0.74 | -0.20 | 0.0 |
| 5.00 | -0.59 | -0.35 | -7.38 | -6.60 | -0.09 | 0.71 | 2.80 | 5.00 |
| 10.00 | -1.33 | -0.80 | -4.24 | -4.73 | -1.74 | -0.18 | 0.05 | 10.00 |
| 15.00 | 0.02 | -3.01 | -4.24 | -3.61 | -2.08 | -1.22 | -2.78 | 15.00 |
| 20.00 | -0.43 | -3.48 | -1.56 | -1.38 | -1.22 | -0.17 | -2.71 | 20.00 |
| 25.00 | -2.18 | -3.08 | -0.77 | 1.68 | 0.88 | 1.47 | -0.48 | 25.00 |
| 30.00 | -2.84 | -3.09 | -0.88 | 2.34 | 2.47 | 2.42 | 2.28 | 30.00 |
| 35.00 | -2.12 | -3.11 | -0.91 | 3.28 | 3.78 | 4.35 | 4.15 | 35.00 |
| 40.00 | -2.08 | -2.81 | 0.34 | 3.76 | 4.53 | 4.74 | 4.61 | 40.00 |
| 45.00 | -2.07 | -2.60 | 0.83 | 4.43 | 5.30 | 7.66 | 6.83 | 45.00 |
| 50.00 | -1.04 | -2.09 | 2.35 | 6.66 | 7.84 | 7.64 | 6.81 | 50.00 |
| 55.00 | -0.49 | -2.48 | 2.35 | 7.07 | 8.88 | 8.66 | 7.19 | 55.00 |
| 60.00 | -0.29 | -2.10 | 2.87 | 7.48 | 8.35 | 8.48 | 7.29 | 60.00 |
| 65.00 | -0.86 | -1.84 | 3.12 | 7.87 | 9.18 | 9.66 | -0.84 | 65.00 |
| 70.00 | -0.88 | -0.86 | 3.49 | 8.07 | 9.85 | -0.74 | -0.11 | 70.00 |
| 75.00 | -0.48 | -0.38 | 3.87 | 8.23 | -6.77 | -9.88 | -9.40 | 75.00 |
| 80.00 | -0.30 | 0.14 | 3.05 | 8.46 | -7.74 | -9.10 | -1.49 | 80.00 |
| 85.00 | -0.11 | 0.84 | 4.18 | 8.83 | -0.18 | -7.80 | -2.81 | 85.00 |
| 90.00 | 0.30 | 1.26 | 3.73 | 8.31 | -7.48 | -8.72 | -2.75 | 90.00 |
| 95.00 | 1.40 | 2.00 | 3.61 | 7.84 | -7.06 | -8.32 | -2.26 | 95.00 |
| 100.00 | 2.48 | 3.39 | 3.76 | -9.11 | -8.41 | -8.36 | -0.97 | 100.00 |
| 105.00 | 3.08 | 3.38 | 3.80 | -6.71 | -7.33 | -8.04 | 1.15 | 105.00 |
| 110.00 | 3.69 | 3.68 | -0.19 | -11.44 | -6.68 | -6.72 | -1.09 | 110.00 |
| 115.00 | 3.81 | 3.63 | -2.24 | -13.36 | -7.07 | -8.23 | -4.47 | 115.00 |
| 120.00 | 3.88 | 3.76 | -6.67 | -12.60 | -10.83 | -8.82 | -10.81 | 120.00 |
| 125.00 | 4.19 | 4.36 | -6.50 | -11.01 | -14.06 | -11.84 | -10.86 | 125.00 |
| 130.00 | 4.34 | 4.47 | -3.08 | -9.24 | -14.38 | -12.84 | -11.69 | 130.00 |
| 135.00 | 4.81 | 4.83 | -1.11 | -6.73 | -11.38 | -12.68 | -12.17 | 135.00 |
| 140.00 | 4.68 | 5.19 | 0.39 | -6.02 | -7.81 | -10.67 | -10.89 | 140.00 |
| 145.00 | 4.60 | 5.30 | 1.83 | -3.66 | -6.73 | -7.98 | -7.88 | 145.00 |
| 150.00 | 5.81 | 4.60 | 2.87 | 0.05 | -4.10 | -6.63 | -6.61 | 150.00 |
| 155.00 | 5.76 | 7.05 | 3.80 | 1.21 | -2.63 | -3.68 | -4.87 | 155.00 |
| 160.00 | 6.76 | 7.76 | 4.87 | 2.14 | -1.21 | -3.17 | -3.27 | 160.00 |
| 165.00 | 6.04 | 8.08 | 5.83 | 3.04 | -0.37 | -1.96 | -2.61 | 165.00 |
| 170.00 | 7.06 | 7.93 | 6.27 | 3.71 | 0.49 | -0.08 | -0.65 | 170.00 |
| 175.00 | 7.05 | 8.47 | 6.80 | 4.07 | 1.30 | 0.88 | 0.20 | 175.00 |
| 180.00 | 7.86 | 8.47 | 6.84 | 4.36 | 1.66 | 1.66 | 0.83 | 180.00 |
| 185.00 | 8.22 | 8.15 | 6.80 | 4.30 | 2.37 | 1.76 | 1.22 | 185.00 |
| 190.00 | 7.29 | 7.96 | 6.64 | 3.85 | 2.68 | 1.92 | 1.60 | 190.00 |
| 195.00 | 7.79 | 7.67 | 6.83 | 3.84 | 2.77 | 2.34 | 1.84 | 195.00 |
| 200.00 | 7.58 | 7.33 | 6.31 | 3.33 | 2.67 | 2.08 | 2.23 | 200.00 |
| 205.00 | 7.86 | 7.87 | 6.40 | 3.66 | 2.66 | 1.87 | 2.36 | 205.00 |
| 210.00 | 7.56 | 7.06 | 6.14 | 2.80 | 2.76 | 1.68 | 2.39 | 210.00 |
| 215.00 | 7.70 | 7.14 | 6.14 | 2.86 | 2.84 | 1.88 | 2.63 | 215.00 |
| 220.00 | 7.79 | 7.43 | 6.28 | 2.30 | 2.80 | 1.80 | 2.68 | 220.00 |
| 225.00 | 7.81 | 7.47 | 6.23 | 2.33 | 2.83 | 1.78 | 2.63 | 225.00 |
| 230.00 | 7.63 | 7.74 | 6.00 | 2.43 | 2.82 | 1.81 | 2.93 | 230.00 |
| 235.00 | 7.66 | 7.83 | 6.22 | 2.50 | 2.93 | 1.88 | 2.64 | 235.00 |
| 240.00 | 7.87 | 7.84 | 6.08 | 2.58 | 2.78 | 1.84 | 2.81 | 240.00 |
| 245.00 | 7.67 | 7.88 | 6.04 | 2.61 | 2.81 | 2.08 | 2.73 | 245.00 |
| 250.00 | 7.78 | 7.88 | 6.09 | 2.51 | 2.71 | 2.18 | 2.84 | 250.00 |
| 255.00 | 7.76 | 7.94 | 6.01 | 2.5 | 2.76 | 2.20 | 3.03 | 255.00 |
| 260.00 | 7.88 | 7.86 | 6.03 | 2.18 | 2.77 | 2.38 | 3.23 | 260.00 |
| 265.00 | 7.87 | 7.78 | 6.06 | 2.07 | 2.74 | 2.63 | 3.38 | 265.00 |
| 270.00 | 7.82 | 7.84 | 6.03 | 2.03 | 2.78 | 2.68 | 3.48 | 270.00 |
| 275.00 | 7.80 | 7.86 | 6.07 | 2.14 | 2.76 | 2.68 | 3.66 | 275.00 |
| 280.00 | 7.74 | 7.84 | 6.11 | 2.16 | 2.76 | 2.63 | 3.60 | 280.00 |
| 285.00 | 7.81 | 7.87 | 6.18 | 2.14 | 2.72 | 2.68 | 3.67 | 285.00 |
| 290.00 | 7.80 | 7.81 | 6.19 | 2.06 | 2.70 | 2.67 | 3.71 | 290.00 |
| 295.00 | 7.78 | 7.86 | 6.01 | 2.02 | 2.67 | 2.63 | 3.79 | 295.00 |
| 300.00 | 7.71 | 7.80 | 6.02 | 2.06 | 2.64 | 2.62 | 3.71 | 300.00 |
| 305.00 | 7.78 | 7.74 | 6.04 | 2.13 | 2.67 | 2.72 | 3.79 | 305.00 |
| 310.00 | 7.70 | 7.77 | 6.03 | 2.14 | 2.68 | 2.78 | 3.68 | 310.00 |
| 315.00 | 7.88 | 7.81 | 6.02 | 2.22 | 2.67 | 2.81 | 3.64 | 315.00 |
| 320.00 | 7.72 | 7.71 | 6.04 | 2.43 | 2.61 | 2.87 | 3.81 | 320.00 |
| 325.00 | 7.78 | 7.61 | 6.04 | 2.30 | 2.78 | 2.78 | 3.14 | 325.00 |
| 330.00 | 7.86 | 7.76 | 6.08 | 2.07 | 2.58 | 2.88 | 2.69 | 330.00 |
| 335.00 | 7.86 | 7.88 | 6.08 | 2.07 | 0.43 | 0.61 | 1.19 | 335.00 |
| 340.00 | 7.81 | 7.76 | 6.04 | 0.70 | 0.42 | -0.88 | -0.68 | 340.00 |
| 345.00 | 7.10 | 7.67 | 6.10 | 1.04 | 2.06 | 0.10 | -1.00 | 345.00 |
| 350.00 | 7.67 | 6.65 | 5.13 | 1.18 | 2.74 | 0.60 | -1.03 | 350.00 |
| 355.00 | 7.08 | 6.93 | 6.67 | 1.08 | 1.64 | 0.88 | -2.09 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 0.61 | 1.67 | 0.73 | -0.67 | -1.97 | -2.11 | -1.91 | |

# BLADE LOADS

TEST 498 CNTR NO. 250 T.C.N. 33 C.R. 92

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 3.0 | -2.95 | -3.03 | -2.57 | -3.19 | 0.26 | 1.45 | 1.34 | 0.0 |
| 5.00 | -2.14 | -2.69 | -2.88 | -3.07 | -0.38 | 0.72 | 0.91 | 5.00 |
| 10.00 | -0.94 | -2.16 | -2.54 | -3.75 | -0.40 | 0.27 | 0.23 | 10.00 |
| 15.00 | -0.44 | -2.09 | -2.26 | -0.98 | 0.24 | 0.98 | 1.04 | 15.00 |
| 20.00 | -0.39 | -1.85 | -1.41 | -0.63 | 0.52 | 1.58 | 1.30 | 20.00 |
| 25.00 | -0.81 | -1.77 | -1.00 | 0.03 | 0.67 | 1.98 | 1.25 | 25.00 |
| 30.00 | -1.49 | -1.24 | -0.67 | 0.49 | 1.11 | 2.33 | 1.91 | 30.00 |
| 35.00 | -1.24 | -1.00 | -0.29 | 1.13 | 1.74 | 2.96 | 2.14 | 35.00 |
| 40.00 | -0.87 | -0.97 | 0.65 | 2.07 | 2.21 | 3.46 | 2.81 | 40.00 |
| 45.00 | -0.86 | -0.97 | 0.53 | 2.81 | 2.46 | 3.69 | 3.30 | 45.00 |
| 50.00 | -0.71 | -0.82 | 0.97 | 3.23 | 2.58 | 3.89 | 3.78 | 50.00 |
| 55.00 | -0.50 | -0.61 | 1.27 | 3.47 | 2.60 | 4.23 | 3.26 | 55.00 |
| 60.00 | -0.35 | -0.47 | 1.44 | 3.28 | 2.38 | 4.44 | 3.19 | 60.00 |
| 65.00 | -0.28 | -0.37 | 1.47 | 3.33 | 1.95 | 3.67 | 4.12 | 65.00 |
| 70.00 | -0.21 | -0.14 | 1.34 | 2.65 | 1.65 | 2.30 | 3.31 | 70.00 |
| 75.00 | -0.03 | 0.08 | 1.20 | 2.21 | 1.18 | 1.34 | 0.97 | 75.00 |
| 80.00 | .13 | 0.34 | 1.08 | 1.72 | 0.42 | 1.12 | -1.49 | 80.00 |
| 85.00 | 0.44 | 0.72 | 0.92 | 1.05 | -0.82 | 0.21 | -3.73 | 85.00 |
| 90.00 | 0.83 | 1.07 | 0.82 | 0.34 | -2.33 | -3.52 | -5.11 | 90.00 |
| 95.00 | 1.14 | 1.37 | 0.88 | -0.32 | -3.90 | -8.02 | -5.76 | 95.00 |
| 100.00 | 1.43 | 1.67 | 1.10 | -0.89 | -5.19 | -10.65 | -6.91 | 100.00 |
| 105.00 | 1.72 | 1.97 | 1.29 | -1.56 | -5.99 | -11.67 | -9.22 | 105.00 |
| 110.00 | 2.11 | 2.29 | 1.40 | -2.36 | -6.35 | -11.18 | -10.53 | 110.00 |
| 115.00 | 2.51 | 2.64 | 1.48 | -3.15 | -6.60 | -9.65 | -11.13 | 115.00 |
| 120.00 | 2.78 | 2.98 | 1.52 | -3.61 | -6.53 | -8.53 | -10.58 | 120.00 |
| 125.00 | 2.97 | 3.28 | 1.52 | -3.93 | -6.40 | -8.58 | -8.97 | 125.00 |
| 130.00 | 3.10 | 3.50 | 1.50 | -3.95 | -6.15 | -8.65 | -8.69 | 130.00 |
| 135.00 | 3.21 | 3.65 | 1.47 | -2.89 | -5.71 | -7.70 | -8.30 | 135.00 |
| 140.00 | 3.33 | 3.79 | 1.53 | -2.25 | -5.06 | -6.88 | -7.15 | 140.00 |
| 145.00 | 3.46 | 3.94 | 1.73 | -1.52 | -4.31 | -5.96 | -6.35 | 145.00 |
| 150.00 | 3.57 | 4.11 | 2.12 | -0.74 | -3.52 | -4.89 | -5.46 | 150.00 |
| 155.00 | 3.61 | 4.31 | 2.64 | 0.06 | -2.64 | -3.80 | -4.37 | 155.00 |
| 160.00 | 3.61 | 4.47 | 3.17 | 0.67 | -1.75 | -2.69 | -3.29 | 160.00 |
| 165.00 | 3.59 | 4.47 | 3.62 | 1.32 | -0.97 | -1.67 | -2.27 | 165.00 |
| 170.00 | 3.48 | 4.33 | 3.91 | 1.99 | -0.34 | -0.74 | -1.28 | 170.00 |
| 175.00 | 3.14 | 3.97 | 4.02 | 2.30 | 0.26 | 0.09 | -0.40 | 175.00 |
| 180.00 | 2.59 | 3.54 | 3.87 | 2.37 | 0.75 | 0.61 | 0.27 | 180.00 |
| 185.00 | 1.92 | 2.87 | 3.46 | 2.31 | 1.11 | 1.01 | 0.72 | 185.00 |
| 190.00 | 1.19 | 2.37 | 2.98 | 2.15 | 1.32 | 1.24 | 1.01 | 190.00 |
| 195.00 | 0.58 | 1.19 | 2.25 | 1.99 | 1.37 | 1.33 | 1.18 | 195.00 |
| 200.00 | 0.22 | 0.38 | 1.60 | 1.52 | 1.33 | 1.33 | 1.24 | 200.00 |
| 205.00 | -0.01 | -0.19 | 1.00 | 1.15 | 1.23 | 1.30 | 1.28 | 205.00 |
| 210.00 | -0.37 | -0.61 | 0.43 | 0.78 | 1.14 | 1.25 | 1.31 | 210.00 |
| 215.00 | -0.73 | -0.93 | 0.13 | 0.44 | 1.05 | 1.20 | 1.36 | 215.00 |
| 220.00 | -1.03 | -1.16 | -0.19 | 0.17 | 1.03 | 1.14 | 1.43 | 220.00 |
| 225.00 | -1.24 | -1.31 | -0.46 | -0.04 | 0.93 | 1.07 | 1.50 | 225.00 |
| 230.00 | -1.39 | -1.25 | -0.70 | -0.20 | 0.91 | 1.04 | 1.55 | 230.00 |
| 235.00 | -1.48 | -1.44 | -0.93 | -0.34 | 0.91 | 1.06 | 1.60 | 235.00 |
| 240.00 | -1.48 | -1.63 | -1.19 | -0.47 | 0.95 | 1.12 | 1.67 | 240.00 |
| 245.00 | -1.44 | -1.78 | -1.41 | -0.63 | 1.00 | 1.19 | 1.78 | 245.00 |
| 250.00 | -1.45 | -1.90 | -1.55 | -0.72 | 1.05 | 1.28 | 1.91 | 250.00 |
| 255.00 | -1.46 | -1.98 | -1.63 | -0.81 | 1.11 | 1.37 | 2.03 | 255.00 |
| 260.00 | -1.49 | -2.02 | -1.69 | -0.95 | 1.16 | 1.48 | 2.14 | 260.00 |
| 265.00 | -1.48 | -2.03 | -1.73 | -0.99 | 1.23 | 1.60 | 2.26 | 265.00 |
| 270.00 | -1.46 | -2.00 | -1.75 | -1.01 | 1.31 | 1.72 | 2.38 | 270.00 |
| 275.00 | -1.44 | -1.97 | -1.75 | -1.03 | 1.40 | 1.85 | 2.53 | 275.00 |
| 280.00 | -1.42 | -1.92 | -1.82 | -1.09 | 1.51 | 2.04 | 2.69 | 280.00 |
| 285.00 | -1.40 | -1.89 | -1.82 | -1.15 | 1.58 | 2.25 | 2.86 | 285.00 |
| 290.00 | -1.37 | -1.87 | -1.80 | -1.23 | 1.85 | 2.52 | 3.16 | 290.00 |
| 295.00 | -1.33 | -1.85 | -1.68 | -0.30 | 2.05 | 2.84 | 3.52 | 295.00 |
| 300.00 | -1.28 | -1.95 | -1.68 | -0.12 | 2.23 | 3.16 | 3.77 | 300.00 |
| 305.00 | -1.25 | -1.92 | -1.84 | -0.23 | 2.34 | 3.36 | 3.87 | 305.00 |
| 310.00 | -1.21 | -1.74 | -1.86 | -0.24 | 2.43 | 3.49 | 3.97 | 310.00 |
| 315.00 | -1.17 | -1.75 | -1.73 | -0.24 | 2.49 | 3.58 | 3.96 | 315.00 |
| 320.00 | -1.15 | -1.75 | -1.57 | -0.21 | 2.49 | 3.58 | 3.99 | 320.00 |
| 325.00 | -1.27 | -1.74 | -1.75 | -0.34 | 2.25 | 3.45 | 3.87 | 325.00 |
| 330.00 | -1.53 | -1.87 | -2.10 | -0.32 | 2.05 | 3.28 | 3.49 | 330.00 |
| 335.00 | -1.70 | -1.94 | -2.53 | -0.21 | 1.86 | 2.71 | 2.97 | 335.00 |
| 340.00 | -1.77 | -1.92 | -2.48 | -0.44 | 1.73 | 2.51 | 2.59 | 340.00 |
| 345.00 | -1.86 | -1.93 | -2.53 | -0.48 | 1.85 | 2.73 | 2.87 | 345.00 |
| 350.00 | -2.12 | -1.87 | -2.90 | -2.13 | 1.82 | 2.76 | 2.90 | 350.00 |
| 355.00 | -2.55 | -1.91 | -2.88 | -2.91 | 0.98 | 2.42 | 2.85 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.56 | 2.08 | 2.92 | 3.12 | 2.80 | 2.87 | 2.74 | |

# BLADE LOADS

TEST 498 CNTR NO. 278 T.C.No. 34 C.R. 33

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.01 | -3.77 | -3.46 | -0.79 | -0.41 | -1.49 | -2.47 | 0.0 |
| 5.00 | -0.98 | -4.16 | -3.63 | -1.20 | -0.11 | 0.10 | -0.60 | 5.00 |
| 10.00 | -0.22 | -2.99 | -4.73 | -1.99 | -0.18 | 0.87 | 0.69 | 10.00 |
| 15.00 | -0.59 | -1.91 | -4.94 | -2.84 | -0.68 | 0.40 | 0.01 | 15.00 |
| 20.00 | -0.61 | -1.65 | -3.96 | -2.91 | -0.63 | 0.17 | -0.70 | 20.00 |
| 25.00 | -0.97 | -2.70 | -1.87 | -0.86 | 0.96 | 1.13 | -0.03 | 25.00 |
| 30.00 | -1.49 | -2.82 | -0.78 | 0.60 | 1.21 | 2.01 | 0.78 | 30.00 |
| 35.00 | -1.81 | -2.19 | -0.25 | 1.75 | 1.78 | 2.73 | 1.62 | 35.00 |
| 40.00 | -1.74 | -1.50 | 0.91 | 2.69 | 2.35 | 3.69 | 2.94 | 40.00 |
| 45.00 | -1.04 | -0.97 | 0.42 | 3.24 | 3.13 | 4.90 | 4.54 | 45.00 |
| 50.00 | -0.28 | -0.76 | 1.27 | 3.42 | 3.80 | 4.74 | 5.89 | 50.00 |
| 55.00 | 0.10 | -0.78 | 1.42 | 4.23 | 4.07 | 6.03 | 5.38 | 55.00 |
| 60.00 | 0.10 | -0.91 | 1.90 | 4.16 | 4.25 | 6.07 | 5.97 | 60.00 |
| 65.00 | -0.12 | -0.98 | 1.38 | 3.95 | 4.34 | 5.67 | 2.94 | 65.00 |
| 70.00 | -0.36 | -0.88 | 1.04 | 3.43 | 3.58 | 1.05 | 1.05 | 70.00 |
| 75.00 | -0.51 | -0.68 | 0.51 | 1.42 | 1.42 | 0.45 | -3.19 | 75.00 |
| 80.00 | -0.56 | -0.49 | 0.01 | 0.74 | -1.17 | -2.42 | -5.80 | 80.00 |
| 85.00 | -0.46 | -0.34 | -0.06 | 0.28 | -1.96 | -6.50 | -7.15 | 85.00 |
| 90.00 | -0.14 | -0.13 | 0.22 | -0.05 | -3.02 | -8.34 | -8.39 | 90.00 |
| 95.00 | 0.38 | 0.42 | 0.81 | 0.39 | -6.97 | -8.07 | -2.71 | 95.00 |
| 100.00 | 0.91 | 1.13 | 1.66 | 0.52 | -7.04 | -4.47 | -1.12 | 100.00 |
| 105.00 | 1.45 | 1.89 | 2.42 | -0.56 | -6.98 | -2.84 | -1.47 | 105.00 |
| 110.00 | 1.98 | 2.52 | 2.52 | -1.82 | -4.82 | -2.03 | -1.86 | 110.00 |
| 115.00 | 2.46 | 3.10 | 3.05 | -2.65 | -4.37 | -3.47 | -1.62 | 115.00 |
| 120.00 | 2.83 | 3.75 | 2.69 | -3.15 | -4.28 | -6.05 | -3.55 | 120.00 |
| 125.00 | 3.14 | 4.23 | 1.76 | -3.48 | -4.04 | -6.95 | -6.09 | 125.00 |
| 130.00 | 3.40 | 4.57 | 0.92 | -3.74 | -7.01 | -6.69 | -6.95 | 130.00 |
| 135.00 | 3.59 | 4.69 | 0.12 | -3.88 | -6.94 | -9.37 | -7.73 | 135.00 |
| 140.00 | 3.69 | 4.63 | 0.19 | -3.75 | -5.66 | -9.46 | -10.27 | 140.00 |
| 145.00 | 3.66 | 4.51 | 0.47 | -3.38 | -4.39 | -8.38 | -9.41 | 145.00 |
| 150.00 | 3.55 | 4.38 | 0.91 | -2.89 | -4.73 | -7.53 | -8.51 | 150.00 |
| 155.00 | 3.51 | 4.41 | 1.48 | -2.11 | -4.66 | -6.53 | -7.17 | 155.00 |
| 160.00 | 3.48 | 4.69 | 2.06 | -1.28 | -4.53 | -4.22 | -6.19 | 160.00 |
| 165.00 | 3.32 | 5.01 | 2.69 | -0.31 | -2.40 | -3.79 | -4.88 | 165.00 |
| 170.00 | 2.95 | 5.21 | 3.34 | 0.72 | -1.24 | -2.30 | -3.33 | 170.00 |
| 175.00 | 2.34 | 5.16 | 3.85 | 1.59 | -0.30 | -0.97 | -1.40 | 175.00 |
| 180.00 | 1.68 | 4.81 | 4.01 | 2.06 | 0.55 | 0.08 | -0.54 | 180.00 |
| 185.00 | 1.02 | 3.98 | 3.81 | 2.32 | 1.22 | 0.98 | .45 | 185.00 |
| 190.00 | 0.49 | 2.87 | 3.30 | 2.34 | 1.72 | 1.42 | 1.15 | 190.00 |
| 195.00 | -0.30 | 1.64 | 2.60 | 2.19 | 1.97 | 1.97 | 1.57 | 195.00 |
| 200.00 | -0.81 | 0.64 | 1.75 | 1.98 | 2.02 | 2.08 | 1.71 | 200.00 |
| 205.00 | -1.19 | -0.04 | 1.09 | 1.75 | 1.96 | 2.05 | 1.74 | 205.00 |
| 210.00 | -1.27 | -0.46 | 0.87 | 1.45 | 1.88 | 1.96 | 1.82 | 210.00 |
| 215.00 | -1.34 | -0.84 | 0.70 | 1.10 | 1.80 | 1.89 | 1.84 | 215.00 |
| 220.00 | -1.40 | -1.15 | -0.09 | 0.89 | 1.74 | 1.84 | 1.82 | 220.00 |
| 225.00 | -1.40 | -1.41 | -0.25 | 0.66 | 1.70 | 1.81 | 1.84 | 225.00 |
| 230.00 | -1.39 | -1.64 | -0.47 | 0.57 | 1.71 | 1.80 | 1.90 | 230.00 |
| 235.00 | -1.32 | -1.84 | -0.72 | 0.37 | 1.75 | 1.84 | 1.99 | 235.00 |
| 240.00 | -1.19 | -1.97 | -1.00 | 0.18 | 1.79 | 1.88 | 2.09 | 240.00 |
| 245.00 | -1.09 | -1.90 | -1.27 | 0.01 | 1.82 | 1.90 | 2.19 | 245.00 |
| 250.00 | -1.09 | -1.86 | -1.43 | -0.16 | 1.82 | 1.90 | 2.27 | 250.00 |
| 255.00 | -1.13 | -1.84 | -1.49 | -0.34 | 1.82 | 1.89 | 2.34 | 255.00 |
| 260.00 | -1.19 | -1.82 | -1.46 | -0.50 | 1.80 | 1.87 | 2.45 | 260.00 |
| 265.00 | -1.12 | -1.77 | -1.45 | -0.61 | 1.79 | 1.84 | 2.52 | 265.00 |
| 270.00 | -1.12 | -1.72 | -1.45 | -0.64 | 1.81 | 1.87 | 2.57 | 270.00 |
| 275.00 | -1.17 | -1.70 | -1.43 | -0.63 | 1.86 | 1.95 | 2.62 | 275.00 |
| 280.00 | -1.21 | -1.70 | -1.40 | -0.55 | 1.93 | 2.06 | 2.67 | 280.00 |
| 285.00 | -1.22 | -1.69 | -1.36 | -0.39 | 2.02 | 2.18 | 2.74 | 285.00 |
| 290.00 | -1.17 | -1.70 | -1.32 | -0.18 | 2.14 | 2.33 | 2.86 | 290.00 |
| 295.00 | -1.12 | -1.73 | -1.32 | -0.01 | 2.26 | 2.55 | 3.01 | 295.00 |
| 300.00 | -1.09 | -1.80 | -1.31 | 0.09 | 2.41 | 2.84 | 3.21 | 300.00 |
| 305.00 | -1.11 | -1.84 | -1.29 | 0.20 | 2.54 | 3.10 | 3.34 | 305.00 |
| 310.00 | -1.13 | -1.77 | -1.29 | 0.30 | 2.60 | 3.33 | 3.46 | 310.00 |
| 315.00 | -1.01 | -1.88 | -1.29 | 0.37 | 2.62 | 3.44 | 3.63 | 315.00 |
| 320.00 | -0.72 | -1.90 | -1.29 | 0.37 | 2.60 | 3.52 | 3.80 | 320.00 |
| 325.00 | -0.40 | -1.93 | -1.29 | 0.22 | 2.60 | 3.60 | 3.90 | 325.00 |
| 330.00 | -0.21 | -1.14 | -1.26 | -0.28 | 2.49 | 3.57 | 3.81 | 330.00 |
| 335.00 | -0.48 | -1.17 | -1.19 | -1.03 | 2.39 | 3.44 | 3.61 | 335.00 |
| 340.00 | -1.11 | -1.31 | -0.99 | -1.60 | 1.95 | 3.09 | 3.25 | 340.00 |
| 345.00 | -1.27 | -1.54 | -0.86 | -1.24 | 0.60 | 1.70 | 2.46 | 345.00 |
| 350.00 | -1.46 | -1.73 | -1.28 | -0.15 | -0.64 | -0.31 | 0.17 | 350.00 |
| 355.00 | -2.01 | -2.28 | -2.87 | -0.14 | -1.19 | -3.09 | -3.01 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.42 | 1.00 | 0.87 | 0.17 | 0.96 | -0.37 | 0.84 | |

# BLADE LOADS

TEST 501 CNTR NO. 246 T.C.No. 35 C.R. 41

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -3.42 | -3.58 | -5.26 | -2.35 | 0.19 | 0.61 | 1.25 | 0.0 |
| 5.00 | 0.37 | -3.99 | -5.27 | -3.71 | 0.85 | 1.22 | 1.78 | 5.00 |
| 10.00 | -0.02 | -2.29 | -5.20 | -3.73 | 0.06 | 1.62 | 1.59 | 10.00 |
| 15.00 | -0.86 | -0.25 | -4.63 | -2.83 | -1.09 | -0.66 | -1.49 | 15.00 |
| 20.00 | -1.63 | -1.08 | -2.84 | -1.77 | -1.24 | -1.28 | -2.64 | 20.00 |
| 25.00 | -2.29 | -2.58 | -1.30 | -0.89 | -0.16 | -0.08 | -1.79 | 25.00 |
| 30.00 | -2.24 | -2.99 | -0.60 | 0.47 | 0.94 | 1.23 | -0.28 | 30.00 |
| 35.00 | -2.39 | -2.82 | -0.56 | 1.73 | 1.67 | 1.91 | 1.16 | 35.00 |
| 40.00 | -2.15 | -2.60 | -0.08 | 2.56 | 2.48 | 3.17 | 3.12 | 40.00 |
| 45.00 | -1.78 | -2.35 | 0.19 | 3.18 | 3.48 | 4.59 | 4.19 | 45.00 |
| 50.00 | -1.21 | -2.14 | 0.09 | 3.58 | 4.25 | 5.56 | 4.6 | 50.00 |
| 55.00 | -0.46 | -1.85 | 0.14 | 3.39 | 4.39 | 4.67 | 1.95 | 55.00 |
| 60.00 | -0.35 | -1.87 | 0.43 | 3.04 | 3.96 | 2.21 | 0.64 | 60.00 |
| 65.00 | -0.71 | -1.98 | 0.79 | 3.11 | 2.38 | 1.89 | -0.97 | 65.00 |
| 70.00 | -0.97 | -1.41 | 1.10 | 3.07 | 1.27 | -0.19 | -2.35 | 70.00 |
| 75.00 | -0.98 | -0.91 | 1.38 | 3.24 | -0.96 | -1.72 | -2.61 | 75.00 |
| 80.00 | -0.81 | -0.24 | 1.62 | 3.57 | -2.22 | -1.09 | -1.56 | 80.00 |
| 85.00 | -0.43 | 0.03 | 2.18 | 2.16 | -1.65 | -1.80 | -2.45 | 85.00 |
| 90.00 | 0.06 | 0.43 | 2.53 | 1.57 | -2.35 | -3.78 | -3.04 | 90.00 |
| 95.00 | 0.68 | 1.35 | 2.59 | 2.33 | -4.64 | -5.39 | -3.55 | 95.00 |
| 100.00 | 1.46 | 1.78 | 2.78 | 0.51 | -6.81 | -6.87 | -2.49 | 100.00 |
| 105.00 | 2.13 | 2.49 | 2.33 | -3.25 | -6.51 | -5.11 | -1.71 | 105.00 |
| 110.00 | 2.61 | 2.90 | 1.46 | -6.73 | -4.40 | -2.24 | -1.97 | 110.00 |
| 115.00 | 2.88 | 3.11 | 0.36 | -6.65 | -4.10 | -2.53 | -3.98 | 115.00 |
| 120.00 | 3.00 | 3.36 | -0.92 | -6.73 | -6.99 | -5.65 | -6.80 | 120.00 |
| 125.00 | 3.01 | 3.68 | -1.76 | -7.02 | -9.27 | -6.12 | -6.81 | 125.00 |
| 130.00 | 3.14 | 3.82 | -1.35 | -6.03 | -10.22 | -9.55 | -7.35 | 130.00 |
| 135.00 | 3.45 | 3.88 | -0.36 | -4.66 | -8.87 | -9.68 | -8.93 | 135.00 |
| 140.00 | 3.77 | 4.14 | 0.43 | -2.94 | -6.31 | -9.24 | -9.22 | 140.00 |
| 145.00 | 3.97 | 4.39 | 1.08 | -1.23 | -4.55 | -6.88 | -6.72 | 145.00 |
| 150.00 | 4.01 | 4.71 | 1.72 | -0.31 | -3.17 | -4.51 | -5.14 | 150.00 |
| 155.00 | 3.85 | 5.09 | 2.35 | 0.39 | -2.71 | -3.19 | -4.65 | 155.00 |
| 160.00 | 3.65 | 5.46 | 3.08 | 0.91 | -1.81 | -2.51 | -3.83 | 160.00 |
| 165.00 | 3.31 | 5.72 | 3.69 | 1.43 | -1.04 | -1.77 | -2.89 | 165.00 |
| 170.00 | 2.70 | 5.71 | 4.35 | 1.99 | -0.41 | -1.23 | -1.85 | 170.00 |
| 175.00 | 1.87 | 5.35 | 4.63 | 2.32 | 0.17 | -0.56 | -0.99 | 175.00 |
| 180.00 | 1.03 | 4.54 | 4.64 | 2.55 | 0.79 | 0.35 | -0.29 | 180.00 |
| 185.00 | 0.24 | 3.61 | 3.52 | 2.73 | 1.32 | 0.52 | 0.23 | 185.00 |
| 190.00 | -0.47 | 2.02 | 3.21 | 2.58 | 1.69 | 0.91 | 0.66 | 190.00 |
| 195.00 | -1.01 | 0.75 | 2.41 | 2.39 | 1.90 | 1.24 | 1.11 | 195.00 |
| 200.00 | -1.28 | -0.03 | 1.44 | 2.10 | 1.98 | 1.41 | 1.50 | 200.00 |
| 205.00 | -1.33 | -0.49 | 0.70 | 1.63 | 1.96 | 1.42 | 1.76 | 205.00 |
| 210.00 | -1.38 | -0.77 | 0.23 | 0.98 | 1.91 | 1.45 | 1.96 | 210.00 |
| 215.00 | -1.39 | -1.04 | -0.08 | 0.62 | 1.90 | 1.39 | 2.10 | 215.00 |
| 220.00 | -1.37 | -1.28 | -0.26 | 0.42 | 1.65 | 1.78 | 2.14 | 220.00 |
| 225.00 | -1.32 | -1.50 | -0.33 | 0.33 | 1.55 | 1.20 | 2.12 | 225.00 |
| 230.00 | -1.23 | -1.63 | -0.48 | 0.35 | 1.56 | 1.19 | 2.06 | 230.00 |
| 235.00 | -1.17 | -1.66 | -0.68 | 0.36 | 1.55 | 1.36 | 2.08 | 235.00 |
| 240.00 | -1.16 | -1.64 | -0.81 | 0.33 | 1.50 | 1.53 | 2.11 | 240.00 |
| 245.00 | -1.16 | -1.72 | -0.84 | 0.39 | 1.90 | 1.58 | 2.19 | 245.00 |
| 250.00 | -1.19 | -1.83 | -0.85 | 0.42 | 1.96 | 1.63 | 2.18 | 250.00 |
| 255.00 | -1.26 | -1.92 | -0.79 | 0.31 | 1.98 | 1.73 | 2.38 | 255.00 |
| 260.00 | -1.31 | -1.97 | -0.66 | 0.21 | 2.00 | 1.77 | 2.57 | 260.00 |
| 265.00 | -1.27 | -1.87 | -0.41 | 0.13 | 2.02 | 1.81 | 2.74 | 265.00 |
| 270.00 | -1.21 | -1.64 | -0.10 | -0.01 | 2.05 | 1.48 | 2.86 | 270.00 |
| 275.00 | -1.12 | -1.73 | -0.04 | -0.15 | 2.08 | 1.92 | 2.93 | 275.00 |
| 280.00 | -1.09 | -1.92 | -0.09 | -0.17 | 2.10 | 1.96 | 2.99 | 280.00 |
| 285.00 | -1.02 | -1.96 | -0.09 | -0.12 | 2.12 | 2.01 | 3.04 | 285.00 |
| 290.00 | -0.91 | -1.77 | -0.08 | -0.07 | 2.16 | 2.09 | 3.13 | 290.00 |
| 295.00 | -0.87 | -1.64 | -0.07 | -0.01 | 2.24 | 2.21 | 3.26 | 295.00 |
| 300.00 | -0.85 | -1.64 | -0.04 | 0.06 | 2.32 | 2.37 | 3.32 | 300.00 |
| 305.00 | -0.92 | -1.65 | -0.07 | 0.14 | 2.37 | 2.47 | 3.32 | 305.00 |
| 310.00 | -0.97 | -1.67 | -0.08 | 0.26 | 2.39 | 2.47 | 3.29 | 310.00 |
| 315.00 | -0.98 | -1.52 | -0.05 | 0.23 | 2.58 | 2.57 | 3.26 | 315.00 |
| 320.00 | -1.26 | -1.50 | -0.01 | -0.01 | 2.78 | 2.73 | 3.30 | 320.00 |
| 325.00 | -1.08 | -1.42 | -0.08 | -0.40 | 2.87 | 2.90 | 3.29 | 325.00 |
| 330.00 | -0.96 | -1.39 | -0.09 | -0.79 | 2.52 | 3.01 | 3.14 | 330.00 |
| 335.00 | -0.92 | -1.05 | -0.03 | -0.97 | 1.37 | 2.51 | 2.70 | 335.00 |
| 340.00 | -1.07 | -1.01 | -0.57 | -1.03 | 0.28 | 0.95 | 1.66 | 340.00 |
| 345.00 | -1.07 | -0.93 | -0.91 | 0.10 | -0.28 | -0.45 | -0.01 | 345.00 |
| 350.00 | -1.05 | -0.22 | -2.30 | 0.42 | 0.38 | -0.25 | -0.73 | 350.00 |
| 355.00 | -1.09 | -1.43 | -3.94 | -0.89 | 0.02 | -1.02 | -0.42 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 0.61 | 1.13 | 0.69 | -0.03 | -0.08 | -0.85 | -0.33 | |

# BLADE LOADS

TEST 902 CNTR NO. 179 T.C.No. 36 C.R. 44

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.9 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.56 | -4.19 | -3.21 | -1.53 | 1.32 | 1.89 | 1.57 | 0.0 |
| 5.00 | -2.51 | -3.32 | -3.94 | -1.97 | -0.17 | 0.93 | 0.58 | 5.00 |
| 10.00 | -1.65 | -2.37 | -2.28 | -1.17 | -0.35 | 0.89 | 0.36 | 10.00 |
| 15.00 | -0.76 | -1.14 | -2.02 | -1.73 | -0.14 | 1.21 | 0.41 | 15.00 |
| 20.00 | -0.30 | -1.33 | -2.25 | -1.25 | 0.18 | 1.44 | 0.46 | 20.00 |
| 25.00 | -0.44 | -1.45 | -1.97 | -0.94 | 0.51 | 1.74 | 0.65 | 25.00 |
| 30.00 | -1.28 | -1.64 | -1.42 | 0.05 | 1.65 | 2.30 | 1.16 | 30.00 |
| 35.00 | -1.21 | -1.18 | -0.99 | 0.92 | 1.87 | 2.06 | 1.08 | 35.00 |
| 40.00 | -0.85 | -0.88 | -0.55 | 2.11 | 2.89 | 3.53 | 2.64 | 40.00 |
| 45.00 | -0.74 | -0.69 | 0.21 | 2.98 | 3.79 | 4.69 | 3.25 | 45.00 |
| 50.00 | -0.53 | -0.50 | 0.77 | 3.48 | 4.21 | 5.05 | 3.84 | 50.00 |
| 55.00 | -0.30 | -0.31 | 1.00 | 3.75 | 4.21 | 5.06 | 4.35 | 55.00 |
| 60.00 | -0.13 | -0.16 | 1.12 | 3.85 | 3.83 | 4.70 | 4.01 | 60.00 |
| 65.00 | -0.03 | -0.10 | 1.16 | 3.23 | 3.05 | 3.85 | 3.09 | 65.00 |
| 75.50 | 0.04 | 0.79 | 1.11 | 2.68 | 2.10 | 2.48 | 1.86 | 70.00 |
| 75.00 | 0.12 | 0.69 | 1.08 | 2.11 | 1.03 | 0.86 | 0.62 | 75.00 |
| 80.00 | 0.27 | 1.13 | 1.06 | 1.57 | -0.05 | -0.72 | -0.91 | 80.00 |
| 85.00 | 0.48 | 1.54 | 1.05 | 1.06 | -1.14 | -2.34 | -2.29 | 85.00 |
| 90.00 | 0.74 | 1.87 | 1.07 | 0.69 | -2.12 | -3.80 | -3.65 | 90.00 |
| 95.00 | 1.14 | 2.23 | 1.14 | 0.52 | -3.09 | -5.07 | -5.34 | 95.00 |
| 100.00 | 1.56 | 2.55 | 1.28 | 0.57 | -4.01 | -6.19 | -6.63 | 100.00 |
| 105.00 | 1.96 | 2.86 | 1.42 | 0.26 | -4.95 | -7.15 | -7.64 | 105.00 |
| 110.00 | 2.34 | 3.13 | 1.48 | -0.31 | -5.82 | -7.90 | -8.44 | 110.00 |
| 115.00 | 2.73 | 3.40 | 1.46 | -0.86 | -6.52 | -8.42 | -8.95 | 115.00 |
| 120.00 | 3.06 | 3.65 | 1.51 | -1.36 | -7.03 | -8.63 | -9.23 | 120.00 |
| 125.00 | 3.29 | 3.88 | 1.59 | -1.85 | -7.22 | -8.61 | -9.22 | 125.00 |
| 130.00 | 3.42 | 4.16 | 1.71 | -2.19 | -7.17 | -8.43 | -9.04 | 130.00 |
| 135.00 | 3.52 | 4.43 | 1.87 | -2.12 | -6.86 | -8.11 | -8.77 | 135.00 |
| 140.00 | 3.64 | 4.67 | 2.12 | -1.78 | -6.30 | -7.58 | -8.20 | 140.00 |
| 145.00 | 3.71 | 4.85 | 2.41 | -1.19 | -5.59 | -6.89 | -7.40 | 145.00 |
| 150.00 | 3.68 | 4.99 | 2.75 | -0.51 | -4.82 | -5.95 | -6.48 | 150.00 |
| 155.00 | 3.58 | 5.14 | 3.15 | 0.22 | -4.01 | -4.76 | -5.49 | 155.00 |
| 160.00 | 3.39 | 5.28 | 3.58 | 0.90 | -3.12 | -3.80 | -4.47 | 160.00 |
| 165.00 | 3.13 | 5.34 | 3.91 | 1.44 | -2.14 | -2.66 | -3.65 | 165.00 |
| 170.00 | 2.83 | 5.26 | 4.18 | 2.39 | -1.75 | -1.82 | -2.44 | 170.00 |
| 175.00 | 2.50 | 4.99 | 4.28 | 2.27 | -0.52 | -1.15 | -1.49 | 175.00 |
| 180.00 | 2.39 | 4.56 | 4.12 | 2.27 | 0.05 | -0.71 | -0.76 | 180.00 |
| 185.00 | 1.56 | 3.97 | 3.74 | 2.08 | 0.41 | -0.43 | -0.29 | 185.00 |
| 190.00 | 1.03 | 3.25 | 3.16 | 1.84 | 0.81 | -0.17 | 0.22 | 190.00 |
| 195.00 | 0.52 | 2.46 | 2.50 | 1.52 | 0.69 | 0.02 | 0.22 | 195.00 |
| 200.00 | 0.23 | 1.64 | 1.75 | 1.17 | 0.69 | 0.16 | 0.29 | 200.00 |
| 205.00 | -0.40 | 1.04 | 1.15 | 0.83 | 0.65 | 0.19 | 0.32 | 205.00 |
| 210.00 | -0.68 | 0.16 | 0.66 | 0.48 | 0.58 | 0.17 | 0.40 | 210.00 |
| 215.00 | -0.93 | -0.35 | 0.16 | 0.12 | 0.57 | 0.12 | 0.52 | 215.00 |
| 220.00 | -1.06 | -0.79 | -0.28 | -0.14 | 0.55 | 0.08 | 0.64 | 220.00 |
| 225.00 | -1.19 | -1.18 | -0.63 | -0.36 | 0.54 | 0.12 | 0.77 | 225.00 |
| 230.00 | -1.39 | -1.53 | -0.94 | -0.53 | 0.59 | 0.22 | 0.93 | 230.00 |
| 235.00 | -1.59 | -1.79 | -1.26 | -0.66 | 0.70 | 0.36 | 1.12 | 235.00 |
| 240.00 | -1.65 | -1.97 | -1.56 | -0.77 | 0.89 | 0.54 | 1.37 | 240.00 |
| 245.00 | -1.65 | -2.14 | -1.85 | -0.95 | 1.13 | 0.79 | 1.72 | 245.00 |
| 250.00 | -1.67 | -2.32 | -2.10 | -0.92 | 1.33 | 1.11 | 2.11 | 250.00 |
| 255.00 | -1.72 | -2.46 | -2.30 | -0.97 | 1.40 | 1.48 | 2.53 | 255.00 |
| 260.00 | -1.76 | -2.52 | -2.45 | -1.03 | 1.82 | 1.85 | 2.93 | 260.00 |
| 265.00 | -1.78 | -2.55 | -2.54 | -1.09 | 2.05 | 2.16 | 3.31 | 265.00 |
| 270.00 | -1.78 | -2.63 | -2.61 | -0.97 | 2.15 | 2.43 | 3.66 | 270.00 |
| 275.00 | -1.74 | -2.72 | -2.67 | -0.93 | 2.31 | 2.68 | 4.00 | 275.00 |
| 280.00 | -1.68 | -2.78 | -2.71 | -0.91 | 2.46 | 2.94 | 4.24 | 280.00 |
| 285.00 | -1.61 | -2.80 | -2.73 | -0.90 | 2.53 | 3.17 | 4.33 | 285.00 |
| 290.00 | -1.56 | -2.77 | -2.77 | -0.87 | 2.54 | 3.29 | 4.28 | 290.00 |
| 295.00 | -1.51 | -2.76 | -2.85 | -0.83 | 2.45 | 3.26 | 4.05 | 295.00 |
| 300.00 | -1.49 | -2.79 | -2.93 | -0.76 | 2.34 | 3.21 | 3.83 | 300.00 |
| 305.00 | -1.48 | -2.79 | -2.97 | -0.67 | 2.30 | 3.23 | 3.74 | 305.00 |
| 310.00 | -1.4 | -2.77 | -3.00 | -0.60 | 2.35 | 3.44 | 3.80 | 310.00 |
| 315.00 | -1.49 | -2.75 | -2.99 | -0.59 | 2.43 | 3.77 | 4.00 | 315.00 |
| 320.00 | -1.50 | -2.74 | -2.82 | -0.68 | 2.47 | 3.90 | 4.27 | 320.00 |
| 325.00 | -1.55 | -2.73 | -2.53 | -0.85 | 2.42 | 3.92 | 4.41 | 325.00 |
| 330.00 | -1.59 | -2.73 | -2.31 | -0.82 | 2.18 | 3.67 | 4.25 | 330.00 |
| 335.00 | -1.49 | -2.76 | -1.79 | -0.70 | 1.78 | 3.25 | 3.74 | 335.00 |
| 340.00 | -1.03 | -2.92 | -0.47 | -0.76 | 1.40 | 2.49 | 3.33 | 340.00 |
| 345.00 | -0.30 | -3.28 | 1.72 | -1.23 | 1.28 | 2.49 | 3.48 | 345.00 |
| 350.00 | -0.61 | -4.02 | 2.73 | -2.82 | 1.46 | 3.22 | 4.15 | 350.00 |
| 355.00 | -1.72 | -5.26 | 1.27 | -3.60 | 1.57 | 3.39 | 3.55 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.02 | 3.60 | 5.16 | 5.48 | 3.10 | 4.32 | 3.26 | |

# BLADE LOADS

TEST 902 CNTR NO. 188 I.C.No. 37 C.R. 45

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.50 | -3.05 | -3.46 | -2.18 | -0.26 | 1.25 | 0.95 | 0.0 |
| 5.00 | -2.24 | -2.77 | -3.52 | -1.85 | -0.92 | 0.50 | 0.48 | 5.00 |
| 10.00 | -1.93 | -2.53 | -2.85 | -2.03 | -0.84 | 0.14 | -0.48 | 10.00 |
| 15.00 | -1.50 | -2.09 | -2.59 | -2.30 | 0.63 | 0.46 | -0.83 | 15.00 |
| 20.00 | -1.58 | -2.07 | -2.13 | -2.02 | -0.50 | 0.47 | -0.35 | 20.00 |
| 25.00 | -0.26 | -2.29 | -2.62 | -1.31 | -0.05 | 1.29 | 0.42 | 25.00 |
| 30.00 | -0.74 | -1.59 | -1.74 | -0.36 | 1.64 | 2.62 | 1.65 | 30.00 |
| 35.00 | -1.48 | -1.26 | -1.02 | 0.84 | 2.38 | 3.85 | 2.48 | 35.00 |
| 40.00 | -1.17 | -1.01 | -0.37 | 2.35 | 3.41 | 4.49 | 3.40 | 40.00 |
| 45.00 | -0.48 | -0.73 | 0.36 | 2.93 | 3.86 | 4.6 | 4.02 | 45.00 |
| 50.00 | 0.02 | -0.45 | 1.06 | 3.32 | 3.93 | 4.89 | 4.38 | 50.00 |
| 55.00 | 0.11 | -0.29 | 1.40 | 3.39 | 3.70 | 4.39 | 3.98 | 55.00 |
| 60.00 | 0.08 | -0.01 | 1.47 | 3.14 | 3.06 | 4.74 | 3.31 | 60.00 |
| 65.00 | 0.14 | 0.37 | 1.37 | 2.81 | 2.11 | 3.77 | 2.43 | 65.00 |
| 70.00 | 0.30 | 0.94 | 1.36 | 2.44 | 1.13 | 2.26 | 1.22 | 70.00 |
| 75.00 | 0.91 | 1.26 | 1.51 | 1.97 | 0.24 | 0.58 | -0.19 | 75.00 |
| 80.00 | 0.80 | 1.64 | 1.71 | 1.49 | -0.53 | -0.75 | -1.39 | 80.00 |
| 85.00 | 1.13 | 2.09 | 1.75 | 1.21 | -1.32 | -2.01 | -2.27 | 85.00 |
| 90.00 | 1.49 | 2.57 | 1.85 | 1.39 | -1.90 | -3.17 | -3.04 | 90.00 |
| 95.00 | 1.85 | 3.03 | 2.07 | 1.10 | -2.44 | -4.24 | -4.22 | 95.00 |
| 100.00 | 2.24 | 3.44 | 2.35 | 1.79 | -3.22 | -5.30 | -5.72 | 100.00 |
| 105.00 | 2.66 | 3.77 | 2.48 | 0.92 | -4.15 | -6.22 | -6.72 | 105.00 |
| 110.00 | 3.28 | 4.03 | 2.49 | 0.55 | -4.86 | -6.90 | -7.60 | 110.00 |
| 115.00 | 3.45 | 4.25 | 2.49 | -0.05 | -5.39 | -7.37 | -8.26 | 115.00 |
| 120.00 | 3.76 | 4.55 | 2.56 | -0.50 | -5.70 | -7.60 | -8.46 | 120.00 |
| 125.00 | 3.99 | 4.86 | 2.68 | -0.76 | -5.87 | -7.58 | -8.37 | 125.00 |
| 130.00 | 4.15 | 5.14 | 2.80 | -0.82 | -5.84 | -7.35 | -8.13 | 130.00 |
| 135.00 | 4.23 | 5.27 | 2.95 | -0.71 | -5.58 | -6.92 | -7.81 | 135.00 |
| 140.00 | 4.24 | 5.35 | 3.20 | -0.44 | -5.05 | -6.32 | -7.25 | 140.00 |
| 145.00 | 4.19 | 5.42 | 3.55 | 0.01 | -4.46 | -5.60 | -6.51 | 145.00 |
| 150.00 | 4.07 | 5.52 | 3.42 | 0.55 | -3.68 | -4.81 | -5.69 | 150.00 |
| 155.00 | 3.88 | 5.58 | 4.20 | 1.11 | -2.81 | -3.91 | -4.79 | 155.00 |
| 160.00 | 3.69 | 5.59 | 4.55 | 1.68 | -1.94 | -2.97 | -3.82 | 160.00 |
| 165.00 | 3.24 | 5.51 | 4.76 | 2.15 | -1.16 | -2.09 | -2.87 | 165.00 |
| 170.00 | 2.82 | 5.27 | 4.87 | 2.45 | -0.55 | -1.37 | -1.90 | 170.00 |
| 175.00 | 2.32 | 4.89 | 4.81 | 2.53 | -0.05 | -0.91 | -1.19 | 175.00 |
| 180.00 | 1.82 | 4.32 | 4.53 | 2.42 | 0.28 | -0.57 | -0.65 | 180.00 |
| 185.00 | 1.28 | 3.57 | 4.03 | 2.14 | 0.49 | -0.23 | -0.28 | 185.00 |
| 190.00 | 0.78 | 2.73 | 3.38 | 1.85 | 0.58 | 0.13 | -0.03 | 190.00 |
| 195.00 | 0.33 | 1.84 | 2.64 | 1.50 | 0.60 | 0.19 | 0.19 | 195.00 |
| 200.00 | -0.03 | 1.04 | 1.90 | 1.11 | 0.58 | 0.09 | 0.18 | 200.00 |
| 205.00 | -0.31 | 0.36 | 1.21 | 0.76 | 0.49 | -0.02 | 0.27 | 205.00 |
| 210.00 | -0.65 | -0.22 | 0.65 | 0.29 | 0.44 | -0.08 | 0.24 | 210.00 |
| 215.00 | -1.00 | -0.67 | 0.15 | 0.03 | 0.36 | -0.11 | 0.30 | 215.00 |
| 220.00 | -1.37 | -1.06 | -0.29 | -0.25 | 0.39 | -0.09 | 0.44 | 220.00 |
| 225.00 | -1.67 | -1.38 | -0.70 | -0.48 | 0.35 | -0.01 | 0.61 | 225.00 |
| 230.00 | -1.84 | -1.53 | -1.05 | -0.70 | 0.43 | 0.13 | 0.89 | 230.00 |
| 235.00 | -1.94 | -1.75 | -1.39 | -0.91 | 0.56 | 0.31 | 1.22 | 235.00 |
| 240.00 | -1.99 | -2.02 | -1.74 | -1.10 | 0.73 | 0.52 | 1.56 | 240.00 |
| 245.00 | -2.00 | -2.31 | -2.06 | -1.24 | 1.00 | 0.78 | 1.92 | 245.00 |
| 250.00 | -2.00 | -2.56 | -2.33 | -1.33 | 1.24 | 1.09 | 2.31 | 250.00 |
| 255.00 | -2.00 | -2.67 | -2.53 | -1.38 | 1.52 | 1.40 | 2.70 | 255.00 |
| 260.00 | -2.00 | -2.79 | -2.74 | -1.40 | 1.71 | 1.73 | 3.08 | 260.00 |
| 265.00 | -2.00 | -3.00 | -2.87 | -1.43 | 1.84 | 2.07 | 3.43 | 265.00 |
| 270.00 | -1.99 | -3.20 | -2.93 | -1.46 | 1.92 | 2.35 | 3.73 | 270.00 |
| 275.00 | -1.97 | -3.33 | -3.01 | -1.49 | 1.98 | 2.53 | 3.96 | 275.00 |
| 280.00 | -1.95 | -3.33 | -3.03 | -1.54 | 1.99 | 2.61 | 3.99 | 280.00 |
| 285.00 | -1.93 | -3.30 | -3.00 | -1.59 | 1.96 | 2.60 | 3.78 | 285.00 |
| 290.00 | -1.91 | -3.29 | -3.01 | -1.62 | 1.86 | 2.50 | 3.44 | 290.00 |
| 295.00 | -1.91 | -3.36 | -3.18 | -1.64 | 1.71 | 2.38 | 3.22 | 295.00 |
| 300.00 | -1.88 | -3.41 | -3.41 | -1.38 | 1.82 | 2.43 | 3.19 | 300.00 |
| 305.00 | -1.96 | -3.38 | -4.02 | -1.23 | 1.95 | 2.48 | 3.41 | 305.00 |
| 310.00 | -1.84 | -3.30 | -3.86 | -1.19 | 2.20 | 2.86 | 3.76 | 310.00 |
| 315.00 | -1.81 | -3.18 | -3.46 | -1.23 | 2.64 | 3.30 | 4.15 | 315.00 |
| 320.00 | -1.87 | -3.10 | -3.22 | -1.32 | 2.59 | 3.55 | 4.42 | 320.00 |
| 325.00 | -2.06 | -3.04 | -2.97 | -1.47 | 2.32 | 3.65 | 4.30 | 325.00 |
| 330.00 | -2.10 | -3.04 | -2.55 | -1.72 | 1.84 | 2.94 | 3.81 | 330.00 |
| 335.00 | -1.86 | -3.13 | -1.84 | -1.97 | 1.17 | 2.33 | 3.46 | 335.00 |
| 340.00 | -1.47 | -3.36 | -1.41 | -1.91 | 0.89 | 2.41 | 3.28 | 340.00 |
| 345.00 | -1.17 | -3.97 | -1.50 | -1.43 | 1.20 | 2.25 | 2.89 | 345.00 |
| 350.00 | -1.56 | -4.47 | -1.89 | -0.31 | 0.92 | 1.35 | 1.67 | 350.00 |
| 355.00 | -2.21 | -3.31 | -3.11 | -0.47 | 0.13 | 0.81 | 0.56 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.64 | 4.36 | 6.41 | 7.73 | 5.45 | 6.98 | 5.79 | |

TEXT NOT REPRODUCIBLE

## BLADE LOADS

TEST 909 CNTR NO. 198 T.C.M. 98 C.R. 98

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.9 | 170.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -3.64 | -3.05 | -4.49 | -4.32 | -1.61 | -0.76 | -0.59 | 0.0 |
| 5.00 | -2.67 | -3.10 | -4.68 | -1.79 | -2.51 | -2.16 | -1.71 | 5.00 |
| 10.00 | -1.84 | -4.72 | -3.18 | -1.84 | -1.79 | -1.15 | -1.35 | 10.00 |
| 15.00 | -0.69 | -3.36 | -2.65 | -3.04 | -0.60 | 0.44 | 0.82 | 15.00 |
| 20.00 | -0.97 | -2.31 | -3.68 | -3.45 | -0.85 | 1.48 | 3.06 | 20.00 |
| 25.00 | -1.33 | -2.31 | -2.31 | -1.46 | 0.49 | 1.85 | 1.34 | 25.00 |
| 30.00 | -1.35 | -1.68 | -1.54 | -0.23 | 1.63 | 2.92 | 2.34 | 30.00 |
| 35.00 | -1.67 | -1.32 | -0.62 | 1.75 | 3.87 | 4.16 | 3.45 | 35.00 |
| 40.00 | -1.67 | -1.86 | -0.68 | 3.89 | 4.17 | 5.30 | 5.04 | 40.00 |
| 45.00 | -1.14 | -1.46 | 0.46 | 4.67 | 4.83 | 6.41 | 6.25 | 45.00 |
| 50.00 | -0.65 | -1.36 | 3.45 | 4.73 | 5.86 | 7.28 | 6.75 | 50.00 |
| 55.00 | -0.72 | -1.07 | 3.46 | 4.66 | 6.00 | 7.16 | 6.49 | 55.00 |
| 60.00 | -0.69 | -0.66 | 3.18 | 4.74 | 6.74 | 6.89 | 5.14 | 60.00 |
| 65.00 | -0.97 | -0.47 | 2.27 | 4.31 | 6.58 | 6.25 | 5.00 | 65.00 |
| 70.00 | -0.92 | -0.16 | 2.72 | 3.88 | 5.79 | 6.47 | 4.55 | 70.00 |
| 75.00 | -0.97 | 0.74 | 3.63 | 3.68 | 2.66 | -.92 | 1.00 | 75.00 |
| 80.00 | 0.07 | 2.38 | 3.67 | 3.66 | 0.79 | 3.18 | -1.00 | 80.00 |
| 85.00 | 0.98 | 3.69 | -0.05 | 3.69 | -0.78 | 1.77 | -4.98 | 85.00 |
| 90.00 | 1.19 | -0.05 | 2.28 | 1.74 | -2.77 | 0.43 | -4.14 | 90.00 |
| 95.00 | 1.39 | 2.64 | 2.84 | 1.16 | -3.04 | -2.64 | -4.04 | 95.00 |
| 100.00 | 2.42 | 3.72 | 2.89 | 0.72 | -3.91 | -3.37 | -3.69 | 100.00 |
| 105.00 | 3.67 | 3.37 | 3.14 | -0.14 | -4.85 | -10.49 | -9.41 | 105.00 |
| 110.00 | 3.68 | 4.38 | 3.67 | -0.64 | -7.79 | -11.33 | -11.04 | 110.00 |
| 115.00 | 4.19 | 4.69 | 3.89 | -1.79 | -9.84 | -10.07 | -11.71 | 115.00 |
| 120.00 | 4.67 | 4.39 | 3.65 | -2.69 | -9.17 | -10.71 | -11.24 | 120.00 |
| 125.00 | 4.64 | 4.32 | 3.96 | -2.72 | -7.84 | -10.60 | -10.49 | 125.00 |
| 130.00 | 4.28 | 3.67 | 3.35 | -2.66 | -7.41 | -10.84 | -10.31 | 130.00 |
| 135.00 | 4.35 | 4.04 | 3.67 | -1.78 | -7.11 | -9.87 | -9.66 | 135.00 |
| 140.00 | 4.39 | 4.44 | 3.91 | -0.66 | -6.34 | -9.07 | -8.91 | 140.00 |
| 145.00 | 4.39 | 4.09 | 4.35 | -0.14 | -5.84 | -8.07 | -7.84 | 145.00 |
| 150.00 | 4.93 | 3.19 | 4.05 | 0.68 | -4.78 | -6.70 | -6.67 | 150.00 |
| 155.00 | 4.18 | 3.74 | 4.36 | 1.67 | -3.18 | -4.21 | -4.39 | 155.00 |
| 160.00 | 4.85 | 3.64 | 3.78 | 2.38 | -1.88 | -2.46 | -4.06 | 160.00 |
| 165.00 | 4.44 | 3.38 | 4.11 | 3.67 | -0.79 | -1.74 | -2.77 | 165.00 |
| 170.00 | 3.68 | 3.08 | 4.28 | 3.69 | 0.11 | -0.78 | -1.68 | 170.00 |
| 175.00 | 3.28 | 2.98 | 4.19 | 3.66 | 0.75 | -0.14 | -0.99 | 175.00 |
| 180.00 | 2.69 | 2.67 | 4.14 | 3.67 | 1.19 | 0.74 | 0.04 | 180.00 |
| 185.00 | 1.68 | 4.42 | 4.67 | 3.33 | 1.44 | 0.69 | 0.66 | 185.00 |
| 190.00 | 0.69 | 3.18 | 4.17 | 3.69 | 1.46 | 0.88 | 0.71 | 190.00 |
| 195.00 | -0.19 | 1.61 | 3.19 | 3.34 | 1.29 | 0.79 | 0.81 | 195.00 |
| 200.00 | -0.48 | 0.79 | 2.19 | 3.31 | 1.33 | 0.68 | 1.07 | 200.00 |
| 205.00 | -0.69 | -0.07 | 1.59 | 1.68 | 1.09 | 0.66 | 1.04 | 205.00 |
| 210.00 | -1.48 | -0.87 | 0.69 | 0.69 | 0.84 | 0.78 | 1.04 | 210.00 |
| 215.00 | -1.89 | -0.85 | -0.26 | -0.09 | 0.74 | 0.38 | 1.01 | 215.00 |
| 220.00 | -1.99 | -1.58 | -0.18 | -0.45 | 0.64 | -0.01 | 0.96 | 220.00 |
| 225.00 | -2.04 | -1.88 | -1.23 | -0.87 | 0.46 | -0.04 | 1.01 | 225.00 |
| 230.00 | -2.14 | -1.99 | -1.68 | -1.38 | 0.49 | -0.00 | 1.14 | 230.00 |
| 235.00 | -2.14 | -2.07 | -1.85 | -1.84 | 0.04 | 0.06 | 1.34 | 235.00 |
| 240.00 | -2.37 | -2.08 | -2.45 | -1.84 | 0.07 | 0.14 | 1.46 | 240.00 |
| 245.00 | -2.14 | -2.23 | -2.14 | -2.07 | 0.44 | 0.10 | 1.41 | 245.00 |
| 250.00 | -2.19 | -2.40 | -2.58 | -2.35 | 0.28 | 0.25 | 1.04 | 250.00 |
| 255.00 | -2.08 | -1.81 | -1.87 | -2.49 | 0.02 | 0.41 | 2.20 | 255.00 |
| 260.00 | -1.89 | -1.64 | -1.30 | -2.09 | 0.02 | 0.74 | 2.44 | 260.00 |
| 265.00 | -1.87 | -1.69 | -1.41 | -2.46 | 1.00 | 0.94 | 2.80 | 265.00 |
| 270.00 | -1.68 | -1.68 | -1.37 | -2.47 | 1.13 | 1.14 | 3.07 | 270.00 |
| 275.00 | -1.66 | -1.67 | -1.27 | -2.46 | 1.25 | 1.49 | 3.36 | 275.00 |
| 280.00 | -1.89 | -1.98 | -1.99 | -2.46 | 1.46 | 1.77 | 3.68 | 280.00 |
| 285.00 | -1.87 | -1.67 | -1.91 | -2.14 | 1.65 | 2.18 | 4.01 | 285.00 |
| 290.00 | -1.76 | -1.67 | -1.74 | -1.89 | 1.98 | 2.46 | 4.25 | 290.00 |
| 295.00 | -1.68 | -1.58 | -1.91 | -1.66 | 2.29 | 3.07 | 4.47 | 295.00 |
| 300.00 | -1.99 | -1.76 | -1.14 | -1.37 | 2.47 | 3.43 | 4.69 | 300.00 |
| 305.00 | -1.76 | -1.58 | -0.66 | -1.20 | 2.77 | 3.77 | 4.99 | 305.00 |
| 310.00 | -1.68 | -1.77 | -0.48 | -1.17 | 2.92 | 3.98 | 5.01 | 310.00 |
| 315.00 | -1.89 | -1.93 | -0.71 | -1.10 | 2.97 | 4.29 | 4.88 | 315.00 |
| 320.00 | -1.87 | -2.07 | -0.14 | -1.05 | 3.04 | 4.33 | 4.84 | 320.00 |
| 325.00 | -1.68 | -2.07 | -0.98 | -1.05 | 2.84 | 4.14 | 4.76 | 325.00 |
| 330.00 | -1.98 | -2.23 | -1.60 | -0.69 | 2.39 | 3.98 | 4.42 | 330.00 |
| 335.00 | -2.09 | -2.64 | -2.1 | -0.60 | 2.22 | 3.85 | 3.89 | 335.00 |
| 340.00 | -2.28 | -2.69 | -2.98 | -2.98 | 2.04 | 3.69 | 3.44 | 340.00 |
| 345.00 | -1.66 | -2.23 | -2.96 | -2.94 | 2.69 | 2.98 | 3.11 | 345.00 |
| 350.00 | -2.11 | -2.39 | -2.39 | -2.15 | 1.21 | 1.97 | 2.81 | 350.00 |
| 355.00 | -2.28 | -2.69 | -2.64 | -2.69 | -1.11 | -0.6 | 1.27 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 1.69 | 3.96 | 4.64 | 5.74 | 4.12 | 4.98 | 5.49 | |

# BLADE LOADS

TEST 494 CNTR NO. 226 T.C.R. 99 C.R. 00

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.8 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -3.37 | -3.30 | -4.47 | -2.18 | -0.79 | -1.09 | -2.87 | 0.0 |
| 5.0C | -2.68 | -5.17 | -5.36 | -3.36 | -0.34 | 0.63 | -0.54 | 5.0C |
| 10.00 | -1.78 | -4.98 | -6.36 | -1.93 | -1.85 | 1.58 | 0.23 | 10.0C |
| 15.0C | -1.81 | -3.31 | -4.47 | -2.75 | -1.23 | 0.29 | -0.74 | 15.0C |
| 20.0C | -0.78 | -1.73 | -5.35 | -2.85 | -1.03 | 0.31 | -1.20 | 20.0C |
| 25.0C | -0.84 | -2.76 | -3.50 | -1.63 | 0.10 | 1.38 | -0.25 | 25.0C |
| 30.0C | -1.94 | -4.38 | -1.04 | 0.13 | 2.84 | 2.92 | 0.98 | 30.0C |
| 35.0C | -2.65 | -4.18 | -0.13 | 1.86 | 3.21 | 3.95 | 1.68 | 35.0C |
| 40.00 | -2.83 | -3.04 | 0.23 | 3.32 | 3.95 | 4.07 | 2.50 | 40.0C |
| 45.0C | -1.99 | -2.50 | 1.15 | 4.31 | 4.62 | 4.44 | 4.83 | 45.0C |
| 50.0C | -0.88 | -1.52 | 1.79 | 5.10 | 5.59 | 7.03 | 6.04 | 50.0C |
| 55.0C | 0.01 | -1.36 | 1.94 | 5.56 | 6.14 | 8.72 | 8.44 | 55.0C |
| 60.0C | 0.26 | -1.34 | 1.76 | 5.77 | 6.40 | 9.51 | 7.23 | 60.0C |
| 65.0C | 0.39 | -1.48 | 1.72 | 5.27 | 6.16 | 8.64 | 6.95 | 65.0C |
| 70.0C | -0.13 | -1.51 | 1.69 | 4.23 | 5.15 | 6.89 | 4.36 | 70.0C |
| 75.0C | -0.41 | -1.45 | 1.04 | 2.99 | 4.41 | 1.82 | 1.61 | 75.0C |
| 80.0C | -0.64 | -1.22 | 0.12 | 1.82 | 1.24 | 0.41 | -3.37 | 80.0C |
| 85.0C | -0.96 | -0.86 | -0.45 | 0.81 | -0.97 | -3.56 | -7.37 | 85.0C |
| 90.0C | -0.18 | -0.37 | -0.21 | 0.00 | -3.26 | -11.96 | -8.45 | 90.0C |
| 95.0C | 0.51 | 0.19 | 0.69 | 0.32 | -4.38 | -15.93 | -9.51 | 95.0C |
| 100.0C | 1.32 | 0.99 | 1.82 | 0.33 | -0.82 | -13.36 | -8.69 | 100.0C |
| 105.0C | 2.11 | 2.05 | 2.98 | -0.14 | -0.61 | -10.37 | -4.58 | 105.0C |
| 110.0C | 2.95 | 3.19 | 3.90 | -1.44 | -7.87 | -7.14 | -1.98 | 110.0C |
| 115.0C | 3.76 | 4.27 | 4.15 | -2.67 | -5.38 | -6.94 | -1.09 | 115.0C |
| 120.0C | 4.53 | 5.35 | 4.48 | -3.07 | -4.99 | -7.09 | -4.03 | 120.0C |
| 125.0C | 5.28 | 6.30 | 3.35 | -3.42 | -0.69 | -8.08 | -7.91 | 125.0C |
| 130.0C | 5.64 | 6.98 | 1.75 | -3.93 | -10.39 | -7.26 | -7.72 | 130.0C |
| 135.0C | 5.88 | 7.18 | 0.83 | -4.47 | -0.72 | -12.33 | -10.14 | 135.0C |
| 140.0C | 5.99 | 7.25 | 0.75 | -4.73 | -10.01 | -12.98 | -14.82 | 140.0C |
| 145.0C | 6.02 | 7.18 | 1.61 | -4.65 | -10.67 | -11.24 | -12.43 | 145.0C |
| 150.0C | 5.99 | 6.97 | 1.38 | -4.17 | -9.91 | -11.71 | -11.41 | 150.0C |
| 155.0C | 5.8C | 6.76 | 1.75 | -3.22 | -8.28 | -9.58 | -9.98 | 155.0C |
| 160.0C | 5.44 | 6.73 | 2.45 | -1.98 | -6.59 | -8.19 | -8.84 | 160.0C |
| 165.0C | 5.06 | 6.99 | 3.28 | -0.59 | -4.99 | -6.13 | -7.22 | 165.0C |
| 170.0C | 4.57 | 7.37 | 4.18 | 0.79 | -3.29 | -3.77 | -4.97 | 170.0C |
| 175.0C | 3.99 | 7.51 | 5.01 | 2.06 | -1.45 | -1.59 | -2.86 | 175.0C |
| 180.0C | 3.28 | 7.17 | 5.45 | 3.09 | 0.03 | 0.21 | -1.01 | 180.0C |
| 185.0C | 2.39 | 6.37 | 5.36 | 3.63 | 1.18 | 1.45 | 0.52 | 185.0C |
| 190.0C | 1.22 | 5.04 | 4.69 | 3.19 | 2.13 | 2.16 | 1.54 | 190.0C |
| 195.0C | 0.03 | 3.38 | 3.67 | 2.69 | 2.59 | 2.41 | 2.14 | 195.0C |
| 200.0C | -0.96 | 1.64 | 2.45 | 2.59 | 2.73 | 2.51 | 2.43 | 200.0C |
| 205.0C | -1.62 | 0.45 | 2.03 | 2.23 | 2.57 | 2.48 | 2.44 | 205.0C |
| 210.0C | -2.04 | -0.47 | 1.18 | 1.81 | 2.35 | 2.38 | 2.37 | 210.0C |
| 215.0C | -2.24 | -1.16 | 0.53 | 1.49 | 2.22 | 2.30 | 2.23 | 215.0C |
| 220.0C | -2.30 | -1.73 | -0.06 | 1.18 | 2.10 | 2.28 | 2.15 | 220.0C |
| 225.0C | -2.31 | -2.19 | -0.58 | 0.85 | 2.03 | 2.29 | 2.24 | 225.0C |
| 230.0C | -2.44 | -2.49 | -0.86 | 0.51 | 2.00 | 2.33 | 2.43 | 230.0C |
| 235.0C | -2.39 | -2.72 | -1.10 | 0.21 | 2.03 | 2.44 | 2.61 | 235.0C |
| 240.0C | -2.28 | -2.89 | -1.50 | -0.09 | 2.08 | 2.59 | 2.79 | 240.0C |
| 245.0C | -2.25 | -3.08 | -1.76 | -0.22 | 2.12 | 2.68 | 2.95 | 245.0C |
| 250.0C | -2.22 | -3.01 | -1.96 | -0.39 | 2.14 | 2.69 | 3.08 | 250.0C |
| 255.0C | -2.23 | -3.02 | -2.10 | -0.55 | 2.13 | 2.77 | 3.21 | 255.0C |
| 260.0C | -2.20 | -2.96 | -2.19 | -0.71 | 2.11 | 2.84 | 3.31 | 260.0C |
| 265.0C | -2.16 | -2.91 | -2.23 | -0.83 | 2.10 | 2.9 | 3.38 | 265.0C |
| 270.0C | -2.13 | -2.81 | -2.21 | -0.85 | 2.09 | 2.97 | 3.44 | 270.0C |
| 275.0C | -2.04 | -2.67 | -2.15 | -0.82 | 2.12 | 3.04 | 3.50 | 275.0C |
| 280.0C | -1.98 | -2.61 | -2.06 | -0.72 | 2.22 | 3.15 | 3.58 | 280.0C |
| 285.0C | -1.94 | -2.65 | -1.97 | -0.50 | 2.38 | 3.29 | 3.70 | 285.0C |
| 290.0C | -1.99 | -2.61 | -1.92 | -0.41 | 2.65 | 3.47 | 3.86 | 290.0C |
| 295.0C | -1.98 | -2.57 | -1.96 | -0.23 | 2.86 | 3.76 | 4.04 | 295.0C |
| 300.0C | -1.95 | -2.65 | -1.89 | -0.03 | 3.15 | 3.99 | 4.22 | 300.0C |
| 305.0C | -1.87 | -2.59 | -1.89 | 0.18 | 3.31 | 4.12 | 4.41 | 305.0C |
| 310.0C | -1.71 | -2.53 | -1.96 | 0.26 | 3.48 | 4.03 | 4.61 | 310.0C |
| 315.0C | -1.52 | -2.41 | -1.92 | 0.31 | 3.62 | 4.04 | 4.62 | 315.0C |
| 320.0C | -1.33 | -2.23 | -1.94 | 0.31 | 3.75 | 4.05 | 4.92 | 320.0C |
| 325.0C | -1.12 | -2.00 | -1.93 | 0.31 | 3.79 | 4.05 | 4.91 | 325.0C |
| 330.0C | -0.85 | -1.81 | -1.87 | 0.07 | 3.71 | 4.01 | 4.73 | 330.0C |
| 335.0C | -0.55 | -1.71 | -1.68 | -1.18 | 3.49 | 4.48 | 4.41 | 335.0C |
| 340.0C | -0.99 | -2.30 | -1.40 | -2.28 | 3.24 | 4.26 | 4.13 | 340.0C |
| 345.0C | -1.26 | -2.73 | -1.38 | -2.57 | 2.64 | 3.38 | 3.43 | 345.0C |
| 350.0C | -2.38 | -2.13 | -1.41 | -1.95 | 0.31 | 1.17 | 1.24 | 350.0C |
| 355.0C | -2.97 | -1.55 | -2.45 | -1.14 | -0.55 | -0.71 | -1.89 | 355.0C |
| | | | | STATIC COMPONENTS | | | | |
| | 0.78 | 2.52 | 1.59 | 1.23 | 0.54 | -0.29 | -0.29 | |

# BLADE LOADS

TEST 497 CNTR NO. 256 T.C.No. 40 C.R. 25

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 159.9 | 170.5 | 189.8 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -1.14 | -4.27 | -5.41 | -2.12 | -0.75 | 0.53 | -1.47 | 0.0 |
| 5.00 | -0.12 | -4.81 | -5.45 | -2.75 | -3.15 | 2.86 | 1.75 | 5.02 |
| 10.00 | -0.87 | -2.16 | -5.75 | -3.92 | -0.63 | 2.45 | 0.00 | 10.00 |
| 15.00 | -1.96 | -1.99 | -5.73 | -2.63 | -6.28 | 2.28 | 0.50 | 15.00 |
| 20.00 | -1.99 | -2.39 | -2.81 | -2.48 | 1.02 | 3.84 | 1.33 | 20.00 |
| 25.00 | -1.66 | -4.27 | -1.17 | 1.27 | 2.13 | 4.85 | 2.34 | 25.00 |
| 30.00 | -1.38 | -4.24 | -0.65 | 2.75 | 3.33 | 5.50 | 4.18 | 30.00 |
| 35.00 | -1.95 | -2.87 | 0.66 | 4.21 | 4.68 | 7.31 | 5.69 | 35.00 |
| 40.00 | -1.84 | -1.74 | 1.46 | 5.57 | 6.02 | 9.13 | 7.74 | 40.00 |
| 45.00 | -0.87 | -1.16 | 2.15 | 6.52 | 8.97 | 10.90 | 9.36 | 45.00 |
| 50.00 | -1.24 | -1.19 | 2.49 | 7.12 | 7.68 | 11.50 | 11.00 | 50.00 |
| 55.00 | -0.80 | -1.19 | 2.51 | 7.25 | 7.63 | 11.54 | 10.11 | 55.00 |
| 60.00 | -0.10 | -1.29 | 2.39 | 6.59 | 7.55 | 10.13 | 6.95 | 60.00 |
| 65.00 | -0.53 | -1.27 | 2.12 | 5.69 | 7.21 | 6.54 | 5.62 | 65.00 |
| 70.00 | -0.81 | -1.15 | 1.26 | 4.27 | 4.08 | 2.77 | 2.26 | 70.00 |
| 75.00 | -0.77 | -0.95 | 0.45 | 3.39 | 1.58 | 0.14 | -3.33 | 75.00 |
| 80.00 | -0.52 | -0.66 | -0.11 | 1.94 | -2.60 | -4.59 | -7.44 | 80.00 |
| 85.00 | -0.11 | -0.39 | -0.21 | 1.14 | -9.28 | -12.16 | -9.96 | 85.00 |
| 90.00 | 0.41 | 0.20 | 0.45 | 1.91 | -7.36 | -15.66 | -9.66 | 90.00 |
| 95.00 | 1.15 | 1.04 | 1.61 | 1.69 | -8.86 | -16.80 | -7.83 | 95.00 |
| 100.00 | 1.97 | 2.19 | 2.43 | 0.96 | -8.54 | -16.03 | -5.26 | 100.00 |
| 105.00 | 2.78 | 3.47 | 3.01 | -0.54 | -7.13 | -7.72 | -2.71 | 105.00 |
| 110.00 | 3.66 | 4.78 | 4.19 | -1.78 | -5.69 | -7.97 | -2.02 | 110.00 |
| 115.00 | 4.47 | 5.87 | 3.93 | -2.58 | -5.34 | -8.38 | -4.63 | 115.00 |
| 120.00 | 5.31 | 6.72 | 3.17 | -3.00 | -9.47 | -8.25 | -8.78 | 120.00 |
| 125.00 | 5.38 | 7.17 | 2.17 | -3.47 | -16.95 | -18.35 | -8.81 | 125.00 |
| 130.00 | 5.63 | 7.75 | 1.42 | -4.06 | -8.59 | -12.94 | -10.64 | 130.00 |
| 135.00 | 5.82 | 7.89 | 1.26 | -4.35 | -8.92 | -12.80 | -13.53 | 135.00 |
| 140.00 | 5.92 | 7.82 | 1.51 | -4.17 | -8.09 | -12.45 | -12.85 | 140.00 |
| 145.00 | 5.88 | 7.61 | 2.08 | -3.50 | -8.82 | -10.86 | -11.92 | 145.00 |
| 150.00 | 5.65 | 7.41 | 2.63 | -2.68 | -7.63 | -10.32 | -10.69 | 150.00 |
| 155.00 | 5.33 | 7.50 | 3.30 | -1.13 | -8.05 | -8.33 | -9.48 | 155.00 |
| 160.00 | 4.99 | 7.75 | 4.13 | 0.46 | -4.37 | -6.38 | -7.95 | 160.00 |
| 165.00 | 4.63 | 7.91 | 4.86 | 1.53 | -2.71 | -4.15 | -6.02 | 165.00 |
| 170.00 | 4.65 | 7.92 | 5.46 | 2.31 | -1.10 | -2.67 | -3.86 | 170.00 |
| 175.00 | 3.26 | 7.38 | 5.75 | 2.77 | 0.05 | -0.36 | -1.93 | 175.00 |
| 180.00 | 2.22 | 6.42 | 5.54 | 2.88 | 0.89 | 0.84 | -0.47 | 180.00 |
| 185.00 | 1.12 | 5.02 | 4.98 | 2.62 | 1.44 | 1.44 | 0.54 | 185.00 |
| 190.00 | 0.21 | 3.31 | 3.96 | 2.28 | 1.78 | 1.77 | 1.69 | 190.00 |
| 195.00 | -0.53 | 1.68 | 2.89 | 1.93 | 1.90 | 1.86 | 1.31 | 195.00 |
| 200.00 | -1.04 | 0.28 | 1.86 | 1.63 | 1.99 | 1.84 | 1.39 | 200.00 |
| 205.00 | -1.58 | -0.67 | 0.95 | 1.78 | 1.85 | 1.77 | 1.42 | 205.00 |
| 210.00 | -1.95 | -1.36 | 0.34 | 0.92 | 1.86 | 1.76 | 1.47 | 210.00 |
| 215.00 | -2.10 | -1.93 | -0.16 | 0.58 | 1.88 | 1.81 | 1.53 | 215.00 |
| 220.00 | -2.29 | -2.18 | -0.59 | 0.32 | 1.93 | 1.89 | 1.61 | 220.00 |
| 225.00 | -2.33 | -2.40 | -1.03 | 0.00 | 1.96 | 1.90 | 1.79 | 225.00 |
| 230.00 | -2.29 | -3.11 | -1.47 | -0.21 | 2.03 | 2.07 | 2.02 | 230.00 |
| 235.00 | -2.21 | -3.29 | -1.87 | -0.42 | 2.04 | 2.16 | 2.25 | 235.00 |
| 240.00 | -2.14 | -3.33 | -2.22 | -0.75 | 2.10 | 2.24 | 2.50 | 240.00 |
| 245.00 | -2.11 | -3.31 | -2.51 | -1.14 | 2.13 | 2.30 | 2.72 | 245.00 |
| 250.00 | -2.08 | -3.39 | -2.71 | -1.48 | 2.11 | 2.32 | 2.85 | 250.00 |
| 255.00 | -2.08 | -3.31 | -2.82 | -1.77 | 2.05 | 2.32 | 2.90 | 255.00 |
| 260.00 | -2.05 | -3.23 | -2.78 | -1.99 | 1.97 | 2.31 | 2.91 | 260.00 |
| 265.00 | -2.08 | -3.13 | -2.69 | -2.07 | 1.93 | 2.32 | 2.95 | 265.00 |
| 270.00 | -1.97 | -3.03 | -2.67 | -2.07 | 1.92 | 2.37 | 3.02 | 270.00 |
| 275.00 | -1.97 | -3.07 | -2.56 | -1.99 | 1.96 | 2.44 | 3.14 | 275.00 |
| 280.00 | -2.01 | -2.97 | -2.51 | -1.84 | 2.06 | 2.59 | 3.29 | 280.00 |
| 285.00 | -2.09 | -2.99 | -2.47 | -1.63 | 2.23 | 2.79 | 3.49 | 285.00 |
| 290.00 | -2.27 | -2.79 | -2.44 | -1.33 | 2.44 | 3.10 | 3.75 | 290.00 |
| 295.00 | -2.33 | -2.67 | -2.43 | -1.10 | 2.67 | 3.56 | 4.03 | 295.00 |
| 300.00 | -2.09 | -2.96 | -2.42 | -0.75 | 2.88 | 3.98 | 4.33 | 300.00 |
| 305.00 | -1.82 | -2.84 | -2.42 | -0.52 | 3.07 | 4.34 | 4.62 | 305.00 |
| 310.00 | -1.78 | -2.78 | -2.42 | -0.43 | 3.22 | 4.59 | 4.84 | 310.00 |
| 315.00 | -1.58 | -2.64 | -2.36 | -0.43 | 3.32 | 4.77 | 5.10 | 315.00 |
| 320.00 | -1.01 | -2.39 | -2.29 | -0.58 | 3.49 | 4.86 | 5.26 | 320.00 |
| 325.00 | 0.70 | -2.11 | -2.10 | -1.08 | 3.47 | 4.85 | 5.69 | 325.00 |
| 330.00 | 0.43 | -1.76 | -1.99 | -2.08 | 3.19 | 4.71 | 4.73 | 330.00 |
| 335.00 | -0.55 | -2.10 | -1.62 | -2.97 | 2.32 | 4.34 | 4.02 | 335.00 |
| 340.00 | -2.99 | -2.91 | -1.26 | -3.11 | 0.65 | 3.67 | 3.42 | 340.00 |
| 345.00 | -3.53 | -2.69 | -1.91 | -2.36 | -0.82 | 0.68 | 1.33 | 345.00 |
| 350.00 | -3.45 | -3.15 | -2.87 | -2.25 | -1.95 | -1.99 | -1.32 | 350.00 |
| 355.00 | -3.36 | -5.31 | -5.39 | -2.04 | -1.48 | -2.12 | -2.49 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.38 | 1.96 | 1.15 | 1.19 | 1.07 | -1.20 | -1.24 | |

# BLADE LOADS

TEST 903 CNTR NO. 120 T.C.No. 41 C.R. 54

SPAN STATION

| DEG | 59.5 | 79.8 | 119.7 | 159.9 | 179.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -3.48 | -5.60 | -4.49 | -4.69 | -1.27 | 0.51 | 0.97 | 0.0 |
| 5.00 | -3.41 | -5.04 | -4.38 | -4.23 | -1.87 | -1.48 | -2.58 | 5.00 |
| 10.00 | -0.74 | -4.13 | -4.14 | -2.22 | -1.73 | -1.51 | -2.29 | 10.00 |
| 15.00 | 0.91 | -4.02 | -4.01 | -2.83 | -1.00 | 0.01 | -0.78 | 15.00 |
| 20.00 | -0.84 | -3.17 | -3.03 | -2.41 | -0.30 | 1.07 | 0.24 | 20.00 |
| 25.00 | -2.18 | -2.92 | -2.69 | -1.35 | 0.49 | 1.52 | 2.73 | 25.00 |
| 30.00 | -2.67 | -2.31 | -1.69 | -0.65 | 1.24 | 2.41 | 1.95 | 30.00 |
| 35.00 | -2.16 | -2.66 | -0.91 | 0.03 | 2.17 | 3.66 | 2.43 | 35.00 |
| 40.00 | -1.49 | -1.97 | -0.10 | 1.97 | 3.26 | 4.92 | 4.05 | 40.00 |
| 45.00 | -1.31 | -1.84 | 0.59 | 3.21 | 4.03 | 5.08 | 5.22 | 45.00 |
| 50.00 | -1.05 | -1.47 | 1.21 | 4.07 | 4.47 | 6.03 | 5.48 | 50.00 |
| 55.00 | -0.76 | -1.35 | 1.25 | 4.90 | 4.96 | 7.27 | 5.34 | 55.00 |
| 60.00 | -0.64 | -1.29 | 1.34 | 4.66 | 4.29 | 6.48 | 6.16 | 60.00 |
| 65.00 | -0.72 | -1.66 | 1.23 | 4.31 | 4.12 | 5.20 | 6.42 | 65.00 |
| 70.00 | -0.91 | -0.91 | 1.24 | 4.07 | 3.69 | 4.27 | 3.77 | 70.00 |
| 75.00 | -0.48 | -0.91 | 1.07 | 3.47 | 2.53 | 4.71 | 0.42 | 75.00 |
| 80.00 | -0.91 | -0.01 | 0.40 | 2.78 | 0.87 | 3.88 | -2.62 | 80.00 |
| 85.00 | 0.09 | 0.56 | 0.77 | 1.82 | -1.21 | -0.31 | -5.29 | 85.00 |
| 90.00 | 0.97 | 1.71 | 0.57 | 0.79 | -3.48 | -4.38 | -7.22 | 90.00 |
| 95.00 | 1.69 | 1.67 | 1.18 | 0.04 | -5.02 | -7.03 | -8.37 | 95.00 |
| 100.00 | 1.96 | 2.44 | 1.64 | -0.49 | -7.96 | -11.20 | -8.71 | 100.00 |
| 105.00 | 2.19 | 3.09 | 2.12 | -1.14 | -9.38 | -13.98 | -8.64 | 105.00 |
| 110.00 | 2.90 | 3.61 | 2.67 | -2.94 | -8.96 | -14.98 | -10.84 | 110.00 |
| 115.00 | 3.39 | 4.22 | 2.70 | -3.75 | -9.37 | -15.23 | -13.47 | 115.00 |
| 120.00 | 3.81 | 4.74 | 2.76 | -4.55 | -10.04 | -13.18 | -14.84 | 120.00 |
| 125.00 | 4.16 | 5.10 | 2.92 | -4.68 | -10.18 | -11.98 | -13.67 | 125.00 |
| 130.00 | 4.42 | 5.51 | 3.41 | -4.45 | -9.94 | -11.72 | -11.93 | 130.00 |
| 135.00 | 4.62 | 5.81 | 3.27 | -3.94 | -9.28 | -10.84 | -11.78 | 135.00 |
| 140.00 | 4.80 | 6.06 | 2.95 | -3.18 | -8.32 | -9.82 | -10.22 | 140.00 |
| 145.00 | 4.94 | 6.21 | 2.79 | -2.15 | -7.07 | -8.45 | -8.98 | 145.00 |
| 150.00 | 4.96 | 6.27 | 3.24 | -1.01 | -5.66 | -6.88 | -7.95 | 150.00 |
| 155.00 | 4.97 | 6.05 | 4.12 | 0.16 | -4.06 | -5.17 | -6.82 | 155.00 |
| 160.00 | 4.84 | 5.36 | 4.85 | 1.25 | -2.48 | -3.42 | -4.80 | 160.00 |
| 165.00 | 4.48 | 5.25 | 5.44 | 2.31 | -1.35 | -2.02 | -2.44 | 165.00 |
| 170.00 | 4.16 | 5.16 | 5.85 | 3.14 | 0.14 | -0.64 | -1.24 | 170.00 |
| 175.00 | 3.69 | 4.79 | 6.07 | 3.66 | 0.99 | 0.34 | -0.24 | 175.00 |
| 180.00 | 2.87 | 3.78 | 5.84 | 3.81 | 1.55 | 1.08 | 0.56 | 180.00 |
| 185.00 | 1.75 | 4.88 | 5.25 | 3.68 | 1.94 | 1.51 | 1.10 | 185.00 |
| 190.00 | 0.72 | 3.97 | 4.39 | 3.44 | 2.13 | 1.69 | 1.47 | 190.00 |
| 195.00 | -0.18 | 2.15 | 3.44 | 3.03 | 2.19 | 1.75 | 1.64 | 195.00 |
| 200.00 | -0.82 | 0.57 | 2.20 | 2.49 | 2.13 | 1.67 | 1.79 | 200.00 |
| 205.00 | -1.01 | 0.09 | 1.63 | 1.84 | 1.97 | 1.57 | 1.64 | 205.00 |
| 210.00 | -1.41 | -0.94 | 0.84 | 1.39 | 1.76 | 1.46 | 1.62 | 210.00 |
| 215.00 | -1.62 | -0.91 | 0.23 | 0.82 | 1.55 | 1.32 | 1.44 | 215.00 |
| 220.00 | -1.89 | -1.29 | -0.22 | 0.37 | 1.30 | 1.15 | 1.28 | 220.00 |
| 225.00 | -1.96 | -1.82 | -0.74 | 0.06 | 1.20 | 1.07 | 1.04 | 225.00 |
| 230.00 | -1.97 | -1.61 | -1.06 | -0.25 | 1.25 | 1.11 | 2.03 | 230.00 |
| 235.00 | -1.90 | -2.25 | -1.24 | -0.57 | 1.27 | 1.17 | 2.23 | 235.00 |
| 240.00 | -1.93 | -2.96 | -1.67 | -0.77 | 1.35 | 1.27 | 2.45 | 240.00 |
| 245.00 | -1.75 | -2.71 | -2.01 | -0.93 | 1.47 | 1.43 | 2.67 | 245.00 |
| 250.00 | -1.82 | -2.90 | -2.29 | -1.10 | 1.62 | 1.65 | 2.89 | 250.00 |
| 255.00 | -1.89 | -2.89 | -2.61 | -1.19 | 1.77 | 1.85 | 3.05 | 255.00 |
| 260.00 | -1.78 | -2.96 | -2.64 | -1.25 | 1.90 | 2.01 | 3.31 | 260.00 |
| 265.00 | -1.84 | -2.87 | -2.64 | -1.20 | 2.00 | 2.16 | 3.58 | 265.00 |
| 270.00 | -1.94 | -2.91 | -2.63 | -1.24 | 2.09 | 2.32 | 3.92 | 270.00 |
| 275.00 | -1.92 | -2.77 | -2.37 | -1.23 | 2.17 | 2.51 | 4.04 | 275.00 |
| 280.00 | -1.99 | -2.69 | -2.42 | -1.20 | 2.27 | 2.75 | 4.25 | 280.00 |
| 285.00 | -1.94 | -2.62 | -2.41 | -1.04 | 2.44 | 3.06 | 4.58 | 285.00 |
| 290.00 | -1.82 | -2.55 | -2.21 | -0.85 | 2.64 | 3.43 | 4.81 | 290.00 |
| 295.00 | -1.61 | -2.54 | -2.05 | -0.64 | 2.93 | 3.79 | 4.12 | 295.00 |
| 300.00 | -1.47 | -2.43 | -2.10 | -0.40 | 3.24 | 4.09 | 5.30 | 300.00 |
| 305.00 | -1.34 | -2.47 | -2.23 | -0.17 | 3.55 | 4.41 | 5.60 | 305.00 |
| 310.00 | -1.32 | -2.35 | -2.25 | -0.03 | 3.82 | 4.87 | 5.78 | 310.00 |
| 315.00 | -1.26 | -2.23 | -2.29 | 0.09 | 3.99 | 5.22 | 5.81 | 315.00 |
| 320.00 | -1.06 | -2.11 | -2.27 | 0.12 | 3.91 | 5.31 | 5.72 | 320.00 |
| 325.00 | -0.95 | -2.07 | -2.02 | 0.20 | 3.44 | 4.18 | 5.45 | 325.00 |
| 330.00 | -1.11 | -2.07 | -2.16 | 0.25 | 3.23 | 4.76 | 4.46 | 330.00 |
| 335.00 | -1.08 | -2.22 | -2.21 | 0.36 | 2.87 | 4.29 | 4.34 | 335.00 |
| 340.00 | -1.12 | -2.36 | -2.47 | 0.41 | 3.09 | 3.99 | 4.07 | 340.00 |
| 345.00 | -1.34 | -2.69 | -2.36 | -1.11 | 3.33 | 4.04 | 4.15 | 345.00 |
| 350.00 | -1.39 | -1.68 | -2.49 | -2.04 | 2.59 | 3.04 | 3.82 | 350.00 |
| 355.00 | -1.72 | -2.07 | -2.44 | -3.91 | -0.91 | 0.49 | 2.72 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.48 | 2.71 | 3.76 | 3.96 | 2.01 | 2.25 | 1.99 | |

# BLADE LOADS

TEST 903 CNTR NO. 140 T.C.No. 42 C.R. 55

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 159.5 | 170.5 | 189.8 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -4.00 | -4.41 | -4.64 | -4.11 | -0.40 | 0.41 | 0.11 | 0.0 |
| 5.00 | -3.11 | -4.00 | -4.32 | -2.11 | -1.40 | -0.42 | -1.01 | 5.00 |
| 10.00 | -1.86 | -3.74 | -4.14 | -3.76 | -1.49 | -0.14 | -0.71 | 10.00 |
| 15.00 | -0.41 | -3.20 | -2.90 | -3.31 | -0.1 | 1.45 | 0.90 | 15.00 |
| 20.00 | -0.00 | -2.64 | -2.48 | -1.00 | 0.77 | 2.26 | 1.41 | 20.00 |
| 25.00 | -1.70 | -3.13 | -3.24 | -0.47 | 1.43 | 2.89 | 1.98 | 25.00 |
| 30.00 | -1.78 | -1.81 | -3.11 | 0.41 | 2.41 | 4.04 | 2.78 | 30.00 |
| 35.00 | -1.04 | -1.69 | -0.31 | 1.75 | 3.45 | 4.36 | 4.03 | 35.00 |
| 40.00 | -1.11 | -1.00 | 0.99 | 3.29 | 4.78 | 5.49 | 5.10 | 40.00 |
| 45.00 | -0.00 | -1.74 | 1.24 | 4.44 | 5.10 | 7.46 | 6.47 | 45.00 |
| 50.00 | -0.31 | -1.11 | 1.34 | 5.10 | 5.63 | 6.12 | 7.07 | 50.00 |
| 55.00 | -0.04 | -0.00 | 2.19 | 6.41 | 6.48 | 8.06 | 6.77 | 55.00 |
| 60.00 | -0.47 | -0.76 | 2.07 | 6.49 | 6.97 | 7.02 | 7.27 | 60.00 |
| 65.00 | -0.49 | -0.01 | 2.10 | 6.00 | 7.01 | 6.00 | 7.27 | 65.00 |
| 70.00 | -0.49 | -0.97 | 1.96 | 6.91 | 6.06 | 6.56 | 6.07 | 70.00 |
| 75.00 | -0.37 | -0.03 | 1.03 | 3.74 | 2.50 | 4.65 | 5.07 | 75.00 |
| 80.00 | -0.04 | 0.49 | 1.44 | 2.04 | 0.74 | 2.76 | -2.75 | 80.00 |
| 85.00 | 0.20 | 0.50 | 1.21 | 1.00 | -1.07 | -0.20 | -0.10 | 85.00 |
| 90.00 | 0.04 | 1.45 | 1.40 | 0.50 | -3.37 | -3.06 | -4.07 | 90.00 |
| 95.00 | 1.30 | 1.00 | 1.05 | 0.21 | -4.60 | -7.47 | -8.21 | 95.00 |
| 100.00 | 1.00 | 2.01 | 1.02 | -0.56 | -5.96 | -11.10 | -8.77 | 100.00 |
| 105.00 | 2.00 | 1.00 | 2.32 | -3.00 | -6.69 | -10.67 | -8.15 | 105.00 |
| 110.00 | 3.31 | 3.04 | 2.37 | -3.06 | -6.61 | -10.67 | -11.06 | 110.00 |
| 115.00 | 3.06 | 4.10 | 3.46 | -4.01 | -10.04 | -15.60 | -14.61 | 115.00 |
| 120.00 | 4.70 | 4.31 | 3.03 | -4.60 | -10.70 | -13.63 | -14.33 | 120.00 |
| 125.00 | 4.00 | 4.26 | 3.03 | -4.01 | -10.20 | -12.10 | -11.06 | 125.00 |
| 130.00 | 4.77 | 4.00 | 3.66 | -4.00 | -9.04 | -11.01 | -11.06 | 130.00 |
| 135.00 | 4.51 | 4.41 | 3.00 | -3.66 | -6.10 | -10.60 | -11.41 | 135.00 |
| 140.00 | 5.10 | 4.10 | 3.34 | -3.20 | -0.11 | -6.70 | -10.01 | 140.00 |
| 145.00 | 4.76 | 4.47 | 3.10 | -3.04 | -4.03 | -8.01 | -8.74 | 145.00 |
| 150.00 | 5.27 | 4.70 | 3.00 | -2.51 | -4.67 | -7.07 | -7.47 | 150.00 |
| 155.00 | 4.10 | 3.62 | 4.01 | 0.04 | -4.03 | -5.33 | -6.07 | 155.00 |
| 160.00 | 4.51 | 3.25 | 4.10 | 1.00 | -3.06 | -5.67 | -4.44 | 160.00 |
| 165.00 | 4.40 | 3.70 | 4.01 | -1.70 | -1.14 | -3.14 | -3.04 | 165.00 |
| 170.00 | 3.00 | 3.10 | 4.24 | 3.04 | 0.07 | -0.04 | -1.77 | 170.00 |
| 175.00 | 3.10 | 4.03 | 4.24 | 3.07 | 0.00 | 0.10 | -0.01 | 175.00 |
| 180.00 | 3.32 | 3.11 | 4.00 | 3.50 | 1.00 | 1.01 | 0.24 | 180.00 |
| 185.00 | 1.47 | 4.00 | 3.74 | 3.00 | 1.00 | 1.01 | 0.24 | 185.00 |
| 190.00 | 0.21 | 3.40 | 2.02 | 3.41 | 1.04 | 1.01 | 1.24 | 190.00 |
| 195.00 | 0.11 | 2.11 | 3.01 | 3.07 | 1.04 | 1.04 | 1.02 | 195.00 |
| 200.00 | -0.20 | 1.00 | 2.03 | 3.00 | 1.04 | 1.01 | 1.05 | 200.00 |
| 205.00 | -0.00 | 0.11 | 1.44 | 1.04 | 1.04 | 1.27 | 1.47 | 205.00 |
| 210.00 | -1.10 | -0.01 | 0.10 | 1.10 | 1.10 | 0.00 | 1.11 | 210.00 |
| 215.00 | -1.12 | -0.02 | 0.10 | 0.07 | 1.12 | 0.00 | 1.14 | 215.00 |
| 220.00 | -1.02 | -1.10 | -0.04 | 0.07 | 1.01 | 0.70 | 1.12 | 220.00 |
| 225.00 | -1.00 | -1.14 | -0.05 | -0.07 | 0.00 | 0.07 | 1.04 | 225.00 |
| 230.00 | -1.00 | -2.11 | -1.20 | -0.00 | 0.00 | 0.00 | 1.00 | 230.00 |
| 235.00 | -1.04 | -2.00 | -1.01 | -0.07 | 0.00 | 0.74 | 1.07 | 235.00 |
| 240.00 | -1.04 | -2.01 | -1.05 | -1.10 | 1.02 | 0.01 | 1.00 | 240.00 |
| 245.00 | -1.01 | -2.14 | -2.11 | -1.14 | 1.14 | 0.04 | 1.00 | 245.00 |
| 250.00 | -1.01 | -2.20 | -2.21 | -1.01 | 1.20 | 1.00 | 2.10 | 250.00 |
| 255.00 | -1.01 | -2.20 | -2.17 | -1.00 | 1.35 | 1.70 | 2.00 | 255.00 |
| 260.00 | -1.01 | -2.11 | -2.00 | -1.70 | 1.44 | 1.44 | 2.07 | 260.00 |
| 265.00 | -1.01 | -2.11 | -2.01 | -1.01 | 1.07 | 1.07 | 2.04 | 265.00 |
| 270.00 | -1.04 | -2.14 | -2.01 | -1.01 | 1.07 | 1.01 | 2.11 | 270.00 |
| 275.00 | -1.10 | -2.14 | -2.01 | -1.01 | 1.11 | 2.02 | 2.42 | 275.00 |
| 280.00 | -1.10 | -2.04 | -2.04 | -1.10 | 1.00 | 2.10 | 3.11 | 280.00 |
| 285.00 | -1.11 | -2.01 | -2.04 | -1.01 | 2.11 | 2.11 | 4.01 | 285.00 |
| 290.00 | -1.14 | -2.01 | -2.01 | -1.02 | 2.10 | 2.02 | 4.01 | 290.00 |
| 295.00 | -1.10 | -2.00 | -2.10 | -1.11 | 2.00 | 3.00 | 4.11 | 295.00 |
| 300.00 | -1.00 | -2.01 | -2.14 | -0.02 | 2.04 | 3.05 | 4.04 | 300.00 |
| 305.00 | -1.00 | -2.01 | -2.00 | -0.10 | 1.07 | 4.00 | 5.10 | 305.00 |
| 310.00 | -1.04 | -2.04 | -2.10 | -0.00 | 1.10 | 4.00 | 5.00 | 310.00 |
| 315.00 | -1.00 | -2.10 | -2.00 | -0.00 | 1.01 | 4.01 | 5.00 | 315.00 |
| 320.00 | -1.10 | -2.11 | -2.01 | -0.00 | 1.02 | 4.00 | 5.00 | 320.00 |
| 325.00 | -1.20 | -2.04 | -2.20 | -0.01 | 1.10 | 4.11 | 5.00 | 325.00 |
| 330.00 | -1.04 | -2.01 | -2.00 | -0.07 | 2.00 | 4.17 | 4.00 | 330.00 |
| 335.00 | -2.00 | -2.01 | -2.01 | -0.21 | 2.00 | 4.00 | 4.14 | 335.00 |
| 340.00 | -2.04 | -2.11 | -2.01 | -0.10 | 1.00 | 3.00 | 3.00 | 340.00 |
| 345.00 | -1.07 | -2.00 | -2.10 | -1.00 | 1.10 | 3.07 | 4.11 | 345.00 |
| 350.00 | -1.01 | -2.11 | -2.00 | -0.07 | 1.00 | 3.14 | 4.00 | 350.00 |
| 355.00 | -2.00 | -2.00 | -2.00 | -0.07 | -0.10 | 1.04 | 2.20 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.00 | 2.00 | 2.10 | 0.27 | 2.00 | 1.00 | 2.01 | |

# BLADE LOADS

TEST 494 CNTR NO. 151 T.C.No. 43 C.R. 06

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -3.45 | -3.31 | -4.67 | -4.90 | 1.22 | 3.62 | 3.27 | 0.0 |
| 5.00 | -3.86 | -4.09 | -4.28 | -3.53 | -1.00 | -0.19 | -0.46 | 5.00 |
| 10.00 | -1.68 | -4.76 | -4.73 | -3.46 | -2.52 | -2.12 | -2.41 | 10.00 |
| 15.00 | -0.36 | -4.41 | -3.94 | -3.78 | -2.07 | -1.74 | -2.59 | 15.00 |
| 20.00 | -0.46 | -3.58 | -3.54 | -3.22 | -1.18 | -0.21 | -0.99 | 20.00 |
| 25.00 | -1.78 | -3.00 | -2.08 | -2.23 | -0.40 | 0.78 | 0.21 | 25.00 |
| 30.00 | -1.74 | -2.63 | -1.92 | -1.20 | 0.78 | 1.13 | 0.94 | 30.00 |
| 35.00 | -1.35 | -2.22 | -1.04 | -0.23 | 1.28 | 1.79 | 1.68 | 35.00 |
| 40.00 | -1.14 | -2.25 | -0.32 | 0.95 | 2.27 | 2.00 | 1.96 | 40.00 |
| 45.00 | -0.55 | -2.19 | 0.23 | 2.30 | 3.21 | 3.96 | 3.31 | 45.00 |
| 50.00 | -0.56 | -2.01 | 0.68 | 3.40 | 4.08 | 4.17 | 4.25 | 50.00 |
| 55.00 | -0.88 | -1.75 | 1.21 | 3.92 | 4.22 | 5.36 | 4.19 | 55.00 |
| 60.00 | -0.68 | -1.50 | 1.73 | 4.12 | 4.26 | 5.00 | 3.58 | 60.00 |
| 65.00 | -0.45 | -1.13 | 1.99 | 3.97 | 3.71 | 5.21 | 4.24 | 65.00 |
| 70.00 | -0.30 | -0.77 | 1.85 | 3.81 | 3.06 | 3.64 | 4.57 | 70.00 |
| 75.00 | -0.15 | -0.34 | 1.73 | 3.72 | 2.26 | 2.41 | 4.66 | 75.00 |
| 80.00 | 0.09 | 0.24 | 1.70 | 3.58 | 1.15 | 2.51 | 1.23 | 80.00 |
| 85.00 | 0.45 | 0.93 | 1.77 | 3.15 | -0.29 | 2.35 | -2.25 | 85.00 |
| 90.00 | 1.07 | 1.69 | 1.93 | 2.32 | -2.16 | 0.56 | -4.66 | 90.00 |
| 95.00 | 1.70 | 2.40 | 2.14 | 1.45 | -3.87 | -1.85 | -5.49 | 95.00 |
| 100.00 | 2.25 | 2.93 | 2.41 | 0.77 | -5.36 | -6.91 | -6.34 | 100.00 |
| 105.00 | 2.64 | 3.37 | 2.68 | 0.82 | -6.77 | -12.46 | -7.97 | 105.00 |
| 110.00 | 3.15 | 3.80 | 3.06 | -1.81 | -8.09 | -14.82 | -11.39 | 110.00 |
| 115.00 | 3.83 | 4.50 | 3.99 | -2.82 | -9.06 | -12.17 | -14.06 | 115.00 |
| 120.00 | 4.27 | 5.00 | 5.06 | -2.83 | -9.44 | -10.81 | -13.67 | 120.00 |
| 125.00 | 4.62 | 5.53 | 5.06 | -3.22 | -9.48 | -10.85 | -11.05 | 125.00 |
| 130.00 | 4.83 | 5.85 | 5.03 | -3.20 | -9.34 | -10.96 | -10.59 | 130.00 |
| 135.00 | 4.55 | 6.07 | 5.00 | -2.83 | -8.77 | -10.29 | -10.42 | 135.00 |
| 140.00 | 5.01 | 6.27 | 5.27 | -2.21 | -7.77 | -9.46 | -9.57 | 140.00 |
| 145.00 | 5.06 | 6.43 | 5.63 | -1.36 | -6.59 | -8.27 | -8.75 | 145.00 |
| 150.00 | 5.09 | 6.49 | 6.07 | -0.30 | -5.40 | -7.09 | -7.61 | 150.00 |
| 155.00 | 5.00 | 6.95 | 6.57 | 0.60 | -4.10 | -5.62 | -6.24 | 155.00 |
| 160.00 | 4.77 | 7.17 | 5.07 | 1.56 | -2.79 | -4.11 | -4.65 | 160.00 |
| 165.00 | 4.43 | 7.29 | 5.57 | 2.43 | -1.21 | -2.67 | -3.09 | 165.00 |
| 170.00 | 3.99 | 7.19 | 5.93 | 3.06 | -0.39 | -1.37 | -1.00 | 170.00 |
| 175.00 | 3.44 | 6.85 | 6.05 | 3.46 | 0.52 | -0.35 | -0.00 | 175.00 |
| 180.00 | 2.77 | 6.26 | 5.94 | 3.62 | 1.21 | 0.49 | -0.11 | 180.00 |
| 185.00 | 1.93 | 5.32 | 5.56 | 3.54 | 1.68 | 0.97 | 0.56 | 185.00 |
| 190.00 | 1.09 | 4.14 | 4.86 | 3.30 | 1.98 | 1.27 | 1.03 | 190.00 |
| 195.00 | 0.15 | 2.94 | 3.86 | 2.92 | 2.06 | 1.42 | 1.32 | 195.00 |
| 200.00 | -0.34 | 1.88 | 2.76 | 2.39 | 1.96 | 1.43 | 1.48 | 200.00 |
| 205.00 | -0.55 | 0.69 | 1.75 | 1.75 | 1.75 | 1.36 | 1.50 | 205.00 |
| 210.00 | -1.03 | -0.24 | 0.98 | 1.09 | 1.52 | 1.18 | 1.40 | 210.00 |
| 215.00 | -1.00 | -0.77 | 0.38 | 0.57 | 1.32 | 0.95 | 1.26 | 215.00 |
| 220.00 | -1.07 | -1.15 | -0.26 | 0.11 | 1.17 | 0.82 | 1.18 | 220.00 |
| 225.00 | -2.04 | -1.56 | -0.88 | -0.25 | 1.05 | 0.74 | 1.22 | 225.00 |
| 230.00 | -2.13 | -1.88 | -1.24 | -0.54 | 0.97 | 0.70 | 1.34 | 230.00 |
| 235.00 | -2.17 | -2.37 | -1.62 | -0.88 | 0.90 | 0.72 | 1.56 | 235.00 |
| 240.00 | -2.20 | -2.71 | -1.98 | -1.03 | 0.90 | 0.81 | 1.69 | 240.00 |
| 245.00 | -2.19 | -2.93 | -2.29 | -1.24 | 1.01 | 0.97 | 1.99 | 245.00 |
| 250.00 | -2.16 | -3.05 | -2.53 | -1.42 | 1.14 | 1.14 | 2.12 | 250.00 |
| 255.00 | -2.09 | -3.24 | -2.74 | -1.58 | 1.22 | 1.24 | 2.33 | 255.00 |
| 260.00 | -2.04 | -3.34 | -2.89 | -1.71 | 1.31 | 1.36 | 2.55 | 260.00 |
| 265.00 | -2.01 | -3.47 | -2.97 | -1.80 | 1.39 | 1.54 | 2.77 | 265.00 |
| 270.00 | -2.01 | -3.42 | -2.94 | -1.84 | 1.50 | 1.76 | 3.00 | 270.00 |
| 275.00 | -2.01 | -3.29 | -2.88 | -1.84 | 1.46 | 2.01 | 3.25 | 275.00 |
| 280.00 | -1.96 | -3.16 | -2.83 | -1.77 | 1.85 | 2.38 | 3.48 | 280.00 |
| 285.00 | -1.90 | -3.13 | -2.82 | -1.62 | 2.06 | 2.64 | 3.74 | 285.00 |
| 290.00 | -1.90 | -3.16 | -2.91 | -1.48 | 2.27 | 2.95 | 4.04 | 290.00 |
| 295.00 | -1.90 | -3.19 | -3.01 | -1.15 | 2.49 | 3.21 | 4.35 | 295.00 |
| 300.00 | -1.86 | -3.05 | -2.96 | -0.85 | 2.78 | 3.65 | 4.72 | 300.00 |
| 305.00 | -1.75 | -2.93 | -2.90 | -0.56 | 3.10 | 4.03 | 5.09 | 305.00 |
| 310.00 | -1.67 | -2.84 | -2.90 | -0.39 | 3.40 | 4.29 | 5.24 | 310.00 |
| 315.00 | -1.61 | -2.80 | -2.76 | -0.39 | 3.62 | 4.67 | 5.34 | 315.00 |
| 320.00 | -1.56 | -2.75 | -2.55 | -0.28 | 3.74 | 4.90 | 5.37 | 320.00 |
| 325.00 | -1.50 | -2.67 | -2.36 | -0.29 | 3.71 | 4.94 | 5.30 | 325.00 |
| 330.00 | -1.41 | -2.57 | -2.07 | -0.25 | 3.49 | 4.74 | 5.05 | 330.00 |
| 335.00 | -1.00 | -2.48 | -3.44 | -0.11 | 3.18 | 4.51 | 4.69 | 335.00 |
| 340.00 | -2.12 | -2.52 | -3.66 | 0.36 | 2.96 | 4.04 | 3.73 | 340.00 |
| 345.00 | -2.04 | -2.66 | -3.64 | 0.16 | 3.20 | 3.91 | 3.42 | 345.00 |
| 350.00 | -1.73 | -2.52 | -4.11 | -1.63 | 4.21 | 3.25 | 3.42 | 350.00 |
| 355.00 | -1.52 | -2.37 | -4.78 | -2.45 | 3.38 | 4.06 | 0.34 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 2.41 | 3.78 | 4.46 | 5.32 | 3.71 | 4.49 | 3.41 | |

# BLADE LOADS

TEST 496 CNTR NO. 176 T.C.No. 44 C.R. 07

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.67 | -4.03 | -4.34 | -3.21 | 2.75 | 1.74 | 1.28 | 0.0 |
| 5.00 | -3.77 | -5.49 | -3.78 | -5.79 | -0.76 | -0.65 | -1.58 | 5.00 |
| 10.00 | -2.10 | -5.41 | -3.19 | -2.86 | -2.42 | -1.38 | -1.97 | 10.00 |
| 15.00 | -0.48 | -4.79 | -2.89 | -1.11 | -1.78 | -0.83 | -1.18 | 15.00 |
| 20.00 | -0.11 | -3.63 | -3.03 | -0.62 | -0.21 | 1.06 | 0.41 | 20.00 |
| 25.00 | -0.00 | -2.80 | -2.16 | -0.42 | 1.34 | 2.92 | 2.00 | 25.00 |
| 30.00 | -1.76 | -2.07 | -0.84 | 0.47 | 2.65 | 4.28 | 3.18 | 30.00 |
| 35.00 | -1.98 | -1.36 | 0.00 | 1.00 | 3.65 | 4.90 | 3.76 | 35.00 |
| 40.00 | -1.22 | -1.33 | 0.91 | 2.95 | 4.63 | 5.48 | 4.46 | 40.00 |
| 45.00 | -0.87 | -1.36 | 1.67 | 4.04 | 5.24 | 6.25 | 5.25 | 45.00 |
| 50.00 | -0.77 | -1.22 | 2.27 | 5.33 | 6.06 | 7.19 | 6.33 | 50.00 |
| 55.00 | -0.46 | -0.97 | 2.84 | 6.20 | 6.66 | 8.17 | 7.32 | 55.00 |
| 60.00 | 0.00 | -0.69 | 3.20 | 6.70 | 6.93 | 8.90 | 8.00 | 60.00 |
| 65.00 | 0.25 | -0.28 | 3.29 | 6.73 | 6.63 | 8.98 | 8.05 | 65.00 |
| 70.00 | 0.29 | -0.01 | 3.26 | 6.49 | 5.57 | 7.97 | 6.48 | 70.00 |
| 75.00 | 0.18 | 0.23 | 3.10 | 5.99 | 5.24 | 8.73 | 7.92 | 75.00 |
| 80.00 | 0.15 | 0.59 | 2.73 | 5.49 | 4.27 | 6.35 | 6.18 | 80.00 |
| 85.00 | 0.35 | 1.02 | 2.39 | 4.69 | 3.30 | 5.61 | 1.62 | 85.00 |
| 90.00 | 0.71 | 1.50 | 2.17 | 3.60 | 1.94 | 1.47 | -3.31 | 90.00 |
| 95.00 | 1.25 | 2.00 | 1.85 | 2.43 | -1.65 | -2.65 | -9.03 | 95.00 |
| 100.00 | 1.81 | 2.35 | 1.06 | 1.20 | -5.33 | -7.94 | -8.25 | 100.00 |
| 105.00 | 2.27 | 2.57 | 1.96 | -0.10 | -8.47 | -14.72 | -12.00 | 105.00 |
| 110.00 | 2.50 | 2.00 | 1.00 | -1.81 | -10.39 | -16.43 | -14.63 | 110.00 |
| 115.00 | 3.00 | 3.12 | 1.74 | -4.07 | -11.44 | -16.13 | -15.38 | 115.00 |
| 120.00 | 3.30 | 3.63 | 1.62 | -6.20 | -12.30 | -14.35 | -16.72 | 120.00 |
| 125.00 | 3.92 | 4.12 | 1.35 | -7.03 | -12.00 | -13.44 | -15.49 | 125.00 |
| 130.00 | 3.69 | 4.44 | 1.00 | -6.98 | -12.50 | -13.66 | -13.64 | 130.00 |
| 135.00 | 3.82 | 4.59 | 0.00 | -6.64 | -12.11 | -12.92 | -12.61 | 135.00 |
| 140.00 | 3.53 | 4.67 | 0.72 | -5.91 | -11.21 | -12.23 | -11.73 | 140.00 |
| 145.00 | 4.00 | 4.86 | 0.65 | -4.84 | -9.84 | -10.94 | -10.70 | 145.00 |
| 150.00 | 4.24 | 5.12 | 0.85 | -3.03 | -8.41 | -9.61 | -9.56 | 150.00 |
| 155.00 | 4.23 | 5.48 | 1.44 | -2.45 | -6.78 | -7.72 | -8.17 | 155.00 |
| 160.00 | 4.07 | 5.86 | 2.28 | -1.32 | -5.66 | -5.94 | -6.53 | 160.00 |
| 165.00 | 3.89 | 6.17 | 3.13 | -0.40 | -3.65 | -4.94 | -4.91 | 165.00 |
| 170.00 | 3.59 | 6.39 | 3.84 | 0.56 | -2.54 | -2.93 | -3.43 | 170.00 |
| 175.00 | 3.16 | 6.23 | 4.39 | 1.33 | -1.52 | -1.69 | -2.13 | 175.00 |
| 180.00 | 2.93 | 5.62 | 4.55 | 1.84 | -0.98 | -0.99 | -1.84 | 180.00 |
| 185.00 | 1.79 | 5.13 | 4.33 | 2.16 | 0.33 | 0.23 | -0.17 | 185.00 |
| 190.00 | 1.04 | 4.15 | 3.81 | 2.29 | 0.99 | 0.83 | 0.90 | 190.00 |
| 195.00 | 0.24 | 2.87 | 3.03 | 2.14 | 1.40 | 1.22 | 0.95 | 195.00 |
| 200.00 | -0.27 | 1.91 | 2.19 | 1.79 | 1.52 | 1.38 | 1.27 | 200.00 |
| 205.00 | -0.81 | 0.43 | 1.39 | 1.39 | 1.44 | 1.39 | 1.42 | 205.00 |
| 210.00 | -1.09 | -0.79 | 0.67 | 0.96 | 1.36 | 1.34 | 1.91 | 210.00 |
| 215.00 | -1.28 | -0.69 | 0.09 | 0.51 | 1.23 | 1.25 | 1.57 | 215.00 |
| 220.00 | -1.41 | -1.06 | -0.32 | 0.00 | 1.12 | 1.16 | 1.62 | 220.00 |
| 225.00 | -1.59 | -1.38 | -0.70 | -0.25 | 1.02 | 1.06 | 1.65 | 225.00 |
| 230.00 | -1.69 | -1.70 | -0.99 | -0.50 | 0.98 | 1.01 | 1.70 | 230.00 |
| 235.00 | -1.74 | -1.97 | -1.22 | -0.68 | 0.84 | 1.02 | 1.80 | 235.00 |
| 240.00 | -1.74 | -2.14 | -1.44 | -0.80 | 0.89 | 1.10 | 1.95 | 240.00 |
| 245.00 | -1.68 | -2.28 | -1.66 | -0.91 | 1.04 | 1.26 | 2.12 | 245.00 |
| 250.00 | -1.63 | -2.40 | -1.87 | -0.97 | 1.20 | 1.45 | 2.31 | 250.00 |
| 255.00 | -1.56 | -2.53 | -2.04 | -1.00 | 1.42 | 1.58 | 2.52 | 255.00 |
| 260.00 | -1.50 | -2.66 | -2.11 | -1.03 | 1.52 | 1.77 | 2.75 | 260.00 |
| 265.00 | -1.46 | -2.71 | -2.14 | -1.09 | 1.62 | 1.98 | 3.01 | 265.00 |
| 270.00 | -1.44 | -2.65 | -2.10 | -1.05 | 1.72 | 2.16 | 3.29 | 270.00 |
| 275.00 | -1.46 | -2.55 | -2.21 | -1.03 | 1.80 | 2.41 | 3.56 | 275.00 |
| 280.00 | -1.54 | -2.45 | -2.21 | -1.00 | 2.00 | 2.70 | 3.83 | 280.00 |
| 285.00 | -1.47 | -2.37 | -2.20 | -0.92 | 2.31 | 3.02 | 4.12 | 285.00 |
| 290.00 | -1.45 | -2.34 | -2.14 | -0.78 | 2.53 | 3.29 | 4.44 | 290.00 |
| 295.00 | -1.54 | -2.33 | -2.09 | -0.62 | 2.77 | 3.57 | 4.72 | 295.00 |
| 300.00 | -1.56 | -2.33 | -2.07 | -0.45 | 2.98 | 3.96 | 4.98 | 300.00 |
| 305.00 | -1.43 | -2.25 | -1.99 | -0.23 | 3.18 | 4.24 | 5.21 | 305.00 |
| 310.00 | -1.17 | -2.21 | -1.99 | -0.12 | 3.35 | 4.53 | 5.35 | 310.00 |
| 315.00 | -1.11 | -2.18 | -1.97 | -0.01 | 3.45 | 4.74 | 5.41 | 315.00 |
| 320.00 | -1.11 | -2.19 | -1.81 | -0.03 | 3.49 | 4.88 | 5.36 | 320.00 |
| 325.00 | -1.12 | -2.17 | -1.78 | -0.13 | 3.42 | 4.90 | 5.31 | 325.00 |
| 330.00 | -1.27 | -2.14 | -2.27 | -0.15 | 3.26 | 4.72 | 5.05 | 330.00 |
| 335.00 | -1.77 | -2.07 | -2.95 | -0.01 | 3.06 | 4.36 | 4.66 | 335.00 |
| 340.00 | -2.15 | -2.06 | -3.34 | 0.43 | 2.86 | 4.04 | 4.27 | 340.00 |
| 345.00 | -2.22 | -1.89 | -3.32 | 1.09 | 3.09 | 4.02 | 4.11 | 345.00 |
| 350.00 | -1.80 | -1.89 | -3.73 | 0.18 | 4.28 | 4.90 | 4.13 | 350.00 |
| 355.00 | -1.45 | -2.27 | -4.58 | -0.48 | 5.31 | 4.39 | 3.73 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.62 | 2.33 | 2.62 | 2.83 | 1.30 | 1.42 | 0.94 | |

# BLADE LOADS

TEST 902 CHTR NO. 220 T.C.R. 45 C.R. 46

SPAN STATION

| RPM | 52.5 | 79.8 | 119.7 | 159.5 | 179.5 | 189.8 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -3.16 | -3.82 | -3.43 | -2.49 | -0.37 | 0.38 | -0.04 | 0.0 |
| 5.00 | -3.04 | -3.29 | -2.82 | -2.74 | -0.44 | 0.34 | -0.23 | 5.00 |
| 10.00 | -2.86 | -2.64 | -2.03 | -2.41 | -0.63 | 0.43 | -0.75 | 10.00 |
| 15.00 | -1.11 | -2.64 | -1.75 | -1.79 | -0.95 | 0.58 | -0.55 | 15.00 |
| 20.00 | -0.84 | -2.73 | -1.95 | -0.96 | -0.20 | 0.93 | 0.03 | 20.00 |
| 25.00 | -0.12 | -1.94 | -1.60 | -0.36 | 0.15 | 1.18 | 0.36 | 25.00 |
| 30.00 | -1.15 | -1.20 | -1.16 | 0.27 | 0.79 | 1.74 | 0.82 | 30.00 |
| 35.00 | -1.20 | -0.83 | -0.82 | 1.09 | 1.88 | 2.49 | 1.32 | 35.00 |
| 40.00 | -0.98 | -0.68 | -0.54 | 1.98 | 2.50 | 3.27 | 2.15 | 40.00 |
| 45.00 | -0.48 | -0.60 | 0.24 | 2.64 | 2.86 | 3.80 | 2.54 | 45.00 |
| 50.00 | -0.28 | -0.97 | 0.80 | 2.04 | 2.96 | 4.30 | 3.12 | 50.00 |
| 55.00 | -0.15 | -0.41 | 1.06 | 2.98 | 2.89 | 4.41 | 3.51 | 55.00 |
| 60.00 | -0.18 | -0.12 | 1.02 | 2.92 | 2.55 | 3.90 | 3.27 | 60.00 |
| 65.00 | -0.14 | 0.23 | 0.87 | 2.69 | 1.97 | 2.68 | 2.44 | 65.00 |
| 70.00 | 0.02 | 0.55 | 0.94 | 2.36 | 1.24 | 1.51 | 1.53 | 70.00 |
| 75.00 | 0.21 | 0.84 | 1.04 | 1.92 | 0.43 | 0.84 | 0.19 | 75.00 |
| 80.00 | 0.40 | 1.18 | 1.10 | 1.53 | -0.36 | -1.29 | -1.07 | 80.00 |
| 85.00 | 0.68 | 1.57 | 1.14 | 1.26 | -1.13 | -2.57 | -2.54 | 85.00 |
| 90.00 | 1.05 | 2.01 | 1.24 | 1.11 | -1.94 | -3.80 | -4.02 | 90.00 |
| 95.00 | 1.47 | 2.41 | 1.48 | 0.95 | -2.83 | -5.29 | -5.30 | 95.00 |
| 100.00 | 1.98 | 2.76 | 1.54 | 0.68 | -3.73 | -6.22 | -6.51 | 100.00 |
| 105.00 | 2.28 | 3.02 | 1.61 | 0.22 | -4.56 | -7.12 | -7.42 | 105.00 |
| 110.00 | 2.61 | 3.29 | 1.72 | -0.36 | -5.13 | -7.77 | -8.09 | 110.00 |
| 115.00 | 2.90 | 3.50 | 1.85 | -0.92 | -5.40 | -7.80 | -8.24 | 115.00 |
| 120.00 | 3.22 | 3.88 | 1.92 | -1.36 | -5.48 | -7.65 | -8.26 | 120.00 |
| 125.00 | 3.49 | 4.14 | 1.95 | -1.59 | -5.65 | -7.40 | -8.04 | 125.00 |
| 130.00 | 3.59 | 4.35 | 2.04 | -1.52 | -5.29 | -7.13 | -7.88 | 130.00 |
| 135.00 | 3.56 | 4.48 | 2.23 | -1.14 | -4.99 | -6.72 | -7.61 | 135.00 |
| 140.00 | 3.51 | 4.60 | 2.47 | -0.99 | -4.52 | -6.18 | -6.98 | 140.00 |
| 145.00 | 3.94 | 4.72 | 2.78 | -0.68 | -3.92 | -5.48 | -6.18 | 145.00 |
| 150.00 | 3.91 | 4.84 | 2.99 | 0.17 | -7.23 | -4.65 | -5.28 | 150.00 |
| 155.00 | 3.89 | 4.95 | 3.32 | 0.80 | -2.50 | -3.74 | -4.33 | 155.00 |
| 160.00 | 3.84 | 5.01 | 3.68 | 1.37 | -1.76 | -2.82 | -3.37 | 160.00 |
| 165.00 | 2.66 | 4.97 | 3.96 | 1.78 | -1.02 | -1.94 | -2.43 | 165.00 |
| 170.00 | 2.27 | 4.79 | 4.04 | 1.87 | -0.39 | -1.17 | -1.58 | 170.00 |
| 175.00 | 1.98 | 4.48 | 3.92 | 1.94 | 0.12 | -0.56 | -0.89 | 175.00 |
| 180.00 | 1.42 | 3.81 | 3.61 | 1.87 | 0.48 | -0.12 | -0.26 | 180.00 |
| 185.00 | 0.98 | 3.11 | 3.09 | 1.74 | 0.68 | 0.16 | 0.16 | 185.00 |
| 190.00 | 0.36 | 2.37 | 2.46 | 1.52 | 0.77 | 0.35 | 0.42 | 190.00 |
| 195.00 | -0.17 | 1.58 | 1.81 | 1.18 | 0.75 | 0.39 | 0.55 | 195.00 |
| 200.00 | -0.62 | 0.81 | 1.17 | 0.78 | 0.67 | 0.35 | 0.60 | 200.00 |
| 205.00 | -0.92 | 0.12 | 0.69 | 0.39 | 0.57 | 0.22 | 0.63 | 205.00 |
| 210.00 | -1.07 | -0.39 | 0.19 | 0.14 | 0.50 | 0.28 | 0.67 | 210.00 |
| 215.00 | -1.22 | -0.75 | -0.20 | -0.07 | 0.45 | 0.27 | 0.73 | 215.00 |
| 220.00 | -1.37 | -1.08 | -0.49 | -0.22 | 0.47 | 0.29 | 0.83 | 220.00 |
| 225.00 | -1.47 | -1.38 | -0.74 | -0.34 | 0.54 | 0.37 | 1.01 | 225.00 |
| 230.00 | -1.46 | -1.64 | -1.00 | -0.46 | 0.65 | 0.50 | 1.26 | 230.00 |
| 235.00 | -1.48 | -1.78 | -1.23 | -0.57 | 0.78 | 0.69 | 1.55 | 235.00 |
| 240.00 | -1.52 | -1.86 | -1.45 | -0.68 | 0.94 | 0.93 | 1.79 | 240.00 |
| 245.00 | -1.52 | -1.94 | -1.67 | -0.78 | 1.13 | 1.20 | 2.06 | 245.00 |
| 250.00 | -1.48 | -2.04 | -1.87 | -0.82 | 1.33 | 1.51 | 2.43 | 250.00 |
| 255.00 | -1.44 | -2.12 | -2.07 | -0.76 | 1.56 | 1.85 | 2.78 | 255.00 |
| 260.00 | -1.42 | -2.23 | -2.11 | -0.68 | 1.78 | 2.20 | 3.16 | 260.00 |
| 265.00 | -1.44 | -2.29 | -2.16 | -0.64 | 1.96 | 2.55 | 3.55 | 265.00 |
| 270.00 | -1.45 | -2.30 | -2.20 | -0.64 | 2.12 | 2.89 | 3.91 | 270.00 |
| 275.00 | -1.43 | -2.33 | -2.26 | -0.66 | 2.22 | 3.23 | 4.21 | 275.00 |
| 280.00 | -1.36 | -2.38 | -2.31 | -0.69 | 2.23 | 3.42 | 4.35 | 280.00 |
| 285.00 | -1.32 | -2.40 | -2.38 | -0.69 | 2.17 | 3.38 | 4.19 | 285.00 |
| 290.00 | -1.39 | -2.41 | -2.44 | -0.65 | 2.07 | 3.26 | 3.86 | 290.00 |
| 295.00 | -1.47 | -2.36 | -2.47 | -0.60 | 2.02 | 3.18 | 3.64 | 295.00 |
| 300.00 | -1.48 | -2.33 | -2.48 | -0.57 | 2.01 | 3.23 | 3.59 | 300.00 |
| 305.00 | -1.38 | -2.32 | -2.45 | -0.58 | 2.07 | 3.36 | 3.65 | 305.00 |
| 310.00 | -1.26 | -2.35 | -2.42 | -0.63 | 2.13 | 3.51 | 3.77 | 310.00 |
| 315.00 | -1.19 | -2.41 | -2.41 | -0.72 | 2.12 | 3.62 | 3.93 | 315.00 |
| 320.00 | -1.32 | -2.44 | -2.26 | -0.83 | 1.94 | 3.59 | 4.05 | 320.00 |
| 325.00 | -1.37 | -2.48 | -1.98 | -1.00 | 1.69 | 3.12 | 3.90 | 325.00 |
| 330.00 | -0.98 | -2.41 | -1.12 | -1.21 | 1.13 | 2.31 | 3.56 | 330.00 |
| 335.00 | -0.91 | -2.31 | -0.85 | -1.38 | 0.51 | 1.61 | 3.25 | 335.00 |
| 340.00 | 0.09 | -1.98 | 0.18 | -1.56 | 0.02 | 1.07 | 2.95 | 340.00 |
| 345.00 | -0.16 | -3.09 | -0.69 | -1.76 | 1.09 | 2.49 | 3.29 | 345.00 |
| 350.00 | -0.96 | -3.73 | -1.92 | -1.52 | 1.02 | 1.92 | 1.75 | 350.00 |
| 355.00 | -2.16 | -3.11 | -3.51 | -1.32 | 0.53 | 0.00 | 0.11 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.12 | 3.09 | 4.75 | 5.05 | 2.04 | 3.02 | 3.06 | |

# BLADE LOADS

TEST 509 CNTR NO. 163 T.C.P. 46 C.R. 56

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.9 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -3.35 | -4.76 | -4.91 | -5.34 | 0.37 | 1.96 | 1.69 | 0.0 |
| 5.00 | -2.36 | -5.01 | -5.36 | -4.76 | -1.72 | -1.95 | -2.02 | 5.00 |
| 10.00 | -1.19 | -3.44 | -3.75 | -3.79 | -2.42 | -2.72 | -3.08 | 10.00 |
| 15.00 | -0.66 | -2.71 | -2.93 | -3.28 | -2.23 | -1.86 | -1.91 | 15.00 |
| 20.00 | -0.54 | -1.91 | -2.94 | -2.72 | -1.43 | -0.17 | -0.29 | 20.00 |
| 25.00 | -0.73 | -2.58 | -2.51 | -1.59 | -0.16 | 1.26 | 0.65 | 25.00 |
| 30.00 | -1.27 | -2.49 | -1.80 | -0.36 | 0.83 | 2.18 | 1.26 | 30.00 |
| 35.00 | -1.36 | -1.76 | -1.07 | 0.74 | 1.73 | 3.29 | 2.31 | 35.00 |
| 40.00 | -0.70 | -1.49 | -0.19 | 1.79 | 2.84 | 4.62 | 3.74 | 40.00 |
| 45.00 | -0.69 | -1.32 | 0.63 | 2.65 | 3.90 | 5.78 | 4.99 | 45.00 |
| 50.00 | -0.80 | -1.13 | 1.07 | 4.09 | 4.69 | 6.74 | 5.80 | 50.00 |
| 55.00 | -0.62 | -1.01 | 1.26 | 4.71 | 4.95 | 7.60 | 5.84 | 55.00 |
| 60.00 | -0.31 | -0.95 | 1.46 | 4.83 | 4.76 | 7.57 | 5.53 | 60.00 |
| 65.00 | -0.24 | -0.82 | 1.71 | 4.65 | 4.38 | 6.38 | 5.41 | 65.00 |
| 70.00 | -0.42 | -0.95 | 1.80 | 4.40 | 3.95 | 4.54 | 6.32 | 70.00 |
| 75.00 | -0.56 | -0.23 | 1.71 | 4.04 | 3.23 | 4.01 | 4.22 | 75.00 |
| 80.00 | -0.34 | 0.25 | 1.58 | 3.56 | 2.09 | 4.12 | 0.83 | 80.00 |
| 85.00 | 0.05 | 0.78 | 1.59 | 2.79 | 0.48 | 5.38 | -2.85 | 85.00 |
| 90.00 | 0.66 | 1.34 | 1.57 | 1.89 | -1.30 | 0.71 | -4.59 | 90.00 |
| 95.00 | 1.22 | 1.92 | 1.65 | 1.29 | -3.26 | -4.26 | -5.77 | 95.00 |
| 100.00 | 1.85 | 2.45 | 1.99 | 0.79 | -5.49 | -10.82 | -6.56 | 100.00 |
| 105.00 | 2.40 | 2.97 | 2.42 | 0.13 | -7.28 | -13.49 | -8.34 | 105.00 |
| 110.00 | 2.96 | 3.47 | 2.73 | -0.94 | -8.45 | -13.85 | -11.76 | 110.00 |
| 115.00 | 3.44 | 3.96 | 2.90 | -2.19 | -8.81 | -12.22 | -13.87 | 115.00 |
| 120.00 | 3.85 | 4.42 | 3.01 | -3.12 | -8.82 | -10.34 | -13.52 | 120.00 |
| 125.00 | 4.11 | 4.82 | 3.03 | -3.55 | -8.76 | -10.72 | -11.27 | 125.00 |
| 130.00 | 4.14 | 5.16 | 2.96 | -3.54 | -8.68 | -10.79 | -10.75 | 130.00 |
| 135.00 | 4.10 | 5.46 | 2.86 | -3.23 | -8.39 | -10.11 | -10.48 | 135.00 |
| 140.00 | 4.08 | 5.75 | 2.80 | -2.50 | -7.41 | -8.95 | -9.29 | 140.00 |
| 145.00 | 4.16 | 6.26 | 2.94 | -1.52 | -6.54 | -7.82 | -8.11 | 145.00 |
| 150.00 | 4.42 | 6.35 | 3.43 | -0.55 | -5.33 | -6.58 | -7.05 | 150.00 |
| 155.00 | 4.66 | 6.62 | 4.02 | 0.38 | -4.12 | -5.24 | -5.94 | 155.00 |
| 160.00 | 4.76 | 6.85 | 4.68 | 1.14 | -2.99 | -3.83 | -4.58 | 160.00 |
| 165.00 | 4.51 | 6.96 | 5.14 | 1.98 | -1.67 | -2.41 | -3.08 | 165.00 |
| 170.00 | 4.09 | 6.89 | 5.54 | 2.81 | -0.52 | -1.11 | -1.82 | 170.00 |
| 175.00 | 3.47 | 6.57 | 5.70 | 3.35 | 0.45 | -0.11 | -0.75 | 175.00 |
| 180.00 | 2.73 | 5.96 | 5.56 | 3.54 | 1.15 | 0.57 | 0.19 | 180.00 |
| 185.00 | 1.90 | 5.01 | 5.07 | 3.39 | 1.63 | 1.05 | 0.69 | 185.00 |
| 190.00 | 0.97 | 3.83 | 4.29 | 3.13 | 1.83 | 1.27 | 1.09 | 190.00 |
| 195.00 | 0.09 | 2.55 | 3.45 | 2.79 | 1.82 | 1.35 | 1.31 | 195.00 |
| 200.00 | -0.58 | 1.35 | 2.53 | 2.31 | 1.73 | 1.28 | 1.34 | 200.00 |
| 205.00 | -0.94 | 0.41 | 1.54 | 1.70 | 1.59 | 1.12 | 1.29 | 205.00 |
| 210.00 | -1.10 | -0.32 | 0.77 | 1.07 | 1.43 | 0.96 | 1.24 | 210.00 |
| 215.00 | -1.51 | -0.88 | 0.15 | 0.53 | 1.26 | 0.84 | 1.20 | 215.00 |
| 220.00 | -1.83 | -1.26 | -0.33 | 0.01 | 1.10 | 0.73 | 1.25 | 220.00 |
| 225.00 | -2.06 | -1.55 | -0.75 | -0.30 | 1.07 | 0.63 | 1.31 | 225.00 |
| 230.00 | -2.17 | -1.85 | -1.14 | -0.56 | 0.97 | 0.57 | 1.47 | 230.00 |
| 235.00 | -2.18 | -2.13 | -1.49 | -0.79 | 0.92 | 0.60 | 1.66 | 235.00 |
| 240.00 | -2.14 | -2.39 | -1.82 | -1.03 | 0.93 | 0.69 | 1.98 | 240.00 |
| 245.00 | -2.07 | -2.62 | -2.11 | -1.15 | 1.02 | 0.83 | 2.10 | 245.00 |
| 250.00 | -2.02 | -2.89 | -2.36 | -1.28 | 1.16 | 1.31 | 2.30 | 250.00 |
| 255.00 | -1.97 | -2.91 | -2.52 | -1.40 | 1.32 | 1.19 | 2.58 | 255.00 |
| 260.00 | -1.93 | -2.99 | -2.61 | -1.46 | 1.48 | 1.34 | 2.73 | 260.00 |
| 265.00 | -1.90 | -3.02 | -2.66 | -1.49 | 1.62 | 1.57 | 2.98 | 265.00 |
| 270.00 | -1.86 | -3.01 | -2.68 | -1.51 | 1.64 | 1.76 | 3.21 | 270.00 |
| 275.00 | -1.81 | -3.00 | -2.68 | -1.51 | 1.76 | 1.99 | 3.63 | 275.00 |
| 280.00 | -1.78 | -2.96 | -2.63 | -1.48 | 1.88 | 2.23 | 3.69 | 280.00 |
| 285.00 | -1.77 | -2.92 | -2.57 | -1.42 | 2.02 | 2.45 | 3.91 | 285.00 |
| 290.00 | -1.77 | -2.88 | -2.52 | -1.26 | 2.20 | 2.68 | 4.12 | 290.00 |
| 295.00 | -1.77 | -2.85 | -2.46 | -1.05 | 2.40 | 2.99 | 4.35 | 295.00 |
| 300.00 | -1.74 | -2.80 | -2.44 | -0.83 | 2.62 | 3.36 | 4.57 | 300.00 |
| 305.00 | -1.73 | -2.73 | -2.41 | -0.63 | 2.84 | 3.73 | 4.71 | 305.00 |
| 310.00 | -1.62 | -2.62 | -2.50 | -0.41 | 3.05 | 3.99 | 4.78 | 310.00 |
| 315.00 | -1.49 | -2.51 | -2.53 | -0.32 | 3.19 | 4.22 | 4.83 | 315.00 |
| 320.00 | -1.30 | -2.43 | -2.36 | -0.32 | 3.28 | 4.34 | 4.82 | 320.00 |
| 325.00 | -1.16 | -2.36 | -2.37 | -0.38 | 3.03 | 4.32 | 4.68 | 325.00 |
| 330.00 | -1.17 | -2.31 | -2.03 | -0.42 | 2.65 | 3.99 | 4.35 | 330.00 |
| 335.00 | -1.28 | -2.37 | -3.47 | -0.39 | 2.22 | 3.41 | 3.68 | 335.00 |
| 340.00 | -1.43 | -2.59 | -3.76 | -0.28 | 1.98 | 2.85 | 3.05 | 340.00 |
| 345.00 | -1.29 | -2.96 | -3.73 | 0.03 | 2.20 | 2.61 | 2.61 | 345.00 |
| 350.00 | -1.18 | -3.49 | -3.98 | -2.89 | 2.21 | 2.51 | 2.54 | 350.00 |
| 355.00 | -2.18 | -4.44 | -4.49 | -3.93 | 1.96 | 2.43 | 3.14 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.15 | 2.93 | 3.23 | 3.42 | 1.84 | 2.16 | 1.99 | |

# BLADE LOADS

TEST 494 CNTR NO. 244 T.C.No. 47 C.R. 09

SPAN STATION

| DEG | 52.5 | 79.8 | 119.7 | 159.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -3.06 | -6.29 | -4.26 | -2.25 | -2.19 | -2.50 | -4.07 | 0.0 |
| 5.00 | -2.28 | -6.54 | -4.63 | -2.63 | -2.75 | -1.69 | -3.41 | 5.00 |
| 10.00 | -1.09 | -4.84 | -4.88 | -3.02 | -1.38 | -0.19 | -1.77 | 10.00 |
| 15.00 | -1.58 | -2.42 | -7.44 | -4.07 | -1.08 | 0.32 | -1.16 | 15.00 |
| 20.00 | -1.10 | -1.39 | -6.36 | -4.09 | -1.58 | -0.26 | -1.92 | 20.00 |
| 25.00 | -1.06 | -2.79 | -4.07 | -2.69 | -0.72 | 0.23 | -1.47 | 25.00 |
| 30.00 | -1.18 | -4.65 | -1.94 | -0.66 | 1.36 | 1.42 | -0.12 | 30.00 |
| 35.00 | -1.97 | -4.51 | -0.94 | 1.30 | 2.44 | 3.03 | 1.18 | 35.00 |
| 40.00 | -2.28 | -3.22 | -0.16 | 2.92 | 3.43 | 4.74 | 3.35 | 40.00 |
| 45.00 | -2.03 | -2.15 | 0.49 | 4.02 | 4.50 | 6.05 | 5.09 | 45.00 |
| 50.00 | -1.49 | -1.31 | 1.04 | 4.74 | 5.69 | 8.74 | 7.43 | 50.00 |
| 55.00 | -0.66 | -0.98 | 1.43 | 5.31 | 6.45 | 8.94 | 8.74 | 55.00 |
| 60.00 | -0.01 | -1.00 | 1.67 | 5.48 | 6.48 | 9.18 | 7.06 | 60.00 |
| 65.00 | 0.20 | -1.18 | 1.76 | 5.09 | 5.85 | 8.31 | 5.03 | 65.00 |
| 70.00 | 0.05 | -1.29 | 1.70 | 4.30 | 5.39 | 4.71 | 4.09 | 70.00 |
| 75.00 | -0.18 | -1.06 | 1.32 | 3.26 | 4.63 | 2.53 | 2.22 | 75.00 |
| 80.00 | -0.42 | -0.68 | 0.82 | 2.45 | 2.36 | 1.05 | -4.39 | 80.00 |
| 85.00 | -0.37 | -0.23 | 0.44 | 1.84 | 0.95 | -1.56 | -5.19 | 85.00 |
| 90.00 | -0.01 | 0.19 | 0.59 | 1.25 | -1.87 | -9.57 | -4.37 | 90.00 |
| 95.00 | 0.59 | 0.66 | 1.38 | 1.17 | -4.46 | -11.71 | -8.38 | 95.00 |
| 100.00 | 1.33 | 1.31 | 2.48 | 1.53 | -7.34 | -10.63 | -8.06 | 100.00 |
| 105.00 | 2.20 | 2.19 | 3.54 | 0.84 | -7.98 | -8.83 | -6.18 | 105.00 |
| 110.00 | 3.06 | 3.27 | 4.29 | -0.80 | -6.79 | -6.69 | -3.42 | 110.00 |
| 115.00 | 3.77 | 4.39 | 4.73 | -2.13 | -5.12 | -6.34 | -2.16 | 115.00 |
| 120.00 | 4.47 | 5.44 | 4.55 | -2.66 | -4.24 | -6.80 | -4.79 | 120.00 |
| 125.00 | 5.15 | 6.33 | 3.59 | -3.00 | -8.50 | -6.95 | -6.71 | 125.00 |
| 130.00 | 5.67 | 6.98 | 2.06 | -3.56 | -10.74 | -7.88 | -7.06 | 130.00 |
| 135.00 | 5.98 | 7.37 | 1.02 | -4.07 | -8.10 | -12.22 | -10.22 | 135.00 |
| 140.00 | 6.13 | 7.43 | 0.92 | -4.34 | -9.21 | -12.72 | -12.84 | 140.00 |
| 145.00 | 6.14 | 7.34 | 1.06 | -4.23 | -10.08 | -11.06 | -12.21 | 145.00 |
| 150.00 | 6.05 | 7.08 | 1.36 | -3.84 | -9.78 | -10.61 | -10.98 | 150.00 |
| 155.00 | 5.88 | 6.76 | 1.94 | -3.18 | -8.53 | -9.51 | -9.44 | 155.00 |
| 160.00 | 5.62 | 6.75 | 2.62 | -2.05 | -6.70 | -7.92 | -8.26 | 160.00 |
| 165.00 | 5.21 | 7.11 | 3.42 | -0.58 | -4.84 | -5.84 | -6.59 | 165.00 |
| 170.00 | 4.68 | 7.54 | 4.24 | 0.89 | -3.79 | -3.66 | -4.44 | 170.00 |
| 175.00 | 4.07 | 7.67 | 4.92 | 2.26 | -1.39 | -1.54 | -2.41 | 175.00 |
| 180.00 | 3.29 | 7.25 | 5.33 | 3.08 | 0.35 | 0.14 | -0.62 | 180.00 |
| 185.00 | 2.34 | 6.35 | 5.28 | 3.33 | 1.22 | 1.49 | 0.90 | 185.00 |
| 190.00 | 1.21 | 4.98 | 4.72 | 3.15 | 2.03 | 2.17 | 1.83 | 190.00 |
| 195.00 | 0.81 | 3.23 | 3.84 | 2.85 | 2.41 | 2.95 | 2.31 | 195.00 |
| 200.00 | -0.94 | 1.69 | 2.80 | 2.54 | 2.65 | 2.83 | 2.49 | 200.00 |
| 205.00 | -1.59 | 0.39 | 1.79 | 2.17 | 2.66 | 2.95 | 2.52 | 205.00 |
| 210.00 | -2.10 | -0.54 | 0.95 | 1.75 | 2.47 | 2.45 | 2.47 | 210.00 |
| 215.00 | -2.49 | -1.19 | 0.33 | 1.33 | 2.33 | 2.34 | 2.47 | 215.00 |
| 220.00 | -2.69 | -1.71 | -0.17 | 0.95 | 2.26 | 2.24 | 2.51 | 220.00 |
| 225.00 | -2.68 | -2.09 | -0.51 | 0.58 | 2.24 | 2.15 | 2.58 | 225.00 |
| 230.00 | -2.56 | -2.39 | -0.90 | 0.40 | 2.25 | 2.17 | 2.77 | 230.00 |
| 235.00 | -2.43 | -2.62 | -1.26 | 0.16 | 2.29 | 2.27 | 2.84 | 235.00 |
| 240.00 | -2.33 | -2.76 | -1.58 | -0.04 | 2.31 | 2.40 | 2.97 | 240.00 |
| 245.00 | -2.28 | -2.80 | -1.86 | -0.23 | 2.32 | 2.52 | 3.11 | 245.00 |
| 250.00 | -2.30 | -2.78 | -2.05 | -0.41 | 2.31 | 2.58 | 3.25 | 250.00 |
| 255.00 | -2.36 | -2.74 | -2.14 | -0.59 | 2.26 | 2.69 | 3.36 | 255.00 |
| 260.00 | -2.27 | -2.72 | -2.16 | -0.74 | 2.20 | 2.59 | 3.42 | 260.00 |
| 265.00 | -2.23 | -2.68 | -2.15 | -0.87 | 2.14 | 2.59 | 3.45 | 265.00 |
| 270.00 | -2.20 | -2.62 | -2.11 | -0.95 | 2.13 | 2.62 | 3.47 | 270.00 |
| 275.00 | -2.20 | -2.58 | -2.05 | -0.95 | 2.18 | 2.67 | 3.50 | 275.00 |
| 280.00 | -2.20 | -2.55 | -1.97 | -0.89 | 2.31 | 2.77 | 3.47 | 280.00 |
| 285.00 | -2.13 | -2.52 | -1.94 | -0.79 | 2.52 | 2.93 | 3.48 | 285.00 |
| 290.00 | -2.08 | -2.46 | -1.93 | -0.65 | 2.79 | 3.09 | 3.84 | 290.00 |
| 295.00 | -2.06 | -2.45 | -1.94 | -0.48 | 3.04 | 3.34 | 4.03 | 295.00 |
| 300.00 | -2.11 | -2.54 | -1.93 | -0.29 | 3.26 | 3.61 | 4.28 | 300.00 |
| 305.00 | -2.05 | -2.52 | -1.91 | -0.06 | 3.42 | 3.89 | 4.55 | 305.00 |
| 310.00 | -1.88 | -2.34 | -1.92 | 0.15 | 3.53 | 4.21 | 4.75 | 310.00 |
| 315.00 | -1.63 | -2.12 | -1.95 | 0.39 | 3.57 | 4.43 | 4.88 | 315.00 |
| 320.00 | -1.36 | -1.92 | -1.95 | 0.59 | 3.58 | 4.62 | 4.96 | 320.00 |
| 325.00 | -0.98 | -1.72 | -1.89 | 0.39 | 3.58 | 4.64 | 4.88 | 325.00 |
| 330.00 | -0.50 | -1.54 | -1.73 | -0.36 | 3.53 | 4.62 | 4.84 | 330.00 |
| 335.00 | -0.19 | -1.40 | -1.52 | -1.57 | 3.20 | 4.38 | 4.36 | 335.00 |
| 340.00 | -0.64 | -2.13 | -1.23 | -2.48 | 2.42 | 3.94 | 3.82 | 340.00 |
| 345.00 | -1.64 | -2.98 | -0.99 | -2.66 | 0.71 | 2.44 | 3.02 | 345.00 |
| 350.00 | -2.57 | -4.03 | -1.36 | -1.76 | -1.30 | -0.08 | 1.48 | 350.00 |
| 355.00 | -2.87 | -5.40 | -2.68 | -1.03 | -2.32 | -2.41 | -1.64 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.63 | 2.18 | 2.36 | 1.52 | 0.73 | -0.61 | -0.49 | |

# BLADE LOADS

TEST 502 CNTR NO. 242 T.C.N. 48 C.R. 47

SPAN STATION

| AZM | 92.5 | 79.8 | 119.7 | 159.5 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | | DYNAMIC COMPONENTS | | | | |
| 0.0 | -2.22 | -3.29 | -3.11 | -2.05 | 0.19 | 0.73 | 0.64 | 0.0 |
| 5.00 | -1.69 | -2.82 | -2.36 | -2.19 | 0.07 | 0.13 | -0.22 | 5.00 |
| 10.00 | -1.29 | -2.07 | -1.95 | -2.25 | -0.03 | 0.04 | -0.04 | 10.00 |
| 15.00 | -0.47 | -1.94 | -1.77 | -1.57 | 0.20 | 1.25 | 0.41 | 15.00 |
| 20.00 | 0.93 | -1.09 | -1.95 | -0.74 | 0.59 | 1.74 | 0.81 | 20.00 |
| 25.00 | -0.19 | -1.77 | -1.20 | -0.15 | 1.01 | 2.90 | 1.44 | 25.00 |
| 30.00 | -1.28 | -1.24 | -0.83 | 0.56 | 1.42 | 3.44 | 2.27 | 30.00 |
| 35.00 | -1.32 | -0.96 | -0.36 | 1.49 | 2.05 | 4.21 | 3.10 | 35.00 |
| 40.00 | -0.77 | -0.63 | 0.27 | 2.49 | 3.00 | 4.93 | 3.84 | 40.00 |
| 45.00 | -0.41 | -0.43 | 0.89 | 3.33 | 4.01 | 5.36 | 4.44 | 45.00 |
| 50.00 | -0.22 | -0.25 | 1.36 | 3.87 | 4.87 | 5.99 | 4.68 | 50.00 |
| 55.00 | -0.12 | -0.00 | 1.66 | 3.99 | 5.08 | 5.43 | 4.45 | 55.00 |
| 60.00 | -0.01 | 0.14 | 1.67 | 3.76 | 5.20 | 4.67 | 3.72 | 60.00 |
| 65.00 | 0.12 | 0.49 | 1.55 | 3.44 | 2.39 | 3.44 | 2.60 | 65.00 |
| 70.00 | 0.28 | 0.87 | 1.47 | 2.91 | 1.43 | 1.87 | 1.48 | 70.00 |
| 75.00 | 0.52 | 1.28 | 1.51 | 2.31 | 0.44 | 0.27 | 0.32 | 75.00 |
| 80.00 | 0.78 | 1.68 | 1.53 | 1.73 | -0.55 | -1.28 | -1.13 | 80.00 |
| 85.00 | 1.22 | 2.11 | 1.55 | 1.26 | -1.48 | -2.80 | -2.91 | 85.00 |
| 90.00 | 1.34 | 2.52 | 1.41 | 1.05 | -2.27 | -4.48 | -4.58 | 90.00 |
| 95.00 | 1.72 | 2.86 | 1.72 | 2.38 | -3.00 | -5.63 | -5.00 | 95.00 |
| 100.00 | 2.28 | 3.18 | 1.82 | 0.77 | -3.82 | -6.68 | -7.12 | 100.00 |
| 105.00 | 2.62 | 3.47 | 1.89 | 0.37 | -4.47 | -7.34 | -7.97 | 105.00 |
| 110.00 | 2.93 | 3.71 | 1.91 | 0.02 | -4.99 | -7.86 | -8.52 | 110.00 |
| 115.00 | 3.18 | 3.97 | 1.94 | -0.51 | -5.38 | -8.12 | -8.82 | 115.00 |
| 120.00 | 3.37 | 4.11 | 2.02 | -1.03 | -5.62 | -8.13 | -8.80 | 120.00 |
| 125.00 | 3.50 | 4.31 | 2.11 | -1.35 | -5.69 | -7.98 | -8.51 | 125.00 |
| 130.00 | 3.58 | 4.51 | 2.19 | -1.45 | -5.53 | -7.66 | -8.19 | 130.00 |
| 135.00 | 3.61 | 4.67 | 2.33 | -1.35 | -5.16 | -6.85 | -7.73 | 135.00 |
| 140.00 | 3.57 | 4.89 | 2.55 | -1.08 | -4.63 | -6.14 | -7.06 | 140.00 |
| 145.00 | 3.49 | 4.91 | 2.79 | -0.63 | -3.98 | -5.38 | -6.28 | 145.00 |
| 150.00 | 3.37 | 5.05 | 3.06 | -0.07 | -3.27 | -4.58 | -5.43 | 150.00 |
| 155.00 | 3.28 | 5.06 | 3.33 | 0.53 | -2.54 | -3.75 | -4.55 | 155.00 |
| 160.00 | 2.97 | 5.03 | 3.65 | 1.37 | -1.83 | -2.93 | -3.65 | 160.00 |
| 165.00 | 2.64 | 4.96 | 3.98 | 1.97 | -1.18 | -2.18 | -2.69 | 165.00 |
| 170.00 | 2.25 | 4.75 | 4.03 | 1.84 | -0.51 | -1.57 | -1.80 | 170.00 |
| 175.00 | 1.83 | 4.38 | 3.96 | 1.94 | -0.18 | -1.33 | -1.00 | 175.00 |
| 180.00 | 1.32 | 3.78 | 3.66 | 1.89 | 0.14 | -0.58 | -0.58 | 180.00 |
| 185.00 | 0.80 | 3.04 | 3.13 | 1.71 | 0.30 | -0.21 | -0.22 | 185.00 |
| 190.00 | 0.25 | 2.25 | 2.44 | 1.45 | 0.30 | 0.09 | 0.02 | 190.00 |
| 195.00 | -0.28 | 1.49 | 1.78 | 1.14 | 0.39 | 0.15 | 0.15 | 195.00 |
| 200.00 | -0.71 | 0.78 | 1.05 | 0.81 | 0.35 | 0.12 | 0.25 | 200.00 |
| 205.00 | -0.94 | 0.12 | 0.54 | 0.46 | 0.28 | 0.23 | 0.30 | 205.00 |
| 210.00 | -1.01 | -0.43 | 0.00 | 0.10 | 0.21 | -0.11 | 0.34 | 210.00 |
| 215.00 | -1.18 | -0.91 | -0.34 | -0.15 | 0.16 | -0.19 | 0.38 | 215.00 |
| 220.00 | -1.37 | -1.38 | -0.78 | -0.41 | 0.16 | -0.17 | 0.48 | 220.00 |
| 225.00 | -1.58 | -1.62 | -1.01 | -0.62 | 0.20 | -0.07 | 0.64 | 225.00 |
| 230.00 | -1.58 | -1.92 | -1.28 | -0.78 | 0.29 | 0.07 | 0.90 | 230.00 |
| 235.00 | -1.60 | -2.13 | -1.54 | -0.89 | 0.43 | 0.23 | 1.18 | 235.00 |
| 240.00 | -1.59 | -2.21 | -1.76 | -0.94 | 0.62 | 0.47 | 1.48 | 240.00 |
| 245.00 | -1.62 | -2.18 | -1.97 | -1.01 | 0.82 | 0.74 | 1.84 | 245.00 |
| 250.00 | -1.64 | -2.12 | -2.13 | -1.08 | 1.03 | 1.02 | 2.21 | 250.00 |
| 255.00 | -1.64 | -2.08 | -2.27 | -1.13 | 1.21 | 1.34 | 2.58 | 255.00 |
| 260.00 | -1.58 | -2.08 | -2.39 | -1.09 | 1.48 | 1.68 | 2.94 | 260.00 |
| 265.00 | -1.53 | -2.01 | -2.58 | -1.06 | 1.58 | 2.38 | 3.27 | 265.00 |
| 270.00 | -1.52 | -2.06 | -2.59 | -1.03 | 1.70 | 2.32 | 3.53 | 270.00 |
| 275.00 | -1.53 | -2.69 | -2.66 | -1.33 | 1.81 | 2.63 | 3.72 | 275.00 |
| 280.00 | -1.53 | -2.65 | -2.73 | -1.35 | 1.87 | 2.69 | 3.82 | 280.00 |
| 285.00 | -1.47 | -2.60 | -2.83 | -1.36 | 1.88 | 3.00 | 3.73 | 285.00 |
| 290.00 | -1.48 | -2.58 | -2.94 | -1.32 | 1.85 | 3.33 | 3.54 | 290.00 |
| 295.00 | -1.43 | -2.69 | -3.03 | -0.92 | 1.81 | 3.31 | 3.32 | 295.00 |
| 300.00 | -1.52 | -2.63 | -3.07 | -5.93 | 1.84 | 3.37 | 3.22 | 300.00 |
| 305.00 | -1.61 | -2.54 | -3.03 | -3.76 | 1.97 | 3.24 | 3.37 | 305.00 |
| 310.00 | -1.69 | -2.54 | -2.92 | -0.75 | 2.05 | 3.48 | 3.58 | 310.00 |
| 315.00 | -1.68 | -2.61 | -2.98 | -0.88 | 2.07 | 3.50 | 3.80 | 315.00 |
| 320.00 | -1.65 | -2.73 | -3.03 | -0.98 | 1.97 | 3.43 | 3.94 | 320.00 |
| 325.00 | -1.51 | -2.76 | -2.88 | -1.03 | 1.52 | 2.92 | 3.79 | 325.00 |
| 330.00 | -1.06 | -2.84 | -1.89 | -1.18 | 0.99 | 2.28 | 3.39 | 330.00 |
| 335.00 | -0.67 | -3.04 | -0.85 | -1.32 | 0.59 | 1.67 | 2.99 | 335.00 |
| 340.00 | -0.68 | -3.01 | 1.36 | -1.57 | 0.59 | 2.13 | 3.08 | 340.00 |
| 345.00 | -1.19 | -4.27 | 0.06 | -1.98 | 0.97 | 2.00 | 3.05 | 345.00 |
| 350.00 | -2.14 | -4.68 | -2.78 | -2.62 | 0.77 | 2.11 | 2.93 | 350.00 |
| 355.00 | -2.91 | -4.87 | -4.14 | -2.85 | 0.12 | 0.95 | 2.23 | 355.00 |
| | | | | STATIC COMPONENTS | | | | |
| | 1.91 | 3.48 | 4.60 | 5.25 | 3.26 | 4.58 | 3.39 | |

# BLADE LOADS

TEST 903 CNTR NO. 178 T.C.N. 49 C.R. 57

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.3 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.81 | -5.74 | -5.11 | -3.95 | -0.79 | 0.47 | -0.13 | 0.0 |
| 5.00 | -2.35 | -4.63 | -4.65 | -3.18 | -2.16 | -0.29 | -0.73 | 5.00 |
| 10.00 | -1.93 | -3.42 | -2.96 | -3.32 | -1.67 | -0.37 | -0.91 | 10.00 |
| 15.00 | -0.59 | -2.24 | -2.60 | -2.47 | -0.87 | 0.90 | -0.02 | 15.00 |
| 20.00 | -1.16 | -2.91 | -2.54 | -1.91 | 0.08 | 1.35 | 0.74 | 20.00 |
| 25.00 | -2.14 | -2.93 | -1.91 | -0.56 | 0.97 | 2.22 | 1.43 | 25.00 |
| 30.00 | -2.54 | -2.25 | -1.03 | 0.38 | 1.91 | 3.30 | 2.57 | 30.00 |
| 35.00 | -1.34 | -1.81 | -0.30 | 1.53 | 3.01 | 4.71 | 4.11 | 35.00 |
| 40.00 | -0.81 | -1.59 | 0.37 | 2.85 | 4.01 | 5.99 | 5.41 | 40.00 |
| 45.00 | -0.84 | -1.33 | 1.06 | 4.03 | 4.79 | 6.83 | 5.95 | 45.00 |
| 50.00 | -0.72 | -1.14 | 1.59 | 4.56 | 5.04 | 7.40 | 6.00 | 50.00 |
| 55.00 | -0.54 | -0.97 | 1.81 | 4.83 | 4.92 | 7.38 | 5.35 | 55.00 |
| 60.00 | -0.49 | -0.81 | 1.75 | 4.78 | 4.56 | 6.46 | 4.45 | 60.00 |
| 65.00 | -0.52 | -0.64 | 1.66 | 4.63 | 4.03 | .11 | 0.31 | 65.00 |
| 70.00 | -0.59 | -0.39 | 1.53 | 4.06 | 3.30 | 4.87 | 4.55 | 70.00 |
| 75.00 | -0.47 | 0.06 | 1.41 | 3.51 | 2.82 | 3.75 | 0.90 | 75.00 |
| 80.00 | -0.10 | 0.63 | 1.37 | 2.86 | 0.39 | 3.01 | -2.27 | 80.00 |
| 85.00 | 0.51 | 1.16 | 1.47 | 1.98 | -1.27 | 0.93 | -5.07 | 85.00 |
| 90.00 | 1.15 | 1.72 | 1.65 | 1.16 | -3.24 | -2.59 | -6.54 | 90.00 |
| 95.00 | 1.78 | 2.23 | 1.94 | 0.58 | -5.36 | -7.64 | -7.66 | 95.00 |
| 100.00 | 2.41 | 2.87 | 2.29 | 0.18 | -7.65 | -14.29 | -9.12 | 100.00 |
| 105.00 | 3.03 | 3.45 | 2.61 | -0.77 | -8.96 | -15.39 | -11.12 | 105.00 |
| 110.00 | 3.63 | 3.98 | 2.82 | -2.09 | -9.32 | -14.56 | -14.47 | 110.00 |
| 115.00 | 4.13 | 4.51 | 2.96 | -3.27 | -9.78 | -12.19 | -14.89 | 115.00 |
| 120.00 | 4.48 | 5.05 | 2.97 | -3.88 | -9.89 | -11.36 | -13.80 | 120.00 |
| 125.00 | 4.70 | 5.47 | 2.98 | -3.95 | -9.69 | -13.69 | -11.45 | 125.00 |
| 130.00 | 4.87 | 5.81 | 2.93 | -3.81 | -9.38 | -10.16 | -11.51 | 130.00 |
| 135.00 | 5.05 | 6.10 | 2.96 | -2.97 | -8.71 | -9.89 | -10.45 | 135.00 |
| 140.00 | 5.19 | 6.38 | 3.39 | -2.14 | -7.68 | -8.85 | -8.93 | 140.00 |
| 145.00 | 5.28 | 6.64 | 3.48 | -1.15 | -6.48 | -7.39 | -7.61 | 145.00 |
| 150.00 | 5.27 | 6.86 | 3.98 | -0.33 | -5.65 | -5.88 | -0.22 | 150.00 |
| 155.00 | 5.15 | 7.04 | 4.50 | 1.02 | -3.65 | -4.48 | -4.76 | 155.00 |
| 160.00 | 4.88 | 7.17 | 5.04 | 1.77 | -2.22 | -3.10 | -3.46 | 160.00 |
| 165.00 | 4.43 | 7.17 | 5.53 | 2.53 | -0.96 | -1.77 | -2.21 | 165.00 |
| 170.00 | 3.95 | 6.95 | 5.87 | 3.12 | -0.19 | -0.68 | -1.16 | 170.00 |
| 175.00 | 3.19 | 6.39 | 5.90 | 3.39 | 0.62 | 0.24 | -0.32 | 175.00 |
| 180.00 | 2.18 | 5.47 | 5.59 | 3.47 | 1.08 | 0.52 | 0.41 | 180.00 |
| 185.00 | 1.37 | 4.32 | 5.12 | 3.35 | 1.40 | 0.95 | 0.95 | 185.00 |
| 190.00 | 0.21 | 2.98 | 4.17 | 2.98 | 1.62 | 1.22 | 1.38 | 190.00 |
| 195.00 | -0.29 | 1.62 | 3.12 | 2.51 | 1.64 | 1.38 | 1.48 | 195.00 |
| 200.00 | -0.67 | 0.55 | 2.09 | 1.99 | 1.51 | 1.20 | 1.54 | 200.00 |
| 205.00 | -1.31 | -0.28 | 1.17 | 1.43 | 1.36 | 1.03 | 1.51 | 205.00 |
| 210.00 | -1.86 | -0.73 | 0.44 | 0.82 | 1.18 | 0.85 | 1.45 | 210.00 |
| 215.00 | -1.95 | -1.04 | -0.21 | 0.30 | 0.99 | 0.73 | 1.38 | 215.00 |
| 220.00 | -2.03 | -1.39 | -0.68 | -0.11 | 0.91 | 0.62 | 1.42 | 220.00 |
| 225.00 | -2.08 | -1.81 | -1.64 | -0.52 | 0.79 | 0.54 | 1.56 | 225.00 |
| 230.00 | -2.09 | -2.24 | -1.60 | -0.87 | 0.73 | 0.51 | 1.69 | 230.00 |
| 235.00 | -2.09 | -2.64 | -1.74 | -1.13 | 0.75 | 0.54 | 1.84 | 235.00 |
| 240.00 | -2.05 | -2.86 | -2.08 | -1.33 | 0.82 | 0.61 | 1.98 | 240.00 |
| 245.00 | -2.01 | -2.97 | -2.39 | -1.59 | 0.92 | 0.73 | 2.13 | 245.00 |
| 250.00 | -1.99 | -3.06 | -2.63 | -1.62 | 1.03 | 0.94 | 2.31 | 250.00 |
| 255.00 | -1.99 | -3.14 | -2.78 | -1.73 | 1.15 | 1.19 | 2.59 | 255.00 |
| 260.00 | -2.01 | -3.19 | -2.82 | -1.74 | 1.27 | 1.47 | 2.92 | 260.00 |
| 265.00 | -2.00 | -3.20 | -2.80 | -1.77 | 1.43 | 1.69 | 3.24 | 265.00 |
| 270.00 | -1.95 | -3.17 | -2.75 | -1.69 | 1.57 | 1.88 | 3.54 | 270.00 |
| 275.00 | -1.89 | -3.11 | -2.72 | -1.64 | 1.62 | 2.04 | 3.80 | 275.00 |
| 280.00 | -1.84 | -3.07 | -2.72 | -1.54 | 1.84 | 2.36 | 4.07 | 280.00 |
| 285.00 | -1.81 | -3.02 | -2.73 | -1.58 | 2.09 | 2.59 | 4.36 | 285.00 |
| 290.00 | -1.81 | -2.96 | -2.66 | -1.18 | 2.39 | 2.94 | 4.67 | 290.00 |
| 295.00 | -1.77 | -2.88 | -2.64 | -0.94 | 2.70 | 3.34 | 4.94 | 295.00 |
| 300.00 | -1.63 | -2.82 | -2.67 | -0.71 | 2.99 | 3.73 | 5.16 | 300.00 |
| 305.00 | -1.52 | -2.74 | -2.75 | -0.49 | 3.22 | 4.16 | 5.31 | 305.00 |
| 310.00 | -1.44 | -2.66 | -2.88 | -0.33 | 3.36 | 4.56 | 5.40 | 310.00 |
| 315.00 | -1.39 | -2.57 | -2.54 | -0.25 | 3.45 | 4.80 | 5.41 | 315.00 |
| 320.00 | -1.25 | 2.49 | -2.64 | -0.33 | 3.37 | 4.84 | 5.31 | 320.00 |
| 325.00 | -1.22 | -2.45 | -3.64 | -0.31 | 3.13 | 4.77 | 5.07 | 325.00 |
| 330.00 | -1.34 | -2.47 | -3.59 | -0.21 | 2.84 | 4.52 | 4.59 | 330.00 |
| 335.00 | -1.66 | -2.79 | -3.40 | 0.45 | 2.59 | 4.23 | 4.01 | 335.00 |
| 340.00 | -1.74 | -3.13 | -3.83 | 1.55 | 3.22 | 4.18 | 3.82 | 340.00 |
| 345.00 | -1.51 | -2.98 | -3.98 | -1.78 | 4.05 | 4.73 | 3.67 | 345.00 |
| 350.00 | -1.91 | -2.21 | -4.33 | -3.49 | 5.72 | 3.18 | 1.40 | 350.00 |
| 355.00 | -2.81 | -4.67 | -5.25 | -3.54 | 2.67 | 0.88 | -0.32 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 3.74 | 2.82 | 3.15 | 3.48 | 2.04 | 2.28 | 1.42 | |

# BLADE LOADS

TEST 694 CNTR NO. 296 T.C.No. 50 C.R. 10

SPAN STATION

| DEG | 92.5 | 79.8 | 119.7 | 153.9 | 178.5 | 189.0 | 199.5 | |
|---|---|---|---|---|---|---|---|---|
| | | | DYNAMIC COMPONENTS | | | | | |
| 0.0 | -2.88 | -7.69 | -5.83 | -2.65 | -1.78 | -1.49 | -3.17 | 0.0 |
| 5.00 | -1.82 | -6.58 | -7.07 | -0.69 | -2.91 | -0.96 | 0.15 | 5.00 |
| 10.00 | -1.68 | -4.21 | -7.61 | -2.64 | -2.44 | -1.05 | -1.83 | 10.00 |
| 15.00 | -1.87 | -2.97 | -4.93 | -4.52 | -2.14 | -1.17 | -2.38 | 15.00 |
| 20.00 | -0.59 | -3.44 | -4.78 | -3.77 | -1.55 | -0.37 | -1.92 | 20.00 |
| 25.00 | -1.96 | -3.71 | -2.42 | -1.75 | 0.06 | 1.23 | -0.38 | 25.00 |
| 30.00 | -3.06 | -3.61 | -1.03 | 0.48 | 1.64 | 2.72 | -1.36 | 30.00 |
| 35.00 | -2.93 | -3.13 | -0.22 | 2.34 | 2.05 | 4.31 | -1.37 | 35.00 |
| 40.00 | -2.22 | -2.22 | 0.44 | 3.63 | 4.13 | 5.89 | 3.15 | 40.00 |
| 45.00 | -1.22 | -1.40 | 1.12 | 4.73 | 5.52 | 7.41 | 6.95 | 45.00 |
| 50.00 | -0.45 | -0.96 | 1.69 | 5.48 | 6.58 | 9.07 | 8.43 | 50.00 |
| 55.00 | 0.05 | -0.91 | 1.99 | 5.86 | 7.07 | 9.78 | 8.99 | 55.00 |
| 60.00 | 0.21 | -1.04 | 2.04 | 5.69 | 6.47 | 9.57 | 6.47 | 60.00 |
| 65.00 | 0.04 | -1.12 | 1.80 | 4.89 | 4.85 | 7.89 | 4.72 | 65.00 |
| 70.00 | -0.19 | -0.99 | 1.23 | 3.60 | 5.56 | 3.59 | 4.63 | 70.00 |
| 75.00 | -0.33 | -0.71 | 0.55 | 2.39 | 3.58 | 1.34 | -1.04 | 75.00 |
| 80.00 | -0.28 | -0.36 | 0.14 | 1.58 | 1.16 | 0.39 | -7.09 | 80.00 |
| 85.00 | -0.01 | 0.10 | 0.20 | 0.93 | -0.46 | -7.22 | -9.04 | 85.00 |
| 90.00 | 0.50 | 0.67 | 0.99 | 0.35 | -3.37 | -11.76 | -9.48 | 90.00 |
| 95.00 | 1.25 | 1.49 | 2.15 | 1.16 | -4.52 | -12.65 | -9.09 | 95.00 |
| 100.00 | 2.13 | 2.44 | 3.90 | 1.33 | -7.83 | -10.09 | -6.54 | 100.00 |
| 105.00 | 3.05 | 3.54 | 4.57 | -0.01 | -7.12 | -8.21 | -4.02 | 105.00 |
| 110.00 | 3.92 | 4.58 | 5.12 | -1.54 | -5.74 | -6.88 | -2.41 | 110.00 |
| 115.00 | 4.72 | 5.49 | 5.11 | -2.33 | -4.05 | -6.49 | -2.38 | 115.00 |
| 120.00 | 5.42 | 6.56 | 4.39 | -2.78 | -6.23 | -7.13 | -4.63 | 120.00 |
| 125.00 | 5.93 | 7.34 | 2.77 | -1.38 | -11.11 | -6.47 | -7.48 | 125.00 |
| 130.00 | 6.29 | 7.75 | 1.27 | -4.02 | -8.92 | -13.01 | -7.01 | 130.00 |
| 135.00 | 6.51 | 7.88 | 0.41 | -4.56 | -7.80 | -12.32 | -12.19 | 135.00 |
| 140.00 | 6.56 | 7.73 | 1.03 | -4.69 | -9.41 | -11.62 | -13.07 | 140.00 |
| 145.00 | 6.51 | 7.44 | 1.28 | -4.37 | -10.95 | -11.51 | -11.81 | 145.00 |
| 150.00 | 6.38 | 7.15 | 1.71 | -3.69 | -9.73 | -10.28 | -10.79 | 150.00 |
| 155.00 | 5.98 | 7.01 | 2.41 | -2.54 | -8.21 | -8.93 | -9.33 | 155.00 |
| 160.00 | 5.56 | 7.14 | 3.19 | -1.02 | -6.40 | -6.82 | -7.68 | 160.00 |
| 165.00 | 5.03 | 7.49 | 3.94 | 0.56 | -4.47 | -4.78 | -5.51 | 165.00 |
| 170.00 | 4.34 | 7.52 | 4.49 | 1.88 | -2.48 | -2.76 | -3.27 | 170.00 |
| 175.00 | 3.48 | 7.50 | 5.29 | 2.98 | -0.65 | -0.80 | -1.19 | 175.00 |
| 180.00 | 2.42 | 6.89 | 5.41 | 3.43 | 0.88 | 0.85 | 0.62 | 180.00 |
| 185.00 | 1.23 | 5.61 | 4.95 | 3.34 | 1.94 | 1.99 | 1.77 | 185.00 |
| 190.00 | 0.09 | 3.93 | 4.13 | 3.11 | 2.55 | 2.61 | 2.48 | 190.00 |
| 195.00 | -0.87 | 2.16 | 3.18 | 2.88 | 2.88 | 2.87 | 2.68 | 195.00 |
| 200.00 | -1.51 | 0.81 | 2.21 | 2.43 | 2.74 | 2.92 | 2.58 | 200.00 |
| 205.00 | -2.03 | -0.41 | 1.29 | 1.99 | 2.59 | 2.31 | 2.50 | 205.00 |
| 210.00 | -2.45 | -1.16 | 0.54 | 1.54 | 2.48 | 2.16 | 2.49 | 210.00 |
| 215.00 | -2.74 | -1.67 | -0.07 | 1.16 | 2.49 | 2.09 | 2.56 | 215.00 |
| 220.00 | -2.84 | -2.15 | -0.49 | 0.79 | 2.33 | 2.09 | 2.64 | 220.00 |
| 225.00 | -2.89 | -2.34 | -0.82 | 0.45 | 2.25 | 2.14 | 2.76 | 225.00 |
| 230.00 | -2.85 | -2.81 | -1.16 | 0.15 | 2.25 | 2.27 | 2.89 | 230.00 |
| 235.00 | -2.73 | -2.95 | -1.54 | -0.04 | 2.28 | 2.46 | 3.02 | 235.00 |
| 240.00 | -2.59 | -3.00 | -1.88 | -0.24 | 2.38 | 2.59 | 3.14 | 240.00 |
| 245.00 | -2.49 | -3.01 | -2.12 | -0.58 | 2.25 | 2.67 | 3.23 | 245.00 |
| 250.00 | -2.46 | -3.04 | -2.26 | -0.78 | 2.15 | 2.68 | 3.29 | 250.00 |
| 255.00 | -2.45 | -3.06 | -2.33 | -0.89 | 2.06 | 2.66 | 3.36 | 255.00 |
| 260.00 | -2.39 | -2.99 | -2.33 | -1.05 | 2.00 | 2.65 | 3.45 | 260.00 |
| 265.00 | -2.34 | -2.95 | -2.30 | -1.17 | 2.00 | 2.66 | 3.55 | 265.00 |
| 270.00 | -2.30 | -2.81 | -2.25 | -1.24 | 2.05 | 2.70 | 3.68 | 270.00 |
| 275.00 | -2.31 | -2.77 | -2.20 | -1.21 | 2.14 | 2.77 | 3.65 | 275.00 |
| 280.00 | -2.33 | -2.73 | -2.14 | -1.08 | 2.26 | 2.98 | 3.72 | 280.00 |
| 285.00 | -2.25 | -2.76 | -2.08 | -0.89 | 2.41 | 3.04 | 3.82 | 285.00 |
| 290.00 | -2.11 | -2.72 | -2.04 | -0.66 | 2.62 | 3.26 | 4.02 | 290.00 |
| 295.00 | -2.00 | -2.70 | -2.03 | -0.43 | 2.87 | 3.44 | 4.27 | 295.00 |
| 300.00 | -2.13 | -2.71 | -2.02 | -0.21 | 3.13 | 3.84 | 4.59 | 300.00 |
| 305.00 | -2.00 | -2.61 | -2.01 | -0.02 | 3.37 | 4.09 | 4.81 | 305.00 |
| 310.00 | -1.79 | -2.45 | -1.99 | 0.18 | 3.55 | 4.33 | 5.07 | 310.00 |
| 315.00 | -1.49 | -2.25 | -1.97 | 0.31 | 3.66 | 4.58 | 5.26 | 315.00 |
| 320.00 | -1.18 | -2.06 | -1.92 | 0.49 | 3.74 | 4.76 | 5.35 | 320.00 |
| 325.00 | -0.81 | -1.78 | -1.91 | 0.29 | 4.02 | 4.89 | 5.32 | 325.00 |
| 330.00 | -0.43 | -1.61 | -1.52 | -0.03 | 4.19 | 4.79 | 5.12 | 330.00 |
| 335.00 | -0.63 | -1.91 | -1.11 | -2.16 | 3.79 | 4.57 | 4.82 | 335.00 |
| 340.00 | -1.22 | -2.56 | -0.83 | -2.63 | 2.29 | 3.92 | 4.21 | 340.00 |
| 345.00 | -1.68 | -2.85 | -0.95 | -2.14 | 0.04 | 1.78 | 2.44 | 345.00 |
| 350.00 | -1.98 | -4.04 | -1.76 | -1.29 | -1.54 | -0.61 | -0.62 | 350.00 |
| 355.00 | -2.65 | -4.12 | -3.79 | -1.09 | -1.96 | -1.85 | -3.31 | 355.00 |
| | | | STATIC COMPONENTS | | | | | |
| | 1.77 | 2.40 | 2.48 | 1.94 | 1.82 | -0.20 | -0.24 | |

## APPENDIX VIII

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

This appendix presents the harmonic components of the lumped lift loads (normal force in pounds) and the pitching moments (blade feathering moments in inch-pounds) for the selected span stations as listed in Table III of Appendix I. These data were used as input in the correlation phase of the research program. Harmonics for 20 test conditions are presented.

The symbols used are:

| | |
|---|---|
| AO | static component |
| AJ | cosine term of jth harmonic |
| BJ | sine term of jth harmonic |
| CJ | resultant of jth harmonic |
| PHIJC | phase angle |

The definition formulas for the Fourier Series of Y = f (X) are

$$Y = AO + \sum_{J=1}^{N} AJ \cos JX + \sum_{J=1}^{N} BJ \sin JX$$

or in complex form

$$Y = AC + \sum_{J=1}^{N} CJ \cos (JX-PHIJC)$$

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.79553 | | | | | 0 | |
| -0.03101 | -0.11033 | 0.11460 | 294.30266 | 1.000000 | 1 | 5.814 |
| 0.07779 | -0.05087 | 0.09295 | 322.87964 | 0.851246 | 2 | 11.628 |
| 0.01196 | -0.09505 | 0.09633 | 282.25977 | 0.491547 | 3 | 17.442 |
| 0.10136 | -0.02982 | 0.10565 | 343.60718 | 0.921948 | 4 | 23.256 |
| 0.00543 | -0.01221 | 0.01336 | 293.90698 | 0.116601 | 5 | 29.070 |
| -0.00065 | 0.00271 | 0.00278 | 103.43387 | 0.024293 | 6 | 34.884 |
| -0.02186 | -0.01660 | 0.02745 | 217.21082 | 0.239566 | 7 | 40.698 |
| -0.00262 | -0.01977 | 0.01995 | 262.45557 | 0.174054 | 8 | 46.512 |
| 0.00037 | -0.00737 | 0.00738 | 272.87012 | 0.064410 | 9 | 52.326 |
| -0.01504 | -0.00527 | 0.01594 | 199.30186 | 0.139064 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.47110 | | | | | 0 | |
| 0.34782 | 0.11632 | 0.36656 | 18.50067 | 1.000000 | 1 | 5.814 |
| -0.06703 | -0.07799 | 0.10284 | 229.22297 | 0.280551 | 2 | 11.628 |
| -0.00227 | 0.01609 | 0.00383 | 168.93369 | 0.220781 | 3 | 17.442 |
| -0.00859 | -0.02112 | 0.00931 | 194.68358 | 0.227202 | 4 | 23.256 |
| 0.05462 | 0.16314 | 0.17204 | 71.49037 | 0.469326 | 5 | 29.070 |
| -0.02322 | -0.01213 | 0.02620 | 207.58568 | 0.071465 | 6 | 34.884 |
| -0.00568 | -0.00799 | 0.00979 | 234.94338 | 0.026611 | 7 | 40.698 |
| 0.02463 | -0.02786 | 0.03719 | 311.47729 | 0.101448 | 8 | 46.512 |
| -0.00415 | 0.00344 | 0.00548 | 140.19385 | 0.014727 | 9 | 52.326 |
| 0.05289 | 0.02344 | 0.05785 | 23.99367 | 0.157827 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.06492 | | | | | 0 | |
| -0.11356 | -0.52859 | 0.53283 | 257.69482 | 1.000000 | 1 | 5.814 |
| 0.38186 | -0.28081 | 0.47399 | 323.6[illegible]041 | 0.889571 | 2 | 11.628 |
| 0.04327 | -0.25471 | 0.26033 | 279.5[illegible]13 | 0.488582 | 3 | 17.442 |
| 0.48088 | -0.13989 | 0.50773 | 344.[illegible]0684 | 0.952883 | 4 | 23.256 |
| 0.02333 | -0.05795 | 0.06247 | 291.92456 | 0.117246 | 5 | 29.070 |
| -0.00004 | 0.01149 | 0.01149 | 90.17888 | 0.021564 | 6 | 34.884 |
| -0.10462 | -0.07843 | 0.13076 | 216.85767 | 0.245402 | 7 | 40.698 |
| -0.09983 | -0.09414 | 0.09465 | 264.04928 | 0.177633 | 8 | 46.512 |
| 0.00242 | -0.03444 | 0.03452 | 273.[illegible]10 | 0.064845 | 9 | 52.326 |
| -0.07020 | -0.02499 | 0.07452 | 199.59663 | 0.139896 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.20042 | | | | | 0 | |
| 1.60780 | 0.54500 | 1.69766 | 18.72505 | 1.000000 | 1 | 5.814 |
| -0.29005 | -0.35517 | 0.46491 | 229.90298 | 0.273499 | 2 | 11.628 |
| -0.38543 | 0.06853 | 0.39147 | 169.91803 | 0.230595 | 3 | 17.442 |
| -0.38769 | -0.10153 | 0.40076 | 194.67482 | 0.236067 | 4 | 23.256 |
| 0.26541 | 0.76263 | 0.80115 | 72.16187 | 0.471912 | 5 | 29.070 |
| -0.10714 | -0.05762 | 0.12165 | 208.27132 | 0.071660 | 6 | 34.884 |
| -0.02787 | -0.04225 | 0.05017 | 237.35301 | 0.029555 | 7 | 40.698 |
| 0.11253 | -0.12732 | 0.16992 | 311.47095 | 0.100090 | 8 | 46.512 |
| -0.02287 | 0.02226 | 0.03191 | 135.76839 | 0.018799 | 9 | 52.326 |
| 0.24681 | 0.10995 | 0.27019 | 24.01225 | 0.159156 | 10 | 58.140 |

TEXT NOT REPRODUCIBLE

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.51761 | | | | | 0 | |
| -0.11862 | -1.23194 | 1.23764 | 264.50000 | 0.995890 | 1 | 5.814 |
| 0.97160 | -0.67827 | 1.18493 | 325.08105 | 0.952711 | 2 | 11.628 |
| 0.04284 | -0.54357 | 0.59505 | 274.05078 | 0.478436 | 3 | 17.442 |
| 1.10991 | -0.32730 | 1.24375 | 344.74243 | 1.000000 | 4 | 23.256 |
| 0.04462 | -0.13873 | 0.14573 | 287.83600 | 0.117170 | 5 | 29.070 |
| 0.01373 | 0.02130 | 0.02534 | 57.18823 | 0.020374 | 6 | 34.884 |
| -0.25423 | -0.18603 | 0.31503 | 216.19404 | 0.253289 | 7 | 40.698 |
| -0.01167 | -0.22660 | 0.22690 | 267.09225 | 0.182433 | 8 | 46.512 |
| 0.03085 | -0.09383 | 0.09424 | 275.38794 | 0.075772 | 9 | 52.326 |
| -0.16261 | -0.05979 | 0.17325 | 200.18671 | 0.139300 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.10348 | | | | | 0 | |
| 3.69990 | 1.27284 | 3.87088 | 19.10523 | 1.000000 | 1 | 5.814 |
| -0.42864 | -0.78195 | 1.00381 | 291.10796 | 0.259118 | 2 | 11.628 |
| -0.09928 | 0.12828 | 0.90830 | 171.00139 | 0.234671 | 3 | 17.442 |
| -0.95137 | -0.34884 | 0.98338 | 194.69984 | 0.254046 | 4 | 23.256 |
| 0.58037 | 1.77193 | 1.84789 | 73.31485 | 0.477381 | 5 | 29.070 |
| -0.24246 | -0.13811 | 0.27983 | 209.66742 | 0.072285 | 6 | 34.884 |
| -0.08693 | -0.12892 | 0.13821 | 241.03436 | 0.035704 | 7 | 40.698 |
| 0.26936 | -0.28229 | 0.37665 | 311.45957 | 0.097303 | 8 | 46.512 |
| -0.06024 | 0.07997 | 0.10579 | 130.00601 | 0.027329 | 9 | 52.326 |
| 0.97137 | 0.29712 | 0.42656 | 24.22023 | 0.161865 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 50
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 31.90806 | | | | | 0 | |
| 0.99311 | -2.38361 | 2.98856 | 293.32129 | 0.998427 | 1 | 5.814 |
| 2.41958 | -1.39391 | 2.79217 | 330.06104 | 1.000000 | 2 | 11.628 |
| -0.48313 | -0.96302 | 1.07741 | 243.25748 | 0.385869 | 3 | 17.442 |
| 2.64315 | -0.57784 | 2.70593 | 347.67212 | 0.968978 | 4 | 23.256 |
| -0.01356 | -0.26864 | 0.26898 | 267.10913 | 0.096333 | 5 | 29.070 |
| 0.19217 | -0.01206 | 0.19265 | 355.44973 | 0.054670 | 6 | 34.884 |
| -0.54318 | -0.34635 | 0.64414 | 212.52667 | 0.230694 | 7 | 40.698 |
| 0.00502 | -0.46123 | 0.46016 | 280.95200 | 0.164828 | 8 | 46.512 |
| 0.04553 | -0.24915 | 0.24934 | 280.52051 | 0.089301 | 9 | 52.326 |
| -0.27117 | -0.11440 | 0.29491 | 202.87329 | 0.105605 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 50
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.57235 | | | | | 0 | |
| 5.31873 | 2.17200 | 5.74543 | 22.22090 | 1.000000 | 1 | 5.814 |
| -0.99864 | -0.89428 | 0.97918 | 245.97489 | 0.170415 | 2 | 11.628 |
| -1.98417 | -0.89318 | 1.96694 | 183.48908 | 0.272728 | 3 | 17.442 |
| -2.18362 | -0.95189 | 2.17481 | 194.78044 | 0.378529 | 4 | 23.256 |
| 0.44662 | 2.99842 | 3.03247 | 81.93256 | 0.527806 | 5 | 29.070 |
| -0.34288 | -0.26995 | 0.43586 | 218.26919 | 0.075862 | 6 | 34.884 |
| -0.19773 | -0.43378 | 0.44149 | 250.81467 | 1.000374 | 7 | 40.698 |
| 0.39988 | -0.34526 | 0.44393 | 311.98894 | 0.000748 | 8 | 46.512 |
| -0.26988 | 0.40672 | 0.48798 | 123.52698 | 0.084919 | 9 | 52.326 |
| 0.98239 | 0.44844 | 1.09284 | 25.21994 | 0.183214 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL 4H-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 42.56137 | | | | | 0 | |
| 3.49227 | -1.02600 | 3.63987 | 343.62744 | 1.000000 | 1 | 5.814 |
| 2.50507 | -0.91278 | 2.66619 | 339.97949 | 0.732495 | 2 | 11.628 |
| -1.90673 | -0.11582 | 1.91117 | 184.39558 | 0.415172 | 3 | 17.442 |
| 2.12160 | -0.17770 | 2.12903 | 355.21216 | 0.584910 | 4 | 23.256 |
| -0.23102 | -0.14864 | 0.27470 | 212.75853 | 0.075471 | 5 | 29.070 |
| 0.36154 | -0.12886 | 0.38382 | 340.38232 | 0.105449 | 6 | 34.884 |
| -0.38029 | -0.15843 | 0.42030 | 202.14486 | 0.115470 | 7 | 40.698 |
| 0.28614 | -0.28897 | 0.40667 | 314.71826 | 0.111726 | 8 | 46.512 |
| 0.08891 | -0.27061 | 0.28422 | 287.88493 | 0.078086 | 9 | 52.326 |
| -0.04531 | -0.06163 | 0.07649 | 233.67296 | 0.021014 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL 4H-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.59729 | | | | | 0 | |
| -0.93263 | 0.55311 | 1.08431 | 149.32913 | 0.600563 | 1 | 5.814 |
| 1.54086 | 0.87895 | 1.78175 | 29.59836 | 1.000000 | 2 | 11.628 |
| -0.42420 | -0.78225 | 0.88986 | 241.53700 | 0.499432 | 3 | 17.442 |
| -1.67086 | -0.43560 | 1.72671 | 194.61488 | 0.969188 | 4 | 23.256 |
| -1.01959 | 0.62674 | 1.19341 | 148.32956 | 0.669796 | 5 | 29.070 |
| 0.09181 | -0.15364 | 0.17899 | 300.86011 | 0.100455 | 6 | 34.884 |
| -0.13693 | -0.65249 | 0.66671 | 258.14195 | 0.374185 | 7 | 40.698 |
| -0.22316 | 0.25792 | 0.34186 | 130.88644 | 0.191420 | 8 | 46.512 |
| -0.44301 | 0.76793 | 0.88695 | 119.97986 | 0.497575 | 9 | 52.326 |
| 0.19498 | 0.13087 | 0.20248 | 40.26599 | 0.113648 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL 4H-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 63.87895 | | | | | 0 | |
| 7.63001 | -0.15310 | 7.63155 | 358.85034 | 1.000000 | 1 | 5.814 |
| 3.02488 | -0.74586 | 3.11548 | 346.14868 | 0.408237 | 2 | 11.628 |
| -2.32308 | 0.24580 | 2.33996 | 173.97954 | 0.306693 | 3 | 17.442 |
| 2.09000 | 0.14786 | 2.09523 | 4.04679 | 0.274548 | 4 | 23.256 |
| -0.48740 | -0.12637 | 0.42655 | 197.23308 | 0.055893 | 5 | 29.070 |
| 0.53193 | -0.27045 | 0.59674 | 333.05005 | 0.078194 | 6 | 34.884 |
| -0.19935 | -0.18491 | 0.22526 | 207.75945 | 0.029518 | 7 | 40.698 |
| 0.44211 | -0.17102 | 0.47404 | 338.85205 | 0.062116 | 8 | 46.512 |
| 0.12697 | -0.29423 | 0.32046 | 293.34229 | 0.041992 | 9 | 52.326 |
| 0.00889 | -0.00648 | 0.13136 | 318.52983 | 0.017213 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL 4H-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -3.41344 | | | | | 0 | |
| -3.11451 | -0.19886 | 3.12072 | 183.61644 | 1.000000 | 1 | 5.814 |
| 2.30001 | 1.81094 | 2.99781 | 37.16324 | 0.960613 | 2 | 11.628 |
| 0.41949 | -0.99329 | 1.07320 | 292.89600 | 0.343898 | 3 | 17.442 |
| -1.36469 | -0.24673 | 1.38681 | 190.24805 | 0.444389 | 4 | 23.256 |
| -1.93627 | -0.76271 | 2.09187 | 201.49988 | 0.666855 | 5 | 29.070 |
| 0.23609 | -0.17305 | 0.29391 | 323.44458 | 0.094179 | 6 | 34.884 |
| -0.01612 | -0.65208 | 0.65228 | 268.58423 | 0.208816 | 7 | 40.698 |
| -0.62858 | 0.61633 | 0.88027 | 135.56815 | 0.282073 | 8 | 46.512 |
| -0.60836 | 1.03646 | 1.19779 | 120.08133 | 0.383817 | 9 | 52.326 |
| -0.45624 | -0.01076 | 0.45637 | 181.35123 | 0.146238 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 67.47194 | | | | | C | |
| 10.00745 | 0.20212 | 10.00949 | 1.15705 | 1.000000 | 1 | 5.814 |
| 2.70769 | -0.56576 | 2.76616 | 348.19800 | 0.276354 | 2 | 11.628 |
| -1.77888 | -0.10076 | 1.78173 | 183.24203 | 0.178004 | 3 | 17.442 |
| 1.72394 | 0.24916 | 1.74185 | 8.22383 | 0.174020 | 4 | 23.256 |
| -0.34376 | -0.17766 | 0.38695 | 207.32983 | 0.038659 | 5 | 29.070 |
| 0.42388 | -0.29550 | 0.51672 | 325.11816 | 0.051623 | 6 | 34.884 |
| 0.07880 | -0.16641 | 0.18411 | 295.33862 | 0.018395 | 7 | 40.698 |
| 0.33743 | -0.04300 | 0.34016 | 352.73755 | 0.033984 | 8 | 46.512 |
| 0.10038 | -0.19908 | 0.22296 | 296.75757 | 0.022275 | 9 | 52.326 |
| 0.09835 | -0.14799 | 0.17769 | 303.60718 | 0.017752 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -3.88130 | | | | | C | |
| 0.56240 | 0.37803 | 0.69300 | 32.62996 | 0.472977 | 1 | 5.814 |
| 0.86281 | 0.96744 | 1.29631 | 48.27437 | 0.888581 | 2 | 11.628 |
| 0.61364 | -0.25980 | 0.66637 | 337.09298 | 0.456777 | 3 | 17.442 |
| -0.61795 | 0.07817 | 0.62288 | 172.74845 | 0.426963 | 4 | 23.256 |
| -1.31303 | -0.63577 | 1.45886 | 205.83621 | 1.000000 | 5 | 29.070 |
| -0.02522 | -0.24854 | 0.24983 | 264.28694 | 0.171253 | 6 | 34.884 |
| 0.10473 | -0.13022 | 0.22601 | 324.81860 | 0.154923 | 7 | 40.698 |
| -0.96388 | 0.38654 | 0.68365 | 145.56923 | 0.468623 | 8 | 46.512 |
| -0.45712 | 0.78146 | 0.83726 | 123.09090 | 0.573918 | 9 | 52.326 |
| -0.59952 | 0.05143 | 0.96198 | 174.74820 | 0.389150 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 55.01814 | | | | | C | |
| 9.11915 | 0.16931 | 9.12072 | 1.06368 | 1.000000 | 1 | 5.814 |
| 2.01850 | -0.30016 | 2.04869 | 351.54175 | 0.223743 | 2 | 11.628 |
| -0.96122 | -0.36594 | 1.02852 | 200.84284 | 0.112767 | 3 | 17.442 |
| 1.23818 | 0.14538 | 1.24720 | 6.69397 | 0.136744 | 4 | 23.256 |
| -0.21852 | -0.20364 | 0.29849 | 222.98158 | 0.032749 | 5 | 29.070 |
| 0.27864 | -0.21565 | 0.35234 | 322.26123 | 0.038631 | 6 | 34.884 |
| 0.16530 | -0.18710 | 0.24966 | 311.45923 | 0.027373 | 7 | 40.698 |
| 0.18687 | 0.03265 | 0.18970 | 9.91109 | 0.020799 | 8 | 46.512 |
| 0.05166 | -0.12487 | 0.13514 | 292.48389 | 0.014817 | 9 | 52.326 |
| 0.06399 | -0.13744 | 0.15160 | 294.96509 | 0.016622 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -2.13438 | | | | | C | |
| 2.56599 | 1.01749 | 2.76036 | 21.62982 | 1.000000 | 1 | 5.814 |
| -0.30282 | 0.23262 | 0.38186 | 142.46938 | 0.138336 | 2 | 11.628 |
| 0.40655 | 0.17664 | 0.44327 | 23.48450 | 0.160582 | 3 | 17.442 |
| -0.09389 | 0.17125 | 0.19530 | 118.73463 | 0.070752 | 4 | 23.256 |
| -0.56774 | -0.31452 | 0.64904 | 209.98604 | 0.235130 | 5 | 29.070 |
| -0.13958 | -0.20652 | 0.24926 | 235.94635 | 0.090301 | 6 | 34.884 |
| 0.20786 | 0.18244 | 0.27657 | 41.27310 | 0.100192 | 7 | 40.698 |
| -0.34180 | 0.11313 | 0.36004 | 161.68606 | 0.130431 | 8 | 46.512 |
| -0.25867 | 0.30639 | 0.40098 | 130.17238 | 0.145265 | 9 | 52.326 |
| -0.36509 | 0.08177 | 0.37413 | 167.37491 | 0.135538 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SWIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 61.89182 | | | | | 0 | |
| 10.68835 | 0.05264 | 10.68848 | 0.28220 | 1.000000 | 1 | 5.814 |
| 2.32710 | -0.02288 | 2.32721 | 359.43652 | 0.217731 | 2 | 11.628 |
| -0.71065 | -0.55688 | 0.90916 | 217.77216 | 0.085060 | 3 | 17.442 |
| 1.39396 | -0.08181 | 1.39336 | 356.43379 | 0.130361 | 4 | 23.256 |
| -0.22906 | -0.32138 | 0.39486 | 234.52101 | 0.036924 | 5 | 29.070 |
| 0.36123 | -0.18759 | 0.40703 | 332.55615 | 0.038081 | 6 | 34.884 |
| 0.14597 | -0.26391 | 0.30159 | 298.94849 | 0.028216 | 7 | 40.698 |
| 0.16424 | 0.10007 | 0.19233 | 31.39491 | 0.017994 | 8 | 46.512 |
| 0.01706 | -0.19473 | 0.19747 | 274.95483 | 0.018479 | 9 | 52.326 |
| 0.08029 | -0.11119 | 0.13715 | 305.83398 | 0.012832 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SWIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.55420 | | | | | 0 | |
| 2.19161 | 2.05298 | 3.00298 | 43.12933 | 1.000000 | 1 | 5.814 |
| -0.74096 | 0.27179 | 0.78923 | 159.85623 | 0.262816 | 2 | 11.628 |
| 0.10236 | 0.17551 | 0.20318 | 59.74753 | 0.067659 | 3 | 17.442 |
| 0.22448 | 0.06532 | 0.23379 | 16.22490 | 0.077852 | 4 | 23.256 |
| -0.39704 | -0.53080 | 0.66929 | 233.61328 | 0.222874 | 5 | 29.070 |
| -0.03093 | -0.07824 | 0.08413 | 248.43062 | 0.028015 | 6 | 34.884 |
| 0.14628 | 0.27523 | 0.31169 | 62.00958 | 0.103793 | 7 | 40.698 |
| -0.27427 | -0.01029 | 0.27488 | 183.01922 | 0.091536 | 8 | 46.512 |
| -0.20224 | 0.12566 | 0.23818 | 148.14612 | 0.079289 | 9 | 52.326 |
| -0.19908 | 0.04678 | 0.20458 | 166.77785 | 0.068128 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SWIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 147.79297 | | | | | 0 | |
| 25.97693 | -0.43212 | 25.98460 | 358.60596 | 1.000000 | 1 | 5.814 |
| 5.99447 | 1.18852 | 6.11116 | 11.21459 | 0.235184 | 2 | 11.628 |
| -0.88595 | -1.54819 | 1.74541 | 242.46996 | 0.067171 | 3 | 17.442 |
| 3.47284 | -1.15740 | 3.66884 | 341.56936 | 0.140877 | 4 | 23.256 |
| -0.53993 | -1.06752 | 1.19630 | 243.17038 | 0.046039 | 5 | 29.070 |
| 1.12421 | -0.18080 | 1.13865 | 350.86353 | 0.043820 | 6 | 34.884 |
| -0.09489 | -0.71523 | 0.71727 | 265.47529 | 0.027604 | 7 | 40.698 |
| 0.30351 | 0.41627 | 0.51516 | 53.90363 | 0.019826 | 8 | 46.512 |
| -0.09519 | -0.74496 | 0.75101 | 262.71826 | 0.028902 | 9 | 52.326 |
| 0.26787 | -0.02536 | 0.26907 | 354.59131 | 0.010355 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SWIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.80797 | | | | | 0 | |
| -1.18486 | 0.09713 | 0.18336 | 98.32510 | 1.000000 | 1 | 5.814 |
| -1.72091 | 1.64994 | 2.38408 | 136.20618 | 0.291333 | 2 | 11.628 |
| -0.98835 | -0.47146 | 1.09504 | 205.90175 | 0.133813 | 3 | 17.442 |
| 1.15622 | -0.58281 | 1.29480 | 333.24902 | 0.158224 | 4 | 23.256 |
| -0.75868 | -2.49388 | 2.60673 | 253.07024 | 0.318541 | 5 | 29.070 |
| 0.71826 | 0.43196 | 0.83809 | 31.02492 | 0.102414 | 6 | 34.884 |
| -0.21842 | 0.46766 | 0.51782 | 114.22464 | 0.062666 | 7 | 40.698 |
| -0.33637 | -0.29767 | 0.44917 | 221.90493 | 0.054888 | 8 | 46.512 |
| -0.28846 | -0.23698 | 0.37348 | 219.38498 | 0.045639 | 9 | 52.326 |
| 0.34885 | -0.17315 | 0.38946 | 333.60278 | 0.047592 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 120.71603 | | | | | C | |
| 23.06674 | -0.79395 | 23.07838 | 358.02832 | 1.000000 | 1 | 5.814 |
| 4.41773 | 1.16333 | 4.76201 | 14.14011 | 0.206341 | 2 | 11.628 |
| 0.66375 | -1.55725 | 1.55855 | 272.34424 | 0.067533 | 3 | 17.442 |
| 2.51561 | -1.04095 | 2.72248 | 337.52051 | 0.117966 | 4 | 23.256 |
| -0.21973 | -0.86345 | 0.89097 | 255.72252 | 0.038606 | 5 | 29.070 |
| 0.76338 | 0.10657 | 0.77078 | 7.94697 | 0.033399 | 6 | 34.884 |
| -0.37856 | -0.31851 | 0.49473 | 220.07610 | 0.021437 | 7 | 40.698 |
| 0.18638 | 0.41199 | 0.45219 | 65.65887 | 0.019594 | 8 | 46.512 |
| -0.08531 | -0.48421 | 0.49167 | 260.00732 | 0.021304 | 9 | 52.326 |
| 0.30669 | -0.03981 | 0.30927 | 352.60449 | 0.013401 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.72650 | | | | | C | |
| -2.93415 | 8.54726 | 9.03686 | 108.94678 | 1.000000 | 1 | 5.814 |
| -1.16547 | 1.98705 | 1.52728 | 139.73842 | 0.169006 | 2 | 11.628 |
| -0.93386 | 0.06171 | 0.93741 | 173.40614 | 0.099469 | 3 | 17.442 |
| 0.94713 | -0.58626 | 1.11389 | 328.24316 | 0.123261 | 4 | 23.256 |
| -0.59648 | -2.42849 | 2.49162 | 257.09473 | 0.275717 | 5 | 29.070 |
| 0.98668 | -0.19137 | 0.97844 | 351.10059 | 0.108274 | 6 | 34.884 |
| -1.61341 | 0.48148 | 1.14006 | 163.01862 | 0.126157 | 7 | 40.698 |
| 0.12510 | 0.28478 | 0.31104 | 66.28468 | 0.034419 | 8 | 46.512 |
| -0.33195 | -0.28979 | 0.44065 | 221.12001 | 0.048761 | 9 | 52.326 |
| 0.99391 | -0.32958 | 1.00922 | 340.94489 | 0.111678 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 194.99419 | | | | | C | |
| 31.69499 | -1.41396 | 31.72650 | 357.44556 | 1.000000 | 1 | 5.814 |
| 4.63144 | 1.15084 | 4.77231 | 13.99347C | 0.150420 | 2 | 11.628 |
| 0.74855 | -2.55628 | 2.66363 | 286.32193 | 0.083956 | 3 | 17.442 |
| 2.27851 | -0.47686 | 2.32787 | 348.17944 | 0.073373 | 4 | 23.256 |
| 0.69959 | -0.82507 | 0.87899 | 270.60864 | 0.026180 | 5 | 29.070 |
| 0.29782 | 0.44160 | 0.51899 | 59.79994 | 0.016105 | 6 | 34.884 |
| -0.99037 | 0.12856 | 0.61803 | 167.87447 | 0.019291 | 7 | 40.698 |
| 0.03388 | 0.47368 | 0.47409 | 85.91837 | 0.014968 | 8 | 46.512 |
| -0.03096 | -0.08212 | 0.08898 | 244.61934 | 0.002865 | 9 | 52.326 |
| 0.40126 | -0.18497 | 0.44184 | 335.25098 | 0.013927 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 538 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.37419 | | | | | 0 | |
| 3.06777 | 11.99269 | 12.60096 | 72.12492 | 1.000000 | 1 | 5.814 |
| -1.42277 | -0.24089 | 1.45288 | 189.94395 | 0.115299 | 2 | 11.628 |
| 1.90852 | 0.69089 | 1.93081 | 25.36826 | 0.122118 | 3 | 17.442 |
| -0.07751 | -0.10791 | 0.13286 | 234.30942 | 0.010544 | 4 | 23.256 |
| -0.61488 | -2.07598 | 2.16487 | 253.52353 | 0.171802 | 5 | 29.070 |
| 0.81934 | -1.65529 | 1.67809 | 299.37964 | 0.132536 | 6 | 34.884 |
| -1.71984 | 0.99424 | 1.95831 | 151.17293 | 0.155410 | 7 | 40.698 |
| 0.40888 | 1.00317 | 1.08028 | 68.22052 | 0.085730 | 8 | 46.512 |
| -0.62240 | -0.19612 | 0.65197 | 197.32185 | 0.051739 | 9 | 52.326 |
| 1.29233 | -0.91014 | 1.29016 | 346.09033 | 0.102386 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 115.48019 | | | | | 0 | |
| 20.23860 | -2.53090 | 20.39622 | 352.87183 | 1.000000 | 1 | 5.814 |
| 2.96958 | 2.51369 | 3.89063 | 40.24718 | 0.190753 | 2 | 11.628 |
| 0.49600 | -2.67065 | 2.71632 | 280.52124 | 0.133178 | 3 | 17.442 |
| 1.27934 | -0.19596 | 1.29426 | 351.29126 | 0.063456 | 4 | 23.256 |
| -0.34059 | -0.57692 | 0.66995 | 239.44394 | 0.032847 | 5 | 29.070 |
| -0.23647 | 0.55665 | 0.60480 | 113.01634 | 0.029652 | 6 | 34.884 |
| 0.20969 | -0.24752 | 0.32440 | 310.27075 | 0.015905 | 7 | 40.698 |
| -0.50657 | 0.08869 | 0.51428 | 170.06941 | 0.025214 | 8 | 46.512 |
| -0.22721 | -0.11764 | 0.25586 | 207.37259 | 0.012544 | 9 | 52.326 |
| -0.14283 | 0.47440 | 0.49543 | 106.75601 | 0.024290 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.69325 | | | | | 0 | |
| 23.26639 | 10.01633 | 25.33083 | 23.29218 | 1.000000 | 1 | 5.814 |
| -1.91503 | 1.12644 | 1.88791 | 143.36894 | 0.074530 | 2 | 11.628 |
| 2.18369 | -4.89834 | 5.36304 | 294.02734 | 0.211720 | 3 | 17.442 |
| -3.34486 | -0.02588 | 3.34496 | 180.44337 | 0.132051 | 4 | 23.256 |
| -0.32577 | 0.98412 | 1.03663 | 108.31581 | 0.040924 | 5 | 29.070 |
| -0.89354 | 0.51869 | 1.03317 | 149.86511 | 0.040787 | 6 | 34.884 |
| 2.02068 | 0.27160 | 2.03885 | 7.65538 | 0.080489 | 7 | 40.698 |
| -0.71315 | -1.87851 | 2.00932 | 249.21133 | 0.079323 | 8 | 46.512 |
| 0.22525 | -0.56893 | 0.61190 | 291.59888 | 0.024156 | 9 | 52.326 |
| -1.19690 | 0.56188 | 1.32222 | 154.85246 | 0.052198 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 163.07796 | | | | | 0 | |
| -15.10080 | -17.89888 | 23.30135 | 229.77868 | 1.000000 | 1 | 5.814 |
| -1.12455 | 4.83070 | 4.95987 | 103.10464 | 0.212129 | 2 | 11.628 |
| 0.09370 | 2.12367 | 2.12574 | 87.47362 | 0.090916 | 3 | 17.442 |
| 4.90988 | 2.50620 | 5.51252 | 27.04161 | 0.235766 | 4 | 23.256 |
| 0.88428 | -3.23582 | 3.35447 | 285.20442 | 0.143468 | 5 | 29.070 |
| -0.60606 | -0.44895 | 0.75423 | 216.52972 | 0.032258 | 6 | 34.884 |
| -1.73205 | -0.47686 | 1.79649 | 195.39313 | 0.076834 | 7 | 40.698 |
| -1.00015 | 1.64746 | 1.92726 | 121.26147 | 0.082428 | 8 | 46.512 |
| 0.24057 | 0.17404 | 0.29692 | 35.88358 | 0.012699 | 9 | 52.326 |
| 1.06500 | -0.03375 | 1.06553 | 358.18481 | 0.045572 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 67.98340 | | | | | 0 | |
| -10.90952 | 1.19934 | 10.97524 | 173.72638 | 1.000000 | 1 | 5.814 |
| -4.69824 | 3.10288 | 5.63039 | 146.55783 | 0.513089 | 2 | 11.628 |
| -0.97248 | -0.60873 | 0.83563 | 226.75780 | 0.076138 | 3 | 17.442 |
| 1.11224 | 4.85506 | 4.98083 | 77.09682 | 0.453824 | 4 | 23.256 |
| 0.86945 | -1.82261 | 2.01937 | 295.50269 | 0.183993 | 5 | 29.070 |
| -0.13831 | -0.07148 | 0.15569 | 207.33072 | 0.014186 | 6 | 34.884 |
| -1.19835 | -1.64140 | 2.02771 | 234.04553 | 0.184753 | 7 | 40.698 |
| -2.20725 | -1.08953 | 2.46151 | 206.27162 | 0.224278 | 8 | 46.512 |
| -0.39229 | -0.09183 | 0.40271 | 193.06477 | 0.036693 | 9 | 52.326 |
| 0.62884 | 0.74574 | 0.97548 | 49.86111 | 0.088880 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 98.69693 | | | | | C | |
| -22.33002 | -15.08862 | 26.94987 | 214.04727 | 1.000000 | 1 | 5.814 |
| -2.34089 | 3.00453 | 3.90880 | 127.92294 | 0.141329 | 2 | 11.628 |
| -0.09909 | 3.28174 | 3.28324 | 91.72954 | 0.121828 | 3 | 17.442 |
| 3.99639 | 2.41257 | 4.66815 | 31.11889 | 0.173214 | 4 | 23.256 |
| 1.06272 | -2.72333 | 2.92334 | 291.31714 | 0.108473 | 5 | 29.070 |
| -0.40528 | -0.69514 | 0.80465 | 239.75677 | 0.029857 | 6 | 34.884 |
| -1.81971 | -0.24199 | 1.83573 | 187.57480 | 0.068116 | 7 | 40.698 |
| -0.60538 | 1.52812 | 1.64367 | 111.61157 | 0.060998 | 8 | 46.512 |
| 0.36471 | 0.24803 | 0.44105 | 34.21834 | 0.016366 | 9 | 52.326 |
| 1.13032 | -0.36490 | 1.18776 | 342.70815 | 0.044073 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 58.06467 | | | | | C | |
| -23.99107 | -3.56303 | 24.25420 | 188.44751 | 1.000000 | 1 | 5.814 |
| -3.57236 | 2.04862 | 4.11888 | 150.16731 | 0.169788 | 2 | 11.628 |
| -1.63228 | 2.47187 | 3.13101 | 121.42131 | 0.129092 | 3 | 17.442 |
| 3.08685 | 4.51535 | 5.44965 | 55.64215 | 0.225513 | 4 | 23.256 |
| 0.92878 | -2.54948 | 2.71338 | 290.01685 | 0.111873 | 5 | 29.070 |
| 0.53396 | -0.65353 | 0.84393 | 309.25000 | 0.034795 | 6 | 34.884 |
| -2.63785 | -1.54312 | 3.05605 | 210.32724 | 0.126001 | 7 | 40.698 |
| -1.32808 | 0.35556 | 1.56111 | 166.03485 | 0.064364 | 8 | 46.512 |
| -0.60091 | 0.25988 | 0.65470 | 156.61278 | 0.026993 | 9 | 52.326 |
| 1.51465 | 0.29401 | 1.54292 | 10.98523 | 0.063615 | 10 | 58.140 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.03126 | | | | | C | |
| -1.94724 | -1.27013 | 2.32485 | 213.11528 | 1.000000 | 1 | 5.814 |
| -0.20680 | 0.29572 | 0.32116 | 130.08409 | 0.138141 | 2 | 11.628 |
| -0.00964 | 0.28644 | 0.28661 | 91.92719 | 0.123279 | 3 | 17.442 |
| 0.33518 | 0.20509 | 0.39295 | 31.46895 | 0.169021 | 4 | 23.256 |
| 0.09152 | -0.22911 | 0.24671 | 291.77534 | 0.106119 | 5 | 29.070 |
| -0.03342 | -0.06067 | 0.06927 | 241.15186 | 0.029794 | 6 | 34.884 |
| -0.15547 | -0.01935 | 0.15667 | 187.09482 | 0.067388 | 7 | 40.698 |
| -0.04938 | 0.12949 | 0.13858 | 110.87631 | 0.059610 | 8 | 46.512 |
| 0.03177 | 0.02153 | 0.03838 | 34.12943 | 0.016509 | 9 | 52.326 |
| 0.09663 | -0.03291 | 0.10208 | 341.19165 | 0.043907 | 10 | 58.140 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 530 TEST COND 1 COMP RUN 53.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.89109 | | | | | C | |
| -2.11796 | -0.33173 | 2.14378 | 188.90161 | 1.000000 | 1 | 5.814 |
| -0.29795 | 0.16878 | 0.34244 | 150.46928 | 0.159734 | 2 | 11.628 |
| -0.14523 | 0.24584 | 0.28554 | 120.57671 | 0.133195 | 3 | 17.442 |
| 0.27409 | 0.33285 | 0.47085 | 54.40068 | 0.219636 | 4 | 23.256 |
| 0.07955 | -0.22106 | 0.23494 | 289.79126 | 0.109592 | 5 | 29.070 |
| 0.04015 | -0.05869 | 0.07656 | 309.94482 | 0.035711 | 6 | 34.884 |
| -0.23260 | -0.13108 | 0.26699 | 209.40332 | 0.124541 | 7 | 40.698 |
| -0.12576 | 0.03819 | 0.13143 | 163.10754 | 0.061308 | 8 | 46.512 |
| -0.05220 | 0.02411 | 0.05757 | 155.23669 | 0.026855 | 9 | 52.326 |
| 0.13384 | 0.02257 | 0.13573 | 9.57356 | 0.063311 | 10 | 58.140 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.98319 | | | | | 0 | |
| 0.00501 | 0.33068 | 0.33072 | 89.12144 | 1.000000 | 1 | 5.714 |
| 0.04281 | 0.14914 | 0.15517 | 73.98813 | 0.469179 | 2 | 11.429 |
| 0.08515 | -0.00421 | 0.08525 | 357.16895 | 0.257771 | 3 | 17.143 |
| 0.07724 | 0.03062 | 0.08309 | 21.62590 | 0.251232 | 4 | 22.857 |
| -0.00301 | 0.03429 | 0.03443 | 95.01901 | 0.104094 | 5 | 28.571 |
| 0.01159 | 0.03399 | 0.03591 | 71.16838 | 0.108579 | 6 | 34.286 |
| -0.04461 | 0.05924 | 0.07538 | 128.19574 | 0.227986 | 7 | 40.000 |
| 0.04166 | 0.04106 | 0.05859 | 44.58475 | 0.176880 | 8 | 45.714 |
| 0.04967 | 0.03164 | 0.05556 | 34.71200 | 0.167992 | 9 | 51.429 |
| -0.00435 | -0.01117 | 0.01285 | 240.36552 | 0.038858 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.61641 | | | | | 0 | |
| 0.13318 | -0.23681 | 0.27169 | 299.35352 | 0.464841 | 1 | 5.714 |
| -0.30057 | -0.50127 | 0.58448 | 239.65217 | 1.000000 | 2 | 11.429 |
| -0.05660 | -0.10089 | 0.10538 | 237.51450 | 0.180301 | 3 | 17.143 |
| -0.27020 | -0.07384 | 0.28075 | 194.78020 | 0.494033 | 4 | 22.857 |
| -0.05129 | -0.04426 | 0.06775 | 220.79944 | 0.115910 | 5 | 28.571 |
| -0.13077 | -0.07913 | 0.15284 | 211.17804 | 0.261505 | 6 | 34.286 |
| -0.06158 | -0.17030 | 0.18109 | 250.11914 | 0.309837 | 7 | 40.000 |
| -0.03176 | -0.05805 | 0.06617 | 241.31448 | 0.113214 | 8 | 45.714 |
| -0.04108 | -0.09284 | 0.10077 | 245.99426 | 0.172416 | 9 | 51.429 |
| 0.00669 | -0.05009 | 0.05053 | 277.60976 | 0.086458 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.00104 | | | | | 0 | |
| 0.83738 | 1.63799 | 1.63842 | 88.69338 | 1.000000 | 1 | 5.714 |
| 0.21064 | 0.76535 | 0.77655 | 74.21912 | 0.472741 | 2 | 11.429 |
| 0.37751 | 0.00735 | 0.37758 | 1.11475 | 0.230455 | 3 | 17.143 |
| 0.38604 | 0.16775 | 0.40321 | 24.58458 | 0.246095 | 4 | 22.857 |
| -0.02541 | 0.17106 | 0.17294 | 98.44963 | 0.105551 | 5 | 28.571 |
| 0.05297 | 0.17377 | 0.18164 | 73.05958 | 0.110876 | 6 | 34.286 |
| -0.22260 | 0.28076 | 0.35829 | 128.48846 | 0.218683 | 7 | 40.000 |
| 0.19782 | 0.19434 | 0.27674 | 44.68760 | 0.168905 | 8 | 45.714 |
| 0.21904 | 0.14967 | 0.26529 | 34.34415 | 0.161919 | 9 | 51.429 |
| -0.02423 | -0.04827 | 0.05401 | 243.34563 | 0.032962 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.60436 | | | | | 0 | |
| 0.59488 | -1.10851 | 1.25804 | 298.21997 | 0.458509 | 1 | 5.714 |
| -1.41668 | -2.34973 | 2.74376 | 238.91354 | 1.000000 | 2 | 11.429 |
| -0.24870 | -0.40190 | 0.47262 | 238.29031 | 0.172253 | 3 | 17.143 |
| -1.32322 | -0.33485 | 1.36493 | 194.28100 | 0.497467 | 4 | 22.857 |
| -0.24425 | -0.20550 | 0.31920 | 220.07632 | 0.116334 | 5 | 28.571 |
| -0.62461 | -0.36762 | 0.72476 | 210.47963 | 0.264156 | 6 | 34.286 |
| -0.29147 | -0.80523 | 0.85636 | 290.18612 | 0.312112 | 7 | 40.000 |
| -0.14581 | -0.27804 | 0.31218 | 242.15947 | 0.113788 | 8 | 45.714 |
| -0.18672 | -0.42891 | 0.46779 | 246.47472 | 0.170493 | 9 | 51.429 |
| 0.03044 | -0.22880 | 0.23168 | 279.09322 | 0.084440 | 10 | 57.143 |

TEXT NOT REPRODUCIBLE

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 13.498271 | | | | | 0 | |
| 0.19005 | 4.23162 | 4.23458 | 87.95740 | 1.000000 | 1 | 5.714 |
| 0.53818 | 1.95452 | 2.02726 | 74.68495 | 0.478747 | 2 | 11.429 |
| 0.78215 | 0.14214 | 0.79496 | 10.30007 | 0.187734 | 3 | 17.143 |
| 0.07773 | 0.30340 | 1.08194 | 29.84525 | 0.255975 | 4 | 22.857 |
| -0.11146 | 0.44718 | 0.46086 | 100.99857 | 0.108834 | 5 | 28.571 |
| 0.11747 | 0.47262 | 0.48699 | 76.04287 | 0.115006 | 6 | 34.286 |
| -0.53287 | 0.06996 | 0.05979 | 128.81095 | 0.203843 | 7 | 40.000 |
| 0.44817 | 0.44252 | 0.63012 | 44.69215 | 0.155417 | 8 | 45.714 |
| 0.53454 | 0.39972 | 0.66221 | 53.65630 | 0.191060 | 9 | 51.429 |
| -0.03095 | -0.09368 | 0.09865 | 251.75375 | 0.023343 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.00000 | | | | | 0 | |
| 1.20099 | -2.58254 | 2.87006 | 295.09044 | 0.444624 | 1 | 5.714 |
| -5.24000 | -3.48095 | 6.42748 | 236.64000 | 1.000000 | 2 | 11.429 |
| -0.00000 | -0.07884 | 1.00000 | 239.91643 | 0.154814 | 3 | 17.143 |
| -1.19706 | -0.77895 | 3.24003 | 193.88446 | 0.504066 | 4 | 22.857 |
| -0.00002 | -0.67896 | 0.75981 | 218.48057 | 0.117224 | 5 | 28.571 |
| -1.84178 | -0.00099 | 1.75199 | 200.10406 | 0.269464 | 6 | 34.286 |
| -0.00079 | -1.91208 | 2.00000 | 290.00036 | 0.310000 | 7 | 40.000 |
| -0.00043 | -0.46894 | 0.73006 | 265.70522 | 0.1140841 | 8 | 45.714 |
| -0.41181 | -0.00000 | 1.07183 | 247.45155 | 0.166746 | 9 | 51.429 |
| 0.10894 | -0.50879 | 0.51093 | 282.11011 | 0.000087 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 90
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.21669 | | | | | 0 | |
| 0.68174 | 11.09005 | 11.11697 | 80.40012 | 1.000000 | 1 | 5.714 |
| 1.37829 | 5.34225 | 5.52694 | 75.04833 | 0.4908826 | 2 | 11.429 |
| 0.42799 | 1.42799 | 1.48000 | 73.18879 | 0.1334019 | 3 | 17.143 |
| 1.76884 | 1.92883 | 2.61301 | 47.53983 | 0.235092 | 4 | 22.857 |
| -0.66794 | 1.22387 | 1.39406 | 118.68939 | 0.125481 | 5 | 28.571 |
| 0.16983 | 1.47406 | 1.48886 | 89.36134 | 0.133432 | 6 | 34.286 |
| -1.16783 | 1.38649 | 1.71298 | 130.29999 | 0.154005 | 7 | 40.000 |
| 0.00001 | 0.00004 | 1.25401 | 40.48195 | 0.112855 | 8 | 45.714 |
| 1.12391 | 0.67902 | 1.31987 | 30.70163 | 0.1188999 | 9 | 51.429 |
| 0.17681 | 0.00791 | 0.17047 | 2.63777 | 0.015074 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 90
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 32.26000 | | | | | 0 | |
| 0.04000 | -0.44002 | 0.04402 | 280.93341 | 0.4000467 | 1 | 5.714 |
| -0.12299 | -0.98196 | 11.04402 | 237.19787 | 1.000000 | 2 | 11.429 |
| -0.12047 | -0.00004 | 0.00403 | 299.99788 | 0.0700068 | 3 | 17.143 |
| -0.13139 | -0.00049 | 0.10847 | 187.98244 | 0.9468224 | 4 | 22.857 |
| -1.17005 | -0.71007 | 1.37340 | 211.16949 | 0.1211236 | 5 | 28.571 |
| -2.19002 | -1.36708 | 3.41699 | 208.72049 | 0.3081114 | 6 | 34.286 |
| -1.20000 | -0.64719 | 3.00703 | 209.46736 | 0.3420083 | 7 | 40.000 |
| -0.42007 | -1.20419 | 1.20361 | 251.70830 | 0.1219868 | 8 | 45.714 |
| -0.47305 | -1.60047 | 1.67204 | 253.99326 | 0.1474394 | 9 | 51.429 |
| 0.41000 | -0.42016 | 0.75207 | 300.72724 | 0.0660363 | 10 | 57.143 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 51.66039 | | | | | 0 | |
| 1.48024 | 12.43953 | 12.52729 | 83.21393 | 1.000000 | 1 | 5.714 |
| 1.46951 | 6.48865 | 6.57407 | 77.11916 | 0.524700 | 2 | 11.429 |
| -2.18043 | 3.38491 | 3.96380 | 175.51155 | 0.316413 | 3 | 17.143 |
| 1.02645 | 3.13539 | 3.29913 | 71.87282 | 0.263355 | 4 | 22.857 |
| -1.37912 | 1.44565 | 1.99797 | 133.65874 | 0.159489 | 5 | 28.571 |
| -0.07768 | 1.98696 | 1.98848 | 92.23886 | 0.158732 | 6 | 34.286 |
| -0.74160 | 0.70254 | 1.02153 | 136.54983 | 0.081545 | 7 | 40.000 |
| 0.42295 | 0.49778 | 0.62326 | 47.26495 | 0.049752 | 8 | 45.714 |
| 0.83737 | 0.33183 | 0.90072 | 21.61780 | 0.071981 | 9 | 51.429 |
| 0.63301 | 0.43310 | 0.76699 | 34.37944 | 0.061226 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 11.93380 | | | | | 0 | |
| -2.95012 | -1.12696 | 3.15804 | 200.90718 | 0.[illegible]12 | 1 | 5.714 |
| -2.55246 | -2.65659 | 3.68409 | 226.14522 | 1.000000 | 2 | 11.429 |
| 1.74257 | 1.36491 | 2.21348 | 38.07069 | 0.600823 | 3 | 17.143 |
| -3.28060 | 0.89766 | 3.40127 | 164.69731 | 0.92[illegible]3 | [illegible] | 22.857 |
| -0.72675 | 0.83455 | 0.72757 | 177.27855 | 0.197489 | 5 | 28.571 |
| -2.14476 | -0.01301 | 2.14480 | 180.34792 | 0.582179 | 6 | 34.286 |
| -0.78113 | -1.78580 | 1.91851 | 248.58421 | 0.520755 | 7 | 40.000 |
| 0.28949 | -0.77932 | 0.88899 | 285.04590 | 0.219846 | 8 | 45.714 |
| 0.45667 | -0.16595 | 0.48532 | 340.00464 | 0.131739 | 9 | 51.429 |
| 0.67196 | 0.46136 | 0.81509 | 34.47325 | 0.221247 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 60.54671 | | | | | 0 | |
| 4.25040 | 15.69866 | 16.26385 | 74.85039 | 1.000000 | 1 | 5.714 |
| 1.62849 | 8.53643 | 8.69887 | 79.19942 | 0.534337 | 2 | 11.429 |
| -4.23397 | 4.73186 | 6.34957 | 131.82158 | 0.390410 | 3 | 17.143 |
| 0.04904 | 4.21822 | 4.21850 | 89.33383 | 0.259379 | 4 | 22.857 |
| -2.21996 | 1.72168 | 2.80934 | 142.20480 | 0.172735 | 5 | 28.571 |
| -0.61154 | 2.13240 | 2.21836 | 106.00218 | 0.136398 | 6 | 34.286 |
| -0.74488 | 0.21859 | 0.77629 | 163.64503 | 0.047731 | 7 | 40.000 |
| 0.41408 | 0.08572 | 0.42206 | 11.69631 | 0.026000 | 8 | 45.714 |
| 0.92905 | 0.20082 | 0.95050 | 12.19728 | 0.058443 | 9 | 51.429 |
| 1.18368 | 0.83608 | 1.44918 | 35.23520 | 0.089104 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.55459 | | | | | 0 | |
| -5.07423 | 1.02924 | 5.17756 | 168.53386 | 1.000000 | 1 | 5.714 |
| -0.60064 | 0.91416 | 1.13973 | 126.67056 | 0.220129 | 2 | 11.429 |
| 2.94489 | 2.57748 | 3.91354 | 41.19373 | 0.755865 | 3 | 17.143 |
| -1.88066 | 1.91542 | 2.62892 | 133.23125 | 0.507753 | 4 | 22.857 |
| -0.62699 | 0.14160 | 0.64278 | 167.27367 | 0.124147 | 5 | 28.571 |
| -1.57583 | 0.75418 | 1.74628 | 154.41328 | 0.337279 | 6 | 34.286 |
| 0.00597 | -0.63877 | 0.63880 | 270.53516 | 0.123378 | 7 | 40.000 |
| 0.78867 | -0.73645 | 1.02046 | 313.81787 | 0.197131 | 8 | 45.714 |
| 0.95672 | 0.57817 | 1.11785 | 31.14555 | 0.215903 | 9 | 51.429 |
| 0.81939 | 1.27919 | 1.51912 | 57.35871 | 0.293405 | 10 | 57.143 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 91.08762 | | | | | 0 | |
| 7.33502 | 13.92839 | 15.74175 | 62.22760 | 1.000000 | 1 | 5.714 |
| 1.10141 | 7.79226 | 7.86972 | 81.95467 | 0.499927 | 2 | 11.429 |
| -3.47281 | 3.45567 | 4.89919 | 135.14177 | 0.311222 | 3 | 17.143 |
| -1.01551 | 3.19032 | 3.34805 | 107.65683 | 0.212686 | 4 | 22.857 |
| -2.12504 | 1.30800 | 2.49533 | 148.38712 | 0.158517 | 5 | 28.571 |
| -1.07382 | 0.95929 | 1.43990 | 138.22420 | 0.091470 | 6 | 34.286 |
| -0.80224 | -0.11507 | 0.81045 | 188.16280 | 0.051484 | 7 | 40.000 |
| 0.64430 | -0.17980 | 0.66892 | 344.40747 | 0.042493 | 8 | 45.714 |
| 1.02031 | 0.23808 | 1.04771 | 13.13435 | 0.066556 | 9 | 51.429 |
| 1.22614 | 0.80392 | 1.44619 | 33.25087 | 0.093140 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.68583 | | | | | 0 | |
| -2.83722 | 1.36506 | 3.14852 | 154.30653 | 1.000000 | 1 | 5.714 |
| -0.63864 | 0.07991 | 0.64362 | 172.86795 | 0.204420 | 2 | 11.429 |
| 2.01082 | 1.43410 | 2.46983 | 35.49617 | 0.784439 | 3 | 17.143 |
| -1.28555 | 1.73578 | 1.72641 | 134.29056 | 0.548325 | 4 | 22.857 |
| -0.71454 | -0.49840 | 0.87005 | 214.78836 | 0.276335 | 5 | 28.571 |
| -0.86614 | 0.47693 | 0.98877 | 151.16087 | 0.314041 | 6 | 34.286 |
| 0.62991 | -0.11043 | 0.63951 | 350.05640 | 0.203115 | 7 | 40.000 |
| 0.60221 | -0.87793 | 1.06462 | 304.44800 | 0.338132 | 8 | 45.714 |
| 0.54633 | 0.25283 | 0.60199 | 24.83347 | 0.191199 | 9 | 51.429 |
| 0.46369 | 1.12097 | 1.21309 | 67.52728 | 0.385287 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 77.84840 | | | | | 0 | |
| 7.60494 | 9.84195 | 12.49304 | 51.97906 | 1.000000 | 1 | 5.714 |
| 0.49687 | 5.38174 | 5.40442 | 84.72504 | 0.432611 | 2 | 11.429 |
| -1.90439 | 1.87529 | 2.67272 | 135.44102 | 0.213936 | 3 | 17.143 |
| -1.13498 | 1.88738 | 2.13420 | 122.12766 | 0.170831 | 4 | 22.857 |
| -1.90745 | 0.82814 | 1.71995 | 151.21724 | 0.137673 | 5 | 28.571 |
| -0.94643 | 0.13912 | 0.95659 | 171.63791 | 0.076570 | 6 | 34.286 |
| -0.63615 | -0.11773 | 0.64495 | 190.48518 | 0.051785 | 7 | 40.000 |
| 0.53435 | -0.18901 | 0.56680 | 340.52002 | 0.045369 | 8 | 45.714 |
| 0.84052 | 0.24391 | 0.87519 | 16.16211 | 0.070054 | 9 | 51.429 |
| 0.87719 | 0.56790 | 1.04497 | 32.91940 | 0.083644 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.46841 | | | | | 0 | |
| -0.63041 | 1.21954 | 1.37284 | 117.33575 | 1.000000 | 1 | 5.714 |
| -0.79360 | -0.09397 | 1.19548 | 228.48343 | 0.870749 | 2 | 11.429 |
| 0.97867 | 0.34583 | 1.03797 | 19.46182 | 0.756076 | 3 | 17.143 |
| -0.85078 | 0.48750 | 0.98055 | 150.18733 | 0.714248 | 4 | 22.857 |
| -0.78706 | -0.72511 | 1.03395 | 224.53185 | 0.753144 | 5 | 28.571 |
| -0.38988 | 0.05289 | 0.39371 | 171.39810 | 0.286784 | 6 | 34.286 |
| 0.65282 | 0.04514 | 0.65586 | 5.52601 | 0.477741 | 7 | 40.000 |
| 0.21270 | -0.73060 | 0.76084 | 287.66479 | 0.554578 | 8 | 45.714 |
| 0.18648 | -0.04551 | 0.19195 | 346.28467 | 0.139820 | 9 | 51.429 |
| 0.13253 | 0.64954 | 0.65903 | 78.39450 | 0.480040 | 10 | 57.143 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 129
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 89.84883 | | | | | 0 | |
| 10.02989 | 10.26571 | 14.35157 | 45.66795 | 1.000000 | 1 | 5.714 |
| 0.67537 | 4.70817 | 4.70877 | 89.08287 | 0.328101 | 2 | 11.429 |
| -1.15467 | 1.78256 | 2.05718 | 124.14510 | 0.143341 | 3 | 17.143 |
| -0.93791 | 1.47110 | 1.74465 | 122.52003 | 0.121565 | 4 | 22.857 |
| -1.40185 | 0.92834 | 1.68078 | 146.47154 | 0.117109 | 5 | 28.571 |
| -0.77490 | 0.04618 | 0.77627 | 176.58969 | 0.054090 | 6 | 34.286 |
| -0.58392 | 0.09726 | 0.59196 | 170.54349 | 0.041247 | 7 | 40.000 |
| 0.17629 | -0.03066 | 0.17894 | 350.13452 | 0.012468 | 8 | 45.714 |
| 0.06119 | 0.27417 | 0.90378 | 17.69924 | 0.062974 | 9 | 51.429 |
| 0.72620 | 0.94958 | 0.91072 | 37.11795 | 0.063458 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 129
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.97436 | | | | | 0 | |
| 0.06659 | 2.06222 | 2.06329 | 88.15150 | 1.000000 | 1 | 5.714 |
| -1.05265 | -1.13291 | 1.54647 | 227.18304 | 0.749515 | 2 | 11.429 |
| 1.07655 | 0.16826 | 1.08841 | 8.44733 | 0.527911 | 3 | 17.143 |
| -0.74301 | 0.41863 | 0.84884 | 151.08420 | 0.411398 | 4 | 22.857 |
| -1.17044 | -0.69989 | 1.35118 | 209.19704 | 0.654825 | 5 | 28.571 |
| -0.27284 | -0.19992 | 0.33573 | 215.70140 | 0.162716 | 6 | 34.286 |
| 0.46562 | 0.23456 | 0.52137 | 26.73642 | 0.252666 | 7 | 40.000 |
| -0.24949 | -0.54986 | 0.60388 | 245.56388 | 0.292292 | 8 | 45.714 |
| 0.10983 | -0.02172 | 0.11899 | 359.99872 | 0.158532 | 9 | 51.429 |
| -0.03974 | 0.43838 | 0.44017 | 95.17993 | 0.213336 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 218.27945 | | | | | 0 | |
| 26.98117 | 22.19212 | 34.93527 | 39.43742 | 1.000000 | 1 | 5.714 |
| -1.14983 | 6.62136 | 6.72832 | 99.84479 | 0.192565 | 2 | 11.429 |
| 0.14499 | 3.72944 | 3.73228 | 87.77354 | 0.106834 | 3 | 17.143 |
| 0.01962 | 2.39858 | 2.39858 | 89.52962 | 0.068629 | 4 | 22.857 |
| -2.35328 | 2.55982 | 3.47362 | 132.64035 | 0.099436 | 5 | 28.571 |
| -0.18186 | 0.74650 | 0.76833 | 103.69139 | 0.021993 | 6 | 34.286 |
| -0.60991 | 1.42591 | 1.55087 | 113.15819 | 0.044393 | 7 | 40.000 |
| -1.51276 | 0.73530 | 1.68199 | 154.07724 | 0.048146 | 8 | 45.714 |
| 1.47615 | 0.62014 | 1.60345 | 22.98529 | 0.045898 | 9 | 51.429 |
| 0.67686 | 1.05731 | 1.25558 | 57.37866 | 0.035940 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.94855 | | | | | 0 | |
| 1.03853 | 8.07294 | 8.13947 | 82.66948 | 1.000000 | 1 | 5.714 |
| -2.37525 | -1.24689 | 2.68262 | 207.69746 | 0.329581 | 2 | 11.429 |
| 3.34695 | 0.68839 | 3.41662 | 11.62374 | 0.419760 | 3 | 17.143 |
| -1.08761 | 1.26682 | 1.61868 | 128.49815 | 0.198868 | 4 | 22.857 |
| -3.92717 | -0.39464 | 3.94695 | 185.73839 | 0.484914 | 5 | 28.571 |
| -0.44169 | -1.11935 | 1.20334 | 248.46680 | 0.147840 | 6 | 34.286 |
| -0.46660 | 1.06169 | 1.15970 | 113.72520 | 0.142479 | 7 | 40.000 |
| -2.38309 | -0.03430 | 2.38424 | 180.82417 | 0.292923 | 8 | 45.714 |
| 1.53877 | 0.64957 | 1.67825 | 22.80835 | 0.205284 | 9 | 51.429 |
| -0.45221 | 0.19375 | 0.49197 | 156.80725 | 0.060443 | 10 | 57.143 |

TEXT NOT REPRODUCIBLE

HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 963 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 176.42334 | | | | | 0 | |
| 29.98184 | 14.98191 | 28.23463 | 31.85411 | 1.000000 | 1 | 5.714 |
| -0.46798 | 3.84253 | 3.87829 | 96.74284 | 0.109825 | 2 | 11.429 |
| 1.09683 | 2.29728 | 2.49242 | 64.91154 | 0.088275 | 3 | 17.143 |
| 1.88892 | 1.81884 | 2.11395 | 90.27046 | 0.074928 | 4 | 22.857 |
| -1.93121 | 1.92745 | 2.44164 | 128.46443 | 0.087185 | 5 | 28.571 |
| 0.95370 | 0.67911 | 1.16846 | 35.29428 | 0.041384 | 6 | 34.286 |
| 0.20614 | 1.78875 | 1.79864 | 83.19876 | 0.063491 | 7 | 40.000 |
| -1.58895 | 0.62444 | 1.69887 | 197.47878 | 0.057744 | 8 | 45.714 |
| 0.54681 | 0.31185 | 0.74427 | 41.42986 | 0.026360 | 9 | 51.429 |
| -0.11296 | 0.70861 | 0.71240 | 99.08886 | 0.025234 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 963 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.46321 | | | | | 0 | |
| 3.28899 | 9.52435 | 10.07525 | 70.96888 | 1.000000 | 1 | 5.714 |
| -0.79887 | -1.11494 | 1.37160 | 234.37888 | 0.136135 | 2 | 11.429 |
| 1.93244 | -0.30829 | 1.97139 | 347.30110 | 0.195946 | 3 | 17.143 |
| -1.38894 | 1.08968 | 1.66961 | 142.38751 | 0.165714 | 4 | 22.857 |
| -2.48889 | -0.48788 | 2.53872 | 191.68788 | 0.251678 | 5 | 28.571 |
| -0.88889 | -1.66692 | 1.78827 | 252.84238 | 0.172529 | 6 | 34.286 |
| -1.48944 | 0.71447 | 1.68782 | 153.68868 | 0.190962 | 7 | 40.000 |
| -1.99898 | 0.48744 | 2.03792 | 167.61598 | 0.202278 | 8 | 45.714 |
| 0.88827 | 0.81873 | 1.21985 | 42.15782 | 0.121074 | 9 | 51.429 |
| -0.19888 | -0.16124 | 0.29449 | 219.31514 | 0.029259 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 963 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 222.77879 | | | | | 0 | |
| 29.28835 | 11.56844 | 31.48826 | 21.99817 | 1.000000 | 1 | 5.714 |
| 1.44253 | 4.55894 | 4.77979 | 72.18288 | 0.151885 | 2 | 11.429 |
| 0.55745 | 1.41318 | 1.51988 | 68.47122 | 0.048244 | 3 | 17.143 |
| 1.28749 | 2.95882 | 3.21947 | 66.42757 | 0.102258 | 4 | 22.857 |
| -2.89944 | 1.68848 | 2.64884 | 141.12848 | 0.083441 | 5 | 28.571 |
| 1.83867 | 0.22875 | 1.85188 | 6.89677 | 0.058889 | 6 | 34.286 |
| 1.28889 | 2.41571 | 2.49782 | 62.57675 | 0.079373 | 7 | 40.888 |
| -0.48848 | -0.24419 | 0.54685 | 206.38419 | 0.017342 | 8 | 45.714 |
| -0.17854 | 1.07281 | 1.08828 | 99.83271 | 0.034288 | 9 | 51.429 |
| -0.38126 | 0.98892 | 0.98799 | 188.33784 | 0.038411 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 963 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -11.24878 | | | | | 0 | |
| 7.79884 | 12.28887 | 14.52159 | 57.74471 | 1.000000 | 1 | 5.714 |
| 1.84888 | -2.83138 | 2.26867 | 298.44489 | 0.156228 | 2 | 11.429 |
| -1.29867 | -2.58943 | 2.8432 | 241.61388 | 0.182823 | 3 | 17.143 |
| -2.88384 | 0.89988 | 2.92318 | 166.15249 | 0.201294 | 4 | 22.857 |
| -0.94198 | -2.35888 | 2.53918 | 248.22473 | 0.174854 | 5 | 28.571 |
| -0.97898 | -2.88849 | 2.73457 | 249.83288 | 0.188311 | 6 | 34.286 |
| -1.98882 | 0.39982 | 1.98886 | 169.48621 | 0.135927 | 7 | 48.888 |
| -0.97884 | -0.17116 | 0.98812 | 190.08869 | 0.067839 | 8 | 45.714 |
| -0.44881 | 1.87881 | 1.16818 | 112.59886 | 0.888382 | 9 | 51.429 |
| 0.38831 | -0.87819 | 0.94288 | 348.24414 | 0.827888 | 10 | 57.143 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 179.75476 | | | | | 0 | |
| 11.95249 | -0.86734 | 11.98392 | 355.84937 | 1.000000 | 1 | 5.714 |
| 0.77899 | 7.60184 | 7.64165 | 84.14986 | 0.637658 | 2 | 11.429 |
| 0.24272 | 1.04971 | 1.08208 | 73.94847 | 0.090295 | 3 | 17.143 |
| 2.33129 | 2.12065 | 2.50309 | 57.68833 | 0.208938 | 4 | 22.857 |
| -1.56567 | 0.98625 | 1.85041 | 147.79222 | 0.154408 | 5 | 28.571 |
| 1.51288 | 0.39914 | 1.56388 | 14.78679 | 0.130498 | 6 | 34.286 |
| 1.86796 | 2.10522 | 2.82751 | 48.12096 | 0.235962 | 7 | 40.000 |
| -0.19353 | -1.13431 | 1.15070 | 260.31787 | 0.096030 | 8 | 45.714 |
| -0.31006 | 2.20770 | 2.22937 | 97.99469 | 0.186050 | 9 | 51.429 |
| 0.39822 | 0.99226 | 1.06919 | 68.13201 | 0.089218 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.66321 | | | | | 0 | |
| 2.51828 | -1.29189 | 2.83932 | 332.84180 | 0.099811 | 1 | 5.714 |
| 0.35563 | 2.69693 | 2.72028 | 82.48887 | 0.086082 | 2 | 11.429 |
| -0.33548 | -0.14040 | 0.35447 | 203.33209 | 0.112191 | 3 | 17.143 |
| 0.09394 | -0.07274 | 0.11861 | 322.24078 | 0.037585 | 4 | 22.857 |
| -2.68178 | -2.37676 | 3.19958 | 228.78821 | 1.000000 | 5 | 28.571 |
| 0.15887 | 0.07148 | 0.17421 | 24.22467 | 0.055139 | 6 | 34.286 |
| 0.29998 | 0.03458 | 0.30206 | 70.22969 | 0.095595 | 7 | 40.000 |
| -1.19881 | -1.68968 | 2.06435 | 235.74179 | 0.647849 | 8 | 45.714 |
| -0.38954 | 1.35961 | 1.39342 | 102.83499 | 0.441826 | 9 | 51.429 |
| 0.13894 | -0.23679 | 0.27454 | 300.48881 | 0.086893 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 211.80476 | | | | | 0 | |
| -0.78520 | -16.12204 | 16.14114 | 267.21167 | 1.000006 | 1 | 5.714 |
| -3.88262 | 11.10475 | 11.83949 | 109.14374 | 0.733497 | 2 | 11.429 |
| 2.96527 | 4.07240 | 5.02467 | 54.14382 | 0.311296 | 3 | 17.143 |
| 0.39375 | 1.14481 | 1.20988 | 71.00751 | 0.074956 | 4 | 22.857 |
| -1.14809 | 3.14287 | 3.34680 | 110.06734 | 0.207296 | 5 | 28.571 |
| 1.99473 | -1.54181 | 2.52113 | 322.29785 | 0.156193 | 6 | 34.286 |
| 1.58159 | 2.90833 | 3.31056 | 61.46202 | 0.205101 | 7 | 40.000 |
| 0.84963 | -1.38644 | 1.38753 | 272.84988 | 0.085962 | 8 | 45.714 |
| -1.13190 | 3.39165 | 3.57534 | 108.45558 | 0.221517 | 9 | 51.429 |
| 1.34610 | 2.17383 | 2.55686 | 58.23293 | 0.158406 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 87.12379 | | | | | 0 | |
| -6.36876 | -11.61343 | 13.24511 | 241.25914 | 1.000000 | 1 | 5.714 |
| -6.68814 | 7.07768 | 9.68166 | 133.02641 | 0.730961 | 2 | 11.429 |
| 2.28657 | 3.75312 | 4.39480 | 58.64832 | 0.331806 | 3 | 17.143 |
| -1.20008 | -1.58236 | 1.98597 | 232.82295 | 0.149940 | 4 | 22.857 |
| -1.61485 | -6.38178 | 1.69096 | 193.30148 | 0.125201 | 5 | 28.571 |
| 0.52896 | -2.80112 | 2.85062 | 280.69360 | 0.215221 | 6 | 34.286 |
| 0.05004 | 3.26272 | 3.26312 | 89.10718 | 0.246364 | 7 | 40.000 |
| -0.05217 | -2.04997 | 2.05063 | 271.45776 | 0.154822 | 8 | 45.714 |
| -1.55072 | 3.45913 | 3.79002 | 114.14661 | 0.286105 | 9 | 51.429 |
| 1.24364 | 1.63789 | 2.05591 | 52.77670 | 0.155220 | 10 | 57.143 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 113.17415 | | | | | 0 | |
| -4.33330 | -13.04888 | 13.74957 | 251.62955 | 1.000000 | 1 | 5.714 |
| -3.78656 | 6.16810 | 7.23765 | 121.54561 | 0.526390 | 2 | 11.429 |
| 2.58637 | 3.22725 | 4.13575 | 51.29076 | 0.300791 | 3 | 17.143 |
| -0.31517 | 0.?4694 | 0.34774 | 155.00356 | 0.025291 | 4 | 22.857 |
| -0.36377 | 2.47532 | 2.50191 | 98.36035 | 0.181962 | 5 | 28.571 |
| 1.15731 | -1.67678 | 2.03739 | 304.61328 | 0.148178 | 6 | 34.286 |
| 0.44471 | 1.68469 | 1.74761 | 74.57877 | 0.127103 | 7 | 40.000 |
| 0.16838 | -0.64025 | 0.66202 | 284.73462 | 0.048149 | 8 | 45.714 |
| -0.90711 | 1.89528 | 2.10117 | 115.57663 | 0.152817 | 9 | 51.429 |
| 0.94453 | 1.50390 | 1.77591 | 57.86879 | 0.129161 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 59.59244 | | | | | 0 | |
| -5.25930 | -8.28648 | 10.32110 | 232.66624 | 1.000000 | 1 | 5.714 |
| -6.10085 | 4.50986 | 7.58677 | 143.52753 | 0.735074 | 2 | 11.429 |
| 2.00439 | 3.15135 | 3.73478 | 57.54193 | 0.361859 | 3 | 17.143 |
| -1.61299 | -1.34497 | 2.10016 | 219.82248 | 0.203482 | 4 | 22.857 |
| -0.19903 | 0.75420 | 0.78002 | 104.78319 | 0.075575 | 5 | 28.571 |
| 0.29987 | -3.00400 | 3.01356 | 274.56543 | 0.291941 | 6 | 34.286 |
| -0.41157 | 2.50739 | 2.54094 | 99.32155 | 0.246189 | 7 | 40.000 |
| 0.71816 | -0.87748 | 1.13390 | 309.29785 | 0.109862 | 8 | 45.714 |
| -1.36862 | 2.47935 | 2.83202 | 118.89905 | 0.274391 | 9 | 51.429 |
| 1.14200 | 1.66058 | 2.01536 | 55.48335 | 0.195266 | 10 | 57.143 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.05872 | | | | | 0 | |
| -0.39277 | -1.09603 | 1.16428 | 250.28465 | 1.000000 | 1 | 5.714 |
| -0.32239 | 0.49702 | 0.59242 | 122.96919 | 0.508833 | 2 | 11.429 |
| 0.21836 | 0.27016 | 0.34736 | 51.05226 | 0.298361 | 3 | 17.143 |
| -0.03096 | 0.00656 | 0.03165 | 168.04848 | 0.027182 | 4 | 22.857 |
| -0.02625 | 0.20702 | 0.20869 | 97.25348 | 0.179241 | 5 | 28.571 |
| 0.09219 | -0.14363 | 0.17149 | 303.11621 | 0.147293 | 6 | 34.286 |
| 0.03319 | 0.13642 | 0.14040 | 76.32800 | 0.120591 | 7 | 40.000 |
| 0.01501 | -0.05033 | 0.05252 | 286.61011 | 0.045109 | 8 | 45.714 |
| -0.07599 | 0.15301 | 0.17084 | 116.41188 | 0.146734 | 9 | 51.429 |
| 0.07829 | 0.12429 | 0.14685 | 57.79454 | 0.126168 | 10 | 57.143 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 563 TEST COND 4 COMP RUN 37.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.92641 | | | | | 0 | |
| -0.53389 | -0.68190 | 0.86604 | 231.94112 | 1.000000 | 1 | 5.714 |
| -0.51725 | 0.37028 | 0.63612 | 144.40266 | 0.734521 | 2 | 11.429 |
| 0.16951 | 0.26555 | 0.31504 | 57.44918 | 0.363773 | 3 | 17.143 |
| -0.13933 | -0.11335 | 0.17962 | 219.13062 | 0.207399 | 4 | 22.857 |
| -0.00904 | 0.07097 | 0.07154 | 97.25708 | 0.082605 | 5 | 28.571 |
| -0.01897 | -0.25676 | 0.25746 | 274.22485 | 0.297278 | 6 | 34.286 |
| -0.03739 | 0.20942 | 0.21274 | 100.12396 | 0.245641 | 7 | 40.000 |
| 0.00497 | -0.00819 | 0.00958 | 313.61475 | 0.110751 | 8 | 45.714 |
| -0.11549 | 0.20567 | 0.23588 | 119.31503 | 0.272362 | 9 | 51.429 |
| 0.09667 | 0.14163 | 0.17148 | 55.68497 | 0.198003 | 10 | 57.143 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.43476 | | | | | 0 | |
| 0.03745 | 0.31927 | 0.32146 | 83.30945 | 1.000000 | 1 | 5.848 |
| 0.23809 | 0.03565 | 0.24075 | 8.51626 | 0.748917 | 2 | 11.696 |
| -0.02422 | 0.02324 | 0.03356 | 136.18881 | 0.104409 | 3 | 17.544 |
| 0.02901 | -0.01241 | 0.03238 | 337.47363 | 0.100741 | 4 | 23.392 |
| 0.02644 | -0.00228 | 0.02676 | 355.41743 | 0.083237 | 5 | 29.240 |
| 0.02463 | 0.01193 | 0.02736 | 25.84493 | 0.085122 | 6 | 35.088 |
| 0.03034 | 0.03597 | 0.04187 | 39.95121 | 0.130264 | 7 | 40.936 |
| -0.01809 | 0.00276 | 0.01830 | 171.33383 | 0.056923 | 8 | 46.784 |
| -0.00322 | -0.04232 | 0.04244 | 269.65405 | 0.132023 | 9 | 52.632 |
| 0.03208 | 0.01447 | 0.03327 | 24.97510 | 0.103527 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -4.72949 | | | | | 0 | |
| 0.18979 | 0.18857 | 0.21865 | 29.77174 | 1.000000 | 1 | 5.848 |
| 0.15931 | -0.04857 | 0.16273 | 342.63306 | 0.744247 | 2 | 11.696 |
| -0.15126 | -0.10988 | 0.18649 | 215.79527 | 0.852934 | 3 | 17.544 |
| -0.02890 | -0.11252 | 0.11617 | 255.99200 | 0.531316 | 4 | 23.392 |
| -0.00984 | 0.04453 | 0.04561 | 102.45848 | 0.208582 | 5 | 29.240 |
| -0.02183 | 0.00031 | 0.02336 | 159.14944 | 0.106829 | 6 | 35.088 |
| -0.10809 | -0.01126 | 0.10868 | 185.96589 | 0.497057 | 7 | 40.936 |
| -0.04285 | 0.03395 | 0.05451 | 141.46125 | 0.249316 | 8 | 46.784 |
| -0.01118 | -0.03787 | 0.03944 | 253.94485 | 0.180390 | 9 | 52.632 |
| -0.03423 | 0.07802 | 0.08603 | 114.90858 | 0.393449 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.04113 | | | | | 0 | |
| 0.17377 | 1.58429 | 1.59379 | 84.74872 | 1.000000 | 1 | 5.848 |
| 1.18169 | 0.10060 | 1.19541 | 4.68962 | 0.750043 | 2 | 11.696 |
| -0.11810 | 0.11067 | 0.16742 | 136.86136 | 0.105044 | 3 | 17.544 |
| 0.15827 | -0.05851 | 0.16873 | 339.71216 | 0.105870 | 4 | 23.392 |
| 0.12986 | -0.01164 | 0.13038 | 354.87915 | 0.081806 | 5 | 29.240 |
| 0.12627 | 0.04001 | 0.13509 | 20.81821 | 0.084758 | 6 | 35.088 |
| 0.27536 | 0.16283 | 0.27803 | 35.84697 | 0.174444 | 7 | 40.936 |
| -0.00916 | 0.00805 | 0.00952 | 174.86262 | 0.056170 | 8 | 46.784 |
| -0.01217 | -0.19218 | 0.19256 | 266.37695 | 0.120821 | 9 | 52.632 |
| 0.15226 | 0.07357 | 0.16911 | 25.78995 | 0.106103 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -22.39365 | | | | | 0 | |
| 0.87389 | 0.41119 | 0.96507 | 25.21854 | 1.000000 | 1 | 5.848 |
| 0.76562 | -0.26229 | 0.79189 | 343.19946 | 0.820552 | 2 | 11.696 |
| -0.72469 | -0.51021 | 0.88628 | 215.14697 | 0.918356 | 3 | 17.544 |
| -0.14612 | -0.52107 | 0.54117 | 254.33556 | 0.560756 | 4 | 23.392 |
| -0.06278 | 0.21747 | 0.22635 | 106.10319 | 0.234538 | 5 | 29.240 |
| -0.08449 | 0.02309 | 0.08799 | 164.71252 | 0.090755 | 6 | 35.088 |
| -0.50915 | -0.05628 | 0.50027 | 186.34821 | 0.526644 | 7 | 40.936 |
| -0.20296 | 0.15788 | 0.25714 | 142.12112 | 0.266444 | 8 | 46.784 |
| -0.04868 | -0.17844 | 0.17726 | 254.96023 | 0.183672 | 9 | 52.632 |
| -0.16635 | 0.14978 | 0.40548 | 114.22047 | 0.420152 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING COMPONENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.90479 | | | | | 0 | |
| 0.39758 | 4.10525 | 4.12445 | 84.46834 | 1.000000 | 1 | 5.848 |
| 3.08322 | 0.48406 | 3.10123 | 8.97980 | 0.751914 | 2 | 11.696 |
| -0.29695 | 0.32229 | 0.43823 | 132.65628 | 0.106252 | 3 | 17.544 |
| 0.49300 | -0.13824 | 0.47362 | 343.03003 | 0.114833 | 4 | 23.392 |
| 0.32594 | -0.03159 | 0.32746 | 354.46436 | 0.079396 | 5 | 29.240 |
| 0.34494 | 0.07571 | 0.35315 | 12.37954 | 0.085624 | 6 | 35.088 |
| 0.47756 | 0.35361 | 0.59425 | 36.52167 | 0.144079 | 7 | 40.936 |
| -0.22842 | -0.00369 | 0.22845 | 180.92459 | 0.055389 | 8 | 46.784 |
| -0.01502 | -0.42036 | 0.42063 | 267.95312 | 0.101985 | 9 | 52.632 |
| 0.36443 | 0.19407 | 0.41288 | 28.03719 | 0.100106 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -53.34464 | | | | | 0 | |
| 1.96321 | 0.50923 | 2.02817 | 14.54133 | 0.953675 | 1 | 5.848 |
| 1.96199 | -0.35507 | 1.99386 | 349.74170 | 0.937536 | 2 | 11.696 |
| -1.76491 | -1.18658 | 2.12670 | 213.91364 | 1.000000 | 3 | 17.544 |
| -0.39836 | -1.18770 | 1.25020 | 251.80588 | 0.587859 | 4 | 23.392 |
| -0.22356 | 0.54830 | 0.59213 | 112.18198 | 0.278424 | 5 | 29.240 |
| -0.11586 | -0.01931 | 0.11667 | 189.52719 | 0.054861 | 6 | 35.088 |
| -1.17270 | -0.14711 | 1.18209 | 187.14083 | 0.555833 | 7 | 40.936 |
| -0.48815 | 0.36299 | 0.60832 | 143.36572 | 0.286038 | 8 | 46.784 |
| -0.09642 | -0.36558 | 0.37808 | 255.22475 | 0.177779 | 9 | 52.632 |
| -0.37251 | 0.88244 | 0.95784 | 112.88631 | 0.450388 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 44.09306 | | | | | 0 | |
| 0.53054 | 10.94140 | 10.95425 | 87.22391 | 1.000000 | 1 | 5.848 |
| 7.98695 | 1.40947 | 8.11036 | 10.00806 | 0.740384 | 2 | 11.696 |
| -0.78198 | 1.02185 | 1.28673 | 127.42540 | 0.117464 | 3 | 17.544 |
| 1.51837 | -0.22287 | 1.53464 | 351.64966 | 0.140095 | 4 | 23.392 |
| 0.79134 | -0.04402 | 0.79256 | 356.81592 | 0.072352 | 5 | 29.240 |
| 1.06882 | -0.21351 | 1.08994 | 348.70312 | 0.099499 | 6 | 35.088 |
| 0.33947 | 0.35152 | 0.48868 | 45.99957 | 0.044611 | 7 | 40.936 |
| -0.60315 | -0.19681 | 0.63445 | 198.07202 | 0.057918 | 8 | 46.784 |
| 0.11633 | -0.44756 | 0.46243 | 284.56982 | 0.042215 | 9 | 52.632 |
| 0.71617 | 0.53886 | 0.89625 | 36.95840 | 0.081818 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -103.64984 | | | | | 0 | |
| 2.63141 | -3.78920 | 4.61328 | 304.77783 | 0.899909 | 1 | 5.848 |
| 5.10781 | 0.44528 | 5.12638 | 4.98300 | 1.000000 | 2 | 11.696 |
| -3.62399 | -1.98969 | 4.13234 | 208.71960 | 0.806092 | 3 | 17.544 |
| -1.18474 | -1.83758 | 2.16639 | 237.18900 | 0.424498 | 4 | 23.392 |
| -1.13875 | 1.40454 | 1.85516 | 127.88670 | 0.361885 | 5 | 29.240 |
| 0.61180 | -0.77234 | 0.98530 | 308.38428 | 0.192201 | 6 | 35.088 |
| -2.01575 | -0.43480 | 2.06194 | 192.15039 | 0.402222 | 7 | 40.936 |
| -1.08118 | 0.61480 | 1.17488 | 148.44713 | 0.229183 | 8 | 46.784 |
| 0.03367 | -0.32328 | 0.32502 | 275.94678 | 0.063402 | 9 | 52.632 |
| -0.50067 | 1.72529 | 1.79647 | 106.18250 | 0.350435 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 90.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 45.37683 | | | | | 0 | |
| -0.13133 | 12.45093 | 12.45123 | 90.60437 | 1.000000 | 1 | 5.860 |
| 9.86746 | 1.81965 | 9.24824 | 11.34733 | 0.742757 | 2 | 11.696 |
| -0.77921 | 1.37162 | 1.57750 | 119.60875 | 0.126695 | 3 | 17.544 |
| 2.38297 | 0.86491 | 2.30388 | 350.30550 | 0.185032 | 4 | 23.392 |
| 0.75868 | -0.85963 | 0.76894 | 355.50537 | 0.061114 | 5 | 29.240 |
| 1.49819 | -0.98816 | 1.71783 | 328.80472 | 0.137988 | 6 | 35.088 |
| -1.07223 | -0.53437 | 1.19881 | 206.48862 | 0.096216 | 7 | 40.936 |
| -0.65363 | -0.35491 | 0.85741 | 220.28895 | 0.068861 | 8 | 46.784 |
| 0.36092 | 0.55298 | 0.66094 | 56.88876 | 0.053094 | 9 | 52.632 |
| 0.40377 | 0.65853 | 0.77246 | 58.68624 | 0.062030 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 90.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -54.24481 | | | | | 0 | |
| -1.10225 | -11.98687 | 12.03644 | 264.74561 | 1.000000 | 1 | 5.860 |
| 9.52376 | 2.80542 | 6.19335 | 26.02917 | 0.514707 | 2 | 11.696 |
| -2.59892 | -0.40592 | 2.90892 | 100.81370 | 0.215253 | 3 | 17.544 |
| -1.91685 | 0.11725 | 1.52137 | 175.57997 | 0.126395 | 4 | 23.392 |
| -2.13197 | 1.40446 | 2.59786 | 145.19182 | 0.215829 | 5 | 29.240 |
| 2.12103 | -1.96844 | 2.89384 | 317.13379 | 0.240419 | 6 | 35.088 |
| -0.44459 | -0.51954 | 0.68388 | 229.44542 | 0.056810 | 7 | 40.936 |
| -0.62738 | 0.87795 | 0.63215 | 172.98316 | 0.052519 | 8 | 46.784 |
| 0.45143 | 0.67172 | 0.80832 | 56.09718 | 0.067180 | 9 | 52.632 |
| 0.22860 | 0.93229 | 0.95990 | 76.22282 | 0.079748 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 90.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 60.05707 | | | | | 0 | |
| 0.56002 | 15.13086 | 15.14922 | 87.88141 | 1.000000 | 1 | 5.860 |
| 13.15063 | 2.49036 | 13.38435 | 10.72322 | 0.883501 | 2 | 11.696 |
| -0.17095 | 1.27972 | 1.29169 | 97.60081 | 0.085225 | 3 | 17.544 |
| 3.85095 | -0.24344 | 3.85844 | 356.30257 | 0.254709 | 4 | 23.392 |
| 0.72778 | -0.74842 | 1.04393 | 314.19891 | 0.068918 | 5 | 29.240 |
| 1.78169 | -1.34716 | 2.23366 | 322.90649 | 0.147444 | 6 | 35.088 |
| -1.63893 | -0.90194 | 1.87072 | 208.82497 | 0.123486 | 7 | 40.936 |
| -0.41667 | -1.14796 | 1.22124 | 250.09874 | 0.080616 | 8 | 46.784 |
| 0.29894 | 0.92800 | 0.97478 | 72.17786 | 0.064345 | 9 | 52.632 |
| 0.20372 | 1.02475 | 1.04480 | 78.75623 | 0.068968 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 90.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -13.90941 | | | | | 0 | |
| -2.67423 | -12.33900 | 12.62546 | 257.77124 | 1.000000 | 1 | 5.860 |
| 5.41093 | 5.19508 | 7.50691 | 43.79181 | 0.594585 | 2 | 11.696 |
| -4.27006 | -0.18332 | 4.27408 | 182.40586 | 0.338520 | 3 | 17.544 |
| -1.18857 | 2.23144 | 2.52824 | 118.04295 | 0.200256 | 4 | 23.392 |
| -2.75477 | -0.23531 | 2.76488 | 184.88237 | 0.218986 | 5 | 29.240 |
| 2.68898 | -2.12173 | 3.42269 | 321.70410 | 0.271173 | 6 | 35.088 |
| 1.09946 | -0.86002 | 1.18199 | 356.87900 | 0.087212 | 7 | 40.936 |
| -0.11953 | -0.71900 | 0.72886 | 260.56128 | 0.057730 | 8 | 46.784 |
| 0.16565 | 1.14121 | 1.15316 | 81.74091 | 0.091372 | 9 | 52.632 |
| 0.69782 | 0.47593 | 0.84466 | 34.29495 | 0.066901 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 63.05029 | | | | | 0 | |
| 2.44471 | 12.00146 | 12.25193 | 78.39461 | 0.831576 | 1 | 5.848 |
| 14.55197 | 2.30499 | 14.73339 | 9.00071 | 1.000000 | 2 | 11.696 |
| 1.29620 | 0.10311 | 1.30030 | 4.54818 | 0.088255 | 3 | 17.544 |
| 4.34029 | -0.80679 | 4.41464 | 349.46973 | 0.299835 | 4 | 23.392 |
| 0.33278 | -1.82418 | 1.85428 | 280.33862 | 0.125856 | 5 | 29.240 |
| 1.29066 | -0.90515 | 1.57642 | 324.95752 | 0.106996 | 6 | 35.088 |
| -0.67100 | -0.30430 | 0.56075 | 212.86537 | 0.038060 | 7 | 40.936 |
| 0.21064 | -1.42121 | 1.43674 | 278.43042 | 0.097516 | 8 | 46.784 |
| -0.21004 | 0.22720 | 0.30947 | 132.74272 | 0.021005 | 9 | 52.632 |
| 0.10347 | 1.09252 | 1.09741 | 84.58948 | 0.074485 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.55222 | | | | | 0 | |
| -0.43775 | 1.44727 | 1.51203 | 106.82890 | 0.220409 | 1 | 5.848 |
| 2.44474 | 5.03422 | 5.58606 | 63.89537 | 0.817201 | 2 | 11.696 |
| -6.75266 | -1.20937 | 6.86010 | 190.15372 | 1.000000 | 3 | 17.544 |
| 0.29497 | 3.13931 | 3.15314 | 84.63216 | 0.459634 | 4 | 23.392 |
| -1.58422 | -3.54092 | 3.87916 | 245.89601 | 0.565466 | 5 | 29.240 |
| 1.01792 | -0.24968 | 1.04810 | 346.21809 | 0.152781 | 6 | 35.088 |
| 1.92850 | 0.85964 | 2.11142 | 24.02514 | 0.307782 | 7 | 40.936 |
| 0.47999 | -1.43859 | 1.51656 | 288.45142 | 0.221069 | 8 | 46.784 |
| -0.99318 | 0.57050 | 1.06827 | 167.72133 | 0.155723 | 9 | 52.632 |
| 0.96334 | 0.13089 | 0.58047 | 13.94472 | 0.084615 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 52.37823 | | | | | 0 | |
| 3.02428 | 7.16166 | 7.77403 | 67.10626 | 0.631028 | 1 | 5.848 |
| 12.20479 | 1.67833 | 12.31964 | 7.82985 | 1.000000 | 2 | 11.696 |
| 2.09027 | -0.64250 | 2.15813 | 342.67993 | 0.175178 | 3 | 17.544 |
| 3.46756 | -1.19333 | 3.65439 | 341.59961 | 0.296632 | 4 | 23.392 |
| -0.02936 | -2.04647 | 2.04668 | 269.17798 | 0.166131 | 5 | 29.240 |
| 0.82293 | -0.47331 | 0.94785 | 330.25146 | 0.076938 | 6 | 35.088 |
| 0.40300 | 0.08544 | 0.41197 | 11.97328 | 0.033440 | 7 | 40.936 |
| 0.36315 | -1.19225 | 1.24633 | 286.96819 | 0.101166 | 8 | 46.784 |
| -0.42234 | -0.17642 | 0.45771 | 202.67165 | 0.037153 | 9 | 52.632 |
| 0.12208 | 0.73807 | 0.74819 | 80.50764 | 0.060724 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.12154 | | | | | 0 | |
| 1.27518 | 9.10861 | 9.19744 | 82.03050 | 1.000000 | 1 | 5.848 |
| 0.45804 | 3.52791 | 3.55752 | 82.68849 | 0.386794 | 2 | 11.696 |
| -6.22698 | -1.28565 | 6.35851 | 191.66565 | 0.691313 | 3 | 17.544 |
| 0.94311 | 2.46018 | 2.63476 | 69.02560 | 0.286467 | 4 | 23.392 |
| -0.34964 | -4.40328 | 4.41714 | 265.45996 | 0.480257 | 5 | 29.240 |
| -0.14627 | 0.77615 | 0.78981 | 100.67294 | 0.085873 | 6 | 35.088 |
| 1.73858 | 0.96450 | 1.98915 | 29.07059 | 0.216272 | 7 | 40.936 |
| 0.56995 | -1.50624 | 1.61046 | 290.72632 | 0.175099 | 8 | 46.784 |
| -1.23831 | 0.20352 | 1.25493 | 170.66673 | 0.136443 | 9 | 52.632 |
| 0.36602 | -0.15101 | 0.39780 | 337.69043 | 0.043251 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 60.76030 | | | | | 0 | |
| 4.36395 | 6.24879 | 7.62177 | 55.07083 | 0.551615 | 1 | 5.848 |
| 13.71459 | 1.68072 | 13.81719 | 6.98675 | 1.000000 | 2 | 11.696 |
| 3.18641 | -1.14066 | 3.38442 | 340.30371 | 0.244943 | 3 | 17.544 |
| 3.38920 | -1.95090 | 3.91059 | 330.07422 | 0.283024 | 4 | 23.392 |
| -0.37738 | -2.63140 | 2.65832 | 261.83838 | 0.192392 | 5 | 29.240 |
| 1.19977 | -0.49572 | 1.29814 | 337.55054 | 0.093951 | 6 | 35.088 |
| 0.81944 | -0.05231 | 0.82111 | 356.34741 | 0.059426 | 7 | 40.936 |
| -0.00867 | -1.32504 | 1.32506 | 269.71143 | 0.095899 | 8 | 46.784 |
| -0.43338 | 0.09482 | 0.44363 | 167.65796 | 0.032107 | 9 | 52.632 |
| 0.43385 | 0.30608 | 0.53096 | 35.20320 | 0.038427 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.33304 | | | | | 0 | |
| 2.66194 | 13.63856 | 13.89591 | 78.95593 | 1.000000 | 1 | 5.848 |
| -0.13202 | 3.11454 | 3.11734 | 92.42726 | 0.224335 | 2 | 11.696 |
| -5.82770 | -0.44710 | 5.84482 | 184.38710 | 0.420615 | 3 | 17.544 |
| 1.22842 | 1.81504 | 2.19166 | 55.90985 | 0.157720 | 4 | 23.392 |
| 0.36525 | -5.42193 | 5.43421 | 273.85400 | 0.391065 | 5 | 29.240 |
| -0.39430 | 0.98737 | 1.06318 | 111.76894 | 0.076511 | 6 | 35.088 |
| 1.88782 | 0.55832 | 1.96865 | 16.47545 | 0.141671 | 7 | 40.936 |
| 0.43829 | -2.16368 | 2.20762 | 281.45117 | 0.158868 | 8 | 46.784 |
| -1.64611 | 0.76520 | 1.65379 | 152.43880 | 0.119013 | 9 | 52.632 |
| 0.63382 | -0.75690 | 0.98723 | 309.94238 | 0.071045 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 150.24147 | | | | | 0 | |
| 11.16046 | 8.60623 | 14.09337 | 37.63708 | 0.443831 | 1 | 5.848 |
| 31.55725 | 3.52836 | 31.75388 | 6.37963 | 1.000000 | 2 | 11.696 |
| 10.26410 | -3.42587 | 10.82074 | 341.54224 | 0.340769 | 3 | 17.544 |
| 5.63548 | -6.95458 | 8.95124 | 309.01855 | 0.281895 | 4 | 23.392 |
| -1.58529 | -6.53261 | 6.82781 | 253.09569 | 0.215017 | 5 | 29.240 |
| 4.21409 | -1.67621 | 4.53522 | 336.30908 | 0.142824 | 6 | 35.088 |
| 2.22391 | -1.21207 | 2.53276 | 331.40859 | 0.079762 | 7 | 40.936 |
| -2.05762 | -2.63078 | 3.34618 | 232.09421 | 0.105379 | 8 | 46.784 |
| -0.45033 | 1.88457 | 1.93763 | 103.43916 | 0.061020 | 9 | 52.632 |
| 2.04709 | -1.38161 | 2.46970 | 325.98389 | 0.077776 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.03943 | | | | | 0 | |
| 8.02028 | 31.29547 | 32.30682 | 75.62575 | 1.000000 | 1 | 5.848 |
| 0.43868 | 4.71548 | 4.73584 | 84.68498 | 0.146589 | 2 | 11.696 |
| -6.43056 | 3.92833 | 7.53551 | 148.57988 | 0.233248 | 3 | 17.544 |
| 1.79087 | -0.15048 | 1.79718 | 355.19678 | 0.055629 | 4 | 23.392 |
| 3.11671 | -11.04416 | 11.47551 | 285.75928 | 0.355204 | 5 | 29.240 |
| -0.07622 | 0.76655 | 0.77033 | 95.67859 | 0.023844 | 6 | 35.088 |
| 3.43099 | -1.56926 | 3.77283 | 335.42163 | 0.116781 | 7 | 40.936 |
| -0.24729 | -5.90715 | 5.91232 | 267.60254 | 0.183005 | 8 | 46.784 |
| -2.50359 | 4.12372 | 4.82421 | 121.26279 | 0.149325 | 9 | 52.632 |
| 2.41774 | -3.89758 | 4.58657 | 301.81201 | 0.141969 | 10 | 58.480 |

TEXT NOT REPRODUCIBLE

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 119.51085 | | | | | 0 | |
| 3.12915 | -3.94945 | 5.03882 | 308.38965 | 0.196454 | 1 | 5.848 |
| 25.40819 | 3.96259 | 25.64880 | 7.98412 | 1.000000 | 2 | 11.696 |
| 9.26082 | -3.68461 | 9.96491 | 338.30377 | 0.388591 | 3 | 17.544 |
| 3.00073 | -6.77304 | 7.44449 | 294.52148 | 0.290247 | 4 | 23.392 |
| -1.26846 | -3.98814 | 4.18409 | 252.39513 | 0.163130 | 5 | 29.240 |
| 2.59022 | -2.34964 | 3.46763 | 317.34424 | 0.135196 | 6 | 35.088 |
| 1.82268 | -0.35283 | 1.89767 | 348.86279 | 0.072627 | 7 | 40.936 |
| -1.42782 | -0.73080 | 1.68220 | 207.13718 | 0.062467 | 8 | 46.784 |
| -0.58020 | 0.19792 | 0.61383 | 161.16417 | 0.023901 | 9 | 52.632 |
| 0.84212 | -1.27187 | 1.52559 | 303.90983 | 0.059472 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 41.89894 | | | | | 0 | |
| 3.68439 | 17.22183 | 17.61153 | 77.92430 | 1.000000 | 1 | 5.848 |
| 4.62426 | 4.38699 | 6.32299 | 42.93457 | 0.359025 | 2 | 11.696 |
| -2.62874 | 3.94974 | 4.74563 | 123.66979 | 0.269408 | 3 | 17.544 |
| -0.92884 | -1.93998 | 2.15046 | 244.63353 | 0.122105 | 4 | 23.392 |
| 5.57044 | -3.29862 | 6.47928 | 329.42627 | 0.367896 | 5 | 29.240 |
| -0.22878 | -2.26262 | 2.27574 | 264.07037 | 0.129228 | 6 | 35.088 |
| 0.02884 | -1.46888 | 1.56488 | 298.12256 | 0.088834 | 7 | 40.936 |
| -0.21784 | -1.22162 | 1.24088 | 259.91167 | 0.070454 | 8 | 46.784 |
| 0.19841 | 0.39158 | 0.43997 | 63.12488 | 0.024985 | 9 | 52.632 |
| 0.76784 | -2.93894 | 3.01528 | 283.57764 | 0.171206 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 141.57822 | | | | | 0 | |
| -9.58888 | -22.28839 | 24.10843 | 246.69844 | 0.771627 | 1 | 5.848 |
| 29.79787 | 5.84344 | 31.24732 | 10.74137 | 1.000000 | 2 | 11.696 |
| 13.29911 | -5.44272 | 14.36975 | 337.74292 | 0.459884 | 3 | 17.544 |
| 3.44494 | -8.88485 | 9.88894 | 291.27244 | 0.284841 | 4 | 23.392 |
| -6.92758 | -2.91819 | 3.88194 | 298.37131 | 0.097878 | 5 | 29.240 |
| 4.88579 | -3.99768 | 3.99783 | 270.48637 | 0.127933 | 6 | 35.088 |
| 2.51306 | 1.84288 | 3.16888 | 36.97734 | 0.100868 | 7 | 40.936 |
| 0.89793 | 1.48821 | 1.88796 | 61.28298 | 0.059889 | 8 | 46.784 |
| -1.66177 | -3.71849 | 4.08112 | 245.66486 | 0.130198 | 9 | 52.632 |
| -1.96449 | -0.14867 | 1.97312 | 183.93529 | 0.050184 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.61647 | | | | | 0 | |
| -2.81288 | 6.98848 | 7.52866 | 111.94888 | 0.498872 | 1 | 5.848 |
| 12.48899 | 8.22384 | 15.09137 | 33.02577 | 1.000000 | 2 | 11.696 |
| -0.33761 | 1.81614 | 3.48886 | 168.86715 | 0.231183 | 3 | 17.544 |
| -5.18499 | -2.24884 | 5.57484 | 203.69444 | 0.369413 | 4 | 23.392 |
| 10.19426 | 4.96467 | 11.13464 | 24.19843 | 0.737815 | 5 | 29.240 |
| -4.88188 | -3.89859 | 5.88861 | 244.31478 | 0.333663 | 6 | 35.088 |
| -0.86894 | 0.18868 | 2.97187 | 177.66658 | 0.178367 | 7 | 40.936 |
| 0.36888 | 5.81784 | 5.42948 | 86.18414 | 0.359782 | 8 | 46.784 |
| 3.81471 | -0.42784 | 7.89989 | 298.12698 | 0.478447 | 9 | 52.632 |
| -0.81882 | -1.48894 | 2.46137 | 214.91951 | 0.163098 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 394 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 107.03493 | | | | | 0 | |
| -9.73069 | -16.39606 | 19.06610 | 239.31177 | 1.000000 | 1 | 5.848 |
| 15.25330 | 2.34079 | 15.43187 | 8.72461 | 0.809388 | 2 | 11.696 |
| 17.53357 | -1.88344 | 17.63443 | 353.86865 | 0.924910 | 3 | 17.544 |
| 2.89366 | -7.44091 | 7.98376 | 291.25824 | 0.418741 | 4 | 23.392 |
| -4.52024 | -4.75769 | 6.56264 | 226.46602 | 0.344204 | 5 | 29.240 |
| 0.40790 | -1.07373 | 1.14859 | 290.80127 | 0.060243 | 6 | 35.088 |
| 2.74206 | 0.85290 | 2.89075 | 17.16016 | 0.151617 | 7 | 40.936 |
| 0.83726 | 1.78229 | 1.96915 | 64.83749 | 0.103288 | 8 | 46.784 |
| -0.68702 | -0.63054 | 0.93251 | 222.54543 | 0.048909 | 9 | 52.632 |
| -0.76465 | -1.35965 | 1.55991 | 240.64720 | 0.081816 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 394 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.73170 | | | | | 0 | |
| -3.23617 | 0.82693 | 3.34015 | 165.66608 | 0.495164 | 1 | 5.848 |
| 6.10649 | 2.86585 | 6.74554 | 25.14128 | 1.000000 | 2 | 11.696 |
| 5.82979 | -1.06716 | 5.92666 | 349.62671 | 0.878804 | 3 | 17.544 |
| -5.26387 | -3.80233 | 6.49289 | 215.84636 | 0.962546 | 4 | 23.392 |
| 3.34828 | 0.74497 | 3.43015 | 12.94356 | 0.508587 | 5 | 29.240 |
| 4.63276 | 3.86934 | 6.03408 | 39.86988 | 0.894826 | 6 | 35.088 |
| -1.21463 | -2.66078 | 2.92491 | 245.46364 | 0.433606 | 7 | 40.936 |
| -2.52537 | -0.26285 | 2.54116 | 186.39867 | 0.376718 | 8 | 46.784 |
| -0.53711 | 1.59587 | 1.68304 | 108.60136 | 0.249622 | 9 | 52.632 |
| 0.94662 | -1.92399 | 2.14429 | 296.19751 | 0.317877 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 394 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 109.38432 | | | | | 0 | |
| -8.76544 | -23.44942 | 25.03619 | 249.50366 | 1.000000 | 1 | 5.848 |
| 5.98204 | 0.00986 | 5.98244 | 0.66013 | 0.238971 | 2 | 11.696 |
| 23.02571 | -0.99433 | 23.04716 | 357.52710 | 0.920627 | 3 | 17.544 |
| 9.60814 | -9.77067 | 11.20790 | 329.01074 | 0.447783 | 4 | 23.392 |
| -8.84534 | -8.24247 | 12.09042 | 222.97039 | 0.482956 | 5 | 29.240 |
| -2.00016 | -2.09567 | 3.47371 | 216.28336 | 0.138798 | 6 | 35.088 |
| 4.82460 | 1.87636 | 5.17663 | 21.25179 | 0.206782 | 7 | 40.936 |
| 2.67329 | 2.71985 | 3.81367 | 45.49461 | 0.152336 | 8 | 46.784 |
| -0.30242 | -0.07890 | 0.31255 | 194.62382 | 0.012485 | 9 | 52.632 |
| -0.01787 | -2.37239 | 2.50941 | 250.97850 | 0.100239 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 394 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 49.71010 | | | | | 0 | |
| 0.97878 | 14.13053 | 14.14238 | 87.65463 | 0.929935 | 1 | 5.848 |
| 1.09313 | 1.96077 | 2.24468 | 60.86814 | 0.147614 | 2 | 11.696 |
| 15.19859 | -0.53261 | 15.20792 | 357.99292 | 1.000000 | 3 | 17.544 |
| 0.17894 | -3.06585 | 3.07061 | 273.19141 | 0.201909 | 4 | 23.392 |
| -4.70605 | -5.04797 | 6.90137 | 227.00763 | 0.453881 | 5 | 29.240 |
| 1.92671 | 4.66852 | 5.05047 | 67.57390 | 0.332095 | 6 | 35.088 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/C.MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 52.05487 | | | | | 0 | |
| -3.82069 | -15.02778 | 15.50586 | 255.73520 | 1.000000 | 1 | 5.848 |
| 0.02641 | -0.55737 | 0.55800 | 272.71240 | 0.035986 | 2 | 11.696 |
| 12.01495 | -0.50473 | 12.02154 | 357.99449 | 0.775548 | 3 | 17.544 |
| 7.90094 | -1.83633 | 7.72245 | 346.24305 | 0.498034 | 4 | 23.392 |
| -5.39080 | -4.89761 | 7.28336 | 222.25552 | 0.469717 | 5 | 29.240 |
| -2.98320 | -1.81115 | 3.48995 | 211.26263 | 0.225073 | 6 | 35.088 |
| 3.05532 | 1.55708 | 3.42921 | 27.00462 | 0.221156 | 7 | 40.936 |
| 2.18363 | 1.71448 | 2.77627 | 38.13725 | 0.179046 | 8 | 46.784 |
| -0.11762 | -0.36249 | 0.38110 | 252.02373 | 0.024578 | 9 | 52.632 |
| -0.60218 | -1.28020 | 1.41475 | 244.80876 | 0.091240 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.75914 | | | | | 0 | |
| 1.87573 | 12.89450 | 12.99863 | 81.69795 | 1.000000 | 1 | 5.848 |
| -0.83339 | 1.29312 | 1.58494 | 123.62613 | 0.115848 | 2 | 11.696 |
| 9.84648 | 0.14029 | 9.84748 | 0.81629 | 0.758045 | 3 | 17.544 |
| 2.63272 | -0.70085 | 2.72441 | 345.09302 | 0.209721 | 4 | 23.392 |
| -4.94436 | -4.13293 | 6.44420 | 219.89186 | 0.496066 | 5 | 29.240 |
| -1.24770 | 1.06504 | 1.64046 | 139.51549 | 0.126280 | 6 | 35.088 |
| 4.67819 | 3.90837 | 6.08855 | 39.91075 | 0.468688 | 7 | 40.936 |
| 1.85740 | -0.58198 | 1.94644 | 342.60229 | 0.149834 | 8 | 46.784 |
| -1.75734 | -3.14048 | 3.59873 | 240.76965 | 0.277025 | 9 | 52.632 |
| -0.55055 | 0.09009 | 0.56577 | 170.83737 | 0.043552 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.89832 | | | | | 0 | |
| -0.29627 | -1.23811 | 1.26529 | 256.45891 | 1.000000 | 1 | 5.848 |
| -0.05488 | -0.09179 | 0.06244 | 236.04388 | 0.049351 | 2 | 11.696 |
| 0.96070 | -0.03955 | 0.96151 | 357.64258 | 0.759916 | 3 | 17.544 |
| 0.62698 | -0.13340 | 0.64102 | 347.98853 | 0.506618 | 4 | 23.392 |
| -0.44002 | -0.39040 | 0.59358 | 222.15814 | 0.469130 | 5 | 29.240 |
| -0.25510 | -0.19241 | 0.29716 | 210.85637 | 0.234859 | 6 | 35.088 |
| 0.25016 | 0.13056 | 0.28218 | 27.56157 | 0.223015 | 7 | 40.936 |
| 0.18312 | 0.14018 | 0.23062 | 37.43509 | 0.182264 | 8 | 46.784 |
| -0.00874 | -0.03183 | 0.03391 | 254.65199 | 0.026083 | 9 | 52.632 |
| -0.04981 | -0.10304 | 0.11445 | 244.20262 | 0.090452 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 354 TEST COND 5 COMP RUN 50.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.68590 | | | | | 0 | |
| 0.16770 | 1.08788 | 1.10073 | 81.23634 | 1.000000 | 1 | 5.848 |
| -0.08364 | 0.10166 | 0.13165 | 129.44542 | 0.119598 | 2 | 11.696 |
| 0.80967 | 0.01573 | 0.80982 | 1.11309 | 0.735718 | 3 | 17.544 |
| 0.23885 | -0.04628 | 0.24330 | 349.03467 | 0.221032 | 4 | 23.392 |
| -0.42407 | -0.34799 | 0.54857 | 219.37206 | 0.498373 | 5 | 29.240 |
| -0.12392 | 0.07142 | 0.14303 | 150.04572 | 0.129939 | 6 | 35.088 |
| 0.39704 | 0.34183 | 0.52459 | 40.66226 | 0.476589 | 7 | 40.936 |
| 0.16792 | -0.04286 | 0.17292 | 345.64966 | 0.157095 | 8 | 46.784 |
| -0.14415 | -0.27838 | 0.31349 | 242.62430 | 0.284804 | 9 | 52.632 |
| -0.05305 | 0.01457 | 0.05502 | 164.64508 | 0.049983 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.54899 | | | | | 0 | |
| -0.55892 | 0.69110 | 0.88882 | 128.96400 | 1.000000 | 1 | 5.848 |
| 0.37020 | -0.20841 | 0.42484 | 330.62183 | 0.477976 | 2 | 11.696 |
| -0.15906 | 0.30540 | 0.34433 | 117.51192 | 0.387404 | 3 | 17.544 |
| [illegible]0.06322 | 0.02639 | 0.06850 | 22.65990 | 0.077071 | 4 | 23.392 |
| -0.17172 | 0.02704 | 0.17384 | 171.05067 | 0.195584 | 5 | 29.240 |
| 0.08219 | 0.03318 | 0.08863 | 21.98315 | 0.099717 | 6 | 35.088 |
| -0.06062 | 0.05629 | 0.08272 | 137.12041 | 0.093065 | 7 | 40.936 |
| 0.03833 | -0.06361 | 0.07426 | 301.07397 | 0.083553 | 8 | 46.784 |
| -0.00084 | -0.03792 | 0.03793 | 268.73657 | 0.042672 | 9 | 52.632 |
| 0.02596 | -0.08491 | 0.08879 | 286.99854 | 0.099893 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -1.20499 | | | | | 0 | |
| 0.59261 | -1.14941 | 1.29319 | 297.27466 | 1.000000 | 1 | 5.848 |
| 0.08640 | -0.08590 | 0.12184 | 315.16504 | 0.094215 | 2 | 11.696 |
| -0.31308 | 0.16840 | 0.35549 | 151.72499 | 0.274895 | 3 | 17.544 |
| -0.04802 | 0.04012 | 0.06869 | 134.35156 | 0.053119 | 4 | 23.392 |
| 0.17372 | 0.15729 | 0.23635 | 42.15710 | 0.181216 | 5 | 29.240 |
| 0.04496 | -0.09864 | 0.10860 | 294.50171 | 0.083822 | 6 | 35.088 |
| -0.10033 | -0.09193 | 0.13600 | 222.49399 | 0.105226 | 7 | 40.936 |
| -0.04488 | -0.05801 | 0.06854 | 220.93747 | 0.060464 | 8 | 46.784 |
| -0.01000 | 0.09413 | 0.09466 | 96.06223 | 0.073201 | 9 | 52.632 |
| 0.04453 | 0.01488 | 0.04695 | 18.47119 | 0.036306 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.79972 | | | | | 0 | |
| -2.76916 | 3.37399 | 4.36486 | 129.37701 | 1.000000 | 1 | 5.848 |
| 1.85603 | -1.81653 | 2.11617 | 331.29077 | 0.484820 | 2 | 11.696 |
| -0.79570 | 1.48487 | 1.68368 | 118.18347 | 0.385736 | 3 | 17.544 |
| 0.29354 | 0.11931 | 0.31530 | 21.44921 | 0.072253 | 4 | 23.392 |
| -0.83565 | 0.11487 | 0.84351 | 172.17314 | 0.193251 | 5 | 29.240 |
| 0.38219 | 0.14721 | 0.40956 | 21.06502 | 0.093830 | 6 | 35.088 |
| -0.29357 | 0.26176 | 0.39332 | 138.27866 | 0.090112 | 7 | 40.936 |
| 0.17892 | -0.29798 | 0.34756 | 300.98218 | 0.079628 | 8 | 46.784 |
| -0.01247 | -0.17922 | 0.17965 | 266.01978 | 0.041159 | 9 | 52.632 |
| 0.11912 | -0.39959 | 0.41696 | 286.59912 | 0.095527 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -5.74265 | | | | | 0 | |
| 2.78931 | -5.31693 | 5.96561 | 296.96753 | 1.000000 | 1 | 5.848 |
| 0.40981 | -0.34878 | 0.53131 | 318.97046 | 0.089063 | 2 | 11.696 |
| -1.51499 | 1.89863 | 1.73746 | 150.68700 | 0.291246 | 3 | 17.544 |
| -0.23652 | 0.21386 | 0.33500 | 146.58592 | 0.056154 | 4 | 23.392 |
| 0.83160 | 0.76276 | 1.12848 | 42.52777 | 0.189194 | 5 | 29.240 |
| 0.20954 | -0.47323 | 0.51754 | 293.80201 | 0.086755 | 6 | 35.088 |
| -0.46530 | -0.42842 | 0.63290 | 222.63699 | 0.106084 | 7 | 40.936 |
| -0.32069 | -0.26884 | 0.41834 | 219.95282 | 0.070136 | 8 | 46.784 |
| -0.04422 | 0.44091 | 0.45129 | 95.87897 | 0.075648 | 9 | 52.632 |
| 0.20938 | 0.07177 | 0.21756 | 19.26321 | 0.036468 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.58415 | | | | | 0 | |
| -7.15699 | 8.50170 | 11.11312 | 130.09172 | 1.000000 | 1 | 5.848 |
| 4.89261 | -2.55729 | 5.32063 | 332.40454 | 0.496767 | 2 | 11.696 |
| -2.08446 | 3.70911 | 4.25568 | 119.35886 | 0.382942 | 3 | 17.544 |
| 0.67286 | 0.23057 | 0.71127 | 18.91525 | 0.064003 | 4 | 23.392 |
| -2.09374 | 0.21345 | 2.10459 | 174.17902 | 0.189379 | 5 | 29.240 |
| 0.87864 | 0.30550 | 0.93023 | 19.17239 | 0.083706 | 6 | 35.088 |
| -0.72933 | 0.60184 | 0.94559 | 140.47055 | 0.085088 | 7 | 40.936 |
| 0.41443 | -0.69521 | 0.80937 | 300.80029 | 0.072830 | 8 | 46.784 |
| -0.06858 | -0.42544 | 0.43093 | 260.84277 | 0.038776 | 9 | 52.632 |
| 0.26444 | -0.94069 | 0.97769 | 285.81396 | 0.087976 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -13.84969 | | | | | 0 | |
| 5.98446 | -12.89245 | 13.49226 | 296.33032 | 1.000000 | 1 | 5.848 |
| 0.91693 | -0.96605 | 1.07757 | 328.31152 | 0.079866 | 2 | 11.696 |
| -3.75796 | 2.26973 | 4.39019 | 148.86880 | 0.325386 | 3 | 17.544 |
| -0.75812 | 0.41837 | 0.86990 | 151.10776 | 0.064477 | 4 | 23.392 |
| 2.82229 | 1.89936 | 2.77439 | 43.20451 | 0.205628 | 5 | 29.240 |
| 0.46906 | -1.19561 | 1.25286 | 292.72339 | 0.092857 | 6 | 35.088 |
| -1.00384 | -0.99937 | 1.49279 | 222.92287 | 0.107676 | 7 | 40.936 |
| -0.78219 | -0.61232 | 0.99336 | 218.05492 | 0.073624 | 8 | 46.784 |
| -0.10503 | 1.08400 | 1.08908 | 95.53429 | 0.080719 | 9 | 52.632 |
| 0.46421 | 0.17710 | 0.49684 | 20.88275 | 0.036824 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 22.10301 | | | | | 0 | |
| -18.89444 | 20.60468 | 27.99625 | 132.52078 | 1.000000 | 1 | 5.848 |
| 13.33588 | -6.35973 | 14.77478 | 334.58391 | 0.528494 | 2 | 11.696 |
| -5.87065 | 8.74578 | 10.53343 | 123.87172 | 0.376783 | 3 | 17.544 |
| 1.14921 | -0.05449 | 1.15060 | 357.18604 | 0.041157 | 4 | 23.392 |
| -5.01013 | -0.07362 | 5.01067 | 180.84187 | 0.179232 | 5 | 29.240 |
| 1.38987 | 0.18508 | 1.40214 | 7.58519 | 0.050155 | 6 | 35.088 |
| -1.70253 | 0.97701 | 1.96295 | 150.15031 | 0.070215 | 7 | 40.936 |
| 0.69431 | -1.21243 | 1.39716 | 299.79810 | 0.049977 | 8 | 46.784 |
| -0.92475 | -0.79558 | 0.95305 | 236.59190 | 0.034091 | 9 | 52.632 |
| 0.37292 | -1.72243 | 1.76234 | 282.21695 | 0.063039 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -28.92458 | | | | | 0 | |
| 6.89744 | -18.33858 | 19.59280 | 290.61206 | 1.000000 | 1 | 5.848 |
| 1.46578 | 1.25182 | 1.92758 | 40.49825 | 0.098382 | 2 | 11.696 |
| -8.59481 | 6.59707 | 10.83413 | 142.48889 | 0.552965 | 3 | 17.544 |
| -2.80819 | -0.86214 | 2.80888 | 181.26768 | 0.143363 | 4 | 23.392 |
| 4.34788 | 4.37419 | 6.31088 | 44.45332 | 0.322102 | 5 | 29.240 |
| 0.77996 | -2.53621 | 2.65214 | 287.00317 | 0.135363 | 6 | 35.088 |
| -1.67324 | -1.99287 | 2.31019 | 223.59038 | 0.117910 | 7 | 40.936 |
| -1.67497 | -0.93868 | 1.92002 | 209.26488 | 0.097996 | 8 | 46.784 |
| -0.14685 | 2.23649 | 2.24131 | 93.75674 | 0.114394 | 9 | 52.632 |
| 0.69345 | 0.38285 | 0.74187 | 31.06830 | 0.037864 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 79
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.46921 | | | | | 0 | |
| -21.24123 | 20.15323 | 29.28040 | 136.50560 | 1.000000 | 1 | 5.848 |
| 16.22934 | -6.22569 | 17.38246 | 339.01270 | 0.593655 | 2 | 11.696 |
| -7.05089 | 8.09104 | 10.73219 | 131.07036 | 0.366532 | 3 | 17.544 |
| 0.12895 | -1.01248 | 1.02066 | 277.25006 | 0.034858 | 4 | 23.392 |
| -4.72969 | -1.21959 | 4.88440 | 194.45920 | 0.166815 | 5 | 29.240 |
| 0.05590 | -0.82306 | 0.82495 | 273.88501 | 0.028174 | 6 | 35.088 |
| -1.51377 | 0.07241 | 1.51590 | 177.26138 | 0.051758 | 7 | 40.936 |
| 0.12002 | -0.33200 | 0.35303 | 289.87451 | 0.012057 | 8 | 46.784 |
| -1.09862 | -0.37187 | 1.15985 | 198.70045 | 0.039612 | 9 | 52.632 |
| -0.14808 | -0.67027 | 0.68643 | 257.54199 | 0.023443 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 79
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -18.98415 | | | | | 0 | |
| -6.21982 | 2.05490 | 6.55048 | 161.71748 | 0.582121 | 1 | 5.848 |
| 0.01711 | 6.01433 | 6.01436 | 89.83698 | 0.534477 | 2 | 11.696 |
| -7.48843 | 8.39932 | 11.25278 | 131.71869 | 1.000000 | 3 | 17.544 |
| -4.40738 | -1.98413 | 4.80111 | 203.36591 | 0.426660 | 4 | 23.392 |
| 3.15332 | 4.18396 | 5.23917 | 52.99579 | 0.465589 | 5 | 29.240 |
| 0.07450 | -1.93206 | 1.93349 | 272.20001 | 0.171823 | 6 | 35.088 |
| 0.02494 | -0.15982 | 0.16175 | 278.86907 | 0.014375 | 7 | 40.936 |
| -1.24067 | 0.07243 | 1.24278 | 176.65865 | 0.110442 | 8 | 46.784 |
| 0.03590 | 1.46699 | 1.46743 | 88.59031 | 0.130406 | 9 | 52.632 |
| -0.20972 | 0.31180 | 0.37577 | 123.92546 | 0.033394 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 47.38120 | | | | | 0 | |
| -25.94527 | 22.78784 | 34.23224 | 138.26273 | 1.000000 | 1 | 5.848 |
| 24.69250 | -3.87972 | 24.99562 | 351.07056 | 0.730172 | 2 | 11.696 |
| -7.36871 | 7.67606 | 10.64048 | 133.82971 | 0.310832 | 3 | 17.544 |
| -1.66036 | 0.37383 | 1.89755 | 168.63812 | 0.055432 | 4 | 23.392 |
| -4.42403 | -3.32521 | 5.53435 | 216.92098 | 0.161671 | 5 | 29.240 |
| -0.63163 | -1.62056 | 1.73931 | 248.78607 | 0.050809 | 6 | 35.088 |
| -1.41989 | -0.70361 | 1.58467 | 206.36024 | 0.046292 | 7 | 40.936 |
| -0.33496 | 0.28679 | 0.44096 | 139.43047 | 0.012881 | 8 | 46.784 |
| -0.92502 | -0.27457 | 0.96492 | 196.53238 | 0.028187 | 9 | 52.632 |
| -0.91429 | 0.18847 | 0.93361 | 168.35342 | 0.027273 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -4.94968 | | | | | 0 | |
| -9.40915 | 19.96388 | 22.07887 | 115.23495 | 1.000000 | 1 | 5.848 |
| -1.79222 | 11.09237 | 11.23623 | 99.17812 | 0.509116 | 2 | 11.696 |
| -7.48074 | 10.42551 | 12.83171 | 125.66106 | 0.581408 | 3 | 17.544 |
| -5.49110 | -2.45566 | 6.01918 | 204.89048 | 0.272549 | 4 | 23.392 |
| 1.71521 | 2.24033 | 2.82153 | 52.56209 | 0.127844 | 5 | 29.240 |
| -1.08090 | -0.88523 | 0.88968 | 204.26489 | 0.040312 | 6 | 35.088 |
| 1.71332 | 0.47702 | 1.77848 | 15.95822 | 0.080584 | 7 | 40.936 |
| -1.15992 | 0.83173 | 1.42730 | 144.35732 | 0.064671 | 8 | 46.784 |
| 0.20349 | 0.97332 | 0.99436 | 78.19122 | 0.045065 | 9 | 52.632 |
| -0.44460 | 0.69413 | 0.75010 | 126.39065 | 0.033987 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 56.24570 | | | | | 0 | |
| -20.34135 | 18.32304 | 27.37708 | 137.98819 | 0.965317 | 1 | 5.848 |
| 28.27945 | 2.14568 | 28.36072 | 4.33895 | 1.000000 | 2 | 11.696 |
| -3.45319 | 4.76541 | 5.88503 | 125.92847 | 0.207507 | 3 | 17.544 |
| -3.89484 | 3.45568 | 5.20687 | 138.41904 | 0.183594 | 4 | 23.392 |
| -2.32137 | -4.60452 | 5.15659 | 243.24498 | 0.181821 | 5 | 29.240 |
| -0.28022 | -1.47155 | 1.49799 | 259.21826 | 0.052819 | 6 | 35.088 |
| -0.68287 | -0.96551 | 1.19734 | 235.22688 | 0.042218 | 7 | 40.936 |
| -0.43859 | 0.44670 | 0.62602 | 134.47557 | 0.022073 | 8 | 46.784 |
| 0.33777 | -0.42811 | 0.54532 | 308.27246 | 0.019228 | 9 | 52.632 |
| -1.36029 | 0.62034 | 1.49506 | 155.48543 | 0.052716 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 14.39225 | | | | | 0 | |
| 2.53129 | 24.48918 | 24.61964 | 84.09863 | 1.000000 | 1 | 5.848 |
| -2.87687 | 11.06347 | 11.43139 | 104.57610 | 0.464320 | 2 | 11.696 |
| -5.58498 | 9.04194 | 9.79104 | 124.77931 | 0.397693 | 3 | 17.544 |
| -3.37115 | -0.57253 | 3.41942 | 189.63863 | 0.138890 | 4 | 23.392 |
| -0.62315 | -2.27294 | 2.35682 | 254.66832 | 0.095729 | 5 | 29.240 |
| 0.36149 | 0.81805 | 0.89436 | 66.15944 | 0.036327 | 6 | 35.088 |
| 2.38506 | -0.10148 | 2.38722 | 357.56348 | 0.096964 | 7 | 40.936 |
| -0.90748 | 0.93540 | 1.30327 | 134.13210 | 0.052936 | 8 | 46.784 |
| 0.12344 | 0.36788 | 0.38804 | 71.45038 | 0.015761 | 9 | 52.632 |
| 0.25987 | 0.92523 | 0.96103 | 74.31174 | 0.039035 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.64954 | | | | | 0 | |
| -12.74469 | 11.44824 | 17.13301 | 138.07190 | 0.685212 | 1 | 5.848 |
| 24.59804 | 4.48708 | 25.00394 | 10.33800 | 1.000000 | 2 | 11.696 |
| -0.47645 | 3.08674 | 3.12132 | 98.78026 | 0.124833 | 3 | 17.544 |
| -4.00233 | 3.45005 | 5.28408 | 139.23828 | 0.211330 | 4 | 23.392 |
| -0.92206 | -3.81052 | 3.92049 | 256.39697 | 0.156795 | 5 | 29.240 |
| 0.03660 | -1.10474 | 1.10535 | 271.89722 | 0.044207 | 6 | 35.088 |
| 0.06241 | -0.89332 | 0.89549 | 273.99634 | 0.035814 | 7 | 40.936 |
| -0.30836 | 0.39301 | 0.49954 | 128.11874 | 0.019979 | 8 | 46.784 |
| 0.77752 | -0.44617 | 0.89644 | 330.15137 | 0.035852 | 9 | 52.632 |
| -1.06995 | 0.55942 | 1.20737 | 152.39742 | 0.048287 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.68430 | | | | | 0 | |
| 8.84209 | 19.67787 | 21.57315 | 65.88956 | 1.000000 | 1 | 5.848 |
| -2.44727 | 8.09730 | 8.42076 | 106.89529 | 0.390335 | 2 | 11.696 |
| -3.68177 | 5.00903 | 6.21657 | 126.31691 | 0.288162 | 3 | 17.544 |
| -1.17536 | 0.90124 | 1.27796 | 156.90735 | 0.059238 | 4 | 23.392 |
| -1.67288 | -4.23138 | 4.54977 | 248.43794 | 0.210900 | 5 | 29.240 |
| 0.51500 | 1.30865 | 1.40634 | 68.51875 | 0.065189 | 6 | 35.088 |
| 1.93937 | -0.59422 | 2.02855 | 342.96655 | 0.094031 | 7 | 40.936 |
| -0.50282 | 0.80969 | 0.94802 | 122.03186 | 0.043945 | 8 | 46.784 |
| -0.19913 | -0.04079 | 0.16428 | 194.37679 | 0.007615 | 9 | 52.632 |
| 0.71505 | 0.76723 | 1.04741 | 47.05598 | 0.048557 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 63.26399 | | | | | 0 | |
| -12.61607 | 10.45641 | 16.38602 | 140.34749 | 0.546196 | 1 | 5.848 |
| 29.55653 | 5.14079 | 30.00026 | 9.86678 | 1.000000 | 2 | 11.696 |
| 0.43193 | 5.34950 | 5.36690 | 85.38374 | 0.178895 | 3 | 17.544 |
| -4.69698 | 1.25165 | 4.86088 | 165.07855 | 0.162028 | 4 | 23.392 |
| -0.91683 | -2.69120 | 2.84308 | 251.18716 | 0.094768 | 5 | 29.240 |
| -0.10334 | -1.38822 | 1.39206 | 265.74243 | 0.046402 | 6 | 35.088 |
| 0.98118 | -1.32258 | 1.64479 | 306.57056 | 0.054855 | 7 | 40.936 |
| -0.22434 | 0.63859 | 0.67885 | 109.35629 | 0.022581 | 8 | 46.784 |
| 0.42129 | -0.47663 | 0.63613 | 311.47339 | 0.021204 | 9 | 52.632 |
| -0.57068 | 0.41306 | 0.70464 | 144.11282 | 0.023488 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 23.68906 | | | | | 0 | |
| 10.58958 | 21.74350 | 24.18332 | 64.04132 | 1.000000 | 1 | 5.848 |
| -2.20337 | 7.91235 | 8.21341 | 105.58111 | 0.339831 | 2 | 11.696 |
| -4.28252 | 5.41549 | 6.90416 | 128.33669 | 0.285493 | 3 | 17.544 |
| -0.05750 | 0.48480 | 0.48806 | 98.68528 | 0.016907 | 4 | 23.392 |
| -2.78813 | -5.81677 | 6.41629 | 245.03459 | 0.265319 | 5 | 29.240 |
| 0.31251 | 1.16426 | 1.20847 | 74.97304 | 0.049847 | 6 | 35.088 |
| 1.78737 | -1.28001 | 2.19843 | 324.39185 | 0.090907 | 7 | 40.936 |
| -0.04179 | 1.36203 | 1.36267 | 91.75739 | 0.056368 | 8 | 46.784 |
| -0.94681 | -0.39334 | 1.02526 | 202.55972 | 0.042395 | 9 | 52.632 |
| 1.16443 | 0.35498 | 1.21925 | 16.92670 | 0.050417 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 170.38020 | | | | | 0 | |
| -25.50807 | 16.21837 | 30.22833 | 147.55447 | 0.401780 | 1 | 5.848 |
| 74.91379 | 6.90304 | 75.23112 | 5.26473 | 1.000000 | 2 | 11.696 |
| 1.71023 | 22.72400 | 22.78825 | 85.69591 | 0.302910 | 3 | 17.544 |
| -10.04453 | -10.53046 | 14.55277 | 226.39292 | 0.193441 | 4 | 23.392 |
| -3.94347 | 0.12252 | 3.94537 | 178.22046 | 0.052442 | 5 | 29.240 |
| -1.16281 | -4.40896 | 4.54479 | 255.95679 | 0.060411 | 6 | 35.088 |
| 5.35002 | -3.96975 | 6.66195 | 323.42432 | 0.088553 | 7 | 40.936 |
| 0.00834 | 2.10098 | 2.10098 | 89.82713 | 0.027927 | 8 | 46.784 |
| -1.93196 | -0.87398 | 2.12045 | 204.34108 | 0.028184 | 9 | 52.632 |
| 1.40824 | -0.00970 | 1.40827 | 359.60522 | 0.018719 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 48.22493 | | | | | 0 | |
| 19.19135 | 47.54929 | 49.70488 | 72.32573 | 1.000000 | 1 | 5.848 |
| -1.79944 | 14.72106 | 14.83063 | 96.96907 | 0.297178 | 2 | 11.696 |
| -12.03886 | 13.72042 | 18.29331 | 131.26508 | 0.368782 | 3 | 17.544 |
| 2.89107 | -1.75005 | 3.37949 | 328.61226 | 0.067719 | 4 | 23.392 |
| -7.34168 | -14.24169 | 16.02246 | 242.72856 | 0.321864 | 5 | 29.240 |
| -0.53853 | 0.15106 | 0.55932 | 164.33127 | 0.011208 | 6 | 35.088 |
| 2.18504 | -4.33872 | 4.85787 | 296.73047 | 0.097342 | 7 | 40.936 |
| 1.68984 | 4.77191 | 5.06190 | 70.49825 | 0.101431 | 8 | 46.784 |
| -5.01079 | -1.96038 | 5.38062 | 201.36697 | 0.107818 | 9 | 52.632 |
| 3.49592 | -1.28344 | 3.68617 | 339.62402 | 0.073864 | 10 | 58.480 |

TEXT NOT REPRODUCIBLE



HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 130.52576 | | | | | 0 | |
| -9.69983 | -8.66780 | 9.68289 | 183.95464 | 0.168952 | 1 | 5.848 |
| 57.29144 | 1.91873 | 57.31155 | 1.91849 | 1.000000 | 2 | 11.696 |
| 3.10956 | 21.27675 | 21.50276 | 81.68512 | 0.375191 | 3 | 17.544 |
| -8.88936 | -12.96860 | 14.26431 | 245.13907 | 0.249240 | 4 | 23.392 |
| -5.39869 | -1.81393 | 5.54328 | 193.69818 | 0.096815 | 5 | 29.240 |
| 8.69779 | -4.28499 | 4.28611 | 271.36737 | 0.074786 | 6 | 35.088 |
| 4.73527 | -1.63986 | 5.01118 | 340.84844 | 0.087438 | 7 | 40.936 |
| 0.58924 | 0.28875 | 0.58158 | 28.66884 | 0.010144 | 8 | 46.784 |
| -1.98370 | -0.77953 | 2.09712 | 202.20828 | 0.036594 | 9 | 52.632 |
| 1.53769 | 0.37133 | 1.58189 | 13.57688 | 0.027602 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 67.37271 | | | | | 0 | |
| 7.26579 | 25.24865 | 26.26171 | 74.06184 | 1.000000 | 1 | 5.848 |
| 2.07742 | 8.49788 | 8.74788 | 76.26129 | 0.331018 | 2 | 11.696 |
| -9.67712 | 8.92220 | 12.69488 | 138.63883 | 0.489149 | 3 | 17.544 |
| 3.88236 | -2.28885 | 3.88877 | 323.41389 | 0.148419 | 4 | 23.392 |
| -3.28886 | -10.82884 | 11.88885 | 253.88882 | 0.417421 | 5 | 29.240 |
| 0.17488 | -0.13739 | 0.22248 | 321.84497 | 0.008486 | 6 | 35.088 |
| -0.10181 | -1.52847 | 1.52886 | 268.97510 | 0.058085 | 7 | 40.936 |
| 0.27582 | 2.15283 | 2.47841 | 68.34367 | 0.093840 | 8 | 46.784 |
| -3.88848 | -1.49844 | 3.87884 | 202.64438 | 0.147144 | 9 | 52.632 |
| 2.42413 | -0.88838 | 2.42864 | 357.96118 | 0.092815 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 142.21251 | | | | | 0 | |
| 10.86484 | -24.02867 | 26.37851 | 294.32910 | 1.000000 | 1 | 5.848 |
| 60.34489 | -8.87844 | 60.57323 | 350.17898 | 1.000000 | 2 | 11.696 |
| 7.44198 | 21.46294 | 22.71648 | 70.87686 | 0.375025 | 3 | 17.544 |
| -4.24937 | -11.13858 | 11.91418 | 249.18836 | 0.196698 | 4 | 23.392 |
| -9.98788 | -11.71762 | 15.84448 | 229.78893 | 0.253321 | 5 | 29.240 |
| 3.88889 | -6.37441 | 7.87977 | 298.79321 | 0.116879 | 6 | 35.088 |
| 3.89881 | 2.88829 | 4.46712 | 27.84175 | 0.073747 | 7 | 40.936 |
| 1.81872 | -2.47828 | 2.67756 | 292.36238 | 0.044204 | 8 | 46.784 |
| -0.15326 | -1.44131 | 1.44982 | 264.81278 | 0.023257 | 9 | 52.632 |
| -0.88436 | 1.76764 | 1.76764 | 98.14122 | 0.029182 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 140.68138 | | | | | 0 | |
| 11.95347 | 8.51990 | 14.67984 | 35.47955 | 1.000000 | 1 | 5.848 |
| 6.38122 | 7.78617 | 10.14194 | 50.13184 | 0.690913 | 2 | 11.696 |
| -9.08136 | 3.13793 | 9.59917 | 160.72999 | 0.653937 | 3 | 17.544 |
| 3.88956 | -2.48849 | 3.89192 | 321.29321 | 0.262362 | 4 | 23.392 |
| 2.51527 | -11.87782 | 12.14122 | 281.98838 | 0.827113 | 5 | 29.240 |
| 3.49571 | 1.23894 | 3.68159 | 19.88817 | 0.248762 | 6 | 35.088 |
| -1.62186 | 3.89121 | 3.49938 | 117.98882 | 0.238395 | 7 | 40.936 |
| -0.88887 | -2.17832 | 2.32998 | 249.33623 | 0.158656 | 8 | 46.784 |
| -0.88812 | -1.29888 | 1.52467 | 238.13818 | 0.103881 | 9 | 52.632 |
| 2.18982 | 3.18815 | 3.82137 | 58.48888 | 0.260329 | 10 | 58.488 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 125.98474 | | | | | 0 | |
| 21.79230 | -25.52528 | 33.53658 | 310.43701 | 0.776102 | 1 | 5.848 |
| 43.15135 | -2.28017 | 43.21155 | 356.97510 | 1.000000 | 2 | 11.696 |
| 5.57698 | 12.24858 | 13.45847 | 65.51942 | 0.311495 | 3 | 17.544 |
| -2.26454 | -5.75274 | 6.18314 | 248.49586 | 0.143090 | 4 | 23.392 |
| -0.87515 | -10.37499 | 14.11821 | 227.20584 | 0.326723 | 5 | 29.240 |
| 2.29475 | -6.90268 | 7.27612 | 288.38098 | 0.168337 | 6 | 35.088 |
| 2.93172 | 1.95926 | 3.94288 | 33.57521 | 0.091287 | 7 | 40.936 |
| 0.18463 | 0.72184 | 0.74510 | 75.68388 | 0.017243 | 8 | 46.784 |
| -0.66693 | -1.31926 | 1.49217 | 248.29488 | 0.033606 | 9 | 52.632 |
| 0.17091 | -0.62291 | 0.64654 | 285.35101 | 0.014959 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 48.26930 | | | | | 0 | |
| 13.26446 | 2.99084 | 13.59857 | 12.57690 | 1.000000 | 1 | 5.848 |
| 4.57666 | 6.38468 | 7.79869 | 54.82353 | 0.573242 | 2 | 11.696 |
| -3.34492 | -1.14330 | 3.53491 | 198.87857 | 0.260100 | 3 | 17.544 |
| 3.14916 | -4.11359 | 5.10862 | 307.49579 | 0.381193 | 4 | 23.392 |
| 2.92682 | -10.36123 | 10.76868 | 285.77360 | 0.792217 | 5 | 29.240 |
| 4.80165 | -2.28109 | 5.28208 | 335.37329 | 0.388858 | 6 | 35.088 |
| 0.60779 | 0.90834 | 1.06839 | 67.91706 | 0.078665 | 7 | 40.936 |
| -1.96813 | -0.94884 | 2.18614 | 206.28817 | 0.160857 | 8 | 46.784 |
| -0.53215 | -3.01999 | 3.06801 | 260.08695 | 0.225835 | 9 | 52.632 |
| 3.23699 | -0.74416 | 3.32143 | 347.09298 | 0.244392 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 130.08381 | | | | | 0 | |
| 27.63469 | -36.83071 | 46.04137 | 306.86646 | 1.000000 | 1 | 5.848 |
| 41.88842 | -3.58136 | 42.03325 | 355.11230 | 0.912549 | 2 | 11.696 |
| 4.42632 | 8.88527 | 9.92496 | 63.91398 | 0.215473 | 3 | 17.544 |
| 0.69336 | -7.15469 | 7.18761 | 275.53564 | 0.156044 | 4 | 23.392 |
| -0.52680 | -11.32206 | 14.79693 | 229.92146 | 0.321244 | 5 | 29.240 |
| 0.75184 | -9.10821 | 9.19832 | 274.68311 | 0.199710 | 6 | 35.088 |
| 3.88543 | 0.89280 | 3.88654 | 1.33488 | 0.084641 | 7 | 40.936 |
| 1.47868 | 2.71948 | 3.89198 | 61.42999 | 0.084527 | 8 | 46.784 |
| -1.48588 | -0.46934 | 1.55741 | 197.53937 | 0.033812 | 9 | 52.632 |
| -0.66546 | -2.89557 | 2.93288 | 256.88184 | 0.063654 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 64.03862 | | | | | 0 | |
| 37.58611 | 21.00784 | 43.05861 | 29.20193 | 1.000000 | 1 | 5.848 |
| 12.09940 | 10.89225 | 16.22345 | 41.98484 | 0.376776 | 2 | 11.696 |
| -9.02853 | -3.92388 | 6.13909 | 215.81972 | 0.142994 | 3 | 17.544 |
| 3.99718 | -8.63198 | 9.38620 | 292.39688 | 0.218025 | 4 | 23.392 |
| 2.88559 | -13.31818 | 13.62711 | 282.22485 | 0.316478 | 5 | 29.240 |
| 5.42885 | -7.38581 | 9.16862 | 305.27832 | 0.212752 | 6 | 35.088 |
| 4.26967 | -1.47159 | 4.51615 | 340.98291 | 0.104884 | 7 | 40.936 |
| -0.58278 | 1.14341 | 1.24907 | 113.73587 | 0.029009 | 8 | 46.784 |
| -2.56621 | -2.66536 | 3.84652 | 220.15234 | 0.089332 | 9 | 52.632 |
| 1.34071 | -3.63935 | 3.87559 | 290.36499 | 0.090007 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 68.04822 | | | | | 0 | |
| 14.17858 | -22.10284 | 26.25961 | 302.67944 | 1.000000 | 1 | 5.848 |
| 19.08043 | -2.08381 | 19.19386 | 353.76733 | 0.730927 | 2 | 11.696 |
| 1.72039 | 3.11582 | 3.55923 | 61.09483 | 0.135540 | 3 | 17.544 |
| 1.63596 | -4.21999 | 4.52600 | 291.13970 | 0.172356 | 4 | 23.392 |
| -4.20711 | -5.93285 | 7.27313 | 234.65872 | 0.276970 | 5 | 29.240 |
| -0.20936 | -4.99699 | 5.00137 | 267.60083 | 0.190458 | 6 | 35.088 |
| 2.08657 | -0.69019 | 2.19775 | 341.69702 | 0.083693 | 7 | 40.936 |
| 1.40378 | 1.58250 | 2.11539 | 48.42493 | 0.080557 | 8 | 46.784 |
| -0.90044 | 0.18225 | 0.91870 | 168.55800 | 0.034985 | 9 | 52.632 |
| -0.81633 | -1.93807 | 2.10297 | 247.15872 | 0.080084 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.31943 | | | | | 0 | |
| 28.88113 | 17.69174 | 33.10954 | 32.21184 | 1.000000 | 1 | 5.848 |
| 9.28366 | 6.97278 | 11.61066 | 36.90953 | 0.349827 | 2 | 11.696 |
| -3.62612 | -2.42140 | 4.36027 | 213.73366 | 0.131375 | 3 | 17.544 |
| 1.65091 | -5.66015 | 5.89599 | 286.26050 | 0.177646 | 4 | 23.392 |
| 1.43822 | -7.29001 | 7.43053 | 281.16040 | 0.223881 | 5 | 29.240 |
| 2.57041 | -5.18118 | 5.78382 | 296.38794 | 0.174266 | 6 | 35.088 |
| 3.48474 | -1.34454 | 3.66061 | 338.65068 | 0.110294 | 7 | 40.936 |
| 0.56098 | 1.15448 | 1.28356 | 64.08405 | 0.038674 | 8 | 46.784 |
| -1.97379 | -0.87619 | 2.15952 | 203.93707 | 0.065066 | 9 | 52.632 |
| -0.56464 | -2.29328 | 2.36176 | 256.16797 | 0.071169 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.39454 | | | | | 0 | |
| 1.13897 | -1.79730 | 2.12353 | 302.18066 | 1.000000 | 1 | 5.848 |
| 1.49145 | -0.16902 | 1.50100 | 353.53442 | 0.706843 | 2 | 11.696 |
| 0.13843 | 0.25082 | 0.26912 | 60.53065 | 0.126751 | 3 | 17.544 |
| 0.14988 | -0.34203 | 0.37153 | 292.98560 | 0.174958 | 4 | 23.392 |
| -0.32746 | -0.47361 | 0.57580 | 235.33926 | 0.271151 | 5 | 29.240 |
| -0.02370 | -0.40170 | 0.40240 | 266.62280 | 0.189498 | 6 | 35.088 |
| 0.16779 | -0.06360 | 0.17944 | 339.24194 | 0.084501 | 7 | 40.936 |
| 0.11905 | 0.12896 | 0.17551 | 47.20773 | 0.082652 | 8 | 46.784 |
| -0.07354 | 0.01936 | 0.07605 | 165.24825 | 0.035813 | 9 | 52.632 |
| -0.07032 | -0.16031 | 0.17506 | 246.21577 | 0.082438 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 306 TEST COND 8 COMP RUN 48.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.19098 | | | | | 0 | |
| 2.33820 | 1.48882 | 2.77196 | 32.48640 | 1.000000 | 1 | 5.848 |
| 0.77463 | 0.57164 | 0.96272 | 36.42572 | 0.347307 | 2 | 11.696 |
| -0.30012 | -0.20032 | 0.36083 | 213.72215 | 0.130173 | 3 | 17.544 |
| 0.12971 | -0.46547 | 0.48320 | 285.57194 | 0.174319 | 4 | 23.392 |
| 0.11392 | -0.58613 | 0.59709 | 280.99878 | 0.215405 | 5 | 29.240 |
| 0.20160 | -0.42944 | 0.47483 | 295.29684 | 0.171298 | 6 | 35.088 |
| 0.28556 | -0.11445 | 0.30764 | 338.15918 | 0.110983 | 7 | 40.936 |
| 0.09393 | 0.09890 | 0.11264 | 61.39738 | 0.040637 | 8 | 46.784 |
| -0.16493 | -0.06344 | 0.17671 | 201.03873 | 0.063749 | 9 | 52.632 |
| -0.09981 | -0.18849 | 0.19751 | 252.61714 | 0.071253 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.45492 | | | | | 0 | |
| -0.41601 | 0.54882 | 0.68867 | 127.16280 | 1.000000 | 1 | 5.882 |
| 0.16511 | -0.03039 | 0.16788 | 349.57007 | 0.243780 | 2 | 11.765 |
| -0.11430 | 0.21017 | 0.23924 | 118.53984 | 0.347398 | 3 | 17.647 |
| -0.03914 | 0.05063 | 0.06400 | 127.70952 | 0.092924 | 4 | 23.529 |
| 0.02043 | 0.03494 | 0.04047 | 59.68217 | 0.058773 | 5 | 29.412 |
| -0.07631 | 0.06191 | 0.09801 | 141.13019 | 0.142321 | 6 | 35.294 |
| 0.02227 | -0.05018 | 0.05490 | 293.93481 | 0.079720 | 7 | 41.176 |
| 0.06777 | 0.04293 | 0.07972 | 32.58545 | 0.115754 | 8 | 47.059 |
| -0.04478 | 0.08788 | 0.09859 | 116.99842 | 0.143165 | 9 | 52.941 |
| -0.08493 | -0.02489 | 0.08850 | 196.33597 | 0.128587 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -2.10802 | | | | | 0 | |
| 0.16300 | 0.19301 | 0.25263 | 49.81978 | 0.741738 | 1 | 5.882 |
| 0.20380 | -0.27289 | 0.34059 | 306.79220 | 1.000000 | 2 | 11.765 |
| -0.14144 | 0.12486 | 0.18867 | 138.56416 | 0.553938 | 3 | 17.647 |
| -0.13263 | -0.18878 | 0.23071 | 234.90950 | 0.677370 | 4 | 23.529 |
| -0.07623 | 0.13857 | 0.15816 | 118.81972 | 0.464388 | 5 | 29.412 |
| -0.12785 | 0.09178 | 0.13794 | 157.95201 | 0.404988 | 6 | 35.294 |
| -0.11068 | -0.05430 | 0.12328 | 206.15485 | 0.361956 | 7 | 41.176 |
| 0.07142 | 0.04634 | 0.08513 | 32.97728 | 0.249949 | 8 | 47.059 |
| -0.07706 | -0.00130 | 0.07707 | 180.96982 | 0.226289 | 9 | 52.941 |
| 0.04370 | -0.02351 | 0.04962 | 331.71582 | 0.145696 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.33603 | | | | | 0 | |
| -2.08461 | 2.79994 | 3.49874 | 127.08410 | 1.000000 | 1 | 5.882 |
| 0.84913 | -0.15269 | 0.86279 | 349.88591 | 0.246640 | 2 | 11.765 |
| -0.55957 | 1.00716 | 1.15217 | 119.05626 | 0.333118 | 3 | 17.647 |
| -0.15987 | 0.24214 | 0.28797 | 122.77014 | 0.083259 | 4 | 23.529 |
| 0.08666 | 0.14311 | 0.16730 | 58.80164 | 0.048371 | 5 | 29.412 |
| -0.34971 | 0.28662 | 0.45214 | 140.66144 | 0.130729 | 6 | 35.294 |
| 0.07796 | -0.23335 | 0.24600 | 288.49142 | 0.071124 | 7 | 41.176 |
| 0.32089 | 0.18814 | 0.37202 | 30.39667 | 0.107560 | 8 | 47.059 |
| -0.20626 | 0.41738 | 0.46556 | 116.29779 | 0.134604 | 9 | 52.941 |
| -0.40351 | -0.11373 | 0.41923 | 195.74004 | 0.121209 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.83436 | | | | | 0 | |
| 0.79897 | 0.73560 | 1.08016 | 42.91265 | 0.696629 | 1 | 5.882 |
| 0.98897 | -1.20001 | 1.55502 | 309.49316 | 1.000000 | 2 | 11.765 |
| -0.68170 | 0.57301 | 0.89041 | 139.65677 | 0.575179 | 3 | 17.647 |
| -0.63003 | -0.86655 | 1.07410 | 233.63643 | 0.692016 | 4 | 23.529 |
| -0.39174 | 0.65712 | 0.76503 | 120.80126 | 0.491974 | 5 | 29.412 |
| -0.59750 | 0.24403 | 0.64564 | 157.73457 | 0.415196 | 6 | 35.294 |
| -0.52446 | -0.25340 | 0.58247 | 205.78784 | 0.374573 | 7 | 41.176 |
| 0.39039 | 0.28481 | 0.39640 | 31.11006 | 0.254915 | 8 | 47.059 |
| -0.35085 | -0.01024 | 0.35119 | 181.63881 | 0.230948 | 9 | 52.941 |
| 0.19148 | -0.11989 | 0.23274 | 326.99414 | 0.149669 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.47647 | | | | | 0 | |
| -9.49025 | 7.31133 | 9.14322 | 126.[illegible]376 | 1.000000 | 1 | 5.882 |
| 2.33048 | -0.40386 | 2.36513 | 350.16821 | 0.258676 | 2 | 11.765 |
| -1.41684 | 2.45417 | 2.83379 | 119.99872 | 0.309934 | 3 | 17.647 |
| -0.23669 | 0.58790 | 0.63376 | 111.92969 | 0.069314 | 4 | 23.529 |
| 0.10839 | -.23892 | 0.28776 | 56.12640 | 0.031473 | 5 | 29.412 |
| -0.78881 | 0.66175 | 1.02290 | 139.68925 | 0.111876 | 6 | 35.294 |
| 0.05938 | -0.53149 | 0.53976 | 276.31592 | 0.059034 | 7 | 41.176 |
| 0.77743 | 0.37972 | 0.86520 | 26.03242 | 0.094628 | 8 | 47.059 |
| -0.46677 | 1.00810 | 1.10347 | 115.01967 | 0.120709 | 9 | 52.941 |
| -0.96759 | -0.25204 | 0.99987 | 194.60004 | 0.109357 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -29.78639 | | | | | 0 | |
| 1.97193 | 0.93880 | 2.18365 | 25.43932 | 0.629809 | 1 | 5.882 |
| 2.44859 | -2.43765 | 3.44717 | 315.32642 | 1.000000 | 2 | 11.765 |
| -1.67869 | 1.32364 | 2.13777 | 141.74385 | 0.616576 | 3 | 17.647 |
| -1.56881 | -1.93068 | 2.48281 | 231.08759 | 0.719477 | 4 | 23.529 |
| -1.07388 | 1.56086 | 1.90802 | 124.37450 | 0.548500 | 5 | 29.412 |
| -1.38769 | 0.58829 | 1.50898 | 157.38821 | 0.433763 | 6 | 35.294 |
| -1.25123 | -0.98678 | 1.59196 | 285.12186 | 0.390583 | 7 | 41.176 |
| 0.81414 | 0.42128 | 0.91664 | 27.39486 | 0.264379 | 8 | 47.059 |
| -0.82177 | -0.04382 | 0.82289 | 182.99687 | 0.237339 | 9 | 52.941 |
| 0.44127 | -0.32471 | 0.54787 | 323.69218 | 0.158017 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 99.00071 | | | | | 0 | |
| -15.43749 | 20.69504 | 25.84083 | 126.81001 | 1.000000 | 1 | 5.882 |
| 7.09367 | -1.18188 | 7.17843 | 350.94346 | 0.278291 | 2 | 11.765 |
| -3.60000 | 5.19647 | 6.32867 | 124.77007 | 0.244759 | 3 | 17.647 |
| 0.77252 | 1.32782 | 1.53649 | 59.80911 | 0.059431 | 4 | 23.529 |
| -0.14157 | -0.49886 | 0.47256 | 252.96729 | 0.018282 | 5 | 29.412 |
| -1.00886 | 1.11307 | 1.49694 | 131.96731 | 0.057897 | 6 | 35.294 |
| -1.00980 | -0.83703 | 1.35832 | 216.87335 | 0.052549 | 7 | 41.176 |
| 1.00199 | 0.04869 | 1.00273 | 1.74072 | 0.038805 | 8 | 47.059 |
| -0.67887 | 1.98889 | 2.09889 | 108.69488 | 0.080871 | 9 | 52.941 |
| -1.95865 | -0.29929 | 1.98788 | 187.57834 | 0.076128 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -99.10889 | | | | | 0 | |
| 6.63845 | -6.39865 | 7.79235 | 304.99863 | 1.000000 | 1 | 5.882 |
| 5.89886 | -0.73895 | 5.94195 | 353.11795 | 0.762535 | 2 | 11.765 |
| -3.62898 | 1.99128 | 4.12284 | 151.98840 | 0.529062 | 3 | 17.647 |
| -3.49841 | -2.98238 | 4.27627 | 216.12714 | 0.[illegible]9035 | 4 | 23.529 |
| -3.39213 | 3.17886 | 4.64851 | 136.86334 | 0.5 8547 | 5 | 29.412 |
| -2.36895 | 1.11886 | 2.61169 | 154.84239 | 0.335161 | 6 | 35.294 |
| -2.64169 | -0.98868 | 2.62159 | 201.34937 | 0.336431 | 7 | 41.176 |
| 1.68866 | 0.17895 | 1.61886 | 6.13594 | 0.207648 | 8 | 47.059 |
| -1.27681 | -0.27996 | 1.30588 | 192.10020 | 0.167472 | 9 | 52.941 |
| 0.93696 | -0.96138 | 1.10188 | 299.16333 | 0.141302 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 79
MODEL XH-51A SWIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 69.08995 | | | | | 0 | |
| -18.85118 | 25.70105 | 31.87335 | 126.25929 | 1.000000 | 1 | 5.882 |
| 9.80631 | -1.46402 | 9.90500 | 351.58879 | 0.311075 | 2 | 11.765 |
| -5.67576 | 3.78349 | 5.27518 | 134.17105 | 0.165504 | 3 | 17.647 |
| 3.15863 | 0.98973 | 3.31006 | 17.39793 | 0.103858 | 4 | 23.529 |
| -1.04152 | -2.30771 | 2.53185 | 245.78924 | 0.079435 | 5 | 29.412 |
| 0.58531 | 0.16842 | 0.60906 | 16.08286 | 0.019109 | 6 | 35.294 |
| -3.16388 | -0.01973 | 3.16394 | 180.35724 | 0.099266 | 7 | 41.176 |
| 1.08271 | -1.42859 | 1.79252 | 307.19771 | 0.056259 | 8 | 47.059 |
| 0.16137 | 1.14242 | 1.15376 | 81.96013 | 0.036198 | 9 | 52.941 |
| -1.16115 | 0.29693 | 1.19851 | 165.69588 | 0.037602 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 79
MODEL XH-51A SWIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -130.89636 | | | | | 0 | |
| 3.98679 | -20.61899 | 21.00807 | 280.94336 | 1.000000 | 1 | 5.882 |
| 5.61594 | 8.37808 | 9.97620 | 57.11966 | 0.475030 | 2 | 11.765 |
| -2.92191 | -0.21980 | 2.93817 | 184.90193 | 0.139926 | 3 | 17.647 |
| -2.74272 | 1.31459 | 3.04149 | 154.39145 | 0.144827 | 4 | 23.529 |
| -4.66785 | 1.82580 | 5.01222 | 158.63731 | 0.238667 | 5 | 29.412 |
| -0.50084 | 0.53515 | 0.73295 | 133.10303 | 0.034901 | 6 | 35.294 |
| -1.31081 | -0.12840 | 1.31788 | 185.59444 | 0.062715 | 7 | 41.176 |
| 0.93833 | -1.30195 | 1.60405 | 305.70876 | 0.076418 | 8 | 47.059 |
| -0.00194 | -0.59975 | 0.59976 | 269.79419 | 0.028562 | 9 | 52.941 |
| -0.42140 | -1.28125 | 1.34877 | 291.79482 | 0.064225 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 80
MODEL XH-51A SWIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 95.36409 | | | | | 0 | |
| -21.21744 | 24.25534 | 40.29481 | 121.77374 | 1.000000 | 1 | 5.882 |
| 14.67262 | -1.55863 | 14.75517 | 353.98628 | 0.366188 | 2 | 11.765 |
| -2.53440 | 3.97801 | 4.71673 | 122.90134 | 0.117058 | 3 | 17.647 |
| 5.17615 | -0.17347 | 5.17905 | 358.00057 | 0.128532 | 4 | 23.529 |
| -1.06181 | -4.22693 | 4.35825 | 255.89891 | 0.108161 | 5 | 29.412 |
| 1.20988 | -0.63618 | 1.36683 | 332.26489 | 0.033922 | 6 | 35.294 |
| -4.46241 | 0.19789 | 4.46679 | 177.46877 | 0.110855 | 7 | 41.176 |
| 1.23498 | -1.79998 | 2.18000 | 305.68842 | 0.053958 | 8 | 47.059 |
| 0.46083 | 0.69804 | 0.83256 | 55.97780 | 0.020662 | 9 | 52.941 |
| -0.38880 | -0.19374 | 0.36459 | 212.19411 | 0.009047 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 80
MODEL XH-51A SWIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -136.78928 | | | | | 0 | |
| 6.89628 | -21.79418 | 22.86963 | 287.49316 | 1.000000 | 1 | 5.882 |
| 3.11358 | 13.23473 | 13.59683 | 76.76198 | 0.594880 | 2 | 11.765 |
| -3.89275 | -0.16584 | 3.89428 | 182.43942 | 0.170821 | 3 | 17.647 |
| -2.41932 | 3.15230 | 3.97367 | 127.90845 | 0.174215 | 4 | 23.529 |
| -5.31555 | -0.68591 | 5.36078 | 186.48163 | 0.234648 | 5 | 29.412 |
| 0.87927 | 0.33741 | 0.94178 | 20.99268 | 0.041290 | 6 | 35.294 |
| -0.33645 | -0.07051 | 0.34395 | 191.82980 | 0.015068 | 7 | 41.176 |
| 1.15196 | -2.03255 | 2.32650 | 299.11401 | 0.101999 | 8 | 47.059 |
| 0.17414 | -0.54875 | 0.57572 | 287.60896 | 0.025241 | 9 | 52.941 |
| -0.95312 | -2.03764 | 2.24955 | 244.93192 | 0.098625 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION .03
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 92.92566 | | | | | 0 | |
| -13.27587 | 30.49028 | 33.25516 | 113.52899 | 1.000000 | 1 | 5.882 |
| 15.70161 | -0.56708 | 15.71185 | 357.93140 | 0.472463 | 2 | 11.765 |
| 0.90394 | 4.00766 | 4.10834 | 77.28943 | 0.123540 | 3 | 17.647 |
| 4.29427 | -2.24536 | 4.84586 | 332.39407 | 0.145718 | 4 | 23.529 |
| 0.14007 | -4.08230 | 4.08469 | 271.96509 | 0.122829 | 5 | 29.412 |
| 0.37479 | -1.09949 | 1.16161 | 288.82275 | 0.034930 | 6 | 35.294 |
| -2.82164 | -0.30490 | 2.83809 | 186.16725 | 0.085343 | 7 | 41.176 |
| 1.44577 | -0.06516 | 1.44734 | 357.41943 | 0.043519 | 8 | 47.059 |
| 0.10791 | 0.42371 | 0.43714 | 75.76318 | 0.013145 | 9 | 52.941 |
| 0.61517 | -1.59416 | 1.70873 | 291.10083 | 0.051382 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -50.46820 | | | | | 0 | |
| 9.56439 | 0.99097 | 9.61642 | 5.96272 | 1.000000 | 1 | 5.882 |
| -1.90713 | 7.33495 | 7.57882 | 104.57462 | 0.788113 | 2 | 11.765 |
| -5.10223 | 2.38474 | 5.59862 | 155.69060 | 0.582194 | 3 | 17.647 |
| -1.41986 | 1.09251 | 1.79153 | 142.42946 | 0.186299 | 4 | 23.529 |
| -3.84338 | -3.58886 | 4.70533 | 229.70180 | 0.489323 | 5 | 29.412 |
| 1.25345 | 0.17898 | 1.26616 | 8.12630 | 0.131667 | 6 | 35.294 |
| 0.38487 | -0.69370 | 0.79331 | 299.02197 | 0.082496 | 7 | 41.176 |
| 1.48516 | -0.57977 | 1.77923 | 326.58091 | 0.185020 | 8 | 47.059 |
| -0.68184 | 0.00849 | 0.68189 | 179.28700 | 0.070909 | 9 | 52.941 |
| -0.62484 | -2.23608 | 2.32174 | 254.38763 | 0.241435 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 79.81736 | | | | | 0 | |
| -6.33557 | 20.65051 | 21.60052 | 107.05605 | 1.000000 | 1 | 5.882 |
| 13.68000 | 0.40496 | 13.61483 | 1.70447 | 0.630001 | 2 | 11.765 |
| 2.47379 | 2.94386 | 3.84525 | 49.95897 | 0.178017 | 3 | 17.647 |
| 2.64270 | -3.11308 | 4.08352 | 310.32788 | 0.189047 | 4 | 23.529 |
| 0.47876 | -2.80328 | 2.84294 | 279.53271 | 0.131596 | 5 | 29.412 |
| 0.03638 | -1.30173 | 1.30224 | 271.60059 | 0.060287 | 6 | 35.294 |
| -1.19773 | -0.48353 | 1.29165 | 201.98398 | 0.059797 | 7 | 41.176 |
| 1.06692 | 0.89119 | 1.39199 | 39.80841 | 0.064443 | 8 | 47.059 |
| 0.07535 | 0.27763 | 0.28768 | 74.81526 | 0.013318 | 9 | 52.941 |
| 0.83184 | -1.84155 | 2.02071 | 294.30908 | 0.093549 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.28961 | | | | | 0 | |
| 7.99189 | 13.57310 | 15.75072 | 59.51302 | 1.000000 | 1 | 5.882 |
| -3.43158 | 2.18894 | 4.07828 | 147.46693 | 0.258419 | 2 | 11.765 |
| -4.93382 | 3.10428 | 5.82849 | 147.81837 | 0.370044 | 3 | 17.647 |
| -0.49768 | -0.73228 | 0.88539 | 235.79078 | 0.056213 | 4 | 23.529 |
| -1.32245 | -4.09998 | 4.26985 | 251.95772 | 0.271089 | 5 | 29.412 |
| 1.11819 | -0.29994 | 1.14989 | 344.90039 | 0.073005 | 6 | 35.294 |
| 0.29877 | -0.79436 | 0.84850 | 299.02100 | 0.053140 | 7 | 41.176 |
| 0.94417 | -0.09186 | 0.94863 | 354.44312 | 0.060228 | 8 | 47.059 |
| -0.64287 | 0.38675 | 0.74955 | 148.93762 | 0.047588 | 9 | 52.941 |
| -0.36469 | -1.69965 | 1.73875 | 257.82520 | 0.110392 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 85.26627 | | | | | 0 | |
| -6.76972 | 19.13240 | 20.29475 | 109.48563 | 1.000000 | 1 | 5.882 |
| 18.14128 | 1.87961 | 18.23837 | 5.91527 | 0.898674 | 2 | 11.765 |
| 2.77168 | 1.89044 | 3.35499 | 34.29816 | 0.165313 | 3 | 17.647 |
| 2.37696 | -4.64827 | 5.22076 | 297.08350 | 0.257247 | 4 | 23.529 |
| -0.26153 | -1.99279 | 2.01298 | 261.99874 | 0.099167 | 5 | 29.412 |
| 0.82166 | -2.71165 | 2.83340 | 286.89742 | 0.139613 | 6 | 35.294 |
| -1.14639 | -0.36395 | 1.28878 | 197.61327 | 0.059265 | 7 | 41.176 |
| 0.35633 | 1.26805 | 1.31716 | 74.30637 | 0.064901 | 8 | 47.059 |
| 1.01664 | 0.29514 | 1.05861 | 16.18849 | 0.052162 | 9 | 52.941 |
| 0.91084 | -1.74169 | 1.96548 | 297.60791 | 0.096847 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.38628 | | | | | 0 | |
| 5.82994 | 19.29883 | 20.15251 | 73.18443 | 1.000000 | 1 | 5.882 |
| -2.59281 | 1.93806 | 3.23788 | 143.22289 | 0.160629 | 2 | 11.765 |
| -6.77739 | 3.34326 | 7.55714 | 153.74384 | 0.374997 | 3 | 17.647 |
| 0.30457 | -1.96038 | 1.99173 | 278.79590 | 0.098833 | 4 | 23.529 |
| -2.08734 | -4.85217 | 4.52211 | 243.64735 | 0.224394 | 5 | 29.412 |
| 1.56926 | -2.15620 | 2.65112 | 308.65308 | 0.131553 | 6 | 35.294 |
| -0.04261 | -0.09903 | 0.10854 | 246.80289 | 0.005386 | 7 | 41.176 |
| -0.62918 | 0.46873 | 0.79029 | 146.99156 | 0.039231 | 8 | 47.059 |
| 0.73995 | 0.69868 | 1.06899 | 43.19797 | 0.050860 | 9 | 52.941 |
| -0.64118 | -1.54021 | 1.66831 | 247.40073 | 0.082784 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 219.83220 | | | | | 0 | |
| -20.86296 | 31.09831 | 37.44653 | 123.85825 | 0.691314 | 1 | 5.882 |
| 53.44898 | 8.79175 | 54.16714 | 9.34088 | 1.000000 | 2 | 11.765 |
| 4.51530 | -1.08874 | 4.64283 | 346.53931 | 0.085713 | 3 | 17.647 |
| 4.39200 | -14.04425 | 14.71498 | 287.36572 | 0.271659 | 4 | 23.529 |
| -5.28495 | -1.30585 | 5.44389 | 193.87917 | 0.100502 | 5 | 29.412 |
| 6.19215 | -10.46723 | 12.1 133 | 300.44907 | 0.224146 | 6 | 35.294 |
| -3.25934 | 0.45962 | 3.2[illegible]18 | 171.97484 | 0.060778 | 7 | 41.176 |
| -2.56780 | 2.07006 | 3.26652 | 141.79953 | 0.060304 | 8 | 47.059 |
| 6.14666 | 6.74707 | 8.19189 | 6.92974 | 0.114311 | 9 | 52.941 |
| 1.23416 | -1.29679 | 1.79020 | 313.58228 | 0.033058 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.15814 | | | | | 0 | |
| -1.11794 | 38.14394 | 38.16031 | 91.67883 | 1.000000 | 1 | 5.882 |
| 3.30391 | 8.91007 | 9.50291 | 69.65486 | 0.249026 | 2 | 11.765 |
| -18.83881 | 4.71309 | 19.41940 | 165.95486 | 0.508890 | 3 | 17.647 |
| 3.14601 | -6.73817 | 7.43642 | 295.02759 | 0.194875 | 4 | 23.529 |
| -8.38319 | -5.60980 | 10.02063 | 216.84372 | 0.262593 | 5 | 29.412 |
| 4.76246 | -11.33272 | 12.29275 | 292.79395 | 0.322134 | 6 | 35.294 |
| -2.59183 | 3.16850 | 4.09353 | 129.28322 | 0.107272 | 7 | 41.176 |
| -8.26516 | 1.33300 | 8.37196 | 170.83029 | 0.219389 | 8 | 47.059 |
| 8.22466 | 2.27097 | 8.53243 | 15.43571 | 0.223594 | 9 | 52.941 |
| -3.86477 | -1.76969 | 3.53901 | 210.00348 | 0.092741 | 10 | 58.824 |

TEXT NOT REPRODUCIBLE

HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 172.91248 | | | | | 0 | |
| -13.71082 | 18.86147 | 17.40164 | 141.61435 | 0.409991 | 1 | 5.882 |
| 42.21269 | 6.18540 | 42.66345 | 8.33619 | 1.000000 | 2 | 11.765 |
| 6.94354 | -8.59831 | 8.57859 | 334.08176 | 0.134018 | 3 | 17.647 |
| 2.41889 | -12.87649 | 13.10157 | 280.63574 | 0.307091 | 4 | 23.529 |
| -9.73825 | -2.63795 | 6.31283 | 204.70823 | 0.1479068 | 5 | 29.412 |
| 8.48943 | -9.37641 | 8.42725 | 320.58864 | 0.197528 | 6 | 35.294 |
| -1.84731 | 0.00000 | 1.05117 | 178.00000 | 0.024639 | 7 | 41.176 |
| -1.89458 | -0.93190 | 1.98782 | 198.68192 | 0.046124 | 8 | 47.059 |
| 3.64799 | 1.94673 | 3.96313 | 28.08884 | 0.092893 | 9 | 52.941 |
| 0.82741 | 0.79832 | 0.79879 | 88.02977 | 0.018693 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 44.32829 | | | | | 0 | |
| -9.77984 | 18.18697 | 19.02468 | 107.68983 | 1.000000 | 1 | 5.882 |
| 6.82479 | 7.61481 | 10.22561 | 48.13159 | 0.986648 | 2 | 11.765 |
| -11.62194 | 2.79990 | 11.95486 | 166.48427 | 0.627350 | 3 | 17.647 |
| 8.73704 | -9.81159 | 5.89814 | 277.23148 | 0.309440 | 4 | 23.529 |
| -3.98184 | -4.43795 | 5.94885 | 228.24988 | 0.312180 | 5 | 29.412 |
| 3.49827 | -9.23889 | 6.17920 | 301.08278 | 0.324899 | 6 | 35.294 |
| -3.95210 | 2.44862 | 4.42522 | 148.78185 | 0.232750 | 7 | 41.176 |
| -5.84825 | -1.71546 | 6.11584 | 196.29534 | 0.320889 | 8 | 47.059 |
| 6.43116 | 3.52173 | 7.33228 | 28.78828 | 0.384884 | 9 | 52.941 |
| -4.01982 | 0.09510 | 4.02094 | 178.64476 | 0.211022 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 190.23828 | | | | | 0 | |
| -2.88124 | -3.19983 | 3.78866 | 236.68892 | 0.097299 | 1 | 5.882 |
| 38.87323 | 0.96147 | 38.89710 | 1.41678 | 1.000000 | 2 | 11.765 |
| 17.64755 | 5.41945 | 18.44894 | 17.09138 | 0.474732 | 3 | 17.647 |
| 2.37659 | -15.52746 | 15.70820 | 278.78198 | 0.403946 | 4 | 23.529 |
| -6.10937 | -11.42093 | 12.98289 | 241.08041 | 0.333077 | 5 | 29.412 |
| 6.67158 | 3.17898 | 7.29886 | 25.67748 | 0.190041 | 6 | 35.294 |
| 3.30218 | -0.72758 | 3.38189 | 347.57422 | 0.086954 | 7 | 41.176 |
| 1.68944 | -3.71689 | 4.09888 | 298.36848 | 0.104998 | 8 | 47.059 |
| -1.94383 | 2.44869 | 3.27908 | 126.35787 | 0.084328 | 9 | 52.941 |
| -1.17463 | 1.91292 | 2.24478 | 121.55211 | 0.057725 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 142.34286 | | | | | 0 | |
| -0.59898 | 7.27896 | 7.29134 | 94.52671 | 0.649962 | 1 | 5.882 |
| 5.89579 | 4.48145 | 7.39752 | 36.74284 | 0.651829 | 2 | 11.765 |
| -2.71898 | 3.89883 | 4.78188 | 125.31993 | 0.416954 | 3 | 17.647 |
| -3.78844 | -5.94840 | 8.68192 | 235.67995 | 0.991972 | 4 | 23.529 |
| 4.89468 | -8.89884 | 11.26756 | 298.92197 | 1.000000 | 5 | 29.412 |
| 2.14443 | 7.89874 | 7.58862 | 73.48146 | 0.665212 | 6 | 35.294 |
| -5.33142 | 0.58893 | 5.33837 | 176.53491 | 0.472705 | 7 | 41.176 |
| 6.56882 | -7.66816 | 7.48838 | 274.23884 | 0.658944 | 8 | 47.059 |
| 1.34885 | 5.98141 | 6.89364 | 77.12347 | 0.534818 | 9 | 52.941 |
| -0.88888 | 2.88286 | 8.39836 | 181.73463 | 0.366142 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 142.54150 | | | | | 0 | |
| 8.11907 | -3.88458 | 9.00051 | 334.43091 | 0.417195 | 1 | 5.882 |
| 21.48434 | -1.96352 | 21.57387 | 354.77088 | 1.000000 | 2 | 11.765 |
| 15.96736 | 4.47623 | 16.58292 | 15.66010 | 0.768658 | 3 | 17.647 |
| 3.71412 | -7.19927 | 8.10888 | 297.28931 | 0.375905 | 4 | 23.529 |
| -6.64291 | -13.79477 | 15.31091 | 244.28665 | 0.709697 | 5 | 29.412 |
| 3.72435 | 0.99070 | 3.85387 | 14.98899 | 0.178636 | 6 | 35.294 |
| 4.28181 | 3.76924 | 5.70448 | 41.35721 | 0.264416 | 7 | 41.176 |
| 1.85793 | -2.80721 | 2.79435 | 311.67383 | 0.129525 | 8 | 47.059 |
| -1.46448 | -2.58956 | 2.98043 | 240.67409 | 0.138442 | 9 | 52.941 |
| -1.78469 | 1.95615 | 2.64795 | 132.37972 | 0.122739 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 96.13492 | | | | | 0 | |
| 5.29930 | 3.82304 | 6.53446 | 35.80707 | 0.630400 | 1 | 5.882 |
| -0.10868 | -0.06501 | 0.19984 | 199.01005 | 0.019497 | 2 | 11.765 |
| 4.82975 | -1.15284 | 4.96566 | 346.56372 | 0.485132 | 3 | 17.647 |
| 2.82480 | -0.99393 | 2.29408 | 333.84546 | 0.220296 | 4 | 23.529 |
| 3.84568 | -9.77206 | 10.23849 | 287.31879 | 1.000000 | 5 | 29.412 |
| 2.84712 | 3.73484 | 4.69965 | 52.67925 | 0.458793 | 6 | 35.294 |
| -0.51854 | 4.44382 | 4.47317 | 96.65695 | 0.437017 | 7 | 41.176 |
| -1.52897 | -4.80429 | 4.28813 | 249.18441 | 0.418743 | 8 | 47.059 |
| 2.17978 | -1.25613 | 2.51235 | 330.08122 | 0.245458 | 9 | 52.941 |
| -2.27983 | 3.97115 | 4.57784 | 119.81670 | 0.447164 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 150.48714 | | | | | 0 | |
| 12.92442 | -12.56292 | 18.02408 | 315.81250 | 0.949788 | 1 | 5.882 |
| 16.67490 | -4.88748 | 17.37640 | 343.66382 | 0.954144 | 2 | 11.765 |
| 18.20935 | 0.28152 | 18.21152 | 0.88574 | 1.000000 | 3 | 17.647 |
| 9.82831 | -3.20935 | 10.33909 | 341.91479 | 0.567723 | 4 | 23.529 |
| -9.31423 | -15.47066 | 18.05812 | 238.94980 | 0.991577 | 5 | 29.412 |
| 0.37970 | -5.89757 | 5.11169 | 274.29977 | 0.280685 | 6 | 35.294 |
| 6.09943 | 4.74180 | 7.72578 | 37.86212 | 0.424225 | 7 | 41.176 |
| 3.01961 | 2.62142 | 3.99873 | 40.96234 | 0.219572 | 8 | 47.059 |
| -1.48194 | -4.93216 | 5.14987 | 253.28059 | 0.282781 | 9 | 52.941 |
| -1.56152 | -2.09568 | 2.61347 | 233.30963 | 0.143506 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 56.84654 | | | | | 0 | |
| 18.10477 | 26.23624 | 31.87664 | 55.39149 | 1.000000 | 1 | 5.882 |
| -4.14861 | 0.66239 | 4.20115 | 170.92847 | 0.131794 | 2 | 11.765 |
| 5.63101 | -7.61524 | 9.47102 | 306.40071 | 0.297114 | 3 | 17.647 |
| 5.99220 | 1.06995 | 6.08698 | 10.12389 | 0.190954 | 4 | 23.529 |
| -0.48242 | -9.57661 | 9.58895 | 267.11621 | 0.300814 | 5 | 29.412 |
| 2.22052 | -4.07885 | 4.64411 | 298.56312 | 0.145690 | 6 | 35.294 |
| 3.47632 | 5.80817 | 6.09644 | 59.23427 | 0.191251 | 7 | 41.176 |
| -2.59885 | 2.60801 | 3.73835 | 134.02501 | 0.117275 | 8 | 47.059 |
| 0.80344 | -4.41185 | 4.41185 | 270.04712 | 0.138404 | 9 | 52.941 |
| 1.40253 | 0.02785 | 1.40281 | 1.13737 | 0.044007 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 73.34781 | | | | | 0 | |
| 7.16172 | -10.26027 | 12.51253 | 304.91528 | 1.000000 | 1 | 5.882 |
| 6.45196 | -3.44208 | 7.31271 | 331.92017 | 0.584431 | 2 | 11.765 |
| 9.51472 | -1.55438 | 9.64085 | 350.72168 | 0.770496 | 3 | 17.647 |
| 7.01787 | -0.49061 | 7.03503 | 356.00098 | 0.562236 | 4 | 23.529 |
| -5.15930 | -7.45418 | 9.06510 | 235.31149 | 0.724514 | 5 | 29.412 |
| -1.17463 | -4.45510 | 4.60734 | 255.22949 | 0.368219 | 6 | 35.294 |
| 3.56891 | 1.84159 | 4.01604 | 27.29408 | 0.320961 | 7 | 41.176 |
| 2.01243 | 3.10629 | 3.70120 | 57.06252 | 0.295800 | 8 | 47.059 |
| -1.00046 | -2.56885 | 2.75679 | 248.72115 | 0.220323 | 9 | 52.941 |
| -0.51909 | -2.88437 | 2.93071 | 259.79785 | 0.234222 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.83574 | | | | | 0 | |
| 13.61173 | 22.15103 | 25.99898 | 58.42937 | 1.000000 | 1 | 5.882 |
| -3.04338 | 1.02164 | 3.21028 | 161.44353 | 0.123477 | 2 | 11.765 |
| 2.28019 | -5.74701 | 6.18283 | 291.64111 | 0.237811 | 3 | 17.647 |
| 3.51270 | 0.94506 | 3.63761 | 15.05839 | 0.139914 | 4 | 23.529 |
| -1.33734 | -4.27795 | 4.48211 | 252.64009 | 0.172396 | 5 | 29.412 |
| 0.44797 | -4.53037 | 4.55246 | 275.64697 | 0.175102 | 6 | 35.294 |
| 2.79748 | 1.71703 | 3.28239 | 31.54074 | 0.126251 | 7 | 41.176 |
| -0.98330 | 3.73105 | 3.85845 | 104.76439 | 0.148408 | 8 | 47.059 |
| -1.58659 | -2.36941 | 2.83319 | 237.87524 | 0.108973 | 9 | 52.941 |
| 1.86595 | -2.14697 | 2.84491 | 310.99414 | 0.109408 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.79677 | | | | | 0 | |
| 0.57785 | -0.86046 | 1.03648 | 303.88354 | 1.000000 | 1 | 5.882 |
| 0.48835 | -0.28511 | 0.56549 | 329.72290 | 0.545581 | 2 | 11.765 |
| 0.79968 | -0.14362 | 0.77314 | 349.29419 | 0.745929 | 3 | 17.647 |
| 0.58206 | -0.02468 | 0.58258 | 357.57227 | 0.562076 | 4 | 23.529 |
| -0.41575 | -0.58874 | 0.72073 | 234.77135 | 0.695364 | 5 | 29.412 |
| -0.10955 | -0.37684 | 0.39244 | 253.79068 | 0.378627 | 6 | 35.294 |
| 0.28941 | 0.14990 | 0.32189 | 25.95847 | 0.310557 | 7 | 41.176 |
| 0.16550 | 0.26798 | 0.31497 | 58.30074 | 0.303884 | 8 | 47.059 |
| -0.08206 | -0.20810 | 0.22184 | 248.28877 | 0.214010 | 9 | 52.941 |
| -0.03823 | -0.25045 | 0.25335 | 261.32056 | 0.244431 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 504 OSC CTR 269 TEST COND 11 COMP RUN 62.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.63777 | | | | | 0 | |
| 1.13463 | 1.86437 | 2.18249 | 58.67596 | 1.000000 | 1 | 5.882 |
| -0.25381 | 0.08869 | 0.26886 | 160.73961 | 0.123191 | 2 | 11.765 |
| 0.17553 | -0.47982 | 0.51092 | 290.09424 | 0.234100 | 3 | 17.647 |
| 0.28618 | 0.08047 | 0.29728 | 15.70586 | 0.136213 | 4 | 23.529 |
| -0.11967 | -0.33348 | 0.35430 | 250.26007 | 0.162339 | 5 | 29.412 |
| 0.02810 | -0.39002 | 0.39103 | 274.12036 | 0.179166 | 6 | 35.294 |
| 0.23529 | 0.12805 | 0.26787 | 28.55522 | 0.122738 | 7 | 41.176 |
| -0.07518 | 0.32493 | 0.33352 | 103.02805 | 0.152815 | 8 | 47.059 |
| -0.13670 | -0.19407 | 0.23738 | 234.84012 | 0.108764 | 9 | 52.941 |
| 0.16240 | -0.19538 | 0.25406 | 309.73315 | 0.116410 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.64508 | | | | | 0 | |
| -0.13792 | 0.47996 | 0.49938 | 106.03223 | 1.000000 | 1 | 5.848 |
| 0.06616 | 0.15488 | 0.16842 | 66.86809 | 0.337249 | 2 | 11.696 |
| 0.05317 | -0.01703 | 0.05583 | 342.23730 | 0.111791 | 3 | 17.544 |
| 0.04652 | 0.03720 | 0.05936 | 38.65018 | 0.118270 | 4 | 23.392 |
| 0.05925 | 0.01586 | 0.06133 | 14.98721 | 0.122815 | 5 | 29.240 |
| 0.01040 | 0.06333 | 0.06418 | 80.67201 | 0.128509 | 6 | 35.088 |
| -0.01808 | 0.06147 | 0.06408 | 106.38800 | 0.128308 | 7 | 40.936 |
| -0.03804 | 0.00992 | 0.03933 | 165.38872 | 0.078765 | 8 | 46.784 |
| -0.01203 | 0.00532 | 0.01316 | 156.15718 | 0.026343 | 9 | 52.632 |
| -0.00118 | 0.00005 | 0.00118 | 177.94623 | 0.002359 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.88017 | | | | | 0 | |
| 0.12950 | 0.67827 | 0.69052 | 79.19106 | 1.000000 | 1 | 5.848 |
| -0.06652 | 0.38821 | 0.39387 | 99.72337 | 0.570393 | 2 | 11.696 |
| 0.01109 | 0.14682 | 0.14724 | 85.67897 | 0.213226 | 3 | 17.544 |
| -0.00732 | 0.12313 | 0.12335 | 93.40353 | 0.178629 | 4 | 23.392 |
| 0.01803 | -0.03773 | 0.04182 | 295.53955 | 0.060562 | 5 | 29.240 |
| -0.00539 | -0.05085 | 0.05114 | 263.99117 | 0.074053 | 6 | 35.088 |
| 0.01958 | -0.09909 | 0.06.11 | 284.77167 | 0.088498 | 7 | 40.936 |
| 0.02899 | -0.01060 | 0.03087 | 339.92467 | 0.044706 | 8 | 46.784 |
| -0.01222 | -0.03985 | 0.04169 | 252.95149 | 0.060369 | 9 | 52.632 |
| -0.03170 | 0.02760 | 0.04203 | 139.95032 | 0.060874 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.48618 | | | | | 0 | |
| -0.70534 | 2.32081 | 2.42569 | 106.90961 | 1.000000 | 1 | 5.848 |
| 0.31741 | 0.74320 | 0.80814 | 66.87323 | 0.333159 | 2 | 11.696 |
| 0.25028 | -0.07993 | 0.26273 | 342.28857 | 0.108311 | 3 | 17.544 |
| 0.21638 | 0.19761 | 0.29303 | 42.40472 | 0.120804 | 4 | 23.392 |
| 0.26919 | 0.08420 | 0.28205 | 17.36888 | 0.116276 | 5 | 29.240 |
| 0.03975 | 0.30288 | 0.30547 | 82.92388 | 0.125932 | 6 | 35.088 |
| -0.08837 | 0.29412 | 0.30711 | 106.72339 | 0.126607 | 7 | 40.936 |
| -0.17830 | 0.03631 | 0.18098 | 162.47360 | 0.077085 | 8 | 46.784 |
| -0.05567 | 0.03357 | 0.06501 | 148.91336 | 0.026800 | 9 | 52.632 |
| -0.00251 | 0.00814 | 0.00851 | 107.13583 | 0.003510 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.59045 | | | | | 0 | |
| 0.64480 | 3.09630 | 3.16273 | 78.23625 | 1.000000 | 1 | 5.848 |
| -0.29010 | 1.82563 | 1.84853 | 99.02910 | 0.584473 | 2 | 11.696 |
| 0.08515 | 0.67803 | 0.68336 | 82.84210 | 0.216065 | 3 | 17.544 |
| -0.02880 | 0.58178 | 0.58249 | 92.83456 | 0.184174 | 4 | 23.392 |
| 0.09637 | -0.18154 | 0.20554 | 297.95996 | 0.064987 | 5 | 29.240 |
| -0.01721 | -0.22900 | 0.22965 | 269.70142 | 0.072610 | 6 | 35.088 |
| 0.07194 | -0.26583 | 0.27540 | 285.14233 | 0.087075 | 7 | 40.936 |
| 0.13229 | -0.04913 | 0.14112 | 339.62622 | 0.044619 | 8 | 46.784 |
| -0.05179 | -0.18336 | 0.19053 | 254.22797 | 0.060242 | 9 | 52.632 |
| -0.15435 | 0.13721 | 0.20652 | 138.36401 | 0.069297 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.27681 | | | | | 0 | |
| -1.92056 | 5.74867 | 6.06100 | 108.47383 | 1.000000 | 1 | 5.848 |
| 0.77500 | 1.81552 | 1.97401 | 66.88354 | 0.325691 | 2 | 11.696 |
| 0.58954 | -0.18713 | 0.61853 | 342.38969 | 0.102050 | 3 | 17.544 |
| 0.49774 | 0.56883 | 0.75585 | 48.81334 | 0.124708 | 4 | 23.392 |
| 0.58946 | 0.24215 | 0.63726 | 22.33290 | 0.105141 | 5 | 29.240 |
| 0.05124 | 0.73535 | 0.73714 | 86.01360 | 0.121620 | 6 | 35.088 |
| -0.22317 | 0.71459 | 0.74863 | 107.34363 | 0.123516 | 7 | 40.936 |
| -0.41598 | 0.17673 | 0.45197 | 156.98163 | 0.074570 | 8 | 46.784 |
| -0.12667 | 0.11826 | 0.17329 | 136.96664 | 0.028591 | 9 | 52.632 |
| 0.00802 | 0.05545 | 0.05603 | 81.77260 | 0.009244 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 64.57403 | | | | | 0 | |
| 1.68083 | 6.85007 | 7.05327 | 76.21349 | 1.000000 | 1 | 5.848 |
| -0.57746 | 4.29189 | 4.33056 | 97.66307 | 0.613979 | 2 | 11.696 |
| 0.35185 | 1.93658 | 1.97635 | 77.10245 | 0.223492 | 3 | 17.544 |
| -0.04182 | 1.38003 | 1.38066 | 91.73561 | 0.195748 | 4 | 23.392 |
| 0.27979 | -0.44576 | 0.52630 | 302.11499 | 0.074617 | 5 | 29.240 |
| -0.00308 | -0.49181 | 0.49182 | 269.64007 | 0.069729 | 6 | 35.088 |
| 0.16298 | -0.56953 | 0.59239 | 285.96973 | 0.083988 | 7 | 40.936 |
| 0.29231 | -0.11226 | 0.31312 | 338.99170 | 0.044394 | 8 | 46.784 |
| -0.09599 | -0.41231 | 0.42325 | 256.94751 | 0.060007 | 9 | 52.632 |
| -0.38707 | 0.35658 | 0.52628 | 137.34747 | 0.074615 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 36.97379 | | | | | 0 | |
| -5.85832 | 13.18822 | 14.42759 | 113.92220 | 1.000000 | 1 | 5.848 |
| 1.69873 | 3.94769 | 4.29767 | 66.71727 | 0.297878 | 2 | 11.696 |
| 1.04957 | -0.28769 | 1.08828 | 344.67114 | 0.075431 | 3 | 17.544 |
| 0.76719 | 1.97351 | 2.11739 | 68.75671 | 0.146760 | 4 | 23.392 |
| 0.63424 | 0.84146 | 1.05371 | 52.99355 | 0.073035 | 5 | 29.240 |
| -0.32249 | 1.53509 | 1.56859 | 101.86407 | 0.108722 | 6 | 35.088 |
| -0.95781 | 1.50860 | 1.60842 | 110.29282 | 0.111482 | 7 | 40.936 |
| -0.72579 | 0.74704 | 1.04121 | 134.15392 | 0.072148 | 8 | 46.784 |
| -0.18838 | 0.99541 | 0.62498 | 107.55701 | 0.043285 | 9 | 52.632 |
| 0.14977 | 0.45372 | 0.47780 | 71.73206 | 0.033117 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 113.63254 | | | | | 0 | |
| 4.59295 | 7.87184 | 9.11378 | 59.73781 | 1.000000 | 1 | 5.848 |
| 0.01917 | 7.72953 | 7.72956 | 89.85779 | 0.848117 | 2 | 11.696 |
| 2.09993 | 2.62780 | 3.00892 | 44.68217 | 0.330056 | 3 | 17.544 |
| 0.16538 | 2.60176 | 2.60700 | 86.36473 | 0.286051 | 4 | 23.392 |
| 1.01587 | -1.01252 | 1.43372 | 315.07202 | 0.157313 | 5 | 29.240 |
| 0.33317 | -0.42567 | 0.54055 | 308.05005 | 0.059311 | 6 | 35.088 |
| 0.20862 | -0.49782 | 0.53984 | 292.79635 | 0.059233 | 7 | 40.936 |
| 0.39882 | -0.16484 | 0.39406 | 335.38347 | 0.043238 | 8 | 46.784 |
| 0.08281 | -0.55256 | 0.55873 | 278.52319 | 0.061306 | 9 | 52.632 |
| -0.92794 | 0.90035 | 1.34987 | 133.42683 | 0.148113 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 58.85596 | | | | | 0 | |
| -7.90727 | 11.41025 | 13.88232 | 124.72186 | 1.000000 | 1 | 5.848 |
| 1.29182 | 2.99501 | 3.26173 | 66.66832 | 0.234956 | 2 | 11.696 |
| 0.38490 | -0.04649 | 0.38770 | 353.11230 | 0.027927 | 3 | 17.544 |
| 0.00892 | 3.01577 | 3.01578 | 89.83037 | 0.217239 | 4 | 23.392 |
| -0.75741 | 1.28322 | 1.49008 | 120.55098 | 0.107336 | 5 | 29.240 |
| -1.07711 | 1.07030 | 1.51845 | 135.18179 | 0.109380 | 6 | 35.088 |
| -0.55761 | 1.06904 | 1.20572 | 117.54651 | 0.086853 | 7 | 40.936 |
| -0.17811 | 1.27362 | 1.28894 | 98.84152 | 0.092848 | 8 | 46.784 |
| 0.02578 | 1.10743 | 1.10773 | 88.66612 | 0.079794 | 9 | 52.632 |
| 0.36964 | 0.98823 | 1.05509 | 69.49214 | 0.076003 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 34.88873 | | | | | 0 | |
| 5.36692 | -7.14448 | 8.93574 | 306.91382 | 1.000000 | 1 | 5.848 |
| 2.41604 | 2.80749 | 3.70395 | 49.28571 | 0.414509 | 2 | 11.696 |
| 4.19010 | -0.47242 | 4.21665 | 353.56714 | 0.471886 | 3 | 17.544 |
| 0.63586 | 1.22212 | 1.37764 | 62.51228 | 0.154172 | 4 | 23.392 |
| 1.56853 | -0.82140 | 1.77059 | 332.39986 | 0.198147 | 5 | 29.240 |
| 1.04381 | 0.90702 | 1.30980 | 43.86125 | 0.146590 | 6 | 35.088 |
| -0.08735 | 1.06377 | 1.06735 | 94.69417 | 0.119447 | 7 | 40.936 |
| -0.28043 | 0.01936 | 0.28110 | 176.05162 | 0.031458 | 8 | 46.784 |
| 0.62320 | 0.23126 | 0.66472 | 20.39886 | 0.074389 | 9 | 52.632 |
| -0.88114 | 1.13377 | 1.43591 | 127.85365 | 0.160693 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 91.86365 | | | | | 0 | |
| -10.95442 | 10.17502 | 14.95093 | 137.11252 | 1.000000 | 1 | 5.848 |
| 0.84693 | 2.22990 | 2.38532 | 69.20276 | 0.159543 | 2 | 11.696 |
| 0.33136 | -0.41640 | 0.53215 | 308.51196 | 0.035593 | 3 | 17.544 |
| -0.01394 | 4.38999 | 4.39001 | 90.18199 | 0.293628 | 4 | 23.392 |
| -1.36712 | 1.85143 | 2.30147 | 126.44264 | 0.153935 | 5 | 29.240 |
| -1.72278 | 1.00937 | 1.66390 | 142.65388 | 0.111291 | 6 | 35.088 |
| -0.41218 | 0.85044 | 0.95046 | 115.70039 | 0.063572 | 7 | 40.936 |
| 0.22853 | 1.54325 | 1.56007 | 81.57649 | 0.104346 | 8 | 46.784 |
| 0.17726 | 1.34090 | 1.35296 | 82.46954 | 0.090467 | 9 | 52.632 |
| 0.47660 | 1.23360 | 1.32746 | 68.87584 | 0.088454 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.93110 | | | | | 0 | |
| 6.29091 | -10.90662 | 12.59087 | 299.97607 | 1.000000 | 1 | 5.848 |
| 2.93459 | 0.02079 | 2.93467 | 0.40594 | 0.233079 | 2 | 11.696 |
| 5.26749 | -2.12571 | 5.68023 | 338.02319 | 0.451139 | 3 | 17.544 |
| 1.02878 | 0.50292 | 1.14513 | 26.05194 | 0.090949 | 4 | 23.392 |
| 1.96765 | -0.26493 | 1.98540 | 352.33154 | 0.157686 | 5 | 29.240 |
| 1.61456 | 1.53050 | 2.22467 | 43.46947 | 0.176689 | 6 | 35.088 |
| 0.14462 | 2.01003 | 2.01678 | 85.30927 | 0.160178 | 7 | 40.936 |
| -0.78952 | -0.00807 | 0.78956 | 180.58974 | 0.062709 | 8 | 46.784 |
| 0.90913 | 0.54282 | 1.05885 | 30.84071 | 0.084097 | 9 | 52.632 |
| -0.86046 | 1.08714 | 1.38646 | 128.36142 | 0.110116 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 505 CSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 93.78369 | | | | | C | |
| -9.85773 | 5.17774 | 11.13480 | 152.28944 | 1.000000 | 1 | 5.848 |
| -0.06863 | 0.73169 | 0.73491 | 95.35872 | 0.066001 | 2 | 11.696 |
| 0.81672 | -1.29407 | 1.53024 | 302.25684 | 0.137429 | 3 | 17.544 |
| 0.73349 | 4.01996 | 4.08631 | 79.65933 | 0.366985 | 4 | 23.392 |
| -0.46741 | 1.65049 | 1.71539 | 105.81192 | 0.154057 | 5 | 29.240 |
| -0.43728 | 0.94879 | 1.04470 | 114.74417 | 0.093823 | 6 | 35.088 |
| 0.02931 | 0.52705 | 0.52787 | 86.81677 | 0.047407 | 7 | 40.936 |
| 0.37022 | 0.81921 | 0.89898 | 65.68068 | 0.080736 | 8 | 46.784 |
| 0.14963 | 0.65158 | 0.66854 | 77.06682 | 0.060040 | 9 | 52.632 |
| 0.23470 | 0.58539 | 0.63069 | 68.15237 | 0.056641 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 505 CSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.46851 | | | | | C | |
| 4.35787 | 2.97203 | 5.27484 | 34.29370 | 1.000000 | 1 | 5.848 |
| 0.09263 | -0.09487 | 0.13259 | 314.31421 | 0.025136 | 2 | 11.696 |
| 2.78908 | -1.51531 | 3.17414 | 331.48462 | 0.601750 | 3 | 17.544 |
| 0.83271 | 0.36189 | 0.90795 | 23.48917 | 0.172129 | 4 | 23.392 |
| 1.23188 | 0.70142 | 1.41757 | 29.65695 | 0.268742 | 5 | 29.240 |
| 1.53966 | 0.59409 | 1.65030 | 21.09950 | 0.312863 | 6 | 35.088 |
| 0.87699 | 1.28961 | 1.55955 | 55.78244 | 0.295659 | 7 | 40.936 |
| -0.75852 | -0.23286 | 0.79346 | 197.06644 | 0.150423 | 8 | 46.784 |
| 0.46182 | 0.05370 | 0.46493 | 6.63196 | 0.088141 | 9 | 52.632 |
| -0.51016 | 0.33129 | 0.60829 | 147.00049 | 0.115319 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 72.28889 | | | | | C | |
| -6.68825 | 1.45133 | 6.84391 | 167.75681 | 1.000000 | 1 | 5.848 |
| -0.66911 | -0.21953 | 0.70420 | 198.14418 | 0.102894 | 2 | 11.696 |
| 0.94552 | -1.56866 | 1.83158 | 301.07983 | 0.267623 | 3 | 17.544 |
| 0.94178 | 2.75978 | 2.91604 | 71.15761 | 0.426079 | 4 | 23.392 |
| 0.19753 | 1.07384 | 1.09186 | 79.57727 | 0.159537 | 5 | 29.240 |
| 0.13218 | 0.72232 | 0.73431 | 79.62967 | 0.107294 | 6 | 35.088 |
| 0.20868 | 0.24502 | 0.32185 | 49.57990 | 0.047027 | 7 | 40.936 |
| 0.27290 | 0.19997 | 0.33832 | 36.23262 | 0.049434 | 8 | 46.784 |
| 0.05806 | 0.09345 | 0.11002 | 58.14719 | 0.016075 | 9 | 52.632 |
| 0.02949 | 0.05448 | 0.05195 | 61.57175 | 0.009051 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -1.10794 | | | | | C | |
| 2.01549 | 10.88519 | 11.07021 | 79.50989 | 1.000000 | 1 | 5.848 |
| -1.52457 | 0.30318 | 1.56419 | 168.82376 | 0.141297 | 2 | 11.696 |
| 0.65403 | -0.62872 | 0.90722 | 316.13013 | 0.081952 | 3 | 17.544 |
| 0.48475 | 0.30474 | 0.57258 | 32.15579 | 0.051723 | 4 | 23.392 |
| 0.42292 | 0.95578 | 1.04517 | 66.13124 | 0.094413 | 5 | 29.240 |
| 1.04737 | -0.20631 | 1.06749 | 348.85620 | 0.096429 | 6 | 35.088 |
| 1.00251 | 0.48056 | 1.11174 | 25.61115 | 0.100426 | 7 | 40.936 |
| -0.52257 | -0.26623 | 0.58648 | 206.99689 | 0.052978 | 8 | 46.784 |
| 0.03950 | -0.29303 | 0.29568 | 277.67676 | 0.026709 | 9 | 52.632 |
| -0.23884 | -0.18249 | 0.30058 | 217.38205 | 0.027152 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 1C COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 76.82947 | | | | | 0 | |
| -0.11150 | 0.51511 | 0.13317 | 175.18222 | 1.000000 | 1 | 5.848 |
| -1.17400 | -0.76824 | 1.40302 | 213.19381 | 0.228759 | 2 | 11.696 |
| 1.02594 | -2.10121 | 2.33830 | 296.02441 | 0.381254 | 3 | 17.544 |
| 0.91112 | 2.50520 | 2.66574 | 70.01407 | 0.434643 | 4 | 23.392 |
| 0.37409 | 0.84914 | 0.92784 | 66.22430 | 0.151291 | 5 | 29.240 |
| 0.16329 | 0.70359 | 0.72424 | 76.96588 | 0.118068 | 6 | 35.088 |
| 0.14367 | 0.07794 | 0.16340 | 28.44458 | 0.026642 | 7 | 40.936 |
| -0.13137 | -0.03581 | 0.13617 | 344.74316 | 0.022202 | 8 | 46.784 |
| -0.05375 | -0.14775 | 0.15722 | 250.01074 | 0.025635 | 9 | 52.632 |
| -0.06364 | -0.21573 | 0.22492 | 253.56748 | 0.036672 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 1C COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -4.70195 | | | | | 0 | |
| 0.60259 | 15.46623 | 15.47597 | 87.76846 | 1.000000 | 1 | 5.848 |
| -2.09085 | 0.49731 | 2.14688 | 166.88033 | 0.138774 | 2 | 11.696 |
| -0.03199 | -0.44979 | 0.45092 | 265.93091 | 0.029137 | 3 | 17.544 |
| 0.42616 | 0.33442 | 0.54170 | 38.12230 | 0.035003 | 4 | 23.392 |
| -0.12199 | 0.94941 | 0.95721 | 97.32182 | 0.061852 | 5 | 29.240 |
| 0.86813 | -0.70473 | 1.11785 | 320.95068 | 0.072231 | 6 | 35.088 |
| 0.96403 | 0.27741 | 1.00315 | 16.05377 | 0.064820 | 7 | 40.936 |
| -0.55692 | -0.17916 | 0.58503 | 197.83258 | 0.037803 | 8 | 46.784 |
| -0.24997 | -0.49089 | 0.55087 | 243.01405 | 0.035595 | 9 | 52.632 |
| -0.25925 | -0.48517 | 0.54990 | 242.31705 | 0.035274 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 14C
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 1A COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 163.41080 | | | | | 0 | |
| -9.61206 | -0.18998 | 9.61394 | 181.13229 | 1.000000 | 1 | 5.848 |
| -4.36039 | -2.88671 | 5.22935 | 213.50574 | 0.543934 | 2 | 11.696 |
| 1.92914 | -5.54191 | 5.86947 | 289.18652 | 0.610565 | 3 | 17.544 |
| 0.73745 | 3.99915 | 4.02725 | 79.64464 | 0.418897 | 4 | 23.392 |
| 0.43835 | 0.78934 | 0.90289 | 60.94479 | 0.093919 | 5 | 29.240 |
| -0.42693 | 1.14037 | 1.22328 | 110.42656 | 0.127241 | 6 | 35.088 |
| -0.36115 | -0.36299 | 0.51204 | 225.14603 | 0.053260 | 7 | 40.936 |
| -0.38408 | -0.36988 | 0.53250 | 223.99527 | 0.055389 | 8 | 46.784 |
| -0.51034 | -0.56365 | 0.77530 | 228.83356 | 0.080643 | 9 | 52.632 |
| -0.27585 | -0.84677 | 0.89059 | 251.95445 | 0.092634 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 14C
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 1A COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -25.12553 | | | | | 0 | |
| -3.34118 | 33.95235 | 34.11535 | 95.62025 | 1.000000 | 1 | 5.848 |
| -3.39850 | 1.03462 | 3.55250 | 163.06793 | 0.104129 | 2 | 11.696 |
| -0.74140 | -0.98363 | 1.23159 | 232.98763 | 0.036100 | 3 | 17.544 |
| 0.67828 | 0.49497 | 0.83382 | 35.56500 | 0.024441 | 4 | 23.392 |
| -1.87705 | 0.91968 | 2.09024 | 153.89651 | 0.061268 | 5 | 29.240 |
| 0.95712 | -2.47513 | 2.65374 | 291.14111 | 0.077785 | 6 | 35.088 |
| 0.93487 | 0.42975 | 1.02892 | 24.68779 | 0.030159 | 7 | 40.936 |
| -1.26741 | 0.29551 | 1.30234 | 166.69979 | 0.038174 | 8 | 46.784 |
| -1.20278 | -1.22599 | 1.71746 | 225.56791 | 0.050347 | 9 | 52.632 |
| -0.79811 | -1.55517 | 1.74889 | 242.86822 | 0.051263 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 105.26019 | | | | | 0 | |
| -3.98134 | -4.85301 | 6.03139 | 233.57407 | 0.951351 | 1 | 5.848 |
| -5.67819 | -2.81983 | 6.33982 | 206.40929 | 1.000000 | 2 | 11.696 |
| 1.78775 | -4.55243 | 4.89088 | 291.43994 | 0.771454 | 3 | 17.544 |
| -0.11620 | 1.93755 | 1.94103 | 93.43228 | 0.306165 | 4 | 23.392 |
| 0.01860 | -0.04414 | 0.04790 | 292.84692 | 0.007555 | 5 | 29.240 |
| -0.40872 | 0.30278 | 0.50865 | 143.46854 | 0.080232 | 6 | 35.088 |
| -0.26079 | -0.32585 | 0.41736 | 231.32797 | 0.065832 | 7 | 40.936 |
| -0.32532 | -0.17922 | 0.37142 | 208.85068 | 0.058586 | 8 | 46.784 |
| -0.29688 | -0.04327 | 0.30001 | 188.29214 | 0.04732 | 9 | 52.632 |
| -0.04981 | -0.13282 | 0.14186 | 249.44383 | 0.022375 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 55.01415 | | | | | 0 | |
| -3.73269 | 20.29944 | 20.63076 | 100.41936 | 1.000000 | 1 | 5.848 |
| -0.98488 | 0.99842 | 1.19757 | 120.38981 | 0.056005 | 2 | 11.696 |
| -1.36244 | -0.43066 | 1.43134 | 197.84665 | 0.069349 | 3 | 17.544 |
| 0.17048 | -0.37262 | 0.40977 | 294.58545 | 0.019853 | 4 | 23.392 |
| -1.94011 | 0.08438 | 1.94812 | 179.63696 | 0.094419 | 5 | 29.240 |
| 0.31384 | -1.98889 | 1.98586 | 279.09668 | 0.096176 | 6 | 35.088 |
| 0.18789 | -0.05187 | 0.19478 | 344.79224 | 0.009433 | 7 | 40.936 |
| -0.63626 | 0.55159 | 0.84287 | 139.07735 | 0.040798 | 8 | 46.784 |
| -0.58383 | -0.86957 | 1.08459 | 239.95123 | 0.048672 | 9 | 52.632 |
| -0.56981 | -1.84419 | 1.22488 | 242.27529 | 0.059342 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 93.98789 | | | | | 0 | |
| -0.28128 | -14.94914 | 14.95178 | 268.98188 | 1.000000 | 1 | 5.848 |
| -11.38978 | -3.83937 | 12.01948 | 198.62848 | 0.803882 | 2 | 11.696 |
| 3.78887 | -5.19583 | 6.39718 | 306.29663 | 0.427849 | 3 | 17.544 |
| -0.12147 | 1.88740 | 1.89131 | 93.68298 | 0.126494 | 4 | 23.392 |
| -0.14868 | -0.18428 | 0.18295 | 215.57338 | 0.012209 | 5 | 29.240 |
| 0.17795 | -0.27486 | 0.32694 | 302.93799 | 0.021848 | 6 | 35.088 |
| 0.45784 | 0.13587 | 0.47735 | 16.43788 | 0.031926 | 7 | 40.936 |
| 0.29874 | 0.27426 | 0.39989 | 43.37898 | 0.026732 | 8 | 46.784 |
| 0.17925 | 0.00882 | 0.17936 | 77.64330 | 0.011990 | 9 | 52.632 |
| 0.22992 | 1.20988 | 1.22992 | 79.39963 | 0.081992 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 221.78234 | | | | | 0 | |
| -1.89412 | 14.48881 | 14.23838 | 97.49472 | 1.000000 | 1 | 5.848 |
| 0.78743 | 1.69998 | 1.83492 | 64.61685 | 0.129004 | 2 | 11.696 |
| -2.97776 | 0.87874 | 2.97888 | 170.29471 | 0.181223 | 3 | 17.544 |
| -0.61898 | -1.88899 | 1.98125 | 251.79958 | 0.139227 | 4 | 23.392 |
| -0.49795 | 0.15918 | 0.45745 | 162.95354 | 0.032146 | 5 | 29.240 |
| 0.49973 | -1.94888 | 1.60749 | 288.61898 | 0.112962 | 6 | 35.088 |
| 0.44548 | -0.78828 | 0.85373 | 301.46484 | 0.059994 | 7 | 40.936 |
| -0.89828 | 0.53903 | 0.53387 | 93.25125 | 0.037517 | 8 | 46.784 |
| 1.6729 | -0.79294 | 1.08992 | 311.88322 | 0.076941 | 9 | 52.632 |
| -0.33176 | -0.74648 | 0.79817 | 293.85078 | 0.056089 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 505 CSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 63.09108 | | | | | 0 | |
| 0.23474 | -9.54313 | 9.54617 | 271.43311 | 0.730647 | 1 | 5.848 |
| -12.65105 | -3.26414 | 13.06536 | 194.46753 | 1.000000 | 2 | 11.696 |
| 4.63343 | -2.69141 | 5.35839 | 329.84888 | 0.410172 | 3 | 17.544 |
| -0.14284 | 2.06469 | 2.06963 | 93.95859 | 0.158406 | 4 | 23.392 |
| -0.29968 | 0.68049 | 0.74355 | 113.76794 | 0.056910 | 5 | 29.240 |
| -0.31107 | 0.33117 | 0.45431 | 133.21324 | 0.034772 | 6 | 35.088 |
| 0.16585 | 0.56749 | 0.59123 | 73.70877 | 0.045251 | 7 | 40.936 |
| 0.29407 | 0.50543 | 0.58475 | 59.80801 | 0.044756 | 8 | 46.784 |
| -0.12485 | 0.77540 | 0.78538 | 99.14696 | 0.060112 | 9 | 52.632 |
| -0.44685 | 0.82804 | 1.94095 | 118.35258 | 0.072019 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 505 CSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 80.33545 | | | | | 0 | |
| 0.61683 | 4.97772 | 5.01579 | 82.93591 | 1.000000 | 1 | 5.848 |
| -2.91439 | 1.13453 | 3.12743 | 158.72780 | 0.623516 | 2 | 11.696 |
| -0.18284 | -0.35477 | 0.39911 | 242.73468 | 0.079570 | 3 | 17.544 |
| -1.80770 | -1.80471 | 2.61149 | 226.19467 | 0.520654 | 4 | 23.392 |
| 0.05687 | 0.83163 | 0.83358 | 86.08780 | 0.166190 | 5 | 29.240 |
| 0.22062 | -0.40529 | 0.46145 | 298.56226 | 0.091999 | 6 | 35.088 |
| 0.13214 | -0.35200 | 0.37599 | 290.57886 | 0.074961 | 7 | 40.936 |
| 0.04062 | 0.10729 | 0.11472 | 69.24379 | 0.022872 | 8 | 46.784 |
| -0.24112 | -0.20667 | 0.34891 | 216.32172 | 0.069563 | 9 | 52.632 |
| -0.44103 | -0.56551 | 0.71715 | 232.04974 | 0.142979 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 505 CSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 62.27272 | | | | | 0 | |
| 1.36998 | -12.83506 | 12.90797 | 276.09253 | 0.765584 | 1 | 5.848 |
| -16.60393 | -2.92913 | 16.86029 | 190.00473 | 1.000000 | 2 | 11.696 |
| 5.04240 | -2.36282 | 5.58854 | 334.89258 | 0.331276 | 3 | 17.544 |
| 0.62395 | 2.61033 | 2.61044 | 89.47432 | 0.154828 | 4 | 23.392 |
| -0.52179 | 0.36604 | 0.63681 | 144.91245 | 0.037770 | 5 | 29.240 |
| -0.47598 | 0.13098 | 0.49365 | 164.62567 | 0.029279 | 6 | 35.088 |
| 0.34935 | 0.34970 | 0.49359 | 45.11050 | 0.029275 | 7 | 40.936 |
| 0.46589 | 0.36482 | 0.59173 | 38.06258 | 0.035096 | 8 | 46.784 |
| 0.71995 | 0.72021 | 0.72140 | 84.82568 | 0.042787 | 9 | 52.632 |
| -0.52468 | 0.85933 | 1.00599 | 121.43655 | 0.059666 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 505 CSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.82706 | | | | | 0 | |
| 3.26548 | 12.64591 | 13.06072 | 75.52106 | 1.000000 | 1 | 5.848 |
| -10.05970 | -0.63327 | 10.07961 | 183.60178 | 0.771750 | 2 | 11.696 |
| -0.04607 | -1.92160 | 1.92215 | 268.62573 | 0.147170 | 3 | 17.544 |
| -1.16495 | -0.03990 | 1.16564 | 181.96134 | 0.089247 | 4 | 23.392 |
| -0.86335 | 1.92607 | 2.11067 | 114.14464 | 0.161604 | 5 | 29.240 |
| -1.22577 | -0.74115 | 1.43242 | 211.15880 | 0.109674 | 6 | 35.088 |
| 0.12980 | 0.08652 | 0.15600 | 33.68452 | 0.011944 | 7 | 40.936 |
| -0.69632 | 1.37070 | 1.53743 | 116.93308 | 0.117714 | 8 | 46.784 |
| -0.90144 | 0.46319 | 1.01347 | 152.80463 | 0.077597 | 9 | 52.632 |
| -0.51031 | -0.20519 | 0.55001 | 201.90453 | 0.042112 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XM-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.66878 | | | | | 0 | |
| 1.24459 | -8.22957 | 8.32315 | 278.59985 | 0.912928 | 1 | 5.848 |
| -9.04173 | -1.16904 | 9.11699 | 187.36713 | 1.000000 | 2 | 11.696 |
| 2.30144 | -1.15566 | 2.57530 | 333.33667 | 0.282473 | 3 | 17.544 |
| 0.10155 | 1.34002 | 1.34386 | 85.66629 | 0.147401 | 4 | 23.392 |
| -0.31724 | -0.10801 | 0.33512 | 198.80220 | 0.036758 | 5 | 29.240 |
| -0.18469 | -0.15449 | 0.24079 | 219.91122 | 0.026411 | 6 | 35.088 |
| 0.31573 | 0.00598 | 0.31579 | 1.08531 | 0.034638 | 7 | 40.936 |
| 0.31590 | 0.07582 | 0.32487 | 13.49727 | 0.035634 | 8 | 46.784 |
| 0.16619 | 0.35311 | 0.39026 | 64.79668 | 0.042806 | 9 | 52.632 |
| -0.15642 | 0.49299 | 0.51721 | 107.60426 | 0.056730 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XM-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.67191 | | | | | 0 | |
| 2.50475 | 9.97321 | 10.28293 | 75.90181 | 1.000000 | 1 | 5.848 |
| -7.26775 | -1.05957 | 7.34459 | 188.29477 | 0.714250 | 2 | 11.696 |
| -0.31799 | -1.51139 | 1.54441 | 8.11841 | 0.150198 | 3 | 17.544 |
| -0.04707 | 0.84141 | 0.84272 | 3.20197 | 0.081954 | 4 | 23.392 |
| -0.82410 | 1.27806 | 1.52072 | 32.81398 | 0.147887 | 5 | 29.240 |
| -1.20299 | -0.59682 | 1.34290 | 206.38669 | 0.130595 | 6 | 35.088 |
| 0.11046 | 0.17497 | 0.20692 | 57.73569 | 0.020123 | 7 | 40.936 |
| -0.63975 | 1.26218 | 1.41506 | 116.87857 | 0.137612 | 8 | 46.784 |
| -0.98239 | 0.47039 | 0.68823 | 136.88396 | 0.066936 | 9 | 52.632 |
| -0.22283 | 0.10055 | 0.24446 | 155.71321 | 0.023774 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XM-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.24498 | | | | | 0 | |
| 0.10524 | -0.67333 | 0.68151 | 278.88354 | 0.930803 | 1 | 5.848 |
| -0.72670 | -0.08931 | 0.73217 | 187.00612 | 1.000000 | 2 | 11.696 |
| 0.18029 | -0.09111 | 0.20200 | 333.19141 | 0.275896 | 3 | 17.544 |
| 0.00910 | 0.10688 | 0.10726 | 85.13541 | 0.146503 | 4 | 23.392 |
| -0.02587 | -0.01183 | 0.02645 | 204.57457 | 0.036056 | 5 | 29.240 |
| -0.01417 | -0.01469 | 0.02041 | 226.04895 | 0.027878 | 6 | 35.088 |
| 0.02663 | -0.00144 | 0.02667 | 356.89722 | 0.036427 | 7 | 40.936 |
| 0.02607 | 0.00480 | 0.02646 | 10.44616 | 0.036133 | 8 | 46.784 |
| 0.01482 | 0.02788 | 0.03157 | 62.00545 | 0.043121 | 9 | 52.632 |
| -0.01132 | 0.03976 | 0.04134 | 105.88792 | 0.056458 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XM-51A SHIP 1002C TEST 505 OSC CTR 354 TEST COND 16 COMP RUN 66.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.68473 | | | | | 0 | |
| 0.20932 | 0.83353 | 0.85941 | 75.90317 | 1.000000 | 1 | 5.848 |
| -0.60390 | -0.09289 | 0.61100 | 188.74461 | 0.710950 | 2 | 11.696 |
| -0.02824 | -0.12654 | 0.12965 | 257.41699 | 0.150861 | 3 | 17.544 |
| 0.00233 | 0.07690 | 0.07694 | 88.26788 | 0.089523 | 4 | 23.392 |
| -0.07001 | 0.10527 | 0.12642 | 123.62479 | 0.147104 | 5 | 29.240 |
| -0.10245 | -0.04989 | 0.11395 | 205.96481 | 0.132588 | 6 | 35.088 |
| 0.00924 | 0.01332 | 0.01806 | 59.24620 | 0.021015 | 7 | 40.936 |
| -0.09422 | 0.10689 | 0.11985 | 116.89857 | 0.139460 | 8 | 46.784 |
| -0.04072 | 0.04021 | 0.05723 | 135.36569 | 0.066591 | 9 | 52.632 |
| -0.01735 | 0.01034 | 0.02020 | 149.21646 | 0.023505 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XM-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.46719 | | | | | 0 | |
| 0.11975 | 0.06137 | 0.13456 | 27.13469 | 0.719091 | 1 | 5.952 |
| 0.17401 | 0.06981 | 0.18712 | 21.57631 | 1.000000 | 2 | 11.905 |
| -0.05768 | 0.02361 | 0.06233 | 157.73541 | 0.333078 | 3 | 17.857 |
| 0.05591 | 0.02746 | 0.06229 | 26.15749 | 0.332881 | 4 | 23.810 |
| -0.04443 | -0.00197 | 0.04447 | 182.54471 | 0.237653 | 5 | 29.762 |
| -0.02532 | -0.00448 | 0.02571 | 190.04085 | 0.137402 | 6 | 35.714 |
| -0.02268 | 0.01435 | 0.02684 | 147.68608 | 0.143442 | 7 | 41.667 |
| -0.02758 | -0.00143 | 0.02761 | 182.96969 | 0.147565 | 8 | 47.619 |
| -0.01756 | -0.01674 | 0.01836 | 245.74788 | 0.098124 | 9 | 53.571 |
| -0.00320 | -0.00917 | 0.00971 | 250.73982 | 0.051885 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XM-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.73410 | | | | | 0 | |
| 0.46540 | 0.25050 | 0.52853 | 28.29141 | 1.000000 | 1 | 5.952 |
| 0.04067 | -0.05296 | 0.06678 | 307.52173 | 0.126350 | 2 | 11.905 |
| -0.00173 | -0.02347 | 0.02353 | 265.79517 | 0.044524 | 3 | 17.857 |
| -0.11259 | -0.03407 | 0.11764 | 196.83449 | 0.222570 | 4 | 23.810 |
| -0.06245 | 0.06455 | 0.08981 | 134.05020 | 0.169931 | 5 | 29.762 |
| 0.00722 | -0.03540 | 0.03547 | 273.59326 | 0.067105 | 6 | 35.714 |
| -0.03459 | -0.07136 | 0.07930 | 244.14209 | 0.150038 | 7 | 41.667 |
| 0.04540 | -0.03213 | 0.05562 | 324.71582 | 0.105232 | 8 | 47.619 |
| -0.03591 | -0.03772 | 0.05208 | 226.40283 | 0.098539 | 9 | 53.571 |
| -0.00321 | -0.05075 | 0.05085 | 266.38647 | 0.096218 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XM-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.43257 | | | | | 0 | |
| 0.62246 | 0.30556 | 0.69341 | 26.14609 | 0.789998 | 1 | 5.952 |
| 0.84369 | 0.31489 | 0.90034 | 20.46690 | 1.000000 | 2 | 11.905 |
| -0.29303 | 0.09387 | 0.30770 | 162.23758 | 0.341681 | 3 | 17.857 |
| 0.28126 | 0.12215 | 0.30664 | 23.47562 | 0.340512 | 4 | 23.810 |
| -0.20798 | -0.01672 | 0.20865 | 184.59756 | 0.231694 | 5 | 29.762 |
| -0.11078 | -0.02544 | 0.11364 | 192.93739 | 0.126191 | 6 | 35.714 |
| -0.10622 | 0.06550 | 0.12531 | 147.95024 | 0.139155 | 7 | 41.667 |
| -0.12926 | -0.00767 | 0.12949 | 183.39362 | 0.143793 | 8 | 47.619 |
| -0.03698 | -0.07654 | 0.08501 | 244.21080 | 0.094397 | 9 | 53.571 |
| -0.01280 | -0.04210 | 0.04400 | 253.08902 | 0.048860 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XM-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.16533 | | | | | 0 | |
| 2.14635 | 1.16465 | 2.44197 | 28.48512 | 1.000000 | 1 | 5.952 |
| 0.19690 | -0.25918 | 0.32549 | 307.22437 | 0.133288 | 2 | 11.905 |
| -0.02530 | -0.10547 | 0.10846 | 256.51123 | 0.044416 | 3 | 17.857 |
| -0.53647 | -0.15335 | 0.55796 | 195.95267 | 0.228486 | 4 | 23.810 |
| -0.28703 | 0.30804 | 0.41958 | 133.16431 | 0.171819 | 5 | 29.762 |
| 0.01297 | -0.16300 | 0.16351 | 274.55103 | 0.066959 | 6 | 35.71- |
| -0.16994 | -0.33657 | 0.37704 | 243.21005 | 0.154399 | 7 | 41.667 |
| 0.20789 | -0.15280 | 0.25800 | 323.68384 | [illegible]5852 | 8 | 47.619 |
| -0.16736 | -0.17058 | 0.24233 | 226.37628 | 234 | 9 | 53.571 |
| -0.01197 | -0.23753 | 0.23783 | 267.11426 | 0.[illegible]393 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.99643 | | | | | C | |
| 1.73619 | 0.79638 | 1.91017 | 24.64050 | 0.862823 | 1 | 5.952 |
| 2.10015 | 0.70023 | 2.21391 | 18.43975 | 1.000000 | 2 | 11.905 |
| -0.78905 | 0.14167 | 0.80167 | 169.82149 | 0.362127 | 3 | 17.857 |
| 0.74553 | 0.75507 | 0.74796 | 18.88747 | 0.355929 | 4 | 23.810 |
| -0.48457 | -0.07355 | 0.49012 | 188.63065 | 0.221393 | 5 | 29.762 |
| -0.22217 | -0.07989 | 0.23610 | 199.77835 | 0.106650 | 6 | 35.714 |
| -0.24757 | 0.15182 | 0.29041 | 148.48138 | 0.131183 | 7 | 41.667 |
| -0.30196 | -0.02235 | 0.30279 | 184.23325 | 0.136774 | 8 | 47.619 |
| -0.09342 | -0.16989 | 0.19412 | 241.06516 | 0.087688 | 9 | 53.571 |
| -0.01969 | -0.09435 | 0.09638 | 258.21338 | 0.043535 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.24356 | | | | | C | |
| 4.85122 | 2.67615 | 5.54040 | 28.88313 | 1.000000 | 1 | 5.952 |
| 0.40876 | -0.65579 | 0.81789 | 306.69678 | 0.147623 | 2 | 11.905 |
| -0.13852 | -0.22936 | 0.26453 | 238.42374 | 0.047745 | 3 | 17.857 |
| -1.29326 | -0.32891 | 1.33443 | 194.26938 | 0.240854 | 4 | 23.810 |
| -0.44425 | 0.79087 | 0.97428 | 131.39577 | 0.175850 | 5 | 29.762 |
| 0.04211 | -0.36719 | 0.36960 | 276.54175 | 0.066709 | 6 | 35.714 |
| -0.43303 | -0.79979 | 0.90593 | 241.44547 | 0.163513 | 7 | 41.667 |
| 0.46287 | -0.38707 | 0.59075 | 321.58472 | 0.106627 | 8 | 47.619 |
| -0.37864 | -0.41146 | 0.55781 | 227.53017 | 0.100681 | 9 | 53.571 |
| -0.01389 | -0.55312 | 0.55329 | 268.56104 | 0.099865 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 50
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 23.12564 | | | | | C | |
| 5.32958 | 2.15355 | 5.74823 | 22.00239 | 1.000000 | 1 | 5.952 |
| 4.78748 | 0.89715 | 4.87081 | 10.61381 | 0.847359 | 2 | 11.905 |
| -2.32267 | -0.45812 | 2.36741 | 191.15764 | 0.411851 | 3 | 17.857 |
| 2.16901 | 0.16905 | 2.17559 | 4.45652 | 0.378479 | 4 | 23.810 |
| -0.82850 | -0.49711 | 0.94623 | 208.88693 | 0.164613 | 5 | 29.762 |
| -0.04460 | -0.33084 | 0.33384 | 267.32153 | 0.058076 | 6 | 35.714 |
| -0.43906 | 0.23107 | 0.49526 | 152.18957 | 0.086159 | 7 | 41.667 |
| -0.54082 | -0.07205 | 0.54559 | 187.58869 | 0.094915 | 8 | 47.619 |
| -0.23803 | -0.19363 | 0.30684 | 219.12709 | 0.053379 | 9 | 53.571 |
| 0.06953 | -0.11819 | 0.13711 | 300.46859 | 0.023853 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 50
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 35.03743 | | | | | C | |
| 6.83528 | 4.02359 | 7.93160 | 30.48318 | 1.000000 | 1 | 5.952 |
| 1.13690 | -1.61009 | 1.97103 | 305.22632 | 0.248503 | 2 | 11.905 |
| -0.96836 | -0.19022 | 0.98687 | 191.11325 | 0.124422 | 3 | 17.857 |
| -2.64533 | -0.31102 | 2.66355 | 186.70569 | 0.335815 | 4 | 23.810 |
| -0.86250 | 1.45940 | 1.69521 | 120.58799 | 0.213729 | 5 | 29.762 |
| 0.19472 | -0.51204 | 0.54782 | 290.82080 | 0.069068 | 6 | 35.714 |
| -1.10685 | -1.49106 | 1.85699 | 233.41254 | 0.234125 | 7 | 41.667 |
| 0.95240 | -0.74720 | 0.95355 | 308.40845 | 0.120221 | 8 | 47.619 |
| -0.94047 | -0.68097 | 0.86938 | 231.56178 | 0.109609 | 9 | 53.571 |
| 0.12075 | -0.99238 | 0.99601 | 277.22959 | 0.121035 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 34.63023 | | | | | 0 | |
| 7.67976 | 2.51139 | 8.07996 | 18.10845 | 1.000000 | 1 | 5.952 |
| 4.25666 | -0.55679 | 4.29292 | 352.54761 | 0.531304 | 2 | 11.905 |
| -3.04252 | -1.90288 | 3.58857 | 212.02303 | 0.444133 | 3 | 17.857 |
| 2.70399 | -0.64455 | 2.77975 | 346.59253 | 0.344030 | 4 | 23.810 |
| -0.20044 | -0.93329 | 0.95457 | 257.87866 | 0.118140 | 5 | 29.762 |
| 0.83366 | -0.56690 | 1.00815 | 325.78345 | 0.124771 | 6 | 35.714 |
| -0.12335 | -0.01675 | 0.12449 | 187.73154 | 0.015407 | 7 | 41.667 |
| -0.16810 | -0.11426 | 0.20326 | 214.20445 | 0.025156 | 8 | 47.619 |
| -0.24543 | 0.17150 | 0.29942 | 145.05576 | 0.037057 | 9 | 53.571 |
| 0.26459 | 0.06931 | 0.27326 | 14.47649 | 0.033820 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 13.72659 | | | | | 0 | |
| -1.93350 | -0.12608 | 1.93761 | 183.73097 | 0.905721 | 1 | 5.952 |
| 1.00392 | -1.61568 | 1.90218 | 301.85522 | 0.889158 | 2 | 11.905 |
| -2.09188 | 0.43943 | 2.13930 | 168.17387 | 1.000000 | 3 | 17.857 |
| -1.69161 | 0.57756 | 1.78749 | 161.14874 | 0.835549 | 4 | 23.810 |
| 0.37895 | 0.81945 | 0.90296 | 65.18317 | 0.422036 | 5 | 29.762 |
| 0.33941 | 0.17012 | 0.37966 | 26.62073 | 0.177467 | 6 | 35.714 |
| -1.16236 | -0.65727 | 1.33532 | 209.48640 | 0.624186 | 7 | 41.667 |
| -0.96056 | -0.45885 | 0.58357 | 231.84006 | 0.272784 | 8 | 47.619 |
| 0.11597 | -0.14079 | 0.18240 | 309.47778 | 0.085263 | 9 | 53.571 |
| 0.37369 | -0.23357 | 0.44068 | 327.99316 | 0.205992 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 54.81366 | | | | | 0 | |
| 14.45716 | 3.17564 | 14.80183 | 12.38885 | 1.000000 | 1 | 5.952 |
| 5.25541 | -1.73312 | 5.53381 | 341.76854 | 0.373860 | 2 | 11.905 |
| -4.31627 | -3.34830 | 5.46272 | 217.80208 | 0.369057 | 3 | 17.857 |
| 2.86546 | -1.30636 | 3.14919 | 335.49170 | 0.212757 | 4 | 23.810 |
| 0.12588 | -1.18495 | 1.19161 | 276.06356 | 0.080504 | 5 | 29.762 |
| 1.53024 | -0.81429 | 1.73340 | 331.98096 | 0.117107 | 6 | 35.714 |
| 0.21967 | -0.22440 | 0.31403 | 314.39014 | 0.021215 | 7 | 41.667 |
| 0.24840 | -0.29347 | 0.38448 | 31 .24487 | 0.025975 | 8 | 47.619 |
| -0.20080 | 0.19660 | 0.28102 | 135.60626 | 0.018985 | 9 | 53.571 |
| 0.31122 | 0.04984 | 0.31519 | 9.09874 | 0.021294 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.63443 | | | | | 0 | |
| -6.15304 | 0.32245 | 6.16148 | 177.00315 | 1.000000 | 1 | 5.952 |
| 0.97774 | -1.84623 | 2.04426 | 295.42749 | 0.331780 | 2 | 11.905 |
| -3.28811 | 0.81813 | 3.31078 | 165.69345 | 0.537335 | 3 | 17.857 |
| -1.10070 | 1.43629 | 1.80954 | 127.46494 | 0.293685 | 4 | 23.810 |
| 0.89026 | 0.05049 | 0.89169 | 3.24531 | 0.144721 | 5 | 29.762 |
| 0.12541 | 0.67233 | 0.74694 | 64.17311 | 0.121227 | 6 | 35.714 |
| -1.10345 | 0.04214 | 1.10425 | 177.81322 | 0.179219 | 7 | 41.667 |
| -1.03418 | -0.11958 | 1.04107 | 186.59541 | 0.168965 | 8 | 47.619 |
| 0.36705 | -0.18563 | 0.41132 | 333.17261 | 0.066756 | 9 | 53.571 |
| 0.40612 | 0.28477 | 0.49601 | 35.03825 | 0.080501 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 59.74098 | | | | | 0 | |
| 19.31865 | 2.68549 | 19.50439 | 7.91394 | 1.000000 | 1 | 5.952 |
| 5.76901 | -1.66063 | 6.00492 | 343.88823 | 0.307875 | 2 | 11.905 |
| -4.15726 | -3.17536 | 5.23122 | 217.37257 | 0.268207 | 3 | 17.857 |
| 1.28220 | -1.19130 | 1.75021 | 317.10445 | 0.089734 | 4 | 23.810 |
| 0.02417 | -0.69779 | 0.69820 | 271.98364 | 0.035797 | 5 | 29.762 |
| 1.24899 | -0.66683 | 1.41585 | 331.90234 | 0.072591 | 6 | 35.714 |
| 0.46722 | -0.22573 | 0.51892 | 334.20850 | 0.026605 | 7 | 41.667 |
| 0.56415 | -0.46132 | 0.72875 | 320.72632 | 0.037363 | 8 | 47.619 |
| -0.03276 | -0.27074 | 0.27272 | 263.10010 | 0.013982 | 9 | 53.571 |
| 0.04784 | -0.19941 | 0.20469 | 283.53101 | 0.010684 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.03994 | | | | | 0 | |
| -2.39456 | 5.68443 | 6.16820 | 112.94329 | 1.000000 | 1 | 5.952 |
| 0.44445 | -1.50829 | 1.54712 | 282.86401 | 0.250871 | 2 | 11.905 |
| -2.84528 | 0.45173 | 2.88165 | 169.72456 | 0.468801 | 3 | 17.857 |
| -0.45281 | 1.50188 | 1.56866 | 106.77758 | 0.254314 | 4 | 23.810 |
| 0.24237 | -0.86081 | 0.87505 | 286.07959 | 0.141844 | 5 | 29.762 |
| -0.09983 | 0.58362 | 0.58370 | 90.98506 | 0.094631 | 6 | 35.714 |
| -0.45965 | 0.47835 | 0.66340 | 133.85793 | 0.107552 | 7 | 41.667 |
| -0.84499 | 0.26825 | 0.88655 | 162.38762 | 0.143729 | 8 | 47.619 |
| -0.01278 | -0.78784 | 0.78793 | 269.10693 | 0.127741 | 9 | 53.571 |
| 0.00530 | 0.38810 | 0.38814 | 89.21745 | 0.062926 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 49.90396 | | | | | 0 | |
| 17.69475 | 1.73857 | 17.77994 | 5.61149 | 1.000000 | 1 | 5.952 |
| 5.13884 | -1.05144 | 5.24531 | 348.43604 | 0.295013 | 2 | 11.905 |
| -3.03844 | -2.24806 | 3.77967 | 216.49464 | 0.212590 | 3 | 17.857 |
| 0.91571 | -0.84637 | 0.84651 | 271.06323 | 0.047611 | 4 | 23.810 |
| -0.09288 | -0.33089 | 0.34368 | 254.32078 | 0.019330 | 5 | 29.762 |
| 0.69246 | -0.17981 | 0.78978 | 331.25513 | 0.044420 | 6 | 35.714 |
| 0.47645 | -0.08995 | 0.48469 | 349.42505 | 0.027260 | 7 | 41.667 |
| 0.57822 | -0.41742 | 0.71314 | 324.17477 | 0.040109 | 8 | 47.619 |
| 0.01663 | -0.53008 | 0.53134 | 273.95312 | 0.029884 | 9 | 53.571 |
| -0.12536 | -0.27446 | 0.30173 | 245.45129 | 0.016970 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.57465 | | | | | 0 | |
| 0.53503 | 7.59256 | 7.61139 | 85.96907 | 1.000000 | 1 | 5.952 |
| -0.07503 | -1.01159 | 1.01437 | 265.75781 | 0.133269 | 2 | 11.905 |
| -2.00917 | 0.17400 | 2.01669 | 175.05034 | 0.264957 | 3 | 17.857 |
| -0.02480 | 1.06098 | 1.06127 | 91.33908 | 0.139432 | 4 | 23.810 |
| -0.10847 | -1.13093 | 1.13617 | 264.52100 | 0.149266 | 5 | 29.762 |
| -0.70425 | 0.27911 | 0.34505 | 126.29404 | 0.045334 | 6 | 35.714 |
| -0.04011 | 0.49901 | 0.49983 | 94.60417 | 0.065642 | 7 | 41.667 |
| -0.42946 | 0.35042 | 0.55428 | 140.78703 | 0.072822 | 8 | 47.619 |
| -0.25443 | -0.98619 | 0.99912 | 255.24709 | 0.131267 | 9 | 53.571 |
| -0.24141 | 0.27468 | 0.36569 | 131.31107 | 0.048045 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 57.44175 | | | | | 0 | |
| 21.19641 | 1.77865 | 21.27090 | 4.79661 | 1.000000 | 1 | 5.952 |
| 5.94028 | -0.54788 | 5.96549 | 354.73022 | 0.280453 | 2 | 11.905 |
| -2.57170 | -2.48226 | 3.57425 | 223.98615 | 0.168035 | 3 | 17.857 |
| -0.66072 | -0.84696 | 1.28076 | 221.39911 | 0.060212 | 4 | 23.810 |
| -0.00383 | -0.45034 | 0.45035 | 269.53760 | 0.021172 | 5 | 29.762 |
| 0.21329 | -0.29506 | 0.36408 | 305.46206 | 0.017116 | 6 | 35.714 |
| 0.79184 | 0.16471 | 0.80879 | 11.75026 | 0.038023 | 7 | 41.667 |
| 0.57299 | -0.35966 | 0.67651 | 327.88403 | 0.031805 | 8 | 47.619 |
| 0.02571 | -0.87049 | 0.87078 | 271.69165 | 0.040938 | 9 | 53.571 |
| -0.22282 | -0.30174 | 0.37510 | 233.55617 | 0.017634 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.42664 | | | | | 0 | |
| -0.01519 | 9.30519 | 9.30511 | 90.09358 | 1.000000 | 1 | 5.952 |
| -0.73057 | -0.85460 | 1.12431 | 229.47365 | 0.120827 | 2 | 11.905 |
| -2.10859 | -0.19857 | 2.11700 | 185.11023 | 0.227509 | 3 | 17.857 |
| 0.09087 | 1.10281 | 1.10654 | 85.28960 | 0.118918 | 4 | 23.810 |
| 0.37590 | -1.64148 | 1.68395 | 282.99526 | 0.180979 | 5 | 29.762 |
| -0.39295 | -0.11470 | 0.40848 | 196.30717 | 0.043899 | 6 | 35.714 |
| 0.10486 | 0.59875 | 0.60786 | 90.06664 | 0.065326 | 7 | 41.667 |
| -0.35297 | 0.32031 | 0.47684 | 137.77751 | 0.051223 | 8 | 47.619 |
| -0.21169 | -1.28226 | 1.29961 | 260.62545 | 0.139666 | 9 | 53.571 |
| -0.48494 | 0.25805 | 0.54932 | 151.98129 | 0.059034 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 141.93933 | | | | | 0 | |
| 50.07939 | 1.33874 | 50.14055 | 3.81425 | 1.000000 | 1 | 5.952 |
| 15.59774 | 0.51779 | 15.60833 | 1.90098 | 0.310942 | 2 | 11.905 |
| -3.73479 | -5.54039 | 6.68165 | 236.01591 | 0.133126 | 3 | 17.857 |
| -4.20518 | -2.13861 | 4.71775 | 206.95431 | 0.093997 | 4 | 23.810 |
| 0.28500 | -1.98875 | 2.00833 | 277.58984 | 0.039974 | 5 | 29.762 |
| 0.88347 | -0.16879 | 0.89907 | 190.69102 | 0.017913 | 6 | 35.714 |
| 2.27603 | 1.94311 | 2.99583 | 30.65715 | 0.059716 | 7 | 41.667 |
| 1.06708 | -0.92711 | 1.11609 | 342.95752 | 0.022237 | 8 | 47.619 |
| -0.22934 | -2.57151 | 2.58177 | 264.89014 | 0.051439 | 9 | 53.571 |
| -0.59370 | -0.34969 | 0.68852 | 210.42590 | 0.013719 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.32419 | | | | | 0 | |
| -5.90948 | 19.66393 | 20.53284 | 106.72815 | 1.000000 | 1 | 5.952 |
| -3.26715 | -1.55592 | 3.61872 | 205.46523 | 0.176241 | 2 | 11.905 |
| -1.18926 | -1.12294 | 5.30326 | 192.20618 | 0.258574 | 3 | 17.857 |
| 0.78963 | 1.94453 | 2.09545 | 66.82448 | 0.097719 | 4 | 23.810 |
| 3.27534 | -4.55853 | 5.61320 | 305.69751 | 0.273377 | 5 | 29.762 |
| -1.11263 | -1.52453 | 1.88736 | 233.87738 | 0.091919 | 6 | 35.714 |
| 0.10740 | 1.09320 | 1.09846 | 84.38872 | 0.053498 | 7 | 41.667 |
| -0.34595 | 0.17519 | 0.38777 | 153.14369 | 0.018886 | 8 | 47.619 |
| -0.03340 | -2.88067 | 2.88087 | 269.33569 | 0.140305 | 9 | 53.571 |
| -1.42311 | 0.35752 | 1.46734 | 165.89781 | 0.071463 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 116.23561 | | | | | C | |
| 34.96359 | 1.18635 | 34.98262 | 1.83828 | 1.000000 | 1 | 5.952 |
| 17.88412 | -2.50265 | 18.05836 | 352.03394 | 0.448293 | 2 | 11.905 |
| -6.94803 | -0.23772 | 6.95209 | 181.95451 | 0.187983 | 3 | 17.857 |
| 0.36816 | -4.18426 | 4.20042 | 275.02832 | 0.113578 | 4 | 23.810 |
| -2.60833 | -1.77202 | 3.15333 | 214.19098 | 0.085265 | 5 | 29.762 |
| 1.92523 | 1.30028 | 2.32319 | 34.03464 | 0.062818 | 6 | 35.714 |
| -0.57659 | -0.16650 | 0.60207 | 196.09457 | 0.016280 | 7 | 41.667 |
| 1.95855 | 0.26498 | 1.97734 | 8.11405 | 0.050763 | 8 | 47.619 |
| -1.10386 | -1.03738 | 1.51482 | 223.22171 | 0.040960 | 9 | 53.571 |
| 0.14870 | -0.36712 | 0.41277 | 297.20312 | 0.011161 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.61255 | | | | | C | |
| 8.82075 | 16.71326 | 16.73338 | 87.18855 | 1.000000 | 1 | 5.952 |
| -1.90549 | -8.57951 | 8.78886 | 257.47827 | 0.525229 | 2 | 11.905 |
| -6.55388 | 8.01758 | 10.35544 | 129.26392 | 0.618849 | 3 | 17.857 |
| 8.84598 | -5.64449 | 8.47286 | 320.49438 | 0.530249 | 4 | 23.810 |
| -2.21170 | -2.82870 | 3.00121 | 222.52887 | 0.179355 | 5 | 29.762 |
| 1.45663 | 1.78741 | 1.94402 | 41.47116 | 0.116176 | 6 | 35.714 |
| -1.59170 | -2.47285 | 2.94084 | 237.23177 | 0.175747 | 7 | 41.667 |
| 2.81891 | 1.37949 | 2.96002 | 27.77753 | 0.176893 | 8 | 47.619 |
| -2.47614 | -1.29364 | 2.79370 | 207.58443 | 0.166954 | 9 | 53.571 |
| 0.03795 | 0.00087 | 0.03796 | 1.51847 | 0.001970 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 150.35910 | | | | | C | |
| 50.25721 | -3.65571 | 50.47128 | 353.10937 | 0.886569 | 1 | 5.952 |
| 33.21860 | -8.82130 | 34.36990 | 345.12817 | 1.000000 | 2 | 11.905 |
| -17.40442 | 6.34651 | 18.52542 | 159.96565 | 0.539001 | 3 | 17.857 |
| 7.70331 | -8.61947 | 11.56011 | 311.78735 | 0.336344 | 4 | 23.810 |
| -7.41232 | -2.29735 | 7.76017 | 197.22012 | 0.225784 | 5 | 29.762 |
| 8.14751 | 3.38949 | 8.82443 | 22.58804 | 0.256749 | 6 | 35.714 |
| -5.78551 | -2.04020 | 6.13470 | 199.47746 | 0.178544 | 7 | 41.667 |
| 4.60410 | 0.02027 | 4.60414 | 0.25229 | 0.133958 | 8 | 47.619 |
| -2.31611 | 0.63933 | 2.40273 | 164.56853 | 0.069908 | 9 | 53.571 |
| 0.71165 | -0.09744 | 0.71763 | 352.59570 | 0.020880 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.33522 | | | | | C | |
| 14.01816 | 20.93492 | 27.62108 | 49.28223 | 1.000000 | 1 | 5.952 |
| 3.33347 | -17.86779 | 18.17606 | 280.56763 | 0.658050 | 2 | 11.905 |
| -11.11764 | 19.31310 | 22.28445 | 119.92708 | 0.806792 | 3 | 17.857 |
| 15.42013 | -14.98066 | 21.22205 | 316.60278 | 0.768328 | 4 | 23.810 |
| -10.03088 | 0.20627 | 10.03300 | 178.82195 | 0.363237 | 5 | 29.762 |
| 4.46684 | 5.76427 | 7.29231 | 52.22842 | 0.264012 | 6 | 35.714 |
| -4.12945 | -6.71127 | 7.87522 | 238.49171 | 0.285116 | 7 | 41.667 |
| 6.87828 | 2.83052 | 7.43784 | 22.38812 | 0.269281 | 8 | 47.619 |
| -6.79480 | 1.33435 | 6.88533 | 168.02561 | 0.249278 | 9 | 53.571 |
| 2.29351 | -0.63583 | 2.38001 | 344.50488 | 0.086167 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 131.25732 | | | | | 0 | |
| -13.42885 | -12.94135 | 18.64972 | 223.94090 | 0.679747 | 1 | 5.952 |
| 29.51788 | 2.39176 | 29.61461 | 4.63241 | 1.000000 | 2 | 11.905 |
| -6.92208 | -7.93151 | 6.96867 | 204.87688 | 0.235312 | 3 | 17.857 |
| -3.10540 | -0.10806 | 3.10728 | 181.99290 | 0.104924 | 4 | 23.810 |
| 2.53005 | -4.24722 | 4.94369 | 300.78198 | 0.166934 | 5 | 29.762 |
| 1.66865 | -0.43891 | 1.75351 | 342.10156 | 0.059211 | 6 | 35.714 |
| -1.09637 | 5.22691 | 6.07520 | 120.64212 | 0.205142 | 7 | 41.667 |
| 3.03806 | -3.31762 | 4.49849 | 312.48145 | 0.151901 | 8 | 47.619 |
| 0.82360 | -2.00997 | 2.17216 | 292.28149 | 0.073348 | 9 | 53.571 |
| -3.25539 | 3.61471 | 4.86454 | 132.00610 | 0.164261 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.88948 | | | | | 0 | |
| 11.34728 | -4.40877 | 12.17366 | 338.76709 | 0.479483 | 1 | 5.952 |
| 13.10480 | 20.97925 | 24.73589 | 58.00873 | 0.974271 | 2 | 11.905 |
| -1.86527 | -25.32053 | 25.38913 | 265.78862 | 1.000000 | 3 | 17.857 |
| -10.54906 | 15.32653 | 18.60605 | 124.53920 | 0.732835 | 4 | 23.810 |
| 13.75915 | -4.36746 | 14.43568 | 342.38940 | 0.568577 | 5 | 29.762 |
| -6.25860 | -5.32888 | 8.21840 | 220.42177 | 0.323697 | 6 | 35.714 |
| 1.11499 | 6.93733 | 7.02636 | 80.86926 | 0.276747 | 7 | 41.667 |
| -2.39762 | -6.00065 | 6.46192 | 248.22025 | 0.254515 | 8 | 47.619 |
| 2.71788 | 5.08496 | 5.76573 | 61.87572 | 0.227096 | 9 | 53.571 |
| -0.16251 | -1.68619 | 1.69400 | 264.49487 | 0.066721 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 171.38010 | | | | | 0 | |
| -44.22029 | -20.06102 | 48.55798 | 204.40193 | 1.000000 | 1 | 5.952 |
| 16.66577 | -3.66340 | 17.06364 | 347.60254 | 0.351408 | 2 | 11.905 |
| 4.89468 | 1.82147 | 5.22260 | 20.41191 | 0.107554 | 3 | 17.857 |
| -4.43703 | 0.04383 | 4.43725 | 179.43402 | 0.091380 | 4 | 23.810 |
| 6.94379 | -7.76433 | 7.32538 | 277.40234 | 0.150858 | 5 | 29.762 |
| 1.89616 | 2.70999 | 3.28472 | 55.59148 | 0.067645 | 6 | 35.714 |
| 0.38405 | 4.38863 | 4.40575 | 84.94695 | 0.090732 | 7 | 41.667 |
| -0.91806 | -3.61464 | 3.70605 | 257.24756 | 0.076322 | 8 | 47.619 |
| 2.01719 | -3.23101 | 3.80900 | 301.97729 | 0.078442 | 9 | 53.571 |
| -0.88661 | 2.92637 | 3.05773 | 106.85541 | 0.062971 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 88.49977 | | | | | 0 | |
| -29.10425 | 7.01685 | 29.93816 | 166.44502 | 1.000000 | 1 | 5.952 |
| 11.41941 | 4.86583 | 12.41287 | 23.07892 | 0.414617 | 2 | 11.905 |
| 8.74567 | -9.06877 | 12.59878 | 313.96094 | 0.420827 | 3 | 17.857 |
| -9.66406 | 7.07359 | 11.97622 | 143.79794 | 0.400032 | 4 | 23.810 |
| 5.00566 | -7.92202 | 9.37097 | 302.28735 | 0.313011 | 5 | 29.762 |
| -2.64016 | 3.97663 | 4.45403 | 124.82793 | 0.148774 | 6 | 35.714 |
| 5.76645 | 2.58249 | 6.31832 | 24.12509 | 0.211046 | 7 | 41.667 |
| -7.18283 | -3.46996 | 10.36308 | 226.12760 | 0.346149 | 8 | 47.619 |
| 2.61470 | 3.67695 | 4.51183 | 54.58315 | 0.150705 | 9 | 53.571 |
| 3.07928 | -0.62289 | 3.14164 | 348.56421 | 0.104938 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 95.72205 | | | | | 0 | |
| -28.83409 | -11.02426 | 30.86971 | 200.92357 | 1.000000 | 1 | 5.952 |
| 1.66586 | -6.37397 | 6.58806 | 284.64673 | 0.213415 | 2 | 11.905 |
| 5.75603 | 4.71054 | 7.43782 | 39.29773 | 0.240942 | 3 | 17.857 |
| -0.73977 | -1.22576 | 1.43169 | 238.88835 | 0.046379 | 4 | 23.810 |
| -1.96071 | -4.32555 | 4.74096 | 245.43597 | 0.153580 | 5 | 29.762 |
| 2.03053 | 3.88812 | 3.94999 | 59.06523 | 0.127957 | 6 | 35.714 |
| 1.30808 | 0.36417 | 1.35783 | 15.55709 | 0.043986 | 7 | 41.667 |
| -1.95288 | -1.24095 | 2.31380 | 212.43375 | 0.074954 | 8 | 47.619 |
| 0.98029 | -1.53163 | 1.81948 | 302.62036 | 0.058908 | 9 | 53.571 |
| 1.37045 | 0.40621 | 1.42939 | 16.51007 | 0.046304 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 72.18336 | | | | | 0 | |
| -30.85437 | 12.17683 | 33.17026 | 158.46310 | 1.000000 | 1 | 5.952 |
| 2.92662 | -11.62247 | 11.98523 | 284.13354 | 0.361375 | 2 | 11.905 |
| 7.60540 | 10.79521 | 13.20525 | 54.83466 | 0.398135 | 3 | 17.857 |
| 0.20542 | -5.54905 | 5.55286 | 272.11987 | 0.167405 | 4 | 23.810 |
| -5.83361 | -4.38892 | 7.30025 | 216.95599 | 0.220084 | 5 | 29.762 |
| 2.85384 | 8.03933 | 8.53084 | 70.45584 | 0.257183 | 6 | 35.714 |
| 3.95665 | -3.10840 | 5.03162 | 321.84615 | 0.151691 | 7 | 41.667 |
| -4.00571 | -2.64315 | 4.79916 | 213.41861 | 0.144683 | 8 | 47.619 |
| -0.40535 | 0.47470 | 0.62422 | 130.49451 | 0.018819 | 9 | 53.571 |
| 3.36259 | 0.36236 | 3.38426 | 6.48716 | 0.102027 | 10 | 59.524 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.71553 | | | | | 0 | |
| -2.37460 | -0.98839 | 2.53534 | 200.51195 | 1.000000 | 1 | 5.952 |
| 0.05370 | -0.55686 | 0.55944 | 275.50757 | 0.220658 | 2 | 11.905 |
| 0.49786 | 0.41641 | 0.64905 | 39.90896 | 0.256001 | 3 | 17.857 |
| -0.04372 | -0.11024 | 0.11863 | 248.37384 | 0.046789 | 4 | 23.810 |
| -0.18032 | -0.35192 | 0.39542 | 242.86992 | 0.155964 | 5 | 29.762 |
| 0.12722 | 0.24149 | 0.33924 | 59.39315 | 0.133804 | 6 | 35.714 |
| 0.11753 | 0.00895 | 0.11787 | 4.35610 | 0.046489 | 7 | 41.667 |
| -0.17341 | -0.09251 | 0.19654 | 208.07982 | 0.077522 | 8 | 47.619 |
| 0.07409 | -0.12120 | 0.14218 | 302.79277 | 0.056069 | 9 | 53.571 |
| 0.12924 | 0.02057 | 0.13086 | 9.045 | 0.051616 | 10 | 59.524 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 351 TEST COND 19 COMP RUN 60.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.05645 | | | | | 0 | |
| -2.64156 | 1.06362 | 2.84793 | 158.07025 | 1.000000 | 1 | 5.952 |
| 0.20143 | -1.07961 | 1.09823 | 280.56836 | 0.385625 | 2 | 11.905 |
| 0.64326 | 1.02765 | 1.21238 | 57.95540 | 0.425704 | 3 | 17.857 |
| 0.07022 | -0.54097 | 0.54551 | 277.33575 | 0.191546 | 4 | 23.810 |
| -0.55588 | -0.35444 | 0.65926 | 212.57245 | 0.231488 | 5 | 29.762 |
| 0.26959 | 0.70677 | 0.75644 | 69.12136 | 0.265611 | 6 | 35.714 |
| 0.32768 | -0.29556 | 0.44128 | 317.95070 | 0.154945 | 7 | 41.667 |
| -0.32466 | -0.19875 | 0.38066 | 211.47444 | 0.133663 | 8 | 47.619 |
| -0.05035 | 0.02233 | 0.05508 | 156.08282 | 0.019339 | 9 | 53.571 |
| 0.28772 | 0.03824 | 0.29026 | 7.57956 | 0.101919 | 10 | 59.524 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.76763 | | | | | 0 | |
| -0.21307 | 0.31422 | 0.37965 | 124.14056 | 1.000000 | 1 | 6.024 |
| 0.17753 | 0.09361 | 0.20069 | 27.80174 | 0.528623 | 2 | 12.048 |
| 0.01915 | 0.01405 | 0.02375 | 36.26714 | 0.062564 | 3 | 18.072 |
| 0.05049 | 0.07940 | 0.09062 | 53.62184 | 0.238799 | 4 | 24.096 |
| 0.02178 | 0.01479 | 0.01490 | 89.13454 | 0.039235 | 5 | 30.120 |
| 0.00712 | 0.04928 | 0.04979 | 81.78836 | 0.131159 | 6 | 36.145 |
| -0.00605 | 0.03521 | 0.03587 | 101.00757 | 0.094486 | 7 | 42.169 |
| -0.02685 | 0.00815 | 0.02806 | 163.12302 | 0.073915 | 8 | 48.193 |
| -0.00959 | 0.01107 | 0.01465 | 130.88589 | 0.038579 | 9 | 54.217 |
| -0.00063 | -0.00436 | 0.00967 | 288.81799 | 0.025471 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.82324 | | | | | 0 | |
| -0.28189 | 0.18790 | 0.33878 | 146.31368 | 1.000000 | 1 | 6.024 |
| 0.04735 | -0.14853 | 0.15589 | 287.68842 | 0.460192 | 2 | 12.048 |
| -0.00991 | -0.04561 | 0.04636 | 261.48747 | 0.136867 | 3 | 18.072 |
| 0.01223 | -0.04401 | 0.04567 | 285.525... | 0.134813 | 4 | 24.096 |
| -0.04127 | 0.13160 | 0.14516 | 114.96513 | 0.428468 | 5 | 30.120 |
| -0.00027 | 0.02614 | 0.09883 | 163.66612 | 0.27^994 | 6 | 36.145 |
| -0.04128 | -0.07778 | 0.08798 | 242.82243 | 0.259784 | 7 | 42.169 |
| -0.00409 | 0.03890 | 0.03127 | 111.29082 | 0.033261 | 8 | 48.193 |
| -0.03985 | -0.02715 | 0.04789 | 214.54172 | 0.141363 | 9 | 54.217 |
| 0.03421 | 0.01796 | 0.03863 | 27.78148 | 0.114039 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.82652 | | | | | 0 | |
| -1.06486 | 1.54915 | 1.88097 | 124.59421 | 1.000000 | 1 | 6.024 |
| 0.09000 | 0.44855 | 0.99280 | 26.59860 | 0.529139 | 2 | 12.048 |
| 0.04739 | 0.07867 | 0.12832 | 35.96488 | 0.063949 | 3 | 18.072 |
| 0.28687 | 0.38117 | 0.47786 | 53.02476 | 0.253622 | 4 | 24.096 |
| 0.00639 | 0.06789 | 0.06799 | 86.29834 | 0.036145 | 5 | 30.120 |
| 0.03372 | 0.23336 | 0.23578 | 81.77888 | 0.125291 | 6 | 36.145 |
| -0.03488 | 0.16281 | 0.16725 | 102.48934 | 0.088915 | 7 | 42.169 |
| -0.13681 | 0.03825 | 0.13114 | 164.68846 | 0.069720 | 8 | 48.193 |
| -0.04058 | 0.04888 | 0.04483 | 132.99784 | 0.023829 | 9 | 54.217 |
| -0.04027 | -0.08487 | 0.04733 | 211.78212 | 0.025169 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.70917 | | | | | 0 | |
| -1.27276 | 0.79772 | 1.50209 | 147.92215 | 1.000000 | 1 | 6.024 |
| 0.21864 | -0.65091 | 0.68625 | 288.39815 | 0.462186 | 2 | 12.048 |
| -0.04496 | -0.31994 | 0.31673 | 261.89862 | 0.212190 | 3 | 18.072 |
| 0.03615 | -0.20851 | 0.21162 | 279.89472 | 0.140887 | 4 | 24.096 |
| -0.29865 | 0.00977 | 0.47689 | 119.71466 | 0.000868 | 5 | 30.120 |
| -0.42191 | 0.11862 | 0.43827 | 164.29834 | 0.291775 | 6 | 36.145 |
| -0.18834 | -0.35777 | 0.40431 | 242.23668 | 0.269144 | 7 | 42.169 |
| -0.02648 | 0.05348 | 0.05967 | 116.34773 | 0.039724 | 8 | 48.193 |
| -0.19972 | -0.12480 | 0.22793 | 213.19952 | 0.151750 | 9 | 54.217 |
| 0.15942 | 0.08799 | 0.17989 | 29.43949 | 0.119190 | 10 | 60.241 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 11.36159 | | | | | 0 | |
| -2.80637 | 3.97059 | 4.86207 | 125.25362 | 1.000000 | 1 | 6.024 |
| 2.34595 | 1.07212 | 2.57932 | 24.56662 | 0.530499 | 2 | 12.048 |
| 0.26264 | 0.10726 | 0.33254 | 35.48836 | 0.066343 | 3 | 18.072 |
| 0.72867 | 0.93189 | 1.18299 | 51.97710 | 0.243302 | 4 | 24.096 |
| -0.00700 | 0.15164 | 0.15187 | 92.90829 | 0.031235 | 5 | 30.120 |
| 0.00842 | 0.53593 | 0.56172 | 81.76003 | 0.115530 | 6 | 36.145 |
| -0.18263 | 0.37341 | 0.38726 | 108.26871 | 0.079648 | 7 | 42.169 |
| -0.29709 | 0.04879 | 0.30095 | 136.09217 | 0.062730 | 8 | 48.193 |
| -0.10946 | 0.18019 | 0.14024 | 137.51750 | 0.028510 | 9 | 54.217 |
| -0.09123 | -0.07093 | 0.12190 | 220.10730 | 0.025071 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 40.04487 | | | | | 0 | |
| -8.74074 | 1.48093 | 3.12211 | 151.648168 | 1.000000 | 1 | 6.024 |
| 0.44884 | -1.36736 | 1.45432 | 288.[illegible]370 | 0.465813 | 2 | 12.048 |
| -0.00884 | -0.77810 | 0.78828 | 262.70149 | 0.249982 | 3 | 18.072 |
| -0.01388 | -0.49705 | 0.49713 | 268.48822 | 0.159208 | 4 | 24.096 |
| -0.71874 | 1.30187 | 1.50485 | 117.21881 | 0.481219 | 5 | 30.120 |
| -1.00104 | 0.22864 | 1.03434 | 168.51988 | 0.330898 | 6 | 36.145 |
| -0.41870 | -0.00098 | 0.00702 | 242.68618 | 0.298814 | 7 | 42.169 |
| -0.09284 | 0.14468 | 0.17289 | 123.44488 | 0.055884 | 8 | 48.193 |
| -0.47829 | -0.28884 | 0.84884 | 214.66211 | 0.179841 | 9 | 54.217 |
| 0.34987 | 0.22810 | 0.48991 | 32.97989 | 0.131292 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 98
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 37.43187 | | | | | 0 | |
| -7.87082 | 10.28196 | 12.94875 | 127.48434 | 1.000000 | 1 | 6.024 |
| 6.49186 | 2.13645 | 6.83267 | 18.21986 | 0.527748 | 2 | 12.048 |
| 0.75244 | 0.99898 | 0.99713 | 36.98772 | 0.077172 | 3 | 18.072 |
| 1.81467 | 2.03019 | 2.72998 | 48.26418 | 0.210521 | 4 | 24.096 |
| -0.28838 | 0.21757 | 0.29798 | 133.89998 | 0.023001 | 5 | 30.120 |
| 0.11899 | 1.07152 | 1.07184 | 89.63880 | 0.082750 | 6 | 36.145 |
| -0.39294 | 0.39982 | 0.66287 | 122.48888 | 0.051207 | 7 | 42.169 |
| -0.53997 | -0.08871 | 0.58948 | 188.48998 | 0.041429 | 8 | 48.193 |
| -0.21991 | 0.08847 | 0.28188 | 173.13837 | 0.017186 | 9 | 54.217 |
| -0.14681 | -0.34884 | 0.37949 | 247.01878 | 0.029038 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 98
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 66.42988 | | | | | 0 | |
| -2.83988 | -1.51232 | 2.99578 | 210.77657 | 1.000000 | 1 | 6.024 |
| 0.68899 | -0.64888 | 1.00241 | 321.41187 | 0.348296 | 2 | 12.048 |
| -0.14187 | -1.48888 | 1.48482 | 268.12789 | 0.563155 | 3 | 18.072 |
| -0.98894 | -0.88899 | 1.30888 | 224.47272 | 0.436898 | 4 | 24.096 |
| -1.88441 | 2.11668 | 2.83222 | 138.44813 | 0.998894 | 5 | 30.120 |
| -1.91881 | 0.27988 | 1.98888 | 171.84888 | 0.484784 | 6 | 36.145 |
| -0.81894 | -1.12815 | 1.28888 | 248.22784 | 0.417889 | 7 | 42.169 |
| -0.48881 | 0.42841 | 0.64887 | 138.98144 | 0.216723 | 8 | 48.193 |
| -1.87888 | -0.38798 | 1.14888 | 199.76689 | 0.387723 | 9 | 54.217 |
| 0.41894 | 0.58665 | 0.87758 | 52.99948 | 0.229178 | 10 | 60.241 |

TEXT NOT REPRODUCIBLE

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 55.42712 | | | | | 0 | |
| -9.53438 | 11.11571 | [illegible].6445/ | 130.6216. | 1.000000 | 1 | 6.024 |
| 7.90913 | 1.30172 | 8.01933 | 9.34622 | 0.347330 | 2 | 12.048 |
| 0.99975 | 0.49680 | 1.21042 | 39.14032 | 0.052053 | 3 | 18.072 |
| 1.86391 | 1.55717 | 2.42877 | 39.876346 | 0.105048 | 4 | 24.096 |
| -0.49811 | -0.87841 | 0.90425 | 180.044836 | 0.0784482 | 5 | 30.120 |
| 0.83345 | 0.59425 | 0.99525 | 80.54602 | 0.037919 | 6 | 36.145 |
| -0.52993 | -0.84477 | 0.99181 | 184.02941 | 0.036915 | 7 | 42.169 |
| -0.19742 | -0.33146 | 0.39010 | 239.59694 | 0.0386592 | 8 | 48.193 |
| -0.13194 | -0.33612 | 0.39922 | 248.45166 | 0.0384329 | 9 | 54.217 |
| -0.01302 | -0.50912 | 0.50928 | 269.65401 | 0.0402239 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.12405 | | | | | 0 | |
| 4.63810 | -0.82248 | 1C.[illegible]033 | 295.25244 | 1.000000 | 1 | 6.024 |
| -0.03343 | 3.93348 | 3.93362 | 90.48788 | 0.3822261 | 2 | 12.048 |
| 0.86398 | -1.28837 | 1.28811 | 273.73442 | 0.1128986 | 3 | 18.072 |
| -2.58779 | -0.51642 | 2.63882 | 191.28868 | 0.2428977 | 4 | 24.096 |
| -1.17991 | -2.16318 | 1.18821 | 187.98811 | 0.1888886 | 5 | 30.120 |
| -0.93126 | -0.35159 | 0.[illegible]942 | 200.68852 | 0.0916884 | 6 | 36.145 |
| 0.38091 | 0.37028 | 0.54324 | 44.28829 | 0.0528829 | 7 | 42.169 |
| -0.91748 | 0.59791 | 1.07389 | 148.61844 | 0.0988873 | 8 | 48.193 |
| -0.92918 | 0.14024 | 0.94189 | 170.87994 | 0.0868884 | 9 | 54.217 |
| -0.34944 | 0.54862 | 0.64384 | 122.89438 | 0.0592894 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 84.18265 | | | | | 0 | |
| -11.12994 | 12.28264 | 16.51604 | 132.36772 | 1.000000 | 1 | 6.024 |
| 11.85435 | 1.26676 | 11.12968 | 6.13044 | 0.6738811 | 2 | 12.048 |
| 1.61995 | 0.57333 | 1.73728 | 19.20944 | 0.1051187 | 3 | 18.072 |
| 2.13168 | 1.12985 | 2.40882 | 27.71878 | 0.1457994 | 4 | 24.096 |
| -0.48843 | -0.38348 | 0.61446 | 218.94184 | 0.0372214 | 5 | 30.120 |
| 0.41364 | 0.26857 | 0.54188 | 29.71884 | 0.0328894 | 6 | 36.145 |
| -0.68895 | -0.21164 | 0.72874 | 197.88888 | 0.0438839 | 7 | 42.169 |
| -0.83888 | -0.29851 | 0.38892 | 262.74812 | 0.0180828 | 8 | 48.193 |
| -0.85558 | -0.38259 | 0.38868 | 259.42476 | 0.0180889 | 9 | 54.217 |
| -0.84716 | -0.52793 | 0.93218 | 262.75824 | 0.0322222 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -31.57118 | | | | | 0 | |
| 7.67434 | -9.15175 | 11.94361 | 309.98193 | 1.000000 | 1 | 6.024 |
| -1.26192 | 5.44656 | 5.75602 | 100.87315 | 0.4811933 | 2 | 12.048 |
| 0.69758 | -1.84389 | 1.97148 | 290.72044 | 0.1648889 | 3 | 18.072 |
| -3.25389 | -0.39673 | 3.27719 | 186.95822 | 0.2744888 | 4 | 24.096 |
| -0.46574 | -1.54884 | 1.61252 | 253.42889 | 0.1348811 | 5 | 30.120 |
| -0.83578 | -0.78916 | 0.71134 | 208.38928 | 0.0595863 | 6 | 36.145 |
| 1.21881 | 1.34681 | 1.83878 | 48.29935 | 0.1512879 | 7 | 42.169 |
| -1.37315 | 0.95642 | 1.67952 | 145.13868 | 0.1481118 | 8 | 48.193 |
| -0.84988 | 0.65141 | 1.87917 | 142.98444 | 0.0878482 | 9 | 54.217 |
| -0.99161 | 0.91222 | 1.34684 | 137.37888 | 0.1127775 | 10 | 60.241 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| 85.46960 | | | | | | |
| -7.63055 | 7.92364 | 11.00042 | 133.92052 | 0.994391 | 1 | 6.024 |
| 10.95158 | 1.56245 | 11.06247 | 8.11951 | 1.000000 | 2 | 12.048 |
| 2.02955 | -0.11574 | 2.03284 | 354.73584 | 0.183760 | 3 | 18.072 |
| 1.69884 | 0.28014 | 1.72311 | 9.62642 | 0.155761 | 4 | 24.096 |
| 0.89970 | -0.59866 | 0.60493 | 279.48608 | 0.054684 | 5 | 30.120 |
| 1.25090 | 0.15005 | 1.25986 | 6.84007 | 0.113886 | 6 | 36.145 |
| -0.47380 | 0.20827 | 0.51736 | 156.27083 | 0.046785 | 7 | 42.169 |
| -0.05856 | 0.21203 | 0.21997 | 105.43980 | 0.019885 | 8 | 48.193 |
| 0.81589 | 0.24512 | 0.24563 | 16.29303 | 0.022204 | 9 | 54.217 |
| -0.27036 | 0.06975 | 0.27921 | 165.53368 | 0.025239 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| -21.46710 | | | | | | |
| 2.45738 | 5.34473 | 5.88259 | 65.30807 | 1.000000 | 1 | 6.024 |
| -3.69089 | 1.08439 | 3.85457 | 163.66060 | 0.655251 | 2 | 12.048 |
| 1.99914 | -2.46231 | 2.83206 | 299.60620 | 0.481431 | 3 | 18.072 |
| -1.37996 | -0.37230 | 1.42950 | 195.00037 | 0.242972 | 4 | 24.096 |
| 0.78222 | -1.20475 | 1.43641 | 302.99087 | 0.244181 | 5 | 30.120 |
| 0.58074 | -0.44430 | 0.75057 | 321.78087 | 0.127592 | 6 | 36.145 |
| 1.33454 | 1.04289 | 1.69370 | 38.00020 | 0.287917 | 7 | 42.169 |
| -1.13366 | 1.16042 | 1.62000 | 134.13486 | 0.276750 | 8 | 48.193 |
| -0.50150 | 0.74820 | 0.90072 | 123.83325 | 0.153117 | 9 | 54.217 |
| -0.96186 | 1.19526 | 1.53372 | 128.80130 | 0.260722 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| 64.43517 | | | | | | |
| -3.93329 | 3.58425 | 5.28283 | 138.44586 | 0.626865 | 1 | 6.024 |
| 8.31645 | 1.42792 | 8.43814 | 9.74257 | 1.000000 | 2 | 12.048 |
| 1.84439 | -0.52523 | 1.91889 | 344.28247 | 0.229777 | 3 | 18.072 |
| 1.11220 | -0.16950 | 1.12504 | 351.33447 | 0.133328 | 4 | 24.096 |
| 0.82082 | -0.78640 | 0.82224 | 300.78345 | 0.097444 | 5 | 30.120 |
| 1.41404 | 0.04280 | 1.41708 | 3.75487 | 0.167917 | 6 | 36.145 |
| -0.17758 | 0.42022 | 0.45620 | 112.98816 | 0.054064 | 7 | 42.169 |
| -0.05444 | 0.39881 | 0.39959 | 97.92961 | 0.046762 | 8 | 48.193 |
| 0.02965 | 0.43862 | 0.43962 | 86.13287 | 0.052099 | 9 | 54.217 |
| -0.29342 | 0.35018 | 0.45699 | 129.97955 | 0.054157 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| -0.47759 | | | | | | |
| -1.44951 | 12.40859 | 12.40582 | 96.66711 | 1.000000 | 1 | 6.024 |
| -3.64876 | -1.74466 | 4.03998 | 205.58546 | 0.323580 | 2 | 12.048 |
| 1.48856 | -2.09685 | 2.56622 | 305.23584 | 0.205544 | 3 | 18.072 |
| 0.06337 | -0.13723 | 0.15116 | 294.78516 | 0.012107 | 4 | 24.096 |
| 1.06845 | -0.64476 | 1.24835 | 328.81982 | 0.099748 | 5 | 30.120 |
| 0.03121 | -0.24953 | 0.69738 | 339.03394 | 0.055857 | 6 | 36.145 |
| 1.00836 | 0.49032 | 1.18252 | 24.18710 | 0.000307 | 7 | 42.169 |
| -0.60469 | 0.98126 | 1.15262 | 121.64325 | 0.092320 | 8 | 48.193 |
| -0.26737 | 0.56042 | 0.59434 | 114.99505 | 0.047604 | 9 | 54.217 |
| -0.00986 | 0.98404 | 1.15770 | 121.78871 | 0.092727 | 10 | 60.241 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 71.21457 | | | | | 0 | |
| -3.18333 | 2.07625 | 3.80038 | 146.88466 | 0.422632 | 1 | 6.024 |
| 8.78031 | 1.58915 | 8.92296 | 10.25891 | 1.000000 | 2 | 12.048 |
| 2.75242 | -0.87431 | 2.41515 | 338.78940 | 0.270779 | 3 | 18.072 |
| 1.14350 | -0.37224 | 1.20256 | 341.96851 | 0.134771 | 4 | 24.096 |
| 0.59815 | -1.28536 | 1.41646 | 294.84497 | 0.158763 | 5 | 30.120 |
| 1.72912 | 0.89548 | 1.73176 | 3.16053 | 0.194079 | 6 | 36.145 |
| 0.06081 | 0.54195 | 0.54535 | 83.59833 | 0.061118 | 7 | 42.169 |
| 0.05126 | 0.29888 | 0.30127 | 80.20357 | 0.033764 | 8 | 48.193 |
| 0.00041 | 0.37733 | 0.37733 | 89.93845 | 0.042287 | 9 | 54.217 |
| -0.24338 | 0.38333 | 0.45407 | 122.41138 | 0.050888 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -2.13081 | | | | | 0 | |
| -3.06362 | 16.82971 | 17.10628 | 100.31700 | 1.000000 | 1 | 6.024 |
| -3.93083 | -2.79349 | 4.82948 | 215.33807 | 0.282334 | 2 | 12.048 |
| 1.09788 | -1.68655 | 2.53098 | 318.37627 | 0.148424 | 3 | 18.072 |
| 0.68115 | 0.92668 | 0.86102 | 37.71164 | 0.050334 | 4 | 24.096 |
| 0.89452 | -0.99236 | 1.33682 | 312.03174 | 0.078181 | 5 | 30.120 |
| 0.66634 | -0.44898 | 0.80349 | 326.02734 | 0.046978 | 6 | 36.145 |
| 1.10403 | 0.10279 | 1.11006 | 9.49091 | 0.065018 | 7 | 42.169 |
| -0.19257 | 1.62646 | 1.64437 | 100.62529 | 0.061052 | 8 | 48.193 |
| -0.34223 | 0.38221 | 0.51303 | 131.84090 | 0.029991 | 9 | 54.217 |
| -0.39930 | 0.77031 | 0.86765 | 117.40028 | 0.050721 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 196.84768 | | | | | 0 | |
| -5.92326 | 0.84848 | 5.92340 | 179.60918 | 0.328466 | 1 | 6.024 |
| 18.20877 | 3.17888 | 18.48367 | 9.89488 | 1.000000 | 2 | 12.048 |
| 5.98818 | -2.67321 | 6.47791 | 335.62598 | 0.350445 | 3 | 18.072 |
| 2.63181 | -0.91017 | 2.78399 | 340.91748 | 0.150619 | 4 | 24.096 |
| 1.48975 | -4.89582 | 5.09475 | 286.86372 | 0.275635 | 5 | 30.120 |
| 3.96827 | 0.14185 | 3.97088 | 2.04726 | 0.214828 | 6 | 36.145 |
| 1.01568 | 1.81723 | 1.43749 | 45.84372 | 0.077771 | 7 | 42.169 |
| 0.68411 | -0.39124 | 0.69888 | 329.82544 | 0.037806 | 8 | 48.193 |
| -0.17456 | -0.17247 | 0.23177 | 221.13596 | 0.012539 | 9 | 54.217 |
| -0.82279 | 0.29944 | 0.38831 | 94.39141 | 0.016247 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.61453 | | | | | 0 | |
| -7.04627 | 36.14948 | 36.82979 | 101.02986 | 1.000000 | 1 | 6.024 |
| -6.86799 | -5.08204 | 8.54380 | 216.49994 | 0.231981 | 2 | 12.048 |
| 4.72859 | -0.83357 | 4.80146 | 350.00220 | 0.130369 | 3 | 18.072 |
| 1.49194 | 3.85381 | 4.33816 | 68.66670 | 0.117790 | 4 | 24.096 |
| 0.00131 | -3.73634 | 3.73634 | 270.02802 | 0.101449 | 5 | 30.120 |
| 0.74944 | -1.99271 | 2.12898 | 290.61868 | 0.057806 | 6 | 36.145 |
| 2.32878 | -0.43874 | 2.36841 | 349.48535 | 0.064898 | 7 | 42.169 |
| 1.24771 | 1.84953 | 2.23104 | 55.99593 | 0.060577 | 8 | 48.193 |
| -1.19260 | 0.07193 | 1.19477 | 176.54828 | 0.032448 | 9 | 54.217 |
| 0.01711 | 0.23965 | 0.24826 | 85.91524 | 0.006523 | 10 | 60.241 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 116.73001 | | | | | 0 | |
| -4.89434 | -6.92685 | 8.45945 | 234.96771 | 0.742243 | 1 | 6.024 |
| 11.20129 | 2.10379 | 11.39714 | 10.63718 | 1.000000 | 2 | 12.048 |
| 5.23182 | -2.62496 | 5.85241 | 333.39571 | 0.513505 | 3 | 18.072 |
| 1.77846 | -0.41388 | 1.82588 | 346.92783 | 0.160198 | 4 | 24.096 |
| 1.51353 | -4.02828 | 4.30816 | 290.59277 | 0.377565 | 5 | 30.120 |
| 2.91989 | -0.32232 | 2.93683 | 353.60007 | 0.257682 | 6 | 36.145 |
| 1.24582 | 0.47297 | 1.23886 | 22.44895 | 0.108699 | 7 | 42.169 |
| 0.42341 | -0.48027 | 0.58264 | 318.60913 | 0.051123 | 8 | 48.193 |
| -0.19249 | -0.78994 | 0.80413 | 259.06060 | 0.070535 | 9 | 54.217 |
| 0.13353 | -0.00001 | 0.13993 | 320.61011 | 0.014032 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -20.68349 | | | | | 0 | |
| -3.98817 | 20.99972 | 21.31949 | 100.94189 | 1.000000 | 1 | 6.024 |
| -1.71384 | -1.52832 | 2.29.98 | 221.72987 | 0.107699 | 2 | 12.048 |
| 2.29842 | -0.29944 | 2.30[illegible] | 359.82710 | 0.107933 | 3 | 18.072 |
| 0.88418 | 3.11947 | 3.23971 | 75.17295 | 0.151869 | 4 | 24.096 |
| -0.44940 | -0.08820 | 1.[illegible]7 | 243.87740 | 0.047237 | 5 | 30.120 |
| -0.98195 | -1.82448 | 1.98884 | 253.16889 | 0.093408 | 6 | 36.145 |
| 0.54881 | -0.84153 | 1.82148 | 302.49796 | 0.047919 | 7 | 42.169 |
| 1.73223 | 0.88126 | 1.94881 | 26.98448 | 0.091161 | 8 | 48.193 |
| -0.27619 | -0.83188 | 0.27709 | 108.42191 | 0.013038 | 9 | 54.217 |
| -0.03404 | -0.24773 | 0.25006 | 262.17529 | 0.011729 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 135.78484 | | | | | 0 | |
| -7.16814 | -18.99832 | 20.30184 | 249.32428 | 1.000000 | 1 | 6.024 |
| 7.57481 | 1.63542 | 7.74094 | 12.18330 | 0.381784 | 2 | 12.048 |
| 7.72784 | -3.64887 | 8.54999 | 334.72481 | 0.420844 | 3 | 18.072 |
| 1.90645 | 0.13853 | 1.64178 | 4.67420 | 0.078098 | 4 | 24.096 |
| 2.49423 | -3.76526 | 4.51644 | 308.52173 | 0.222465 | 5 | 30.120 |
| 3.32351 | -1.08879 | 3.48981 | 342.23122 | 0.171884 | 6 | 36.145 |
| 1.37284 | -0.84289 | 1.37381 | 350.21021 | 0.067684 | 7 | 42.169 |
| -0.13562 | 0.18179 | 0.22681 | 126.72394 | 0.011172 | 8 | 48.193 |
| -0.85758 | -1.05828 | 1.08677 | 244.87644 | 0.052853 | 9 | 54.217 |
| -0.02005 | -0.00804 | 0.02815 | 199.81813 | 0.000993 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1003C TEST 498 OSC CTR 494 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -63.78783 | | | | | 0 | |
| -2.38841 | 12.61685 | 12.83844 | 100.68523 | 1.000000 | 1 | 6.024 |
| 1.98889 | 0.94452 | 2.12727 | 26.33960 | 0.165693 | 2 | 12.048 |
| 0.54972 | -2.57973 | 2.63768 | 282.02930 | 0.205446 | 3 | 18.072 |
| -0.83810 | 0.90837 | 1.21983 | 133.05788 | 0.094781 | 4 | 24.096 |
| 0.85778 | 3.93959 | 4.02798 | 77.76427 | 0.313738 | 5 | 30.120 |
| -2.15896 | -1.26847 | 2.49811 | 210.40921 | 0.194421 | 6 | 36.145 |
| -1.77579 | -1.62226 | 2.04884 | 222.41[illegible]2 | 0.159344 | 7 | 42.169 |
| 1.79817 | 0.15484 | 1.79685 | 4.94951 | 0.139956 | 8 | 48.193 |
| 1.43235 | 0.79946 | 1.63887 | 29.13742 | 0.127729 | 9 | 54.217 |
| -0.00892 | 0.94115 | 0.87898 | 199.72815 | 0.068432 | 10 | 60.241 |

TEXT NOT REPRODUCIBLE

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1082C TEST 498 OSC CTR 4PP TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 92.18765 | | | | | 0 | |
| -4.76491 | -13.42116 | 14.24190 | 250.45361 | 1.000000 | 1 | 6.024 |
| -0.69522 | -1.28382 | 1.45907 | 241.56343 | 0.102512 | 2 | 12.048 |
| 0.23741 | -2.14675 | 2.15230 | 345.06787 | 0.151107 | 3 | 18.072 |
| 1.35490 | 0.28494 | 1.38491 | 11.94031 | 0.097262 | 4 | 24.096 |
| 0.77517 | -4.02111 | 4.09815 | 280.91130 | 0.287842 | 5 | 30.120 |
| 2.47066 | -0.89073 | 2.47135 | 350.69018 | 0.173627 | 6 | 36.145 |
| 1.34737 | -0.97728 | 1.66448 | 324.00868 | 0.116872 | 7 | 42.169 |
| -0.28213 | -0.60822 | 0.67137 | 245.15114 | 0.047141 | 8 | 48.193 |
| -0.13194 | 0.03241 | 0.13567 | 166.13009 | 0.009512 | 9 | 54.217 |
| 0.29464 | 0.33492 | 0.43799 | 54.12967 | 0.030754 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1082C TEST 498 OSC CTR 4PP TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.91090 | | | | | 0 | |
| -2.81874 | -0.18204 | 2.82462 | 183.69319 | 0.619963 | 1 | 6.024 |
| -3.80140 | -0.34433 | 3.82109 | 186.54454 | 0.4638644 | 2 | 12.048 |
| 3.97931 | -2.21912 | 4.55425 | 330.68888 | 1.000000 | 3 | 18.072 |
| -1.21253 | -1.00225 | 1.62927 | 221.79083 | 0.336712 | 4 | 24.096 |
| 0.90843 | 0.02032 | 0.90866 | 1.28048 | 0.199833 | 5 | 30.120 |
| -1.44007 | 0.90035 | 1.74009 | 145.66230 | 0.383010 | 6 | 36.145 |
| -1.32257 | -2.32573 | 2.67548 | 240.37437 | 0.587210 | 7 | 42.169 |
| 0.37153 | -0.07350 | 0.94023 | 293.09175 | 0.206835 | 8 | 48.193 |
| 0.73222 | 1.38208 | 1.56407 | 62.08842 | 0.343279 | 9 | 54.217 |
| 0.54231 | 0.13334 | 0.55846 | 13.81261 | 0.122570 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1082C TEST 498 OSC CTR 4PP TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 88.40875 | | | | | 0 | |
| -3.81454 | -18.28854 | 18.49143 | 260.59692 | 1.000000 | 1 | 6.024 |
| -4.59883 | -2.93428 | 7.22682 | 204.21881 | 0.391024 | 2 | 12.048 |
| 9.15189 | -1.46324 | 9.35973 | 347.87989 | 0.507263 | 3 | 18.072 |
| 3.87749 | 1.73465 | 3.94440 | 29.67861 | 0.192893 | 4 | 24.096 |
| 0.59410 | -5.88851 | 5.83301 | 279.25206 | 0.316128 | 5 | 30.120 |
| 2.58285 | -0.09519 | 2.58460 | 357.98948 | 0.140876 | 6 | 36.145 |
| 1.21402 | -0.38588 | 1.26949 | 343.63795 | 0.074221 | 7 | 42.169 |
| -0.43469 | -0.72471 | 0.84508 | 239.04175 | 0.045888 | 8 | 48.193 |
| -0.34795 | -0.09195 | 0.35989 | 194.88299 | 0.019505 | 9 | 54.217 |
| 0.53290 | 1.06036 | 1.18674 | 63.31732 | 0.064317 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1082C TEST 498 OSC CTR 4PP TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.49110 | | | | | 0 | |
| 1.38001 | 4.59038 | 4.74356 | 73.08105 | 0.492239 | 1 | 6.024 |
| -0.63546 | -4.27727 | 9.63671 | 280.34990 | 1.000000 | 2 | 12.048 |
| 7.53733 | -2.49424 | 7.93930 | 341.60945 | 0.823860 | 3 | 18.072 |
| 0.18762 | -0.44339 | 0.48146 | 292.93530 | 0.049961 | 4 | 24.096 |
| 0.46062 | -2.02673 | 2.07843 | 282.80396 | 0.215678 | 5 | 30.120 |
| -0.95850 | 2.04336 | 2.25700 | 115.13857 | 0.234208 | 6 | 36.145 |
| -1.14789 | -0.76946 | 1.39322 | 214.52164 | 0.144574 | 7 | 42.169 |
| 0.29130 | -2.48655 | 2.42412 | 276.90186 | 0.251550 | 8 | 48.193 |
| 0.42318 | -0.16945 | 0.45258 | 339.23535 | 0.046964 | 9 | 54.217 |
| 0.94021 | 1.02364 | 1.00040 | 71.31300 | 0.112134 | 10 | 60.241 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 496 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 41.38074 | | | | | 0 | |
| -0.79325 | -11.33217 | 11.35990 | 265.99561 | 1.000000 | 1 | 6.024 |
| -4.87541 | -1.73800 | 5.17593 | 199.62024 | 0.455632 | 2 | 12.048 |
| 4.32786 | -0.93494 | 4.42769 | 347.88957 | 0.389765 | 3 | 18.072 |
| 2.17385 | 1.48459 | 2.63242 | 34.33032 | 0.231729 | 4 | 24.096 |
| 0.37024 | -3.26496 | 3.28588 | 276.46948 | 0.289253 | 5 | 30.120 |
| 1.25816 | -0.22574 | 1.27825 | 349.82812 | 0.112523 | 6 | 36.145 |
| 0.54074 | 0.23234 | 0.58855 | 23.25201 | 0.051809 | 7 | 42.169 |
| -0.27126 | -0.22384 | 0.35169 | 219.52847 | 0.030959 | 8 | 48.193 |
| -0.23929 | -0.25071 | 0.34658 | 226.33513 | 0.030509 | 9 | 54.217 |
| 0.31639 | 0.75994 | 0.82317 | 67.39630 | 0.072463 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 496 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 22.45663 | | | | | 0 | |
| 2.78177 | 5.48181 | 6.14724 | 63.09422 | 0.928184 | 1 | 6.024 |
| -5.63464 | -3.68148 | 6.62343 | 211.71072 | 1.000000 | 2 | 12.048 |
| 4.40451 | -1.35899 | 4.60940 | 342.85254 | 0.695923 | 3 | 18.072 |
| 0.76778 | 0.26194 | 0.79233 | 19.30478 | 0.119626 | 4 | 24.096 |
| 0.83716 | -1.11694 | 1.11756 | 271.90527 | 0.168728 | 5 | 30.120 |
| -0.32655 | 1.13400 | 1.18008 | 106.06442 | 0.178168 | 6 | 36.145 |
| -0.57057 | 0.50502 | 0.76197 | 138.48747 | 0.115041 | 7 | 42.169 |
| 0.25792 | -1.68561 | 1.70523 | 278.69946 | 0.257454 | 8 | 48.193 |
| 0.20143 | -0.87809 | 0.90090 | 282.91968 | 0.136017 | 9 | 54.217 |
| -0.17141 | 0.94439 | 0.95982 | 100.28766 | 0.144913 | 10 | 60.241 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 496 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.24651 | | | | | 0 | |
| -0.85425 | -0.92452 | 0.92611 | 266.64160 | 1.000000 | 1 | 6.024 |
| -0.48864 | -0.14144 | 0.43053 | 199.17920 | 0.464886 | 2 | 12.048 |
| 0.34087 | -0.07344 | 0.34869 | 347.84082 | 0.376517 | 3 | 18.072 |
| 0.18801 | 0.12496 | 0.21913 | 34.76718 | 0.236610 | 4 | 24.096 |
| 0.03029 | -0.26361 | 0.26534 | 276.55469 | 0.286514 | 5 | 30.120 |
| 0.09941 | -0.01980 | 0.10136 | 348.73511 | 0.109452 | 6 | 36.145 |
| 0.04160 | 0.02327 | 0.04766 | 29.22272 | 0.051466 | 7 | 42.169 |
| -0.02216 | -0.01634 | 0.02753 | 216.39476 | 0.029727 | 8 | 48.193 |
| -0.01978 | -0.02211 | 0.02967 | 228.18088 | 0.032037 | 9 | 54.217 |
| 0.02577 | 0.06308 | 0.06814 | 67.78114 | 0.073572 | 10 | 60.241 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 496 TEST COND 21 COMP RUN 36.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.87820 | | | | | 0 | |
| 0.24545 | 0.47111 | 0.53122 | 62.48000 | 0.968824 | 1 | 6.024 |
| -0.46381 | -0.29245 | 0.54831 | 212.23349 | 1.000000 | 2 | 12.048 |
| 0.35788 | -0.10905 | 0.37412 | 343.05371 | 0.682316 | 3 | 18.072 |
| 0.06702 | 0.02625 | 0.07198 | 21.39259 | 0.131269 | 4 | 24.096 |
| 0.00044 | -0.09081 | 0.09081 | 270.40234 | 0.165625 | 5 | 30.120 |
| -0.02397 | 0.09169 | 0.09477 | 104.65358 | 0.172841 | 6 | 36.145 |
| -0.04508 | 0.05047 | 0.06767 | 131.77121 | 0.123423 | 7 | 42.169 |
| 0.02158 | -0.13960 | 0.14126 | 278.78662 | 0.257628 | 8 | 48.193 |
| 0.01568 | -0.07896 | 0.08050 | 281.22925 | 0.146810 | 9 | 54.217 |
| -0.01735 | 0.07995 | 0.08182 | 102.24634 | 0.149215 | 10 | 60.241 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.72997 | | | | | 0 | |
| -0.70514 | 0.44248 | 0.83248 | 147.89159 | 1.000000 | 1 | 5.848 |
| 0.24343 | -0.33770 | 0.41630 | 305.78564 | 0.500071 | 2 | 11.696 |
| -0.06548 | 0.06851 | 0.09491 | 133.79457 | 0.114005 | 3 | 17.544 |
| 0.03342 | -0.02202 | 0.04002 | 326.62427 | 0.048075 | 4 | 23.392 |
| -0.05222 | -0.05237 | 0.07396 | 225.00510 | 0.088848 | 5 | 29.240 |
| 0.02477 | -0.01524 | 0.02908 | 328.40388 | 0.034937 | 6 | 35.088 |
| -0.00728 | -0.04253 | 0.04315 | 260.28613 | 0.051836 | 7 | 40.936 |
| -0.01099 | -0.03169 | 0.03354 | 250.80019 | 0.040288 | 8 | 46.784 |
| 0.00798 | -0.04425 | 0.04496 | 280.21777 | 0.054010 | 9 | 52.632 |
| -0.00162 | -0.03283 | 0.03287 | 267.17163 | 0.039481 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -2.17835 | | | | | 0 | |
| -0.20325 | 0.98832 | 1.00117 | 101.71326 | 1.000000 | 1 | 5.848 |
| -0.26221 | -0.04563 | 0.26616 | 189.87188 | 0.265845 | 2 | 11.696 |
| -0.28469 | 0.04851 | 0.28899 | 170.33692 | 0.288653 | 3 | 17.544 |
| 0.00423 | 0.00873 | 0.01081 | 60.51593 | 0.010897 | 4 | 23.392 |
| -0.06798 | -0.03043 | 0.07448 | 204.11943 | 0.074391 | 5 | 29.240 |
| -0.01116 | -0.10081 | 0.10138 | 264.14486 | 0.101254 | 6 | 35.088 |
| 0.01150 | 0.00873 | 0.01159 | 3.40913 | 0.011513 | 7 | 40.936 |
| -0.00000 | 0.01239 | 0.01520 | 125.30091 | 0.015181 | 8 | 46.784 |
| 0.01492 | 0.01622 | 0.02204 | 47.39287 | 0.022014 | 9 | 52.632 |
| -0.02352 | 0.01954 | 0.02713 | 150.07275 | 0.027103 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.71857 | | | | | 0 | |
| -3.55277 | 2.21507 | 4.18672 | 148.69739 | 1.000000 | 1 | 5.848 |
| 1.19540 | -1.63087 | 2.02235 | 306.25220 | 0.483030 | 2 | 11.696 |
| -0.35095 | 0.31063 | 0.47099 | 138.40767 | 0.114646 | 3 | 17.544 |
| 0.16119 | -0.09405 | 0.18699 | 329.73218 | 0.044866 | 4 | 23.392 |
| -0.26096 | -0.25339 | 0.36807 | 223.90636 | 0.087913 | 5 | 29.240 |
| 0.11786 | -0.07467 | 0.13934 | 328.59361 | 0.033284 | 6 | 35.088 |
| -0.04009 | -0.20157 | 0.20568 | 258.53174 | 0.049126 | 7 | 40.936 |
| -0.09263 | -0.14247 | 0.15188 | 249.72444 | 0.036276 | 8 | 46.784 |
| 0.03946 | -0.20967 | 0.20881 | 279.01030 | 0.049708 | 9 | 52.632 |
| -0.00996 | -0.14939 | 0.14972 | 266.18433 | 0.035761 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.48319 | | | | | 0 | |
| -0.87980 | 4.44644 | 4.55214 | 101.13362 | 1.000000 | 1 | 5.848 |
| -1.24964 | -0.12182 | 1.25556 | 185.54004 | 0.275810 | 2 | 11.696 |
| -1.33561 | 0.17605 | 1.34716 | 172.49892 | 0.295900 | 3 | 17.544 |
| 0.02826 | 0.07904 | 0.08394 | 70.32367 | 0.018439 | 4 | 23.392 |
| -0.33126 | -0.13483 | 0.35765 | 202.14038 | 0.078567 | 5 | 29.240 |
| -0.07452 | -0.51043 | 0.51581 | 261.71606 | 0.113312 | 6 | 35.088 |
| 0.04086 | -0.00184 | 0.04087 | 358.74538 | 0.010900 | 7 | 40.936 |
| -0.04176 | 0.03862 | 0.07316 | 126.74147 | 0.016071 | 8 | 46.784 |
| 0.05886 | 0.07886 | 0.09840 | 53.26434 | 0.021616 | 9 | 52.632 |
| -0.10613 | 0.04588 | 0.11562 | 156.62119 | 0.025400 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/C0MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.05592 | | | | | 0 | |
| -9.44058 | 5.82451 | 11.09278 | 148.32668 | 1.000000 | 1 | 5.848 |
| 3.04447 | -4.03059 | 5.05230 | 307.06325 | 0.455469 | 2 | 11.696 |
| -1.07130 | 0.73281 | 1.30044 | 145.70084 | 0.117253 | 3 | 17.544 |
| 0.39714 | -0.17743 | 0.43498 | 335.92603 | 0.039213 | 4 | 23.392 |
| -0.72597 | -0.42832 | 0.84811 | 220.87584 | 0.076454 | 5 | 29.240 |
| 0.27779 | -0.16017 | 0.32066 | 330.08296 | 0.028907 | 6 | 35.088 |
| -0.12674 | -0.48099 | 0.49741 | 255.23769 | 0.044841 | 7 | 40.936 |
| -0.12818 | -0.38475 | 0.33861 | 247.18840 | 0.029864 | 8 | 46.784 |
| 0.07394 | -0.46819 | 0.47399 | 278.97412 | 0.042730 | 9 | 52.632 |
| -0.09417 | -0.32825 | 0.33882 | 264.09762 | 0.029791 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/C0MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -25.74432 | | | | | 0 | |
| -1.71207 | 9.89821 | 9.94723 | 99.87369 | 1.000000 | 1 | 5.848 |
| -3.01368 | 0.14084 | 3.01491 | 177.33944 | 0.303077 | 2 | 11.696 |
| -3.12000 | 0.17498 | 3.12367 | 176.00232 | 0.312947 | 3 | 17.544 |
| 0.10496 | 0.35882 | 0.39471 | 72.70850 | 0.039516 | 4 | 23.392 |
| -0.08807 | -0.27998 | 0.87787 | 108.98232 | 0.087870 | 5 | 29.240 |
| -0.27815 | -1.19818 | 1.23047 | 257.03498 | 0.122703 | 6 | 35.088 |
| 0.00828 | -0.00294 | 0.00884 | 340.91844 | 0.000885 | 7 | 40.936 |
| -0.11384 | 0.15988 | 0.17998 | 129.24488 | 0.018018 | 8 | 46.784 |
| 0.00883 | 0.19738 | 0.21827 | 66.35788 | 0.021934 | 9 | 52.632 |
| -0.22988 | 0.02384 | 0.23048 | 173.51198 | 0.023077 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 90
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/C0MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.09867 | | | | | 0 | |
| -27.12563 | 16.34090 | 31.66739 | 148.98468 | 1.000000 | 1 | 5.848 |
| 7.78810 | -9.23464 | 12.08788 | 309.69904 | 0.379794 | 2 | 11.696 |
| -4.04074 | 1.20489 | 4.21899 | 162.64013 | 0.133188 | 3 | 17.544 |
| 0.00193 | 0.13888 | 0.89107 | 0.77545 | 0.008167 | 4 | 23.392 |
| -2.24162 | -1.30998 | 2.68788 | 211.00823 | 0.084891 | 5 | 29.240 |
| 0.92295 | -0.21887 | 0.94823 | 337.34788 | 0.017888 | 6 | 35.088 |
| -0.92162 | -0.98811 | 1.08888 | 240.81788 | 0.032861 | 7 | 40.936 |
| -0.26948 | -0.22898 | 0.34882 | 221.44887 | 0.011853 | 8 | 46.784 |
| 0.04144 | -0.68844 | 0.69378 | 273.42434 | 0.021906 | 9 | 52.632 |
| -0.16342 | -0.38134 | 0.38748 | 249.09536 | 0.012234 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 90
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/C0MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -97.79180 | | | | | 0 | |
| 0.10811 | 10.69178 | 10.69334 | 88.98848 | 1.000000 | 1 | 5.848 |
| -0.02816 | 4.26488 | 7.41331 | 144.69848 | 0.693291 | 2 | 11.696 |
| -2.48888 | -1.99823 | 3.76101 | 208.23138 | 0.338787 | 3 | 17.544 |
| 0.37273 | 2.08747 | 2.14334 | 79.81595 | 0.200628 | 4 | 23.392 |
| -2.04848 | -0.18884 | 2.05884 | 182.88187 | 0.191782 | 5 | 29.240 |
| -1.48848 | -2.88727 | 2.36771 | 234.37883 | 0.248118 | 6 | 35.088 |
| -0.13884 | -0.29774 | 0.29128 | 248.28132 | 0.027232 | 7 | 40.936 |
| -0.32441 | 0.27128 | 0.42388 | 140.88898 | 0.039864 | 8 | 46.784 |
| -0.24921 | 0.48258 | 0.68888 | 125.33446 | 0.064444 | 9 | 52.632 |
| -0.21852 | -0.78833 | 0.78711 | 253.44911 | 0.071736 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 39.63546 | | | | | 0 | |
| -34.06177 | 19.76944 | 39.38316 | 149.86914 | 1.000000 | 1 | 5.848 |
| 8.05826 | -7.84973 | 11.26358 | 315.67790 | 0.286000 | 2 | 11.696 |
| -6.55605 | 0.19130 | 6.55804 | 178.32863 | 0.166539 | 3 | 17.544 |
| 0.72338 | 1.06832 | 1.29819 | 55.89740 | 0.032960 | 4 | 23.392 |
| -3.02094 | -1.18697 | 3.24576 | 201.45849 | 0.082415 | 5 | 29.240 |
| 0.24553 | 0.06153 | 0.25322 | 14.06311 | 0.006430 | 6 | 35.088 |
| -0.87859 | -0.45041 | 0.99146 | 207.00497 | 0.025175 | 7 | 40.936 |
| -0.19427 | 0.61379 | 0.64379 | 107.56285 | 0.016347 | 8 | 46.784 |
| -0.19051 | 0.07833 | 0.21341 | 158.46484 | 0.005419 | 9 | 52.632 |
| -0.38025 | 0.46821 | 0.50674 | 126.39599 | 0.012867 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -46.66686 | | | | | 0 | |
| 7.92843 | -11.66091 | 14.10806 | 304.19263 | 1.000000 | 1 | 5.848 |
| -9.80529 | 11.10748 | 11.74121 | 108.91864 | 0.832234 | 2 | 11.696 |
| -1.50300 | -0.12861 | 6.30828 | 256.21686 | 0.447140 | 3 | 17.544 |
| 1.00955 | 4.18740 | 4.32803 | 75.41516 | 0.306692 | 4 | 23.392 |
| -2.98195 | 0.89448 | 2.15890 | 156.67764 | 0.152983 | 5 | 29.240 |
| -2.84870 | -0.61905 | 2.90754 | 192.30922 | 0.206090 | 6 | 35.088 |
| -0.69672 | -0.37440 | 0.98897 | 219.90340 | 0.070084 | 7 | 40.936 |
| -0.37868 | 0.13929 | 0.40330 | 159.79952 | 0.028587 | 8 | 46.784 |
| -1.30413 | 0.46835 | 1.38568 | 160.24951 | 0.098219 | 9 | 52.632 |
| 0.37976 | -2.10721 | 2.14119 | 280.21606 | 0.151760 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 56.52972 | | | | | 0 | |
| -43.44232 | 22.99880 | 49.13994 | 152.14484 | 1.000000 | 1 | 5.848 |
| 9.27837 | -6.13351 | 11.12242 | 326.53296 | 0.226366 | 2 | 11.696 |
| -9.37912 | -1.68658 | 9.52955 | 190.19415 | 0.193963 | 3 | 17.544 |
| 0.72782 | 0.99161 | 1.22957 | 53.79220 | 0.025024 | 4 | 23.392 |
| -3.63330 | -1.85447 | 4.07020 | 207.04015 | 0.082819 | 5 | 29.240 |
| 0.05803 | -0.10559 | 0.12087 | 299.12476 | 0.002460 | 6 | 35.088 |
| -1.88546 | -0.74442 | 1.31903 | 214.62158 | 0.026845 | 7 | 40.936 |
| -0.24765 | 0.76724 | 0.80622 | 107.80939 | 0.016408 | 8 | 46.784 |
| -0.33780 | 0.22954 | 0.42518 | 147.31843 | 0.008651 | 9 | 52.632 |
| -0.40981 | 0.49793 | 0.64408 | 129.49551 | 0.013124 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -27.99675 | | | | | 0 | |
| 14.19753 | -14.54659 | 20.32864 | 314.30420 | 1.000000 | 1 | 5.848 |
| -4.86394 | 15.88734 | 16.39884 | 104.34051 | 0.806767 | 2 | 11.696 |
| 0.25883 | -0.39883 | 0.48177 | 271.71869 | 0.023698 | 3 | 17.544 |
| 1.27220 | 5.56681 | 5.71883 | 77.12709 | 0.280928 | 4 | 23.392 |
| -1.38756 | 0.95898 | 1.68183 | 145.93429 | 0.082740 | 5 | 29.240 |
| -3.18293 | 0.12731 | 3.18384 | 177.69048 | 0.156702 | 6 | 35.088 |
| -0.65432 | -0.38827 | 0.76257 | 210.00012 | 0.037516 | 7 | 40.936 |
| -0.29124 | -0.81696 | 0.29173 | 103.39192 | 0.014352 | 8 | 46.784 |
| -1.79958 | 0.05305 | 1.76829 | 178.27287 | 0.086980 | 9 | 52.632 |
| 0.76342 | -2.89407 | 2.99506 | 284.77734 | 0.147268 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XM-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 54.94440 | | | | | 0 | |
| -34.88702 | 15.37667 | 38.12540 | 156.21423 | 1.000000 | 1 | 5.848 |
| 6.92258 | -1.32375 | 7.04800 | 349.17432 | 0.184864 | 2 | 11.696 |
| -8.19591 | -3.60443 | 8.95348 | 203.73912 | 0.234843 | 3 | 17.544 |
| 0.62072 | -0.55014 | 0.82943 | 318.44971 | 0.021755 | 4 | 23.392 |
| -2.39238 | -2.58622 | 3.52307 | 227.22955 | 0.092407 | 5 | 29.240 |
| 0.01683 | -0.64245 | 0.64267 | 271.50073 | 0.016857 | 6 | 35.088 |
| -0.63232 | -1.40482 | 1.54057 | 245.76723 | 0.040408 | 7 | 40.936 |
| -0.30075 | -0.17719 | 0.34907 | 210.50520 | 0.009156 | 8 | 46.784 |
| -0.22408 | -0.38789 | 0.44796 | 239.98515 | 0.011750 | 9 | 52.632 |
| -0.28807 | -0.32853 | 0.43694 | 228.75420 | 0.011461 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XM-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.72523 | | | | | 0 | |
| 11.68803 | 10.53405 | 15.73455 | 42.02733 | 1.000000 | 1 | 5.848 |
| -5.25075 | 10.95543 | 12.14874 | 115.60767 | 0.772106 | 2 | 11.696 |
| -3.66790 | -4.68080 | 4.72821 | 261.87915 | 0.300498 | 3 | 17.544 |
| 0.45072 | 3.54191 | 3.57047 | 82.74789 | 0.226919 | 4 | 23.392 |
| 0.30483 | -0.35538 | 0.46821 | 310.62109 | 0.029757 | 5 | 29.240 |
| -0.79262 | -0.07814 | 0.79846 | 185.63000 | 0.050619 | 6 | 35.088 |
| 0.29298 | 0.43158 | 0.52163 | 55.82884 | 0.033152 | 7 | 40.936 |
| 0.12720 | -0.17153 | 0.21358 | 306.57373 | 0.013574 | 8 | 46.784 |
| -0.05615 | -0.71943 | 1.11829 | 220.04042 | 0.071072 | 9 | 52.632 |
| 0.53118 | -1.71166 | 1.79218 | 287.24072 | 0.113901 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XM-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 41.28958 | | | | | 0 | |
| -20.91209 | 7.42731 | 22.19189 | 160.44658 | 1.000000 | 1 | 5.848 |
| 3.53606 | 1.66042 | 3.90722 | 25.14028 | 0.176065 | 2 | 11.696 |
| -5.60222 | -3.85206 | 6.79877 | 214.51222 | 0.306353 | 3 | 17.544 |
| 0.48371 | -1.19313 | 1.28745 | 292.06836 | 0.058014 | 4 | 23.392 |
| -1.11130 | -2.37818 | 2.62502 | 244.95372 | 0.118287 | 5 | 29.240 |
| 0.09481 | -0.70715 | 0.71348 | 277.63599 | 0.032150 | 6 | 35.088 |
| -0.22577 | -1.32852 | 1.34757 | 260.35522 | 0.060723 | 7 | 40.936 |
| -0.22161 | -0.66291 | 0.69897 | 251.51556 | 0.031497 | 8 | 46.784 |
| -0.83496 | -0.63610 | 0.63706 | 266.85425 | 0.028707 | 9 | 52.632 |
| -0.13131 | -0.66944 | 0.68219 | 258.90186 | 0.030741 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XM-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.61069 | | | | | 0 | |
| 6.63576 | 22.79766 | 23.74376 | 73.77116 | 1.000000 | 1 | 5.848 |
| -4.81652 | 5.32955 | 7.18352 | 132.10538 | 0.302544 | 2 | 11.696 |
| -1.31966 | -1.30302 | 1.85456 | 224.63646 | 0.078107 | 3 | 17.544 |
| -0.22093 | 1.49476 | 1.51091 | 98.38510 | 0.063634 | 4 | 23.392 |
| 1.07586 | -1.08020 | 1.52456 | 314.88452 | 0.064209 | 5 | 29.240 |
| 0.69872 | -0.32199 | 0.76934 | 335.25806 | 0.032402 | 6 | 35.088 |
| 0.71112 | 0.67710 | 0.98191 | 43.59647 | 0.041355 | 7 | 40.936 |
| 0.41405 | -0.19672 | 0.45841 | 334.58716 | 0.019306 | 8 | 46.784 |
| -0.12725 | -0.87570 | 0.88490 | 261.73218 | 0.037269 | 9 | 52.632 |
| 0.23346 | -0.63267 | 0.67444 | 290.27051 | 0.028405 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJ | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.83131 | | | | | 0 | |
| -17.06711 | 9.91506 | 18.06305 | 160.88489 | 1.000000 | 1 | 5.848 |
| 1.34480 | 3.37044 | 3.62883 | 68.26796 | 0.200898 | 2 | 11.696 |
| -5.53067 | -4.78848 | 7.26347 | 220.40904 | 0.402118 | 3 | 17.544 |
| 0.50814 | -1.13774 | 1.24605 | 294.06641 | 0.068984 | 4 | 23.392 |
| -0.83415 | -2.55397 | 2.68674 | 251.91248 | 0.148742 | 5 | 29.240 |
| 0.42623 | -0.52165 | 0.67343 | 309.25146 | 0.037293 | 6 | 35.088 |
| -0.14098 | -1.05266 | 1.06206 | 262.37158 | 0.058797 | 7 | 40.936 |
| -0.10235 | -0.79531 | 0.80186 | 262.66626 | 0.044393 | 8 | 46.784 |
| 0.20143 | -0.62722 | 0.63875 | 287.80444 | 0.035469 | 9 | 52.632 |
| -0.03978 | -0.60564 | 0.60694 | 266.24146 | 0.033601 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.18994 | | | | | 0 | |
| 4.16354 | 29.90457 | 30.19301 | 82.07373 | 1.000000 | 1 | 5.848 |
| -5.15693 | 3.94440 | 6.49247 | 142.58864 | 0.215032 | 2 | 11.696 |
| -1.56448 | -0.11819 | 1.56894 | 184.32030 | 0.051964 | 3 | 17.544 |
| -0.87928 | 0.99856 | 1.33951 | 131.36533 | 0.044367 | 4 | 23.392 |
| 1.37686 | -1.69159 | 2.18068 | 309.12720 | 0.072222 | 5 | 29.240 |
| 1.37695 | -0.59781 | 1.48564 | 337.94678 | 0.049205 | 6 | 35.088 |
| 0.81586 | 0.46792 | 0.95580 | 31.39577 | 0.031656 | 7 | 40.936 |
| 0.86160 | -0.18878 | 0.88096 | 347.96436 | 0.029178 | 8 | 46.784 |
| 0.01033 | -0.78124 | 0.78131 | 279.75708 | 0.025877 | 9 | 52.632 |
| 0.13421 | -0.50614 | 0.51784 | 285.02075 | 0.017151 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 94.18570 | | | | | 0 | |
| -20.31818 | 9.43250 | 22.40069 | 155.09741 | 1.000000 | 1 | 5.848 |
| -5.61215 | 10.94189 | 12.20831 | 117.26778 | 0.544992 | 2 | 11.696 |
| -11.79451 | -11.49847 | 16.47194 | 224.27180 | 0.735325 | 3 | 17.544 |
| 1.38157 | -0.53785 | 1.48257 | 338.72852 | 0.066183 | 4 | 23.392 |
| -1.31556 | -4.84525 | 5.02367 | 254.80946 | 0.224128 | 5 | 29.240 |
| 2.14894 | 0.33698 | 2.17520 | 8.91207 | 0.097103 | 6 | 35.088 |
| -0.30477 | -0.00957 | 0.31786 | 196.37697 | 0.014181 | 7 | 40.936 |
| 0.43337 | -1.10362 | 1.18566 | 291.43872 | 0.052929 | 8 | 46.784 |
| 1.20602 | -0.49710 | 1.30445 | 337.59937 | 0.058232 | 9 | 52.632 |
| 0.19423 | -0.04315 | 0.19896 | 347.47510 | 0.008882 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 55.53918 | | | | | 0 | |
| 0.80754 | 59.55826 | 59.56372 | 89.22313 | 1.000000 | 1 | 5.848 |
| -9.58614 | 6.94940 | 11.84011 | 144.06007 | 0.198781 | 2 | 11.696 |
| -2.76029 | 0.89333 | 2.90125 | 162.06651 | 0.048708 | 3 | 17.544 |
| -3.54319 | 1.67852 | 3.92066 | 154.65160 | 0.065823 | 4 | 23.392 |
| 2.43899 | -4.37345 | 5.00368 | 299.06738 | 0.084005 | 5 | 29.240 |
| 3.14486 | -1.60064 | 3.52805 | 333.01929 | 0.059232 | 6 | 35.088 |
| 0.96824 | -0.60581 | 1.14215 | 327.[illegible]4655 | 0.019175 | 7 | 40.936 |
| 3.19101 | -0.23816 | 3.19989 | 355.73149 | 0.053722 | 8 | 46.784 |
| -0.22424 | -0.39894 | 0.45764 | 240.65977 | 0.007683 | 9 | 52.632 |
| 0.13722 | -1.53841 | 1.54452 | 275.09717 | 0.025931 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| 95.37241 | | | | | | |
| 1.28191 | -2.09708 | 2.45705 | 301.43677 | 0.160916 | 1 | 5.848 |
| -8.34944 | 11.90275 | 14.55070 | 125.11307 | 1.000000 | 2 | 11.696 |
| -0.81419 | -10.24347 | 14.20861 | 226.28188 | 0.979040 | 3 | 17.544 |
| 2.93952 | -0.09844 | 2.92214 | 357.94434 | 0.173335 | 4 | 23.392 |
| -0.21594 | -2.91368 | 2.92167 | 268.76074 | 0.200702 | 5 | 29.240 |
| 1.38681 | 0.55294 | 1.41098 | 22.02634 | 0.097528 | 6 | 35.088 |
| 0.12988 | 0.69949 | 0.67212 | 79.07972 | 0.046191 | 7 | 40.936 |
| 0.04823 | -0.91292 | 0.90642 | 328.99766 | 0.062654 | 8 | 46.784 |
| 0.02317 | -0.29416 | 0.86343 | 342.08037 | 0.059839 | 9 | 52.632 |
| 0.24622 | 0.22601 | 0.33432 | 42.54093 | 0.022969 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 1[illegible]
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 C[illegible] 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| 42.99828 | | | | | | |
| 0.77632 | 28.29498 | 28.28623 | 88.42607 | 1.000000 | 1 | 5.848 |
| -0.83213 | 0.78819 | 0.68787 | 120.58480 | 0.024315 | 2 | 11.696 |
| -2.30504 | 0.04480 | 2.30646 | 178.92210 | 0.081600 | 3 | 17.544 |
| -2.14488 | 1.19778 | 2.48771 | 190.88884 | 0.086892 | 4 | 23.392 |
| 1.05850 | -2.01314 | 2.01804 | 298.01348 | 0.070721 | 5 | 29.240 |
| 1.29817 | -0.00000 | 1.29480 | 359.99998 | 0.045806 | 6 | 35.088 |
| 0.05257 | -0.59413 | 0.59662 | 275.41095 | 0.019898 | 7 | 40.936 |
| 2.43844 | -0.38715 | 2.46183 | 351.02246 | 0.087777 | 8 | 46.784 |
| 0.00073 | -0.18542 | 0.18542 | 270.22534 | 0.006560 | 9 | 52.632 |
| 0.42783 | -1.04480 | 1.12980 | 292.38784 | 0.039982 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| 30.30044 | | | | | | |
| 22.00334 | -20.63403 | 30.79316 | 317.00035 | 1.000000 | 1 | 5.848 |
| -0.92008 | 19.84010 | 22.18971 | 116.58402 | 0.721306 | 2 | 11.696 |
| -14.31326 | -14.56477 | 20.42062 | 225.44098 | 0.663074 | 3 | 17.544 |
| 5.54990 | -2.24449 | 5.98663 | 337.97076 | 0.194455 | 4 | 23.392 |
| 1.45171 | -3.00048 | 3.34462 | 295.73903 | 0.108613 | 5 | 29.240 |
| -0.33398 | -0.34959 | 0.47053 | 225.00990 | 0.015999 | 6 | 35.088 |
| 0.64784 | -0.18691 | 0.67427 | 343.98674 | 0.021904 | 7 | 40.936 |
| 1.12824 | -0.72739 | 1.34239 | 327.18970 | 0.043606 | 8 | 46.784 |
| -0.09195 | -1.01419 | 1.01898 | 264.81958 | 0.033112 | 9 | 52.632 |
| 0.09300 | -0.70934 | 0.71348 | 277.46899 | 0.023262 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| | | | | | 0 | |
| 123.00080 | | | | | | |
| 10.32082 | 7.40404 | 12.79497 | 35.92712 | 0.998807 | 1 | 5.848 |
| -4.29889 | 12.19712 | 12.87879 | 109.27161 | 1.000000 | 2 | 11.696 |
| -4.79380 | -2.08138 | 5.55163 | 210.30311 | 0.431068 | 3 | 17.544 |
| 0.64053 | 1.02972 | 1.21269 | 58.11638 | 0.094162 | 4 | 23.392 |
| 0.86946 | -0.99830 | 1.32560 | 327.99005 | 0.079635 | 5 | 29.240 |
| -0.00083 | -0.13400 | 0.09871 | 180.63269 | 0.007782 | 6 | 35.088 |
| -0.99455 | 0.42530 | 0.84804 | 133.95423 | 0.006997 | 7 | 40.936 |
| 1.67506 | -1.13983 | 2.02253 | 325.72070 | 0.157028 | 8 | 46.784 |
| 0.98429 | -1.18678 | 1.40804 | 307.38615 | 0.115053 | 9 | 52.632 |
| 1.00092 | -0.35496 | 1.07019 | 340.51695 | 0.083097 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.93106 | | | | | 0 | |
| 27.38416 | -18.72572 | 33.17445 | 325.63501 | 1.000000 | 1 | 5.860 |
| -6.48884 | 16.19873 | 17.42044 | 111.58577 | 0.525116 | 2 | 11.696 |
| -11.50139 | -9.58948 | 14.92354 | 219.58432 | 0.449850 | 3 | 17.544 |
| 2.73483 | -3.38688 | 4.35268 | 308.91187 | 0.131206 | 4 | 23.392 |
| 2.62279 | -2.69491 | 3.79197 | 314.68137 | 0.112495 | 5 | 29.240 |
| -0.83452 | -0.21378 | 0.21868 | 200.30498 | 0.006838 | 6 | 35.088 |
| -0.77797 | -0.36873 | 0.85965 | 205.17899 | 0.025913 | 7 | 40.936 |
| -0.16967 | -0.34588 | 9.38526 | 243.84998 | 0.011613 | 8 | 46.784 |
| -0.49855 | -0.47484 | 0.68795 | 223.98469 | 0.020737 | 9 | 52.632 |
| -0.44710 | -0.69617 | 0.79481 | 235.73074 | 0.023935 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 31.12978 | | | | | 0 | |
| 8.94484 | -1.22782 | 9.02874 | 352.10488 | 0.979289 | 1 | 5.860 |
| -6.17460 | 6.84468 | 9.21989 | 132.09841 | 1.000000 | 2 | 11.696 |
| -5.08739 | -5.19615 | 7.21422 | 226.08977 | 0.782697 | 3 | 17.544 |
| 2.44150 | -1.11869 | 2.70384 | 335.99842 | 0.293271 | 4 | 23.392 |
| 1.87481 | 2.09133 | 2.80866 | 48.12482 | 0.304657 | 5 | 29.240 |
| -2.17946 | -0.27439 | 2.19866 | 187.17483 | 0.238257 | 6 | 35.088 |
| -1.33382 | -1.23826 | 1.81999 | 222.87216 | 0.197403 | 7 | 40.936 |
| 1.03939 | -0.85779 | 1.34784 | 320.46753 | 0.146178 | 8 | 46.784 |
| 1.18863 | 0.34990 | 1.22958 | 16.22227 | 0.133365 | 9 | 52.632 |
| -0.90962 | -0.29804 | 0.96469 | 206.84953 | 0.001249 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 26.21960 | | | | | 0 | |
| 33.18201 | -20.63649 | 43.84335 | 319.18995 | 1.000000 | 1 | 5.860 |
| -6.17371 | 16.86166 | 17.20729 | 111.82350 | 0.392672 | 2 | 11.696 |
| -12.14823 | -9.07362 | 15.15630 | 216.77946 | 0.345694 | 3 | 17.544 |
| 2.88848 | -4.83200 | 5.23283 | 292.59854 | 0.119355 | 4 | 23.392 |
| 3.99375 | -3.66319 | 5.10373 | 314.13110 | 0.116408 | 5 | 29.240 |
| 0.19765 | 0.22038 | 0.29603 | 48.11235 | 0.006752 | 6 | 35.088 |
| -1.69207 | -0.41914 | 1.74321 | 193.91870 | 0.039760 | 7 | 40.936 |
| -1.02986 | -0.39879 | 1.22254 | 212.80844 | 0.027884 | 8 | 46.784 |
| -0.66111 | -0.33968 | 0.74327 | 207.19879 | 0.016953 | 9 | 52.632 |
| -0.52769 | -0.44101 | 0.68771 | 219.80728 | 0.015684 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.54642 | | | | | 0 | |
| 18.49840 | 12.57906 | 22.37013 | 34.21400 | 1.000000 | 1 | 5.860 |
| -6.88753 | 10.89533 | 12.79836 | 122.14086 | 0.572029 | 2 | 11.696 |
| -9.29960 | -7.84059 | 11.66415 | 217.12881 | 0.521416 | 3 | 17.544 |
| 2.32995 | -2.97011 | 3.77248 | 308.06919 | 0.168639 | 4 | 23.392 |
| 4.84234 | 1.84298 | 4.44916 | 24.63896 | 0.198782 | 5 | 29.240 |
| -1.84089 | -0.82702 | 1.84029 | 180.84119 | 0.082286 | 6 | 35.088 |
| -1.93188 | -0.99983 | 1.82863 | 213.14545 | 0.081744 | 7 | 40.936 |
| -0.88672 | -2.23219 | 2.23220 | 269.82739 | 0.099785 | 8 | 46.784 |
| 1.43126 | 0.57905 | 1.48860 | 14.03330 | 0.066186 | 9 | 52.632 |
| -0.98337 | -0.55335 | 1.12834 | 209.36679 | 0.050441 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.78113 | | | | | 0 | |
| 17.24347 | -18.17653 | 25.05440 | 313.49097 | 1.000000 | 1 | 5.848 |
| -2.94484 | 7.47636 | 8.03356 | 111.50414 | 0.320645 | 2 | 11.696 |
| -5.96244 | -4.41357 | 7.41824 | 216.50995 | 0.296085 | 3 | 17.544 |
| 0.98322 | -2.71786 | 2.89023 | 289.88818 | 0.115358 | 4 | 23.392 |
| 1.88784 | -2.08502 | 2.81269 | 312.15845 | 0.112263 | 5 | 29.240 |
| 0.07045 | 0.24222 | 0.25226 | 73.78291 | 0.010068 | 6 | 35.088 |
| -0.95758 | -0.23185 | 0.98520 | 193.59909 | 0.039322 | 7 | 40.936 |
| -0.68648 | -0.49483 | 0.84623 | 215.78510 | 0.033776 | 8 | 46.784 |
| -0.35752 | -0.18537 | 0.40271 | 207.40627 | 0.016074 | 9 | 52.632 |
| -0.20046 | -0.13530 | 0.24185 | 214.01776 | 0.009653 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.34357 | | | | | 0 | |
| 13.25468 | 12.2[illegible]42 | 18.04608 | 42.73581 | 1.000000 | 1 | 5.848 |
| -2.86452 | 7.49380 | 8.02262 | 110.92948 | 0.444563 | 2 | 11.696 |
| -6.14804 | -3.71193 | 7.18170 | 211.12183 | 0.397964 | 3 | 17.544 |
| 0.82073 | [illegible] | 2.07759 | 293.26855 | 0.115127 | 4 | 23.392 |
| 2.66158 | 0.[illegible]74 | 2.69686 | 9.27680 | 0.149443 | 5 | 29.240 |
| -0.54515 | 0.17553 | 0.57271 | 162.15169 | 0.031736 | 6 | 35.088 |
| -0.67371 | 0.01319 | 0.67384 | 178.87854 | 0.037340 | 7 | 40.936 |
| -0.58139 | -1.70225 | 1.77456 | 253.58791 | 0.098335 | 8 | 46.784 |
| 0.73681 | -0.07794 | 0.74013 | 353.95532 | 0.041013 | 9 | 52.632 |
| -0.42761 | -0.35547 | 0.55606 | 219.73685 | 0.030814 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.64761 | | | | | 0 | |
| 1.37686 | -1.48713 | 2.02665 | 312.79492 | 1.000000 | 1 | 5.848 |
| -0.23170 | 0.58632 | 0.63045 | 111.56305 | 0.311078 | 2 | 11.696 |
| -0.47172 | -0.34818 | 0.58630 | 216.43118 | 0.289295 | 3 | 17.544 |
| 0.07727 | -0.21944 | 0.23265 | 289.39917 | 0.114794 | 4 | 23.392 |
| 0.15133 | -0.16851 | 0.22649 | 311.92676 | 0.111755 | 5 | 29.240 |
| 0.00542 | 0.02085 | 0.02154 | 72.44046 | 0.010629 | 6 | 35.088 |
| -0.07761 | -0.01863 | 0.07981 | 193.49547 | 0.039381 | 7 | 40.936 |
| -0.05673 | -0.04115 | 0.07008 | 215.95743 | 0.034581 | 8 | 46.784 |
| -0.02872 | -0.01478 | 0.03230 | 207.22691 | 0.015935 | 9 | 52.632 |
| -0.01526 | -0.00969 | 0.01808 | 212.42140 | 0.008921 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 501 OSC CTR 346 TEST COND 23 COMP RUN 42.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.29449 | | | | | 0 | |
| 1.09852 | 1.04172 | 1.51391 | 43.47968 | 1.000000 | 1 | 5.848 |
| -0.22164 | 0.61823 | 0.65676 | 109.72354 | 0.433815 | 2 | 11.696 |
| -0.58563 | -0.29728 | 0.58655 | 210.45331 | 0.387439 | 3 | 17.544 |
| 0.06134 | -0.15684 | 0.16841 | 291.36060 | 0.111246 | 4 | 23.392 |
| 0.21890 | 0.02906 | 0.22082 | 7.56195 | 0.145859 | 5 | 29.240 |
| -0.03983 | 0.01607 | 0.04221 | 157.62811 | 0.027880 | 6 | 35.088 |
| -0.05253 | 0.00663 | 0.05295 | 172.80597 | 0.034975 | 7 | 40.936 |
| -0.04564 | -0.14193 | 0.14908 | 252.17334 | 0.098476 | 8 | 46.784 |
| 0.05869 | -0.00899 | 0.05938 | 351.28931 | 0.039221 | 9 | 52.632 |
| -0.03349 | -0.02918 | 0.04442 | 221.06369 | 0.029340 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.91601 | | | | | 0 | |
| -0.83733 | 1.06157 | 1.35205 | 128.26508 | 1.000000 | 1 | 5.917 |
| 0.03663 | -0.80295 | 0.80378 | 272.61157 | 0.594492 | 2 | 11.834 |
| -0.34667 | 0.41723 | 0.41983 | 96.38188 | 0.310513 | 3 | 17.751 |
| -0.15499 | 0.01582 | 0.15579 | 174.17134 | 0.115227 | 4 | 23.669 |
| -0.12626 | 0.14795 | 0.19450 | 130.47647 | 0.143858 | 5 | 29.586 |
| -0.02985 | 0.04699 | 0.05567 | 122.41971 | 0.041175 | 6 | 35.503 |
| -0.06048 | 0.14670 | 0.15869 | 112.40497 | 0.117364 | 7 | 41.421 |
| -0.11536 | 0.06109 | 0.13054 | 152.09552 | 0.096547 | 8 | 47.337 |
| -0.11523 | 0.00877 | 0.11556 | 175.64548 | 0.085471 | 9 | 53.254 |
| -0.09763 | -0.03606 | 0.10408 | 200.27327 | 0.076977 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.80710 | | | | | 0 | |
| -0.36058 | -0.63458 | 0.72987 | 240.39362 | 0.891187 | 1 | 5.917 |
| -0.79551 | -0.17882 | 0.81899 | 193.75235 | 1.000000 | 2 | 11.834 |
| -0.57884 | 0.17886 | 0.60585 | 162.82957 | 0.739751 | 3 | 17.751 |
| 0.13297 | 0.02660 | 0.13560 | 11.31472 | 0.165572 | 4 | 23.669 |
| 0.01178 | 0.27627 | 0.27653 | 87.95768 | 0.337644 | 5 | 29.586 |
| 0.16207 | 0.00001 | 0.18443 | 28.58395 | 0.225191 | 6 | 35.503 |
| -0.08869 | -0.00613 | 0.08891 | 183.95374 | 0.108556 | 7 | 41.420 |
| -0.09893 | -0.06252 | 0.11703 | 212.28922 | 0.142894 | 8 | 47.337 |
| -0.24960 | -0.12956 | 0.28122 | 207.43134 | 0.343378 | 9 | 53.254 |
| -0.10591 | -0.09256 | 0.14065 | 221. 9321 | 0.171743 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.53385 | | | | | 0 | |
| -4.22043 | 5.16353 | 6.66889 | 129.26182 | 1.000000 | 1 | 5.917 |
| 0.24122 | -3.91043 | 3.92584 | 273.52271 | 0.588681 | 2 | 11.834 |
| -0.28301 | 1.98631 | 2.00637 | 98.10905 | 0.300856 | 3 | 17.751 |
| -0.72047 | 0.03903 | 0.72153 | 176.89986 | 0.108193 | 4 | 23.669 |
| -0.83207 | 0.68265 | 0.93033 | 139.79860 | 0.139503 | 5 | 29.936 |
| -0.13435 | 0.19257 | 0.23481 | 124.98327 | 0.035209 | 6 | 35.503 |
| -0.29891 | 0.67280 | 0.73621 | 113.95497 | 0.110395 | 7 | 41.420 |
| -0.53675 | 0.27086 | 0.60122 | 153.22381 | 0.090152 | 8 | 47.337 |
| -0.54890 | 0.03355 | 0.55005 | 176.29399 | 0.082480 | 9 | 53.254 |
| -0.46459 | -0.17950 | 0.49804 | 201.12495 | 0.074684 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -3.82202 | | | | | 0 | |
| -1.78319 | -2.98534 | 3.48092 | 238.45990 | 0.875275 | 1 | 5.917 |
| -3.79350 | -0.89315 | 3.89469 | 193.25737 | 1.000000 | 2 | 11.834 |
| -2.76414 | 0.83341 | 2.88896 | 163.23288 | 0.741769 | 3 | 17.751 |
| 0.63919 | 0.08753 | 0.64516 | 7.79773 | 0.165691 | 4 | 23.669 |
| 0.04791 | 1.27781 | 1.27791 | 87.85130 | 0.328116 | 5 | 29.586 |
| 0.76112 | 0.38578 | 0.85331 | 26.67831 | 0.219095 | 6 | 35.503 |
| -0.40416 | -0.84150 | 0.48629 | 185.86275 | 0.124918 | 7 | 41.420 |
| -0.45805 | -0.30982 | 0.55299 | 214.07361 | 0.141986 | 8 | 47.337 |
| -1.19582 | -0.62149 | 1.31232 | 208.26695 | 0.336950 | 9 | 53.254 |
| -0.48242 | -0.44095 | 0.65356 | 222.42813 | 0.167814 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J C | FREQUENCY |
|---|---|---|---|---|---|---|
| 11.69868 | | | | | 0 | |
| -11.22186 | 12.92624 | 17.11775 | 130.96277 | 1.000000 | 1 | 5.917 |
| 0.88434 | -9.86637 | 9.90592 | 275.12183 | 0.578693 | 2 | 11.834 |
| -0.95765 | 4.78093 | 4.87589 | 101.32683 | 0.284844 | 3 | 17.751 |
| -1.65518 | -0.07095 | 1.65670 | 182.45378 | 0.096783 | 4 | 23.669 |
| -1.66210 | 1.54441 | 2.26087 | 137.10194 | 0.132545 | 5 | 29.586 |
| -0.28824 | 0.32195 | 0.43213 | 131.63052 | 0.025244 | 6 | 35.503 |
| -0.76934 | 1.50300 | 1.68846 | 117.10668 | 0.098638 | 7 | 41.420 |
| -1.23538 | 0.56116 | 1.35686 | 155.57051 | 0.079266 | 8 | 47.337 |
| -1.32274 | 0.05732 | 1.32398 | 177.51872 | 0.077345 | 9 | 53.254 |
| -1.11736 | -0.46757 | 1.21124 | 202.70720 | 0.070759 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J C | FREQUENCY |
|---|---|---|---|---|---|---|
| -9.10644 | | | | | 0 | |
| -6.90430 | -6.66700 | 7.93402 | 234.68412 | 0.867825 | 1 | 5.917 |
| -9.14117 | -1.99855 | 9.35667 | 192.52845 | 1.000000 | 2 | 11.834 |
| -6.70525 | 1.92302 | 6.97170 | 163.99113 | 0.745940 | 3 | 17.751 |
| 1.56662 | 0.03206 | 1.56696 | 1.20169 | 0.167478 | 4 | 23.669 |
| 0.07011 | 2.89005 | 2.90098 | 88.45711 | 0.310035 | 5 | 29.586 |
| 1.78444 | 0.77736 | 1.94649 | 23.94497 | 0.208033 | 6 | 35.503 |
| -0.89865 | -0.19506 | 0.90418 | 189.92619 | 0.096635 | 7 | 41.420 |
| -1.04383 | -0.00114 | 1.31503 | 217.90624 | 0.140630 | 8 | 47.337 |
| -2.63453 | -1.51735 | 3.04034 | 209.93944 | 0.324928 | 9 | 53.254 |
| -1.06231 | -1.06272 | 1.50262 | 225.01088 | 0.160593 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J O | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.99139 | | | | | 0 | |
| -32.28949 | -30.99863 | 44.44876 | 136.98151 | 1.000000 | 1 | 5.917 |
| 4.68986 | -24.16453 | 24.61343 | 280.93586 | 0.553748 | 2 | 11.834 |
| -4.22444 | 9.74337 | 10.61976 | 113.44028 | 0.238921 | 3 | 17.751 |
| -2.54937 | -1.68814 | 3.09819 | 213.29798 | 0.069698 | 4 | 23.669 |
| -4.57868 | 2.29413 | 5.10347 | 153.78854 | 0.114817 | 5 | 29.586 |
| -0.38861 | -0.67623 | 0.74332 | 245.46938 | 0.016723 | 6 | 35.503 |
| -2.00496 | 1.92112 | 2.77679 | 136.22548 | 0.062472 | 7 | 41.420 |
| -1.97843 | 0.28971 | 1.99957 | 171.66948 | 0.044986 | 8 | 47.337 |
| -2.69788 | -0.14065 | 2.70189 | 183.13375 | 0.060787 | 9 | 53.254 |
| -2.26348 | -1.28264 | 2.68181 | 209.59664 | 0.090535 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J O | FREQUENCY |
|---|---|---|---|---|---|---|
| -18.36983 | | | | | 0 | |
| -12.28727 | -9.94361 | 15.25860 | 216.35361 | 0.816522 | 1 | 5.917 |
| -18.68982 | -2.72015 | 18.68488 | 188.37886 | 1.000000 | 2 | 11.834 |
| -13.97767 | 3.11416 | 14.32038 | 167.43991 | 0.766416 | 3 | 17.751 |
| 3.49175 | -1.99498 | 3.83876 | 335.45068 | 0.205447 | 4 | 23.669 |
| -0.16665 | 4.25083 | 4.25389 | 92.24519 | 0.227665 | 5 | 29.586 |
| 3.19812 | 0.17692 | 3.20381 | 3.16644 | 0.171423 | 6 | 35.503 |
| -1.86735 | -0.85809 | 1.95998 | 219.32780 | 0.072464 | 7 | 41.420 |
| -1.94933 | -2.14286 | 2.69384 | 234.07541 | 0.144961 | 8 | 47.337 |
| -3.98297 | -3.29439 | 5.36246 | 219.90893 | 0.276291 | 9 | 53.254 |
| -1.28888 | -2.15365 | 2.46659 | 240.03945 | 0.132088 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 54.04971 | | | | | 0 | |
| -30.62924 | 28.56035 | 49.66315 | 144.89468 | 1.000000 | 1 | 5.917 |
| 8.87383 | -23.63846 | 25.24918 | 290.57593 | 0.508409 | 2 | 11.834 |
| -7.82330 | 6.11004 | 9.92655 | 142.00998 | 0.199878 | 3 | 17.751 |
| -0.04584 | -4.29014 | 4.29038 | 269.38770 | 0.086390 | 4 | 23.669 |
| -5.53002 | -0.49168 | 5.55184 | 185.08084 | 0.111790 | 5 | 29.586 |
| 0.45753 | -3.19243 | 3.22505 | 278.15601 | 0.064938 | 6 | 35.503 |
| -2.20998 | -1.10434 | 2.47040 | 206.54536 | 0.049743 | 7 | 41.420 |
| -0.12980 | -1.59351 | 1.59879 | 265.34326 | 0.032193 | 8 | 47.337 |
| -1.71306 | -0.64547 | 1.83061 | 200.64456 | 0.036861 | 9 | 53.254 |
| -1.35844 | -1.49567 | 2.04760 | 226.92421 | 0.041230 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.18304 | | | | | 0 | |
| -13.87199 | 4.04185 | 14.25692 | 163.53076 | 1.000000 | 1 | 5.917 |
| -11.70704 | 1.22493 | 11.77095 | 174.02676 | 0.825630 | 2 | 11.834 |
| -9.59677 | 0.32299 | 9.60220 | 178.07240 | 0.673511 | 3 | 17.751 |
| 2.76326 | -4.46944 | 5.25467 | 301.72656 | 0.368569 | 4 | 23.669 |
| -0.81494 | -0.75083 | 1.10610 | 222.65514 | 0.077723 | 5 | 29.586 |
| 1.68221 | -2.83228 | 3.03199 | 290.91162 | 0.212668 | 6 | 35.503 |
| 0.94605 | -1.64237 | 1.89536 | 299.94317 | 0.132943 | 7 | 41.420 |
| 0.19992 | -2.40648 | 2.41476 | 274.74902 | 0.169375 | 8 | 47.337 |
| 0.36567 | -2.47198 | 2.50188 | 278.86743 | 0.175486 | 9 | 53.254 |
| 1.20273 | -1.35978 | 1.81537 | 311.49268 | 0.127332 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.00655 | | | | | 0 | |
| -52.41072 | 32.21965 | 61.52226 | 148.41876 | 1.000000 | 1 | 5.917 |
| 10.99775 | -22.73477 | 25.25487 | 295.61396 | 0.410500 | 2 | 11.834 |
| -13.53969 | 3.64072 | 14.01953 | 164.95050 | 0.227877 | 3 | 17.751 |
| 0.78102 | -5.21153 | 5.26973 | 278.52295 | 0.085656 | 4 | 23.669 |
| -7.61498 | -2.93449 | 8.16260 | 201.06972 | 0.132677 | 5 | 29.586 |
| 1.95862 | -4.68365 | 4.89278 | 293.59741 | 0.079529 | 6 | 35.503 |
| -2.71628 | -2.19172 | 3.49024 | 218.89952 | 0.056731 | 7 | 41.420 |
| 1.11977 | -2.83166 | 3.04503 | 291.57617 | 0.049495 | 8 | 47.337 |
| -0.93349 | -0.87604 | 1.28018 | 223.18161 | 0.020808 | 9 | 53.254 |
| -0.71759 | -1.52362 | 1.68414 | 244.78056 | 0.027375 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.30657 | | | | | 0 | |
| -12.07334 | 23.92265 | 26.79060 | 116.77934 | 1.000000 | 1 | 5.917 |
| -10.52645 | 4.82591 | 11.57959 | 155.37469 | 0.432129 | 2 | 11.834 |
| -7.55582 | -0.94923 | 7.61521 | 187.16046 | 0.284186 | 3 | 17.751 |
| 1.36935 | -6.31713 | 6.46384 | 282.23047 | 0.241219 | 4 | 23.669 |
| -1.42735 | -3.91464 | 4.16655 | 249.90626 | 0.155488 | 5 | 29.586 |
| -0.38479 | -4.67405 | 4.68986 | 265.29370 | 0.175017 | 6 | 35.503 |
| 2.18580 | -1.90352 | 2.89847 | 318.94873 | 0.108160 | 7 | 41.420 |
| 1.09562 | -2.90136 | 3.10133 | 290.68774 | 0.115736 | 8 | 47.337 |
| 3.55998 | -1.87280 | 4.02254 | 332.25244 | 0.150114 | 9 | 53.254 |
| 2.29693 | -1.11119 | 2.55160 | 334.18335 | 0.095221 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 38.24594 | | | | | 0 | |
| -42.83588 | 27.13570 | 50.70757 | 147.64655 | 1.000000 | 1 | 5.917 |
| 5.67587 | -10.93950 | 12.32429 | 297.42212 | 0.243046 | 2 | 11.834 |
| -15.48360 | 0.80146 | 15.50433 | 177.03691 | 0.305760 | 3 | 17.751 |
| -0.52705 | -2.23196 | 2.29334 | 256.71362 | 0.045227 | 4 | 23.669 |
| -7.35461 | -3.37301 | 8.09119 | 204.63741 | 0.159566 | 5 | 29.586 |
| 3.02087 | -2.41697 | 3.86877 | 321.33691 | 0.076296 | 6 | 35.503 |
| -2.23716 | -0.21034 | 2.24702 | 185.37112 | 0.044313 | 7 | 41.420 |
| 1.00527 | -1.90783 | 2.15647 | 297.79549 | 0.042528 | 8 | 47.337 |
| -0.17356 | -0.44536 | 0.47799 | 244.70934 | 0.009426 | 9 | 53.254 |
| -0.04627 | -0.71944 | 0.72033 | 266.32007 | 0.014217 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.95230 | | | | | 0 | |
| -2.31724 | 38.48378 | 38.55347 | 93.44585 | 1.000000 | 1 | 5.917 |
| -10.94945 | 5.70430 | 12.36623 | 152.48199 | 0.320737 | 2 | 11.834 |
| -5.14585 | -0.10292 | 5.14687 | 181.14531 | 0.133500 | 3 | 17.751 |
| -1.05140 | -3.96924 | 4.10613 | 255.16376 | 0.106505 | 4 | 23.669 |
| -1.37584 | -2.86073 | 3.15637 | 244.15776 | 0.081870 | 5 | 29.586 |
| -0.92061 | -3.07067 | 3.20570 | 253.31087 | 0.083150 | 6 | 35.503 |
| 1.56801 | -0.68309 | 1.71035 | 336.45996 | 0.044363 | 7 | 41.420 |
| 0.36272 | -2.16276 | 2.19296 | 279.52051 | 0.056881 | 8 | 47.337 |
| 3.31743 | -0.75043 | 3.40125 | 347.25366 | 0.088221 | 9 | 53.254 |
| 0.79524 | -0.96914 | 1.25365 | 309.37085 | 0.032517 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 26.81673 | | | | | 0 | |
| -25.87039 | 17.68193 | 31.33621 | 145.64874 | 1.000000 | 1 | 5.917 |
| 1.67316 | -1.29586 | 1.68253 | 309.62939 | 0.053693 | 2 | 11.834 |
| -13.37859 | -1.09717 | 13.42350 | 184.68928 | 0.428370 | 3 | 17.751 |
| -1.00529 | -0.45855 | 1.10493 | 204.51978 | 0.035260 | 4 | 23.669 |
| -5.39507 | -2.41746 | 5.91192 | 204.13651 | 0.188661 | 5 | 29.586 |
| 2.46181 | -0.72709 | 2.56694 | 343.56541 | 0.081916 | 6 | 35.503 |
| -1.34305 | 0.99425 | 1.67103 | 216.28375 | 0.053411 | 7 | 41.420 |
| 0.44109 | -0.71057 | 0.83631 | 301.83203 | 0.026688 | 8 | 47.337 |
| -0.00223 | -0.14173 | 0.14174 | 269.10034 | 0.004523 | 9 | 53.254 |
| 0.17282 | -0.18197 | 0.25096 | 313.52227 | 0.008009 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.07860 | | | | | 0 | |
| 3.05736 | 35.99564 | 36.12523 | 85.14507 | 1.000000 | 1 | 5.917 |
| -9.08126 | 4.79942 | 10.27150 | 152.14366 | 0.284330 | 2 | 11.834 |
| -3.27790 | 0.41919 | 3.30447 | 172.72980 | 0.091473 | 3 | 17.751 |
| -1.77859 | -1.43891 | 2.28776 | 218.97346 | 0.063329 | 4 | 23.669 |
| -1.08971 | -0.97610 | 1.46295 | 221.85236 | 0.040497 | 5 | 29.586 |
| -0.99850 | -1.42242 | 1.73790 | 234.93231 | 0.048108 | 6 | 35.503 |
| 0.82544 | 0.24790 | 0.86234 | 16.70644 | 0.023871 | 7 | 41.420 |
| -0.43203 | -1.01254 | 1.10086 | 246.89322 | 0.030473 | 8 | 47.337 |
| 1.76225 | -0.04983 | 1.76295 | 358.38013 | 0.048801 | 9 | 53.254 |
| -0.41315 | -0.68037 | 0.79599 | 238.73192 | 0.022034 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.09364 | | | | | C | |
| -20.33417 | 15.44069 | 25.83763 | 141.90584 | 1.000000 | 1 | 5.917 |
| -1.04902 | 4.11210 | 4.27287 | 104.21185 | 0.165374 | 2 | 11.834 |
| -15.96028 | -3.38331 | 16.31079 | 191.89983 | 0.631280 | 3 | 17.751 |
| -0.42195 | -1.11757 | 1.19457 | 249.31532 | 0.046234 | 4 | 23.669 |
| -5.38512 | -1.84254 | 5.69160 | 198.88817 | 0.220283 | 5 | 29.586 |
| 1.56978 | -0.74910 | 1.73845 | 334.47534 | 0.067284 | 6 | 35.503 |
| -0.79660 | 0.76898 | 1.10735 | 136.01808 | 0.042858 | 7 | 41.420 |
| -0.10019 | 0.10236 | 0.14323 | 134.39405 | 0.005544 | 8 | 47.337 |
| -0.56231 | -0.23695 | 0.61029 | 202.44967 | 0.023617 | 9 | 53.254 |
| 0.10912 | -0.17945 | 0.20951 | 301.38918 | 0.008109 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 36.66518 | | | | | C | |
| 3.16593 | 41.36415 | 41.68454 | 85.64417 | 1.000000 | 1 | 5.917 |
| -2.71535 | 5.43382 | 11.13173 | 150.78117 | 0.267047 | 2 | 11.834 |
| -3.54119 | 0.42200 | 3.56625 | 173.20421 | 0.085553 | 3 | 17.751 |
| -2.02021 | -0.09549 | 2.02246 | 182.70616 | 0.048518 | 4 | 23.669 |
| -1.76268 | 0.08693 | 1.76482 | 177.17670 | 0.042337 | 5 | 29.586 |
| -1.76798 | -1.46827 | 2.29816 | 219.70894 | 0.055132 | 6 | 35.503 |
| 0.88014 | 1.12751 | 1.42484 | 51.85098 | 0.034181 | 7 | 41.420 |
| -1.68067 | 0.20052 | 1.69239 | 173.19626 | 0.040605 | 8 | 47.337 |
| 0.44720 | 0.21734 | 0.49721 | 25.91953 | 0.011928 | 9 | 53.254 |
| -0.96716 | -0.31219 | 1.01630 | 197.88962 | 0.024381 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 54.73444 | | | | | C | |
| -19.29793 | 22.23297 | 29.44002 | 130.95757 | 0.677493 | 1 | 5.917 |
| -5.81878 | 23.76741 | 24.46925 | 103.75603 | 0.558947 | 2 | 11.834 |
| -41.15700 | -14.91361 | 43.77742 | 199.92459 | 1.000000 | 3 | 17.751 |
| 3.46272 | -8.70489 | 9.36879 | 291.69214 | 0.213998 | 4 | 23.669 |
| -9.92905 | -0.98057 | 9.97540 | 185.52579 | 0.227866 | 5 | 29.586 |
| -2.01220 | -3.59604 | 4.12179 | 240.77469 | 0.094142 | 6 | 35.503 |
| 0.41968 | -1.55949 | 1.61401 | 295.07129 | 0.036869 | 7 | 41.420 |
| -2.07666 | 2.42774 | 3.19475 | 130.54338 | 0.072977 | 8 | 47.337 |
| -3.86217 | -1.34914 | 4.09103 | 199.25534 | 0.093451 | 9 | 53.254 |
| -0.54388 | -1.11435 | 1.26277 | 241.94495 | 0.028844 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 82.60177 | | | | | C | |
| -0.07829 | 96.45035 | 96.45035 | 90.05194 | 1.000000 | 1 | 5.917 |
| -17.87601 | 13.86179 | 22.60854 | 142.24860 | 0.261520 | 2 | 11.834 |
| -9.16163 | -1.09134 | 9.22840 | 186.79311 | 0.106725 | 3 | 17.751 |
| -1.99033 | 2.92230 | 3.44040 | 122.89737 | 0.040259 | 4 | 23.669 |
| -5.79229 | 3.41641 | 6.72497 | 149.46611 | 0.077790 | 5 | 29.586 |
| -8.92640 | -4.83151 | 8.12018 | 216.51253 | 0.093929 | 6 | 35.503 |
| 3.00117 | 4.15265 | 5.12359 | 54.14433 | 0.059266 | 7 | 41.420 |
| -8.96681 | 4.70395 | 9.40611 | 145.97360 | 0.097236 | 8 | 47.337 |
| -3.86011 | 0.79760 | 3.94165 | 168.32552 | 0.045594 | 9 | 53.254 |
| -2.81619 | 0.73475 | 2.71741 | 164.31779 | 0.031433 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.81190 | | | | | 0 | |
| 7.34850 | -2.72592 | 7.83780 | 339.64746 | 0.206934 | 1 | 5.917 |
| -4.63139 | 28.21846 | 28.59599 | 99.32066 | 0.754997 | 2 | 11.834 |
| -34.84749 | -14.84033 | 37.87589 | 203.06746 | 1.000000 | 3 | 17.751 |
| 4.70945 | -10.23315 | 11.26482 | 294.71240 | 0.297414 | 4 | 23.669 |
| -5.71779 | 0.60877 | 5.75011 | 173.92767 | 0.151814 | 5 | 29.586 |
| -4.18005 | -3.66646 | 5.56019 | 221.25508 | 0.146800 | 6 | 35.503 |
| 1.25850 | -2.99490 | 3.21173 | 293.06934 | 0.084796 | 7 | 41.420 |
| -1.93222 | 1.79651 | 2.61128 | 137.72728 | 0.068943 | 8 | 47.337 |
| -3.24422 | -1.58659 | 3.61140 | 206.06096 | 0.095348 | 9 | 53.254 |
| -0.95067 | -1.25512 | 1.57451 | 232.85835 | 0.041570 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 42.16490 | | | | | 0 | |
| 8.56780 | 33.49443 | 34.56792 | 75.68362 | 1.000000 | 1 | 5.917 |
| -1.63711 | 14.51085 | 14.60291 | 96.43696 | 0.422441 | 2 | 11.834 |
| -5.89658 | -3.07342 | 6.64770 | 207.53748 | 0.192308 | 3 | 17.751 |
| 4.03137 | 0.93627 | 4.13866 | 13.07487 | 0.119726 | 4 | 23.669 |
| -0.88026 | 4.38927 | 4.47666 | 101.33989 | 0.129503 | 5 | 29.586 |
| -4.45364 | -3.60194 | 5.72740 | 218.96461 | 0.165700 | 6 | 35.503 |
| 3.74868 | 0.11422 | 3.75042 | 1.74516 | 0.108494 | 7 | 41.420 |
| -1.70179 | 2.46690 | 2.74484 | 115.97392 | 0.079382 | 8 | 47.337 |
| -3.34293 | 1.22754 | 3.56118 | 159.83656 | 0.103020 | 9 | 53.254 |
| -1.74823 | -1.42149 | 3.09408 | 207.34970 | 0.089507 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.08894 | | | | | 0 | |
| 32.93987 | -35.11264 | 48.14490 | 313.17114 | 1.000000 | 1 | 5.917 |
| -1.25043 | 42.96710 | 42.99029 | 91.66719 | 0.892728 | 2 | 11.834 |
| -44.55415 | -17.01154 | 47.69135 | 200.89771 | 0.990579 | 3 | 17.751 |
| 4.51421 | -14.61474 | 15.29605 | 287.16479 | 0.317789 | 4 | 23.669 |
| -3.23647 | -0.33192 | 3.25345 | 185.85558 | 0.067576 | 5 | 29.586 |
| -4.23780 | -2.72693 | 5.03935 | 212.76033 | 0.104670 | 6 | 35.503 |
| 0.23475 | -3.86221 | 3.86933 | 273.47827 | 0.080368 | 7 | 41.420 |
| -0.49288 | -1.33605 | 1.42407 | 249.75060 | 0.029579 | 8 | 47.337 |
| -0.98126 | -1.82463 | 2.07175 | 241.72922 | 0.043032 | 9 | 53.254 |
| -1.45126 | -1.66111 | 2.20577 | 228.85725 | 0.045815 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.94813 | | | | | 0 | |
| 35.89224 | -20.53491 | 41.35130 | 330.22510 | 1.000000 | 1 | 5.917 |
| 19.29789 | 24.68686 | 29.01086 | 58.31505 | 0.701571 | 2 | 11.834 |
| -5.25497 | -8.49156 | 9.98603 | 238.24904 | 0.241493 | 3 | 17.751 |
| 13.67931 | -4.41449 | 14.37397 | 342.11426 | 0.347606 | 4 | 23.669 |
| 7.93330 | 6.27548 | 9.65202 | 40.55620 | 0.233415 | 5 | 29.586 |
| -2.25337 | -2.86097 | 3.64181 | 231.77516 | 0.088070 | 6 | 35.503 |
| 6.27790 | -7.60693 | 9.86292 | 309.53223 | 0.238515 | 7 | 41.420 |
| 9.32605 | -3.52031 | 9.96818 | 339.32129 | 0.241061 | 8 | 47.337 |
| 0.51241 | 1.88181 | 1.95567 | 74.20245 | 0.047294 | 9 | 53.254 |
| -3.74380 | -8.33798 | 7.30111 | 239.42990 | 0.178014 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.43558 | | | | | 0 | |
| 35.25105 | -37.20055 | 51.24956 | 313.45150 | 1.000000 | 1 | 5.917 |
| 6.53902 | 34.21931 | 34.83849 | 79.18161 | 0.679781 | 2 | 11.834 |
| -34.34764 | -8.66751 | 35.42436 | 194.16270 | 0.691213 | 3 | 17.751 |
| 0.35226 | -16.49030 | 16.49405 | 271.22363 | 0.321838 | 4 | 23.669 |
| 4.77101 | -2.32823 | 5.30879 | 333.98779 | 0.103587 | 5 | 29.586 |
| -1.18766 | 3.12291 | 3.34112 | 110.82216 | 0.065193 | 6 | 35.503 |
| -3.87615 | -3.81299 | 5.43722 | 224.92940 | 0.106093 | 7 | 41.420 |
| 2.17969 | -5.18343 | 5.62307 | 292.88713 | 0.109719 | 8 | 47.337 |
| 2.11071 | 0.13222 | 2.11485 | 3.58451 | 0.041266 | 9 | 53.254 |
| -2.01511 | -1.71005 | 2.64290 | 220.31839 | 0.051569 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -9.91276 | | | | | 0 | |
| 18.81487 | -18.70186 | 26.52844 | 315.17236 | 1.000000 | 1 | 5.917 |
| -5.29586 | 18.89760 | 19.62540 | 105.65280 | 0.739787 | 2 | 11.834 |
| -11.34631 | -15.09906 | 18.88702 | 233.07664 | 0.711954 | 3 | 17.751 |
| 11.43414 | -2.38272 | 11.67977 | 348.22876 | 0.440273 | 4 | 23.669 |
| 1.05857 | 6.48062 | 6.56651 | 80.72299 | 0.247527 | 5 | 29.586 |
| -4.31182 | -4.44217 | 6.19069 | 225.85304 | 0.233360 | 6 | 35.503 |
| 3.96481 | -4.66335 | 6.12099 | 310.37134 | 0.230733 | 7 | 41.420 |
| 2.31280 | -1.57606 | 2.80371 | 325.79639 | 0.105687 | 8 | 47.337 |
| 1.68188 | -1.41121 | 2.19550 | 320.00098 | 0.082760 | 9 | 53.254 |
| 0.76109 | -0.63120 | 0.98877 | 320.32935 | 0.037272 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.71305 | | | | | 0 | |
| 39.60817 | -45.07562 | 60.00514 | 311.30591 | 1.000000 | 1 | 5.917 |
| 5.65654 | 35.71957 | 36.16081 | 81.00035 | 0.602629 | 2 | 11.834 |
| -36.24031 | -9.01283 | 37.35295 | 193.96257 | 0.622496 | 3 | 17.751 |
| 0.38937 | -18.33612 | 18.34024 | 271.21655 | 0.305644 | 4 | 23.669 |
| 7.17903 | -2.95217 | 7.76233 | 337.64648 | 0.129361 | 5 | 29.586 |
| -0.49960 | 3.87176 | 3.90386 | 97.35271 | 0.065059 | 6 | 35.503 |
| -3.70656 | -4.32897 | 5.69899 | 229.42903 | 0.094975 | 7 | 41.420 |
| 2.25788 | -4.90121 | 5.39629 | 294.73438 | 0.089930 | 8 | 47.337 |
| 1.77257 | -1.39378 | 2.25491 | 321.82178 | 0.037579 | 9 | 53.254 |
| -0.10157 | -3.08057 | 3.08224 | 268.11133 | 0.051366 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.70383 | | | | | 0 | |
| 26.87242 | -6.73589 | 27.70377 | 345.92798 | 1.000000 | 1 | 5.917 |
| -4.99844 | 27.23976 | 27.69455 | 100.39804 | 0.999667 | 2 | 11.834 |
| -22.15523 | -11.66129 | 25.03676 | 207.75983 | 0.903731 | 3 | 17.751 |
| 3.08160 | -7.11586 | 7.75447 | 293.41553 | 0.279907 | 4 | 23.669 |
| 1.93576 | -1.19081 | 2.25200 | 329.26831 | 0.081289 | 5 | 29.586 |
| 0.95521 | -0.82336 | 1.26109 | 319.23975 | 0.045520 | 6 | 35.503 |
| 2.23153 | 0.67699 | 2.33196 | 16.87657 | 0.084175 | 7 | 41.420 |
| -3.02214 | -2.42033 | 3.87186 | 218.69000 | 0.139759 | 8 | 47.337 |
| 3.64511 | -3.94051 | 5.36791 | 312.76978 | 0.193761 | 9 | 53.254 |
| 2.72208 | 2.89428 | 3.98078 | 46.64081 | 0.143691 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR .84 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.45469 | | | | | 0 | |
| 19.65755 | -24.19311 | 31.14146 | 309.14111 | 1.000000 | 1 | 5.917 |
| 1.10145 | 17.43846 | 17.47321 | 86.38582 | 0.561091 | 2 | 11.834 |
| -17.80516 | -5.06729 | 18.51218 | 195.88615 | 0.594454 | 3 | 17.751 |
| 0.68392 | -8.52234 | 8.54974 | 274.59813 | 0.274545 | 4 | 23.669 |
| 3.31391 | -1.34948 | 3.57814 | 337.84277 | 0.114900 | 5 | 29.586 |
| -0.22964 | 1.30134 | 1.32144 | 100.00768 | 0.042434 | 6 | 35.503 |
| -0.99124 | -2.10243 | 2.32439 | 244.75728 | 0.074640 | 7 | 41.420 |
| 0.72085 | -1.57520 | 1.73231 | 294.59009 | 0.055627 | 8 | 47.337 |
| 0.30181 | -1.61333 | 1.64132 | 280.59595 | 0.052705 | 9 | 53.254 |
| 0.97893 | -1.98835 | 2.21626 | 296.21265 | 0.071160 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.40520 | | | | | 0 | |
| 18.92363 | 0.14823 | 18.92419 | 0.44879 | 1.000000 | 1 | 5.917 |
| 1.59126 | 16.82393 | 16.89900 | 84.59680 | 0.892984 | 2 | 11.834 |
| -13.87524 | -2.53472 | 14.10486 | 190.35260 | 0.745335 | 3 | 17.751 |
| -2.17227 | -5.91828 | 6.30434 | 249.84464 | 0.333137 | 4 | 23.669 |
| 2.49858 | -4.29481 | 4.96873 | 300.18945 | 0.262580 | 5 | 29.586 |
| 3.46601 | 1.74672 | 3.88727 | 26.74614 | 0.205095 | 6 | 35.503 |
| 0.47101 | 2.19991 | .24977 | 77.91524 | 0.118883 | 7 | 41.420 |
| -2.49888 | -2.01925 | 3.21275 | 218.94029 | 0.169769 | 8 | 47.337 |
| 2.59094 | -2.46931 | 3.57848 | 316.38843 | 0.189096 | 9 | 53.254 |
| 1.51196 | 1.99781 | 2.50545 | 52.88116 | 0.132394 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT PEAK SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.18385 | | | | | 0 | |
| 1.55884 | -1.93588 | 2.48548 | 308.84229 | 1.000000 | 1 | 5.917 |
| 0.68847 | 1.37833 | 1.38003 | 87.15616 | 0.555238 | 2 | 11.834 |
| -1.40867 | -0.40769 | 1.46648 | 196.14104 | 0.590017 | 3 | 17.751 |
| 0.05940 | -0.66959 | 0.67222 | 275.06905 | 0.270460 | 4 | 23.669 |
| 0.26113 | -0.10597 | 0.28182 | 337.91211 | 0.113385 | 5 | 29.586 |
| -0.01757 | 0.09685 | 0.09843 | 100.28160 | 0.039602 | 6 | 35.503 |
| -0.06931 | -0.16625 | 0.19012 | 247.36746 | 0.072470 | 7 | 41.420 |
| 0.05285 | -0.11530 | 0.12692 | 294.60889 | 0.051063 | 8 | 47.337 |
| 0.01753 | -0.13847 | 0.13957 | 277.21533 | 0.056156 | 9 | 53.254 |
| 0.08963 | -0.16313 | 0.18613 | 298.78613 | 0.074887 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT PEAK SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 184 TEST COND 25 COMP RUN 22.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.65833 | | | | | 0 | |
| 1.56261 | 0.05594 | 1.56361 | 2.05039 | 1.000000 | 1 | 5.917 |
| 0.16969 | 1.37213 | 1.38258 | 82.95023 | 0.884223 | 2 | 11.834 |
| -1.13561 | -0.18389 | 1.14737 | 188.21198 | 0.733795 | 3 | 17.751 |
| -0.21645 | -0.49884 | 0.54194 | 246.45932 | 0.346596 | 4 | 23.669 |
| 0.21477 | -0.38431 | 0.44025 | 299.19849 | 0.281560 | 5 | 29.586 |
| 0.30949 | 0.16946 | 0.35000 | 27.84125 | 0.223842 | 6 | 35.503 |
| 0.02946 | 0.19722 | 0.19941 | 81.50436 | 0.127531 | 7 | 41.420 |
| -0.21164 | -0.16911 | 0.27091 | 218.62669 | 0.173257 | 8 | 47.337 |
| 0.21465 | -0.20238 | 0.29501 | 316.68408 | 0.188673 | 9 | 53.254 |
| 0.12253 | 0.16474 | 0.20652 | 53.60696 | 0.132076 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.46538 | | | | | 0 | |
| -1.00815 | 1.30877 | 1.65204 | 127.60743 | 1.000000 | 1 | 5.917 |
| 0.19848 | -1.17852 | 1.19512 | 279.55981 | 0.723419 | 2 | 11.834 |
| 0.08096 | 0.45602 | 0.46315 | 79.93271 | 0.280349 | 3 | 17.751 |
| -0.11135 | -0.28456 | 0.30557 | 248.62901 | 0.184968 | 4 | 23.669 |
| 0.01797 | 0.05316 | 0.05612 | 71.32164 | 0.033968 | 5 | 29.586 |
| 0.07259 | 0.11759 | 0.13819 | 58.31276 | 0.083647 | 6 | 35.503 |
| -0.10355 | 0.27479 | 0.29365 | 110.64845 | 0.177751 | 7 | 41.420 |
| -0.17255 | 0.14786 | 0.22723 | 139.48459 | 0.137545 | 8 | 47.337 |
| -0.13183 | 0.03148 | 0.13553 | 166.56750 | 0.082040 | 9 | 53.254 |
| -0.03960 | -0.02251 | 0.04556 | 209.61639 | 0.027575 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.04479 | | | | | 0 | |
| -0.69833 | -1.89386 | 2.01851 | 249.75945 | 1.000000 | 1 | 5.917 |
| -1.27005 | -0.27750 | 1.30001 | 192.32512 | 0.644046 | 2 | 11.834 |
| -0.59767 | 0.02204 | 0.59808 | 177.88849 | 0.296297 | 3 | 17.751 |
| -0.05038 | -0.04433 | 0.06711 | 221.34839 | 0.033246 | 4 | 23.669 |
| -0.12916 | 0.29994 | 0.32581 | 112.65063 | 0.161415 | 5 | 29.586 |
| 0.30888 | 0.05496 | 0.30584 | 10.39200 | 0.151529 | 6 | 35.503 |
| 0.00408 | -0.20391 | 0.20395 | 271.12378 | 0.101041 | 7 | 41.420 |
| 0.13367 | -0.25819 | 0.28366 | 290.11377 | 0.140528 | 8 | 47.337 |
| 0.01760 | -0.23069 | 0.23136 | 274.36182 | 0.114621 | 9 | 53.254 |
| 0.02509 | -0.21119 | 0.21268 | 276.77612 | 0.105360 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.32941 | | | | | 0 | |
| -5.04516 | 6.32693 | 8.09220 | 128.56927 | 1.000000 | 1 | 5.917 |
| 1.01176 | -5.71453 | 5.80340 | 280.04004 | 0.717160 | 2 | 11.834 |
| 0.33016 | 2.19860 | 2.21534 | 81.42896 | 0.273763 | 3 | 17.751 |
| -0.53119 | -1.35866 | 1.45881 | 248.64467 | 0.180273 | 4 | 23.669 |
| 0.03584 | 0.20447 | 0.20759 | 80.05865 | 0.025653 | 5 | 29.586 |
| 0.36385 | 0.55035 | 0.66044 | 56.90968 | 0.082356 | 6 | 35.503 |
| -0.52772 | 1.28019 | 1.39209 | 112.27678 | 0.172029 | 7 | 41.420 |
| -0.08884 | 0.69871 | 1.06823 | 139.15018 | 0.132008 | 8 | 47.337 |
| -0.65024 | 0.14816 | 0.66691 | 167.16411 | 0.082414 | 9 | 53.254 |
| -0.20040 | -0.11153 | 0.22935 | 209.09721 | 0.028342 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.03312 | | | | | 0 | |
| -3.37613 | -8.93631 | 9.55279 | 249.30341 | 1.000000 | 1 | 5.917 |
| -6.14190 | -1.37100 | 6.29305 | 192.50331 | 0.658766 | 2 | 11.834 |
| -2.92159 | 0.10233 | 2.92338 | 177.99405 | 0.306024 | 3 | 17.751 |
| -0.26388 | -0.23971 | 0.35644 | 222.26157 | 0.037313 | 4 | 23.669 |
| -0.56087 | 1.48560 | 1.51337 | 111.75325 | 0.158422 | 5 | 29.586 |
| 1.43298 | 0.24327 | 1.45340 | 9.63476 | 0.152153 | 6 | 35.503 |
| 0.05248 | -0.98782 | 0.98922 | 273.04126 | 0.103552 | 7 | 41.420 |
| 0.62007 | -1.21649 | 1.36905 | 297.30713 | 0.143315 | 8 | 47.337 |
| 0.09308 | -1.12044 | 1.12430 | 274.74878 | 0.117693 | 9 | 53.254 |
| 0.13930 | -1.00241 | 1.01205 | 277.91138 | 0.105942 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XM-91A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.12398 | | | | | 0 | |
| -13.29905 | 15.66549 | 20.52339 | 130.24414 | 1.000000 | 1 | 5.917 |
| 2.73889 | -14.22638 | 14.48763 | 280.89722 | 0.705908 | 2 | 11.834 |
| 0.54360 | 5.36177 | 5.38925 | 84.21082 | 0.262591 | 3 | 17.751 |
| -1.28343 | -3.28006 | 3.52967 | 248.67770 | 0.171983 | 4 | 23.669 |
| -0.13959 | 0.27125 | 0.30586 | 117.23172 | 0.014864 | 5 | 29.586 |
| 0.95884 | 1.33734 | 1.64555 | 54.31035 | 0.080179 | 6 | 35.503 |
| -1.42799 | 3.00975 | 3.33133 | 115.38226 | 0.162319 | 7 | 41.420 |
| -1.88402 | 1.65816 | 2.50979 | 138.64842 | 0.122289 | 8 | 47.337 |
| -1.66887 | 0.34876 | 1.70414 | 168.19086 | 0.083034 | 9 | 53.254 |
| -0.93622 | -0.28823 | 0.60877 | 208.25903 | 0.029662 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XM-91A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.73878 | | | | | 0 | |
| -0.38814 | -21.14618 | 22.73878 | 268.42899 | 1.000000 | 1 | 5.917 |
| -15.21701 | -3.92659 | 15.62831 | 193.04814 | 0.6868944 | 2 | 11.834 |
| -7.37844 | 0.23459 | 7.50216 | 178.17896 | 0.324651 | 3 | 17.751 |
| -0.74581 | -0.70714 | 1.02638 | 223.55223 | 0.045195 | 4 | 23.669 |
| -1.19895 | 3.28160 | 3.49183 | 109.94675 | 0.153527 | 5 | 29.586 |
| 3.45162 | 0.58188 | 3.48792 | 9.27388 | 0.153391 | 6 | 35.503 |
| 0.27821 | -2.45518 | 2.47089 | 276.64484 | 0.108664 | 7 | 41.420 |
| 1.47487 | -3.04358 | 3.38168 | 295.84253 | 0.148719 | 8 | 47.337 |
| 0.26631 | -2.79762 | 2.81827 | 275.43774 | 0.123989 | 9 | 53.254 |
| 0.42541 | -2.39987 | 2.43649 | 280.05518 | 0.107151 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 50
MODEL XM-91A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.86111 | | | | | 0 | |
| -36.99488 | 35.63954 | 51.36859 | 136.06833 | 1.000000 | 1 | 5.917 |
| 8.97168 | -33.93198 | 34.48877 | 284.42578 | 0.669882 | 2 | 11.834 |
| -0.95944 | 11.92633 | 11.96486 | 94.99943 | 0.232922 | 3 | 17.751 |
| -2.62266 | -0.86194 | 7.34578 | 249.08183 | 0.143000 | 4 | 23.669 |
| -2.13725 | -1.38395 | 2.58362 | 211.38757 | 0.048738 | 5 | 29.586 |
| 2.63343 | 2.89038 | 3.88867 | 47.26538 | 0.075545 | 6 | 35.503 |
| -4.35975 | 5.27258 | 6.84154 | 129.58405 | 0.133185 | 7 | 41.420 |
| -3.17578 | 3.21951 | 4.58225 | 134.68832 | 0.088835 | 8 | 47.337 |
| -4.34694 | 0.78671 | 4.43374 | 170.04284 | 0.086312 | 9 | 53.254 |
| -1.63245 | 2.74895 | 1.79685 | 284.84525 | 0.034964 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 50
MODEL XM-91A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.98620 | | | | | 0 | |
| -19.38782 | -40.59293 | 44.94833 | 244.56877 | 1.000000 | 1 | 5.917 |
| -34.64923 | -9.44356 | 35.91389 | 193.24551 | 0.799086 | 2 | 11.834 |
| -18.23441 | 0.44315 | 18.23978 | 178.68782 | 0.405794 | 3 | 17.751 |
| -2.47888 | -2.69886 | 3.62858 | 226.79143 | 0.080748 | 4 | 23.669 |
| -0.87169 | 5.77330 | 5.84871 | 98.56311 | 0.129943 | 5 | 29.586 |
| 6.97669 | 0.25297 | 6.98127 | 2.07662 | 0.155318 | 6 | 35.503 |
| 1.99868 | -5.83635 | 6.16811 | 288.87780 | 0.137227 | 7 | 41.420 |
| 2.81701 | -7.24554 | 7.77398 | 291.24561 | 0.172952 | 8 | 47.337 |
| 0.98871 | -6.57398 | 6.64663 | 278.48486 | 0.147873 | 9 | 53.254 |
| 1.79914 | -4.73407 | 5.09833 | 290.98652 | 0.113359 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.61247 | | | | | C | |
| -44.64763 | 30.61540 | 54.13606 | 145.56113 | 1.000000 | 1 | 5.917 |
| 11.40649 | -30.04644 | 32.13872 | 290.78809 | 0.593666 | 2 | 11.834 |
| -5.30341 | 9.33457 | 10.73593 | 119.60300 | 0.198314 | 3 | 17.751 |
| -1.71281 | -4.64639 | 4.95204 | 249.76447 | 0.091474 | 4 | 23.669 |
| -5.56568 | -4.98160 | 7.44948 | 221.83037 | 0.137976 | 5 | 29.586 |
| 3.20382 | 1.78981 | 3.66986 | 29.18900 | 0.067790 | 6 | 35.503 |
| -5.79526 | 1.52503 | 5.99256 | 165.29679 | 0.110694 | 7 | 41.420 |
| -0.73712 | 1.60106 | 1.76259 | 114.72110 | 0.032559 | 8 | 47.337 |
| -4.79068 | 0.41819 | 4.76905 | 174.96931 | 0.088094 | 9 | 53.254 |
| -2.10011 | -0.83987 | 2.26153 | 201.77858 | 0.041775 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 21.37607 | | | | | 0 | |
| -16.72455 | -18.99852 | 25.31114 | 228.64224 | 0.799222 | 1 | 5.917 |
| -29.89888 | -10.44164 | 31.66471 | 199.25882 | 1.000000 | 2 | 11.834 |
| -18.16350 | 0.10232 | 18.16377 | 179.67723 | 0.573538 | 3 | 17.751 |
| -3.64029 | -4.18117 | 5.54382 | 228.95587 | 0.175051 | 4 | 23.669 |
| 2.68486 | 1.66549 | 3.09179 | 32.59393 | 0.097626 | 5 | 29.586 |
| 4.36707 | -1.44476 | 4.60617 | 341.65776 | 0.145444 | 6 | 35.503 |
| 4.22127 | -5.24803 | 6.73505 | 308.81192 | 0.212665 | 7 | 41.420 |
| 1.14730 | -6.77098 | 6.86749 | 279.61694 | 0.216847 | 8 | 47.337 |
| 1.46998 | -6.03978 | 6.21689 | 283.67871 | 0.196279 | 9 | 53.254 |
| 2.89649 | -2.68199 | 3.94750 | 317.20198 | 0.124646 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.85431 | | | | | C | |
| -54.79836 | 30.93896 | 62.89433 | 150.93317 | 1.000000 | 1 | 5.917 |
| 10.62166 | -28.23685 | 30.16850 | 290.61490 | 0.479670 | 2 | 11.834 |
| -11.35767 | 4.77439 | 12.32036 | 157.19972 | 0.195890 | 3 | 17.751 |
| -1.68642 | -2.72813 | 3.20729 | 238.27730 | 0.050995 | 4 | 23.669 |
| -11.59486 | -10.48450 | 15.68195 | 222.22153 | 0.249066 | 5 | 29.586 |
| 4.80375 | -1.96702 | 5.19887 | 337.73193 | 0.082533 | 6 | 35.503 |
| -6.98989 | -8.99513 | 7.08037 | 188.10254 | 0.112258 | 7 | 41.420 |
| -0.67282 | -0.73538 | 0.99673 | 227.54384 | 0.015848 | 8 | 47.337 |
| -4.56605 | -2.02438 | 4.99469 | 203.91028 | 0.079414 | 9 | 53.254 |
| -1.79661 | -1.10265 | 2.10800 | 211.53894 | 0.033516 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.12654 | | | | | C | |
| -12.97881 | 10.18791 | 16.18781 | 140.99510 | 0.907457 | 1 | 5.917 |
| -30.66759 | -8.77504 | 31.89830 | 195.96762 | 1.000000 | 2 | 11.834 |
| -17.39844 | -1.01237 | 17.38815 | 183.33775 | 0.545112 | 3 | 17.751 |
| -5.23810 | -5.20450 | 7.37840 | 224.85942 | 0.231310 | 4 | 23.669 |
| 3.83551 | -1.94593 | 4.30090 | 333.09912 | 0.134832 | 5 | 29.586 |
| 3.63064 | -2.80339 | 4.58699 | 322.32642 | 0.143800 | 6 | 35.503 |
| 5.20037 | -2.50797 | 5.77354 | 334.25342 | 0.180998 | 7 | 41.420 |
| -3.02477 | -6.72694 | 7.37569 | 245.78886 | 0.231225 | 8 | 47.337 |
| 1.69992 | -6.47208 | 6.59829 | 279.30954 | 0.206900 | 9 | 53.254 |
| 2.79525 | -1.34478 | 3.10191 | 334.30786 | 0.097244 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.66522 | | | | | 0 | |
| -41.56508 | 23.14043 | 47.57242 | 150.89412 | 1.000000 | 1 | 5.917 |
| 1.23737 | -14.97900 | 15.03002 | 274.72217 | 0.315940 | 2 | 11.834 |
| -14.03838 | -3.64712 | 14.50439 | 194.56376 | 0.304891 | 3 | 17.751 |
| -1.76525 | -0.27808 | 1.78701 | 188.95212 | 0.037564 | 4 | 23.669 |
| -14.37739 | -12.53005 | 19.07121 | 221.07748 | 0.400888 | 5 | 29.586 |
| 5.21669 | -7.18714 | 8.88081 | 305.97335 | 0.186680 | 6 | 35.503 |
| -4.57585 | -1.46289 | 4.80400 | 197.72893 | 0.100983 | 7 | 41.420 |
| -2.66850 | -3.08821 | 4.08141 | 229.16989 | 0.085794 | 8 | 47.337 |
| -1.83554 | -5.34167 | 5.64825 | 251.03571 | 0.118730 | 9 | 53.254 |
| 0.11366 | -1.09732 | 1.10319 | 275.91455 | 0.023190 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 22.12680 | | | | | 0 | |
| -1.82999 | 39.62907 | 39.67130 | 92.64397 | 1.000000 | 1 | 5.917 |
| -23.88918 | -0.35839 | 23.89186 | 180.85947 | 0.602246 | 2 | 11.834 |
| -8.35210 | -2.52954 | 8.72675 | 196.84956 | 0.219976 | 3 | 17.751 |
| -4.64168 | -3.30063 | 5.69555 | 215.41608 | 0.143569 | 4 | 23.669 |
| 0.82723 | -3.66089 | 3.75319 | 282.73291 | 0.094607 | 5 | 29.586 |
| 3.28075 | -2.29650 | 4.00465 | 325.09806 | 0.100946 | 6 | 35.503 |
| 2.55460 | 3.02504 | 3.96628 | 49.90321 | 0.099979 | 7 | 41.420 |
| -7.69267 | -4.06175 | 8.69914 | 207.83412 | 0.219280 | 8 | 47.337 |
| -0.71283 | -4.92553 | 4.97684 | 261.76514 | 0.125452 | 9 | 53.254 |
| 0.13016 | -0.43921 | 0.45713 | 286.54224 | 0.011523 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.28008 | | | | | 0 | |
| -23.61282 | 13.46971 | 26.66499 | 149.65901 | 1.000000 | 1 | 5.917 |
| -4.27532 | -3.42692 | 5.47946 | 218.71428 | 0.205485 | 2 | 11.834 |
| -12.47282 | -7.17900 | 14.39129 | 209.92348 | 0.539707 | 3 | 17.751 |
| -1.26394 | 0.69110 | 1.44054 | 151.33080 | 0.054024 | 4 | 23.669 |
| -11.85096 | -9.99107 | 15.50054 | 220.13290 | 0.581307 | 5 | 29.586 |
| 4.12234 | -7.81862 | 8.83881 | 297.80029 | 0.331476 | 6 | 35.503 |
| -1.89966 | -1.08647 | 2.18840 | 209.76659 | 0.082070 | 7 | 41.420 |
| -2.87362 | -3.16835 | 4.27740 | 227.79269 | 0.160413 | 8 | 47.337 |
| -0.04587 | -5.38474 | 5.38493 | 269.51172 | 0.201947 | 9 | 53.254 |
| 1.13405 | -0.91892 | 1.45962 | 320.98218 | 0.054739 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 14.24753 | | | | | 0 | |
| 3.73165 | 43.51823 | 43.67792 | 85.09889 | 1.000000 | 1 | 5.917 |
| -15.05708 | 4.46639 | 15.70555 | 163.47804 | 0.359576 | 2 | 11.834 |
| -1.90644 | -2.89853 | 3.46929 | 236.66594 | 0.079429 | 3 | 17.751 |
| -2.87949 | -1.47609 | 3.23578 | 207.14066 | 0.074083 | 4 | 23.669 |
| -1.14484 | -3.22797 | 3.42498 | 250.47229 | 0.078414 | 5 | 29.586 |
| 2.28975 | -1.27794 | 2.62223 | 330.69150 | 0.060036 | 6 | 35.503 |
| 0.61167 | 4.61386 | 4.65403 | 82.44780 | 0.106553 | 7 | 41.420 |
| -7.47742 | -1.52215 | 7.63077 | 191.50624 | 0.174705 | 8 | 47.337 |
| -1.44488 | -2.76970 | 3.12393 | 242.45004 | 0.071522 | 9 | 53.254 |
| -1.36890 | -0.16607 | 1.37883 | 186.91750 | 0.031568 | 10 | 59.172 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J C | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.43290 | | | | | | |
| -16.32727 | 11.12089 | 19.75484 | 145.74031 | 1.000000 | 1 | 5.917 |
| -6.85196 | 3.55469 | 7.71914 | 152.58047 | 0.390747 | 2 | 11.834 |
| -14.85697 | -9.64587 | 17.71361 | 212.99358 | 0.896672 | 3 | 17.751 |
| -0.46748 | 0.72865 | 0.86577 | 122.68303 | 0.043823 | 4 | 23.669 |
| -11.33256 | -9.00734 | 14.47615 | 218.47835 | 0.732790 | 5 | 29.586 |
| 4.02298 | -8.24437 | 9.17355 | 296.01074 | 0.464370 | 6 | 35.503 |
| -0.24492 | -1.38264 | 1.40416 | 259.95459 | 0.071079 | 7 | 41.420 |
| -1.85679 | -2.62021 | 3.21141 | 234.67647 | 0.162563 | 8 | 47.337 |
| 0.19235 | -4.78905 | 4.79290 | 272.30005 | 0.242619 | 9 | 53.254 |
| 1.65051 | -1.44909 | 2.19637 | 318.71777 | 0.111181 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J C | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.41586 | | | | | | |
| 4.65024 | 51.29723 | 51.50757 | 84.82007 | 1.000000 | 1 | 5.917 |
| -13.64050 | 7.09391 | 14.84514 | 151.45424 | 0.288213 | 2 | 11.834 |
| -0.18272 | -3.19746 | 3.20264 | 266.74170 | 0.062178 | 3 | 17.751 |
| -2.32474 | -1.30695 | 2.66693 | 209.34427 | 0.051777 | 4 | 23.669 |
| -1.69547 | -3.33619 | 3.72434 | 243.60867 | 0.072307 | 5 | 29.586 |
| 1.50340 | -0.81247 | 1.70889 | 331.61206 | 0.033178 | 6 | 35.503 |
| 0.64928 | 4.17307 | 4.29862 | 78.49657 | 0.082679 | 7 | 41.420 |
| -6.33554 | 0.25584 | 6.34070 | 177.68933 | 0.123102 | 8 | 47.337 |
| -1.90523 | -1.74878 | 2.58614 | 222.54829 | 0.050209 | 9 | 53.254 |
| -1.93070 | -0.57250 | 2.01379 | 196.51634 | 0.039097 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J C | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.75197 | | | | | | |
| -9.92661 | 12.57838 | 16.02194 | 128.28426 | 0.365163 | 1 | 5.917 |
| -15.95340 | 29.29552 | 33.35773 | 118.57137 | 0.760270 | 2 | 11.834 |
| -37.60579 | -22.60362 | 43.87617 | 211.00870 | 1.000000 | 3 | 17.751 |
| 2.65928 | -0.53874 | 2.71330 | 348.54736 | 0.061848 | 4 | 23.669 |
| -16.51717 | -11.27869 | 20.00063 | 214.32706 | 0.455942 | 5 | 29.586 |
| 6.79599 | -12.21239 | 13.97598 | 299.09521 | 0.318532 | 6 | 35.503 |
| 4.17371 | -3.75023 | 5.61107 | 318.05908 | 0.127884 | 7 | 41.420 |
| 2.96615 | -0.78709 | 3.06880 | 345.13843 | 0.069942 | 8 | 47.337 |
| -0.74539 | -3.34147 | 3.42360 | 257.42480 | 0.078029 | 9 | 53.254 |
| 3.65935 | -4.59338 | 5.87281 | 308.54272 | 0.133850 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J C | FREQUENCY |
|---|---|---|---|---|---|---|
| 95.84401 | | | | | | |
| 5.50735 | 102.56303 | 102.71077 | 86.92627 | 1.000000 | 1 | 5.917 |
| -20.26506 | 18.32693 | 27.32301 | 137.87509 | 0.266019 | 2 | 11.834 |
| -0.73299 | -7.56924 | 7.60465 | 264.46875 | 0.074039 | 3 | 17.751 |
| -1.30236 | -3.32421 | 3.57022 | 248.60574 | 0.034760 | 4 | 23.669 |
| -2.28698 | -5.33378 | 5.80341 | 246.79164 | 0.056502 | 5 | 29.586 |
| -1.15033 | -0.20785 | 1.16896 | 190.24213 | 0.011381 | 6 | 35.503 |
| 4.87645 | 0.79888 | 4.94146 | 9.30378 | 0.048110 | 7 | 41.420 |
| -2.36800 | 5.59741 | 6.07770 | 112.93100 | 0.059173 | 8 | 47.337 |
| -3.46999 | 0.50198 | 3.50611 | 171.76859 | 0.034136 | 9 | 53.254 |
| -3.75177 | -3.07479 | 4.85072 | 219.33571 | 0.047227 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.55352 | | | | | 0 | |
| 13.49402 | -8.75489 | 16.08528 | 327.02441 | 0.412261 | 1 | 5.917 |
| -13.04769 | 36.77092 | 39.01720 | 109.53461 | 1.000000 | 2 | 11.834 |
| -32.24901 | -18.99945 | 37.42963 | 210.50438 | 0.959311 | 3 | 17.751 |
| 3.18153 | -3.13409 | 4.46931 | 314.70068 | 0.113009 | 4 | 23.669 |
| -6.68465 | -4.13400 | 7.85968 | 211.73393 | 0.201441 | 5 | 29.586 |
| 2.83300 | -3.11758 | 4.21290 | 312.26196 | 0.107965 | 6 | 35.503 |
| 2.31619 | -2.19823 | 3.19327 | 316.49658 | 0.081843 | 7 | 41.420 |
| 3.82699 | 0.76849 | 3.90186 | 11.24286 | 0.100004 | 8 | 47.337 |
| -0.12294 | 0.72482 | 0.73517 | 99.62698 | 0.018842 | 9 | 53.254 |
| 2.43155 | -1.73344 | 2.98617 | 324.51489 | 0.076535 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 21.48846 | | | | | 0 | |
| 10.19318 | 35.65765 | 37.08595 | 74.04672 | 1.000000 | 1 | 5.917 |
| -6.44601 | 16.97101 | 18.15393 | 110.72887 | 0.489510 | 2 | 11.834 |
| -2.59403 | -7.60747 | 8.02475 | 251.44170 | 0.216382 | 3 | 17.751 |
| 2.97932 | -1.97348 | 3.57365 | 326.47949 | 0.096361 | 4 | 23.669 |
| -8.86247 | -2.68218 | 2.81743 | 252.17495 | 0.075970 | 5 | 29.586 |
| -1.71139 | 0.32742 | 1.74243 | 169.16911 | 0.046984 | 6 | 35.503 |
| 1.98139 | -2.82772 | 3.45281 | 305.01800 | 0.093103 | 7 | 41.420 |
| 4.87763 | 1.87764 | 4.48016 | 24.72481 | 0.121048 | 8 | 47.337 |
| 0.98864 | 2.66120 | 2.83613 | 69.77136 | 0.076475 | 9 | 53.254 |
| -2.98277 | -1.19803 | 2.48273 | 209.98797 | 0.066789 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -8.59837 | | | | | 0 | |
| 37.40929 | -40.19875 | 54.88332 | 312.96997 | 0.952824 | 1 | 5.917 |
| -16.94331 | 55.05237 | 57.60068 | 107.10670 | 1.000000 | 2 | 11.834 |
| -41.74091 | -25.13327 | 48.72354 | 211.05321 | 0.845805 | 3 | 17.751 |
| 0.21688 | -6.37485 | 6.37851 | 271.94116 | 0.110737 | 4 | 23.669 |
| -5.66558 | -7.05102 | 9.04520 | 231.21767 | 0.157033 | 5 | 29.586 |
| 2.79080 | 2.08433 | 3.48324 | 36.79447 | 0.060472 | 6 | 35.503 |
| -3.93805 | 1.10205 | 4.09934 | 164.36994 | 0.070995 | 7 | 41.420 |
| -0.87718 | -2.14774 | 2.31994 | 247.78963 | 0.040276 | 8 | 47.337 |
| 2.78543 | -0.68414 | 2.86827 | 346.20044 | 0.049795 | 9 | 53.254 |
| 2.57018 | 3.64706 | 4.46237 | 54.83255 | 0.077471 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -111.63611 | | | | | 0 | |
| 30.09181 | -25.30255 | 39.31584 | 319.94116 | 1.000000 | 1 | 5.917 |
| -5.33457 | 25.42287 | 25.97652 | 101.85068 | 0.660714 | 2 | 11.834 |
| -6.09844 | -20.07159 | 20.97760 | 253.09924 | 0.533566 | 3 | 17.751 |
| 12.48620 | 0.37744 | 12.49190 | 1.73146 | 0.317732 | 4 | 23.669 |
| -2.12759 | 0.70132 | 2.24019 | 161.75626 | 0.056979 | 5 | 29.586 |
| -1.68150 | -0.58670 | 1.78091 | 199.23453 | 0.045297 | 6 | 35.503 |
| -4.01428 | -2.38018 | 4.66687 | 210.66496 | 0.118702 | 7 | 41.420 |
| 5.41841 | -8.89799 | 8.77162 | 308.14966 | 0.223107 | 8 | 47.337 |
| 8.04043 | 4.96167 | 8.49842 | 35.95936 | 0.214937 | 9 | 53.254 |
| -3.12247 | 2.31375 | 3.88629 | 143.46195 | 0.098848 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -14.73008 | | | | | C | |
| 35.23986 | -37.26355 | 51.30135 | 313.41724 | 1.000000 | 1 | 5.917 |
| -6.62609 | 41.23286 | 41.76187 | 99.12936 | 0.814050 | 2 | 11.834 |
| -28.12054 | -11.58677 | 30.41411 | 202.39359 | 0.592632 | 3 | 17.751 |
| -7.02561 | -2.68854 | 7.52174 | 200.92647 | 0.146619 | 4 | 23.669 |
| -5.75377 | -12.53385 | 13.79142 | 245.34206 | 0.268831 | 5 | 29.586 |
| 9.56167 | 1.66349 | 9.78529 | 9.86927 | 0.190682 | 6 | 35.503 |
| -4.28876 | 7.26133 | 8.43329 | 120.56741 | 0.164387 | 7 | 41.420 |
| -4.61952 | -2.90116 | 5.45497 | 212.12970 | 0.106332 | 8 | 47.337 |
| 3.44562 | -1.63402 | 3.81344 | 334.62817 | 0.074334 | 9 | 53.254 |
| 2.17906 | 4.83676 | 5.30496 | 65.74739 | 0.103408 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -28.27319 | | | | | C | |
| 14.66709 | -0.05876 | 14.66720 | 359.77026 | 0.346750 | 1 | 5.917 |
| -35.80858 | 17.49153 | 39.85231 | 153.96574 | 0.942155 | 2 | 11.834 |
| -5.63698 | -41.97281 | 42.29909 | 262.34155 | 1.000000 | 3 | 17.751 |
| 26.13074 | 4.09023 | 26.44275 | 8.81065 | 0.625138 | 4 | 23.669 |
| -6.16080 | 13.90244 | 15.20636 | 113.90033 | 0.359496 | 5 | 29.586 |
| -10.77946 | -2.72587 | 11.11877 | 194.19121 | 0.262861 | 6 | 35.503 |
| 0.73360 | -6.98759 | 7.02599 | 275.99316 | 0.166103 | 7 | 41.420 |
| 7.68161 | -1.67605 | 7.86233 | 347.69141 | 0.185875 | 8 | 47.337 |
| 1.14092 | 3.27511 | 3.33330 | 82.15300 | 0.197482 | 9 | 53.254 |
| -0.84513 | -1.97491 | 6.92902 | 188.92442 | 0.163810 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -20.64124 | | | | | 0 | |
| 33.99860 | -43.22914 | 54.99693 | 308.18408 | 1.000000 | 1 | 5.917 |
| -8.97183 | 38.66653 | 39.60526 | 102.49960 | 0.720136 | 2 | 11.834 |
| -25.60101 | -10.97982 | 27.85620 | 203.21362 | 0.506905 | 3 | 17.751 |
| -10.36157 | 1.97494 | 10.54811 | 169.20972 | 0.191794 | 4 | 23.669 |
| -12.16691 | -16.45380 | 20.46364 | 233.51857 | 0.372087 | 5 | 29.586 |
| 12.98661 | -4.16415 | 13.63789 | 342.22144 | 0.247975 | 6 | 35.503 |
| 0.28128 | 9.74998 | 9.75403 | 88.34744 | 0.177356 | 7 | 41.420 |
| -6.48270 | 0.43023 | 6.49496 | 176.20300 | 0.118133 | 8 | 47.337 |
| 1.47373 | -2.70730 | 3.08243 | 298.56177 | 0.056047 | 9 | 53.254 |
| 2.00633 | 3.49063 | 4.02614 | 60.11073 | 0.073207 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.73653 | | | | | 0 | |
| 23.04893 | 31.97220 | 39.41414 | 54.21193 | 0.769676 | 1 | 5.917 |
| -44.78143 | 24.83867 | 51.20874 | 150.98444 | 1.000000 | 2 | 11.834 |
| -14.95159 | -46.88257 | 49.20898 | 252.31165 | 0.960949 | 3 | 17.751 |
| 24.79092 | -4.31693 | 25.12456 | 350.10620 | 0.490838 | 4 | 23.669 |
| 5.28066 | 12.93050 | 13.96722 | 67.78548 | 0.272751 | 5 | 29.586 |
| -13.13607 | 9.40533 | 16.15599 | 144.39763 | 0.315493 | 6 | 35.503 |
| -7.38086 | -10.40174 | 12.75434 | 234.64125 | 0.249066 | 7 | 41.420 |
| 10.97567 | -5.71184 | 12.37298 | 332.50700 | 0.241618 | 8 | 47.337 |
| 2.08686 | 12.94069 | 13.10787 | 80.83910 | 0.259969 | 9 | 53.254 |
| -12.07636 | 0.00039 | 12.07636 | 179.99814 | 0.235826 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 CSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.82507 | | | | | 0 | |
| 14.94649 | -22.99886 | 27.42889 | 303.01904 | 1.000000 | 1 | 5.917 |
| -6.06596 | 17.40974 | 18.43623 | 109.20958 | 0.672146 | 2 | 11.834 |
| -11.56504 | -6.29555 | 13.16754 | 208.56213 | 0.480061 | 3 | 17.751 |
| -5.24355 | 2.55408 | 5.83250 | 154.02979 | 0.212641 | 4 | 23.669 |
| -8.27093 | -8.30851 | 11.72346 | 225.12984 | 0.427413 | 5 | 29.586 |
| 6.27302 | -4.37696 | 7.64909 | 325.09473 | 0.278870 | 6 | 35.503 |
| 2.13224 | 4.70894 | 5.16920 | 65.63860 | 0.188458 | 7 | 41.420 |
| -3.44000 | 1.79486 | 3.88009 | 152.44921 | 0.141460 | 8 | 47.337 |
| -0.31399 | -1.64885 | 1.67848 | 259.21802 | 0.061194 | 9 | 53.254 |
| 0.80159 | 0.90833 | 1.21145 | 48.57193 | 0.044167 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 CSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 22.05492 | | | | | 0 | |
| 16.88136 | 23.08122 | 28.59584 | 53.81862 | 1.000000 | 1 | 5.917 |
| -19.23248 | 15.49883 | 24.70023 | 141.13580 | 0.863770 | 2 | 11.834 |
| -11.18937 | -19.86676 | 22.80109 | 240.61081 | 0.797357 | 3 | 17.751 |
| 8.33278 | -6.38542 | 10.49804 | 322.53687 | 0.367118 | 4 | 23.669 |
| 8.45108 | 1.36768 | 9.09736 | 21.72684 | 0.318136 | 5 | 29.586 |
| -5.47509 | 10.29099 | 11.65681 | 118.01424 | 0.407640 | 6 | 35.503 |
| -8.12926 | -5.41332 | 9.76672 | 213.65988 | 0.341543 | 7 | 41.420 |
| 5.97492 | -5.57854 | 8.17433 | 316.96484 | 0.285857 | 8 | 47.337 |
| 2.38680 | 7.43093 | 7.80484 | 72.19301 | 0.272936 | 9 | 53.254 |
| -7.25605 | 1.17463 | 7.35051 | 170.80453 | 0.257048 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.86670 | | | | | 0 | |
| 1.16195 | -1.84082 | 2.17686 | 302.26074 | 1.000000 | 1 | 5.917 |
| -0.50071 | 1.35769 | 1.44708 | 110.24362 | 0.664754 | 2 | 11.834 |
| -0.90184 | -0.50705 | 1.03461 | 209.34622 | 0.475274 | 3 | 17.751 |
| -0.41818 | 0.22177 | 0.47335 | 152.06161 | 0.217445 | 4 | 23.669 |
| -0.68241 | -0.66160 | 0.95048 | 224.11285 | 0.436626 | 5 | 29.586 |
| 0.49679 | -0.37462 | 0.62221 | 322.98071 | 0.285828 | 6 | 35.503 |
| 0.19278 | 0.37289 | 0.41977 | 62.66145 | 0.192834 | 7 | 41.420 |
| -0.27583 | 0.16095 | 0.31936 | 149.73605 | 0.146705 | 8 | 47.337 |
| -0.03719 | -0.13443 | 0.13948 | 254.53773 | 0.064075 | 9 | 53.254 |
| 0.06128 | 0.06232 | 0.08740 | 45.48511 | 0.040150 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 264 TEST COND 26 COMP RUN 11.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.86744 | | | | | 0 | |
| 1.39956 | 1.92310 | 2.37846 | 53.95427 | 1.000000 | 1 | 5.917 |
| -1.49590 | 1.26520 | 1.95920 | 139.77618 | 0.823726 | 2 | 11.834 |
| -0.93161 | -1.53940 | 1.79935 | 238.81874 | 0.756517 | 3 | 17.751 |
| 0.61667 | -0.55578 | 0.83016 | 317.97241 | 0.369034 | 4 | 23.669 |
| 0.73811 | 0.23347 | 0.77415 | 17.55243 | 0.325484 | 5 | 29.586 |
| -0.42368 | 0.88196 | 0.97845 | 115.65886 | 0.411377 | 6 | 35.503 |
| -0.69610 | -0.43325 | 0.81992 | 211.89796 | 0.344725 | 7 | 41.420 |
| 0.48059 | -0.47335 | 0.67456 | 315.43433 | 0.283611 | 8 | 47.337 |
| 0.20396 | 0.60182 | 0.63544 | 71.27831 | 0.267164 | 9 | 53.254 |
| -0.59101 | 0.10618 | 0.60048 | 169.81473 | 0.252464 | 10 | 59.172 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.08770 | | | | | 0 | |
| -0.[illegible]4203 | 1.15083 | 1.49358 | 129.59926 | 1.000000 | 1 | 5.848 |
| 0.17[illegible]2[illegible] | -1.33408 | 1.34594 | 277.61035 | 0.901151 | 2 | 11.696 |
| 0.27341 | 0.43187 | 0.51114 | 57.66312 | 0.342226 | 3 | 17.544 |
| -0.17090 | -0.44014 | 0.47215 | 248.77988 | 0.316120 | 4 | 23.392 |
| 0.18731 | 0.04017 | 0.19157 | 12.10343 | 0.128261 | 5 | 29.240 |
| 0.16445 | 0.00085 | 0.16445 | 0.29615 | 0.110108 | 6 | 35.088 |
| 0.03796 | 0.26663 | 0.26932 | 81.89658 | 0.180318 | 7 | 40.936 |
| -0.17628 | 0.19047 | 0.25952 | 132.78413 | 0.173757 | 8 | 46.784 |
| -0.14711 | 0.0.419 | 0.14780 | 174.49147 | 0.098955 | 9 | 52.632 |
| -0.04200 | 0.02640 | 0.04739 | 154.93246 | 0.045118 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.43333 | | | | | 0 | |
| -1.15402 | -1.49117 | 1.85489 | 231.98708 | 1.000000 | 1 | 5.848 |
| -1.08679 | -0.24784 | 1.11451 | 192.88647 | 0.601108 | 2 | 11.696 |
| -0.83287 | 0.27869 | 0.87499 | 161.97885 | 0.471925 | 3 | 17.544 |
| 0.27434 | 0.20483 | 0.34238 | 36.74460 | 0.184664 | 4 | 23.392 |
| -0.16459 | 0.10932 | 0.19834 | 147.38389 | 0.105357 | 5 | 29.240 |
| 0.20887 | -0.10804 | 0.23511 | 333.52244 | 0.126648 | 6 | 35.088 |
| 0.23179 | 0.14679 | 0.23679 | 56.19276 | 0.127712 | 7 | 40.936 |
| 0.16488 | -0.04413 | 0.17307 | 346.72870 | 0.094422 | 8 | 46.784 |
| -0.08504 | 0.00004 | 0.08542 | 174.59933 | 0.046073 | 9 | 52.632 |
| -0.17910 | -0.03772 | 0.18311 | 191.84681 | 0.098758 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.49297 | | | | | 0 | |
| -4.88285 | 5.97572 | 7.35987 | 130.74123 | 1.000000 | 1 | 5.848 |
| 0.91872 | -0.47488 | 0.93973 | 270.07568 | 0.088662 | 2 | 11.696 |
| 1.23405 | 2.07944 | 2.41884 | 59.31281 | 0.328579 | 3 | 17.544 |
| -0.79858 | -2.11684 | 2.26243 | 249.33279 | 0.307434 | 4 | 23.392 |
| 0.83988 | 0.17958 | 0.85877 | 12.08498 | 0.116695 | 5 | 29.240 |
| 0.79178 | -0.01832 | 0.79185 | 359.25342 | 0.107601 | 6 | 35.088 |
| 0.13668 | 1.27841 | 1.28668 | 83.98165 | 0.174787 | 7 | 40.936 |
| -0.83827 | 0.89863 | 1.22526 | 133.16936 | 0.166497 | 8 | 46.784 |
| -0.72864 | 0.08558 | 0.72978 | 173.22787 | 0.098613 | 9 | 52.632 |
| -0.30555 | 0.13495 | 0.33403 | 156.17887 | 0.045390 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.03730 | | | | | 0 | |
| -5.53544 | -6.87428 | 8.82593 | 231.15749 | 1.000000 | 1 | 5.848 |
| -5.27991 | -1.20695 | 5.41618 | 192.87621 | 0.613658 | 2 | 11.696 |
| -4.05472 | 1.31962 | 4.28483 | 161.97235 | 0.485128 | 3 | 17.544 |
| 1.29000 | 0.96223 | 1.61040 | 36.53336 | 0.183142 | 4 | 23.392 |
| -0.82206 | 0.93541 | 0.98184 | 140.92398 | 0.111185 | 5 | 29.240 |
| 0.96304 | -0.47048 | 1.09244 | 334.47883 | 0.123776 | 6 | 35.088 |
| 0.84539 | 0.97297 | 1.13444 | 55.32620 | 0.128535 | 7 | 40.936 |
| 0.08171 | -0.21170 | 0.82919 | 345.20776 | 0.093949 | 8 | 46.784 |
| -0.39154 | 0.01229 | 0.39173 | 178.20210 | 0.044387 | 9 | 52.632 |
| -0.81049 | -0.28291 | 0.85958 | 194.09511 | 0.094664 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 450 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.52978 | | | | | 0 | |
| -12.78091 | 13.86035 | 18.85909 | 132.69769 | 1.000000 | 1 | 5.848 |
| 2.52981 | -16.14632 | 16.36329 | 278.99479 | 0.866600 | 2 | 11.696 |
| 2.66830 | 5.11137 | 5.76361 | 62.47797 | 0.305615 | 3 | 17.544 |
| -1.85341 | -3.19297 | 3.91342 | 298.39667 | 0.292348 | 4 | 23.392 |
| 1.70543 | 0.37875 | 1.82516 | 11.97683 | 0.096779 | 5 | 29.240 |
| 1.64488 | -0.89889 | 1.94017 | 337.34961 | 0.103381 | 6 | 35.088 |
| 0.12528 | 3.11822 | 3.12086 | 87.64421 | 0.165483 | 7 | 40.936 |
| -2.01348 | 2.09129 | 2.90383 | 133.91415 | 0.153933 | 8 | 46.784 |
| -1.82464 | 0.28790 | 1.84919 | 171.84311 | 0.098053 | 9 | 52.632 |
| -0.78264 | 0.36687 | 0.86436 | 154.88483 | 0.045833 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 450 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.21504 | | | | | 0 | |
| -13.51167 | -16.38965 | 21.24112 | 230.49771 | 1.000000 | 1 | 5.848 |
| -13.19983 | -3.84620 | 13.72691 | 193.80090 | 0.657897 | 2 | 11.696 |
| -10.10485 | 3.31670 | 10.71093 | 161.96083 | 0.504236 | 3 | 17.544 |
| 3.84276 | 2.25731 | 3.82992 | 36.12440 | 0.180280 | 4 | 23.392 |
| -2.19788 | 1.43878 | 2.59336 | 146.38252 | 0.122101 | 5 | 29.240 |
| 2.27738 | -1.84273 | 2.59480 | 336.31736 | 0.122214 | 6 | 35.088 |
| 1.62892 | 2.22872 | 2.76467 | 53.72872 | 0.130197 | 7 | 40.936 |
| 1.91931 | -0.47355 | 1.97486 | 346.14814 | 0.093006 | 8 | 46.784 |
| -0.88197 | -0.08647 | 0.88640 | 183.72821 | 0.041730 | 9 | 52.632 |
| -1.75754 | -0.99448 | 1.89536 | 190.68782 | 0.089247 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 50
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 450 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.37663 | | | | | 0 | |
| -37.09854 | 32.07176 | 49.08846 | 139.11903 | 1.000000 | 1 | 5.848 |
| 8.23822 | -30.11412 | 30.99882 | 282.16726 | 0.791899 | 2 | 11.696 |
| 5.82935 | 11.55953 | 11.94180 | 75.36883 | 0.243005 | 3 | 17.544 |
| -3.10825 | -11.29414 | 11.72805 | 254.28401 | 0.239004 | 4 | 23.392 |
| 1.64469 | 0.25631 | 1.64484 | 8.89779 | 0.033516 | 5 | 29.240 |
| 4.40240 | -0.63824 | 4.44843 | 351.78098 | 0.090778 | 6 | 35.088 |
| -1.61486 | 6.77995 | 6.98821 | 103.40163 | 0.142357 | 7 | 40.936 |
| -4.82857 | 5.62987 | 5.43882 | 137.76137 | 0.110821 | 8 | 46.784 |
| -4.47694 | 1.44098 | 4.70870 | 162.88188 | 0.095926 | 9 | 52.632 |
| -2.07220 | 1.18722 | 2.39828 | 150.19843 | 0.048735 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 50
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 450 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.51837 | | | | | 0 | |
| -29.38882 | -32.96829 | 44.15761 | 228.29188 | 1.000000 | 1 | 5.848 |
| -30.98875 | -7.71975 | 31.93582 | 193.98845 | 0.723224 | 2 | 11.696 |
| -24.25168 | 8.07049 | 25.84489 | 161.78471 | 0.585333 | 3 | 17.544 |
| 5.91270 | 9.99758 | 7.13727 | 34.06266 | 0.161632 | 4 | 23.392 |
| -6.87136 | 4.38262 | 7.44182 | 144.47958 | 0.168518 | 5 | 29.240 |
| 4.84422 | -1.16747 | 5.00814 | 346.71924 | 0.113891 | 6 | 35.088 |
| 3.00884 | 4.36106 | 5.00868 | 47.49882 | 0.113336 | 7 | 40.936 |
| 3.98488 | -0.73987 | 4.03887 | 349.20001 | 0.091866 | 8 | 46.784 |
| -1.14815 | -1.18413 | 1.64869 | 220.13220 | 0.037359 | 9 | 52.632 |
| -1.88888 | -2.28888 | 2.09875 | 230.49209 | 0.044359 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.72791 | | | | | 0 | |
| -44.85460 | 28.49449 | 54.84320 | 148.69708 | 1.000000 | 1 | 5.848 |
| 11.42785 | -34.83470 | 36.66130 | 288.16260 | 0.668475 | 2 | 11.696 |
| -3.76996 | 9.41970 | 10.14610 | 111.81238 | 0.184982 | 3 | 17.544 |
| -0.69872 | -8.84296 | 8.87052 | 269.48193 | 0.161749 | 4 | 23.392 |
| -3.42396 | -0.89147 | 3.53811 | 194.59372 | 0.064513 | 5 | 29.240 |
| 3.58913 | -1.56432 | 3.91523 | 336.44995 | 0.071390 | 6 | 35.088 |
| -4.92596 | 5.07778 | 7.07453 | 134.13098 | 0.128999 | 7 | 40.936 |
| -2.40995 | 1.88760 | 2.64309 | 159.70172 | 0.048193 | 8 | 46.784 |
| -4.52938 | 2.57537 | 5.21036 | 150.37785 | 0.095005 | 9 | 52.632 |
| -2.24551 | 1.59772 | 2.75591 | 144.56794 | 0.050251 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.25740 | | | | | 0 | |
| -22.19469 | -18.34357 | 28.76311 | 219.62395 | 0.972511 | 1 | 5.848 |
| -20.59092 | -7.71967 | 29.57613 | 199.12999 | 1.000000 | 2 | 11.696 |
| -23.55853 | 7.81264 | 24.82010 | 161.63311 | 0.839196 | 3 | 17.544 |
| 3.00070 | 1.32337 | 3.27956 | 23.79845 | 0.110885 | 4 | 23.392 |
| -7.38293 | 5.60204 | 9.28421 | 142.50841 | 0.311201 | 5 | 29.240 |
| 3.23202 | 1.10887 | 3.41695 | 18.93695 | 0.115531 | 6 | 35.088 |
| 4.80222 | 2.38925 | 4.66115 | 30.83634 | 0.157598 | 7 | 40.936 |
| 2.41565 | 0.13382 | 2.41956 | 3.17056 | 0.081808 | 8 | 46.784 |
| 0.59052 | -2.97898 | 3.02544 | 280.89912 | 0.102294 | 9 | 52.632 |
| 2.61684 | -3.45474 | 4.33396 | 307.14233 | 0.146536 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.94303 | | | | | 0 | |
| -99.03342 | 28.72638 | 65.65172 | 154.02190 | 1.000000 | 1 | 5.848 |
| 11.57899 | -32.28702 | 34.30049 | 289.72900 | 0.522461 | 2 | 11.696 |
| -13.98739 | 5.46895 | 15.01853 | 158.64493 | 0.228761 | 3 | 17.544 |
| 1.48382 | -8.68083 | 8.80673 | 279.69971 | 0.134143 | 4 | 23.392 |
| -10.39640 | -1.50358 | 10.44490 | 188.26870 | 0.159101 | 5 | 29.240 |
| 2.10315 | -4.49586 | 4.92726 | 295.26709 | 0.075052 | 6 | 35.088 |
| -7.14899 | 3.63404 | 8.01962 | 153.09449 | 0.122154 | 7 | 40.936 |
| -2.13419 | -0.00628 | 2.13420 | 180.16356 | 0.032518 | 8 | 46.784 |
| -5.80194 | 1.63676 | 6.02801 | 164.24490 | 0.091818 | 9 | 52.632 |
| -1.95244 | 1.27840 | 2.81186 | 140.92921 | 0.042832 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 44.58618 | | | | | 0 | |
| -13.84188 | 7.29151 | 15.64486 | 152.22089 | 0.997181 | 1 | 5.848 |
| -30.49388 | -4.68495 | 30.85156 | 188.73422 | 1.000000 | 2 | 11.696 |
| -23.21251 | 7.72664 | 24.46449 | 161.52930 | 0.792981 | 3 | 17.544 |
| 0.98562 | 0.17840 | 1.00163 | 10.25945 | 0.032466 | 4 | 23.392 |
| -7.57778 | 5.75476 | 9.51525 | 142.78686 | 0.308420 | 5 | 29.240 |
| 1.64782 | 1.55903 | 2.26894 | 43.41486 | 0.073528 | 6 | 35.088 |
| 5.31928 | 1.92442 | 5.53541 | 19.99143 | 0.179356 | 7 | 40.936 |
| -1.75807 | 2.34628 | 2.93186 | 126.84441 | 0.095031 | 8 | 46.784 |
| 0.88505 | -5.47163 | 5.54274 | 279.18799 | 0.179658 | 9 | 52.632 |
| 5.89764 | -3.78167 | 7.00594 | 327.33130 | 0.227085 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.43365 | | | | | 0 | |
| -45.61771 | 20.17435 | 49.8'964 | 156.14268 | 1.000000 | 1 | 5.848 |
| 3.40341 | -15.68314 | 16.04817 | 282.24390 | 0.32.738 | 2 | 11.696 |
| -21.23489 | -2.52980 | 21.38702 | 185.79320 | 0.428773 | 3 | 17.544 |
| 2.66722 | -7.74265 | 8.18919 | 289.00806 | 0.164179 | 4 | 23.392 |
| -13.54028 | -0.71758 | 13.55928 | 183.03362 | 0.271840 | 5 | 29.240 |
| -0.97951 | -7.13454 | 7.17174 | 262.14990 | 0.143781 | 6 | 35.088 |
| -4.61375 | 0.62833 | 4.65633 | 172.24474 | 0.093351 | 7 | 40.936 |
| -2.14290 | 0.63499 | 2.23500 | 163.49432 | 0.044808 | 8 | 46.784 |
| -5.70446 | -2.03157 | 6.05769 | 199.59503 | 0.121446 | 9 | 52.632 |
| 0.57199 | -0.47408 | 0.74292 | 320.34717 | 0.014894 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 56.63481 | | | | | 0 | |
| 8.28440 | 38.98488 | 38.98590 | 89.58195 | 1.000000 | 1 | 5.848 |
| -23.78909 | 3.60986 | 23.98232 | 171.34283 | 0.615153 | 2 | 11.696 |
| -13.86220 | 3.95757 | 14.41607 | 164.06630 | 0.369776 | 3 | 17.544 |
| 0.48057 | 0.73012 | 0.83278 | 61.24925 | 0.021361 | 4 | 23.392 |
| -3.55593 | 2.73759 | 4.48765 | 142.40855 | 0.115110 | 5 | 29.240 |
| -0.80340 | -1.12042 | 1.37870 | 234.35741 | 0.035364 | 6 | 35.088 |
| 5.83389 | 1.05966 | 5.92640 | 10.30011 | 0.152014 | 7 | 40.936 |
| -7.15624 | 4.90346 | 8.67508 | 145.38101 | 0.222516 | 8 | 46.784 |
| -1.80453 | -6.00952 | 6.09290 | 260.91029 | 0.156285 | 9 | 52.632 |
| 5.81795 | -1.61277 | 5.27075 | 342.18262 | 0.135196 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.45291 | | | | | 0 | |
| -25.70752 | 10.73749 | 27.86754 | 157.29200 | 1.000000 | 1 | 5.848 |
| -1.72155 | -2.04029 | 2.66995 | 229.84308 | 0.095796 | 2 | 11.696 |
| -20.41283 | -6.10645 | 21.30861 | 196.65443 | 0.764567 | 3 | 17.544 |
| 2.83843 | -6.44846 | 7.04951 | 293.75757 | 0.252822 | 4 | 23.392 |
| -10.88264 | 8.08649 | 10.88799 | 179.54466 | 0.390526 | 5 | 29.240 |
| -2.46293 | -6.96589 | 7.01262 | 249.43837 | 0.251641 | 6 | 35.088 |
| -1.64058 | -1.60825 | 2.31154 | 224.08614 | 0.082948 | 7 | 40.936 |
| -1.32271 | 1.32545 | 1.67365 | 142.21480 | 0.060057 | 8 | 46.784 |
| -4.29581 | -3.52877 | 5.43499 | 217.77167 | 0.195015 | 9 | 52.632 |
| 1.36662 | -1.48556 | 2.01894 | 312.61204 | 0.072433 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 32.42311 | | | | | 0 | |
| 6.18717 | 45.36827 | 45.78821 | 82.23404 | 1.000000 | 1 | 5.848 |
| -14.92369 | 7.45104 | 16.68141 | 153.47032 | 0.364321 | 2 | 11.696 |
| -6.51404 | 0.28738 | 6.52038 | 177.47388 | 0.142403 | 3 | 17.544 |
| 1.27879 | 1.01042 | 1.62980 | 38.31364 | 0.035594 | 4 | 23.392 |
| -0.69571 | 1.62700 | 1.58756 | 113.99092 | 0.034672 | 5 | 29.240 |
| -2.58494 | -3.06894 | 3.96223 | 230.78705 | 0.086534 | 6 | 35.088 |
| 5.16517 | 3.33824 | 5.17623 | 3.74658 | 0.113047 | 7 | 40.936 |
| -7.55131 | 5.30681 | 9.22979 | 144.98245 | 0.201574 | 8 | 46.784 |
| -2.4[illegible]981 | -4.67582 | 5.29670 | 241.96123 | 0.115678 | 9 | 52.632 |
| 3.10836 | -0.34346 | 3.12695 | 353.74927 | 0.068292 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -3.18796 | | | | | 0 | |
| -18.41272 | 8.48502 | 20.21371 | 155.25864 | 0.773399 | 1 | 5.848 |
| -3.06326 | 6.52622 | 7.20938 | 115.14430 | 0.275022 | 2 | 11.696 |
| -24.77979 | -8.55134 | 26.21379 | 199.03922 | 1.000000 | 3 | 17.544 |
| 4.71491 | -8.93160 | 10.10530 | 297.88916 | 0.385496 | 4 | 23.392 |
| -9.16814 | 1.21598 | 9.24843 | 172.44492 | 0.352808 | 5 | 29.240 |
| -4.15993 | -6.64883 | 7.84883 | 237.99200 | 0.299111 | 6 | 35.088 |
| -0.07173 | -4.97396 | 4.97448 | 269.17338 | 0.189766 | 7 | 40.936 |
| 0.40698 | 1.26483 | 1.32869 | 72.16356 | 0.050687 | 8 | 46.784 |
| -4.46111 | -3.41677 | 5.61924 | 217.44855 | 0.214362 | 9 | 52.632 |
| 1.13103 | -2.71494 | 2.94111 | 292.61621 | 0.112197 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 63.05219 | | | | | 0 | |
| 6.38384 | 54.80992 | 55.18044 | 83.35649 | 1.000000 | 1 | 5.848 |
| -12.88108 | 11.16119 | 17.04388 | 139.09175 | 0.308875 | 2 | 11.696 |
| -7.94983 | -2.32878 | 7.89625 | 197.15291 | 0.143099 | 3 | 17.544 |
| 4.40895 | 0.20355 | 4.41364 | 2.64331 | 0.079986 | 4 | 23.392 |
| 0.25032 | 4.18194 | 4.18942 | 86.57443 | 0.075922 | 5 | 29.240 |
| -6.10434 | -5.84429 | 8.44480 | 223.85898 | 0.153002 | 6 | 35.088 |
| 7.03216 | -1.47963 | 7.18932 | 348.14868 | 0.130215 | 7 | 40.936 |
| -6.65006 | 7.35219 | 9.91353 | 132.12941 | 0.179657 | 8 | 46.784 |
| -5.30787 | -4.62792 | 7.09819 | 220.69148 | 0.128636 | 9 | 52.632 |
| 3.20642 | -0.85971 | 3.31967 | 344.99072 | 0.060160 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -17.10902 | | | | | 0 | |
| -11.79420 | 8.84712 | 14.74363 | 143.12555 | 0.228790 | 1 | 5.848 |
| -4.24314 | 38.73843 | 38.97011 | 96.25092 | 0.604733 | 2 | 11.696 |
| -61.13487 | -20.37849 | 64.44186 | 198.43510 | 1.000000 | 3 | 17.544 |
| 15.89383 | -28.28735 | 32.44669 | 299.33032 | 0.503503 | 4 | 23.392 |
| -8.97157 | 5.49864 | 8.87783 | 141.74649 | 0.137765 | 5 | 29.240 |
| -11.99896 | -10.33659 | 15.83579 | 220.74820 | 0.245738 | 6 | 35.088 |
| 4.44425 | -21.19315 | 21.65451 | 281.84863 | 0.336032 | 7 | 40.936 |
| 8.37999 | 2.34192 | 8.70108 | 15.61386 | 0.135022 | 8 | 46.784 |
| -8.49453 | -3.43014 | 9.16094 | 201.98912 | 0.147158 | 9 | 52.632 |
| -0.63178 | -8.56604 | 8.58931 | 265.78174 | 0.133288 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 142.59592 | | | | | 0 | |
| 2.41286 | 115.76431 | 115.78944 | 88.80589 | 1.000000 | 1 | 5.848 |
| -21.62808 | 29.22522 | 36.35776 | 126.50327 | 0.313999 | 2 | 11.696 |
| -24.46059 | -15.11401 | 28.75331 | 211.71159 | 0.248424 | 3 | 17.544 |
| 23.01472 | -2.46062 | 23.14587 | 353.89722 | 0.199896 | 4 | 23.392 |
| -0.03488 | 22.81979 | 22.81981 | 90.08762 | 0.197080 | 5 | 29.240 |
| -24.68390 | -20.86847 | 32.32317 | 220.21211 | 0.279155 | 6 | 35.088 |
| 20.41159 | -9.98368 | 22.72238 | 333.93579 | 0.196239 | 7 | 40.936 |
| -3.99915 | 19.78227 | 20.17456 | 101.31749 | 0.174235 | 8 | 46.784 |
| -20.33688 | -7.99442 | 21.85175 | 201.45975 | 0.188728 | 9 | 52.632 |
| 7.59018 | -6.17516 | 9.78485 | 320.86914 | 0.084504 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -18.59933 | | | | | 0 | |
| 13.13640 | -12.88191 | 18.39859 | 315.56030 | 0.359327 | 1 | 5.848 |
| -1.58380 | 43.98143 | 44.00993 | 92.06242 | 0.859520 | 2 | 11.696 |
| -48.97617 | -14.93580 | 51.20294 | 196.95963 | 1.000000 | 3 | 17.544 |
| 10.00086 | -29.27435 | 27.48060 | 293.15454 | 0.536856 | 4 | 23.392 |
| 2.93784 | 1.56243 | 3.32677 | 28.01181 | 0.064972 | 5 | 29.240 |
| -6.54784 | -4.38243 | 7.87842 | 213.79715 | 0.153866 | 6 | 35.088 |
| 5.68099 | -15.38705 | 16.40584 | 290.29053 | 0.320393 | 7 | 40.936 |
| 6.74773 | 1.11760 | 6.83965 | 9.40430 | 0.133579 | 8 | 46.784 |
| -3.11090 | -1.91304 | 3.65886 | 211.52361 | 0.071458 | 9 | 52.632 |
| 0.02022 | -5.89356 | 5.89359 | 270.19653 | 0.115103 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 48.98080 | | | | | 0 | |
| 0.10884 | 62.42676 | 62.42685 | 89.99847 | 1.000000 | 1 | 5.848 |
| -19.26887 | 13.72997 | 23.69023 | 144.52809 | 0.379091 | 2 | 11.696 |
| -9.91319 | -23.30480 | 24.12006 | 255.00005 | 0.386373 | 3 | 17.544 |
| 23.59372 | 9.02225 | 25.25993 | 20.98884 | 0.404633 | 4 | 23.392 |
| -8.05223 | 18.96870 | 20.23209 | 113.48277 | 0.324093 | 5 | 29.240 |
| -14.61866 | -19.54073 | 24.41817 | 233.18048 | 0.391140 | 6 | 35.088 |
| 13.61873 | -3.45156 | 13.84777 | 345.56665 | 0.221824 | 7 | 40.936 |
| -8.93877 | 8.74097 | 8.75756 | 93.52719 | 0.140285 | 8 | 46.784 |
| -11.00447 | -4.63238 | 11.99586 | 202.71765 | 0.192146 | 9 | 52.632 |
| 4.19300 | -3.58161 | 5.51586 | 319.58171 | 0.088344 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -27.52222 | | | | | 0 | |
| 35.08701 | -47.53154 | 59.07913 | 306.43408 | 0.991457 | 1 | 5.848 |
| -3.45057 | 59.40941 | 59.58989 | 93.31967 | 1.000000 | 2 | 11.696 |
| -56.78313 | -16.07532 | 58.84472 | 195.88682 | 0.998356 | 3 | 17.544 |
| 2.57005 | -26.85065 | 26.97348 | 275.44099 | 0.452695 | 4 | 23.392 |
| 4.81083 | -0.39478 | 9.67816 | 299.81177 | 0.162364 | 5 | 29.240 |
| 1.66630 | -3.15770 | 3.57008 | 297.82831 | 0.059916 | 6 | 35.088 |
| 6.88685 | -4.79552 | 8.39134 | 325.14624 | 0.140819 | 7 | 40.936 |
| 0.41939 | 0.43172 | 0.60189 | 45.83026 | 0.010101 | 8 | 46.784 |
| 2.56344 | -4.66717 | 5.27241 | 299.09351 | 0.088479 | 9 | 52.632 |
| 3.67833 | -1.83601 | 4.11108 | 333.47412 | 0.068998 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -76.11040 | | | | | 0 | |
| 18.79805 | 30.19679 | 32.06761 | 76.33220 | 0.640040 | 1 | 5.848 |
| -37.88473 | -8.39897 | 37.00641 | 180.54741 | 0.738614 | 2 | 11.696 |
| 22.61278 | -44.78952 | 50.10249 | 296.82910 | 1.000000 | 3 | 17.544 |
| 20.22293 | 31.00219 | 42.57942 | 48.48389 | 0.849846 | 4 | 23.392 |
| -21.79674 | 12.32213 | 25.04880 | 150.47434 | 0.499853 | 5 | 29.240 |
| 0.16353 | -20.95612 | 20.95674 | 270.44702 | 0.418277 | 6 | 35.088 |
| 6.30889 | 9.00454 | 11.04852 | 54.64566 | 0.220359 | 7 | 40.936 |
| -5.72560 | -3.87132 | 6.91156 | 214.06427 | 0.137948 | 8 | 46.784 |
| 0.92569 | -3.83102 | 3.94127 | 283.98398 | 0.078644 | 9 | 52.632 |
| 0.99301 | -1.52815 | 1.77542 | 300.60181 | 0.035436 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 105
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -30.02180 | | | | | 0 | |
| 28.55952 | -32.18744 | 43.03111 | 311.58228 | 1.000000 | 1 | 5.848 |
| -6.26169 | 37.28339 | 37.80554 | 99.53383 | 0.878563 | 2 | 11.696 |
| -31.97827 | -9.23065 | 33.28384 | 196.10098 | 0.773483 | 3 | 17.544 |
| -6.98598 | -9.42744 | 11.68629 | 233.77570 | 0.271578 | 4 | 23.392 |
| -2.58838 | -13.45940 | 13.70565 | 259.12221 | 0.318506 | 5 | 29.240 |
| 7.75132 | -2.65405 | 8.19310 | 341.09863 | 0.190400 | 6 | 35.088 |
| 2.98726 | 4.30112 | 5.23673 | 55.21878 | 0.121696 | 7 | 40.936 |
| -2.23632 | -0.51385 | 2.29460 | 192.94038 | 0.053324 | 8 | 46.784 |
| 4.86849 | 1.16880 | 4.99138 | 12.74073 | 0.115995 | 9 | 52.632 |
| -1.49246 | 4.66826 | 4.89980 | 107.28281 | 0.113815 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 105
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -16.83415 | | | | | 0 | |
| 6.46915 | 13.94962 | 15.37666 | 65.12838 | 0.393828 | 1 | 5.848 |
| -33.24329 | 16.40814 | 37.07213 | 153.73809 | 0.949493 | 2 | 11.696 |
| -0.44406 | -38.12812 | 38.04414 | 257.50977 | 1.000000 | 3 | 17.544 |
| 25.28156 | 3.79016 | 25.56407 | 8.52617 | 0.654748 | 4 | 23.392 |
| -2.33624 | 18.33627 | 18.48450 | 97.26106 | 0.473426 | 5 | 29.240 |
| -9.82326 | -6.41417 | 11.73192 | 213.14279 | 0.300478 | 6 | 35.088 |
| 4.43488 | -5.95384 | 5.94146 | 310.28174 | 0.152173 | 7 | 40.936 |
| 2.87580 | 6.42290 | 7.03657 | 65.87717 | 0.180221 | 8 | 46.784 |
| -13.49818 | 0.90327 | 13.57081 | 176.16930 | 0.346283 | 9 | 52.632 |
| 1.04849 | -10.25052 | 10.29861 | 273.28857 | 0.448284 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -36.36720 | | | | | 0 | |
| 29.49247 | -36.74921 | 47.09512 | 308.71021 | 1.000000 | 1 | 5.848 |
| -13.61538 | 35.12686 | 37.67325 | 111.18668 | 0.799939 | 2 | 11.696 |
| -23.33869 | -14.67180 | 32.79558 | 206.57512 | 0.696369 | 3 | 17.544 |
| -3.40252 | -3.95924 | 7.52780 | 211.73212 | 0.159842 | 4 | 23.392 |
| -8.67705 | -11.40637 | 14.33166 | 232.73901 | 0.304313 | 5 | 29.240 |
| 4.51459 | -8.24588 | 9.40885 | 298.78044 | 0.199814 | 6 | 35.088 |
| 8.40939 | 3.93726 | 8.28544 | 25.08856 | 0.175963 | 7 | 40.936 |
| -1.58710 | 6.69569 | 6.84230 | 103.41223 | 0.145287 | 8 | 46.784 |
| -0.81662 | 2.28807 | 2.28813 | 90.41777 | 0.048415 | 9 | 52.632 |
| -0.15327 | 4.98061 | 4.98296 | 91.76265 | 0.105806 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 48.79552 | | | | | 0 | |
| 16.58653 | 24.18555 | 29.28149 | 55.68660 | 0.914408 | 1 | 5.848 |
| -11.19801 | 30.00928 | 32.02234 | 110.45406 | 1.000000 | 2 | 11.696 |
| -28.71817 | -8.73354 | 30.01678 | 196.91515 | 0.937370 | 3 | 17.544 |
| -7.88698 | -19.66798 | 21.16077 | 248.34991 | 0.660813 | 4 | 23.392 |
| 20.09877 | -8.54939 | 21.84152 | 336.99654 | 0.682071 | 5 | 29.240 |
| 7.34159 | 18.47288 | 19.07752 | 68.32500 | 0.628739 | 6 | 35.088 |
| -16.04907 | 1.30272 | 16.10184 | 175.35941 | 0.502831 | 7 | 40.936 |
| 6.82679 | -4.90081 | 8.40375 | 324.32617 | 0.262434 | 8 | 46.784 |
| -8.93818 | 15.78869 | 18.06921 | 119.64758 | 0.564269 | 9 | 52.632 |
| -17.07535 | -14.45490 | 22.37210 | 220.24910 | 0.698640 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -18.44615 | | | | | 0 | |
| 14.59891 | -21.36177 | 25.87328 | 304.34741 | 1.000000 | 1 | 5.848 |
| -9.14255 | 17.05624 | 19.35204 | 118.19243 | 0.747955 | 2 | 11.696 |
| -14.37130 | -9.78115 | 17.38403 | 214.23932 | 0.671891 | 3 | 17.544 |
| -1.66014 | -1.12994 | 2.00819 | 214.24030 | 0.077616 | 4 | 23.392 |
| -5.70036 | -3.59201 | 6.73770 | 212.21657 | 0.260412 | 5 | 29.240 |
| -0.09317 | -6.27731 | 6.27800 | 269.14941 | 0.242644 | 6 | 35.088 |
| 6.79240 | 0.90010 | 6.85178 | 7.54864 | 0.264821 | 7 | 40.936 |
| -0.35853 | 6.49317 | 6.50306 | 93.16049 | 0.251343 | 8 | 46.784 |
| -2.48146 | 0.66030 | 2.56781 | 165.09923 | 0.099246 | 9 | 52.632 |
| 1.45857 | 1.62648 | 2.18484 | 48.11885 | 0.084444 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 39.42859 | | | | | 0 | |
| 13.12320 | 15.57409 | 20.36591 | 49.88145 | 0.822336 | 1 | 5.848 |
| 5.11933 | 16.49317 | 17.23120 | 72.71664 | 0.695762 | 2 | 11.696 |
| -16.70555 | 9.36949 | 19.15366 | 150.71364 | 0.773387 | 3 | 17.544 |
| -19.49463 | -15.27453 | 24.76593 | 218.07957 | 1.000000 | 4 | 23.392 |
| 16.54343 | -18.37523 | 24.72516 | 311.99707 | 0.998354 | 5 | 29.240 |
| 13.88812 | 18.42686 | 23.07442 | 52.99504 | 0.931700 | 6 | 35.088 |
| -17.22900 | 5.55973 | 18.10382 | 162.11533 | 0.730997 | 7 | 40.936 |
| 3.43171 | -9.79827 | 10.38184 | 289.30200 | 0.419199 | 8 | 46.784 |
| 1.11952 | 13.47916 | 13.52557 | 85.25212 | 0.546136 | 9 | 52.632 |
| -16.50348 | -1.81292 | 16.60274 | 186.26884 | 0.670386 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -1.46830 | | | | | 0 | |
| 1.15602 | -1.72725 | 2.07840 | 303.79370 | 1.000000 | 1 | 5.848 |
| -0.75361 | 1.34492 | 1.54167 | 119.26378 | 0.741754 | 2 | 11.696 |
| -1.13409 | -0.80424 | 1.39031 | 215.34233 | 0.668931 | 3 | 17.544 |
| -0.11496 | -0.07724 | 0.13850 | 213.89833 | 0.066638 | 4 | 23.392 |
| -0.46978 | -0.26107 | 0.53745 | 209.06224 | 0.258587 | 5 | 29.240 |
| -0.03419 | -0.52360 | 0.52471 | 266.26318 | 0.252459 | 6 | 35.088 |
| 0.56891 | 0.05984 | 0.57205 | 6.00410 | 0.275236 | 7 | 40.936 |
| -0.02344 | 0.55236 | 0.55286 | 92.43016 | 0.266002 | 8 | 46.784 |
| -0.22575 | 0.04794 | 0.23078 | 168.01178 | 0.111036 | 9 | 52.632 |
| 0.13264 | 0.11996 | 0.17884 | 42.12494 | 0.086046 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 458 TEST COND 27 COMP RUN 39.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.32200 | | | | | 0 | |
| 1.09756 | 1.27697 | 1.68383 | 49.32069 | 0.782049 | 1 | 5.848 |
| 0.53236 | 1.32723 | 1.43002 | 68.14380 | 0.664167 | 2 | 11.696 |
| -1.36067 | 0.90557 | 1.63446 | 146.35504 | 0.759119 | 3 | 17.544 |
| -1.72983 | -1.28200 | 2.15310 | 216.54266 | 1.000000 | 4 | 23.392 |
| 1.39314 | -1.62165 | 2.13789 | 310.66528 | 0.992934 | 5 | 29.240 |
| 1.21914 | 1.57249 | 1.98973 | 52.21375 | 0.924173 | 6 | 35.088 |
| -1.47510 | 0.49578 | 1.55619 | 161.42268 | 0.722[illegible] | 7 | 40.936 |
| 0.27447 | -0.86114 | 0.90382 | 287.67847 | 0.419776 | 8 | 46.784 |
| 0.15072 | 1.13661 | 1.14656 | 82.44638 | 0.532515 | 9 | 52.632 |
| -1.40305 | -0.08399 | 1.40556 | 183.42587 | 0.652805 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.28256 | | | | | 0 | |
| -0.73360 | 1.08147 | 1.30681 | 124.15056 | 1.000000 | 1 | 5.848 |
| 0.05734 | -1.18174 | 1.18313 | 272.77783 | 0.905360 | 2 | 11.696 |
| 0.36271 | 0.34997 | 0.50402 | 43.97520 | 0.385689 | 3 | 17.544 |
| -0.23249 | -0.27981 | 0.36379 | 230.27690 | 0.278380 | 4 | 23.392 |
| 0.07451 | 0.13583 | 0.15492 | 61.25421 | 0.118550 | 5 | 29.240 |
| 0.02440 | -0.10982 | 0.11250 | 282.52612 | 0.086089 | 6 | 35.088 |
| 0.07692 | 0.21390 | 0.22731 | 70.22177 | 0.173940 | 7 | 40.936 |
| -0.14007 | 0.18960 | 0.23572 | 126.45544 | 0.180381 | 8 | 46.784 |
| -0.10354 | 0.05639 | 0.11790 | 151.42360 | 0.090219 | 9 | 52.632 |
| -0.02996 | 0.02273 | 0.03761 | 142.81239 | 0.028782 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.36259 | | | | | 0 | |
| -1.44487 | -0.90485 | 1.70482 | 212.05675 | 1.000000 | 1 | 5.848 |
| -0.94148 | -0.22624 | 0.96828 | 193.51192 | 0.567968 | 2 | 11.696 |
| -0.79324 | 0.18136 | 0.81370 | 167.12169 | 0.477297 | 3 | 17.544 |
| 0.51757 | 0.09381 | 0.52601 | 10.27361 | 0.308541 | 4 | 23.392 |
| -0.03699 | 0.01084 | 0.03855 | 163.66419 | 0.022610 | 5 | 29.240 |
| 0.19103 | -0.25468 | 0.31835 | 306.87524 | 0.186734 | 6 | 35.088 |
| 0.23278 | 0.08860 | 0.24907 | 20.83698 | 0.146099 | 7 | 40.936 |
| 0.12645 | -0.23233 | 0.26451 | 298.55762 | 0.155157 | 8 | 46.784 |
| -0.04172 | 0.06169 | 0.07448 | 124.07118 | 0.043687 | 9 | 52.632 |
| -0.06115 | 0.00509 | 0.06136 | 175.24579 | 0.035991 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.45859 | | | | | 0 | |
| -3.75479 | 5.25853 | 6.46147 | 125.52826 | 1.000000 | 1 | 5.848 |
| 0.32814 | -5.73624 | 5.74562 | 273.27393 | 0.889212 | 2 | 11.696 |
| 1.65703 | 1.70014 | 2.37407 | 45.73573 | 0.367420 | 3 | 17.544 |
| -1.06252 | -1.36255 | 1.71213 | 231.64116 | 0.264976 | 4 | 23.392 |
| 0.31197 | 0.69893 | 0.76539 | 65.94623 | 0.118454 | 5 | 29.240 |
| 0.11854 | -0.52655 | 0.53975 | 282.69727 | 0.083534 | 6 | 35.088 |
| 0.34863 | 1.04897 | 1.10538 | 71.61555 | 0.171073 | 7 | 40.936 |
| -0.65366 | 0.90618 | 1.11734 | 125.80444 | 0.172923 | 8 | 46.784 |
| -0.48847 | 0.29703 | 0.57169 | 148.69690 | 0.088477 | 9 | 52.632 |
| -0.13469 | 0.12999 | 0.18718 | 136.01697 | 0.028969 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.51272 | | | | | 0 | |
| -6.85382 | -4.30679 | 8.09464 | 212.14433 | 1.000000 | 1 | 5.848 |
| -4.58176 | -1.10699 | 4.71359 | 193.58279 | 0.582313 | 2 | 11.696 |
| -3.83002 | 0.89232 | 3.93259 | 166.88510 | 0.485827 | 3 | 17.544 |
| 2.46216 | 0.41697 | 2.49722 | 9.61196 | 0.308503 | 4 | 23.392 |
| -0.21580 | 0.06775 | 0.22618 | 162.57118 | 0.027942 | 5 | 29.240 |
| 0.88552 | -1.21743 | 1.50542 | 306.03076 | 0.185978 | 6 | [illegible] |
| 1.12141 | 0.40507 | 1.19233 | 19.86028 | 0.147299 | 7 | 40.936 |
| 0.57114 | -1.09584 | 1.23574 | 297.52808 | 0.152662 | 8 | 46.784 |
| -0.20493 | 0.25205 | 0.32485 | 129.11301 | 0.040131 | 9 | 52.632 |
| -0.29146 | 0.00422 | 0.29149 | 179.16974 | 0.036010 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.02581 | | | | | 0 | |
| -10.22903 | 13.15622 | 16.66490 | 127.86530 | 1.000000 | 1 | 5.848 |
| 1.04043 | -14.30756 | 14.34934 | 274.15918 | 0.860811 | 2 | 11.696 |
| 3.67145 | 4.24679 | 5.61380 | 49.15578 | 0.336864 | 3 | 17.544 |
| -2.35620 | -3.27903 | 4.03779 | 234.30019 | 0.242293 | 4 | 23.392 |
| 0.55676 | 1.91978 | 1.99888 | 73.82712 | 0.119946 | 5 | 29.240 |
| 0.29679 | -1.28428 | 1.31812 | 283.01221 | 0.079096 | 6 | 35.088 |
| 0.75942 | 2.66412 | 2.77025 | 74.00945 | 0.166232 | 7 | 40.936 |
| -1.51359 | 2.19734 | 2.66819 | 124.56829 | 0.160109 | 8 | 46.784 |
| -1.15557 | 0.84465 | 1.43136 | 143.83563 | 0.085890 | 9 | 52.632 |
| -0.28799 | 0.41174 | 0.50246 | 124.97061 | 0.030151 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 15.79279 | | | | | 0 | |
| -10.38365 | -18.36176 | 19.30547 | 212.31079 | 1.000000 | 1 | 5.848 |
| -11.48045 | -2.00046 | 11.81708 | 193.70062 | 0.609585 | 2 | 11.696 |
| -9.46218 | 2.27918 | 9.73281 | 166.49699 | 0.502067 | 3 | 17.544 |
| 5.91770 | 0.86891 | 5.98115 | 8.25318 | 0.308538 | 4 | 23.392 |
| -0.69982 | 0.23628 | 0.73863 | 161.34399 | 0.038102 | 5 | 29.240 |
| 2.02268 | -2.[illegible]333 | 3.57958 | 304.48625 | 0.184653 | 6 | 35.088 |
| 2.79916 | 0.84902 | 2.90193 | 18.04718 | 0.149694 | 7 | 40.936 |
| 1.23455 | -2.59114 | 2.87821 | 295.47559 | 0.148460 | 8 | 46.784 |
| -0.52183 | 0.[illegible]1743 | 0.66825 | 141.34276 | 0.034472 | 9 | 52.632 |
| -0.78311 | -0.08065 | 0.78772 | 186.54381 | 0.034508 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.87156 | | | | | 0 | |
| -31.52063 | 31.20927 | 44.35728 | 135.28439 | 1.000000 | 1 | 5.848 |
| 4.48625 | -33.80591 | 34.10228 | 277.55933 | 0.768889 | 2 | 11.696 |
| 5.00740 | 10.19382 | 11.35729 | 63.83582 | 0.256041 | 3 | 17.544 |
| -3.02614 | -6.87573 | 7.51221 | 246.24463 | 0.169357 | 4 | 23.392 |
| -0.48351 | 5.94706 | 5.96668 | 94.64812 | 0.134514 | 5 | 29.240 |
| 0.92777 | -2.63144 | 2.79020 | 289.42114 | 0.062903 | 6 | 35.088 |
| 0.85039 | 6.83458 | 6.88728 | 82.90729 | 0.155267 | 7 | 40.936 |
| -2.49286 | 4.68288 | 5.23458 | 118.43941 | 0.118010 | 8 | 46.784 |
| -2.02369 | 2.97759 | 3.60916 | 124.28190 | 0.081363 | 9 | 52.632 |
| -0.23188 | 1.02367 | 1.03835 | 97.24426 | 0.041444 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 32.11539 | | | | | 0 | |
| -32.37200 | -22.10208 | 39.19821 | 214.32275 | 1.000000 | 1 | 5.848 |
| -27.26167 | -7.20117 | 28.19672 | 194.79671 | 0.719337 | 2 | 11.696 |
| -21.32200 | 5.89504 | 22.12268 | 164.54565 | 0.564380 | 3 | 17.544 |
| 11.82624 | 0.44611 | 11.83466 | 2.16128 | 0.301918 | 4 | 23.392 |
| -3.06672 | 1.08746 | 3.25382 | 160.47542 | 0.083009 | 5 | 29.240 |
| 3.22719 | -6.89389 | 6.89567 | 297.96454 | 0.175918 | 6 | 35.088 |
| 6.03126 | 1.13121 | 6.13643 | 10.62284 | 0.156549 | 7 | 40.936 |
| 1.31538 | -5.81459 | 5.18424 | 284.69800 | 0.132257 | 8 | 46.784 |
| -1.19822 | -0.91046 | 1.50488 | 217.22903 | 0.038392 | 9 | 52.632 |
| -1.43884 | -1.81278 | 1.75954 | 213.14107 | 0.044888 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.01848 | | | | | 0 | |
| -42.68987 | 29.12392 | 51.67810 | 145.69739 | 1.000000 | 1 | 5.848 |
| 7.71910 | -30.94865 | 31.89676 | 284.00464 | 0.617220 | 2 | 11.696 |
| -2.69984 | 9.47544 | 9.85256 | 105.90393 | 0.190653 | 3 | 17.544 |
| 1.95451 | -5.06216 | 5.42637 | 291.11157 | 0.105003 | 4 | 23.392 |
| -3.95340 | 8.23275 | 9.13278 | 115.65056 | 0.176724 | 5 | 29.240 |
| 0.95457 | -1.87848 | 2.10711 | 296.93774 | 0.040774 | 6 | 35.088 |
| -0.98851 | 7.07694 | 7.14564 | 97.95168 | 0.138272 | 7 | 40.936 |
| -0.37434 | 3.18383 | 3.20576 | 96.70590 | 0.062033 | 8 | 46.784 |
| -0.77523 | 4.42874 | 4.49607 | 99.92848 | 0.087002 | 9 | 52.632 |
| 0.57263 | 3.11521 | 3.16740 | 79.58420 | 0.061291 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 21.60318 | | | | | 0 | |
| -18.12421 | -14.49580 | 23.20807 | 218.65292 | 0.869458 | 1 | 5.848 |
| -25.66748 | -7.32630 | 26.69258 | 195.93039 | 1.000000 | 2 | 11.696 |
| -17.95581 | 6.27647 | 19.02116 | 160.73288 | 0.712601 | 3 | 17.544 |
| 7.14008 | -2.39433 | 7.53084 | 341.46167 | 0.282132 | 4 | 23.392 |
| -5.41080 | 2.05498 | 5.78789 | 159.20364 | 0.216835 | 5 | 29.240 |
| -0.01188 | -4.17155 | 4.17157 | 269.83667 | 0.156282 | 6 | 35.088 |
| 4.84480 | -0.78624 | 4.90502 | 351.01270 | 0.183760 | 7 | 40.936 |
| -1.83309 | -2.35590 | 2.98504 | 232.11406 | 0.111830 | 8 | 46.784 |
| -1.21584 | -4.25800 | 4.42818 | 254.06361 | 0.165896 | 9 | 52.632 |
| -0.92709 | -2.40673 | 2.57911 | 248.93294 | 0.096623 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 23.07211 | | | | | 0 | |
| -55.60186 | 35.30357 | 65.14801 | 151.32234 | 1.000000 | 1 | 5.848 |
| 8.76301 | -28.80873 | 30.11200 | 286.91846 | 0.476848 | 2 | 11.696 |
| -13.92274 | 7.02783 | 15.59593 | 153.21658 | 0.246974 | 3 | 17.544 |
| 6.53684 | -6.26920 | 9.05721 | 316.19727 | 0.143428 | 4 | 23.392 |
| -9.46857 | 11.80978 | 15.12562 | 128.71526 | 0.239685 | 5 | 29.240 |
| -1.99532 | -3.35327 | 3.90202 | 239.24571 | 0.061792 | 6 | 35.088 |
| -2.99881 | 5.92046 | 6.63653 | 116.86147 | 0.105095 | 7 | 40.936 |
| 0.34624 | 2.51315 | 2.53688 | 82.15569 | 0.040174 | 8 | 46.784 |
| -1.99902 | 4.48271 | 4.90824 | 114.03410 | 0.077726 | 9 | 52.632 |
| 0.98670 | 3.06919 | 3.22389 | 72.17810 | 0.051053 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.32346 | | | | | 0 | |
| -6.11909 | 6.70106 | 9.07454 | 132.40086 | 0.317116 | 1 | 5.848 |
| -28.30521 | -4.20516 | 28.61596 | 188.45033 | 1.000000 | 2 | 11.696 |
| -17.24067 | 6.21541 | 18.33150 | 160.18062 | 0.640606 | 3 | 17.544 |
| 5.01885 | -3.30293 | 6.00817 | 326.65063 | 0.209960 | 4 | 23.392 |
| -7.37544 | 3.22164 | 8.04836 | 156.40398 | 0.281255 | 5 | 29.240 |
| -3.54987 | -4.14869 | 5.46015 | 229.44769 | 0.190809 | 6 | 35.088 |
| 5.58330 | -2.01607 | 5.93617 | 340.14575 | 0.207442 | 7 | 40.936 |
| -5.76595 | 2.10965 | 6.13977 | 159.90341 | 0.214558 | 8 | 46.784 |
| -3.00071 | -6.43414 | 7.09947 | 244.99689 | 0.248096 | 9 | 52.632 |
| -0.75255 | -3.25712 | 3.34293 | 256.98999 | 0.116821 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 16.95709 | | | | | 0 | |
| -43.28391 | 21.15820 | 48.17847 | 153.94952 | 1.000000 | 1 | 5.848 |
| 3.73489 | -14.10375 | 14.59473 | 284.82739 | 0.302931 | 2 | 11.696 |
| -22.23135 | -0.09496 | 22.23154 | 180.24472 | 0.461441 | 3 | 17.544 |
| 2.47774 | -8.44350 | 11.27871 | 311.52856 | 0.234103 | 4 | 23.392 |
| -12.02361 | 11.29578 | 16.49731 | 136.78770 | 0.342421 | 5 | 29.240 |
| -7.11188 | -5.56217 | 9.02865 | 218.02876 | 0.187400 | 6 | 35.088 |
| -3.96799 | 0.35409 | 3.98551 | 174.33250 | 0.074421 | 7 | 40.936 |
| -0.47363 | 1.53223 | 1.60376 | 107.17714 | 0.033288 | 8 | 46.784 |
| -4.82115 | 1.07944 | 4.94056 | 167.37750 | 0.102547 | 9 | 52.632 |
| 0.40257 | 0.14432 | 0.42759 | 19.69814 | 0.008875 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.26576 | | | | | 0 | |
| 4.46385 | 37.05556 | 37.32344 | 83.13098 | 1.000000 | 1 | 5.848 |
| -22.70114 | 4.24507 | 23.09464 | 169.40813 | 0.618770 | 2 | 11.696 |
| -12.38228 | 2.68095 | 12.66919 | 167.78316 | 0.339443 | 3 | 17.544 |
| 4.16004 | -0.54159 | 4.19515 | 352.58228 | 0.112400 | 4 | 23.392 |
| -5.44730 | 3.41242 | 6.42799 | 147.93373 | 0.172224 | 5 | 29.240 |
| -5.76674 | -4.67330 | 7.42260 | 219.02087 | 0.198872 | 6 | 35.088 |
| 6.09882 | -1.64108 | 6.31575 | 344.93945 | 0.169217 | 7 | 40.936 |
| -7.35735 | 7.05689 | 10.19462 | 136.19415 | 0.273143 | 8 | 46.784 |
| -5.21447 | -4.25822 | 6.73225 | 219.23557 | 0.180376 | 9 | 52.632 |
| -0.99387 | -1.97009 | 2.04646 | 254.29704 | 0.054831 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.78875 | | | | | 0 | |
| -24.69083 | 10.84741 | 26.96855 | 156.28270 | 1.000000 | 1 | 5.848 |
| 0.43978 | -1.84764 | 1.89925 | 283.38867 | 0.070425 | 2 | 11.696 |
| -21.72191 | -3.69008 | 22.03310 | 189.64125 | 0.816992 | 3 | 17.544 |
| 4.10900 | -8.62080 | 10.56589 | 305.32275 | 0.391786 | 4 | 23.392 |
| -0.59338 | 8.32905 | 12.70457 | 139.03523 | 0.471088 | 5 | 29.240 |
| -8.30353 | -5.36173 | 9.88416 | 212.85100 | 0.366507 | 6 | 35.088 |
| -2.74685 | -3.31195 | 4.30280 | 230.32851 | 0.159549 | 7 | 40.936 |
| -0.59997 | 0.60943 | 0.85521 | 134.55194 | 0.031711 | 8 | 46.784 |
| -5.11399 | -0.98979 | 5.20889 | 190.95387 | 0.193147 | 9 | 52.632 |
| -0.20729 | -1.63604 | 1.64912 | 262.77856 | 0.061150 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XM-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 41.24561 | | | | | 0 | |
| 7.32739 | 42.97798 | 43.59813 | 80.32454 | 1.000000 | 1 | 5.848 |
| -14.32932 | 8.11867 | 16.46942 | 150.46509 | 0.377755 | 2 | 11.696 |
| -7.89256 | -0.24817 | 7.89646 | 181.80098 | 0.181119 | 3 | 17.544 |
| 3.77645 | 1.25632 | 3.97994 | 18.40079 | 0.091287 | 4 | 23.392 |
| -2.94713 | 3.19824 | 4.34906 | 132.66010 | 0.099753 | 5 | 29.240 |
| -5.89958 | -4.46292 | 7.32590 | 217.53148 | 0.168032 | 6 | 35.088 |
| 5.35921 | -1.08713 | 5.46836 | 348.59296 | 0.125426 | 7 | 40.936 |
| -5.84888 | 7.66622 | 9.64263 | 127.34155 | 0.221171 | 8 | 46.784 |
| -5.16402 | -1.85789 | 5.48995 | 199.78049 | 0.125922 | 9 | 52.632 |
| -0.22712 | -0.69797 | 0.73399 | 251.97533 | 0.016835 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.69536 | | | | | 0 | |
| -18.12715 | 7.50237 | 19.61852 | 157.51657 | 0.714797 | 1 | 5.848 |
| 0.46738 | 6.33596 | 6.35317 | 85.78104 | 0.231479 | 2 | 11.696 |
| -26.69580 | -5.46814 | 27.44401 | 191.49207 | 1.000000 | 3 | 17.544 |
| 7.47330 | -12.41156 | 14.48782 | 301.05322 | 0.527866 | 4 | 23.392 |
| -7.69431 | 8.96132 | 11.81134 | 130.64984 | 0.430348 | 5 | 29.240 |
| -10.63291 | -5.30151 | 11.88127 | 206.50056 | 0.432894 | 6 | 35.088 |
| -2.79210 | -7.32650 | 7.84049 | 249.13834 | 0.285670 | 7 | 40.936 |
| 0.53964 | -0.29200 | 0.61357 | 331.58228 | 0.022356 | 8 | 46.784 |
| -5.97194 | -1.45059 | 5.75766 | 194.59238 | 0.209781 | 9 | 52.632 |
| -1.07337 | -2.99591 | 3.18239 | 250.28838 | 0.115951 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 48.82066 | | | | | 0 | |
| 7.58712 | 49.67807 | 50.25409 | 81.31650 | 1.000000 | 1 | 5.848 |
| -11.63570 | 11.54249 | 16.38959 | 135.23041 | 0.326134 | 2 | 11.696 |
| -9.12390 | -1.69014 | 9.27192 | 190.25162 | 0.184581 | 3 | 17.544 |
| 5.44000 | 2.86844 | 5.82745 | 20.79027 | 0.115960 | 4 | 23.392 |
| -2.28168 | 4.99859 | 5.49886 | 114.78947 | 0.108615 | 5 | 29.240 |
| -8.29438 | -6.35837 | 10.49185 | 217.47357 | 0.287964 | 6 | 35.088 |
| 7.01192 | -1.81052 | 7.24189 | 345.92197 | 0.144105 | 7 | 40.936 |
| -4.82380 | 8.90148 | 10.12450 | 118.49378 | 0.201466 | 8 | 46.784 |
| -6.04297 | -1.32578 | 6.18669 | 192.37418 | 0.123108 | 9 | 52.632 |
| 0.56183 | -0.10403 | 0.57138 | 349.51001 | 0.011370 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.90861 | | | | | 0 | |
| -14.22965 | 3.16481 | 14.57735 | 167.46095 | 0.213649 | 1 | 5.848 |
| 6.41449 | 37.67017 | 38.21239 | 80.33629 | 0.560049 | 2 | 11.696 |
| -67.21945 | -11.70220 | 68.23044 | 189.87561 | 1.000000 | 3 | 17.544 |
| 19.47206 | -37.30823 | 42.08401 | 297.56104 | 0.616792 | 4 | 23.392 |
| -4.33718 | 19.42972 | 19.90788 | 102.58321 | 0.291774 | 5 | 29.240 |
| -26.76089 | -7.96553 | 26.01059 | 197.83287 | 0.381217 | 6 | 35.088 |
| -4.31235 | -25.97131 | 26.32689 | 260.57227 | 0.385853 | 7 | 40.936 |
| 8.89495 | -3.79412 | 7.89872 | 331.43286 | 0.115862 | 8 | 46.784 |
| -9.13883 | -1.88364 | 9.33093 | 191.64635 | 0.136756 | 9 | 52.632 |
| -4.80830 | -8.45742 | 9.72871 | 240.38039 | 0.142586 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XM-91A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 101.85904 | | | | | 0 | |
| 9.43422 | 93.64528 | 94.12128 | 84.23502 | 1.000000 | 1 | 5.848 |
| -14.78395 | 29.82939 | 33.29199 | 116.36385 | 0.353714 | 2 | 11.696 |
| -25.87788 | -8.25074 | 27.16135 | 197.68402 | 0.288578 | 3 | 17.544 |
| 18.52979 | 4.44269 | 19.05959 | 13.54115 | 0.202500 | 4 | 23.392 |
| -3.34686 | 17.49664 | 17.81386 | 100.82910 | 0.189265 | 5 | 29.240 |
| -24.49783 | -19.12912 | 31.08160 | 217.98447 | 0.330229 | 6 | 35.088 |
| 18.89302 | -6.73430 | 20.09733 | 340.38159 | 0.213101 | 7 | 40.936 |
| -3.66058 | 17.24426 | 17.62849 | 101.98477 | 0.187295 | 8 | 46.784 |
| -12.61444 | -2.34740 | 12.83099 | 190.54150 | 0.136324 | 9 | 52.632 |
| 3.89809 | 0.81014 | 3.98139 | 11.74067 | 0.042301 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -7.19651 | | | | | 0 | |
| 7.71254 | -17.41536 | 19.04672 | 293.88647 | 0.376215 | 1 | 5.848 |
| 9.56551 | 40.17929 | 41.29832 | 76.60750 | 0.815773 | 2 | 11.696 |
| -50.29407 | -6.13560 | 50.62723 | 186.96088 | 1.000000 | 3 | 17.544 |
| 12.72792 | -28.65717 | 31.35654 | 293.94800 | 0.619361 | 4 | 23.392 |
| -.61938 | 9.84083 | 9.97318 | 80.65523 | 0.196992 | 5 | 29.240 |
| -13.52060 | -5.89950 | 14.75163 | 203.57327 | 0.291377 | 6 | 35.088 |
| 1.49430 | -18.52322 | 18.58339 | 274.61206 | 0.367063 | 7 | 40.936 |
| 5.65796 | -2.69435 | 6.26674 | 334.53589 | 0.123782 | 8 | 46.784 |
| -2.89777 | -2.21397 | 3.64674 | 217.38077 | 0.072031 | 9 | 52.632 |
| -2.59005 | -4.74121 | 5.40254 | 241.35291 | 0.106712 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.50627 | | | | | 0 | |
| 7.69239 | 43.90521 | 44.65279 | 80.00002 | 1.000000 | 1 | 5.848 |
| -12.52780 | 20.11186 | 23.69455 | 121.91908 | 0.530640 | 2 | 11.696 |
| -14.18835 | -18.85301 | 23.59383 | 232.83130 | 0.528366 | 3 | 17.544 |
| 21.74706 | 6.71543 | 22.76030 | 17.16054 | 0.509717 | 4 | 23.392 |
| -5.89565 | 17.30998 | 18.28642 | 104.08852 | 0.409525 | 5 | 29.240 |
| -15.12040 | -16.35866 | 22.27626 | 227.25259 | 0.4[illegible]8877 | 6 | 35.088 |
| 12.52155 | -0.78359 | 12.54605 | 356.41895 | 0.280963 | 7 | 40.936 |
| -4.79461 | 7.23565 | 8.68008 | 123.52995 | 0.194389 | 8 | 46.784 |
| -9.13825 | -5.09182 | 7.23383 | 224.73991 | 0.162002 | 9 | 52.632 |
| 4.78098 | 0.49787 | 4.72727 | 6.34554 | 0.105867 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -17.33690 | | | | | 0 | |
| 24.23195 | -49.39913 | 55.01730 | 296.13184 | 1.000000 | 1 | 5.848 |
| 14.24386 | 40.40248 | 51.41467 | 73.91733 | 0.934508 | 2 | 11.696 |
| -50.01973 | -2.53864 | 50.08895 | 182.90199 | 0.910321 | 3 | 17.544 |
| 6.83598 | -22.34041 | 23.36287 | 287.01367 | 0.424641 | 4 | 23.392 |
| -3.32060 | 1.22074 | 3.53708 | 159.81534 | 0.064304 | 5 | 29.240 |
| -3.49439 | -11.69839 | 12.17073 | 253.31470 | 0.221214 | 6 | 35.088 |
| 10.29989 | -8.57374 | 13.49203 | 320.21680 | 0.245594 | 7 | 40.936 |
| 1.11003 | 0.98259 | 1.21951 | 24.35947 | 0.022167 | 8 | 46.784 |
| 2.00782 | -6.19961 | 6.47859 | 288.09428 | 0.117754 | 9 | 52.632 |
| 2.27661 | 0.10081 | 2.27884 | 2.53539 | 0.041428 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -77.68188 | | | | | 0 | |
| 19.74245 | 13.40585 | 23.86334 | 34.17635 | 0.564961 | 1 | 5.848 |
| -25.88939 | 28.49970 | 32.98248 | 141.70479 | 0.780856 | 2 | 11.696 |
| -6.24068 | -41.77533 | 42.23889 | 261.50162 | 1.000000 | 3 | 17.544 |
| 32.77191 | 9.28235 | 34.06111 | 15.81429 | 0.806392 | 4 | 23.392 |
| -10.22793 | 21.01997 | 23.37625 | 115.94678 | 0.553490 | 5 | 29.240 |
| -5.73302 | -13.82149 | 14.98363 | 247.46892 | 0.354762 | 6 | 35.088 |
| 4.38844 | 7.78315 | 8.86549 | 60.33002 | 0.209889 | 7 | 40.936 |
| -12.05125 | -1.66698 | 12.16998 | 187.87541 | 0.288028 | 8 | 46.784 |
| 1.49781 | -7.19739 | 7.34355 | 281.45020 | 0.173857 | 9 | 52.632 |
| 0.91049 | -2.21424 | 2.39413 | 292.35229 | 0.056681 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -18.99298 | | | | | 0 | |
| 21.81421 | -31.84087 | 38.59663 | 304.41504 | 1.000000 | 1 | 5.848 |
| 7.36795 | 31.88248 | 32.72275 | 76.98747 | 0.847813 | 2 | 11.696 |
| -27.57768 | 0.45920 | 27.58150 | 179.04604 | 0.714609 | 3 | 17.544 |
| 0.14333 | -5.10794 | 5.10995 | 271.60718 | 0.132394 | 4 | 23.392 |
| -9.39861 | -1.65300 | 9.54287 | 189.97496 | 0.247246 | 5 | 29.240 |
| 1.97504 | -10.19249 | 10.38208 | 280.96655 | 0.268989 | 6 | 35.088 |
| 8.87971 | 0.64601 | 8.91992 | 5.44240 | 0.231104 | 7 | 40.936 |
| -1.21486 | 1.31395 | 1.78951 | 132.79627 | 0.046364 | 8 | 46.784 |
| 4.27468 | -4.71388 | 6.00247 | 315.41040 | 0.155518 | 9 | 52.632 |
| 4.12424 | 3.01421 | 5.10831 | 36.16132 | 0.132351 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -21.22678 | | | | | 0 | |
| 13.20494 | -5.42766 | 14.27690 | 337.65552 | 0.389804 | 1 | 5.848 |
| -0.91266 | 31.47707 | 31.00099 | 107.48012 | 0.899182 | 2 | 11.696 |
| -31.32088 | -19.13054 | 36.70114 | 211.41624 | 1.000000 | 3 | 17.544 |
| 14.42842 | -16.74696 | 22.10519 | 310.74658 | 0.602303 | 4 | 23.392 |
| 12.85017 | 10.22422 | 16.42137 | 38.50745 | 0.447435 | 5 | 29.240 |
| -8.49567 | 6.78191 | 10.87064 | 141.40042 | 0.296193 | 6 | 35.088 |
| -9.14635 | -7.68360 | 11.94543 | 220.03270 | 0.325478 | 7 | 40.936 |
| 12.43776 | -5.77455 | 13.71289 | 335.09570 | 0.373637 | 8 | 46.784 |
| -1.80202 | 17.96306 | 18.03321 | 95.72870 | 0.491898 | 9 | 52.632 |
| -20.53085 | -8.41319 | 22.18777 | 202.28296 | 0.604553 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -20.98105 | | | | | 0 | |
| 20.86304 | -34.27881 | 40.12857 | 301.32568 | 1.000000 | 1 | 5.848 |
| 0.62605 | 29.64313 | 29.64972 | 88.79004 | 0.738868 | 2 | 11.696 |
| -24.56887 | -2.75587 | 24.52419 | 186.45213 | 0.611140 | 3 | 17.544 |
| 0.65032 | 2.64447 | 2.72326 | 76.18414 | 0.067863 | 4 | 23.392 |
| -15.18127 | 1.71172 | 15.27746 | 173.56696 | 0.380713 | 5 | 29.240 |
| -0.45805 | -13.22063 | 13.22855 | 268.01538 | 0.329654 | 6 | 35.088 |
| 11.48495 | 0.71564 | 11.50683 | 3.56570 | 0.286749 | 7 | 40.936 |
| 1.69025 | 4.02830 | 4.36853 | 67.23735 | 0.108863 | 8 | 46.784 |
| 4.46675 | -1.28300 | 4.64736 | 343.97412 | 0.115812 | 9 | 52.632 |
| 6.02053 | 4.07453 | 7.26970 | 34.08908 | 0.181160 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.27785 | | | | | 0 | |
| 30.94360 | -13.51924 | 33.76797 | 336.39941 | 0.537443 | 1 | 5.848 |
| 25.45142 | 57.02972 | 62.45128 | 65.94951 | 0.993960 | 2 | 11.696 |
| -59.74272 | 19.45546 | 62.83078 | 161.98196 | 1.000000 | 3 | 17.544 |
| -18.62553 | -40.98764 | 44.98824 | 245.51987 | 0.715386 | 4 | 23.392 |
| 31.88739 | -11.37908 | 33.85687 | 349.36084 | 0.538858 | 5 | 29.240 |
| 0.62546 | 23.94125 | 23.94942 | 88.50345 | 0.381173 | 6 | 35.088 |
| -22.84109 | -11.26480 | 25.47783 | 206.25165 | 0.405340 | 7 | 40.936 |
| 25.88802 | -14.55080 | 29.69704 | 330.66089 | 0.472651 | 8 | 46.784 |
| 6.27432 | 35.78534 | 36.33121 | 80.09522 | 0.578239 | 9 | 52.632 |
| -33.44180 | -1.50910 | 33.47589 | 182.58379 | 0.532793 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -10.01601 | | | | | 0 | |
| 9.29022 | -19.38072 | 21.49232 | 295.61084 | 1.000000 | 1 | 5.848 |
| -2.06231 | 13.80537 | 13.95855 | 98.49629 | 0.649467 | 2 | 11.696 |
| -11.28662 | -2.96623 | 11.66989 | 194.72488 | 0.542979 | 3 | 17.544 |
| 1.04827 | 3.22786 | 3.39381 | 72.00848 | 0.157908 | 4 | 23.392 |
| -8.77629 | 2.32006 | 9.07777 | 165.19226 | 0.422373 | 5 | 29.240 |
| -1.57498 | -7.53510 | 7.69793 | 258.19385 | 0.358171 | 6 | 35.088 |
| 6.74076 | -0.39510 | 6.75232 | 356.64551 | 0.314174 | 7 | 40.936 |
| 2.20899 | 3.13244 | 3.83299 | 54.80862 | 0.178342 | 8 | 46.784 |
| 1.91787 | 0.49317 | 1.98027 | 14.42081 | 0.092138 | 9 | 52.632 |
| 3.49924 | 2.12776 | 4.09537 | 31.30226 | 0.190551 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 16.13881 | | | | | 0 | |
| 23.36996 | -8.93604 | 25.02014 | 339.07446 | 0.572981 | 1 | 5.848 |
| 25.76254 | 35.25710 | 43.66658 | 53.84418 | 1.000000 | 2 | 11.696 |
| -35.60233 | 23.59753 | 42.71263 | 146.46324 | 0.978154 | 3 | 17.544 |
| -21.63771 | -25.81317 | 33.68248 | 230.02879 | 0.771356 | 4 | 23.392 |
| 19.73975 | -14.16140 | 24.29407 | 324.34399 | 0.556354 | 5 | 29.240 |
| 5.78168 | 16.19801 | 17.19893 | 70.35657 | 0.393869 | 6 | 35.088 |
| -15.17498 | -4.06957 | 15.71119 | 195.01213 | 0.359799 | 7 | 40.936 |
| 14.05267 | -10.45370 | 17.51448 | 323.35449 | 0.401096 | 8 | 46.784 |
| 7.48164 | 20.59801 | 21.91466 | 70.03794 | 0.501863 | 9 | 52.632 |
| -17.92958 | 3.52471 | 18.27274 | 168.87323 | 0.418460 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.79006 | | | | | 0 | |
| 0.72356 | -1.56107 | 1.72061 | 294.86792 | 1.000000 | 1 | 5.848 |
| -0.19262 | 1.08185 | 1.09886 | 100.09566 | 0.638848 | 2 | 11.696 |
| -0.88289 | -0.25379 | 0.91864 | 196.03729 | 0.533907 | 3 | 17.544 |
| 0.09100 | -0.28967 | 0.29505 | 72.03554 | 0.171480 | 4 | 23.392 |
| -0.71149 | 0.20134 | 0.73943 | 164.19974 | 0.429751 | 5 | 29.240 |
| -0.14047 | -0.60872 | 0.62472 | 257.00513 | 0.363083 | 6 | 35.088 |
| 0.54631 | -0.03931 | 0.54773 | 355.88403 | 0.318333 | 7 | 40.936 |
| 0.19121 | 0.26171 | 0.32412 | 53.84694 | 0.188377 | 8 | 46.784 |
| 0.14877 | 0.05285 | 0.15787 | 19.55623 | 0.091795 | 9 | 52.632 |
| 0.28362 | 0.17022 | 0.33078 | 30.97107 | 0.192248 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 500 OSC CTR 570 TEST COND 31 COMP RUN 40.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.37162 | | | | | 0 | |
| 1.94623 | -0.73616 | 2.08081 | 339.29076 | 0.574009 | 1 | 5.848 |
| 2.20075 | 2.88056 | 3.62504 | 52.72012 | 1.000000 | 2 | 11.696 |
| -2.89889 | 2.03992 | 3.54469 | 144.86633 | 0.977834 | 3 | 17.544 |
| -1.86499 | -2.11673 | 2.82112 | 228.61772 | 0.778231 | 4 | 23.392 |
| 1.61582 | -1.22589 | 2.02762 | 322.83545 | 0.559336 | 5 | 29.240 |
| 0.52161 | 1.33866 | 1.43669 | 68.71163 | 0.396323 | 6 | 35.088 |
| -1.25052 | -0.30803 | 1.28789 | 193.83752 | 0.355277 | 7 | 40.936 |
| 1.13333 | -0.86734 | 1.42714 | 322.57300 | 0.393688 | 8 | 46.784 |
| 0.64376 | 1.67155 | 1.79123 | 68.93687 | 0.494128 | 9 | 52.632 |
| -1.44133 | 0.32878 | 1.47835 | 167.15033 | 0.407816 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.88888 | | | | | 0 | |
| -1.33467 | 0.86750 | 1.35022 | 140.02257 | 1.000000 | 1 | 5.848 |
| 0.16140 | -0.58728 | 0.60905 | 285.36646 | 0.451077 | 2 | 11.696 |
| -0.13921 | 0.28031 | 0.31298 | 116.41084 | 0.231795 | 3 | 17.544 |
| -0.02548 | 0.02481 | 0.03556 | 135.76378 | 0.026333 | 4 | 23.392 |
| -0.10957 | 0.11127 | 0.15616 | 134.55856 | 0.115657 | 5 | 29.240 |
| -0.01319 | 0.06039 | 0.06182 | 102.32454 | 0.045784 | 6 | 35.088 |
| -0.04116 | 0.12552 | 0.13209 | 108.15565 | 0.097831 | 7 | 40.936 |
| -0.06229 | 0.03647 | 0.07218 | 149.65589 | 0.053460 | 8 | 46.784 |
| -0.07407 | 0.07189 | 0.10322 | 135.85310 | 0.076448 | 9 | 52.632 |
| -0.05879 | -0.00409 | 0.06892 | 183.40274 | 0.051041 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.06811 | | | | | 0 | |
| 0.02716 | 0.34352 | 0.34459 | 85.47948 | 0.581861 | 1 | 5.848 |
| -0.58946 | 0.05716 | 0.59222 | 174.46127 | 1.000000 | 2 | 11.696 |
| -0.18094 | 0.00945 | 0.18119 | 177.01125 | 0.305943 | 3 | 17.544 |
| -0.07663 | -0.04990 | 0.09144 | 213.07408 | 0.154405 | 4 | 23.392 |
| -0.09169 | 0.08448 | 0.12467 | 137.34303 | 0.210516 | 5 | 29.240 |
| 0.03395 | 0.02215 | 0.04053 | 33.12888 | 0.068444 | 6 | 35.088 |
| -0.02874 | 0.04919 | 0.05697 | 120.30104 | 0.096196 | 7 | 40.936 |
| -0.08982 | 0.02062 | 0.09215 | 167.07280 | 0.155606 | 8 | 46.784 |
| -0.08560 | -0.12622 | 0.15251 | 235.85759 | 0.257523 | 9 | 52.632 |
| -0.08072 | -0.06353 | 0.10272 | 218.20346 | 0.173441 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.35949 | | | | | 0 | |
| -5.05815 | 4.22953 | 6.59346 | 140.09831 | 1.000000 | 1 | 5.848 |
| 0.80303 | -2.85508 | 2.96586 | 285.70923 | 0.449818 | 2 | 11.696 |
| -0.68295 | 1.34113 | 1.50501 | 116.98692 | 0.228258 | 3 | 17.544 |
| -0.11799 | 0.09752 | 0.15308 | 140.42723 | 0.023216 | 4 | 23.392 |
| -0.53302 | 0.52607 | 0.74891 | 135.37508 | 0.113584 | 5 | 29.240 |
| -0.06045 | 0.26733 | 0.27408 | 102.74150 | 0.041569 | 6 | 35.088 |
| -0.20631 | 0.58796 | 0.62311 | 109.33559 | 0.094504 | 7 | 40.936 |
| -0.29140 | 0.16439 | 0.33457 | 150.57170 | 0.050743 | 8 | 46.784 |
| -0.35386 | 0.33531 | 0.48749 | 136.54230 | 0.073936 | 9 | 52.632 |
| -0.32549 | -0.02047 | 0.32613 | 183.59901 | 0.049462 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.27699 | | | | | 0 | |
| 0.08804 | 1.67758 | 1.67989 | 86.99567 | 0.597562 | 1 | 5.848 |
| -2.79575 | 0.29465 | 2.81124 | 173.98373 | 1.000000 | 2 | 11.696 |
| -0.88500 | 0.05909 | 0.88697 | 176.18045 | 0.315509 | 3 | 17.544 |
| -0.34982 | -0.25201 | 0.43114 | 215.76811 | 0.153364 | | 23.392 |
| -0.44748 | 0.39267 | 0.59534 | 138.73268 | 0.211771 | 5 | 29.240 |
| 0.15885 | 0.09001 | 0.18258 | 29.53764 | 0.064946 | 6 | 35.088 |
| -0.12738 | 0.22818 | 0.26133 | 119.17270 | 0.092957 | 7 | 40.936 |
| -0.42270 | 0.09819 | 0.43395 | 166.92276 | 0.154363 | 8 | 46.784 |
| -0.40119 | -0.59634 | 0.71873 | 236.06862 | 0.255664 | 9 | 52.632 |
| -0.37840 | -0.29351 | 0.47888 | 217.79941 | 0.170347 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 11.07374 | | | | | 0 | |
| -12.77568 | 10.63239 | 16.62123 | 140.23155 | 1.000000 | 1 | 5.848 |
| 2.09032 | -7.14073 | 7.44640 | 286.31641 | 0.447844 | 2 | 11.696 |
| -1.73558 | 3.25824 | 3.69166 | 118.04309 | 0.222105 | 3 | 17.544 |
| -0.26898 | 0.14116 | 0.30377 | 152.30923 | 0.018276 | 4 | 23.392 |
| -1.33470 | 1.24958 | 1.82835 | 136.88635 | 0.110001 | 5 | 29.240 |
| -0.13475 | 0.59175 | 0.56796 | 103.72395 | 0.034171 | 6 | 35.088 |
| -0.54364 | 1.37161 | 1.47542 | 111.62125 | 0.088767 | 7 | 40.936 |
| -0.67790 | 0.35379 | 0.76466 | 152.64009 | 0.046005 | 8 | 46.784 |
| -0.85738 | 0.77543 | 1.15602 | 137.67320 | 0.069551 | 9 | 52.632 |
| -0.77421 | -0.05381 | 0.77608 | 183.97594 | 0.046692 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.45196 | | | | | 0 | |
| 0.02491 | 4.22951 | 4.22958 | 89.66797 | 0.628416 | 1 | 5.848 |
| -6.68144 | 0.81152 | 6.73054 | 173.07480 | 1.000000 | 2 | 11.696 |
| -2.23739 | 0.20631 | 2.24686 | 174.73177 | 0.333833 | 3 | 17.544 |
| -0.77398 | -0.67218 | 1.02512 | 220.97314 | 0.152309 | 4 | 23.392 |
| -1.12696 | 0.90192 | 1.44343 | 141.32910 | 0.214460 | 5 | 29.240 |
| 0.36984 | 0.14646 | 0.39778 | 21.60400 | 0.059101 | 6 | 35.088 |
| -0.26361 | 0.52201 | 0.58479 | 116.79306 | 0.086887 | 7 | 40.936 |
| -0.99518 | 0.23653 | 1.02290 | 166.63039 | 0.151979 | 8 | 46.784 |
| -0.93701 | -1.41454 | 1.69673 | 236.47884 | 0.252094 | 9 | 52.632 |
| -0.88408 | -0.66594 | 1.10683 | 216.98941 | 0.164449 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.28387 | | | | | 0 | |
| -31.15231 | 25.49628 | 40.25575 | 140.70177 | 1.000000 | 1 | 5.848 |
| 5.66044 | -17.03476 | 17.95038 | 288.38086 | 0.445913 | 2 | 11.696 |
| -4.16095 | 6.88609 | 8.04560 | 121.14268 | 0.199862 | 3 | 17.544 |
| -0.41135 | -0.57192 | 0.70448 | 234.27470 | 0.017500 | 4 | 23.392 |
| -3.12614 | 2.38854 | 3.93420 | 142.61823 | 0.097730 | 5 | 29.240 |
| -0.21179 | 0.27197 | 0.34471 | 127.90892 | 0.008563 | 6 | 35.088 |
| -1.53060 | 2.34228 | 2.79803 | 123.16322 | 0.069506 | 7 | 40.936 |
| -1.1532* | 0.3257z | 1.19834 | 164.22794 | 0.029768 | 8 | 46.784 |
| -1.79183 | 1.27956 | 2.28180 | 144.46916 | 0.056695 | 9 | 52.632 |
| -1.48680 | -0.14943 | 1.49390 | 185.58658 | 0.037110 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.45883 | | | | | 0 | |
| -1.87444 | 9.71181 | 9.89104 | 100.92418 | 0.747708 | 1 | 5.848 |
| -13.00356 | 2.42906 | 13.22849 | 169.41913 | 1.000000 | 2 | 11.696 |
| -5.50031 | 1.02323 | 5.59467 | 169.46167 | 0.422926 | 3 | 17.544 |
| -0.92154 | -1.99646 | 2.16263 | 244.77827 | 0.163483 | 4 | 23.392 |
| -2.72579 | 1.46904 | 3.09645 | 151.67793 | 0.234074 | 5 | 29.240 |
| 0.66146 | -0.38192 | 0.75400 | 331.31445 | 0.056998 | 6 | 35.088 |
| -0.14915 | 0.78655 | 0.80056 | 100.73724 | 0.060518 | 7 | 40.936 |
| -1.82247 | 0.49194 | 1.88770 | 164.89406 | 0.142699 | 8 | 46.784 |
| -1.65335 | -2.64328 | 3.11777 | 237.97437 | 0.235686 | 9 | 52.632 |
| -1.53056 | -0.93248 | 1.79224 | 211.35158 | 0.135484 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.93735 | | | | | 0 | |
| -30.91029 | 24.53181 | 39.46207 | 141.56290 | 1.000000 | 1 | 5.848 |
| 6.57181 | -15.40535 | 17.20955 | 292.44946 | 0.436104 | 2 | 11.696 |
| -4.23444 | 4.88217 | 6.46267 | 130.93604 | 0.163769 | 3 | 17.544 |
| 0.03267 | -2.17330 | 2.17355 | 270.86108 | 0.055079 | 4 | 23.392 |
| -2.91529 | 1.17128 | 3.14179 | 158.11113 | 0.079615 | 5 | 29.240 |
| 0.05063 | -1.61547 | 1.61627 | 271.79492 | 0.040957 | 6 | 35.088 |
| -1.86597 | 0.58633 | 1.95592 | 162.55621 | 0.049564 | 7 | 40.936 |
| -0.25866 | -0.61560 | 0.66773 | 247.20932 | 0.016921 | 8 | 46.784 |
| -1.22803 | 0.18157 | 1.24138 | 171.58971 | 0.031458 | 9 | 52.632 |
| -0.74904 | -0.17513 | 0.76926 | 193.15913 | 0.019494 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.03573 | | | | | 0 | |
| -4.95347 | 9.33752 | 10.57006 | 117.94562 | 1.000000 | 1 | 5.848 |
| -7.10495 | 3.39217 | 7.87319 | 154.47842 | 0.744857 | 2 | 11.696 |
| -5.49766 | 1.89481 | 5.81503 | 160.98315 | 0.550141 | 3 | 17.544 |
| 0.76328 | -2.48821 | 2.60265 | 287.05371 | 0.246229 | 4 | 23.392 |
| -2.65664 | 0.10246 | 2.65861 | 177.79126 | 0.251523 | 5 | 29.240 |
| 0.18813 | -1.59955 | 1.61057 | 276.70776 | 0.152371 | 6 | 35.088 |
| 0.73552 | -0.05365 | 0.73748 | 355.82812 | 0.069770 | 7 | 40.936 |
| -0.71044 | 0.31789 | 0.77832 | 155.89322 | 0.073634 | 8 | 46.784 |
| -0.48584 | -1.21979 | 1.31298 | 248.28287 | 0.124217 | 9 | 52.632 |
| -0.42368 | 0.23807 | 0.48599 | 150.66859 | 0.045978 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 36.25294 | | | | | 0 | |
| -36.72913 | 28.47388 | 46.47354 | 142.21574 | 1.000000 | 1 | 5.848 |
| 7.74629 | -15.14098 | 17.00745 | 297.09473 | 0.365960 | 2 | 11.696 |
| -6.75614 | 3.89626 | 7.79912 | 150.02803 | 0.167818 | 3 | 17.544 |
| 0.39938 | -3.08426 | 3.11001 | 277.37793 | 0.066920 | 4 | 23.392 |
| -3.67141 | 0.22084 | 3.67805 | 176.55775 | 0.079143 | 5 | 29.240 |
| 0.99061 | -2.87724 | 3.01492 | 287.38062 | 0.064874 | 6 | 35.088 |
| -2.24252 | 0.02691 | 2.24268 | 179.31253 | 0.048257 | 7 | 40.936 |
| 0.31262 | -1.25931 | 1.29754 | 283.94165 | 0.027920 | 8 | 46.784 |
| -0.77571 | -0.59762 | 0.97922 | 217.61150 | 0.021071 | 9 | 52.632 |
| -0.18567 | -0.35621 | 0.40169 | 242.46994 | 0.008643 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 14.90214 | | | | | 0 | |
| -4.22881 | 18.29579 | 18.77812 | 103.01460 | 1.000000 | 1 | 5.848 |
| -4.96664 | 6.40768 | 8.10715 | 127.77954 | 0.431734 | 2 | 11.696 |
| -5.81910 | 2.31994 | 6.26451 | 158.26396 | 0.333607 | 3 | 17.544 |
| 1.51993 | -3.16364 | 3.50982 | 295.66113 | 0.186910 | 4 | 23.392 |
| -3.00127 | -1.46076 | 3.33788 | 205.95285 | 0.177753 | 5 | 29.240 |
| -0.44748 | -2.21925 | 2.26391 | 258.59985 | 0.120561 | 6 | 35.088 |
| 1.48934 | -0.26655 | 1.51298 | 349.85669 | 0.080572 | 7 | 40.936 |
| 0.16327 | -0.01093 | 0.16363 | 356.17065 | 0.008714 | 8 | 46.784 |
| 0.60300 | -0.86111 | 1.05124 | 305.00171 | 0.055982 | 9 | 52.632 |
| 0.10284 | 0.31230 | 0.32879 | 71.77353 | 0.017509 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 36.41295 | | | | | 0 | |
| -31.80388 | 24.47452 | 40.13089 | 142.42010 | 1.000000 | 1 | 5.848 |
| 5.71986 | -7.78576 | 9.66099 | 306.30298 | 0.240737 | 2 | 11.696 |
| -9.11304 | 2.28113 | 9.39420 | 165.94679 | 0.234089 | 3 | 17.544 |
| 0.45860 | -1.98478 | 2.03707 | 283.01025 | 0.050761 | 4 | 23.392 |
| -3.79521 | -0.37997 | 3.81418 | 185.71722 | 0.095043 | 5 | 29.240 |
| 1.80211 | -2.06287 | 2.75917 | 311.14014 | 0.068256 | 6 | 35.088 |
| -1.62570 | 0.78696 | 1.80616 | 154.16948 | 0.045007 | 7 | 40.936 |
| 0.28808 | -0.89321 | 0.93852 | 287.97524 | 0.023386 | 8 | 46.784 |
| -0.22931 | -0.62342 | 0.66426 | 249.90501 | 0.016552 | 9 | 52.632 |
| 0.15279 | -0.46997 | 0.49419 | 288.00952 | 0.012314 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 26.13504 | | | | | 0 | |
| 2.34165 | 28.46529 | 28.56143 | 85.29720 | 1.000000 | 1 | 5.848 |
| -4.95299 | 8.51577 | 9.85142 | 120.18340 | 0.344920 | 2 | 11.696 |
| -4.05180 | 1.19860 | 4.22536 | 163.52077 | 0.147939 | 3 | 17.544 |
| 0.57112 | -2.47008 | 2.53524 | 283.01880 | 0.088765 | 4 | 23.392 |
| -2.41908 | -2.33994 | 3.36560 | 224.04718 | 0.117837 | 5 | 29.240 |
| -1.03132 | -1.17891 | 1.56635 | 228.62039 | 0.054841 | 6 | 35.088 |
| 1.38826 | 0.31659 | 1.40441 | 13.02804 | 0.049172 | 7 | 40.936 |
| 0.58837 | -0.41401 | 0.71943 | 324.85743 | 0.025189 | 8 | 46.784 |
| 1.15821 | -1.27530 | 1.72274 | 312.24512 | 0.060317 | 9 | 52.632 |
| -0.13537 | -0.90256 | 0.91266 | 261.46997 | 0.031954 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.39221 | | | | | 0 | |
| -20.83002 | 16.13281 | 26.34685 | 142.24229 | 1.000000 | 1 | 5.848 |
| 3.31726 | -1.52175 | 3.64965 | 335.35718 | 0.138523 | 2 | 11.696 |
| -8.84698 | 0.83053 | 8.88587 | 174.63695 | 0.337265 | 3 | 17.544 |
| 0.33673 | -1.14145 | 1.19008 | 286.43628 | 0.045170 | 4 | 23.392 |
| -2.99592 | -0.43157 | 3.02684 | 189.19730 | 0.114884 | 5 | 29.240 |
| 1.66755 | -1.02668 | 1.95827 | 328.38013 | 0.074326 | 6 | 35.088 |
| -0.87686 | 1.07167 | 1.38469 | 129.29063 | 0.052556 | 7 | 40.936 |
| 0.07196 | -0.32337 | 0.33128 | 282.54614 | 0.012574 | 8 | 46.784 |
| -0.05309 | -0.31639 | 0.32081 | 260.47485 | 0.012176 | 9 | 52.632 |
| 0.15152 | -0.32641 | 0.35986 | 294.90063 | 0.013659 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.82803 | | | | | 0 | |
| 5.31667 | 27.18372 | 27.69875 | 78.93353 | 1.000000 | 1 | 5.848 |
| -4.16683 | 7.53903 | 8.61391 | 118.92953 | 0.310986 | 2 | 11.696 |
| -2.41508 | 0.27698 | 2.43091 | 173.65735 | 0.087763 | 3 | 17.544 |
| -0.09091 | -1.38780 | 1.39077 | 266.25220 | 0.050211 | 4 | 23.392 |
| -1.51589 | -2.01068 | 2.51809 | 232.98665 | 0.090910 | 5 | 29.240 |
| -1.11795 | -0.35858 | 1.17405 | 197.78355 | 0.042386 | 6 | 35.088 |
| 0.92568 | 0.56250 | 1.08319 | 31.28560 | 0.039108 | 7 | 40.936 |
| 0.55557 | -0.42771 | 0.70114 | 322.40845 | 0.025313 | 8 | 46.784 |
| 0.98707 | -1.21678 | 1.56680 | 309.04932 | 0.056566 | 9 | 52.632 |
| -0.35563 | -1.32712 | 1.37394 | 254.99858 | 0.049603 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.97099 | | | | | 0 | |
| -17.14880 | 14. 3775 | 22.28888 | 140.29895 | 1.000000 | 1 | 5.848 |
| 2.89066 | 2. 5739 | 3.66766 | 37.98721 | 0.164551 | 2 | 11.696 |
| -11.39724 | -0.!8275 | 11.40074 | 181.42113 | 0.511499 | 3 | 17.544 |
| 0.32278 | -1.'9311 | 1.82193 | 280.20435 | 0.081742 | 4 | 23.392 |
| -3.17647 | -0.!4294 | 3.18576 | 184.37349 | 0.142930 | 5 | 29.240 |
| 1.32710 | -0.!1957 | 1.61456 | 325.28125 | 0.072438 | 6 | 35.088 |
| -0.61045 | 1..2127 | 1.27668 | 118.56525 | 0.057279 | 7 | 40.936 |
| -0.19880 | 0.21369 | 0.29187 | 132.93294 | 0.013095 | 8 | 46.784 |
| -0.39935 | 0.03754 | 0.40111 | 174.63026 | 0.017996 | 9 | 52.632 |
| -0.06606 | -0.03047 | 0.07275 | 204.76611 | 0.003264 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.07442 | | | | | 0 | |
| 6.52243 | 31.05891 | 31.73637 | 78.14009 | 1.000000 | 1 | 5.848 |
| -4.03015 | 8.11467 | 9.06035 | 116.41133 | 0.285488 | 2 | 11.696 |
| -2.90287 | 0.09800 | 2.90452 | 178.06650 | 0.091520 | 3 | 17.544 |
| -0.09272 | -0.86610 | 0.87105 | 263.88940 | 0.027447 | 4 | 23.392 |
| -1.36150 | -1.94473 | 2.37395 | 235.00432 | 0.074802 | 5 | 29.240 |
| -1.36494 | -0.53082 | 1.46452 | 201.25079 | 0.046146 | 6 | 35.088 |
| 1.03705 | 0.66295 | 1.23084 | 32.58932 | 0.038783 | 7 | 40.936 |
| 0.50330 | -0.18370 | 0.535?7 | 339.94824 | 0.016882 | 8 | 46.784 |
| 0.74189 | -1.10204 | 1.32849 | 303.94849 | 0.041860 | 9 | 52.632 |
| -0.56313 | -1.37047 | 1.48166 | 247.66208 | 0.046686 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 62.44922 | | | | | 0 | |
| -17.30672 | 18.53600 | 25.35951 | 133.03575 | 0.809610 | 1 | 5.848 |
| 5.59681 | 15.90053 | 16.85678 | 70.30846 | 0.538158 | 2 | 11.696 |
| -30.98291 | -4.60411 | 31.32312 | 188.45238 | 1.000000 | 3 | 17.544 |
| 0.52807 | -7.79560 | 7.81346 | 273.87524 | 0.249447 | 4 | 23.392 |
| -6.28859 | 0.59527 | 6.29679 | 174.57542 | 0.201027 | 5 | 29.240 |
| 0.18114 | -2.12791 | 2.13561 | 274.86572 | 0.068180 | 6 | 35.088 |
| -0.59849 | 1.19857 | 1.33968 | 116.53461 | 0.042770 | 7 | 40.936 |
| -1.35452 | 2.11555 | 2.51203 | 122.63025 | 0.080197 | 8 | 46.784 |
| -2.52802 | 1.40938 | 2.89435 | 150.86031 | 0.092403 | 9 | 52.632 |
| -1.26318 | 1.34441 | 1.84474 | 133.21558 | 0.058894 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 63.93462 | | | | | 0 | |
| 11.16264 | 63.31299 | 64.28947 | 80.00096 | 1.000000 | 1 | 5.848 |
| -5.69581 | 15.69206 | 16.68018 | 109.82048 | 0.259454 | 2 | 11.696 |
| -8.81128 | 0.34778 | 8.81814 | 177.73970 | 0.137163 | 3 | 17.544 |
| 1.10796 | 0.07116 | 1.11024 | 3.67474 | 0.017269 | 4 | 23.392 |
| -2.04534 | -2.35502 | 3.11922 | 229.02556 | 0.048518 | 5 | 29.240 |
| -3.41580 | -2.61440 | 4.30149 | 217.42984 | 0.066908 | 6 | 35.088 |
| 2.41918 | 0.77833 | 2.54130 | 17.83463 | 0.039529 | 7 | 40.936 |
| 0.60239 | 0.98224 | 1.15224 | 58.47997 | 0.017923 | 8 | 46.784 |
| 0.04644 | -0.77240 | 0.77379 | 273.44043 | 0.012036 | 9 | 52.632 |
| -1.59076 | -1.39473 | 2.11561 | 221.28332 | 0.032908 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 42.21254 | | | | | 0 | |
| 2.27726 | -1.44032 | 2.69773 | 327.57959 | 0.106880 | 1 | 5.848 |
| 3.95351 | 17.39070 | 17.83441 | 77.19228 | 0.706574 | 2 | 11.696 |
| -24.65167 | -5.42104 | 25.24068 | 192.40224 | 1.000000 | 3 | 17.544 |
| 0.39338 | -7.50437 | 7.51468 | 273.00073 | 0.297721 | 4 | 23.392 |
| -3.60859 | 0.62440 | 3.66227 | 170.18327 | 0.145092 | 5 | 29.240 |
| -1.23462 | -1.52094 | 1.95896 | 230.93207 | 0.077611 | 6 | 35.088 |
| -0.16134 | -0.23888 | 0.28876 | 235.96428 | 0.011420 | 7 | 40.936 |
| -1.25001 | 1.65816 | 2.07654 | 127.01103 | 0.082269 | 8 | 46.784 |
| -2.19999 | 1.04291 | 2.43467 | 154.63664 | 0.096458 | 9 | 52.632 |
| -1.13953 | 1.21713 | 1.66731 | 133.11415 | 0.066057 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 36.06674 | | | | | 0 | |
| 4.18996 | 30.09284 | 30.37321 | 82.07077 | 1.000000 | 1 | 5.848 |
| -1.49973 | 6.93299 | 7.09334 | 102.20613 | 0.233539 | 2 | 11.696 |
| -3.98802 | 0.55172 | 4.02600 | 172.12340 | 0.132591 | 3 | 17.544 |
| 1.50800 | 1.09552 | 1.86303 | 36.99739 | 0.061368 | 4 | 23.392 |
| 0.37676 | 0.93767 | 1.01053 | 68.10937 | 0.033270 | 5 | 29.240 |
| -3.45071 | -0.67572 | 3.51624 | 191.07953 | 0.115768 | 6 | 35.088 |
| -0.06250 | -0.97243 | 0.97444 | 266.32251 | 0.032082 | 7 | 40.936 |
| 0.96994 | 0.41550 | 1.05518 | 23.18900 | 0.034741 | 8 | 46.784 |
| 0.10310 | 1.24557 | 1.24983 | 85.26830 | 0.041149 | 9 | 52.632 |
| -1.66238 | 0.52631 | 1.74370 | 162.43233 | 0.057409 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.01123 | | | | | 0 | |
| 17.55301 | -24.31245 | 29.98671 | 305.82837 | 1.000000 | 1 | 5.848 |
| 6.08464 | 23.36346 | 24.14278 | 75.40244 | 0.805116 | 2 | 11.696 |
| -27.44000 | -6.08316 | 28.18619 | 192.49971 | 0.937288 | 3 | 17.544 |
| 0.30910 | -9.29166 | 9.29680 | 271.90527 | 0.310031 | 4 | 23.392 |
| -1.53446 | -0.62305 | 1.65613 | 202.09898 | 0.055229 | 5 | 29.240 |
| -0.88407 | -0.62656 | 1.08358 | 215.32620 | 0.036135 | 6 | 35.088 |
| -0.84115 | -1.33826 | 1.58065 | 237.84895 | 0.052712 | 7 | 40.936 |
| -0.64061 | -0.53569 | 0.83507 | 219.90260 | 0.027848 | 8 | 46.784 |
| -0.66268 | -0.20969 | 0.69587 | 197.55894 | 0.023179 | 9 | 52.632 |
| -0.71082 | 0.51819 | 0.87965 | 143.90796 | 0.029325 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.47827 | | | | | 0 | |
| 2.53329 | 3.33926 | 4.19144 | 52.81459 | 0.663235 | 1 | 5.848 |
| -0.04211 | 3.14899 | 3.14927 | 90.76627 | 0.498326 | 2 | 11.696 |
| 1.24055 | -0.33518 | 1.28503 | 344.88013 | 0.203337 | 3 | 17.544 |
| 2.56268 | 1.08333 | 2.78225 | 22.91544 | 0.440251 | 4 | 23.392 |
| 3.26307 | 4.91492 | 5.89940 | 56.41934 | 0.933510 | 5 | 29.240 |
| -5.60530 | 2.91876 | 6.31969 | 152.49336 | 1.000000 | 6 | 35.088 |
| -3.40518 | -3.97555 | 4.93759 | 226.39803 | 0.781303 | 7 | 40.936 |
| 2.32485 | -1.24568 | 2.63755 | 331.81689 | 0.417394 | 8 | 46.784 |
| 1.49539 | 2.83511 | 3.18685 | 62.82648 | 0.504273 | 9 | 52.632 |
| -2.06840 | 1.38413 | 2.48079 | 146.21048 | 0.393813 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 26.38705 | | | | | 0 | |
| 24.43614 | -27.54730 | 36.82361 | 311.57495 | 1.000000 | 1 | 5.848 |
| 9.65292 | 22.22458 | 24.23036 | 66.92292 | 0.658012 | 2 | 11.696 |
| -23.25789 | -2.06500 | 23.34937 | 185.07381 | 0.634087 | 3 | 17.544 |
| -1.14337 | -10.67048 | 10.73156 | 263.88379 | 0.291431 | 4 | 23.392 |
| 3.51757 | -2.18133 | 4.13902 | 328.19580 | 0.112401 | 5 | 29.240 |
| 1.12812 | 2.60445 | 2.83827 | 66.58008 | 0.077078 | 6 | 35.088 |
| -2.85218 | -1.29832 | 3.13378 | 204.47519 | 0.085102 | 7 | 40.936 |
| 0.99603 | -4.20042 | 4.31689 | 283.33984 | 0.117232 | 8 | 46.784 |
| 2.59895 | -0.14665 | 2.60308 | 356.77026 | 0.070691 | 9 | 52.632 |
| -1.25990 | 1.03069 | 1.62778 | 140.71443 | 0.044205 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.02576 | | | | | 0 | |
| 8.95815 | -5.96754 | 10.76383 | 326.33008 | 0.890588 | 1 | 5.848 |
| -2.96478 | 11.71692 | 12.08619 | 104.19977 | 1.000000 | 2 | 11.696 |
| -8.03984 | -5.32138 | 9.64138 | 213.49963 | 0.797718 | 3 | 17.544 |
| 5.38023 | -0.74074 | 5.43098 | 352.16089 | 0.449354 | 4 | 23.392 |
| 0.85332 | 4.52438 | 4.60415 | 79.31920 | 0.380943 | 5 | 29.240 |
| -4.05858 | -0.78279 | 4.13338 | 190.91672 | 0.341992 | 6 | 35.088 |
| 0.87221 | -2.34008 | 2.49734 | 290.44165 | 0.206627 | 7 | 40.936 |
| -0.29664 | 1.11207 | 1.15096 | 104.93564 | 0.095229 | 8 | 46.784 |
| -1.33242 | -0.66781 | 1.49040 | 206.62010 | 0.123314 | 9 | 52.632 |
| 0.71190 | -1.84685 | 1.97931 | 291.07983 | 0.163766 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.06830 | | | | | 0 | |
| 30.55579 | -35.41098 | 46.77171 | 310.79053 | 1.000000 | 1 | 5.848 |
| 10.85904 | 25.47679 | 27.69450 | 66.91464 | 0.592121 | 2 | 11.696 |
| -25.61382 | -2.27582 | 25.71471 | 185.07747 | 0.549792 | 3 | 17.544 |
| -1.25309 | -12.30444 | 12.36809 | 264.18481 | 0.264435 | 4 | 23.392 |
| 4.42151 | -2.74212 | 5.20278 | 328.19360 | 0.111238 | 5 | 29.240 |
| 2.14909 | 2.35555 | 3.18860 | 47.62431 | 0.068174 | 6 | 35.088 |
| -1.70655 | -1.10687 | 2.03408 | 212.96748 | 0.043490 | 7 | 40.936 |
| 1.16093 | -3.02268 | 3.23796 | 291.01050 | 0.069229 | 8 | 46.784 |
| 1.11711 | -0.81913 | 1.38525 | 323.74854 | 0.029617 | 9 | 52.632 |
| -0.31296 | -1.03883 | 1.08495 | 253.23442 | 0.023197 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.88058 | | | | | 0 | |
| 25.52922 | -3.78050 | 25.80760 | 351.57642 | 1.000000 | 1 | 5.848 |
| 1.00817 | 22.73753 | 22.75986 | 87.46117 | 0.88190_ | 2 | 11.696 |
| -17.33240 | -4.46565 | 17.89842 | 194.44789 | 0.693533 | 3 | 17.544 |
| 1.41496 | -4.74256 | 4.94888 | 286.60254 | 0.191761 | 4 | 23.392 |
| 3.02550 | -0.21446 | 3.03309 | 355.94531 | 0.117527 | 5 | 29.240 |
| 0.27978 | 0.69221 | 0.74661 | 67.99179 | 0.028930 | 6 | 35.088 |
| 0.39295 | 0.44859 | 0.59635 | 48.78288 | 0.023 08 | 7 | 40.936 |
| -2.19563 | -1.40923 | 2.60897 | 212.69385 | 0.101 03 | 8 | 46.784 |
| 0.93145 | -2.79311 | 2.90641 | 288.69189 | 0.112618 | 9 | 52.632 |
| 1.44757 | 0.50319 | 1.53253 | 19.16776 | 0.059383 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 14.66283 | | | | | 0 | |
| 15.67504 | -19.47658 | 25.00087 | 308.82764 | 1.000000 | 1 | 5.848 |
| 4.78181 | 12.65497 | 13.52826 | 69.30040 | 0.541112 | 2 | 11.696 |
| -12.48511 | -1.58472 | 12.58529 | 187.23381 | 0.503394 | 3 | 17.544 |
| -0.39497 | -5.94352 | 5.95685 | 266.13306 | 0.234266 | 4 | 23.392 |
| 1.76211 | -1.29615 | 2.18747 | 323.66309 | 0.087496 | 5 | 29.240 |
| 1.18332 | 0.48881 | 1.28030 | 22.44461 | 0.051210 | 6 | 35.088 |
| 0.09149 | -0.42210 | 0.43190 | 282.22974 | 0.017276 | 7 | 40.936 |
| 0.39354 | -0.31310 | 0.50289 | 321.49414 | 0.020115 | 8 | 46.784 |
| -0.61622 | -0.76230 | 0.98022 | 231.04868 | 0.039207 | 9 | 52.632 |
| 0.44884 | -1.59167 | 1.65375 | 285.74805 | 0.066148 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 14.90164 | | | | | 0 | |
| -14.12552 | -0.70647 | 18.13927 | 357.76782 | 1.000000 | 1 | 5.848 |
| 2.87982 | 13.75134 | 14.04965 | 78.17194 | 0.774544 | 2 | 11.696 |
| -10.44580 | -0.83182 | 10.47887 | 184.55296 | 0.577690 | 3 | 17.544 |
| -1.73703 | -3.77859 | 4.15873 | 245.31151 | 0.229267 | 4 | 23.392 |
| 2.81996 | -2.24136 | 3.60220 | 321.52148 | 0.198586 | 5 | 29.240 |
| 2.01155 | 1.70800 | 2.63887 | 40.33441 | 0.145478 | 6 | 35.088 |
| -0.80630 | 1.30918 | 1.53755 | 121.62813 | 0.084764 | 7 | 40.936 |
| -1.46861 | -2.26183 | 2.69679 | 237.00420 | 0.148672 | 8 | 46.784 |
| 1.97122 | -1.67710 | 2.58812 | 319.60913 | 0.142681 | 9 | 52.632 |
| 0.60055 | 1.85514 | 1.95067 | 72.37104 | 0.107550 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.16954 | | | | | 0 | |
| 1.25004 | -1.56691 | 2.00445 | 308.58179 | 1.000000 | 1 | 5.848 |
| 0.37278 | 1.00387 | 1.07085 | 69.62791 | 0.534237 | 2 | 11.696 |
| -0.98733 | -0.13044 | 0.99591 | 187.52573 | 0.496849 | 3 | 17.544 |
| -0.02891 | -0.46075 | 0.46166 | 266.40942 | 0.230318 | 4 | 23.392 |
| 0.13543 | -0.10226 | 0.16970 | 322.94556 | 0.084661 | 5 | 29.240 |
| 0.09553 | 0.03129 | 0.10053 | 18.13377 | 0.050152 | 6 | 35.088 |
| 0.01795 | -0.03195 | 0.03664 | 299.32520 | 0.018280 | 7 | 40.936 |
| 0.02931 | -0.01142 | 0.03145 | 338.71753 | 0.015691 | 8 | 46.784 |
| -0.06216 | -0.06455 | 0.08961 | 226.36136 | 0.044708 | 9 | 52.632 |
| 0.04255 | -0.13873 | 0.14511 | 287.05127 | 0.072395 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 498 OSC CTR 250 TEST COND 33 COMP RUN 32.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.25161 | | | | | 0 | |
| 1.50302 | -0.04225 | 1.50361 | 358.38965 | 1.000000 | 1 | 5.848 |
| 0.25576 | 1.12151 | 1.15030 | 77.15315 | 0.765025 | 2 | 11.696 |
| -0.85214 | -0.05656 | 0.85364 | 183.39554 | 0.567725 | 3 | 17.544 |
| -0.16592 | -0.31673 | 0.35756 | 242.35229 | 0.237801 | 4 | 23.392 |
| 0.23862 | -0.20305 | 0.31332 | 319.60474 | 0.208379 | 5 | 29.240 |
| 0.18183 | 0.15068 | 0.23614 | 39.64764 | 0.157051 | 6 | 35.088 |
| -0.07482 | 0.11590 | 0.13879 | 122.62030 | 0.092307 | 7 | 40.936 |
| -0.12144 | -0.19725 | 0.23163 | 238.38127 | 0.154052 | 8 | 46.784 |
| 0.17352 | -0.13732 | 0.22128 | 321.64136 | 0.147168 | 9 | 52.632 |
| 0.04672 | 0.16550 | 0.17197 | 74.23463 | 0.114369 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.34897 | | | | | 0 | |
| -0.81784 | 0.92482 | 1.23455 | 131.48718 | 1.000000 | 1 | 5.848 |
| 0.18773 | -0.64435 | 0.67114 | 286.24341 | 0.543623 | 2 | 11.696 |
| 0.02549 | 0.21825 | 0.21974 | 83.33786 | 0.177987 | 3 | 17.544 |
| -0.06401 | -0.06908 | 0.09128 | 225.47313 | 0.073941 | 4 | 23.392 |
| -0.02179 | -0.03331 | 0.03980 | 236.80228 | 0.032240 | 5 | 29.240 |
| 0.01125 | -0.04903 | 0.05031 | 282.91968 | 0.040748 | 6 | 35.088 |
| -0.06655 | -0.01290 | 0.06779 | 193.97282 | 0.054909 | 7 | 40.936 |
| -0.09621 | -0.04704 | 0.10709 | 206.05411 | 0.086743 | 8 | 46.784 |
| -0.10958 | -0.07092 | 0.13061 | 212.88903 | 0.105793 | 9 | 52.632 |
| -0.08249 | -0.06236 | 0.10341 | 217.09520 | 0.083762 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.19518 | | | | | 0 | |
| 0.05414 | 0.94751 | 0.84924 | 86.34496 | 1.000000 | 1 | 5.848 |
| -0.30342 | -0.04264 | 0.30641 | 188.00017 | 0.360801 | 2 | 11.696 |
| -0.35462 | 0.12963 | 0.37757 | 159.92084 | 0.444599 | 3 | 17.544 |
| 0.08574 | -0.28841 | 0.30089 | 286.55542 | 0.354301 | 4 | 23.392 |
| -0.06207 | -0.07822 | 0.09986 | 231.57027 | 0.117584 | 5 | 29.240 |
| -0.02652 | -0.02432 | 0.03599 | 222.52502 | 0.042375 | 6 | 35.088 |
| -0.11438 | -0.07349 | 0.13596 | 212.71835 | 0.160091 | 7 | 40.936 |
| -0.01317 | -0.16121 | 0.16175 | 265.32910 | 0.190462 | 8 | 46.784 |
| -0.02078 | -0.15114 | 0.15256 | 262.17139 | 0.179643 | 9 | 52.632 |
| 0.03804 | -0.14625 | 0.15111 | 284.57983 | 0.177939 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.96338 | | | | | 0 | |
| -4.11776 | 4.56487 | 6.14768 | 132.09225 | 1.000000 | 1 | 5.848 |
| 3.92576 | -3.10442 | 3.23951 | 286.60498 | 0.526949 | 2 | 11.696 |
| 0.06780 | 1.05537 | 1.05755 | 86.32434 | 0.172024 | 3 | 17.544 |
| -0.29773 | -0.30370 | 0.42530 | 225.56908 | 0.069180 | 4 | 23.392 |
| -0.13325 | -0.14195 | 0.19469 | 226.81216 | 0.031669 | 5 | 29.240 |
| 0.04300 | -0.22398 | 0.22807 | 280.86646 | 0.037098 | 6 | 35.088 |
| -0.32743 | -0.05203 | 0.33154 | 189.02971 | 0.053929 | 7 | 40.936 |
| -0.45934 | -0.21020 | 0.50515 | 204.58943 | 0.082170 | 8 | 46.784 |
| -0.52711 | -0.32185 | 0.61760 | 211.40793 | 0.100461 | 9 | 52.632 |
| -0.39836 | -0.28299 | 0.48864 | 215.38921 | 0.079484 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.26430 | | | | | 0 | |
| 0.17970 | 4.07897 | 4.08292 | 87.47739 | 1.000000 | 1 | 5.848 |
| -1.42789 | -0.15414 | 1.43619 | 186.16129 | 0.351755 | 2 | 11.696 |
| -1.68954 | 0.61842 | 1.79916 | 159.89601 | 0.440655 | 3 | 17.544 |
| 0.39136 | -1.35535 | 1.41072 | 286.10620 | 0.345517 | 4 | 23.392 |
| -0.31367 | -0.35255 | 0.47189 | 228.34001 | 0.115578 | 5 | 29.240 |
| -0.12175 | -0.10593 | 0.16139 | 221.02565 | 0.039527 | 6 | 35.088 |
| -0.53447 | -0.34218 | 0.63462 | 212.62822 | 0.155433 | 7 | 40.936 |
| -0.07942 | -0.74943 | 0.75365 | 263.93579 | 0.184586 | 8 | 46.784 |
| -0.10306 | -0.69784 | 0.70541 | 261.59888 | 0.172770 | 9 | 52.632 |
| 0.16272 | -0.68232 | 0.70145 | 283.41309 | 0.171802 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.09773 | | | | | 0 | |
| -10.92977 | 11.72333 | 16.02797 | 132.99371 | 1.000000 | 1 | 5.848 |
| 2.37377 | -7.63935 | 7.99965 | 287.26147 | 0.499106 | 2 | 11.696 |
| -0.08016 | 2.61445 | 2.61568 | 91.75621 | 0.163195 | 3 | 17.544 |
| -0.68475 | -0.70319 | 0.98150 | 225.76128 | 0.061237 | 4 | 23.392 |
| -0.45470 | -0.26623 | 0.52691 | 210.34904 | 0.032874 | 5 | 29.240 |
| 0.55955 | -0.49613 | 0.64923 | 274.38867 | 0.031148 | 6 | 35.088 |
| -0.83627 | -0.08256 | 0.84034 | 185.63832 | 0.052429 | 7 | 40.936 |
| -1.11165 | -0.44359 | 1.19688 | 201.75386 | 0.074674 | 8 | 46.784 |
| -1.29133 | -0.70296 | 1.47027 | 208.56256 | 0.091731 | 9 | 52.632 |
| -0.98452 | -0.61788 | 1.16234 | 212.11234 | 0.072520 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 44
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 23.85921 | | | | | 0 | |
| 0.07794 | 10.01878 | 10.01909 | 89.55426 | 1.000000 | 1 | 5.848 |
| -3.36120 | -0.14902 | 3.36458 | 182.53848 | 0.335809 | 2 | 11.696 |
| -4.07240 | 1.49439 | 4.33793 | 159.84909 | 0.432967 | 3 | 17.544 |
| 0.86561 | -3.18178 | 3.29742 | 285.21899 | 0.329114 | 4 | 23.392 |
| -0.83764 | -0.75835 | 1.12992 | 222.15561 | 0.112777 | 5 | 29.240 |
| -0.27259 | -0.21010 | 0.34416 | 217.62401 | 0.034351 | 6 | 35.088 |
| -1.24063 | -0.78875 | 1.47015 | 212.44659 | 0.146733 | 7 | 40.936 |
| -0.26848 | -1.72188 | 1.74269 | 261.13745 | 0.173937 | 8 | 46.784 |
| -0.26582 | -1.58113 | 1.60348 | 260.42114 | 0.160043 | 9 | 52.632 |
| 0.30817 | -1.57906 | 1.60885 | 281.04297 | 0.160579 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.15140 | | | | | 0 | |
| -31.36267 | 30.32550 | 43.62620 | 135.96324 | 1.000000 | 1 | 5.848 |
| 5.96928 | -17.03968 | 18.05405 | 289.30713 | 0.413834 | 2 | 11.696 |
| -2.34866 | 6.08302 | 6.52068 | 111.11165 | 0.149467 | 3 | 17.544 |
| -1.18480 | -1.03211 | 1.57070 | 221.07913 | 0.036004 | 4 | 23.392 |
| -2.18688 | 0.28352 | 2.20518 | 172.61384 | 0.050547 | 5 | 29.240 |
| -0.39222 | -0.48243 | 0.62176 | 230.88663 | 0.014252 | 6 | 35.088 |
| -2.14482 | 0.3 073 | 2.16722 | 171.75670 | 0.049677 | 7 | 40.936 |
| -2.29941 | -0.24535 | 2.31246 | 186.09847 | 0.053006 | 8 | 46.784 |
| -2.79833 | -0.63662 | 2.88133 | 193.78610 | 0.066046 | 9 | 52.632 |
| -2.20366 | -0.59830 | 2.28344 | 195.18982 | 0.052341 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 39.63193 | | | | | 0 | |
| -3.47055 | 21.56944 | 21.84686 | 99.14069 | 1.000000 | 1 | 5.848 |
| -6.04933 | 1.68879 | 6.27849 | 164.47217 | 0.287386 | 2 | 11.696 |
| -8.38067 | 3.13179 | 8.87931 | 159.34705 | 0.406434 | 3 | 17.544 |
| 0.99643 | -5.66539 | 5.75235 | 279.97518 | 0.263303 | 4 | 23.392 |
| -2.49256 | -0.68047 | 2.56387 | 193.54475 | 0.117356 | 5 | 29.240 |
| -0.41113 | 0.84803 | 0.91392 | 173.33701 | 0.041847 | 6 | 35.088 |
| -2.13572 | -1.22813 | 2.46365 | 209.98888 | 0.112769 | 7 | 40.936 |
| -1.29418 | -2.64843 | 2.99773 | 243.93717 | 0.137127 | 8 | 46.784 |
| -0.71373 | -2.24186 | 2.35197 | 252.33447 | 0.107657 | 9 | 52.632 |
| -0.12877 | -2.54667 | 2.54992 | 267.18522 | 0.116718 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 41.14027 | | | | | 0 | |
| -39.23779 | 33.06451 | 51.31146 | 139.88017 | 1.000000 | 1 | 5.848 |
| 6.42207 | -13.88326 | 15.29066 | 294.82422 | 0.298114 | 2 | 11.696 |
| -8.15741 | 5.30560 | 8.12792 | 139.24982 | 0.158404 | 3 | 17.544 |
| -0.18113 | -0.00549 | 0.18122 | 181.73651 | 0.003532 | 4 | 23.392 |
| -3.99100 | 1.73474 | 4.35171 | 156.50716 | 0.084810 | 5 | 29.240 |
| -1.22160 | 0.62502 | 1.37220 | 152.90393 | 0.026743 | 6 | 35.088 |
| -2.27817 | 1.08365 | 2.52277 | 154.56113 | 0.049166 | 7 | 40.936 |
| -1.54380 | 1.11568 | 1.90487 | 144.14008 | 0.037124 | 8 | 46.784 |
| -2.16439 | 1.02168 | 2.39341 | 154.73080 | 0.046645 | 9 | 52.632 |
| -1.85309 | 0.90768 | 2.06345 | 153.90349 | 0.040214 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.57559 | | | | | 0 | |
| -9.31552 | 16.93408 | 19.32722 | 118.81544 | 1.000000 | 1 | 5.848 |
| -2.25153 | 5.32196 | 5.77864 | 112.93149 | 0.298989 | 2 | 11.696 |
| -5.29132 | 2.10047 | 5.69298 | 158.34863 | 0.294558 | 3 | 17.544 |
| -0.00297 | -1.93587 | 2.13610 | 244.99356 | 0.110523 | 4 | 23.392 |
| -3.18459 | 1.45540 | 3.50140 | 155.43892 | 0.181164 | 5 | 29.240 |
| 0.10875 | 0.96537 | 0.95161 | 83.43769 | 0.049237 | 6 | 35.088 |
| -0.47035 | -0.05254 | 0.47328 | 186.37389 | 0.024488 | 7 | 40.936 |
| -2.33101 | 0.00492 | 2.33102 | 179.87903 | 0.120608 | 8 | 46.784 |
| -0.80993 | 0.55759 | 0.98445 | 145.35883 | 0.050936 | 9 | 52.632 |
| -1.69321 | -0.30664 | 1.72076 | 190.26497 | 0.089033 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 65.26616 | | | | | 0 | |
| -48.95316 | 39.46570 | 62.88046 | 141.12448 | 1.000000 | 1 | 5.848 |
| 10.06084 | -12.73005 | 16.22574 | 308.32007 | 0.258041 | 2 | 11.696 |
| -9.02728 | 3.51356 | 9.68695 | 158.73315 | 0.154053 | 3 | 17.544 |
| 1.95728 | -1.38278 | 2.39647 | 324.75952 | 0.038111 | 4 | 23.392 |
| -4.65910 | 0.73279 | 4.71638 | 171.06166 | 0.075005 | 5 | 29.240 |
| -0.87078 | -0.56304 | 1.03694 | 212.88713 | 0.016491 | 6 | 35.088 |
| -2.44545 | 0.14594 | 2.44980 | 176.58472 | 0.038960 | 7 | 40.936 |
| -1.22616 | 0.67722 | 1.40075 | 151.08795 | 0.022276 | 8 | 46.784 |
| -2.25709 | 0.87393 | 2.42037 | 158.83385 | 0.038492 | 9 | 52.632 |
| -2.15952 | 0.71787 | 2.27571 | 161.61206 | 0.036191 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.50073 | | | | | 0 | |
| -7.81337 | 22.61914 | 23.93060 | 109.05658 | 1.000000 | 1 | 5.848 |
| -0.49229 | 8.71856 | 8.73245 | 93.23180 | 0.364907 | 2 | 11.696 |
| -3.38211 | 0.54763 | 3.42616 | 170.90291 | 0.143170 | 3 | 17.544 |
| -1.27626 | -0.39533 | 1.33638 | 197.25471 | 0.055844 | 4 | 23.392 |
| -3.12977 | 1.37403 | 3.41811 | 156.29753 | 0.142834 | 5 | 29.240 |
| 1.30199 | 0.66623 | 1.46255 | 27.09877 | 0.061116 | 6 | 35.088 |
| 1.33305 | -0.07437 | 1.33524 | 350.72013 | 0.055796 | 7 | 40.936 |
| -2.40545 | 0.34115 | 2.42952 | 171.92789 | 0.101527 | 8 | 46.784 |
| -0.91753 | 1.61115 | 1.85409 | 119.66103 | 0.077478 | 9 | 52.632 |
| -3.39396 | -0.01399 | 3.09399 | 180.25900 | 0.129290 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 66.30495 | | | | | 0 | |
| -37.68810 | 31.54204 | 49.20985 | 139.98398 | 1.000000 | 1 | 5.848 |
| 11.99723 | -7.88637 | 14.35717 | 326.66091 | 0.291754 | 2 | 11.696 |
| -7.36018 | -0.68735 | 7.09355 | 185.56053 | 0.144149 | 3 | 17.544 |
| 4.08657 | -4.55335 | 6.11826 | 311.90747 | 0.124330 | 4 | 23.392 |
| -2.13043 | -3.01742 | 3.69372 | 234.77618 | 0.075061 | 5 | 29.240 |
| 1.08265 | -3.74942 | 3.94104 | 285.94482 | 0.080086 | 6 | 35.088 |
| -1.50099 | -2.41974 | 2.84748 | 238.18613 | 0.057864 | 7 | 40.936 |
| -0.89432 | -1.79965 | 2.00961 | 243.57516 | 0.040838 | 8 | 46.784 |
| -2.11501 | -1.52270 | 2.60612 | 215.75146 | 0.052959 | 9 | 52.632 |
| -2.15862 | -1.47809 | 2.61618 | 214.40042 | 0.053164 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.16486 | | | | | 0 | |
| 4.59535 | 29.22649 | 29.59554 | 81.06433 | 1.000000 | 1 | 5.848 |
| -1.16001 | 7.70000 | 7.78689 | 99.56728 | 0.263199 | 2 | 11.696 |
| -1.49353 | -1.45144 | 2.08262 | 224.18115 | 0.070393 | 3 | 17.544 |
| 0.52560 | -.08247 | 1.20332 | 295.99917 | 0.040673 | 4 | 23.392 |
| -1.00272 | -1.64823 | 1.92927 | 238.68530 | 0.065210 | 5 | 29.240 |
| 2.39866 | -1.13047 | 2.65170 | 334.76563 | 0.089628 | 6 | 35.088 |
| 2.41692 | -1.31082 | 2.74950 | 331.52651 | 0.092934 | 7 | 40.936 |
| -0.43245 | -1.91679 | 1.96496 | 257.28589 | 0.066416 | 8 | 46.784 |
| -0.61278 | -0.06622 | 0.61635 | 186.16812 | 0.020833 | 9 | 52.632 |
| -2.73794 | -1.76710 | 3.25868 | 212.83861 | 0.110144 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.[illegible]06. | | | | | 0 | |
| -11.68570 | 19.61960 | 29.24376 | 137.86357 | 1.000000 | 1 | 5.848 |
| 9.57336 | -3.08045 | 10.05675 | 342.16309 | 0.343894 | 2 | 11.696 |
| -4.83745 | -2.58904 | 5.48671 | 208.15599 | 0.187620 | 3 | 17.544 |
| 3.91543 | -5.09809 | 6.42815 | 307.52490 | 0.219813 | 4 | 23.392 |
| -0.43630 | -4.14706 | 4.16994 | 263.99340 | 0.142593 | 5 | 29.240 |
| 1.86226 | -4.52173 | 4.89022 | 292.38403 | 0.167223 | 6 | 35.088 |
| -0.55478 | -2.92638 | 2.97850 | 259.26516 | 0.101851 | 7 | 40.936 |
| -0.58556 | -2.48925 | 2.55719 | 256.76245 | 0.087444 | 8 | 46.784 |
| -1.54847 | -2.31113 | 2.78192 | 236.17764 | 0.095129 | 9 | 52.632 |
| -1.60889 | -2.16586 | 2.69789 | 233.59098 | 0.092255 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.04173 | | | | | 0 | |
| 9.81911 | 26.4[illegible]11 | 28.25981 | 69.66803 | 1.000000 | 1 | 5.848 |
| -1.87961 | 5.17186 | 5.50284 | 109.97266 | 0.194723 | 2 | 11.696 |
| -0.51941 | 1.78672 | 1.86149 | 253.61691 | 0.065163 | 3 | 17.544 |
| 1.33618 | -1.29740 | 1.86083 | 317.89819 | 0.063726 | 4 | 23.392 |
| 0.21576 | -3.01397 | 3.02169 | 274.09473 | 0.106925 | 5 | 29.240 |
| 2.16224 | -1.82408 | 2.82883 | 319.84688 | 0.100102 | 6 | 35.088 |
| 2.15161 | -1.63461 | 2.70211 | 322.77539 | 0.095617 | 7 | 40.936 |
| 0.66803 | -2.64720 | 2.73019 | 284.16309 | 0.096610 | 8 | 46.784 |
| -0.28635 | -1.12964 | 1.16537 | 255.77559 | 0.041258 | 9 | 52.632 |
| -1.68693 | -2.26391 | 2.82324 | 233.31035 | 0.099903 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 53.64009 | | | | | 0 | |
| -17.66835 | 17.89716 | 25.14912 | 134.63142 | 1.000000 | 1 | 5.848 |
| 8.09863 | -0.20710 | 8.10127 | 358.53516 | 0.322129 | 2 | 11.696 |
| -6.47709 | -3.34628 | 7.29042 | 207.32239 | 0.289888 | 3 | 17.544 |
| 3.57164 | -5.33776 | 6.42249 | 303.78750 | 0.255376 | 4 | 23.392 |
| -0.75542 | -4.21937 | 4.28646 | 259.84937 | 0.170442 | 5 | 29.240 |
| 2.17046 | -4.84583 | 5.30978 | 294.12744 | 0.211131 | 6 | 35.088 |
| -0.04430 | -2.43108 | 2.43148 | 268.95581 | 0.096682 | 7 | 40.936 |
| -0.63197 | -2.14913 | 2.24012 | 253.61348 | 0.089074 | 8 | 46.784 |
| -1.39828 | -2.11269 | 2.53351 | 236.50151 | 0.100739 | 9 | 52.632 |
| -1.41652 | -1.91624 | 2.38303 | 233.52553 | 0.094756 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.22221 | | | | | 0 | |
| 10.65152 | 30.31499 | 32.13181 | 70.64043 | 1.000000 | 1 | 5.848 |
| -3.37793 | 4.94452 | 5.9882. | 124.33965 | 0.186364 | 2 | 11.696 |
| -0.34561 | -1.01439 | 1.07165 | -251.18542 | 0.033352 | 3 | 17.544 |
| 1.22250 | -0.43389 | 1.29722 | 340.55898 | 0.040372 | 4 | 23.392 |
| 0.00987 | -4.01423 | 4.01424 | 270.14087 | 0.124930 | 5 | 29.240 |
| 1.76602 | -2.20332 | 2.82373 | 308.71313 | 0.087880 | 6 | 35.088 |
| 1.99458 | -1.61536 | 2.56666 | 320.99683 | 0.079879 | 7 | 40.936 |
| 0.81205 | -2.53816 | 2.66490 | 287.74121 | 0.082936 | 8 | 46.784 |
| -0.14619 | -1.53989 | 1.54681 | 264.57666 | 0.048140 | 9 | 52.632 |
| -1.21378 | -2.11245 | 2.43632 | 240.11943 | 0.075823 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 113.02132 | | | | | 0 | |
| -22.90837 | 29.57571 | 37.41010 | 127.76022 | 1.000000 | 1 | 5.848 |
| 6.50824 | 10.24832 | 12.14024 | 57.58220 | 0.324518 | 2 | 11.696 |
| -22.55872 | -6.16577 | 23.38614 | 195.28676 | 0.625129 | 3 | 17.544 |
| 3.38449 | -8.28120 | 8.94611 | 292.22949 | 0.239136 | 4 | 23.392 |
| -5.20113 | -4.76026 | 7.05066 | 222.46588 | 0.188469 | 5 | 29.240 |
| 3.58135 | -7.35177 | 8.17768 | 295.97266 | 0.218596 | 6 | 35.088 |
| 1.46601 | 0.05895 | 1.46720 | 2.30284 | 0.039219 | 7 | 40.936 |
| -1.38404 | -0.01445 | 1.38411 | 180.59802 | 0.036998 | 8 | 46.784 |
| -1.83159 | -0.61719 | 1.93278 | 198.62218 | 0.051665 | 9 | 52.632 |
| -1.58033 | -0.29764 | 1.60788 | 190.67853 | 0.042980 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 66.59651 | | | | | 0 | |
| 11.96007 | 64.26355 | 65.36699 | 79.45728 | 1.000000 | 1 | 5.848 |
| -11.54095 | 10.04865 | 15.33546 | 138.81317 | 0.234605 | 2 | 11.696 |
| -1.33156 | 2.69231 | 3.00360 | 116.31604 | 0.045950 | 3 | 17.544 |
| -0.03428 | 3.79792 | 3.79808 | 90.51721 | 0.058104 | 4 | 23.392 |
| -2.60567 | -8.56356 | 8.95120 | 253.07629 | 0.136938 | 5 | 29.240 |
| 0.50808 | -3.86666 | 3.89990 | 277.48584 | 0.059662 | 6 | 35.088 |
| 2.19288 | -1.57384 | 2.69920 | 324.33276 | 0.041293 | 7 | 40.936 |
| 0.21157 | -1.76208 | 1.77473 | 276.84644 | 0.027150 | 8 | 46.784 |
| 0.06815 | -2.73060 | 2.73145 | 271.42993 | 0.041786 | 9 | 52.632 |
| -0.71042 | -1.30453 | 1.48543 | 241.42815 | 0.022725 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 35 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 68.80083 | | | | | 0 | |
| -0.28974 | 5.03657 | 5.01494 | 93.31212 | 0.221214 | 1 | 5.848 |
| -1.42351 | 16.52457 | 16.58575 | 94.92361 | 0.731613 | 2 | 11.696 |
| -22.26418 | -4.27090 | 22.67013 | 193.85904 | 1.000000 | 3 | 17.544 |
| 0.87888 | -5.22035 | 5.29381 | 279.55640 | 0.233515 | 4 | 23.392 |
| -4.65909 | -1.91309 | 5.03657 | 202.32370 | 0.222168 | 5 | 29.240 |
| 1.95767 | -3.44709 | 3.96420 | 299.59302 | 0.174865 | 6 | 35.088 |
| 2.03962 | 1.84493 | 2.75009 | 42.13347 | 0.121309 | 7 | 40.936 |
| -0.22330 | 2.19158 | 2.20292 | 95.81783 | 0.097173 | 8 | 46.784 |
| -0.50220 | 1.31627 | 1.40882 | 110.88353 | 0.062145 | 9 | 52.632 |
| -0.00749 | 1.27551 | 1.27553 | 90.33673 | 0.056245 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 72.30826 | | | | | 0 | |
| 3.65484 | 31.70799 | 31.91792 | 83.42474 | 1.000000 | 1 | 5.848 |
| -7.60465 | 8.07074 | 11.86908 | 133.29494 | 0.367425 | 2 | 11.696 |
| -1.98489 | 2.40044 | 3.11479 | [illegible] | 0.097587 | 3 | 17.544 |
| -1.16050 | 4.11678 | 4.27722 | [illegible] 74290 | 0.134007 | 4 | 23.392 |
| -1.75701 | -3.77718 | 4.16583 | [illegible] 09371 | 0.130517 | 5 | 29.240 |
| -1.44617 | -1.26798 | 1.92332 | [illegible] | 0.060258 | 6 | 35.088 |
| 0.22850 | -0.04990 | 0.23389 | 347.68042 | 0.007328 | 7 | 40.936 |
| -0.88474 | 0.60900 | 1.07408 | 145.45859 | 0.033651 | 8 | 46.784 |
| -0.00692 | -1.52407 | 1.52408 | 269.74365 | 0.047750 | 9 | 52.632 |
| 0.19697 | 0.38927 | 0.43627 | 63.15990 | 0.013668 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 93.49861 | | | | | 0 | |
| 24.01964 | -23.87001 | 33.86325 | 315.17896 | 1.000000 | 1 | 5.848 |
| -1.74679 | 28.22270 | 28.27682 | 93.56578 | 0.835030 | 2 | 11.696 |
| -29.03625 | -5.68845 | 29.58821 | 191.08435 | 0.873756 | 3 | 17.544 |
| 2.20133 | -8.62705 | 8.90347 | 284.31445 | 0.262924 | 4 | 23.392 |
| -2.56355 | -4.34042 | 5.04093 | 239.43291 | 0.148861 | 5 | 29.240 |
| 2.39700 | -3.50198 | 4.24375 | 304.39038 | 0.125320 | 6 | 35.088 |
| 2.74443 | 0.09132 | 2.74491 | 1.07122 | 0.081059 | 7 | 40.936 |
| 1.44850 | 1.66922 | 2.21008 | 49.04948 | 0.065265 | 8 | 46.784 |
| 0.06787 | 0.62152 | 0.62918 | 81.05133 | 0.018580 | 9 | 52.632 |
| 0.85779 | -0.01068 | 0.85786 | 359.28662 | 0.025333 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 130.04541 | | | | | 0 | |
| 8.56341 | 5.78465 | 10.33412 | 34.03934 | 0.793041 | 1 | 5.848 |
| -3.59044 | 12.52488 | 13.03100 | 106.02105 | 1.000000 | 2 | 11.696 |
| -4.90265 | -2.49805 | 5.50238 | 207.00021 | 0.422253 | 3 | 17.544 |
| 0.19577 | 1.93521 | 1.94509 | 84.22354 | 0.149266 | 4 | 23.392 |
| 1.64386 | 0.39528 | 1.69071 | 13.52042 | 0.129745 | 5 | 29.240 |
| -1.85087 | 0.67378 | 1.97038 | 159.94203 | 0.151207 | 6 | 35.088 |
| -0.54707 | 0.04273 | 0.54873 | 175.53337 | 0.042110 | 7 | 40.936 |
| -1.12341 | 0.11179 | 1.12896 | 174.31728 | 0.086636 | 8 | 46.784 |
| -0.33093 | -1.49949 | 1.53958 | 257.55444 | 0.117840 | 9 | 52.632 |
| -0.38210 | -0.35278 | 0.52006 | 222.73516 | 0.039909 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 39.33698 | | | | | 0 | |
| 30.36392 | -25.54828 | 39.66695 | 319.90405 | 1.000000 | 1 | 5.848 |
| 3.07820 | 21.26820 | 21.48979 | 81.76457 | 0.541756 | 2 | 11.696 |
| -21.53174 | -1.91529 | 21.61674 | 185.08319 | 0.544956 | 3 | 17.544 |
| 0.10713 | -7.49110 | 7.49186 | 270.81909 | 0.188869 | 4 | 23.392 |
| -0.10530 | -3.92468 | 3.92609 | 268.46289 | 0.098976 | 5 | 29.240 |
| 1.94081 | -1.77582 | 2.63064 | 317.54175 | 0.066318 | 6 | 35.088 |
| 1.33874 | 0.57416 | 1.45667 | 23.21344 | 0.036723 | 7 | 40.936 |
| 0.77692 | 0.17657 | 0.79673 | 12.80405 | 0.020086 | 8 | 46.784 |
| 0.59799 | 0.06175 | 0.60117 | 5.89571 | 0.015155 | 9 | 52.632 |
| 0.99544 | -0.91677 | 1.07191 | 301.21021 | 0.027023 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.50874 | | | | | 0 | |
| 10.88590 | 2.03978 | 11.07536 | 10.61289 | 0.760888 | 1 | 5.848 |
| -6.60901 | 12.96894 | 14.55534 | 117.00359 | 1.000000 | 2 | 11.696 |
| -7.98494 | -4.29140 | 9.06507 | 208.25519 | 0.622779 | 3 | 17.544 |
| 3.45358 | -0.22852 | 3.46113 | 356.21411 | 0.237783 | 4 | 23.392 |
| 1.65748 | 0.33655 | 1.69130 | 11.47798 | 0.116194 | 5 | 29.240 |
| -1.28028 | 0.45326 | 1.35815 | 160.50426 | 0.093306 | 6 | 35.088 |
| -1.47786 | -0.08967 | 1.48058 | 183.47215 | 0.101717 | 7 | 40.936 |
| 0.02738 | -1.29046 | 1.25076 | 271.25439 | 0.085929 | 8 | 46.784 |
| 0.44171 | -0.44588 | 0.62763 | 314.73096 | 0.043119 | 9 | 52.632 |
| -0.90256 | 0.12374 | 0.91080 | 172.19165 | 0.062573 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 38.08438 | | | | | 0 | |
| 35.81340 | -34.35320 | 49.62[illegible] | 316.19[illegible] | 1.000000 | 1 | 5.848 |
| 3.02714 | 21.97072 | 22.17827 | 82.15509 | 0.446907 | 2 | 11.696 |
| -22.80194 | -2.86718 | 22.98149 | 187.16690 | 0.463092 | 3 | 17.544 |
| 0.86192 | -9.26865 | 9.30864 | 275.31274 | 0.187575 | 4 | 23.392 |
| 0.86035 | -5.25606 | 5.32600 | 279.29614 | 0.107323 | 5 | 29.240 |
| 1.99160 | -1.87893 | 2.73804 | 316.66724 | 0.055173 | 6 | 35.088 |
| 0.46744 | 0.41246 | 0.62340 | 41.42444 | 0.012562 | 7 | 40.936 |
| 0.60160 | -0.04346 | 0.60336 | 355.86938 | 0.012158 | 8 | 46.784 |
| 0.47065 | -0.26774 | 0.54148 | 330.36523 | 0.010911 | 9 | 52.632 |
| 0.35810 | -1.14094 | 1.19581 | 287.42505 | 0.024096 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 58.08354 | | | | | 0 | |
| 28.72374 | 18.06207 | 33.93068 | 32.16251 | 1.000000 | 1 | 5.848 |
| -6.66755 | 22.05185 | 23.03778 | 106.82317 | 0.678966 | 2 | 11.696 |
| -17.89586 | -3.71556 | 18.27750 | 191.72917 | 0.538672 | 3 | 17.544 |
| 1.96626 | -6.80939 | 7.08759 | 286.10645 | 0.208884 | 4 | 23.392 |
| 6.61857 | -1.99696 | 6.91136 | 343.20557 | 0.203691 | 5 | 29.240 |
| -0.29357 | 1.55163 | 1.57916 | 100.71391 | 0.046541 | 6 | 35.088 |
| -1.57993 | 0.40216 | 1.63031 | 165.71898 | 0.048048 | 7 | 40.936 |
| -1.61237 | -0.70182 | 1.75849 | 273.52208 | 0.051826 | 8 | 46.784 |
| 0.03374 | -1.19561 | 1.19668 | 271.91446 | 0.[illegible] | 9 | 52.632 |
| -0.10202 | -1.07908 | 1.08389 | 264.59912 | 0.03[illegible] | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 16.88060 | | | | | 0 | |
| 18.10190 | -20.05139 | 27.01364 | 312.07495 | 1.000000 | 1 | 5.848 |
| 0.63589 | 10.95350 | 10.97194 | 86.67744 | 0.406163 | 2 | 11.696 |
| -11.39630 | -2.23434 | 11.61327 | 191.09261 | 0.429904 | 3 | 17.544 |
| 1.09441 | -5.08961 | 5.20594 | 282.13525 | 0.192715 | 4 | 23.392 |
| 0.66167 | -3.05733 | 3.12811 | 282.21167 | 0.115797 | 5 | 29.240 |
| 0.93784 | -1.06533 | 1.41932 | 311.35815 | 0.052541 | 6 | 35.088 |
| -0.33765 | -0.09315 | 0.10047 | 247.99518 | 0.003719 | 7 | 40.936 |
| 0.33658 | 0.01544 | 0.33693 | 2.62660 | 0.012473 | 8 | 46.784 |
| 0.09537 | -0.25890 | 0.27591 | 290.22266 | 0.010214 | 9 | 52.632 |
| 0.12844 | -0.55514 | 0.56961 | 283.02710 | 0.021093 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 48.83833 | | | | | 0 | |
| 21.00070 | 14.72148 | 25.64665 | 35.03043 | 1.000000 | 1 | 5.848 |
| -2.18125 | 13.95523 | 14.12467 | 98.88370 | 0.550741 | 2 | 11.696 |
| -12.22990 | -1.30247 | 12.29906 | 186.07901 | 0.479558 | 3 | 17.544 |
| -0.27247 | -6.03214 | 6.03829 | 267.41357 | 0.235441 | 4 | 23.392 |
| 5.45951 | -1.78603 | 5.74930 | 341.91333 | 0.223939 | 5 | 29.240 |
| 0.29715 | 1.33280 | 1.36552 | 77.43138 | 0.053244 | 6 | 35.088 |
| -0.62367 | 0.43225 | 0.75882 | 145.27699 | 0.029587 | 7 | 40.936 |
| -1.65682 | 0.12135 | 1.66125 | 175.81090 | 0.064775 | 8 | 46.784 |
| -0.31060 | -1.01231 | 1.05889 | 252.94269 | 0.041288 | 9 | 52.632 |
| 0.39327 | -1.17167 | 1.23591 | 288.55420 | 0.048190 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.31011 | | | | | 0 | |
| 1.43986 | -1.62475 | 2.17094 | 311.54736 | 1.000000 | 1 | 5.848 |
| 0.04106 | 0.86809 | 0.86906 | 87.29221 | 0.400313 | 2 | 11.696 |
| -0.90377 | -0.18611 | 0.92274 | 191.63603 | 0.425040 | 3 | 17.544 |
| 0.09421 | -0.40921 | 0.41991 | 282.96509 | 0.193423 | 4 | 23.392 |
| 0.05548 | -0.24782 | 0.25376 | 282.62769 | 0.116889 | 5 | 29.240 |
| 0.07373 | -0.08581 | 0.11314 | 310.67017 | 0.052114 | 6 | 35.088 |
| -0.00638 | -0.01066 | 0.01242 | 239.10129 | 0.005722 | 7 | 40.936 |
| 0.02695 | 0.00148 | 0.02699 | 3.14710 | 0.012433 | 8 | 46.784 |
| 0.00600 | -0.[illegible]2204 | 0.02284 | 285.22925 | 0.010523 | 9 | 52.632 |
| 0.00953 | -0.[illegible]4397 | 0.04499 | 282.22583 | 0.020723 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 175 TEST COND 36 COMP RUN 44.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.09169 | | | | | 0 | |
| 1.74518 | 1.23633 | 2.13972 | 35.31477 | 1.000000 | 1 | 5.848 |
| -0.16064 | 1.14233 | 1.15357 | 98.00500 | 0.539371 | 2 | 11.696 |
| -1.00984 | -0.09700 | 1.01449 | 185.48671 | 0.474343 | 3 | 17.544 |
| -0.03578 | -0.50979 | 0.51104 | 265.98496 | 0.238948 | 4 | 23.392 |
| 0.45840 | -0.15098 | 0.48262 | 341.76953 | 0.225658 | 5 | 29.240 |
| 0.02884 | 0.11218 | 0.11582 | 75.58133 | 0.054156 | 6 | 35.088 |
| -0.04772 | 0.03700 | 0.06038 | 142.21573 | 0.028234 | 7 | 40.936 |
| -0.14129 | 0.01495 | 0.14207 | 173.96126 | 0.066429 | 8 | 46.784 |
| -0.02833 | -0.08506 | 0.08965 | 251.57942 | 0.041918 | 9 | 52.632 |
| 0.03635 | -0.10027 | 0.10665 | 289.92651 | 0.049867 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.70629 | | | | | 0 | |
| -0.92161 | 1.21403 | 1.52421 | 127.20319 | 1.000000 | 1 | 5.917 |
| 0.37062 | -0.67346 | 0.67715 | 275.38657 | 0.444265 | 2 | 11.834 |
| 0.02969 | 0.25091 | 0.25266 | 83.25146 | 0.165764 | 3 | 17.751 |
| -0.09046 | 0.00518 | 0.09052 | 177.98602 | 0.059384 | 4 | 23.669 |
| -0.01603 | -0.04054 | 0.04359 | 248.43062 | 0.028599 | 5 | 29.586 |
| -0.04784 | -0.01110 | 0.04911 | 193.06461 | 0.032221 | 6 | 35.503 |
| -0.03401 | 0.00484 | 0.03435 | 171.90584 | 0.022541 | 7 | 41.420 |
| -0.10626 | -0.03741 | 0.11266 | 199.39348 | 0.073911 | 8 | 47.337 |
| -0.10683 | -0.02928 | 0.11077 | 195.32697 | 0.072674 | 9 | 53.254 |
| -0.10992 | -0.07612 | 0.13370 | 214.70348 | 0.087717 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.87297 | | | | | 0 | |
| 0.25472 | 0.79931 | 0.83892 | 72.32448 | 1.000000 | 1 | 5.917 |
| -0.28916 | -0.04126 | 0.29209 | 188.11983 | 0.348175 | 2 | 11.834 |
| -0.21696 | 0.12806 | 0.25193 | 149.44971 | 0.300308 | 3 | 17.751 |
| -0.07877 | -0.24873 | 0.26090 | 252.42731 | 0.311001 | 4 | 23.669 |
| -0.07833 | 0.02445 | 0.08206 | 162.86742 | 0.097817 | 5 | 29.586 |
| -0.15900 | -0.15627 | 0.22294 | 224.50409 | 0.265751 | 6 | 35.503 |
| -0.11341 | -0.09125 | 0.14556 | 218.31973 | 0.173504 | 7 | 41.420 |
| -0.12815 | -0.23623 | 0.26875 | 241.52174 | 0.320351 | 8 | 47.337 |
| -0.18224 | -0.09262 | 0.20442 | 206.94014 | 0.243675 | 9 | 53.254 |
| -0.02881 | -0.12291 | 0.12624 | 256.80933 | 0.150485 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.70911 | | | | | 0 | |
| -4.61901 | 5.97025 | 7.54846 | 127.72813 | 1.000000 | 1 | 5.917 |
| 0.36118 | -3.25798 | 3.27793 | 276.32593 | 0.434252 | 2 | 11.834 |
| 0.11170 | 1.20242 | 1.20759 | 84.69264 | 0.159979 | 3 | 17.751 |
| -0.42029 | 0.00248 | 0.42030 | 179.66165 | 0.055680 | 4 | 23.669 |
| -0.09637 | -0.17792 | 0.20234 | 241.55858 | 0.026805 | 5 | 29.586 |
| -0.22085 | -0.05408 | 0.22737 | 193.75455 | 0.030122 | 6 | 35.503 |
| -0.16364 | 0.02853 | 0.16578 | 170.79225 | 0.021962 | 7 | 41.420 |
| -0.49187 | -0.17032 | 0.52034 | 199.10712 | 0.068933 | 8 | 47.337 |
| -0.49714 | -0.12973 | 0.51379 | 194.62534 | 0.068065 | 9 | 53.254 |
| -0.50909 | -0.35159 | 0.61866 | 214.82213 | 0.081959 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 8.75083 | | | | | 0 | |
| 1.14094 | 3.88463 | 4.04871 | 73.63211 | 1.000000 | 1 | 5.917 |
| -1.34664 | -0.16632 | 1.35688 | 187.04074 | 0.335138 | 2 | 11.834 |
| -1.05083 | 0.81011 | 1.21511 | 149.86086 | 0.300122 | 3 | 17.751 |
| -0.38497 | -1.16288 | 1.22494 | 251.68288 | 0.302551 | 4 | 23.669 |
| -0.37548 | 0.13556 | 0.39920 | 160.14848 | 0.098600 | 5 | 29.586 |
| -0.72866 | -0.73761 | 1.03683 | 225.34978 | 0.256090 | 6 | 35.503 |
| -0.52846 | -0.43256 | 0.68292 | 219.30154 | 0.168675 | 7 | 41.420 |
| -0.80032 | -1.09440 | 1.24823 | 241.25345 | 0.308304 | 8 | 47.337 |
| -0.83177 | -0.43467 | 0.94470 | 207.39413 | 0.233335 | 9 | 53.254 |
| -0.14091 | -0.56742 | 0.58466 | 256.05298 | 0.144405 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.50281 | | | | | 0 | |
| -12.16920 | 15.23553 | 19.49898 | 128.61574 | 1.000000 | 1 | 5.917 |
| 0.98271 | -8.07685 | 8.13641 | 276.93701 | 0.417274 | 2 | 11.834 |
| 0.13416 | 2.93006 | 2.93313 | 87.37837 | 0.150425 | 3 | 17.751 |
| -0.96451 | -0.05155 | 0.96588 | 183.05957 | 0.049535 | 4 | 23.669 |
| -0.32314 | -0.35975 | 0.48357 | 228.06882 | 0.024800 | 5 | 29.586 |
| -0.50020 | -0.13581 | 0.51826 | 195.16856 | 0.026579 | 6 | 35.503 |
| -0.40103 | 0.07973 | 0.40947 | 168.77170 | 0.020999 | 7 | 41.420 |
| -1.11877 | -0.37668 | 1.17985 | 198.51567 | 0.060508 | 8 | 47.337 |
| -1.14453 | -0.26834 | 1.17557 | 193.19508 | 0.060289 | 9 | 53.254 |
| -1.16057 | -0.79719 | 1.40799 | 214.48518 | 0.072208 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.30933 | | | | | 0 | |
| 2.42031 | 9.71036 | 10.00745 | 76.00415 | 1.000000 | 1 | 5.917 |
| -3.10505 | -0.26364 | 3.11623 | 184.85323 | 0.311391 | 2 | 11.834 |
| -2.61084 | 1.47062 | 2.99853 | 150.60861 | 0.299430 | 3 | 17.751 |
| -0.97189 | -2.70238 | 2.87184 | 250.21925 | 0.286970 | 4 | 23.669 |
| -0.91537 | 0.41346 | 1.00441 | 155.69215 | 0.100366 | 5 | 29.586 |
| -1.62526 | -1.74644 | 2.38569 | 227.09829 | 0.238391 | 6 | 35.503 |
| -1.21997 | -1.03278 | 1.59842 | 220.24905 | 0.159723 | 7 | 41.420 |
| -1.40067 | -2.49685 | 2.86289 | 240.70857 | 0.286076 | 8 | 47.337 |
| -1.88790 | -1.01783 | 2.14479 | 208.33043 | 0.214320 | 9 | 53.254 |
| -0.35628 | -1.28516 | 1.33364 | 254.50511 | 0.133284 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 50
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 34.72113 | | | | | 0 | |
| -34.01956 | 38.52362 | 51.39189 | 131.44389 | 1.000000 | 1 | 5.917 |
| 2.92443 | -16.55487 | 16.78391 | 278.95654 | 0.365503 | 2 | 11.834 |
| -3.84312 | 6.30981 | 6.36589 | 97.61082 | 0.123849 | 3 | 17.751 |
| -1.25573 | -0.55088 | 1.65038 | 199.49884 | 0.032114 | 4 | 23.669 |
| -1.47171 | -0.02280 | 1.47188 | 180.88742 | 0.028640 | 5 | 29.586 |
| -0.72447 | -0.24943 | 0.76621 | 198.99854 | 0.014909 | 6 | 35.503 |
| -0.85721 | 0.32433 | 0.91691 | 159.27599 | 0.017834 | 7 | 41.420 |
| -1.63297 | -0.43905 | 1.69096 | 195.04909 | 0.032903 | 8 | 47.337 |
| -1.79805 | -0.14192 | 1.80361 | 184.50040 | 0.035095 | 9 | 53.254 |
| -1.72131 | -1.19099 | 2.07513 | 213.95303 | 0.040379 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 50
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.29373 | | | | | 0 | |
| 1.40957 | 22.47195 | 22.51994 | 86.25839 | 1.000000 | 1 | 5.917 |
| -4.98364 | 0.62958 | 5.02325 | 172.79996 | 0.223058 | 2 | 11.834 |
| -6.07232 | 3.04788 | 6.79421 | 153.34657 | 0.301702 | 3 | 17.751 |
| -2.41805 | -4.53819 | 5.14219 | 241.95024 | 0.228339 | 4 | 23.669 |
| -1.84736 | 1.70308 | 2.58702 | 138.02854 | 0.114877 | 5 | 29.586 |
| -2.12387 | -3.95470 | 3.98837 | 236.87341 | 0.177075 | 6 | 35.503 |
| -2.06031 | -1.98745 | 2.86266 | 223.98881 | 0.127117 | 7 | 41.420 |
| -2.42118 | -3.69743 | 4.41983 | 236.78204 | 0.196254 | 8 | 47.337 |
| -2.57398 | -1.74758 | 3.11118 | 214.17412 | 0.138152 | 9 | 53.254 |
| -0.82938 | -1.82991 | 2.00909 | 245.41821 | 0.089214 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 51.51508 | | | | | 0 | |
| -41.41690 | 40.61255 | 58.00626 | 135.56181 | 1.000000 | 1 | 5.917 |
| 3.44920 | -16.15112 | 16.62692 | 283.73999 | 0.286640 | 2 | 11.834 |
| -3.05816 | 4.65938 | 5.57225 | 123.26154 | 0.096063 | 3 | 17.751 |
| -0.07769 | -1.40320 | 1.40535 | 266.83081 | 0.024228 | 4 | 23.669 |
| -2.67461 | 1.37136 | 3.00569 | 152.85431 | 0.051817 | 5 | 29.586 |
| 0.15887 | -0.26839 | 0.26205 | 307.32031 | 0.004518 | 6 | 35.503 |
| -0.66530 | 0.52271 | 0.84608 | 141.84416 | 0.014586 | 7 | 41.420 |
| 0.26727 | 0.40946 | 0.48897 | 56.86560 | 0.008430 | 8 | 47.337 |
| -0.07827 | 0.76448 | 0.76848 | 95.84596 | 0.013248 | 9 | 53.254 |
| 0.21014 | 0.23541 | 0.31556 | 48.24617 | 0.005440 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.43437 | | | | | 0 | |
| -5.72928 | 20.63916 | 21.41960 | 105.51428 | 1.000000 | 1 | 5.917 |
| -0.41662 | 2.98371 | 3.01265 | 97.94890 | 0.140649 | 2 | 11.834 |
| -5.39115 | 1.97403 | 5.74119 | 159.38921 | 0.268035 | 3 | 17.751 |
| -2.40971 | -0.91471 | 2.57748 | 200.78644 | 0.120333 | 4 | 23.669 |
| -1.42876 | 2.80084 | 3.14421 | 117.02704 | 0.146791 | 5 | 29.586 |
| 1.16784 | -1.45219 | 1.86352 | 308.80591 | 0.087001 | 6 | 35.503 |
| -0.31942 | -1.09543 | 1.10271 | 253.16180 | 0.051491 | 7 | 41.420 |
| -0.64071 | 0.43619 | 0.77509 | 145.75322 | 0.036186 | 8 | 47.337 |
| 0.97591 | -0.49871 | 1.09595 | 332.93188 | 0.051166 | 9 | 53.254 |
| -0.81422 | 0.44025 | 0.93042 | 151.05843 | 0.043438 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 78.47054 | | | | | 0 | |
| -53.36279 | 48.50726 | 72.11476 | 137.72888 | 1.000000 | 1 | 5.917 |
| 6.62257 | -15.35841 | 16.72539 | 293.32568 | 0.231927 | 2 | 11.834 |
| -6.05230 | 3.20849 | 6.85016 | 152.07076 | 0.094996 | 3 | 17.751 |
| 1.45646 | -3.18694 | 3.50398 | 294.56079 | 0.048589 | 4 | 23.669 |
| -3.86543 | 1.25577 | 4.06430 | 162.00246 | 0.056359 | 5 | 29.586 |
| 0.61385 | -1.21740 | 1.36340 | 296.75854 | 0.018906 | 6 | 35.503 |
| -1.20813 | 0.43562 | 1.28427 | 160.17210 | 0.017809 | 7 | 41.420 |
| 0.82488 | 1.09553 | 1.37136 | 53.02206 | 0.019016 | 8 | 47.337 |
| 0.34773 | 1.49594 | 1.53583 | 76.91393 | 0.021297 | 9 | 53.254 |
| 0.91591 | 1.14545 | 1.46641 | 51.35396 | 0.020337 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.10279 | | | | | 0 | |
| -4.11107 | 27.35776 | 27.66450 | 98.54596 | 1.000000 | 1 | 5.917 |
| 2.01827 | 5.89875 | 6.23447 | 71.11147 | 0.225357 | 2 | 11.834 |
| -4.70284 | 0.44094 | 4.72346 | 174.64362 | 0.170739 | 3 | 17.751 |
| -2.03630 | 0.52082 | 2.10185 | 165.69315 | 0.075975 | 4 | 23.669 |
| -1.28111 | 2.92870 | 3.19864 | 113.62614 | 0.115549 | 5 | 29.586 |
| 3.66239 | -0.49659 | 3.69591 | 352.27832 | 0.133595 | 6 | 35.503 |
| 1.93957 | -0.91896 | 2.14626 | 334.64844 | 0.077580 | 7 | 41.420 |
| 0.39613 | 1.65335 | 1.70015 | 76.52646 | 0.061455 | 8 | 47.337 |
| 2.67397 | -0.51318 | 2.72276 | 349.13599 | 0.098419 | 9 | 53.254 |
| -1.69534 | 1.55139 | 2.29804 | 137.53877 | 0.083067 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 80.04221 | | | | | 0 | |
| -44.99490 | 40.37262 | 60.45236 | 138.09930 | 1.000000 | 1 | 5.917 |
| 7.70496 | -9.36731 | 12.12901 | 309.43848 | 0.200638 | 2 | 11.834 |
| -7.17383 | 0.71043 | 7.20892 | 174.34438 | 0.119250 | 3 | 17.751 |
| 2.18910 | -4.40325 | 4.91739 | 296.43433 | 0.081343 | 4 | 23.669 |
| -3.23651 | -1.04191 | 3.40008 | 197.84465 | 0.056244 | 5 | 29.586 |
| 0.37063 | -2.76531 | 2.79004 | 277.53379 | 0.046153 | 6 | 35.503 |
| -1.78859 | -0.14229 | 1.79424 | 184.54840 | 0.029680 | 7 | 41.420 |
| -0.40696 | 1.01214 | 1.09089 | 111.90401 | 0.018046 | 8 | 47.337 |
| -0.77010 | 1.24171 | 1.46113 | 121.80679 | 0.024170 | 9 | 53.254 |
| -0.14973 | 0.88037 | 0.89301 | 99.35207 | 0.014772 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.24680 | | | | | 0 | |
| 8.49491 | 30.94476 | 32.09958 | 74.64937 | 1.000000 | 1 | 5.917 |
| 0.79718 | 6.58126 | 6.62936 | 83.09340 | 0.206559 | 2 | 11.834 |
| -2.03766 | -1.45483 | 2.50372 | 215.52574 | 0.078025 | 3 | 17.751 |
| -0.42468 | -0.67662 | 0.79886 | 237.88524 | 0.024895 | 4 | 23.669 |
| -1.04591 | 0.56168 | 1.18719 | 151.76320 | 0.036996 | 5 | 29.586 |
| 3.33663 | -0.42103 | 3.36309 | 352.80811 | 0.104803 | 6 | 35.503 |
| 3.53011 | -1.24451 | 3.74306 | 340.58032 | 0.116644 | 7 | 41.420 |
| 0.30494 | -1.09894 | 1.14046 | 285.50854 | 0.035540 | 8 | 47.337 |
| 0.99794 | -1.84619 | 1.92247 | 301.09717 | 0.059909 | 9 | 53.254 |
| -2.60980 | 0.52225 | 2.66154 | 168.68393 | 0.082941 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 62.31049 | | | | | 0 | |
| -28.65584 | 26.16841 | 38.80647 | 137.59779 | 1.000000 | 1 | 5.917 |
| 6.08028 | -3.73903 | 7.13794 | 329.41064 | 0.183937 | 2 | 11.834 |
| -6.31928 | -0.66242 | 6.35390 | 185.98416 | 0.163733 | 3 | 17.751 |
| 1.85964 | -3.95720 | 4.37238 | 295.17041 | 0.112671 | 4 | 23.669 |
| -2.09225 | -2.09264 | 2.95916 | 225.00525 | 0.076254 | 5 | 29.586 |
| 0.23365 | -2.98755 | 2.99667 | 274.47168 | 0.077221 | 6 | 35.503 |
| -1.40625 | -0.42127 | 1.46799 | 196.67644 | 0.037829 | 7 | 41.420 |
| -0.93634 | 0.61017 | 1.11760 | 146.90959 | 0.028799 | 8 | 47.337 |
| -1.19199 | 0.65865 | 1.36089 | 151.15016 | 0.035069 | 9 | 53.254 |
| -0.74058 | 0.36148 | 0.82409 | 153.98242 | 0.021236 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
ODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.76645 | | | | | 0 | |
| 13.19118 | 26.14296 | 29.28242 | 63.22542 | 1.000000 | 1 | 5.917 |
| -0.64839 | 5.32029 | 5.35965 | 96.94935 | 0.183033 | 2 | 11.834 |
| -0.25015 | -1.75926 | 1.77696 | 261.90723 | 0.060683 | 3 | 17.751 |
| 0.49397 | -1.18518 | 1.28400 | 292.62573 | 0.043849 | 4 | 23.669 |
| -0.80273 | -1.10631 | 1.36685 | 234.03574 | 0.046678 | 5 | 29.586 |
| 2.02841 | -0.52740 | 2.09585 | 345.42554 | 0.071574 | 6 | 35.503 |
| 3.18604 | -1.16306 | 3.39169 | 339.94531 | 0.115827 | 7 | 41.420 |
| 0.00748 | -2.46719 | 2.46721 | 270.17383 | 0.084255 | 8 | 47.337 |
| -0.37730 | -1.88996 | 1.92725 | 258.71021 | 0.065816 | 9 | 53.254 |
| -2.30840 | -0.37349 | 2.33842 | 189.19067 | 0.079857 | 10 | 59.172 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 198 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 67.82172 | | | | | 0 | |
| -24.68956 | 24.31120 | 34.64480 | 135.44241 | 1.000000 | 1 | 5.917 |
| 5.36903 | -1.10060 | 5.48028 | 348.41528 | 0.158173 | 2 | 11.834 |
| -7.58234 | -1.38611 | 7.70799 | 190.35970 | 0.222454 | 3 | 17.751 |
| 1.81723 | -4.19356 | 4.57037 | 293.42896 | 0.131902 | 4 | 23.669 |
| -1.95291 | -2.58190 | 3.23736 | 232.89757 | 0.093431 | 5 | 29.586 |
| 0.72306 | -3.57914 | 3.65147 | 281.42114 | 0.105382 | 6 | 35.503 |
| -0.61337 | -0.54664 | 0.82161 | 221.70789 | 0.023712 | 7 | 41.420 |
| -0.74057 | 0.37436 | 0.82981 | 153.16324 | 0.023949 | 8 | 47.337 |
| -1.12410 | 0.23854 | 1.14913 | 168.01939 | 0.033164 | 9 | 53.254 |
| -0.75631 | 0.05675 | 0.75844 | 175.70891 | 0.021889 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 198 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.06554 | | | | | 0 | |
| 14.83141 | 29.62715 | 33.13213 | 63.40732 | 1.000000 | 1 | 5.917 |
| -1.95623 | 5.72030 | 6.04555 | 108.87971 | 0.182468 | 2 | 11.834 |
| 0.48840 | -1.21723 | 1.31156 | 291.86230 | 0.039586 | 3 | 17.751 |
| 0.78532 | -0.65343 | 1.02162 | 320.23755 | 0.030835 | 4 | 23.669 |
| -1.12018 | -2.56101 | 2.79529 | 246.37546 | 0.084368 | 5 | 29.586 |
| 1.62289 | -0.90445 | 1.88784 | 329.27783 | 0.056979 | 6 | 35.503 |
| 2.89265 | -1.21022 | 3.13561 | 337.29619 | 0.094640 | 7 | 41.420 |
| -0.13809 | -2.76811 | 2.78955 | 267.16235 | 0.084195 | 8 | 47.337 |
| -0.73063 | -1.96767 | 2.09893 | 249.62919 | 0.063350 | 9 | 53.254 |
| -1.93364 | -0.85108 | 2.11265 | 203.75644 | 0.063764 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 198 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 190.91661 | | | | | 0 | |
| -33.64131 | 40.88614 | 52.94727 | 129.44774 | 1.000000 | 1 | 5.917 |
| 5.74663 | 6.21996 | 8.46963 | 47.25511 | 0.159963 | 2 | 11.834 |
| -19.93155 | -3.91110 | 20.31165 | 191.10188 | 0.383620 | 3 | 17.751 |
| 2.60361 | -8.12387 | 8.53089 | 287.77002 | 0.161120 | 4 | 23.669 |
| -3.41140 | -4.84867 | 6.22965 | 231.10701 | 0.117658 | 5 | 29.586 |
| 3.77270 | -7.90421 | 8.75842 | 295.51514 | 0.165418 | 6 | 35.503 |
| 3.03794 | -1.04784 | 3.21350 | 340.97314 | 0.060692 | 7 | 41.420 |
| 1.01004 | -0.12393 | 1.01761 | 353.00464 | 0.019219 | 8 | 47.337 |
| -0.43890 | -1.00336 | 1.09515 | 246.37418 | 0.020684 | 9 | 53.254 |
| -0.19863 | -0.80746 | 0.83153 | 256.17969 | 0.015705 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XM-51A SHIP 1002C TEST 502 OSC CTR 198 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 66.09619 | | | | | 0 | |
| 22.61122 | 64.52805 | 68.37494 | 70.68901 | 1.000000 | 1 | 5.917 |
| -7.57755 | 12.38772 | 14.52153 | 121.45415 | 0.212381 | 2 | 11.834 |
| 1.66563 | 1.43187 | 2.19649 | 40.68411 | 0.032124 | 3 | 17.751 |
| 1.44576 | 2.75425 | 3.11064 | 62.30405 | 0.045494 | 4 | 23.669 |
| -3.43611 | -8.80183 | 9.44876 | 248.67497 | 0.138190 | 5 | 29.586 |
| 1.88319 | -3.33688 | 3.83160 | 299.43848 | 0.056039 | 6 | 35.503 |
| 2.80312 | -1.85712 | 3.36250 | 326.47485 | 0.049177 | 7 | 41.420 |
| -0.59828 | -3.38792 | 3.44034 | 259.98511 | 0.050316 | 8 | 47.337 |
| -0.98200 | -2.81069 | 2.97729 | 250.74135 | 0.043544 | 9 | 53.254 |
| -1.12631 | -2.45273 | 2.69897 | 245.33501 | 0.039473 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 100.16368 | | | | | 0 | |
| -6.39938 | 11.25508 | 12.94716 | 119.62163 | 0.703833 | 1 | 5.917 |
| 0.35353 | 11.60438 | 11.60976 | 88.25494 | 0.631130 | 2 | 11.834 |
| -18.14438 | -3.02749 | 18.39520 | 189.47284 | 1.000000 | 3 | 17.751 |
| 6.61549 | -5.82871 | 5.86111 | 276.02783 | 0.318622 | 4 | 23.669 |
| -3.68842 | -3.20355 | 4.88540 | 220.97572 | 0.265560 | 5 | 29.586 |
| 2.65139 | -5.52529 | 6.21765 | 297.29639 | 0.338004 | 6 | 35.503 |
| 4.28220 | -0.84138 | 4.36407 | 348.88379 | 0.237240 | 7 | 41.420 |
| 2.34037 | -0.39245 | 2.37304 | 350.48071 | 0.129003 | 8 | 47.337 |
| 0.80315 | -0.90386 | 1.20914 | 311.62354 | 0.065731 | 9 | 53.254 |
| 0.47605 | -0.89725 | 1.01572 | 297.94897 | 0.055217 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 72.41861 | | | | | 0 | |
| 10.21353 | 32.03632 | 33.62787 | 72.31863 | 1.000000 | 1 | 5.917 |
| -5.08035 | 8.62367 | 10.00888 | 120.50311 | 0.297636 | 2 | 11.834 |
| 0.68951 | 1.85817 | 1.98197 | 69.64169 | 0.058938 | 3 | 17.751 |
| 3.72077 | 3.65643 | 3.72679 | 78.84857 | 0.110824 | 4 | 23.669 |
| -2.34986 | -6.15020 | 6.58383 | 249.08910 | 0.195785 | 5 | 29.586 |
| -0.05465 | -2.36386 | 2.36449 | 268.67529 | 0.070313 | 6 | 35.503 |
| -0.05634 | -0.62678 | 0.62931 | 264.86328 | 0.018714 | 7 | 41.420 |
| -0.93336 | -0.78198 | 1.22151 | 220.17232 | 0.036324 | 8 | 47.337 |
| -1.17639 | -1.67454 | 2.04645 | 234.91124 | 0.060856 | 9 | 53.254 |
| -0.00077 | -2.13649 | 2.13649 | 269.97925 | 0.063533 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 90.02259 | | | | | 0 | |
| 15.49877 | -18.12086 | 23.84486 | 310.54028 | 0.941362 | 1 | 5.917 |
| -0.84245 | 21.32890 | 21.34552 | 92.26196 | 0.824708 | 2 | 11.834 |
| -25.73218 | -2.76250 | 25.88002 | 186.14756 | 1.000000 | 3 | 17.751 |
| -0.86936 | -8.13004 | 8.17639 | 263.89624 | 0.315934 | 4 | 23.669 |
| -5.90821 | -4.37234 | 7.35012 | 216.50314 | 0.284007 | 5 | 29.586 |
| 0.95324 | -5.46017 | 5.54276 | 279.90283 | 0.214171 | 6 | 35.503 |
| 4.17415 | -1.11386 | 4.32021 | 345.05884 | 0.166932 | 7 | 41.420 |
| 2.92434 | 0.03654 | 2.92457 | 0.71578 | 0.113005 | 8 | 47.337 |
| 1.03185 | 0.15440 | 1.04334 | 8.51042 | 0.040314 | 9 | 53.254 |
| 0.22268 | -0.77229 | 0.80375 | 286.08423 | 0.031057 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 133.38715 | | | | | 0 | |
| 11.52376 | 4.58299 | 12.40166 | 21.68765 | 1.000000 | 1 | 5.917 |
| -2.67217 | 10.11223 | 10.45933 | 104.80220 | 0.843381 | 2 | 11.834 |
| -2.37068 | -1.22489 | 2.66842 | 207.32466 | 0.215166 | 3 | 17.751 |
| 1.25128 | 2.15666 | 2.49337 | 59.67796 | 0.201051 | 4 | 23.669 |
| -0.58331 | -2.95141 | 3.00850 | 258.82067 | 0.242588 | 5 | 29.586 |
| -1.30112 | -0.60195 | 1.43361 | 204.82730 | 0.115598 | 6 | 35.503 |
| -0.73714 | 0.49364 | 0.88716 | 146.19182 | 0.071535 | 7 | 41.420 |
| -1.74112 | -0.45162 | 1.79876 | 194.54117 | 0.145040 | 8 | 47.337 |
| -3.81685 | -2.49095 | 3.76025 | 221.48651 | 0.303205 | 9 | 53.254 |
| -1.33733 | -2.36726 | 2.71890 | 240.53661 | 0.219237 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 64.96563 | | | | | 0 | |
| 24.43706 | -20.81222 | 32.09882 | 319.57935 | 1.000000 | 1 | 5.917 |
| 1.15222 | 18.84410 | 18.92537 | 86.68756 | 0.589597 | 2 | 11.834 |
| -20.52028 | 0.00973 | 20.52026 | 179.97282 | 0.639284 | 3 | 17.751 |
| -1.92577 | -7.25516 | 7.50639 | 255.13448 | 0.233853 | 4 | 23.669 |
| -2.63145 | -4.03965 | 4.82113 | 236.91956 | 0.150196 | 5 | 29.586 |
| 0.20209 | -2.13248 | 2.14204 | 275.41357 | 0.066733 | 6 | 35.503 |
| 1.24277 | 0.21843 | 1.26046 | 9.61843 | 0.039268 | 7 | 41.420 |
| 1.00707 | 0.59185 | 1.23765 | 28.35771 | 0.038557 | 8 | 47.337 |
| 0.68094 | -0.02610 | 0.68943 | 357.83857 | 0.021478 | 9 | 53.254 |
| 0.32732 | -0.69934 | 0.73612 | 296.40161 | 0.022933 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.75517 | | | | | 0 | |
| 11.66893 | 2.91251 | 12.02691 | 14.05441 | 0.979039 | 1 | 5.917 |
| -6.50955 | 10.40387 | 12.32343 | 121.88570 | 1.000000 | 2 | 11.834 |
| -0.88665 | -2.71821 | 8.45298 | 198.70068 | 0.685921 | 3 | 17.751 |
| 3.36146 | -1.82426 | 3.82457 | 331.51123 | 0.310350 | 4 | 23.669 |
| 1.92139 | -0.47222 | 1.97857 | 346.19214 | 0.160554 | 5 | 29.586 |
| -0.28643 | 2.01368 | 2.03387 | 98.09589 | 0.165041 | 6 | 35.503 |
| -0.86982 | 2.39356 | 2.58887 | 110.26402 | 0.203585 | 7 | 41.420 |
| -0.84618 | -0.11826 | 0.85334 | 187.42372 | 0.069245 | 8 | 47.337 |
| -0.28917 | -0.39947 | 0.48830 | 233.68687 | 0.039624 | 9 | 53.254 |
| 0.22882 | -0.38405 | 0.38054 | 306.96387 | 0.030879 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 65.71657 | | | | | 0 | |
| 30.22191 | -30.09441 | 42.65016 | 315.12109 | 1.000000 | 1 | 5.917 |
| 0.85408 | 20.37248 | 20.39037 | 87.59935 | 0.478004 | 2 | 11.834 |
| -22.28081 | -0.89110 | 22.22506 | 182.29778 | 0.521120 | 3 | 17.751 |
| -1.90507 | -8.97108 | 9.09645 | 260.47807 | 0.213281 | 4 | 23.669 |
| -2.67793 | -4.97044 | 5.44593 | 241.68539 | 0.132378 | 5 | 29.586 |
| -0.32011 | -2.09900 | 2.12327 | 261.32086 | 0.049783 | 6 | 35.503 |
| 0.03470 | 0.10415 | 0.44318 | 9.31853 | 0.015000 | 7 | 41.420 |
| 1.44065 | 0.91494 | 1.70663 | 32.41907 | 0.040015 | 8 | 47.337 |
| 0.63649 | 0.34299 | 0.72302 | 28.31935 | 0.016952 | 9 | 53.254 |
| 0.08448 | -0.69272 | 0.69809 | 277.11597 | 0.016368 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 64.96788 | | | | | 0 | |
| 33.83928 | 20.12695 | 39.37245 | 30.74336 | 1.000000 | 1 | 5.917 |
| -6.93153 | 18.33981 | 19.60597 | 110.70413 | 0.497942 | 2 | 11.834 |
| -16.37619 | -1.99027 | 16.40541 | 186.95093 | 0.416758 | 3 | 17.751 |
| 2.37126 | -7.40401 | 7.87114 | 289.83862 | 0.199915 | 4 | 23.669 |
| 5.96197 | -2.10596 | 5.94731 | 339.26147 | 0.151053 | 5 | 29.586 |
| -0.51454 | 0.96114 | 1.09020 | 118.16194 | 0.027689 | 6 | 35.503 |
| 0.12595 | 1.70221 | 1.70606 | 85.76831 | 0.043334 | 7 | 41.420 |
| -0.33983 | 1.02235 | 1.07735 | 108.38673 | 0.027363 | 8 | 47.337 |
| -0.17686 | -0.19995 | 0.26695 | 228.50719 | 0.006780 | 9 | 53.254 |
| 1.08404 | -0.65960 | 1.26894 | 328.68091 | 0.032229 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 10020 TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.27258 | | | | | 0 | |
| 15.46444 | -18.41714 | 24.04869 | 310.01929 | 1.000000 | 1 | 5.917 |
| -0.47743 | 10.04285 | 10.05420 | 92.72193 | 0.418077 | 2 | 11.834 |
| -11.13255 | -1.16333 | 11.19317 | 185.96562 | 0.465438 | 3 | 17.751 |
| -0.35183 | -4.83359 | 4.84838 | 265.83657 | 0.201524 | 4 | 23.669 |
| -1.67223 | -2.64382 | 3.12828 | 237.58834 | 0.130081 | 5 | 29.586 |
| -0.41329 | -1.27283 | 1.33825 | 252.31111 | 0.055648 | 6 | 35.503 |
| 0.36589 | -0.19453 | 0.36250 | 327.54561 | 0.015074 | 7 | 41.420 |
| 1.03368 | 0.49981 | 1.14817 | 25.80516 | 0.047744 | 8 | 47.337 |
| 0.28641 | 0.41542 | 0.50458 | 55.41553 | 0.020982 | 9 | 53.254 |
| -0.11872 | -0.30862 | 0.33086 | 248.97179 | 0.013758 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 10020 TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 52.46475 | | | | | 0 | |
| 25.40349 | 15.83143 | 29.93277 | 31.93112 | 1.000000 | 1 | 5.917 |
| -2.46062 | 11.65067 | 11.90767 | 101..2564 | 0.397814 | 2 | 11.834 |
| -10.50045 | -0.45702 | 10.51039 | 182.49214 | 0.351133 | 3 | 17.751 |
| 0.51848 | -5.49964 | 5.52402 | 275.33550 | 0.184548 | 4 | 23.669 |
| 3.94026 | -1.83606 | 4.34704 | 335.01562 | 0.145227 | 5 | 29.586 |
| -0.52058 | -0.36956 | 0.63842 | 215.37135 | 0.021328 | 6 | 35.503 |
| 0.55020 | 0.19837 | 0.58425 | 19.63479 | 0.019519 | 7 | 41.420 |
| -0.03988 | 0.96585 | 0.96667 | 92.36343 | 0.032295 | 8 | 47.337 |
| -0.42870 | -0.30039 | 0.52347 | 215.01871 | 0.017488 | 9 | 53.254 |
| 0.60286 | -0.72740 | 0.94475 | 309.65161 | 0.031562 | 10 | 59.172 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 10020 TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.37178 | | | | | 0 | |
| 1.23272 | -1.50079 | 1.94215 | 309.39917 | 1.000000 | 1 | 5.917 |
| -0.04796 | 0.79523 | 0.79668 | 93.46125 | 0.410204 | 2 | 11.834 |
| -0.88349 | -0.10033 | 0.88916 | 186.47864 | 0.457823 | 3 | 17.751 |
| -0.02339 | -0.38774 | 0.38844 | 266.54810 | 0.200007 | 4 | 23.669 |
| -0.13607 | -0.21174 | 0.25169 | 237.27316 | 0.129595 | 5 | 29.586 |
| -0.03576 | -0.10320 | 0.10922 | 250.89079 | 0.056237 | 6 | 35.503 |
| 0.02375 | -0.01809 | 0.02986 | 322.73044 | 0.015372 | 7 | 41.420 |
| 0.08544 | 0.04025 | 0.09445 | 25.22415 | 0.048631 | 8 | 47.337 |
| 0.02233 | 0.03573 | 0.04213 | 57.99884 | 0.021693 | 9 | 53.254 |
| -0.01127 | -0.02609 | 0.02840 | 246.93170 | 0.013695 | 10 | 59.172 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 10020 TEST 502 OSC CTR 188 TEST COND 37 COMP RUN 45.1

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.18199 | | | | | 0 | |
| 2.11619 | 1.32581 | 2.49720 | 32.06755 | 1.000000 | 1 | 5.917 |
| -0.18457 | 0.95422 | 0.97191 | 100.94724 | 0.389199 | 2 | 11.834 |
| -0.86161 | -0.03007 | 0.86213 | 181.99864 | 0.345240 | 3 | 17.751 |
| 0.03201 | -0.45820 | 0.45932 | 275.99659 | 0.183932 | 4 | 23.669 |
| 0.32670 | -0.15475 | 0.36150 | 334.65405 | 0.144763 | 5 | 29.586 |
| -0.04418 | -0.03892 | 0.05888 | 221.37421 | 0.023578 | 6 | 35.503 |
| 0.04936 | 0.00824 | 0.05004 | 9.47256 | 0.020040 | 7 | 41.420 |
| -0.00148 | 0.08203 | 0.08205 | 91.03357 | 0.032855 | 8 | 47.337 |
| -0.03752 | -0.02581 | 0.04554 | 214.53117 | 0.018236 | 9 | 53.254 |
| 0.04892 | -0.05607 | 0.07903 | 308.24731 | 0.031647 | 10 | 59.172 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.28804 | | | | | 0 | |
| -1.16903 | 1.28998 | 1.74009 | 132.10417 | 1.000000 | 1 | 5.882 |
| 0.28534 | -1.20223 | 1.23563 | 283.13156 | 0.709769 | 2 | 11.765 |
| -0.01981 | 0.54294 | 0.54291 | 92.09894 | 0.311856 | 3 | 17.647 |
| -0.16674 | -0.29239 | 0.33678 | 240.31859 | 0.193452 | 4 | 23.529 |
| -0.07844 | -0.02615 | 0.08079 | 198.68738 | 0.046405 | 5 | 29.412 |
| 0.00841 | 0.07507 | 0.10154 | 47.65564 | 0.058340 | 6 | 35.294 |
| -0.16760 | 0.20968 | 0.26843 | 128.63710 | 0.154192 | 7 | 41.176 |
| -0.20746 | 0.14255 | 0.25171 | 145.50568 | 0.144589 | 8 | 47.059 |
| -0.21680 | 0.03523 | 0.21984 | 170.77866 | 0.126167 | 9 | 52.941 |
| -0.11937 | -0.02033 | 0.12109 | 189.46577 | 0.069555 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.03099 | | | | | 0 | |
| -1.85736 | -1.27522 | 1.65656 | 230.33575 | 1.000000 | 1 | 5.882 |
| -0.86794 | -0.29776 | 0.91760 | 198.93550 | 0.553917 | 2 | 11.765 |
| -0.47014 | 0.25192 | 0.53319 | 151.85414 | 0.321869 | 3 | 17.647 |
| 0.09794 | 0.03068 | 0.10267 | 22.85644 | 0.061998 | 4 | 23.529 |
| 0.01748 | 0.44383 | 0.44416 | 87.84222 | 0.268194 | 5 | 29.412 |
| 0.10917 | 0.04280 | 0.11934 | 18.98679 | 0.120036 | 6 | 35.294 |
| 0.03415 | 0.06817 | 0.07454 | 2.60784 | 0.045018 | 7 | 41.176 |
| 0.24671 | -0.28483 | 0.32866 | 320.29987 | 0.198570 | 8 | 47.059 |
| 0.09424 | -0.19305 | 0.21642 | 295.78838 | 0.130747 | 9 | 52.941 |
| 0.23712 | 0.00000 | 0.25330 | 20.50987 | 0.152988 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.58061 | | | | | 0 | |
| -5.84278 | 6.29577 | 8.59990 | 133.84436 | 1.000000 | 1 | 5.882 |
| 1.66459 | -5.89807 | 6.83140 | 286.08347 | 0.794611 | 2 | 11.765 |
| -0.14186 | 2.68856 | 2.68943 | 93.12241 | 0.312939 | 3 | 17.647 |
| -0.74848 | -1.39511 | 1.58859 | 248.77562 | 0.186793 | 4 | 23.529 |
| -0.38770 | -0.16757 | 0.42236 | 203.37550 | 0.049142 | 5 | 29.412 |
| 0.35451 | 0.35443 | 0.50130 | 44.99339 | 0.058344 | 6 | 35.294 |
| -0.81422 | 0.98488 | 1.27725 | 129.68418 | 0.148213 | 7 | 41.176 |
| -0.98667 | 0.67327 | 1.17082 | 145.14330 | 0.137621 | 8 | 47.059 |
| -1.03886 | 0.18479 | 1.05185 | 170.97995 | 0.122388 | 9 | 52.941 |
| -0.56827 | -0.18263 | 0.57744 | 198.23764 | 0.067441 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.95679 | | | | | 0 | |
| -5.84852 | -5.99302 | 7.83485 | 229.08921 | 1.000000 | 1 | 5.882 |
| -0.19827 | -1.42817 | 4.42629 | 198.71420 | 0.564901 | 2 | 11.765 |
| -2.26481 | 1.18000 | 2.55752 | 152.34931 | 0.326379 | 3 | 17.647 |
| 0.47371 | 0.12083 | 0.48888 | 14.30988 | 0.062388 | 4 | 23.529 |
| 0.11954 | 2.17394 | 2.17811 | 86.99986 | 0.277960 | 5 | 29.412 |
| 0.91781 | 0.29959 | 0.96870 | 18.16081 | 0.122600 | 6 | 35.294 |
| 0.18719 | 0.02619 | 0.18876 | 7.37640 | 0.024088 | 7 | 41.176 |
| 1.16415 | -0.98819 | 1.52191 | 319.98889 | 0.194219 | 8 | 47.059 |
| 0.45841 | -0.95160 | 1.05372 | 299.38566 | 0.134471 | 9 | 52.941 |
| 1.12600 | 0.39171 | 1.19351 | 19.36304 | 0.152318 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XX-91A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.79926 | | | | | 0 | |
| -19.32227 | 15.97728 | 21.84996 | 134.52734 | 1.000000 | 1 | 5.882 |
| 4.30752 | -14.66194 | 15.19889 | 285.28889 | 0.695603 | 2 | 11.765 |
| -0.59790 | 6.77944 | 6.36391 | 95.02585 | 0.291255 | 3 | 17.647 |
| -1.81791 | -3.[illegible]781 | 3.82694 | 241.64551 | 0.175146 | 4 | 23.529 |
| -1.66128 | -0.[illegible]985 | 1.20130 | 299.91289 | 0.054979 | 5 | 29.412 |
| 0.90429 | 0.89976 | 1.29384 | 44.44953 | 0.059215 | 6 | 35.294 |
| -2.83884 | 2.38044 | 3.87358 | 131.43885 | 0.148868 | 7 | 41.176 |
| -2.23139 | 1.59484 | 2.74343 | 144.42471 | 0.125558 | 8 | 47.059 |
| -2.52952 | 0.38338 | 2.55445 | 171.36813 | 0.116909 | 9 | 52.941 |
| -1.36776 | -0.27361 | 1.39486 | 191.31233 | 0.063836 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XX-91A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.52604 | | | | | 0 | |
| -12.21882 | -14.07850 | 18.63487 | 229.03879 | 1.000000 | 1 | 5.882 |
| -10.84617 | -9.43804 | 10.91788 | 198.31286 | 0.585838 | 2 | 11.765 |
| -5.57204 | 2.81723 | 6.24375 | 153.17800 | 0.335057 | 3 | 17.647 |
| 1.17488 | -0.01852 | 1.17423 | 359.09588 | 0.063012 | 4 | 23.529 |
| 0.42307 | 0.00466 | 0.42124 | 0.63000 | 0.022609 | 5 | 29.412 |
| 2.25206 | 0.72189 | 2.36958 | 17.76878 | 0.126999 | 6 | 35.294 |
| 0.56293 | 0.09658 | 0.56527 | 9.74430 | 0.030334 | 7 | 41.176 |
| 2.79406 | -2.36290 | 3.66245 | 319.14063 | 0.195644 | 8 | 47.059 |
| 1.09225 | -2.68283 | 2.63878 | 291.65215 | 0.141608 | 9 | 52.941 |
| 2.69786 | 0.82999 | 2.82818 | 16.97898 | 0.151339 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 90
MODEL XX-91A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.27339 | | | | | 0 | |
| -42.30812 | 30.13910 | 98.70267 | 139.94998 | 1.000000 | 1 | 5.882 |
| 12.64887 | -33.13607 | 37.36827 | 289.08818 | 0.478817 | 2 | 11.765 |
| -2.00828 | 13.77498 | 14.07612 | 101.72488 | 0.258865 | 3 | 17.647 |
| -3.07848 | -4.92489 | 7.57982 | 240.00883 | 0.139998 | 4 | 23.529 |
| -2.03137 | -2.82829 | 4.86777 | 229.09813 | 0.073826 | 5 | 29.412 |
| 3.09148 | 1.73865 | 3.54488 | 29.35313 | 0.063875 | 6 | 35.294 |
| -4.01158 | 4.08225 | 6.31888 | 139.66798 | 0.113888 | 7 | 41.176 |
| -3.96660 | 3.87993 | 6.73134 | 139.30570 | 0.089089 | 8 | 47.059 |
| -3.40483 | 3.76859 | 5.45552 | 132.14494 | 0.097840 | 9 | 52.941 |
| -2.81489 | -0.79525 | 2.92474 | 195.77762 | 0.052988 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 90
MODEL XX-91A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.96893 | | | | | 0 | |
| -28.92842 | -20.98878 | 36.69439 | 225.96917 | 1.000000 | 1 | 5.882 |
| -23.30748 | -7.22484 | 24.48842 | 197.81388 | 0.668849 | 2 | 11.765 |
| -12.44716 | 9.31487 | 15.53488 | 130.87778 | 0.389293 | 3 | 17.647 |
| 2.79699 | -2.87322 | 3.98842 | 313.79888 | 0.108679 | 4 | 23.529 |
| 2.98822 | 0.98885 | 3.27872 | 73.61472 | 0.252982 | 5 | 29.412 |
| 5.88829 | 1.99485 | 5.29882 | 17.88498 | 0.144883 | 6 | 35.294 |
| 2.28899 | 3.89421 | 2.28618 | 0.88498 | 0.061825 | 7 | 41.176 |
| 5.86846 | -6.94648 | 7.28883 | 310.77898 | 0.197836 | 8 | 47.059 |
| 2.32842 | -5.82648 | 6.27879 | 298.78758 | 0.171078 | 9 | 52.941 |
| 5.94881 | 0.49572 | 5.41884 | 5.28229 | 0.147781 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 29.79654 | | | | | 0 | |
| -30.72446 | 32.48884 | 60.23224 | 147.36765 | 1.000000 | 1 | 5.882 |
| 17.39863 | -33.24161 | 37.49222 | 297.56761 | 0.622441 | 2 | 11.765 |
| -5.83536 | 10.27549 | 11.81682 | 119.59190 | 0.196188 | 3 | 17.647 |
| -0.68984 | -4.51286 | 4.56524 | 261.31128 | 0.075794 | 4 | 23.529 |
| -3.86424 | -5.42553 | 6.62751 | 234.94868 | 0.110032 | 5 | 29.412 |
| 4.39658 | 0.93668 | 4.49523 | 12.02591 | 0.074632 | 6 | 35.294 |
| -4.44429 | 1.29729 | 4.62976 | 163.72748 | 0.076845 | 7 | 41.176 |
| -0.34679 | 1.49321 | 1.53295 | 103.07498 | 0.025451 | 8 | 47.059 |
| -3.91879 | 0.27869 | 3.92812 | 176.04854 | 0.065214 | 9 | 52.941 |
| -1.78346 | -1.00954 | 2.04936 | 209.51230 | 0.034024 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 11.00097 | | | | | 0 | |
| -17.30896 | -10.24969 | 20.11174 | 210.63960 | 0.991726 | 1 | 5.882 |
| -19.69278 | -4.84304 | 20.27954 | 193.81653 | 1.000000 | 2 | 11.765 |
| -10.13496 | 2.48432 | 10.43580 | 166.22782 | 0.514558 | 3 | 17.647 |
| 2.42317 | -7.88075 | 8.16844 | 287.25650 | 0.402792 | 4 | 23.529 |
| 4.35613 | 2.71150 | 5.13189 | 31.99841 | 0.253018 | 5 | 29.412 |
| 4.22917 | 1.84546 | 4.35647 | 13.88532 | 0.214821 | 6 | 35.294 |
| 3.65539 | -0.85778 | 3.65585 | 350.89424 | 0.180273 | 7 | 41.176 |
| 2.44162 | -3.44081 | 4.24130 | 305.14697 | 0.209142 | 8 | 47.059 |
| 1.63852 | -5.71811 | 5.94683 | 285.91528 | 0.293203 | 9 | 52.941 |
| 3.14014 | -2.10868 | 3.82764 | 325.12329 | 0.188744 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 86
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 46.24759 | | | | | 0 | |
| -63.84880 | 35.84464 | 72.15079 | 150.94075 | 1.000000 | 1 | 5.882 |
| 29.91948 | -32.79585 | 36.37125 | 301.27344 | 0.531820 | 2 | 11.765 |
| -10.64446 | 5.88566 | 12.16329 | 151.06841 | 0.168581 | 3 | 17.647 |
| 0.11156 | -2.82570 | 2.82790 | 272.26674 | 0.039194 | 4 | 23.529 |
| -7.13171 | -10.38219 | 12.59568 | 235.51418 | 0.174574 | 5 | 29.412 |
| 6.96723 | -2.86830 | 7.26947 | 343.52637 | 0.100698 | 6 | 35.294 |
| -4.38413 | -0.65883 | 4.43286 | 188.43372 | 0.061428 | 7 | 41.176 |
| 0.83842 | -0.74298 | 1.11428 | 318.18891 | 0.015444 | 8 | 47.059 |
| -2.47973 | -1.54436 | 2.92132 | 211.91441 | 0.040499 | 9 | 52.941 |
| -0.58959 | -1.21273 | 1.34671 | 244.22523 | 0.018665 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 86
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.98274 | | | | | 0 | |
| -18.16136 | 15.26215 | 18.33537 | 123.65523 | 0.857629 | 1 | 5.882 |
| -21.33782 | -1.33220 | 21.37915 | 183.57257 | 1.000000 | 2 | 11.765 |
| -8.00949 | 0.91765 | 8.14137 | 173.52817 | 0.380809 | 3 | 17.647 |
| 1.20971 | -11.62360 | 11.68630 | 275.94141 | 0.546625 | 4 | 23.529 |
| 4.51321 | -2.15245 | 5.00201 | 334.51221 | 0.233967 | 5 | 29.412 |
| 4.18426 | -0.48194 | 4.21182 | 353.44165 | 0.197006 | 6 | 35.294 |
| 3.82688 | 1.09835 | 3.21652 | 19.81900 | 0.150451 | 7 | 41.176 |
| -1.40869 | -4.35763 | 4.57985 | 252.10925 | 0.214183 | 8 | 47.059 |
| 0.66170 | -6.81782 | 6.84985 | 275.96346 | 0.320399 | 9 | 52.941 |
| 1.81013 | -4.24371 | 4.36227 | 283.38892 | 0.204043 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.69843 | | | | | 0 | |
| -49.91968 | 28.35324 | 57.40974 | 150.40442 | 1.000000 | 1 | 5.882 |
| 11.02798 | -18.79042 | 21.78751 | 300.40845 | 0.379509 | 2 | 11.765 |
| -12.76725 | -1.71158 | 12.88147 | 187.63556 | 0.224378 | 3 | 17.647 |
| -0.94429 | -0.99512 | 1.37182 | 226.50247 | 0.023895 | 4 | 23.529 |
| -9.55068 | 12.62273 | 15.82874 | 232.88791 | 0.275715 | 5 | 29.412 |
| 7.58955 | -6.04499 | 9.70274 | 321.46289 | 0.169009 | 6 | 35.294 |
| -2.66059 | -1.08521 | 2.87339 | 202.18965 | 0.050051 | 7 | 41.176 |
| -0.61500 | -2.92973 | 2.99359 | 258.14453 | 0.052144 | 8 | 47.059 |
| -0.22652 | -3.78135 | 3.79813 | 266.57178 | 0.065984 | 9 | 52.941 |
| 0.93853 | -0.87356 | 1.27632 | 316.80884 | 0.022232 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 32.34057 | | | | | 0 | |
| -0.79021 | 41.27928 | 41.29683 | 91.09674 | 1.000000 | 1 | 5.882 |
| -19.88125 | 3.71564 | 19.43964 | 168.98005 | 0.470843 | 2 | 11.765 |
| -3.25284 | 0.41162 | 3.27799 | 172.78627 | 0.079395 | 3 | 17.647 |
| -1.24519 | -8.62027 | 8.70974 | 261.78052 | 0.210957 | 4 | 23.529 |
| 0.67911 | -4.00047 | 4.05770 | 279.63452 | 0.098281 | 5 | 29.412 |
| 3.05384 | -2.70452 | 4.07926 | 318.47144 | 0.098803 | 6 | 35.294 |
| -0.83458 | 2.77453 | 2.89731 | 106.73906 | 0.070175 | 7 | 41.176 |
| -4.98518 | -5.59056 | 7.49037 | 228.27658 | 0.181423 | 8 | 47.059 |
| -0.73159 | -5.94164 | 5.98653 | 262.97949 | 0.144998 | 9 | 52.941 |
| -1.09884 | -3.59987 | 3.67762 | 252.62775 | 0.089075 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.62563 | | | | | 0 | |
| -29.39984 | 17.86761 | 34.48285 | 148.71039 | 1.000000 | 1 | 5.882 |
| 3.28682 | -5.91858 | 6.72441 | 298.48267 | 0.195461 | 2 | 11.765 |
| -11.43174 | -5.22678 | 12.56993 | 204.57031 | 0.365975 | 3 | 17.647 |
| -1.44358 | -6.17828 | 1.45455 | 187.04048 | 0.042288 | 4 | 23.529 |
| -8.36825 | -10.34256 | 13.30399 | 231.02338 | 0.386712 | 5 | 29.412 |
| 6.85238 | -8.36609 | 8.78399 | 313.55298 | 0.255327 | 6 | 35.294 |
| -1.83346 | -0.69239 | 1.24398 | 213.82103 | 0.036159 | 7 | 41.176 |
| -1.26033 | -2.96446 | 3.22143 | 246.96849 | 0.093636 | 8 | 47.059 |
| 0.78593 | -3.76279 | 3.84399 | 281.79761 | 0.111735 | 9 | 52.941 |
| 1.44368 | -0.51542 | 1.53292 | 340.35229 | 0.044558 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.23547 | | | | | 0 | |
| 3.23006 | 43.47549 | 43.59537 | 85.74985 | 1.000000 | 1 | 5.882 |
| -13.54078 | 5.44062 | 14.60038 | 158.03717 | 0.334907 | 2 | 11.765 |
| -0.52717 | 0.12358 | 0.54146 | 166.80719 | 0.012420 | 3 | 17.647 |
| -2.02444 | -4.98245 | 4.93684 | 245.78979 | 0.113238 | 4 | 23.529 |
| -1.51948 | -3.55395 | 3.86520 | 246.84935 | 0.088661 | 5 | 29.412 |
| 1.62224 | -3.13643 | 3.53113 | 297.34888 | 0.080998 | 6 | 35.294 |
| -2.38456 | 2.66039 | 3.57861 | 131.78494 | 0.082087 | 7 | 41.176 |
| -4.98892 | -4.64041 | 6.76882 | 223.51239 | 0.155265 | 8 | 47.059 |
| -1.13844 | -3.81116 | 3.97756 | 253.36852 | 0.091238 | 9 | 52.941 |
| -1.61515 | -2.08155 | 2.63469 | 232.19077 | 0.060435 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 15.29645 | | | | | 0 | |
| -22.98999 | 15.57674 | 27.77002 | 145.88062 | 1.000000 | 1 | 5.882 |
| 0.10664 | 1.14142 | 1.15657 | 88.71359 | 0.041648 | 2 | 11.765 |
| -14.08272 | -7.96409 | 15.90557 | 208.24186 | 0.575641 | 3 | 17.647 |
| -1.54164 | -0.14108 | 1.54808 | 185.22856 | 0.055746 | 4 | 23.529 |
| -0.97496 | -0.62419 | 12.00011 | 228.29055 | 0.444174 | 5 | 29.412 |
| 6.16055 | -9.63300 | 9.05257 | 312.88581 | 0.325983 | 6 | 35.294 |
| 0.09965 | -0.37694 | 0.38989 | 284.88859 | 0.014040 | 7 | 41.176 |
| -0.74267 | -2.31795 | 2.43482 | 252.23448 | 0.087649 | 8 | 47.059 |
| 0.84819 | -3.39477 | 3.50205 | 284.21851 | 0.126109 | 9 | 52.941 |
| 1.92171 | -0.73509 | 2.05750 | 339.86714 | 0.074091 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.14772 | | | | | 0 | |
| 3.16388 | 50.58601 | 50.68484 | 86.42107 | 1.000000 | 1 | 5.882 |
| -12.38177 | 6.87365 | 14.16176 | 150.56349 | 0.279488 | 2 | 11.765 |
| -0.72984 | 0.29379 | 0.78676 | 158.07338 | 0.015522 | 3 | 17.647 |
| -2.59290 | -3.35987 | 4.24087 | 232.30862 | 0.083671 | 4 | 23.529 |
| -2.30199 | -4.31952 | 4.76090 | 245.13344 | 0.093931 | 5 | 29.412 |
| 0.93287 | -3.44512 | 3.61742 | 284.94116 | 0.071371 | 6 | 35.294 |
| -1.99434 | 2.19276 | 2.98405 | 132.28494 | 0.058888 | 7 | 41.176 |
| -4.82863 | -3.53269 | 5.35814 | 221.24742 | 0.105715 | 8 | 47.059 |
| -1.25822 | -2.70566 | 2.98854 | 245.19965 | 0.058895 | 9 | 52.941 |
| -1.44287 | -1.81238 | 2.31609 | 231.49150 | 0.045694 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.49942 | | | | | 0 | |
| -23.07150 | 20.26997 | 30.71100 | 138.69838 | 0.727675 | 1 | 5.882 |
| -4.88946 | 24.12369 | 24.61420 | 101.45770 | 0.583216 | 2 | 11.765 |
| -37.63646 | -19.09712 | 42.20178 | 206.90369 | 1.000000 | 3 | 17.647 |
| -2.24923 | -1.78918 | 2.86165 | 219.18761 | 0.067805 | 4 | 23.529 |
| -14.97589 | -13.91792 | 19.87939 | 222.84335 | 0.471028 | 5 | 29.412 |
| 11.78773 | -9.58440 | 15.13049 | 320.69482 | 0.358586 | 6 | 35.294 |
| 3.33395 | 0.67958 | 3.44802 | 14.77934 | 0.081698 | 7 | 41.176 |
| 2.42869 | -0.09993 | 2.42143 | 358.58252 | 0.057374 | 8 | 47.059 |
| 0.48725 | -2.76874 | 2.81129 | 279.98096 | 0.066611 | 9 | 52.941 |
| 4.44829 | -2.31637 | 5.03301 | 332.59766 | 0.119254 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 99.83044 | | | | | 0 | |
| 0.79241 | 100.35231 | 100.35475 | 89.59891 | 1.000000 | 1 | 5.882 |
| -18.97449 | 15.89134 | 24.75005 | 140.05347 | 0.246626 | 2 | 11.765 |
| -5.89278 | -0.37801 | 5.90489 | 183.67039 | 0.059840 | 3 | 17.647 |
| -4.01161 | -4.10003 | 5.73613 | 225.62448 | 0.057159 | 4 | 23.529 |
| -2.95321 | -10.18729 | 10.45595 | 256.99292 | 0.104184 | 5 | 29.412 |
| -1.03044 | -6.21444 | 6.30962 | 260.24438 | 0.062837 | 6 | 35.294 |
| 1.51931 | -0.17454 | 1.52933 | 353.42920 | 0.015199 | 7 | 41.176 |
| -0.47169 | -0.41257 | 0.62666 | 221.17488 | 0.006244 | 8 | 47.059 |
| -1.90887 | -0.50745 | 1.59192 | 198.50839 | 0.015863 | 9 | 52.941 |
| -0.76749 | -3.23314 | 3.32299 | 256.64688 | 0.033112 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 16.46027 | | | | | 0 | |
| 6.91392 | -3.93886 | 7.95719 | 330.32983 | 0.214891 | 1 | 5.882 |
| -6.47384 | 32.42970 | 33.07347 | 101.32339 | 0.893178 | 2 | 11.765 |
| -32.61119 | -17.54015 | 37.02899 | 208.27386 | 1.000000 | 3 | 17.647 |
| -8.94260 | -4.09974 | 4.28670 | 257.09151 | 0.113606 | 4 | 23.529 |
| -7.16585 | -7.00960 | 10.02416 | 224.36848 | 0.270711 | 5 | 29.412 |
| 6.74715 | -2.31159 | 7.13214 | 341.08838 | 0.192610 | 6 | 35.294 |
| 1.40429 | 1.29046 | 1.90718 | 42.58187 | 0.051505 | 7 | 41.176 |
| 2.30089 | 0.65422 | 2.39998 | 15.81868 | 0.064813 | 8 | 47.059 |
| 0.86793 | 0.19511 | 0.88868 | 10.13230 | 0.023811 | 9 | 52.941 |
| 2.61440 | -0.50794 | 2.66328 | 349.00513 | 0.071924 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.88487 | | | | | 0 | |
| 6.85639 | 34.29791 | 34.97650 | 78.69513 | 1.000000 | 1 | 5.882 |
| -3.68133 | 14.96280 | 15.82009 | 104.18644 | 0.429457 | 2 | 11.765 |
| -4.81341 | -2.07569 | 5.24188 | 203.32721 | 0.149869 | 3 | 17.647 |
| -0.33555 | -1.16347 | 1.21009 | 253.91237 | 0.034620 | 4 | 23.529 |
| 0.12322 | -7.22005 | 7.22118 | 270.97778 | 0.206456 | 5 | 29.417 |
| -1.19233 | -2.73287 | 2.98165 | 246.42860 | 0.085247 | 6 | 35.294 |
| 1.98690 | -2.84813 | 3.42756 | 303.88322 | 0.097996 | 7 | 41.176 |
| 3.82079 | 0.20026 | 3.82742 | 3.79283 | 0.086556 | 8 | 47.059 |
| 1.53449 | 1.15878 | 1.92287 | 37.05864 | 0.054976 | 9 | 52.941 |
| 0.29154 | -0.95242 | 0.99604 | 287.01929 | 0.028477 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 13.26315 | | | | | 0 | |
| 35.53943 | -35.11388 | 49.96833 | 315.34497 | 1.000000 | 1 | 5.882 |
| -7.00989 | 49.04068 | 49.65852 | 99.84768 | 0.993959 | 2 | 11.765 |
| -41.54523 | -24.22855 | 48.09395 | 210.29000 | 0.962643 | 3 | 17.647 |
| -3.82474 | -9.19579 | 9.64249 | 251.71823 | 0.193003 | 4 | 23.529 |
| -5.33397 | -12.36100 | 13.46275 | 246.65898 | 0.269469 | 5 | 29.412 |
| 7.59153 | 2.38341 | 7.93329 | 16.87875 | 0.158792 | 6 | 35.294 |
| -4.55342 | 2.67548 | 5.28127 | 149.56250 | 0.105709 | 7 | 41.176 |
| -1.83567 | -3.73690 | 4.16343 | 243.83938 | 0.083335 | 8 | 47.059 |
| 3.99027 | -0.88186 | 4.07004 | 348.63745 | 0.081465 | 9 | 52.941 |
| 1.46595 | 3.31032 | 3.62023 | 66.12000 | 0.072462 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -118.47276 | | | | | 0 | |
| 28.91300 | -29.57031 | 38.60385 | 318.50269 | 1.000000 | 1 | 5.882 |
| 0.29579 | 22.00698 | 22.00888 | 89.25690 | 0.570045 | 2 | 11.765 |
| -1.00400 | -14.19865 | 14.29583 | 263.31519 | 0.370321 | 3 | 17.647 |
| 9.34641 | 1.39748 | 9.45038 | 8.50387 | 0.244882 | 4 | 23.529 |
| -0.83460 | -2.15224 | 2.30840 | 248.80458 | 0.059797 | 5 | 29.412 |
| -3.44956 | -2.18919 | 4.00598 | 212.48044 | 0.103834 | 6 | 35.294 |
| -1.76654 | -6.48934 | 6.72548 | 254.77182 | 0.174218 | 7 | 41.176 |
| 3.78593 | -5.44392 | 6.63894 | 304.81618 | 0.171789 | 8 | 47.059 |
| 4.91563 | 1.23793 | 4.68224 | 15.33066 | 0.121289 | 9 | 52.941 |
| -2.57824 | -0.14574 | 2.58236 | 183.23531 | 0.066894 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.04189 | | | | | 0 | |
| 35.97246 | -37.82607 | 52.19989 | 313.56104 | 1.000000 | 1 | 5.882 |
| 1.15632 | 37.63075 | 37.64850 | 88.23991 | 0.721237 | 2 | 11.765 |
| -3.26522 | -9.25308 | 31.64001 | 197.00017 | 0.606285 | 3 | 17.647 |
| -10.19711 | -7.45764 | 12.63319 | 216.17981 | 0.242016 | 4 | 23.529 |
| -3.20662 | -17.19998 | 17.50237 | 259.26318 | 0.335295 | 5 | 29.412 |
| 12.34991 | 3.96846 | 12.97185 | 17.01404 | 0.248503 | 6 | 35.294 |
| -6.62053 | 8.11852 | 10.46957 | 129.22441 | 0.200567 | 7 | 41.176 |
| -5.38731 | -4.10993 | 6.77683 | 217.33963 | 0.129809 | 8 | 47.059 |
| 3.16383 | -2.16006 | 3.83212 | 325.60994 | 0.073412 | 9 | 52.941 |
| 0.90279 | 4.24268 | 4.35722 | 78.04254 | 0.083472 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -31.13425 | | | | | 0 | |
| 18.78868 | 2.64955 | 18.98875 | 8.97243 | 0.381124 | 1 | 5.882 |
| -30.20551 | 15.05341 | 30.21824 | 157.42348 | 0.879638 | 2 | 11.765 |
| -1.62588 | -44.54574 | 44.57541 | 267.90942 | 1.000000 | 3 | 17.647 |
| 30.82921 | 8.41945 | 31.95819 | 15.27498 | 0.716947 | 4 | 23.529 |
| -18.04411 | 18.07458 | 25.67883 | 119.86598 | 0.463907 | 5 | 29.412 |
| -18.94812 | -8.69917 | 20.87664 | 199.37117 | 0.450398 | 6 | 35.294 |
| 3.96158 | -15.32697 | 15.73533 | 283.88179 | 0.353005 | 7 | 41.176 |
| 11.69546 | 0.82475 | 11.68468 | 4.04755 | 0.262131 | 8 | 47.059 |
| -2.21333 | 9.86889 | 9.32738 | 103.72787 | 0.209248 | 9 | 52.941 |
| -9.81821 | -5.59519 | 10.59189 | 211.63295 | 0.237617 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -3.49841 | | | | | 0 | |
| 37.19781 | -42.22040 | 56.24289 | 311.35059 | 1.000000 | 1 | 5.882 |
| -2.11178 | 34.99420 | 35.13228 | 95.08159 | 0.624653 | 2 | 11.765 |
| -26.44202 | -10.81740 | 28.56914 | 202.24940 | 0.507960 | 3 | 17.647 |
| -12.42236 | -2.69526 | 12.71139 | 192.24164 | 0.226009 | 4 | 23.529 |
| -8.23745 | -21.66261 | 23.17593 | 249.18008 | 0.412069 | 5 | 29.412 |
| 16.11555 | 0.35000 | 16.11935 | 1.24701 | 0.286602 | 6 | 35.294 |
| -3.00004 | 11.96276 | 12.55182 | 107.62285 | 0.223172 | 7 | 41.176 |
| -8.88164 | -1.29776 | 8.89680 | 188.38751 | 0.158185 | 8 | 47.059 |
| 1.33430 | -3.32822 | 3.58572 | 291.84619 | 0.063754 | 9 | 52.941 |
| 0.58905 | 4.26597 | 4.30645 | 82.13820 | 0.076569 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 6.14228 | | | | | 0 | |
| 28.00961 | 19.74168 | 34.31343 | 35.12309 | 0.716812 | 1 | 5.882 |
| -33.54823 | 27.66049 | 45.04196 | 142.11311 | 0.940932 | 2 | 11.765 |
| -18.10767 | -44.31256 | 47.86951 | 247.77333 | 1.000000 | 3 | 17.647 |
| 26.73706 | -4.47659 | 27.10922 | 350.49512 | 0.566315 | 4 | 23.529 |
| 2.22260 | 18.25137 | 18.38620 | 83.05678 | 0.384090 | 5 | 29.412 |
| -23.59943 | 3.98626 | 23.91658 | 170.59984 | 0.499620 | 6 | 35.294 |
| -1.60354 | -20.66583 | 20.66827 | 265.94443 | 0.431763 | 7 | 41.176 |
| 18.27875 | 1.80733 | 18.36787 | 5.64683 | 0.383707 | 8 | 47.059 |
| -7.16680 | 15.71140 | 17.26878 | 114.52029 | 0.360747 | 9 | 52.941 |
| -12.37358 | -9.52629 | 15.61587 | 217.90229 | 0.326217 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -1.63032 | | | | | 0 | |
| 17.42445 | -21.04906 | 27.32533 | 309.61792 | 1.000000 | 1 | 5.882 |
| -4.65698 | 15.49393 | 16.14035 | 106.77005 | 0.590674 | 2 | 11.765 |
| -10.91714 | -7.54112 | 13.26847 | 214.63513 | 0.485574 | 3 | 17.647 |
| -5.48998 | 0.82055 | 5.55096 | 171.49928 | 0.203143 | 4 | 23.529 |
| -6.12727 | -10.95860 | 12.55525 | 240.78917 | 0.459473 | 5 | 29.412 |
| 8.84715 | -1.67331 | 8.21932 | 348.25165 | 0.300795 | 6 | 35.294 |
| -0.21144 | 6.30265 | 6.30419 | 91.92204 | 0.230709 | 7 | 41.176 |
| -5.17510 | 0.68501 | 5.22023 | 172.45979 | 0.191040 | 8 | 47.059 |
| -0.09913 | -1.86989 | 1.87251 | 266.96533 | 0.068527 | 9 | 52.941 |
| 0.09322 | 1.85951 | 1.86185 | 87.13004 | 0.068136 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.48168 | | | | | 0 | |
| 20.14287 | 10.68813 | 22.52788 | 26.60303 | 1.000000 | 1 | 5.882 |
| -9.58153 | 19.31778 | 21.56343 | 116.38123 | 0.957189 | 2 | 11.765 |
| -15.71686 | -15.05808 | 21.76558 | 223.77515 | 0.966162 | 3 | 17.647 |
| 6.79636 | -9.18242 | 11.42398 | 306.58684 | 0.507104 | 4 | 23.529 |
| 8.27604 | 5.36658 | 9.86372 | 32.96129 | 0.437845 | 5 | 29.412 |
| -10.29997 | 7.58875 | 12.79289 | 143.61552 | 0.567869 | 6 | 35.294 |
| -4.19163 | -10.29021 | 11.11118 | 247.83682 | 0.493219 | 7 | 41.176 |
| 9.96469 | 0.12242 | 9.96544 | 0.70386 | 0.442360 | 8 | 47.059 |
| -4.46054 | 8.89288 | 9.95784 | 116.74060 | 0.442023 | 9 | 52.941 |
| -4.18497 | -5.24297 | 8.10818 | 220.28780 | 0.359918 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.13025 | | | | | 0 | |
| 1.36931 | -1.47006 | 2.15965 | 309.34888 | 1.000000 | 1 | 5.882 |
| -0.40444 | 1.20140 | 1.26784 | 108.60558 | 0.586967 | 2 | 11.765 |
| -0.83839 | -0.62111 | 1.04340 | 216.53249 | 0.483132 | 3 | 17.647 |
| -0.42873 | 0.09084 | 0.43825 | 168.03725 | 0.202924 | 4 | 23.529 |
| -0.50978 | -0.87241 | 1.01044 | 239.70059 | 0.467871 | 5 | 29.412 |
| 0.63981 | -0.15435 | 0.63816 | 346.43652 | 0.304754 | 6 | 35.294 |
| 0.00281 | 0.50496 | 0.50497 | 89.68158 | 0.233819 | 7 | 41.176 |
| -0.42035 | 0.07008 | 0.42615 | 170.53447 | 0.197324 | 8 | 47.059 |
| -0.01706 | -0.15106 | 0.15202 | 263.55640 | 0.070389 | 9 | 52.941 |
| 0.00506 | 0.14447 | 0.14456 | 87.99467 | 0.066936 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 226 TEST COND 39 COMP RUN 8.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.30207 | | | | | 0 | |
| 1.66774 | 0.81169 | 1.85478 | 25.95222 | 1.000000 | 1 | 5.882 |
| -0.67202 | 1.59649 | 1.73216 | 112.82816 | 0.933894 | 2 | 11.765 |
| -1.32582 | -1.11791 | 1.73422 | 220.13695 | 0.935002 | 3 | 17.647 |
| 0.46649 | -0.80893 | 0.93380 | 299.97095 | 0.503458 | 4 | 23.529 |
| 0.73908 | 0.38555 | 0.83360 | 27.54918 | 0.449433 | 5 | 29.412 |
| -0.88302 | 0.66740 | 1.04416 | 140.26968 | 0.562958 | 6 | 35.294 |
| -0.37117 | -0.81846 | 0.89869 | 245.60544 | 0.484526 | 7 | 41.176 |
| 0.80234 | 0.00199 | 0.80234 | 0.14192 | 0.432580 | 8 | 47.059 |
| -0.36751 | 0.71986 | 0.80807 | 117.05190 | 0.435669 | 9 | 52.941 |
| -0.49210 | -0.42292 | 0.64886 | 220.67606 | 0.349833 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 0.78170 | | | | | 0 | |
| 1.04780 | 1.28829 | 1.66060 | 129.12224 | 1.000000 | 1 | 5.848 |
| 0.14963 | -1.13582 | 1.14563 | 277.50488 | 0.689893 | 2 | 11.696 |
| 0.16056 | 0.48885 | 0.51454 | 71.91773 | 0.309851 | 3 | 17.544 |
| -0.25455 | -0.17956 | 0.31151 | 215.19844 | 0.187587 | 4 | 23.392 |
| -0.13707 | 0.01178 | 0.13757 | 175.08754 | 0.082846 | 5 | 29.240 |
| 0.02163 | 0.07307 | 0.07620 | 73.51222 | 0.045886 | 6 | 35.088 |
| 0.04114 | 0.27628 | 0.27933 | 81.53021 | 0.168211 | 7 | 40.936 |
| 0.03518 | 0.24541 | 0.24792 | 81.84123 | 0.149294 | 8 | 46.784 |
| 0.02020 | 0.19870 | 0.21073 | 70.54224 | 0.126903 | 9 | 52.632 |
| 0.09035 | 0.10292 | 0.13695 | 48.72113 | 0.082469 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.63100 | | | | | 0 | |
| 0.82612 | -2.20728 | 2.35682 | 290.51953 | 1.000000 | 1 | 5.848 |
| -0.07087 | 1.77288 | 1.77430 | 92.28912 | 0.752837 | 2 | 11.696 |
| 0.04789 | -0.64796 | 0.64973 | 274.22705 | 0.275679 | 3 | 17.544 |
| 0.42099 | -0.01696 | 0.42132 | 357.74683 | 0.178766 | 4 | 23.392 |
| 0.59383 | -0.17323 | 0.61838 | 343.73218 | 0.262381 | 5 | 29.240 |
| 0.06247 | -0.37711 | 0.38225 | 279.40552 | 0.162188 | 6 | 35.088 |
| 0.04823 | -0.47285 | 0.48294 | 281.73560 | 0.204914 | 7 | 40.936 |
| -0.02634 | -0.50414 | 0.50483 | 267.00903 | 0.214201 | 8 | 46.784 |
| -0.07199 | -0.35488 | 0.36211 | 258.53271 | 0.153642 | 9 | 52.632 |
| -0.10580 | -0.38526 | 0.39952 | 254.64445 | 0.169518 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.83469 | | | | | 0 | |
| -5.27319 | 6.31500 | 8.22713 | 129.86278 | 1.000000 | 1 | 5.848 |
| 0.78975 | -5.56259 | 5.61837 | 278.08032 | 0.682908 | 2 | 11.696 |
| 0.71318 | 2.37975 | 2.48432 | 73.31709 | 0.301967 | 3 | 17.544 |
| -1.21084 | -0.85855 | 1.48434 | 215.33827 | 0.180421 | 4 | 23.392 |
| -0.69046 | 0.03837 | 0.69142 | 176.98436 | 0.084041 | 5 | 29.240 |
| 0.12534 | 0.33738 | 0.35991 | 69.81923 | 0.043746 | 6 | 35.088 |
| 0.16592 | 1.32519 | 1.33954 | 82.88319 | 0.162833 | 7 | 40.936 |
| 0.16235 | 1.16115 | 1.17245 | 82.04039 | 0.142510 | 8 | 46.784 |
| 0.30956 | 0.95845 | 1.00720 | 72.10056 | 0.122424 | 9 | 52.632 |
| 0.40833 | 0.49844 | 0.64434 | 50.67499 | 0.078319 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 38.04222 | | | | | 0 | |
| 3.77836 | -10.36498 | 11.03217 | 290.02832 | 1.000000 | 1 | 5.848 |
| -0.48885 | 8.32545 | 8.33978 | 93.36049 | 0.755951 | 2 | 11.696 |
| 0.13449 | -2.99711 | 3.00013 | 272.56934 | 0.271944 | 3 | 17.544 |
| 1.93437 | -0.13083 | 1.93879 | 356.13562 | 0.175739 | 4 | 23.392 |
| 2.79062 | -0.80783 | 2.90519 | 343.85522 | 0.263338 | 5 | 29.240 |
| 0.29395 | -1.79134 | 1.81530 | 279.31885 | 0.164546 | 6 | 35.088 |
| 0.48918 | -2.23897 | 2.29179 | 282.32446 | 0.207737 | 7 | 40.936 |
| -0.13161 | -2.39245 | 2.39607 | 266.85107 | 0.217189 | 8 | 46.784 |
| -0.39005 | -1.69583 | 1.73158 | 258.33667 | 0.156957 | 9 | 52.632 |
| -0.51823 | -1.84123 | 1.91277 | 254.28011 | 0.173381 | 10 | 58.480 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 9.75858 | | | | | 0 | |
| -13.98636 | 16.02538 | 21.27042 | 131.11330 | 1.000000 | 1 | 5.848 |
| 2.25233 | -14.09391 | 14.27274 | 279.07959 | 0.671014 | 2 | 11.696 |
| 1.48406 | 5.96627 | 6.14807 | 76.03152 | 0.289043 | 3 | 17.544 |
| -2.91000 | -2.08347 | 3.57895 | 215.60147 | 0.168260 | 4 | 23.392 |
| -1.83416 | -0.00201 | 1.83416 | 180.06285 | 0.086230 | 5 | 29.240 |
| 0.40342 | 0.76449 | 0.86440 | 62.17963 | 0.040639 | 6 | 35.088 |
| 0.20338 | 3.23453 | 3.24524 | 85.34483 | 0.152570 | 7 | 40.936 |
| 0.36739 | 2.76223 | 2.78656 | 82.42387 | 0.131006 | 8 | 46.784 |
| 0.63316 | 2.36371 | 2.44704 | 75.00449 | 0.115044 | 9 | 52.632 |
| 0.88383 | 1.23823 | 1.52131 | 54.48137 | 0.071522 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 85.44423 | | | | | 0 | |
| 8.39206 | -24.29636 | 25.70485 | 289.05493 | 1.000000 | 1 | 5.848 |
| -1.86474 | 19.51794 | 19.60880 | 95.45752 | 0.762766 | 2 | 11.696 |
| -0.10105 | -6.81576 | 6.81651 | 269.15039 | 0.265184 | 3 | 17.544 |
| 4.33838 | -0.55129 | 4.37326 | 352.79806 | 0.170134 | 4 | 23.392 |
| 6.59553 | -1.86801 | 6.81648 | 344.09497 | 0.265183 | 5 | 29.240 |
| 0.69188 | -4.29377 | 4.34915 | 279.15356 | 0.169196 | 6 | 35.088 |
| 1.27527 | -5.33395 | 5.48427 | 283.44604 | 0.213356 | 7 | 40.936 |
| -0.34505 | -5.72372 | 5.73411 | 266.55005 | 0.223075 | 8 | 46.784 |
| -0.87584 | -4.11057 | 4.20283 | 257.97168 | 0.163504 | 9 | 52.632 |
| -1.31351 | -4.46396 | 4.65320 | 253.60347 | 0.181024 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.48611 | | | | | 0 | |
| -40.02614 | 39.78815 | 56.43747 | 135.17085 | 1.000000 | 1 | 5.848 |
| 7.81212 | -35.20990 | 36.06613 | 282.50977 | 0.639046 | 2 | 11.696 |
| 1.15267 | 14.38665 | 14.43275 | 85.41916 | 0.255730 | 3 | 17.544 |
| -5.80750 | -4.37298 | 7.26980 | 218.97932 | 0.128812 | 4 | 23.392 |
| -5.08976 | -0.72575 | 5.14123 | 188.11507 | 0.091096 | 5 | 29.240 |
| 1.74262 | 1.30191 | 2.17525 | 36.74341 | 0.038543 | 6 | 35.088 |
| -0.73041 | 6.96849 | 7.00466 | 95.98372 | 0.124149 | 7 | 40.936 |
| 0.59423 | 5.30884 | 5.34000 | 83.61093 | 0.094618 | 8 | 46.784 |
| 0.28626 | 5.39022 | 5.40380 | 86.96332 | 0.095746 | 9 | 52.632 |
| 0.85629 | 2.89583 | 3.01978 | 73.52719 | 0.053507 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 159.98865 | | | | | 0 | |
| 10.18176 | -44.21494 | 45.37210 | 282.96777 | 1.000000 | 1 | 5.848 |
| -9.99226 | 34.42267 | 35.84361 | 106.18709 | 0.789992 | 2 | 11.696 |
| -4.17458 | -10.97831 | 10.90869 | 247.49991 | 0.240427 | 3 | 17.544 |
| 5.84799 | -3.28948 | 6.70967 | 330.64233 | 0.147881 | 4 | 23.392 |
| 11.88826 | -2.92502 | 12.21543 | 346.14575 | 0.269232 | 5 | 29.240 |
| 1.22397 | -8.49192 | 8.57967 | 278.20166 | 0.189096 | 6 | 35.088 |
| 3.90493 | -10.35482 | 10.93192 | 288.69995 | 0.240939 | 7 | 40.936 |
| -0.86452 | -11.28320 | 11.31627 | 265.61841 | 0.249419 | 8 | 46.784 |
| -2.07960 | -8.58579 | 8.83485 | 256.38428 | 0.194702 | 9 | 52.632 |
| -3.28099 | -9.37889 | 9.93621 | 250.71873 | 0.218994 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.36481 | | | | | 0 | |
| -49.94797 | 40.64584 | 64.39629 | 140.86256 | 1.000000 | 1 | 5.848 |
| 11.71242 | -35.78601 | 37.63492 | 288.13208 | 0.584427 | 2 | 11.696 |
| -3.60125 | 13.67171 | 14.13805 | 104.75706 | 0.219548 | 3 | 17.544 |
| -3.49705 | -3.05092 | 4.64805 | 221.10225 | 0.072867 | 4 | 23.392 |
| -6.37108 | -2.12158 | 6.71504 | 198.41788 | 0.104277 | 5 | 29.240 |
| 3.05606 | 0.02095 | 3.05613 | 0.39285 | 0.047458 | 6 | 35.088 |
| -3.10984 | 5.21510 | 6.07152 | 120.88177 | 0.094284 | 7 | 40.936 |
| -0.03882 | 2.67923 | 2.67951 | 90.83020 | 0.041610 | 8 | 46.784 |
| -1.97497 | 4.52553 | 4.93770 | 113.57680 | 0.076677 | 9 | 52.632 |
| -1.40847 | 2.57611 | 2.93600 | 118.66748 | 0.045593 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 73.48930 | | | | | 0 | |
| -7.56915 | -15.57118 | 17.31339 | 244.07558 | 0.771292 | 1 | 5.848 |
| -19.52335 | 11.07784 | 22.44725 | 150.42879 | 1.000000 | 2 | 11.696 |
| -10.90431 | 1.51265 | 11.00873 | 172.10231 | 0.490427 | 3 | 17.544 |
| -2.54414 | -6.64327 | 7.11448 | 249.02982 | 0.316942 | 4 | 23.392 |
| 4.29591 | -0.22461 | 4.30177 | 357.00484 | 0.191639 | 5 | 29.240 |
| 0.43429 | -4.91129 | 4.93044 | 275.05322 | 0.219646 | 6 | 35.088 |
| 4.10088 | -5.41691 | 6.79412 | 307.12744 | 0.302671 | 7 | 40.936 |
| -1.02156 | -6.35728 | 6.43883 | 260.87805 | 0.286843 | 8 | 46.784 |
| -1.94211 | -5.98834 | 6.21459 | 251.78949 | 0.276853 | 9 | 52.632 |
| -3.33820 | -6.49613 | 7.30365 | 242.80243 | 0.325369 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.34621 | | | | | 0 | |
| -62.95364 | 47.19696 | 78.68189 | 143.14876 | 1.000000 | 1 | 5.848 |
| 14.76491 | -36.66296 | 39.52435 | 291.93555 | 0.502336 | 2 | 11.696 |
| -10.22262 | 12.36909 | 16.04668 | 129.57254 | 0.203944 | 3 | 17.544 |
| -2.69347 | -2.23328 | 3.49901 | 219.66365 | 0.044469 | 4 | 23.392 |
| -10.64528 | -4.83975 | 11.69388 | 204.44835 | 0.148623 | 5 | 29.240 |
| 4.10151 | -3.63629 | 5.48133 | 318.44867 | 0.069665 | 6 | 35.088 |
| -4.83071 | 4.28262 | 6.46173 | 138.48874 | 0.082125 | 7 | 40.936 |
| -1.64305 | 0.92059 | 1.88338 | 150.73839 | 0.023937 | 8 | 46.784 |
| -4.17396 | 2.81132 | 5.03244 | 146.03830 | 0.063960 | 9 | 52.632 |
| -2.61776 | 2.11926 | 3.36430 | 141.08678 | 0.042759 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 34.47842 | | | | | 0 | |
| -14.24577 | 15.94411 | 21.38121 | 131.78023 | 0.747783 | 1 | 5.848 |
| -28.58910 | 0.66346 | 28.59279 | 178.67039 | 1.000000 | 2 | 11.696 |
| -14.86980 | 8.32736 | 17.04276 | 150.75037 | 0.596051 | 3 | 17.544 |
| -8.10660 | -9.21825 | 12.27531 | 228.67343 | 0.429315 | 4 | 23.392 |
| -1.31556 | -0.76214 | 1.52037 | 210.08402 | 0.053173 | 5 | 29.240 |
| 0.53060 | -3.59472 | 3.59529 | 278.61972 | 0.125741 | 6 | 35.088 |
| 4.42751 | -1.39520 | 4.63827 | 342.98120 | 0.161938 | 7 | 40.936 |
| -2.98281 | -3.15323 | 4.28593 | 227.36781 | 0.149895 | 8 | 46.784 |
| -2.03863 | -4.48977 | 4.93095 | 245.57898 | 0.172454 | 9 | 52.632 |
| -3.33540 | -4.16627 | 5.33402 | 231.32814 | 0.186653 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 21.02428 | | | | | 0 | |
| -49.43367 | 38.38499 | 62.58670 | 142.17085 | 1.000000 | 1 | 5.848 |
| 9.94075 | -20.82179 | 23.07303 | 295.52075 | 0.368657 | 2 | 11.696 |
| -14.17428 | 5.10583 | 15.06584 | 160.19006 | 0.240719 | 3 | 17.544 |
| -2.53280 | -1.19083 | 2.79877 | 205.18115 | 0.044718 | 4 | 23.392 |
| -12.94090 | -6.39330 | 14.43462 | 206.29112 | 0.230624 | 5 | 29.240 |
| 3.01234 | -7.80818 | 8.36910 | 291.09619 | 0.133720 | 6 | 35.088 |
| -3.38781 | 2.46571 | 4.19010 | 143.95216 | 0.066949 | 7 | 40.936 |
| -3.21845 | -0.08381 | 3.21954 | 181.49158 | 0.051441 | 8 | 46.784 |
| -4.11410 | -0.76258 | 4.18418 | 190.50099 | 0.066854 | 9 | 52.632 |
| -1.38992 | 0.54917 | 1.49448 | 158.44040 | 0.023878 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION [illegible]
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP [illegible] 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 37.91988 | | | | | 0 | |
| -1.93661 | 40.43401 | 40.48035 | 92.74216 | 1.000000 | 1 | 5.848 |
| -23.37604 | 5.49082 | 24.01224 | 166.78137 | 0.593183 | 2 | 11.696 |
| -8.88369 | 5.41466 | 10.40377 | 148.63745 | 0.257008 | 3 | 17.544 |
| -6.20856 | -6.56773 | 9.03777 | 226.61021 | 0.223263 | 4 | 23.392 |
| -3.60617 | -4.39244 | 5.68313 | 230.61415 | 0.140392 | 5 | 29.240 |
| 1.28545 | -3.10851 | 3.36381 | 292.46431 | 0.083097 | 6 | 35.088 |
| 2.44434 | 1.67612 | 2.96381 | 34.43898 | 0.073216 | 7 | 40.936 |
| -4.90584 | -0.93907 | 4.99491 | 190.83641 | 0.123391 | 8 | 46.784 |
| -1.42767 | -2.67815 | 3.03492 | 241.93871 | 0.074973 | 9 | 52.632 |
| -1.82975 | -1.01792 | 2.09383 | 209.08801 | 0.051725 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.47801 | | | | | 0 | |
| -28.71859 | 24.49387 | 37.73920 | 139.53152 | 1.000000 | 1 | 5.848 |
| 4.58295 | -6.15891 | 7.67695 | 306.65356 | 0.203421 | 2 | 11.696 |
| -13.36372 | 0.11794 | 13.36424 | 179.49437 | 0.354121 | 3 | 17.544 |
| -2.17274 | -0.64966 | 2.26779 | 196.64496 | 0.060091 | 4 | 23.392 |
| -10.83909 | -5.30087 | 12.06587 | 206.06100 | 0.319717 | 5 | 29.240 |
| 1.79505 | -7.92677 | 8.11874 | 282.48413 | 0.215127 | 6 | 35.088 |
| -1.40429 | 1.06335 | 1.76145 | 142.86647 | 0.046674 | 7 | 40.936 |
| -2.92961 | -0.36611 | 2.95240 | 187.12320 | 0.078232 | 8 | 46.784 |
| -2.76061 | -2.21175 | 3.53734 | 218.70114 | 0.093731 | 9 | 52.632 |
| -0.24999 | -0.48184 | 0.54283 | 242.57857 | 0.014384 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 39.62769 | | | | | 0 | |
| 6.11853 | 42.07384 | 42.51639 | 81.72577 | 1.000000 | 1 | 5.848 |
| -14.11330 | 8.90098 | 16.68564 | 147.76149 | 0.392452 | 2 | 11.696 |
| -3.21978 | 1.58743 | 3.58983 | 153.75560 | 0.084434 | 3 | 17.544 |
| -2.82642 | -3.31928 | 4.35962 | 229.58524 | 0.102540 | 4 | 23.392 |
| -3.99086 | -5.38157 | 6.36514 | 237.72296 | 0.149710 | 5 | 29.240 |
| 1.29704 | -2.24327 | 2.59125 | 300.03613 | 0.060947 | 6 | 35.088 |
| 0.73356 | 2.13973 | 2.26198 | 71.07684 | 0.053202 | 7 | 40.936 |
| -4.33929 | -0.15887 | 4.34220 | 182.03674 | 0.102130 | 8 | 46.784 |
| -0.69203 | -1.35655 | 1.52287 | 242.97203 | 0.035818 | 9 | 52.632 |
| -0.65222 | 0.40849 | 0.76852 | 148.04697 | 0.018076 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 11.49231 | | | | | 0 | |
| -22.05284 | 23.30090 | 32.08206 | 133.42374 | 1.000000 | 1 | 5.848 |
| 2.48021 | 1.89865 | 3.12351 | 37.43469 | 0.097360 | 2 | 11.696 |
| -16.56193 | -1.96493 | 16.65920 | 186.77411 | 0.519237 | 3 | 17.544 |
| -2.27618 | -0.83376 | 2.42407 | 200.11760 | 0.075558 | 4 | 23.392 |
| -10.79938 | -4.32710 | 11.63402 | 201.83501 | 0.362633 | 5 | 29.240 |
| 1.61057 | -0.69061 | 0.83859 | 280.49902 | 0.275499 | 6 | 35.088 |
| -0.09941 | 0.25108 | 0.27004 | 111.60048 | 0.008417 | 7 | 40.936 |
| -2.05649 | -0.63427 | 2.15208 | 197.14104 | 0.067080 | 8 | 46.784 |
| -2.09493 | -2.46202 | 3.23269 | 229.60550 | 0.100763 | 9 | 52.632 |
| -0.09864 | -1.35457 | 1.35816 | 265.83496 | 0.042334 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 53.17549 | | | | | 0 | |
| 8.28132 | 51.78781 | 52.44576 | 80.91478 | 1.000000 | 1 | 5.848 |
| -11.28590 | 11.70475 | 16.25954 | 133.95634 | 0.310026 | 2 | 11.696 |
| -2.00631 | 1.11615 | 2.29414 | 150.88786 | 0.043743 | 3 | 17.544 |
| -1.98737 | -2.46850 | 3.16989 | 231.16267 | 0.060426 | 4 | 23.392 |
| -4.11529 | -6.93544 | 7.72319 | 237.00180 | 0.147260 | 5 | 29.240 |
| 1.47912 | -1.67249 | 2.23272 | 311.48877 | 0.042572 | 6 | 35.088 |
| 0.19334 | 1.85730 | 1.86754 | 83.99596 | 0.035589 | 7 | 40.936 |
| -3.29593 | -0.32980 | 3.31239 | 185.71414 | 0.063158 | 8 | 46.784 |
| -0.24633 | -1.17204 | 1.19723 | 258.22437 | 0.022828 | 9 | 52.632 |
| -0.28172 | 0.28297 | 0.39930 | 134.87369 | 0.007614 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 23.34537 | | | | | 0 | |
| -21.11832 | 41.42529 | 46.49771 | 117.01222 | 1.000000 | 1 | 5.848 |
| 0.22579 | 28.07907 | 28.07997 | 89.53923 | 0.603900 | 2 | 11.696 |
| -43.37000 | -6.66958 | 43.87982 | 188.74263 | 0.943699 | 3 | 17.544 |
| -5.14902 | -3.43284 | 6.18844 | 213.69133 | 0.133091 | 4 | 23.392 |
| -17.97052 | -3.15807 | 18.24588 | 189.96715 | 0.392404 | 5 | 29.240 |
| 4.04699 | -15.66017 | 16.17464 | 284.48975 | 0.347859 | 6 | 35.088 |
| 3.89055 | -1.22155 | 4.08544 | 342.60229 | 0.087863 | 7 | 40.936 |
| 0.97989 | -1.72972 | 1.98799 | 299.53174 | 0.042755 | 8 | 46.784 |
| -1.29031 | 2.82046 | 3.10165 | 245.41675 | 0.066704 | 9 | 52.632 |
| -0.58786 | -4.90794 | 4.94302 | 263.16964 | 0.106307 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 131.31152 | | | | | 0 | |
| 12.15987 | 118.60513 | 119.22641 | 84.14813 | 1.000000 | 1 | 5.848 |
| -14.80134 | 25.78862 | 29.73436 | 119.85370 | 0.249394 | 2 | 11.696 |
| -4.26756 | 2.62782 | 5.01173 | 148.37663 | 0.042035 | 3 | 17.544 |
| -1.46232 | -3.42055 | 3.72002 | 246.85268 | 0.031201 | 4 | 23.392 |
| -9.85953 | -12.53326 | 15.94456 | 231.80891 | 0.133750 | 5 | 29.240 |
| 1.78014 | -0.00282 | 1.78014 | 359.90918 | 0.014931 | 6 | 35.088 |
| -0.58513 | -0.03328 | 0.58608 | 183.25542 | 0.004916 | 7 | 40.936 |
| 0.35096 | -2.57556 | 2.60047 | 277.93628 | 0.021811 | 8 | 46.784 |
| 1.11277 | -2.23828 | 2.49963 | 296.43457 | 0.020965 | 9 | 52.632 |
| -0.44944 | -2.10260 | 2.15009 | 257.93433 | 0.018034 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.98265 | | | | | 0 | |
| 5.73022 | 9.43138 | 11.03568 | 58.71835 | 0.295430 | 1 | 5.848 |
| -1.81668 | 35.49889 | 35.54533 | 92.92824 | 0.951963 | 2 | 11.696 |
| -36.96090 | -5.35481 | 37.39469 | 188.24174 | 1.000000 | 3 | 17.544 |
| -5.73874 | -8.34628 | 7.84456 | 222.98582 | 0.210002 | 4 | 23.392 |
| -9.13549 | -1.56087 | 9.26926 | 189.74976 | 0.248142 | 5 | 29.240 |
| 4.47413 | -8.93788 | 8.25468 | 302.82856 | 0.220981 | 6 | 35.088 |
| 3.29833 | 0.76419 | 3.37791 | 13.07937 | 0.090428 | 7 | 40.936 |
| 1.54259 | -0.56765 | 1.64371 | 339.79888 | 0.044003 | 8 | 46.784 |
| 0.44096 | -1.11029 | 1.19465 | 291.66089 | 0.031981 | 9 | 52.632 |
| 0.93863 | -3.64804 | 3.76696 | 284.43335 | 0.100843 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 40.26644 | | | | | 0 | |
| 0.07141 | 68.25879 | 68.93776 | 81.43884 | 1.000000 | 1 | 5.848 |
| -4.93501 | 14.81698 | 14.73227 | 107.98845 | 0.241758 | 2 | 11.696 |
| 1.87283 | -1.[illegible]9819 | 2.26798 | 298.23145 | 0.037218 | 3 | 17.544 |
| 4.84862 | -0.[illegible]8 | 4.85878 | 355.98884 | 0.866884 | 4 | 23.392 |
| -9.57847 | -5.06286 | 7.49319 | 221.88629 | 0.122965 | 5 | 29.240 |
| -1.63577 | 2.16614 | 2.71639 | 127.85849 | 0.044344 | 6 | 35.088 |
| -2.07828 | -1.49848 | 2.55758 | 215.64699 | 0.041969 | 7 | 40.936 |
| 1.21712 | -3.11543 | 3.34474 | 291.33911 | 0.054888 | 8 | 46.784 |
| 1.54826 | -2.63389 | 3.09455 | 300.45557 | 0.050126 | 9 | 52.632 |
| 0.28492 | -1.93701 | 1.93785 | 278.36768 | 0.032129 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.28087 | | | | | 0 | |
| 30.15919 | -29.93373 | 42.49240 | 319.21484 | 0.824846 | 1 | 5.848 |
| 0.79817 | 51.54694 | 51.55387 | 89.11585 | 1.000000 | 2 | 11.696 |
| -46.74391 | -3.95430 | 46.91006 | 184.83540 | 0.909953 | 3 | 17.544 |
| -12.54072 | -9.65230 | 15.82948 | 217.98463 | 0.306969 | 4 | 23.392 |
| -9.24181 | -9.01622 | 12.91879 | 224.29459 | 0.250437 | 5 | 29.240 |
| 9.38813 | -2.61816 | 9.66717 | 344.33545 | 0.187519 | 6 | 35.088 |
| 0.76759 | 7.79482 | 7.83252 | 84.37589 | 0.151931 | 7 | 40.936 |
| -3.58836 | 1.69823 | 3.99928 | 154.72878 | 0.076868 | 8 | 46.784 |
| -0.81888 | -2.61913 | 2.61919 | 269.98038 | 0.050806 | 9 | 52.632 |
| 4.89887 | -1.36137 | 5.08374 | 344.46784 | 0.098612 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -79.59326 | | | | | 0 | |
| 19.40921 | 0.81953 | 21.31903 | 24.43780 | 1.000000 | 1 | 5.848 |
| -8.23379 | 9.20981 | 12.35378 | 131.79758 | 0.579472 | 2 | 11.696 |
| 7.80569 | -18.13788 | 19.47203 | 291.33911 | 0.913364 | 3 | 17.544 |
| 17.40347 | 1.90258 | 17.50714 | 6.23898 | 0.821190 | 4 | 23.392 |
| -2.18484 | 4.45627 | 5.14338 | 115.13721 | 0.241258 | 5 | 29.240 |
| -10.01166 | 3.95225 | 10.76353 | 158.45766 | 0.504879 | 6 | 35.088 |
| -5.39884 | -3.19594 | 6.27328 | 210.62885 | 0.294252 | 7 | 40.936 |
| -1.86455 | -3.99549 | 4.45249 | 243.81795 | 0.208698 | 8 | 46.784 |
| 1.78896 | -2.31882 | 2.87588 | 308.26172 | 0.134893 | 9 | 52.632 |
| -1.08347 | 0.39365 | 1.15277 | 160.03287 | 0.054072 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -4.30682 | | | | | 0 | |
| 37.70174 | -36.66461 | 52.59006 | 315.79883 | 1.000000 | 1 | 5.848 |
| 10.03291 | 42.30272 | 43.47618 | 76.65765 | 0.826700 | 2 | 11.696 |
| -33.73590 | 4.20089 | 33.99643 | 172.90190 | 0.646442 | 3 | 17.544 |
| -16.11900 | -6.14353 | 16.64304 | 194.41623 | 0.316467 | 4 | 23.392 |
| -10.65502 | -13.52130 | 17.21495 | 231.76123 | 0.327342 | 5 | 29.240 |
| 12.81279 | -2.85318 | 13.12662 | 347.44604 | 0.249603 | 6 | 35.088 |
| 1.16845 | 12.05317 | 12.10968 | 84.46292 | 0.230265 | 7 | 40.936 |
| -6.65856 | 3.29556 | 7.42947 | 153.66757 | 0.141271 | 8 | 46.784 |
| -0.02836 | -2.52401 | 2.52117 | 269.35522 | 0.047940 | 9 | 52.632 |
| 4.52397 | 3.30931 | 5.60516 | 36.18573 | 0.106582 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -15.48890 | | | | | 0 | |
| 14.61738 | 5.38223 | 15.01517 | 21.00520 | 0.373485 | 1 | 5.848 |
| -33.61038 | 17.50748 | 37.89682 | 152.48523 | 0.942640 | 2 | 11.696 |
| -9.59441 | -39.04124 | 40.20287 | 256.19287 | 1.000000 | 3 | 17.544 |
| 30.11971 | -1.46358 | 30.15523 | 357.21862 | 0.750077 | 4 | 23.392 |
| -1.93503 | 18.26440 | 18.36661 | 96.04787 | 0.456848 | 5 | 29.240 |
| -20.65344 | 4.57904 | 21.15494 | 167.49924 | 0.526205 | 6 | 35.088 |
| -4.13032 | -14.31242 | 14.89648 | 253.90274 | 0.370533 | 7 | 40.936 |
| 9.73020 | -2.61663 | 10.07589 | 344.94824 | 0.250626 | 8 | 46.784 |
| 0.90461 | 9.30282 | 9.34670 | 84.44594 | 0.232488 | 9 | 52.632 |
| -11.08995 | 0.48445 | 11.10053 | 177.49869 | 0.276113 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -13.75029 | | | | | 0 | |
| 43.76773 | -40.81984 | 59.84860 | 316.99609 | 1.000000 | 1 | 5.848 |
| 5.24808 | 42.12547 | 42.45111 | 82.99848 | 0.709308 | 2 | 11.696 |
| -31.29565 | 0.98497 | 31.31114 | 178.19731 | 0.523172 | 3 | 17.544 |
| -16.57257 | 1.18789 | 16.61507 | 175.90015 | 0.277618 | 4 | 23.392 |
| -17.36865 | -15.53436 | 23.30205 | 221.80913 | 0.389350 | 5 | 29.240 |
| 13.25757 | -7.69477 | 15.32882 | 329.86865 | 0.256127 | 6 | 35.088 |
| 4.97432 | 11.71431 | 12.72258 | 67.03481 | 0.212581 | 7 | 40.936 |
| -8.45517 | 6.87741 | 9.43229 | 133.18610 | 0.157602 | 8 | 46.784 |
| -2.54393 | -1.49364 | 2.94992 | 210.41971 | 0.049290 | 9 | 52.632 |
| 3.28652 | 2.54942 | 4.15941 | 37.80148 | 0.069499 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 40 COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 35.10547 | | | | | 0 | |
| 36.06985 | 6.02532 | 36.56963 | 9.48346 | 0.798804 | 1 | 5.848 |
| -22.60637 | 39.80960 | 45.78047 | 119.59065 | 1.000000 | 2 | 11.696 |
| -28.56305 | -30.47987 | 41.77164 | 226.85942 | 0.912434 | 3 | 17.544 |
| 16.32756 | -15.33956 | 20.46591 | 322.91968 | 0.447045 | 4 | 23.392 |
| 7.44860 | 8.52966 | 11.32417 | 48.87061 | 0.247358 | 5 | 29.240 |
| -13.61365 | 12.88306 | 18.74310 | 136.57942 | 0.409413 | 6 | 35.088 |
| -12.30077 | -13.86007 | 18.53133 | 228.41103 | 0.404787 | 7 | 40.936 |
| 13.74422 | -9.41505 | 16.65973 | 325.58813 | 0.363905 | 8 | 46.784 |
| 5.69920 | 16.59123 | 17.54279 | 71.04199 | 0.383194 | 9 | 52.632 |
| -19.15370 | 4.01829 | 19.57065 | 168.15163 | 0.427489 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 4C COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -6.63640 | | | | | 0 | |
| 21.51875 | -20.29442 | 29.57904 | 316.67700 | 1.000000 | 1 | 5.848 |
| -1.27374 | 19.34998 | 19.39185 | 93.76619 | 0.655594 | 2 | 11.696 |
| -13.89817 | -2.18161 | 14.06835 | 188.92096 | 0.475619 | 3 | 17.544 |
| -7.01801 | 2.27758 | 7.37833 | 162.32005 | 0.249445 | 4 | 23.392 |
| -10.46495 | -7.31978 | 12.77084 | 214.97110 | 0.431753 | 5 | 29.240 |
| 5.53993 | -5.40131 | 7.73725 | 315.72543 | 0.261579 | 6 | 35.088 |
| 3.78909 | 4.53202 | 5.90732 | 50.10196 | 0.199713 | 7 | 40.936 |
| -2.47894 | 4.59454 | 5.22063 | 118.34865 | 0.176497 | 8 | 46.784 |
| -2.34966 | -0.20008 | 2.37809 | 184.82620 | 0.080398 | 9 | 52.632 |
| 0.99716 | 0.20744 | 1.01851 | 11.75185 | 0.034433 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 4C COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.60786 | | | | | 0 | |
| 27.44920 | 0.45653 | 27.45302 | 0.95 | 1.000000 | 1 | 5.848 |
| -0.78448 | 26.54453 | 26.55611 | 91.69284 | 0.967329 | 2 | 11.696 |
| -19.05238 | -6.50548 | 20.13242 | 198.85257 | 0.733341 | 3 | 17.544 |
| -1.14684 | -10.11181 | 10.17683 | 263.52930 | 0.370693 | 4 | 23.392 |
| 8.01914 | -2.52741 | 8.43859 | 341.45889 | 0.307383 | 5 | 29.240 |
| -1.16132 | 9.57402 | 9.64420 | 95.91623 | 0.351298 | 6 | 35.088 |
| -9.59752 | -4.18427 | 10.46999 | 203.55595 | 0.381378 | 7 | 40.936 |
| 6.05900 | -7.58090 | 9.70472 | 308.63330 | 0.353503 | 8 | 46.784 |
| 4.90767 | 9.12941 | 10.36491 | 61.73894 | 0.377551 | 9 | 52.632 |
| -10.85021 | 3.58922 | 11.42846 | 161.69594 | 0.416291 | 10 | 58.480 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 4C COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.52900 | | | | | 0 | |
| 1.70503 | -1.60958 | 2.34475 | 316.64941 | 1.000000 | 1 | 5.848 |
| -0.14509 | 1.51510 | 1.52203 | 95.47031 | 0.649120 | 2 | 11.696 |
| -1.08131 | -0.20313 | 1.10023 | 190.63925 | 0.469229 | 3 | 17.544 |
| -0.54297 | 0.20150 | 0.57915 | 159.53940 | 0.246998 | 4 | 23.392 |
| -0.85215 | -0.57652 | 1.02885 | 214.08038 | 0.438788 | 5 | 29.240 |
| 0.42773 | -0.44735 | 0.61893 | 313.71582 | 0.263962 | 6 | 35.088 |
| 0.31636 | 0.34490 | 0.46802 | 47.47131 | 0.199604 | 7 | 40.936 |
| -0.18840 | 0.37848 | 0.42278 | 116.46341 | 0.180308 | 8 | 46.784 |
| -0.20092 | -0.00945 | 0.20114 | 182.69309 | 0.085782 | 9 | 52.632 |
| 0.07144 | 0.00468 | 0.07159 | 3.75193 | 0.030534 | 10 | 58.480 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 497 OSC CTR 256 TEST COND 4C COMP RUN 25.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.14438 | | | | | 0 | |
| 2.28817 | 0.00941 | 2.28814 | 0.23551 | 1.000000 | 1 | 5.848 |
| 0.05589 | 2.18711 | 2.19783 | 88.53518 | 0.956161 | 2 | 11.696 |
| -1.57164 | -0.41787 | 1.62524 | 194.98994 | 0.710726 | 3 | 17.544 |
| -0.19776 | -0.84955 | 0.87226 | 256.89630 | 0.381211 | 4 | 23.392 |
| 0.68660 | -0.28703 | 0.74418 | 337.31299 | 0.325234 | 5 | 29.240 |
| -0.02801 | 0.79684 | 0.79733 | 92.01346 | 0.348462 | 6 | 35.088 |
| -0.80196 | -0.30220 | 0.85701 | 200.64798 | 0.374545 | 7 | 40.936 |
| 0.47389 | -0.63524 | 0.79253 | 306.72314 | 0.346364 | 8 | 46.784 |
| 0.4357 | 0.71663 | 0.84478 | 60.68878 | 0.369202 | 9 | 52.632 |
| -0.17811 | 0.30328 | 0.92901 | 160.94606 | 0.406013 | 10 | 58.480 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| C.50636 | | | | | C | |
| -0.92572 | 1.11068 | 1.44587 | 129.81018 | 1.000000 | 1 | 5.882 |
| 0.25790 | -0.87658 | 0.91373 | 286.39453 | 0.631959 | 2 | 11.765 |
| -0.00217 | 0.40201 | 0.40201 | 90.30898 | 0.278042 | 3 | 17.647 |
| -0.03811 | -0.06718 | 0.07724 | 240.43816 | 0.053420 | 4 | 23.529 |
| -0.16492 | 0.01543 | 0.16524 | 174.44359 | 0.114287 | 5 | 29.412 |
| 0.01385 | -0.06991 | 0.07127 | 281.20459 | 0.049289 | 6 | 35.294 |
| -0.04650 | 0.14217 | 0.14958 | 108.11090 | 0.103452 | 7 | 41.176 |
| -0.10352 | -0.00351 | 0.10358 | 181.93942 | 0.071636 | 8 | 47.059 |
| -0.07340 | 0.03473 | 0.08120 | 154.67973 | 0.056162 | 9 | 52.941 |
| -0.07029 | -0.02953 | 0.07624 | 202.78534 | 0.052730 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.40085 | | | | | C | |
| -0.51979 | 0.02371 | 0.52033 | 177.38826 | 0.545884 | 1 | 5.882 |
| -0.94343 | -0.13601 | 0.95318 | 188.20332 | 1.000000 | 2 | 11.765 |
| -0.41892 | 0.07031 | 0.42477 | 170.47258 | 0.445639 | 3 | 17.647 |
| -0.14566 | -0.16826 | 0.22255 | 229.11762 | 0.233482 | 4 | 23.529 |
| -0.05484 | 0.18003 | 0.18820 | 106.94081 | 0.197441 | 5 | 29.412 |
| 0.00716 | 0.00688 | 0.00972 | 44.84887 | 0.009377 | 6 | 35.294 |
| 0.00493 | -0.09107 | 0.09120 | 273.09912 | 0.095681 | 7 | 41.176 |
| -0.01422 | -0.04886 | 0.05069 | 253.71123 | 0.053180 | 8 | 47.059 |
| -0.07392 | -0.10293 | 0.12672 | 234.31319 | 0.132945 | 9 | 52.941 |
| -0.05118 | -0.10220 | 0.11430 | 243.39896 | 0.119912 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.64192 | | | | | C | |
| -4.67454 | 5.44309 | 7.17483 | 130.69628 | 1.000000 | 1 | 5.882 |
| 1.28823 | -4.26045 | 4.45095 | 286.82373 | 0.620356 | 2 | 11.765 |
| -0.07125 | 1.92770 | 1.92902 | 92.11690 | 0.268859 | 3 | 17.647 |
| -0.18026 | -0.33270 | 0.37839 | 241.55109 | 0.052739 | 4 | 23.529 |
| -0.81821 | 0.08031 | 0.82214 | 174.39427 | 0.114587 | 5 | 29.412 |
| 0.06188 | -0.34043 | 0.34601 | 280.30249 | 0.048225 | 6 | 35.294 |
| -0.24051 | 0.67075 | 0.71256 | 109.72655 | 0.099314 | 7 | 41.178 |
| -0.49068 | -0.01362 | 0.49086 | 181.59086 | 0.068415 | 8 | 47.059 |
| -0.35819 | 0.16597 | 0.39478 | 155.13095 | 0.055023 | 9 | 52.941 |
| -0.34010 | -0.13614 | 0.36633 | 201.81635 | 0.051058 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.59926 | | | | | C | |
| -2.52170 | 0.18976 | 2.52883 | 175.69650 | 0.557656 | 1 | 5.882 |
| -4.49206 | -0.62079 | 4.53473 | 187.86830 | 1.000000 | 2 | 11.765 |
| -2.00611 | 0.35705 | 2.03764 | 169.90799 | 0.449339 | 3 | 17.647 |
| -0.67868 | -0.79282 | 1.04363 | 229.43561 | 0.230141 | 4 | 23.529 |
| -0.26517 | 0.84464 | 0.88530 | 107.42892 | 0.195226 | 5 | 29.412 |
| 0.31061 | 0.31123 | 0.43971 | 45.05688 | 0.096964 | 6 | 35.294 |
| 0.81119 | -0.41835 | 0.41898 | 271.53174 | 0.092287 | 7 | 41.176 |
| -0.07711 | -0.21139 | 0.22502 | 249.95883 | 0.049621 | 8 | 47.059 |
| -0.35104 | -0.47834 | 0.59332 | 233.72594 | 0.130839 | 9 | 52.941 |
| -0.29285 | -0.46842 | 0.55230 | 241.69998 | 0.117383 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.40944 | | | | | 0 | |
| -12.44619 | 13.80684 | 18.50201 | 132.07892 | 1.000000 | 1 | 5.882 |
| 3.37525 | -10.65089 | 11.17290 | 287.58325 | 0.600629 | 2 | 11.765 |
| -0.44833 | 4.70275 | 4.72407 | 95.44588 | 0.253955 | 3 | 17.647 |
| -0.42861 | -0.85918 | 0.96015 | 243.48726 | 0.051615 | 4 | 23.529 |
| -2.12825 | 0.22451 | 2.14006 | 173.97815 | 0.115044 | 5 | 29.412 |
| 0.13057 | -0.85399 | 0.86392 | 278.69287 | 0.046442 | 6 | 35.294 |
| -0.66589 | 1.58688 | 1.72093 | 112.76396 | 0.092513 | 7 | 41.176 |
| -1.17131 | -0.01884 | 1.17146 | 180.92154 | 0.062975 | 8 | 47.059 |
| -0.90187 | 0.40237 | 0.98756 | 155.95596 | 0.053089 | 9 | 52.941 |
| -0.94337 | -0.30755 | 0.89770 | 200.03549 | 0.048253 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 15.58699 | | | | | 0 | |
| -6.28359 | 0.80584 | 6.33505 | 172.69196 | 0.581108 | 1 | 5.882 |
| -10.81488 | -1.37289 | 10.90167 | 187.23476 | 1.000000 | 2 | 11.765 |
| -4.88209 | 0.96085 | 4.97574 | 168.86583 | 0.456420 | 3 | 17.647 |
| -1.54639 | -1.87181 | 2.44014 | 230.06439 | 0.223831 | 4 | 23.529 |
| -0.65688 | 1.97661 | 2.08290 | 108.38383 | 0.191062 | 5 | 29.412 |
| 0.70622 | 0.71820 | 1.00726 | 45.48189 | 0.092395 | 6 | 35.294 |
| -0.82892 | -0.93790 | 0.93835 | 268.23340 | 0.086074 | 7 | 41.176 |
| -0.22844 | -0.41685 | 0.47534 | 241.27602 | 0.043602 | 8 | 47.059 |
| -0.84979 | -1.09837 | 1.38330 | 232.56265 | 0.126889 | 9 | 52.941 |
| -0.69836 | -1.04512 | 1.23095 | 238.10654 | 0.112914 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.22957 | | | | | 0 | |
| -36.06293 | 34.15356 | 49.66890 | 136.55765 | 1.000000 | 1 | 5.882 |
| 9.37749 | -25.28854 | 26.97122 | 290.34578 | 0.543020 | 2 | 11.765 |
| -3.21618 | 10.15293 | 10.65015 | 107.57609 | 0.214423 | 3 | 17.647 |
| -0.81320 | -2.27378 | 2.41482 | 290.32077 | 0.048618 | 4 | 23.529 |
| -5.70981 | 0.78302 | 5.76325 | 172.19138 | 0.116033 | 5 | 29.412 |
| 0.04017 | -2.03722 | 2.03761 | 271.12964 | 0.041024 | 6 | 35.294 |
| -2.13994 | 2.93085 | 3.62894 | 126.13481 | 0.073063 | 7 | 41.176 |
| -2.27909 | 0.09496 | 2.28107 | 177.61418 | 0.045926 | 8 | 47.059 |
| -2.28106 | 0.84206 | 2.35738 | 159.07167 | 0.047462 | 9 | 52.941 |
| -1.93643 | -0.43099 | 1.98557 | 192.77296 | 0.039976 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.67285 | | | | | 0 | |
| -14.91220 | 4.82927 | 15.44697 | 164.87978 | 0.706906 | 1 | 5.882 |
| -21.77600 | -1.81523 | 21.85152 | 184.76509 | 1.000000 | 2 | 11.765 |
| -10.35318 | 2.69251 | 10.74965 | 164.39852 | 0.491941 | 3 | 17.647 |
| -2.51916 | -3.41228 | 4.24144 | 233.56293 | 0.194103 | 4 | 23.529 |
| -1.49136 | 3.92404 | 3.82862 | 112.93788 | 0.175119 | 5 | 29.412 |
| 1.06134 | 1.16737 | 1.57772 | 47.72399 | 0.072202 | 6 | 35.294 |
| -0.57453 | -1.28244 | 1.40525 | 245.86795 | 0.064309 | 7 | 41.176 |
| -0.85720 | 0.04767 | 0.85852 | 176.81723 | 0.039289 | 8 | 47.059 |
| -1.48172 | -1.72684 | 2.41842 | 229.73835 | 0.110609 | 9 | 52.941 |
| -1.78693 | -1.30219 | 2.14494 | 217.39948 | 0.098251 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 35.19328 | | | | | C | |
| -45.82849 | 34.77974 | 57.53156 | 142.80475 | 1.000000 | 1 | 5.882 |
| 11.19006 | -23.50546 | 26.03313 | 295.45728 | 0.452502 | 2 | 11.765 |
| -7.21685 | 7.58085 | 10.46672 | 133.59093 | 0.181930 | 3 | 17.647 |
| -0.39951 | -2.54946 | 2.57959 | 261.09033 | 0.044838 | 4 | 23.529 |
| -6.60086 | 1.12377 | 6.69584 | 170.33823 | 0.116385 | 5 | 29.412 |
| -0.37126 | -1.93375 | 1.96906 | 259.13184 | 0.034226 | 6 | 35.294 |
| -3.01802 | 1.26790 | 3.27353 | 157.21230 | 0.056900 | 7 | 41.176 |
| -1.22734 | 0.33370 | 1.27189 | 164.78969 | 0.022108 | 8 | 47.059 |
| -2.15043 | 0.58092 | 2.22751 | 164.88297 | 0.038718 | 9 | 52.941 |
| -1.68793 | 0.11723 | 1.69200 | 176.02721 | 0.029410 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 10.40001 | | | | | C | |
| -13.60126 | 8.72264 | 16.15791 | 147.32750 | 1.000000 | 1 | 5.882 |
| -13.50563 | 1.12228 | 13.55218 | 175.24980 | 0.838733 | 2 | 11.765 |
| -7.46777 | 3.78345 | 8.37151 | 153.13158 | 0.518106 | 3 | 17.647 |
| -0.23746 | -1.37565 | 1.39600 | 260.20605 | 0.086397 | 4 | 23.529 |
| -1.28350 | 1.12500 | 1.70675 | 138.76511 | 0.105629 | 5 | 29.412 |
| -0.13567 | 0.12401 | 0.18381 | 137.57047 | 0.011376 | 6 | 35.294 |
| -1.44545 | 0.53163 | 1.54011 | 159.80604 | 0.095316 | 7 | 41.176 |
| -1.36708 | 1.85053 | 2.30073 | 126.45517 | 0.142390 | 8 | 47.059 |
| -0.97973 | -0.03765 | 0.98046 | 182.20056 | 0.060680 | 9 | 52.941 |
| -1.87905 | 0.83088 | 2.05455 | 156.14592 | 0.127155 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.03537 | | | | | C | |
| -60.58458 | 41.68105 | 73.53772 | 145.47278 | 1.000000 | 1 | 5.882 |
| 12.89931 | -23.25159 | 26.59000 | 299.02026 | 0.361583 | 2 | 11.765 |
| -12.81946 | 6.07001 | 14.18392 | 154.65249 | 0.192879 | 3 | 17.647 |
| -0.31191 | -2.43334 | 2.45325 | 262.69556 | 0.033360 | 4 | 23.529 |
| -8.53148 | 0.84658 | 8.36441 | 174.19098 | 0.113743 | 5 | 29.412 |
| 0.31695 | -1.95833 | 1.98381 | 279.19336 | 0.026977 | 6 | 35.294 |
| -3.91419 | 0.78614 | 3.99236 | 168.64359 | 0.054290 | 7 | 41.176 |
| -0.55161 | 0.41820 | 0.69222 | 142.83234 | 0.009413 | 8 | 47.059 |
| -1.95108 | 0.49361 | 2.01255 | 165.80252 | 0.027368 | 9 | 52.941 |
| -1.54375 | 0.53564 | 1.63403 | 160.86469 | 0.022220 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 13.01936 | | | | | 0 | |
| -9.95326 | 23.97389 | 25.95793 | 112.54686 | 1.000000 | 1 | 5.882 |
| -11.05273 | 5.22219 | 12.22433 | 154.71021 | 0.470928 | 2 | 11.765 |
| -6.15316 | 4.39426 | 7.56114 | 144.46761 | 0.291284 | 3 | 17.647 |
| 0.66037 | -0.72443 | 0.98029 | 312.35107 | 0.037763 | 4 | 23.529 |
| -1.24278 | -1.07079 | 1.64045 | 220.74881 | 0.063197 | 5 | 29.412 |
| -0.95968 | -0.33381 | 1.01608 | 199.17943 | 0.039143 | 6 | 35.294 |
| -2.14027 | 2.09472 | 2.99477 | 135.61629 | 0.115370 | 7 | 41.176 |
| -1.67002 | 2.33967 | 2.87455 | 125.51899 | 0.110739 | 8 | 47.059 |
| -0.21934 | 0.98774 | 1.01180 | 102.52031 | 0.038978 | 9 | 52.941 |
| -1.95131 | 1.41628 | 2.41112 | 144.02745 | 0.092885 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 1C3
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 45.81015 | | | | | 0 | |
| -51.85204 | 36.06535 | 63.16124 | 145.17972 | 1.000000 | 1 | 5.882 |
| 8.49995 | -13.96478 | 16.34795 | 301.32812 | 0.258829 | 2 | 11.765 |
| -14.46166 | 2.87283 | 14.74424 | 168.74439 | 0.233438 | 3 | 17.647 |
| -0.40403 | -1.17794 | 1.24531 | 251.00805 | 0.019716 | 4 | 23.529 |
| -7.15529 | -0.46961 | 7.17069 | 183.75562 | 0.113530 | 5 | 29.412 |
| 1.85577 | -1.37528 | 2.30982 | 323.45850 | 0.036570 | 6 | 35.294 |
| -2.97737 | 1.22223 | 3.21848 | 157.68147 | 0.050957 | 7 | 41.176 |
| -0.20010 | 0.15389 | 0.25243 | 142.43747 | 0.003997 | 8 | 47.059 |
| -0.85320 | 0.34531 | 0.92043 | 157.96545 | 0.014573 | 9 | 52.941 |
| -0.89795 | 0.49639 | 1.02602 | 151.06615 | 0.016244 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 1C3
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 31.42935 | | | | | 0 | |
| -0.07490 | 38.41766 | 38.41772 | 90.11177 | 1.000000 | 1 | 5.882 |
| -10.35427 | 7.84525 | 12.99073 | 142.84943 | 0.338144 | 2 | 11.765 |
| -4.14496 | 2.67936 | 4.93555 | 147.12084 | 0.128471 | 3 | 17.647 |
| -0.29877 | -1.26038 | 1.29530 | 256.66406 | 0.033716 | 4 | 23.529 |
| -0.93022 | -2.23499 | 2.42085 | 247.40254 | 0.063014 | 5 | 29.412 |
| -0.95427 | -0.07672 | 0.95735 | 184.59671 | 0.024919 | 6 | 35.294 |
| -1.56079 | 2.21445 | 2.70922 | 125.17690 | 0.070520 | 7 | 41.176 |
| -1.04488 | 0.39619 | 1.11744 | 159.23786 | 0.029087 | 8 | 47.059 |
| 0.57127 | 0.68027 | 0.85703 | 52.53809 | 0.022308 | 9 | 52.941 |
| -1.09015 | -0.35818 | 1.14749 | 198.18852 | 0.029869 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 37.52022 | | | | | 0 | |
| -33.24414 | 24.12709 | 41.07661 | 144.07957 | 1.000000 | 1 | 5.882 |
| 1.84022 | -5.13664 | 6.41344 | 306.78223 | 0.156134 | 2 | 11.765 |
| -12.47841 | 0.16761 | 12.47954 | 179.23042 | 0.303811 | 3 | 17.647 |
| -0.30981 | -0.77088 | 0.83081 | 248.10484 | 0.020226 | 4 | 23.529 |
| -4.88084 | -1.10850 | 5.00513 | 192.79549 | 0.121849 | 5 | 29.412 |
| 2.03698 | -0.94039 | 2.24357 | 335.21924 | 0.054619 | 6 | 35.294 |
| -1.66622 | 1.15985 | 2.03015 | 145.15846 | 0.049424 | 7 | 41.176 |
| -0.17965 | -0.01751 | 0.18051 | 185.56540 | 0.004394 | 8 | 47.059 |
| -0.24073 | 0.13640 | 0.27668 | 150.46416 | 0.006736 | 9 | 52.941 |
| -0.44314 | 0.27607 | 0.52210 | 148.07780 | 0.012710 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 35.07028 | | | | | 0 | |
| 4.53328 | 36.37717 | 36.65854 | 82.89647 | 1.000000 | 1 | 5.882 |
| -8.15404 | 7.14739 | 10.84313 | 138.76398 | 0.295787 | 2 | 11.765 |
| -2.57670 | 1.05218 | 2.78324 | 157.78764 | 0.075923 | 3 | 17.647 |
| -0.83257 | -1.28924 | 1.51794 | 236.73665 | 0.041408 | 4 | 23.529 |
| -0.70382 | -1.98207 | 2.10332 | 250.45033 | 0.057376 | 5 | 29.412 |
| -0.78107 | -0.04137 | 0.78216 | 183.03159 | 0.021336 | 6 | 35.294 |
| -0.72080 | 1.49743 | 1.66188 | 115.70427 | 0.045334 | 7 | 41.176 |
| -0.53906 | -0.71356 | 0.89429 | 232.93085 | 0.024395 | 8 | 47.059 |
| 0.57846 | 0.13433 | 0.59385 | 13.07345 | 0.016200 | 9 | 52.941 |
| -0.43618 | -1.33381 | 1.40331 | 251.89111 | 0.038281 | 10 | 58.824 |

## HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.40067 | | | | | 0 | |
| -28.41074 | 22.49011 | 36.23499 | 141.63466 | 1.000000 | 1 | 5.882 |
| 1.83670 | -0.68422 | 1.96001 | 339.56838 | 0.054092 | 2 | 11.765 |
| -15.27601 | -2.36138 | 15.45744 | 188.78728 | 0.426589 | 3 | 17.647 |
| -0.11516 | -1.99809 | 1.99941 | 266.69800 | 0.055175 | 4 | 23.529 |
| -5.04922 | -1.47405 | 5.25998 | 196.27443 | 0.145163 | 5 | 29.412 |
| 1.62910 | -1.47370 | 2.19676 | 317.86719 | 0.060625 | 6 | 35.294 |
| -1.23681 | 0.92113 | 1.54214 | 143.32277 | 0.042559 | 7 | 41.176 |
| -0.68265 | 0.11168 | 0.69173 | 170.70872 | 0.019090 | 8 | 47.059 |
| -0.61974 | -0.13086 | 0.63340 | 191.92348 | 0.017480 | 9 | 52.941 |
| -0.56679 | 0.15154 | 0.58670 | 165.03094 | 0.016192 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 40.01480 | | | | | 0 | |
| 4.57430 | 40.82634 | 41.12825 | 83.05324 | 1.000000 | 1 | 5.882 |
| -9.04131 | 7.55344 | 11.03254 | 136.79187 | 0.268247 | 2 | 11.765 |
| -2.83587 | 0.91361 | 2.95083 | 163.95449 | 0.071747 | 3 | 17.647 |
| -1.08719 | -0.86230 | 1.38784 | 218.41945 | 0.033739 | 4 | 23.529 |
| -1.19760 | -1.99849 | 2.32547 | 239.15227 | 0.056542 | 5 | 29.412 |
| -1.10125 | -0.74169 | 1.32776 | 213.95926 | 0.032283 | 6 | 35.294 |
| -0.19847 | 1.34432 | 1.35860 | 98.31477 | 0.033033 | 7 | 41.176 |
| -0.91373 | -0.73431 | 1.17223 | 218.78677 | 0.028502 | 8 | 47.059 |
| 0.21446 | -0.39090 | 0.44585 | 298.74829 | 0.010841 | 9 | 52.941 |
| -0.19839 | -1.65007 | 1.66148 | 256.42603 | 0.041273 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 14C
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 70.28828 | | | | | 0 | |
| -36.79198 | 35.74713 | 51.29820 | 135.82523 | 1.000000 | 1 | 5.882 |
| -1.34601 | 12.70073 | 12.77186 | 96.04961 | 0.248973 | 2 | 11.765 |
| -41.09692 | -13.69155 | 43.35249 | 198.56395 | 0.845107 | 3 | 17.647 |
| 0.92695 | -11.03794 | 11.07679 | 274.80029 | 0.215929 | 4 | 23.529 |
| -10.77989 | -3.35152 | 11.30798 | 197.24082 | 0.220436 | 5 | 29.412 |
| -0.14156 | -5.50427 | 5.50635 | 268.42261 | 0.107340 | 6 | 35.294 |
| -1.28464 | -0.23733 | 1.30618 | 190.46861 | 0.025462 | 7 | 41.176 |
| -3.35359 | 0.79270 | 3.44600 | 166.70094 | 0.067176 | 8 | 47.059 |
| -3.54716 | -1.38518 | 3.80802 | 201.33088 | 0.074233 | 9 | 52.941 |
| -2.05271 | -0.21649 | 2.06409 | 184.02039 | 0.040237 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 14C
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 77.08566 | | | | | 0 | |
| 3.70869 | 80.05197 | [illegible] 82 | 87.34729 | 1.000000 | 1 | 5.882 |
| -13.15063 | 14.42177 | [illegible] 32 | 132.36046 | 0.243547 | 2 | 11.765 |
| -7.73523 | 1.38827 | [illegible] 92 | 169.92526 | 0.098064 | 3 | 17.647 |
| -1.40735 | 0.84387 | [illegible] 96 | 149.05247 | 0.020477 | 4 | 23.529 |
| -4.44504 | -4.57777 | .66 | 210.11128 | 0.064120 | 5 | 29.412 |
| -4.03706 | -4.[illegible] | 232 | 229.44682 | 0.077200 | 6 | 35.294 |
| 1.32627 | 1.[illegible] | 87639 | 47.85129 | 0.024462 | 7 | 41.176 |
| -3.42681 | 0.[illegible] | 66430 | 171.79686 | 0.045725 | 8 | 47.059 |
| -1.75194 | -2.51073 | 3.08776 | 233.14725 | 0.036035 | 9 | 52.941 |
| -1.42601 | -2.64303 | 3.00319 | 241.65157 | 0.037475 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.32860 | | | | | 0 | |
| -4.49239 | 5.45085 | 7.06352 | 129.49417 | 0.189488 | 1 | 5.882 |
| -2.24158 | 19.72739 | 19.85432 | 96.48265 | 0.532617 | 2 | 11.765 |
| -34.37384 | -14.42252 | 37.27693 | 202.76186 | 1.000000 | 3 | 17.647 |
| 1.88316 | -12.35702 | 12.49968 | 278.66479 | 0.335320 | 4 | 23.529 |
| -6.06658 | -3.13235 | 6.82752 | 207.30858 | 0.183157 | 5 | 29.412 |
| -0.94237 | -4.80852 | 4.89999 | 258.91162 | 0.131448 | 6 | 35.294 |
| 0.24782 | -1.53883 | 1.55865 | 279.14844 | 0.041813 | 7 | 41.176 |
| -2.22962 | 0.00651 | 2.22963 | 179.83267 | 0.059813 | 8 | 47.059 |
| -2.63088 | -2.03627 | 3.32685 | 217.73941 | 0.089247 | 9 | 52.941 |
| -0.91830 | -0.84000 | 1.24453 | 222.45035 | 0.033396 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 50.03387 | | | | | 0 | |
| 3.29508 | 32.29955 | 32.46718 | 84.17502 | 1.000000 | 1 | 5.882 |
| -4.21268 | 10.06799 | 10.91381 | 112.70560 | 0.336149 | 2 | 11.765 |
| -5.02462 | -1.41881 | 5.22110 | 195.76811 | 0.1608.1 | 3 | 17.647 |
| 1.49436 | 0.68891 | 1.64590 | 24.74992 | 0.050682 | 4 | 23.529 |
| -2.86986 | 1.97797 | 3.48547 | 145.42451 | 0.107354 | 5 | 29.412 |
| -5.72095 | -2.99476 | 6.45739 | 207.63078 | 0.198890 | 6 | 35.294 |
| 1.02494 | -2.79114 | 2.97338 | 290.16382 | 0.091581 | 7 | 41.176 |
| -0.51951 | 0.90968 | 1.04757 | 119.73032 | 0.032265 | 8 | 47.059 |
| -1.67885 | -0.05356 | 1.67971 | 181.82739 | 0.051735 | 9 | 52.941 |
| -2.58568 | -1.60048 | 3.04093 | 211.75670 | 0.093662 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 50. OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 33.44855 | | | | | 0 | |
| 21.93697 | -27.33914 | 35.05229 | 308.74341 | 0.772549 | 1 | 5.882 |
| 0.37773 | 33.17526 | 33.17740 | 89.34761 | 0.731228 | 2 | 11.765 |
| -42.21053 | -16.64049 | 45.37216 | 201.51564 | 1.000000 | 3 | 17.647 |
| 3.07144 | -17.43996 | 17.70834 | 279.98828 | 0.390291 | 4 | 23.529 |
| -1.84570 | -5.07622 | 5.40135 | 250.01888 | 0.119045 | 5 | 29.412 |
| 1.00642 | -3.66011 | 3.79996 | 285.37451 | 0.083743 | 6 | 35.294 |
| 0.71767 | -2.81299 | 2.90310 | 284.31750 | 0.063984 | 7 | 41.176 |
| 0.09916 | -2.59146 | 2.74302 | 299.13525 | 0.060458 | 8 | 47.059 |
| 0.16884 | -2.52092 | 2.53455 | 273.81958 | 0.055861 | 9 | 52.941 |
| 0.45684 | -1.58142 | 1.64608 | 286.11279 | 0.036280 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 52.74775 | | | | | 0 | |
| 14.26289 | -7.09996 | 15.93233 | 333.53613 | 1.000000 | 1 | 5.882 |
| 0.14454 | 14.13611 | 14.13088 | 89.40416 | 0.886931 | 2 | 11.765 |
| -4.32366 | -8.08259 | 9.16637 | 241.85603 | 0.575331 | 3 | 17.647 |
| 0.60489 | -2.17124 | 6.95451 | 341.88782 | 0.436503 | 4 | 23.529 |
| -0.37194 | 0.17940 | 0.18785 | 92.68364 | 0.513914 | 5 | 29.412 |
| -0.79469 | 0.35117 | 0.76100 | 177.93823 | 0.012654 | 6 | 35.294 |
| 0.00616 | -0.95983 | 0.95987 | 270.42310 | 0.562370 | 7 | 41.176 |
| 4.72198 | -0.04877 | 4.72223 | 359.40820 | 0.296393 | 8 | 47.059 |
| -0.64589 | 3.55602 | 3.61420 | 100.29454 | 0.226847 | 9 | 52.941 |
| -4.19478 | -2.58212 | 4.92573 | 211.61510 | 0.309166 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 105
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 20.68338 | | | | | 0 | |
| 30.30534 | -26.32074 | 40.13969 | 319.02490 | 1.000000 | 1 | 5.882 |
| 2.71693 | 29.61052 | 29.73489 | 84.75745 | 0.740705 | 2 | 11.765 |
| -35.38669 | -9.73855 | 36.70227 | 195.38710 | 0.914383 | 3 | 17.647 |
| 0.55754 | -17.21732 | 17.22633 | 271.85474 | 0.429160 | 4 | 23.529 |
| 3.22170 | -3.33443 | 4.63654 | 314.01486 | 0.115511 | 5 | 29.412 |
| -0.49166 | 1.38638 | 1.47097 | 109.52644 | 0.036646 | 6 | 35.294 |
| -2.56476 | -4.14378 | 4.87329 | 238.24484 | 0.121408 | 7 | 41.176 |
| 4.29620 | -4.73532 | 6.39379 | 312.21631 | 0.159288 | 8 | 47.059 |
| 3.14693 | 1.72328 | 3.58787 | 28.78549 | 0.089385 | 9 | 52.941 |
| -2.63566 | 0.14002 | 2.63937 | 176.95891 | 0.065755 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 105
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.02710 | | | | | 0 | |
| 9.37480 | -1.51703 | 9.49675 | 350.80786 | 0.606782 | 1 | 5.882 |
| -8.32041 | 13.25610 | 15.65099 | 122.11519 | 1.000000 | 2 | 11.765 |
| -9.48449 | -10.89482 | 14.44481 | 229.93877 | 0.92. `3 | 3 | 17.647 |
| 7.25980 | -1.50946 | 7.41906 | 348.25439 | 0.472776 | 4 | 23.529 |
| -0.31914 | 4.55128 | 4.56245 | 94.01109 | 0.291512 | 5 | 29.412 |
| -3.03516 | -2.16593 | 3.72873 | 215.51222 | 0.238242 | 6 | 35.294 |
| 2.36808 | -2.42650 | 3.39053 | 314.30200 | 0.216634 | 7 | 41.176 |
| -1.09537 | 1.45727 | 1.82304 | 126.93063 | 0.116481 | 8 | 47.059 |
| -1.83723 | -3.09595 | 3.56536 | 238.98239 | 0.227804 | 9 | 52.941 |
| 2.45151 | -2.78237 | 3.70830 | 311.38281 | 0.236[illegible]7 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 18.47418 | | | | | 0 | |
| 36.10614 | -35.60971 | 50.71198 | 315.39648 | 1.000000 | 1 | 5.882 |
| 1.84218 | 32.26616 | 32.31870 | 86.73230 | 0.637299 | 2 | 11.765 |
| -30.32460 | -8.90773 | 39.34618 | 193.08484 | 0.775875 | 3 | 17.647 |
| -0.64239 | -18.60710 | 18.61818 | 268.02246 | 0.367136 | 4 | 23.529 |
| 3.54557 | -4.35654 | 5.61699 | 309.14038 | 0.110762 | 5 | 29.412 |
| 0.33680 | 0.91403 | 0.97411 | 69.77245 | 0.019209 | 6 | 35.294 |
| -1.61660 | -3.60166 | 3.94782 | 245.82706 | 0.077848 | 7 | 41.176 |
| 2.86567 | -2.97696 | 4.13212 | 313.90869 | 0.081482 | 8 | 47.059 |
| 1.14364 | -0.23469 | 1.16747 | 348.40283 | 0.023022 | 9 | 52.941 |
| -0.29406 | -2.35449 | 2.36816 | 263.04131 | 0.046698 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 51.90708 | | | | | 0 | |
| 27.71084 | 17.68695 | 32.88103 | 32.54129 | 1.000000 | 1 | 5.882 |
| -8.30545 | 26.14520 | 27.43268 | 107.62334 | 0.834301 | 2 | 11.765 |
| -24.38910 | -9.44769 | 26.15904 | 201.17503 | 0.795445 | 3 | 17.647 |
| 1.45917 | -0.60997 | 9.72012 | 278.63379 | 0.295615 | 4 | 23.529 |
| 5.17905 | -2.39200 | 5.70475 | 335.20947 | 0.173497 | 5 | 29.412 |
| 2.12325 | 1.11304 | 2.39730 | 27.66420 | 0.072908 | 6 | 35.294 |
| -0.24441 | 1.01080 | 1.03992 | 103.59314 | 0.031627 | 7 | 41.176 |
| -2.39709 | -2.30083 | 3.32263 | 223.82622 | 0.101050 | 8 | 47.059 |
| 2.72773 | -3.96813 | 4.81524 | 304.50488 | 0.146444 | 9 | 52.941 |
| 2.54163 | 1.74041 | 3.08041 | 34.40175 | 0.093683 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 7.63253 | | | | | 0 | |
| 18.21483 | -21.36061 | 28.07231 | 310.45508 | 1.000000 | 1 | 5.882 |
| 0.18081 | 15.87075 | 15.87178 | 89.34723 | 0.565389 | 2 | 11.765 |
| -18.65709 | -4.24101 | 19.13303 | 192.80649 | 0.681562 | 3 | 17.647 |
| -0.49706 | -8.70625 | 8.72043 | 266.73218 | 0.310642 | 4 | 23.529 |
| 1.21981 | -2.65359 | 2.92052 | 294.68726 | 0.104036 | 5 | 29.412 |
| 0.86986 | -0.43258 | 0.97148 | 333.55908 | 0.034607 | 6 | 35.294 |
| 0.25004 | -1.11043 | 1.13823 | 282.68994 | 0.040546 | 7 | 41.176 |
| 0.20490 | -0.21032 | 0.29363 | 314.25195 | 0.010460 | 8 | 47.059 |
| -0.76418 | -1.65711 | 1.82482 | 245.24321 | 0.065004 | 9 | 52.941 |
| 1.57688 | -2.50304 | 2.95834 | 302.21021 | 0.105383 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 43.60296 | | | | | 0 | |
| 22.07230 | 14.29366 | 26.29628 | 32.92642 | 1.000000 | 1 | 5.882 |
| -2.13914 | 17.74110 | 17.86958 | 96.87531 | 0.679548 | 2 | 11.765 |
| -17.09044 | -3.16912 | 17.29622 | 190.61163 | 0.657744 | 3 | 17.647 |
| -2.15551 | -8.35617 | 8.62971 | 255.53560 | 0.328172 | 4 | 23.529 |
| 5.08076 | -3.73383 | 6.30521 | 323.68799 | 0.239776 | 5 | 29.412 |
| 2.43820 | 2.64185 | 3.59502 | 47.29553 | 0.136712 | 6 | 35.294 |
| -1.78098 | 1.00840 | 2.04665 | 150.48125 | 0.077830 | 7 | 41.176 |
| -0.62751 | -3.11733 | 3.17986 | 258.61841 | 0.120924 | 8 | 47.059 |
| 3.46907 | -1.06962 | 3.82174 | 343.75000 | 0.145334 | 9 | 52.941 |
| 0.17013 | 2.99200 | 2.99683 | 86.74541 | 0.113964 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENC |
|---|---|---|---|---|---|---|
| 0.58641 | | | | | C | |
| 1.44866 | -1.73602 | 2.26105 | 309.84399 | 1.000000 | 1 | 5.882 |
| 0.00597 | 1.25646 | 1.25648 | 89.72763 | 0.555765 | 2 | 11.765 |
| -1.47482 | -0.33331 | 1.51201 | 192.73477 | 0.668720 | 3 | 17.647 |
| -0.04197 | -0.68441 | 0.68569 | 266.49097 | 0.303262 | 4 | 23.529 |
| 0.09101 | -0.21593 | 0.23433 | 292.85547 | 0.103636 | 5 | 29.412 |
| 0.07687 | -0.04398 | 0.08856 | 330.22363 | 0.039167 | 6 | 35.294 |
| 0.06160 | -0.08035 | 0.08634 | 291.46680 | 0.038188 | 7 | 41.176 |
| 0.00238 | -0.00208 | 0.00316 | 318.89575 | 0.001397 | 8 | 47.059 |
| -0.07590 | -0.14880 | 0.16704 | 242.97504 | 0.073878 | 9 | 52.941 |
| 0.14444 | -0.21384 | 0.25810 | 304.03174 | 0.114148 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 503 OSC CTR 163 TEST COND 46 COMP RUN 56.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.61043 | | | | | C | |
| 1.84710 | 1.70174 | 2.50362 | 33.04824 | 1.000000 | 1 | 5.882 |
| -0.14814 | 1.46303 | 1.47051 | 95.78192 | 0.667317 | 2 | 11.765 |
| -1.48699 | -0.23525 | 1.42652 | 189.49200 | 0.647352 | 3 | 17.647 |
| -0.20483 | -0.70465 | 0.73382 | 253.79128 | 0.333004 | 4 | 23.529 |
| 0.43231 | -0.32690 | 0.54199 | 322.99405 | 0.245955 | 5 | 29.412 |
| 0.21087 | 0.23342 | 0.31456 | 47.90482 | 0.142748 | 6 | 35.294 |
| -0.16028 | 0.08727 | 0.18250 | 151.43059 | 0.082817 | 7 | 41.176 |
| -0.04443 | -0.27012 | 0.27375 | 260.65869 | 0.124228 | 8 | 47.059 |
| 0.31791 | -0.07558 | 0.32677 | 346.62622 | 0.148288 | 9 | 52.941 |
| 0.00187 | 0.26228 | 0.26229 | 89.59186 | 0.119025 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 1.02227 | | | | | 0 | |
| -1.06534 | 1.51218 | 1.84976 | 125.16490 | 1.000000 | 1 | 5.882 |
| 0.20187 | -1.38766 | 1.40227 | 278.27686 | 0.758080 | 2 | 11.765 |
| 0.17603 | 0.51559 | 0.54481 | 71.14908 | 0.294531 | 3 | 17.647 |
| -0.18242 | -0.32091 | 0.36913 | 240.38310 | 0.199557 | 4 | 23.529 |
| -0.00534 | -0.04338 | 0.04371 | 262.97632 | 0.023628 | 5 | 29.412 |
| 0.10247 | 0.03345 | 0.10779 | 18.08087 | 0.058271 | 6 | 35.294 |
| -0.09545 | 0.22969 | 0.22975 | 91.35864 | 0.124205 | 7 | 41.176 |
| -0.11071 | 0.16919 | 0.20220 | 123.19882 | 0.109310 | 8 | 47.059 |
| -0.11261 | 0.11990 | 0.16449 | 133.20335 | 0.088925 | 9 | 52.941 |
| -0.08544 | 0.02180 | 0.08818 | 165.68347 | 0.047668 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 29
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.32009 | | | | | 0 | |
| -1.05820 | -1.10651 | 1.53106 | 226.27846 | 1.000000 | 1 | 5.882 |
| -1.21612 | 0.11666 | 1.22170 | 174.52061 | 0.797944 | 2 | 11.765 |
| -0.43850 | 0.32012 | 0.54292 | 143.86926 | 0.354607 | 3 | 17.647 |
| -0.08873 | 0.01958 | 0.09086 | 167.55486 | 0.059346 | 4 | 23.529 |
| 0.04482 | 0.37959 | 0.38223 | 83.26649 | 0.249648 | 5 | 29.412 |
| 0.15498 | -0.18739 | 0.24317 | 309.59180 | 0.158825 | 6 | 35.294 |
| 0.00059 | -0.12505 | 0.12505 | 270.26929 | 0.081674 | 7 | 41.176 |
| 0.09432 | -0.22007 | 0.23943 | 293.19849 | 0.156380 | 8 | 47.059 |
| -0.16898 | -0.14042 | 0.21971 | 219.72525 | 0.143503 | 9 | 52.941 |
| -0.03487 | 0.00622 | 0.03542 | 169.88896 | 0.023137 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 4.92037 | | | | | 0 | |
| -5.37846 | 7.35223 | 9.10950 | 126.18706 | 1.000000 | 1 | 5.882 |
| 1.00529 | -6.74122 | 6.81576 | 278.48169 | 0.746284 | 2 | 11.765 |
| 0.75998 | 2.48218 | 2.59592 | 72.97668 | 0.284968 | 3 | 17.647 |
| -0.88702 | -1.52815 | 1.76693 | 239.86682 | 0.193966 | 4 | 23.529 |
| -0.09410 | -0.23414 | 0.25234 | 248.10402 | 0.027701 | 5 | 29.412 |
| 0.49111 | 0.15233 | 0.51419 | 17.23311 | 0.056446 | 6 | 35.294 |
| -0.07861 | 1.09226 | 1.09454 | 93.69865 | 0.120154 | 7 | 41.176 |
| -0.52399 | 0.80088 | 0.95707 | 123.19530 | 0.105063 | 8 | 47.059 |
| -0.55834 | 0.57979 | 0.80492 | 133.92023 | 0.088361 | 9 | 52.941 |
| -0.41849 | 0.10798 | 0.43220 | 165.53180 | 0.047445 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 36
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -1.29529 | | | | | 0 | |
| -5.03662 | -5.19485 | 7.23560 | 225.88597 | 1.000000 | 1 | 5.882 |
| -5.82976 | 0.51897 | 5.85281 | 174.91290 | 0.808891 | 2 | 11.765 |
| -2.11056 | 1.51628 | 2.59876 | 144.30563 | 0.359163 | 3 | 17.647 |
| -0.41466 | 0.03865 | 0.41646 | 174.67516 | 0.057557 | 4 | 23.529 |
| 0.24184 | 1.77201 | 1.78843 | 82.22847 | 0.247171 | 5 | 29.412 |
| 0.74916 | -0.90329 | 1.17352 | 309.67114 | 0.162187 | 6 | 35.294 |
| 0.02777 | -0.60811 | 0.60875 | 272.61490 | 0.084132 | 7 | 41.176 |
| 0.42731 | -1.08036 | 1.16180 | 291.56066 | 0.160567 | 8 | 47.059 |
| -0.80791 | -0.72094 | 1.08251 | 221.75821 | 0.149609 | 9 | 52.941 |
| -0.17479 | -0.02435 | 0.17642 | 187.93489 | 0.024382 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 12.91934 | | | | | 0 | |
| -14.33872 | 18.39221 | 23.32106 | 127.94031 | 1.000000 | 1 | 5.882 |
| 2.62083 | -16.83836 | 17.04109 | 278.84692 | 0.730717 | 2 | 11.765 |
| 1.47457 | 6.09968 | 6.27539 | 76.40970 | 0.269087 | 3 | 17.647 |
| -2.21929 | -3.68002 | 4.29741 | 238.90737 | 0.184272 | 4 | 23.529 |
| -0.53843 | -0.68998 | 0.87449 | 231.99665 | 0.037498 | 5 | 29.412 |
| 1.19789 | 0.39521 | 1.26313 | 15.64321 | 0.053305 | 6 | 35.294 |
| -0.37292 | 2.62355 | 2.64992 | 98.09019 | 0.113628 | 7 | 41.176 |
| -1.24720 | 1.90678 | 2.27844 | 123.18813 | 0.097699 | 8 | 47.059 |
| -1.44497 | 1.43627 | 2.03735 | 135.17299 | 0.087361 | 9 | 52.941 |
| -1.06867 | 0.27890 | 1.09472 | 165.26773 | 0.047027 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 45
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -2.07902 | | | | | 0 | |
| -12.11716 | -12.17204 | 17.17509 | 225.12944 | 1.000000 | 1 | 5.882 |
| -14.21415 | 1.00367 | 14.25540 | 175.64327 | 0.830004 | 2 | 11.765 |
| -5.18431 | 3.61431 | 6.31983 | 145.11725 | 0.367965 | 3 | 17.647 |
| -0.96289 | -3.15494 | 0.97527 | 189.14091 | 0.056784 | 4 | 23.529 |
| 0.71144 | 4.10593 | 4.16471 | 80.16859 | 0.242602 | 5 | 29.412 |
| 1.85475 | -2.22500 | 2.89667 | 309.81445 | 0.168655 | 6 | 35.294 |
| 0.18028 | -1.52190 | 1.53254 | 276.75586 | 0.089230 | 7 | 41.176 |
| 0.92995 | -2.74891 | 2.90194 | 288.69043 | 0.168962 | 8 | 47.059 |
| -1.95737 | -1.97358 | 2.77962 | 225.23618 | 0.161840 | 9 | 52.941 |
| -0.46010 | -0.30384 | 0.55137 | 213.44012 | 0.032103 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 31.22418 | | | | | 0 | |
| -41.64433 | 43.43155 | 60.17099 | 133.79699 | 1.000000 | 1 | 5.882 |
| 7.24799 | -39.83675 | 40.49986 | 280.31104 | 0.672927 | 2 | 11.765 |
| -0.85450 | 13.72314 | 13.72325 | 90.22762 | 0.228071 | 3 | 17.647 |
| -5.26744 | -7.46648 | 9.13752 | 234.79785 | 0.151859 | 4 | 23.529 |
| -3.75792 | -2.30626 | 4.45149 | 212.41428 | 0.073981 | 5 | 29.412 |
| 2.50311 | 0.61553 | 2.57760 | 13.81536 | 0.042839 | 6 | 35.294 |
| -2.69486 | 5.29049 | 5.91926 | 116.64836 | 0.098374 | 7 | 41.176 |
| -2.32609 | 3.72406 | 4.39082 | 121.98941 | 0.072972 | 8 | 47.059 |
| -3.89984 | 3.40483 | 5.13932 | 138.90867 | 0.085412 | 9 | 52.941 |
| -2.66967 | 0.78272 | 2.78205 | 163.65933 | 0.046236 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 58
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 5.19123 | | | | | 0 | |
| -24.65364 | -22.67747 | 33.49745 | 222.60893 | 1.000000 | 1 | 5.882 |
| -30.29180 | 0.41223 | 30.29459 | 179.21920 | 0.903191 | 2 | 11.765 |
| -11.49929 | 6.99427 | 13.49933 | 148.69981 | 0.402852 | 3 | 17.647 |
| -1.54675 | -2.66415 | 3.08060 | 239.86147 | 0.091905 | 4 | 23.529 |
| 2.75050 | 6.92372 | 7.49005 | 68.19412 | 0.223406 | 5 | 29.412 |
| 4.19858 | -4.91262 | 6.44239 | 310.51880 | 0.192171 | 6 | 35.294 |
| 1.41999 | -3.74223 | 4.00243 | 290.77304 | 0.119405 | 7 | 41.176 |
| 1.09708 | -6.97398 | 7.05975 | 278.93994 | 0.210735 | 8 | 47.059 |
| -0.07464 | -6.22271 | 7.43008 | 238.78311 | 0.222049 | 9 | 52.941 |
| -1.28281 | -2.93747 | 3.20536 | 246.40883 | 0.095690 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 5C COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.34433 | | | | | 0 | |
| -52.87590 | 40.62105 | 66.55617 | 142.60387 | 1.000000 | 1 | 5.882 |
| 9.40775 | -36.79198 | 37.75832 | 282.99048 | 0.567315 | 2 | 11.765 |
| -6.77375 | 11.13494 | 13.03344 | 121.31340 | 0.195826 | 3 | 17.647 |
| -4.51702 | -4.68231 | 6.78978 | 223.59940 | 0.102016 | 4 | 23.529 |
| -9.26355 | -3.81083 | 9.99993 | 204.75732 | 0.136726 | 5 | 29.412 |
| 1.80825 | -0.06873 | 1.80996 | 357.82300 | 0.027188 | 6 | 35.294 |
| -5.62375 | 3.20704 | 6.47392 | 150.30530 | 0.097270 | 7 | 41.176 |
| -1.12598 | 1.95079 | 2.25235 | 119.99428 | 0.033841 | 8 | 47.059 |
| -4.35406 | 2.49799 | 5.28966 | 145.47507 | 0.079477 | 9 | 52.941 |
| -2.72213 | 0.84731 | 2.86309 | 161.94594 | 0.043018 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 73
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 5C COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 23.32115 | | | | | 0 | |
| -13.35819 | -8.43341 | 17.52130 | 208.77184 | 0.780351 | 1 | 5.882 |
| -22.23169 | -3.14548 | 22.45309 | 188.05310 | 1.000000 | 2 | 11.765 |
| -9.21690 | 1.66842 | 9.92011 | 158.29695 | 0.441815 | 3 | 17.647 |
| -0.22269 | -6.53007 | 6.53389 | 268.04663 | 0.291007 | 4 | 23.529 |
| 4.31326 | 1.26212 | 4.49413 | 16.31020 | 0.200156 | 5 | 29.412 |
| 3.59479 | -4.30413 | 5.38104 | 311.91650 | 0.239657 | 6 | 35.294 |
| 3.09790 | -3.54969 | 4.71125 | 311.11353 | 0.209826 | 7 | 41.176 |
| -1.14901 | -7.25325 | 7.34962 | 261.00562 | 0.327332 | 8 | 47.059 |
| -2.79247 | -8.53277 | 8.97820 | 251.87538 | 0.399865 | 9 | 52.941 |
| -1.55851 | -6.64461 | 6.82494 | 256.79956 | 0.303964 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 5C COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 19.63641 | | | | | 0 | |
| -66.99539 | 44.15057 | 80.15149 | 146.57542 | 1.000000 | 1 | 5.882 |
| 8.48787 | -36.45779 | 37.43271 | 283.10571 | 0.467024 | 2 | 11.765 |
| -13.94898 | 7.06070 | 15.63418 | 153.15237 | 0.195058 | 3 | 17.647 |
| -4.99530 | -3.91096 | 5.83257 | 211.07983 | 0.072769 | 4 | 23.529 |
| -14.68498 | -7.47105 | 16.47620 | 206.96490 | 0.205563 | 5 | 29.412 |
| 2.09126 | -3.98387 | 4.49940 | 297.69629 | 0.056136 | 6 | 35.294 |
| -7.63081 | 1.52359 | 7.78121 | 168.70900 | 0.097081 | 7 | 41.176 |
| -1.79072 | -0.04926 | 1.79139 | 181.57579 | 0.022350 | 8 | 47.059 |
| -5.14196 | 0.85507 | 5.21257 | 170.55847 | 0.065034 | 9 | 52.941 |
| -2.54307 | 0.49519 | 2.57359 | 171.16690 | 0.032109 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 88
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 5C COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 36.41603 | | | | | 0 | |
| -7.34622 | 15.92426 | 17.53706 | 114.76505 | 0.815819 | 1 | 5.882 |
| -21.40314 | -1.99991 | 21.49626 | 185.33556 | 1.000000 | 2 | 11.765 |
| -7.45888 | 1.80807 | 7.67489 | 166.37399 | 0.357034 | 3 | 17.647 |
| -0.79617 | -8.34970 | 8.38387 | 264.82544 | 0.390015 | 4 | 23.529 |
| 1.72648 | -3.43732 | 5.06970 | 317.31128 | 0.235841 | 5 | 29.412 |
| 4.03762 | -4.52984 | 6.06810 | 311.71191 | 0.282286 | 6 | 35.294 |
| 4.10653 | -1.27176 | 4.35630 | 343.02588 | 0.202654 | 7 | 41.176 |
| -4.79092 | -7.11956 | 8.58143 | 236.06245 | 0.399206 | 8 | 47.059 |
| -7.27252 | -9.92813 | 10.28944 | 256.99756 | 0.479010 | 9 | 52.941 |
| -1.84032 | -8.24934 | 8.46096 | 257.15942 | 0.393602 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 3.62889 | | | | | 0 | |
| -52.26813 | 35.07866 | 62.94814 | 146.13330 | 1.000000 | 1 | 5.882 |
| 3.37762 | -22.28217 | 22.53665 | 278.61938 | 0.358019 | 2 | 11.765 |
| -15.18576 | -1.37698 | 15.24806 | 185.18118 | 0.242232 | 3 | 17.647 |
| -3.32501 | -1.53367 | 3.66167 | 204.76164 | 0.058170 | 4 | 23.529 |
| -15.88649 | -9.73480 | 18.63187 | 211.49879 | 0.295988 | 5 | 29.412 |
| 7.64188 | -9.06371 | 9.44089 | 286.25024 | 0.149979 | 6 | 35.294 |
| -4.82345 | -0.12694 | 4.82517 | 181.50752 | 0.076652 | 7 | 41.176 |
| -3.36239 | -1.92733 | 3.87560 | 209.82146 | 0.061568 | 8 | 47.059 |
| -3.78035 | -3.09969 | 4.88866 | 219.34997 | 0.077662 | 9 | 52.941 |
| -0.95513 | -0.87481 | 1.29521 | 227.48656 | 0.020576 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 103
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.00105 | | | | | 0 | |
| 1.28540 | -1.45064 | 41.47055 | 88.22374 | 1.000000 | 1 | 5.882 |
| -18.98259 | 5.11222 | 19.65892 | 164.92722 | 0.474045 | 2 | 11.765 |
| -3.32245 | 0.40157 | 3.44260 | 164.81804 | 0.083013 | 3 | 17.647 |
| -2.75215 | -4.08082 | 4.92213 | 236.00385 | 0.118690 | 4 | 23.529 |
| -0.69562 | -5.04904 | 5.09673 | 262.15552 | 0.122900 | 5 | 29.412 |
| 3.66402 | -4.54648 | 5.83914 | 308.86523 | 0.140802 | 6 | 35.294 |
| 2.63511 | 3.18584 | 4.13426 | 50.40298 | 0.099691 | 7 | 41.176 |
| -7.14865 | -3.48921 | 7.95473 | 206.01669 | 0.191816 | 8 | 47.059 |
| -1.72406 | -5.84961 | 6.09838 | 253.57823 | 0.147053 | 9 | 52.941 |
| -1.47542 | -3.89014 | 4.16053 | 249.22952 | 0.100325 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.07664 | | | | | 0 | |
| -30.27376 | 21.74968 | 37.27664 | 144.30528 | 1.000000 | 1 | 5.882 |
| -0.22273 | -8.54995 | 8.55285 | 268.50781 | 0.229442 | 2 | 11.765 |
| -12.52398 | -5.40552 | 13.64074 | 203.34567 | 0.365932 | 3 | 17.647 |
| -1.67336 | -0.79761 | 1.85373 | 205.48499 | 0.049729 | 4 | 23.529 |
| -12.19158 | -8.27398 | 14.73408 | 214.16330 | 0.395263 | 5 | 29.412 |
| 2.59973 | -9.24269 | 9.60135 | 285.70996 | 0.257570 | 6 | 35.294 |
| -1.69298 | 0.67462 | 1.82244 | 201.72649 | 0.048890 | 7 | 41.176 |
| -3.04927 | -2.11718 | 3.71221 | 214.77316 | 0.099585 | 8 | 47.059 |
| -1.57934 | -4.04707 | 4.50517 | 243.93761 | 0.120858 | 9 | 52.941 |
| 0.19693 | -1.35196 | 1.36627 | 278.28735 | 0.036651 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 115
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 17.96631 | | | | | 0 | |
| 4.27180 | 43.65617 | 43.86467 | 84.41126 | 1.000000 | 1 | 5.882 |
| -13.63906 | 8.01119 | 15.81781 | 149.57132 | 0.360605 | 2 | 11.765 |
| -0.76284 | 0.37818 | 0.85144 | 153.62984 | 0.019411 | 3 | 17.647 |
| -2.96893 | -0.62455 | 3.03391 | 191.87959 | 0.069165 | 4 | 23.529 |
| -2.82317 | -4.26427 | 5.11413 | 236.49333 | 0.116589 | 5 | 29.412 |
| 2.43454 | -3.51070 | 4.27123 | 304.74385 | 0.097386 | 6 | 35.294 |
| 1.11222 | 4.10140 | 4.24953 | 74.82729 | 0.096878 | 7 | 41.176 |
| -6.04511 | -0.88752 | 6.10991 | 188.35229 | 0.139290 | 8 | 47.059 |
| -1.16764 | -2.23433 | 2.52103 | 242.40880 | 0.057473 | 9 | 52.941 |
| -1.03111 | -0.63253 | 1.20966 | 211.52669 | 0.027577 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 494 CSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | C | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.32442 | | | | | 0 | |
| -23.54164 | 19.00632 | 30.25638 | 141.08438 | 1.000000 | 1 | 5.882 |
| -1.49641 | -1.41338 | 2.05837 | 223.36548 | 0.068031 | 2 | 11.765 |
| -14.75849 | -7.69308 | 16.64320 | 207.53143 | 0.550073 | 3 | 17.647 |
| -0.87519 | -0.85580 | 1.22407 | 224.35809 | 0.040457 | 4 | 23.529 |
| -11.57042 | -7.66588 | 13.87949 | 213.52611 | 0.458729 | 5 | 29.412 |
| 3.47870 | -9.74407 | 10.34641 | 289.64697 | 0.341958 | 6 | 35.294 |
| 0.39262 | -0.79298 | 0.88477 | 296.32910 | 0.029242 | 7 | 41.176 |
| -1.76795 | -1.84013 | 2.55181 | 226.14603 | 0.084340 | 8 | 47.059 |
| -1.09037 | -3.79830 | 3.95170 | 253.98251 | 0.130607 | 9 | 52.941 |
| 0.90813 | -1.88632 | 2.09354 | 295.70752 | 0.069193 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 125
MODEL XH-51A SHIP 1002C TEST 494 CSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 28.33733 | | | | | 0 | |
| 3.77386 | 51.28983 | 51.42847 | 85.79175 | 1.000000 | 1 | 5.882 |
| -12.12153 | 9.91546 | 15.66052 | 140.71616 | 0.304511 | 2 | 11.765 |
| -0.36529 | 0.81176 | 0.89655 | 114.04431 | 0.017433 | 3 | 17.647 |
| -3.18501 | 0.23605 | 3.19375 | 175.78144 | 0.062101 | 4 | 23.529 |
| -3.32239 | -4.96515 | 5.97419 | 236.21187 | 0.116165 | 5 | 29.412 |
| 2.02081 | -3.44243 | 3.99174 | 300.41436 | 0.077617 | 6 | 35.294 |
| 1.02233 | 3.18542 | 3.34564 | 72.20744 | 0.065054 | 7 | 41.176 |
| -5.07999 | -0.33303 | 5.09089 | 183.75079 | 0.098990 | 8 | 47.059 |
| -1.29221 | -1.65601 | 2.10052 | 232.03452 | 0.040843 | 9 | 52.941 |
| -1.30441 | -0.37799 | 1.35807 | 196.16035 | 0.026407 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 44.53578 | | | | | 0 | |
| -24.77600 | 26.57936 | 36.33609 | 132.98889 | 0.848955 | 1 | 5.882 |
| -4.22693 | 19.97797 | 20.42023 | 101.94647 | 0.477098 | 2 | 11.765 |
| -38.71286 | -18.25476 | 42.80095 | 205.24586 | 1.000000 | 3 | 17.647 |
| -0.00757 | -3.09222 | 3.09223 | 269.85962 | 0.072247 | 4 | 23.529 |
| -18.25427 | -10.27751 | 20.94862 | 209.38033 | 0.489443 | 5 | 29.412 |
| 9.92884 | -15.37035 | 18.29834 | 302.86133 | 0.427522 | 6 | 35.294 |
| 6.53946 | -0.60825 | 6.56768 | 354.68604 | 0.153447 | 7 | 41.176 |
| 3.71278 | -0.89270 | 3.81859 | 346.48067 | 0.089217 | 8 | 47.059 |
| 0.78791 | -2.51257 | 2.63321 | 287.41044 | 0.061522 | 9 | 52.941 |
| 5.52462 | -4.38714 | 5.62760 | 308.77832 | 0.131483 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 140
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 99.40358 | | | | | 0 | |
| 0.63044 | 103.99137 | 103.99319 | 89.65262 | 1.000000 | 1 | 5.882 |
| -16.43491 | 20.67212 | 26.40913 | 128.48570 | 0.253951 | 2 | 11.765 |
| -2.23228 | 1.65905 | 2.78128 | 143.37991 | 0.026745 | 3 | 17.647 |
| -3.44735 | 0.27536 | 3.45833 | 175.43309 | 0.033255 | 4 | 23.529 |
| -3.57658 | -11.09030 | 11.99749 | 247.57574 | 0.115368 | 5 | 29.412 |
| 1.14129 | -5.66499 | 5.77881 | 281.39063 | 0.055569 | 6 | 35.294 |
| 2.60701 | -2.52582 | 3.62991 | 315.90601 | 0.034905 | 7 | 41.176 |
| -3.05146 | -1.51688 | 3.40769 | 206.43192 | 0.032768 | 8 | 47.059 |
| -3.00107 | -3.84164 | 4.87489 | 232.00319 | 0.046877 | 9 | 52.941 |
| -4.20764 | -3.68493 | 5.59312 | 221.21089 | 0.053783 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 26.71735 | | | | | 0 | |
| 3.88854 | -0.87394 | 3.94652 | 347.20581 | 0.102285 | 1 | 5.882 |
| -5.48844 | 30.86880 | 31.40576 | 100.80670 | 0.813964 | 2 | 11.765 |
| -34.74216 | -16.78357 | 38.58374 | 205.78469 | 1.000000 | 3 | 17.647 |
| -0.94861 | -4.71596 | 4.80953 | 258.62451 | 0.124652 | 4 | 23.529 |
| -8.26029 | -5.94744 | 10.95199 | 212.27083 | 0.283850 | 5 | 29.412 |
| 7.12516 | -5.11793 | 8.77275 | 324.31055 | 0.227369 | 6 | 35.294 |
| 3.45718 | 0.57842 | 3.50524 | 9.49811 | 0.090847 | 7 | 41.176 |
| 4.54703 | 0.34759 | 4.56028 | 4.37027 | 0.118152 | 8 | 47.059 |
| 1.85433 | 1.04262 | 2.12735 | 29.34734 | 0.055136 | 9 | 52.941 |
| 3.14764 | -1.55631 | 3.51137 | 333.49043 | 0.091007 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 157
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 25.56729 | | | | | 0 | |
| 4.33601 | 37.95419 | 38.38045 | 40.50087 | 1.000000 | 1 | 5.882 |
| -2.58009 | 15.27609 | 15.56406 | 101.03882 | 0.405520 | 2 | 11.765 |
| -1.71357 | -3.95717 | 4.31225 | 246.58562 | 0.112355 | 3 | 17.647 |
| 2.82956 | 1.63750 | 3.26920 | 30.05861 | 0.085179 | 4 | 23.529 |
| -3.40466 | -6.37299 | 7.22541 | 241.88745 | 0.188258 | 5 | 29.412 |
| -3.14179 | -2.46287 | 3.99207 | 218.09309 | 0.104013 | 6 | 35.294 |
| -0.46182 | -6.40773 | 6.42433 | 265.87939 | 0.167386 | 7 | 41.176 |
| 1.31285 | -2.64581 | 2.95362 | 296.39067 | 0.076956 | 8 | 47.059 |
| -1.09114 | -1.43167 | 1.80001 | 232.68977 | 0.046899 | 9 | 52.941 |
| -3.27755 | -2.15494 | 3.92246 | 213.32314 | 0.102199 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 27.71921 | | | | | 0 | |
| 26.77766 | -33.76879 | 44.36757 | 310.43750 | 0.839839 | 1 | 5.882 |
| -10.74827 | 48.77779 | 49.94794 | 102.42671 | 0.945470 | 2 | 11.765 |
| -46.96104 | -26.15771 | 52.82866 | 207.26077 | 1.000000 | 3 | 17.647 |
| -8.77137 | -9.27580 | 11.48442 | 233.47039 | 0.217390 | 4 | 23.529 |
| -9.82159 | -12.28484 | 15.72832 | 231.35912 | 0.297723 | 5 | 29.412 |
| 7.03835 | 0.24629 | 7.04266 | 2.00468 | 0.133311 | 6 | 35.294 |
| -4.72098 | 2.48899 | 5.53479 | 148.53561 | 0.104769 | 7 | 41.176 |
| -0.44469 | -1.07239 | 1.15843 | 247.45568 | 0.021924 | 8 | 47.059 |
| 1.79227 | 0.23167 | 1.80718 | 7.36517 | 0.034208 | 9 | 52.941 |
| 3.21374 | 2.41690 | 4.02097 | 36.94946 | 0.076110 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 172
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -101.82155 | | | | | 0 | |
| 28.17485 | -23.20447 | 36.46167 | 320.47555 | 1.000000 | 1 | 5.882 |
| -2.18533 | 20.81431 | 20.93367 | 95.99723 | 0.574128 | 2 | 11.765 |
| -1.64733 | -22.24014 | 22.31673 | 265.25146 | 0.612060 | 3 | 17.647 |
| 15.14434 | 5.59013 | 16.14687 | 20.25534 | 0.442345 | 4 | 23.529 |
| -7.39335 | 0.36693 | 7.40245 | 177.15871 | 0.203020 | 5 | 29.412 |
| -11.19510 | -0.79341 | 11.22122 | 184.05638 | 0.307809 | 6 | 35.294 |
| -6.06325 | -4.05703 | 10.08358 | 233.03499 | 0.276553 | 7 | 41.176 |
| 1.96508 | -4.75379 | 5.13632 | 292.29269 | 0.140869 | 8 | 47.059 |
| 1.36733 | 3.68261 | 3.92852 | 69.69873 | 0.107689 | 9 | 52.941 |
| -3.94828 | 1.95927 | 4.40724 | 153.61951 | 0.120873 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.12599 | | | | | 0 | |
| 31.04383 | -35.47913 | 47.14293 | 311.18506 | 1.000000 | 1 | 5.882 |
| -0.47762 | 37.08832 | 37.09071 | 90.65289 | 0.786771 | 2 | 11.765 |
| -33.12909 | -8.53293 | 34.21033 | 194.44351 | 0.725672 | 3 | 17.647 |
| -11.81068 | -6.97919 | 13.71865 | 210.57974 | 0.291001 | 4 | 23.529 |
| -8.46010 | -16.06310 | 18.15477 | 242.22500 | 0.385101 | 5 | 29.412 |
| 10.78807 | -0.17620 | 10.78951 | 359.06421 | 0.228868 | 6 | 35.294 |
| -[illegible].15868 | 7.33890 | 8.43529 | 119.53868 | 0.178930 | 7 | 41.176 |
| -[illegible]22938 | -1.12693 | 5.33379 | 192.19740 | 0.113141 | 8 | 47.059 |
| [illegible].69462 | -1.64438 | 2.36130 | 315.86182 | 0.050088 | 9 | 52.941 |
| 1.48009 | 3.67161 | 3.95871 | 68.04478 | 0.083972 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 185
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -25.21188 | | | | | 0 | |
| 14.01236 | -1.43671 | 14.08582 | 354.14575 | 0.342269 | 1 | 5.882 |
| -32.50604 | 17.33258 | 36.83830 | 151.93298 | 0.895111 | 2 | 11.765 |
| -7.54180 | -40.45808 | 41.15580 | 259.44043 | 1.000000 | 3 | 17.647 |
| 27.35129 | 3.50225 | 27.57458 | 7.29685 | 0.670018 | 4 | 23.529 |
| -5.46216 | 14.95552 | 15.92177 | 110.06363 | 0.386873 | 5 | 29.412 |
| -16.90182 | 0.00290 | 16.90181 | 179.99016 | 0.410687 | 6 | 35.294 |
| -2.91318 | -11.44618 | 11.83046 | 255.74460 | 0.287461 | 7 | 41.176 |
| 7.23618 | -2.22939 | 7.57182 | 342.87646 | 0.183983 | 8 | 47.059 |
| 0.53306 | 7.75460 | 7.77290 | 86.06754 | 0.188869 | 9 | 52.941 |
| -7.42985 | -0.60461 | 7.44762 | 184.65651 | 0.180965 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -2.92328 | | | | | 0 | |
| 31.38957 | -43.36964 | 53.53719 | 305.89575 | 1.000000 | 1 | 5.882 |
| -2.19642 | 33.60706 | 33.67874 | 93.73936 | 0.629072 | 2 | 11.765 |
| -30.05264 | -9.68086 | 31.57339 | 197.85530 | 0.589747 | 3 | 17.647 |
| -13.73214 | -3.58249 | 14.19175 | 194.62160 | 0.265082 | 4 | 23.529 |
| -12.93602 | -20.82664 | 24.51712 | 238.15435 | 0.457946 | 5 | 29.412 |
| 16.14580 | -4.47978 | 16.75574 | 344.49292 | 0.312974 | 6 | 35.294 |
| 0.17764 | 12.00311 | 12.00442 | 89.15204 | 0.224226 | 7 | 41.176 |
| -7.33447 | 3.01799 | 7.93112 | 157.63377 | 0.148142 | 8 | 47.059 |
| -1.13928 | -1.46117 | 1.85037 | 232.35388 | 0.034562 | 9 | 52.941 |
| 0.32972 | 3.45175 | 3.46708 | 84.68931 | 0.064760 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 195
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 30.25787 | | | | | 0 | |
| 26.37395 | 26.09116 | 37.09895 | 44.69116 | 0.741522 | 1 | 5.882 |
| -37.46416 | 29.58371 | 47.73634 | 141.70349 | 0.954138 | 2 | 11.765 |
| -23.41229 | -44.21481 | 50.03084 | 242.09816 | 1.000000 | 3 | 17.647 |
| 27.33159 | -9.43629 | 28.91467 | 340.95264 | 0.577937 | 4 | 23.529 |
| 8.73543 | 17.78687 | 19.81615 | 63.84352 | 0.396079 | 5 | 29.412 |
| -20.39178 | 13.26781 | 24.32616 | 146.95016 | 0.486263 | 6 | 35.294 |
| -9.35320 | -17.67023 | 19.99297 | 242.10660 | 0.399613 | 7 | 41.176 |
| 16.89436 | -4.04403 | 17.34295 | 340.31494 | 0.358638 | 8 | 47.059 |
| 3.41792 | 16.35684 | 16.71011 | 78.19730 | 0.333998 | 9 | 52.941 |
| -12.28720 | 2.51673 | 12.54230 | 168.42450 | 0.250691 | 10 | 58.824 |

# HARMONIC COMPONENTS OF AIRLOADS AND PITCHING MOMENTS

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -1.35367 | | | | | 0 | |
| 14.17350 | -23.52174 | 27.46198 | 301.07178 | 1.000000 | 1 | 5.882 |
| -3.38696 | 14.55103 | 14.94001 | 103.10318 | 0.544025 | 2 | 11.765 |
| -13.29818 | -6.98867 | 15.02275 | 207.72351 | 0.547038 | 3 | 17.647 |
| -6.35477 | -0.29239 | 6.36149 | 182.63440 | 0.231647 | 4 | 23.529 |
| -7.86984 | -10.95269 | 13.48687 | 234.30157 | 0.491111 | 5 | 29.412 |
| 8.93394 | -3.72369 | 9.67890 | 337.37329 | 0.352447 | 6 | 35.294 |
| 1.74681 | 6.90770 | 7.12514 | 75.80858 | 0.259455 | 7 | 41.176 |
| -3.81001 | 3.28001 | 5.02739 | 139.27507 | 0.183067 | 8 | 47.059 |
| -1.91210 | -0.33819 | 1.94178 | 190.03023 | 0.070708 | 9 | 52.941 |
| -0.23335 | 1.37650 | 1.39614 | 99.62158 | 0.050839 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 204
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 24.00443 | | | | | 0 | |
| 20.23088 | 18.78166 | 27.60504 | 42.87257 | 1.000000 | 1 | 5.882 |
| -14.19813 | 19.25211 | 23.92133 | 126.40822 | 0.866556 | 2 | 11.765 |
| -17.06429 | -18.92628 | 25.48320 | 227.96158 | 0.923136 | 3 | 17.647 |
| 10.43137 | -14.01632 | 14.46167 | 316.16284 | 0.523878 | 4 | 23.529 |
| 10.37617 | 1.33018 | 12.70419 | 35.23904 | 0.460213 | 5 | 29.412 |
| -9.93431 | 12.23591 | 15.76096 | 129.07307 | 0.570945 | 6 | 35.294 |
| -7.88199 | -10.10984 | 12.80702 | 232.12932 | 0.463936 | 7 | 41.176 |
| 11.25643 | -4.87984 | 12.26866 | 336.56250 | 0.444436 | 8 | 47.059 |
| 3.12472 | 10.92270 | 11.36086 | 74.03542 | 0.411550 | 9 | 52.941 |
| -7.16165 | 3.19110 | 7.84043 | 155.98314 | 0.284021 | 10 | 58.824 |

HARMONIC ANALYSIS OF LIFT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| -0.10920 | | | | | 0 | |
| 1.10730 | -1.88321 | 2.18894 | 300.38867 | 1.000000 | 1 | 5.882 |
| -0.29372 | 1.12713 | 1.16477 | 104.60587 | 0.532116 | 2 | 11.765 |
| -1.03363 | -0.57726 | 1.18390 | 209.18233 | 0.540853 | 3 | 17.647 |
| -0.49931 | -0.00526 | 0.49934 | 180.60399 | 0.228120 | 4 | 23.529 |
| -0.64114 | -0.87649 | 1.08596 | 233.81503 | 0.496111 | 5 | 29.412 |
| 0.72026 | 0.31335 | 0.78547 | 336.48877 | 0.358836 | 6 | 35.294 |
| 0.15855 | 0.55977 | 0.58180 | 74.18556 | 0.265788 | 7 | 41.176 |
| -0.30472 | 0.26116 | 0.41461 | 137.30276 | 0.189411 | 8 | 47.059 |
| -0.16746 | -0.02254 | 0.16897 | 187.66425 | 0.077193 | 9 | 52.941 |
| -0.02338 | 0.10526 | 0.10782 | 102.52535 | 0.049259 | 10 | 58.824 |

HARMONIC ANALYSIS OF PITCHING MOMENT AT MEAN SPAN STATION 209
MODEL XH-51A SHIP 1002C TEST 494 OSC CTR 256 TEST COND 50 COMP RUN 10.0

| AJ | BJ | CJ | PHIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|
| 2.02891 | | | | | 0 | |
| 1.68525 | 1.56530 | 2.30005 | 42.88654 | 1.000000 | 1 | 5.882 |
| -1.08000 | 1.58018 | 1.91399 | 124.35118 | 0.832152 | 2 | 11.765 |
| -1.41848 | -1.46835 | 2.04160 | 225.98964 | 0.887835 | 3 | 17.647 |
| 0.79236 | -0.85759 | 1.16760 | 312.73584 | 0.507841 | 4 | 23.529 |
| 0.89439 | 0.56602 | 1.05844 | 32.32768 | 0.460184 | 5 | 29.412 |
| -0.78656 | 1.03691 | 1.30148 | 127.18239 | 0.565851 | 6 | 35.294 |
| -0.66063 | -0.81834 | 1.05172 | 231.08694 | 0.457260 | 7 | 41.176 |
| 0.92753 | -0.40866 | 1.01357 | 336.22192 | 0.440673 | 8 | 47.059 |
| 0.26435 | 0.89979 | 0.93782 | 73.62773 | 0.407737 | 9 | 52.941 |
| -0.58119 | 0.27524 | 0.64307 | 154.65924 | 0.279591 | 10 | 58.824 |

## APPENDIX IX

## HARMONIC COMPONENTS OF STRUCTURAL LOADS

Harmonic components of all structural loads, flapwise and chordwise bending moments, torsion, and pitch link load are presented in this appendix for the 20 selected test conditions.

The following abbreviations are used:

| | |
|---|---|
| T | test number |
| CTR | counter number |
| CR | computer run |
| TR | trace number |
| FL.BEND. | flapwise bending moment at station |
| CH.BEND. | chordwise bending moment at station |
| TORSION | torsion moment at station |

The symbols used are:

| | |
|---|---|
| AO | static component |
| AJ | cosine term of jth harmonic |
| BJ | sine term of jth harmonic |
| CJ | resultant of jth harmonic |
| PHIJC | phase angle |
| PHIJC | PHIJC/j, azimuth position of first maximum |

The definition formulas for the Fourier Series of $Y = f(X)$ are

$$Y = AO + \sum_{J=1}^{N} AJ \cos JX + \sum_{J=1}^{N} BJ \sin JX$$

or in complex form

$$Y = AO + \sum_{J=1}^{N} CJ \cos (JX-PHIJC)$$

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1340487E 03 | | | | | | | |
| 0.4282766E 04 | -0.6237777E 04 | 0.7561785E 04 | 304.602 | 304.602 | 1.000000 | 1 | 5.882 |
| 0.2756111E 03 | -0.4197024E 03 | 0.5021869E 03 | 303.292 | 191.646 | 0.066577 | 2 | 11.765 |
| 0.4373208E 03 | 0.6970144E 04 | 0.8270477E 03 | 57.895 | 19.298 | 0.109105 | 3 | 17.647 |
| 0.2C210944E 02 | C.3372769E 03 | 0.3378816E 03 | 86.571 | 21.643 | 0.044681 | 4 | 23.529 |
| -0.2577866E 02 | -0.2493891E 03 | 0.2506389E 03 | 264.096 | 52.819 | 0.033233 | 5 | 29.412 |
| -0.3981002E C2 | 0.1518975E 02 | 0.3890421E 02 | 157.625 | 26.171 | 0.003158 | 6 | 35.294 |
| 0.2746629E 02 | -0.5196614E 01 | 0.2795351E 02 | 349.286 | 44.898 | 0.003706 | 7 | 41.176 |
| -0.7414713E 02 | 0.1990485E 02 | 0.7684171E 02 | 165.342 | 20.668 | 0.010162 | 8 | 47.059 |
| 0.1335525E 02 | -0.2938313E 02 | 0.3215346E 02 | 297.591 | 33.066 | 0.004396 | 9 | 52.941 |
| -0.2047900E C2 | -0.2102204E 02 | 0.2992422E 02 | 226.823 | 22.692 | 0.003968 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| C.3270947E 04 | | | | | | | |
| 0.1864217E 04 | -0.1652237E 04 | 0.2506024E 04 | 318.753 | 318.753 | 1.000000 | 1 | 5.882 |
| 0.2839000E C2 | -0.6407282E 02 | 0.7091790E 02 | 293.635 | 146.818 | 0.028257 | 2 | 11.765 |
| -0.3358306E 01 | -0.3102960E 02 | 0.3208636E 02 | 263.977 | 87.992 | 0.012772 | 3 | 17.647 |
| 0.3406453E 01 | -0.7260023E 02 | 0.7269108E 02 | 272.769 | 68.187 | 0.029007 | 4 | 23.529 |
| 0.7527213E 02 | 0.1765839E 03 | 0.1919577E 03 | 66.913 | 13.383 | 0.076998 | 5 | 29.412 |
| -0.3490591E 02 | -0.2402614E 02 | 0.4237438E 02 | 214.538 | 35.756 | 0.016989 | 6 | 35.294 |
| -0.4530978E 02 | -0.2915584E 02 | 0.5182463E 02 | 209.039 | 29.863 | 0.020680 | 7 | 41.176 |
| C.1102179E 02 | -0.2090659E 01 | 0.1199970E 02 | 350.123 | 43.765 | 0.004788 | 8 | 47.059 |
| -0.1795184E 02 | 0.1340094E 02 | 0.2240208E 02 | 143.259 | 15.918 | C.008939 | 9 | 52.941 |
| 0.2188976E C2 | 0.1826247E 02 | 0.2726959E 02 | 36.610 | 3.661 | 0.010882 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| C.1618186E 04 | | | | | | | |
| 0.3942646E 03 | -0.4444768E 03 | 0.5983472E 03 | 3CA.559 | 308.559 | 1.000000 | 1 | 5.882 |
| -0.9908839E 02 | -0.2365213E 01 | 0.9915648E 02 | 181.362 | 90.681 | 0.175059 | 2 | 11.765 |
| -0.5812659E 02 | -0.1268938E 03 | 0.1364397E 03 | 248.445 | 92.815 | 0.2400C57 | 3 | 17.647 |
| -0.1702874E 02 | -0.7338921E 02 | 0.7554739E 02 | 256.271 | 64.068 | C.132925 | 4 | 23.529 |
| 0.2197299E C2 | 0.7044211E 02 | 0.7341309E 02 | 73.122 | 14.624 | 0.129521 | 5 | 29.412 |
| -0.1690838E 02 | -0.1667027E 02 | 0.2374780E 02 | 224.597 | 37.433 | 0.041775 | 6 | 35.294 |
| -0.1863437E 02 | 0.9874184E 01 | 0.2072632E 02 | 154.036 | 22.005 | 0.036448 | 7 | 41.176 |
| -0.2231187E 01 | 0.2318570E 02 | 0.2329279E 02 | 95.497 | 11.937 | C.040983 | 8 | 47.059 |
| -0.2242978E C2 | 0.4471327E 01 | 0.2287109E 02 | 168.726 | 18.747 | 0.040241 | 9 | 52.941 |
| 0.7C876129 01 | 0.5117194E 01 | 0.8675951E 01 | 36.139 | 3.614 | 0.015267 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1861443E 03 | | | | | | | |
| -0.1939866E C3 | -0.2195782E 03 | 0.2929932E 03 | 228.541 | 228.541 | 1.000000 | 1 | 5.882 |
| -0.1581445E 03 | 0.4330799E 02 | 0.1639672E 03 | 164.685 | 82.343 | 0.559628 | 2 | 11.765 |
| -0.1099927E 03 | -0.1579334E 03 | 0.1922038E 03 | 236.134 | 78.711 | 0.649175 | 3 | 17.647 |
| -0.4896989E 01 | 0.5551439E C1 | 0.1065710E 02 | 148.606 | 37.152 | C.036379 | 4 | 23.529 |
| -0.2780647E C2 | -0.3838719E 02 | 0.4736963E 02 | 233.968 | 46.794 | 0.161675 | 5 | 29.412 |
| 0.2084839E 01 | 0.2194679E 02 | 0.2204558E 02 | 84.573 | 14.096 | 0.075243 | 6 | 35.294 |
| 0.1544680E 02 | 0.1994637E 02 | 0.2522062E 02 | 45.913 | 6.559 | 0.075772 | 7 | 41.176 |
| -0.4041858E 01 | 0.2152680E 01 | 0.5298714E 01 | 156.033 | 19.504 | 0.018085 | 8 | 47.059 |
| 0.1814767E C1 | -0.3497818E 01 | 0.[illegible]E 01 | 297.489 | 33.054 | 0.013419 | 9 | 52.941 |
| 0.6931820E 01 | 0.1305146E 00 | 0.[illegible]E 01 | 1.145 | 0.114 | 0.023663 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1337788E 03 | | | | | | | |
| -0.4633064E 03 | -0.2525839E 03 | 0.5276848E 03 | 208.598 | 208.598 | 1.000000 | 1 | 5.882 |
| -0.1594884F 03 | 0.4410332E 01 | 0.1595493E 03 | 178.416 | 89.208 | 0.302357 | 2 | 11.765 |
| -0.1560896E 03 | -0.1307840E 03 | 0.2036379E 03 | 219.959 | 73.320 | 0.385908 | 3 | 17.647 |
| -0.1256051E 02 | 0.507C703E 02 | 0.5223953E 02 | 103.913 | 25.978 | 0.098998 | 4 | 23.529 |
| -0.4826049E 02 | -0.6918137E 02 | 0.8433980E 02 | 235.112 | 47.022 | 0.159830 | 5 | 29.412 |
| -0.4989420E 00 | 0.7729403E 01 | 0.7741496E 01 | 93.695 | 15.618 | 0.014671 | 6 | 35.294 |
| 0.4171427E 01 | -0.1389560E 02 | 0.1450822E 02 | 286.709 | 40.958 | 0.027494 | 7 | 41.176 |
| 0.2477217E 02 | -0.734C576E 01 | 0.2583687E 02 | 343.494 | 47.937 | 0.048963 | 8 | 47.059 |
| 0.4830390E 01 | -0.1173789E 02 | 0.1269294E 02 | 292.368 | 32.485 | 0.024054 | 9 | 52.941 |
| 0.9144449E 01 | -0.5855713E 01 | 0.1087559E 02 | 327.423 | 32.742 | 0.020610 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2043979E 03 | | | | | | | |
| -0.6860068E 03 | -0.2844736E 03 | 0.7426909E 03 | 202.523 | 202.523 | 1.000000 | 1 | 5.882 |
| -0.2030400E 03 | 0.3103387E 02 | 0.2053980E 03 | 171.310 | 85.655 | 0.276574 | 2 | 11.765 |
| -0.1383105E 03 | -0.8506667E 02 | 0.1606764E 03 | 211.967 | 70.656 | 0.216355 | 3 | 17.647 |
| 0.5949942E 00 | 0.7197444E 02 | 0.7197689E 02 | 89.526 | 22.382 | 0.096919 | 4 | 23.529 |
| -0.4270346E 02 | -0.1055603E 03 | 0.1138708E 03 | 247.975 | 49.595 | 0.153330 | 5 | 29.412 |
| 0.3019083E 01 | -0.9573689E 01 | 0.1003869E 02 | 287.507 | 47.918 | 0.013517 | 6 | 35.294 |
| -0.7179570E 02 | -0.3763158F 02 | 0.4348753E 02 | 239.922 | 34.275 | 0.058557 | 7 | 41.176 |
| 0.2689428F 02 | 0.3704453E 01 | 0.2713829E 02 | 7.846 | 0.981 | 0.036542 | 8 | 47.059 |
| 0.7C333S2E 00 | 0.7563876E 01 | 0.7566505E 01 | 84.687 | 9.410 | 0.010229 | 9 | 52.941 |
| -0.6551175E 00 | 0.2966787E 01 | 0.2940687E 01 | 102.872 | 10.287 | 0.003960 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8169545E 03 | | | | | | | |
| -0.7224951E 03 | -0.2515685E 03 | 0.7650396E 03 | 199.198 | 199.198 | 1.000000 | 1 | 5.882 |
| -0.2254424E 03 | -0.1493613E 02 | 0.2259366E 03 | 183.790 | 91.895 | 0.295327 | 2 | 11.765 |
| -0.1347717E 03 | -0.4926871E 02 | 0.1449047E 03 | 199.877 | 66.626 | 0.189488 | 3 | 17.647 |
| 0.4310425E 01 | 0.9523296E 02 | 0.9533043E 02 | 87.408 | 21.852 | 0.124688 | 4 | 23.529 |
| -0.1507726F 02 | -0.8475378E 02 | 0.8608440E 02 | 259.913 | 51.983 | 0.112523 | 5 | 29.412 |
| 0.1134982F 02 | -0.2825987E 02 | 0.3045389E 02 | 291.882 | 48.647 | 0.039807 | 6 | 35.294 |
| -0.3937590E 01 | -0.5223541E 02 | 0.5238322E 02 | 265.694 | 37.956 | 0.068471 | 7 | 41.176 |
| 0.3114931E 02 | 0.1328889F 02 | 0.3386552E 02 | 23.104 | 2.888 | 0.044246 | 8 | 47.059 |
| -0.9482577E 01 | -0.9342522E 01 | 0.1331172E 02 | 224.574 | 24.953 | 0.017400 | 9 | 52.941 |
| 0.3716091F 01 | -0.8613688F 00 | 0.3814614E 01 | 346.949 | 34.695 | 0.004986 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8649185E 03 | | | | | | | |
| -0.5572903F 03 | -0.1899500E 03 | 0.5887727E 03 | 198.821 | 198.821 | 1.000000 | 1 | 5.882 |
| -0.1706833E 03 | -0.3297281F 02 | 0.1738349E 03 | 190.934 | 95.467 | 0.295256 | 2 | 11.765 |
| -0.1151382F 03 | -0.7654785F 01 | 0.1153924E 03 | 183.804 | 61.268 | 0.195988 | 3 | 17.647 |
| -0.4562106E 00 | 0.8805371E 02 | 0.8805487E 02 | 90.297 | 22.574 | 0.149557 | 4 | 23.529 |
| -0.9317259E 01 | -0.6015224E 02 | 0.6089626E 02 | 264.990 | 52.998 | 0.103429 | 5 | 29.412 |
| 0.2721039F 02 | -0.3899097E 02 | 0.4754678E 02 | 304.910 | 50.818 | 0.080758 | 6 | 35.294 |
| -0.2190637E 02 | -0.4584545E 02 | 0.5062997E 02 | 244.362 | 34.909 | 0.085992 | 7 | 41.176 |
| 0.2181924F 02 | 0.7458889E 01 | 0.2303893E 02 | 18.873 | 2.359 | 0.039164 | 8 | 47.059 |
| -0.1547508F 02 | 0.2802110E 01 | 0.1572672E 02 | 169.737 | 18.860 | 0.026711 | 9 | 52.941 |
| -0.7790796F 00 | 0.3718146F 01 | 0.3798891E 01 | 101.834 | 10.183 | 0.006452 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2369904E 05 | | | | | | | |
| 0.2C33261E 05 | -0.2274533E 04 | 0.2045943E 05 | 353.617 | 353.617 | 1.CCCCCC | 1 | 5.882 |
| 0.1415737E C4 | 0.5041980E 03 | 0.1502839E 04 | 19.603 | 9.8C1 | 0.073455 | 2 | 11.765 |
| 0.1102861E 04 | 0.9877986E 03 | 0.1440557E 04 | 41.850 | 13.65C | 0.072365 | 3 | 17.647 |
| 0.1C725989E 03 | 0.6391275E 02 | 0.1248571E 03 | 30.790 | 7.697 | 0.0C6103 | 4 | 23.529 |
| -0.7808596E 01 | -0.6016335E 03 | 0.6016841E 03 | 269.256 | 53.851 | 0.029409 | 5 | 29.417 |
| -0.2509766E C2 | 0.8904080E 00 | 0.251 343E 02 | 177.968 | 29.661 | 0.001227 | 6 | 35.294 |
| 0.1265251E 03 | -0.9750098E 02 | 0.1597342E 03 | 322.382 | 46.055 | 0.007807 | 7 | 41.176 |
| -0.2240498E 03 | -0.8144661E 02 | 0.2383943E 03 | 199.977 | 24.997 | 0.011652 | 8 | 47.059 |
| 0.1365116E 03 | -0.1023697E 02 | 0.1377244E 03 | 352.391 | 39.155 | C.CC6732 | 9 | 52.941 |
| -0.7334493E C2 | -0.2164713E 03 | 0.2304559E 03 | 251.441 | 25.144 | C.011264 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2112496E 05 | | | | | | | |
| 0.1170935E 05 | -0.3831162E 03 | 0.1171561E 05 | 358.126 | 358.126 | 1.000000 | 1 | 5.882 |
| 0.6883994E 03 | 0.3990591E 03 | 0.7957019E 03 | 30.100 | 15.05C | 0.C67918 | 2 | 11.765 |
| 0.5239050E 03 | 0.9276950E 03 | 0.1065329E 04 | 60.542 | 20.181 | 0.C90932 | 3 | 17.647 |
| -0.6423523E 02 | -0.2239992E 03 | 0.2330275E 03 | 253.999 | 63.500 | 0.C19890 | 4 | 23.529 |
| 0.3718945E 02 | -0.4017715E 03 | 0.4034888E 03 | 275.298 | 55.058 | 0.034440 | 5 | 29.412 |
| 0.9782280E 02 | 0.3770449E 03 | 0.3895278E 03 | 75.455 | 12.576 | 0.033245 | 6 | 35.294 |
| 0.1121001E 03 | 0.179C376E 01 | 0.2112366E 03 | 57.948 | 8.278 | 0.018C3C | 7 | 41.176 |
| -0.8016699E 02 | 0.5409450C 02 | 0.9671088E 02 | 145.990 | 18.249 | 0.CC8255 | 8 | 47.059 |
| -0.4467543E C2 | -0.5383842E 02 | 0.6992856E 02 | 230.345 | 25.564 | C.009969 | 9 | 52.941 |
| 0.32032C0E 02 | -0.2004893E 02 | 0.3770899E 02 | 327.957 | 32.796 | 0.003226 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6207859E 04 | | | | | | | |
| 0.5131164E 04 | -0.4744282E 03 | 0.5153047E 04 | 354.717 | 354.717 | 1.0000CC | 1 | 5.882 |
| 0.4148311E 03 | 0.7029860E 02 | 0.4207451E 03 | 9.618 | 4.8C9 | 0.081650 | 2 | 11.765 |
| 0.1988398E 03 | 0.4853225E 03 | 0.6281807E 03 | 50.586 | 10.862 | 0.121905 | 3 | 17.647 |
| -0.7827741E C2 | -0.1433219E 03 | 0.1635693E 03 | 241.189 | 60.297 | C.031742 | 4 | 23.529 |
| -0.8456206E 02 | -0.1274754E 03 | 0.1529729E 03 | 236.441 | 47.288 | 0.029686 | 5 | 29.412 |
| 0.4309613E 02 | 0.4766719E 03 | 0.4766240E 03 | 84.812 | 14.135 | 0.092494 | 6 | 35.294 |
| 0.1497514E 03 | 0.8836751E 02 | 0.1728723E 03 | 29.974 | 4.282 | C.C33548 | 7 | 41.176 |
| 0.5746504E C2 | -0.7860324E 02 | 0.9736888E 02 | 306.170 | 38.271 | 0.018895 | 8 | 47.059 |
| -0.5973894F 01 | 0.1135388E 03 | 0.1136958E 03 | 93.012 | 10.335 | 0.022064 | 9 | 52.941 |
| 0.3892719E 02 | 0.1534744E 02 | 0.4184339E 02 | 21.517 | 2.152 | 0.CC812C | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 538 CR 53.1 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4798398E 04 | | | | | | | |
| 0.2224811E 04 | 0.2488150F 02 | 0.2224949E 04 | 0.641 | 0.641 | 1.CCCCCC | 1 | 5.882 |
| 0.1108611F 03 | -0.4241937E 02 | 0.1186995E 03 | 339.061 | 169.531 | C.C53349 | 2 | 11.765 |
| 0.2654519E C3 | 0.9986607E 02 | 0.2816088E 03 | 20.613 | 6.871 | 0.127067 | 3 | 17.647 |
| -0.6857291E 02 | -0.1163169E 03 | 0.1350254E 03 | 239.479 | 59.870 | 0.060687 | 4 | 23.529 |
| -0.1C09907E 03 | -0.8362292E 02 | 0.1304259E C3 | 219.878 | 43.976 | 0.058820 | 5 | 29.412 |
| 0.1519225E 02 | 0.2569883E 03 | 0.2574368E 03 | 86.617 | 14.436 | 0.115705 | 6 | 35.294 |
| 0.1242107E C3 | 0.1108688E 03 | 0.1644993E 03 | 41.752 | 5.965 | 0.074030 | 7 | 41.176 |
| 0.5738042E 02 | -0.9451162E 02 | 0.1105866E 03 | 301.263 | 37.658 | 0.049694 | 8 | 47.059 |
| 0.4968676F 02 | 0.6918130E 02 | 0.8517496E 02 | 54.314 | 6.035 | 0.038282 | 9 | 52.941 |
| 0.5440802E 02 | 0.2037616C 02 | 0.5809836E 02 | 20.531 | 2.053 | 0.026112 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 530 CR 53.1 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.21344486 03 | | | | | | | |
| 0.1924232E 02 | 0.4566849E 02 | 0.4950153E 02 | 67.125 | 67.125 | 1.000000 | 1 | 5.882 |
| -0.1741827E 02 | 0.1456032E 00 | 0.1741887E 02 | 179.521 | 89.761 | 0.351885 | 2 | 11.765 |
| -0.4930002E 01 | -0.2095469E 02 | 0.2111010E 02 | 256.507 | 85.502 | 0.426857 | 3 | 17.647 |
| 0.5302574E 01 | 0.6705484E 01 | 0.8604845E 01 | 51.194 | 12.798 | 0.173830 | 4 | 23.529 |
| -0.1477208E 00 | -0.3492453E 02 | 0.3492484E 02 | 269.758 | 53.952 | 0.705530 | 5 | 29.412 |
| 0.1173908E 01 | 0.2714846E 02 | 0.1276888E 02 | 86.727 | 14.121 | 0.257969 | 6 | 35.294 |
| -0.1786850E 01 | 0.1413088E 01 | 0.2278079E 01 | 141.662 | 20.237 | 0.046020 | 7 | 41.176 |
| -0.2144150E 02 | 0.1727126E 01 | 0.2151094E 02 | 175.395 | 21.924 | 0.434551 | 8 | 47.059 |
| -0.1062786E 02 | -0.4262712E-01 | 0.1062795E 02 | 180.230 | 20.026 | 0.214696 | 9 | 52.941 |
| 0.4105214E 01 | 0.2579299E 01 | 0.4848250E 01 | 32.141 | 3.214 | 0.097941 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 530 CR 53.1 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.26649816 02 | | | | | | | |
| -0.2421387E 02 | 0.1110779E 02 | 0.2664008E 02 | 155.357 | 155.357 | 1.000000 | 1 | 5.882 |
| -0.2183167E 01 | 0.6904961E 01 | 0.7241870E 01 | 107.546 | 53.773 | 0.271841 | 2 | 11.765 |
| -0.5553581E 01 | -0.2076395E 01 | 0.5929051E 01 | 200.500 | 66.833 | 0.222561 | 3 | 17.647 |
| -0.3457681E-01 | 0.7917879E 01 | 0.7917791E 01 | 90.264 | 22.566 | 0.297197 | 4 | 23.529 |
| -0.1675870E 01 | -0.1155818E 02 | 0.1167904E 02 | 261.750 | 52.350 | 0.438401 | 5 | 29.412 |
| 0.2470345E 01 | 0.1760082E 01 | 0.3037888E 01 | 35.592 | 5.932 | 0.114034 | 6 | 35.294 |
| 0.3823818E 00 | -0.2679436E 01 | 0.2706583E 01 | 278.122 | 39.732 | 0.101548 | 7 | 41.176 |
| -0.1334301E 02 | -0.4074427E 01 | 0.1393671E 02 | 196.784 | 24.598 | 0.523148 | 8 | 47.059 |
| -0.5304620E 01 | 0.1540520E-01 | 0.5304640E 01 | 179.835 | 19.982 | 0.201375 | 9 | 52.941 |
| -0.8954170E 00 | 0.1280521E 01 | 0.1539458E 01 | 123.744 | 12.374 | 0.057806 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 530 CR 53.1 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.7356913E 02 | | | | | | | |
| -0.4623065E 02 | 0.2208461E 02 | 0.5123477E 02 | 154.466 | 154.466 | 1.000000 | 1 | 5.882 |
| -0.8104777E 00 | 0.8308851E 01 | 0.8348281E 01 | 95.571 | 47.785 | 0.162942 | 2 | 11.765 |
| -0.1214875E 01 | 0.1593597E 02 | 0.1598221E 02 | 94.360 | 31.453 | 0.311941 | 3 | 17.647 |
| -0.7190458E 01 | -0.2017100E 00 | 0.7199283E 01 | 181.606 | 45.401 | 0.140516 | 4 | 23.529 |
| 0.3788574E 01 | 0.1484129E 01 | 0.4068896E 01 | 21.392 | 5.278 | 0.079417 | 5 | 29.412 |
| 0.4568067E-01 | 0.3520849E 00 | 0.3550346E 00 | 82.607 | 13.768 | 0.006930 | 6 | 35.294 |
| 0.1179539E 01 | -0.1390782E 00 | 0.1187709E 01 | 353.275 | 50.468 | 0.023182 | 7 | 41.176 |
| 0.1582960E 01 | -0.2329216E 00 | 0.1600024E 01 | 351.629 | 43.954 | 0.031229 | 8 | 47.059 |
| -0.5399768E 00 | -0.6614087E 00 | 0.8538376E 00 | 230.772 | 25.641 | 0.016665 | 9 | 52.941 |
| -0.6073939E 00 | -0.5685382E 00 | 0.8319633E 00 | 223.107 | 22.311 | 0.016230 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 530 CR 53.1 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1061388E 02 | | | | | | | |
| 0.4030396E 00 | -0.7982517E 00 | 0.8940504E 00 | 296.795 | 296.795 | 1.000000 | 1 | 5.882 |
| -0.1732853E-02 | 0.3539841E-01 | 0.3543081E-01 | 92.803 | 46.402 | 0.039630 | 2 | 11.765 |
| -0.5947113E-02 | -0.3589644E-01 | 0.3638579E-01 | 260.593 | 86.864 | 0.040698 | 3 | 17.647 |
| -0.3065000E-01 | -0.1604632E-01 | 0.3490258E-01 | 208.579 | 52.145 | 0.039039 | 4 | 23.529 |
| -0.9176177E-02 | -0.7102858E-02 | 0.1176279E-01 | 217.146 | 43.429 | 0.013157 | 5 | 29.412 |
| 0.8563757E-02 | 0.1571602E-02 | 0.8706767E-02 | 10.399 | 1.733 | 0.009739 | 6 | 35.294 |
| -0.2384106E-02 | 0.1390250E-01 | 0.1410944E-01 | 99.731 | 16.247 | 0.015777 | 7 | 41.176 |
| 0.2871858E-02 | -0.2727270E-02 | 0.3960498E-02 | 316.479 | 39.560 | 0.004430 | 8 | 47.059 |
| 0.1125553E-01 | -0.3939416E-02 | 0.1192501E-01 | 340.710 | 37.857 | 0.013338 | 9 | 52.941 |
| 0.1993192E-02 | 0.2293613E-02 | 0.3032113E-02 | 49.151 | 4.915 | 0.003391 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 4

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.43001772E 04 | | | | | | | |
| 0.35409485E 04 | -0.1864541E 05 | 0.11029276 05 | 288.726 | 288.726 | 1.000000 | 1 | 5.714 |
| 0.8348604E 03 | -0.1671699E 03 | 0.8514326E 03 | 348.677 | 174.339 | 0.077198 | 2 | 11.429 |
| -0.4872698E 03 | -0.7C8%615E 07 | 0.4924001E 03 | 188.278 | 62.759 | 0.044645 | 3 | 17.143 |
| -0.5957786E 02 | 0.1388071E 02 | 0.61150950E 02 | 166.957 | 41.739 | 0.005544 | 4 | 22.857 |
| -0.4914763E 03 | 0.1525107E 03 | 0.5149974E 03 | 162.759 | 32.552 | 0.046657 | 5 | 28.571 |
| -0.9287794E 01 | -0.1929677E 02 | 0.21068318E 02 | 244.642 | 40.774 | 0.001906 | 6 | 34.286 |
| 0.1908470E 03 | 0.1947441E 02 | 0.1916306E 03 | 5.857 | 0.837 | 0.013749 | 7 | 40.000 |
| -0.9777594E 02 | -0.1125692E 02 | 0.98421399E 02 | 186.568 | 23.321 | 0.008924 | 8 | 45.714 |
| -0.7152711E 02 | -0.3435077E 02 | 0.79347095E 02 | 205.653 | 22.85G | 0.007194 | 9 | 51.429 |
| -0.5367499E 01 | 0.2879570E 02 | 0.2929166E 02 | 100.559 | 10.056 | 0.002656 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.6239348E 04 | | | | | | | |
| 0.2980213E 04 | -0.3214229E 04 | 0.43832948E 04 | 312.836 | 312.836 | 1.000000 | 1 | 5.714 |
| -0.3892122E 02 | -0.2241894E 03 | 0.2279438E 03 | 260.151 | 130.075 | 0.051812 | 2 | 11.429 |
| -0.1703276E 03 | -0.1857401E 02 | 0.17133773E 03 | 186.223 | 62.074 | 0.039089 | 3 | 17.143 |
| -0.3559994E 02 | -0..3176308E 02 | 0.4247897E 02 | 213.065 | 53.266 | 0.009691 | 4 | 22.857 |
| 0.1345865E 03 | -0.1240800E 02 | 0.13504143E 03 | 354.698 | 70.940 | 0.030818 | 5 | 28.571 |
| -0.8135294E 02 | 0.3567399E 02 | 0.88831146E 02 | 156.321 | 26.054 | 0.020264 | 6 | 34.286 |
| -0.1244139E 03 | -0.2804590E 02 | 0.12754206E 03 | 192.712 | 27.530 | 0.029090 | 7 | 40.000 |
| 0.2618835E 02 | 0.2536800E 02 | 0.3645490E 02 | 44.079 | 5.510 | 0.008317 | 8 | 45.714 |
| 0.4478813E 02 | 0.9509642E 00 | 0.44789931E 02 | 0.704 | 0.078 | 0.010218 | 9 | 51.429 |
| 0.1940195E 01 | 0.2112911E 02 | 0.2118182E 02 | 89.806 | 8.981 | 0.004832 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 6 FL. BEND 75

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1737190E 04 | | | | | | | |
| 0.5695872E 03 | -0.6512709E 03 | 0.10242908E 04 | 303.706 | 303.706 | 1.000000 | 1 | 5.714 |
| -0.1429814E 03 | -0.9307622E 02 | 0.1702722E 03 | 213.136 | 106.568 | 0.166240 | 2 | 11.429 |
| 0.7690449E 02 | -0.5945988E 01 | 0.7711393E 02 | 355.579 | 118.526 | 0.075287 | 3 | 17.143 |
| 0.1908702E 02 | -0.1506203E 02 | 0.2424623E 02 | 321.776 | 80.4 . | 0.023672 | 4 | 22.857 |
| 0.1427114E 03 | -0.2468310E 02 | 0.14483082E 03 | 350.187 | 70.037 | 0.141408 | 5 | 28.571 |
| -0.3660954E 00 | 0.1739097E 02 | 0.1739481E 02 | 91.209 | 15.201 | 0.010904 | 6 | 34.286 |
| -0.2629969E 02 | 0.2851570E 02 | 0.3876480E 02 | 132.642 | 18.949 | 0.037847 | 7 | 40.000 |
| -0.4832089E 01 | -0.1252626E 02 | 0.1342990E 02 | 248.988 | 31.113 | 0.013100 | 8 | 45.714 |
| 0.7296698E 01 | -0.7305616E 01 | 0.10329908E 02 | 314.957 | 36.995 | 0.010079 | 9 | 51.429 |
| 0.7467109E 01 | -0.9159[illegible]E 01 | 0.11814468E 02 | 309.199 | 38.920 | 0.011535 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 563 [illegible] 37.3 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSI. | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0. 4704198E 03 | | | | | | | |
| -0.1279419E 02 | -0.4589308E 01 | 0.46833798E 03 | 259.780 | 259.7.3 | 1.000000 | 1 | 5.714 |
| -0.1847799E 02 | -0.3490095E 02 | 0.1000593E 03 | 190.716 | 95.358 | 0.403268 | 2 | 11.429 |
| 0.2910095E 03 | 0.6714829E 02 | 0.2990863E 03 | 14.937 | 4.979 | 0.598578 | 3 | 17.143 |
| 0.7130794E 02 | 0.7194083E 01 | 0.7166849E 02 | 5.721 | 1.430 | 0.153046 | 4 | 22.857 |
| -0.1180748E 02 | 0.2003107E 02 | 0.2868061E 02 | 114.900 | 22.982 | 0.061947 | 5 | 28.571 |
| 0.5021115E 02 | 0.1051644E 02 | 0.5130061E 02 | 11.829 | 1.972 | 0.110007 | 6 | 34.286 |
| 0.9442067E 02 | 0.7470108E 01 | 0.9471568E 02 | 4.524 | 0.646 | 0.203105 | 7 | 40.000 |
| -0.1210613E 01 | -0.1987709E 02 | 0.23272611E 02 | 230.424 | 29.803 | 0.049905 | 8 | 45.714 |
| -0.3687679E 02 | -0.4682404E 00 | 0.36879718E 02 | 180.731 | 20.081 | 0.077360 | 9 | 51.429 |
| -0.4487340E 01 | 0.5829E44E 01 | 0.7907866E 01 | 127.092 | 12.709 | 0.015671 | 10 | 57.143 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 4

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8521599E 03 | | | | | | | |
| -0.3422888E 03 | -0.4561953E 03 | 0.5703293E 03 | 233.119 | 233.119 | 1.000000 | 1 | 5.714 |
| -0.2044984E 03 | 0.3575006E 02 | 0.2075999E 03 | 170.084 | 85.042 | 0.364000 | 2 | 11.429 |
| 0.2218827E 02 | 0.9620578E 02 | 0.2418421E 03 | 23.441 | 7.814 | 0.424039 | 3 | 17.143 |
| 0.5462000E 02 | 0.7837836E 02 | 0.9553276E 02 | 55.128 | 13.782 | 0.167505 | 4 | 22.857 |
| -0.1562808E 03 | 0.6236084E 02 | 0.1682634E 03 | 158.246 | 31.649 | 0.295028 | 5 | 28.571 |
| 0.2600859E 02 | -0.3881488E 02 | 0.4032373E 02 | 310.165 | 51.694 | 0.070702 | 6 | 34.286 |
| -0.2290511E 02 | -0.2343174E 02 | 0.3282745E 02 | 225.559 | 32.223 | 0.057559 | 7 | 40.000 |
| 0.9071177E-01 | -0.1129480E 02 | 0.1129516E 02 | 270.460 | 33.808 | 0.019805 | 8 | 45.714 |
| 0.1796997E 02 | -0.1173258E 02 | 0.2144095E 02 | 326.856 | 36.318 | 0.037629 | 9 | 51.429 |
| 0.5247417E 01 | -0.2007206E 02 | 0.2074539E 02 | 284.637 | 28.464 | 0.036374 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1373932E 04 | | | | | | | |
| -0.4260476E 03 | -0.9005508E 03 | 0.7261304E 03 | 223.577 | 223.577 | 1.000000 | 1 | 5.714 |
| -0.2140476E 03 | 0.6700510E 02 | 0.2242901E 03 | 162.618 | 81.309 | 0.308881 | 2 | 11.429 |
| 0.1883136E 03 | 0.6933044E 02 | 0.2006707E 03 | 20.212 | 6.737 | 0.276353 | 3 | 17.143 |
| 0.1523197E 02 | 0.3946252E 02 | 0.4230816E 02 | 68.894 | 17.224 | 0.058254 | 4 | 22.857 |
| -0.1866435E 03 | 0.1008633E 03 | 0.2121713E 03 | 151.616 | 30.323 | 0.292191 | 5 | 28.571 |
| -0.1571249E 02 | -0.6134575E 02 | 0.6332868E 02 | 255.634 | 42.606 | 0.087209 | 6 | 34.286 |
| -0.6785970E 02 | -0.3684091E 02 | 0.7721319E 02 | 208.497 | 29.785 | 0.106337 | 7 | 40.000 |
| 0.3322394E 02 | 0.9831116E 01 | 0.3454795E 02 | 16.484 | 2.060 | 0.047719 | 8 | 45.714 |
| 0.3401447E 02 | -0.1131786E 02 | 0.3591772E 02 | 341.597 | 37.955 | 0.049468 | 9 | 51.429 |
| 0.1700822E 02 | -0.1879549E 02 | 0.2534856E 02 | 312.142 | 31.214 | 0.034909 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1665171E 04 | | | | | | | |
| -0.4842925E 03 | -0.3936721E 03 | 0.6241128E 03 | 219.107 | 219.107 | 1.000000 | 1 | 5.714 |
| -0.2044521E 03 | 0.2278360E 02 | 0.2057177E 03 | 173.641 | 86.821 | 0.329616 | 2 | 11.429 |
| 0.1340243E 03 | 0.9971342E 02 | 0.1670485E 03 | 36.649 | 12.216 | 0.267657 | 3 | 17.143 |
| -0.2573383E 02 | 0.3921741E 02 | 0.4690469E 02 | 123.272 | 30.818 | 0.075157 | 4 | 22.857 |
| -0.1749757E 03 | 0.7630571E 02 | 0.1905236E 03 | 156.390 | 31.278 | 0.305271 | 5 | 28.571 |
| -0.5367621E 02 | -0.2113705E 02 | 0.5768803E 02 | 201.494 | 33.582 | 0.092432 | 6 | 34.286 |
| -0.1024128E 03 | -0.7131089E 02 | 0.1247996E 03 | 214.853 | 30.693 | 0.199982 | 7 | 40.000 |
| 0.1183309E 02 | 0.3619789E 02 | 0.3808287E 02 | 71.897 | 8.987 | 0.061019 | 8 | 45.714 |
| 0.5188841E 02 | -0.1498327E 02 | 0.5398986E 02 | 344.302 | 38.256 | 0.086561 | 9 | 51.429 |
| 0.7875746E 01 | -0.1227805E 02 | 0.1458756E 02 | 302.677 | 30.268 | 0.023379 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1884043E 04 | | | | | | | |
| -0.3728857E 03 | -0.2955809E 03 | 0.4520674E 03 | 214.427 | 214.427 | 1.000000 | 1 | 5.714 |
| -0.1430894E 03 | -0.2135672E 02 | 0.1446744E 03 | 188.489 | 94.244 | 0.320028 | 2 | 11.429 |
| 0.9338672E 02 | 0.6228227E 02 | 0.1122504E 03 | 33.700 | 11.233 | 0.248304 | 3 | 17.143 |
| -0.2099918E 02 | 0.1627232E 02 | 0.3725266E 02 | 150.702 | 37.675 | 0.073957 | 4 | 22.857 |
| -0.1262909E 03 | 0.7303917E 02 | 0.1458907E 03 | 149.997 | 29.991 | 0.322719 | 5 | 28.571 |
| -0.4773506E 02 | -0.2129053E 01 | 0.4778227E 02 | 182.549 | 30.425 | 0.105697 | 6 | 34.286 |
| -0.1188309E 03 | -0.3744324E 02 | 0.1249000E 03 | 197.488 | 28.213 | 0.276318 | 7 | 40.000 |
| 0.6317634E 01 | 0.3840015E 02 | 0.3891635E 02 | 80.657 | 10.082 | 0.086085 | 8 | 45.714 |
| 0.8079618E 02 | -0.1726454E 02 | 0.8319997E 02 | 347.147 | 38.239 | 0.139832 | 9 | 51.429 |
| 0.1774464E 02 | -0.1764206E 02 | 0.2502228E 02 | 315.166 | 31.517 | 0.055351 | 10 | 57.143 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 4

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2479791E 05 | | | | | | | |
| 0.3972219E 05 | -0.7241711E 04 | 0.4037691E 05 | 349.668 | 349.668 | 1.000000 | 1 | 5.714 |
| 0.9380000E 01 | 0.8709244E 02 | 0.9420344E 03 | 5.305 | 2.652 | 0.023331 | 2 | 11.429 |
| -0.3138311E 04 | -0.4405984E 03 | 0.3169088E 04 | 187.992 | 62.664 | 0.078488 | 3 | 17.143 |
| -0.8554717E 03 | -0.1347766E 04 | 0.1596349E 04 | 237.595 | 59.399 | 0.039536 | 4 | 22.857 |
| -0.6852754E 03 | -0.3904021E 03 | 0.7886799E 03 | 209.670 | 41.934 | 0.019533 | 5 | 28.571 |
| -0.5562521E 02 | -0.3597910E 03 | 0.5625476E 03 | 264.325 | 44.054 | 0.013932 | 6 | 34.286 |
| -0.1900935E 03 | -0.7196804E 04 | 0.7443623E 03 | 255.204 | 36.458 | 0.018435 | 7 | 40.000 |
| 0.2039116E 02 | -0.1943754E 03 | 0.1954421E 03 | 275.989 | 34.499 | 0.004840 | 8 | 45.714 |
| -0.3156389E 03 | -0.6498674E 03 | 0.7224648E 03 | 244.094 | 27.122 | 0.017893 | 9 | 51.429 |
| -0.4554199E 02 | -0.3717922E 03 | 0.3745710E 03 | 263.016 | 26.302 | 0.009277 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1770337E 05 | | | | | | | |
| 0.2339229E 05 | -0.2242927E 04 | 0.2349957E 05 | 354.523 | 354.523 | 1.000000 | 1 | 5.714 |
| 0.4387078E 03 | 0.2335499E 03 | 0.4970010E 03 | 28.029 | 14.014 | 0.021149 | 2 | 11.429 |
| -0.2316993E 04 | -0.2483258E 03 | 0.2330262E 04 | 186.117 | 62.039 | 0.099162 | 3 | 17.143 |
| -0.6346526E 03 | -0.5862168E 03 | 0.8639641E 03 | 222.728 | 55.682 | 0.036765 | 4 | 22.857 |
| -0.5165046E 03 | 0.4404849E 02 | 0.5163867E 03 | 175.107 | 35.021 | 0.021974 | 5 | 28.571 |
| 0.1248991E 03 | -0.5356350E 03 | 0.5500039E 03 | 283.126 | 47.188 | 0.023405 | 6 | 34.286 |
| 0.2277956E 03 | 0.2294141E 02 | 0.2289479E 03 | 5.751 | 0.822 | 0.009743 | 7 | 40.000 |
| -0.2314864E 03 | -0.7255801E 02 | 0.2425917E 03 | 197.403 | 24.675 | 0.010323 | 8 | 45.714 |
| -0.1250392E 03 | -0.1417513E 02 | 0.1258401E 03 | 186.468 | 20.719 | 0.005355 | 9 | 51.429 |
| -0.1909868E 03 | -0.7706250E 02 | 0.2059480E 03 | 201.974 | 20.197 | 0.008764 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5902797E 04 | | | | | | | |
| 0.9944234E 04 | -0.1652304E 04 | 0.1008057E 05 | 350.566 | 350.566 | 1.000000 | 1 | 5.714 |
| 0.3935837E 03 | 0.1264619E 02 | 0.3937866E 03 | 1.840 | 0.920 | 0.039064 | 2 | 11.429 |
| -0.1101901E 04 | 0.1382399E 03 | 0.1110544E 04 | 172.847 | 57.616 | 0.110167 | 3 | 17.143 |
| -0.3192761E 03 | -0.1758067E 03 | 0.3644792E 03 | 208.839 | 52.210 | 0.036157 | 4 | 22.857 |
| -0.1499503E 03 | 0.1432988E 03 | 0.2074116E 03 | 136.299 | 27.260 | 0.020575 | 5 | 28.571 |
| 0.1268756E 03 | -0.4802187E 03 | 0.4966963E 03 | 284.800 | 47.467 | 0.049273 | 6 | 34.286 |
| 0.3362896E 03 | -0.2472942E 03 | 0.4173970E 03 | 323.676 | 46.239 | 0.041406 | 7 | 40.000 |
| -0.4761484E 03 | -0.7102962E 02 | 0.4814170E 03 | 188.485 | 23.561 | 0.047757 | 8 | 45.714 |
| 0.2396519E 03 | 0.2017515E 03 | 0.3102180E 03 | 40.568 | 4.508 | 0.030774 | 9 | 51.429 |
| -0.2213534E 02 | 0.8084006E 02 | 0.8381578E 02 | 105.313 | 10.531 | 0.008315 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 563 CR 37.0 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4759379E 04 | | | | | | | |
| 0.3883297E 04 | -0.4496614E 03 | 0.3909242E 04 | 353.395 | 353.395 | 1.000000 | 1 | 5.714 |
| 0.2142692E 03 | -0.3845264E 02 | 0.2176922E 03 | 349.826 | 174.913 | 0.055687 | 2 | 11.429 |
| -0.3620088E 03 | 0.1165982E 03 | 0.3803228E 03 | 162.147 | 54.049 | 0.097288 | 3 | 17.143 |
| -0.1232070E 03 | -0.7088850E 02 | 0.1421448E 03 | 209.914 | 52.479 | 0.036361 | 4 | 22.857 |
| 0.6114664E 02 | 0.1279691E 03 | 0.1418273E 03 | 64.660 | 12.892 | 0.036280 | 5 | 28.571 |
| -0.1820760E 01 | -0.2109098E 03 | 0.2109177E 03 | 269.505 | 44.918 | 0.053954 | 6 | 34.286 |
| 0.2409669E 03 | -0.1801184E 03 | 0.3008447E 03 | 323.222 | 46.175 | 0.076957 | 7 | 40.000 |
| -0.2517924E 03 | 0.8397447E 01 | 0.2519324E 03 | 178.090 | 22.261 | 0.064445 | 8 | 45.714 |
| 0.1977009E 03 | 0.1810923E 03 | 0.2401333E 03 | 48.950 | 5.439 | 0.061427 | 9 | 51.429 |
| -0.1542167E 02 | 0.7594031E 02 | 0.7749034E 02 | 101.479 | 10.148 | 0.019822 | 10 | 57.143 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 4

HARMONIC ANALYSIS MODEL XH-51A SHIP 1007C T 498 CTR 563 CR 37.0 IR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.34526206 03 | | | | | | | |
| 0.88329266 01 | 0.53433176 02 | 0.54158316 02 | 80.613 | 80.613 | 0.872812 | 1 | 5.714 |
| -0.10695166 02 | 0.13562166 02 | 0.17256186 02 | 128.301 | 64.150 | 0.278100 | 2 | 11.429 |
| 0.13801036 02 | 0.17534426 02 | 0.22314216 02 | 51.724 | 17.241 | 0.359614 | 3 | 17.143 |
| -0.12042746 02 | 0.25257806 02 | 0.27981676 02 | 115.491 | 23.873 | 0.450951 | 4 | 22.857 |
| -0.61843486 02 | 0.50628086 01 | 0.62050356 02 | 175.320 | 35.064 | 1.000000 | 5 | 28.571 |
| 0.36731166 01 | 0.91290286 01 | 0.98402716 01 | 68.082 | 11.347 | 0.158585 | 6 | 34.286 |
| 0.98517646 01 | 0.25103916 02 | 0.26967826 02 | 68.573 | 9.796 | 0.434612 | 7 | 40.000 |
| -0.79517896 01 | 0.17695306 02 | 0.19399846 02 | 114.198 | 14.275 | 0.312647 | 8 | 45.714 |
| 0.58493646 01 | -0.60272756 01 | 0.84129336 01 | 314.240 | 34.915 | 0.135582 | 9 | 51.429 |
| -0.27341906 01 | -0.19891826 01 | 0.48362546 01 | 235.573 | 23.557 | 0.077941 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1007C T 498 CTR 563 CR 37.0 IR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.13925046 03 | | | | | | | |
| -0.11825526 01 | 0.17381716 02 | 0.17421876 02 | 93.892 | 93.892 | 0.601871 | 1 | 5.714 |
| -0.10485216 02 | 0.16502296 02 | 0.19551596 02 | 122.431 | 61.216 | 0.675445 | 2 | 11.429 |
| 0.38857626 01 | 0.20278906 02 | 0.20647836 02 | 79.153 | 26.384 | 0.713317 | 3 | 17.143 |
| -0.31554066 01 | 0.91348006 01 | 0.68769096 01 | 121.571 | 30.393 | 0.238211 | 4 | 22.857 |
| -0.27787386 02 | 0.81081646 01 | 0.28946216 02 | 163.733 | 32.747 | 1.000000 | 5 | 28.571 |
| -0.69434096 00 | 0.23856796 01 | 0.23967306 01 | 105.844 | 17.641 | 0.082799 | 6 | 34.286 |
| 0.11012676 02 | 0.93739216 01 | 0.14461996 02 | 40.486 | 5.772 | 0.499816 | 7 | 40.000 |
| -0.20386496 01 | 0.48157486 01 | 0.52294846 01 | 112.944 | 16.118 | 0.180662 | 8 | 45.714 |
| 0.58925246 01 | -0.36990396 01 | 0.69573496 01 | 327.881 | 36.431 | 0.240354 | 9 | 51.429 |
| -0.61976276 01 | -0.17641936 01 | 0.64441186 01 | 195.889 | 19.589 | 0.222624 | 10 | 57.143 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1007C T 498 CTR 563 CR 37.0 IR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.20766746 02 | | | | | | | |
| -0.91183436 02 | 0.68291596 02 | 0.11392176 03 | 143.169 | 143.169 | 1.000000 | 1 | 5.714 |
| -0.16261206 02 | 0.29868076 02 | 0.34007756 02 | 118.565 | 59.283 | 0.298519 | 2 | 11.429 |
| -0.17399416 01 | 0.39011396 01 | 0.42699386 01 | 113.988 | 37.996 | 0.037481 | 3 | 17.143 |
| 0.70036346 01 | -0.42822736 01 | 0.82090656 01 | 328.557 | 82.139 | 0.072059 | 4 | 22.857 |
| 0.53085946 01 | 0.38816396 01 | 0.65580886 01 | 36.074 | 7.215 | 0.057567 | 5 | 28.571 |
| -0.10058076 01 | -0.69902786 00 | 0.19979416 01 | 199.287 | 33.215 | 0.017538 | 6 | 34.286 |
| -0.20126296 01 | 0.14318676 01 | 0.24780006 01 | 144.570 | 20.653 | 0.021682 | 7 | 40.000 |
| -0.24596856 01 | 0.81824066 00 | 0.25922136 01 | 161.600 | 20.200 | 0.022754 | 8 | 45.714 |
| 0.27567946 01 | -0.17683666-01 | 0.27568836 01 | 359.551 | 39.950 | 0.019811 | 9 | 51.429 |
| 0.29504636 00 | 0.17087306 00 | 0.34094946 00 | 30.077 | 3.008 | 0.002993 | | 57.143 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1007C T 498 CTR 563 CR 37.0 IR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.13270906 02 | | | | | | | |
| -0.40867336-02 | -0.90136216 00 | 0.90137136 00 | 269.740 | 269.740 | 1.000000 | 1 | 5.714 |
| -0.79791936-02 | 0.52188496-02 | 0.95022016-02 | 145.450 | 72.725 | 0.010209 | 2 | 11.429 |
| -0.13759866-01 | -0.44156156-01 | 0.46864326-01 | 250.358 | 83.453 | 0.052014 | 3 | 17.143 |
| -0.33157356-01 | -0.22736286-01 | 0.40203836-01 | 214.439 | 53.610 | 0.044603 | 4 | 22.857 |
| 0.98266046-02 | -0.40845056-02 | 0.10641686-01 | 337.429 | 67.486 | 0.011806 | 5 | 28.571 |
| 0.19407096-01 | -0.34661036-02 | 0.19714176-01 | 349.874 | 58.312 | 0.021871 | 6 | 34.286 |
| -0.33776766-02 | -0.40158396-02 | 0.57190256-02 | 233.800 | 33.400 | 0.006345 | 7 | 40.000 |
| -0.77909886-02 | -0.19623736-01 | 0.21116496-01 | 248.326 | 31.041 | 0.023427 | 8 | 45.714 |
| -0.28293936-02 | -0.74802406-02 | 0.79974726-02 | 249.281 | 27.698 | 0.008873 | 9 | 51.429 |
| 0.63410336-02 | -0.95396026-02 | 0.11454886-01 | 303.612 | 30.361 | 0.012708 | 10 | 57.143 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 5

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 2 FL. BEND A

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -3.1297477E 00 | | | | | | | |
| -0.1621346E 04 | -0.8426874E 04 | 0.8580645E 04 | 259.108 | 259.108 | 1.000000 | 1 | 5.917 |
| -0.6394773E 03 | 0.3479774E 03 | 0.7278330E 03 | 151.474 | 75.737 | 0.084823 | 2 | 11.834 |
| 0.2009609E 04 | -0.6684897E 03 | 0.2063477E 04 | 346.879 | 115.626 | 0.240480 | 3 | 17.751 |
| -0.1619682E 02 | 0.9912300E 03 | 0.9916517E 03 | 91.069 | 22.897 | 0.068929 | 4 | 23.669 |
| 0.5294822E 03 | -0.7942841E 03 | 0.9545232E 03 | 303.691 | 60.738 | 0.111241 | 5 | 29.586 |
| 0.6296461E 02 | 0.1227174E 03 | 0.1379719E 03 | 62.830 | 10.473 | 0.016074 | 6 | 35.503 |
| 0.8866850E 02 | 0.1265998E 03 | 0.1500876E 03 | 57.487 | 8.212 | 0.017491 | 7 | 41.420 |
| 0.5281250E 02 | -0.2961479E 01 | 0.5289544E 02 | 356.790 | 44.559 | 0.006165 | 8 | 47.337 |
| -0.6783637E 01 | 0.1733919E 02 | 0.1861843E 02 | 111.367 | 12.374 | 0.002170 | 9 | 53.254 |
| -0.6117404E 02 | 0.5490847E 02 | 0.8330885E 02 | 139.316 | 13.932 | 0.009709 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2774089E 04 | | | | | | | |
| 0.3450358E 03 | -0.2381098E 04 | 0.2405958E 04 | 278.245 | 278.245 | 1.000000 | 1 | 5.917 |
| -0.5128683E 02 | 0.2090850E 02 | 0.5541228E 02 | 157.751 | 78.876 | 0.023031 | 2 | 11.834 |
| -0.7464186E 02 | -0.4546544E 02 | 0.8739857E 02 | 211.346 | 70.449 | 0.036326 | 3 | 17.751 |
| 0.2556413E 02 | -0.1911735E 03 | 0.1928752E 03 | 277.616 | 69.404 | 0.080166 | 4 | 23.669 |
| -0.2109338E 03 | 0.4523704E 03 | 0.4991311E 03 | 114.999 | 28.750 | 0.207456 | 5 | 29.586 |
| -0.1173749E 03 | 0.7098639E 01 | 0.1175889E 03 | 176.539 | 29.423 | 0.048874 | 6 | 35.503 |
| -0.1727282E 03 | -0.9375458E 02 | 0.1965323E 03 | 208.492 | 29.785 | 0.081686 | 7 | 41.420 |
| -0.6936812E 02 | 0.6405566E 02 | 0.9441371E 02 | 137.277 | 17.160 | 0.039242 | 8 | 47.337 |
| -0.4094119E 02 | -0.7102668E 01 | 0.4115862E 02 | 189.937 | 21.104 | 0.017107 | 9 | 53.254 |
| -0.4492216E 01 | 0.3859979E 02 | 0.3879610E 02 | 96.590 | 9.659 | 0.016125 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1202106E 04 | | | | | | | |
| 0.6600628E 01 | -0.8089892E 03 | 0.8089360E 03 | 270.468 | 27.468 | 1.000000 | 1 | 5.917 |
| -0.2914089E 03 | -0.4799071E 02 | 0.2971170E 03 | 193.398 | 9.699 | 0.256036 | 2 | 11.834 |
| -0.3965359E 03 | 0.3188470E 02 | 0.3958220E 03 | 175.380 | 58.460 | 0.489312 | 3 | 17.751 |
| -0.1304095E 02 | -0.1296404E 03 | 0.1332033E 03 | 255.638 | 63.909 | 0.164665 | 4 | 23.669 |
| -0.1197344E 03 | 0.2539640E 03 | 0.2790916E 03 | 114.499 | 22.900 | 0.345011 | 5 | 29.586 |
| -0.6142825E 01 | 0.2000525E 02 | 0.2092703E 02 | 107.069 | 17.845 | 0.025870 | 6 | 35.503 |
| -0.4141139E 01 | -0.9762878E 01 | 0.1060489E 02 | 247.015 | 35.288 | 0.013110 | 7 | 41.420 |
| 0.2794359E 02 | 0.2643385E 02 | 0.3673784E 02 | 43.689 | 5.211 | 0.045615 | 8 | 47.337 |
| 0.4731346E 01 | 0.1497400E 02 | 0.1570370E 02 | 72.465 | 8.052 | 0.019413 | 9 | 53.254 |
| -0.6899809E 01 | -0.2472745E 02 | 0.2565598E 02 | 254.538 | 28.493 | 0.031716 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4373826E 03 | | | | | | | |
| -0.1746632E 03 | -0.5646609E 03 | 0.5910569E 03 | 252.812 | 252.812 | 0.993795 | 1 | 5.917 |
| -0.3694409E 03 | -0.7330248E 02 | 0.3768503E 03 | 191.226 | 95.613 | 0.630127 | 2 | 11.834 |
| -0.6828993E 03 | 0.1432978E 03 | 0.6976899E 03 | 166.630 | 55.543 | 1.000000 | 3 | 17.751 |
| -0.6692361E 02 | 0.1943695E 02 | 0.6809442E 02 | 164.897 | 41.224 | 0.109885 | 4 | 23.669 |
| 0.3892325E 02 | -0.6885749E 02 | 0.6790431E 02 | 298.712 | 59.342 | 0.109578 | 5 | 29.586 |
| 0.6794997E 02 | 0.2899721E 02 | 0.7351030E 02 | 23.233 | 3.872 | 0.118624 | 6 | 35.503 |
| 0.6868009E 02 | 0.3864403E 02 | 0.7880551E 02 | 29.365 | 4.195 | 0.127169 | 7 | 41.420 |
| 0.5199199E 02 | -0.2654337E 02 | 0.5784189E 02 | 332.684 | 41.586 | 0.093360 | 8 | 47.337 |
| 0.9153293E 01 | 0.6222913E 01 | 0.1106009E 02 | 34.208 | 3.801 | 0.017861 | 9 | 53.254 |
| 0.2693270E 02 | -0.3839573E 01 | 0.2658302E 02 | 352.131 | 39.213 | 0.042897 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 5

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 10 FL. SEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1836418E 04 | | | | | | | |
| -0.2552330E 03 | -0.5172856E 03 | 0.5759436E 03 | 243.916 | 243.916 | 0.802150 | 1 | 5.917 |
| -0.5792297E 03 | -0.9748264E 02 | 0.5834312E 03 | 189.618 | 94.809 | 0.812578 | 2 | 11.834 |
| -0.7053220E 03 | 0.1444375E 03 | 0.7180000E 03 | 168.395 | 56.132 | 1.000000 | 3 | 17.751 |
| -0.3953394E 02 | 0.1387870E 01 | 0.1443078E 03 | 105.900 | 26.475 | 0.200986 | 4 | 23.669 |
| 0.1755135E 03 | -0.2601051E 03 | 0.3137786E 03 | 304.011 | 60.802 | 0.437017 | 5 | 29.586 |
| 0.1978246E 02 | 0.2346252E 02 | 0.3036443E 02 | 50.585 | 8.431 | 0.042297 | 6 | 35.503 |
| -0.1400532E 02 | -0.1994302E 02 | 0.2437180E 02 | 234.913 | 33.559 | 0.033944 | 7 | 41.420 |
| -0.2518095E 02 | -0.4220396E 02 | 0.4914523E 02 | 239.178 | 29.897 | 0.068447 | 8 | 47.337 |
| -0.3459926E 02 | 0.1328586E 01 | 0.3462335E 02 | 177.921 | 19.769 | 0.051007 | 9 | 53.254 |
| -0.6214273E 01 | 0.4119177E 02 | 0.4165902E 02 | 98.580 | 9.859 | 0.058020 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 11 FL. SEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1812832E 04 | | | | | | | |
| -0.2143940E 03 | -0.4441829E 03 | 0.4931780E 03 | 244.244 | 244.244 | 0.681879 | 1 | 5.917 |
| -0.6879595E 03 | -0.1504467E 03 | 0.5848025E 03 | 192.734 | 96.367 | 0.946824 | 2 | 11.834 |
| -0.6919216E 03 | 0.2106032E 03 | 0.7232627E 03 | 163.071 | 54.357 | 1.000000 | 3 | 17.751 |
| -0.3157144E 02 | 0.2059591E 03 | 0.2083648E 03 | 98.715 | 24.679 | 0.288090 | 4 | 23.669 |
| 0.2108468E 03 | -0.3423499E 03 | 0.4020691E 03 | 301.628 | 60.326 | 0.555910 | 5 | 29.586 |
| 0.3800938E 02 | -0.7256782E 01 | 0.3869591E 02 | 349.191 | 58.198 | 0.053502 | 6 | 35.503 |
| -0.6700943E 02 | -0.7312766E 02 | 0.9918625E 02 | 227.500 | 32.500 | 0.137137 | 7 | 41.420 |
| -0.6291362E 02 | 0.6798706E 00 | 0.6291720E 02 | 179.381 | 22.423 | 0.086991 | 8 | 47.337 |
| -0.1966795E 02 | -0.4825783E 02 | 0.5211186E 02 | 247.626 | 27.536 | 0.072051 | 9 | 53.254 |
| -0.9608194E 01 | -0.1597703E 01 | 0.9740126E 01 | 189.441 | 18.944 | 0.013467 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 13 FL. SEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1873818E 04 | | | | | | | |
| -0.9799364E 02 | -0.1961043E 03 | 0.2191995E 03 | 243.462 | 243.462 | 0.316804 | 1 | 5.917 |
| -0.6742695E 03 | -0.1552416E 03 | 0.6919097E 03 | 192.986 | 96.493 | 1.000000 | 2 | 11.834 |
| -0.6301843E 03 | 0.2007507E 03 | 0.6613672E 03 | 162.379 | 54.110 | 0.955887 | 3 | 17.751 |
| -0.1312363E 02 | 0.2197679E 03 | 0.2201597E 03 | 93.419 | 23.355 | 0.318191 | 4 | 23.669 |
| 0.2384555E 03 | -0.3174902E 03 | 0.3930789E 03 | 307.346 | 61.469 | 0.568107 | 5 | 29.586 |
| 0.2289519E 01 | -0.2853685E 02 | 0.2862619E 02 | 274.579 | 45.763 | 0.041373 | 6 | 35.503 |
| -0.1113e.2E 03 | -0.1209188E 03 | 0.1643122E 03 | 227.333 | 32.476 | 0.237476 | 7 | 41.420 |
| -0.7998215E 02 | -0.1449049E 02 | 0.7735152E 02 | 190.792 | 23.850 | 0.111796 | 8 | 47.337 |
| -0.2541882E 02 | -0.9124179E 01 | 0.2700679E 02 | 199.744 | 22.194 | 0.039032 | 9 | 53.254 |
| 0.4548811E 01 | 0.9059041E 00 | 0.4639118E 01 | 11.261 | 1.126 | 0.006705 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 14 FL. SEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1658074E 04 | | | | | | | |
| -0.2695738E 02 | -0.8934874E 02 | 0.9332536E 02 | 253.214 | 253.214 | 0.178182 | 1 | 5.917 |
| -0.5283376E 03 | -0.1264209E 03 | 0.5233218E 03 | 193.986 | 96.993 | 1.000000 | 2 | 11.834 |
| -0.5061760E 04 | 0.1104860E 03 | 0.5190937E 03 | 167.681 | 55.894 | 0.989085 | 3 | 17.751 |
| 0.6356046E 01 | 0.2092542E 03 | 0.2094365GE 03 | 58.178 | 22.049 | 0.399638 | 4 | 23.669 |
| 0.2085866E 03 | -0.2094177E 03 | 0.2955742E 03 | 314.888 | 62.977 | 0.564265 | 5 | 29.586 |
| -0.1033067E 02 | -0.1936122E 02 | 0.2194492E 02 | 241.917 | 40.319 | 0.041894 | 6 | 35.503 |
| -0.1099064E 03 | -0.1064915E 03 | 0.1530355E 03 | 224.096 | 32.014 | 0.292152 | 7 | 41.420 |
| -0.7724489E 02 | 0.7416110E 00 | 0.7724890E 02 | 179.450 | 22.431 | 0.147471 | 8 | 47.337 |
| -0.3137342E 01 | -0.7428107E 01 | 0.8063478E 01 | 247.103 | 27.456 | 0.015396 | 9 | 53.254 |
| -0.1103094E 02 | -0.1806320E 02 | 0.1948608E 02 | 235.522 | 23.552 | 0.037200 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 5

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1249477E 05 | | | | | | | |
| 0.2399165E 05 | -0.2736207E 04 | 0.2414718E 05 | 353.493 | 353.493 | 1.000000 | 1 | 5.917 |
| 0.6290671E 04 | 0.2777134E 04 | 0.6876383E 04 | 23.821 | 11.910 | 0.284770 | 2 | 11.834 |
| 0.3698083E 04 | -0.4224678E 03 | 0.3722201E 04 | 353.465 | 117.822 | 0.153732 | 3 | 17.751 |
| 0.2306810E 03 | -0.3706096E 03 | 0.4365376E 03 | 301.900 | 75.475 | 0.018078 | 4 | 23.669 |
| 0.9053252E 03 | -0.8579927E 03 | 0.9107003E 03 | 289.589 | 57.918 | 0.037715 | 5 | 29.586 |
| -0.8278178E 02 | -0.3207939E 03 | 0.3313027E 03 | 255.530 | 42.588 | 0.013720 | 6 | 35.503 |
| 0.2667974E 03 | -0.4086284E 03 | 0.4880142E 03 | 303.141 | 43.306 | 0.020210 | 7 | 41.420 |
| 0.1738180E 03 | 0.1300779E 03 | 0.2171013E 03 | 36.810 | 4.601 | 0.008991 | 8 | 47.337 |
| 0.2112155E 03 | 0.2434388E 03 | 0.3222942E 03 | 49.054 | 5.450 | 0.013347 | 9 | 53.254 |
| 0.1074935E 03 | 0.8016188E 02 | 0.1340924E 03 | 36.713 | 3.671 | 0.005553 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1358777E 05 | | | | | | | |
| 0.1484816E 05 | -0.6505239E 03 | 0.1486241E 05 | 357.491 | 357.491 | 1.000000 | 1 | 5.917 |
| 0.4182570E 04 | 0.1941140E 04 | 0.4457465E 04 | 20.227 | 10.114 | 0.299919 | 2 | 11.834 |
| 0.2567590E 04 | 0.1984102E 03 | 0.2579244E 04 | 4.419 | 1.473 | 0.173277 | 3 | 17.751 |
| -0.3555527E 03 | 0.1002609E 03 | 0.3694128E 03 | 164.255 | 41.064 | 0.024856 | 4 | 23.669 |
| -0.4361218E 02 | -0.7638425E 03 | 0.7650864E 03 | 266.732 | 53.346 | 0.051478 | 5 | 29.586 |
| -0.9253461E 02 | 0.1530034E 03 | 0.1788091E 03 | 121.165 | 20.194 | 0.012031 | 6 | 35.503 |
| 0.2012198E 03 | 0.2484484E 03 | 0.3197126E 03 | 50.936 | 7.285 | 0.021511 | 7 | 41.420 |
| 0.2587466E 02 | -0.2414637E 03 | 0.2427461E 03 | 276.116 | 34.515 | 0.016340 | 8 | 47.337 |
| 0.7799913E 02 | -0.3068196E 02 | 0.8381671E 02 | 338.527 | 37.614 | 0.005644 | 9 | 53.254 |
| 0.4879720E 02 | -0.7648517E 02 | 0.9080999E 02 | 302.504 | 30.250 | 0.006110 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 8 CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8820531E 04 | | | | | | | |
| 0.5962184E 04 | -0.5912439E 03 | 0.5991426E 04 | 354.337 | 354.337 | 1.000000 | 1 | 5.917 |
| 0.2038413E 04 | 0.4370791E 03 | 0.2084746E 04 | 12.102 | 6.051 | 0.347955 | 2 | 11.834 |
| 0.1102672E 04 | -0.1256050E 03 | 0.1109802E 04 | 353.501 | 117.834 | 0.185232 | 3 | 17.751 |
| -0.3405542E 03 | 0.2783965E 03 | 0.4398655E 03 | 140.735 | 35.184 | 0.073416 | 4 | 23.669 |
| -0.1118142E 03 | -0.2276441E 03 | 0.2536402E 03 | 243.843 | 40.769 | 0.042334 | 5 | 29.586 |
| 0.4596169E 02 | 0.9454350E 02 | 0.1051235E 03 | 64.074 | 12.679 | 0.017546 | 6 | 35.503 |
| 0.2644116E 03 | 0.2801277E 03 | 0.3852075E 03 | 46.853 | 6.665 | 0.064293 | 7 | 41.420 |
| -0.2496672E 03 | -0.4128191E 03 | 0.4824441E 03 | 238.835 | 29.854 | 0.080522 | 8 | 47.337 |
| -0.3151082E 03 | -0.9994644E 02 | 0.3305786E 03 | 197.598 | 21.955 | 0.055175 | 9 | 53.254 |
| -0.1199651E 03 | -0.1272839E 02 | 0.1206384E 03 | 186.056 | 18.606 | 0.020135 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 50.1 TR 12 CH. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6130812E 04 | | | | | | | |
| 0.2280873E 04 | -0.7072466E 02 | 0.2281950E 04 | 358.239 | 358.239 | 1.000000 | 1 | 5.917 |
| 0.9308159E 03 | 0.1178065E 02 | 0.9308904E 03 | 0.725 | 0.363 | 0.407936 | 2 | 11.834 |
| 0.3704045E 03 | -0.1474732E 03 | 0.3986824E 03 | 338.298 | 112.763 | 0.174711 | 3 | 17.751 |
| -0.2004054E 03 | 0.1658757E 03 | 0.2601479E 03 | 140.585 | 35.098 | 0.114007 | 4 | 23.669 |
| -0.3378558E 02 | -0.4896193E 02 | 0.5948727E 02 | 235.393 | 47.079 | 0.026069 | 5 | 29.586 |
| 0.6446375E 02 | 0.2312946E 02 | 0.6848753E 02 | 19.736 | 3.290 | 0.030013 | 6 | 35.503 |
| 0.1135721E 03 | 0.1604833E 03 | 0.1966041E 03 | 54.713 | 7.816 | 0.086156 | 7 | 41.420 |
| -0.1908754E 03 | -0.2331077E 03 | 0.3012849E 03 | 230.688 | 28.836 | 0.132030 | 8 | 47.337 |
| -0.2833699E 03 | -0.8000671E 02 | 0.2944478E 03 | 195.766 | 21.752 | 0.129033 | 9 | 53.254 |
| -0.9358197E 02 | -0.1535147E 02 | 0.9483272E 02 | 189.316 | 15.932 | 0.041558 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 5

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 5C.1 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1532669E 03 | | | | | | | |
| 0.9242792E 02 | 0.5329349E 02 | 0.7475888E 02 | 45.469 | 45.469 | C.992613 | 1 | 5.917 |
| 0.1107395E 02 | 0.1691244E 02 | 0.1988196E 02 | 56.152 | 28.076 | P.144949 | 2 | 11.834 |
| -0.2611147E 02 | -0.1221577E 02 | 0.2882759E 02 | 205.072 | 68.357 | 0.224660 | 3 | 17.751 |
| 0.6351312E 02 | -0.8442289E 01 | 0.6407837E 02 | 352.384 | 88.096 | 0.499376 | 4 | 23.669 |
| 0.5892799E 02 | -0.1149986E 03 | 0.1283164E 03 | 296.337 | 59.267 | 1.000000 | 5 | 29.586 |
| 0.2600264E 02 | -0.2210389E 02 | 0.3412794E 02 | 319.633 | 53.272 | 0.265967 | 6 | 35.503 |
| 0.1797697E 02 | 0.1095998E 02 | 0.2105449E 02 | 31.369 | 4.481 | 0.164083 | 7 | 41.420 |
| -0.1569819E 01 | -0.4918980E 00 | 0.1645082E 01 | 197.398 | 24.675 | 0.012821 | 8 | 47.337 |
| 0.1291231E 02 | -0.1904151E 01 | 0.1305195E 02 | 351.611 | 39.068 | 0.101717 | 9 | 53.254 |
| 0.2003166E 01 | 0.5331312E 01 | 0.5695221E 01 | 69.407 | 6.941 | 0.044384 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 5C.1 TR 19 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4930309E 02 | | | | | | | |
| 0.5364832E 02 | 0.5322003E 02 | 0.7556792E 02 | 44.770 | 44.770 | 1.000000 | 1 | 5.917 |
| -0.1825342E 02 | -0.7660308E 01 | 0.1979572E 02 | 202.767 | 101.383 | 0.261959 | 2 | 11.834 |
| 0.1162918E 02 | -0.2344679E 01 | 0.1185927E 02 | 348.597 | 116.199 | 0.156935 | 3 | 17.751 |
| 0.2937473E 02 | 0.5586053E 01 | 0.2989740E 02 | 10.729 | 2.682 | 0.395636 | 4 | 23.669 |
| 0.1117495E 02 | -0.5081459E 02 | 0.5202885E 02 | 282.483 | 94.081 | 0.688905 | 5 | 29.586 |
| 0.4073716E 01 | 0.4397583E-01 | 0.4073951E 01 | 0.618 | 0.103 | 0.053911 | 6 | 35.503 |
| 0.4544323E 01 | 0.5828762E 01 | 0.6821778E 01 | 58.697 | 8.385 | 0.090273 | 7 | 41.420 |
| -0.4337419E 01 | -0.9523279E 00 | 0.4440734E 01 | 192.384 | 24.048 | 0.058765 | 8 | 47.337 |
| 0.1608695E 01 | -0.3861749E 01 | 0.4184948E 01 | 292.720 | 32.524 | 0.055115 | 9 | 53.254 |
| 0.3825784F 00 | -0.4928337E 01 | 0.4933193E 01 | 274.443 | 27.444 | 0.065414 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 5C.1 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3484497E C2 | | | | | | | |
| -0.3210392E 01 | 0.2247637E 02 | 0.2310052E 02 | 97.989 | 97.989 | 0.970710 | 1 | 5.917 |
| 0.2659235E 01 | 0.6356594E 01 | 0.6890413E 01 | 67.298 | 33.649 | 0.289543 | 2 | 11.834 |
| 0.1837910F 02 | 0.1511704E 02 | 0.2379755E 02 | 39.437 | 13.146 | 1.000000 | 3 | 17.751 |
| -0.2008962F C2 | 0.5168336E 01 | 0.2074158E 02 | 165.594 | 41.398 | 0.871985 | 4 | 23.669 |
| -0.3928426E 01 | 0.4363267E 01 | 0.5871167E 01 | 131.998 | 26.400 | 0.246713 | 5 | 29.586 |
| -0.1405919E 01 | 0.2670094E 01 | 0.3022740E 01 | 117.709 | 19.618 | 0.127019 | 6 | 35.503 |
| 0.2722009E C1 | 0.1014397E 01 | 0.2904875E 01 | 20.439 | 2.920 | 0.122006 | 7 | 41.420 |
| 0.1617393F C1 | 0.2483183E 01 | 0.2946733E 01 | 56.710 | 7.089 | 0.123829 | 8 | 47.337 |
| -0.2999880E 00 | -0.1489728E 01 | 0.2012215E 01 | 261.426 | 29.047 | 0.084556 | 9 | 53.254 |
| 0.1302578E 01 | 0.6016846E 00 | 0.1434829E 01 | 24.793 | 2.479 | 0.060293 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 354 CR 5C.1 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.7557105E C1 | | | | | | | |
| 0.1432314E 01 | -0.1847809E 01 | 0.2369671E 01 | 307.188 | 307.188 | 1.000000 | 1 | 5.917 |
| 0.1944469E-01 | 0.3171359E-01 | 0.3749626E-01 | 63.308 | 31.654 | 0.014979 | 2 | 11.834 |
| -0.5773902E-01 | -0.5008068E-01 | 0.8626942E-01 | 225.458 | 75.219 | C.034861 | 3 | 17.751 |
| 0.2142397E-C1 | -0.3230042E-02 | 0.2166604E-01 | 351.426 | 87.857 | 0.009143 | 4 | 23.669 |
| -0.9017836E-02 | -0.1498288E-01 | 0.1580080E-01 | 251.484 | 50.297 | 0.006668 | 5 | 29.586 |
| -0.1492140E-01 | 0.1876440E-01 | 0.2397417E-01 | 128.491 | 21.415 | 0.010117 | 6 | 35.503 |
| 0.9276601E-03 | -0.4585422E-02 | 0.4678[ 3E-02 | 281.437 | 40.205 | C.001974 | 7 | 41.420 |
| -0.2428679E-C2 | 0.8357763E-02 | 0.8703429E-02 | 106.202 | 13.275 | 0.003673 | 8 | 47.337 |
| -0.1416680E-01 | 0.2369984E-01 | 0.2761124E-01 | 120.869 | 13.430 | 0.011652 | 9 | 53.254 |
| 0.1045020E-01 | 0.1973510E-01 | 0.2189054E-01 | 61.485 | 6.149 | 0.009238 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 5

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.11288335 05 | | | | | | | |
| -0.1470217E 04 | -0.5675891E 04 | 0.5863215E 04 | 255.478 | 255.478 | 1.000000 | 1 | 5.882 |
| -0.3887935E 04 | 0.7978552E 03 | 0.3968995E 04 | 168.403 | 84.202 | 0.676924 | 2 | 11.765 |
| 0.1306871E 04 | -0.4252900E 04 | 0.4449168E 04 | 287.082 | 95.694 | 0.759827 | 3 | 17.647 |
| 0.8416162E 03 | 0.3586289E 03 | 0.9149496E 03 | 23.080 | 5.770 | 0.156035 | 4 | 23.529 |
| -0.1287249E 04 | -0.1603568E 04 | 0.2056317E 04 | 231.249 | 46.249 | 0.350715 | 5 | 29.412 |
| 0.3511002E 02 | -0.1086059E 03 | 0.1144516E 03 | 288.391 | 49.065 | 0.019520 | 6 | 35.294 |
| 0.2291403E 03 | 0.1054774E 02 | 0.2294394E 03 | 2.706 | 0.387 | 0.038109 | 7 | 41.176 |
| -0.3126518E 01 | 0.2326344E 02 | 0.2367259E 02 | 97.695 | 12.207 | 0.004053 | 8 | 47.059 |
| 0.7629860E 02 | 0.1544303E 02 | 0.7784572E 02 | 11.442 | 1.271 | 0.013277 | 9 | 52.941 |
| 0.1189444E 02 | -0.1198839E 02 | 0.1689971E 02 | 314.678 | 31.468 | 0.002872 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.4277095E 04 | | | | | | | |
| 0.1809604E 04 | -0.3059316E 04 | 0.3554449E 04 | 300.604 | 300.604 | 1.000000 | 1 | 5.882 |
| -0.3900447E 03 | -0.4451720E 02 | 0.3928619E 03 | 187.248 | 93.624 | 0.099274 | 2 | 11.765 |
| -0.3428329E 02 | -0.1782790E 02 | 0.4132462E 02 | 198.084 | 66.028 | 0.011626 | 3 | 17.647 |
| -0.1623536E 03 | -0.2301140E 03 | 0.2814221E 03 | 234.796 | 58.699 | 0.079231 | 4 | 23.529 |
| 0.7890378E 03 | 0.5539888E 03 | 0.9640974E 03 | 35.073 | 7.015 | 0.271237 | 5 | 29.412 |
| -0.8000000E 02 | 0.7262354E 02 | 0.1140972E 03 | 140.468 | 23.411 | 0.032100 | 6 | 35.294 |
| -0.2292660E 03 | 0.1205364E 02 | 0.2256332E 03 | 176.734 | 25.248 | 0.063479 | 7 | 41.176 |
| -0.5833904E 02 | -0.1701654E 02 | 0.5313643E 02 | 198.678 | 24.835 | 0.014949 | 8 | 47.059 |
| -0.3000362E 02 | 0.1657942E 02 | 0.3468682E 02 | 151.954 | 16.839 | 0.009752 | 9 | 52.941 |
| 0.1453015E 02 | -0.1586709E 02 | 0.2291309E 02 | 316.172 | 31.617 | 0.006446 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1979208E 04 | | | | | | | |
| 0.6690581E 03 | -0.1132549E 04 | 0.1325469E 04 | 301.317 | 301.317 | 1.000000 | 1 | 5.882 |
| -0.1098089E 03 | 0.5985526E 02 | 0.1981973E 03 | 162.671 | 81.335 | 0.149504 | 2 | 11.765 |
| -0.2774487E 03 | 0.6883247E 03 | 0.6688075E 03 | 114.517 | 38.172 | 0.504849 | 3 | 17.647 |
| -0.1417925E 03 | -0.7205875E 02 | 0.1590521E 03 | 206.948 | 51.735 | 0.119976 | 4 | 23.529 |
| 0.4773598E 03 | 0.4363010E 03 | 0.6467188E 03 | 42.426 | 8.485 | 0.487834 | 5 | 29.412 |
| 0.5491102E 01 | 0.2735197E 02 | 0.2789771E 02 | 78.648 | 13.108 | 0.021044 | 6 | 35.294 |
| -0.2162418E 02 | 0.2198075E 02 | 0.3083459E 02 | 134.932 | 19.219 | 0.023259 | 7 | 41.176 |
| -0.5195040E 01 | 0.1725896E 02 | 0.1799812E 02 | 106.478 | 15.310 | 0.013576 | 8 | 47.059 |
| 0.9309514E 01 | 0.1191500E 02 | 0.1517252E 02 | 51.749 | 5.750 | 0.011445 | 9 | 52.941 |
| -0.7507154E 01 | 0.2542868E 02 | 0.2609746E 02 | 106.207 | 10.621 | 0.020289 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7049892E 02 | | | | | | | |
| 0.4795862E 03 | -0.8648726E 03 | 0.9897151E 03 | 299.395 | 299.395 | 0.831017 | 1 | 5.882 |
| -0.4711204E 03 | -0.2941873E 02 | 0.4718054E 03 | 183.688 | 91.844 | 0.404323 | 2 | 11.765 |
| -0.4098099E 03 | 0.1099387E 04 | 0.1164902E 04 | 114.788 | 38.263 | 1.000000 | 3 | 17.647 |
| -0.3978955E 02 | 0.5594095E 02 | 0.6820241E 02 | 125.560 | 31.390 | 0.058516 | 4 | 23.529 |
| -0.2098246E 03 | -0.4957320E 02 | 0.2137350E 03 | 191.763 | 38.353 | 0.183364 | 5 | 29.412 |
| 0.3492009E 02 | -0.2073821E 02 | 0.4061523E 02 | 322.134 | 53.689 | 0.040119 | 6 | 35.294 |
| 0.9969911E 02 | 0.1203101E 03 | 0.1004523E 03 | 7.224 | 1.032 | 0.086185 | 7 | 41.176 |
| 0.3621008E 02 | 0.3499511E 02 | 0.5085275E 02 | 43.668 | 5.457 | 0.042894 | 8 | 47.059 |
| 0.1531909E 02 | 0.4165900E 02 | 0.1438571E 02 | 69.815 | 7.757 | 0.030837 | 9 | 52.941 |
| 0.9321390E 01 | 0.1204174E 02 | 0.1326491E 02 | 75.499 | 7.550 | 0.011367 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 8

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1026735E 04 | | | | | | | |
| 0.4985940E 03 | -0.8470684E 03 | 0.9829092E 03 | 300.481 | 300.481 | 0.850827 | 1 | 5.882 |
| -0.8565723E 03 | -0.1010223E 03 | 0.8625088E 03 | 186.726 | 93.363 | 0.746606 | 2 | 11.765 |
| -0.6124880E 03 | 0.9795085E 03 | 0.1155239E 04 | 122.018 | 40.673 | 1.000000 | 3 | 17.647 |
| 0.5107559E 02 | 0.2165883E 03 | 0.2225291E 03 | 76.731 | 19.183 | 0.192626 | 4 | 23.529 |
| -0.5679878E 03 | -0.4410144E 03 | 0.7190991E 03 | 217.828 | 43.566 | 0.622468 | 5 | 29.412 |
| 0.2555188E 02 | -0.9747809E 01 | 0.2734808E 02 | 339.118 | 56.520 | 0.023673 | 6 | 35.294 |
| -0.8950907E 01 | 0.1495451E 02 | 0.1742859E 02 | 120.902 | 17.277 | 0.015087 | 7 | 41.176 |
| -0.1042591E 01 | -0.9651523E 01 | 0.9789388E 01 | 253.794 | 31.724 | 0.008495 | 8 | 47.059 |
| 0.1585693E 01 | 0.2140945E 02 | 0.2146908E 02 | 85.764 | 9.529 | 0.018583 | 9 | 52.941 |
| 0.1390636E 02 | -0.1598102E 02 | 0.2110909E 02 | 311.207 | 31.121 | 0.018272 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1090654E 04 | | | | | | | |
| 0.3467908E 03 | -0.6536804E 03 | 0.7399741E 03 | 297.947 | 297.947 | 0.720045 | 1 | 5.882 |
| -0.9415432E 03 | -0.6837515E 02 | 0.9440225E 03 | 184.154 | 92.077 | 0.918592 | 2 | 11.765 |
| -0.6424485E 03 | 0.8021191E 03 | 0.1027684E 04 | 128.693 | 42.898 | 1.000000 | 3 | 17.647 |
| 0.1900475E 03 | 0.3916809E 03 | 0.4353525E 03 | 64.117 | 16.029 | 0.423625 | 4 | 23.529 |
| -0.6655127E 03 | -0.5452522E 03 | 0.8603528E 03 | 219.328 | 43.866 | 0.837176 | 5 | 29.412 |
| -0.2523785E 02 | -0.5799585E 02 | 0.6324905E 02 | 246.483 | 41.080 | 0.061545 | 6 | 35.294 |
| -0.1150702E 03 | -0.2787436E 02 | 0.1183982E 03 | 193.617 | 27.660 | 0.115209 | 7 | 41.176 |
| -0.2169218E 02 | -0.6231049E 02 | 0.6606267E 02 | 249.182 | 31.148 | 0.064867 | 8 | 47.059 |
| -0.8409294E 01 | -0.3290189E 02 | 0.3399953E 02 | 255.663 | 28.407 | 0.033045 | 9 | 52.941 |
| -0.1342769E 02 | 0.3358438E 02 | 0.3616922E 02 | 111.793 | 11.179 | 0.035195 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1958505E 04 | | | | | | | |
| 0.6658398E 02 | -0.4198869E 03 | 0.4251135E 03 | 279.011 | 279.011 | 0.451107 | 1 | 5.882 |
| -0.9423557E 03 | 0.6414469E 01 | 0.9423774E 03 | 179.610 | 89.805 | 1.000000 | 2 | 11.765 |
| -0.5755127E 03 | 0.9430286E 03 | 0.7912600E 03 | 136.664 | 45.555 | 0.839642 | 3 | 17.647 |
| 0.1654913E 03 | 0.3310576E 01 | 0.3701167E 03 | 63.440 | 15.860 | 0.392748 | 4 | 23.529 |
| -0.5376880E 03 | -0.4434604E 03 | 0.6969687E 03 | 219.514 | 43.903 | 0.739586 | 5 | 29.412 |
| -0.3300862E 02 | -0.4413051E 02 | 0.5510962E 02 | 233.204 | 38.867 | 0.058479 | 6 | 35.294 |
| -0.1171592E 03 | -0.9475002E 07 | 0.1293207E 03 | 205.047 | 29.292 | 0.137228 | 7 | 41.176 |
| -0.3089825E 02 | -0.5591248E 01 | 0.3140005E 02 | 190.257 | 23.782 | 0.033320 | 8 | 47.059 |
| -0.1034417E 02 | -0.4730502E 01 | 0.1137470E 02 | 204.575 | 22.731 | 0.012079 | 9 | 52.941 |
| 0.2004967E 02 | 0.1551294E 07 | 0.2535034E 02 | 37.730 | 3.773 | 0.026900 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1657871E 04 | | | | | | | |
| -0.2011019E 03 | -0.7974771E 02 | 0.2163369E 03 | 201.631 | 201.631 | .183207 | 1 | 5.882 |
| -0.7814822E 03 | -0.6052002E 02 | 0.7838833E 03 | 184.944 | 92.272 | .000000 | 2 | 11.765 |
| -0.3484109E 03 | 0.3896313E 03 | 0.5226877E 03 | 131.803 | 43.934 | 0.664291 | 3 | 17.647 |
| 0.4859315E 02 | 0.2791443E 03 | 0.2833418E 03 | 80.125 | 20.031 | 0.372923 | 4 | 23.529 |
| -0.3930610E 03 | -0.3652202E 03 | 0.5079741E 03 | 225.970 | 45.194 | 0.664989 | 5 | 29.412 |
| 0.1606769E 02 | 0.9381824E 02 | 0.9518617E 02 | 80.282 | 13.380 | 0.124886 | 6 | 35.294 |
| -0.2379357E 03 | -0.1095866E 03 | 0.2610161E 03 | 204.583 | 29.226 | 0.341696 | 7 | 41.176 |
| 0.3462952E 02 | -0.7837846E 02 | 0.8568770E 02 | 293.837 | 34.730 | 0.112174 | 8 | 47.059 |
| 0.1161618E 02 | 0.9907883E 02 | 0.9975748E 02 | 83.313 | 9.257 | 0.130593 | 9 | 52.941 |
| -0.1034321E 03 | -0.4827494E 01 | 0.1035447E 03 | 182.672 | 18.267 | 0.135550 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 3

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2268054E 05 | | | | | | | |
| 0.4282872E 05 | -0.2041114E 05 | 0.4744379E 05 | 334.519 | 334.519 | 1.000000 | 1 | 5.882 |
| 0.1722970E 05 | 0.3491231E 04 | 0.1271826E 05 | 15.933 | 7.966 | 0.268070 | 2 | 11.765 |
| 0.4517754E 04 | -0.4546863E 04 | 0.6409684E 04 | 314.816 | 104.939 | 0.135101 | 3 | 17.647 |
| 0.5517278E 03 | 0.1113613E 03 | 0.5628540E 03 | 11.411 | 2.853 | 0.011864 | 4 | 23.529 |
| -0.1552729E 04 | -0.1897437E 04 | 0.2451782E 04 | 230.705 | 46.141 | 0.051678 | 5 | 29.412 |
| -0.4414634E 03 | 0.6132053E 02 | 0.4457017E 03 | 172.092 | 28.682 | 0.009394 | 6 | 35.294 |
| -0.2776213E 03 | 0.3953841E 02 | 0.2804224E 03 | 171.895 | 24.556 | 0.005911 | 7 | 41.176 |
| -0.1484200E 03 | -0.3511674E 03 | 0.3812393E 03 | 247.088 | 30.886 | 0.008036 | 8 | 47.059 |
| 0.4046572E 03 | 0.7402693E 03 | 0.8436504E 03 | 61.337 | 6.815 | 0.017782 | 9 | 52.941 |
| 0.2717556E 03 | -0.1363188E 04 | 0.3031377E 03 | 333.698 | 33.370 | 0.006389 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1943.57E 04 | | | | | | | |
| 0.2581C22E 05 | -0.1097460E 05 | 0.2804655E 05 | 336.965 | 336.965 | 1.000000 | 1 | 5.882 |
| 0.8445891E 04 | 0.2316441E 04 | 0.8757783E 04 | 15.337 | 7.665 | 0.312259 | 2 | 11.765 |
| 0.4C954.4E 04 | -0.3497184E 04 | 0.5386227E 04 | 319.512 | 106.504 | 0.192046 | 3 | 17.647 |
| 0.1162?A0E 04 | 0.1048168E 04 | 0.1565631E 04 | 42.027 | 10.507 | 0.055823 | 4 | 23.529 |
| -0.2104012E 04 | -0.3999795E 03 | 0.2:466055E 04 | 190.739 | 38.148 | 0.076537 | 5 | 29.412 |
| 0.1802708E 03 | 0.4048247E 03 | 0.4446870E 03 | 65.555 | 10.926 | 0.015855 | 6 | 35.294 |
| 0.2e567.6E 03 | 0.6921365E 03 | 0.5592673E 03 | 61.638 | 8.805 | 0.019941 | 7 | 41.176 |
| -0.1272492E 03 | 0.3244106E 03 | 0.3484746E 03 | 111.418 | 13.927 | 0.012425 | 8 | 47.059 |
| -0.4786895E 02 | 0.2590985E 03 | 0.2634827E 03 | 100.467 | 11.163 | 0.009394 | 9 | 52.941 |
| 0.4276584E 01 | -0.3196343E 02 | 0.3218878E 02 | 277.635 | 27.764 | 0.001148 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 8 CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2414250E 04 | | | | | | | |
| 0.9957348E 04 | -0.5074699E 04 | 0.1064483E 05 | 331.528 | 331.528 | 1.000000 | 1 | 5.8A4 |
| 0.3854641E 04 | 0.5835364E 03 | 0.3899574E 04 | 8.309 | 4.154 | 0.366335 | 2 | 11.765 |
| 0.1323079E 04 | -0.2021213E 04 | 0.2415748E 04 | 303.208 | 101.069 | 0.226941 | 3 | 17.647 |
| 0.1137012E 04 | 0.9827664E 03 | 0.1502872E 04 | 40.838 | 10.210 | 0.141183 | 4 | 23.529 |
| -0.1265166E 04 | 0.5332708E 03 | 0.1372961E 04 | 157.144 | 31.429 | 0.128975 | 5 | 29.412 |
| 0.4204417E 03 | -0.4293564E 03 | 0.6009309E 03 | 45.601 | 7.600 | 0.056453 | 6 | 35.294 |
| 0.6093679E 03 | 0.4753550E 03 | 0.7728462E 03 | 37.957 | 5.422 | 0.072603 | 7 | 41.176 |
| 0.2280410E 03 | 0.2689375E 03 | 0.3526045E 03 | 49.704 | 6.213 | 0.033124 | 8 | 47.059 |
| -0.5243222E 03 | -0.4188042E 01 | 0.5243394E 03 | 180.458 | 20.051 | 0.049258 | 9 | 52.941 |
| -0.1253676E 03 | 0.2084685E 03 | 0.2432718E 03 | 121.026 | 12.103 | 0.022854 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 12 CH. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4312588E 04 | | | | | | | |
| 0.3319172E 04 | -0.2286505E 04 | 0.4030509E 04 | 325.438 | 325.438 | 1.000000 | 1 | 5.882 |
| 0.1566762E 04 | 0.1678066E 03 | 0.1575723E 04 | 6.113 | 3.057 | 0.390949 | 2 | 11.765 |
| 0.5769229E 03 | -0.8124729E 03 | 0.9964290E 03 | 305.379 | 101.793 | 0.247222 | 3 | 17.647 |
| 0.5965C93E 03 | 0.4563184E 03 | 0.7494648E 03 | 37.508 | 9.377 | 0.185943 | 4 | 23.529 |
| -0.5788511E 03 | 0.2813767E 03 | 0.6436157E 03 | 154.076 | 30.815 | 0.159686 | 5 | 29.412 |
| 0.2521583E 03 | 0.3082478E 03 | 0.3982466E 03 | 50.715 | 8.453 | 0.098808 | 6 | 35.294 |
| 0.4199929E 03 | 0.1690395E 03 | 0.4527341E 03 | 21.924 | 3.132 | 0.112327 | 7 | 41.176 |
| 0.2011C19E 03 | 0.1958929E 03 | 0.2807417E 03 | 44.248 | 5.531 | 0.069654 | 8 | 47.059 |
| -0.4318047E 03 | -0.1346478E 02 | 0.4320144E 03 | 181.786 | 20.198 | 0.107186 | 9 | 52.941 |
| -0.3793509E 02 | 0.2492310E 03 | 0.2521015E 03 | 98.655 | 9.865 | 0.062548 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 8

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.21565C4E C3 | | | | | | | |
| 0.1496648E 01 | 0.29073246 02 | 0.1574919E 01 | 10.991 | 10.991 | 0.515362 | 1 | 5.882 |
| 0.1644525E 02 | 0.44021706 02 | 0.8610008E 02 | 79.594 | 37.797 | 0.223392 | 2 | 11.765 |
| -0.1493495C 03 | 0.1277629E 03 | 0.1965417E 03 | 139.454 | 46.685 | 0.664233 | 3 | 17.647 |
| -0.5445905E C2 | -0.1229415E 03 | 0.1344634E 03 | 246.108 | 41.927 | 0.454433 | 4 | 23.529 |
| -0.2415455E 03 | -0.17C9049E 03 | 0.2958929E 03 | 215.281 | 43.C56 | 1.000000 | 5 | 29.412 |
| -0.1573227E 02 | -0.6475146E 02 | 0.6663522E 02 | 256.344 | 42.724 | 0.225201 | 6 | 35.294 |
| 0.2189485E 02 | 0.2926473E 01 | 0.2208955E 02 | 7.613 | 1.088 | 0.074654 | 7 | 41.176 |
| 0.7592353E C1 | -0.1866528E 02 | 0.2015033E 02 | 292.135 | 36.517 | 0.068100 | 8 | 47.059 |
| -0.1697595E 02 | 0.2392046E 02 | 0.2933208E 02 | 125.363 | 13.929 | 0.099131 | 9 | 52.941 |
| 0.4616787E 01 | -0.2624484E 01 | 0.5310614E 01 | 330.383 | 33.038 | 0.017948 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5850650E 02 | | | | | | | |
| 0.1704784E 03 | 0.8869519E 02 | 0.1921711E 03 | 27.487 | 27.487 | 1.000000 | 1 | 5.882 |
| -0.2956944E C2 | 0.2998409E 02 | 0.3644533E 02 | 134.501 | 67.251 | 0.189650 | 2 | 11.765 |
| -0.4161850E 02 | 0.4221887E 02 | 0.5914325E 02 | 134.452 | 44.817 | 0.307784 | 3 | 17.647 |
| -0.1368713E 02 | -0.2009488E 02 | 0.2946659E 02 | 242.322 | 60.581 | 0.153335 | 4 | 23.529 |
| -0.8337727E 02 | -0.7804468E 02 | 0.1132536E 03 | 222.591 | 44.519 | 0.589337 | 5 | 29.412 |
| -0.1712705E C1 | -0.2860811E 02 | 0.2865134E 02 | 266.573 | 44.429 | 0.149093 | 6 | 35.294 |
| 0.1681104E 02 | -0.6403880E 01 | 0.1743001E 02 | 344.685 | 49.241 | 0.090780 | 7 | 41.176 |
| 0.2704024E 01 | -0.5349549E 00 | 0.2756433E 01 | 348.809 | 49.601 | 0.014344 | 8 | 47.059 |
| -0.1399042E 02 | 0.1969150E 02 | 0.2419547E 02 | 125.393 | 13.933 | 0.125898 | 9 | 52.941 |
| 0.1122188E C2 | -0.3946002E 01 | 0.1189338E 02 | 340.654 | 34.065 | 0.061890 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| C.9014284E 02 | | | | | | | |
| -0.5995822E 02 | 0.5307690E 02 | 0.7712636E 02 | 138.514 | 138.514 | 1.000000 | 1 | 5.882 |
| 0.2630150E C1 | 0.1055914E 02 | 0.1088177E 02 | 76.013 | 38.006 | 0.141090 | 2 | 11.765 |
| 0.5010762E 02 | -0.3589262E 02 | 0.6117406E 02 | 324.995 | 108.332 | 0.793167 | 3 | 17.647 |
| 0.9696804E 01 | 0.3528088E 02 | 0.3659488E 02 | 74.634 | 18.659 | 0.474479 | 4 | 23.529 |
| 0.9069002E 02 | 0.1178881E 02 | 0.3281744E 02 | 21.038 | 4.208 | 0.425582 | 5 | 29.412 |
| -0.9172721E 00 | 0.5269972E 01 | 0.5295294E 01 | 95.606 | 15.934 | 0.068657 | 6 | 35.294 |
| 0.1949360E 01 | 0.2145237E 00 | 0.1961127E 01 | 6.280 | 0.897 | 0.025427 | 7 | 41.176 |
| 0.1184642E 01 | 0.1326505E 01 | 0.1778493E 01 | 48.233 | 6.029 | 0.023059 | 8 | 47.059 |
| -0.2478893E CC | 0.6661864E 00 | 0.7108052E 00 | 110.409 | 12.268 | 0.009216 | 9 | 52.941 |
| 0.3576233E 01 | 0.1419047E 01 | 0.3847484E 01 | 21.643 | 2.164 | 0.049885 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 306 CR 48.1 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| C.1092869E 02 | | | | | | | |
| 0.8463554E C0 | -0.9505827E 01 | 0.9570498E 01 | 278.739 | 278.739 | 1.000000 | 1 | 5.882 |
| 0.2833848E-01 | 0.3465477E-01 | 0.4476631E-01 | 50.726 | 25.363 | 0.000036 | 2 | 11.765 |
| -0.2985051E-01 | 0.1057374E 00 | 0.1098701E 00 | 105.765 | 35.255 | 0.010724 | 3 | 17.647 |
| -0.3574832E-01 | -0.2401302E-01 | 0.4340245E-01 | 214.348 | 53.63 | 0.CC7791 | 4 | 23.529 |
| 0.5944543E-C2 | 0.7246870E-01 | 0.6352875E-C2 | 20.655 | 4.131 | 0.001140 | 5 | 29.412 |
| 0.2883485E-02 | 0.1588345E-01 | 0.1614312E-01 | 79.709 | 13.285 | 0.002898 | 6 | 35.294 |
| 0.4480917E-02 | -0.1167228E-01 | 0.1250283E-01 | 291.001 | 41.572 | 0.002244 | 7 | 41.176 |
| -0.1130997E-01 | 0.4119765E-02 | 0.1203317E-01 | 159.979 | 19.997 | 0.CC2160 | 8 | 47.059 |
| -0.4713349E-C2 | -0.2140048E-01 | 0.2191337E-01 | 257.579 | 28.62C | 0.003934 | 9 | 52.941 |
| -0.1210CC3E-01 | 0.2476242E-02 | 0.1235120E-01 | 168.435 | 16.843 | 0.002217 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 11

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 7 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.69299306E 04 | | | | | | | |
| -0.46399594E 04 | -0.95727466E 04 | 0.10637826E 05 | 244.142 | 244.142 | 1.000000 | 1 | 5.917 |
| -0.20303088E 04 | 0.38718906E 03 | 0.20668908E 04 | 169.203 | 94.462 | 0.194296 | 2 | 11.834 |
| 0.22037526E 04 | -0.20733306E 04 | 0.30257596E 04 | 316.747 | 109.582 | 0.284434 | 3 | 17.751 |
| 0.25499126E 03 | 0.10898066E 04 | 0.11193276E 04 | 76.832 | 19.208 | 0.105221 | 4 | 23.669 |
| 0.16279408E 02 | -0.18781066E 04 | 0.18781768E 04 | 270.497 | 94.069 | 0.176556 | 5 | 29.586 |
| 0.38966606E 03 | 0.53231746E 01 | 0.38971146E 03 | 0.995 | 0.164 | 0.029114 | 6 | 35.503 |
| 0.10606346E 03 | -0.48630206E 02 | 0.11662596E 03 | 335.356 | 47.908 | 0.010963 | 7 | 41.420 |
| 0.19602916E 03 | -0.17701756E 03 | 0.24412606E 03 | 317.917 | 39.740 | 0.074829 | 8 | 47.337 |
| 0.12391956E 02 | 0.67993706E 01 | 0.13901156E 02 | 28.944 | 2.964 | 0.001307 | 9 | 53.254 |
| -0.69061896E 02 | -0.48533846E 02 | 0.84410166E 02 | 215.098 | 21.510 | 0.007935 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.53380356E 04 | | | | | | | |
| 0.43273976E 03 | -0.26841986E 04 | 0.26991136E 04 | 279.226 | 279.226 | 1.000000 | 1 | 5.917 |
| -0.22499776E 02 | -0.10459146E 03 | 0.10693526E 03 | 257.854 | 128.927 | 0.039615 | 2 | 11.834 |
| -0.31590956E 02 | -0.79888096E 02 | 0.85911136E 02 | 248.419 | 42.806 | 0.031829 | 3 | 17.751 |
| 0.45486056E 01 | -0.26888066E 03 | 0.26888946E 03 | 270.977 | 67.744 | 0.099621 | 4 | 23.669 |
| -0.88191036E 02 | 0.73432066E 03 | 0.73868166E 03 | 96.229 | 19.244 | 0.273676 | 5 | 29.586 |
| -0.96735476E 02 | -0.69528926E 02 | 0.11918046E 03 | 215.707 | 35.951 | 0.044137 | 6 | 35.503 |
| -0.16071996E 04 | 0.11216686E 03 | 0.19599056E 03 | 145.089 | 20.727 | 0.072613 | 7 | 41.420 |
| -0.14129096E 03 | 0.47895366E 02 | 0.14916786E 03 | 161.272 | 20.159 | 0.055265 | 8 | 47.337 |
| -0.39811286E 02 | 0.35643546E 02 | 0.53469306E 02 | 138.122 | 15.347 | 0.019810 | 9 | 53.254 |
| -0.32032756E 02 | 0.11745366E 03 | 0.12174336E 03 | 105.255 | 10.526 | 0.045105 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.21577256E 04 | | | | | | | |
| 0.34111696E 03 | -0.88286236E 03 | 0.94647056E 03 | 291.125 | 291.125 | 1.000000 | 1 | 5.917 |
| -0.12821096E 03 | -0.63946066E 02 | 0.14327306E 03 | 206.508 | 103.254 | 0.151376 | 2 | 11.834 |
| -0.44249076E 03 | 0.18532666E 03 | 0.49843336E 03 | 158.177 | 52.724 | 0.526623 | 3 | 17.751 |
| -0.74179666E 02 | -0.16505116E 03 | 0.18095276E 03 | 245.800 | 61.450 | 0.191187 | 4 | 23.669 |
| 0.63139416E 02 | 0.90222226E 03 | 0.90617486E 03 | 82.835 | 16.967 | 0.534802 | 5 | 29.586 |
| -0.43994026E 02 | 0.19242656E 02 | 0.47982336E 02 | 156.357 | 26.060 | 0.050696 | 6 | 35.503 |
| 0.69867896E 02 | -0.76209246E 02 | 0.10019466E 03 | 310.402 | 44.345 | 0.105861 | 7 | 41.420 |
| 0.47434866E 02 | 0.30277286E 02 | 0.56274126E 02 | 32.590 | 4.069 | 0.059457 | 8 | 47.337 |
| -0.41135736E 02 | -0.13644986E 02 | 0.43339746E 02 | 198.351 | 22.035 | 0.045791 | 9 | 53.254 |
| 0.24961156E 02 | -0.48661106E 02 | 0.54618446E 02 | 296.594 | 29.659 | 0.057696 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.10277946E 03 | | | | | | | |
| 0.32426156E 03 | -0.74864656E 03 | 0.81401056E 03 | 293.473 | 293.473 | 0.9PE355 | 1 | 5.917 |
| -0.41823076E 03 | -0.57672416E 02 | 0.42218426E 03 | 187.851 | 93.926 | 0.511575 | 2 | 11.834 |
| -0.66933946E 03 | 0.45907346E 03 | 0.82527156E 03 | 146.147 | 48.716 | 1.000000 | 3 | 17.751 |
| -0.88546496E 02 | 0.44867006E 02 | 0.98897006E 02 | 153.552 | 38.388 | 0.119836 | 4 | 23.669 |
| -0.23953926E 02 | -0.26780816E 01 | 0.20913486E 03 | 263.533 | 52.707 | 0.253613 | 5 | 29.586 |
| 0.85800346E 02 | 0.90167296E 01 | 0.86272576E 02 | 5.998 | 1.000 | 0.104538 | 6 | 35.503 |
| 0.19359406E 03 | -0.11783006E 02 | 0.15403926E 03 | 355.643 | 50.806 | 0.186653 | 7 | 41.420 |
| 0.13598056E 03 | -0.68547056E 02 | 0.15215106E 03 | 333.345 | 41.668 | 0.184364 | 8 | 47.337 |
| -0.28230186E 02 | -0.16789006E 02 | 0.26417516E 02 | 220.021 | 24.447 | 0.032011 | 9 | 53.254 |
| -0.42755846E 02 | 0.10487756E 02 | 0.44023936E 02 | 166.218 | 16.622 | 0.053344 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 11

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1090088E 04 | | | | | | | |
| 0.2778582E 03 | -0.7096135E 03 | 0.7620737E 03 | 291.383 | 291.383 | 0.8C5247 | 1 | 5.917 |
| -0.6937583E 03 | -0.1870609E 03 | 0.7185347E 03 | 195.090 | 97.545 | C.759241 | 2 | 11.834 |
| -0.7420103E C3 | 0.5874233E 03 | 0.9463853E 03 | 141.633 | 47.211 | 1.000000 | 3 | 17.751 |
| 0.7174635E 01 | 0.2056750E 03 | 3.2058001E 03 | 88.002 | 22.CC1 | 0.217459 | 4 | 23.669 |
| 0.9983044E 02 | -0.5400056E 03 | 0.5491550E 03 | 280.474 | 56.095 | 0.58C267 | 5 | 29.586 |
| 0.4522601E 02 | -0.5018472E 02 | 0.C755663E 02 | 312.025 | 52.004 | 0.C71384 | 6 | 35.503 |
| 0.5347858E 02 | 0.8398179E 01 | 0.5413397E 02 | 8.925 | 1.275 | C.057201 | 7 | 41.420 |
| -0.4465671E 02 | -0.1077720E 02 | 0.4593875E 02 | 193.568 | 24.196 | 0.040541 | 8 | 47.337 |
| -0.6648372E 02 | 0.1844609E 02 | 0.6904895E 02 | 164.333 | 18.259 | 0.072961 | 9 | 53.254 |
| -C.2944702E 02 | 0.7777979E 02 | 0.8282617E 02 | 110.104 | 11.010 | C.C87518 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1823149E 04 | | | | | | | |
| 0.7642CB3F 03 | -0.6755239E 03 | 0.7253540E 03 | 291.361 | 291.361 | 0.753637 | 1 | 5.917 |
| -0.8165Z83E C3 | -0.7890144E 03 | 0.8861682E 03 | 199.492 | 99.746 | C.899942 | 2 | 11.834 |
| -0.8462561F C3 | 0.4584783E 03 | 0.9624714E 03 | 151.552 | 50.517 | 1.000000 | 3 | 17.751 |
| -0.7849986E 02 | 0.4161627E 03 | 0.4235994E 03 | 100.680 | 25.170 | 0.440117 | 4 | 23.669 |
| 0.1268312F 03 | -C.8088264E 03 | 0.8187100E 03 | 278.912 | 55.782 | 0.850633 | 5 | 29.586 |
| 0.1074082E C1 | -0.2884847E 01 | 0.3059575E 01 | 290.552 | 48.425 | C.003179 | 6 | 35.503 |
| -0.1563265E C3 | -0.1877544E 02 | 0.1574499E 03 | 186.849 | 26.693 | 0.163589 | 7 | 41.420 |
| -0.1377426E 03 | -0.2390051E 02 | 0.1390008E 03 | 189.844 | 23.730 | 0.145252 | 8 | 47.337 |
| 0.9681866F 01 | 0.3437201F 02 | 0.3[/09756E 02 | 74.269 | 8.252 | 0.037102 | 9 | 53.254 |
| -0.1651102E 02 | 0.2887183E 02 | 0.3329552E 02 | 119.764 | 11.976 | 0.034556 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1977438E 04 | | | | | | | |
| C.1160893E 03 | -0.4399976E 03 | 0.4550491E 03 | 284.778 | 284.778 | 0.576146 | 1 | 5.917 |
| -0.7154490E 03 | -0.1677879E 03 | 0.7348604E 03 | 193.199 | 96.599 | 0.930420 | 2 | 11.834 |
| -0.7823788 03 | 0.2957065E 03 | 0.7898159E 03 | 158.013 | 52.671 | 1.000000 | 3 | 17.751 |
| -0.1601C 1[ 02 | 0.3692849E 03 | 0.3901414E 03 | 95.903 | 23.976 | 0.443320 | 4 | 23.669 |
| 0.1021074 C3 | -C.6011230E 03 | 0.6097327E 03 | 279.640 | 55.928 | 0.771993 | 5 | 29.586 |
| -0.1818966F 02 | -0.7542984E 02 | 0.7714767E 02 | 257.886 | 42.981 | 0.097678 | 6 | 35.503 |
| -0.2C00523E 01 | -0.1595082E 02 | 0.2006872E 03 | 184.359 | 26.366 | 0.254094 | 7 | 41.420 |
| -0.1355090E 03 | C.2255623E 02 | 0.1373735E 03 | 170.549 | 21.319 | 0.173931 | 8 | 47.337 |
| C.2748138E 02 | 0.4404542E 02 | 0.8842447E 02 | 71.893 | 7.988 | 0.111956 | 9 | 53.254 |
| 0.3877266F C2 | 0.7674764E 01 | 0.3947588E 02 | 11.211 | 1.121 | 0.049981 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -C.1794332F C4 | | | | | | | |
| -0.7872462E 02 | -0.2873857F 03 | 0.2979744E 03 | 254.680 | 254.680 | 0.529101 | 1 | 5.917 |
| -0.5486749E C3 | -0.1112919E 03 | 0.5598479E 03 | 191.466 | 95.733 | 0.986584 | 2 | 11.834 |
| -0.5325276E C3 | 0.1960271E 03 | 0.5674612E 03 | 159.791 | 53.264 | 1.000000 | 3 | 17.751 |
| 0.3051924E 02 | C.2678220E 03 | 0.2695552E 03 | 83.499 | 20.875 | 0.475020 | 4 | 23.669 |
| 0.9419930E 02 | -0.3400801E 03 | 0.3528835E 03 | 285.481 | 57.096 | 0.621864 | 5 | 29.586 |
| -0.1046294E C3 | -0.1[8245[E 03 | 0.2153868E 03 | 240.935 | 40.156 | 0.379527 | 6 | 35.503 |
| -0.2603938F 03 | -0.4875485E 02 | 0.2649185E 03 | 190.605 | 27.229 | 0.466845 | 7 | 41.420 |
| -0.1525316F 03 | 0.1082959E 03 | 0.1870665E 03 | 144.626 | 18.078 | 0.329655 | 8 | 47.337 |
| 0.3718335E 02 | 0.4706831E 02 | 0.5998355E 02 | 51.592 | 5.744 | 0.105705 | 9 | 53.254 |
| 0.7618469E C2 | -0.5281168E 02 | 0.5893779E 02 | 296.355 | 29.636 | 0.103862 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 11

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1476059E 05 | | | | | | | |
| 0.3382672E 05 | -0.4395441E 04 | 0.3407472E 05 | 353.541 | 353.541 | 1.000000 | 1 | 5.917 |
| 0.1076701E 05 | 0.2587468E 04 | 0.1107355E 05 | 13.513 | 6.756 | 0.288396 | 2 | 11.834 |
| 0.3728045E 04 | -0.1122639E 04 | 0.3893409E 04 | 343.241 | 114.414 | 0.099646 | 3 | 17.751 |
| 0.2858027E 03 | 0.2010611E 02 | 0.2865090E 03 | 4.024 | 1.006 | 0.007332 | 4 | 23.669 |
| 0.3504871E 03 | -0.2189832E 04 | 0.2217702E 04 | 279.093 | 55.819 | 0.056752 | 5 | 29.586 |
| 0.9334874E 02 | -0.1918217E 03 | 0.2133297E 03 | 295.949 | 49.325 | 0.005460 | 6 | 35.503 |
| 0.3049075E 03 | -0.4312595E 03 | 0.5279644E 03 | 305.136 | 43.591 | 0.013558 | 7 | 41.420 |
| 0.2000715E 03 | -0.7256150E 03 | 0.7529093E 03 | 285.474 | 35.684 | 0.019268 | 8 | 47.337 |
| -0.4312717E 03 | -0.4376279E 03 | 0.6144211E 03 | 225.419 | 25.047 | 0.015724 | 9 | 53.254 |
| -0.2814766E 03 | -0.1231227E 03 | 0.3072266E 03 | 203.625 | 20.363 | 0.007863 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1677255E 05 | | | | | | | |
| 0.2387176E 05 | -0.1172173E 04 | 0.2390052E 05 | 357.189 | 357.189 | 1.000000 | 1 | 5.917 |
| 0.7590328E 04 | 0.1675213E 04 | 0.7577812E 04 | 12.772 | 6.386 | 0.317056 | 2 | 11.834 |
| 0.2999663E 04 | -0.5667014E 03 | 0.3052725E 04 | 349.302 | 116.434 | 0.127726 | 3 | 17.751 |
| -0.1164088E 03 | 0.6620859E 03 | 0.6722415E 03 | 99.972 | 24.993 | 0.028127 | 4 | 23.669 |
| -0.1242300E 04 | -0.1517936E 04 | 0.1961489E 04 | 230.703 | 46.141 | 0.082069 | 5 | 29.586 |
| 0.3092456E 03 | -0.7232053E 02 | 0.3175894E 03 | 346.837 | 57.806 | 0.013288 | 6 | 35.503 |
| 0.2136389E 03 | -0.2870715E 03 | 0.3578430E 03 | 306.656 | 43.808 | 0.014972 | 7 | 41.420 |
| -0.9977007E 02 | 0.2300737E 02 | 0.1023885E 03 | 167.014 | 20.877 | 0.004284 | 8 | 47.337 |
| 0.6163042E 02 | -0.1899605E 03 | 0.1997080E 03 | 287.975 | 31.997 | 0.008356 | 9 | 53.254 |
| 0.9520345E 02 | -0.2806000E 02 | 0.9925249E 02 | 343.578 | 34.358 | 0.004153 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8049766E 04 | | | | | | | |
| 0.9111723E 04 | -0.1382424E 04 | 0.9215992E 04 | 351.373 | 351.373 | 1.000000 | 1 | 5.917 |
| 0.3421288E 04 | 0.2849084E 03 | 0.3433130E 04 | 4.760 | 2.380 | 0.372519 | 2 | 11.834 |
| 0.1153551E 04 | -0.6675029E 03 | 0.1332756E 04 | 329.944 | 109.981 | 0.144613 | 3 | 17.751 |
| -0.2103306E 03 | 0.5326069E 03 | 0.5726333E 03 | 111.549 | 27.887 | 0.062135 | 4 | 23.669 |
| -0.9258193E 03 | -0.4658308E 03 | 0.1036407E 04 | 206.709 | 41.342 | 0.112457 | 5 | 29.586 |
| 0.1202383E 03 | -0.3065586E 01 | 0.3292952E 03 | 291.416 | 46.569 | 0.035731 | 6 | 35.503 |
| 0.9581570E 02 | -0.1590365E 03 | 0.1856694E 03 | 301.068 | 43.010 | 0.020146 | 7 | 41.420 |
| 0.2951880E 02 | 0.4443049E 01 | 0.4472151E 03 | 86.344 | 10.753 | 0.048526 | 8 | 47.337 |
| 0.4434451E 03 | 0.7571056E 02 | 0.4498816E 03 | 9.689 | 1.077 | 0.048813 | 9 | 53.254 |
| 0.3111719E 03 | 0.2740479E 02 | 0.3123035E 03 | 4.730 | 0.473 | 0.038057 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5538289E 04 | | | | | | | |
| 0.3569778E 04 | -0.6472114E 03 | 0.3627974E 04 | 349.724 | 349.724 | 1.000000 | 1 | 5.917 |
| 0.1631332E 04 | -0.9955034E 02 | 0.1634366E 04 | 356.508 | 178.254 | 0.450490 | 2 | 11.834 |
| 0.3923923E 03 | -0.7919221E 02 | 0.4003037E 03 | 348.590 | 116.197 | 0.110,38 | 3 | 17.751 |
| -0.1956823E 03 | 0.9453765E 01 | 0.3969587E 03 | 119.535 | 29.884 | 0.109416 | 4 | 23.669 |
| -0.7578702E 01 | 0.7355435E 02 | 0.2680894E 03 | 164.076 | 32.815 | 0.073895 | 5 | 29.586 |
| 0.5949489E 02 | -0.2247044E 03 | 0.2324472E 03 | 284.830 | 47.472 | 0.064071 | 6 | 35.503 |
| 0.1667596E 03 | -0.6749880E 02 | 0.1800679E 03 | 337.834 | 48.262 | 0.049633 | 7 | 41.420 |
| 0.8959037E 00 | 0.7394093E 03 | 0.2394109E 03 | 89.786 | 11.223 | 0.065990 | 8 | 47.337 |
| 0.2740896E 03 | 0.2090488E 01 | 0.3447119E 03 | 37.333 | 4.148 | 0.095015 | 9 | 53.254 |
| 0.2222649E 03 | 0.6839436E 02 | 0.2274715E 03 | 12.284 | 1.228 | 0.062699 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 11

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.3428183E 02 | | | | | | | |
| 0.8112643E 02 | 0.8527077E 02 | 0.1176973E 03 | 46.427 | 46.427 | 0.626887 | 1 | 5.917 |
| -0.2639514E 02 | 0.4556248E 02 | 0.5269599E 02 | 120.085 | 60.042 | 0.280459 | 2 | 11.834 |
| -0.8720724E 02 | -0.3319083E 00 | 0.8727786E 02 | 180.218 | 60.073 | 0.464492 | 3 | 17.751 |
| 0.3846897E 01 | -0.7788744E 02 | 0.7779274E 02 | 272.836 | 68.209 | 0.414344 | 4 | 23.669 |
| 0.2711531E 02 | -0.1864419E 01 | 0.1877490E 03 | 276.765 | 55.353 | 1.000000 | 5 | 29.586 |
| 0.3898160E 02 | -0.7642639E 01 | 0.3972568E 02 | 348.908 | 58.151 | 0.211589 | 6 | 35.503 |
| 0.4939856E 02 | 0.1490735E 02 | 0.5257834E 02 | 20.028 | 2.861 | 0.280046 | 7 | 41.420 |
| -0.8899040E 01 | 0.2547859E 02 | 0.2698798E 02 | 109.253 | 13.657 | 0.143765 | 8 | 47.337 |
| 0.1096445E 02 | 0.1686484E 01 | 0.1109784E 02 | 8.741 | 0.971 | 0.059110 | 9 | 53.254 |
| 0.4155914E 01 | -0.6741604E 01 | 0.7919644E 01 | 301.652 | 30.165 | 0.042182 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.6759273E 02 | | | | | | | |
| 0.6672803E 02 | 0.7907790E 02 | 0.1034695E 03 | 49.841 | 49.841 | 1.000000 | 1 | 5.917 |
| -0.2337997E 02 | -0.1091078E 02 | 0.2590054E 02 | 205.017 | 102.509 | 0.249394 | 2 | 11.834 |
| -0.1250028E 02 | -0.9917215E 01 | 0.1599492E 02 | 219.503 | 73.034 | 0.148460 | 3 | 17.751 |
| 0.2129059E 02 | -0.3326959E 01 | 0.2154895E 02 | 351.118 | 87.780 | 0.208264 | 4 | 23.669 |
| 0.5299726E 01 | -0.6509174E 02 | 0.6530711E 02 | 274.659 | 54.931 | 0.631172 | 5 | 29.586 |
| -0.2480002E 01 | -0.8311729E 01 | 0.8791469E 01 | 248.949 | 41.425 | 0.084961 | 6 | 35.503 |
| 0.6105611E 01 | 0.9200184E 01 | 0.1104183E 02 | 56.430 | 8.061 | 0.106716 | 7 | 41.420 |
| -0.3082474E 01 | 0.1718150E 02 | 0.1745581E 02 | 100.171 | 12.921 | 0.168705 | 8 | 47.337 |
| 0.1199604E 02 | -0.6908298E 01 | 0.1384353E 02 | 330.060 | 36.673 | 0.133793 | 9 | 53.254 |
| 0.3449594E 01 | 0.1699807E 01 | 0.3844693E 01 | 26.232 | 2.623 | 0.037167 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.4320358E 02 | | | | | | | |
| -0.3183397E 01 | 0.2360667E 02 | 0.2382033E 02 | 97.680 | 97.680 | 1.000000 | 1 | 5.917 |
| -0.1475369E 01 | 0.6500223E 01 | 0.6665594E 01 | 102.788 | 51.394 | 0.279826 | 2 | 11.834 |
| 0.2039511E 02 | 0.9447299E 01 | 0.2207544E 02 | 22.498 | 7.499 | 0.926748 | 3 | 17.751 |
| -0.1914867E 02 | 0.5472892E 01 | 0.1994312E 02 | 163.773 | 40.943 | 0.837231 | 4 | 23.669 |
| 0.1209742E 01 | 0.1951106E 02 | 0.1954652E 02 | 86.452 | 17.290 | 0.820666 | 5 | 29.586 |
| 0.7660135E 01 | -0.1872525E 01 | 0.7885683E 01 | 346.263 | 57.711 | 0.331068 | 6 | 35.503 |
| 0.1233360E 01 | 0.1957898E 01 | 0.2230013E 01 | 56.422 | 8.060 | 0.093618 | 7 | 41.420 |
| -0.1440071E 01 | -0.9326026E 00 | 0.1715635E 01 | 212.928 | 26.616 | 0.072024 | 8 | 47.337 |
| 0.7263477E 01 | 0.1819309E 01 | 0.2903999E 01 | 38.791 | 4.310 | 0.121913 | 9 | 53.254 |
| 0.1796906E 01 | 0.4783749E 00 | 0.1859492E 01 | 14.908 | 1.491 | 0.078061 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 504 CTR 269 CR 62.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.9534496E 01 | | | | | | | |
| 0.1313334E 01 | -0.3025784E 01 | 0.3302188E 01 | 293.436 | 293.436 | 1.000000 | 1 | 5.917 |
| 0.8137960E-01 | 0.3585100E-02 | 0.8145652E-01 | 2.523 | 1.261 | 0.024667 | 2 | 11.834 |
| -0.9462447E-02 | -0.1522544E-01 | 0.1772630E-01 | 238.139 | 79.380 | 0.005429 | 3 | 17.751 |
| 0.1343854E-01 | -0.4355799E-01 | 0.4558391E-01 | 287.146 | 71.786 | 0.013804 | 4 | 23.669 |
| -0.7313919E-01 | 0.1756623E-01 | 0.7521439E-01 | 166.510 | 33.302 | 0.022777 | 5 | 29.586 |
| -0.2322692E-01 | -0.5659784E-01 | 0.6117847E-01 | 247.687 | 41.281 | 0.018527 | 6 | 35.503 |
| 0.2506019E-01 | -0.3729235E-01 | 0.4493041E-01 | 303.901 | 43.414 | 0.013606 | 7 | 41.420 |
| 0.3007017E-01 | -0.3204928E-02 | 0.3024043E-01 | 353.916 | 44.240 | 0.009158 | 8 | 47.337 |
| -0.9594841E-02 | 0.2379523E-01 | 0.2565685E-01 | 111.961 | 12.440 | 0.007770 | 9 | 53.254 |
| -0.2932138E-01 | 0.1493744E-01 | 0.3290701E-01 | 153.004 | 15.300 | 0.009965 | 10 | 59.172 |

HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1c

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1360556E 05 | | | | | | | |
| -0.2866644E 04 | -0.7393167E 04 | 0.7929492E 04 | 249.807 | 248.807 | 1.000000 | 1 | 5.882 |
| 0.1589131E 04 | 0.4179962E 03 | 0.1643083E 04 | 14.723 | 7.362 | 0.207212 | 2 | 11.765 |
| -0.7623633E 02 | 0.5131296E 03 | 0.5187617E 03 | 98.451 | 32.817 | 0.065422 | 3 | 17.647 |
| -0.1128216E 03 | -0.2113391E 03 | 0.2395682E 03 | 241.905 | 60.476 | 0.050212 | 4 | 23.529 |
| 0.2095004E 02 | 0.3181841E 03 | 0.3188728E 03 | 86.233 | 17.247 | 0.040214 | 5 | 29.412 |
| -0.4358391E 02 | -0.3397124E 02 | 0.9519632E 02 | 217.939 | 36.331 | 0.006961 | 6 | 35.294 |
| 0.6919379E 01 | 0.3547559E 02 | 0.3614407E 02 | 78.963 | 11.280 | 0.004558 | 7 | 41.176 |
| -0.6024261E 02 | -0.1703883E 02 | 0.6370114E 02 | 202.948 | 25.368 | 0.005911 | 8 | 47.059 |
| -0.5162065E 02 | -0.1800552E 02 | 0.5467073E 02 | 199.239 | 22.137 | 0.000005 | 9 | 52.941 |
| -0.1868008E 02 | 0.7697482E 01 | 0.1316558E 02 | 144.721 | 14.422 | 0.001660 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2576753E 04 | | | | | | | |
| -0.4971869E 03 | -0.1984227E 04 | 0.2018479E 04 | 255.749 | 255.749 | 1.000000 | 1 | 5.882 |
| 0.1175710E 03 | 0.2409304E 02 | 0.1200861E 03 | 11.562 | 5.781 | 0.059495 | 2 | 11.765 |
| -0.9222209E 02 | -0.6924467E 02 | 0.1153244E 03 | 216.981 | 72.300 | 0.057136 | 3 | 17.647 |
| -0.7325963E 02 | 0.7282854E 02 | 0.1032908E 03 | 135.170 | 33.792 | 0.051178 | 4 | 23.529 |
| -0.4828139E 02 | -0.9360580E 02 | 0.1051088E 03 | 242.784 | 48.561 | 0.052875 | 5 | 29.412 |
| -0.1468827E 02 | 0.4386895E 02 | 0.4597900E 02 | 108.493 | 18.082 | 0.022790 | 6 | 35.294 |
| -0.6279492E 02 | -0.2637812E 02 | 0.6810713E 02 | 202.779 | 28.968 | 0.033763 | 7 | 41.176 |
| 0.6638098E 02 | 0.3270642E 02 | 0.7403316E 02 | 26.272 | 3.284 | 0.036679 | 8 | 47.059 |
| 0.1648619E 02 | 0.5667699E 02 | 0.5901723E 02 | 73.783 | 8.198 | 0.029140 | 9 | 52.941 |
| 0.2704116E 02 | 0.3794413E 02 | 0.4662160E 02 | 53.638 | 5.364 | 0.023098 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1071926E 04 | | | | | | | |
| -0.9905108E 01 | -0.7079090E 03 | 0.7076536E 03 | 269.230 | 269.230 | 1.000000 | 1 | 5.882 |
| -0.1200000E 00 | -0.9404407E 02 | 0.1931013E 03 | 217.900 | 108.950 | 0.2160951 | 2 | 11.765 |
| 0.7271158E 01 | -0.8971907E 02 | 0.9001310E 02 | 270.689 | 91.544 | 0.127199 | 3 | 17.647 |
| -0.7040909E 01 | -0.7403901E 01 | 0.1020630E 02 | 226.620 | 56.655 | 0.014900 | 4 | 23.529 |
| 0.1937891E 02 | -0.1304365E 00 | 0.1938130E 02 | 270.385 | 55.305 | 0.191214 | 5 | 29.412 |
| 0.3036211E 02 | -0.1490709E 01 | 0.3030717E 02 | 357.267 | 59.541 | 0.042955 | 6 | 35.294 |
| -0.2390000E 01 | -0.2790539E 01 | 0.3677408E 01 | 229.391 | 32.793 | 0.0004197 | 7 | 41.176 |
| 0.4695408E 01 | -0.1400011E 02 | 0.1404040E 02 | 290.443 | 36.059 | 0.020076 | 8 | 47.059 |
| -0.6010067E 01 | -0.2524000E 02 | 0.2595300E 02 | 296.990 | 28.910 | 0.020676 | 9 | 52.941 |
| -0.1340957E 02 | -0.2108917E 02 | 0.2499139E 02 | 237.990 | 23.799 | 0.0193116 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4960613E 00 | | | | | | | |
| 0.1675000E 00 | -0.4013679E 03 | 0.4013679E 03 | 292.562 | 292.562 | 1.000000 | 1 | 5.882 |
| -0.2567428E 00 | -0.8223799E 02 | 0.2099737E 03 | 197.762 | 98.881 | 0.617161 | 2 | 11.765 |
| -0.4052184E 01 | -0.8851808E 02 | 0.8892739E 02 | 267.066 | 89.022 | 0.203990 | 3 | 17.647 |
| 0.4082819E 00 | -0.1797536E 02 | 0.4432286E 02 | 336.000 | 84.320 | 0.101496 | 4 | 23.529 |
| 0.1599999E 01 | 0.2467137E 02 | 0.2471933E 02 | 86.450 | 17.286 | 0.056902 | 5 | 29.412 |
| 0.7100041E 01 | -0.6497035E 01 | 0.9633599E 01 | 310.066 | 53.011 | 0.022085 | 6 | 35.294 |
| 0.4413009E 00 | 0.1815162E 02 | 0.4257291E 02 | 13.062 | 1.900 | 0.097800 | 7 | 41.176 |
| -0.1741498E 00 | -0.4138949E 01 | 0.1780992E 02 | 199.343 | 24.168 | 0.040976 | 8 | 47.059 |
| -0.1452822E 00 | -0.5098861E 01 | 0.1967809E 02 | 202.000 | 22.453 | 0.035093 | 9 | 52.941 |
| -0.8006390E 00 | 0.1813159E 02 | 0.1816901E 02 | 94.969 | 9.497 | 0.023203 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 16

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 10 PL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.14359746 04 | | | | | | | |
| 0.10835016 03 | -0.29874396 03 | 0.31778546 03 | 289.935 | 289.935 | 1.000000 | 1 | 5.882 |
| -0.23744856 03 | -0.63917976 02 | 0.24590006 03 | 195.066 | 97.533 | 0.773796 | 2 | 11.765 |
| 0.96856466 01 | -0.64037486 02 | 0.64765766 02 | 278.681 | 92.847 | 0.203803 | 3 | 17.647 |
| 0.47905626 02 | -0.71386586 01 | 0.48039036 02 | 351.454 | 87.864 | 0.151168 | 4 | 23.529 |
| -0.73496346 01 | 0.11587966 03 | 0.11607946 03 | 93.630 | 18.726 | 0.365320 | 5 | 29.411 |
| -0.13679126 02 | 0.17022006 01 | 0.15700106 02 | 173.515 | 28.919 | 0.049436 | 6 | 35.294 |
| 0.10248306 02 | 0.66134916 01 | 0.12196976 02 | 32.835 | 4.691 | 0.038381 | 7 | 41.176 |
| 0.21079076 02 | 0.65777136 00 | 0.21806296 02 | 1.869 | 0.234 | 0.068354 | 8 | 47.059 |
| 0.99207766 01 | 0.13350076 02 | 0.16632606 02 | 53.384 | 5.931 | 0.052399 | 9 | 52.941 |
| 0.19043376 01 | 0.34090076 02 | 0.34143206 02 | 86.803 | 8.680 | 0.107441 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 11 PL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.18200006 04 | | | | | | | |
| 0.52200616 02 | -0.23949516 03 | 0.24117216 03 | 282.500 | 282.500 | 1.000000 | 1 | 5.882 |
| -0.20963916 03 | -0.49581056 02 | 0.21862636 03 | 192.498 | 96.249 | 0.873244 | 2 | 11.765 |
| -0.13986196 02 | -0.24027326 02 | 0.28542026 02 | 240.704 | 80.235 | 0.118917 | 3 | 17.647 |
| 0.49322696 02 | 0.15759556 02 | 0.51779216 02 | 17.720 | 4.430 | 0.214698 | 4 | 23.529 |
| -0.27983066 01 | 0.16586596 03 | 0.16591956 03 | 90.466 | 18.193 | 0.687971 | 5 | 29.412 |
| -0.36325706 02 | -0.69982006 01 | 0.36992146 02 | 190.892 | 31.815 | 0.153385 | 6 | 35.294 |
| -0.23277346 02 | -0.13951036 02 | 0.27137806 02 | 210.536 | 30.134 | 0.112523 | 7 | 41.176 |
| 0.30958076 02 | 0.48227136 01 | 0.31932156 02 | 8.854 | 1.107 | 0.129917 | 8 | 47.059 |
| 0.21383066 01 | -0.96259226 01 | 0.12609226 02 | 310.213 | 34.468 | 0.052266 | 9 | 52.941 |
| 0.13587186 02 | -0.61006096 01 | 0.13699776 02 | 328.948 | 32.895 | 0.056761 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 13 PL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.16222206 04 | | | | | | | |
| 0.44304426 02 | -0.12056076 03 | 0.12846146 03 | 290.173 | 290.173 | 0.981134 | 1 | 5.882 |
| -0.10933886 03 | -0.91836236 01 | 0.10944206 03 | 182.773 | 91.387 | 0.809603 | 2 | 11.765 |
| -0.41917396 02 | 0.14429776 02 | 0.43952166 02 | 160.840 | 53.613 | 0.335673 | 3 | 17.647 |
| 0.40732166 02 | 0.11680426 02 | 0.42376026 02 | 16.011 | 4.003 | 0.323640 | 4 | 23.529 |
| 0.13703096 02 | 0.13821636 03 | 0.13809356 03 | 83.993 | 16.799 | 1.000000 | 5 | 29.412 |
| -0.49794066 02 | -0.42117306 01 | 0.45953806 02 | 185.258 | 30.876 | 0.350960 | 6 | 35.294 |
| -0.42719336 02 | -0.29619696 02 | 0.51806466 02 | 214.597 | 30.681 | 0.396122 | 7 | 41.176 |
| 0.40957416 02 | 0.17111256 02 | 0.43244116 02 | 19.043 | 2.380 | 0.330534 | 8 | 47.059 |
| 0.11780096 01 | -0.13062696 02 | 0.19185296 02 | 273.888 | 30.426 | 0.146716 | 9 | 52.941 |
| 0.18686906 02 | -0.38674916 02 | 0.35918706 02 | 301.990 | 30.199 | 0.274524 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 14 PL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.12883116 04 | | | | | | | |
| 0.39003406 02 | -0.70910796 02 | 0.73297296 02 | 289.338 | 289.338 | 0.828626 | 1 | 5.882 |
| 0.97219366 00 | -0.46689086 01 | 0.47731526 01 | 281.997 | 140.999 | 0.053973 | 2 | 11.765 |
| -0.23268176 02 | -0.19045226 01 | 0.23322746 02 | 183.820 | 61.307 | 0.263762 | 3 | 17.647 |
| 0.31501856 02 | -0.86101716 01 | 0.32759106 02 | 344.618 | 86.155 | 0.367436 | 4 | 23.529 |
| -0.67043926 01 | 0.88643966 02 | 0.89004936 02 | 94.316 | 18.863 | 1.006990 | 5 | 29.412 |
| -0.31073476 02 | -0.16394066 02 | 0.35132076 02 | 207.916 | 34.636 | 0.396355 | 6 | 35.294 |
| -0.51900476 02 | -0.25727776 02 | 0.57622916 02 | 206.918 | 29.503 | 0.646747 | 7 | 41.176 |
| 0.12331106 02 | -0.80591506 01 | 0.14731186 02 | 326.833 | 48.894 | 0.166540 | 8 | 47.059 |
| -0.17292796 01 | -0.33092676 02 | 0.33113706 02 | 267.009 | 29.668 | 0.371931 | 9 | 52.941 |
| 0.19936096 02 | -0.28826726 02 | 0.32908396 02 | 298.935 | 29.893 | 0.369693 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1906838E 04 | | | | | | | |
| 0.1630151E 05 | 0.8000941E 04 | 0.1819914E 05 | 26.142 | 26.142 | 1.000000 | 1 | 5.882 |
| 0.2018734E 04 | 0.3709727E 04 | 0.4322695E 04 | 62.019 | 31.009 | 0.236944 | 2 | 11.765 |
| 0.1904268E 03 | 0.9236197E 02 | 0.1333835E 03 | 30.242 | 10.081 | 0.010099 | 3 | 17.647 |
| 0.9958333E 02 | -0.3653500E 02 | 0.1023281E 03 | 339.081 | 84.770 | 0.005635 | 4 | 23.529 |
| -0.1982693E 03 | 0.3842946E 02 | 0.2019592E 03 | 169.031 | 33.806 | 0.011122 | 5 | 29.412 |
| -0.4271559E 02 | -0.9826648E 02 | 0.1071491E 03 | 246.506 | 41.084 | 0.005901 | 6 | 35.294 |
| 0.7149020E 02 | -0.1990318E 03 | 0.1743452E 03 | 294.194 | 42.028 | 0.009601 | 7 | 41.176 |
| 0.2200832E 03 | -0.3773477E 03 | 0.4372703E 03 | 300.219 | 37.527 | 0.024080 | 8 | 47.059 |
| 0.1085291E 03 | -0.6885426E 02 | 0.1283281E 03 | 327.608 | 36.401 | 0.007078 | 9 | 52.941 |
| -0.7683951E 02 | -0.8362086E 02 | 0.1135639E 03 | 227.420 | 22.742 | 0.006254 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1029003E 05 | | | | | | | |
| 0.1032111E 05 | 0.5848191E 04 | 0.1106282E 05 | 29.537 | 29.537 | 1.000000 | 1 | 5.882 |
| 0.1454309E 04 | 0.2378562E 04 | 0.2787934E 04 | 58.987 | 29.279 | 0.235014 | 2 | 11.765 |
| -0.1367844E 03 | 0.1018377E 03 | 0.1705315E 03 | 143.332 | 47.777 | 0.014375 | 3 | 17.647 |
| 0.1025607E 02 | 0.4443033E 02 | 0.4803476E 02 | 67.663 | 16.916 | 0.004049 | 4 | 23.529 |
| -0.7815179E 02 | 0.1126343E 03 | 0.1372919E 03 | 124.755 | 24.951 | 0.011556 | 5 | 29.412 |
| -0.3313161E 02 | -0.8148989E 02 | 0.8826413E 02 | 247.953 | 41.325 | 0.007460 | 6 | 35.294 |
| 0.1190799E 03 | -0.6164860E 02 | 0.1340634E 03 | 331.895 | 47.413 | 0.010998 | 7 | 41.176 |
| -0.1334479E 02 | 0.2908311E 01 | 0.1334799E 02 | 176.792 | 22.344 | 0.001292 | 8 | 47.059 |
| -0.1914048E 02 | -0.3005696E 02 | 0.4259914E 02 | 243.300 | 27.033 | 0.003591 | 9 | 52.941 |
| -0.1911929E 02 | -0.2424294E 02 | 0.3087490E 02 | 231.799 | 25.174 | 0.002483 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 8 CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1144590E 05 | | | | | | | |
| 0.1827659E 04 | 0.1776197E 04 | 0.4219670E 04 | 24.893 | 24.893 | 1.000000 | 1 | 5.882 |
| 0.7783439E 03 | 0.6863354E 03 | 0.1174316E 04 | 49.009 | 24.502 | 0.278295 | 2 | 11.765 |
| -0.4151749E 02 | -0.8612942E 01 | 0.4240108E 02 | 191.720 | 63.907 | 0.010049 | 3 | 17.647 |
| 0.7564086E 02 | 0.7218239E 02 | 0.1045612E 03 | 43.697 | 10.914 | 0.024779 | 4 | 23.529 |
| -0.9974978E 01 | 0.4425719E 02 | 0.4528118E 02 | 102.200 | 20.442 | 0.010731 | 5 | 29.412 |
| -0.4047211E 02 | -0.2611432E 02 | 0.5413911E 02 | 206.450 | 34.408 | 0.012830 | 6 | 35.294 |
| 0.1728012E 03 | -0.9861178E 02 | 0.1998629E 03 | 332.312 | 47.473 | 0.046113 | 7 | 41.176 |
| -0.1396360E 03 | 0.2331214E 02 | 0.2717422E 03 | 170.921 | 19.115 | 0.064398 | 8 | 47.059 |
| -0.1669439E 03 | -0.3709108E 02 | 0.1710142E 03 | 192.525 | 21.392 | 0.040528 | 9 | 52.941 |
| 0.5755099E 01 | -0.4377019E 02 | 0.4416670E 02 | 277.487 | 27.749 | 0.010467 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 12 CH. BEND 137

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6884293E 04 | | | | | | | |
| 0.1536260E 04 | 0.5648271E 03 | 0.1458731E 04 | 22.913 | 22.913 | 1.000000 | 1 | 5.882 |
| 0.2814144E 03 | 0.1848730E 03 | 0.3372579E 03 | 33.445 | 16.722 | 0.231174 | 2 | 11.765 |
| -0.6697818E 02 | -0.1312869E 03 | 0.1473879E 03 | 242.971 | 80.990 | 0.101005 | 3 | 17.647 |
| 0.7327256E 01 | 0.4993764E 02 | 0.5004694E 02 | 81.581 | 20.395 | 0.034298 | 4 | 23.529 |
| -0.1440645E 02 | 0.6601044E 02 | 0.6735981E 02 | 102.104 | 20.421 | 0.046018 | 5 | 29.412 |
| -0.9420790E 01 | -0.2674562E 01 | 0.9740345E 01 | 194.717 | 32.453 | 0.006714 | 6 | 35.294 |
| 0.2459043E 03 | -0.4914480E 01 | 0.2495936E 03 | 358.855 | 51.265 | 0.169524 | 7 | 41.176 |
| -0.9842230E 02 | 0.1156643E 03 | 0.1513378E 03 | 129.578 | 16.197 | 0.104818 | 8 | 47.059 |
| -0.1212264E 03 | -0.1222018E 03 | 0.1721311E 03 | 225.230 | 25.025 | 0.118651 | 9 | 52.941 |
| -0.1992944E 02 | -0.1353770E 02 | 0.2409261E 02 | 214.188 | 21.419 | 0.016607 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 16

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1281212E 03 | | | | | | | |
| 0.45257268 01 | 0.4469C945E 02 | 0.47127268 02 | 84.485 | 84.489 | 0.681527 | 1 | 5.882 |
| -0.56732798 02 | -0.39939448 02 | 0.69149948 02 | 214.872 | 107.436 | 1.000000 | 2 | 11.765 |
| 0.99481978 01 | -0.30361838 02 | 0.31681388 02 | 288.565 | 99.532 | 0.458157 | 3 | 17.647 |
| -0.28204588 02 | 0.11100098 01 | 0.29661748 02 | 182.585 | 40.521 | 0.4286[illegible] | 4 | 23.529 |
| -0.33623378 01 | 0.27843968 02 | 0.28046238 02 | 96.886 | 19.377 | 0.405988 | 5 | 29.412 |
| -0.19059298 02 | 0.64028098 01 | 0.16391718 02 | 146.783 | 20.117 | 0.237047 | 6 | 35.294 |
| -0.64642718 01 | -0.49544238 01 | 0.81445128 01 | 217.463 | 31.067 | 0.117781 | 7 | 41.176 |
| -0.11633108 02 | -0.10017378 02 | 0.15331778 02 | 220.732 | 27.591 | 0.222000 | 8 | 47.059 |
| -0.48983668 01 | -0.24296048 02 | 0.24599828 02 | 260.410 | 28.934 | 0.355748 | 9 | 52.941 |
| -0.33883998 01 | -0.62027118 01 | 0.70678758 01 | 241.353 | 24.135 | 0.102211 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| .1513028 03 | | | | | | | |
| 0.14043678 02 | 0.36150318 00 | 0.38782338 02 | 68.770 | 68.770 | 0.[illegible]4727 | 1 | 5.882 |
| -0.3[illegible]6038 02 | -0.27469088 02 | 0.41091358 02 | 222.002 | 111.001 | 1.000000 | 2 | 11.765 |
| -0.1[illegible]23408 01 | -0.12169488 02 | 0.12219738 02 | 265.011 | 88.337 | 0.297972 | 3 | 17.647 |
| -0.11[illegible]9748 02 | 0.14063888 01 | 0.13468988 02 | 173.635 | 43.409 | 0.326885 | 4 | 23.529 |
| -0.40 [illegible]258 01 | 0.10024848 02 | 0.11716888 02 | 114.562 | 22.912 | 0.[illegible]999 | 5 | 29.412 |
| -0.10[illegible]9478 02 | 0.69914888 01 | 0.12927378 02 | 147.529 | 24.587 | 0.310987 | 6 | 35.294 |
| -0.4[illegible]7938 01 | -0.60811888 01 | 0.77089788 01 | 231.695 | 33.100 | 0.[illegible]783 | 7 | 41.176 |
| -0.3[illegible]3888 01 | -0.33788888 01 | 0.46879338 01 | 226.116 | 28.269 | 0.114189 | 8 | 47.059 |
| -0.2827[illegible]38 01 | -0.10763888 02 | 0.10959188 02 | 259.331 | 28.815 | 0.264817 | 9 | 52.941 |
| -0.2758[illegible]88 01 | -0.9[illegible]72798 01 | 0.10236888 02 | 254.365 | 25.436 | 0.249947 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.59481298 02 | | | | | | | |
| [illegible].29819798 02 | 0.17129[illegible]3E 00 | 0.39389458 02 | 29.874 | 29.874 | 1.000000 | 1 | 5.882 |
| 0.57274088 01 | 0.83622[illegible]7E 01 | 0.10119168 02 | 55.528 | 27.764 | 0.256252 | 2 | 11.765 |
| -0.43434088 00 | -0.[illegible]9020[illegible]3E 00 | 0.44436328 01 | 101.421 | 63.974 | 0.113031 | 3 | 17.647 |
| 0.1[illegible]8[illegible]9[illegible]3E 0[illegible] | -0.73[illegible]9[illegible]8E 0[illegible] | 0.19710448 02 | 331.914 | 82.978 | 0.[illegible]0849 | 4 | 23.529 |
| 0.16[illegible]8076[illegible] 01 | -0.[illegible]0909[illegible]3E 01 | 0.82316748 01 | 281.320 | 56.264 | 0.2[illegible]9948 | 5 | 29.412 |
| 0.[illegible]7843[illegible]3E 01 | -0.40737[illegible]1E 01 | 0.49258828 01 | 304.152 | 50.692 | 0.143215 | 6 | 35.294 |
| -0.66[illegible]5118 00 | -0.2[illegible]807[illegible]1E 00 | 0.26358708 01 | 259.462 | 36.498 | 0.[illegible]6824 | 7 | 41.176 |
| -0.72[illegible]78728 00 | -0.[illegible]0[illegible]0[illegible]8E 01 | 0.30[illegible]8[illegible]8E 01 | 256.457 | 32.[illegible]57 | 0.[illegible]0731 | 8 | 47.059 |
| 0.[illegible]9[illegible]7[illegible]9[illegible]2 00 | -0.[illegible]3[illegible]97[illegible]1E 01 | 0.24[illegible]0[illegible]5E 01 | 284.344 | 31.594 | 0.[illegible]6[illegible]9 | 9 | 52.941 |
| -0.9[illegible]6[illegible]52[illegible]E-01 | -0.[illegible]2[illegible]6[illegible]6E 01 | 0.22[illegible]7[illegible]3E 01 | 267.588 | 26.739 | 0.[illegible]6[illegible]2[illegible] | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 505 CTR 354 CR 66.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.34[illegible].5958 01 | | | | | | | |
| 0.15823638 01 | -0.276[illegible]3458 00 | 0.15278198 01 | 349.967 | 349.967 | 1.000000 | 1 | 5.882 |
| -0.13423968-[illegible] | -0.60363468-01 | [illegible].42309[illegible]E-01 | 259.667 | 127.833 | 0.040788 | 2 | 11.765 |
| 0.36747278-[illegible] | -0.32376928-01 | [illegible].4[illegible]9[illegible]77E-01 | 318.567 | 106.196 | 0.032836 | 3 | 17.647 |
| -0.8[illegible]9[illegible]8-[illegible] | 0.19868278-[illegible] | 0.12909968-01 | .28.622 | 32.155 | 0.[illegible]8488 | 4 | 23.529 |
| 0.17[illegible]9[illegible]2E-01 | -0.[illegible]1[illegible]9[illegible]8-01 | 0.20682878-01 | 327.248 | 65.448 | 0.013518 | 5 | 29.412 |
| -0.9[illegible]7[illegible]8-02 | -0.16[illegible]71[illegible]E-01 | 0.17272[illegible]E-01 | 233.133 | 38.189 | 0.[illegible]1[illegible]3[illegible] | 6 | 35.294 |
| 0.[illegible]2[illegible]8[illegible]-09 | -0.49787[illegible]E-02 | 0.49787[illegible]E-02 | 277.041 | 38.577 | 0.[illegible]2[illegible]7 | 7 | 41.176 |
| 0.16[illegible]7[illegible]-[illegible] | -0.69191[illegible]E-02 | [illegible].[illegible]1[illegible]9[illegible]E-02 | 283.[illegible]8 | 35.[illegible]1 | 0.[illegible]4[illegible]9 | 8 | 47.059 |
| -0.67[illegible]9[illegible]E-[illegible] | -0.27[illegible]1[illegible]-[illegible]3 | [illegible].72611[illegible]E-[illegible]3 | 282.671 | 22.519 | 0.[illegible]0[illegible]5 | 9 | 52.941 |
| -0.[illegible]8[illegible]9[illegible]E-01 | -0.[illegible]9[illegible]1[illegible]E-[illegible]3 | 0.13[illegible]6[illegible]7E-01 | 182.198 | 18.228 | 0.[illegible]0[illegible]2 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1?

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.18266C7E 05 | | | | | | | |
| 0.54801566 04 | -0.6979223E 04 | 0.8818699E 04 | 308.420 | 308.420 | 1.000000 | 1 | 5.882 |
| -0.9424287E 03 | 0.1857417E 04 | 0.1416440E 04 | 131.789 | 65.895 | 0.160618 | 2 | 11.765 |
| 0.1442292E 04 | -5.8804877E 02 | 0.1444856E 04 | 354.986 | 118.462 | 0.163840 | 3 | 17.647 |
| 0.1809584E 03 | 0.2081134E 03 | 0.2808296E 03 | 47.822 | 11.956 | 0.031845 | 4 | 23.529 |
| 0.1029020E 02 | -0.7504854E 03 | 0.7505557E 03 | 270.785 | 54.157 | 0.085110 | 5 | 29.412 |
| 0.4270192E 02 | 0.1324516E 03 | 0.1464534E 03 | 64.667 | 10.778 | 0.016617 | 6 | 35.294 |
| -0.9446988E 01 | 0.1637539E 03 | 0.1640257E 03 | 93.302 | 13.329 | 0.018600 | 7 | 41.176 |
| 0.2102803E 02 | 0.6995523E 02 | 0.7256860E 02 | 73.156 | 9.144 | 0.008229 | 8 | 47.059 |
| 0.5984893E 02 | 0.1406860E 02 | 0.5128555E 02 | 13.271 | 1.475 | 0.006949 | 9 | 52.941 |
| -0.1539277E 02 | 0.2280320E 02 | 0.2002145E 02 | 140.247 | 14.025 | 0.002270 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.5275676E 04 | | | | | | | |
| 0.2592262E 04 | -0.1636164E 04 | 0.3065418E 04 | 327.741 | 327.741 | 1.000000 | 1 | 5.882 |
| -0.1036670E 03 | 0.1149316E 02 | 0.1041821E 03 | 173.674 | 86.837 | 0.034025 | 2 | 11.765 |
| 0.3381900E 02 | -0.1156826E 03 | 0.1205246E 03 | 286.296 | 95.432 | 0.039318 | 3 | 17.647 |
| -0.4362424E 02 | -0.5177681E 02 | 0.8202974E 02 | 219.138 | 54.785 | 0.026760 | 4 | 23.529 |
| 0.1263010E 02 | 0.3994551E 02 | 0.3990375E 02 | 87.033 | 17.407 | 0.013019 | 5 | 29.412 |
| -0.7531076E 02 | 0.1139854E 01 | 0.7531926E 02 | 179.137 | 29.856 | 0.024571 | 6 | 35.294 |
| 0.1919096E 02 | -0.8678851E 02 | 0.8788458E 02 | 282.474 | 40.353 | 0.028697 | 7 | 41.176 |
| 0.7544684E 02 | -0.9431715E 02 | 0.1207931E 03 | 308.665 | 38.583 | 0.039403 | 8 | 47.059 |
| -0.2290499E 02 | 0.1639528E 02 | 0.2784383E 02 | 143.926 | 15.992 | 0.009083 | 9 | 52.941 |
| -0.3117693E 02 | 0.2717122E 02 | 0.4139516E 02 | 138.927 | 13.893 | 0.013491 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2421130E 04 | | | | | | | |
| 0.3176004E 03 | -0.4479557E 03 | 0.5487996E 03 | 305.361 | 305.361 | 1.000000 | 1 | 5.882 |
| -0.1.941708 03 | -0.9398211E 02 | 0.1487869E 03 | 219.133 | 109.566 | 0.271113 | 2 | 11.765 |
| -0.2364710 03 | -0.1550089E 00 | 0.2364705E 03 | 180.038 | 60.013 | 0.430807 | 3 | 17.647 |
| -0.7454736E 02 | 0.2391283E 02 | 0.7823967E 02 | 162.215 | 40.554 | 0.142654 | 4 | 23.529 |
| 0.9888501E 01 | 0.1988391E 03 | 0.1990467E 03 | 87.382 | 17.477 | 0.362695 | 5 | 29.412 |
| 0.4569097E 02 | -0.1400928E 02 | 0.4776207E 02 | 342.957 | 57.159 | 0.087096 | 6 | 35.294 |
| 0.1082159E 02 | -0.1420764E 02 | 0.1785954E 02 | 307.295 | 43.899 | 0.032543 | 7 | 41.176 |
| -0.1257981E 01 | 0.1323642E 01 | 0.1826073E 01 | 133.543 | 16.693 | 0.003327 | 8 | 47.059 |
| -0.1620984E 02 | 0.8917540E 01 | 0.1380118E 02 | 139.031 | 15.448 | 0.024784 | 9 | 52.941 |
| 0.1945013E 02 | -0.2052777E 02 | 0.2827890E 02 | 313.456 | 31.346 | 0.051529 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.9487266E 03 | | | | | | | |
| -0.6122629E 03 | -0.3943718E 03 | 0.7282822E 03 | 212.786 | 212.786 | 1.000000 | 1 | 5.882 |
| -0.1791567E 03 | -0.1234662E 03 | 0.2142971E 03 | 214.179 | 107.554C | 0.294250 | 2 | 11.765 |
| -0.4629092E 03 | 0.1289188E 02 | 0.4631138E 03 | 178.173 | 59.391 | 0.635913 | 3 | 17.647 |
| 0.7403726E 01 | 0.4987998 02 | 0.4628241E 02 | 80.765 | 20.186 | 0.063550 | 4 | 23.529 |
| 0.1660259E 02 | -0.4424408E 02 | 0.4725656E 02 | 290.569 | 58.114 | 0.064888 | 5 | 29.412 |
| 0.3343102E 02 | 0.4846190E 02 | 0.5887440E 02 | 55.400 | 9.233 | 0.080840 | 6 | 35.294 |
| -0.1389629E 02 | 0.5543643E 02 | 0.5715158E 02 | 104.072 | 14.867 | 0.078476 | 7 | 41.176 |
| 0.2908673E 02 | 0.5167409E 02 | 0.6475779E 02 | 62.607 | 7.826 | 0.089193 | 8 | 47.059 |
| 0.8964321E 01 | 0.5642212E 01 | 0.1059215E 02 | 32.107 | 3.576 | 0.014546 | 9 | 52.941 |
| 0.3983521E 02 | -0.4031864E 01 | 0.4012768E 02 | 353.085 | 39.368 | 0.055048 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 19

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2166649E 03 | | | | | | | |
| -0.9427456E 03 | -0.3722334E 03 | 0.1013571E 04 | 201.546 | 201.546 | 1.000000 | 1 | 5.882 |
| -0.2736411E 03 | -0.1627944E 03 | 0.3184036E 03 | 210.749 | 105.375 | 0.314140 | 2 | 11.765 |
| -0.4200071E 03 | -0.2874681E 01 | 0.4200168E 03 | 180.392 | 60.131 | 0.414393 | 3 | 17.647 |
| 0.1604473E 03 | 0.1007452E 03 | 0.1894563E 03 | 32.125 | 8.031 | 0.186918 | 4 | 23.529 |
| 0.1073020E 02 | -0.1972526E 03 | 0.1975442E 03 | 273.114 | 54.623 | 0.194899 | 5 | 29.412 |
| 0.2862613E 02 | 0.7937239E 02 | 0.8472118E 02 | 69.522 | 11.589 | 0.083587 | 6 | 35.294 |
| -0.4350948E 02 | 0.6126047E 02 | 0.7513931E 02 | 125.384 | 17.912 | 0.074133 | 7 | 41.176 |
| 0.4059504E 02 | 0.4357430E 02 | 0.5955309E 02 | 47.027 | 5.878 | 0.058757 | 8 | 47.059 |
| -0.1028840E 02 | -0.1709924E 02 | 0.1995583E 02 | 238.965 | 26.552 | 0.019689 | 9 | 52.941 |
| -0.1246C49E 02 | 0.8178575E 00 | 0.1248730E 02 | 176.245 | 17.624 | 0.012320 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1677538E 03 | | | | | | | |
| -0.1112041E 04 | -0.3522449E 03 | 0.1166495E 04 | 197.576 | 197.576 | 1.000000 | 1 | 5.882 |
| -0.4203564E 03 | -0.1772735E 03 | 0.4562075E 03 | 202.866 | 101.433 | 0.391093 | 2 | 11.765 |
| -0.2846365E 03 | 0.8618901E 02 | 0.2968257E 03 | 163.523 | 54.508 | 0.254460 | 3 | 17.647 |
| 0.1375964E 03 | 0.1206521E 03 | 0.1829718E 03 | 41.254 | 10.314 | 0.156856 | 4 | 23.529 |
| 0.1055353E 02 | -0.2580957E 03 | 0.2583113E 03 | 272.342 | 54.468 | 0.221442 | 5 | 29.412 |
| 0.2502590E 01 | -0.3208691E 02 | 0.3218434E 02 | 274.460 | 45.743 | 0.027591 | 6 | 35.294 |
| 0.1516762E 02 | -0.7327652E 02 | 0.7482980E 02 | 281.695 | 40.242 | 0.064149 | 7 | 41.176 |
| 0.6690378E 01 | -0.1600970E 02 | 0.1739138E 02 | 292.680 | 36.585 | 0.014875 | 8 | 47.059 |
| 0.1046851E 02 | 0. 9931993E 02 | 0.2251379E 02 | 62.291 | 6.921 | 0.019300 | 9 | 52.941 |
| -0.2663705E 02 | 0.3893211E 02 | 0.4716963E 02 | 124.375 | 12.437 | 0.040437 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4183877E 03 | | | | | | | |
| -0.9661118E 03 | -0.1673812E 03 | 0.9805042E 03 | 189.829 | 189.829 | 1.000000 | 1 | 5.882 |
| -0.5890662E 03 | -0.1549273E 03 | 0.6090986E 03 | 194.735 | 97.368 | 0.621210 | 2 | 11.765 |
| -0.1436263E 03 | 0.3509772E 02 | 0.1478525E 03 | 166.268 | 55.423 | 0.150792 | 3 | 17.647 |
| 0.1212641E 03 | 0.1020442E 03 | 0.1584865E 03 | 40.081 | 10.020 | 0.161638 | 4 | 23.529 |
| 0.3085C13E 02 | -0.1332185E 03 | 0.1367439E 03 | 283.038 | 56.6C8 | 0.139463 | 5 | 29.412 |
| -0.7771640E 01 | -0.4426451E 02 | 0.4492383E 02 | 260.038 | 43.340 | 0.045817 | 6 | 35.294 |
| 0.7049690E 02 | -0.7770024E 02 | 0.1049149E 03 | 312.217 | 44.602 | 0.107001 | 7 | 41.176 |
| 0.3172775E C2 | -0.5186583E 02 | 0.6080060E 02 | 301.455 | 37.602 | 0.062010 | 8 | 47.059 |
| 0.1639026E 02 | 0.5224900E 01 | 0.1720290E 02 | 17.681 | 1.965 | 0.017545 | 9 | 52.941 |
| 0.6774027E 01 | C.6302375E 01 | 0.9252424E 01 | 42.934 | 4.293 | 0.CC9436 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6713997E C3 | | | | | | | |
| -0.5396274E 03 | -0.1032323E 03 | 0.5494128E 03 | 190.830 | 190.830 | 0.998982 | 1 | 5.8P2 |
| -0.5486567E C3 | -0.1516316E 03 | 0.5499727E 03 | 196.004 | 98.002 | 1.CC0000 | 2 | 11.765 |
| -0.7013872E C2 | 0.6168597E 02 | 0.9342807E 02 | 138.681 | 46.227 | C.169878 | 3 | 17.647 |
| 0.1142995E 03 | 0.1293200E 03 | 0.1725914E 03 | 48.528 | 12.132 | 0.313818 | 4 | 23.529 |
| 0.1668787E 02 | -0.8232872E 02 | 0.8400298E 02 | 281.458 | 56.292 | 0.152740 | 5 | 29.412 |
| -0.4339734E 02 | -0.7286127E 02 | 0.8486818E 02 | 239.221 | 39.870 | 0.154201 | 6 | 35.294 |
| 0.7078692E 02 | -0.4660762E 02 | 0.8473621E 02 | 326.631 | 44.662 | 0.154073 | 7 | 41.176 |
| 0.3896722E 02 | 0.1202103E 02 | 0.4077927E 02 | 17.145 | 2.143 | 0.074148 | 8 | 47.059 |
| 0.4152767E 01 | -C.6099158E 02 | 0.6113280E 02 | 273.895 | 30.433 | 0.111156 | 9 | 52.941 |
| -0.1224052E 02 | -C.6868835E 02 | 0.7587845E 02 | 244.856 | 24.486 | C.137968 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 6C.C TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2954357E 05 | | | | | | | |
| 0.2985378E 05 | 0.1379978E 04 | 0.2988565E 05 | 2.647 | 2.647 | 1.000000 | 1 | 5.882 |
| 0.2949873E 04 | 0.9748835E 03 | 0.3102993E 04 | 18.311 | 9.156 | 0.103829 | 2 | 11.765 |
| 0.2917984E 04 | -0.1768121E 04 | 0.3407598E 04 | 328.743 | 109.581 | 0.114021 | 3 | 17.647 |
| -0.1602893E 03 | -0.7677703E 03 | 0.7843237E 03 | 258.208 | 64.552 | 0.026244 | 4 | 23.529 |
| 0.2631240E 03 | -0.1346488E 04 | 0.1371956E 04 | 281.057 | 56.211 | 0.045907 | 5 | 29.412 |
| 0.5670453E 02 | -0.6765042E 03 | 0.6788762E 03 | 274.791 | 45.799 | 0.022716 | 6 | 35.294 |
| 0.3855034E 01 | -0.3157617E 03 | 0.3157849E 03 | 270.699 | 38.671 | 0.010566 | 7 | 41.176 |
| 0.2829340E 02 | -0.4405503E 03 | 0.4414377E 03 | 273.675 | 34.209 | 0.014771 | 8 | 47.059 |
| -0.9007324E 02 | -0.2526460E 03 | 0.2682222E 03 | 250.378 | 27.820 | 0.008975 | 9 | 52.941 |
| 0.1502799E 03 | -0.3967495E 03 | 0.4242561E 03 | 290.746 | 29.075 | 0.014196 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 6C.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2254848E 05 | | | | | | | |
| 0.1762688E 05 | 0.1395082E 04 | 0.1768199E 05 | 4.525 | 4.525 | 1.000000 | 1 | 5.882 |
| 0.1970019E 04 | 0.6144138E 03 | 0.2063608E 04 | 17.322 | 8.661 | 0.116707 | 2 | 11.765 |
| 0.2400189E 04 | -0.9856016E 03 | 0.2594855E 04 | 337.677 | 112.559 | 0.146751 | 3 | 17.647 |
| -0.4268425E 03 | -0.5193403E 03 | 0.6722415E 03 | 230.583 | 57.646 | 0.038018 | 4 | 23.529 |
| -0.4172893E 03 | -0.9463027E 03 | 0.1034224E 04 | 246.204 | 49.241 | 0.058490 | 5 | 29.412 |
| 0.3035530E 03 | -0.2095024E 03 | 0.4264341E 03 | 315.385 | 52.564 | 0.024117 | 6 | 35.294 |
| -0.4161827E 02 | -0.1356286E 03 | 0.1412703E 03 | 252.941 | 36.134 | 0.008023 | 7 | 41.176 |
| -0.1441683E 03 | -0.4410972E 03 | 0.4640593E 03 | 251.900 | 31.488 | 0.026245 | 8 | 47.059 |
| -0.7431298E 02 | -0.8741914E 02 | 0.1147364E 03 | 229.633 | 25.515 | 0.006489 | 9 | 52.941 |
| 0.9322472E 02 | -0.2110986E 03 | 0.2307672E 03 | 293.827 | 29.383 | 0.013051 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 6C.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5285492F 04 | | | | | | | |
| 0.8059965E 04 | 0.2737871E 03 | 0.8064609E 04 | 1.946 | 1.946 | 1.000000 | 1 | 5.882 |
| 0.8819590E 03 | -0.1800211E 01 | 0.8819607E 03 | 359.883 | 179.942 | 0.109362 | 2 | 11.765 |
| 0.1036350E 04 | -0.7681991E 03 | 0.1290015E 04 | 323.452 | 107.817 | 0.159961 | 3 | 17.647 |
| -0.3161184E 03 | 0.5950862E 02 | 0.3216707E 03 | 169.339 | 42.335 | 0.039887 | 4 | 23.529 |
| -0.4949341E 03 | -0.3433433E 03 | 0.6023655E 03 | 214.750 | 42.950 | 0.074692 | 5 | 29.412 |
| 0.2564072E 03 | -0.1989147E 03 | 0.3245173E 03 | 322.197 | 53.699 | 0.040240 | 6 | 35.294 |
| -0.2285133E 03 | 0.1101071E 03 | 0.2536571E 03 | 154.273 | 22.039 | 0.031453 | 7 | 41.176 |
| -0.3224150E 03 | 0.1771201E 02 | 0.3229000E 03 | 176.056 | 22.107 | 0.040039 | 8 | 47.059 |
| 0.2237713E 03 | 0.8419824E 02 | 0.2390877E 03 | 20.620 | 7.291 | 0.029647 | 9 | 52.941 |
| -0.6469824F 02 | 0.2144443E 02 | 0.6815959E 02 | 161.662 | 18.165 | 0.008452 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 351 CR 6C.0 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4270734F 04 | | | | | | | |
| 0.3466219E 04 | 0.4456782E 03 | 0.3494753E 04 | 7.327 | 7.327 | 1.000000 | 1 | 5.882 |
| 0.4226960E 03 | 0.5877267E 02 | 0.4267622E 03 | 7.916 | 3.958 | 0.122119 | 2 | 11.765 |
| 0.3830291E 03 | -0.3271858E 03 | 0.5037478F 03 | 319.496 | 106.499 | 0.144144 | 3 | 17.647 |
| -0.1487965E 03 | 0.7823351E 02 | 0.1681097E 03 | 152.266 | 38.066 | 0.048103 | 4 | 23.529 |
| -0.3292852E 03 | -0.2019071E 03 | 0.3862578E 03 | 211.515 | 42.303 | 0.110525 | 5 | 29.412 |
| 0.1293250F 03 | -0.1347592E 03 | 0.1867752E 03 | 313.821 | 52.303 | 0.053444 | 6 | 35.294 |
| -0.7790039E 02 | 0.1078941E 03 | 0.1330775E 03 | 125.830 | 17.976 | 0.038079 | 7 | 41.176 |
| -0.9535258E 02 | 0.6115784E 01 | 0.9554849E 02 | 176.330 | 22.041 | 0.027341 | 8 | 47.059 |
| 0.1199929E 03 | 0.1281816E 03 | 0.1830095E 03 | 49.030 | 5.448 | 0.052367 | 9 | 52.941 |
| -0.5772423E 02 | 0.7846537E 01 | 0.5825508E 02 | 172.259 | 17.226 | 0.016669 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 1

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.6624707E 02 | | | | | | | |
| 0.2345677E 02 | 0.6678510E 02 | 0.7031308E 02 | 70.912 | 70.912 | 1.000000 | 1 | 5.882 |
| -0.7122544E 01 | -0.1558419E 02 | 0.1713467E 02 | 245.438 | 122.719 | 0.243691 | 2 | 11.765 |
| -0.3262329E 02 | -0.3076651E 02 | 0.4484258E 02 | 223.322 | 74.441 | 0.637756 | 3 | 17.647 |
| -0.9718184E 00 | -0.2367737E 02 | 0.2369730E 02 | 267.649 | 66.912 | 0.337025 | 4 | 23.529 |
| 0.2117451E 02 | -0.5631589E 02 | 0.6016510E 02 | 290.606 | 58.121 | 0.855674 | 5 | 29.412 |
| 0.7129936E 01 | -0.3060257E 01 | 0.7755262E 01 | 336.759 | 56.126 | 0.110296 | 6 | 35.294 |
| 0.1318399E 02 | 0.1264311E 02 | 0.1826451E 02 | 43.800 | 6.257 | 0.259788 | 7 | 41.176 |
| 0.3208593E 01 | 0.9897806E 01 | 0.1040488E 02 | 72.039 | 9.005 | 0.147979 | 8 | 47.059 |
| 0.7425096E 00 | 0.1858647E 01 | 0.2001471E 01 | 68.224 | 7.580 | 0.028465 | 9 | 52.941 |
| 0.9646844E 00 | 0.4239066E 00 | 0.1053745E 01 | 23.726 | 2.373 | 0.014986 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1301C16E 03 | | | | | | | |
| -0.3C24857E 02 | 0.2431602E 02 | 0.3881016E 02 | 141.205 | 141.205 | 1.CC0CCC | 1 | 5.882 |
| -0.2091024E 00 | -0.3604390E 01 | 0.3610450E 01 | 266.680 | 133.340 | 0.093028 | 2 | 11.765 |
| 0.6961534E 01 | -0.1455519E 02 | 0.1613432E 02 | 295.561 | 98.520 | 0.415722 | 3 | 17.647 |
| -0.1269278E 01 | -0.3356500E 01 | C.3629052E 01 | 247.807 | 61.952 | 0.093484 | 4 | 23.529 |
| 0.6637993E 01 | -0.2602849E 02 | 0.2684148E 02 | 284.306 | 56.861 | 0.692121 | 5 | 29.412 |
| -0.4763180E 01 | -0.6549051E 00 | 0.4807990E 01 | 187.729 | 31.365 | 0.123804 | 6 | 35.294 |
| 0.1113729E C2 | 0.3314198E 01 | 0.1161994E 02 | 16.572 | 2.367 | 0.2994U3 | 7 | 41.176 |
| -0.7829460E 01 | -0.9508945E 01 | 0.1156298E 02 | 227.381 | 28.423 | 0.297899 | 8 | 47.059 |
| 0.5591542E 01 | 0.2378929E 01 | 0.6076564E 01 | 23.047 | 2.561 | 0.156571 | 9 | 52.941 |
| 0.1017575E 01 | -0.7200661E 01 | 0.7272205E 01 | 278.043 | 27.804 | 0.187378 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.9349395E 02 | | | | | | | |
| -0.6620718E 02 | 0.1077673E 02 | 0.6707851E 02 | 170.795 | 170.795 | 1.CCCCCC | 1 | 5.882 |
| -0.1403109E C2 | 0.6249115E 01 | 0.1535979E 02 | 155.993 | 77.996 | 0.228982 | 2 | 11.765 |
| 0.7881586E C1 | 0.2229427E 02 | 0.2358051E 02 | 70.988 | 23.663 | 0.351536 | 3 | 17.647 |
| -0.5593994E 01 | 0.6435404E 01 | 0.8526851E 01 | 130.999 | 32.750 | 0.127117 | 4 | 23.529 |
| 0.1379910E 00 | 0.3121521E 01 | 0.3124569E C1 | 87.489 | 17.494 | 0.046581 | 5 | 29.412 |
| -0.1711549E 01 | -0.1710207E 00 | 0.1720367E 01 | 185.706 | 30.951 | 0.025043 | 6 | 35.294 |
| 0.3493504E C1 | -0.2851030E 01 | 0.4509205E 01 | 320.782 | 45.826 | 0.067229 | 7 | 41.176 |
| -0.5258170E 00 | -0.8534834E 00 | 0.1002455E 01 | 238.363 | 29.795 | 0.014964 | 8 | 47.059 |
| -0.8126864E 00 | -0.8199869E 00 | 0.1154186E C1 | 225.241 | 25.027 | 0.017206 | 9 | 52.941 |
| 0.1173022E 01 | -0.4718212E 00 | 0.1264280E 01 | 338.097 | 33.810 | C.018848 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 351 CR 60.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1108750E 02 | | | | | | | |
| 0.1210299E 01 | -0.1569892E 01 | 0.1982266E 01 | 307.630 | 307.630 | 1.CCC000 | 1 | 5.882 |
| -0.3545284E-C2 | -0.7042456E-01 | 0.7051367E-01 | 267.118 | 133.559 | 0.035572 | 2 | 11.765 |
| -0.7110423E-01 | -0.9306008E-01 | 0.1171153E 00 | 232.618 | 77.539 | 0.059081 | 3 | 17.647 |
| -0.1170118E 00 | -0.7710136E-02 | 0.1172655E 00 | 183.770 | 45.947 | 0.059157 | 4 | 23.529 |
| -0.7419952E-01 | 0.7193232E-01 | 0.1038614E 00 | 136.165 | 27.233 | 0.052395 | 5 | 29.412 |
| 0.3983254E-01 | 0.1028278E 00 | 0.1102732E 00 | 68.825 | 11.471 | 0.055630 | 6 | 35.294 |
| 0.7901646E-01 | 0.1187250E-01 | 0.7990158E-01 | 8.545 | 1.221 | 0.040308 | 7 | 41.176 |
| 0.5469402E-01 | -0.9209919E-01 | 0.1068102E 00 | 300.427 | 37.553 | 0.053883 | 8 | 47.059 |
| -0.2450636E-01 | -0.5484181E-01 | 0.6008643E-01 | 245.930 | 27. | C.C30312 | 9 | 52.941 |
| -0.5616871E-01 | -0.1121198E-01 | 0.5727680E-01 | 191.28. | 19.1. | .028895 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 21

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1717200E 05 | | | | | | | |
| -0.4547887E 04 | -0.6795734E 04 | 0.8163902E 04 | 236.052 | 236.052 | 1.000000 | 1 | 6.061 |
| 0.1052775E 04 | -0.2715237E 03 | 0.1053125E 04 | 350.522 | 170.261 | 0.129114 | 2 | 12.121 |
| 0.4182493E 03 | 0.5501779E 02 | 0.4218523E 03 | 7.494 | 2.498 | 0.051800 | 3 | 18.182 |
| 0.2208095E 02 | 0.1026714E 02 | 0.2435939E 02 | 24.928 | 6.232 | 0.002991 | 4 | 24.242 |
| 0.1889558E 03 | -0.3211879E 03 | 0.3726465E 03 | 300.469 | 60.094 | 0.045758 | 5 | 30.303 |
| 0.1242444E 03 | -0.6291128E 02 | 0.1390838E 03 | 333.292 | 55.546 | 0.017078 | 6 | 36.364 |
| 0.1007845E 03 | -0.1365332E 02 | 0.1017051E 03 | 352.285 | 50.326 | 0.012488 | 7 | 42.424 |
| -0.1953630E 02 | -0.7785318E 02 | 0.8026741E 02 | 255.912 | 31.989 | 0.009856 | 8 | 48.485 |
| -0.3735925E 02 | -0.6103722E 02 | 0.7156293E 02 | 238.530 | 26.503 | 0.008787 | 9 | 54.545 |
| 0.4436849E 01 | -0.5508824E 02 | 0.5524667E 02 | 274.606 | 27.461 | 0.006784 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| C.1237883E 04 | | | | | | | |
| -0.9307637E 03 | -0.1763786E 04 | 0.1976441E 04 | 241.908 | 241.908 | 1.000000 | 1 | 6.061 |
| 0.2983134E 02 | -0.6322594E 01 | 0.3049399E 02 | 348.033 | 174.017 | 0.015427 | 2 | 12.121 |
| 0.1451369E 02 | -0.1541176E 02 | 0.2117000E 02 | 313.281 | 104.427 | 0.010710 | 3 | 18.182 |
| -0.1594333E 02 | -0.9805522E 02 | 0.9927950E 02 | 260.992 | 65.248 | 0.050226 | 4 | 24.242 |
| -0.1414781E 03 | 0.2274187E 03 | 0.2681099E 03 | 121.980 | 24.380 | 0.135639 | 5 | 30.303 |
| -0.1011342E 03 | 0.5074259E 01 | 0.1012614E 03 | 177.128 | 29.521 | 0.051229 | 6 | 36.364 |
| -0.1334582E 03 | -0.4300807E 02 | 0.1402177E 03 | 197.662 | 28.266 | 0.070937 | 7 | 42.424 |
| 0.9111879E 02 | -0.3232189E 02 | 0.4498737E 02 | 313.914 | 39.239 | 0.022699 | 8 | 48.485 |
| 0.1543247E 02 | -0.8169482E 01 | 0.1555418E 02 | 356.967 | 39.662 | 0.007818 | 9 | 54.545 |
| 0.3106279E 02 | 0.1890016E 02 | 0.3701974E 02 | 19.336 | 1.934 | 0.018654 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3416179E 03 | | | | | | | |
| -0.8906125E 02 | -0.4641821E 03 | 0.4719114E 03 | 259.616 | 259.616 | 1.000000 | 1 | 6.061 |
| -0.1916643E 03 | -0.4697156E 02 | 0.1973361E 03 | 193.770 | 96.885 | 0.418163 | 2 | 12.121 |
| -0.5777837E 02 | 0.6247228E 01 | 0.5811511E 02 | 173.829 | 57.943 | 0.123148 | 3 | 18.182 |
| -0.2282514E 02 | -0.6559766E 02 | 0.6919650E 02 | 251.440 | 62.860 | 0.146538 | 4 | 24.242 |
| -0.5528089E 02 | 0.8364880E 02 | 0.1002695E 03 | 123.463 | 24.693 | 0.212475 | 5 | 30.303 |
| -0.4210778E 02 | 0.8735847E 01 | 0.4300394E 02 | 348.279 | 28.047 | 0.091127 | 6 | 36.364 |
| -0.6409820E 01 | -0.9518703E 01 | 0.1347149E 02 | 234.495 | 33.491 | 0.028596 | 7 | 42.424 |
| -0.3935695E 01 | 0.3381911E 02 | 0.3404773E 02 | 96.638 | 12.080 | 0.072148 | 8 | 48.485 |
| -0.1599072E 01 | -0.1840663E 00 | 0.1569908E 01 | 186.733 | 20.748 | 0.003327 | 9 | 54.545 |
| 0.2719818E 01 | 0.1035944E 02 | 0.1071053E 02 | 75.289 | 7.529 | 0.022696 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6546823E 03 | | | | | | | |
| 0.4665105E 02 | -0.3498123E 03 | 0.3529089E 03 | 277.596 | 277.596 | 0.926524 | 1 | 6.061 |
| -0.3797482E 03 | -0.2964864E 02 | 0.3808958E 03 | 184.464 | 92.232 | 1.000000 | 2 | 12.121 |
| -0.1748120E 03 | 0.9401611E 00 | 0.1748128E 03 | 179.823 | 59.941 | 0.458952 | 3 | 18.182 |
| -0.1718910E 02 | -0.4686293E 01 | 0.1781645E 02 | 195.250 | 48.812 | 0.046775 | 4 | 24.242 |
| 0.3545302E 02 | -0.3698384E 02 | 0.5123189E 02 | 313.789 | 62.758 | 0.134504 | 5 | 30.303 |
| 0.1162000E 02 | 0.2017860E 02 | 0.2328529E 02 | 60.064 | 10.011 | 0.061133 | 6 | 36.364 |
| 0.5120990E 02 | 0.3108760E 02 | 0.6032637E 02 | 31.910 | 4.559 | 0.158980 | 7 | 42.424 |
| -0.9485517E-01 | 0.1720891E 02 | 0.1720915E 02 | 90.314 | 11.289 | 0.045391 | 8 | 48.485 |
| -0.1492984E 02 | 0.1793489E 02 | 0.1850951E 02 | 143.782 | 15.976 | 0.048584 | 9 | 54.545 |
| -0.1515727E 02 | -0.2802238E 01 | 0.1541415E 02 | 190.474 | 19.047 | 0.040468 | 10 | 60.606 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 21

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1481052E 04 | | | | | | | |
| 0.2546126E 02 | -0.2479368E 03 | 0.2492407E 03 | 275.863 | 275.863 | 0.540137 | 1 | 6.061 |
| -0.4555847E 03 | -0.7327592E 02 | 0.4614397E 03 | 189.137 | 94.569 | 1.000000 | 2 | 12.121 |
| -0.2088150E 03 | 0.1916452E 02 | 0.2096926E 03 | 174.756 | 58.252 | 0.454431 | 3 | 18.182 |
| 0.1343533E 02 | 0.4095377E 02 | 0.4272137E 02 | 71.670 | 17.918 | 0.092583 | 4 | 24.242 |
| 0.5831960E 02 | -0.1160249E 03 | 0.1298579E 03 | 296.686 | 59.337 | 0.281418 | 5 | 30.303 |
| 0.2462729E 02 | -0.2762831E 01 | 0.2478168E 02 | 353.601 | 58.953 | 0.053705 | 6 | 36.364 |
| -0.1421743E 02 | -0.1447802E 02 | 0.2029156E 02 | 225.520 | 32.217 | 0.043974 | 7 | 42.424 |
| 0.4762817E 01 | -0.3687811E 00 | 0.4777070E 01 | 355.572 | 44.447 | 0.010353 | 8 | 48.485 |
| 0.6431247E 01 | -0.1366738E 01 | 0.6574764E 01 | 348.006 | 38.667 | 0.014248 | 9 | 54.545 |
| 0.6324036E 01 | -0.3787865E 01 | 0.7371555E 01 | 329.081 | 32.908 | 0.015975 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1642639E 04 | | | | | | | |
| 0.4081937E 02 | -0.1979352E 03 | 0.1871635E 03 | 282.346 | 282.346 | 0.418795 | 1 | 6.061 |
| -0.4536011E 03 | -0.4276477E 02 | 0.4556123E 03 | 183.386 | 92.693 | 1.000000 | 2 | 12.121 |
| -0.2184673E 03 | 0.6921228E 02 | 0.2291687E 03 | 162.421 | 54.140 | 0.502991 | 3 | 18.182 |
| 0.2449249E 02 | 0.7376270E 02 | 0.7772266E 02 | 71.632 | 17.908 | 0.170589 | 4 | 24.242 |
| 0.3551212E 02 | -0.1910137E 03 | 0.1913390E 03 | 283.233 | 56.647 | 0.340493 | 5 | 30.303 |
| 0.1122651E 02 | -0.1715471E 02 | 0.2058106E 02 | 303.202 | 50.534 | 0.044998 | 6 | 36.364 |
| -0.2435135E 02 | -0.1078758E 02 | 0.2660150E 02 | 203.736 | 29.105 | 0.058386 | 7 | 42.424 |
| 0.2137569E 02 | 0.1554939E 02 | 0.3279614E 02 | 28.302 | 3.538 | 0.071963 | 8 | 48.485 |
| -0.1871178E 02 | 0.3852079E 02 | 0.3998235E 02 | 105.540 | 11.727 | 0.087755 | 9 | 54.545 |
| 0.4424906E 00 | 0.1284112E 00 | 0.4607888E 00 | 16.184 | 1.618 | 0.001011 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1644611E 04 | | | | | | | |
| 0.5197088E 02 | -0.9184640E 00 | 0.5197736E 02 | 359.891 | 359.891 | 0.131330 | 1 | 6.061 |
| -0.3923491E 03 | -0.1731392E 02 | 0.3927307E 03 | 182.927 | 91.263 | 1.000000 | 2 | 12.121 |
| -0.2296936E 03 | 0.6889995E 02 | 0.2397665E 03 | 163.380 | 54.433 | 0.610511 | 3 | 18.182 |
| 0.9739372E 01 | 0.6079150E 02 | 0.6156673E 02 | 80.898 | 20.224 | 0.156766 | 4 | 24.242 |
| 0.3753931E 02 | -0.1144848E 03 | 0.1204822E 03 | 288.154 | 57.631 | 0.306781 | 5 | 30.303 |
| -0.1562234E 02 | 0.3303612E 02 | 0.3654370E 02 | 115.309 | 19.218 | 0.093050 | 6 | 36.364 |
| -0.7886233E 02 | -0.1138875E 02 | 0.7691020E 02 | 188.516 | 26.931 | 0.195834 | 7 | 42.424 |
| 0.3274406E 02 | 0.3603784E 01 | 0.3294255E 02 | 6.280 | 0.785 | 0.083881 | 8 | 48.485 |
| 0.2737801E 02 | 0.1635465E 02 | 0.3189079E 02 | 30.852 | 3.428 | 0.081203 | 9 | 54.545 |
| 0.1583607E 02 | 0.3582964E 02 | 0.3917325E 02 | 66.155 | 8.616 | 0.099746 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1217499E 04 | | | | | | | |
| 0.1905465E 02 | 0.7903346E 02 | 0.8045448E 02 | 79.215 | 79.215 | 0.327196 | 1 | 6.061 |
| -0.2458599E 03 | -0.3902126E 01 | 0.2458909E 03 | 180.909 | 90.455 | 1.000000 | 2 | 12.121 |
| -0.1065503E 03 | 0.4588013E 02 | 0.1920903E 03 | 166.206 | 55.402 | 0.781201 | 3 | 18.182 |
| 0.2665407E 02 | 0.4956511E 02 | 0.5620085E 02 | 61.732 | 15.433 | 0.228605 | 4 | 24.242 |
| 0.2166170E 02 | -0.7194812E 02 | 0.7513824E 02 | 286.756 | 57.351 | 0.305576 | 5 | 30.303 |
| -0.3436007E 00 | -0.1110600E 02 | 0.1111132E 02 | 268.228 | 44.705 | 0.045188 | 6 | 36.364 |
| -0.8844536E 02 | 0.1458689E 02 | 0.8960014E 02 | 170.635 | 24.376 | 0.364552 | 7 | 42.424 |
| 0.3177612E 02 | 0.1616743E 01 | 0.3181723E 02 | 2.913 | 0.364 | 0.129396 | 8 | 48.485 |
| -0.1429769E 01 | 0.3033737E 02 | 0.3034603E 02 | 92.699 | 10.300 | 0.123494 | 9 | 54.545 |
| 0.6227647E 01 | 0.2591627E 01 | 0.6745377E 01 | 22.595 | 2.259 | 0.027432 | 10 | 60.606 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 21

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3194450E 04 | | | | | | | |
| 0.5891008E 04 | -0.1537976E 04 | 0.6088457E 04 | 345.368 | 345.368 | 1.000000 | 1 | 6.061 |
| 0.3290649E 04 | 0.2704555E 04 | 0.4259457E 04 | 39.616 | 19.7CP | 0.699595 | 2 | 12.121 |
| 0.1383656E 04 | 0.4525789E 03 | 0.1455792E 04 | 18.112 | 6.037 | 0.239107 | 3 | 18.182 |
| 0.4C95856E 03 | 0.4687334E 03 | 0.6224717E 03 | 48.853 | 12.213 | 0.102238 | 4 | 24.242 |
| 0.6418506E 03 | C.1033429E 03 | 0.6501167E 03 | 9.147 | 1.829 | 0.106779 | 5 | 30.303 |
| 0.2650974E 03 | 0.1165902E 03 | 0.2896028E 03 | 23.746 | 3.957 | 0.047566 | 6 | 36.364 |
| 0.1028C65E 03 | 0.4292835E 02 | 0.1385820E 03 | 42.111 | 6.C16 | 0.022761 | 7 | 42.424 |
| 0.4888330E 03 | 0.2743364E 03 | 0.5605515E 03 | 29.301 | 3.663 | 0.092068 | 8 | 48.485 |
| 0.2829665E 02 | 0.1887566E 03 | 0.1908658E 03 | 81.474 | 9.053 | 0.031349 | 9 | 54.545 |
| 0.1018589E C3 | 0.1935824F 03 | 0.2187948E 03 | 62.248 | 6.225 | 0.035928 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.95024146 04 | | | | | | | |
| 0.3909404E C4 | -0.8124095E 02 | 0.3910248E 04 | 358.809 | 358.809 | 1.000000 | 1 | 6.061 |
| 0.2375127E 04 | 0.1791327E 04 | 0.2974088E 04 | 37.024 | 18.517 | 0.760798 | 2 | 12.121 |
| 0.1071713E 04 | 0.5903501E 03 | 0.1223953E 04 | 28.848 | 9.616 | 0.312909 | 3 | 18.182 |
| 0.2002579E 03 | 0.2420128E 03 | 0.3141230E 03 | 50.393 | 12.598 | 0.080333 | 4 | 24.242 |
| 0.1445414E 03 | -0.6330783E 02 | 0.1577977E 03 | 336.347 | 67.269 | 0.040355 | 5 | 30.303 |
| 0.1774834E 03 | 0.2540058E 03 | 0.3106079E 03 | 55.152 | 9.192 | 0.079434 | 6 | 36.364 |
| 0.2309633E 03 | 0.2042215E 03 | 0.3083025E 03 | 41.484 | 5.926 | 0.078845 | 7 | 42.424 |
| 0.3635850E 01 | 0.1752594E 03 | 0.1752975E 03 | 88.811 | 11.101 | 0.044830 | 8 | 48.485 |
| -0.1762749E 02 | 0.1434052E 03 | 0.1444845E 03 | 97.008 | 10.778 | 0.036950 | 9 | 54.545 |
| 0.1644116E 02 | 0.2090905E 03 | 0.2097516E 03 | 85.449 | 8.545 | 0.053642 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1130888E 05 | | | | | | | |
| 0.1269833E 04 | -0.1697861E 03 | 0.1281133E 04 | 352.384 | 352.384 | 0.962629 | 1 | 6.061 |
| 0.1220143E 04 | 0.5314727E 03 | 0.1330869E 04 | 23.537 | 11.769 | 1.000000 | 2 | 12.121 |
| 0.4887788E 03 | 0.1060732E 03 | 0.4C06296E 03 | 12.750 | 4.250 | 0.361140 | 3 | 18.182 |
| 0.4095474E C2 | 0.3204349E 02 | 0.5200072E 02 | 38.040 | 9.510 | 0.039073 | 4 | 24.242 |
| -0.1563878E 02 | -0.5936339E 02 | 0.6138878E 02 | 255.241 | 51.C48 | 0.046127 | 5 | 30.303 |
| 0.4321017E 02 | 0.2095128E 02 | 0.4802161E 02 | 25.867 | 4.311 | 0.036083 | 6 | 36.364 |
| 0.1737089E 03 | 0.2734840E 02 | 0.1266957E 03 | 12.466 | 1.781 | 0.095198 | 7 | 42.424 |
| -0.4585811E C3 | 0.1207576E 03 | 0.4742139E 03 | 165.247 | 20.656 | 0.356319 | 8 | 48.485 |
| -0.5245833E 02 | 0.4281282E 02 | 0.6771124E 02 | 140.781 | 15.642 | 0.050877 | 9 | 54.545 |
| -0.3211805E 00 | 0.1698166E 02 | 0.1698468E 02 | 91.084 | 9.108 | 0.012762 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7313637E 04 | | | | | | | |
| 0.2688542E 03 | 0.8327414E 02 | 0.2814553E 03 | 17.210 | 17.210 | 0.654362 | 1 | 6.061 |
| 0.3860967E 03 | 0.1895629E 03 | 0.4301216E 03 | 26.150 | 13.075 | 1.000000 | 2 | 12.121 |
| 0.1905202E 03 | 0.4726030E 02 | 0.1962943E 03 | 13.932 | 4.644 | 0.456369 | 3 | 18.182 |
| -0.1152199E 02 | 0.4089645E 02 | 0.4248851E 02 | 105.734 | 26.434 | 0.098783 | 4 | 24.242 |
| -0.4388317E 01 | 0.9042220E 02 | 0.9052820E 02 | 92.773 | 18.555 | 0.210471 | 5 | 30.303 |
| 0.1451042E 03 | 0.7779431E 02 | 0.1646444E 03 | 28.197 | 4.699 | 0.382736 | 6 | 36.364 |
| 0.9480044E 02 | 0.8361382E 02 | 0.1258098E 03 | 41.652 | 5.95C | 0.292498 | 7 | 42.424 |
| -0.1295635E 03 | 0.1937757E 03 | 0.2331002E 03 | 123.768 | 15.471 | 0.541940 | 8 | 48.485 |
| -0.6310638E 02 | 0.3839778E 02 | 0.7387018E 02 | 148.681 | 16.520 | 0.171742 | 9 | 54.545 |
| 0.1420128E 02 | 0.6113173E 01 | 0.1435541E 02 | 29.734 | 2.974 | 0.038025 | 10 | 60.606 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 21

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.22226286 03 | | | | | | | |
| 0.49242806 02 | 0.1458374E 02 | 0.51356906E 02 | 16.497 | 16.497 | 1.000000 | 1 | 6.061 |
| -0.42627111E 02 | -0.1943733E 02 | 0.46864953E 02 | 204.912 | 102.256 | 0.912233 | 2 | 12.121 |
| 0.30726117E 02 | -0.8136630E 01 | 0.31785923E 02 | 345.168 | 115.056 | 0.618908 | 3 | 18.182 |
| -0.51945836E 01 | 0.4887219E 02 | 0.41200968E 02 | 97.243 | 24.311 | 0.802247 | 4 | 24.242 |
| 0.29161616E 02 | -0.3962450E 02 | 0.46938832E 02 | 302.416 | 60.483 | 0.913742 | 5 | 30.303 |
| 0.97553176 01 | 0.4644156E 00 | 0.97663646E 01 | 2.726 | 0.454 | 0.190126 | 6 | 36.364 |
| 0.24527856E 02 | -0.1330484E 01 | 0.24663768E 02 | 356.987 | 59.987 | 0.480242 | 7 | 42.424 |
| 0.60186226E 01 | 0.2249180E 02 | 0.23244496E 02 | 74.994 | 9.374 | 0.452606 | 8 | 48.485 |
| -0.25219946E 01 | 0.1230145E 02 | 0.12557326E 02 | 101.586 | 11.287 | 0.244510 | 9 | 54.545 |
| -0.82240066E 01 | 0.2610578E 01 | 0.86284056E 01 | 162.389 | 16.239 | 0.168008 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 19 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.11207946 03 | | | | | | | |
| 0.46837626E 02 | 0.3852217E 01 | 0.46995766E 02 | 4.702 | 4.702 | 1.000000 | 1 | 6.061 |
| -0.29865236E 02 | -0.1182460E 02 | 0.32120916E 02 | 201.600 | 100.800 | 0.683485 | 2 | 12.121 |
| -0.67025726E 01 | 0.2514839E 01 | 0.71508826E 01 | 159.434 | 53.145 | 0.152329 | 3 | 18.182 |
| 0.98346956E 01 | 0.4137931E 00 | 9.98439576E 01 | 2.409 | 0.602 | 0.209456 | 4 | 24.242 |
| 0.20091976E 02 | -0.7259690E 01 | 0.22173026E 02 | 340.897 | 68.179 | 0.471989 | 5 | 30.303 |
| -0.83247946E 01 | 0.2816278E 01 | 0.87881906E 01 | 161.318 | 26.885 | 0.187086 | 6 | 36.364 |
| 0.67799186E 01 | -0.3743336E 01 | 0.77446566E 01 | 331.096 | 47.299 | 0.164795 | 7 | 42.424 |
| 0.24952496E 01 | 0.1877668E 02 | 0.11852446E 02 | 77.174 | 9.647 | 0.252179 | 8 | 48.485 |
| -0.12705266E 02 | 0.1060573E 02 | 0.16558066E 02 | 140.147 | 15.572 | 0.352161 | 9 | 54.545 |
| -0.35488056E 01 | -0.1537065E 01 | 0.38675316E 01 | 203.417 | 20.342 | 0.082295 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.46695146E 02 | | | | | | | |
| 0.16490896E 02 | 0.2539096E 02 | 0.30243936E 02 | 57.092 | 57.092 | 1.000000 | 1 | 6.061 |
| 0.83363446E 01 | 0.1037126E 02 | 0.13306266E 02 | 51.208 | 25.604 | 0.439970 | 2 | 12.121 |
| -0.87519126E 01 | 0.1073538E 02 | 0.13850796E 02 | 129.180 | 43.060 | 0.457975 | 3 | 18.182 |
| 0.71799036E 01 | -0.1167698E 02 | 0.13787816E 02 | 301.587 | 75.397 | 0.453268 | 4 | 24.242 |
| -0.35215236E 01 | 0.5768230E 01 | 0.67513956E 01 | 121.440 | 24.288 | 0.223234 | 5 | 30.303 |
| -0.14622506E 01 | 0.1000879E 01 | 0.10183716E 01 | 143.529 | 23.921 | 0.060124 | 6 | 36.364 |
| 0.20847596E 00 | 0.2422667E 01 | 0.24309666E 01 | 85.270 | 12.181 | 0.080380 | 7 | 42.424 |
| 0.79379366E 00 | 0.2288829E 01 | 0.24218146E 01 | 70.867 | 8.858 | 0.080077 | 8 | 48.485 |
| -0.16733696E 01 | 0.2418918E 01 | 0.29410026E 01 | 124.680 | 13.853 | 0.097244 | 9 | 54.545 |
| -0.14491526E 01 | 0.2944018E 01 | 0.29298316E 01 | 119.999 | 11.960 | 0.096742 | 10 | 60.606 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 494 CR 36.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.49272386E 01 | | | | | | | |
| 0.16394766E 01 | -0.6365004E 00 | 0.12188066E 01 | 328.520 | 328.520 | 1.000000 | 1 | 6.061 |
| 0.99013896E-02 | -0.4745359E-01 | 0.48475968E-01 | 281.786 | 140.893 | 0.039771 | 2 | 12.121 |
| 0.13921076E-01 | -0.3111446E-01 | 0.34086926E-01 | 294.184 | 98.035 | 0.027966 | 3 | 18.182 |
| -0.22337866E-01 | -0.1214422E-01 | 0.25425616E-01 | 208.531 | 52.133 | 0.020860 | 4 | 24.242 |
| -0.90131196E-02 | -0.2639169E-01 | 0.26863996E-01 | 259.245 | 51.849 | 0.022040 | 5 | 30.303 |
| -0.38220816E-02 | -0.2001659E-02 | 0.36696416E-02 | 214.965 | 35.760 | 0.003011 | 6 | 36.364 |
| 0.95764776E-02 | -0.1922292E-01 | 0.21476246E-01 | 296.481 | 42.354 | 0.017620 | 7 | 42.424 |
| 0.68359096E-02 | -0.9194096E-02 | 0.11456996E-01 | 306.629 | 38.329 | 0.009399 | 8 | 48.485 |
| -0.34104986E-02 | 0.9754498E-02 | 0.10336166E-01 | 109.313 | 13.664 | 0.008480 | 9 | 54.545 |
| -0.13709286E-01 | -0.1547652E-01 | 0.20675276E-01 | 228.465 | 22.846 | 0.016963 | 10 | 60.606 |

HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 2

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.19736B7E 05 | | | | | | | |
| 0.8323B35E 03 | -0.2795980E 03 | 0.8780773E 03 | 341.436 | 341.436 | 0.309285 | 1 | 5.848 |
| 0.3416041E 03 | -0.2796982E 04 | 0.2819837E 04 | 280.999 | 140.500 | 1.000000 | 2 | 11.696 |
| 0.1104665E 04 | -0.4648164E 03 | 0.1272583E 04 | 338.977 | 112.859 | 0.448245 | 3 | 17.544 |
| -0.2018675E 03 | 0.1401949E 03 | 0.3086992E 03 | 150.301 | 37.620 | 0.109016 | 4 | 23.392 |
| 0.3727899E 03 | -0.6042070E 03 | 0.7099943E 03 | 301.674 | 60.335 | 0.250069 | 5 | 29.240 |
| 0.1035675E 03 | 0.8877679E 02 | 0.2938097E 03 | 29.812 | 4.302 | 0.0716.6 | 6 | 35.088 |
| 0.1034598E 03 | 0.8041634E 02 | 0.1058394E 03 | 28.409 | 4.058 | 0.065459 | 7 | 40.936 |
| -0.1281451E 03 | 0.1102430E 00 | 0.1281451E 03 | 179.951 | 22.494 | 0.045137 | 8 | 46.784 |
| -0.3220405E 02 | 0.2076103E 02 | 0.4317883E 02 | 130.232 | 15.359 | 0.015209 | 9 | 52.632 |
| -0.3946191E 02 | -0.2819856E 02 | 0.4850156E 02 | 215.949 | 21.595 | 0.017204 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.6990647E 03 | | | | | | | |
| 0.6807126E 03 | -0.1424487E 03 | 0.7013313E 03 | 348.281 | 348.281 | 1.000000 | 1 | 5.848 |
| 0.2203403E 02 | -0.6238908E 01 | 0.2290815E 02 | 344.191 | 172.096 | 0.032652 | 2 | 11.696 |
| -0.9444468E 02 | 0.5090851E 02 | 0.1071438E 03 | 151.821 | 50.607 | 0.152772 | 3 | 17.544 |
| 0.6331651E 02 | 0.7884224E 01 | 0.6378108E 02 | 6.920 | 1.730 | 0.090913 | 4 | 23.392 |
| -0.1201604E 03 | 0.3706259E 03 | 0.3896174E 03 | 107.903 | 21.593 | 0.555548 | 5 | 29.240 |
| -0.8409808E 01 | 0.2917361E 00 | 0.8409842E 01 | 179.830 | 29.972 | 0.1210.3 | 6 | 35.088 |
| -0.1229808E 03 | -0.6211572E 02 | 0.1373529E 03 | 206.387 | 29.555 | 0.195646 | 7 | 40.936 |
| 0.5929804E 02 | 0.3197460E 02 | 0.6737027E 02 | 28.334 | 3.542 | 0.096081 | 8 | 46.784 |
| 0.2016701E 02 | 0.1560471E 02 | 0.3222980E 02 | 29.080 | 3.231 | 0.045955 | 9 | 52.632 |
| -0.4946060E 01 | 0.2108429E 02 | 0.2149680E 02 | 102.264 | 10.226 | 0.030651 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1145394E 04 | | | | | | | |
| 0.6736428E 03 | -0.4900947E 03 | 0.8346770E 03 | 324.044 | 324.044 | 1.000000 | 1 | 5.848 |
| -0.1533778E 03 | 0.3277524E 03 | 0.3618645E 03 | 115.078 | 57.539 | 0.433938 | 2 | 11.696 |
| -0.8958314E 02 | 0.4697539E 02 | 0.1010816E 03 | 152.307 | 50.769 | 0.121103 | 3 | 17.544 |
| 0.4304829E 02 | -0.1014433E 02 | 0.4421040E 02 | 346.788 | 86.697 | 0.052987 | 4 | 23.392 |
| -0.6999954E 02 | 0.1671838E 03 | 0.1998442E 03 | 110.504 | 22.101 | 0.239427 | 5 | 29.240 |
| -0.2327394E 02 | 0.7691294E 01 | 0.2443726E 02 | 162.247 | 27.041 | 0.029277 | 6 | 35.088 |
| -0.4574246E 00 | 0.1404685E 02 | 0.1405429E 02 | 91.865 | 13.124 | 0.016858 | 7 | 40.936 |
| -0.7995429E 01 | -0.1044012E 02 | 0.2010620E 02 | 246.568 | 30.821 | 0.024089 | 8 | 46.784 |
| -0.2404408E 02 | -0.1960833E 02 | 0.2704516E 02 | 203.274 | 22.506 | 0.032402 | 9 | 52.632 |
| 0.4397407E 01 | 0.5451571E 01 | 0.7704059E 01 | 51.109 | 5.111 | 0.000391 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1071406E 03 | | | | | | | |
| 0.7833759E 03 | -0.6044805E 03 | 0.1040245E 04 | 318.857 | 318.857 | 1.000000 | 1 | 5.848 |
| -0.2032462E 03 | 0.3715206E 03 | 0.4235247E 03 | 118.693 | 59.347 | 0.407153 | 2 | 11.696 |
| -0.1505430E 03 | 0.1933761E 03 | 0.2487977E 03 | 128.991 | 42.997 | 0.239174 | 3 | 17.544 |
| -0.6585403E 01 | 0.2319080E 02 | 0.2411528E 02 | 105.848 | 26.462 | 0.023183 | 4 | 23.392 |
| 0.1000315E 02 | -0.4570203E 02 | 0.8638022E 02 | 277.185 | 55.437 | 0.083039 | 5 | 29.240 |
| 0.4052454E 02 | 0.1653169E 02 | 0.4376480E 02 | 22.193 | 3.699 | 0.042074 | 6 | 35.088 |
| 0.8939539E 02 | 0.8522990E 02 | 0.1235139E 03 | 43.634 | 6.233 | 0.118737 | 7 | 40.936 |
| -0.9864572E 02 | -0.1798394E 02 | 0.1002537E 03 | 190.276 | 23.784 | 0.096376 | 8 | 46.784 |
| -0.5002807E 02 | 0.1619263E 01 | 0.5005505E 02 | 178.146 | 19.794 | 0.048119 | 9 | 52.632 |
| -0.1170304E 02 | 0.1904253E 02 | 0.2903705E 02 | 120.534 | 12.053 | 0.022146 | 10 | 58.480 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 23

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5447187E 03 | | | | | | | |
| 0.6098464E 03 | -0.6851960E 03 | 0.9172920E 03 | 311.672 | 311.672 | 1.000000 | 1 | 5.848 |
| -0.1287328E 03 | 0.2667668E 03 | 0.2999866E 03 | 115.673 | 57.837 | 0.322688 | 2 | 11.696 |
| -0.8989495E 02 | 0.2486356E 03 | 0.2643889E 03 | 109.879 | 36.626 | 0.288240 | 3 | 17.544 |
| -0.4506851E 02 | 0.9033197E 02 | 0.9432494E 02 | 146.639 | 36.519 | 0.099226 | 4 | 23.392 |
| 0.9888969E 01 | -0.1906228E 03 | 0.1907138E 03 | 271.770 | 54.354 | 0.207919 | 5 | 29.240 |
| 0.1164901E 02 | -0.8349263E 01 | 0.1433212E 02 | 324.369 | 54.062 | 0.015627 | 6 | 35.088 |
| -0.2030208E 02 | -0.1875908E 02 | 0.2764109E 02 | 222.738 | 31.820 | 0.030136 | 7 | 40.936 |
| 0.1895045E 02 | -0.1003902E 02 | 0.2144590E 02 | 332.087 | 41.511 | 0.023380 | 8 | 46.784 |
| -0.7123121E 01 | -0.1225947E 02 | 0.1417517E 02 | 239.834 | 26.648 | 0.015454 | 9 | 52.632 |
| 0.8746685E 00 | -0.6649364E 01 | 0.6706645E 01 | 277.494 | 27.749 | 0.007312 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 11 FL. BEND 15?

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9563870E 03 | | | | | | | |
| 0.3800364E 03 | -0.4999807E 03 | 0.6280193E 03 | 307.239 | 307.239 | 1.000000 | 1 | 5.848 |
| -0.7463636E 02 | 0.1203274E 03 | 0.1414059E 03 | 121.817 | 60.909 | 0.225468 | 2 | 11.696 |
| -0.3676785E 02 | 0.2638818E 03 | 0.2644507E 03 | 97.932 | 32.644 | 0.424240 | 3 | 17.544 |
| -0.7229128E 02 | 0.3187079E 02 | 0.7900422E 02 | 156.[illegible] | 39.052 | 0.125800 | 4 | 23.392 |
| 0.2575737E 02 | -0.2828625E 03 | 0.2840327E 03 | 275.203 | 55.041 | 0.452267 | 5 | 29.240 |
| 0.2024698E 02 | -0.3000383E 02 | 0.3619626E 02 | 304.012 | 50.669 | 0.057636 | 6 | 35.088 |
| -0.7830049E 02 | -0.7213519E 02 | 0.1062429E 03 | 222.703 | 31.823 | 0.169171 | 7 | 40.936 |
| 0.1413469E 03 | 0.1239583E 02 | 0.1418094E 03 | 5.012 | 0.626 | 0.225932 | 8 | 46.784 |
| 0.3303357E 02 | 0.1358409E 02 | 0.3571734E 02 | 22.353 | 2.484 | 0.056873 | 9 | 52.632 |
| 0.1262574E 02 | -0.4050984E 01 | 0.1329978E 02 | 342.211 | 34.221 | 0.021114 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5662878E 03 | | | | | | | |
| 0.1389251E 03 | -0.2854343E 03 | 0.3174475E 03 | 295.953 | 295.953 | 1.000000 | 1 | 5.848 |
| -0.1831281E 02 | -0.6911284E 01 | 0.1943593E 02 | 199.573 | 99.787 | 0.061226 | 2 | 11.696 |
| 0.3333575E 02 | 0.2945609E 03 | 0.2947341E 03 | 82.539 | 27.513 | 0.888745 | 3 | 17.544 |
| -0.1287953E 03 | 0.7721262E 02 | 0.1501667E 03 | 149.057 | 37.264 | 0.473044 | 4 | 23.392 |
| 0.4209714E 02 | -0.2901814E 01 | 0.2939975E 03 | 280.362 | 56.072 | 0.737122 | 5 | 29.240 |
| 0.2968187E 02 | -0.3795987E 02 | 0.4818677E 02 | 308.023 | 51.337 | 0.151794 | 6 | 35.088 |
| -0.9912683E 02 | -0.9192884E 02 | 0.1351926E 03 | 222.842 | 31.835 | 0.425874 | 7 | 40.936 |
| 0.1522910E 03 | 0.1351676E 02 | 0.1528897E 03 | 5.072 | 0.634 | 0.481622 | 8 | 46.784 |
| 0.6461137E 02 | -0.8669927E 01 | 0.6518993E 02 | 352.361 | 39.151 | 0.205397 | 9 | 52.632 |
| 0.1891[illegible]4E 02 | 0.4847870E 01 | 0.1952922E 02 | 14.373 | 1.437 | 0.061520 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2404183E 03 | | | | | | | |
| -0.5911821E 02 | -0.5100931 02 | 0.7808270E 02 | 220.789 | 220.789 | 0.357738 | 1 | 5.848 |
| -0.2094742E 02 | -0.[illegible]4907E 02 | 0.4440581E 02 | 242.437 | 121.219 | 0.203446 | 2 | 11.696 |
| 0.9342704E 02 | 0.1972617E 03 | 0.2182681E 03 | 64.657 | 21.552 | 1.000000 | 3 | 17.544 |
| -0.9291846E 02 | 0.7[illegible]95129E 02 | 0.1209010E 03 | 140.224 | 35.056 | 0.553911 | 4 | 23.392 |
| -0.7656650E 01 | -0.[illegible]5091P0E 03 | 0.1511120E 03 | 267.095 | 53.419 | 0.692323 | 5 | 29.240 |
| 0.4986156E 02 | -0.4043857E 02 | 0.6813747E 02 | 317.636 | 52.827 | 0.312173 | 6 | 35.088 |
| -0.6826295E 02 | -0.9478133E 02 | 0.8792611E 02 | 218.747 | 31.250 | 0.402803 | 7 | 40.936 |
| 0.1995521E 03 | -0.9168540E 01 | 0.1963358E 03 | 358.145 | 44.768 | 0.731375 | 8 | 46.784 |
| 0.5033467E 0[illegible] | -0.1341584E 02 | 0.5209189E 02 | 345.076 | 38.342 | 0.238666 | 9 | 52.632 |
| 0.3145459E 02 | 0.1484306E 02 | 0.3478004E 02 | 25.262 | 2.926 | 0.159349 | 10 | 58.480 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. [illegible]

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.8218173E 04 | | | | | | | |
| 0.7227242E 04 | 0.2421240E 05 | 0.2526603E 05 | 73.380 | 73.380 | 1.000000 | 1 | 5.848 |
| -0.3791917E 04 | 0.3195873E 04 | 0.4928559E 04 | 139.576 | 69.788 | 0.195050 | 2 | 11.696 |
| -0.3920491E 03 | -0.5165542E 03 | 8.6484954E 03 | 232.801 | 77.600 | 0.029665 | 3 | 17.544 |
| -0.1415172E 03 | 0.6946510E 02 | 0.1576469E 03 | 153.855 | 38.464 | 0.006239 | 4 | 23.392 |
| 0.4726641E 03 | -0.5619284E 02 | 0.4757609E 03 | 353.459 | 70.692 | 0.018829 | 5 | 29.240 |
| -0.5118283E 02 | -0.6788477E 02 | 0.8501176E 02 | 232.985 | 38.831 | 0.003365 | 6 | 35.088 |
| -0.1307668E 03 | -0.1788487E 03 | 0.2215555E 03 | 233.827 | 31.404 | 0.008768 | 7 | 40.936 |
| -0.7909639E 02 | 0.4036045E 03 | 0.4112812E 03 | 101.088 | 1..636 | 0.016277 | 8 | 46.784 |
| -0.6200412E 02 | 0.1692339E 02 | 0.6427216E 02 | 164.734 | 18.304 | 0.002544 | 9 | 52.632 |
| 0.2291222E 02 | 0.7381042E 02 | 0.7728482E 02 | 72.755 | 8.275 | 0.003059 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.7459033E 04 | | | | | | | |
| 0.3843137E 04 | 0.1487866E 05 | 0.1536699E 05 | 75.517 | 75.517 | 1.000000 | 1 | 5.848 |
| -0.2338213E 04 | 0.2368035E 04 | 0.3322199E 04 | 134.734 | 67.367 | 0.216191 | 2 | 11.696 |
| 0.2646321E 02 | -0.1534938E 02 | 0.3060260E 02 | 329.853 | 109.951 | 0.001991 | 3 | 17.544 |
| 0.4138335E 02 | 0.2256073E 03 | 0.2293714E 03 | 79.606 | 19.901 | 0.014926 | 4 | 23.392 |
| 0.4633365E 02 | -0.1344211E 03 | 0.1421824E 03 | 289.019 | 57.804 | 0.009252 | 5 | 29.240 |
| -0.3020410E 02 | -0.1322011E 03 | 0.1356856E 03 | 257.138 | 42.856 | 0.008830 | 6 | 35.088 |
| 0.8735785E 02 | 0.4098773E 02 | 0.1001598E 03 | 29.282 | 4.183 | 0.006518 | 7 | 40.936 |
| 0.1208877E 03 | -0.3496896E 02 | 0.1259439E 03 | 343.866 | 42.983 | 0.008189 | 8 | 46.784 |
| 0.7787407E 02 | 0.1681651E 02 | 0.8613837E 02 | 25.383 | 2.811 | 0.005605 | 9 | 52.632 |
| 0.1180729E 02 | -0.9406938E 00 | 0.1184645E 02 | 355.328 | 39.533 | 0.000771 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 501 CTR 346 CR 42.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1015685E 05 | | | | | | | |
| 0.1370976E 04 | 0.5782863E 04 | 0.5943152E 04 | 76.863 | 76.363 | 1.000000 | 1 | 5.848 |
| -0.4227659E 03 | 0.1103187E 04 | 0.1266830E 04 | 119.445 | 59.723 | 0.213158 | 2 | 11.696 |
| 0.7536848E 02 | 0.8008972E 01 | 0.7579279E 02 | 6.066 | 2.022 | 0.012753 | 3 | 17.544 |
| 0.1622132E 03 | 0.2161051E 03 | 0.2782119E 03 | 53.107 | 13.277 | 0.046846 | 4 | 23.392 |
| -0.9967903E 02 | -0.3092822E 02 | 3.1043669E 03 | 197.238 | 39.448 | 0.017541 | 5 | 29.240 |
| 0.1933530E 03 | -0.2645409E 03 | 0.2849084E 03 | 334.617 | 52.353 | 0.047939 | 6 | 35.088 |
| 0.5569421E 03 | -0.7418977E 02 | 0.5123428E 03 | 351.674 | 50.239 | 0.086207 | 7 | 40.936 |
| -0.3027917E 02 | -0.4087363E 03 | 9.4098562E 03 | 269.763 | 33.220 | 0.068963 | 8 | 46.784 |
| 0.4707866E 02 | -0.1794719E 03 | 0.1855440E 03 | 284.698 | 31.633 | 0.031220 | 9 | 52.632 |
| -0.8830843E 02 | -0.2406813E 02 | 0.9152950E 02 | 195.245 | 19.525 | 0.015401 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 501 CTR 346 [illegible] 2.0 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5207910E 04 | | | | | | | |
| 0.4488381E 03 | 0.1973734E 04 | 0.2028654E 04 | 76.638 | 76.638 | 1.000000 | 1 | 5.848 |
| -0.2022693E 03 | 0.3[illegible]58232E 03 | 0.4006376E 03 | 120.323 | 60.162 | 0.197487 | 2 | 11.696 |
| 0.8983745E 02 | 0.25[illegible]3044E 02 | 0.9325923E 02 | 15..69 | 5.190 | 0.045971 | 3 | 17.544 |
| 0.8189311E 02 | 0.130[illegible]272E 03 | 0.1340956E 03 | 57.876 | 14.469 | 0.079915 | 4 | 23.392 |
| -0.7572292E 01 | -0.6992[illegible]4E 01 | 0.1003990E 02 | 221.043 | 44.209 | 0.004949 | 5 | 29.240 |
| 0.1736352E 03 | -0.3889734E 02 | 0.1779387E 03 | 347.373 | 57.896 | 0.087713 | 6 | 35.088 |
| 0.2839492E 03 | -0.2189055E 02 | 0.2847913E 03 | 355.592 | 50.799 | 0.140384 | 7 | 40.936 |
| -0.6958929E 02 | -0.2620742E 03 | 0.2711558E 03 | 255.129 | 31.891 | 0.133643 | 8 | 46.784 |
| 0.8236953E 02 | -0.6639441E 02 | 0.1057592E 03 | 321.159 | 35.684 | 0.052133 | 9 | 52.632 |
| -0.6762169E 02 | 0.9045380E 02 | 0.8434984E 02 | 143.273 | 14.327 | 0.041589 | 10 | 58.480 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS --- TEST CONDITION NO. 23

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 501 CTR 346 CR 42.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 3.2420227E 03 | | | | | | | |
| 0.8473291E 02 | 0.5993959E 01 | 0.8491736E 02 | 3.777 | 3.777 | 0.864176 | 1 | 5.060 |
| -0.2991791E 02 | 0.7081607E 02 | 0.7699029E 02 | 112.990 | 56.495 | 0.779595 | 2 | 11.090 |
| -0.9304005E 02 | -0.1008406E 02 | 0.9440866E 02 | 186.126 | 62.042 | 0.961501 | 3 | 17.544 |
| 0.3617307E 02 | 0.1004628E 02 | 0.9020955E 02 | 10.657 | 4.664 | 0.603360 | 4 | 23.392 |
| 0.8533709E 02 | -0.7334328E 02 | 0.9826309E 02 | 311.704 | 62.341 | 1.000000 | 5 | 29.240 |
| 0.3226449E 02 | 0.1433291E 02 | 0.3530914E 02 | 23.949 | 3.992 | 0.399332 | 6 | 35.088 |
| 0.2221220E 02 | 0.2919785E 01 | 0.2240327E 02 | 7.489 | 1.070 | 0.227991 | 7 | 40.936 |
| 0.4825743E 01 | -0.6059624E 01 | 0.7744407E 01 | 308.533 | 38.567 | 0.078833 | 8 | 46.784 |
| -0.1310730E 01 | -0.6781263E 01 | 0.6908774E 01 | 259.080 | 28.784 | 0.070280 | 9 | 52.632 |
| 0.9776136E 01 | 0.1177971E 02 | 0.1530790E 02 | 50.310 | 5.031 | 0.155784 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 501 CTR 346 CR 42.0 TR 15 TORSION 105

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2346917E 03 | | | | | | | |
| 0.4728999E 02 | 0.7184362E 02 | 0.8599027E 02 | 56.667 | 56.667 | 1.000000 | 1 | 5.060 |
| -0.2057208E 02 | 0.1433509E 02 | 0.2491809E 02 | 144.871 | 72.435 | 0.289688 | 2 | 11.090 |
| -0.3609080E 02 | 0.2999944E 01 | 0.3697890E 02 | 170.837 | 56.279 | 0.430041 | 3 | 17.544 |
| 0.1908442E 02 | 0.8396834E-01 | 0.1908463E 02 | 0.251 | 0.063 | 0.221980 | 4 | 23.392 |
| 0.3818787E 02 | -0.2812967E 02 | 0.4742673E 02 | 323.620 | 64.724 | 0.551942 | 5 | 29.240 |
| 0.1883942E 02 | 0.6446919E 01 | 0.1911644E 02 | 48.858 | 6.682 | 0.152535 | 6 | 35.088 |
| -0.2481444E 01 | 2.1829811E 01 | 0.2612863E 01 | 156.793 | 22.399 | 0.030386 | 7 | 40.936 |
| 0.9233233E 01 | -0.1918640E 01 | 0.9430473E 01 | 348.261 | 43.533 | 0.109870 | 8 | 46.784 |
| -0.1147871E 01 | -0.5344528E 01 | 0.5466349E 01 | 257.870 | 28.653 | 0.069571 | 9 | 52.632 |
| 0.3419190E 00 | 0.7189826E 01 | 0.7194859E 01 | 87.276 | 8.728 | 0.083642 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 501 CTR 346 CR 42.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2779394E 02 | | | | | | | |
| -0.1008609E 02 | 0.4994108E 02 | 0.5837737E 02 | 101.527 | 101.527 | 1.000000 | 1 | 5.060 |
| -0.6379914E 01 | -0.6414018E 01 | 0.9047270E 01 | 225.196 | 112.598 | 0.179588 | 2 | 11.090 |
| 0.2975204E 02 | 0.8099903E 01 | 0.3104285E 02 | 16.576 | 5.525 | 0.416288 | 3 | 17.54 |
| -0.1903598E 02 | -0.1187959E 02 | 0.2277859E 02 | 211.434 | 52.859 | 0.442195 | 4 | 23.392 |
| -0.1008608E 02 | 0.9256994E 01 | 0.1190959E 02 | 153.887 | 38.761 | 0.230405 | 5 | 29.240 |
| -0.2916918E 01 | 0.1331862E 00 | 0.2920349E 01 | 176.785 | 29.451 | 0.046899 | 6 | 35.088 |
| -0.1073181E 01 | -0.3440879E 00 | 0.1126892E 01 | 197.774 | 28.253 | 0.022369 | 7 | 40.936 |
| 0.1429340E 01 | 0.9871329E 00 | 0.1692084E 01 | 32.401 | 4.630 | 0.033604 | 8 | 46.784 |
| 0.3267414E 01 | -0.2917257E 00 | 0.3277866E 01 | 355.394 | 39.910 | 0.063850 | 9 | 52.632 |
| 0.8260951E 00 | 0.1021737E 01 | 0.1034420E 01 | 51.016 | 5.102 | 0.020491 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 501 CTR 346 CR 42.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3614136E 01 | | | | | | | |
| 0.1208353E 01 | -0.1091117E 01 | 0.2129965E 01 | 307.301 | 307.301 | 1.000000 | 1 | 5.060 |
| -0.7811941E-02 | 0.5118142E-01 | 0.5169584E-01 | 98.492 | 49.246 | 0.024316 | 2 | 11.090 |
| -0.5384156E-01 | 0.1817719E-01 | 0.5945365E-01 | 163.039 | 54.346 | 0.026004 | 3 | 17.544 |
| 0.5230053E-01 | 0.9992613E-01 | 0.6579044E-01 | 37.358 | 9.340 | 0.030888 | 4 | 23.392 |
| -0.1414511E-02 | 0.7833578E-02 | 0.7963524E-02 | 100.498 | 20.100 | 0.003652 | 5 | 29.240 |
| -0.4093237E-02 | -0.1376597E-01 | 0.1434443E-01 | 250.602 | 41.767 | 0.006605 | 6 | 35.088 |
| -0.4284209E-02 | -0.1879268E-02 | 0.4400160E-02 | 203.674 | 29.096 | 0.002201 | 7 | 40.936 |
| 0.1941770E-01 | 0.1441481E-01 | 0.2260091E-01 | 39.611 | 4.951 | 0.010619 | 8 | 46.784 |
| 0.2264097E-02 | 0.2132082E-01 | 0.2143998E-01 | 83.936 | 9.326 | 0.010065 | 9 | 52.632 |
| -0.1977205E-02 | 0.1120082E-01 | 0.1138187E-01 | 100.064 | 10.000 | 0.005354 | 10 | 58.480 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 25

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 496 CTR 184 CR 22.1 TR 2 FLAP BEND S

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.20691446E 05 | | | | | | | |
| 0.22641206E 04 | 0.26C8991E 04 | 0.3494478E 04 | 49.048 | 49.048 | 0.616853 | 1 | 5.917 |
| 0.46166000E 03 | -0.9989466E 04 | 0.9888042E 04 | 274.112 | 137.056 | 1.CCCCCC | 2 | 11.834 |
| 0.23267325E 04 | 0.31966196E 03 | 0.2348091E 04 | 7.824 | 2.608 | 0.419296 | 3 | 17.751 |
| -0.42041404E 03 | 0.23935246E 03 | 0.48377186E 03 | 150.346 | 37.586 | 0.086386 | 4 | 23.669 |
| 0.65321136E 03 | -0.24705461E 02 | 0.65386004E 03 | 357.854 | 71.567 | 0.116727 | 5 | 29.586 |
| -0.22067836E 03 | -0.94695965E 02 | 0.23999804E 03 | 203.298 | 33.877 | 0.042044 | 6 | 35.503 |
| 0.19187388E 03 | -0.47983818E 02 | 0.1967092E 03 | 346.157 | 49.451 | 0.035148 | 7 | 41.420 |
| -0.73518225E 02 | 0.66883495E 02 | 0.99389974E 02 | 137.706 | 17.213 | 0.017768 | 8 | 47.337 |
| -0.13773335E 02 | 0.12818435E 03 | 0.12897186E 03 | 96.538 | 10.726 | 0.021662 | 9 | 53.254 |
| 0.37889546E 01 | 0.47459906E 02 | 0.47618096E 02 | 85.435 | 8.544 | 0.CC8502 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 496 CTR 184 CR 22.1 TR 4 FLAPWISE 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.64981236E 03 | | | | | | | |
| 0.10983186E 04 | 0.30414206E 03 | 0.1161663E 04 | 19.318 | 19.318 | 1.CCCCCC | 1 | 5.917 |
| -0.11051795E 03 | -0.1232333E 03 | 0.16553146E 03 | 228.114 | 114.057 | 0.142495 | 2 | 11.834 |
| -0.77057106E 02 | -0.92384457E 01 | 0.78280666E 02 | 186.784 | 62.261 | 0.067521 | 3 | 17.751 |
| 0.25882906E 03 | 0.12220942E 03 | 0.29958071E 03 | 25.343 | 6.336 | 0.245775 | 4 | 23.669 |
| -0.13780618E 03 | 0.52127772E 02 | 0.14662804E 03 | 159.174 | 31.835 | 0.126216 | 5 | 29.586 |
| 0.13866178E 03 | 0.78169578E 02 | 0.15915636E 03 | 29.414 | 4.902 | 0.137089 | 6 | 35.503 |
| -0.21386625E 03 | 0.10866526E 03 | 0.23971396E 03 | 153.626 | 21.947 | 0.209409 | 7 | 41.420 |
| 0.92110277E 02 | -0.8939794E 01 | 0.92944636E 02 | 354.829 | 44.354 | 0.079823 | 8 | 47.337 |
| -0.29481746E 02 | -0.56988811E 02 | 0.62418977E 02 | 245.516 | 27.280 | 0.053988 | 9 | 53.254 |
| -0.64784126E 02 | -0.34688049E 02 | 0.73444086E 02 | 208.108 | 20.811 | 0.063225 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 496 CTR 184 CR 22.1 TR 6 FLAPWISE 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.229[illegible]03E 03 | | | | | | | |
| 0.10111008E 04 | -0.98290008E 03 | 0.11293937E 04 | 333.557 | 333.557 | 1.CCCCCC | 1 | 5.917 |
| -0.19969382E 03 | 0.99629044E 01 | 0.42797308E 03 | 188.166 | 94.083 | 0.999700 | 2 | 11.834 |
| -0.24699822E 03 | -0.1995[illegible]7E 02 | 0.26773911E 03 | 184.278 | 61.423 | 0.237073 | 3 | 17.751 |
| 0.91981459E 02 | 0.64433118E 02 | 0.11238041E 03 | 35.011 | 8.753 | 0.099642 | 4 | 23.669 |
| -0.10286328E 03 | 0.66700028E 02 | 0.12259481E 03 | 147.039 | 29.408 | 0.108594 | 5 | 29.586 |
| 0.44056138E 01 | 0.53648248E 02 | 0.53853159E 02 | 85.051 | 14.175 | 0.047686 | 6 | 35.503 |
| 0.74589597E 01 | 0.46869997E 02 | 0.47297328E 02 | 80.918 | 11.546 | 0.041891 | 7 | 41.420 |
| -0.16996195E 02 | 0.34745295E 02 | 0.38679047E 02 | 116.004 | 16.572 | 0.034258 | 8 | 47.337 |
| -0.29741706E 01 | 0.12936118E 02 | 0.13273618E 02 | 102.944 | 11.439 | 0.011753 | 9 | 53.254 |
| 0.16432778E 02 | 0.[illegible]1148166E 02 | 0.63317728E 02 | 74.998 | 7.498 | 0.056044 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 496 CTR 184 CR 22.1 TR 7 PLA[illegible]WISE 113

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.64410218E 03 | | | | | | | |
| 0.11089048E 04 | -0.91290838E 03 | 0.14790888E 04 | 320.334 | 320.334 | 1.CCCCCC | 1 | 5.917 |
| -0.83190868E 02 | 0.69384148E 03 | 0.69928789E 03 | 96.842 | 48.421 | 0.488498 | 2 | 11.834 |
| -0.28198878E 03 | 0.13781358E 03 | 0.2449888E 03 | 345.981 | 48.668 | 0.171297 | 3 | 17.751 |
| -0.34382586E 01 | -0.67244614E 02 | 0.67331995E 02 | 267.073 | 66.768 | 0.047697 | 4 | 23.669 |
| -0.57838888E 01 | 0.28727446E 01 | 0.47582888E 01 | 142.788 | 28.558 | 0.003323 | 5 | 29.586 |
| -0.87710988E 02 | -0.90473779E 02 | 0.10541579E 03 | 213.698 | 35.615 | 0.073753 | 6 | 35.503 |
| 0.99984698E 02 | -0.11884698E 03 | 0.14988466E 03 | 312.886 | 44.684 | 0.104278 | 7 | 41.420 |
| -0.52489288E 02 | -0.10882698E 02 | 0.33433378E 02 | 198.789 | 23.849 | 0.047374 | 8 | 47.337 |
| -0.17789898E 02 | 0.47982826E 01 | 0.18428188E 02 | 164.921 | 16.325 | 0.012884 | 9 | 53.254 |
| 0.57195778E 01 | -0.77882216E 01 | 0.98629178E 01 | 308.291 | 30.829 | 0.006758 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 25

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 10 FLAPWISE 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.00035166 03 | | | | | | | |
| 0.02503296 03 | -0.89599106 03 | 0.12189916 04 | 312.678 | 312.678 | 1.000000 | 1 | 5.917 |
| 0.25909146 01 | 0.42037046 03 | 0.42037826 03 | 89.652 | 44.826 | 0.351536 | 2 | 11.834 |
| -0.11620196 03 | 0.35479016 03 | 0.37319476 03 | 108.195 | 36.065 | 0.306373 | 3 | 17.751 |
| -0.11043976 03 | -0.59116416 02 | 0.12343816 03 | 206.523 | 51.631 | 0.101289 | 4 | 23.669 |
| 0.49166026 02 | -0.79362186 02 | 0.89988856 02 | 303.119 | 60.624 | 0.073840 | 5 | 29.586 |
| -0.19909566 01 | -0.32952516 02 | 0.34011296 02 | 266.630 | 44.438 | 0.027916 | 6 | 35.503 |
| -0.42096126 02 | -0.50621376 02 | 0.65812136 02 | 230.208 | 32.887 | 5.05E-007 | 7 | 41.420 |
| 0.30023606 02 | -0.46978676 02 | 0.60944026 02 | 309.571 | 38.696 | 0.054813 | 8 | 47.337 |
| 0.78809716 01 | 0.12776706 01 | 0.79804096 01 | 9.302 | 1.034 | 0.006487 | 9 | 53.254 |
| -0.11440156 02 | -0.49246736 02 | 0.50559066 02 | 256.913 | 25.691 | 0.041490 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 11 FLAPWISE 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.12183396 04 | | | | | | | |
| 0.49310656 03 | -0.66566206 03 | 0.81003996 03 | 304.832 | 304.832 | 1.000000 | 1 | 5.917 |
| 0.38779816 02 | 0.19410786 03 | 0.19794256 03 | 78.696 | 39.348 | 0.244696 | 2 | 11.834 |
| 0.88042946 02 | 0.44461136 03 | 0.45342026 03 | 78.687 | 26.229 | 0.559129 | 3 | 17.751 |
| -0.17012466 03 | 0.13644956 03 | 0.21811136 03 | 141.259 | 35.315 | 0.268964 | 4 | 23.669 |
| -0.21474206 00 | -0.12138456 03 | 0.12138476 03 | 269.898 | 53.980 | 0.149684 | 5 | 29.586 |
| 0.78274296 02 | -0.37573196 02 | 0.86825126 02 | 334.358 | 55.726 | 0.107067 | 6 | 35.503 |
| -0.10889196 03 | 0.75925066 02 | 0.12363196 03 | 142.818 | 20.403 | 0.152521 | 7 | 41.420 |
| 0.67352976 02 | -0.14210416 02 | 0.68839716 02 | 348.086 | 43.511 | 0.084884 | 8 | 47.337 |
| 0.13810366 02 | -0.28097786 02 | 0.32028236 02 | 295.543 | 32.838 | 0.039495 | 9 | 53.254 |
| -0.11609566 00 | -0.11960126 02 | 0.11960666 02 | 269.444 | 26.944 | 0.014706 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 13 FLAPWISE 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.74912306 03 | | | | | | | |
| 0.14090486 03 | -0.39986626 03 | 0.42396636 03 | 289.412 | 289.412 | 0.873936 | 1 | 5.917 |
| 0.38382436 02 | -0.37957136 02 | 0.53983566 02 | 315.736 | 157.868 | 0.110241 | 2 | 11.834 |
| 0.23978926 03 | 0.42196266 01 | 0.48533486 03 | 60.302 | 20.131 | 1.000000 | 3 | 17.751 |
| -0.19879816 03 | 0.16246596 03 | 0.25670926 03 | 140.737 | 35.184 | 0.529033 | 4 | 23.669 |
| -0.41959966 02 | -0.12112326 03 | 0.12816396 03 | 250.894 | 50.179 | 0.264115 | 5 | 29.586 |
| 0.81527186 02 | -0.60194386 02 | 0.10134126 03 | 323.560 | 53.927 | 0.208807 | 6 | 35.503 |
| -0.12096866 03 | 0.13764696 01 | 0.17947686 03 | 132.348 | 18.907 | 0.369801 | 7 | 41.420 |
| 0.26178346 02 | 0.44639976 02 | 0.51729466 02 | 59.649 | 7.456 | 0.106583 | 8 | 47.337 |
| 0.15081676 01 | 0.73046946 01 | 0.74753496 01 | 77.734 | 8.637 | 0.015402 | 9 | 53.254 |
| 0.89747486 01 | 0.16253026 02 | 0.16564276 02 | 61.093 | 6.109 | 0.034135 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 14 FLAPWISE 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.39991606 03 | | | | | | | |
| -0.79937656 02 | -0.12888296 03 | 0.14959096 03 | 239.493 | 239.493 | 0.338960 | 1 | 5.917 |
| 0.15625426 02 | -0.14288506 03 | 0.14373776 03 | 276.241 | 138.120 | 0.325705 | 2 | 11.834 |
| 0.31225206 03 | 0.31559036 01 | 0.44392026 03 | 45.301 | 15.100 | 1.000000 | 3 | 17.751 |
| -0.11522646 03 | 0.20205466 03 | 0.23260006 03 | 119.695 | 29.924 | 0.529059 | 4 | 23.669 |
| -0.94760426 02 | -0.72535316 02 | 0.90872866 02 | 232.959 | 46.592 | 0.206701 | 5 | 29.586 |
| 0.81145826 02 | -0.64218506 02 | 0.10348206 03 | 321.642 | 53.607 | 0.233105 | 6 | 35.563 |
| -0.94262236 02 | 0.13866506 03 | 0.14768236 03 | 124.213 | 17.745 | 0.377723 | 7 | 41.420 |
| 0.12546076 02 | 0.56669256 02 | 0.58046316 02 | 77.521 | 9.690 | 0.132742 | 8 | 47.337 |
| -0.29098216 02 | -0.97888046 00 | 0.29114626 02 | 181.925 | 20.214 | 0.069904 | 9 | 53.254 |
| -0.35336906 01 | -0.48687476 01 | 0.68199536 01 | 234.630 | 23.463 | 0.013952 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 25

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 1 CHORD BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.63626911E 04 | | | | | | | |
| 0.94366049E 03 | 0.29032180E 05 | 0.29037644E 05 | 88.888 | 88.888 | 1.000000 | 1 | 5.917 |
| -0.37071638E 04 | 0.97937677E 03 | 0.38111740E 04 | 165.501 | 82.750 | 0.134713 | 2 | 11.834 |
| -0.39747773E 03 | -0.75528356E 03 | 0.85341178E 03 | 242.241 | 80.747 | 0.029390 | 3 | 17.751 |
| -0.47318138E 02 | 0.10900746E 03 | 0.11956008E 03 | 113.315 | 28.328 | 0.004118 | 4 | 23.669 |
| -0.51097308E 02 | 0.57181095E 02 | 0.57329208E 03 | 95.114 | 19.023 | 0.019763 | 5 | 29.583 |
| 0.91362638E 02 | 0.14066708E 03 | 0.17279566E 03 | 90.000 | 0.000 | 0.005951 | 6 | 35.503 |
| -0.20915238E 03 | -0.40426444E 01 | 0.20919114E 03 | 181.107 | 25.072 | 0.007204 | 7 | 41.420 |
| -0.70756278E 02 | 0.17929087E 03 | 0.19277475E 03 | 111.536 | 13.942 | 0.006638 | 8 | 47.337 |
| 0.71054178E 02 | -0.34749975E 03 | 0.35469364E 03 | 281.557 | 31.284 | 0.012213 | 9 | 53.254 |
| 0.79377829E 03 | 0.89004179E 01 | 0.28392446E 03 | 1.814 | 0.181 | 0.009778 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 5 CHORD 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.13883798E 05 | | | | | | | |
| -0.32968439E 03 | 0.17717946E 05 | 0.17720952E 05 | 91.066 | 91.066 | 1.000000 | 1 | 5.917 |
| -0.20339951E 04 | 0.76469984E 03 | 0.21720311E 04 | 159.397 | 79.698 | 0.122622 | 2 | 11.834 |
| 0.14361682E 03 | 0.30933799E 03 | 0.33734088E 03 | 64.782 | 21.594 | 0.019049 | 3 | 17.751 |
| 0.24816595E 03 | 0.45232708E 03 | 0.51238093E 03 | 62.044 | 15.511 | 0.028911 | 4 | 23.669 |
| 0.17497908E 03 | 0.73454944E 02 | 0.18984955E 03 | 22.828 | 4.566 | 0.010713 | 5 | 29.586 |
| -0.94433111E 03 | -0.93996731E 02 | 0.35746119E 03 | 195.578 | 32.596 | 0.020172 | 6 | 35.503 |
| 0.19329047E 03 | -0.51122108E 02 | 0.19994108E 03 | 345.186 | 49.312 | 0.011283 | 7 | 41.420 |
| -0.2677787 E 02 | -0.70594915E 02 | 0.75464453E 02 | 249.214 | 31.152 | 0.004258 | 8 | 47.337 |
| 0.30707704E 02 | 0.66000443E 02 | 0.77217724E 02 | 59.041 | 6.560 | 0.004361 | 9 | 53.254 |
| 0.20875215E 02 | -0.38074044E 01 | 0.21090713E 02 | 351.002 | 35.100 | 0.004190 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 8 CHORD 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.10334414E 05 | | | | | | | |
| 0.42852808E 03 | 0.72610847E 04 | 0.72734028E 04 | 80.660 | 80.660 | 1.000000 | 1 | 5.917 |
| 0.91313035E 02 | 0.82416508E 03 | 0.82920837E 03 | 83.678 | 41.839 | 0.114004 | 2 | 11.834 |
| 0.47746412E 03 | 0.79822366E 03 | 0.93012359E 03 | 99.114 | 16.765 | 0.127878 | 3 | 17.751 |
| 0.40310108E 03 | 0.44979823E 03 | 0.10779084E 04 | 63.373 | 15.843 | 0.148196 | 4 | 23.669 |
| 0.91451208E 02 | 0.44146842E 03 | 0.44446446E 03 | 83.660 | 16.728 | 0.061057 | 5 | 29.586 |
| -0.32934137E 03 | 0.29710259E 03 | 0.44098884E 03 | 137.908 | 22.651 | 0.060973 | 6 | 35.503 |
| 0.12387964E 03 | 0.18981709E 03 | 0.20099186E 03 | 59.384 | 9.619 | 0.039724 | 7 | 41.420 |
| 0.98220897E 01 | 0.10457944E 03 | 0.10980347E 03 | 84.634 | 10.579 | 0.014441 | 8 | 47.337 |
| 0.18208317E 03 | 0.50641758E 03 | 0.51074068E 03 | 70.525 | 8.725 | 0.071845 | 9 | 53.254 |
| -0.40887088E 02 | 0.79331777E 03 | 0.29738035E 03 | 101.371 | 10.137 | 0.000513 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 184 CR 22.1 TR 12 CHORD 197

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.71120444E 04 | | | | | | | |
| -0.30012358E 03 | 0.24387138E 04 | 0.24491068E 04 | 97.039 | 97.039 | 1.000000 | 1 | 5.917 |
| -0.24091038E 03 | 0.45687138E 00 | 0.24091107E 03 | 179.892 | 89.946 | 0.098363 | 2 | 11.834 |
| 0.82099308E 02 | -0.82298228E 01 | 0.82491098E 02 | 354.272 | 118.091 | 0.033669 | 3 | 17.751 |
| 0.18735144E 03 | 0.70000011E 02 | 0.20083239E 03 | 20.511 | 5.128 | 0.081673 | 4 | 23.669 |
| 0.30190428E 02 | -0.81181078E 02 | 0.86539044E 02 | 290.421 | 58.084 | 0.035334 | 5 | 29.586 |
| -0.26409308E 03 | -0.60285138E 02 | 0.27108118E 03 | 192.944 | 32.157 | 0.110976 | 6 | 35.503 |
| 0.87360808E 02 | -0.60900439E 02 | 0.11131191E 03 | 321.709 | 45.958 | 0.045450 | 7 | 41.420 |
| -0.30982308E 02 | -0.51063908E 02 | 0.59806708E 02 | 236.803 | 29.850 | 0.024374 | 8 | 47.337 |
| 0.39110044E 03 | 0.18741338E 01 | 0.19145232E 03 | 78.218 | 8.690 | 0.078869 | 9 | 53.254 |
| -0.11290881E 03 | 0.66495338E 02 | 0.13111828E 03 | 149.523 | 14.952 | 0.053529 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 25

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 184 CR 22.1 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1A966306E 03 | | | | | | | |
| 0.19134444E 03 | -0.16017979E 03 | 0.22714444E 03 | 311.781 | 311.781 | 1.000000 | 1 | 9.917 |
| -0.53587044E 02 | 0.14357448E 03 | 0.15488097E 03 | 110.241 | 99.129 | 0.681988 | 2 | 11.834 |
| -0.16487359E 03 | -0.7877 .19E 02 | 0.18197898E 03 | 205.630 | 60.943 | 0.801166 | 3 | 17.751 |
| 0.93571408E 02 | 0.6348068E 02 | 0.83171346E 02 | 49.901 | 12.415 | 0.366161 | 4 | 23.669 |
| 0.99482256E 02 | -0.66717779E 01 | 0.99955248E 02 | 353.680 | 70.726 | 0.263512 | 5 | 29.586 |
| 0.12437586E 02 | 0.24589994E 02 | 0.27536444E 02 | 63.179 | 10.526 | 0.121317 | 6 | 35.503 |
| 0.5[illegible]E 02 | -0.8863944E 01 | 0.52091594E 02 | 351.231 | 58.176 | 0.232854 | 7 | 41.420 |
| -0.3309[illegible]E 02 | 0.39249581E 02 | 0.51368832E 02 | 130.183 | 14.269 | 0.225884 | 8 | 47.337 |
| 0.34716499E 02 | 0.42791884E 02 | 0.55056499E 02 | 50.988 | 5.656 | 0.242587 | 9 | 53.254 |
| -0.70116779E 01 | 0.38249783E 01 | 0.84997188E 01 | 153.884 | 15.309 | 0.038948 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 184 CR 22.1 TR 19 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.25205346E 03 | | | | | | | |
| 0.70474877E 02 | -0.49767277E 02 | 0.86279659E 02 | 324.771 | 324.771 | 1.000000 | 1 | 9.917 |
| -0.29411211E 02 | 0.40052932E 02 | 0.46392706E 02 | 120.307 | 60.153 | 0.537727 | 2 | 11.834 |
| -0.98484578E 02 | -0.73771788E 01 | 0.51020728E 02 | 188.314 | 62.771 | 0.591389 | 3 | 17.751 |
| 0.12492435E 02 | 0.11381488E 02 | 0.16886132E 02 | 42.288 | 10.571 | 0.195725 | 4 | 23.669 |
| 0.31898987E 02 | -0.91348688E 01 | 0.33142678E 02 | 344.082 | 68.808 | 0.384149 | 5 | 29.586 |
| 0.68221468E 01 | 0.12798888E 02 | 0.14088198E 02 | 62.238 | 10.373 | 0.162795 | 6 | 35.503 |
| 0.19872888E 02 | 0.73828888E 01 | 0.20423888E 02 | 20.991 | 2.998 | 0.236718 | 7 | 41.420 |
| -0.11837888E 02 | 0.14988218E 02 | 0.19098828E 02 | 128.442 | 16.058 | 0.220918 | 8 | 47.337 |
| 0.19998988E 02 | 0.85237288E 01 | 0.18888138E 02 | 28.114 | 3.124 | 0.209835 | 9 | 53.254 |
| -0.44738838E 00 | 0.13891228E 01 | 0.14993818E 01 | 107.851 | 10.785 | 0.016919 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 184 CR 22.1 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.99277228E 02 | | | | | | | |
| -0.51741884E 02 | 0.97447838E 02 | 0.11033218E 03 | 117.967 | 117.967 | 1.000000 | 1 | 9.917 |
| 0.17884328E 02 | -0.26878138E 02 | 0.27313588E 02 | 318.688 | 159.418 | 0.247588 | 2 | 11.834 |
| 0.52912788E 02 | 0.25212278E 02 | 0.58251538E 02 | 25.646 | 8.549 | 0.527865 | 3 | 17.751 |
| -0.18784258E 02 | -0.37839358E 02 | 0.38588728E 02 | 253.798 | 63.437 | 0.349678 | 4 | 23.669 |
| -0.98782588E 01 | 0.38784288E 01 | 0.97718268E 01 | 161.656 | 32.331 | 0.088567 | 5 | 29.586 |
| -0.49842358E 01 | -0.11193488E 02 | 0.12228958E 02 | 245.378 | 48.988 | 0.110781 | 6 | 35.503 |
| 0.31288[illegible]E 01 | -0.99849988E 00 | 0.31748488E 01 | 344.937 | 49.991 | 0.028818 | 7 | 41.420 |
| -0.14987768E 01 | 0.23448898E 01 | 0.27828888E 01 | 122.588 | 17.323 | 0.025223 | 8 | 47.337 |
| -0.15423248E 01 | 0.43251988E 01 | 0.45987118E 01 | 109.861 | 12.207 | 0.041681 | 9 | 53.254 |
| -0.92788128E 00 | 0.38124768E 01 | 0.39235488E 01 | 103.666 | 10.367 | 0.035561 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 184 CR 22.1 TR 26 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.32672318E 01 | | | | | | | |
| 0.12419788E 01 | -0.17138518E 01 | 0.21163138E 01 | 305.921 | 305.921 | 1.000000 | 1 | 9.917 |
| -0.26142468E-01 | 0.23697888E-01 | 0.35284228E-01 | 137.989 | 68.995 | 0.016672 | 2 | 11.834 |
| -0.32228888E-01 | -0.21494128E-01 | 0.38714498E-01 | 213.653 | 71.218 | 0.018294 | 3 | 17.751 |
| 0.12887248E-01 | 0.12279458E 00 | 0.12339518E 00 | 84.376 | 21.094 | 0.058289 | 4 | 23.669 |
| 0.46242338E-02 | -0.14293198E-02 | 0.48488878E-02 | 342.824 | 68.565 | 0.002287 | 5 | 29.586 |
| 0.78841588E-02 | 0.24879778E-02 | 0.74631918E-02 | 18.829 | 3.137 | 0.003526 | 6 | 35.503 |
| -0.14796738E-01 | 0.31588488E-02 | 0.15128298E-01 | 167.979 | 23.997 | 0.007140 | 7 | 41.420 |
| 0.68879918E-02 | 0.10514488E-01 | 0.19649368E-01 | 78.438 | 8.803 | 0.009289 | 8 | 47.337 |
| 0.75223718E-02 | -0.13882898E-01 | 0.15892288E-01 | 299.898 | 33.322 | 0.007531 | 9 | 53.254 |
| -0.11588528E-01 | -0.2828883E-01 | 0.3845718E-01 | 247.885 | 24.788 | 0.018492 | 10 | 59.172 |

HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 26

HARMONIC ANALYSIS MODEL MM-51A SHIP 1002C T 4.96 CTR 264 CR 11.0 TR 2 PL. BOWD 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/C1MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.31911288E 00 | | | | | | | |
| 0.28112288E 04 | 0.5496617E 04 | 0.6001309E 04 | 29.263 | 65.263 | 0.792002 | 1 | 5.862 |
| 0.31000000E 00 | -0.7914797E 04 | 0.7576621E 04 | 277.329 | 130.662 | 1.000000 | 2 | 11.705 |
| 0.21364788E 04 | -0.1042718E 03 | 0.2141195E 04 | 356.137 | 116.712 | 0.281627 | 3 | 17.647 |
| -0.20464788E 00 | -0.1042711E 03 | 0.4013985E 03 | 207.331 | 51.033 | 0.052972 | 4 | 23.529 |
| -0.22464978E 00 | -0.4488861E 00 | 0.4495129E 03 | 184.984 | 44.987 | 0.059400 | 5 | 29.412 |
| -0.17199138E 00 | -0.2402728E 03 | 0.2954634E 03 | 234.418 | 30.068 | 0.038997 | 6 | 35.294 |
| 0.28129128E 03 | -0.2387708E 00 | 0.3609863E 03 | 319.674 | 45.668 | 0.046850 | 7 | 41.176 |
| -0.2842248E 00 | 0.2099288E 00 | 0.3149288E 00 | 180.128 | 17.266 | 0.001516 | 8 | 47.059 |
| -0.1284848E 02 | -0.7484467E 02 | 0.1228848E 03 | 217.643 | 24.185 | 0.016187 | 9 | 52.941 |
| 0.4848778E 02 | -0.1448648E 03 | 0.1507934E 03 | 286.358 | 28.634 | 0.019897 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL MM-51A SHIP 1002C T 4.96 CTR 264 CR 11.0 TR 4 PL. BOWD 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/C1MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.19987028E 04 | | | | | | | |
| 0.12999788E 04 | 0.6837484E 03 | 0.1312284E 04 | 32.396 | 32.106 | 1.000000 | 1 | 5.882 |
| -0.10778888E 00 | -0.2824488E 00 | 0.2833811E 03 | 247.782 | 125.831 | 0.107806 | 2 | 11.765 |
| -0.11323078E 00 | -0.1799717E 03 | 0.2004888E 00 | 237.238 | 79.079 | 0.138874 | 3 | 17.647 |
| 0.10214888E 00 | 0.1148214E 00 | 0.2162251E 03 | 32.488 | 0.152 | 0.148881 | 4 | 23.529 |
| 0.24178848E 00 | 0.2147128E 00 | 0.3788919E 03 | 34.999 | 6.911 | 0.290881 | 5 | 29.412 |
| 0.78487288E 02 | 0.8884488E 02 | 0.1137918E 03 | 47.813 | 7.969 | 0.078844 | 6 | 35.294 |
| -0.6448888E 00 | 0.6788288E 02 | 0.4828488E 03 | 168.844 | 24.121 | 0.298898 | 7 | 41.176 |
| 0.2818888E 00 | -0.2812888E 03 | 0.4274818E 03 | 318.887 | 39.897 | 0.288877 | 8 | 47.059 |
| 0.1628848E 00 | 0.1544884E 03 | 0.2248888E 00 | 43.243 | 4.841 | 0.148187 | 9 | 52.941 |
| -0.4888884E 02 | 0.1148288E 00 | 0.1318978E 03 | 116.198 | 11.815 | 0.007217 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL MM-51A SHIP 1002C T 4.96 CTR 264 CR 11.0 TR 6 PL. BOWD 75

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/C1MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.11647788E 00 | | | | | | | |
| 0.2884888E 04 | -0.6128988E 03 | 0.1178698E 04 | 328.637 | 328.637 | 1.000000 | 1 | 5.882 |
| -0.1988888E 03 | 0.7888888E 00 | 0.7988438E 03 | 181.493 | 90.747 | 0.678887 | 2 | 11.765 |
| -0.2822258E 00 | -0.1278648E 03 | 0.2917734E 03 | 288.888 | 48.669 | 0.247885 | 3 | 17.647 |
| 0.1218788E 00 | 0.8782951E 02 | 0.1498884E 03 | 34.538 | 8.633 | 0.125788 | 4 | 23.529 |
| 0.2348888E 00 | 0.1137138E 03 | 0.2582278E 03 | 78.134 | 5.227 | 0.219485 | 5 | 29.412 |
| 0.1788778E 01 | 0.8948218E 02 | 0.9948677E 02 | 88.351 | 14.725 | 0.858492 | 6 | 35.294 |
| 0.4488848E 00 | -0.1478888E 02 | 0.5284848E 02 | 341.151 | 48.748 | 0.884823 | 7 | 41.176 |
| -0.7818888E 02 | -0.8888488E 02 | 0.7872278E 02 | 288.978 | 25.867 | 0.888887 | 8 | 47.059 |
| 0.8488788E 01 | -0.7158888E 02 | 0.7288848E 02 | 278.782 | 38.731 | 0.848257 | 9 | 52.941 |
| 0.1848788E 02 | -0.7588848E 02 | 0.7868847E 02 | 288.289 | 28.529 | 0.848942 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL MM-51A SHIP 1002C T 4.96 CTR 264 CR 11.0 TR 7 PL. BOWD 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/C1MAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.67614498E 03 | | | | | | | |
| 0.1888844E 04 | -0.1888488E 04 | 0.1498183E 04 | 312.999 | 312.999 | 1.000000 | 1 | 5.882 |
| -0.9484478E 01 | 0.8888888E 03 | 0.8883578E 03 | 98.618 | 49.309 | 0.598772 | 2 | 11.765 |
| -0.1848278E 00 | 0.2488278E 03 | 0.3783991E 03 | 118.971 | 39.657 | 0.186799 | 3 | 17.647 |
| 0.2888788E 02 | -0.1488948E 00 | 0.1467527E 03 | 277.914 | 69.479 | 0.888888 | 4 | 23.529 |
| -0.2838488E 02 | -0.2814988E 02 | 0.3887388E 02 | 211.953 | 42.391 | 0.829958 | 5 | 29.412 |
| 0.1194822E 02 | 0.2888878E 02 | 0.2942881E 02 | 44.845 | 11.888 | 0.819743 | 6 | 35.294 |
| 0.1588848E 00 | -0.5782788E 02 | 0.1642597E 03 | 339.498 | 48.588 | 0.118828 | 7 | 41.176 |
| -0.1488778E 00 | 0.1488978E 03 | 0.2298188E 03 | 131.254 | 18.407 | 0.151282 | 8 | 47.059 |
| -0.1384828E 00 | 0.1827488E 02 | 0.1318639E 03 | 175.985 | 24.881 | 0.887844 | 9 | 52.941 |
| -0.2888788E 02 | -0.1178948E 02 | 9.2864784E 02 | 288.578 | 28.857 | 0.817882 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 26

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 264 CR 11.0 TR 16 PL. BOOM 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.73044638E 02 | | | | | | | |
| 0.63037258E 03 | -0.11886838E 04 | 0.12194228E 04 | 301.579 | 301.579 | 1.000000 | 1 | 5.862 |
| 0.78124038E 02 | 0.53716468E 00 | 0.94281628E 03 | 01.725 | 48.862 | 0.448142 | 2 | 11.748 |
| 0.88488748E 02 | 0.43631918E 03 | 0.43584358E 03 | 78.806 | 26.169 | 0.3547e2 | 3 | 17.647 |
| -0.98267148E 02 | -0.19780028E 03 | 0.16480988E 03 | 234.514 | 58.629 | 0.134827 | 4 | 23.529 |
| -0.30163138E 00 | -0.21341188E 03 | 0.48726488E 00 | 269.214 | 41.843 | 0.398271 | 5 | 29.412 |
| -0.43883168E 01 | -0.98877888E 02 | 0.98172618E 02 | 267.484 | 44.581 | 0.080307 | 6 | 35.294 |
| -0.18842918E 03 | 0.58152318E 00 | 0.18888888E 03 | 179.667 | 25.667 | 0.082831 | 7 | 41.176 |
| 0.54721828E 02 | -0.68888841E 02 | 0.88848337E 02 | 308.833 | 38.504 | 0.072884 | 8 | 47.059 |
| 0.21567368E 02 | 0.68328828E 00 | 0.21575768E 02 | 1.432 | 0.178 | 0.017698 | 9 | 52.941 |
| -0.12844258E 02 | 0.79941288E 02 | 0.77888138E 02 | 99.681 | 9.960 | 0.063861 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 264 CR 11.0 TR 11 PL. BOOM 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.88921388E 03 | | | | | | | |
| 0.38614778E 03 | -0.79498187E 00 | 0.87287878E 03 | 294.888 | 294.888 | 1.000000 | 1 | 5.882 |
| 0.18844818E 00 | 0.18241328E 03 | 0.28823988E 03 | 81.161 | 28.981 | 0.238864 | 2 | 11.768 |
| 0.25778318E 00 | 0.41413988E 03 | 0.44788818E 23 | 38.125 | 19.375 | 0.258788 | 3 | 17.647 |
| -0.11828978E 00 | -0.41348887E 02 | 3.12388888E 03 | 188.288 | 48.817 | 0.148812 | 4 | 23.529 |
| -0.88121518E 03 | -0.2788259E 00 | 0.48479888E 03 | 283.382 | 48.666 | 0.788118 | 5 | 29.412 |
| -0.97471188E 02 | -0.25388688E 03 | 0.26888888E 03 | 257.344 | 42.674 | 0.298187 | 6 | 35.294 |
| -0.78188888E 03 | -0.19488318E 02 | 0.17888888E 03 | 188.887 | 27.884 | 0.282288 | 7 | 41.176 |
| 0.18148488E 00 | -0.21868387E 03 | 0.28223738E 03 | 288.888 | 38.881 | 0.288884 | 8 | 47.888 |
| 0.88888128E 02 | -0.61788888E 02 | 0.11221648E 03 | 328.188 | 38.811 | 0.128888 | 9 | 52.941 |
| 0.88387848E 02 | 0.11488988E 02 | 0.41482148E 02 | 18.981 | 1.871 | 0.878884 | 10 | 58.884 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 264 CR 11.0 TR 13 PL. BOOM 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.32899828E 03 | | | | | | | |
| 0.11173278E 03 | -0.44484488E 03 | 0.47884718E 03 | 288.482 | 283.482 | 0.788847 | 1 | 5.882 |
| 0.11888168E 03 | -0.11888888E 03 | 0.16271188E 03 | 317.182 | 138.991 | 0.288138 | 2 | 11.788 |
| 0.38423348E 03 | 0.38889888E 03 | 0.53257828E 03 | 46.888 | 18.817 | 0.844823 | 3 | 17.647 |
| -0.97468988E 02 | -0.35284888E 01 | 0.57877718E 02 | 183.512 | 48.878 | 0.891248 | 4 | 23.529 |
| -0.57944318E 03 | -0.24818428E 03 | 0.68882528E 03 | 283.178 | 48.634 | 1.888888 | 5 | 29.412 |
| -0.81316878E 02 | -0.33584388E 03 | 0.34888928E 03 | 256.381 | 42.738 | 0.547888 | 6 | 35.294 |
| -0.17888888E 03 | -0.18864888E 03 | 0.28778888E 03 | 218.273 | 38.838 | 0.224888 | 7 | 41.176 |
| 0.78488888E 88 | -0.23858384E 03 | 0.37384428E 03 | 321.894 | 48.237 | 0.982777 | 8 | 47.888 |
| 0.12854718E 03 | -0.64888288E 02 | 0.14313488E 03 | 332.146 | 38.888 | 0.278888 | 9 | 52.941 |
| 0.75212348E 02 | -0.16248888E 88 | 0.12788888E 03 | 388.278 | 38.829 | 0.268579 | 10 | 58.884 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 496 CTR 264 CR 11.0 TR 14 PL. BOOM 188

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.64884648E 02 | | | | | | | |
| -0.81868788E 02 | -0.25812878E 03 | 0.26784218E 03 | 252.289 | 252.289 | 0.383677 | 1 | 5.882 |
| 0.98478888E 02 | -0.23987248E 03 | 0.24434368E 03 | 281.923 | 148.981 | 0.532271 | 2 | 11.768 |
| 0.38232848E 03 | 0.22898888E 88 | 0.44288218E 03 | 38.318 | 18. 85 | 0.884788 | 3 | 17.647 |
| 0.44487548E 02 | 0.41772588E 02 | 0.61171288E 02 | 43.888 | 18.787 | 0.138254 | 4 | 23.529 |
| -0.44834488E 03 | -0.12728538E 88 | 0.49888888E 03 | 193.517 | 98.783 | 1.888888 | 5 | 29.412 |
| -0.13933818E 88 | -0.27258378E 03 | 0.38818288E 03 | 243.998 | 48.588 | 0.662788 | 6 | 35.294 |
| -0.14738248E 03 | -0.13338838E 03 | 0.19234888E 03 | 219.886 | 31.414 | 0.418891 | 7 | 41.176 |
| 0.38362888E 03 | -0.28944988E 88 | 0.38883738E 03 | 319.428 | 38.829 | 0.388883 | 8 | 47.888 |
| 0.85286778E 02 | -0.73648318E 02 | 0.11258378E 03 | 319.248 | 33.472 | 0.248849 | 9 | 52.941 |
| 0.37922428E 87 | -0.13874118E 88 | 0.13812998E 03 | 288.178 | 28.617 | 0.298841 | 10 | 58.884 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 26

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 264 CR 11.0 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.11321395 05 | | | | | | | |
| -0.2050264E 04 | 0.3747297E 05 | 0.3752901E 05 | 93.132 | 93.132 | 1.000000 | 1 | 5.882 |
| -0.1000351E 04 | -0.1363829E 04 | 0.3368643E 04 | 283.869 | 181.934 | 0.089756 | 2 | 11.765 |
| -0.3295454E 03 | -0.3273254E 03 | 0.4644404E 03 | 224.885 | 74.935 | 0.012377 | 3 | 17.647 |
| -0.3561497E 03 | -0.5354337E 02 | 0.3601519E 03 | 188.550 | 47.137 | 0.009597 | 4 | 23.529 |
| -0.3470352E 03 | -0.3001663E 03 | 0.3001522E 03 | 226.064 | 45.213 | 0.007327 | 5 | 29.412 |
| 0.3027740E 02 | 0.8779650E 02 | 0.9614520E 02 | 65.888 | 10.981 | 0.002562 | 6 | 35.294 |
| -0.4851453E 03 | -0.2654124E 03 | 0.5530005E 03 | 208.682 | 29.812 | 0.014735 | 7 | 41.176 |
| 0.1826320E 03 | -0.7665674E 03 | 0.7880227E 03 | 283.401 | 35.425 | 0.020998 | 8 | 47.059 |
| -0.7850501E 02 | 0.3[illegible] | 0.3179360E 03 | 104.206 | 11.580 | 0.008472 | 9 | 52.941 |
| 0.7457849E 02 | -0.9106377E 00 | 0.7458447E 02 | 359.308 | 39.930 | 0.001987 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 264 CR 11.0 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1667000E 05 | | | | | | | |
| -0.1731142E 04 | 0.2238951E 05 | 0.2246833E 05 | 94.421 | 94.421 | 1.000000 | 1 | 5.882 |
| -0.1702671E 04 | -0.6869994E 03 | 0.1824326E 04 | 201.095 | 100.547 | 0.081190 | 2 | 11.765 |
| 0.5000647E 02 | 0.3315635E 03 | 0.3306128E 03 | 80.863 | 20.688 | 0.014990 | 3 | 17.647 |
| 0.7159214E 03 | 0.2677344E 03 | 0.7643499E 03 | 20.904 | 5.726 | 0.034037 | 4 | 23.529 |
| -0.3997700E 03 | -0.1982613E 03 | 0.4462332E 03 | 206.379 | 41.276 | 0.019871 | 5 | 29.412 |
| -0.6364409E 02 | 0.6144470E 03 | 0.6178952E 03 | 90.720 | 16.495 | 0.018672 | 6 | 35.294 |
| 0.1667914E 00 | 0.1809299E 03 | 0.1942154E 03 | 34.118 | 4.874 | 0.000864 | 7 | 41.176 |
| -0.2158279E 03 | 0.1670895E 03 | 0.2720724E 03 | 142.089 | 17.757 | 0.012176 | 8 | 47.059 |
| 0.1900464E 02 | -0.2439464E 03 | 0.2443948E 03 | 276.440 | 30.819 | 0.010883 | 9 | 52.941 |
| 0.1946445E 03 | -0.1883332E 03 | 0.1871806E 03 | 329.740 | 32.574 | 0.008332 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 264 CR 11.0 TR 8 CH. BEND 119

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9695109E 04 | | | | | | | |
| -0.7717044E 03 | 0.9462570E 04 | 0.9513982E 04 | 94.653 | 94.653 | 1.000000 | 1 | 5.882 |
| -0.6984424E 03 | -0.9444277E 03 | 0.8899637E 03 | 217.936 | 108.968 | 0.093501 | 2 | 11.765 |
| 0.1934709E 03 | 0.2829823E 02 | 0.1974290E 03 | 7.655 | 2.552 | 0.020752 | 3 | 17.647 |
| 0.7983269E 03 | 0.1448294E 02 | 0.7984985E 03 | 1.195 | 0.299 | 0.083889 | 4 | 23.529 |
| -0.6335869E 02 | 0.2118743E 03 | 0.2211427E 03 | 106.647 | 21.329 | 0.023244 | 5 | 29.412 |
| -0.3075137E 02 | 0.5195947E 03 | 0.5204214E 03 | 93.321 | 15.554 | 0.054701 | 6 | 35.294 |
| 0.2792234E 03 | 0.5114140E 02 | 0.2838670E 03 | 10.379 | 1.483 | 0.029837 | 7 | 41.176 |
| 0.2790308E 03 | 0.6390280E 03 | 0.6908334E 03 | 66.377 | 8.297 | 0.072602 | 8 | 47.059 |
| -0.1179938E 03 | -0.5795980E 03 | 0.5914204E 03 | 258.492 | 28.721 | 0.062164 | 9 | 52.941 |
| 0.9694064E 02 | -0.1601133E 03 | 0.1871730E 03 | 301.193 | 30.119 | 0.019674 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 494 CTR 264 CR 11.0 TR 12 CH. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6661336E 04 | | | | | | | |
| -0.3590421E 03 | 0.3858272E 04 | 0.3875000E 04 | 95.326 | 95.326 | 1.000000 | 1 | 5.882 |
| -0.4152627E 03 | -0.3811440E 03 | 0.5630624E 03 | 222.547 | 111.274 | 0.145461 | 2 | 11.765 |
| 0.2036055E 00 | 0.1540842E 02 | 0.2042736E 03 | 4.340 | 1.449 | 0.052716 | 3 | 17.647 |
| 0.3876704E 03 | -0.2729826E 02 | 0.3886357E 03 | 355.979 | 88.995 | 0.100293 | 4 | 23.529 |
| 0.9000000E 01 | 0.7529[illegible]E 02 | 0.7593239E 02 | 82.948 | 16.590 | 0.019595 | 5 | 29.412 |
| -0.2079825E 02 | 0.2673012E 03 | 0.2684599E 03 | 96.143 | 16.024 | 0.069431 | 6 | 35.294 |
| 0.1504000E 00 | -0.5280979E 02 | 0.1648232E 03 | 341.812 | 48.830 | 0.043681 | 7 | 41.176 |
| 0.2004870E 03 | 0.4267275E 03 | 0.4[illegible]E 03 | 63.961 | 7.995 | 0.122564 | 8 | 47.059 |
| -0.1048254E 03 | -0.3000000E 03 | 0.[illegible]E 03 | 250.000 | 27.778 | 0.062413 | 9 | 52.941 |
| 0.2239464E 02 | -0.1946797E 02 | 0.2733130E 02 | 329.022 | 32.902 | 0.007053 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 26

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 4% CTR 264 CR 11.0 TR 9 TORSION 113

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.10077082E 03 | | | | | | | |
| 0.11071614E 00 | -0.12782644E 00 | 0.16910099E 03 | 310.000 | 310.000 | 0.766600 | 1 | 9.002 |
| -0.17200279E 03 | 0.10799444E 03 | 0.20200097E 03 | 147.984 | 72.007 | 0.992777 | 2 | 11.700 |
| -0.66081966E 02 | -0.2.884140E 00 | 0.22894088E 03 | 284.662 | 84.021 | 1.000000 | 3 | 17.007 |
| 0.10170000E 02 | 0.11483000E 03 | 0.11677088E 03 | 89.004 | 21.201 | 0.515601 | 4 | 23.529 |
| -0.99349044E 02 | -0.11321868E 03 | 0.15064088E 03 | 228.737 | 48.747 | 0.644881 | 5 | 29.412 |
| 0.79580823E 02 | 0.20977088E 02 | 0.84708813E 02 | 20.686 | 3.304 | 0.372000 | 6 | 35.294 |
| 0.82691082E 02 | -0.26438678E 01 | 0.82733823E 02 | 356.169 | 51.167 | 0.368203 | 7 | 41.176 |
| -0.79980266E 02 | -0.14428044E 02 | 0.80873668E 02 | 190.348 | 23.881 | 0.358894 | 8 | 47.059 |
| 0.24191934E 02 | 0.43237771E 01 | 0.25004894E 02 | 10.670 | 1.628 | 0.110878 | 9 | 52.941 |
| -0.91673728E 01 | -0.30844612E 01 | 0.96666364E 01 | 198.495 | 10.849 | 0.042871 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 4% CTR 264 CR 11.0 TR 19 TORSION 180

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.21144738E 02 | | | | | | | |
| 0.27287998E 02 | 0.28436838E 02 | 0.39628966E 02 | 36.911 | 36.911 | 0.318262 | 1 | 9.002 |
| -0.10888644E 03 | -0.49994128E 01 | 0.10991988E 03 | 182.680 | 91.329 | 1.000000 | 2 | 11.700 |
| 0.23961298E 02 | -0.87881088E 02 | 0.90864478E 02 | 285.140 | 95.000 | 0.818892 | 3 | 17.007 |
| 0.15184128E 02 | 0.47728000E 02 | 0.50080828E 02 | 72.436 | 18.109 | 0.448196 | 4 | 23.529 |
| -0.48687168E 02 | -0.30468788E 02 | 0.56888598E 02 | 223.488 | 44.681 | 0.503788 | 5 | 29.412 |
| 0.14136048E 02 | 0.46413648E 01 | 0.14888848E 02 | 18.152 | 3.028 | 0.129848 | 6 | 35.294 |
| 0.20448288E 02 | -0.58428868E 01 | 0.21278288E 02 | 344.082 | 49.152 | 0.190811 | 7 | 41.176 |
| -0.16628048E 02 | -0.23998328E 02 | 0.28948878E 02 | 234.444 | 29.308 | 0.278574 | 8 | 47.059 |
| 0.24288828E 02 | -0.25254417E 01 | 0.24611918E 02 | 350.842 | 50.340 | 0.220817 | 9 | 52.941 |
| -0.85737048E 01 | 0.29181758E 01 | 0.90867958E 01 | 161.283 | 10.128 | 0.084707 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 4% CTR 264 CR 11.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.11306188E 03 | | | | | | | |
| -0.62978279E 02 | 0.14652093E 03 | 0.16159778E 03 | 112.937 | 112.937 | 1.000000 | 1 | 9.002 |
| 0.99932738E 02 | -0.28840095E 02 | 0.58759968E 02 | 339.539 | 169.769 | 0.363819 | 2 | 11.700 |
| 0.32911438E 02 | 0.32882699E 02 | 0.44227144E 02 | 45.388 | 19.189 | 0.280869 | 3 | 17.007 |
| 0.22442918E 02 | -0.30721918E 02 | 0.38075248E 02 | 306.209 | 76.552 | 0.238617 | 4 | 23.529 |
| -0.74991088E 01 | 0.21448898E 02 | 0.22719788E 02 | 109.146 | 21.833 | 0.140898 | 5 | 29.412 |
| -0.76303978E 01 | -0.29326978E 00 | 0.76668118E 02 | 253.232 | 42.205 | 0.048073 | 6 | 35.294 |
| 0.80999978E 01 | -0.24819088E 01 | 0.84988148E 01 | 343.667 | 49.095 | 0.052581 | 7 | 41.176 |
| -0.47958048E 00 | -0.14978378E 01 | 0.15718118E 01 | 252.305 | 31.538 | 0.009824 | 8 | 47.059 |
| 0.32276128E 01 | 0.39019088E 01 | 0.51294168E 01 | 50.670 | 5.663 | 0.031717 | 9 | 52.941 |
| -0.12995518E 01 | -0.39193258E 01 | 0.41167428E 01 | 252.184 | 29.218 | 0.025679 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1082C T 4% CTR 264 CR 11.0 TR 26 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.31505278E 01 | | | | | | | |
| 0.10188268E 01 | -0.14773058E 01 | 0.17945578E 01 | 304.592 | 304.592 | 1.000000 | 1 | 9.002 |
| -0.61381288E-01 | 0.26000178E-01 | 0.66677288E-01 | 156.413 | 78.207 | 0.037222 | 2 | 11.700 |
| 0.46894678E-02 | -0.67006758E-01 | 0.42364958E-01 | 276.197 | 92.052 | 0.024752 | 3 | 17.007 |
| -0.67446358E-01 | 0.90481748E-01 | 0.11279118E 00 | 126.725 | 31.681 | 0.062882 | 4 | 23.529 |
| 0.31733918E-01 | -0.39957978E-01 | 0.47958048E-01 | 311.429 | 62.286 | 0.026724 | 5 | 29.412 |
| 0.47795778E-02 | 0.64486778E-02 | 0.79988228E-02 | 53.260 | 8.877 | 0.004482 | 6 | 35.294 |
| -0.28043538E-01 | -0.12828418E-01 | 0.30914378E-01 | 203.216 | 29.031 | 0.017004 | 7 | 41.176 |
| 0.36983738E-01 | -0.24853788E-03 | 0.36984518E-01 | 359.627 | 44.953 | 0.020609 | 8 | 47.059 |
| -0.95373248E-02 | -0.48328988E-02 | 0.10854928E-01 | 202.921 | 22.547 | 0.005778 | 9 | 52.941 |
| 0.42918798E-02 | 0.48221748E-02 | 0.58928068E-02 | 43.418 | 4.341 | 0.003284 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 27

HARMONIC ANALYSIS MODEL SH-51A SHIP 1002C T 500 CTR 458 CR 39.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.3174258E 05 | | | | | | | |
| -0.5071292E 03 | 0.7341384E 04 | 0.7358975E 04 | 93.952 | 93.952 | 0.955872 | 1 | 5.882 |
| 0.1241127E 04 | -0.7507804E 04 | 0.7698594E 04 | 279.277 | 139.639 | 1.000000 | 2 | 11.765 |
| 0.4996279E 04 | -0.1107597E 04 | 0.5117582E 04 | 347.500 | 115.833 | 0.664742 | 3 | 17.647 |
| -0.1067423E 04 | 0.1588192E 04 | 0.1873957E 04 | 122.520 | 30.630 | 0.243415 | 4 | 23.529 |
| 0.2617078E 04 | -0.8196107E 03 | 0.2742239E 04 | 342.623 | 68.525 | 0.356200 | 5 | 29.412 |
| -0.3712290E 03 | -0.1360595E 03 | 0.3956877E 03 | 200.251 | 33.375 | 0.051397 | 6 | 35.294 |
| 0.4857012E 03 | -0.9382632E 03 | 0.7250854E 03 | 312.061 | 44.580 | 0.094174 | 7 | 41.176 |
| -0.3848240E 03 | 0.5972773E 03 | 0.7105151E 03 | 122.794 | 15.349 | 0.092791 | 8 | 47.059 |
| -0.6195373E 02 | 0.3000954E 02 | 0.6883675E 02 | 154.155 | 17.128 | 0.008962 | 9 | 52.941 |
| -0.1498774E 02 | 0.7856545E 02 | 0.7998219E 02 | 100.000 | 10.000 | 0.010389 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL SH-51A SHIP 1002C T 500 CTR 458 CR 39.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2203941E 04 | | | | | | | |
| 0.5601331E 03 | 0.1619118E 04 | 0.1713264E 04 | 70.917 | 70.917 | 1.000000 | 1 | 5.882 |
| -0.3332434E 02 | -0.1079854E 03 | 0.1087427E 03 | 252.069 | 126.035 | 0.063179 | 2 | 11.765 |
| -0.3066592E 03 | -0.1725863E 03 | 0.3536391E 03 | 209.212 | 69.737 | 0.206408 | 3 | 17.647 |
| 0.4214626E 03 | 0.9402174E 02 | 0.4318225E 03 | 12.576 | 3.144 | 0.252066 | 4 | 23.529 |
| -0.1214534E 04 | 0.2948574E 03 | 0.1251'36E 04 | 166.376 | 33.275 | 0.730824 | 5 | 29.412 |
| 0.2205981E 03 | 0.8688568E 02 | 0.2370846E 03 | 21.498 | 3.583 | 0.138381 | 6 | 35.294 |
| -0.6262881E 03 | 0.6292807E 03 | 0.8877666E 03 | 134.867 | 19.267 | 0.518171 | 7 | 41.176 |
| 0.3805564E 03 | -0.5493947E 03 | 0.6^21365E 03 | 304.780 | 42.687 | 0.389978 | 8 | 47.059 |
| 0.1476259E 03 | 0.1219159E 02 | 0.1481275E 03 | 4.721 | 0.525 | 0.086459 | 9 | 52.941 |
| 0.2188310E 02 | 0.8410828E 02 | 0.8690837E 02 | 75.416 | 7.542 | 0.050727 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL SH-51A SHIP 1002C T 500 CTR 458 CR 39.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1944841E 03 | | | | | | | |
| 0.1809494E 04 | -0.3447102E 03 | 0.1806687E 04 | 341.146 | 341.146 | 1.000000 | 1 | 5.882 |
| -0.3228498E 03 | 0.9364598E 03 | 0.9905488E 03 | 109.022 | 54.511 | 0.548622 | 2 | 11.765 |
| -0.6691321E 03 | 0.4111639E 02 | 0.6709940E 03 | 176.484 | 58.828 | 0.628682 | 3 | 17.647 |
| 0.1666167E 03 | -0.2144173E 03 | 0.2727791E 03 | 308.181 | 77.045 | 0.259722 | 4 | 23.529 |
| -0.6048096E 03 | 0.1774309E 03 | 0.6303752E 03 | 163.652 | 32.730 | 0.590965 | 5 | 29.412 |
| 0.9968044E 02 | 0.3993991E 02 | 0.9902081E 02 | 23.788 | 3.965 | 0.092830 | 6 | 35.294 |
| 0.2922049E 02 | 0.6916113E 02 | 0.7508369E 02 | 67.090 | 9.584 | 0.070390 | 7 | 41.176 |
| -0.5418093E 02 | -0.1247113E 02 | 0.5560387E 02 | 192.960 | 24.120 | 0.052129 | 8 | 47.059 |
| -0.3459588E 02 | -0.2233812E 02 | 0.4118089E 02 | 212.850 | 23.650 | 0.038606 | 9 | 52.941 |
| -0.2192491E 02 | -0.2404382E 02 | 0.3253931E 02 | 227.639 | 22.764 | 0.030585 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL SH-51A SHIP 1002C T 500 CTR 458 CR 39.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9928975E 03 | | | | | | | |
| 0.1067410E 04 | -0.9390137E 03 | 0.1419018E 04 | 318.783 | 318.783 | 1.000000 | 1 | 5.882 |
| -0.1156853E 03 | 0.9141987E 03 | 0.9214788E 03 | 97.207 | 48.604 | 0.649378 | 2 | 11.765 |
| -0.5512959E 03 | 0.5490777E 03 | 0.7790720E 03 | 135.105 | 45.035 | 0.549027 | 3 | 17.647 |
| -0.9636040E 02 | -0.2579618E 03 | 0.2636577E 03 | 257.695 | 64.414 | 0.185803 | 4 | 23.529 |
| 0.3477217E 03 | -0.7703711E 02 | 0.3561928E 03 | 347.508 | 69.502 | 0.250985 | 5 | 29.412 |
| 0.3468539E 02 | 0.5692101E 02 | 0.6661479E 02 | 58.702 | 9.784 | 0.046944 | 6 | 35.294 |
| 0.2742422E 03 | -0.2518604E 03 | 0.3718064E 03 | 317.527 | 45.381 | 0.262017 | 7 | 41.176 |
| -0.1999142E 03 | 0.3932901E 03 | 0.4859355E 03 | 119.504 | 14.938 | 0.286868 | 8 | 47.059 |
| -0.6780466E 01 | 0.7863909E 02 | 0.7895474E 02 | 95.419 | 10.602 | 0.050804 | 9 | 52.941 |
| 0.2099975E 02 | 0.9029598E 02 | 0.9266629E 02 | 76.902 | 7.690 | 0.065383 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 27

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 459 CR 36.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1036507E 04 | | | | | | | |
| 0.7058865E 03 | -0.8736101E 03 | 0.1123152E 04 | 308.938 | 308.938 | 1.000000 | 1 | 5.882 |
| -0.1088552E 03 | 0.4104729E 03 | 0.4246614E 03 | 104.853 | 52.426 | 0.378098 | 2 | 11.765 |
| -0.3006930E 03 | 0.7043704E 03 | 0.7658401E 03 | 113.111 | 37.704 | 0.681867 | 3 | 17.647 |
| -0.7128246E 03 | 0.4943279E 01 | 0.2178830E 03 | 178.659 | 44.665 | 0.189541 | 4 | 23.529 |
| 0.6001819E 03 | -0.1819797E 03 | 0.6271641E 03 | 343.132 | 68.626 | 0.558397 | 5 | 29.412 |
| -0.5694156E 02 | -0.5696289E 02 | 0.8054259E 02 | 225.011 | 37.502 | 0.071711 | 6 | 35.294 |
| -0.8319568E 02 | 0.2427069E 02 | 0.8666364E 02 | 163.736 | 23.391 | 0.077161 | 7 | 41.176 |
| 0.6016888E 02 | -0.6719113E 02 | 0.9019388E 02 | 311.844 | 38.980 | 0.080304 | 8 | 47.059 |
| 0.4905795E 02 | -0.7001871E 01 | 0.4959430E 02 | 351.884 | 39.058 | 0.044156 | 9 | 52.941 |
| 0.4725173E 02 | 0.4520636E 02 | 0.6539372E 02 | 43.733 | 4.373 | 0.058223 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 458 CR 36.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9906753E 03 | | | | | | | |
| 0.3120012E 03 | -0.6930693E 03 | 0.7509517E 03 | 294.549 | 294.549 | 1.000000 | 1 | 5.882 |
| -0.1528356E 03 | 0.4790840E 02 | 0.1601685E 03 | 162.596 | 81.298 | 0.213287 | 2 | 11.765 |
| -0.2211682E 02 | 0.6836960E 02 | 0.6840535E 02 | 91.853 | 30.618 | 0.910915 | 3 | 17.647 |
| -0.2403113E 03 | 0.2960178E 03 | 0.3811343E 03 | 133.188 | 33.297 | 0.467586 | 4 | 23.529 |
| 0.6119290E 03 | -0.2910057E 03 | 0.6779434E 03 | 334.505 | 66.901 | 0.902775 | 5 | 29.412 |
| -0.1836573E 03 | -0.1341651E 03 | 0.2274389E 03 | 216.150 | 36.025 | 0.302868 | 6 | 35.294 |
| -0.3288203E 03 | 0.1385215E 03 | 0.3567881E 03 | 157.155 | 22.451 | 0.475115 | 7 | 41.176 |
| 0.2382817E 03 | -0.3391672E 03 | 0.4144863E 03 | 305.091 | 38.136 | 0.551948 | 8 | 47.059 |
| 0.9467833E 02 | -0.9049310E 02 | 0.1089997E 03 | 303.404 | 33.712 | 0.144350 | 9 | 52.941 |
| 0.9250992E 02 | -0.6054622E 02 | 0.6872217E 02 | 298.233 | 29.823 | 0.091513 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 458 CR 36.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5437754E 03 | | | | | | | |
| 0.7061364E 02 | -0.3084038E 03 | 0.3136379E 03 | 280.482 | 280.482 | 0.513821 | 1 | 5.882 |
| -0.1907842E 03 | -0.2533410E 03 | 0.3171450E 03 | 233.017 | 116.509 | 0.519557 | 2 | 11.765 |
| 0.1981974E 03 | 0.5033679E 03 | 0.5409817E 03 | 68.508 | 22.836 | 0.886270 | 3 | 17.647 |
| -0.1283616E 03 | 0.3087156E 03 | 0.3313489E 03 | 111.300 | 27.825 | 0.542837 | 4 | 23.529 |
| 0.4857661E 03 | -0.1334332E 03 | 0.5037588E 03 | 344.640 | 68.928 | 0.825289 | 5 | 29.412 |
| -0.2391657E 03 | -0.1603644E 03 | 0.2881189E 03 | 213.820 | 35.637 | 0.472014 | 6 | 35.294 |
| -0.4708225E 03 | 0.1310704E 03 | 0.4887126E 03 | 164.449 | 23.493 | 0.800640 | 7 | 41.176 |
| 0.6020498E 03 | -0.4592910E 03 | 0.6104026E 03 | 311.198 | 38.900 | 1.000000 | 8 | 47.059 |
| 0.3561423E 02 | -0.9698811E 02 | 0.1031202E 03 | 290.163 | 32.240 | 0.169266 | 9 | 52.941 |
| -0.2103093E 02 | -0.1360777E 03 | 0.1376965E 03 | 261.211 | 26.121 | 0.225580 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 458 CR 36.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5472896E 03 | | | | | | | |
| -0.8644965E 02 | -0.1581288E 03 | 0.1802172E 03 | 241.334 | 241.334 | 0.293368 | 1 | 5.882 |
| -0.9375134E 02 | -0.2888028E 03 | 0.3032942E 03 | 252.094 | 126.047 | 0.493719 | 2 | 11.765 |
| 0.2564202E 03 | 0.3555613E 03 | 0.4383777E 03 | 54.202 | 18.067 | 0.713616 | 3 | 17.647 |
| -0.7566617E 02 | 0.3282712E 03 | 0.3368787E 03 | 102.980 | 25.745 | 0.548398 | 4 | 23.529 |
| 0.4263868E 03 | -0.8180597E 02 | 0.4321973E 03 | 349.089 | 69.818 | 0.703955 | 5 | 29.412 |
| -0.1931721E 03 | -0.7890950E 02 | 0.2086676E 03 | 202.220 | 33.703 | 0.339821 | 6 | 35.294 |
| -0.4378574E 03 | 0.1059833E 03 | 0.4505012E 03 | 166.393 | 23.770 | 0.733351 | 7 | 41.176 |
| 0.3484143E 03 | -0.4915708E 03 | 0.6143049E 03 | 306.850 | 38.356 | 1.000000 | 8 | 47.059 |
| 0.4971906E 02 | -0.8198744E 02 | 0.9588496E 02 | 301.233 | 33.470 | 0.156087 | 9 | 52.941 |
| -0.3771507E 02 | -0.1498649E 03 | 0.1545377E 03 | 255.874 | 25.587 | 0.251565 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 27

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 458 CR 35.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1370760E 05 | | | | | | | |
| -0.4854094E 04 | 0.5362419E 05 | 0.5384344E 05 | 95.172 | 95.172 | 1.000000 | 1 | 5.882 |
| 0.2713920E 04 | -0.1647877E 04 | 0.3175037E 04 | 328.734 | 164.367 | 0.058968 | 2 | 11.765 |
| -0.1093148E 04 | 0.1459256E 03 | 0.1102845E 04 | 172.396 | 57.465 | 0.020482 | 3 | 17.647 |
| 0.2530776E 03 | -0.8314630E 02 | 0.2669979E 03 | 341.805 | 85.451 | 0.004958 | 4 | 23.529 |
| 0.1361704E 04 | 0.2149861E 04 | 0.2544558E 04 | 57.660 | 11.532 | 0.047258 | 5 | 29.412 |
| -0.9580225E 03 | -0.6290791E 03 | 0.1146101E 04 | 213.291 | 35.548 | 0.021286 | 6 | 35.294 |
| 0.1391634E 03 | 0.9582339E 02 | 0.1689632E 03 | 34.550 | 4.936 | 0.C03138 | 7 | 41.176 |
| -0.9973333E 03 | -0.7710396E 03 | 0.1260625E 04 | 217.708 | 27.213 | 0.023413 | 8 | 47.059 |
| 0.1521871E 04 | 0.1048246E 04 | 0.1847948E 04 | 34.559 | 3.840 | 0.034321 | 9 | 52.941 |
| -0.3409854E 03 | 0.5345681E 03 | 0.6340615E 03 | 122.533 | 12.253 | 0.011776 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 458 CR 39.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1688314E 05 | | | | | | | |
| -0.2874373E 04 | 0.3341578E 05 | 0.3353917E 05 | 94.916 | 94.916 | 1.000000 | 1 | 5.882 |
| 0.1816666E 04 | -0.1367973E 04 | 0.2274120E 04 | 323.020 | 161.510 | 0.067805 | 2 | 11.765 |
| 0.3321C28E 03 | 0.1582680E 04 | 0.1617148E 04 | 78.149 | 26.050 | 0.048217 | 3 | 17.647 |
| 0.6C2000SE 03 | 0.5108345E 03 | 0.7895291E 03 | 40.317 | 10.079 | 0.023541 | 4 | 23.529 |
| 0.5026899E 03 | -0.3718956E 02 | 0.5040635E 03 | 355.769 | 71.154 | 0.015029 | 5 | 29.412 |
| 0.4904622E 02 | 0.5981633E 03 | 0.6001506E 03 | 85.312 | 14.219 | 0.017894 | 6 | 35.294 |
| 0.1706367E 03 | 0.1249617E 03 | 0.2108173E 03 | 34.821 | 4.974 | 0.006524 | 7 | 41.176 |
| 0.2379086E 03 | 0.5827759E 03 | 0.6295490E 03 | 68.019 | 9.502 | 0.018948 | 8 | 47.059 |
| -0.6593144E 02 | -0.2276262E 03 | 0.2368824E 03 | 253.844 | 28.205 | 0.007066 | 9 | 52.941 |
| 0.1618525E 03 | 0.1207382E 03 | 0.2019256E 03 | 36.722 | 3.672 | 0.006021 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 458 CR 39.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8906406E 04 | | | | | | | |
| -0.1061008E 04 | 0.1444432E 05 | 0.1448324E 05 | 94.201 | 94.201 | 1.000000 | 1 | 5.882 |
| 0.6754814E 03 | -0.1085136E 04 | 0.1278200E 04 | 301.982 | 150.991 | 0.088254 | 2 | 11.765 |
| 0.5367676E 03 | 0.4713706E 03 | 0.7143594E 03 | 41.288 | 13.763 | 0.049323 | 3 | 17.647 |
| 0.1010709E 04 | 0.4173300E 03 | 0.1091479E 04 | 22.436 | 5.609 | 0.075580 | 4 | 23.529 |
| -0.4700049E 03 | -0.2644204E 03 | 0.5402632E 03 | 209.547 | 41.909 | 0.037303 | 5 | 29.412 |
| 0.7571235E 04 | 0.2137552E 03 | 0.7867192E 03 | 15.766 | 2.628 | 0.054319 | 6 | 35.294 |
| 0.1510000E 03 | 0.3396680E 03 | 0.3720691E 03 | 65.638 | 9.377 | 0.025745 | 7 | 41.176 |
| C.9183574E 03 | 0.2098220E 03 | 0.9420220E 03 | 12.870 | 1.609 | 0.065042 | 8 | 47.059 |
| -0.1418029E C4 | -0.2393881E 03 | 0.1438094E 04 | 189.582 | 21.065 | 0.099294 | 9 | 52.941 |
| -0.1760245E 03 | -0.2145000E 03 | 0.2790283E 03 | 230.887 | 23.089 | 0.019266 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 458 CR 35.0 TR 12 CM. BEND 197

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7221477E C4 | | | | | | | |
| -0.5523943E 03 | 0.6038902E 04 | 0.6064113E 04 | 95.226 | 95.226 | 1.000000 | 1 | 5.882 |
| -0.7713997E 02 | -0.5599783E 03 | 0.5652604E 03 | 262.154 | 131.078 | 0.093215 | 2 | 11.765 |
| 0.2972402E 03 | 0.1652728E 03 | 0.3400981E 03 | 29.075 | 9.692 | C.056084 | 3 | 17.647 |
| 0.5469951E 03 | 0.2284944E 03 | 0.5929656E 03 | 22.712 | 5.678 | 0.097783 | 4 | 23.529 |
| -0.4275790E 03 | -0.1105330E 03 | 0.4416355E 03 | 194.494 | 38.899 | 0.072828 | 5 | 29.412 |
| 0.4799539E 03 | -0 2125053E 02 | 0.4814773E 03 | 357.177 | 59.529 | 0.079153 | 6 | 35.294 |
| 0.1027604E 03 | 0.1707000E 03 | 0.1993221E 03 | 58.965 | 8.424 | 0.032871 | 7 | 41.176 |
| 0.5814900E 03 | 0.9875043E 02 | 0.5898152E 03 | 9.638 | 1.205 | 0.097263 | 8 | 47.059 |
| -0.8907852E 03 | 0.3136145E 02 | 0.8993320E 03 | 178.002 | 19.778 | 0.148304 | 9 | 52.941 |
| -0.2746025E 03 | -0.4872525E 02 | 0.2788916E 03 | 190.042 | 19.004 | 0.045990 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 27

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 900 CTR 450 CR 35.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1837809E 03 | | | | | | | |
| 0.1040958E 03 | -0.5919818E 02 | 0.1204145E 03 | 330.593 | 330.593 | 0.452319 | 1 | 5.882 |
| -0.6351936E 02 | 0.1533324E 03 | 0.1661533E 03 | 112.476 | 56.238 | 0.624131 | 2 | 11.765 |
| -0.1720411E 03 | -0.4762326E 02 | 0.1785108E 03 | 195.473 | 65.158 | 0.670550 | 3 | 17.647 |
| 0.3248773E 02 | 0.9783978E 02 | 0.1030925E 03 | 71.631 | 17.908 | 0.387252 | 4 | 23.529 |
| 0.2467085E 03 | -0.1082285E 03 | 0.2662156E 03 | 337.930 | 67.586 | 1.000000 | 5 | 29.412 |
| -0.4814629E 02 | -0.6836866E 01 | 0.4862979E 02 | 188.082 | 31.347 | 0.182649 | 6 | 35.294 |
| 0.8849859E 02 | -0.1130443E 03 | 0.1435844E 03 | 308.059 | 44.008 | 0.539287 | 7 | 41.176 |
| -0.1450848E 02 | 0.1394474E 03 | 0.1402001E 03 | 95.940 | 11.992 | 0.526641 | 8 | 47.059 |
| -0.8833131E 02 | 0.1628532E 03 | 0.1852662E 03 | 118.475 | 13.164 | 0.695926 | 9 | 52.941 |
| -0.2233492E 02 | 0.4278589E 02 | 0.4782195E 02 | 117.843 | 11.784 | 0.179696 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 900 CTR 450 CR 35.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.6074988E 02 | | | | | | | |
| 0.1407773E 01 | 0.9934812E 02 | 0.9937309E 02 | 89.188 | 89.188 | 0.562465 | 1 | 5.882 |
| 0.1684795E 02 | 0.9778600E 01 | 0.1781873E 02 | 10.925 | 9.461 | 0.100814 | 2 | 11.765 |
| -0.3269299E 02 | 0.7748122E 02 | 0.8409616E 02 | 112.877 | 37.626 | 0.476010 | 3 | 17.647 |
| -0.6484367E 02 | 0.1449319E 02 | 0.6566355E 02 | 167.247 | 41.812 | 0.371675 | 4 | 23.529 |
| 0.1431965E 03 | -0.1034732E 03 | 0.1766490E 03 | 324.148 | 64.830 | 1.000000 | 5 | 29.412 |
| 0.1667212E 02 | 0.7732870E 02 | 0.7910712E 02 | 77.831 | 12.972 | 0.447770 | 6 | 35.294 |
| -0.7697294E 02 | -0.3511159E 02 | 0.8459360E 02 | 204.532 | 29.219 | 0.478673 | 7 | 41.176 |
| 0.5776329E 02 | -0.3076359E 02 | 0.6544693E 02 | 331.961 | 41.495 | 0.370436 | 8 | 47.059 |
| 0.1912371E 01 | 0.1284568E 03 | 0.1284718E 03 | 89.147 | 9.905 | 0.727185 | 9 | 52.941 |
| -0.6911388E 02 | 0.2667397E 02 | 0.7408257E 02 | 158.896 | 15.890 | 0.419330 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 900 CTR 450 CR 35.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.7836678E 02 | | | | | | | |
| -0.9062326E 02 | 0.2095867E 03 | 0.2179025E 03 | 109.800 | 109.800 | 1.000000 | 1 | 5.882 |
| 0.7253879E 02 | -0.3038306E 02 | 0.8243224E 02 | 332.269 | 166.134 | 0.378299 | 2 | 11.765 |
| 0.8878783E 02 | 0.1798242E 02 | 0.8268608E 02 | 12.561 | 4.187 | 0.379464 | 3 | 17.647 |
| -0.7082804E 01 | -0.4733393E 02 | 0.4786131E 02 | 261.483 | 65.371 | 0.219644 | 4 | 23.529 |
| -0.6922743E 01 | 0.8049187E 00 | 0.6976513E 01 | 172.882 | 34.576 | 0.032017 | 5 | 29.412 |
| -0.9710911E 01 | 0.1194188E 02 | 0.1992394E 02 | 129.713 | 21.619 | 0.091243 | 6 | 35.294 |
| -0.7761984E 00 | -0.3919688E 01 | 0.3804297E 01 | 257.563 | 36.795 | 0.016941 | 7 | 41.176 |
| 0.3918846E 01 | -0.2097293E 00 | 0.3916294E 01 | 356.989 | 44.624 | 0.017973 | 8 | 47.059 |
| -0.1640753E 02 | 0.9874609E 01 | 0.1914984E 02 | 148.959 | 16.551 | 0.087881 | 9 | 52.941 |
| -0.1432328E 02 | -0.2993159E 01 | 0.1463268E 02 | 191.803 | 19.180 | 0.067152 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 900 CTR 450 CR 35.0 TR 36 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.5237960E 01 | | | | | | | |
| 0.1698041E 01 | -0.1101429E 01 | 0.1592626E 01 | 313.184 | 313.184 | 1.000000 | 1 | 5.882 |
| -0.8877432E-01 | 0.9066398E-01 | 0.1022738E 00 | 150.277 | 75.138 | 0.064178 | 2 | 11.765 |
| -0.6986469E-01 | -0.3768044E-01 | 0.7938182E-01 | 208.345 | 69.448 | 0.049837 | 3 | 17.647 |
| 0.3279994E-01 | 0.2121697E 00 | 0.2146768E 00 | 81.228 | 20.307 | 0.134777 | 4 | 23.529 |
| -0.3573192E-01 | 0.2343651E-01 | 0.4386108E-01 | 144.554 | 28.911 | 0.027537 | 5 | 29.412 |
| 0.8040824E-03 | 0.1428095E-01 | 0.1431628E-01 | 86.459 | 14.410 | 0.008988 | 6 | 35.294 |
| 0.5721361E-02 | 0.3494888E-01 | 0.3540540E-01 | 80.701 | 11.529 | 0.022228 | 7 | 41.176 |
| -0.7123044E-02 | -0.1814549E-01 | 0.1744695E-01 | 248.194 | 35.774 | 0.011679 | 8 | 47.059 |
| 0.2777783E-01 | -0.5726626E-01 | 0.6364733E-01 | 295.874 | 32.875 | 0.039959 | 9 | 52.941 |
| 0.1256294E-02 | -0.1605244E-02 | 0.2038378E-02 | 308.046 | 30.805 | 0.001280 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 31

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.29031716 05 | | | | | | | |
| -0.11709176 04 | 0.71880396 04 | 0.78767626 04 | 98.608 | 98.608 | 1.000000 | 1 | 5.848 |
| -0.47160006 02 | -0.70673956 04 | 0.70675126 04 | 269.616 | 134.808 | 0.894722 | 2 | 11.696 |
| 0.95349146 04 | -0.88791106 03 | 0.56056136 04 | 350.908 | 116.963 | 0.711665 | 3 | 17.544 |
| -0.14344046 04 | 0.16765416 04 | 0.22044816 04 | 130.551 | 32.638 | 0.280125 | 4 | 23.392 |
| 0.38227676 04 | -0.45885626 03 | 0.30572766 04 | 351.383 | 70.277 | 0.388159 | 5 | 29.240 |
| -0.46128176 03 | -0.14714006 03 | 0.58327396 03 | 197.001 | 32.833 | 0.063893 | 6 | 35.088 |
| 0.40944176 03 | -0.59037336 03 | 0.71057066 03 | 314.2.. | 44.887 | 0.090212 | 7 | 40.936 |
| -0.28105146 03 | 0.38639096 03 | 0.47827226 03 | 126.188 | 15.764 | 0.060719 | 8 | 46.784 |
| 0.99203876 02 | 0.50436636 02 | 0.70368886 02 | 56.143 | 6.238 | 0.[illegible] | 9 | 52.632 |
| -0.93171656 01 | 0.24260516 02 | 0.24836396 02 | 102.342 | 10.234 | 0.[illegible] | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.16332066 04 | | | | | | | |
| 0.30403716 03 | 0.16823576 04 | 0.17256396 04 | 77.140 | 77.140 | 1.000000 | 1 | 5.848 |
| -0.14547156 03 | -0.15809126 03 | 0.20901906 03 | 225.895 | 112.9[illegible] | 0.121126 | 2 | 11.696 |
| -0.35774046 03 | -0.23947236 03 | 0.42850426 03 | 213.398 | 71.133 | 0.248316 | 3 | 17.544 |
| 0.57956956 03 | 0.45757726 02 | 0.58137266 03 | 4.514 | 1.129 | 0.336983 | 4 | 23.392 |
| -0.12913236 04 | 0.78082166 02 | 0.12933206 04 | 176.758 | 35.352 | 0.726298 | 5 | 29.240 |
| 0.19402946 03 | 0.71842336 02 | 0.20765316 03 | 20.241 | 3.374 | 0.120334 | 6 | 35.088 |
| -0.66742016 03 | 0.44497276 03 | 0.78960256 03 | 145.580 | 20.786 | 0.455253 | 7 | 40.936 |
| 0.37447046 03 | -0.34308806 03 | 0.50783796 03 | 317.509 | 39.689 | 0.294290 | 8 | 46.784 |
| 0.10520406 03 | 0.39146106 02 | 0.11225106 03 | 20.410 | 2.268 | 0.065049 | 9 | 52.632 |
| 0.50406956 02 | 0.84313426 02 | 0.10256706 03 | 55.288 | 5.529 | 0.059437 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.39403476 03 | | | | | | | |
| 0.98076946 03 | -0.41209876 03 | 0.99009016 03 | 335.374 | 335.374 | 1.000000 | 1 | 5.848 |
| -0.28582396 03 | 0.84174616 03 | 0.88249176 03 | 107.477 | 53.738 | 0.890595 | 2 | 11.696 |
| -0.84858286 03 | -0.26522806 02 | 0.84000106 03 | 181.808 | 60.603 | 0.848531 | 3 | 17.544 |
| 0.28131596 03 | -0.27271616 03 | 0.39180646 03 | 315.889 | 78.972 | 0.395489 | 4 | 23.392 |
| -0.71878326 03 | -0.75052476 00 | 0.71878346 03 | 180.060 | 36.012 | 0.725392 | 5 | 29.240 |
| 0.99912006 02 | 0.30887406 02 | 0.10721396 03 | 21.267 | 3.544 | 0.108199 | 6 | 35.088 |
| -0.93858136 01 | 0.26959106 02 | 0.28520006 02 | 109.044 | 15.578 | 0.028782 | 7 | 40.936 |
| -0.56351006 02 | 0.20131406 01 | 0.56386096 02 | 177.934 | 22.244 | 0.056905 | 8 | 46.784 |
| -0.33273626 02 | -0.09952046 01 | 0.34543756 02 | 195.784 | 21.765 | 0.034882 | 9 | 52.632 |
| -0.23702626 02 | -0.30992236 02 | 0.46110566 02 | 239.067 | 23.907 | 0.046535 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.36006026 03 | | | | | | | |
| 0.10505306 04 | -0.10446146 04 | 0.14814256 04 | 315.165 | 315.165 | 1.000000 | 1 | 5.848 |
| -0.27739046 02 | 0.81540976 03 | 0.81596126 03 | 91.948 | 45.974 | 0.550795 | 2 | 11.696 |
| -0.69461526 03 | 0.45838306 03 | 0.82785016 03 | 147.041 | 49.014 | 0.558820 | 3 | 17.544 |
| -0.11669146 03 | -0.29006666 03 | 0.31301496 03 | 248.120 | 62.030 | 0.211293 | 4 | 23.392 |
| 0.31471996 03 | -0.67831426 01 | 0.31679206 03 | 358.773 | 71.755 | 0.213843 | 5 | 29.240 |
| 0.72505006 01 | 0.37479456 02 | 0.38170386 02 | 79.050 | 13.179 | 0.025766 | 6 | 35.088 |
| 0.28973296 03 | -0.14237116 03 | 0.32282286 03 | 333.831 | 47.690 | 0.217914 | 7 | 40.936 |
| -0.19963096 03 | 0.19445896 03 | 0.27442116 03 | 134.878 | 16.860 | 0.185241 | 8 | 46.784 |
| -0.42043016 02 | 0.44517216 02 | 0.61232736 02 | 133.363 | 14.818 | 0.041334 | 9 | 52.632 |
| -0.22432906 02 | 0.22206896 02 | 0.31565596 02 | 135.290 | 13.529 | 0.021308 | 10 | 58.480 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 31

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 10 PL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8668398E 03 | | | | | | | |
| 0.7100644E 03 | -0.1040522E 04 | 0.1259714E 04 | 304.310 | 304.310 | 1.000000 | 1 | 5.848 |
| -0.1361719E 02 | 0.3443618E 03 | 0.3446106E 03 | 92.265 | 44.132 | 0.273562 | 2 | 11.696 |
| -0.4053486E 03 | 0.8337300E 03 | 0.7522069E 03 | 122.604 | 40.868 | 0.597187 | 3 | 17.544 |
| -0.3357273E 03 | -0.3865552E 02 | 0.3379451E 03 | 186.568 | 46.642 | 0.268271 | 4 | 23.392 |
| 0.6415608E 03 | -0.4807288E 02 | 0.6932299E 03 | 356.023 | 71.205 | 0.550307 | 5 | 29.240 |
| -0.1076668E 03 | -0.1039913E 03 | 0.1496874E 03 | 224.005 | 37.334 | 0.118826 | 6 | 35.088 |
| -0.3779077E 02 | -0.1304831E 02 | 0.4187956E 02 | 198.156 | 28.308 | 0.033242 | 7 | 40.936 |
| 0.3625085E 02 | -0.7286104E 02 | 0.8086975E 02 | 296.710 | 37.089 | 0.064208 | 8 | 46.784 |
| 0.1023196E 02 | -0.4821811E 02 | 0.6279085E 02 | 309.841 | 34.427 | 0.049851 | 9 | 52.632 |
| 0.9549979E 02 | 0.3245351E 01 | 0.5590457E 02 | 3.347 | 0.335 | 0.044133 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 11 PL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7544170E 03 | | | | | | | |
| 0.3584507E 03 | -0.8370947E 03 | 0.9108121E 03 | 293.181 | 293.181 | 1.000000 | 1 | 5.848 |
| -0.9942551E 02 | 0.9907166E 01 | 0.9993837E 02 | 174.873 | 87.036 | 0.109756 | 2 | 11.696 |
| -0.1308506E 03 | 0.5878599E 03 | 0.6022466E 03 | 102.549 | 34.183 | 0.661365 | 3 | 17.544 |
| -0.4171804E 03 | 0.1971956E 03 | 0.4614305E 03 | 154.701 | 38.675 | 0.506734 | 4 | 23.392 |
| 0.7026948E 03 | -0.7297586E 01 | 0.7027327E 03 | 359.405 | 71.881 | 0.771715 | 5 | 29.240 |
| -0.2388867E 03 | -0.1814022E 03 | 0.2999558E 03 | 217.212 | 36.202 | 0.329460 | 6 | 35.088 |
| -0.3141780E 09 | 0.3788763E 02 | 0.3164539E 03 | 173.124 | 24.732 | 0.347518 | 7 | 40.936 |
| 0.2280231E 03 | -0.2588037E 03 | 0.3398407E 03 | 310.447 | 38.806 | 0.372441 | 8 | 46.784 |
| 0.4043729E 02 | -0.1137451E 03 | 0.1207191E 03 | 289.571 | 32.174 | 0.132549 | 9 | 52.632 |
| 0.5221962E 02 | -0.3713220E 02 | 0.6407567E 02 | 324.504 | 32.458 | 0.070365 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 13 PL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.3861177E 03 | | | | | | | |
| 0.1044023E 03 | -0.5035659E 03 | 0.5147422E 03 | 281.961 | 281.961 | 0.797316 | 1 | 5.848 |
| -0.1062369E 03 | -0.2624453E 03 | 0.3180438E 03 | 237.649 | 118.825 | 0.457865 | 2 | 11.696 |
| 0.5854057E 02 | 0.4380454E 03 | 0.4419395E 03 | 82.388 | 27.463 | 0.650205 | 3 | 17.544 |
| -0.3388838E 03 | 0.2286650E 03 | 0.4088152E 03 | 145.930 | 36.498 | 0.601471 | 4 | 23.392 |
| 0.6793032E 03 | 0.7712054E 02 | 0.6796924E 03 | 6.519 | 1.303 | 1.000000 | 5 | 29.240 |
| -0.3327251E 03 | -0.1717416E 03 | 0.3744343E 03 | 207.301 | 34.550 | 0.550888 | 6 | 35.088 |
| -0.4827384E 03 | -0.6263101E 02 | 0.4866783E 03 | 187.392 | 26.770 | 0.716183 | 7 | 40.936 |
| 0.3707373E 03 | -0.3168818E 03 | 0.4949337E 03 | 320.163 | 40.020 | 0.727585 | 8 | 46.784 |
| 0.1574809E 02 | -0.1215208E 03 | 0.1225378E 03 | 277.304 | 30.820 | 0.180283 | 9 | 52.632 |
| 0.3574684E 02 | -0.8330754E 02 | 0.9065309E 02 | 293.224 | 29.322 | 0.133374 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 14 PL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4650933E 03 | | | | | | | |
| -0.4463307E 02 | -0.4044961E 03 | 0.4069509E 03 | 263.703 | 263.703 | 0.706714 | 1 | 5.848 |
| -0.8165147E 02 | -0.3287961E 03 | 0.3387827E 03 | 256.053 | 128.027 | 0.588033 | 2 | 11.696 |
| 0.1516351E 03 | 0.2943869E 03 | 0.3314109E 03 | 62.771 | 20.924 | 0.575531 | 3 | 17.544 |
| -0.1816029E 03 | 0.1725852E 03 | 0.2505299E 03 | 136.458 | 34.115 | 0.435072 | 4 | 23.392 |
| 0.5702380E 03 | 0.8009331E 02 | 0.5758352E 03 | 7.995 | 1.599 | 1.000000 | 5 | 29.240 |
| -0.3036360E 03 | -0.7118457E 02 | 0.3118684E 03 | 193.196 | 32.199 | 0.541593 | 6 | 35.088 |
| -0.4527075E 02 | -0.5883430E 02 | 0.4565144E 03 | 187.405 | 26.772 | 0.792787 | 7 | 40.936 |
| 0.3454868E 03 | -0.3385581E 03 | 0.4837175E 03 | 315.580 | 39.448 | 0.840028 | 8 | 46.784 |
| -0.3199242E 02 | -0.7673376E 02 | 0.8313993E 02 | 247.367 | 27.485 | 0.144374 | 9 | 52.632 |
| 0.7231906E 01 | -0.1322620E 03 | 0.1324590E 03 | 273.129 | 27.313 | 0.230880 | 10 | 58.480 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 31

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 1 CH. BEND 5

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1352820E 05 | | | | | | | |
| -0.6132078E 04 | 0.5362991E 05 | 0.5397935E 05 | 96.523 | 96.523 | 1.000000 | 1 | 5.848 |
| 0.2930201E 04 | -0.1736333E 04 | 0.3406014E 04 | 329.350 | 164.675 | 0.063098 | 2 | 11.696 |
| -0.3238574E 03 | -0.7158921E 03 | 0.7857385E 03 | 245.659 | 81.886 | 0.014556 | 3 | 17.544 |
| 0.2527753E 03 | 0.2522909E 03 | 0.3571357E 03 | 44.945 | 11.236 | 0.006616 | 4 | 23.392 |
| 0.1513680E 04 | 0.2009387E 04 | 0.2515723E 04 | 53.009 | 10.602 | 0.046605 | 5 | 29.240 |
| -0.1118105E 04 | -0.8179080E 03 | 0.1385327E 04 | 216.186 | 36.031 | 0.025664 | 6 | 35.088 |
| 0.6252956E 02 | -0.3951426E 03 | 0.4000593E 03 | 278.992 | 39.856 | 0.007411 | 7 | 40.936 |
| -0.5752874E 03 | 0.1817529E 02 | 0.5755742E 03 | 178.190 | 22.274 | 0.010663 | 8 | 46.784 |
| 0.1553165E 04 | 0.1110564E 04 | 0.1909354E 04 | 35.566 | 3.952 | 0.035372 | 9 | 52.632 |
| -0.7093771E 02 | 0.8361362E 03 | 0.8391369E 03 | 94.849 | 9.485 | 0.015546 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1736983E 05 | | | | | | | |
| -0.3917444E 04 | 0.3346[illegible]06E 05 | 0.3364668E 05 | 96.686 | 96.686 | 1.000000 | 1 | 5.848 |
| 0.1963976E 04 | -0.1570[illegible] 04 | 0.2514836E 04 | 321.348 | 160.674 | 0.074742 | 2 | 11.696 |
| 0.8004558E 03 | 0.2055976[illegible] 04 | 0.2240524E 04 | 66.582 | 22.194 | 0.066590 | 3 | 17.544 |
| 0.2782307E 03 | 0.4648320E 03 | 0.5417388E 03 | 59.097 | 14.774 | 0.016101 | 4 | 23.392 |
| 0.6672612E 03 | -0.4980872E 03 | 0.8326633E 03 | 323.260 | 64.652 | 0.024747 | 5 | 29.240 |
| -0.2715984E 03 | -0.1358671E 03 | 0.3036509E 03 | 206.580 | 34.430 | 0.009025 | 6 | 35.088 |
| 0.2652373E 03 | 0.1340448E 02 | 0.2655796E 03 | 2.910 | 0.416 | 0.007893 | 7 | 40.936 |
| 0.2271804E 03 | 0.3189058E 03 | 0.3915503E 03 | 54.535 | 6.817 | 0.011637 | 8 | 46.784 |
| -0.2000431E 03 | -0.4241023E 03 | 0.4728230E 03 | 243.761 | 27.085 | 0.014053 | 9 | 52.632 |
| 0.5737770E 02 | 0.8327408E 02 | 0.1011275E 03 | 55.432 | 5.543 | 0.003006 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8322500E 04 | | | | | | | |
| -0.1627153E 04 | 0.1457875E 05 | 0.1466927E 05 | 96.369 | 96.369 | 1.000000 | 1 | 5.848 |
| 0.5476760E 03 | -0.1222138E 04 | 0.1339242E 04 | 294.138 | 147.069 | 0.091296 | 2 | 11.696 |
| 0.8186582E 03 | 0.7232400E 03 | 0.1092372E 04 | 41.459 | 13.820 | 0.074467 | 3 | 17.544 |
| 0.8540010E 03 | 0.4611072E 03 | 0.9705344E 03 | 28.366 | 7.092 | 0.066161 | 4 | 23.392 |
| -0.4856533E 03 | -0.6691682E 03 | 0.8268284E 03 | 234.029 | 46.806 | 0.056365 | 5 | 29.240 |
| 0.3974932E 03 | -0.7828819E 02 | 0.4051292E 03 | 348.858 | 58.143 | 0.027618 | 6 | 35.088 |
| -0.6425726E 02 | 0.5367200E 03 | 0.5405605E 03 | 96.827 | 13.832 | 0.036850 | 7 | 40.936 |
| 0.6090952E 03 | -0.9055750E 02 | 0.6165417E 03 | 351.554 | 43.944 | 0.042029 | 8 | 46.784 |
| -0.1978418E 04 | -0.3238225E 03 | 0.2002770E 04 | 189.305 | 21.034 | 0.136528 | 9 | 52.632 |
| -0.3105828E 03 | -0.5810249E 03 | 0.5894807E 03 | 238.205 | 23.821 | 0.040185 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 12 CH. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6303113E 04 | | | | | | | |
| -0.9135945E 03 | 0.5929677E 04 | 0.5999441E 04 | 98.759 | 98.759 | 1.000000 | 1 | 5.848 |
| 0.8711967E 02 | -0.8272378E 03 | 0.8318125E 03 | 276.012 | 138.006 | 0.138648 | 2 | 11.696 |
| 0.6112632E 03 | 0.2445681E 03 | 0.6583738E 03 | 21.806 | 7.269 | 0.109739 | 3 | 17.544 |
| 0.3924250E 03 | 0.1209984E 03 | 0.4106548E 03 | 17.136 | 4.284 | 0.068449 | 4 | 23.392 |
| -0.2646748E 03 | -0.4609985E 03 | 0.5315752E 03 | 240.138 | 48.028 | 0.088604 | 5 | 29.240 |
| 0.2258551E 03 | -0.8879605E 02 | 0.2426835E 03 | 338.537 | 56.423 | 0.040451 | 6 | 35.088 |
| 0.7603754E 02 | 0.2912971E 03 | 0.3010574E 03 | 75.370 | 10.767 | 0.050181 | 7 | 40.936 |
| 0.3923489E 03 | -0.5882735E 02 | 0.3956272E 03 | 352.619 | 44.077 | 0.065944 | 8 | 46.784 |
| -0.1351952E 04 | -0.2529135E 03 | 0.1375405E 04 | 190.596 | 21.177 | 0.229255 | 9 | 52.632 |
| -0.1534709E 03 | -0.2240161E 03 | 0.2715498E 03 | 235.584 | 23.558 | 0.045263 | 10 | 58.480 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 31

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.16841096 03 | | | | | | | |
| 0.13332206 03 | -0.20001016 03 | 0.24037226 03 | 303.687 | 303.687 | 0.859422 | 1 | 5.848 |
| 0.33621056 02 | 0.19919366 03 | 0.20201106 03 | 80.420 | 40.210 | 0.722266 | 2 | 11.696 |
| -0.27994356 03 | 0.90713576 01 | 0.27986046 03 | 178.141 | 99.380 | 1.000000 | 3 | 17.544 |
| 0.97191246 02 | 0.98231066 02 | 0.13818046 03 | 45.305 | 11.326 | 0.494089 | 4 | 23.392 |
| 0.21544516 03 | -0.57307566 02 | 0.22293646 03 | 345.104 | 69.021 | 0.797083 | 5 | 29.240 |
| -0.78317436 02 | -0.11380786 03 | 0.13819156 03 | 235.466 | 39.244 | 0.493944 | 6 | 35.088 |
| 0.79614266 02 | -0.90357576 02 | 0.12042816 03 | 311.383 | 44.483 | 0.430576 | 7 | 40.936 |
| 0.58894126 02 | 0.19973856 03 | 0.20607126 03 | 75.750 | 9.470 | 0.736782 | 8 | 46.784 |
| -0.72146596 02 | 0.13855336 03 | 0.15821146 03 | 117.507 | 13.056 | 0.558517 | 9 | 52.632 |
| 0.11793796 01 | 0.41422006 02 | 0.41438776 02 | 88.369 | 8.837 | 0.148159 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.53312386 02 | | | | | | | |
| 0.17864006 02 | -0.36119806 02 | 0.48298146 02 | 296.322 | 296.322 | 0.232425 | 1 | 5.848 |
| 0.84452036 02 | 0.48799406 02 | 0.97773646 02 | 25.764 | 12.882 | 0.468853 | 2 | 11.696 |
| -0.98656306 02 | 0.90634 786 02 | 0.13396916 03 | 137.427 | 45.809 | 0.772685 | 3 | 17.544 |
| -0.68191076 02 | -0.49856496 02 | 0.82179636 02 | 213.920 | 53.480 | 0.473060 | 4 | 23.392 |
| 0.15933696 03 | -0.68357576 02 | 0.17338116 03 | 336.780 | 67.356 | 1.000000 | 5 | 29.240 |
| -0.16207436 02 | 0.67367876 02 | 0.69289216 02 | 103.527 | 17.255 | 0.399635 | 6 | 35.088 |
| -0.56968376 02 | -0.47073366 02 | 0.73988566 02 | 219.567 | 31.367 | 0.426232 | 7 | 40.936 |
| 0.98057506 02 | 0.18809766 00 | 0.98057666 02 | 0.110 | 0.014 | 0.565561 | 8 | 46.784 |
| -0.38596216 02 | 0.98154136 02 | 0.10546996 03 | 111.466 | 12.385 | 0.608312 | 9 | 52.632 |
| -0.64358126 02 | 0.10209726 02 | 0.65162896 02 | 170.986 | 17.099 | 0.375836 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.95226396 02 | | | | | | | |
| -0.66114266 02 | 0.19735886 03 | 0.20813846 03 | 108.521 | 108.521 | 1.000000 | 1 | 5.848 |
| 0.47408516 02 | -0.66644476 02 | 0.81786616 02 | 305.427 | 152.713 | 0.392943 | 2 | 11.696 |
| 0.11563696 03 | 0.13619796 02 | 0.11643626 03 | 6.717 | 2.239 | 0.559417 | 3 | 17.544 |
| -0.34646616 02 | -0.10297616 03 | 0.10866466 03 | 251.407 | 62.852 | 0.521991 | 4 | 23.392 |
| 0.14964916 02 | -0.94471776 01 | 0.17360466 02 | 327.031 | 65.406 | 0.083408 | 5 | 29.240 |
| -0.12189476 02 | 0.33664326 02 | 0.35803196 02 | 109.905 | 18.317 | 0.172016 | 6 | 35.088 |
| 0.90852326 01 | -0.36364346 01 | 0.12559136 02 | 316.451 | 45.207 | 0.060225 | 7 | 40.936 |
| 0.90173816 01 | 0.10490846 02 | 0.13833386 02 | 49.318 | 6.165 | 0.066462 | 8 | 46.784 |
| -0.14350926 02 | 0.12343866 02 | 0.18929346 02 | 139.300 | 15.478 | 0.090946 | 9 | 52.632 |
| -0.16314476 02 | 0.14364726 01 | 0.16377986 02 | 174.948 | 17.497 | 0.078686 | 10 | 58.480 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 500 CTR 570 CR 40.0 TR 34 BLADE ANGL

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.33352936 01 | | | | | | | |
| 0.10846596 01 | -0.11065796 01 | 0.15495166 01 | 314.427 | 314.427 | 1.000000 | 1 | 5.848 |
| -0.36691786-01 | 0.35941786-01 | 0.51298176-01 | 135.781 | 67.761 | 0.033106 | 2 | 11.696 |
| -0.11477786 00 | -0.42535046- | 0.12240576 00 | 200.334 | 66.778 | 0.078996 | 3 | 17.544 |
| 0.16107846 00 | 0.25873316 00 | 0.30477716 00 | 58.095 | 14.524 | 0.196692 | 4 | 23.392 |
| -0.60289756-01 | 0.17241696-01 | 0.62706656-01 | 164.041 | 32.808 | 0.040469 | 5 | 29.240 |
| 0.19411676-01 | -0.10436966-01 | 0.22039386-01 | 331.736 | 55.289 | 0.014223 | 6 | 35.088 |
| -0.44229806-02 | -0.49212906-02 | 0.66161496-02 | 228.058 | 32.580 | 0.004270 | 7 | 40.936 |
| -0.12480976-01 | -0.62591376-01 | 0.63823566-01 | 258.723 | 32.340 | 0.041189 | 8 | 46.784 |
| 0.18051156-01 | -0.64928116-01 | 0.67390626-01 | 285.537 | 31.726 | 0.043491 | 9 | 52.632 |
| 0.78866876-03 | -0.19249766-01 | 0.19265576-01 | 272.322 | 27.232 | 0.012433 | 10 | 58.480 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 33

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2629859E 05 | | | | | | | |
| 0.1978177E 04 | 0.1817619E 04 | 0.2224574E 04 | 27.222 | 27.222 | 0.540142 | 1 | 5.882 |
| -0.5309172E 03 | -0.4084137E 04 | 0.4118494E 04 | 262.593 | 131.297 | 1.000000 | 2 | 11.765 |
| 0.1835378E 04 | -0.3560359E 03 | 0.1869592E 04 | 349.022 | 116.341 | 0.453950 | 3 | 17.647 |
| -0.4228538E 03 | 0.2784982E 03 | 0.5063220E 03 | 146.631 | 36.658 | 0.122939 | 4 | 23.529 |
| 0.6594498E 03 | -0.4066877E 03 | 0.7744971E 03 | 328.377 | 65.675 | 0.188053 | 5 | 29.412 |
| 0.1449121E 02 | 0.5900850E 02 | 0.6161871E 02 | 76.398 | 12.733 | 0.014961 | 6 | 35.294 |
| 0.1109569E 03 | 0.4828233E 01 | 0.1170565E 03 | 2.364 | 0.338 | 0.028422 | 7 | 41.176 |
| -0.1106690E 03 | 0.2786284E 02 | 0.1140527E 03 | 166.557 | 20.820 | 0.029101 | 8 | 47.059 |
| -0.5697747E 02 | -0.1435330E 02 | 0.5836974E 02 | 194.235 | 21.582 | 0.014173 | 9 | 52.941 |
| 0.5317209E 02 | 0.4695149E 02 | 0.7093454E 02 | 41.445 | 4.144 | 0.017223 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1819029E 04 | | | | | | | |
| 0.9228506E 03 | 0.8127901E 02 | 0.9264224E 03 | 5.033 | 5.033 | 1.000000 | 1 | 5.882 |
| -0.8482605E 02 | -0.7390660E 02 | 0.1125590E 03 | 221.096 | 110.548 | 0.121408 | 2 | 11.765 |
| -0.7186299E 02 | -0.4178967E 02 | 0.8242983E 02 | 210.446 | 70.149 | 0.088976 | 3 | 17.647 |
| 0.1473634E 03 | 0.2502866E 02 | 0.1490867E 03 | 9.938 | 2.482 | 0.161785 | 4 | 23.529 |
| -0.1730394E 03 | 0.1696162E 03 | 0.2421662E 03 | 135.696 | 27.121 | 0.261399 | 5 | 29.412 |
| 0.2284207E 02 | -0.1690185E 02 | 0.2817926E 02 | 324.154 | 54.026 | 0.030417 | 6 | 35.294 |
| -0.8957687E 02 | 0.9826498E 02 | 0.9752985E 02 | 148.974 | 21.282 | 0.105276 | 7 | 41.176 |
| 0.9943987E 02 | -0.3704059E 01 | 0.9958879E 02 | 357.864 | 44.733 | 0.107412 | 8 | 47.059 |
| 0.2042445E 02 | -0.7051988E 01 | 0.2160757E 02 | 340.952 | 37.884 | 0.023324 | 9 | 52.941 |
| -0.3694286E 02 | -0.2927804E 02 | 0.4666468E 02 | 218.848 | 21.885 | 0.050371 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2594599E 03 | | | | | | | |
| 0.7560558E 03 | -0.4567089E 03 | 0.8858108E 03 | 328.781 | 328.781 | 1.000000 | 1 | 5.882 |
| -0.1170649E 03 | 0.4237409E 03 | 0.4396426E 03 | 105.443 | 52.722 | 0.496786 | 2 | 11.765 |
| -0.2106937E 03 | 0.3856908E 02 | 0.2220687E 03 | 169.998 | 56.666 | 0.250922 | 3 | 17.647 |
| 0.4446671E 02 | -0.2041108E 02 | 0.4892598E 02 | 335.342 | 83.836 | 0.055283 | 4 | 23.529 |
| -0.1116009E 03 | 0.1332575E 03 | 0.1738681E 03 | 129.966 | 25.993 | 0.196459 | 5 | 29.412 |
| -0.2083444E 02 | 0.1983209E 02 | 0.3336758E 02 | 143.934 | 23.922 | 0.037703 | 6 | 35.294 |
| 0.1387119E 01 | 0.1089327E 02 | 0.1998166E 02 | 86.803 | 12.286 | 0.022587 | 7 | 41.176 |
| -0.1240259E 02 | -0.4656798E 00 | 0.1241133E 02 | 182.190 | 22.769 | 0.014024 | 8 | 47.059 |
| 0.8998220E 01 | -0.6098390E 01 | 0.1136369E 02 | 322.292 | 39.810 | 0.012840 | 9 | 52.941 |
| -0.9404219E 01 | 0.6421309E 01 | 0.7767860E 01 | 117.930 | 11.793 | 0.008212 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL SM-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7689103E 03 | | | | | | | |
| 0.8857944E 03 | -0.7901387E 03 | 0.1186992E 04 | 318.267 | 318.267 | 1.000000 | 1 | 5.882 |
| -0.4911780E 02 | 0.4904119E 03 | 0.4928652E 03 | 95.720 | 47.860 | 0.415222 | 2 | 11.765 |
| -0.4018009E 03 | 0.1361517E 03 | 0.2434429E 03 | 145.994 | 48.665 | 0.205092 | 3 | 17.647 |
| -0.1990683E 02 | -0.3111481E 02 | 0.4394808E 02 | 225.145 | 56.286 | 0.037025 | 4 | 23.529 |
| 0.1299306E 02 | -0.2747809E 02 | 0.3822610E 02 | 294.622 | 58.924 | 0.029465 | 5 | 29.412 |
| -0.3260582E 02 | 0.2367873E 02 | 0.4029866E 02 | 144.012 | 24.002 | 0.033940 | 6 | 35.294 |
| 0.3701463E 02 | -0.8031120E 01 | 0.3787630E 02 | 347.795 | 49.679 | 0.031900 | 7 | 41.176 |
| -0.5083279E 02 | -0.1829384E 02 | 0.5402440E 02 | 199.793 | 24.974 | 0.045514 | 8 | 47.059 |
| -0.2918402E 02 | -0.2000357E 02 | 0.3974403E 02 | 222.736 | 24.751 | 0.033465 | 9 | 52.941 |
| 0.1320967E 02 | -0.7816188E 01 | 0.1541774E 02 | 329.539 | 32.954 | 0.012989 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 33

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 490 CTR 250 CR 32.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1282567E 04 | | | | | | | |
| 0.6349998E 03 | -0.7517043E 03 | 0.9840142E 03 | 310.189 | 310.189 | 1.000000 | 1 | 5.882 |
| -0.1424540E 01 | 0.3438047E 03 | 0.3438069E 03 | 90.237 | 45.116 | 0.349392 | 2 | 11.765 |
| -0.8529340E 02 | 0.2682134E 03 | 0.2814485E 03 | 107.641 | 35.880 | 0.286021 | 3 | 17.647 |
| -0.6913400E 02 | 0.7355177E 01 | 0.6954796E 02 | 173.557 | 43.389 | 0.066613 | 4 | 23.529 |
| 0.9428737E 02 | -0.1549511E 03 | 0.1810418E 03 | 301.386 | 60.277 | 0.183983 | 5 | 29.412 |
| 0.3215199E 02 | -0.4541293E 02 | 0.5564747E 02 | 305.298 | 50.883 | 0.056546 | 6 | 35.294 |
| -0.1074470E 02 | -0.2226434E 02 | 0.2450826E 02 | 245.241 | 35.042 | 0.024906 | 7 | 41.176 |
| 0.3597014E 02 | -0.2290181E 02 | 0.4264203E 02 | 327.515 | 40.939 | 0.043335 | 8 | 47.059 |
| 0.9954630E 00 | 0.2461161E 01 | 0.2654853E 01 | 67.970 | 7.553 | 0.002698 | 9 | 52.941 |
| -0.1707671E 02 | -0.2114973E 02 | 0.2718317E 02 | 231.082 | 23.108 | 0.027625 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 490 CTR 250 CR 32.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1244417E 04 | | | | | | | |
| 0.4139561E 03 | -0.6847695E 03 | 0.7928748E 03 | 304.391 | 304.391 | 1.000000 | 1 | 5.882 |
| 0.1561956E 02 | 0.1926692E 03 | 0.1933013E 03 | 85.365 | 42.683 | 0.243758 | 2 | 11.765 |
| 0.9277094E 02 | 0.3080977E 01 | 0.3217615E 03 | 73.242 | 24.414 | 0.405840 | 3 | 17.647 |
| -0.3248631E 02 | 0.8C80630E 02 | 0.9550144E 02 | 107.887 | 27.472 | 0.120411 | 4 | 23.529 |
| 0.1008618E 03 | -0.2275627E 03 | 0.2469134E 03 | 293.904 | 58.781 | 0.311440 | 5 | 29.412 |
| 0.4171429E 02 | -0.9444947E 02 | 0.1032518E 03 | 293.829 | 48.971 | 0.130285 | 6 | 35.294 |
| -0.2238127E 02 | 0.1264238E 02 | 0.2560728E 02 | 150.929 | 21.561 | 0.032301 | 7 | 41.176 |
| 0.5799078E 02 | 0.2738694E 01 | 0.5802444E 02 | 2.705 | 0.338 | 0.C73174 | 8 | 47.059 |
| 0.7209995E 02 | 0.1256117E 01 | 0.2213521E 02 | 3.253 | 0.361 | 0.030203 | 9 | 52.941 |
| -0.1105707E 02 | 0.2159990E 02 | 0.2426549E 02 | 117.1C8 | 11.711 | 0.03111C | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 490 CTR 250 CR 32.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1023482E 04 | | | | | | | |
| 0.1126953E 03 | -0.2896948E 03 | 0.3108428E 03 | 291.257 | 291.257 | 0.989797 | 1 | 5.882 |
| 0.6861936E 01 | 0.1639117E 02 | 0.1747620E 02 | 69.784 | 34.892 | 0.051151 | 2 | 11.765 |
| 0.1813760E 03 | 0.2895437E 03 | 0.3416616E 03 | 57.936 | 19.312 | 1.000000 | 3 | 17.647 |
| -0.6006170E 02 | 0.1817397E 03 | 0.1840663E 03 | 110.531 | 27.633 | 0.538007 | 4 | 23.529 |
| 0.5177768E 02 | -0.1773609E 03 | 0.1847642E 03 | 286.274 | 57.255 | 0.540781 | 5 | 29.412 |
| 0.9981622E 02 | -0.6963167E 02 | 0.8826341E 02 | 311.962 | 51.994 | 0.258136 | 6 | 35.294 |
| -0.4292521E 02 | 0.3521334E 02 | 0.5521208E 02 | 140.373 | 20.053 | 0.161999 | 7 | 41.176 |
| 0.8148030E 02 | 0.7665181E 02 | 0.1118941E 03 | 43.243 | 5.405 | 0.327383 | 8 | 47.059 |
| 0.2402597E 02 | 0.3907131E 02 | 0.4702132E 02 | 57.988 | 6.443 | 0.137625 | 9 | 52.941 |
| -0.2854553E 01 | 0.2153133E 02 | 0.2171971E 02 | 97.552 | 9.755 | 0.063571 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 490 CTR 250 CR 32.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8457141E 03 | | | | | | | |
| -0.1736915E 02 | -0.1211943E 03 | 0.1208838E 03 | 252.777 | 252.777 | 0.450757 | 1 | 5.882 |
| -0.4814476E 02 | -0.4303766E 02 | 0.6457674E 02 | 221.794 | 110.897 | 0.224488 | 2 | 11.765 |
| 0.2288975E 03 | 0.1744941E 03 | 0.2819027E 03 | 38.356 | 12.769 | 1.000000 | 3 | 17.647 |
| -0.1888293E 02 | 0.1893971E 03 | 0.1897009E 03 | 93.809 | 23.522 | 0.673017 | 4 | 23.529 |
| 0.2272278E 01 | -0.9294221E 02 | 0.9296096E 02 | 271.488 | 54.280 | 0.330263 | 5 | 29.412 |
| 0.3596219E 02 | -0.7268249E 02 | 0.8104484E 02 | 296.287 | 49.381 | 0.287976 | 6 | 35.294 |
| -0.2098877E 02 | 0.7353011E 02 | 0.7644708E 02 | 105.931 | 15.133 | 0.271639 | 7 | 41.176 |
| 0.6189165E 02 | 0.1087207E 03 | 0.1102164E 03 | 58.430 | 7.304 | 0.419949 | 8 | 47.059 |
| 0.1512688E 02 | 0.1867614E 02 | 0.2357051E 02 | 50.076 | 5.564 | 0.089791 | 9 | 52.941 |
| -0.6604959E 01 | 0.4464439E 02 | 0.4710965E 02 | 98.060 | 9.806 | 0.167351 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 33

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2348764E 04 | | | | | | | |
| 0.4339078E 04 | 0.2465698E 05 | 0.2498362E 05 | 81.390 | 81.350 | 1.000000 | 1 | 5.882 |
| -0.4195461E 04 | 0.2274121E 04 | 0.4737027E 04 | 151.310 | 75.655 | 0.163438 | 2 | 11.765 |
| -0.5231506E 03 | -0.9058130E 03 | 0.1046032E 04 | 239.991 | 79.997 | 0.036090 | 3 | 17.647 |
| 0.1471778E 03 | 0.2391987E 03 | 0.2808508E 03 | 58.396 | 14.599 | 0.009690 | 4 | 23.529 |
| 0.4098443E 03 | -0.1539054E 01 | 0.4096670E 03 | 359.785 | 71.957 | 0.014134 | 5 | 29.412 |
| -0.3197557E 02 | -0.4262445E 02 | 0.5328490E 02 | 233.124 | 38.854 | 0.001838 | 6 | 35.294 |
| -0.4237242E 02 | 0.4973805E 01 | 0.4266333E 02 | 173.305 | 24.759 | 0.001472 | 7 | 41.176 |
| -0.1403132E 03 | 0.1061469E 03 | 0.1759402E 03 | 142.893 | 17.862 | 0.006070 | 8 | 47.059 |
| 0.1915316E 02 | 0.5066740E 02 | 0.5418083E 02 | 69.253 | 7.695 | 0.001869 | 9 | 52.941 |
| 0.3915207E 02 | 0.1928635E 02 | 0.4364455E 02 | 26.225 | 2.622 | 0.001506 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1186C90E 05 | | | | | | | |
| 0.1932042E 04 | 0.1741309F 05 | 0.1751994E 05 | 83.669 | 83.669 | 1.000000 | 1 | 5.882 |
| -0.2543305E 04 | 0.1614271E 04 | 0.3013426E 04 | 147.564 | 73.782 | 0.172000 | 2 | 11.765 |
| -0.1687?30E 03 | -0.3556191E 03 | 0.3934431E 03 | 244.671 | 81.557 | 0.022457 | 3 | 17.647 |
| 0.2364527E 03 | 0.3680576E 03 | 0.4374656E 03 | 57.282 | 14.320 | 0.024970 | 4 | 23.529 |
| 0.6261154E 02 | -0.1764006E 03 | 0.1947867E 03 | 295.094 | 59.019 | 0.011118 | 5 | 29.412 |
| -0.5310006E 02 | 0.9539005E 02 | 0.1092186E 03 | 119.145 | 19.857 | 0.006234 | 6 | 35.294 |
| 0.8541612E 02 | 0.1049763E 03 | 0.1353364E 03 | 50.866 | 7.267 | 0.007725 | 7 | 41.176 |
| -0.3812022E 02 | 0.5660265E 02 | 0.6824226E 02 | 123.959 | 15.495 | 0.003895 | 8 | 47.059 |
| 0.5375879E 02 | -0.8985154E 01 | 0.5458449E 02 | 350.911 | 38.944 | 0.003111 | 9 | 52.941 |
| 0.6045187E 02 | -0.4266969E 02 | 0.7399411E 02 | 324.784 | 32.478 | 0.004223 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 8 CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1083907E 05 | | | | | | | |
| 0.5292776E 03 | 0.6992434E 04 | 0.7012434E 04 | 85.671 | 85.671 | 1.000000 | 1 | 5.882 |
| -0.6783337F 03 | 0.8197829E 03 | 0.1063978E 04 | 129.609 | 64.805 | 0.151727 | 2 | 11.765 |
| -0.1768?14E 03 | -0.1584252E 03 | 0.2368017E 03 | 221.992 | 73.997 | 0.033769 | 3 | 17.647 |
| 0.4113010E 03 | 0.3135229E 03 | 0.5171702E 03 | 37.317 | 9.329 | 0.073756 | 4 | 23.529 |
| -0.9574039E 02 | 0.1716547E 02 | 0.5833653E 02 | 162.869 | 32.574 | 0.008319 | 5 | 29.412 |
| -0.1873493E 03 | 0.1118045E 03 | 0.2178062E 03 | 149.335 | 24.889 | 0.031060 | 6 | 35.294 |
| 0.1808332E 03 | 0.7536479E 02 | 0.1959094E 03 | 22.625 | 3.232 | 0.027937 | 7 | 41.176 |
| 0.1464530E 03 | 0.3435405E 02 | 0.1584203E 03 | 13.201 | 1.650 | 0.021492 | 8 | 47.059 |
| 0.10?..204E 02 | -0.7189929E 02 | 0.7269139E 02 | 278.466 | 38.941 | 0.010366 | 9 | 52.941 |
| -0.8925092E 02 | -0.1664972E 03 | 0.1889101E 03 | 241.886 | 24.181 | 0.026939 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 12 CH. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9922986E 04 | | | | | | | |
| -0.6609167E 02 | 0.2799090E 04 | 0.2799860E 04 | 91.353 | 91.353 | 1.000000 | 1 | 5.882 |
| -0.2161289E 03 | 0.3229524E 03 | 0.3889338E 03 | 123.863 | 61.933 | 0.138912 | 2 | 11.765 |
| 0.9630042E 01 | -0.7021533E 02 | 0.7084677E 02 | 277.656 | 92.552 | 0.025304 | 3 | 17.647 |
| 0.2467344E 03 | 0.1043232E 03 | 0.3079819E 03 | 36.762 | 9.190 | 0.109999 | 4 | 23.529 |
| 0.5365147E 02 | -0.6685316E 02 | 0.8569780E 02 | 309.005 | 61.817 | 0.030303 | 5 | 29.412 |
| -0.3852951E 02 | 0.9635687E 02 | 0.1037744E 03 | 111.795 | 18.632 | 0.037064 | 6 | 35.294 |
| -0.1131932E 02 | 0.1577439E 03 | 0.1581404E 03 | 94.103 | 13.443 | 0.056484 | 7 | 41.176 |
| 0.3970090E 02 | 0.3661057E 02 | 0.5401051E 02 | 42.675 | 5.334 | 0.019290 | 8 | 47.059 |
| -0.1438978E 02 | -0.4276291E 02 | 0.4511908E 02 | 251.402 | 27.934 | 0.01?115 | 9 | 52.941 |
| 0.9322916E 01 | -0.1069415E 03 | 0.1073471E 03 | 274.982 | 27.498 | 0.038340 | 10 | 58.824 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 33

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.17597386E 03 | | | | | | | |
| 0.13411746E 03 | -0.11359006E 03 | 0.17576166E 03 | 319.735 | 319.735 | 1.000000 | 1 | 5.882 |
| -0.29605946E 01 | 0.10468341E 03 | 0.10607946E 03 | 91.599 | 45.800 | 0.603919 | 2 | 11.765 |
| -0.13548976E 03 | -0.16259066E 02 | 0.13646176E 03 | 186.843 | 62.281 | 0.776489 | 3 | 17.647 |
| 0.77493486E 02 | 0.33119406E 02 | 0.84272976E 02 | 23.139 | 5.785 | 0.479471 | 4 | 23.529 |
| 0.45341876E 02 | -0.62062506E 02 | 0.76861156E 02 | 306.151 | 61.230 | 0.437389 | 5 | 29.412 |
| 0.33433936E 02 | 0.15050056E 02 | 0.37001046E 02 | 25.345 | 4.228 | 0.210518 | 6 | 35.294 |
| 0.24005586E 01 | 0.12456816E 02 | 0.12725376E 02 | 78.208 | 11.173 | 0.072401 | 7 | 41.176 |
| 0.12015796E 02 | -0.93776346E 01 | 0.15241906E 02 | 322.031 | 40.254 | 0.086719 | 8 | 47.059 |
| 0.90583106E 01 | 0.21361956E 02 | 0.23526986E 02 | 65.227 | 7.247 | 0.133857 | 9 | 52.941 |
| 0.80059456E 01 | 0.47580676E 00 | 0.80191726E 01 | 3.402 | 0.340 | 0.045625 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.85973006E 02 | | | | | | | |
| 0.65811306E 02 | -0.27047906E 02 | 0.89210536E 02 | 342.351 | 342.351 | 1.000000 | 1 | 5.882 |
| -0.84900476E 01 | 0.34522586E 02 | 0.35553136E 02 | 103.829 | 51.915 | 0.398531 | 2 | 11.765 |
| -0.38290436E 02 | 0.51656156E 01 | 0.38649426E 02 | 172.318 | 57.439 | 0.433193 | 3 | 17.647 |
| 0.19461756E 02 | 0.17040366E 02 | 0.25872896E 02 | 41.218 | 10.305 | 0.290020 | 4 | 23.529 |
| 0.29163706E 02 | -0.20162206E 02 | 0.30709506E 02 | 318.963 | 63.793 | 0.344236 | 5 | 29.412 |
| 0.11149466E 02 | -0.12004406E 00 | 0.11140326E 02 | 359.383 | 59.897 | 0.124944 | 6 | 35.294 |
| 0.44652436E 00 | -0.34470326E 00 | 0.58005416E 00 | 323.940 | 46.220 | 0.006502 | 7 | 41.176 |
| 0.21856216E 01 | 0.59480646E 01 | 0.63200776E 01 | 70.567 | 8.818 | 0.070853 | 8 | 47.059 |
| 0.65169716E 01 | 0.10038116E 02 | 0.11968076E 02 | 57.007 | 6.334 | 0.134195 | 9 | 52.941 |
| 0.47312726E 01 | 0.44644156E 01 | 0.64300346E 01 | 44.478 | 4.447 | 0.074310 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.11432306E 03 | | | | | | | |
| -0.19926396E 02 | 0.78322796E 02 | 0.87912266E 02 | 117.011 | 117.011 | 1.000000 | 1 | 5.882 |
| -0.19370076E 01 | -0.22130926E 02 | 0.22210306E 02 | 266.027 | 133.013 | 0.252540 | 2 | 11.765 |
| 0.40814166E 02 | 0.75772636E 01 | 0.41511586E 02 | 10.517 | 3.506 | 0.472193 | 3 | 17.647 |
| -0.23131746E 02 | -0.23040906E 02 | 0.33226246E 02 | 225.075 | 56.469 | 0.377925 | 4 | 23.529 |
| -0.80836756E 01 | 0.69879206E 01 | 0.10617266E 02 | 139.411 | 27.882 | 0.120771 | 5 | 29.412 |
| -0.76823566E 01 | -0.40082956E 01 | 0.90393806E 01 | 212.751 | 35.459 | 0.102823 | 6 | 35.294 |
| -0.10310886E 01 | -0.12900606E 01 | 0.16521146E 01 | 231.304 | 33.055 | 0.018793 | 7 | 41.176 |
| 0.80147256E 00 | 0.24783276E 01 | 0.26978096E 01 | 72.025 | 9.003 | 0.030682 | 8 | 47.059 |
| 0.10468956E 01 | 0.10917086E 01 | 0.21990756E 01 | 61.183 | 6.798 | 0.024959 | 9 | 52.941 |
| 0.20825576E 01 | 0.10716076E 01 | 0.23421266E 01 | 27.230 | 2.723 | 0.026642 | 10 | 58.824 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 498 CTR 250 CR 32.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.33719486E 01 | | | | | | | |
| 0.16248776E 01 | -0.23624906E 01 | 0.27585056E 01 | 301.081 | 301.081 | 1.000000 | 1 | 5.882 |
| -0.18480856E-01 | 0.20141836E-01 | 0.27355746E-01 | 132.522 | 66.261 | 0.009917 | 2 | 11.765 |
| -0.98141686E-01 | -0.11869676E-01 | 0.51527646E-01 | 193.320 | 64.439 | 0.018680 | 3 | 17.647 |
| 0.89587786E-01 | 0.69978126E-01 | 0.10664976E 00 | 40.997 | 10.249 | 0.038669 | 4 | 23.529 |
| 0.48762936E-02 | -0.98384946E-02 | 0.70124386E-02 | 314.057 | 62.811 | 0.002542 | 5 | 29.412 |
| 0.21220926-01 | 0.46062466E-02 | 0.21732206E-01 | 12.453 | 2.075 | 0.007878 | 6 | 35.294 |
| -0.11613936E-01 | 0.17960316E-01 | 0.21399006E-01 | 122.933 | 17.562 | 0.007757 | 7 | 41.176 |
| 0.67959676E-02 | -0.14163126E-02 | 0.69420006E-02 | 348.228 | 49.528 | 0.002517 | 8 | 47.059 |
| -0.24398076E-02 | 0.96105386E-02 | 0.97215186E-02 | 104.531 | 11.615 | 0.003524 | 9 | 52.941 |
| -0.21908046E-01 | 0.25112636E-02 | 0.21743546E-01 | 173.368 | 17.397 | 0.007882 | 10 | 58.824 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 36

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 GR 44.1 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.17920790E 03 | | | | | | | |
| -0.13260515E 04 | -0.24028092E 04 | 0.27448000E 04 | 241.093 | 241.093 | 0.756405 | 1 | 5.952 |
| -0.64040860E 02 | -0.36282090E 04 | 0.36280644E 04 | 268.989 | 134.494 | 1.000000 | 2 | 11.905 |
| 0.87010990E 03 | -0.75146146E 03 | 0.11497962E 04 | 319.187 | 106.396 | 0.316835 | 3 | 17.857 |
| -0.48990697E 03 | 0.33804644E 03 | 0.59199800E 03 | 140.616 | 35.104 | 0.144589 | 4 | 23.810 |
| 0.90252818E 02 | -0.83195078E 03 | 0.83486690E 03 | 274.674 | 94.819 | 0.229842 | 5 | 29.762 |
| 0.59111768E 01 | -0.16366788E 03 | 0.16375058E 03 | 271.979 | 45.321 | 0.045124 | 6 | 35.714 |
| 0.18619208E 03 | -0.12772998E 03 | 0.22979768E 03 | 325.544 | 46.508 | 0.062212 | 7 | 41.667 |
| 0.17747188E 02 | -0.39961368E 02 | 0.40102148E 02 | 294.267 | 37.033 | 0.011051 | 8 | 47.619 |
| 0.31021918E 02 | 0.79557948E 02 | 0.86138098E 02 | 67.498 | 7.495 | 0.023737 | 9 | 53.571 |
| -0.94618458E 01 | 0.69174588E 02 | 0.69389778E 02 | 94.514 | 9.451 | 0.019122 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 GR 44.1 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.78562788E 03 | | | | | | | |
| 0.42789488E 03 | -0.63179248E 03 | 0.76257478E 03 | 304.061 | 304.061 | 1.000000 | 1 | 5.952 |
| -0.91866868E 01 | -0.91488718E 01 | 0.19186258E 02 | 224.271 | 112.136 | 0.017187 | 2 | 11.905 |
| -0.11674468E 03 | 0.29193768E 02 | 0.12832978E 03 | 165.979 | 55.326 | 0.157794 | 3 | 17.857 |
| 0.15617968E 03 | 0.60137858E 01 | 0.15629838E 03 | 2.205 | 0.551 | 0.204951 | 4 | 23.810 |
| 0.11912788E 03 | 0.47724348E 03 | 0.49188658E 03 | 75.984 | 15.197 | 0.645034 | 5 | 29.762 |
| -0.44678678E 02 | 0.17895518E 03 | 0.17664838E 03 | 104.646 | 17.441 | 0.231718 | 6 | 35.714 |
| -0.18629218E 03 | 0.25767958E 02 | 0.18802618E 03 | 172.123 | 24.589 | 0.246567 | 7 | 41.667 |
| 0.52602878E 02 | 0.18234598E 01 | 0.52724478E 02 | 1.984 | 0.248 | 0.069140 | 8 | 47.619 |
| 0.85621478E 01 | -0.36825948E 02 | 0.37467368E 02 | 278.568 | 30.952 | 0.075368 | 9 | 53.571 |
| 0.21795468E 02 | 0.56298148E 01 | 0.22472298E 02 | 14.508 | 1.451 | 0.029464 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 GR 44.1 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.73242318E 03 | | | | | | | |
| 0.79988678E 03 | -0.74499778E 03 | 0.10933008E 04 | 315.551 | 315.551 | 1.000000 | 1 | 5.952 |
| -0.11823228E 03 | 0.42498618E 03 | 0.44110648E 03 | 105.547 | 52.774 | 0.414847 | 2 | 11.905 |
| -0.76729788E 02 | 0.85487418E 02 | 0.11486588E 03 | 131.906 | 43.969 | 0.108028 | 3 | 17.857 |
| 0.10649648E 03 | -0.98045858E 02 | 0.11763318E 03 | 334.821 | 83.705 | 0.110658 | 4 | 23.810 |
| 0.56888578E 02 | 0.23798028E 03 | 0.24447648E 03 | 76.742 | 15.348 | 0.229822 | 5 | 29.762 |
| -0.32919088E 01 | 0.42998038E 02 | 0.43116128E 02 | 94.378 | 15.730 | 0.040549 | 6 | 35.714 |
| -0.17223948E 02 | 0.22652658E 01 | 0.17377228E 02 | 172.508 | 24.644 | 0.016338 | 7 | 41.667 |
| -0.17993638E 02 | 0.22873268E 02 | 0.28421268E 02 | 129.046 | 16.131 | 0.026729 | 8 | 47.619 |
| -0.92487258E 01 | -0.29093088E 01 | 0.96955138E 01 | 197.462 | 21.940 | 0.009118 | 9 | 53.571 |
| -0.53305938E 01 | 0.13432028E 02 | 0.14444178E 02 | 111.660 | 11.166 | 0.013582 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 GR 44.1 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.89291268E 03 | | | | | | | |
| 0.86729598E 03 | -0.91243388E 03 | 0.12588638E 04 | 313.547 | 313.547 | 1.000000 | 1 | 5.952 |
| -0.24096708E 03 | 0.49994198E 03 | 0.55459038E 03 | 116.473 | 58.236 | 0.440365? | 2 | 11.905 |
| -0.99016108E 02 | 0.28779948E 03 | 0.29689108E 03 | 97.731 | 32.577 | 0.230391 | 3 | 17.857 |
| -0.73205348E 02 | 0.62077838E 02 | 0.95982158E 02 | 139.703 | 34.926 | 0.076245 | 4 | 23.810 |
| -0.78186618E 02 | -0.62095218E 02 | 0.99828998E 02 | 218.463 | 43.693 | 0.079301 | 5 | 29.762 |
| -0.24120498E 02 | -0.22297078E 02 | 0.32847858E 02 | 222.751 | 37.125 | 0.026093 | 6 | 35.714 |
| 0.82814088E 02 | 0.49329658E 02 | 0.96407178E 02 | 28.692 | 4.899 | 0.074994 | 7 | 41.667 |
| -0.20588688E 02 | 0.58091928E 02 | 0.62385458E 02 | 109.265 | 13.658 | 0.049557 | 8 | 47.619 |
| -0.23631118E 01 | 0.73689088E 02 | 0.73726798E 02 | 91.837 | 10.204 | 0.058566 | 9 | 53.571 |
| -0.23470988E 02 | 0.29444148E 02 | 0.37654298E 02 | 128.588 | 12.858 | 0.029911 | 10 | 59.524 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 36

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1468708E 04 | | | | | | | |
| 0.7322305E 03 | -0.9369790E 03 | 0.1189156E 04 | 308.007 | 308.007 | 1.000000 | 1 | 5.952 |
| -0.1516926E 03 | 0.3462976E 03 | 0.3780644E 03 | 113.655 | 56.828 | 0.317926 | 2 | 11.905 |
| 0.1037650E 03 | 0.3512515E 03 | 0.3662576E 03 | 73.542 | 24.514 | 0.307908 | 3 | 17.857 |
| -0.8008723E 02 | 0.5045255E 02 | 0.9469422E 02 | 147.790 | 36.948 | 0.079596 | 4 | 23.810 |
| -0.1022562E 03 | -0.2532466E 03 | 0.2731110E 03 | 248.012 | 49.602 | 0.229669 | 5 | 29.762 |
| 0.6525465E 01 | -0.4141040E 02 | 0.4192137E 02 | 278.955 | 46.493 | 0.035253 | 6 | 35.714 |
| 0.1114807E 02 | 0.8585001E 00 | 0.1118110E 02 | 4.404 | 0.629 | 0.009403 | 7 | 41.667 |
| 0.1620401E 02 | -0.9121094E 00 | 0.1622964E 02 | 356.778 | 44.557 | 0.013648 | 8 | 47.619 |
| 0.4229424E 01 | -0.3182264E 01 | 0.4995177E 01 | 332.940 | 36.993 | 0.005882 | 9 | 53.571 |
| 0.1795003E 02 | 0.[illegible]7134E 00 | 0.1795253E 02 | 0.960 | 0.096 | 0.015097 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1852-77E 04 | | | | | | | |
| 0.4424214E 03 | -0.6991567E 03 | 0.8273794E 03 | 302.325 | 302.325 | 1.000000 | 1 | 5.952 |
| -0.4783333E 02 | 0.1772458E 03 | 0.1837826E 03 | 110.942 | 55.471 | 0.220378 | 2 | 11.905 |
| 0.2191890E 03 | 0.3373567E 03 | 0.4023098E 03 | 56.987 | 18.996 | 0.486246 | 3 | 17.857 |
| -0.6378900E 02 | 0.7817480E 02 | 0.1005823E 03 | 128.993 | 32.248 | 0.121567 | 4 | 23.810 |
| -0.7909341E 02 | -0.3556841E 03 | 0.3643718E 03 | 257.463 | 51.493 | 0.440393 | 5 | 29.762 |
| 0.7252536E 01 | -0.6045464E 02 | 0.6088811E 02 | 276.841 | 46.140 | 0.073591 | 6 | 35.714 |
| -0.9106261E 02 | -0.3885652E 02 | 0.9900616E 02 | 203.108 | 29.015 | 0.119662 | 7 | 41.667 |
| 0.2996854E 02 | -0.2629036E 02 | 0.3986597E 02 | 318.740 | 39.843 | 0.048183 | 8 | 47.619 |
| 0.1176331E 02 | -0.5864799E 02 | 0.5981607E 02 | 281.342 | 31.260 | 0.072296 | 9 | 53.571 |
| 0.8153008E 01 | -0.3372879E 02 | 0.3470018E 02 | 289.589 | 28.359 | 0.041940 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1532291E 04 | | | | | | | |
| 0.1574793E 03 | -0.4393916E 03 | 0.4667293E 03 | 289.718 | 289.718 | 1.000000 | 1 | 5.952 |
| -0.2833226E 02 | 0.9583557E 01 | 0.2990922E 02 | 161.312 | 80.656 | 0.064079 | 2 | 11.905 |
| 0.2697277E 03 | 0.2837214E 03 | 0.3914690E 03 | 46.440 | 15.483 | 0.838695 | 3 | 17.857 |
| -0.4798305E 02 | 0.1235715E 03 | 0.1324162E 03 | 111.060 | 27.765 | 0.283693 | 4 | 23.810 |
| -0.6329378E 02 | -0.3432075E 03 | 0.3489949E 03 | 259.551 | 51.910 | 0.747697 | 5 | 29.762 |
| 0.1048399E 02 | -0.4755675E 02 | 0.4869864E 02 | 282.432 | 47.072 | 0.104333 | 6 | 35.714 |
| -0.1018160E 03 | -0.3698500E 02 | 0.1083253E 03 | 199.984 | 28.566 | 0.232079 | 7 | 41.667 |
| 0.3635196E 02 | -0.4728816E 02 | 0.5964432E 02 | 307.552 | 38.444 | 0.127784 | 8 | 47.619 |
| -0.2891049E 00 | -0.5245718E 02 | 0.5245798E 02 | 269.684 | 29.965 | 0.112388 | 9 | 53.571 |
| -0.1686674E 02 | -0.3130099E 02 | 0.3555614E 02 | 241.682 | 24.168 | 0.076177 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1139147E 04 | | | | | | | |
| -0.8734445E 02 | -0.1562956E 03 | 0.1790657E 03 | 240.802 | 240.802 | 0.491479 | 1 | 5.952 |
| -0.4219377E 02 | -0.4771143E 02 | 0.6369218E 02 | 228.512 | 114.256 | 0.174836 | 2 | 11.905 |
| 0.3121350E 03 | 0.1878469E 03 | 0.3643000E 03 | 31.040 | 10.347 | 1.000000 | 3 | 17.857 |
| -0.1276909E 02 | 0.1560584E 03 | 0.1565799E 03 | 94.678 | 23.669 | 0.429810 | 4 | 23.810 |
| -0.7887239E 02 | -0.2472572E 03 | 0.2595320E 03 | 252.308 | 50.461 | 0.712413 | 5 | 29.762 |
| -0.3520419E 01 | -0.2252087E 02 | 0.2279438E 02 | 261.115 | 43.519 | 0.062570 | 6 | 35.714 |
| -0.1345891E 03 | 0.3949760E 01 | 0.1346470E 03 | 178.319 | 25.474 | 0.369865 | 7 | 41.667 |
| 0.2000595E 02 | -0.2585771E 02 | 0.3269361E 02 | 307.729 | 38.466 | 0.089743 | 8 | 47.619 |
| 0.1042847E 01 | -0.4217987E 02 | 0.4219275E 02 | 271.416 | 30.157 | 0.115819 | 9 | 53.571 |
| -0.7127143E 01 | -0.2217862E 02 | 0.2329564E 02 | 252.185 | 25.218 | 0.063996 | 10 | 59.524 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 36

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 3 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3275546E 04 | | | | | | | |
| 0.1833519E 05 | 0.3200772E 05 | 0.3689725E 05 | 60.167 | 60.167 | 1.000000 | 1 | 5.952 |
| -0.3561496E 04 | 0.5853383E 04 | 0.6851363E 04 | 121.175 | 60.508 | 0.195417 | 2 | 11.905 |
| -0.1625499E 04 | -0.6900745E 03 | 0.1765913E 04 | 203.003 | 67.668 | 0.047860 | 3 | 17.857 |
| 0.3054572E 03 | 0.2254958E 03 | 0.3799993E 03 | 36.400 | 9.100 | 0.010299 | 4 | 23.810 |
| 0.3655881E 03 | -0.5850930E 03 | 0.6899189E 03 | 301.999 | 60.400 | 0.018698 | 5 | 29.762 |
| -0.5773003E 01 | -0.3486877E 03 | 0.3487354E 03 | 269.051 | 44.842 | 0.009452 | 6 | 35.714 |
| -0.3839478E 03 | -0.3502461E 03 | 0.5251248E 03 | 223.017 | 31.860 | 0.014232 | 7 | 41.667 |
| -0.3091663E 03 | 0.2652273E 03 | 0.4043164E 03 | 139.005 | 17.376 | 0.010958 | 8 | 47.619 |
| 0.5739029E 02 | 0.6661328E 02 | 0.8792595E 02 | 49.254 | 5.473 | 0.002383 | 9 | 53.571 |
| -0.9106792E 02 | -0.1050962E 03 | 0.1390632E 03 | 229.090 | 22.909 | 0.003769 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1144915E 05 | | | | | | | |
| 0.1063609E 05 | 0.1986561E 05 | 0.2253370E 05 | 61.835 | 61.835 | 1.000000 | 1 | 5.952 |
| -0.1652854E 04 | 0.3863719E 04 | 0.4202406E 04 | 113.161 | 56.580 | 0.186494 | 2 | 11.905 |
| -0.8469194E 03 | -0.2066026E 03 | 0.8717551E 03 | 193.709 | 64.570 | 0.038687 | 3 | 17.857 |
| 0.4978102E 02 | 0.3491066E 03 | 0.3526377E 03 | 81.885 | 20.471 | 0.015649 | 4 | 23.810 |
| -0.3087717E 03 | -0.5081284E 03 | 0.5945874E 03 | 238.714 | 47.743 | 0.026387 | 5 | 29.762 |
| 0.1280329E 02 | -0.1796265E 03 | 0.1800822E 03 | 274.077 | 45.679 | 0.007992 | 6 | 35.714 |
| 0.2736357E 03 | -0.4409927E 02 | 0.2771663E 03 | 350.845 | 50.121 | 0.012300 | 7 | 41.667 |
| 0.1667859E 02 | -0.7679569E 02 | 0.7857614E 02 | 282.255 | 35.282 | 0.003487 | 8 | 47.619 |
| 0.7382280E 02 | 0.9822113E 02 | 0.1228706E 03 | 53.072 | 5.897 | 0.005453 | 9 | 53.571 |
| -0.2229752E 02 | 0.7259592E 02 | 0.7594299E 02 | 107.074 | 10.707 | 0.003370 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9929559E 04 | | | | | | | |
| 0.3659948E 04 | 0.7561641E 04 | 0.8416559E 04 | 63.952 | 63.952 | 1.000000 | 1 | 5.952 |
| -0.2644687E 03 | 0.1589042E 04 | 0.1607284E 04 | 99.543 | 49.772 | 0.190967 | 2 | 11.905 |
| -0.3084330E 03 | -0.1725273E 01 | 0.3086077E 03 | 180.320 | 60.107 | 0.036667 | 3 | 17.857 |
| 0.2932827E 03 | 0.1270450E 03 | 0.3196172E 03 | 23.421 | 5.855 | 0.037975 | 4 | 23.810 |
| -0.2162572E 03 | -0.1124052E 03 | 0.2437254E 03 | 207.464 | 41.493 | 0.028958 | 5 | 29.762 |
| 0.1736284E 02 | -0.2159741E 02 | 0.2771129E 02 | 308.797 | 51.466 | 0.003292 | 6 | 35.714 |
| 0.4108799E 03 | -0.7013427E 03 | 0.4975086E 03 | 333.892 | 47.699 | 0.059365 | 7 | 41.667 |
| 0.1302244E 03 | -0.3900864E 03 | 0.4112488E 03 | 288.461 | 36.058 | 0.048862 | 8 | 47.619 |
| -0.1433282E 03 | -0.2690801E 03 | 0.3048721E 03 | 241.958 | 26.884 | 0.036223 | 9 | 53.571 |
| 0.2018829E 03 | 0.1276659E 02 | 0.2022989E 03 | 3.675 | 0.367 | 0.024036 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5855617E 04 | | | | | | | |
| 0.1498392E 04 | 0.2722323E 04 | 0.3106482E 04 | 61.203 | 61.203 | 1.000000 | 1 | 5.952 |
| -0.1114934E 03 | 0.7219175E 03 | 0.7304761E 03 | 98.779 | 49.390 | 0.235146 | 2 | 11.905 |
| -0.1363991E 03 | -0.3752740E 02 | 0.1414673E 03 | 195.383 | 65.128 | 0.045539 | 3 | 17.857 |
| 0.1016139E 03 | 0.6602234E 02 | 0.1271789E 03 | 33.013 | 8.253 | 0.039060 | 4 | 23.810 |
| -0.5893375E 02 | -0.4745128E 02 | 0.7566246E 02 | 218.860 | 43.758 | 0.024356 | 5 | 29.762 |
| -0.2002357E 02 | -0.1321897E 03 | 0.1336976E 03 | 261.386 | 43.564 | 0.043038 | 6 | 35.714 |
| 0.2947310E 03 | -0.1723517E 03 | 0.2600483E 03 | 318.489 | 45.498 | 0.083712 | 7 | 41.667 |
| -0.1367327E 02 | -0.2981187E 03 | 0.2984897E 03 | 267.012 | 38.376 | 0.083210 | 8 | 47.619 |
| -0.1261958E 03 | -0.9361642E 02 | 0.1571287E 03 | 216.569 | 24.063 | 0.050581 | 9 | 53.571 |
| 0.1551594E 03 | 0.7534787E 02 | 0.1724869E 03 | 25.902 | 2.590 | 0.055525 | 10 | 59.524 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 36

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4877876E 02 | | | | | | | |
| 0.1078766E 03 | 0.2942584E 02 | 0.1118178E 03 | 15.258 | 15.258 | 0.776747 | 1 | 5.952 |
| -0.2498240E 02 | 0.8420789E 02 | 0.8783960E 02 | 106.526 | 53.262 | 0.610153 | 2 | 11.905 |
| -0.1062944E 03 | 0.1350406E 02 | 0.1071500E 03 | 172.760 | 57.587 | 0.744327 | 3 | 17.857 |
| 0.7443152E 02 | 0.3401929E 01 | 0.7450920E 02 | 2.617 | 0.654 | 0.517581 | 4 | 23.810 |
| 0.1511253E 02 | -0.1431611E 03 | 0.1439586E 03 | 276.026 | 55.205 | 1.000000 | 5 | 29.762 |
| 0.3711856E 02 | -0.2746201E 02 | 0.4617302E 02 | 323.584 | 53.917 | 0.320743 | 6 | 35.714 |
| 0.2975011E 02 | -0.3372211E 01 | 0.2994061E 02 | 353.533 | 50.565 | 0.207984 | 7 | 41.667 |
| -0.6062225E 01 | 0.1259953E 02 | 0.1398208E 02 | 115.694 | 14.462 | 0.097127 | 8 | 47.619 |
| -0.1044262E 02 | 0.1256591E 02 | 0.1633861E 02 | 129.728 | 14.414 | 0.113497 | 9 | 53.571 |
| 0.6521341E 01 | 0.1158164E 02 | 0.1329145E 02 | 60.617 | 6.062 | 0.092330 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 15 TORSION 105

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6652059E 01 | | | | | | | |
| 0.7777917E 02 | 0.1020148E 03 | 0.1282833E 03 | 52.677 | 52.677 | 1.000000 | 1 | 5.952 |
| -0.3882813E 02 | 0.3397588E 02 | 0.4597652E 02 | 132.550 | 66.275 | 0.355280 | 2 | 11.905 |
| -0.3898874E 02 | 0.2197591E 02 | 0.4480978E 02 | 150.542 | 50.181 | 0.340336 | 3 | 17.857 |
| 0.1907822E 02 | 0.4833458E 01 | 0.1669328E 02 | 14.031 | 4.208 | 0.130128 | 4 | 23.810 |
| 0.1919344E 02 | -0.4895384E 02 | 0.5258182E 02 | 291.409 | 58.282 | 0.409888 | 5 | 29.762 |
| 0.1426733E 02 | -0.7042640E 01 | 0.1632918E 02 | 330.895 | 55.149 | 0.127298 | 6 | 35.714 |
| 0.5754343E 01 | 0.6423084E 01 | 0.8623655E 01 | 48.143 | 6.878 | 0.067223 | 7 | 41.667 |
| -0.9815404E 00 | 0.1093454E 02 | 0.1095000E 02 | 93.044 | 13.631 | 0.085358 | 8 | 47.619 |
| -0.3786183E C1 | -0.1786220E 01 | 0.4186378E 01 | 205.257 | 22.806 | 0.032634 | 9 | 53.571 |
| 0.3278491E 01 | 0.1534840E 01 | 0.3619977E 01 | 25.087 | 2.509 | 0.028219 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1388790E 01 | | | | | | | |
| 0.1347801E C2 | 0.5665491E 02 | 0.5819025E 02 | 76.809 | 76.809 | 1.000000 | 1 | 5.952 |
| -0.1325894E 02 | -0.5757015E 01 | 0.1445485E 02 | 203.470 | 101.735 | 0.248407 | 2 | 11.905 |
| 0.3643089E 01 | -0.2476997E 01 | 0.3651500E 02 | 356.110 | 118.703 | 0.627511 | 3 | 17.857 |
| -0.3227184E 02 | -0.1491851E 02 | 0.3538707E 02 | 204.222 | 51.056 | 0.608127 | 4 | 23.810 |
| -0.2911678E C1 | 0.1178759E 02 | 0.1214188E 02 | 103.875 | 20.775 | 0.208658 | 5 | 29.762 |
| -0.2760360E 01 | 0.2119767E 01 | 0.3480372E 01 | 142.478 | 23.746 | 0.059810 | 6 | 35.714 |
| -0.1184951E 01 | 0.4994884E 00 | 0.1283154E 01 | 170.299 | 24.328 | 0.019473 | 7 | 41.667 |
| -0.1371216E 00 | 0.1040757E 01 | 0.1043847E 01 | 92.582 | 11.573 | 0.052309 | 8 | 47.619 |
| 0.9425481E C0 | -0.1979902E 01 | 0.2198208E 01 | 299.497 | 32.829 | 0.037683 | 9 | 53.571 |
| -0.8074523E 00 | 0.1228495E 01 | 0.1470094E 01 | 123.316 | 12.332 | 0.025264 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 175 CR 44.1 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3520829E C1 | | | | | | | |
| 0.1191460E 01 | -0.2147964E 01 | 0.2456283E 01 | 299.017 | 299.017 | 1.000000 | 1 | 5.952 |
| -0.1899004E-01 | 0.4029843E-01 | 0.4454468E-01 | 115.232 | 57.616 | 0.018137 | 2 | 11.905 |
| -0.2647985E-01 | 0.7859360E-02 | 0.2762159E-01 | 163.469 | 54.490 | 0.011245 | 3 | 17.857 |
| 0.6056529E-C1 | 0.2814823E-01 | 0.6680363E-01 | 24.958 | 6.240 | 0.027197 | 4 | 23.810 |
| 0.1299755E-01 | -0.1670339E-01 | 0.2116458E-01 | 307.888 | 61.578 | 0.008617 | 5 | 29.762 |
| -0.5842738E-02 | -0.1438644E-01 | 0.1529011E-01 | 247.472 | 41.245 | 0.006209 | 6 | 35.714 |
| -0.1448383E-01 | -0.1608965E-01 | 0.2164852E-01 | 228.007 | 32.572 | 0.008814 | 7 | 41.667 |
| 0.1124965E-C1 | 0.6487634E-02 | 0.1294629E-01 | 29.972 | 3.746 | 0.005287 | 8 | 47.619 |
| 0.2537965E-01 | -0.2017061E-01 | 0.3241866E-01 | 321.524 | 35.725 | 0.013198 | 9 | 53.571 |
| -0.4358370E-02 | -0.1933147E-02 | 0.4479147E-02 | 193.336 | 19.334 | 0.001824 | 10 | 59.524 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 37

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1390410E 05 | | | | | | | |
| -0.4971727E 04 | -0.4933687E 04 | 0.6729870E 04 | 222.374 | 222.374 | 1.000000 | 1 | 5.988 |
| -0.1137411E 03 | -0.3316300E 04 | 0.3318250E 04 | 268.035 | 134.018 | 0.493067 | 2 | 11.976 |
| 0.3648445E 02 | -0.8876580E 03 | 0.9597124E 03 | 292.344 | 97.448 | 0.142606 | 3 | 17.964 |
| -0.3742532E 03 | 0.1738098E 03 | 0.4126423E 03 | 155.090 | 38.772 | 0.061316 | 4 | 23.952 |
| -0.7071820E 02 | -0.9515085E 01 | 0.9541328E 02 | 265.748 | 53.150 | 0.141777 | 5 | 29.940 |
| -0.1499863E 02 | -0.1841923E 03 | 0.1847699E 03 | 269.468 | 44.245 | 0.027455 | 6 | 35.928 |
| 0.1473857E 03 | -0.4999837E 02 | 0.1556394E 03 | 341.261 | 48.752 | 0.023126 | 7 | 41.916 |
| 0.2225053E 02 | -0.3383322E 02 | 0.4049411E 02 | 303.331 | 37.916 | 0.006017 | 8 | 47.904 |
| -0.1630967E 01 | 0.3209288E 02 | 0.3213429E 02 | 92.909 | 10.323 | 0.004775 | 9 | 53.892 |
| -0.9993099E 01 | 0.3321115E 02 | 0.3367882E 02 | 99.560 | 9.956 | 0.005004 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.2853373E 04 | | | | | | | |
| -0.2720803E 03 | -0.1918604E 04 | 0.1944593E 04 | 254.932 | 254.932 | 1.000000 | 1 | 5.988 |
| 0.2794965E 02 | -0.1004019E 02 | 0.3327892E 02 | 327.146 | 163.573 | 0.031790 | 2 | 11.976 |
| -0.1143443E 03 | 0.1132878E 02 | 0.1149041E 03 | 174.342 | 58.114 | 0.109789 | 3 | 17.964 |
| 0.1594885E 03 | -0.9187671E 02 | 0.1798469E 03 | 329.537 | 82.384 | 0.171645 | 4 | 23.952 |
| 0.2881197E 03 | 0.4768185E 03 | 0.5587207E 03 | 66.587 | 13.317 | 0.498628 | 5 | 29.940 |
| -0.4324488E 02 | 0.1393349E 03 | 0.1460867E 03 | 107.219 | 17.870 | 0.139503 | 6 | 35.928 |
| -0.2063004E 03 | 0.6488352E 02 | 0.2168807E 03 | 162.764 | 23.252 | 0.206385 | 7 | 41.916 |
| 0.4169468E 02 | -0.6879429E 01 | 0.4209540E 02 | 351.702 | 43.963 | 0.040221 | 8 | 47.904 |
| 0.3479869E 02 | -0.2086902E 02 | 0.4057333E 02 | 329.051 | 36.561 | 0.038767 | 9 | 53.892 |
| 0.3944557E 02 | -0.3304128E 00 | 0.3944717E 02 | 359.453 | 39.945 | 0.037669 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 6 FL. BEND 79

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1048279E 04 | | | | | | | |
| 0.9882915E 03 | -0.8858672E 03 | 0.1059000E 04 | 303.227 | 303.227 | 1.000000 | 1 | 5.988 |
| -0.1103491E 03 | 0.4933964?E 03 | 0.4473918E 03 | 104.282 | 52.141 | 0.422463 | 2 | 11.976 |
| -0.9187825E 02 | 0.1031345E 03 | 0.1154437E 03 | 116.780 | 38.926 | 0.109011 | 3 | 17.964 |
| 0.6584749E 02 | -0.2718716E 02 | 0.7123924E 02 | 337.565 | 84.391 | 0.067270 | 4 | 23.952 |
| 0.7329290E 02 | 0.2735732E 03 | 0.2832207E 03 | 75.002 | 15.000 | 0.267440 | 5 | 29.940 |
| -0.2960981E 02 | 0.2678591E 02 | 0.3711894E 02 | 133.816 | 22.303 | 0.035051 | 6 | 35.928 |
| -0.1665939E 02 | 0.2165984E 02 | 0.2732217E 02 | 127.571 | 18.224 | 0.025800 | 7 | 41.916 |
| -0.3006873E 02 | -0.4585679E 01 | 0.3040017E 02 | 188.670 | 23.584 | 0.028714 | 8 | 47.904 |
| -0.2062160E 02 | 0.6816420E 01 | 0.2942216E 02 | 166.684 | 18.512 | 0.027783 | 9 | 53.892 |
| -0.1630484E 02 | -0.2619980E 01 | 0.1691334E 02 | 189.115 | 18.911 | 0.015993 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8429892E 03 | | | | | | | |
| 0.9339564E 03 | -0.9868639E 03 | 0.1358465E 04 | 313.410 | 313.410 | 1.000000 | 1 | 5.988 |
| -0.2096478E 03 | 0.4732124E 03 | 0.5175083E 03 | 113.879 | 56.939 | 0.380951 | 2 | 11.976 |
| 0.9652989E 02 | 0.2914661E 03 | 0.2960972E 03 | 70.324 | 20.341 | 0.218593 | 3 | 17.964 |
| -0.4831871E 02 | 0.6885369E 02 | 0.7233282E 02 | 123.877 | 30.969 | 0.053246 | 4 | 23.952 |
| -0.6540846E 02 | -0.4733813E 02 | 0.8074133E 02 | 215.894 | 43.179 | 0.059434 | 5 | 29.940 |
| 0.1124567E 02 | -0.5336194E 02 | 0.5453408E 02 | 281.988 | 46.997 | 0.040144 | 6 | 35.928 |
| 0.1082419E 03 | 0.2831683E 01 | 0.1082814E 03 | 1.618 | 0.231 | 0.079822 | 7 | 41.916 |
| 0.7988988E 01 | -0.8866866E 01 | 0.1193281E 02 | 314.720 | 39.340 | 0.000357 | 8 | 47.904 |
| 0.5302273E 01 | 0.5013709E 01 | 0.7040599E 01 | 47.635 | 5.295 | 0.005792 | 9 | 53.892 |
| 0.1952966E 01 | -0.1819478E 01 | 0.2666459E 01 | 317.089 | 31.769 | 0.001963 | 10 | 59.880 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 37

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1591513E 04 | | | | | | | |
| 0.7983843E 03 | -0.9825615E 03 | 0.1266035E 04 | 309.096 | 309.056 | 1.000000 | 1 | 5.988 |
| -0.1515535E 03 | 0.3879773E 03 | 0.4169269E 03 | 111.337 | 55.668 | 0.329001 | 2 | 11.976 |
| 0.1522550E 03 | 0.3415417E 03 | 0.3739414E 03 | 65.973 | 21.991 | 0.295364 | 3 | 17.964 |
| -0.5842610E 02 | 0.4095773E 02 | 0.7135225E 02 | 144.969 | 36.242 | 0.056359 | 4 | 23.952 |
| -0.1174882E 03 | -0.2984910E 03 | 0.3207805E 03 | 248.515 | 49.703 | 0.253374 | 5 | 29.940 |
| -0.5337258E 01 | -0.5230482E 02 | 0.5257642E 02 | 264.174 | 44.029 | 0.041528 | 6 | 35.928 |
| -0.3187537E 02 | 0.9324069E 01 | 0.3321109E 02 | 163.695 | 23.385 | 0.026232 | 7 | 41.916 |
| 0.4036351E 02 | 0.3376445E 02 | 0.5262494E 02 | 39.914 | 4.989 | 0.041567 | 8 | 47.904 |
| 0.2344577E 02 | 0.2213675E 02 | 0.3237642E 02 | 43.549 | 4.839 | 0.025573 | 9 | 53.892 |
| 0.7901618E 01 | 0.4375386E 01 | 0.9032141E 01 | 28.975 | 2.897 | 0.007134 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2061899E 04 | | | | | | | |
| 0.9215056E 03 | -0.7754277E 03 | 0.9344817E 03 | 303.922 | 303.922 | 1.000000 | 1 | 5.988 |
| -0.1174258E 03 | 0.2191341E 03 | 0.2486133E 03 | 118.185 | 59.093 | 0.266044 | 2 | 11.976 |
| 0.2513013E 03 | 0.3360791E 03 | 0.4212478E 03 | 53.376 | 17.792 | 0.450782 | 3 | 17.964 |
| -0.2803568E 02 | 0.1015182E 03 | 0.1053183E 03 | 105.438 | 26.360 | 0.112702 | 4 | 23.952 |
| -0.1304275E 03 | -0.3668354E 03 | 0.3893320E 03 | 250.427 | 50.085 | 0.416629 | 5 | 29.940 |
| -0.5803499E 01 | -0.6601556E 02 | 0.6620485E 02 | 265.666 | 44.278 | 0.070847 | 6 | 35.928 |
| -0.1162476E 03 | -0.3002071E 02 | 0.1208814E 03 | 194.480 | 27.783 | 0.129479 | 7 | 41.916 |
| 0.9999525E 00 | -0.5744900E 00 | 0.1153232E 01 | 330.122 | 41.265 | 0.001234 | 8 | 47.904 |
| -0.2598869E 02 | 0.2413208E 01 | 0.2610248E 02 | 174.695 | 19.411 | 0.027933 | 9 | 53.892 |
| -0.1009346E 02 | 0.8918104E 01 | 0.1346888E 02 | 138.538 | 13.854 | 0.014413 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1772829E 04 | | | | | | | |
| 0.2866772E 03 | -0.5365254E 03 | 0.5749563E 03 | 291.067 | 291.067 | 1.000000 | 1 | 5.988 |
| -0.3554889E 02 | 0.9332932E 02 | 0.9987032E 02 | 110.892 | 55.426 | 0.173701 | 2 | 11.976 |
| 0.3978084E 03 | 0.2713955E 03 | 0.4098125E 03 | 41.471 | 13.824 | 0.712772 | 3 | 17.964 |
| -0.3463031E 02 | 0.1012554E 03 | 0.1070136E 03 | 108.881 | 27.220 | 0.186125 | 4 | 23.952 |
| -0.7695257E 02 | -0.3434534E 03 | 0.3713250E 03 | 258.181 | 51.636 | 0.645892 | 5 | 29.940 |
| -0.1583286E 02 | -0.3912544E 02 | 0.4220757E 02 | 247.988 | 41.328 | 0.073410 | 6 | 35.928 |
| -0.1270498E 03 | -0.6038454E 02 | 0.1406689E 03 | 205.421 | 29.346 | 0.244660 | 7 | 41.916 |
| -0.2290468E 02 | -0.2578627E 02 | 0.3449988E 02 | 228.387 | 28.548 | 0.059987 | 8 | 47.904 |
| -0.2318183E 00 | 0.2632486E 01 | 0.2642673E 01 | 95.033 | 10.559 | 0.004596 | 9 | 53.892 |
| -0.2993365E 02 | -0.2294911E 02 | 0.3315842E 02 | 223.797 | 22.359 | 0.057671 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1364518E 04 | | | | | | | |
| -0.4330295E 02 | -0.2093394E 03 | 0.2137712E 03 | 258.313 | 258.313 | 0.543980 | 1 | 5.988 |
| 0.1099004E 02 | -0.6557895E 01 | 0.1279792E 02 | 329.175 | 164.587 | 0.032567 | 2 | 11.976 |
| 0.3951516E 03 | 0.2051922E 03 | 0.3929761E 03 | 31.476 | 10.492 | 1.000000 | 3 | 17.964 |
| 0.7046827E 01 | 0.1007529E 03 | 0.1009991E 03 | 85.999 | 21.500 | 0.257011 | 4 | 23.952 |
| -0.5092389E 02 | -0.2588206E 03 | 0.2637875E 03 | 258.869 | 51.774 | 0.671263 | 5 | 29.940 |
| 0.2294967E 02 | -0.3125638E 02 | 0.3878873E 02 | 306.311 | 51.052 | 0.098705 | 6 | 35.928 |
| -0.1216514E 03 | -0.5852203E 02 | 0.1317252E 03 | 202.553 | 28.936 | 0.335199 | 7 | 41.916 |
| -0.7446885E 01 | -0.2187321E 02 | 0.2310612E 02 | 251.198 | 31.400 | 0.058798 | 8 | 47.904 |
| -0.2902443E 02 | -0.2085292E 02 | 0.3573878E 02 | 215.696 | 23.966 | 0.090944 | 9 | 53.892 |
| -0.3244220E 02 | -0.3316340E 02 | 0.4639081E 02 | 225.627 | 22.563 | 0.118050 | 10 | 59.880 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 37

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 189 CR 45.1 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1023235E 04 | | | | | | | |
| 0.2561722E 05 | 0.3088922E 05 | 0.4013269E 05 | 50.334 | 50.334 | 1.000000 | 1 | 5.988 |
| -0.7478713E 03 | 0.5627145E 04 | 0.5676621E 04 | 97.571 | 49.78[illegible] | 0.141446 | 2 | 11.976 |
| -0.1534809E 04 | -0.1311441E 03 | 0.1540401E 04 | 184.884 | 61.628 | 0.038383 | 3 | 17.964 |
| 0.2449339E 02 | -0.1806577E 03 | 0.3043513E 03 | 323.588 | 80.857 | 0.007584 | 4 | 23.952 |
| 0.3547800E 03 | -0.8136655E 03 | 0.8876487E 03 | 293.558 | 58.712 | 0.022118 | 5 | 29.940 |
| 0.1101256E 03 | -0.4639243E 03 | 0.4768157E 03 | 283.354 | 47.226 | 0.011881 | 6 | 35.928 |
| -0.1436604E 03 | -0.2997356E 03 | 0.3323848E 03 | 244.392 | 34.913 | 0.008282 | 7 | 41.916 |
| 0.5377866E C3 | 0.1356518E 03 | 0.5544311E 03 | 14.177 | 1.770 | 0.013820 | 8 | 47.904 |
| 0.2272243E 03 | -0.2046910E 03 | 0.3085168E 03 | 317.434 | 35.270 | 0.007687 | 9 | 53.892 |
| -0.3935977E 03 | 0.1107059E 03 | 0.4088701E 03 | 164.290 | 18.429 | 0.010188 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.9615665E 04 | | | | | | | |
| 0.1506693E 05 | 0.1979311E 05 | 0.2903471E 05 | 52.998 | 52.998 | 1.000000 | 1 | 5.988 |
| 0.1568591E 03 | 0.3539055E 04 | 0.3543428E 04 | 87.463 | 43.731 | 0.141541 | 2 | 11.976 |
| -0.7277744E C3 | 0.5309375E 02 | 0.7297885E 03 | 175.827 | 58.669 | 0.029148 | 3 | 17.964 |
| 0.1136594E 03 | 0.8616513E 02 | 0.1426285E 03 | 37.166 | 9.291 | 0.005697 | 4 | 23.952 |
| -0.5718010E 03 | -0.7344045E 03 | 0.9307556E 03 | 232.096 | 46.419 | 0.037179 | 5 | 29.940 |
| -0.1409939E 02 | -0.4706086E 01 | 0.4708196E 03 | 268.284 | 44.714 | 0.018807 | 6 | 35.928 |
| 0.1212921E 03 | -0.6707031E 02 | 0.1366000E 03 | 331.059 | 47.294 | 0.005536 | 7 | 41.916 |
| -0.1781351E 03 | -0.8776843E 02 | 0.1914399E 03 | 207.288 | 25.911 | 0.007647 | 8 | 47.904 |
| 0.5225151E 01 | 0.3294542E 02 | 0.3335719E 02 | 80.988 | 8.999 | 0.001332 | 9 | 53.892 |
| -0.4918545E 02 | 0.6281531E 02 | 0.7970007E 02 | 128.062 | 12.806 | 0.003187 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1059059E 05 | | | | | | | |
| 0.5268660E 04 | 0.7345951E 04 | 0.9039285E 04 | 54.348 | 54.348 | 1.000000 | 1 | 5.988 |
| 0.9024558E C3 | 0.1403179E 04 | 0.1547846E 04 | 71.047 | 35.524 | 0.171147 | 2 | 11.976 |
| -0.4482327E 03 | 0.7259435E 02 | 0.4540730E 03 | 170.800 | 56.933 | 0.050233 | 3 | 17.964 |
| 0.1099364E 03 | 0.9033598E 02 | 0.1422986E 03 | 39.410 | 9.853 | 0.015741 | 4 | 23.952 |
| -0.4434905E 03 | -0.1604061E 03 | 0.4716758E 03 | 199.907 | 39.981 | 0.052181 | 5 | 29.940 |
| -0.2846593E C2 | -0.2561721E 03 | 0.2577485E 03 | 263.659 | 43.943 | 0.028514 | 6 | 35.928 |
| 0.2941047E 03 | -0.1308650E 03 | 0.3219055E 03 | 336.013 | 48.002 | 0.035612 | 7 | 41.916 |
| -0.5709442E 03 | -0.1570007E 03 | 0.5907549E 03 | 194.918 | 24.365 | 0.065354 | 8 | 47.904 |
| -0.1304706E 03 | 0.1618906E 03 | 0.2079261E 03 | 128.868 | 14.319 | 0.023002 | 9 | 53.892 |
| 0.1373977E 03 | -0.1844491E 03 | 0.2392192E 03 | 306.096 | 30.610 | 0.025001 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6000262E 04 | | | | | | | |
| 0.1901824E 04 | 0.2477805E 04 | 0.3123532E 04 | 52.492 | 52.492 | 1.000000 | 1 | 5.988 |
| 0.1672596E 03 | 0.5975823E 03 | 0.6205483E 03 | 74.363 | 37.182 | 0.198669 | 2 | 11.976 |
| -0.2442347E 03 | 0.7762982E 02 | 0.2562749E 03 | 162.367 | 54.122 | 0.082046 | 3 | 17.964 |
| 0.1139788E 03 | 0.4886838E 02 | 0.1287077E 03 | 14.790 | 4.947 | 0.038645 | 4 | 23.952 |
| -0.3279182E 03 | -0.8687570E 02 | 0.3387476E 03 | 194.860 | 38.972 | 0.108450 | 5 | 29.940 |
| -0.7060509E 02 | -0.1275341E 03 | 0.1457738E 03 | 241.030 | 40.172 | 0.046670 | 6 | 35.928 |
| 0.1749784E 03 | -0.6332367E 02 | 0.1860766E 03 | 340.104 | 48.586 | 0.059572 | 7 | 41.916 |
| -0.4377134E 03 | -0.6753374E 02 | 0.4429026E 03 | 188.771 | 23.596 | 0.141792 | 8 | 47.904 |
| 0.1036370E 02 | 0.1860213E 03 | 0.1863089E 03 | 86.817 | 9.646 | 0.059647 | 9 | 53.892 |
| 0.1379074E 03 | -0.1584583E 03 | 0.2101180E 03 | 311.050 | 31.105 | 0.067269 | 10 | 59.880 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 37

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1887067E 02 | | | | | | | |
| 0.1047025E 03 | 0.49127955E 02 | 0.11565552E 03 | 25.136 | 25.136 | 0.851690 | 1 | 5.988 |
| -0.1640605E 02 | 0.68761875 02 | 0.79691915E 02 | 103.419 | 51.710 | 0.520575 | 2 | 11.976 |
| -0.8782085E 02 | 0.35950805E 01 | 0.87894388E 02 | 177.694 | 90.219 | 0.647258 | 3 | 17.964 |
| 0.5822998E 02 | 0.26833795E 01 | 0.58291768E 02 | 2.638 | 0.460 | 0.429263 | 4 | 23.952 |
| -0.2212247E 02 | -0.13390808E 03 | 0.13579469E 03 | 260.624 | 52.175 | 1.000000 | 5 | 29.940 |
| -0.2474284E 00 | -0.34071882E 02 | 0.34072771E 02 | 269.584 | 44.931 | 0.250913 | 6 | 35.928 |
| 0.2320013E 02 | 0.5470360E 01 | 0.23838633E 02 | 13.267 | 1.899 | 0.175532 | 7 | 41.916 |
| -0.1118298E 01 | 0.1941833E 02 | 0.19450508E 02 | 93.296 | 11.662 | 0.143234 | 8 | 47.904 |
| -0.2126674E 02 | 0.22793123E 02 | 0.31128448E 02 | 133.094 | 14.788 | 0.229232 | 9 | 53.892 |
| 0.1361200E 02 | 0.55388093E 00 | 0.13623268E 02 | 2.330 | 0.233 | 0.100322 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 19 TORSION 145

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1892984E 02 | | | | | | | |
| 0.1107544E 03 | 0.11035808E 03 | 0.15635035 03 | 44.897 | 44.897 | 1.000000 | 1 | 5.988 |
| -0.3130446E 02 | 0.39026595E 02 | 0.50034125 02 | 128.100 | 64.050 | 0.320490 | 2 | 11.976 |
| -0.3629654E 02 | 0.11386908E 02 | 0.38016895 02 | 162.697 | 54.232 | 0.243152 | 3 | 17.964 |
| 0.2464693E 02 | -0.10951935E 02 | 0.31086185E 02 | 322.435 | 80.609 | 0.198824 | 4 | 23.952 |
| 0.1459568E 02 | -0.57809135E 02 | 0.59706465E 02 | 284.158 | 56.830 | 0.301877 | 5 | 29.940 |
| 0.5252490E 01 | -0.29906565E 00 | 0.52610025E 01 | 356.741 | 99.457 | 0.033849 | 6 | 35.928 |
| 0.1099496E 01 | 0.11890015E 02 | 0.11936765E 02 | 84.927 | 12.132 | 0.076346 | 7 | 41.916 |
| -0.6759033E 01 | 0.27937585E 01 | 0.73136595E 01 | 157.543 | 19.693 | 0.046777 | 8 | 47.904 |
| -0.7044609E 01 | 0.25935135E 01 | 0.75066505E 01 | 159.789 | 17.754 | 0.048013 | 9 | 53.892 |
| 0.7331773E 01 | -0.36465195E 01 | 0.81885255E 01 | 333.556 | 33.356 | 0.052373 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2467892E 02 | | | | | | | |
| 0.3392758E 02 | 0.34361775E 02 | 0.48285315E 02 | 45.360 | 45.360 | 1.000000 | 1 | 5.988 |
| -0.1427269E 02 | 0.30213605E 01 | 0.14779365E 02 | 169.011 | 82.986 | 0.306001 | 2 | 11.976 |
| 0.2706421E 02 | 0.35962115E 01 | 0.27302085E 02 | 7.569 | 2.523 | 0.565432 | 3 | 17.964 |
| -0.2905797E 02 | -0.10724115E 02 | 0.30977345E 02 | 200.257 | 50.064 | 0.641465 | 4 | 23.952 |
| -0.3323258E 00 | 0.14573475E 02 | 0.14577265E 02 | 91.306 | 18.261 | 0.301890 | 5 | 29.940 |
| 0.1843268E 01 | 0.20662085E 01 | 0.27689605E 01 | 48.265 | 8.044 | 0.057346 | 6 | 35.928 |
| -0.4830538E 00 | 0.43458285E 01 | 0.43717955E 01 | 96.344 | 13.763 | 0.090541 | 7 | 41.916 |
| 0.1124797E 00 | 0.23928085E 01 | 0.23947315E 01 | 87.308 | 10.913 | 0.049595 | 8 | 47.904 |
| -0.1176718E 01 | 0.16285425E 00 | 0.11879255E 01 | 172.125 | 19.124 | 0.024602 | 9 | 53.892 |
| 0.3343222E 00 | 0.45878195E 01 | 0.45999835E 01 | 85.832 | 8.583 | 0.095267 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 502 CTR 188 CR 45.1 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3762203E 01 | | | | | | | |
| 0.1098309E 01 | -0.21879866E 01 | 0.24402105E 01 | 296.657 | 296.657 | 1.000000 | 1 | 5.988 |
| 0.3410737E-02 | 0.32942035-01 | 0.33138015-01 | 84.092 | 42.046 | 0.013536 | 2 | 11.976 |
| -0.5749416E-01 | 0.42744995-02 | 0.57612955-01 | 175.745 | 58.582 | 0.023533 | 3 | 17.964 |
| 0.7172638E-01 | 0.43454866-01 | 0.83862905E-01 | 31.209 | 7.802 | 0.034255 | 4 | 23.952 |
| -0.4105248E-02 | 0.68382025-02 | 0.7975917E-02 | 120.978 | 24.196 | 0.003258 | 5 | 29.940 |
| -0.2264208E-02 | 0.13997698-01 | 0.14179625-01 | 99.188 | 16.531 | 0.005792 | 6 | 35.928 |
| 0.1440837E-01 | -0.3662056E-02 | 0.1485872E-01 | 345.732 | 49.356 | 0.006069 | 7 | 41.916 |
| -0.6992310E-02 | -0.18364305-01 | 0.19650435-01 | 249.155 | 31.144 | 0.008026 | 8 | 47.904 |
| 0.4522532E-02 | 0.78586975-02 | 0.9067103E-02 | 60.080 | 6.376 | 0.003704 | 9 | 53.892 |
| -0.7219987E-02 | 0.2717733E-02 | 0.7708933E-02 | 159.357 | 15.936 | 0.003149 | 10 | 59.880 |

HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 30

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.28712718E 05 | | | | | | | |
| 0.14673468E 05 | 0.42283598E 04 | 0.42308988E 04 | 88.012 | 88.012 | 0.359124 | 1 | 5.917 |
| 0.13807778E 04 | -0.74943718E 04 | 0.75678038E 04 | 279.098 | 139.949 | 1.000030 | 2 | 11.834 |
| 0.19176138E 04 | -0.87616098E 03 | 0.21074628E 04 | 335.494 | 111.891 | 0.278507 | 3 | 17.751 |
| -0.21758078E 03 | -0.70590082E 02 | 0.23067518E 03 | 190.302 | 49.848 | 0.030484 | 4 | 23.669 |
| 0.89812938E 02 | -0.13635748E 04 | 0.13662718E 04 | 273.601 | 94.720 | 0.180956 | 5 | 29.586 |
| 0.13092408E 03 | -0.12841978E 03 | 0.18339208E 03 | 315.553 | 52.592 | 0.024236 | 6 | 35.503 |
| 0.27887908E 03 | 0.16128578E 03 | 0.31496128E 03 | 30.786 | 4.398 | 0.041623 | 7 | 41.420 |
| -0.25780618E 03 | -0.48743698E 01 | 0.25710798E 03 | 181.086 | 22.636 | 0.033977 | 8 | 47.337 |
| 0.38044638E 02 | -0.10994638E 03 | 0.11.46337E 03 | 286.441 | 31.827 | 0.015149 | 9 | 53.254 |
| 0.44129288E 02 | -0.92829538E 02 | 0.68835578E 02 | 309.872 | 30.987 | 0.009097 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.14387648E 04 | | | | | | | |
| 0.76312968E 03 | 0.74114188E 03 | 0.10637948E 04 | 44.163 | 44.163 | 1.000030 | 1 | 5.917 |
| -0.91777538E 02 | -0.14083228E 03 | 0.14993898E 03 | 249.749 | 124.874 | 0.140818 | 2 | 11.834 |
| -0.60878498E 02 | -0.10888128E 03 | 0.10445448E 03 | 292.040 | 84.013 | 0.104673 | 3 | 17.751 |
| 0.19821468E 03 | 0.14711498E 03 | 0.24524088E 03 | 36.841 | 9.215 | 0.230384 | 4 | 23.669 |
| 0.16709978E 03 | 0.79524298E 03 | 0.77367218E 03 | 77.469 | 15.494 | 0.727276 | 5 | 29.586 |
| -0.10906378E 03 | 0.49788378E 02 | 0.12040948E 03 | 155.987 | 25.931 | 0.113109 | 6 | 35.503 |
| -0.22942188E 03 | -0.19312268E 03 | 0.29988838E 03 | 220.090 | 31.441 | 0.281988 | 7 | 41.420 |
| 0.30858488E 03 | 0.89995828E 02 | 0.39974418E 03 | 12.423 | 1.553 | 0.375772 | 8 | 47.337 |
| 0.23395288E 02 | 0.15888888E 03 | 0.16078848E 03 | 81.629 | 9.070 | 0.151083 | 9 | 53.254 |
| -0.90428428E 02 | 0.78938218E 02 | 0.87882368E 02 | 125.488 | 12.541 | 0.081813 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.18388788E 03 | | | | | | | |
| 0.10995948E 04 | -0.54614258E 03 | 0.12323098E 04 | 332.755 | 332.755 | 1.000000 | 1 | 5.917 |
| -0.33348648E 03 | 0.98716448E 03 | 0.98651228E 03 | 110.183 | 99.091 | 0.784318 | 2 | 11.834 |
| -0.19913918E 03 | 0.28915898E 02 | 0.19726998E 03 | 171.571 | 97.198 | 0.160082 | 3 | 17.751 |
| 0.68977918E 02 | 0.18914938E 03 | 0.12502758E 03 | 60.009 | 15.282 | 0.101498 | 4 | 23.669 |
| 0.67482748E 02 | 0.45386298E 03 | 0.45861698E 03 | 81.542 | 16.308 | 0.372161 | 5 | 29.586 |
| -0.67454838E 02 | 0.32838278E 02 | 0.76934728 02 | 154.182 | 25.697 | 0.060000 | 6 | 35.503 |
| 0.20888888E 02 | 0.34128368E 02 | 0.39582128 02 | 99.553 | 8.508 | 0.032128 | 7 | 41.420 |
| -0.67791648E 00 | -0.38114648E 02 | 0.38120698E 02 | 268.981 | 33.623 | 0.030954 | 8 | 47.337 |
| 0.50884018E 02 | -0.10984848E 02 | 0.51996188E 02 | 348.560 | 38.729 | 0.042162 | 9 | 53.254 |
| 0.22883458E 02 | -0.14442088E 02 | 0.26497018E 02 | 326.453 | 32.645 | 0.021502 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.88239828E 03 | | | | | | | |
| 0.12349088E 04 | -0.10376798E 04 | 0.16126958E 04 | 319.951 | 319.951 | 1.000000 | 1 | 5.917 |
| -0.21161298E 03 | 0.10202408E 04 | 0.10419038E 04 | 101.718 | 50.859 | 0.646188 | 2 | 11.834 |
| -0.16988178E 03 | 0.46828818E 03 | 0.49778888E 03 | 159.853 | 34.618 | 0.308669 | 3 | 17.751 |
| -0.10488148E 02 | -0.61138888E 02 | 0.62023298E 02 | 260.316 | 65.079 | 0.038448 | 4 | 23.669 |
| -0.27944798E 02 | -0.11578348E 03 | 0.11898618E 03 | 256.615 | 51.323 | 0.073781 | 5 | 29.586 |
| 0.88216788E 01 | 0.63598888E 02 | 0.64086768E 02 | 82.717 | 13.786 | 0.039727 | 6 | 35.503 |
| 0.81998838E 02 | 0.11328548E 03 | 0.13944068E 03 | 54.302 | 7.757 | 0.086489 | 7 | 41.420 |
| -0.26262798E 03 | -0.27268698E 02 | 0.20445018E 03 | 187.665 | 23.458 | 0.126775 | 8 | 47.337 |
| -0.71988688E 02 | -0.34988858E 02 | 0.79658058E 02 | 206.017 | 22.891 | 0.049394 | 9 | 53.254 |
| -0.31994488E 02 | -0.48761118E 02 | 0.51448788E 02 | 232.398 | 23.268 | 0.031903 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 39

HARMONIC ANALYSIS MODEL XH-91A SHIP 1082C T 494 CTR 226 CR 8.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1024690E 04 | | | | | | | |
| 0.9208774E 03 | -0.1004055E 04 | 0.1362403E 04 | 312.526 | 312.526 | 1.000000 | 1 | 5.917 |
| -0.6739284E 02 | 0.6678379E 03 | 0.6735315E 03 | 97.455 | 48.728 | 0.494370 | 2 | 11.834 |
| 0.7517944E 01 | 0.6881763E 00 | 0.6882178E 03 | 89.357 | 29.789 | 0.499278 | 3 | 17.751 |
| -0.5201764E 02 | -0.7390961E 02 | 0.9037941E 02 | 234.862 | 58.714 | 0.066338 | 4 | 23.669 |
| -0.2259048E 03 | -0.6248821E 03 | 0.6644897E 03 | 250.118 | 50.024 | 0.487734 | 5 | 29.586 |
| 0.7135876E 02 | -0.5927849E 02 | 0.9276849E 02 | 320.283 | 53.380 | 0.068092 | 6 | 35.503 |
| -0.8377419E 02 | -0.6719867E 01 | 0.8484284E 02 | 184.583 | 26.369 | 0.061687 | 7 | 41.420 |
| 0.4862964E 02 | -0.3806999E 01 | 0.4878552E 02 | 355.418 | 44.427 | 0.035808 | 8 | 47.337 |
| 0.2387237E 01 | 0.5941682E 02 | 0.5944159E 02 | 87.776 | 9.753 | 0.043645 | 9 | 53.254 |
| -0.4922217E 02 | 0.3741492E 02 | 0.6182796E 02 | 142.761 | 14.276 | 0.045382 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-91A SHIP 1082C T 494 CTR 226 CR 8.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1134v842E 04 | | | | | | | |
| 0.5093810E 03 | -0.8044312E 03 | 0.9972263E 03 | 306.229 | 306.229 | 1.000000 | 1 | 5.917 |
| -0.8009992E 00 | 0.3310432E 03 | 0.3310439E 03 | 90.139 | 45.069 | 0.331961 | 2 | 11.834 |
| 0.2590624E 03 | 0.7327217E 03 | 0.7765803E 03 | 71.093 | 23.698 | 0.778655 | 3 | 17.751 |
| -0.3629454E 02 | 0.3789334E 02 | 0.5186795E 02 | 134.407 | 33.602 | 0.052011 | 4 | 23.669 |
| -0.3941994E 03 | -0.7893862E 03 | 0.8822582E 03 | 243.444 | 48.693 | 0.884695 | 5 | 29.586 |
| 0.8226441E 02 | -0.2692844E 03 | 0.2815728E 03 | 286.988 | 47.831 | 0.282352 | 6 | 35.503 |
| -0.7172138E 02 | -0.1366607E 03 | 0.1816216E 03 | 244.741 | 33.249 | 0.182125 | 7 | 41.420 |
| 0.2738804E 03 | -0.1413326E 03 | 0.2742524E 03 | 337.046 | 44.631 | 0.275012 | 8 | 47.337 |
| 0.1311854E 03 | 0.9912990E 02 | 0.1642287E 03 | 22.704 | 2.933 | 0.142693 | 9 | 53.254 |
| -0.2820984E-01 | 0.2440573E 02 | 0.2440573E 02 | 90.068 | 9.003 | 0.024473 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-91A SHIP 1082C T 494 CTR 226 CR 8.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6792131E 03 | | | | | | | |
| 0.2321592E 03 | -0.4240945E 03 | 0.4834818E 03 | 290.697 | 290.697 | 0.656482 | 1 | 5.917 |
| -0.1191214E 02 | 0.3005933E 02 | 0.3233340E 02 | 111.618 | 55.809 | 0.043903 | 2 | 11.834 |
| 0.3829751E 03 | 0.5918521E 03 | 0.7049529E 03 | 57.094 | 19.031 | 0.957201 | 3 | 17.751 |
| 0.2842688E 02 | 0.7207605E 02 | 0.7491446E 02 | 74.177 | 18.544 | 0.101721 | 4 | 23.669 |
| -0.3203743E 03 | -0.6631387E 03 | 0.7364729E 03 | 244.214 | 48.843 | 1.000000 | 5 | 29.586 |
| 0.9147433E 02 | -0.3032285E 03 | 0.3167253E 03 | 286.787 | 47.798 | 0.430057 | 6 | 35.503 |
| -0.5137193E 00 | -0.2022643E 03 | 0.2022644E 03 | 269.854 | 38.551 | 0.274443 | 7 | 41.420 |
| 0.3499129E 03 | 0.6480365E 02 | 0.3551521E 03 | 9.667 | 1.242 | 0.509590 | 8 | 47.337 |
| 0.1246345E 03 | 0.4603401E 02 | 0.1328042E 03 | 20.272 | 2.292 | 0.180406 | 9 | 53.254 |
| 0.7951221E 02 | 0.7493219E 01 | 0.7987099E 02 | 5.637 | 0.564 | 0.108838 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-91A SHIP 1082C T 494 CTR 226 CR 8.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.3620769E 03 | | | | | | | |
| 0.8290074E 01 | -0.1597092E 03 | 0.1599245E 03 | 272.973 | 272.973 | 0.264243 | 1 | 5.917 |
| -0.1981270E 02 | -0.1052658E 03 | 0.1071141E 03 | 259.341 | 129.670 | 0.176984 | 2 | 11.834 |
| 0.4200852E 03 | 0.4356809E 03 | 0.6052183E 03 | 46.044 | 15.348 | 1.000000 | 3 | 17.751 |
| 0.9884776E 02 | 0.1157987E 03 | 0.1522505E 03 | 49.515 | 12.379 | 0.251563 | 4 | 23.669 |
| -0.2820703E 03 | -0.4397129E 03 | 0.5224087E 03 | 237.320 | 47.464 | 0.863174 | 5 | 29.586 |
| 0.4855558E 02 | -0.2567209E 03 | 0.2612722E 03 | 280.710 | 46.785 | 0.431699 | 6 | 35.503 |
| 0.2934467E 02 | -0.1764378E 03 | 0.1788642E 03 | 279.450 | 39.921 | 0.295537 | 7 | 41.420 |
| 0.3633604E 03 | 0.3800081E 02 | 0.3653961E 03 | 5.989 | 0.748 | 0.603667 | 8 | 47.337 |
| 0.1294125E 03 | 0.3579367E 02 | 0.1342713E 03 | 15.462 | 1.718 | 0.221856 | 9 | 53.254 |
| 0.1088188E 03 | -0.4362099E 02 | 0.1172362E 03 | 338.156 | 33.816 | 0.193709 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 39

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.8794492E 04 | | | | | | | |
| -0.1157437E 04 | 0.4079753E 05 | 0.4081394E 05 | 91.625 | 91.625 | 1.000000 | 1 | 5.917 |
| -0.3360615E 04 | -0.2960286E 03 | 0.3373627E 04 | 185.034 | 92.517 | 0.082659 | 2 | 11.834 |
| -0.6660918E 03 | -0.1044960E 04 | 0.1257808E 04 | 238.024 | 79.341 | 0.030818 | 3 | 17.751 |
| -0.4970359E 03 | -0.6162173E 02 | 0.5008411E 03 | 187.067 | 46.767 | 0.012271 | 4 | 23.669 |
| 0.2881280E 03 | -0.4739680E 03 | 0.7053723E 03 | 287.161 | 57.432 | 0.017283 | 5 | 29.586 |
| 0.1849592E 03 | -0.1270454E 03 | 0.2243727E 03 | 325.512 | 54.252 | 0.005497 | 6 | 35.503 |
| -0.2066355E 03 | -0.2300582E 03 | 0.3092327E 03 | 228.070 | 32.581 | 0.007577 | 7 | 41.420 |
| 0.6649814E 01 | -0.9047285E 03 | 0.9047515E 03 | 270.410 | 33.801 | 0.022168 | 8 | 47.337 |
| -0.3595159E 03 | 0.3710622E 03 | 0.5166467E 03 | 134.096 | 14.900 | 0.012659 | 9 | 53.254 |
| -0.2046339E 02 | 0.8885931E 02 | 0.9129861E 02 | 103.274 | 10.327 | 0.002237 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1676280E 05 | | | | | | | |
| -0.1594713E 04 | 0.2521765E 05 | 0.2526592E 05 | 93.528 | 93.528 | 1.000000 | 1 | 5.917 |
| -0.1914611E 04 | 0.2390942E 02 | 0.1914768E 04 | 179.285 | 89.642 | 0.075785 | 2 | 11.834 |
| 0.1048969E 02 | -0.2002964E 03 | 0.2005709E 03 | 272.998 | 90.999 | 0.007939 | 3 | 17.751 |
| 0.6628232E 03 | 0.5523545E 03 | 0.8620835E 03 | 39.886 | 9.951 | 0.034149 | 4 | 23.669 |
| -0.3632583E 03 | -0.3458687E 03 | 0.5015791E 03 | 223.595 | 44.719 | 0.019852 | 5 | 29.586 |
| 0.1324498E 03 | 0.8410635E 03 | 0.8514316E 03 | 81.049 | 13.508 | 0.033699 | 6 | 35.503 |
| 0.6833493E 01 | 0.3440754E 03 | 0.3441426E 03 | 88.867 | 12.695 | 0.013621 | 7 | 41.420 |
| -0.8790082E 02 | 0.1143876E 03 | 0.1443141E 03 | 127.568 | 15.946 | 0.005712 | 8 | 47.337 |
| 0.1020581E 03 | -0.1008844E 03 | 0.1409599E 03 | 313.246 | 34.805 | 0.005896 | 9 | 53.254 |
| 0.1622721E 03 | 0.3197609E 02 | 0.1693197E 03 | 11.011 | 1.101 | 0.006943 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 8 CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1026644E 05 | | | | | | | |
| -0.1679504E 04 | 0.1052139E 05 | 0.1957662E 05 | 95.859 | 95.859 | 1.000000 | 1 | 5.917 |
| -0.7605060E 03 | -0.2518264E 03 | 0.8008658E 03 | 198.267 | 99.133 | 0.075720 | 2 | 11.834 |
| 0.4806607E 02 | -0.3363335E 03 | 0.3397509E 03 | 278.133 | 92.711 | 0.032123 | 3 | 17.751 |
| 0.9097622E 03 | 0.4299851E 03 | 0.1002643E 04 | 25.394 | 6.349 | 0.094798 | 4 | 23.669 |
| -0.3888215E 03 | 0.2561287E 03 | 0.4656004E 03 | 146.626 | 29.325 | 0.044022 | 5 | 29.586 |
| 0.1341632E 03 | 0.7716499E 03 | 0.7832227E 03 | 80.138 | 13.356 | 0.074053 | 6 | 35.503 |
| 0.2248916E 03 | 0.4767249E 03 | 0.5271079E 03 | 64.765 | 9.249 | 0.049837 | 7 | 41.420 |
| 0.2065970E 03 | 0.7286399E 03 | 0.7573099E 03 | 74.174 | 9.272 | 0.071611 | 8 | 47.337 |
| 0.3490283E 03 | -0.4084534E 03 | 0.5374888E 03 | 310.723 | 34.525 | 0.050582 | 9 | 53.254 |
| 0.1223604E 03 | -0.9584963E 02 | 0.1345013E 03 | 335.469 | 33.547 | 0.012717 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 12 CH. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7085109E 04 | | | | | | | |
| -0.5640635E 03 | 0.4181746E 04 | 0.4219613E 04 | 97.682 | 97.682 | 1.000000 | 1 | 5.917 |
| -0.4609590E 03 | -0.7459694E 02 | 0.4672795E 03 | 189.435 | 94.717 | 0.110740 | 2 | 11.834 |
| 0.1270994E 02 | -0.1412404E 03 | 0.1418112E 03 | 275.142 | 91.714 | 0.033608 | 3 | 17.751 |
| 0.4428109E 03 | 0.9817534E 02 | 0.4518090E 03 | 11.510 | 2.878 | 0.107095 | 4 | 23.669 |
| -0.1203381E 03 | 0.2735469E 03 | 0.3013304E 03 | 114.788 | 22.958 | 0.071412 | 5 | 29.586 |
| 0.1051395E 03 | 0.4537875E 03 | 0.4657302E 03 | 76.953 | 12.825 | 0.110373 | 6 | 35.503 |
| 0.2221903E 03 | 0.3779761E 03 | 0.4384148E 03 | 59.558 | 8.508 | 0.103899 | 7 | 41.420 |
| 0.3089148E 03 | 0.4942778E 03 | 0.5828711E 03 | 57.995 | 7.249 | 0.138134 | 8 | 47.337 |
| 0.1081952E 03 | -0.3339038E 03 | 0.3508040E 03 | 287.641 | 31.960 | 0.083037 | 9 | 53.254 |
| 0.5814404E 02 | -0.4437706E 02 | 0.7314452E 02 | 322.648 | 32.265 | 0.017334 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 39

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.19113296 03 | | | | | | | |
| 0.14201536 03 | -0.97335826 02 | 0.17217036 03 | 329.573 | 329.573 | 0.662199 | 1 | 5.917 |
| -0.13685086 03 | 0.10346916 03 | 0.17094386 03 | 142.742 | 71.371 | 0.657482 | 2 | 11.834 |
| -0.43194086 02 | -0.19581896 03 | 0.16164946 03 | 294.986 | 84.835 | 0.621909 | 3 | 17.751 |
| 0.97682396 01 | 0.12601146 03 | 0.12838396 03 | 85.676 | 21.409 | 0.493787 | 4 | 23.669 |
| -0.59457146 02 | -0.25310836 03 | 0.25999786 03 | 256.789 | 51.396 | 1.000000 | 5 | 29.586 |
| 0.65146976 02 | 0.77009606 02 | 0.10086926 03 | 49.778 | 8.295 | 0.387962 | 6 | 35.503 |
| 0.49063726 02 | 0.68371666 02 | 0.68884496 02 | 44.605 | 6.372 | 0.264963 | 7 | 41.420 |
| -0.24192926 02 | -0.27657186 02 | 0.36745296 02 | 228.822 | 28.603 | 0.141329 | 8 | 47.337 |
| 0.72520486 00 | 0.42656996 01 | 0.43269076 01 | 80.351 | 8.928 | 0.016642 | 9 | 53.254 |
| -0.48150226 01 | 0.26273326 02 | 0.26710886 02 | 100.305 | 10.039 | 0.102795 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 19 TORSION 165

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.11038316 03 | | | | | | | |
| 0.44625236 02 | 0.42517986 02 | 0.61637506 02 | 43.615 | 43.615 | 0.610092 | 1 | 5.917 |
| -0.99323946 02 | -0.73246 46 01 | 0.99593256 02 | 184.218 | 92.109 | 1.000000 | 2 | 11.834 |
| 0.23390476 02 | -0.53125346 02 | 0.58044076 02 | 293.769 | 97.923 | 0.582661 | 3 | 17.751 |
| 0.27562536 02 | 0.66006916 02 | 0.66844026 02 | 65.648 | 16.412 | 0.671178 | 4 | 23.669 |
| -0.39408946 02 | -0.71815096 02 | 0.81913606 02 | 241.249 | 48.250 | 0.822482 | 5 | 29.586 |
| 0.42962546 01 | 0.80993506 01 | 0.91047416 01 | 62.845 | 10.341 | 0.092022 | 6 | 35.503 |
| 0.23279086 02 | 0.65512356 01 | 0.24188106 02 | 15.728 | 2.246 | 0.242789 | 7 | 41.420 |
| 0.09591536 01 | -0.32906096 01 | 0.95433036 01 | 339.778 | 42.472 | 0.095824 | 8 | 47.337 |
| 0.58021366-01 | 0.13654026 02 | 0.13654046 02 | 89.753 | 9.973 | 0.137107 | 9 | 53.254 |
| 0.51355926 01 | 0.95719306 01 | 0.79911466 01 | 47.222 | 4.722 | 0.076221 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.81945066 02 | | | | | | | |
| -0.59265096 02 | 0.14283276 03 | 0.15423986 03 | 112.192 | 112.192 | 1.000000 | 1 | 5.917 |
| 0.41778706 02 | -0.16374716 02 | 0.44873856 02 | 338.598 | 169.299 | 0.290893 | 2 | 11.834 |
| 0.33471136 02 | 0.27237906 02 | 0.43193236 02 | 39.137 | 13.046 | 0.279746 | 3 | 17.751 |
| 0.35167466 01 | -0.26597136 02 | 0.28574366 02 | 277.069 | 69.267 | 0.185239 | 4 | 23.669 |
| -0.17842196 02 | 0.23 J0466 02 | 0.29187946 02 | 127.679 | 25.536 | 0.189810 | 5 | 29.586 |
| 0.33409716 01 | -0.19616836 02 | 0.19900016 02 | 279.691 | 46.615 | 0.129083 | 6 | 35.503 |
| 0.44857146 01 | 0.26861466 01 | 0.52284876 01 | 30.914 | 4.416 | 0.033894 | 7 | 41.420 |
| -0.11646176 01 | 0.18244976 01 | 0.19912546 01 | 138.667 | 17.333 | 0.018086 | 8 | 47.337 |
| 0.10537166 01 | 0.49552866 01 | 0.50459996 01 | 77.995 | 8.666 | 0.032801 | 9 | 53.254 |
| 0.23731016 00 | -0.89992056 00 | 0.93071276 00 | 284.777 | 28.478 | 0.006093 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 226 CR 8.0 TR 26 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.31653866 01 | | | | | | | |
| 0.12936186 01 | -0.16921426 01 | 0.21059216 01 | 306.533 | 306.533 | 1.000000 | 1 | 5.917 |
| -0.37518596-01 | 0.68277966-01 | 0.77907696-01 | 118.789 | 59.394 | 0.036994 | 2 | 11.834 |
| -0.32625096-01 | -0.13852176-01 | 0.35444026-01 | 203.005 | 67.668 | 0.016831 | 3 | 17.751 |
| -0.57847916-01 | 0.86585006-01 | 0.10406606 00 | 123.773 | 30.943 | 0.049416 | 4 | 23.669 |
| 0.38889256-02 | -0.13950096-01 | 0.14481706-01 | 285.577 | 57.115 | 0.006877 | 5 | 29.586 |
| -0.36006776-02 | 0.29101976-01 | 0.29131906-01 | 97.032 | 16.172 | 0.013967 | 6 | 35.503 |
| -0.19986686-01 | 0.43412826-02 | 0.20452736-01 | 167.745 | 23.964 | 0.009712 | 7 | 41.420 |
| 0.33746126-01 | 0.21356266-01 | 0.39932116-01 | 32.331 | 4.041 | 0.013962 | 8 | 47.337 |
| -0.61162826-02 | 0.84237756-02 | 0.10410046-01 | 125.982 | 13.998 | 0.004943 | 9 | 53.254 |
| 0.12677936-01 | 0.10304776-01 | 0.16236546-01 | 39.108 | 3.911 | 0.007757 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 40

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.27186368 05 | | | | | | | |
| 0.6921643E 03 | 0.31350178 04 | 0.32105188 04 | 77.550 | 77.550 | 0.376763 | 1 | 5.988 |
| -0.3983740E 03 | -0.8512000F 04 | 0.8521312E 04 | 267.320 | 133.660 | 1.000000 | 2 | 11.976 |
| 0.9454687E 03 | -0.2191116E 04 | 0.2386441E 04 | 293.340 | 97.780 | 0.280056 | 3 | 17.964 |
| 0.2983941E-01 | 0.1272444E 03 | 0.1272446E 03 | 89.987 | 22.497 | 0.014933 | 4 | 23.952 |
| -0.1463706E 04 | -0.1499862E 04 | 0.2239554E 04 | 229.189 | 49.838 | 0.262818 | 5 | 29.940 |
| 0.1705820E 03 | -0.5695308E 03 | 0.6137136E 03 | 286.138 | 47.690 | 0.072021 | 6 | 35.928 |
| 0.1712112E 03 | -0.2083019E 03 | 0.2696345E 03 | 309.418 | 44.203 | 0.031642 | 7 | 41.916 |
| -0.1318079E 03 | 0.9774380E 02 | 0.1648947E 03 | 143.441 | 17.930 | 0.019257 | 8 | 47.904 |
| 0.9364040E C1 | -0.1012741E 03 | 0.1017061E 03 | 275.283 | 30.587 | 0.011935 | 9 | 53.892 |
| -0.9166850E 02 | -0.1447005E 03 | 0.1712932E 03 | 237.645 | 23.765 | 0.070102 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5790034E 03 | | | | | | | |
| 0.9771074E C3 | 0.3310188E 03 | 0.1031659E 04 | 18.715 | 18.715 | 0.904170 | 1 | 5.988 |
| -0.3312282E 02 | -0.3229473E 03 | 0.3246411E 03 | 264.147 | 132.072 | 0.284524 | 2 | 11.976 |
| -0.1521621E 03 | -0.1124617E 03 | 0.1892114E 03 | 216.468 | 72.156 | 0.165838 | 3 | 17.964 |
| 0.2582505E 03 | -0.1207094E 02 | 0.2585322E 03 | 357.324 | 89.331 | 0.226585 | 4 | 23.952 |
| 0.8373059E 03 | 0.7751874E 03 | 0.1140994E 04 | 42.791 | 8.558 | 1.000000 | 5 | 29.940 |
| -0.6290068E 02 | 0.2984887E 03 | 0.3058493E 03 | 101.900 | 16.983 | 0.267949 | 6 | 35.928 |
| -0.3676812E 03 | 0.1087[illegible]E 02 | 0.3678416E 03 | 178.306 | 29.472 | 0.322306 | 7 | 41.916 |
| 0.9164138E 03 | -0.1809857E 03 | 0.3689594E 03 | 329.151 | 41.144 | 0.323812 | 8 | 47.904 |
| 0.2125842E C3 | 0.5877175E 02 | 0.2189630E 03 | 13.432 | 1.492 | 0.191955 | 9 | 53.892 |
| 0.6888279E 02 | 0.1846323E 03 | 0.1967898E 03 | 69.759 | 6.976 | 0.172466 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.4191211E 03 | | | | | | | |
| 0.1043969E 04 | -0.96[illegible]12E 03 | 0.1291990E 04 | 323.928 | 323.928 | 1.000000 | 1 | 5.988 |
| -0.1499436E 03 | 0.9358879E 01 | 0.9478232E 03 | 99.152 | 49.591 | 0.733939 | 2 | 11.976 |
| -0.8954954E 02 | 0.1249422E 03 | 0.1514219E 03 | 124.399 | 41.466 | 0.117236 | 3 | 17.964 |
| 0.1572449E 03 | -0.4721983E 02 | 0.1641866E 03 | 343.286 | 85.821 | 0.127119 | 4 | 23.952 |
| 0.4982500E 03 | 0.4389410E 03 | 0.6781411E 03 | 43.783 | 8.741 | 0.525042 | 5 | 29.940 |
| -0.3202341E 02 | 0.3311656E 02 | 0.4202312E 02 | 121.085 | 20.181 | 0.040621 | 6 | 35.928 |
| 0.2401303E 02 | -0.3390869E 01 | 0.2425122E 02 | 351.943 | 50.280 | 0.018776 | 7 | 41.916 |
| -0.1191894E 02 | 0.1969044E 02 | 0.2302368E 02 | 121.177 | 15.147 | 0.017826 | 8 | 47.904 |
| -9.6604166E 02 | -0.2468787E 02 | 0.7843544E 02 | 200.344 | 22.260 | 0.034594 | 9 | 53.892 |
| -0.4010591E 02 | -0.6723480E 02 | 0.7830055E 02 | 239.058 | 29.906 | 0.060693 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4735269E C3 | | | | | | | |
| 0.1215405E 04 | -0.1305194E 04 | 0.1783518E 04 | 312.962 | 312.962 | 1.000000 | 1 | 5.988 |
| -0.5862956E 02 | 0.1124262E 04 | 0.1129401E 04 | 92.579 | 46.289 | 0.631006 | 2 | 11.976 |
| 0.1472046E 03 | 0.5790959E 03 | 0.5983866E 03 | 75.769 | 25.250 | 0.335464 | 3 | 17.964 |
| 0.4995035E 01 | -0.8421342E 02 | 0.8436140E 02 | 273.395 | 68.349 | 0.047301 | 4 | 23.952 |
| -0.1976549E 03 | -0.1208576E 03 | 0.1986496E 03 | 217.474 | 43.495 | 0.111381 | 5 | 29.940 |
| 0.1465297E 02 | -0.2997838E 02 | 0.3336777E 02 | 296.049 | 49.341 | 0.018709 | 6 | 35.928 |
| 0.1676062E 03 | 0.4192479E 02 | 0.1731654E 03 | 14.597 | 2.080 | 0.097092 | 7 | 41.916 |
| -0.1352912E 03 | 0.1422476E 03 | 0.1963112E 03 | 133.944 | 16.656 | 0.110078 | 8 | 47.904 |
| -0.7063676E 02 | 0.9296291E 02 | 0.1284791E 03 | 129.502 | 14.389 | 0.067591 | 9 | 53.892 |
| -0.1244301E 02 | 0.8408522E 01 | 0.1501838E 02 | 145.952 | 16.595 | 0.008421 | 10 | 59.880 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 40

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8426833E 03 | | | | | | | |
| 0.8769021E 03 | -0.1[illegible]34917E 04 | 0.1514588E 04 | 305.378 | 305.378 | 1.000000 | 1 | 5.988 |
| -0.7508897E 02 | 0.7[illegible]000786E 03 | 0.7338591E 03 | 95.873 | 47.936 | 0.484527 | 2 | 11.976 |
| 0.3900947E 03 | 0.7287236E 03 | 0.8265662E 03 | 61.839 | 20.613 | 0.545736 | 3 | 17.964 |
| -0.4313220E 02 | -0.6854329E 02 | 0.8099492E 02 | 237.819 | 59.455 | 0.053470 | 4 | 23.952 |
| -0.6910928E 03 | -0.5244895E 03 | 0.8675810E 03 | 217.196 | 43.439 | 0.572817 | 5 | 29.940 |
| 0.6794850E 02 | -0.1464425E 03 | 0.1614385E 03 | 294.891 | 49.148 | 0.106589 | 6 | 35.928 |
| -0.3872768F C2 | 0.2747142E 02 | 0.4748169E 02 | 144.650 | 20.664 | 0.031350 | 7 | 41.916 |
| 0.3120229E 02 | -0.1413309E 02 | 0.3425385E 02 | 335.632 | 41.954 | 0.022616 | 8 | 47.904 |
| 0.6421468F 02 | 0.4413174E 02 | 0.7791747E 02 | 34.499 | 3.833 | 0.051445 | 9 | 53.892 |
| 0.2171872E 02 | 0.7133864E 02 | 0.7457143E 02 | 73.067 | 7.307 | 0.049235 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8512458E 03 | | | | | | | |
| 0.5342959E 03 | -0.9800598E 03 | 0.1116239E 04 | 298.598 | 298.598 | 0.986767 | 1 | 5.988 |
| -0.5307588E 02 | 0.3808857E 03 | 0.3845657E 03 | 97.933 | 48.967 | 0.339960 | 2 | 11.976 |
| 0.6124189E 03 | 0.7539365E 03 | 0.9713271E 03 | 50.913 | 16.971 | 0.858664 | 3 | 17.964 |
| 0.9526221E 02 | 0.5586128E 02 | 0.1104326E 03 | 30.387 | 7.597 | 0.097624 | 4 | 23.952 |
| -0.8785000E 03 | -0.7126505E 03 | 0.1131200E 04 | 219.049 | 43.810 | 1.000000 | 5 | 29.940 |
| -0.5064196E 01 | -0.2449368E 03 | 0.2449892E 03 | 268.815 | 44.803 | 0.216573 | 6 | 35.928 |
| -0.2147144E C3 | -0.1626681E 03 | 0.2693752E 03 | 217.148 | 31.021 | 0.238131 | 7 | 41.916 |
| 0.1147798E 03 | -0.1936045E 03 | 0.2250713E 03 | 300.662 | 37.583 | 0.198965 | 8 | 47.904 |
| 0.7278210E 02 | -0.1003604E 03 | 0.1239801E 03 | 305.948 | 33.994 | 0.109600 | 9 | 53.892 |
| 0.7608517E 02 | 0.2044871E 01 | 0.2616519E 02 | 4.482 | 0.448 | 0.023130 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6076440E 03 | | | | | | | |
| 0.1622559E 03 | -0.5433301E 03 | 0.5670398E 03 | 286.627 | 286.627 | 0.562826 | 1 | 5.988 |
| -0.8798389E 02 | 0.8922492E 01 | 0.8843513E 02 | 174.209 | 87.105 | 0.087778 | 2 | 11.976 |
| 0.7038739E 03 | 0.5081614E 03 | 0.8681392E 03 | 35.827 | 11.942 | 0.861687 | 3 | 17.964 |
| 0.1718581E 03 | 0.1166555E 03 | 0.2077106E 03 | 34.168 | 8.542 | 0.206167 | 4 | 23.952 |
| -0.8112715E 03 | -0.5973869E 03 | 0.1007488E 04 | 216.366 | 43.273 | 1.000000 | 5 | 29.940 |
| -0.1258474E C3 | -0.2937742E 03 | 0.3199947E 03 | 246.811 | 41.135 | 0.317219 | 6 | 35.928 |
| -0.1962671E 02 | -0.2606042E 03 | 0.3262441E 03 | 233.016 | 33.288 | 0.323820 | 7 | 41.916 |
| 0.2348891E 03 | -0.2488812E 03 | 0.3422202E 03 | 313.343 | 39.168 | 0.339677 | 8 | 47.904 |
| 0.1104324E 0 | -0.1757409E 03 | 0.2375577E 03 | 302.145 | 33.572 | 0.2[illegible]0[illegible]5 | 9 | 53.892 |
| 0.2079174E C2 | -0.1103064E 03 | 0.1121554E 03 | 280.418 | 28.042 | 0.111322 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.3318503F 03 | | | | | | | |
| -0.2662125E 02 | -0.2502608E 03 | 0.2516728E 03 | 263.928 | 263.928 | 0.340983 | 1 | 5.988 |
| -0.1090392E 03 | -0.1595062E 03 | 0.1932120E 03 | 235.644 | 117.822 | 0.261715 | 2 | 11.976 |
| 0.6671528E 03 | 0.3192839E 03 | 0.6859858E 03 | 27.739 | 9.246 | 0.929202 | 3 | 17.964 |
| 0.2323573E 03 | 0.1286376F 03 | 0.2655889E 03 | 28.970 | 7.242 | 0.359753 | 4 | 23.952 |
| -0.6298003F 03 | -0.3851863E 03 | 0.7382524E 03 | 211.450 | 42.290 | 1.000000 | 5 | 29.940 |
| -0.1482397E C3 | -0.2495644E 03 | 0.2868394E 03 | 238.882 | 39.814 | 0.388538 | 6 | 35.928 |
| -0.1793116E 03 | -0.2115020E 03 | 0.2772825E 03 | 229.709 | 32.816 | 0.375593 | 7 | 41.916 |
| 0.2187621E 03 | -0.2390944E 03 | 0.3240320E 03 | 312.449 | 39.056 | 0.438518 | 8 | 47.904 |
| 0.3 5406F 02 | -0.1679294E 03 | 0.1712292E 03 | 281.267 | 31.252 | 0.231939 | 9 | 53.892 |
| -0.1329189E C1 | -0.1258492E 03 | 0.1258562E 03 | 269.395 | 26.939 | 0.170478 | 10 | 59.880 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 40

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.93321027 04 | | | | | | | |
| 0.4189031E 04 | 0.398335CE 05 | 0.4005316E 05 | 83.997 | 83.997 | 1.000000 | 1 | 5.988 |
| -0.240775.E 04 | 0.2114580E 04 | 0.3204487E 04 | 138.709 | 69.355 | 0.080006 | 2 | 11.976 |
| -0.1484528E 04 | -0.4687576E 03 | 0.1556777E 04 | 197.524 | 65.841 | 0.038868 | 3 | 17.964 |
| -0.5486514E 03 | 0.1249548E 02 | 0.5487935E 03 | 178.695 | 44.674 | 0.013702 | 4 | 23.952 |
| -0.2112650E 03 | -0.5375369E 03 | 0.5775906E 03 | 248.545 | 49.709 | 0.014421 | 5 | 29.940 |
| -0.8415141E C2 | 0.3247146E 03 | 0.3354414E 03 | 104.529 | 17.421 | 0.008375 | 6 | 35.928 |
| -0.4795183E 03 | 0.1542945E 03 | 0.5037305E 03 | 162.163 | 23.166 | 0.012577 | 7 | 41.916 |
| -0.1234085E 04 | -0.6515999E 03 | 0.1397314E 04 | 207.796 | 25.974 | 0.034886 | 8 | 47.904 |
| 0.2187847E 03 | 0.1112323E 04 | 0.1133538E 04 | 78.897 | 8.766 | 0.028301 | 9 | 53.892 |
| 0.1294401E C3 | 0.2853503E 03 | 0.3134187E 03 | 65.567 | 6.557 | 0.007825 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1304143E 05 | | | | | | | |
| 0.1775114E C4 | 0.2465544E 05 | 0.2471925E 05 | 85.882 | 85.882 | 1.000000 | 1 | 5.988 |
| -0.1359565E 04 | 0.1908234E 04 | 0.2343027E 04 | 125.469 | 62.734 | 0.094785 | 2 | 11.976 |
| -0.4716943E 03 | -0.3149968E 03 | 0.5683194E 03 | 213.903 | 71.301 | 0.022991 | 3 | 17.964 |
| 0.1230719E 04 | -0.9124174E 02 | 0.1234898E 04 | 355.760 | 88.940 | 0.049924 | 4 | 23.952 |
| -0.7100132E C3 | 0.1123797E 03 | 0.7188516E 03 | 171.006 | 34.201 | 0.029081 | 5 | 29.940 |
| 0.7159211E 03 | 0.2896774E 03 | 0.7722869E 03 | 22.026 | 3.671 | 0.031242 | 6 | 35.928 |
| 0.2698403E 03 | 0.3441753E 03 | 0.4373445E 03 | 51.903 | 7.415 | 0.017692 | 7 | 41.916 |
| 0.3390911E 03 | 0.2608673E 03 | 0.4278220E 03 | 37.571 | 4.696 | 0.017307 | 8 | 47.904 |
| -0.2307140E C2 | -0.2494630E 03 | 0.2505246E 03 | 264.716 | 29.413 | 0.010135 | 9 | 53.892 |
| 0.257367.E 01 | -0.4052202E 02 | 0.4060365E 02 | 273.634 | 27.363 | 0.001643 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1048746E C5 | | | | | | | |
| 0.2691376E 03 | 0.1039948E 05 | 0.1040296E 05 | 88.517 | 88.517 | 1.000000 | 1 | 5.988 |
| -0.5767119E 03 | 0.4715229E 03 | 0.7449369E 03 | 140.730 | 70.365 | 0.071600 | 2 | 11.976 |
| -0.3221983E 02 | -0.4716375E 03 | 0.4727366E 03 | 266.092 | 88.697 | 0.045442 | 3 | 17.964 |
| 0.1268544E C4 | -0.1309558E 03 | 0.1272555E 04 | 355.450 | 88.862 | 0.122326 | 4 | 23.952 |
| -0.1341999E 03 | 0.5065229E 03 | 0.5239998E 03 | 104.839 | 20.968 | 0.050370 | 5 | 29.940 |
| 0.5015859E 03 | 0.2857490E 03 | 0.5772700E 03 | 29.670 | 4.945 | 0.055491 | 6 | 35.928 |
| 0.6502678E 03 | 0.9500781E 02 | 0.6571716E 03 | 8.312 | 1.187 | 0.063172 | 7 | 41.916 |
| 0.1244490E C3 | 0.1086270E 03 | 0.1282187E 04 | 13.928 | 1.741 | 0.123252 | 8 | 47.904 |
| -0.5397920E 03 | -0.1033044E 04 | 0.1165571E 04 | 242.412 | 26.935 | 0.112062 | 9 | 53.892 |
| -0.1329457E 03 | -0.2337586E 03 | 0.2689192E 03 | 240.372 | 24.037 | 0.025858 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 12 CM. BEND 15?

| A | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.7C256888E 04 | | | | | | | |
| -C.6174034E 02 | 0.3950335E 04 | 0.3950817E 04 | 90.895 | 90.895 | 1.CCCCCC | 1 | 5.988 |
| -0.3181343E 03 | 0.1292820E 03 | 0.3434551E 03 | 157.888 | 78.944 | 0.086933 | 2 | 11.976 |
| 0.2781068E 02 | -0.2551241E 03 | 0.2566362E 03 | 276.223 | 92.074 | 0.064958 | 3 | 17.964 |
| 0.5800278E 03 | -0.8546544E 02 | 0.5862703E 03 | 351.618 | 87.904 | 0.148397 | 4 | 23.952 |
| 0.6245551E 02 | 0.3051057E 01 | 0.3114324E 03 | 78.431 | 15.686 | 0.078827 | 5 | 29.940 |
| 0.1809003E 03 | 0.1732365E 03 | 0.2501824E 03 | 43.824 | 7.304 | 0.063324 | 6 | 35.928 |
| 0.4426860E 03 | -0.1209240E 03 | 0.4589045E 03 | 344.722 | 49.246 | 0.116154 | 7 | 41.916 |
| 0.7596521E 03 | 0.4154012E 01 | 0.7596633E 03 | 0.313 | 0.039 | 0.192280 | 8 | 47.904 |
| -0.5185442E 03 | -0.9755332E 03 | 0.1104782E 04 | 227.982 | 25.331 | 0.196080 | 9 | 53.892 |
| -0.7784488E 02 | -0.1700140E 03 | 0.1869882E 03 | 245.398 | 24.540 | 0.047329 | 10 | 59.880 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 41

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.19270728 03 | | | | | | | |
| 0.1649292E 03 | -0.16348064E 03 | 0.2321520E 03 | 315.235 | 315.235 | 0.792853 | 1 | 5.988 |
| -0.1011223E 03 | 0.1311703E 03 | 0.1656242E 03 | 127.430 | 52.814 | 0.522839 | 2 | 11.976 |
| -0.5898302E 02 | -0.1141753E 03 | 0.1285116E 03 | 242.678 | 80.893 | 0.405683 | 3 | 17.964 |
| 0.5547748E 02 | 0.7569408E 02 | 0.9384816E 02 | 53.762 | 13.440 | 0.296258 | 4 | 23.952 |
| -0.2470686E 03 | -0.1982574E 03 | 0.3167786E 03 | 218.745 | 43.749 | 1.000000 | 5 | 29.940 |
| 0.8721222E 02 | 0.2576047E 02 | 0.9093724E 02 | 16.496 | 2.743 | 0.287069 | 6 | 35.928 |
| 0.6712619E 02 | 0.3019696E 01 | 0.6719403E 02 | 2.576 | 0.368 | 0.212117 | 7 | 41.916 |
| -0.1829257E 02 | 0.8095323E 01 | 0.1894894E 02 | 156.059 | 19.507 | 0.042974 | 8 | 47.904 |
| -0.1834930E 02 | -0.1648536E 02 | 0.1965875E 02 | 238.079 | 28.453 | 0.062059 | 9 | 53.892 |
| 0.1361075E 02 | 0.3500294E 01 | 0.1409383E 02 | 14.427 | 1.442 | 0.044364 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1472234E 02 | | | | | | | |
| 0.9930394E 02 | 0.6449936E 01 | 0.9965282E 02 | 6.203 | 6.203 | 0.459298 | 1 | 5.988 |
| -0.8822932E 02 | -0.3092387E 01 | 0.8828333E 02 | 182.027 | 91.014 | 0.664340 | 2 | 11.976 |
| 0.1377194E 02 | -0.6069084E 02 | 0.6223358E 02 | 282.785 | 94.262 | 0.479169 | 3 | 17.964 |
| 0.3949789E 02 | 0.3329869E 02 | 0.5165604E 02 | 40.126 | 10.031 | 0.397727 | 4 | 23.952 |
| -0.1120074E 03 | -0.6974712E 02 | 0.1298782E 03 | 210.412 | 42.082 | 1.000000 | 5 | 29.940 |
| 0.1657948E 02 | 0.3743188E 01 | 0.1121745E 02 | 10.493 | 1.249 | 0.086369 | 6 | 35.928 |
| 0.3848445E 02 | -0.2978642E 02 | 0.4831372E 02 | 226.193 | 46.608 | 0.356903 | 7 | 41.916 |
| 0.9738724E 00 | -0.8009904E 01 | 0.8029626E 01 | 276.090 | 34.262 | 0.061824 | 8 | 47.904 |
| -0.3445138E 01 | -0.7358635E 01 | 0.8125175E 01 | 244.912 | 27.217 | 0.062560 | 9 | 53.892 |
| -0.1002447E 02 | 0.1821430E 01 | 0.1018860E 02 | 169.702 | 16.970 | 0.078447 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1005240E 03 | | | | | | | |
| -0.9022579E 02 | 0.1466954E 03 | 0.1550554E 03 | 108.900 | 108.900 | 1.000000 | 1 | 5.988 |
| 0.2335981E 02 | -0.2208565E 02 | 0.3214743E 02 | 316.606 | 158.303 | 0.207329 | 2 | 11.976 |
| 0.3699422E 02 | 0.3324647E 00 | 0.3699568E 02 | 0.512 | 0.171 | 0.238596 | 3 | 17.964 |
| -0.1837335E 02 | -0.1511626E 02 | 0.2378245E 02 | 219.445 | 54.861 | 0.153445 | 4 | 23.952 |
| 0.4462269E 01 | 0.2592388E 02 | 0.2591096E 02 | 80.089 | 16.017 | 0.167108 | 5 | 29.940 |
| -0.6399966E 01 | -0.3454565E 02 | 0.3513347E 02 | 259.504 | 43.251 | 0.226587 | 6 | 35.928 |
| 0.3944462E 01 | -0.5984239E 01 | 0.7151687E 01 | 303.497 | 43.356 | 0.046123 | 7 | 41.916 |
| 0.3356215E 01 | -0.3799137E 00 | 0.3377648E 01 | 353.542 | 44.193 | 0.021763 | 8 | 47.904 |
| 0.3867782E 01 | -0.9906489E 00 | 0.3992956E 01 | 345.633 | 38.404 | 0.025749 | 9 | 53.892 |
| -0.3121812E 00 | -0.4993513E 01 | 0.5003260E 01 | 266.425 | 24.642 | 0.032268 | 10 | 59.880 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 497 CTR 256 CR 25.0 TR 26 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3598403E 01 | | | | | | | |
| 0.1206202E 01 | -0.2433094E 01 | 0.2715671E 01 | 296.370 | 296.370 | 1.000000 | 1 | 5.988 |
| -0.9948140E-01 | 0.1950356E-01 | 0.1013762E 00 | 168.905 | 84.452 | 0.037310 | 2 | 11.976 |
| -0.3079928E-01 | -0.7541125E-02 | 0.3171381E-01 | 193.793 | 64.598 | 0.011678 | 3 | 17.964 |
| 0.1252821E-01 | 0.2861529E-01 | 0.3123764E-01 | 66.355 | 16.589 | 0.011503 | 4 | 23.952 |
| 0.1736866E-01 | 0.1701143E-01 | 0.2429742E-01 | 44.438 | 8.888 | 0.008947 | 5 | 29.940 |
| 0.6389987E-02 | -0.9139480E-02 | 0.8197866E-02 | 321.212 | 53.535 | 0.003019 | 6 | 35.928 |
| -0.8862916E-02 | 0.1622624E-01 | 0.1848097E-01 | 118.444 | 16.949 | 0.006808 | 7 | 41.916 |
| 0.2733273E-01 | 0.1346720E-02 | 0.2736588E-01 | 2.821 | 0.353 | 0.010077 | 8 | 47.904 |
| -0.1171297E-02 | -0.2987226E-02 | 0.3208653E-02 | 248.590 | 27.621 | 0.001182 | 9 | 53.892 |
| 0.2014873E-01 | 0.8151501E-02 | 0.2173515E-01 | 22.027 | 2.203 | 0.008004 | 10 | 59.880 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 46

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 LR 56.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2199186E 05 | | | | | | | |
| -0.3169526E 04 | 0.1238199E 04 | 0.3394562E 04 | 158.630 | 158.6CC | 0.429604 | 1 | 5.952 |
| -0.2486658E 03 | -0.3862215E 04 | 0.5391596E 04 | 267.441 | 133.721 | 1.000000 | 2 | 11.905 |
| 0.1496799E 04 | -0.1493752E 04 | 0.2107574E 04 | 314.866 | 104.955 | 0.390901 | 3 | 17.857 |
| -0.1787669E 03 | 0.1964705E 03 | 3.2641519E 03 | 132.591 | 33.148 | 0 048993 | 4 | 23.810 |
| 0.5125320E C3 | -0.3424585E 03 | 0.6164033E 03 | 326.252 | 65.25C | 0.114327 | 5 | 29.762 |
| -0.5657628E 02 | 0.8579752E 02 | 0.1027720E 03 | 123.402 | 20.567 | 0.019062 | 6 | 35.714 |
| 0.7620870E 02 | -0.8530164E 02 | 0.1143862E 03 | 311.774 | 44.539 | 0.021215 | 7 | 41.667 |
| -0.8251644E 02 | -0.5867706E 02 | 0.1012520E 03 | 215.416 | 28.927 | 0.018780 | 8 | 47.619 |
| 0.5299826E C2 | -0.1070075E 03 | 0.1194124E 03 | 296.348 | 32.928 | 0.022148 | 9 | 53.571 |
| 0.8153645E 02 | 0.2848647E 02 | 0.8636877E 02 | 19.257 | 1.926 | 0.016019 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3330098E 03 | | | | | | | |
| -0.1384360E 03 | 0.1741503E 03 | 0.2224698E 03 | 128.482 | 128.482 | 1.000000 | 1 | 5.952 |
| -0.1929120E 03 | -0.7083344E 02 | 0.2059052E 03 | 200.162 | 100.081 | 0.923744 | 2 | 11.905 |
| -0.1912605E 03 | -0.7315109E 02 | 0.2047722E 03 | 200.930 | 66.977 | 0.920449 | 3 | 17.857 |
| 0.1650374E C3 | 0.8339451F 01 | 0.1661443E 03 | 2.874 | 0.718 | 0.746026 | 4 | 23.810 |
| -0.4977039E 02 | 0.1377960E 03 | 0.1465088E 03 | 109.859 | 21.972 | 0.658596 | 5 | 29.762 |
| 0.6763275E 02 | 0.1457176F 02 | 0.6918469E 02 | 12.159 | 2.026 | 0.310885 | 6 | 35.714 |
| -0.1586775E 03 | -0.1598107E 02 | 0.1594802E 03 | 185.751 | 26.536 | 0.716862 | 7 | 41.667 |
| 0.6990529E 02 | 0.2984506E 02 | 0.7608327E 02 | 23.096 | 2.887 | 0.341994 | 8 | 47.619 |
| 0.3408534E 02 | 0.4586397E 00 | 0.3408842E 02 | 0.771 | 0.086 | 0.153227 | 9 | 53.571 |
| -0.2475654E 02 | 0.8799006E 00 | 0.2477219E 02 | 177.964 | 17.796 | 0.111351 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.7134814E C3 | | | | | | | |
| 0.7525906E 03 | -0.6412808E 03 | 0.9887534E 03 | 319.566 | 319.566 | 1.000000 | 1 | 5.952 |
| -0.1876989E 03 | 0.6659802E 03 | 0.6919250E 03 | 105.740 | 52.870 | 0.699795 | 2 | 11.905 |
| -0.1617048E 03 | 0.1451719E 03 | 0.2173093E 03 | 138.084 | 46.028 | 0.219781 | 3 | 17.857 |
| 0.4834456E C2 | 0.2100386E 02 | 0.5271013E 02 | 23.483 | 5.871 | 0.053310 | 4 | 23.810 |
| -0.4700787E 02 | 0.6326221E 02 | 0.7881525E 02 | 126.615 | 25.323 | 0.079712 | 5 | 29.762 |
| 0.1722903E 02 | 0.1674658E 02 | 0.2402681E 02 | 44.186 | 7.364 | 0.024300 | 6 | 35.714 |
| 0.1248751E 02 | 0.1469793E 02 | 0.1928644E 02 | 49.648 | 7.093 | 0.019506 | 7 | 41.667 |
| 0.6260989E 01 | -0.3[*2557E 01 | 0.7053347E 01 | 332.722 | 41.59C | 0.007134 | 8 | 47.619 |
| 0.8C89048E 01 | -0.1506698E 02 | 0.1709821E 02 | 298.212 | 33.135 | 0.017293 | 9 | 53.571 |
| 0.1709976E 02 | 0.1462172E 01 | 0.1717187E 02 | 14.626 | 1.463 | 0.017873 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.4835025E 03 | | | | | | | |
| 0.1116149E 04 | -0.1098818E 04 | 0.1566266E 04 | 315.448 | 315.448 | 1.000000 | 1 | 5.952 |
| -0.9488349F 02 | 0.7750187E 03 | 0.7808049E 03 | 96.980 | 48.490 | 0.498514 | 2 | 11.905 |
| 0.7011837E 01 | 0.4266870E 03 | 0.4267444E 03 | 89.059 | 29.686 | 0.272460 | 3 | 17.857 |
| -0.1536540E 02 | -0.1500869E 02 | 0.2146347E 02 | 224.381 | 56.09C | 0.013704 | 4 | 23.810 |
| -0.3558145E 02 | -0.1079389E 01 | 0.3580327E 02 | 186.381 | 37.276 | 0.022859 | 5 | 29.762 |
| -0.6239127E 02 | 0.6002061E 00 | 0.6239419E 02 | 179.449 | 29.908 | 0.C39836 | 6 | 35.714 |
| 0.4086432E 02 | -0.1993509E 02 | 0.4546756E 02 | 333.995 | 47.714 | 0.029029 | 7 | 41.667 |
| -0.3383546E 02 | -0.1959974E 02 | 0.3923325E 02 | 210.411 | 26.3C1 | 0.025045 | 8 | 47.619 |
| -0.2659963E 02 | 0.3303658E 01 | 0.2682335E 02 | 170.871 | 18.986 | 0.013295 | 9 | 53.571 |
| -0.1576292E 02 | -0.1787474E 02 | 0.2383223E 02 | 228.592 | 22.859 | 0.015216 | 10 | 59.524 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 46

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.10688076 04 | | | | | | | |
| 0.8884987E 03 | -0.1162186E 04 | 0.1462909E 04 | 307.398 | 307.398 | 1.000000 | 1 | 5.952 |
| 0.2715184E 02 | 0.5416094E 03 | 0.5422893E 03 | 87.130 | 43.565 | 0.370692 | 2 | 11.905 |
| 0.2015547E 03 | 0.5960405E 03 | 0.6291965E 03 | 71.317 | 23.772 | 0.430099 | 3 | 17.857 |
| -0.2889957E 02 | 0.7259634E 02 | 0.7813708E 02 | 111.707 | 27.927 | 0.053412 | 4 | 23.810 |
| -0.3414595E 02 | -0.5137649E 02 | 0.6168881E 02 | 236.391 | 47.278 | 0.042169 | 5 | 29.762 |
| -0.2380409E 01 | -0.1280157E 02 | 0.1302100E 02 | 259.466 | 43.244 | 0.008901 | 6 | 35.714 |
| -0.4015692E 02 | -0.4347395E 02 | 0.5918245E 02 | 227.271 | 32.467 | 0.040455 | 7 | 41.667 |
| 0.2114284E 02 | -0.2161305E 02 | 0.3023480E 02 | 314.370 | 39.296 | 0.020668 | 8 | 47.619 |
| -0.2817264E 01 | 0.8381374E 01 | 0.8842194E 01 | 108.579 | 12.064 | 0.006044 | 9 | 53.571 |
| -0.4107266E 02 | -0.1921176E 02 | 0.4534373E 02 | 205.068 | 20.507 | 0.030998 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1181424E 04 | | | | | | | |
| 0.5869204E 03 | -0.9108245E 03 | 0.1083548E 04 | 302.797 | 302.797 | 1.000000 | 1 | 5.952 |
| 0.5379237E 02 | 0.2997090E 03 | 0.3044978E 03 | 79.825 | 39.912 | 0.281019 | 2 | 11.905 |
| 0.3916167E 03 | 0.6331892E 03 | 0.7445078E 03 | 58.264 | 19.421 | 0.687102 | 3 | 17.857 |
| -0.5688530E 02 | 0.2012426E 03 | 0.2091288E 03 | 105.784 | 26.446 | 0.193003 | 4 | 23.810 |
| -0.6491357E 02 | -0.6082681E 02 | 0.8895880E 02 | 223.138 | 44.628 | 0.082100 | 5 | 29.762 |
| 0.3748874E 02 | -0.5788113E 01 | 0.3793243E 02 | 351.223 | 58.537 | 0.035008 | 6 | 35.714 |
| -0.5258699E 02 | 0.4901595E 02 | 0.7188847E 02 | 137.013 | 19.573 | 0.066345 | 7 | 41.667 |
| 0.4440638E 02 | 0.8272609E 02 | 0.9393443E 02 | 61.725 | 7.716 | 0.086691 | 8 | 47.619 |
| -0.1977047E 01 | 0.2724391E 02 | 0.2769479E 02 | 100.353 | 11.150 | 0.025559 | 9 | 53.571 |
| -0.1694881E 02 | 0.2548627E 02 | 0.3060738E 02 | 123.625 | 12.362 | 0.028247 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8124407E 03 | | | | | | | |
| 0.2549307E 03 | -0.6189636E 03 | 0.6694067E 03 | 292.385 | 292.385 | 0.914432 | 1 | 5.952 |
| 0.4629959E 02 | 0.7011507E 02 | 0.8402243E 02 | 56.562 | 28.281 | 0.114777 | 2 | 11.905 |
| 0.4910059E 03 | 0.5429600E 03 | 0.7320464E 03 | 47.877 | 15.959 | 1.000000 | 3 | 17.857 |
| -0.3369579E 02 | 0.3031348E 03 | 0.3050015E 03 | 96.343 | 24.086 | 0.416642 | 4 | 23.810 |
| -0.8276979E 02 | -0.4005200E 02 | 0.9195105E 02 | 205.822 | 41.164 | 0.125608 | 5 | 29.762 |
| 0.3234143E 02 | -0.7358911E 02 | 0.8003015E 02 | 323.894 | 53.982 | 0.054603 | 6 | 35.714 |
| -0.8823448E 02 | 0.1007883E 03 | 0.1339538E 03 | 131.200 | 18.743 | 0.182985 | 7 | 41.667 |
| 0.3610434E 02 | 0.1238980E 03 | 0.1265513E 03 | 73.754 | 9.219 | 0.176288 | 8 | 47.619 |
| -0.7709133E 01 | 0.6127571E 02 | 0.6175874E 02 | 97.171 | 10.797 | 0.084364 | 9 | 53.571 |
| 0.1553579E 02 | 0.4200554E 02 | 0.4478644E 02 | 69.703 | 6.970 | 0.061180 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5938032E 03 | | | | | | | |
| 0.7107429E 01 | -0.2670398E 03 | 0.2691335E 03 | 271.513 | 271.513 | 0.423276 | 1 | 5.952 |
| 0.1464C64E 02 | -0.4579385E 02 | 0.4872357E 02 | 289.970 | 144.985 | 0.076625 | 2 | 11.905 |
| 0.5167449E 03 | 0.3704866E 03 | 0.6358345E 03 | 35.639 | 11.880 | 1.000000 | 3 | 17.857 |
| 0.7989326E 01 | 0.2932871E 03 | 0.2933958E 03 | 88.440 | 22.110 | 0.461434 | 4 | 23.810 |
| -0.1089277E 03 | 0.3576273E 01 | 0.1089864E 03 | 178.120 | 35.624 | 0.171407 | 5 | 29.762 |
| 0.3819919E 01 | -0.2603915E 02 | 0.2631784E 02 | 278.346 | 46.391 | 0.041391 | 6 | 35.714 |
| -0.4190161E 02 | 0.8291016E 02 | 0.9289691E 02 | 116.811 | 16.687 | 0.146102 | 7 | 41.667 |
| 0.5905146E 02 | 0.1708939E 03 | 0.1807711E 03 | 70.933 | 8.867 | 0.284305 | 8 | 47.619 |
| -0.1599854E 02 | 0.7900124E 02 | 0.7180615E 02 | 102.874 | 11.430 | 0.112932 | 9 | 53.571 |
| -0.1417118E 02 | 0.3289079E 02 | 0.3581377E 02 | 113.309 | 11.331 | 0.056326 | 10 | 59.524 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 46

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 1 CM. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.8746633E 04 | | | | | | | |
| 0.7986367E 04 | 0.3282928E 05 | 0.3378673E 05 | 76.327 | 76.327 | 1.000000 | 1 | 5.952 |
| -0.3783118E 04 | 0.1824292E 04 | 0.4200000E 04 | 154.256 | 77.128 | 0.124305 | 2 | 11.905 |
| -0.6548252E 03 | -0.1574664E 04 | 0.1705392E 04 | 247.420 | 82.473 | 0.050475 | 3 | 17.857 |
| -0.1566814E 03 | 0.1632764E 03 | 0.2262925E 03 | 133.819 | 33.455 | 0.006698 | 4 | 23.810 |
| 0.4553066E 03 | 0.1164486E 03 | 0.4699714E 03 | 14.351 | 2.870 | 0.013910 | 5 | 29.762 |
| 0.1518077E 02 | -0.3710774E 02 | 0.4009288E 02 | 292.250 | 48.708 | 0.001187 | 6 | 35.714 |
| -0.7406152E 02 | -0.4097266E 02 | 0.8439307E 02 | 208.310 | 29.759 | 0.002496 | 7 | 41.667 |
| 0.1407401E 03 | 0.2151270E 02 | 0.1578643E 03 | 26.936 | 3.367 | 0.004672 | 8 | 47.619 |
| -0.1837317E 02 | 0.1888055E 02 | 0.2635046E 02 | 134.208 | 14.912 | 0.000780 | 9 | 53.571 |
| -0.9267187E 02 | -0.9241676E 02 | 0.1308775E 03 | 224.921 | 22.492 | 0.003874 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 5 CM. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1497309E 05 | | | | | | | |
| 0.4363539E 04 | 0.2035739E 05 | 0.2081978E 05 | 77.902 | 77.902 | 1.000000 | 1 | 5.952 |
| -0.1789128E 04 | 0.1266867E 04 | 0.2192243E 04 | 144.698 | 72.349 | 0.105296 | 2 | 11.905 |
| -0.1496745E 03 | -0.5254790E 03 | 0.5456919E 03 | 268.368 | 89.456 | 0.025250 | 3 | 17.857 |
| 0.1722725E 03 | 0.2995352E 03 | 0.3455415E 03 | 60.095 | 15.024 | 0.016597 | 4 | 23.810 |
| 0.1084237E 03 | -0.2541967E 03 | 0.2763540E 03 | 293.100 | 58.620 | 0.013274 | 5 | 29.762 |
| -0.1778973E 03 | 0.1858029E 03 | 0.2572356E 03 | 133.755 | 22.292 | 0.012355 | 6 | 35.714 |
| 0.2066760E 03 | 0.1259483E 02 | 0.2072590E 03 | 3.484 | 0.498 | 0.009955 | 7 | 41.667 |
| -0.1147104E 03 | -0.8557725E 01 | 0.1150291E 03 | 184.267 | 23.033 | 0.005525 | 8 | 47.619 |
| 0.1456161E 03 | -0.3499641E 02 | 0.1497624E 03 | 346.486 | 38.498 | 0.007193 | 9 | 53.571 |
| -0.3011523E 02 | -0.7177094E 02 | 0.7783310E 02 | 247.237 | 24.724 | 0.003738 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 8 CM. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9472293E 04 | | | | | | | |
| 0.1031912E 04 | 0.8167219E 04 | 0.8232148E 04 | 82.799 | 82.799 | 1.000000 | 1 | 5.952 |
| -0.3993811E 03 | 0.4488955E 03 | 0.5750320E 03 | 128.680 | 64.340 | 0.069852 | 2 | 11.905 |
| -0.1488356E 03 | -0.1910325E 03 | 0.2421683E 03 | 232.077 | 77.359 | 0.029417 | 3 | 17.857 |
| 0.5960127E 03 | 0.2416899E 03 | 0.6431579E 03 | 22.073 | 5.518 | 0.078127 | 4 | 23.810 |
| -0.9071799E 02 | -0.1709869E 03 | 0.1935[illegible] 03 | 242.052 | 48.410 | 0.023513 | 5 | 29.762 |
| -0.5516296E 02 | 0.2276389E 01 | 0.2342273E 03 | 103.622 | 17.270 | 0.028453 | 6 | 35.714 |
| 0.3817717E 03 | -0.8883170E 02 | 0.3919702E 03 | 346.901 | 49.557 | 0.047615 | 7 | 41.667 |
| -0.2305226E 03 | 0.2596147E 02 | 0.2319798E 03 | 173.574 | 21.697 | 0.028180 | 8 | 47.619 |
| 0.8778732E 02 | -0.[illegible]361E 02 | 0.9301166E 02 | 340.705 | 37.856 | 0.011299 | 9 | 53.571 |
| -0.8198425E 02 | -0.[illegible]439E 01 | 0.8201199E 02 | 181.491 | 18.149 | 0.009967 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 503 CTR 163 CR 56.0 TR 12 CM. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.5511262E 04 | | | | | | | |
| 0.2629080E 03 | 0.2967934E 04 | 0.2979556E 04 | 84.938 | 84.938 | 1.000000 | 1 | 5.952 |
| -0.2364081E 03 | 0.9525060E 02 | 0.2548754E 03 | 158.055 | 79.028 | 0.085541 | 2 | 11.905 |
| -0.4176312E 02 | -0.1592110E 03 | 0.1649974E 03 | 255.302 | 85.101 | 0.055242 | 3 | 17.857 |
| 0.2714934E 03 | 0.1194201E 03 | 0.2965969E 03 | 23.763 | 5.936 | 0.099544 | 4 | 23.810 |
| -0.1019503E 03 | -0.1181904E 03 | 0.1560860E 03 | 229.219 | 45.844 | 0.052386 | 5 | 29.762 |
| -0.7540445E 02 | 0.1023896E 03 | 0.1271431E 03 | 126.375 | 21.062 | 0.042672 | 6 | 35.714 |
| 0.1055441E 03 | -0.8548831E 02 | 0.1358227E 03 | 320.993 | 45.856 | 0.045585 | 7 | 41.667 |
| -0.4980122E 02 | -0.4982094E 02 | 0.6988019E 02 | 225.475 | 28.184 | 0.023453 | 8 | 47.619 |
| -0.2277106E 02 | 0.9500916E 01 | 0.2467363E 02 | 157.352 | 17.484 | 0.008281 | 9 | 53.571 |
| 0.5290174E 01 | -0.4538464E 02 | 0.4569191E 02 | 276.648 | 27.665 | 0.015335 | 10 | 59.524 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 46

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 903 CTR 163 CR 56.0 TR 9 TORSION 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.6677C07E 02 | | | | | | | |
| 0.1143906E 03 | 0.1141923E 02 | 0.1149592E 03 | 5.701 | 5.701 | 0.616858 | 1 | 5.952 |
| -0.5143365E 02 | 0.1267048E 03 | 0.1367462E 03 | 112.094 | 56.047 | 0.733756 | 2 | 11.905 |
| -0.1855416E 03 | -0.1747493E 02 | 0.1863647E 03 | 185.300 | 61.767 | 1.000000 | 3 | 17.857 |
| 0.7226801E 02 | 0.3038506E 02 | 0.7839507E 02 | 22.804 | 5.701 | 0.420658 | 4 | 23.810 |
| 0.2924194E 02 | -0.4282339E 02 | 0.8783394E 02 | 289.446 | 57.889 | 0.471301 | 5 | 29.762 |
| 0.3138678E 02 | 0. 0974916E 02 | 0.3325023E 02 | 19.273 | 3.212 | 0.178415 | 6 | 35.714 |
| 0.1601093E 02 | -0.6959059E 01 | 0.1745789E 02 | 336.508 | 48.073 | 0.093676 | 7 | 41.667 |
| 0.1263038E 02 | 0.1867257E 02 | 0.2250085E 02 | 55.852 | 6.982 | 0.120736 | 8 | 47.619 |
| 0.2721408E 02 | 0.4516602E 00 | 0.2721782E 02 | 0. 951 | 0.106 | 0.146046 | 9 | 53.571 |
| 0.1403258E 02 | 0.4789069E 01 | 0.1482729E 02 | 18.844 | 1.884 | 0.079561 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 903 CTR 163 CR 56.0 TR 15 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1453257E 03 | | | | | | | |
| 0.6749597E 02 | 0.1033796E 03 | 0.1234627E 03 | 56.860 | 56.860 | 1.000000 | 1 | 5.952 |
| -0.4199040E 02 | 0.3539939E 02 | 0.5487250E 02 | 139.831 | 69.915 | 0.444446 | 2 | 11.905 |
| -0.5663047E 02 | 0.5489448E 01 | 0.5669082E 02 | 174.444 | 58.148 | 0.459222 | 3 | 17.857 |
| 0.1349396E 02 | 0.8389004E 01 | 0.1580987E 02 | 31.869 | 7.967 | 0.128005 | 4 | 23.810 |
| 0.2399072E 02 | -0.3594051E 02 | 0.4321196E 02 | 303.724 | 60.745 | 0.350000 | 5 | 29.762 |
| 0.1597908E 02 | -0.9203267E 00 | 0.1600554E 02 | 356.704 | 59.451 | 0.129639 | 6 | 35.714 |
| 0.1675005E 01 | -0.1093334E 01 | 0.2000255E 01 | 326.306 | 46.615 | 0.016201 | 7 | 41.667 |
| 0.9922066E 00 | 0.1357090E 02 | 136C720E 02 | 85.818 | 10.727 | 0.110213 | 8 | 47.619 |
| 0.1605943E 02 | -0.8153110E 00 | .1608009E 02 | 357.094 | 39.677 | 0.130242 | 9 | 53.571 |
| 0.9776014E 01 | 0.1367559E 01 | 0.9871202E 01 | 7.963 | 0.796 | 0.079953 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 903 CTR 163 CR 56.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.4926935E 02 | | | | | | | |
| 0.6980886E 01 | 0.6825548E 02 | 0.6861150E 02 | 84.160 | 84.160 | 1.000000 | 1 | 5.952 |
| 0.1:401306 02 | -0.1849361E 02 | 0.2172562E 02 | 301.694 | 150.847 | 0.316647 | 2 | 11.905 |
| 0.6C67691E 02 | 0.5475453E 01 | 0.6092345E 02 | 5.136 | 1.719 | 0.887948 | 3 | 17.857 |
| -0.2090506E 02 | -0.2144418E 02 | 0.2994785E 02 | 225.729 | 56.432 | 0.436484 | 4 | 23.810 |
| -0.8224189E 01 | 0.1568176E 02 | 0.1770747E 02 | 117.674 | 29.535 | 0.258083 | 5 | 29.762 |
| -0.7765619E 01 | -0.3234136E 01 | 0.8393701E 01 | 202.663 | 33.777 | 0.122337 | 6 | 35.714 |
| 0.1869338E 01 | -0.6564183E 00 | 0.1981238E 01 | 340.651 | 48.664 | 0.028876 | 7 | 41.667 |
| -0.1378068E 00 | 0.2991317E 01 | 0.2994689E 01 | 92.638 | 11.580 | 0.043644 | 8 | 47.619 |
| 0.1968251E 01 | 0.5088619E 01 | 0.5956006E 01 | 68.854 | 7.650 | 0.079526 | 9 | 53.571 |
| 0.3C91121E 01 | 0.3201180E 01 | 0.4490008E 01 | 44.802 | 4.600 | 0.064858 | 10 | 59.524 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 903 CTR 163 CR 56.0 TR 34 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3599675E C1 | | | | | | | |
| 0.1033742E 01 | -0.1888657E 01 | 0.2153054E 01 | 298.694 | 298.694 | 1.000000 | 1 | 5.952 |
| -0.2283912F-01 | 0.5528407E-01 | 0.5981674E-01 | 112.446 | 56.223 | 0.027782 | 2 | 11.905 |
| -0.8966338E-01 | 0.2822163E-01 | 0.9819238E-01 | 161.786 | 53.922 | 0.041890 | 3 | 17.857 |
| 0.7038659E-01 | 0.7855108E-01 | 0.1039798E 00 | 47.410 | 11.852 | 0.048294 | 4 | 23.810 |
| 0.4285175E-02 | -0.4861116E-02 | 0.6480213E-02 | 311.397 | 62.279 | 0.003010 | 5 | 29.762 |
| 0.1892498E-01 | 0.7144609E-04 | 0.1892510E-01 | 0.216 | 0.036 | 0.008790 | 6 | 35.714 |
| -0.6952178E-02 | -0.1780988E-02 | 0.7176675E-02 | 194.369 | 27.767 | 0.003333 | 7 | 41.667 |
| -0.8896654E-02 | 0.8954736E-03 | 0.8162062E-02 | 171.644 | 21.456 | 0.002862 | 8 | 47.619 |
| 0.1928C11E-03 | 0.5905230E-02 | 0.5908374E-02 | 88.130 | 9.792 | 0.002744 | 9 | 53.571 |
| -0.2299502E-01 | -0.1877957E-01 | 0.2968910E-01 | 219.238 | 21.924 | 0.013789 | 10 | 59.524 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 50

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 2 FL. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2737CA9E 05 | | | | | | | |
| -0.3471913E 04 | C.36507971E 04 | 0.5038098E 04 | 133.561 | 133.561 | 0.673124 | 1 | 5.917 |
| 0.1180020F 04 | -0.7391043E 04 | 0.7486445E 04 | 279.071 | 139.536 | 1.000000 | 2 | 11.834 |
| 0.1591121E 04 | -0.9265840E 03 | 0.1841256F 04 | 329.786 | 109.929 | 0.246004 | 3 | 17.751 |
| -0.3881082E 03 | -0.1112775E 04 | 0.4037456E 03 | 195.999 | 49.000 | 0.053963 | 4 | 23.669 |
| 0.7570627E 02 | -0.1412173E 04 | 0.1414200E 04 | 273.069 | 54.614 | 0.188947 | 5 | 29.586 |
| 0.7482497E 02 | -0.2198834E 03 | 0.2335453E 03 | 289.722 | 48.287 | 0.031209 | 6 | 35.503 |
| 0.2835549E 03 | 0.1179778E 03 | 0.3071189E 03 | 22.591 | 3.227 | 0.041033 | 7 | 41.420 |
| -0.3995869E 03 | 0.9297363E 02 | 0.4102605E 03 | 166.902 | 20.863 | 0.054814 | 8 | 47.337 |
| -0.6533311E 02 | -0.4160314E 02 | 0.1045344E 03 | 231.319 | 25.702 | 0.013967 | 9 | 53.254 |
| 0.2987619E 02 | -0.6992307E 02 | 0.7603827E 02 | 293.134 | 29.314 | 0.010159 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 4 FL. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1217853F 04 | | | | | | | |
| -0.1033548E 03 | 0.5239492E 03 | 0.5340457E 03 | 101.159 | 101.159 | 0.662881 | 1 | 5.917 |
| -0.6320453E 02 | -0.1371217E 03 | 0.1509873E 03 | 245.253 | 122.627 | 0.187412 | 2 | 11.834 |
| -0.3524429E 02 | -0.1861504E 03 | 0.1894575E 03 | 259.279 | 86.426 | 0.235163 | 3 | 17.751 |
| 0.1461779E 03 | 0.2550214E 02 | 0.2939451E 03 | 60.179 | 15.045 | 0.364857 | 4 | 23.669 |
| 0.1730667E 03 | 0.7868352E 02 | 0.8056436E 03 | 77.595 | 15.519 | 1.000000 | 5 | 29.586 |
| -0.1452999E 03 | 0.1920652E 03 | 0.2408179E 03 | 127.111 | 21.185 | 0.298914 | 6 | 35.503 |
| -0.3089491E 03 | -0.1601807E 03 | 0.3405693E 03 | 208.956 | 29.722 | 0.422726 | 7 | 41.420 |
| 0.4702359E 03 | 0.1404259E 03 | 0.4830959E 03 | 16.477 | 2.310 | 0.599990 | 8 | 47.337 |
| 0.8259656E 02 | 0.2143717E 03 | 0.2297334E 03 | 68.928 | 7.659 | 0.285195 | 9 | 53.254 |
| -0.7850938E 02 | 0.1390308E 03 | 0.1596662E 03 | 119.493 | 11.945 | 0.198185 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 6 FL. BEND 73

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9862209E 01 | | | | | | | |
| 0.9423759E 03 | -0.7196259E 03 | 0.1183296E 04 | 322.787 | 322.787 | 1.000000 | 1 | 5.917 |
| -0.2886519E 03 | 0.9313672E 03 | 0.9750715E 03 | 107.219 | 53.610 | 0.824030 | 2 | 11.834 |
| -0.1799551E 03 | 0.2627266E 02 | 0.1812692E 03 | 171.666 | 57.227 | 0.153190 | 3 | 17.751 |
| 0.1542973E 03 | 0.9350748E 02 | 0.1804198E 03 | 31.217 | 7.804 | 0.152472 | 4 | 23.669 |
| 0.1888548E 03 | 0.9064707E 03 | 0.5405354E 03 | 69.550 | 13.910 | 0.456805 | 5 | 29.586 |
| -0.8003873E 02 | 0.8284799E 02 | 0.1151954E 03 | 134.012 | 22.335 | 0.097351 | 6 | 35.503 |
| -0.4495436E 01 | 0.3560428E 02 | 0.3588695E 02 | 97.196 | 13.885 | 0.030328 | 7 | 41.420 |
| 0.2635197E 02 | -0.1949907E 02 | 0.3278164E 02 | 323.500 | 40.438 | 0.027704 | 8 | 47.337 |
| 0.4499352E 02 | -0.2128432E 02 | 0.4977386E 02 | 334.683 | 37.187 | 0.042064 | 9 | 53.254 |
| 0.2551300E 02 | -0.2174536E 02 | 0.3352272E 02 | 319.558 | 31.956 | 0.028330 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 7 FL. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.8056387E 03 | | | | | | | |
| 0.1253231E 04 | -0.1122463E 04 | 0.1682412E 04 | 318.151 | 318.151 | 1.000000 | 1 | 5.917 |
| -0.9818402E 02 | 0.1110052E 04 | 0.1114185E 04 | 95.055 | 47.527 | 0.662374 | 2 | 11.834 |
| -0.8110036E 02 | 0.5860982E 03 | 0.9916804E 03 | 97.878 | 32.626 | 0.351686 | 3 | 17.751 |
| -0.2760092E 02 | -0.2386599E 02 | 0.3648827E 02 | 220.849 | 55.212 | 0.021688 | 4 | 23.669 |
| -0.6278631E 02 | -0.1025993E 03 | 0.1202392E 03 | 238.566 | 47.713 | 0.071468 | 5 | 29.586 |
| 0.2501620E 02 | 0.1815192E 02 | 0.3090796E 02 | 35.965 | 5.994 | 0.018371 | 6 | 35.503 |
| 0.1124230E 03 | 0.1528441E 03 | 0.1867973E 03 | 53.664 | 7.666 | 0.112777 | 7 | 41.420 |
| -0.2242984F 03 | 0.1260345E 02 | 0.2246502E 03 | 176.784 | 22.098 | 0.133529 | 8 | 47.337 |
| -0.1274798E C3 | -0.1278231E 02 | 0.1281190E 03 | 185.726 | 20.636 | 0.076152 | 9 | 53.254 |
| -0.3904983E 02 | -0.1247339E 02 | 0.4099263E 02 | 197.715 | 19.771 | 0.024365 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 50

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 1C.C TR 10 FL. BEND 140

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.10007R9E C4 | | | | | | | |
| 0.9256040E 03 | -0.1092648E 04 | 0.1431999E 04 | 310.269 | 310.269 | 1.000000C | 1 | 5.917 |
| -0.2888029E 02 | 0.7229387E 03 | 0.7235151E 03 | 92.288 | 46.144 | 0.5C5248 | 2 | 11.834 |
| C.9264946E 02 | 0.7478032E 03 | 0.7535205E 03 | 82.937 | 27.646 | 0.526207 | 3 | 17.751 |
| -0.1564778E C3 | -0.6808430E 02 | 0.1706480E 03 | 2C3.514 | 50.879 | 0.119168 | 4 | 23.669 |
| -0.3051584E 03 | -0.6429932E 03 | 0.7117314E 03 | 244.611 | 48.922 | 0.497015 | 5 | 29.586 |
| 0.3696832E 02 | -0.9221457E 02 | 0.9934877E 02 | 291.865 | 48.641 | 0.069378 | 6 | 35.503 |
| -0.4386792E 02 | -0.2750398E 02 | 0.5177281E 02 | 212.090 | 30.298 | 0.036154 | 7 | 41.420 |
| 0.3C291186 C2 | -0.3202032E 02 | 0.4547549E 02 | 315.241 | 39.405 | 0.031757 | 8 | 47.337 |
| 0.9055793E 01 | 0.4128201E 02 | 0.4159044E 02 | 83.018 | 9.224 | 0.029064 | 9 | 53.254 |
| -0.3681908E 02 | 0.7815470E 02 | 0.8642944E 02 | 115.214 | 11.521 | 0.060356 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 1C.C TR 11 FL. BEND 157

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1136323E C4 | | | | | | | |
| 0.5816648E 03 | -0.9605347E 03 | 0.1112697E 04 | 300.317 | 300.317 | 1.000000C | 1 | 5.917 |
| -0.8240980E 01 | 0.3571821E 03 | 0.3572771E 03 | 91.322 | 45.661 | 0.321091 | 2 | 11.834 |
| 0.2828735E 03 | 0.7620261E 03 | 0.8128352E 03 | 69.634 | 23.211 | C.730509 | 3 | 17.751 |
| -0.1084965E C3 | 0.3486106E 01 | 0.1085524E 03 | 178.160 | 44.54C | 0.097558 | 4 | 23.669 |
| -0.5037056E 03 | -0.8089480E 03 | 0.9529512E 03 | 238.091 | 47.618 | 0.856434 | 5 | 29.586 |
| 0.7769948E 02 | -0.3224756E 03 | 0.3317041E 03 | 283.547 | 47.258 | 0.298108 | 6 | 35.503 |
| -0.1164982E 03 | -0.1910567E 03 | 0.2238775E 03 | 238.583 | 34.083 | 0.201203 | 7 | 41.420 |
| 0.2741042E C3 | -0.7178418E 02 | 0.2833479E 03 | 345.324 | 43.166 | 0.254650 | 8 | 47.337 |
| 0.1105935E 03 | -0.5259664F 01 | 0.1107184E 03 | 357.277 | 39.697 | 0.099505 | 9 | 53.254 |
| 0.4803450F 02 | C.2458263E 02 | 0.5305941E 02 | 27.102 | 2.710 | 0.C48494 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 1C.0 TR 13 FL. BEND 172

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6638928E 03 | | | | | | | |
| 0.2592341E 03 | -0.5081326E 03 | 0.5704392E 03 | 297.029 | 297.029 | 0.648361 | 1 | 5.917 |
| -0.9191175F 01 | 0.6427881E 02 | 0.6493256E 02 | 98.138 | 49.069 | 0.C79404 | 2 | 11.834 |
| 0.4107446E C3 | 0.6376821E 03 | 3.7585178E 03 | 57.214 | 19.071 | 0.928616 | 3 | 17.751 |
| -0.2796586E 02 | 0.9535925E 02 | 0.9937091E 02 | 106.336 | 26.584 | 0.121655 | 4 | 23.669 |
| -0.4177063E 03 | -0.7019451F 03 | 0.8168262E 03 | 239.244 | 47.849 | 1.0CCCCC | 5 | 29.586 |
| 0.1412749E 02 | -0.3523491E 03 | 0.3526521E 03 | 272.296 | 45.383 | 0.431735 | 6 | 35.503 |
| -0.7899794F 01 | -0.2486545E 03 | 0.2497800E 03 | 268.180 | 38.311 | 0.304569 | 7 | 41.420 |
| 0.4197632E 03 | 0.2531683E 02 | 0.4205259E 03 | 3.451 | 0.431 | 0.514825 | | 47.337 |
| 0.1625123E 03 | -0.1831619E 02 | 0.1635412E 03 | 353.569 | 39.285 | 0.2C0215 | 9 | 53.254 |
| 0.7868364E 02 | -0.2210951E 02 | 0.8173090E 02 | 344.305 | 34.430 | 0.100059 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 1C.0 TR 14 FL. BEND 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.2968508E 03 | | | | | | | |
| -0.3339956F 02 | -0.2983516E 03 | 0.3002139E 03 | 263.614 | 263.614 | 0.477749 | 1 | 5.917 |
| 0.1140739E 02 | -0.1060977E 03 | 0.1067727E 03 | 276.446 | 138.223 | 0.169914 | 2 | 11.834 |
| 0.4520391E C3 | 0.4365059E 03 | 0.6283921E 03 | 43.998 | 14.666 | 1.000000 | 3 | 17.751 |
| 0.7466997E 02 | 0.9152365F 02 | 0.1181193E 03 | 50.791 | 12.698 | 0.187971 | 4 | 23.669 |
| -0.3606377E 03 | -0.4852446F 03 | 0.6045840E 03 | 233.380 | 46.676 | 0.962113 | 5 | 29.586 |
| -0.1769208E 02 | -0.3024558E 03 | 0.3029727E 03 | 266.652 | 44.442 | 0.482139 | 6 | 35.503 |
| 0.2407C74E C2 | -0.2728819E 03 | 0.2737419E 03 | 275.045 | 39.292 | 0.435623 | 7 | 41.420 |
| 0.4209480E 03 | -0.1954897E 02 | 0.4214014E 03 | 357.341 | 44.668 | 0.670803 | 8 | 47.337 |
| C.1667474E 02 | -0.2814200F 02 | 0.1691055E 03 | 350.420 | 38.936 | 0.269108 | 9 | 53.254 |
| 0.7734656E 02 | -0.6849760E 02 | 0.1033170E 03 | 318.472 | 31.847 | 0.164415 | 10 | 59.172 |

## HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 5

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 1 CH. BEND 6

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.9072937E 04 | | | | | | | |
| -0.3419911E 04 | 0.3728933E 05 | 0.3744582E 05 | 95.240 | 95.240 | 1.000000 | 1 | 5.917 |
| -0.2138365E 04 | -0.7678647E 04 | 0.2272052E 04 | 199.753 | 99.876 | 0.060676 | 2 | 11.834 |
| -0.2782161E 03 | -0.6582971E 03 | 0.7146741E 03 | 247.090 | 82.363 | 0.019086 | 3 | 17.751 |
| -0.1743128E 03 | 0.4488498E 02 | 0.1799989E 03 | 165.560 | 41.390 | 0.004807 | 4 | 23.669 |
| -0.3392271E 02 | -0.6071172E 03 | 0.6080640E 03 | 266.802 | 53.360 | 0.016238 | 5 | 29.586 |
| 0.5301597E 03 | -0.1370978E 02 | 0.5303367E 03 | 358.519 | 59.753 | 0.014163 | 6 | 35.503 |
| -0.1264561E 03 | -0.8809191E 02 | 0.1541089E 03 | 214.859 | 30.694 | 0.004116 | 7 | 41.420 |
| 0.3732483E 03 | -0.1277247E 04 | 0.1330667E 04 | 286.290 | 35.786 | 0.035536 | 8 | 47.337 |
| 0.6256331E 01 | 0.5418232E 03 | 0.5418591E 03 | 89.338 | 9.926 | 0.014470 | 9 | 53.254 |
| -0.3129065E 02 | 0.1533568E 03 | 0.1565185E 03 | 101.532 | 10.153 | 0.004180 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 5 CH. BEND 45

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.1470853E 05 | | | | | | | |
| -0.2453496E 04 | 0.2338465E 05 | 0.2351300E 05 | 95.990 | 95.990 | 1.000000 | 1 | 5.917 |
| -0.1037645E 04 | -0.2568706E 03 | 0.1068966E 04 | 193.904 | 96.952 | 0.045463 | 2 | 11.834 |
| 0.2444926E 03 | 0.2973193E 03 | 0.3849355E 03 | 50.565 | 16.856 | 0.016371 | 3 | 17.751 |
| 0.9013115E 03 | 0.4007837E 03 | 0.1041504E 04 | 22.631 | 5.658 | 0.044295 | 4 | 23.669 |
| -0.7434927E 03 | -0.4527227E 03 | 0.8704819E 03 | 211.338 | 42.268 | 0.037021 | 5 | 29.586 |
| 0.5281501E 03 | 0.6670762E 03 | 0.8508425E 03 | 51.630 | 8.605 | 0.036186 | 6 | 35.503 |
| 0.9038216E 02 | 0.4444785E 03 | 0.4731902E 03 | 78.988 | 11.284 | 0.020125 | 7 | 41.420 |
| -0.5834428E 02 | 0.1940585E 03 | 0.2026395E 03 | 106.734 | 13.342 | 0.008618 | 8 | 47.337 |
| 0.1845777E 03 | -0.1210076E 03 | 0.2207074E 03 | 326.731 | 36.306 | 0.009387 | 9 | 53.254 |
| 0.1714928E 03 | -0.5838897E 02 | 0.1811635E 03 | 341.195 | 34.119 | 0.007705 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 8 CH. BEND 115

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1016432E 05 | | | | | | | |
| -0.1367365E 04 | 0.1006474E 05 | 0.1015720E 05 | 97.737 | 97.737 | 1.000000 | 1 | 5.917 |
| -0.3525308E 03 | -0.9266714E 03 | 0.4806162E 03 | 222.820 | 111.410 | 0.047318 | 2 | 11.834 |
| 0.2418457E 03 | -0.1525815E 03 | 0.2859719E 03 | 327.754 | 109.251 | 0.028155 | 3 | 17.751 |
| 0.1007519E 04 | 0.3036851E 03 | 0.1052292E 04 | 16.774 | 4.193 | 0.103601 | 4 | 23.669 |
| -0.4863767E 03 | 0.2899290E 03 | 0.5661909E 03 | 149.198 | 29.840 | 0.055743 | 5 | 29.586 |
| 0.4367493E 03 | 0.6497903E 03 | 0.7829285E 03 | 56.093 | 9.349 | 0.077081 | 6 | 35.503 |
| 0.2918408E 03 | 0.3758806E 03 | 0.4758750E 03 | 52.174 | 7.453 | 0.046851 | 7 | 41.420 |
| 0.1570333E 03 | 0.1117022E 04 | 0.1128206E 04 | 81.998 | 13.250 | 0.111055 | 8 | 47.337 |
| 0.1006803E 03 | -0.5869138E 03 | 0.5954866E 03 | 279.734 | 31.082 | 0.058627 | 9 | 53.254 |
| 0.9078113E 02 | -0.9867825E 02 | 0.1340475E 03 | 312.627 | 31.263 | 0.013197 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XM-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 12 CH. BEND 137

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.6944437E 04 | | | | | | | |
| -0.5278823E 03 | 0.4153418E 04 | 0.4186878E 04 | 97.243 | 97.243 | 1.000000 | 1 | 5.917 |
| -0.2621653E 03 | -0.1640406E 03 | 0.3103225E 03 | 212.348 | 106.174 | 0.074119 | 2 | 11.834 |
| 0.1081189E 03 | -0.1069582E 03 | 0.1520847E 03 | 315.309 | 105.103 | 0.036325 | 3 | 17.751 |
| 0.5200479E 01 | 0.8953125E 02 | 0.5276982E 03 | 9.768 | 2.442 | 0.126038 | 4 | 23.669 |
| -0.1162667E 03 | 0.2713320E 03 | 0.2951931E 03 | 113.195 | 22.439 | 0.070505 | 5 | 29.586 |
| 0.1690485E 03 | 0.3449219E 03 | 0.3841201E 03 | 63.890 | 10.648 | 0.091745 | 6 | 35.503 |
| 0.2971777E 03 | 0.1419278E 03 | 0.3293294E 03 | 25.528 | 3.647 | 0.078658 | 7 | 41.420 |
| 0.3411174E 03 | 0.6786589E 03 | 0.7595649E 03 | 63.314 | 7.914 | 0.181418 | 8 | 47.337 |
| -0.1330999E 03 | -0.4473904E 03 | 0.4667695E 03 | 253.432 | 28.159 | 0.111485 | 9 | 53.254 |
| 0.3996179E 02 | -0.8203743E 02 | 0.9125282E 02 | 295.971 | 29.597 | 0.021795 | 10 | 59.172 |

# HARMONIC COMPONENTS OF STRUCTURAL LOADS -- TEST CONDITION NO. 50

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 9 TORSION LIN

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.1588250E 03 | | | | | | | |
| 0.1399254E 03 | -0.1192290E 03 | 0.1812646E 03 | 320.528 | 320.528 | 0.696310 | 1 | 5.917 |
| -0.1479374E 03 | 0.9473767E 02 | 0.1756771E 03 | 147.369 | 73.692 | 0.674827 | 2 | 11.834 |
| -0.4901590E 02 | -0.1593080E 03 | 0.1626017E 03 | 252.655 | 84.152 | 0.624619 | 3 | 17.751 |
| 0.1959717E 02 | 0.8890033E 02 | 0.9103447E 02 | 77.568 | 19.392 | 0.349701 | 4 | 23.669 |
| -0.1052903E 03 | -0.2186784E 03 | 0.2603215E 03 | 244.143 | 49.229 | 1.000000 | 5 | 29.586 |
| 0.8298019E 02 | 0.5832872E 02 | 0.1014295F 03 | 35.104 | 5.851 | 0.389632 | 6 | 35.503 |
| 0.9574310E 02 | 0.2534277E 02 | 0.6123355E 02 | 24.448 | 3.493 | 0.235273 | 7 | 41.420 |
| -0.3735384E 02 | 0.2146649E 00 | 0.3735445E 02 | 179.671 | 22.459 | 0.143493 | 8 | 47.337 |
| 0.2077791E 02 | 0.2117876E 02 | 0.2966890E 02 | 45.548 | 5.061 | 0.113970 | 9 | 53.254 |
| 0.4068318E 01 | 0.1891719E 02 | 0.1934969E 02 | 77.863 | 7.786 | 0.074330 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 19 TORSION 185

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| -0.9264925E 02 | | | | | | | |
| 0.4731113E 02 | 0.2328633F 02 | 0.5273135E 02 | 26.206 | 26.206 | 0.558493 | 1 | 5.917 |
| -0.9204469F 02 | -0.8375454E 01 | 0.9242493F 02 | 185.199 | 92.600 | 0.978899 | 2 | 11.834 |
| 0.2018915E 02 | -0.9604448E 02 | 0.5956999E 02 | 289.811 | 96.604 | 0.630923 | 3 | 17.751 |
| 0.1787408E 02 | 0.5275787E 02 | 0.5570346E 02 | 71.284 | 17.821 | 0.589971 | 4 | 23.669 |
| -0.4915909E 02 | -0.8061263E 02 | 0.9441725E 02 | 238.626 | 47.725 | 1.000000 | 5 | 29.586 |
| 0.1131794F 02 | 0.3890794E 01 | 0.1196804E 02 | 18.972 | 3.162 | 0.126757 | 6 | 35.503 |
| 0.3715245E 02 | -0.9036566E 01 | 0.3823515E 02 | 346.332 | 49.476 | 0.404954 | 7 | 41.420 |
| 0.7712850E 01 | -0.2997155E 01 | 0.8274718F 01 | 338.766 | 42.346 | 0.087640 | 8 | 47.337 |
| 0.1444980F 02 | 0.1758537E 02 | 0.2276053E 02 | 50.590 | 5.621 | 0.241063 | 9 | 53.254 |
| 0.8163007E 00 | 0.7308234E 01 | 0.7353680E 01 | 83.627 | 8.363 | 0.077885 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 29 PITCH LINK

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.8286452F 02 | | | | | | | |
| -0.3718805E 02 | 0.1442269E 03 | 0.1489441E 03 | 104.458 | 104.458 | 1.000000 | 1 | 5.917 |
| 0.4265755E 02 | -0.1064288E 02 | 0.4396236E 02 | 345.990 | 172.995 | 0.295160 | 2 | 11.834 |
| 0.3060530E 02 | 0.2488342E 02 | 0.3944450E 02 | 39.113 | 13.038 | 0.264928 | 3 | 17.751 |
| 0.9902733F-01 | -0.2794676E 02 | 0.2794693E 02 | 270.203 | 67.551 | 0.187634 | 4 | 23.669 |
| -0.1106840E 02 | 0.2777610E 02 | 0.2990074E 02 | 111.726 | 27.945 | 0.200751 | 5 | 29.586 |
| 0.7086093E 01 | -0.2070322E 02 | 0.2188231E 02 | 288.895 | 48.149 | 0.146918 | 6 | 35.503 |
| 0.4947394E 01 | 0.8590024E 00 | 0.5023131E 01 | 9.962 | 1.423 | 0.033729 | 7 | 41.420 |
| -0.1764049F 01 | 0.9454679E-01 | 0.1766580E 01 | 176.932 | 22.117 | 0.011861 | 8 | 47.337 |
| -0.2035532E 01 | 0.3024989E 01 | 0.3644087E 01 | 123.937 | 13.771 | 0.024460 | 9 | 53.254 |
| 0.3475189E-02 | -0.2359866L 01 | 0.2358671E 01 | 270.084 | 27.008 | 0.015836 | 10 | 59.172 |

HARMONIC ANALYSIS MODEL XH-51A SHIP 1002C T 494 CTR 256 CR 10.0 TR 26 BLADE ANGLE

| AJ | BJ | CJ | PHIJC | PSIJC | CJ/CJMAX | J | FREQUENCY |
|---|---|---|---|---|---|---|---|
| 0.3225628E 01 | | | | | | | |
| 0.1079130E 01 | -0.1395497E 01 | 0.1764067E 01 | 307.715 | 307.715 | 1.000000 | 1 | 5.917 |
| -0.7389534E-01 | 0.6615486E-01 | 0.9885891F-01 | 139.036 | 69.518 | 0.055473 | 2 | 11.834 |
| -0.3087740E-01 | -0.1693007E-01 | 0.3516625E-01 | 208.593 | 69.531 | 0.019935 | 3 | 17.751 |
| -0.2233047E-01 | 0.5845888E-01 | 0.6257862E-01 | 110.906 | 27.727 | 0.035476 | 4 | 23.669 |
| 0.6015829E-03 | 0.3383477E-02 | 0.3436542E-02 | 79.918 | 15.984 | 0.001948 | 5 | 29.586 |
| -0.1532716E-01 | 0.3978629E-01 | 0.4 240?9E-01 | 111.918 | 18.636 | 0.023378 | 6 | 35.503 |
| -0.2138139E-01 | -0.2339151E-01 | 0.2138263E-01 | 180.627 | 25.804 | 0.012121 | 7 | 41.420 |
| 0.7879335E-02 | 0.1949109E-01 | 5.2102346E-01 | 67.989 | 8.499 | 0.011918 | 8 | 47.337 |
| -0.4794966E-02 | 0.8385710E-02 | 0.9659804E-02 | 119.761 | 13.307 | 0.005476 | 9 | 53.254 |
| -0.4422478E-02 | 0.3530555E-02 | 0.5658895E-02 | 141.399 | 14.140 | 0.003208 | 10 | 59.172 |

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13. ABSTRACT

This report presents the results of a two-phase research program consisting of (1) in-flight measurement of aerodynamic pressures and structural loads on a compound, rigid-rotor helicopter and (2) correlation of these data with theoretical results.

Flight test data obtained in Phase I and recorded on an oscillograph were read on an oscillograph reading machine and were processed in an automatic data reduction program. This data processing consisted of integration of the pressure data to obtain the distribution of aerodynamic lift and pitching moments over the rotor blade, as functions of azimuth position. Airload and structural load data were harmonically analyzed.

Output of the data reduction program was used in Phase II as input to the correlation program. The measured airloads were used to compute the theoretical bending and torsion responses of the blade. The measured torsion moments were used in the theoretical prediction of the airloads. The results of the applied theories are compared with the flight measurements.

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|---|---|---|---|---|---|---|
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| Differential Pressure Measurements | | | | | | |
| Dynamic Response | | | | | | |
| Harmonic Analysis | | | | | | |
| Helicopter | | | | | | |
| High Advance Ratio | | | | | | |
| Modes of Vibration | | | | | | |
| Pressure Measurements | | | | | | |
| Rigid Rotor | | | | | | |
| Rotor Loads | | | | | | |
| XH-51A | | | | | | |

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