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FROST INVESTIGATIONS

1949-1950

SUMMARY TABULATION OF AIRFIELD PAVEMENTS

1943-1949

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PREPARED BY
FROST EFFECTS LABORATORY
CORPS OF ENGINEERS, U. S. ARMY
NEW ENGLAND DIVISION, BOSTON, MASS.
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NEW ENGLAND DIVISION
CORPS OF ENGINEERS, U. S. ARMY
BOSTON, MASS.

SUMMARY TABULATION OF AIRFIELD PAVEMENTS
AT AIR FORCE INSTALLATIONS CONSTRUCTED ON
FROST SUSCEPTIBLE SUBGRADES

FROST EFFECTS LABORATORY

JUNE 1950

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SUMMARY TABULATION OF AIRFIELD PAVEMENTS

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SUMMARY TABULATION OF AIRFIELD PAVEMENTS

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SYNOPSIS

This report presents a summary tabulation of the pertinent data on pavements, base courses, and subgrades and on traffic histories from twenty-five Air Force bases where the pavement design is effected by frost conditions. The gross plane load evaluations of the pavements during both the normal period, where there is no weakening due to frost melting, and during the frost melting period have been determined using criteria presented in Chapters 2, 3 and 4, Part XII of the Engineering Manual.

Results of pavement condition surveys made at fifteen of the airfields are tabulated and correlated with the pavement evaluations and traffic histories.

All of the fields included in the tabulation have been subjected to a relatively large number of operations by planes of weights exceeding both the "normal" and "frost condition" evaluations which has generally resulted in pavement failures or distress at the portions of the fields receiving the most traffic usage.

Rigid pavements generally have given satisfactory performance where the slab thickness was at least 70 per cent of the "frost condition" design thickness required to support the heaviest type of planes using the field an average of five or more operations daily.

A limited amount of flexible pavement service behavior data is presently available from four of the airfields.

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SUMMARY TABULATION OF AIRFIELD PAVEMENTS
AT AIR FORCE INSTALLATIONS CONSTRUCTED ON
FROST SUSCEPTIBLE SUBGRADES

PART I. INTRODUCTION

1-01. Authorization. The Frost Investigations for 1949-1950, of which this investigation is a part, were authorized by the Chief of Engineers by teletype dated 22 November 1949, File: ENGMG.

This summary tabulation was authorized at the Consultant's Conference held at the Frost Effects Laboratory on 28 and 29 November 1949.

1-02. Purpose. The object of this report is to present in tabular form the traffic histories and pavement conditions at several of the major Air Force bases constructed on frost susceptible subgrades and to correlate the performance records of the pavements with the latest design criteria in the Engineering Manual for Airfield Pavement Design. The purpose of such a comparative study is to verify, or to provide information for the revision of, the existing design and evaluation criteria.

A similar tabulation which included all data available up to June 1948 was previously prepared and was included as Appendix B to Addendum No. 1, dated October 1949, to Report on Frost Investigation, dated April 1947.

1-03. Scope. This investigation has consisted of collating data on details of pavement construction, traffic histories and plane load evaluation of pavements at twenty-five Air Force bases which frost susceptible conditions exist and comparing the data with pavement service behavior records available from fifteen of the airfields.

PART II. PREPARATION OF DATA

2-01. Sources of Data. The data used in the preparation of this summary tabulation were obtained principally from the following five sources:

a. Airfield Pavement Evaluation Reports prepared by the offices of the Corps of Engineers in the Divisions and Districts in which the airfields are located.

b. Airfield Pavement Failure Reports prepared by the Division and District Offices of the Corps of Engineers, which were based on pavement condition surveys made during 1944.

c. Monthly Runway Traffic Reports of Airplane Landings and Take-Offs furnished by the Headquarters of the United States Air Force.

d. Pavement Condition Survey Reports at ten of the airfields prepared by the Ohio River Division in 1947 as part of the Rigid Pavement Investigations.

e. Data obtained in conjunction with the Frost Investigations at several of the sites included in the tabulation.

2-02. Presentation of Data. The locations of the twenty-five airfields investigated are shown on the geographical location map on Plate 1. Plans of the fields showing the layout of the runways and taxiways are contained on Plates 3 to 27 inclusive.

The details of the pavement construction, the gross plane evaluation of the pavements, the summary of traffic history and the available pavement condition information for the twenty-five airfields are presented in Table 1. More detailed records of the annual traffic at the airfields together with traffic distribution data are given in Table 2.

The data tabulated in Table 1 permit a comparison between the weights of planes using the airfields, the frost condition evaluation of the pavements and the pavement performance. Using the average single wheel load of the maximum weight plane group using the airfield with a frequency of five or more landings and take-offs per day and the design criteria presented in Chapter 4, Part XII of the Engineering Manual, the slab thicknesses for rigid pavements and combined thickness of pavement and base for flexible pavements required by frost design criteria have been determined, as tabulated on Table 1. The percentage ratio of the actual thickness to the theoretical design thickness for frost conditions has been computed for each area where pavement condition survey data are available. The per cent design, computed in this manner, has been plotted on Plate 2 against the average wheel load of the weight group of planes using the airfields at least five cycles of landings and take-offs per day prior to the condition survey. The plotted points on Plate 2 indicate whether the pavement was satisfactory or failed. The plotted points are also numbered to cross reference with line numbers on Table 1, where the detailed data are presented.

The descriptions of the pavement conditions were obtained from Airfield Pavement Reports or Pavement Condition Survey Reports. For purposes of tabulation the data have been condensed and wording has been changed only where necessary for consistency. Where extensive cracking, rutting or ravelling was reported or a large number of the concrete slabs had corner cracks the pavement has been considered to have failed even though the pavement might be suitable for the operation of planes at the present rate for several years before extensive repairs would be necessary. Since the purpose of this study is to determine the adequacy of the design criteria, conditions of extensive cracking are considered structural failures which would become progressively worse in a short period of time if subjected to more intense traffic usage. It has not been considered within the scope of this investigation to determine whether it would be more economical to extend with extra maintenance the life of pavements which have shown signs of distress or whether it would have been cheaper to have provided additional pavement thicknesses in the original construction.

2-03. Evaluation Criteria. The evaluations of the flexible and rigid pavements for the normal strength period during which there is no weakening due to frost melting, and which are shown in Table 1, are based on Chapter 2 and Chapter 3, Part XII of the Engineering Manual dated May 1947 and July 1946 respectively. The normal period evaluations for rigid pavements have been determined using the subgrade

modulus k when available. For cases where the modulus of the subgrade has not been determined, the modulus k of the base has been used to evaluate the pavements. Fields evaluated in the latter manner are Dow, Mitchel, Presque Isle, Stewart, Spokane and Wendover.

The pavement evaluations during the frost melting period have been determined using Chapter 4, Part XII of the Engineering Manual as revised in May 1950. The subgrade moduli used for rigid pavement evaluations during the frost melting period were obtained from Figure 7 of Chapter 4. Where the thickness of non-frost-susceptible base is less than 6 inches, the frost melting period evaluation is given as less than 30,000 pounds gross load.

Of the fifteen airfields for which pavement behavior data are presented, all have frost-susceptible subgrade soils, and seven have frost-susceptible base materials. The frost condition evaluations and design thicknesses shown on Table 1 are based on frost action in the frost-susceptible soils, whether base course or subgrade. It is not known whether ice segregation actually occurred in the soils considered frost-susceptible. The water table at six of the fifteen airfields is below the depth of influence.

2-04. Analysis of Results. Results of pavement condition surveys are available from fifteen of the twenty-five fields for which pertinent data are tabulated on Table 1. A comparison between the "frost condition" evaluation of the pavements, the actual traffic usage to which the pavements were subjected and the results of the pavement condition surveys reveals that the fields received relatively heavy usage

by planes having weights in excess of the "frost condition" evaluations. As might be expected, a high percentage of failures resulted, particularly in those sections of the fields at which the records indicate concentration of traffic. The plots of per cent design against wheel load for both rigid and flexible pavements on Plate 2 also show the large number of failures which occurred. The failures that occurred, particularly of concrete pavements, are not necessarily attributable to frost action. At five of the fifteen fields for which pavement behavior data are available, frost action was reported as a contributing cause to the failures. The weight of planes using the fifteen airfields in excess of an average of five operations daily was greater than the normal period evaluation. Therefore the pavements were overloaded during the normal period, at which time some of the failures may have occurred, although with frost-susceptible conditions existing at the fields the degree of overloading was much greater during the frost melting period.

At Wright Field a 60,000 pound wheel load was used to determine the "frost condition" design thickness representing planes of the 120,000 - 135,000 pound weight-group which used the field an average of five operations daily. The "frost condition" design thicknesses at all of the other fifteen airfields at which pavement behavior data are available were determined using wheel loads of plane weight-groups using the fields for an average of ten or more operations daily, while at ten of the fifteen airfields the average actual daily operations of planes, of the weight-group represented by the design wheel loads, were

in excess of 25 and ranged to a maximum of 677 operations at Lockbourne Air Base. In some cases the number of passages of this arbitrarily selected wheel load over any specific location on the pavements during the frost melting period is a relatively small percentage of the total usage and greater damage might have resulted from more frequent coverages by the planes of lighter weight groups. A time interval of a few days between wheel load repetitions over a specific pavement area would tend to allow the subgrade to regain strength between load application and appreciable loss in subgrade strength due to remolding under traffic deformations would be unlikely.

The only instances of failure of a rigid pavement when the pavement thickness was 70 per cent of "frost condition" design thickness or greater was at Chanute Air Force Base where local cracking occurred on three of the four runways. The traffic history at this field prior to failure is incomplete and the taxiways, apron and N-S Runway (which receives approximately 30 per cent of the traffic), were in satisfactory condition, although of similar construction to the three runways showing distress. These failures may be due to local conditions not revealed by the data tabulated in Table 1.

Where the rigid pavement thicknesses were less than 70 per cent of "frost condition" design, based on the average wheel load of the planes using the field for 5 or more daily operations, failures occurred in fifteen out of thirty-eight pavements. Of the sixteen pavements with slab thicknesses less than 50 per cent of the design thicknesses, ten failed and generally showed extensive cracking over

large areas. The six pavements with slab thicknesses less than 50 per cent of design which did not fail either were at fields with a small number of operations or the unfailed pavements were located at portions of the field where traffic usage was light.

Failures were reported at three of the four airfields at which flexible pavement data were available. The data from these fields are plotted in Figure 2, Plate 2. The points numbered 1 through 4 represent data from Casper Air Force Base where five of the eleven taxiways became cracked and rutted followed by complete breakup of pavement and base course. The three runways also showed distress. The plan of the field on Plate 3 and traffic distribution data on Sheet 1 of Table 2 indicates that at least five of the six taxiways at which satisfactory pavements were reported were probably used infrequently.

The other two flexible paved areas on Figure 2, Plate 2, represented by plotted points 14 and 15, and which were in satisfactory condition, are at Dow Air Force Base, for which the combined pavement and base thickness is 67 per cent of "frost condition" design thickness. This field had only 14 average daily operations of planes weighing 50,000 to 75,000 pounds, on which the per cent of design thickness was based. This apparently did not result in sufficient coverages over any specific pavement area, as traffic tests on twenty-nine test lanes at this field during the frost melting periods of 1944 and 1945 showed progressive cracking and failure at all of the twelve locations at which the pavement and base thicknesses were less than 80 per cent of the "frost condition" design thicknesses for the traffic test wheel loads.

A comparison of the behavior of rigid pavements when placed directly on a frost susceptible subgrade and when placed on a base course is possible at two airfields. At Offutt Air Force Base the NW-SE Runway consists of a 9-inch thick slab on 2-1/2-inches of asphalt and 9-1/2-inches of bituminous stabilized gravel. The NE-SW Runway has an 11-inch concrete slab placed directly on the CL subgrade. The concrete flexural strength is the same for both runways while the NW-SE Runway receives 60 per cent of the traffic and the NE-SW Runway only 31 per cent. The NW-SE Runway with the thinner slab and most traffic is reported to be in excellent condition while the NE-SW Runway has a large number of transverse and diagonal cracks. A somewhat similar condition exists at Wright Field where the 7-inch thick apron slabs placed directly on an ML subgrade have cracked extensively while the 7-inch thick slabs of the NE-SW Runway having a 9-inch sand and gravel base are in good to excellent condition. However, the apron undoubtedly is subjected to more traffic coverages and more severe usage than the NE-SW Runway which receives 40 per cent of the traffic at the field.

PART III. CONCLUSIONS

3-01. Based on the service behavior at fifteen of the twenty-five fields tabulated the following conclusions are presented:

a. At all the installations included in this tabulation the pavements have been subjected to a relatively large number of operations of planes with weights exceeding both the "normal" and "frost condition" evaluations, thus tending to make isolation of the effect of frost action more difficult. However, the effect of overloading may be assumed to be much greater in the frost melting period than in the normal period.

b. Portland cement concrete pavements with slab thicknesses at least 70 per cent of those required under "frost condition" design to support wheel loads of planes using fields in excess of an average of five operations per day generally have given satisfactory performance. When the actual slab thicknesses have been less than 70 per cent of "frost condition" design, failures have increased and when less than 50 per cent of design thickness extensive cracking and pavement break-up have occurred at a large percentage of the pavements.

c. At two airfields, namely Offutt Air Force Base and Wright Field, rigid pavements gave satisfactory service when constructed on a base course while pavements of equal or greater thickness placed directly on the frost susceptible subgrades failed. The base course at Offutt, however, consisted of 2-1/2 inches of asphalt and 9-1/2 inches of bituminous stabilized gravel which undoubtedly has greater strength than a typical base course material. At Wright

Field the failed pavement without a base was on the apron while the satisfactory pavement constructed on a 9-inch sand and gravel base course was on a runway and presumably was subjected to less severe usage.

d. The service behavior of all pavements at three of the fields, Clinton County, Dow and Patterson airfields, has been satisfactory under the usage received while pavement elements at several of the other fields have also shown satisfactory performance.

e. It is concluded that pavements designed using the criteria presented in Chapter 4, Part XII of the Engineering Manual entitled Frost Conditions will give satisfactory service behavior with an adequate factor of safety to allow for increased operations of traffic when necessary.

AIRFIELD	LOCATION	PAVEMENT			BASE						SUBGRADE			
		TYPE	THICKNESS (INCHES)	FLEXURAL STRENGTH OF CONCRETE AT 28 DAYS (LBS./SQ. IN.)	TYPE	THICKNESS (INCHES)	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.02 mm)	C.B.R. OR SUBGRADE MODULUS			AIRFIELD CLASSIFICATION	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.02mm)
									K	K _f (1)	C.B.R.			
Casper Air Force Base, Casper, Wyoming	N-S, E-W, NW-SE Runways	Asphaltic Concrete	6.0-6.6	-	Sand	6.6-7.8	10-17	Yes (4-9)	-	-	40	SF, ML, CL, SW, SP, SC	8-68	Yes (6-60)
					SC, ML, SF, CL, SP, SW	12.0-11.4	P-68	Yes (6-60)	-	-	1-5			
	Taxiways 1 & 5	Asphaltic Concrete	5.4	-	Sand	6.6	10-17	Yes (4-9)	-	-	40	ML, SC, SF	8-68	Yes (6-60)
					SF, SC	8.4	P-68	Yes (6-60)	-	-	24			
	Taxiways, 2, 3, 4, and 7	Asphaltic Concrete	7.2	-	Sand	4.8	10-17	Yes (4-9)	-	-	40	SF, SC, SP, ML, CL, SW	8-68	Yes (6-60)
					ML, SC, SF, SP	9.6	P-68	Yes (6-60)	-	-	21			
Taxiways, 9-12 inclusive	Asphaltic Concrete	6.0	-	Sand	8.4	10-17	Yes (4-9)	-	-	40	SF, CL, SW	8-68	Yes (6-60)	
				ML, SF, CL	9.6	P-68	Yes (6-60)	-	-	7				
NE-SW Runway	Asphaltic Concrete	6.6	-	Sand	7.8	10-17	Yes (4-9)	-	-	40	SF, SC, ML, SF	8-68	Yes (6-60)	
Apron	P.C.C.	9-7-13.5	675	None	-	-	-	-	-	-	SW, CL, SC	8-68	Yes (6-60)	
Chanute Air Force Base, Rantoul, Illinois	Original Apron	P.C.C.	8-6-8	700	None	-	-	-	-	-	CL-OL	62-87	Yes (51-65)	
	NE-SW Runway	P.C.C.	8-6-8	700	None	-	-	-	-	-	CL-OL	62-87	Yes (51-65)	
	NW-SE Runway	P.C.C.	8-6-8	700	None	-	-	-	-	-	CL-OL	62-87	Yes (51-65)	
	Taxiways A-E	P.C.C.	8-6-8	700	None	-	-	-	-	-	CL-OL	62-87	Yes (51-65)	
	N-S Runway	P.C.C.	8-6-8	815	Pit Run Sand and Gravel	6	4-15	Yes (3-10)	63	-	-	CL	62-87	Yes (51-65)
	E-W Runway	P.C.C.	8	815	Mech. Stab. Pit Run S. & G.	6	4-15	Yes (3-10)	63	-	-	CL	62-87	Yes (51-65)
Clinton County Air Force Base, Wilmington, Ohio	Runways	P.C.C.	7	730	Pit Run Gravel	6	13-18	Yes (10)	-	-	-	ML-CL	60-85	Yes (41-58)
	Aprons & Taxi A	P.C.C.	8	680	Pit Run Gravel	6	13-18	Yes (10)	-	-	-	ML	60-85	Yes (41-58)
	Taxiway B	P.C.C.	8	730	Pit Run Gravel	6	13-18	Yes (10)	-	-	-	ML	60-85	Yes (41-58)
Dow Air Force Base, Bangor, Maine	Runways	Bit. Conc.	3 1/2	-	Bank Run S.&G.	18	2-7	Borderline	-	-	60	CL-SF	31-88	Yes (21-70)
	Main Service Apron	P.C.C.	8-6-8	607	Bank Run S.&G.	18	2-7	Borderline	315	65	-	CL-SF	31-88	Yes (21-70)
	Taxiways, B, C, D, E Runway Turn-arounds.	Bit. Conc.	3 1/2	-	Bank Run S.&G.	18	2-7	Borderline	-	-	80	CL-SF	31-88	Yes (21-70)
		P.C.C.	10-7-10	607	Bank Run S.&G.	17	2-7	Borderline	315	60	-	CL-SF	31-88	Yes (21-70)
Great Falls Air Force Base, Great Falls, Montana	Taxiways	Asphaltic Concrete	6	-	Pit Run Gravel	10	9-20	Yes (12)	-	-	50	CL, SF, SC	71-92	Yes (45-75)
	N-S Runway	Asphaltic Concrete	6	-	Pit Run Gravel	7	9-20	Yes (10)	-	-	50	CL, SF, SC	71-92	Yes (45-75)
	NE-SW Runway	Asphaltic Concrete	6	-	Pit Run Gravel	9	9-20	Yes (12)	-	-	50	CL, SF, SC	71-92	Yes (45-75)
	NW-SE Runway	Asphaltic Concrete	6	-	Pit Run Gravel	10	9-20	Yes (10)	-	-	50	CL, SF, SC	71-92	Yes (45-75)
	E-W Runway	Asphaltic Concrete	6	-	Pit Run Gravel	11	9-20	Yes (12)	-	-	50	CL, SF, SC	71-92	Yes (45-75)
	Large Parking Apron	P.C.C.	7	693	None	-	-	-	-	-	-	CL, SF, SC	71-92	Yes (45-75)
Hill Air Force Base, Ogden, Utah	Original Anchorage	P.C.C.	6	385	Compacted Sand Subgrade	6	10-85	Yes (6-55)	-	-	-	SF, SF, SW	10-85	Yes (6-55)
	b-c, NE-SW, NW-SE Runways	P.C.C.	6	516	Compacted Sand Subgrade	6	10-85	Yes (6-55)	-	-	-	SF, SF, SW	10-85	Yes (6-55)
	EW Runway	P.C.C.	6	516	Compacted Sand Subgrade	6	10-85	Yes (6-55)	-	-	-	SF, SF, SW	10-85	Yes (6-55)
		P.C.C.	6	516	Compacted Sand Subgrade	6	10-85	Yes (6-55)	-	-	-	SF, SF, SW	10-85	Yes (6-55)

(1) K_f = Subgrade Modulus during Frost
(2) Depth of Frost Penetration from Fr
(3) The figures tabulated denote the s
year of usage prior to pavement co
given cycles prior to the first of
" pavement Condition" traffic data

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EVALUATION LBS. GROSS PLANE WEIGHT		TRAFFIC		PAVEMENT CONDITION						
NORMAL PERIOD M. PART XIII JULY 1946	FROST CONDITIONS E.M. PART XII	GROSS PLANE WT. (LBS.)	MAX. AVG. DAILY TRAFFIC (3)	LOCATION	LINE (4)	DESIGN THICKNESS	% OF DESIGN (8)	DESCRIPTION	DATE OF SURVEY	REPORTED CAUSE OF FAILURE
10,000	< 10,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	- - 95 - - -	Taxiways 1 and 5 Taxiways 2, 3, 4, 7 Taxiways 9-13 ind.	1 2 3	18 18 18	30 40 33	Cracking and rutting, on scattered areas of taxiways 1, 2, 9, 12 and 13 followed by complete breakup of pavement and base course. Taxiways 3, 4, 5, 7, 10 and 11 satisfactory.	Mar. 1944	Local poor subgrade, ponding, poor base, slight frost action in subgrade.
24,000	< 10,000			Runways and Runway shoulders	4	18	33	Small depressed cracked and checked areas.		Differential settlement under traffic.
20,000	< 10,000			Apron	5	11	64	Cracking and slab displacement.		Overstressing along taxiway lanes.
20,000	< 10,000									
50,000	< 10,000									
< 30,000	< 30,000									
< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	115	E-W Runway NE-SW and NW-SE Runways	6 7	7 8	114 75	Sheared tongue and groove joints, corner cracks, spalling and fracturing of concrete for a width of several inches at joints.	June 1944	Overloading subgrade, weakening of subgrade during thaw.
< 30,000	< 30,000			Apron and Taxiways	8	11	55	Satisfactory conditions.		
30,000	< 30,000			N-S Runway	9	7	86	Satisfactory conditions.		
30,000	< 30,000			Design thicknesses determined using a 20,000 lb. wheel load						
< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	- 12 7 11 0cc. 6/No. 1/No.	Runways Aprons and taxiway A Taxiway B	10 11 12	10 13 13	70 65 65	Good to very good condition except for some cracking and joint spalling on Taxiway A.	April 1947	
30,000	< 30,000									
107,000	26,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	- 2 - 4 - - -	Main service apron Runways Taxiways	13 14 15	13 13 13	46 67 67	Satisfactory condition.	Spring 1943 Fall 1946	
< 30,000	< 30,000			Apron widening, turnaround and warm-up apron (Not controlling pavements).		13	54	Random and corner cracks. 9% of slabs cracked in Spring of 1943. 30% cracked by Fall of 1946.		Settlement of subgrade, low strength of concrete and frost action.
72,000	26,000		3/No.							
< 30,000	< 30,000									
15,000	< 10,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	- 56 - - - -	Runways Taxiways	16 17	13 13	46 46	Longitudinal cracking at joints between runway or taxiway pavement and shoulder pavement allowing water to enter base. Depressions occurred under traffic.	Not Reported (1944)	Inadequate drainage. Frost action.
13,000	< 10,000									
16,000	< 10,000									
18,000	< 10,000			Apron	18	9	78	Satisfactory condition.		
30,000	< 30,000									
< 30,000	< 30,000									
< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	119 136 18 15 0cc. 1 -	No Data						
< 30,000	< 30,000									
< 30,000	< 30,000									
< 30,000	< 30,000									

Headings denote plotted points on Plate 2.

is the ratio of the actual pavement thickness to design thickness x 100.
For average wheel load of heaviest weight class of planes using field
by of 5 or more cycles of landings and take-offs per day prior to condition

materials under flexible paved areas are frost susceptible they were considered
borderline materials were considered non-frost susceptible.

SUMMARY TABULATION OF AIRFIELD PAVEMENTS

AIRFIELD	LOCATION	PAVEMENT			BASE					SUBGRADE						
		TYPE	THICKNESS (INCHES)	FLEXURAL STRENGTH OF CONCRETE AT 28 DAYS (LBS./SQ IN.)	TYPE	THICKNESS (INCHES)	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.075 mm)	C.B.R. OR SUBGRADE MODULUS			AIRFIELD CLASSIFICATION	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.075 mm)	ATTERBERG LIMITS	
									K	K _{f(1)}	C.B.R.				L.L.	P.L.
Kearney Air Force Base, Kearney, Nebraska	Apron	F.C.C.	12-4 1/2-11	450	Sand Cushion	8	26-89	Yes (12-55)	-	-	-	CL, ML, CH	82-94	Yes (12-55)	50-52	16-24
	Taxiways	F.C.C.	12-4 1/2-11	425	Sand Cushion	8	26-89	Yes (10-55)	-	-	-	CL, ML	82-94	Yes (12-55)		
	B-3 Runway	F.C.C.	12-4 1/2-11	490	Sand Cushion	8	26-89	Yes (12-55)	-	-	-	CL, CH, ML, SF	82-94	Yes (12-55)		
	NE-SW Runway	F.C.C.	7	450	Sand Cushion	5	26-89	Yes (12-55)	-	-	-	CL, ML	82-94	Yes (12-55)		
	NW-SE Runway	F.C.C.	12-4 1/2-11	400	A.C. Pavement Sand Cushion	2 8	26-89	Yes (12-55)	-	-	-	CL, ML	82-94	Yes (12-55)		
Lockbourne Air Force Base, Columbus, Ohio	Main Apron Ext. Taxiways F, G, H, J	F.C.C.	8	590	Stabilized Gravel	5	24-41	Yes (10-16)	-	-	-	CL, ML	44-67	Yes (28-42)	24-52	13-25
	East and West Wing	F.C.C.	8	590	Stabilized Gravel	6	23-41	Yes (10-16)	-	-	-	CL, ML	44-67	Yes (28-42)		
	N-S and NE-SW Runways, Taxiways C, D, E, Main Apron	F.C.C.	10-7-10	590	Stabilized Gravel	5-6-5	23-41	Yes (10-16)	-	-	-	CL	44-67	Yes (28-42)		
	NW-SE Runway Taxiway A E-W Runway Taxiway B	F.C.C.	10-7-10	610	Stabilized Gravel	5-7-5	23-41	Yes (10-16)	-	-	-	CL	44-67	Yes (28-42)		
Lowry Air Force Base, Denver, Colorado	Apron No. 1	F.C.C.	14-8	520-565	None	-	-	-	-	-	-	SF-CL, SF, CH	32-69	Yes (14-48)	16-50	15-28
	Taxiways Runways	F.C.C.	14-8	565	None	-	-	-	-	-	-	CL, SF	32-69	Yes (14-48)		
	Apron No. 2	F.C.C.	18-12-14	520	None	-	-	-	-	-	-	CL, SF	32-69	Yes (14-48)		
Marshall Air Force Base, Fort Riley, Kansas	Taxiways and Aprons	F.C.C.	6	500	None	-	-	-	-	-	-	ML, CH, CL	46-96	Yes (28-54)	21-67	15-28
	Runways	F.C.C.	6	500	None	-	-	-	-	-	-	ML, CH, CL	46-96	Yes (28-54)		
Mitchel Air Force Base, Hempstead, Long Island, New York	Hanger Apron	F.C.C.	6	430	Sand and Gravel	12	7-46	Yes (4-32)	140	-	-	GF	20-87	Yes (12-56)	25	23
	NE-SW Runway	F.C.C.	18-6	506	Mech. Stab. sand and Gravel	12	7-46	Yes (4-32)	250	-	-	SW	20-87	Yes (12-56)		
	E-W Taxiway	F.C.C.	6	525	Compacted Subg. Silt, Sand, Gravel	12	7-46	Yes (4-32)	160	-	-	GC	20-97	Yes (12-56)		
	E-W Runway	F.C.C.	6	480	Mech. Stab. sand and Gravel	12	7-46	Yes (4-32)	210	-	-	SW	20-87	Yes (12-56)		
	NE-SW Runway	F.C.C.	6	515	Compacted Subg. Silt, Sand, Gravel	12	7-46	Yes (4-32)	240	-	-	GF	20-87	Yes (12-56)		
	B-3 Runway	F.C.C.	6	534	Compacted Subg. Selected Borrow	12	7-46	Yes (4-32)	400	-	-	GF	20-87	Yes (12-56)		
Offutt Air Force Base, Fort Crook, Nebraska	B-3 Runway	Asphaltic Concrete	2 1/2	-	Gravel (Bit. Stab.)	9 1/2	-	-	-	-	80	CL	85-94	Yes (14-65)	36-48	18-25
	Hanger Apron	F.C.C.	6	685	None	-	-	-	-	-	-	CL	85-94	Yes (14-65)		
	NE-SW Runway	F.C.C.	11	685	None	-	-	-	-	-	-	CL	85-94	Yes (14-65)		
	NW-SE Runway	F.C.C.	9	685	Asphalt Bit. Stab. Gravel	2 1/2	-	-	405	45	-	CL, ML	85-94	Yes (14-65)		
Greentree Air Force Base, Millstone, Pennsylvania	Taxiway between runways 24 and 32	Bit. Conc.	1	-	No. 4 Trap Hook	8	-	No	-	-	80	CL	46-65	Yes (10-25)	20-22	16-19
	Runway 10-32 Runway 11-9	F.C.C.	6	316	None	-	-	-	-	-	-	CL	46-72	Yes (16-47)		
Fatherhood Field, Fairfield, Ohio	Apron	F.C.C.	6	710	Fit Run Gravel	18	2-12	Assumed No	400	65	-	GF	22-90	Yes (14-75)	22-71	17-32
	Taxiway No. 1	F.C.C.	8	735	Fit Run Gravel	6	2-12	Assumed No	-	-	-	CL	22-90	Yes (14-75)		
	Runway A	F.C.C.	7	710	Stab. Gravel	8	10	Yes (1-10)	-	-	-	ML	22-90	Yes (14-75)		
	Runways B & C	F.C.C.	9	695	Fit Run Gravel	6	2-12	Assumed No	-	-	-	ML, CL	22-90	Yes (14-75)		

(1) K_f = Subgrade Modulus during Frost Melting Period.
 (2) Depth of Frost Penetration from Freezing Index Curve.
 (3) The figures tabulated denote the average daily cycle year of usage prior to pavement condition survey. It gives cycles prior to the first of the two conditions. "Pavement Condition" traffic data is for period prior

A

FROST INVESTIGATION
1949-1950
SUMMARY TABULATION OF AIRFIELD PAVEMENTS

C.B.R. OR GRADE MODULUS		SUBGRADE								GROUND WATER DEPTH (FEET)	SUBSURFACE DRAINAGE	APPROX FREEZING INDEX	FROST PENE- TRATION (INCHES)	EVALUATION		TRAFFIC	
		AIRFIELD CLASSIFICATION	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.075mm)	ATTERBERG LIMITS		C.B.R. OR SUBGRADE MODULUS							NORMAL PERIOD E.M. PART XII JULY 1948	FROST CONDITIONS E.M. PART XII	GROSS PLANE WT. (LBS.)	MAX DA TRA
					L.L.	P.L.	K	K _f (1)	C.B.R.								
-	-	CL, ML, CH	42-94	Yes (45-69)	50-51	14-24	14.3	-	-	19-40	None reported	100	12 (2)	< 30,000	< 30,000	< 15,000	-
-	-	CL, ML	82-94	Yes (45-69)	-	-	14.3	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	-
-	-	CL, CH, ML, SF	82-94	Yes (45-69)	-	-	14.3	-	-	-	-	-	-	30,000	< 30,000	35-50,000	-
-	-	CL, ML	82-94	Yes (45-69)	-	-	14.3	-	-	-	-	-	-	35,000	< 30,000	50-75,000	-
-	-	CL, ML	82-94	Yes (45-69)	-	-	14.3	-	-	-	-	-	-	50,000	< 30,000	75-120,000	-
-	-	CL, ML	82-94	Yes (45-69)	-	-	14.3	-	-	-	-	-	-	50,000	< 30,000	120-155,000	-
-	-	CL, ML	44-67	Yes (28-42)	24-52	15-25	50	-	-	3-5	Perforated pipe in trenches backfilled with graded filter material on either side of runways.	100	25	< 30,000	< 30,000	< 15,000	-
-	-	CL, ML	44-67	Yes (28-42)	-	-	50	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	12
-	-	CL	44-67	Yes (28-42)	-	-	50	-	-	-	-	-	-	30,000	< 30,000	35-50,000	13
-	-	CL	44-67	Yes (28-42)	-	-	50	-	-	-	-	-	-	30,000	< 30,000	50-75,000	67
-	-	CL	44-67	Yes (28-42)	-	-	50	-	-	-	-	-	-	30,000	< 30,000	75-120,000	94
-	-	CL	44-67	Yes (28-42)	-	-	50	-	-	-	-	-	-	30,000	< 30,000	120-155,000	94
-	-	SF-CL, SF, CH	32-69	Yes (14-48)	15-50	15-28	52	-	-	5	Open joint pipe and gravel backfill trenches along shoulders of some pavements.	200	21 (2)	< 30,000	< 30,000	< 15,000	76
-	-	CL, SF	32-69	Yes (14-48)	-	-	52	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	150
-	-	CL, SF	32-69	Yes (14-48)	-	-	52	-	-	-	-	-	-	30,000	< 30,000	35-50,000	173
-	-	CL, SF	32-69	Yes (14-48)	-	-	52	-	-	-	-	-	-	30,000	< 30,000	50-75,000	50
-	-	CL, SF	32-69	Yes (14-48)	-	-	52	-	-	-	-	-	-	30,000	< 30,000	75-120,000	80
-	-	CL, SF	32-69	Yes (14-48)	-	-	52	-	-	-	-	-	-	30,000	< 30,000	120-155,000	80
-	-	ML, CH, CL	84-96	Yes (28-54)	21-67	15-28	112	-	-	0-18	None	200	21 (2)	< 30,000	< 30,000	< 15,000	51
-	-	ML, CH, CL	84-96	Yes (28-54)	-	-	112	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	10
-	-	ML, CH, CL	84-96	Yes (28-54)	-	-	112	-	-	-	-	-	-	< 30,000	< 30,000	35-50,000	1
-	-	ML, CH, CL	84-96	Yes (28-54)	-	-	112	-	-	-	-	-	-	< 30,000	< 30,000	50-75,000	8/9
-	-	ML, CH, CL	84-96	Yes (28-54)	-	-	112	-	-	-	-	-	-	< 30,000	< 30,000	75-120,000	Dec
-	-	ML, CH, CL	84-96	Yes (28-54)	-	-	112	-	-	-	-	-	-	< 30,000	< 30,000	120-155,000	Dec
-	-	GP	20-87	Yes (12-56)	25	23	-	-	-	21	Open joint drain pipe along edge of road areas.	150	18 (2)	< 30,000	< 30,000	< 15,000	16
-	-	SW	20-87	Yes (12-56)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	10
-	-	GC	20-87	Yes (12-56)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	35-50,000	4
-	-	SW	20-87	Yes (12-56)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	50-75,000	19
-	-	GP	20-87	Yes (12-56)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	75-120,000	6/No
-	-	GP	20-87	Yes (12-56)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	120-155,000	14/No
-	-	GP	20-87	Yes (12-56)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	> 155,000	-
-	80	CL	85-94	Yes (44-65)	36-48	18-25	-	-	8	Not Reported	None	740	39 (2)	19,000	< 10,000	< 15,000	7
-	-	CL	85-94	Yes (44-65)	-	-	83	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	6
-	-	CL	85-94	Yes (44-65)	-	-	83	-	-	-	-	-	-	50,000	< 30,000	35-50,000	1
45	-	CL, ML	85-94	Yes (44-65)	-	-	-	-	-	-	-	-	-	30,000	< 30,000	50-75,000	1
-	80	CL	46-65	Yes (10-25)	20-22	16-19	-	-	3	Not Reported	Perforated concrete pipe 4.5 ft. from edge pav- ements in trenches, back- filled with crushed stone under 6" of con- solidated earth.	150	-	< 10,000	< 10,000	< 15,000	6
-	-	CL	46-72	Yes (16-47)	-	-	100	-	-	-	-	-	-	< 30,000	< 30,000	15-35,000	10
-	-	CL	46-72	Yes (16-47)	-	-	100	-	-	-	-	-	-	< 30,000	< 30,000	35-50,000	10
-	-	CL	46-72	Yes (16-47)	-	-	100	-	-	-	-	-	-	< 30,000	< 30,000	50-75,000	3/4
-	-	CL	46-72	Yes (16-47)	-	-	100	-	-	-	-	-	-	< 30,000	< 30,000	75-120,000	6/4
-	-	CL	46-72	Yes (16-47)	-	-	100	-	-	-	-	-	-	< 30,000	< 30,000	120-155,000	6/4
65	-	GP	22-90	Yes (14-75)	22-71	17-32	-	-	-	4-7	None	150	23	< 30,000	< 30,000	< 15,000	98
-	-	CL	22-90	Yes (14-75)	-	-	40	25	-	-	-	-	-	< 30,000	< 30,000	15-35,000	17
-	-	ML	22-90	Yes (14-75)	-	-	80	-	-	-	-	-	-	40,000	30,000	35-50,000	21
-	-	ML, CL	22-90	Yes (14-75)	-	-	80	25	-	-	-	-	-	40,000	30,000	50-75,000	5/4
-	-	ML, CL	22-90	Yes (14-75)	-	-	80	25	-	-	-	-	-	50,000	30,000	75-120,000	5/4
-	-	ML, CL	22-90	Yes (14-75)	-	-	80	25	-	-	-	-	-	50,000	30,000	120-155,000	5/4
-	-	ML, CL	22-90	Yes (14-75)	-	-	80	25	-	-	-	-	-	50,000	30,000	> 155,000	5/4

NOTES

(1) K_p = Subgrade Modulus during Frost Melting Period.

(2) Depth of Frost Penetration from Freezing Index Curve, Chapter 4, Part XIII of Engineering Manual.

(3) The figures tabulated denote the average daily cycles of landing and take-offs for the maximum year of usage prior to pavement condition survey. Where two columns are tabulated, left column gives cycles prior to the first of the two condition surveys. Where "No Data" is shown under "Pavement Condition" traffic data is for period prior to January 1950.

(4) Numbers under "Line" heading denote plotted points on Plate 2.

(5) "Percent of Design" is the ratio of the actual pavement thickness to design thickness is for average wheel load of heaviest weight class with average frequency of 5 or more cycles of landings and take-offs survey.

Where base or subbase materials under flexible paved areas are frost as controlling the design. Borderline materials were considered non-

B

EMENTS

EVALUATION LBS. GROSS PLANE WEIGHT	TRAFFIC		PAVEMENT CONDITION								
	NORMAL PERIOD E.M. PART XII JULY 1946	FROST CONDITIONS E.M. PART XII	GROSS PLANE WT. (LBS.)	MAX. AVG. DAILY TRAFFIC (3)	LOCATION	LINE (4)	DESIGN THICKNESS	% OF DESIGN (5)	DESCRIPTION	DATE OF SURVEY	REPORTED CAUSE OF FAILURE
< 30,000	< 30,000	< 15,000	-	33	Apron	19	18	47	Complete failure taxiway 1A and S.E. corner of apron. Excessive cracking particularly at joints on Taxiways 1B, 2 and 3.	Mar. 1947	Poor subgrade and insufficient pavement thickness. Frequent load repetitions over confined areas.
< 30,000	< 30,000	15-35,000	-	4	Taxiways 1A, 1B, 2 and 3	20	18	47			
30,000	< 30,000	35-50,000	4	5							
38,000	< 30,000	50-75,000	4	5	NE-SW Runway	21	14	50			
30,000	< 30,000	75-120,000	-	-	NW-SE Runway	22	13	65	Numerous cracks and joint failures.	May 1947	Overloading and poor subgrade conditions.
30,000	< 30,000	120-135,000	-	-	N-S Runway	23	14	61			
30,000	< 30,000	> 135,000	-	-	Taxiways	20	18	47	Excessive cracking and joint failures		Overloading and poor subgrade conditions.
< 30,000	< 30,000	< 15,000	-	-	Main Apron	24	15	53	75% of slab with cracks, corner breaks or spalls.	Mar. 1947	Pavement 11 years old. Age and large slab size believed responsible for failure.
< 30,000	< 30,000	15-35,000	12	-							
< 30,000	< 30,000	35-50,000	13	-	Apron Int., Apron Wings and Taxiways	25	15	53	Good to excellent condition		
< 30,000	< 30,000	50-75,000	67	-	N-S and NE-SW Runway	26	12	67			
36,000	< 30,000	75-120,000	Dec.	-	NW-SE Runway	27	12	58			
< 30,000	< 30,000	> 135,000	9 Mo.	-	E-W Runway	28	11	44			
< 30,000	< 30,000	< 15,000	76	-	Apron No. 1 and Taxiways	29	23	26	Fair to poor condition, considerable cracking, especially shrinkage cracks.	May 1947	Shrinkage cracks due to construction during cold weather period. Pavements consistently overloaded.
< 30,000	< 30,000	15-35,000	150	-							
< 30,000	< 30,000	35-50,000	173	-	Apron No. 2	30	23	52	Good condition.		Fair condition
36,000	< 30,000	50-75,000	5c	-	Runways	31	16	38			
< 30,000	< 30,000	< 15,000	51	-	No Data.						
< 30,000	< 30,000	15-35,000	10	-							
< 30,000	< 30,000	35-50,000	2	0 Mo.							
< 30,000	< 30,000	50-75,000	2	0 Mo.							
< 30,000	< 30,000	75-120,000	Dec.	-							
< 30,000	< 30,000	120-135,000	Dec.	-							
< 30,000	< 30,000	> 135,000	-	-							
< 30,000	< 30,000	< 15,000	167	-	No Data						
< 30,000	< 30,000	15-35,000	104	-							
< 30,000	< 30,000	35-50,000	47	-							
< 30,000	< 30,000	50-75,000	192	-							
< 30,000	< 30,000	75-120,000	6 Mo.	-							
< 30,000	< 30,000	120-135,000	14 Mo.	-							
< 30,000	< 30,000	> 135,000	-	-							
19,000	< 10,000	< 15,000	71	-	NW-SE Runway	32	15	60	Good to excellent condition.	May 1947	Not Reported.
< 30,000	< 30,000	15-35,000	64	-	NE-SW Runway	33	15	73	Fair condition. Large number of transverse and diagonal cracks.		
< 30,000	< 30,000	35-50,000	18	-							
50,000	< 30,000	50-75,000	1	-	Hanger Apron	34	19	32	Extensive cracking. Numerous shattered slabs, and spalls.		
34,000	< 30,000	75-120,000	17	-							
< 30,000	< 30,000	> 135,000	-	-							
< 10,000	< 10,000	< 15,000	61	-	No Data						
< 30,000	< 30,000	15-35,000	10	-							
< 30,000	< 30,000	35-50,000	10	-							
< 30,000	< 30,000	50-75,000	7	-							
< 30,000	< 30,000	75-120,000	5 Mo.	-							
< 30,000	< 30,000	120-135,000	6 Mo.	-							
< 30,000	< 30,000	> 135,000	-	-							
< 30,000	< 30,000	< 15,000	-	-	Apron	35	11	55	Good to very good condition.	April 1947	
< 30,000	< 30,000	15-35,000	96	-	Taxiways	36	12	67			
< 30,000	< 30,000	35-50,000	17	-	Runway A	37	9	78			
40,000	30,000	50-75,000	21	-	Runways B and C	38	10	90			
58,000	30,000	75-120,000	6 Mo.	-							
58,000	30,000	120-135,000	2	-							
58,000	30,000	> 135,000	-	-							

"me" heading denote plotted points on Plate 2.

"m" is the ratio of the actual pavement thickness to design thickness x 100.
 is for average wheel load of heaviest weight class of planes using field frequency of 5 or more cycles of landings and take-offs per day prior to condition

base materials under flexible paved areas are frost susceptible they were considered the design. Borderline materials were considered non-frost susceptible.

SUMMARY TABULATION OF AIRFIELD PAVEMENTS

AIRFIELD	LOCATION	PAVEMENT			BASE						SUBGRADE					
		TYPE	THICKNESS (INCHES)	FLEXURAL STRENGTH OF CONCRETE AT 28 DAYS (LBS./SQ. IN.)	TYPE	THICKNESS (INCHES)	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.02 mm)	C.B.R. OR SUBGRADE MODULUS			AIRFIELD CLASSIFICATION	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.02mm)	ATYPERE LIMITS	
									K	K _f (1)	C.B.R.				L.L.	P
Presque Isle Air Force Base, Presque Isle, Maine	Hangar Service Aprons and Taxiways A to F, Runways	P.C.C.	3-6-8	553	Sand & Gravel	0-2 1/2 (12 Avg.)	3-10	Borderline (0-2)	300	2 1/2	-	GF	18-50	Yes (12-43)	30	
		Bit. Conc.	3 1/2-4 1/2	-	Sand & Gravel	1-1 1/4 (12 Avg.)	3-10	Borderline (0-2)	-	-	60	GF	18-50	Yes (12-43)		
Rome Airfield, Griffiss Air Force Base, Rome, New York	Runways	P.C.C.	7	665	None	-	-	-	-	-	-	GF (small area SP, WP)	2-1 1/4	Yes (1-6)	22-42	19-
Scott Air Force Base, Belleville, Illinois	Apron and apron extension, taxiways A, B, C and E-W, NE-SW, NW-SE Runways, N-S Runway, Taxiways D, E, and F	P.C.C.	8-6-8	590	None	-	-	-	-	-	-	OL, CL	96-98	Yes (52-74)	25-43	18-
		P.C.C.	8-6-8	590	None	-	-	-	-	-	-	OL	96-98	Yes (52-74)		
		P.C.C.	9-6-9	700	None	-	-	-	-	-	-	OL	96-98	Yes (52-74)		
Selfridge Air Force Base, Mt. Clemens, Michigan	Original E-W Runway (used as apron) original N-S Runway (used as taxiway) NE-SW and E-W Runways, N-S Runway, Apron	P.C.C.	8-6-8	649	None	-	-	-	-	-	-	ML	35-93	Yes (18-73)	21-52	20-
		P.C.C.	12-9-12	742	Gravel Sand	6 18	6-12 5	Yes (3-5) No (1)	176	-	-	ML, CR	35-93	Yes (18-75)		
		P.C.C.	12-9-12	723	Gravel Sand	6 18	6-12 5	Yes (3-5) No (1)	190	-	-	ML	35-93	Yes (18-73)		
		P.C.C.	12-10-12	750	Gravel	12	6-12	Yes (3-5)	130	-	-	ML	35-93	Yes (18-73)		
Sherman Air Force Base, Fort Leavenworth, Kansas	N-S & NW-SE Runway ends, Runways, Taxiways	P.C.C.	9-6-9	-	Cinders	6	-	-	-	-	-	-	-	-	-	-
		Cinders	6	-	-	-	-	-	-	-	-	-	-	-	-	-
		P.C.C.	9-6-9	-	Cinders	6	-	-	-	-	-	-	-	-	-	-
Smoky Hill Air Force Base, Salina, Kansas	NE-SW & E-W Runways, NW-SE Runway, Taxiways 1-2, L-12, original apron, N-S Runway	P.C.C.	8	490	None	-	-	-	-	-	-	CL, CR	66-99	Yes (30-76)	35-65	17-3
		P.C.C.	8	540	None	-	-	-	-	-	-	CL, CR	66-99	Yes (30-76)		
		P.C.C.	8	613	None	-	-	-	-	-	-	CL, CR	66-99	Yes (30-76)		
		P.C.C.	8	613	None	-	-	-	-	-	-	CL, CR	66-99	Yes (30-76)		
Spokane Air Force Base, Spokane, Washington	NE-SW Runway, Left and right wing, Center Taxiways, E-W, N-S Runway, Apron	P.C.C.	8-6-8	675	Pit Run Gravel	12	4-10	Assumed No	217	45	-	GF, GW, SG, SP, ML	2-73	Yes (2-44)	16-33	16-3
		P.C.C.	8-6-8	675	Pit Run Gravel	12	4-10	Assumed No	217	45	-	GF, GW, SG, SP, ML	2-73	Yes (2-44)		
		P.C.C.	8-6-8	919	Pit Run Gravel	12	4-10	Assumed No	217	45	-	GF, GW, SP, SP, ML	2-73	Yes (2-44)		

(1) K_f = Subgrade Modulus during Frost Melting Period.
 (2) Depth of Frost Penetration from Freezing Index Cur.
 (3) The figures tabulated denote the average daily cycle year of usage prior to pavement condition survey. gives cycles prior to the first of the two condition "Pavement Condition" traffic data is for period pri

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**FROST INVESTIGATION
1949 - 1950
SUMMARY TABULATION OF AIRFIELD PAVEMENTS**

SUBGRADE							GROUND WATER DEPTH (FEET)	SUBSURFACE DRAINAGE	APPROX. FREEZING INDEX	FROST PENETRATION (INCHES)	EVALUATION		TRAFFIC		
PASSING 200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.075mm)	ATTERBERG LIMITS		C.B.R. OR SUBGRADE MODULUS							NORMAL PERIOD E.M. PART XII JULY 1946	FROST CONDITIONS E.M. PART XII	GROSS PLANE WT. (LBS.)	MAX. AVG. DAILY TRAFFIC (3)	
		L.L.	P.L.	K	K _f (1)	C.B.R.									
18-50	Yes (12-43)	50	20	-	-	-	2-6	Perforated metal pipe in trenches backfilled with coarse graded sand and 75% open joint pipe with run of bank gravel backfill laid edges of runways.	200	71	< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	- - 5 25 - -	Partic
13-50	Yes (12-43)	-	-	-	-	10					65,000	13,000			Apron
2-14	Yes (1-8)	20-42	19-26	220	-	-	Not Reported	Not Reported.	750	39 (2)	30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	78 48 50 3 7/Mo. 20/Mo.	No Data
9-98	Yes (52-74)	25-43	18-26	66	-	-	Below Influence depth	Open joint tile drains along edges of runway pavement	150	12	< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	157 208 21 12 2/Mo. 16/Mo.	Apron E-W Runway
9-98	Yes (52-74)	-	-	66	-	-					< 30,000	< 30,000			N-S, Apron
9-98	Yes (52-74)	-	-	66	-	-					< 30,000	< 30,000			Apron E-W Runway
3-93	Yes (18-73)	21-52	20-27	85	-	-	0.5-6.0	Perforated tile pipe backfilled with bank run gravel along edges of all pavements. Open joint tile pipe backfilled with gravel on 30' centers under apron and interior of field.	520	30	< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	100 110 14 75 -	Original NE-SW Apron
35-93	Yes (18-73)	-	-	48	-	-					34,000	< 30,000		13/Mo. Dec.	N-S Apron
35-93	Yes (18-73)	-	-	48	-	-					55,000	< 30,000			N-S Apron
35-93	Yes (18-73)	-	-	48	-	-					36,000	< 30,000			
-	-	-	-	-	-	-	Shallow	Not Reported.	250	21 (2)	-	-	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	13 4 3 5/Mo. -	No Data
6-49	Yes (30-76)	35-65	17-29	84	-	-	Not Reported	Not Reported.	150	18 (2)	30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	20 25 8 25	No Data
6-49	Yes (30-76)	-	-	84	-	-					30,000	< 30,000			
6-49	Yes (30-76)	-	-	84	-	-					< 35,000	< 30,000		1/Mo. 41 Dec.	
6-49	Yes (30-76)	-	-	84	-	-					40,000	< 30,000			
2-73	Yes (2-44)	16-33	15-37	-	-	-	Not Reported	Not Reported.	250	24	< 30,000	< 30,000	<15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 >135,000	27 40 10 9 10/Mo. 15 Dec.	No Data
2-73	Yes (2-44)	-	-	-	-	-					30,000	< 30,000			
2-73	Yes (2-44)	-	-	-	-	-					30,000	< 30,000			

NOTES

(1) Values during Frost Melting Period.

(2) Penetration from Freezing Index Curve, Chapter II, Part XII of Engineering Manual.

(3) Data denote the average daily cycles of landings and take-offs for the maximum prior to pavement condition survey. Where two columns are tabulated, left column prior to the first of the two condition surveys. Where "No Data" is shown under "Traffic" traffic data is for period prior to January 1950.

(4) Numbers under "Line" heading denote plotted points on Plate 2.

(5) "Percent of Design" is the ratio of the actual pavement thickness to design thickness. Design thickness is for average wheel load of heaviest weight class of planes using with average frequency of 5 or more cycles of landings and take-offs per day prior to survey.

Where base or subbase materials under flexible paved areas are frost susceptible they are controlling the design. Borderline materials were considered non-frost susceptible.

B

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EVALUATION		TRAFFIC		PAVEMENT CONDITION						
CLASSIFICATION	FROST CONDITIONS	GROSS PLANE WT.	MAX. AVG. DAILY TRAFFIC	LOCATION	LINE	DESIGN THICKNESS	% OF DESIGN	DESCRIPTION	DATE OF SURVEY	REPORTED CAUSE OF FAILURE
DO NOT EXCEED	E.M. PART XII	(LBS.)	(3)		(4)		(5)			
00	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	- - 5 25 - -	Portion of N-W Runway	59	55	48	Developed weaving during Spring, then of 1945 causing some cracking and rutting.	Spring 1945	Severe frost action in subgrade.
00	15,000			Aprons and Taxiways	59a	15	40	Good condition		
00	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	78 48 50 5 7/No. 20/No. -	No Data.						
00	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	157 208 21 12 2/No. 16/No.	Apron E-W Runway	40 41	15 11	40 55	Cracking at tongue and groove joints and corners on apron. Long cracks on E-W Runway parallel to longitudinal joints.	Fall 1945	Lack of subsurface drainage. Overloading during Spring and Fall of 1945.
00	< 30,000			N-S, SE-SW, NW-SE Runways Apron extension in Taxiways	42 43	11 13	55 46	Generally good condition.	May 1947	
00	< 30,000			Apron E-W Runway	40 41	15 11	40 55	50% of slabs cracked or shattered.		Overloading particularly during thaw.
00	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	100 110 44 75 - 15/No. Dec.	Original E-W and N-S Runways	44	14	45	Extensive cracking and spalling. Transverse cracks open and raveling.	May 1947	Condition consistent with age (15 years) and use.
00	< 30,000			SE-SW Runway Apron	45 46	9 12	100 83	Fair condition with sealing and shrinkage cracks on 50% of slabs.		Constructed during winter. CaCl used in curing process. Not considered failure.
00	< 30,000			N-S and E-W Runways	45	9	100	Good condition.		
00	-	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	15 4 3 5/No. - - -	No Data						
00	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	20 25 8 25 1/No. 41 Dec.	No Data						
00	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	27 40 10 9 10/No. 15 Dec.	No Data						

denote plotted points on Plate 2.

Ratio of the actual pavement thickness to design thickness x 100.

Page wheel load of heaviest weight class of planes using field or more cycles of landings and take-offs per day prior to condition

Slabs under flexible paved areas are frost susceptible they were considered

Borderline materials were considered non-frost susceptible.

SUMMARY TABULATION OF AIRFIELD PAVEMENTS

C

AIRFIELD	LOCATION	PAVEMENT			BASE					AIRFIELD CLASSIFICATION	% PASSING #200 SIEVE		
		TYPE	THICKNESS (INCHES)	FLEXURAL STRENGTH OF CONCRETE AT 28 DAYS (LBS./ SQ. IN.)	TYPE	THICKNESS (INCHES)	% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.075 mm)	C.B.R. OR SUBGRADE MODULUS				
								K	K ₁ (1)	C.B.R.			
Stewart Air Force Base, Newburgh, New York	Taxiways K-1, and I-M	P.C.C.	6	666	Gravel	12	4-14	Yes (5-8)	550	-	-	GF	6-82
	Landing Mat	P.C.C.	4	663	Gravel	12	4-14	Yes (4-6)	411	-	-	GF	6-82
	SE-38 Runway	P.C.C.	6	606	Gravel	12	4-14	Yes (5-8)	250	-	-	GF	6-82
	S-W Runway	P.C.C.	6	606	Gravel	12	4-14	Yes (5-8)	410	-	-	GF	6-82
	SE-38 Runway	P.C.C.	6	606	Gravel	12	4-14	Yes (5-8)	240	-	-	GF	6-82
	S-L Runway	P.C.C.	6	606	Gravel	12	4-14	Yes (5-8)	410	-	-	GF	6-82
Weaver Air Base, (Rapid City Air Force Base), Rapid City, South Dakota	Taxiways A-E, Runway	P.C.C.	7	580	None	-	-	-	-	-	-	CB, CL, GF, OL	55-85
	S-W Runway	P.C.C.	7	565	Asphalt Conc.	5 1/2	-	-	282	-	-	CB, CL, GF	55-85
	SE-24 Runway	P.C.C.	7	580	Asphalt Conc.	5 1/2	9-26	Yes (10)	282	-	-	CB, CL	55-85
	S-W Runway	P.C.C.	7	635	Gravel	8	9-26	Yes (10)	282	-	-	CB, GF, UF, SF	55-85
Hendover Air Force Base, Hendover, Utah	Anchorage Extension "C"	P.C.C.	6	674	Gravel	25	11	Yes (8)	596	-	-	CL, ML, SF, OL	87-99
	Old North Taxiway	P.C.C.	6	683	Gravel	18	11	Yes (8)	406	-	-	ML, SF	87-99
	Anchorage "A" (Original)	P.C.C.	6	683	Gravel	24	11	Yes (8)	406	-	-	CL, ML, SF, OL	87-99
	SE-66 Runway	P.C.C.	6	650	Gravel	17	11	Yes (8)	406	-	-	CL, ML	87-99
	S-W Runway	P.C.C.	6	650	Gravel	24	11	Yes (8)	440	-	-	CL, ML	87-99
	SE-38 Runway	P.C.C.	6	726	Gravel	12-23	11	Yes (8)	500	-	-	CL, SF	87-99
Wright Field Dayton, Ohio	SE-28 Runway	P.C.C.	7	750	Sand & Gravel	9	6	No	-	-	-	ML	1-90
	Taxiways & Apron	P.C.C.	10	650	Bank Run Gravel	6	6	No	-	-	-	ML	1-90
	SE-14 Runway	P.C.C.	8	650	Bank Run Gravel	6	6	No	-	-	-	ML	1-90
	S-W Runway	P.C.C.	9	650	Bank Run Gravel	6	6	No	-	-	-	ML	1-90
	Original Apron	P.C.C.	7	790	None	-	-	-	-	-	-	ML	1-90
	Apron	P.C.C.	6	750	Bank Run Gravel	18	6	No	-	-	-	ML	1-90

(1) K₁ = Subgrade Modulus during
(2) Depth of Frost Penetration
(3) The figures tabulated denote year of usage prior to pavement condition test

A

**FROST INVESTIGATION
1949-1950
SUMMARY TABULATION OF AIRFIELD PAVEMENTS**

L.S. L.B.R.	AIRFIELD CLASSIFICATION	SUBGRADE						GROUND WATER DEPTH (FEET)	SUBSURFACE DRAINAGE	APPROX. FREEZING INDEX	FROST PENE- TRATION (INCHES)	EVALUATION		TRAFFIC			
		% PASSING #200 SIEVE	FROST SUSCEPTIBLE (% FINER THAN 0.075mm)	ATTERBERG LIMITS		C.B.R. OR SUBGRADE MODULUS						NORMAL PERIOD E.M. PART XII JULY 1948	FROST CONDITIONS E.M. PART XII	GROSS PLANE WT. (LBS.)	MAX. AVG. DAILY TRAFFIC (3)		
				L.L.	P.L.	K	K ₁ (1)										C.B.R.
-	GF	6-82	Yes (1-54)	23-22	16-17	-	-	-	0-7	Open joint pipe in previous granular back- fill at low points.	300	50	< 30,000	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	152 246 17 17 Mo. Occ. Occ. -	No Data
-	GF	6-82	Yes (1-54)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	GF	6-82	Yes (1-54)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	GF	7-89	Yes (1-54)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	GF	6-82	Yes (1-54)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	GF	6-82	Yes (1-54)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	CB, CL, GF, OL	53-85	Yes (54)	26-68	11-30	58	-	-	600	None	1,300	10 (2)	< 30,000	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	- 15 27 7 79 101 -	No Data Apron Other All Apron
-	CB, CL, GF	53-85	Yes (54)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	CB, CL	53-85	Yes (54)	-	-	-	-	-	-	-	-	-	30,000	< 30,000	-	-	-
-	CB, GF, UP, BP	53-85	Yes (54)	-	-	-	-	-	-	-	-	-	30,000	< 30,000	-	-	-
-	CL, ML, SP, OL	87-99	Yes (68-96)	23-19	15-40	-	-	-	2-7	None Reported	550	-	< 30,000	< 30,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	6 12 4 90 Occ. 4 -	No Data
-	ML, MW	87-99	Yes (68-96)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	CL, ML, SP, OL	87-99	Yes (68-96)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	CL, ML	87-99	Yes (68-96)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	CL, MW	87-99	Yes (68-96)	-	-	-	-	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	CL, MW	87-99	Yes (68-96)	-	-	-	-	-	-	-	-	-	30,000	< 30,000	-	-	-
-	ML	1-90	Yes (0-54)	20-39	15-26	40	35	-	15-20	MW-SE and KE-CW Runways have side drains of pre- vious material in tranches over 8" pipe. Interceptor drains for Aprons and Taxiways.	150	24	30,000	35,000	< 15,000 15-35,000 35-50,000 50-75,000 75-120,000 120-135,000 > 135,000	- 248 16 12 18 Mo. 5 -	No Data Apron MW-SE E-W Runway 6" Apron Original
-	ML	1-90	Yes (0-54)	-	-	40	25	-	-	-	-	-	35,000	35,000	-	-	-
-	ML	1-90	Yes (0-54)	-	-	40	25	-	-	-	-	-	40,000	35,000	-	-	-
-	ML	1-90	Yes (0-54)	-	-	40	25	-	-	-	-	-	48,000	48,000	-	-	-
-	ML	1-90	Yes (0-54)	-	-	40	25	-	-	-	-	-	< 30,000	< 30,000	-	-	-
-	ML	1-90	Yes (0-54)	-	-	40	25	-	-	-	-	-	< 30,000	< 30,000	-	-	-

NOTES

- (1) K₁ = Subgrade Modulus during Frost Melting Period.
- (2) Depth of Frost Penetration from Freezing Index Curve, Chapter 4, Part XII of Engineering Manual.
- (3) The figures tabulated denote the average daily cycles of landings and take-offs for the maximum year of usage prior to pavement condition survey. Where two columns are tabulated, left column gives cycles prior to the first of the two condition surveys. Where "No Data" is shown under "Pavement Condition" traffic data is for period prior to January 1950.

- (4) Numbers under "Line" heading denote plotted points on Plate 2.
- (5) "Percent of Design" is the ratio of the actual pavement thickness to design thickness. Design thickness is for average wheel load of heaviest weight class of planes using with average frequency of 5 or more cycles of landings and take-offs per day prior survey.
Where base or subbase materials under flexible paved areas are frost susceptible of as controlling the design. Borderline materials were considered non-frost susceptible.

B

MENTS

EVALUATION LBS. GROSS PLANE WEIGHT		TRAFFIC		PAVEMENT CONDITION						
NORMAL PERIOD E.M. PART XII JULY 1946	FROST CONDITIONS E.M. PART XII	GROSS PLANE WT. (LBS.)	MAX. AVG. DAILY TRAFFIC (3)	LOCATION	LINE (4)	DESIGN THICKNESS	% OF DESIGN (8)	DESCRIPTION	DATE OF SURVEY	REPORTED CAUSE OF FAILURE
< 30,000	< 30,000	< 15,000	1-2	No Data						
< 30,000	< 30,000	15-35,000	2L6							
< 30,000	< 30,000	35-50,000	17							
< 30,000	< 30,000	50-75,000	17 Mo.							
< 30,000	< 30,000	75-120,000	Occ.							
< 30,000	< 30,000	120-135,000	Occ.							
< 30,000	< 30,000	> 135,000	-							
< 30,000	< 30,000	< 15,000	-	E-W Runway and shoulders	47	11	64	Setting under traffic in joint areas	Mar. 1945	Moisture penetration into base and subgrade through longitudinal joints. Continued overloading since 1943.
< 30,000	< 30,000	15-35,000	-	Apron	48	16	64	Extensive cracking and crazing	Mar. 1947	
30,000	< 30,000	35-50,000	79	Other Runways	49	11	64	Good condition with considerable scaling.	Mar. 1947	
30,000	< 30,000	50-75,000	-	All taxiways except B	50	16	64	Good to fair condition with considerable scaling.	Mar. 1947	
30,000	< 30,000	75-120,000	-	Apron and taxiway B	48	16	64	Extensive cracking, shattered slabs and joints spalls.	Mar. 1947	
< 30,000	< 30,000	< 15,000	6	No Data						
< 30,000	< 30,000	15-35,000	12							
< 30,000	< 30,000	35-50,000	4							
< 30,000	< 30,000	50-75,000	90							
< 30,000	< 30,000	75-120,000	Occ.							
< 30,000	< 30,000	120-135,000	4							
< 30,000	< 30,000	> 135,000	-							
30,000	< 30,000	< 15,000	-	SE-SW Runway	51	14	50	Good to excellent condition	Mar. 1947	
35,000	34,000	15-35,000	248	Apron (10")	52	20	50			
40,000	34,000	35-50,000	16	SW-SI Runway	53	15	53			
40,000	34,000	50-75,000	12	E-W Runway	54	15	60			
40,000	44,000	75-120,000	18 Mo.	6" Apron and connecting taxiway Original Apron	55	17	41	Fair condition, extensive cracking, numerous shattered slabs.	Mar. 1947	Failures believed due to large slabs.
40,000	44,000	120-135,000	5		56	17	35			
< 30,000	< 30,000	> 135,000	-							
< 30,000	< 30,000	< 15,000	-							

heading denote plotted points on Plate 2.

is the ratio of the actual pavement thickness to design thickness x 100.
for average wheel load of heaviest weight class of planes using field
may of 5 or more cycles of landings and take-offs per day prior to condition

se materials under flexible pave! areas are frost susceptible they were considered
Design. Barrierline materials were considered non-frost susceptible.

SUMMARY TABULATION OF AIRFIELD PAVEMENTS

TRAFFIC HISTORY

1943-1949

AIRFIELD	GROSS PLANE WEIGHT (LBS.)	CYCLES OF LANDINGS AND TAKE OFFS												TRAFFIC DISTRIBUTION			
		1943		1944		1945		1946		1947		1948		1949		RUNWAY	% OF TRAFFIC
		TOTAL	APPROX DAILY	TOTAL	APPROX DAILY	TOTAL	APPROX DAILY	TOTAL	APPROX DAILY	TOTAL	APPROX DAILY	TOTAL	APPROX DAILY				
Casper Air Force Base, Casper, Wyoming	<15,000	-	-	-	-	-	-	-	-	808	2	700	2	6,805	17	HW-SW	62
	15-35,000	-	-	-	-	90	45/mo.	-	-	877	1	800	17/mo.	1,460	4	B-W	29
	35-50,000	-	95	-	95	19	10/mo.	-	-	102	9/mo.	131	11/mo.	204	17/mo.	HW-SE	5
	50-75,000	-	-	-	-	6,714	112	-	-	13	1/mo.	14	1/mo.	-	-	B-W	4
	75-100,000	-	-	-	-	-	-	-	-	-	-	1	0/mo.	-	-	-	-
Chambers Air Force Base, Bensenville, Illinois	<15,000	-	-	-	-	-	-	-	-	17,049	47	19,121	98	23,785	65	HW-SW	30
	15-35,000	-	445	-	445	5,094	14	21,170	90	5,475	15	10,977	30	8,030	22	B-W	30
	35-50,000	-	<15,000	75,000	-	2,124	6	44,895	125	28,236	78	25,461	70	28,470	78	B-W	27
	50-75,000	-	-	-	-	6,139	17	3,285	9	901	2	300	1	345	1	HW-SE	13
	75-100,000	-	-	-	-	-	-	30	3/mo.	-	-	-	-	-	-	-	-
Clinton County Air Force Base, Great Falls, Montana	<15,000	-	-	-	-	-	-	-	-	2,380	7	5,912	16	7,300	20	HW-SW	72
	15-35,000	-	-	-	-	2,353	6	4,444	12	5,463	15	4,799	12	1,460	4	HW-SE	28
	35-50,000	-	6	-	6	1,294	3	2,387	7	2,092	6	3,209	9	2,190	6	-	-
	50-75,000	-	1	-	1	4,087	11	1,884	5	1,449	5	5,398	15	2,555	7	-	-
	75-100,000	-	-	-	-	49	4/mo.	180	4	0/mo.	-	0/mo.	-	-	-	-	-
Dow Air Force Base, Bangor, Maine	<15,000	-	-	-	-	-	-	-	-	22,523	62	25,470	70	29,200	80	HW-SW	51
	15-35,000	-	2	-	2	8,090	22	4,765	13	3,982	11	5,385	9	2,555	7	HW-SE	48
	35-50,000	-	4	-	4	4,765	14	1,004	3	981	2	1,995	4	1,460	4	B-W	1
	50-75,000	-	-	-	-	5,110	14	1,004	3	17	1/mo.	158	13/mo.	131	11/mo.	-	-
	75-100,000	-	-	-	-	36	3/mo.	-	-	2	0/mo.	-	-	12	1/mo.	-	-
Great Falls Air Force Base, Great Falls, Montana	<15,000	-	-	-	-	-	-	-	-	4,707	13	1,506	4	1,014	3	HW-SW	73
	15-35,000	-	-	36	-	10,088	30	24,227	68	5,344	15	4,875	13	5,860	16	B-W	15
	35-50,000	-	-	-	-	1,360	4	1,004	3	987	3	2,304	6	1,095	3	B-W	8
	50-75,000	-	-	-	-	1,091	3	3,045	9	3,899	9	18,224	50	78,118	214	HW-SW	4
	75-100,000	-	-	-	-	27	2/mo.	182	24/mo.	210	17/mo.	191	16/mo.	168	14/mo.	-	-
Hill Air Force Base, Ogden, Utah	<15,000	-	-	-	-	-	-	-	-	43,313	119	24,198	66	11,315	31	HW-SW	43
	15-35,000	-	11	-	11	19,718	43	49,746	136	4,982	14	7,086	22	9,185	25	B-W	20
	35-50,000	-	18	-	18	3,486	10	4,122	12	3,379	9	4,261	12	4,765	13	B-W	20
	50-75,000	-	1	-	1	9,412	19	1,779	4	1,805	5	1,980	5	1,095	3	B-W	17
	75-100,000	-	-	-	-	34	1	242	1	448	1	764	2/mo.	612	51/mo.	-	-
Hosey Air Force Base, Hosey, Nebraska	<15,000	-	-	-	-	-	-	-	-	18,989	33	14,419	40	897	9	B-W	71
	15-35,000	-	-	-	-	2,061	6	1,460	4	1,843	4	9,294	25	2,634	29	HW-SE	17
	35-50,000	-	-	-	-	430	1	244	1/mo.	470	1	705	2	375	4	HW-SW	12
	50-75,000	-	45	-	45	1,490	5	30	3/mo.	13	1/mo.	240	1	63	21/mo.	-	-
	75-100,000	-	-	-	-	4,277	12	4	0/mo.	-	-	41	3/mo.	32	10/mo.	-	-
Hurlburt Air Force Base, Columbus, Ohio	<15,000	-	-	-	-	-	-	-	-	16,346	43	26,200	72	35,770	98	B-W	46
	15-35,000	-	-	-	-	1,485	4	15,267	42	9,091	27	9,095	27	4,745	13	HW-SE	31
	35-50,000	-	105	-	105	1,099	5	4,490	13	4,344	12	6,570	18	1,825	5	B-W	13
	50-75,000	-	1	-	1	27,131	677	485	1	13	1/mo.	56	0/mo.	148	9/mo.	-	-
	75-100,000	-	-	-	-	70	6/mo.	107	9/mo.	2	0/mo.	38	3/mo.	24	2/mo.	-	-
Lawry Air Force Base, Denver, Colorado	<15,000	-	-	-	-	-	-	-	-	27,448	76	27,127	74	29,200	80	B-W	48
	15-35,000	-	190	-	190	1,264	9	38,398	138	21,338	58	23,080	62	24,090	66	HW-SW	28
	35-50,000	-	-	-	-	13,277	36	19,695	54	5,145	14	5,077	14	8,030	22	B-W	24
	50-75,000	-	-	-	-	28,387	76	4,149	11	957	3	805	2	1,095	3	-	-
	75-100,000	-	-	-	-	89,180	80	387	1	198	13/mo.	193	16/mo.	1,095	3	-	-
Marshall Air Force Base, Fort Riley, Kansas	<15,000	-	-	-	-	-	-	-	-	19,911	48	18,617	51	6,805	17	B-W	97
	15-35,000	-	10	-	10	-	-	-	-	1,487	4	1,987	5	1,460	4	HW-SW	43
	35-50,000	-	-	10	-	-	-	-	-	787	8	245	6/mo.	730	2	-	-
	50-75,000	-	8/mo.	-	8/mo.	-	-	-	-	90	0/mo.	23	2/mo.	6	0/mo.	-	-
	75-100,000	-	-	-	-	-	-	-	-	4	-	-	-	2	0/mo.	-	-
Mitchell Air Force Base, Hempstead, Long Island, New York	<15,000	-	-	-	-	-	-	-	-	61,098	167	49,068	134	35,770	98	HW-SW	48
	15-35,000	-	-	-	-	13,289	37	37,889	104	13,477	37	19,988	55	18,290	50	HW-SE	48
	35-50,000	-	-	-	-	7,874	21	7,281	20	7,398	21	14,281	39	17,135	47	B-W	6
	50-75,000	-	192	-	192	8,444	24	2,130	6	1,097	3	979	3	730	2	B-W	1
	75-100,000	-	-	-	-	62	5/mo.	1	0/mo.	2	0/mo.	2	0/mo.	72	6/mo.	-	-
Offutt Air Force Base, Fort Creek, Nebraska	<15,000	-	-	-	-	-	-	-	-	25,098	71	18,615	51	15,695	43	HW-SE	60
	15-35,000	-	35	-	35	-	-	-	-	2,959	8	3,518	10	6,570	18	HW-SW	31
	35-50,000	-	-	18	-	-	-	-	-	1,002	4	4,006	11	7,645	21	B-W	9
	50-75,000	-	-	-	-	-	-	-	-	895	1	800	2	3,285	9	-	-
	75-100,000	-	-	17	-	-	-	-	-	32	3/mo.	20	2/mo.	6	0/mo.	-	-
Shaw Air Force Base, Middletown, Pennsylvania	<15,000	-	-	-	-	-	-	-	-	22,400	61	18,986	51	14,235	39	B-W	62
	15-35,000	-	-	-	-	9,183	25	38,906	105	7,480	20	8,123	22	8,760	24	HW-SE	38
	35-50,000	-	30	-	30	1,321	4	2,846	8	3,088	9	3,358	9	3,650	10	-	-
	50-75,000	-	-	-	-	2,106	6	1,946	5	2,335	7	2,977	8	1,825	5	-	-
	75-100,000	-	-	-	-	2	0/mo.	-	-	71	6/mo.	182	10/mo.	16	1/mo.	-	-

See sheet 2 of 2 for notes

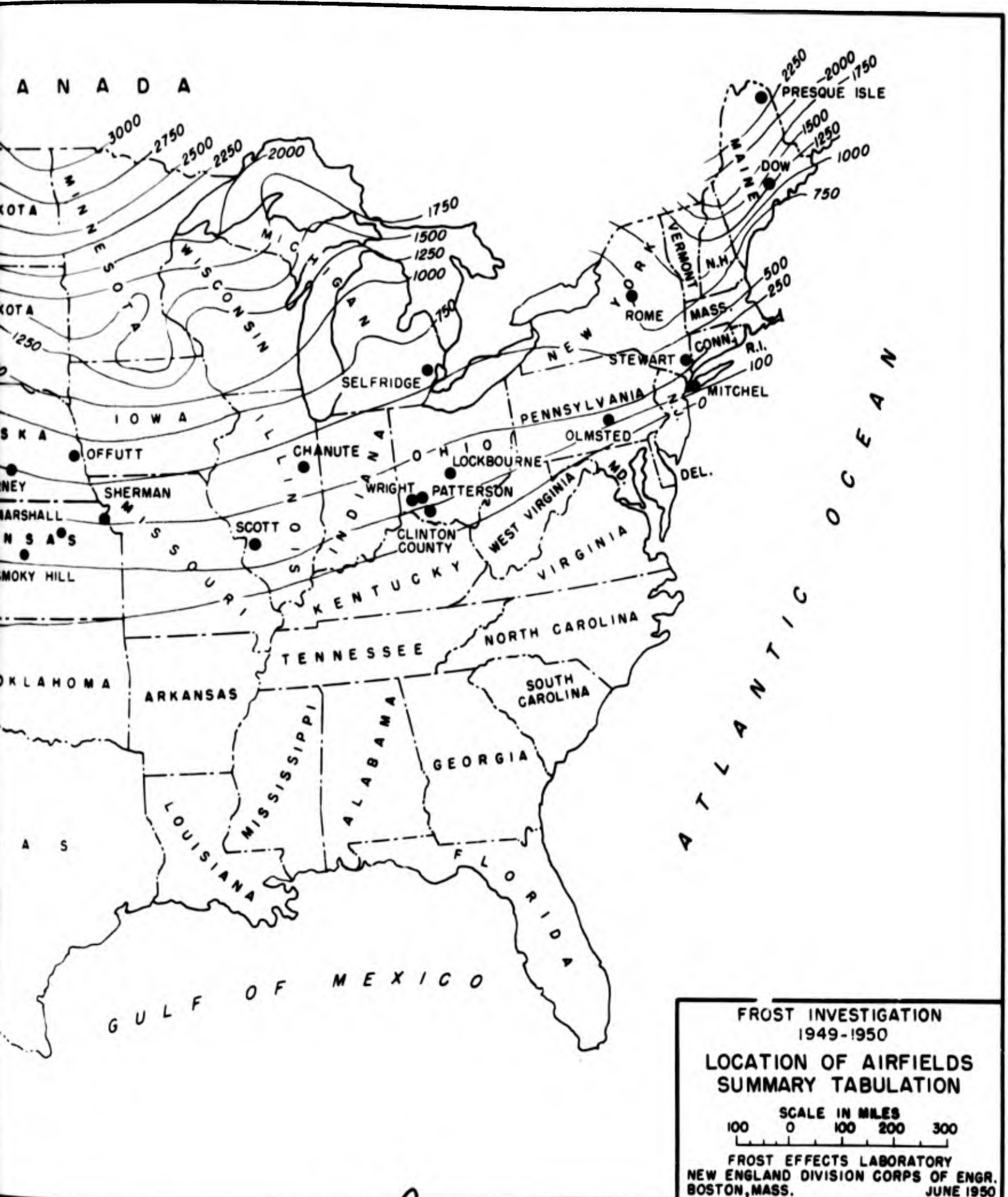
TRAFFIC HISTORY

1943-1949

AIRFIELD	GROSS PLANE WEIGHT (LBS.)	CYCLES OF LANDINGS AND TAKE OFFS												TRAFFIC DISTRIBUTION			
		1943		1944		1945		1946		1947		1948		1949		RUNWAY	% OF TRAFFIC
		TOTAL	APPROX. DAILY	TOTAL	APPROX. DAILY	TOTAL	APPROX. DAILY	TOTAL	APPROX. DAILY	TOTAL	APPROX. DAILY	TOTAL	APPROX. DAILY				
Petterson Field, Fairfield, Ohio	<15,000	-	-	No Data	-	-	-	-	14,899	41	21,398	99	24,090	66	NE-SW (A)	56	
	15-35,000	-	87	-	21,420	79	35,683	88	14,289	39	19,323	53	20,803	57	NE-SW (B)	23	
	35-50,000	-	15	-	5,898	16	6,178	17	6,600	18	9,415	26	11,680	32	NE-SW	21	
	50-75,000	-	12	-	7,534	21	4,681	13	3,185	9	5,000	8	1,885	5	-	-	
	75-120,000	-	-	-	56	5/No.	-	-	-	-	-	16	221	5	-	-	
120-135,000	-	-	-	247	1	878	2	753	2	1,080	3	1,095	3	-	-		
>135,000	-	-	-	-	-	-	-	-	-	45	4/No.	72	6/No.	-	-		
Prosser Isle Air Force Base, Prosser Isle, Maine	<15,000	-	-	No Data	-	-	-	-	496	1	51	10/No.	No Data	-	E-W	16	
	15-35,000	-	-	-	-	-	2,980	8	2,889	6	327	4	-	-	E-W	31	
	35-50,000	-	5	-	120	10/No.	10	87	7/No.	11	4/No.	-	-	-	NE-SW	23	
	50-75,000	-	85	-	260	20/No.	260	53	4/No.	26	8/No.	-	-	-	-	-	
	75-120,000	-	-	-	-	-	-	-	8	0cc.	-	-	-	-	-	-	
120-135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Rome Airfield, (Griffis Air Force Base), Rome, New York	<15,000	-	-	No Data	-	-	-	-	28,344	78	21,955	60	12,775	35	E-W	57	
	15-35,000	-	-	-	3,613	10	17,465	48	2,509	7	4,174	11	3,885	9	NE-SW	36	
	35-50,000	-	90	-	1,880	4	373	2	1,824	3	1,616	5	2,190	6	NE-SW	7	
	50-75,000	-	-	-	1,307	4	648	2	815	2	984	3	730	2	-	-	
	75-120,000	-	-	-	3	0cc.	-	-	-	-	81	7/No.	4	0cc.	-	-	
120-135,000	-	-	-	12	1/No.	59	4/No.	82	7/No.	296	20/No.	-	-	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Scott Air Force Base, Belleville, Illinois	<15,000	-	150	-	14,822	41	74,871	208	57,329	157	46,686	128	37,960	104	E-W	53	
	15-35,000	-	-	-	2,839	8	7,488	21	28,000	77	30,513	84	22,995	63	NE-SW	23	
	35-50,000	-	<15,000 - 75,000	-	4,381	12	530	2	6,853	17	7,409	20	10,280	28	NE-SW	19	
	50-75,000	-	-	-	191	14/No.	96	4/No.	630	2	531	14/No.	600	30/No.	E-W	9	
	75-120,000	-	-	-	-	-	-	-	-	-	-	-	1	0cc.	-	-	
120-135,000	-	-	-	-	-	-	-	-	-	-	-	72	6/No.	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Selfridge Air Force Base, Mt. Clemens, Michigan	<15,000	-	-	No Data	-	-	-	-	34,498	100	37,804	104	59,890	166	E-W	51	
	15-35,000	-	-	-	1,269	3	40,186	110	14,875	39	4,880	13	4,880	13	E-W	41	
	35-50,000	-	-	-	15,886	44	1,578	4	1,376	4	1,772	5	6,878	18	NE-SW	8	
	50-75,000	-	75	-	4,381	3	518	1	343	1	699	2	1,480	40/No.	-	-	
	75-120,000	-	-	-	2	0cc.	-	-	-	-	-	-	-	-	-	-	
120-135,000	-	-	-	13	1/No.	95	5/No.	199	13/No.	138	11/No.	730	2	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Sherman Air Force Base, Fort Leavenworth, Kansas	<15,000	-	-	No Data	-	-	-	-	4,812	13	4,544	12	4,015	11	E-W	77	
	15-35,000	-	-	-	-	-	-	-	770	2	960	3	1,460	4	NE-SW	23	
	35-50,000	-	-	-	-	-	-	-	878	2	1,088	3	960	30/No.	-	-	
	50-75,000	-	-	-	-	-	-	-	55	5/No.	35	3/No.	36	3/No.	-	-	
	75-120,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
120-135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Smoky Hill Air Force Base, Salina, Kansas	<15,000	-	-	No Data	-	-	-	-	4,308	12	7,402	20	2,980	8	E-W	77	
	15-35,000	-	-	-	8,994	25	-	-	2,999	6	4,788	13	4,015	11	NE-SW	17	
	35-50,000	-	-	-	804	2	-	-	1,409	4	2,118	6	2,990	8	NE-SW	5	
	50-75,000	-	25	-	3,941	11	-	-	374	1	448	1	365	1	E-W	1	
	75-120,000	-	-	-	-	-	-	-	11	1/No.	-	-	-	-	-	-	
120-135,000	-	-	-	14,994	41	-	-	7,465	20	5,865	16	6,205	17	-	-		
>135,000	-	-	-	-	-	-	-	-	-	1	0cc.	2	0cc.	-	-		
Spokane Air Force Base, Spokane, Washington	<15,000	-	-	-	-	-	-	-	9,889	27	5,884	16	790	2	NE-SW	79	
	15-35,000	-	10	-	8,205	14	14,100	40	3,433	9	3,565	10	2,995	7	E-W	12	
	35-50,000	-	10	-	350	1	1,992	5	1,847	5	1,610	4	1,460	4	E-W	9	
	50-75,000	-	-	-	3,150	9	841	2	698	2	368	1	221	19/No.	-	-	
	75-120,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
120-135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
>135,000	-	-	-	12	1/No.	330	1	2,188	6	5,959	15	4,300	12	0cc.	-		
Stewart Air Force Base, Newburgh, New York	<15,000	-	(10 - 30/Day)	-	-	-	-	-	55,574	152	37,780	104	20,440	56	E-W	44	
	15-35,000	-	-	-	916	2	89,803	246	1,502	10	2,287	6	3,885	17	NE-SW	22	
	35-50,000	-	-	-	1,103	3	2,213	6	2,836	8	6,329	17	6,205	17	NE-SW	22	
	50-75,000	-	-	-	827	19/No.	115	10/No.	215	17/No.	114	10/No.	72	6/No.	E-W	12	
	75-120,000	-	-	-	-	-	-	-	5	0cc.	-	-	2	0cc.	-	-	
120-135,000	-	-	-	5	0cc.	5	0cc.	1	0cc.	3	0cc.	2	0cc.	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Weaver Air Base, (Rapid City Air Force Base), Rapid City, South Dakota	<15,000	-	-	-	-	-	-	-	6,763	19	6,367	17	2,190	6	E-W	57	
	15-35,000	-	-	-	2,248	6	9,772	27	4,162	12	6,675	18	5,840	16	NE-SW	39	
	35-50,000	-	-	-	1,232	3	2,657	7	1,151	3	1,861	5	1,825	5	E-W	4	
	50-75,000	-	79	-	36,847	101	100	8/No.	212	17/No.	119	12/No.	221	19/No.	-	-	
	75-120,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-	
120-135,000	-	-	-	21	2/No.	47	4/No.	1,194	3	2,381	7	1,825	5	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	156	13/No.	-	-		
Wendover Air Force Base, Wendover, Utah	<15,000	-	-	No Data	-	-	-	-	1,182	3	2,190	6	730	2	NE-SW	60	
	15-35,000	-	-	-	1,638	4	4,245	12	1,330	4	1,095	3	376	1	NE-SW	21	
	35-50,000	-	-	-	1,278	4	58	1	615	2	349	1	136	13/No.	E-W	19	
	50-75,000	-	90	-	1,949	6	1,486	4	300	1	36	3/No.	36	3/No.	-	-	
	75-120,000	-	-	-	-	-	-	-	-	-	-	-	2	0cc.	-	-	
120-135,000	-	-	-	1,209	3	36	11/No.	1,614	4	752	2	156	13/No.	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	-	-	-	-		
Wright Field, Dayton, Ohio	<15,000	-	-	No Data	-	-	-	-	38,068	104	45,423	124	42,777	117	NE-SW	40	
	15-35,000	-	33	-	6,087	17	90,400	248	3,888	10	5,190	14	6,205	17	NE-SW	36	
	35-50,000	-	17	-	5,905	15	5,911	16	7,825	20	9,540	26	5,175	14	E-W	24	
	50-75,000	-	-	-	4,353	12	3,137	9	2,402	7	1,709	5	1,460	4	-	-	
	75-120,000	-	-	-	57	5/No.	214	18/No.	258	1	368	1	72	6/No.	-	-	
120-135,000	-	-	-	1,477	4	1,800	5	1,351	4	1,403	4	1,095	3	-	-		
>135,000	-	-	-	-	-	-	-	-	-	-	-	24	2/No.	-	-		

TRAFFIC HISTORY

Notes - Traffic Histories for 1943 and 1944 obtained from Payment Evaluation Reports.
 Traffic Histories for 1945-1949 inc. summarized from data made available by Air Force Headquarters.
 Traffic shown as 15-35,000 lb. gross load for years 1945 and 1946 also includes planes with gross weight below 15,000 lbs.
 Traffic distribution based on data from 1945-1949 inclusive.



B

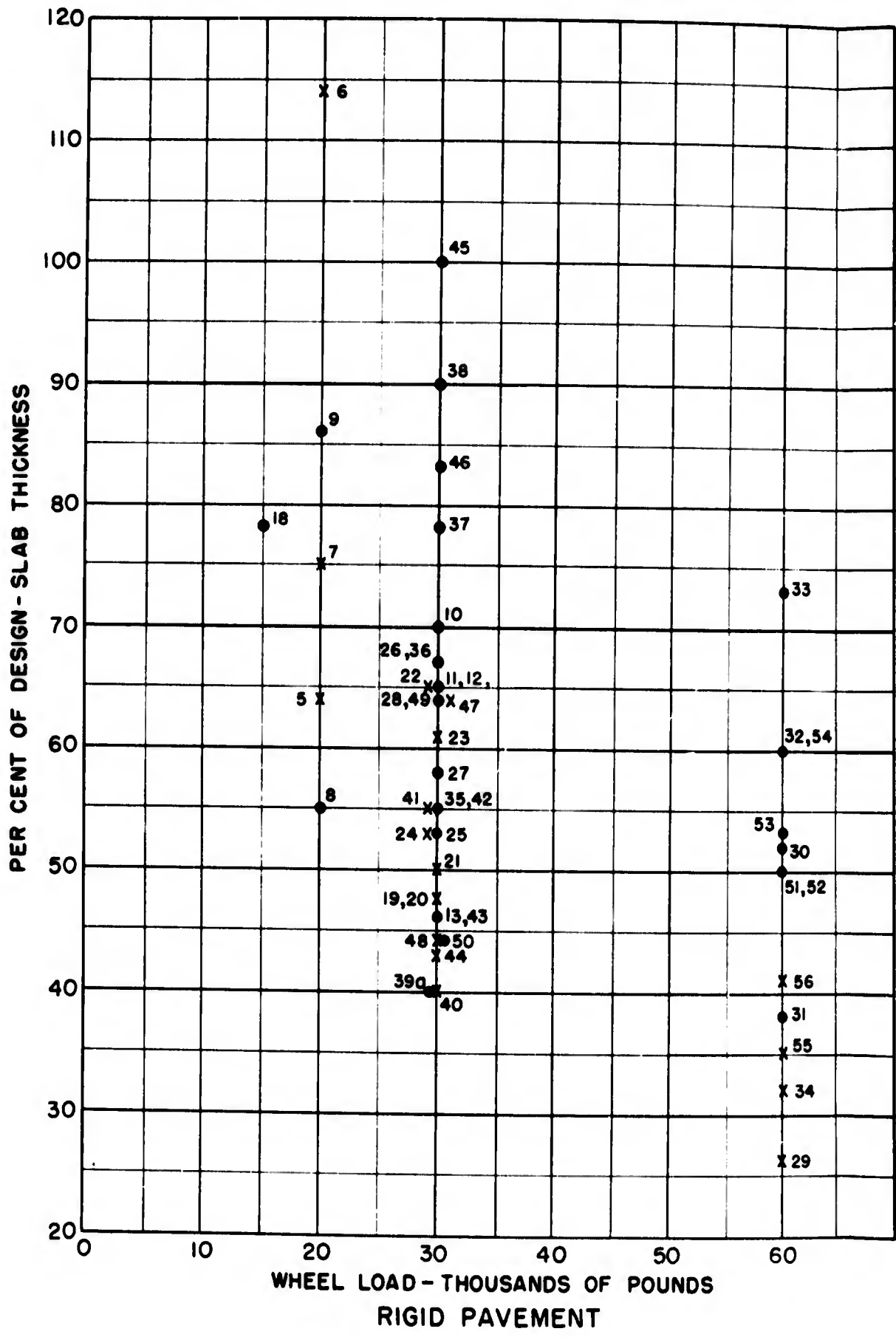


FIG.1

A

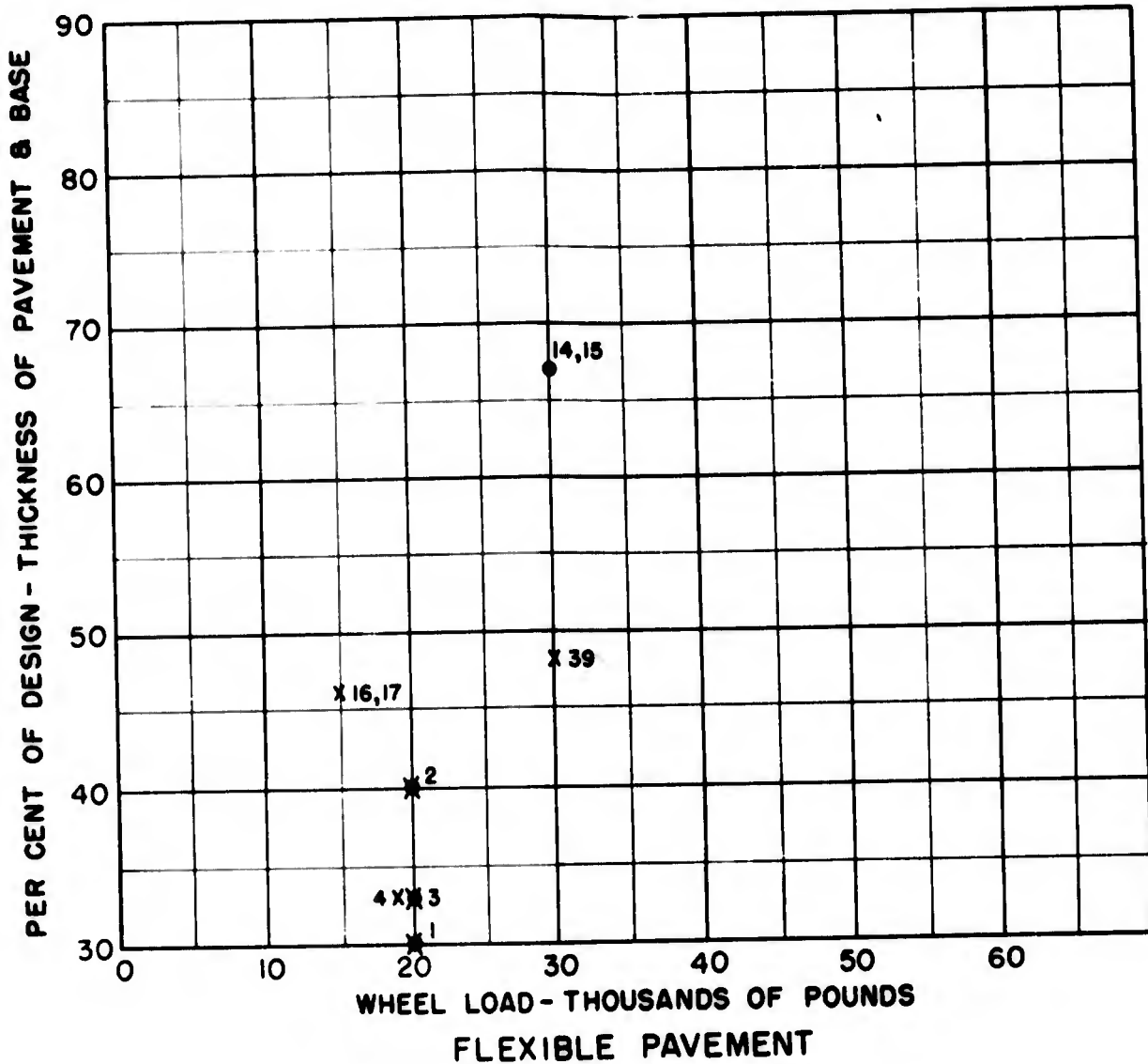


FIG.2

NOTE:

Numbers adjacent to plotted points on Figure 1 and Figure 2 refer to line numbers on Summary Tabulation Table 1, Sheets 1 to 4.

Wheel loads plotted are of heaviest class of planes using field with frequency of 5 or more cycles of landings and take offs per day for the year with maximum traffic prior to failure study or condition survey.

Wheel load considered to be one half of gross plane load.

The wheel loads plotted represent planes in the following gross weight ranges:

15,000 lb. wheel load-	15,000 to 35,000 gross plane wt.
20,000 " " "	35,000 to 50,000 " " "
30,000 " " "	50,000 to 75,000 " " "
60,000 " " "	120,000 to 135,000 " " "

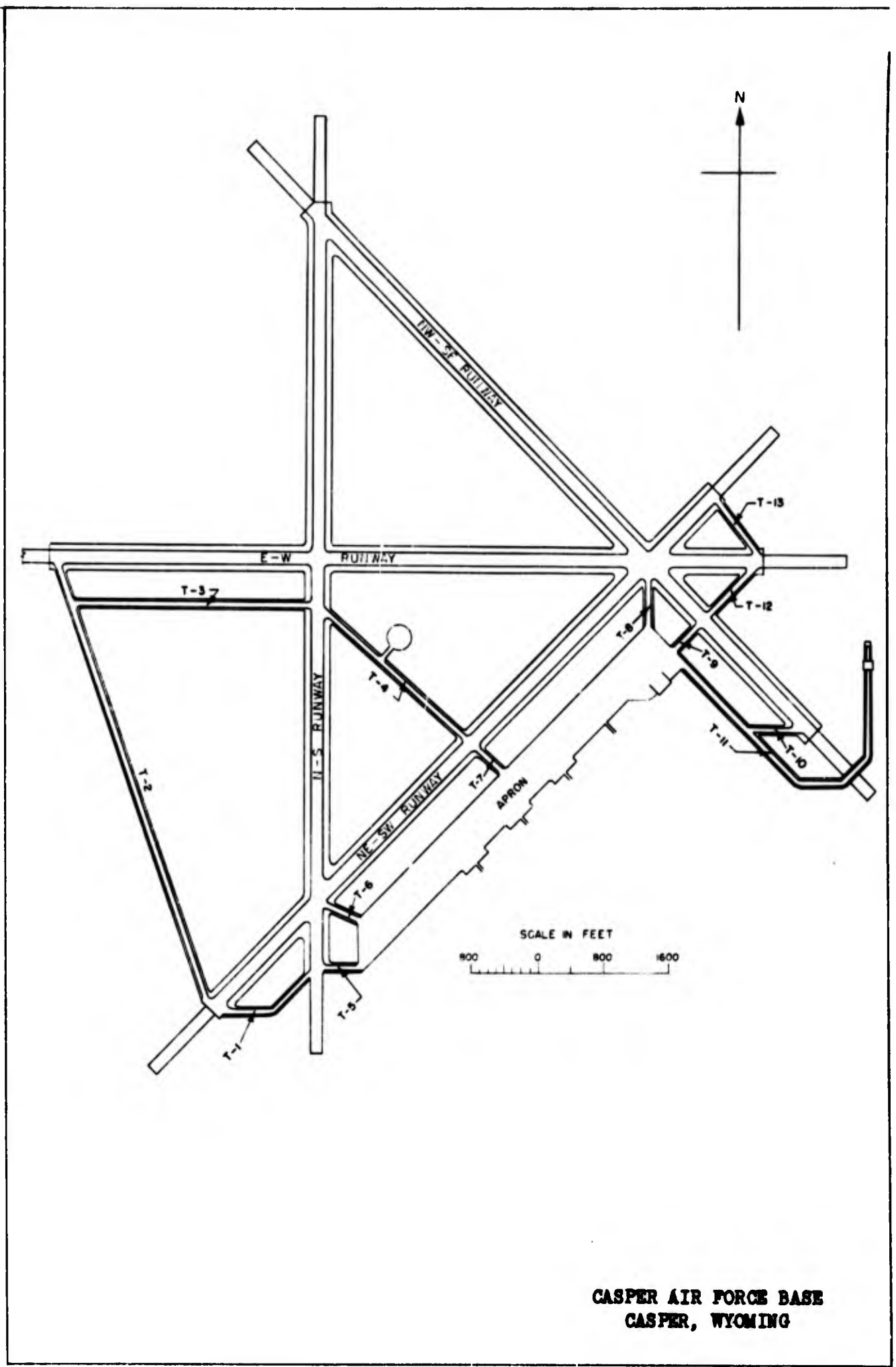
LEGEND

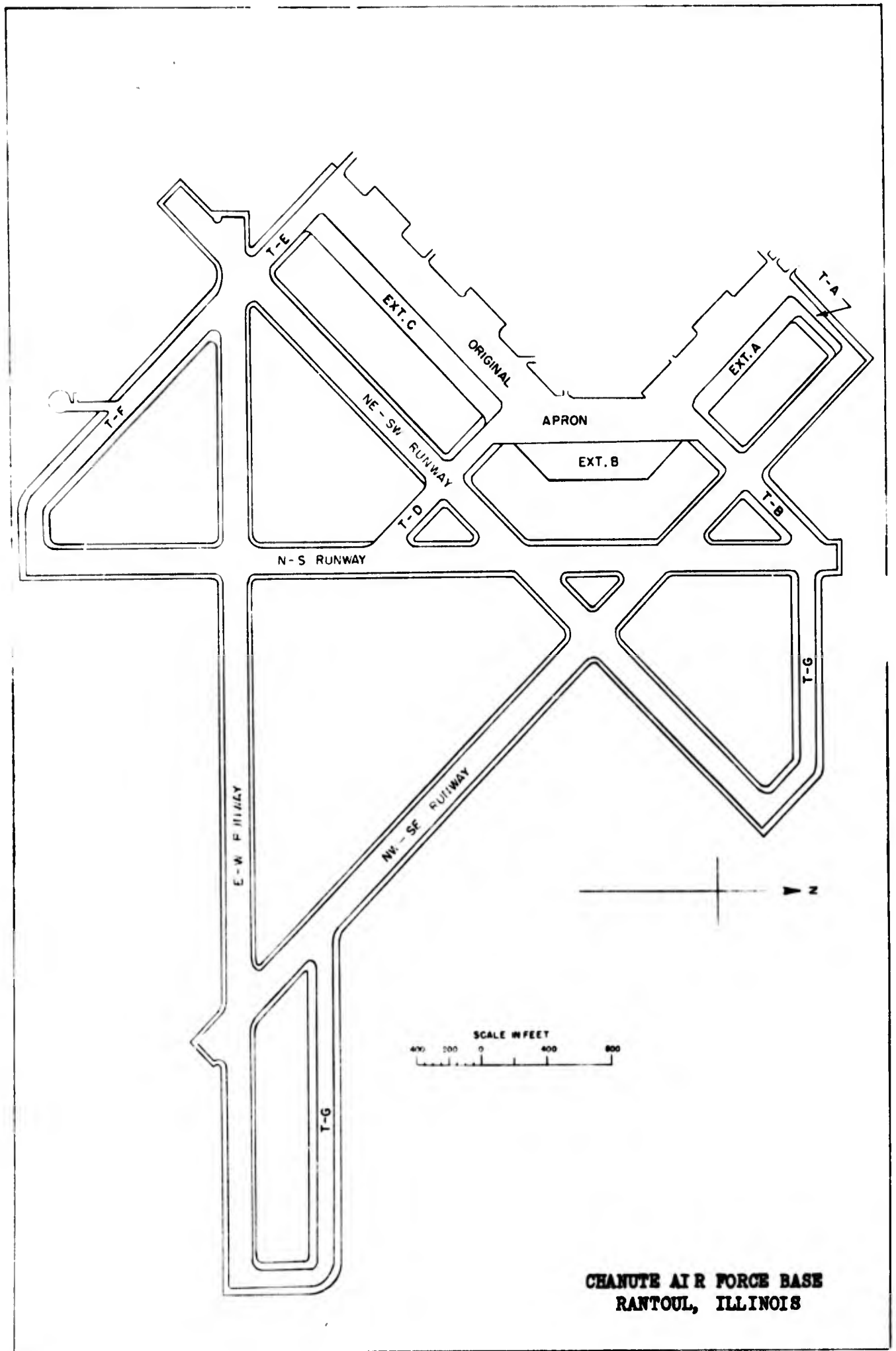
- X Failed
- Satisfactory

FROST INVESTIGATION
1949-1950
PAVEMENT BEHAVIOR
VS
PER CENT OF DESIGN
THICKNESS

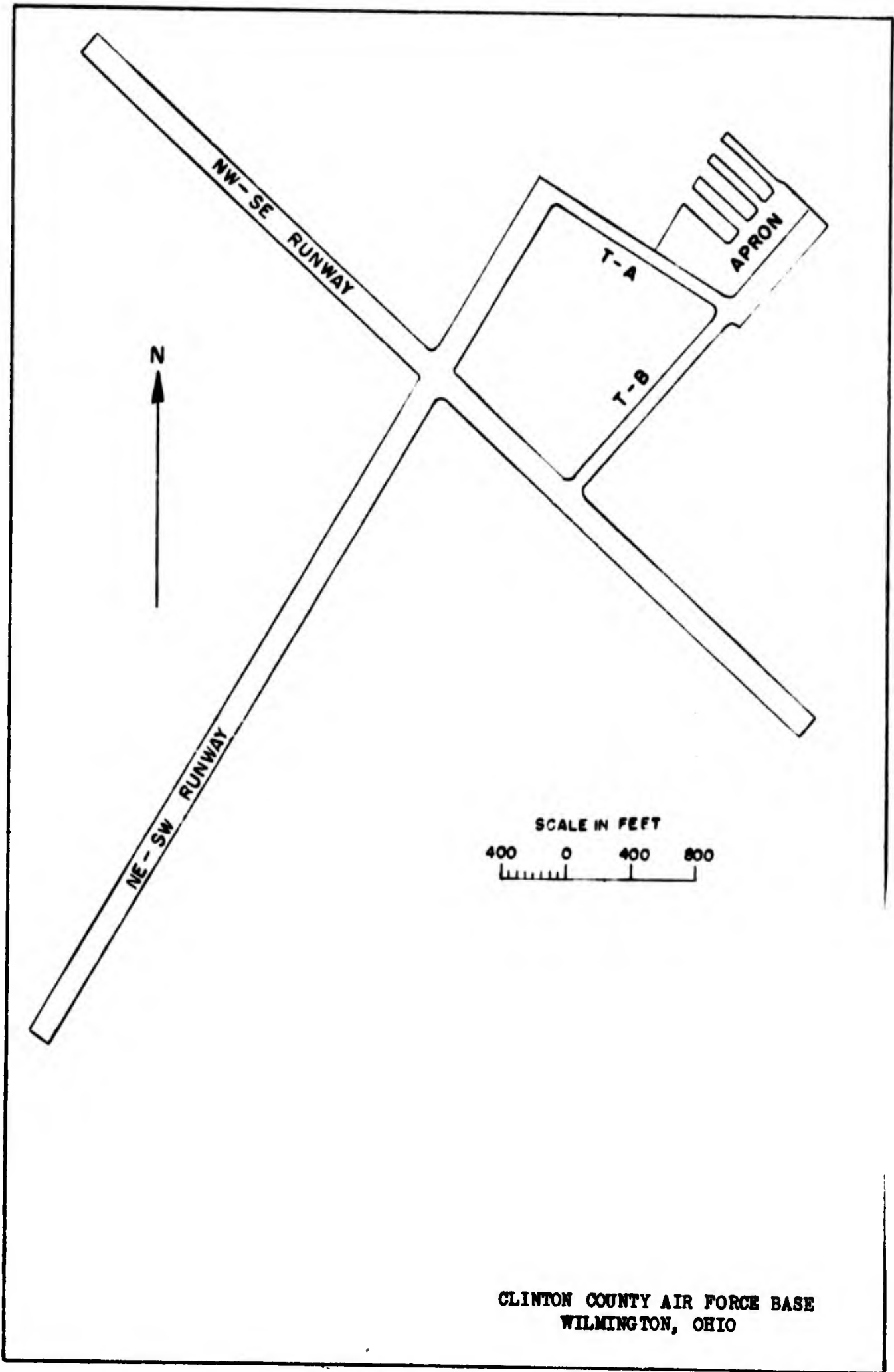
FROST EFFECTS LABORATORY
NEW ENGLAND DIVISION CORPS OF ENGR.
BOSTON, MASS.
JUNE 1950

B

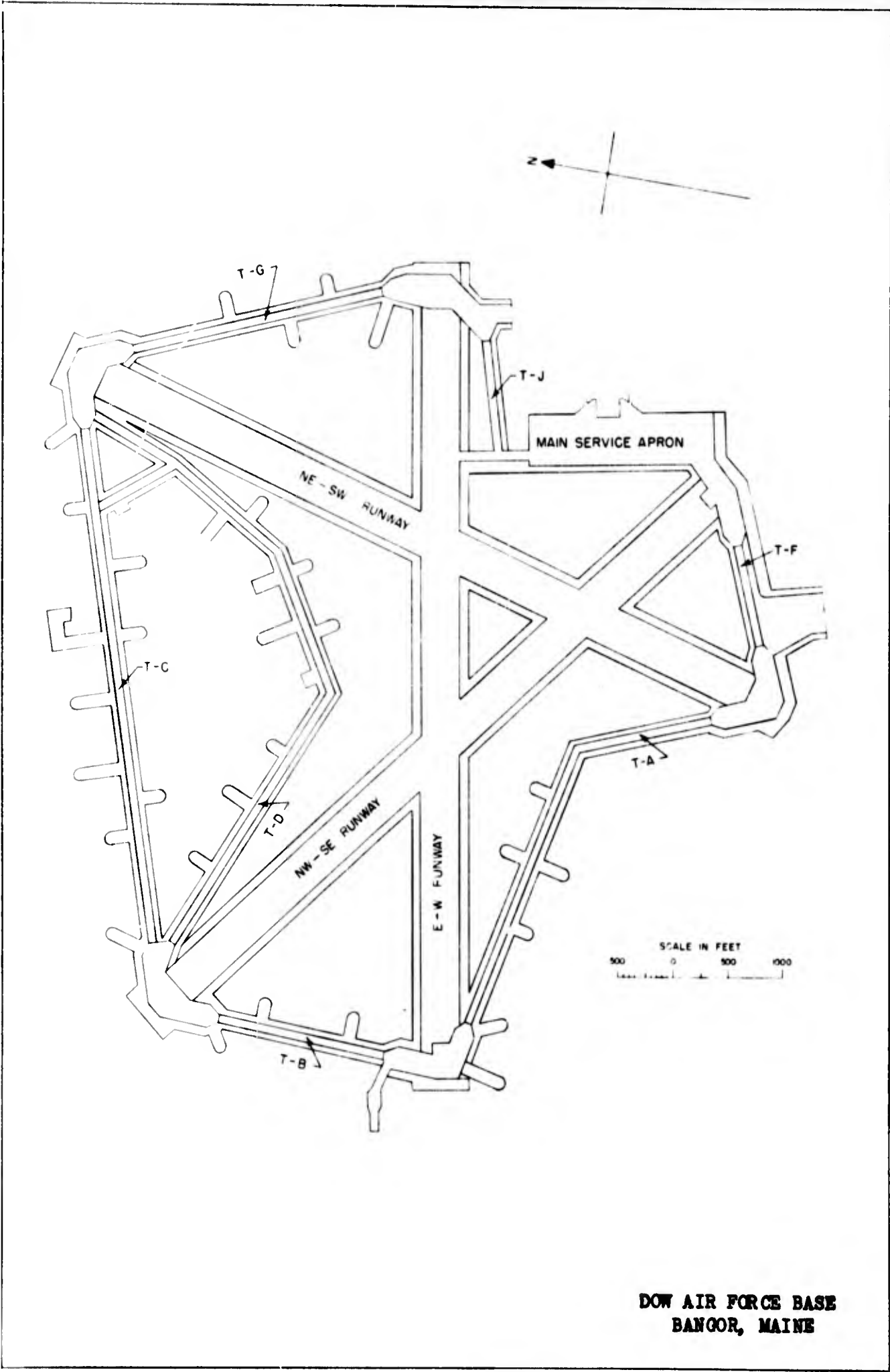




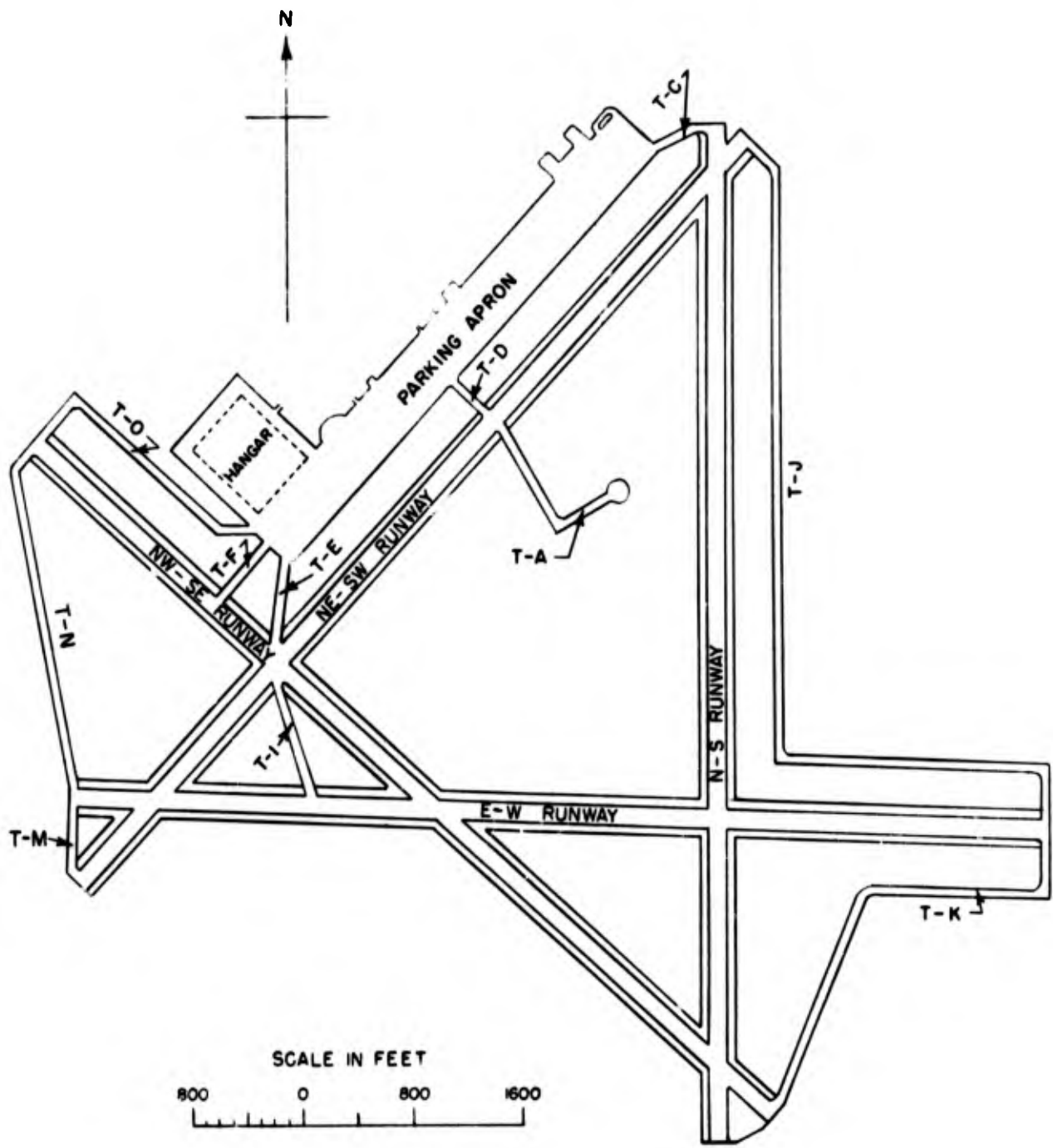
**CHANUTE AIR FORCE BASE
 RANTOUL, ILLINOIS**



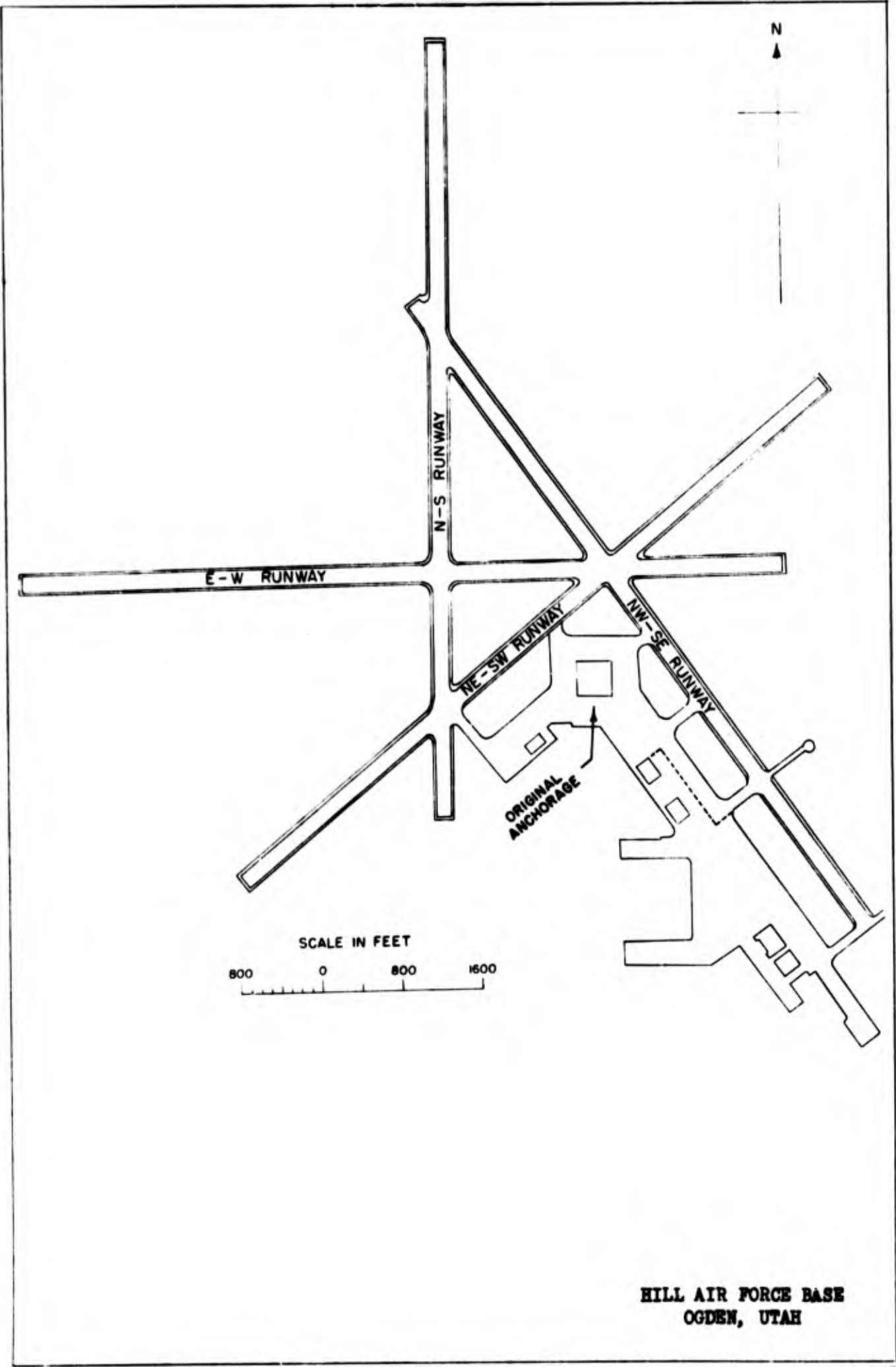
CLINTON COUNTY AIR FORCE BASE
WILMINGTON, OHIO



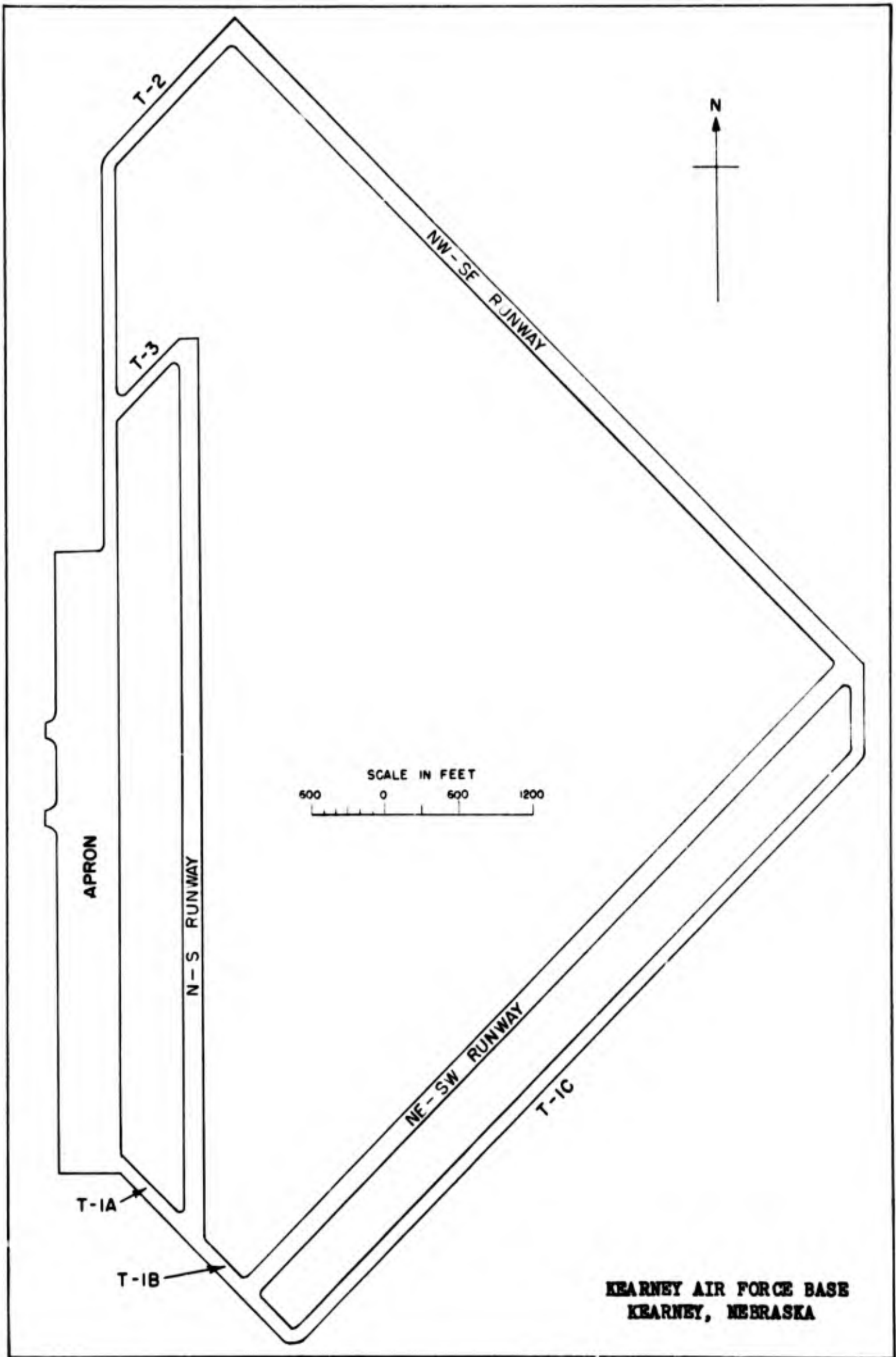
**DOW AIR FORCE BASE
BANGOR, MAINE**



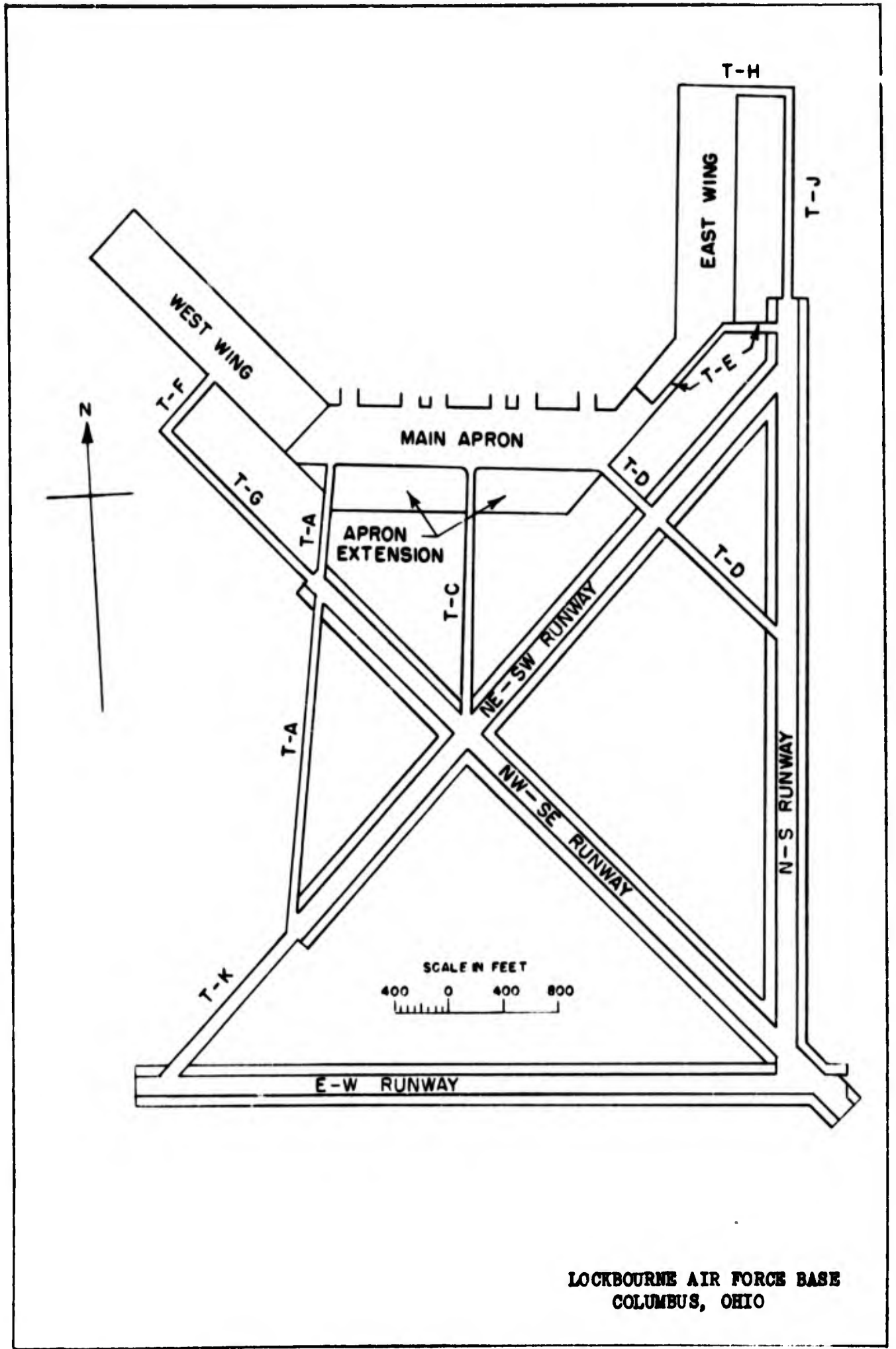
GREAT FALLS AIR FORCE BASE
GREAT FALLS, MONTANA



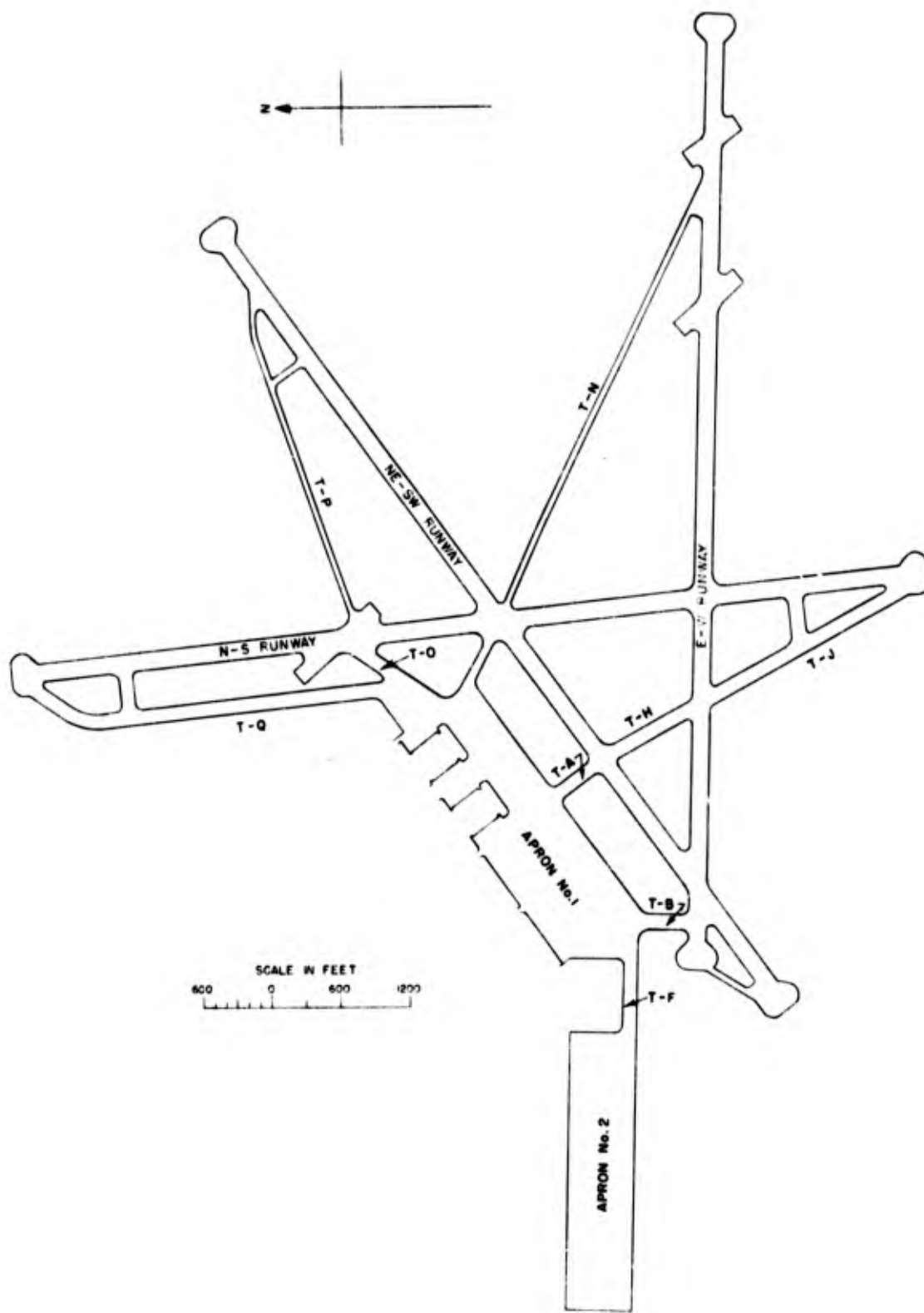
HILL AIR FORCE BASE
OGDEN, UTAH



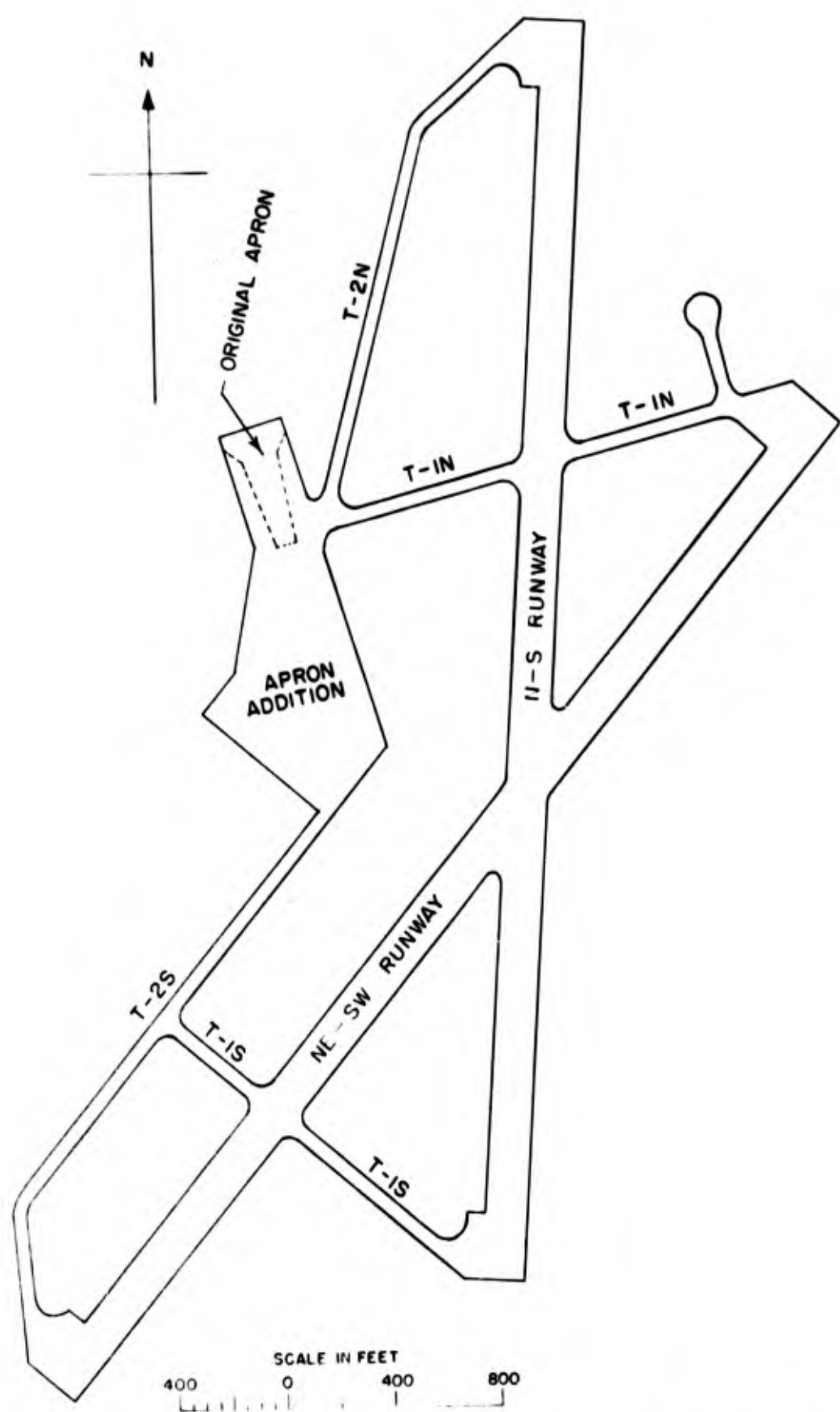
**KEARNEY AIR FORCE BASE
KEARNEY, NEBRASKA**



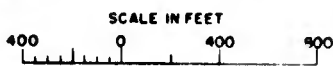
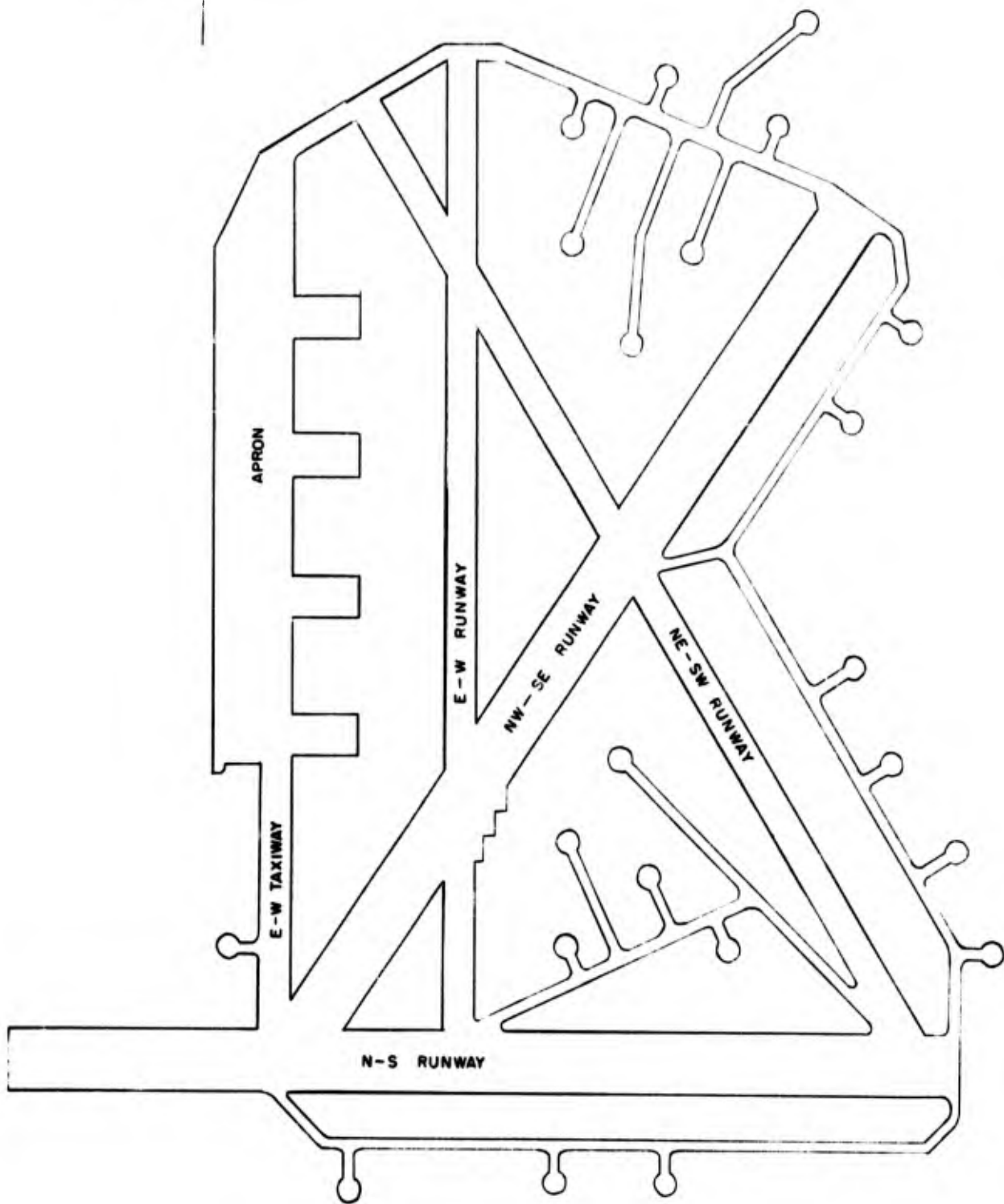
LOCKBOURNE AIR FORCE BASE
COLUMBUS, OHIO



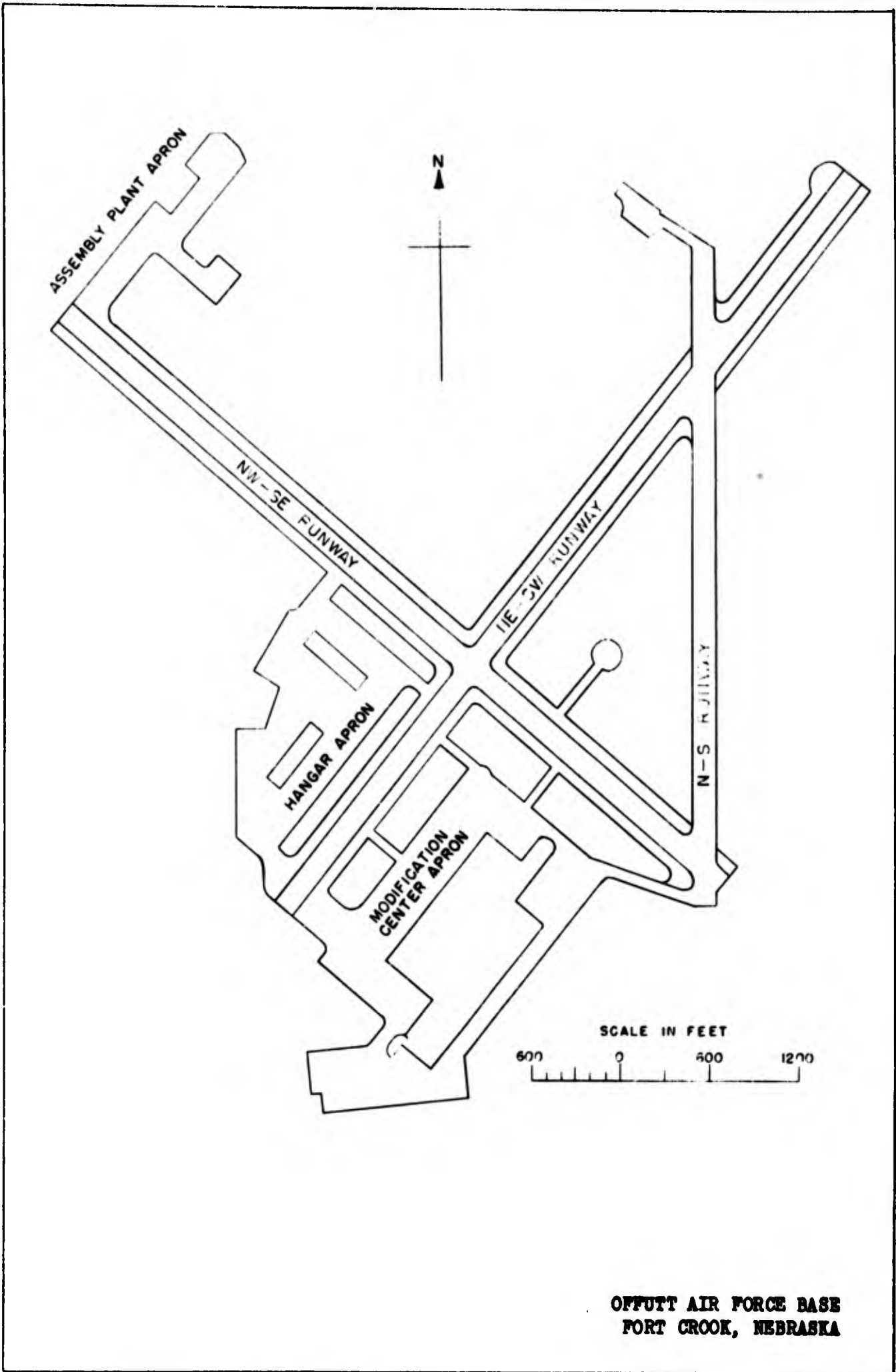
LOWRY AIR FORCE BASE
DENVER, COLORADO

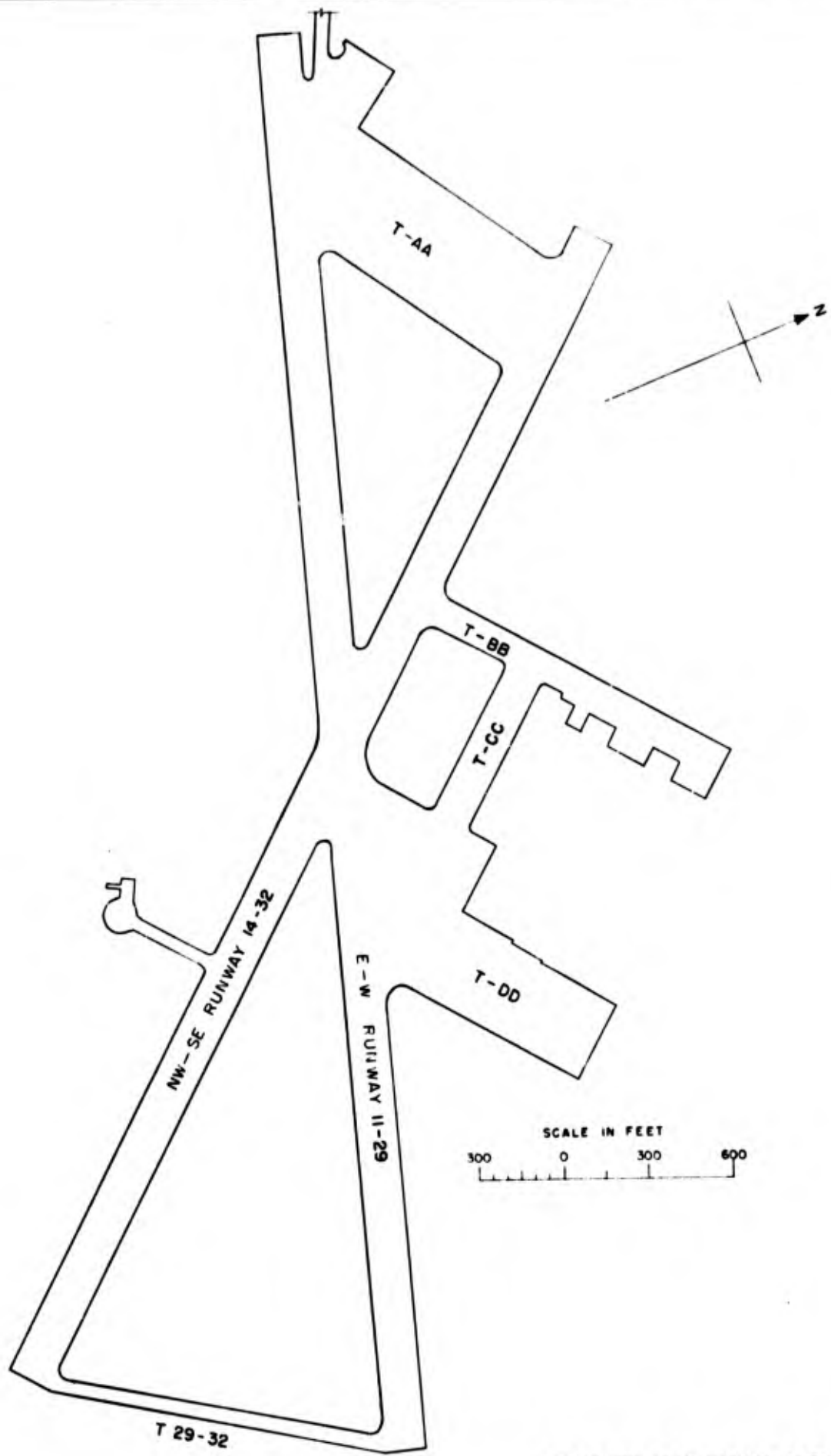


MARSHALL AIR FORCE BASE
FORT RILEY, KANSAS

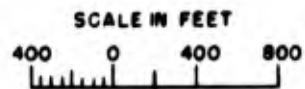
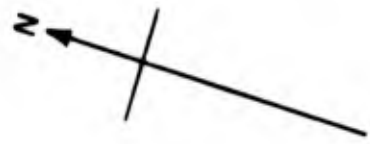
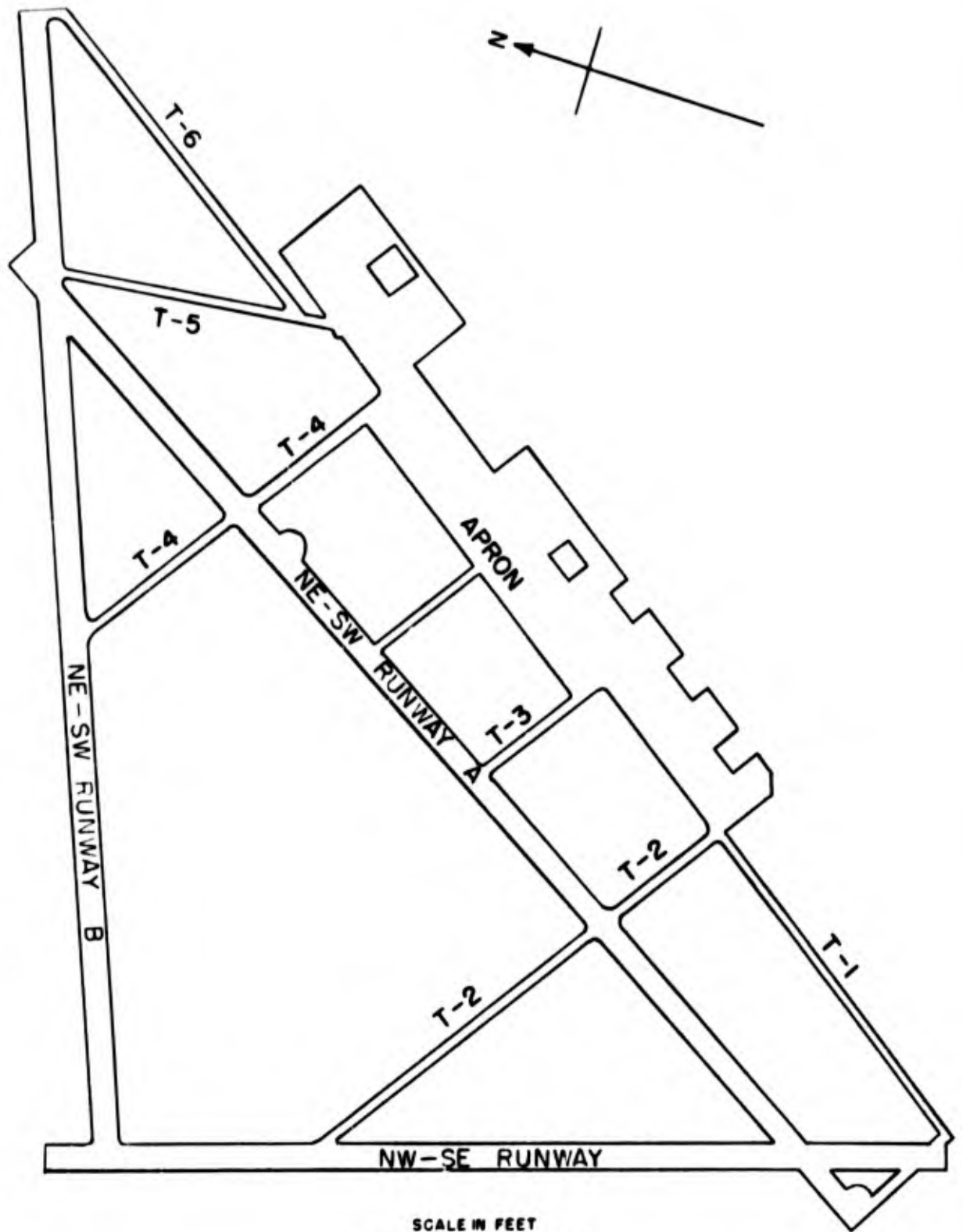


MITCHEL AIR FORCE BASE
HEMPSTEAD, LONG ISLAND, NEW YORK

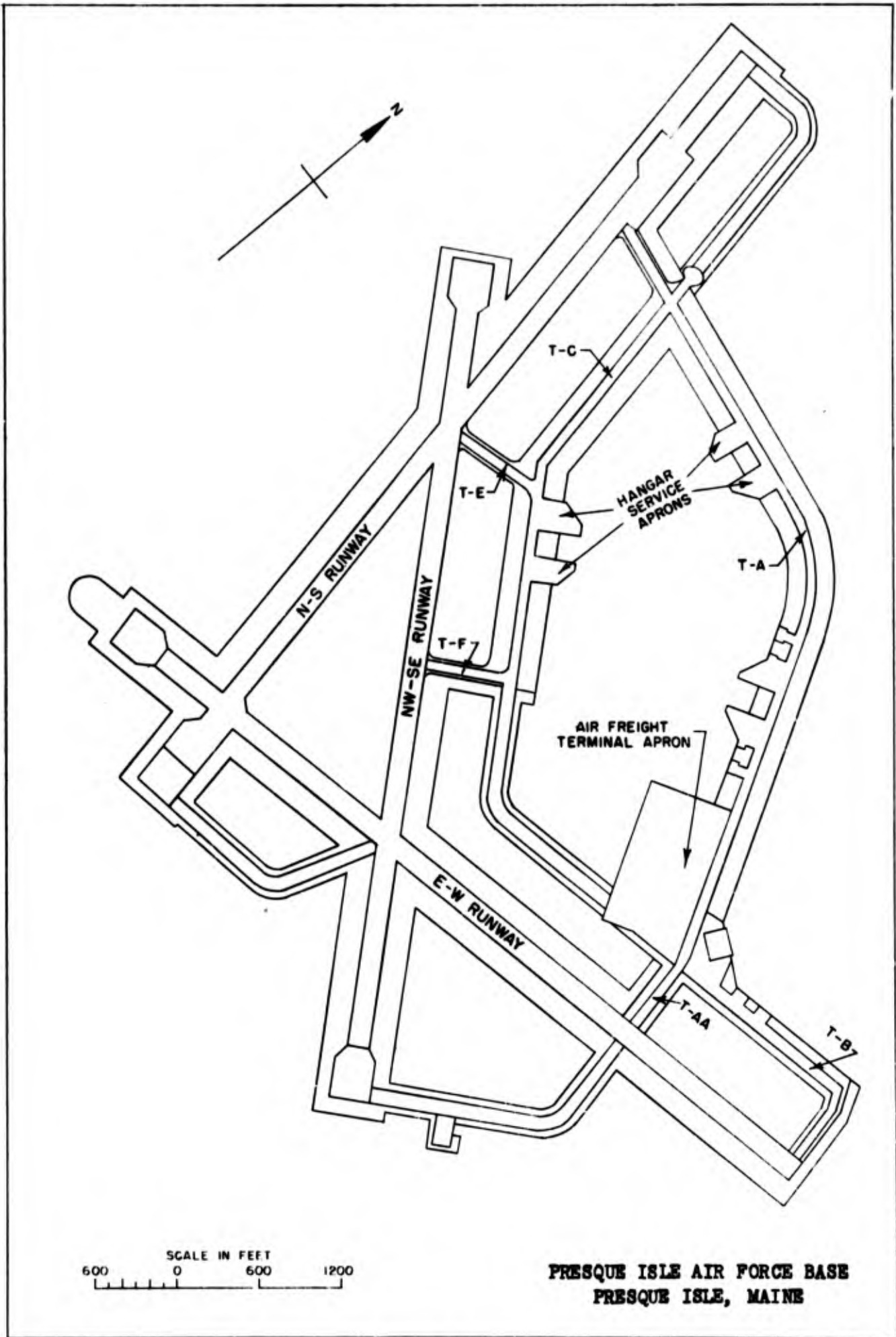




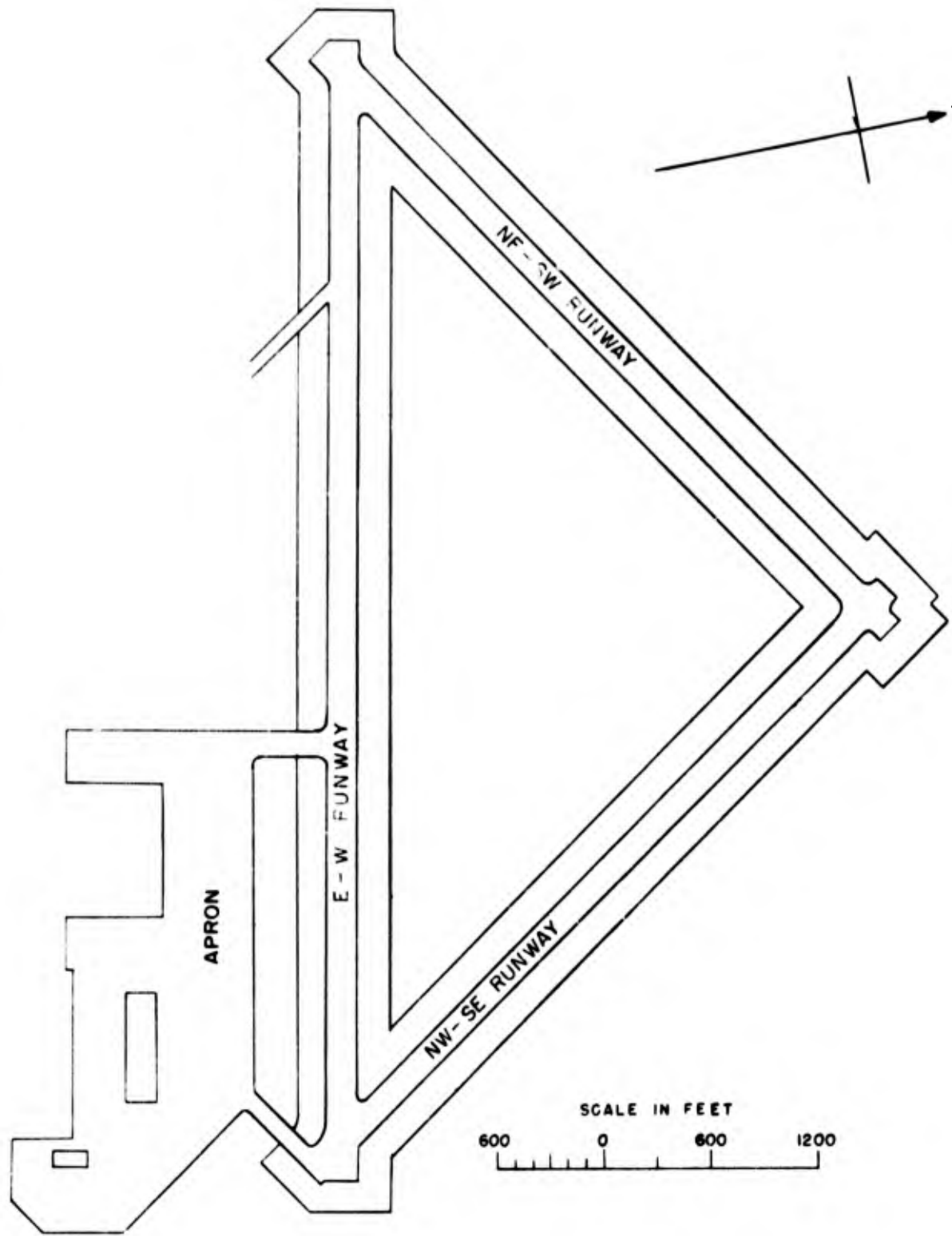
**OLMSTED AIR FORCE BASE
MIDDLETOWN, PENNSYLVANIA**



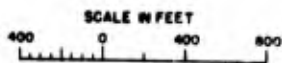
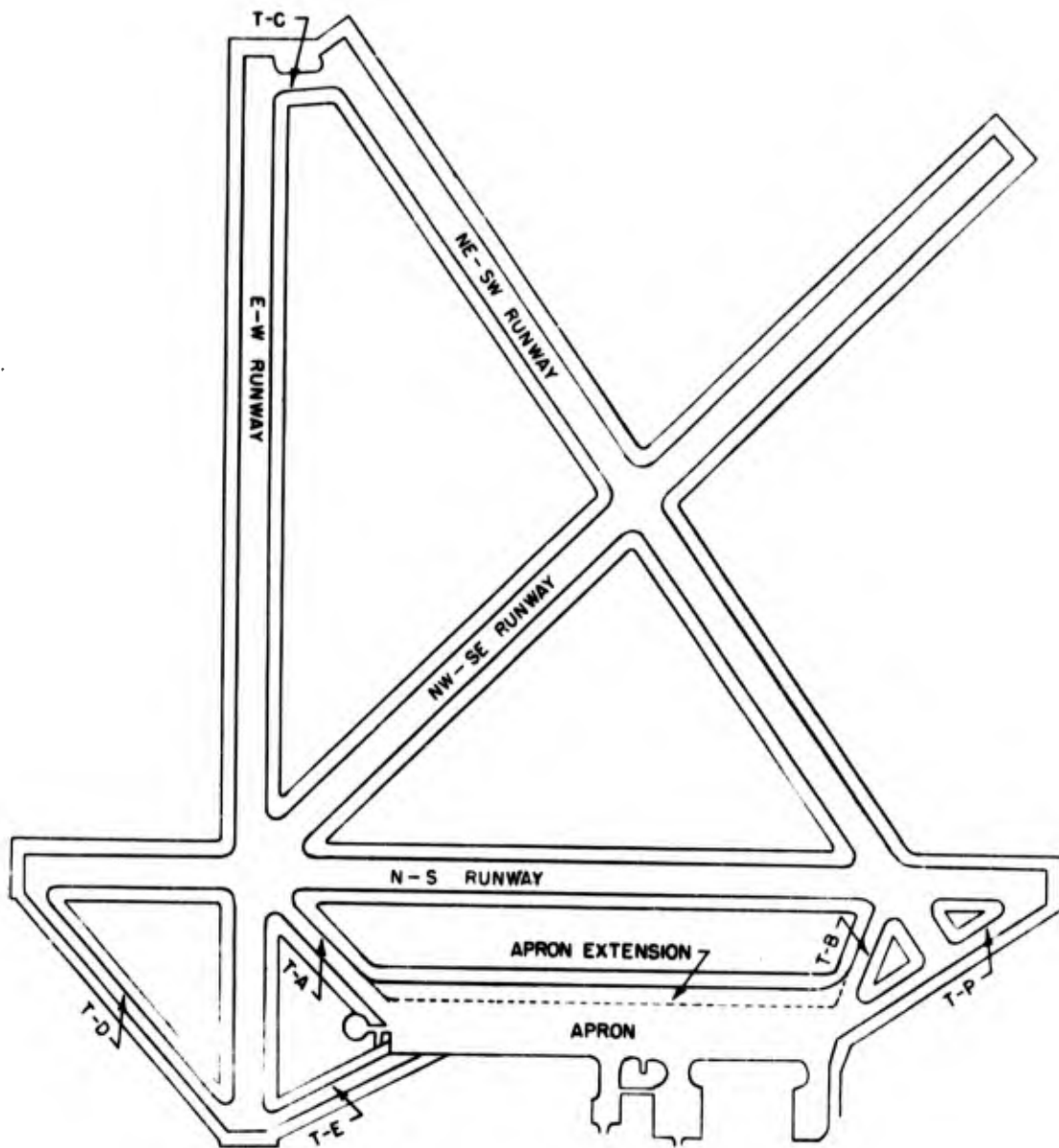
PATTERSON FIELD
FAIRFIELD, OHIO



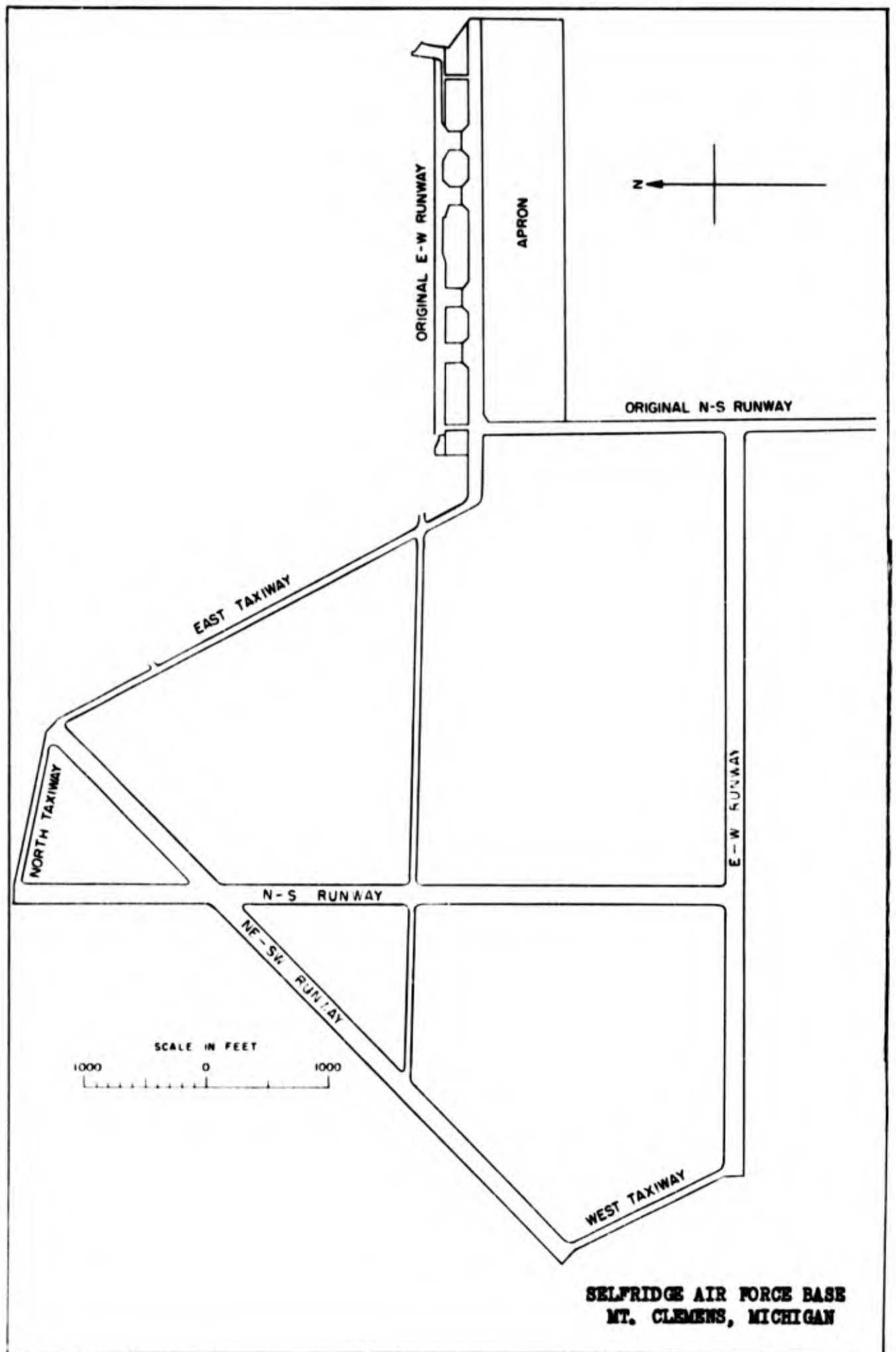
PRESQUE ISLE AIR FORCE BASE
PRESQUE ISLE, MAINE



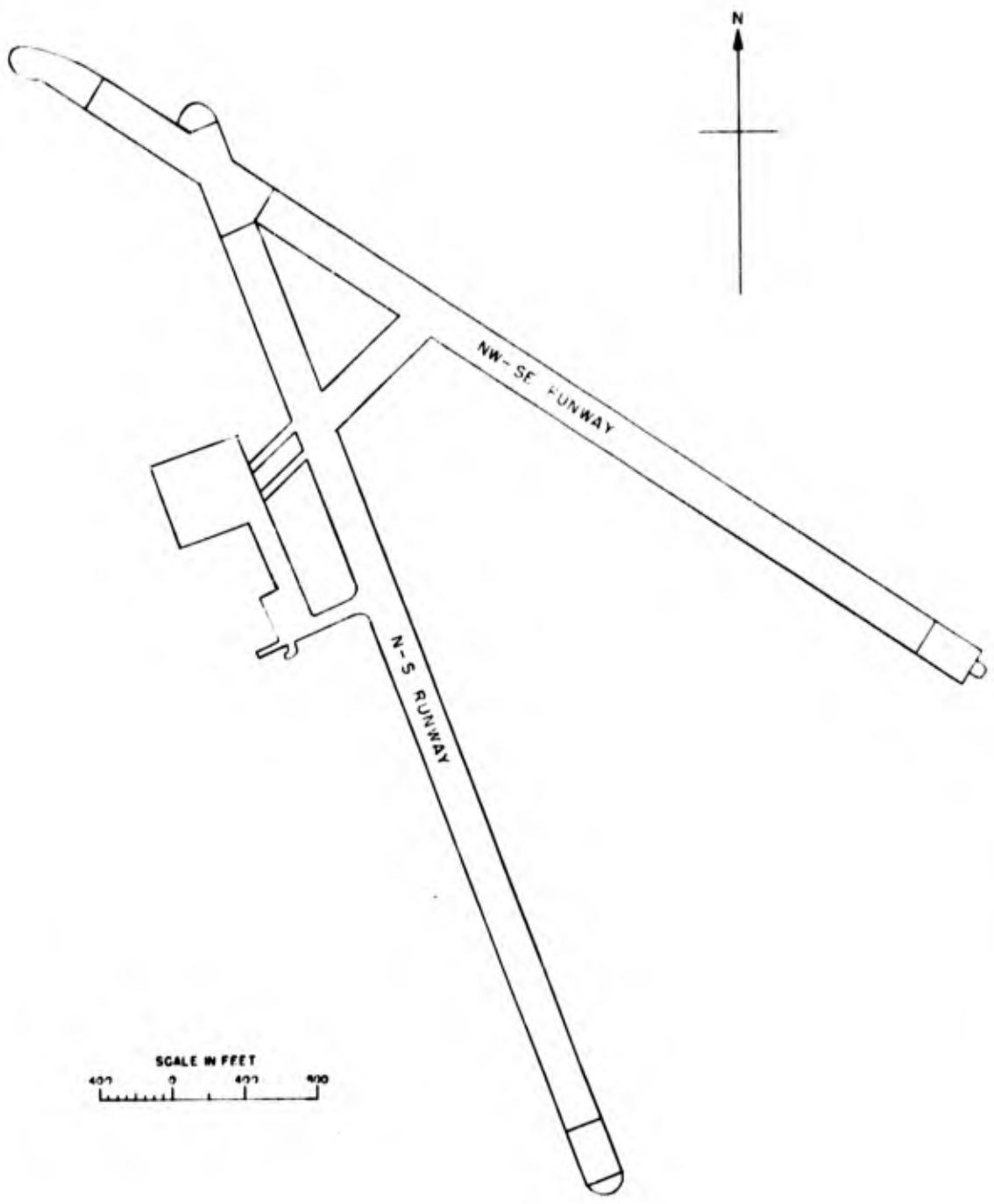
ROME AIRFIELD
(GRIFFISS AIR FORCE BASE)
ROME, NEW YORK



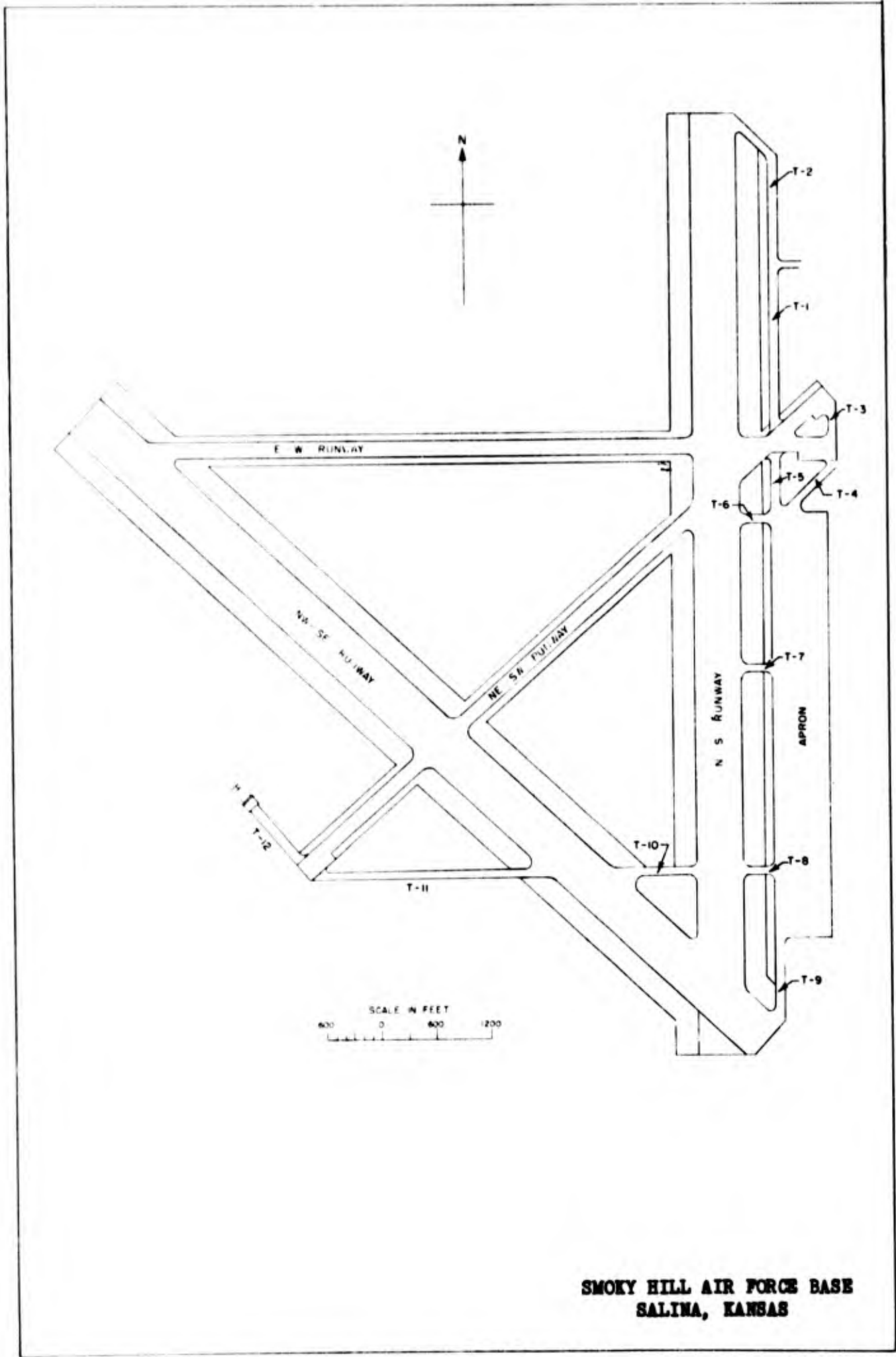
SCOTT AIR FORCE BASE
BELLEVILLE, NEW YORK



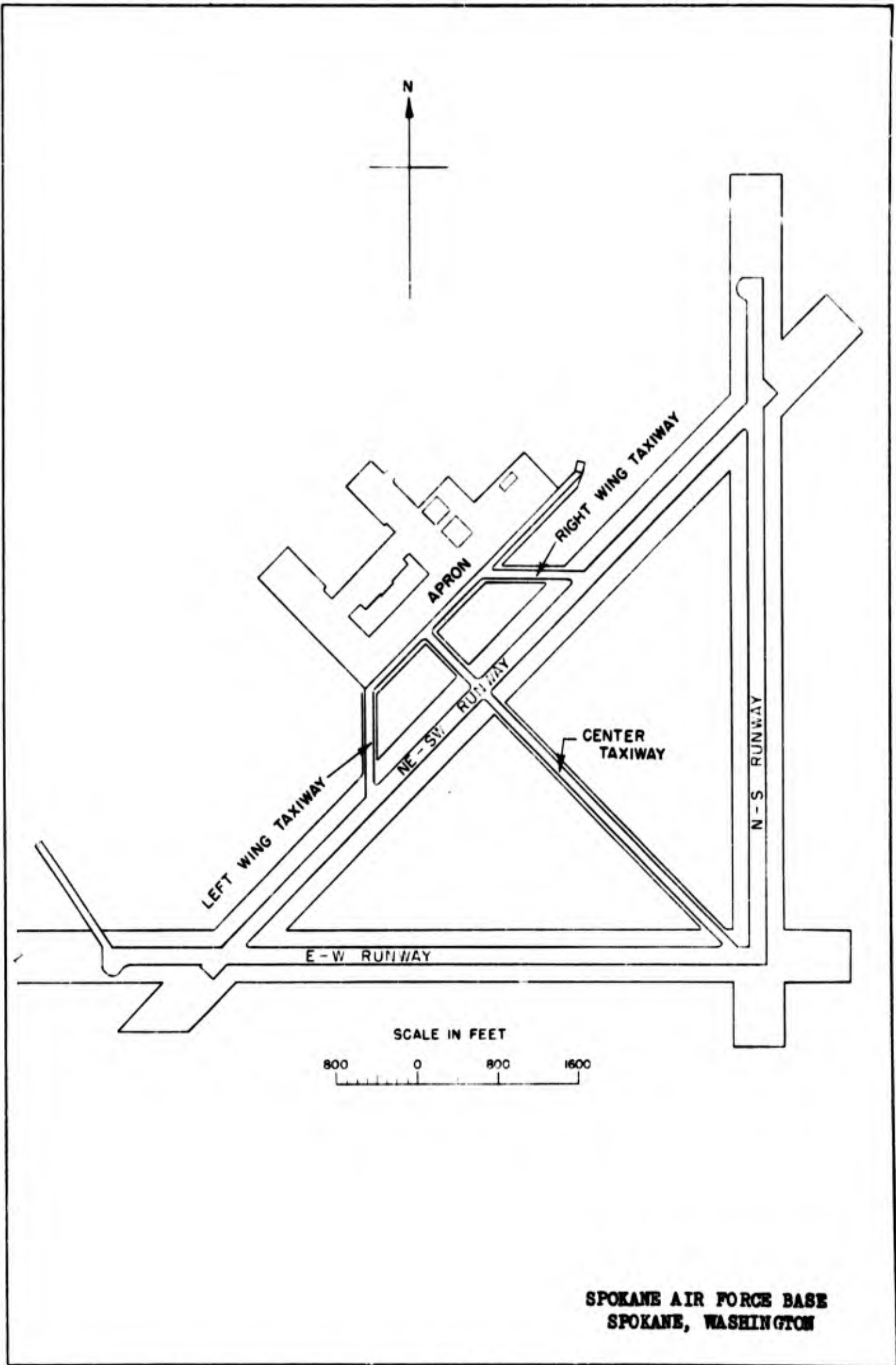
**SELFRIDGE AIR FORCE BASE
MT. CLEMENS, MICHIGAN**



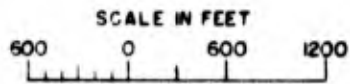
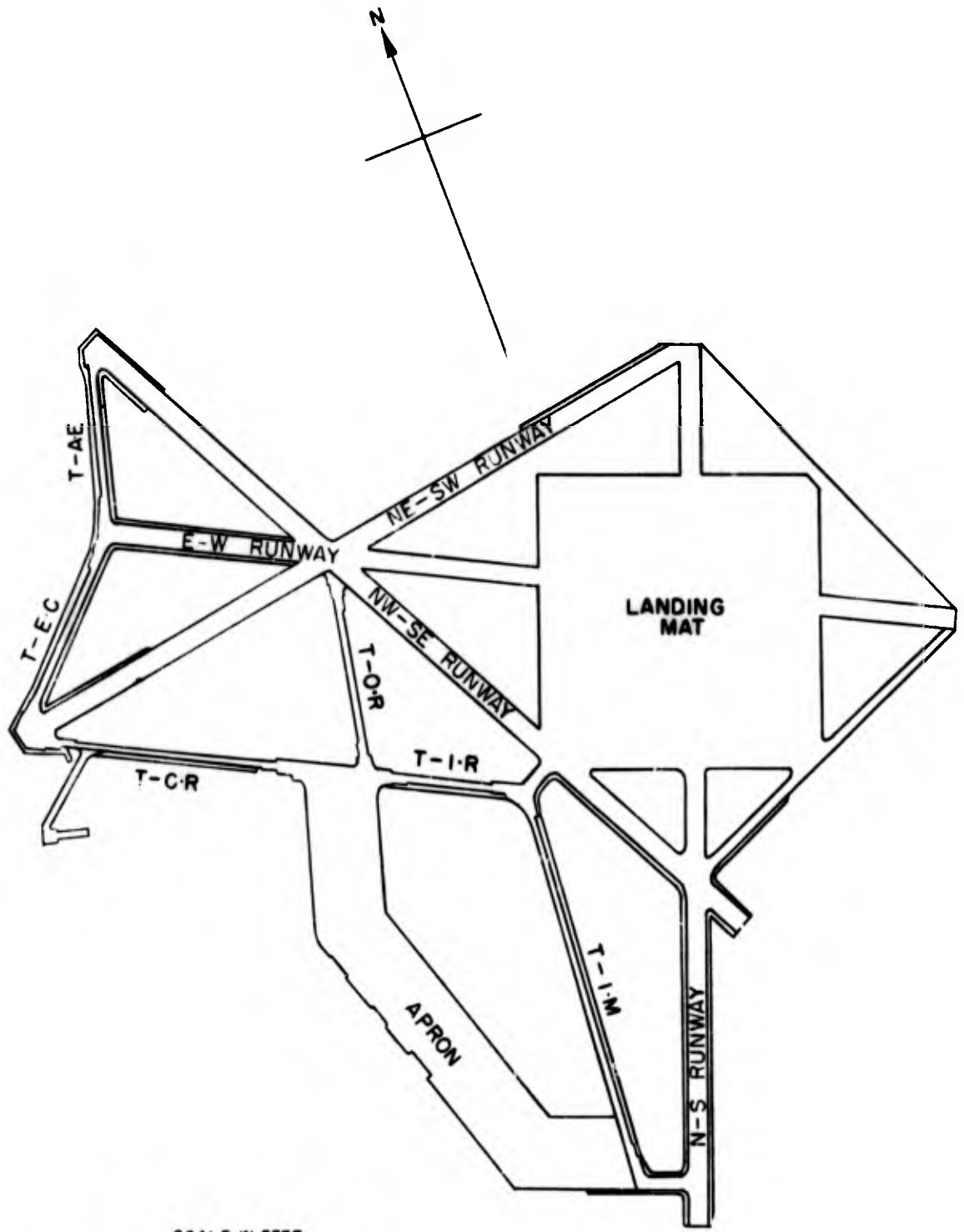
**SHERMAN AIR FORCE BASE
FORT LEAVENWORTH, KANSAS**



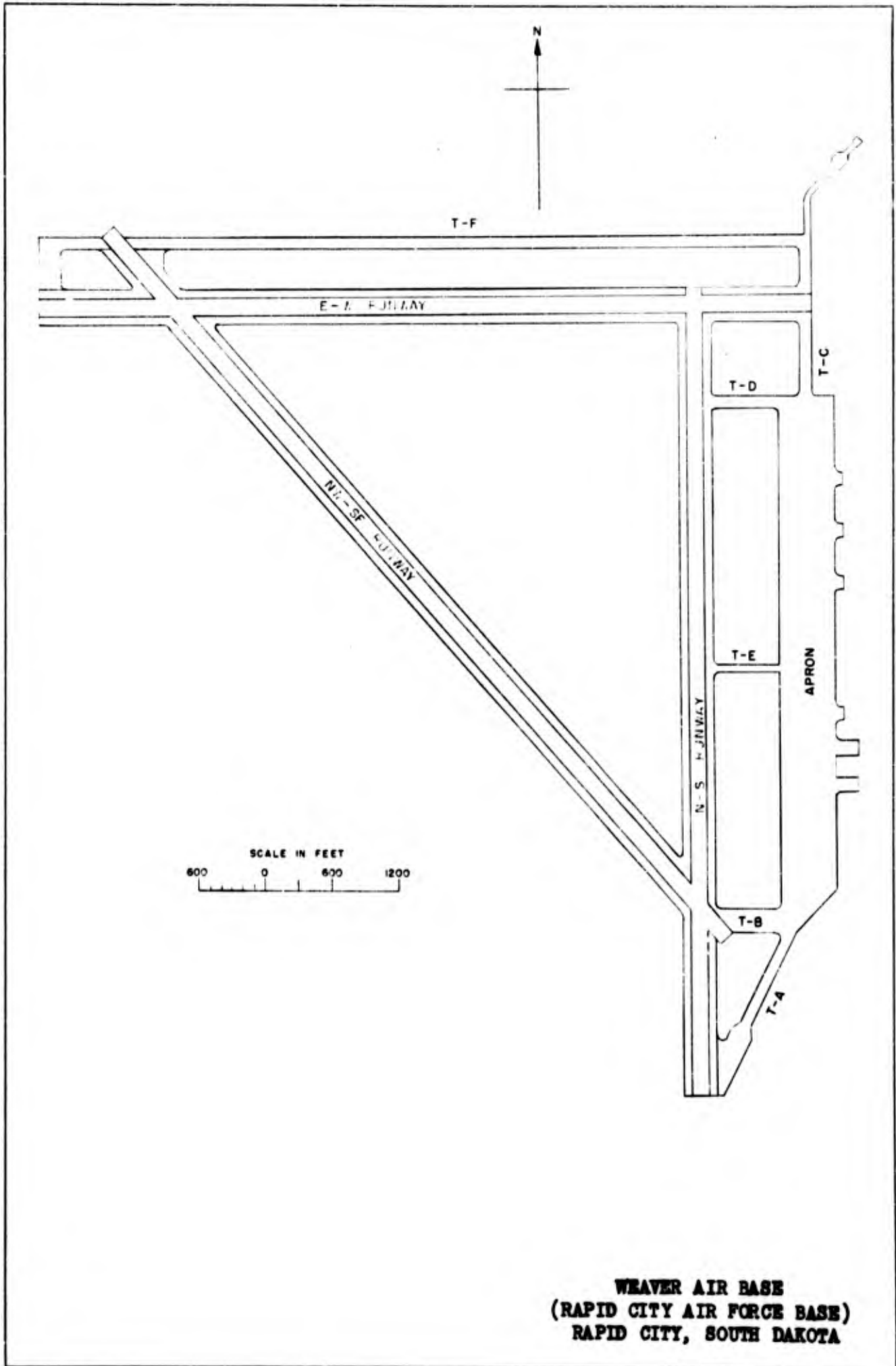
**SMOKY HILL AIR FORCE BASE
 SALINA, KANSAS**



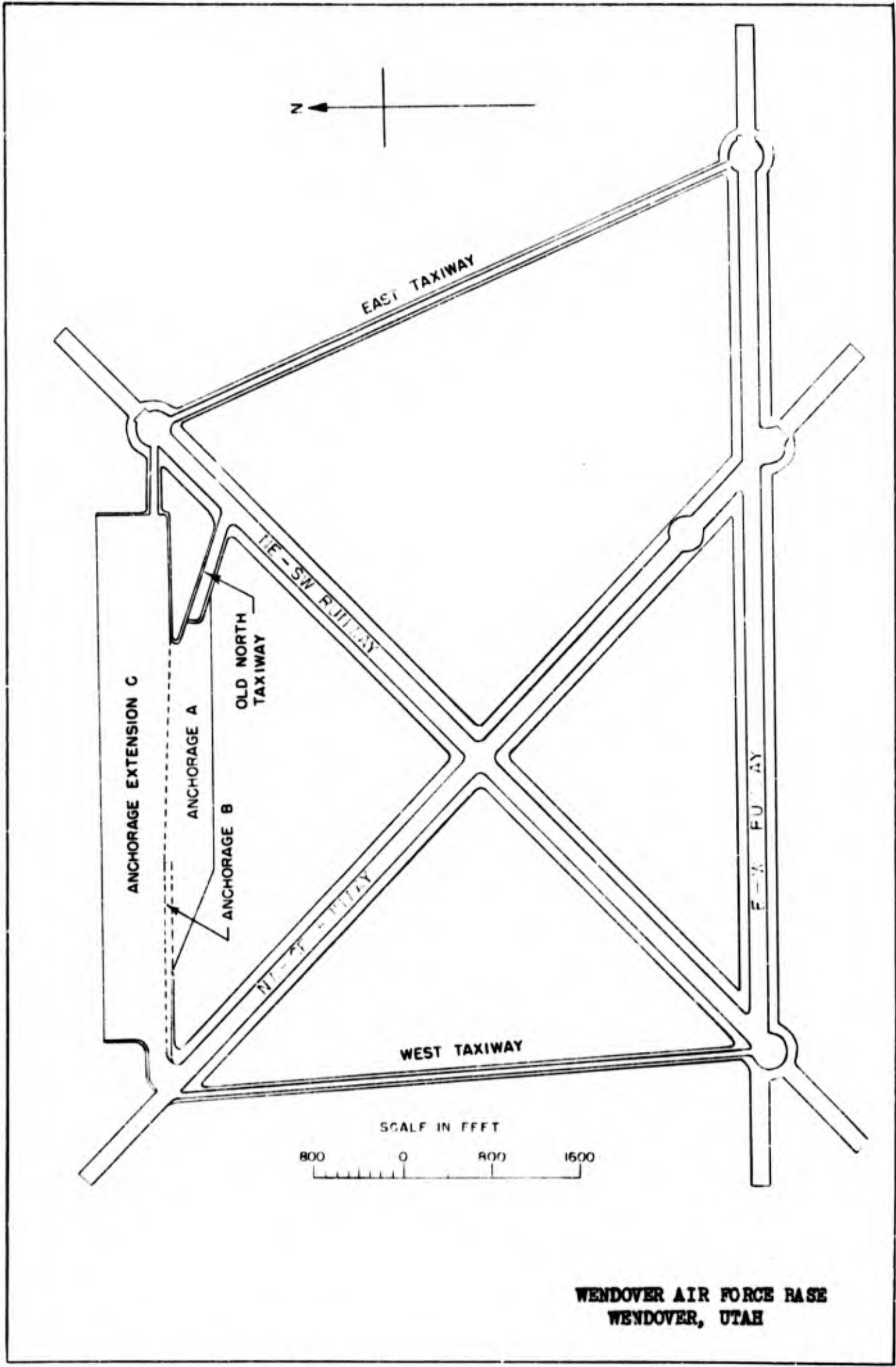
SPOKANE AIR FORCE BASE
SPOKANE, WASHINGTON



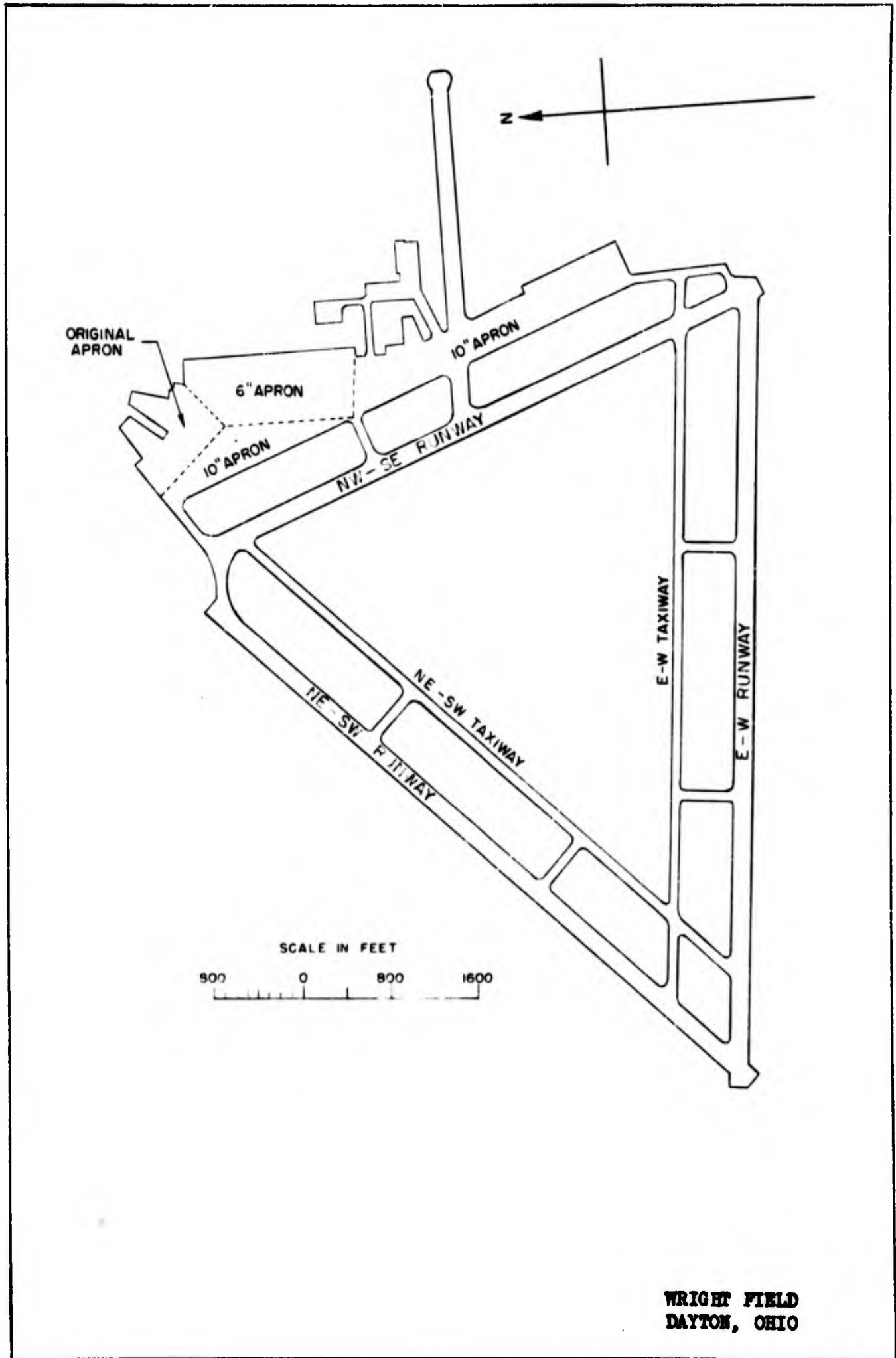
STEWART AIR FORCE BASE
NEWBURGH, NEW YORK



**WEAVER AIR BASE
 (RAPID CITY AIR FORCE BASE)
 RAPID CITY, SOUTH DAKOTA**



WENDOVER AIR FORCE BASE
WENDOVER, UTAH



WRIGHT FIELD
DAYTON, OHIO