



DEPARTMENT OF THE NAVY

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3 April 2018

VIA SAME DAY E-MAIL to

Paul Moser

[REDACTED]
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SUBJECT: FOIA CASE DON-NAVY-2017-008080

Dear Mr. Moser,

This is in response to your Freedom of Information Act (FOIA), submitted 30 June 2017, in which you requested Naval Air Development Center Report No. NADC-AE-6718 of 18 Aug. 1967, "Flight Evaluation and Analysis of An/AAS-10(XE-1), Reconofax VI and Reconofax IX Infrared Mapping Sets (U)."

We have located the responsive documents and you are granted full access to these records. A copy is enclosed.

If you have any questions regarding your request, you can contact Barbara Nimmerrichter by telephone at (301) 995-3089 or by email at kori.l.wilson@navy.mil.

Sincerely,

//s// Kori Wilson

Kori Wilson
Attorney



COPY

NAVAL AIR DEVELOPMENT CENTER

Johnsville, Warminster, Pennsylvania

AD 384685

Report No. NADC-AE-6718

18 Aug 1967

FLIGHT EVALUATION AND ANALYSIS OF
AN/AAS-10(XE-1), RECONOFAX VI
AND RECONOFAX IX
INFRARED MAPPING SETS (U)

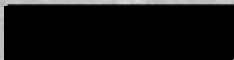
FINAL REPORT
AIRTASK NO. A36533804/2021/F001-05-05
Work Unit No. 1

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this document and must be met, each transmittal
outside the Department of Defense must have prior
approval of Commanding Officer, Naval Air
Development Center.~~



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DEPARTMENT OF THE NAVY
U. S. NAVAL AIR DEVELOPMENT CENTER
JOHNSVILLE
WARMINSTER, PA. 18974

Aero-Electronic Technology Department

REPORT NO. NADC-AE-6718

18 August 1967

FLIGHT EVALUATION AND ANALYSIS OF
AN/AAS-10(XE-1), RECONOFAX VI, AND RECONOFAX IX
INFRARED MAPPING SETS (U)

FINAL REPORT
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Three experimental infrared mapping systems, the U. S. Air Force Reconofax IX, U. S. Army AN/AAS-10(XE-1), and the U. S. Navy Reconofax VI, were flight-tested simultaneously on RA-3B aircraft, BuNo. 144839. Control ground targets and targets of opportunity were used. The three systems met their respective primary design specifications, but each system has shortcomings that need to be improved before service use. Recommendations are included for further development of infrared mapping systems. (U)

Reported by:

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Technical Director

~~In addition to security requirements which apply to this document and must be met, each transmittal outside the Department of Defense must have prior approval of Commanding Officer, Naval Air Development Center.~~

S U M M A R Y

INTRODUCTION

AIRTASK No. A36533804/2021/F001-05-05, Work Unit No. 1 directed the Naval Air Development Center (NAVAIRDEVCCEN) to install and simultaneously flight test the U. S. Army AN/AAS-10(XE-1) and the U. S. Air Force Reconofax IX infrared mappers in U. S. Navy RA-3B aircraft, BuNo. 144839. The purpose of the test was to compare the performance of the two sets for reconnaissance aircraft. The results of these tests were to be used to establish realistic system parameters for reconnaissance aircraft. The NAVAIRDEVCCEN installed the Army and Air Force equipments, and a modified Reconofax VI in the RA-3B aircraft. This project became known unofficially as the "JANE TEN IR Flight Program."


RESULTS

From January to March 1966 flight tests were conducted, both night and day, over controlled targets and targets of opportunity. Film imagery taken at aircraft altitudes of 2000 feet revealed existence of targets such as roads, SAM sites, and bridges. Imagery taken at 1000 feet identified targets such as tanks, self-propelled guns, and automobiles. When targets were covered by heavy foliage, the infrared images were not discernible except when targets were much hotter or colder than the surroundings, or if the targets were very large. There was a noticeable deterioration in angular resolution for all equipments when the flight data was compared to the laboratory data. The temperature control of the thermal resolution targets was less than the designed thermal resolution of the equipments; consequently, accurate determination of thermal sensitivity was not made.

CONCLUSIONS

Current infrared mappers for reconnaissance aircraft are capable of meeting specific performance requirements such as high thermal sensitivity, high angular resolution, and capability of operation at high velocity to height ratio (V/H). For reconnaissance used in areas similar to those found in Southeast Asia, emphasis should be placed in high thermal and angular resolution capabilities with low to moderate V/H ratios not exceeding one rad/sec.

Inflight operation and performance of the infrared mappers indicated single axis (roll) stabilization was adequate to obtain desirable target imagery. Detector cooling systems employing liquid helium presented serious logistic problems resulting in a lack of standby flight readiness and a relatively short flight duration. Closed cycle coolers proved to be reliable and logistically more suitable than open liquid coolers. The lack of a real-time display made on-the-spot evaluation impossible.

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RECOMMENDATIONS

Infrared equipments for reconnaissance aircraft flying from 1000 to 3500 feet altitude should have:

1. Angular resolution 0.5 to 1 milliradian
2. Thermal sensitivity 0.5 to 1 degree centigrade
3. Closed cycle system for detector
4. Availability of real time viewer
5. Single axis (roll) stabilization.

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D I S C U S S I O N

DESCRIPTION OF EQUIPMENT

Reconofax IX (U. S. Air Force, HRB-Singer, Incorporated)

The Reconofax IX is a high velocity to height ratio (V/H) infrared mapping set developed by HRB-Singer, Incorporated (Contract AF33(657)-8870) and is comprised of these basic units (figure 1):

Scanner

Control

Monitor (oscilloscope)

Figure 2 is a block diagram of the Reconofax IX line-scanning system. Both the scanning optics and the recording optics are mounted on the same shaft which rotates at 17,000 rpm. The energy collected by the optical scanner unit is focused on a seven-element array of copper doped germanium infrared detectors. Each detector output is amplified and modulates a crater lamp (glow tube). Light from the crater lamps is put into the proper format (the same as the seven-element detector array) and imaged on the recording film.

The functions of the control unit are to provide:

Responsivity calibration

Average density calibration

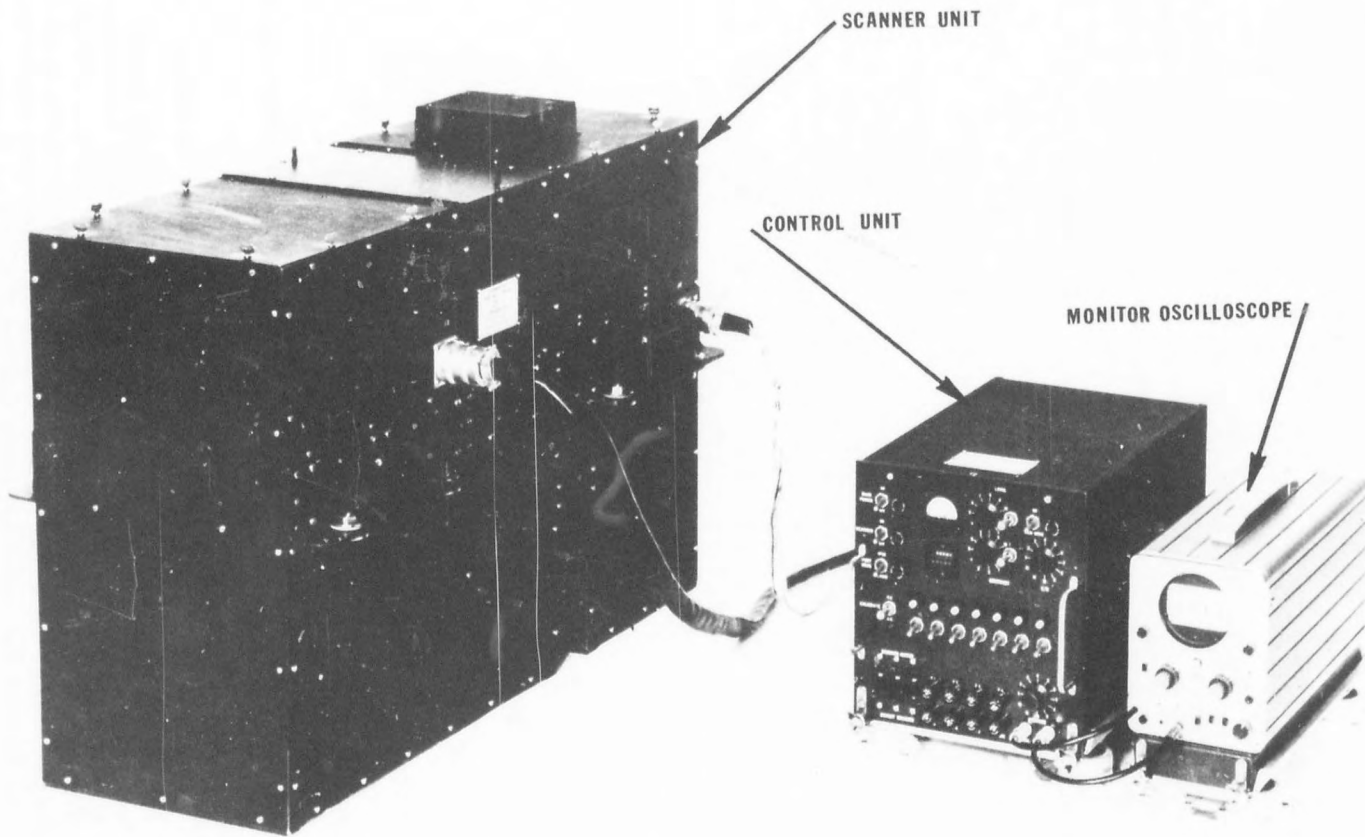
Overall gain adjustments

Power (primary) control

Film drive rate control

An oscilloscope monitor provides, in an x-y format, a means to observe the signals from each of the seven detector channels.

The combined requirements of $\frac{V}{H} = 4$ rad/sec., an instantaneous field of view (I FOV) of 1 milliradian (mv), and the corresponding large number of scans per second (4000) that had to be generated necessitated the use of a multielement detector array (seven channels) and a high speed scanner. Through the use of a two-sided scanner mirror rotating at 17,000 rpm and a seven-element detector array, a scan rate of 4000 lines/sec is achieved. The use of the seven-element detector leads to a number of fundamental design differences between high V/H and conventional IR line-scanning systems. These differences are primarily those required to insure that each channel of the high V/H system possesses the same overall



SCANNER UNIT

CONTROL UNIT

MONITOR OSCILLOSCOPE

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FIGURE 1 - Reconofax IX IR Detecting Set

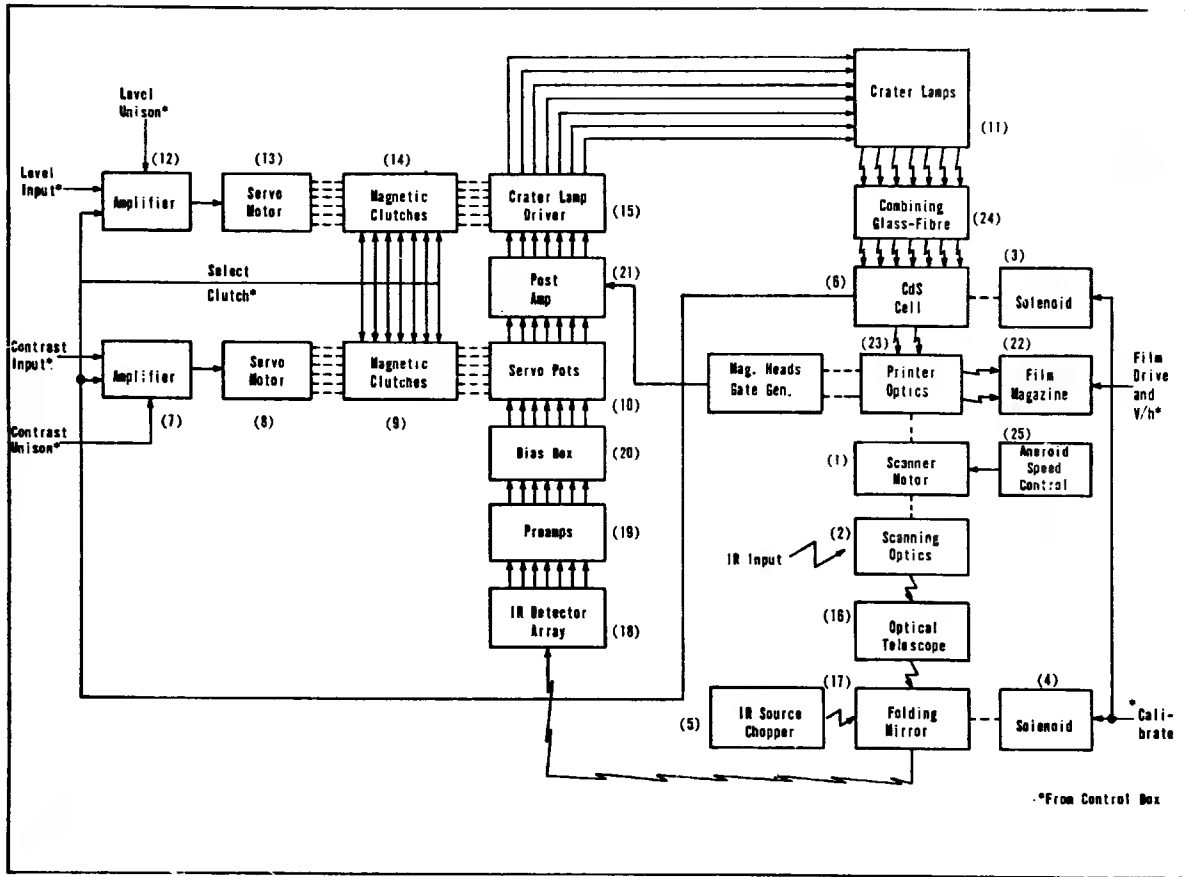


FIGURE 2 - Reconofax IX Scanner - Block Diagram

responsivity and produces the same average density on the recording film; also, the required upper limit of frequency response in each channel is considerably higher than normal, making it necessary to employ special techniques to extend the upper frequency to 1.2 mhz; in addition, a fiber optic bundle is needed to combine the light from the seven crater lamps into the same format as that of the seven-element IR detector array. This particular system employs single-axis (roll) stabilization.

AN/AAS-10(XE-1) (U. S. Army, Texas Instruments, Incorporated)

The AN/AAS-10(XE-1) is a high resolution infrared mapping system developed by Texas Instruments, Incorporated (Contract DA 36-039-AMC-00133CE1). This system is composed of scanner, stabilization, and control units (figure 3). It is a multichannel (5) device which provides good angular (0.5 mr) and temperature (0.5° C) resolutions and operates at relatively high V/H (1 rad/sec) ratios and moderate scan speeds (6000 rpm). Figure 4 shows the detector-cooler assembly, optical scanning assembly, and electronic circuitry.

Energy collected by the rotating four-sided scan mirror (6000 rpm) and an all-reflective Dahl-Kirkman optical system is focused on a five-element mercury-doped germanium detector array. The detector-array outputs, after suitable signal conditioning, modulate glow tubes whose light outputs are focused by an optical-mechanical recorder on the film. The result is a density which is a function of the IR energy level incident upon the detector array. Glow modulator tubes used as light transducers expose the film, and four rotating microscope objectives image the illuminated end of a fiber optic bundle on the film and provide scan motion.

The stabilization system for the AN/AAS-10 is a gyro-controlled, three-axis, self-contained control unit. This unit consists of one directional gyro for azimuth control and one vertical gyro for roll and pitch control.

A control panel, having on-off switches for the system power, electronics, detector-cooler assembly, stabilization unit, scan motor, and film drive, contains a test point control for selecting individual video channels, an input voltage meter and selector switch, and a V/H selector dial.

Reconofax VI, Modified (U. S. Navy, HRB-Singer, Incorporated)

The Reconofax VI infrared mapping set, a high thermal sensitivity device procured from HRB-Singer, Incorporated (Contract N62269-2202), consists of a scanner unit and a remote control unit (figure 5). All major components such as infrared optical system, film magazine, amplifier package, and detector are contained in the scanner unit. A control panel contains fuses, connectors, and all operating controls for the system.

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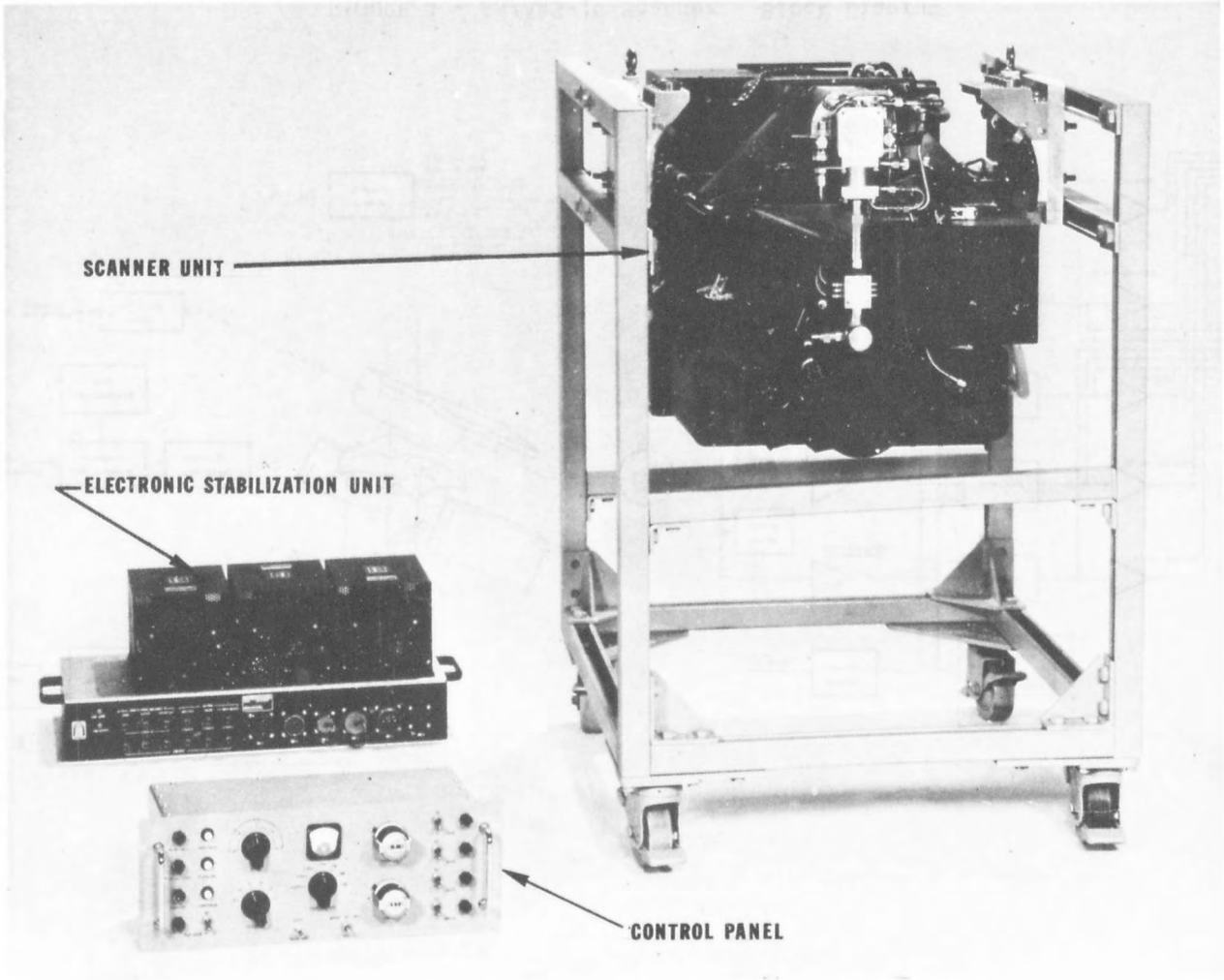
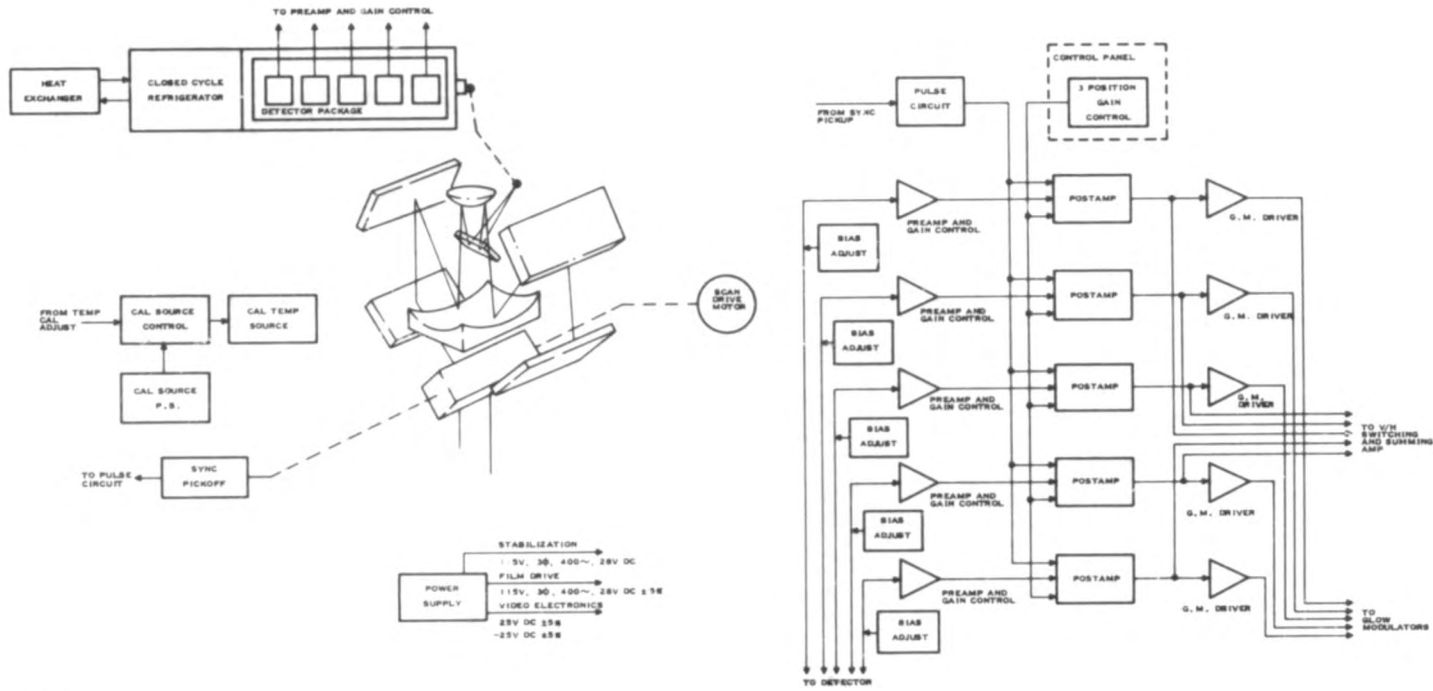


FIGURE 3 - AN/AAS-10 IR Detecting Set

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FIGURE 4 - AN/AAS-10 Scanner - Block Diagram

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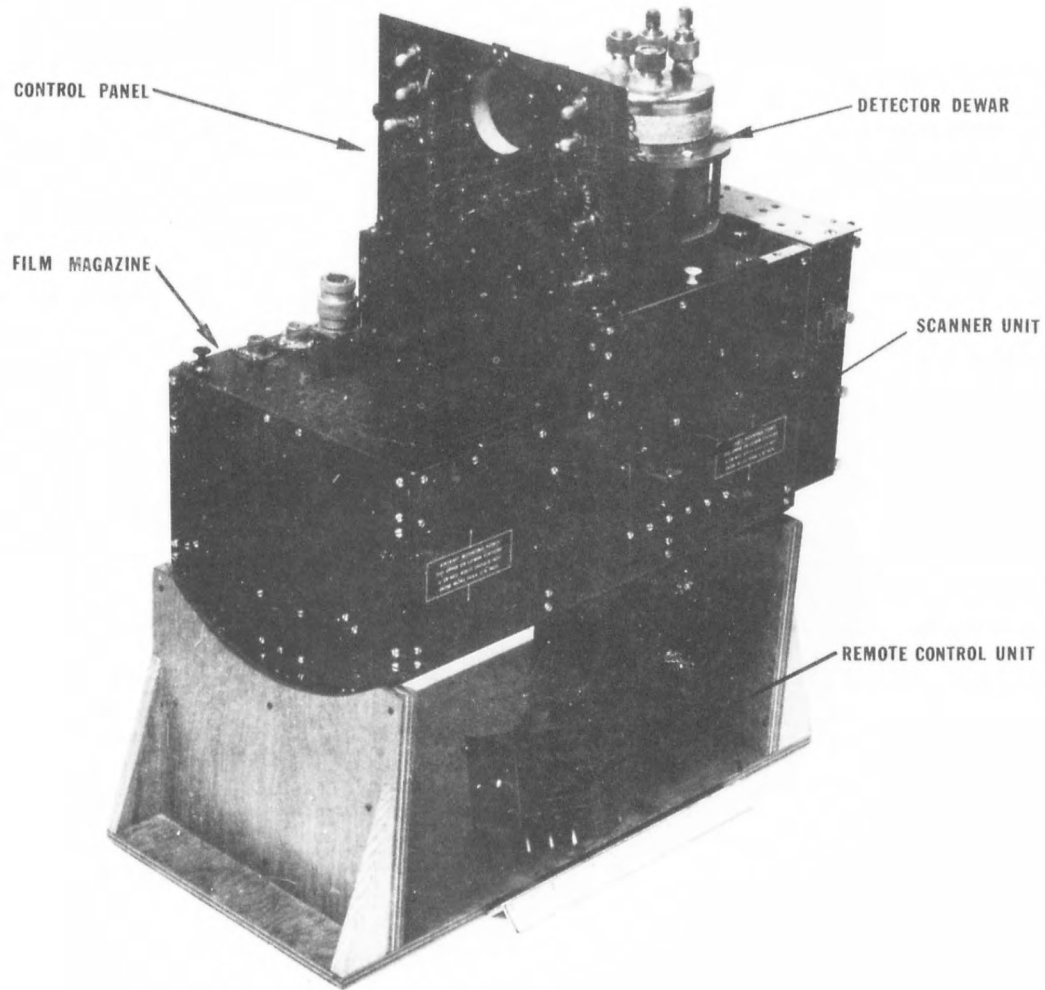


FIGURE 5 - Reconofax VI IR Detecting Set

The major components of the receiving and recording optical systems are:

Receiving

Double-faced scanner mirror
 Parabolic mirror
 3-1/4 in. dia. (6 in. focal length)
 Folding mirror

Recording

Glow modulator lamp
 Field Stop
 Folding mirror
 Objective lens

The geometry of the line scan is illustrated in figure 6. The terrain directly beneath the aircraft carrying the equipment is scanned at right angles to the direction of flight by the rotating scanner mirror. Motion of the aircraft provides the forward component of scan. The IR radiation received in this manner is focused on the detector whose video output varies with the amount of energy received from each point in the scan. After suitable signal processing, the video signal modulates the brightness of a glow tube. The light output of the glow tube, after reflection from a double-faced folding mirror, is focused to a small spot on the recording film by a pair of microscope objectives. With the recording and scanning optics on the same shaft, perfect synchronization is assured.

The combination of the line scanning and the recording systems lends itself to a very simple and effective means of gyro stabilization against roll; only the film magazine is stabilized. Since the film magazine is held in an upright position regardless of aircraft roll up to +30 degrees, any target vertically below the aircraft will be recorded at the center of the film, thus providing roll stabilization.

Characteristics of the AN/AAS-10, Reconofax IX, Reconofax VI (modified) infrared mapping systems are itemized in table I.

Appendix A gives a description of the aircraft modification and installation procedures required to accommodate the three infrared mappers in the RA-3B aircraft.

DETAIL RESULTS

A summary of the flight test program and comments regarding specific equipment problems and corrective measures taken are presented in appendix B.

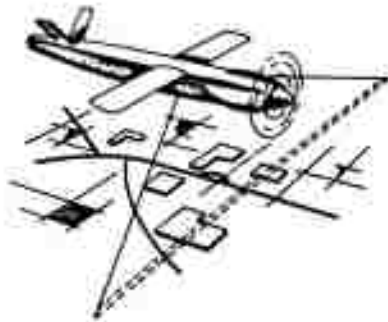
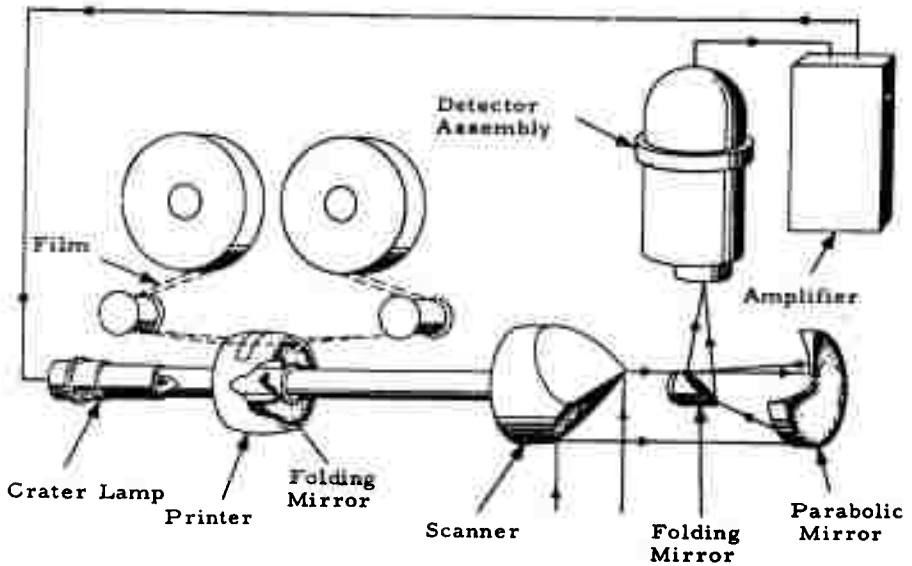


FIGURE 6 - Reconofax VI Optical System and Scanning Method

T A B L E I
EQUIPMENT CHARACTERISTICS

	AN/AAS-10(XE-1)	Reconofax IX	Modified Reconofax VI
I FOV	0.5 mr	1.0 mr	3.3 mr
Total FOV	140 deg	140 deg	140 deg
V/H	0.2-1.0 rad/sec	0.1-4.0 rad/sec	0.1-1.3 rad/sec
Scan mirror angular velocity	6000 rpm	17,000 rpm	12,000 rpm
Scan mirror type	4-sided 2 x 8 in.	2-sided 5 in. dia	2-sided 3 1/4 in. dia
Scans/second (max)	2000	4000	400
Detector type	Ge:Hg 5 elements 0.64 x 0.64 mm	Ge:Cu, 7 elements 0.25 mm dia	Ge:Cu, 1 element 0.5 mm dia
Detector cooling	Norelco, 2-stage sterling cycle closed loop	liquid helium/nitrogen double dewar	liquid helium/nitrogen double dewar
Infrared filter	None used	germanium, 2 μ cut-on long pass; daytime only	germanium, 8 μ cut-on long pass

TABLE I (continued)

	AN/AAS-10(XE-1)	Reconofax IX	Modified Reconofax VI
Responsivity Balancing	all 5 channels balanced by variable control in preamplifiers	all 7 channels balanced with Cds cell against cali- brated IR source	not required for single-channel
Detectivity (AVG)D (500 deg K)	$1.5-2.0 \times 10^{10} \frac{\text{cm-Hz}^{1/2}}{\text{watt}}$	$2 \times 10^9 \frac{\text{cm-Hz}^{1/2}}{\text{watt}}$	$8.5 \times 10^9 \frac{\text{cm-Hz}^{1/2}}{\text{watt}}$
Noise equivalent temperature difference (NE ΔT)	0.68 C° (lab)	2.5 C° (lab)	0.15 C° (lab)
Stabilization	Scanner: 3-axis +10 deg pitch, yaw and roll	Recorder: single axis, +10 deg roll	Recorder: single axis, +30 deg roll
Recording film	5 in. x 250 ft Kodak Tri-X SO 260	70 mm x 125 ft Kodak 2475	70 mm x 100 ft Kodak Tri-X 5063
Recording format	4 in. image, 3/4 flight data block, 6 in. intervals	70 mm image, no film marking provisions	70 mm image, manual film marking
Recorder type	Glow modulators, fiber optics	Glow modulators, fiber optics	Glow modulator
Recording film speed (max)	8.2 ft/min	20 ft/min	6.15 ft/min

TABLE I (continued)

	AN/AAS-10(XE-1)	Reconofax IX	Modified Reconofax VI
Recording film processing	EH-38 Versamat	DK-60 "A" Chemistry, hand processed	EH-38 Versamat
Weight	Scanner 330 lb 3-axis stab. 120 stab. elec. 50 control unit $\frac{5}{505}$ lb	Scanner 180 lb Control unit 60 Monitor oscill. $\frac{17}{257}$ lb	Scanner 60 lb Control Unit $\frac{1}{61}$ lb
Size	Scanner/recorder/ 3-axis stabilization 45 x 22 x 45 in. Control unit 19 x 7 x 7 in. Stab-electronics 12 x 12 x 26 in. Total volume = 25.78+74+2.16 = 28.68 cu ft	Scanner/recorder 12 x 23 x 35 in. Control unit 10 1/4 x 12 5/16 x 19 5/16 in. Monitor oscilloscope 5 7/8 x 11 7/16 x 18 3/4 in. Total volume = 5.6+1.4+0.7 = 7.7 cu ft	Scanner/recorder 11 1/4 x 19 x 23 in. Control unit 2 3/4 x 4 3/4 x 3 1/2 in. Total volume = 2.84 + 0.026 = 2.866 cu ft

T A B I E I (c o n t i n u e d)

	AN/AAS-10(XE-1)	Reconofax IX	Modified Reconofax VI
"Air window" slot size in RA-3B A/C	23 in. x 66 in.	3.5 in. x 44 in.	5 in. x 18 in.
Power 28VDC	10 amp normal 30 amp surge	4 amp normal 10 amp surge	9 amp normal 20 amp surge
30 115V 400 cycle	5 amp/phase normal 10 amp/phase surge	5 amp/phase normal 10 amp/phase surge	
Approximate procurement cost of one unit	\$300,000	\$170,000	\$60,000

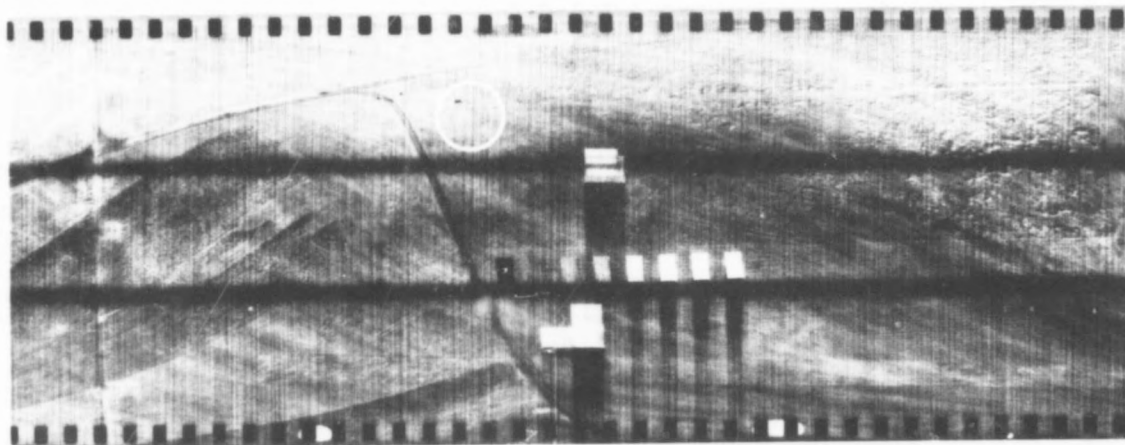
Table II presents the pertinent parameters measured either in flight or in the laboratory, together with the corresponding ones from the manufacturers' specifications for the three infrared mapping systems.

T A B L E I I
MEASUREMENT COMPARISON

	Reconofax IX		AN/AAS-10		Reconofax VI	
	Mfgs Spec	Measured	Spec	Measured	Spec	Measured
Thermal (C°) Sensitivity	1	2.5* (Lab)	0.5	0.7* (Lab)	0.15	0.15* (Lab)
Angular (mr) Resolution	1	2 (Flt)	0.5	0.75 (Flt)	3.3	5.0 (Flt)
V/H (max) (rad/sec)	4	4 (Flt)	1.0	1.0 (Flt)	1.3	1.3 (Flt)

*Laboratory measurement

Flight imagery of the three infrared systems is presented in thirty-three photographs (figures 7 through 37). Because the photographs were reproduced from negatives made from positive duplicates of the original films, the copies are greatly degraded from the original imagery. These pictures contain selected imagery from all the target sites, listed in appendix C, and illustrate the operational flight capability of each infrared mapper. In addition to the caption information on each print, amplifying comments pertinent to these pictures are catalogued in the following text.



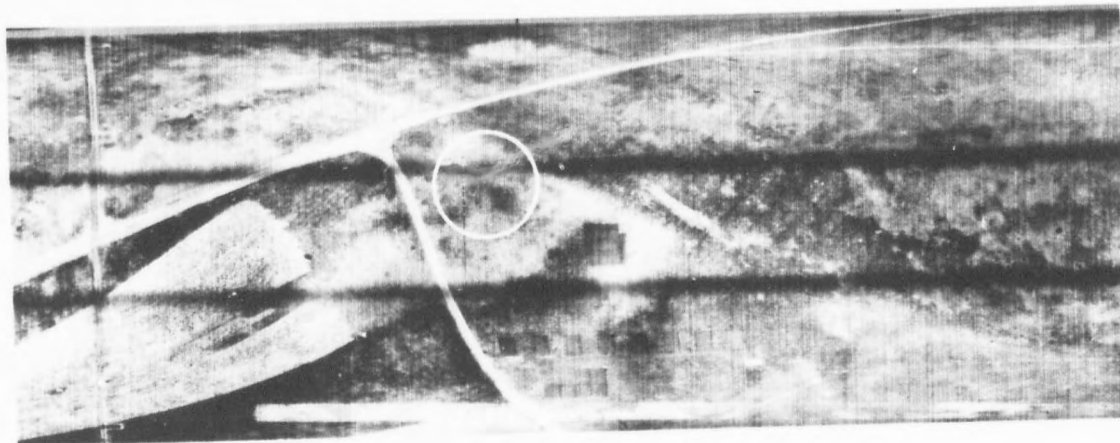
NADC-AE-6718

RECONOFAX IX
FLIGHT 10
RUN 3
V/H 4

DATE: 2/17/66
TIME: 1427R
ALTITUDE: 190 ft
SPEED: 450 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Resolution targets at Patterson Field
WEATHER: Clear, visibility unlimited
DETECTORS: All 7; Ge:Cu

FIGURE 7 - Flight Imagery of the Three IR Systems



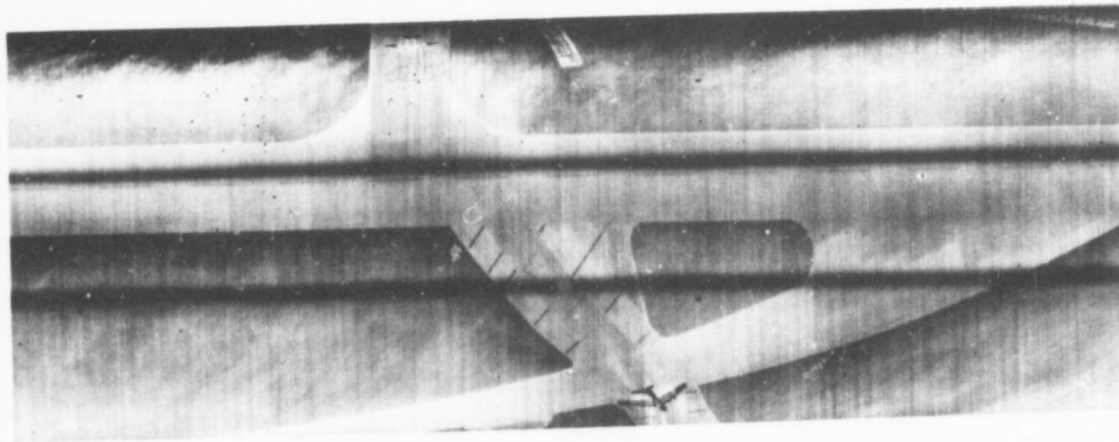
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RECONOFAX IX
FLIGHT 11
RUN 3
V/H 4

DATE: 2/17/66
TIME: 1930R
ALTITUDE: 190 ft
SPEED: 450 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Resolution targets at Patterson Field
WEATHER: Clear, visibility unlimited
DETECTORS: All 7; Ge:Cu

FIGURE 8 - Flight Imagery of the Three IR Systems



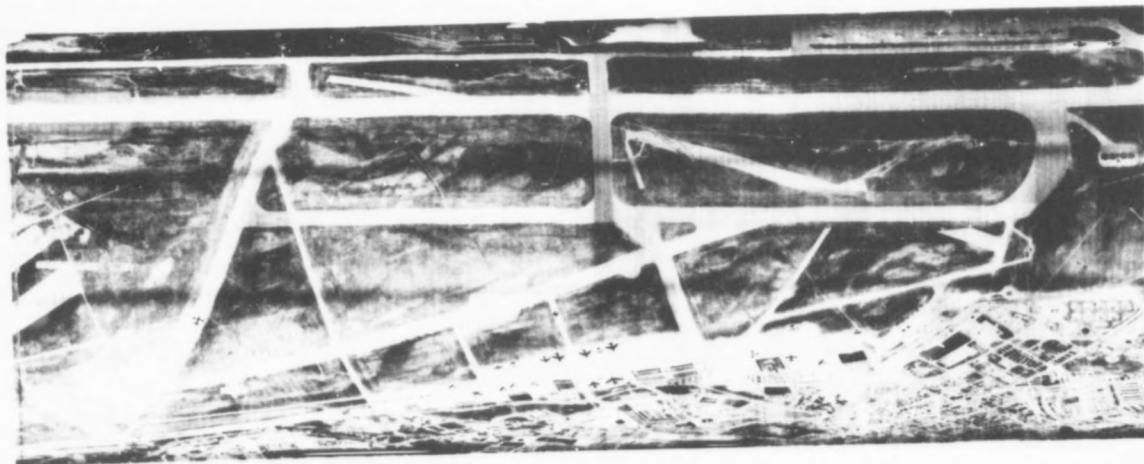
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RECONOFAX IX
FLIGHT 13
RUN 4
V/H 2

DATE: 2/18/66
TIME: 1915R
ALTITUDE: 370 ft
SPEED: 450 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Aircraft on Patterson Field
WEATHER: 10K broken visibility 15 miles in haze/smoke
DETECTORS: #2, 3, 5, 6; Ge:Gu

FIGURE 9 - Flight Imagery of the Three IR Systems



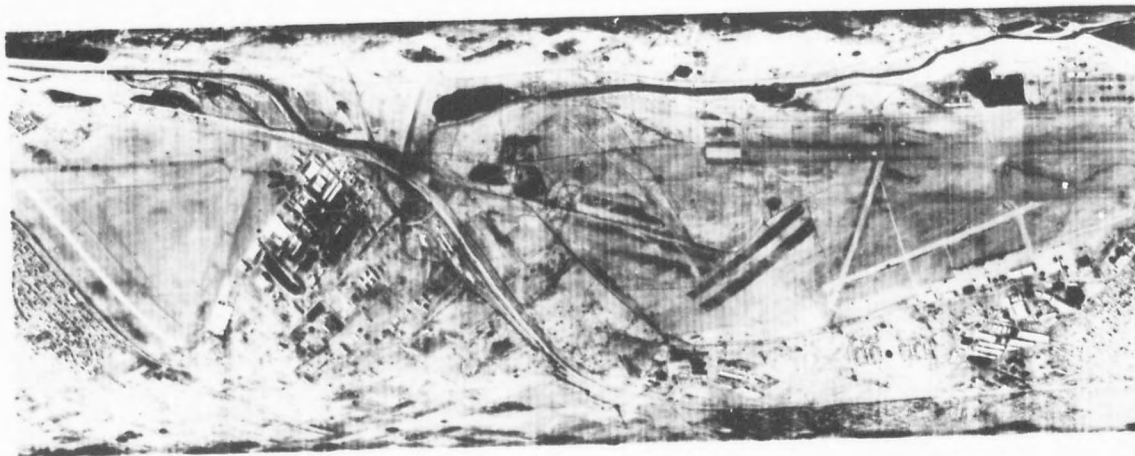
NADC-AE-6718

RECONOFAX IX
FLIGHT 11
RUN 4
V/H 0.25

DATE: 2/17/66
TIME: 1936R
ALTITUDE: 2000 ft
SPEED: 300 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Patterson Field complex
WEATHER: Clear, visibility unlimited
DETECTORS: All 7; Ge:Cu

FIGURE 10 - Flight Imagery of the Three IR Systems



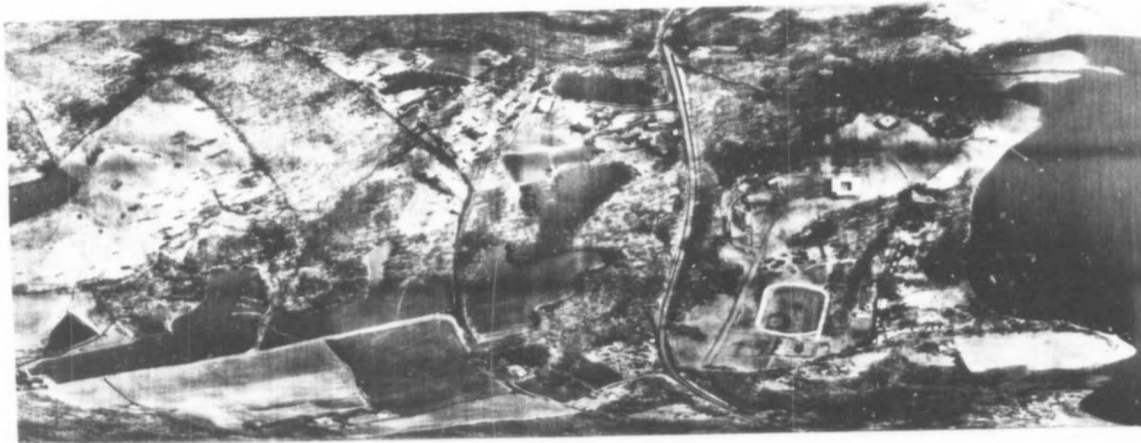
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RECONOFAX IX
FLIGHT 12
RUN 9
V/H 0.1

DATE: 2/18/66
TIME: 1450R
ALTITUDE: 5000 ft
SPEED: 300 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Wright and Patterson Fields
WEATHER: 20K scattered, visibility 25 miles, light haze
DETECTORS: #3, Ge:Cu

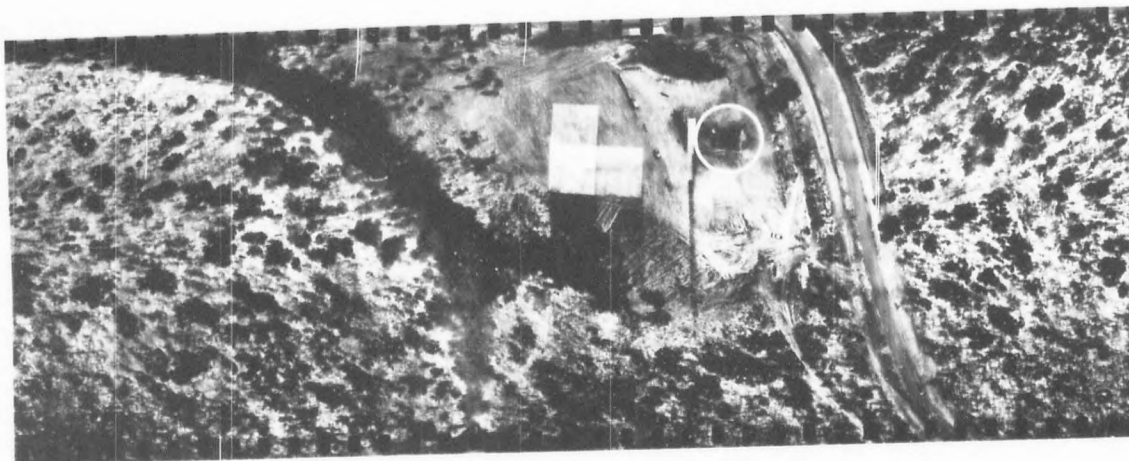
FIGURE 11 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX IX DATE: 3/5/66 AREA: Enroute NAF Johnsville to NAS Sanford, Florida
CHECKOUT
FLIGHT 6 TIME: 1400R TARGET: Countryside (West Virginia)
V/H 0.17 ALTITUDE: 3000 ft WEATHER: Hazy, visibility 3 miles
SPEED: 300 kn DETECTORS: Single element array; Ge:Cu

FIGURE 12 - Flight Imagery of the Three IR Systems



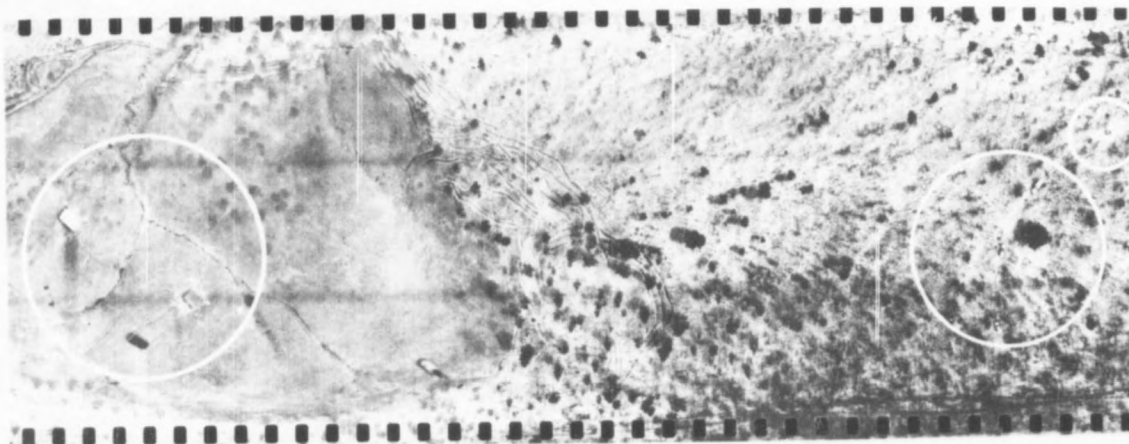
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RECONOFAX IX
FLIGHT 16
RUN 12
V/H 2.7

DATE: 3/11/66
TIME: 12:12S
ALTITUDE: 250 ft
SPEED: 400 kn

AREA: Eglin Air Force Base, Florida
TARGET: Resolution targets
WEATHER: 6K, light overcast, visibility 7 miles
DETECTORS: #1, 2, 3, 5, 6; Ge:Cu

FIGURE 13 - Flight Imagery of the Three IR Systems



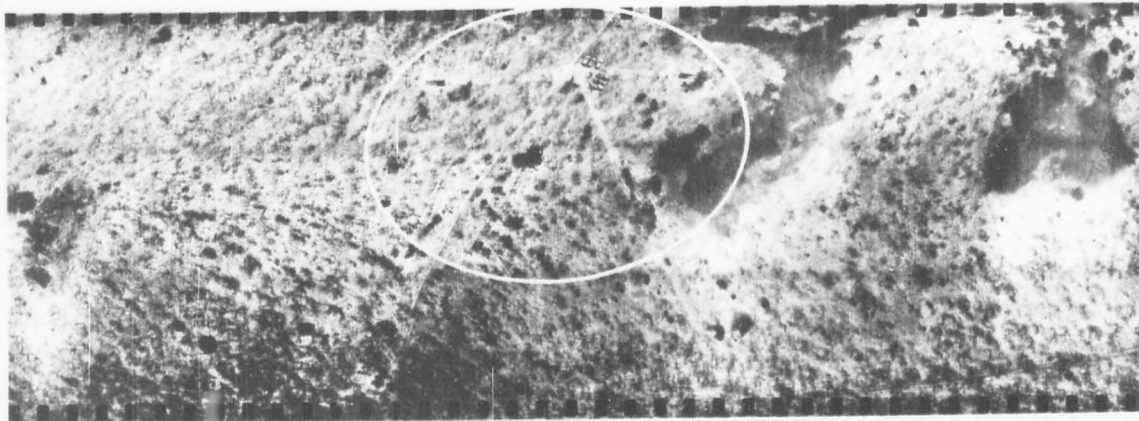
NADC-AE-6718

RECONOFAX IX
FLIGHT 16
RUN 12
V/H 2.7

DATE: 3/11/66
TIME: 1212S
ALTITUDE: 250 ft
SPEED: 400 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site I Village complex
WEATHER: 6K, light overcast, visibility 7 miles
DETECTORS: #1, 2, 3, 5, 6; Ge:Cu

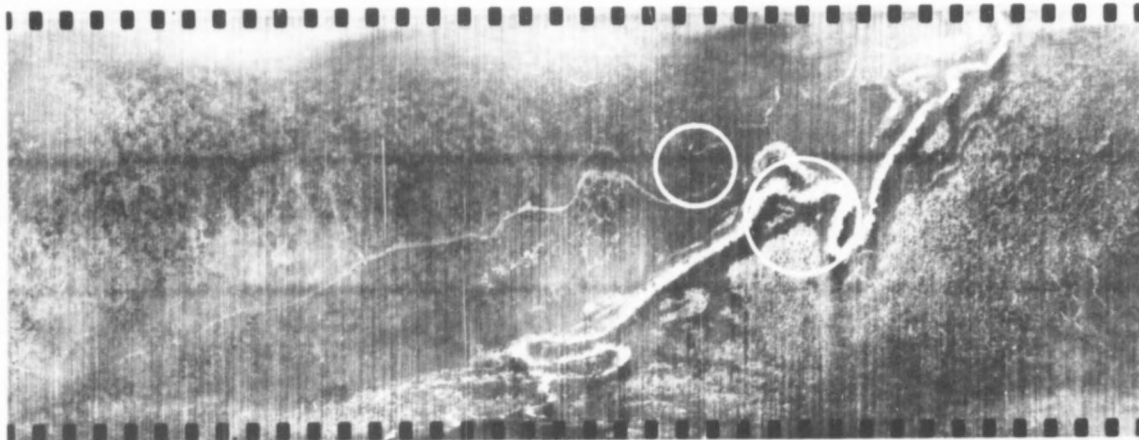
FIGURE 14 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX IX DATE: 3/11/66 AREA: Eglin Air Force Base, Florida
FLIGHT 16 TIME: 1212S TARGET: SAM Site
RUN 12 ALTITUDE: 250 ft WEATHER: 6K, light overcast, visibility 7 miles
V/H 2.7 SPEED: 400 kn DETECTORS: #1, 2, 3, 5, 6; Ge:Cu

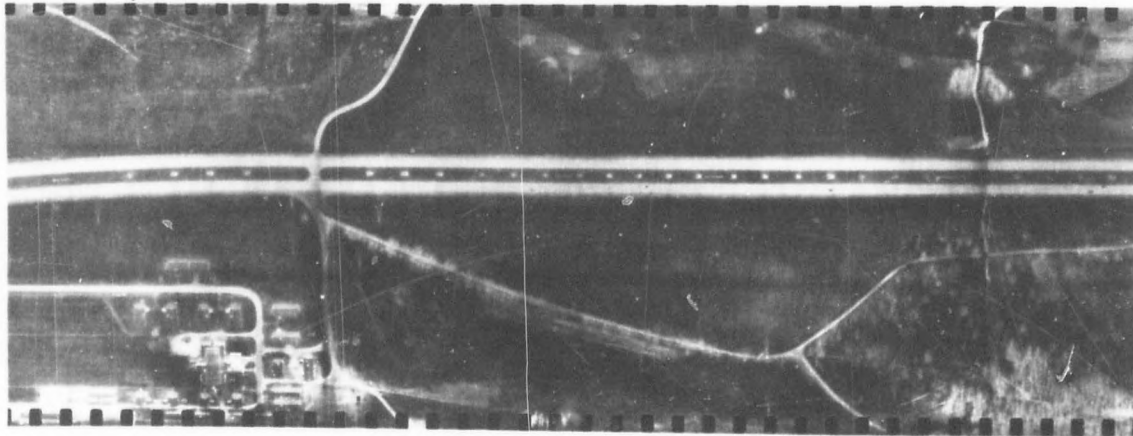
FIGURE 15 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX IX	DATE: 3/25/66	AREA: Eglin Air Force Base, Florida
FLIGHT 20	TIME: 0043S	TARGET: Site III Village complex and Sampans
RUN 10	ALTITUDE: 750 ft	WEATHER: Clear
V/H 1	SPEED: 450 kn	DETECTORS: #2, 6; Ge:Cu

FIGURE 16 - Flight Imagery of the Three IR Systems



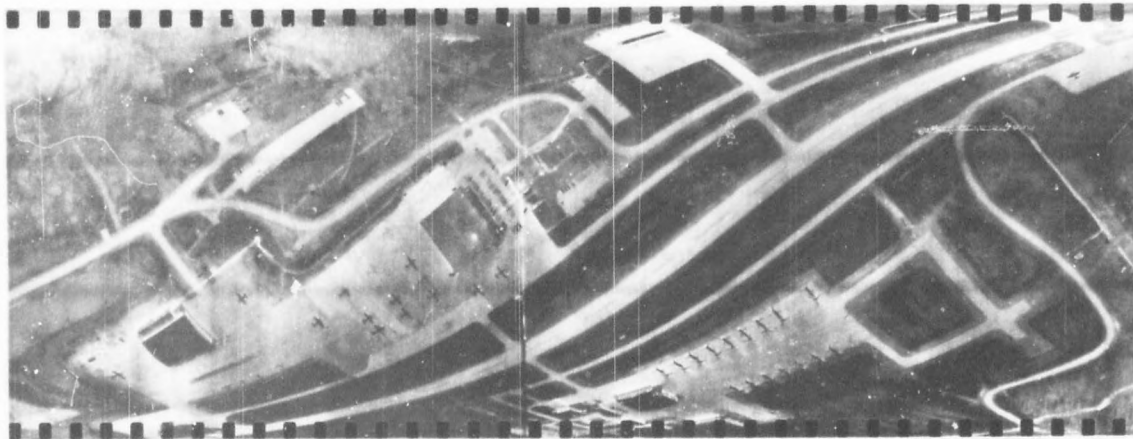
NADC-AE-6718

RECONOFAX IX
FLIGHT 22
RUN 5
V/H 1

DATE: 3/29/66
TIME: 2100R
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Aberdeen Proving Ground, Maryland
TARGET: Tanks and armored vehicles
WEATHER: Clear
DETECTORS: Single element array; Ge:Cu

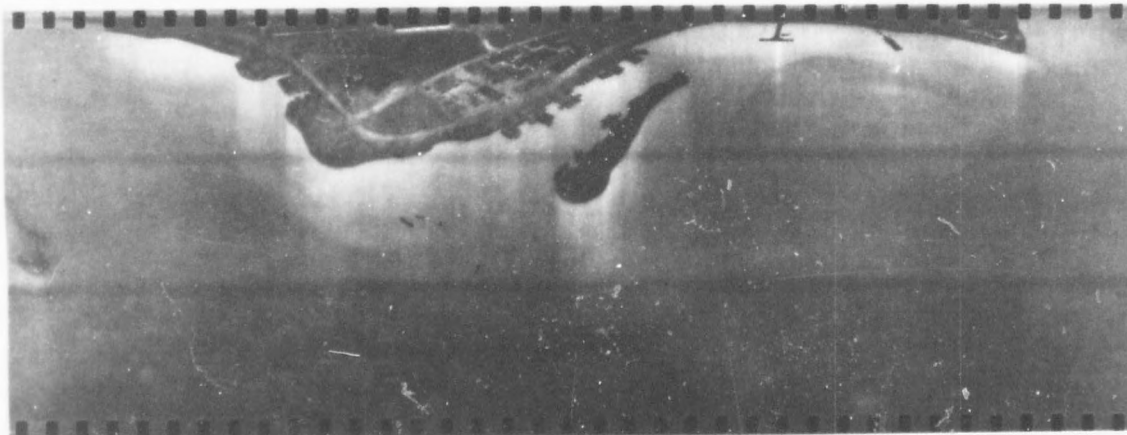
FIGURE 17 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX IX DATE: 3/29/66 AREA: Ft. Belvoir, Virginia
FLIGHT 22 TIME: 2147R TARGET: Airfield
RUN 12 ALTITUDE: 500 ft WEATHER: Clear
V/H 1 SPEED: 300 kn DETECTORS: Single element array; Ge:Cu

FIGURE 18 - Flight Imagery of the Three IR Systems



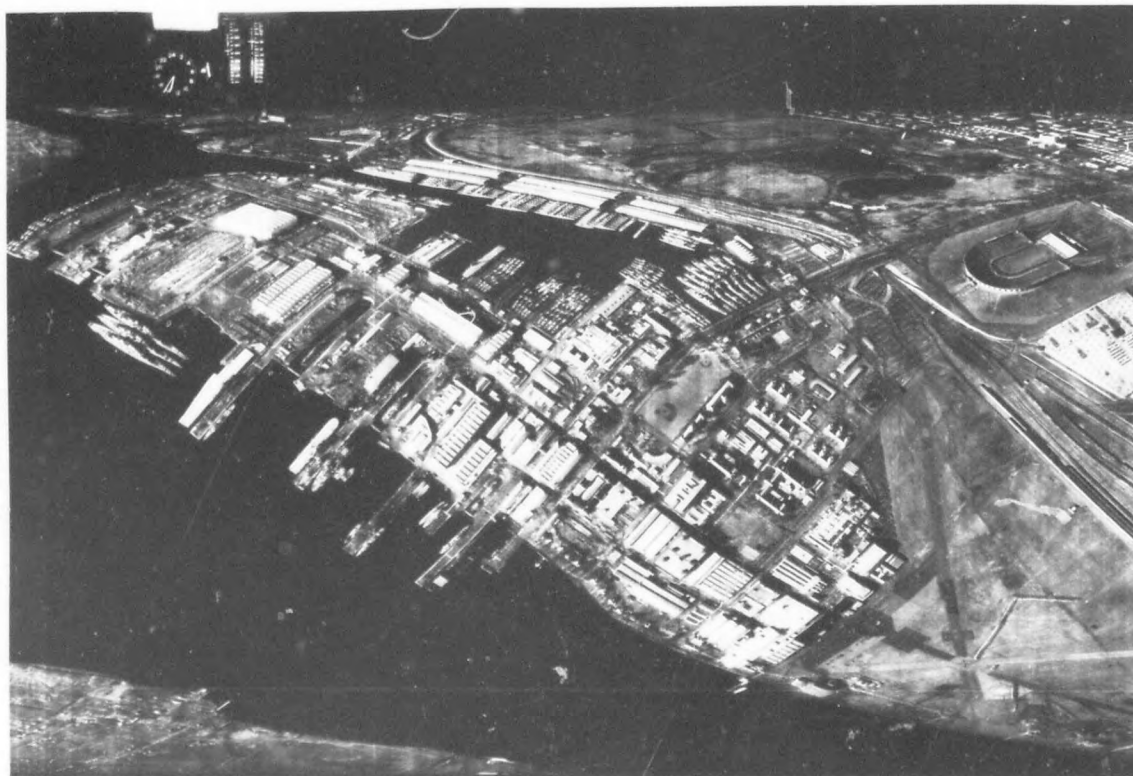
NADC-AE-6718

RECONOFAX IX
FLIGHT 22
RUN 13
V/H 1

DATE: 3/29/66
TIME: 2151R
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Ft. Belvoir, Virginia
TARGET: Pontoon bridge complex
WEATHER: Clear
DETECTORS: Single element array; Ge:Cu

FIGURE 19 - Flight Imagery of the Three IR Systems



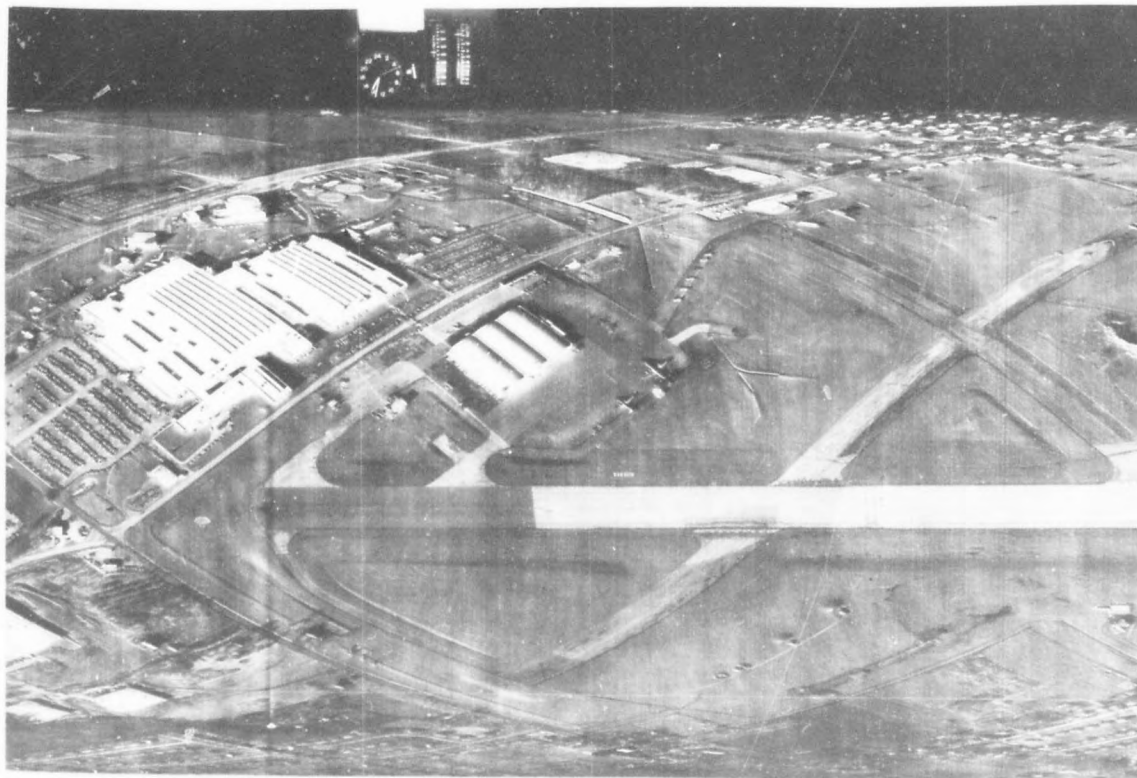
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 1
RUN 1
V/H 0.25

DATE: 1/20/66
TIME: 1335R
ALTITUDE: 2000 ft
SPEED: 300 kn

AREA: South Philadelphia industrial complex
TARGET: Philadelphia Naval Shipyard
WEATHER: 4.5K scattered, visibility 10 miles
DETECTORS: 5 Ge:Hg

FIGURE 20 - Flight Imagery of the Three IR Systems



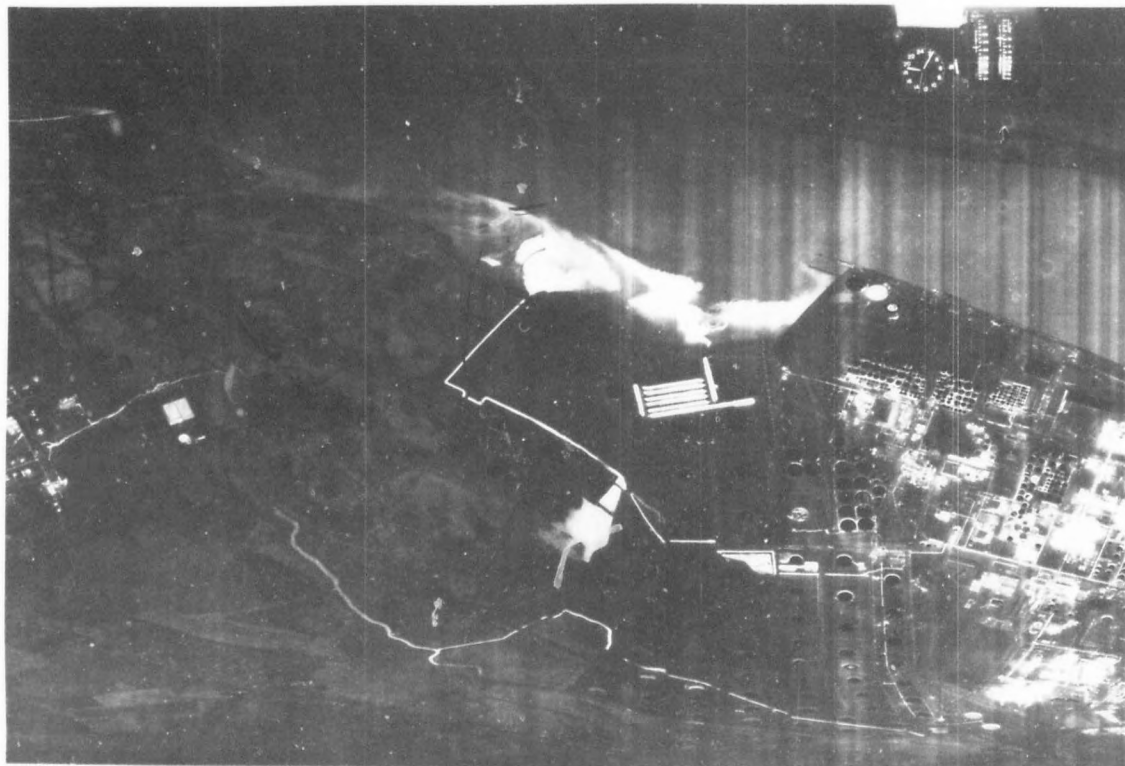
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 1
RUN 6
V/H 0.5

DATE: 1/20/66
TIME: 1432R
ALTITUDE: 1000 ft
SPEED: 300 kn

AREA: NAF Johnsville, Pennsylvania
TARGET: Airfield complex and resolution targets
WEATHER: 4.5K scattered, visibility 10 miles
DETECTORS: 5 Ge:Hg

FIGURE 21 - Flight Imagery of the Three IR Systems



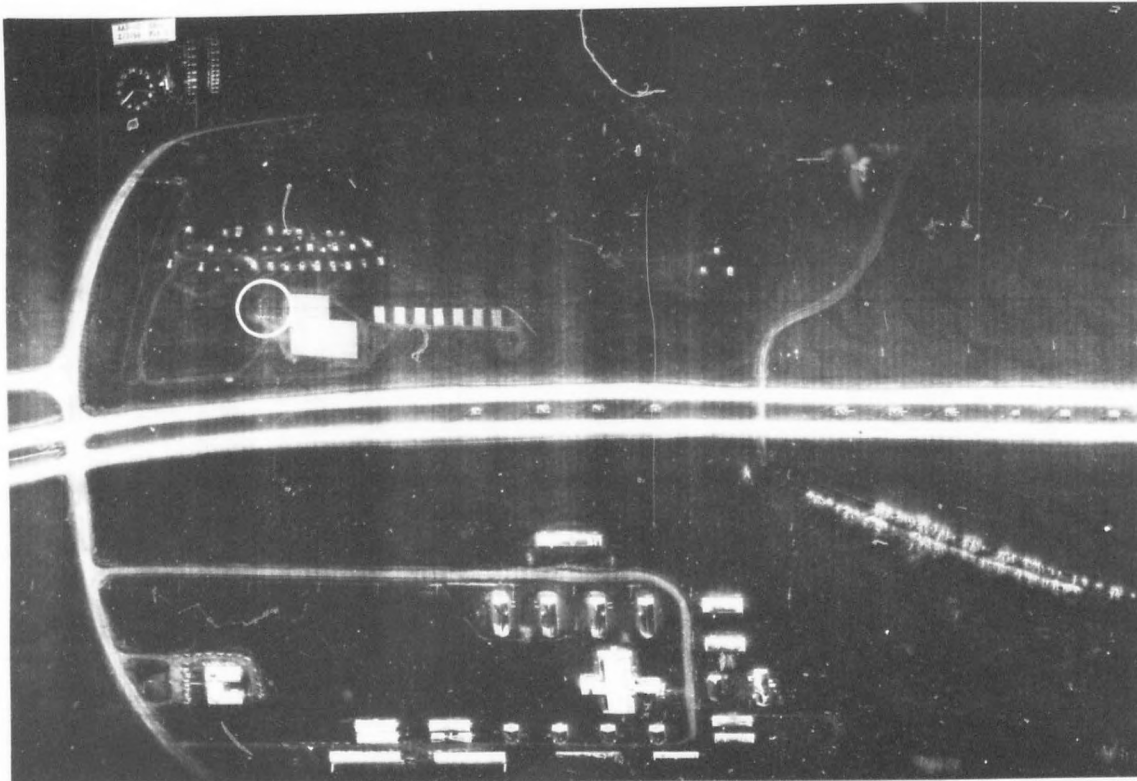
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 2
RUN 1
V/H 0.25

DATE: 1/20/66
TIME: 1900R
ALTITUDE: 2000 ft
SPEED: 300 kn

AREA: South Philadelphia industrial complex
TARGET: Oil tank farms
WEATHER: 4K scattered, visibility 10 miles
DETECTORS: 5 Ge:Hg

FIGURE 22 - Flight Imagery of the Three IR Systems



NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 5
RUN 5

DATE: 2/3/66
TIME: 1539R
ALTITUDE: 500 ft

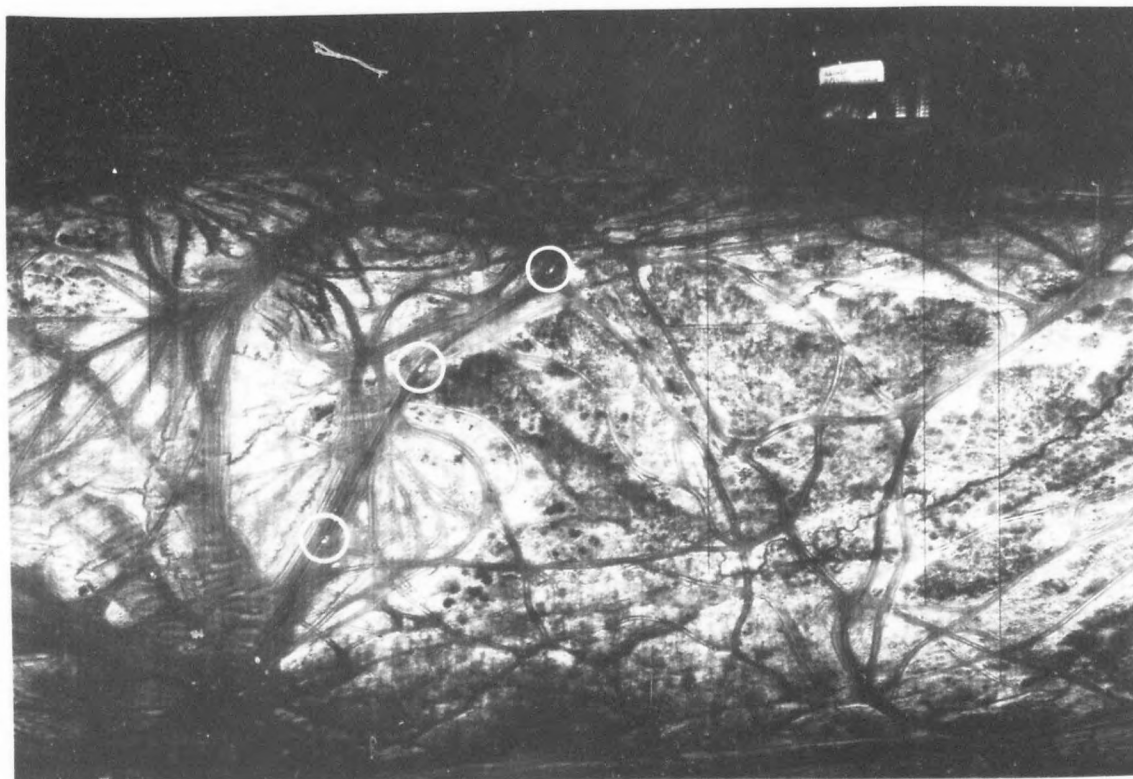
AREA: Aberdeen Proving Ground, Maryland
TARGET: Tanks and armored vehicles, resolution targets
WEATHER: Broken clouds, visibility fair in haze, snow
on ground

V/H 1

SPEED: 300 kn

DETECTORS: 5 Ge:Hg

FIGURE 23 - Flight Imagery of the Three IR Systems



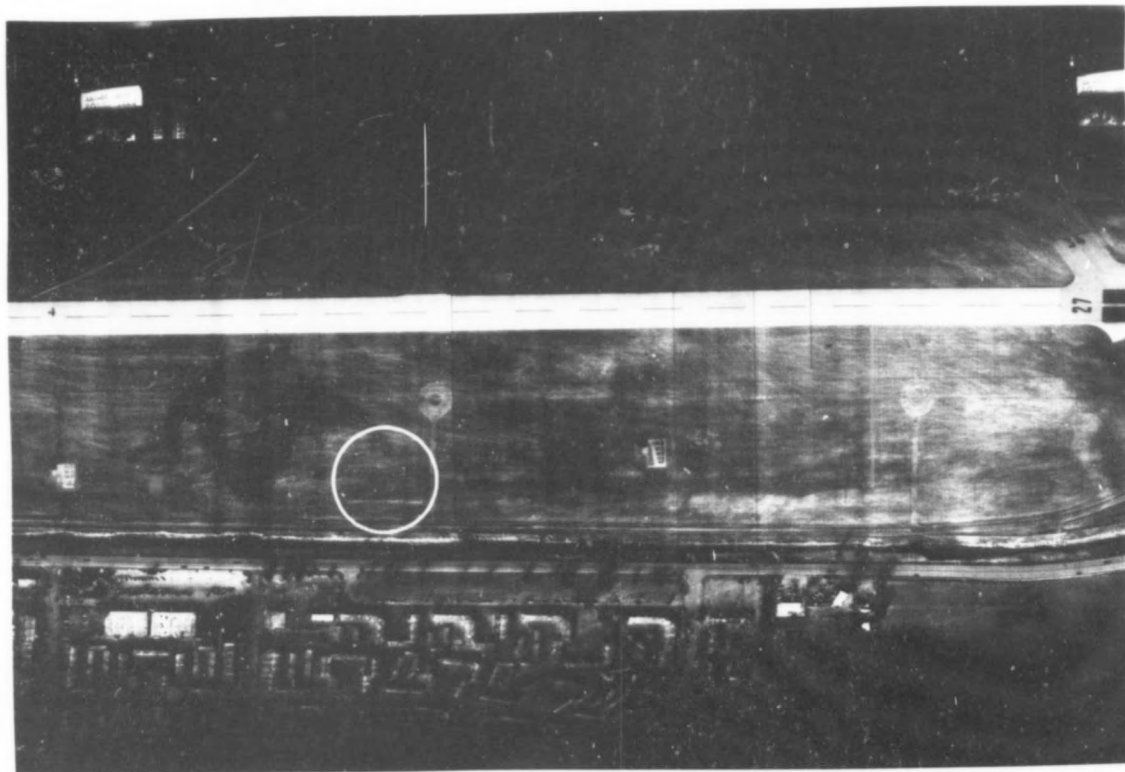
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 8
RUN 2
V/H 1

DATE: 2/15/66
TIME: 1337R
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Ft. Knox, Kentucky
TARGETS: Tanks
WEATHER: 5K scattered, visibility 7 miles in haze
DETECTORS: 5 Ge:Hg

FIGURE 24 - Flight Imagery of the Three IR Systems



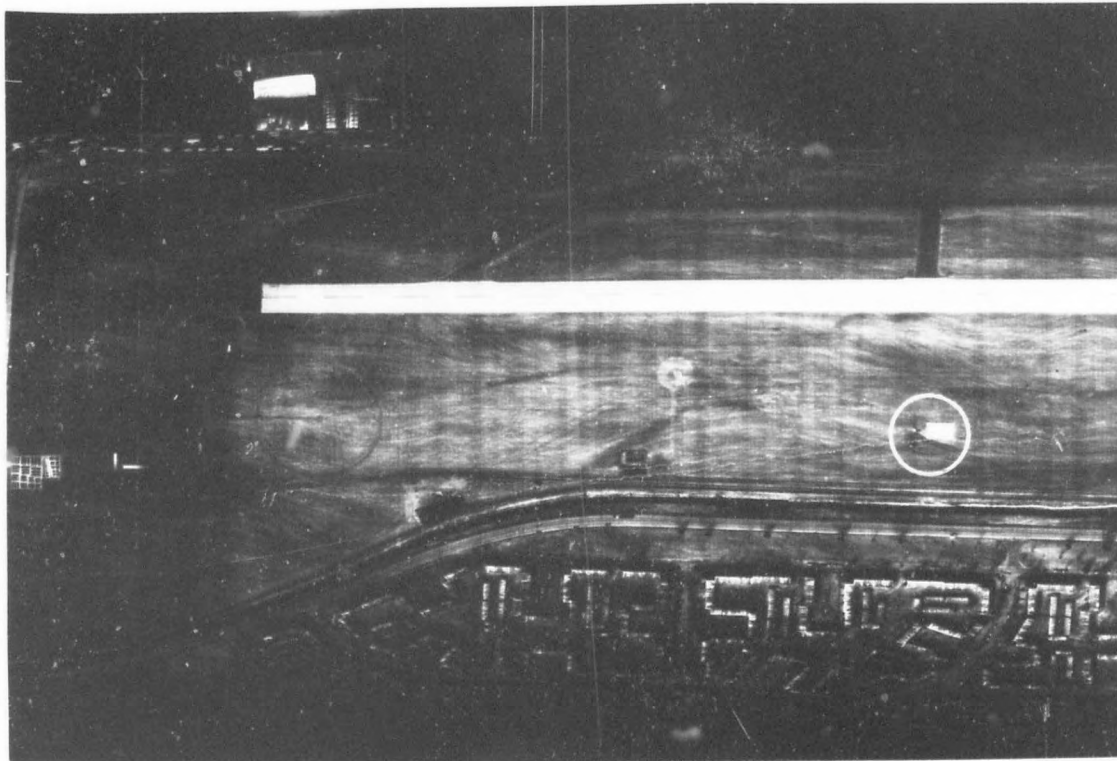
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 8
RUN 9
V/H 0.5

DATE: 2/15/66
TIME: 1444R
ALTITUDE: 750 ft
SPEED: 220 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Thermal resolution targets on Wright Field
WEATHER: 5K scattered, visibility 7 miles in haze
DETECTORS: 5 Ge:Hg

FIGURE 25a - Flight Imagery of the Three IR Systems



NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 8

DATE: 2/15/66
TIME: 1444R

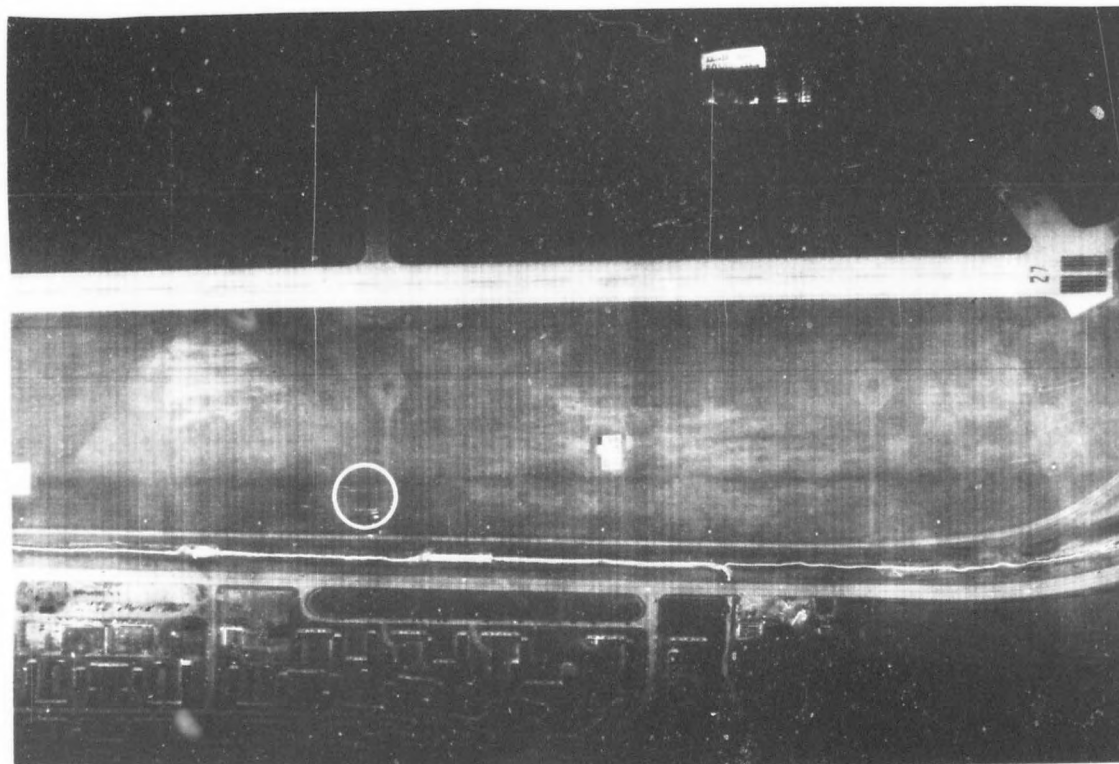
AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Thermal sensitivity and photographic resolution
targets on Wright Field

RUN 9
V/H 0.5

ALTITUDE: 750 ft
SPEED: 220 kn

WEATHER: 5K scattered, visibility 7 miles in haze
DETECTORS: 5 Ge:Hg

FIGURE 25b - Flight Imagery of the Three IR Systems



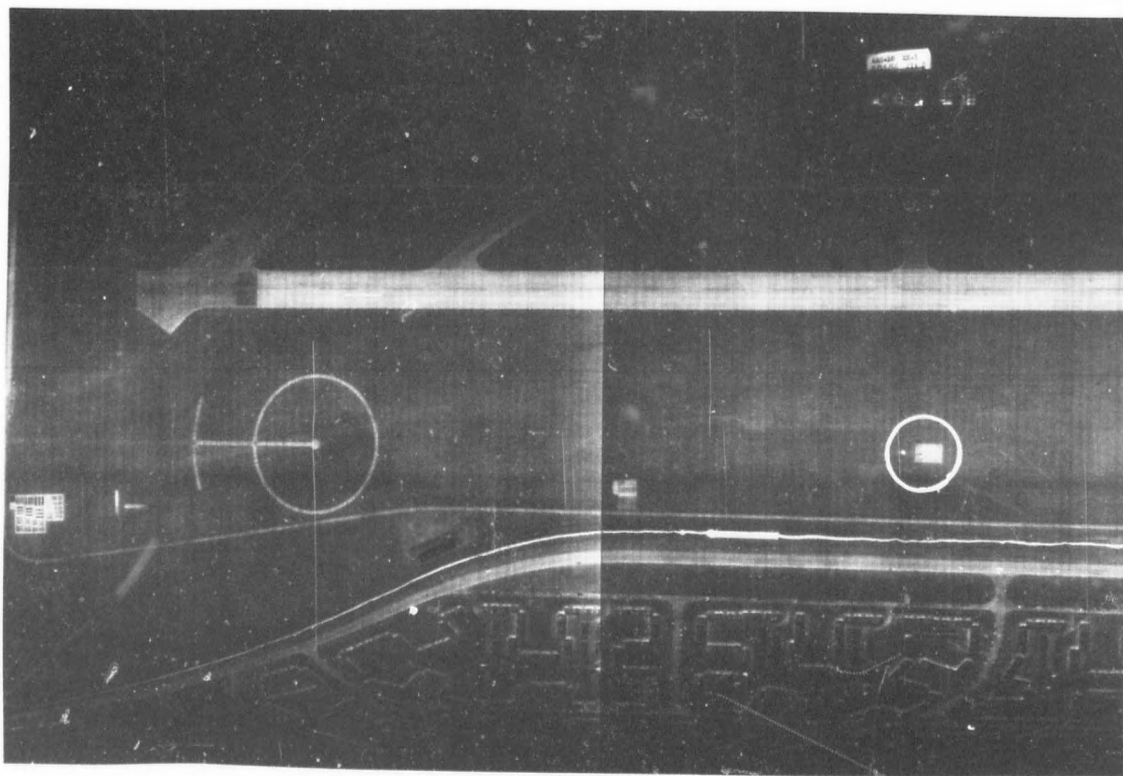
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 9
RUN 10
V/H 1

DATE: 2/15/66
TIME: 2031R
ALTITUDE: 750 ft
SPEED: 450 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Thermal resolution targets on Wright Field
WEATHER: 7K scattered, visibility 10 miles in light haze
DETECTORS: 5 Ge:Hg

FIGURE 26a - Flight Imagery of the Three IR Systems



NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 9

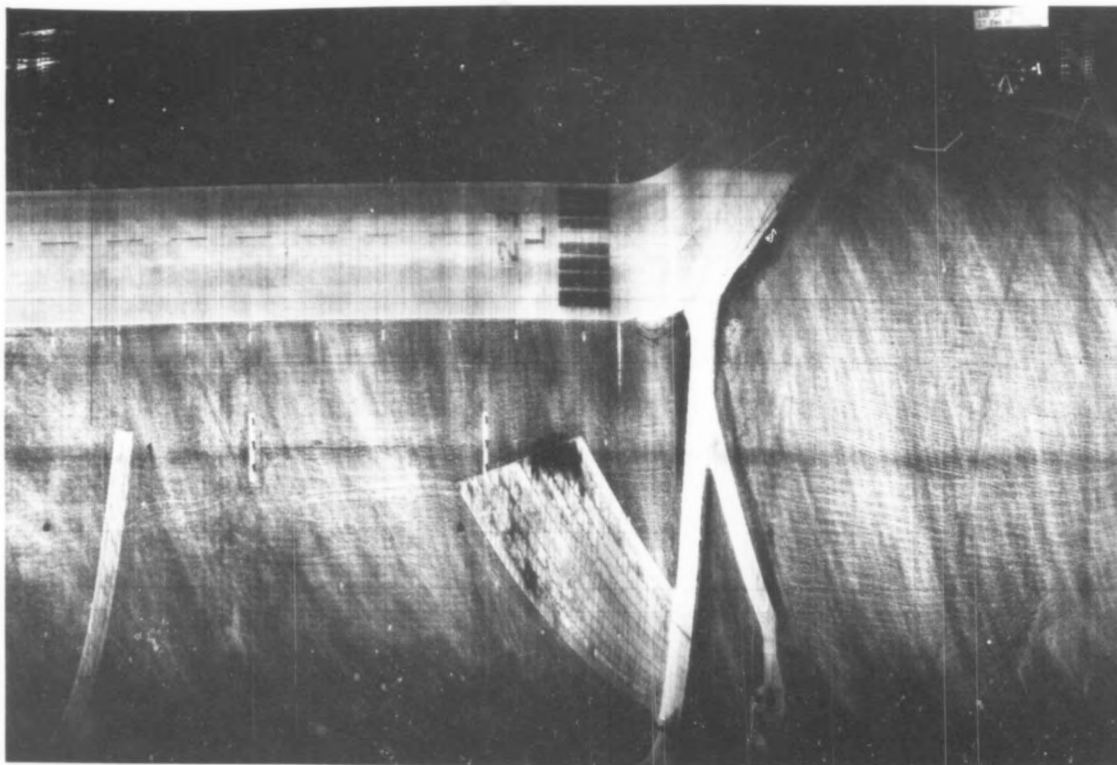
DATE: 2/15/66
TIME: 2031R

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Thermal sensitivity and photographic
resolution targets on Wright Field
WEATHER: 7K scattered, visibility 10 miles in light haze
DETECTORS: 5 Ge:Hg

RUN 10
V/H 1

ALTITUDE: 750 ft
SPEED: 450 kn

FIGURE 26b - Flight Imagery of the Three IR Systems



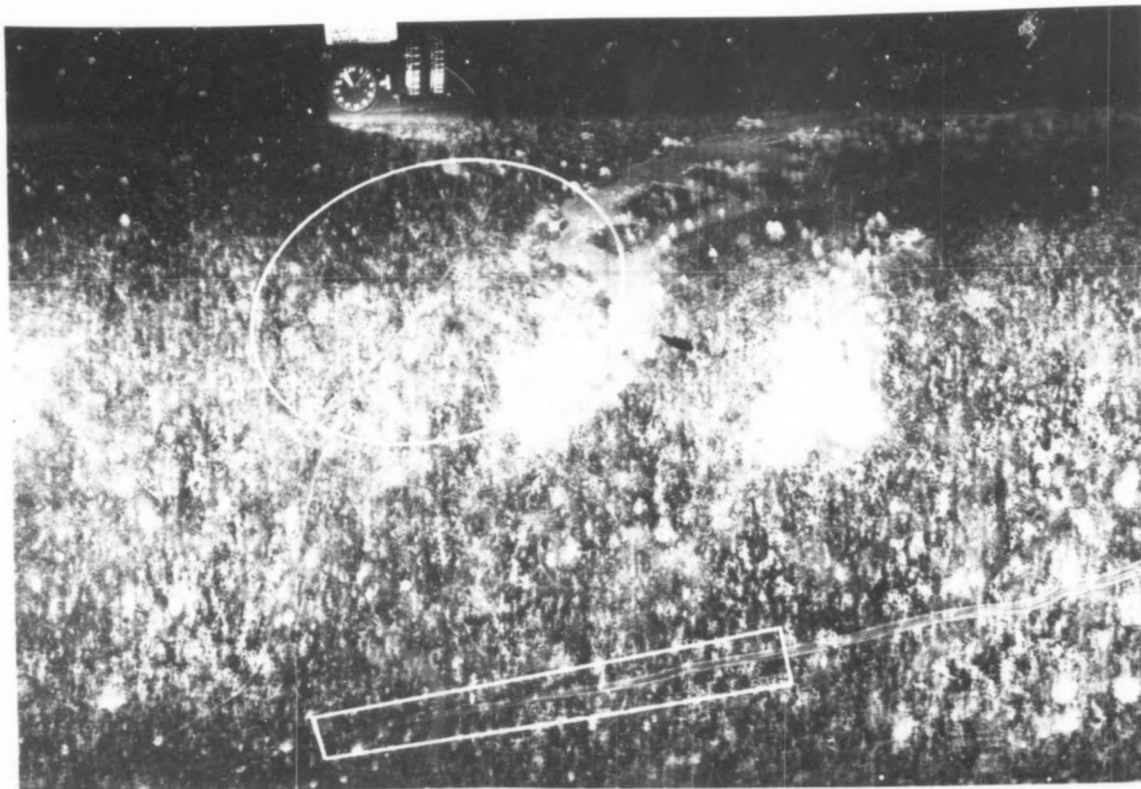
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 10
RUN 3
V/H 4

DATE: 2/17/66
TIME: 1427R
ALTITUDE: 190 ft
SPEED: 450 kn

AREA: Wright-Patterson Air Force Base, Ohio
TARGET: Aircraft on Patterson Field
WEATHER: Clear, visibility unlimited
DETECTORS: 5 Ge:Hg

FIGURE 27 - Flight Imagery of the Three IR Systems



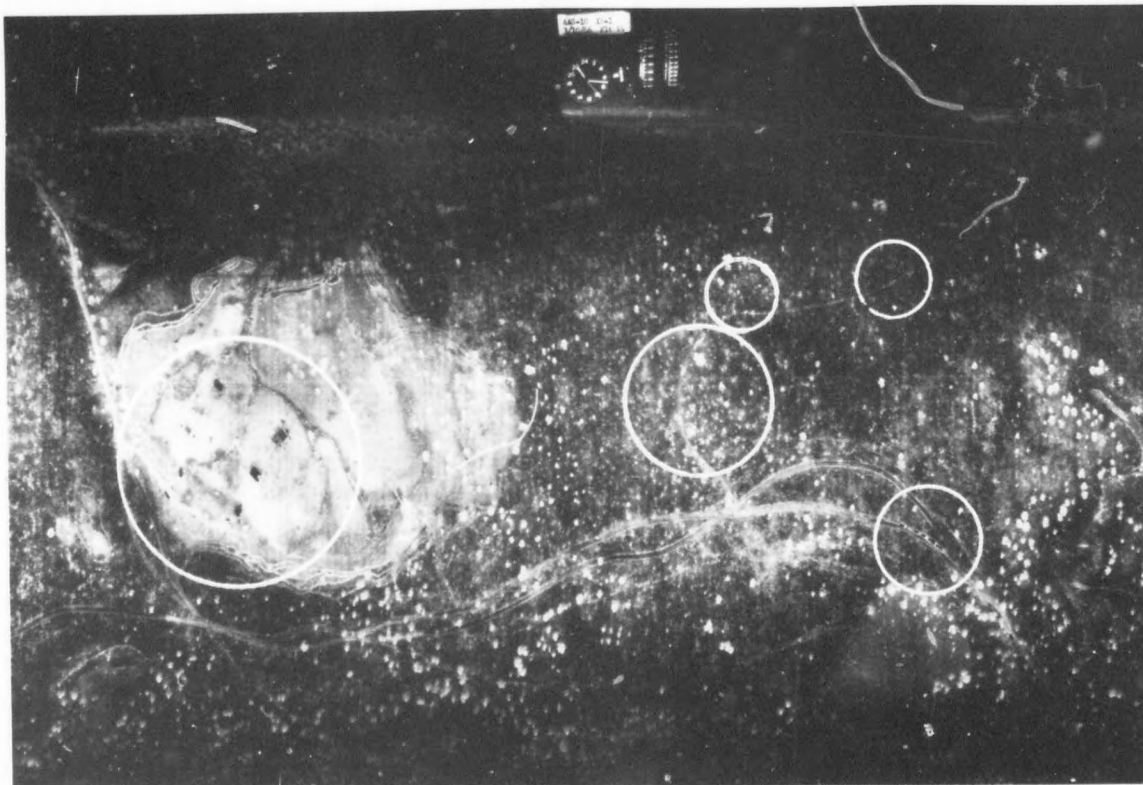
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 15
RUN 5
V/H 1

DATE: 3/10/66
TIME: 2055S
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: SAM site
WEATHER: Clear, visibility 7 miles
DETECTORS: 5 Ge:Hg

FIGURE 28 - Flight Imagery of the Three IR Systems



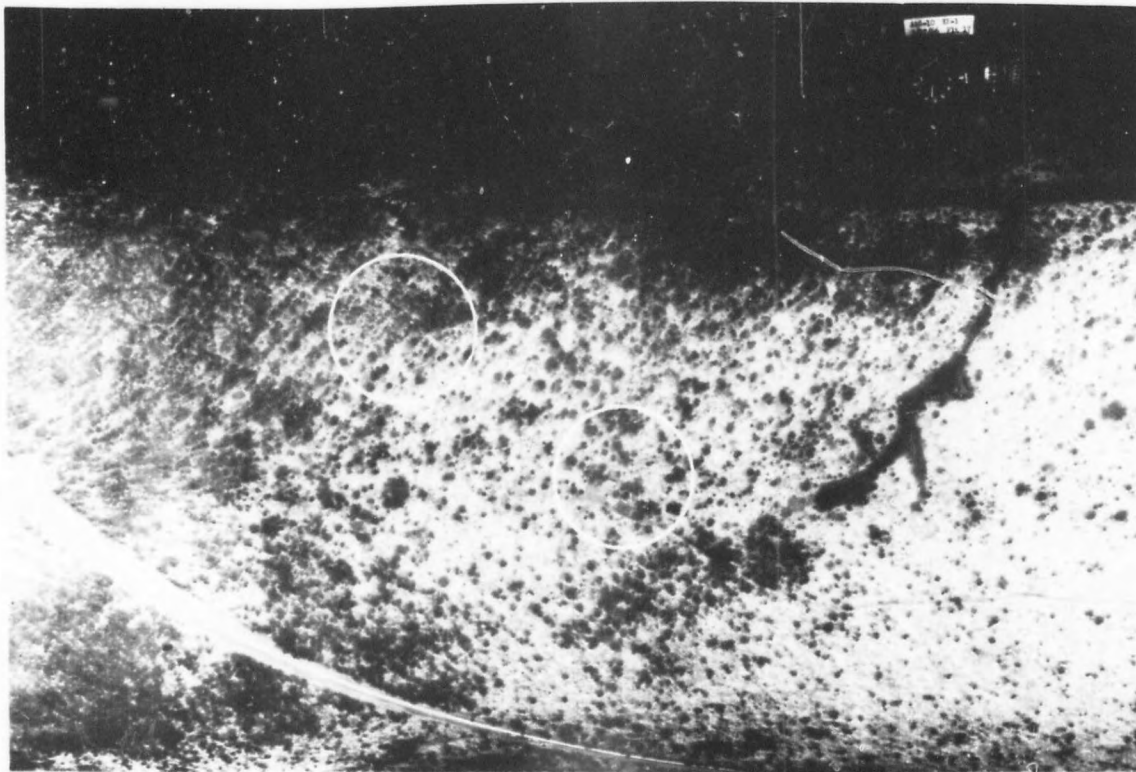
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 15
RUN 7
V/H 0.75

DATE: 3/10/66
TIME: 2117S
ALTITUDE: 750 ft
SPEED: 340 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site I Village complex
WEATHER: Clear, visibility 7 miles
DETECTORS: 5 Ge:Hg

FIGURE 29 - Flight Imagery of the Three IR Systems



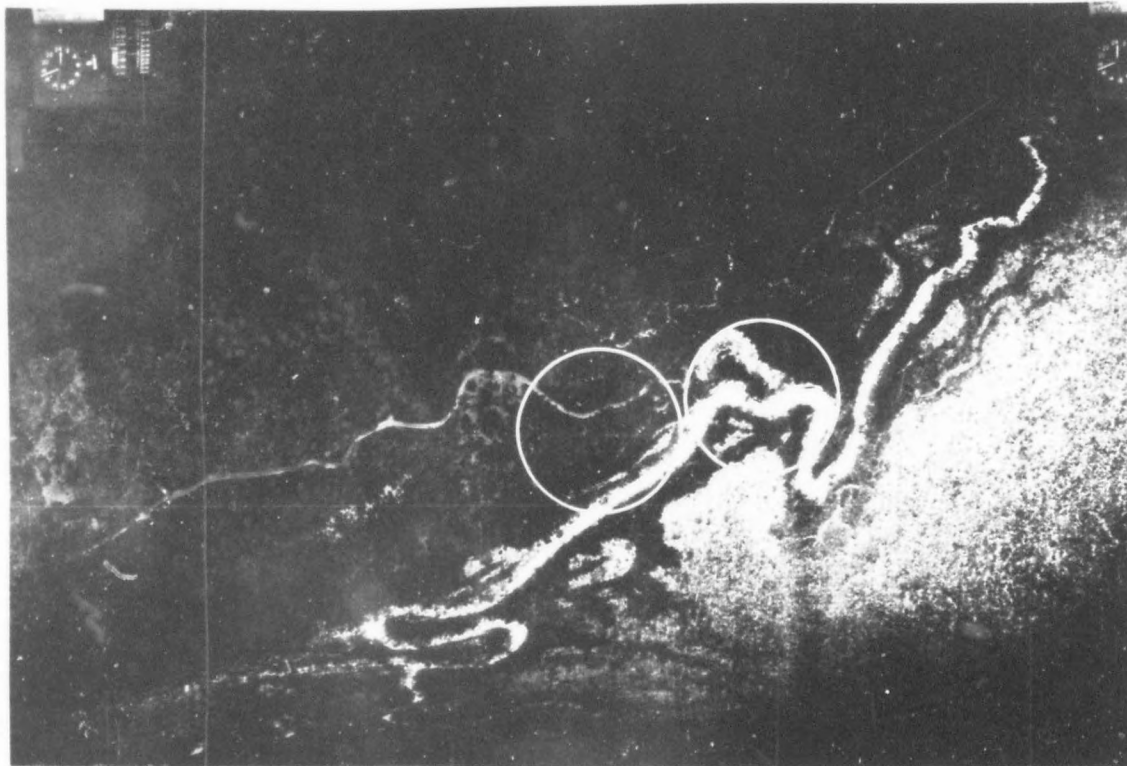
AN/AAS-10(XE-1)
FLIGHT 17
RUN 4
V/H 0.75

DATE: 3/17/66
TIME: 1225S
ALTITUDE: 670 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site II Village complex
WEATHER: Clear
DETECTORS: 5 Ge:Hg

FIGURE 30 - Flight Imagery of the Three IR Systems

NADC-AE-6718



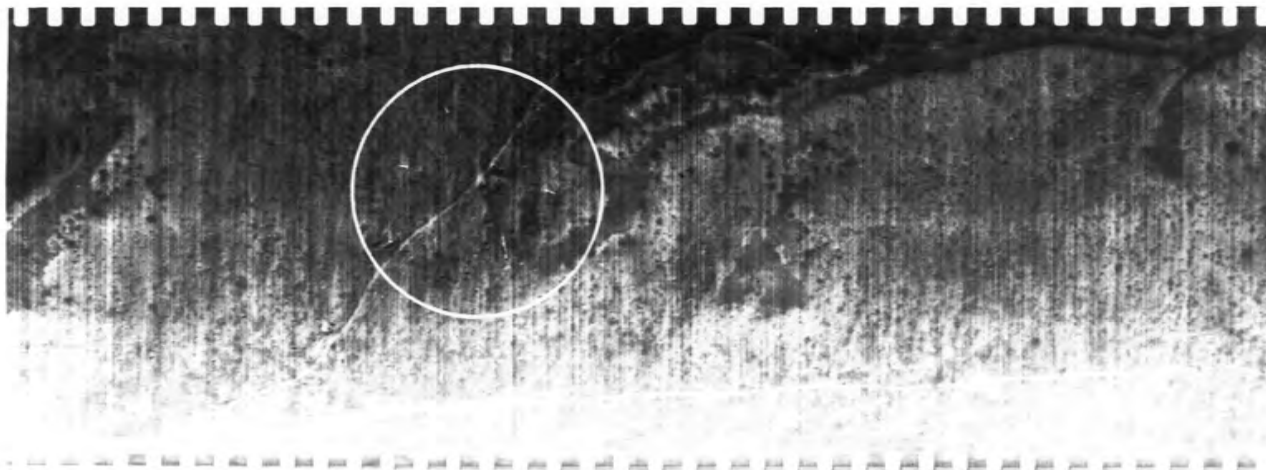
NADC-AE-6718

AN/AAS-10(XE-1)
FLIGHT 20
RUN 10
V/H 1

DATE: 3/25/66
TIME: 0043S
ALTITUDE: 750 ft
SPEED: 450 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site III Village complex and Sampans
WEATHER: Clear
DETECTORS: 5 Ge:Hg

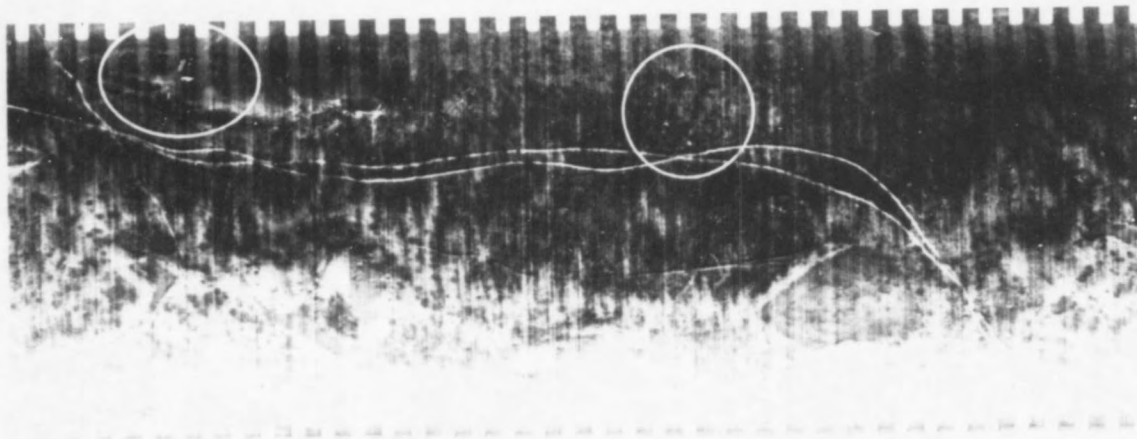
FIGURE 31 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX VI	DATE: 3/9/66	AREA: Eglin Air Force Base, Florida
FLIGHT 14	TIME: 1656S	TARGET: SAM Site
RUN 6	ALTITUDE: 670 ft	WEATHER: Clear
V/H 0.75	SPEED: 300 kn	DETECTORS: 1 Ge:Cu

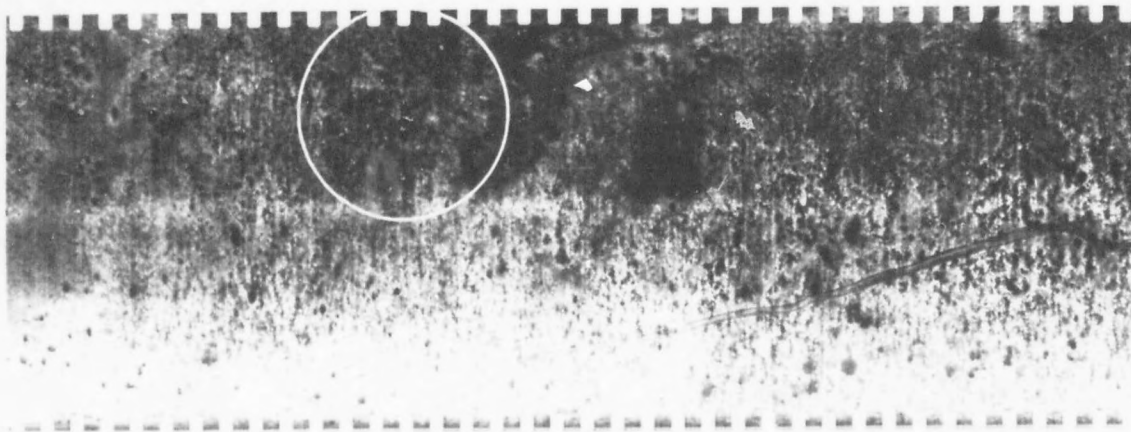
FIGURE 32 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX VI	DATE: 3/9/66	AREA: Eglin Air Force Base, Florida
FLIGHT 14	TIME: 1656S	TARGET: Site I Village complex
RUN 6	ALTITUDE: 670 ft	WEATHER: Clear
V/H 0.75	SPEED: 300 kn	DETECTORS: 1 Ge:Cu

FIGURE 33 - Flight Imagery of the Three IR Systems



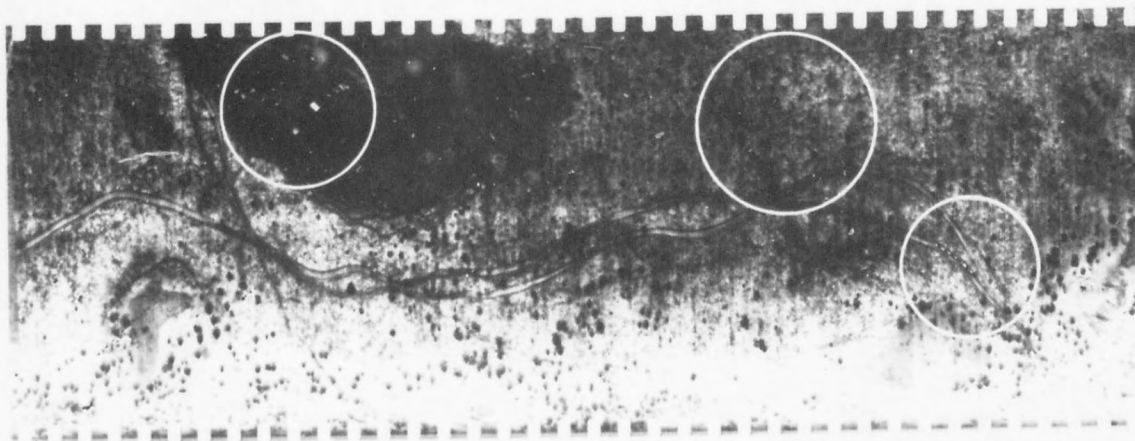
NADC-AE-6718

RECONOFAX VI
FLIGHT 15
RUN 5
V/H 1

DATE: 3/10/66
TIME: 2055S
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: SAM Site
WEATHER: Clear, visibility 7 miles
DETECTORS: 1 Ge:Cu

FIGURE 34 - Flight Imagery of the Three IR Systems



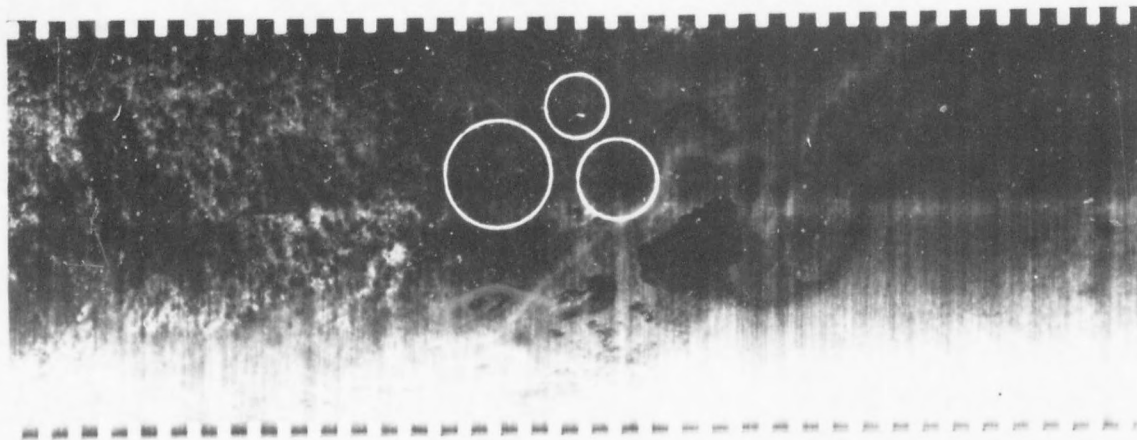
NADC-AE-6718

RECONOFAX VI
FLIGHT 15
RUN 5
V/H 1


DATE: 3/10/66
TIME: 2055S
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site I Village complex
WEATHER: Clear, visibility 7 miles
DETECTORS: 1 Ge:Cu

FIGURE 35 - Flight Imagery of the Three IR Systems



NADC-AE-6718

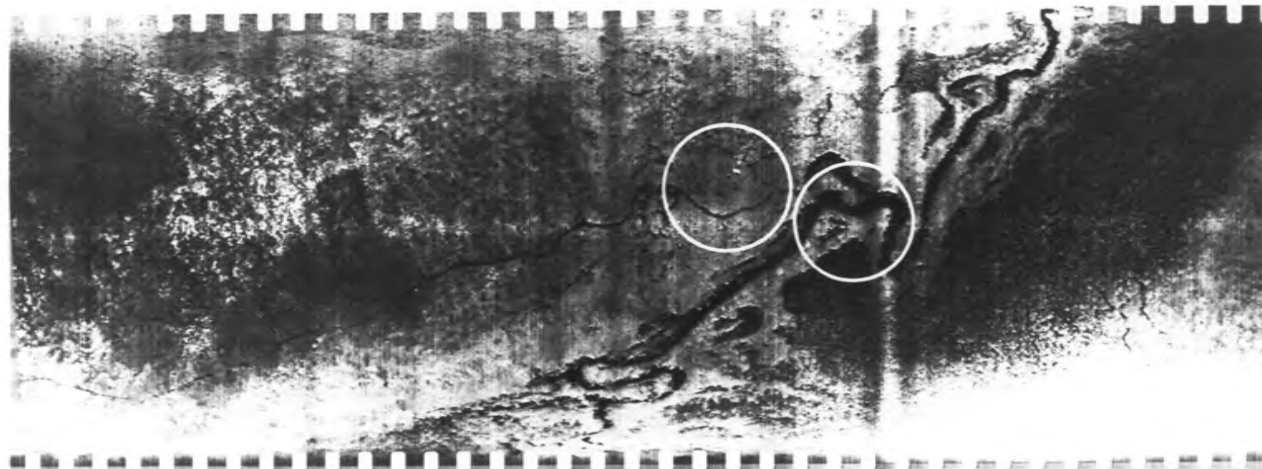


RECONOFAX VI
FLIGHT 18
RUN 7
V/H 1

DATE: 3/23/66
TIME: 1852S
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site III Village complex and sampans
WEATHER: 8K broken
DETECTORS: 1 Ge:Cu

FIGURE 36 - Flight Imagery of the Three IR Systems



NADC-AE-6718

RECONOFAX VI
FLIGHT 20
RUN 10
V/H 1

DATE: 3/25/66
TIME: 0043S
ALTITUDE: 750 ft
SPEED: 450 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site III Village complex and sampans
WEATHER: Clear
DETECTORS: 1 Ge:Cu

FIGURE 37 - Flight Imagery of the Three IR Systems

Reconofax IX

Figures 7 and 8 - All thermal resolution targets (12 in each direction) can be counted at maximum V/H during the day or night.

Figure 9 - Taxiing aircraft are easily identified at night at a V/H ratio of 2.

Figures 10 and 11 - Day and night presentations at higher than normal altitudes are illustrated.

Figure 12 - Representation of improved sensitivity in flight from NAVAIRDEVCCEN to Sanford, Florida, with the use of a new, single, element detector.

Figure 13 - A comparison check of performance with resolution targets at a different location (Eglin Air Force Base) and climate.

Figure 14 - Simulated Vietnam village at site I (light foliage). Huts, firepots, motorized vehicles, horse-drawn carts, and bicycle carts are easily seen; personnel and fox holes, 150 yards to the left and rimming the curved trail, are unidentifiable without prior knowledge of their locations. The same is true for the troop column at the end of this curved trail.

Figure 15 - Simulated SA-2 missile site is easily identified, including SAMS partially covered with foliage.

Figure 16 - Simulated Vietnam village at site III (dense foliage). Sampans along creek are discernible despite overhanging foliage. The fire pots about the village, and larger metal-roofed huts are detectable.

Figure 17 - Compares night flight over Aberdeen's static display of tanks and armored vehicles with previous day flight (figure 23). Site IV area was not available.

Figure 18 - Night photograph of the Fort Belvoir runway and hangar area with an assortment of light aircraft and helicopters and, interestingly, a steam line running under concrete from the hangar runway area to other buildings.

Figure 19 - Pontoon bridge building complex at Fort Belvoir. A new single-element detector was used in place of the seven-element array (figures 17, 18, and 19).

Because the contractor indicated that the copper-doped germanium detector array had insufficient thermal sensitivity, 12 additional flights of the Reconofax IX, with a new detector array (mercury-doped germanium) were conducted over NAVAIRDEVCCEN and Eglin Air Force Base. The evaluation of these flights appears in appendix D.

AN/AAS-10

Figures 20, 21, and 22 - Alternate flights over the Johnsville-Philadelphia area to supplement those cancelled because of bad weather. Figure 20 shows the mothball fleet at aircraft altitudes of 2000 feet. It is interesting to note that the arresting gear cables on the stern of the aircraft carrier Shangri-La can be counted. Figure 21 shows part of the NAF Johnsville area, hangar area, and a steam line (under concrete) running from the hangar area to the laboratory area at NAVAIRDEVGEN.

Figure 23 - Thermal resolution targets (hot and cold), gray scale and edge patterns seen at site IV.

Figure 24 - Tanks and tank tracks are visible throughout the entire area.

Figures 25a, 25b, 26a, and 26b - Thermal resolution targets during day and night operations.

Figure 27 - Although V/H was 4 times greater than the design parameter, resulting in compressed imagery, the runway number is distinguishable.

Figure 28 - All SAMS are easily detected, even those partially covered with foliage.

Figure 29 - Night imagery over site I for comparison with day imagery of same site (figure 14).

Figure 30 - Site II, simulated Vietnam village (medium foliage). Fire pots, large huts, and vehicles are easily detected. Horse-drawn carts, bicycle carts, small huts, fox holes, and troop columns are not discernible.

Figure 31 - Same flight run as figures 16 and 37.

Reconofax VI

Figures 32, 33, 34, and 35 - Compares day and night imagery obtained at site I.

Figure 36 - Presents a dusk flight over site III.

Figure 37 - Night imagery obtained over site III. Same flight run as figures 16 and 31.

SUMMARY OF RESULTS

1. Thermal sensitivity could not be calculated because of the coarse temperature differentials of the thermal targets.

2. Target imagery, used to calculate angular resolution, reveals a 1/3 mr to 1/2 mr loss of resolution caused by film duplication.

3. Operating tanks, armored vehicles, and trucks can be detected from an aircraft altitude of 2000 feet and identified from 1000 feet.

4. Horse drawn carts and bicycle carts can be detected from 750 feet and identified from 500 feet.

5. Large huts with metal roofs can be detected from aircraft altitudes of 2000 feet; small huts with thatched roofs are detectable from 750 feet.

6. Fire pots, sampans, and trails can be detected from aircraft altitudes of 2000 feet.

7. A troop column can be detected from aircraft altitudes of 500 feet.

8. Missile sites can be detected from aircraft altitudes of 1000 feet and identified at 500 feet.

The observations on the various types of targets are given with the understanding that foliage covering is light. When there is heavy foliage coverage, as at site III, Eglin Air Force Base, only the large huts with metal roofs, sampans, fire pots, and large vehicles (running) are detected.

A P P E N D I X A

AIRCRAFT INSTALLATION

Aircraft modifications and installation mounts for the AN/AAS-10(XE-1) and the Reconofax IX infrared mapping systems in an RA-3B aircraft were completed on schedule at the NAVAIRDEVCON. On 6 December 1965 an aerodynamic and safety test flight of the aircraft demonstrated that the performance of the aircraft was not affected by the modifications.

The Reconofax IX was installed in the aircraft on 5 January 1966 after HRB-Singer, Incorporated engineers performed a laboratory check-out of the equipment and instructed U. S. Navy crewmen on its inflight operation. Three checkout flights were conducted during 7-10 January 1966.

On 12 January 1966, the RA-3B aircraft was flown to NAS, Dallas, Texas, for the installation of the AN/AAS-10(XE-1). Texas Instruments, Incorporated personnel briefed the U. S. Navy crewmen on the inflight operation of this system and installed the equipment. A checkout flight was conducted 14 January 1966, and the aircraft returned to NAVAIRDEVCON on 15 January 1966.

A modified Reconofax VI mapping set, was acquired in late September 1965. Installation provisions for the modified Reconofax VI were made in the after-section of the aircraft in the position normally occupied by the AN/ARN-6 low-frequency radio compass antenna. The Reconofax VI was installed on 7 February 1966, and a checkout flight conducted on 10 February 1966.

Figures A-1 through A-6 show the aircraft installation of the AN/AAS-10(XE-1) and the Reconofax IX. Figures A-7 and A-8 illustrate the Reconofax VI installation.

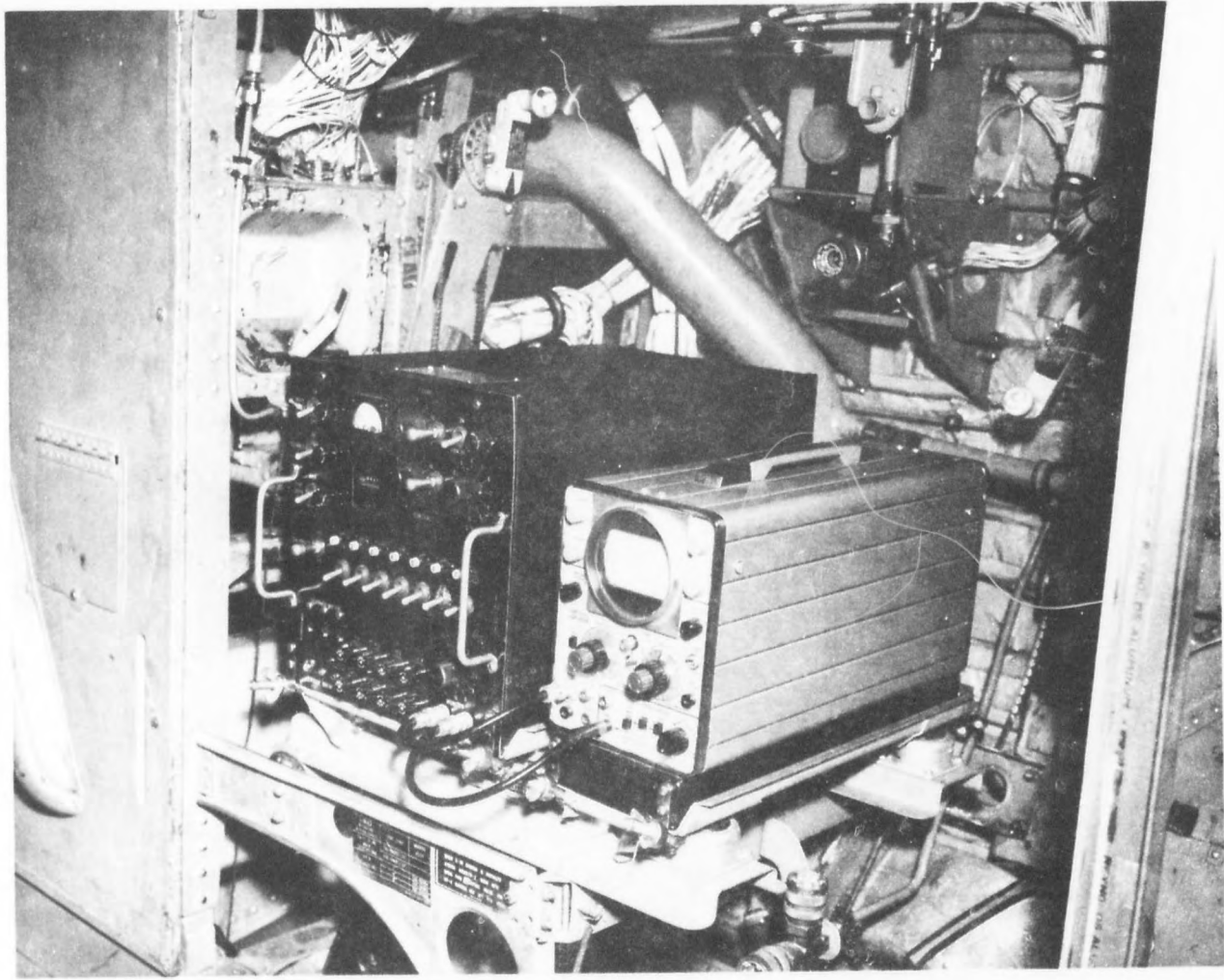
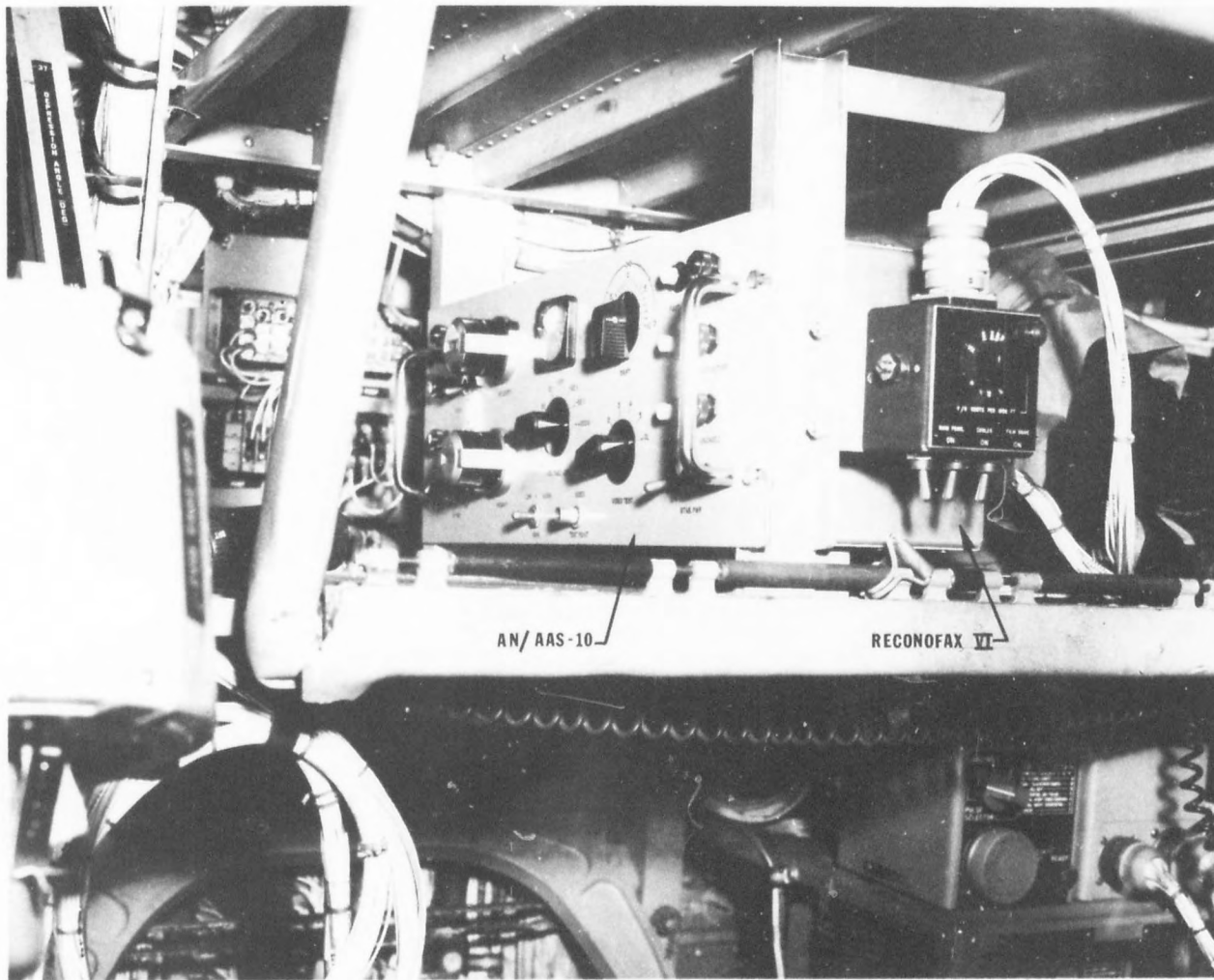


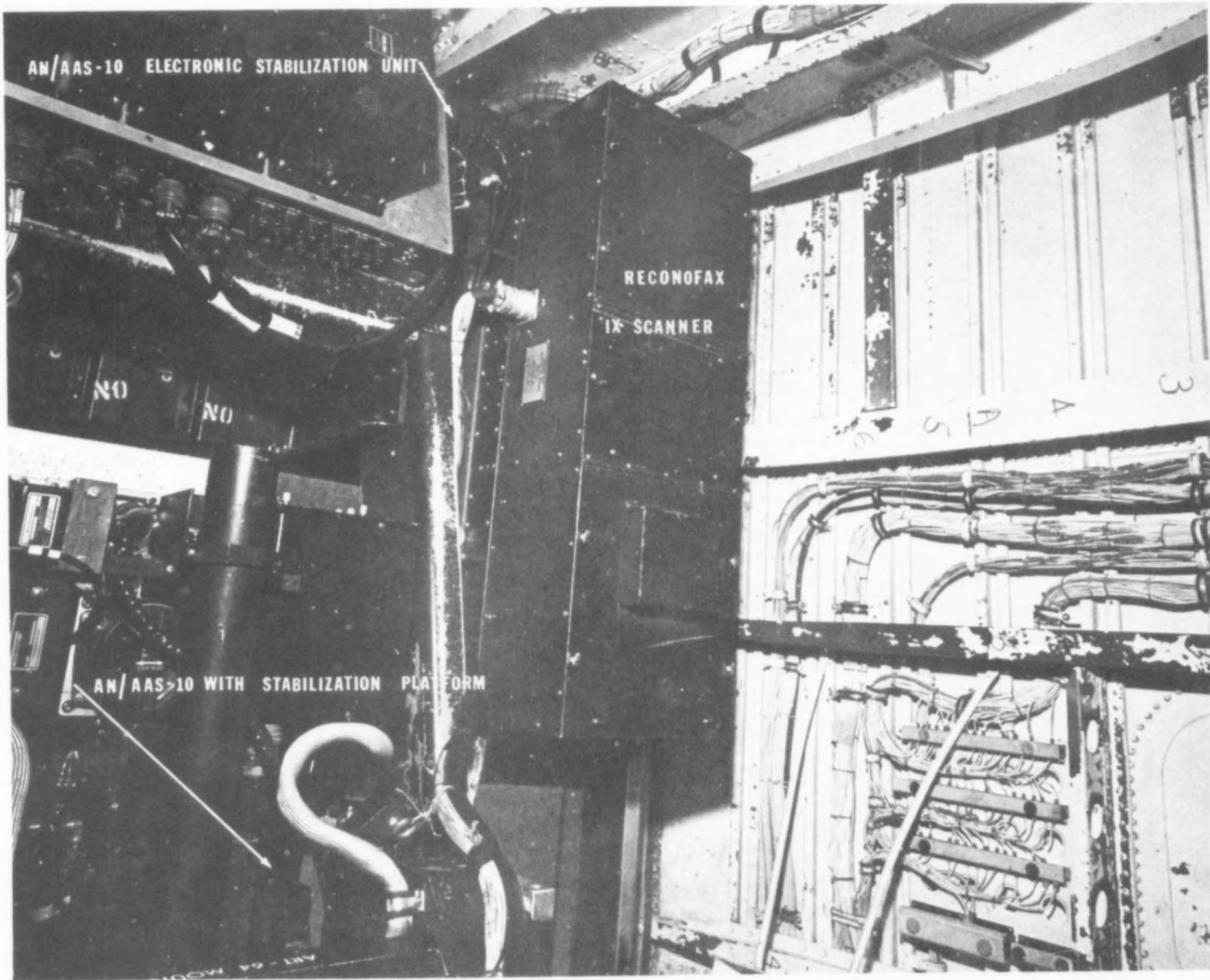
FIGURE A-1 - Reconofax IX Control Unit and Monitor Oscilloscope in Aircraft



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FIGURE A-2 - AN/AAS-10 and Reconofax VI Control Panels in Aircraft





- A-4 -

NADG-AE-6718

FIGURE A-3 - Reconofax IX and AN/AAS-10 in Aircraft Bomb Bay

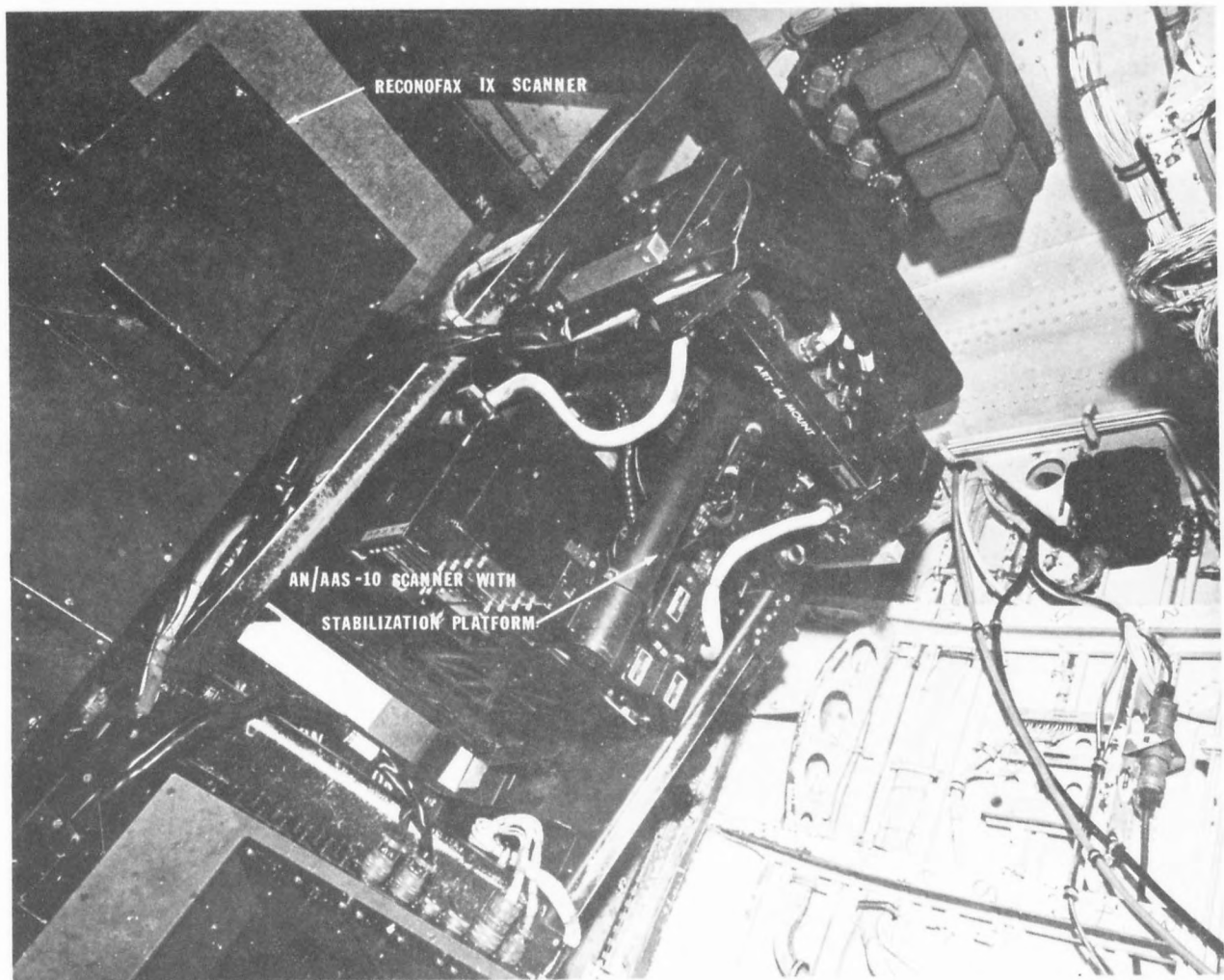


FIGURE A-4 - AN/AAS-10 and Reconofax IX in Aircraft Bomb Bay

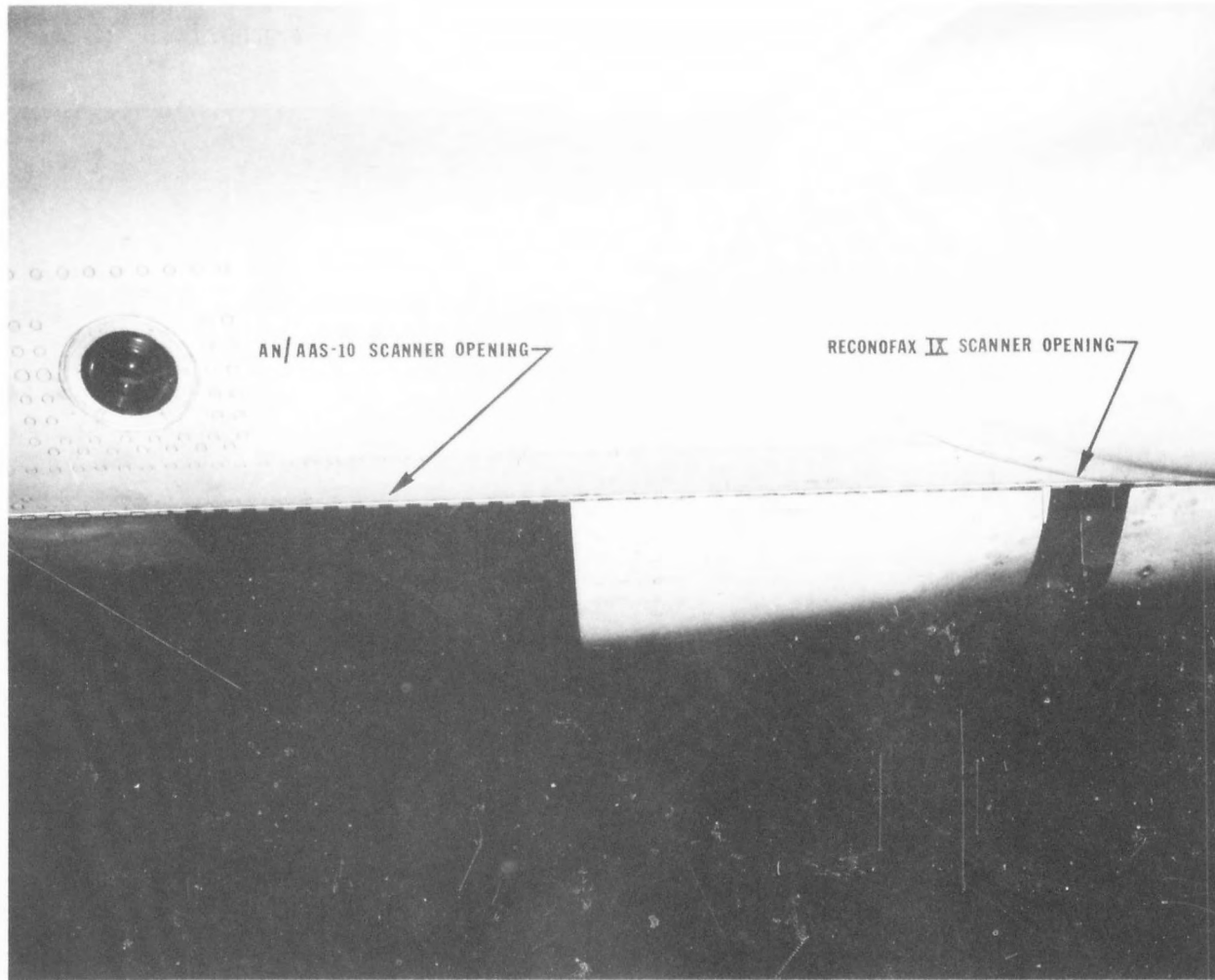
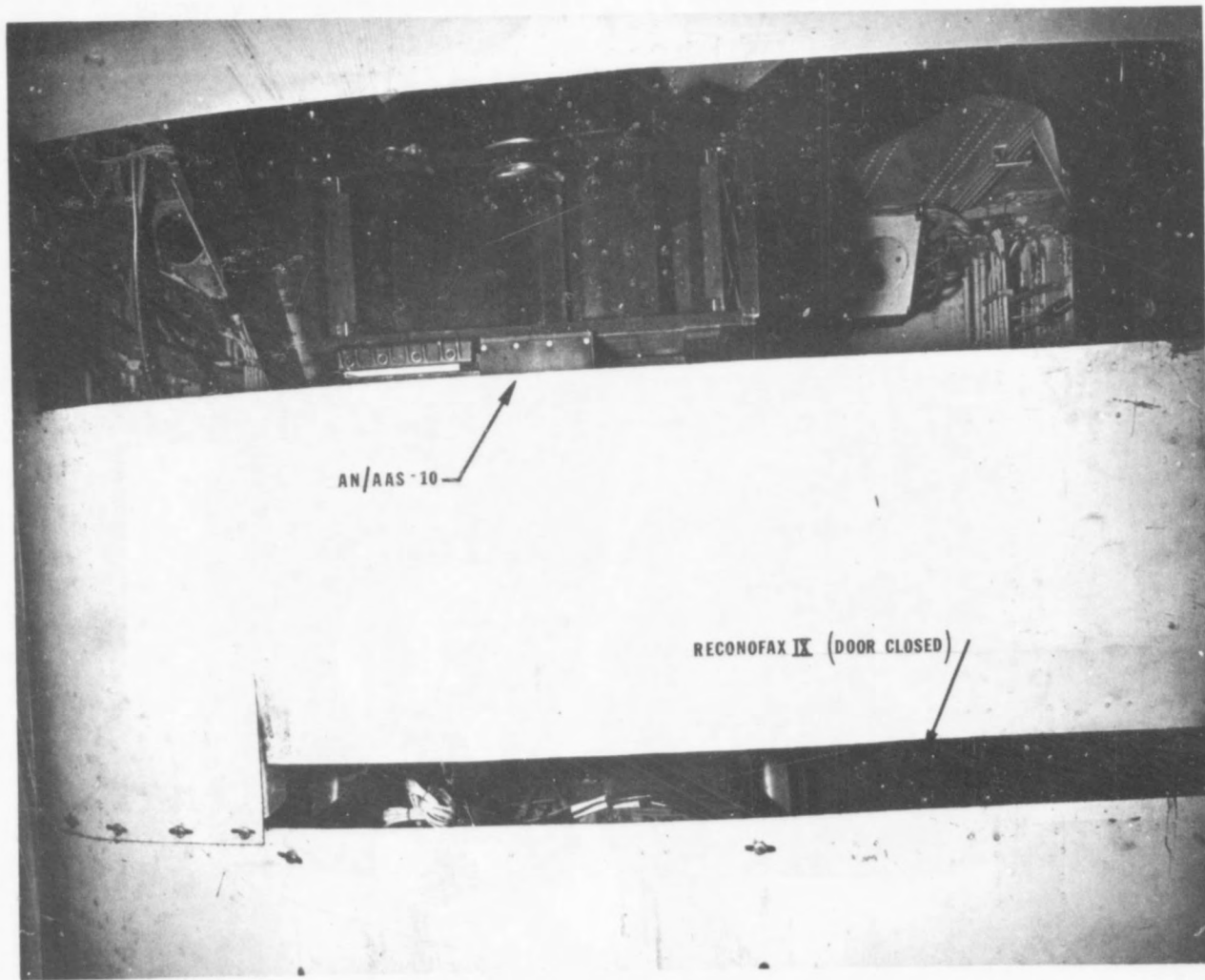


FIGURE A-5 - Modified Fairings and Openings in Aircraft Bomb Bay for IR Sets

CONFIDENTIAL

- A-7 -



NADC-AE-6718

FIGURE A-6 - Underside View of Aircraft Bomb Bay Showing Openings for IR Sets

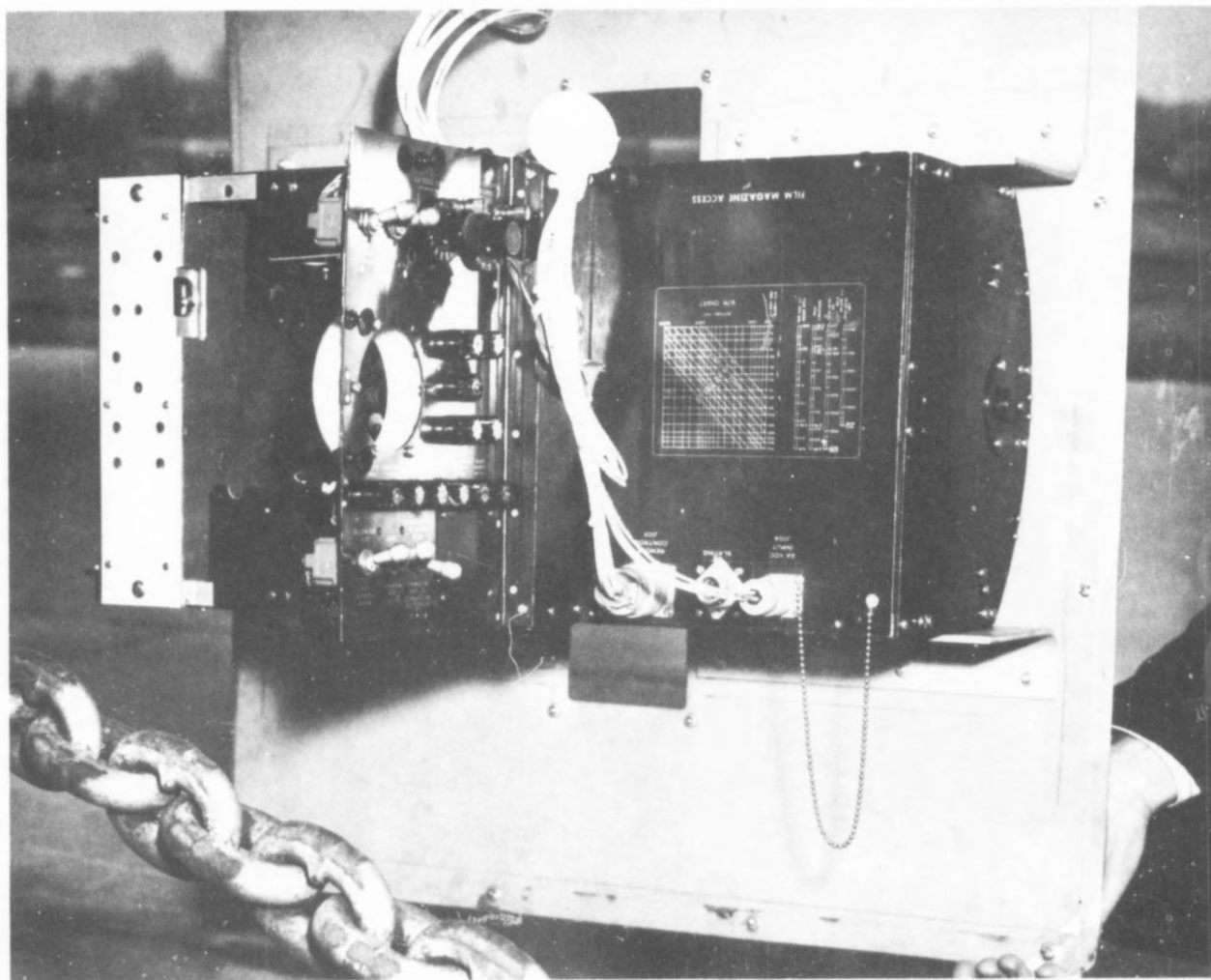
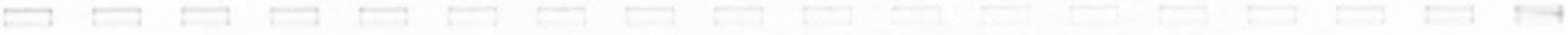
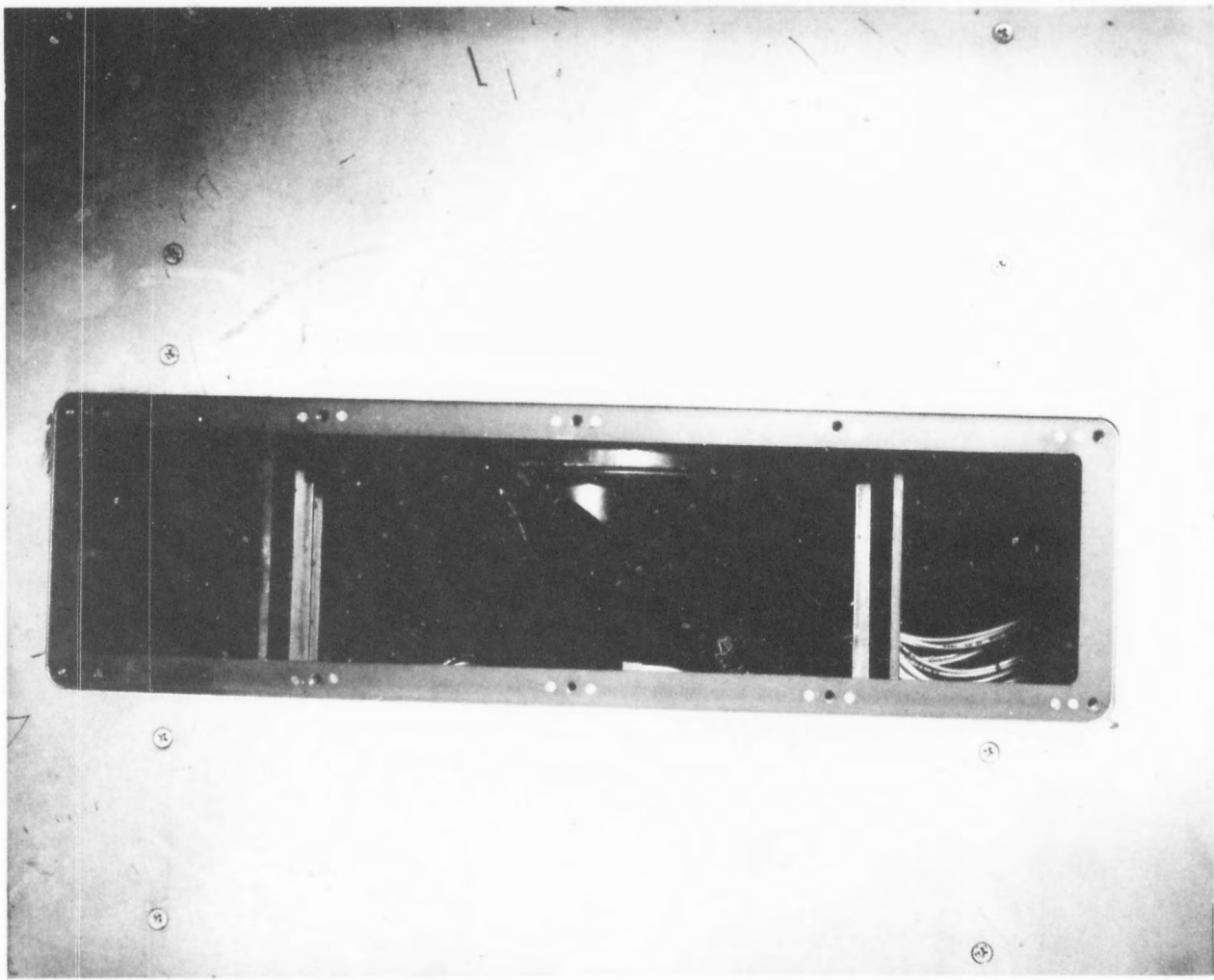


FIGURE A-7 - Reconofax VI Mounted on Aft Access Door of Aircraft
(Detector Dewar Removed and Door Opened)



- A-9 -

Da A 10 blank



[Redacted]

NADC-AE-6718

FIGURE A-8 - Underside View of Closed Access Door Showing Opening for Reconofax VI Scanner

A P P E N D I X B
FLIGHT EXERCISES AND COMMENTARY

Table B-I catalogues the date, flight time, target sites, and operating systems on the 28 "JANE TEN" flights conducted during January-March 1966 (including six checkout flights). The 22 test flights consisted of 1 dusk flight, 8 night flights, and 13 day flights; the check-out flights consisted of 1 night flight and 5 day flights.

Deficiencies encountered during the 22 test flights are summarized chronologically for the three infrared mapping systems.

Reconofax IX

Flights 1 through 4 - Loss of stabilization was caused by malfunction of reference coil in servo drive unit controlling mechanical linkages to stabilization platform. (Problem corrected for remaining flights.)

Flight 6 - Replaced Royal Pan film with Kodak 2475. (Marked improvement in processed film apparent.)

Flight 7 - Under-developed film - caused by impurities in the chemical mix and insufficient hot water at Wright-Patterson Air Force Base.

Flights 12 and 13 - Partial loss of imagery was caused by intermittent loss of video. (Ground short in insulation wire controlling +20 volts in scanner unit replaced.) Installed electric heaters in magazine before flight 14.

Flight 14 - Washed-out imagery resulted from misadjustment of detector(s) operation.

Flight 15 - Detectors were "inactive" because the detector dewar was not filled completely with liquid helium.

Flight 16 - Results obtained were good. Magazine pressure marks still present on imagery despite the installation of electric heaters in the magazine.

Flight 17 - Detectors became inactive after two target runs. (Replaced dewar because of suspected thermal leak. Also replaced three glow tubes.)

Flight 19 - Results were good despite the lack of automatic changing of the d-c level on cell No. 7 caused by a disengaged bound clutch in the d-c servo unit.

Flight 22 - A single element detector dewar, with a hold-time of 2 hours, did not permit the scheduled runs over the Washington, D. C. area.

AN/AAS-10(XE-1)

Flight 3 - Good imagery was obtained despite a bad glow tube. (Glow tube was replaced.)

Flight 4 - Lost two runs because of temperature instability of the drag switch controlling the magazine take-up reel. After this flight, the four microscope objective lenses were adjusted to maximize the recorder resolution. A vacuum leak in the closed-cycle cooler was repaired.

Flight 6 - Intermittent gating, caused by arcing in a glow tube, was observed in the film imagery.

Flight 7 - No imagery was obtained because the V/H control wire, linking the control unit with the scanner unit, was broken.

Flight 10 - Partial loss of imagery resulted from a bad glow tube. Excessive noise in one operating channel was caused by a defective capacitor (vibration breakdown) in the preamplifier.

Flight 11 - Transistor failure in the driver amplifier circuit (caused by a bad glow tube) resulted in the loss of several runs.

Flights 12 and 13 - Equipment was not operated because of suspected slippage of the banding filters in the optical system.

Flight 18 - Bad glow tubes permitted only one acceptable run.

Flight 19 - Bad glow tubes permitted only three acceptable runs.

Flight 20 - The film exhibited too little contrast caused by insufficient light from the glow tubes.

Flight 22 - A magazine jam caused the loss of two runs over Washington, D. C. area.

Reconofax VI

Flights 1 through 6 - Equipment was not installed in the aircraft.

Flights 7 through 13 - (before debugging) - Imagery obtained included the following faults: improper focus, faulty stabilization, ramping, striations caused by nonuniform film drive, and ineffective AGC.

Flights 14 through 22 - (after debugging) - Good results were achieved, and not a single target run was lost because of mechanical and/or electrical problems. Film imagery showed slightly too much contrast.

T A B L E B - I
INFRARED FLIGHT TEST PROGRAM SUMMARY

Flt No.	Date	Time (Approx)	Sites	EQUIPMENTS OPERATING			
				Reconofax IX	AN/AAS-10	Reconofax VI	Camera
C-1	7 Jan 66	1000-1200	Phila., parts of Del., Md. & N.J., NAVAIRDEVCON	x			
C-2	7 Jan 66	1745-1945	Same	x			
C-3	10 Jan 66	1200-1400	WPAFB	x			
C-4	14 Jan 66	1100-1200	Dallas, Texas		x		
1	20 Jan 66	1400-1600	Phila., Lakehurst, NAVAIRDEVCON	x	x		KA-45
2	20 Jan 66	1800-2000	Same	x	x		
3	21 Jan 66	1400-1600	Same	x	x		KA-45
4	24 Jan 66	1800-2100	WPAFB	x	x		
5	3 Feb 66	1430-1730	Aberdeen Proving Ground	x	x		
6	4 Feb 66	1230-1400	Same	x	x		KA-62
C-5	10 Feb 66	1400-1500	NAVAIRDEVCON			x	
7	12 Feb 66	1400-1600	WPAFB	x	x	x	
8	15 Feb 66	1300-1600	Fort Knox & WPAFB	x	x	x	

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TABLE B - I (continued)

Flt No.	Date	Time (Approx)	Sites	EQUIPMENTS OPERATING			
				Reconofax IX	AN/AAS-10	Reconofax VI	Camera
9	15 Feb 66	1900-2100	WPAFB	x	x	x	
10	17 Feb 66	1400-1600	Same	x	x	x	
11	17 Feb 66	1900-2100	Same	x	x	x	
12	18 Feb 66	1345-1500	Same	x		x	
13	18 Feb 66	1800-2000	Fort Knox & WPAFB	x		x	
C-6	5 Mar 66	1300-1500	NAVAIRDEVCCEN to NAS Sanford	x	x	x	
14	9 Mar 66	1630-1930	Eglin AFB, Simulated Vietnam villages	x	x	x	
15	10 Mar 66	2000-2330	Same	x	x	x	
16	11 Mar 66	1115-1515	Same	x	x	x	
17	17 Mar 66	1200-1415	Same	x	x	x	
18	23 Mar 66	1800-2100	Same	x	x	x	
19	24 Mar 66	1630-1915	Same	x	x	x	
20	25 Mar 66	0000-0300	Same	x	x	x	

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TABLE B - I (continued)

EQUIPMENTS OPERATING

Flt No.	Date	Time (Approx)	Sites	Reconofax IX	AN/AAS-10	Reconofax VI	Camera
21	28 Mar 66	1200-1430	APG, Ft. Belvoir, Washington, D.C.	x	x	x	
22	29 Mar 66	2000-2245	Same	x	x	x	

Flights C-1 through C-6 were equipment checkout flights

- B-5 -

Pg B-6 blank

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A P P E N D I X C

TARGET SITES

The following target sites were selected for the evaluation program:

NAVAIRDEVCCEN

Wright-Patterson Air Force Base

Aberdeen Target Range

Eglin Air Proving Ground

NAVAIRDEVCCEN

A variety of targets, utilized to determine the inflight spatial and thermal resolutions of infrared mapping systems, was placed adjacent to the runway. These targets included:

1. Two rows of blackened 300-watt light bulbs placed perpendicular to each other. The distances between the bulbs were not uniform.
2. A large photo-resolution chart
3. A 12 x 12-inch extended area, temperature controlled black body source
4. A dual-control electric blanket
5. An array of plywood panels of various sizes blackened on one side and aluminized on the other. For daytime operations, the blackened surfaces were placed up; for nighttime operations, the aluminized surfaces were exposed. These panels were spaced on the airfield at intervals equal to their widths, providing an array of grassy sections and blackened or aluminized sections.

Wright-Patterson Air Force Base

This site was chosen because of the multisensor target range available at Wright field. Layout of the thermal, geodetic, and resolution target arrays, together with the photographic edge, thermal resolution, high-to-low contrast, and gray scale target arrays are shown in figure C-1a. High V/H flights were permitted over Patterson Field only and the portable thermal resolution targets were located as shown in figure C-1b. Detailed descriptions of the multisensor target range at Wright-Patterson Air Force Base are given in Technical Report AFAL-TR-266.

Aberdeen Target Range

The Aberdeen target range consisted of four areas - outlined in figure C-2. Site I (along Access road) was an ordnance museum display of tanks and self-propelled guns, approximately 45 items. Site II was an ordnance museum display of foreign equipment, approximately 30 tanks and 45 field artillery pieces. Site III was an ordnance museum display of field artillery and missiles, approximately 34 items. Site IV was a special display of current equipment (approximately 37 items) including tanks, armored personnel carriers, field artillery, and rocket launchers. The latter site was most important because many motorized vehicles were operating, and it contained hot and cold resolution targets, gray scale, and edge targets.

Eglin Air Proving Ground

The target arrays at Eglin Air Proving Ground included three simulated Vietnam villages under varying degrees of terrain cover, a simulated Soviet SA-2, a surface-to-air missile complex, and sampans in nearby rivers. The targets were moved and/or changed once per week. The operation schedule of the sites were:

Site I (figure C-3a) - active 7-11 March 1966 (sparsely covered terrain)

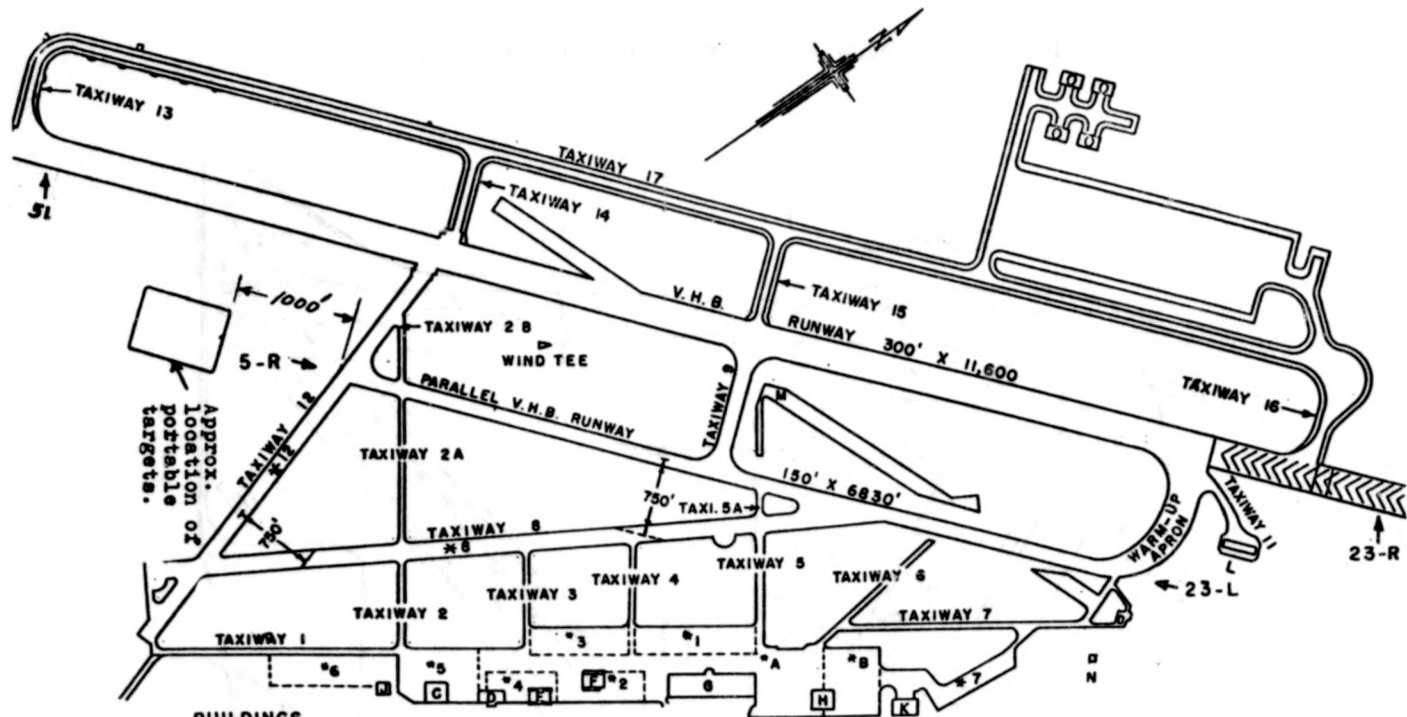
Site II (figure C-3b) - active 14-18 March 1966 (medium covered terrain)

Site III (figure C-3c) - active 21-25 March 1966 (heavy covered terrain)

The simulated Vietnam villages included huts with metal, canvas, and thatched roofs; personnel, carts, bicycles, fire pots, fox holes, mortars, horses, and vehicle convoys. In addition, optical and infrared resolution targets were placed near the target area.

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- C-4 -



- BUILDINGS**
- C- SHOPS, -OFFICES
 - D- WOOD HANGAR
 - E- BLACK ■
 - F- STEEL ■
 - G- OPERATIONS, - HANGAR
 - H- TERMINAL
 - J- INSTRUMENT SCHOOL
 - K- READINESS HANGAR
 - L- ALERT ■
 - M- G. C. A. SITE
 - N- ROCKET STORAGE CHECK-OUT
 - O- HANGARS

- PARKING ZONES**
- *A, *B, *1,
 - *2, *3, *4,
 - *5, *6, *7,
 - *8 *12



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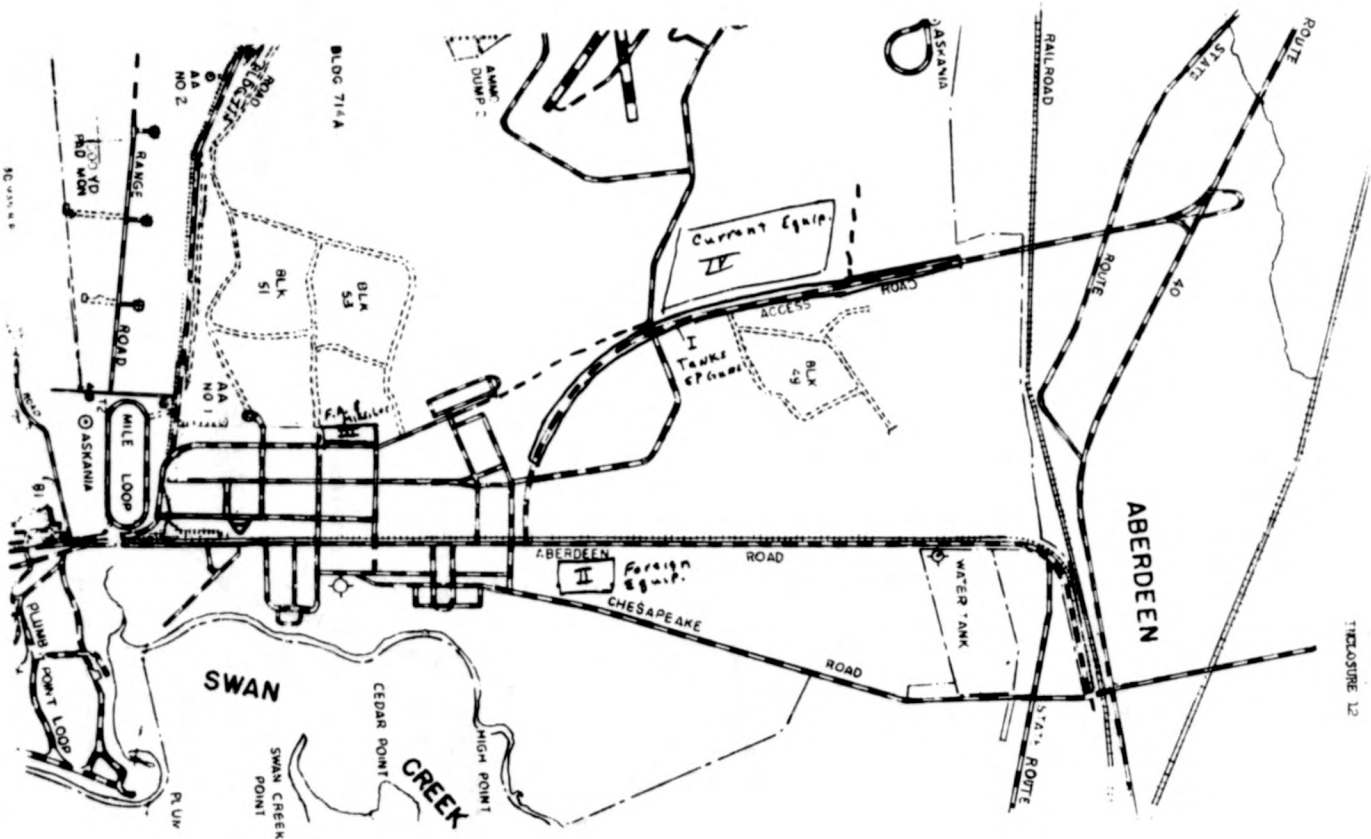


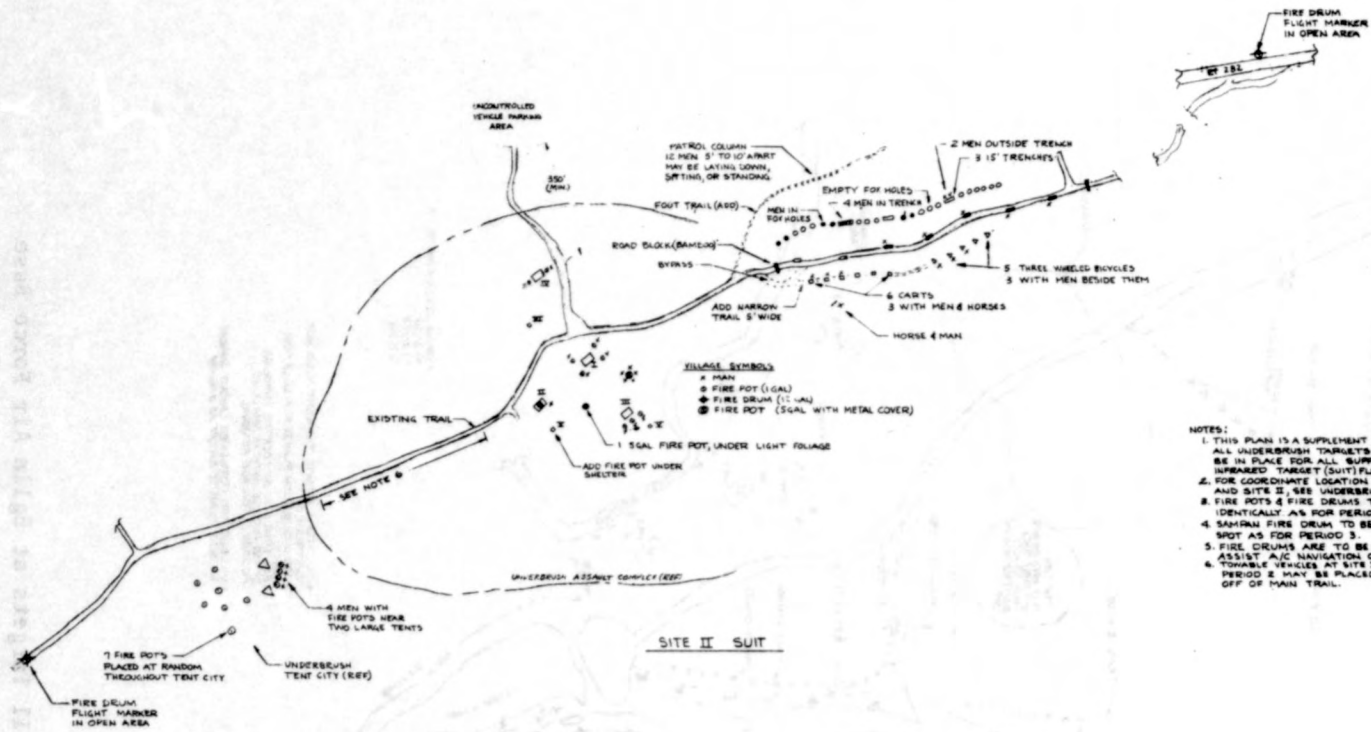
FIGURE C-2 - Location of Four Test Sites at Aberdeen Proving Ground

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- NOTES:
1. THIS PLAN IS A SUPPLEMENT TO UNDERBRUSH PLAN II. ALL UNDERBRUSH TARGETS (EXCEPT WEAPONS) WILL BE IN PLACE FOR ALL SUPPLEMENTED UNDERBRUSH INCREASED TARGET (SUIT) FLIGHTS.
 2. FOR COORDINATE LOCATION OF SAMRANS, SAM SITE, AND SITE II, SEE UNDERBRUSH PLAN II.
 3. FIRE POTS & FIRE DRUMS TO BE MAINTAINED IDENTICALLY AS FOR PERIOD 3, SUIT PLAN II.
 4. SAMRAN FIRE DRUM TO BE LOCATED AT SAME SPOT AS FOR PERIOD 3.
 5. FIRE DRUMS ARE TO BE LIT AS REQUIRED TO ASSIST A/C NAVIGATION OVER TARGET AREA.
 6. TOWABLE VEHICLES AT SITE II FOR UNDERBRUSH PERIOD 2 MAY BE PLACED IN THIS AREA, JUST OFF OF MAIN TRAIL.

c3b

FIGURE C-3b - Site II Targets at Eglin Air Force Base

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A P P E N D I X D

RECONOFAX IX SUPPLEMENTARY FLIGHT EVALUATION
(MERCURY-DOPED GERMANIUM (Ge:Hc) DETECTORS)

INTRODUCTION

After the original evaluation of the Reconofax IX Infrared Mapping Set, the equipment manufacturer, H. R. B. Singer, Incorporated, claimed that the IR imagery could be enhanced by replacing the relatively old copper-doped germanium (Ge:Cu) detector array with a new mercury-doped germanium (Ge:Hg) detector array. Cognizant Air Force and Navy personnel agreed to conduct several supplementary test flights during September 1966 over the Eglin Air Force Base IR Test Range in the same Navy RA-3B aircraft. The location and type of ground targets at the Eglin Range are identical to those outlined in appendix C.

EVALUATION AND RESULTS

A total of twelve flights were flown; the first five were conducted in the local Johnsville area and considered "shake-down" flights for the equipment. The remaining seven flights, upon which this evaluation is based, were conducted over the Eglin Air Force Base IR Test Range. The date, time, flight number and site location of all these supplementary flights are summarized in table D-I.

A comparison of the seven-element detector arrays (Ge:Hg versus Ge:Cu) includes an evaluation of the following:

Thermal and Angular Resolution - There were no suitable thermal resolution targets at Eglin or Johnsville to obtain quantitative thermal sensitivity measurements. Imagery over the Johnsville IR targets, obtained during the shake-down flights of the Ge:Hg detector array, indicated that the angular resolution was the same (1.5-2.0 mr) as that previously measured for the Ge:Cu detector array.

Flight Imagery - Figures D-1 through D-5 show day and night flight imagery over various types of targets at different altitudes (190 to 3000 ft) and speeds (300 to 450 kn). This imagery substantiates the earlier results enumerated in the main body of this report; i.e. tactical targets such as trucks, missiles, sampans, village huts, and fire pots can be detected and/or identified at certain altitudes, limited by the denseness of the ground foliage and thermal intensity of the targets.

Velocity-to-Height Ratio - The new detector array (Ge:Hg) did not affect the V/H capability of the equipment. Twelve daytime runs were conducted to verify this fact. However, during flight No. 8, it was discovered that one of the detector elements was defective, causing some degradation to the imagery (figure D-6).

Video Contrast Levels - To insure that flight imagery would be enhanced, the video contrast levels were changed on alternate runs (of flight No. 10) from settings of 8-10 v peak-to-peak to 10-12 v peak-to-peak. Since no apparent improvement was observed with either setting, the original setting (8-10 v peak-to-peak) was utilized for the remaining flights.

CONCLUSIONS

There was no significant overall improvement in the imagery obtained with the Ge:Hg detector array. The night imagery was slightly improved over the Ge:Cu detector array, while the daytime imagery was slightly worse.

Since these detector arrays (Ge:Hg and Ge:Cu) were not compared during simultaneous flights and many variables (time of year, weather conditions, etc.) cannot be correlated, it appears that neither detector array has an advantage over the other.

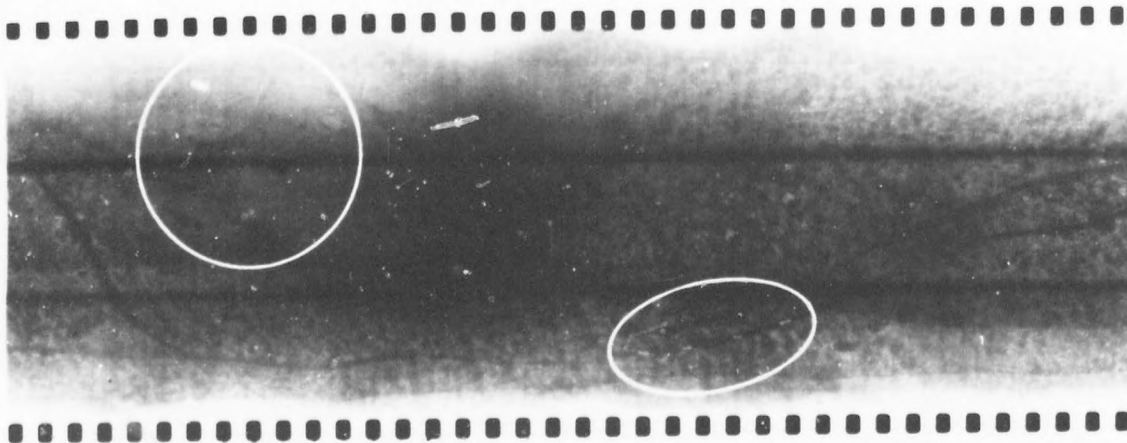
RECOMMENDATIONS

Since the Ge:Hg detector array is readily adaptable to closed-cycle cooling (a logistic advantage), it would be recommended in view of its equal performance to the Ge:Cu detector array.

T A B L E D - I

INFRARED FLIGHT TEST PROGRAM SUMMARY
RECONOFAX IX SUPPLEMENTARY FLIGHTS

Flt No.	Date	Time (Approx)	Sites
S-1	26 Aug 1966	1115-1230Q	NAVAIRDEVCEN Johnsville, Philadelphia area
S-2	29 Aug 1966	1430-1545Q	NAVAIRDEVCEN infrared target range
S-3	30 Aug 1966	1045-1200Q	NAVAIRDEVCEN infrared target range
S-4	30 Aug 1966	2030-2230Q	Aberdeen Proving Ground, Md. and NAVAIRDEVCEN infrared target range
S-5	2 Sep 1966	1000-1145Q	Philadelphia and Wilmington areas and NAVAIRDEVCEN infrared target range
S-6	7 Sep 1966	1300-1530R	Eglin AFB, Simulated Vietnam village - Site I
S-7	8 Sep 1966	2015-2245R	Eglin AFB, Simulated Vietnam village - Site I
S-8	12 Sep 1966	0900-1200R	Eglin AFB, Simulated Vietnam village - Site II
S-9	12 Sep 1966	2000-2215R	Eglin AFB, Simulated Vietnam village - Site II and missile site
S-10	13 Sep 1966	2015-2300R	Eglin AFB, Simulated Vietnam village - Site II and missile site
S-11	14 Sep 1966	0600-0845R	Eglin AFB, Simulated Vietnam village - Site III, Site II (inactive) and missile site
S-12	14 Sep 1966	2015-2300R	Eglin AFB, Simulated Vietnam village - Site III, Site II (inactive) and missile site



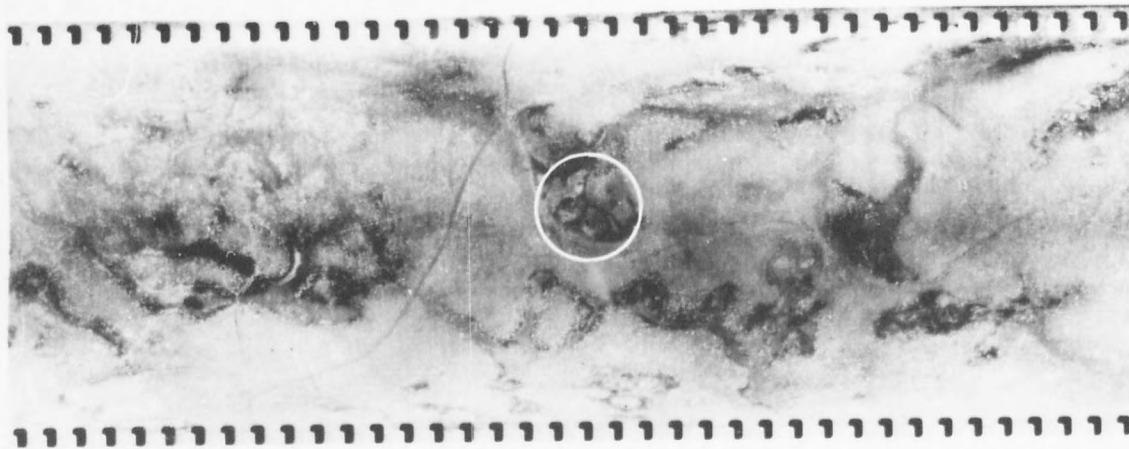
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RECONOFAX IX
FLIGHT 6
RUN 4
V/H 3

DATE: 9/7/66
TIME: 1327S
ALTITUDE: 250 ft
SPEED: 450 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site I complex
DETECTORS: GE:HG #1, 2, 3, 5, 6, 7

FIGURE D-1 - Flight Imagery Using GE:HG Detector Array



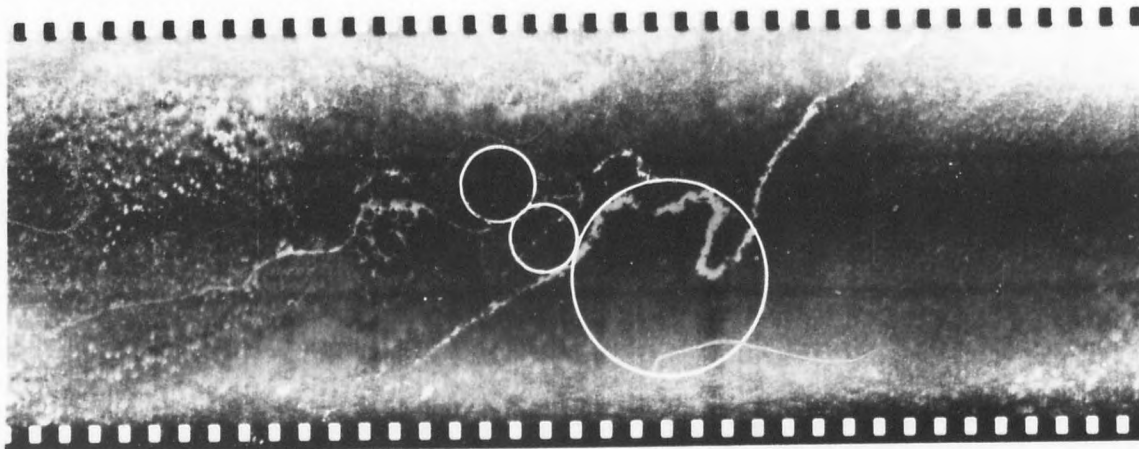
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RECONOFAX IX
FLIGHT 7
RUN 2B
V/H 0.25


DATE: 9/8/66
TIME: 2015S
ALTITUDE: 2000 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site I complex
DETECTORS: GE:HG #1

FIGURE D-2 - Flight Imagery Using GE:HG Detector Array



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RECONOFAX IX
FLIGHT 12
RUN 4
V/H 1

DATE: 9/14/66
TIME: 2034S
ALTITUDE: 500 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site III complex and sampans
DETECTORS: GE:HG #1, 7

FIGURE D-3 - Flight Imagery Using GE:HG Detector Array

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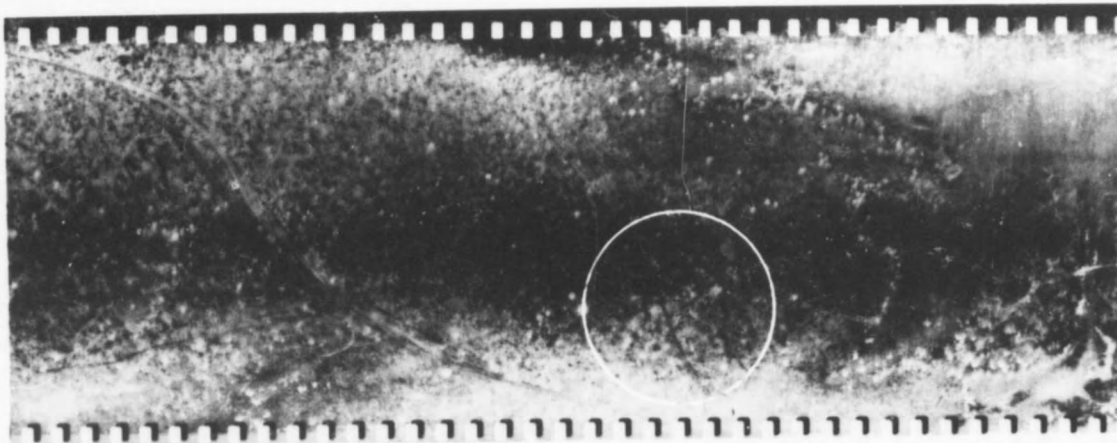
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RECONOFAX IX
FLIGHT 12
RUN 2
V/H 0.33

DATE: 9/14/66
TIME: 2018S
ALTITUDE: 1500 ft
SPEED: 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: Site III complex and sampans
DETECTORS: GE:HG #1

FIGURE D-4 - Flight Imagery Using GE:HG Detector Array



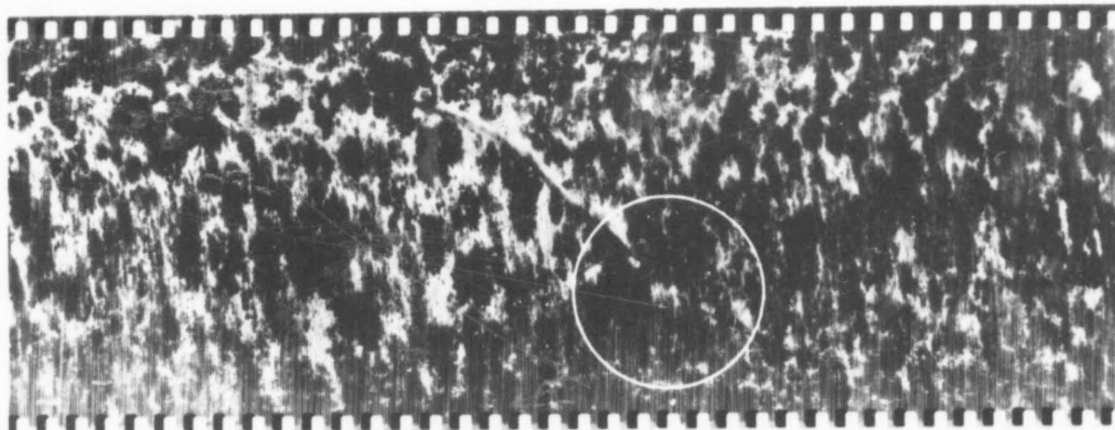
NADC-AE-6718

RECONOFAX IX
FLIGHT 12
RUN 4
V/H 1

DATE: 9/14/66
TIME: 2034S
ALTITUDE 500 ft
SPEED 300 kn

AREA: Eglin Air Force Base, Florida
TARGET: SAM Missile complex
DETECTORS: GE:HG #1, 7

FIGURE D-5 - Flight Imagery Using GE:HG Detector Array



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RECONOFAX IX
FLIGHT 8
RUN 6
V/H 4

DATE: 9/12/66
TIME: 0940S
ALTITUDE: 190 ft
SPEED: 450 kn

AREA: Eglin Air Force Base, Florida
TARGET: Vehicles Site II complex
DETECTORS: All seven GE:HG

FIGURE D-6 - Flight Imagery Using GE:HG Detector Array

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	2b. GROUP 4

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FLIGHT EVALUATION AND ANALYSIS OF AN/AAS-10(XE-1), RECONOFAX VI AND RECONOFAX IX INFRARED MAPPING SETS (U)

4. DESCRIPTIVE NOTES (Type of report and, inclusive dates)
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5. AUTHOR(S) (First name, middle initial, last name)
L. B. JUDGE

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11. SUPPLEMENTARY NOTES	12. SPONSORING MILITARY ACTIVITY NAVAL AIR SYSTEMS COMMAND DEPARTMENT OF THE NAVY
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13. ABSTRACT
Three experimental infrared mapping systems, the U. S. Air Force Reconofax IX, U. S. Army AN/AAS-10(XE-1), and the U. S. Navy Reconofax VI, were flight-tested simultaneously on RA-3B aircraft, BuNo. 144839. Control ground targets and targets of opportunity were used. The three systems met their respective primary design specifications, but each system has shortcomings that need to be improved before service use. Recommendations are included for further development of infrared mapping systems. (U)

4.

KEY WORDS

LINK A

LINK B

LINK C

ROLE

WT

ROLE

WT

ROLE

WT

INFRARED
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EVALUATION
ANALYSIS

NAVAL AIR DEVELOPMENT CENTER, JOHNSVILLE, PA.
AERO-ELECTRONIC TECHNOLOGY DEPARTMENT
(REPORT NO. NADC-AE-6718)

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60, 10, 6, 8, AND 10 P. FINAL REPORT.

INCLUDES APPENDIXES.

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THE U. S. AIR FORCE RECONOFAX IX, U. S. ARMY
AN/AAS-10(XE-1), AND THE U. S. NAVY RECONOFAX

1. INFRARED
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 3. EVALUATION
 4. ANALYSIS
1. JUDGE, L.

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1. JUDGE, L.

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NO. 1
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VI, WERE FLIGHT-TESTED SIMULTANEOUSLY ON RA-3B AIRCRAFT, BU NO. 144839. CONTROL GROUND TARGETS AND TARGETS OF OPPORTUNITY WERE USED. THE THREE SYSTEMS MET THEIR RESPECTIVE PRIMARY DESIGN SPECIFICATIONS, BUT EACH SYSTEM HAS SHORTCOMINGS THAT NEED TO BE IMPROVED BEFORE SERVICE USE. RECOMMENDATIONS ARE INCLUDED FOR FURTHER DEVELOPMENT OF INFRARED MAPPING SYSTEMS.

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