

Directional Current Probe Measurements in Multipactor Breakdown

October 16, 2018

Aimee A. Hubble and Matthew S. Feldman
Propulsion Science Department
Space Materials Laboratory

Prepared for:

Space and Missile Systems Center
Air Force Space Command
483 N. Aviation Blvd.
El Segundo, CA 90245-2808

Contract No. FA8802-19-C-0001

Authorized by: Engineering and Technology Group

Distribution Statement A: Approved for public release; distribution unlimited.



This report was submitted by The Aerospace Corporation, El Segundo, CA 90245-4691, under Contract No. FA8802-19-C-0001 with the Space and Missile Systems Center, 483 N. Aviation Blvd., El Segundo, CA 90245. It was reviewed and approved for The Aerospace Corporation by Charles L. Gustafson, Senior Vice Principal, Engineering and Technology Group. Davis I. Choi was the project officer for the SMC/PIM program.

This report has been reviewed by the Public Affairs Office (PAS) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nationals.

This technical report has been reviewed and is approved for publication. Publication of this report does not constitute Air Force approval of the report's findings or conclusions. It is published only for the exchange and stimulation of ideas.

Approval in Other Supporting Files, 06/05/2019.

Davis I. Choi
GG-14, SMC/PIM

All trademarks, service marks, and trade names are the property of their respective owners.

REPORT DOCUMENTATION PAGE			<i>Form Approved</i> <i>OMB No. 0704-0188</i>		
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing this collection of information. Send comments regarding this burden, estimate or any other aspect of this collection of information, including suggestions for reducing this burden to Department of Defense, Washington Headquarters Services, Directorate for Information Operations and Reports (0704-0188), 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302. Respondents should be aware that notwithstanding any other provision of law, no person shall be subject to any penalty for failing to comply with a collection of information if it does not display a currently valid OMB control number. PLEASE DO NOT RETURN YOUR FORM TO THE ABOVE ADDRESS.					
1. REPORT DATE (DD-MM-YYYY) 16-10-2018		2. REPORT TYPE TR		3. DATES COVERED (From - To)	
4. TITLE AND SUBTITLE Directional Current Probe Measurements in Multipactor Breakdown			5a. CONTRACT NUMBER FA8802-19-C-0001		
			5b. GRANT NUMBER		
			5c. PROGRAM ELEMENT NUMBER		
6. AUTHOR(S) Aimee A. Hubble Matthew S. Feldman			5d. PROJECT NUMBER		
			5e. TASK NUMBER		
			5f. WORK UNIT NUMBER		
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) The Aerospace Corporation Physical Sciences Laboratories 2310 E. El Segundo Blvd. El Segundo, CA 90245-4691			8. PERFORMING ORGANIZATION REPORT NUMBER TR-2019-00126		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES) Space and Missile Systems Center Air Force Space Command 483 N. Aviation Blvd. El Segundo, CA 90245			10. SPONSOR/MONITOR'S ACRONYM(S) SMC		
			11. SPONSOR/MONITOR'S REPORT NUMBER(S)		
12. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited.					
13. SUPPLEMENTARY NOTES					
14. ABSTRACT Current probes (or electron probes) are a simple and yet highly effective diagnostic in detecting multipactor breakdown. The most common geometry for these probes is a piece of semi-rigid cable with a small segment of the center conductor exposed. A small positive bias is applied to the center conductor to collect electrons from the multipactor breakdown. Probes are highly sensitive when set up correctly and within line of sight of the breakdown region – however, they are generally isotropic and are not useful for finely identifying the position of the breakdown. In this work, a Directional Current Probe (DCP) design is discussed and tested, demonstrating enhanced ability to localize a breakdown region as opposed to standard probes. The DCP consists of a biased collector surrounded by a biased shield, similar to a Faraday cup. By applying a negative bias to this shield, electron collection is limited to the line of sight allowed by the shield opening.					
15. SUBJECT TERMS biased, breakdown, cable, collector, conductor, cap, diagnostic, direction, electron, Faraday, isotropic, line of sight, measurements, multipactor, probes, semi-rigid, shield.					
16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT	18. NUMBER OF PAGES 11	19a. NAME OF RESPONSIBLE PERSON Aimee A. Hubble
a. REPORT UNCLASSIFIED	b. ABSTRACT UNCLASSIFIED	c. THIS PAGE UNCLASSIFIED			19b. TELEPHONE NUMBER (include area code) (310) 336-2457

Abstract

Current probes (or electron probes) are a simple and yet highly effective diagnostic in detecting multipactor breakdown. The most common geometry for these probes is a piece of semi-rigid cable with a small segment of the center conductor exposed. A small positive bias is applied to the center conductor to collect electrons from the multipactor breakdown. Probes are highly sensitive when set up correctly and within line of sight of the breakdown region; however, they are generally isotropic and are not useful for finely identifying the position of the breakdown.

In this work, a directional current probe (DCP) design is discussed and tested, demonstrating enhanced ability to localize a breakdown region as opposed to standard probes. The DCP consists of a biased collector surrounded by a biased shield, similar to a Faraday cup. By applying a negative bias to this shield, electron collection is limited to the line of sight allowed by the shield opening.

Contents

1.	Directional Current Probe Design.....	1
1.1	Background and motivation	1
1.2	Device Geometry.....	1
2.	Test Data	2
2.1	DCP Sensitivity	2
2.2	DCP Normal Spatial Resolution.....	3
2.3	DCP Lateral Spatial Resolution	4
3.	Conclusions.....	5
	References.....	5

Figures

Figure 1. Probe configuration.	1
Figure 2. Probe photograph.....	1
Figure 3. Setup to assess DCP effectiveness.....	2
Figure 4. Probe response measured as a ratio of current measured on the DCP to the current measured on the control probe.....	2
Figure 5. Schematic depicting generalized setup and directions of probe interrogation.	3
Figure 6. Setup to assess probe response with distance from the breakdown region in the direction across the breakdown device (y-axis from Figure 4).....	3
Figure 7. Probe response as a ratio of DCP measured current to center conductor diagnostic measured current.	3
Figure 9. Probe response as a ratio of DCP measured current to control probe measured current, normalized to the probes' respective responses at $x = 0$ cm. Faceplate diameter is 0.125" (left) and 0.375" (right), and collector bias is fixed at +18 V.....	4
Figure 8. Setup to assess probe response with distance from the breakdown region in the direction parallel to the breakdown device. The DCP (foreground) is attached to a motion stage which allows it to move right to left (the x-axis).....	4

1. Directional Current Probe Design

1.1 Background and motivation

Current probes (also frequently called electron probes) are what is called a “local” breakdown diagnostic for multipactor testing [1]. These probes use a positive bias on a collecting surface to directly measure current from the RF discharge. All other multipactor diagnostics measure side-effects of the breakdown, such as impact on RF performance (phase null, reflected power detection, and harmonic detection), or photon emission [2].

As they make direct measurements, current probes are regarded as a high sensitivity diagnostic as long as they are properly implemented. This typically requires vent path or other access to the breakdown region. However, current probes collect isotropically, and it can be difficult to use current probes to localize the source of a breakdown. Often when performing testing, being able to localize the source of a breakdown is of key importance, particularly when no breakdown is expected (by either design or modeling).

1.2 Device Geometry

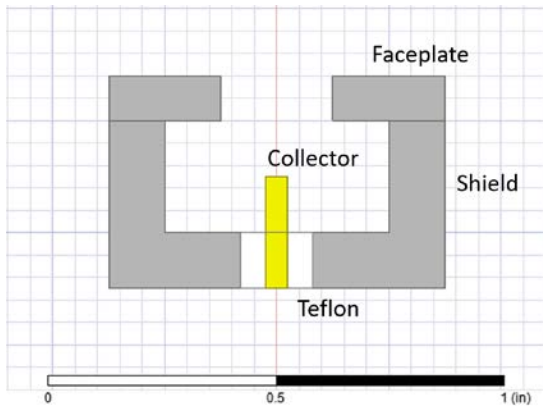


Figure 1. Probe configuration.

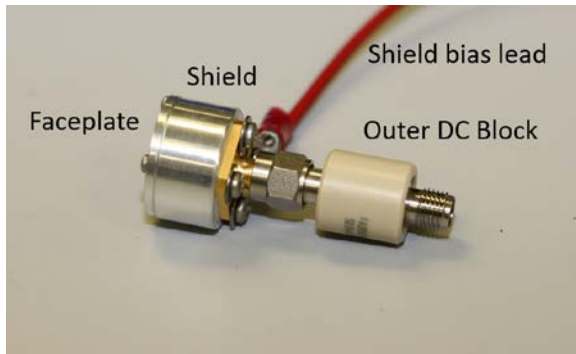


Figure 2. Probe photograph.

Figure 1 depicts the general configuration of the probe. An SMA flange feedthrough serves as the collector. The Teflon insulator of the SMA feedthrough prevents the collector pin from shorting to the outer conductor. The outer conductor shield bolts to the SMA flange, and interchangeable plates can be attached to the shield to effectively limit the field of view of the probe.

The inner collector is biased positively to attract electrons from the multipactor discharge. Both +18 V and +36 V biases were used in this work. The most effective way to apply this bias is simply using 9 V batteries in parallel, usually enclosed within a grounded box. Collector current is measured with a Keithley 6485 picoammeter. The outer shield can be biased either positively or negatively, with a negative bias being essential for performing spatially resolved measurements. The probe is essentially a simple Faraday cup, and the use of interchangeable face plates allows for careful selection of the degree of spatial resolution that is desired. An outer DC block is used to isolate the shield voltage from ground. A photo of the probe is shown in Figure 2.

2. Test Data

2.1 DCP Sensitivity

The effectiveness of the probe both in sensitivity to breakdown and in its capacity to make spatially resolved measurements was assessed using a stripline breakdown device. To assess overall sensitivity to breakdown, the DCP was compared to a control probe. In this test, the control probe was simply the SMA feedthrough with no shield attached.

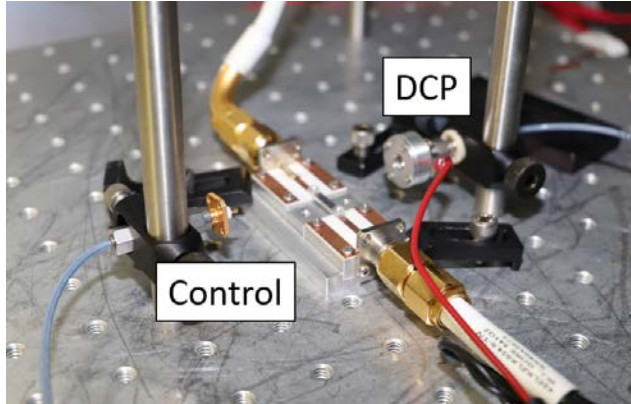


Figure 3. Setup to assess DCP effectiveness.

The probes were placed on opposite sides of the breakdown device, roughly equidistant from the stripline (Figure 3). The same bias was applied to both collectors (either +18 V or +36 V). The collected current on both probes was measured for each breakdown using the analog output voltage of the picoammeters. The ratio of DCP response to control probe response was used to assess the performance of the DCP with shield voltage and faceplate diameter. This corrects for any variation in the electron density of the multipactor breakdown itself.

To initiate breakdown, power was applied to the device in an “instant on” capacity (compared to a traditional breakdown test which ramps test power slowly). This was done to minimize differences in electron density between discharges. A shutdown box [3] was employed to prevent damage to the breakdown device and to minimize device conditioning. The power level was set to 65 W at 1 GHz, which was roughly 1 dB over the breakdown threshold of the device.

Shield voltage was varied from +30 to -30 V for faceplate diameters of 0.125”, 0.375”, and 0.5”. Collector probe bias was set to both +18 V and +36 V. Results are given in Figure 4 below.

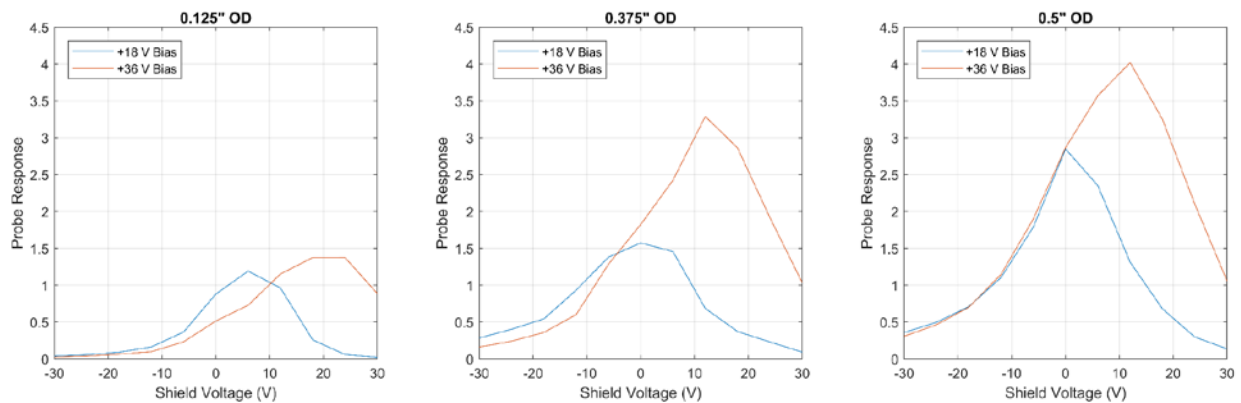


Figure 4. Probe response measured as a ratio of current measured on the DCP to the current measured on the control probe.

Unsurprisingly, probe sensitivity is reduced as faceplate diameter gets smaller and the shield voltage is reduced. A slight positive bias can have an enhancing effect on the probe response, likely because a slight positive bias helps draw current towards the vicinity of the collector, but due to the higher voltage on the collector the majority of current from the discharge still makes its way there. The DCPs can be used this way when probe sensitivity is an issue and spatial resolution is not necessary. Probe sensitivity can frequently be an issue when there is great distance between the device under test and the probe, where breakdown is expected to be internal to a device and the probe must be positioned outside a vent hole, or in magnetic devices where electron confinement prevents electrons from reaching the probe.

2.2 DCP Normal Spatial Resolution

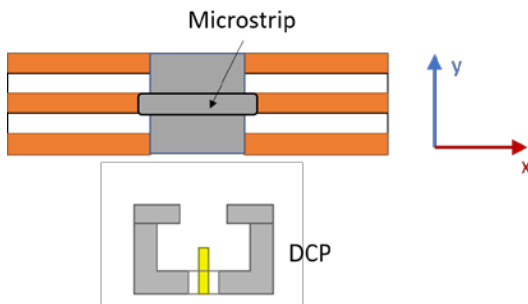


Figure 5. Schematic depicting generalized setup and directions of probe interrogation.

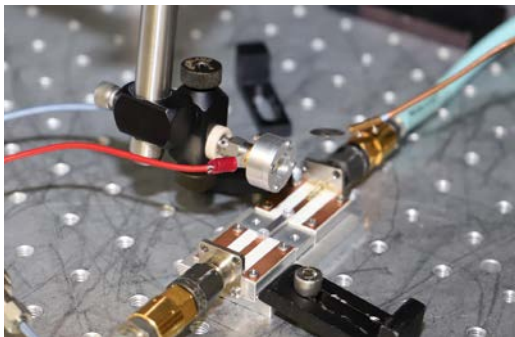


Figure 6. Setup to assess probe response with distance from the breakdown region in the direction across the

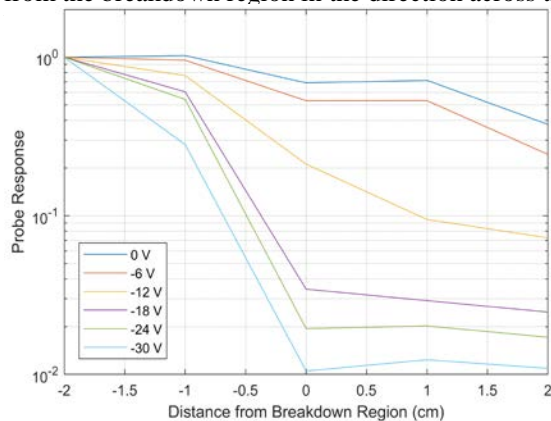


Figure 7. Probe response as a ratio of DCP measured current to center conductor diagnostic measured current.

Next, the spatial resolution of the DCP was evaluated both in the direction along the length of the breakdown device (x) and across the breakdown device (y) (see Figure 5). Due to the orientation of the shield, it is expected that the probe will have optimal shielding in (y) as all field of view of the discharge will be largely blocked by the shield once the probe is beyond the plane of the discharge. To assess this capability, the DCP was attached to a motion arm and translated across the breakdown region perpendicularly (in the y-axis). A photograph of the setup is shown in Figure 6.

Probe response was measured as a ratio of the DCP measured current to the measured current of a center conductor diagnostic [4]. This was needed because it was found the presence of the DCP above the microstrip greatly affected the current measured by a control probe placed within the vicinity of the breakdown region. The probe response versus DCP position is plotted for different shield voltages in Figure 7, normalized to the relative response at $y = -2$ cm, the measurement with optimal DCP field of view of the breakdown region. The middle of the microstrip in this instance corresponds to $y = 0$ cm, which is already well shielded even at relatively low voltages. The DCP is highly effective at shielding itself from detecting multipactor events when the body of the shield prevents line of sight to the

discharge and a negative bias is applied that is on the order of the collector voltage. The shielding effect is enhanced for narrow faceplate openings and more strongly negative shield voltages, but since both these qualities are known to reduce overall probe sensitivity, DCP characteristics should be optimized for the precise application.

2.3 DCP Lateral Spatial Resolution

Figure 8 depicts a photo of the setup of the lateral probe assessment. A control probe is fixed centered on the breakdown region. The test probe is affixed to a motion stage and current draw is measured along the x-axis. Probe response is plotted in Figure 9 as a ratio of DCP measured current to control probe measured current, normalized to the probes' respective responses at $x=0$. This plot depicts the effective reduction in probe response as the DCP moves away from the center of the breakdown region. A control (non-shielded) probe was also swept in the x-direction to determine the effect that only the distance from the breakdown region had upon probe response.

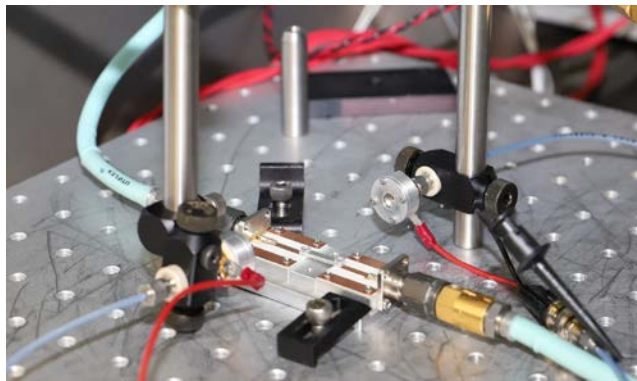


Figure 9. Setup to assess probe response with distance from the breakdown region in the direction parallel to the breakdown device. The DCP (foreground) is attached to a motion stage which allows it to move right to left (the x-axis).

The probe response at $x > 2$ cm is reduced at all voltages for the smaller faceplate than the larger faceplate, unsurprisingly. The way the probe response is calculated (a normalized ratio of DCP response to control probe response) removes the effect of overall probe sensitivity from the data, so the reduction in response seen is entirely due to the reduction of the field of view due to the smaller faceplate. A smaller faceplate is therefore more effective in resolving the position of the breakdown. Note that for this device, the center of the breakdown region is at $x=0$, but since the stripline is 12.7 mm long, $x=1$ cm is effectively still looking at the breakdown directly.

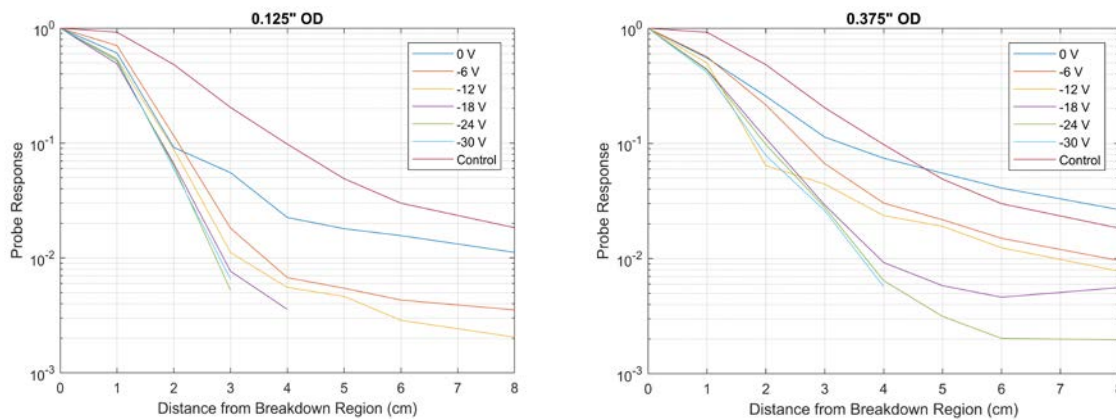


Figure 8. Probe response as a ratio of DCP measured current to control probe measured current, normalized to the probes' respective responses at $x = 0$ cm. Faceplate diameter is 0.125" (left) and 0.375" (right), and collector bias is fixed at +18 V.

At all voltages there is an immediate reduction in probe response at $x = 2$ cm and beyond, but in general spatial resolution of the probe response gets better with stronger shield voltage. In practice, it will be wise to select a probe faceplate and shield bias that will adequately resolve the position of the breakdown while maintaining diagnostic sensitivity in order to avoid false results. This means selecting as large a faceplate and as small a shield bias as is sensible (while still maintaining adequate spatial resolution.) Ultimately, this will also depend on the strength of the multipactor event and the distance between the probe position and breakdown region.

For the 0.375" faceplate and no shield bias, the DCP actually has a stronger probe response than the control probe when far away from the breakdown region. This is due to the sensitivity enhancing nature of the shield when unbiased (or at a slight positive bias).

3. Conclusions

Direct electron population measurement of a multipactor discharge is often the most straightforward and unambiguous sign of RF breakdown. This is most commonly done using an exposed wire or plate which has a positive bias applied. While effective, this technique lacks spatial resolution and, while useful for determining whether a breakdown has occurred or not, is not always useful for determining the location of breakdown.

A directional current probe DCP was developed using a biased shield around the probe collector. This technique was demonstrated using a microstrip breakdown device and the relationship between shield voltage, faceplate diameter, and collector bias determined. The probe is most effective in determining the location of a breakdown when it can be positioned so that one potential location is completely obscured by the shield while maintaining field of view of another potential location.

It was also found that these probes can be used to enhance overall probe sensitivity using an open faceplate and a slight positive shield bias. This encourages a broader collection of electrons, and while this technique generally lacks spatial resolution, it may be useful in cases where probe use is otherwise limited or insensitive.

References

- [1] "Standard/Handbook for Multipactor Breakdown Prevention in Spacecraft Components," document ANSI/AIAA S-142-2016, November 2016.
- [2] ECSS Secretariat, Space Engineering, Multipaction Design and Test, European Cooperation for Space Standardization, ECSS-E-20-01A, Rev. 1.1 March 2013.
- [3] Graves, T.P. et al. Rev. Sci. Inst., 85, 024704 (2014).

Technical Reports Addendum Asset Summary #2018101609435129227

Report Name: Directional Current Probe Measurements in Multipactor Breakdown

Aerospace Report Number: TR-2019-00126

First Aerospace Author / PI: Hubble, Aimee A

Created By: Aimee A Hubble

NON Aerospace MTE: *No assets reported.*

ACJ139 AGILENT U2001A

Usage Dates: 08/14/2018 - 08/31/2018 (!)

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
03/24/2017	08/19/2018 (!)	3F7CC508-3CFF-4BDD-BC7F-352F7A569BE0	TMT-NORMAL

(!) Calibration expired during test.

ADM149 KEITHLEY INSTRUMENTS INC. 6485

Usage Dates: 08/14/2018 - 08/31/2018 (!)

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
07/28/2017	08/26/2018 (!)	BDEA9D81-45E0-4DD8-BB56-7681960D CAD8	TMT-NORMAL

(!) Calibration expired during test.

Technical Reports Addendum Asset Summary #2018101609435129227

ABI702 AGILENT E3632A

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
02/13/2017	12/09/2018	596CFBDA-4E64-405D-9DCB-3B91C140 8AA5	TMT-NORMAL

ABN161 KEITHLEY INSTRUMENTS INC. 6485

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
11/22/2016	04/21/2019	69558CD1-CD3F-4670-AA6D-2607B7A7 EEB9	TMT-NORMAL

ABU655 AGILENT N5181A

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
02/05/2018	02/03/2019	F1A2DDEA-6F21-43CF- B91E-06C208660DAC	TMT-NORMAL

ACA701 AGILENT U2001A

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
05/16/2018	10/11/2020	0CA43B11-D66D-42EE-B8DD- D015E68B3C0A	TMT-NORMAL

ACR503 HUBER-SUHNER 74 Z-0-0-21

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
02/28/2018	06/28/2020	8C84F48F-8BB7-40BD- A531-ECA3951683EB	TMT-LMTD

Technical Reports Addendum Asset Summary #2018101609435129227

ACR538 AGILENT N5222A

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
12/28/2017	12/23/2018	D8DA9D4B-7B5F-4149-A35D-71053DF1 9CD2	TMT-NORMAL

ACR569 HUBER-SUHNER 74 Z-0-0-192

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
03/01/2018	06/28/2020	27B75EEE-383B-4D45-9192-49153BCE3 FED	TMT-LMTD

ADM148 KEITHLEY INSTRUMENTS INC. 6485

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
08/02/2017	09/02/2018	A39C1892-A741-408B-96B1-A8DA94E3B A5E	TMT-NORMAL

AEF889 KEYSIGHT DSOX2014A

Usage Dates: 08/14/2018 - 08/31/2018

Calibration Date	Calibration Due Date	Certificate Number	Certificate Notes
07/25/2018	08/25/2019	0FF7B884-D357-4CA2-8FC5-359BCC733 7A9	TMT-NORMAL

External Distribution

REPORT TITLE

Directional Current Probe Measurements in Multipactor Breakdown

REPORT NO.

TR-2019-00126

PUBLICATION DATE

November 30, 2018

SECURITY CLASSIFICATION

UNCLASSIFIED

DAVIS I. CHOI
GG-14 USAF AFSPC SMC/PIM
davis.choi.1@us.af.mil

MATTHEW J. KWAWEGEN
1st Lt USAF AFSPC SMC/PIC
matthew.kwawegen@us.af.mil

MARK J. SCATOLINI
GS-13 USAF AFSPC SMC/PIC
mark.scatolini@us.af.mil

APPROVED BY _____
(AF OFFICE)

DATE _____

Directional Current Probe Measurements in Multipactor Breakdown

Cognizant Program Manager Approval:

Thomas J. Curtiss, DIRECTOR DEPT
PROPULSION SCIENCE DEPT
SPACE MATERIALS LABORATORY
ENGINEERING & TECHNOLOGY GROUP

Aerospace Corporate Officer Approval:

Charles L. Gustafson, SR VP ENG & TECH
ENGINEERING & TECHNOLOGY GROUP

© The Aerospace Corporation, 2019.

All trademarks, service marks, and trade names are the property of their respective owners.

SQ0312

Directional Current Probe Measurements in Multipactor Breakdown

Content Concurrence Provided Electronically by:

Aimee A. Hubble, RES SCIENTIST
ELECTRIC PROPULSION & PLASMA SCIENCE
PROPULSION SCIENCE DEPT
ENGINEERING & TECHNOLOGY GROUP

© The Aerospace Corporation, 2019.

All trademarks, service marks, and trade names are the property of their respective owners.

SQ0312