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BuShips Problem M43

NAVY DEPARTMENT

Report of

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Test on Insulating Material, Body Mix No. 158
and 32
Submitted by

Ohio Brass Co.

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APPENDICES

AUTHORIZATION

1. This problem was authorized by reference (a). References (b), (c), and (d) are also pertinent.

References:

(a) BuShips ltr. S67/61 (480V) of August 19, 1942 to NRL
(b) BuShips ltr. S67/61 (5-23-480) of May 23, 1941
(c) BuShips ltr. S67/61 (480V) of July 17, 1942
(d) Specifications RE 13A 317F.

OBJECT OF TEST

2. The object of the test w as to determine whether the samples of Ceramic submitted by The Ohio Brass Co., comply with reference (d) for Grade F or G insulating material amd also to determine the modulus of rupture of this material.

ABSTRACT OF TEST

3. The dry a nd wet loss factors were determined by measurements made at 1000 kilocycles, in compliance with paragraph two of reference (b), paragraph 6-1 of reference (d), and in accordance with A.S.T.M. Standards on Testing Electrical Insulating Materials of December 1941. The wet loss factor was measured after the samples had been immersed in distilled water for 48 hours. The modulus of rupture test was made on a Standard Southwark Testing Machine.

4. Moisture absorption measurements were made in accordance with paragraph 6-2 of reference (d).

CONCLUSIONS

It is concluded:

(a) That these samples of Ceramic submitted by the Ohio Brass Co., comply w ith reference (d) for Grade F insulating material.

RECOMMENDATIONS

It is recommended:

(a) That these samples of Ceramic, submitted by the Ohio Brass Company be approved as Grade F insulating material.

DESCRIPTION OF MATERIAL UNDER TEST

5. The three white, unglazed samples numbered 441, 442 and 443 by NRL were approximately 15 cm. square and 0.63 cm. thick. The three brown, glazed samples numbered 444, 445 and 446 were of approximately the same dimensions but badly warped. The twelve cylindrical samples numbered 37 to 48 inclusive (6 white unglazed and 6 brown glazed respectfully) were approximately 6 inches long and 1-1/8 inches thick. The samples numbered 486, 487 and 488 were forwarded to NRL after completion of tests on above mentioned samples. These were approximately 15.1 cm. square and 0.62 cm. thick. They were not glazed on the edges, but were not as badly warped as the previous glazed samples. Since the body mix number was not designated, they were assumed to be of Body Mix No. 32.

METHOD OF TEST

6. Physical measurements of the samples were made with micrometers and a metric rule; the electrical measurements by the susceptance variation method of parallel substitution. The dielectric properties were determined from these data.

7. The standard measuring circuit consists of the following equipment:

1000 kc crystal controlled master oscillator power amplifier, assembled by NRL;

NRL Standard inductance No. 6;

General Radio quartz insulated precision condenser, Type 722-Q Serial No. 460;

General Radio vacuum tube voltmeter, Type 726-A, Serial No. 1483.

8. The factor of merit of the variable capacitor is stated by the manufacturer to be better than 0.003×10^{-12} Farads. The factor of merit of the entire test circuit is better than 1.11×10^{-12} Farads or one C.G.S. electrostatic unit. The effective Q of the entire measuring circuit is approximately 344 units, measured at 1000 kc.

9. The dry loss factor was determined after allowing the test samples to come to a static equilibrium of ambient temperature and relative humidity with that of the standard measuring circuit, which is assumed to occur in about 24 to 48 hours. Each sample was made into a capacitor by applying foil to both surfaces with petroleum oil. The factors of merit of the standard circuit with and without the samples were measured and each expressed as the ratio of total effective conductance to the resonant angular velocity. The difference between the two factors thus measured is equal to the factor of merit of the sample. When the conductance of the sample is small and can be neglected in comparison with its susceptance, the power factor is equal to the difference in reading of the standard, taken at resonance, with and without the sample; provided, the residual inductance (L) of the standard capacitor is sufficiently small to make W^2LCs negligible as compared to unity.

10. The dielectric permittivity (K) was determined from physical measurements made upon the sample, as outlined in A.S.T.M. Standards. The loss factor is defined as the product of the power factor and the dielectric permittivity. The wet loss factor was determined in a similar manner after the samples had been immersed in distilled water for a period of 48 hours in compliance with reference (d).

11. The moisture absorption tests were carried out on newly fractured pieces as detailed in paragraph 6-2 of reference (d) and paragraph 3 of reference (c) where the newly fractured surface was approximately 50% of the unfractured surface of each sample. The samples were first immersed in distilled water at room temperature for 96 hours during which time the water was boiled for a period of one hour during the 1st, 25th, 49th and 74th hours. At the end of 96 hours the samples were removed from the water, carefully dried with filter paper and immediately weighed. They were then placed in a desiccator for 96 hours after which time they were again weighed.

12. The modulus of rupture test was made by applying a direct load, at a rate of 250 lbs. per minute, midway between two points of restraint. These points were separated by a distance of 5.00 inches. The radius of curvature of the three points was 0.125 inches. A standard Southwark Testing Machine was used for this purpose.

DATA RECORDED DURING TEST

13. The data recorded during test are given in Tables I, II and III.

PROBABLE ERROR IN RESULTS

14. The error in the determination of the power factor is not greater than 2%, while that of the loss factor is not greater than 3%. The error in the determination of the weight in the moisture absorption test is approximately 0.00125%. The error in the determination of the modulus of rupture is not greater than 2%.

15. The data relating to dielectric properties have been corrected for the fringing of the dielectric flux external to the periphery of the electrodes.

16. Corrections to include the residual errors in the standard measuring circuit have not been applied to these data.

RESULTS OF TEST

17. Results of test are given in Table I, II and III. The data recorded in Table I shows the wet loss factor to be Grade F for all samples.

18. Table II shows that the samples comply with paragraph 6-2 of reference (d) for the moisture absorption test.

19. Table III gives the value of the Modulus of Rupture for the samples numbered 37 to 48 inclusive.

CONCLUSIONS

20. It is concluded:

(a) That these samples of Ceramic submitted by the Ohio Brass Co., comply with reference (b) for Grade F insulating material.

TABLE I

Ohio Brass Company

441-2-3 unglazed 444-5-6 glazed except on one edge

Dielectric Properties

NRL No.	Dielectric Constant Dry	Wet	Power Factor Dry	Wet	Loss Factor Dry	Wet	Grade
441	6.12	6.09	0.980	1.05	5.56	6.38	F
442	6.00	6.08	0.933	1.08	5.60	6.56	F
443	5.99	6.00	0.948	1.18	5.68	7.02	F
444	5.97	5.92	0.976	1.03	5.82	6.10	F
445	5.87	5.86	1.01	1.03	5.82	6.06	F
446	6.03	5.99	0.982	1.06	5.92	6.38	F
486	6.04	6.03	0.978	0.951	5.41	5.74	F
487	6.04	5.95	1.02	0.946	6.14	5.63	F
488	6.11	6.07	0.984	0.974	6.01	5.41	F

TABLE II

Moisture Absorption

NRL No.	Weight in Grams Dry	Wet	Gain Grams	Gain %
441	47.3841	47.3770	0.0017	0.015
444	44.8618	44.8559	0.0059	0.013
486	44.748	44.756	0.008	0.011

TABLE III

Modulus of Rupture

Numbers 37-42 inclusive, unglazed 43-48 inclusive, glazed, except on one end

NRL No.	Direct Load lbs.	Diameter inches	Modulus lbs/in^2
37	945	1.11	8798
38	1145	1.11	10656
39	1035	1.11	9636
40	1100	1.11	10241
41	1175	1.12	9858
42	1045	1.11	9729
43	1560	1.12	13088
44	1555	1.12	13046
45	1540	1.12	12921
46	1590	1.12	12840
47	1585	1.12	13298
48	1605	1.12	13466