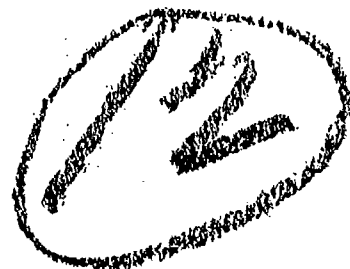


**Band Model Parameters for the 2.7- μ m Bands of
H₂O and CO₂ in the 100 to 3000°K
Temperature Range**

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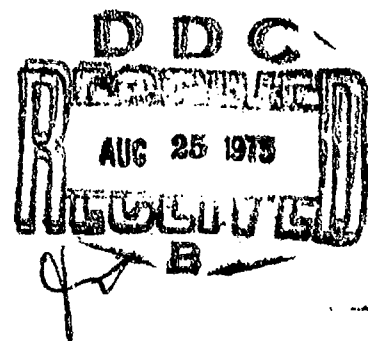
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31 July 1975

Interim Report

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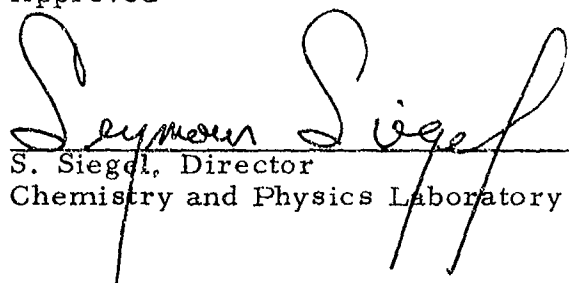
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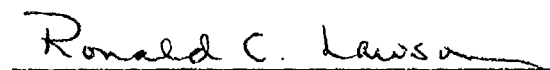
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20. ABSTRACT (Continued)

The former set adequately describes the low-temperature variation of the parameters but is inadequate for some high-temperature applications. The latter set is suitable for high-temperature applications but fails for some low-temperature cases. Examples of the deficiencies of these two sets are presented by comparison with experimental absorption and emission spectra for low- and high-temperature gas samples. The adequacy of the combined band model parameter set (COMB parameters) is demonstrated by comparison with the same experimental data. Criteria for and examples of the construction of the combined sets are given, and tabulations of the parameter sets are included in an Appendix. An example of the use of the new parameter sets is given by computation of the effective transmittance of the atmosphere for a hot H_2O/CO_2 emission source viewed over a long atmospheric slant path.

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I. INTRODUCTION

In a previous report,¹ band model techniques were applied to the problem of computing the effective transmittance of the atmosphere for radiation arising from hot gaseous H_2O and CO_2 emission sources. Effects of line correlation between the emission spectra and atmospheric absorption spectra were accounted for by treatment of the entire optical path consisting of the atmospheric slant path plus the line-of-sight continuation through the source as a single, highly inhomogeneous radiating and absorbing entity. Approximations for handling the large degree of inhomogeneity caused by pressure, temperature, and species concentration gradients along such an optical path were discussed.

The single most important variable that affects the degree of inhomogeneity of the path is the temperature distribution along the path. Through the atmospheric portion of the total path, the temperature variations are slight, and for many applications, the atmosphere can be considered as isothermal. In the transition region between the atmospheric portion and the source portion of the path, and within the source portion itself, large temperature gradients can exist. The effect of these temperature gradients is introduced into the band model calculations through the temperature variation of the fundamental band model parameters that describe the absorption effects of all the spectral lines in a small spectral interval $\Delta\nu$.

In the previous work, two sets of band model parameters were employed. The set designated LINAVE was generated from the line

¹S. J. Young, Band Model Calculations of Atmospheric Transmittance for Hot Gas Line Emission Sources, TR-0075(5647)-1, The Aerospace Corp., El Segundo, Calif. (31 December 1974).

strength and width data of the Air Force Cambridge Research Laboratories (AFCRL) line atlas.² The parameter set designated GD* was taken from the NASA Handbook of Infrared Radiation from Combustion Gases.³ The former set was expected to be reasonably accurate for low temperatures since the AFCRL line atlas was compiled primarily for atmospheric applications. Its use at higher temperatures was demonstrated to be inadequate in the 2.7- μ m band wing regions. The latter set, since it was constructed for high-temperature problems, was expected to be adequate for temperatures above about 1000°K but to be of questionable utility for low temperatures. If the problem of atmospheric transmittance could be treated in a manner in which the source emission and atmospheric absorption were decoupled processes, these existing parameter sets would be sufficient to handle transmittance computations. Since the correct account of line correlation requires the entire optical path to be treated as a single entity, however, a single set of band model parameters, applicable to the entire temperature range from atmospheric temperatures (at least as low as 200°K) to combustion gas temperatures (at least as high as 2500°K), is required.

The work described in this report is concerned with the construction of band model parameter sets for the 2.7- μ m bands of H₂O and CO₂ that

* These parameters were generated by workers at General Dynamics, hence the designation GD. Most people, however, refer to these data as the NASA parameters. The latter designation will be used in the remainder of this report.

² R. A. McClatchey, W. S. Benedict, S. A. Clough, D. E. Burch, R. F. Calfe, K. Fox, L. S. Rothman, and J. S. Garing, AFCRL Atmospheric Absorption Line Parameters Compilation, AFCRL-TR-73-006, Air Force Cambridge Research Laboratories, Mass. (25 January 1973).

³ C. B. Ludwig, W. Malkmus, J. E. Reardon, and J. A. L. Thompson, Handbook of Infrared Radiation from Combustion Gases, eds. R. Goulard and J. A. L. Thompson, NASA SP-3080, Marshall Space Flight Center, Huntsville, Ala. (1973).

are internally consistent for the temperature range from 100 to 3000°K. Section II of this report discusses the generation of the LINAVE and NASA parameter sets and gives examples of their deficiencies. The combining of these two parameter sets to give consistent sets for H₂O and CO₂ is done in Sect. III. An example of their use in an atmospheric transmittance problem is given in Sect. IV.

II. BAND MODEL PARAMETERS

A. BAND MODEL FORMULATION

The statistical band model formulation* for absorption by a random array of pressure-broadened Lorentz lines depends on the specification of three fundamental band model parameters. The mean absorption coefficient $\bar{k}$ describes the strength of absorption effected by all the lines in a spectral interval $\Delta\nu$, the mean line-spacing parameter δ_e measures the effective average distance between adjacent lines in $\Delta\nu$, and $\bar{\gamma}$ gives the mean line width of the lines in $\Delta\nu$. For most applications, δ_e and $\bar{\gamma}$ do not need to be known individually, and the mean line width to spacing parameter

$$\beta = \frac{2\pi \bar{\gamma}}{\delta_e} \quad (1)$$

along with $\bar{k}$ suffices to specify the absorption characteristic of $\Delta\nu$. In general, the parameters $\bar{k}$ and δ_e are functions of spectral position and temperature while $\bar{\gamma}$ depends additionally on the pressure and species composition of the absorbing gas.

For a homogeneous optical path and a single active gas species, the mean transmittance in $\Delta\nu$ is

$$\bar{\tau} = \exp \left(- \frac{\bar{W}}{\delta} \right) \quad (2)$$

* More accurately, we mean the approximation to the statistical band model in which the number of lines in an interval $\Delta\nu$ is assumed to be infinite and for which the absorption by each line whose center occurs in $\Delta\nu$ is complete within $\Delta\nu$.

where $\overline{W}$ is the mean equivalent width of all the lines in $\Delta\nu$ and

$$\delta = \frac{\Delta\nu}{N} \quad (3)$$

is the mean line-spacing parameter. The number of lines in $\Delta\nu$ is N . In terms of band model parameters,

$$\frac{\overline{W}}{\delta} = \beta f(x) \quad (4)$$

where

$$x = \frac{\overline{k} u}{\beta} \quad (5)$$

is the dimensionless optical depth parameter. The optical depth u is the product of the total gas pressure p , the mole fraction of the active gas c , and the geometric path length L :

$$u = p c L \quad (6)$$

The curve-of-growth function $f(x)$ depends on the line strength distribution function assumed for the lines in $\Delta\nu$. For equal intensity lines,

$$f(x) = L(x) \quad (7)$$

where $L(x)$ is the Ladenburg-Reiche function. For an exponential distribution of line strengths,

$$f(x) = \frac{x}{\sqrt{1 + \frac{\pi x}{2}}} \quad (8)$$

while for the exponential-tailed inverse distribution, ^{*4}

$$f(x) = \frac{1}{\pi} \left[\sqrt{1 + 2\pi x} - 1 \right]. \quad (9)$$

These curve-of-growth functions are all defined so that $f(x) \rightarrow x$ for small x and $f(x) \rightarrow (2x/\pi)^{1/2}$ for large x . In this way, the same band model parameters are appropriate for all three distribution functions.

For application of the statistical band model to inhomogeneous optical paths, approximations must be introduced to account for pressure, species concentration, and temperature gradients along the line of sight. In both the Curtis-Godson (CG) and Lindquist-Simmons (LS) approximations, this account is made by the employment of path-averaged values of the band model parameters. For a path extending from the geometric position $s = 0$ to the general position s along the line of sight, the appropriate path averages are

$$\bar{k}_e(s) = \frac{1}{u(s)} \int_0^s c(s') p(s') \bar{k}(s') ds' \quad (10)$$

and

$$\beta_e(s) = \frac{1}{u(s) \bar{k}_e(s)} \int_0^s c(s') p(s') \bar{k}(s') \beta(s') ds' \quad (11)$$

^{*}The exponential-tailed inverse line strength distribution was invented by Malkmus (Ref. 4) as an approximation to the purely inverse line strength distribution function. The resulting curve of growth function [Eq. (9)] is substantially simpler in form than that for the inverse distribution.

⁴W. Malkmus, J. Opt. Soc. Am. 57, 323 (1967).

where

$$u(s) = \int_0^s c(s') p(s') ds' \quad (12)$$

In the CG approximation, $\bar{k}_e$ and β_e are used in place of $\bar{k}$ and β , respectively, in the equations for a homogeneous optical path. In the LS approximation, these path-averaged parameters are used to define the quantities

$$x_e(s) = \frac{\bar{k}_e(s) u(s)}{\beta_e(s)} \quad (13)$$

and

$$\rho(s) = \frac{\beta(s)}{\beta_e(s)} \quad (14)$$

which are used in turn to give the transmittance derivative function

$$y(s) = y[x_e(s), \rho(s)] \quad (15)$$

The functional form of $y(x, \rho)$ with x and ρ depends on the line shape and the line strength distribution employed. The transmittance in the LS approximation is then given by Eq. (2) where $\bar{W}/\delta$ is given by

$$\frac{\bar{W}(s)}{\delta} = \int_0^s c(s') p(s') \bar{k}(s') y(s') ds' \quad (16)$$

A more detailed account of these approximations is given elsewhere.^{1, 5}

⁵S. J. Young, Band Model Formulation for Inhomogeneous Optical Paths, TR-0075(5647)-4, The Aerospace Corp., El Segundo, Calif. (19 December 1974).

The important feature of both of these approximations is that the parameters $\bar{k}$, δ_e , and $\bar{\gamma}$ need to be known for the entire range of variation of the thermodynamic properties of the path. For the highly inhomogeneous optical path consisting of a long atmospheric slant path, plus a line-of-sight continuation through a hot-gas missile exhaust plume, for example, the path temperature $T(s)$ can range from as low as $\sim 190^\circ\text{K}$ to as high as $\sim 3000^\circ\text{K}$. Thus, both $\bar{k}$ and δ_e must be known for this same range of temperature variation in order to compute the path averages of Eqs. (10) and (11). It is this variation of $\bar{k}$ and δ_e over large temperature ranges that is of primary concern. The variation of $\bar{\gamma}$ with temperature and pressure is adequately described by variations of the form $\bar{\gamma} \sim p/T^n$ where n is of the order of unity. Thus, $\bar{\gamma}$ will vary about an order of magnitude between the temperature limits indicated above. For this same temperature range, however, $\bar{k}$ and δ_e may vary by several orders of magnitude.

B. BAND MODEL PARAMETERS FROM LINE DATA
(LINAVE PARAMETERS)

If the line strength $S(i)$ and line width $\gamma(i)$ of all the important lines in $\Delta\nu$ are known, the band model parameters $\bar{k}$, δ_e , and $\bar{\gamma}$ can be derived in terms of $S(i)$ and $\gamma(i)$. The procedure is to force an exact agreement between the weak and strong limits of absorption for the statistical band model described in terms of the line parameters and the model described in terms of the band model parameters. For the former description, we write the mean equivalent width for all the lines in $\Delta\nu$ as

$$\frac{\bar{W}}{\delta} = \frac{1}{\delta} \left\{ \frac{1}{N} \sum_{i=1}^N W(i) \right\} = \frac{1}{\Delta\nu} \sum_{i=1}^N W(i) \quad (17)$$

where $W(i)$ is the equivalent width of the i^{th} line. For a Lorentz line (and homogeneous path),

$$W(i) = 2\pi \gamma(i) L(x) \quad (18)$$

where

$$x = \frac{S(i) u}{2\pi \gamma(i)} \quad (19)$$

The description in terms of band model parameters is given by Eqs. (1), (4), and (5). Repeating for convenience,

$$\frac{\overline{W}}{\delta} = \beta f(x) \quad (20)$$

$$\beta = \frac{2\pi \overline{\gamma}}{\delta_e} \quad (21)$$

and

$$x = \frac{\overline{k} u}{\beta} \quad (22)$$

In the limit of weak absorption (that is, as $x \rightarrow 0$), Eqs. (17) through (19) give

$$\frac{\overline{W}}{\delta} \approx \frac{u}{\Delta \nu} \sum_{i=1}^N S(i)$$

while Eqs. (20) through (22) yield

$$\frac{\bar{W}}{\delta} \simeq \bar{k} u .$$

Equation of these two weak-limit expressions for $\bar{W}/\delta$ yields the solution for $\bar{k}$

$$\bar{k} = \frac{1}{\Delta v} \sum_{i=1}^N S(i) . \quad (23)$$

For strong absorption (as $x \rightarrow \infty$), Eqs. (17) through (19), give

$$\frac{\bar{W}}{\delta} \simeq \frac{2 \sqrt{u}}{\Delta v} \sum_{i=1}^N \sqrt{S(i) \gamma(i)}$$

while Eqs. (20) through (22) yield

$$\frac{\bar{W}}{\delta} \simeq 2 \sqrt{u} \sqrt{\frac{\bar{k} \gamma}{\delta_e}} .$$

Equation of these two strong-limit forms for $\bar{W}/\delta$ yields the solution for δ_e

$$\frac{1}{\delta_e} = \frac{1}{\bar{k} \gamma} \left[\frac{1}{\Delta v} \sum_{i=1}^N \sqrt{S(i) \gamma(i)} \right]^2 . \quad (24)$$

The forced agreement for weak and strong absorption supplies two conditions for the determination of the three band model parameters. In order to complete the determination, we simply define $\bar{\gamma}$ to be

$$\bar{\gamma} = \frac{1}{N} \sum_{i=1}^N \gamma(i) \quad (25)$$

Equations (23), (24), and (25) define the band model parameters $\bar{k}$, δ_e , and $\bar{\gamma}$ in terms of the line data $S(i)$ and $\gamma(i)$, $i = 1, 2, \dots, N$.

These defining equations have been used to construct band model parameter sets for both H_2O and CO_2 . The line strength and width data were derived from the comprehensive line atlas compiled by AFCRL.* This compilation provides line data for each of over 120,000 lines for seven atmospheric absorbing gas species including H_2O and CO_2 . The data given for each line include the line position ν (cm^{-1}), the line strength S_a ($cm^{-1}/molecule \cdot cm^{-2}$ at 296°K), the line half-width γ_a (cm^{-1} for air-broadening at 296°K and 1 atm pressure), and the energy of the lower level of the transition E (cm^{-1}). The line strength for the i^{th} line at temperature T is computed from the value S_a given at the standard temperature $T_a = 296^\circ K$ by

$$S_i(T) = C(T) S_a \frac{Q_R(T_a) Q_V(T_a)}{Q_R(T) Q_V(T)} \left[\frac{1 - e^{-\nu(i)/kT}}{1 - e^{-\nu(i)/kT_a}} \right] \times \exp \left[-\frac{E(i)}{k} \left(\frac{1}{T} - \frac{1}{T_a} \right) \right] \quad (26)$$

The factors Q_R and Q_V are the rotational and vibrational partition functions, respectively, of the molecule. The exponential term accounts for the

* The compilation version dated 4 Feb 1975 by AFCRL was used in this work.

Boltzmann distribution population of molecules in the energy level $E(i)$, and the term in brackets accounts for stimulated emission. The ratio of rotational partition functions is approximated by

$$\frac{Q_R(T_a)}{Q_R(T)} \approx \left(\frac{T_a}{T} \right)^m \quad (27)$$

where $m = 1.5$ for H_2O (H_2O is assumed to be a nearly symmetric-top molecule) and $m = 1$ for CO_2 . The molecular vibrational partition function is assumed to be the product of simple harmonic oscillator partition functions for each vibrational mode of the molecule:

$$Q_V(T) = \left[1 - e^{-\nu_1/kT} \right]^{-d_1} \left[1 - e^{-\nu_2/kT} \right]^{-d_2} \left[1 - e^{-\nu_3/kT} \right]^{-d_3} \quad (28)$$

where ν_1 , ν_2 , and ν_3 are the fundamental oscillatory frequencies of the molecule and d_1 , d_2 , and d_3 are the degeneracies associated with these modes of vibration. For CO_2 , $\nu_1 = 1388.17 \text{ cm}^{-1}$, $\nu_2 = 667.40 \text{ cm}^{-1}$, and $\nu_3 = 2349.16 \text{ cm}^{-1}$. For H_2O , $\nu_1 = 3657.0 \text{ cm}^{-1}$, $\nu_2 = 1594.7 \text{ cm}^{-1}$, and $\nu_3 = 3755.7 \text{ cm}^{-1}$. The degeneracies for all modes of both CO_2 and H_2O are unity, except for the doubly degenerate bending mode ν_2 in the linear CO_2 molecule, for which $d_2 = 2$. The value of $1/k$ is $1.439 \text{ cm}^{-1} \cdot ^\circ\text{K}$.

The factor $C(T)$ of Eq. (26) converts the line strength from the AFCRL unit of $\text{cm}^{-1}/\text{molecule-cm}^{-2}$ to the unit $\text{cm}^{-2}/\text{atm}$ and is

$$C(T) = 2.480 \times 10^{19} \frac{296^\circ\text{K}}{T} \frac{\text{molecules}}{\text{atm cm}^3} \quad (29)$$

Equations (26) through (29) give the required line strengths $S(i)$ to be used in Eq. (23) to calculate $\bar{k}$ for any spectral interval $\Delta\nu$ and at any temperature T .

The line-broadening parameters of the AFCRL atlas are the broadening parameters appropriate to foreign gas broadening by air at 296°K. The mean line width parameter $\bar{\gamma}_a$ computed according to Eq. (25) will reflect broadening for these same conditions. Specification of the line-broadening parameter in terms of air broadening would be suitable if only atmospheric absorption paths were considered. In a hot, combustion gas environment, however, this description is not quite as appropriate. Now, account has to be made of broadening by H_2O and CO_2 as well. In addition, even if the concentrations of H_2O and CO_2 are small, the remaining gas is usually not air but N_2 (the O_2 having been used in the combustion process).

An adequate description of line pressure broadening for the species s is given by

$$\bar{\gamma}_s(p, T) = p \left[c_s (\bar{\gamma}_s^*)_0 \left(\frac{273}{T} \right)^{n_s^*} + \sum_f \left\{ c_f (\bar{\gamma}_s^f)_0 \left(\frac{273}{T} \right)^{n_s^f} \right\} \right] \quad (30)$$

The summation term accounts for foreign gas broadening ($f \neq s$) and non-resonant self-broadening ($f = s$) contributions to the line width. The first term accounts for resonant self-broadening effects that occur primarily for H_2O . The c terms are the mole fractions of the gas constituents, and the $(\bar{\gamma})_0$ parameters are the broadening parameters for standard temperature (273°K) and pressure (1 atm) conditions. The exponents, n , determine the degree of temperature variation. Nominally, $n \sim 1/2$ and $n^* \sim 1$. Values of $(\bar{\gamma})_0$ and exponent parameters recommended in the NASA Handbook³ are given in Table 1.

Table 1. Line-Broadening Parameters for H₂O and CO₂^a

Molecule (s)	Broadener (f)	$(\bar{\nu}_s^*)_0$ (cm ⁻¹ /atm)	n_s^*	$(\bar{\nu}_s^f)_0$ (cm ⁻¹ /atm)	n_s^f
H ₂ O	H ₂ O	0.44	1.0	(0.09)	0.5
	CO ₂			0.12	0.5
	N ₂			0.09	0.5
	O ₂			0.04	0.5
CO ₂	CO ₂	0.01	1.0	0.09	0.5
	H ₂ O			(0.07)	0.5
	N ₂			0.07	0.5
	O ₂			0.055	0.5

^aData taken from Ref. 3. Values in parentheses are estimates.

Of the three parameters $(\bar{\gamma}_s^*)_0$, $(\bar{\gamma}_s^f)_0$, and $(\bar{\gamma}_s^s)_0$, the latter has been selected here as the fundamental line-broadening parameter; that is, the value for nonresonant self-broadening at STP. If $\bar{\gamma}_a$ is the mean width parameter for air broadening at 1 atm and 296°K computed according to Eq. (25), then Eq. (30) and Table 1 can be used to derive

$$\bar{\gamma}_0 \equiv (\bar{\gamma}_s^s)_0 = c \bar{\gamma}_a \quad (31)$$

where $c = 1.186$ for $s = \text{H}_2\text{O}$ and $c = 1.405$ for $s = \text{CO}_2$. The actual mean line width $\bar{\gamma}$ can be computed from the thermodynamic conditions of the optical path and $\bar{\gamma}_0$ by means of Eq. (30) written in the form

$$\bar{\gamma} = \bar{\gamma}_0 P \left[c_s \alpha_s^* \left(\frac{273}{T} \right)^{n_s^*} + \sum_f c_f \alpha_s^f \left(\frac{273}{T} \right)^{n_s^f} \right] \quad (32)$$

where the α coefficients are the ratios of the $(\bar{\gamma})_0$ coefficients to $(\bar{\gamma}_s^s)_0$ and are obtained from Table 1 ($\alpha_s^s = 1$). Note that none of these considerations on the line width parameters affect the evaluation of δ_e by Eq. (24) since any conversion factors applied to $\gamma(i)$ cancel.

For the present work, two sets of line-averaged band model parameters were generated. The set for H_2O (LINA VEH2O) contains $\bar{k}(\nu, T)$, $1/\delta_e(\nu, T)$, and $\bar{\gamma}_0(\nu)$ for $\nu = 2500$ to 4500 cm^{-1} by steps of 25 cm^{-1} with $\Delta\nu = 25 \text{ cm}^{-1}$ and for the 14 values of temperature $T = 100, 150, 200, 250, 300, 350, 400, 500, 750, 1000, 1500, 2000, 2500$, and 3000°K . The set for CO_2 (LINA VECO2) contains the same parameters for the same temperatures but for $\nu = 3080$ to 3860 cm^{-1} by steps of 5 cm^{-1} and $\Delta\nu = 5 \text{ cm}^{-1}$. In all cases, $\bar{k}$ has the unit $\text{cm}^{-1}/\text{atm}$, δ_e has the unit cm^{-1} , and $\bar{\gamma}_0$ has the unit $\text{cm}^{-1}/\text{atm}$ for nonresonant self-broadening at STP.

C. NASA PARAMETERS

Sets of band model parameters generated by General Dynamics and intended primarily for use in high-temperature combustion gas applications have been in existence for several years. The most recent publication of these parameter sets is given by Ludwig et al. in the NASA Handbook.³

The data for CO_2 are the result of theoretical calculations based on the known quantum mechanical properties of linear triatomic molecules.⁶ The approach is similar to that presented in the preceding section. Line strengths were computed theoretically and averaged to yield $\bar{k}$ and δ_e . For the 2.7- μm band region, $\bar{k}$ values are given for the temperature range from 300 to 3000°K but δ_e is given only up to 1800°K. The δ_e data for temperatures between 1800 and 3000°K, however, can be obtained from the report by Huffaker and Dash.⁷ With the data from these two sources, a CO_2 band model parameter set (NASACO2) was constructed* for $\nu = 3000$ to 3770 cm^{-1} by 5- cm^{-1} steps and for the seven temperatures $T = 300, 600, 1200, 1500, 1800, 2400,$ and 3000°K. The spectral resolution of the data appears to be

*When required, linear interpolations with respect to ν and semilogarithmic interpolations with respect to T were used. The δ_e data at $\nu = 3080 \text{ cm}^{-1}$ was assumed to prevail between 3000 and 3080 cm^{-1} . The spurious temperature variation at $T = 1200^\circ\text{K}$ for $3110 \leq \nu \leq 3150 \text{ cm}^{-1}$ was removed from the $\bar{k}$ data by defining these values to be zero. An order-of-magnitude error in the 1200°K data at $\nu = 3660 \text{ cm}^{-1}$ was corrected in the $\bar{k}$ data by using $\bar{k} = 0.3471 \text{ cm}^{-1}$ rather than the listed value of 0.03471 cm^{-1} . This correction also affects the values on either side of 3660 cm^{-1} ; the $\bar{k}$ value at 3655 cm^{-1} was changed from 0.1877 to 0.3439 cm^{-1} and the value at 3665 cm^{-1} from 0.2197 to 0.3759 cm^{-1} . An apparent order-of-magnitude error in $\bar{k}$ for $T = 300^\circ\text{K}$ at $\nu = 3540 \text{ cm}^{-1}$ was corrected by replacing the value 4.889×10^{-2} by $4.889 \times 10^{-3} \text{ cm}^{-1}$.

⁶W. Malkmus, J. Opt. Soc. Am. **54**, 751 (1964).

⁷R. M. Huffaker and M. J. Dash, A General Program for the Calculation of Radiation from an Inhomogeneous, Nonisobaric, Nonisothermal Rocket Exhaust Plume, NASA TM X-53622, Marshall Space Flight Center, Huntsville, Ala. (19 June 1967).

$\Delta\nu \approx 5 \text{ cm}^{-1}$. The NASA unit for $\bar{k}$ is cm^{-1} at STP and was converted to the unit $\text{cm}^{-1}/\text{atm}$ by multiplication by $273/T$. The $\bar{\gamma}_0$ coefficient is taken as a constant for all $\Delta\nu$ intervals with the value (from Table 1) $\bar{\gamma}_0 = 0.09 \text{ cm}^{-1}/\text{atm}$.

The NASA parameters for H_2O were derived for the most part from experimental measurements.⁸ Because of the nonlinearity of H_2O , exact theoretical calculation of band model parameters is extremely complicated and difficult, particularly at high temperatures. The bulk of the H_2O data above $\sim 1200^\circ\text{K}$ were obtained in a consistent manner from emission-absorption measurements made on very long strip-burner H_2/O_2 flames. Data below $\sim 1200^\circ\text{K}$ are based on extrapolations from these high-temperature data and on the analysis of published low-temperature H_2O spectra. For the $2.7\text{-}\mu\text{m}$ region, $\bar{k}$ values are given for the temperature range from 300 to 3000°K , but δ_e is given only down to 600°K . With these data, an H_2O band model parameter set (NASA H_2O) was constructed between $\nu = 2500$ and 4500 cm^{-1} by 25-cm^{-1} steps at the seven temperatures $T = 300, 600, 1000, 1500, 2000, 2500,$ and 3000°K . The spectral resolution of the data is $\Delta\nu = 25 \text{ cm}^{-1}$. The 300°K values of δ_e at each wave number was obtained from a semilogarithmic extrapolation from the 600 and 1200°K data. Again, the unit of $\bar{k}$ was converted from cm^{-1} at STP to $\text{cm}^{-1}/\text{atm}$, and $\bar{\gamma}_0$ was taken as (Table 1) $\bar{\gamma}_0 = 0.09 \text{ cm}^{-1}/\text{atm}$ for all ν .

D. EVALUATION OF PARAMETER SETS

The AFCRL line atlas was compiled primarily for use in atmospheric transmittance problems. As a result, only those lines that are likely to be important near ambient atmospheric temperatures (say less than $\sim 300^\circ\text{K}$) are specifically included. For most absorbing gases, these lines are absorption lines whose transition originates (in absorption) from the $\nu = 0$ vibrational level of the ground electronic state of the molecule. For high-temperature problems, transitions originating from $\nu \geq 1$ (hot bands) are likely to be important. Although many lines for which $\nu \geq 1$ are included

⁸C. B. Ludwig, App. Opt. 10, 1057 (1971).

in the AFCRL atlas, it can be anticipated that the LINAVE band model parameters derived from the atlas data may not be adequate for temperatures much above 300°K.

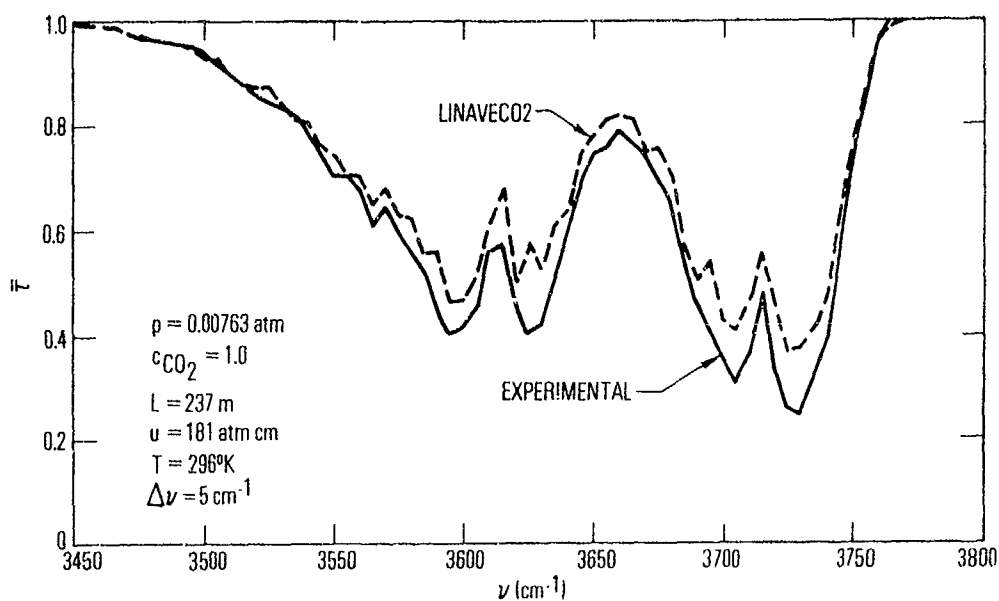
Conversely, the NASA parameters were generated specifically for high-temperature applications. Here, the problem is that the parameters are not particularly useful for low-temperature problems. Indeed, neither the set for CO₂ nor H₂O give any data for $T < 300^{\circ}\text{K}$, the region of most importance for atmospheric application.

The deficiencies of both the LINAVE and NASA parameters have been investigated quantitatively by comparing absorption spectra computed through the use of the parameters with high-quality experimental measurements made for homogeneous paths. Comparisons were made for both CO₂ and H₂O and for both room-temperature and hot-gas conditions. The curve-of-growth function for the exponential-tailed inverse line strength distribution was used in the calculations.

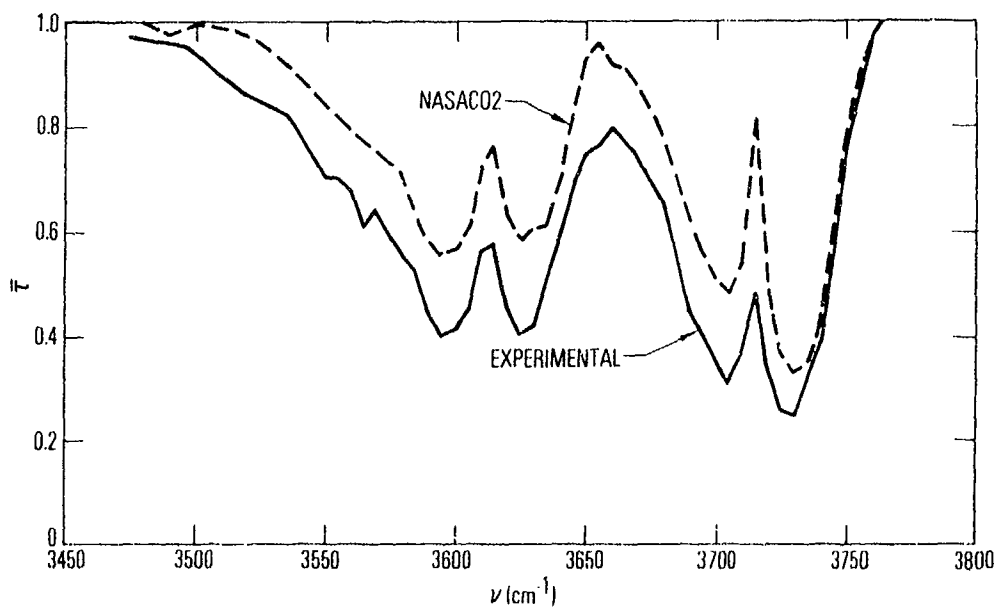
1. CO₂ AT 296°K

Burch et al.⁹ have made high-resolution measurements of the absorption spectra of CO₂ at 296°K for a wide variety of optical thickness, partial pressure of CO₂, and total pressure (with N₂ as the foreign gas). For most of the sample experimental cases, extensive tables are given from which the integrated absorptance between any two wave numbers can be calculated. In Fig. 1, the solid curves are the $\bar{\tau}$ result for their sample no. 9 for which $p = 0.00763$ atm, $c = 1.00$, and $L = 237$ m. The optical depth is $u = 181$ atm cm. The curve was constructed for $\Delta\nu = 5\text{ cm}^{-1}$ and extends through the band center region from 3450 to 3775 cm^{-1} . Figure 1(a) shows the comparison of the experimental spectrum with the spectrum computed with the

⁹D. E. Burch, D. A. Gryvnak, and R. R. Patty, Absorption by CO₂ Between 3100 and 4100 cm^{-1} (2.44-3.22 Microns), U-4132, Aeronutronic Div., Philco-Ford Corp., Newport Beach, Calif. (30 April 1968).



(a)



(b)

Fig. 1. Low-Temperature Transmission Spectra for CO_2 in the Band Center Region. The LINAVERCO2 (a) and the NASACO2 (b) curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 9 for sample no. 9 and for $\Delta\nu = 5 \text{ cm}^{-1}$.

LINAVECO2 parameters while Fig. 1(b) shows the comparison with the result obtained with the NASACO2 parameters. Both of the parameter sets give results that underestimate the degree of absorption displayed by the experimental results. The LINAVECO2 set, though, gives results that are in adequate agreement with the experimental spectrum. The underestimation of the absorptance in both cases may be the result of using a statistical rather than a regular line-spacing band model for CO₂ at low temperatures.

A similar comparison was made in the far wing region between 3100 and 3500 cm⁻¹. Here, a much more strongly absorbing sample was chosen so that the absorptance would be measurable. The solid curves of Fig. 2 are the experimental results for sample no. 1 for which $p = 2.5$ atm, $c = 1.00$, and $L = 933$ m. The optical thickness is $u = 2.33 \times 10^5$ atm cm and again, $\Delta\nu = 5$ cm⁻¹. The NASACO2 values for $\bar{k}$ are zero at 300°K for $\nu \leq 3280$ cm⁻¹, and consequently, no amount of absorption is effected in the band wing. The LINAVE parameters yield an absorption spectrum that is in adequate agreement with the experimental spectrum.

2. CO₂ AT 1200°K

A high-temperature emission comparison was made between calculated emissivity spectra and an experimental spectrum of Burch and Gryvnak.¹⁰ The experimental conditions were: $p = 0.997$ atm, $c = 1.00$, $L = 7.75$ cm, and $T = 1200^\circ\text{K}$. The optical thickness is $u = 7.73$ atm cm and $\Delta\nu \approx 7$ cm⁻¹. The comparison is shown in Fig. 3. Even at this high temperature, the result computed with the LINAVECO2 parameters is in good agreement with the experimental result above $\nu \approx 3550$ cm⁻¹. In the wing region below 3500 cm⁻¹, however, the LINAVECO2 parameters seriously underestimate the degree of emission and, below 3450 cm⁻¹, predict no emission at all. The NASACO2

¹⁰D. E. Burch and D. A. Gryvnak, Infrared Radiation Emitted by Hot Gases and Its Transmission Through Synthetic Atmospheres, U-1929, Aeronutronic Div., Philco-Ford Corp., Newport Beach, Calif. (31 October 1962).

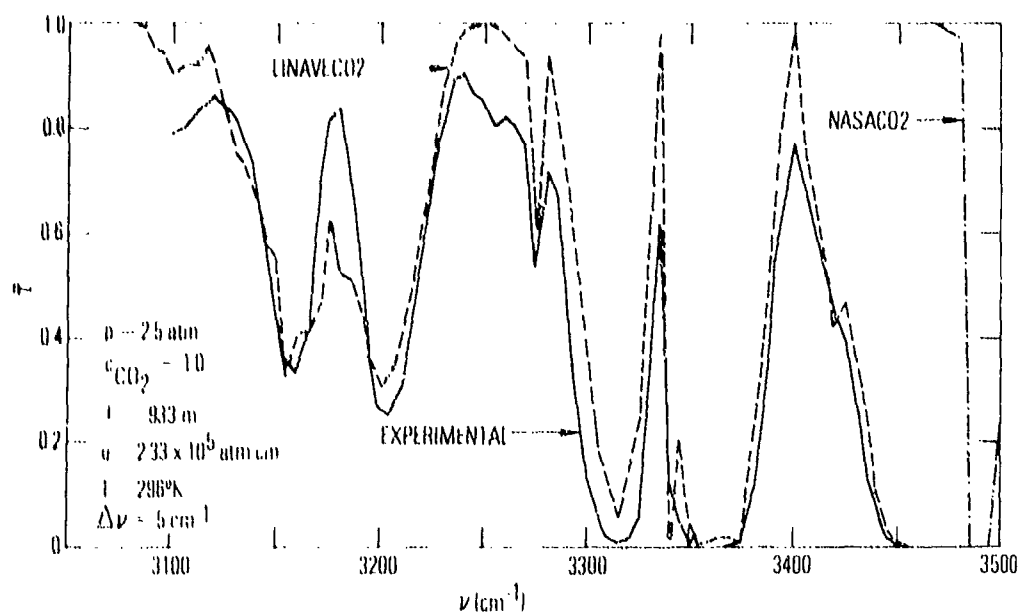


Fig. 2. Low-Temperature Transmission Spectra for CO_2 in the Band Wing Region. The LINAVECO2 and NASACO2 curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 9 for sample no. 1 and for $\Delta\nu = 5 \text{ cm}^{-1}$.

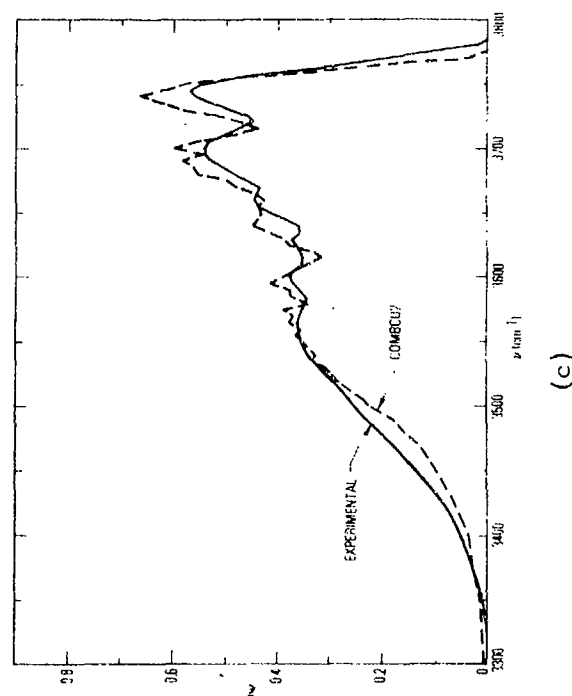
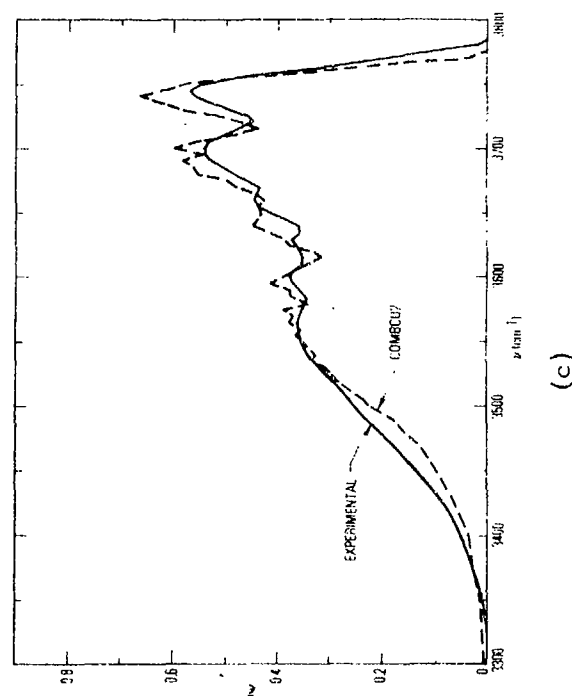
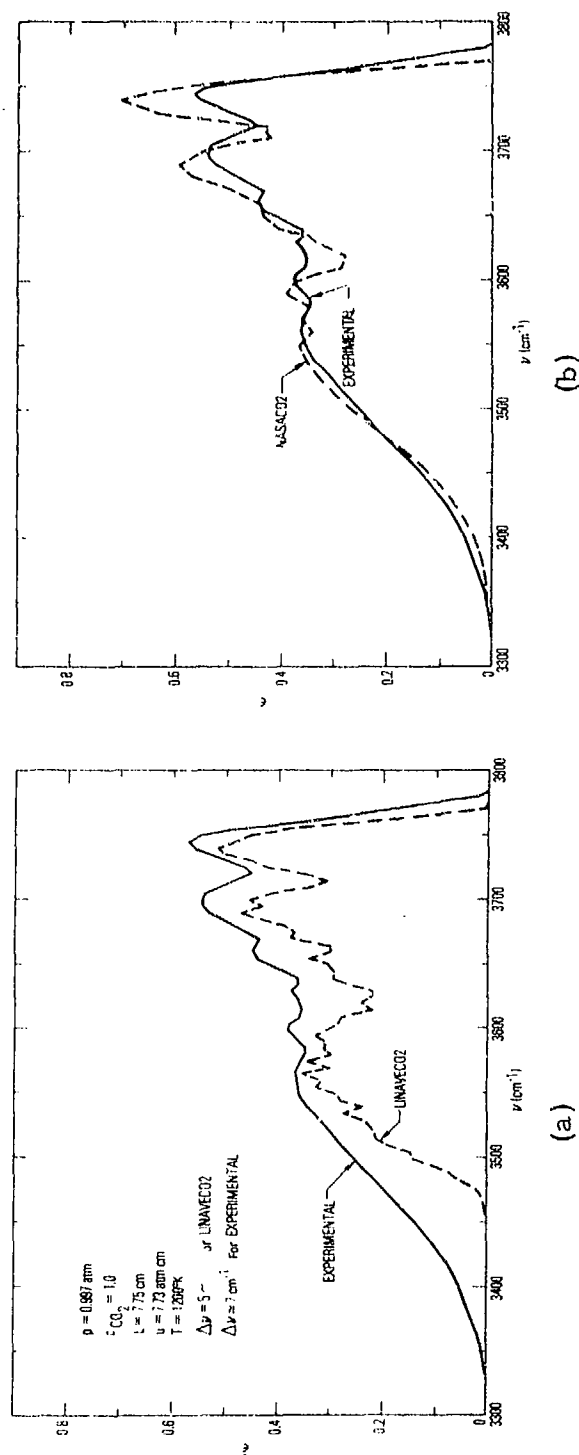


Fig. 3. High-Temperature Emission Spectra for CO_2 . The LINAVECO2 (a), NASACO2 (b), and COMBCO2 (c) curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is taken from Ref. 10.

parameters, on the other hand, provide results that are in excellent agreement with the experimental spectrum for the whole spectral region below $\nu \approx 3600$ cm^{-1} and that are in adequate agreement for the rest of the band.

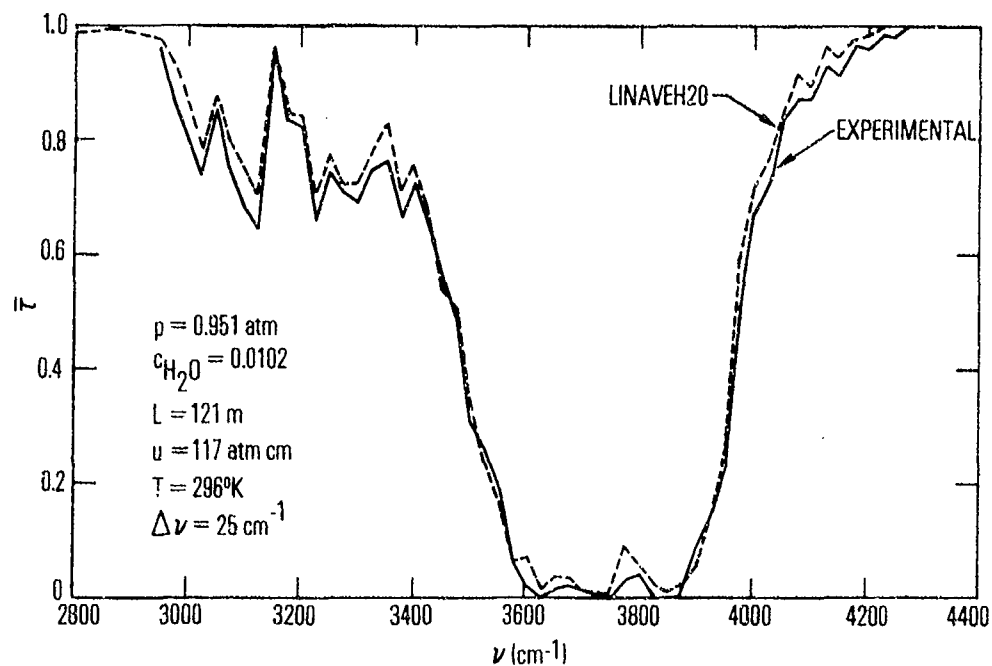
3. H_2O At 296°K

High-resolution spectra and tables of integrated absorptance similar to those of CO_2 are given for H_2O by Burch et al.¹¹ The solid curve of Fig. 4 is the transmittance spectrum for sample no. 39 with $p = 0.951$ atm, $c = 0.0102$ (with N_2 as the remaining gas), and $L = 121$ m. The optical thickness is $u = 117$ atm cm and $\Delta\nu = 25$ cm^{-1} . Figure 4(a) shows the comparison of the experimental spectrum with the spectrum computed with the LINA VEH_2O parameters. The agreement between the two spectra is very good over the whole region from 2950 to 4300 cm^{-1} . Figure 4(b) displays the comparison with the result obtained using the NASA H_2O parameters. As for CO_2 , only a general qualitative agreement exists between the two curves; the quantitative agreement is decidedly poor.

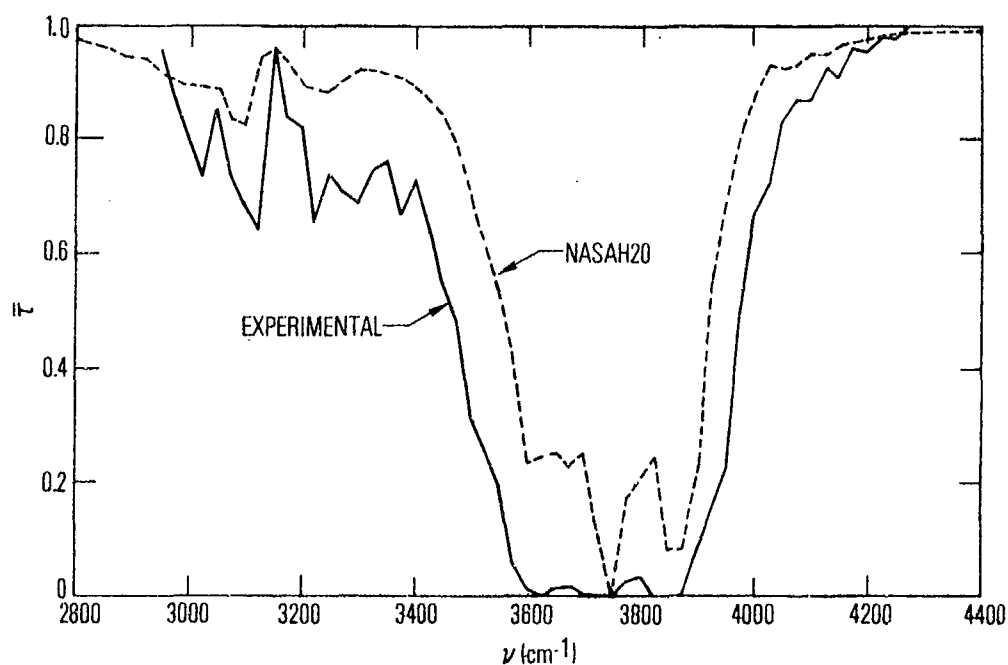
A comparison in the band center region from 3400 to 4200 cm^{-1} for a less absorbing sample is given in Fig. 5. The experimental conditions (sample no. 38) are: $p = 0.176$ atm, $c = 0.031$, $L = 4.16$ m, and $u = 2.27$ atm cm. Again, the LINA VEH_2O parameters yield excellent agreement with experiment and the NASA H_2O parameters, poor agreement.

A more strongly absorbing sample (sample no. 40) with $p = 0.20$ atm, $c = 0.101$, $L = 933$ m, and $u = 1875$ atm cm was used to show comparison in the wing region from 2800 to 3500 cm^{-1} . The results are given in Fig. 6 and again display the adequacy of the LINA VEH_2O parameters and the inadequacy of the NASA H_2O parameters at yielding accurate low-temperature H_2O absorption spectra.

¹¹D. E. Burch, D. A. Gryvnak, and R. R. Patty, Absorption by H_2O Between 2800 and 4500 cm^{-1} (2.7 Micron Region), U-3202, Aeronutronic Div., Philco-Ford Corp., Newport Beach, Calif. (30 September 1965).



(a)



(b)

Fig. 4. Low-Temperature Transmission Spectra for H_2O . The LINA VEH2O (a) and NASA H2O (b) curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 11 for sample no. 39 and for $\Delta\nu \approx 25 \text{ cm}^{-1}$.

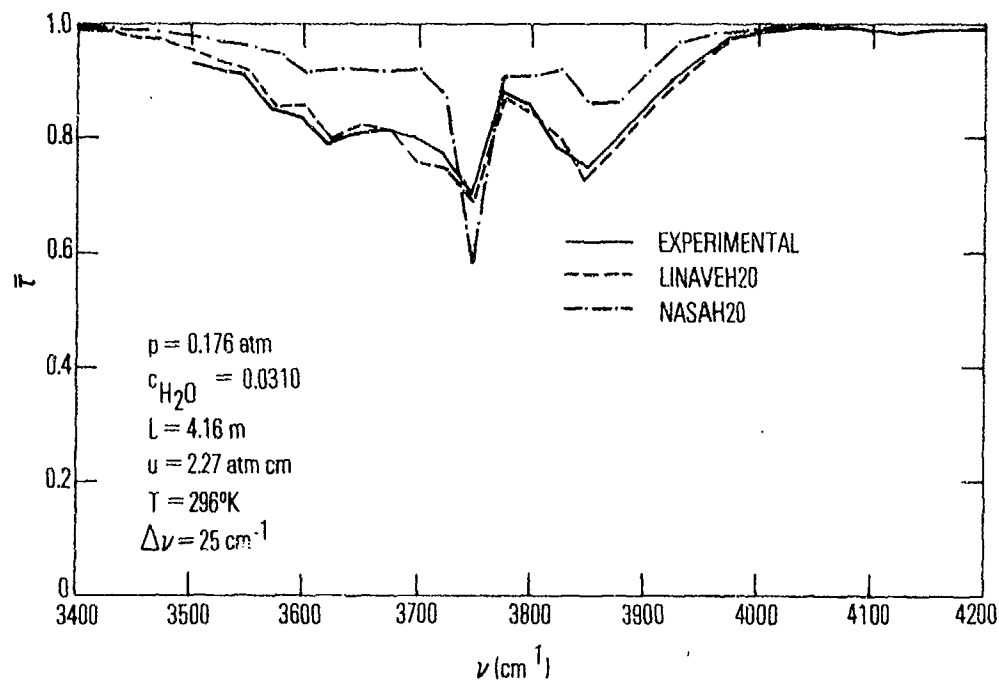


Fig. 5. Low-Temperature Transmission Spectra for H_2O in the Band Center Region. The LINAHEH2O and NASAH2O curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 11 for sample no. 38 and for $\Delta\nu = 25 \text{ cm}^{-1}$.

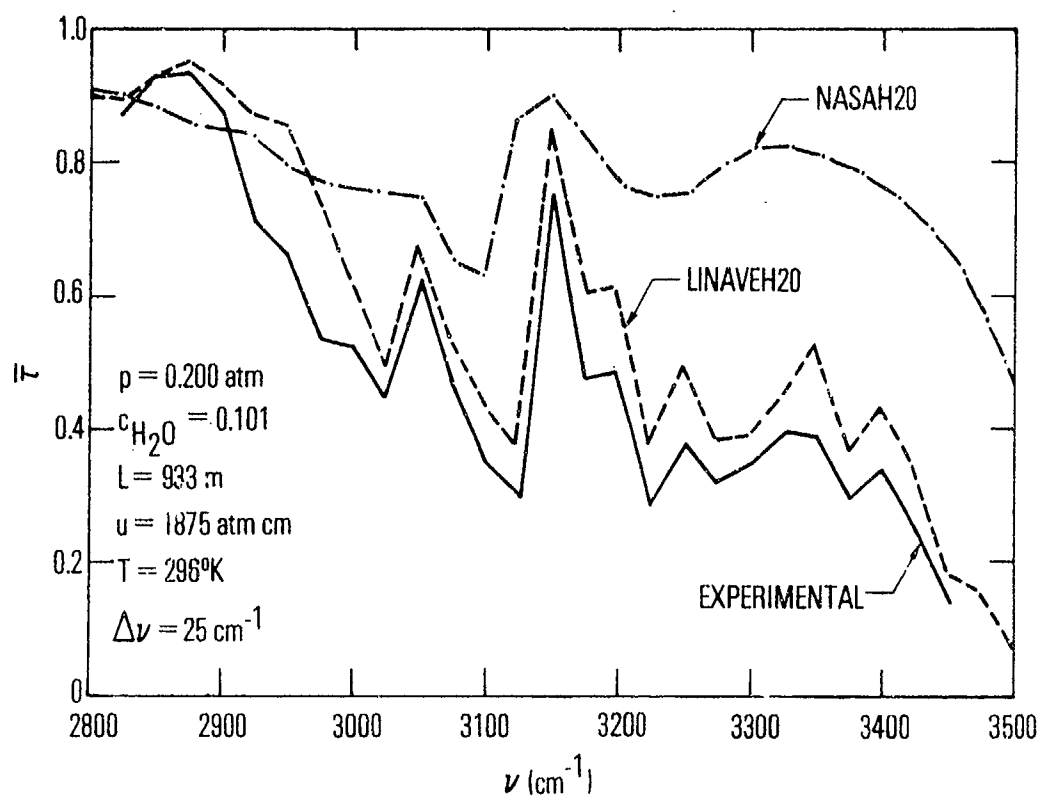


Fig. 6. Low-Temperature Transmission Spectra for H_2O in the Band Wing Region. The LINAVERH2O and NASAH2O curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is derived from the tables of Ref. 11 for sample no. 40 and for $\Delta\nu = 25 \text{ cm}^{-1}$.

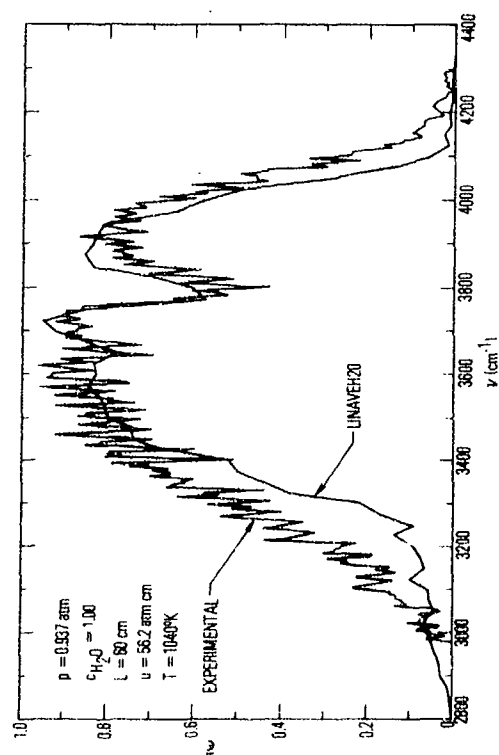
4. H₂O AT 1040°K

A medium resolution emissivity spectrum for pure H₂O given by Simmons et al.¹² was used for this comparison. The experimental conditions are: $p = 0.937$ atm, $c = 1.00$, $L = 60$ cm, $T = 1040^\circ\text{K}$, and $u = 56.2$ atm cm. The experimental spectrum and the results using the LINAVEH₂O parameters are shown in Fig. 7(a) while the results using the NASAH₂O parameters are shown in Fig. 7(b). In the band center region between 3400 and 4050 cm^{-1} , either set approximately reproduces the band contour of the experimental result, with the LINAVEH₂O parameters possibly giving a slightly better fit. In the wing regions above 4050 cm^{-1} and below 3400 cm^{-1} , the LINAVEH₂O parameters significantly underestimate the emissivity. The NASAH₂O parameters, on the other hand, provide results that are in excellent agreement with the experimental wing contours. There is a general underestimation of the emissivity by the NASAH₂O parameters between 3400 and 3700 cm^{-1} . It should be remembered, however, that even at this temperature, these parameters are not experimentally measured but are extrapolated from higher temperature measurements. An example of the good fit between measured and computed values at 2500°K is given in Ref. 3.

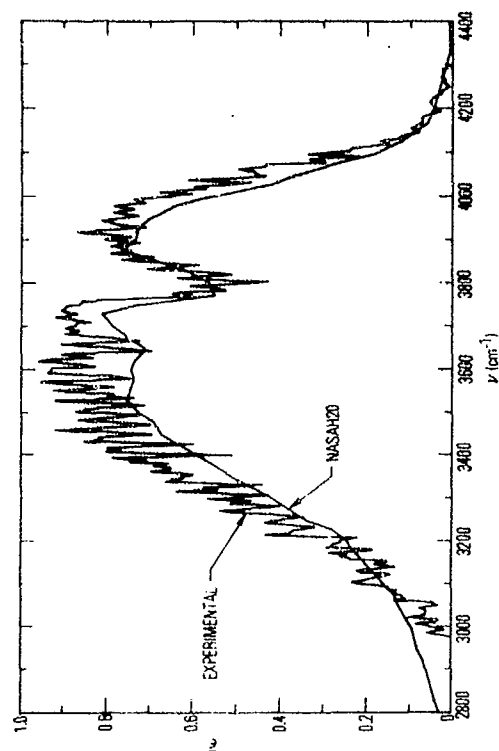
These comparisons confirm the initial suspicions that the LINAVE parameters should be adequate for low-temperature applications but deficient at high temperatures whereas the converse is generally true for the NASA parameters. To summarize the comparison results:

1. The LINAVE parameters are adequate for both CO₂ and H₂O throughout the $2.7\text{-}\mu\text{m}$ bands of these species for $T \approx 300^\circ\text{K}$.
2. The LINAVE parameters are adequate near the $2.7\text{-}\mu\text{m}$ band centers for temperatures at least as high as $T \approx 1000^\circ\text{K}$ but are inadequate in the band wings for this and higher temperatures. This holds for both H₂O and CO₂.

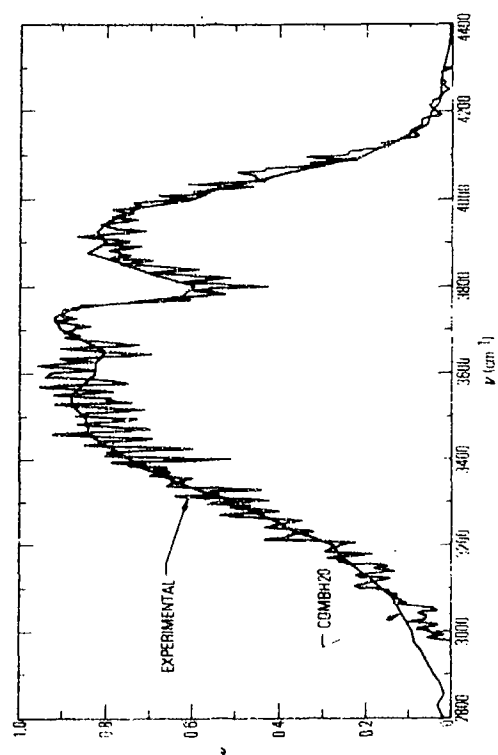
¹²F. S. Simmons, C. B. Arnold, and D. H. Smith, Studies of Infrared Radiative Transfer in Hot Gases, I: Spectral Absorptance Measurements in the $2.7\text{-}\mu\text{H}_2\text{O}$ Bands, Rep. No. 4613-91-T, Willow Run Laboratory, Ann Arbor, Mich. (August 1965).



(a)



(b)



(c)

Fig. 7. High-Temperature Emission Spectra for H_2O . The LINAVEH2O (a), NASA H2O (b), and COMB H2O (c) curves show spectra computed with the indicated band model parameter set. The EXPERIMENTAL curve is taken from Ref. 12.

3. The NASA parameters are adequate for both CO_2 and H_2O throughout the $2.7\text{-}\mu\text{m}$ bands of these species for temperatures above $T \approx 1000^\circ\text{K}$.
4. The NASA parameters are inadequate for both H_2O and CO_2 anywhere in the $2.7\text{-}\mu\text{m}$ spectral region for $T \approx 300^\circ\text{K}$.

III. COMBINED PARAMETER SETS

A. GENERAL PROCEDURE

Parameter sets for both CO_2 and H_2O that are consistent for the whole temperature range from 100 to 3000°K were generated by combining the low-temperature variation of the LINAVE parameters with the high-temperature variation of the NASA parameters. This combination was performed at each spectral position by making semilogarithmic plots of the parameters from each set as functions of temperature, and connecting some "low" temperature point on the LINAVE curve with some "high" temperature point on the NASA curve. The designations "low" and "high" temperature are relative terms only, since the connection at some spectral positions was best done by connecting, for example, the 1000°K value for the LINAVE parameter with the 1500°K value for the NASA parameter or, in other cases, the 250°K value of the LINAVE parameter with the 300°K value for the NASA parameter. Examples of the method are given in Figs. 8 through 11 for several spectral intervals for both CO_2 and H_2O .

This procedure is admittedly subjective, although several rules and guidelines were followed for making the transition from one curve to the other:

1. The transition from one curve to the other should make the overall variation as smooth as possible.
2. The LINAVE parameters for $T \lesssim 300^\circ\text{K}$ should remain reasonably unchanged.
3. The NASA parameters for $T \gtrsim 2000^\circ\text{K}$ should remain reasonably unchanged.
4. No redefinition of parameter values in either set is made. The temperature variation of the combined set consists of established values from one set or the other, or values interpolated from the transition line.
5. The match-up for each spectral interval should be consistent with the match-up made for adjacent spectral intervals.
6. The match-up for δ_e should reflect a monotonic increase of the density ($1/\delta_e$) with temperature.

Even with these guidelines, several ways of connecting the sets were sometimes possible. An iterative procedure was used in these cases. A first-guess match-up was made and spectra generated for the homogeneous path conditions described in the previous section. A comparison of these spectra with the experimental curves and inspection of the parameter plots were made to see if another transition line would give a better result. If it could, the change was made and tested by generating new spectra for comparison.

B. H₂O PARAMETER SET (COMBH₂O)

Parameter plots for both $\bar{k}$ and $1/\delta_e$ were made for 81 spectral positions from 2500 to 4500 cm^{-1} (equal steps of 25 cm^{-1}). The four main types of variations for $\bar{k}$ that occurred are shown in Fig. 8. The LINAVEH₂O variation displayed in Fig. 8(a) ($\nu = 2500 \text{ cm}^{-1}$) is typical for all of the spectral intervals in the band wing region. The absorption coefficient increases with temperature up to $\sim 1000^\circ\text{K}$ but thereafter levels off or falls slightly. The increasing discrepancy between the LINAVEH₂O and the NASAH₂O curves reflects the lack of hot band lines in the AFCRL atlas for the wing region.

Figures 8(a) ($\nu = 2500 \text{ cm}^{-1}$) and 8(d) ($\nu = 4075 \text{ cm}^{-1}$) show variations in which several reasonable transition lines could be drawn. In the latter ($\nu = 4075 \text{ cm}^{-1}$), the line from 150°K on the LINAVEH₂O curve to 300°K on the NASAH₂O curve was the first guess based on the "smoothness" criterion. Better overall agreement with the experimental spectra, however, was obtained using the transition line from 300°K on the LINAVEH₂O curve to 1000°K on the NASAH₂O curve. The variations at $\nu = 3400$ and 3700 cm^{-1} [Figs. 8(b) and 8(c), respectively] are examples where little judgment was required to make the match-up. In general, throughout regions of strong absorption, the match-up procedure was relatively self-evident.

The variations of δ_e for H₂O with temperature were very consistent throughout the whole spectral region and were simple variations of the forms shown in Fig. 9. In all cases, the first-guess match-up was sufficient.

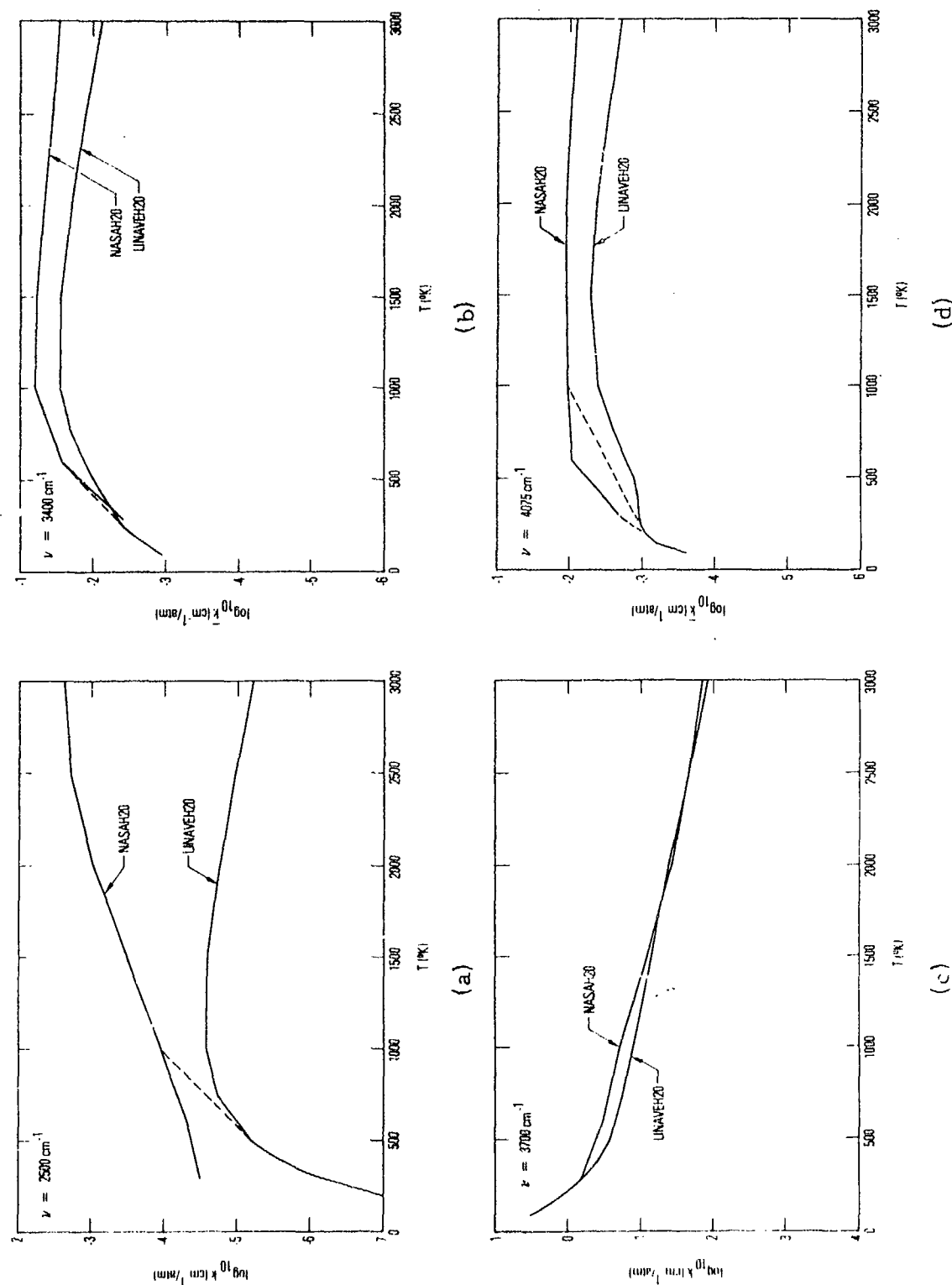
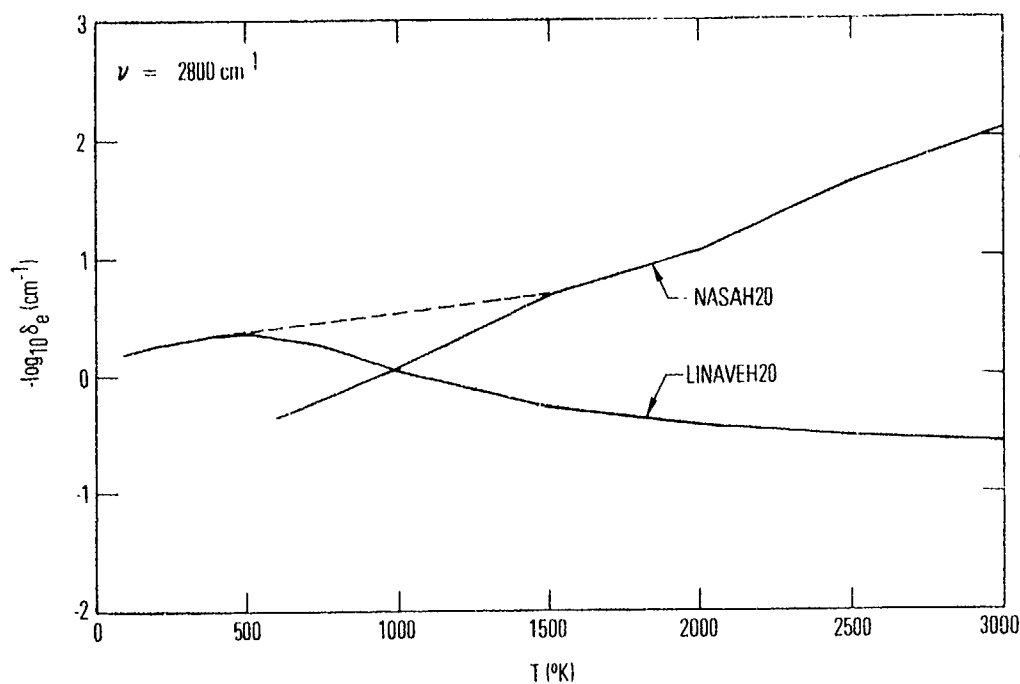
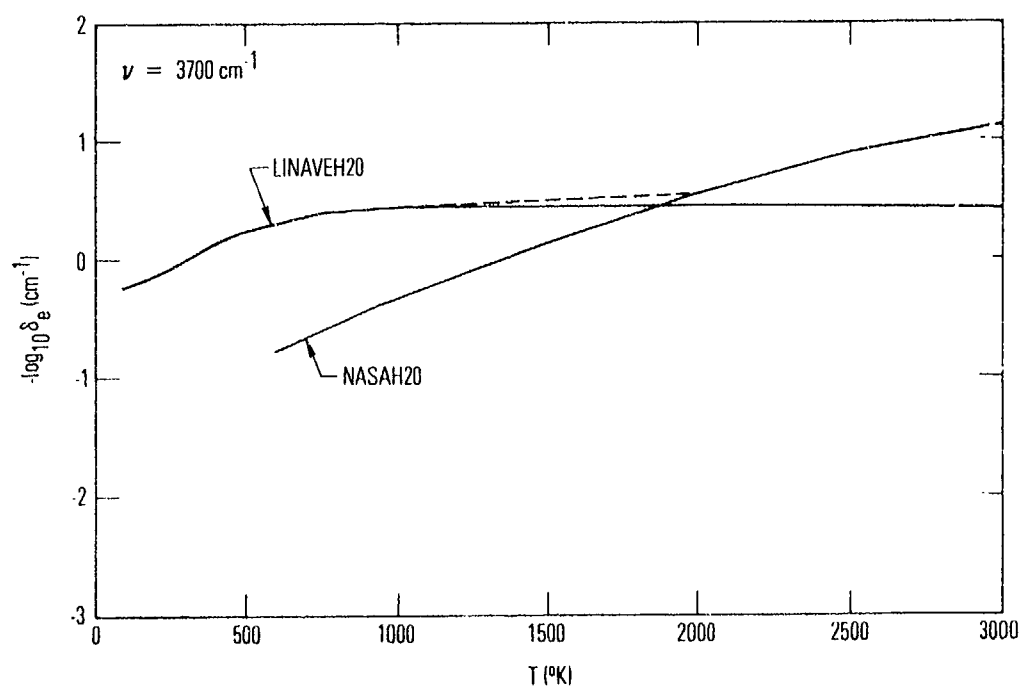


Fig. 8. Variation of $\bar{k}(\text{H}_2\text{O})$ with Temperature for Selected Spectral Intervals. The LINA H2O and NASA H2O curves are the variations for the indicated band model parameter set; dashed curves show transitions from one curve to the other.



(a)



(b)

Fig. 9. Variation of $1/\delta_e$ (H₂O) with Temperature for Selected Spectral Intervals. The LINAVERH2O and NASAH2O curves are the variations for the indicated band model parameter set; dashed curves show transitions from one curve to the other.

A final parameter set was generated for H_2O for the spectral region $\nu = 2500$ to 4500 cm^{-1} by steps of 25 cm^{-1} and reflects a spectral resolution of $\Delta\nu = 25 \text{ cm}^{-1}$. The ten temperature values $T = 100, 200, 300, 500, 750, 1000, 1500, 2000, 2500,$ and 3000°K were chosen to represent the temperature variation. The mean line width parameter $\bar{\gamma}_0$ from the LINAVEH2O set was chosen to represent this parameter for the combined set. Spectra for the homogeneous path conditions of Sect. II were generated with the final parameter set to verify its validity. For all of the low-temperature cases, the spectra generated with the COMBH2O parameters were indistinguishable (in plots) from those generated using the LINAVEH2O parameters. The spectrum for the 1040°K path is shown in Fig. 7(c). The overall agreement with the experimental curve is better than was obtained with either the LINAVEH2O or NASAH2O parameters. A tabulation of the COMBH2O parameter set is included in the Appendix.

C. CO_2 PARAMETER SET (COMBCO2)

Parameter plots for $\bar{k}$ and $1/\delta_e$ were made for the 135 spectral positions from 3100 to 3770 cm^{-1} (equal steps of 5 cm^{-1}). Examples of match-ups are illustrated in Fig. 10. In the band wing region, the variation of the LINAVE $\bar{k}$ parameter is similar to that for H_2O in the wing region. That is, the value increases with temperature up to about 500°K and then decreases owing to the lack of data in the AFCRL compilation for hot band lines. The examples for $\nu = 3525$ and 3725 cm^{-1} in Fig. 10 are cases where the match-up is easily made.

Examples of the match-up of the line spacing parameter δ_e are shown in Fig. 11. In most cases, the selection of the transition line was reasonably self-evident.

After several match-up iterations, a final parameter set was generated for CO_2 for the spectral region $\nu = 3100$ to 3770 cm^{-1} by steps of 5 cm^{-1} and reflects a spectral resolution of $\Delta\nu = 5 \text{ cm}^{-1}$. The same ten temperatures as for H_2O were chosen to represent the temperature variation of the set.

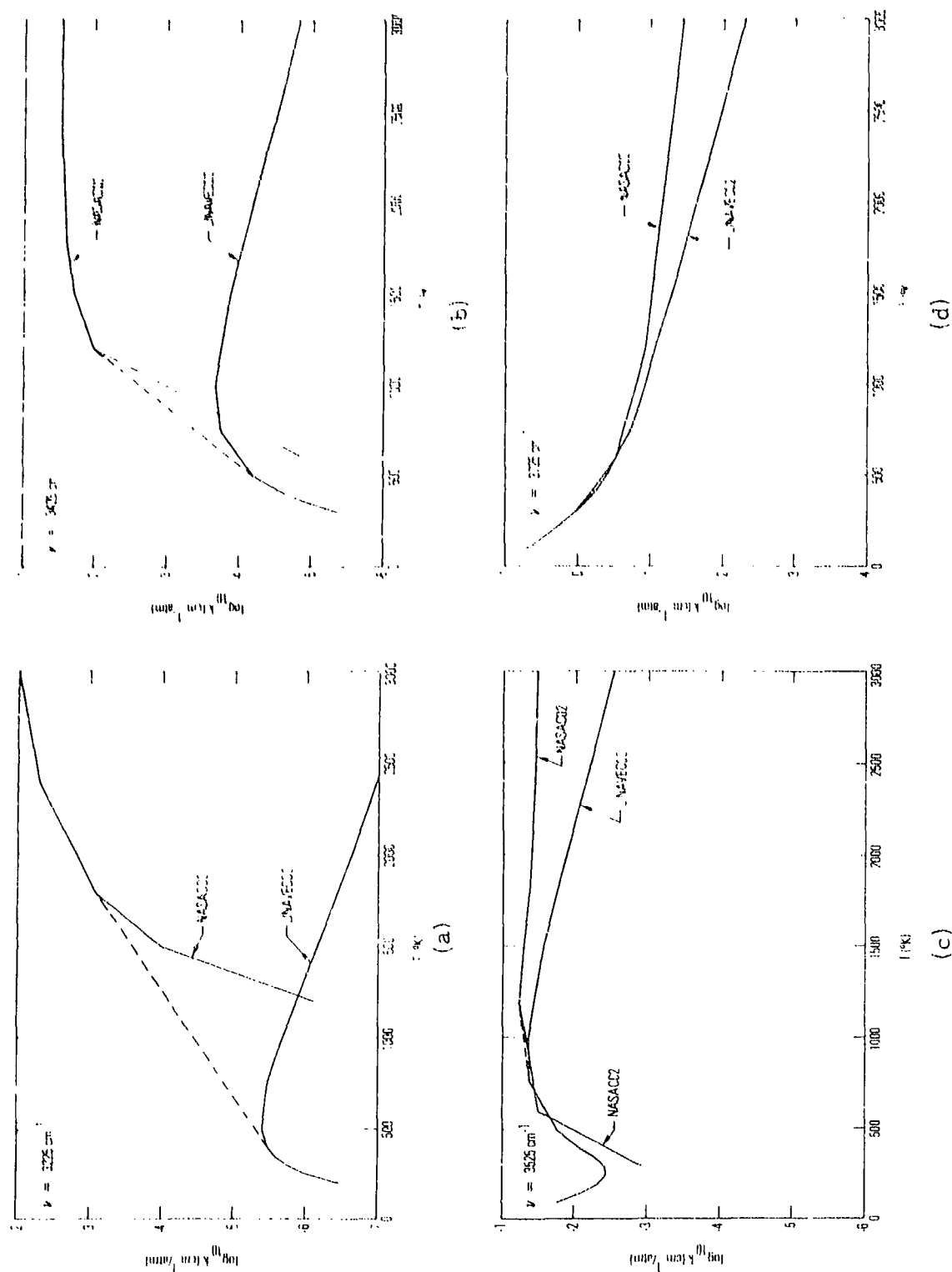
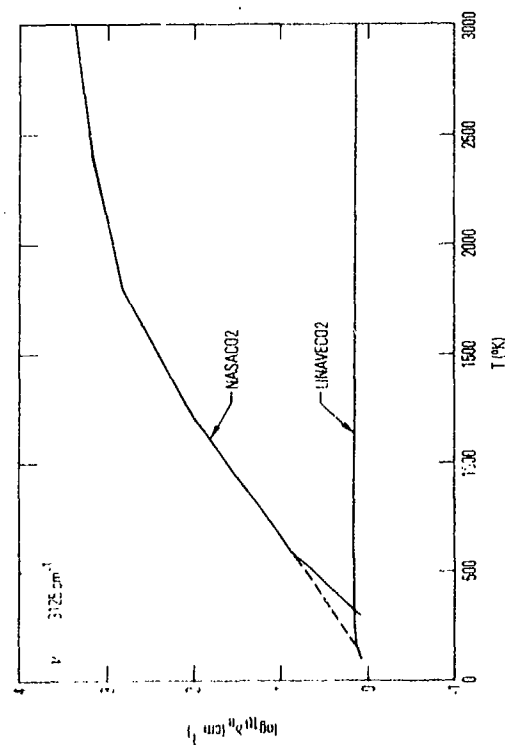
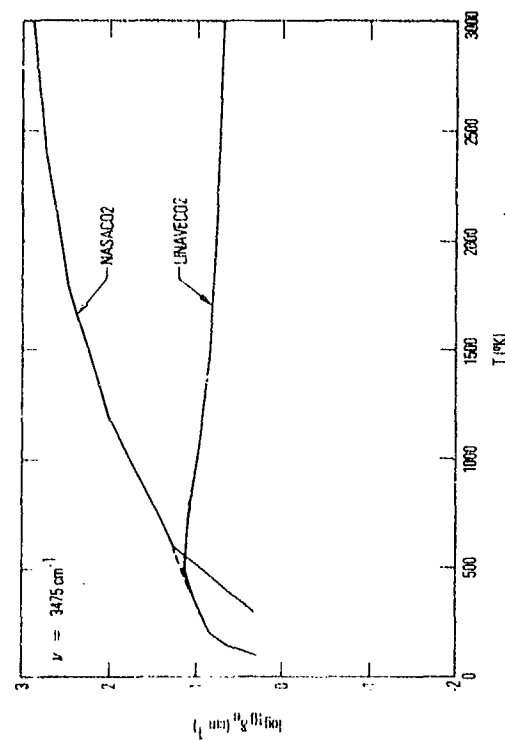


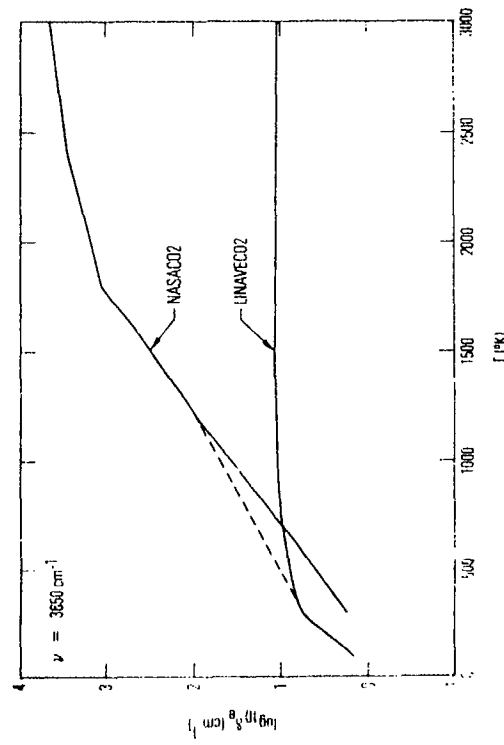
Fig. 10. Variation of $\bar{k}(\text{CO}_2)$ with Temperature for Selected Spectral Intervals. The LINAVECO2 and NASACO2 curves are the variations for the indicated band model parameter set; dashed curves show transitions from one curve to the other.



(a)



(b)



(c)

Fig. 11. Variation of $1/\delta_e(\text{CO}_2)$ with Temperature for Selected Spectral Intervals. The LINAVECO2 and NASAC02 curves are the variations for the indicated band model parameter set; dashed curves show transitions from one curve to the other.

The mean line width parameter $\bar{\gamma}_0$ from the LINAVERCO2 set was chosen to represent this parameter in the final set. The $\bar{k}$ and $1/\delta_e$ parameters of the LINAVERCO2 set are zero for the 5-cm^{-1} intervals centered on $\nu = 3245$ and 3250 cm^{-1} because no lines occur in these regions. The data from the NASACO2 set for the whole temperature range were used for these intervals.

Spectra for the homogeneous path conditions of Sect. II were computed with the final parameter set to verify its validity. For the low-temperature cases, the results were indistinguishable from the LINAVERCO2 curves of Figs. 1 and 2 except in the 3625- and 3725-cm^{-1} valleys, where a slight improvement in agreement with the experimental curve was noted. The spectrum for the 1200°K case is shown in Fig. 3(c). The overall agreement with the experimental curve is better than was obtained with either the LINAVERCO2 or NASACO2 parameters. A tabulation of the COMBCO2 parameters is included in the Appendix.

IV. ATMOSPHERIC TRANSMITTANCE CALCULATION

In Ref. 1, radiative transfer calculations for two atmospheric paths and a hypothetical hot $\text{H}_2\text{O}/\text{CO}_2$ plume at 20-km altitude were made with either the LINAVE or NASA parameters. The results for the slant path (20 km to space at a 75-deg zenith angle) have been recomputed for the LINAVE and NASA parameters and are compared here with the results obtained using the COMB parameters. The source path represents a single line of sight through the diameter position of a homogeneous, isothermal, circular cylindrical plume at an aspect angle of 90 deg. The source path length is 7.73 m, the temperature is 1249°K, the mole fraction of H_2O is 0.2533, and the mole fraction of CO_2 is 0.03714. A tropical model atmosphere was used.¹³ The calculations were performed for the Lorentz line shape, with an exponential-tailed inverse line strength distribution, and used the Lindquist-Simmons approximation.

The band model parameters for CO_2 were reduced in resolution from 5 to 25 cm^{-1} in order to be compatible with the resolution of the H_2O parameters. The band model parameters for the 5- cm^{-1} -wide interval centered on ν_i and the parameters for the two lower and two higher adjacent intervals were averaged to give the parameters for the 25- cm^{-1} -wide interval centered on ν_i according to

$$\bar{k} = \frac{1}{5} \sum_{j=i-2}^{i+2} \bar{k}(j)$$

¹³R. A. McClatchey, R. W. Fenn, J. E. A. Selby, F. E. Volz, and J. S. Garing, Optical Properties of the Atmosphere (Revised), AFCRL-71-0279, Air Force Cambridge Research Laboratories, Mass. (10 May 1971).

$$\bar{\gamma}_0 = \frac{1}{5} \sum_{j=i-2}^{i+2} \bar{\gamma}_0(j)$$

and

$$\frac{1}{\delta_e} = \frac{1}{\bar{k} \bar{\gamma}_0} \left[\frac{1}{5} \sum_{j=i-2}^{i+2} \sqrt{\frac{\bar{k}(j) \bar{\gamma}_0(j)}{\delta_e(j)}} \right]^2$$

The results obtained with the three parameter sets for the radiance at the boundary of the source and after transmission along the absorbing atmospheric path are shown in Fig. 12. The transmittance $\bar{\tau}$, obtained without account of line correlation, is illustrated in Fig. 13. Similarly, the effective transmittance of the atmosphere $\bar{\tau}_e$, obtained by taking account of line correlation between the source emission spectrum and the atmospheric absorption spectrum, is given in Fig. 14. Detailed discussions of the source radiance and atmospheric transmittance $\bar{\tau}$ spectra are not required since these would parallel those already given in Sect. II of this report. The only new result displayed by these spectra is the effective transmittance $\bar{\tau}_e$ (Fig. 14). Although $\bar{\tau}_e$ is a source-dependent quantity and, therefore, depends on the band model parameters used to describe the source emission, there is a great similarity between the $\bar{\tau}_e$ spectra computed using the LINAVE and COMB parameters. A comparison between the NASA and COMB results, on the other hand, reveals a significant dissimilarity. These results would indicate that an accurate description of the atmosphere (that is, an accurate knowledge of band model parameters for low temperatures) is more important than an accurate description of the hot gas source in determining $\bar{\tau}_e$.

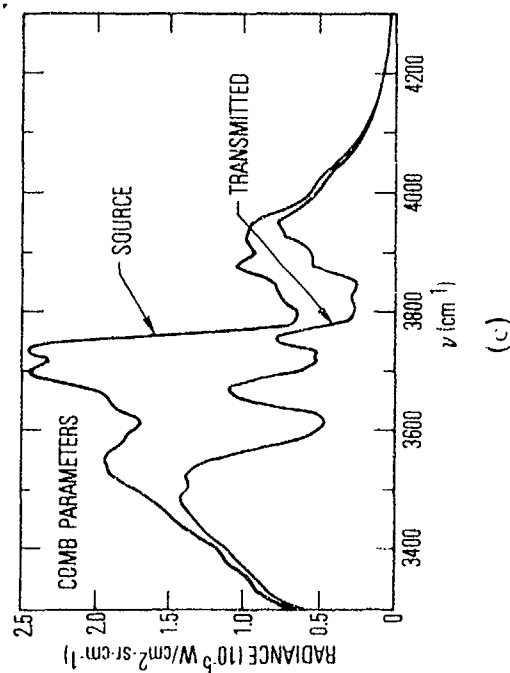
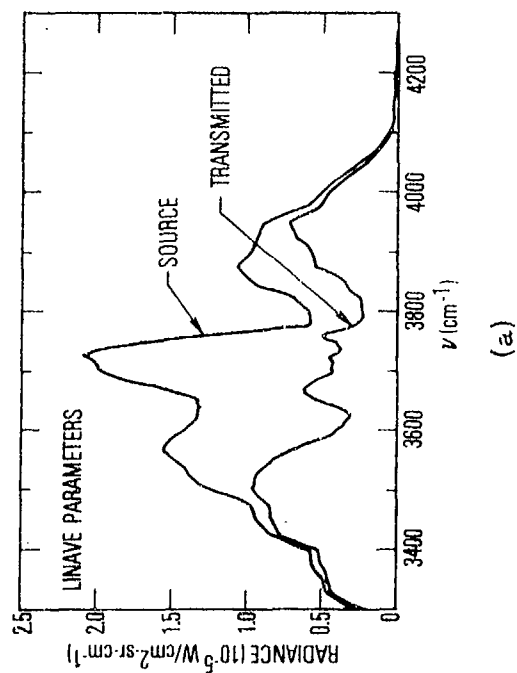
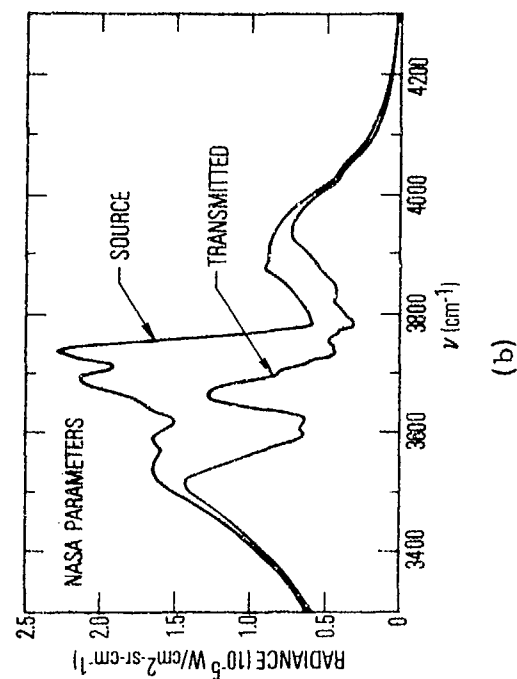


Fig. 12. Source and Transmitted Radiance Spectra for Atmospheric Slant Path. (a) Results using LINAVE parameters; (b) Results using NASA parameters; (c) Results using COMB parameters.

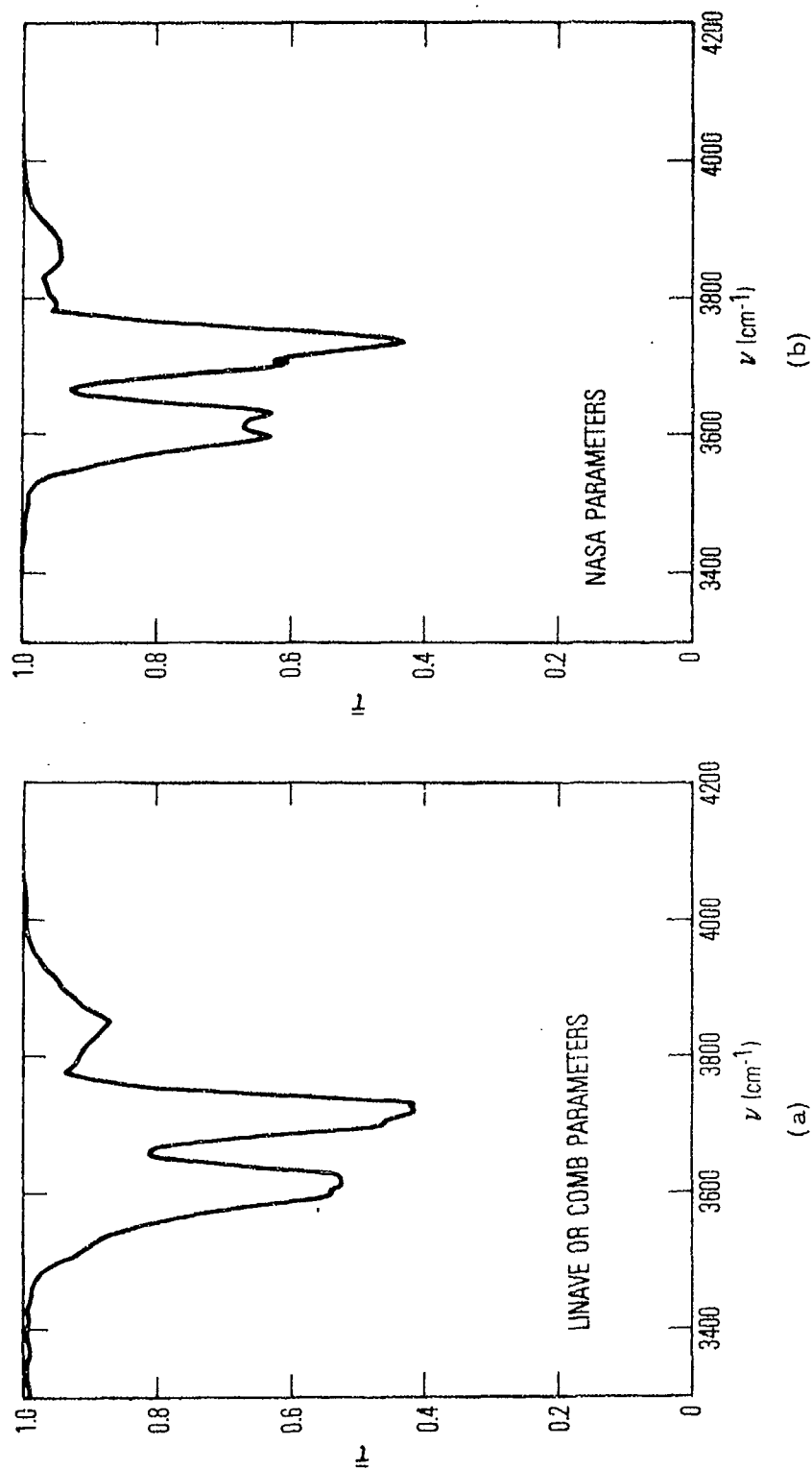
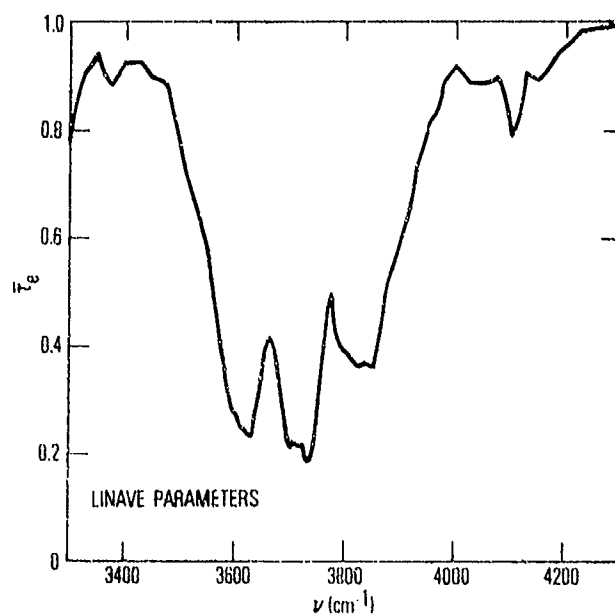
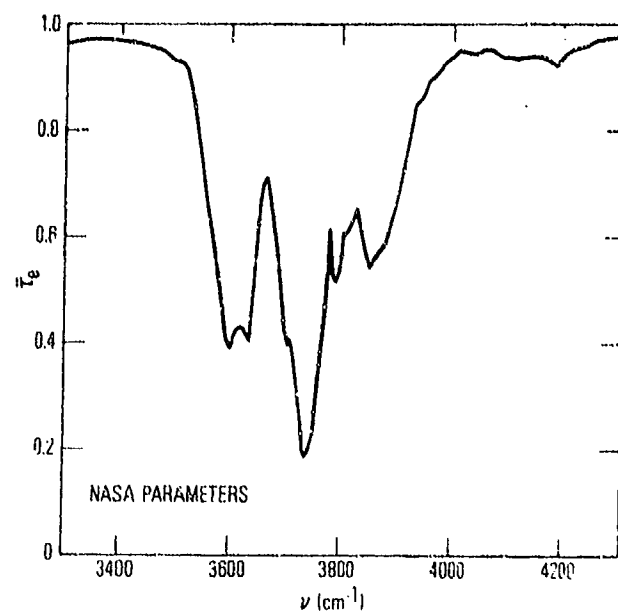


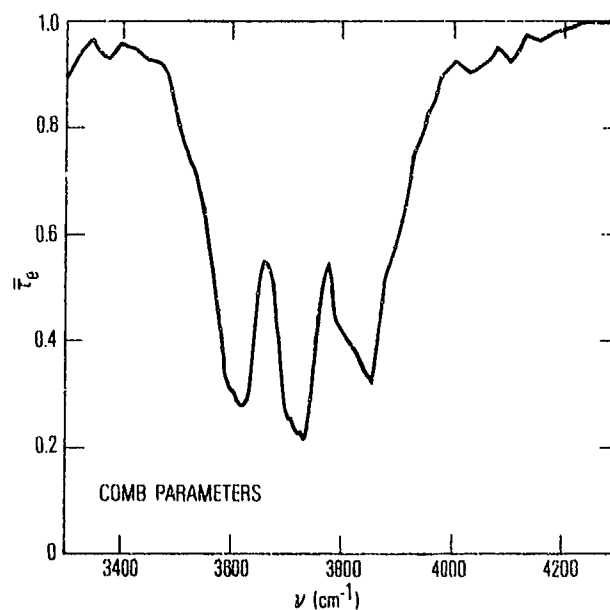
Fig. 13. Transmittance Spectra for Atmospheric Slant Path. (a) Results using LINAVE or COMB parameters; (b) Results using NASA parameters.



(a)



(b)



(c)

Fig. 14. Effective Transmittance Spectra for Atmospheric Slant Path.
(a) Results using LINAVE parameters; (b) Results using NASA parameters; (c) Results using COMB parameters.

APPENDIX

COMBH2O AND COMBCO2 PARAMETER SET LISTINGS

Tabulations of the COMBH2O and COMBCO2 parameters are given in Tables A1 and A2, respectively. A description of these listings follows. IDNAME is simply an identification name for the parameter set. RESOLUTION is the value of $\Delta\nu$ appropriate for the set. ALPHA (1) through ALPHA (5) are the ratios of the efficiency of pressure broadening by the indicated mechanisms to that of nonresonant self-broadening. ALPHA (6) is the atomic mass of the absorbing species. The WAVENUMBER array lists the center value of all the $\Delta\nu$ intervals included in the set. NW is the number of such intervals. The TEMPERATURE array similarly lists the temperatures for which the data are tabulated. NT is the number of such temperatures. The ABSORPTION COEFFICIENT array is $\bar{k}$. The first column of this array is the interval center wave number, and the rows are the values at the temperatures of the TEMPERATURE array. The EFFECTIVE LINE DENSITY array is the parameter $1/\delta_e$ and is presented in the same format as $\bar{k}$. The MEAN LINE WIDTH array is the parameter $\bar{\gamma}_0$ for nonresonant self-broadening at STP. The values correspond to the wave numbers listed in the WAVENUMBER array.

Table A1. Listing of COMBH2O Band Model Parameter Set

BAND MODEL PARAMETERS			
IONAME		COMBH2O	
RESOLUTION(CM-1)		25.0000	
ALPHA(1)	.4390E+01	RESPONANT SELF-BROADENING	
ALPHA(2)	0.	FOREIGN-GAS BROADENING(H2O)	
ALPHA(3)	.1330E+01	FOREIGN-GAS BROADENING(CO2)	
ALPHA(4)	.1000E+01	FOREIGN-GAS BROADENING(N2)	
ALPHA(5)	.4440E+00	FOREIGN-GAS BROADENING(O2)	
ALPHA(6)	.1800E+02	ATOMIC WEIGHT(CMU)	
WAVENUMBER(WN)	APRAY(CM-1)	NW	RI
2.500E+03	2.525E+03	2.550E+03	2.575E+03
2.750E+03	2.775E+03	2.800E+03	2.825E+03
3.000E+03	3.025E+03	3.050E+03	3.075E+03
3.250E+03	3.275E+03	3.300E+03	3.325E+03
3.500E+03	3.525E+03	3.550E+03	3.575E+03
3.750E+03	3.775E+03	3.800E+03	3.825E+03
4.000E+03	4.025E+03	4.050E+03	4.075E+03
4.250E+03	4.275E+03	4.300E+03	4.325E+03
4.500E+03			
TEMPERATURE(T)	ARRAY(DEGK)	NT=	10
1.000E+02	2.000E+02	3.000E+02	5.000E+02
		7.500E+02	1.000E+03
		1.500E+03	2.000E+03
		2.500E+03	3.000E+03
ABSORPTION COEFFICIENT(K) ARRAY(CM-1/ATM)			
2500.00	9.160E-09	1.109E-07	6.922E-07
2525.00	3.230E-08	3.548E-07	1.824E-06
2550.00	8.543E-07	9.548E-06	3.400E-05
2575.00	3.458E-06	4.471E-05	1.014E-04
2600.00	2.518E-05	1.624E-04	2.350E-03
2625.00	1.641E-04	3.875E-03	4.231E-02
2650.00	1.111E-03	7.368E-02	6.752E-01
2675.00	1.874E-02	1.106E-01	8.672E-01
2700.00	2.042E-01	9.852E-01	1.191E-01
2725.00	3.327E-01	1.641E-01	1.330E-01
2750.00	5.079E-01	2.666E-01	1.774E-01
2775.00	2.065E-01	1.376E-01	2.375E-01
2800.00	1.050E-01	1.017E-01	1.208E-01
2825.00	6.877E-02	4.817E-02	1.326E-01
2850.00	2.107E-02	2.599E-02	1.901E-01
2875.00	1.344E-02	1.611E-02	1.366E-01
2900.00	1.505E-02	1.798E-02	6.802E-01
2925.00		1.798E-01	
2950.00		3.962E-01	
2975.00		6.994E-01	
3000.00		1.231E-01	
3025.00		2.548E-01	
3050.00		2.293E-01	
3075.00		3.952E-01	
3100.00		7.677E-01	
3125.00		1.755E-01	
3150.00		1.755E-01	
3175.00		1.755E-01	
3200.00		1.755E-01	
3225.00		1.755E-01	
3250.00		1.755E-01	
3275.00		1.755E-01	
3300.00		1.755E-01	
3325.00		1.755E-01	
3350.00		1.755E-01	
3375.00		1.755E-01	
3400.00		1.755E-01	
3425.00		1.755E-01	
3450.00		1.755E-01	
3475.00		1.755E-01	
3500.00		1.755E-01	
3525.00		1.755E-01	
3550.00		1.755E-01	
3575.00		1.755E-01	
3600.00		1.755E-01	
3625.00		1.755E-01	
3650.00		1.755E-01	
3675.00		1.755E-01	
3700.00		1.755E-01	
3725.00		1.755E-01	
3750.00		1.755E-01	
3775.00		1.755E-01	
3800.00		1.755E-01	
3825.00		1.755E-01	
3850.00		1.755E-01	
3875.00		1.755E-01	
3900.00		1.755E-01	
3925.00		1.755E-01	
3950.00		1.755E-01	
3975.00		1.755E-01	
4000.00		1.755E-01	

Table A1. Listing of COMBH2O Band Model Parameter Set (Cont'd)

[illegible]

Table A1. Listing of COMBH2O Band Model Parameter Set (Cont'd)

[illegible]

Table A1. Listing of COMBH2O Band Model Parameter Set (Cont'd)

[illegible]

HEAVY LINEWIDTH(N) ARRAY(CM-17ATM, HWHH = 0.2) NON-RESONANT SELF-BROADENING AT 570)

[illegible]

Table A2. Listing of COMBCO2 Band Model Parameter Set

BAND MODEL PARAMETERS		COMBCO2B	
IDNAME		5.0000	
RESOLUTION(CM-1)			
ALP4A(1)	.1110E+00	RESCNANT SELF-BROADENING	
ALP4A(2)	.7730E+00	FOREIGN-GAS BROADENING(H2O)	
ALP4A(3)	0.	FOREIGN-GAS BROADENING(CO2)	
ALP4A(4)	.7730E+00	FOREIGN-GAS BROADENING(N2)	
ALP4A(5)	.6110E+00	FOREIGN-GAS BROADENING(O2)	
ALP4A(6)	.4400E+02	ATOMIC WEIGHT(AHJ)	

WAVELENGTH(MM)	ARRAY(CM-1)	NW 132
3.100E+03	3.105E+03	3.110E+03
3.150E+03	3.155E+03	3.160E+03
3.200E+03	3.205E+03	3.210E+03
3.250E+03	3.255E+03	3.260E+03
3.300E+03	3.305E+03	3.310E+03
3.350E+03	3.355E+03	3.360E+03
3.400E+03	3.405E+03	3.410E+03
3.450E+03	3.455E+03	3.460E+03
3.500E+03	3.505E+03	3.510E+03
3.550E+03	3.555E+03	3.560E+03
3.600E+03	3.605E+03	3.610E+03
3.650E+03	3.655E+03	3.660E+03
3.700E+03	3.705E+03	3.710E+03
3.750E+03	3.755E+03	3.760E+03
3.800E+03	3.805E+03	3.810E+03
3.850E+03	3.855E+03	3.860E+03
3.900E+03	3.905E+03	3.910E+03
3.950E+03	3.955E+03	3.960E+03
4.000E+03	4.005E+03	4.010E+03
4.050E+03	4.055E+03	4.060E+03
4.100E+03	4.105E+03	4.110E+03
4.150E+03	4.155E+03	4.160E+03
4.200E+03	4.205E+03	4.210E+03
4.250E+03	4.255E+03	4.260E+03
4.300E+03	4.305E+03	4.310E+03
4.350E+03	4.355E+03	4.360E+03
4.400E+03	4.405E+03	4.410E+03
4.450E+03	4.455E+03	4.460E+03
4.500E+03	4.505E+03	4.510E+03
4.550E+03	4.555E+03	4.560E+03
4.600E+03	4.605E+03	4.610E+03
4.650E+03	4.655E+03	4.660E+03
4.700E+03	4.705E+03	4.710E+03
4.750E+03	4.755E+03	4.760E+03
4.800E+03	4.805E+03	4.810E+03
4.850E+03	4.855E+03	4.860E+03
4.900E+03	4.905E+03	4.910E+03
4.950E+03	4.955E+03	4.960E+03
5.000E+03	5.005E+03	5.010E+03
5.050E+03	5.055E+03	5.060E+03
5.100E+03	5.105E+03	5.110E+03
5.150E+03	5.155E+03	5.160E+03
5.200E+03	5.205E+03	5.210E+03
5.250E+03	5.255E+03	5.260E+03
5.300E+03	5.305E+03	5.310E+03
5.350E+03	5.355E+03	5.360E+03
5.400E+03	5.405E+03	5.410E+03
5.450E+03	5.455E+03	5.460E+03
5.500E+03	5.505E+03	5.510E+03
5.550E+03	5.555E+03	5.560E+03
5.600E+03	5.605E+03	5.610E+03
5.650E+03	5.655E+03	5.660E+03
5.700E+03	5.705E+03	5.710E+03
5.750E+03	5.755E+03	5.760E+03
5.800E+03	5.805E+03	5.810E+03
5.850E+03	5.855E+03	5.860E+03
5.900E+03	5.905E+03	5.910E+03
5.950E+03	5.955E+03	5.960E+03
6.000E+03	6.005E+03	6.010E+03
6.050E+03	6.055E+03	6.060E+03
6.100E+03	6.105E+03	6.110E+03
6.150E+03	6.155E+03	6.160E+03
6.200E+03	6.205E+03	6.210E+03
6.250E+03	6.255E+03	6.260E+03
6.300E+03	6.305E+03	6.310E+03
6.350E+03	6.355E+03	6.360E+03
6.400E+03	6.405E+03	6.410E+03
6.450E+03	6.455E+03	6.460E+03
6.500E+03	6.505E+03	6.510E+03
6.550E+03	6.555E+03	6.560E+03
6.600E+03	6.605E+03	6.610E+03
6.650E+03	6.655E+03	6.660E+03
6.700E+03	6.705E+03	6.710E+03
6.750E+03	6.755E+03	6.760E+03
6.800E+03	6.805E+03	6.810E+03
6.850E+03	6.855E+03	6.860E+03
6.900E+03	6.905E+03	6.910E+03
6.950E+03	6.955E+03	6.960E+03
7.000E+03	7.005E+03	7.010E+03
7.050E+03	7.055E+03	7.060E+03
7.100E+03	7.105E+03	7.110E+03
7.150E+03	7.155E+03	7.160E+03
7.200E+03	7.205E+03	7.210E+03
7.250E+03	7.255E+03	7.260E+03
7.300E+03	7.305E+03	7.310E+03
7.350E+03	7.355E+03	7.360E+03
7.400E+03	7.405E+03	7.410E+03
7.450E+03	7.455E+03	7.460E+03
7.500E+03	7.505E+03	7.510E+03
7.550E+03	7.555E+03	7.560E+03
7.600E+03	7.605E+03	7.610E+03
7.650E+03	7.655E+03	7.660E+03
7.700E+03	7.705E+03	7.710E+03
7.750E+03	7.755E+03	7.760E+03
7.800E+03	7.805E+03	7.810E+03
7.850E+03	7.855E+03	7.860E+03
7.900E+03	7.905E+03	7.910E+03
7.950E+03	7.955E+03	7.960E+03
8.000E+03	8.005E+03	8.010E+03
8.050E+03	8.055E+03	8.060E+03
8.100E+03	8.105E+03	8.110E+03
8.150E+03	8.155E+03	8.160E+03
8.200E+03	8.205E+03	8.210E+03
8.250E+03	8.255E+03	8.260E+03
8.300E+03	8.305E+03	8.310E+03
8.350E+03	8.355E+03	8.360E+03
8.400E+03	8.405E+03	8.410E+03
8.450E+03	8.455E+03	8.460E+03
8.500E+03	8.505E+03	8.510E+03
8.550E+03	8.555E+03	8.560E+03
8.600E+03	8.605E+03	8.610E+03
8.650E+03	8.655E+03	8.660E+03
8.700E+03	8.705E+03	8.710E+03
8.750E+03	8.755E+03	8.760E+03
8.800E+03	8.805E+03	8.810E+03
8.850E+03	8.855E+03	8.860E+03
8.900E+03	8.905E+03	8.910E+03
8.950E+03	8.955E+03	8.960E+03
9.000E+03	9.005E+03	9.010E+03
9.050E+03	9.055E+03	9.060E+03
9.100E+03	9.105E+03	9.110E+03
9.150E+03	9.155E+03	9.160E+03
9.200E+03	9.205E+03	9.210E+03
9.250E+03	9.255E+03	9.260E+03
9.300E+03	9.305E+03	9.310E+03
9.350E+03	9.355E+03	9.360E+03
9.400E+03	9.405E+03	9.410E+03
9.450E+03	9.455E+03	9.460E+03
9.500E+03	9.505E+03	9.510E+03
9.550E+03	9.555E+03	9.560E+03
9.600E+03	9.605E+03	9.610E+03
9.650E+03	9.655E+03	9.660E+03
9.700E+03	9.705E+03	9.710E+03
9.750E+03	9.755E+03	9.760E+03
9.800E+03	9.805E+03	9.810E+03
9.850E+03	9.855E+03	9.860E+03
9.900E+03	9.905E+03	9.910E+03
9.950E+03	9.955E+03	9.960E+03
10.000E+03	10.005E+03	10.010E+03

TEMPERATURE(K)	ARRAY(DESK)	NT= 10
1.000E+02	2.000E+02	3.000E+03
2.000E+02	3.000E+02	4.000E+03
3.000E+02	4.000E+02	5.000E+03
4.000E+02	5.000E+02	6.000E+03
5.000E+02	6.000E+02	7.000E+03
6.000E+02	7.000E+02	8.000E+03
7.000E+02	8.000E+02	9.000E+03
8.000E+02	9.000E+02	1.000E+04
9.000E+02	1.000E+03	1.100E+04
1.000E+03	1.100E+03	1.200E+04
1.100E+03	1.200E+03	1.300E+04
1.200E+03	1.300E+03	1.400E+04
1.300E+03	1.400E+03	1.500E+04
1.400E+03	1.500E+03	1.600E+04
1.500E+03	1.600E+03	1.700E+04
1.600E+03	1.700E+03	1.800E+04
1.700E+03	1.800E+03	1.900E+04
1.800E+03	1.900E+03	2.000E+04
1.900E+03	2.000E+03	2.100E+04
2.000E+03	2.100E+03	2.200E+04
2.100E+03	2.200E+03	2.300E+04
2.200E+03	2.300E+03	2.400E+04
2.300E+03	2.400E+03	2.500E+04
2.400E+03	2.500E+03	2.600E+04
2.500E+03	2.600E+03	2.700E+04
2.600E+03	2.700E+03	2.800E+04
2.700E+03	2.800E+03	2.900E+04
2.800E+03	2.900E+03	3.000E+04
2.900E+03	3.000E+03	3.100E+04
3.000E+03	3.100E+03	3.200E+04
3.100E+03	3.200E+03	3.300E+04
3.200E+03	3.300E+03	3.400E+04
3.300E+03	3.400E+03	3.500E+04
3.400E+03	3.500E+03	3.600E+04
3.500E+03	3.600E+03	3.700E+04
3.600E+03	3.700E+03	3.800E+04
3.700E+03	3.800E+03	3.900E+04
3.800E+03	3.900E+03	4.000E+04
3.900E+03	4.000E+03	4.100E+04
4.000E+03	4.100E+03	4.200E+04
4.100E+03	4.200E+03	4.300E+04
4.200E+03	4.300E+03	4.400E+04
4.300E+03	4.400E+03	4.500E+04
4.400E+03	4.500E+03	4.600E+04
4.500E+03	4.600E+03	4.700E+04
4.600E+03	4.700E+03	4.800E+04
4.700E+03	4.800E+03	4.900E+04
4.800E+03	4.900E+03	5.000E+04
4.900E+03	5.000E+03	5.100E+04
5.000E+03	5.100E+03	5.200E+04
5.100E+03	5.200E+03	5.300E+04
5.200E+03	5.300E+03	5.400E+04
5.300E+03	5.400E+03	5.500E+04
5.400E+03	5.500E+03	5.600E+04
5.500E+03	5.600E+03	5.700E+04
5.600E+03	5.700E+03	5.800E+04
5.700E+03	5.800E+03	5.900E+04
5.800E+03	5.900E+03	6.000E+04
5.900E+03	6.000E+03	6.100E+04
6.000E+03	6.100E+03	6.200E+04
6.100E+03	6.200E+03	6.300E+04
6.200E+03	6.300E+03	6.400E+04
6.300E+03	6.400E+03	6.500E+04
6.400E+03	6.500E+03	6.600E+04
6.500E+03	6.600E+03	6.700E+04
6.600E+03	6.700E+03	6.800E+04
6.700E+03	6.800E+03	6.900E+04
6.800E+03	6.900E+03	7.000E+04
6.900E+03	7.000E+03	7.100E+04
7.000E+03	7.100E+03	7.200E+04
7.100E+03	7.200E+03	7.300E+04
7.200E+03	7.300E+03	7.400E+04
7.300E+03	7.400E+03	7.500E+04
7.400E+03	7.500E+03	7.600E+04
7.500E+03	7.600E+03	7.700E+04
7.600E+03	7.700E+03	7.800E+04
7.700E+03	7.800E+03	7.900E+04
7.800E+03	7.900E+03	8.000E+04
7.900E+03	8.000E+03	8.100E+04
8.000E+03	8.100E+03	8.200E+04
8.100E+03	8.200E+03	8.300E+04
8.200E+03	8.300E+03	8.400E+04
8.300E+03	8.400E+03	8.500E+04
8.400E+03	8.500E+03	8.600E+04
8.500E+03	8.600E+03	8.700E+04
8.600E+03	8.700E+03	8.800E+04
8.700E+03	8.800E+03	8.900E+04
8.800E+03	8.900E+03	9.000E+04
8.900E+03	9.000E+03	9.100E+04
9.000E+03	9.100E+03	9.200E+04
9.100E+03	9.200E+03	9.300E+04
9.200E+03	9.300E+03	9.400E+04
9.300E+03	9.400E+03	9.500E+04
9.400E+03	9.500E+03	9.600E+04
9.500E+03	9.600E+03	9.700E+04
9.600E+03	9.700E+03	9.800E+04
9.700E+03	9.800E+03	9.900E+04
9.800E+03	9.900E+03	1.000E+05

ABSORPTION COEFFICIENT(K)	ARRAY(CM-1/ATM)
1.00E-00	1.00E-00
1.05E-00	1.05E-00
1.10E-00	1.10E-00
1.15E-00	1.15E-00
1.20E-00	1.20E-00
1.25E-00	1.25E-00
1.30E-00	1.30E-00
1.35E-00	1.35E-00
1.40E-00	1.40E-00
1.45E-00	1.45E-00
1.50E-00	1.50E-00
1.55E-00	1.55E-00
1.60E-00	1.60E-00
1.65E-00	1.65E-00
1.70E-00	1.70E-00
1.75E-00	1.75E-00
1.80E-00	1.80E-00
1.85E-00	1.85E-00
1.90E-00	1.

Table A2. Listing of COMBCC2 Band Model Parameters: COMBCC2

[illegible]

Table A2. Listing of COMBCO2 Band Model Parameter Set (Cont'd)

[illegible]

Table A2. Listing of COMBICO2 Band Model Parameter Set (Cont'd)

3738.00	2.935E-02	2.445E-01	7.594E-01	4.273E-01	2.948E-01	1.576E-01	1.083E-01	7.537E-02	4.554E-02	3.837E-02
3745.00	3.047E-04	3.547E-02	1.341E-01	2.473E-01	2.159E-01	1.530E-01	1.042E-01	6.734E-02	4.047E-02	2.465E-02
3750.00	2.268E-03	4.126E-03	3.776E-02	1.393E-01	1.694E-01	1.526E-01	1.047E-01	6.041E-02	3.534E-02	2.093E-02
3755.00	2.060E-04	2.755E-04	6.515E-02	5.366E-02	9.594E-02	5.350E-02	3.320E-02	4.711E-02	2.771E-02	1.632E-02
3760.00	2.535E-11	1.184E-05	7.940E-04	1.594E-02	4.402E-02	2.302E-02	3.034E-02	1.331E-02	3.008E-02	1.169E-02
3765.00	1.269E-12	1.764E-07	4.595E-05	2.873E-03	1.402E-03	2.302E-03	3.034E-03	1.331E-03	1.194E-02	6.989E-03
3770.00	4.269E-12	2.036E-08	8.385E-07	1.400E-04	1.219E-03	3.180E-03	7.462E-03	5.806E-03	3.794E-03	2.281E-03

EFFECTIVE LINE DENSITY(D) ARRAY(LINES/CM-1)

3100.00	7.283E-01	9.445E-01	1.255E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3105.00	5.872E-01	8.481E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3110.00	7.963E-01	9.877E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3115.00	6.652E-01	9.989E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3120.00	1.158E+00	1.672E+00	2.473E+00	5.023E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3125.00	1.212E+00	1.597E+00	2.371E+00	4.366E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3130.00	1.419E+00	2.408E+00	3.167E+00	5.812E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3135.00	1.766E+00	2.985E+00	3.737E+00	5.812E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3140.00	2.402E+00	3.985E+00	5.167E+00	5.812E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3145.00	2.011E+00	2.597E+00	3.581E+00	5.609E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3150.00	6.411E-01	1.041E+00	1.691E+00	4.664E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3155.00	6.341E-01	1.023E+00	1.684E+00	4.664E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3160.00	6.341E-01	1.023E+00	1.684E+00	4.664E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3165.00	6.905E-01	1.074E+00	1.733E+00	4.515E+00	1.380E+01	3.998E+01	2.448E+02	7.952E+02	1.379E+03	2.070E+03
3170.00	6.905E-01	1.074E+00	1.733E+00	4.515E+00	1.380E+01	3.998E+01	2.448E+02	7.952E+02	1.379E+03	2.070E+03
3175.00	2.240E+00	1.523E+00	2.677E+00	5.945E+00	1.380E+01	3.998E+01	2.448E+02	7.952E+02	1.379E+03	2.070E+03
3180.00	2.240E+00	1.523E+00	2.677E+00	5.945E+00	1.380E+01	3.998E+01	2.448E+02	7.952E+02	1.379E+03	2.070E+03
3185.00	1.073E+00	2.657E+00	4.267E+00	8.536E+00	2.019E+01	4.766E+01	2.501E+02	1.292E+03	1.514E+03	1.547E+03
3190.00	6.517E-01	8.504E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3195.00	6.517E-01	8.504E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3200.00	6.517E-01	8.504E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3205.00	6.203E-01	8.717E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3210.00	5.664E-01	8.730E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3215.00	5.321E-01	8.707E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3220.00	5.321E-01	8.707E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3225.00	5.114E-01	7.915E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3230.00	4.923E-01	7.768E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3235.00	4.923E-01	7.768E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3240.00	4.923E-01	7.768E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3245.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3250.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3255.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3260.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3265.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3270.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3275.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3280.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3285.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3290.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3295.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03
3300.00	0.907E-01	9.918E-01	1.225E+00	4.007E+00	1.369E+01	3.950E+01	2.440E+02	9.208E+02	1.535E+03	2.241E+03

Table A2. Listing of COMBCO2 Band Model Parameter Set (Cont'd)

[illegible]

Table A2. Listing of COMBCO2 Band Model Parameter Set (Cont'd)

[illegible]

MEAN LINEWIDTH(W) AREA(CM-1/ATM; HWHM FOR NON-RESONANT SELF-BROADENING AT STP)

[illegible]

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The Laboratory Operations of The Aerospace Corporation is conducting experimental and theoretical investigations necessary for the evaluation and application of scientific advances to new military concepts and systems. Versatility and flexibility have been developed to a high degree by the laboratory personnel in dealing with the many problems encountered in the nation's rapidly developing space and missile systems. Expertise in the latest scientific developments is vital to the accomplishment of tasks related to these problems. The laboratories that contribute to this research are:

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Materials Sciences Laboratory: Development of new materials; metal matrix composites and new forms of carbon; test and evaluation of graphite and ceramics in reentry; spacecraft materials and electronic components in nuclear weapons environment; application of fracture mechanics to stress corrosion and fatigue-induced fractures in structural metals.

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