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A NUMERICAL STUDY OF AN IDEALIZED EMP PROBLEM. (U)  
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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Accurate results were obtained for the time history of the electric-field strength between two parallel, infinite, aluminum plates caused by Compton electrons generated by a transient, high-intensity, gamma-ray flux. Two numerical methods, Hamming's method and an exponential differencing technique, were used to solve the resulting ordinary differential equations of the problem. The two techniques and their results are examined and			

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Compared, and it is set forth that the exponential differencing method provides a more efficient solution to the ordinary differential equations of the type involved in this problem.

FOREWORD

The Army Multiple Systems Evaluation Program (MSEP) is a comprehensive program developing general analytic techniques for the prediction of high-electromagnetic-pulse vulnerability and hardening technology and for the application of these techniques to a list of critical systems. The analytic techniques have been verified for a large class of tactical systems. The hardening techniques have been applied to specific systems and are now resulting in product improvement programs leading to hardened equipment in the field.

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## 1. INTRODUCTION

This effort was written under the sponsorship of the Multiple Systems Evaluation Program (MSEP) which has as its main objective to harden Army tactical systems to the exoatmospheric electromagnetic-pulse (EMP) threat. Along with this major objective, the MSEP is also tasked with the aim to develop experimental and analytical evaluation techniques that are applicable to all systems' problems. This work illuminates several numerical techniques that can be used to solve ordinary differential equations that might arise in making EMP vulnerability assessments for tactical Army systems. Therefore, the objective of providing analytic methods is satisfied.

A study was undertaken to expand upon the results obtained in a paper by Wyatt<sup>1</sup> and to investigate and compare two numerical techniques in solving ordinary differential equations that occur in an EMP problem. It was conducted with the purpose of refining the previous calculations.<sup>1</sup> The numerical techniques employed are fairly standard methods, but whereas Wyatt was concerned only with approximate solutions, this work deals mainly with the specific numerical techniques used in the solution of the problem. An analysis of truncation errors was employed to deal with the accuracy of the solutions that better solidifies the results. The methods utilized were the predictor-corrector technique known as Hamming's method and an exponential differencing method that was developed by Pope.<sup>2</sup> This effort does not attempt to explain the physics of the problem or the derivation of the ordinary differential equations. This material is fully detailed by Wyatt.<sup>1</sup>

In the following sections, some general comments are made concerning Runge-Kutta solutions and predictor-corrector solutions of ordinary differential equations. The two techniques employed in the solution of the problem are described fully, along with a discussion and comparison of the results. At the end, some conclusions are made concerning the results and the numerical methods that were used.

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<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

<sup>2</sup>David A. Pope, *An Exponential Method of Numerical Integration of Ordinary Differential Equations*, *Communications of the ACM* 6, No. 8 (August 1963), 491-493.

## 2. GENERAL PHYSICAL PROBLEM

The problem that was dealt with was the determination of the time history of the electric-field strength between two parallel, infinite, aluminum plates caused by Compton electrons generated by a transient, high-intensity, gamma-ray flux. The ordinary differential equations that are solved are a result of the application of Poisson's equation to the free charge that is the spatially distributed current of Compton electrons. Since the conductivity of the air is significant, Poisson's equation is modified by Ohm's law, which relates the air conductivity, electric-field strength, and conduction current. In the case examined here, methane was used instead of air, and it was found by Wyatt<sup>1</sup> that methane reduced the peak electric-field strength. The resulting ordinary differential equations to be solved are

$$\frac{dE(t)}{dt} + \frac{q\mu}{\epsilon} N_e(0) e^{rt} E(t) = \frac{J_c(t)}{\epsilon} e^{rt}, \quad t < 0 \quad (1)$$

$$\frac{dE(t)}{dt} + \frac{q\mu}{\epsilon} N_e(t) E(t) = \frac{J_c(t)}{\epsilon}, \quad t \geq 0, \quad (2)$$

where

$E(t)$  is the electric-field strength,

$q$  is the electronic charge,

$\mu$  is the electron mobility,

$\epsilon$  is the permittivity of free space,

$N_e(t)$  is the free electron density,

$r$  is the model parameter for gamma-flux rate history,

$J_c$  is the Compton electron current density.

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<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

### 3. RUNGE-KUTTA AND PREDICTOR-CORRECTOR METHODS

When attempting to solve ordinary differential equations numerically, two well-known methods, the Runge-Kutta technique and the predictor-corrector technique, are often employed to find the solution. Depending on various constraints such as time, computing funds available, accuracy, and stability, there are accompanying advantages and disadvantages to both methods. Thus, before examining Hamming's method in the solution of equations (1) and (2), a few general remarks concerning fourth-order Runge-Kutta solutions and fourth-order predictor-corrector methods are made to give some background and rationale for the technique utilized.

It is generally recognized that predictor-corrector methods are more difficult to code than Runge-Kutta methods. However, although Runge-Kutta techniques are more straightforward, predictor-corrector methods provide a much easier analysis and examination of errors and are generally much faster. For example, the evaluation of  $f(x,y)$  (i.e.,  $dy/dx = f(x,y)$ ) is usually the most time-consuming part of solving differential equations, and fourth-order Runge-Kutta methods require four evaluations of  $f(x,y)$  per step, while fourth-order predictor-corrector methods require only two evaluations of  $f(x,y)$  per step. This means that the fourth-order predictor-corrector methods are generally nearly twice as fast as fourth-order Runge-Kutta techniques. Thus, the evaluation of errors and the speed of computation are two compelling reasons to use predictor-corrector methods instead of Runge-Kutta methods. However, since predictor-corrector methods are not self-starting and Runge-Kutta techniques do have the self-starting capability, Runge-Kutta methods are quite useful in generating starting values for the solution and may be used to change the interval between steps when desired. This usefulness makes Runge-Kutta methods an indispensable tool in using predictor-corrector techniques. Therefore, a combination of these two methods, (1) the Runge-Kutta to determine starting values and change the per-step interval and (2) the predictor-corrector to actually solve the differential equation and analyze the errors involved, gives a technique that is highly desirable in computing the solution of ordinary differential equations.

### 4. HAMMING'S METHOD

Since Hamming's method is not self-starting, the Runge-Kutta technique was used to start the solution. This involves writing the differential equation as

$$\frac{dy}{dx} = f(x,y)$$

and then finding

$$k_1 = f(x_1, y_1)h ,$$

$$k_2 = f(x_1 + \frac{1}{2}h, y_1 + \frac{1}{2}k_1)h ,$$

$$k_3 = f(x_1 + \frac{1}{2}h, y_1 + \frac{1}{2}k_2)h ,$$

$$k_4 = f(x_1 + h, y_1 + k_3)h ,$$

where  $h$  is the desired increment step size. Once these values are computed for a particular increment,  $\Delta y$  is calculated by

$$\Delta y = \frac{1}{6}(k_1 + 2k_2 + 2k_3 + k_4) ,$$

and then

$$y_{i+1} = y_i + \Delta y .$$

This process is continued until the desired number of starting values is obtained. In Hamming's method, three values from the Runge-Kutta technique are used to start the solution process.

Once the starting values have been determined from the Runge-Kutta technique, the general procedure for Hamming's method is used, as is done by most predictor-corrector techniques. This procedure is illustrated by the flow chart in figure 1. The specific formulas used in Hamming's method and shown in figure 1 are as follows:

$$\text{Predictor: } y_{i+1}^{(0)} = y_{i-3} + \frac{4h}{3}(2y_i' - y_{i-1}' + 2y_{i-2}') ,$$

$$\text{Corrector: } y_{i+1}^{(j+1)} = \frac{1}{8}(9y_i - y_{i-2}) + \frac{3h}{8} \left( \left[ y_{i+1}^{(j)} \right]' + 2y_i' - y_{i-1}' \right) ,$$

$$\text{Truncation error: } T_i \approx \frac{9}{121} \left[ y_{i+1} - y_{i+1}^{(0)} \right] ,$$

where  $h$  is the interval step size.

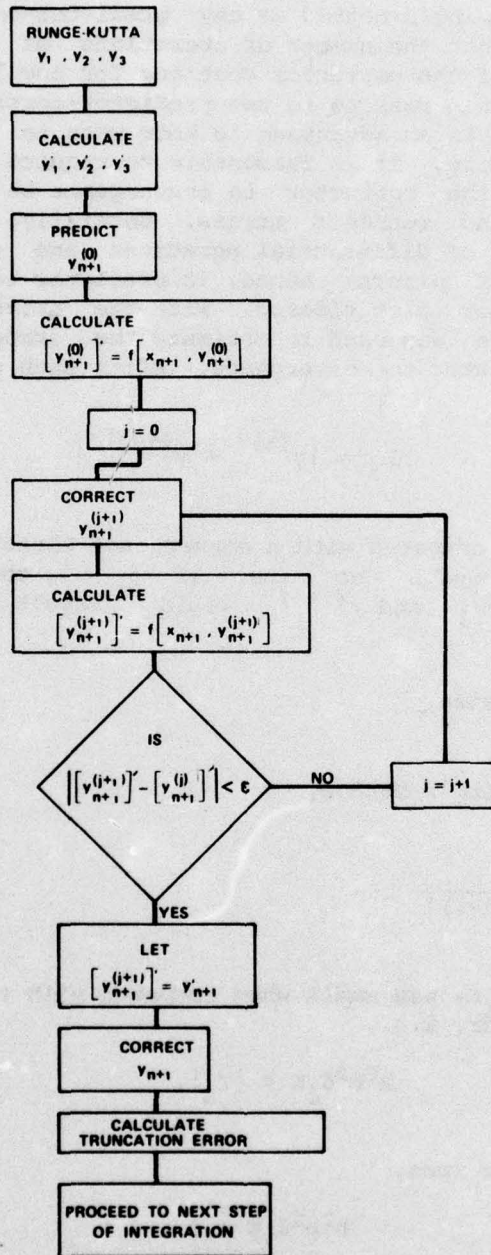


Figure 1. General Predictor-Corrector Method.

In applying Hamming's method or any predictor-corrector method, one must be cautious about the number of iterations of the corrector. To let the iteration of the corrector continue for any length of time would defeat one of the main reasons to use predictor-corrector methods, speed of computation. It is an advantage to know when to stop iterating the corrector. Therefore, it is reasonable to require that any error made by not iterating the corrector to convergence be small when compared with truncation and roundoff errors. Generally, truncation errors affect the solution of differential equations and cause instabilities more than roundoff errors; hence, in predictor-corrector techniques, only truncation error is considered. With the above point in mind, the following procedure was used to estimate the error incurred by not iterating the corrector to convergence. After each corrector iteration,

$$\delta_i = |y^{(i)} - y^{(i-1)}|$$

was computed and compared with a convergence factor,  $\epsilon$  ( $\epsilon$  in fig. 1). The value  $\epsilon$  was chosen so that if  $\delta_i < \epsilon$ , then terminating the iteration with  $[y^{(i)}]$  and  $y^{(i+1)}$  would result in an error value of  $h^2 b^2 \delta_i K$ , where

$h$  = time step size,

$b = \frac{3}{8}$  for Hamming's method,

$$K = \frac{\delta_i}{|y^{(i)} - y^{(i-1)}|}$$

This value,  $h^2 b^2 \delta_i K$ , was small when compared with the absolute value of the truncation error, i.e.,

$$h^2 b^2 \delta_i K < |T_n|.$$

In all the computer runs,

$$h^2 b^2 \delta_i K = 0,$$

which was indeed less than the absolute value of the truncation error in every instance of the calculations. Also, utilizing this procedure, only two iterations of the corrector were required for convergence in most cases.

## 5. EXPONENTIAL DIFFERENCING METHOD

The second method used to solve differential equations (1) and (2) was an exponential differencing technique developed by Pope.<sup>2</sup> This method has been shown to have superior stability properties for large step sizes when dealing with a large class of differential equations. Hence, this technique may be used with a large step size to decrease significantly the total computing time for a solution, particularly in those engineering problems, like EMP problems, where high accuracy is not necessarily needed. However, in this work, the accuracy is a significant part of the effort, and, as it turns out, the exponential differencing method does provide precise results, which are shown in section 7. The exponential differencing technique is now described.

Consider

$$y' = f(x, y) \quad (3)$$

with the initial condition  $y(x_0) = y_0$ . The exponential difference equation used to solve equation (3) is given by

$$y_{n+1} = y_n + hf + y'' f_y^{-2} \left( e^{hf} y - 1 - hf_y \right), \quad (4)$$

where

$h$  is the time step size,

$$y'' = f_x + f \cdot f_y,$$

$f_x, f_y$  are the partial derivatives of  $f$  with respect to  $x$  and  $y$ . The truncation error for this algorithm is

$$T_{n+1} \approx \frac{1}{6} h^3 \left( f_{xx} + 2f \cdot f_{xy} + f^2 \cdot f_{yy} \right).$$

If the value of  $|hf_y|$  is small, at least if  $|hf_y| < 0.1$ , then in place of the exponential formula, the series form

$$y_{n+1} = y_n + hf + y'' \sum_{k=2}^{\infty} \frac{h^k f_y^{k-2}}{k!} \quad (5)$$

<sup>2</sup>David A. Pope, *An Exponential Method of Numerical Integration of Ordinary Differential Equations*, *Communications of the ACM*, 6, No. 8 (August 1963), 491-493.

is used to avoid loss of significance due to cancellation of terms. In this case, only a few terms of the series are needed; we used only three. If the value of  $hf_y$  is fairly large, then the exponential subroutines should be used.

To find the solutions for equations (1) and (2) using the exponential differencing method, we let

$$f(t,E) = \frac{dE}{dt} = \frac{J_c}{\epsilon} e^{rt} - \frac{q\mu}{\epsilon} N_e(0) e^{rt} E, \quad t < 0,$$

$$g(t,E) = \frac{dE}{dt} = \frac{J_c}{\epsilon} - \frac{q\mu}{\epsilon} N_e(t) E, \quad t > 0.$$

The various equations needed to use equations (4) and (5) are now generated. For the function  $f(t,E)$ , its derivatives and partial derivatives are

$$f_t = \frac{r}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E],$$

$$f_E = -\frac{q\mu}{\epsilon} N_e(0) e^{rt},$$

$$E'' = f_t + f \cdot f_E = \frac{r}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E] + \frac{q\mu}{\epsilon^2} N_e(0) e^{2rt} [q\mu N_e(0) E - J_c],$$

$$f_{tt} = \frac{r^2}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E],$$

$$f_{EE} = 0,$$

$$f_{tE} = -\frac{q\mu}{\epsilon} N_e(0) r e^{rt}.$$

The truncation error is

$$T_{n+1} \approx \frac{1}{6} h^3 \left\{ \frac{r^2}{\epsilon} e^{rt} [J_c - q\mu N_e(0) E] + \frac{2q\mu}{\epsilon^2} N_e(0) e^{2rt} [q\mu N_e(0) E - J_c] \right\}.$$

For the function  $g(t,E)$ , its derivatives and partial derivatives are found to be

$$g_t = -\frac{q\mu}{\epsilon} EN'_0(t) = -\frac{q\mu}{\epsilon} S \cdot E ,$$

$$g_E = -\frac{q\mu}{\epsilon} N_0(t) ,$$

$$E'' = g_t + g \cdot g_E$$

$$= -\frac{q\mu}{\epsilon} S \cdot E + \frac{q\mu}{\epsilon} N_0(t) [q\mu N_0(t) E - J_C] ,$$

$$g_{tt} = 0 ,$$

$$g_{EE} = 0 ,$$

$$g_{tE} = -\frac{q\mu}{\epsilon} S ,$$

where  $N_0(t)$  is described in section 6. The truncation error is given by

$$T_{n+1} \approx \frac{1}{6} h^3 \left\{ \frac{2q\mu}{\epsilon^2} [q\mu N_0(t) E - J_C] \right\} .$$

It is an easy, straightforward process to code these quantities to calculate equations (4) and (5). The general procedure used to solve the exponential difference equation is given in figure 2.

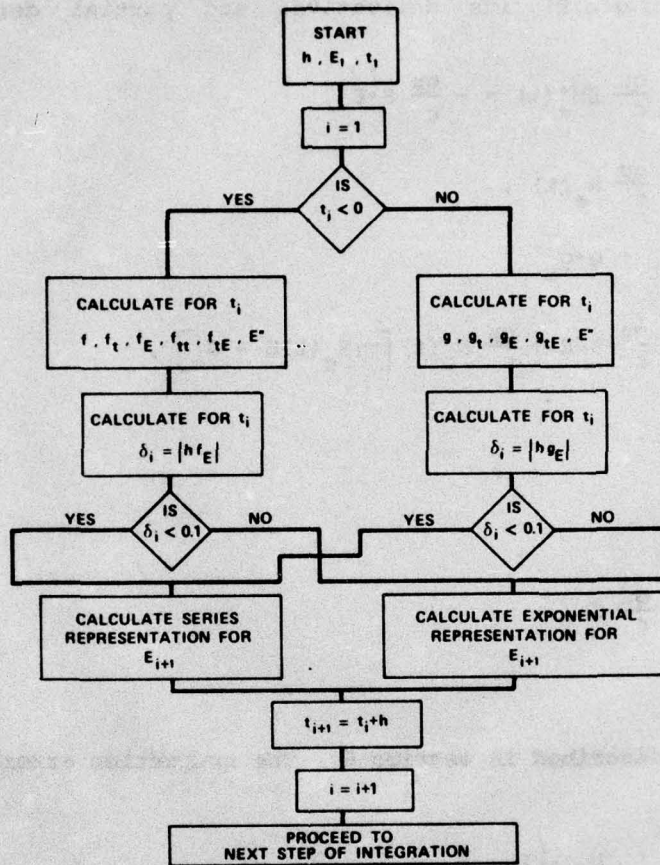


Figure 2. Exponential Differencing Method.

## 6. NUMERICAL VALUES

Finding the solution of equations (1) and (2) required the use of the same hypothetical numerical values as applied by Wyatt<sup>1</sup> for the various constant parameters. These values are as follows:

$$q = 1.6 \cdot 10^{-19} \text{ C,}$$

$$N_e(0) = 1.133 \cdot 10^{11} / \text{cm}^3,$$

$$\mu = 2.0 \text{ m}^2/\text{V/s},$$

$$J_c(t) = 1.34 \cdot 10^3 \text{ A/m}^2 \text{ for all } t,$$

$$\epsilon = 8.85 \cdot 10^{-2} \text{ F/m},$$

$$r = 5.0 \cdot 10^8 / \text{s},$$

$$E(0) = 3.697 \cdot 10^4 \text{ V/m}.$$

The free-electron density,  $N_e(t)$ , is given by

$$N_e(t) = N_e(0) + St, \quad (6)$$

where  $t$  is the time and  $S$  is the rate of production of ion pairs per unit volume and is given the value

$$S = 5.664 \cdot 10^{25} / \text{m}^3/\text{s}.$$

Since equation (6) is valid for methane only to 9 ns, any solutions for times beyond this were not possible to calculate. However, it was possible to obtain excellent results and make some interesting comparisons for this restrictive time frame, which are shown in section 7.

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<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

## 7. RESULTS AND COMPARISONS

Two computer codes were written to solve differential equations (1) and (2). Computer code HAMMING was written to solve the equations by Hamming's method, and the code EXPDIFF was used to solve the equations by the exponential differencing methods. The listings of HAMMING and EXPDIFF are in appendices A and B, respectively.

Although the solutions from HAMMING compare favorably with the results of Wyatt,<sup>1</sup> the solutions obtained are considered more accurate, since truncation errors are calculated and examined. In table I, specific values from Wyatt<sup>1</sup> and HAMMING are listed to show the agreement of the results. Regarding these results, numerous computer runs were

TABLE I. RESULTS OF ORIGINAL AND HAMMING

Time (s)	Original Electric field strength (V/m)	HAMMING Electric field strength ( $\Delta t = 1.0 \cdot 10^{-12}$ ) (V/m)
$-4.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6970 \cdot 10^4$
$-3.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6965 \cdot 10^4$
$-2.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6961 \cdot 10^4$
$-1.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6960 \cdot 10^4$
0	$3.80 \cdot 10^4$	$3.6959 \cdot 10^4$
$5.0 \cdot 10^{-10}$	$3.00 \cdot 10^4$	$3.2129 \cdot 10^4$
$1.0 \cdot 10^{-9}$	$2.48 \cdot 10^4$	$2.6259 \cdot 10^4$
$1.5 \cdot 10^{-9}$	$2.10 \cdot 10^4$	$2.2092 \cdot 10^4$
$2.0 \cdot 10^{-9}$	$1.85 \cdot 10^4$	$1.9107 \cdot 10^4$
$3.0 \cdot 10^{-9}$	$1.47 \cdot 10^4$	$1.5093 \cdot 10^4$
$4.0 \cdot 10^{-9}$	$1.20 \cdot 10^4$	$1.2496 \cdot 10^4$
$5.0 \cdot 10^{-9}$	$1.00 \cdot 10^4$	$1.0670 \cdot 10^4$
$6.0 \cdot 10^{-9}$	$8.80 \cdot 10^3$	$9.3132 \cdot 10^3$
$7.0 \cdot 10^{-9}$	$8.00 \cdot 10^3$	$8.2648 \cdot 10^3$
$8.0 \cdot 10^{-9}$	$7.40 \cdot 10^3$	$7.4296 \cdot 10^3$
$9.0 \cdot 10^{-9}$	$7.00 \cdot 10^3$	$6.7483 \cdot 10^3$

<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).*

made with different time step sizes, which revealed some interesting facts. When the time step size  $\Delta t = 1.0 \cdot 10^{-10}$  was used, stability of the solution was obtained from 0 to approximately 6.5 ns, while from 6 to 9 ns, the solution became dominated by very large truncation errors and, thus, resulted in an unstable solution over this time frame. Using the time step sizes  $\Delta t = 1.0 \cdot 10^{-11}$  and  $\Delta t = 1.0 \cdot 10^{-12}$  did not produce any stability problems during the time frame 0 to 9 ns, and the truncation errors were considerably smaller than for  $\Delta t = 1.0 \cdot 10^{-10}$ . The truncation errors did not decrease, however, when the time step size was lowered to  $\Delta t = 1.0 \cdot 10^{-13}$ , as they remained approximately on the same order of magnitude. An example of these results appears in table II.

TABLE II. HAMMING'S TRUNCATION ERRORS FOR DIFFERENT TIME STEP SIZES

Time (s)	Truncation errors for time step sizes ( $\Delta t$ )			
	$\Delta t = 1.0 \cdot 10^{-10}$	$\Delta t = 1.0 \cdot 10^{-11}$	$\Delta t = 1.0 \cdot 10^{-12}$	$\Delta t = 1.0 \cdot 10^{-13}$
0	0	0	0	0
$1.0 \cdot 10^{-10}$	0	$3.4909 \cdot 10^{-6}$	$-8.6590 \cdot 10^{-11}$	$-1.2123 \cdot 10^{-10}$
$2.0 \cdot 10^{-10}$	0	$4.1106 \cdot 10^{-6}$	$-1.7318 \cdot 10^{-11}$	$-6.9272 \cdot 10^{-11}$
$3.0 \cdot 10^{-10}$	0	$4.0913 \cdot 10^{-6}$	$-5.1954 \cdot 10^{-11}$	$-1.2123 \cdot 10^{-10}$
$4.0 \cdot 10^{-10}$	$1.9735 \cdot 10^{-1}$	$3.6824 \cdot 10^{-6}$	$-6.9272 \cdot 10^{-11}$	$-1.3854 \cdot 10^{-10}$
$1.0 \cdot 10^{-9}$	$8.5146 \cdot 10^{-2}$	$5.5282 \cdot 10^{-7}$	$-6.9272 \cdot 10^{-11}$	$-6.0613 \cdot 10^{-11}$
$2.0 \cdot 10^{-9}$	$-1.1649 \cdot 10^{-3}$	$-1.5846 \cdot 10^{-8}$	$-5.1954 \cdot 10^{-11}$	$-4.3295 \cdot 10^{-11}$
$3.0 \cdot 10^{-9}$	$-1.7558 \cdot 10^{-4}$	$-3.2038 \cdot 10^{-9}$	$-6.4942 \cdot 10^{-11}$	$-5.1954 \cdot 10^{-11}$
$4.0 \cdot 10^{-9}$	$-1.0871 \cdot 10^{-4}$	$-8.9188 \cdot 10^{-10}$	$-3.8965 \cdot 10^{-11}$	$-2.5977 \cdot 10^{-11}$
$5.0 \cdot 10^{-9}$	$-8.4018 \cdot 10^{-3}$	$-3.4203 \cdot 10^{-10}$	$-2.1647 \cdot 10^{-11}$	$-3.0306 \cdot 10^{-11}$
$6.0 \cdot 10^{-9}$	$-1.2692 \cdot 10^1$	$-1.6019 \cdot 10^{-10}$	$-3.0306 \cdot 10^{-11}$	$-3.0306 \cdot 10^{-11}$
$7.0 \cdot 10^{-9}$	$-2.3989 \cdot 10^5$	$-8.6590 \cdot 10^{-11}$	$-3.4636 \cdot 10^{-11}$	$-3.0306 \cdot 10^{-11}$
$8.0 \cdot 10^{-9}$	$-5.0072 \cdot 10^{10}$	$-6.4942 \cdot 10^{-11}$	$-1.9483 \cdot 10^{-11}$	$-2.1647 \cdot 10^{-11}$
$9.0 \cdot 10^{-9}$	$-9.8303 \cdot 10^{16}$	$-3.2471 \cdot 10^{-11}$	$-1.2988 \cdot 10^{-11}$	$-1.0824 \cdot 10^{-11}$

Some interesting occurrences were noted when analyzing the results of EXPDIFF. First, EXPDIFF was very simple to code. In fact, because of the relative ease and simplicity in programming EXPDIFF, valid results were obtained on the first computer run. Second, the results of EXPDIFF were quite favorable when compared to the results obtained by Wyatt<sup>1</sup> and again are considered more accurate because of the calculation

<sup>1</sup>W. T. Wyatt, *Internal EMP Strength and Time Dependence for an Idealized Problem*, Report 1994, U.S. Army Mobility Equipment Research and Development Center, Fort Belvoir, VA (February 1971).

TABLE III. RESULTS OF ORIGINAL, HAMMING, AND EXPDIFF

Time (s)	Original Electric field strength (V/m)	HAMMING Electric field strength $\Delta t = 1.0 \cdot 10^{-12}$ (V/m)	EXPDIFF Electric field strength $\Delta t = 1.0 \cdot 10^{-12}$ (V/m)
$-4.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6970 \cdot 10^4$	$3.6970 \cdot 10^4$
$-3.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6965 \cdot 10^4$	$3.6965 \cdot 10^4$
$-2.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6961 \cdot 10^4$	$3.6961 \cdot 10^4$
$-1.0 \cdot 10^{-9}$	$3.80 \cdot 10^4$	$3.6960 \cdot 10^4$	$3.6960 \cdot 10^4$
0	$3.80 \cdot 10^4$	$3.6959 \cdot 10^4$	$3.6959 \cdot 10^4$
$5.0 \cdot 10^{-10}$	$3.00 \cdot 10^4$	$3.2129 \cdot 10^4$	$3.2135 \cdot 10^4$
$1.0 \cdot 10^{-9}$	$2.48 \cdot 10^4$	$2.6259 \cdot 10^4$	$2.6264 \cdot 10^4$
$1.5 \cdot 10^{-9}$	$2.10 \cdot 10^4$	$2.2092 \cdot 10^4$	$2.2095 \cdot 10^4$
$2.0 \cdot 10^{-9}$	$1.85 \cdot 10^4$	$1.9107 \cdot 10^4$	$1.9110 \cdot 10^4$
$3.0 \cdot 10^{-9}$	$1.47 \cdot 10^4$	$1.5093 \cdot 10^4$	$1.5094 \cdot 10^4$
$4.0 \cdot 10^{-9}$	$1.20 \cdot 10^4$	$1.2496 \cdot 10^4$	$1.2497 \cdot 10^4$
$5.0 \cdot 10^{-9}$	$1.00 \cdot 10^4$	$1.0670 \cdot 10^4$	$1.0670 \cdot 10^4$
$6.0 \cdot 10^{-9}$	$8.80 \cdot 10^3$	$9.3132 \cdot 10^3$	$9.3138 \cdot 10^3$
$7.0 \cdot 10^{-9}$	$8.00 \cdot 10^3$	$8.2648 \cdot 10^3$	$8.2652 \cdot 10^3$
$8.0 \cdot 10^{-9}$	$7.40 \cdot 10^3$	$7.4296 \cdot 10^3$	$7.4299 \cdot 10^3$
$9.0 \cdot 10^{-9}$	$7.00 \cdot 10^3$	$6.7483 \cdot 10^3$	$6.7486 \cdot 10^3$

and analysis of the truncation errors (table III). Probably the most significant aspect of EXPDIFF was the results of comparisons with HAMMING.

In comparing the codes, several significant points of interest were revealed. There was a noticeable ease in the programming of EXPDIFF compared with the more difficult effort required for HAMMING. In fact, a very generous analysis of this coding effort was that HAMMING took at least twice as long to code as EXPDIFF. Although HAMMING is generally considered to give more accurate calculations, EXPDIFF yielded results that were extremely close (sometimes exact) to the solutions obtained from HAMMING (table III). However, the most significant result was the stability of EXPDIFF when compared with HAMMING. For the time step size  $\Delta t = 1.0 \cdot 10^{-11}$ , the truncation errors were approximately the same size, except in several cases where truncation errors from HAMMING were

an order of magnitude smaller. When the time step size was increased to  $\Delta t = 1.0 \cdot 10^{-10}$ , HAMMING became unstable at about 6.5 ns, while EXPDIFF yielded truncation errors on the order of  $10^{-6}$  for 0 to 9 ns. This timing is illustrated in table IV. An even more meaningful result was noticed when considering the large step size of  $\Delta t = 1.0 \cdot 10^{-9}$ . For this step size, EXPDIFF was stable through 9 ns, since truncation errors on the order of  $10^{-2}$  were tolerated. Whereas EXPDIFF exhibited reasonable truncation errors for this step size, HAMMING, as expected, became dominated by the buildup of truncation errors and, thus, was unstable. The truncation errors of EXPDIFF for  $\Delta t = 1.0 \cdot 10^{-9}$  can be seen in table V.

TABLE IV. TRUNCATION ERRORS FOR DIFFERENT TIME STEP SIZES FOR HAMMING AND EXPDIFF

Time (s)	Truncation errors at time step size $1.0 \cdot 10^{-10}$		Truncation errors at time step size $1.0 \cdot 10^{-11}$	
	HAMMING	EXPDIFF	HAMMING	EXPDIFF
0	0	$7.4679 \cdot 10^{-5}$	0	$5.0168 \cdot 10^{-8}$
$1.0 \cdot 10^{-10}$	0	$5.9718 \cdot 10^{-11}$	$3.4909 \cdot 10^{-6}$	$3.9421 \cdot 10^{-9}$
$2.0 \cdot 10^{-10}$	0	$5.1673 \cdot 10^{-6}$	$4.1106 \cdot 10^{-6}$	$6.740 \cdot 10^{-9}$
$3.0 \cdot 10^{-10}$	0	$8.4422 \cdot 10^{-6}$	$4.0913 \cdot 10^{-6}$	$8.3.3 \cdot 10^{-9}$
$4.0 \cdot 10^{-10}$	$1.9735 \cdot 10^{-1}$	$1.0322 \cdot 10^{-5}$	$3.6824 \cdot 10^{-6}$	$9.0334 \cdot 10^{-9}$
$1.0 \cdot 10^{-9}$	$8.5146 \cdot 10^{-2}$	$9.7018 \cdot 10^{-6}$	$5.5282 \cdot 10^{-7}$	$7.0506 \cdot 10^{-9}$
$2.0 \cdot 10^{-9}$	$-1.1649 \cdot 10^{-3}$	$5.3903 \cdot 10^{-6}$	$-1.5846 \cdot 10^{-8}$	$3.6655 \cdot 10^{-9}$
$3.0 \cdot 10^{-9}$	$-1.7558 \cdot 10^{-4}$	$3.5640 \cdot 10^{-6}$	$-3.2038 \cdot 10^{-9}$	$2.2718 \cdot 10^{-9}$
$4.0 \cdot 10^{-9}$	$-1.0871 \cdot 10^{-4}$	$2.6160 \cdot 10^{-6}$	$-8.9188 \cdot 10^{-10}$	$1.5602 \cdot 10^{-9}$
$5.0 \cdot 10^{-9}$	$-8.4018 \cdot 10^{-3}$	$2.0477 \cdot 10^{-6}$	$-3.4203 \cdot 10^{-10}$	$1.1436 \cdot 10^{-9}$
$6.0 \cdot 10^{-9}$	$-1.2692 \cdot 10^1$	$1.6749 \cdot 10^{-6}$	$-1.6019 \cdot 10^{-10}$	$8.7743 \cdot 10^{-10}$
$7.0 \cdot 10^{-9}$	$-2.3989 \cdot 10^5$	$1.4142 \cdot 10^{-6}$	$-8.6590 \cdot 10^{-11}$	$6.9648 \cdot 10^{-10}$
$8.0 \cdot 10^{-9}$	$-5.0072 \cdot 10^{10}$	$1.2230 \cdot 10^{-6}$	$-6.4942 \cdot 10^{-11}$	$5.6760 \cdot 10^{-10}$
$9.0 \cdot 10^{-9}$	$-9.8303 \cdot 10^{16}$	$1.0775 \cdot 10^{-6}$	$-3.2471 \cdot 10^{-11}$	$4.7242 \cdot 10^{-10}$

TABLE V. EXPDIFF TRUNCATION ERRORS AT TIME STEP SIZE  $1.0 \cdot 10^{-9}$

Time (s)	Truncation errors
0	$8.7131 \cdot 10^{-1}$
$1.0 \cdot 10^{-9}$	$2.1944 \cdot 10^{-7}$
$2.0 \cdot 10^{-9}$	$5.1673 \cdot 10^{-2}$
$3.0 \cdot 10^{-9}$	$3.4598 \cdot 10^{-2}$
$4.0 \cdot 10^{-9}$	$2.5851 \cdot 10^{-2}$
$5.0 \cdot 10^{-9}$	$2.0672 \cdot 10^{-2}$
$6.0 \cdot 10^{-9}$	$1.7226 \cdot 10^{-2}$
$7.0 \cdot 10^{-9}$	$1.4766 \cdot 10^{-2}$
$8.0 \cdot 10^{-9}$	$1.2920 \cdot 10^{-2}$
$9.0 \cdot 10^{-9}$	$1.1484 \cdot 10^{-2}$

## 8. CONCLUSIONS

With regard to the comparisons made between the predictor-corrector routine HAMMING and the exponential differencing method EXPDIFF, there seem to be two compelling factors that make the exponential differencing technique superior. First, the ease and simplicity of the programming effort required for EXPDIFF far outweigh the more complicated coding work needed for HAMMING. Second and probably more important, the stability properties of EXPDIFF are excellent, whereas the solutions calculated by HAMMING became dominated by truncation errors during the time frame examined for particular time step sizes. This stability property is best exemplified by the large step size ( $1.0 \cdot 10^{-9}$ ) that can be used with relative assuredness of accurate results. Thus, this stability factor represented by the reasonable truncation errors of EXPDIFF far outweigh the somewhat smaller truncation errors of HAMMING. Therefore, considering the ease of programming and the stability properties, the exponential differencing method provides an efficient and reliable solution to the differential equations involved in this EMP problem and is strongly recommended for solving other differential equations of this type.

### SYMBOLS

$E(t)$	Electric-field strength
$\epsilon$	Permittivity of free space
$J_c(t)$	Compton electron current density
$\mu$	Electron mobility
$N_e(t)$	Free electron density
$q$	Electronic charge
$r$	Model parameter for gamma flux rate history
$s$	Rate of production of ion pairs per unit volume
$t$	Time

**APPENDIX A.--COMPUTER CODE HAMMING**

**This appendix contains a complete listing of HAMMING.**

```

1  PROGRAM HANNING(INPUT,OUTPUT,TAPES=INPUT,TAPE6=OUTPUT)
   INTEGER FLAG
   REAL NORD(10),NABS(10)
   COMMON/A/E(5000),M(5000),EP(5000),DEL,START,ESTART
5  COMMON/B/VAL(5000),CF(5000)
   COMMON/C/RNE(5000),SRE(5000)
   DIMENSION N(5000),TITLE(20)
   DIMENSION ERROR(5000)
   DIMENSION TERR(5000)
   DIMENSION ECOREC(60),ECORECP(60)
10  L=1
   IT=0
   READ(5,20)DEL,THAX,EPSLON,START,ESTART,M
15  FORMAT(SE10.3,15)
   CF(I)=EPSLON
   C  CALCULATE STARTING VALUES Y1,Y2,Y3,USING RUNGE-KUTTA TECHNIQUE
   C
   CALL RUNGE
   DO 30 J=1,4
   CF(J)=EPSLON
30  EP(J)=FET(H(J),E(J),J)
   I=4
   C  PREDICT Y(N+1) USING MILNE'S PREDICTOR
   C
   C  CALL PREDICT(I,EPDIP)
   CF(I+1)=EPSLON
   H(I+1)=H(I)+DEL
   EPDIP=FET(H(I+1),EPDIP,0)
   ECOREC(I)=EPDIP
   ECORECP(I)=EPDIP
   C  CORRECT Y(N+1) USING HANNING'S CORRECTOR
   C
35  CALL CORRECT(I,ECORECP(I),ECOREC(I+1))
   ECOREC(I+1)=FET(H(I+1),ECOREC(I),0)
   IF(L.EQ.1) GO TO 55
   C  CHECK TO SEE IF ERROR RESULTS FROM NOT ITERATING TO CONVERGENCE
   C
   CALL EROR(I,L,EPDIP,ECOREC(L),ECOREC(L+1),ECORECP(L),
   ECORECP(L+1),FLAG,IT)
   IF(FLAG) 53,60,60
45  ERROR(I+1)=ABS(ECORECP(L+1)-ECOREC(L))
   IF(L.GT.50) GO TO 65
   L=L+1
   GO TO 50
60  K(I+1)=L-1
   C  CALCULATE CORRECT VALUE OF Y(N+1) USING HANNING'S CORRECTOR
   C
   CALL CORRECT(I,ECORECP(L+1),ECOR)
   E(I+1)=ECOR
   EP(I+1)=FET(H(I+1),E(I+1),I+1)
55  C  CALCULATE TRUNCATION ERROR

```

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PROGRAM NAMING 74/74 DPT-1

```

60      C
        TERR(I+1) = (9./121.) * (E(I+1) - EPD(I))
        N=1+1
        I=1+1
        L=1
        IF(ME11.L6.TMAX) GO TO 40
        WRITE(6,70)
        FORMAT(I1)
        WRITE(6,80) DEL.TMAX,N,EPSLON,START
        FORMAT(I1X,17HDELTA TIME STEPS,1PE10.3,5X,
        120HMAXIMUM TIME TO BE PLOTTED: 1PE10.3,5X,
        220HINCREMENT OF OUTPUT VALUES: 15./,
        344HCONVERGENCE TOLERANCE: 1PE10.3,
        45HSTARTING TIME 1PE10.3,/,/,/)
        IF(L6.50.AND.FLAG.E6.-1) GO TO 140
        WRITE(6,90)
        FORMAT(17,/,/,53X,9HNUMBER OF,10X,8HERROR BY)
        WRITE(6,100)
        FORMAT(4X,4HTIME,14X,1ME,7X,16HTRUNCATION ERROR,3X,
        110HCONVERGENCE CYCLES,3X,13HNOT ITERATING,3X,
        210HCONVERGENCE FACTOR,5X,6HOLD ME,8X,6HNEN ME)
        WRITE(6,110)
        FORMAT(4X,4H-----,14X,1H-,7X,16H-----,3X,
        118H-----,13X,13H-----,8X,6H-----)
        210H-----,5X,6H-----)
        DO 130 J=1,M*N
        WRITE(6,120) M(J),E(J),TERR(J),K(J),VAL(J),CF(J),RME(J),SME(J)
        FORMAT(I1X,3(1PE11.4,5X),7X,13,11X,1PE11.4,8X,1PE11.4,7X,1PE11.4,
        13X,1PE11.4)
        130 CONTINUE
        C
        C
        TITLE(1) = 10HTEMP TIME D
        TITLE(2) = 10HDEPENDENCY
        TITLE(3) = 5HSTUDY
        TITLE(4) = 1H
        TITLE(5) = 1H
        MORD(1) = 10HELECTRIC F
        MORD(2) = 10HFIELD STREN
        MORD(3) = 10HGM V/M
        MABS(1) = 4HTIME
        MABS(2) = 1H
        MABS(3) = 1H
        C
        C
        CALL PLOT(IN,MAX)
        CALL PATPLOT(E,MAX,TITLE,MABS,MORD,0.,0.,100)
        GO TO 155
        KL=1+1
        140 WRITE(6,150) KL,ERROR(KL)
        150 FORMAT(17,/,/,12X,MORD) NOT CONVERGE IN 50 ITERATIONS WHILE CALC.
        155 READ(5,160) IK
        160 FORMAT(9X,11)
        GO TO (30,170),IK
        170 CONTINUE
        END
    
```

PROGRAM NAMING 74/74 OPT=1  
 CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

312 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

APPENDIX A

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	SM TYPE	RELOCATION	SM TYPE	REFERENCES	SM TYPE	REFERENCES
4111 NAMING	1							
VARIABLES								
11A10 CF	REAL	ARRAY B	REAL	ARRAY B	REFS	5	84	21
35230 DEL	REAL	ARRAY A	REAL	ARRAY A	REFS	4	29	13
O E	REAL	ARRAY A	REAL	ARRAY A	REFS	4	22	84
4645 EGR	REAL	ARRAY A	REAL	ARRAY A	DEFINED	54	54	
42352 ECDREC	REAL	ARRAY A	REAL	ARRAY A	REFS	53	37	2042
42346 ECDREC	REAL	ARRAY A	REAL	ARRAY A	REFS	10	36	2045
23A20 EP	REAL	ARRAY A	REAL	ARRAY A	REFS	10	34	2042
4443 EPDIP	REAL	ARRAY A	REAL	ARRAY A	DEFINED	32	37	53
4444 EPDIP	REAL	ARRAY A	REAL	ARRAY A	REFS	4	22	55
4637 EPLOW	REAL	ARRAY A	REAL	ARRAY A	REFS	27	30	42
16332 EMDR	REAL	ARRAY A	REAL	ARRAY A	REFS	32	30	59
35232 ESTART	REAL	ARRAY A	REAL	ARRAY A	REFS	15	21	66
4633 FLAG	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	8	107	45
11010 H	REAL	ARRAY A	REAL	ARRAY A	DEFINED	4	13	72
4642 I	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	2	42	30
4651 IK	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	2	22	29
4635 IT	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	4	29	30
4641 J	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	104	22	37
4676 K	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	4	22	29
4650 KL	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	27	28	30
4634 L	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	49	53	4055
4640 M	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	27	28	61
4647 MAX	INTEGER	ARRAY A	INTEGER	ARRAY A	REFS	49	53	61
4646 N	INTEGER	ARRAY A	INTEGER	ARRAY A	DEFINED	106	54	61
4644 NMS	REAL	ARRAY A	REAL	ARRAY A	REFS	112	110	
4652 NORD	REAL	ARRAY A	REAL	ARRAY A	REFS	42	12	
O RME	REAL	ARRAY C	REAL	ARRAY C	REFS	21	4022	20
11010 SRE	REAL	ARRAY C	REAL	ARRAY C	REFS	7	84	49
35231 START	REAL	ARRAY A	REAL	ARRAY A	REFS	20107	106	2037
30342 TERR	REAL	ARRAY A	REAL	ARRAY A	REFS	31	32	72
16306 TITLE	REAL	ARRAY A	REAL	ARRAY A	REFS	47	49	11
4636 TMAX	REAL	ARRAY B	REAL	ARRAY B	REFS	66	83	13
O VAL	REAL	ARRAY B	REAL	ARRAY B	REFS	103	104	60
					REFS	83	104	99
					REFS	3	104	100
					REFS	3	104	57
					REFS	6	84	
					REFS	6	84	
					REFS	4	64	13
					REFS	9	84	59
					REFS	7	104	90
					REFS	63	64	91
					REFS	5	64	92
					REFS	63	64	93

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74/74 OPT-1

FILE NAMES	MODE	READS	WRITES	REFERENCES	EXT REFS
0 INPUT					
2041 OUTPUT	FMT	13		53	
0 TAPES					
2041 TAPEA	FMT	64	66	30	110
EXTERNALS					
CORRECT	TYPE	ARGS	REFERENCES		
ERROR		3	36		
FET	REAL	9	42		
PLOT		3	22		
PREDICT		2	103		
PRIPLOT		2	27		
RUNGE		9	104		
		0	19		

107

84

79

75

73

110

64

37

55

INLINE FUNCTIONS TYPE ARG3 ARG4 DEF LINE REFERENCES

ABS REAL 1 INTRIN 45

STATEMENT LABELS DEF LINE REFERENCES

4312 10	11	112
4425 20	14	13
0 30	22	20
4134 40	27	63
4150 50	36	48
0 53	45	64
4200 55	47	38
4202 60	49	2044
4228 65	64	46
4433 70	65	64
4445 80	67	64
4473 90	74	73
4503 100	76	75
4524 110	80	79
4555 120	85	86
0 130	87	83
4310 140	106	72
4572 150	108	107
4316 155	110	105
4613 160	111	110
4327 170	113	112

LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES

4122 30	0 J	20 22	118	EXT REFS
4244 130	0 J	83 87	238	EXT REFS

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)

A	15003	1500C DEL (11)	5000 H (5000)
B	10000	0 VAL (5000)	15001 START (11)
C	10000	0 PNE (5000)	5000 CF (5000)

STATISTICS

PROGRAM LENGTH	362378	15519
BUFFER LENGTH	41038	2315
CM LABELLED COMMON LENGTH	1042738	35003

10000 EP (5000)

15002 ESTART (11)

```

SUBROUTINE RUNGE
COMMON/AF/E(5000),H(5000),EP(5000),DEL,START,E,START
M(1)=START
E(1)=START
I=1
10 R1=FET(H(1),E(1),0)*DEL
T2=M(1)+.5*DEL
E2=E(1)+.5*E1
R2=FET(T2,E2,0)*DEL
E3=E(1)+.5*E2
R3=FET(T2,E3,0)*DEL
T4=M(1)+DEL
E4=E(1)+R3
R4=FET(T4,E4,0)*DEL
DELE=(R1+.2*R2+.2*R3+.4*R4)/6.
E(1+1)=E(1)+DELE
I=I+1
M(1)=M(1)+DEL
IF(I.GT.3) RETURN
GO TO 10
END
    
```

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS I RUNGE	DEF LINE 1	REFERENCES 19	VARIABLES 35230 DEL	SM REAL	TYPE REAL	RELOCATION A	REFERENCES 9	ARGS 6	REFERENCES 9	TYPE REAL	ARGS 3	REFERENCES 6	
113	DELE	REAL	REAL	REAL	REAL	REAL	10	2	6	DEFINED	7	11	12
0	E	REAL	REAL	REAL	REAL	REAL	15	16	DEFINED	15	11	12	14
23420	EP	REAL	REAL	REAL	REAL	REAL	8	2	6	DEFINED	10	13	16
35232	E,START	REAL	REAL	REAL	REAL	REAL	10	4	16	DEFINED	10	13	16
104	E2	REAL	REAL	REAL	REAL	REAL	11	2	4	DEFINED	8	10	14
106	E3	REAL	REAL	REAL	REAL	REAL	13	11	DEFINED	10	10	13	16
111	E4	REAL	REAL	REAL	REAL	REAL	14	14	DEFINED	13	12	16	2016
11610	H	REAL	REAL	REAL	REAL	REAL	7	2	6	DEFINED	7	10	12
101	I	INTEGER	INTEGER	INTEGER	INTEGER	INTEGER	3	3	10	DEFINED	10	12	13
102	R1	REAL	REAL	REAL	REAL	REAL	206	206	7	DEFINED	8	12	13
105	R2	REAL	REAL	REAL	REAL	REAL	17	19	19	DEFINED	5	17	2016
107	R3	REAL	REAL	REAL	REAL	REAL	8	15	15	DEFINED	6	17	2016
112	R4	REAL	REAL	REAL	REAL	REAL	10	15	15	DEFINED	6	17	2016
35231	START	REAL	REAL	REAL	REAL	REAL	13	15	15	DEFINED	9	17	2016
103	T2	REAL	REAL	REAL	REAL	REAL	15	15	15	DEFINED	11	17	2016
110	T4	REAL	REAL	REAL	REAL	REAL	3	3	3	DEFINED	14	17	2016
EXTERNALS	FET	REAL	REAL	REAL	REAL	REAL	2	9	11	DEFINED	7	11	14

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SUBROUTINE RUNGE	74/74	OPT-1	
STATEMENT LABELS	6	DEF LINE REFERENCES	20
COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)	
A	15003	OF (5000)	10000 EP (5000)
		1500C DEL (1)	15002 ESTART (1)
STATISTICS			
PROGRAM LENGTH	1146	5000 H (5000)	
CR LABELED COMMON LENGTH	352338	15001 START (1)	
	15003		

```

SUBROUTINE PREDICT(I,EPDIC)
COMMON/A/E(15000),M(5000),EP(5000),DEL,START,ESTART
V=2, *EP(I)-EP(I-1)+2, *EP(I-2)
EPDIC=EP(I-3)+((4.*DEL)/3.)*V
RETURN
END
    
```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS 3 PREDICT 1 REFERENCES 5

VARIABLES	SM	TYPE	RELOCATION
35230 DEL		REAL	A
0 E		REAL	A
29420 EP		REAL	A
0 EPDIC		REAL	F.P.
35232 ESTART		REAL	A
11610 M		REAL	A
0 I		INTEGER	F.P.
35231 START		REAL	A
22 V		REAL	A

2	4
2	4
2	3-3
1	4
2	
2	4
3-3	4
2	DEFINED
4	DEFINED

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)
A	15003	0 E (15000)
		15000 DEL (1)

5000 M	(15000)
15001 START	(1)
10000 EP	(15000)
15002 ESTART	(1)

STATISTICS	PROGRAM LENGTH	230	19
CM LABELED COMMON LENGTH	35238	15003	

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74/74 OPT-1

SUBROUTINE CORRECT

```

SUBROUTINE CORRECT(I,EDICP,ECREC)
COMMON/A/(15000),M(15000),EP(15000),DEL,START,ESTART
V1=19.0E(11-E(1)-2)/R
V2=EDICP+2.0E(11)-E(11-1)
ECREC=V1+113.0E(11)/R.1072
RETURN
END
    
```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS DEF LINE REFERENCES

3 CORRECT 1 6

VARIABLES	SN	TYPE	RELOCATION	REFS
35230 DEL	0	REAL	ARRAY A	REFS
0 E	0	ECREC	F.P.	REFS
0 EDICP	0	REAL	F.P.	DEFINED
0 EDICP	0	REAL	F.P.	DEFINED
35230 EP	0	REAL	ARRAY A	REFS
35232 ESTART	0	REAL	ARRAY A	REFS
11010 M	0	REAL	ARRAY A	REFS
0 I	0	INTEGER	F.P.	REFS
35231 START	0	REAL	ARRAY A	REFS
26 V1	26	REAL		REFS
27 V2	27	REAL		REFS

COMMON BLOCKS LENGTH MEMBERS - BIAS NAME(LENGTH)

A 15003 0 E (15000)  
15000 DEL (1)

STATISTICS PROGRAM LENGTH 308 24  
CN LABELED COMMON LENGTH 35238 15003

```

SUBROUTINE EROR(I,L,EPOIC,P,C,PP,CP,FLAG,IT)
COMMON/VAL(5000),N(5000),EP(5000),DEL,START,ESTART
INTEGER FLAG
B=3./D.
DELTA=ABS(CP-PP)
IF(DELTA.LE.CF(I+1)) GO TO 20
JFIL.LE.JD) GO TO 35
CF(I+1)=DELTA+CF(I+1)
FLAG=-1
RETURN
ARG=C-P
IF(ARG.EQ.0.) ARG=1.0E-5
AN=DELTA/ABS(ARG)
VAL(I+1)=(DEL+D2)+(B*D2)*DELTA*AK
CALL CORRECT(I,PP,C)
EC=C
ERR=1./I2L-1)*(EC-EPOIC)
P(VAL(I+1),GT.ABS(ERR)) GO TO 40
FLAG=0
RETURN
IPI=I+1
IF(I+1.GT.0) GO TO 80
WRITE(6,60)
FORMAT(3H)
WRITE(6,70)
FORMAT(/,/,1X,40THE ERROR INCURRED BY NOT ITERATING THE
16)INCORRECTOR BY NOT,/,16X,12ITERATING TO,5X,10TRUNCATION
3/,6X,4HE(1),6X,11INCORVERGENCE,6X,5HERROR)
IT=1
80 WRITE(6,90) IPI,VAL(I+1),ERR
90 FORMAT(5X,2HE(,16,1MI),5X,1PE11.4,5X,1PE11.4)
FLAG=1
RETURN
END
    
```

35

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF	LINE	REFERENCES	21	35
3	1	11	11		
VARIABLES	SM	TYPE	RELOCATION		
162 ARG	REAL			REFS	13
160 B	REAL			15	14
160 C	REAL			12	16
13A10 CF	REAL	F.P.	ARRAY	17	17
13A10 CP	REAL	F.P.		9	16
35290 DEL	REAL	A		1	17
161 DELTA	REAL			6	15
160 E	REAL	A	ARRAY	7	15
164 EC	REAL	A		2	14
23A20 EP	REAL	A	ARRAY	10	17
				2	17
				13	13
				15	13
				12	1
				3	9
				6	9
				2	1
				7	1
				2	15
				10	14
				2	15
				10	15
				2	17
				2	17



SUBROUTINE PLOT 74/74 OPT=1 FTH 4.54434 06/04/76 13.30.02 PAGE 1

```

SUBROUTINE PLOT(M,MAX)
COMMON/4/(5000),M(5000),EP(5000),DEL,START,ESTART
BY=H/100.
IDEL=INT(MT)
IF(IDEL.EQ.0) IDEL=1
L=1
DO 10 I=1,M,IDEI
M(I)=M(I)
E(I)=E(I)
L=L+1
10 CONTINUE
MAX=L
RETURN
END
    
```

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS 3 PLOT	DEF LINE 1	REFERENCES 13	RELOCATION	REFS
VARIABLES	SM	TYPE		
35230 DEL		REAL	A	REFS
0 E		REAL	A	REFS
29420 EP		REAL	ARRAY A	REFS
35232 ESTART		REAL	ARRAY A	REFS
11020 M		REAL	ARRAY A	REFS
34 I		INTEGER		REFS
32 IDEL		INTEGER		REFS
39 L		INTEGER		REFS
0 MAX		INTEGER		REFS
0 N		INTEGER	F.P.	REFS
31 AT		REAL	F.P.	REFS
35231 START		REAL	A	REFS
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	REFERENCES
INT	INTEGER	1	INTBIN	REFERENCES
STATEMENT LABELS			DEF LINE	REFERENCES
0 10			11	7
LOOPS LABEL	INDEX	FROM-TO	LENGTH	PROPERTIES
17 10	1	7 11	4B	INSTACK
COMMON BLOCKS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)	
4	15003	0 E	(5000)	
		15000 DEL	(1)	
STATISTICS				
PROGRAM LENGTH		350	29	
CH LABELED COMMON LENGTH		35233B	15003	
		5000 M	(5000)	
		15001 START	(1)	
		10000 EP	(5000)	
		15002 ESTART	(1)	



```

FUNCTION NE 74/74 OPT-1
1 REAL FUNCTION NEIT(K)
COMMON/C/RNE(1000),SNE(1000)
REAL NEQ
NEQ=1.133E+11
S=5.694E+19
IF (T.GE.0.) GO TO 10
NE=1.133E+11
RNE(K)=0.
SNE(K)=0.
RETURN
10 NE=NEQ+S*OT
IF (K.EQ.0) RETURN
SNE(K)=NE
RNEQ=1.133E+11
RS=1.022E+20
DELTA=1.0008E+8
A=4.E-7
ARG=AR.S*(1+2)
X=.5*ARG
Y=DELTA*OT
Z=X-Y
F1=R5/(2.*DELTA)
F2=1.*EXP(X)
F3=EXP(Y)-1.
F4=EXP(Z)
RNE(K)=(F1*F2*F3+RNEQ)*F4
RETURN
END
    
```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	12	27
4	ME	1	10	
VARIABLES				
70	A	REAL		REFS
71	ARG	REAL		REFS
67	DELTA	REAL		REFS
75	F1	REAL		REFS
76	F2	REAL		REFS
77	F3	REAL		REFS
100	F4	REAL		REFS
0	K	INTEGER		REFS
62	ME	REAL		REFS
63	NEQ	REAL		REFS
6	RNE	REAL		REFS
45	RNEQ	REAL	ARRAY	REFS
66	RS	REAL		REFS
64	S	REAL		REFS
10610	SNE	REAL	ARRAY	REFS
0	T	REAL		REFS
72	X	REAL		REFS

DEF LINE	REFERENCES	12	27
10	REFS		REFS
19	REFS		REFS
20	REFS		REFS
26	REFS		REFS
26	REFS		REFS
26	REFS		REFS
26	REFS		REFS
26	REFS		REFS
8	REFS		REFS
1	REFS		REFS
13	REFS		REFS
3	REFS		REFS
2	REFS		REFS
26	REFS		REFS
10	REFS		REFS
11	REFS		REFS
2	REFS		REFS
6	REFS		REFS
21	REFS		REFS

APPENDIX A

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FTN 4.54414

74/74 OPT=1

FUNCTION NE	74/74	OPT=1	RELOCATION	REFS	21	24	DEFINED	20
VARIABLES	SM	TYPE		REFS	25	DEFINED	21	
73	V	REAL		REFS				
74	Z	REAL						
EXTERNALS	TYPE	ARGS	REFERENCES		24			
END	REAL	1	LIBRARY	23				
STATEMENT LABELS			DEF LINE	REFERENCES				
15	10		11					
COMMON BLOCKS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)		5000	SNE	(5000)	
C	10000	0	RNE	(5000)				
STATISTICS								
PROGRAM LENGTH		1018		65				
CR LABELED COMMON LENGTH		234208		10000				

FUNCTION JC 74/74 OPT=1

```

1 REAL FUNCTION JC(I)
R=5.E+8
IFIT=0.1 GO TO 10
JC=1.34E+3*EXP(R*I)
RETURN
10 JC=1.34E+3
RETURN
END

```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	7	RELOCATION	DEFINED REFS
4 JC	1	5			4
VARIABLES	SM	TYPE			4
20 JC		REAL			4
21 R		REAL			3
0 T		REAL		F.P.	4
EXTERNALS	TYPE	ARGS	REFERENCES		2
EXP	REAL	1	LIBRARY	4	4
STATEMENT LABELS		DEF LINE	REFERENCES		1
14 10		6	3		
STATISTICS		PROGRAM LENGTH			
		220	10		

```

1  C SUBROUTINE PRTPLT (HORZ,VERT,MPTS,HEAD,MLAB,VLAB,MLAB,VLAB,MREF,VREF,J)
  C THIS FORTRAN SUBROUTINE PRODUCES A FULL PAGE X-Y PRINTER PLOT.
  C
  C HORZ - REAL ARRAY TO BE PLOTTED ALONG HORIZONTAL AXIS.
  C VERT - REAL ARRAY TO BE PLOTTED ALONG VERTICAL AXIS.
  C MPTS - NUMBER OF VALUES IN HORZ,VERT (NTE 101)
  C HEAD - PLOT HEADING (MUST BE 5 WORDS)
  C MLAB - LABEL FOR HORIZONTAL AXIS (MUST BE 3 WORDS)
  C VLAB - LABEL FOR VERTICAL AXIS (MUST BE 3 WORDS)
  C MREF - REFERENCE VALUE FOR HORIZONTAL AXIS.
  C VREF - REFERENCE VALUE FOR VERTICAL AXIS.
  C J THIS DETERMINES THE SIZE OF THE ARRAYS HORZ AND VERT--NTE 100
  C
15  DIMENSION HORZ(J),VERT(J),HEAD(5),MLAB(3),VLAB(3),LINE(101),
  C IVER(101),JHORZ(101),JVERT(101),VERTIC(101),YAXIS(30),DOWNT(21)
  C INTEGER BLANK,STAR,DOT,EYE
  C
  C DATA BLANK/1H /,STAR/1H*,DOT/1H.,MINUS/1H-/ ,EYE/1H/
  C
  C CALL DATE( DAT )
  C CALL TIME( TIM )
  C HEAD(4)=DAT
  C HEAD(5)=TIM
  C MD = 1
  C NUN = 1
  C N = MPTS
  C DE 10 J = 1,N
  C HORZ(1) = HORZ(1)
  C VERT(1) = VERT(1)
  C 10 CONTINUE
  C
  C DECODE (30,1000,VLAB(1)) (YAXIS(1),1-1,30)
  C 1000 FORMAT(30I1)
  C 20 NA = N - 1
  C DO 30 J = 1,NA
  C IF (VERTIC(J).GE.VERTIC(J+1)) GO TO 30
  C HOLD = VERTIC(J)
  C VERTIC(J) = VERTIC(J+1)
  C VERTIC(J+1) = HOLD
  C SAVE = HORZ(J)
  C HORZ(J) = HORZ(J+1)
  C HORZ(J+1) = SAVE
  C 30 CONTINUE
  C DO 40 J = 1,NA
  C IF (VERTIC(J).LT.VERTIC(J+1)) GO TO 20
  C 40 CONTINUE
  C VMAX = VERTIC(1)
  C VMIN = VERTIC(N)
  C HMAX = HORZ(1)
  C HMIN = HORZ(N)
  C DO 50 I = 2,N
  
```

```

55      MZ = HORIZ(I)
      HMAX = AMAXI(HMAX,MZ)
      HMIN = AMINI(HMIN,MZ)
      50      CONTINUE
      DO 60 I = 1,N
      JVER = 50.*(VERTIC(I)-VMINI)/(VMAX-VMINI) + 1.5
      IVER(I) = 52 - JVER
      60      JHOR(I) = 100.*(HORIZ(I)-HMIN)/(HMAX-HMIN) + 1.5
      KHREF = 100.*(HREF-HMIN)/(HMAX-HMIN) + 1.5
      IF (KHREF.LT.1) KHREF = 150
      IF (KHREF.GT.101) KHREF = 150
      KVREF = 50.*(VREF-VMINI)/(VMAX-VMINI) + 1.5
      KVREF = 52 - KVREF
      IF (KVREF.LT.1) KVREF = 1
      IF (KVREF.GT.51) KVREF = 1
      UP = (VMAX-VMINI)/50.
      PRINT 2,OC, HEAD
      70      FORMAT(1M1,35X,SAL0//)
      DO 200 K = 1,51
      LINE(K) = EYE
      LINE(101) = EYE
      DO 70 I = 2,100
      70      LINE(I) = BLANK
      IF (K.EQ.1) GO TO 90
      IF (K.EQ.51) GO TO 90
      IF (K.NE.KVREF) GO TO 120
      DO 80 I = 2,100
      80      LINE(I) = DOT
      GO TO 120
      90      DO 100 I = 2,100
      100      LINE(I) = MINUS
      DO 110 I = 6,100,5
      110      LINE(I) = EYE
      GO TO 130
      120      IF (KHREF.EQ.150) GO TO 130
      IF (KHREF.EQ.1) GO TO 130
      LINE(KHREF) = DOT
      130      IF (K.EQ.IVER(NUM)) GO TO 140
      IF (K.LT.IVER(NUM)) GO TO 160
      NUM = NUM + 1
      GO TO 130
      140      IF (JHOR(NUM).GT.101) GO TO 150
      IF (JHOR(NUM).LT.1) GO TO 150
      JH = JHOR(NUM)
      LINE(JH) = STAR
      150      NUMBER = NUM + 1
      IF (IVER(NUM).NE.IVER(NUMBER)) GO TO 160
      NUM = NUMBER
      GO TO 140
      160      T = K - 1
      UP = VMAX - T*UP
      IF (K.LT.11) GO TO 170
      IF (K.GT.51) GO TO 170

```

APPENDIX A

PAGE 3

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FTN 4.6+620

SUBROUTINE PATPLT 76/74 DPT-1

```

110 TAXIS = VAXIS(MO)
    MC = MC + 1
    PRINT 3000, TAXIS, UPT, LINE
    3000 FORMAT(5X, A1, 4X, IPE9, 2, 2X, I01A1)
    GO TO 400
170 PRINT 4000, UPT, LINE
    4000 FORMAT(9X, IPE9, 2, 2X, I01A1)
200 CONTINUE
    DLN = (HMAX - HMIN) / 20.
    Y = HMIN
    DO 210 I = 1, 21
        DOWN(I) = Y
        Y = Y + DOWN
210 CONTINUE
    5000 PRINT 5000, (DOWN(I), I = 1, 21, 2)
    5000 FORMAT(75X, IPE10, 2)
    6000 PRINT 6000, (DOWN(I), I = 2, 20, 2)
    6000 FORMAT(20X, IPE10, 2)
    7000 PRINT 7000, HLAB
    7000 FORMAT(/50X, 3A30)
    RETURN
    END

```

**APPENDIX B.--COMPUTER CODE EXPDIFF**

**This appendix contains a complete listing of EXPDIFF.**

PROGRAM EXPDIFF 74/74 OPT=1 FTN 4.5+014 06/06/76 13.30.36 PAGE 1

```

1  PROGRAM EXPDIFF (INPUT, OUTPUT, TAPES-INPUT, TAPES-OUTPUT)
   REAL JC, MU, ME, MORD(3), MABS(3)
   COMMON /A/R, EPS, G, MU, S
   DIMENSION TITLE(15)
   S=5.064E+19
   R=5.0E+8
   EPS=9.05E-12
   G=1.0E-19
   MU=2.0
10  CONTINUE
   I=1
   READ(5,20) DEL, TSTART, TMAX, ESTART, N, J
20  FORMAT(4E10.3, 15, 15)
   T(1)=TSTART
   E(1)=ESTART
   TERR(1)=0
   IF(J.NE.1) GO TO 30
   T(1)=T(0)
   E(1)=E(0)
   TSTART=T(1)
   ESTART=E(1)
30  CONTINUE
   IF(T(1).GT.TMAX) GO TO 70
   IF(T(1).GE.0.) GO TO 50
   CALL FCALC(I, F, FE, FTT, FTE)
   EDP=FT*F0FE
   DELTA(1)=ABS(DELOFE)
   IF(DELTA(1).LT..1) GO TO 40
   X=EXP(DELOFE)-1.-DELOFE
   E(1)=E(1)+DEL*EDP+EDP*(FE001-2))X
   TERR(1)=((DELO03)*(FTT+2.0E+TE))/6.
   T(1)=T(1)+DEL
   I=I+1
35  GO TO 30
40  S1=(DELO02)/2.
   S2=(DELO03)*FE/6.
   S3=(DELO04)*(FE002)/24.
   E(1)=E(1)+DEL*(EDP+EDP*(S1+S2+S3)
   TERR(1)=((DELO03)*(FTT+2.0E+TE))/6.
   T(1)=T(1)+DEL
   I=I+1
50  CALL GCALC(I, G, GT, GE, GTE)
   EDP=GT*G0GE
   DELTA(1)=ABS(DELOGE)
   IF(DELTA(1).LT..1) GO TO 60
   X=EXP(DELOGE)-1.-DELOGE
   E(1)=E(1)+DEL*(G0G+EDP*(GE001-2))X
   TERR(1)=((DELO03)*(2.0E+GTE))/6.
   T(1)=T(1)+DEL
   I=I+1
60  S1=(DELO02)/2.
   S2=(DELO03)*GE/6.
   S3=(DELO04)*(GE002)/24.
   E(1)=E(1)+DEL*(G0G+EDP*(S1+S2+S3)

```

APPENDIX B

PAGE 2

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FTN 4.5+414

PROGRAM EXPDIFF 74/74 OPT=1

```

60      TORD(1)=((DEL**3)**2.6**CTE1)/6.
        T(1)=T(1)*DEL
        I=1
        GO TO 30
70      CONTINUE
        N=1
        CALL OTHREIT(M,DEL,START,TRAX)

        TITLE(1)=10HWP TIME D
        TITLE(2)=10HDEPENDENCY
        TITLE(3)=5HSTUDY
        TITLE(4)=3H
        TITLE(5)=3H
        NORD(1)=10HELECTRIC F
        NORD(2)=10HFIELD STREN
        NORD(3)=10HCTH V/M
        NARS(1)=4HTIME
        NARS(2)=2H
        NARS(3)=3H

        C
        C
80      CALL PLOT(M,MAX)
        CALL PRIPLY(T,E,MAX,TITLE,NARS,NORD,O..O..100)
        READ(5,90) IK
90      FORMAT(9X,13)
        GO TO (10,90),IK
95      STOP
        END
    
```

48

CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

04 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS 6111 EXPDIFF	DEF LINE 1	REFERENCES	RELOCATION	REFS	2930	31	32	33	36	37
VARIABLES 4455 DEL	SM	TYPE	REAL	REFS	2930	31	32	33	36	37
29420 DELTA		REAL		30	40	41	46	2040	49	50
31610 E		REAL		51	55	56	57	58	59	64
4471 EDP		REAL	ARRAY B	13	29	47	DEFINED	28	46	57
4471 EPS		REAL	ARRAY B	REFS	4	20	31	39	49	57
4460 ESTART		REAL	A	01	16	20	31	39	49	57
		REAL		REFS	30	49	57	DEFINED	27	45
		REAL		REFS	31	49	57	DEFINED	27	45
		REAL		REFS	3	8	22			
		REAL		REFS	16	13				



APPENDIX B

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FTR 4-S-014

74/74 OPT-1

STATEMENT LABELS	DEF LINE	REFERENCES
4121 10	12	04
4112 20	14	13
4126 30	23	18
4175 40	36	29
4233 50	44	25
4256 60	54	47
4302 70	62	24
4422 80	83	82
4357 90	85	84

COMMON BLOCKS	LENGTH	MEMBERS	DIAS NAME(LENGTH)
A	5	0 R	(11)
B	20000	3 RU	(11)
		0 T	(5000)
		15000 TERR	(5000)

STATISTICS	PROGRAM LENGTH	4 EPS	1 EPS
PROGRAM LENGTH	6148	4 S	(11)
BUFFER LENGTH	61028	5000 E	(5000)
CR LABELED COMMON LENGTH	478458	2 0	(11)
		10000 DELTA	(5000)

```

1 SUBROUTINE FCALC(I,FOFTE,FSUBT,FSUDE,FSUBTT,FSUBTE)
  REAL JC,MU,NE
  COMMON/BI/EP5,0,MU,S
  COMMON/DT/TS0001,E(5000),DELTA(5000),TERR(5000)
  RT=RT(I)
  FOFTE=(JC(I)-Q*NU*NE(I)*E(I)*EXP(ART))/EPS
  FSUDE=(JC(I)-Q*NU*NE(I)*E(I)*EXP(ART))/EPS
  FSUBTT=(JC(I)-Q*NU*NE(I)*E(I)*EXP(ART))/EPS
  FSUBTE=(Q*NU*NE(I)*E(I)*EXP(ART))/EPS
  RETURN
  END
  
```

SYMBOLIC REFERENCE MAP (R=3)

ENTRY POINTS	DEF LINE	REFERENCES	SM	TYPE	RELOCATION	REFS
3 FCALC	1	11				
VARIABLES						
23420 DELTA	REAL	ARRAY	B			4
31630 E	REAL	ARRAY	B			4
1 EP5	REAL	ARRAY	A			6
0 FOFTE	REAL	F.P.				7
0 FSUDE	REAL	F.P.				7
0 FSUBTT	REAL	F.P.				8
0 FSUBTE	REAL	F.P.				10
0 I	INTEGER	F.P.				7
3 MU	REAL	ARRAY	A			3+6
2 0	REAL	ARRAY	B			3
0 R	REAL	ARRAY	B			7
0 RT	REAL	ARRAY	B			7
4 S	REAL	ARRAY	B			7
0 T	REAL	ARRAY	B			8
35230 TERR	REAL	ARRAY	B			5
EXTERNALS						
EXP	REAL	LIBRARY	A			10
JC	REAL	LIBRARY	A			9
NE	REAL	LIBRARY	A			9
COMMON BLOCKS						
A	LENGTH	MEMBERS	-	BIAS NAME(LENGTH)		
B	20000	0	BI	(1)		
		3	MU	(1)		
		0	T	(5000)		
		15000	TERR	(5000)		
STATISTICS						
PROGRAM LENGTH		1148				
CM LABELED COMMON LENGTH		470450				
		20005				



```

1  SUBROUTINE DTWRIT(N,DEL,TSTART,TMAX)
COMMON/DTWRIT(5000),DELTA(5000),TERR(5000)
11=0
K=1
5  WRITE(6,10)
10  FORMAT(1M1)
20  WRITE(6,20)DEL,TSTART,TMAX,N
30  FORMAT(1X,17#DELTA TIME STEPS,1PE10.3,5X,15#STARTING TIMES,
40  11PE10.3,5X,20#MAXIMUM TIME TO BE PLOTTED,1PE10.3,/,34X,
50  22#INCREMENT OF OUTPUT VALUES,15,/,/,/,/)
60  WRITE(6,30)
70  FORMAT(1X,4#TIME,14X,1#E,7X,1#TRUNCATION ERROR,8X,5#DELTA)
80  WRITE(6,40)
90  FORMAT(1X,4#M,14X,1#E,7X,1#M,10#-----,8X,5#-----)
100 DD 110 1=1,M,N
110 WRITE(6,50)T(1),E(1),TERR(1),DELTA(1)
120 IF(11.EQ.1) GO TO 60
130 IF(11.EQ.50) GO TO 70
140 IF(11.EQ.500) GO TO 70
150 K=K+1
160 GO TO 110
170 CONTINUE
180 WRITE(6,60)
190 FORMAT(1M1)
200 WRITE(6,90)
210 FORMAT(1X,4#TIME,14X,1#E,7X,1#TRUNCATION ERROR,8X,5#DELTA)
220 WRITE(6,100)
230 FORMAT(1X,4#M,14X,1#E,7X,1#M,10#-----,8X,5#-----)
240 11=1
250 K=1
260 CONTINUE
270 RETURN
280 END

```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES	SYMBOLIC REFERENCE MAP (R-3)
3	DTWRIT	1	33
VARIABLES	SM	TYPE	RELOCATION
0 DEL	REAL	ARRAY	F.P.
29420 DELTA	REAL	ARRAY	0
1810 E	REAL	ARRAY	0
206 I	INTEGER		
204 IT	INTEGER		
205 K	INTEGER		
0 M	INTEGER		F.P.
0 N	INTEGER		F.P.
0 T	REAL	ARRAY	0
35230 TERR	REAL	ARRAY	0
0 TMAX	REAL	ARRAY	0
0 TSTART	REAL	ARRAY	F.P.
		REFS	
		7	DEFINED 1
		2	16
		2	16
		4+16	DEFINED 15
		10	DEFINED 3
		19	20
		7	15
		15	DEFINED 1
		2	16
		2	16
		7	DEFINED 1
		7	DEFINED 1

APPENDIX B

SUBROUTINE DTURIT 74/74 OPT-1 PTM 4.5-416 06/04/76 13.30.36 PAGE 2 20  
 FILE NAMES MODE PRT WRITES 5 7 11 13 16 24 26 28  
 TAPES PRT

STATEMENT LABELS	DEF LINE	REFERENCES
70 10	4	5
80 10	6	7
101 20	12	11
124 30	14	13
135 40	17	16
152 50	20	18
64 60	23	19
50 70	25	24
160 80	27	26
165 90	29	28
276 100	32	22
60 110		

LOOPS LABEL INDEX FROM-TO LENGTH PROPERTIES EXT REFS  
 30 110 0 1 15 32 338  
 COMMON BLOCKS LENGTH 20000 MEMBERS - DIAS NAME(LENGTH) 5000 E (5000) 10000 DELTA (5000)  
 0 T (5000)  
 15000 TEAR (5000)

STATISTICS  
 PROGRAM LENGTH 2218 145  
 CN LABELED COMMON LENGTH 470008 20000

SUBROUTINE PLOT 74/74 OPT=1

```

1 SUBROUTINE PLOT(N,MAX)
COMMON/B/T(5000),E(5000),DELTA(5000),TERR(5000)
BT=M/100.
IDEL=INTERT
IF(IDEL.EQ.0) IDEL=1
L=1
DO 10 I=1,M,IDEI
T(I)=T(I)
E(I)=E(I)
L=L+1
10 CONTINUE
T(L)=T(M)
E(L)=E(M)
M=M-L
RETURN
END
15

```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS	DEF LINE	REFERENCES						
3 PLOT	1	15						
VARIABLES	SM	TYPE	RELOCATION					
29420 DELTA	REAL	ARRAY	0	REFS				
11410 E	REAL	ARRAY	0	REFS				
37 I	INTEGER			REFS				
35 IDEL	INTEGER			REFS				
36 L	INTEGER			REFS				
0 MAX	INTEGER			REFS				
0 N	INTEGER			REFS				
34 RT	REAL			REFS				
0 T	REAL			REFS				
95230 TERR	REAL	ARRAY	0	REFS				
INLINE FUNCTIONS	TYPE	ARGS	DEF LINE	DEF LINE	REFERENCES			
INT	INTEGER	1	INTRIN	DEF LINE	REFERENCES			
STATEMENT LABELS			DEF LINE	REFERENCES				
0 10			11	7				
LOOPS LABEL	INDEX	FROM--TO	LENGTH	PROPERTIES				
17 10	1	7 11	40	INSTACK				
COMMON BLOCKS	LENGTH	MEMBERS	- BIAS NAME(LENGTH)					
0	20000	0 T	(5000)					
		15000 TERR	(5000)					
STATISTICS								
PROGRAM LENGTH		400	32					
CM LABELED COMMON LENGTH		470400	20000					
		5000 E	(5000)					
		10000 DELTA	(5000)					

APPENDIX B

PAGE 1

06/04/76 13.30.36

FTN 4.5+14

74/74 OPT=1

```

1 REAL FUNCTION NE(II)
  REAL NE0
  COMMON/M,R,EPS,0,MU,S
  COMMON/T(15000),E(15000),DELTA(5000),TERR(5000)
  NE0=1.133E+11
  IF(T(II).GE.0.) GO TO 10
  C NE MULTIPLIED BY 1.E+6 FOR CORRECTION TO METERS
  NE=NE0*1.E+6
  RETURN
10 C NE MULTIPLIED BY 1.E+6 FOR CORRECTION TO METERS
  NE=(NE0*S*(II))*1.E+6
  RETURN
END
  
```

SYMBOLIC REFERENCE MAP (R-3)

ENTRY POINTS 4 VE DEF LINE 1 REFERENCES 9 12

VARIABLES	SM	TYPE	RELOCATION	REFS
29420 DELTA	REAL	ARRAY B		4
31610 E	REAL	ARRAY B		4
1 EPS	REAL	ARRAY A		3
0 I	INTEGER	F.P.		6
3 4U	INTEGER	A		3
22 NE	REAL		DEFINED	0
23 NE0	REAL			2
2 0	REAL			0
0 R	REAL	A		3
4 S	REAL	A		3
0 T	REAL	ARRAY B		3
35230 TERR	REAL	ARRAY B		6

STATEMENT LABELS 13 10 DEF LINE 11 REFERENCES 6

COMMON BLOCKS	LENGTH	MEMBERS - BIAS NAME(LENGTH)	REFS
A	5	0 R (1)	1 EPS (1)
B	20000	3 MU (1)	4 S (1)
		0 T (5000)	5000 E (5000)
		15000 TERR (5000)	10000 DELTA (5000)

STATISTICS PROGRAM LENGTH 248 20  
 CH LABELED COMMON LENGTH 470458 20005



APPENDIX B

SUBROUTINE PRTPLT 7/74 OPT=1 F7N 4-64420 10/27/76 09.31.03 PAGE 1

```

1  C SUBROUTINE PRTPLT (HORZ,VERT,NPTS,HEAD,HLAB,VLAB,HREF,VREF,J)
2  C THIS FORTRAN SUBROUTINE PRODUCES A FULL PAGE X-Y PRINTER PLOT.
3  C
4  C
5  C HORZ - REAL ARRAY TO BE PLOTTED ALONG HORIZONTAL AXIS.
6  C VERT - REAL ARRAY TO BE PLOTTED ALONG VERTICAL AXIS.
7  C NPTS - NUMBER OF VALUES IN HORZ,VERT (NTE NPTS)
8  C HEAD - PLOT HEADING (MUST BE 5 WORDS)
9  C HLAB - LABEL FOR HORIZONTAL AXIS (MUST BE 3 WORDS)
10 C VLAB - LABEL FOR VERTICAL AXIS (MUST BE 3 WORDS)
11 C HREF - REFERENCE VALUE FOR HORIZONTAL AXIS.
12 C VREF - REFERENCE VALUE FOR VERTICAL AXIS.
13 C J - THIS DETERMINES THE SIZE OF THE ARRAYS HORZ AND VERT--NTE 100
14 C
15 C DIMENSION HORZ(J),VERT(J),HEAD(5),HLAB(3),VLAB(3),LINE(101),
16 C IVER(101),JHOR(101),MHORZ(101),VERTIC(101),YAXIS(30),DOWNT(21)
17 C INTEGER BLANK,STAR,DOT,EYE
18 C
19 C
20 C DATA BLANK/IN /,STAR/1HOZ,OUT/IN /,MINUS/0H-,EYE/WHIZ
21 C CALL DATE(0AT)
22 C CALL TIME(TIM)
23 C HEAD(5)=DAT
24 C HEAD(5)=TR
25 C MD = 1
26 C MUR = 1
27 C N = NPTS
28 C N = MIN(01,101)
29 C DO 10 I = 1,N
30 C   HORZ(I) = HORZ(I)
31 C   VERTIC(I) = VERT(I)
32 C 10 CONTINUE
33 C
34 C DECODE (30,1000,VLAB(1)) (YAXIS(1),1-1,30)
35 C 1000 FORMAT(30A1)
36 C 20 NA = N - 1
37 C DO 30 I = 1,NA
38 C   IF (VERTIC(I).GE.VERTIC(I+1)) GO TO 30
39 C   HOLD = VERTIC(I)
40 C   VERTIC(I) = VERTIC(I+1)
41 C   VERTIC(I+1) = HOLD
42 C   SAVE = HORZ(I)
43 C   HORZ(I) = HORZ(I+1)
44 C   HORZ(I+1) = SAVE
45 C 30 CONTINUE
46 C DO 40 I = 1,NA
47 C   IF (VERTIC(I).LT.VERTIC(I+1)) GO TO 20
48 C 40 CONTINUE
49 C VMAX = VERTIC(1)
50 C VMIN = VERTIC(N)
51 C HMAX = HORZ(1)
52 C HMIN = HORZ(N)
53 C DO 50 I = 1,NA

```

```

55 MZ = MODIZ(1)
   MMZ = AMZ(1)
   MMIA = AMI(1)
50 CC=AMU
   DL 60 J = 1,K
   JVER = 50.0*(VERTIC(1)-VMINI)/(VMAX-VMINI) + 1.5
   IVER(1) = 52 - JVER
60 JHOR(1) = 100.0*(HORIZ(1)-HMIN)/(HMAX-HMIN) + 1.5
   KHREF = 100.0*(HREF-HMIN)/(HMAX-HMIN) + 1.5
   IF (KHREF-LT-1) KHREF = 150
   IF (KHREF-GT-101) KHREF = 150
65 KVREF = 50.0*(VREF-VMINI)/(VMAX-VMINI) + 1.5
   KVREF = 52 - KVREF
   IF (KVREF-LT-1) KVREF = 1
   IF (KVREF-GT-51) KVREF = 1
   UP = (VMAX-VMINI)/50.
   PRINT 200, HEAD
70 200 FORMAT(1H1,35X,5A10//)
   DD 200 A = 1,51
   LINE(1) = EYE
   LINE(1C) = EYE
75 DL 70 J = 2,100
   LINE(1) = BLANK
   IF (K-EJ-1) GO TO 90
   IF (K-EJ-51) GO TO 90
   IF (K-NE-KVREF) GO TO 120
80 JC 80 J = 2,100
   LINE(1) = DOT
   GO TO 120
90 DD 100 I = 2,100
   LINE(1) = HINDS
95 JC 110 J = 6,100,5
   LINE(1) = EYE
100 JC 1,10
   IF (KHREF-EG-150) GO TO 130
   IF (KHREF-EG-1) GO TO 130
110 LINE(KHREF) = DOT
   IF (K-EG-IVER(NUM)) GO TO 140
   IF (K-LT-IVER(NUM)) GO TO 160
   NUM = NUM + 1
   GO TO 130
120 IF (JHOR(NUM)-GT-101) GO TO 150
   IF (JHOR(NUM)-LT-1) GO TO 150
   JM = JHOR(NUM)
   LINE(JM) = STAR
130 NUMBER = NUM + 1
   IF (IVER(NUM)-NE-IVER(NUMBER)) GO TO 160
   NUM = NUMBER
   GO TO 140
140 T = N - 1
150 UPT = VMAX - T*UP
   IF (K-LT-11) GO TO 170
   IF (K-GT-41) GO TO 170

```

APPENDIX B

PAGE 3

10/27/76 09.31.03

FTM 4.8-4.20

SUBROUTINE PRTPLE 74/74 OPT=1

```

110      TARI5 = VARI5(MD)
        MC = MC + 1
        PRINT 3000, TARI5, UPT, LINE
        FORMAT(4X, A1, 4X, IPE9.2, 2X, I01A1)
        GO TO 200
170      PRINT 4000, UPT, LINE
        FORMAT(9X, IPE9.2, 2X, I01A1)
200      CONTINUE
        DLUN = (MMAX - MMIN) / 20.
        T = MMIN
        DC 210 I = 1, 21
        DOUNT(1) = T
        Y = T + DDUM
210      CONTINUE
        PRINT 5000, (DOUNT(I), I = 1, 21, 2)
        FORMAT(15X, IPIE10.2)
        PRINT 6000, (DOUNT(I), I = 2, 20, 2)
        FORMAT(20X, IPIE10.2)
        PRINT 7000, MLAB
        FORMAT(50X, 3A10)
        RETURN
        END
115
120
125

```

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