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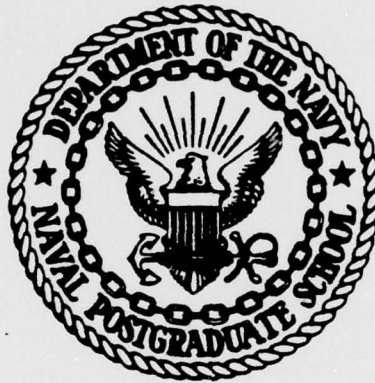
NAVAL POSTGRADUATE SCHOOL  
MONTEREY, CALIFORNIA

DECEMBER 1976

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# NAVAL POSTGRADUATE SCHOOL

## Monterey, California



# THESIS

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by

Michael D. Shutt

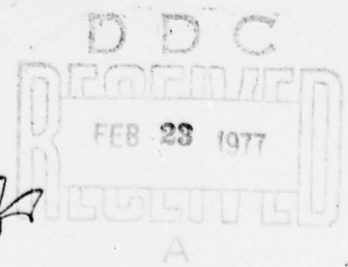
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Robert E. Ball

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SUBJECTED TO AXISYMMETRIC AND NEARLY AXISYMMETRIC STEP  
PRESSURE LOADS USING SATANS-IIA, A MODIFIED VERSION OF  
SATANS-II

by

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Lieutenant  
B.S., Oregon State University, 1970

Submitted in partial fulfillment of the  
requirements for the degree of

MASTER OF SCIENCE IN AERONAUTICAL ENGINEERING

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ABSTRACT

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A digital computer program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution (SATANS-II) was modified to more accurately account for the conditions at the pole of the shell. This program was used to determine the buckling load of shallow spherical shells of various sizes when subjected to static axisymmetric, dynamic axisymmetric, and dynamic nearly axisymmetric step-pressure loads of infinite duration. A comparison was made between the new buckling results and previous results obtained without the new pole routine. The comparison revealed a significant change in the buckling pressures, due solely to the change in the pole routine. The new static axisymmetric, dynamic axisymmetric, and even the dynamic asymmetric critical buckling pressure loads appear to be fairly reliable results for perfect, shallow shells.

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## LIST OF SYMBOLS

b	= nondimensional inplane stiffness
E	= the modulus of elasticity of the shell
H	= the rise of the spherical cap at the pole
h	= the thickness of the shell
m	= the mass density of the shell
M <sub>s</sub>	= the meridional bending moment per unit length
n	= the Fourier index
P	= a nondimensional applied load
P <sub>CRIT</sub>	= the nondimensional critical pressure
q <sub>o</sub>	= the classical buckling pressure of a complete sphere
q <sup>(n)</sup>	= a column matrix containing the coefficients of the n <sup>th</sup> term in the series expansion of the applied load
r	= the normal distance from the axis of revolution to the surface of the cap
r <sub>o</sub>	= the normal distance from the axis to the cap in the base plane; the maximum value of r
R <sub>s</sub> , R <sub>θ</sub>	= the radii of curvature in the s and θ directions, respectively
s	= the meridional distance along the surface of the shell
t	= the nondimensional time
T	= the time
T <sub>o</sub>	= a reference time

$U, V, W$  = the displacements in the  $s$ ,  $\theta$  and  $J$  directions, respectively  
 $u, v, w$  = nondimensional series coefficients of  $U, V, W$   
 $\bar{V}$  = a nondimensional measure of the volume of the shell deformation  
 $\bar{V}_{MAX}$  = the peak in the time history of the parameter  $\bar{V}$   
 $w^{(n)}$  = the displacement in the  $J$  direction in the  $n^{\text{th}}$  harmonic  
 $\delta t$  = the nondimensional time increment  
           = distance between stations  
 $\epsilon^{(n)}$  = the nondimensional parameter governing the magnitude of the load applied in the asymmetric harmonics  
 $J$  = the coordinate normal to the surface of the shell  
 $\theta$  = the circumferential angle measured about the axis of revolution  
 $\lambda$  = a nondimensional geometric parameter used to describe the spherical cap  
 $\nu$  = Poisson's ratio  
 $\xi$  = the normal distance from the base plane to the middle surface of the undeformed cap

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## I. INTRODUCTION

In 1973 a digital computer study was presented by Ball and Burt [1] for the dynamic buckling load of clamped shallow spherical shells subjected to axisymmetric and nearly axisymmetric step-pressure loads. A static buckling analysis of the same spherical shells had been carried out in 1970 by Stilwell and Ball [2]. In these two studies the digital computer program SATANS-I [3] was used to calculate the critical buckling pressures for a large range of shell sizes. Other studies of the buckling of shallow shells have been conducted by Huang [4,5], by Stephens and Fulton [6], by Lock et al. [7], by Stricklin [8], and most recently by Akkas [9]. In Reference 1 the results from these other studies, except for those by Akkas, are compared with the results from SATANS-I for both static and dynamic buckling. In the axisymmetric static analysis the comparison with the results obtained by Huang [4] revealed that the SATANS-I results were higher than Huang's results for several shell sizes. In the dynamic, axisymmetric buckling analysis the SATANS-I results again either agreed closely with, or were somewhat higher than, the results by Huang [5], Stephens and Fulton [6], and Stricklin [8]. However, it was noted then that there was a general lack of consistent agreement among any of the sets of results. As a consequence, it appeared at that time that the axisymmetric buckling problem had not yet been totally resolved and that additional studies would be appropriate.

In the asymmetric dynamic buckling analysis of Reference 1 the few comparisons that could be made for the critical load also indicated that the SATANS-I results may be too

high. A comparison of the recent estimates for the asymmetric dynamic buckling load obtained by Akkas [9] with the SATANS-I results also reveals the SATANS-I results to be well above those of Akkas [9]. However, it should be noted that the results obtained by Akkas were from his attempt to obtain a lower bound on the critical asymmetric load. This bound on the buckling load is obtained without the execution of a complete transient response analysis on the asymmetric part of the response of the shell, as is done in SATANS-I. In Akkas' analysis (Problem 1) the transient nonlinear axisymmetric response is computed, and a determinant is examined for possible bifurcation into asymmetric motion at each time step. The minimum load at which the determinant becomes zero is defined as the lower bound of the critical load.

As a consequence of the generally high buckling loads predicted by SATANS-I, a re-examination of the static and dynamic buckling of the shallow spherical shell was made in an attempt to determine the possible cause, or causes, of the high buckling loads. In our search we discovered that a modification of the manner in which the pole conditions are numerically approximated significantly lowered the buckling loads to values that are now in good agreement with the other results. The new procedure for handling the pole condition is given in section III of this thesis. The new buckling results are given in section V.

In addition to the pole condition modifications and the new buckling results the author has also made another significant change to the SATANS family of codes. In particular, the SATANS-II program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution, developed by Ryan [10] in 1972 to handle more complex and larger problems, was modified to make the computer memory requirement a variable quantity. This

quantity is specified by the user to fit the particular problem being run. It eliminates the large core requirement of SATANS-II for small problems and allows for much larger problems to be solved than could be solved by SATANS-II. The new program with the pole condition and memory modifications will hereafter be called SATANS-IIA. It is described in section II.

## II. DESCRIPTION OF SATANS-IIA

SATANS-II was developed by Ryan [10] from SATANS-I and incorporated the full trigonometric expansion of the applied load and solution vector, and introduced the handling of imperfections into the code. These modifications allow the analysis of shells under totally arbitrary loads, as well as imperfection studies on actual shells with measured imperfections [11]. Unfortunately, the original deck of cards for SATANS-II was destroyed. Professor Johann Arbocz of CALTECH had a listing of SATANS-II and punched a deck of cards with the changes to SATANS-I given in that listing. A copy of this deck was sent to Professor Ball. These cards have been added by the author to the original SATANS-I described by Ryan [10] and a complete version of SATANS-II has been reconstructed. SATANS-IIA is a modification by the author of the reconstructed SATANS-II program. A listing of SATANS-IIA can be found in Appendix A. The listing contains an example problem for the dynamic analysis of a clamped, truncated cone subjected to an impulsive loading which is uniform along the meridian and varies in a cosine distribution over one-half of the circumference. This problem is a sample problem suggested by the Lockheed Missiles and Space Corp. [12]. A condensed version of the output from the example problem is given in Appendix B. Input data preparation for SATANS-IIA can be found in Appendix C. The basic users manual, which includes preparation of input subroutines and the theory of the program, is contained in Reference 3, which can be obtained through COSMIC (M70-10098, LAR-10736), or ASIAC [13]. A users manual which includes preparation and handling of imperfection data within the SATANS programs can be found in

Ref. [10]. The above information, along with the following discussion, will inform the user on the capabilities and proper use of SATANS-IIA.

The modification of the SATANS-II program to make its core requirement variable was accomplished by putting in a single dimension statement at the beginning of the program, with subsequent dimensioning within the subroutines to only the first element of the vector or matrix. This is a convenient feature of the FORTRAN-IV language in which the program is written. The actual vector and matrix sizes are transmitted to the subroutines by an individual parameter list. Construction of the initial dimension statement and core request size is as follows:

The basic size of the program on the IBM-360/67 Digital Computer, without the initial dimension statement, is 272,000 bytes. This figure includes approximately 19,000 bytes of buffer space required for execution. Within the main dimension statement are fifteen variables. However, only three parameters are needed to specify the sizes of these fifteen variables.

Let  $a$  = The number of stations along the meridian of the shell times the number of harmonics considered.  
Let  $b$  =  $a$ , plus two fictitious stations times the number of harmonics considered.  
Let  $c$  = The number of harmonics considered.

The main dimension statement would then be constructed as,

```
DIMENSION P(4,4,a), DEE(4,4,a), DST(4,4,a), X(4,a),  
           PHIXB(a), PHITB(a), Z(4,b), ZO(4,b),  
           Z2(4,b), Z3(4,b), ZDOT(4,b), IS(99,c),  
           JS(99,c), ID(99,c), JD(99,c)
```

The 99's above limit the user to 99 harmonics in any one run and an unlimited number of meridional stations. The core requirement for the general case would be,

$$272,000 + 216a + 80b + 1584c = \text{bytes of core required.}$$

For a sample calculation of the core requirements consider the example of a spherical cap with 40 stations along the meridian, and an asymmetric analysis with two harmonics. Therefore,

$$a = 40(\text{stations}) \times 2(\text{harmonics}) = 80$$

$$b = 80 + 2 \times 2(\text{harmonics}) = 84$$

$$c = 2(\text{harmonics})$$

Thus, for the variables P, DEE, DST,

$$3 \times (4 \times 4 \times 80) = 3840 \text{ (words)} \times 4 = 15,360 \text{ bytes}$$

for the variable X,

$$4 \times (80) = 320 \text{ (words)} \times 4 = 1280 \text{ bytes}$$

for the variables PHIXB, PHITB,

$$2 \times (80) = 160 \text{ (words)} \times 4 = 640 \text{ bytes}$$

for the variables Z, Z0, Z2, Z3, ZDOT,

$$5 \times (4 \times 84) = 1680 \text{ (words)} \times 4 = 6720 \text{ bytes}$$

lastly, for the variables ID, JD, IS, JS,

$$4 \times (99 \times 2) = 792 \text{ (words)} \times 4 = 3168 \text{ bytes}$$

Therefore, the total size of the main dimension statement would be 27,168 bytes. This figure would be rounded up to the nearest even thousand bytes, i.e. 28,000 bytes. Finally, the core requirement for this example problem would be

$$272,000 + 28,000 = 300,000 \text{ bytes.}$$

### III. IMPROVED POLE ROUTINE

The SATANS code is based upon Sander's geometrically nonlinear equations under the conditions of small strains and moderately small rotations. The formulation is in four second order nonlinear partial differential equations in terms of  $U$ ,  $V$ ,  $W$ , and  $M_s$ , where  $U$ ,  $V$ , and  $W$  are the meridional, circumferential and normal displacements respectively, and  $M_s$  is the meridional bending moment. The nonlinear partial differential equations in the coordinates  $s$ ,  $\theta$ , and  $t$  are reduced to uncoupled sets of linear differential equations in  $s$  and  $t$  by expanding the variables in trigonometric series in the circumferential coordinate  $\theta$ , and treating the nonlinear terms as pseudo loads. The first and second derivatives in the meridional coordinate  $s$  are replaced by the conventional central finite difference approximations, ie.

$$\{z\}'_i = 1/2\Delta (\{z\}_{i+1} - \{z\}_{i-1}) \quad (1)$$

and

$$\{z\}''_i = 1/\Delta^2 (\{z\}_{i+1} - 2\{z\}_i + \{z\}_{i-1}) \quad (2)$$

where  $\{z\}_i$  is the vector of  $U$ ,  $V$ ,  $W$ , and  $M_s$  at the  $i^{\text{th}}$  station,  $\Delta$  is the uniform dimension between stations, and primes denote partial derivatives with respect to  $s$ . Applying these approximations to the governing set of domain

equations leads to

$$[C]_i \{z\}_{i-1} + [B]_i \{z\}_i + [A]_i \{z\}_{i+1} = \{g\}_i \quad (3)$$

When the shell does not have a pole, fictitious stations one increment off of the shell are introduced at each end. Both the governing domain equations and the boundary conditions are applied at the two boundary points. Thus, all finite difference approximations to the derivatives, including those of the boundary conditions, are of order

$\Delta^2$ . However, prior to the development of SATANS-IIA, the treatment of the conditions to be applied at a pole at either end of a shell was handled by a simple Euler forward or backward difference approximation to the first derivative, with truncation error of order  $\Delta$ . For example, for a pole at  $s=0$ , where  $i=1$ , the first derivative at the pole was approximated with

$$\{z\}'_1 = 1/\Delta (\{z\}_2 - \{z\}_1). \quad (4)$$

At the time this procedure for handling the pole conditions was developed (1967) it was thought that this would not significantly alter the solution. However, it has since been discovered that such is not the case.

For the new pole routine, an expanded forward difference approximation of order  $\Delta^2$  is used at  $s=0$  which takes into account the two stations after the pole, instead of just one station after the pole as in the Euler scheme. This approximation is

$$\{z\}'_1 = 1/2\Delta (-3\{z\}_1 + 4\{z\}_2 - \{z\}_3). \quad (5)$$

The conditions to be imposed upon the dependent variables at a pole are derived in Reference 14. They are :

$$\text{For } N=0, \quad u_1 = v_1 = w_1' = m_1' = 0.$$

Applying equation (5), these conditions can be put into the matrix form

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & -3 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 4 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & -1 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

where the above 3 matrices are DL, DG, and DF within the SATANS programs.

$$\text{For } N=1, \quad u_1 \pm v_1 = u' = w = m_s = 0,$$

where the plus sign applies at an initial pole, and the minus sign at a final pole. The matrix form for these conditions is

$$\begin{bmatrix} -3 & 0 & 0 & 0 \\ 1 \pm 1 & 0 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & 1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 4 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} -1 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

$$\text{For } N=2, \quad u = v = w = m_s' = 0$$

the matrix form is

$$\begin{bmatrix} 1 & 0 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 0 \\ 0 & 0 & 0 & -3 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_1 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 4 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_2 + \begin{bmatrix} 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & 0 \\ 0 & 0 & 0 & -1 \end{bmatrix} \begin{Bmatrix} u \\ v \\ w \\ m_s \end{Bmatrix}_3 = 0.$$

$$\text{For } N > 2, \quad u = v = w = m_s = 0$$

and DL= identity matrix, DG= DF= null matrices.

The solution procedure in SATANS is an elimination scheme and starts with

$$\{z\}_1 = - [P]_1 \{z\}_2 + \{x\}_1, \quad (6)$$

where the values in  $[P]_1$  based upon the Euler approximation are defined in Reference 14. The higher order approximation defines a new  $[P]_1$ . This new  $[P]_1$  is obtained by simultaneously solving the pole conditions

$$[DL] \{z\}_1 + [DG] \{z\}_2 + [DF] \{z\}_3 = \{0\}, \quad (7)$$

and the domain equation at station 2 next to the pole

$$[C]_2 \{z\}_1 + [B]_2 \{z\}_2 + [A]_2 \{z\}_3 = \{g\}_2, \quad (8)$$

to eliminate  $\{z\}_3$ . Thus,

$$\{z\}_3 = [A]_2^{-1} (\{g\}_2 - [C]_2 \{z\}_1 - [B]_2 \{z\}_2). \quad (9)$$

Substituting equation (9) into equation (7) gives

$$[DL] \{z\}_1 + [DG] \{z\}_2 + [DF] [A]_2^{-1} (\{g\}_2 - [C]_2 \{z\}_1 - [B]_2 \{z\}_2) = 0. \quad (10)$$

Combining like coefficients of the  $\{z\}$  vector leads to

$$([DL] - [DF] [A]_2^{-1} [C]_2) \{z\}_1 + ([DG] - [DF] [A]_2^{-1} [B]_2) \{z\}_2 = - [DF] [A]_2^{-1} \{g\}_2. \quad (11)$$

Finally, solving for  $\{z\}_1$  yields

$$\begin{aligned} \{z\}_1 &= - [DL - DF \times A_2^{-1} \times C_2]^{-1} [DG - DF \times A_2^{-1} \times B_2] \{z\}_2 \\ &+ [DL - DF \times A_2^{-1} \times C_2]^{-1} [-DF \times A_2^{-1}] \{g\}_2. \end{aligned} \quad (12)$$

Thus,  $[P]_1 = - [DL - DF \times A_2^{-1} \times C_2]^{-1} [DG - DF \times A_2^{-1} \times B_2]$  and  $\{x\}_1 = [DL - DF \times A_2^{-1} \times C_2]^{-1} [-DF \times A_2^{-1}] \{g\}_2$ . The new  $[P]_1$  matrix has been placed into the "PMATRIX" subroutine of SATANS-IIA and the new  $\{x\}_1$  vector has been placed in the "FORCE" subroutine.

A listing of the pole routine may be found in Appendix D. To incorporate this new routine into a SATANS-I or-II program, first proceed to the "PMATRIX" subroutine and remove the fifteen cards that are between, but not including, "IF(NN.GT.2) GO TO 90" and "11 CONTINUE". These cards are located after statement number "14" and just before statement number "11". Replace the cards removed by the ones listed in Appendix D which read from "C IN PMATRIX" to "90 M3=MN". Then proceed to the "FORCE" subroutine and remove statement number "10". Replace statement number "10" with the nine cards listed in Appendix D which read from "C IN FORCE" to "DO 11 I= 1,4". Also place "COMMON /IBL5/IBCINL, IBCFNL" into the common area of the "FORCE" subroutine.

This completes the implementation of the new pole routine into either SATANS-I or II.

#### IV. PROBLEM DESCRIPTION

The geometry of the shallow spherical shell used in this study is identical to that used in Reference 1. Briefly, the shallow shell can be specified by the non-dimensional parameter  $\lambda$ , where

$$\lambda = 2[ 3 ( 1 - \nu^2 ) ]^{1/4} ( H / h )^{1/2}. \quad (1)$$

H is the rise of the shell, h is the thickness, and  $\nu$  is Poisson's ratio. The mass density of the shell is  $m$ . All shells analyzed had the following dimensions;

Radii of Curvature	$R = R_s = 250$ inches
Thickness	$h = 0.25$ inches
Modulus of Elasticity	$E = 30,000,000$ psi
Poisson's Ratio	$\nu = 0.3$

All buckling pressures obtained will be listed as a percent of the classical buckling pressure of a complete sphere,  $q_0$ , where

$$q_0 = [ 2 E ( h / R_s )^2 ] / [ 3 ( 1 - \nu^2 ) ]^{1/2} \quad (2)$$

Forty stations were used over the meridian. The nondimensional time increment  $\delta t$ , where

$$t = T / ( R_s^2 m / E )^{1/2}, \quad (3)$$

was taken as 0.05 for 3000 time steps, which is a total nondimensional time of 150. In addition, the axisymmetric analysis was repeated with a larger time step of  $\delta t = 0.2$  for a total time of 600. In this study  $m$  was selected such that  $t$  is equal to  $T$ . The necessity for the long response time is explained in Reference 6.

In the axisymmetric analysis only the  $N=0$  harmonic is considered. However, in the asymmetric analysis a second harmonic is excited by applying an incremental load in that harmonic. In addition, analyses of the shells  $\lambda = 6, 7.5,$  and  $11$  were made using five harmonics. The step pressure load for the axisymmetric harmonic is

$$\{q^{(0)}\} = P q_0 \{1\}, \quad (4)$$

and the step pressure load for the asymmetric second harmonic is

$$\{q^{(n)}\} = P q_0 \xi^{(n)} \{1\}, \quad (5)$$

where  $n > 0$ , and  $\xi^{(n)}$  is taken as 0.0001. The value taken for the second harmonic in the asymmetric analysis was the same as the critical harmonic for the static buckling analysis presented by Stilwell and Ball [2]. When there was an uncertainty as to which was the critical static harmonic the two harmonics in question were both tested. Run times using SATANS-IIA with a two-harmonic analysis for 3000 time steps and 40 stations on the meridian took an average of 28 minutes on the IBM 360/67.

The parameter used to determine the minimum load at which dynamic buckling occurs is the peak value of  $\bar{v}$ , called

$\bar{V}_{MAX}$ , where  $\bar{V}$  is defined as

$$\bar{V} = \int_0^{r_0} r w^{(0)} dr / \int_0^a r \xi dr \quad (6)$$

$r$  is the normal distance from the axis to the shell,  $r_0$  is the maximum value of  $r$ ,  $w^{(0)}$  is the normal displacement of the axisymmetric response and  $\xi$  is the vertical distance from the base plane to the undeformed shell. The  $\bar{V}$  is a measure of the volume of the shell deformation. The Fortran statements computing  $\bar{V}$  and  $\bar{V}_{MAX}$  are given in Appendix E.

When working a problem that requires these calculations the nineteen cards are inserted directly into the "DYNAMIC" subroutine right after the "IF" statement that calls the "OUTPUT" subroutine.

For convenience, the response in each asymmetric harmonic is also measured using equation (6), with  $w^{(0)}$  replaced with  $w^{(n)}$ . The parameter  $\bar{V}$  for the asymmetric harmonics does not represent a volume of deformation as it does for the axisymmetric harmonic. It can, however, be used to indicate the relative excitation of the asymmetric harmonics.

The buckling criterion for both the axisymmetric and the asymmetric dynamic buckling analysis defines the critical load as that load  $P$  where a very small increase in  $P$  causes a very large increase in  $\bar{V}_{MAX}$ . This is the same criterion

as that used in Ref. [1].

## V. RESULTS AND DISCUSSION

### A. STATIC AXISYMMETRIC BUCKLING ANALYSIS

Table I presents the new results from the static axisymmetric buckling analyses for  $\lambda = 4$  through 13 using the new pole routine. The two upper curves in Figure 1 present a comparison of the new results obtained by SATANS-IIA with those obtained by Stilwell and Ball [2] using the SATANS-I program. As can be seen in this figure, fairly significant changes in the buckling load occurred in the neighborhood of  $\lambda = 4, 5$ , and 9; and somewhat smaller differences occurred in the region  $\lambda = 10$  through 13. The upper data points in Figure 2 present the comparison of the new results from SATANS-IIA with those obtained by Huang [4]. This comparison shows a very good agreement between the two sets of results, except for the largest values of  $\lambda$ . The new results have eliminated the differences that existed between the SATANS-I results and Huang's results.

### B. DYNAMIC AXISYMMETRIC BUCKLING ANALYSIS

Figure 3 presents the new results for the peak value of  $\bar{v}_{MAX}$  versus P for the various values of  $\lambda$  tested. Table II presents all of the new results for the dynamic axisymmetric buckling load. These loads are selected from figures constructed just like Figure 3. In every case,

except for  $\lambda = 4$ , a value of  $P$  slightly above the  $P_{CRIT}$  value caused a  $\bar{V}_{MAX}$  indicative of buckling, as well as a nonconvergence of the iterative solution procedure.

The lower two curves of Figure 1 present a comparison versus  $\lambda$  of the new axisymmetric dynamic buckling results with the previous buckling results obtained by Ball and Burt [1]. In every case the new critical pressure is lower than the critical pressure obtained using the Euler approximation at the pole.

The lower data points of Figure 2 present a comparison of the new results with those obtained by Huang [5], by Stephens and Fulton [6], and by Stricklin [8]. Just as in the case of the static axisymmetric buckling analysis, the new results compare much more favorably with the other results than did the results of Reference 1. It's interesting to note that the new results now tend to be slightly lower than the other results, whereas the results of Reference 1 were higher for almost all values of  $\lambda$ .

### C. DYNAMIC ASYMMETRIC BUCKLING ANALYSIS

Table III presents the new results for the critical pressures obtained from the dynamic asymmetric analysis. The second harmonics, or critical static harmonics, used in the analyses are also presented in Table III. A comparison of the critical pressures from the asymmetric analyses, Table III, with the critical pressures from the axisymmetric analyses, Table II, reveals that only the shell  $\lambda = 6$  buckled at a load below the axisymmetric buckling load. For the shell  $\lambda = 7$  the critical buckling load was slightly

larger when asymmetric motion was considered. In all other cases the buckling was not influenced by the presence of the second harmonic. These new buckling results and those by Ball and Burt [2] are plotted in Figure 4. The new results can be seen to be significantly different from the SATANS-I results, where the asymmetric buckling loads were lower than the axisymmetric loads for five out of the ten values of tested.

Except for  $\lambda = 6$  and  $7$ , the relationship between  $\bar{V}_{MAX}$  and  $P$  for the  $N=0$  harmonic, in the two-harmonic analyses, was found to be essentially identical to the relationship found in the axisymmetric buckling analysis shown in Figure 3. Table IV A presents the  $\bar{V}_{MAX}$  versus  $P$  data for both the  $N=0$  harmonic and the second harmonic, for all values of  $\lambda$  tested, except for  $\lambda = 6$ . Note that, except for  $\lambda = 7$  and  $11$ ,  $\bar{V}_{MAX}$  for the asymmetric harmonic is generally very small, even when the  $\bar{V}_{MAX}$  for the  $N=0$  harmonic indicates that the shell has buckled. Thus, except for the shells  $\lambda = 6$  and  $7$ , the presence of the asymmetric motion does not influence the axisymmetric motion, and except for the shells  $\lambda = 6, 7$  and  $11$  the asymmetric motion is very small prior to buckling in the axisymmetric harmonic.

A more detailed analysis of the shell  $\lambda = 6$  has been conducted since it was the only shell that revealed any significant axisymmetric sensitivity to asymmetric motion. This shell was studied using two two-harmonic analyses ( $N=0, 1$  and  $N=0, 2$ ) and a five-harmonic analysis ( $N=0, 1, 2, 3$ , and  $4$ ). Figure 5 and Tables IV B and IV C contain values of  $\bar{V}_{MAX}$  versus  $P$  for both of the asymmetric harmonics,  $N=1$

and  $N=2$ , in the two two-harmonic analyses, as well as the values of  $\bar{V}_{MAX}$  for the axisymmetric harmonic,  $N=0$ . Figure 6 and Table IV D present the values of  $\bar{V}_{MAX}$  versus  $P$  for the  $N=0,1,2,3$ , and 4 harmonics from the five-harmonic study. A comparison of the critical buckling load predicted from the results of the two two-harmonic analyses in Figure 5 with the critical load from the five-harmonic analysis obtained from Figure 6 shows that the presence of the additional harmonics results in the shell buckling at a slightly lower load (0.50), with significant motion in the  $N=1$  harmonic instead of the  $N=2$  harmonic (see the nonconverged solution at  $P=0.51$ ), which is the critical harmonic for static asymmetric buckling. Studies using five harmonics have also been conducted for  $\lambda=7.5$  and  $\lambda=11$ . As can be seen in Table IV D the critical harmonic for  $\lambda=7.5$  remained  $N=3$ ; however, significant motion occurred in that harmonic at  $P=.41$  and  $.44$ . In the case of  $\lambda=11$ , relatively large asymmetric motion occurred in the asymmetric mode of  $N=5$  vice 6 at a value of  $P=.46$ .

The comparison of the new results for the critical pressure for dynamic asymmetric buckling with those obtained analytically by Stricklin [8], by Akkas [9], and experimentally by Lock et al [7] is illustrated in Figure 7. The comparison reveals an agreement with Stricklin in every case, in general a higher value of  $P_{CRIT}$  than those obtained by Akkas, and most importantly a very good agreement with Lock's experimental results.

When making the comparison between the new results and those obtained by Akkas, it is necessary to look at the differences in the problem solution parameters used in the two studies. For example, buckling results obtained from SATANS-IIA using the same time increment as used by Akkas,

$\delta t = .2$  for 3000 time steps, were significantly higher than those using the time step of  $\delta t = .05$  for many values of  $\lambda$ . Furthermore, the new results had, in some cases, instances of buckling occurring as far out in time as 130. Akkas, to shorten computer run times, observed the cap only for a time of less than 5. Furthermore, only the harmonics  $N = 1$  or 2 or 3 were studied by Akkas for shells  $\lambda = 5$  through 12. If the critical harmonic is not studied, the predicted load will be too high. Thus, it appears that Akkas' lower bound loads may not be true lower bounds.

Two additional features of the shell response should be noted. First, shells  $\lambda = 6, 7.5,$  and 11 exhibited a non-buckled response in the axisymmetric harmonic to a load larger than the defined critical buckling load. This can be seen in Tables IV A and IV C. Second, and most importantly, the buckling load proposed by Ball and Burt [1], and used here, defines buckling to occur when the  $\bar{v}_{MAX}$  in the axisymmetric harmonic undergoes a large change due to a small change in  $P$ . Another criterion for dynamic buckling in the asymmetric analysis discussed in Reference 1 is to define the buckling load as that threshold load that initiates significant growth in the asymmetric harmonic. Re-examination of the  $\bar{v}_{MAX}$  versus  $P$  data in Table IV A through D reveals that shells  $\lambda = 6, 7,$  and 11 exhibited relatively large asymmetric motion at loads smaller than the defined buckling load when compared with other  $\bar{v}_{MAX}$  values for those shells, even though the numbers themselves were small when compared with the axisymmetric harmonic. Shells  $\lambda = 7.5$  and 12 appear to be borderline cases. If the alternate criterion for buckling is used, the critical buckling loads for shells  $\lambda = 6, 7,$  and 11 become 0.47, 0.45, and 0.45, respectively. The shells  $\lambda = 7.5$  and 12 could have buckling

loads as low as 0.40 and 0.44, respectively. These values are more conservative than the definition based upon axisymmetric response. These five shells are the same five shells that exhibited an asymmetric buckling load lower than the axisymmetric buckling load in Reference 1.

## VI. SUMMARY AND CONCLUSIONS

A digital computer program for the geometrically nonlinear analysis of totally arbitrarily loaded shells of revolution (SATANS-II) was modified to more accurately account for the conditions at the pole of the shell. This program, called SATANS-IIA, was used to determine the buckling load of shallow spherical shells of various sizes when subjected to static axisymmetric, dynamic axisymmetric, and dynamic nearly axisymmetric step-pressure loads of infinite duration. The cap sizes ranged from  $\lambda = 4$  to 13 including  $\lambda = 7.5$ . A comparison was made between the new buckling results with the improved pole handling routine and the results that did not have the new pole routine. The comparison revealed a significant change in buckling pressures, due solely to the change from an order  $\Delta$  finite difference approximation of the first derivatives at the pole to an approximation of order  $\Delta^2$ . These new critical pressures are in very good agreement with the results from other studies of the same spherical shells. This good agreement with other results, which came about as a result of the modification of the pole handling routine, is a strong indication that the manner in which the pole condition is handled is vital to the accuracy of the solutions obtained.

In the asymmetric analysis, two harmonics were included for most of the shells; the axisymmetric harmonic and one asymmetric harmonic. Five-harmonic analyses were conducted for three of the shells. Two buckling criteria for the

asymmetric analysis were considered. One defined buckling as that threshold load that caused a large increase in a deformation parameter,  $\bar{v}_{MAX}$ , in the axisymmetric harmonic.

The other, more conservative than the first, defined buckling as that threshold load that caused a large increase in the  $\bar{v}_{MAX}$  value for the asymmetric harmonic. Both values

have been presented.

The new static axisymmetric, dynamic axisymmetric, and even the dynamic asymmetric critical buckling pressure loads appear to be fairly reliable results for perfect, shallow shells. The effect of realistic imperfections remains to be determined.

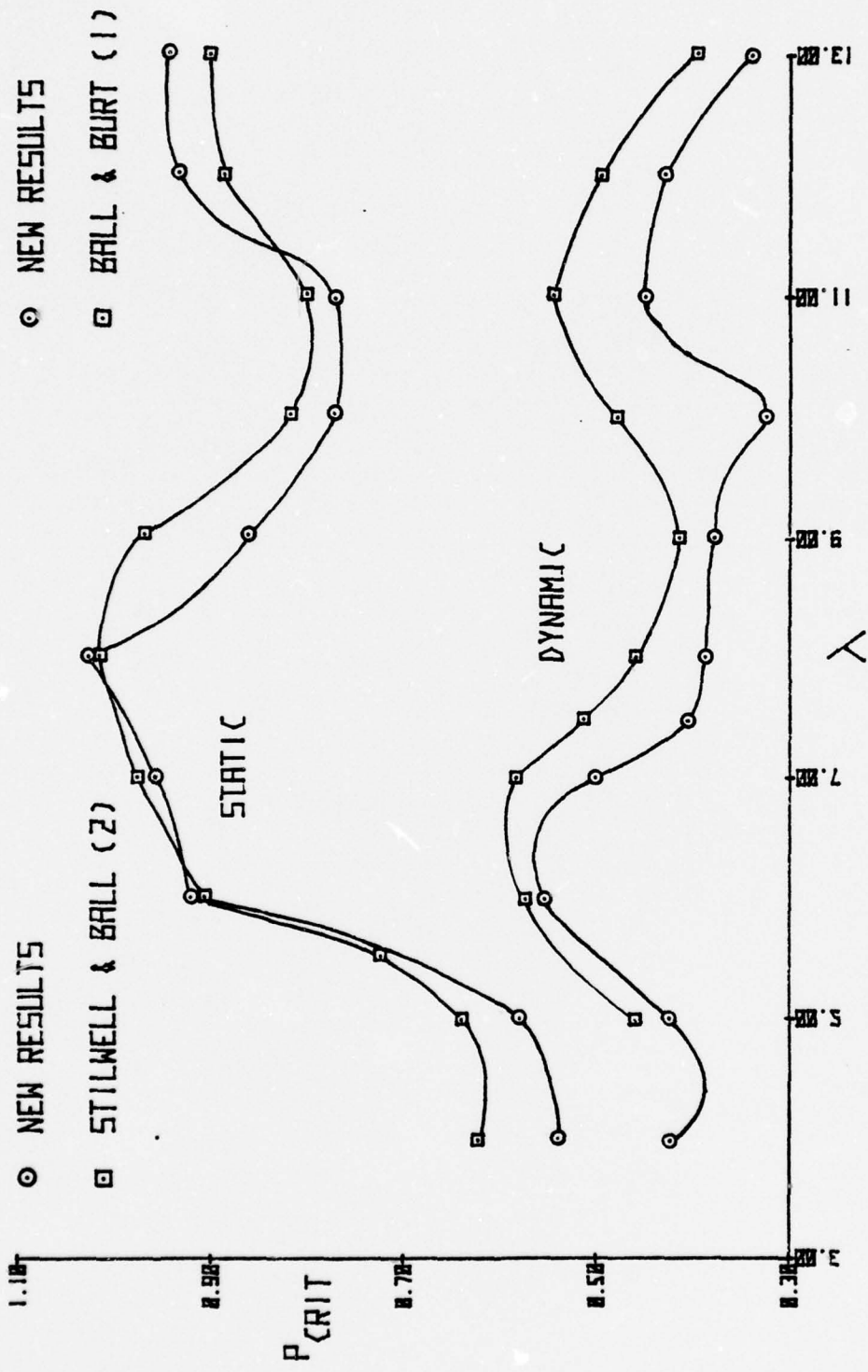


Figure 1 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
 AXISYMMETRIC (SATANS-I VERSUS SATANS-IIA)

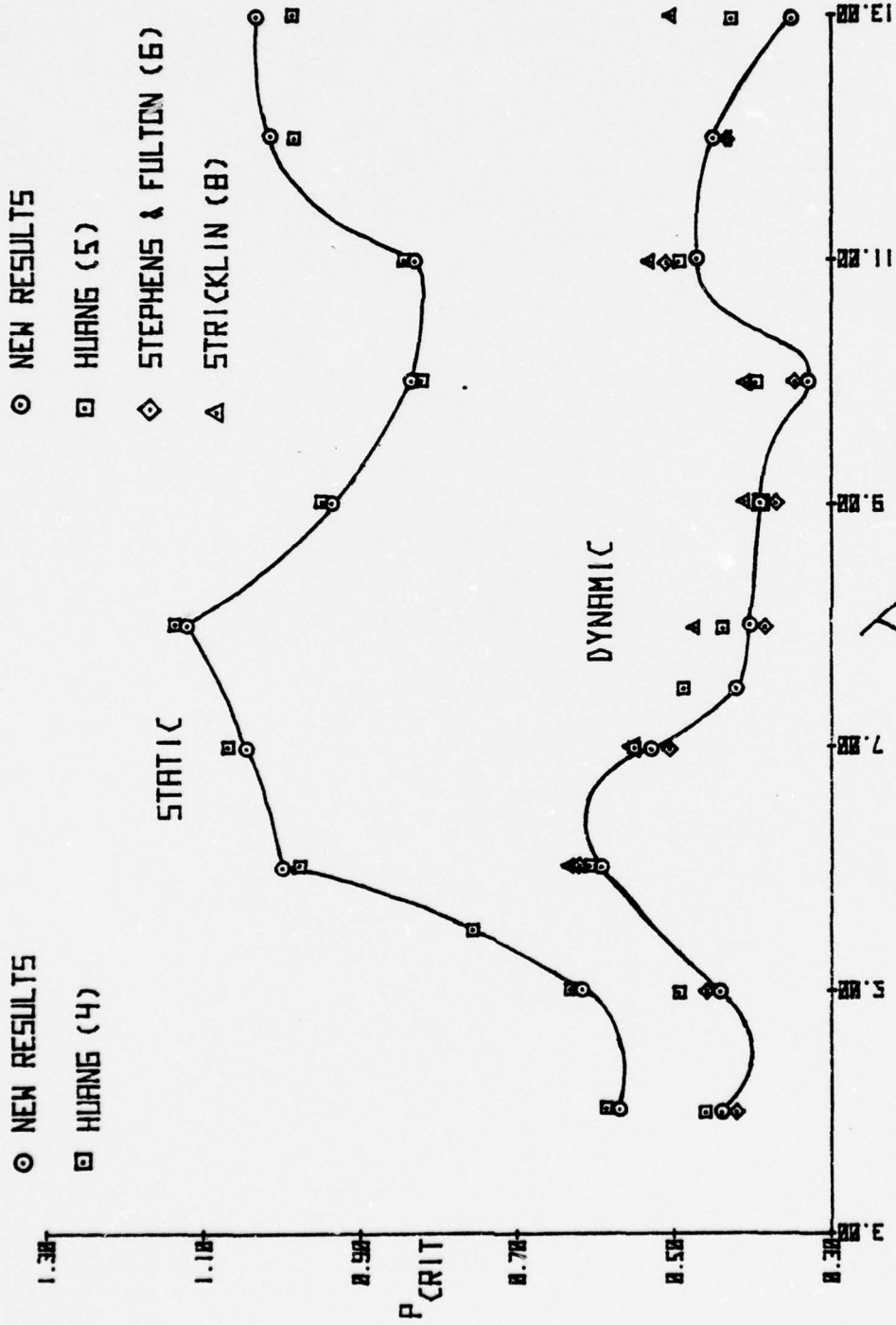


Figure 2 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
 AXISYMMETRIC (SATANS-1IA VERSUS ALL OTHERS)

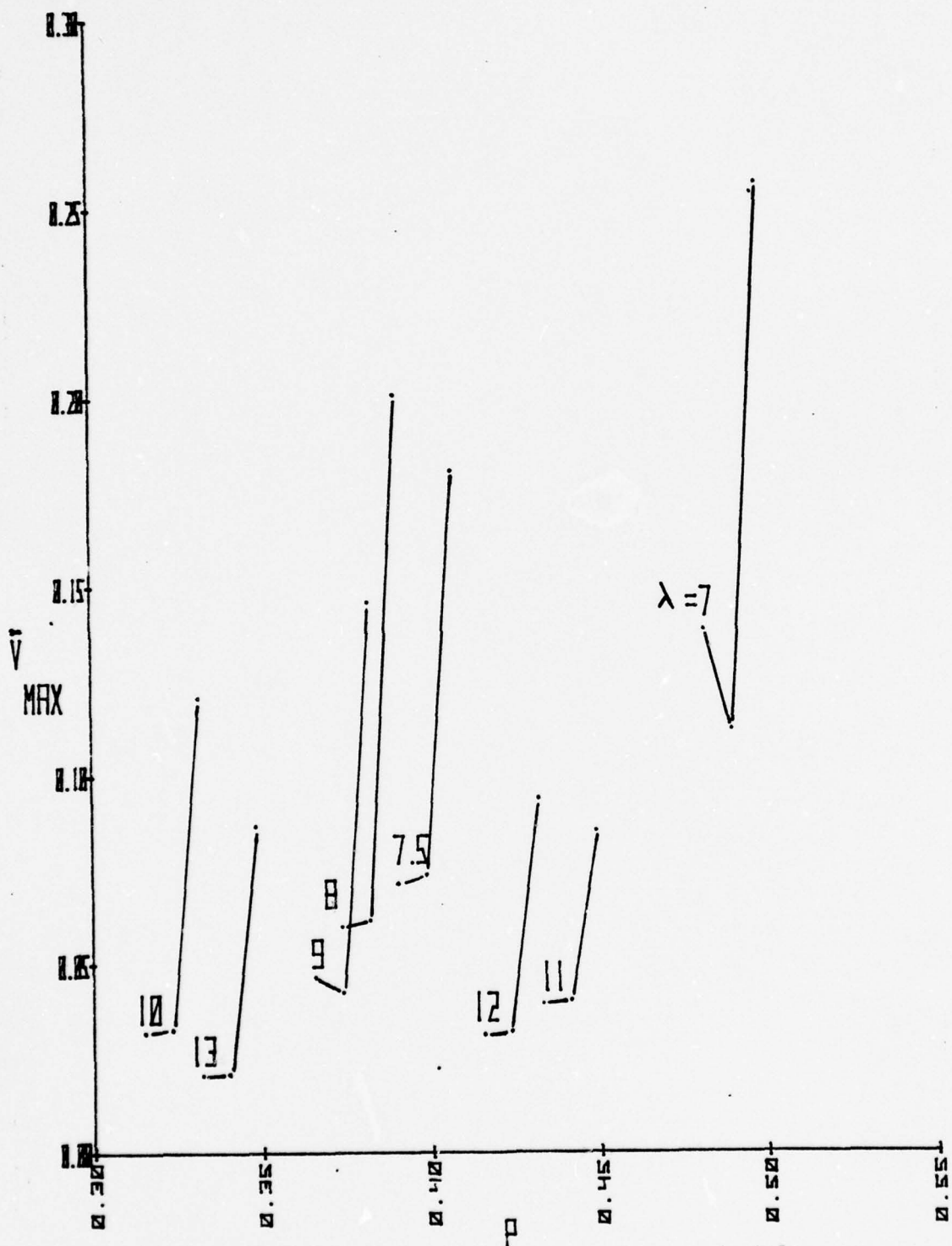


Figure 3 - PEAK DEFLECTION VERSUS P, AXISYMMETRIC AND ASYMMETRIC CASES FOR VARIOUS VALUES OF  $\lambda$  (SATANS-IIA)

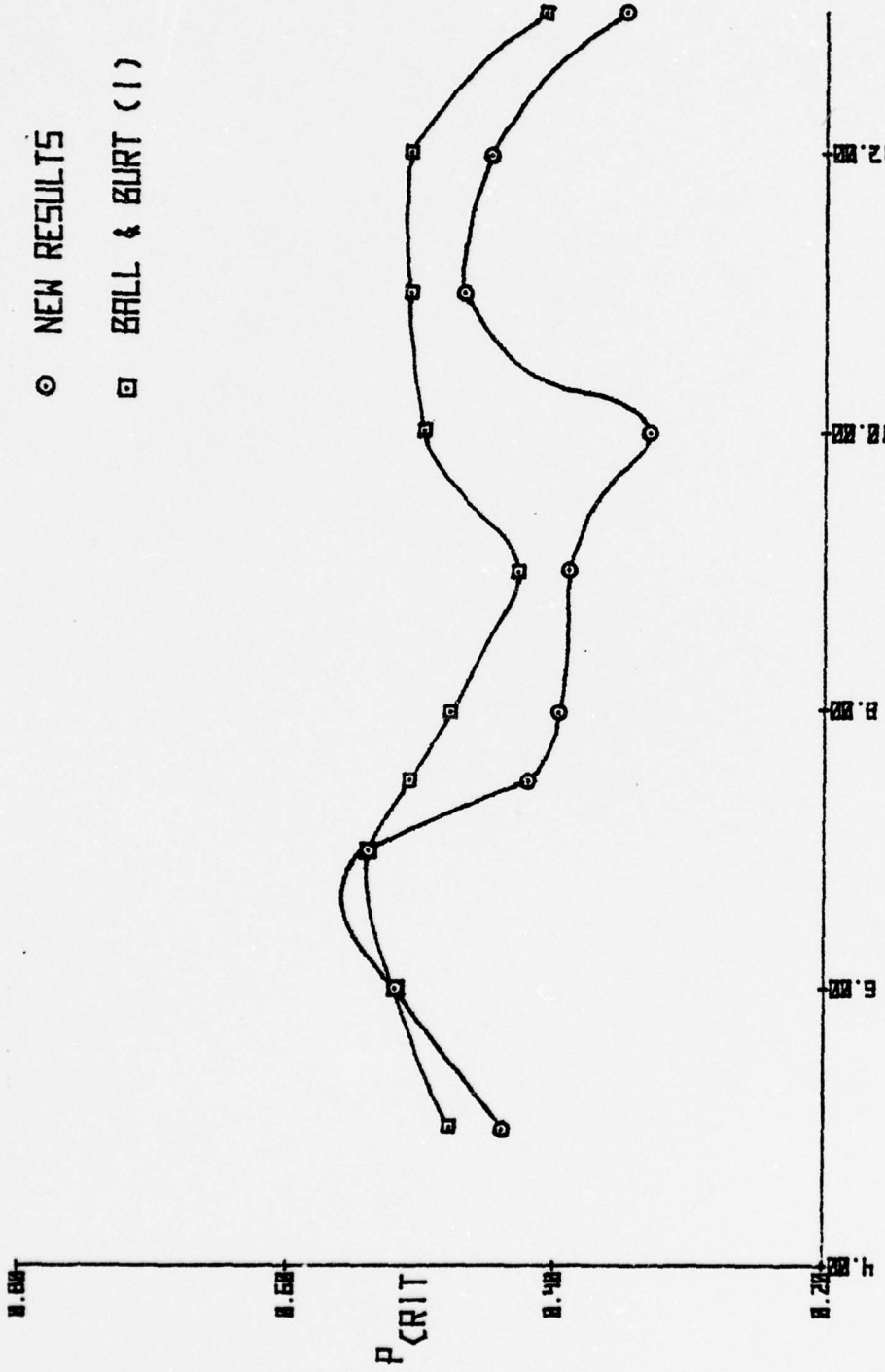


Figure 4 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
 ASYMMETRIC ANALYSES (SATANS-I VERSUS SATANS-IIA)

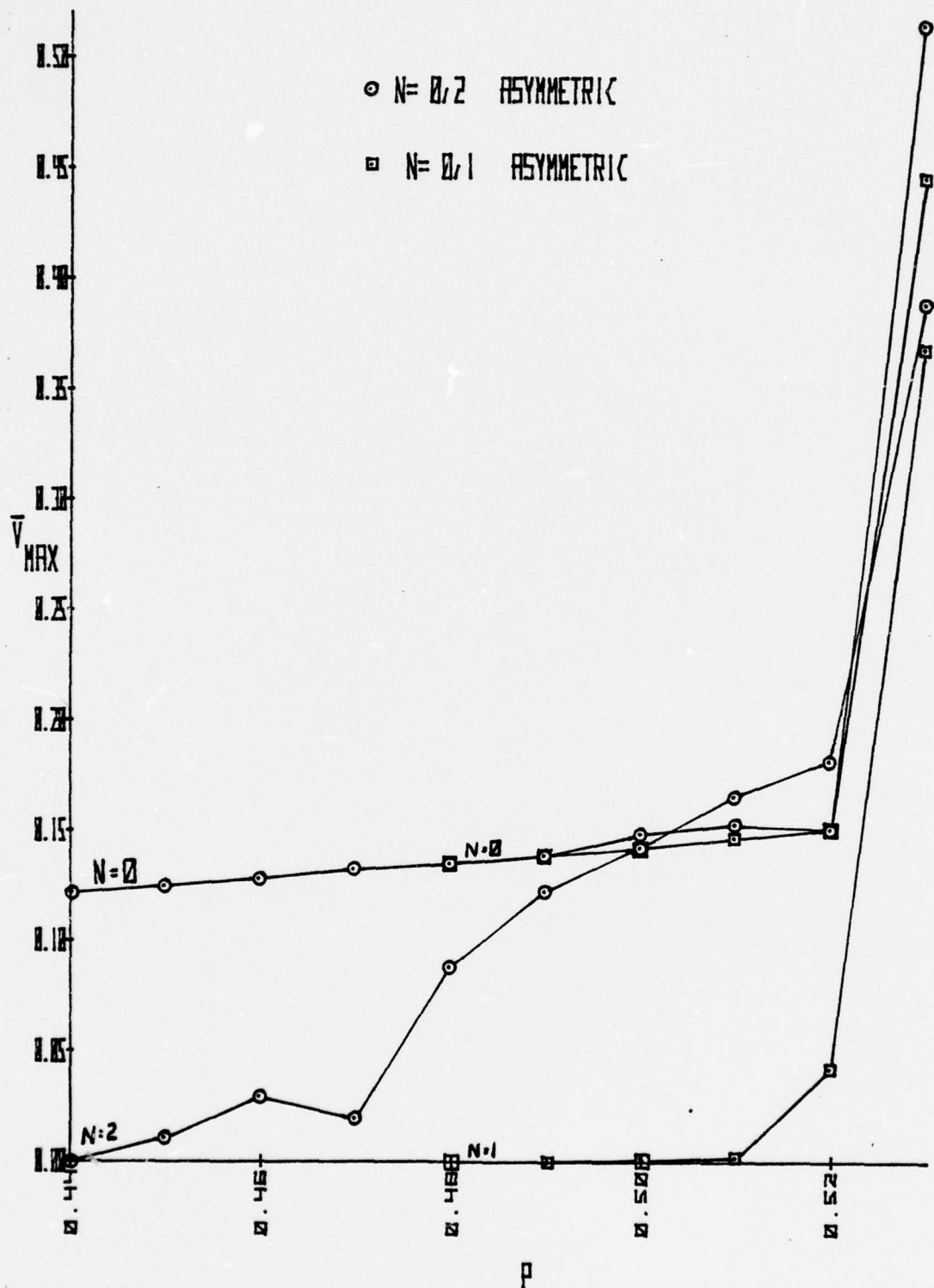


Figure 5 - PEAK DEFLECTION VERSUS P FOR THE ASYMMETRIC ANALYSES OF  $\lambda = 6$  (N=0,1 AND N=0,2)

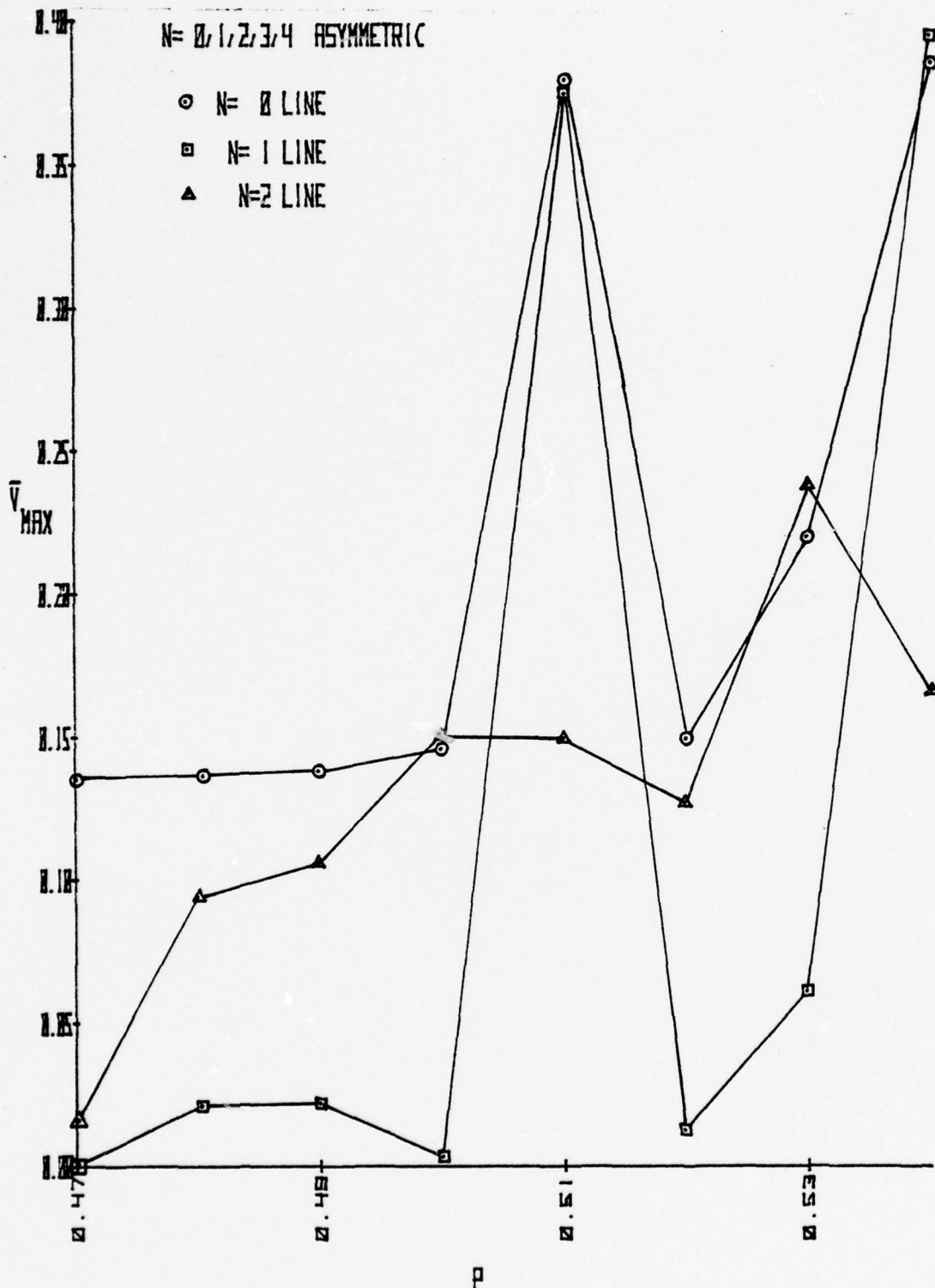


Figure 6 - PEAK DEFLECTION VERSUS P FOR THE ASYMMETRIC ANALYSES OF  $\lambda = 6$  (N=0, 1, 2, 3, AND 4, ONLY N=0, 1, AND 2 PLOTTED)

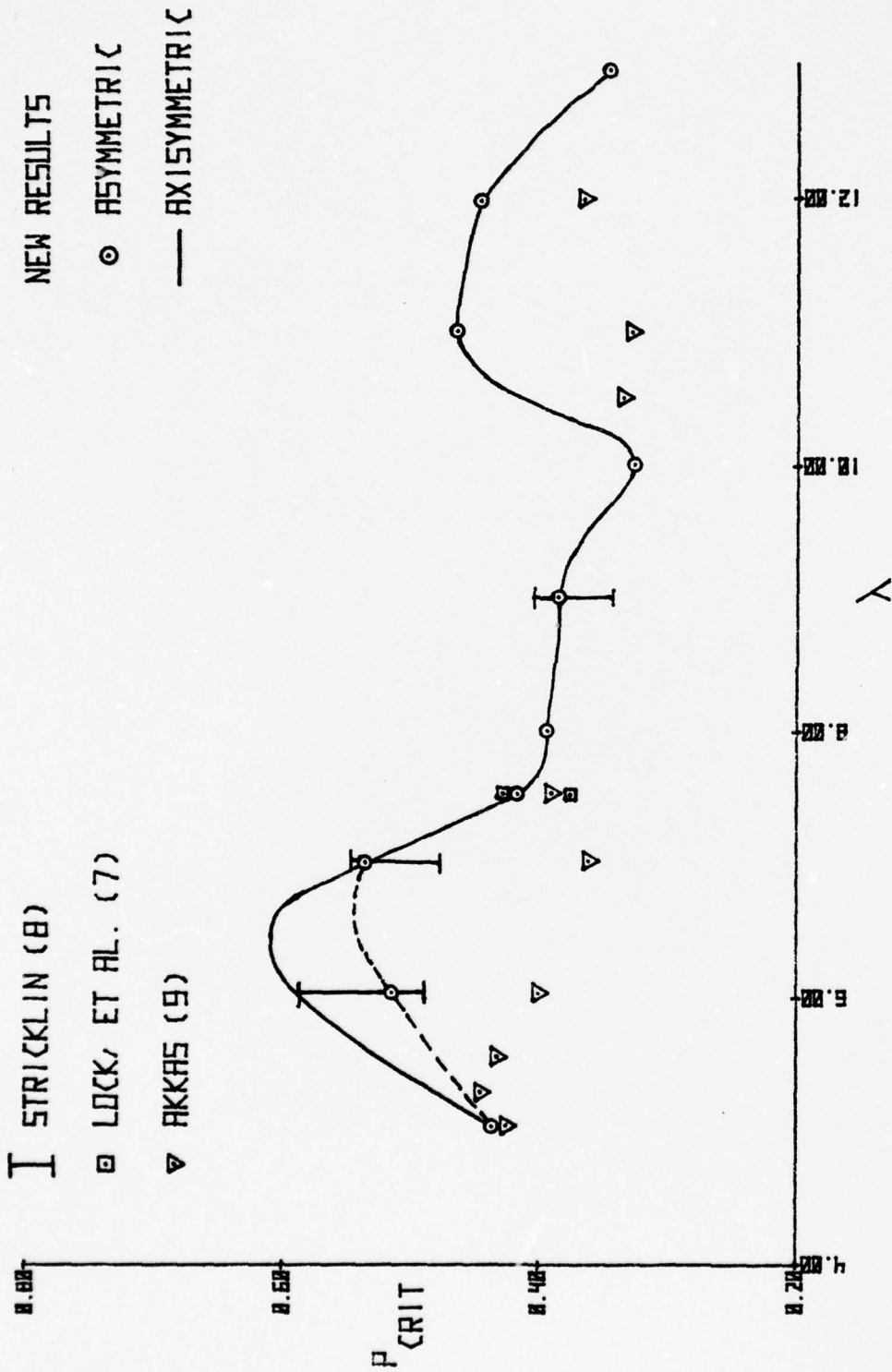


Figure 7 - CRITICAL STEP-PRESSURE LOAD VERSUS  $\lambda$   
ASYMMETRIC ANALYSES (SATANS-IIA VERSUS ALL OTHERS)

A. TABLES

1. TABLE I Critical pressure loads from the static axisymmetric analyses.

$\lambda$	4	5	6	7	8	9	10	11	12	13
$P_{CRIT}$	.568	.616	1.0	1.048	1.12	.936	.832	.832	1.016	1.032

2. TABLE II Critical step-pressure loads from the axisymmetric dynamic analyses.

$\lambda$	4	5	6	7	7.5	8	9	10	11	12	13
$P_{CRIT}$	.45	.44	.59	.53	.42	.40	.39	.33	.47	.45	.35

3. TABLE III Critical step-pressure loads from the dynamic asymmetric analyses and critical asymmetric harmonics.

$\lambda$	5	6	7	7.5	8	9	10	11	12	13
$P_{CRIT}$	.44	.52	.54	.42	.40	.39	.33	.47	.45	.35
$N_{CRIT}$	1	2	3	3	4	5	6	7	8	9

4. TABLE IV Dynamic asymmetric analyses for  $\bar{V}_{MAX}$  versus

P.

1. TABLE IV A. Two-harmonic analyses for all values of  $\lambda$  except  $\lambda = 6$ .

$\lambda = 5$  N= 0 and 2

N= 0 and 1

P	.43	.44	.45	P	.44	.45
N= 0	.1659	.1676	.6606	N= 0	.1675	.6606
N= 2	.0004787	.0000566	.0687	N= 1	.0003145	.0687
				P	.46	
				N= 0	.7653	
				N= 1	.001092	

$\lambda = 7$ , N= 0 and 3

P	.45	.46	.47	.48	.49	.50	.52
N= 0	.09452	.09571	.09812	.1005	.1029	.1052	.1099
N= 3	.000889	.007456	.05052	.04323	.0279	.0335	.07488
P	.53	.54	.55				
N= 0	.1122	.1146	.2709				
N= 3	.05997	.06252	.03809				

$\lambda = 7.5$ , N= 0 and 3

P	.40	.41	.42	.43	.44	.45
N= 0	.0703	.07228	.07429	.2636	.07837	.2076
N= 3	.0001094	.001296	.0004304	.002754	.001188	.000338
P	.46					
N= 0	.200					
N= 3	.0003276					

$\lambda = 8, N = 0 \text{ and } 4$

P	.38	.39	.40	.41	.42	.43
N= 0	.05893	.0607	.0624	.1964	.1713	.1957
N= 4	.0000566	.0000703	.0000364	.0000333	.0000274	.0000299
P	.44					
N= 0	.2297					
N= 4	.0000326					

$\lambda = 9, N = 0 \text{ and } 4$

P	.38	.39	.40		P	.40
N= 0	.04738	.04875	.1576		N= 0	.05012
N= 4	.00003597	.00004635	.00004497		N= 5	.00008385

$N = 0 \text{ and } 5$

$\lambda = 10, N = 0 \text{ and } 5$

P	.32	.33	.34	.36	.38	.40
N= 0	.03239	.03347	.1086	.1217	.1288	.1235
N= 5	.0000281	.0000472	.00004125	.00002103	.0000449	.000114

$\lambda = 11, N = 0 \text{ and } 6$

P	.45	.46	.46	.48	.49	.50
N= 0	.03910	.04004	.04099	.09814	.04241	.08824
N= 6	.004595	.01332	.02232	.02864	.03955	.02813

$\lambda = 12, N = 0 \text{ and } 7$

P	.44	.45	.46
N= 0	.03236	.03316	.08633
N= 7	.00004214	.0004561	.00005158

$\lambda = 13, N = 0 \text{ and } 8$

P	.34	.35	.36	.38	.40
N= 0	.02119	.02185	.06637	.07844	.07381
N= 8	.00001148	.00001134	.000006607	.000008245	.000119

2. TABLE IV B. Two-harmonic analyses with  $N=0$  and 1,  
 $\lambda = 6$  only.

P	.48	.49	.50	.51	.52	.53
N= 0	.1350	.1385	.1421	.1460	.1499	.4453
N= 1	.0002797	.000195	.000245	.000926	.04081	.3668

3. TABLE IV C. Two-harmonic analyses with  $N=0$  and 2,  
 $\lambda = 6$  only.

P	.44	.45	.46	.47	.48	.49	.50
N= 0	.1218	.1250	.1276	.1320	.1350	.1385	.1479
N= 2	.000239	.0101	.0293	.01976	.08768	.1223	.1419
P	.51	.52	.53	.54	.55	.56	
N= 0	.1526	.1499	.5137	.5060	.2040	.5305	
N= 2	.1654	.1816	.3878	.3996	.2156	.3617	

4. TABLE IV D Five-harmonic analyses for selected  
shells.

$\lambda = 6$   $N=0,1,2,3,$  and 4

P	.47	.48	.49	.50	.51	.52	.53
N= 0	.1313	.1347	.1382	.1460	.3797	.1498	.2200
N= 1	.00021	.02108	.02215	.003676	.3743	.01276	.0616
N= 2	.0187	.0953	.1069	.1507	.1502	.1279	.2385
N= 3	.000181	.006237	.01437	.00163	.0405	.0123	.03978
N= 4	.0031	.04757	.05428	.04402	.05896	.0495	.064
P	.54						
N= 0	.3854						
N= 1	.3953						
N= 2	.1671						
N= 3	.05298						
N= 4	.0613						

$\lambda = 7.5$   $N = 0, 1, 2, 3, 4$  and 4

P	.40	.41	.42	.43	.44	.45
N= 0	.0703	.07228	.07429	.2592	.07837	.2544
N= 1	.00004855	.00004198	.00006093	.0002737	.0001167	.005952
N= 2	.0001164	.00007456	.0004184	.0000982	.000788	.0003188
N= 3	.0001277	.001187	.0004597	.0002853	.00107	.0003188
N= 4	.0008224	.0001898	.0002448	.0000526	.000280	.000134

$\lambda = 11$   $N = 0, 4, 5, 6,$  and 7

P	.45	.46	.47	.48	.49	.50
N= 0	.03910	.04004	.0499	.04195	.04291	.1040
N= 4	.0005759	.001263	.0009774	.001388	.002657	.001565
N= 5	.009568	.0140	.0124	.02239	.02759	.01548
N= 6	.002560	.007828	.02330	.02767	.02602	.02644
N= 7	.0001743	.0001486	.0002021	.01202	.02048	.02064

APPENDIX A

LISTING OF SATANS-IIA

```

C*****SAT00010
C THIS PROGRAM SERVES AS THE 'MAIN' PROGRAM, AND CALLS 'SATANS', *SAT00020
C AND CHECKS 'IRNAGN', TO SEE IF WE DESIRE ANOTHER RUN
C*****SAT00030
C*****
C DIMENSION P(4,4,124), DEE(4,4,124), DST(4,4,124), X(4,124), Z(4,132),
C (4,132), Z2(4,132), Z3(4,132), ZCCCF(4,132), IS(59,4), JS(95,4),
C (59,4), JD(99,4), PHIXB(124), PHITE(124)
C *****
C CCMMCN /BLTHTA/ IRNAGN
C CCMMCN /BLTHTA/ THETAM, COEFF
C CCNTINUE
C CALL SATANS (P, DEE, DST, X, Z, Z0, Z2, Z3, ZDOT, IS, JS, ID, JD, PHIXB, PHITB)
C IF (IRNAGN.EQ.1) GC TO 1
C CALL FLYNVY
C STCF
C END

```

```

C*****
C SLERCUTINE GEOM
C *****
C THIS SUBROUTINE COMPUTES THE NONDIMENSIONAL GEOMETRY FUNCTIONS *
C *****
C CF TFE SHELL
C *****
C REAL NU, LAM, LAM2, JAY, MT, LSD18, LSDIN, MASS
C *****
C CCMMCN /BL4/ KMAX, KL
C CCMMCN /BL8/ R(500), GAM(500), OMT(500)
C CCMMCN /BL11/ OMXI(500), PHEE, f0, f2
C CCMMCN /BL17/ DEL
C CCMMCN /BL20/ DEOMX(500)
C CCMMCN /BL32/ TKN, ELAST, CHAR, SIGC
C CCMMCN /BL102/ DELOAD
C CCMMCN /BL103/ MASS(500)
C CCMMCN /BLTHTA/ THETAM
C *****
C AKX=KMAX-1
C DEL=1./AKX
C TFE=ARSIN(2.2801/CHAR)
C CC 11 K=1, KMAX
C AK=K
C R(K)=(7.9455+(AK-1.)*(2.2801)/AKX)/CHAR
C GAM(K)=(2.2801/CHAR)/R(K)
C OMXI(K)=0.
C DEOMX(K)=0.
C CCNT(K)=CCS(THET)/R(K)
C MASS(K)=1.
C CCNTINUE
C RETURN
C *****

```

```

C*****
C SLERCUTINE BCB(K,B,CB,D,DD)
C *****
SAT00080
SAT00090
SAT00100
SAT00110
SAT00120
SAT00130
SAT00140
SAT00150
SAT00160
SAT00170
SAT00180
SAT00190
SAT00200
SAT00210
SAT00220
SAT00230
SAT00240
SAT00250

```

```

C*****
SAT00350
SAT00360
SAT00370
SAT00380
SAT00390

```

```

C *****
C THIS SUBROUTINE COMPUTES THE NCNDIMENSIONAL IN-PLANE AND
C BENDING STIFFNESSES OF THE SHELL
C *****
C REAL NU, LAM, LAM2, JAY, MT, LSD18, LSD19
C CCMCN /BL15/ NU, U1(99), V1(99), W1(99), U2(99), U3(99),
C CCMCN /BL17/ DEL
C CCMCN /BL32/ TKN, ELAST, CHAR, SIGC
C B=1. C89C82
C L=.C5C15683
C DE=C.
C LL=0.
C RETURN
C ENCL

```

```

*SA100400
*SA100410
*SA100420
*SA100430
*SA100440
*SA100450
*SA100460
*SA100470

```

```

C *****
C SLRROUTINE PLOAD(K,Z)
C *****
C THIS SUBROUTINE ESTABLISHES THE NON-DIMENSIONAL FCURIER
C COEFFICIENTS OF THE LOADS APPLIED TO THE SPELL
C *****
C REAL MASS
C DIMENSION Z(4,1), MNMAX
C CCMCN /IBL1/ MNMAX
C CCMCN /IBL2/ NN(99), MNINIT
C CCMCN /IBL4/ KMAX, KL
C CCMCN /IBL8/ LSTEP, ITR
C CCMCN /BL3/ PR(99), PT(99)
C CCMCN /BL6/ SOE, OSE, ALOAD
C CCMCN /BL8/ R(500), GAM(500), OMT(500)
C CCMCN /BL32/ TKN, ELAST, CHAR, SIGC
C CCMCN /BL102/ DELGAD
C CCMCN /BL103/ MASS(500)
C CCMCN /BL17/ DEL/BL1CC/TEEO, $DYNMC
C CCMCN /BLTHTA/ THTAM, COEFF
C RETURN
C ENCL

```

```

SA100520
SA100530
SA100540
SA100550
SA100560
SA100570
SA100580
SA100590
SA100600
SA100610
SA100620
SA100630
SA100640
SA100650
SA100660
SA100670
SA100680
SA100690
SA100700
SA100710
SA100720

```

```

C *****
C SLRROUTINE INITL (Z,ZC,Z2,Z3,ZCCT)
C *****
C THIS SUBROUTINE DESCRIBES THE INITIAL CONDITIONS FOR DYNAMIC CASES
C *****
C IMPLICIT LOGICAL*1 ($)
C DIMENSION Z(4,1), ZC(4,1), Z2(4,1), Z3(4,1), ZCCT(4,1)
C CCMCN /IBL1/ MNMAX
C CCMCN /IBL2/ NN(55), MNINIT
C CCMCN /IBL4/ KMAX, KL
C CCMCN /IBL5/ MAXM
C CCMCN /IBL12/ KMAX1, KMAX2, NCONV
C CCMCN /BL6/ SOE, CSE, ALOAD

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SA100910
SA100920
SA101110
SA101120
SA101130
SA101140
SA101150
SA101160
SA101170
SA101180
SA101190
SA101200
SA101210
SA101220

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SAT01230  
SAT01240  
SAT01250

CCMMGN /BL32/ TKN, ELAST, CHAR, SIGC  
CCMMCN /BL100/ TEEC \$DYNMC  
CCMPON /BL101/ DELSD

NN(1)=0  
NN(2)=1  
NN(3)=2  
NN(4)=4  
PI=3.14159  
CC Z N=1, MAXM  
IF(P.EQ.1) VEL=-444.08/PI  
IF(P.EQ.2) VEL=-444.08/2  
IF(P.EQ.3) VEL=-444.08\*2./(3.\*PI)  
IF(P.EQ.4) VEL=-444.08\*2./(15.\*PI)  
IF(P.EQ.4) VEL= 444.08\*2./(15.\*PI)  
CC Z N=2, KL  
I=K+1+(N-1)\*KMAX2

2 ZCCT(3, I)=VEL\*ELAST\*TEEG/(CHAR\*SIGC)\*10  
RETURN

END  
SUBROUTINE TLOAD(K, Z)  
C\*\*\*\*\*  
C\*\*\*\*\* SUBROUTINE DESCRIBES TPE THERMAL LOADING CN TPE SHELL  
C\*\*\*\*\*  
C\*\*\*\*\*  
REAL NU  
DIMENSION Z(4, 1)  
CCMMCN /IBL1/ MNMAX  
CCMMCN /IBL2/ NN(99), MNINIT  
CCMMCN /IBL5/ NU, U1(99), V1(99), W1(99), U2(99), U3(99), U3(99),  
1 CCMMON /BL32/ TKN, ELAST, CHAR, SIGC  
CCMMCN /IBL8/ LSTEP, ITR  
CCMMCN /BL5/ TT(99), EMT(99), DT(99), DMT(99)  
2 CCMMON /BL6/ SOE, OSE, ALOAD  
RETURN  
END  
SUBROUTINE IMPERF (PHIXB, PHITB)  
DIMENSION PHIXB(1), PHITB(1)  
CCMMCN /IBL4/ KMAX, KL  
CCMMCN /IBL9/ MAXM  
KACM=KMAX\*MAXM  
CC I I=1, KANDM  
PHIXB(I)=0.  
PHITB(I)=0.  
1 CCONTINUE  
RETURN  
END  
SUBROUTINE SATANS (P, CEE, DST, X, Z, ZC, Z2, Z3, ZCCT, IS, JS, ID, JD, PH, IXB,  
SAT01260  
SAT01270  
SAT00940  
SAT00950  
SAT00960  
SAT00970  
SAT00980  
SAT00990  
SAT01000  
SAT01010  
SAT01020  
SAT01030  
SAT01040  
SAT01050  
SAT01060  
SAT01070  
SAT01080  
SAT01090  
SAT01100  
SAT01280  
SAT01290

SAT01300  
SAT01310  
SAT01320

1

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PHITB)
C** THIS SUBROUTINE READS ALL DATA, PRINTS THE CUIPUT TITLE PAGE,
C** AND PASSES CONTROL TO ONE OF THE MAJOR CCNTFCLLING SUBROUTINES
C**
C** *****
C** INFLICIT LCGICAL*1 ($), MT, LSD18, LSCD1N, MASS
C** REAL#4 NU, LAM, LAM2, JAY, DEE(4,4,1), DST(4,4,1), X(4,1), Z(4,1),
C** DIMENSION P(4,4,1), Z3(4,1), ZDOT(4,1), JS(99,1), IS(99,1), IC(99,1),
C** ZC(4,1), PHIXB(1), PHITB(1)
C** COMMON /IBL1/ MNMAX
C** COMMON /IBL4/ KMAX, KL
C** COMMON /IBL5/ IBCINL, IBCFNL
C** COMMON /IBL9/ MAXM
C** COMMON /IBL10/ IFRREG, NTHMAX
C** COMMON /IBL13/ ITRMAX, LSMAX
C** /IBLJ/ JUMP
C** COMMON /BL13/ OMEG1(4,4), CAPL1(4,4), OMEGL(4,4), CAPLL(4,4),
C** UNIT(4,4)
C** COMMON /BL15/ NU, U1(99), V1(99), W1(99), V2(99), U2(99), W2(99), U3(99),
C** V3(99), W3(99)
C** COMMON /BL16/ EPS
C** COMMON /BL18/ ELL(4)
C** COMMON /BL19/ TH(36)
C** COMMON /BL32/ TKN, ELAST, CHAR, SIGC
C** COMMON /BL100/ TEELC, $DYNMC
C** COMMON /BL102/ DELCAD
C** COMMON /BLPLOT/ IRADII, IGAMMA, ICMEGS, IOMEGT, ICEOMS, IBSTIF, IDSTIF,
C** IBBSTIF, IDDSIF, IPR, IPS, IPT, IPT, IMT, IDIT, IDMI, INS,
C** INTH, INSTH, IQS, IMS, IMCDAL
C** IPHIT, IPHI, $PLOTS, $MCDAL
C** ITITLE, NO, IMCDE, NDIEN, IPRINT, LCHMAX, IC
C**
C** COMMON /BLDATA/ IRNAGN
C** COMMON /BLRUN/ IRNAGN
C** DIMENSION TITLE (18)
C**
C** READ IN DATA FOR THIS RUN
C**
C** READ (5,100) TITLE
C** READ (5,101) NO, $CYNMC, IMODE, NDIEN, NTHMAX, IFREQ, IFRINT, IBCINL,
C** IBCFNL, KMAX, MNMAX, MAXM, LSMAX, LCHMAX, ITRMAX, IC
C** READ (5,102) NU, SIGC, ELAST, TKN, CHAR, TEEO
C** READ (5,103) DELLOAD, EPS
C** READ (5,101) JUMP
C** IF (NTH, MAX, EQ, 0) GC TO 1
C** READ (5,104) (TH, NTH), NTH=1, NTHMAX)
C** CC 2 NTH=1, NTHMAX)
C** IF (NTH) =TF, (NTH)*6.2831853/360.0
C** 1 IF (IBCINL.EQ.0) READ (5,105) OMEG1, CAPL1, ELL

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IF (IPS) WRITE (6,225)
IF (IPT) WRITE (6,226)
IF (IMT) WRITE (6,227)
IF (ICT) WRITE (6,228)
IF (ICT) WRITE (6,229)
IF (ICT) WRITE (6,230)
IF (ICT) WRITE (6,231)
IF (ICT) WRITE (6,232)
IF (ICT) WRITE (6,233)
IF (ICT) WRITE (6,234)
IF (ICT) WRITE (6,235)
IF (ICT) WRITE (6,236)
IF (ICT) WRITE (6,237)
IF (ICT) WRITE (6,238)
IF (ICT) WRITE (6,239)
IF (ICT) WRITE (6,240)
IF (ICT) WRITE (6,241)
IF (ICT) WRITE (6,242)
IF (ICT) WRITE (6,243)
IF (ICT) WRITE (6,244)
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IF (ICT) WRITE (6,252)
IF (ICT) WRITE (6,253)
IF (ICT) WRITE (6,254)
IF (ICT) WRITE (6,255)
IF (ICT) WRITE (6,256)
IF (ICT) WRITE (6,257)
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IF (ICT) WRITE (6,259)
IF (ICT) WRITE (6,260)
IF (ICT) WRITE (6,261)
IF (ICT) WRITE (6,262)
IF (ICT) WRITE (6,263)
IF (ICT) WRITE (6,264)
IF (ICT) WRITE (6,265)
IF (ICT) WRITE (6,266)
IF (ICT) WRITE (6,267)
IF (ICT) WRITE (6,268)
IF (ICT) WRITE (6,269)
IF (ICT) WRITE (6,270)
IF (ICT) WRITE (6,271)
IF (ICT) WRITE (6,272)
IF (ICT) WRITE (6,273)
IF (ICT) WRITE (6,274)
IF (ICT) WRITE (6,275)

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SAT02290
SAT02300
SAT02310
SAT02320
SAT02330
SAT02340
SAT02350
SAT02360
SAT02370
SAT02380
SAT02390
SAT02400
SAT02410
SAT02420
SAT02430
SAT02440
SAT02450
SAT02460
SAT02470
SAT02480
SAT02490
SAT02500
SAT02510
SAT02520
SAT02530
SAT02540
SAT02550
SAT02560
SAT02570
SAT02580
SAT02590
SAT02600
SAT02610
SAT02620
SAT02630
SAT02640
SAT02650
SAT02660
SAT02670
SAT02680
SAT02690
SAT02700
SAT02710
SAT02720
SAT02730
SAT02740
SAT02750

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1C5 FCRMAT (4E16.8)
1C6 FCRMAT (2L2,29I2)
1C7 FCRMAT (12)
C** *****
C** WRITE STATEMENT FCRMAT FOLLOW *****
C** *****
C** *****
2C0 FCRMAT (1,48X,18A4,15,---,///)
2C1 FCRMAT (1,38X,18A4,15,---,///)
2C2 FCRMAT (1,49X,18A4,15,---,///)
***** THE BCUNCARY CCNDI *****
2C3 FCRMAT (1,110,THE SHELL HAS AN INITIAL PCLE,/)
2C4 FCRMAT (1,110,AT THE INITIAL EDGE,//2X,-----CMEGA BS *****
1A9 FCRMAT (1,15X,-----LAMDA BAR-----,1 *****
22X,-----EL-----,/)
2C5 FCRMAT (1,4E10.3,NS (,4E10.3,) U (,E10 *****
2C6 FCRMAT (1,4E10.3,NST + (,4E10.3,) V = (,E10 *****
2C7 FCRMAT (1,4E10.3,CS (,4E10.3,) W (,E10 *****
2C8 FCRMAT (1,4E10.3,PHIS (,4E10.3,) MS (,E10 *****
209 FCRMAT (1,110,THE SHELL HAS A FINAL PCLE,/)
210 FCRMAT (1,110,AT THE FINAL EDGE,//2X,-----OMEGA BARS *****
1X,-----EL-----,/)
211 FCRMAT (1,4X,NUMBER OF STATIONS-----,13/5X,NS *****
212 FCRMAT (1,4X,NUMBER OF STATIONS-----,13/5X,IN *****
NUMBER OF MODES-----,F6.3/5X,MAXIMUM NUMBER OF *****
2ACTOR-----,13/5X,MAXIMUM NUMBER OF ITERATION *****
3-----,13/5X,MAXIMUM NUMBER OF ITERATION *****
4AXIMUM NUMBER OF LOAD FACTOR CHANGES-----,13/5X, *****
5ICN-----,F6.4/5X,MAXIMUM NUMBER OF ITERATION *****
213 FCRMAT (1,4X,CHARACTERISTIC SHELL DIMENSION-----,E12.4/5X *****
REFERENCE THICKNESS-----,E12.4/5X,REFERENCE *****
1ASTICITY-----,E12.4/5X,REFERENCE STRESS *****
3-----,E12.4/5X,PCISSON$ RATIO *****
4-----,E12.4/5X,PCISSON$ RATIO *****
214 FCRMAT (1,110,PLCTS HAVE BEEN REQUESTED FOR THE BELCW LISTED *****
FCMETRY, STIFFNESS OR LOADING QUANTITIES:/) *****
1FCRMAT (1,170,RADIUS,/) *****
215 FCRMAT (1,170,GAMMA,/) *****
216 FCRMAT (1,170,CMEGA-S,/) *****
217 FCRMAT (1,170,CMEGA-THETA,/) *****
218 FCRMAT (1,170,DECMEGA-S,/) *****
219 FCRMAT (1,170,B-STIFFNESS,/) *****
220 FCRMAT (1,170,C-STIFFNESS,/) *****
221 FCRMAT (1,170,B-PRIME,/) *****
222 FCRMAT (1,170,B-PRIME,/) *****
SAT02770
SAT02780
SAT02790
SAT02800
SAT02810
SAT02820
SAT02830
SAT02840
SAT02850
SAT0286C
SAT02870
SAT02880
SAT02890
SAT02900
SAT02910
SAT02920
SAT02930
SAT02940
SAT02950
SAT02960
SAT02970
SAT02980
SAT02990
SAT03000
SAT03010
SAT03020
SAT03030
SAT03040
SAT03050
SAT0306C
SAT03070
SAT03080
SAT03090
SAT03100
SAT03110
SAT03120
SAT03130
SAT03140
SAT03150
SAT03160
SAT03170
SAT03180
SAT03190
SAT03200
SAT03210
SAT03220
SAT03230
SAT03240

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C      NESSES, LOADING (PHYSICAL AND/OR THERMAL), AND INITIAL CCNTIDICNS. *SAT03730
C      IT CCNTRCLS PROBLEM SCLUTICN PRCCEDURE. *SAT03740
C      ***** *SAT03750
C      IMPLICIT LCGICAL*1 ($) *SAT03760
C      REAL*4 NU, LAM, LAM2, JAY, MT, LSD18, LSCIN, MASS *SAT03770
C      DIMENSION P(4,4,1), DEE(4,4,1), X(4,1), Z(4,1), *SAT03780
C      IZC(4,1), Z2(4,1), Z3(4,1), ZDOT(4,1), JS(99,1), IC(55,1), *SAT03790
C      ZJC(55,1), PHIXB(1), PHITB(1) *SAT03800
C      CCMPON /IBL1/ MNMAX *SAT03810
C      CCMPON /IBL2/ N(99) *SAT03820
C      CCMPON /IBL3/ MO, MI, M2, M3 *SAT03830
C      CCMPON /IBL4/ KMAX, KL, IBCFNL *SAT03840
C      CCMPON /IBL5/ KLL *SAT03850
C      CCMPON /IBL6/ KLL *SAT03860
C      CCMPON /IBL7/ MNMAX, MAXD(99), MAXS(99), MAXSY(99), IJS(99) *SAT03870
C      CCMPON /IBL8/ LSTEP, ITR *SAT03880
C      CCMPON /IBL9/ MAXM *SAT03890
C      CCMPON /IBL10/ IFREG, NTHMAX *SAT03900
C      CCMPON /IBL11/ ICORFL, IPASS *SAT03910
C      CCMPON /IBL12/ KMAX1, KMAX2, NCCNV *SAT03920
C      CCMPON /IBL13/ ITRMAX, LSMAX *SAT03930
C      CCMPON /BL1/ A(4,4), BEE(4,4), C(4,4) *SAT03940
C      CCMPON /BL3/ PR(99), PX(99), ZF2M(4,4,99), *SAT03950
C      CCMPON /BL4/ ZF1M(4,4,99), ZF4M(4,4,99) *SAT03960
C      CCMPON /BL5/ ZF3M(4,4,99), DT(99), DMT(95) *SAT03990
C      CCMPON /BL6/ MT, APPEARS AS 'EMT' IN SUBRCUTINES INLPOL & FNLPOL *SAT04000
C      CCMPON /BL7/ SOE, CSE, ALOAD *SAT04010
C      CCMPON /BL8/ DI, 500 *SAT04020
C      CCMPON /BL9/ R(500), GAM(500), DMT(500) *SAT04030
C      CCMPON /BL10/ FFS(4,99), ELIS(4), GEES(4,99) *SAT04050
C      CCMPON /BL11/ PHIX(99), PHIT(99), PHI(99) *SAT04060
C      CCMPON /BL12/ DMXI(500), PHEE, T0, T2 *SAT04070
C      CCMPON /BL13/ TDLI, TDEL *SAT04080
C      CCMPON /BL14/ OMEGI(4,4), CAPL1(4,4), OMEGL(4,4), CAPLL(4,4), *SAT04090
C      CCMPON /BL15/ UNIT(4,4) *SAT04100
C      CCMPON /BL16/ LAM2, LSD18, LSCIN *SAT04110
C      CCMPON /BL17/ NU, UI(99), V1(99), W1(99), V2(59), U2(59), h2(99), U3(99), *SAT04120
C      CCMPON /BL18/ V3(99), W3(99) *SAT04130
C      CCMPON /BL19/ EPS *SAT04140
C      CCMPON /BL20/ DEL *SAT04150
C      CCMPON /BL21/ ELL(4) *SAT04160
C      CCMPON /BL22/ TH(36) *SAT04170
C      CCMPON /BL23/ DEOMX(500) *SAT04180
C      CCMPON /BL24/ JAY(4,4), H(4,4) *SAT04190
C      CCMPON /BL25/ DL(4,4,99), DG(4,4,55), DF(4,4,55) *SAT04200
C      CCMPON /BL25/ E(4,4), F(4,4), G(4,4)

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CCMCMC /BL27/ BX3(99), BT3(99), BX13(99), BE3(55)
CCMCMC /BL28/ EXX3(99), ET3(99), ETX3(99), EX3(99), ET3(99)
CCMCMC /BL29/ BX11(99), BT11(99), BTX11(99), BX11(99), BT11(99)
1 CCMCMC /BL30/ EXX1(99), ET11(99), ETX1(99), EX1(99), ET1(99), EXX2(99), ET2(99)
1 CCMCMC /BL31/ DELSQ, EX11(99)
CCMCMC /BL32/ TKN, ELAST, CHAR, SIGC
CCMCMC /BL100/ TEEO, $DYNMC
CCMCMC /BL101/ DELSCAD
CCMCMC /BL102/ DELCAD
CCMCMC /BL103/ MASS(500)
CCMCMC /BL110/ TX(99), TTH(99), TTI(99), MX(99), MTH(99), MXT(99),
1 CCMCMC /BL111/ ABZ, ABZ0, ABZN, ABZ3, CD2
CCMCMC /BLPHS/ PHX(99), PHT(99)
CCMCMC /BLPLOT/ IRRADI, IGAMMA, ICMEGS, IOMEGT, IDECMS, IPSTIF, IDSTIF,
1 IBBSTF, IDSTF, IPRIPS, IPT, IT, IMT, ICI, ICM, INS,
2 INTH, INSTH, IQS, IMS, IMTH, IMSTH, IU, IV, IW, IPHS,
3 IPHI, IPHI, $PLOTS, $MODAL
1 XRACTI(200), YGAMMA(200), YCMEGS(200), YCMEGT(200),
2 YDECMS(200), YBSTIF(200), YPSTIF(200), YPSTIF(200), YBSTIF(200),
3 YDDSTF(200), YPR(200), YP(200), YP(200), YP(200), YP(200),
4 YMT(200), YDT(200), YDMT(200), YNS(200), YNTF(200),
5 YNSTH(200), YQS(200), YMS(200), YMTH(200), YNSTH(200),
6 YU(200), YV(200), YW(200), YPHI(200), YPFT(200),
CCMCMC /BLDATA/ YPHI(200), XSTATN(200)
DIMENSICN SIGT(2), TITLE, NG, IMODE, NDCIMEN, IPRINT, LCHMAX, IC
C *****
WRITE (6,8888)
DELSD=DELCAD*DELOAD
KLL=KMAX-1
KMAX1=KMAX+1
KMAX2=KMAX+2
AK=KL
SIGT(1)=SIGO*TKN
SIGT(2)=SIGO/ELAST
SIGC(1)=SIGO*CHAR/ELAST
SIGC(2)=SIGO*TKN*3/CHAR
IF (IBCINL.LT.0) GC TO 14
DC 58 I=1,4
CC 58 J=1,4
KKLM=J/4+1
CMEGT(I,J)=CMEGT(I,J)*SIGT(KKLM)
CAPL(I,J)=CAPL(I,J)*SIGC(KKLM)
14 IF(IBCINF.LT.0) GC TO 17
58
14

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SAT04680  
 SAT04690  
 SAT04700  
 SAT04710  
 SAT04720  
 SAT04730  
 SAT04740  
 SAT04750  
 SAT04760  
 SAT04770  
 SAT04780  
 SAT04790  
 SAT04800  
 SAT04810  
 SAT04820  
 SAT04830  
 SAT04840

SAT04850  
 SAT04860  
 SAT04870  
 SAT04880  
 SAT04890  
 SAT04900  
 SAT04910  
 SAT04920  
 SAT04930  
 SAT04940  
 SAT04950  
 SAT04960  
 SAT04970  
 SAT04980  
 SAT04990  
 SAT05000  
 SAT05010  
 SAT05020  
 SAT05030  
 SAT05040  
 SAT05050  
 SAT05060  
 SAT05070  
 SAT05080  
 SAT05090  
 SAT05100  
 SAT05110  
 SAT05120  
 SAT05130

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CC 99 I=1,4
CC 99 J=1,4
KKLM=J/4+1
CMEGL(I,J)=CMEGL(I,J)*SIGT(KKLM)
CAPLL(I,J)=CAPLL(I,J)*SIGC(KKLM)
LAN=TKN/CHAR
SCE=SIGC/ELAST
CFI=1.0-NU
SI=1.0+NU
LAN2=LAM*#2
IF (NDIMEN.LT.1) GC TO 228
ELAST=1.0
TMA=1.0
CFAR=1.0
CC 230 N=1,MAXM
PFX(M)=C.0
PFT(M)=C.0
PX(M)=0.0
PT(M)=0.0
PR(M)=0.0
TT(M)=0.0
NT(M)=0.0
LT(M)=0.0
LMT(M)=C.0
MAXC(M)=0
MAXS(M)=0
CALL GECM
ICFCK1=IABS(IGAMMA)+IABS(IOMECS)+IABS(IOMEGT)+IABS(ICEOMS)
+IABS(IRADII)
1 ICFCK2=IABS(IBSTIF)+IABS(IDSTIF)+IABS(IBBSTF)+IABS(ICDSTF)
IF (.NOT. $PLOTS) GC TO 1001
CC 2 K=1,KMAX
XSTAIN(K)=FLOAT(K)
2 IF (ICFCK1.EQ.0) GO TO 1001
CC 1 K=1,KMAX
XRADII(K)=R(K)*CHAR
YGAMMA(K)=GAM(K)/CHAR
YOMECS(K)=CMT(K)/CHAR
YOMEGT(K)=CMT(K)/CHAR
YECMS(K)=DEOMX(K)/(CHAR*CHAR)
1 CCNTINUE
1001 CC 86 K=1,KMAX
66 MASS(K)=0.

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SAT05140  
 SAT05150  
 SAT05160  
 SAT05170  
 SAT05180  
 SAT05190  
 SAT05200  
 SAT05210  
 SAT05220  
 SAT05230  
 SAT05240  
 SAT05250  
 SAT05260  
 SAT05280  
 SAT05290  
 SAT05300  
 SAT05310  
 SAT05320  
 SAT05330  
 SAT05340  
 SAT05350  
 SAT05360  
 SAT05370  
 SAT05380  
 SAT05390  
 SAT05400  
 SAT05410  
 SAT05420  
 SAT05430  
 SAT05440  
 SAT05450  
 SAT05460  
 SAT05470  
 SAT05480  
 SAT05490  
 SAT05500  
 SAT05510  
 SAT05520  
 SAT05530  
 SAT05540  
 SAT05550  
 SAT05560  
 SAT05570  
 SAT05580  
 SAT05590  
 SAT05600  
 SAT05610

WRITE(6,802)  
 DC 890 K=1,KMAX  
 CALL PLCCAD(1,Z)  
 CALL TLCCAD(1,Z)  
 DC 889 M=1,MNMAX  
 WRITE(6,113) N(M)  
 WRITE(6,114)  
 ICHK3= IABS(IPR)+IABS(IPT)+IABS(ITT)+IABS(IMT)  
 +IABS(IDTT)+IABS(IDMT)  
 DC 890 K=1,KMAX  
 CALL PLCCAD(K,Z)  
 CALL TLCCAD(K,Z)  
 PFM=PR(M)/ABN  
 PTM=PT(M)/ABN  
 FXM=PX(M)/ABN  
 TTM=TT(M)\*ZN  
 EMTM=MT(M)/CHAR\*ZN  
 LTM=DT(M)/CHAR\*ZN  
 DMTM=DMT(M)\*ZN\*TKN\*TKN/(CHAR\*CHAR)  
 WRITE(6,115) K,PRM,PXM,PTM,TTM,EMTM,DTM,DMTM

978  
 805

838

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IF (.NCT.$PLCTS.GR.(ICHCK3.EG.0)) GG TO 890
YPR(K)=PRM
YFS(K)=PXM
YPT(K)=PTM
YTT(K)=TTM
YMT(K)=EMTM
YCTT(K)=DTM
YCMT(K)=DMTM
CCN INUE
85C IF (M.EG.1) ICHCK3=ICHCK1+ICHCK2+ICHCK3
IF ($PLCTS.AND.(ICHCK3.GT.0)) CALL PLOT1(M)
855 CCN INUE
CCLSQ=DEL*2
TCLLI=.5/DEL
TCEL=2.C*DEL
MNNINIT=1.NMAX
MNCXG=1.NMAX
CC 20 I=1,4
CC 20 J=1,4
LNIT(I,J)=0.0
IF(I.EQ.J) UNIT(I,J)=1.0
2C DC 22 K=1,NMAX
DC 22 I=1,4
ZCCT(I,K)=0.0
ZC(I,K)=0.0
Z2(I,K)=0.0
Z3(I,K)=0.0
Z(I,K)=0.0
ALCAD=DELCAD
CALL IMPERF (PHIXB,PHITB)
LSTEP=1
LCHANG=0
ITR=1
ICRFL=0
IF(MNMAX.EG.MAXM) ICORFL=1
IPASS=0
CALL XANDZ (P,DEE,CST,X,Z,ZC,Z2,Z3,ZDOT,IS,JS,ID,JD,PTIXB,PHITB)
4CC IF(ITRMAX.EQ.1) GC TO 50
MNCXG=MNMAX
IF(IPASS.LT.2) CALL MCODES (IS,JS,IC,JD,P,X,ZC,Z2,Z3,DEE,CST)
IF(INCONV.EQ.1).AND.(ITR.GT.1) GC TO 50
IF(ITR.LT.ITRMAX) GC TO 23
IF(LCHANG.LT.LCHMAX) GO TO 30
WRITE(6,220) NO
GC TO 500
5C FL=LSTEP

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SAI05620
SAI05630
SAI05640
SAI05650
SAI05660
SAI05670
SAI05680
SAI05690
SAI05700
SAI05710
SAI05720
SAI05730
SAI05740
SAI05750
SAI05760
SAI05770
SAI05780
SAI05790
SAI05800
SAI05810
SAI05820
SAI05830
SAI05840
SAI05850
SAI05860
SAI05870
SAI05880
SAI05890
SAI05900
SAI05910
SAI05920
SAI05930
SAI05940
SAI05950
SAI05960
SAI05970
SAI05980
SAI05990
SAI06000
SAI06010
SAI06020
SAI06040
SAI06050
SAI06060
SAI06070
SAI06080
SAI06090

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```

FI=IPRINT
LI=LSTEP/IFRINT
FLI=LI
IF(FT.EC.O.) CALL OUTPUT(IMCDE,P,LEE,DST,X,Z,ZC,Z2,Z3,ZCCT,IS,JS,
1 I{LSTEP.EC.1}) ITR=
IF(LSTEP.EC.1) ITRPK=1
IF(LSTEP.GT.ITRPR) ITRPR=ITR
IF(LSTEP.GE.LSMAX) GO TC 360
CC 61 MN=1,MNMAXO
CC 61 K=1,KMAX2
IK=K+(MN-1)*KMAX2
CC 61 I=1,4
ZN=2.0*Z(I,IK)-ZC(I,IK)
ZC(I,IK)=Z(I,IK)
Z(I,IK)=ZNE.LSMAX) GO TC 360
1 ALCAC=ALOAD+DELOAD
LSTEP=LSTEP+1
ITR=1
GC TO 400
WRITE(6,221) NO
GC TO 500
ITR=ITR+1
GC TO 400
IF(LSTEP-1) 310,310,320
GC TO 500
WRITE(6,222)
LCHANG=LCHANG+1
LSTEP=LSTEP-1
ALCAC=ALOAD-DELOAD
DELCCAD=DELCCAD/5.0
CC 32 MN=1,MNMAXC
CC 32 K=1,KMAX2
IK=K+(MN-1)*KMAX2
CC 32 I=1,4
Z(I,IK)=ZC(I,IK)
GC TO 62
C*****
71 FCFRMT(20X,13,4X,4E20.6)
112 FCFRMT(///,17X,12H STATION 20H B STIFFNESS 20H C ST
113 FCFRMT(///,25X,44HPRESSURE AND TEMPERATURE CCEFFICIENTS FOR N=13,8H D PRIME //)
114 FCFRMT(5X,7HSTATION,3X,15H PR 15H MT 15H PX 15H DTT 15H
1 FCFRMT(5X,15H

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SAT06100
SAT06110
SAT06120
SAT06130
SAT06140
SAT06150
SAT06160
SAT06170
SAT06180
SAT06190
SAT06200
SAT06210
SAT06220
SAT06230
SAT06240
SAT06250
SAT06260
SAT06270
SAT06280
SAT06290
SAT06300
SAT06310
SAT06320
SAT06330
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SAT06350
SAT06360
SAT06370
SAT06380
SAT06390
SAT06400
SAT06410
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SAT06490
SAT06500
SAT06510
SAT06520
SAT06530
SAT06540
SAT06550
SAT06560
SAT06570

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251 DMT
FCRMA(13,7X,7E15.4)
115 FCRMAT(IHL,80H) THE MAXIMUM NUMBER CF LOAC CFANGES HAVE BES
22C LEN MADE. END PROBLEM NUMBER I4)
221 FCRMAT(IHL,79H) THE MAXIMUM NUMBER CF LOAC STEPS FAVE BEEN
222 TAKEN. END PROBLEM NUMBER I4)
125 FCRMAT(IHL,119H) THE SOLUTION DID NOT CCNVERGE WITHIN THE M
126 MAXIMUM NUMBER OF ITERATIONS. THE LOAD FACTOR HAS BEEN CIVIDEC BY
252 FCRMAT(IHL,69H) THE SOLUTION DID NOT CCNVERGE FOR THE FIRS
127 ITY LOAD INCREMENT. /11X,7IHLOOK FOR AN ERRCR IN THE INPUT DATA, OR T
227 TRY A SMALLER VALUE FOR DELCAD.)
8C2 FCRMAT(IHL,17X,15H STATION 16H RACILS 16H GAMMA
16F OMEGA S DECMEGA S //)
8C3 FCRMAT(20X,13,9X,5E16.4)
888 FCRMAT(0,120, EXECUTING IN SUBROUTINE "STATIC")
5CC RETURN
END
SUBROUTINE DYNAMC (P,DEE,DST,X,Z,ZC,Z2,Z3,ZCCT,IS,JS,ID,JD,PT,IXB,
IPFITB)
C *****
C THIS SUBROUTINE IS ONE OF THE MAJOR CONTRCLLING SLBRCLTINES FCR
C ALL CYRAMIC ANALYSIS PROBLEMS. IT OPERATES IN A FASHION SIMILAR
C TO SUBROUTINE STATIC.
C *****
C IMPLICIT LCGICAL*1 ($)
REAL*4 NU,LAM,LAM2,JAY,MT,LSD18,LSD1N,MASS
DIMENSION P(4,4,1),CEE(4,4,1),DST(4,4,1),X(4,1),Z(4,1)
1ZC(4,1),Z2(4,1),Z3(4,1),ZCCT(4,1),IS(99,1),JS(99,1),ID(99,1),
2JJC(99,1),PHIXB(1),PHITB(1)
CCMMCN /IBL1/ MNMAX
CCMMCN /IBL2/ N(99)
CCMMCN /IBL3/ MNINIT AS 'NN' IN SUBROUTINES PLOAD & EFG
CCMMCN /IBL4/ MO,M1,M2,M3
CCMMCN /IBL5/ KMAX,KL
CCMMCN /IBL6/ IBCINL,IBCFNL
CCMMCN /IBL7/ KLL
CCMMCN /IBL8/ MNMAXO,MAXD(99),MAXS(99),MAXSY(99),IJS(99)
CCMMCN /IBL9/ LSTEP,I TR
CCMMCN /IBL10/ MAXM
CCMMCN /IBL11/ IFRFQ,NTHMAX
CCMMCN /IBL12/ ICCRFL,IPASS
CCMMCN /IBL13/ KMAX1,KMAX2,NCONV
CCMMCN /IBL14/ ITRMAX,LSMAX
CCMMCN /IBL15/ A(4,4),BEE(4,4),C(4,4)
CCMMCN /IBL16/ PR(99),PX(99),PT(99)
CCMMCN /IBL17/ ZFIM(4,4,99),ZF2M(4,4,99)
CCMMCN /IBL18/ ZF3M(4,4,99),ZF4M(4,4,99)
CCMMCN /IBL19/
CCMMCN /IBL20/

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SAT06580
SAT06590
SAT06600
SAT06610
SAT06620
SAT06630
SAT06640
SAT06650
SAT06660
SAT06670
SAT06680
SAT06690
SAT06700
SAT06710
SAT06720
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SAT06910
SAT06920
SAT06930
SAT06940
SAT06950
SAT06960
SAT06970
SAT06980
SAT06990
SAT07000
SAT07010
SAT07020
SAT07030

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CCMCMN	/BL5/	TT(99), MT(99), DT(99), DMT(99) ; MT, APPEARS AS 'EMT' IN SUBRCUTINES INLPCL & FALPOL	SAT07060
CCMCMN	/BL6/	SOE, QSE, ALOAD	SAT07070
CCMCMN	/BL7/	DI, SI	SAT07080
CCMCMN	/BL8/	R(500), GAM(500), GMT(500)	SAT07090
CCMCMN	/BL9/	FFS(4,99), ELIS(4), GEES(4,99)	SAT07100
CCMCMN	/BL10/	PHIX(99), PHIT(99), PFI(99)	SAT07120
CCMCMN	/BL11/	OMXI(500), PHEE, TO, T2	SAT07130
CCMCMN	/BL12/	TDLI, TDEL	SAT07140
CCMCMN	/BL13/	OMEGI(4,4), CAPLI(4,4), OMEGL(4,4), CAPLL(4,4),	SAT07150
1	CCMCMN	UNIT(4,4)	SAT07160
1	CCMCMN	LAM2, LSD18, LSCIN	SAT07170
1	CCMCMN	NU, UI(99), VI(99), W1(99), V2(99), L2(99), W2(99), U3(99),	SAT07180
1	CCMCMN	V3(99), W3(99)	SAT07190
CCMCMN	/BL16/	EPS	SAT07200
CCMCMN	/BL17/	DEL	SAT07210
CCMCMN	/BL18/	ELI(4), ELL(4)	SAT07220
CCMCMN	/BL19/	TH(36), 500	SAT07230
CCMCMN	/BL20/	DEOMX(4,4), F(4,4)	SAT07240
CCMCMN	/BL21/	JAY(4,4,4,4), DG(4,4,4,4), DF(4,4,4,4)	SAT07250
CCMCMN	/BL22/	DL(4,4,4,4), G(4,4,4,4)	SAT07270
CCMCMN	/BL23/	E(4,4,4,4), F(4,4,4,4), G(4,4,4,4)	SAT07280
CCMCMN	/BL24/	BX3(99), BX2(99), BX1(99), BE2(99)	SAT07290
CCMCMN	/BL25/	EXX3(99), EIT3(99), ETX3(99), EX3(99), ET3(99)	SAT07300
CCMCMN	/BL26/	BX1(99), BTL(99), BXT1(99), BE1(99), BX2(99), B12(99),	SAT07310
CCMCMN	/BL27/	BX2(99), BE2(99)	SAT07320
1	CCMCMN	EXX1(99), EIT1(99), ETX1(99), EX1(99), ET1(99), EXX2(99),	SAT07330
1	CCMCMN	ETX2(99), ETX2(99), EXT2(99), EX2(99), ET2(99)	SAT07340
CCMCMN	/BL31/	DELSQ, EXT1(99)	SAT07350
CCMCMN	/BL32/	TKN, ELAST, CHAR, SIGC	SAT07360
CCMCMN	/BL100/	TTEEG, \$DYNMC	SAT07370
CCMCMN	/BL101/	DELOAD	SAT07380
CCMCMN	/BL102/	DELOAD	SAT07390
CCMCMN	/BL103/	MASS(500)	SAT07400
CCMCMN	/BL110/	TX(99), TTH(99), TXT(99), MX(99), MTH(99), NTH(99), MXT(99),	SAT07410
1	CCMCMN	QS(99)	SAT07420
1	CCMCMN	ABZ, ABZC, ABZN, ABZ3, DC2	SAT07430
CCMCMN	/BLPFS/	PHX(99), PHT(99)	SAT07440
CCMCMN	/BLFLGT/	IRADII, IGAMMA, ICMEGS, IOMEGI, ICEOMS, IPSTIF, IDSTIF,	SAT07450
1	CCMCMN	IBBSTF, IDBSTF, IPRS, IPT, IIT, IMT, ICIT, ICMT, IAS,	SAT07460
2	CCMCMN	INTH, INSTH, IQS, IMS, IMTH, INSH, IU, IV, IW, IFHIS,	SAT07470
3	CCMCMN	IPHIT, IPHI, \$PLOTS, \$MODAL, YCMEGS(200), YCMEGT(200),	SAT07480
1	CCMCMN	XRADII(200), YGAMMA(200), YDSTIF(200), YDSTIF(200),	SAT07490
2	CCMCMN	YDECMS(200), YBSTIF(200), YPS(200), YPT(200), YTT(200),	SAT07500
3	CCMCMN	YDDSTF(200), YPR(200), YMS(200), YMT(200), YNTH(200),	SAT07510
4	CCMCMN	YMT(200), YD(200), YQS(200), YMS(200), YMTH(200), YMSTH(200),	SAT07520
5	CCMCMN	YNSTH(200), YV(200), YW(200), YPHIS(200), YPHIT(200),	SAT07530
5	CCMCMN	YL(200), YV(200), YW(200), YPHIS(200), YPHIT(200),	SAT07540

C

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6 CCMGON /BLDATA/ XSTATN(200)
  DIMENSICN SIGT(2), TITLE(18)
  DIMENSICN VBAR(99), AVB(99)
  WRITE(6,8888)
  DELSD=DELCAD*DELCAC
  KLL=KMAX-1
  KMAX1=KMAX+1
  KMAX2=KMAX+2
  AK=KL
  SIGT(1)=SIGC*TKNST
  SIGT(2)=SIGO/ELAST
  SIGC(1)=SIGO*CHAR/ELAST
  IF(IBCINL.LT.0) GO TO 14
  DCC 58 I=1,4
  DCC 58 J=1,4
  KKLMM=J/4+1
  OMEGL(I,J)=OMEG1(I,J)*SIGT(KKLM)
  CAPLI(I,J)=CAPLI(I,J)*SIGC(KKLM)
  IF(IBCFL.LT.0) GC TO 17
  DCC 59 I=1,4
  DCC 59 J=1,4
  KKLMM=J/4+1
  OMEGL(I,J)=OMEG1(I,J)*SIGT(KKLM)
  CAPLL(I,J)=CAPLI(I,J)*SIGC(KKLM)
  LAM=TKN/CHAR
  SCCE=5*SCF
  DDI=1.0+NU
  LAM2=LAMEN*2
  IF(NDIMEN.LT.1) GC TO 228
  ELAST=1.0
  TKN=1.0
  CC 230 N=1,MAXM
  PFX(M)=C.0
  PFT(M)=0.0
  PX(M)=0.0
  PT(M)=0.0
  PR(M)=0.0
  TT(M)=0.0
  MT(M)=0.0

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SAI07530
SAI07540
SAI07550
SAI07560
SAI07570
SAI07580
SAI07590
SAI07600
SAI07610
SAI07620
SAI07630
SAI07640
SAI07650
SAI07660
SAI07670
SAI07680
SAI07690
SAI07700
SAI07710
SAI07720
SAI07730
SAI07740
SAI07750
SAI07760
SAI07770
SAI07780
SAI07790
SAI07800
SAI07810
SAI07820
SAI07830
SAI07840
SAI07850
SAI07860
SAI07870
SAI07880
SAI07890
SAI07900
SAI07910
SAI07920
SAI07930
SAI07940
SAI07950
SAI07960
SAI07970
SAI07980

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SAT07990  
 SAT08000  
 SAT08010  
 SAT08020  
 SAT08030  
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 SAT08370  
 SAT08380  
 SAT08390  
 SAT08400  
 SAT08410  
 SAT08420  
 SAT08430  
 SAT08440  
 SAT08450  
 SAT08460

```

LT(M)=0.0
DMT(M)=C.0
MAXL(M)=0
MAXS(M)=0
MAXSY(M)=0
CALL GECM
ICFCK1=IABS(IGAMMA)+IABS(IOMEGS)+IABS(IOMEGT)+IABS(ICEOMS)
1 ICFCK2=IABS(IRADII)+IABS(IBSTIF)+IABS(IDSTIF)+IABS(IBBSTF)+IABS(ICDSTF)
IF (.NOT.$PLOTS) GO TO 1001
CC 2 K=1,KMAX
XSTAIN(K)=FLQAT(K) GC TO 1001
2 IF (ICHECK1.EQ.0) GC TO 1001
CC 1 K=1,KMAX
XRADII(K)=R(K)*CHAR
YGAMMA(K)=GAM(K)/CHAR
YCMEGS(K)=OMXI(K)/CHAR
YCECMS(K)=DEOMX(K)/(CHAR*CHAR)
CCCONTINUE
1 CCCONTINUE(6,810)
8C4 WTEC=TEEC
IF(NDIMEN.EQ.1) TEEC=1.0
CC 579 K=1,KMAX
RKK=R(K)*CHAR
CMXIK=CMXI(K)/CHAR
GAMK=GAM(K)/CHAR
DECMXK=DEOMX(K)/(CHAR*CHAR)
975 AMSS=MASS(K)*TEED**2*ELAST*TKN/CHAR**2
8C5 WRITE(6,813) K,RKK,GAMK,CMXIK,CMTK,DEOMXK,AMSS
M1=0
M2=0
M3=0
AEN=CHAR/SIGO/TKN
ZK=SIGC*TKN
MCC WRITE(6,112)
CC 888 K=1,KMAX
CALL BDE(K,B,DB,D,CC)
ZST=ELAST*TKN**3
B=B*BST
C=C*ZST
LB=CB/CFAR*BST
CC=DD/CFAR*ZST
WRITE (6,71) K,B,C,CB,DD

```

IF (.NOT. \$PLOTS.DR.(ICCHK2.EQ.0)) GC TO 888

SAT08470  
SAT08480  
SAT08490  
SAT08500  
SAT08510  
SAT08520  
SAT08530  
SAT08540  
SAT08550  
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SAT08570  
SAT08580  
SAT08590  
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SAT08690  
SAT08700  
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SAT08880  
SAT08890  
SAT08900  
SAT08910  
SAT08920  
SAT08930

```

888 CALL FLCCAD(1,Z)
      CALL TLCCAD(1,Z)
      DELSQ=DEL*2
      TCELL=.5/DEL
      TCELL=2.*C*DEL
      MNMAXC=MNMAX
      DC 20 I=1,4
      DC 20 J=1,4
      UNIT(I,J)=0.0
      IF(I.EQ.XM*KMAX2) UNIT(I,J)=1.0
      CC 22 K=1,MNMAX
      CC 22 I=1,4
      ZCCT(I,K)=0.0
      ZC(I,K)=0.0
      Z3(I,K)=0.0
      Z(I,K)=0.0
      Z(I,K)=0.0
      IF(IC.EC.0) GO TO 834
      CALL INITL(Z,Z0,Z2,Z3,ZCOT)
      ACC=CHAR*SIGC/ELAST
      ACN=SIGC*TKN**3/CHAR
      DC 830 M=1,MNMAX
      WRITE(6,126) N(M)
      WRITE(6,127)
      DO 831 K=2,KMAX1
      MK=K+MM
      TL=ACC*Z0(1,MK)
      TV=ACC*Z0(2,MK)
      TW=ACC*Z0(3,MK)
      TP=ACC*ZC(4,MK)
      KK=K-1
      WRITE(6,71) KK,TU,TV,TW,TM
      WRITE(6,125)
      CC 830 K=2,KMAX1
      ACC=CFAR*SIGC/(ELAST*TEEO)
      AMC=SIGC*TKN**3/(CHAR*TEEO)
      MK=K+MM
      TL=ACC*ZDOT(1,MK)
      TV=ACC*ZDOT(2,MK)

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SAT089550  
 SAT089600  
 SAT089670  
 SAT089980  
 SAT089990  
 SAT090000  
 SAT090100  
 SAT090200  
 SAT090300  
 SAT090400  
 SAT090500  
 SAT090600  
 SAT090700  
 SAT090800  
 SAT090900  
 SAT091000  
 SAT091100  
 SAT091200  
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 SAT093000  
 SAT093100  
 SAT093200  
 SAT093300  
 SAT093400  
 SAT093500  
 SAT093600  
 SAT093700  
 SAT093800  
 SAT093900  
 SAT094000  
 SAT094100  
 SAT094200  
 SAT094300  
 SAT094400

```

TM=ACD*ZDOT(3,MK)
TM=AMD*ZDOT(4,MK)
KK=K-1
WRITE(6,71) KK,TU,TV,TH,TM
CC 830 I=1,4
Z2(I,MK)=ZO(I,MK)+ZCCT(I,MK)*DELCAC
Z3(I,MK)=ZO(I,MK)-ZDOT(I,MK)*DELCAC
Z3(I,MK)=ZC(I,MK)-2.*ZDOT(I,MK)*CELOAD
83C CCNTINUE
834 ALCAD=1.0
CALL IMPERF (PHIXB,PHITB)
CALL FMATRIX (P,X,ZC,Z2,Z3,DEE,DST)
LSTEP=1
LCFANG=C
ITR=1
ICORFL=0
IF(MNMAX.EQ.MAXM) ICORFL=1
IPASS=0
ITEST=0
4CC CALL XMAXZ (P,DEE,DST,X,Z,ZC,Z2,Z3,ZDOT,IS,JS,IC,JD,PTIXB,PHITB)
IF(ITRMAX.EQ.1) GO TO 5C
MNXC=MNX
IF(IPASS.LT.2) CALL MCODES (IS,JS,IC,JD,P,X,ZC,Z2,Z3,CEE,CST)
IF(INCNV.EQ.1) GO TO 50
IF(ITR.LT.ITRMAX) GC TO 23
5C FL=LSTEP
FI=IPRINT
LI=LSTEP/IPRINT
FLI=LI
FT=FLI-FL/FI
IF(FT.EQ.0.) CALL OUTPUT(IMCDE,P,CEE,DST,X,Z,ZC,Z2,Z3,ZCOT,IS,JS,
1 I L,JD,PTIXB,PHITB)
IF(LSTEP.GE.LSMAX) GC TC 360
LC 65 MN=1,MNX2
DC 65 K=1,KMAX2
IK=K+(MN-1)*KMAX2
DC 65 I=1,4
ZK=3.0*(Z(I,I,IK)-ZC(I,IK))
Z2(I,IK)=Z2(I,IK)
ZC(I,IK)=ZC(I,IK)
ZC(I,IK)=ZN
65 Z(I,IK)=ZN
ALCAD=1.0
LSTEP=LSTEP+1
ITR=1
GC TO 400
23 ITR=ITR+1

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```

36C GC TO 400
WRITE(6,271) (AVB(M),M=1,MAXM)
WRITE(6,188) ITRPR
WRITE(6,189)
GC TO 500
365 IF(LSTEP.EC.1) GO TO 367
WRITE(6,266) ITRMAX,LSTEP,NC
WRITE(6,188) (AVB(M),M=1,MAXM)
GC TO 500
367 WRITE(6,273)
GC TO 500
C*****
71 FCFRMT(20X,13,4X,4E20,6)
72 FCFRMT(//17X,12H STATION 20F 20H B STIFFNESS 20F //) C ST
126 IFFNNESS //5X,29H THE INITIAL CONDITIONS FOR N=I3,8H FOLLOW//)
127 FCFRMT(19X,7H STATION,3X,20H U M S DOT V DOT
125 FCFRMT(//19X,7H STATION,3X,20H W DOT
188 FCFRMT(// THE MAXIMUM VBAR FOR EACH MCDE IS, /10E11.4)
189 FCFRMT(// THE MAXIMUM NUMBER OF ITERATIONS TAKEN IS, I3)
266 FCFRMT(1H,1,35H THE SOLUTION DID NOT CONVERGE IN I3,24H ITERATIONS
271 FCFRMT(1H,1,75H AT TIME STEPS I5,21H. END PROBLEM NUMBER I4,1F.)
273 FCFRMT(1H,1,69H TAKEN. I1,69H THE MAXIMUM NUMBER OF ITERATIONS
17X,7H LOCK FOR AN ERROR IN THE INPUT DATA, CR T
273 ITR TIME INCREMENT, /11X,7H LOCK FOR AN ERROR IN THE INPUT DATA, CR T
17X,7H LOCK FOR AN ERROR IN THE INPUT DATA, CR T
81C FCFRMT(1H,1,5X,15H STATION 16H RADIUS 16H GAMMA
16H MASS 16H DECMEGA S 16H
813 FCFRMT(8X,13,9X,6E16,4)
888 FCFRMT(//)
5CC RETURN
ENCL
SUBROUTINE PLOTIT(X,Y,NN,MODCUR)
THIS SUBROUTINE AND THE THREE THAT FOLLOW IT COMPRISE THE SELF-
CONTAINED PLOTTING CAPABILITY OF PROGRAM SATANS. THEY RECEIVE
DATA TO BE PLOTTED, ROUND IT, SCALE IT, AND DRAW IS ON THE HIGH-
SPEED LINE PRINTER.
*****
DIMENSION X(1),Y(1),RANGE(1),XMAX,(RANGE(2),XMIN),(RANGE(3),YMAX),
EQUIVALENCE RANGE(4),YMIN)
1 KA=IABS(NN)
IF(MODCUR.GT.1) GC TO 5

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SAT09450
SAT09460
SAT09470
SAT09480
SAT09490
SAT09500
SAT09510
SAT09520
SAT09530
SAT09540
SAT09550
SAT09560
SAT09570
SAT09580
SAT09590
SAT09600
SAT09610
SAT09620
SAT09630
SAT09640
SAT09650
SAT09660
SAT09670
SAT09680
SAT09690
SAT09700
SAT09710
SAT09720
SAT09730
SAT09740
SAT09750
SAT09760
SAT09770
SAT09780
SAT09790
SAT09800
SAT09810
SAT09820
SAT09830
SAT09840
SAT09850
SAT09860
SAT09870
SAT09880
SAT09890
SAT09900
SAT09910
SAT09920
SAT09930
SAT09940
SAT09950
SAT09960
SAT09970
SAT09980
SAT09990
SAT10000

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C***** RCUND MAXIMUM TO NEXT HIGHEST 2 SIG FIGS*****
C***** XMAX=AMAXI(0.,XMAX)*****
C***** CALL RCUND(XMAX,IMX,FMX)*****
C***** IFMX=FMX*10.*****
C***** 3 IF(XMX.GE.XMAX) GC TO 2*****
C***** IFMX=FMX*****
C***** IFMX=IMM*****
C***** GC TO 3*****
C***** RCUND MINIMUM TO NEXT LOWEST 2 SIG FIGS*****
C***** XMIN=AMINI(0.,XMIN)*****
C***** 2 CALL RCUND(XMIN,IMN,FMN)*****
C***** IFMN=FMN*10.*****
C***** 14 IF(XMIN.GE.XMN) GC TO 11*****
C***** IFMN=FMN*****
C***** IFMN=IMM*****
C***** GC TO 14*****
C***** RCUND MAX & MIN TC 1. OR .1 IF RANGE LARGE*****
C***** 11 XSC=XMX-XMN*****
C***** IF(XSC/CIV.LE.SM) GC TO 12*****
C***** 5 IF(ABS(XMN).LT.SM.AND.ABS(XMN).GT.0.) XMN=SIGN(SM,XMN)*****
C***** 12 IF(ABS(XMX).LT.SM.AND.ABS(XMX).GT.0.) XMX=SIGN(SM,XMX)*****
C***** IF(IM.GT.0) GO TO 19*****
C***** SM=.1*****
C***** IF(SM=IM+1)*****
C***** GC TO 9*****
C***** RCUND RANGE (MAX-MIN) TC 2 SIG FIGS*****
C***** 15 XSC=XMX-XMN*****
C***** CALL RCUND(XSC,ISIC,FACTX)*****
C***** FINC FACTOR WHICH IS MULTIPLE OF IDIV*****
C***** FACTX=FACTX*10.*****
C***** CFAC=FACTX*****

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```

SAT110410
SAT110420
SAT110430
SAT110440
SAT110450
SAT110460
SAT110470
SAT110480
SAT110490
SAT110500
SAT110510
SAT110520
SAT110530
SAT110540
SAT110550
SAT110560
SAT110570
SAT110580
SAT110590
SAT110600
SAT110610
SAT110620
SAT110630
SAT110640
SAT110650
SAT110660
SAT110670
SAT110680
SAT110690
SAT110700
SAT110710
SAT110720
SAT110730
SAT110740
SAT110750
SAT110760
SAT110770
SAT110780
SAT110790
SAT110800
SAT110810
SAT110820
SAT110830
SAT110840
SAT110850
SAT110860
SAT110870
SAT110880

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```

IS10=IS10-1
IFX=FACTX
IF(MOD(IFX, IDIV).EQ.0.AND.FACTX.GE.OFAC) GO TC 10
IFX=IFX+1
FACTX=IFX
GC TO 20
1C IF(IDIV.GT.4) GO TC 15
C *****
C IF X SCALE BETWEEN 8. AND 10., RCUND TO 10.
C *****
C FFX=ABS(FACTX/10.)
IF(FFX.GT.8.AND.FFX.LT.10.) FFX=10.
IF(FACTX.LT.0.) FFX=-10.
FACTX=FFX*10.
15 XSC=FACTX*10.**IS10
C *****
C COMPUTE NEW MAX & MIN FROM RCUNDED SCALE
C *****
C IF(XM N*XM X.NE.0.) GO TO 4
IF(XM N.LT.0.) XMIN=-XSC
IF(XM X.GT.C.) XMAX=XSC
RETURN XSC+XMN
4 XMIN=XMN
RETURN
C *****
C SLBROLLINE ROUND(ANUM, IS, FACT)
C *****
C EXPRESS ANUM IN SCIENTIFIC NOTATION WHERE
ANUM=FACT*10.**IS
IF(ANUM.EQ.0.) GO TC 15
ANUM=ANUM
BNUM=ANUM.LT.0.) BNUM=-BNUM
IF(BNUM.LT.0.) BNUM=43425448
IS=ALCG(BNUM/10.**IS)
C *****
C FIND PCWER OF 10
C *****
C ICC=-3
R2=0
DC 10 I I=1,5
ICL=ICL+1
R1=R2
R2=10.**(ICL+1)
IF(FACT.GE.R1.AND.FACT.LT.R2) GC TO 8

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SAT110890
SAT110900
SAT110910
SAT110920
SAT110930
SAT110940
SAT110950
SAT110960
SAT110970
SAT110980
SAT110990
SAT111000
SAT111010
SAT111020
SAT111030
SAT111040
SAT111050
SAT111060
SAT111070
SAT111080
SAT111090
SAT111100
SAT111110
SAT111120
SAT111130
SAT111140
SAT111150
SAT111160
SAT111170
SAT111180
SAT111190
SAT111200
SAT111210
SAT111220
SAT111230
SAT111240
SAT111250
SAT111260
SAT111270
SAT111280
SAT111290
SAT111300
SAT111310
SAT111320
SAT111330
SAT111340
SAT111350
SAT111360

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1C CCNTINUE*10.**(-IDD)
C FACT=IS+IDD
C RCLND MANTISSA TO 2 SIG FIGS
C IFAC=FACT*10.+*0.05
C FACT=IFAC/10.
C IF(FACT.LT.10.) GC TO 20
C SET TO 1 IF LESS THAN 10.
C FACT=1.
C IS=IS+1
C IF INPUT NEGATIVE, SET MANTISSA NEGATIVE
C 2C IF(ANUM.LT.0.) FACT=-FACT
C RETURN
C SET TO C. IF 0.
C IF FACT=0.
C IS=C
C RETURN
C SUBROUTINE DRAWIT(X,Y,NCATA,RANGE,KKZ,MOCCUR)
C DIMENSION X(1),Y(1),RANGE(4)
C INTEGER*2 GR1D,BLANK,DCT,XCHAR(4)/1H+,1H.,1H*,1HX/
C DATA DOT,BLANKZ
C KLATA=NCAT*GT.1) GC TO 444
C IF(MOCCUR.GT.1) GC TO 444
C GRID IS THE MATRIX USED TO PLOT THE POINTS
C IERR=0
C XMAX=RANGE(1)
C XMIN=RANGE(2)
C YMAX=RANGE(3)
C YMIN=RANGE(4)
C CHECKING X AND Y PCINTS AND PLOTTING THOSE CUT OF RANGE
C AT THE MARGIN
C 30 I=1,KCATA,KKZ

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SAT111370
SAT111380
SAT111390
SAT111400
SAT111410
SAT111420
SAT111430
SAT111440
SAT111450
SAT111460
SAT111470
SAT111480
SAT111490
SAT111500
SAT111510
SAT111520
SAT111530
SAT111540
SAT111550
SAT111560
SAT111570
SAT111580
SAT111590
SAT111600
SAT111610
SAT111620
SAT111630
SAT111640
SAT111650
SAT111660
SAT111670
SAT111680
SAT111690
SAT111700
SAT111710
SAT111720
SAT111730
SAT111740
SAT111750
SAT111760
SAT111770
SAT111780
SAT111790
SAT111800
SAT111810
SAT111820
SAT111830
SAT111840

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```

IF (X(I).GT.XMAX.OR.X(I).LT.XMIN.CR.Y(I).GT.YMAX.OR.Y(I).LT.YMIN)
1 IERR=IERR+1
IF (X(I).LE.XMAX) GC TC 205
X(I)=XMAX
GTC 21C
IF (X(I).GE.XMIN) GO TO 210
(I)=XMIN
205 X IF (Y(I).LE.YMAX) GC TO 215
IF (Y(I)=YMAX
21C Y GTC 3C
IF (Y(I).GE.YMIN) GC TO 30
(I)=YMIN
215 Y CCNTINUE
C***
C***
C***
PLCTTING X AND Y AXIS, IF NECESSARY
C***
C***
JERR=0
XRANGE=XMAX-XMIN
YRANGE=YMAX-YMIN
IF (YRANGE.NE.0.) GO TO 298
IF (YMIN.EQ.0.) GO TC 889
YRANGE=0.
YRANGE=YMAX
GC TO 259
258 IF (XRANGE.NE.0.) GO TO 295
IF (XMIN.EQ.0.) GO TC 887
XRANGE=0.
XRANGE=XMAX
C***
C***
BLANKING CUT MATRIX--(GRID)
C***
C***
C 300 I=1,61
C 301 JJ=1,81
C 302 GRIC(I, JJ)=BLANK
301 CCNTINUE
IF (XMAX*XMIN.GE.0.) GO TO 222
IYAXIS=80.*(-XMIN)/XRANGE+1.5
C 40 I=1,61
GRIC(I, IYAXIS)=DOT
40 GRIC(I, YMIN.GE.0.) GO TO 333
IYAXIS=60.*YMAX/YRANGE+1.5
C 60 I=1,81
GRID(IYAXIS, I)=DOT
C***
C***
CCMPUTE PROPER SCALE NUMBERS
C***
C***
333 XINCR=XRANGE/6.

```

SAT111850  
SAT111860  
SAT111870  
SAT111880  
SAT111890  
SAT111900  
SAT111910  
SAT111920  
SAT111930  
SAT111940  
SAT111950  
SAT111960  
SAT111970  
SAT111980  
SAT111990  
SAT112000  
SAT112010  
SAT112020  
SAT112030  
SAT112040  
SAT112050  
SAT112060  
SAT112070  
SAT112080  
SAT112090  
SAT112100  
SAT112110  
SAT112120  
SAT112130  
SAT112140  
SAT112150  
SAT112160  
SAT112170  
SAT112180  
SAT112190  
SAT112200  
SAT112210  
SAT112220  
SAT112230  
SAT112240  
SAT112250  
SAT112260  
SAT112270  
SAT112280  
SAT112290  
SAT112300  
SAT112310  
SAT112320



```

18 WRITE(6,18) YSCALE(II),(GRID(IK,IX),IX=1,81),YSCALE(II)
FCRMAT(3X,1PE10.3,2X,1H+,1X,81A1,1X,1H+,2X,E10.3)
GC TO 4C3
4C4 WRITE(6,118) YSCALE(II),(GRID(IK,IX),IX=1,81),YSCALE(II)
118 FCRMAT(2X,F11.2,'+',81A1,'+',F11.2)
4C5 GC TO 101
52 WRITE(6,19) (GRID(IK,IX),IX=1,81)
19 FCRMAT(15X,'*',81A1,'*')
1C1 CONTINUE
IF(AXR.LT.1.E+8.AND.AXR.GE..95) GC TO 402
22 WRITE(6,22) XSCALE
FCRMAT(15X,'**',8('***/12X,1PE10.3,4(10X,E10.3),//))
GC TO 4C3
4C2 WRITE(6,217) XSCALE
217 FCRMAT(15X,'**',8('***/8X,F11.2,4(9X,F11.2),//))
4C3 IF(IERR.GT.0) WRITE(6,20) IERR
20 FCRMAT(10X,'NUMBER OF PCINITS OUT OF RANGE =',I4)
10CC RETURN
8E5 WRITE(6,888)
8E8 FCRMAT(10X,'ALL Y VALUES=0. CANNOT SETUP PLCT GRID. CHECK MAX & MIN Y
      1 WHEN MCDCUR=0 OR 1.0')
RETURN
887 WRITE(6,886)
8E6 FCRMAT(10X,'ALL X VALUES=0. CANNOT SETUP PLCT GRID. CHECK MAX & MIN X
      1 WHEN MCDCUR=0 OR 1.0')
RETURN
8E5 WRITE(6,884)
884 FCRMAT(10X,'GRID NOT SETUP WHEN MOCCUR LAST 0 CR 1. NC PLOT UNTIL GRID
      10 PROPERLY SETUP.')
```

```

SUBROUTINE OUTPUT(IMCDE,P,DEE,DST,X,Z,Z0,Z2,Z3,ZDCT,IS,JS,ID,JD,
IPFIXB,PPFITB)
C*****
C THIS SUBROUTINE PREPARES THE PRINTOUT MATERIAL. EVERY IPRINT *****
C CONVERGED SOLUTION IS PRINTED. THE FOURIER COEFFICIENTS OF THE *****
C BENDING FORCES, MERIDIONAL TRANSVERSE FORCE, CIRCUMFERENTIAL *****
C AND BENDING MOMENT, TWISTING MOMENT AND RECTANGULAR CAN BE *****
C COMPUTED. THE SOLUTIONS FOR THE CURVING COEFFICIENTS *****
C OF THE THREE DIAPHRAGMS AND MERIDIONAL BENDING *****
C CUTPLATE MATERIAL IS CONVERTED FROM DIMENSIONLESS *****
C SIGNALS TO DIMENSIONAL VALUES. ONLY AT STATIONS *****
C 1, 2, 3, 4, 5, 6, 7, 8, 9, 10, 11, 12, 13, 14, 15, 16, 17, 18, *****
C 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, *****
C 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, *****
C 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, *****
C 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, *****
C 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, *****
C 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, *****
C 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, *****
C 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, *****
C 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, *****
C 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, *****
C 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, *****
C 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, *****
C 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, *****
C 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, *****
C 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, *****
C 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, *****
C 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, *****
C 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, *****
C 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, *****
C 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, *****
C 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, *****
C 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, *****
C 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, *****
C 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, *****
C 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, *****
C 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, *****
C 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, *****
C 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, *****
C 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, *****
C 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, *****
C 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, *****
C 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, *****
C 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, *****
C 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, *****
C 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, *****
C 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, *****
C 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, *****
C 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, *****
C 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, *****
C 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, *****
C 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, *****
C 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, *****
C 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, *****
C 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, *****
C 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, *****
C 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, *****
C 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, *****
C 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, *****
C 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, *****
C 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, *****
C 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, *****
C 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, *****
C 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, *****
C 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, *****
C 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, *****
C 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, *****
C 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, *****
C 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, *****
C 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, *****
C 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, *****
C 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, *****
C 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, *****
C 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, *****
C 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, *****
C 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, *****
C 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, *****
C 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, *****
C 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, *****
C 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, *****
C 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, *****
C 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, *****
C 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, *****
C 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, *****
C 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, *****
C 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, *****
C 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, *****
C 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, *****
C 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, *****
C 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, *****
C 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, *****
C 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, *****
C 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, *****
C 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, *****
C 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, *****
C 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, *****
C 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, *****
C 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, *****
C 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, *****
C 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, *****
C 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, *****
C 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, *****
C 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, *****
C 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, *****
C 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, *****
C 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, *****
C 994, 995, 996, 997, 998, 999, 1000, 1001, 1002, 1003, *****
C 1004, 1005, 1006, 1007, 1008, 1009, 1010, 1011, 1012, *****
C 1014, 1015, 1016, 1017, 1018, 1019, 1020, 1021, 1022, *****
C 1024, 1025, 1026, 1027, 1028, 1029, 1030, 1031, 1032, *****
C 1034, 1035, 1036, 1037, 1038, 1039, 1040, 1041, 1042, *****
C 1044, 1045, 1046, 1047, 1048, 1049, 1050, 1051, 1052, *****
C 1054, 1055, 1056, 1057, 1058, 1059, 1060, 1061, 1062, *****
C 1064, 1065, 1066, 1067, 1068, 1069, 1070, 1071, 1072, *****
C 1074, 1075, 1076, 1077, 1078, 1079, 1080, 1081, 1082, *****
C 1084, 1085, 1086, 1087, 1088, 1089, 1090, 1091, 1092, *****
C 1094, 1095, 1096, 1097, 1098, 1099, 1100, 1101, 1102, *****
C 1104, 1105, 1106, 1107, 1108, 1109, 1110, 1111, 1112, *****
C 1114, 1115, 1116, 1117, 1118, 1119, 1120, 1121, 1122, *****
C 1124, 1125, 1126, 1127, 1128, 1129, 1130, 1131, 1132, *****
C 1134, 1135, 1136, 1137, 1138, 1139, 1140, 1141, 1142, *****
C 1144, 1145, 1146, 1147, 1148, 1149, 1150, 1151, 1152, *****
C 1154, 1155, 1156, 1157, 1158, 1159, 1160, 1161, 1162, *****
C 1164, 1165, 1166, 1167, 1168, 1169, 1170, 1171, 1172, *****
C 1174, 1175, 1176, 1177, 1178, 1179, 1180, 1181, 1182, *****
C 1184, 1185, 1186, 1187, 1188, 1189, 1190, 1191, 1192, *****
C 1194, 1195, 1196, 1197, 1198, 1199, 1200, 1201, 1202, *****
C 1204, 1205, 1206, 1207, 1208, 1209, 1210, 1211, 1212, *****
C 1214, 1215, 1216, 1217, 1218, 1219, 1220, 1221, 1222, *****
C 1224, 1225, 1226, 1227, 1228, 1229, 1230, 1231, 1232, *****
C 1234, 1235, 1236, 1237, 1238, 1239, 1240, 1241, 1242, *****
C 1244, 1245, 1246, 1247, 1248, 1249, 1250, 1251, 1252, *****
C 1254, 1255, 1256, 1257, 1258, 1259, 1260, 1261, 1262, *****
C 1264, 1265, 1266, 1267, 1268, 1269, 1270, 1271, 1272, *****
C 1274, 1275, 1276, 1277, 1278, 1279, 1280, 1281, 1282, *****
C 1284, 1285, 1286, 1287, 1288, 1289, 1290, 1291, 1292, *****
C 1294, 1295, 1296, 1297, 1298, 1299, 1300, 1301, 1302, *****
C 1304, 1305, 1306, 1307, 1308, 1309, 1310, 1311, 1312, *****
C 1314, 1315, 1316, 1317, 1318, 1319, 1320, 1321, 1322, *****
C 1324, 1325, 1326, 1327, 1328, 1329, 1330, 1331, 1332, *****
C 1334, 1335, 1336, 1337, 1338, 1339, 1340, 1341, 1342, *****
C 1344, 1345, 1346, 1347, 1348, 1349, 1350, 1351, 1352, *****
C 1354, 1355, 1356, 1357, 1358, 1359, 1360, 1361, 1362, *****
C 1364, 1365, 1366, 1367, 1368, 1369, 1370, 1371, 1372, *****
C 1374, 1375, 1376, 1377, 1378, 1379, 1380, 1381, 1382, *****
C 1384, 1385, 1386, 1387, 1388, 1389, 1390, 1391, 1392, *****
C 1394, 1395, 1396, 1397, 1398, 1399, 1400, 1401, 1402, *****
C 1404, 1405, 1406, 1407, 1408, 1409, 1410, 1411, 1412, *****
C 1414, 1415, 1416, 1417, 1418, 1419, 1420, 1421, 1422, *****
C 1424, 1425, 1426, 1427, 1428, 1429, 1430, 1431, 1432, *****
C 1434, 1435, 1436, 1437, 1438, 1439, 1440, 1441, 1442, *****
C 1444, 1445, 1446, 1447, 1448, 1449, 1450, 1451, 1452, *****
C 1454, 1455, 1456, 1457, 1458, 1459, 1460, 1461, 1462, *****
C 1464, 1465, 1466, 1467, 1468, 1469, 1470, 1471, 1472, *****
C 1474, 1475, 1476, 1477, 1478, 1479, 1480, 1481, 1482, *****
C 1484, 1485, 1486, 1487, 1488, 1489, 1490, 1491, 1492, *****
C 1494, 1495, 1496, 1497, 1498, 1499, 1500, 1501, 1502, *****
C 1504, 1505, 1506, 1507, 1508, 1509, 1510, 1511, 1512, *****
C 1514, 1515, 1516, 1517, 1518, 1519, 1520, 1521, 1522, *****
C 1524, 1525, 1526, 1527, 1528, 1529, 1530, 1531, 1532, *****
C 1534, 1535, 1536, 1537, 1538, 1539, 1540, 1541, 1542, *****
C 1544, 1545, 1546, 1547, 1548, 1549, 1550, 1551, 1552, *****
C 1554, 1555, 1556, 1557, 1558, 1559, 1560, 1561, 1562, *****
C 1564, 1565, 1566, 1567, 1568, 1569, 1570, 1571, 1572, *****
C 1574, 1575, 1576, 1577, 1578, 1579, 1580, 1581, 1582, *****
C 1584, 1585, 1586, 1587, 1588, 1589, 1590, 1591, 1592, *****
C 1594, 1595, 1596, 1597, 1598, 1599, 1600, 1601, 1602, *****
C 1604, 1605, 1606, 1607, 1608, 1609, 1610, 1611, 1612, *****
C 1614, 1615, 1616, 1617, 1618, 1619, 1620, 1621, 1622, *****
C 1624, 1625, 1626, 1627, 1628, 1629, 1630, 1631, 1632, *****
C 1634, 1635, 1636, 1637, 1638, 1639, 1640, 1641, 1642, *****
C 1644, 1645, 1646, 1647, 1648, 1649, 1650, 1651, 1652, *****
C 1654, 1655, 1656, 1657, 1658, 1659, 1660, 1661, 1662, *****
C 1664, 1665, 1666, 1667, 1668, 1669, 1670, 1671, 1672, *****
C 1674, 1675, 1676, 1677, 1678, 1679, 1680, 1681, 1682, *****
C 1684, 1685, 1686, 1687, 1688, 1689, 1690, 1691, 1692, *****
C 1694, 1695, 1696, 1697, 1698, 1699, 1700, 1701, 1702, *****
C 1704, 1705, 1706, 1707, 1708, 1709, 1710, 1711, 1712, *****
C 1714, 1715, 1716, 1717, 1718, 1719, 1720, 1721, 1722, *****
C 1724, 1725, 1726, 1727, 1728, 1729, 1730, 1731, 1732, *****
C 1734, 1735, 1736, 1737, 1738, 1739, 1740, 1741, 1742, *****
C 1744, 1745, 1746, 1747, 1748, 1749, 1750, 1751, 1752, *****
C 1754, 1755, 1756, 1757, 1758, 1759, 1760, 1761, 1762, *****
C 1764, 1765, 1766, 1767, 1768, 1769, 1770, 1771, 1772, *****
C 1774, 1775, 1776, 1777, 1778, 1779, 1780, 1781, 1782, *****
C 1784, 1785, 1786, 1787, 1788, 1789, 1790, 1791, 1792, *****
C 1794, 1795, 1796, 1797, 1798, 1799, 1800, 1801, 1802, *****
C 1804, 1805, 1806, 1807, 1808, 1809, 1810, 1811, 1812, *****
C 1814, 1815, 1816, 1817, 1818, 1819, 1820, 1821, 1822, *****
C 1824, 1825, 1826, 1827, 1828, 1829, 1830, 1831, 1832, *****
C 1834, 1835, 1836, 1837, 1838, 1839, 1840, 1841, 1842, *****
C 1844, 1845, 1846, 1847, 1848, 1849, 1850, 1851, 1852, *****
C 1854, 1855, 1856, 1857, 1858, 1859, 1860, 1861, 1862, *****
C 1864, 1865, 1866, 1867, 1868, 1869, 1870, 1871, 1872, *****
C 1874, 1875, 1876, 1877, 1878, 1879, 1880, 1881, 1882, *****
C 1884, 1885, 1886, 1887, 1888, 1889, 1890, 1891, 1892, *****
C 1894, 1895, 1896, 1897, 1898, 1899, 1900, 1901, 1902, *****
C 1904, 1905, 1906, 1907, 1908, 1909, 1910, 1911, 1912, *****
C 1914, 1915, 1916, 1917, 1918, 1919, 1920, 1921, 1922, *****
C 1924, 1925, 1926, 1927, 1928, 1929, 1930, 1931, 1932, *****
C 1934, 1935, 1936, 1937, 1938, 1939, 1940, 1941, 1942, *****
C 1944, 1945, 1946, 1947, 1948, 1949, 1950, 1951, 1952, *****
C 1954, 1955, 1956, 1957, 1958, 1959, 1960, 1961, 1962, *****
C 1964, 1965, 1966, 1967, 1968, 1969, 1970, 1971, 1972, *****
C 1974, 1975, 1976, 1977, 1978, 1979, 1980, 1981, 1982, *****
C 1984, 1985, 1986, 1987, 1988, 1989, 1990, 1991, 1992, *****
C 1994, 1995, 1996, 1997, 1998, 1999, 2000, 2001, 2002, *****
C 2004, 2005, 2006, 2007, 2008, 2009, 2010, 2011, 2012, *****
C 2014, 2015, 2016, 2017, 2018, 2019, 2020, 2021, 2022, *****
C 2024, 2025, 2026, 2027, 2028, 2029, 2030, 2031, 2032, *****
C 2034, 2035, 2036, 2037, 2038, 2039, 2040, 2041, 2042, *****
C 2044, 2045, 2046, 2047, 2048, 2049, 2050, 2051, 2052, *****
C 2054, 2055, 2056, 2057, 2058, 2059, 2060, 2061, 2062, *****
C 2064, 2065, 2066, 2067, 2068, 2069, 2070, 2071, 2072, *****
C 2074, 2075, 2076, 2077, 2078, 2079, 2080, 2081, 2082, *****
C 2084, 2085, 2086, 2087, 2088, 2089, 2090, 2091, 2092, *****
C 2094, 2095, 2096, 2097, 2098, 2099, 2100, 2101, 2102, *****
C 2104, 2105, 2106, 2107, 2108, 2109, 2110, 2111, 2112, *****
C 2114, 2115, 2116, 211
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1 YDEGMS(200), YBSTIF(200), YCSTIF(200), YBSTIF(200), YBSTIF(200),
2 YDDSTIF(200), YPR(200), YPS(200), YPT(200), YPT(200), YPT(200),
3 YMT(200), YDT(200), YDMT(200), YNS(200), YNTF(200),
4 YNSTH(200), YQS(200), YMS(200), YMTH(200), YMSTH(200),
5 YU(200), YV(200), YW(200), YPFI(200), YPFI(200),
6 YPHI(200), XSTATN(200)
C*****
DIMENSION PTF(500), *****
AEZC=SIGO/ELAST *****
IF ($DYAMC) GO TO 181 *****
WRITE(6,101) LSTEP,ALOAD,ITR *****
GC TO 182 *****
TI=LSTEP*DELOAD *****
CII=TI*TEEG *****
WRITE(6,151) LSTEP,TI,DTI,ITR *****
LAW=TKN/CHAR *****
ENL=1 *****
AEZ=SIGC*TKN *****
AEZ3=ABZ*TKN*TKN/CHAR *****
AEZIN=CHAR*SIGO/ELAST *****
IF (ITRMAX.EQ.1) ENL=0. *****
CC2=1.-NU*#2 *****
CPI=1./CD2 *****
CNI=1./CI *****
TCLSQI=5/DELSQ *****
ICCHK1=IABS(INTH)+IABS(INSTH)+IABS(IQS)+IABS(IMS) *****
ICCHK2=IABS(IU)+IABS(IV)+IABS(IW)+IABS(IPHIS)+IABS(IPHIT) *****
IF (NT+MAX.EQ.0) GC TO 991 *****
CC 21 NTH=1,NTHMAX *****
CC 1 MN=1,MNMAX *****
I1=I+(MN-1)*KMAX2 *****
U1(MN)=Z(1,I1) *****
U2(MN)=Z(1,I2) *****
V1(MN)=Z(2,I1) *****
V2(MN)=Z(2,I2) *****
W1(MN)=Z(3,I1) *****
W2(MN)=Z(3,I2) *****
WRITE(6,116) THET *****
CC 121 K=1,KMAX *****
K1=K+1 *****
CALL BCE(K,BS,DB,CS,DD) *****
IF(K.EQ.1) AND.IBCINL.LT.0) CALL PCLE(K,P,DEE,CST,X,Z,ZO,Z2,Z3, *****
1 ZCCT,IS,JS,JD,PHIXB,PHITE) *****
SAT113770
SAT113780
SAT113790
SAT113800
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SAT114000
SAT114010
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SAT114090
SAT114100
SAT114110
SAT114120
SAT114130
SAT114140
SAT114150
SAT114160
SAT114170
SAT114180
SAT114190
SAT114200
SAT114210
SAT114220
SAT114230
SAT114240

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IF(K.EQ.1.AND.IBCINL.LT.0) GO TC 999
IF(K.EQ.KMAX.AND.IBCFNL.LT.0) CALL POLE(K,P,CEE,DST,X,Z,ZO,Z2,Z3,
1ZCCT,IS,JS,JD,PHIXB,PHITB)
IF(K.EQ.KMAX.AND.IBCFNL.LT.0) GO TO 999
CALL PHIBET(K,Z,IS,JS,JD,PHIXB,PHITB)
CEX=DEGPMX(K)
FRA=1./R(K)
CX=CMXI(K)
CT=CMT(K)
GA=GAM(K)
DCXT=OX-CT
CCC=GA*COXT
CL2C=CC2*DS
CC 3 MN=1,MNMAXJ
ENR=EN*FRA
CALL TLOAD(K,Z)
TTS=TT(MN)*ALOAD
EX=(U3(MN)-U1(MN))*TDLI+OX*W2(MN)+ENL*OSE*(EX3(MN)+BE3(MN))
ET=ENR*V2(MN)+GA*U2(MN)+ENL*OSE*(BT3(MN)+BE3(MN))
EXT=.5*((V3(MN)-V1(MN))*TDLI-ENR*U2(MN)-GA*V2(MN)+ENL*SCE*BXT3(MN))
1)
KT=ENR*PHIT(MN)+GA*PHIX(MN)
KXT=.5*(ENR*(-PHIX(MN)-GA*W2(MN)+(W3(MN)-W1(MN))*TDLI)+GCO*V2(MN)
+OT*(V3(MN)-V1(MN))*TDLI-GA*PHIT(MN)-CCXT*PHI(MN))
TX(MN)=ES*(EX+NU*ET)-TTS
TTH(MN)=BS*DI*EXT
TKI=KI+(MN-1)*KMAX2
MX(MN)=Z(4,MKI)
MTF(MN)=NU*MX(MN)+DD20*KT-DI*MT(MN)*ALOAD
MKI=MKI+1
MKKI=MKI-1
1)
CS(MN)=SIGO*TKN*LAM2*(GA*MX(MN)+(Z(4,MKI)-Z(4,MKKI))*TDLI
+ENR*MX(MN)-GA*MTH(MN))
MX(MN)=MX(MN)*ABZ3
MTF(MN)=MTH(MN)*ABZ3
TX(MN)=TX(MN)*ABZ
TTH(MN)=TTH(MN)*ABZ
PHIX(MN)=PHIX(MN)*ABZ0
PHIT(MN)=PHIT(MN)*ABZC
PLI(MN)=PLI(MN)*ABZ0
L2(MN)=L2(MN)
VI(MN)=V2(MN)

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SAT114250
SAT114260
SAT114270
SAT114280
SAT114290
SAT114300
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SAT114370
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SAT114390
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SAT114720

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3  V1(MN)=V3(MN)
   W2(MN)=W3(MN)
   FK=K-1
   FIFREQ=IFREQ
   K1ST=(K-1)/IFREQ
   FK1ST=FKTST
   FK1ST=FK/FIFREQ-FKTST
   IF(K.EQ.1.OR.K.EQ.KMAX) GO TO 995
   IF(FKTEST.NE.0.) GO TO 2
555 X(1,K)=0.
     X(2,K)=C.
     X(3,K)=0.
     X(4,K)=C.
     PTF(K)=C.
     PPF(K)=0.
     AMX=0.
     AMTF=0.
     ANXTH=0.
     ANX=0.
     ANTF=0.
     ANXTH=0.
     ACS=0.
     IF(JUMP.EQ.2) GO TO 73
72  CC 72 MN=1,MNMAXO
     EN=N(MN)
     FC=EN*TFET
     SN=SIN(FC)
     CS=COS(FC)
     X(1,K)=X(2,K)+U1(MN)*CS*ABZN
     X(2,K)=X(3,K)+V1(MN)*SN*ABZN
     X(3,K)=X(4,K)+W1(MN)*CS*ABZN
     X(4,K)=X(1,K)+PHIX(MN)*CS
     PTF(K)=PTF(K)+PHIT(MN)*SN
     AMX=AMX+MX(MN)*CS
     AMTF=AMTF+MTH(MN)*CS
     ANXTH=AMXTH+MX(MN)*SN
     ANX=ANX+TX(MN)*CS
     ANTF=ANTF+TTH(MN)*CS
     ACS=ACS+QS(MN)*CS
     ANXTH=ANXTH+TX(MN)*SN
     PPF(K)=PPF(K)+PHI(MN)*SN
C*****
72  CC 72 MN=3,MNMAXO,JUMP
C*****
73  EN=N(MN)
     FC=EN*TFET
     SN=SIN(FC)

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SATI15210  
SATI15220  
SATI15230  
SATI15240  
SATI15250  
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SATI15640  
SATI15650  
SATI15660  
SATI15670  
SATI15680

```
CS=CS(FC)
MNM=MN-1
X(1,K)=X(1,K)+(UI(MN)*CS+VI(MNM)*SN)*ABZN
X(2,K)=X(2,K)+(VI(MN)*CS+VI(MNM)*SN)*ABZN
X(3,K)=X(3,K)+(WI(MN)*CS+WI(MNM)*SN)*ABZN
X(4,K)=X(4,K)+(PHIX(MN)*CS+PHIX(MNM)*SN)*CS
PTF(K)=PTF(K)+PHIT(MN)*SN+PHIT(MNM)*CS
AMX=AMX+MX(MN)*CS+MX(MNM)*SN
AMTH=AMTH+MTH(MN)*CS+MTH(MNM)*SN
AMXT=AMXT+MX(MN)*SN+MX(MNM)*CS
ANX=ANX+TX(MN)*CS+TX(MNM)*SN
ANTH=ANTH+TTH(MN)*CS+TTH(MNM)*SN
ANXTH=ANXTH+TX(MN)*SN+TX(MNM)*CS
ACS=ACS+QS(MN)*CS+QS(MNM)*SN
PF(K)=PF(K)+PHI(MN)*SN+PHI(MNM)*CS
X(1,K)=X(1,K)+(UI(1)*ABZN
X(2,K)=X(2,K)+(VI(1)*ABZN
X(3,K)=X(3,K)+(WI(1)*ABZN
X(4,K)=X(4,K)+(PHIX(1)
PTF(K)=PTF(K)+PHIT(1)
PF(K)=PF(K)+PHI(1)
AMX=AMX+MX(1)
AMTH=AMTH+MTH(1)
AMXT=AMXT+MX(1)
ANX=ANX+TX(1)
ANTH=ANTH+TTH(1)
ANXTH=ANXTH+TX(1)
ACS=ACS+QS(1)
C*****
C CONTINUE
IF(K.EQ.1) WRITE(6,117)
WRITE(6,118) K,ANX,ANTH,ANXTH,AQS,AMX,AMTH,AMXTH
IF ($MOD CAL.OR.(ICHECK1.EQ.0)) GO TO 2
YNS(K)=ANX
YNSH(K)=ANXTH
YCS(K)=AQS
YMSH(K)=AMXTH
YMSH(K)=AMXTH
CCNTINUE
CC 66C K=1,KMAX
FK=K-1
FIFREQ=IFREQ
FKTST=(K-1)/IFREQ
FKTEST=FK/FIFREQ-FKTST
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74

C\*\*\*\*\*  
425

121

SAT115690  
 SAT115700  
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 SAT116100  
 SAT116110  
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 SAT116130  
 SAT116140  
 SAT116150  
 SAT116160

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IF (K.EQ.1.OR.K.EQ.KMAX) GO TO 661
IF (K.EQ.1) GO TO 658
IF (K.EQ.1) WRITE (6,217)
WRITE (6,218) K,X(1,K),X(2,K),X(3,K),X(4,K),FTF(K),PF(K)
IF ($MOCAL.OR.(ICFCK2.EQ.0)) GO TO 658
YL(K)=X(1,K)
YV(K)=X(2,K)
YK(K)=X(3,K)
YPHIS(K)=X(4,K)
YPHIT(K)=PF(K)
YFFI(K)=PF(K)
DC 659 I=1,4
CCNTINUE
IF ($PLCTS.AND..NOT.$MOCAL.AND.((ICCHK1.GT.0).OR.(ICFCK2.GT.0)))
1 CALL PLOT2(NTH)
21 CCNTINUE
IF (IMCDE.LE.0) RETURN
CC 534 MN=1,MNMAX0
WRITE (6,749) N(MN)
DC 521 MM=1,MNMAXC
I1=1+(MM-1)*KMAX2
I2=I1+1
U1(MM)=Z(1,I1)
U2(MM)=Z(1,I2)
V1(MM)=Z(2,I1)
V2(MM)=Z(2,I2)
W1(MM)=Z(3,I1)
W2(MM)=Z(3,I2)
CCNTINUE
DC 445 K=1, KMAX
K1=K+1
CALL BCE(K,BS,DB,CS,DC)
IF (K.EQ.1.AND.IBCINL.LT.0) CALL PCLE(K,P,DEE,CST,X,Z,Z0,Z2,Z3,
1 ZCCT,IS,JS,IO,JD,PHIXB,PHITB)
IF (K.EQ.KMAX.AND.IBCFNL.LT.0) CALL POLE(K,P,DEE,DST,X,Z,Z0,Z2,Z3,
1 ZCCT,IS,JS,IO,JD,PHIXB,PHITB)
T XZ=TX(MN)
T THZ=TF(MN)
T XT=TX(MN)
T XZ=MX(MN)
T THZ=MT(MN)
T XZ=MX(MN)
C SZ=QS(MN)
X(1,K)=PHIX(MN)
X(2,K)=PHIT(MN)
X(3,K)=PHI(MN)
IF (K.EQ.1.AND.IBCINL.LT.0) GO TO 583

```

IF(K.EQ.KMAX.AND.IBCFNL.LT.0) GC TC 583  
CALL PHIBET(K,Z,IS,JS,IO,JD,PHIXB,PHITB)  
LEX=DECPIX(K)  
LERR=1./R(K)  
CX=CMXI(K)  
CT=CMT(K)  
GA=GAM(K)  
LCCX=OX-CT  
LCCC=GA\*CCXT  
DLZC=CDZ\*DS  
ENR=EN(MN)  
ENR=EN\*RRRA  
CALL LCCAD(K,Z)  
TTS=TT(MN)\*ALOAD  
EX=(U3(MN)-UI(MN))\*TDLI+OX\*W2(MN)+ENL\*OSE\*(BX3(MN)+BE3(MN))  
ET=ENR\*V2(MN)+GA\*U2(MN)+OT\*W2(MN)+ENL\*OSE\*(BT3(MN)+BE3(MN))  
EXT=.5\*((V3(MN)-V1(MN))\*TDLI-ENR\*U2(MN)-GA\*V2(MN)+ENL\*SOE\*BXT3(MN))

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SATI16590  
SATI16600  
SATI16610  
SATI16620  
SATI16630  
SATI16640

KT=ENR\*PHIT(MN)+GA\*PHIX(MN)  
KXT=.5\*(ENR\*(-PHIX(MN)-GA\*W2(MN)+(W3(MN)-W1(MN))\*TDLI)+GCO\*V2(MN)  
+OT\*(V3(MN)-V1(MN))\*TDLI-GA\*PHIT(MN)-CCXT\*PHI(MN))  
TXZ=(BS\*(EX+NU\*EI)-TTS)\*ABZ  
THZ=(BS\*(ET+NU\*EX)-TTS)\*ABZ  
TXIZ=BS\*DI\*EXT\*ABZ  
PXI=KI+(MN-1)\*KMAX2  
AMXZ=Z(4,MK1)  
AMXIZ=NU\*AMXZ+DD2D\*KT-DI\*MT(MN)\*ALCAD  
AMXII=MKI+1  
MKKI=MKI-1  
CSZ=SIGO\*TKN\*LAM2\*(GA\*AMXZ+(Z(4,MK1)-Z(4,MK1))\*TDLI+ENR\*AMXTZ  
-GA\*AMTHZ)  
AMXZ=AMXZ\*ABZ3  
AMTHZ=AMTHZ\*ABZ3  
AMXIZ=AMXIZ\*ABZ3  
X(1,K)=PHIX(MN)\*ABZC  
X(2,K)=PHIT(MN)\*ABZC  
X(3,K)=FFI(MN)\*ABZC  
X(4,K)=MM=1,MNMAXC  
LI(MN)=L2(MN)  
L3(MN)=U3(MN)  
V1(MN)=U3(MN)  
V2(MN)=V3(MN)  
W1(MN)=W2(MN)  
W2(MN)=W3(MN)  
FK=K-1  
FIFREQ=IFREQ  
KTST=(K-1)/IFREQ

```

FKTST=FK/FIFREQ-FKST
IF(K.EQ.1.OR.K.EQ.KMAX) GO TO 583
IF(FKTEST.NE.0.) GC TC 445
CCNTINUE
IF(K.EQ.1) WRITE(6,117)
WRITE(6,118) K, TXZ, TTHZ, TXTZ, QSZ, AMXZ, AMTFZ, AMXTZ
IF(.NOT.$PLOTS.OR..NOT.$MODAL.CR.(ICCHK1.EC.C)) GC TC 445
YNS(K)=TXZ
YNTF(K)=TTHZ
YNSTH(K)=TXTZ
YCS(K)=CSZ
YMS(K)=AMXZ
YMTF(K)=AMTHZ
YMSH(K)=AMXTZ
CCNTINUE
WRITE(6,217)
DC 447 K=1, KMAX
FK=K-1
FIFREQ=IFREQ
FKTST=(K-1)/IFREQ
FKTST=FKTST
FKTST=FK/FIFREQ-FKST
IF(K.EQ.1.CR.K.EQ.KMAX) GO TO 593
IF(FKTEST.NE.0.) GO TO 447
KZ=K+1+(MN-1)*KMAX2
VF=Z(1,KZ)*ABZN
VF=Z(2,KZ)*ABZN
VF=Z(3,KZ)*ABZN
WRITE(6,218) K, UP, VP, WP, X(1,K), X(2,K), X(3,K)
IF(.NOT.$PLOTS.OR..NCT.$MODAL.CR.(ICCHK2.EC.O)) GC TC 447
YL(K)=UP
YV(K)=VF
YW(K)=WF
YFFIS(K)=X(1,K)
YFFIT(K)=X(2,K)
YFFI(K)=X(3,K)
CCNTINUE
IF ($FLCTS.AND.$MODAL.AND.(ICCHK1.GT.0).OR.(ICCHK2.GT.0))
  CALL PLCT2(1)
1 CCNTINUE
C*****
IC1 FCRMAT(1, ' THE LCAC STEP NUMBER IS ', I2, '
ITERATIONS', I1, ' E11.4, ' THE SOLUTION CONVERGED IN ', I2, '
FCRMAT(0, ' THE SUMMED FCRCES, MCMENTS, DISPLACEMENTS ANS
IC RCTATIONS FOLLOW FOR THETA =', E15.6//)
117 FCRMAT (/, STATION N S N THETA N STHETA

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SAT116690
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SAT117120

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CCMCON /BL3/ PR(99),PX(99),PT(95)
CCMCON /BL4/ ZF1M(4,4,99),ZF2M(4,4,99),
1 CCMCON /BL5/ ZF3M(4,4,99),ZF4M(4,4,99),
CCMCON /BL6/ TT(99),MT(99),DT(95),DMT(95)
CCMCON /BL7/ SDE, CSE, ALOAD
CCMCON /BL8/ DI, SI
CCMCON /BL9/ DI(500), GAM(500), DMT(500)
CCMCON /BL14/ RFFS(4,99), ELIS(4), CEES(4,99)
CCMCON /BL15/ LAM2, LSD18, LSD1N
1 CCMCON /BL16/ NU, UI(99), VI(99), W1(99), V2(59), U2(99), W2(55), U3(99),
CCMCON /BL17/ V3(99), W3(99)
CCMCON /BL18/ ELL(4), ELL(4)
CCMCON /BL27/ BX3(95), BT3(99), BX13(99), BE3(59)
CCMCON /BL28/ EXX3(59), ET3(99), ETX3(99), EX2(95), ET3(59)
CCMCON /BL29/ BX1(99), BT1(99), BX1(99), BE1(59), BT2(99),
1 CCMCON /BL30/ BX12(59), BE2(59)
1 CCMCON /BL31/ EXX1(99), ET1(99), EX1(99), ET1(59), EXX2(99),
CCMCON /BL100/ ETT2(99), ETX2(99), EXT2(99), ET2(59)
CCMCON /BL101/ DELSQ, EXTI(99)
CCMCON /BL102/ TEESC, $DYNMC
CCMCON /BL103/ DELOAD
DIMENSION ELLS(4), FLS(4), ZI(4), IPIVOT(4), INCEX(4,2)
1, CLO(4,4), CLI(4,4), ZDD(4)
2, TZMAX(4,99), ZDO(4)
C***** I=1,4
CC 201 I=1,4 MNMAX
CC 201 M=1, MNMAX
AJ=1+(M-1)*KMAX2
TZMAX(I,M)=ABS(Z(I,MJ))
CC 201 K=2, KMAX2
KA=K+(M-1)*KMAX2
AZTST=ABS(Z(I,KM))
IF(AZTST.GT.TZMAX(I,M)) TZMAX(I,M)=AZTST
CCATINUE
NCCNV=1
IF(ITRM.AX.EQ.1) GC TC 66
DC 1 MNMAXO
I=1+(KM+2)*(M-1)
LI(M)=Z(1,I)
VI(M)=Z(2,I)
W1(M)=Z(3,I)
I1=I+1
L2(M)=Z(1,I1)
V2(M)=Z(2,I1)
SAT17610
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 SATI18550  
 SATI18560

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1 W2(M)=Z(3,11) GC TO 100
  IF(IBCINL,LT,0) GC TO 100
  CALL PHIBET(1,Z,IS,JS,ID,JD,PHIXE,PHITB)
  CC 2 P=1,MNMAX
  BX1(M)=BX3(M)
  BT1(M)=BT3(M)
  BX11(M)=BX13(M)
  BE1(M)=BE3(M)
  CALL TEAETA(1,Z,IS,JS,ID,JD)
  CC 3 M=1,MNMAX
  EXX1(M)=EXX3(M)
  ET11(M)=ET13(M)
  ETX11(M)=ETX3(M)
  EX11(M)=EX13(M)
  ET1(M)=ET3(M)
  CALL PHIBET(2,Z,IS,JS,ID,JD,PHIXE,PHITB)
  CC 4 P=1,MNMAX
  BX2(M)=BX3(M)
  BT2(M)=BT3(M)
  BX12(M)=BX13(M)
  BE2(M)=BE3(M)
  CALL TEAETA(2,Z,IS,JS,ID,JD)
  CC 5 P=1,MNMAX
  EXX2(M)=EXX3(M)
  ETX2(M)=ETX3(M)
  EX12(M)=EX13(M)
  ET2(M)=ET3(M)
  CALL PHIBET(3,Z,IS,JS,ID,JD,PHIXB,PHITB)
  CC 6 CONTINUE
  IF(IBCINL,LT,0) GC TO 20
  CALL BOB(1,BI,DB,D,CD)
  GAMI=GAM(1)
  CALL TLCAD(1,Z)
  CC 8 P=1,MNMAX
  IF(ITRMAX,EQ,1) GO TO 67
  FFS(1,M)=-TT(M)*ALCAD+OSE*(EX1(M)+BE1(M)+NU*(BT1(M)+BE1(M))*B1
  FFS(2,M)=OSE*(BI *DI *BT1(M)+EX1(M)+ET1(M))
  FFS(3,M)=LAM2*GAMI*DI *MT(M)*ALOAD-(EXX1(M)+ETX1(M))*SOE
  GC TO 8
  CC 9 I=1,4
  FFS(1,M)=-TT(M)*ALCAD
  FFS(2,M)=0
  FFS(3,M)=LAM2*GAMI*DI *MT(M)*ALOAD
  FFS(4,M)=0
  CC 9 I=1,4

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5  ELIS(I)=ALOAD*ELI(I)
20 CALL FORCE(1,P,X,DEE,DST,Z,ZO,Z2,Z3)
   CALL FCRCE(2,P,X,DEE,DST,Z,ZO,Z2,Z3)
   CC 10 K=3,KLL
   KF=K+1
   IF(ITRMAX.EQ.1) GO TO 1C
   CALL UPDATE
   CALL PHIBET(KP,Z,IS,JS,JD,PHIXE,PHITB)
   CALL TEAETA(KP,Z,IS,JS,JD)
   CALL FCRCE(K,P,X,DEE,DST,Z,ZO,Z2,Z3)
1C  IF(ITRMAX.NE.1) CALL UPDATE
   IF(ITRCFNL.LT.0) GO TO 120
   IF(ITRMAX.EQ.1) GO TO 11
   CALL PHIBET(KMAX,Z,IS,JS,JD,PHIXB,PHITB)
   CALL TEAETA(KMAX,Z,IS,JS,JD)
11  CALL FCRCE(KL,P,X,DEE,DST,Z,ZO,Z2,Z3)
   CC 12 I=1,4
12  ELIS(I)=ALOAD*ELL(I)
   CALL BCB(KMAX,BL,DB,D,DD)
   GAML=GAM(KMAX)
   FLS(4)=C
   CALL TLCAD(KMAX,Z)
   CC 14 M=1,MNMAX
   IF(M.GT.1) ELLS(I)=0.0
   IF(ITRMAX.EQ.1) GC TO 68
   FLS(1)=-TT(M)*ALCAD*USE*(BX3(M)+BE3(M)+NU*(ET3(M)+BE3(M))) *BL
   FLS(2) = OSE*(BL*DI*BT3(M)+EX3(M)+ET3(M))
   FLS(3) = LAM2#GAML*DI*MT(M)*ALOAD-(EXX3(M)+ETX3(M))*SOE
   GC TO 65
6E  FLS(1)=-TT(M)*ALOAD
65  FLS(2)=C
   FLS(3)=LAM2#GAML*DI*MT(M)*ALOAD
   CCNTINUE
   IK=KL+KMAX*(M-1)
   IJ=KMAX*M
   L=M*KMAX2
   DC 14 I=1,4
   SUMZ=0.
   CC 15 J=1,4
   C*****
   C THE FOLLOWING CARC CAUSES BOUNDARY CONS TO EXIST FCR MODE 'O' ONLY*****
   C*****
   C IF (M.NE.1) ELLS(J)=0
15  SUMZ=SUMZ+ZF1M(I,J,M)*ELLS(J)+ZF2M(I,J,M)*X(J,IJ)+ZF3M(I,J,M)*
14  Z(I,I,L)=SUMZ
   L=L+1

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SAT18600
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 SATI19510  
 SATI19520

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15C CC 16 M=1, MNMAX
    CC 16 L=LS, KMAX
    K=KMAX2-L
    KFX=K-1
    KZ=K+1
    IJ=KPX+(H-1)*KMAX
    JK=KZ+(M-1)*KMAX2
    CC 17 I=1,4
    SUMZ=0.
18 DC 18 J=1,4
    SUMZ=SUMZ-P(I,J,IJ)*Z(J,JK)
    ASUMZ=SUMZ+X(I,IJ)
    ASUMZ=ABS(SUMZ)
    IF(ASUMZ.GT.1.E+15) ITR=ITRMAX
    IF(NCCNV.NE.1.OR.ASUMZ.LT.1.E-05) GC TC 17
    DELZ=ABS(Z(I,JK))-SUMZ
    ZTEST=EFPS*ZMAX(I,M)
    IF(DELZ.GT.ZTEST) NCCNV=0
    Z(I,JK)=SUMZ
17 CC CONTINUE
16 IF(IBCINL.LT.0) GO TO 30
    CC 25 M=1, MNMAX
    CALL EFG(I,M,ZD,Z2,Z3)
    CALL ABC
    IJ=2+(M-1)*KMAX2
    I=IJ+1
    I2=IJ-1
    CC 21 I=1,4
    SUMZ=0.
22 DC 22 J=1,4
    SUMZ=SUMZ-A(I,J,IJ)*Z(J,IJ)-BEE(I,J)*Z(J,IJ)
21 ZT(I)=SUMZ+GEES(I,M)
    CALL MATINV(C,4,Z1,I,DETERM,IPIVOT,INDEX,4,ISCALE)
23 CC 23 I=1,4
    Z(I,IJ2)=ZT(I)
25 CC CONTINUE
100 RETURN
    CALL INLPOL (Z,PHIXB,PHITB)
    CC 101 M=1, MNMAX
    U1(M)=U2(M)
    V1(M)=V2(M)
    W1(M)=W2(M)
    I=3+KMAX2*(M-1)
    U2(M)=Z(I,IJ)
    V2(M)=Z(2,IJ)
    W2(M)=Z(3,IJ)
    GC TC IC2
  
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120 IF(ITRMAX.NE.1) CALL FNLPOL (Z,PF,IX8,PHITB)
CALL FCRCE(KL,P,X,DEE,DST,Z,ZC,Z2,Z3)
IF(M2.EQ.0) GO TO 122
L=KL+(M2-1)*KMAX
L1=KMAX1+(M2-1)*KMAX2
CC 130 I=1,4
SUM=0.
CC 131 J=1,4
SUM=SUM+CL2(I,J)*X(J,L)
SUMZ=ABS(SUM)
IF(NCONV.NE.1 .OR. ASUMZ.LT.1.E-05) GO TC 130
DELZ=ABS(Z(I,L1)-SUM)
ZTEST=EPS*IZMAX(I,M2)
IF(DELZ.GT.ZTEST) NCONV=0
Z(I,L1)=SUM
IF(M1.EQ.0) GO TO 123
L=KL+(M1-1)*KMAX
L1=KMAX1+(M1-1)*KMAX2
CC 132 I=1,4
SUM=0.
CC 133 J=1,4
SUM=SUM+CL1(I,J)*X(J,L)
SUMZ=ABS(SUM)
IF(NCONV.NE.1 .OR. ASUMZ .LT. 1.E-05) GO TC 132
DELZ=ABS(Z(I,L1)-SUM)
ZTEST=EPS*IZMAX(I,M1)
IF(DELZ.GT.ZTEST) NCONV=0
Z(I,L1)=SUM
IF(M0.EQ.0) GO TO 124
L=KL+(M0-1)*KMAX
L1=KMAX1+(M0-1)*KMAX2
CC 134 I=1,4
SUM=0.
CC 135 J=1,4
SUM=SUM+CL0(I,J)*X(J,L)
SUMZ=ABS(SUM)
IF(NCONV.NE.1 .OR. ASUMZ.LT.1.E-06) GO TC 134
DELZ=ABS(Z(I,L1)-SUM)
ZTEST=EPS*IZMAX(I,M0)
IF(DELZ.GT.ZTEST) NCONV=0
Z(I,L1)=SUM
L3=2
CC TO 150
ENC
SLROUTINE PLOT2(NTI)
C***** THIS SUBROUTINE CALLS PLOTTING ROUTINES FCR APPROPRIATE (USER *****
C***** SAT120000
SAT119530
SAT119550
SAT119560
SAT119570
SAT119580
SAT119590
SAT119600
SAT119610
SAT119620
SAT119630
SAT119640
SAT119650
SAT119660
SAT119670
SAT119680
SAT119690
SAT119700
SAT119710
SAT119720
SAT119730
SAT119740
SAT119750
SAT119760
SAT119770
SAT119780
SAT119790
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SAT119980
SAT119990
SAT120000

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C***** SPECIFIED) OUTPUT QUANTITIES *****
C***** I ($) *****
C***** IBL4/ KMAX, KL *****
C***** /BL19/ TH(36) *****
C***** /BLPLOT/ *****
1 I, IGAMMA, ICMEGS, IOMEGT, IDEOMS, IBSTIF, IDSTIF,
2 IBSTIF, IPRI, IPS, IPT, IIT, IMT, ICTT, ICM, INS,
3 INPHI, INSTH, IQS, IMS, IMTH, IMSTH, IU, IV, IW, IFHIS,
4 IPHI, IPLCTS, $MCCAL *****
C***** /BLPLT1/ *****
1 XRADII(200), YGAMMA(200), YCMEGS(200), YCMEGT(200),
2 YDECMS(200), YBSTIF(200), YDSTIF(200), YBBSIF(200),
3 YDDSTF(200), YPR(200), YPS(200), YPT(200), YTT(200),
4 YMT(200), YDIT(200), YNS(200), YNSTH(200),
5 YNSTH(200), YQS(200), YMS(200), YMTH(200),
6 YL(200), YV(200), YW(200), YPHIS(200), YPFI(200),
C***** XSTAIN(200) *****
C***** NGKMAX=-KMAX *****
C***** GO TO 121 *****
IF ($MCCAL) GO TO 121
IF (INS.EQ.0) GO TO 4
IF (INS.EQ.1000)
IF (INS.EQ.0) CALL PLOTIT (XSTAIN, YNS, KMAX, C)
IF (INS.LT.0) CALL PLOTIT (XSTAIN, YNS, NGKMAX, 0)
IF (INS.EQ.1001) GO TO 5
IF (INS.EQ.0)
IF (INS.EQ.1000)
IF (INTF.GT.0) CALL PLOTIT (XSTAIN, YNTH, KMAX, C)
IF (INTF.LT.0) CALL PLOTIT (XSTAIN, YNTH, NGKMAX, 0)
IF (INTF.LT.0) TH(NTH)
IF (INS.EQ.1002) GO TO 6
IF (INS.EQ.0)
IF (INS.EQ.1000)
IF (INSTH.GT.0) CALL PLOTIT (XSTAIN, YNSTH, KMAX, 0)
IF (INSTH.LT.0) CALL PLOTIT (XSTAIN, YNSTH, NGKMAX, 0)
IF (INS.EQ.1003) TH(NTH)
IF (ICS.EQ.0) GO TO 7
IF (ICS.EQ.1000)
IF (IQS.GT.0) CALL PLOTIT (XSTAIN, YQS, KMAX, C)
IF (IQS.LT.0) CALL PLOTIT (XSTAIN, YQS, NGKMAX, 0)
IF (IMS.EQ.0) GO TO 8
IF (IMS.EQ.1000)
IF (IMS.GT.0) CALL PLOTIT (XSTAIN, YMS, KMAX, C)
IF (IMS.LT.0) CALL PLOTIT (XSTAIN, YMS, NGKMAX, 0)
IF (IMT.EQ.0) GO TO 9
IF (IMT.EQ.1000)
IF (IMT.GT.0) CALL PLOTIT (XSTAIN, YMT, KMAX, 0)
IF (IMT.LT.0) CALL PLOTIT (XSTAIN, YMT, NGKMAX, 0)

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 SAT20960

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5      WRITE (6,1C06) TH(NTH)
      IF (IMSTH.EQ.0) GO TO 1211
      WRITE (6,1000)
      IF (IMSTH.GT.0) CALL PLCTIIT (XSTATN,YMSTH,KMAX,0)
      IF (IMSTH.LT.0) CALL PLCTIIT (XSTATN,YMSTH,NGKMAX,0)
      WRITE (6,1007) TH(NTH)
      IF (IU.EQ.0) GO TO 10
      WRITE (6,1000)
      IF (IU.GT.0) CALL FLCTIIT (XSTATN,YU,KMAX,0)
      IF (IU.LT.0) CALL FLCTIIT (XSTATN,YU,NGKMAX,C)
      WRITE (6,1010) TF(NTH)
      IF (IV.EQ.0) GO TO 11
      WRITE (6,1000)
      IF (IV.GT.0) CALL PLCTIIT (XSTATN,YV,KMAX,C)
      IF (IV.LT.0) CALL PLCTIIT (XSTATN,YV,NGKMAX,C)
      WRITE (6,1009) TH(NTH)
      IF (IW.EQ.0) GO TO 12
      WRITE (6,1000)
      IF (IW.GT.0) CALL PLOTIIT (XSTATN,YW,KMAX,0)
      IF (IW.LT.0) CALL PLOTIIT (XSTATN,YW,NGKMAX,0)
      WRITE (6,1008) TF(NTH)
      IF (IPHIS.EQ.0) GO TO 13
      WRITE (6,1000)
      IF (IPHIS.GT.0) CALL PLCTIIT (XSTATN,YPHIS,KMAX,0)
      IF (IPHIS.LT.0) CALL PLCTIIT (XSTATN,YPHIS,NGKMAX,0)
      WRITE (6,1011) TH(NTH)
      IF (IPHI.EQ.0) GO TO 14
      WRITE (6,1000)
      IF (IPHI.GT.0) CALL FLCTIIT (XSTATN,YPHI,KMAX,0)
      IF (IPHI.LT.0) CALL FLCTIIT (XSTATN,YPHI,NGKMAX,0)
      WRITE (6,1012) TH(NTH)
      IF (IPII.EQ.0) GO TO 21
      WRITE (6,1000)
      IF (IPII.GT.0) CALL PLCTIIT (XSTATN,YPHI,KMAX,0)
      IF (IPII.LT.0) CALL PLCTIIT (XSTATN,YPHI,NGKMAX,0)
      WRITE (6,1013) TH(NTH)
      RETURN
      IF (INS.EQ.0) GO TO 15
      WRITE (6,1000)
      IF (INS.GT.0) CALL PLOTIIT (XSTATN,YNS,KMAX,C)
      IF (INS.LT.0) CALL PLOTIIT (XSTATN,YNS,NGKMAX,0)
      WRITE (6,2001)
      IF (INTF.EQ.0) GO TO 16
      WRITE (6,1000)
      IF (INTF.GT.0) CALL FLCTIIT (XSTATN,YNTH,KMAX,C)
      IF (INTF.LT.0) CALL FLCTIIT (XSTATN,YNTH,NGKMAX,0)
      WRITE (6,2002)
      IF (INSTH.EQ.0) GO TO 17
  
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WRITE (6,1000)
IF (INSTH.GT.0) CALL PLOTIT (XSTATN,YNSTH,KMAX,0)
IF (INSTH.LT.0) CALL PLOTIT (XSTATN,YNSTH,NGKMAX,0)
WRITE (6,2003) GO TO 18
IF (ICS.EQ.0) GO TO 18
WRITE (6,1000)
IF (IQS.GT.0) CALL PLOTIT (XSTATN,YQS,KMAX,C)
IF (IQS.LT.0) CALL PLOTIT (XSTATN,YQS,NGKMAX,C)
WRITE (6,2004) GO TO 19
IF (IMS.EQ.0) GO TO 19
WRITE (6,1000)
IF (IMS.GT.0) CALL PLOTIT (XSTATN,YMS,KMAX,C)
IF (IMS.LT.0) CALL PLOTIT (XSTATN,YMS,NGKMAX,0)
WRITE (6,2005) GO TO 22
IF (IMTH.EQ.0) GO TO 22
WRITE (6,1000)
IF (IMTH.GT.0) CALL PLOTIT (XSTATN,YMTH,KMAX,C)
IF (IMTH.LT.0) CALL PLOTIT (XSTATN,YMTH,NGKMAX,0)
WRITE (6,2006) GC TO 231
IF (IMSTH.EQ.0) GC TO 231
WRITE (6,1000)
IF (IMSTH.GT.0) CALL PLOTIT (XSTATN,YMSTH,KMAX,0)
IF (IMSTH.LT.0) CALL PLOTIT (XSTATN,YMSTH,NGKMAX,0)
WRITE (6,2007) GO TO 23
IF (IU.EQ.0) GO TO 23
WRITE (6,1000)
IF (IU.GT.0) CALL PLOTIT (XSTATN,YU,KMAX,C)
IF (IU.LT.0) CALL PLOTIT (XSTATN,YU,NGKMAX,0)
WRITE (6,2010) GO TO 24
IF (IV.EQ.0) GO TO 24
WRITE (6,1000)
IF (IV.GT.0) CALL PLOTIT (XSTATN,YV,KMAX,C)
IF (IV.LT.0) CALL PLOTIT (XSTATN,YV,NGKMAX,C)
WRITE (6,2009) GO TO 25
IF (IW.EQ.0) GO TO 25
WRITE (6,1000)
IF (IW.GT.0) CALL PLOTIT (XSTATN,Yh,KMAX,0)
IF (IW.LT.0) CALL PLOTIT (XSTATN,Yh,NGKMAX,C)
WRITE (6,2008) GO TO 26
IF (IPHS.EQ.0) GO TO 26
WRITE (6,1000)
IF (IPHS.GT.0) CALL PLOTIT (XSTATN,YPHIS,KMAX,0)
IF (IPHS.LT.0) CALL PLOTIT (XSTATN,YPHIS,NGKMAX,0)
WRITE (6,2011) GO TO 27
IF (IPHIT.EQ.0) GO TO 27
WRITE (6,1000)
IF (IPHIT.GT.0) CALL PLOTIT (XSTATN,YPHIT,KMAX,0)
IF (IPHIT.LT.0) CALL PLOTIT (XSTATN,YPHIT,NGKMAX,0)

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WRITE (6,1000)
CALL FLCTIT (XSTATN,YDSTIF,NGKMAX,0)
IF (IBBSTF.EQ.0) GO TO 10
WRITE (6,1000)
CALL PLCTIT (XSTATN,YBBSTF,NGKMAX,0)
IF (ICDSTF.EQ.0) GO TO 1
WRITE (6,1000)
CALL FLCTIT (XSTATN,YDCSTF,NGKMAX,0)
IF (IPR.EQ.0) GO TO 11
WRITE (6,1000)
CALL PLCTIT (XSTATN,YPR,NGKMAX,0)
IF (IPS.EQ.0) GO TO 12
WRITE (6,1000)
CALL PLCTIT (XSTATN,YPS,NGKMAX,0)
IF (IPT.EQ.0) GO TO 13
WRITE (6,1000)
CALL PLCTIT (XSTATN,YPT,NGKMAX,0)
IF (ITT.EQ.0) GO TO 14
WRITE (6,1000)
CALL PLCTIT (XSTATN,YTT,NGKMAX,0)
IF (IMT.EQ.0) GO TO 15
WRITE (6,1000)
CALL PLCTIT (XSTATN,YMT,NGKMAX,0)
IF (IDT.EQ.0) GO TO 16
WRITE (6,1000)
CALL PLCTIT (XSTATN,YDTT,NGKMAX,0)
IF (ICMT.EQ.0) GO TO 17
WRITE (6,1000)
CALL PLCTIT (XSTATN,YDMT,NGKMAX,0)
WRITE (6,1000)
RETURN
*****
10CC FCRMAT ('D',T10,'RADIUS VS STATION')
10C1 FCRMAT ('O',T10,'GAMMA VS STATION')
10C2 FCRMAT ('O',T10,'OMEGA-S VS STATION')
10C4 FCRMAT ('O',T10,'OMEGA-THEA VS STATION')
10C5 FCRMAT ('O',T10,'DECMEGA-S VS STATION')

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AD-A035 911

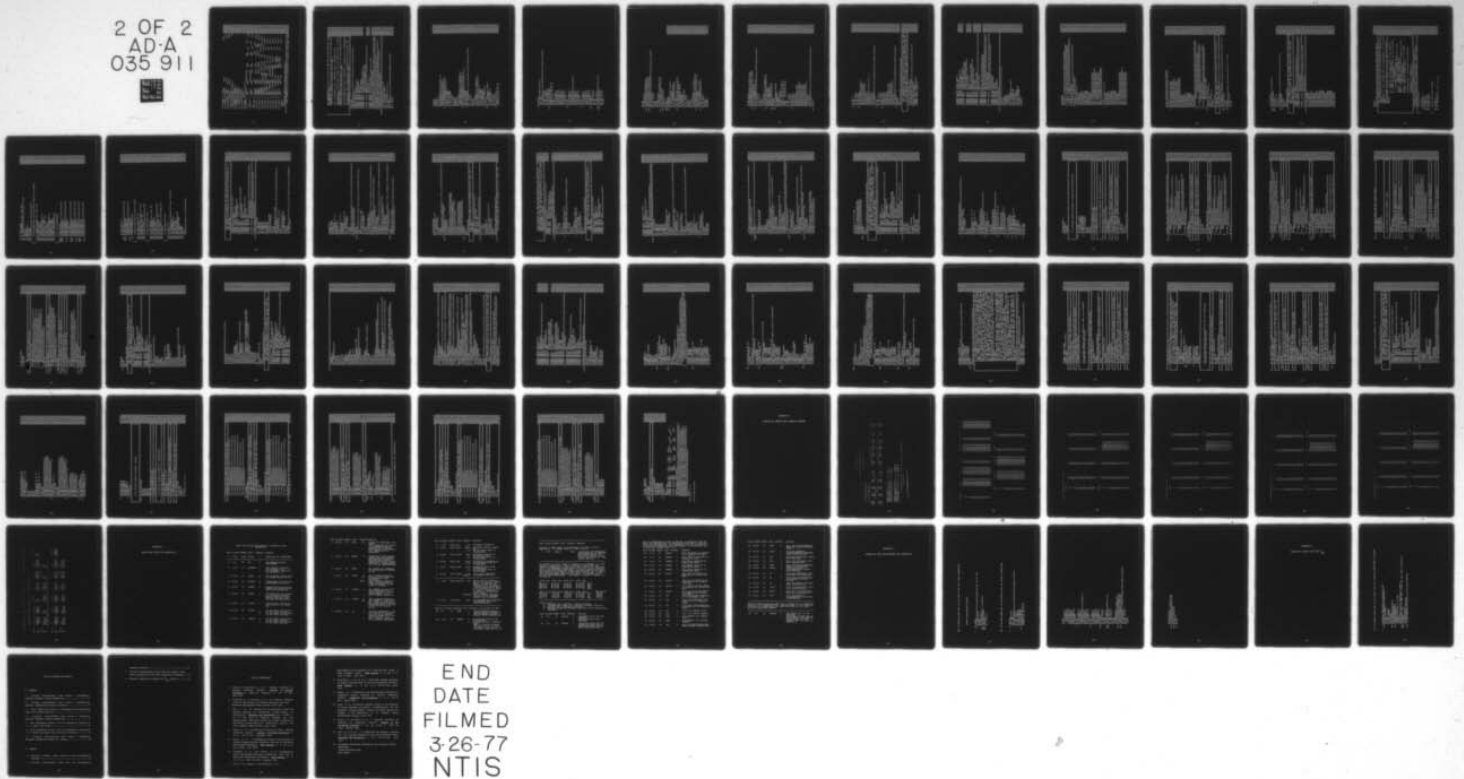
NAVAL POSTGRADUATE SCHOOL MONTEREY CALIF  
STATIC AND DYNAMIC BUCKLING OF SHALLOW SPHERICAL SHELLS SUBJECT--ETC(U)  
DEC 76 M D SHUTT

F/G 20/11

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C AND PANDD(K,MN) TO SET UP THE P, P-BAR AND P-HAT MATRICES GIVEN00001320
C BY EQUATIONS (30)*00C01330
C INTERNALLY, MATRICES DL, DG AND DF ARE SET UP FOR THE CALCULA-00001340
C TION OF X(I) GIVEN BY EQUATION (31A), WHERE00001350
C X(I) = DL*SMALL-L(I) + DG*SMALL-G(I) + DF*SMALL-F(I)00001360
C THE SPECIAL P MATRIX FOR A SHELL WITH AN INITIAL FCLE IS ALSO00001370
C COMPLETED HERE*00001380
C MATRICES ZF1M,ZF2M,ZF3M,ZF4M ARE SET UP FOR THE CALCULATION OF00001390
C Z(K+1) GIVEN BY EQUATION (31B), WHERE*00C01400
C Z(K+1)=ZF1M*SMALL-L(K) + ZF2M*X(K) + ZF3M*X(K-1) + ZF4M*SMALL-00001410
C F00001420
C IF THE SHELL HAS A FINAL POLE, THE MATRICES CLC,CL1,CL2 ARE00001430
C PREPARED FOR THE CALCULATION OF Z(K)*00001440
C *****00001450
C *****00001460
C *****00001470
C *****00001480
C *****00001490
C *****00C01500
C *****00C01510
C *****00C01520
C *****00C01530
C *****00001540
C *****00001550
C *****00001560
C *****00001570
C *****00001600
C *****00001610
C *****00001620
C *****00001640
C *****00C01650
C *****00001660
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C *****00001780
C *****00001790

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```

SUMA=0.
SUMB=0.
SUMC=0.
SUMA J=0.
L=1,4
SUMA=SUMA+C(I,L)*JAY(L,J)
SUMB=SUMB+C(I,L)*BEE(L,J)
SUMC=SUMC+CMEGI(I,L)*H(L,J)
4 PATA(I,J)=SUMA+UNIT(I,J)
3 PETA(I,J)=SUMB
PCTA(I,J)=SUMC
PCTA(I,J)=SUMJ
PCTA(I,J)=1,4
SUMCB=0.
SUMCA=0.
SUMC L=1,4
SUMCB=SUMCA+POTA(I,L)*PATA(L,J)
SUMCA=SUMCC+POTA(I,L)*PATA(L,J)
SUMCC=SUMCC+POTA(I,L)*C(L,J)
6 PCTR(I,J)=SUMOB+PJT A(I,J)+CAPL1(I,J)
5 PCCR(I,J)=SUMOC
PCCR(I,J)=1,4
CALL MATINV(DLL,4,PTR,4,DETERM,IPIVOT,INDEX,4,ISCALE)
SUMD=0.
SUME=0.
SUMD L=1,4
SUME=SUMD+DLL(I,L)*DGG(L,J)
7 PCCR(I,J,MN)=DLL(I,L)*CMEGI(L,J)
PCCR(I,J,MN)=SUMD
DF(I,J,MN)=SUME
I=1+KMAX*(MN-1)
1 PCTR(I,J,IJ)=PTR(I,J)
1C GC TO 2C
MN=MNINIT,MNMAX
IJ=IABSN(MN)
I=1+KMAX*(MN-1)
X(I,IJ)=0.
PCTR(I,J,IJ)=1,4
14 PCTR(I,J,IJ)=0.
IF(MN.GT.3) GO TO 11
IF(MN.GT.2) GO TO 50

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```

C IN FMATRX
CALL EFG(2,MN,Z0,Z2,Z3)
CALL ABC
CALL MATINV(A,4,G1,0,DETERM,IPIVGT,INDEX,4,ISCALE)
CC 901 II=1,4
CC 901 JJ=1,4
DCL(I,II,JJ,MN)=0.
CG(I,II,JJ,MN)=0.
CF(I,II,JJ,MN)=0.
IF(IN.GT.1) GO TO 13
IF(MN.GT.0) GO TO 13
MC=MN
CL(1,1,MN)=1.
CL(2,2,MN)=1.
CL(3,3,MN)=-3.
CL(4,4,MN)=-3.
CG(3,3,MN)=4.
DG(4,4,MN)=4.
CF(3,3,MN)=-1.
CF(4,4,MN)=-1.
GC TO SC2
13 M1=MN
CL(1,1,MN)=-3.
CL(2,2,MN)=1.
CL(3,3,MN)=1.
CL(4,4,MN)=1.
IF(N(M1)-LT.0)DL(2,2,MN)=-1.
CL(3,3,MN)=1.
CL(4,4,MN)=1.
CG(1,1,MN)=4.
CF(1,1,MN)=-1.
GC TO SC2
12 M2=MN
CL(1,1,MN)=1.
CL(2,2,MN)=1.
CL(3,3,MN)=1.
CL(4,4,MN)=-3.
CG(4,4,MN)=4.
CF(4,4,MN)=-1.
CCNT INUE II=1,4
CC 903 JJ=1,4
CTF=0.
CC 904 L=1,4
CTF=ITP+DF(I,I,L,MN)*A(L,JJ)
9C4 TL0(I,II,JJ)=ITP
9C5 II=1,4
CC 905 JJ=1,4
CTF=0.

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TTC=0.
CC 5C6 L=1,4 CLO(I,I,L)*C(L,JJ)
TTF=TTQ+CLO(I,I,L)*BEE(L,JJ)
TTC=TTQ+CLO(I,I,L)*BEE(L,JJ)
CL1(I,I,JJ)=DL(I,I,JJ,MN)-TTP
CL2(I,I,JJ)=DG(I,I,JJ,MN)-TTQ
CC 5C7 MATINV(CLL,4,GI,0,DETERM, IPIVOT, INDEX,4, ISCALE)
DC 507 I=1,4
DC 5C7 JJ=1,4
TTP=0.
TTC=C.
CC 5C8 L=1,4 CLI(I,I,L)*CLO(L,JJ)
TTF=TTQ+CLI(I,I,L)*CLO(L,JJ)
TTC=TTQ+CLI(I,I,L)*CLO(L,JJ)
CL(I,I,JJ,MN)=-TTP
CC 5C7 GC TO I
M2=MN
M3=MN
CC N1 NUE
CC N1 KLAST=KMAX
IF(IBC FN L, LT, 0) KLAST=KL
CC 23 K=2 KLAST
CC 23 MN=MNINIT, MNMAX
CALL EFG(K, MN, Z0, Z2, Z3)
CALL ABC
CALL PFANDD(K, MN, P, CEE, DST, X)
IF(IBC FN L, LT, 0) GC TO 30
DC 40 MN=MNINIT, MNMAX
IKL=MN*KMAX-1
JKL=KMAX*MN
CALL FJ(KMAX, MN)
CC 41 I=1,4
CC 41 J=1,4
SUMC=0.
SUMF=0.
SUMJ=0.
DC 42 L=1,4 CMEGL(I,L)*H(L,J)
SUMF=SUMP+(I,L)*K)*P(L,J,JKL)
SUMJ=SUMJ+CMEGL(I,L)*JAY(L,J)
42 PATA(I,J)=SUMO
PETA(I,J)=UNIT(I,J)-SUMF
41 PJTA(I,J)=SUMJ+CAPLL(I,J)
CC 43 I=1,4
CC 43 J=1,4
SUMCP=0.
SUMJP=0.
SUMCM=0.

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0000273C
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00003010
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00003100
00003110
00003120
00003130
00003140
00003150
00003160
00003170
00003180
00003190
00003200

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44 L=1,4
SUMOP=SUMOP+PATA(I,L)*PBTA(L,J)
SUMJP=SUMJP+PJTA(I,L)*P(L,J,JKL)
SUMCM=SUMCM-PATA(I,L)*P(L,J,IKL)
42 ZF1(I,J)=SUMOP-SUMJP
CALL MATINV(ZF1,4,ZF2,4,DETERM,IFIVOT,INDEX,4,ISCALE)
45 I=1,4
45 J=1,4
ZF2=0.
SZF4=0.
46 L=1,4
SZF3=SZF3+ZF1(I,L)*PATA(L,J)
SZF4=SZF4-ZF1(I,L)*CMEGL(L,J)
45 ZF2M(I,J,MN)=SZF3
45 ZF4M(I,J,MN)=SZF4
45 ZF1M(I,J)=ZF1(I,J)
45 ZF2M(I,J,MN)=ZF2(I,J)
45 CCNT INUE
45 RETL RN
45 MN=MN+INIT,MMAX
45 I=1,4
45 J=1,4
45 MN=ABS(N(MN))
45 NN=N(MN)
45 IF(NN.GT.3) GO TO 31
45 IF(NN.GT.2) GO TO 300
45 IF(NN.GT.1) GO TO 33
45 IF(NN.GT.0) GC TC 34
45 CC=MN
45 J=1,4
45 I=1,4
45 CLC(I,J)=0.
45 ZFPC(I,I)=1.
45 ZFFP(1,1)=1.
45 ZFFP(2,2)=P(3,1,IKL)
45 ZFFP(3,1)=P(3,2,IKL)+1.
45 ZFFP(3,2)=P(3,3,IKL)
45 ZFFP(3,3)=P(3,4,IKL)
45 ZFFP(4,1)=P(4,1,IKL)
45 ZFFP(4,2)=P(4,2,IKL)
45 ZFFP(4,3)=P(4,3,IKL)
45 ZFFP(4,4)=P(4,4,IKL)+1.
45 CLC(3,3)=1.
45 CLC(4,4)=1.
45 CALL MATINV(ZFPO,4,CLO,4,DETERM,IFIVOT,INDEX,4,ISCALE)
45 GC TO 31
45 ME=MN
3CC

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CCMCMN /IBL5/ IBCINL, IBCFNL
CCMCMN /IBL8/ LSTEP, ITR
CCMCMN /IBL12/ KMAX1, KMAX2, NCONV
CCMCMN /IBL13/ ITRMAX, LSMAX
CCMCMN /IBL3/ PR(99), PX(99), PT(99)
CCMCMN /IBL4/ ZF1M(4,4,99), ZF2M(4,4,99),
1 ZF3M(4,4,99), ZF4M(4,4,99)
CCMCMN /BL5/ TT(99), MT(99), DT(99), DMT(99)
CCMCMN /BL6/ SQE, ALOAD
CCMCMN /BL7/ DI, S1
CCMCMN /BL8/ R(500), GAM(500), DMT(500)
CCMCMN /BL9/ RFS(4,99), ELIS(4), GEES(4,99)
CCMCMN /BL11/ OMXI(500), PHEE, T0, T2
CCMCMN /BL12/ TDLI, TDEL
CCMCMN /BL14/ LAM2, LSD18, LSD19
CCMCMN /BL15/ NU, U1(99), V1(99), W1(99), V2(99), U2(99), W2(99), U3(99),
1 V3(99), W3(99)
CCMCMN /BL17/ DEL
CCMCMN /BL24/ DL(4,99), DG(4,4,99), DF(4,4,99)
CCMCMN /BL27/ BX3(99), BT3(99), BXT3(99), BE3(99)
CCMCMN /BL28/ EXX3(99), ET3(99), ETX3(99), EX3(99), ET3(99)
CCMCMN /BL29/ BXT1(99), BT1(99), BXT1(99), BE1(99),
1 BXT2(99), BE2(99)
1 CCMCMN /BL30/ EXX1(99), ET1(99), ETX1(99), EX1(99), ET1(99), EXX2(99),
1 ET2(99), ETX2(99), EX2(99), ET2(99)
CCMCMN /BL31/ DELSC, EX11(99)
CCMCMN /BL100/ TEEED, $DYNMC
CCMCMN /BL101/ DELSD
CCMCMN /BL102/ DELLOAD
CCMCMN /BL103/ MASS(500)
DIMENSION GEE(4)
C*****(A,B,C)=(-1.5*A+2.*B-.5*C)/CEL
RS=R(K)
RF=1./RS
GA=GAM(K)
CX=CMT(K)
L12=DI*LAM2
CALL BCB(K,BS,DBS,D,DD)
CALL PLCCAD(K,Z)
CALL TLCCAD(K,Z)
MASS=MASS(K)
LC 4 F=1, MNMAX
I2=K+1+(M-1)*KMAX2
IK1=IK-1
EN=A(N)
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CXX=-FCIFF( EXX2T, EXX2(M), EXX1(M) )
CETX=-FDIFF( ETX2T, ETX2(M), ETX1(M) )
GC TO 7
CBX=IDL I*( BX3(M)-BX1(M) )
CBEI=ICLI I*( BE3(M)-BE1(M) )
CCEI=ICLI I*( BX3(M)-BX1(M) )
CCEI=ICLI I*( ET3(M)-ET1(M) )
CCEI=ICLI I*( EX3(M)-EX1(M) )
CCEI=ICLI I*( EXX3(M)-EXX1(M) )
DET X=IDL I*( ETX3(M)-ETX1(M) )
BX2T=BX2(M)
BX1T=BX1(M)
BE2T=BE2(M)
BE1T=BE1(M)
EXX2T=EXX2(M)
ETX2T=ETX2(M)
EXX1T=EXX1(M)
ETX1T=ETX1(M)
GEE(1)=GEE(1)+ENR*DI*BS*(CBX+DBE+GA*DI*(BX2T-ET2T)+NU*(CBT+DBE)
1 GEE(2)=GEE(2)+OSE*(BS*(BX2T+BE2T+ETX2T)-ENR*(BX2T+ETX2T))*TDEL
2 (EXX2T+ETX2T)-ENR*(BX2T+ETX2T))*TDEL
1 GEE(3)=GEE(3)+OSE*(BS*(BX2T+BE2T+ETX2T)-DI*(ETX2T+EXX2T)
2 (CBX+DBE+GA*DI*(BX2T+BE2T+ETX2T))*TDEL
1 IF(K.GT.1) GO TO 10
2 IF(M.GT.1) ELIS(1)=0.0
5C CC 20 I=1,4
GEE(I,M)=GEE(I)
SUMX=0.
CC 21 J=1,4
C *** FLOWING CARD CAUSES A SPECIFIED BOUNDARY CCNDITION VALUE TC
C EXISTS ONLY FOR MODE 'C'.
C *** IF (M.NE.1) ELIS(J)=0.
21 SUMX=SUMX+DL(I,J,M)*ELIS(J)+DG(I,J,M)*GEE(J)+DF(I,J,M)*FFS(J,M)
2C GC TO 4
C IN FCRC
1C IF(K.NE.2)OR.(K.EQ.2.ANC.IBCINL.GE.0)) GC TC 501
CC 502 I=1,4
SUMX=0.

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RETURN
END
SUBROUTINE MATINV(A,N,B,M,DETERM,IPIVOT,INDEX,NMAX,ISCALE)
*****
THIS SUBROUTINE SOLVES THE MATRIX EQUATION AX=B, WHERE A IS
A SQUARE COEFFICIENT MATRIX AND B IS A MATRIX OF CCNSTANT VEC-
TORS.
A(INVERSE) IS ALSO OBTAINED AND THE DETERMINANT OF A IS AVAIL-
ABLE.
THE FOLLOWING MUST BE DIMENSIONED IN THE CALLING PROGRAM:
IPIVOT(N MAX), INDEX(N MAX,2), A(N MAX,N MAX), B(N MAX,N MAX)
WHERE:
A = NAME OF 2-DIMENSIONAL ARRAY TO BE INVERTED
N = CRDER OF A - 1<=N<=NMAX
B = NAME OF 2-DIMENSIONAL ARRAY TO BE MULTIPLIED
BY A(INVERSE)
M = NUMBER OF COLUMNS VECTORS IN B
IPIVOT = TEMPORARY STORAGE BLOCK
INDEX = TEMPORARY STORAGE BLOCK
NMAX = MAXIMUM ORDER OF A (AS DIMENSIONED IN THE
CALLING PROGRAM)
DETERM= VALUE OF DETERMINANT AS GIVEN BELOW
ISCALE = USED IN FORMULA BELOW
DETERMINANT(A) = (1C*18)** ISCALE*(DETERM)
A(INVERSE) IS STORED IN A
A(INVERSE)*B IS STORED IN B
*****
DIMENSION IPIVOT(N),A(NMAX,N),B(NMAX,M),INDEX(NMAX,2)
EQUIVALENCE (IROW,JRCW),(ICOLU,JCCLU), (AMAX,T,SKAP)
*****
INITIALIZATION
*****
ISCALE=C
5 R1=10.0**18
6 R2=1.0/R1
7 CC TERM=1.0
10 CC J=1,N
12 CC IF IPIVOT(J)=0
20 CC
23 CC
*****
SEARCH FOR PIVOT ELEMENT
4C AMAX=0.0
45 CC 105 J=1,N
5C IF (IPIVOT(J)-1) 60, 105, 60

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6C 100 K=I/N
7C IF (IPIVOT(K)-1) 80, 100, 740
8C IF (ABS(AMAX)-ABS(A{J,K})) 85, 10C, 100
9C CM=J
5C ICCLUM=K
5C AMAX=A(J,K)
1CC CONTINUE
1CE CCNTINUE
11C IF IPIVOT(ICCLUM)=IPIVCT(ICCLUM)+1
C INTERCHANGE ROWS TO PUT PIVOT ELEMENT ON DIAGCNAL
C
120 IF (IROW-ICCLUM) 140, 260, 140
14C DETERM=-DETERM
150 L=I,N
16C SWAP=A(IROW,L)
17C A(IROW,L)=A(ICCLUM,L)
20CC A(ICCLUM,L)=SWAP
21C IF (M) 260, 260, 210
22C L=L-1, M
23C SWAP=B(IROW,L)
24C B(IROW,L)=B(ICCLUM,L)
25C B(ICCLUM,L)=SWAP
26C INDEX(I,1)=IROW
27C INDEX(I,2)=ICCLUM
28C PIVCT=A(ICCLUM,ICCLUM)
C SCALE THE DETERMINANT
C
10CC PIVCTI=PIVOT
10C5 IF (ABS(DETERM)-R1) 1030, 1010, 1010
101C DETERM=DETERM/R1
101C ISCALE=ISCALE+1
102C IF (ABS(DETERM)-R1) 1060, 1020, 102C
102C DETERM=DETERM/R1
102C ISCALE=ISCALE+1
102C ISCALE=ISCALE
103C IF (ABS(DETERM)-R2) 1040, 1040, 1060
104C DETERM=DETERM*R1
104C ISCALE=ISCALE-1
105C IF (ABS(DETERM)-R2) 1050, 1050, 1060
105C DETERM=DETERM*R1
105C ISCALE=ISCALE-1
106C IF (ABS(PIVCTI)-R1) 109C, 1070, 107C
107C PIVCTI=PIVCTI/R1
107C ISCALE=ISCALE+1
108C IF (ABS(PIVOTI)-R1) 320, 1080, 1080
108C PIVCTI=PIVCTI/R1

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1050 ISCALE=ISCALE+1
1060 GC TO 320
1070 IF (ABS(PIVOTI)-R2) 200C, 2000, 320
1080 PIVCTI=PIVCTI+R1
1090 ISCALE=ISCALE-1
1100 IF (ABS(PIVOTI)-R2) 2010, 2010C, 320
1110 PIVCTI=PIVCTI+R1
1120 ISCALE=ISCALE-1
1130 DETERM=DETERM*PIVOTI
1140
1150 DIVIDE PIVCT ROW BY PIVCT ELEMENT
1160
1170 A(ICOLU, ICCLUM)=1.0
1180 DC 350 L=1, N
1190 A(ICOLU, L)=A(ICOLU, L)/PIVCT
1200 IF (M) 380, 380, 360
1210 DC 370 L=1, M
1220 B(ICOLU, L)=B(ICOLU, L)/PIVCT
1230
1240 REDUCE NON-PIVOT RCWS
1250
1260 DC 550 L1=1, N
1270 IF (L1-ICOLU) 400, 550, 400
1280 T=A(L1, ICOLU)
1290 A(L1, ICOLU)=0.0
1300 DC 450 L=1, N
1310 A(L1, L)=A(L1, L)-A(ICCLUM, L)*T
1320 IF (M) 550, 550, 460
1330 DC 500 L=1, M
1340 B(L1, L)=B(L1, L)-B(ICCLUM, L)*T
1350 CCNTINUE
1360
1370 INTERCHANGE COLUMNS
1380
1390 DC 710 I=1, N
1400 L=N+1-I
1410 IF (INDEX(L, 1)-INDEX(L, 2)) 630, 710, 630
1420 JFCW=INDEX(L, 1)
1430 JCCLUM=INDEX(L, 2)
1440 DC 705 K=1, N
1450 SWAP=A(K, JROW)
1460 A(K, JROW)=A(K, JCOLUMN)
1470 A(K, JCOLUMN)=SWAP
1480 CCNTINUE
1490 RETURN
1500 ENCL
1510 SUBROUTINE INLPGL (Z, PFIXB, PHITB)

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C *****
C THIS SUBROUTINE COMPUTES THE NCN-LINEAR TERMS BETA-SUB S;
C -SUB S-THETA, -SUB S-THETA, ETA-SUB S-S ANC -SUB THETA-S AT AN
C INITIAL POLE.
C *****
C DIMENSION Z(4,1), PHIXB(1), PHITB(1)
C CCMMCN /IBL1/ MNMAX
C CCMMCN /IBL3/ MO,M1,M2,M3
C CCMMCN /IBL12/ KMAX1,KMAX2,NCCNV
C CCMMCN /IBL13/ ITRMAX,LSMAX
C /IBLJ/ JUMP
C CCMMCN /BL5/ TT(55),EMT(99),DT(55),DMT(99)
C CCMMCN /BL6/ SOE,CSE,ALOAD
C CCMMCN /BL7/ DI,S1
C CCMMCN /BL11/ OMXI(200),PHEE,TO,T2
C CCMMCN /BL11A/ PHEN,T2N
C CCMMCN /BL17/ DEL
C CCMMCN /BL29/ BXT1(99),BXT1(99),BE1(99),BX2(99),BT2(99),
1 CCMMCN /BL30/ EXXI(99),ET1(99),EX1(99),ET1(99),EXX2(99),
1 CCMMCN /BL31/ EXX2(99),ET2(99),EX2(99),ET2(99)
C *****
C CC 1 MN=1,MNMAX
C BT1 (MN)=0.
C BXT1 (MN)=0.
C BE1 (MN)=0.
C ET1 (MN)=0.
C EXX1 (MN)=0.
C EXX1 (MN)=0.
1 IF (M1.EQ.0) RETURN
I2=I2+(M1-1)*KMAX2
I3=I2+1
I4=I3+1
IF (JUMP.EQ.2) GO TO 1000
PTEE=(1.5*Z(3,I2)-2.*Z(3,I3)+.5*Z(3,I4))/DEL+CMXI(1)*Z(1,I2)
BET=5*PHEE**2
IF (ITRMAX.EQ.1) BET=0.
I2=C.
IF (M2.EQ.0) GO TO 2
CALL BDB(1,B,DB,C,CC)
I2=I2+(M2-1)*KMAX2
I4=I3+1
I4=I3+1
I2=B*DI*((-1.5*Z(1,I2)+2.*Z(1,I3)-.5*Z(1,I4))/DEL+.5*SOE*BET)
C1=.5*PTEE*T2
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BX1(M2)=BET
BT1(M2)=-BET
EXT1(M2)=-BET
EXT1(M1)=Q1 GO TO 2
IF(M3.EQ.0) GO TO 2
EXT1(M3)=Q1
EXT1(M3)=-Q1
TC=0.
2 IF(MO.EQ.0) GO TO 3
EXT1(MO)=BET
BT1(MO)=BET
CALL BDE(I, B, DB, D, CC)
CALL TLCAD(1, Z)
I2=2+(MO-1)*KMAX2
I3=I2+1
I4=I3+1
TC=B*SI*((-1.5*Z(1, I2)+2.*Z(1, I3)-.5*Z(1, I4))/DEL+CMXI(1)*Z(3, I2)
1+.5*SOE*BET)-TT(MO)*ALCAD
3 EXXI(M1)=PTEE*(T0+.5*T2)
RETLRN
1CCC CCNTINUE
PTEE=(1.5*Z(3, I2)-2.*Z(3, I3)+.5*Z(3, I4))/DEL+CMXI(1)*Z(1, I2)
T2=C.
IF(M2.EQ.0) GO TO 1002
CALL BDE(I, B, DB, D, CC)
I2=2+(M2-1)*KMAX2
I3=I2+1
I4=I3+1
IHXB(KMAX+1)
PFX2=PHXB(2*KMAX+1)
PFX2=(1.5*Z(3, I2-KMAX2)-2.*Z(3, I3-KMAX2)+.5*Z(3, I4-KMAX2))/DEL+
1CMXI(1)*Z(1, I2-KMAX2)
BX1(M2)=.5*(PHEE*(PTEE+2.*PFX1)-PTEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX1(M2)=0.
BT1(M2)=-BX1(M2)
T2=B*D1*((-1.5*Z(1, I2)+2.*Z(1, I3)-.5*Z(1, I4))/DEL+.5*SOE*BX1(M2))
M2L=M2-1
EXT1(M2L)=PTEE*(PTEN+PHX2)+PHX1*PTEN
IF(ITRMAX.EQ.1) BX1(M2L)=0.
BT1(M2L)=-BX1(M2L)
EXT1(M2L)=BX1(M2L)
T2N=B*D1*((-1.5*Z(1, I2-KMAX2)+2.*Z(1, I3-KMAX2)-.5*Z(1, I4-KMAX2))
1 /CEL+.5*SOE*BX1(M2L))
1002 TC=C.
IF(MO.EQ.0) GO TO 1003
EXT1(MO)=.5*(PHEE*(PTEE+2.*PHX1)+PTEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX1(MO)=0.

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BT1(M0)=BX1(M0)
CALL BCR(1,B,DB,0,DC)
CALL TLCCAD(1,Z)
I2=2+(MC-1)*KMAX2
I3=I2+1
I4=I3+1
I5=I4+1
I6=I5+1
I7=I6+1
I8=I7+1
I9=I8+1
I10=I9+1
I11=I10+1
I12=I11+1
I13=I12+1
I14=I13+1
I15=I14+1
I16=I15+1
I17=I16+1
I18=I17+1
I19=I18+1
I20=I19+1
I21=I20+1
I22=I21+1
I23=I22+1
I24=I23+1
I25=I24+1
I26=I25+1
I27=I26+1
I28=I27+1
I29=I28+1
I30=I29+1
I31=I30+1
I32=I31+1
I33=I32+1
I34=I33+1
I35=I34+1
I36=I35+1
I37=I36+1
I38=I37+1
I39=I38+1
I40=I39+1
I41=I40+1
I42=I41+1
I43=I42+1
I44=I43+1
I45=I44+1
I46=I45+1
I47=I46+1
I48=I47+1
I49=I48+1
I50=I49+1
I51=I50+1
I52=I51+1
I53=I52+1
I54=I53+1
I55=I54+1
I56=I55+1
I57=I56+1
I58=I57+1
I59=I58+1
I60=I59+1
I61=I60+1
I62=I61+1
I63=I62+1
I64=I63+1
I65=I64+1
I66=I65+1
I67=I66+1
I68=I67+1
I69=I68+1
I70=I69+1
I71=I70+1
I72=I71+1
I73=I72+1
I74=I73+1
I75=I74+1
I76=I75+1
I77=I76+1
I78=I77+1
I79=I78+1
I80=I79+1
I81=I80+1
I82=I81+1
I83=I82+1
I84=I83+1
I85=I84+1
I86=I85+1
I87=I86+1
I88=I87+1
I89=I88+1
I90=I89+1
I91=I90+1
I92=I91+1
I93=I92+1
I94=I93+1
I95=I94+1
I96=I95+1
I97=I96+1
I98=I97+1
I99=I98+1
I100=I99+1

10C3 *****
BT1(M0)=BX1(M0)
CALL BCR(1,B,DB,0,DC)
CALL TLCCAD(1,Z)
I2=2+(MC-1)*KMAX2
I3=I2+1
I4=I3+1
I5=I4+1
I6=I5+1
I7=I6+1
I8=I7+1
I9=I8+1
I10=I9+1
I11=I10+1
I12=I11+1
I13=I12+1
I14=I13+1
I15=I14+1
I16=I15+1
I17=I16+1
I18=I17+1
I19=I18+1
I20=I19+1
I21=I20+1
I22=I21+1
I23=I22+1
I24=I23+1
I25=I24+1
I26=I25+1
I27=I26+1
I28=I27+1
I29=I28+1
I30=I29+1
I31=I30+1
I32=I31+1
I33=I32+1
I34=I33+1
I35=I34+1
I36=I35+1
I37=I36+1
I38=I37+1
I39=I38+1
I40=I39+1
I41=I40+1
I42=I41+1
I43=I42+1
I44=I43+1
I45=I44+1
I46=I45+1
I47=I46+1
I48=I47+1
I49=I48+1
I50=I49+1
I51=I50+1
I52=I51+1
I53=I52+1
I54=I53+1
I55=I54+1
I56=I55+1
I57=I56+1
I58=I57+1
I59=I58+1
I60=I59+1
I61=I60+1
I62=I61+1
I63=I62+1
I64=I63+1
I65=I64+1
I66=I65+1
I67=I66+1
I68=I67+1
I69=I68+1
I70=I69+1
I71=I70+1
I72=I71+1
I73=I72+1
I74=I73+1
I75=I74+1
I76=I75+1
I77=I76+1
I78=I77+1
I79=I78+1
I80=I79+1
I81=I80+1
I82=I81+1
I83=I82+1
I84=I83+1
I85=I84+1
I86=I85+1
I87=I86+1
I88=I87+1
I89=I88+1
I90=I89+1
I91=I90+1
I92=I91+1
I93=I92+1
I94=I93+1
I95=I94+1
I96=I95+1
I97=I96+1
I98=I97+1
I99=I98+1
I100=I99+1

10C1 *****
BT1(M0)=BX1(M0)
CALL BCR(1,B,DB,0,DC)
CALL TLCCAD(1,Z)
I2=2+(MC-1)*KMAX2
I3=I2+1
I4=I3+1
I5=I4+1
I6=I5+1
I7=I6+1
I8=I7+1
I9=I8+1
I10=I9+1
I11=I10+1
I12=I11+1
I13=I12+1
I14=I13+1
I15=I14+1
I16=I15+1
I17=I16+1
I18=I17+1
I19=I18+1
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I26=I25+1
I27=I26+1
I28=I27+1
I29=I28+1
I30=I29+1
I31=I30+1
I32=I31+1
I33=I32+1
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I35=I34+1
I36=I35+1
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I38=I37+1
I39=I38+1
I40=I39+1
I41=I40+1
I42=I41+1
I43=I42+1
I44=I43+1
I45=I44+1
I46=I45+1
I47=I46+1
I48=I47+1
I49=I48+1
I50=I49+1
I51=I50+1
I52=I51+1
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I54=I53+1
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I67=I66+1
I68=I67+1
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I70=I69+1
I71=I70+1
I72=I71+1
I73=I72+1
I74=I73+1
I75=I74+1
I76=I75+1
I77=I76+1
I78=I77+1
I79=I78+1
I80=I79+1
I81=I80+1
I82=I81+1
I83=I82+1
I84=I83+1
I85=I84+1
I86=I85+1
I87=I86+1
I88=I87+1
I89=I88+1
I90=I89+1
I91=I90+1
I92=I91+1
I93=I92+1
I94=I93+1
I95=I94+1
I96=I95+1
I97=I96+1
I98=I97+1
I99=I98+1
I100=I99+1

*****
SUBROUTINE ABC
*****
THIS SUBROUTINE COMPUTES THE ELEMENTS OF THE A, BEE, ANC C
*****
MATRICES.
*****
COMMON /BL1/ A(4,4),BEE(4,4),C(4,4)
COMMON /BL2/ TDEL
COMMON /BL3/ DEL
COMMON /BL4/ E(4,4),F(4,4),G(4,4)
*****
C2=2./DEL
DO 1 I=1,4
DO 2 J=1,4
DEIJ=D2*(I,J)
FIJ=F(I,J)
BEE(I,J)=-2.*DEIJ+TDEL*(I,J)
C(I,J)=DEIJ-FIJ
1 / (I,J)=DEIJ+FIJ
RETURN
END
SUBROUTINE PAND(K,MN,P,DEE,DST,X)
*****
THIS SUBROUTINE COMPUTES THE ELEMENTS OF THE P, P-BAR, AND
*****

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C *****
C P-HAT MATRICES FOR EACH MEDICIAN STATIGN K AND FOURIER MCCE MN* 00008400
C THESE MATRICES ARE COMPUTED AND SAVED BECAUSE THEY DC NCT * 00008410
C CHANGE DURING EITHER THE ITERATION PROCEDURE CR THE LOAC INCRE - 00008420
C MENT PROCEDURE - AS THEY ARE A FUNCTION CF THE SPELL'S INITIAL * 00008430
C GEOMETRY AND STIFFNESS. ***** 00008440
C ***** 00008450
C DIMENSION P(4,4,1),CEE(4,4,1),DST(4,4,1),X(4,1) 00008460
C COMMON /IBL4/ KMAX, KL BEE(4,4),C(4,4,99), 00008470
C COMMON /BL1/ A(4,4),ZF2M(4,4,99),ZF4M(4,4,99), 00008480
C COMMON /BL4/ ZF3M(4,4,99),ZP(4,4,99),INDEX(4,2),X2(4) *****
C ***** 00008510
C DIMENSION TM(4,4),***** 00008520
C INL=K+KMAX*(MN-1) ***** 00008530
C KLI=IKL-1 ***** 00008540
C CC 1 I=1,4 ***** 00008550
C CC 1 J=1,4 ***** 00008560
C SUM=0. ***** 00008570
C CC 2 L=1,4 ***** 00008580
C SUM=SUM+C(I,L)*P(L,J,KLI) ***** 00008590
C TM(I,J)=BEE(I,J)-SUM ***** 00008600
C CALL MATINV(TM,4,X2,0,DETERM,IPIVCT,INDEX,4,ISCALE) ***** 00008610
C DC 5 I=1,4 ***** 00008620
C DC 5 J=1,4 ***** 00008630
C SUMA=0. ***** 00008640
C CC 6 L=1,4 ***** 00008650
C SUMA=SUMC+TM(I,L)*A(L,J) ***** 00008660
C SUMC=SUMC+TM(I,L)*C(L,J) ***** 00008670
C P(I,J,IKL)=SUMA ***** 00008680
C DEE(I,J,IKL)=TM(I,J) ***** 00008690
C DST(I,J,IKL)=SUMC ***** 00008700
C RETURN ***** 00008710
C ***** 00008720
C ***** 00008730
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C ***** 00010000

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CCMCON /BL6/ SOE,CSE,ALOAD
CCMCON /BL7/ DI,S1
CCMCON /BL11/ OMXI(500),PHEE,TO,T2
CCMCON /BL11A/ PHEN,T2N
CCMCON /BL17/ DEL
CCMCON /BL27/ BX3(99),BI3(99),BXI3(99),BE2(99)
CCMCON /BL28/ EXX3(99),ETI3(99),ETX3(99),EX3(99),ET3(99)
C*****
DC 1 MN=1,MNMAX
EX3 (MN)=0.
ETI3 (MN)=0.
EXI3 (MN)=0.
ETX3 (MN)=0.
ETX3 (MN)=0.
EXX3 (MN)=0.
CALL BC8(KMAX,B,DB,D,DB)
IF (M1.EQ.0) RETURN
KM=KMAX1+(M1-1)*KMAX2
KM1=KM-1
KM2=KM-2
PFEE=-1.5*Z(3,KM)-2.*Z(3,KM1)+.5*Z(3,KM2))/DEL+CMXI(KMAX)*Z(1,KM)
IF (JUMP.EQ.2) GO TO 1000
BET=.5*PFEE#2
IF (ITRMAX.EQ.1) BET=0.
T2=C.
IF (M2.EQ.0) GO TO 2
KM=KMAX1+(M2-1)*KMAX2
KM1=KM-1
KM2=KM-2
T2=B#01*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+.5*SCE*BET)
C1=.5*PFEE#T2
EXI3 (M2)=-BET
ETI3 (M2)=BET
ETX3 (M1)=Q1
IF (M3.EQ.0) GO TO 2
EXX3 (M3)=Q1
ETX3 (M3)=-Q1
TC=0.
2 IF (M0.EQ.0) GO TO 3
CALL TLCAD(KMAX,Z)
KM1=KMAX1+(M0-1)*KMAX2
KM2=KM-1
KM3=KM-2
EXI3 (M0)=BET

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00C09360
00009370
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00C09500
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00C09550
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00009620
00C09630
00009640
00009650
00C09660
00009670
00009680
00C09690
00C09700
00009710
00009720
00009730
00C09740
00C09750
00009760
00C09770
00009780
00009790
00C09800
00C09810
00009820
00009830

TC=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+GMXI(KMAX))*
1 Z(3,KM)+.5*SOE*BE1)-TT(MO)*ALOAD
3 EX3(M1)=PHEE*(TO+.5*T2)
RETURN
C*****
10CC CCNT INUE
T2=C.
IF(M2.EQ.0) GO TO 1002
KA=KMAX1+(M2-1)*KMAX2
KA1=KM-1
KA2=KM-2
J=KMAX*2
I=J+KMAX
XB(J)
PFX1=PHIXB(I)
PFX2=PHIXB(I)
PFEN=-1.5*Z(3,KM-KMAX2)-2.*Z(3,KM1-KMAX2)+.5*Z(3,KM2-KMAX2))/DEL
1+CMXI(KMAX)*Z(1,KM-KMAX2)
BX3(M2)=.5*(PHEE*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX3(M2)=0.
BT3(M2)=-BX3(M2)
BAT3(M2)=BX3(M2)
M2L=M2-1
BX3(M2L)=PHEE*(PHEN+PHX2)+PFX1*PFEN
IF(ITRMAX.EQ.1) BX3(M2L)=0.
BT3(M2L)=-BX3(M2L)
BAT3(M2L)=-BX3(M2L)
T2=B*DI*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+.5*SCE*BX3(M2))
T2A=B*DI*((1.5*Z(1,KM-KMAX2)-2.*Z(1,KM1-KMAX2)+.5*Z(1,KM2-KMAX2))
1 /DEL+.5*SOE*BX3(M2L))
10C2 TC=C.
IF(MO.EQ.0) GO TO 1003
CALL TLCAD(KMAX,Z)
KA=KMAX1+(MO-1)*KMAX2
KA1=KM-1
KA2=KM-2
EX3(MO)=.5*(PHEE*(PHEE+2.*PHX1)+PFEN*(PHEN+2.*PHX2))
IF(ITRMAX.EQ.1) BX3(MO)=0.
BT3(MO)=BX3(MO)
TC=B*SI*((1.5*Z(1,KM)-2.*Z(1,KM1)+.5*Z(1,KM2))/DEL+CMXI(KMAX))*
Z(3,KM)+.5*SOE*BX3(MO))-TT(MO)*ALOAD
10C3 IF(ITRMAX.EQ.1) GO TO 1001
PFSS=PHEN+PHX1
PFSP=PHEN+PHX2
MIL=M1-1
EXX3(M1)=PHSS*TO+.5*(PHSS*T2+PHSP*T2N)
ETX3(M1)=PHSS*TO-.5*(PHSS*T2+PHSP*T2N)
ETX3(M1)=.5*(PHSS*T2+PHSP*T2N)
ETX3(M1L)=.5*(-PHSS*T2+PHSS*T2N)

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00010070
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00010180
00010190
00010200
00010210
00010220
00010230
00010240
00010250
00010260
00010270
00010280
00010290
00010300
00010310

IF(M3.EQ.0) GO TO 1001
MEL=M3-1
MAX3(M3)=.5*(PHSS*T2-PHSP*T2N)
EXT3(M3)=.5*(PHSS*T2N+PHSP*T2)
ETX3(M3)=.5*(-PHSS*T2+PHSP*T2N)
ETX3(M3)=.5*(-PHSS*T2-PHSS*T2N)
CCONTINUE
1001 RETURN
C*****
SUBROUTINE PHIBET(K,Z,IS,JS,ID,JC,PHIXB,PHIIB)
C*****
C THIS SUBROUTINE CALCULATES THE PHIS AND CARRIES CLT THE BETA
C MULTIPLYING AND SUMMATION PROCEDURE FOR COMPUTING THE BETA
C NON-LINEAR TERMS FOR A GIVEN MERIDIONAL STATION K. THE ARRAYS
C IS, JS, ID, JC, PHIXB, MAXC, MAXSY ARE PREPARED IN SUB-
C ROUTINE MCODES AND USED HERE.
C*****
DIMENSION Z(4,1), IS(99,1), JS(99,1), ID(99,1), JD(99,1), PHIXB(1),
1 PHIB(1)
COMMON /IBL1/ MNMAX
COMMON /IBL2/ N(99), MNINIT
COMMON /IBL4/ KMAX, KL, MAXD(99), MAXS(59), MAXSY(59), IJS(59)
COMMON /IBL7/ MNMAXO, KMAX1, KMAX2, NCONV
COMMON /IBL12/ KMAX1, KMAX2, ITRMAX, LSMAX
COMMON /IBL13/ JUMP
COMMON /IBLJ/ SOE, CSE, ALGAD
COMMON /BL6/ R(500), GAM(500), OMT(500)
COMMON /BL8/ PHIX(99), PHIT(99), PHI(99)
COMMON /BL10/ OMXI(500), PHEE, TO, T2
COMMON /BL11/ TDLI, TDEL
COMMON /BL12/ NU, UI(99), V1(99), V2(59), U2(95), U3(59),
COMMON /BL15/ V3(95), W3(99)
COMMON /BL27/ BX3(99), BXT3(99), BEX(55)
COMMON /BLPHS/ PHX(99), PHT(99)
C*****
CX=CMXI(K)
CT=CMT(K)
RRA=1./R(K)
GA=GAM(K)
KF2=K+2
CC 1 N=1, MNMAXO
EN=N(M)
IK=KP2+(M-1)*KMAX2
U3(M)=Z(1,IK)
V3(M)=Z(2,IK)
W3(M)=Z(3,IK)
PHIX(M)=-1/CL1*(W3(M)-W1(M))+CX*L2(M)
C*****

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1 PHI(M)=EN*W2(M)*RRA+V2(M)*CT
  IF(ITRMAX.EQ.1) RETURN
  IF(JUMP.EQ.2) GO TO 1111
  LC 5 P=1, MNMAX
  SMC=0.
  SMT=0.
  SMR=0.
  IF(N(M).EQ.0) GO TO 20
  MAXL=MAXS(M)
  IF(MAXL.EQ.0) GO TO 2
  DO 3 L=1, MAXL
  I=IS(L,M)
  J=JS(L,M)
  SMC=SMO+PHIX(I)*PHIX(J)
  SMT=SMT+PHIT(I)*PHIT(J)
  SMR=SMR+PHIX(I)*PHIX(J)+PHIX(J)*PHIT(I)
  SMC=SMF+PHI(I)*PHI(J)
  SMC=SMAXC(M)
  IF(MAXL.EQ.0) GO TO 4
  LC 5 L=1, MAXL
  I=IC(L,M)
  J=JC(L,M)
  SMC=SMO+PHIX(I)*PHIX(J)
  SMT=SMT+PHIT(I)*PHIT(J)
  SMR=SMR+PHIX(I)*PHIT(J)+PHIX(J)*PHIT(I)
  SMC=SMF+PHI(I)*PHI(J)
  IF(MAXSY(M).EQ.0) GC TO 10
  I=IJS(M)
  J=JCS(M)
  SMC=SMO+PHIX(I)**2/2.
  SMT=SMT-PHIT(I)**2/2.
  SMR=(SMR+PHIX(I))*PHIT(I)
  SMC=SMF-PHI(I)**2/2.
  GC TO 1C
  LC 21 L=1, MNMAX
  SMC=SMO+PHIX(L)**2
  SMT=SMT+PHIT(L)**2
  SMF=SMF+PHI(L)**2
  IF(N.GT.MNMAXC) GC TO 11
  SMC=SMO+PHIX(M)**2
  BEE3(M)=SMC*.5
  BEE2(M)=SMT*.5
  BEE1(M)=SMF*.5
  BEE(M)=0.
  GC TO 9
  EX3(M)=SMT
  BE3(M)=SMT

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00010320
00010330
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00010370
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00010390
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00010690
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00010780
00010790

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C ***** EXECUTE BELOW IF J=1 IN DIFFERENCE COMBINATIONS *****
C ***** SMC=(PHIX(I)*PHIX(I)+PHX(I)*PHX(I))*PHIX(I)*PHIX(I)*2.0 *****
C ***** SMT=(PHIT(I)*PHIT(I)+PHT(I)*PHT(I))*PHIT(I)*PHIT(I)*2.0 *****
C ***** SMR=(SMR+(PHIX(I)*PHIX(I)+PHX(I)*PHX(I))*PHIT(I)*PHIT(I) *****
C ***** SMF=(SMF+(PHIT(I)*PHIT(I)+PHT(I)*PHT(I))*PHIX(I)*PHIX(I)*2.0 *****
C ***** CCN=CCN *****
C ***** TEST FOR PRESENCE OF SAME-INDEX COMBINATION *****
C ***** 44 IF(MAXSY(M).EQ.0) GO TO 410 *****
C ***** SET UP INDICES AND CCMPLE SUMS *****
C ***** I=IJS(M) *****
C ***** I=I-1 *****
C ***** SMC=SMO+PHIX(I)*2/2. *****
C ***** SMT=-PHIT(I)*PHIX(I)*2/2. *****
C ***** SMR=SMR+PHIX(I)*PHIT(I)*2/2. *****
C ***** SMF=SMF-PHI(I)*2/2. *****
C ***** GC TO 410 *****
C ***** THIS SECTION HANDLES CASES WHERE MODE 0 IS INCLUDED *****
C ***** SMC=SMO+PHIX(L)*2 *****
C ***** SMT=SMT+PHIT(L)*2 *****
C ***** SMR=SMR+(PHIX(L)*PHIX(L)+PHIT(L)*PHIT(L))*PHIX(L) *****
C ***** SMF=SMF+PHIX(M)*2 *****
C ***** SMC=SMC+PHIX(M)*PHIX(M) *****
C ***** SMT=SMT+PHIT(I)*PHIT(I)+2.0*PHIT(I) *****
C ***** SMR=SMR+(PHIX(L)*PHIX(L)+PHX(L)*PHX(L))*PHIT(L)*2.0 *****
C ***** SMF=SMF+PHIX(L)*PHIX(L)+PHX(L)*PHX(L)*PHIT(L)+1 *****
C ***** SMC=SMC+PHIX(L)*PHIX(L)+PHX(L)*PHX(L)*PHIT(L)-1 *****
C *****

```

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00011760
00011770
00011780
00011790
00011800
00011810
00011820
00011830
00011840
00011850
00011860
00011870
00011880
00011890
00011900
00011910
00011920
00011930
00011940
00011950
00011960
00011970
00011980
00011990
00012000
00012010
00012020
00012030
00012040
00012050
00012060
00012070
00012080
00012090
00012100
00012110
00012120
00012130
00012140
00012150
00012160
00012170
00012180
00012190
00012200
00012210
00012220
00012230

```

```

C *** CCMPLE BETA TERMS FOR THIS SPECIAL CASE ***
C *** SMO*.5 ***
C *** B13(M)=SMO*.5 ***
C *** B13(M)=SMF*.5 ***
C *** B13(I)=SMR*.5 ***
C *** CC TO 45 ***
C *** THIS SECTION HANDLES ASYMMETRIC MODES ***
C *** MF=M+1 ***
C *** IC1 MAXL=MAXS(MP) ***
C *** TEST FCR PRESENCE CF SUMMATION COMBINATICS ***
C *** IF (MAXL.EQ.0) GO TO 102 ***
C *** SET UP INDICES FOR SUMMATION COMBINATIONS ***
C *** DC 103 L=1,MAXL ***
C *** I=IS(L,MP) ***
C *** J=JS(L,MP) ***
C *** JJ=J-1 ***
C *** TEST FCR MCDE 1 AND COMPILE SUMS ***
C *** IF (I.EQ.1) GO TO 103 ***
C *** SMC=SMO+PHX(I)*PHX(JJ)+PHX(JJ)*PHX(II)+ ***
C *** SPT=SMI+PHI(I)*PHI(II)+PHI(II)*PHI(JJ)+PHI(JJ)*PHI(I)+ ***
C *** SMR=SMR+PHX(I)*PHI(II)+PHI(II)*PHX(JJ)+PHI(JJ)*PHI(I)+ ***
C *** (PHI(I)*PHI(II)+PHI(II)*PHI(JJ)+PHI(JJ)*PHI(I)-PHI(I)*PHI(II)-PHI(I)*PHI(II)) ***
C *** SMF=SMF+PHI(I)*PHI(II)+PHI(JJ)*PHI(II) ***
C *** CCNTINUE ***
C *** TEST FOR PRESENCE OF DIFFERENCE COMBINATICS ***
C *** IC2 MAXL=MAXD(MP) ***
C *** IF (MAXL.EQ.0) GO TO 1C4 ***
C *** SET UP INDICES FOR DIFFERENCE COMBINATICS ***
C ***
00012240
00012250
00012260
00012270
00012280
00012290
00012300
00012310
00012320
00012330
00012340
00012350
00012360
00012370
00012380
00012390
00012400
00012410
00012420
00012430
00012440
00012450
00012460
00012470
00012480
00012490
00012500
00012510
00012520
00012530
00012540
00012550
00012560
00012570
00012580
00012590
00012600
00012610
00012620
00012630
00012640
00012650
00012660
00012670
00012680
00012690
00012700
00012710

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```

BEZ(M)=SMF
CCONTINUE
ENCL
SLE ROUTINE HJ(K,MN)
*****
THIS SUBROUTINE COMPUTES THE ELEMENTS OF THE H AND JAY
MATRICES FOR BOTH FOUNDARIES OF THE SPELL
*****
REAL L2,LAM2,LSDIN, LSD18,JAY,NU
CCOMMON /IBL2/,N(99),MNINIT
CCOMMON /IBL4/,KMAX,KL
CCOMMON /IBL8/,GAM(500),OMI(500)
CCOMMON /BL11/,OMXI(500),PHEE,I0,I2
CCOMMON /BL14/,LAM2,LSD18,LSDIN
CCOMMON /BL15/,NU,UI(99),VI(99),W1(99),W2(99),U3(99),
1
CCOMMON /BL17/,DEL
CCOMMON /BL20/,DEOMX(500)
CCOMMON /BL23/,JAY(4,4),H(4,4)
EQUIVALENCE(L2,LAM2)
*****
CALL BCE(K,B,DB,U,DD)
YAF=1
IF(K.EQ.1.GR.K.EQ.KMAX)YAH=2.
CI=(1.-NU)
GA=GAM(K)
CX=CMXI(K)
RA=NR(K)
ENR=EN(MN)
REG=0.
IF(YAF.EQ.2.) REG=1.
CI=CMT(K)
CXI=3.*CMXI(K)-OMI(K)
CXI=3.*CMXI(K)-CMXI(K)
CL=C*L2*D1*ENR
F(1,1)=8
F(1,2)=0.
F(1,3)=C.
F(1,4)=C.
F(2,1)=0.
F(2,2)=8*D1/2.+L2*D*D1/8.*OTX**2*REG
F(2,3)=CL/2.*OTX*REG
F(2,4)=0.
F(3,1)=0.
F(3,2)=CL*YAH/4.
ENR2=ENR**2

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00013200
00013210
00013220
00013230
00013240
00013250
00013260
00013270
00013280
00013290
00013300
00013310
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00013330
00013340
00013350
00013360
00013370
00013380
00013390
00013400
00013410
00013420
00013430
00013440
00013450
00013460
00013470
00013480
00013490
00013500
00013510
00013520
00013530
00013540
00013550
00013560
00013570
00013580
00013590
00013600
00013610
00013620
00013630
00013640
00013650
00013660
00013670

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F(3,3)=L2*D*DI*(YAH*ENR2+(1.+NU)*GA**2)
GA2=GA**2
F(3,4)=L2
F(4,1)=0.
F(4,2)=C.
F(4,3)=-1.
F(4,4)=C.
JAY(1,1)=NU*GA*B
JAY(1,2)=NU*B*ENR
JAY(1,3)=B*(OX+NU*CT)
JAY(1,4)=0.
JAY(2,1)=-B*D1*ENR/2.-DL/8.*OXT*CTX*REG
JAY(2,2)=-GA**H(2,2)
JAY(2,3)=-GA**H(2,3)
JAY(2,4)=0.
JAY(3,1)=-L2*D*DI*((1.+NU)*GA2*OX+ENR2/4.*CXT*YAH)
JAY(3,2)=-GA*DL/2.*{2.*CT*(1.+NU)+OXT/2.*YAH}
JAY(3,3)=-L2*D*DI*((1.+NU+YAH)*GA*ENR2
JAY(3,4)=L2*D1*GA
JAY(4,1)=OX
JAY(4,2)=0.
JAY(4,3)=0.
JAY(4,4)=0.
CC 1 I=1,4
CC 1 J=1,4
1 H(I,J)=F(I,J)/2./DEL
ENR
END
SLEROUTINE EFG(K,MN,ZC,Z2,Z3)
C** THIS SUBROUTINE PREPARES THE ELEMENTS CF THE E, F, AND G
C** FOR EACH MERIDIAN STATION K AND FOR EACH FCURIER MCCE, MN.
C** INFLICIT LCGICAL*1 ($), LAM2, LSD18, LSDIN, MASS, MAS
REAL NU, N, Z0(4,1), Z2(4,1), Z3(4,1)
DIMENSION /BL2/NN(99), MNINIT
COMMON /BL8/ R(50C), GAM(50C), GMT(500)
COMMON /BL11/ OMXI(500), PHEE, IO, I2
COMMON /BL14/ LAM2, LSD18, LSDIN
COMMON /BL15/ NU, UI(99), VI(99), W1(99), W2(99), W3(99), U2(99), U3(99),
1 U4(99), V2(99), V3(99), W4(99), U5(99), V5(99)
COMMON /BL20/ DEOMX(500)
COMMON /BL25/ E(4,4), F(4,4), G(4,4)
COMMON /BL100/ TEEC, $DYNMC
COMMON /BL101/ DELSD
COMMON /BL102/ DELLOAD
COMMON /BL103/ MASS(500)
00013680
00013690
00013700
00013710
00013720
00013730
00013740
00013750
00013760
00013770
00013780
00013790
00013800
00013810
00013820
00013830
00013840
00013850
00013860
00013870
00013880
00013890
00013900
00013910
00013920
00013930
00013940
00013950
00013960
00013970
00013980
00013990
00014000
00014010
00014020
00014030
00014040
00014050
00014060
00014070
00014080
00014090
00014100
00014110
00014120
00014130
00014140
00014150

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CCMMGN /IBL3/ MO,M1,M2,M3
CCMMGN /IBL4/ KMAX,KL,IBCFNL
CCMMGN /IBL5/ IBCINL,MAXD(99),MAXS(59),MAXSY(99),IJS(99)
CCMMGN /IBL7/ MNMAXO, LSTEP, ITR
CCMMGN /IBL8/ LSTEP, ITR
CCMMGN /IBL10/ IIFREQ,NT,FMX
CCMMGN /IBL12/ KMAX1,KMAX2,ACGNV
CCMMGN /IBLJ/ JUMP
1 CCMMGN /BL5/ ZFIM(4,4,59),ZF2M(4,4,99),
CCMMGN /BL6/ ZFIM(4,4,59),ZF4M(4,4,99),
CCMMGN /BL7/ TT(99),MT(99),DT(99),DMT(99)
CCMMGN /BL8/ SQE,S1
CCMMGN /BL10/ R(500),GAM(500),CMT(500)
CCMMGN /BL11/ PHIX(59),PHIT(99),PHI(99)
CCMMGN /BL11A/ OMXI(500),PHEE,T0,T2
CCMMGN /BL12/ PHEN,T2N
CCMMGN /BL14/ TDLI,DEL
CCMMGN /BL15/ LAM2,LSD18,LSCIN
1 CCMMGN /BL17/ NU,U1(99),V1(99),W1(99),V2(99),U2(99),W2(99),U3(99),
CCMMGN /BL17/ V3(99),W3(99)
CCMMGN /BL19/ DEL
CCMMGN /BL20/ TH(36)
CCMMGN /BL27/ DEOMX(500)
CCMMGN /BL31/ BX3(59),BT3(99),BXT3(99),BE3(59)
CCMMGN /BL32/ DELSQ,EXT1(99)
CCMMGN /BL100/ TKN,ELAST,CHAR,SIGC
CCMMGN /BL101/ TEEG,$DYNMC
CCMMGN /BL102/ DELCAD
CCMMGN /BL103/ MASS(500)
CCMMGN /BL110/ TX(99),TTH(99),TXT(99),MTH(55),MTH(99),MXT(55),
1 CCMMGN /BL111/ QS(99)
CCMMGN /BL111/ ABZ,ABZ0,ABZN,ABZ3,DD2
C*****
CALL BCR(K,BS,DB,CS,DD)
M1=M1-1
M2=M2-1
IF(K.EQ.KMAX) GO TC 301
LL 202 MN=1,MNMAXO
V1(MN)=L2(MN)
V1(MN)=V2(MN)
W1(MN)=W2(MN)
I1=I3+(MN-1)*KMAX2
I2=I3-1
V2(MN)=Z(1,I3)
V2(MN)=Z(2,I3)
W2(MN)=Z(3,I3)

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00015120
00015130
00015140
00015150
00015160
00015170
00015180
00015190

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00015220
00015230
00015240
00015250
00015260
00015270
00015280
00015290
00015300
00015310
00015320
00015330
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00015350
00015360
00015370
00015380
00015390
00015400
00015410
00015420
00015430
00015440
00015450
00015460
00015470
00015480
00015490
00015500
00015510
00015520
00015530
00015540
00015550
00015560
00015570
00015580
00015590

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```

2C3 IF(MO.EQ.0) GO TO 206
I3=3+(MC-1)*KMAX2
I4=I3+1
CALL TLQAD(I,Z)
TX(MO)=BS*SI*(2.*Z(1,I3)-.5*Z(1,I4))/DEL+OMXI(1)*Z(3,I3-1))*ABZ
1
TTF(MO)=TX(MO)
MTF(MO)=MX(MO)
IF(N2.EC.0) GO TO 205
I3=3+(M2-1)*KMAX2
I4=I3+1
TX(M2)=BS*DI*(2.*Z(1,I3)-.5*Z(1,I4))/DEL
TTF(M2)=TX(M2)
MTF(M2)=MX(M2)
TTF(M2)=TX(M2)
MTF(M2)=MX(M2)
MXT(M2)=MX(M2)
IF(JUMP.EQ.1) GO TO 205
TX(M2L)=BS*DI*(2.*Z(1,I3-KMAX2)-.5*Z(1,I4-KMAX2))/DEL
TTF(M2L)=TX(M2L)
MTF(M2L)=MX(M2L)
MXT(M2L)=MX(M2L)
REFLRN
2C5 CCN TINUE MN=1,MNMAXC
3C1 L1(MN)=L2(MN)
V1(MN)=V2(MN)
W1(MN)=W2(MN)
FFIX(MN)=0.
PFI(MN)=0.
FK1(MN)=0.
IK=KMAX1+(MN-1)*KMAX2
M>(MN)=Z(4,IK)*ABZ3
MTF(MN)=0.
CS(MN)=C.
TX(MN)=C.
TTF(MN)=0.
TTF(MN)=0.
IF(M1.EC.0) GO TO 303
CALL FNLPC(LZ,PHIXB,PHITB)
PFI(M1)=PHEE*ABZC
PFI(M1)=PHEE*ABZC
IF(JUMP.EQ.1) GO TO 1002
PFI(M1L)=PHEN*ABZC
PFI(M1L)=PHIX(M1L)
00016080
00016090
00016100
00016110
00016120
00016130
00016140
00016150
00016160
00016170
00016180
00016190
00016200
00016210
00016220
00016230
00016240
00016250
00016260
00016270
00016280
00016290
00016300
00016310
00016320
00016330
00016340
00016350
00016360
00016370
00016380
00016390
00016400
00016410
00016420
00016430
00016440
00016450
00016460
00016470
00016480
00016490
00016500
00016510
00016520
00016530
00016540
00016550

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10C2 CCNTINUE
      II=KMAX+(M1-1)*KMAX2
      IF I=II+1
      IA I=II-1
      GAK=GAM(KL)
      CALL BCB(KL,BS,DB,CS,DD)
      PHIXX=Z(3,II)*TDLI+OMXI(KL)*Z(1,II)
      PHITT=Z(3,II)/R(KL)*Z(2,II)
      PSI=(Z(2,II)*Z(1,II)-DS*DC2*(PHITT/R(KL))+PHIXX)
      CS(MI)=SI*GOTKN*LCAC-DS*DI*(-PHIXX/R(KL)-GAK*(CMXI(KL)
1 *GAK)+CI*MT(MI)*ALCAC-DS*DI*(TDLI-GAK*Z(3,II))/R(KL)+GAK*(CMXI(KL)
2 (KL))*PHI+(-Z(3,IMI)*TDLI-GAK*Z(3,II))/R(KL)+GAK*(CMXI(KL)
3 (KL))*OMT(KL))*Z(2,II)+CMT(KL)*(Z(2,IMI)-Z(2,IMI))*TDLI)*.5)
4 /CEL
      IF(MO.EQ.0) GO TO 304
      TX(MO)=TO*ABZ
      TTH(MO)=TO*ABZ
      MTF(MO)=MX(MO)
3C4 IF(M2.EQ.0) GO TO 305
      TX(M2)=T2*ABZ
      TTT(M2)=-T2*ABZ
      TTT(M2)=T2*ABZ
      MTF(M2)=-MX(M2)
      MXT(M2)=MX(M2)
      IF(JUMP.EQ.1) GO TC 305
      TX(M2L)=T2N*ABZ
      TTT(M2L)=-TX(M2L)
      TTT(M2L)=-TX(M2L)
      MTF(M2L)=-MX(M2L)
      MXT(M2L)=-MX(M2L)
      GO TO 305
3C3 IF(MO.EQ.0) GO TO 306
      IKM=KMAX+(MO-1)*KMAX2
      IA I=IKM-1
      CALL TLCAD(KMAX,Z)
      TX(MO)=BS*SI*(-2.*Z(1,IKM)+.5*Z(1,IMI))/CEL+CMXI(KMAX)*Z(3,IKM+1)
1 *ABZ-TT(MC)*ABZ*ALCAD
      TTF(MO)=TX(MO)
      IF(M2.EQ.0) GO TO 3C5
      IA I=IKM-1
      TX(M2)=BS*DI*(-2.*Z(1,IKM)+.5*Z(1,IMI))/CEL
      TTT(M2)=TX(M2)*ABZ
      TTT(M2)=-TX(M2)
      MTF(M2)=-MX(M2)

```

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00016560
00016570
00016580
00016590
00016600
00016610
00016620
00016630
00016640
00016650
00016660
00016670
00016680
00016690
00016700
00016710
00016720
00016730
00016740
00016750
00016760
00016770
00016780
00016790
00016800
00016810
00016820
00016830
00016840
00016850
00016860
00016870
00016880
00016890
00016900
00016910
00016920
00016930
00016940
00016950
00016960
00016970
00016980
00016990
00017000
00017010
00017020
00017030

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00C17040
00017050
00017060
00017070
00017080
00017090
00017100
00017110
00017120
00017130
00017140
00017150
00017160
00017170
00017180
00017190
00017200
00017210
00017220
00017230
00017240
00017250
00017260
00017270
00017280
00017290
00017300
00017310
00017320
00017330
00017340
00017350
00017360
00017370
00017380
00017390
00017400
00017410
00017420
00017430
00017440
00017450
00017460
00017470
00017480
00017490
00017500
00017510

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MXT(M2) = MX(M2) TC 305  
IF(JUMP.EQ.1) GO TO 305  
T>(M2L)=BS\*DI\*(-2.\*Z(1,IKM-KMAX2)+.5\*Z(1,IM1-KMAX2))/CEL  
TTF(M2L)=-TX(M2L)\*ABZ  
TTF(M2L)=-TX(M2L)  
MXT(M2L)=-MX(M2L)  
MXT(M2L)=-MX(M2L)  
RETURN  
305  
END  
SUBROUTINE MODES (IS,JS,JD,P,X,ZC,Z2,Z3,CEE,DST)  
\* THIS SUBROUTINE ARRAYS THAT DEFINE THE SETS OF INDICES  
\* IN THE COMBINATION OF THE FIRST FOURIER TERMS IS  
\* MINED. EACH MODE IS CALLED A FOURIER INDEX AND THE LOCATION OF EACH MODE IS STORED IN THE  
\* REACHED. EACH MODE IS CALLED A FOURIER INDEX AND THE LOCATION OF EACH MODE IS STORED IN THE  
\* ALL OTHER FOURIER INDICES TO SEE IF THE LOCATION OF EACH MODE IS STORED IN THE  
\* IF IT DOES, THE LOCATION OF EACH MODE IS STORED IN THE  
\* BINARIES ARE STORED IN TWO SPECIAL 2-DIMENSIONAL ARRAYS, I AND INDEX  
\* JD. THE ARGUMENT IS THE NUMBER OF INDICES OF THE NEW INDEX  
\* ALSO GIVE THE VALUE OF THE NEW INDEX. IF A NEW FOURIER TERM HAS  
\* PROGRAM THAT MATCHES THE NEW INDEX, THEN A NEW FOURIER TERM HAS  
\* BEEN GENERATED AND WILL BE CONSIDERED IN THE NEXT ITERATION FOR  
\* SOLUTION.  
\* THE VARIABLE MAXD STORES THE TOTAL NUMBER OF SUCH COMBINATIONS  
\* FOR EACH VALUE OF THE FOURIER INDEX. IN A SIMILAR MANNER, EACH  
\* INDEX IS ADDED TO THE RESULT IS STORED IN THE 2-DIMENSIONAL ARRAY  
\* IS AND JS. IN THE SAME MANNER AS WAS DONE FOR THE CF SUMMATION  
\* CASE, THE VARIABLE MAXS STORES THE TOTAL NUMBER OF  
\* COMBINATIONS FOR EACH VALUE OF THE FOURIER INDEX. INDEX IS ADDED  
\* A SPECIAL ROUTINE HANDLES THE 2-DIMENSIONAL ARRAY IJS STORES THE  
\* AND SUBTRACTED FROM ITSELF. AND THE SERIES OF PRODUCTS THAT MAKE UP THE  
\* TOTAL NUMBER OF SUCH COMBINATIONS. THE VARIABLE MAXSY STORES THE  
\* WITH THIS PROCEDURE, THE SERIES OF PRODUCTS THAT MAKE UP THE  
\* BETA'S AND ALPHA'S CONTAINING ZERO TERM, AND THE SPECIFICALLY CE-  
\* CARRIED OUT IN PHIBET(K) AND TEAETA(K) OVER SPECIFICALLY CE-  
\* FINED LIMITS.  
\* DIMENSION P(4,4),JSD(4,4),X(4,1),ZC(4,1),Z2(4,1),  
1Z(4,1),IS(99,1),JS(99,1),ID(99,1),JD(99,1)  
COMMON /IBL1/ MNMAX  
COMMON /IBL2/ N(95),MNINIT  
COMMON /IBL7/ MNMAXC,MAXD(99),MAXS(99),MAXSY(99),IJS(99)

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00017520
00017530
00017540
00017550
00017560
00017570
00017580
00017590
00017600
00017610
00017620
00017630
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00017650
00017660
00017670
00017680
00017690
00017700
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00017900
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00017960
00017970
00017980
00017990

COMMON /IBL9/ MAXM
7/IELJ/ JUMP
*****
CETERMINE IF NEED FCR MCOAL COUPLING EXISTS
IF(MAXM.EQ.1) RETURN
SEE IF ENOUGH NEW MODES HAVE ALREADY BEEN GENERATED
IF(MNINIT.GT.MAXM) RETURN
*****
THIS SECTION HANDLES MODES GENERATED FROM THE DIFFERENCE
COMBINATIONS OF EXISTING MODES
*****
SET UP INITIAL LOCP FCR DIFFERENCE COMBINATIONS
DC 1 MN=1,MNMAXO,JUMP
NPN=N(MN)
NNS=MN
IF(MNINIT.GT.MN) NNS=MNINIT
SET UP SECCND LOOP ← TC SUBTRACT PRESENT MCEE FROM ALL CTFER
MCCES
*****
CC 1 MM=NNS,MNMAXC,JUMP
NPN=N(MM)
CREATE DIFFERENCE
NTEST=IABS(NMN-NMM)
SET UP 3RD LOOP - TC CCMPARE DIFFERENCE WITH ALL CTFER MODES
CC 2 MMFT=1,MNMAX,JUMP
IF WE SATISFY HERE, MODE EXISTS, GC TO INCREMENT -MAXC-
IF(NTEST.EQ.N(MMFT)) GC TO 10
CCNT INUE
2
*****
IF WE MAKE IT TO HERE, WE HAVE GENERATED A NEW MODE
*****
CC WE WANT ANY MORE NEW MODES
*****

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C *** SET LP THIRD LOOP -- TC COMPARE SUM WITH ALL OTHER MCDES *** 00018480
C *** CC 302 MMFT=1, MNMAX JUMP *** 00018490
C *** IF WE SATISFY HERE, MODE EXISTS, GC TO INCREMENT -MAXS- CR *** 00018500
C *** -MAXSY-) *** 00018520
C *** IF(NTTEST.EQ.N(MMFT)) GC TO 310 *** 00018530
C *** 3C2 CC CONTINUE *** 00018550
C *** IF WE MAKE IT TO HERE, WE HAVE GENERATED A NEW MODE *** 00018570
C *** CC WE WANT ANY MORE NEW MODES *** 00018580
C *** IF(ICORFL.EQ.1) GC TO 301 *** 00018590
C *** IF(MNMAX.GE.MAXM) GO TO 301 *** 00018600
C *** INCREMENT -MNMAX- AND ESTABLISH NEW MODE NUMBER *** 00018620
C *** MNMAX=MNMAX+JUMP *** 00018630
C *** N(MNMAX)=NTTEST *** 00018640
C *** IF (JUMP.GT.1) N(MNMAX-1)=-NTTEST *** 00018650
C *** MMFT=MNMAX *** 00018660
C *** IF(MNMAX.GE.MAXM) ICORFL=1 *** 00018670
C *** IF MCDE WAS ADDED TO ITSELF, GO TO -MAXSY AND IJS- SECTION *** 00018680
C *** 31C IF(MN.EQ.NM) GC TO 360 *** 00018700
C *** MAKE ENTRIES IN -LOCS-, -IS- AND -JS- *** 00018720
C *** LCCS=MAXS(MMFT)+1 *** 00018730
C *** MAXS(MMFT)=LOCS *** 00018740
C *** IJS(LOCS,MMFT)=MN *** 00018750
C *** GC TO 301 *** 00018760
C *** SEE IF THE SUM OF THE MCDE WITH ITSELF WAS THE 0-TH MCDE *** 00018770
C *** 3C3 IF(MN.EQ.C) GO TO 301 *** 00018790
C *** IF HERE, IT WASN-T, MAKE ENTRIES IN -MAXSY- AND -IJS- *** 00018800
C *** MAXSY(MMFT)=1 *** 00018820
C *** IJS(MMFT)=MN *** 00018830
C *** CC CONTINUE *** 00018840
C *** MNINIT=MNMAXG+JUMP *** 00018850
C *** IF(ICORFL.GT.0) IPASS=IPASS+1 *** 00018860
C *** 3C1 *** 00018870
C *** *** 00018880
C *** *** 00018890
C *** *** 00018910
C *** *** 00018920
C *** *** 00018930
C *** *** 00018950
C *** *** 00018950

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```

IF(IPASS.LT.2.AND.MNINIT.LE.MNMAX) CALL PMATRIX (P,X,ZC,Z2,Z3,CEE,
1DST)
IF RETURN
ENCL
SLROUTINE TEAETA(K,Z,IS,JS,ID,JC)
C***** THIS SUBROUTINE CALCULATES THE INPLANE FORCES AND CARRIES CUT
C***** THIS SUBROUTINE AND SUMMATION PROCEDURE FOR COMPUTING THE ETA
C***** ACN-LINEAR TERMS FOR A GIVEN MERIDIONAL STATION K. THE ARRAYS
C***** IS, JS, ID, JS, MAXS, MAXC, MAXSY PREFARED IN SUBRCUTINE
C***** MODES ARE USED HERE
C***** REAL NU, MT
C***** DIMENSION Z(4,1), IS(99,1), JS(99,1), ID(99,1), JC(99,1)
C***** COMMON /IBL1/ MNMAX
C***** COMMON /IBL2/ N(99), MNINIT
C***** COMMON /IBL7/ MNMAXO, MAXD(99), MAXS(99), MAXSY(99), IJS(99)
C***** COMMON /IBL8/ LSTEP, ITR
C***** COMMON /IBL13/ ITRMAX, LSMAX
5 /IBLJ/ JUMP
C***** COMMON /BL5/ TT(99), MT(99), DT(99), DMT(99)
C***** COMMON /BL6/ SOE, CSE, ALOAD
C***** COMMON /BL7/ DI, SCCL
C***** COMMON /BL8/ R(500), GAM(500), DMT(500)
C***** COMMON /BL10/ PHIX(99), PHT(99), PHI(99)
C***** COMMON /BL11/ OMXI(500), PHEE, TO, T2
C***** COMMON /BL12/ TDLI, TDEL
C***** COMMON /BL15/ NU, UI(99), VI(99), W1(99), V2(99), U2(99), W2(99), U3(99),
C***** /BL27/ BX3(99), BT3(99), BX1(99), BE2(99)
C***** COMMON /BL28/ EXX3(99), ETX3(99), ETX3(99), EX3(99), ET3(99)
C***** COMMON /BLPHS/ PHX(99), PHT(99)
C***** DIMENSION TX(99), TTH(99), TTX(99)
C***** RRA=1./R(K)
C***** GA=GAM(K)
C***** CX=CMX(K)
C***** CT=CMT(K)
C***** CALL BCE(K,BS,DB,CS,DD)
C***** DC I = I, MNMAXO
C***** PHIX(M)=PHIX(M)+PHX(M)
C***** PHT(M)=PHT(M)+PHT(M)
C***** EN=N(M)
C***** CALL TLGAD(K,Z)
C***** TTS=TT(M)*ALOAD
C***** EX=(U3(M)-UI(M))*TDLI+OX*W2(M)+CSE*(BX3(M)+EE3(M))
C***** ET=EN #V2(M)*RRA+GA*U2(M)+OT*W2(M)+OSE*(BT2(M)+BE3(M))
C***** EXT=.5*(TDLI*(V3(M)-VI(M))-EN #U2(M)*RRA-GA*V2(M))+CSE*EXT3(M)
00018960
00018970
00018980
00018990
00019000
00019010
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00019370
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00019390
00019400
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TX(N)=BS*(EX+NU*EI)-TIS
TTH(M)=BS*(ET+NU*EX)-TTS
1 IF(JUMP.EQ.2) GO TC 1111
CC 9 N=1,MNMAX
SSMF=0.
SSMV=0.
SSME=0.
SSMT=0.
SSNF=0.
IF(N(M).EQ.0) GO TC 20
IF(MAXL=MAXS(N)) GO TO 2
CC 3 L=1,MAXL
J=JS(L,M)
SSMF=SMF+TX(I)*PHIX(J)+TX(J)*PHIX(I)
SSMV=SMS+TTH(I)(J)+TTH(J)(J)*PHIT(I)
SSME=SME-PHIX(I)*TX(I)(J)-PHIT(J)(J)*TXI(I)
SSMT=SMN+TX(I)*PHI(J)+TX(J)*PHI(I)
SSNF=SMX+TTH(I)*PHI(J)+TTH(J)*PHI(I)
3 IF(MAXL.EQ.0) GO TO 4
CC 5 L=1,MAXL
J=JL(L,M)
SSMF=SMF+TX(I)*PHIX(J)+TX(J)*PHIX(I)
SSMV=SMS-TTH(I)(J)+TTH(J)(J)*PHIT(I)
SSME=SME-PHIX(I)*TX(I)(J)+PHIX(J)(J)*TXI(I)
SSMT=SMN-TTH(I)*PHI(J)+TTH(J)*PHI(I)
5 IF(MAXSY(M).EQ.0) GO TC 10
J=JS(M)
SSMF=SMF+TX(I)*PHIX(I)
SSMV=SMS+TTH(I)(J)*PHIT(I)
SSME=SME-PHIX(I)*TXI(I)
SSMT=SMN+TX(I)*PHI(I)
SSNF=SMF+TTH(I)*PHI(I)
CC 21 L=1,MNMAXO
SSMF=SMF+TX(L)*PHIX(L)
21 IF(M.GT.MNMAXO) GO TO 10
SSNF=SMF+TX(M)*PHIX(M)

```



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C***          00020400
C   CCMPLE SUMS FOR SYMMETRIC SUM COMBINATIONAL MODES          *
C***          00020410
C   SMF=SMF+TX(I)*PHIX(J)+TX(I)*PHIX(I)-PHIX(I)*TX(JJ)      *
C***          00020420
C   SPS=SMS+TTH(I)*PHIX(J)+TTH(J)*PHIT(I)+PHIT(I)*TTH(JJ)  *
C***          00020440
C   SMV=SMV-PHIT(I)*PHIT(J)+PHIT(I)*PHIT(I)*TX(JJ)         *
C***          00020450
C   SPE=SME+PHIX(I)*PHIX(J)+PHIX(I)*PHIX(I)*TX(JJ)         *
C***          00020470
C   SPN=SMN+TX(I)*PHI(J)+TX(I)*PHI(I)*TX(JJ)                *
C***          00020490
C   SPT=SMT+TTH(I)*PHI(J)+TTH(J)*PHI(I)*TTH(JJ)            *
C***          00020510
C   CCNTINUE
C   43 MAXL=MAXD(M)
C   42 TEST FOR PRESENCE OF SYMMETRIC DIFFERENCE COMBINATIONS
C***          00020560
C   IF (MAXL.EQ.0) GO TO 44
C***          00020580
C   SET UP COUPLING MODES - INDICES AND TEST FOR MODE 1
C***          00020600
C   DC 45 L=1,MAXL
C   1 IC(L,M)
C   1 J=JC(L,M)
C   1 J=J-1
C   1 IF (J.EQ.1) GO TO 442
C***          00020610
C   CCMPLE SUMS FOR SYMMETRIC DIFFERENCE COMBINATIONS
C***          00020620
C   SMF=SMF+TX(I)*PHIX(J)+TX(I)*PHIX(I)+PHIX(I)*TX(JJ)
C***          00020630
C   SPS=SMS-TTH(I)*PHI(J)+TTH(J)*PHIT(I)-PHIT(I)*TTH(JJ)
C***          00020640
C   SMV=SMV+PHIT(I)*PHIT(J)+PHIT(I)*PHIT(I)*TX(JJ)
C***          00020650
C   SPE=SME-PHIX(I)*PHIX(J)+PHIX(I)*PHIX(I)*TX(JJ)
C***          00020660
C   SPN=SMN-TX(I)*PHI(J)+TX(I)*PHI(I)*TX(JJ)
C***          00020670
C   SPT=SMT-TTH(I)*PHI(J)+TTH(J)*PHI(I)*TTH(JJ)
C***          00020680
C   GC TO 45
C***          00020690
C   EXECUTE BELOW IF J=1 IN DIFF-COMB. (OR I=1 IN SUM COMB)
C***          00020700
C   44
C   45

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C***442 SMF=SMF+(PHIX(I))*TX(I)+PHIX(I))*TX(I))*2.C
C***442 SPS=SPS+(PHIT(I))*TTF(I)+PHIT(I))*TTF(I))*2.C
C***442 SME=SME+(PHIX(I))*TX(I)+PHIX(I))*TX(I))*2.C
C***442 SMN=SMN+(PHI(I))*PHI(I)+PHI(I))*PHI(I))*2.C
C***442 SMT=SMT+(PHI(I))*TTH(I)+PHI(I))*TTH(I))*2.C
C***442 CCNTINUE
C***442 TEST FOR PRESENCE OF SAME-INDEX COMBINATIONS
C***442 IF (MAXSY(M).EQ.0) GO TO 410
C***442 SET UP INDICES AND CCMPFILE SUMS
C***442 I=IJS(M)
C***442 II=I-1
C***442 SMF=SMF+PHIX(I)*PHIX(I)-PHIX(I))*PHIX(I))*TX(I)
C***442 SPS=SPS+TTH(I)*PHIT(I)+PHIT(I))*PHIT(I))*TTF(I)
C***442 SME=SME+PHIX(I)*TX(I)+PHIX(I))*PHIX(I))*TX(I)
C***442 SMN=SMN+PHI(I)*PHI(I)+PHI(I))*PHI(I))*PHI(I)
C***442 SMT=SMT+TTH(I)*PHI(I)+PHI(I))*PHI(I))*TTH(I)
C***442 GO TO 410
C***442 FERE WE HANDLE CASES WHERE N(M)=0
C***442 CC 421 L=1,MNMAXO
C***442 SMF=SMF+TX(L)*PHIX(L)
C***442 SMV=SMV+TX(L)*PHIT(L)
C***442 CC 422 L=3,MNMAXO,2
C***442 LL=L-1
C***442 SPS=SPS+PHIT(LL)*TTH(LL)+PHIT(LL))*TTH(LL)
C***442 SME=SME+PHIX(LL)*TX(LL)+PHIX(LL))*TX(LL)
C***442 SMN=SMN+PHI(LL)*PHI(LL)+PHI(LL))*PHI(LL)
C***442 SMT=SMT+PHI(LL)*TTH(LL)+PHI(LL))*TTH(LL)
C***442 CCNTINUE
C***442 SMF=SMF+PHIX(I)
C***442 SPS=SPS+TTH(I)*PHIT(I)+PHIT(I))*PHIT(I))*2.0
C***442 SME=SME+TX(I)*PHIX(I)+PHIX(I))*PHIX(I))*2.0
C***442 SMN=SMN+TX(I)*PHI(I)+PHI(I))*PHI(I))*2.0
C***442 SMT=SMT+TTH(I)*PHI(I)+PHI(I))*PHI(I))*2.0
C***442 GO TO 410
C***442
C
C
C

```

THIS SECTION HANDLES ASYMMETRIC MCEE COMBINATIONS

```

C** 101 MF=M+1
C** MAXL=MAXS(MP)
C** TEST FOR PRESENCE OF SUMMATION COMBINATIONS
C** IF (MAXL.EQ.0) GO TO 102
C** SET UP COUPLING INDICES AND TEST FOR MODE 1
C** DC 103 L=1,MAXL
C** I=JS(L,MP)
C** J=JL(L,MP)
C** JJ=J-I
C** IF (I.EC.1) GO TO 103
C** CCPILE SUMS FOR ASYMMETRIC SUMMATION COMBINATIONS
C** SMF=SMF+PHIX(I)*TX(JJ)+PHIX(J)*TX(I)+PHIX(I)*TX(J)
C** 1 SMS=SMS-PHIT(I)*TTH(JJ)-PHIT(J)*TTH(I)+PHI(I)*TTH(J)
C** 1 SMV=SMV+PHIT(I)*TTH(JJ)+PHIT(J)*TTH(I)+PHI(I)*TTH(J)
C** 1 SME=SME+PHIX(I)*TX(JJ)+PHIX(J)*TX(I)-PHIX(I)*TX(J)
C** 1 SMN=SMN-PHI(I)*TX(JJ)-PHI(J)*TX(I)+PHI(I)*TX(J)
C** 1 SMT=SMT-PHI(I)*TTH(JJ)-PHI(J)*TTH(I)+PHI(I)*TTH(J)
C** 1 CCNTINUE
C** TEST FOR PRESENCE OF DIFFERENCE COMBINATIONS
C** IC2 MAXL=MAXD(MP)
C** IF (MAXL.EQ.0) GO TO 104
C** SET UP COUPLING MGDES - INDICES AND TEST FOR MCDE 1
C** DC 105 L=1,MAXL
C** I=JL(L,MP)
C** J=JL(L,MP)
C** JJ=J-I
C** IF (J.EC.1) GO TO 123

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000021830

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C *****
C CMFILE SUMS FOR ASYMMETRIC DIFFERENCE COMBINATIONS
C SMF=SMF-PFIX(I)*TX(JJ)+PHIX(J)*TX(II)+PHIX(II)*TX(J)
C 1 -PHIX(JJ)*TX(I)
C 1 SMS=SMS+PHIT(I)*TTH(JJ)+PHIT(J)*TTH(II)+PHIT(II)*TTH(J)
C 1 SPV=SMV+PHIT(I)*TTH(I)+PHIT(J)*TTH(II)+PHIT(II)*TTH(J)
C 1 SME=SME+PHIX(I)*TX(JJ)+PHIX(J)*TX(II)+PHIX(II)*TX(J)
C 1 SPN=SMN+PHI(I)*TX(JJ)+PHI(J)*TX(II)+PHI(II)*TX(J)
C 1 SMT=SMT+PHI(I)*TTH(JJ)+PHI(J)*TTH(II)+PHI(II)*TTH(J)
C 1 GC TO IC5
C *****
C EXECUTE BELOW IF J=1 IN DIFF-COMB (OR I=1 IN SUM-COMB)
C *****
C 123 SPF=SMF+(PHIX(I)*TX(II)+PHIX(II)*TX(I))*2.0
C SPV=SMV+(PHIT(I)*TTH(II)+PHIT(II)*TTH(I))*2.0
C SME=SME+(PHIX(I)*TX(II)+PHIX(II)*TX(I))*2.0
C SMT=SMT+(PHI(I)*TTH(II)+PHI(II)*TTH(I))*2.0
C *****
C IC5 CCNTINUE
C *****
C TEXT FOR PRESENCE CF SAME-INDEX COMBINATIONS
C *****
C IC4 IF (MAXSY(MP).EQ.0) GC TO 410
C *****
C SET UP COUPLING MCCES- INDICES AND COMPILE SUMS
C *****
C I=IJS(MP)
C I=I-I
C SMF=SMF+PHIX(I)*TX(II)+PHIX(II)*TX(I)
C SPV=SMV+PHIT(I)*TTH(II)+PHIT(II)*TTH(I)
C SME=SME+PHIX(I)*TX(II)-PHIX(II)*TX(I)
C SMT=SMT+PHI(I)*TTH(II)+PHI(II)*TTH(I)
C *****
C 41C CCNTINUE
C *****
C PREP+RE -AETA- TERMS
C *****
C ETX3(M)=SMF*0.5
C ETX3(M)=SMV*0.5
C ETX3(M)=SME*0.5
C *****
00021840
00021850
00021860
00021870
00021880
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00021900
00021910
00021920
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00021940
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00021960
00021970
00021980
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APPENDIX B

LISTING OF OUTPUT FROM EXAMPLE PROBLEM

---ORIGEN NUMBER 1---

IMPACT TEST CASE, IMPULSIVELY LOADED CORE

---INPUT DATA RECORD---

THE BOUNDARY CONDITIONS ARE:

AT THE INITIAL EDGE

0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

AT THE FINAL EDGE

0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

NUMBER OF STATIONS----- 31  
 NUMBER OF MODES----- 4  
 INCREMENTAL TIME----- 1824E-01  
 MAXIMUM NUMBER OF TIME STEPS----- 750  
 MAXIMUM NUMBER OF ITERATIONS----- 29  
 CONVERGENCE CRITERION----- 0.0100

CHARACTERISTIC SHELL DIMENSION----- 0.1500E 02  
 REFERENCE THICKNESS----- 0.5430E 00  
 REFERENCE STIFFNESS----- 0.7500E 07  
 REFERENCE TIME----- 0.1000E-04  
 POISSON'S RATIO----- 0.2800E 03

0.0 CIRCUMFERENTIAL COORDINATES FOR THE POINT RECIPO, IN RADIAN MEASURE, ARE:  
 3.1415920258

THE DATA PRINTED IS DIMENSIONAL  
 EXECUTING IN SUPPLYTIME MBYRATPR

STATION	RADIUS	GAMMA	CIRCUIT	PHASE	MASS
1	0.7950E 01	0.1412E 01	0.1243E 00	0.0	0.1021E 03
2	0.8026E 01	0.1873E 01	0.1241E 00	0.0	0.1021E 03
3	0.8102E 01	0.1876E 01	0.1220E 00	0.0	0.1021E 03
4	0.8178E 01	0.1858E 01	0.1209E 00	0.0	0.1021E 03
5	0.8254E 01	0.1841E 01	0.1197E 00	0.0	0.1021E 03
6	0.8330E 01	0.1824E 01	0.1185E 00	0.0	0.1021E 03
7	0.8406E 01	0.1807E 01	0.1174E 00	0.0	0.1021E 03
8	0.8482E 01	0.1792E 01	0.1162E 00	0.0	0.1021E 03
9	0.8558E 01	0.1776E 01	0.1151E 00	0.0	0.1021E 03
10	0.8634E 01	0.1760E 01	0.1140E 00	0.0	0.1021E 03
11	0.8710E 01	0.1745E 01	0.1129E 00	0.0	0.1021E 03
12	0.8786E 01	0.1730E 01	0.1118E 00	0.0	0.1021E 03
13	0.8862E 01	0.1715E 01	0.1107E 00	0.0	0.1021E 03
14	0.8938E 01	0.1700E 01	0.1096E 00	0.0	0.1021E 03
15	0.9014E 01	0.1685E 01	0.1085E 00	0.0	0.1021E 03
16	0.9090E 01	0.1672E 01	0.1074E 00	0.0	0.1021E 03
17	0.9166E 01	0.1658E 01	0.1063E 00	0.0	0.1021E 03
18	0.9242E 01	0.1644E 01	0.1052E 00	0.0	0.1021E 03
19	0.9318E 01	0.1631E 01	0.1041E 00	0.0	0.1021E 03
20	0.9394E 01	0.1618E 01	0.1030E 00	0.0	0.1021E 03
21	0.9470E 01	0.1605E 01	0.1019E 00	0.0	0.1021E 03
22	0.9546E 01	0.1592E 01	0.1008E 00	0.0	0.1021E 03
23	0.9622E 01	0.1579E 01	0.1007E 00	0.0	0.1021E 03
24	0.9698E 01	0.1567E 01	0.1016E 00	0.0	0.1021E 03
25	0.9774E 01	0.1554E 01	0.1025E 00	0.0	0.1021E 03
26	0.9850E 01	0.1543E 01	0.1034E 00	0.0	0.1021E 03
27	0.9926E 01	0.1531E 01	0.1043E 00	0.0	0.1021E 03
28	0.1000E 02	0.1519E 01	0.9958E -01	0.0	0.1021E 03
29	0.1028E 02	0.1507E 01	0.9807E -01	0.0	0.1021E 03
30	0.1015E 02	0.1497E 01	0.9734E -01	0.0	0.1021E 03
31	0.1023E 02	0.1485E 01	0.9663E -01	0.0	0.1021E 03

STATION	R STIFFNESS	D STIFFNESS	K PRIME	D PRIME
1	0.208163E 07	0.511471E 05	0.0	0.0
2	0.208163E 07	0.511471E 05	0.0	0.0
3	0.208163E 07	0.511471E 05	0.0	0.0
4	0.208163E 07	0.511471E 05	0.0	0.0
5	0.208163E 07	0.511471E 05	0.0	0.0
6	0.208163E 07	0.511471E 05	0.0	0.0
7	0.208163E 07	0.511471E 05	0.0	0.0
8	0.208163E 07	0.511471E 05	0.0	0.0
9	0.208163E 07	0.511471E 05	0.0	0.0
10	0.208163E 07	0.511471E 05	0.0	0.0
11	0.208163E 07	0.511471E 05	0.0	0.0
12	0.208163E 07	0.511471E 05	0.0	0.0
13	0.208163E 07	0.511471E 05	0.0	0.0
14	0.208163E 07	0.511471E 05	0.0	0.0
15	0.208163E 07	0.511471E 05	0.0	0.0
16	0.208163E 07	0.511471E 05	0.0	0.0
17	0.208163E 07	0.511471E 05	0.0	0.0
18	0.208163E 07	0.511471E 05	0.0	0.0
19	0.208163E 07	0.511471E 05	0.0	0.0
20	0.208163E 07	0.511471E 05	0.0	0.0
21	0.208163E 07	0.511471E 05	0.0	0.0
22	0.208163E 07	0.511471E 05	0.0	0.0
23	0.208163E 07	0.511471E 05	0.0	0.0
24	0.208163E 07	0.511471E 05	0.0	0.0
25	0.208163E 07	0.511471E 05	0.0	0.0
26	0.208163E 07	0.511471E 05	0.0	0.0
27	0.208163E 07	0.511471E 05	0.0	0.0
28	0.208163E 07	0.511471E 05	0.0	0.0
29	0.208163E 07	0.511471E 05	0.0	0.0
30	0.208163E 07	0.511471E 05	0.0	0.0
31	0.208163E 07	0.511471E 05	0.0	0.0

THE INITIAL CONDITIONS FOR N = 0 FOLLOW

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U INT	V INT	W INT	M S INT
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

THE INITIAL CONDITIONS FOR M = 1. FLOW

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U DOT	V DOT	W DOT	M S DOT
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

THE INITIAL CONDITIONS FOR N= 2 EQUATION

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U DOT	V DOT	W DOT	M S DOT
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

IFF INITIAL CONDITIONS FOR R= 4 FOLLOW

STATION	U	V	W	M S
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

STATION	U DDT	V DDT	W DDT	M S DDT
1	0.0	0.0	0.0	0.0
2	0.0	0.0	0.0	0.0
3	0.0	0.0	0.0	0.0
4	0.0	0.0	0.0	0.0
5	0.0	0.0	0.0	0.0
6	0.0	0.0	0.0	0.0
7	0.0	0.0	0.0	0.0
8	0.0	0.0	0.0	0.0
9	0.0	0.0	0.0	0.0
10	0.0	0.0	0.0	0.0
11	0.0	0.0	0.0	0.0
12	0.0	0.0	0.0	0.0
13	0.0	0.0	0.0	0.0
14	0.0	0.0	0.0	0.0
15	0.0	0.0	0.0	0.0
16	0.0	0.0	0.0	0.0
17	0.0	0.0	0.0	0.0
18	0.0	0.0	0.0	0.0
19	0.0	0.0	0.0	0.0
20	0.0	0.0	0.0	0.0
21	0.0	0.0	0.0	0.0
22	0.0	0.0	0.0	0.0
23	0.0	0.0	0.0	0.0
24	0.0	0.0	0.0	0.0
25	0.0	0.0	0.0	0.0
26	0.0	0.0	0.0	0.0
27	0.0	0.0	0.0	0.0
28	0.0	0.0	0.0	0.0
29	0.0	0.0	0.0	0.0
30	0.0	0.0	0.0	0.0
31	0.0	0.0	0.0	0.0

THE TIME STEP NUMBER IS 250 THE TIME IS 4.5600E-03 SECONDS THE SOLUTION CONVERGED IN 2 ITERATIONS

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.0

STATION	N S	N THETA	M	M THETA	Q S	M S	M THETA	K THETA
1	-0.3459E 04	-0.0471E 03	0.0	-0.2172E 04	0.2386E 03	0.5424E 02	0.0	
14	0.7320E 04	0.2551E 04	0.0	-0.2551E 04	0.7320E 04	0.0	0.0	
27	0.3080E 04	-0.5224E 03	0.0	-0.2760E 04	-0.4155E 03	-0.1715E 03	0.0	
31	0.2831E 04	0.7475E 03	0.0	0.1122E 04	-0.9755E 03	-0.5740E 02	0.0	

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.161501 CL

STATION	U	V	W	PHI C	PHI THETA	PHI	K THETA
1	0.0	0.0	0.2749E -09	0.1778E -09	0.0	0.0	0.0
14	-0.6017E -02	0.0	0.1312E 00	-0.3565E -01	0.0	0.0	0.0
27	-0.4079E -02	0.0	0.3927E -01	0.5681E -01	0.0	0.0	0.0
31	-0.1578E -09	0.0	-0.6352E -10	-0.5080E -09	0.0	0.0	0.0

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.161501 CL

STATION	N S	N THETA	M	M THETA	Q S	M S	M THETA	K THETA
1	-0.4580E 04	-0.1275E 04	-0.3960E -02	-0.1035E 04	0.1454E 04	0.6159E 03	-0.1914E -04	
14	-0.4554E 04	-0.3291E 05	-0.1549E -02	-0.2551E 04	-0.8859E 03	-0.3320E 03	0.1956E -04	
27	-0.3588E 04	-0.6111E 04	0.4616E -02	0.3650E 04	0.5926E 03	0.1065E 03	-0.7260E -04	
31	-0.1638E 04	-0.5050E 03	0.3203E -02	0.5698E 04	0.1458E 04	0.6288E 03	-0.1140E -04	

THE SUMMED FORCES, MOMENTS, DISPLACEMENTS AND ROTATIONS FOLLOW FOR THETA = 0.161501 CL

STATION	U	V	W	PHI C	PHI THETA	PHI	K THETA
1	0.0	0.0	-0.6935E -09	0.4810E -09	0.1078E -15	-0.2664E -08	0.0
14	0.5233E -02	-0.3005E -07	-0.2072E 00	0.7570E -01	0.1772E 00	0.2737E 00	0.0
27	0.2689E -02	-0.1181E -07	-0.6809E -01	-0.3030E -01	-0.4166E -04	0.3145E -08	0.0
31	0.3275E -10	-0.4139E -15	-0.3176E -10	0.2566E -09	-0.6057E -14	0.2155E -08	0.0

APPENDIX C

INPUT DATA GUIDE FOR SATANS-IIA

INPUT DATA GUIDE FOR SATANS-I, SATANS-II, AND  
SATANS-IIA

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
1	1-72	18A4	TITLE	-	ENTER ANY 72 CHARACTERS
-----					
2	1-5	I5	NO	1	THE PROBLEM NUMBER, 0<N<10000.
2	6-10	L5	\$DYNAMIC	F T	FOR A STATIC ANALYSIS, SET \$DYNAMIC = F. FOR A DYNAMIC ANALYSIS, SET \$DYNAMIC = T.
2	11-15	I5	IMODE	0 1	FOR NO MODAL OUTPUT DATA FOR MODAL OUTPUT DATA.
2	16-20	I5	NDIMEN	0 1	DIMENSIONAL OUTPUT DATA. NONDIMENSIONAL OUTPUT.
2	21-25	I5	NTHMAX	8	SUMMED SOLUTION WILL BE PRINTED AT NTHMAX MERIDI- ANS, 0<NTHMAX<=36.
2	26-30	I5	IFREQ	2	SOLUTION WILL BE PRINTED AT THE FIRST STATION, EVERY SUBSEQUENT IFREQ STATION AND THE LAST STATION, 0<IFREQ<=KMAX.
2	31-35	I5	IPRINT	3	EVERY IPRINT CONVERGED SOLUTION WILL BE PRINT- ED.
2	36-40	I5	IBCINL	-1 0	IF THE SHELL HAS A POLE AT THE FIRST STATION. IF THE SHELL HAS NO POLE AT THE FIRST STATION.
2	41-45	I5	IBCFNL	-1 0	IF THE SHELL HAS A POLE AT THE LAST STATION. IF THE SHELL HAS NO POLE AT THE LAST STATION.

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
2	46-50	I5	KMAX	35	NUMBER OF MERIDIONAL STATICS. NOTE: KMAX<201 FOR SATANS -I WITHOUT PLCTS AND KMAX<101 FOR SATANS-I WITH PLOTS OR FOR SATANS -II. SATANS-IIA IS UNLIMITED.
2	51-55	I5	MNMAX	7	NUMBER OF SERIES COEFFICIENTS USED TO DESCRIBE THE INITIAL CONDITIONS, PRESSURE AND THERMAL LOADS (AND INITIAL IMPERFECTIONS IF USING SATANS -II OR IIA). MNMAX<=MAXM.
2	56-60	I5	MAXM	7	MAX NUMBER OF HARMONICS IN THE SOLUTION, LIMITED TO 99.
2	61-65	I5	LSMAX	1 99 3000	FOR A LINEAR ANALYSIS. USE MANY LOAD STEPS FOR A NONLINEAR STATIC ANALYSIS. FOR A DYNAMIC ANALYSIS, LSMAX IS THE NUMBER OF TIME INCREMENTS, WHERE $LSMAX = T_{MAX}/\Delta T$ .
2	66-70	I5	LCHMAX	2 0	THE NUMBER OF LOAD STEP SIZE REDUCTIONS IN A STATIC ANALYSIS, RECOMMENDED RANGE = 2-4. FOR A DYNAMIC ANALYSIS.
2	71-75	I5	ITRMAX	1 30	FOR A LINEAR ANALYSIS. THE NUMBER OF ITERATIONS AT A LOAD OR TIME STEP. FOR A NONLINEAR ANALYSIS, SUGGESTED RANGE = 10-30, UP TO 50 FOR SPECIAL CASES.
2	76-80	I5	IC	0 1	INITIAL CONDITIONS. SET TO 0 FOR A STATIC ANALYSIS, OR FOR A DYNAMIC ANALYSIS WHERE THE SPILL IS AT REST AT $T=0$ . FOR A DYNAMIC ANALYSIS WITH INITIAL CONDITIONS.

CARD	COLUMNS	FORMAT	ITEM	EXAMPLE	MEANING
3	1-12	E12.3	NU	0.3	POISSON'S RATIO, $\nu$ .
3	12-24	E12.3	SIG0	1000.0 1.0	REFERENCE STRESS LEVEL, IF THE INPUT DATA IS DIMENSIONAL.
3	24-36	E12.3	ELAST	.3E8 1.0	REFERENCE MODULUS OF ELASTICITY, $E$ . IF THE INPUT DATA IS DIMENSIONAL.
3	37-48	E12.3	TKN	.4E-2 1.0	REFERENCE THICKNESS, $h$ . IF THE INPUT DATA IS DIMENSIONAL.
3	49-60	E12.3	CHAR	8.16 1.0	CHARACTERISTIC SHELL DIMENSION, $a$ . IF THE INPUT DATA IS DIMENSIONAL.
3	61-72	E12.3	TEEO	0.0 .996E-5	IF A STATIC ANALYSIS. REFERENCE TIME, $T_0$ .
-----					
4	1-12	E12.3	DELCAD	0.2  0.1823E-6	FOR A STATIC ANALYSIS, DELCAD IS THE LOAD INCRE- MENT. IT REMAINS UN- CHANGED UNTIL THE SOLU- TION FAILS TO CONVERGE IN ITERMAX ITERATIONS, WHEN IT IS REDUCED BY A FACTOR OF FIVE. A MAXIMUM OF LCHMAX SUCH REDUCTIONS WILL OCCUR. FOR A DYNAMIC ANALYSIS, DELCAD IS THE NONDIMEN- SIONAL TIME INCREMENT.
4	13-24	E12.3	EPS	0.01	THE CONVERGENCE CRITERION RECOMMENDED RANGE OF 0.01 < EPS < 0.001.
-----					
CARD 4A IS ONLY INCLUDED FOR A SATANS-II OR SATANS-IIA RUN.					
4A	1-5	I5	JUMP	1 2	FOR AN ANALYSIS USING SINGLE SERIES EXPANSIONS. FOR AN ANALYSIS USING DOUBLE SERIES EXPANSIONS.
4A	5-10	I5	MPERFS	0 1	AN ANALYSIS WITHOUT IM- PERFECTIONS. AN ANALYSIS WITH IMPERFEC- TIONS. NOTE: IF JUMP=28 MPERFS MAY BE 0 OR 1. IF JUMP =1, MPERFS MUST BE 0. IF MPERFS=1, JUMP MUST BE 2.

-----

CARD COLUMN FORMAT ITEM EXAMPLE MEANING

INCLUDE AS MANY CARDS 5 AS NECESSARY TO SPECIFY NTHMAX MERIDIANS. IF NTHMAX EQUALS 0, OMIT CARD 5.

5 1-72 6E12.3 10.0 A LIST OF CIRCUMFERENTIAL COORDINATES  $\phi$ , IN DEGREES AND TENTHS, WHERE THE SOLUTION PRINTOUT IS DESIRED. THE LIST MUST HAVE NTHMAX ENTRIES.

-----

IF IBCINL = -1, OMIT CARDS 6 THROUGH 14. IF IBCFNL = -1, OMIT CARDS 15 THROUGH 23. CARDS 6 THROUGH 23 DESCRIBE THE BOUNDARY CONDITIONS AT THE FIRST, AND THEN AT THE LAST STATION. THE BOUNDARY CONDITIONS EXIST ON THE TOTAL VARIABLES, NOT ON THE INDIVIDUAL HARMONICS. LOADINGS APPLIED THROUGH SPECIFICATION OF BOUNDARY CONDITIONS ARE TAKEN IN THE ZEROETH HARMONIC (N=0) ONLY, AS THE COLUMN MATRIX  $\{f\}$  IS SET TO ZERO FOR HARMONICS GREATER THAN ZERO. THE BOUNDARY CONDITIONS ARE DIMENSIONAL. THE FORMAT OF CARDS 6 THROUGH 23 IS 4E16.8.

CARD 6,15    CARD 7,16    CARD 8,17    CARD 9,18

$$\begin{bmatrix} \Omega(1,1) \\ \Omega(2,1) \\ \Omega(3,1) \\ \Omega(4,1) \end{bmatrix} \begin{bmatrix} \Omega(1,2) \\ \Omega(2,2) \\ \Omega(3,2) \\ \Omega(4,2) \end{bmatrix} \begin{bmatrix} \Omega(1,3) \\ \Omega(2,3) \\ \Omega(3,3) \\ \Omega(4,3) \end{bmatrix} \begin{bmatrix} \Omega(1,4) \\ \Omega(2,4) \\ \Omega(3,4) \\ \Omega(4,4) \end{bmatrix} \begin{bmatrix} N_s \\ N_{s0} \\ Q_s \\ \phi_s \end{bmatrix} +$$

CARD 10,19    CARD 11,20    CARD 12,21    CARD 13,22    CARD 14,23

$$\begin{bmatrix} \Lambda(1,1) \\ \Lambda(2,1) \\ \Lambda(3,1) \\ \Lambda(4,1) \end{bmatrix} \begin{bmatrix} \Lambda(1,2) \\ \Lambda(2,2) \\ \Lambda(3,2) \\ \Lambda(4,2) \end{bmatrix} \begin{bmatrix} \Lambda(1,3) \\ \Lambda(2,3) \\ \Lambda(3,3) \\ \Lambda(4,3) \end{bmatrix} \begin{bmatrix} \Lambda(1,4) \\ \Lambda(2,4) \\ \Lambda(3,4) \\ \Lambda(4,4) \end{bmatrix} \begin{bmatrix} U \\ V \\ W \\ M_s \end{bmatrix} = \begin{bmatrix} \lambda(1) \\ \lambda(2) \\ \lambda(3) \\ \lambda(4) \end{bmatrix}$$

- 
- CARD 24 IS:
1. INCLUDED FOR A SATANS-I STATIC ANALYSIS.
  2. INCLUDED BUT BLANK FOR A SATANS-I DYNAMIC ANALYSIS.
  3. OMITTED FOR A SATANS-II ANALYSIS.
  4. INCLUDED BLANK FOR DYNAMIC USED FOR STATIC SATANS-IIA ANALYSES.

CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	1-2	L2	\$PLOTS	F	INDICATES PLOTS ARE NOT DESIRED.
				T	INDICATES PLOTS ARE DESIRED.
24	3-4	L2	\$MODAL	F	INDICATES PLOTS ARE FOR SUMMED SOLUTIONS ONLY.
				T	INDICATES PLOTS ARE FOR MODAL SOLUTIONS ONLY.

FOR THE REMAINDER OF CARD 24 ENTRIES, 0 INDICATES THAT NO PLOTS ARE DESIRED FOR THE PARTICULAR ITEM, AND 1 INDICATES THAT THEY ARE DESIRED. ALL GRAPHS ARE PLOTTED AS THE INDICATED ITEM VERSUS THE STATIC NUMBER. IF A COMPLETE PLOT IS DESIRED, INSUTE IFREQ = 1.

CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	5-6	I2	IRADII	1	PLCT THE RADII AS COMPUTED BY SUBROUTINE GEOM.
24	7-8	I2	IGAMMA	1	PLCT $P/P$ AS COMPUTED BY SUBROUTINE GEOM.
24	9-10	I2	IOMEGS	1	PLCT $\omega_s$ AS COMPUTED BY SUBROUTINE GEOM.
24	11-12	I2	IOMEGT	1	PLCT $\omega_\theta$ AS COMPUTED BY SUBROUTINE GEOM.
24	13-14	I2	IDECMS	1	PLCT $\omega'_s$ AS COMPUTED BY SUBROUTINE GEOM.
24	15-16	I2	IBSTIF	1	PLCT THE STIFFNESS D AS COMPUTED BY SUBROUTINE BCB.
24	17-18	I2	IDSTIF	1	PLOT THE STIFFNESS D AS COMPUTED BY THE SUBROUTINE BDB.
24	19-20	I2	IBBSTF	1	PLCT THE STIFFNESS $db/ds$ AS COMPUTED BY SUBROUTINE BCB.
24	21-22	I2	IDDSTF	1	PLCT THE STIFFNESS $dd/ds$ AS COMPUTED BY SUBROUTINE BDB.
24	23-24	I2	IPR	1	PLOT THE NORMAL COMPONENT OF THE PRESSURE LOAD.
24	25-26	I2	IPS	1	PLOT THE MERIDIONAL COMPONENT OF THE PRESSURE LOAD.
24	27-28	I2	IPT	1	PLCT THE CIRCUMFERENTIAL COMPONENT OF THE PRESSURE LOAD.
24	29-30	I2	ITT	1	PLCT THE THERMAL LOAD.
24	31-32	I2	IMT	1	PLOT THE THERMAL MOMENT.
24	33-34	I2	IDTT	1	PLCT $d/ds$ OF THE THERMAL LOAD.
24	35-36	I2	IDMT	1	PLOT $d/ds$ OF THE THERMAL MOMENT.
24	37-38	I2	INS	1	PLOT THE MERIDIONAL MEMBRANE FORCE DISTRIBUTION.

CARD	COLUMN	FORMAT	ITEM	EXAMPLE	MEANING
24	39-40	I2	INTH	1	PLCT THE CIRCUMFERENTIAL MEMBRANE FORCE DISTRIBUTION.
24	41-42	I2	INSTH	1	PLCT THE MERIDIO-CIRCUMFERENTIAL MEMBRANE FORCE DISTRIBUTION.
24	43-44	I2	IQS	1	PLCT THE TRANSVERSE FORCE DISTRIBUTION.
24	45-46	I2	IMS	1	PLCT THE MERIDIONAL MOMENT DISTRIBUTION.
24	47-48	I2	IMTH	1	PLCT THE CIRCUMFERENTIAL MOMENT DISTRIBUTION.
24	49-50	I2	IMSTH	1	PLCT THE MERIDIO-CIRCUMFERENTIAL MOMENT DISTRIBUTION.
24	51-52	I2	IU	1	PLCT THE MERIDIONAL DISPLACEMENT DISTRIBUTION.
24	53-54	I2	IV	1	PLCT THE CIRCUMFERENTIAL DISPLACEMENT DISTRIBUTION.
24	55-56	I2	IW	1	PLCT THE NORMAL DISPLACEMENT DISTRIBUTION.
24	57-58	I2	IPHS	1	PLCT THE MERIDIONAL ROTATION DISTRIBUTION.
24	59-60	I2	IPHIT	1	PLCT THE CIRCUMFERENTIAL ROTATION DISTRIBUTION.
24	61-62	I2	IPHI	1	PLCT THE MERIDIO-CIRCUMFERENTIAL ROTATION DISTRIBUTION.

-----

INCERT IMPERFECTION DATA HERE FOR A SATANS-II OR SATANS-IIA ANALYSIS WITH IMPERFECTIONS. INSURE FORMAT OF THE IMPERFECTION DATA IS COMPATIBLE WITH THAT SPECIFIED IN THE USER-WRITTEN SUBROUTINE IMPERF.

-----

25	1-2	I2	IRNAGN	0	INDICATES THIS IS THE ONLY RUN.
				1	INDICATES ANOTHER RUN IS TO BE MADE. AND ANOTHER COMPLETE SET OF DATA CARDS AFTER THIS CARD IS IRNAGN= 1.

APPENDIX D

LISTING OF NEW POLE ROUTINE FOR SATANS-IIA

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE FCRCE SUBROUTINE

CCPMCN /IBL5/IBCINL, IBCFNL

```
C   IN FCRCE
10  IF(K.NE.2.OR.(K.EQ.2.AND.IBCINL.GE.0)) GO TO 501
    DC 502  I1=1,4
    SUMX=0.
    DC 503  L=1,4
    SUMX=SUMX+DL(I1,L,N)*GEE(L)
    DC 504  X(I1,IK1)=SUMX
    DC 505  CCNTINUE
    DC 506  I1 I=1,4
```

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE PMATRIX SUBROUTINE

```
C   IN PMATRIX
    CALL EFG(2,MN)
    CALL ABC
    CALL MATINV(A,4,G1,0,DETERM,IPIVCT,INDEX,4,ISCALE)
    DC 501  I1=1,4
    DC 502  J1=1,4
    CL(I1,J1,MN)=0.
    CL(I1,J1,MN)=0.
    CL(I1,J1,MN)=0.
    DC 503  IF(MN.GT.1) GO TO 12
    DC 504  IF(MN.GT.0) GO TO 13
```

```

MC=MN
CL(1,1,MN)=1.
CL(1,2,MN)=1.
CL(1,3,MN)=-3.
CL(1,4,MN)=-3.
CG(3,3,MN)=4.
CG(4,3,MN)=4.
CG(4,4,MN)=-1.
GC TO 9C2
13
M1=MN
CL(1,1,MN)=-3.
CL(2,1,MN)=1.
CL(2,2,MN)=1.
IF(A(M1).LT.0) DL(2,2,MN)=-1
CL(3,3,MN)=1.
CL(4,4,MN)=4.
CG(1,1,MN)=-1.
GC TO 9C2
12
M2=MN
CL(1,1,MN)=1.
CL(2,2,MN)=1.
CL(3,3,MN)=-3.
CL(4,4,MN)=4.
CG(4,4,MN)=-1.
CCCATINUE
CC 5C3 IJ=1,4
CC 5C3 JJ=1,4
TTF=0.
CC 5C4 L=1,4
TTF=ITP+OF(I,I,L,MN)*A(L,JJ)
9C3
CC 5C5 IJ=1,4
CC 5C5 JJ=1,4
TTF=0.
TTC=0.
CC 9C6 L=1,4
TTF=ITP+CL0(I,I,I,L)*C(L,I,JJ)
TTC=ITQ+CLC(I,I,I,JJ)*BEE(L,JJ)
9C6
CL1(I,I,JJ)=DL(I,I,JJ,MN)-TTP
CL2(I,I,JJ)=DG(I,I,JJ,MN)-TTC
9C5
CALL MAIINV(CLI,4,GI,0,DETERM,IFIVOT,INDEX,4,ISCALE)
CC 5C7 IJ=1,4
CC 5C7 JJ=1,4
TTF=0.
TTC=0.

```

LC SC8 L=11<sup>4</sup>  
TF=TTP+CL1(I,I,L)\*CL0(L,JJ)  
TQ=TIQ+CL1(I,I,L)\*CL2(L,JJ)  
CL(I,I,JJ,MN)=TTP  
P(I,I,JJ)=TQ  
GC TC 11  
SC P3=MN

APPENDIX E

LISTING OF CARDS FOR  $\bar{V}$  AND  $\bar{V}_{MAX}$

THE FOLLOWING CARDS ARE TO BE PLACED INTO THE DYNAMIC SUBROUTINE IF NEEDED

```

C  STATEMENTS FOR MAIN TO CALCULATE VBAR
185  CC 186 M=1,MAXM
      CNLM=0
      MM=(M-1)*KMAX2
184  CC 184 K=2,KL
      KT=K+1+MM
      CNLM=CNLM+Z(3,KT)*R(K)
186  CC 187 M=1,MAXM
      VBAR(M)=DNLM*DEL#SOE
      IF(ITTEST=ITTEST+1) CC TG 963
      ITTEST=C
183  WRITE(6,183)(LSTEP,(VBAR(M),M=1,MAXM))
963  FORMAT(5X,'VBAR AT TIME STEP ',I4,' FOR EACH MODE IS'/5E16.4)
      CC 187 M=1,MAXM
187  IF(ABS(VBAR(M)).GT.AVB(M)) AVB(M)=ABS(VBAR(M))

```

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