

AD-A036 432

STANFORD UNIV CALIF DEPT OF APPLIED MECHANICS

F/G 11/6

LINEAR THERMOMECHANICAL COUPLING EFFECT IN TRANSIENT DEFORMATION--ETC(U)

AUG 76 R W YOUNG

N00014-75-C-0698

UNCLASSIFIED

SUDAM-75-10

NL

1 OF 1
AD-A
036 432



END
DATE
FILMED
4-4-77
NTIS

U.S. DEPARTMENT OF COMMERCE
National Technical Information Service

AD-A036 432

LINEAR THERMOMECHANICAL COUPLING EFFECT
IN TRANSIENT DEFORMATION

STANFORD UNIVERSITY
CALIFORNIA

AUGUST 1976

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER Contract No. 25	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) LINEAR THERMOMECHANICAL COUPLING EFFECT IN TRANSIENT DEFORMATION	5. TYPE OF REPORT & PERIOD COVERED Technical Interim	
	6. PERFORMING ORG. REPORT NUMBER SUDAM No. 75-10	
7. AUTHOR(s) RICHARD W. YOUNG	8. CONTRACT OR GRANT NUMBER(s) N00014-75-C-0698	
	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS NR 064-471	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Stanford University Department of Applied Mechanics Stanford, California 94305	12. REPORT DATE August 1976	
	13. NUMBER OF PAGES 42	
11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research Department of the Navy Washington, D. C. 20025	15. SECURITY CLASS. (of this report) UNCLASSIFIED	
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report) Same as above.		
18. SUPPLEMENTARY NOTES - 0 -		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Thermomechanical coupling Irreversible thermodynamics Elasticity Non-oscillatory deformation Finite elasticity Viscoelasticity		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The interaction between the quasi-static mechanical deformation and the thermal state of solids is studied. Principles of classical thermodynamics are used to calculate temperature changes arising from the isentropic deformation of elastic solids. The theory of irreversible thermodynamics is used to predict temperature changes due to the adiabatic deformation of viscoelastic solids. continued on next page		

Unclassified

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

cont
20. cont.

It is found that such temperature changes are small and that the effect of thermomechanical coupling may usually be neglected in the non-oscillatory deformation of linear elastic, finite (rubber) elastic, and linear viscoelastic solids. Data are presented for several metals, rubbers, and plastics. Dynamic processes are not considered.

ADA 036432

ONR Scientific Report
Contract Report No. 25

LINEAR THERMOMECHANICAL COUPLING EFFECTS
IN TRANSIENT DEFORMATION

BY

R. W. Young

Office of Naval Research
Grant N00014-75-C-0698

SUDAM 75-10
AUGUST 1976

Approved for Public Release;
Distribution unlimited.

REPRODUCED BY
NATIONAL TECHNICAL
INFORMATION SERVICE
U. S. DEPARTMENT OF COMMERCE
SPRINGFIELD, VA. 22161

DIVISION
OF
**APPLIED
MECHANICS**

DEPARTMENT
OF
**MECHANICAL
ENGINEERING**



**STANFORD
UNIVERSITY**
STANFORD,
CALIFORNIA
94305

LINEAR THERMOMECHANICAL COUPLING EFFECTS
IN TRANSIENT DEFORMATION*

Richard W. Young
Department of Applied Mechanics
Stanford University
Stanford, California 94305

UNCLASSIFIED	
NR0	White Section <input checked="" type="checkbox"/>
CR0	Soft Section <input type="checkbox"/>
TRANSFORMED	<input type="checkbox"/>
IDENTIFICATION	
BY	
DISTRIBUTION/AVAILABILITY CODES	
Dist.	AVAIL. and/or SPECIAL
A	

*This research was supported by Contract No. N00014-75-C-0698 of the Office of Naval Research, Washington, D.C.

ABSTRACT

The interaction between the mechanical deformation and the thermal state of solids is studied. Principles of classical thermodynamics are used to calculate temperature changes arising from the isentropic deformation of elastic solids. The theory of irreversible thermodynamics is used to predict temperature changes due to the adiabatic deformation of viscoelastic solids.

It is found that such temperature changes are small and that the effect of thermomechanical coupling may usually be neglected in the non-oscillatory deformation of linear elastic, finite (rubber) elastic, and linear viscoelastic solids. Data are presented for several metals, rubbers, and plastics.

INTRODUCTION

In the analysis of mechanical deformation, thermal effects are usually not considered beyond the occasional noting of the temperature of the material at the onset of testing. Because the mechanical properties of the material can be essentially independent of the temperature over large temperature ranges, this approximation is usually justifiable. Even when the material properties exhibit significant thermal dependence, the deformation process can cause such a small change in temperature that its effects may be ignored.

There are some cases, however, especially in the realm of viscoelastic materials, in which the temperature change and the ensuing variation of mechanical properties can be important.

We shall concern ourselves with essentially static loadings, such as simple extension, shear, or bulk compression of solids. These "static" processes will be referred to as transient. Changes in the temperature of a body which result from its deformation under such loadings will be calculated. Knowledge of the effect of temperature upon the mechanical properties then enables us to gauge the importance of thermomechanical coupling in a given problem.

The following chapters will deal with the transient loadings of linear elastic, rubber elastic, and linear viscoelastic solids. We will not consider here dynamic processes such as vibration or shock loading.

CHAPTER ONE

LINEAR ELASTIC DEFORMATIONS

The effect of thermomechanical coupling in linear elastic solids is easily derived from the basic equations of thermodynamics and thermoelasticity. Results in this field are already well established (see for example Nowacki [1] and Biot [2]), and the following derivation is presented primarily as a basis and as a source of comparison for subsequent developments.

In the ensuing equations, quantities such as internal energy, U , heat, Q , work, W , entropy, S , et cetera, are measured per unit of original volume of an infinitesimal body. We write the first law of thermodynamics as¹

$$dU = dQ + dW \quad (1)$$

The absolute temperature of the body is denoted by T . From the second law of thermodynamics, applied to reversible processes, we write:

$$dQ = TdS \quad (2)$$

The work done on the body, per unit of original volume, is expressed by²

$$dW = \sigma_{ij} d\epsilon_{ij} \quad (3)$$

1 dW is the total increment of work done on (not by) the body, and it includes work done by atmospheric pressure and any other pre-loads. These are departures from usual thermodynamic convention. dQ denotes the increment of heat added to the body.

2 Summation convention will be used, implying summation over repeated free indices. Thus

$$\sigma_{ij} d\epsilon_{ij} = \sum_{i=1}^3 \sum_{j=1}^3 \sigma_{ij} d\epsilon_{ij}$$

where σ_{ij} and ϵ_{ij} are the conventional stresses and infinitesimal strains of classical elasticity.³

Using the definition of the Helmholtz free energy,

$$A = U - TS, \quad (4)$$

entropy may be expressed as a function of temperature and the strain tensor, $S = S(T, \underline{\epsilon})$. From eqs. (1-4), we have

$$dA = \sigma_{ij} d\epsilon_{ij} - SdT \quad (5)$$

Thus:⁴

$$\left. \frac{\partial A}{\partial \epsilon_{ij}} \right|_{T, \underline{\epsilon}'} = \sigma_{ij}, \quad \left. \frac{\partial A}{\partial T} \right|_{\underline{\epsilon}} = -S \quad (6a,b)$$

It follows from the commutivity of partial differentiation and the regular behavior of A that

$$\left. \frac{\partial S}{\partial \epsilon_{ij}} \right|_{T, \underline{\epsilon}'} = - \left. \frac{\partial \sigma_{ij}}{\partial T} \right|_{\underline{\epsilon}} \quad (7)$$

From eq. (2) and the definition of heat capacity, we write

3 To be precise, these can be interpreted as the second Piola-Kirchoff stress (force per unit of undeformed area) and the Lagrange strain (attributed to Cauchy.) In the infinitesimal case, these measures differ insignificantly from various other common measures. For detailed discussion of these points, see Truesdell and Noll [3] and Rivlin [4].

4 The notation $\left|_{\underline{\epsilon}'}\right.$ implies that all elements of $\underline{\epsilon}$ are held fixed with the exception $\underline{\epsilon}_i$ of the one indicated in the partial differential operator.

$$\left. \frac{\partial S}{\partial T} \right|_{\underline{\epsilon}} = \frac{\rho_0 C_V}{T} \quad (8)$$

where ρ_0 is the material density in the undeformed state and C_V the heat capacity per unit mass at constant volume or, to be more precise, constant strain.

The partial derivative on the right-hand side of eq. (7) may be evaluated directly from consideration of the thermoelastic stress-strain laws. Letting μ and λ denote the isothermal Lamé constants, α the volumetric coefficient of thermal expansion, and θ the increase in temperature from the strain-free state, strain is given by

$$\epsilon_{ij} = \frac{1}{2\mu}(\sigma_{ij} - \sigma_{o_{ij}}) - \frac{\lambda}{2\mu(2\mu+3\lambda)}(\sigma_{kk} - \sigma_{o_{kk}})\delta_{ij} + \frac{\alpha}{3}\theta\delta_{ij} \quad (9)$$

where $\sigma_{o_{ij}}$ is the pre-loading, the loads existing in the strain-free state. The most common example of pre-loading is atmospheric pressure. Inverting these relations, we have

$$\sigma_{ij} = \sigma_{o_{ij}} + 2\mu\epsilon_{ij} + \lambda\epsilon_{kk}\delta_{ij} - \alpha K\theta\delta_{ij} \quad (10)$$

where $K = \lambda + \frac{2\mu}{3}$ is the isothermal bulk modulus.

Writing entropy in terms of its partial derivatives, and substituting from eqs. (7), (8), and (10):

$$dS = \frac{\rho_0 C_V}{T} dT + \alpha K\theta_{,ij} d\epsilon_{ij} \quad (11)$$

Thermomechanical coupling effects are usually ignored in non-oscillatory situations. An argument often cited in support of this

approximation is one which we shall refer to here as the "equivalent heat" argument. Stated simply, it states that if one were to supply the thermodynamic system (the infinitesimal body) with an amount of heat equivalent to the mechanical work done on the system, the resulting change in temperature of the system would be an upper bound for the actual change in temperature. (The change in temperature predicted by this argument is denoted by dT_{eqh} .) Thus:

$$dW = dQ = \rho_0 C_V dT_{eqh} \quad (12)$$

and from eq. (3),

$$dT_{eqh} = \frac{\sigma_{ij} d\epsilon_{ij}}{\rho_0 C_V} \quad (13)$$

dT_{eqh} is compared with the result of the thermodynamic analysis, denoted by dT_{thm} . For an adiabatic, reversible process, $dS = 0$ and eq. (11) becomes:

$$dT_{thm} = - \frac{\alpha TK}{\rho_0 C_V} \delta_{ij} d\epsilon_{ij} = - \frac{\alpha TK}{\rho_0 C_V} d\epsilon_{kk} \quad (14)$$

Integrating eqs. (13) and (14), making the approximations that α and K are constant, C_V is linear in temperature, and ΔT is small with respect to T , we find that:

$$\Delta T_{thm} = - \frac{\alpha TK}{\rho_0 C_V} \Delta \epsilon_{kk} \quad (15)$$

and

$$\Delta T_{eqh} = \frac{1}{\rho_o C_v} (\sigma_{o_{ij}} + \frac{1}{2} \Delta \sigma_{ij}) \Delta \epsilon_{ij} \quad (16)$$

Comparison of eqs. (15) and (16) shows that ΔT_{eqh} is a poor measure of ΔT_{thm} , the actual temperature change. ΔT_{thm} is dependent solely upon the volume change and is thus identically zero for any equivo-luminal deformation. ΔT_{eqh} , however, is proportional to the incre-ment in strain energy and is affected by shear deformations. In such cases, ΔT_{eqh} does indeed serve as an upper bound for the change in temperature, but it is misleading to place an upper bound on a quantity which must be zero.

In the case of hydrostatic compression, ΔT_{eqh} can fall far short of ΔT_{thm} . As an example, consider the compression of a speci-men by a pressure of n atmospheres. Denoting one atmosphere of pressure by P , then $\sigma_{o_{ij}} = -P\delta_{ij}$, $\Delta \sigma_{ij} = -nP\delta_{ij}$, and $\Delta \epsilon_{ij} = -nP\delta_{ij}/3K$. Substitution into eqs. (15) and (16) leads to:

$$\frac{\Delta T_{thm}}{\Delta T_{eqh}} = \frac{2\alpha TK}{(2+n)P} \quad (17)$$

The ratio can be quite large, as is seen in the following tabulation:

TABLE 1:⁵ Sample Values of ($\alpha TK/P$)

<u>Material</u>	<u>$\alpha, (^{\circ}K^{-1})$</u>	<u>$K, (psi)$</u>	<u>$\alpha TK/P, (--)$</u>
mild steel	3.6×10^{-5}	24.6×10^6	1.8×10^4
polyisoprene (ebonite rubber)	1.9×10^{-4}	6.0×10^5	2.3×10^3
polyethylene (low density)	7.4×10^{-4}	4.8×10^5	7.2×10^3

5 From [5], table 1-59; [6], p. 708; [7], sec VI; [8], table 9.1 .

Even in the case of ebonite, the most favorable case presented, the ratio of ΔT_{thm} to ΔT_{eqh} does not reach unity until the material is compressed by almost 4600 atmospheres. Pearson [9] presents a calculation for a cube of steel compressed from an initially unstressed state. In his example, the ratio of ΔT_{thm} to ΔT_{eqh} is unbounded as the applied pressure approaches zero, as may be seen by examination of eqs. (15) and (16) with $\sigma_{ij} = 0$.

Despite the failure of ΔT_{eqh} to predict, or even to provide an upper bound on, the thermal effects of deformation, these effects are still negligible for infinitesimal elastic deformation, as is later seen in Chapter Four.

CHAPTER TWO

FINITE ELASTIC DEFORMATIONS

Since many polymers exhibit rubber elasticity, we perform a similar analysis for finite elasticity. We will deal only with principal stresses, and will use extension ratios and true stress (force per unit of deformed area, sometimes called Cauchy stress) defined as follows:^{6,7}

$$\lambda_i = L_i/L_{o(i)} = 1 + \epsilon_{i(i)} \quad (18)$$

$$t_i = f_i/L_j L_k = \sigma_{i(i)}/\lambda_j \lambda_k, \quad i \neq j \neq k \quad (19)$$

In terms of these variables, the first law of thermodynamics becomes, for reversible processes:

$$dU = TdS + (V/V_o)t_i d\text{Ln}\lambda_i \quad (20)$$

Eq. (5) becomes:

$$dA = (V/V_o)t_i d\text{Ln}\lambda_i - SdT \quad (21)$$

We proceed as in the infinitesimal case, noting that $V = V_o \lambda_1 \lambda_2 \lambda_3$, so that constant λ ($\lambda = (\lambda_1, \lambda_2, \lambda_3)^T$) implies constant volume.⁸

6 The extension ratio is closely related to the natural, or logarithmic, strain; $\epsilon_i = \text{Ln}\lambda_i$.

7 Numerical indices and indices hidden in parentheses are not subject to implied summation.

8 T used as a superscript to a vector or a matrix will denote the transpose of that quantity. T used as a scalar will continue to denote absolute temperature.

As in eq. (8),

$$\left. \frac{\partial S}{\partial T} \right|_{\lambda} = \rho_o C_V / T \quad (22)$$

Similarly to eqs. (6),

$$\left. \frac{\partial A}{\partial T} \right|_{\lambda} = -S, \quad \left. \frac{\partial A}{\partial \lambda_i} \right|_{T, \lambda} = \frac{V t_i}{V_o \lambda(i)} \quad (23a, b)$$

Thus:

$$\left. \frac{\partial S}{\partial \lambda_i} \right|_{T, \lambda} = \frac{-V}{V_o \lambda(i)} \left. \frac{\partial t_i}{\partial T} \right|_{\lambda} \quad (24)$$

From eqs. (22) and (24) we have

$$dS = \frac{\rho_o C_V}{T} dT - \frac{V}{V_o \lambda(i)} \left. \frac{\partial t_i}{\partial T} \right|_{\lambda} d\lambda_i \quad (25)$$

For an isentropic process, we have

$$dT_{thm} = \frac{VT}{\rho_o V_o C_V \lambda(i)} \left. \frac{\partial t_i}{\partial T} \right|_{\lambda} d\lambda_i, \quad (26)$$

whereas the equivalent heat argument gives

$$dT_{eqh} = dW / \rho_o C_V = \frac{V}{V_o \rho_o C_V} \frac{t_i}{\lambda(i)} d\lambda_i \quad (27)$$

Integrating eqs. (26) and (27),

$$\Delta T_{\text{thm}} = \frac{T_0}{\rho_0 V_0 C_V} \int \frac{V}{\lambda_{(i)}} \left. \frac{\partial t_i}{\partial T} \right|_{\lambda} d\lambda_i \quad (28)$$

$$\Delta T_{\text{eqh}} = \frac{1}{\rho_0 V_0 C_V} \int \frac{V}{\lambda_{(i)}} t_i d\lambda_i \quad (29)$$

At this point we consider possible forms of the function $t_i = t_i(\lambda, T)$. In most references, it is assumed that stress varies as a linear function of temperature in strain control experiments. This assumption is well verified by experimental results (Meyer and Ferri [10] and Anthony, Caston, and Guth [11] as cited in Treloar [12]). As a further motivation, we shall show that this linear dependence is a direct result of another physical observation, that the heat capacity at constant volume is independent of the deformational state over large ranges of deformation, that is to say,

$$C_V(\lambda, T) = C_V(T) \quad (30)$$

Taking eqs. (22) and (24) and invoking the commutivity of partial differentiation, derivation of the second partial derivate of S with respect to λ_i and T requires that

$$\left. \frac{\rho_0}{T} \frac{\partial C_V}{\partial \lambda_i} \right|_{T, \lambda} = \frac{-V}{V_0 \lambda_{(i)}} \left. \frac{\partial^2 t_i}{\partial T^2} \right|_{\lambda} \quad (31)$$

Eq. (31) and the form of eq. (30) require that

$$\left. \frac{\partial^2 t_i}{\partial T^2} \right|_{\lambda} = 0 \quad (32)$$

which, integrated twice, becomes:

$$t_i(\lambda, T) = h_i(\lambda)T + g_i(\lambda) \quad (33)$$

Conversely, assumption of eq. (33) leads to eq. (30). Using the form of eq. (33), eqs. (28) and (29) become:

$$\Delta T_{thm} = \frac{T_o}{\rho_o V_o C_V} \int \frac{V}{\lambda^{(i)}} h_i(\lambda) d\lambda_i \quad (34)$$

$$\Delta T_{eqh} = \Delta T_{thm} + \frac{1}{\rho_o V_o C_V} \int \frac{V}{\lambda^{(i)}} g_i(\lambda) d\lambda_i \quad (35)$$

As a sample calculation using eqs. (34) and (35), we consider the uniaxial extension of natural rubber and use data given in Treloar [12]. Using the simple extension law for a Mooney material and the form of Eq. (33) as guides, the data presented may be reasonably well fitted by:

$$t(\lambda, T) = [.01(\lambda^2 - \lambda^{-1}) - .001] T + 1.7(\lambda - \lambda^{-2}) + 0.4 \text{ (Kg/cm}^2\text{)} \quad (36)$$

Letting $V = V_o$ and $T = 300^\circ K$, tables of $\rho_o C_V \Delta T_{thm}$ and $\rho_o C_V (\Delta T_{eqh} - \Delta T_{thm})$ are presented.

TABLE 2a: $\rho_o C_V \Delta T_{thm}$

λ	$\Delta\lambda$.001	.01	.1	1.
1.0		*	*	.014	2.8
1.1		.00055	.0058	.092	3.2
1.2		.0013	.013	.16	3.9
1.5		.0030	.030	.32	5.0
2.0		.0051	.051	.53	6.9
3.0		.0086	.087	.87	10.2

TABLE 2b: $\rho_o C_V (\Delta T_{eqh} - \Delta T_{thm})$

λ	$\Delta\lambda$.001	.01	.1	1.
1.0		*	*	.061	1.3
1.1		.00078	.0080	.093	1.4
1.2		.00105	.0106	.115	1.5
1.5		.0015	.015	.15	1.7
2.0		.0017	.017	.17	1.7
3.0		.0018	.018	.18	1.8

(table values in Kg/cm²)

No calculations are made at points marked with (*) because the results would be far too sensitive to the constants chosen in eq. (36) to be meaningful.

In the case of uniaxial extension, ΔT_{eqh} consistently overestimates the temperature rise. This overestimation varies from around 20% to over 400% in the examples calculated, and is seen to be more reasonable for higher initial and subsequent extensions. Again, the actual temperature rise is seen to be negligible. For the most extreme case shown, extension of a specimen from $\lambda = 3$ to $\lambda = 4$, thermodynamics predicts an increase of 0.65°C (ΔT_{eqh} is 0.76°C .) In rubber elasticity, such effects may be ignored.

CHAPTER THREE

LINEAR VISCOELASTIC DEFORMATIONS

The thermodynamic analysis of viscoelastic materials is far more complicated than that of elastic media. In the viscoelastic case, stress and strain are no longer simple functions of each other, but can instead be related through differential operators or through more general functionals. Furthermore, deformation processes are irreversible. Comprehensive discussion of these problems may be found in several texts, and reference is made here to Flügge [13], Lee [14], and Christensen [15].

In this work, we shall deal with stress-strain relations in the form of hereditary integrals over the entire previous history of the material. We shall restrict ourselves to consideration of viscoelastic materials which can be described as linear in the sense that a Boltzmann superposition may be employed for complicated or continuously varying stress or strain histories. Discussion of this technique may be found in references [13-15], and further comments, including some examples of limitations and exceptions to this linearity, are available in Staverman and Schwarzl [16], Leaderman [17], and Matsuoka, Aloisio, and Blair [18].

Further complication is introduced by the fact that viscoelastic material properties exhibit marked temperature dependence. Polymer chemists have long noted this behavior and have searched for good macroscopic descriptions as well as microscopic explanations for the phenomena. Ferry [19] and Tobolsky, in conjunction with several co-workers [20-23], provide many data showing a particular relationship between the temperature and the time history of mechanical deformations. Schwarzl and

Staverman [24] discuss the physics of this relationship and provide the term "thermorheologically simple" to denote the class of materials exhibiting it. Morland and Lee [25] have generalized the time-temperature relationship to include the effects of continuously varying temperature history. Many polymers can be modeled as thermorheologically simple. This work, however, deals with small temperature excursions from the equilibrium state, and the question of thermorheological simplicity need not be considered.

Rivlin [26] and Green and Rivlin [27] use functionals to express viscoelastic mechanical properties and they examine the form which these functionals may assume. Coleman [28] applies this procedure to the remaining thermodynamic variables. The same approach is developed in a more phenomenological manner by Hunter [29], Pipkin [30], Breuer and Onat [31], Christensen and Naghdi [32], and Cost [33]. In their work, material laws are expressed in single and multiple integral form.

The dissipation inherent in viscoelasticity necessitates the consideration of non-equilibrium, irreversible thermodynamics. Two of the classical texts in this field, providing reference to the pioneering efforts and discussion of the basic principles involved, are those of De Groot [34] and Prigogine [35].

In the application of irreversible thermodynamics to viscoelasticity, Biot [36,37] expresses entropy in "near-equilibrium" states as a quadratic expansion in an indefinitely large number of "hidden coordinates" and proceeds to derive stress-strain laws analogous to spring-dashpot models of viscoelasticity. Eringen [38] and Schapery [39] apply this procedure to several problems in continuum mechanics.

In 1966, Valanis [40] published a paper showing that solutions to the equations resulting from the hidden variable approach may be expressed as integral operators of the form employed in the phenomenological approach.

In this chapter, thermodynamical equations will be formulated in terms of hidden coordinates, as in reference [39], and will be solved in the manner suggested by Valanis [40]. The solutions will then be used to prove an important symmetry property; this, in turn, will enable us to apply the results to the question of thermomechanical coupling effects.

Keeping our previous notation for entropy, internal energy (both per unit original volume), and temperature, we now denote stress and strain by six-element column vectors, $\underline{\sigma}$ and \underline{q}_1 , respectively, such that $dW = \underline{\sigma}^T d\underline{q}_1$. A column vector of "hidden variables," \underline{q}_2 , is defined as the vector whose elements consist of all the variables necessary to complete the definition of the thermodynamic state. The unknown number of elements of \underline{q}_2 will be denoted by N . As before, our thermodynamic system is an infinitesimal, homogeneous body having uniform temperature.

In the manner of De Groot [34], we define the quantity dS_I , the internal entropy production, by:

$$dS_I = dS - dQ/T \quad (37)$$

We express the entropy as a function of the state variables, U , \underline{q}_1 , and \underline{q}_2 , and introduce the convenient notation:

$${}^1_{\underline{\partial}} S = \left. \frac{\partial S}{\partial \underline{q}_1} \right|_{U, \underline{q}'_1, \underline{q}_2}, \quad {}^2_{\underline{\partial}} S = \left. \frac{\partial S}{\partial \underline{q}_2} \right|_{U, \underline{q}_1, \underline{q}'_2} \quad (38a, b)$$

No work can be done if the deformations, q_1 , are held fixed, and there are no internal irreversibilities associated with processes for which $dq_1 = 0 = dq_2$ (see Schapery [39]). Therefore, from eqs. (1) and (2):

$$\left. \frac{\partial S}{\partial U} \right|_{q_1, q_2} = 1/T \quad (39)$$

From eqs. (38) and (39):

$$TdS = dU + T(\overset{1}{\partial S})^T dq_1 + T(\overset{2}{\partial S})^T dq_2 \quad (40)$$

Rewriting eqs. (1) and (37):

$$dU = dQ + \overset{\sigma}{\sigma}^T dq_1 \quad (41)$$

$$TdS_I = TdS - dQ \quad (42)$$

Summing eqs. (40-42), we have:

$$TdS_I = [\overset{\sigma}{\sigma}^T + T(\overset{1}{\partial S})^T] dq_1 + T(\overset{2}{\partial S})^T dq_2 \quad (43)$$

We define:

$$\overset{x}{x}_1 = \overset{\sigma}{\sigma} + T(\overset{1}{\partial S})^T, \quad \overset{x}{x}_2 = T(\overset{2}{\partial S})^T \quad (44a,b)$$

and write:

$$TdS_I = \overset{x}{x}_1^T dq_1 + \overset{x}{x}_2^T dq_2 \quad (45)$$

Dividing both sides of eq. (45) by a small time increment, we write:

$$T\dot{S}_I = X_1^T \dot{q}_1 + X_2^T \dot{q}_2 \quad (46)$$

where a superposed dot denotes differentiation with respect to time or, as later used under an integral, with respect to the time-like argument.

We now seek more information about the function \dot{S}_I . The coefficients, X_1^T and X_2^T , in eq. (46) can depend upon the state variables, T , q_1 , and q_2 , and, additionally, upon the applied stresses, σ . If we postulate a relationship between these quantities and the rates of change of the system, \dot{q}_1 , \dot{q}_2 , and $\dot{\theta}$, we can write \dot{S}_I as a function of these latter variables directly. Accordingly, we shall expand \dot{S}_I in a truncated Taylor series about an equilibrium state (in which $\dot{\theta} = 0$, $\dot{q}_1 = 0 = \dot{q}_2$), neglecting all terms of higher than second order.

$$\begin{aligned} \dot{S}_I = & \alpha_0 + \alpha_1^T \dot{q}_1 + \alpha_2^T \dot{q}_2 + \alpha_3 \dot{\theta} + \frac{1}{2} \dot{q}_1^T (\beta_1 \dot{q}_1 + \beta_2 \dot{q}_2) + \\ & + \frac{1}{2} \dot{q}_2^T (\beta_2^T \dot{q}_1 + \beta_3 \dot{q}_2) + (\dot{q}_1^T \gamma_1 + \dot{q}_2^T \gamma_2) \dot{\theta} + \frac{1}{2} \gamma_3 \dot{\theta}^2 \end{aligned} \quad (47)$$

β_1 , β_2 , and β_3 are constant matrices, β_1 and β_3 being symmetric. This expansion may be simplified by noting that, according to the second law of thermodynamics, $\dot{S}_I = 0$ in an equilibrium state; thus $\alpha_0 = 0$. The second law also requires that \dot{S}_I never be negative. Since the \dot{q}_i 's and $\dot{\theta}$ may be arbitrarily small and are

not restricted as to sign, this requires that $\alpha_1 = 0 = \alpha_2$, that $\alpha_3 = 0$, and that β_1 and β_3 be positive semi-definite. Since the elements of \underline{q}_2 are all associated with internal dissipation, β_3 must actually be positive definite. Eq. (47) now reduces to

$$\begin{aligned} \dot{S}_I = & \frac{1}{2}[\dot{q}_1^T(\beta_1\dot{q}_1 + \beta_2\dot{q}_2 + \gamma_1\dot{\theta}) + \dot{q}_2^T(\beta_2^T\dot{q}_1 + \beta_3\dot{q}_2 + \gamma_2\dot{\theta}) + \\ & + (\gamma_1^T\dot{q}_1 + \gamma_2^T\dot{q}_2 + \gamma_3\dot{\theta})\dot{\theta}] \end{aligned} \quad (48)$$

Comparison with eq. (46) reveals that the three sets of terms in parentheses are the three "irreversible forces" associated with \dot{q}_1^T , \dot{q}_2^T , and $\dot{\theta}$. We note, however, that the third term is zero, since $\dot{\theta}$ does not appear explicitly in eq. (46). This is reasonable since an increase in temperature of the system, if not accompanied by any changes in the mechanical or "hidden" coordinates, does not cause internal dissipation. This further reduces eq. (48) by requiring that $\gamma_3 = 0$ and that $\gamma_1 = 0 = \gamma_2$. We now write the "irreversible forces" as:

$$\underline{X}_1 = \frac{1}{2}T_0(\beta_1\dot{q}_1 + \beta_2\dot{q}_2) \quad (49a)$$

$$\underline{X}_2 = \frac{1}{2}T_0(\beta_2^T\dot{q}_1 + \beta_3\dot{q}_2) \quad (49b)$$

where T becomes T_0 in keeping with the truncation of the power series (eq. (47)) to second order, and solutions for the \underline{X}_1 involving antisymmetric matrices are suppressed in accordance with the symmetry requirements of Onsager's principle [41,42]. It should also be noted that the quadratic terms in eq. (47), resulting from our assumption of

a relationship between the \dot{q}_i 's and $\dot{\theta}$ and the state variables, reflect Onsager's principle of linear relationship between "forces and fluxes." Onsager's principle is restricted to near-equilibrium states; our derivation is also, due to the truncation of the Taylor series after the quadratic terms.

We now introduce the free enthalpy (Gibbs' function):

$$G = U - TS - \sigma_o^T q_1 \quad (50)$$

where σ_o is the stress in the unstrained state. Differentiating eq. (50) and substituting from eqs. (41-43):

$$dG = -SdT - [\sigma_o + T(^1\partial S)]^T dq_1 - T(^2\partial S)^T dq_2 \quad (51)$$

so that

$$\left. \frac{\partial G}{\partial q_1} \right|_{T, q_1', q_2} = - [\sigma_o + T(^1\partial S)] \quad (52a)$$

$$\left. \frac{\partial G}{\partial q_2} \right|_{T, q_1, q_2'} = - T(^2\partial S) \quad , \quad \left. \frac{\partial G}{\partial T} \right|_{q_1, q_2} = - S \quad (52b, c)$$

If the free enthalpy is expanded about an unstrained equilibrium state (in which $\theta = 0$, $q_1 = 0 = q_2$), we obtain:

$$G = G_o + a_3 \theta + a_1^T q_1 + a_2^T q_2 - \frac{1}{2} b_3 \theta^2 + \frac{1}{2} q_1^T (B_1 q_1 + B_2 q_2) + \frac{1}{2} q_2^T (B_2^T q_1 + B_3 q_2) + (b_1^T q_1 + b_2^T q_2) \theta \quad (53)$$

where B_1 and B_3 are symmetric. It may be shown (see ref. [39]) that $G \geq G_0$ for any nearby states in which $\theta = 0$. Therefore, $a_1 = 0 = a_2$ and B_1 and B_3 must be positive semi-definite. Irreversibility further requires that B_3 be positive definite. The negative sign is assigned to the θ^2 term for later convenience.

Differentiating eq. (53),

$$\frac{\partial G}{\partial \dot{q}_1} = -T \left(\frac{\partial S}{\partial \dot{q}_1} \right) - \sigma_0 = B_1 \dot{q}_1 + B_2 \dot{q}_2 + b_1 \theta \quad (54a)$$

$$\frac{\partial G}{\partial \dot{q}_2} = -T \left(\frac{\partial S}{\partial \dot{q}_2} \right) = B_2^T \dot{q}_1 + B_3 \dot{q}_2 + b_2 \theta \quad (54b)$$

$$\frac{\partial G}{\partial T} = -S = a_3 + b_1^T \dot{q}_1 + b_2^T \dot{q}_2 - b_3 \theta \quad (54c)$$

Hence, from eqs. (44), (49), and (54),

$$\sigma - \sigma_0 = \frac{1}{2} T_0 (\beta_1 \dot{q}_1 + \beta_2 \dot{q}_2) + B_1 \dot{q}_1 + B_2 \dot{q}_2 + b_1 \theta \quad (55a)$$

$$Q = \frac{1}{2} T_0 (\beta_2^T \dot{q}_1 + \beta_3 \dot{q}_2) + B_2^T \dot{q}_1 + B_3 \dot{q}_2 + b_2 \theta \quad (55b)$$

We note that B_3 and β_3 may be simultaneously diagonalized by a non-singular matrix, V (see Franklin [43]). Since both matrices are positive definite, we may further require that V be such that

$$V^T B_3 V = \Lambda \quad \text{and} \quad V^T \beta_3 V = I \quad (56a,b)$$

where I is the $N \times N$ identity matrix and Λ is a diagonal matrix of positive constants. If we define the transformation of variables

$$\underline{q} = V^{-1} \underline{q}_2, \quad (57)$$

eq. (55b) may be rewritten as

$$\underline{0} = \frac{1}{2} T_0 \dot{\underline{q}} + \frac{1}{2} T_0 V^T B_2^T \underline{\dot{q}}_1 + V^T B_2^T \underline{q}_1 + \Lambda \underline{q} + V^T \underline{b}_2 \theta \quad (58)$$

Analogous to a result in Valanis [40],

$$\underline{q}(t) = - \int_0^t e^{-\frac{2}{T_0}(t-\tau)\Lambda} V^T [B_2^T \underline{\dot{q}}_1(\tau) + \frac{2}{T_0} (B_2^T \underline{q}_1(\tau) + \underline{b}_2 \theta(\tau))] d\tau \quad (59)$$

solves eq. (58). Integration by parts yields a more desirable form of this equation:

$$\begin{aligned} \underline{q} = & - \Lambda^{-1} V^T [B_2^T \underline{q}_1 + \underline{b}_2 \theta] - \int_0^t E_x(t-\tau) [V^T B_2^T - \Lambda^{-1} V^T B_2^T] \dot{\underline{q}}_1 d\tau + \\ & + \int_0^t E_x(t-\tau) \Lambda^{-1} V^T \underline{b}_2 \dot{\theta} d\tau \end{aligned} \quad (60)$$

where:

$$E_x(t-\tau) = e^{-\frac{2}{T_0}(t-\tau)\Lambda} \quad (61)$$

and E_x commutes with Λ and Λ^{-1} .

The form of eq. (60) is of great significance. We have started with N "hidden coordinates", q_2 , where N is an unknown, arbitrarily large number. After rearranging these coordinates in a convenient manner (see eq. (57)), we find that they are simply various complicated expressions of the previous deformation and temperature histories. Thus the current state of the thermodynamic system is prescribed as a functional of the temperature and the physical deformation from the onset of activity to the current time. Furthermore, the fact that the elements of Λ are positive shows that this functional is similar to the relaxation modulus, familiar in isothermal viscoelasticity.

Applying eqs. (57), (58), and (60) to eq. (55a), we find that

$$\begin{aligned}
 \sigma - \sigma_0 &= [B_1 - B_2 V \Lambda^{-1} V^T B_2^T] q_1 + [b_1 - B_2 V \Lambda^{-1} V^T b_2] \theta + \\
 &+ \frac{1}{2} T_0 [\beta_1 - \beta_2 V V^T \beta_2^T] \dot{q}_1 + \\
 &+ \int_0^t [B_2 V \Lambda^{-1} - \beta_2 V] E_x(t-\tau) V^T b_2 \dot{\theta} d\tau + \\
 &- \int_0^t [B_2 V \Lambda^{-1} - \beta_2 V] E_x(t-\tau) [\Lambda V^T \beta_2^T - V^T B_2^T] \dot{q}_1 d\tau
 \end{aligned} \tag{62}$$

Referring to eq. (54c) and taking $a_3 = -S|_{\text{equil}} \equiv -S_0$, application of eqs. (57) and (60) yields:

$$\begin{aligned}
s - s_0 &= [b_2^T V \Lambda^{-1} V^T B_2^T - b_1^T] \underline{q}_1 + [b_3 + b_2^T V \Lambda^{-1} V^T b_2] \theta + \\
&+ b_2^T V \int_0^t E_x(t-\tau) [V^T \beta_2^T - \Lambda^{-1} V^T B_2^T] \dot{\underline{q}}_1 d\tau + \\
&- b_2^T V \int_0^t E_x(t-\tau) \Lambda^{-1} V^T b_2 \dot{\theta} d\tau
\end{aligned} \tag{63}$$

Eqs. (62) and (63) can be compared with those resulting from the phenomenological approach, in this case eqs. 3.9 and 3.10 in Christensen [15]. Modifying his notation, to bring it in line with this development, we write:

$$\sigma - \sigma_0 = \int_0^t G(t-\tau, 0) \dot{\underline{q}}_1 d\tau - \int_0^t \phi(0, t-\tau) \dot{\theta} d\tau \tag{64a}$$

$$s - s_0 = \int_0^t \phi^T(t-\tau, 0) \dot{\underline{q}}_1 d\tau + \int_0^t m(t-\tau, 0) \dot{\theta} d\tau \tag{64b}$$

Taking the \underline{q}_1 and θ terms in eqs. (62) and (63) under the integrals, we make the association:

$$\begin{aligned}
G(t-\tau) &= B_1 - B_2 V \Lambda^{-1} V^T B_2^T - [B_2 V - \beta_2 V \Lambda] E_x(t-\tau) \cdot \\
&\cdot [V^T \beta_2^T - \Lambda^{-1} V^T B_2^T] + \frac{1}{2} \tau_0 [\beta_1 - \beta_2 V V^T \beta_2^T] \delta(\tau-t)
\end{aligned} \tag{65a}$$

$$m(t-\tau) = b_3 + b_2^T V \Lambda^{-1} V^T b_2 - b_2^T V E_x(t-\tau) \Lambda^{-1} V^T b_2 \tag{65b}$$

$$\begin{aligned}
\phi(0, t-\tau) &= -b_1 + B_2 V \Lambda^{-1} V^T b_2 - B_2 V E_x(t-\tau) \Lambda^{-1} V^T b_2 + \\
&+ \beta_2 V E_x(t-\tau) V^T b_2
\end{aligned} \tag{65c}$$

$$\begin{aligned} \phi^T(t-\tau,0) = & - b_1^T + b_2^T V \Lambda^{-1} V^T B_2^T + b_2^T V E_x(t-\tau) \cdot \\ & \cdot [V^T \beta_2^T - \Lambda^{-1} V^T B_2^T] \end{aligned} \quad (65d)$$

It can now be seen from eqs. (65c&d) that $\phi(0,t) = \phi(t,0)$, a symmetry property which is assumed in many works [15,29,32,33] but apparently has not been proven previously.

Another interesting feature of the stress-strain law, eq. (62), is the appearance of the \dot{q}_1 term outside the integrals. This term represents the dependence of the stress state upon the instantaneous strain rate, which is now seen to be a natural result of the second-order approximations of entropy production and free enthalpy. The term may be incorporated under the strain-rate history integral by use of the Dirac delta function. This has been done in eq. (65a) to facilitate comparison of eqs. (62) and (64a). It would seem advantageous, however, to consider this term separately from the relaxation modulus. Its presence precludes any instantaneous elastic response. Since solid materials generally exhibit a measurable instantaneous response, the coefficient of \dot{q}_1 is customarily taken to be zero.

Much of the derivation up to this point has been aimed at deducing this symmetry of ϕ in its two arguments. With this accomplished, and with the machinery at hand, we address the question of thermomechanical coupling.

Since most polymeric materials have poor thermal conductivity and since small temperature changes are anticipated, it is reasonable to model most transient deformation tests as adiabatic processes.

This approximation reduces eq. (37) to $dS_I = dS$, which we shall write as

$$\dot{S}_I = \dot{S} \quad (66)$$

From eqs. (48) and (54c), we then have:

$$\frac{1}{2}[\dot{q}_1^T \beta_1 \dot{q}_1 + 2\dot{q}_1^T \beta_2 \dot{q}_2 + \dot{q}_2^T \beta_3 \dot{q}_2] = b_3 \dot{\theta} - b_1^T \dot{q}_1 - b_2^T \dot{q}_2 \quad (67)$$

After application of eqs. (56b) and (57),

$$0 = \frac{1}{2}\dot{q}_1^T \beta_1 \dot{q}_1 + \dot{q}_1^T \beta_2 V \dot{q} + \frac{1}{2}\dot{q}^T \dot{q} - b_3 \dot{\theta} + b_1^T \dot{q}_1 + b_2^T V \dot{q} \quad (68)$$

After elimination of \dot{q} , using eq. (58), and much cancellation of terms:

$$\begin{aligned} 0 = & -b_3 \dot{\theta} - \frac{2}{T_o} b_2^T V V^T b_2 \theta + [b_1^T - b_2^T V V^T \beta_2^T] \dot{q}_1 + \\ & - \frac{2}{T_o} b_2^T V V^T B_2^T q_1 + \frac{4}{T_o} b_2^T V V^T B_2^T q_1 \theta + \frac{2}{T_o} b_2^T V V^T b_2 \theta^2 + \\ & + \frac{2}{T_o} q_1^T B_2 V V^T B_2^T q_1 + \frac{1}{2} \dot{q}_1^T [\beta_1 - \beta_2 V V^T \beta_2^T] \dot{q}_1 - \frac{2}{T_o} b_2^T V \Lambda q + \\ & + \frac{4}{T_o} b_2^T V \Lambda q \theta + \frac{4}{T_o} q_1^T B_2 V \Lambda q + \frac{2}{T_o} q^T \Lambda^2 q \end{aligned} \quad (69)$$

Eq. (60) is used to eliminate q , giving:

$$\begin{aligned}
0 = & -b_3 \dot{\theta} + [b_1^T - b_2^T v v^T \beta_2^T] \dot{q}_1 + \frac{1}{2} \dot{q}_1^T [\beta_1 - \beta_2 v v^T \beta_2^T] \dot{q}_1 + \\
& - \frac{2}{T_0} b_2^T v \int_0^t E_x(t-\tau) \{ [v^T \beta_2^T - \Lambda v^T \beta_2^T] \dot{q}_1 + v^T b_2 \dot{\theta} \} d\tau + \\
& + \frac{4}{T_0^2} b_2^T v \left[\int_0^t E_x(t-\tau) \dot{\theta} d\tau \right] \left[\int_0^t E_x(t-\tau) \{ v^T \beta_2^T - \Lambda v^T \beta_2^T \} \dot{q}_1 d\tau \right] + \\
& + \frac{2}{T_0^2} \left[\int_0^t \dot{q}_1^T \{ \beta_2 v - \beta_2 v \Lambda \} E_x(t-\tau) d\tau \right] \left[\int_0^t E_x(t-\tau) \{ v^T \beta_2^T + \right. \\
& \left. - \Lambda v^T \beta_2^T \} \dot{q}_1 d\tau \right] + \frac{2}{T_0} b_2^T v \left[\int_0^t E_x(t-\tau) \dot{\theta} d\tau \right]^2 v^T b_2
\end{aligned} \tag{70}$$

Since eq. (70) must hold for arbitrarily small values of $\dot{\theta}$ and \dot{q}_1 , the sum of the first-order terms must itself approach zero.

Thus:

$$\begin{aligned}
b_3 \dot{\theta} + \frac{2}{T_0} b_2^T v \int_0^t E_x(t-\tau) v^T b_2 \dot{\theta}(\tau) d\tau = & [b_1^T - b_2^T v v^T \beta_2^T] \dot{q}_1 + \\
& + \frac{2}{T_0} b_2^T v \int_0^t E_x(t-\tau) [\Lambda v^T \beta_2^T - v^T \beta_2^T] \dot{q}_1(\tau) d\tau
\end{aligned} \tag{71}$$

Comparison of eq. (71) with eqs. (65b&c) shows that eq. (71) may be expressed as

$$\frac{d}{dt} \int_0^t m(t-\tau) \dot{\theta}(\tau) d\tau = - \frac{d}{dt} \int_0^t \phi^T(t-\tau) \dot{q}_1(\tau) d\tau \tag{72}$$

A similar result is derived by different means by Christensen [15].

Examination of eqs. (64) gives physical insight into the nature of the functions m and ϕ . ϕ , in eq. (64a), is the viscoelastic material function whose elastic analogue is the product of the volumetric coefficient of thermal expansion and the isothermal bulk modulus. In eq. (64b), m is the creep-type function corresponding to the heat capacity at constant volume in the elastic case. From the second law of thermodynamics, we see that this function must be non-decreasing. ϕ is harder to classify. The contribution of the thermal expansion will be a creep-type function, while the bulk modulus will be a relaxation-type function. Their product will be a hybrid of sorts, probably increasing for some short time and then slowly decreasing again.

While the heat capacity, thermal expansion, and bulk modulus have all been shown experimentally to exhibit time-dependent behavior, such effects are usually small and the functions can be sufficiently well approximated by step functions. Constant values for C_V , α , and K are reported in most handbooks. Taking these constants to be appropriate asymptotic values, and noting that isotropy requires that ϕ take the form

$$\phi = -\alpha K(1,1,1,0,0,0)^T \quad (73)$$

(where the strain vector, \underline{q}_1 , is arranged in the usual fashion; the three shear components following the three normal components), eq. (72) can be simplified to:

$$\rho_0 C_V \dot{\theta} = -\alpha K T_0 \dot{\epsilon}_{kk} \quad (74)$$

Equation (74) specifies the thermodynamic relationship between volumetric strain and the induced thermal change. It should be noted that a very important phenomenon, that of heating due to shear dissipation, is not accounted for in this formula. The contribution of shear deformation to thermal change has been lost in the linearization which entered the derivation in eqs. (54) and (71).

Heating due to shear deformation must be independent of the sense of shear when the deformation occurs from an unstrained state. Consequently, the dependence of $\dot{\theta}$ on $\dot{\epsilon}$ must be an even function in each of the shear deformation components and cannot be included in a linear approximation.

To include this phenomenon in the present report would not only require retention of the quadratic terms currently present in eq. (70), but would also necessitate the introduction of cubic terms in the expansion of the Gibbs' free enthalpy (eq. (53)) so that quadratic terms would appear in the expression for entropy (eq. (54c)).

The ensuing analysis becomes quite involved and is not included in this report. Derivation of a phenomenological expression for heating due to shear dissipation remains a subject for future investigation.

CHAPTER FOUR

COMPARISON AND SUMMARY

Although the derivations necessary to find the temperature change due to deformation differ in a great many details between the infinitesimal elastic and viscoelastic cases, the results (eqs. (15) and (74)) are essentially identical. It remains to evaluate the material properties of significance, and to determine from them the extent to which thermomechanical coupling effects need to be considered.

Since eq. (74) will be applied to small deformations of metals, rubbers, and plastics alike, data are presented in Table Three for all three classes of material. Calculations have been made for a temperature of 25°C. $\Delta\epsilon_{kk}$ is the volumetric strain necessary to induce a temperature change of one degree centigrade. P is the hydrostatic pressure necessary to cause that volumetric strain. ϵ_{lin} is the longitudinal strain associated with $\Delta\epsilon_{kk}$ in a uniaxial tension test. Units used in Table Three are: α , $10^{-5}/^{\circ}\text{C}$; ρ , gram/cm^3 ; E , K , $10^4 \text{ cal}/\text{cm}^3$; C_v , $\text{cal}/\text{gram}/^{\circ}\text{C}$; P , 10^4 psi .

The volumetric strain associated with a one degree change in temperature is seen to vary from about 0.1% to 0.7%, with the polymeric materials exhibiting much more diversity than the metals. The compressive stress associated with this volume change varies from 500 to 4000 psi among the polymers, and from 700 to 5000 psi among the metals.

Also calculated is the strain that is necessary in uniaxial tension to cause a temperature drop of one degree centigrade. The values for metals are fairly consistent, ranging from 0.44% to 0.60%, with the

TABLE 3. TEMPERATURE CHANGE VS. VOLUMETRIC STRAIN⁹

MATERIAL	α	K	E	ρ_o	C_V	$\frac{\alpha KT}{\rho_o C_V}$	$\Delta \epsilon_{kk}$	P	ϵ_{lin}
METALS									
Aluminum	7.5	1.80	1.7	2.70	.204	730.	.0014	1.5	.0044
Copper	5.0	3.29	3.2	8.96	.0893	610.	.0016	3.2	.0050
Iron	3.1	3.34	4.4	7.39	.107	390.	.0026	5.3	.0060
Lead	8.7	1.10	0.40	11.35	.0281	890.	.0011	0.73	.0090
Nickel	3.9	4.49	5.1	8.90	.105	560.	.0018	4.9	.0048
Silver	5.7	2.48	1.9	10.5	.0540	740.	.0013	2.0	.0052
Tin	6.0	1.39	1.2	7.31	.0523	650.	.0015	1.3	.0054
Zinc	10.5	1.66	2.5	7.0	.0851	870.	.0011	1.1	.0022
Steel	3.5	3.6	4.5	7.9	.118	400.	.0025	5.4	.0059
RUBBERS									
Polyisoprene (Hevea)	67.	.047		.913	.386	270.	.0038	0.11	
Polyisoprene (Ebonite)	19.	.10	.072	1.17	.322	150.	.0067	0.41	.028
P'butadiene- co-styrene	53.	.060	.11	1.15	.314	260.	.0038	0.14	.0063
Neoprene	60.	.050		1.23	.476	150.	.0066	0.20	
PLASTICS									
Polystyrene	23.	.072	.079	1.05	.28	170.	.0060	0.26	.016
Polyvinyl- chloride	24.	.098		1.41	.24	210.	.0048	0.29	
P'methyl Meth- acrylate	27.	.096	.099	1.17	.31	210.	.0047	0.27	.014
Low density P'ethylene (75.)		.079	.024	.91	.25	780.	.0013	0.062	.013
High density P'ethylene		.11		.96	.21	1200.	.00082	0.055	
Nylon 6	62.	.079		1.1	.26	510.	.0020	0.096	

⁹ Data from [5], [9], [44] for metals; [7], sec. 6., for rubbers; and [8], tables 4.10, 5.3, and 9.3 for polymers.

exceptions of lead (0.90%) and zinc (0.22%). These two metals differ primarily in their Poisson's ratios. It should be noted that ϵ_{lin} exceeds the elastic limit for most, if not all, the metals presented. This does not imply that such strains are obtainable elastically; it is merely a result of the choice of 1° C. as a benchmark. Since the strain-temperature effect is linear, these values can be used in calculating the thermal effect of lesser strains.

Calculations were also made for those polymers for which values of Young's modulus were found. These materials show more variation; ϵ_{lin} ranging from 0.6% to almost 3%. The discussion concerning ϵ_{lin} for metals is applicable to the rubbers and plastics as well.

The thermomechanical coupling effect has been shown to be insignificant in the infinitesimal transient deformation of solids in almost all cases. It should be reiterated that eqs. (15), (26), and (74) can be used to accurately predict these small thermal changes, allowing one to decide, in light of the known thermal dependence of the mechanical properties and the accuracy desired, if thermomechanical coupling effects need be considered. It has been shown in earlier chapters that the equivalent heat argument is wholly unsatisfactory for such purposes.

The insignificance of the thermomechanical coupling effect has also been shown for the finite elastic deformation of rubbers. Finite, non-linear deformations of metals and viscoelastic materials are not considered in this work.

BIBLIOGRAPHY

1. Nowacki, W., Thermoelasticity, Addison Wesley, Palo Alto, Cal. (1962).
2. Biot, M. A., "Thermoelasticity and Irreversible Thermodynamics",
J. Applied Physics, 27, p. 240 (1956).
3. Truesdell, C., and Noll, W., "The Non-Linear Field Theories of
Mechanics", Handbuch der Physik III/3, ed. S. Flügge, Springer-
Verlag, Berlin (1965).
4. Rivlin, R. S., "Large Elastic Deformations of Isotropic Materials.
IV. Further Developments of the General Theory", Phil. Trans. Roy.
Soc., A241, p. 381 (1948).
5. CRC Handbook of Tables for Applied Engineering Science, 2nd ed.,
Chemical Rubber Publ. Co., Cleveland, Ohio (1973).
6. Smithells, C. J., Metals Reference Handbook, v.III, 4th ed., Plenum
Press, New York (1967).
7. Brandrup, J., and Immergut, E. H., Polymer Handbook, Interscience,
New York (1966).
8. Van Krevelen, D. W., Properties of Polymers: Correlation with Chem-
ical Structure, Elsevier, Amsterdam (1972).
9. Pearson, C. E., Theoretical Elasticity, Harvard Press, Cambridge,
Mass. (1959).
10. Meyer, K.H., and Ferri, C., "On the Elasticity of Rubber" (in French),
Helvetica Chimica Acta, 18, p. 570 (1935).
11. Anthony, R. L., Caston, R. H., and Guth, E., "Equations of State
for Natural and Synthetic Rubberlike Materials. I. Unaccelerated
Natural Soft Rubber", J. Phys. Chem., 46, p. 826 (1942).
12. Treloar, L. R. G., The Physics of Rubber Elasticity, 2nd ed., Oxford
University Press, London (1958).

13. Flügge, W., Viscoelasticity, Ginn/Blaisdell, Waltham, Mass. (1967).
14. Lee, E. H., "Viscoelasticity", Handbook of Engineering Mechanics, ed. W. Flügge, ch. 53, McGraw-Hill, New York (1962).
15. Christensen, R. M., Theory of Viscoelasticity, an Introduction, Academic Press, New York (1971).
16. Staverman, A. J., and Schwarzl, F., "Linear Deformation Behavior of High Polymers", Die Physik der Hochpolymeren, ed. H. Stuart, Springer-Verlag, Berlin (1956).
17. Leaderman, H., "Creep, Elastic Hysteresis, and Damping in Bakelite under Torsion", J. Applied Mechanics (Trans. ASME), 61, p. A-79 (1939).
18. Matsuoka, S., Aloisio, C. J., and Blair, H. E., "Interpretation of the Shift of Relaxation Time with Deformation in Glassy Polymers in Terms of Excess Enthalpy", J. Appl. Phy., 44, p. 4265 (1973).
19. Ferry, J. D., Viscoelastic Properties of Polymers, Wiley, London (1961).
20. Andrews, R. D., Hofman-Bang, N., and Tobolsky, A. V., "Elastoviscous Properties of Polyisobutylene. I. Relaxation of Stress in Whole Polymer of Different Molecular Weights at Elevated Temperatures", J. Polymer Science, 3, p. 669 (1948).
21. Bischoff, J., Catsiff, E., and Tobolsky, A. V., "Elastoviscous Properties of Amorphous Polymers in the Transition Region. I.", J. American Chemical Soc., 74, p. 3378 (1952).
22. Catsiff, E., and Tobolsky, A. V., "Elastoviscous Properties of Amorphous Polymers in the Transition Region. II. Stress-Relaxation of Butadiene-Styrene Copolymers", J. Appl. Phy., 25, p. 1092 (1954).
23. Tobolsky, A. V., "Stress Relaxation Studies of the Viscoelastic Properties of Polymers", J. Appl. Phy., 27, p. 673 (1956).

24. Schwarzl, F., and Staverman, A. J., "Time-Temperature Dependence of Linear Viscoelastic Behavior", J. Appl. Phys., 23, p. 838 (1952).
25. Morland, L. W., and Lee, E. H., "Stress Analysis for Linear Viscoelastic Materials with Temperature Variation", Trans. Soc. Rheology, IV, p. 233 (1960).
26. Rivlin, R. S., "Constitutive Equations for Classes of Deformations", Viscoelasticity, Phenomenological Aspects, ed. J. Bergen, p. 93, Academic Press, New York (1960).
27. Green, A. E., and Rivlin, R. S., "The Mechanics of Non-Linear Materials with Memory", Arch. Rat. Mech. Anal., 1, p. 1, (1957).
28. Coleman, B. D., "Thermodynamics of Materials with Memory", Arch. Rat. Mech. Anal., 17, p. 1 (1964).
29. Hunter, S. C., "Tentative Equations for the Propagation of Stress, Strain, and Temperature Fields in Viscoelastic Solids", J. Mech. and Phys. of Solids, 9, p. 39 (1961).
30. Pipkin, A. C., "Small Finite Deformations of Viscoelastic Solids", Rev. Modern Physics, 36, p. 1034 (1964).
31. Breuer, S., and Onat, E. T., "On the Determination of Free Energy in Linear Viscoelastic Solids", Z. Angew. Math. and Phys., 15, p. 184 (1964).
32. Christensen, R. M., and Naghdi, P. M., "Linear Non-Isothermal Viscoelastic Solids", Acta Mechanica, 3, p. 1 (1967).
33. Cost, T. L., "A Free Energy Functional for Thermorheologically Simple Materials", Acta Mechanica, 17, p. 153 (1973).
34. De Groot, S. R., Thermodynamics of Irreversible Processes, North-Holland, Amsterdam (1952).

35. Prigogine, I., Thermodynamics of Irreversible Processes, 3rd ed., Wiley, New York (1967).
36. Biot, M. A., "Theory of Stress-Strain Relations in Anisotropic Viscoelasticity and Relaxation Phenomena", J. Appl. Phy., 25, p. 1385 (1954).
37. Biot, M. A., "Linear Thermodynamics of the Mechanics of Solids", Proc. 3rd U.S. Nat. Congr. of Appl. Mech. (ASME), p. 1 (1958).
38. Eringen, A. C., "Irreversible Thermodynamics and Continuum Mechanics", Physical Review, ser. 2, 117, p. 1175 (1960).
39. Schapery, R. A. "Application of Thermodynamics to Thermomechanical, Fracture, and Birefringent Phenomena in Viscoelastic Media", J. Appl. Phy., 35, p. 1451 (1964).
40. Valanis, K. C., "Thermodynamics of Large Viscoelastic Deformation", J. Math. and Physics, 45, p. 197 (1966).
41. Onsager, L., "Reciprocal Relations in Irreversible Thermodynamics. I". Phy. Rev., ser. 2, 37, p. 405 (1931).
42. Onsager, L., "Reciprocal Relations in Irreversible Thermodynamics. II.", Phy. Rev., ser. 2, 38, p. 2265 (1931).
43. Franklin, J. N., Matrix Theory, Prentice Hall, Englewood Cliffs, New Jersey (1968).
44. Hultgren, R., Orr, R. L., Anderson, P.D., and Kelley, K. K., Selected Values of Thermodynamic Properties of Metals and Alloys, Wiley and Sons, New York (1963).

ACKNOWLEDGEMENTS

The author is indebted to Professor E. H. Lee for his guidance in this research and to the Office of Naval Research for its sponsorship of the project.