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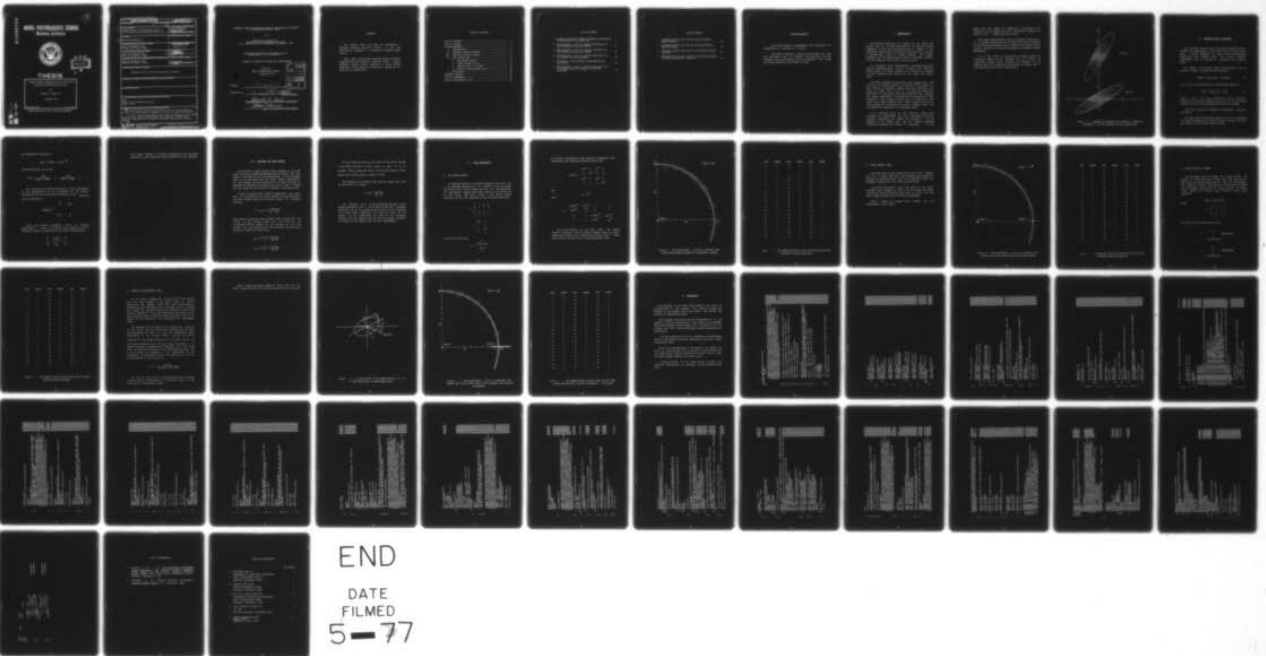
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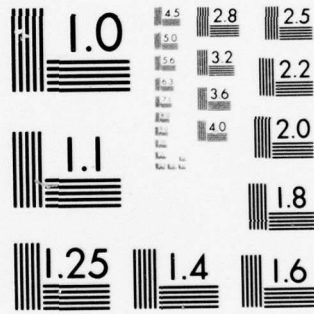
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THESIS

EXTENDED KALMAN FILTERING APPLIED TO THE POSITION
LOCATING AND REPORTING SYSTEM (PLRS)

by

Bernard M. de Mahy, Jr.

December 1976

Thesis Advisor: H. A. Titus

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REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER	2. GOVT ACCESSION NO. 9	3. RECIPIENT'S CATALOG NUMBER	
4. TITLE (and Subtitle) Extended Kalman Filtering Applied to the Position Locating and Reporting System (PLRS).		5. TYPE OF REPORT & PERIOD COVERED Master's Thesis, December 1976	
7. AUTHOR(s) Bernard M. de Mahy, Jr		6. PERFORMING ORG. REPORT NUMBER	
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940 ✓		8. CONTRACT OR GRANT NUMBER(s)	
11. CONTROLLING OFFICE NAME AND ADDRESS Naval Postgraduate School Monterey, California 93940		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 12 58 p.	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) Naval Postgraduate School Monterey, California 93940		12. REPORT DATE 11 Dec 1976	
		13. NUMBER OF PAGES 59	
		15. SECURITY CLASS. (of this report) Unclassified	
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
18. SUPPLEMENTARY NOTES			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) PLRS Position Locating Reporting System Kalman Filter			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Marine Corps and Army are developing a Position Locating Reporting System to aid the battlefield commander in locating his assets during battle. This study has applied Extended Kalman Filtering techniques to that problem, evolving from a simple Extended Kalman Filter Observer to three moving observers, whose position is uncertain, estimating the position of another unit.			

EXTENDED KALMAN FILTERING APPLIED TO THE POSITION LOCATING
AND REPORTING SYSTEM (PLRS)

by

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Captain, United States Marine Corps
B.S., University of Southwestern Louisiana, 1969

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the
NAVAL POSTGRADUATE SCHOOL
December 1976

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NTIS	White Section	<input checked="" type="checkbox"/>
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UNANNOUNCED		<input type="checkbox"/>
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ABSTRACT

The Marine Corps and Army are developing a Position Locating Reporting System to aid the battlefield commander in locating his assets during battle.

This study has applied Extended Kalman Filtering techniques to that problem, evolving from a simple Extended Kalman Filter Observer to three moving observers, whose position is uncertain, estimating the position of another unit.

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ACKNOWLEDGEMENTS

The author wishes to acknowledge the assistance of Professors H. A. Titus and D. E. Kirk.

The author, moreover, wishes to acknowledge the love and sacrifices that he received from his wife, Pam, and children, Marc and Jennifer, while he conducted this study and hereby dedicates this Thesis to them.

I. INTRODUCTION

The precise location of all assets in and about the battle area is of prime importance to the tactical Marine Commander. In the past locating has had to depend on the individual knowing his own position and being able to report it through radio links to higher command. This system suffered from the limitations of terrain, daylight, weather, and the volume of radio traffic during battle.

To alleviate these shortcomings the Marine Corps and Army are investigating a Position Locating and Reporting System (PLRS) to collect, process, and, display the location of units, vehicles, and aircraft in and about the battle area.

The PLRS consists of field units and a master unit. The field unit is compact enough to be carried in the field by a man, vehicle, or aircraft. These units will determine the range to other field units in the area and report this information to the master unit for processing and display. The range information is determined by measuring the time required to send a signal from one unit to another and back again plus some "system" delay. When a unit's position is being updated it is referred to as the "Update" unit; and all others are referred to as "Ranging" units.

In a previous study in this area,[1], tests were conducted to investigate the use of the error ellipse in visually displaying the degree of uncertainty of the position of an update unit and the effect of numerous updates on reducing that degree of uncertainty. It was

found that the degree of uncertainty is reduced in the direction of the ranging unit with consecutive updates as shown in Fig 1 taken from that study.

That study also simulated one jet aircraft flying Mach 1 in a constant radius turn as an update unit being ranged on by two stationary ranging units to explore the proper random forcing excitation covariance necessary for adequate filter performance.

It is the intent of this study to further expand the simulation begun in the previous work by adding an additional ranging unit, allowing the movement of the ranging units, and considering the effect of ranging from a unit whose position is not known exactly

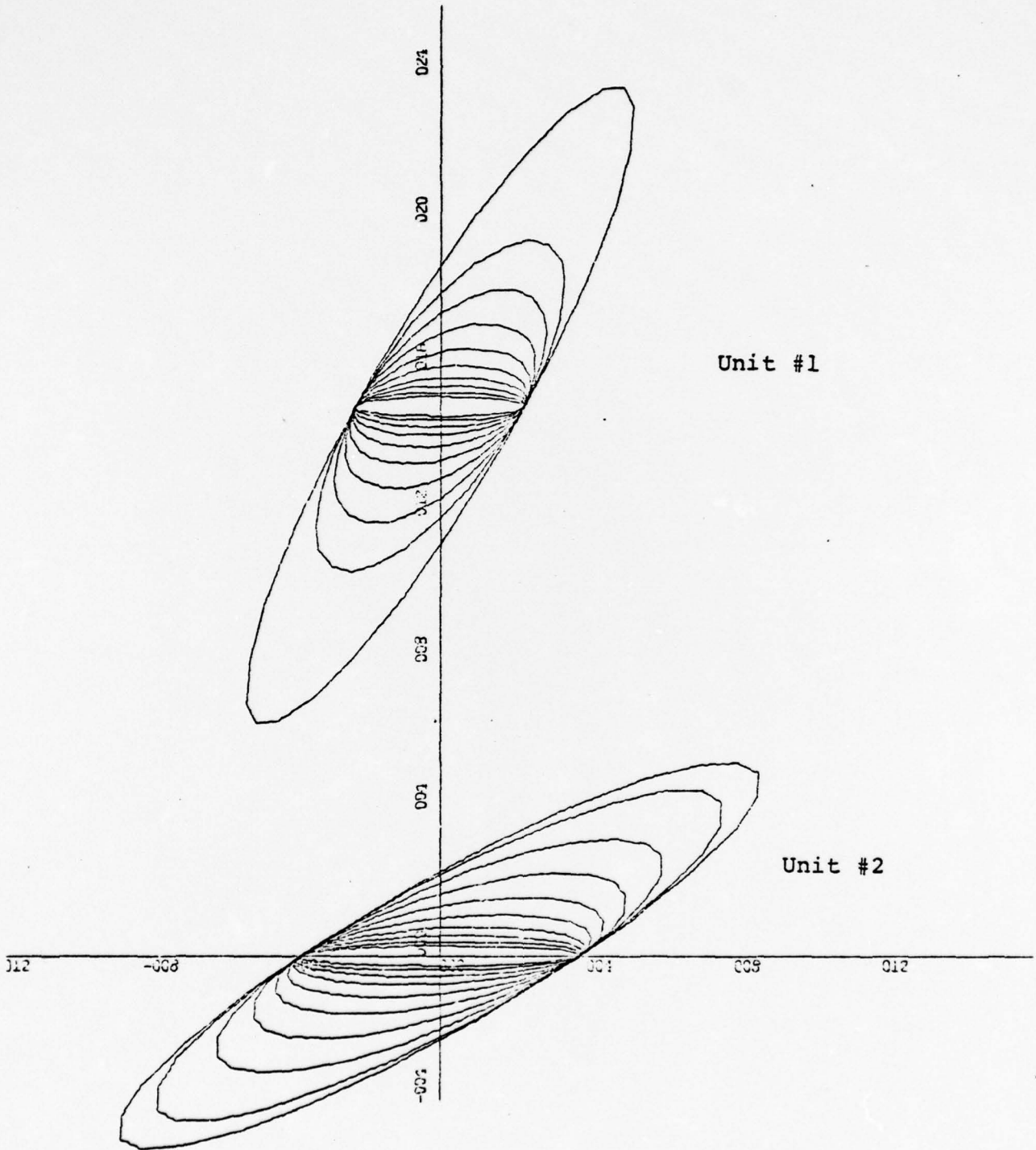


Figure 1 - CONSECUTIVE UPDATES WILL REDUCE THE DEGREE OF UNCERTAINTY IN THE DIRECTION OF THE RANGING UNIT

II. EXTENDED KALMAN FILTERING

The Extended Kalman Filter is widely documented and no attempt at a development of that theory will be made in this work. A brief treatment has been included to establish nomenclature and formulas used. For a more complete development one is referred to reference [2] or similar texts.

As defined in this work, PLRS is described by a set of discrete, linear, cartesian system equations

$$\underline{x}(k+1) = \underline{\phi}(k) \underline{x}(k) + \underline{\Gamma}(k) \underline{w}(k) \quad (1)$$

and a set of discrete non-linear measurement equations

$$\underline{z}(k) = \underline{m}(\underline{x}(k), k) + \underline{v}(k) \quad (2)$$

where $\underline{\phi}$ and $\underline{\Gamma}$ are linear functions and \underline{m} is a nonlinear function of the state variables $\underline{x}(k)$; $\underline{w}(k)$ is the excitation noise and $\underline{v}(k)$ is the measurement noise of the system.

The plant noises are considered uncorrelated, zero-mean, and white.

The non-linear measurement equations can be linearized by expanding equation (2) around the best estimate at time k and using the first-order terms yielding

$$\underline{z}(k) = \underline{H}(k) \underline{x}(k) + \underline{v}(k)$$

where

$$H(k) = \frac{\partial m}{\partial \underline{x}} \underline{x} = \underline{\hat{x}}(k/k-1) \quad (3)$$

$\underline{\hat{x}}(k/k)$ is the estimated value of the state at k after the k^{th} measurement and $\underline{\hat{x}}(k/k-1)$ is the predicted value of the state at time k before the k^{th} measurement.

The state error vector is

$$\underline{\hat{x}}'(k/k) = \underline{\hat{x}}(k/k) - \underline{\hat{x}}(k)$$

and the predicted error vector is

$$\underline{\hat{x}}'(k/k-1) = \underline{\hat{x}}(k/k-1) - \underline{x}(k)$$

The covariance of the state error matrix is

$$P(k/k) = E[\underline{\hat{x}}'(k/k) \underline{\hat{x}}'^T(k/k)]$$

and the predicted covariance of the state error matrix is

$$P(k/k-1) = E[\underline{\hat{x}}'(k/k-1) \underline{\hat{x}}'^T(k/k-1)] .$$

The state excitation matrix is

$$Q(k) = E[\underline{\Gamma}(k) \underline{w}(k) \underline{w}^T(k) \underline{\Gamma}^T(k)]$$

and the measurement noise covariance matrix is

$$R(k) = E[\underline{v}(k) \underline{v}^T(k)] .$$

The equations that made up the Kalman Filter used in this work are as follows:

$$P(k/k-1) = \underline{\phi}(k) P(k/k) \underline{\phi}^T(k) + Q(k)$$

$$G(k) = P(k/k-1) H^T(k) [H(k) P(k/k-1) H^T(k) + R(k)]^{-1}$$

$$P(k/k) = [I - G(k) H(k)] P(k/k-1)$$

$$\hat{\underline{x}}(k/k) = \hat{\underline{x}}(k/k-1) + G(k) [\underline{z}(k) - H(k) \hat{\underline{x}}(k/k-1)]$$

$$\hat{\underline{x}}(k/k-1) = \underline{\phi}(k) \hat{\underline{x}}(k/k)$$

$$\underline{z}(k) = \underline{m}(\hat{\underline{x}}(k/k-1), k)$$

Since the only observations in this system are ranges,

the observation equation is

$$\underline{z}(k) = [x^2(k) + y^2(k)]^{1/2} ;$$

and from equation (3) we get

$$H(k) = \frac{x(k)}{x^2(k) + y^2(k)} \quad 0 \quad \frac{y(k)}{x^2(k) + y^2(k)} \quad 0 .$$

The covariance of estimation error, P , is an expression of the uncertainty in the estimation of the states. Considering only the estimation's position error, P position can be expressed as

$$P_{\text{position}} = \begin{matrix} \sigma_x^2 & \sigma_x \sigma_y \\ \sigma_y \sigma_x & \sigma_y^2 \end{matrix}$$

Since the position estimation error is normally distributed, a curve of constant error probability can be defined by using the exponent of the normal distribution,

$$\frac{x^2}{\sigma_x^2} - \frac{2r_{xy}}{\sigma_x \sigma_y} + \frac{y^2}{\sigma_y^2}$$

This curve defines an ellipse. Graphically, for the given probability, the estimation may be anywhere in that ellipse.

III. CHOOSING THE BEST RANGER

To move from a simple Kalman Filter observer to the PLRS model the first problem encountered was to choose the best ranger from which to take the measurement. In the previous work [1], it was shown that the most useful measurement, the one causing the most reduction in the error ellipse, is obtained by observing the update unit from a point aligned with the major axis of the error ellipse of the update unit.

To find the ranger most closely aligned with the major axis of the update unit's error ellipse the orientation of the error ellipse must first be found using the following equation.

$$\theta = \frac{1}{2} \tan^{-1} \frac{2 \text{Cov}(x,y)}{\sigma_x^2 - \sigma_y^2}$$

This angle(θ) gives the angle between -90° and 90° that the x-axis of the ellipse makes with the x-axis of the co-ordinate system. Looking at the ellipse in this new posture one can find the new "Uncorrelated" variances that define the major and minor axes.

$$\sigma_x'^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} + \frac{\text{Cov}(x,y)}{\sin 2\theta}$$

$$\sigma_y'^2 = \frac{\sigma_x^2 + \sigma_y^2}{2} - \frac{\text{Cov}(x,y)}{\sin 2\theta}$$

If σ_x^2 is greater than σ_y^2 the x-axis of the error ellipse is the major axis and θ is the angle we seek. If σ_y^2 is greater than σ_x^2 then the y-axis of the error ellipse is the major axis and the angle we seek is $\theta + 90^\circ$.

The bearing of the update unit from the ranger must then be found and it is simply

$$\beta = \text{Tan}^{-1} \frac{Y_u - Y_R}{X_u - X_R} .$$

The absolute value of the difference between θ , after proper correction, and β was chosen as the best alignment indicator; but to be aligned and to be 180° out of alignment is of equal value; therefore the absolute value of the cosine of the differences was used as the alignment indicator and the ranger found to have the largest indicator was chosen as the ranging unit for that measurement.

IV. PLRS SIMULATION

A. TWO RANGING UNITS

In previous work,[1], the PLRS simulation was setup for a jet aircraft flying Mach 1 in a constant 10 Km turn about the origin to act as the update unit for all measurements. Two stationary ranging units were placed at the origin and at 10Km north, 10Km east. Using a one second sample interval, the jet was described by the following matrices:

$$\phi = \begin{array}{cccc} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{array}$$

$$\Gamma = \begin{array}{cc} 0.5 & 0 \\ 1 & 0 \\ 0 & 0.5 \\ 0 & 1 \end{array}$$

Its initial state was

$$\underline{x} = \begin{array}{c} 0 \\ 0.333 \text{ Km/s} \\ 10 \text{ Km} \\ 0 \end{array}$$

Its initial covariance of error matrix, measurement noise covariance, and excitation forcing matrix were

$$P(1/0) = \begin{bmatrix} 10^{-4} & 0 & 10^{-4} & 0 \\ 0 & 10^{-4} & 0 & 0 \\ 10^{-4} & 0 & 10^{-4} & 0 \\ 0 & 0 & 0 & 10^{-4} \end{bmatrix}$$

and

$$R = 10^{-4}$$

with

$$Q = \begin{bmatrix} 2.5 \times 10^{-5} & 5 \times 10^{-5} & 0 & 0 \\ 5 \times 10^{-5} & 10^{-4} & 0 & 0 \\ 0 & 0 & 2.5 \times 10^{-5} & 5 \times 10^{-5} \\ 0 & 0 & 5 \times 10^{-5} & 10^{-4} \end{bmatrix}$$

Fig 2 is a display of its final runs. The filter tracked accurately and the error ellipses shown are twenty times their actual size to make them visible. Table 1 shows which was the ranging unit at each measurement time.

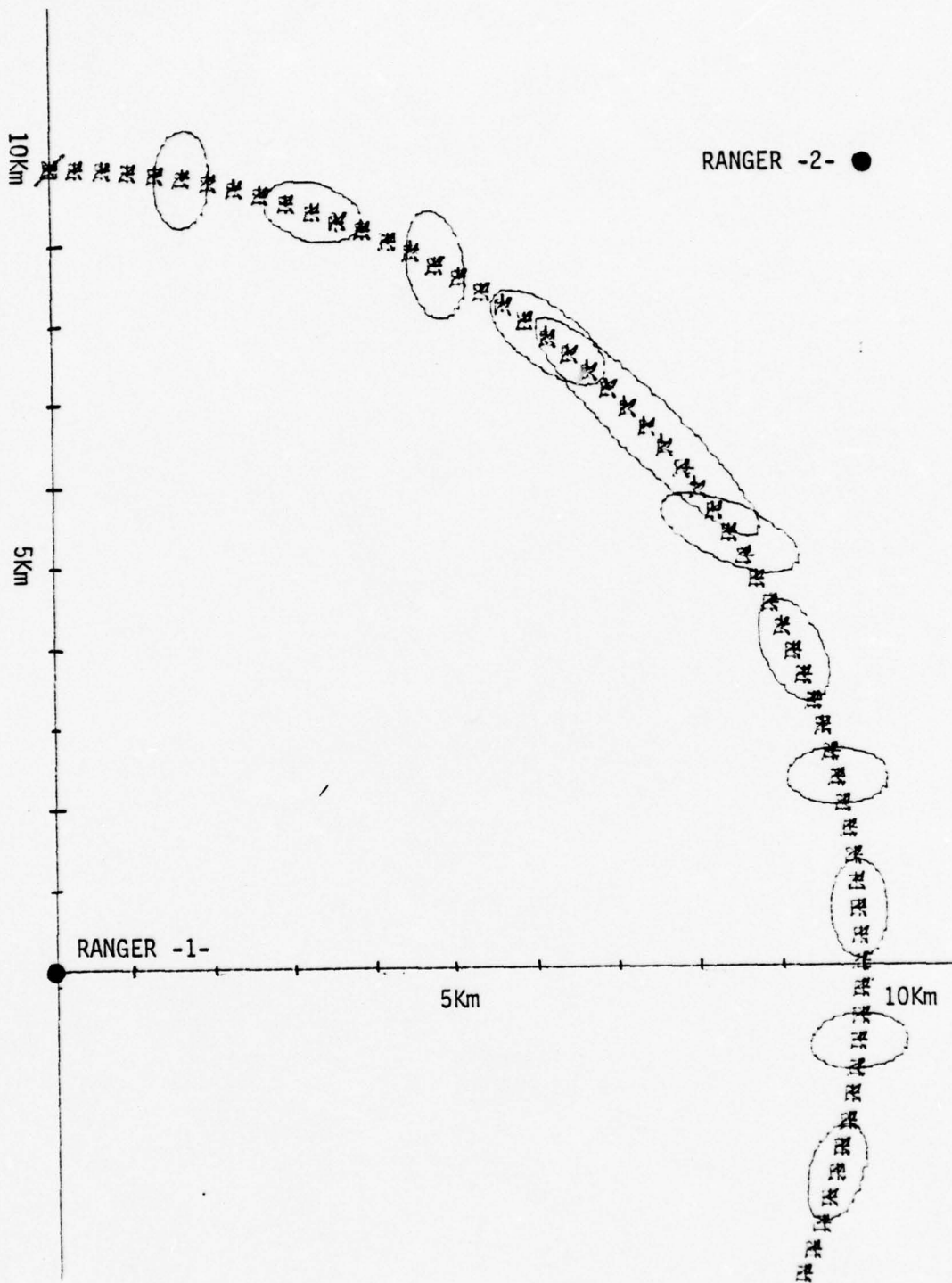


Figure 2 - PLRS SIMULATION - A JET IN A CONSTANT 10KM RADIUS TURN FLYING BETWEEN TWO STATIONARY RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	1	42	2
3	2	23	2	43	1
4	1	24	1	44	2
5	2	25	1	45	1
6	1	26	2	46	2
7	2	27	1	47	1
8	1	28	2	48	2
9	2	29	1	49	1
10	1	30	2	50	2
11	2	31	1	51	1
12	1	32	2	52	2
13	2	33	1	53	1
14	1	34	2	54	2
15	2	35	1	55	1
16	1	36	2	56	2
17	2	37	1	57	1
18	1	38	2	58	2
19	2	39	1	59	1
20	1	40	2	60	2

TABLE 1 - THE RANGER CHOSEN AT EACH TIME FOR THE PLSR TWO STATIONARY RANGER SIMULATION

B. THREE RANGING UNITS

The first step of this study was to add a third ranging unit at 0 north, 10Km east. The algorithm was enlarged to include the additional unit and its comparison with the alignment indicators of the other ranging units.

It can be seen in Fig 3 that the size of the error ellipses were reduced in size in the mid-range area where the jet and the two original units were in line; and the third ranger provides the triangular measurement.

Table 2 shows the ranging unit chosen for the measurement at each time k.

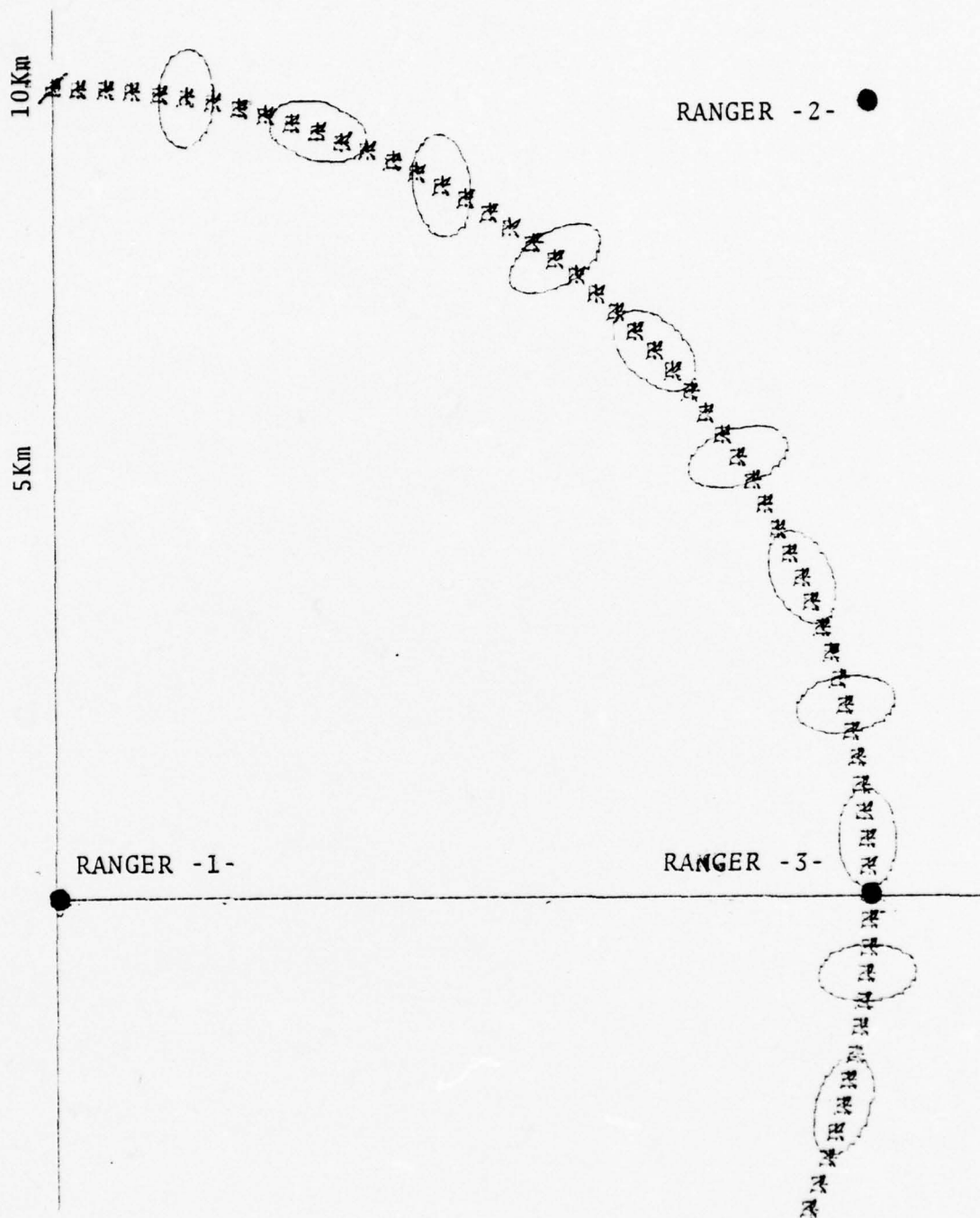


Figure 3 - PLRS SIMULATION - A JET IN A CONSTANT 10KM RADIUS TURN FLYING AMONG THREE STATIONARY RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	3	42	3
3	2	23	2	43	1
4	1	24	3	44	3
5	2	25	1	45	1
6	1	26	3	46	3
7	2	27	1	47	1
8	1	28	3	48	2
9	2	29	1	49	1
10	1	30	3	50	2
11	2	31	1	51	1
12	1	32	3	52	3
13	2	33	1	53	1
14	3	34	3	54	3
15	2	35	1	55	1
16	3	36	3	56	3
17	2	37	1	57	1
18	3	38	3	58	3
19	2	39	1	59	1
20	3	40	3	60	3

TABLE 2 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE STATIONARY RANGER SIMULATION

C. RANGING UNITS IN MOTION

In the second step the rangers are given motion. The rangers at the origin and at 10Km north, 10Km east were to move north and south respectively at 3Kts as infantrymen. The ranger at 0 north, 10Km east was to move west at 120Kts as a helicopter. Again using one second sample intervals, their motion was defined using discrete linear state equations

$$x(k+1) = \phi(k) x(k) ,$$

where

$$\phi = \begin{bmatrix} 1 & 1 & 0 & 0 \\ 0 & 1 & 0 & 0 \\ 0 & 0 & 1 & 1 \\ 0 & 0 & 0 & 1 \end{bmatrix}$$

with the initial states shown below;

$$x = \begin{bmatrix} 0 \\ 0 \\ 0 \\ 1.67 \times 10^3 \text{ Km/s} \end{bmatrix} \quad \text{INFANTRYMAN}$$

$$x = \begin{bmatrix} 10 \\ 0 \\ 10 \\ -1.67 \times 10^3 \text{ Km/s} \end{bmatrix} \quad \text{INFANTRYMAN}$$

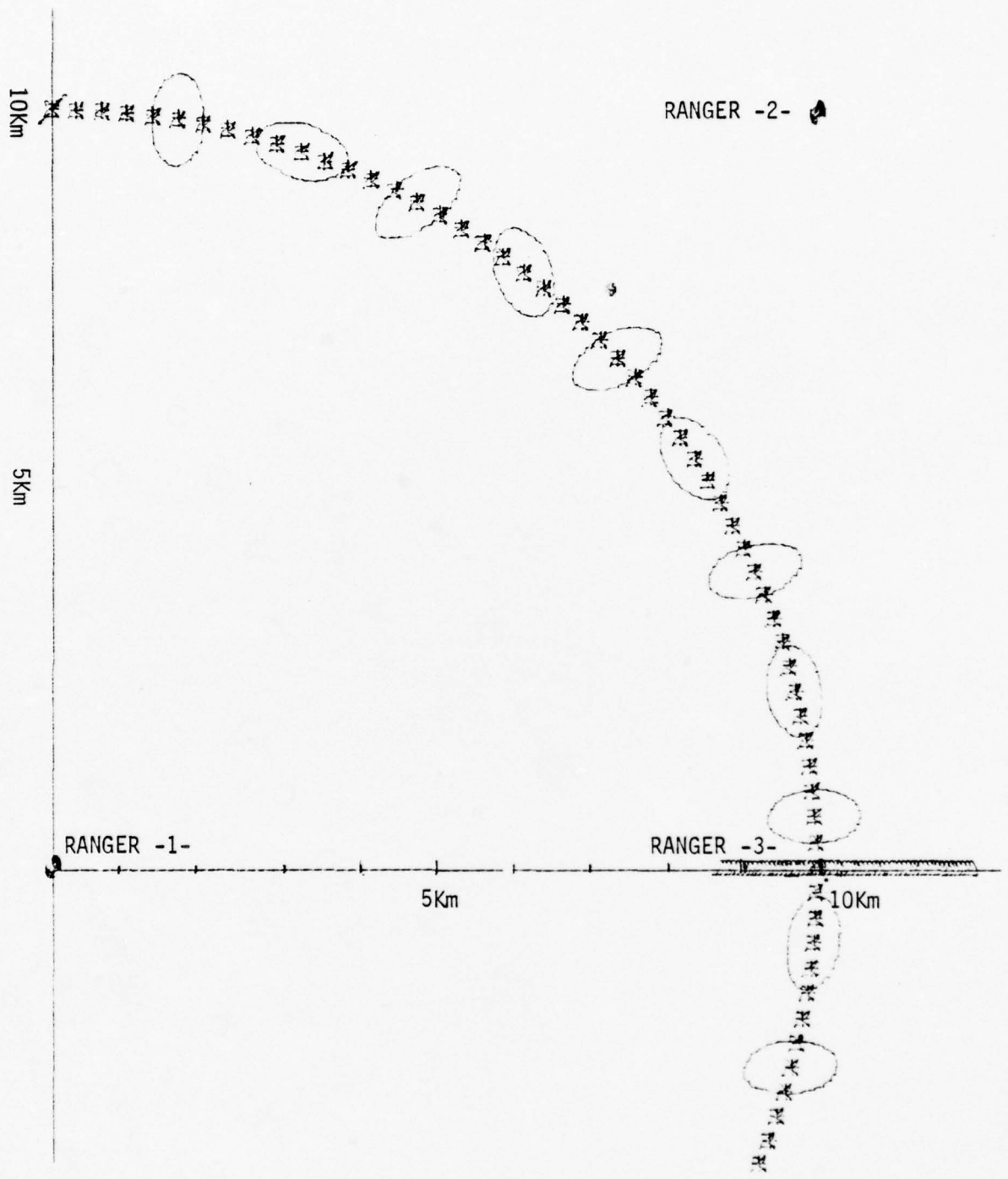


Figure 4 - PLRS SIMULATION - A JET IN A CONSTANT 10KM RADIUS TURN FLYING AMONG THREE MOVING RANGERS

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	3	41	3
2	1	22	2	42	1
3	2	23	3	43	2
4	1	24	2	44	1
5	2	25	3	45	2
6	1	26	1	46	1
7	2	27	3	47	2
8	1	28	1	48	1
9	2	29	3	49	2
10	1	30	1	50	1
11	2	31	3	51	2
12	1	32	1	52	1
13	3	33	3	53	2
14	1	34	1	54	1
15	3	35	3	55	2
16	2	36	1	56	1
17	3	37	3	57	2
18	2	38	1	58	1
19	3	39	3	59	2
20	2	40	1	60	1

TABLE 3 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
MOVING RANGER SIMULATION

D. SOURCE OF MEASUREMENT NOISE

In the above simulations the position of the ranging unit has been assumed to be exact; while in actual application the ranging units will have covariances of estimation error defining an error ellipse; and the ranging unit might be anywhere within that ellipse. To bring this position uncertainty into the simulation, the radius of the error ellipse along the bearing from the ranging unit to the update unit was defined as the covariance of measurement error.

The equation for the radius of an ellipse is a function of the major axis, the minor axis, and the angle at which the measurement is made. To find the measurement noise covariance, or the ellipse radius, σ_x^2 and σ_y^2 must be compared and the larger defined as M_j , the major axis, and the smaller defined as M_n , the minor axis. The angle, α , at which the radius is determined is measured from the major axis and thus is calculated as the difference between θ and β . Fig 5 shows the geometry of the calculation of the covariance of measurement noise. The equation for R and the radius squared of the ellipse is:

$$R = r^2 = \frac{M_j M_n}{M_j \sin^2 \alpha + M_n \cos^2 \alpha}$$

It can be seen in Fig 6 that performance was improved slightly using the covariance of estimation error as the sole source of measurement noise.

Table 4 shows the ranger chosen at each time for the three moving rangers with position uncertainty simulation.

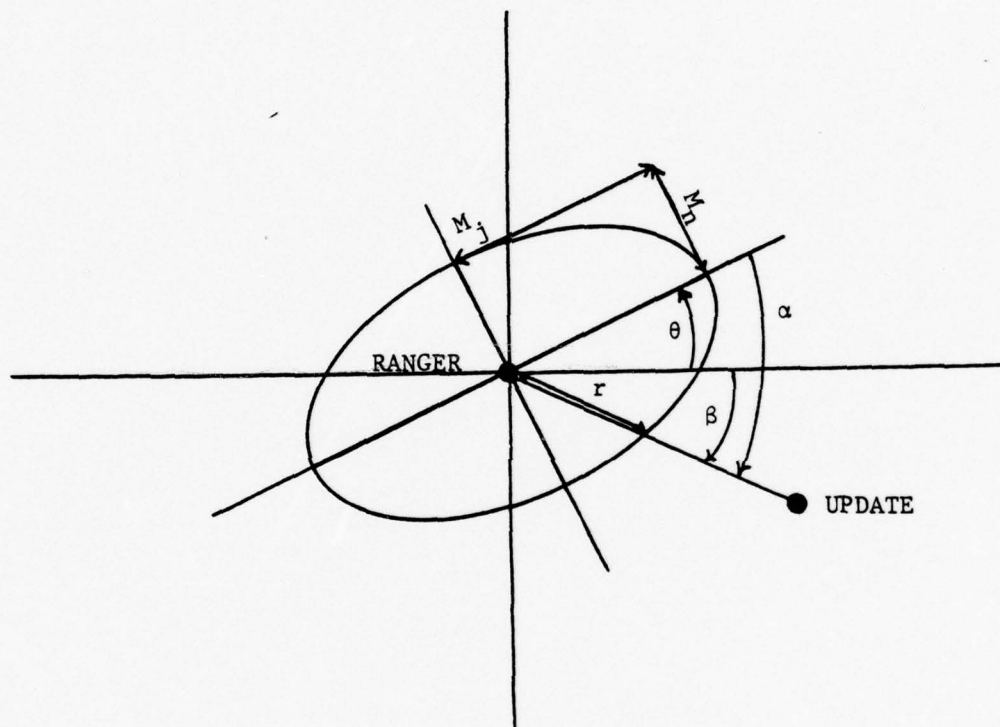


Figure 5 - r IS THE RADIUS OF THE ERROR ELLIPSE - $r^2 = R$
 IS THE COVARIANCE OF MEASUREMENT NOISE

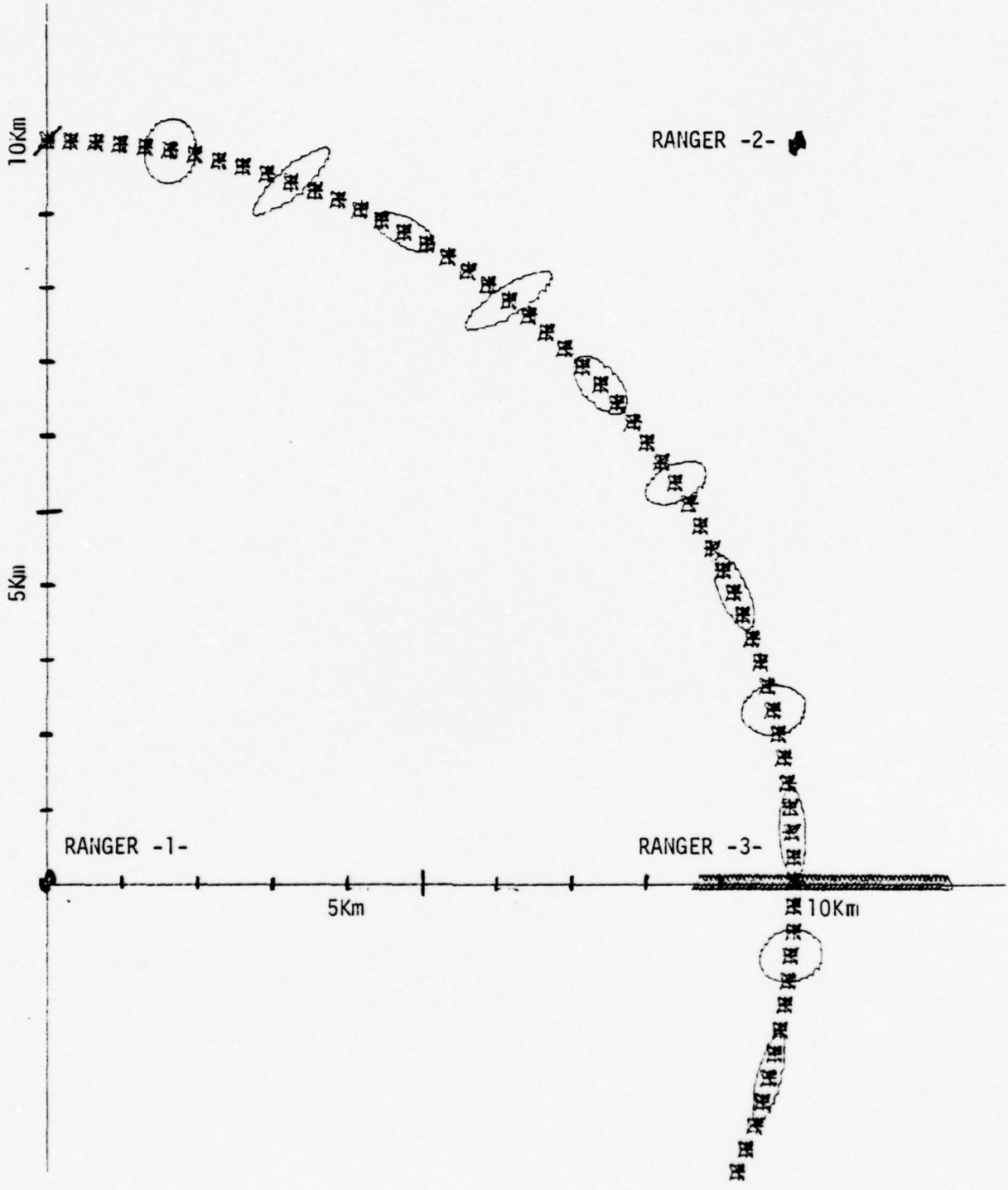


Figure 6 - PLSR SIMULATION - A JET IN A CONSTANT 10KM RADIUS TURN FLYING AMONG THREE MOVING RANGERS WITH POSITION UNCERTAINTY

TIME	RANGER	TIME	RANGER	TIME	RANGER
1	2	21	2	41	1
2	1	22	3	42	2
3	2	23	2	43	1
4	1	24	3	44	2
5	2	25	1	45	1
6	1	26	3	46	2
7	2	27	1	47	1
8	1	28	3	48	2
9	2	29	1	49	1
10	3	30	3	50	2
11	1	31	1	51	1
12	3	32	3	52	2
13	1	33	1	53	1
14	3	34	3	54	2
15	1	35	1	55	1
16	3	36	3	56	2
17	1	37	1	57	1
18	3	38	3	58	2
19	2	39	1	59	1
20	3	40	3	60	2

TABLE 4 - THE RANGER CHOSEN AT EACH TIME FOR THE THREE
MOVING RANGERS WITH POSITION UNCERTAINTY SIMULATION

V. CONCLUSION

The placement of the third ranger showed the value of triangulation of the rangers. The closer to normal the bearings of the rangers are to each other, the better the results of consecutive ranges.

The allowance for motion and the representation of the ranger's position uncertainty as the source of measurement error were important steps toward full simulation of the system; and they were accomplished without degradation of performance.

A better simulation may be to represent the measurement error as the ranger's position uncertainty plus some system measurement error.

Still to be accomplished is the ability to update all units at each ranging, and to provide a gating system that will demand more frequent updates for faster moving units and less frequent updates for slower units.

A program listing of the three moving rangers with position uncertainty is included with an annotated data deck.


```

C      DC 23 I=1,N
      DO 23 J=1,N
      PHIS(I,J) = PHI(I,J)
      WRITE (6,131)
      CALL MWRITE (PHI,N,N)
C
C      CALL MREAD (H,M,N)
      DO 25 I=1,M
      DO 25 J=1,N
      HS(I,J) = H(I,J)
      WRITE (6,132)
      CALL MWRITE (H,M,N)
C
C      CALL MREAD (R,M,M)
      WRITE (6,133)
      CALL MWRITE (R,M,M)
C
C      CALL MREAD (COVW,IN,IN)
      WRITE (6,134)
      CALL MWRITE (COVW,IN,IN)
      CALL MREAD (GAMMA,N,IN)
C
C      DO 30 I=1,N
      DO 30 J=1,IN
      GAMMAS(I,J) = GAMMA(I,J)
      WRITE (6,136)
      CALL MWRITE (GAMMA,N,IN)
C
C      CALL MREAD (PKKMI,N,N)
      WRITE (6,137)
      CALL MWRITE (PKKMI,N,N)
C
C      DO 311 K=2,NR
      CALL MREAD (PRR,N,N)
      DO 310 I=1,N
      DO 310 J=1,N
      PR(I,J,K) = PRR(I,J)
      310 CONTINUE
C
C      CALL VREAD (SIGV,M)
      WRITE (6,138)

```

```

MCSP0204
MCSP0205
MCSP0207
MCSP0208
MCSP0210
MCSP0211
MCSP0212
MCSP0213
MCSP0215
MCSP0217
MCSP0219
MCSP0220
MCSP0222
MCSP0223
MCSP0224
MCSP0225
MCSP0227
MCSP0228
MCSP0229
MCSP0230
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MCSP0253
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MCSP0257
MCSP0258
MCSP0259
CH3****1
CH3****2
CH3****3
CH3****4
CH3****5
CH3****6
MCSP0260
MCSP0262
MCSP0263

```

```

MCSP0264
MCSP0265
MCSP0272
CH200007
MCSP0275
CH200008
MCSP0277
MCSP0292
CH200009
CH200010
MCSP0294
MCSP0295
CH200011
MCSP0302
MCSP0247
MCSP0304
MCSP0250
MCSP0307
CH200012
MCSP0308
CH200013
CH200014
CH200015
MCSP0313
MCSP0314
MCSP0221
MCSP0316
MCSP0317
MCSP0318
MCSP0320
MCSP0321
MCSP0322
MCSP0323
MCSP0324
MCSP0325
MCSP0319
MCSP0327
MCSP0328
MCSP0329
MCSP0356
MCSP0357
MCSP0358
CH200016
MCSP0359
MCSP0360
MCSP0361

```

```

C      CALL VWRITE (SIGV,M)
C
C      DO 340 I=1,NR
C      READ (5,144) (XHATZ(I,J),J=1,N)
C      WRITE (6,140)
C      WRITE (6,146) (XHATZ(I,J),J=1,N)
C
C      340
C
C      36  DO 360 I=1,NR
C      READ (5,144) (XS(I,J,1),J=1,N)
C      INITIAL CONDITION HAS BEEN READ
C      WRITE (6,143)
C      WRITE (6,146) (XS(I,J,1),J=1,N)
C
C      360
C
C      38  CALL TRACK
C
C      DO 390 K=1,NR
C      WRITE (6,145)
C      WRITE (6,146) (XS(K,I,1),I=1,N)
C      WRITE (6,146) (XS(K,I,NSAM),I=1,N)
C      390 CCNTINUE
C
C      THE FOLLOWING SECTION PREPARES FOR THE MONTE CARLO LOOP
C      FORM NXN IDENTITY MATRIX IN DOUBLE PRECISION
C
C      DO 41 I=1,N
C      DO 41 J=1,N
C      EI(I,J) = 0.00
C      41 IF (I.EQ.J) EI(I,J)=1.00
C
C      GIVEN THE MATRIX GAMMA AND THE COVARIANCE OF W COMPUTE Q
C      USING DOUBLE PRECISION ARITHMETIC
C
C      CALL QMAT
C      WRITE (6,135)
C      CALL MWRITE (Q,N,N)
C
C      SET UP ARRAYS FOR COMPUTING STATISTICS
C
C      DO 48 I=1,NR
C      DO 48 K=1,NSAM
C      DC 48 J=1,N

```

CH200017
 CH200019
 MCSPO3364
 MCSPO3365
 MCSPO3366
 MCSPO3367
 MCSPO3368
 MCSPO3369
 MCSPO3370
 MCSPO3371
 MCSPO3372
 MCSPO3375
 MCSPO3376
 CH200018
 MCSPO3378
 MCSPO3379
 MCSPO3380
 MCSPO3381
 MCSPO3382
 MCSPO3383
 MCSPO3384
 CH200020
 MCSPO3386
 MCSPO3396
 MCSPO3397
 MCSPO3398
 MCSPO400
 MCSPO401
 MCSPO402
 MCSPO403
 MCSPO404
 MCSPO405
 MCSPO406
 MCSPO407
 MCSPO408
 MCSPO409
 MCSPO411
 MCSPO414
 MCSPO415
 MCSPO416
 MCSPO417
 MCSPO418
 MCSPO419
 MCSPO420
 MCSPO421
 MCSPO422
 MCSPO423
 CH200022

```

    XM(I,J,K) = 0.
    ERR(I,J,K) = 0.
    DO 48 L=1,N
  48 VAR(J,L,K) = 0.
    BEGIN MAIN ITERATION LOOP HERE
    DC 54 ITER=1, NENS
    DO 50 I=1,N
  50 XHKKM1(I) = XHATZ(1,I)
    DO 54 K=1, NSAM
    FORM NOISY MEASUREMENT FROM TRUE STATE VALUE
    DO 51 I=1,N
  51 X(I) = XS(1,I,K)
    CALL GAIN
    DO 52 I=1,N
    DO 52 J=1,M
  52 GKS(I,J,K) = G(I,J)
    UPDATE THE STATE ESTIMATE
    CALL ESTIM
    UPDATE RUNNING SUMS USED IN COMPUTING STATISTICS
    CALL STAT
    DO 54 CCNTINUE
    DIVIDE RUNNING SUMS COMPUTED BY SUBROUTINE STAT BY ENSEMBLE
    SIZE TO COMPUTE STATISTICS
    ENS = NENS
    DO 56 K=1, NSAM
  56 ERR(I,J,K) = ERR(1,J,K)/ENS
  
```



```

C
REAL*8  GAMMA, COVW, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON  EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), PHI(4,4), PR
1TEMP(4,4), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), ERR(4,4), X(4,4),
2VAR(4,4,60), GK(4,4,60), PKKS(4,4,60), XM(4,4,60), HS(4,4,60), V(4,4), SIGV(4,4),
3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), XHKKMI(4,4), VTMP(4,4), Z(4,4), V(4,4), SIGV(4,4),
4SIGXZ(4,4), XZMEAN(4,4), XHKK(4,4), HS(4,4,60), HS(4,4,60), GK(4,4,60), X(4,4),
5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), EST, ND, NR
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR

C
CALL PROD (GAMMA, COVW, N, IN, IN, TEMP)
CALL TRANS (GAMMA, N, IN, TEMPI)
CALL PROD (TEMP, TEMPI, N, IN, N, Q)
RETURN
END
SUBROUTINE QON
IF Q IS TO BE COMPUTED ON-LINE (IFLQ.NE.0) IT IS DONE
IN THIS SUBROUTINE
REAL*8  GAMMA, COVW, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON  EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), PHI(4,4), PR
1TEMP(4,4), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), ERR(4,4), X(4,4),
2VAR(4,4,60), GK(4,4,60), PKKS(4,4,60), XM(4,4,60), HS(4,4,60), V(4,4), SIGV(4,4),
3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), XHKKMI(4,4), VTMP(4,4), Z(4,4), V(4,4), SIGV(4,4),
4SIGXZ(4,4), XZMEAN(4,4), XHKK(4,4), HS(4,4,60), HS(4,4,60), GK(4,4,60), X(4,4),
5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), EST, ND, NR
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR

C
THE APPROPRIATE STATEMENTS FOR COMPUTING Q ON-LINE MUST
BE INSERTED HERE BY THE USER
RETURN
END
SUBROUTINE RON
IF R IS TO BE COMPUTED ON-LINE (IFLR.NE.0) IT IS DONE
IN THIS SUBROUTINE
REAL*8  GAMMA, COVW, R, PHI, H, TEMP, TEMPI, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON  EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVW(4,4), PHI(4,4), PR
1TEMP(4,4), TEMPI(4,4), TEMP2(4,4), H(4,4), PKKM1(4,4), R(4,4), ERR(4,4), X(4,4),
2VAR(4,4,60), GK(4,4,60), PKKS(4,4,60), XM(4,4,60), HS(4,4,60), V(4,4), SIGV(4,4),
3GAMMAS(4,4), PHIS(4,4), XS(4,4,60), XHKKMI(4,4), VTMP(4,4), Z(4,4), V(4,4), SIGV(4,4),
4SIGXZ(4,4), XZMEAN(4,4), XHKK(4,4), HS(4,4,60), HS(4,4,60), GK(4,4,60), X(4,4),
5XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), EST, ND, NR
6N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
CH2

```

```

MCSP0772
CH3**774
MCSP0775
CH200025
CH200026
MCSP0778
CH200004
CH2
MCSP0781
MCSP0782
MCSP0783
MCSP0784
MCSP0785
MCSP0786
MCSP0787
MCSP0788
MCSP0789
MCSP0790
MCSP0791
MCSP0792
CH3**795
MCSP0794
MCSP0795
CH200028
CH200029
MCSP0798
CH200004
CH2
MCSP0801
MCSP0802
MCSP0803
MCSP0804
MCSP0805
MCSP0806
MCSP0807
MCSP0808
MCSP0809
MCSP0810
MCSP0811
CH3**813
MCSP0814
CH200031
CH200032
MCSP0817
CH200004
CH2

```


MCSP0977
 MCSP0978
 MCSP0979
 MCSP0980
 MCSP0981
 MCSP0982
 MCSP0983
 MCSP0984
 MCSP0985
 MCSP0986
 MCSP0987
 MCSP0988
 MCSP0989
 MCSP0990
 MCSP0991
 MCSP0992
 MCSP0993
 MCSP0994
 MCSP0995
 MCSP0996
 MCSP0997
 MCSP0998
 MCSP0999
 MCSP1000
 MCSP1001
 MCSP1002
 MCSP1003
 MCSP1004
 MCSP1005
 MCSP1006
 MCSP1007
 MCSP1008
 MCSP1009
 MCSP1010
 MCSP1011
 MCSP1012
 MCSP1013
 MCSP1014
 MCSP1015
 MCSP1016
 MCSP1017
 MCSP1018
 MCSP1019
 MCSP1020
 MCSP1021
 MCSP1022
 MCSP1023
 MCSP1024

```

C      2  FORMAT (8F10.0)
      END
      SLBROUTINE MWRITE (A,N,M)
      THIS SUBROUTINE WRITES THE ENTRIES OF THE NXM MATRIX A
      REAL*8 A
      DIMENSION A(4,4)
      DC 1 I=1,N
      1  WRITE (6,2) (A(I,J),J=1,M)
      RETURN
      2  FORMAT (9(2X,1PE12.5))
      END
      SLBROUTINE PROD (A,B,N,M,L,C)
      THIS SUBROUTINE COMPUTES THE MATRIX PRODUCT AB AND STORES THE
      RESULT IN C
      A = NXM, B = MXL, C = NXL
      REAL*8 A,B,C,T
      DIMENSION A(4,4),B(4,4),C(4,4),T(4,4)
      DC 1 I=1,N
      DO 1 J=1,L
      1  T(I,J) = 0.0
      DC 2 I=1,N
      DO 2 J=1,L
      2  T(I,J) = T(I,J)+A(I,K)*B(K,J)
      DC 3 I=1,N
      DO 3 J=1,L
      3  C(I,J) = T(I,J)
      RETURN
      END
      SLBROUTINE SUB (A,B,N,M,C)
      THIS SUBROUTINE SUBTRACTS THE NXM MATRIX B FROM THE NXM MATRIX
      A AND STORES THE RESULT IN C
      REAL*8 A,B,C
      DIMENSION A(4,4),B(4,4),C(4,4)
  
```

MCSPI025
 MCSPI026
 MCSPI027
 MCSPI028
 MCSPI029
 MCSPI030
 MCSPI031
 MCSPI032
 MCSPI033
 MCSPI034
 MCSPI035
 MCSPI036
 MCSPI037
 MCSPI038
 MCSPI039
 MCSPI040
 MCSPI041
 MCSPI042
 MCSPI043
 MCSPI044
 MCSPI045
 MCSPI046
 MCSPI047
 MCSPI048
 MCSPI049
 MCSPI050
 MCSPI051
 MCSPI052
 MCSPI053
 MCSPI054
 MCSPI055
 MCSPI056
 MCSPI057
 MCSPI058
 MCSPI059
 MCSPI060
 MCSPI061
 MCSPI062
 MCSPI063
 MCSPI064
 MCSPI065
 MCSPI066
 MCSPI067
 MCSPI068
 MCSPI069
 MCSPI070
 MCSPI071
 MCSPI072

```

C      DC 1 I=1,N
C      DC 1 J=1,M
C      1 C(I,J) = A(I,J)-B(I,J)
C      RETURN
C      END
C      SUBROUTINE TRANS (A,N,M,C)
C      THIS SUBROUTINE FORMS THE MATRIX TRANSPOSE OF A STORING THE
C      RESULT IN C
C      A = NXM, C = MXN
C      DIMENSION A(4,4),C(4,4)
C      DO 1 I=1,N
C      DC 1 J=1,M
C      1 C(J,I) = A(I,J)
C      RETURN
C      END
C      SUBROUTINE VADD (X,Y,N,Z)
C      THIS SUBROUTINE COMPUTES THE SUM OF THE N-VECTORS X AND
C      Y AND STORES THE RESULT IN THE N-VECTOR Z
C      REAL*4 X(4),Y(4),Z(4)
C      DO 1 I=1,N
C      1 Z(I) = X(I)+Y(I)
C      RETURN
C      END
C      SUBROUTINE VPROD (A,X,M,N,Y)
C      THIS SUBROUTINE COMPUTES THE PRODUCT OF THE MXN MATRIX
C      A AND THE N-VECTOR X AND STORES THE RESULT IN THE
C      M-VECTOR Y
C      REAL*4 A(4,4),X(4),Y(4),T(4)
C      DO 1 I=1,M
C      T(I) = 0.00
C      DO 1 J=1,N
C      1 T(I) = T(I)+A(I,J)*X(J)
C      C
  
```


MCSP0918
MCSP0919

```
TPI = 2.*3.14159265  
DC 5 K=2,NSAM  
EKMI = K-1  
T = 1.0*EKMI  
A=0.03333*T  
IF(A.LT.TPI) GO TO 10  
FM=MM  
A = A - FM*TPI  
10 CCNTINUE  
XS(1,1,K)=10.*SIN(A)  
XS(1,2,K)=.3333*COS(A)  
XS(1,3,K)=10.*COS(A)  
XS(1,4,K)=-.3333*SIN(A)  
DO 7 I=2,NR  
EKMI = K-1  
XS(I,1,EKMI) = XS(I,2,1)  
XS(I,2,EKMI) = XS(I,1,1)  
XS(I,3,EKMI) = XS(I,4,1)  
XS(I,4,EKMI) = XS(I,3,1)  
7 5 CCNTINUE  
C  
RETURN  
END  
SUBROUTINE MEAS  
THIS SUBROUTINE STARTS WITH THE TRUE STATE VALUE XS  
AND ADDS ZERO-MEAN WHITE GAUSSIAN NOISE TO H*XS TO  
GENERATE A NOISY VECTOR OF MEASUREMENTS Z.  
C  
C  
C  
C  
REAL*8 GAMMA,COVM,R,PHI,H,TEMP,TEMP1,TEMP2,PKKMI,G,PKK,Q,EI,PR  
COMMON EI(4,4),Q(4,4),G(4,4),PKK(4,4),GAMMA(4,4),COVM(4,4),  
1TEMP(4,4,60),TEMP2(4,4,60),H(4,4),PKKMI(4,4),ERR(4,4,60),  
2VAR(4,4,60),GKS(4,4,60),PKKS(4,4,60),XM(4,4,60),PHI(4,4),  
3GAMMAS(4,4),PHIS(4,4),XS(4,4,60),HS(4,4),GK(4,4),X(4),  
4SIGXZ(4),XZMEAN(4),XHKKMI(4),VTMP(4),Z(4),V(4),SIGV(4),  
5XHATZ(4,4),XZ(60),YZ(60),PX(10),PY(10),PR(4,4,4),  
6N,NSAM,IQ,M,ITER,I TRK,IN,ISTAT,K,ITRO,IXZ,IV,IV,IV,IV,IV,IV,IV,IV,  
ALPHA = XS(1,3,K)  
BETA = XS(1,1,K)  
Z(1) = SQRT(ALPHA**2+BETA**2)  
Z(2) = ATAN2(ALPHA,BETA)  
CALL SNORM (IV,V,M)  
C  
DC 1 I=1,M  
1 V(I) = SIGV(I)*V(I)  
C  
CALL VADD (Z,V,M,Z)
```

CH2000046
CH2000047
CH2000048
CH2000049
CH2000050
CH2000051
CH2000053
CH2000054
CH2000055
CH2000056
CH2000057
MCSP0925
MCSP0926
MCSP0933
MCSP0734
MCSP0735
MCSP0736
MCSP0737
MCSP0738
MCSP0739
CH3****
MCSP0741
MCSP0742
CH2000058
CH2000059
MCSP0745
CH200000*
CH2
CH2000061
CH2000062
MCSP0750
MCSP0751
MCSP0752
MCSP0753
MCSP0754
MCSP0755
MCSP0756
MCSP0757

CH200067
CH200068
CH200069
CH200070

```
IO = IN + 1  
IF (ABS(XHKKM1(1)-XS(IO,1,K)).GT.0) GO TO 9  
XHKKM1(1) = 0.000001+XS(IO,1,K)  
BE(IN) = ATAN((XHKKM1(3)-XS(IO,3,K))/(XHKKM1(1)-XS(IO,1,K)))  
9 CONTINUE  
63 DO 4 IN=1,3  
66 ER(IN) = ABS(THE-BE(IN))  
4
```

CC

```
CHOOSE BEST RANGER  
IF (ABS(COS(ER(1))) .LE. ABS(COS(ER(2)))) GO TO 7  
IF (ABS(COS(ER(1))) .LE. ABS(COS(ER(3)))) GO TO 7  
IN=1  
7 GO TO 8  
GC TO 8  
IN=2  
70 GO TO 8  
IN=3  
8 XIN=IN  
IC=IN + 1
```

CC

```
CALCULATE H  
RR = ((XHKKM1(1)-XS(IO,1,K))**2 + (XHKKM1(3)-XS(IO,3,K))**2)**.5  
WRITE (6,22)  
FORMAT(/,6X, 'THE', 12X, 'SIG2X', 8X, 'SIG2Y', 10X, 'BE(1)', 8X, 'BE(2)',  
18X, 'XIN', 10X, 'ER(1)', 9X, 'ER(2)', 10X, 'RR',  
WRITE (6,146) THE, SIG2X, SIG2Y, BE(1), BE(2), XIN, ER(1), ER(2), RR  
146 FORMAT (9(2X,1PE12.5)/)  
H(1,1) = (XHKKM1(1)-XS(IO,1,K))/RR  
H(1,3) = (XHKKM1(3)-XS(IO,3,K))/RR  
IF (DABS(PR(1,1,IN)-PR(3,3,IN)).GT.0) GO TO 20  
PR(3,3,IN) = PR(1,1,IN)+0.000001  
20 CONTINUE
```

CC

```
FIND RANGER'S ERROR ELLIPSE ORIENTATION (THER)  
THER = 0.5*DATAN(2.*PR(1,3,IN)/(PR(1,1,IN)-PR(3,3,IN)))  
IF (ABS(THER).GT.0) GO TO 19  
THER = 0.00001  
19 SIG2XR = (PR(1,1,IN) + PR(3,3,IN)) / 2. + PR(1,3,IN) / SIN(2.*THER)  
1)
```

CC

```
CALCULATE RANGER'S UNCORRELATED VARIANCES  
SIG2YR = (PR(1,1,IN) + PR(3,3,IN)) / 2. - PR(1,3,IN) / SIN(2.*THER)  
1)  
IF (SIG2YR.GE.0.) GO TO 21
```

PLR06200
PLR06210
PLR06220
CH200071
CH3*****
CH3*****
MCSP0634
CH200072
CH200073
CH3*****
CH3*****
PLR06300
PLR06310
CH3*****
CH3*****
CH3*****
CH3*****
CH#3*****


```

154 FORMAT (6X, I3, I3X, I1, I0X, IPEI4.7, 2(6X, IPEI4.7))
155 FORMAT (//)
156 FCRMAT (1,1)
157 FORMAT (10X, THE SAMPLE COVARIANCE OF EST. ERROR MATRIX IS, //)
158 RETURN

```

```

END
SUBROUTINE PLT
REAL*8 GAMMA, COVM, R, PHI, H, TEMP, TEMP1, TEMP2, PKKM1, G, PKK, Q, EI, PR
COMMON EI(4,4), Q(4,4), G(4,4), PKK(4,4), GAMMA(4,4), COVM(4,4), PHI(4,4), PR
1  VAR(4,4,60), GK(4,4,60), PKKS(4,4,60), XM(4,4,60), ERR(4,4,60), X(4,4),
2  GAMMAS(4,4), PHIS(4,4), XHKKM1(4), HS(4,4), GK(4,4), SIGW(4), X(4),
3  SIGXZ(4), XZMEAN(4), XHKK(4), XHKKM1(4), VTM(4), V(4), SIGV(4),
4  XHATZ(4,4), XZ(60), YZ(60), PX(10), PY(10), PR(4,4,4), IEST, ND, NR
5  N, NSAM, IQ, M, ITER, ITRK, IN, ISTAT, K, ITRO, IXZ, IV, IW, IEST, ND, NR
6  INTEGER*4 ITB(12)/12*0/
REAL*4 RTB(28)/28*0.0/
DIMENSION XP(60), YP(60)
EQUIVALENCE (TITLE, RTB(5))
REAL*8 TITLE(12)/X = TRUE, + = FILTER, SQUARE = NOISY*/

```

```

MCSP0644
MCSP0645
MCSP0646
MCSP0647
MCSP0648

```

```

CH3*****
MCSP0879
MCSP0880
CH200083
CH200084
MCSP0883
CH200000*
CH2

```

```

IGPLT=1
ITHVPL=1
INTPLT=1
ISMPPLT=1
ISVPPLT=1
DO 500 KY=1, NR
KX=NR+1-KY
DO 50 K=1, NSAM
XP(K) = XM(KX, 1, K)
YP(K) = XM(KX, 3, K)
50 CALL PLOTP(XP, YP, NSAM, 0)
500 CCNTINUE
ITB(1)=1
ITB(2)=1
CALL DRAWP(60, XP, YP, ITB, RTB)
DO 51 K=1, NSAM
XP(K)=XS(1, 1, K)+ERR(1, 1, K)
YP(K)=XS(1, 3, K)+ERR(1, 3, K)
51 CALL PLOTP(XP, YP, NSAM, 0)
ITB(1)=2
ITB(2)=2
CALL DRAWP(60, XP, YP, ITB, RTB)
ITB(2)=0
DO 2 J=1, 60, 5
IF (ABS(PKKS(1, 1, J)-PKKS(3, 3, J)).GT.0) GO TO 11

```

```

CH2*****
CH2*****
CH2*****
CH2*****

```

```

CH200088
CH200089

```

C C

```

PKKS(1,1,J)=PKKS(3,3,J)+0.000001
11 CONTINUE
   THE=0.5*TAN(2.*PKKS(1,3,J)/(PKKS(1,1,J)-PKKS(3,3,J)))
   IF (ABS(THE).GT.0) GO TO 10
   THE=0.000001
10 CONTINUE
   SIG2X=(PKKS(1,1,J)+PKKS(3,3,J))/2.+PKKS(1,3,J)/SIN(2.*THE)
   SIG2Y=(PKKS(1,1,J)+PKKS(3,3,J))/2.-PKKS(1,3,J)/SIN(2.*THE)
146 WRITE (6,146) THE, SIG2X, SIG2Y
      FCRRMAT (9(2X,1PE12.5),7)
      SX=(SIG2X)**.5*20.
      SY=(SIG2Y)**.5*20.
      PT=3.14159265/12.
      CT=COS( THE )
      ST=SIN( THE )
      DO 1 I=1,25
      XI=I
      XP(I)=SX*COS(PT*XI)*CT-SY*SIN(PT*XI)*ST+XS(1,1,J)
      YP(I)=SX*COS(PT*XI)*ST+SY*SIN(PT*XI)*CT+XS(1,3,J)
      DO 201 J=2, NR
      DO 200 K=1, NSAM
      XP(K)=XS(J,1,K)
      YP(K)=XS(J,3,K)
      IT=(J/2)+3
      ITB(2)=IT
201 CALL DRAMP (60,XP,YP,ITB,RTB)
      ITB(1)=3
      ITB(2)=3
      CALL DRAMP(60,XZ,YZ,ITB,RTB)
      DO 65 K=1, NSAM
65 XP(K) = K
      IF (IGPLT.NE.1) GO TO 68
      DO 67 I=1,N
      DO 67 J=1,M
      DO 66 K=1, NSAM
66 YP(K) = GKS(I,J,K)
      WRITE (6,156)
      CALL PLOTP (XP,YP,NSAM,0)
67 WRITE (6,159) I,J
      C 68 IF (ITHVPL.NE.1) GO TO 71

```

```

CH200090
CH200091
CH200092
CH200093
CH200094
CH200095
CH200096
CH200097
CH200098

```

```

MCSP0491
MCSP0492
MCSP0493
MCSP0494
MCSP0495
MCSP0496
MCSP0497
MCSP0498
MCSP0499
MCSP0500
MCSP0501
MCSP0502
MCSP0503
MCSP0504
MCSP0505
MCSP0506
MCSP0507
MCSP0508

```

MCSP0509
 MCSP0510
 MCSP0511
 MCSP0512
 MCSP0513
 MCSP0514
 MCSP0515
 MCSP0516
 MCSP0517
 MCSP0518
 MCSP0519
 MCSP0520
 MCSP0521
 MCSP0522
 CH200099
 MCSP0524
 MCSP0525
 MCSP0526
 MCSP0527
 MCSP0528
 MCSP0529
 MCSP0530
 MCSP0531
 MCSP0532
 MCSP0533
 CH2
 MCSP0535
 MCSP0536
 MCSP0537
 MCSP0538
 MCSP0539
 MCSP0540
 MCSP0541
 MCSP0542
 MCSP0543
 MCSP0544
 MCSP0545
 MCSP0546
 MCSP0547
 MCSP0548
 MCSP0549
 MCSP0550
 MCSP0551
 MCSP0649
 MCSP0650
 MCSP0651

```

C      DO 70 I=1,N
C      DO 69 K=1,NSAM
C      69 YP(K) = PKKS(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      70 WRITE (6,160) I,I
C      71 IF (IMTPLT.NE.1) GO TO 74
C      DO 73 I=1,N
C      DO 72 K=1,NSAM
C      72 YP(K) = XM(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      73 WRITE (6,161) I
C      74 IF (ISMPLT.NE.1) GO TO 77
C      DO 76 I=1,N
C      DO 75 K=1,NSAM
C      75 YP(K) = ERR(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      76 WRITE (6,162) I,I
C      77 IF (ISVPLT.NE.1) GO TO 80
C      DO 79 I=1,N
C      DO 78 K=1,NSAM
C      78 YP(K) = VAR(I,I,K)
C      WRITE (6,156)
C      CALL PLOTP (XP,YP,NSAM,0)
C      79 WRITE (6,163) I
C      80 CONTINUE
C      WRITE (6,156)
C      156 FORMAT (,I,)
C      159 FORMAT (12X, 'G(, ,I1, ,I1, ,) VS. K')
C      160 FORMAT (12X, 'PKK(, ,I1, ,I1, ,) VS. K')
C      161 FORMAT (12X, 'MEAN OF X(, ,I1, ,I1, ,) VS. K')
  
```

MCSP0652
MCSP0653

162 FORMAT (I2X, 'XHATKK(', I1, ') -X(', I1, ') VS. K')
163 FORMAT (I2X, 'ERROR VARIANCE(', I1, ') VS.. K')
RETURN
END
//GO.FT06F001 DD SYSOUT=A, SPACE=(CYL,(4,1))
//GO.SYSIN DD *

\$\$\$\$\$DATA DECK\$\$\$\$\$

ND 4 M 1 IN 2 NSAM 60 NENS 1 NR 4

IPRT IPLT 1

1.0 1.0 PHI
1.0 1.0

1.0 1.0 H
1.0 1.0

0.0001
COVM
.0001 .0001

GAMMA
0.5
1.0

.0001
PKKM1
.0001

.0001
PRR(1)
.0001

.0001
PRR(2)
.0001

.0001
PRR(3)
.0001

LIST OF REFERENCES

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