

AD-A054 214

NAVAL SURFACE WEAPONS CENTER WHITE OAK LAB SILVER SP--ETC F/G 12/1
AN INVERSE REGRESSION METHOD FOR DETERMINING AN ENSEMBLE OF STA--ETC(U)
DEC 77 R S BRUNSVOLD

NSWC/WOL/TR-77-183

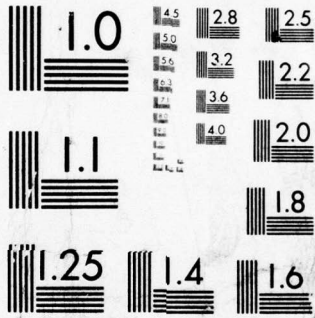
NL

UNCLASSIFIED

| OF |
AD
A054214



END
DATE
FILMED
6-78
DDC



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

FOR FURTHER TRAN : ~~SECRET~~

~~SECRET~~ (11)
R

NSWC/WOL TR 77-183

AD A 054214

AN INVERSE REGRESSION METHOD FOR DETERMINING AN ENSEMBLE OF STATE ERROR VECTORS FROM A COVARIANCE MATRIX

BY RONALD S. BRUNSVOLD
ADVANCED WEAPONS DEPARTMENT

5 DECEMBER 1977

Approved for public release; distribution unlimited.

DDC
MAY 23 1978
F

AD No. _____
DDC FILE COPY



NAVAL SURFACE WEAPONS CENTER

Dahlgren, Virginia 22448 • Silver Spring, Maryland 20910

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER 14 NSWC/WOL/TR-77-183	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) 6 AN INVERSE REGRESSION METHOD FOR DETERMINING AN ENSEMBLE OF STATE ERROR VECTORS FROM A COVARIANCE MATRIX,		5. TYPE OF REPORT & PERIOD COVERED 9 Interim rept.,
7. AUTHOR(S) 10 Ronald S./Brunsvold		8. CONTRACT OR GRANT NUMBER(s) 12 79p.
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Surface Weapons Center White Oak Laboratory Silver Spring, Maryland 20910		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 11221N, J0094, J0094; WA0707;
11. CONTROLLING OFFICE NAME AND ADDRESS		12. REPORT DATE 11 5 Dec 77
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		13. NUMBER OF PAGES 35
		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for Public Release; distribution unlimited		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Regression, Error Model, Monte-Carlo, Covariance Matrix, Inverse Regression		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A method is described to determine an ensemble of initial condition state vector errors for use in a Monte-Carlo type error model. The state vector errors are found from a given (N x N) error covariance matrix and are properly correlated with one another. The method used is an inverse regression scheme which randomly introduces a gaussian distribution of errors with determined variances about linear regression curves calculated from the given covariance Matrix. A FORTRAN coded		

DD FORM 1473 1 JAN 73

EDITION OF 1 NOV 65 IS OBSOLETE
S/N 0102-014-6601

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

391 596

next page
Dun

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

implementation of the method is included.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

SUMMARY

This report outlines a technique for deriving a set of initial error states from an error covariance matrix. The need for an ensemble of state errors arises in a Monte-Carlo error model for the re-entry portion of flight of a ballistic missile. Typically the boost and vacuum coast part of a trajectory is accurately modeled with a covariance propagation scheme. During reentry, however, errors become nonlinear in time and are highly cross correlated with one another and interact strongly with the dynamics of the vehicle flight. To accurately model the errors during reentry a Monte-Carlo approach is often required. The interface between a covariance propagation scheme and a Monte-Carlo model requires that an ensemble of initial condition errors be extracted from an arrival covariance matrix. The errors must be properly correlated and have the proper distribution of magnitudes. The method described herein is one technique for defining the interface between the two types of error models.

Since the original draft of this report, the author has found that a method with equivalent results has been used to determine wind profiles from a matrix of wind correlation coefficients. (e.g., Hankerson, S. H., "Wind Profiles," NWL-TN-G-4/72, Feb 1972). It is likely that other uses for the general method can be found, especially in the field of system error modeling.

The present work was sponsored by the Navy's Strategic Systems Project Office, Mr. Roger Stanton, SP-27232, monitor, as part of the Improved Accuracy Program (IAP). Program guidance of Dr. J. Goeller, Acting Re-Entry Technology Co-ordinator, Naval Surface Weapons Center, is gratefully acknowledged.

R. A. Niemann
R. A. NIEMANN
By direction

i/ii

ACCESSION for	
NTIS	Wide Section <input checked="" type="checkbox"/>
DDC	Brief Section <input type="checkbox"/>
UNANNOUNCED	<input type="checkbox"/>
JUS:1 10A 10N _____	
BY	
DISTRIBUTION/AVAILABILITY CODES	
USC	SP CIAL
A	

CONTENTS

	Page
I. INTRODUCTION	1
II. LINEAR REGRESSION	2
A. Two Variable Regression	2
B. Multiple Linear Regression	5
III. INVERSE REGRESSION	5
A. Method Description	5
B. Proof of Proper Correlation	7
IV. CODE DESCRIPTION	9
V. CONCLUSIONS	10
APPENDIX	
A. SYMBOLS	A-1
B. CODE	B-1

FIGURE

1	Least Squares Regression Line	3
---	---	---

I. INTRODUCTION

Often it is desired to determine the performance of a physical system in an average or statistical sense. That is, for many repetitions of a phenomena, what are the operating limits within which a system may be expected to perform and how are deviations from nominal behavior distributed about the average of the many repetitions. A study of the statistical behavior of such physical phenomena is here referred to as system error modeling.

There are two common methods of constructing system error models. The first method is the deterministic or Monte-Carlo method. This method attempts to mathematically model the physical laws which affect a system and allow the parameters within the physical laws to vary in a particular manner within their limits of uncertainty. The parametric variations allowed have a certain randomness associated with them since the exact values of the parameters are never precisely known. Correlations between the parameter errors are permitted if they can be determined a priori. The system is allowed to operate within the framework of the Math model for many realizations of the event being studied. After exercising the model in this Monte-Carlo mode, the system states for the many realizations of an event can be analyzed and statistical variations of state amplitude and distribution can be determined. This statistical description of the system is the result being sought.

The second method of system error modeling is the covariance propagation scheme or analytic model. This model represents the uncertainties or errors in the state of a system in a covariance matrix. The elements of this matrix describe the magnitude of state errors and their correlations with one another in a statistical sense. The analytic error model propagates this covariance matrix with time to describe how the state errors change. Since all of the desired statistical information is available in the covariance matrix it need only be propagated once for each event. This method has the advantage of reduced complexity; however, it is not as versatile as the Monte-Carlo method and determination of the proper way of propagating a covariance matrix is not always a simple matter.

In some instance it may be desirable or necessary to mix the two methods of error modeling for a given physical system. If, say, the initial part of an event is modeled with the analytic error model and the latter stages with a Monte-Carlo model, then how are the two models interfaced at the point of transition? What technique will be used to calculate the ensemble of initial deterministic state vectors from a terminal covariance matrix in order to begin the Monte-Carlo process? The following analysis describes one method of defining the interface.

II. LINEAR REGRESSION

A. Two Variable Regression

Given an $(n \times n)$ symmetric error covariance matrix:

$$\begin{bmatrix} S_{11} & S_{12} & S_{13} & \dots & S_{1n} \\ S_{21} & S_{22} & S_{23} & \dots & S_{2n} \\ \vdots & & & & \\ \vdots & & & & \\ S_{n1} & S_{n2} & S_{n3} & \dots & S_{nn} \end{bmatrix}$$

The diagonal terms of this matrix represent the variance of error in a state property. If a state property is quantified by a known part Y_k plus an uncertain zero mean error in the state property say Y_u , then the property Y may be expressed as:

$$Y = Y_k + Y_u \quad (1a)$$

The S_{11} term of the error covariance matrix then represents the statistical variance of Y_u for many realizations of the state.

$$S_{11} = \frac{\sum Y_{u1}^2}{N} \quad (1)$$

N is the large number of realizations of Y_u . Similar definitions exist for the other $(N - 1)$ states implicit in the covariance matrix. The off-diagonal terms of the matrix are the covariances of the (N) states defined by:

$$S_{12} = \frac{\sum Y_{u1} Y_{u2}}{N} \quad (2)$$

The magnitude of the covariances indicate the degree to which state errors are dependent on one another. To put this dependence in a nondimensional form a correlation coefficient can be written:

$$r_{12} = \frac{S_{12}}{(S_{11} S_{22})^{1/2}} \quad (3)$$

In this nondimensional form, a correlation of +1 indicates perfect correlation between errors Y_{u1} and Y_{u2} , and a correlation of 0 indicates no correlation exists. This definition of correlation coefficient is applicable only for linear correlation analysis. A non linear correlation may exist for $r_{12} = 0$. The present method assumes only linear correlations exist among the state errors.

If the state errors of two state variables are known for many realizations of the two states, then a least square regression line (see Figure (1)) can be described by

$$\begin{pmatrix} Y_{u2} \\ \text{est.} \end{pmatrix} = \left(\frac{\sum Y_{u1} Y_{u2}}{\sum Y_{u1}^2} \right) \begin{pmatrix} Y_{u1} \\ \text{actual} \end{pmatrix} \quad (4)$$

The mean values of the errors are clearly assumed to be zero (i.e., no biases exist).

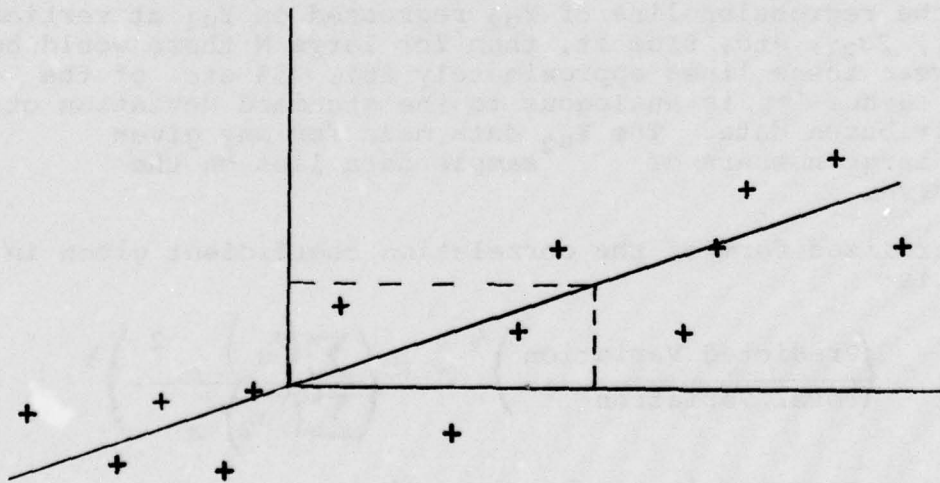


FIGURE 1. LEAST SQUARES REGRESSION LINE.

For a given actual value of Y_{u1} , an estimate of Y_{u2} , can be made from the equation of the least square regression line according to equation (4). The "goodness" of the estimate depends on how well Y_{u2} is correlated with Y_{u1} . If the correlation were perfect (i.e., $r_{12} = 1$) then there would be no scatter in the data points in Figure (1). All the data would be directly on the linear regression line. Conversely, a poor correlation would be seen as much scatter of the data about the regression line in Figure (1), and the estimate of Y_{u2} from the regression equation would not be expected to be very good.

Equation (4) can be rewritten in terms of the covariance from equations (1) and (2) as:

$$\left(Y_{u2}\right)_{\text{est.}} = \frac{S_{12}}{S_{11}} \left(Y_{u1}\right)_{\text{actual}} \quad (5)$$

A quantitative measure of the data scatter about the regression curve is defined as a "Standard Error of Estimate":

$$\sigma_{21} = \left(\frac{\sum \left(\left(Y_{u2}\right)_a - \left(Y_{u2}\right)_e \right)^2}{N} \right)^{\frac{1}{2}} \quad (6)$$

The difference of the two terms in equation (6) is the difference between each data point and the regression curve approximating the data. The standard error of estimate is similar to a deviation of the data about the regression curve. If lines are constructed parallel to the regression line of Y_{u2} regressed on Y_{u1} at vertical distances σ_{21} , $2\sigma_{21}$, etc., from it, then for large N there would be included between these lines approximately 68%, 95% etc. of the data points. Hence σ_{21} is analogous to the standard deviation of normally distributed data. The Y_{u2} data mean for any given Y_{u1} and very large numbers of sample data lies on the regression curve.

A generalized form of the correlation coefficient given in equation (3) is:

$$r_{21} = \left(\frac{\text{Predicted Variation}}{\text{Total Variation}} \right)^{\frac{1}{2}} = \pm \left(\frac{\sum \left(Y_{u2}\right)_e^2}{\sum \left(Y_{u2}\right)_a^2} \right)^{\frac{1}{2}} \quad (7)$$

and for linear regression it can be shown that

$$\sum \left[\left(Y_{u2}\right)_a - \left(Y_{u2}\right)_e \right]^2 = \sum \left(Y_{u2}\right)_a^2 - \sum \left(Y_{u2}\right)_e^2 \quad (8)$$

hence with (8), (7) and (6)

$$\sigma_2 = S_{22}^{1/2} (1 - r_{21}^2)^{1/2} \quad (9)$$

B. Multiple Linear Regression

When multiple correlation exist among a set of random variables as is the case when given an $N \times N$ covariance matrix, multi-dimensional regression equations can be constructed. Generalizing equation (5) to the multi-dimension equation:

$$\left(\frac{Y_{uN}}{S_{NN}^{1/2}} \right)_e = a_1 \left(\frac{Y_{u1}}{S_{11}^{1/2}} \right)_a + a_2 \left(\frac{Y_{u2}}{S_{22}^{1/2}} \right)_a + \dots + a_{N-1} \left(\frac{Y_{u_{n-1}}}{S_{(n-1)(n-1)}^{1/2}} \right)_a \quad (10)$$

Where the a_n coefficients are found from simultaneous solution of the algebraic equations:

$$\begin{aligned} a_1 r_{11} + a_2 r_{12} + a_3 r_{13} + \dots + a_{n-1} r_{1(n-1)} &= r_{1n} \\ a_1 r_{21} + a_2 r_{22} + a_3 r_{23} + \dots + a_{n-1} r_{2(n-1)} &= r_{2n} \\ \vdots & \\ a_1 r_{(n-1)1} + a_2 r_{(n-1)2} + a_3 r_{(n-1)3} + \dots + a_{(n-1)} r_{(n-1)(n-1)} &= r_{(n-1)n} \end{aligned}$$

and the standard error of estimate about the multiple regression line is an expanded form of equation (9):

$$\sigma_n = S_{nn}^{1/2} \left(1 - r_{n,1} a_1 - r_{n,2} a_2 - \dots - r_{n,(n-1)} a_{n-1} \right)^{1/2} \quad (12)$$

III. INVERSE REGRESSION

A. Method Description

If it is desired to find an ensemble of state vectors which include random errors and if it is also necessary that the random errors included in the state vectors have the proper statistical cross correlations, then it may be possible to construct such an ensemble, given the covariance matrix of errors. The process would be an inverse regression scheme as follows.

Making the assumption that all errors are normally distributed about linear regression lines it is possible to construct a set of regression lines and then statistically

"scatter" the errors about the line using a zero mean normally distributed random number generator with a variance equal to σ^2 (equation 12). The errors so generated would be added to the mean value of the state vector and repeated many times to build an ensemble of state vectors with properly correlated errors.

A consistent scheme of selecting the order of regression should be used. One such scheme would be as follows:

1. Select the two elements of the state vector that are least correlated (i.e., smallest $|S_{nm}|$, $N \neq M$).
2. Continue selecting elements in a monotonically increasing order of correlation.
3. Choose the selected initial two elements (from step 1) and construct a regression curve from equation (5) similar to Figure (1).
 - 3a. Find the so-called actual value $(Y_{u1})_a$ from a zero mean normal random generator (NRNG) with variance S_{11} .
 - 3b. Solve for the estimated value of Y_{u2}
4. Introduce scatter to $(Y_{u2})_e$ by adding an error term found from (NRNG) using variance σ_2 as found from equation (9).

Solve for the so-called actual value of Y_{u2}

$$\begin{pmatrix} Y_{u2} \\ \end{pmatrix}_a = \begin{pmatrix} Y_{u2} \\ \end{pmatrix}_e + (\text{NRNG}) \sigma_2 \quad (13)$$
5. Repeat the process to calculate actual values for all the state errors.

Equation (13) is a defined value of a single realization of the error in the Y_2 element of the state vector. When this process is repeated for each element of the state vector, it is necessary to use the expanded multiple regression equation (10) and variance, equation (12).

For example when finding the third error term, (Y_{u3}) , from (10):

$$\begin{pmatrix} Y_{u3} \\ \end{pmatrix}_e = a_1 \begin{pmatrix} Y_{u1} \\ \end{pmatrix}_a + a_2 \begin{pmatrix} Y_{u2} \\ \end{pmatrix}_a \quad (14)$$

where $(Y_{u1})_a$ and $(Y_{u2})_a$ are the same values as found in the preceding steps. The variance used to introduce "scatter" into the $(Y_{u3})_{est.}$ of equation (14) is:

$$\sigma_3^2 = \left[S_{33}^{1/2} \left(1 - r_{31} a_1 - r_{32} a_2 \right)^{1/2} \right]^2 \quad (15)$$

The process is complete when all N values of the state vector have been altered by an error term as in equation (1a).

For a given covariance matrix of errors, the A_N coefficients of equation (11) need only be calculated once. They change only when the covariance matrix changes. However, the value of the " A_N " coefficient are different for each value of N in equation 10. A set of coefficients correspond to each value of N which is the order of the given covariance matrix. As many realizations as desired of the state vector can be generated for a given covariance matrix. Each new realization is constructed from a new (NRNG) value for the first error term Y_{u1} .

B. Proof of Proper Correlation

It remains to show that the order chosen for regressing the variables does not affect the statistical cross correlations of the errors in the final ensemble of state vectors. If we accept equations (13) as a valid method of introducing "scatter" or randomness to regression generated errors, then it is sufficient to show that cross correlations of error states are correct, independent of the order of their regression.

$$\left(Y_{u_n} \right)_a = \left(Y_{u_n} \right)_e + (NRNG)_{\sigma_n} \quad (16)$$

The term $(NRNG)_{\sigma_n}$ is a single realization of a normal random number generator with standard deviation, σ_n .

Let us arbitrarily choose two elements of an error state vector Y_{u1} and Y_{u2} and regress Y_{u2} on Y_{u1} :

$$\left(Y_{u2} \right)_e = \frac{S_{12}}{S_{11}} \left(Y_{u1} \right)_a \quad (17)$$

Where $\left(Y_{u1} \right)_a$ is chosen from $(NRNG) (S_{11})^{1/2}$

$$\text{Then } \left(Y_{u2} \right)_a = \left(Y_{u2} \right)_e + (NRNG)_{\sigma_2} \quad (18)$$

σ_2 being found from (9).

The cross correlation between $(Y_{u1})_a$ and $(Y_{u2})_a$ for a large number of realizations of equation (18) is:

$$(CC)_{12} = \sum (Y_{u1})_a (Y_{u2})_a / N$$

from (17) and (18)

$$\begin{aligned} (CC)_{12} &= \sum (Y_{u1})_a \left[\frac{S_{12}}{S_{11}} (Y_{u1})_a + (NRNG)_{\sigma_2} \right] / N \\ &= S_{12} + \sum (Y_{u1})_a (NRNG)_{\sigma_2} / N \end{aligned} \quad (19)$$

The term on the right is equal to zero in the limit since each term of the product has zero mean and the terms are uncorrelated. Hence as expected:

$$(CC)_{12} = S_{12} = \sum (Y_{u1})_a (Y_{u2})_a / N \quad (20)$$

From (10) the regression equation for a third variable is:

$$(Y_{u3})_e = \frac{S_{33}^{1/2} A_1}{S_{11}^{1/2}} (Y_{u1})_a + \frac{S_{33}^{1/2} A_2}{S_{22}^{1/2}} (Y_{u2})_a \quad (21)$$

$$(Y_{u3})_a = (Y_{u3})_e + (NRNG)_{\sigma_3} \quad (22)$$

Now check to see if $(Y_{u3})_a$ generated by (22) is properly correlated with $(Y_{u1})_a$:

$$\begin{aligned} \frac{\sum (Y_{u1})_a (Y_{u3})_a}{N} &= \\ \frac{\sum (Y_{u1})_a \left[\frac{S_{33}^{1/2} A_1}{S_{11}^{1/2}} (Y_{u1})_a + \frac{S_{33}^{1/2} A_2}{S_{22}^{1/2}} (Y_{u2})_a + (NRNG)_{\sigma_3} \right]}{N} & \end{aligned} \quad (23)$$

N

This quickly reduces to:

$$= S_{11}^{1/2} S_{33}^{1/2} A_1 + \frac{S_{33}^{1/2} S_{12}}{S_{22}^{1/2}} A_2 + \frac{\sum (y_{u_1})_a (NRNG) \sigma_3}{N} \quad (24)$$

Since the last term is zero in the limit for a product of uncorrelated zero mean variables, (24) is:

$$\frac{\sum (y_{u_1})_a (y_{u_3})_a}{N} = S_{11}^{1/2} S_{33}^{1/2} A_1 + \frac{S_{33}^{1/2} S_{12}}{S_{22}^{1/2}} A_2 \quad (25)$$

The A_1 and A_2 coefficients are found from (10) to be:

$$A_1 = \frac{r_{13} - r_{12} r_{23}}{1 - r_{12}^2}; \quad A_2 = \frac{r_{23} - r_{12} r_{13}}{1 - r_{12}^2} \quad (26)$$

Substituting (3) and (26) into (25):

$$\sum \frac{(y_{u_1})_a (y_{u_3})_a}{N} = S_{13}$$

Hence, even though Y_{u_3} was the third variable chosen it is properly correlated with the first variable. In a similar fashion, the third variable can be shown to be properly correlated with the second variable. This process can be continued for all subsequent elements of the state vector regardless of their order of regression. Therefore, the order chosen to regress the state vector errors is arbitrary and has no adverse effect on the cross correlations of the ensemble of state vectors so generated.

IV. CODE DESCRIPTION

The inverse regression method described has been coded for use in a trajectory program. If a state error covariance matrix is available at some point in a vehicle's trajectory and it is

desired to complete the trajectory with a Monte-Carlo error analysis, then it is necessary to determine an ensemble of initial state vectors. One state vector from the ensemble is used as an initial condition for each trajectory of the Monte-Carlo series.

A listing is enclosed as Appendix B for the subroutines that read in the covariance matrix and then determine the coefficients and standard deviation required to solve for state error vectors. Subroutine COVSET(M) stores in common the "A" coefficients and "S" variances of equation (10). Also stored are the standard deviations of equation (12) for the M-dimensional square covariance matrix. These stored parameters along with a normal random number generator are sufficient to form a state error vector by repeatedly solving equation (10) for M values of the state (\bar{u}) est. This error state determines the initial condition for one trajectory realization. Additional realizations of the Monte-Carlo series can be found with the same stored coefficients (i.e., these need not be calculated again). The normal random number generator with previously calculated standard deviation supplies the required variation of the state vector for subsequent trajectories.

Subroutine FILL uses a system supplied function (MAM) to solve the set of simultaneous equations (11). Any simultaneous algebraic equation solver may be substituted here. Subroutine IMOD actually generates the desired error vectors.

V. CONCLUSIONS

A method has been described which allows mixed modes of error modeling for a single event. The method defines the interface between a covariance propagation error model and a Monte-Carlo deterministic error model. Given an arrival uncertainty covariance matrix for a physical system at some point in time, it is possible to construct an ensemble of state error vectors which may be used as initial conditions for the error state in order to exercise a Monte-Carlo model of the system. The error states so generated have been shown to be properly cross correlated with each other and have the correct distribution of magnitudes. A FORTRAN computer program has been written to facilitate implementation of the method within trajectory codes.

APPENDIX A

SYMBOLS

a	Regression coefficients
cc	Error covariance
N	Number of samples or summation index
NRNG	Zero mean normal random number generator
r	correlation coefficients
S_{NN}	Variance of error
S_{jk}	Covariance of errors
Y	Element of state vector
Y_k	Known part of state vector element
Y_u	Unknown part of state vector element
σ	Standard deviation for gaussian distribution
Σ	Summation symbol
<u>Subscripts</u>	
est. or e	Regression estimated value of an error
actual or a	Determined actual value of an error

NSWC/WOL TR 77-183
APPENDIX B
COMPUTER CODE LISTING

```

SUBROUTINE COVSET(M)
  BRUNSVOLD   MAY 77

C
C
C   FOR A GIVEN MONTE-CARLO RUN SET, THE FOLLOWING INFORMATION
C   NEED BE CALCULATED ONLY ONCE.
C
C   CALCULATE CERTAIN COEFFICIENTS FROM ARRIVAL UNCERTAINTY
C   COVARIANCE MATRIX (INITIAL CONDITIONS FOR EACH RUN)
C
C   STORAGE IN THE X ARRAY BEGINS AT X(1) AND IS OPEN ENDED
C   STORAGE LOCATIONS = *A* STORAGE + SIGMA STORAGE + S(N) STORAGE
C   = ((M-1)+(M-2)+.....+(2))+(M-1)+M
C   X ARRAY NOW SUFFICIENT TO HANDLE A 12 X 12
C
COMMON X(90)
DIMENSION RMM(3),SMM(3,3),ARRAY(2,2),IC(2)
200 FORMAT(5F15.7,5X)
201 FORMAT(1H ,5F15.7,5X)
202 FORMAT(1H1)
X(2)=FLOAT(M)
C   READ IN COVARIANCE MATRIX
READ(5,200)SMM
WRITE(6,202)
WRITE(6,201)SMM
C   TO SIMPLIFY COMPUTATIONS, DIAGONAL ELEMENTS OF SMM MATRIX ARE
C   SQRT OF ORIGINAL COVARIANCE DIAGONAL ELEMENTS.
C   CALCULATE CORRELATION COEFFICIENTS MATRIX FROM ARRIVAL COVARIANCE
DO 10 K=1,M
DO 10 J=1,M
IF(K.GE.J)GO TO 10
C   CALCULATE THE *R* VALUES (CORRELATION COEFFICIENTS)
C   CORRELATION COEFFICIENT MATRIX BECOMES SMM AS WE WRITE ON TOP OF
C   ORIGINAL COVARIANCE MATRIX TO SAVE STORAGE.
SMM(J,K)=SMM(J,K)/(SMM(J,J)*SMM(K,K))
SMM(K,J)=SMM(J,K)
10 CONTINUE
DO 11 J=1,M
C   PUT THE S(N) VALUES IN STORAGE. THESE ARE THE DIAGONAL ELEMENTS OF
C   THE COVARIANCE MATRIX EQUAL TO THE STANDARD DEVIATION. FIRST
C   LOCATION IS X(3).
X(2+J)=SMM(J,J)
C   SET THE DIAGONAL ELEMENTS OF THE CORRELATION MATRIX TO 1.0
11 SMM(J,J)=1.
C   X(2)=M AND X(1)=S(1,2)/S(1,1). ARE COEFFICIENTS FOR YU2 ESTIMATE
X(1)=SMM(1,2)*X(4)/X(3)
N=1 % NB=MC=M+2 % M1=M-1
12 N=N+1
C   CALCULATE THE *A*S AND PUT INTO STORAGE, A(1) AND A(2) FIRST.
C   THESE ARE THE UNKNOWN VARIABLES OF THE SIMULTANEOUS ALGEBRAIC
C   EQUATIONS. SUBROUTINE FILL SOLVES THESE EQUATIONS.
C   BMM=SOLUTION VECTORS=*A*S., SMM=CORRELATION COEFFICIENT MATRIX,
C   M=ORDER OF SMM, N=NUMBER OF SIMULTANEOUS EQUATIONS TO BE SOLVED
C   IN THIS PASS THROUGH FILL. ARRAY AND IC=DUMMY MATRIX THAT MUST BE
C   DIMENSIONED IN COVSET. DIMENSION TO M-1

```

```

CALL FILL(RMM,SMM,M,N,ARRAY,IC)
DO 13 ILO=1,N
MM=ILO+MB
C STORE SOLUTION VECTORS FROM FILL. FIRST LOCATION IS X(M+3).
X(MM)=RMM(ILO)
13 CONTINUE
IF(N.EQ.M1)GO TO 14
MB=MM
GO TO 12
C CALCULATE M-1 PERMANENT VALUES OF SIGMA, SIGMA(2) IS FIRST AT
C LOCATION X(MM+1)=X(3+M+(M-1)+(M-2)+...+2)
C CALCULATE SIGMA(2)
14 X(MM+1)=X(4)*(1.-SMM(1,2)**2)**.5
C CALCULATE SIGMA(3) TO SIGMA(M)
DO 21 K=2,M1
REST=0.
DO 22 L=1,K
REST=SMM(K+1,L)*X(MC+L)+REST
22 CONTINUE
MC=MC+K
C PUT CALCULATED SIGMA S INTO X ARRAY
X(MM+K)=X(K+3)*(1.-REST)**.5
21 CONTINUE
C WITH SIGMA S, *A*S, AND S(N) S, ERROR VECTORS MAY BE GENERATED
C WITH NORMAL RANDOM NUMBER GENERATOR. A SUBROUTINE FOR THIS
C CALLED "IMOD" IS INCLUDED.
RETURN
END

C
C
SUBROUTINE FILL(R,RMM,M,N,ARRAY,IC)
BRUNSVOLD MAY 77
C THIS SUBROUTINE FINDS THE SOLUTION VECTOR FOR THE "A" COEFFICIENTS
C
DIMENSION RMM(M,M),ARRAY(N,N),R(N),IC(N)
DO 15 K=1,N
C GENERATE RIGHT SIDE OF ALGEBRAIC EQUATIONS FROM CORRELATION MATRIX
B(K)=RMM(K,N+1)
DO 15 J=1,N
C GENERATE COEFFICIENTS OF ALGEBRAIC EQUATIONS FROM CORRELATION
C MATRIX AND PUT INTO APRAY.
ARRAY(J,K)=RMM(J,K)
ARRAY(K,J)=ARRAY(J,K)
15 CONTINUE
C MAM IS SYSTEM SUBROUTINE THAT SOLVES LINEAR SET OF ALGEBRAIC EQNS.
CALL MAM(ARRAY,N,N,R,1,IC,ID)
IF(ID.EQ.2)GO TO 20
GO TO 16
20 WRITE(6,100)
100 FORMAT(1H ,26HFAILURE IN SUBROUTINE FILL)
STOP
C RETURN TO CONVSET WITH SOLUTION VECTOR R.
16 RETURN $ END

```

```

SUBROUTINE IMOD
THIS INITIAL MODULE SOLVES FOR THE INITIAL ERRORS IN THE STATE VEC
COMMON X(90)
DIMENSION Y(9)
M=IFIX(X(2)) $ QA=0.
C FIND THE PROPER INDEX IN THE X ARRAY
J=0 $ M1=M-1
DO 5 I=2,M
J=I+J
5 CONTINUE
MM=J+2
C GENERATE A NORMALLY DISTRIBUTED RANDOM NUMBER, (RN), OF
C SIGMA=1. AND MEAN=0.
25 CALL RANNUM(QA,1.,0.,R,RN)
C GENERATE THE FIRST STATE ERROR Y(1).
Y(1)=RN*X(3)
CALL RANNUM(QA,1.,0.,R,RN)
C GENERATE THE SECOND STATE ERROR.
Y(2)=X(1)*Y(1)+ N*X(MM+1)
MC=M+2
C SOLVE FOR THE REMAINING Y ERRORS
DO 10 K=2,M1
REST =0.
DO 20 L=1,K
REST=(X(MC+L)*Y(L)/X(L+2))+REST
20 CONTINUE
CALL RANNUM(QA,1.,0.,R,RN)
Y(K+1)=X(K+3)*REST+RN*X(MM+K)
MC=MC+K
10 CONTINUE
C THE Y VECTOR GENERATED IS ONE ERROR VECTOR REALIZATION TO BE ADDED
C TO MEANS. ADDITIONAL REALIZATIONS CAN BE GENERATED WITH OTHER SET
C OF RANDOM NUMBERS, RN'S.
WRITE(6,100)Y
100 FORMAT(1H0.9F10.6)
RETURN $ END

```

BEST AVAILABLE COPY

DISTRIBUTION

	Copies
Commander Naval Sea Systems Command Headquarters Attn: Chief Technical Analyst SEA-05121 SEA-033 SEA-031 SEA-09G32 SEA-035	2
Department of the Navy Washington, D. C. 20362	
Commander Naval Air Systems Command Headquarters Attn: AIR-03B AIR-03C AIR-320 AIR-320C AIR-310 AIR-50174	2
Department of the Navy Washington, D. C. 20361	
Office of Naval Research Attn: ONR 100 800 N. Quincy Street Arlington, Virginia 22217	2
Commander David Taylor Naval Research and Development Center Attn: Central Library (5641) Bethesda, Maryland 20034	2
Commander Naval Weapons Center Attn: Technical Library (533) China Lake, California 93555	

Copies

Director
U.S. Naval Research Laboratory
Attn: Library
Washington, D.C. 20390

NASA
Langley Research Center
Attn: MS/185 Technical Library
Langley Station
Hampton, Virginia 23665

NASA
Lewis Research Center
Attn: Library 60-3
21000 Brookpark Road
Cleveland, Ohio 44135

NASA
George C. Marshall Space Flight Center
Attn: Library
Huntsville, Alabama 35812

NASA
Attn: F. C. Schwenk, Director,
Research (Code RR)
600 Independence Avenue, S.W.
Washington, D.C. 20546

NASA
P. O. Box 33
College Park, Maryland 20740

Director
Defense Research and Engineering (DDR&E)
Attn: Technical Library
Room 3E1063, The Pentagon, Stop 103
Washington, D.C. 20301

Defense Documentation Center
Cameron Station
Alexandria, Virginia 22314

12

Commander (5632.2)
Naval Missile Center
Attn: Technical Library
Point Mugu, California 93041

Copies

Commanding Officer
USA Aberdeen Research and
Development Center
Attn: STEAP-TL
AMXRD-XSE
Aberdeen Proving Ground
Maryland 21005

Director
Strategic Systems Project Office
Attn: SP-27232
Department of the Navy
Washington, D.C. 20390

Director of Intelligence
Headquarters, USAF (AFNINDE)
Attn: AFOIN-3B
Washington, D.C. 20330

Los Angeles Air Force Station
SAMSO/DYAE
Attn: Code RSSE
Code RSSM
P. O. Box 92960
Worldway Postal Center
Los Angeles, California 90009

Headquarters, Arnold Engineering
Development Center
Attn: Library/Documents
Arnold Air Force Station
Tennessee 37389

Commanding Officer
Harry Diamond Laboratories
Attn: Library
Washington, D.C. 20438

Commanding General
U.S. Army Missile Command
Attn: AMSMI-RR
Chief, Document Section
Redstone Arsenal
Alabama 35809

Department of the Army
Office of the Chief of
Research and Development
ABMDA, The Pentagon
Washington, D.C. 20350

Copies

Commanding Officer
Picatinny Arsenal
Attn: SMUPA-VC-3 (A. A. Loeb)
Dover, New Jersey 07801

Commander (ADL)
Naval Air Development Center
Attn: Dr. R. K. Lobb
Johnsville, Pennsylvania 18974

Air Force Weapons Laboratory
Kirtland Air Force Base
Attn: Technical Library (SUL)
Albuquerque, New Mexico 87117

U.S. Army Ballistic Missile
Defense Agency
1300 Wilson Boulevard
Arlington, Virginia 22209

The Johns Hopkins University, (C/NOW 7386)
Attn: Document Library
Applied Physics Laboratory
Johns Hopkins Road
Laurel, Maryland 20810

Director, Defense Nuclear Agency
Headquarters, DASA
Attn: STSP (SPAS)
Washington, D.C. 20305

Commanding Officer
Naval Intelligence Support Center
4301 Suitland Road
Washington, D.C. 20390

Department of Aeronautics, DFAN
Attn: Library
USAF, Academy
Colorado 80840

Armament Development and Test Center
Attn: Technical Library, DLOSL
Eglin AFB, Florida 32542

Copies

Commander
U.S. Army Natick Development Center
AMSNM-UBS
Attn: AMXNM-UBS (G. A. Barnard)
Natick, Massachusetts 01760

NASA Ames Research Center
Attn: Library
Moffett Field, California 94035

Wright Aeronautical Laboratories
Attn: Technical Library
Wright-Patterson Air Force Base
Dayton, Ohio 45433

Naval Research Laboratory
Attn: Dr. J. Boris
Washington, D.C. 20375

ONR Branch Office/Pasadena
Attn: Dr. Richard Lau
1030 East Green Street
Pasadena, California 91101

Aerospace Engineering Program
University of Alabama
Attn: Prof. W. K. Rey, Chm.
P. O. Box 6307
University of Alabama 35486

AME Department
University of Arizona
Attn: Dr. L. B. Scott
Tucson, Arizona 85721

TASC
Attn: Dr. Thomas Mottl
6 Jacob Way
Reading, Massachusetts 01867

Polytechnic Institute of New York
Graduate Center Library
Route 110, Farmingdale
Long Island, New York 11735

Polytechnic Institute of New York
Spicer Library
Attn: Reference Dept.
333 Jay Street
Brooklyn, New York 11201

Copies

California Institute of Technology
Graduate Aeronautical Laboratories Aero.
Attn: Librarian
Pasadena, California 91109

University of California
Department of Mechanical Engineering
Attn: Prof. R. Greif
Berkeley, California 94720

Dept. of Aerospace Engineering
University of Southern California
Attn: Dr. J. Laufer
University Park
Los Angeles, California 90007

University of California, San Diego
Department of Aerospace and
Mechanical Engineering Sciences
Attn: Dr. P. A. Libby
LaJolla, California 92037

The Charles Stark Draper Laboratory, Inc.
Attn: Harvey Feltquate
555 Technology Square
Cambridge, Massachusetts 02139

The Catholic University
Attn: Dr. C. C. Chang
Washington, D.C. 20017

University of Cincinnati
Department of Aerospace Engineering
Attn: Dr. Arnold Polak
Cincinnati, Ohio 45221

Department of Aerospace Engineer Sciences
University of Colorado
Boulder, Colorado 80302

Cornell University
Graduate School of Aerospace Engineering
Attn: Prof. A. R. George
Ithaca, New York 14850

University of Delaware
Mechanical and Aeronautical Engineering Dept.
Attn: Dr. James E. Danberg
Newark, Delaware 19711

Georgia Institute of Technology
Attn: Dr. Arnold L. Ducoffe
225 North Avenue, N.W.
Atlanta, Georgia 30332

Technical Reports Collection
Gordon McKay Library
Harvard University
Division of Engineering and Applied Physics
Attn: George Carrier
Pierce Hall, Oxford Street
Cambridge, Massachusetts 02138

Systems Control, Inc.
Attn: W. E. Hall, Jr.
1801 Page Mill Road
Palo Alto, California 94304

Illinois Institute of Technology
Attn: Dr. M. V. Morkovin
3300 South Federal
Chicago, Illinois 60616

Iowa State University
Aerospace Engineering Department
Ames, Iowa 50010

The Johns Hopkins University
Attn: Prof. S. Corrsin
Baltimore, Maryland 21218

University of Kentucky
Wenner-Gren Aero. Lab.
Attn: C. F. Knapp
Lexington, Kentucky 40506

Department of Aero. Engineering, ME 106
Louisiana State University
Attn: Dr. P. H. Miller
Baton Rouge, Louisiana 70803

University of Maryland
Attn: John D. Anderson, Jr.
Dept. of Aerospace Engineering
College Park, Maryland 20740

Michigan State University
Attn: Library Documents Dept.
East Lansing, Michigan 48823

Massachusetts Institute of Technology
Attn: Aero. Engineering Library
Cambridge, Massachusetts 02139

University of Michigan
Engineering Library
Ann Arbor, Michigan 48104

Serials and Documents Section
General Library
University of Michigan
Ann Arbor, Michigan 48104

Mississippi State Univ.
Dept. of Aerophysics and
Aerospace Engineering
Attn: Mr. Charles B. Cliett
P. O. Drawer A
State College, Mississippi 39762

U. S. Naval Academy
Engineering Dept. Aerospace Div.
Annapolis, Maryland 21402

Library, Code 2124
U. S. Naval Postgraduate School
Technical Reports Section
Monterey, California 93940

D. H. Hill Library
North Carolina State University
P. O. Box 5007
Raleigh, North Carolina 27607

University of North Carolina
Chapel Hill
Dept. of Aero. Engineering
North Carolina 27514

Northwestern University
Technological Institute
Attn: Dept. of Mech. Engineering
Library
Evanston, Illinois 60201

Copies

Dept. of Aero-Astro Engineering
Ohio State University
Attn: Engineering Library
2036 Neil Avenue
Columbus, Ohio 43210

The Pennsylvania State Univ.
Department of Aero. Engr.
Hammond Bldg.
Library, Documents Section
University Park, Pennsylvania 18602

Bevier Engr. Library
126 Benedum Hall
University of Pittsburgh
Pittsburgh, Pennsylvania 15261

Princeton University
Aerospace and Mech. Science Dept.
Attn: Dr. I. E. Vas
D-214 Engr. Quadrangel
Princeton, New Jersey 08540

Purdue University
School of Aeronautical and
Engineering Sciences
Attn: Dr. B. Reese, Head, Dept. of
Aero. and Astro.
Lafayette, Indiana 47907

Rennselaer Polytechnic Institute
Department of Aeronautical
Engineering and Astronautics
Troy, New York 12181

Department of Mechanical
Industrial and Aerospace Engineering
Attn: R. H. Page
Rutgers - The State University
New Brunswick, New Jersey 08903

Stanford University
Librarian, Dept. of Aeronautics
and Astronautics
Stanford, California 94305

Stevens Institute of Technology
Attn: Mechanical Engineering Dept.
Library
Hoboken, New Jersey 07030

The University of Texas at Austin
Applied Research Laboratories
Attn: Director
Engr. S.B.114/Dr. Friedrich
P. O. Box 8029
Austin Texas 78712

University of Toledo
Department of Aero Engineering
2801 W. Bancroft
Toledo, Ohio 43606

University of Virginia
School of Engineering and Applied Science
Attn: Dr. I. D. Jacobson
Charlottesville, Virginia 22091

University of Washington
Attn: Engineering Library
Dept. of Aeronautics and Astronautics
Seattle, Washington 98105

West Virginia University
Attn: Library
Morgantown, West Virginia 26506

Federal Reports Center
University of Wisconsin
Attn: S. Reilly
Mechanical Engineering Building
Madison, Wisconsin 53706

Los Alamos Scientific Laboratory
Attn: Reports Library
P. O. Box 1663
Los Alamos, New Mexico 87544

Institute for Defense Analyses
Attn: Classified Library
400 Army-Navy Drive
Arlington, Virginia 22202

Copies

University of Florida
Attn: Dept. Engineering Science
Dr. B. M. Leadon
Gainesville, Florida 32601

Kaman Sciences Corporation
Attn: Library
Mr. D. Foxwell
P. O. Box 7463
Colorado Springs, Colorado 80933

Rockwell International Corporation
Technical Information Center
4300 E. Fifth Avenue
Columbus, Ohio 43216

M.I.T. Lincoln Laboratory
Attn: Library A-082
Dr. A. B. Wardlaw
P. O. Box 73
Lexington, Massachusetts

The RAND Corporation
1700 Main Street
Library - D.
Santa Monica, California 90406

Aerojet Electrosystems Co.
Engineering Library
1100 W. Hollyvale Avenue
Azusa, California 91702

The Boeing Company
Attn: 87-67
P. O. Box 3999
Seattle, Washington 98124

United Aircraft Corporation
Attn: Library
400 Main Street
East Hartford, Connecticut 06108

Hughes Aircraft Company
Attn: Company Tech. Doc. Center
6/Ell, B. W. Campbell
Centinela at Teale
Culver City, California 90230

Copies

Lockheed Missiles and Space Co., Inc.
Attn: C. Grolemond
P. O. Box 504
Sunnyvale, California 94086

Lockheed Missiles and Space Co., Inc.
Attn: Technical Information Center
3251 Hanover Street
Palo Alto, California 94304

Lockheed-California Co.
Attn: Central Library Dept.
Burbank, California 91503

Vice President and Chief Scientist
Dept. 03-10
Lockheed Aircraft Corp.
P. O. Box 551
Burbank, California 91503

Martin-Marietta Corporation
Attn: Science-Technology Library
(Mail No. 398)
P. O. Box 988
Baltimore, Maryland 21203

Martin Marietta Corp.
Orlando Division
P. O. Box 5837
Attn: Mr. H. J. Diabolt
Orlando, Florida 32805

General Dynamics
Attn: Research Library 2246
P. O. Box 748
Fort Worth, Texas 76101

Calspan Corporation
Attn: Library
4455 Genesee Street
Buffalo, New York 14221

Air Force University Library
(SE) 63-578
Maxwell Air Force Base
Alabama 36112

McDonnell Douglas Corp.
Attn: R. D. Detrich, Dept. 209 Bld. 33
P. O. Box 516
St. Louis, Missouri 63166

McDonnell Douglas Astronautics
Company - West
Attn: J. S. Murphy, A3
368, B4A0
5301 Bolsa Avenue
Huntington Beach, California 92647

Fairchild Hiller
Engineering Library
Republic Aviation Division
Farmingdale, New York 11735

General Applied Sciences Labs, Inc.
Attn: Dr. F. Lane
L. M. Nucci
Merrick and Stewart Avenues
Westbury, Long Island
New York 11590

General Electric Company
R&D Labs (Comb. Bld.)
Attn: Dr. H. T. Nagamtsu
Schenectady, New York 12301

The Whitney Library
General Electric Research and
Development Center
Attn: M. F. Orr, Manager
The Knolls, K-1
P. O. Box 8
Schenectady, New York 12301

General Electric Company
Missile and Space Division
Attn: MSD Library
P. O. Box 8555
Philadelphia, Pennsylvania 19101

General Electric Company
AEG Technical Information Center, N-32
Cincinnati, Ohio 45215

General Electric Company
Reentry & Environmental Systems Division
Attn: J. Immel
3198 Chestnut Street
Philadelphia, Pennsylvania 19101

AVCO-Everett Research Lab.
Attn: Library
2385 Revere Beach Pkwy.
Everett, Massachusetts 02149

LTV Aerospace Corporation
Vought Systems Division
Attn: Unit 2-51131 (Library)
P. O. Box 5907
Dallas, Texas 75222

LTV Corporation
Attn: MDS-T-Library
P. O. Box 5907
Dallas, Texas 75222

Northrop Norair
Attn: Tech. Info. 3343-32
3901 West Broadway
Hawthorne, California 90250

Government Documents
The Foundren Library
Rice Institute
P. O. Box 1892
Houston, Texas 77001

Grumman Aerospace Corporation
Attn: Dr. R. E. Melnik
Bethpage, Long Island
New York 11714

Marquardt Company
Attn: Library
P. O. Box 2013
Van Nuys, California 91409

ARDE Associates
Attn: Librarian
P. O. Box 286
580 Winters Avenue
Paramus, New Jersey 07652

Copies

Aerophysics Company
Attn: Mr. G. D. Boehler
3500 Connecticut Ave., N.W.
Washington, D.C. 20003

Aeronautical Research Associates of Princeton
Attn: Dr. C. duP. Donadson
50 Washington Road
Princeton, New Jersey 08540

General Research Corporation
Attn: Tech. Info. Office
5383 Hollister Avenue
P. O. Box 3587
Santa Barbara, California 93105

Sandia Laboratories
Attn: Dr. C. Peterson
Dr. G. W. Stone
Dr. K. Touryan
Dr. R. Eaton
Kurt Putz, Div. 1333
Box 5800
Albuquerque, New Mexico 87115

Hercules Incorporated
Attn: Library
Allegany Ballistics Lab.
P. O. Box 210
Cumberland, Maryland 21502

General Electric Company
Attn: Dvae Hovis, Rm. 4109
P. O. Box 2500
Daytona Beach, Florida 32015

TRW Incorporated
Attn: Tech. Library/Doc. Acquisitions
1 Space Park
Redondo Beach, California 90278

Stanford Research Institute
Attn: Dr. G. Abrahamson
333 Ravenswood Avenue
Menlo Park, California 94025

Hughes Aircraft Company
Attn: Tech. Library, 600-C222
P. O. Box 3310
Fullerton, California 92634

Westinghouse Electric Corp.
Astronuclear Laboratory
Attn: Library
P. O. Box 10864
Pittsburgh, Pennsylvania 15236

University of Tennessee
Space Institute
Attn: Prof. J. M. Wu
P. O. Box 10864
Pittsburgh, Pennsylvania 15236

CONVAIR Division of General Dynamics
Library and Information
P. O. Box 12009
San Diego, California 92112

CONVAIR Division of General Dynamics
Attn: Research Library
P. O. Box 80986
San Diego, California 92138

AVCO Missiles Systems Division
Attn: E. E. H. Schurmann
N. Tyson
H. Rosenbaum
201 Lowell Street
Wilmington, Massachusetts 01887

Chrysler Corporation
Space Division
Attn: N. D. Kemp 2910
E. A. Rawls, Dept. 2920
P. O. Box 29200
New Orleans, Louisiana 70129

General Dynamics
Pomona Division
Attn: Tech. Doc. Center (6-20)
P. O. Box 2507
Pomona, California 91766

Ford Aerospace & Communications Corp.
Ford & Jamboree Roads
Attn: Dr. A. Demetriades
Newport Beach, California 92660

Raytheon Company
Attn: D. P. Forsmo
Missile Systems Division
Hartwell Road
Bedford, Maine 01730

TRW Defense & Space Systems Group
Attn: M. W. Sweeney, Jr.
Space Park Drive
Houston, Texas 77058

Marine Bioscience Laboratory
Attn: Dr. A. C. Charters
513 Sydnor Street
Ridgecrest, California 93555

Applied Mechanics Review
Southwest Research Institute
8500 Culebra Road
San Antonio, Texas 78228

American Institute of Aeronautics and
Astronautics
Attn: J. Newbauer
New York, New York 10019

Technical Information Services
AIAA
Attn: Miss P. Marshall
750 Third Avenue
New York, New York 10017

Faculty of Aeronautical Systems
University of West Florida
Attn: Dr. R. Fledderman
Pensacola, Florida 32504

Space Research Corporation
Chittenden Bank Building
Attn: Library, J. A. Finkel
North Troy, Vermont 05859

The Aerospace Corporation
Attn: E. Ndefo
J. M. Lyons
P. O. Box 92957
Los Angeles, California 90009

Copies

Notre Dame University
Department of Aerospace Engineering
College of Engineering
Library
Notre Dame, Indiana 46556

Acurex Corp. Aerotherm
485 Clyde Avenue
Attn: M. Abbett
Mt. View, California 94042

Mathematics Research Center
Attn: Prof. Seymour V. Parter
U. S. Army
University of Wisconsin
Madison, Wisconsin 53706

TRW Defense & Space Systems Group
One Space Park
Attn: B. Pearce
Aerodynamics Dept.
Garth W. Lippmann, Bldg. R-5, Rm. 2230
Redondo Beach, California 92078

Lockheed Missiles and Space Co., Inc.
Continental Bldg., Suite 445
Attn: R. Fortune
El Segundo, California 90245