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**3D/4D AREA NAVIGATION SYSTEM
DESIGN, DEVELOPMENT, AND
IMPLEMENTATION**

Volume II Support Data and Program Listings

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SECTION I
INTRODUCTION AND
SUMMARY

1.1 Summary of Volume II

This volume describes the detailed design and final implementation of the software for the 3D/4D Base and ILS and 2D/Time Control Systems. The systems were constructed by modifying the software structure used for the ANS-70A Area Navigation System.

A description of the 3D/4D software effort requires some knowledge of the ANS-70A software structure. A brief functional description of the ANS-70A software is given in the following paragraphs.

Sections 2 and 3 describe the software modifications used to effect the BASE and 2D/Time Control Systems respectively. Section 4 presents the RNAV to ILS interface design procedure. Sections 5 and 6 present the development of the lateral and longitudinal control laws respectively. Program listings are found in the appendices.

1.2 Overview of ANS-70A Software System

The ANS-70A software system has several different priority levels. The highest level of software functions have been assigned to processor channels. Each channel is allocated processing time on a sequential basis. Channels of particular interest for the present treatment are the Navigation and CDU Application Channels. Major functions assigned to these channels are illustrated in Figures 1-1 and 1-2.

The classification of major functions for the Navigation Channel remains unchanged for the 3D/4D systems. Secondary functions have been added to the software modules that support the major tasks of Aircraft Systems Coupler (ASC) Input, Lateral Navigation, and ASC Output. Navigation tasks that are unique to the 3D/4D Base and 2D Plus Time Control systems are described in Sections 2.0 and 3.0 respectively.

the CDU Channel. In addition to providing software for the CDU interface, this channel supervises tasks related to navigation support and Flight Plan Management.

Background support for the navigation function is provided by routines called the Radio Selection Program, Kalman Filter, and the Flight Plan Monitor. Each of these programs is called on a cyclic basis by the CDU Main Program. The first two routines are used without modification for the 3D/4D systems.

The Flight Plan Monitor serves as an interface between the Navigation software and the Flight Plan Editor. A primary task for the Flight Plan Monitor consists of retrieving flight plan parameters required by the Lateral and Vertical Navigation routines. Another major task consists of supervising flight plan maintenance that is required at waypoint passage. 3D/4D modifications to the Flight Plan Monitor are given in later sections of this volume.

Figure 1-3 illustrates software interfaces that are required for Flight Plan Management. Initial verification of flight plan revisions entered via the CDU are performed by the CDU Software. If a given revision fails initial tests, processing of the entry is discontinued and error annunciation is given on the CDU scratchpad. Valid revisions are recorded in the Flight Event Table by calling the Flight Plan Editor. Flight Plan parameters required by the Navigation software are then updated by the Flight Plan Monitor.

In addition to recording flight plan revisions, the Flight Plan Editor performs all geometry computations that are required as internal flight plan parameters (e.g., distance and course information). The impact of Base Offsets on the Flight Plan Editor is treated in Section 2.2.

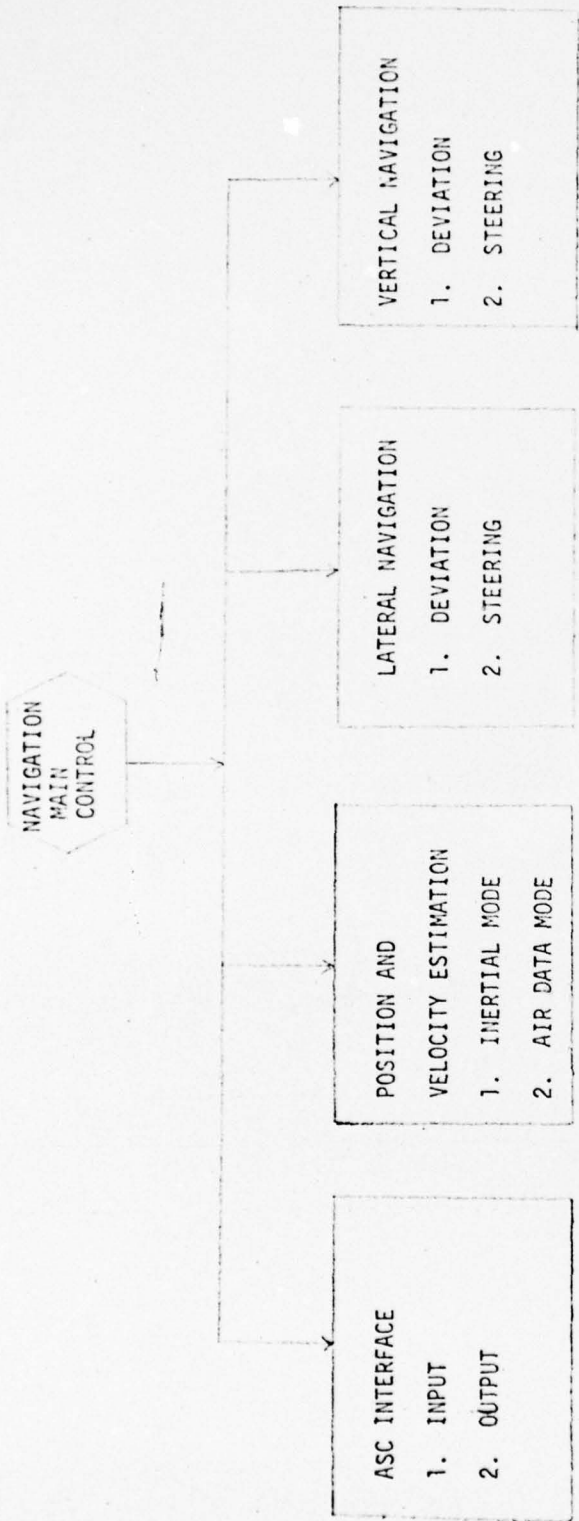


FIGURE 1-1

Major ANS-70A Functions for the Navigation Channel

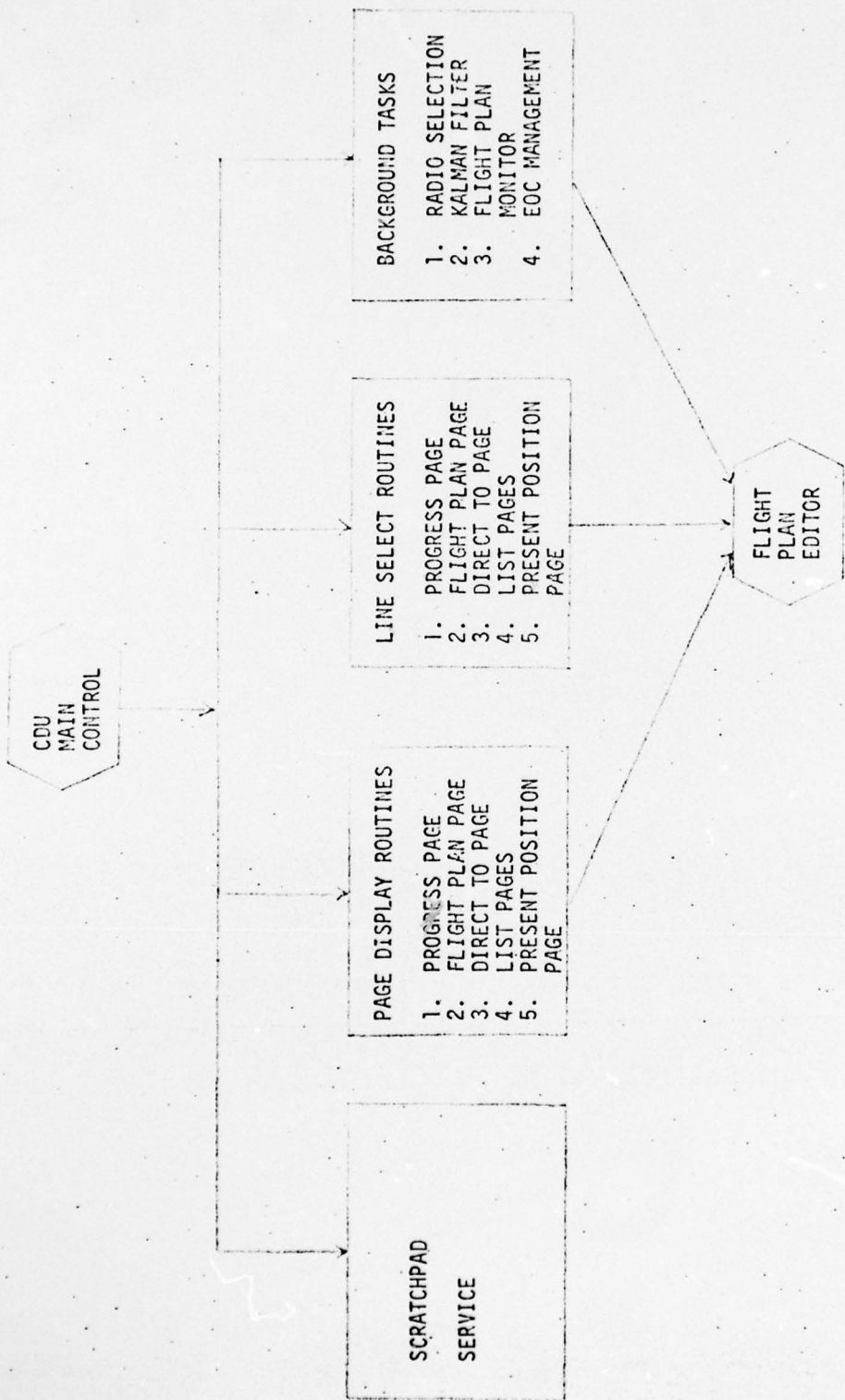
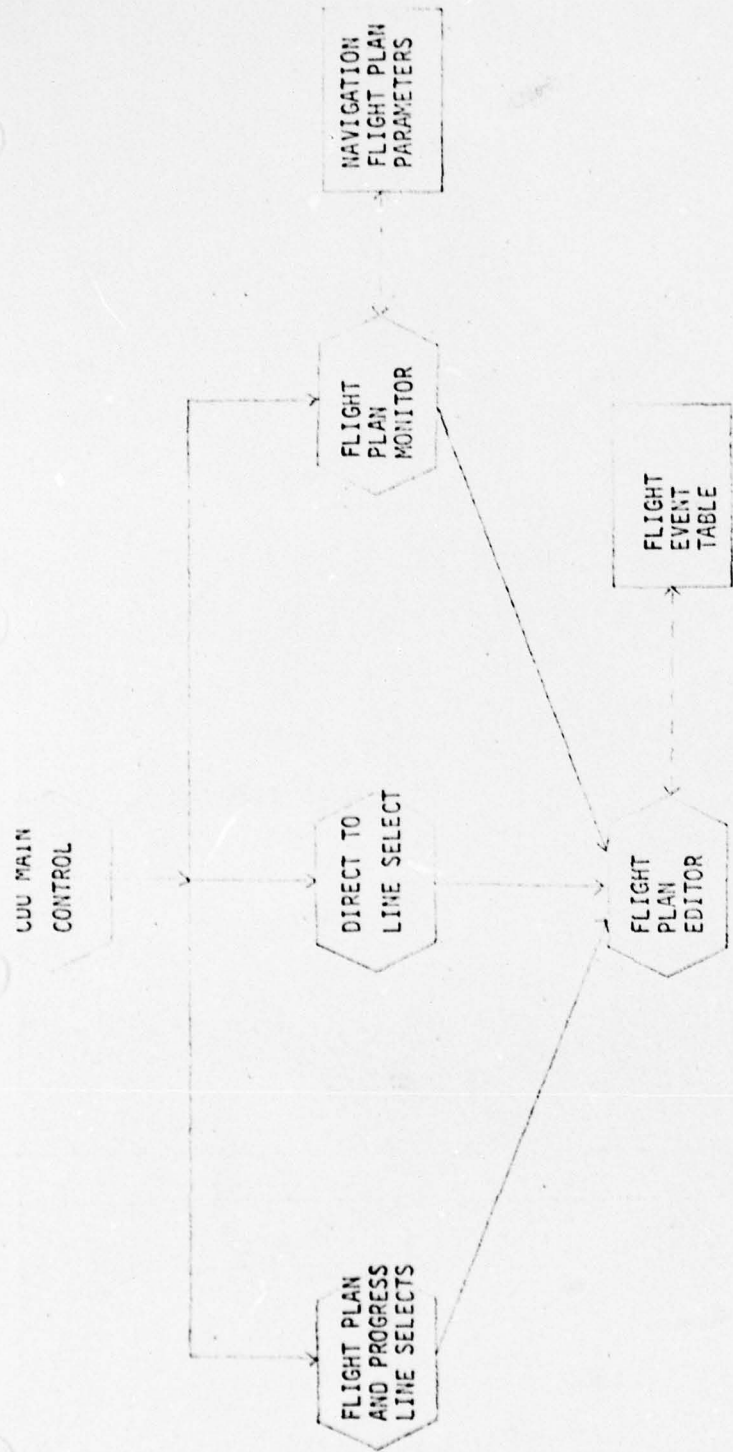


FIGURE 1-2
Major ANS-70A Functions for the CDU Channel



ANS-70A Software Interfaces for Flight Plan Management

Section 2 3D/4D BASE SYSTEM

A major goal for the software design stage was to construct a software package that minimized the impact of 3D/4D operational requirements on the existing ANS-70A Software Interfaces. In addition to ensuring system integrity, additional goals consisted of ensuring flexibility for additional changes and minimizing core requirements to the extent that software overlays could be avoided.

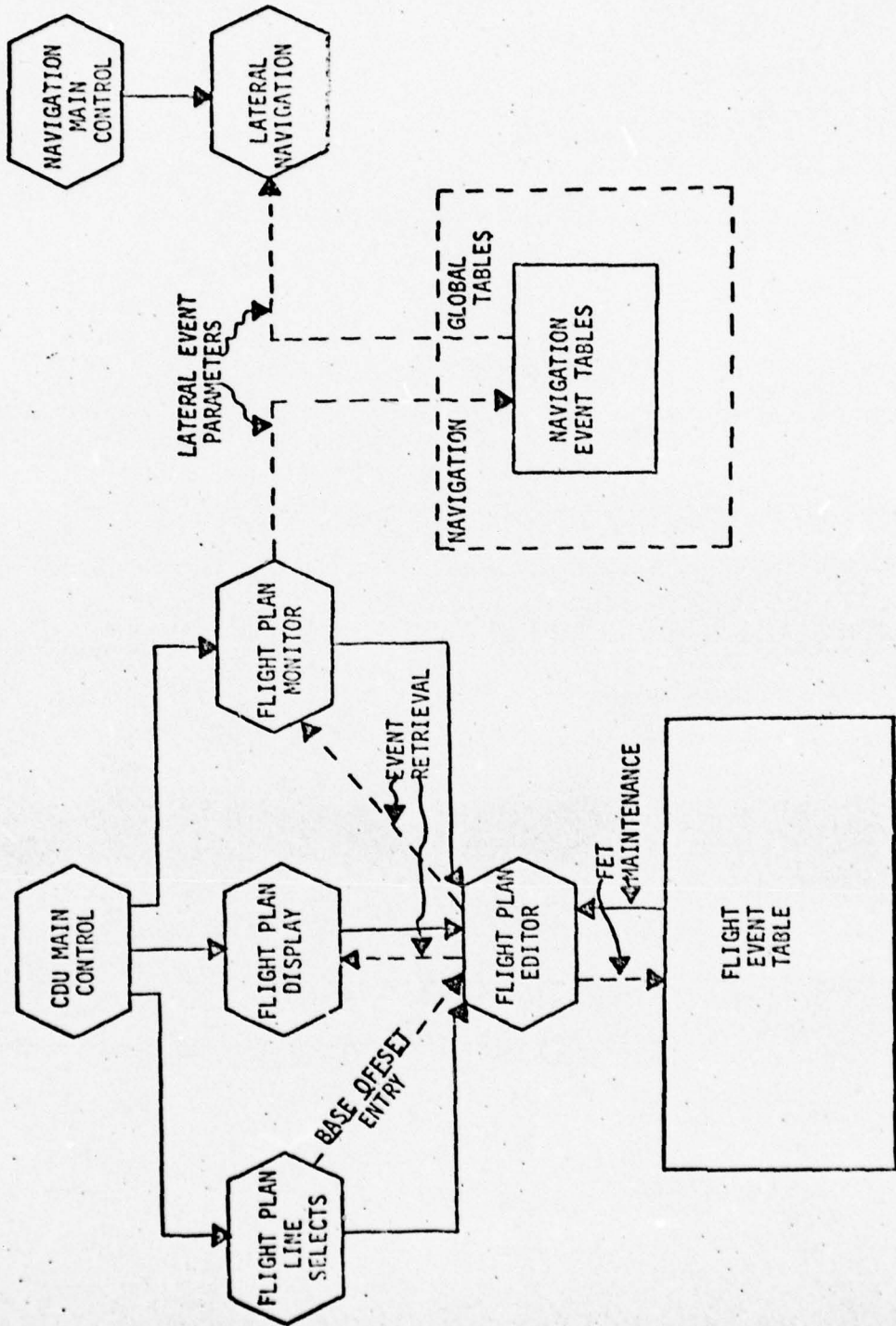
A core reduction effort was required before the 3D/4D tasks could be added to the ANS-70A configuration. Approximately 500 words of core were freed for 3D/4D usage by deleting software for Holding Patterns, the Inertial mode of navigation, Heading and Armed modes, and Commanded Vertical Angle. An additional 1500 words were gained by reducing the Data Base to 1000 words.

Once the core reduction effort was completed, the following major software tasks were implemented:

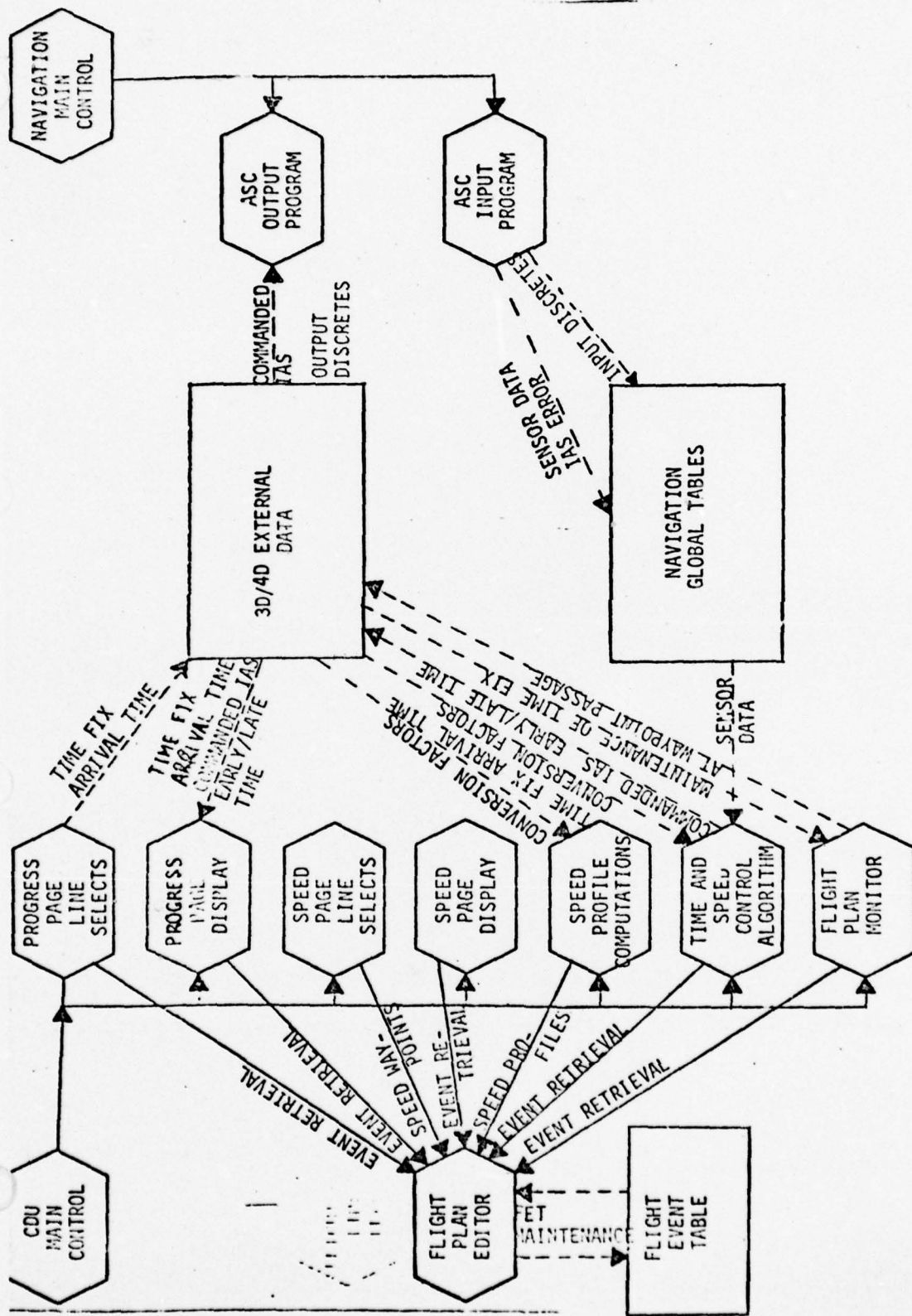
- 1) External Data Files
- 2) Base Offsets
- 3) Speed Page
- 4) Speed Profile Algorithm
- 5) Time Control Algorithm
- 6) Navigation Modifications
- 7) ASC Modifications

Each of these items is explained in detail by sections 2.1 through 2.6.

Software and data interfaces required for the major software tasks are illustrated in Figures 2.1 through 2.3. Routines for Base Offsets, the Speed Page, the Speed Profile Algorithm, and the Time Control Algorithm are supervised by the CDU Main Control Program. The ASC interface and navigation computations are controlled by the Navigation Main Control Program.



SOFTWARE INTERFACES FOR BASE OFFSETS
 FIGURE 2-1



SOFTWARE INTERFACES FOR TIME CONTROL
FIGURE 2-2

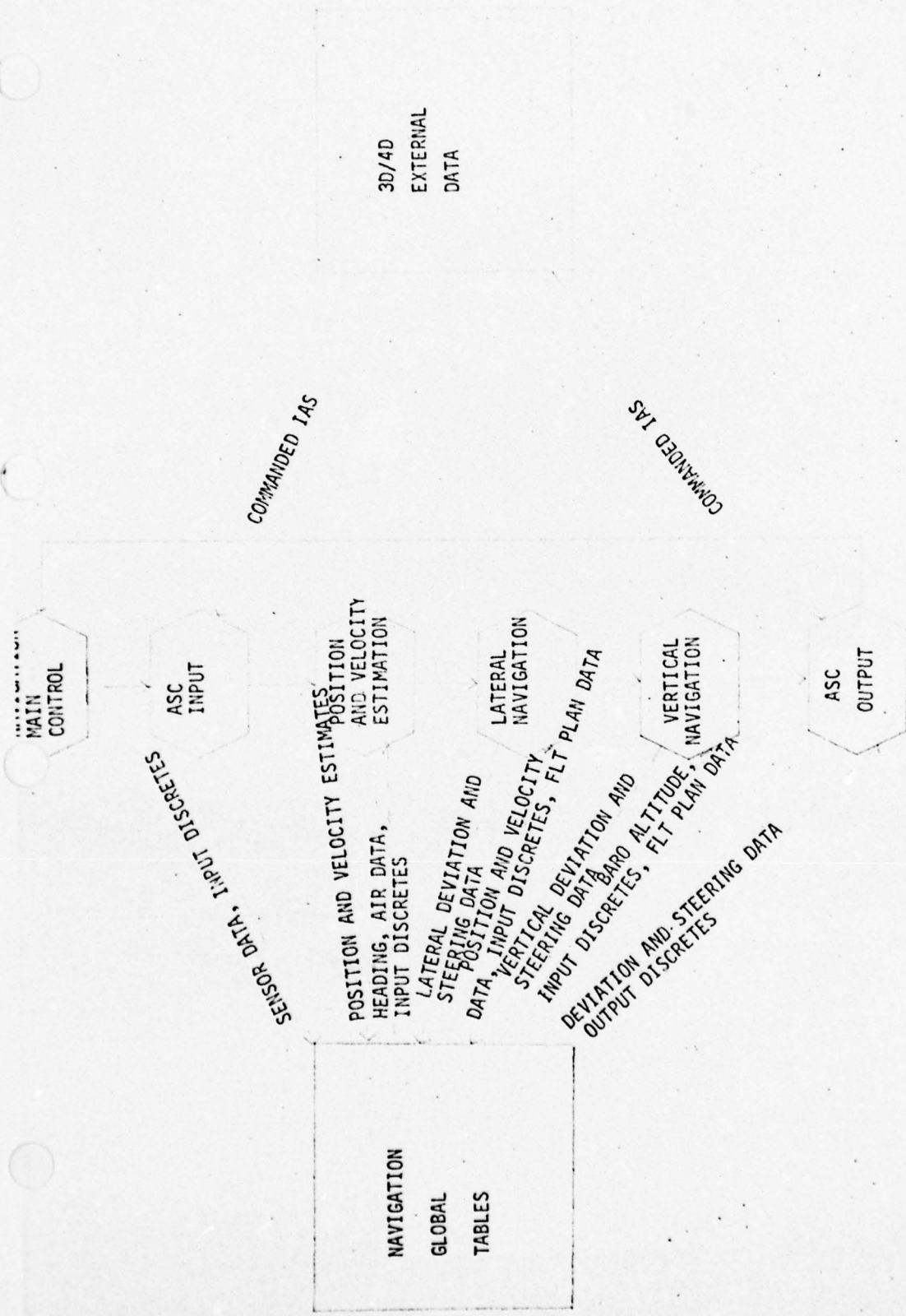


FIGURE 2-3
Software Interfaces for Navigation and ASC Interfaces

2.1 External Data Files

Program descriptions given in later sections of this volume reference data parameters whose data declarations are external to the given programs. The purpose of this section is to provide data descriptions for this external data set.

Data parameters required by more than one program have been classified by function into three basic categories. Separate compilation units have been assigned to each class of parameters for core allocation purposes. Each unit has been given a corresponding INSERT file which provides data declarations. Programs that require data declarations for a given function include an INSERT statement for the appropriate file.

The three basic EXTERNAL data files used for the Base System are 1) 3D/4D External Data File, 2) Flight Plan Editor File, and 3) the Navigation Global Tables File. A description of the data parameters assigned to each file is given below.

2.1.1 3D/4D External Data

The majority of EXTERNAL variables that are unique to the 3D/4D Task II effort are defined by the 3D/4D External Data Insert and 3D/4D External Data Preset files. Data definitions for this set of variables are given below.

<u>Symbolic Name</u>	<u>Assigned Value</u>	<u>Description</u>
VALID	0	Used to assign a valid status to 3D/4D Integer parameters that are treated as boolean data.
INVALID	1	Used to assign an invalid status to the same set of Integer parameters described for the VALID synonym.

The following list of synonyms are used for VCOMIF.

<u>Synonym Name</u>	<u>Assigned Value</u>	<u>IAS Data Display On Progress Page</u>	<u>Description</u>
IASVALID	15	Value of IAS that is maintained in VCOMI.	A valid commanded IAS has been calculated by the Time and Speed Control algorithm.
NODATA	31	----	No IAS has been entered on the Speed Page.
IVGMT	14	GMT?	Either GMT has not been entered on the Present Position Page, or a power interrupt of duration exceeding two seconds has invalidated GMT.
IVTAS	13	TAS?	The Air Data Sensor input for TAS is invalid.
IVALT	11	ALT?	The Altimeter Sensor input for Baro Altitude is invalid.
IVCOCH	7	CRS!	A Teardrop Procedure is required to capture at least one of the legs used for Time Control computations.

Integer Declarations

<u>Symbolic Name</u>	<u>Initial Value</u>	<u>Description</u>
IASMSK	"FFFFFF00"	Mask used in "AND" operations for the removal of the IASF component.
TFIX	0	ASCII identifier of the waypoint assigned as the Time-Fix.
TCOM	0	Commanded time of arrival for the Time-Fix. TCOM is recorded in GMT units (i.e., as a fraction of 1200 hours).
TFIXF	Invalid	Validity flag for TFIX.
VCOMIF	Invalid	Validity flag for VCOMI and VCOMT.
TCOMF	Invalid	Validity flag for TCOM.
TIMERF	Invalid	Validity flag for TIMERR.
COMPRF	INVALID	Validity flag that is assigned a VALID status by the Flight Plan Monitor whenever a flight plan revision has occurred. SPDPRF, the Speed Profile Routine, assigns an INVALID status to COMPRF whenever speed profile computations are performed.

<u>Symbolic Name</u>	<u>Initial Value</u>	<u>Description</u>
TCONF	INVALID	Validity flag that is assigned a VALID status by the speed profile routine whenever speed profiles are updated. TCONF is assigned an INVALID status whenever Time Control computations are performed.
Real Declarations		
<u>Symbolic Name</u>	<u>Initial Value</u>	<u>Description</u>
MINR	.00000001	Minimum magnitude that REAL numbers may be assigned on the U-1108.
VCOMI	.050	Commanded IAS displayed on the Flight Progress Page and IAS instrument. VCOMI is a fraction of 1000 kts.
VCOMT	.050	Commanded TAS calculated by the Speed and Time Control Algorithm.
MINRATE	.038566097	Value of 40 kts/min Speed Gradient. $\text{MINRATE} = 1 / \{ (40 \text{ KT/MIN}) / (1000 \text{ KT LAT VEL BASE}) * 60 \text{ MIN/HR} * 10.8039624 \text{ HRS LAT TIME BASE} \}$
EARLY	.0	Expected arrival time error for the Time-Fix. EARLY is expressed in Lateral Navigation Time Units. The Early Lat. Display on the Flight Progress Page is based on the value of EARLY. A positive value indicates a late status.
TIMERR	.0	Magnitude of EARLY. TIMERR is used by the CDU software for display of EARLY/LATE data on the Progress Page.

2.1.2 Flight Plan Editor Files

Lateral and vertical flight plan parameters maintained by the Flight Plan Editor are illustrated in Figures 2-4 and 2-5. The IASR, IASI, IASF, POFSI, and POFSIC components are the only parameters that are unique to the 3D/4D systems. Descriptions for this set of parameters are given below.

The component structure for IAS parameters is given as follows:



The IASF component is used to record the status of the IAS entry. Synonyms used for this parameter are given below.

<u>Synonym Name</u>	<u>Assigned Value</u>	<u>Description</u>
PIAS	7	Pilot-Defined IAS.
PRQUOTE	11	Profile IAS Displayed on the Speed Page as ".
PRDOWN	13	Profile IAS Displayed on the Speed Page as ↓.
PRUP	14	Profile IAS Displayed on the Speed Page as ↑.
NOIAS	15	No IAS Specified.

The first 24 bits of the entry are used to record the actual IAS magnitude as a REAL-valued fraction of 1000 kts. Although real arithmetic operations are required for the 3D/4D Speed Control and Profile Algorithms, it is also necessary to provide the capability of integer masking operations for the IASF component. Thus, the user is provided with both REAL (IASR) and INTEGER (IASI) component declarations for the IAS parameter.

WORD NUMBER	LABEL	MEANING
-3	VERS	Current Flight Plan Version (VERSFE)
-2	ABEVNO	Absolute Event Number for Event
-1	CNTRWORD	Control Word
0	WYPTID	Waypoint ID
1	WYPTLAT	Waypoint Latitude
2	WYPTLONG	Waypoint Longitude
3	WYPTVAR	Magnetic Variation (Not Supplied by the Editor)
4	POFS/POFSF	Parallel Offset (POFSFE)
5	AOFS	Along Track Offset and Status
6	DFTO	Distance from "TO" LE
7	APOF	Along Path Offset (Always = AOFS)
8	CRSI	Course In
9	CRSO	Course Out
10	AWYID	Airway ID
11	IASR/IASI IASF	Indicated Airspeed Word and Flag

FIGURE 2-4
Lateral Event Parameters Maintained by the
Flight Plan Editor

WORD NUMBER	LABEL	MEANING
-3	VERS	Current Flight Plan Version (VERSFE)
-2	ABEVNO	Absolute Event Number for Event
-1	CNTRWORD	Control Word
0	WYPTID	Waypoint ID
1	WYPTLAT	Waypoint Latitude
2	WYPTLONG	Waypoint Longitude
3	WYPTVAR	Magnetic Variation (Not Supplied by Editor)
4	POFS	Parallel Offset (POFSFE)
5	AOFS	Along Track Offset
6	DFTO	Distance from "TO" LE
7	APOF	Along Path Offset (Always = AOFS)
8	VPAI	Vertical Path Angle In
9	VPAO	Vertical Path Angle Out
10	ALTD	Altitude at VE

FIGURE 2.5
 Vertical Event Parameters Maintained by the
 Flight Plan Editor

The POFS component is used to record both parallel and base offsets. This component is defined as follows:

POFS/POFSI

POFSF

Base and Parallel offsets are treated as Real-valued fractions of π times the radius of earth in nautical miles. The component declarations for POFS, POFSI, and POFSF are similar in structure to IASR, IASI, and IASF, respectively. Synonyms applicable to the POFSF component are given below. Figure 2-6 illustrates the Base Leg waypoints identified by the POFSF synonyms.

POFSF Synonyms

<u>Symbolic Name</u>	<u>Assigned Value</u>	<u>Description</u>
PARALLEL	7	Identifies Parallel Offset Entry. The synonym "PARALLEL" serves a dual purpose. The Flight Plan Editor monitors the POFSF component for one-to-one replace edits to determine the Insertion/Deletion of Parallel Offsets for the Flight Plan. Procedures that use the Flight Plan Editor "GET" routines test the POFSF component for a value of "PARALLEL" to determine the existence of a Parallel Offset.
BASEOFST	8	Identifies the POFSI component as a base offset. This value is used to inform the Flight Plan Editor that the Flight Plan Revision is for a Base Offset.

<u>Symbolic Name</u>	<u>Assigned Value</u>	<u>Description</u>
STRT90	13	Identifies initial waypoint associated with a base offset that provides a 90 degree capture with the localizer leg.
END90	11	Identifies final waypoint associated with a base offset that provides a 90 degree localizer capture.
STRTBASE	12	Identifies initial waypoint associated with a base offset that provides a shallow capture of the localizer leg.
ENDBASE	10	Identifies waypoint whose CRSI component defines the Base Leg for a Base Offset defined for a shallow localizer capture angle.
INTERCEP	9	Identifies waypoint whose CRSI and CRSO components define the intercept point for localizer capture.
NOPOFS	15	No offset entry has been made.
CANCEL	14	Identifies an edit that cancels an existing offset.

POFSE is used to record the value of an existing Parallel or Base Offset.

PFSTAT is used to record the present status of offsets. Synonyms PARALLEL,

BASEOFST, and NOPOFS are used to indicate offset status.

With the exception of the Flight Plan Editor, POFSE and PFSTAT are treated as read-only parameters. Any requirement to change the offset parameters is accomplished via a one-to-one replace edit with the desired change specified via the POFSE component.

2.1.3 Navigation Global Tables

External parameters required for navigation computations are stored in the Navigation Global Tables. A single version of this file is used for all three Task II systems. The remaining portion of this section describes 3D/4D modifications to the Navigation Global Tables.

The ANS-70A version of the ADHD table has been expanded to include sensor inputs for Indicated Airspeed Error, Localizer Deviation, Glideslope Deviation, and HSI Course Input. A description of the ADHD components used for the 3D/4D systems is given below.

<u>Symbolic Name</u>	<u>Component Position</u>	<u>Description</u>	<u>Validity Flag</u>
LAT	0	Aircraft Latitude as maintained by the Lateral Filter.	N/A
LONG	1	Aircraft Longitude as maintained by the Lateral Filter.	N/A
PSIM	2	Magnetic Heading	PSMF
BALT	3	Barometric Altitude	BALF
TAS	4	True Air Speed	TASF
VRT	5	Vertical Rate (not input for the 3D/4D system)	N/A
PALT	6	Pressure Altitude (not input for the 3D/4D system)	N/A
DELV	7	Indicated Air Speed Error	DELVF
LOC	8	Localizer Deviation	LOCF
GS	9	Glideslope Deviation	GSF
HSICRS	10	HSI Course Input	HSICRSF

ANS-70A Lateral Deviation computations always reference the parent waypoint of the Lateral To-Event. Similar computations for the 3D/4D system use the leg intersection of the path actually being flown as the frame of reference. The following set of parameters is used for this task:

<u>Symbolic Name</u>	<u>Description</u>
TOLEG	Array used to record the coordinates of the leg intersection defined for the Lateral To-Event.
BFLEG	Work area used to record bearing from the leg intersection to the aircraft.
BTLEG	Work area used to record bearing from the aircraft to the leg intersection.
DTLEG	Distance between the aircraft and the oncoming leg intersection.

Parameters used to record ASC input discretes that are unique to the 3D/4D systems are given below.

<u>Symbolic Name</u>	<u>Description</u>
APENG	Status of the Auto-Pilot-Engaged discrete. APENG is assigned a TRUE status whenever the Area Nav system is coupled to the Auto-Pilot.
RNAVENG	Status of the RNAV-Engaged discrete. RNAVENG is assigned a TRUE status whenever the RNAV system provides lateral navigation and possibly lateral steering.
VNAVENG	Status of the VNAV-Engaged discrete. VNAVENG is assigned a TRUE status whenever the RNAV system provides vertical navigation and possibly vertical steering.

2.2 Base Offsets

Figure 2-6 illustrates the software interfaces that have been implemented for the Base Offset function. The key interface is provided by the Flight Plan Editor Utility Module. A description of this module will follow a brief summary of the roles played by the CDU Line-Select and Flight Plan Monitor modules.

Classification of a CDU scratch-pad entry as a candidate for a Base Offset is performed by the CDU software. Base Offset entries are permitted for waypoints that appear on the Flight Plan, Progress, or Speed pages. Valid candidates are passed onto the Flight Plan Editor Utility Module for additional processing. "ERROR" is annunciated on the scratch-pad if either of the following conditions invalidates the edit: range tests are failed, or the existing flight plan already includes a parallel offset.

Automatic cancellation of an existing Base Offset occurs following passage of the last waypoint associated with the given offset. This task is performed by the Flight Plan Monitor. The Base Offset is cancelled whenever waypoint passage occurs for the waypoint whose POFSF component has an assigned value of INTERCEP or END90.

The Flight Plan Editor Utility Module provides an interface between the CDU software and a modified version of the ANS-70A Flight Plan Editor. All flight plan revisions entered by the pilot are routed through this module. Most of the major software tasks required for the Base Offset function are provided by this module. The remaining portion of the section provides a description of tasks that have been implemented for the Flight Plan Editor.

A primary task consists of verifying geometry requirements for Base Offset entries. Figure 2-7 illustrates the basic geometries for Base Offsets.

Geometry requirements for the Two-Waypoint configuration are given as follows:

$$(1) \quad X = ||\text{COCH}(W_{I-1})|-90^\circ| \leq 2^\circ$$

and $|\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$

$$(2) \quad X = ||\left[\sum_{J=I-1}^I \text{COCH}(W_J) \right] |-180^\circ| \leq 2^\circ$$

and $|\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$

and $Y = ||\text{COCH}(W_I)|-90^\circ| \leq 2^\circ$

and $|\text{POFS}(\text{WKPTR})| * (\pi Y / 180^\circ) \leq 0.2 \text{ NM}$

Geometry tests that must be performed for the Three-Waypoint configuration are given as:

$$(1) \quad X = ||\text{COCH}(W_{I-1})|-90^\circ| \leq 2^\circ$$

and $|\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$

$$(2) \quad X = ||\left[\sum_{J=I}^{I+1} \text{COCH}(W_J) \right] |-90^\circ| \leq 2^\circ$$

and $|\text{POFS}(\text{WKPTR})| * (\pi X / 180^\circ) \leq 0.2 \text{ NM}$

and $Y = ||\left[\sum_{J=I-1}^{I+1} \text{COCH}(W_J) \right] |-180^\circ| \leq 2^\circ$

and $|\text{POFS}(\text{WKPTR})| * (\pi Y / 180^\circ) \leq 0.2 \text{ NM}$

This set of tests is intended to provide protection against absurd offset geometries. If the geometry is found to be valid, POFS and POFSF components are updated for the offset waypoints and recorded in the Flight Event Table. If the geometry requirements are not met, control is returned to the CDU software. In either case, a return argument is used to indicate the status of the Base Offset entry.

A second major task consists of enforcing a set of operational rules that have been imposed on all flight plan revisions. The purpose of this set of rules is to insure that flight plan revisions do not invalidate the geometry for an existing Base Offset.

Special operational rules are required for DIRECT TO entries. As with the ANS-70A system, an existing Parallel Offset is cancelled whenever a valid DIRECT TO revision is made. A Base Offset, however, is cancelled only if the resulting flight plan revision affects the Base Offset waypoint configuration. A summary of the logic used to cancel Base Offsets for DIRECT TO entries is given in Table 2-1.

Operational rules that are implemented for remaining flight plan revisions are given as follows:

- 1) A Base Offset entry is to be inhibited whenever the current flight plan includes a Parallel Offset. The converse is also true, i.e., a Parallel Offset entry is not allowed for a flight plan that already includes a Base Offset.
- 2) The magnitude of an existing Base Offset may be revised at any time. A Parallel Offset may be overwritten at any time by entering another Parallel Offset into the flight plan.
- 3) No flight plan revision is allowed that would change the geometry of an existing Base Offset configuration.

Table 2-2 provides a summary of the logic that has been implemented for the above set of rules. PFSTAT, which appears in the table, is a parameter which is used to record current offset status. PFSTAT has three possible states: BASEOFST, PARALLEL, or NOPOFS. POFSF is an input parameter that is used to identify a flight plan revision. POFSF is assigned one of 4 possible states

by the calling program: BASEOFST, PARALLEL, NOPOFS, or CANCEL. A description of this set of data parameters is given in Section 2.1.2.

The Utility Module provides four routines that are called by the CDU software. The ADD4D and REPLY4D routines are used for all flight plan revisions that occur on the Flight Plan, Speed, and Progress pages. The ADDDIR and REPDIR routines are called for DIRECT TO edits. Program listings for this set of routines are given in Appendix A.

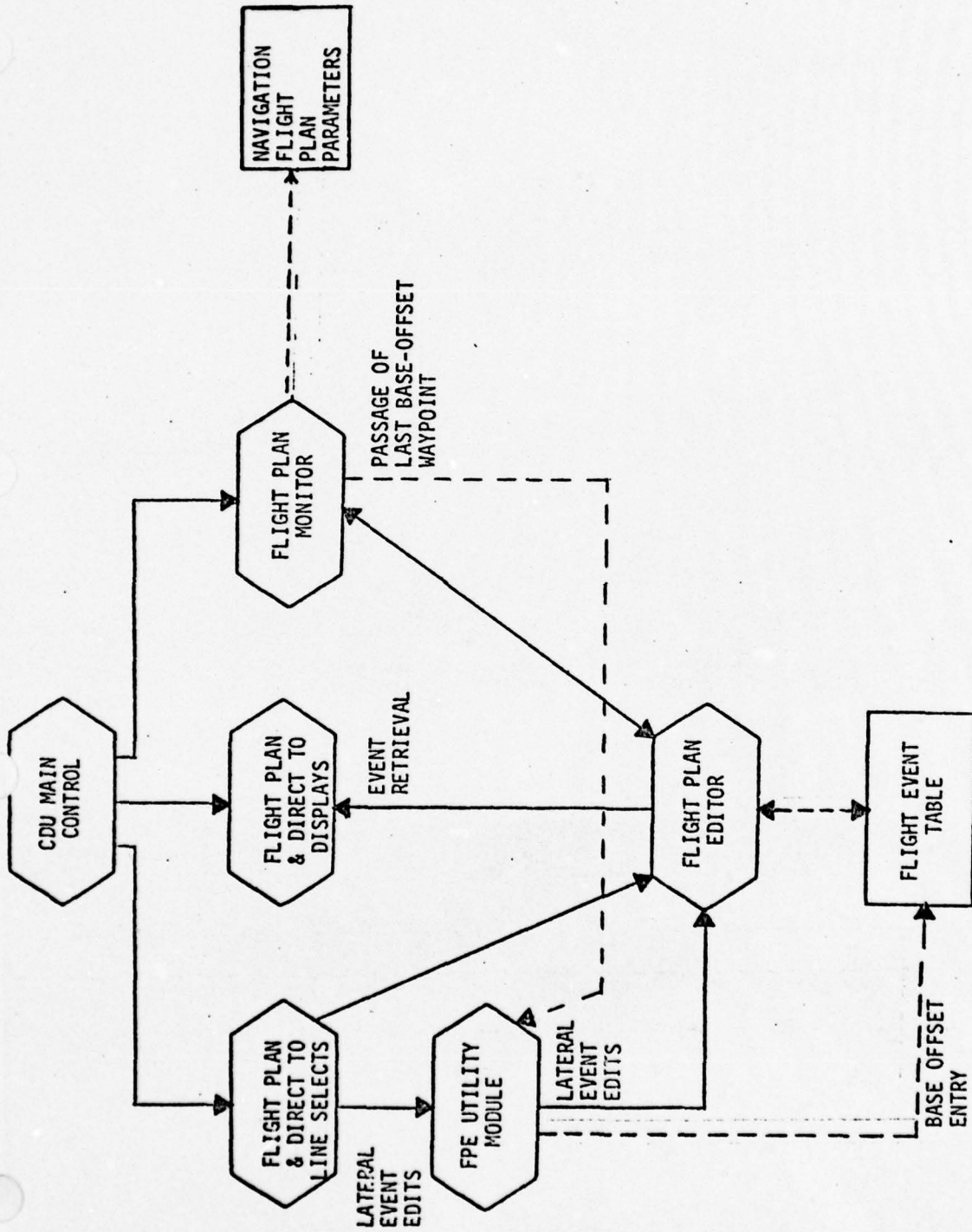
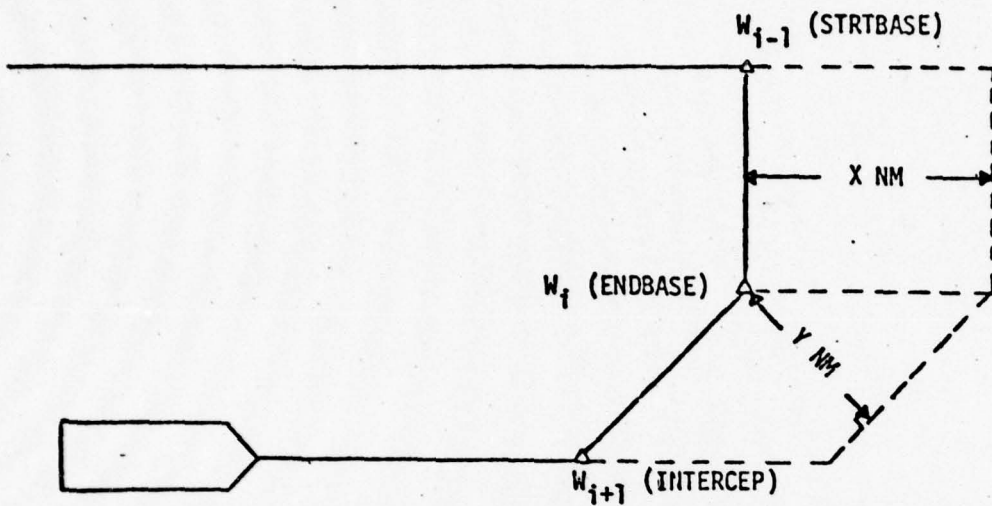


FIGURE 2-6
Software Interfaces for Base Offsets



$$Y = -X * \text{SIGN}[\text{COCH}(W_{i+1})] * \text{SIN}[|\text{COCH}(W_{i+1})|]$$

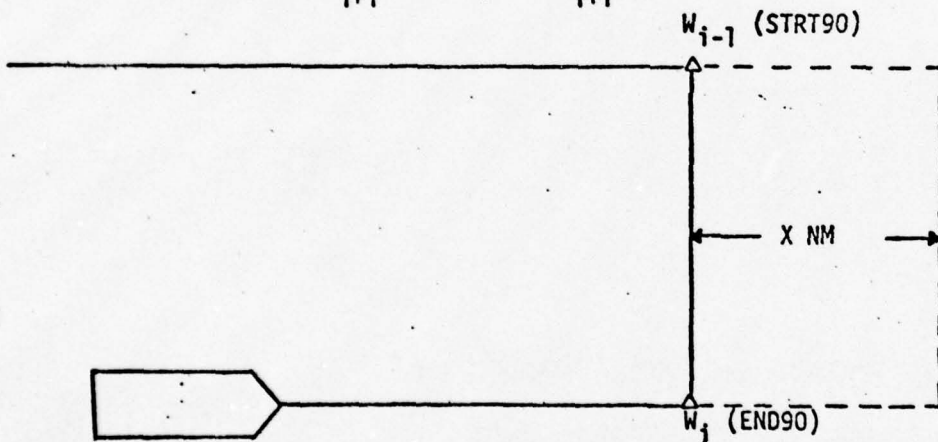


FIGURE 2-7

Basic Geometries for Base Offsets

Type of DIRECT TO

Requirements for cancelling an
existing Base Offset

DIRECT TO the TO-
Waypoint

The TO-Waypoint must be a Base
Offset waypoint.

DIRECT TO the
Scratchpad entry

The TO-Waypoint must be a Base
Offset waypoint.

DIRECT TO a waypoint
in the flight plan other
than the TO-Waypoint

The flight plan must contain a
Base Offset waypoint that is
entered either at or before the
"DIRECT TO waypoint."

TABLE 2-1

Operational rules used to cancel Base Offsets
for DIRECT TO entries

DECISION LOGIC		NP	NP	NP	NP	D	B	B	B	B	B	P	P	P	F
CONDITIONS	PESTAT (CURRENT OFFSET CONFIG.)	NP	B	NP	NP	NP	B	B	B	B	B	P	P	P	F
	POFSF (DESIRED OFFSET CONFIG.)	NP	B	NP	NP	NP	B	B	B	B	B	P	P	P	F
	EDIT TOUCHES BASE OFFSET					N	Y								S
	GEOMETRY CHECKS ARE SATISFIED		N	Y			N	Y							F
ACTIONS	CANCEL OFFSETS							X	X			X	X		
	ENTER NEW OFFSET				X			X				X			
	PASS EDIT TO FPE	X				X							X		
	MARK BASE OFFSET WAYPOINTS				X				X						
	EDIT DISALLOWED		X				X	X							X
	CDU PREVENTS OCCURRENCE										X	X			

NP = NOPOFS
 B = BASEOFFST
 P = PARALLEL
 C = CANCEL

TABLE 2-2
 Summary of Logic used to Implement Operational Rules for Flight Plan Revisions

2.3 Speed Profile Algorithm

Software interfaces required for implementation of the Speed Profile Algorithm are shown in Figure 2-8. An IAS entry on the Speed Page is recorded as a flight plan parameter in the Flight Event Table. A description of the IAS parameter was given in Section 2.1.2.

Speed profile computations are implemented within the CDU channel by a routine called SPDFRF. Computations are performed whenever a flight plan revisions occurs.

Special logic is required for the From-Waypoint. This waypoint is always treated as a speed-control waypoint whenever the flight plan contains an IAS entry. This is done to ensure that a speed profile presently being flown will not be changed at waypoint passage.

The task description for SPDFRF is given below. A diagram illustrating the use of program parameters is given in Figure 2-9. A program listing of SPDFRF is given in Appendix B.

Task Specification for SPDRF

Procedure Type

Integer Procedure SPDRF

Module

3D/4D Time and Speed Algorithms

Task Summary

Speed profile computations are performed for all lateral events that are not considered to be speed-control waypoints. (Speed-Control waypoints are waypoints for which speed has been entered via the CDU.) The lateral FROM-event is treated as a speed-control waypoint to ensure that a speed profile presently being flown will not change at waypoint passage. Results of profile computations are recorded in the IASR/IASI/IASF component structure for lateral events.

Notation

- W(J) Used to denote the Jth lateral event
- IASR(J) Used to denote the value of the IASR component for W(J). Similar notation is used for other components defined by the Flight Plan Editor.

Internal Data Structures

Integer Data

- FRST Absolute Lateral Event Number Index for the initial speed-control waypoint of a given profile.
- LAST Absolute Lateral Event Number Index for the final speed-control waypoint of a given profile.
- FRST.STATUS Used to record the validity of FRST for a given profile.
- LAST.STATUS Used to record the validity of LAST for a given profile.
- J Absolute Event number of the Jth lateral event.

Real Data

PROFDST The along-track distance between W(FRST) and W(LAST).
DVEL The velocity change between W(J-1) and W(LAST).
DJ The along-track distance between W(J-1) and W(J).
DELDIST The along-track distance between W(J) and W(LAST).
T1 The time required to fly from W(J-1) to W(LAST) at a rate of 40 knots/minute.
AVEV The average velocity required for a linear speed profile between W(J-1) and W(LAST).
T2 The time required to fly from W(J-1) to W(LAST) assuming a constant velocity of AVEV.
DPP The distance required to realize a velocity change of DVEL at the rate of greater than or equal to 40 knots/minute.

Calling Sequence

SPDPRF()

Return Values

Speeds assigned to intermediate profile points are recorded in the Flight Plan Editor's FET structure.

Task Description

IF a flight plan revision has occurred since the last speed profile computation

THEN

BEGIN ... SPDPRF loop.

Starting with the FROM-waypoint, scan the flight plan for a speed entry.

IF no speed entry has been found

THEN

BEGIN No Speed Entry loop.

Update bookkeeping to indicate that another attempt to compute speed profiles is not required for the present flight plan (this is intended to assist CDU keyboard response time).

```

    RETURN to calling program.
END No Speed Entry loop.
Assign the first speed to the FROM-waypoint.
Tag the FROM-waypoint as FRST.
Assign VALID to FRST.STATUS.
WHILE FRST.STATUS EQL VALID DO
BEGIN    ...FRST Valid loop

    Assign INVALID to LAST.STATUS

    Starting with W(FRST+1) scan the flight plan for a speed-control
    waypoint.

    IF the speed-control waypoint is found
    THEN
        BEGIN    ...LAST Valid loop

            Assign VALID to LAST.STATUS.

            Tag the speed-control waypoint as LAST.

            Determine PROFDST, the along-track distance between W(FRST)
            and W(LAST).

            IF LAST NEQ (FRST+1)    ...Note that speed profile computations,
            i.e., the Profile loop, will be bypassed if successive lateral
            events are defined as speed-control waypoints.

        THEN

        BEGIN    ...Profile loop.

            IF the speed for W(FRST) and W(LAST) are equal
            THEN

                BEGIN    ...Same Speed loop.

                    FOR J=(FRST+1) STEP 1 UNTIL LAST DO
                    BEGIN    ...Assign Same Speed loop

                        Assign the speed for W(FRST) to W(J).

```

$$IASR(J) = \text{SQRT} [V_0^2 + (V_F^2 - V_0^2) * \frac{D}{DPP}]$$

Where:

D=DJ
 V₀=IASR(J-1)
 V_F=IASR(LAST)
 DPP=DJ+DELDIST

Assign either PRUP or PRDOWN to the IASF component of W(J) for CDU display purposes.

END ...Linear loop

ELSE ...At this point it has been determined that an average speed rate less than 40 kts/min is required to fly from W(J-1) to W(LAST).

IF an average rate of less than 40 kts/min is also required to fly from W(J) to W(LAST), assign IASR(J-1) to IASR(J).

BEGIN ...40 Kts/Min loop

Determine DPP, the distance required to realize a velocity change of DVEL at the rate of 40 Kts/Min, i.e.,
 DPP=T1*AVEV

IF the distance, DELDIST, between W(J) and W(LAST) is greater than or equal to DPP

THEN

BEGIN ...No Change loop

Assign IASR(J-1) to IASR(J) and PRQUOTE to IASR(J).

END ...No Change loop

ELSE

BEGIN ...Min Rate Zone loop

Calculate a velocity for W(J) that is based on a 40 kt/min velocity rate between W(J-1) and W(J), i.e.,

$$IASR(J) = \text{SQRT} [V_0^2 + (V_F^2 - V_0^2) * \frac{D}{DPP}]$$

Where

$V_0 = \text{IASR}(J-1)$
 $V_f = \text{IASR}(\text{LAST})$
 $D = \text{DPP} - \text{DELDIST}$

Assign either PRUP or PRDOWN to IASR(J-1).

END ...Min Rate Zone loop

END ...Min Rate Zone loop

END ...Velocity Change loop

END ...Profile loop

Define parameters for next cycle of FRST.VALUE loop:

FRST=LAST.

FRST.STATUS=LAST.STATUS.

LAST.STATUS=INVALID

END ...LAST Valid loop

END ...FRST Valid loop

Update bookkeeping to indicate that speed profile computations have been performed for the existing flight plan.

END ...SPDPRF loop

RETURN to calling program.

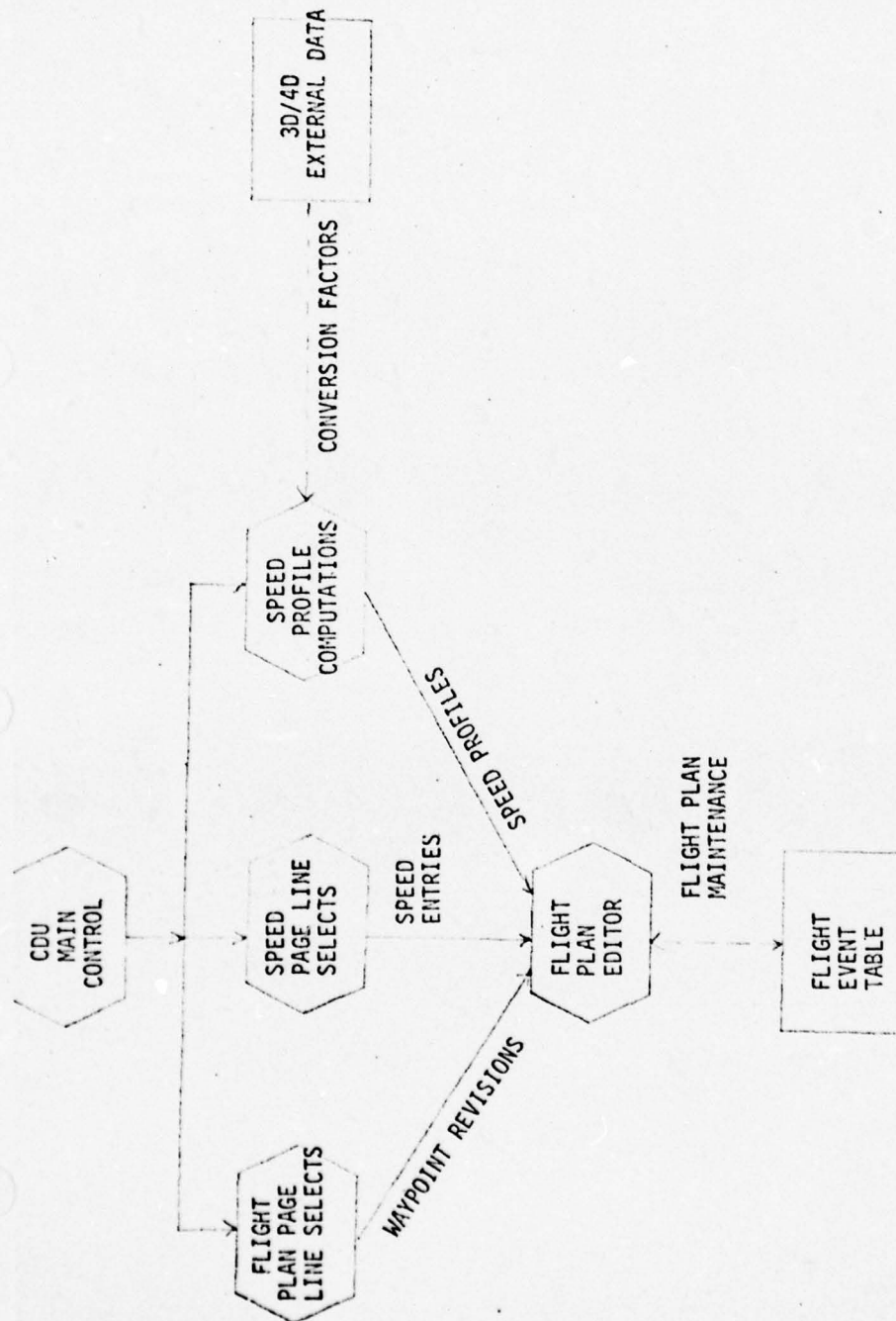


FIGURE 2-8

Software Interfaces for Speed Profiles

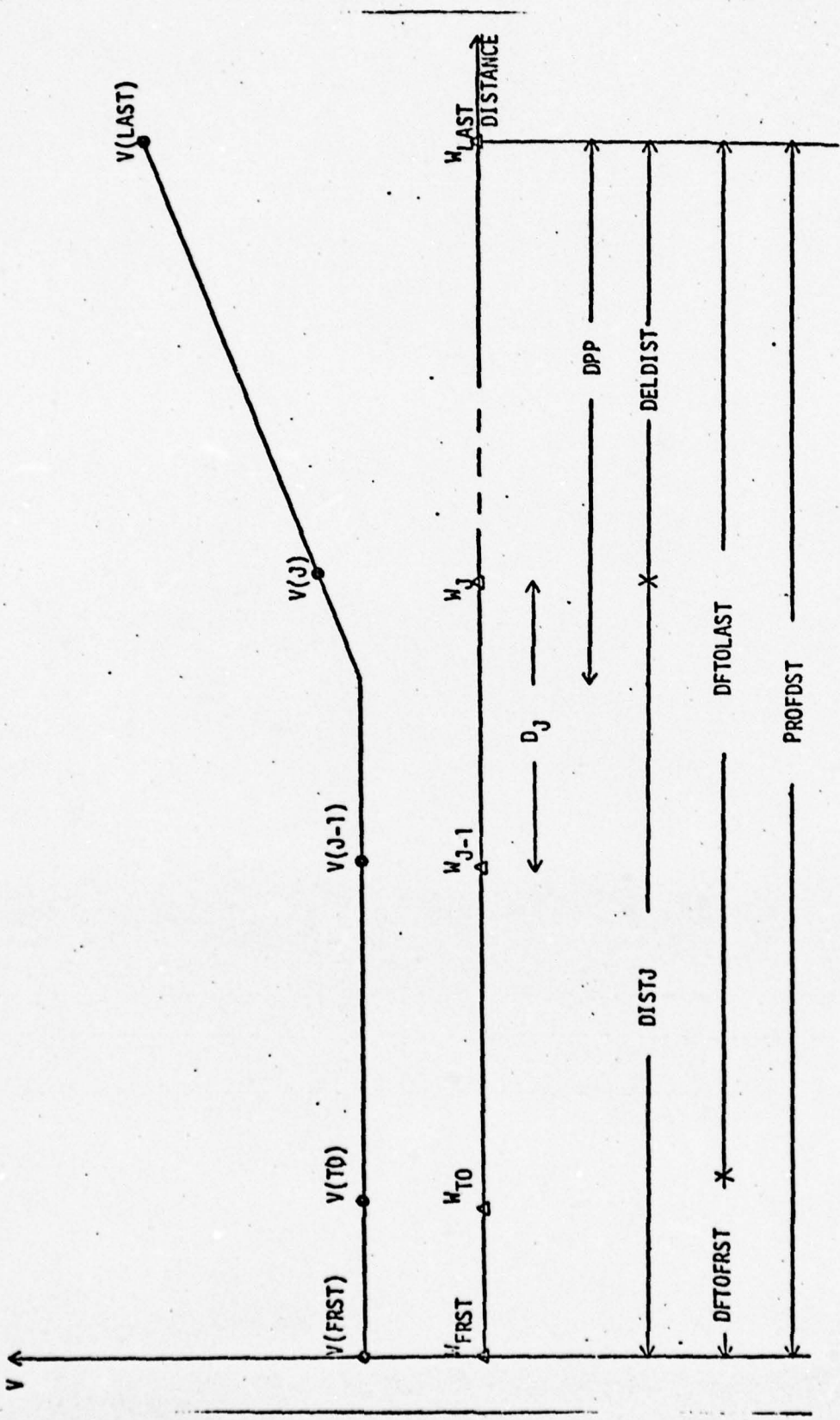


FIGURE 2-9
Description of Program Parameters used to implement the Speed Profile Algorithm

2.4 Time Control Algorithm

Figure 2-8 illustrates the basic software interfaces required for maintenance of the Time Control parameters. Data declarations for the Time Control Parameters were given in Section 2.1.1. With the exception of aircraft sensor data, all parameters are maintained by procedures that are called by the CDU Main Control procedure. The Time Fix and Commanded Arrival Time are CDU entries made on the Flight Progress Page. The same page is used to display the software computations for Commanded IAS and Arrival Time Error (Early/Late Indication). The Flight Plan Monitor monitors waypoint passage of the Time-Fix to determine the necessity of invalidating algorithm computations.

2.4.1 CDU Display of Time Control Parameters

The last two line pairs of the Flight Progress Page are used for the display of Time Control parameters. Data declarations for this set of parameters are given in Section 2.1.1. Line pair #5 provides information for the Time-Fix, TFIX, Commanded Arrival Time, TCOM, and Commanded Air Speed, VCOMI. The validity flags TFIXF and TCOMF are monitored to determine the need to display blank data fields for TFIX and TCOM, respectively. The value stored in VCOMI is displayed for the Commanded Air Speed data field whenever VCOMIF has an assigned value of IASVALID.

Line pair #6 is used for the Early/Late and Navigation Downmode displays. The latter function is identical to that defined for the ANS-70A system. Values for the Early/Late display are recorded in TIMERR and EARLY. The EARLY label is displayed whenever EARLY is valid and negative; LATE is displayed for a valid positive value. The value recorded in TIMERR is used for display of the Early/Late data line. No display is required for the Early/Late label and data lines whenever the validity flag TIMERF is assigned an INVALID status.

2.4.2 CDU Line-Select Operations

Line pair #5 for the Flight Progress Page provides the pilot with the capability of designating a waypoint as the Time-Fix and a Commanded Arrival Time for this waypoint. The two data fields used to enter this information may be entered (or revised) separately or simultaneously.

Rules governing line-select entries are as follows:

TIME Entries:

- 1) The same range checks used for GMT entries on the Present Position Page apply to the Time Entry.
- 2) The value of the Time Entry is recorded in TCOM and the associated validity flag, TCOMF, is assigned a VALID status.

WAYPOINT Entries:

- 1) The waypoint must be stored in the Flight Plan prior to the WAYPOINT entry on the Flight Progress Page.
- 2) A valid entry is recorded in TFIX. TFIXF is assigned a VALID status to indicate that a Time-Fix has been designated.

A single scratch pad entry of a minus (-) sign is used to invalidate both fields. An INVALID status is assigned to both TFIXF and TCOMF whenever this entry is made.

2.4.3 Functional Description of Time Control Algorithm

The description of the Time Control Algorithm uses the following notation:

i Subscript used to represent the i^{TH} waypoint. The following values of i will be of special significance:

- $i = 0$ For the FROM-WAYPOINT
- $= 1$ For the TO-WAYPOINT
- $= T$ For the waypoint designated as the time-fix.

W_i The i^{TH} waypoint.

CRS_i The course into W_i as given by the flight plan.

- $WATK_i$ The along-track component of wind for W is $WATK_i = -(NWND * \cos(CRS_i) + EWND * \sin(CRS_i))$, where NWND and EWND represent present lateral filter estimates for north and east wind components, respectively. $WATK_i$ denotes the present along-track component of wind.
- \overline{VNOM} The nominal value for present commanded TAS. \overline{VNOM} is a function of $\overline{V}_0, \overline{V}_1$, the time estimated to fly the along-path distance between W_0 and W_1 , and the actual distance from the aircraft to the TO waypoint.
- VCOM The present commanded IAS of the aircraft. VCOM represents the commanded IAS displayed on the Flight Progress Page.
- \overline{VCOM} The present commanded TAS of the aircraft.
- VACT Air data sensor input for present aircraft TAS.
- VACT Present aircraft IAS as given by the speed and time control algorithm.
- V_i The IAS (Indicated Air Speed) associated with W_i .
- \overline{V}_i The TAS (True Air Speed) associated with W_i .
- \overline{TTGCOM}_i The commanded (actual) time required to reach W_i . In particular, the commanded time required to reach the desired time fix, \overline{TTGCOM}_T , is given by $\overline{TTGCOM}_T = (\text{Time commanded to arrive at the time fix}) - (\text{Present Time})$.
- \overline{TTGNOM}_i The nominal time required to reach W_i . \overline{TTGNOM}_i is a function of IAS entries and flight path geometry.
- D_i The leg distance between W_{i-1} and W_i . D_i is defined as the actual distance from the aircraft to the To-Waypoint.
- D_i' That portion of D_i that is to be flown at a constant speed.
- D_i'' That portion of D_i that requires a velocity change.

An important concept of the Task II Speed Control Philosophy is the utilization of minimum 40 knot/minute speed change profiles. Pilot reaction to speed changes is not required until a minimum speed change of 40 knots/minute is needed to reach a desired airspeed. This means that the speed profile for any given leg may be presented as one of the two situations depicted in Figure 10.

Ignoring wind, let K denote the proportionality factor that represents the proportion of nominal speed that is required to arrive at the time fix on schedule (K=1 if no change in the nominal profile is required to meet the desired schedule).

Then $V_{COM} = K * V_{NOM}$ where K is to be determined from the relation:

$$K = \overline{TTGNOM}_T / \overline{TTGCOM}_T$$

As noted before, \overline{TTGCOM}_T is merely the difference between the time (GMT) commanded to arrive at W_T and the present time (Present value of GMT). \overline{TTGNOM}_T is given by summing the nominal times required to fly all legs until W_T is reached, i.e.,

$$\overline{TTGNOM}_T = \frac{MTG'}{V_0 + WATK_1} + \frac{MTG''}{(V_0 + V_1)/2 + WATK_1} + \sum_{i=2}^T \left(\frac{D_{i-1}'}{V_{i-1} + WATK_{i-1}} + \frac{D_{i-1}''}{(V_{i-1} + V_i)/2 + WATK_{i-1}} \right)$$

In the above expression, $MTG = MTG' + MTG''$ is the actual distance from the aircraft to the To-Waypoint. MTG' and MTG'' are analogous to D_i' and D_i'' , respectively.

Having found K, the value of the commanded TAS for the present leg is given by $V_{COM} = K * V_{NOM}$. The best available along-track component of wind for the present leg is given by using the Lateral Filter's Estimates for north and east wind components. This dynamic computation for along-track wind cannot be proportionately modified for the remaining portion of the present leg. At best, it may only be used to directly modify the dynamic computations for V_{COM} and V_{NOM} . Thus,

$$\overline{V_{COM}} + W = K * (\overline{V_{NOM}} + WATK_1) \text{ or}$$

$$\overline{V_{COM}} = K * \overline{V_{NOM}} + WATK_1 * (K-1), \text{ where } WATK_1 \text{ represents the present component of along-track wind.}$$

\overline{VCOM} represents the present commanded true air speed that is necessary to arrive at W_T on time. The corresponding commanded IAS is computed by the relationship

$$VCOM = (1-K_1h) * \overline{VCOM}$$

The value used for K_1 is the value relating present IAS to present TAS and is computed as follows. The present aircraft IAS ($VACT$) is not directly available to the computer but can be computed from the IAS command ($VCOM$) and IAS airspeed error (ΔV) signals which are available from the max allowable airspeed instrument, i.e.,

$$VACT = VCOM + \Delta V.$$

Present values for aircraft TAS (\overline{VACT}) and altitude (h) are resident in the RNAV computer memory. Using the relationship

$$VACT = \overline{VACT} (1 - K_1h),$$

the altitude proportionality constant, K_1 , may then be determined by combining the above equations, i.e.,

$$(1-K_1h) = (VCOM + \Delta V)/\overline{VACT}$$

$$\text{and } K_1 = (\overline{VACT} - VCOM - \Delta V)/(h * \overline{VACT})$$

With h in feet, K_1 should vary from 0.00001 to 0.000015. Because of sensitivity problems as h becomes small, K_1 is to be limited to the above values in the IAS to TAS speed conversions. In the TAS to IAS conversion regarding the commanded velocity the $(1-K_1h)$ ratio can be used directly, avoiding any sensitivity problem.

The Commanded Speed displayed on the Flight Progress Page is then given by:

$$VCOM = (1-K_1h) * \overline{VCOM}$$

The final portion of the algorithm deals with the early/late computation. This computation is based upon the expected time error at the time-fix that would result by flying the present leg at the actual rather than commanded TAS.

As before, let:

\overline{VCOM} Represent the present value for commanded TAS.

\overline{TTGCOM}_T Represent the commanded time required to reach W_T .

\overline{VACT} Represent the present air data sensor input for TAS.

Also, let:

D_T Represent the modified along-track distance from the aircraft to W_T . The modification consists of using actual distance from the aircraft to the To-waypoint for the present leg.

\overline{TTGACT}_T Represent the time required to traverse D_T assuming a TAS of \overline{VACT} .

Since the Distance, D_T , must be flown to arrive at W_T using either velocity, it follows that:

$$\begin{aligned} D_T &= (\overline{VACT} + WATK_1) * \overline{TTGACT}_T \\ &= (\overline{VCOM} + WATK_1) * \overline{TTGCOM}_T \end{aligned}$$

The expected time error, $\overline{TTGACT}_T - \overline{TTGCOM}_T$ is then given by:

$$(\overline{TTGACT}_T - \overline{TTGCOM}_T) = \overline{TTGCOM}_T * \left[\frac{(\overline{VCOM} + WATK_1)}{(\overline{VACT} + WATK_1)} - 1 \right]$$

where a positive error is to be displayed as a LATE indication.

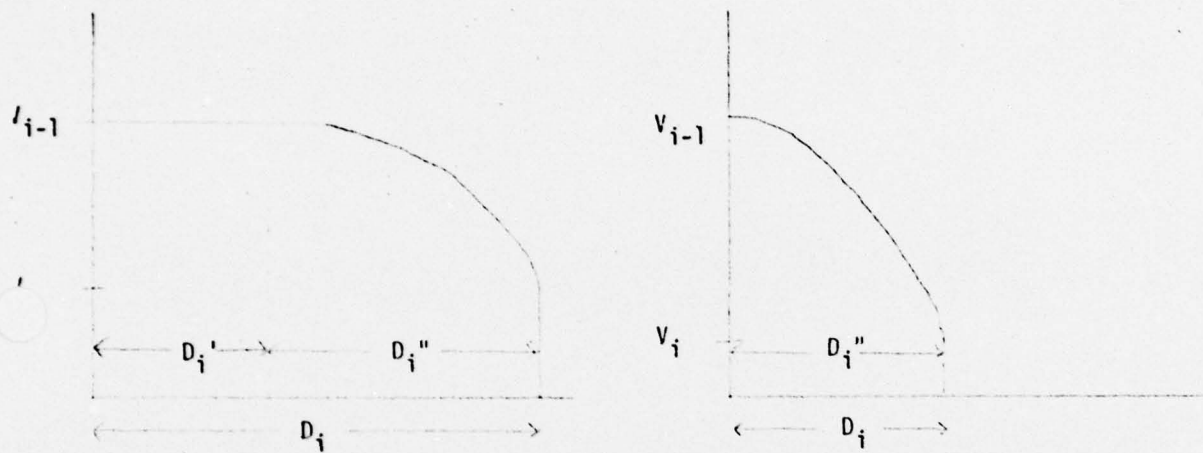


FIGURE 2-10

Speed Profiles

$D_i''=0$ whenever $V_{i-1}=V_i$ and $D_i'=0$ whenever a speed change in excess of 40 KTS/Min is required for the entire leg distance D_i .

2.4.4 Software Implementation of the Algorithm

Algorithm computations are performed by procedure TIMCNTRL. Although control is given to this procedure every cycle by the CDU Main Control Program, computations are only attempted whenever either 1) ten seconds have elapsed since the last algorithm computation, or 2) a Flight Plan revision has occurred since the last execution of the algorithm.

Since TIMCNTRL is a procedure called within the CDU channel, it is possible for sensor data maintained by the Navigation channel to change during any given execution of the algorithm. To ensure that the same set of parameters is used for a given algorithm computation, it is necessary to take a snapshot of the sensor data as part of the initialization logic for the algorithm.

A task description for TIMCNTRL is given below. A program listing of TIMCNTRL is given in Appendix C.

Task Specification For TIMCNTRL

Procedure Type

Procedure TIMCNTRL()

Module

40 Time and Speed Algorithms

Task Summary

The Time and Speed Control Algorithm is based upon speed and time errors with respect to a waypoint (the Time-Fix) for which an arrival time has been assigned. The value calculated for VCOMI, the Commanded Velocity displayed on the Flight Progress Page, represents the present indicated air speed that should be flown to arrive at the Time-Fix on schedule. The computation for TIMERR provides the best estimate of the total time error that is expected for the desired arrival time. Computations for VCOMI are provided whenever the Present Flight Plan, exclusive of the From-event, contains at least one speed waypoint. The computation for TIMERR is made whenever the validity flag WFIXF indicates that a Time-Fix has been defined for the system.

Notation

- W(J)** Used to denote the Jth Lateral Event.
- IASR(J)** Used to denote the value of the IASR component for W(J). Similar notation is used for other components defined by the Flight Plan Editor.

Internal Data Structure

Synonyms

- INITEVNO** Initial Absolute Event Number required for retrieval of event data from the Flight Plan Editor.

Integer Data

- J** Event Number for the Jth Event.
- CNTRL** Control parameter for the main loop.
- VTIMF** Flag used to control computations for the case where a Time-Fix has not been entered but VCOMI is to be calculated for the To-waypoint.

Real Data

- PREVIASR** Temporary storage used to record IASR(J-1).
- PREVDFTO** Temporary storage used to record DFTO(J-1).
- TTGACT** Present estimate of actual time required to reach the Time-Fix.
- TTGCOM** Commanded time to reach the Time-Fix.
- COCHPREV** Temporary storage used to record CRSO(J-1)-CRSI(J-1).
- HZ** Altitude used for IAS to TAS conversion.
- LEGDST** Along-track distance from W(J-1) to W(J).
- WATK** The along-track component of wind applied to W(J).
- WATKTO** The along-track component of wind applied to the leg presently being flown.
- KALT** The altitude proportionality constant used for conversions between IAS and TAS.
- TASPREV** Temporary storage used to record computed TAS for W(J-1).
- TASJ** Temporary storage used to record computed TAS for W(J).
- DV** The speed change between W(J-1) and W(J).
- T1** The time required to fly from W(J-1) to W(J) at a rate of 40 kts/min.

AVEV	The average ground velocity required for a linear speed profile between W(J-1) and W(LAST).
T2	The time required to fly from W(J-1) to W(J) assuming a constant velocity of AVEV.
DPP	The portion of the leg between W(J-1) and W(J) that requires a speed change.
DELT	The expected time required to fly from W(J-1) to W(J).
DP	The portion of the leg between W(J-1) and W(J) that should be flown at the velocity assigned to W(J-1).
GMTCONV	Conversion factor used to convert GMT to navigation time units.
VGNOB	Nominal ground velocity calculated for the present leg.
KSCALE	Scaling factor used to protect against overflow.

Calling Sequence

TIMCNTRL()

Return Values

VCOMI	Commanded IAS for the present leg that is to be displayed on the Flight Progress Page and IAS instrument.
VCOMIF	Validity flag for VCOMI.
TIMERR	Expected time error for arrival at the Time-Fix.
TIMERF	Validity flag for TIMERR.

Task Description

IF 10 seconds have not elapsed since the last execution of the Time Control Algorithm
 AND a Flight Plan revision has not occurred since the last cycle
 THEN RETURN to calling program.

Update own clock reading.

Update own version of Flight Plan Revision number

Assign INVALID status to TIMERF, the validity flag for arrival time error.

Comment: assign an initial validity status to VCOMIF, the validity flag for commanded IAS.

IF VCOMIF=

```

IF invalid GMT THEN IVGMT
ELSE IF invalid aircraft true air speed THEN IVTAS
ELSE IF invalid aircraft altitude THEN IVALT
ELSE NODATA) NEQ NODATA

```

THEN RETURN to calling program.

IF the Lateral From-event is invalid

OR no speed is defined for this event

THEN RETURN to the calling program. Note that VCOMIF will have a value of NODATA and TIMERF will have an INVALID STATUS.

Comment: Keep a snapshot of sensor data, i.e.,

ACTAS = Aircraft True Air Speed

ACALT = Aircraft Altitude

ACIASERR = IAS Instrument Error

ACNWND = North Component of Wind

ACEWND = East Component of Wind

Assign IASR component of the Lateral From-Event to PREVIASR.

Assign DFTO(FROM) to PREVDFTO.

Initialize event number index by assigning INITEVNO to J.

Initialize nominal time-to-go, TTGNOM, to 0.0.

Initialize COCHPREV to value of CRSO(FROM)-CRSO(FROM).

Assign an initial status of VALID to VTIMF to ensure computations are performed for TO-waypoint.

WHILE the Jth event is not the Time-Fix.

AND the (J=J+1)th event is valid.
AND VTIMF EQL VALID.

GIN ... Calculate TTG block.

IF event J is a Vertical event

THEN

BEGIN ...Vertical Event block

IF event J is the Vertical TO-event

THEN assign value of ACALT to HZ.

ELSE assign ALTD(J) to HZ.

END ...Vertical Event block

ELSE

IF event J is a Lateral eventNote that End-Of-Continuity events are bypassed.

THEN

BEGIN ...Lateral Event block

Calculate LEGDST, the distance from W(J-1) to W(J), i.e.,

$$\text{LEGDST} = \text{DFTO}(\text{J}) - \text{PREVDFTO}.$$

Update PREVDFTO to value of DFTO(J).

Calculate WATK, the along-track component of wind, i.e.,

$$\text{WATK} = -(\text{ACNWND} * \cos(\text{CRSI}(\text{J})) + \text{ACEWND} * \sin(\text{CRSI}(\text{J}))).$$

Calculate KALT, the altitude proportionality constant, i.e.,

$$\text{KALT} = \frac{[\text{ACTAS} - \text{VCOMI} - \text{ACIASERR}]}{[\text{HZ} * \text{ACTAS}]}$$

Limit KALT to the interval (.00001, .000015)

Convert IAS for W(J-1) to TAS, i.e.,

$$\text{TASPREV} = \frac{\text{PREVIASR}}{(1.0 - \text{HZ} * \text{KALT})}$$

Convert IAS for W(J) to TAS, i.e.,

$$\text{TASJ} = \frac{\text{IASR}(\text{J})}{(1.0 - \text{HZ} * \text{KALT})}$$

Calculate DV, the speed gradient between W(J-1) and W(J), i.e.,

$$\text{DV} = \text{TASJ} - \text{TASPREV}.$$

Calculate T1, the time required to fly from W(J-1) to W(J) at a rate of 40 kts/min.

$$\text{T1} = |\text{DV} * \text{MINRATE}|.$$

Calculate AVEV, the average ground velocity required for a linear speed profile between W(J-1) and W(J), i.e.,

$$\text{AVEV} = 0.5(\text{TASPREV} + \text{TASJ}) + \text{WATK}$$

Calculate T2, the time required to fly from W(J-1) to W(J) assuming a constant velocity of AVEV, i.e.,

$$\text{T2} = |\text{LEGDST} / \text{AVEV}|$$

IF the velocity change, DV, between W(J-1) and W(J) requires a velocity rate greater than or equal to 40 kts/min (i.e., if $\text{T2} \leq \text{T1}$)

THEN

BEGIN ...Linear Profile Block

Assign T2 to DELT, the time required to fly the leg from W(J-1) to W(J).

Assign LEGDST to DPP, the portion of the leg into W(J) that requires a speed change.

END ...Linear Profile Block

ELSE ...Part of the leg into W(J) should be flown at the velocity for W(J-1), the remaining portion at a velocity rate of 40 kts/min. Calculate time and distance parameters for the portion requiring a speed change.

BEGIN ...40 kts/min Block

Assign T1 to DELT.

Assign T1*AVEV to DPP.

END ...40 kts/min Block

IF W(J) is the Lateral To-Event

THEN

BEGIN ...To-Event Block

Assign IASVALID to VCOMIF to indicate VCOMI computation has been performed.

Assign value of TFIXF to VTIMF.

Save the along-track wind component for the Lateral To-Event, WATK, in WATKTO.

Save value of KALT in KALTTO.

IF the velocity change, DV, between W(J-1) and W(J) requires a velocity rate that exceeds 40 kts/min (i.e., if $T2 < T1$)

OR the distance from the aircraft to the Lateral To-Event is within that portion of the leg that requires a velocity change (i.e., if $MTG < DPP$)

THEN

BEGIN ...To-Event Velocity Change Block

Calculate VGNOM, the present nominal aircraft velocity (GS-referenced at this point) that must be flown to arrive at the Time-Fix on schedule, i.e.,

$$V_0 = TASPREV + WATK$$

$$V_F = TASJ + WATK$$

$$VGNOM = \text{SQRT} [V_0^2 + (V_F^2 - V_0^2) \frac{MTG}{DPP}]$$

Calculate DELT, the time required to fly from aircraft present position to W(J) if the aircraft is on schedule, i.e.,

IF DMTG > DPP
THEN DELT = T2 + (DMTG > DPP)/VGNOM
ELSE

$$\text{DELT} = \frac{2 * \text{MTG}}{(\text{VGNOM} + \text{TASJ} + \text{WATK})}$$

END ...To-Event Velocity Change Block

ELSE ...Velocity change is not required for present portion of leg into the Lateral To-Event.

BEGIN ...To-Event constant velocity block.

Assign velocity for W(J-1) to VGNOM, i.e.,

$$\text{VGNOM} = \text{TASPREV} + \text{WATK}$$

BEGIN ...Excessive Course Change block.

Tag commanded IAS display as invalid by assigning IVCOCH to VCOMIF.

RETURN to calling program. Note that TIMERF is returned with an INVALID status and VCOMIF indicates that "CRS!" will appear for the commanded IAS display on the Progress Page:

END ...Excessive Course Change block.

ELSE

BEGIN ...Leg Capture Compensation block.

Compensate for aircraft turn made for leg capture at W(J-1), i.e.,

$$\text{DELT} = \frac{\text{TASPREV} * [|\text{COCHPREV}| - 2 * \text{TAN}(\frac{|\text{COCHPREV}|}{2})]}{g * \text{TAN}(25^\circ)}$$

where g=Acceleration due to gravity.

Increment TTGNOM by DELT.

END ...Leg Capture Compensation block.

END ...Beyond To-Event block.

Update COCHPREV to value of

$$\text{COCHPREV} = \text{CRSO}(J) - \text{CRSI}(J)$$

D ...Lateral Event block.

.D ...Calcttg Block

Calculate 1) K, the proportion of nominal speed that is required to arrive at
 the Time-Fix on schedule, and
 2) TTGCOM, the commanded Time-To-Go for arrival at the Time-Fix, i.e.,

IF TIMERF = (TCOMF .V. TFIXF) NEQ VALID
 ...Computations for TIMERR, K, and TTGCOM are dependent upon status of pilot
 entries for Time-Fix and Commanded Arrival Time

THEN

 BEGIN ...TTGCOM Invalid Block

 K = KSCALE ...Reversionary Mode. Set K = (1) * (Scale Factor).

 KVAL = VALID ...Indicate K valid for later computation of VCOMI.

 END ...TTGCOM Invalid Block

ELSE

 BEGIN ...TTGCOM Valid Block

 Update Commanded Arrival Time, I.E.,

 TTGCOM = (TCOM-GMTS)/GMTCONV

 Determine validity of computation for K. K is invalid when TTGCOM approaches
 zero, I.E.,

 IF TTGNOM*KSCALE > |TTGCOM|

 THEN Assign an INVALID to KVAL

 ELSE

 BEGIN

 K = (TTGNOM*KSCALE) / TTGCOM

 KVAL = VALID

 END

 END ...TTGCOM Valid Block.

IF VCOMIF EQL IASVALID ...Computations for VCOMI and TIMERR only valid if To-Event
 has a defined IAS.

THEN

 BEGIN ...VCOMIF Valid Block

 IF KVAL EQL VALID ...Test for validity of K before updating VCOMI.

 THEN

 BEGIN ...Update VCOMI Block

Calculate Commanded TAS, I.E.,

$$VCOMT = (K*VGNO*)/KSCALE-WATKTO.$$

Convert VCOMT to IAS for display purposes, I.E.,

$$VCOMI = \frac{1.0-KALTTO*ACALT}{KALTSCALE} *VCOMT$$

Limit VCOMI to upper limit of IAS Instrument.

END ...Update VCOMI Block

Calculate the expected time error for arrival at the Time-Fix, I.E.,

IF TIMERF EQL VALID

THEN

BEGIN ...Update TIMERR

$$EARLY = (TTGNOM*VGNO*)/(ACTAS+WATKTO)-TTGCOM.$$

$$TIMERR = |EARLY|.$$

END ...Update TIMERR

END ...VCOMIF Valid Block

RETURN to Calling Program

2.5 ASC Software Modifications

This section describes the 3D/4D modifications to the ANS-70A version of the Aircraft Systems Coupler (ASC) software. One version of this software has been constructed for use by all three of the Task II systems. In addition to changes implemented for the Base and 2D Plus Time Control Systems, this section will describe ASC software modifications that have been added for the 3D/4D Localizer/Glideslope System.

Table 2-3 lists the sensor data inputs that require additional processing by the ASC Input software. The first three items are required for the Localizer/Glideslope System. Each input has an associated high-level flag which is used to indicate current hardware status for the given sensor input. This status serves as one of the criteria used to determine validity of the sensor input.

Due to radio receiver limitations, localizer frequency is input in the same sensor slot normally used for the secondary VOR frequency. In addition to processing localizer frequency, this requires the ASC software to suppress system usage of the secondary navaid during the localizer mode of navigation. Use of this navaid is inhibited by setting a flag that is normally used to indicate a frequency mismatch.

A software switch whose value is specified for the Link Edit Computer run is used to determine which of two sets of computations are required for processing of IAS Airspeed Error. Computations for the G-I instrument are linear for the range of speeds that have been defined for the instrument. A Least-Squares approximation on the data furnished for the C-880 instrument has resulted in the use of a fourth-degree polynomial to determine IAS error.

The sensor word reserved for the HSI Input for Selected Course is processed every cycle by the ASC Input Program. The 2D Plus Time Control System version of the Flight Plan Monitor is the only program for the three systems that monitors this processed data. The net result is that the ASC software is allowed to process the input for all three Task II systems.

Current status of the "Engaged" discretes is recorded for system usage. The Lateral Navigation program suppresses waypoint passage whenever the Area Navigation System is disengaged from the auto-pilot. The other two discretes are used by the Localizer/Glideslope System.

Table 2-4 provides a summary of sensor data outputs that require additional processing by the ASC Output Program. IAS Command is the only output that is required for all three systems. As with the input for IAS error, conversions for the C-880 instrument are straight-forward. A fourth-degree polynomial is used to convert IAS in knots to degrees for the C-880 instrument.

Remaining outputs are required for the Localizer/Glideslope system. Deviation displays are sent to the HSI and ADI instruments. The ASC Output Program monitors internal flags to determine which navigation modes are controlling the instrument displays.

The Localizer Enable discrete is used to activate tuning the VOR/LOC receiver to localizer frequencies. Once again, internal flags are used to determine the setting of this discrete.

The "Arm" and "Capture/Track" discretes are used to control displays on the Mode Annunciator that has been implemented for Localizer/Glideslope usage. Internal flags are monitored each cycle to determine the settings of these discretes.

One additional feature has been added to the ASC Software that is unique to the 3D/4D systems. The Air Data Computer input for True Air Speed is flagged as invalid whenever TAS falls below 150 knots. 3D/4D usage in terminal area operations will require Time Control and Localizer/Glideslope modes at slow speeds. For this reason, a scheme has been implemented that uses IAS to approximate TAS whenever the latter speed reaches its limit of 150 knots.

INPUT SENSOR DATA

Localizer Frequency + High-Level Flag
Localizer Deviation + High-Level Flag
Glideslope Deviation + High-Level Flag
IAS Airspeed Error + High-Level Flag
HSI Input for Selected Course
Auto-Pilot Engaged Discrete
RNAV-Engaged Discrete
VNAV-Engaged Discrete

TABLE 2-3

Sensor Data Inputs that have been added for the 3D/4D systems

OUTPUT SENSOR DATA

Commanded Localizer Frequency + Localizer Enable discrete

Localizer Deviation

Glideslope Deviation

Localizer Track Angle Error

IAS Command

Localizer Arm Discrete

Localizer Capture/Track Discrete

Glideslope Arm Discrete

Glideslope Capture/Track Discrete

Flight Director Computer Flag

TABLE 2-4

Sensor Data Outputs that have been added for the 3D/4D systems

2.6 Navigation Software Modifications

All of the ANS-70A Navigation software programs were modified for 3D/4D usage. Functional modifications were only implemented for the Lateral Navigation program. Remaining changes were the result of the core reduction effort discussed in Section 2.0. Tasks implemented for the Lateral Navigation software consisted of modifying the ANS-70A criterions for waypoint passage and the Distance-To-Go computation.

The 3D/4D geometry for waypoint passage is illustrated in Figure 2-11. Geometry is shown for the case where the flight plan includes an offset, POFS. Passage of the T0-waypoint occurs whenever both of the following conditions are true:

- 1) The Lateral-Distance-Along-Track (LDAT) to the offset waypoint defined for the T0-waypoint is less than the calculated Leg-Switch-Distance (SWD).

When flying legs without offsets, the offset waypoint is defined to be coincidental with the parent waypoint of the T0-event.

- 2) The bisector defined at this same leg intersection has been crossed.

Referring to figure 2-11, the bisector is given by

$$\text{BISECTOR} = \text{CRSO} - 1/2 (\text{CRSO} - \text{CRSI}) + \pi / 2 \text{SIGN} (\text{CRSO} - \text{CRSI})$$

The bisector is passed once the expressions $(\text{BFLEG} - \text{BISECTOR})$ and $(\text{CRSI} + \pi - \text{BISECTOR})$ have opposite signs.

Geometry for the Distance-To-Go computation is shown in Figure 2-11. The ANS-70A system always uses the parent waypoint for the Lateral To-Event as a reference point for this computation. This is considered to be undesirable

for Time Control procedures when flying offset legs. The 3D/4D system uses the offset waypoint as a reference point for the Distance-To-Go computation.

The ANS-70A system records the coordinates of the parent waypoint in the Flight Plan Table. This was left unchanged for the 3D/4D systems. Coordinates of the offset waypoint are calculated by the Flight Plan Monitor whenever revisions are made to the flight plan.

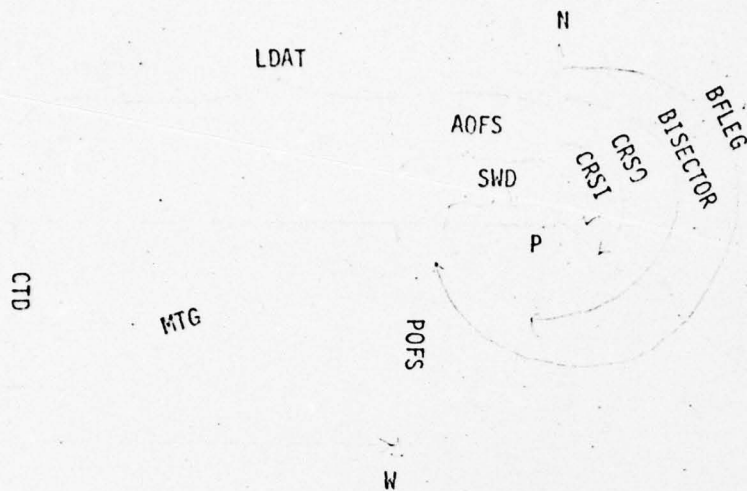


FIGURE 2-11
Geometry for Waypoint Passage

<u>PARAMETER</u>	<u>DESCRIPTION</u>
W	Parent Waypoint of Lateral To-Event
P	Offset Waypoint of Lateral To-Event
SWD	Switching Distance
LDATA	Lateral-Distance-Along-Track to the Offset Waypoint
CTD	Cross-Track Distance
MTG	Miles-To-Go from Aircraft to the Offset Waypoint
POFS	Offset (Base or Parallel) that has been defined for W
AOFS	Along-Path-Offset that must be flown beyond W to reach P
CRSI	Course Into P as determined by Flight Plan
CRSO	Course Out of P as determined by Flight Plan
BIASECTOR	Bisector constructed at P
BFLEG	Course (True) from P to the Aircraft

Section 3
2D PLUS TIME CONTROL SYSTEM

The 2D Plus Time Control System provides the Task II capability of simulating Time Control for non automatic RNAV systems. Major software tasks for this system include the following items:

1) Implementation of CDU software for the revised Progress page. Software implementation for this task is described in Section 3.2.

In addition to the Progress page, CDU software allows pilot access to the Flight Plan and Present Position pages. The Flight Plan page is required for data assemblies. The Present Position page is to be used for pilot updates of aircraft present position.

2) Maintenance of RNAV waypoint parameters in an array structure that is maintained by the CDU software. The Flight Plan Editor is not used for maintenance of the Flight Plan Table. The pilot has the capability of specifying waypoint parameters for ten waypoints at any given time. Ten 3-word arrays are maintained to record entries for waypoint identifier, bearing, and distance. Two additional arrays are maintained as CDU work areas. A description of the array components used to identify the waypoint parameters is given in Section 3.1.

3) Use of HSI analog input for Desired Course. A description of the software implementation for this task is given in Section 3.3.

4) Implementation of a Time Control Algorithm that is unique to the 2D Plus Time Control System. All Time Control computations reference the leg presently being flown. A software description of this algorithm is given in Section 3.4.

An additional task consists of suppressing the ANS-70A computations for leg switching and waypoint passage. This has been achieved by constructing a version of the Lateral Navigation program that is unique to this System. This program was constructed by modifying the Base System version of Lateral Navigation. The only other change to this module consisted of implementing a 20-second Waypoint Alert criterion to replace the 15-second criterion used for the other systems.

.1 External Data Structure

Data parameters unique to the 2D Plus Time Control System have been assigned to a separate module. Data definition for this set of parameters are given below. With the exception of FP.EDIT and NLTOCHG, all parameters are completely maintained by the CDU software.

<u>DATA TYPE</u>	<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
Integer	Display.Wypt	Waypoint Number currently being displayed.
Integer	Use.Wypt	Waypoint Number for waypoint currently being used for navigation.
Integer	FP.Edit	Validity flag that is assigned a VALID status by the CDU software whenever a CDU edit has been made that affects the current navigation leg. FP.EDIT is assigned an INVALID status by the Flight Plan Monitor after the Navigation Event Table (NLTO array) is updated to reflect the edit.
Integer	NLTOCHG	Validity flag that is assigned a VALID status by the Flight Plan Monitor whenever an input (via either the CDU or the HSI Course knob) has been processed that affects the current navigation leg. NLTOCHG is assigned an invalid status by the Speed and Time Control Procedure after the Time and Speed Control computations are updated.

<u>DATA TYPE</u>	<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
Integer	OFFSTF	Validity flag for OFFSET. OFFSTF = valid whenever a lateral offset is commanded, invalid otherwise.
Real	OFFSET	Lateral Offset currently being flown.
Real Array	ARR0, ARR1 ARR9, ARRA, ARRC	Waypoint arrays used to record Ident, Bearing, and Distance information for the IRNAV waypoints.
Pointer Array	PTR.ARRAY	Array of 12 pointers used to reference the waypoint arrays.
Integer Component	WYPT.IDENT	Component used to record ASCII identifier Waypoint Number. Assigned a component position of 0.
Real Component	WYPT.BRG	Component used to record True Bearing from navaid to waypoint. Assigned a component position of 1.
Real Component	WYPT.DIST	Component used to record distance from navaid to waypoint. Assigned a component position of 2.

3.2 Functional Description of Revised Progress Page

Display formats for the Progress page are illustrated in Figures 3-1 and 3-2. A functional description of data fields for the Progress page is given below.

I) [STATION]

This field provides the pilot with a means of specifying the navaid that is to be used for navigation and tuning purposes. Allowable entries consist of three-character station identifiers that are stored in the data base. The scratchpad message "NOT STORED" is annunciated for attempts to enter invalid identifiers.

II) [MODE]

This field provides a CDU display of the current navigation mode. Current usage of VOR, DME, and Air Data/Heading information for navigation purposes is indicated by displaying V, D, and A respectively. The absence of a given mode is indicated by displaying a dash (-) for the corresponding letter. A downgrade of mode will result in the annunciation of the data field. The annunciation may be cancelled via a line-select entry of a single minus sign (-).

III) [OFST]

Parallel offsets are commanded by means of the OFST field. The initial character of an offset entry must be either an "L" or "R." The magnitude portion of the entry is allowed to have a range of 0.0 to 50.0 (NM). Thus, an entry of L5.1 would be used to indicate a left offset of 5.1 NM. An existing offset is cancelled via a L0 (L followed by a zero) or R0 entry.

IV) [WIND]

The data field for Wind serves as a display field only. Bearing information is displayed as magnetic bearing from the station. Dashes are displayed whenever Air Data or Heading Information is invalid.

V) [WPT/BRG/DIST]

The third pair of CDU lines has been reserved for waypoint information. Waypoint parameters consist of Identifier, Bearing (Magnetic) from navaid, and distance from navaid. Allowable entries consist of editing all three fields with one entry or revising any field with a single edit.

A total of 10 waypoints may be designated at any given time. Digits 0 through 9 are used to designate waypoint identifiers. Display of a waypoint other than the USE-waypoint is indicated by blinking the identifier field. A waypoint may be deleted via an entry of a single minus sign for Line-Pair No. 3. Waypoint deletion will result in a display of dashes for the BRG and DIST data fields. Navigation computations reference the navaid presently being used whenever the USE-waypoint is deleted. Deletion of a waypoint will result in the software assignment of 0.0 to the Bearing and Distance fields associated with the given waypoint.

A description of allowable edits for the WPT/BRG/DIST fields is given below:

Entry for Waypoint Identifier:

Acceptable entries consist of a single scratch pad digit (0 through 9)

Entry for Bearing:

Entries must be preceded by a single slash (/).

Range: 0.0 to 360.0 degrees

Increment: 0.1 degrees

Examples: /5.1
 /05.1
 /005.1

Entry for Distance:

Entries must be preceded by two slashes (//).

Range: 0.0 to 200.0 NM

Increment: 0.1 NM

Examples: //2.9
 //02.9
 // 002.9

VI) TTW

The Time-to-Waypoint field serves as a display field only. The value displayed represents the current estimate of time required to reach the waypoint specified by the Use-waypoint, HSI input for desired course, and current parallel offset.

Range: .0 to 99.9 minutes (values exceeding 99.9 minutes will be displayed as 99.9 minutes).

Resolution: 0.1 minutes

VII) DIST

This field is used to display Distance to the present To-waypoint.

Edits are not allowed.

Range: .0 to 999.9 NM

Resolution: 0.1 NM

VIII) GS

This field is used to display the Present estimate for Ground Speed.

Range: 0 to 999 knots

Resolution: 1 knot

IX) [DTA]

Desired Time of Arrival (GMT units) is to be entered for this field. DTA may be revised or deleted at any time. DTA deletion is accomplished by an entry of a single minus sign. Software is required to invalidate an existing DTA entry upon selection of a new USE waypoint, or revision to any of the WYPT, BRG, or DIST fields of the USE-Waypoint.

Range: .0 to 2359.9 where modulo arithmetic of 60.0 minutes is applied to the last three digits.

Resolution: 0.1 minute

X) GMT

A GMT entry must be preceded by a slash mark (/). Rules for range, resolution, and display format are the same as those for the DTA field.

XI) IAS CMD

This field is used to display Commanded IAS as calculated by the Time and Speed Control Algorithm. Line-Select entries are not allowed.

Line Pair 6 is used for the Early/Late Display. Display formats for the label and data fields are identical to those used for the Base System.

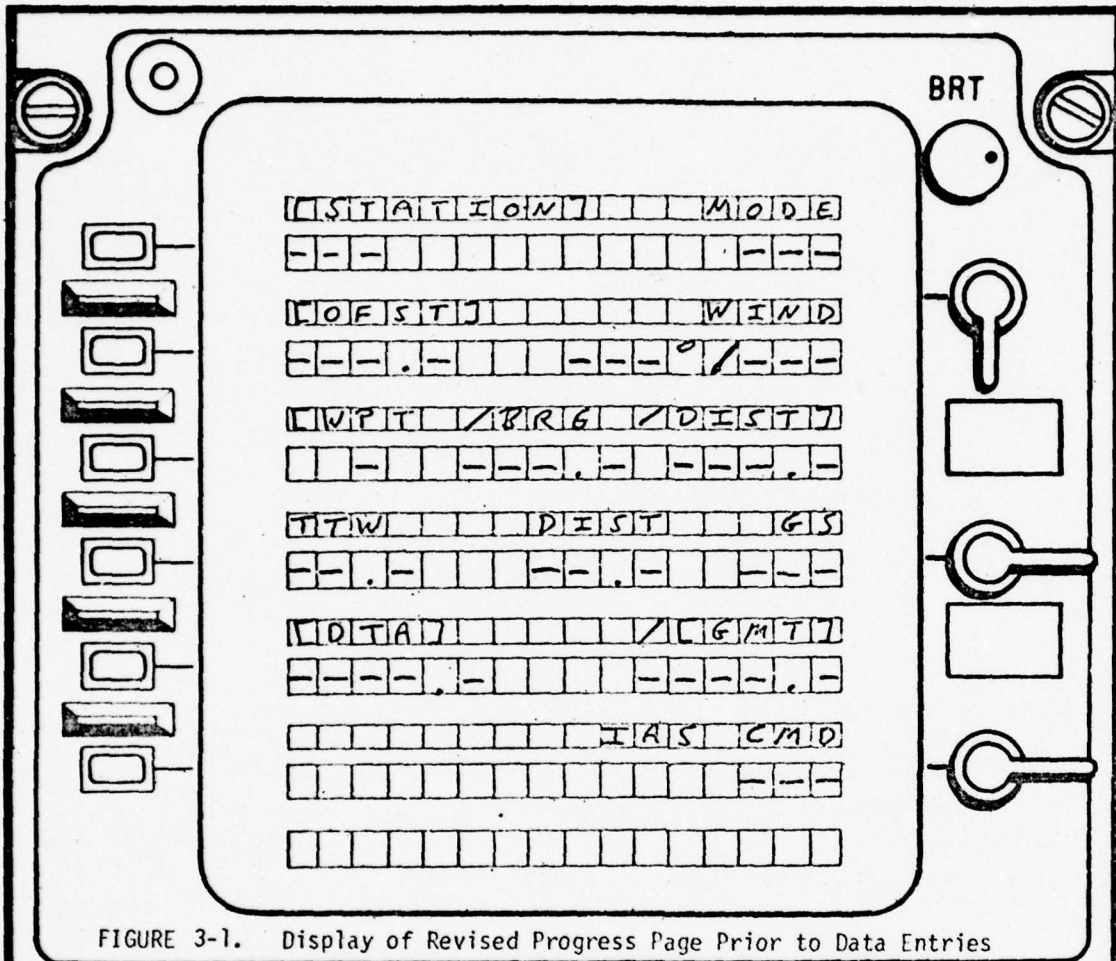
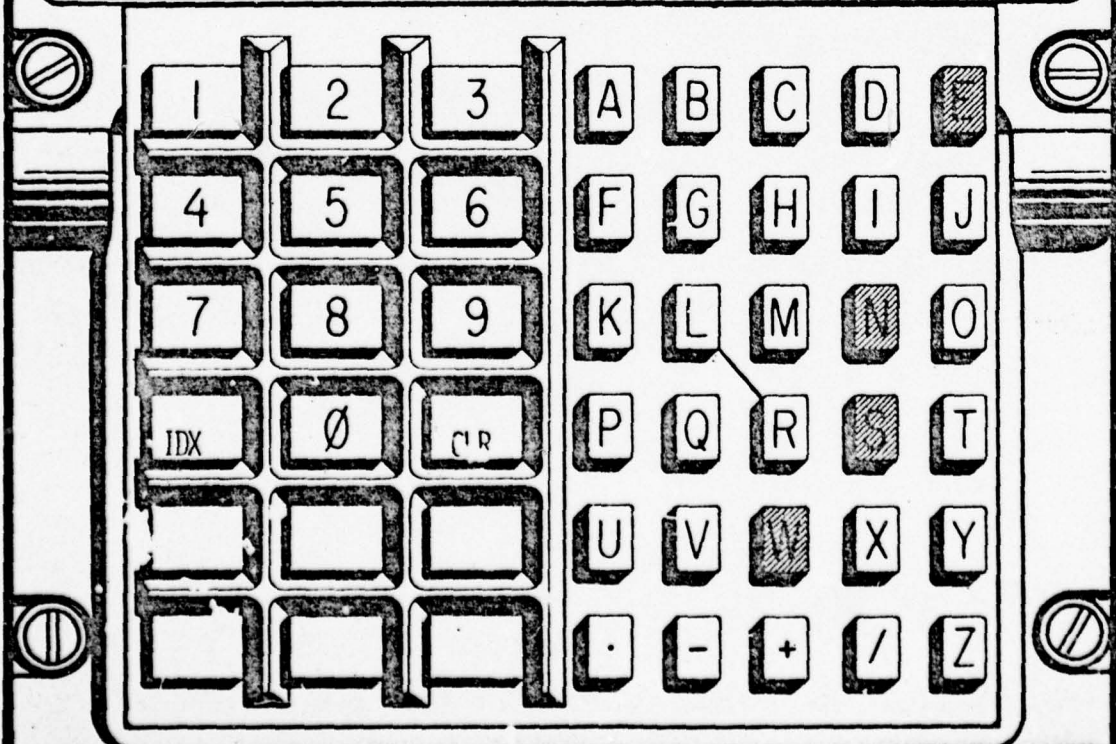


FIGURE 3-1. Display of Revised Progress Page Prior to Data Entries



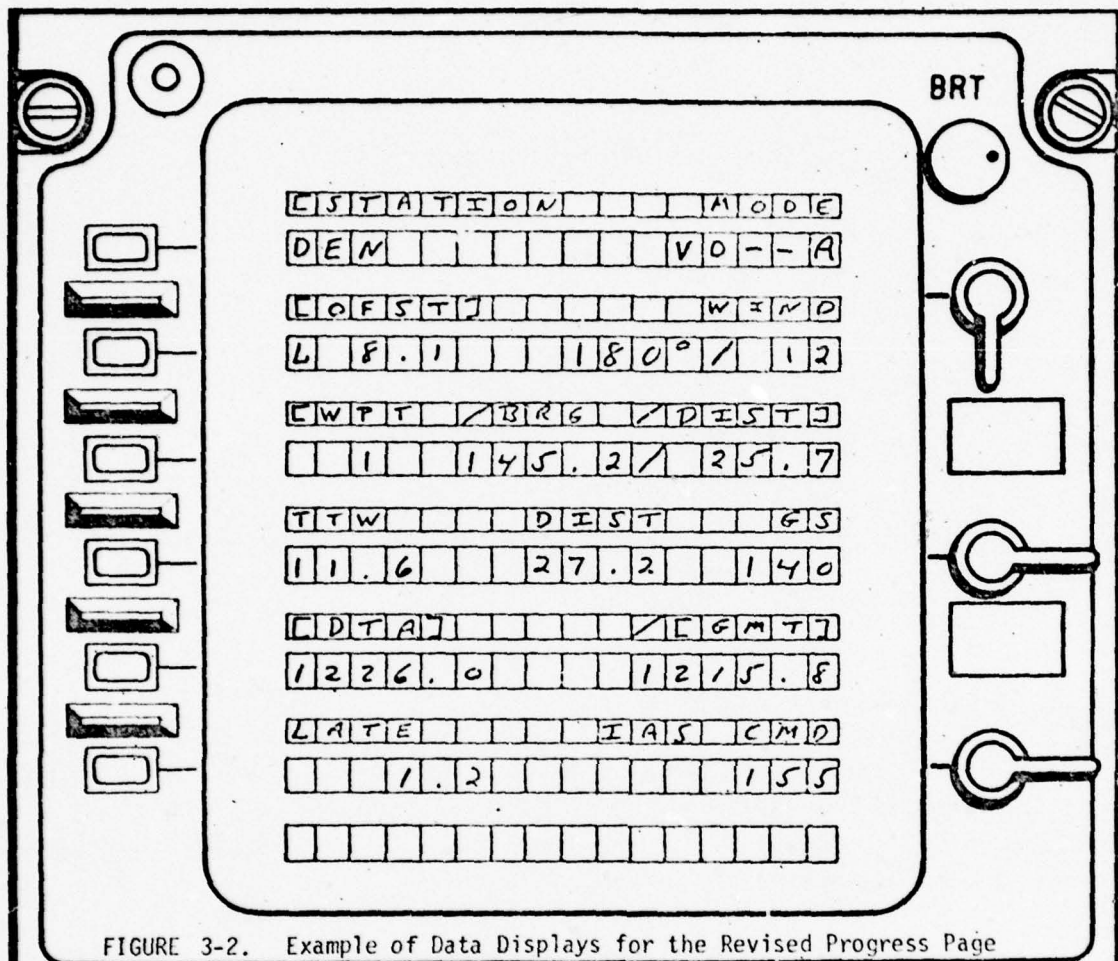
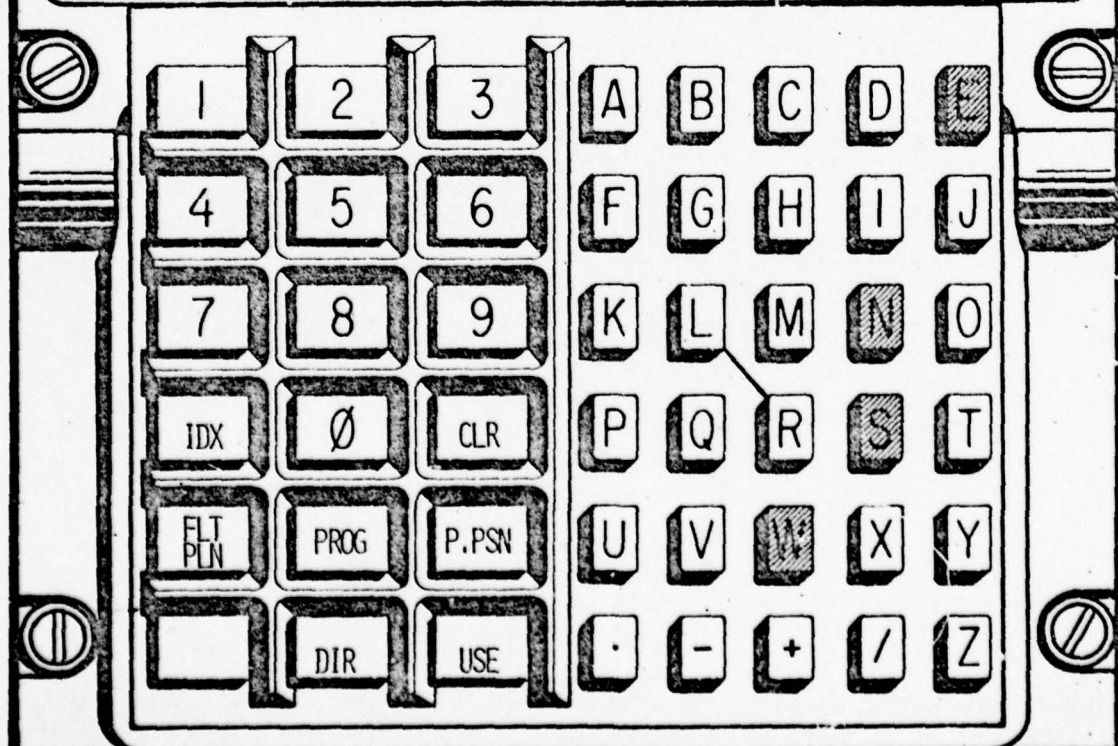


FIGURE 3-2. Example of Data Displays for the Revised Progress Page



3.3 HSI Input for Selected Course

Figure 3-3 illustrates software interfaces for programs that require access to the HSI Input for Selected Course. The final objective is to pass the Selected Course input to the Lateral Navigation program as a course command for the present leg.

Initial processing of the input is performed by the ASC Input Program. Converted data is recorded in the ADHD data structure. The Flight Plan Monitor uses the Course input to determine the coordinates of the TO-waypoint. The Selected Course Input is then passed to the Navigation Channel as the flight plan parameter for Course-Into-the-Waypoint (CRSI Component).

Geometry for computation of the TO-Waypoint is given in Figure 3-4.

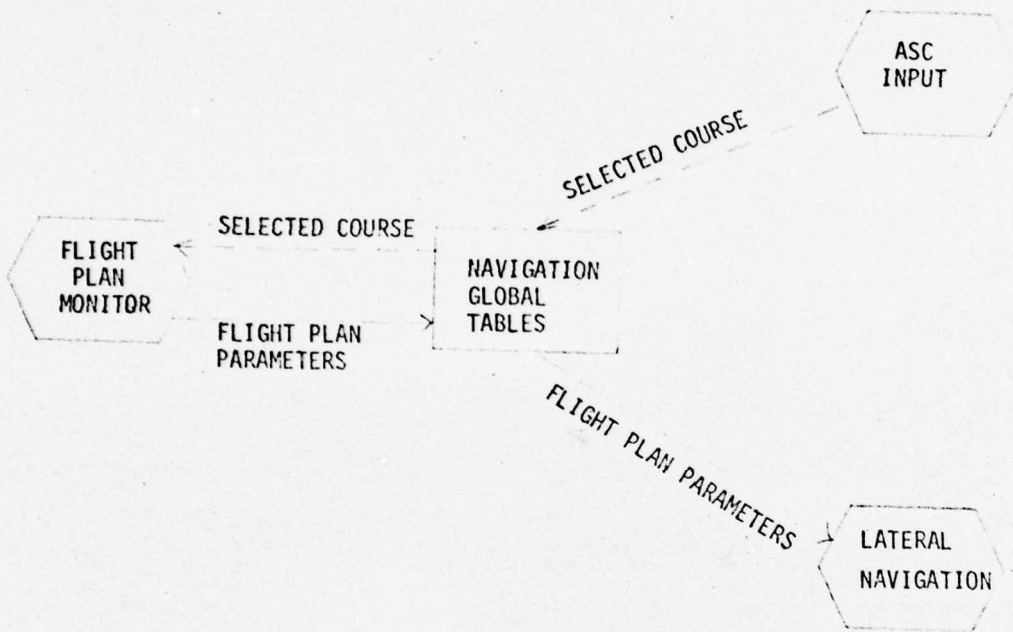


FIGURE 3-3

Software Interfaces used to implement HSI Input for Selected Course

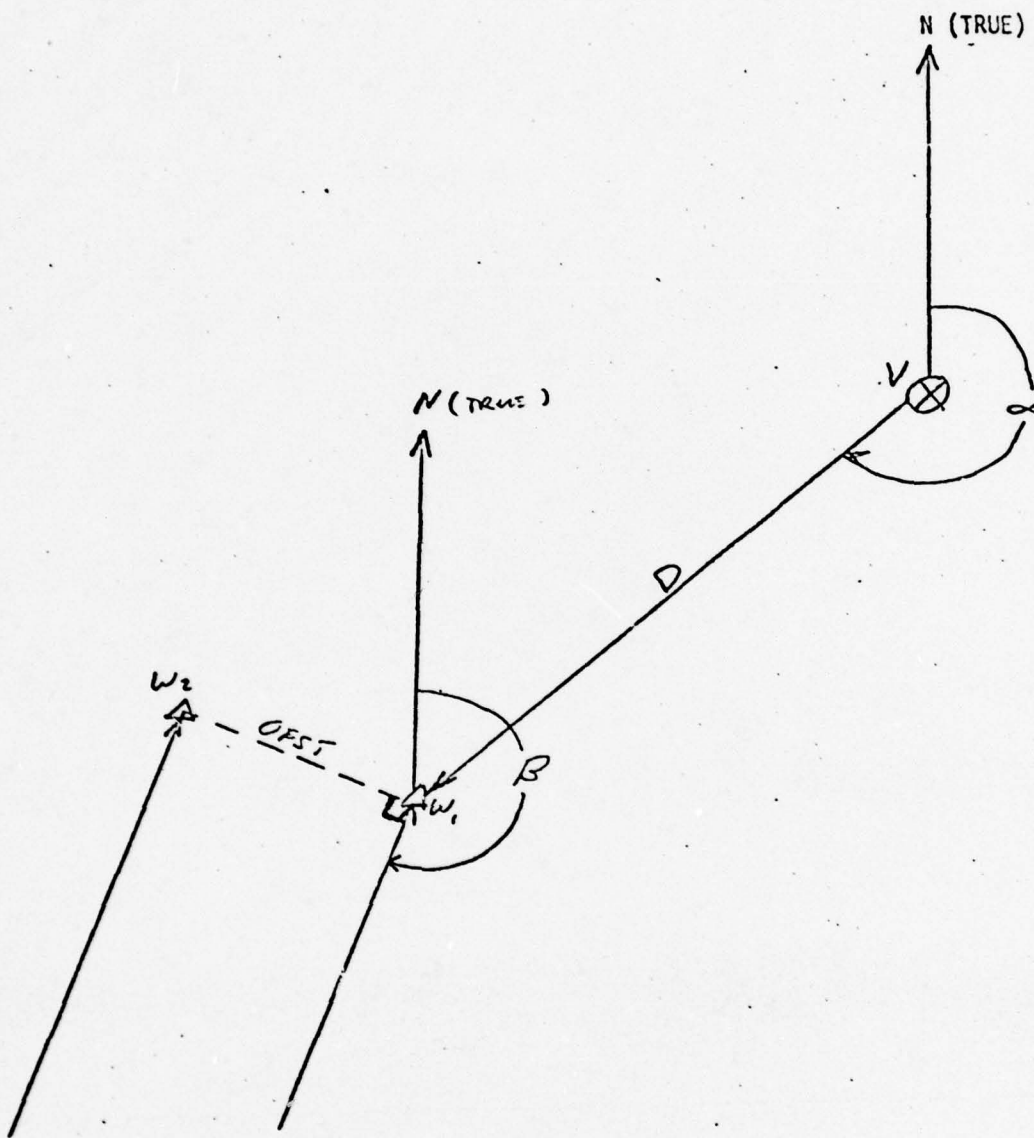


FIGURE 3-4

Geometry for Computation of Waypoint Referenced for Navigation Purposes

- V: Navaid specified on Progress page
- α : Bearing specified as Waypoint Parameter on Progress page
- D: Distance specified as Waypoint Parameter on Progress page
- W_1 : Coordinates of Use Waypoint
- B: HSI Input for Desired Course
- OFST: Parallel Offset as specified on Progress page
- W_2 : Coordinates of Waypoint referenced for Navigation

3.4 Time Control Algorithm

The 2D Plus Time Control System computations for Time Control are only applicable to the leg presently being flown. Maximum use is made of existing data declarations for the Base System. Software interfaces are similar to those defined for the Base System, i.e., control is given to a procedure called TIMCNTRL every cycle by the CDU Main Control Program. Procedure TIMCNTRL will monitor the system clock and status of flight plan revisions to determine the necessity of executing the Time Control Algorithm for the given cycle. A task description for TIMCNTRL is given below.

A program listing of the TIMCNTRL routine is given in Appendix D.

Task Description for the 2D Plus Time Control System

Time Control Algorithm

Task Specification for 2D System TIMCNTRL Procedure

Procedure Type

Procedure TIMCNTRL ()

Module

2D Plus Time Control System Version of Time and Speed Control

Task Summary

Time Control computations for the system are only valid for the present leg. Computations are performed whenever either 1) ten seconds have elapsed since the last execution of the Time Control Algorithm, or 2) a Flight Plan Revision has occurred since the last cycle. The latter condition is determined by monitoring NLTOCHG for a value of VALID.

Computations required for the display of Time Control parameters are recorded in VCOMI, VCOMIF, EARLY, TIMERR, and TIMERF. Declarations for this set of parameters are defined by the Base System insert file DATAZ611.

Internal Data Structure

Synonym Declarations:

CYCLE.TIME Minimum time allowed between Time-Control computations.
CYCLE.TIME is to be assigned a value of 10 seconds, i.e.,
(10 sec) (1000000 us/sec)
CYCLE.TIME = $\frac{(10 \text{ sec}) (1000000 \text{ us/sec})}{(409.6 \text{ us/count})}$

Integer Declarations:

<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
TALCLOCK	Own record of last time that the Time Control Computations were executed.
GMTI	Own copy of GMTS expressed in terms of GMT units (12 hours).

Real Declarations:

<u>SYMBOLIC NAME</u>	<u>DESCRIPTION</u>
ACTAS	Own snapshot of Aircraft True Air Speed.
ACALT	Own snapshot of Aircraft Baro Altitude.
ACIASERR	Own snapshot of IAS error as recorded by the IAS Instrument.
ACNWND	Own snapshot of the North Component for Wind.
ACEWND	Own snapshot of the East Component for Wind.
DESIRED.CRS	Own snapshot of the HSI course input.
WATK	Along-track component of wind for the vector whose origin and direction are given as present aircraft coordinates and DESIRED.CRS, respectively.
KALT	Altitude Proportionality factor required for the conversion from TAS to IAS.
KALTSKALE	Scale Factor required to prevent overflow for the TAS to IAS computation.
GMTR	Own copy of GMTS expressed in terms of Navigation Time Units.
GMTCONV	Conversion factor used to convert GMT to Navigation Time Units. GMTCONV = 10.8039624/12.
TTGCOM	Commanded Time-to-Go to arrive at the To-Waypoint.

Data Declarations External to Procedure TIMCNTRL;

Synonym Declarations assigned to VCOMIF:

<u>SYMBOLIC NAME</u>	<u>ASSIGNED VALUE</u>	<u>INSERT FILE</u>	<u>DESCRIPTION</u>
IASVALID	15	DATAZ611	A valid commanded IAS has been calculated by TIMCNTRL.
IVGMT	14	DATAZ611	Either 1) GMT has not been entered via the CDU, or 2) a power interrupt of duration exceeding two seconds has invalidated GMT.
IVTAS	13	DATAZ611	The Air Data Sensor input for TAS is invalid.
IVALT	11	DATAZ611	The Altimeter sensor input for Baro Altitude is invalid.

Integer Declarations:

<u>SYMBOLIC NAME</u>	<u>INSERT FILE</u>	<u>DESCRIPTION</u>
TCOM	DATAZ611	Commanded Arrival Time for the To-Waypoint.
TCOMF	DATAZ611	Validity flag (full word) for TCOM.
VCOMIF	DATAZ611	Validity flag (full word) for VCOMI.
TIMERF	DATAZ611	Validity flag (full word) for TIMEFRA and EARLY.
GMTS		Present value of GMT in seconds.
DMTGF	NTABN611	Validity flag (Byte) for DMTG.
DTTGF	NTABN611	Validity flag (Byte) for DTTG.
TASF	NTABN611	Validity flag (Byte) for TAS. TASF is declared as a component for pointer ADHD.
BALF	NTABN611	Validity flag (Byte) for Baro Altitude. BALF is declared as a component for pointer ADHD.

Real Declarations:

<u>SYMBOLIC NAME</u>	<u>INSERT FILE</u>	<u>DESCRIPTION</u>
VCOMI	DATAZ6I1	Commanded IAS displayed on the CDU and IAS instrument. VCOMI is a fraction of 1000 kts.
VCOMT	DATAZ6I1	Commanded TAS calculated by TIMCNTRL.
EARLY	DATAZ6I1	Early/Late indicator calculated by TIMCNTRL and used to control the EARLY and Late displays on the CDU. A positive value is used to indicate a late status.
TIMERR	DATAZ6I1	Expected arrival time error for the To-Waypoint. TIMERR is expressed in lateral navigation time units.
MINR	DATAZ6I1	Minimum magnitude that REAL numbers may be assigned on the U-1108.
MAX64		Maximum magnitude that Real numbers may be assigned on the U-1108.
DMTG	NTABN6I1	Distance between the aircraft and the To-Waypoint.
DTTG	NTABN6I1	Estimated time required to arrive at the To-waypoint.
TAS	NTABN6I1	Sensor input for True Air Speed. TAS is declared as a component for the ADHD structure.
BALT	NTABN6I1	Sensor input for Baro Altitude. BALT is declared as a component for the ADHD structure.
DELV	NTABN6I1	IAS Instrument Error. DELV is declared as a component for the ADHD structure.
HSICRS	NTABN6I1	Desired course as input via the HSI. HSICRS is declared as a component for the ADHD structure.
NWND	NTABN6I1	North Component of Wind.
EWND	NTABN6I1	East Component of Wind.

Task Description

IF Ten seconds have elapsed since the last execution of the Time Control Algorithm

OR A flight plan revision has occurred since the last cycle (i.e., NLTOCHG EQL VALID)

THEN BEGIN ... Computations Required

Update own clock reading.

Assign an INVALID status to TIMERF, the validity flag for arrival time error.

Record the status of VCOMI i.e.,

VCOMIF = IF invalid GMT THEN IVGMT
ELSE IF invalid aircraft true air speed THEN IVTAS
ELSE IF invalid aircraft altitude THEN IVALT
ELSE IASVALID

IF VCOMIF has a status of IASVALID

THEN BEGIN ... VCOMI VALID

After yielding channel time, record a snapshot of sensor data needed for own computations, i.e.,

ACTAS = Aircraft True Air Speed,
ACALT = Aircraft Baro Altitude,
ACIASERR = IAS Instrument Error,
ACNWND = North Component of Wind,
ACEWND = East Component of Wind,
DESIRED.CRS = HSI Course Input.

Calculate the along-track component of wind for the course presently input via the HSI, i.e.,

WATK = $-[ACNWND * \text{NCOS}(\text{DESIRED.CRS}) + ACEWND * \text{NSIN}(\text{DESIRED.CRS})]$.

Calculate KALT, the Altitude Proportionality constant, i.e.,

KALT = $\text{RLMTF}[\text{ACTAS} - \text{VCOMI} - \text{ACIASERR}] * \text{KALTSCALE}, \text{ACALT} * \text{ACTAS} - \text{MINR}]$
...Limit function used to protect against overflow in KALT computation.

KALT = $\text{KALT} / (\text{ACALT} * \text{ACTAS})$.

Limit KALT to the interval (.10, .15), i.e.,

KALT = $\text{RMAXF}[\text{RMINF}(\text{KALT}, .15), .1]$.

IF a commanded arrival time has been entered via the CDU,

THEN BEGIN ... Valid Arrival Time

Calculate VCOMT, the commanded True Air Speed, i.e.,

$$VCOMT = RLMTF(DMTG, DTTG - MINR) / DTTG - WATK.$$

Convert Commanded TAS to Commanded IAS, i.e.,

$$VCOMI = [MAX64 - (KALT * ACALT) / KALTSCALE] * VCOMT.$$

Limit VCOMI to upper limit of IAS instrument (300 kts for G-I,
410 kts for C-880).

Determine commanded Time-To-Go, i.e.,

GMTI = TCOM - GMTS ... Integer arithmetic required as GMTS is
declared an Integer.

TTGCOM = GMTR / GMTCONV ... Convert to Lateral Nav Time Units.

EARLY = TTGCOM - DTTG. ... Sign of EARLY provides EARLY/LATE
indication for CDU Display.

TIMERR = ABS (EARLY) ... Record magnitude of arrival time
error for CDU display.

END ... Valid Arrival Time.

END ... VCOMI VALID.

Assign an INVALID status to NLTOCHG to indicate computations are not required
next cycle.

END ... Computations Required.

Section 4
RNAV/ILS INTERFACE DESIGN

4.1 Introduction

The ILS program is managed by a main or executive routine. This routine is an interface between the ILS program and the navigation program. This section describes operations which transition the boundary between the ILS executive program and the 3D/4D main program. A description of the executive program is contained in Appendix E.

4.2 Operation

4.2.1 Mode Selection

The overall view of the ILS mode is achieved by selecting the ILS page. This is done by pushing the ILS line select key with the INDEX page on the CDU. After pushing this key, the ILS page will appear on the CDU. Refer to Figure 1 for a diagram of the ILS CDU page. If the localizer programs are not in core, the ILS page will indicate dashed lines under the STATUS label. At any time the parameters ILS FREQ, TD WPT (touchdown waypoint), RWY CRS (runway course), LENGTH (runway length) can be entered for data storage to be used for the ILS computations. Allowable ranges for these parameters are as follows:

- | | | |
|-----------------------|---|---|
| a. Runway courses | 0-360 degrees | error message on scratchpad if not within these bounds -- will not accept further commands until error message removed. |
| b. Runway length | 5-16 thousand feet | error message if not within these bounds -- defaults to 9,000 feet |
| c. ILS frequency | a valid ILS frequency | error message if non-ILS frequency -- cannot accept further commands |
| d. Touchdown waypoint | A waypoint already entered in the flight plan | error message if cannot be found -- cannot accept other commands until message has been cleared. |

The ILS program tape will be loaded when the ILS page is "up" and when mode is selected for the first time. The three modes available are LOC, APPR AUTO, and RNAV. LOC is an ILS mode using only localizer guidance. APPR AUTO is an ILS mode using localizer and glideslope guidance. The operation of the ILS modes will be discussed in a later paragraph.

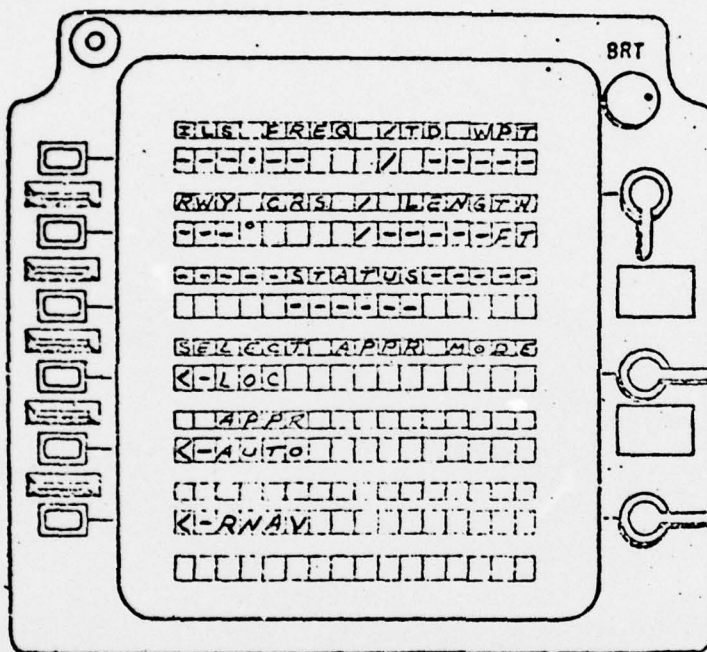


Figure 4-1. ILS Data Page Prior to Data Entry

When the program is loaded, a message will indicate that a "DATA SEARCH" is in effect. The ILS computations will not be accessed until the program is completely loaded. The mode selected will be checked for validities and if the mode is not generated, an INVALID message will be displayed near the mode selector (on the same line). If at any time the mode becomes valid, INVALID will be extinguished. If the mode is again selected, LOC or APPR AUTO will be displayed under STATUS and it will become engaged. If during the engagement of LOC a capture has not been effected and APPR AUTO is selected, and if the validities are checked and approved for APPR AUTO, then APPR AUTO will replace LOC under STATUS. If the validities do not check, INVALID will be displayed by APPR AUTO mode. Once the INVALID extinguishes, if it does, the mode must be reselected before it will take. Before any attempt to use either mode, the INVALID will not appear. In other words, the INVALID can occur only after a request has been checked and refused. Notice that the refusal of APPR AUTO does not discontinue the present use of LOC. The program tape will be loaded if R-NAV is selected. The program tape will also be loaded with the selection of the LOC or APPR AUTO modes. When R-NAV is used to load the program tape, R-NAV remains as the STATUS or selected mode.

To discontinue the use of ILS modes, R-NAV is selected. If AP is disengaged, R-NAV will appear under STATUS and R-NAV will be engaged and a message will appear in the scratchpad: PUSH TO RELOAD R-NAV DATA. Upon the second selection of R-NAV, the R-NAV data base will be overlaid, removing the ILS program. DATA SEARCH will be displayed on the scratchpad while the transition is occurring. ILS will not be used or serviced in any manner during the transition. If localizer is in progress and the autopilot is engaged, R-NAV will not become engaged with the selections of R-NAV. A message will appear on the scratchpad indicating that "DISENGAGE A/P BEFORE SELECTING R-NAV." The re-loading of the R-NAV data will also be prevented until A/P disengage.

4.2.2

Annunciators

An ILS ANNUNCIATOR panel will be mounted on the glareshield. The annunciator panel will display messages as shown in Figure 2. LAT NAV will be annunciated when the autopilot is engaged (APENG) or the flight director is engaged (FDENG), the R-NAV system is engaged and the system is not ignoring conventional R-NAV steering outputs (i.e., not during localizer capture/tracking). LOC ARM is annunciated during localizer arm. LOC is annunciated during localizer capture.

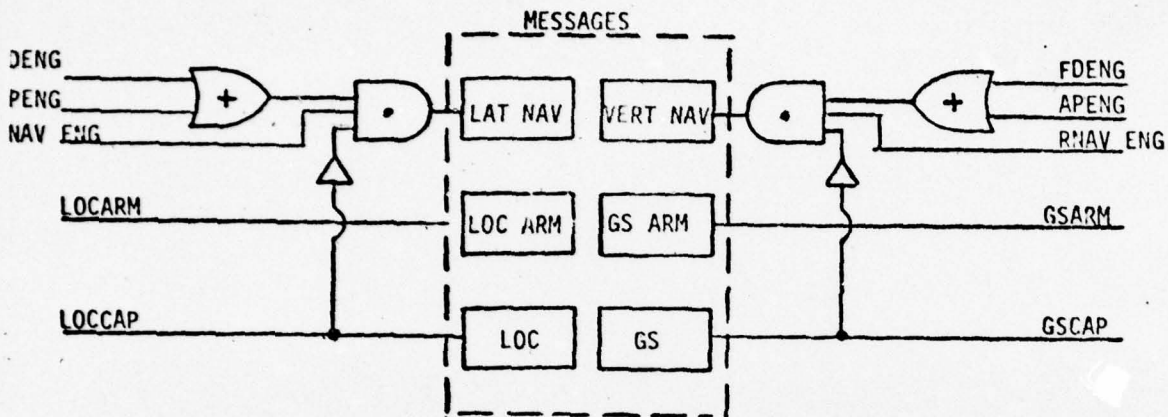


Figure 4-2. RNAV/ILS Annunciator Panel Messages

Similar logic holds for V-NAV. VNAV is annunciated when the auto-pilot is engaged, (APENG) or the flight director is engaged (FDENG), the VNAV system is engaged and the system is not in glideslope capture/tracking. G/S ARM is annunciated during glideslope arm. G/S is annunciated during glideslope capture.

4.2.3 Mode Description

LOC (LOCALIZER) MODE

Selection of the LOC mode will automatically inhibit the glideslope computations. Only a localizer capture and/or track will then result. If the capture conditions or logics have not been satisfied and the processor is in a valid R-NAV submode it will continue to fly the submode until the capture conditions are satisfied. If capture conditions are satisfied and exceeded (track conditions exist) the computations will automatically compute track computations. At the time of LOC mode selection, all validities or parameters monitored must be valid to engage the mode. Once engaged, loss of any validity will cause the computer flag output to drive the computer flag in the ADI.

Signals monitored: LOC SUPER FLAG, LOC FREQ, COMPASS.

Annunciator sequencing: LAT NAV, LAT NAV and LOC ARM, LOC

APPR AUTO (APPROACH AUTOMATIC) MODE

APPR AUTO mode is much like LOC mode except automatic glideslope captures can be effected. The computer will sense and switch both localizer and glideslope computations according to the level of the logics. That is, if localizer and glideslope capture conditions are not satisfied, the submodes will continue to be used. Upon proper detection of the necessary conditions to effect captures, the captures will occur automatically. If the capture conditions have been satisfied by either or both channels, either or both will start computing the track computations. Glideslope capture is inhibited from occurring before LOC capture.

Signals monitored: ALL OF THOSE IN 4.2.3 and G/S SUPER FLAG, ALTITUDE.

Annunciator sequencing: LAT NAV AND VERT NAV, LAT NAV AND VERT NAV and G/S ARM and LOC ARM, LOC and G/S.

4.2.4 Display Control

The ILS maneuver will be performed using an ADI and HSI much as is done with existing conventional systems. Steering commands for the flight director will be supplied to the flight director computer for display on the ADI. Deviation indicators will be driven by the 3D/4D ILS computations during the ILS approach.

The HSI will be controlled whenever a valid LOC ARM is annunciated or latched. Control over the course pointer, deviation indicators and distance readout will be effected by the 3D/4D main program at that time.

4.3 ILS EXECUTIVE PROGRAM OPERATION

The ILS executive program interfaces the ILS approach computations with the overall 3D/4D main computational program. The executive program converts data passed to it from the main 3D/4D program for use in the glideslope and localizer computational routines. In the ILS executive program decisions are also made on validities and mode selection logic. Basically the ILS executive program provides overall administration to the computational routines. The operation as described in the previous sections of this paper are partly accomplished by the ILS executive program. The other part is accomplished by the 3D/4D main program. Figure 4-3 is the flow diagram for the ILS executive program. AED coding of ILS executive program is included in Appendix E. From Figure 4-3, when the ILS page has been selected and the ILS program has been loaded from tape, the ILS executive program is serviced by transferring data to the ILS executive program. This is followed by a preset (initial conditions operation).

From data passed from the 3D/4D program and ILS page, the distance to touch-

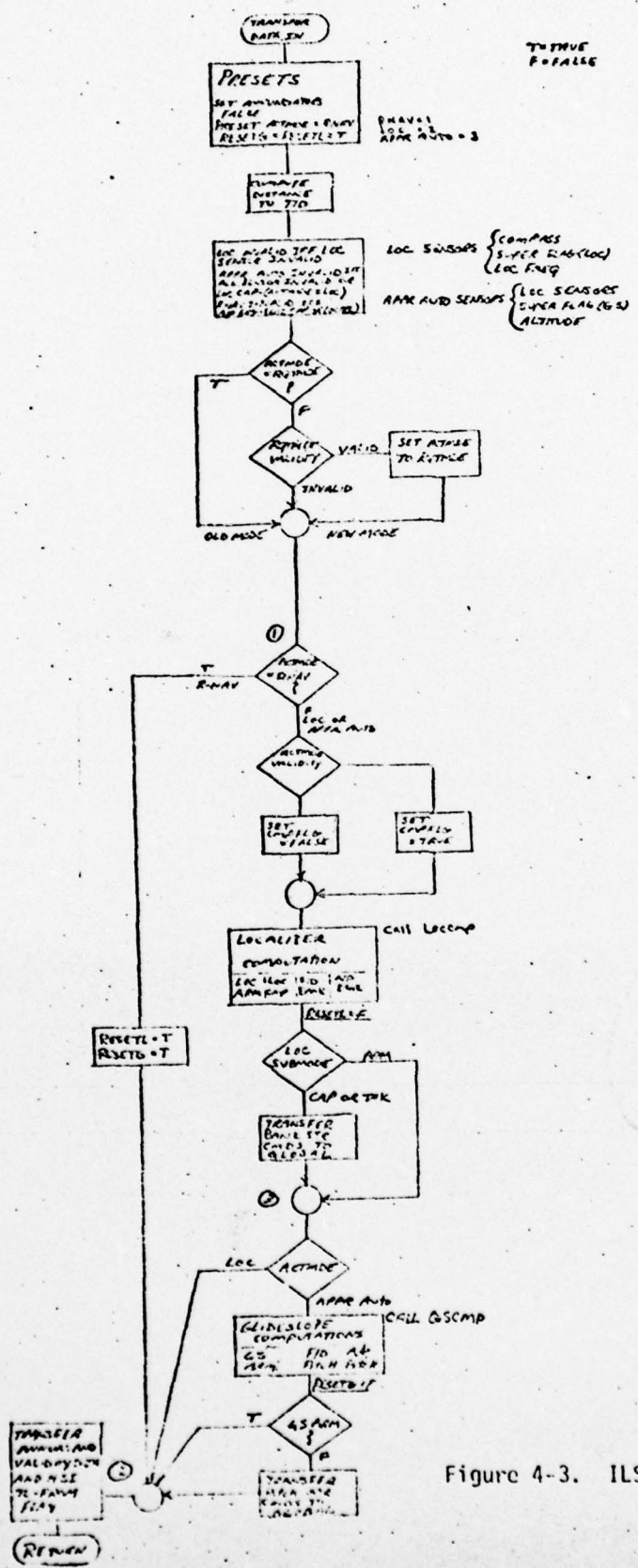


Figure 4-3. ILS Executive Program Flow

down is now computed. Next in sequence, the mode validities are update to establish the validity of each mode serviced by the ILS executive program.

At this point, the present requested mode is compared to the mode now considered active by the ILS executive program. If the requested and active mode are the same, program flow is routed to point 1.

If the requested mode is not the same as the active mode, the validity of the requested mode is checked. If the requested mode validity is true (mode valid) then the active mode is set to the requested mode. If the requested mode is false (mode checked invalid), the previous active mode is retained (requested mode denied).

Program flow now proceeds to point 1. If the active mode is R-NAV, program flow is routed directly to point 2. R-NAV pitch and roll steering data is transferred back to the 3D/4D main program unaltered. Notice also before control is transferred back to the 3D/4D main program, annunciator and mode validity updates are transferred back to the 3D/4D main program. This is true every computational cycle.

The parameter RESETL and RESETG was set true when program flow was routed control from point 1 directly to point 2. These parameters are always maintained true until after the first time either the localizer computation or glideslope computation is executed. The resets will be further treated below.

At point 1, should the active mode be either localizer (LOC) or approach auto (APPR AUTO), then the next action is to check the validity of the active mode. The computer flag is next set depending upon whether the active mode validity is true or false. If the validity is true (mode determined valid), the computer flag is set true (not displayed). If the validity is false, the computer flag is set false (the computer flag on the ADI is displayed).

At this point the localizer computations (localizer control laws for determining roll steering commands) are serviced. When control returns to the ILS executive routine RESETL is set false. RESETL has been used to establish that the localizer computations have been serviced for the first time. This is used as a key for setting initial conditions. Notice that RESETL will now be false unless R-NAV mode is re-established.

From information passed to the executive program from the localizer computation, the ILS main program passes bank steering commands to the 3D/4D main program if the localizer mode has been determined to be in a capture or track submode. If in the arm submode, bank steering commands are not passed to the 3D/4D main program. Control is essentially achieved therefore by the ILS main program overwriting the R-NAV steering commands. Notice that no overwriting will occur if the arm submode is the present status. R-NAV continues to be flown during the arm submode.

After passing through the localizer routines, a decision is made based upon whether the active mode is localizer or approach auto. If localizer mode is the active mode program flow proceeds directly to point 2. Otherwise the glideslope computations are serviced. The operation of the ILS executive program in regard to the glideslope computations is almost identical to that described above for the localizer computation. RESETG is used in an identical manner to the use described for RESETL above.

Once point 2 has been reached independent of the route, annunciator and validity data is transferred to the 3D/4D main program. The HSI to-from flag information is also passed at this point. The ILS executive program is now exited and program flow moves to the 3D/4D main program.

The flow graph of Figure 4-3 describes one computational cycle of the ILS executive program. The ILS computation is processed five times a second and its throughput time is in the order of milliseconds.

Section 5
LATERAL ILS CONTROL LAW
DESCRIPTION AND ANALYSIS

5.1 Introduction

There has been interest for some time in using area navigation system derived data to aid in localizer captures. Reference 1 describes one preliminary Collins' study that investigated this technique. Localizer capture algorithms in general suffer from two important disadvantages. Range information is not generally available, hence the capture law is usually optimized for a given range and performance degradation occurs on either side of the optimum range. Reference 2 describes an attempt to overcome some of this deficiency by estimating range from beam and air data. This approach showed promise but if an area navigation system were available, range information would be inherently present. The second difficulty in localizer captures is that the localizer beam provides angular deviation from a reference centerline. Hence as one moves closer to the localizer antenna, the "beamwidth" of the localizer beam in distance units (e.g. ft.) grows smaller. Thus the available space to execute a turn onto final course once the beam is intercepted shrinks rapidly. As an example, the turn radius associated with 30° of bank at an airspeed of 200 ft/sec implies that for a 90 degree beam intercept, centerline overshoot will occur at ranges shorter than 7.5 nm assuming capture starts (with instantaneous 30° of bank) at 200° A deviation. At higher airspeeds, the minimum range without overshoot will increase. An area navigation system offers potential alleviation of this situation by permitting the initiation of captures prior to beam intercept, thus avoiding the geometry limits described above. The R-NAV aided approach also has problems, however. The inherent errors in the R-NAV estimates of position and velocity are such that if care is not exercised, a capture initiated on R-NAV data may turn short missing the beam entirely or such a capture may turn late resulting in gross overshoots. Reference 1 described two approaches to overcoming these problems. The first approach involved never turning to a lesser course cut than 45° before intercepting the beam. This worked well in terms of localizer overshoot but resulted in two distinct "up-down" bank commands or a "double bank" characteristic which was considered by some to be objectionable. The second approach studied in Reference 1 was to always initiate the R-NAV aided capture with 30° of bank command, but to start fading the bank command almost immediately so that hopefully a smooth blend with beam based bank commands at localizer intercept resulted. This approach had a more desirable bank characteristic but appeared to pose formidable difficulties in properly programming the bank command fade in general. The approach to be discussed in this section avoids the double bank characteristic, uses an adaptable initial bank command (i.e. not always 30 degrees), and provides a solution to the bank command fade problem in the case where the system is tending to turn short of the beam.

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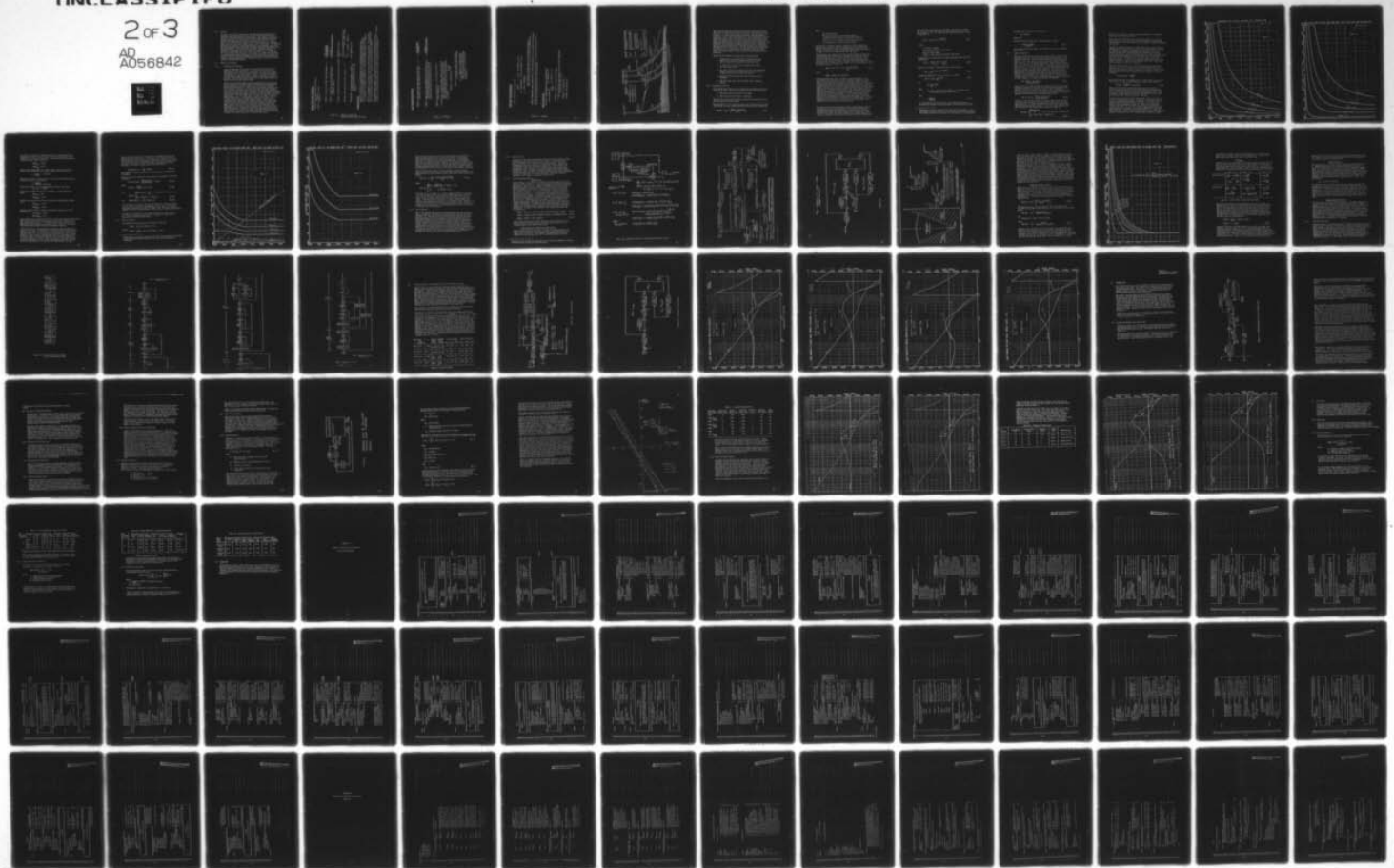
ROCKWELL INTERNATIONAL CEDAR RAPIDS IA COLLINS AVION--ETC F/G 1/5
3D/4D AREA NAVIGATION SYSTEM DESIGN, DEVELOPMENT AND IMPLEMENTA--ETC(U)
JUN 77 J M BRUCKNER, F B BENSON DOT-FA72WA-3123

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5.2 Summary

An R-NAV aided capture algorithm has been developed which provides good localizer capture performance in the presence of nominal R-NAV errors. The system uses R-NAV aiding only when needed. When geometry constraints permit, the system uses primarily beam data and bank information relying on the R-NAV system only for range as a primary piece of data. Track angle error from the R-NAV system is used in this mode but in a way that makes the system relatively insensitive to errors in this data. The technique developed here assumes an integrated R-NAV/ILS flight computer, but could be readily adapted to separate R-NAV and flight computers with minimal interface requirements. This report does not detail simulation results, but design goals of maximum localizer overshoot less than 30 μ A and bank activity in established track less than 1° rms with 2.5 μ A, 1 σ beam noise ($\tau = 4$ sec.) and R-NAV errors of ± 2 nm in CTD, $\pm 2^\circ$ in TAE, and ± 40 ft/sec in ground speed have been demonstrated in hybrid simulation at ranges from 5 nm to 25 nm from localizer antenna and course cuts from 0 to 90 degrees. Simulation results are detailed in Reference 4. Table 5-1 provides a concise summary of the developed system.

5.3 Details of the Study

5.3.1 Framing of the Strategy

Figure 5-1 illustrates three potential situations that may occur when performing an R-NAV aided capture. For convenience they will be referred to as the "turn short", "good data", and "turn long" cases. For captures with trip point within the beam, as shown in the fourth case of Figure 5-1, no R-NAV aiding is needed. Also shown in Figure 5-1 are the required bank traces for each case if a successful capture is to occur. The following argument serves to validate the selection of these three R-NAV aided cases as basic.

If one is to start the capture based on R-NAV data, he has no choice but to establish a trip point algorithm based on area navigation data and consequently must design a system to be tolerant of trip point shifts due to R-NAV errors. Since capture trip points in general must be a function of velocity, this means not only cross track distance errors but also velocity errors will affect the trip point computation. Assuming a constant bank capture algorithm, the three possible situations that may exist once the capture has begun are shown in Figure 5-1 as discussed above. The "turn long" case is critical in terms of amount of bank command to use. If the system is turning long then a "reserve" of bank command must be available (once beam data is present) to increase the bank command to the required amount. Hence, since the "turn long" case may be present, the nominal bank in an R-NAV aided capture should not be the bank command limit (normally about 30°). Note, however, that this is not an absolute constraint but rather a consequence of the strategy being considered here. One could always force the system to "turn short" (see below) and thus avoid the "turn long" case entirely, but the strategy adopted here seems more natural to the author. In summary, the approach adopted is to leave some room for bank to increase in case the "turn long" case occurs.

CAPTURE TRIP POINT COMPUTATIONS

CAPTRP = Cross Track Distance Trip Point

$$\text{CAPTRP} = \left(\frac{\text{CAPNAV}}{\text{CAPILS}} \right) + \text{CTD.ADJ}$$

$$\text{CAPNAV} = \text{Trip Point for RNAV initiated capture} \quad \text{---} \quad = \frac{V_g^2 (1 - \cos(\text{TAE}))}{g \tan(\text{CAP.BNK})}$$

$$\text{CAPILS} = \text{Trip Point for ILS initiated capture} \quad \text{---} \quad = \frac{(\text{CTR.BCI})^2}{(g \tan(\text{CAP.BNK})) (1 + \cos(\text{TAE}))}$$

(CTRBCI is cross track rate from the beam data filter)

$$\text{CTD.ADJ} = \text{Compensation for bank rate command limit (RCL)} = \frac{\text{CAP.BNK}}{\text{RCL}} * V_g \sin(\text{TAE})$$

$$\text{CAP.BNK} = \text{Bank (deg) to be used in capture} \quad \text{---} \quad = \begin{cases} -\text{MAX.CAP.BNK} + \frac{\text{TAE}}{90} & \text{if magnitude of result is } \geq 5^\circ \\ -5 * \text{sign}(\text{TAE}) & \text{otherwise} \end{cases}$$

MAX.CAP.BNK = Programming parameter on CAP.BNK, --- = $8^\circ + \frac{17}{3} * \text{RNGLOC} \leq 25^\circ$
 Corresponds to CAP.BNK at TAE = 90° .
 RNGLOC is distance (nm) to localizer antenna.

CAPTURE INHIBITS

Capture is inhibited at computed (based on R-NAV data) deviations greater than nominally 7° to guard against decreasing localizer receiver output at wide angles. This computation is sensitive to ANAV errors and could compute a value as low as 4° or as high as 10° with typical A-NAV errors. Applicable software variable is "DEVFLG".

RNAV is inhibited if the range is such that R-NAV aiding is not needed. This prevents early trip (NAVCAP) in those cases where CTD errors from the ANAV would initiate (unnecessarily) capture outside the beam edge. Applicable software variable is "ILSLOK".

Localizer deviation (LOCDEV) is rate command limited (limit is programmed with TAE and airspeed) to protect against sudden transients which could cause false captures as well as command transients. Applicable software variable is MXDLDV ("maximum delta in deviation").

Table 5-1. Summary of RNAV Aided Localizer Capture and Track Laws

BANK COMMAND DURING CAPTURE

BCMDNC - Bank command "NAV CAP" based on R-NAV data
 (CTDNAV is cross track distance from R-NAV)
$$= \frac{Vg^2(1-\cos(TAE))}{g \text{ CTDNAV}}$$

BCMDBC - Bank command "beam capture" based on ILS data
 (CTRBC = $\text{CTRBC} \cdot \cos(TAE) + (Vg \sin TAE) \cdot (1 - \cos TAE)$)
$$= \frac{(\text{CTRBC})^2}{g \text{ CTDDBC}(1 + \cos(TAE))}$$

 where CTRBCI and CTDDBC are cross track rate and distance respectively from the beam data filter.

BCMDNC fades to BCMDBC with a 1 sec exponential fade at beam interception.

If "turn short" is detected BCMDNC fades by the algorithm below until beam intercept. Turn short test is $|TAE| < .95 \cdot TAE_{BE}$ where TAE_{BE} is the magnitude of the predicted track angle error at beam intercept (see text)

$$\text{BCMDNC}(t) = \text{BCMDNC}(t_s) * e^{-\left[\frac{t-t_s}{\tau_B} \right]}$$

where t_s is the time at which "turn short" is detected and the fade is started;

τ_B is a computed time constant (see text) that fixes the permissible additional heading change in NAVCAP to insure against turning parallel to the beam.

TRACK TRIP POINT COMPUTATIONS

Track Computations are used when

$$\begin{aligned} & \text{LOCDEV} < 30 \mu\text{A} \quad \text{for } \text{RNGLOC} \leq 13 \text{ nm} \\ \text{or } & \text{LOCDEV} * \text{RNGLOC} < .091 \text{ nm for } \text{RNGLOC} > 13 \text{ nm} \\ \text{or } & |\text{TAE}| < .9 * \text{TAE} \text{TRK} \end{aligned}$$

where TAE_{TRK} is the magnitude of the predicted track angle error at track intercept (i.e. 30 μ A or .091 nm as appropriate)

Capture Computations fade exponentially to track computations with a 5 second time constant.

The TAE test is to prevent turning parallel to the beam in extreme cases and should not normally be the determining factor in initiating Track.

TRACK COMPUTATIONS

$$\text{BNK.CMD} = \text{RNGPGM}(\text{KCTDTRK} * \text{CTDBC} + \text{KCTRTRK} * \text{CTRBC})$$

where $\text{RNGPGM} = \begin{cases} 1 & \text{for } \text{RNGLOC} \leq 7 \text{ nm} \\ 7 & \text{for } \text{RNGLOC} > 7 \text{ nm} \\ \text{RNGLOC} & \end{cases}$

and RNGLOC is distance to localizer antenna.

CTDBC and CTRBC are cross track distance and rate respectively from the beam data filter.

$$\text{KCTDTRK} = (3.2 \text{ deg}/70 \text{ ft.})$$

$$\text{KCTRTRK} = (35 \text{ deg}/70 \text{ fps}).$$

The other disconcerting situation that can occur is the "turn short" case. Here one must be very careful because the beam could be missed entirely (i.e. beam intercept might not occur). To guard against this situation, some means must be present to detect when the system has turned far enough. Recall that Reference 1 took the approach of never letting the system turn to less than a 45° course cut relative to the beam. The approach here is similar in that it restricts course cut relative to the beam, but is a new development in that it conditions the permissible minimum course cut based on the state of the system and provides a precise bank command fade algorithm which is a function of the computed minimum course cut. This will be discussed in more detail in Section 5.3.2. For the moment, we note that in the "turn short" case a "blend down" algorithm must be provided to prevent turning parallel to the beam and to smoothly transition bank command to beam based data.

Several design problems are posed by the discussion above:

1. A capture trip point algorithm is needed which keeps nominal bank in capture significantly less than the bank command limit to handle the "turn long" case.
2. A "blend down" algorithm must be provided to handle the "turn short" case.
3. Good data filtering is needed to provide noise suppression without excessive lag in order that the real system will closely approximate the theoretical system.
4. Smooth transition between modes and data bases must be provided.
5. The individual pieces must be melded into a composite system.

5.3.2 "Blend-Down" Algorithm

As discussed above, the need for a blend-down algorithm arises in the "turn short" case. There are two aspects of the blend-down problem.

1. When should the blend-down be initiated?
2. How should the blend-down be programmed?

The first of these questions requires addressing the problem of "when has the system turned far enough?"

From Reference 2, if the system is executing a constant bank turn onto final course, the bank command (BNK-CMD) should obey the relationship

$$\text{BNK.CMD} = -\tan^{-1} \left(\frac{Vg^2 * (1 - \text{COS}(TAE))}{g * \text{CTD}} \right) \quad (5.1)$$

where

Vg is ground speed

TAE is track angle error or angle of ground velocity vector relative to the runway centerline

CTD is cross track distance to localizer centerline

g is gravitational constant (32.17 ft/sec²)

and consistent units are assumed. Equation 5.1 holds through the entire capture maneuver; and if all assumptions are satisfied, TAE and CTD change in such a way that BNK.CMD remains constant, assuming no wind. If there is a wind, the bank must change during the capture in order to maintain a circular track over the ground.

In particular, for a capture initiated outside the beam on R-NAV data and neglecting wind for the moment, Equation 5.1 should hold at the instant of beam intercept. Now at beam intercept, since one knows range and localizer deviation (LOC.DEV), he can compute cross track distance at the beam edge (CTDBE). Further, since Vg and BNK.CMD are known, one can compute the track angle error at the beam edge (TAEBE) by solving Equation 5.1 for TAE as

$$TAEBE = \cos^{-1} \left[1. - \frac{g \cdot \tan(-BNK.CMD) \cdot CTDBE}{Vg^2} \right] \quad (5.2)$$

where

$$CTDBE = \text{Range} * \sin(\text{LOC.DEV})$$

with appropriate units used. If wind is present Equation 5.2 will still hold at any particular instant in the turn. However, in simulation, certain combinations of errors caused BNK.CMD to converge in such a way that the TAEBE computation converged toward zero. Since this is highly undesirable it was judged best to compute TAEBE once only at capture initiation and accept any resulting anomalies due to wind, which should not be too serious since wind will still be factored correctly into command. Equation 5.2 is basically only used to define the trip point for transition to the blend-down submode. That is, one computes TAEBE at the initiation of capture and as the capture proceeds, he continually tests TAE against TAEBE. If the condition TAE = TAEBE occurs prior to encounter of the beam edge, the system is presumably turning too fast and fading of the bank command should begin. If beam encounter occurs prior to TAE = TAEBE, then the system should fade immediately to bank command based on beam data.

The second aspect of the blend-down problem is the question of how to fade the bank. Assuming an exponential fade on bank command, the following development shows that the time constant of the fade can be computed such that for a fade beginning at the point TAE = TAEBE, the system will never turn further than to TAE = k*TAEBE where 0 < k < 1. That is, a parameter k can be specified such that under no conditions

will the system turn parallel to the beam. For example, if TAEBE = 30° and k = .5, then the system will always intersect the beam at TAE ≥ k*TAEBE = 15°. The expression for faded bank command is given in Equation 5.3

$$\phi_c(t) = \phi_c(t_0) \exp \left[\frac{-(t-t_0)}{\tau} \right] \quad (5.3)$$

where

t is time in seconds

t₀ is time at which the fade begins

φ_c(t) is bank command

φ_c(t₀) is bank command just before fade starts

If the maneuver is coordinated and neglecting lags between bank and bank command

$$\dot{\psi}(t) = \frac{g \tan \phi_c(t)}{U_0} \approx \frac{g \phi_c(t)}{U_0} \quad (5.4)$$

where U₀ is airspeed. Substituting from equation (5.3)

$$\dot{\psi}(t) = \frac{g}{U_0} \phi_c(t_0) \exp \left[\frac{-(t-t_0)}{\tau} \right] \quad (5.5)$$

Integrating equation 5.5 from t = t₀ to t = ∞ yields

$$\psi(\infty) = \psi(t_0) + \frac{g\tau}{U_0} \phi_c(t_0) \quad (5.6)$$

or

$$\Delta\psi = \frac{g\tau}{U_0} \phi_c(t_0)$$

where

Δψ = ψ(∞) - ψ(t₀) is the change in ψ that would occur if the fade continued indefinitely.

Thus

$$\tau = \frac{U_0 \Delta\psi}{g\phi_c(t_0)} \quad (5.7)$$

is a relation for the time constant of the fade which permits us to specify the maximum permissible change in heading during the fade*.

*Admittedly a number of approximations are made here, notably $\dot{\psi} \approx \tan \dot{\psi}$ and neglecting of bank loop lags, but inclusion of these details would be somewhat gruesome and would not alter the essence of the development.

An appropriate choice for $\Delta\psi$ seems to be

$$\Delta\psi = k * TAEBE$$

where $0 < k < 1$.

Substituting this choice for $\Delta\psi$ into Equation 5.7 yields

$$\tau = \frac{U_0 (k * TAEBE)}{g \phi(t_0)} \quad (5.8)$$

as an expression for the fader time constant to be used in the blend-down submode.

5.3 Capture Trip Point

The basic requirement for capture trip point is that it be such that reasonable banks are used in capture and reasonable overshoots occur under all conditions. Generally bank command is restricted to less than 30° in magnitude and it is highly desirable to keep overshoots less than $30 \cdot A (-.4^\circ)$ of localizer deviation. Other factors may also enter. For example, if no R-NAV system is available, clearly the trip point must be within the beam resulting in geometry limits for certain close-in captures. Pilots often have very definite opinions about how the bank should behave under given conditions. It should also be apparent that the conditions above involve the form of the capture bank command at least implicitly. That is, the capture trip point is obviously not independent of the bank to be used in capture. If one assumes a circular capture (i.e. constant bank), it is interesting to solve Equation 5.1 for CTD to illustrate the CTD required to execute a circular capture as a function of V_g , TAE, and $BNK.CMD$

$$CTD = \frac{V_g^2 (1 - \cos (TAE))}{g \tan (BNK.CMD)} \quad (5.9)$$

Equation 5.9 illustrates the generally applicable point that capture trip point expressed in CTD terms is a function of ground speed, TAE, and bank command to be used in the capture. Since it appeared feasible to specify a desired bank during capture, the approach decided on in this study was to specify the capture bank ($CAP.BNK$) and then use Equation 5.9 to determine the trip point, specifically

$$CTD \text{ Trip Point} = \frac{V_g^2 (1 - \cos (TAE))}{g \tan (CAP.BNK)} \quad (5.10)$$

Further, it was felt that $CAP.BNK$ should be a function of TAE, that is at high angle course cuts more bank should be used than for lower angle course cuts. Further, to prevent very small bank captures, the restriction was added that $|CAP.BNK| \geq 5^\circ$ in all cases. Summarizing this relationship, the capture bank in degrees is given by

$$CAP.BNK = \begin{cases} \frac{-MAX.CAP.BNK}{90^\circ} * TAE \dots (\text{if magnitude of result} \geq 5^\circ) \\ -5 * \text{Sign} (TAE) \dots (\text{otherwise}) \end{cases} \quad (5.11)$$

where TAE is in degrees. Before choosing MAX.CAP.BNK it is important to consider the following factors.

Recall from the earlier discussion of the "turn long" case that one must leave room for the bank to increase once the beam is encountered. The question is, "How much increase space is needed?" Figure 5-2 provides some insight.

Figure 5-2, based on Equation 5.1, shows (assuming a circular capture) CAP.BNK versus CTD with TAE as a parameter for a ground speed of 200 fps. For example, if a capture is begun at .5 nmi and TAE is 90°, then 22.3° of bank must be applied instantaneously and held through the turn. Consider, however, the situation when CTD from RNAV is in error by .2 nmi such that the capture in reality begins at .3 nmi instead of .5 nmi. The required instantaneous bank for this case is 34.3° to execute a no overshoot capture. Obviously, with a 30° bank command limit, this cannot be achieved. Further, the inclusion of rate command limits and inherent system lags will make this situation worse (i.e., bank cannot step instantaneously from 0° to CAP.BNK).

Two things are important here. First, the trip point should be such that .2 nmi errors do not cause the required CAP.BNK to exceed 30°. Secondly, the rate command limit turns out to be rather significant and the trip point should be moved to account for its effect. This is most simply done by noting that the approximate time required to build to CAP.BNK is

$$\text{Time-to-CAP.BNK} = \frac{\text{CAP.BNK}}{\text{RCL}}$$

where RCL is the bank rate command limit. Further the CTD traversed in this interval of time is (neglecting any turning in this interval)

$$\text{CTD.ADJ} = \frac{\text{CAP.BNK}}{\text{RCL}} * Vg \sin(\text{TAE}) \quad (5.12)$$

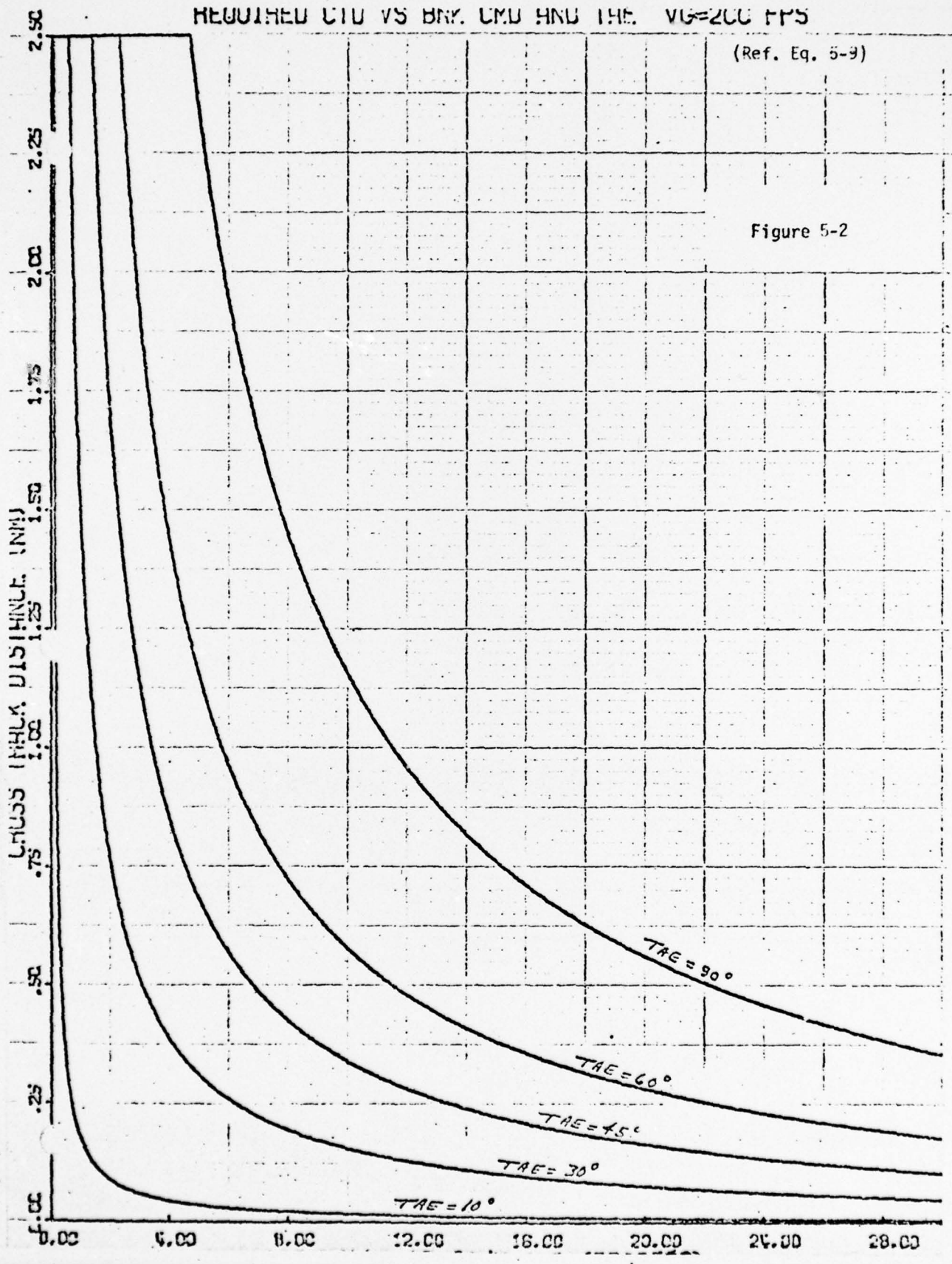
Hence the trip point as computed from Equation (5.10) should be incremented by Equation (5.12) with CAP.BNK determined from Equation (5.11). Figure 5-3 represents Figure 5-2 corrected by equation 5.12 to account for the time to build to the required capture bank. Given the value of CAP.BNK and TAE, therefore, the CAPTURE trip point may be read from Figure 5-3 for the case $Vg = 200$ fps.

The only item as yet unresolved is MAX.CAP.BNK., the maximum bank to be used in capture which as shown in Equation 5.11 becomes one of the significant programming parameters on CAP.BNK. In the event one is doing an RNAV aided capture and the "turn long" case arises, the required "room to increase" on bank once the beam is encountered is a function of range. To see this, consider captures beginning at the same CTD and course cut but at varying range (RNAV data is used until beam intercept). Intuitively, the further out one is in range, the more beam width in feet is available after beam intercept to correct the problem or conversely less time is spent using an erroneous command.

REQUIRED LTD VS BRK. LTD AND THE. $V_G=200$ FPS

(Ref. Eq. 5-9)

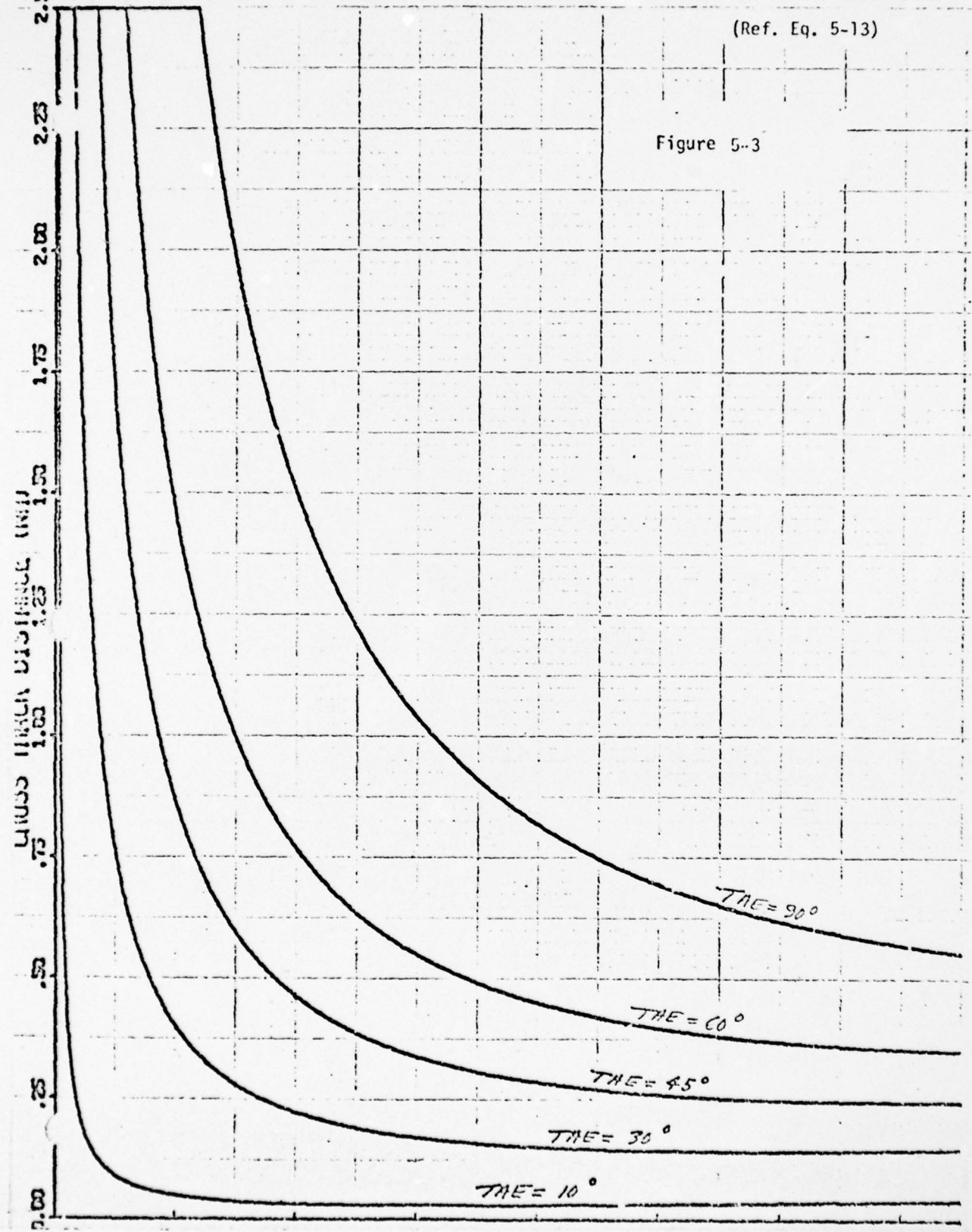
Figure 5-2



REQUIRED CTD VS BNK CMD AND TAE..RATE CMD LHM AND VG=200 FPS

(Ref. Eq. 5-13)

Figure 5-3



For example, consider 90° captures at 5 nm and 8 nm respectively at a groundspeed of 200 fps and using -20° of bank in the capture. From Equation 5.2, if there are no errors, the respective track angle errors at the beam edge (TAEBE) should be

$$\text{TAEBE}_{8\text{nm}} = 70.25^\circ$$

$$\text{TAEBE}_{5\text{nm}} = 54.11^\circ$$

where a 200 μA "beam edge" is assumed. Now in either case at 20° of constant bank the rate of turn is also constant and has the value

$$\dot{\psi} = \frac{g \tan \phi}{Vg} = -3.35^\circ/\text{sec}$$

Now if the trip point in each case is .2 nm late, the capture starts τ_D seconds late where τ_D is given by

$$\tau_D = \frac{.2 \text{ nm}}{200 \text{ fps}} = 6.076 \text{ sec.}$$

Therefore in each case $\Delta\tau$ of heading change would be lost where

$$\Delta\psi = \tau_D * \dot{\psi} = 20.35^\circ$$

Hence the real TAEBE in each case is (adding $\Delta\psi$ to the TAEBE values above)

$$\text{TAEBE}_{8\text{nm}} = 90^\circ$$

$$\text{TAEBE}_{5\text{nm}} = 74.46^\circ$$

Further, the respective cross track distances at the beam edge (CTDBE) are

$$\text{CTDBE}_{8\text{nm}} = .37 \text{ nm}$$

$$\text{CTDBE}_{5\text{nm}} = .23 \text{ nm}$$

Thus the required bank to complete the capture in each case is (from Equation 5.1)

$$\text{CAP.BNK}_{8\text{nm}} = -28.9^\circ$$

$$\text{CAP.BNK}_{5\text{nm}} = -33.1^\circ$$

Notice that for the capture at 8 nm with .2 nm of error in CTD, $(28.9^\circ - 20.0^\circ) = 8.9^\circ$ of bank increase was required while at 5 nm $(33.1^\circ - 20.0^\circ) = 13.1^\circ$ of bank increase was required. This example supports the contention that MAX.CAP.BNK should decrease as range decreases. Further, it is apparent and desirable that R-NAV aiding be used only when necessary.

If the trip point is within the beam, then capture will not begin until beam data is present. If MAX.BNK.CAP is made sufficiently large at longer ranges, it will force the capture to be within the beam in those cases (see Equation 5.10). It was decided to make MAX.CAP.BNK = 25° at longer ranges to insure localizer based captures there and to decrease the value at shorter ranges. From the example above, at 5 nm a bank increase of 13.1° was required in the "turn long" case while at 8 nm a bank increase of 8.9° was required. Further, it can be shown that for a 90° intercept at 200 fps, MAX.CAP.BNK = 25° implies R-NAV aided captures at ranges

shorter than 13 nm range; hence this seems a reasonable point to start programming MAX.CAP.BNK. down. Simulation results supported the 5 nm conclusions above and indicated that slightly more increase was required for the case of a 20% ground velocity error in the slow direction. For this reason, provision of about 15° possible increase at 5 nm seemed advisable. The resulting range program for MAX.CAP.BNK is

$$\text{MAX.CAP.BNK} = 8. + \frac{17.}{13.} * \text{RNGLOC} \quad (3.13)$$

where RNGLOC is range to localizer in nm and the units on MAX.CAP.BNK are degrees.

Collecting the above discussion, the trip point computation is performed as follows

$$\text{CTD Trip Point} = \frac{Vg^2(1-\text{COSTAE})}{g \tan(\text{CAP.BNK})} + \text{CTD.ADJ} \quad (3.13a)$$

where

$$\text{CTD.ADJ} = \frac{\text{CAP.BNK}}{\text{RCL}} * Vg \sin(\text{TAE}) \quad (3.13b)$$

and

$$\text{CAP.BNK} = \begin{cases} -\text{MAX.CAP.BNK} * \frac{\text{TAE}}{90} \dots \text{if magnitude of result is } > 5^\circ \\ -5 * \text{SIGN}(\text{TAE}) \dots \text{otherwise} \end{cases} \quad (3.13c)$$

and

$$\text{MAX.CAP.BNK} = 8. + \frac{17.}{13.} * \text{RNGLOC} \leq 25^\circ \quad (3.13d)$$

CTD trip point as a function of range and course cut is shown in Figures 5-4 for a speed of 200 fps. Superimposed are lines for 200 μ A (ILS CAP "beam-edge") localizer deviation and "track trip". These are significant boundaries for they delineate NAVCAP, ILSCAP, and track regions respectively.*

An alternate presentation of trip point information is shown in Figure 5-5. Here, for constant course cuts of 90 degrees, CTD trip point is plotted versus ground speed and range.

5.3.4 Track Trip Point

The transition from capture to track normally occurs when

$$\text{LOCDEV} < 30 \mu\text{A for } \text{RNGLOC} \leq 13 \text{ nm}$$

and for

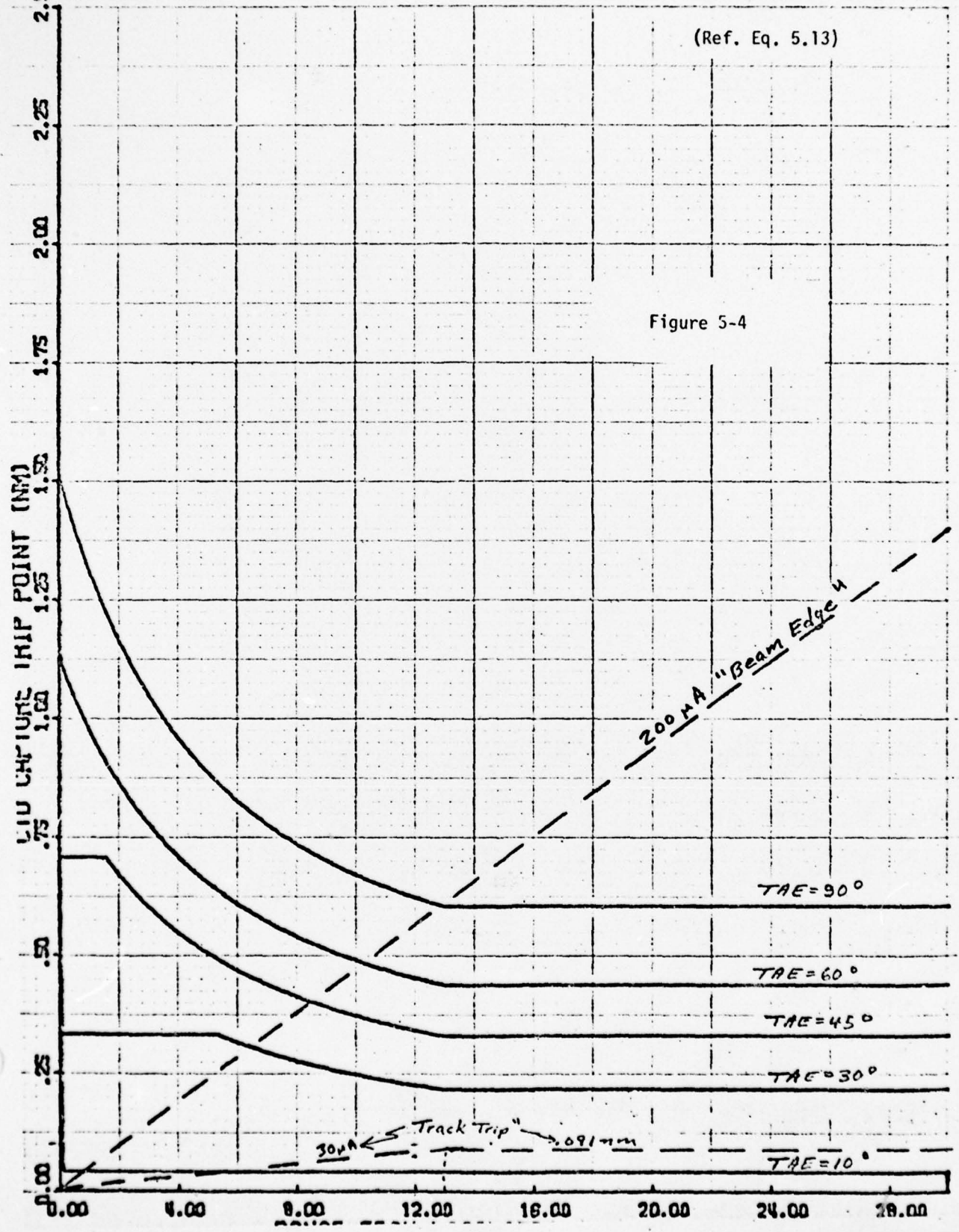
$$\text{LOCDEV} * \text{RNGLOC} < .091 \text{ nm for } \text{RNGLOC} > 13 \text{ nm}$$

*If the capture trip point lies within the "Track Trip" boundary, capture mode is deleted and the system transitions directly from heading mode to track mode.

CAPTURE TRIP PT VS RANGE AND TAE...RATE CMD LIM AND VG=200 FPS

(Ref. Eq. 5.13)

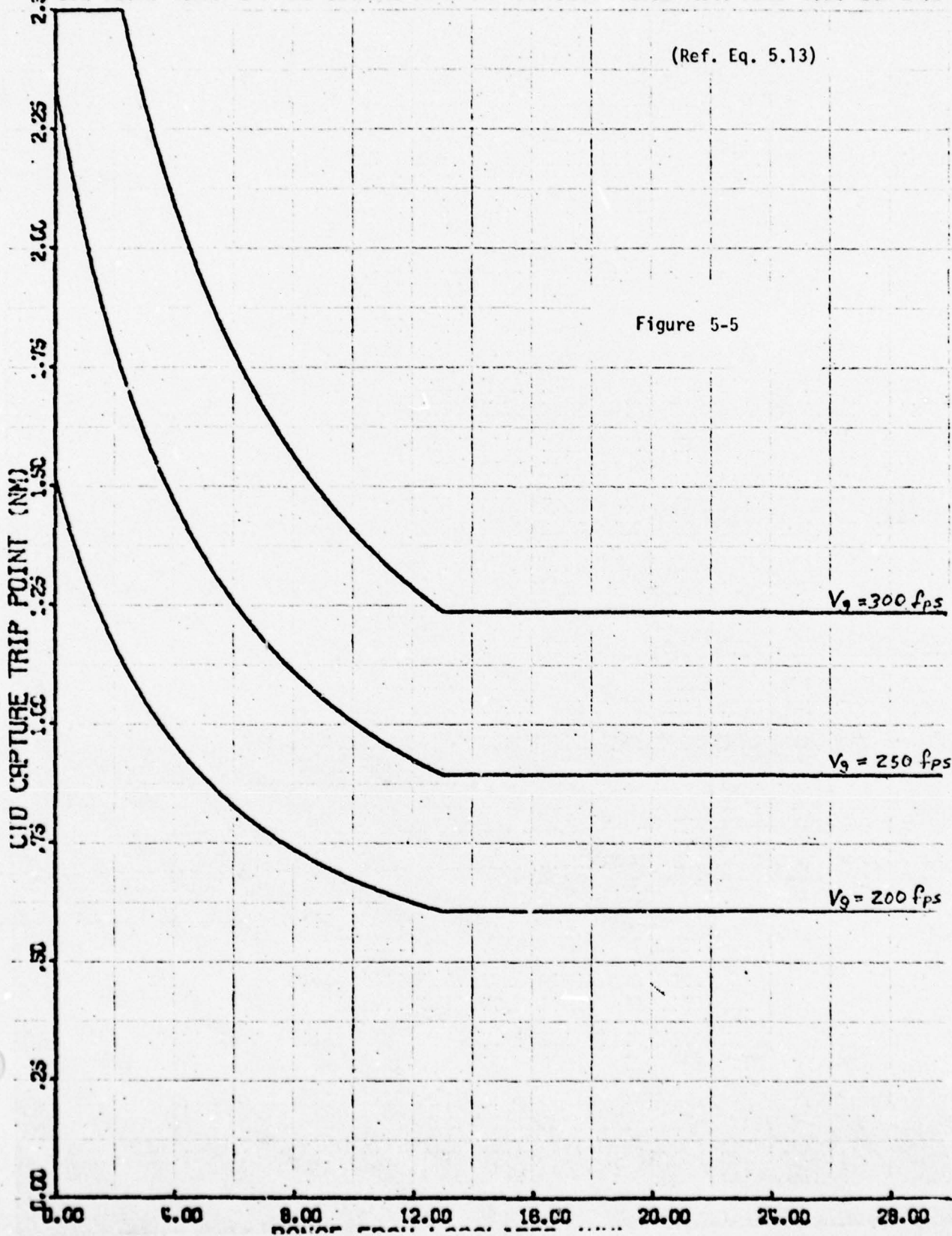
Figure 5-4



CAPTURE TRIP PT VS RANGE AND VG ... RATE CMD LIM AND TAE=90 DEG

(Ref. Eq. 5.13)

Figure 5-5



The transition from angular to linear CTD criterion for transition to track prevents going to track at high values of TAE at long ranges where $30 \mu A$ represents significant linear deviation. The advantage here lies in maintaining capture mode and hence the circular nature of the capture as long as possible. However, in the event of severe crosswinds or unusually bad initialization the possibility of turning parallel to the beam during ILSCAP exists. To provide a final safeguard against turning parallel the following override trip to track feature is provided.

Since in ILSCAP the system is still performing a circular capture a slight derivative of Equation 5.2 for the TAEBE (track angle error at the beam edge) can be used to compute TAETRK (track angle error at track trip point).

$$\text{TAE TRK} = \cos^{-1} \left[1 - \frac{g \cdot \tan(-\text{BNKCMD}) \cdot \text{CTDTRK}}{v_g^2} \right] \quad (5.14)$$

where

$$\text{CTD TRK} = \begin{cases} \left(30 \mu A * \frac{\text{RNGLOC}}{(75)(57.3)} \right) \text{ nm, RNGLOC} \leq 13 \text{ nm} \\ .091 \quad \text{nm, RNGLOC} > 13 \text{ nm} \end{cases}$$

The system tests for $(|TAE| < .9 * \text{TAETRK})$, computing TAETRK via Equation 5.14; and if this condition occurs during ILSCAP, generates an override trip into the TRK mode. The flattening of the TAETRK curves at long ranges is due to the fixed CTD track trip point at ranges greater than 13 nmi. The flattening at short ranges is due to a bottom limit of 7° imposed on the computation (actually 7.73° on TAETRK so that $.9 * \text{TAETRK} > 7^\circ$) to ensure that this final test never drops below that value. That is, the system is constrained under all circumstances to go to track from ILSCAP if TAE drops less than 7 degrees.

5.3.5 Data Filtering

All of the foregoing discussion has neglected noise and lags on sensor data. In order for the conclusions and predictions above to be accurate, the data filtering, particularly on localizer data, must not introduce excessive lag. The often used system of about one second lag on radio and a complementary filter using radio and bank or heading to derive beam rate introduces lags that significantly compromise the performance of the system described here based on simulation results. For this reason a second order data filter for radio was developed which employs a bank input to provide complementing for both beam rate and position. With this filter, better performance in capture resulted and bank activity in track due to beam noise was very significantly decreased. This filter is described in detail in Reference 3 and performance is documented in Reference 4, hence it will not be discussed further here.

5.3.6 Mode Transition

As implied in the preceding discussion, there are several distinct modes in the system that have evolved from this study. It is assumed that there is a heading select mode which is controlling the aircraft to a fixed heading (or course) prior to initiation of capture. Capture may be initiated either on R-NAV data or on beam data. In the former case, a blend-down submode may occur, and eventual transition to beam based capture must occur. Finally, a track mode assumes control once capture is completed. The transitions from mode to mode must be handled smoothly with no switching transients. The general mode switching smoothing technique is shown in Figure 5-6. The fade is basically a digitized exponential fade with 1 to 5 second time constants being typical.

5.3.7 Final System Description

Capture Modes

A block diagram of the total R-NAV aided ILS localizer capture and track system is shown in Figure 5-7. It should be noted that there are basically two potential capture modes. Capture computations are based on R-NAV data (NAVCAP) or based on ILS data (ILSCAP). Further there is a blend-down submode (BLNDWN) of NAVCAP which is provided to fade the bank command down in the "turn short" case. If R-NAV aiding is needed, the NAVCAP mode will occur first, transitioning to ILSCAP when localizer deviation becomes less than 200 μ A. If during NAVCAP the system turns too far [determined by continually comparing TAE with predicted TAE at the beam edge (TAE_{BE}) during NAVCAP], the BLNDWN submode is automatically selected and fades the bank command according to the fade algorithm discussed in Section 5.3.2. ILSCAP can occur in two ways. First, if NAVCAP is in progress and localizer deviation decreases below 200 μ A, then ILSCAP is selected immediately. The other case occurs when the capture trip point is such that localizer deviation at that point will be less than 200 μ A. In this case no R-NAV aiding is needed and the ILSCAP mode is selected immediately. In terms of logic equations, the capture conditions may be expressed as

$$\text{NAVCAP} = [(\text{LOC DEV} > 200 \mu\text{A}) \cdot (\text{CTDNAV} < \text{CAPTRP})] \cdot (\text{RNGLOC} < \text{ILSLOK}) \quad (5.15)$$

$$\text{ILSCAP} = [(\text{LOCDEV} \leq 200 \mu\text{A}) \cdot (\text{NAVCAP} + (\text{CTDILS} < \text{CAPTRIP}))] \cdot (\text{DEVFLG}) \quad (5.16)$$

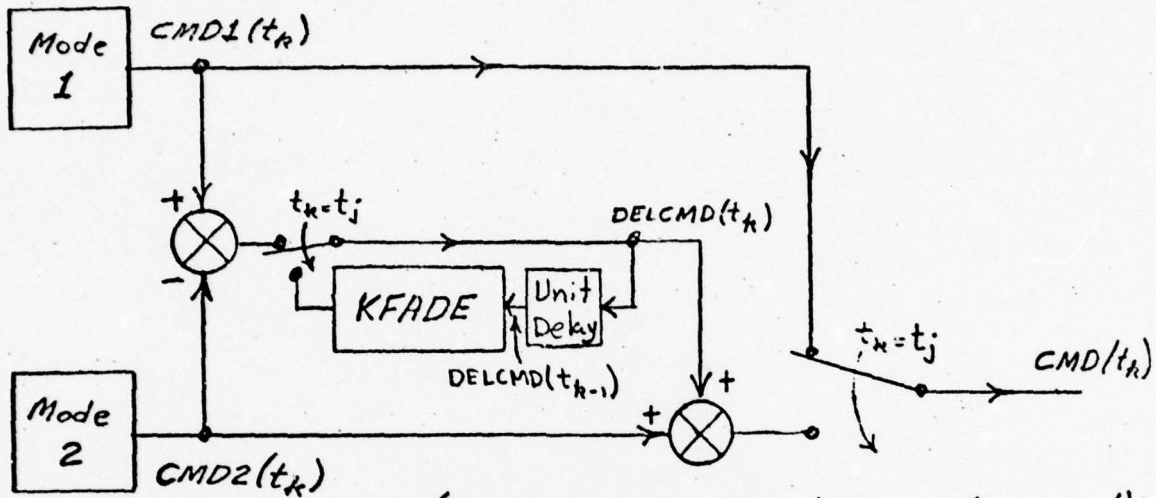
$$\text{BLNDWN} = \text{NAVCAP} : (|\text{TAE}| \leq |\text{TAE}_{\text{BE}}|) \quad (5.17)$$

where ILSLOK and DEVFLG are added protections against R-NAV trip at excessive range due to CTDNAV errors and false ILSCAP trips due to decreasing LOCDEV at wide angle* respectively.

False Trip Guards and Deviation Rate Limit

Both of these protections are shown in Figure 5-8. DEVFLG basically inhibits localizer computations at greater than a nominal deviation of 7° from the beam centerline. Seven degrees was chosen so that even with R-NAV errors the computed value will lie reliably between 4° and 10°.

*Localizer signal strength in a +10 degree sector should be adequate to saturate the receiver but may drop off at wider angles.



($t_k = kT$ where T is the sample period)

(Mode changes from Mode 1 to Mode 2 at time $t_k = t_j$)

$$KFADE = e^{-T/\tau}$$

1. For $t_k < t_j$

$$CMD(t_k) = CMD1(t_k)$$

$$DELCMD(t_k) = CMD1(t_k) - CMD2(t_k)$$
2. At $t_k = t_j$

$$DELCMD(t_j) = CMD1(t_j) - CMD2(t_j)$$

$$CMD(t_j) = CMD2(t_j) + DELCMD(t_j) = CMD1(t_j)$$
3. For $t_k > t_j$

$$t_k - t_j = (k-j)T$$

$$DELCMD(t_k) = DELCMD(t_j) * (KFADE)^{(k-j)}$$

$$= DELCMD(t_j) * e^{-\frac{(k-j)T}{\tau}}$$

$$CMD(t_k) = CMD2(t_k) + DELCMD(t_k)$$
4. For $(t_k - t_j) \gg \tau$

$$CMD(t_k) \approx CMD2(t_k)$$

Figure 5-6. Smoothing Technique For Mode Switching (Digital System)

30/90 Gulfstream I Inner Loops
(SPRO Autopilot)

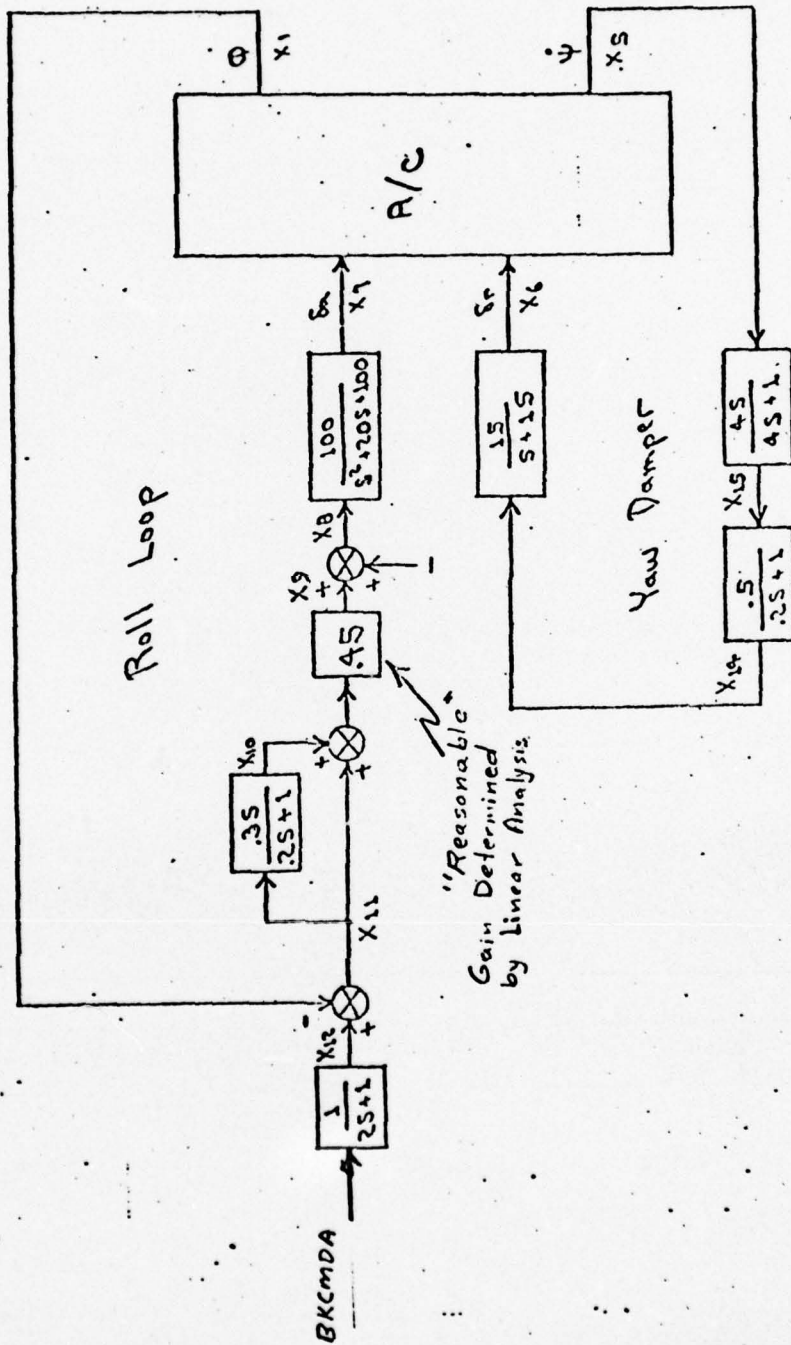
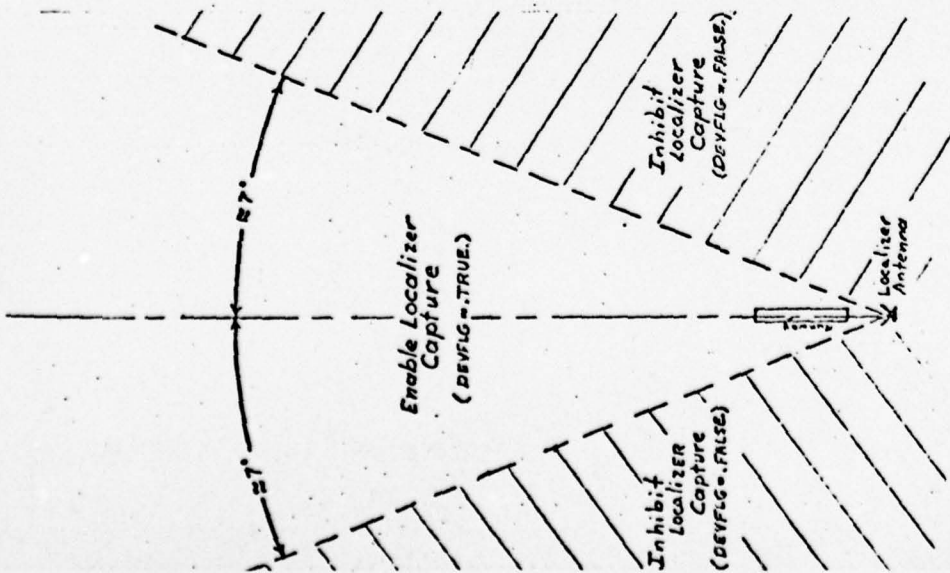
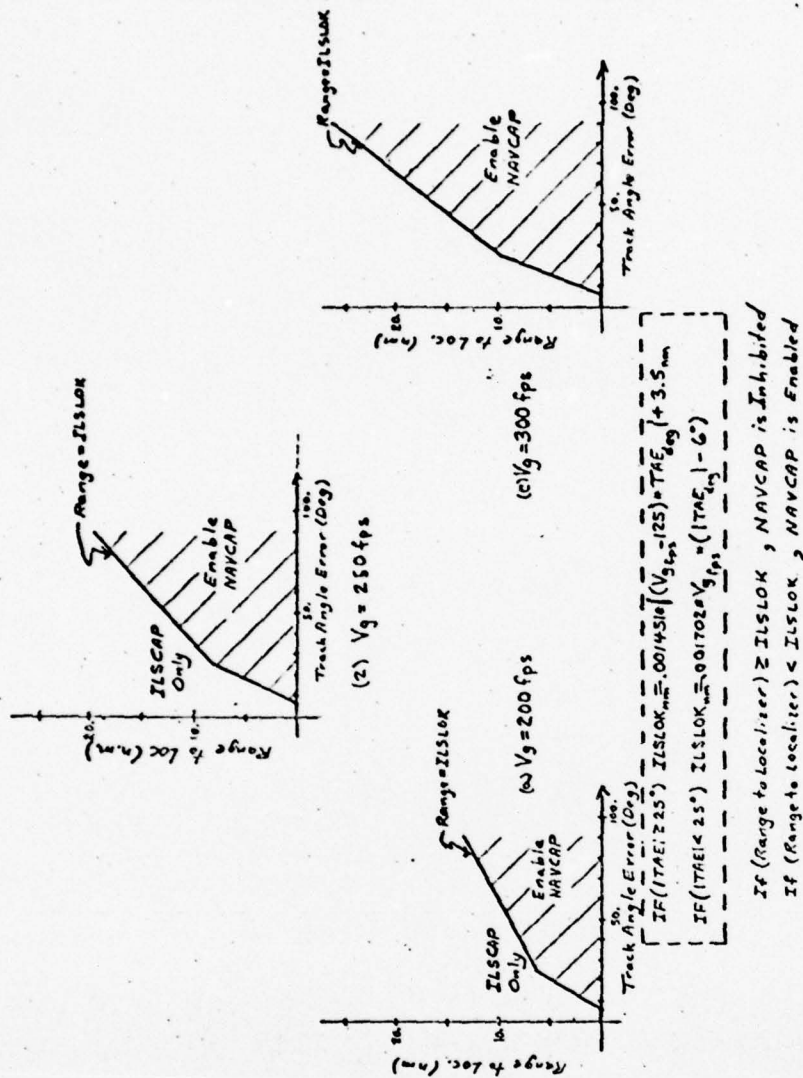


Figure 5-7b



(a) Guard Against Decreasing Localizer Deviation At Wide Angles



(b) Guard Against A-NBV Auding At Excessive Range Due to A-NBV Cross-Track Distance Errors

Figure 5-8. Capture Trip Point Guards

ILSLOK basically inhibits NAVCAP if RNGLOC and TAE and VG data indicate that a non-R-NAV aided capture can be made. The only protection really is against early capture due to R-NAV CTD errors in regions where RNAV aiding is not needed. The equation for ILSLOK was generated by tabulating the ranges at which various TAE capture trip points intercept the beam edge (200 μ A) at 200, 250, and 300 fps and then curve fitting to this data. It should be noted that if LOCDEV $> 200 \mu$ A, then CAPTRP is based on R-NAV data, but if LOCDEV $\leq 200 \mu$ A, it is based on beam data. This feature is necessary to prevent R-NAV errors from corrupting the trip point of an ILS data only capture. To protect against decreasing LOCDEV at wide angles, DEVFLG, as discussed above, is used and to prevent false trips due to momentary interference as well as to guard against sudden transients a rate limit on LOCDEV is included. This rate limit is programmed with TAE and speed but lower limited at 9 μ A/sec under all conditions. Figure 5-9 shows the programming on the rate limit which is basically determined by dividing the cross track rate of the aircraft by range and then increasing this value by 30% to provide a conservative estimate of deviation rate.

Fade From NAVCAP to ILSCAP

Notice that during NAVCAP a fader circuit like the one of Figure 5-6 is prepared to fade from NAVCAP to ILSCAP when the need arises. Similarly during ILSCAP a companion fader stands ready to blend to the track mode. The bank command in either NAVCAP or ILSCAP is the proper one to generate a circular capture and both are essentially the same as Equation 5.1 although the form used in ILSCAP is modified to more appropriately use beam based data. This form is easily derived from Equation 5.1 which is repeated below

$$\text{BNK.CMD} = -\tan^{-1} \left(\frac{Vg^2 * (1 - \cos(\text{TAE}))}{g * \text{CTD}} \right) \quad (5.18)$$

Multiplying numerator and denominator of the arctan argument by $(1 + \cos \text{TAE})$ and substituting $\text{SIN}^2(\text{TAE})$ for $1 - \text{COS}^2(\text{TAE})$ in the numerator yields

$$\text{BNK.CMD} = -\tan^{-1} \frac{(Vg * \text{SIN}(\text{TAE}))^2}{g * \text{CTD} * (1 + \text{COS}(\text{TAE}))}$$

But

$$Vg * \text{SIN}(\text{TAE}) = \text{Cross Track Rate (CTR)}$$

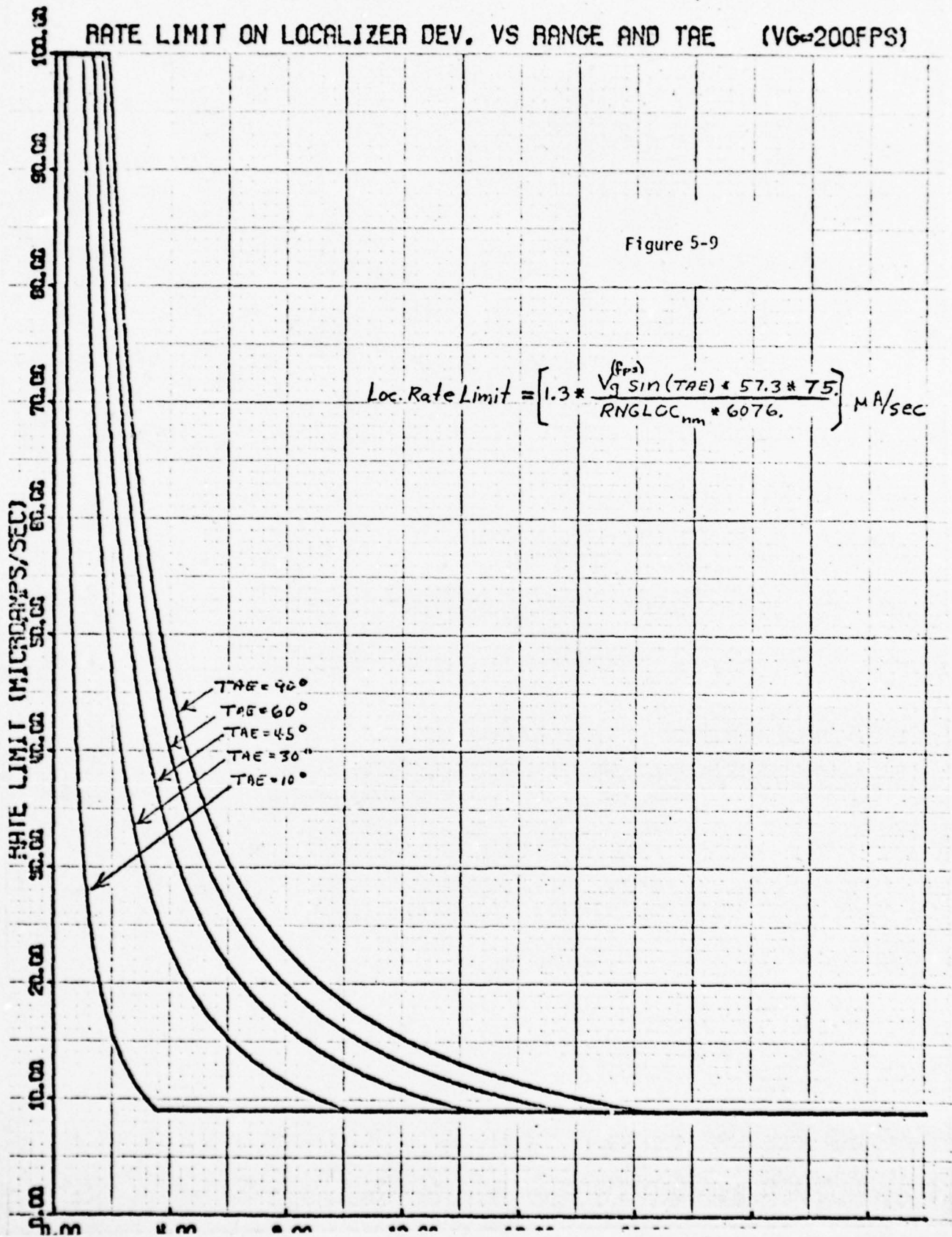
Hence

$$\text{BNK.CMD} = -\tan^{-1} \frac{(\text{CTR})^2}{g * (\text{CTD}) * (1 + \text{COS}(\text{TAE}))} \quad (5.19)$$

Equation (5.19) uses CTR as well as CTD explicitly and can thus make effective use of the beam data filter output. Groundspeed estimate errors will not influence Equation (5.18) directly and TAE errors will not have a large effect, particularly as the system approaches transition to track since as $\text{TAE} \rightarrow 0$, $\text{COS}(\text{TAE}) \rightarrow 1$, and $(1 + \text{COS}(\text{TAE})) \rightarrow 2$. Thus, this term does not have the effect that it does in Equation (5.13), where

RATE LIMIT ON LOCALIZER DEV. VS RANGE AND TAE (VG=200FPS)

Figure 5-9



$(1 - \cos(\text{TAE})) \rightarrow 0$ as $\text{TAE} \rightarrow 0$. The form of Equation 5.19 is no better than that of 5.18 in NAVCAP, however, since in NAVCAP, $\text{CTR} = -V_g \sin(\text{TAE})$ which simply would bring back TAE in a different form.

Track Mode

The track mode is a conventional proportional combination of position and rate relative to the beam center to form bank command. The trip point for going to track mode was discussed in Section 5.3.4. Track gains are given in Table 5-2 in several different forms for ease of correlation with other work. A stability analysis of the track mode appears in Section 5.4.

	Range < 7 nm	Range \geq 7 nm	Range = 8 nm
Gain on Position	$\left(\frac{3.2}{70} = .046\right) \frac{\text{deg}}{\text{ft}}$ or $(.2795) \frac{\text{deg}}{\text{nm}}$	$(.45) \frac{\text{deg}}{\mu\text{A}}$ or $(13.6) \frac{\text{deg}}{\text{dot}}$	$(.45) \frac{\text{deg}}{\mu\text{A}}$ or $(13.6) \frac{\text{deg}}{\text{dot}}$
Gain on Rate	$\left(\frac{35}{70} = .5\right) \frac{\text{deg}}{\text{fps}}$ or $(.844) \frac{\text{deg}}{\text{kt}}$	$.5 * \frac{7}{\text{RNGLOC}} \frac{\text{deg}}{\text{fps}}$ or $\left(.844 * \frac{7}{\text{RNGLOC}}\right) \frac{\text{deg}}{\text{kt}}$	$(.438) \frac{\text{deg}}{\text{fps}}$ or $(.739) \frac{\text{deg}}{\text{kt}}$

Table 5-2. Rate & Position Gains for Track Mode

Notice that the output of the data processing filter is position and position rate to provide the requisite data to the capture computations. This is also the appropriate form for the track mode at close ranges. However, at longer ranges the effects of beam noise, particularly excessive bank activity, require that gains be softened, usually such that the track law becomes angularly based rather than position based. The RNGPGM block of Figure 5-7 may be seen to provide this feature since at ranges beyond 7 nm (neglecting the filter for the moment since its parameters are not range dependent),

$$\text{CTDTRK} = \frac{7}{\text{RNGLOC}} * \text{RNGLOC} * \text{LOCDEV}$$

$$\text{CTDTRK} = 7 * \text{LOCDEV} \tag{5.20}$$

Equation 5.20 shows that CTDTRK beyond 7 nm is really in angular units with the 7 being the required factor for blending properly with the linearized portion. Alternately, the combination of RNGPGM programming downstream of the filter and RNGLOC programming of LOCDEV upstream of the filter provides linearization of LOCDEV out to 7 nm and a constant gain beyond that range. The rate is treated similarly to take care of the radio contribution to rate. There is no real necessity to program the bank

contribution to rate and in fact stability would be aided by not doing so. However, in order to maintain system simplicity, no separate provision was made for bank contributed rate.

Data Processing

The data processing portion of the block diagram consists primarily of a double complementing filter (DCF) as described in Reference 3. Since in this application roll or bank is used for generating acceleration, it is termed the roll radio double complementing filter (RRDCF). The proportional combination of RRDCF rate and R-NAV based rate using the function KYDBLN provides slightly improved rate for capture. The basic idea here is that although bank provides information about acceleration orthogonal to the aircraft fuselage reference line, the RRDCF filter requires acceleration relative to the beam centerline. Hence bank is processed as

$$\ddot{y}_{\phi} = -g \tan(\psi) \cos(\text{TAE})$$

At high course cuts, therefore, bank does not provide very good information about acceleration relative to the beam. The necessity of complementing RRDCF filter rate against R-NAV rate in capture is not firmly established. R-NAV rate is used to initialize RRDCF and low frequency updates by radio rate might then provide sufficiently good rate. The function used for KYDBLN is $\cos(\text{TAE})$ so that as the system turns onto the final course, the influence of R-NAV rate is removed. A washout on bank is used during track to prevent beam tracking standoff due to bank bias.

Output Command Processing

The final aspect of the system block diagram is the output command processing shown at the right side of Figure 5-7a. Basically a 5 degree per second rate command limit and a 30 degree command limit are imposed. The lead-lag compensation is necessary for the specific Gulfstream I autopilot interface provided for in this application. The system interface to the Sperry SP40 autopilot interposes a 2 second lag between the available heading error port and the bank command summing point. Figure 11b shows the equivalent block diagram of the SP40 autopilot. It should be noted that this is a somewhat sluggish autopilot having particularly large servo lags. This factor necessitates running somewhat lower outer loop gains than one might prefer in approach.

5.3.8 Software Organization

The basic software organization required to implement the system described above is shown in Figure 5-10. The localizer capture and track computation are a submode to the ILS main program which interfaces with the R-NAV main software. The chosen approach is to process the data in one software block, determine the proper mode in another, and then perform control computations based on the determined mode. Finally, the output control processing does the rate and amplitude command limiting and the lead-lag compensation as shown in Figure 5-7a. A more detailed block diagram is provided in Figure 5-11. The program listing is given in Appendix F.

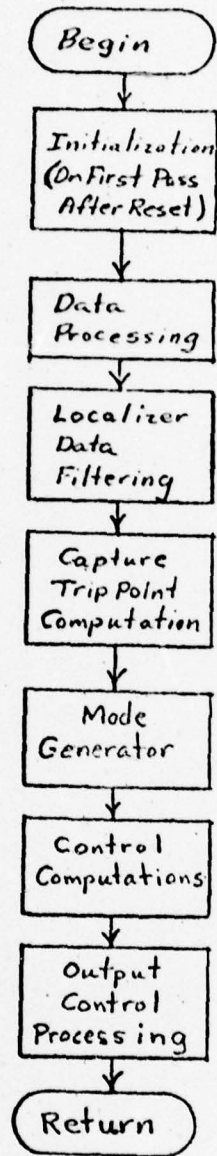


Figure 5-10. Basic Software Organization
Lateral Computational Module

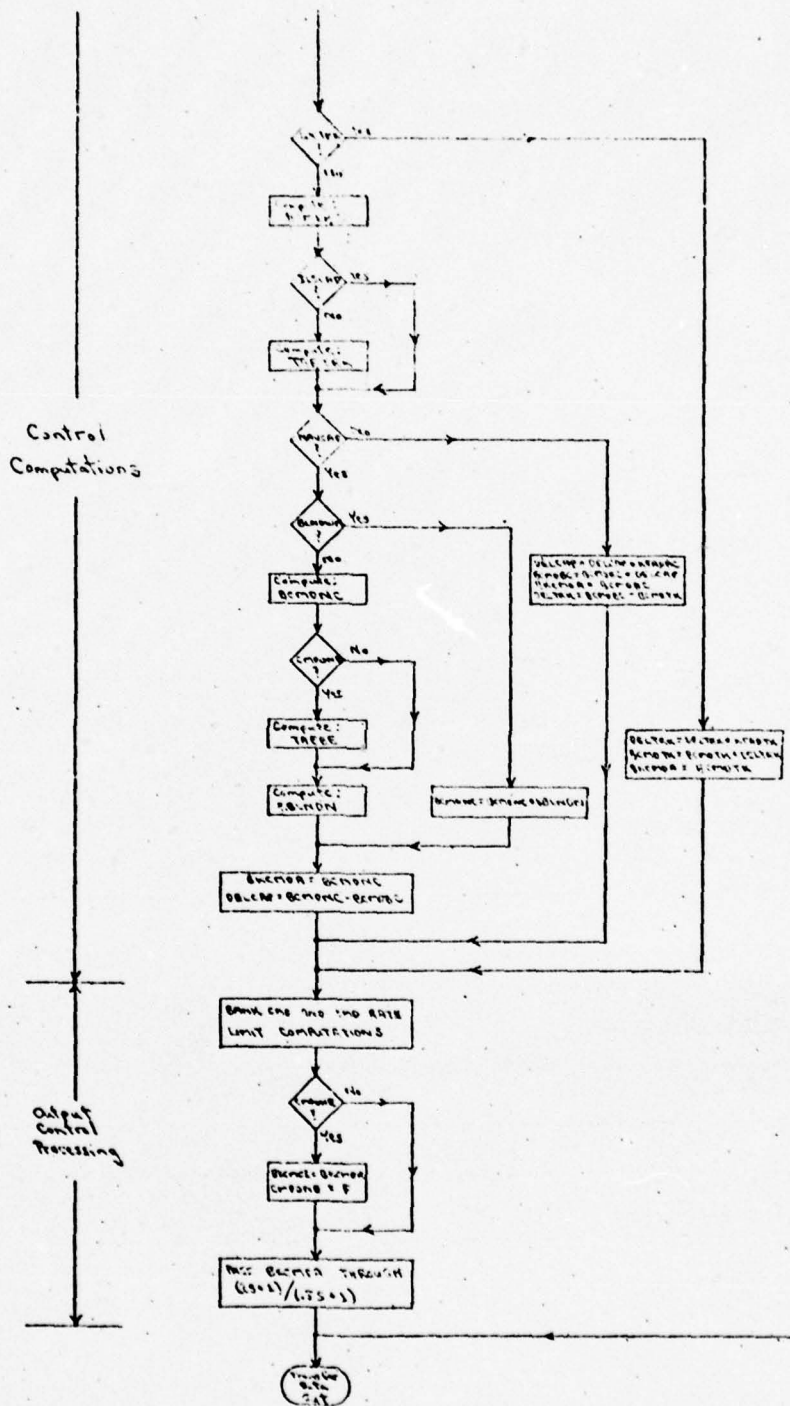


Figure 5-11. Detailed Lateral Flow Chart Section 3 out of 3

30/40 Localizer Module
Flow Program

5.4 Stability Analysis of the 3D/4D Lateral ILS Localizer Track Laws

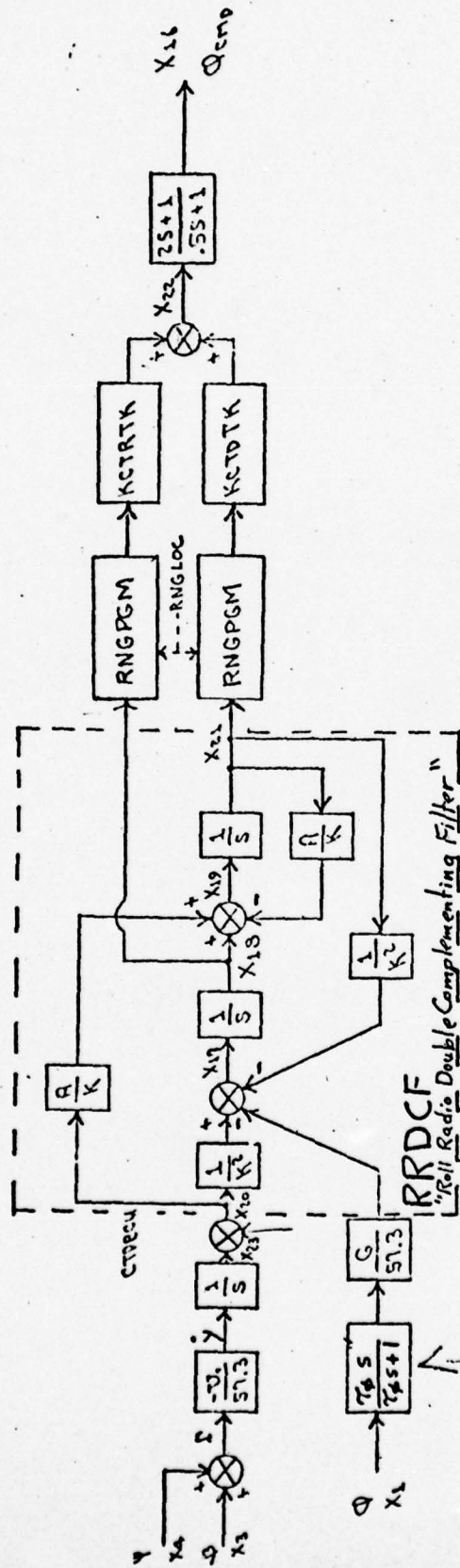
Figure 5-12 shows a block diagram of the track control laws from sensor inputs to bank command while Figure 5-13 shows the block diagram for autopilot and aircraft. (Note the rather sluggish aileron servo.) From Reference 3 the pole-zero parameter A in the RRDCF filter (see Figure 5-12) was set at 2 with the bandwidth parameter K fading from 3.036 (the capture value) to 10 once track was well established. Stability and PSD data was therefore computed for both extreme values of K recognizing that the results for K=3.036 will be applicable early in track while those for K=10.0 apply for well established track. Loops were broken at radio and at bank command. The loop at radio plots must be interpreted carefully particularly for K=10, because the complementing effect of the bank feed through to position (see Reference 3) permits somewhat lower than conventional bandwidths in the radio loop.

The system was linearized (RNGPGM) only to 7 nm from the localizer antenna since linearizing further produced excessive bank activity.

At long ranges, therefore, the bandwidth of the system both at radio and bank command decreases considerably ($-20 \log \left(\frac{7 \text{ nm}}{25 \text{ nm}} \right) = -11.06 \text{ db}$). Stability was checked carefully, therefore, at the assumed extreme range of 25 nm. Figures 5-14 to 5-17 show gain/phase plots for loops broken at radio and bank command for K=3.036 and K=10 respectively, all at 25 nm. Note on Figures 5.14 and 5-15 the phase dip below 180° at low frequency. This dip is due to the bank washout shown in Figure 5-12. The magnitude of the dip is greater for shorter than for longer washout time constants. For this reason a 60 second washout is used at 25 nm programmed down to 30 seconds at 50 nm. The long washout at near range is undesirable due to the long charging time required to remove bank biases which are more troublesome at near than at far ranges. Bank biases, if not washed out, result in both position and rate biases out of RRDCF (see Reference 3). Table 5-3 tabulates the stability margin and crossover data from Figures 5-14 through 5-17. Also shown in Table 5-3 is the analogous data for 5 nm range.

Range	W/O Time Const.	K	RNGPGM*	RNGPGM*	Loop at Radio			Loop at Bank Cmd		
			KCTDTK deg/ft	KCTRK deg/fps	Wc.o.	P.M.	G.M.	Wc.o.	P.M.	G.M.
25 nm	60	3.036	$7 \frac{(3.2)}{25 \sqrt{70}}$	$7 \frac{(35)}{25 \sqrt{70}}$.092	25°	11	.101	38°	24
25 nm	60	10.0	$7 \frac{(3.2)}{25 \sqrt{70}}$	$7 \frac{(35)}{25 \sqrt{70}}$.070	20°	7	.092	42°	24
<7 nm	30	3.036	$\frac{(3.2)}{\sqrt{70}}$	$\frac{(35)}{\sqrt{70}}$.155	31°	8	.26	57°	13
<7 nm	30	10.0	$\frac{(3.2)}{\sqrt{70}}$	$\frac{(35)}{\sqrt{70}}$.09	24°	10	.295	60°	13

Table 5-3. Stability Margins



$$\text{RNGPGM} = \begin{cases} 1 & \text{if } \text{RNGLOC} < 7\text{mm} \\ \frac{1}{\text{RNGLOC}} & \text{if } \text{RNGLOC} > 7\text{mm} \end{cases}$$

$$\begin{aligned} \text{KCTD TK} &= .0(4/10) = .0457 \\ \text{KCTR TK} &= (35/10) = .50 \\ A &= 2.0 \\ K &= 3.036 \\ U_0 &= 200 \end{aligned}$$

$$\tau_d = (22.5 + 1.5 * \text{RNGLOC}_{\text{mm}}) \text{ sec}$$

Figure 5-12. 3D.4D Track Laws

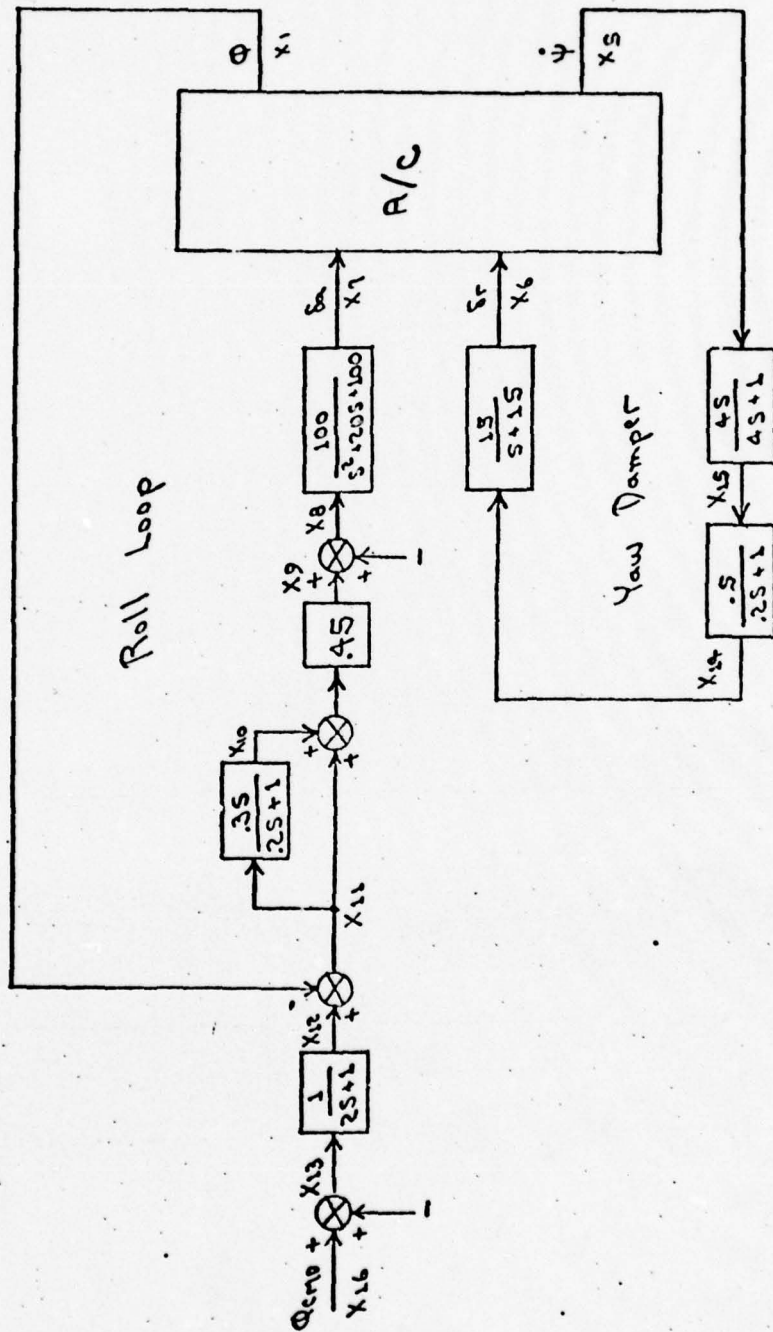


Figure 5-13. Gulfstream I Inner Loops

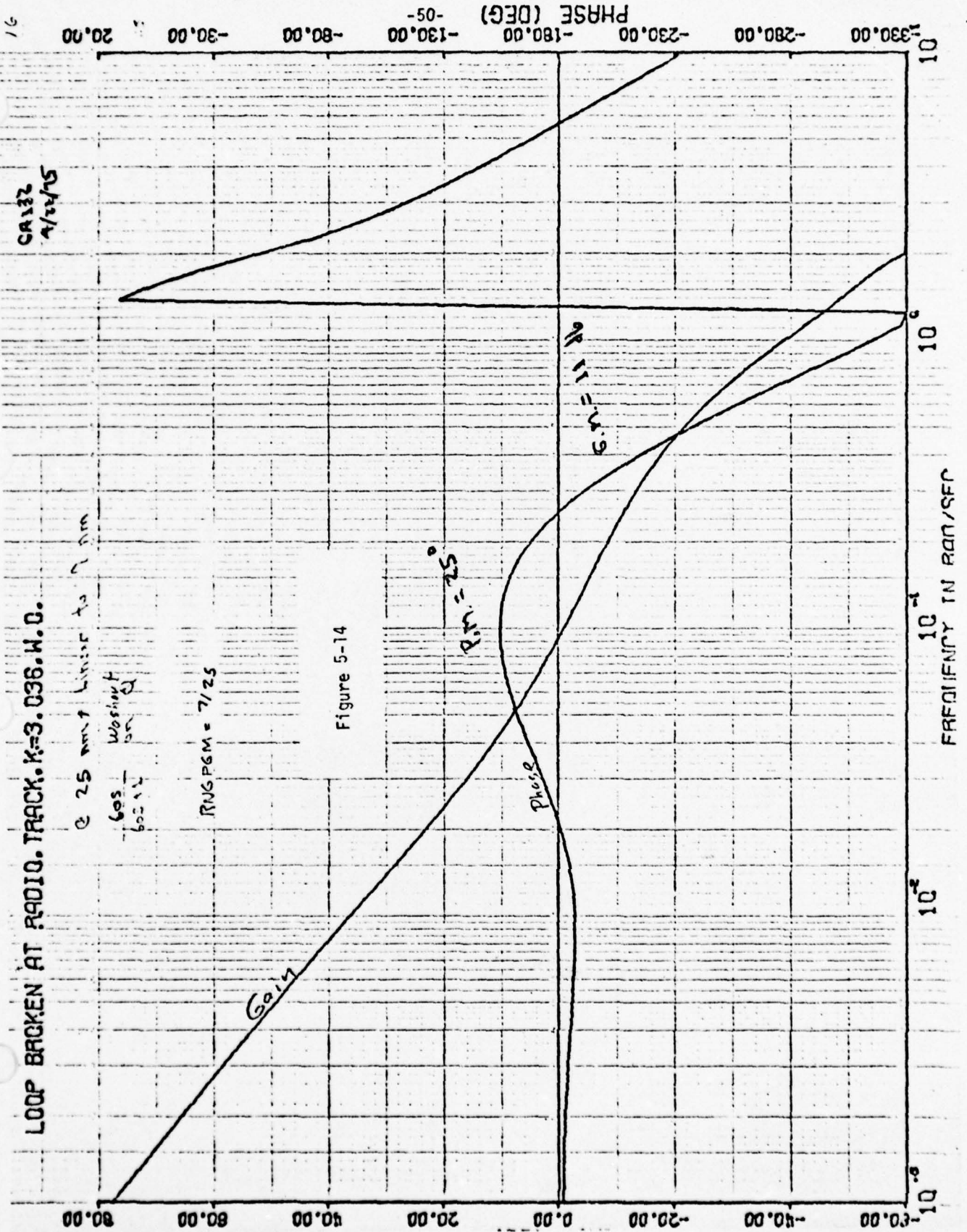
LOOP BACKEN AT RADIO. TRACK. K=3.036. H.O.

Q 25 mmf limit to 7 mm

605 - Washburn
605 1/2

RNG PGM = 7/25

Figure 5-14

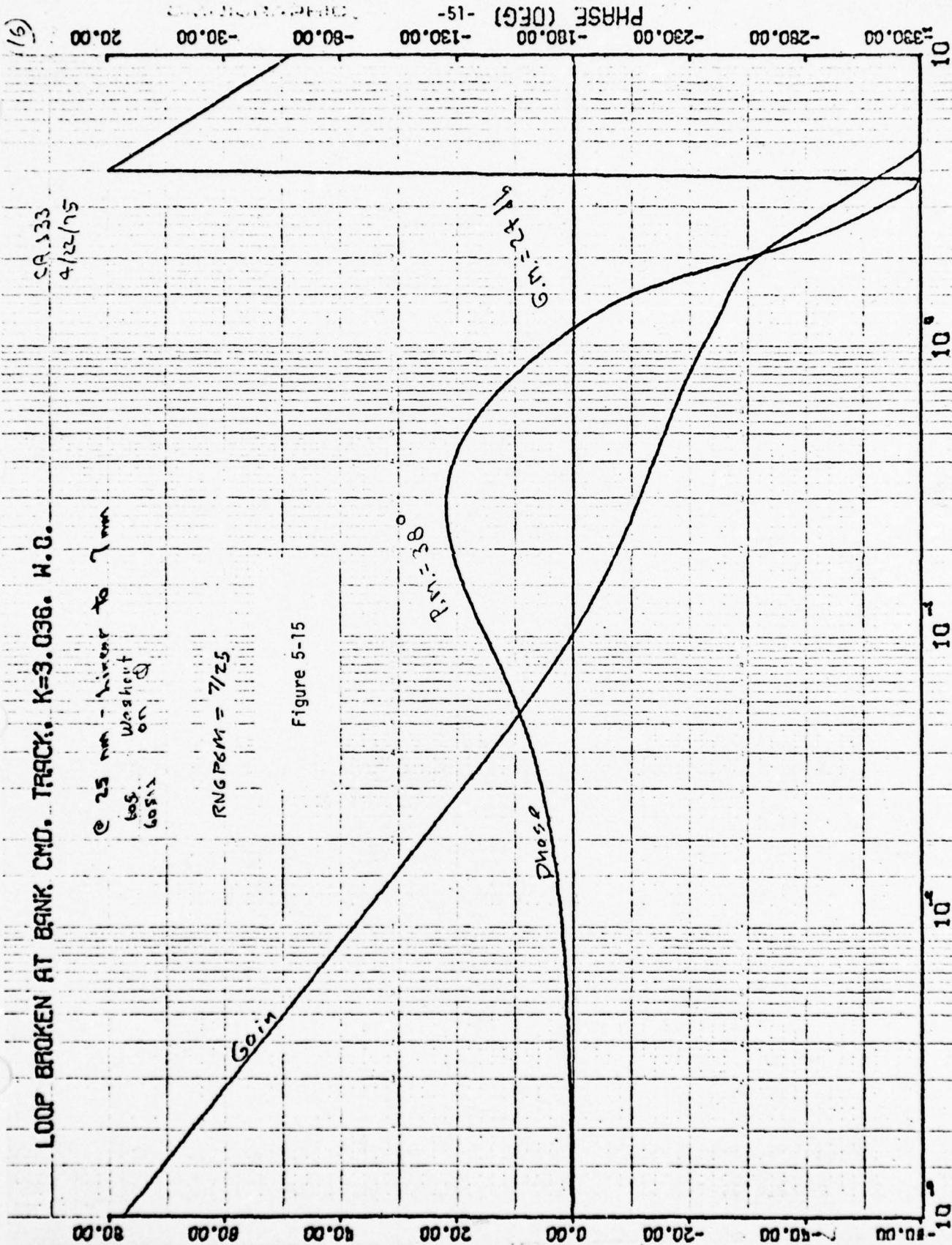


LOOP BROKEN AT BANK CMD. TRACK. K=3.036. H.O.

© 25 mm - linear to 7 mm
605. Washout on
60512

RNGP6M = 7/25

Figure 5-15

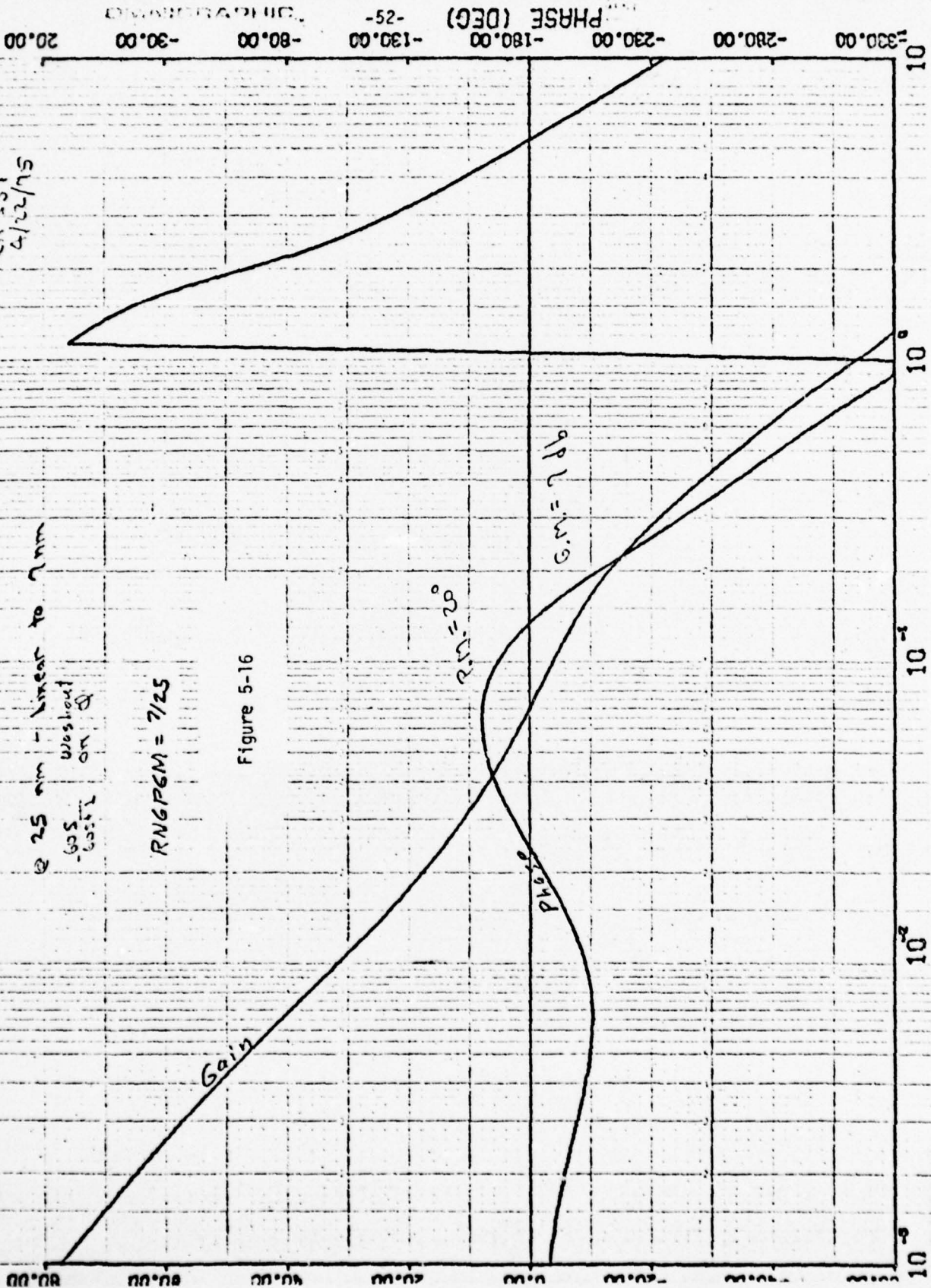


LOOP BROKEN AT RADIO. TRACK. K=10... W.O.

@ 25 mm - linear to 7mm
-60S Washout
-60S on @

RNGP6M = 7/25

Figure 5-16



LOOP BROKEN AT BANK CMD. TRACK. K=10. H.C.

@ 25 min - instant to 7 min
605 Washout
605.1 on 10

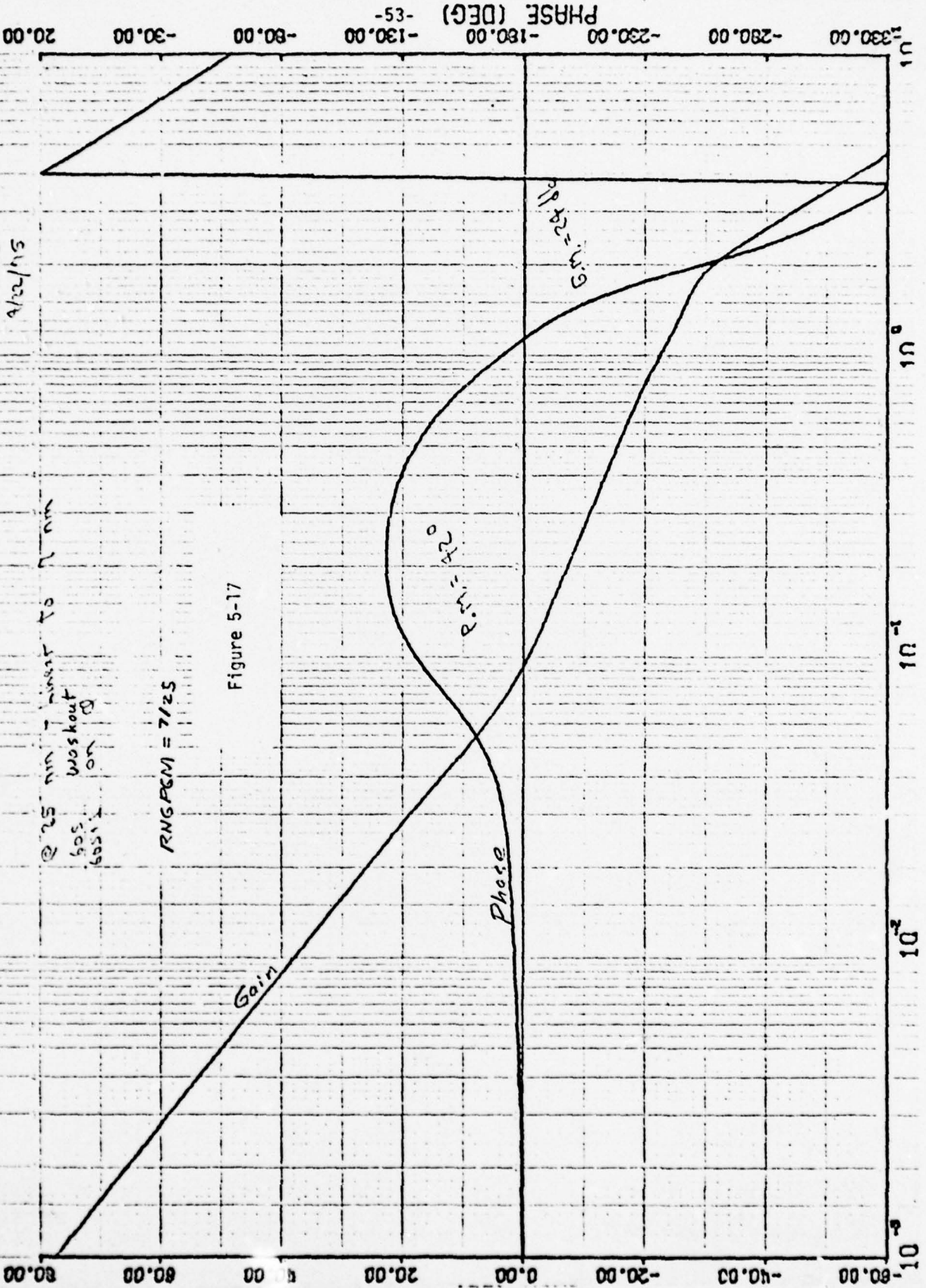
RNG PCM = 7125

Gain

Phase

Figure 5-17

CA 136
9/25/45



PHASE (DEG)

80.00 60.00 40.00 20.00 0.00 -20.00 -40.00 -60.00 -80.00 -100.00 -120.00 -140.00 -160.00 -180.00 -200.00 -220.00 -240.00 -260.00 -280.00 -300.00

10⁻³ 10⁻² 10⁻¹ 10⁰ 10¹

6.1 INTRODUCTION

The glideslope portion of the ILS approach control laws are presented by this report. The control laws provide for a smooth, transientless capture of the glideslope beam. The control laws will automatically adapt for varying airspeed, wind and beam angles. In addition, both above and below the beam intercepts can be accommodated.

The control laws developed rely upon derived vertical rate to enhance the adaptive capture capabilities and to supplement basic autopilot and flight director path dampening and gust alleviation. The autopilot and flight director both accept pitch commands from the glideslope control laws in the 3D/4D processor to an altitude hold port. Once attitude is closed in a glideslope control loop, it has been found that vertical rate is of some benefit for gust alleviation, but it cannot be used to its fullest advantage. The control laws, therefore, have some advantages over conventional pitch implemented controls while exhibiting similar tracking performance.

A description of the glideslope computations, stability and performance analyses are contained herein. The glideslope control laws digital program listing is contained in Appendix G.

6.2 GLIDESLOPE OPERATION AND DESCRIPTION

Glideslope control laws are provided for vertical navigation of an RNAV/ILS approach capability. An adaptive capture capability has been designed into the glideslope control laws. The control laws are illustrated in Figure 6-1.

Glideslope operation is performed with the 3D/4D system just as is done with any conventional flight guidance computer. Basically glideslope capture is initiated from a flight path which has been set up to intercept the glideslope beam. Most often the glideslope is intercepted from a zero

flight path angle or altitude hold maneuver. Unlike some glideslope operations the control laws in the 3D/4D system will also allow the user to capture from above.

Operationally, glideslope capture and tracking can be accomplished in the approach auto mode (APPR AUTO) of the ILS portion of the 3D/4D system. Once an intercept has been established so that the aircraft will intercept the glideslope beam, capture is completely automatic. The system compares beam and vertical rates with beam deviation and polarity to establish a capture trip point. Figure 6-1 also includes the capture logic which dictates when capture occurs. When pitch command is sensed to go through zero in the correct direction as determined by comparing its polarity with that of beam deviation, capture is initiated.

Since the capture is a function of both beam closure rate and vertical rate, capture is a function of ground speed and flight path angle. Ground speed in turn makes the capture a function of aircraft speed and wind. If a capture is initiated from altitude hold, the capture trip point will vary as a function of how fast the glideslope beam is approached. The trip point will move further from the glideslope beam center as the closure rate increases no matter what reason. Similarly, if the aircraft has a vertical rate established, capture will be adjusted to compensate for the vertical rate. As an example, when capturing from above, capture will be initiated further from the glideslope for a greater vertical rate or flight path intercept. Of course, beam rate alone can also sense this higher closure rate, but the addition of vertical rate has proved to be more accurate in adjusting the trip point especially in above the beam captures.

Once capture has been initiated, the beam rate is held by a track/store operation. Also notice that at the instant of capture a fader or washout is initiated on both stored beam rate and vertical rate. The action is such that at the instant of capture, pitch command is zero, and the aircraft proceeds toward the glideslope beam. Deviation therefore decreases while the rate signals (which are being slowly faded out) provide a nose up or nose down pitch command, whichever is appropriate to transition the aircraft to the glideslope path. The fader washes out all of the beam rate and initial vertical rate as the aircraft acquires the beam centerline. In this manner the control laws smoothly and transientlessly transition the aircraft from its intercept flight path to the beam center.

After capture, tracking is provided by glideslope deviation and washed out vertical rate. The capture bias provided by the stored beam rate is completely removed. Vertical rate is washed out to prevent the vertical rate or descent rate from causing a deviation standoff in the control laws.

The control laws developed for the 3D/4D use vertical rate to good advantage as was explained in the introduction. It should also be pointed out that for autopilot operation, vertical rate is required to dampen the deviation path. Pitch attitude used for deviation path dampening in the autopilot is washed out (by the 5 sec forward integration) faster than can normally be done to provide stability with stiff glideslope tracking.

A breakdown of the glideslope operation and details is given below:

6.2.1 Overview of Glideslope Operation

The glideslope computation may be entered via a transition from the LOC or the RNAV mode. The RNAV computation will request the ILS main program to perform this transition. If all system validities are acceptable, the ILS main program will activate the localizer and glideslope computations. Each time a transition is requested, the ILS main program will initialize the glideslope computation by setting the logical variable RESETG true for one program cycle.

As long as the localizer computation is in the LOCARM condition, the RNAV steering commands are used to control both the lateral and longitudinal axes. The transition to LOCCAP terminates RNAV control of the lateral steering commands only. ILS control of longitudinal steering command will occur when the glideslope capture mode is entered (GSCAP) subsequent to LOCCAP. However, deactivation of the ILS computation, after LOCCAP, can only be achieved by disengaging the autopilot and reselecting the RNAV mode. Re-entry of the ILS computation is possible and will be treated as an initial request by the ILS main program.

6.2.2 Glideslope Arm (GSARM) Logic

The glideslope control law will be set to the GSARM mode whenever the logic signal RESETG from the ILS main program is true. The computation will remain in this mode as long as the localizer computation is in the arm condition (LOCARM). While in this mode, the computation will estimate the distance to and the approach rate of the glideslope beam. Following LOCCAP that information will be used to select an appropriate point to transition into the capture mode (GSCAP). The transition will occur at the first opportunity following the termination of LOCARM and prior to the intercept of the glideslope.

6.2.3 Glideslope Arm Computation

While in the arm mode, external steering commands are passed directly through the computation without modification. The radio deviation is passed through a gain programmer to estimate linear distance to the glideslope. A rate deriver estimates the approach rate of the glideslope and these two signals are combined with derived barometric altitude rate to generate a pitch command. That command signal is routed to the capture logic rather than the steering command.

6.2.4 Glideslope Capture Logic

Assuming the localizer computation is not in the arm mode and the aircraft is on a course which will at some future time intersect the glideslope, radio deviation will establish the major portion of the pitch command and the rate signal will contribute a portion in opposition to the radio signal. As the glideslope is approached the closure rate will cancel and then exceed the radio signal. When this occurs the pitch command will initially be zero and then of a polarity which directs a flight path away from the

glideslope beam. The capture detector monitors the localizer computation status, the polarity of radio deviation and that of the pitch command. When the condition described above exists, the glideslope computation is switched to the capture mode. Once this mode is enabled the computations are latched in that mode. The GSARM mode can only be reinitiated by the RESETG command generated in the ILS main program. While in the GSCAP mode the VOR/DME/baro altitude based RNAV steering command will be overwritten by the computed pitch command.

Derived barometric rate is used in the capture logic to sense glideslope intercepts from other than a zero flight path. This enables captures to be made from all practical intercept angles, including above the beam captures.

6.2.5 Glideslope Capture and Track Computations

Figure G-1 also identifies the capture computations. There are two major functions performed by this control law: (1) generate a pitch command which will provide good capture and tracking of the glideslope beam and (2) smoothly transition from external (RNAV) control of the steering command. The first task is accomplished by mixing radio deviation with barometric altitude rate to obtain a pitch command. The radio deviation is gain programmed, and altitude rate is washed out to remove its steady state value. Derived radio rate is held to the value it has when the capture mode is enabled, and since this signal enters pitch command via the same path as altitude rate, it will be smoothly removed by the same washout used to eliminate the steady state value of altitude rate. Notice that the washout is utilized only after capture. The value of the external steering command, at the time of transition to GSCAP, is added to the computed pitch command via a washout. Since pitch command is effectively zero at that time, overwriting the steering command will not cause an unacceptable transient while the previously coupled command is faded out.

6.3. Control Law Analysis

Control law analysis was performed on the system shown in Figure G-1. Included in the figure is a model of the autopilot. The autopilot model was derived from time response data taken on the NAFEC Gulfstream I aircraft. The gains and time constants were selected to match the following data parameters for a step command:

- a) Time to peak: .42 sec.
- b) Settling time: .92 sec.
- c) Overshoot: 30%
- d) Forward Gain: 4 deg δ e/deg θ
- e) Integration Rate: 1.5° δ e/sec.

The only modification was a 4:1 reduction in forward gain. The probable cause of this change is an invalid elevator sensitivity in the aerodynamic data available at Collins.

Figure 6-2 illustrates the manual throttle control loop. The model has shown good correlation with manual pilot performance.

6.3.1 Radio Gain Programmer

The gain programmer converts radio deviation (214 $\mu\text{a}/\text{deg}$) to linear feet of cross track distance (.496 $\text{ft}/\mu\text{a}\text{-nm}$) out to 5.58 nm from the end of the runway. Beyond this point cross track distance is fixed at 2.8 $\text{ft}/\mu\text{a}$. To extend the range of the programmer beyond this point would invariably result in unacceptable performance due to beam noise. Assuming a shallow 2.5 degree glideslope, the programmer will be effective to an altitude of 1,480 ft. Consequently, normal captures will be performed within the linear range of the programmer. The programmer is a function of distance to touchdown rather than altitude.

6.3.2 Capture Detection

Although it is certainly possible to initiate a capture outside the linear range of the gain programmer, the effect of the non-linearity on the capture detector is marginal and the following discussion will therefore be presented assuming linear programmer range. Referring to figure 6-1, an internal pitch command is formed when the glide-slope computation is in the arm condition (GSARM). The value of that signal will be

$$\theta = K_h (K_{\Delta h} \Delta h + \dot{h}) + K_h \Delta h \quad \text{Eq. 6-1}$$

where

θ = degrees of pitch command (+ directs a pitch down attitude)

Δh = approach rate of the glideslope beam (ft/sec)

\dot{h} = ascent rate (ft/sec)

Δh = cross track distance (ft), positive above the glideslope

Any flight path intersecting or almost paralleling the glideslope will result in the rate terms having a polarity opposite to that of Δh . When the rate term equals or exceeds the position term, the glideslope capture mode will be enabled (GSCAP). Two conditions exist which will result in a missed capture: (1) transversal of the capture window while LOCARM is active, and (2) a flight path paralleling the glideslope which never established sufficient proximity and/or closure rate to intersect the capture window.

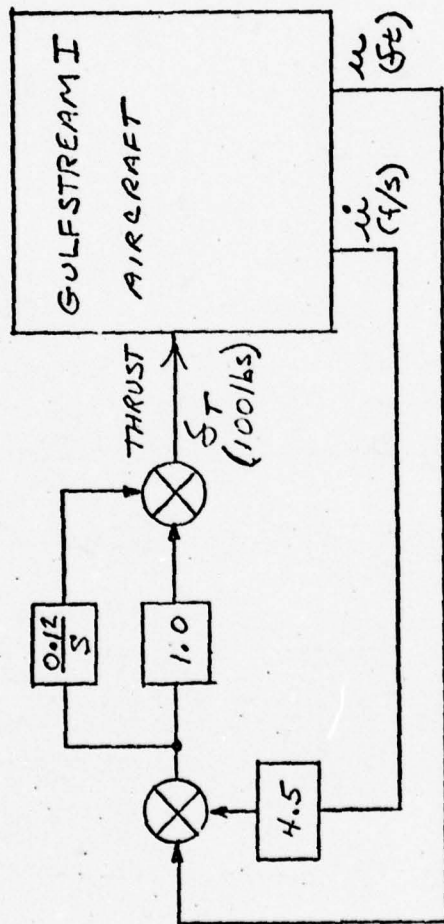


Figure 6-2. AIRSPEED LOOP TO SIMULATE
MANUAL PILOT AIRSPEED
CONTROL

Figure 6-2.

The glideslope capture window may be more clearly defined by expressing the rate terms as functions of flight path angle:

$$\dot{h} = U_0 \sin(a)$$

$$\dot{\Delta h} = U_0 \sin(a - a_g)$$

where

U_0 = true airspeed

a = flight path angle measured as positive counterclockwise from horizontal

a_g = glideslope angle (nominally -2.5 deg.)

Substituting those expressions into equation 6-1 and setting $\theta=0$ yields the crosstrack distance at capture as a function of flight path angle:

$$\Delta h_c = -\frac{K_h^i}{K_h} U_0 [K_{\Delta h}^i \sin(a - a_g) + \sin a] \quad \text{Eq. 6-2}$$

where

$$K_h^i = .15 \text{ deg}/(\text{ft}/\text{sec})$$

$$K_h = .05 \text{ deg}/\text{ft}$$

$$K_{\Delta h}^i = 2.22 (\text{ft}/\text{sec})/(\text{ft}/\text{sec})$$

$$U_0 = 200 \text{ ft}/\text{sec}$$

$$a_g = -2.5 \text{ deg.}$$

then

$$\Delta h = -(33.8a + 58.2) \quad \text{Eq. 6-3}$$

Equation 6-3 assumes the flight path angle relative to both the glideslope and the horizontal reference line is small enough to allow the substitution of $\sin(x)=x$. The mode logic tests the polarity of equation 6-1 against that of Δh , i.e. if $(\text{sgn } x) \neq (\text{sgn } \Delta h)$ then capture is initiated. Therefore, the capture window is defined as:

$$0 < \Delta h < -\frac{K_h^i}{K_h} U_0 [K_{\Delta h}^i \sin(a - a_g) + \sin a]$$

$$0 > \Delta h > -\frac{K_h^i}{K_h} U_0 [K_{\Delta h}^i \sin(a - a_g) + \sin a]$$

Figure G-3 graphically presents the glideslope capture window obtained via equation 6-2. Capture will occur when (1) the aircraft is below the beam and the flight path angle is on or above the line described by equation 6-2, or (2) the aircraft is above the beam and the flight path angle is below the line described by equation 6-2.

Five capture boundary lines are shown to illustrate the effect of longitudinal wind and varying glideslope angles.

Clearly, an RNAV approach paralleling the glideslope must, at some point, close to within 58 feet of the glideslope. Since RNAV errors of 150 feet are not out of the question, there is a possibility of missing the glideslope if capture is attempted with R-NAV assist. However, random variations in the beam as well as the aircraft position will normally result in a capture. A more probable cause of missed capture would be a close-in approach which resulted in a flight path angle in the -1.0 to $-.2$ degree range. Here, the capture window can become quite small. Similar arguments apply to captures from below the beam. Although it would be possible to modify the capture laws to encompass parallel RNAV approach configurations additional development will be required.

Since the capture window is actually determined by measured position and rate information, the capture point will be moved to compensate for along track and cross track wind conditions as well as variations in glideslope angle. Simulation data included in this report demonstrate the use of capture point movement to maintain a relatively smooth performance during the capture maneuver. Estimates of distance to and closure rate of the beam in equation 6-3 compensate for environmental variations but cannot distinguish between ascending, descending, or constant altitude capture conditions. The altitude rate term does provide this information and is used to extend the capture point thereby suppressing excessive vertical rates. Examination of simulated captures from above the beam shows the complete absence of overshoot under these conditions.

Table 6-1 summarizes data for simulated approaches. The intercept point is defined as the beam altitude at the intersection of the glideslope and the flight path prior to capture. The approaches were simulated to evaluate system performance capturing and tracking the glideslope.

Figure 6-3
Capture Boundary

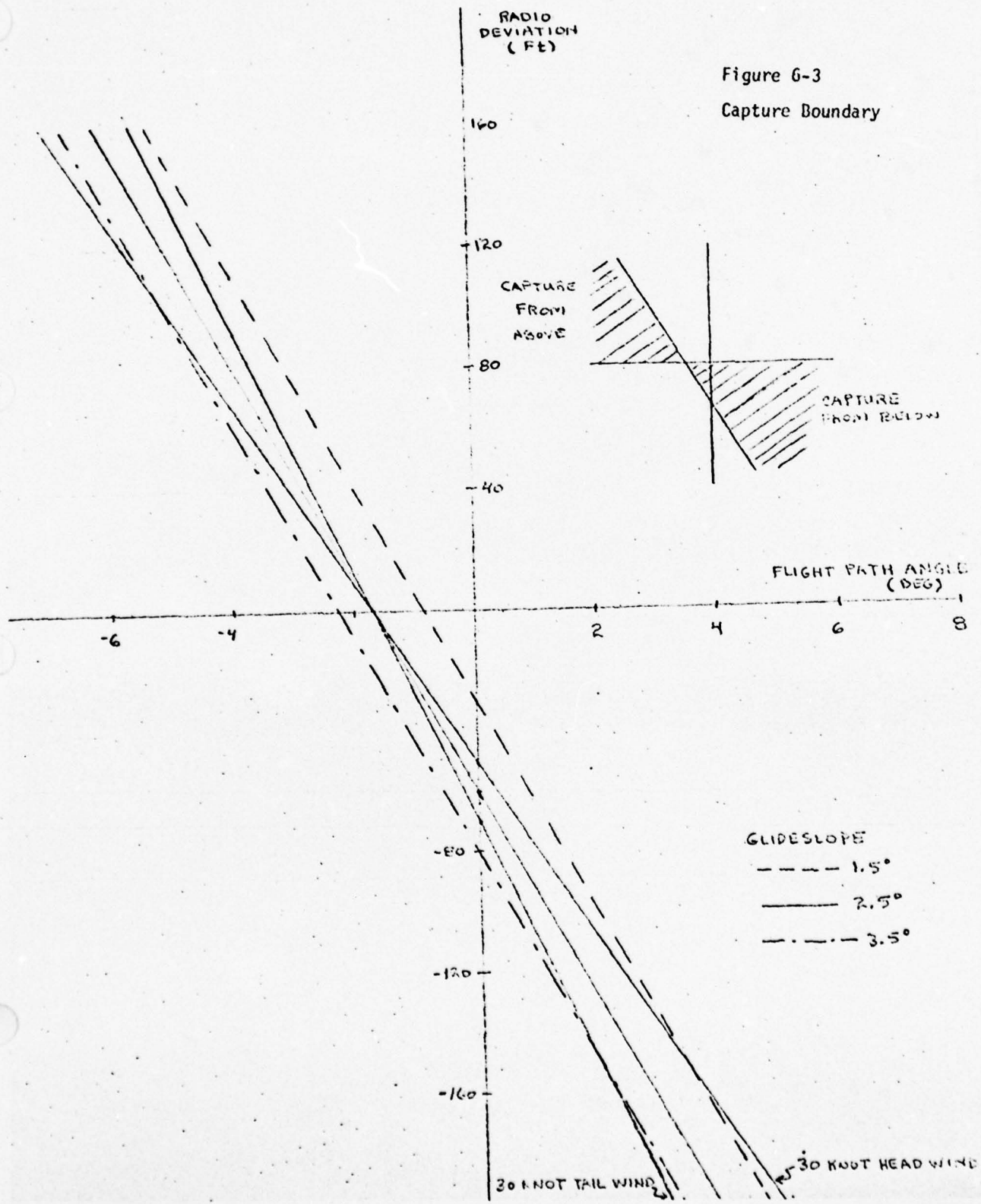


Table 6-1. Simulated Capture Data

Intercept Point (ft)	Flight Path Angle (deg)	Capture Point (ft)	Predicted Value (ft)	Overshoot (ft)	Settling Time (sec)	Strip Chart
1000	0	-50	-58.2	--	8	1A
1000 (From above)	-5	+125	+132	--	45	1B
1300	0	-50	-58.2	--	10	1C
1300 (From above)	-5	+125	+132	--	45	1D
1500	0	-54	>- 58.2	6	20	1E
1800	0	-58	>- 58.2	12	28	2C
1800 (From above)	-5	+90	<132	--	55	2D

As would be expected the data confirms anticipated results. Along with the previously mentioned adaptive behavior, the gain programmer is seen to reduce the capture window as distance to touchdown increases. This is the only non-linear effect in the capture maneuver.

Analog computer simulation results are somewhat different than the predicted values due to a dead zone in the analog capture logic. The predicted values were attained when simulations were performed using the digital version of the control laws.

6.3.3 Stability Margin Analysis

To analyze the stability of the glideslope control laws of Figure 6-1 frequency response or Bode plots were obtained. Reference to Autothrottles in this discussion is to Figure 6-2. Figure 6-4 is an open loop bode plot of the radio or deviation loop. This plot indicates the stability of the aircraft when tracking the glideslope beam. Autothrottles were also used for Figure 6-4. The aircraft used to obtain this plot was the Gulfstream I approach flight condition (200 ft/sec airspeed). From Figure 6-4 it can be seen that the bandwidth is sufficient to achieve good Category II tracking performance. The stability margins as summarized in Table 6-2 indicate good stability for the glideslope maneuver.

Figure 6-5 illustrates the outer loop or deviation loop broken as in

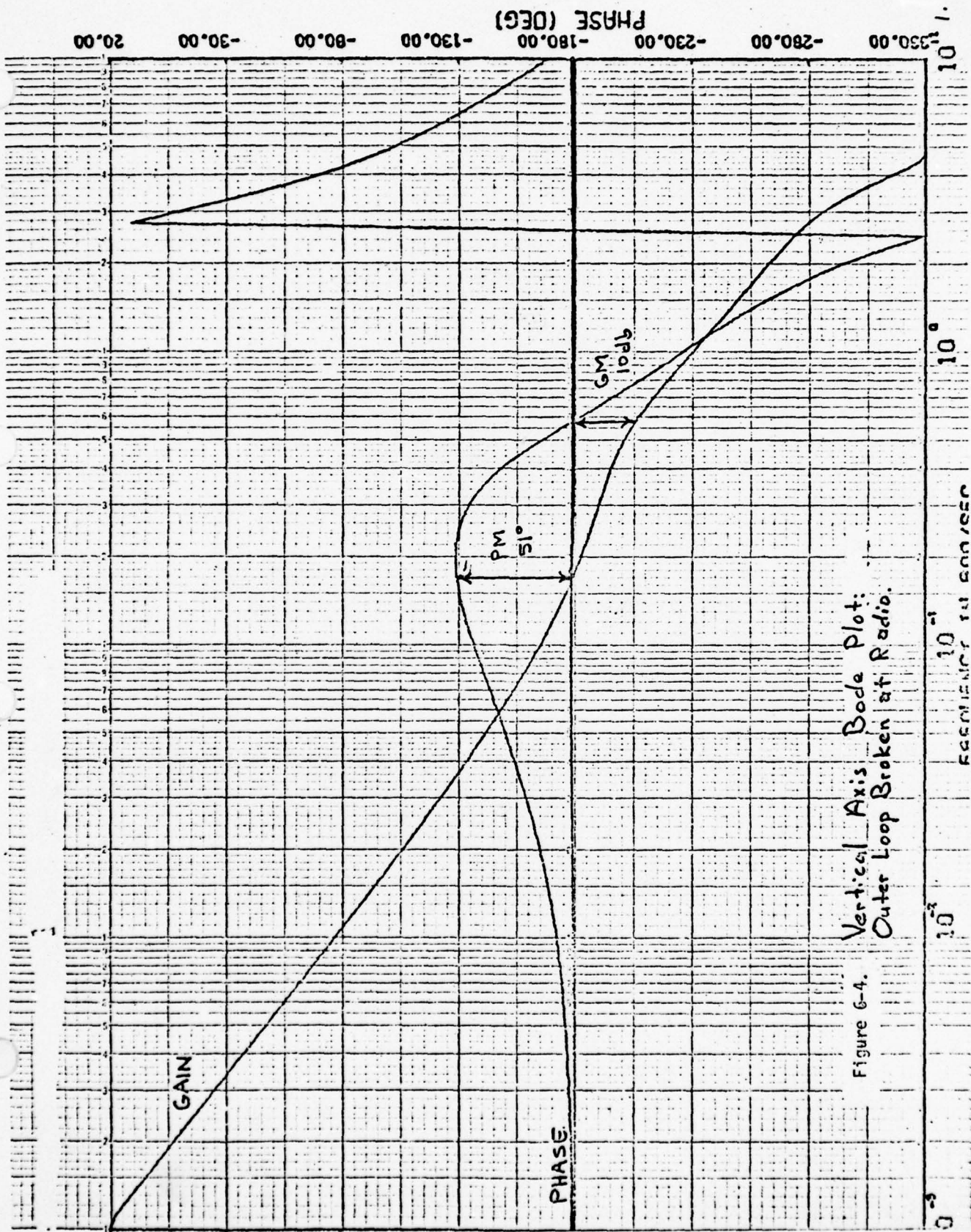


Figure 6-4. Vertical Axis Bode Plot:
Outer Loop Broken at Radio.

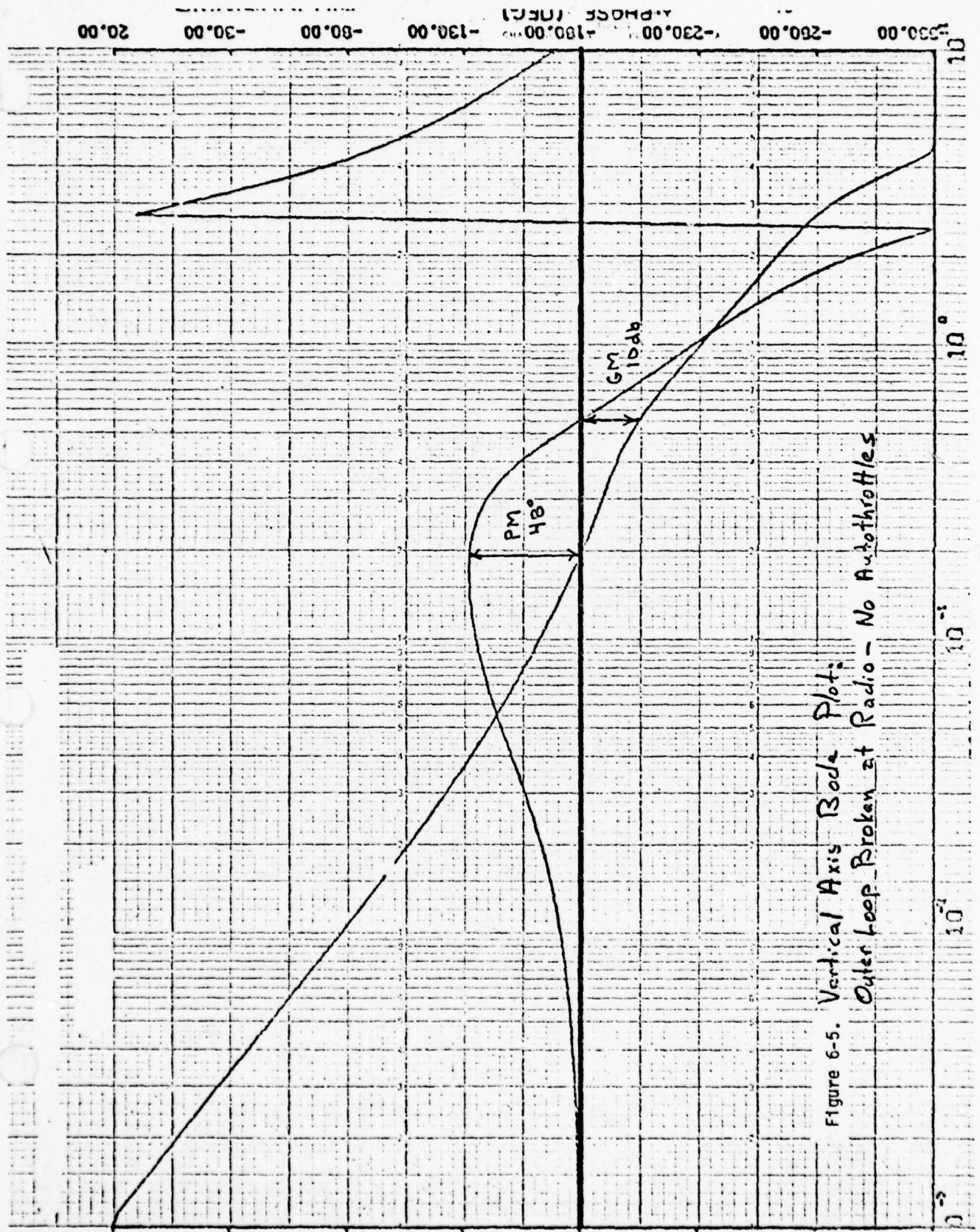


Figure 6-4, but the autothrottles were removed. As can be seen by comparing the two figures, airspeed control does not greatly effect glideslope tracking stability.

Figure 6-6 is a bode plot of the control laws of Figure 6-1 broken in the inner loop or at the servo. All outer loops are closed. This plot is indicative of the inner loop or elevator activity and stability while the system is tracking the glideslope. The bandwidth and stability indicated by Figure 6-6 is typical of good Category II glideslope computations. The stability margins and bandwidth are summarized in Table 6-2. Figure 6-7 is the same as Figure 6-6 except for the lack of autothrottles. As can be seen airspeed control does not effect the inner loop stability or bandwidth to any great extent.

Table 6-2. Frequency Response Data

FIGURE	GAIN MARGIN (db)	PHASE MARGIN (deg)	BANDWIDTH (rad)	OPENED LOOP	CONFIGURATION
6-4	10	51	.175	Radio	Autothrottles
6-5	10	48	.2	Radio	No autothrottles
6-6	10	75	.7	Servo	Autothrottles
6-7	10	75	.7	Servo	No autothrottles

OMNIGRAPHIC
PHASE (DEG)
-330.00 -280.00 -230.00 -180.00 -130.00 -80.00 -30.00 00.00

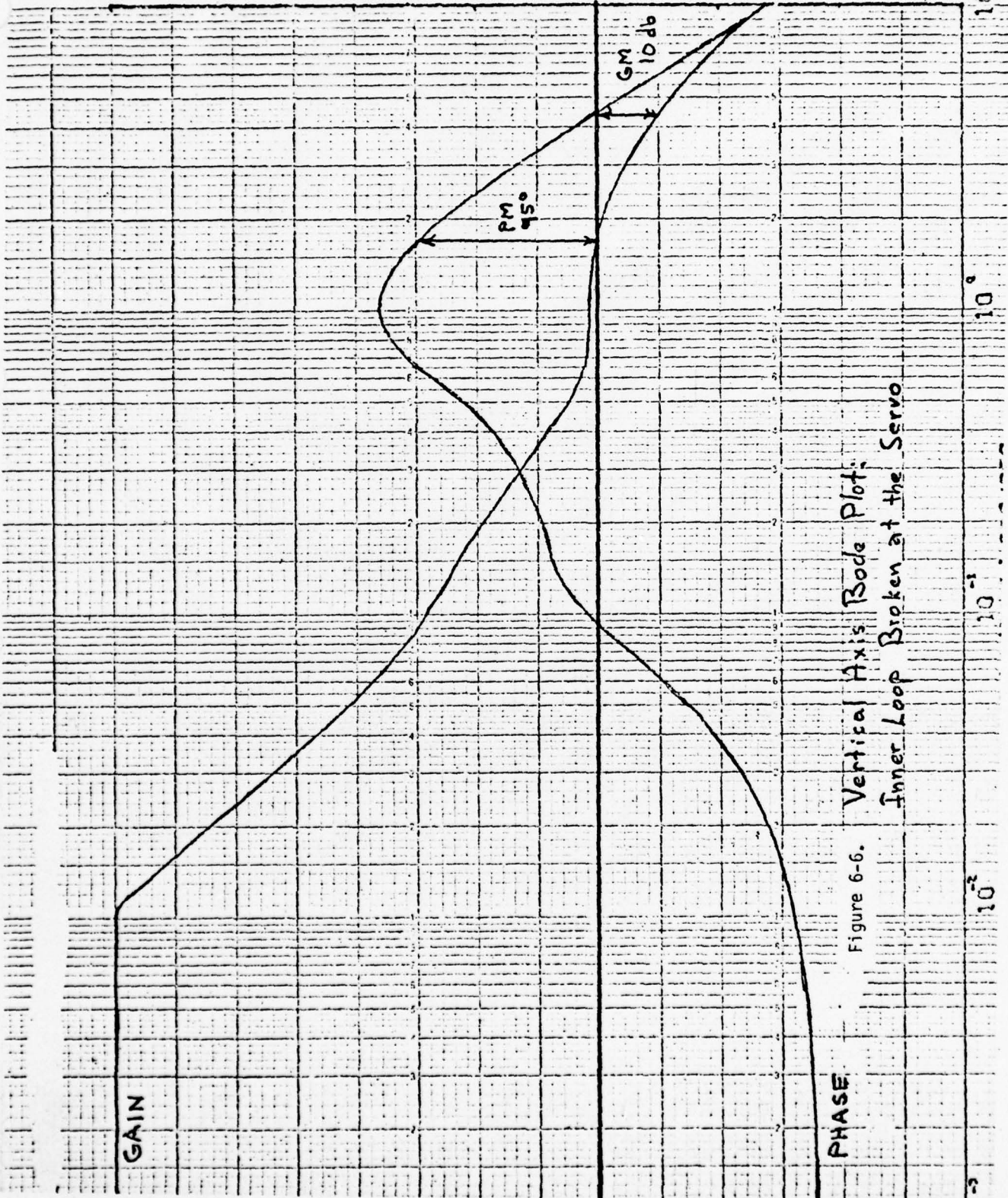


Figure 6-6. Vertical Axis Bode Plot;
Inner Loop Broken at the Servo

10⁻³ 10⁻¹ 10¹ 10³

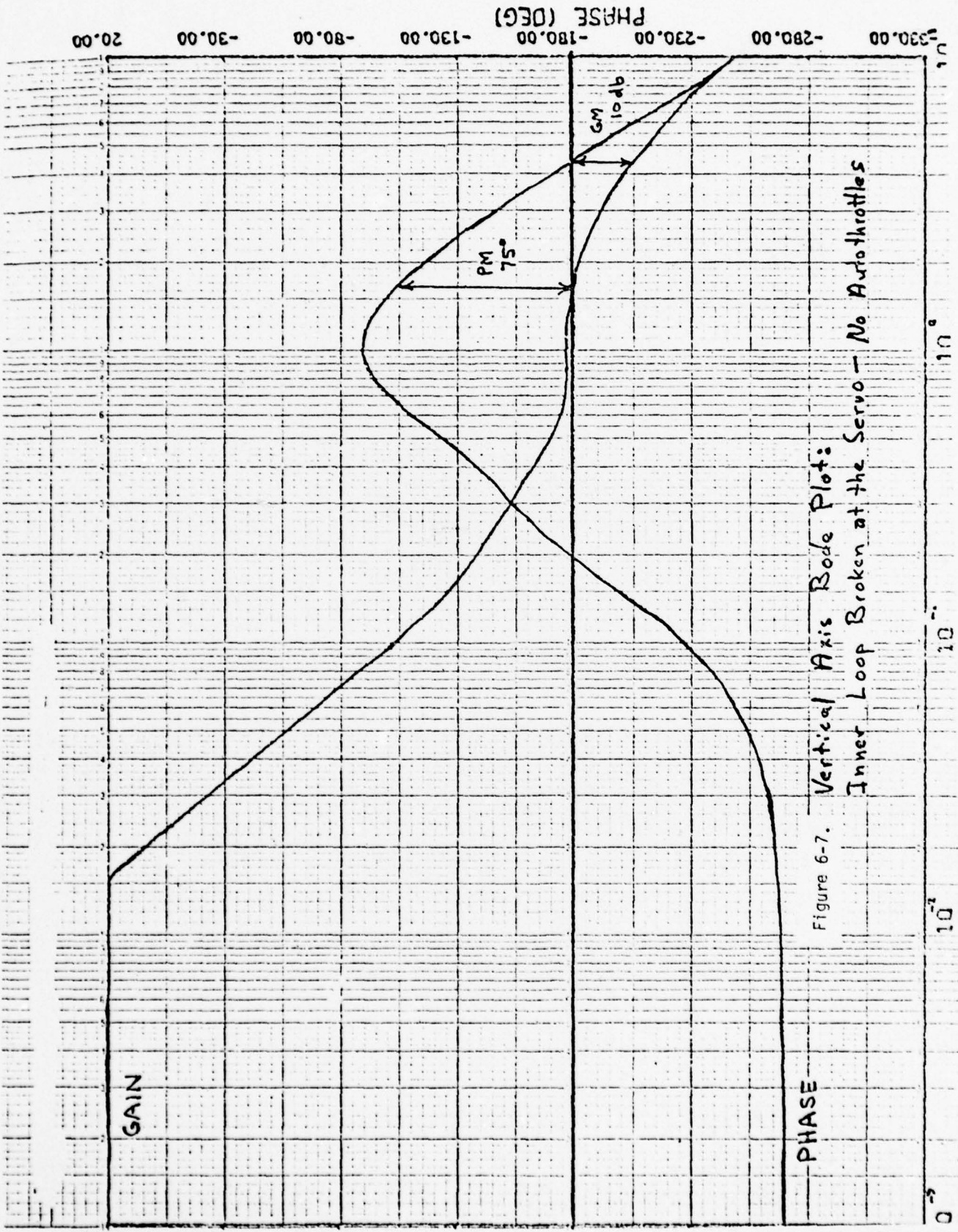


Figure 6-7. Vertical Axis Bode Plot:
Inner Loop Broken at the Servo - No Autothrottles

6.4 Performance

To evaluate the performance of the glideslope computations, the system was simulated on the EAI 680. The system of Figure 6-1 was used with a simulation of the Gulfstream I aircraft (approach flight condition). To simulate manual airspeed control, the autothrottle system shown in Figure 6-2 was used. The autothrottle system was adjusted to give airspeed control similar to what is known to be typical of manual operation. Strip chart recordings were taken using radio noise, vertical wind turbulence, longitudinal wind turbulence and radio steps.

6.4.1 Radio Steps

Strip chart recordings were taken for step changes in glideslope. These recordings illustrated the stability of the glideslope computations when tracking the glideslope beam. The glideslope tracking performance had sufficient stability and bandwidth. The responses were smooth and well damped.

6.4.2 Vertical Turbulence

The following represents the 2σ vertical turbulence transfer function (ref. 5) used for the performance simulation.

$$\text{white noise} \quad \boxed{\frac{K}{1+(L/V)S}} \quad \text{-- } \sigma\sigma$$

where

S = complex variable of Laplacian operator
V = approach speed (200 ft/sec)
L = vertical scale length (30 ft.)
 $\sigma\sigma$ = 1.3 deg RMS (2σ level)

It should be strongly pointed out that the RMS level of vertical turbulence represents a 2σ value. In other words, this level of turbulence would be expected on only 5% of the approaches if a random selection were made over a total every day operation.

For the assumed flight condition this model corresponds to .15 sec. correlated noise, and RMS output value of 1.3 degrees was used in the simulation effort. At an airspeed of 200 ft/sec this is equivalent to 5.6 ft/sec (RMS) vertical gusts. System response to wind gusts at fixed distances from the runway is summarized in Table 6-3.

Table 6-3. System Deviations to Vertical Gusts

Gust Strength (deg) RMS	Distance (nm)	Airspeed (f/s) RMS	Pitch (deg) RMS	Pitch Command RMS	Deviation (ft) RMS	Altitude Rate (f/s) RMS	Servo Command (deg) RMS
1.3	7.46	.12	.183	.233	4	1.75	.24
	6	.12	.267	.267	6.67	2.167	.316
	4.54*	.12	.2	.267	4	1.67	.267
	5.7-2.2*	.12	.2	.3	4.53	2.	.3

*typical of performance in the linear range of the radio programmer

The performance exhibited indicates no problem. Performance capable of Cat. II performance has been achieved. Servo or control activity as can be seen from Table 6-3 is satisfactory.

6.4.3 Longitudinal Gust Performance

As was the case for vertical gusts, Reference 5 provided the following 2σ longitudinal gust transfer function:

$$\text{white noise} \left[\frac{K}{1+(L/V)S} \right] \mu g$$

where

- S = complex variable of Laplacian operator
- L = longitudinal scale length (600 ft)
- V = approach speed (200 f/sec)
- μg = 6 ft/sec RMS (2σ level)

An RMS output of 6 ft/sec was employed during simulated approaches. Again data runs were made at fixed distances inside, outside, and at altitudes corresponding to the knee of the radio gain programmer. Table 6-4 summarizes the data recorded.

Table 6-4. System Deviations to Longitudinal Gusts

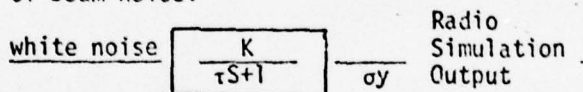
Gust Strength (f/s) RMS	Airspeed (ft/sec) RMS	Pitch (deg) RMS	Pitch Command (deg) RMS	Deviation (ft) RMS	Altitude Rate (f/s) RMS	Servo Command (deg) RMS	Distance (nm)
6.	1.5	.266	.88	5.33	2.0	.267	4.36
	1.5	.317	.567	12.0	2.83	.383	6.0
	1.67	.383	.767	13.3	3.75	.333	7.64
	1.625	.3	.567	7.65	2.75	.333	3.2-.377

*typical approach condition

From Table 6-4 it can be seen that the system tracks the glideslope beam quite well during the longitudinal turbulence. Cat. II performance is achieved. Servo or control activity is indicative of that known acceptable from past experience on other systems.

6.4.4 Radio Noise Performance

The following noise model was used to estimate system performance in the presence of beam noise:



where

S = complex variable of Laplacian operator

τ = 4 sec.

σ_y = 10 μ a RMS

This model is considered a low quality Cat. I facility.

Table 6-5 summarizes the performance from some of the recordings for various distances. Table 6-5 illustrates that Cat. II performance is achieved and servo or control activity is not excessive.

Table 6-5. System Deviations to Radio Noise

Radio Noise (ua)	Distance (nm)	Airspeed (ft/sec) RMS	Pitch (deg) RMS	Pitch Command (deg) RMS	Deviation (ft) RMS	Altitude Rate (ft/sec)	Servo Command (deg) RMS
(12.5 ft) 3.35	7.46	.12	.18	.35	8.0	1.25	.167
(10.65 ft) 3.55	6.0	.117	.25	.434	6.67	1.5	.217
(7.85 ft) 3.45	4.54	.117	.183	.33	7.35	1.25	.125

6.5 CONCLUSION

Simulation and analysis results indicate category II performance can be expected from these glideslope control laws. In addition, these control laws have been shown to be capable of acceptable performance when glideslope captures are initiated from other than an altitude hold mode. This capability may be considered a first step to area navigation aided vertical approach maneuvers.

APPENDIX A

Program Listing of the Flight Plan

Editor Utility Module


```
57 PRESET EVENT=03FFFFFFF1
58 ***** PROCEDURE DECLARATIONS *****
59 POINTER PROCEDURE
60 MASSACHU ***** RMS SEARCH ROUTINE //
61 PROCEDURE
62 ***** CLEAR ALL OFFSETS //
63 ***** ZERO ***** //
64 ***** ZERO ***** //
65 ***** COPY RTN ***** //
66 REAL PROCEDURE
67 SIGN ***** SIGN OF REAL NUMBER *****
68 ***** EXTERNAL DECLARATIONS *****
69 EXTERNAL
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114 PROGRAM START
115 ... LAD OWN REGISTER
116 ... CHECK VERSION NUMBER//
117 ... CHECK VERSION MISMATCH//
118 ... REPORT NO VERSION //
119 GOTO RETURN
120 FIND
121 ***** VERSION MISMATCH*****
122 ... INHIBIT ACCESS TO FET //
123 ... MAKE START OF DELETE PTR //
124 ... MAKE STOP OF DELETE PTR //
125 ... CHECK RAS FOR ROOM //
126 ... CALL CHARGE RAS OVERFLOW//
127 ... A ONE-FOR-ONE REPLACE IS
128 ... A SPECIAL CASE WHERE ONE
129 ... LATERAL EVENT IS
130 ... OVERRITTEN BY ANOTHER. A
131 ... ONE-FOR-ONE REPLACE
132 ... REQUIRES THE FOLLOWING
133 ... 1. EVENTS MUST BE
134 ... LATERAL EVENTS
135 ... 2. ONE ITEM MUST BE
136 ... DELETED
137 ... 3. ONE ITEM MUST BE
138 ... ADDED
139 ... 4. ID'S MUST MATCH //
140 ... MUST BE LATERAL EVENT //
141 ... ***** LATERAL EVENT *****//
142 ... IUS MUST MATCH //
143 ... DELETE 1 ITEM //
144 ... ADD 1 ITEM //
145 ... ***** ONE-FOR-ONE REPLACE//
146 ... OVERRITT LATERAL EVENT //
147 ... FAX FOR ADJUSTING //
148 ... GO FIXUP FET AND RETURN //
149 ... ***** ONE-FOR-ONE REPLACE//
150 ... ***** LATERAL EVENT *****//
151 ... THE FLIGHT PLAN EDITOR
152 ... MUST INSURE THAT
153 ... SUFFICIENT ROOM EXISTS IN
154 ... THE FET FOR THE NEW ITEMS
155 ... PRIOR TO MAKING ANY FIXES
156 ... TO THE FET //
157 ... ROOM MADE BY DELETE PLUS //
158 ... UNUSED FET IS COMPARED //
159 ... WITH MAX SIZE OF INSERT //
160 ... ***** NO ROOM ***** //
161 NO ROOM:
162 ... REPLACE OLD VERSION NUM // 00000282
163 ... REPORT NO ROOM // 00000283
164 GOTO RETURN
165 FIND
166 ***** NO ROOM ***** //
167 ... DELETE ALL ITEMS FROM
168 ... STRVNO TO STOPVNO
169 ... INCLUSIVE. DELETE CONSISTS
170 ... OF OVERRITTING SPECIFIED
    
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171 ... NEW ITEMS ARE ADDED USING
172 THE ROUTINE ADDSTR.
173 PATER THAN ADDATE SO
174 THAT VERSFL CAN BE
175 INDEPENDENTLY CONTROLLED
176 BY BOTH REPLACE AND
177 ADDATE
178 ... OVERWRITE REPLACED EVENTS //
179
180 GOODRTN:
181 ACDSRNG(PNTR,ITEM,NO,PROC,WKPTR) ... ADD NEW EVENTS //
182 ... FIXFLT WILL VALIDATE ALL
183 RMS ITEMS, CALCULATE DFTG
184 FOR ALL ITEMS AND
185 CALCULATE FLIGHT PARAMS
186 IN NEIGHBORHOOD OF NEW
187 ITEMS
188 FIXFLT(STOP,NOITEMS) //
189 VERSFL=SVRSFL+1 //
190 REPLACE = GORTN //
191 GOTO RETURN //
192 END
193
194 ... ***** PROC REPLACE *****//
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228 ... THE FLIGHT PLAN EDITOR
229 MUST INSURE THAT THERE IS
230 ADEQUATE ROOM FOR THE
231 ITEMS TO BE ADDED PRIOR
232 TO CHANGING THE FET
233 //
234 // ... CHECK RMS
235 // ... NO KUCH
236 // ... REPORT NO HOW
237
238 ***** NO ROOM *****
239 //
240 // INSURE LGCT EVENT NUMBER//
241 // ***** HAN EVENT NUM *****//
242 // ... REPORT NO SUCH EVENT //
243
244 ***** DAN EVENT NUM *****//
245 //
246 // INHIBIT FET //
247 // ... CONSTRUCT ITEM POINTER //
248
249 // ***** OVRWRITE ORIGIN *****//
250 // ... DELTE ORG //
251 // ... SHOW P-PSH INVALID //
252 // ***** OVRWRITE ORIGIN *****//
253 // ... ADD LE & EGC BEFORE //
254 // ... AT-PTR, AID OTHERS //
255 // ... AFTER AT-PTR //
256 // ... NEW ITEMS ARE ADDED USING
257 // THE ROUTINE ADJUSTING
258 // RATHER THAN DIRECTLY SO
259 // THAT VESSEL CAN BE
260 // CONTROLLED INDEPENDENTLY
261 // BY ADDATEL AND REPLACE //
262 // ... ADD ITEMS. //
263 // ... FIXFLT WILL VALIDATE ALL
264 // RMS ITEMS, CALCULATE NETO
265 // FLIGHT PARAMS IN
266 // NEIGHBORHOOD OF NEW ITEMS//
267 // ... FIX FET & RMS //
268 // ... RUMP VESSEL NUMBER //
269 // ... REPORT GOOD RETURN //
270 //
271 // ... ***** PRCC ADDATE *****//
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273 .....
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285 DEFINE PROCEDURE ADDSTRNG(IAT,PNT1,NOITEMS,PROC,WKPTR)
286   WHERE POINTER AT,PNT1
287   INTEGER NOITEMS
288   POINTER PROCEDURE PROC
289   POINTER WKPTR TOBE
290
291   BEGIN
292   OWN POINTER FETCH
293   OWN POINTER PNT1
294   OWN POINTER PNT2
295   OWN POINTER FRMLV1
296   OWN POINTER FRMLV2
297   OWN POINTER ADD,PTR
298   OWN INTEGER ITEMS
299   OWN INTEGER TYPE1
300   PNT1 <<= PNT1
301   PNT2 <<= FRMLV1
302   FETCH $<< FRMLV1
303
304   FETCH=LOC PROC
305   ADD,PTR=AT,PNT1
306   ITEMS=NOITEMS
307
308   NEXT,ITM: IF FETCH NEG NULL AND
309   ITEMS NEG 0
310   THEN BEGIN
311   ITEMS=ITEMS+1
312   FETM=POIT(FETCH,WKPTR)
313   ...
314   ...
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342 AND 'TO' EVENTS ARE
343 DEFINED. THE START OF THE
344 FLT IS FOUND. EVENT
345 NUMBER 1 IS FOUND
346 FIRST, MARK TOEVE & FRREV//
347 ... INVALID ON ALL ITEMS. //
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THIS ROUTINE SEARCHES THE RWS COUNTING EMPTY ITEMS. IT THEN COMPARES THE RESULT WITH IOWITEAS. IF IOWITEAS IS GREATER,

```

599      * A NEGATIVE VALUE IS RETURNED.
600
601 .....
602 //
603 DEFINE INTEGER PROCEDURE RMS.CHECK(NOITEMS)
604   WHERE INTEGER NOITEMS TOBE
605   BEGIN
606     OWN INTEGER CNTRI
607     OWN POINTER PTRI
608
609     CNTRE=ZKNOI
610     FOR PTR=START.FMS STEP 3 ... COUNT EMPTY ITEMS IN FMS.//
611     UNTIL STOP.FMS
612     DO IF #0(PTR) EOL ZERO ... ZERO FOR IN HEALS EMPTY //
613     THEN CNTRE=CNTRE+1
614     RMS.CHECK=CNTRE-NOITEMS! ... RETURN MFG IF NO ROOM //
615     GOTO RETURN
616     ENCI
617
618 .....
619     SRCHFET
620     POINTER = SRCHFET(STRT.AFT, TYPMASK)
621
622     THIS ROUTINE SEARCHES THE FLIGHT PLAN FOR THE FIRST
623     FIVE OF A TYPE SPECIFIED BY TYPMASK. A POINTER TO
624     THIS ITEM IS RETURNED. A NULL INDICATES NOT FOUND.
625     SEARCH BEGINS AT ITEM FOLLOWING STRT.AFT.
626 .....
627 //
628
629 DEFINE POINTER RECURSIVE PROCEDURE SRCHFET(STRT.AFT, TYPMASK)
630   WHERE POINTER STRT.AFT:
631   WHERE INTEGER TYPMASK TUBE
632
633   BEGIN
634     OWN POINTER PTRI
635     PTR=STRT.AFT:
636     IF PTR#155 FESTRT
637     THEN PTR:=FESTRT-ITM.SIZE:
638     LOOP:
639     IF PTR# CRT FETEND
640     THEN BEGIN
641       SRCHFET = NULL:
642       GOTO RETURN
643     END:
644     OWN ZERO
645     THEN GOTO LOOP:
646     SRCHFET = PTRI
647     GOTO RETURN
648     ENCI
649 .....
650
651 .....
652     VALUE = CONVERT(EVENTHO)
653
654 .....
655

```

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456 * THIS ROUTINE CONVERTS AN ABSOLUTE EVENT NUMBER TO A
457 * FLIGHT EVENT TABLE ITEM POINTER, THIS IS COMPLICATED
458 * BY THE FACT THAT THE ABSOLUTE EVENT NUMBERING SCHEME
459 * IS SUCH THAT EVENTS ARE NUMBERED ...20-1+1+2...
460 * THE ABSENCE OF A ZERO EVENT REQUIRES SPECIAL HANDLING.
461 *
462 *
463 * DEFINE POINTER RECURSIVE PROCEDURE CONVFE(LVENTNO)
464 * WHERE INTEGER EVENTNO TOBE
465 * BEGIN
466 *   OWN, POINTER PTRTMP
467 *
468 *   ... EVENT NUM TIMES 4 PLUS
469 *   ADDR OF ITEM 1 IS OK IF
470 *   EVENT NUM WAS NEG. BUT IS
471 *   ONE ITEM OFF IF POS. //
472 *   // 00000606
473 *   ... POS OR NEG? //
474 *   THEN PTRTMP=PTRTMP-ITM.SIZE! ... POS. RACK UP 1 ITEM //
475 *   CONVFF = PTRTMP1
476 *   GOTO RETURN
477 *   ENCL
478 *   ...
479 *   ...
480 *   ...
481 *   ...
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513 OF A SEVFKR COURSE CHANGE
514 IURT 160 DEGJ FOR'E ANFS
515 TO ZERO WAKING TURN PFGIN
516 WHEN AIRCRAFT EVEN WITH
517 WAYPOINT. //
518
519 IF PFSTAT EOL PARALLEL AND
520 ((ANG GRT DEGRD AND
521 HALF * POFSEFE GEQ 0.0)
522 OR ANG LES DEGRD)
523 THEN ANFSLE=POFSFE*NSIN(HALF)/NCOS(HALF)
524 GOTO RETURN
525 END
526
527 ... ***** PROC AUFSE ***** //
528
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570 REPT:PRINT=SAVEI      ... FSTORE R4S POINTER //
571 R4SFE(1)=IPATH-STRI,R4S+31/31      ... CALC R4S ITEM NUMBER//
572      ... BLTD AND A4YID GO IN WRG2//
573 VE.TYPE: W2(1)=A1D(FROM1)
574 STOR.CM: C.BITS(1)=
575 (C4TRKOR(FROM),R4S,3) .V. 61      ... TOCVF=FMMLV=INVALID // 0000065A
576 IF TYPE NEW LTP
577 THEN I4YTES(1)=AUX*CTL(FROM1)      ... STORE EXTRA CTL BITS // 00000659
578 GOTO RETURN;
579 ENB1
580      ... ***** PROC INSERT ***** //
581 *****
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627 LATERAL PATH ANGLES AND DISTANCE FROM FIRST EVENT IN THE
628 FET. BEYOND THE SPAN OF THE EDIT, IT ADDS THE DISTANCE
629 INCREMENT TO ALL LATERAL EVENTS. IF POPS WAS CHANGED, THE
630 SPAN OF THE EDIT IS CHANGED TO INCLUDE ALL EVENTS. THUS ALL
631 FLIGHT PARAMETERS ARE RECALCULATED.
632
633 *****
634 // 00000682
635 // 00000683
636
637 DEFINE PROCEDURE FTXFEET(LASTITM,NOITEMS)
638 WHENC POINTER LASTITM
639 1C INTEGER NOITEMS TODR
640 BEGIN
641   ... ***** PROC FIXFEET ***** //
642   ... ONJ REGISTERS //
643
644   ONJ REAL TMP,REALI
645   ONJ POINTER PRV,VEI
646   ONJ POINTER ITEMI
647   ONJ POINTER V,EVENTI
648   ONJ POINTER PTRI
649   ONJ INTEGER I
650   ONJ REAL DELTAI
651   ONJ INTEGER TMP,INTBI
652   TMP,INTBI = TMP,REALI
653
654   POINTER MAYROR1
655   REAL OLD,DISI
656   VE,VDIST
657   REAL POPS,IMPI
658   PRESET POPS,IMP = 0.01
659
660   FOR PNT=START,RMS STEP 3   ... PROGRAM START //
661   UNTIL STOP,RWS           ... INVALIDATE ALL //
662   DO WIP(PNTR)=1(PNTR) ,V, "80" //
663
664   INITL:
665   IF TYPEFF(FESTRT) EQL CTYP   ... AUTO DELETE OF EOC EVENT //
666   THEN FSTRT=ABS.1=FESTRT+ITM,SIZEI   ... WHEN FOC IS EVENT 1 //
667   ITR=FESTRTI   ... FSTRT ALWAYS LE OR OF. //
668   PRV,AVFV,EVENTI=EOC.P,IR=NULLI   ... INIT VE POINTERS. //
669   VE,DISI = 0.01   ... INIT DIST TO PREVIOUS VE //
670   MAYDOP2 = SPCFEET(LASTITM,LDMSK)I   ... END OF EDIT SPAN //
671   ... START OF EDIT IS LAST ITEM //
672   IN EDIT - ITEMS IN EDIT -
673   * THE "W" INSURES THAT LE
674   PRECEDING EDIT IS INCLUDED.
675   IT IS 4 TRFS, EOC EVENT.
676   2 DEP EVENTS, IF ITSELF. //
677   ... IF PARALLEL OFFSET (POFS)
678   WAS CHANGED WITH THIS
679   EDIT,THE SPAN OF THE EDIT
680   IS INCREASED TO INCLUDE
681   ALL ITEMS TO THE FET.
682   THIS REARS ALL FLIGHT
683   PARAMS ARE RECALCULATED //
684
685   IF POFSFF NEG POFS,IMP
686   THEN REGTR
687   ... ***** POFS CHANGED ***** //
688
```

```

684 POFS.TMP = POFSFEI
685 MAYB02 = PETENDI
686 MAYB01 = FESJRTI
687 ENDI
688 IF MAYB01 LEQ FESJRTI
689 THEN DISTFE(FESTAT)=0.01
690 GOTO D00P11
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NAT.ITEM:

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... UPDATE FIXFEY.POFS //
... GO TO END OF FFT //
... START AT FFT START //
... ***** POFS CHANGED ***** //
... IF SPAN OF EDIT INCLUDES //
... 1ST LE, REDEFINE DIST. //
... FINISH INIT OF FIRST EVNT //
... MAIN LOOP OF FIXFEI //

... ***** OUT OF ITEMS ***** //
... IF ITEM IS DEST EVENT, WE //
... LOOP THRU NONE1 TO CALC //
... VERT PATH ANGLES FOR THE //
... LAST VERT PATH LEG. THESE //
... WERE NOT CALCULATED AT THE //
... FEI'S LAST EVENT WAS VERT //
... ***** DEST EVENT ***** //
... IF 1 EVENT, CRSI = 0 //

... ***** DEST EVENT ***** //
... PROCESS AN ITEM. IF VF //
... WAS FOUND, REMEMBER IT //
... UNTILL THE DIST CALC FOR //
... THE ASSOCIATED LE IS MADE //

... ***** REMEMBER VE ***** //
... STORE POSITVEY AT VE //
... FIXES LAST VE IN FEI //
... FIXES FIRST VE IN FEI //
... LOOK SOME MORE //
... ***** REMEMBER VE ***** //
... MAYB01 IS START OF EDIT //
... PRIOR TO SPAN OF EDIT //
... IF PARAMS ARE CALCULATED //

... ***** END OF EDIT SPAN ***** //
... COMPLETE DIST FOR MAYB02 //
... RESTORE ITEM TYPE //
... CALC INCREASED DIST. //
... ***** END OF EDIT SPAN ***** //
... MAYB02 WAS IN LIST TOO //
... ***** BEYOND EDIT ***** //
... BEYOND SPAN OF EDIT //
... INCREASED DIST IS ADDED //
... TO LE'S //

... ***** REMEMBER VE ***** //
... STORE POSITVEY AT VE //
... FIXES LAST VE IN FEI //
... FIXES FIRST VE IN FEI //
... LOOK SOME MORE //
... ***** REMEMBER VE ***** //
... MAYB01 IS START OF EDIT //
... PRIOR TO SPAN OF EDIT //
... IF PARAMS ARE CALCULATED //

... ***** END OF EDIT SPAN ***** //
... COMPLETE DIST FOR MAYB02 //
... RESTORE ITEM TYPE //
... CALC INCREASED DIST. //
... ***** END OF EDIT SPAN ***** //
... MAYB02 WAS IN LIST TOO //
... ***** BEYOND EDIT ***** //
... BEYOND SPAN OF EDIT //
... INCREASED DIST IS ADDED //
... TO LE'S //

```

```

741 DST=RU(ITEM)=DSTWRD(ITEM)+DELTA // ... FIX DISTANCE. //
742 FOTO COREI //
743 ... BEYOND EDIT ***** //
744 ... WITHIN SPAN OF EDIT, ALL //
745 FLIGHT PARAMS ARE //
746 CALCULATED //
747 IF RMSFE(PRV.LE) EQL ZERO OR //
748 (CTLWD(PSWSPTR(PRV.LE)) .V. // ... BITS FOR EITHER POINT // 00000049
749 CTLWRD(PSWSPTR(ITEM)) .A. // ... FIRST LIMP IN CHAIN. // 00000050
750 "30" NEW 0 //
751 THEN REGN //
752 ... OR PRV.LE IS ORIGIN EVHT //
753 ... ***** BYPASS LLTD ***** //
754 DST=RU(ITEM)=DSTWRD(PRV.LE)+ITEM // ... BEFAT 1/10 LIM //
755 PRSFE(ITEM)=CMSOFE(PRV.LE) // ... ALL LAT ANGLES = //
756 =CMSIFE(PRV.LE) // ... LAST VALID CML. //
757 IF FOC.PTR EQL NULL // ... VPAT IS FLAGGED //
758 THEN, LOCAL.PTR=CMCHFE(ITEM,VMSK) // ... FOR VP PAST EOC //
759 FOTO COREI //
760 ENDI //
761 LLTD(PSWSPTR(PRV.LE)+1,RMSPTR(ITEM)+1,ANSR) // ... ERMG-DIST //
762 TMP.REAL=RU(ANSR) //
763 ... CALC CRSN //
764 TMP.INTG=(TMP.INTG //
765 ... SWITCH RANGE OF OWN REF SC // 00000060
766 ... *L CAN PROTECT BYTE 3 // 00000061
767 ... V. C-BITS(PRV.LE) //
768 CRSD(PSWSPTR(ITEM)+1,ANSR) //
769 IF C-BITS(ITEM) .A. "80" EQL ZERO //
770 THEN REGN //
771 ... ***** COURSE EDIT SET ***** //
772 IF ITEM EQL ABS.1 //
773 THEN, FOTO CALCAGEST //
774 ... TO EVENT ONLY. //
775 C-BITS(ITEM)=C-BITS(ITEM) .V. "80" // ... CRSD INVALID //
776 ENDI //
777 ... ***** COURSE EDIT SET ***** //
778 TMP.REAL=RU(ANSR)+UEGARH0 //
779 ... CALC CRST //
780 TMP.INTG=(TMP.INTG //
781 ... V. "FFFFFF00" //
782 ... V. RMSFE(ITEM) //
783 ... ADD BYTE 3 //
784 ... STORE //
785 ... CALC AOFB //
786 ... CALC AOFB //
787 DSTWRD(PRV.LE)=DSTWRD(PRV.LE)+TMP.REAL //
788 TYPEFF(PRV.LE)=LTYPE //
789 OLD=DSTWRD(ITEM) //
790 TMP.REAL=DSTWRD(PRV.LE) //
791 ... SAVE OLD DIST FOR DELTA //
792 ... STORE PARTIAL DIST. AOFB //
793 ... IS ADDER NEXT LL. //
794 ... THE FOLLOWING LOGIC CORRECTS //
795 ... THE DISTANCE VALUE FOR BASE //
796 ... OFFSETS. THE DIST VALUES FOR //
797 ... THE 1ST WAYPOINT OF THE //
798 ... OFFSET CONFIG & THE WAYPOINT //
799 ... PAST THE LAST OFFSET EVENT //
800 ... HAVE THE OFFSET VALUE //
801 ... 300EU. //
802 ... START OF 2-EVENT PATTERN //
803 ... START OF 3-EVENT PATTERN //
804 ... FVT PAST 2-EVENT PATTERN //
805 ... FVT PAST 3-EVENT PATTERN //
806 ... ADU OFFSET TO LISTANCE //
807 ... BUT IN THIS FILE //
808 ... ***** REMOVE DUPLICATE EVIS //
809 IF OFTEG(ITEM) EQL STR190 //
810 OR OFTEG(ITEM) EQL STR190 //
811 OR OFTEG(PRV.LE) EQL ENJ90 //
812 OR OFTEG(PRV.LE) EQL INTERCEP //
813 THEN TMP.PAL=TMP.REAL+PFSFE //
814 ... ADU OFFSET TO LISTANCE //
815 ... BUT IN THIS FILE //
816 ... ***** REMOVE DUPLICATE EVIS //
817 ... ***** REMOVE DUPLICATE EVIS //
818 ... ***** REMOVE DUPLICATE EVIS //
819 ... ***** REMOVE DUPLICATE EVIS //
820 ... ***** REMOVE DUPLICATE EVIS //
821 ... ***** REMOVE DUPLICATE EVIS //
822 ... ***** REMOVE DUPLICATE EVIS //
823 ... ***** REMOVE DUPLICATE EVIS //
824 ... ***** REMOVE DUPLICATE EVIS //
825 ... ***** REMOVE DUPLICATE EVIS //
826 ... ***** REMOVE DUPLICATE EVIS //
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866 ... ***** REMOVE DUPLICATE EVIS //
867 ... ***** REMOVE DUPLICATE EVIS //
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895 ... ***** REMOVE DUPLICATE EVIS //
896 ... ***** REMOVE DUPLICATE EVIS //
897 ... ***** REMOVE DUPLICATE EVIS //

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```

798 THEN BEGIN
799   ITEM=CMPRSEL(ITEM,ITEM)
800   ADJUSTING(ITEM,NULL,0,NULL)
801   COTO SHITL
802   END
803
804   DONE:
805
806   DONE1:
807   IF V-FVBT NEG NULL
808   THEN BEGIN
809     IF PRV.VE NEG NULL
810     THEN BEGIN
811       TMP.REAL=
812       NTAN((ALTUPE(V.EVENT)-ALTUPE(PRV.VE))/ALTCORV,
813           DSTWRD(PRV.LE)-VE,0.15))
814       *A. "FFFFFF00"
815       *V. IDYTES(IV,LEVI)
816       *V. IDYTES(IV,LEVI)
817       *V. IDYTES(IV,LEVI)
818       *A. "FFFFFF00"
819       *V. C.BITS(PRV,VE)
820       *V. C.BITS(PRV,VE)
821       *V. C.BITS(PRV,VE)
822       *V. C.BITS(PRV,VE)
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1000      *V. C.BITS(PRV,VE)

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912          THEN REGIN
913          NOITE#
914          GETTYPE = NOEVTI
915          GOTO RETURNI
916          ENDI
917          IF TYPVASK .A. EVMASK(TYPEFE(PNTR))
918             ... SEARCH FAILED *****//
919             ... REPORT FAILURE.
920             ... WITH LOOKUP TABLE MASK
921             ... NO WATCH
922             ... FOUND ONF. BUMP COUNTER
923             ... BACK-UP POINTER *****//
924             PTR=PTR-ITM+SIZEI
925             GOTO LOOP2I
926             ENDI
927             FOUND:
928             GETTYPE=BUILDFE(PNTR,WKPTR)I
929             GOTO RETURNI
930             ENDI
931             ... ***** PROC GETTYPE *****//
932             *****
933             *****
934             *****
935             *****
936             *****
937             *****
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969 DEFINE INTEGER RECURSIVE PROCEDURE BUILDFE(ITEM, PTR, MKPTR)
970 WHERE POINTER ITEM, PTR, MKPTR TO BE
971 BEGIN
972   OWN REAL RTNSIGN
973   OWN REAL CUCHE
974   OWN POINTER TO, PTR1
975   OWN POINTER LE, PTR1
976   OWN POINTER ITR, PTR1
977   OWN POINTER HRS, PTR1
978   OWN INTEGER TEMPI
979   OWN INTEGER INDX1
980   OWN INTEGER SVE, VERS1
981   INDX ← 3
982   CUCHE
983
984   ... IF VERSFEED, FFT INHIBITED
985   AND VERSION MISMATCH IS
986   RETURNED. //
987
988   ... INITIALIZATION SECTION //
989   ... LOAD OWN REGISTERS //
990   ... FET ITEM POINTER //
991   ... CALC ABSOLUTE EVENT NUM //
992   ... COMPENSATE FOR NO ZERO EV//
993   ... CONVERT PTR TO ABS FVT NO//
994   ... ORIGIN, DEST, AND LOC //
995   ... ** INVALUATE CNTRWORD //
996   ... ** INVALUATE CNTRWORD //
997   ... ** INVALUATE CNTRWORD //
998   ... ** INVALUATE CNTRWORD //
999   ... ** INVALUATE CNTRWORD //
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1022   ... ** INVALUATE CNTRWORD //
1023   ... ** INVALUATE CNTRWORD //
1024   ... ** INVALUATE CNTRWORD //
1025   ... ** INVALUATE CNTRWORD //

```

```

1026 THEN TEMP=TEMP .V. "8000"
1027 CATR*ORD(TO,PTR)=TEMP; //
1028 EC*YD(10,PIR)=INDX; //
1029 E*WYD(10,PIR)=NOI APTAG(TO,PIR) // ONF OR THE OTHER //
1030 IF INDX NEQ L*YTP //
1031 THEN AUX.CIL(TO,PIR)= //
1032 MOI(TM,PIR) .A. "30" //
1033 C*Y*TR*H(TO,PIR)=AS.PIR //
1034 A*G*E*S(TO,PIR)=A*P*O*F(TO,PIR)=A*G*E*S*E*I(TM,PIR) // COPY W*Y*P TO .LAT. LONG. //
1035 D*F(TO,PIR)=D*ST*W*O*U*L*E(PTR)=-D*ST*W*O*U*L*E(PTR) // ... CALC OF TO //
1036 IF INDX EQL V*YTP // 00001151 //
1037 THEN BEGIN // 00001006 //
1038 C*Y*TR*H(TO,PIR)=I*ITM(PTR) // ... V*P*AI,V*P*AO, AND ALTD // 00001007 //
1039 IF F*O*C*P*TR EQL I*ITM(PTR) // F*L*A*G*E*Y F*L*A*G*S VE AFTER F*O*C // 00001009 //
1040 THEN L*V*P*AI(10,PIR)=T*R*U*E // ... AS V*P*AI W*E*H*E IS I*N*V*AI*LD. // 00001000 //
1041 CO*IN EX*IT // 00001126 //
1042 END // 00001009 //
1043 I*AS*I(TO,PIR)=S*P*E*E*D(L*E,PIR) // ... R*E*T*U*RN I*AS W*O*R*D // 00001010 //
1044 // 00001164 //
1045 NO*IS*I(TO,PIR)=NO*IS*I(TO,PIR)=Z*E*R*G // ... F*L*A*N*K O*U*T G*A*R*R*A*G*E //
1046 P*O*F*S(TO,PIR)=P*O*F*S*E*I // ... S*T*O*R*E F*O*W N*O*P*O*F*S & P*A*R*AL //
1047 IF P*O*F*S*E*I(TO,PIR)=P*E*F*S*T*AT E*G*L B*A*S*E*O*F*S //
1048 THEN BEGIN //
1049 ... B*A*S*E O*F*S*E*T ***** //
1050 P*O*F*S(TO,PIR)=O*0 // ... F*U*R S*T*R*A*S*E & S*T*R*193 //
1051 C*O*U*R*S*O*U*L*E(PTR)=C*R*S*IM*U*L*E(PTR) // ... C*O*U*R*S*E C*H*G. //
1052 P*T*I*N*S*I*G*N(C*O*U*H) // ... S*I*G*N O*F C*R*S C*H*G //
1053 IF T*E*M*P=O*F*I*G*U*L*E(PTR) E*G*L E*N*D*R*A*S*E //
1054 THEN P*O*F*S(TO,PIR)=P*O*F*S*E*P*T*I*N*S*I*G*N // ... E*N*D*U*P* //
1055 IF T*E*M*P E*G*L I*N*V*E*R*P //
1056 THEN BEGIN //
1057 P*O*F*S(TO,PIR)= //
1058 -P*O*F*S*E*P*T*I*N*S*I*G*N(I*AS*I(C*O*U*H)) //
1059 A*C*F*S(TO,PIR)= //
1060 -P*O*F*S*E*P*O*C*S(I*AS*I(C*O*U*H)) //
1061 END //
1062 IF T*E*M*P E*G*L S*T*R*193 O*N T*E*M*P E*G*L S*T*R*193 // ... S*T*R*193 //
1063 THEN A*G*E*S(10,PIR)=P*O*F*S*E*I // ... O*N S*T*R*193 //
1064 P*O*F*S*E*I(TO,PIR)=T*E*M*P // ... O*V*E*R*R*I*F* F*L*A*G C*O*M*P*O*S*I*T //
1065 END // ... B*A*S*E O*F*S*E*T ***** //
1066 //
1067 B*U*I*L*D*E*P*O*V*E*R //
1068 IF V*E*R*S*E E*G*L S*V*E.V*E*R*S //
1069 THEN CO*IN R*E*T*U*RN //
1070 //
1071 B*U*I*L*D*E*P*O*V*E*R //
1072 G*O*T*O R*E*T*U*RN //
1073 END //
1074 END //
1075 END P*Y*E //

```



```

57 EXTERNAL
58 RNEVPI,
59 DIBN,
60 P90,
61
62 PRESET BEGIN
63 R2 = 0.01111111 // ... 2 DEGREES //
64 RMPRT2 = 0.000016511 // ... 2/10 NAUTICAL MILE //
65
66 END
67
68 ***** POINTERS *****//
69
70 POINTER
71 RSTRT,
72 RSTMP,
73 RPS.1,
74 RPS.1,
75 RSTRT,
76 RSTMP,
77
78 *****
79
80 ADD4D
81
82
83
84
85
86
87
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171      GOTO MDEXIT;
172
173      ... TWO-POINT BASE OFFSET
174      GEOMETRY WAS NOT SATISFIED.
175      THIS SECTION CHECKS THREE-
176      POINT BASE OFFSET
177      GEOMETRY. //
178
179      ... CALC ABS COURSE CHANGE ERR //
180      FM *I1) TO *I1+1). //
181
182      ANG. ERR=ABS(ABS(COCH(I1,D,STRT))-390);
183      ANG. ER1)=ANG. ER1
184      IF ANG. ER1 GRT D2 //
185      THEN GOTO RETURN;
186      IF TOTLEK(PTR,ANG,ERR,TDISTE(I1)) ... CR DIST ERR //
187      THEN GOTO RETURN;
188      ... CALC ABS COURSE CHANGE ERR //
189      FM *I1-1) TO *I1). //
190
191      ANG. ER2=ABS(ABS(COCH(I1,D,STRT))-3180);
192      ANG. ER2)=ANG. ER2
193      IF ANG. ER2 GRT D2 //
194      THEN GOTO RETURN;
195      IF TOTLEK(PTR,ANG,ERR,TDISTE(2)) ... CR DIST ERR //
196      THEN GOTO RETURN;
197      ... TWO-POINT BASE OFFSET //
198      GEOMETRY SATISFIED //
199      CLEAR ANY OLD OFFSET //
200      ... CHECK ANY OLD OFFSET //
201      ... CLEAR ANY OLD OFFSET //
202      ... CLEAR ANY OLD OFFSET //
203      ... CLEAR ANY OLD OFFSET //
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226      ... CLEAR ANY OLD OFFSET //
227      ... CLEAR ANY OLD OFFSET //

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```
228 REPLND=REPLACFE1STABEVNO,SPABEVNO,NOITFMS,PROC,WKPTR) I  
229 END I  
230 ... ***** CANCEL OFFSETS ***** //  
231 ... IF EVT IS BASE OFFSET FVT //  
232 GOTO RETURN I  
233 PERP406GKTH I  
234 GOTO RETURN I  
235  
236  
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238  
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285 1 = FLIP
286 ENDI
287 STATE=KITI
288 LE.PTR = ABS(1-ITM,SIZE)
289 BSTRT = SCHEFFILE.PTR.LMSK)
290
291 LE.PTR = SCHEFFILE.PTR.LMSK)
292 IF LE.PTR EQL LULL
293 THEN BEGIN
294   SCARBASE=ROLVTI
295   GOTO RETURN;
296 ENDI
297 IF STATE EQL INIT
298 THEN BEGIN
299   IF NOT(IGILE.PTR) NEO NOPOFS
300   THEN BEGIN
301     STATE=FLIMI
302     GOTO LOOP;
303 ENDI
304
305   PSTRT = LL.PTRI
306   GOTO LOOP;
307 ENDI
308
309   BSTOP = IE.PTRI
310   IF NOT(CALL.PTR) NEW NOPOFS
311   THEN GOTO LOOP;
312   SCARBASE = RDRTNI
313   GOTO RETURN;
314 ENDI
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342 DEFINE REAL PROCEDURE CK90(FEI,PTR)
343 WHERE POINTER FLT,PTR
344 TOBE BEGIN //
345   ... ***** PROC CK90 ***** //
346   OWN POINTER PTR1 //
347   PTR=PREV.LE(FLT,PTM) //
348   IF PTR.POL NULL //
349     THEN HEIGHT //
350     CK90=901 //
351     GOTO RETURN1 //
352   FLDJ //
353   CK90=ABS(CKSOAD(PTR)-CRSI*D(PTR))-D901 //
354   GOTO RETURN1 //
355   ENCL //
356   ***** PROC CK90 ***** //
357   ABSCOCH ***** //
358   ***** //
359   KTN.VLU = ABSCOCH(I,J,FLT,PTH) ***** //
360   ***** //
361   ***** THIS ROUTINE CALCS THE //
362   ABSOLUTE VALUE OF THE SUM //
363   OF COURSE CHARGES FROM //
364   Y LE'S PRIOR TO FLT.PTR //
365   TO J LE'S AFTER FLT.PTR. //
366   ***** //
367   ***** PROC ABSCOCH ***** //
368   ***** //
369   TOBE BEGIN //
370   OWN POINTER PTM1 //
371   OAN INTEGER X1 //
372   CAN INTEGER Y1 //
373   OWN REAL SUM1 //
374   ABSCOCH=SUM=0.01 //
375   PTR = FLT.PTR1 //
376   FOR X=0 STEP 1 UNTIL I-1 //
377   DO PTH=PREV.LE(PTM)1 //
378   ***** //
379   ***** SUM COURSE CHARGES //
380   ***** //
381   X = I + J1 //
382   FOR Y=0 STEP 1 UNTIL X //
383   DO PEGTH //
384   IF PTH.EAL NULL //
385     THEN GOTO RETURN1 //
386     SUM=SUM + (CRSUND(PTR)-CRSI*D(PTR))1 //
387     PTH=SKCH(PTM,LMSK)1 //
388     FLDJ //
389     ABSCOCH=ABS(SUM)1 //
390     GOTO RETURN1 //
391     ENCL //
392     ***** PROC ABSCOCH ***** //
393     ***** //
394     PREV.LE ***** //
395     ***** //
396     PTR = PREV.LE(FLT,PTM)1 //
397     ***** //
398     ***** //

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199 ... THIS PROC FINDS THE LF
200 POINT TO THE ONE POINTED
201 AT IN THE FET. THUS IT IS
202 A BACKWARD SEARCH ROUTINE.//
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APPENDIX B
Program Listing of the Speed Profile
Algorithm

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57	ALTC	REAL COMPONENT	SPECIFIED WAYPOINT TO THE TO-WAYPOINT. FLIGHT PLAN EDITOR FLIGHT PLAN COMPONENT USED TO RECORD ALTITUDE FOR A VERTICAL EVENT.
58	IASK	REAL COMPONENT	FLIGHT PLAN EDITOR FLIGHT PLAN COMPONENT USED TO RECORD INDICATED AIRSPEED LEVITS WAGE VIA THE SPECIF PART.
59	IASF	INTEGER COMPONENT	FLIGHT PLAN EDITOR FLIGHT PLAN COMPONENT USED TO RECORD IAS TYPE.
60	PIAS	SYNONYM	CODE RETURNED IN THE IAS COMPONENT THAT INDICATES A PILOT-DEFINED IAS.
61	PROOUT	SYNONYM	CODE RETURNED IN THE IAS COMPONENT THAT INDICATES THAT THE IAS ENTRY FOR THE GIVEN WAYPOINT IS IDENTICAL TO THAT OF THE PRECEDING WAYPOINT IN THE WAYPOINT.
62	PROCHI	SYNONYM	CODE RETURNED IN THE IAS COMPONENT THAT INDICATES THAT THE GIVEN IAS IS PART OF A DECREASING PROFILE.
63	PROP	SYNONYM	CODE RETURNED IN THE IAS COMPONENT THAT INDICATES THAT THE GIVEN IAS IS PART OF AN ASCENDING PROFILE.
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91	WPA1	POINTER	CONTAINS ADDRESS OF WPA AREA USED BY THE CDU CHANNEL.
92	ZILCH	INTEGER PROCEDURE	NULL PROCEDURE USED TO SATISFY PROCEDURE ARGUMENT REQUIREMENTS FOR CASES WHERE SPECIAL DEFAULT LOGIC IS NOT REQUIRED.
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114	VALID	SYNONYM	PERFORMED. VALUE ASSIGNED TO INTEGER FLAG TO INDICATE VALID STATUS.
115	TCOMF	INTEGER	VALIDITY FLAG THAT IS ASSIGNED A VALID STATUS BY SENSOR WHENEVER SPECIFIC PROGRAM COMPUTATIONS ARE UPDATED. TCOMF IS ASSIGNED AN INVALID STATUS BY THE TIME CONTROL PROGRAMME WHENEVER THE CURRENT COMPUTATIONS ARE PERFORMED.
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126	5) AFOLIB INSERT FILE	DECLARATION	DESCRIPTION
127	SYMBOLIC NAME	TYPE	
128			
129	.CRPT	PROCEDURE	SUPERVISORY SOFTWARE ROUTINE THAT IS CALLED TO YIELD OWN CHANNEL TIME FOR CLEARPNT CYCLE.
130			
131			
132			
133			
134	6) MATHPACK INSERT FILE	DECLARATION	DESCRIPTION
135	SYMBOLIC NAME	TYPE	
136			
137	RLMIF	REAL PROCEDURE	ROUTINE THAT LIMITS THE FIRST ARGUMENT TO THE MAGNITUDE GIVEN BY THE SECOND ARGUMENT.
138			
139	RMVAF	REAL PROCEDURE	ROUTINE WHOSE RETURN ARGUMENT IS THE LARGER OF TWO VALUES SPECIFIED AS INPUT ARGUMENTS.
140			
141	RMVIF	REAL PROCEDURE	ROUTINE WHOSE RETURN ARGUMENT IS THE SMALLER OF TWO VALUES SPECIFIED AS INPUT ARGUMENTS.
142			
143	ABS	REAL PROCEDURE	PROCEDURE THAT DETERMINES THE MAGNITUDE OF A GIVEN INPUT ARGUMENT.
144			
145	RRDCT2	REAL PROCEDURE	PROCEDURE THAT DETERMINES THE SQUARE ROOT OF A GIVEN INPUT ARGUMENT.
146			
147			
148			
149			
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152			
153			
154	7) MATHPACK INSERT FILE	DECLARATION	DESCRIPTION
155	SYMBOLIC NAME	TYPE	
156			
157	ADHD	POINTER	POINTER TO ARRAY WHERE SENSOR INPUT FOR HEADING AND AIR DATA INFORMATION IS RECORDED.
158			
159	TAS	REAL COMPONENT	ADHD COMPONENT USED TO RECORD SENSOR INPUT FOR TRACK AIRSPEED.
160			
161	DELV	REAL COMPONENT	ADHD COMPONENT USED TO RECORD SENSOR INPUT FOR IAS INSTRUMENT ERROR.
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171 ***** INTERNAL DATA STRUCTURE *****
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COMMENT
INTEGER DECLARATIONS
*** STATUS OF IAS COMPONENT FOR WPT
TAGGED AS FIRST FOR A GIVEN PROFILE //
*** ABS EVENT NO. OF JIM LAT EVENT //
*** SPECIFICS LAT/VAL FROM EVENT NUMBER //
*** SPECIFICS LAT/VAL EVENT NUMBERS //
*** IAS DISPLAY CLEAR PARAMETER //
*** FLAG TO INDICATE IF ADJACENT KRYPTS //
HAVE PIAS //
*** ONE ITEM IS TO BE REPLACED //
*** EVENT NO. FOR INITIAL SPEED CONTROL //
*** WAYPOINT OF A GIVEN PROFILE //
*** EVENT NO. INDEX FOR FINAL SPEED-CONTROL //
*** WAYPOINT OF A GIVEN PROFILE //
*** PARAMETER USED TO RECORD EXISTENCE OF //
ANOTHER SPEED PROFILE IN THE REMAINING //
FLIGHT PLAN //

*** STATUS :
FRST.STATUS :

COMMENT
REAL DECLARATIONS
*** AIRCRAFT TRUE AIR SPEED //
*** IAS INSTRUMENT ERROR //
*** AIRCRAFT ALTITUDE //
*** AIRCRAFT OR KRYPT ALTITUDE //
*** SAVES THE IAS VALUE OF *IFRST) //
*** SAVES THE IAS VALUE OF *LAST) //
*** DIST FROM THE TO-EVENT TO *IFRST) //
*** DIST FROM THE TO-EVENT TO *LAST) //
*** DIST BETWEEN TO-EVENT AND *TO-E) //
*** DIST BETWEEN TO-EVENT AND *TO) //
*** IAS OF *TO-E) //
*** DIST BETWEEN *IFRST) AND *TO) //
*** TEMP VAR TO HANDLE IAS CALC OF *TO) //
*** ALTITUDE PROPORTIONALITY CONSTANT //
USED TO CONVERT IAS TO TAS //
*** KALT SCALING FACTOR //
*** PREVIASP SQUARED //
*** ALONG TRK DIST FROM *IFRST) TO *LAST) //
*** VLL CHNG BETWEEN *TO-E) AND *LAST) //
*** ALONG TRK DIST BETWEEN *TO-E) AND *TO) //
*** ALONG TRK DIST BETWEEN *TO) AND *LAST) //
*** TIME TO FLY FROM *TO-E) TO *LAST) //
AT RATE OF *KIMATE //
*** AVE VEL REQUIRED FOR A LINEAR SPEED //
PROFILE BETWEEN *TO-E) AND *LAST) //
*** TIME TO FLY FROM *TO-E) TO *LAST) //
WITH CONSTANT VELOCITY OF *AVE //
*** LIST TO RECALC VLL CHNG OF VLL AT //
DATE OF *KIMATE //

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285 OAN REAL PREVIOUSLY OCCURRED. IAS (KNOTS) IS :
286 IF COVERED, NEG VALID
287 ... IF FLIGHT PLAN HAS BEEN MODIFIED
288 SINCE THE LAST SPEED PROFILE
289 COMPUTATION, THEN UPDATE SPEED
290 PROFILE, OTHERWISE RETURN. //
291 THEN GOTO VERBERGATE
292 WPT=K1
293 TECH=VALID
294
295 COMMENT SCAN FLIGHT PLAN FOR LAST SPEED PROFILE WAYPOINT. ASSIGN
296 THE IAS ASSOCIATED WITH THIS WAYPOINT TO ALL RELEVANT
297 WAYPOINTS IN THE FLIGHT PLAN
298
299 SAVEL1 :
300 LEVTO=FROMLEVH0+2
301 WHILE GETTIME(L*SK*LEVH0*WPT) EOL GLENH
302 DO
303 BEGIN
304 IF IAS(WPT) EOL PIAS
305 THEN
306 BEGIN
307 LASTIAS=IAS(WPT)
308 ... RECORD LAST PILOT-DEFINED IAS
309 IN LASTIAS
310
311 SAVE=LEVH0+1
312 END
313 LEVTO=LEVH0+1
314 END
315 LEVTO=SAVE
316 WHILE GETTIME(L*SK*LEVH0*WPT) EOL GLENH
317 DO
318 BEGIN
319 IAS(WPT)=LASTIAS
320 ... ENTER LAST PIAS SPEED FOR WAYPT SFC//
321 IAS(WPT)=P*QUOTE
322 ... AND DISPLAY QUOTE//
323 IF REPLACE(LEVH0*WPT),REPLACE(WPT),DELTA,ZILCH*WPT)
324
325
326
327 LEVTO=LEVH0+1
328 END
329
330 COMMENT TAKE ONE SHOTS OF CURRENT SENSOR DATA
331
332 .CKPT1 :
333 ... YIELD CHANNEL TIME TO ENSURE TIME
334 TO GET A GOOD SHOTS OF SENSOR DATA//
335 ACTASIAS(ADR) :
336 ... AIRCRAFT TRUE AIR SPEED
337 ACISE=REF(ADR)
338 ... IAS INSTRUMENT ERROR
339
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342 THEN GOTO VERIFYDATE ;
343 PRST=1 ;
344 LEVNTJ=1 ;
345 IF PRSTIAS=IAS(EMPTY) AND NOIAS
346 ... IF FROM-EVENT HAS AN AIRSPEED
347 ... ASSOCIATED WITH IT
348 ... THEN LABEL IT A PIAS
349
350
351 COMMENT FROM-WAYPOINT HAS NO IAS. SEARCH FOR FIRST PILOT-
352 ENTERED IAS AND ASSIGN THIS TO THE FROM-WAYPOINT ;
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... INITIALIZE PRST TO -1
... BEGIN SEARCH FOR PIAS WITH 10-EVENT //

... IF FROM-EVENT HAS AN AIRSPEED
... ASSOCIATED WITH IT
... THEN LABEL IT A PIAS //

COMMENT FROM-WAYPOINT HAS NO IAS. SEARCH FOR FIRST PILOT-
ENTERED IAS AND ASSIGN THIS TO THE FROM-WAYPOINT ;

... IF NO PIAS WAS FOUND RETURN //

... RETAIN THE FOUND TASK. THIS IS TO
REPLACE THE FROM-EVENT IAS //

... GET FROM-EVENT INTO WORK AREA //

COMMENT UPDATE FLIGHT PLAN TABLE FOR THE FROM-WAYPOINT. INITIALIZE
PARAMETERS FOR FIRST SPEED PROFILE COMPUTATION ;

... ASSIGN SPEED TO FROM-EVENT //

... ASSIGN PIAS TO FROM-EVENT //

... REPLACE (EMPTY) WITH ZII(EMPTY) NEG NORTH //

... (DEFINED IN
... THE REAL
... DECLARATIONS ABOVE
... START SEARCH FOR NEXT ENTERED SPEED
... WITH EVENT AFTER 10-EVENT //

COMMENT FIRST VALID LOOP.
INITIALIZE PARAMETERS FOR PREVIOUS PROFILE ;

... VALIDATE PRST-STATUS CONCLUSION //

... THIS LOOP CONSTRUCTS EACH PROFILE.
FIRST IT MUST FIND THE NEXT SPEED
CONTROL WAYPOINT. //

... SET ADJACENT SPEED CONTROLS CHECK //

```

399      SCAR FLIGHT PLAN FOR LAST WAYPOINT OF GIVEN PROFILE.
400
401      GLNEXT,SPEEDWPT
402      IF GETITFFF(LASKELEVENTJ,WKPT) NEQ GURTH ... GET NEXT EVENT //
403      THEN GOTO VERUPDATE
404      IF IASFWKPT) NEQ PIAS ... YES, IS IT A SPEED CONTROL WPT ? //
405      YES
406      BEGIN
407      LCNT=1
408      LEV=LEVENTJ+1
409      GOTO GLNEXT,SPEEDWPT
410      END
411
412
413
414
415
416      COMMENT END OF NEXT SPEED LOOP
417      UPDATE PARAMETERS RELATED TO W(LAST)
418
419      LAST, IAS(IAS(WKPT))
420      IAS(IAS(IAS(WKPT)))
421      ... SAVE LAST SPEED CONTROL VALUE //
422      ... SAVE ONE LESS THAN ACTUAL AOS PV NO. //
423      ... THIS IS A RESULT OF BEING USED //
424      WITH GELIAPFE //
425      ... DEFINED IN THE //
426      PRODESTO(LAST-OFFERS)
427      ... REA_ RECLAMATIONS //
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456 END
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458
459 COMMENT END OF SAME SPEED LOOP.
460
461 ELSE
462
463 COMMENT VELOCITY CHANGE LOOP.
464 WFIRST AND WLAST HAVE DIFFERENT SPEEDS. RETRIEVE ALL
465 EVENTS BETWEEN WFIRST AND WLAST AND ASSIGN APPROPRIATE
466 PROFILE SPEED TO THE LATERAL EVENTS.
467
468 FOR ANEVEFIRST=1 STEP 1 UNTIL LAST-1
469 DO
470 BEGIN
471 IF GETHAF (AN*SP*ANEV*WKPT) NEQ GJNTH
472 THEN GOTO VERTUPDATE
473 IF ECOTYP(WKPT) EQL VTP ... IS THIS A VERT EVENT ? //
474 THEN ... Y S. SET HZ. //
475
476
477 COMMENT VERT LOOP.
478 EVENT IS OF VERTICAL TYPE. UPDATE ALTITUDE THAT IS REQUIRED
479 FOR SAS TO HAS CONVERSION
480
481 BEGIN
482 IF NOT TOFVEL(WKPT) ... IS IT ALSO A TO-EVENT //
483 THEN HZ=HZ ... FOR TO-EVENT HZ=PILOT ALTITUDE //
484 ELSE HZ=ALT(WKPT)
485 ... OTHERWISE HZ=PILOT ENTERED ALT //
486
487 END
488
489 COMMENT END OF VERT LOOP
490
491 COMMENT LATERAL LOOP.
492 EVENT IS OF LATERAL TYPE. UPDATE PROFILE VELOCITY.
493
494 ELSE
495 IF ECOTYP(WKPT) EQL LTP ... IS THIS A L. EVENT ?
496 NOTICE THAT EVENTS OTHER THAN
497 LAT AND VERT ARE BYPASSED //
498
499 THEN
500 BEGIN
501 DTOTJ=GETJ(WKPT)
502 DTOTJ=PREVDTOTJ
503 DELTST=DTOTJ-LASTDTOTJ
504 DIST=PREVDTOTJ-DELDTOTJ ... WFIRST TO WLJ
505 WALTER=PREVWALTER+VC MI=PREVWALTER+DELDTOTJ*WFIRST
506 WALTER=PREVWALTER+DELDTOTJ*WLAST
507 ... LIMIT ALT TO THE INTERVAL
508 BETWEEN DTOTJ AND DTOTJ+1 TO THE REAL
509 WHICH THIS IS EQUAL TO
510 DTOTJ+1 TO DTOTJ+1 //
511
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513

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513 T1=ABS(VLL-WLRATE) ;
514 AVEV=5*(PREVJASR+LASTJASR)/(WAL*WZ)/KALTSCLAF) ;
515 T2=(DELJST*DJ)/AVEV ;
516
517 IF T2 LFO 11 ... IF T2 LEQ 11 THEN THE VELOCITY
518 CHNG BETWEEN W(J-1) AND W(LAST)
519 REQUIRES A VEL CHG/ RATE GT OR EQL
520 TO MINRATE //
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ROCKWELL INTERNATIONAL CEDAR RAPIDS IA COLLINS AVION--ETC F/G 1/5
3D/4D AREA NAVIGATION SYSTEM DESIGN, DEVELOPMENT AND IMPLEMENTA--ETC(U)
JUN 77 J M BRUCKNER, F B BENSON DOT-FA72WA-3123

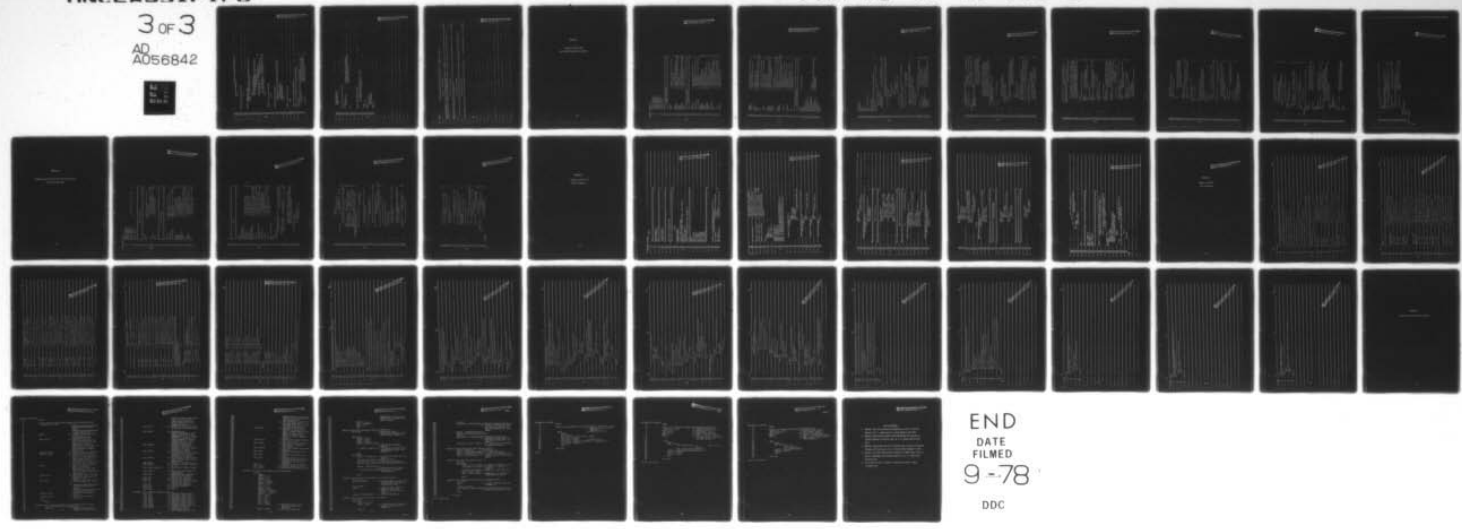
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570 IASFK(WKPT)=PROUTE I
571 END
572
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574
575 COMMENT END OF NO CHANGE LOOP
576
577 ELSE
578
579
580 COMMENT MINRATE ZONE LOOP.
581 CALCULATE A VELOCITY FOR W(J) THAT IS BASED ON A 40 KT/MTN
582 VELOCITY RATE BETWEEN W(J-1) AND W(J).
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... ASSIGN SAVE SPEED AS PREVIOUS WPT //

IASFK(WKPT)=PROUTE I
END

COMMENT END OF NO CHANGE LOOP

ELSE

COMMENT MINRATE ZONE LOOP.
CALCULATE A VELOCITY FOR W(J) THAT IS BASED ON A 40 KT/MTN
VELOCITY RATE BETWEEN W(J-1) AND W(J).

BTG11
P=VISM2=PREVIASR+PREVIASR I
JIASR=PROUTE(I=PRVISR2+(LASTIASR-LASTIASR-PRVISR2)*
(OPP-VELUIST)/DPP) I
... CALC SPEED AT W(J)
IASK(WPT)=JIASR I ... ASSIGN NEW SPEED
IF JIASR LES PREVIASR ... IF SPEED DECREASES FROM
W(J-1) TO W(J)
THEN IASFK(WPT)=PRODM ... AND EITHER ARROW DOWN //
ELSE IASFK(WPT)=PROP I ... OR ARROW UP //

END I

COMMENT END OF MINRATE ZONE LOOP

END I

COMMENT END OF MINRATE LOOP.

IF REPLACE(AREVNO(WKPT),ABEVNO(WKPT),ONEITM,ZILCH,WKPT)
REQ CDRTN
THEN GOTO VERHUPATE I
PREVTAS=IASR(WKPT) I
PREVCFI=DUFTO(WKPT) I
END I

COMMENT END OF LATERAL LOOP.

END I

COMMENT END OF VELOCITY CHANGE LOOP.

COMMENT PRIME PARAMETERS FOR NEXT PROFILE COMPUTATION

RLATPROFILE I
... RECEIVE PARAMETERS FOR NEXT PROFILE COMPS
... WILL START SEARCH FOR NEXT SPEED
CONTROL WPT WITH THE LAT. EVENT
FOLLOWING THE LAST SPEED CONTROL //

FAST=LAST I
... TAKE PRST PARAMETERS //

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```
627 OFTURSI=DEFICIAST ;  
628 FFSTIASR=LASTASK ;  
629 FND ;  
630  
631  
632  
633 COMMENT END OF FIRST VALID LOOP  
634  
635 VERUPDATE $  
636 COMPFF=INVALID ; ... INVALIDATE COMPFF TO INDICATE THAT  
637 SPCD PKGFILES HAVE BEEN UPDATED FOR  
638 EXISTING FLIGHT PLAN. //  
639  
640  
641  
642  
643  
644 DEFINE REAL PROCEDURE SIGN(X)  
645 ...  
646 THIS PROCEDURE TAKES THE SIGN OF A NUMBER .  
647 IE SIGN(-5) = -1, SIGN(10) = 1 .  
648 //  
649  
650 WHERE REAL X ;  
651 TURE  
652 BLGIN  
653 IF X GTO 0.  
654 THEN SIGN=MAX-4  
655 ELSE SIGN=MAX ;  
656 END ;  
657 END FINI
```

NEWS

COLLINS RADIO COMPANY NEWS PROCESSOR LEVEL 1.0 THURSDAY, OCT 23, 1975

MULTI-TPK OCT 22 1975

A NEW TPR PROCESSOR NOW ON THE SYSTEM WILL ALLOW MULTIPLE COPIES TO MULTIPLE SITES. MAXIMUM SITES=3, MAXIMUM COPIES PER SITE=9.
EX-AMPL ***** 7/27PM MMS011/3,MMS011/2,P2/5
WOULD SEND 3 COPIES TO REMOTE MMS011, AND 5 COPIES TO THE UNSITE 1104 PRINTER IN BUILDING 400.

NEWS-LIMIT OCT 22 1975

EFFECTIVE IMMEDIATELY NO DEMAND USER WILL BE ALLOWED TO SIGN ON WITH MORE THAN 15 MINUTES ESTIMATED HIGH TIME DURING WAKEUP SHIFT.
PRIVE SHIFT IS 8:00 AM TO 6:00 PM DALLAS TIME.

MISOB-OUTAGE OCT 22 1975

THE U-1708 WILL BE OUT OF SERVICE FROM 0400 P.M. UNTIL 1200 P.M. SATURDAY OCTOBER 25, 1975 FOR SYSTEM PROGRAM TEST.

SOFTWARE-INDX AUG 29 1974

INDEX OF SOFTWARE AVAILABLE ON THE COLLINS U-1108 SYSTEM - FOR LISTING INSERT .. '77/RELEASES SOFTWARE-INDX' IN YOUR NEWSSTREAM

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APPENDIX C

Program Listing of the
Base System Time Control Algorithm

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40=CREFILL.TL00176A2

```

1 BEGIN
2 .INSEMI PDEF611 ;
3 .INSEMI STRUCT15 ;
4 .INSEMI COM101PS ;
5 .INSEMI DATA611 ;
6 .INSEMI AED15 ;
7 .INSEMI KAT10PACK ;
8 .INSEMI HTA10611 ;
9 .EXTERNAL GMTSF ;
10 .EXTERNAL CBRU ;
11
12 .....
13 INTEGER DECLARATIONS
14 .....
15
16 INSEEN
17 CBRU,
18
19
20
21
22
23
24
25
26
27
28
29
30
31
32
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56
REAL
VCURTMAX,
VLOMTMAX.G1,
VCURTMAX.CBRU,
ABSOCIN,
ACTIAS,
ACTIASRR,
ACALT,
KZ,
PREVCFIO,
PREVIASR,
KALI,
KALTSALL,
UJ,
T1,
AVEV,
ACALTO,
ACALTOB,

```

```

.....
... AIRCRAFT TYPE SPECIFIED BY LINK EDIT
C860 = 0 FOR G-1
      = 1 FOR C860
...
... BUS EVENT NO. OF JHM LAT EVENT
... SPECIFIES LATERAL FROM-EVENT NUMBER
... 10-EVENT FLAG. EXPLAINED IN DETAIL LATER//
... EXT INTEGER
... EXT NOT ENTERED FLAG
... INTERNAL VALUE REPRESENTING TEN SECS
... INTERNAL TIME UPDATED EVERY TEN SECONDS//
... A CONSTANT VALIDITY FLAG
.....
REAL DECLARATIONS
.....
... IAS INSTRUMENT UPPER LIMIT FOR
  COMMANDED IAS
... VCOVI UPPER LIMIT (300 KTS) FOR G-1
... IAS INSTRUMENT
... VCOVI UPPER LIMIT (410 KTS) FOR C-860
... IAS INSTRUMENT
... FACSICCOHPREV
... AIRCRAFT TRUE AIR SPEED
... IAS INSTRUMENT ERROR
... AIRCRAFT ALTITUDE
... AIRCRAFT OP WPT ALTITUDE
... JUST BEFORE TO-EVENT AND W(U-1)
... IAS OF W(U-1)
... ALTITUDE PROPORTIONALITY CONSTANT
  USED TO CONVERT IAS TO TAS
... KALT SCALING FACTOR
... ALONG TRK DIST BEFORE W(U-1) AND W(U)
... TIME TO FLY FROM W(U-1) TO W(LAST)
... AT RATE OF MIRMAIL
... AVE VLL REQUIRED FOR A LINEAR SPEED
  PROFILE BETWEEN W(U-1) AND W(LAST)
... EAST COMPONENT OF WIND
... NORTH COMPONENT OF WIND

```


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```
114 PMLVDFIOF3. ;
115 KALTSSCALE=1 ;
116 KVALRU ;
117 PRU ;
118 PRSD ;
119 AVLVD0. ;
120 PRU ;
121 ELFINE PROCDURE IPRCH ;
122 TUBE
123 PRU ;
124 ORU POINTER WPT ;
125 ORU THUNDER ABLVU ;
126 ORU REAL ACTAS.DLT.ITUNOW.TASPREV.T1.T2.KALT.VGRW0 ;
127 GRIP $B GRT1 ;
128 WPTZKAL ;
129 IF .CLOCK1-FALCLCK LFS ILSSEC //
130 AND TCRH NEG VALID //
131 THEN WOTO EGST1 ;
132 FALCLCK=ELCCK1 ; //
133 FALCLCK=ELCCK1 ; //
134 ... INITIALIZE WORK AREA POINTER //
135
136 ...
137 IF VCOM1=1P GATSE GRT 0 //
138 THEN IVOM1 //
139 ELSE //
140 IF TASP(AH01) GRT 0 //
141 THEN IVOM1 //
142 ELSE //
143 IF ISTR(ELCCK IANZF) GRT 0 //
144 THEN AVALT //
145 ELSE (HDATA) NEG NDATA //
146 THEN GOTO EGST1 ; //
147
148 ...
149 DETERMINE VCOM1MAX, THE UPPER LIMIT FOR VCOM1, AS REQUIRED //
150 BY THE AIRCRAFT IAS INSTRUMENT //
151 VCOM1MAX = IF LDC CDBU GRT 0 THEN VCOM1MAX-CDB0 //
152 ELSE VCOM1MAX.G1 ; //
153
154 ...
155 NOW CHECK VALIDITY STATUS OF FROM-EVENT. WILL EXIT IF //
156 FROM-EVENT IS NOT IN FLPLAN. THERE IS A VERSION MISMATCH //
157 OR NO SPEED IS DEFINED FOR FROM-EVENT //
158 IF GETTIME(ELCCK FROM-EVENT) NEG GURTA //
159 OR IAS (GRT) LCL HOLDS //
160 THEN GOTO EGST1 ; //
161
162 ...
163 GET ( ) ; //
164 GET A SHAPSHOT OF SENSOR DATA //
165 TO GET A GOOD SHAPSHOT //
166 ... AIRCRAFT TRUE AIR SPEED //
167 ... AIRCRAFT ALTITUDE //
168 ... IAS INSTRUMENT ERROR //
169 ... NORTH COMPONENT OF WIND //
170 ... EAST COMPONENT OF WIND //
171 ... INITIALIZE HC TO THE AIRCRAFTS ALT //
```


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```

228 T1=ASJ(SV*MINRATE) : ... TIME TO FLY REQUIRED BY AT.
229 ACCELERATION OF 1/MINRATE //
230 AVEL=0.5*(TASPREV+TAS)*RAIK :
231 T2=ASJ(SV/AVEV) : ... TIME TO FLY THE PRESENT LEG
232 ASSUMING IT IS FLOWN AT AVEV //
233
234 ...
235 CAN NOW DETERMINE THE TYPE OF PROFILE TO BE FLOWN
236 FOR THIS LEG. IF T2 LCG T1 THEN THE VELOCITY CHANGE
237 BETWEEN W(U-A) AND W(U) WILL BE AT A CONSTANT RATE
238 CLO Migrate FOR A TIME T2. OTHERWISE THE LEG IS FLOWN
239 AT A CONST VELOCITY FOR DISTANCE UP AND AT AN
240 ACCELERATION OF MINRATE FOR DISTANCE DPP AND TIME T1
241 //
242 IF T2 LEQ T1
243 THEN
244 FOR GREATER THAN OR EQUAL TO MINRATE //
245 BEGIN
246 DUELE12 : ... TIME TO FLY THE LEG //
247 DPP=DU : ... DPP IS THE LEG DISTANCE //
248 END
249 ELSE
250 FOR LESS THAN Migrate //
251 BEGIN
252 DUELE1 : ... TIME TO FLY THE CHANGE IN VELOCITY //
253 DPP1=AVLV : ... DISTANCE TO DO THE SAME //
254 END
255
256 ...
257 DETERMINE IF W(U) IS THE TO-EVENT //
258 TRUE IF W(U) IS TO-EVENT //
259 THEN
260 BEGIN TO-EVENT BLOCK //
261 BEGIN
262 WCONIF=IASVALU : ... VALIDATE COMMAND IAS VAL FLAG //
263 VTIMEFTFAF : ... TRAFF IS SET VALID-INVALID BY FPMON.
264 IF THERE IS NO TIME FIX WE LEAVE
265 CALCUL BLOCK AFTER CALCUL TIGORA //
266 WAKTUWRAIK : ... ALONG TRACK WIND COMPONENT TO-EVENT //
267 IF LOWIAS NEG VALID ... IF TRUE AIR SPEED IS LESS
268 THAN TASLIM (150 KTS) * HOLD //
269 KALTU CONSISTI //
270 THEN KALTUWRAIK : ... OTHERWISE UPDATE KALTU //
271
272 ...
273 NOW DECIDE IF THERE WILL BE A VEL CHNG BETWEEN THE //
274 FROM AND TO EVENTS
275 IF T2 LEQ T1 OR DMTG LCG DPP //
276 THEN
277 ... DETERMINE DELT FOR A VELOCITY RATE //
278 GREATER THAN MINRATE //
279 BEGIN
280 VGTASPREV+RAIK : ... W(U-1)+WIND(U) //
281 VGTASU+RAIK : ... W(U)+WIND(U) //
282 LIMIT DMTG TO LEG DPP //
283 IF DMTG ORI DPP //
284 THEN DTGUPPERMAXON //
285 ELSE DTGUPPERMAXON //
286 ELSE DTGUPPERMAXON //
287 ELSE DTGUPPERMAXON //
288 ELSE DTGUPPERMAXON //
289 ELSE DTGUPPERMAXON //
290 ELSE DTGUPPERMAXON //
291 ELSE DTGUPPERMAXON //
292 ELSE DTGUPPERMAXON //
293 ELSE DTGUPPERMAXON //
294 ELSE DTGUPPERMAXON //

```

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```

285 IF UNTG GR1 DPP
286 THEN DELT=T2*(DM1G-DMP)/AVGNOM
287 ELSE
288 DELT=DM1G/10.5*(V61GOM+VF1) ;
289 END
290
291 ELSE ... NO VEL CORR REQUIRED FOR FIRST PART
292 OF THIS LEG INTO TO-EVENT. DETERMINE
293 HOW MUCH OF LEG IS LEFT TO FLY AND
294 HOW LONG IT WILL TAKE //
295
296 BEGIN
297 V61GOM=V1ASPREV*W1K ;
298 UP=DM1G-DPP ; ... PORTION OF LEG REMAINING TO BE FLOWN
299 AT CONSTANT VELOCITY //
300 DELT=T1+UP/AVGNOM ; ... TIME TO FLY THIS PORTION //
301 END ;
302
303 ...
304
305 NOW DETERMINE ITG TO TO-EVENT //
306 ITGOM=ITGOM+DELT ; //
307 END
308
309 ...
310
311 BEGIN BEYOND TO-EVENT BLOCK //
312 DETERMINE T1G UP TO THE TIME FIX. INCLUDED //
313 ARE CORRECTIONS FOR LEG CAPTURE AT W1G-1) //
314 AND VALIDATE CALCULG COMPUTATIONS FOR //
315 COCH GEG 1G0 //
316 BEGIN
317 IF T2 GR1 T1 //
318 THEN
319 BEGIN
320 OPENJ-DPP ; ... SECTION OF LEG FLOWN AT CONSTANT //
321 VELOCITY. TASPRLY. //
322 DELT=T1+DP/(TASPREV+W1K) ; ... TOTAL TIME TO FLY LEG //
323 END ; //
324
325 ITGOM=ITGOM+DELT ; ... ADD THIS LEG TO THE TOTAL //
326 TIME TO GO TO T-FIX //
327
328 ...
329
330 WILL NOW MAKE ADJUSTMENT FOR SLIGHTLY DIFFERENT //
331 PATH FLOWN DUE TO TURNS. ECI NOT ALLOWING //
332 COURSE CHANGES GEG 1G0 DEGREES //
333 IF ABS(COCHPREV) GEG D1G0 //
334 THEN
335 BEGIN
336 INVALID COCH //
337 VCOCH=V1GUCH ; ... INVALIDATE COMMANDD IAS FOR //
338 GEG 1G0S11 ; //
339 END ; //
340
341 ...
342
343 VALID COCH //
344 ABS(COCH)=ABS(COCHPREV) ; //
345 DELT = GEG*ABS(COCH)/COS(10.5*ABS(COCH)) //
346 - ABS(10.5*ABS(COCH))/SIN(10.5* //
347 ABS(COCHPREV)/DELT+PI/180) ; //
348
349 ...
350
351

```

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```

342 DELT = DELT*(0.5*ACOS(0.5*ABS(COCH)) : //
343 TIGOR=TI(0.5*DELTA) : ... AND TO TIGOR //
344 END : //
345 END RETURN TO EVENT BLOCK //
346 COCH=ARLVECS(S(KRPT))-CRS(KRPT) : //
347 PREVIAS=IAS(KRPT) : ... UPDATE COCHREV //
348 END //
349 END LATERAL EVENT BLOCK //
350 IS LEVHT APLVJ A VERTICAL EVENT ? //
351 ELSE //
352 BEGIN VERTICAL EVENT BLOCK //
353 THEN //
354 BEGIN //
355 IF NOT TOEVE(WAPT) ... TRUE IF W(U) IS TO-EVENT //
356 THEN HZ=ACALL ... ASSIGN AIRCRAFT ALT TO HZ //
357 ELSE HZ=ALT(KRPT) : //
358 ... ASSIGN ALT(DJ) TO HZ //
359 END : //
360 ARFVJ=ARVJ+1 : ... INCREMENT EVENT NUMBER //
361 END : //
362 ... END CALCUL BLOCK //
363 TIMCALC //
364 IF (TIMERR=TCOMF .V. TFIX) NEO VALID ... SET TIMERR FLAG //
365 THEN //
366 BEGIN //
367 KERSCALE : ... IF THERE IS NO TIME-FIX OR TCOMF //
368 ... THEN TIGCOM AND HZSCALE ALSO K CAR NOT BE //
369 DETERMINED SO LET KERSCALE //
370 ... VALID SO WE CAN CALC VCO*1,VCOM1 //
371 KVAL=KVAL : //
372 END //
373 ELSE //
374 OPTI=(COM-OMIS) : ... CONVERTS INTEGER TO REAL //
375 TIGCOM=OPTI/VICOM : ... BECAUSE GRIV 323 OYTI //
376 KVAL=KVAL : ... CALC THE CORRECTED TIG FOR ARRIVAL //
377 AT THE TIME FIX //
378 KVAL=KVAL : ... INITIALLY SET KVAL INVALID //
379 IF THE PRODUCT OF TIGCOM AND KSCALE IS LFSS //
380 THAT THE ABS(TIGCOM) WE WILL HAVE A MEANTIMEFULL //
381 CONSTANT K. GENERALLY THIS PROTECTS AGAINST THE CASE //
382 WHERE TIGCOM GOES TO ZERO //
383 IF KVAL=0 ... KSCALE LEW ABS(TIGCOM) //
384 THEN //
385 BEGIN //
386 KVAL=ABS(TIGCOM) : //
387 KVAL=KVAL : //
388 END : //
389 END : //
390 IF VCO*1 EQV IASVALID ... VCO*1 WILL NOT BE VALID FOR //
391 THE CASE WHERE THERE IS NO SPEED DEFINED //
392 FOR THE TO-EVENT OTHERWISE ITS VALID //
393 THEN //
394 BEGIN //
395

```

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```
599      ...
600      IF KVAL EQL VALIU
601      THEN
602      BEGIN
603      VCOMI=(K*VGMNU)/SCALE*WAKTO ; ... CALC COMMANDED TAS
604      VCOBI=(MAXON-(CALIJD@VALI)/KALISCALE)*VCOMI ;
605      ... CONVERT VCOMI TO IAS
606      VCOMI = MAXAFIRMIMP(VCOMI*(COIMAX), 0) ; ... RESTRICT VCOMI
607      TO LIMITS IMPOSED BY THE IAS INSTRUMENT
608      END ;
609      IF TIMEHF EQL VALIU ... IF THERE IS A TIME-FIX UP COMMANDED
610      THEN TIME THEN CAN CALC TIMEHF
611      THEN
612      EARLY=(TIGNUM*VGMNU)/(ACTAS*WAKTO)-TIGCOM ;
613      ... CALC THE EXPECTED TIME ERROR FOR
614      ARRIVAL AT THE TIME FIX
615      TIMEHF=ABS(EARLY) ; ... DO THIS TO MAKE CORRECTION FOR NEGATIVE
616      NUMBERS
617      END ;
618      EGSITS
619      FCONF=INVALID ;
620      END ;
621      END FINI
622
623      SPT.S D.TCONZFAI
```

APPENDIX D

Program Listing of the 2D Plus Time Control System
Time Control Algorithm


```

171 G*FI = ICOM - GMS ; //
172 //
173 ... INTEGER ARITHMETIC REQUIRED //
174 TIGCM = INTX/GXICGM ; //
175 ... CONVERT TO NAV TIME UNITS //
176 //
177 CALCULATE VALUES FOR COMMANDS TAS //
178 AND COMMANDS IAS. //
179 //
180 //
181 //
182 //
183 //
184 //
185 //
186 //
187 //
188 //
189 //
190 //
191 //
192 //
193 //
194 //
195 //
196 //
197 //
198 //
199 //
200 //
201 //
202 //
203 //
204 //
205 //
206 //

```

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APPENDIX E

Program Listing of ILS
Executive Routines

```

10 WORKF1, E, ILSBMDA1
1 BEGIN
2
3
4
5
6 .INSERT LCGSIDJ1 $
7 .INSERT MATHPACK $
8
9
10
11 .INSERT NTARM611 $
12 .INSERT AELIB $
13
14
15
16
17
18
19
20
21 BEGIN
22
23
24 PROCEDURE GSCMP $
25 PROCEDURE LOCCMP $
26
27 COMMENT INTERNAL DECLARATIONS $
28 BOOLEAN LOCARM, LOCAP, GSCAP, GSARM, RESFTG,
29 LOCTR $
30 REAL LATDIS, LNCDIS $
31 INTEGER AC, POE $
32 COMMENT SET ILS VARIABLES TO ANAV VARIABLES $
33
34
35
36
37
38
39
40
41
42
43
44
45
46
47
48
49
50
51
52
53
54
55
56

```

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```

COMMENT ***** DATA DECLARATIONS FOR LOGIC USED TO DRIVE
THE MSI TO/FROM FLAG ***** $
REAL TOCRSDEV I
REAL REG90 I
REAL ARRAY TOP0e11 I
... TAE RELATIVE TO TOUCHDOWN ANU
... 90 DEGREES
... COORDINATES OF TOUCHDOWN USED FOR

```

```

57 CALL TO LTRUD. ARRAY IS NEEDED TO
58 ENSURE CONSECUTIVE CORE LOCATIONS
59 FOR TOUCHDOWN COORDINATES. //
60 REAL ARRAY ACTOTD(2) I ***
61 USED TO RECORD LTRUD BEARING AND
62 DISTANCE COMPUTATIONS BETWEEN THE
63 AIRCRAFT AND TOUCHDOWN. //
64 ACTOTD ELEMENT USED TO RECORD BEARING
65 FROM AIRCRAFT TO TOUCHDOWN
66 ACTOTD ELEMENT USED TO RECORD BEARING
67 FROM TOUCHDOWN TO AIRCRAFT
68 ACTOTD ELEMENT USED TO RECORD
69 DISTANCE BETWEEN AIRCRAFT AND
70 TOUCHDOWN. //
71 PRESET
72 TDCRDEV = .0 I
73 DEGR0 = .5 I
74 TPOSD = .0.0 I
75 ACTOTD = .0.0.0.0 I
76 END I
77 LOCDEV = LOC(ADHD) S.
78 GSDDEV = GSI(ADHD) S.
79 AIRSPD = TAS(ADHD) S.
80 ACHOG = PSIM(ADHD) S.
81 SELVAL = IF LOC(ADHD) EOL 0 THEN TRUE ELSE FALSE S.
82 COMVAL = IF IBYTEO (LOC HEADF) EOL 0 THEN TRUE ELSE FALSE S.
83 SFGVAL = IF GSF(ADHD) EOL 0 THEN TRUE ELSE FALSE S.
84 ALTVL = IF IBYTEO(LOC HZH2F) EOL 0 THEN TRUE ELSE FALSE S.
85
86
87
88
89 COMMENT SET ANNUNCIATORS FALSE S.
90 PRESET
91 BEGIN
92 LUCARM = FALSE S.
93 LUCCAP = FALSE S.
94 GSRM = FALSE S.
95 GSCAP = FALSE S.
96 END *** PRESET ANNUNCIATORS FALSE
97
98 COMMENT SET ACTIVE MODE TO RNAV ** RNAV IS ONE ** LOC IS TWO **
99 APPR AUTO IS THREE S.
100 PRESET
101 BEGIN
102 ACTMDE = 1 S.
103 END *** PRESET ACTIVE MODE S.
104
105 COMMENT SET LOCTRK FALSE S.
106 PRESET
107 BEGIN
108 LOCTRK = FALSE S.
109 END *** SETTING LOCTRK S.
110
111 COMMENT INITIATE RESETS S.
112 PRESET
113 BEGIN

```

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```

178 IF (IREQMOD EQL 1) AND RHAVAL1
179 THEN BEGIN
180   LOCARM = FALSE $;
181   NAVCAP = FALSE $;
182   LOCCAP = FALSE $;
183   GSARM = FALSE $;
184   GSCAP = FALSE $;
185   END
186   ... RESET ANNUNCIATORS FALSE $;
187   IF (IREQMOD EQL 1) AND RHAVAL1 OR (IREQMOD
188     EQL 2) AND LOCCAL) OR (IREQMOD EQL 3) AND
189     AVAL1)
190   THEN ACTMDE = REQMOD $;
191   ... END CHECKING REQUESTED
192   MODE VALIDITIES $;
193   END $;
194
195 COMMENT SERVICE COMPUTATIONS , SET FLAGS $;
196 IF ACTMDE NEQ 3
197 THEN BEGIN
198   IF ((ACTMDE EQL 2) AND LOCCAL) OR ((ACTMDE
199     EQL 3) AND AVAL1)
200   THEN CPEFLG = TRUE
201   ELSE CPEFLG = FALSE $;
202
203   ...
204   LOCMP(RESETL,LOCDFV,BANK,LANGUIS,LATDIS,LOCARM,LOCCAP,
205     LOCTRK,BKCMDA,BKCMDF)
206   $;
207   ...
208   RSETL = FALSE $;
209   IF NOT LOCARM
210   THEN BEGIN
211     PHICA = BKCMDA $;
212     PHICF = BKCMDF $;
213     END ... OUT LATERAL BANK CMDS $;
214     IF ACTMDE NEQ 2
215     THEN BEGIN
216       PTCFDA = VSAC $;
217       PTCDFD = VSAC $;
218
219   ...
220   GSCMP(GSDEV,RNGTD,VALTRTE,TIMD,RESETG,GSARM,USCAP,LOCARM,PTCMDA) $;
221   ...
222   MESETG = FALSE $;
223   IF NOT GSARM
224   THEN BEGIN
225     VSCCA = PTCMDA $;
226     VSCLF = PTCMDF $;
227

```

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```

228 END ... OUT PITCH_CMDS $,
229 END $,
230 END ... END OF PROCESSING STEERING
231 COMPUTATIONS //
232 ELSE BEGIN
233 R-SETL = TRUE $,
234 R-SETG = TRUE $,
235
236 END $,
237
238
239
240
241 LOCAA = LOCARM $,
242 LOCCA = LOCCAP $,
243 GSA = GSARM $,
244 GSCA = GSCAP $,
245 STAHN = *CTMDE $,
246
247
248
249
250 COMMENT ***** CONTROL THE HSI TO/FROM FLAG BY ASSIGNING ONE OF THE
251 FOLLOWING VALUES TO THE RWAY FLAG CALLED TOWARD
252
253 TOWARD = 1 IF AIRCRAFT HAS NOT PASSED THE PERPENDICULAR
254 TO RWYHDG AS CONSTRUCTED AT TOUCHDOWN,
255 = 0 OTHERWISE . ***** $,
256
257 IF LOCARM OR LOCCAP
258 THEN BEGIN
259 TDPOS(0) = LATTDI
260 TDPOS(1) = LONGTD I
261 ILTBD(LOC LATAP, LOC TDPOS, LOC ACTO'D) I
262 TDCKSEV = RWYHDG - ACTO'D(BRG.TUOAC) I
263 TOWARD = IF ANS(TDCKSEV) GRT DEG90
264 THEN 1
265 ELSE 0 I
266 END I
267
268 ... END OF LOGIC THAT CONTROLS THE
269 HSI TO/FROM FLAG //
270
271 ... END OF SERVICING COMPUTATIONS, SETTING FLAGS $,
272
273 END $,
274
275 END FINI

```

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APPENDIX F

Program Listing Of
Localizer Routine


```

114 REAL CDBANK *** MAX VALUE OF BANK (RADIANS) :
115 REAL REFROT *** REFERENCE FRAME ROTATION ANGLE
116 (RADIANS) :
117 REAL CTU *** CROSS TRACK DISTANCE FROM NAV DATA
118 (FT) :
119 REAL CTCHAY *** CROSS TRACK DISTANCE FROM NAV DATA
120 (FT) :
121 REAL TAL *** TRACK ANGLE ERROR (RADIANS) :
122 REAL Y6 *** GROUND SPEED (FT / SEC) :
123 // *** TRACK VARIABLES *** //
124 //
125 // LOCALIZER TRACK TRIP POINT
126 (MICROSECS) :
127 REAL ABSDC *** ABSOLUTE VALUE OF DC-MISC (RADIANS) :
128 REAL TACMP *** VARIABLE USED IN COMPUTATION OF
129 TACTRK :
130 REAL TACTRK *** THEORETICAL TRACK ANGLE ERROR (RADIANS) :
131 TRACK (RADIANS) :
132 REAL DCOTK *** BANK CMD - TRACK (DEG) :
133 REAL CTBTRK *** CROSS TRACK RATE - TRACK (FT / SEC) :
134 REAL CTOTK *** CROSS TRACK DISTANCE - TRACK (FT) :
135 REAL KCOTK *** GAIN ON CROSS TRACK DISTANCE - TRACK
136 (DEG / FT) :
137 REAL FCOTK *** FUNCTIONAL MULTIPLIER IN GAIN ON
138 CROSS-TRACK DISTANCE :
139 REAL KCOTRK *** GAIN ON CROSS TRACK RATE - TRACK (DEG
140 / INT / SEC) :
141 REAL FCOTRK *** FUNCTIONAL MULTIPLIER IN GAIN ON
142 CROSS-TRACK RATE - TRACK :
143 REAL MAXRNG *** MAXIMUM RANGE TO LINEARIZE TRACK LAWS
144 (FT) :
145 REAL RUSHGK *** GAIN ON OUTPUT OF RUSHO - LAMB TRACK :
146 REAL KFADTK *** GAIN ON FASER IN TRACK :
147 REAL TFADTK *** TIME CONSTANT OF FASER IN TRACK (SEC)
148
149 REAL DELTK *** OUTPUT OF TRACK FASER (DEG) :
150 REAL WASHOT *** BANK WASHOUT TIME CONSTANT (SEC) :
151 REAL BURKOP *** BANK WASHOUT LIVITY (DEG) :
152 REAL BURKLP *** LO-PASSED BANK (DEG) :
153 REAL KOTK *** ELAPSED TIME AFTER LOCKIN THAT BANK
154 WASHOUT IS INSERTED (SEC) :
155 REAL TPASTR *** ELAPSED TIME AFTER LOCKIN (SEC) :
156 REAL FILEAD *** GAIN ON FASER OF FILEC :
157 REAL TRPOT *** COUNTER USED TO DETERMINE WHEN TO
158 TRIP IN INCREASED BANDWIDTH IN FILTER
159 C (SEC) :
160 REAL FILING *** NUMBER OF SECONDS AFTER TRACK WHEN
161 INCREASED BANDWIDTH IS TRIPPED INTO
162 FILTER C (SEC) :
163 REAL YKREIC *** VARYING BANDWIDTH PARAMETER OF FILTER
164 C :
165 REAL DIFILC *** VARYING PARAMETER USED IN COMPUTING
166 FILEC :
167 REAL FIDREC *** FASER BANDWIDTH PARAMETER USED IN
168 FILTER C :
169 REAL FADTIC *** TIME CONSTANT OF THE INCREASED

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171 BANDWIDTH PAPER USEL IN FILTER C
172 (SEC) : ... //
173 //
174 ... ** * COMMON I/O VARIABLES ** ** *
175 //
176 RANGE TO LOCALIZER (FT) : ... //
177 //
178 ... ** * COMMON VARIABLES ** ** * //
179 //
180 LOCALIZER DEVIATION THROUGH RATE
181 LIMITER (MICROAMPS) :
182 LOCALV - LOCALV (MICROAMPS) :
183 MAX LOCALIZER DEVIATION DIFFERENCE
184 BETWEEN LOCALIZER (MICROAMPS) :
185 COMPUTATIONAL TIME INCH/SEC (SEC) :
186 ACCELERATION FEED INTO FILTER C (FT /
187 SEC) :
188 POLI - ZERO PARAMETER OF FILTER C :
189 INITIAL BANDWIDTH PARAMETER OF FILTER
190 C :
191 ... TRUL UNTIL FIRST GENERAL I/O OF BKCRDA
192 ... RATE LIMIT ON BANK CMD (LEG / SEC) :
193 ... AMPLITUDE LIMIT ON BANK CMD (DB) :
194 ... MAXIMUM ALLOWABLE CHANGE OF BKCRDA
195 (DB) :
196 ... LAST VALUE OF BKCRDA - SAVED BEFORE
197 LEAD-LAG (DB) :
198 ... LAST VALUE OF BKCRDA OUTPUT BY LOPASS
199 OF LEAD-LAG (DB) :
200 ... DIFFERENCE BETWEEN PRESENT BANK
201 COMMAND AND LAST (LEG) :
202 ... TIME CONSTANT FOR THE LEAD-ON-BANK
203 CMD (SEC) :
204 ... TIME CONSTANT FOR THE LAG ON BANK CMD
205 (SEC) : ... //
206 //
207 REAL SCAL1,SCAL2,SCAL3,SCAL4,SCAL5,SCAL6,SCAL7,SCAL8,SCAL9,SCAL10,
208 SCAL11,SCAL12,SCAL13,SCAL14,SCAL15,SCAL16,SCAL17,SCAL18,SCAL19,
209 COMPI,COMP2,COMP3,COMP4,COMP5,COMP6 :
210 REAL PROCEDURE LIMIT,LOPASS,HEAP :
211 PROCEDURE PROCE : ... //
212 //
213 PRESET
214
215 BEGIN
216 TIMSTP = 2 :
217 KEALOC = 010751 :
218 KEALOC = 063709 :
219 FALFAC = 023356 :
220 KEJDK = 032375 :
221
222 KEJTK = 050 :
223
224 PARAMG = 042532 :
225 KEJLN = 06067 :
226 RATELN = 050556 :
227 RATELN = 05 :
228
229 EXP(-TIMSTP / 1. ) :
230 EXP(-TIMSTP / 5. ) :
231 EXP(-TIMSTP / 30. ) :
232 1. / ( 0. ((14. / 100. ) / (70. /
233 15.)) ) :
234 1. / ( 35. / 100. ) / (70. / 153. ) :
235
236 PARAMG = 042532 :
237 KEJLN = 06067 :
238 RATELN = 050556 :
239 RATELN = 05 :
240
241 EXP(-TIMSTP / 1. ) :
242 EXP(-TIMSTP / 5. ) :
243 EXP(-TIMSTP / 30. ) :
244 1. / ( 0. ((14. / 100. ) / (70. /
245 15.)) ) :
246 1. / ( 35. / 100. ) / (70. / 153. ) :

```

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226 MFILC = .3015 ... 3.0306 / 10.1
227 FILTERP = .50 ... 50. / 100.1
228 FIMALC = .06992 ... 10. / 10.1
229
230
231 DEBULK = .5
232 DEBULK = .01111 ... 2. / 100.1
233 DEBULK = .10 ... 10. / 100.1
234 SCAL1 = .002417 ... 1. / 1.0001
235 SCAL2 = .0 ... 200. / 215.1
236 SCAL3 = .007013 ... 300. / 175.1
237 SCAL4 = .041082 ... 1. / 22.1741
238 SCAL5 = .044444 ... 8. / 100.1
239 SCAL6 = .034914 ... 1. / 1117. / .1492. / .113. / .0016.
240
241 SCAL7 = .108809 ... 25. / 100.1
242 SCAL8 = .027170 ... 5. / 100.1
243 SCAL9 = .605607 ... 200. / 200.1
244 SCAL10 = .006545 ... 2.667 / 57.51
245 SCAL11 = .5 ... 1. / 100.1
246 SCAL12 = .5 ... 100.1
247 SCAL13 = .005 ... 100. / 100.1
248 SCAL14 = .002 ... 100. / 100.1
249 SCAL15 = .020089 ... 7. / 100.1
250 SCAL16 = .009 ... 9. / 100.1
251 SCAL17 = .7023 ... 1. / 1.31
252 SCAL18 = .028980 ... 113. / 6076. / 150.1
253 SCAL19 = .042211 ... 7.776 / 100.1
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F-6

IF RESET
JREN P0214
265 LCCAMP = TRUE
266 LCCAMP = FALSE
267 LCCAMP = FALSE
268 LCCAMP = FALSE
269 LCCAMP = FALSE
270 LCCAMP = FALSE
271 LCCAMP = TRUE
272 LCCAMP = TRUE
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276 LCCAMP = FALSE
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279 LCCAMP = FALSE
280 LCCAMP = FALSE
281 LCCAMP = FALSE
282 LCCAMP = FALSE

COMMENT

COMMENT THE FOLLOWING CARDS MUST BE REMOVED BEFORE CROSS-COMPILING :

```

285 .....
286 .....
287 .....
288 REAL PROCEDURE LGIN=NCOSINTAN ;
289 LOCDEV = LOCDEV/300. ;
290 .....
291 IF LOCDEV = 0. ;
292 THEN LOCDEV = .99999 ;
293 IF LOCDEV = .99999 ;
294 THEN LOCDEV = 1. ;
295 IF RESET ;
296 THEN LOCDEV = LOCDEV ;
297 DATA = DATA/5.215927 ;
298 MARGIN = MARGIN/3.1415927 ;
299 ACROSS = ACROSS/3.1415927 ;
300 AIRSPD = AIRSPD/100. ;
301 GROUND = GROUND/100. ;
302 RAYTRG = RAYTRG/3.1415927 ;
303 GAMMA = GAMMA/3.1415927 ;
304 RHO = RHO/100. ;
305 LYSOIS = LYSOIS/100. ;
306 PLYTH = PLYTH/10. ;
307 LATDIS = LATDIS/100. ;
308 SCAL11 = 1. ;
309 SCAL12 = 1. ;
310 SCAL13 = .01 ;

```

COMMENT THE ABOVE CARDS MUST BE REMOVED BEFORE CROSS-COMPILING :

```

311 .....
312 .....
313 .....
314 CONVERT .....
315 .....
316 COMMENT ..... DATA_PROCESSING_MODULE .....
317 .....
318 COMMENT ..... RANGE TO LOCALIZER COMPUTATION ..... ;
319 RANGLOC = (RANGLOC*ULTM*.1) + .0076 ;
320 .....
321 COMMENT ..... TRACK ANDLE ERROR COMPUTATIONS ..... ;
322 TAE = (TAE-1.0)/10.0 ;
323 .....
324 COMMENT ..... CHANGE GROUND SPEED FROM KNOTS TO FT / SEC ..... ;
325 VS = GROUND/SCAL1 ;
326 .....
327 COMMENT ..... RATE LIMIT ON LOCDEV ..... ;
328 XLOCV = (XLOCV+1.0)/10.0 ;
329 IF XLOCV = 1.0 ;
330 THEN XLOCV = SCAL16 ;
331 GLOW = LOCDEV-XLOCV ;
332 LOCDEL = LOCDEL-LIMIT*(GLOW/XLOCV) ;
333 .....
334 IF NOT LOCDEL ;
335 THEN BEGIN
336 .....
337 .....
338 .....
339 .....
340 .....
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342 COMMENT ***** NAV CROSS TRACK DISTANCE COMPUTATIONS *****
343 REFPOI = RAYH05*5.
344 CTD = LATDIS*(COS(REFPOI)*LNGDIS+MSIN(REFPOI) :
345 CTUNAV = (CTD*.6076)/.1 :
346 END
347 ***** //
348 ... //
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```

330 CAPDM = (CPBXX/5)*TAE I
340 IF ABS(CAPDM) LES SCALB
350 THEN CAPDM = (SCALB*TAE)/ABS(TAE) I
360 CAPAV = ((VG*2)/(9000-NCOS(TAE))*SCA/4)/(HCSH(CAPDMK)/
370 ACCS(CAPDMK))) I
380 CAPILS = ((TREC1*2/3)*SCAL4*HCS(CAPDMK))/ABSIN(CAPDMK) I
390 *0000*HCS(CAPDMK)/HCS(TAE) I
400 IF ABS(LOCPL) LES SCAL9
410 THEN CAPTR = CAPILS
420 ELSE CAPTR = CAPAV I
430 CAPTR = CAPTR*(CAPDM*VG*01)/(KATLIN/TMSIP) I
440 END I ... //
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```

436      ... TEST FOR TRACK //
437      THEN BEGIN
438      ILSCAP = FALSE ;
439      LCTRK = TRUE ;
440      LCCAPM = FALSE ;
441      LCCAP = TRUE ;
442      END ;
443
444      END ;
445      LCCAP = ILSCAP OR NAVCAP OR LCCAP ;
446      END ;
447
448      COMMENT ***** CONTIN. COMPUTATIONS ***** //
449      ... //
450      IF NOT LCCAP
451      THEN BEGIN
452
453      COMMENT INTERMEDIATE TRACK COMPUTATIONS ;
454      IF PARLOL LES MARKS
455      THEN BEGIN
456      ELSE MARKS = MARKS/RNGLOC ;
457      CTDIRK = MAGNIF*CTLOC ;
458      CTDIRK = MDCORC*CTDIRK ;
459      SCOUTK = CTDIRK/CTDIRK*CTDIRK/CTDIRK ;
460      IF NOT LCTRK
461      THEN BEGIN
462      COMPS = ((CTDIRK**2)/.1)*SCALE4 ;
463      COMPA = CTDIRK*.9999*CTDIRK*NGON(JAEL) ;
464      IF CTDIRK LES .0
465      THEN BEGIN
466      COMPS = -COMPS ;
467      COMPA = -COMPA ;
468      END ;
469      BERLOC = -NIAI(COMPS,COMPA) ;
470      IF NOT ILSCAP
471      THEN BEGIN
472      ANBNC = ANS(BERLOC) ;
473      TALCOP = .9999*((COS(ANBNC)/COS(ANBNC))*RNGLOC*
474      TRDIRP*SCALE3)/(VGM**2) ;
475      COMPS = SORTI(.9999-TALCOP**2) ;
476      TAETRK = .5*(TALCOP+TALCOP*COMPS) ; ... TAETRA =
477      ACOS(TAETRK) //
478      IF TAETRK LES SCALE3
479      THEN TAETRK = SCALE3 ;
480      END ;
481
482      COMMENT NAV CAP COMPUTATIONS ;
483      IF NAVCAP
484      THEN BEGIN
485      IF NOT BLDOWN
486      THEN BLDIN
487      COMPS = (VGM**2)/.1*(.9999-COS(TALCOP))*SCALE4
488      ;
489      COMPS = CTDIRK ;
490      IF CTDIRK LES .0
491      THEN BEGIN
492      COMPS = -COMPS ;
493      END ;
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570 COMMENT

571 COMMENT THE FOLLOWING CARDS MUST BE REMOVED BEFORE CROSS-COLLING

572

573 COMMENT

574

575

576

577

578

579 COMMENT

580

581 COMMENT THE ABOVE CARDS MUST BE REMOVED BEFORE CROSS-COLLING

582

583 COMMENT

584

585

586

587

588

END I

END FINI

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```

1 2LS*REQ,INDEF
2 3      BLCIN
3 4  DEFINE PROCEDURE KROCF(INPUT,PZ,FRQ,TIMSTR,POSITN,RATE,ACCEL)
4 5  AMERF
5 6  REAL INPUT,PZ,FRQ,TIMSTR,POSITN,RATE,ACCEL...//
6 7  TUNE
7 8  BEGIN
8 9  REAL TSC,TCK,TOKS,A11,A12,A21,A22,U11,U12,U21,U22,LSTPOS,LSTRAT,L
9 10  REAL PZPARM,FRQRM ;
10 11  PZPARM = .1/PZ ;
11 12  FRQRM = .1/FRQ ;
12 13  TSC = TIMSTR**2 ;
13 14  TCK = TIMSTR*FRQRM ;
14 15  TOKS = TCK**2 ;
15 16  A11 = .99999-(TOKS*.5) ;
16 17  A12 = -(TCK*FRQRM)*(.99999-((TCK*.5)/PZPARM)) ;
17 18  A21 = -A12/(FRQRM**2) ;
18 19  A22 = (PZPARM*(TCK**2)+A11+A12)/(PZPARM*FRQRM) ;
19 20  U11 = -A12 ;
20 21  U12 = (PZPARM*FRQRM*A21+ (.99999-A11))/(PZPARM*FRQRM) ;
21 22  U21 = .99999-A22 ;
22 23  U22 = (.99999-A11)/(FRQRM**2) ;
23 24  LSTPOS = POSITH ;
24 25  LSTRAT = RATE ;
25 26  RATE = A11*LSTRAT+((A12*LSTPOS)/.02)/.5+((U11*INPUT)/.02)/.5+(U12*
26 27  ACCEL)/.1 ;
27 28  POSITH = (A21*LSTRAT)+U1+A22*LSTPOS+U21*INPUT+(U22*ACCEL)/.001 ;
28 29  END ;
29 30  END FINI

```

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1 2 3 4 5 6 7 8 9 10 11 12
F-3600-10-1
BEGIN
DEFINE REAL PROCEDURE LIMIT(INPUT,LIMVAL) WHERE ... //
REAL INPUT,LIMVAL ... //
TONE
BEGIN
IF ABS(INPUT) LES LIMVAL
THEN LIMIT=L-INPUT
ELSE LIMIT = (LIMVAL+ABS(INPUT))/INPUT ;
END ;
END F-3600-10-1

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2
1 L5=AEQ,L0P55
2 BEGIN
3 DEFINE REAL PROCEDURE L0PASS(INPUT,L5LOPS,STC,STIMST) WHERE ... //
4 REAL INPUT,STC,STIMST,L5LOPS ... //
5
6 BEGIN
7 L5LOPS = L5LOPS*(INPUT-L5LOPS)/(STIMST/SFC) ;
8 L0PASS = L5LOPS ;
9 END ;
10
11 END-FINI

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```
1LS*APC*153  
1 BEGIN  
2  
3 DEFINE REAL PROCEDURE NEXP(X) WHERE ... //  
4 REAL X ... //  
5  
6  
7 BEGIN  
8 X = -X I  
9 NEXP = .4922998 - .2990504 * X + .4982922 * X * X - .1525332 * X * X * X + .021641 * X * X * X  
10 END I  
11  
12 END FINI
```

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APPENDIX G

Program Listing Of Glideslope Routines

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J:WORKFILE.GSCF00A1

```
1 BEGIN
2
3 DEFINE PROCEDURE GSCMP(GSDEV,D,HDOCT,T,RESETG,GSARM,GSCAP,
4 LOCARM,PTCMDA) WHERE ... ..
5 *****
6 *****
7 INPUTS
8 *****
9 ***** //
10 REAL D ... DISTANCE TO TOUCHDOWN 100
11 NM FULL SCALE (+)
12 APPROACHING THE RWAY ;
13 REAL PTCMDA ... EXTERNALLY SUPPLIED
14 STEERING COMMAND, 100 DEG
15 FULL SCALE ***NOTE*** THE
16 INPUT VALUE WILL BE
17 OVERRITTEN IF AND ONLY IF
18 THIS ROUTINE IS IN THE
19 GSCAP STATUS. + IMPLIES
20 PITCH DOWN ;
21 BOOLEAN LOCARM ... TRUE PRIOR TO LOC CAPTURE ;
22 BOOLEAN RESETG ... INITIALIZATION COMMAND ;
23 ... GSCMP IS SET TO THE ARM
24 STATUS AND ALL FILTERS ARE
25 INITIALIZED *** NOTE ***
26 THIS BOOLEAN SHOULD BE
27 EXTERNALLY SET FALSE AFTER
28 THE FIRST CALL TO GSCMP //
29 REAL T ... TIME SINCE LAST CALL TO
30 GSCMP .. INTERNAL
31 COMPUTATIONS ASSUME THE
32 NOMINAL SAMPLE INTERVAL ON
33 THE FIRST ACCESS 10.004 HRS
34 FULL SCALE ;
35 REAL GSDEV ... GLIDESLOPE RADIO DEVIATION
36 300 U-AMPS FULL SCALE (+)
37 ABOVE THE BEAM ;
38 REAL HDOCT ... VERTICAL RATE 500 FEET /
39 SEC FULL SCALE (+) UPWARD ;
40 ...
41 *****
42 *****
43 OUTPUTS
44 *****
45 ***** //
46 BOOLEAN GSARM ... GLIDESLOPE COMPUTATION
47 STATUS ;
48 BOOLEAN GSCAP ... GLIDESLOPE COMPUTATION
49 STATUS //
50 TOBE
51 BEGIN
52
53 COMMENT ***** GAINS CONSTANTS AND CONVERSION FACTORS ***** ;
54 REAL PROCEDURE LOPASS,WSHOOT,LIMIT ;
55 REAL RY ... DIVIDED BY 10) EQUALS
56 : G-2 DEGREES OF PITCH COMMAND /
```

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57 FOOT OF LINEAR DEVIATION OR
 58 MULTIPLIED BY MAXRNG /
 59 .2016 EQUALS DEGREES OF
 60 PITCH COMMAND PER U-AMP
 61 BEYOND MAXRNG NM. ;
 62 REAL KHDOT ... DEGREES OF PITCH COMMAND /
 63 FT PER SEC OF VERTICAL RATE
 64 ;
 65 REAL KYDOT ... MULTIPLIED BY
 66 KHDOT*KDIS*MAXRNG / .2016
 67 EQUALS DEGREES OF PITCH
 68 COMMAND PER U-AMP / SEC OR
 69 MULTIPLIED BY KHDOT / 10.
 70 EQUALS DEGREES OF PITCH
 71 COMMAND PER FT / SEC OF
 72 LINEAR DEVIATION RATE ;
 73 REAL MAXRNG ... DISTANCE BEYOND WHICH
 74 DEVIATION (DELTA) IS
 75 EXPRESSED IN U-AMPS (SCALE
 76 IDENTICAL TO RGTD) ;
 77 REAL BYTODI ... NM(DISTANCE) -SMALL
 78 DOTS(DEVIATION) PER FOOT OF
 79 DEVIATION, A 2.5 DEGREE
 80 GLIDESLOPE IS ASSUMED ;
 81 REAL GAIN10 ... REAL GAIN10 ...DIVISION BY
 82 THIS CONSTANT WILL YIELD A
 83 GAIN OF 10 ;
 84 REAL GAIN5 ... DIVIDE BY FOR GAIN OF 5 ;
 85 REAL GAIN.5 ... MULTIPLY BY GAIN.5 FOR GAIN
 86 OF .5 ;
 87 REAL ARRAY SCALE(1) ... AND ARRAY OF SCALE FACTORS
 88 ;
 89 REAL DELTAT ... SAMPLE INTERVAL 1000. SEC
 90 FULL SCALE ;
 91 REAL TNOF ... NOMINAL SAMPLE INTERVAL
 92 SAME SCALE AS DELTAT ;
 93 REAL TC1 ... FILTER TIME CONSTANT ;
 94 REAL TC2 ... FILTER TIME CONSTANT ;
 95 REAL TC3 ... FILTER TIME CONSTANT SCALE
 96 THE SAME AS DELTAT ;
 97 REAL TC4 ... FILTER TIME CONSTANT ;
 98 REAL TC5 ... LAG TIME CONSTANT ;
 99 REAL ONE ... UNITY ;
 100 REAL ZERO ... 0.0 ;
 101
 102 COMMENT ***** INTERNAL VARIABLES ***** ;
 103 REAL LIN2 ... PREVIOUS FILTER INPUT ;
 104 REAL LIN3 ... PREVIOUS FILTER INPUT ;
 105 REAL LIN4 ... PREVIOUS FILTER INPUT ;
 106 REAL LOUT1 ... PREVIOUS FILTER OUTPUT ;
 107 REAL LOUT2 ... PREVIOUS FILTER OUTPUT ;
 108 REAL LOUT3 ... PREVIOUS FILTER OUTPUT ;
 109 REAL LOUT4 ... PREVIOUS FILTER OUTPUT ;
 110 REAL LOUT5 ... PREVIOUS FILTER OUTPUT ;
 111 REAL DELTAN ... LINEAR FEET TO THE
 112 GLIDESLOPE CLAMP //
 113 ... OR (BEYOND MAXRNG) THE

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114		ANGULAR ERROR IN THE FLIGHT
115		PATH ANGLE WITH RESPECT TO
116		THE GLIDESLOPE //
117		... DIVIDE MAXRNG BY DYTFT TO
118		GET FULL SCALE FEET - - -
119		NUM 1000 FOR 3.76 NM AND A
120		2.5 DEGREE GLIDESLOPE ;
121	REAL YDOT	... RADIO DEV RATE (BEYOND
122		MAXRNG) OR CONVERGENCE
123		RATE (INSIDE MAXRNG) FULL
124		SCALE U - AFPS / SEC =
125		MAXRNG / DYTFT OR FULL
126		SCALE FT / SEC = MAXRNG /
127		DYTFT ;
128	REAL DEVRTE	... BLAM CLOSURE RATE U-AFPS /
129		SEC OR FT / SEC ;
130	REAL PTCMD	... PITCH COMMAND 100 DEGREES
131		FULL SCALE. + INFLIES
132		PITCH DOWN ;
133	REAL MAXCMD	... ILS PITCH COMMAND LIMIT 100
134		DEGREES ;
135	REAL TMAX	... LARGEST RECOGNIZED TIME
136		STEP ;
137	REAL TMIN	... SMALLEST RECOGNIZED TIME
138		STEP ;
139	REAL TEXP	... INITIAL COMPOSITE ILS AND
140		EXTERNAL PITCH COMMAND FOR
141		TRANSITION TO TOTAL ILS
142		CONTROL ;
143	REAL Y	... FILTERED RADIO DEVIATION ;
144	REAL HDOTLL	... FILTERED ALTITUDE RATE ;
145	REAL LOGPRF	... LEAD BREAK FREQUENCY RAD/SEC
146		
147	COMMENT ***** COMPILATION VALUES ***** ;	
148	PRESET	
149	BEGIN.	
150	GAIN.5 = .5 ;	
151	GAIN.5 = .2 ;	
152	GAIN.10 = .1 ;	
153	TNOM = .0002 ;	
154	DYTFT = .1008 ;	
155	KHOCT = .15 ;	
156	KY = .75 ;	
157	KYDOT = .66 ;	
158	MAXRNG = .0556 ;	
159	SCALE(0) = .5667 ;	
160	SCALE(1) = .025707 ;	
161	LOGPRF = .5 ;	
162	TC1 = .0005 ;	
163	TC2 = .002 ;	
164	TC3 = .02 ;	
165	TC4 = .005 ;	
166	TC5 = .001 ;	
167	TMAX = .00025	
168		... SET TO ONE HALF OF THE
169		SMALLEST FILTER TIME
170		CONSTANT ;
	TMIN = .0001	... SET TO AT LEAST THE

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```
171 RESOLUTION OF THE OBJECT  
172 MACHINE OR A MINIMUM CYCLE  
173 TIME IF KNOWN ;  
174 MAXCMD = .1 ;  
175 ONE = .99999999 ;  
176 ZERO = .0 ;  
177 END ;  
178  
179 COMMENT *****EXECUTABLE PROGRAM ***** ;  
180 IF RESETG ... INITIALIZE STATE  
181 LOGIC,RADIO LOWPASS FILTER  
182 AND THE TIME INTERVAL //  
183 THEN BEGIN  
184 DELTAT = TNOM ;  
185 GSARM = TRUE ;  
186 GSCAP = FALSE ;  
187 HDOTLL = LOUT5 = HDOT ;  
188 ... INITIALIZE LEAD-LAG ON  
189 HDOT //  
190 Y = LOUT1 = GSDEV $, ... INITIALIZE FILTERED RADIO  
191 DEVIATION TO AVOID FALSE  
192 CAPTURES //  
193 END  
194 ELSE BEGIN  
195 DELTAT = 1/SCALE(1) ; ... CONVERT TO 1000 SEC FULL  
196 SCALE //  
197 IF DELTAT GEQ Tmax OR DELTAT LEQ Tmin  
198 THEN DELTAT = TMOF ... LIMIT SAMPLE INTERVAL ;  
199 HDOTLL = HDOT-(LOPASS(HDOT,LOUT5,TC5,DELTAT))*LDBRR  
200 ;  
201 HDOTLL = HDOTLL/LDBRR ;  
202 ... LEAD-LAG FILTERED HDOT //  
203 Y = LOPASS(GSDEV,LOUT1,TC1,DELTAT) ... FILTER  
204 RAW DEVIATION ;  
205  
206 END ;  
207  
208 COMMENT ***** ESTIMATE THE DISTANCE TO THE BEAM ***** ;  
209 DELTAN = Y*  
210 IF D GEQ MAXRNG ... BEYOND MAXRNG THE DEVIATION  
211 IS ESTIMATED WITH RESPECT  
212 TO ANGULAR ERROR //  
213 THEN MAXRNG  
214 ELSE D ... INSIDE MAXRNG DELTAN IS  
215 EQUAL TO THE LINEAR  
216 DISTANCE TO THE BEAM IN  
217 FEET ;  
218 DELTAN = DELTAN/DTTOFT ... UNITS CONVERSION ;  
219  
220 COMMENT ***** DERIVE BEAM CLOSURE RATE ***** ;  
221 IF RESETG  
222 THEN BEGIN  
223 LINS2 = DELTAN $,  
224 LOUT2 = ZERO ... INITIALIZE RATE DERIVER TO  
225 CURRENT INPUT AND ZERO  
226 OUTPUT //  
227 END $;
```

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```
228 IF GSARM
229 THEN YDOT = WSHOUT(DELTAH,LOUT2,TC2,DELTAI,LIN2)*GAIN.5
230 ... AFTER THE CAPTURE CONDITION
231 HAS BEEN MET CLOSURE RATE
232 WILL BE COMPUTED FROM HDCT
233 ALONE ;
234 DEVRTL = KYDOT+YDOT/GAIN.10 ;
235 DEVRTL = (HDCTLL+DEVRTL)/GAIN.5 ;
236 IF GSCAP
237 THEN DEVRTL = WSHOUT(DEVRTL,LOUT3,TC3,DELTAI,LIN3)
238 ... WASHOUT THE YDOT BIAS AND
239 THE STEADY STATE VALUE OF
240 HDCT //
241 ELSE LIN3 = LOUT3 = DEVRTL ... INITIALIZE THE WASHOUT
242 TO EXACTLY DEVRTL ;
243
244 COMMENT ***** COMPUTE THE PITCH COMMAND ***** ;
245 PTCMD = KY*DELTAH ... FORWARD FEED ;
246 PTCMD = PTCMD+(DEVRTL*KHDOT) ... RATE DAMPENING ;
247 PTCMD = LIMIT(PTCMD,MAXCMD) ... LIMIT THE COMMAND SIZE ;
248 PTCMD = PTCMD*SCALE(0) ... CONVERT TO 180 DEGREES FULL
249 SCALE ;
250
251 COMMENT ***** TEST FOR CAPTURE ***** ;
252 IF GSARM
253 THEN BEGIN
254 GSCAP = ((Y LEQ ZERO) AND (PTCMD GEQ ZERO)) OR ((Y
255 GEQ ZERO) AND (PTCMD LEQ ZERO)) ... TEST FOR
256 CAPTURE ;
257 IF LOCARM THEN GSCAP = FALSE ; ... WAIT FOR LOC //
258 GSAPP = NOT GSCAP ;
259 TEMP = LIN4 = LOUT4 = PTCMDA-PTCMD ... PREPARE TO
260 TRANSITION TO ILS //
261 END ;
262
263 COMMENT ***** OUTPUT THE PITCH STEERING COMMAND ***** ;
264 IF GSARM
265 THEN ... DO NOT OVERWRITE EXTERNAL
266 COMMAND //
267 PTCMDA = PTCMD
268 ELSE PTCMDA = PTCMD+WSHOUT(TEMP,LOUT4,TC4,DELTAI,LIN4)
269 ... FADE OUT EXTERNAL COMMAND ;
270 END ;
271
272 END FINI
```

RT+S D.LIMRGAL

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WORKFILE.LIMRGOA1

```
1      BEGIN
2
3      DEFINE REAL PROCEDURE LIMIT(INPUT,LIMVAL) WHERE REAL LIMVAL
4                                     ... LARGEST ALLOWABLE OUTPUT
5                                     MAGNITUDE //
6      INPUT                                     ... INPUT VALUE ; TEMP
7      BEGIN
8      REAL TEMP ;
9      IF INPUT LES .0 THEN TEMP = -INPUT
10     ELSE TEMP = INPUT ;
11     IF TEMP GET LIMVAL ... LIMIT TEST //
12     THEN LIM1 = LIMVAL*TEMP/INPUT ... SATURATION //
13     ELSE LIM1 = INPUT ;
14     END ;
15
16     END FIN1
```

FIN

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DD:DDPKFILE:SHRGDA1

```
1      BEGIN
2
3      DEFINE REAL PROCEDURE WSHOUT(INPUT,LSTOUT,TC,T,LASTIN)
4      WHERE REAL INPUT          ... CURRENT INPUT SIGNAL ;
5      REAL LASTIN              ... LAST INPUT SIGNAL ;
6      REAL LSTOUT              ... LAST OUTPUT SIGNAL ;
7      REAL TC                  ... FILTER TIME CONSTANT ;
8      REAL T                    ... REAL T ... SAMPLE INTERVAL
9                                ... NOTE TO ABL 1 MUST HAVE
10                                 THE SAME SCALING !!
11
12      TOBE
13      BEGIN
14      REAL K1,K2 ;
15          K1 = TC/(TC+.5*T) ...          FOR T = 0. 10
16          TC / 2 ;
17          K2 = (TC-.5*T)/(TC+.5*T) ;
18      LSTOUT = K2*LSTOUT+(INPUT-LASTIN)*K1 ;
19      WSHOUT = LSTOUT ;
20      LASTIN = INPUT ;
21      END ;
22      END FTHI
```

DDPKFILE:SHRGDA1

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QD*WORKFILE.LOPRGDA1

```
1          BEGIN
2
3          DEFINE REAL PROCEDURE LOPASS(INPUT,LSTOUT,TC,T)
4          WHERE REAL INPUT          ... CURRENT INPUT SIGNAL ;
5          REAL LSTOUT                ... LAST OUTPUT SIGNAL ;
6          REAL TC                    ... FILTER TIME CONSTANT ;
7          REAL T                     ... REAL T ...SAMPLE INTERVAL ;
8                                     ... NOTE TC AND T MUST HAVE THE
9                                     SAME SCALING //
10         TOBL
11         BEGIN
12         REAL K1,K2 ;
13             K1 = T/TC ;
14             K2 = (TC-T)/TC ;
15         LSTOUT = K1*INPUT+K2*LSTOUT ;
16         LOPASS = LSTOUT ;
17         END ;
18
19         END FINI
```

QPRINT S D*WSH-RGDA1

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