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DEVELOPMENT OF TECHNIQUES FOR SHORT-RANGE
PRECIPITATION FORECASTS

Robert K. Crane

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1. INTRODUCTION

1.1 Program Objectives

The ultimate goal of the work reported herein is the development of a real-time method for the short-range (0-20 minute) forecast of storm development and motion. The initial step in this program was the development of objective techniques for the efficient representation of information obtained from a single Doppler weather radar (Crane, 1977). The radar data are processed to obtain fixed and peak referenced reflectivity contours and peak referenced tangential shear contours. The essential information contained in the contour data are represented by a set of attributes. In this report, we consider the second step in the program, the assembly of data obtained from a set of radar scans into a set of attributes that characterize the three-dimensional structure of the small precipitation cells and surrounding echo regions, their motion, and their development in time. Initial consideration is given to the problem of forecasting precipitation cell development and motion.

1.2 Summary of Results

The work performed under this contract was concentrated in three major areas: (a) improvement to the cell detection program developed under the previous contract (Crane, 1977), (b) development of the volume cell detection and tracking program, and (c) preparatory data analysis to support the development of cell forecast algorithms.

The cell detection program was extensively revised to reduce the amount of core storage required for some of the integer arrays used in peak referenced contour analysis; to process reflectivity, tangential shear, and Doppler spread data simultaneously; to include spread information in the reflectivity and tangential shear peak attributes; to use the relatively spiky nature of ground clutter as an aid in rejecting ground clutter; to resolve automatically Doppler velocity ambiguities using radial velocity data from resolution elements adjacent in range and in azimuth; and to vary the quantization steps used in the peak referenced contouring operation. In the process of revising the program additional refinements were made in the cell detection logic to correct several

defects detected using actual radar data and to improve the technique used to store temporarily the peak referenced contour data to increase the speed of the processing algorithm and reduce overall core storage. At present, the entire program required for the simultaneous processing of reflectivity, tangential shear, and Doppler spread data fits into the core storage available on the CDC 6600; a result not anticipated at the start of the program.

The program is currently relatively slow in operation due to (1) the extensive number of input and output tape or disk operations used to read the input radar data, store data for plotting, store data for subsequent volume cell detection and tracking and to store data for B scan printouts and (2) the large number of bit manipulation operations required to pack and unpack data for storage. A considerable time savings can still be accomplished by reducing the amount of output data and by rewriting the program in assembler language to reduce the time spent in subroutine calls for bit manipulation and indirect storage addressing.

A volume cell detection and tracking algorithm was developed to combine the data from successive radar scans. The fixed and peak referenced contouring operations are performed independently for each azimuth scan of the radar. The reflectivity cells (peak referenced) are associated from one elevation angle to the next to form a volume cell and from one volume cell to the next to form a track. The reflectivity cells are used to identify the basic organization of the radar data. Fixed contours that enclose associated reflectivity cells are used to determine the 3-dimensional echo envelope for the reflectivity cell (or cells). Tangential shear and Doppler spread cells are likewise associated from scan-to-scan; associated with reflectivity cells (if possible); and identified with fixed contour envelopes. The lowest threshold fixed contour that encloses each of the reflectivity, shear, or spread cells is used to tag that cell to aid in the association processing.

A new set of attributes are developed for each volume cell. A list of these attributes are given in Table I for fixed contours and for reflectivity, shear, and spread cells. The attributes to be calculated for each volume cell are readily modified. The basic volume cell detection and tracking algorithm is used to perform the scan-to-scan association.

TABLE I

VOLUME CELL ATTRIBUTES

<u>Fixed Contours</u>	<u>Reflectivity Peaks</u>	<u>Tangential Shear Peaks</u>	<u>Doppler Spread Peaks</u>
Surface Area	Reflectivity at Peak	Shear at Peak	Spread at Peak
Echo Top	Height of Peak	Height of Peak	Height of Peak
Enclosed Volume	Height of Top	Height of Top	Height of Top
Centroid Location*	Height of Base	Height of Base	Height of Base
Total Surface Precipitation	Centroid Location*	Centroid Location*	Centroid Location*
Average Surface Rain Rate	Area at Peak	Area at Peak	Area at Peak
Average Reflectivity	Volume	Volume	Volume
Maximum Enclosed Peak Values	Area at Surface	Area at Surface	Area at Surface
Profile of Areas vs Centroid Heights	Reflectivity at Surface	Shear at Surface	Spread at Surface
Profile of Average Reflectivity vs Centroid Heights	Average Tangential Shear	Average Velocity Spread	Associated Reflectivity Peaks
Number of Enclosed Peaks (by type)	Average Radial Shear	Associated Reflectivity Peaks	Associated Shear Peaks
Nearest Neighbor Distances for Enclosed Cells	Average Vertical Shear	Associated Spread Peaks	
	Associated Shear Peaks		
	Associated Spread Peaks		

*Centroid Locations are Defined on the Surface Using Data from the Lowest Possible Elevation Angle

When data from two scans are associated, they can be used readily to calculate any desired attribute. The lists given in Table I are preliminary in nature covering the parameters we currently expect to be most important in subsequent analyses. Experience with the use of these programs for a larger data set will be required before a final set of attributes can be specified.

Experience with a larger data set is required as a prerequisite to the development of cell forecast algorithms. Crane (1976) processed reflectivity data from a number of radar scans obtained at Wallops Island during the summer of 1973 by the Johns Hopkins Applied Physics Laboratory (APL) in the process of initially establishing the utility of the peak referenced contouring technique. These data were used by Crane (1976) to investigate cell lifetime and possible cell tracking/extrapolation techniques. In this study, we used the same data set to determine the relative spacings between cells. The object of the spacing study was to determine if preferred spacings are evident in nature. If so, the preferred structure can be used to forecast the most probable location for new cell development. The ability to forecast locations for new cell development would add significantly to the 0-20 minute forecast because the median cell lifetime is less than 20 minutes and forecasting by extrapolation along a cell track is not adequate. An examination of the Wallops Island data revealed that the nearest neighbor distances between cells were between 7 and 9 km and that these distance values did not depend on the type of rain observed. This suggests that new cell site forecasts are feasible.

1.3 Software Development

The goal of this contract with the Air Force Geophysics Laboratory (AFGL) is to provide efficient computer software to obtain parameters to represent the essential information obtained in a sequence of scans of a single Doppler weather radar. The radar used to provide the data is the C-band Doppler radar operated by the Weather Radar Branch of AFGL at Sudbury, Massachusetts. The computer programs were prepared for the CDC-6600 at AFGL.

There are now three separate programs in the sequence of programs to be used for weather radar data processing. The first is the cell

detection program which was developed under the previous contract (Crane, 1977) and extensively modified during the course of this contract. The second is a plotting program used to display contours and cell centroids. This program was developed under the previous contract and modified under this contract to display separately the locations of the centroids of the fixed echo regions and the centroids for each of the peak detected cells - reflectivity, tangential shear, and Doppler spread cells. The third program detects and tracks volume cells. It was developed under this contract. This program uses data generated by the cell detection program to develop three-dimensional cells and to describe their location, height and intensity. The volume cell attributes are listed in Table I.

The ultimate goal of this work will be the development of real-time radar processing techniques to be used on a dedicated computer system that is an integral part of the radar system. The programs generated to date on the current contract are exploratory in nature. They were designed to fit within the core storage limitations of the CDC-6600 computer but still have a high degree of flexibility in modifying storage array sizes and in providing auxilliary output for testing the program. The program design had real-time processing in mind and, in the end, should be reasonably efficient when tailored to an on-site computer system. Listing and operating instructions for the programs developed on this contract are included in the appendices.

1.4 Organization of the Report

A summary of the modifications to the cell detection program and plotting program is given in Section 2. A description of the volume cell detection program is given in Section 3. Initial consideration of the cell forecasting problem is given in Section 4. Sample outputs are provided in Section 5. Section 6 summarizes progress to date and provides recommendations.

2. IMPROVEMENTS TO THE CELL DETECTION PROGRAM

2.1 Cell Detection Logic Changes

The cell detection program was modified to include the detection of Doppler spread peaks and to pack integer addresses used in the peak detection routine six to a CDC word. The latter change was required to make room for the additional data used in Doppler spread processing. In the process of revising the address storage procedure, a number of minor logic errors were detected. These errors were associated with the operation of the radial-to-radial association of contours at different threshold levels (see Section 5.2 of Crane, 1977). The errors have been corrected and, in the process, changes were also made to streamline the storage of the temporary contour data.

At present, the temporary attribute storage array (TATR in subroutine PEAKD, see Appendix D) is used to identify active cells at each possible threshold level (relative to the peak level for the cell) and to store pointers to previously associated active cells as well as provide partial attribute summations for the active cells. The TATR array is doubly subscripted maintaining temporary storage for the number identification of the peak for the active cells. For each active cell the stored data includes the current estimate of the peak value; a set of partially summed attribute values for each of the nested contours for each possible threshold level below the peak, area, average value, centroid location plus, for reflectivity cells, Doppler spread, radial shear, tangential shear, and radial velocity; the azimuth count for the last azimuth on which the attributes for each contour were updated; and a pointer to the enclosing fixed contour. This last item is included for later use in the volume cell detection program. If a cell is not active at a particular threshold level but was previously active on the current radial, the area attribute contains a pointer to the cell, now active at that level. After processing the data for a radial the cell-to-cell pointers are zeroed. If a cell becomes inactive, all pointers to that cell are also zeroed before processing data for the next radial.

The program as it now stands is configured to allow rapid changes in the dimensions of all the storage arrays. This convenience costs in

producing relatively longer processing times than for a program with fixed storage allocations. A final program modification should be made when the exploratory runs of the computer program are finished to fix the array sizes and optimize the program for rapid operation.

2.2 Refinements in Velocity Data Processing

The program was modified to provide automatic resolution of Doppler velocity ambiguities. The first detected velocity data for each scan is assumed to be in the velocity interval spanning zero velocity. Successive observations at different but adjacent range or azimuth locations are assumed to differ from the first observation by less than the velocity ambiguity. If the difference is larger, it is adjusted so that it is smaller by adding or subtracting a value equal to the velocity ambiguity ($\lambda/2 \cdot \text{PRF}$ where λ is the wavelength and PRF is the pulse repetition frequency). The data for each radial are then reexamined to ensure that each velocity observation differs from the average of the velocity values for the two surrounding range intervals by less than the velocity ambiguity and adjusted again if required.

The above processing is used for contiguous range and azimuth elements. If large spacings exist between regions of radar data above the processing threshold, the first data point in one region is compared with the average velocity for the previous region. The data therefore are objectively adjusted to remove ambiguities. Provision is provided to reject data from this analysis if the Doppler spread is not within pre-set bounds but this option has not been exercised.

The processed data appear to be reasonably smoothly varying as indicated in Figure 1. The tangential shear data obtained by numerically differentiating the radial velocity data are however, more variable as illustrated in the figure. The apparent noise evident in the tangential shear field led to the inclusion of Doppler spread data in the analysis process. The program was also modified to introduce a new constant to specify the quantization interval for peak detection contouring. By setting this constant, additional control is exercised over the peak detection process. Referring to Figure 1, no peaks would be detected if the quantization step is 1 m/s but a number of peaks are detected for a 0.1 m/s quantization step (see Section 5).

NA RANGE (3/2 M. INCREMENTS)

0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

REFLECTIVITY 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

RADIAL VELOCITY 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

VELOCITY SPREAD 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

TANGENTIAL SHEAR 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

NA

0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9 0 1 2 3 4 5 6 7 8 9

AZIMUTH

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Figure 1 Sample Data Set Including Two Fixed Contour Echo Areas and Three Reflectivity Peaks

2.3 Doppler Spread Processing

Velocity variance data may now be routinely processed using the computer program. Facilities to analyze this data field were added because of the apparently high noise levels in the tangential shear data and the expectation that at high signal-to-noise ratios, the spread data may be more reliable. As discussed before (Crane, 1977), the spread data are assumed to contain the same information as the tangential shear data due to the dominant effect of velocity fluctuations on the scale of the antenna beamwidth at the observation range. Both data fields are now processed to allow an intercomparison between the information available from each field and to investigate their relative sensitivity to noise.

The velocity variance output from the pulse pair processor is known to be adversely affected by low signal-to-noise ratios. A noise level dependent threshold parameter is provided for thresholding the velocity variance data but has not been exercised as yet. To reduce the sensitivity of the variance data due to noise, the square root of the variance is used for analysis of the Doppler spread. A sample of this data is depicted in Figure 1. It is noted that the velocity data, radial velocity, Doppler spread, and tangential shear, are processed only when the reflectivity values are above the lowest (processing) threshold level which, for this figure, is 20 dBZ. High Doppler spreads are evident in two regions of the figure, (1) at low reflectivity values and (2) at high reflectivity values. The high spreads at low values are presumably caused by signal-to-noise problems and should be suppressed using the signal-to-noise threshold level. The high values corresponding to the higher reflectivity values are presumably real, although the correlation with the tangential shear values is not good for the data in this figure. A larger data sample must be analyzed to optimize the processing of tangential shear and/or Doppler spread data.

Modifications for Doppler spread processing were made in several areas of the program. The largest change included the addition of temporary attribute storage arrays for the detection of Doppler spread peaks. In addition, the reflectivity peak and tangential shear peak detection algorithms were changed to increase the number of attributes so the average Doppler spread within a detected cell could be determined. This attribute is now listed with the others as described in Section 5.

3. VOLUME CELL DETECTION AND TRACKING

3.1 Definition of a Volume Cell

The cell detection program provides, as one of its outputs, a list of attributes for fixed contours, reflectivity peaks, tangential shear peaks, and Doppler spread peaks. At a minimum, each attribute list defines the average value, area, and centroid location of each cell for each azimuth scan of an elevation scan sequence. The expected scan sequence for the radar includes azimuth scans (or azimuth sectors in a raster scan) at successively higher elevation angles until a complete volume scan is completed. The data for each elevation or tilt of the scan sequence must be combined with the data from other tilts to provide a three-dimensional picture of each cell or echo volume.

The process of combining data from scan to scan in a volume scan sequence is illustrated schematically in Figure 2. This figure represents a height section through three cells. The contours represent quantized data (e.g. reflectivity data in 1 dB steps) that have been processed on each azimuth scan to produce a set of reflectivity peak cells. The minimum attribute set is identified by the length of the heavy bar (detected length or in three-dimensions, the cell area) and its location (centroid) on each tilt. The data obtained for the lowest tilt is assumed to extend to the surface. The height of the centroid is determined from the range to the centroid and the elevation angle for the scan.

The three-dimensional cell or volume cell is defined by the volume enclosed within the peak detected cells that are associated from scan-to-scan. A criterion similar to the one used to define a peak referenced cell is used to define the volume cell. From the sequence of attributes for cells detected scan-to-scan, cells 1, 2 and 3 on this figure, a peak value and its height may be selected. The top and base of the volume cell are defined by the height at which the reported average value drops the required number of quantization units below the peak value. This height is determined by extrapolation if detected cells are obtained for each tilt or is taken as halfway between the height of a value above the required threshold and the expected height of the intersection of the cell with the next tilt plane if no associated cell was detected on the next scan. The locations of the peaks, tops, and bases are depicted on the

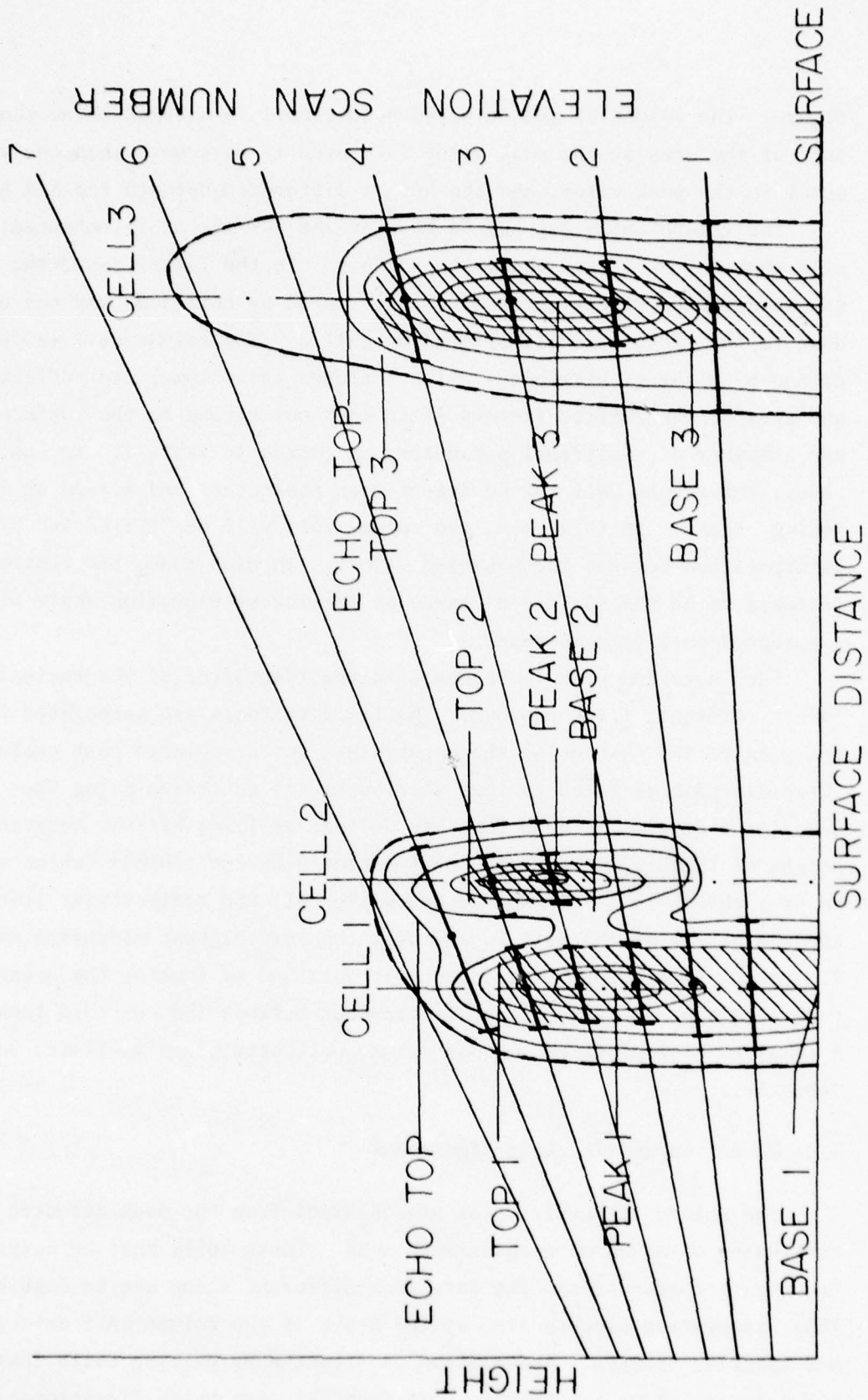


Figure 2 Illustration of Scan-to-Scan Data Association in a Volume Scan Sequence

figure. The volume of the detected volume cell is assumed to be the product of the area at the peak value (averaged if have more than one value equal to the peak value) and the height difference between top and base.

The volume cells may have a base at the surface as illustrated by cell number 1 or a base above the surface. In the latter case, the cell may be detected at the surface as illustrated by cell 3 or may not extend down to the surface as illustrated by cell 2. The volume cell is described by a set of attributes which includes its volume, its reflectivity and area at the surface (zeroes if it does not extend to the surface) and a number of additional parameters as listed in Table I. In some cases, the volume cell may be detected on some scans and missed on intervening scans. In this case, the volume cell will be "filled in" by interpolation between the measured values. In each case, the centroid is taken to be the surface distance at the lowest elevation angle with a detected cell (single scan).

Each detected peak is tagged with the identifier of the enclosing lowest threshold fixed contour. The fixed contours are associated from one scan to the next using the identifiers for associated peak cells. Three-dimensional fixed contour attributes are generated using the associated data. The echo tops are defined as lying halfway between the height of the highest detected peak enclosed by the contour (which may be at a threshold level many dB below the cell top reflectivity level) and the height of the cell location at the next highest elevation angle. The volume within the fixed contour is obtained by summing the areas on each scan and using the height differences between the centroid locations. A complete list of fixed contour volume cell attributes is listed in Table I.

3.2 Detection and Tracking Algorithms

The volume cell attributes are obtained from the peak detected cell attributes obtained on each azimuth scan. These cells must be associated from scan-to-scan before the data from different scans can be combined. This association process lies at the heart of the volume cell detection and tracking process. Association is affected by pairing cells that are sufficiently close together to come from the same three-dimensional structure. The location of the contours surrounding each peak is not available

for use by the association algorithm. Association is accomplished by first selecting cells from each scan whose centroid locations, when projected on the surface, are separated by less than the square root of the combined areas, plus the distance the cell might move during the interval between scans, plus a fixed distance to account for the statistical centroid location uncertainty introduced by the expected variability of the radar data. Comparison is always made between the cell location for a particular scan and the detected volume cell location from the lowest elevation scan on which it was observed.

In most cases, only pairs of cells will be evident from the association algorithm listed above. Occasionally, in a cluster of cells, more than one cell may meet the association criterion. In this case, the cells will be associated by picking those cells which are closest after a uniform offset is made between cell locations to provide the largest number of associations. This is illustrated in Figure 3. In this figure, the cell to be tested, cell A, is closest to the previously detected volume cell number 2, but after translation of the surface locations relative to each other by the amount shown by the straight line on the figure, all three cells (lettered) may be associated with the detected cells (numbered) with smaller physical separations. This procedure for conflict resolution (correlation) will be used only when the resultant translation is physically realizable (i.e. corresponds to a possible cell tilt or translation velocity).

The scan-to-scan cell association logic is also used for volume-to-volume scan sequence association for cell tracking. For the tracking problem, the translation analysis for conflict resolution becomes more important and guidance in selecting the appropriate translations is taken either from a prescribed wind vector (700 mb wind for instance) or from the results from the previous scan. The conflict resolution or correlation algorithm is performed separately for large echo regions in that the translation values are allowed to vary from one echo region to the next.

3.3 Volume Cell Attributes

The volume cell attributes were partially defined in Section 3.1 and are listed in Table 1. A different set of attributes is generated for

+ surface location detected
volume cell

• surface projection of peak
cell

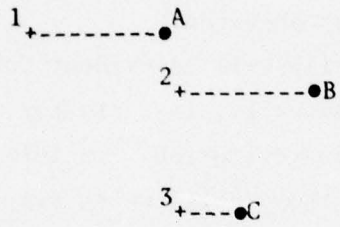


Figure 3 Illustration of Scan-to-Scan Association
for Volume Cell Detection and Tracking

each volume cell type. Fixed contour attributes include measurements of the total precipitation produced within the echo region, average rain rates on the surface, profiles of area and of average reflectivity for the data contained within the fixed contour envelope, and summaries of the numbers and locations of peak referenced cells detected within the echo envelope. The peak referenced volume cell attributes include the size, intensity, and location parameters listed above plus information on associated volume cells of different types. The reflectivity peak attributes also include average spread and shear values for data obtained within the cell (between base and top). The vertical shear values are calculated using the variation of the average radial velocity with height.

Each detected volume cell is characterized by its attributes. Each volume cell track by the time variation of its attributes. In addition, tracks may be characterized by a lifetime and average velocity. Observations obtained to date indicate that the individual peak referenced reflectivity cells neither merge nor split but only develop and translate. Observations of a much larger data set are needed to verify this model for small cell behavior. The larger fixed contour regions may merge or split depending upon its stage of development. By tracking the enclosed cells and maintaining the cell to fixed contour identification relationship, the merger, growth, division and decay of the larger echo regions may be automatically taken into account. The morphology of the echo development process may be important to the understanding of precipitation dynamics, however, suitable attributes to characterize the relevant processes have yet to be defined. Again, experience with a significantly larger data set is required before further progress can be made.

3.4 Software for Volume Cell Detection and Tracking

A computer program (TRACK) was generated under this contract to associate cells from scan-to-scan, resolve conflicts between multiple associations and generate the volume cell attributes listed in Table I. The listing is provided in Appendix D and operating instructions are given in Appendix C. The program processes data which have been generated by the cell detection program (EXTRAD) and then recorded on disk or tape; the algorithms described in Sections 3.1 to 3.3 are used. The current output is a list of attributes for each detected volume cell (or

track). These outputs are again stored on disk or tape and listed on printout for subsequent analysis. Programs have not been generated as yet to summarize the track histories, do climatological analysis, or provide samples for case study analysis.

4. CELL FORECASTING

4.1 Extrapolation Along Cell Tracks

Short range, 0-20 minute, forecasts are of importance for severe weather warning and weather hazard avoidance. The objective of a forecast on this time (and by implication comparatively small distance) scale is the occurrence of a severe event at a point or over a small area such as an airport or the approach path to the airport. Events such as high winds produced by downbursts or by gust fronts, or regions of intense hail fall are of most interest. Larger time and area forecasts may be made of the probable occurrence of a severe weather event but the problem considered here is the remote detection, tracking, and prediction of the development and decay of a severe weather event. The first parts of the problem, the detection and tracking of small scale features in the radar data, were considered in previous sections. The association of these features with severe weather events is a second problem that is not being considered under this contract. The third part, the forecast of cell development and motion are given initial consideration in this section.

The short range forecast problem considered here is different from most meteorological forecast problems in that the occurrence of at least one cell is assumed. The problems are where will it move, how will it develop in time, where will new ones develop, and will it produce a severe weather event. The measure of success of the forecast procedure must depend upon the particular problem addressed. The success of a cell position forecast should be measured by the distance between its actual position and forecast position at forecast time. The success of the cell development forecast should be measured by the difference between the actual intensity (reflectivity, say) and forecast intensity at forecast time. Classical evaluation procedures that test the occurrence or non-occurrence of the event at a number of geographical locations are not recommended in that the reason for failure of the forecast may not be readily apparent.

Crane (1976) used data obtained by APL at Wallops Island to perform some initial tests of cell tracking/track position forecast algorithms. He assumed that a single cell motion vector would adequately describe the

propagation of a field of cells and tested that assumption by measuring the along track and cross track position errors as a function of forecast time (0-20 minutes). His results showed that the forecast error (position) was the order of the cell diameter (median value) at the half life (median lifetime) of the cell. He also found that the half life was of the order of 10 to 15 minutes and the median cell diameter was of the order of 3 km. This result was, however, based on a limited amount of data.

Crane found that the operation of the track extrapolation forecast procedure could be improved by using different motion vectors for different regions of the display area (see Figure 4 for an example showing the different directions possible for cell tracks observed during the same time interval). This idea is incorporated in the volume cell detection and tracking program. The major problem of using extrapolation along a track for forecasting is the relatively short lifetime of most cells. The largest and most intense cells persisted for a relatively long time, 40 to 50 minutes. Except for these cells, the cell could disappear by forecast time and a significant number of new cells could appear. Forecasts based upon cell time histories could be used to estimate cell lifetime but the forecast of new cell site development is a major problem for any radar data based short range forecast procedure.

4.2 New Cell Site Development

The requirement for a procedure to forecast the most probable sites for new cell development and the observation of a seemingly persistent organization or structure for the location of active cells lead to an investigation of the most probable distance or spacing between the cells. The Wallops Island data previously processed by Crane (1976) were used for this analysis. The data consisted of computer prepared maps of detected cell locations for each of the azimuth scans processed from the 1975 summer data set provided by APL. Nearest neighbor distances were obtained from the data to investigate the existence of persistent dominant scales for cell organization. The smallest, second and third shortest distances between each cell and its neighbors were determined and tabulated for each cell for each available volume scan. It is noted that with the processing technique used, the distance between two closely spaced cells is counted twice, each cell being the nearest neighbor of the other. Nearest

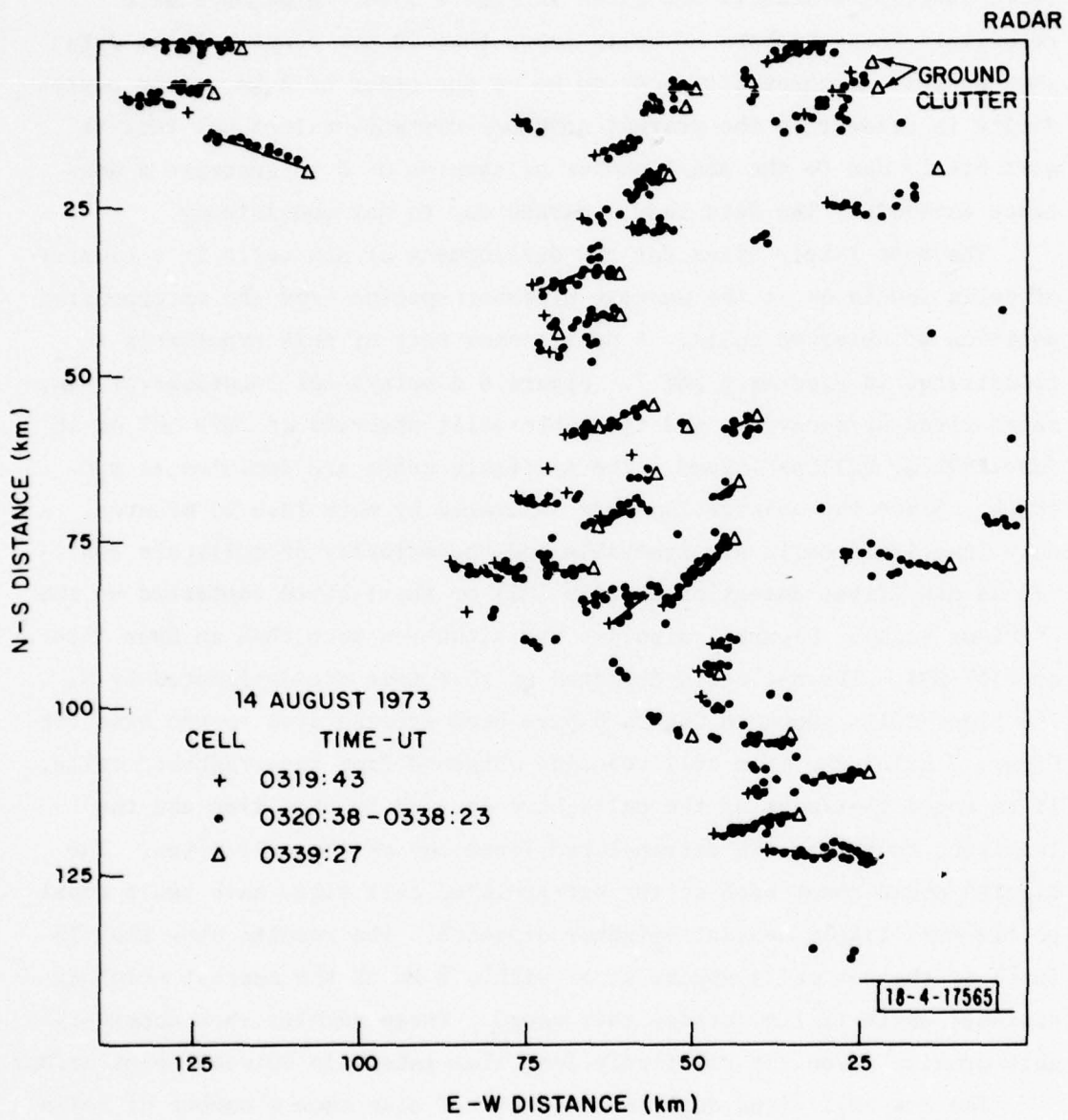


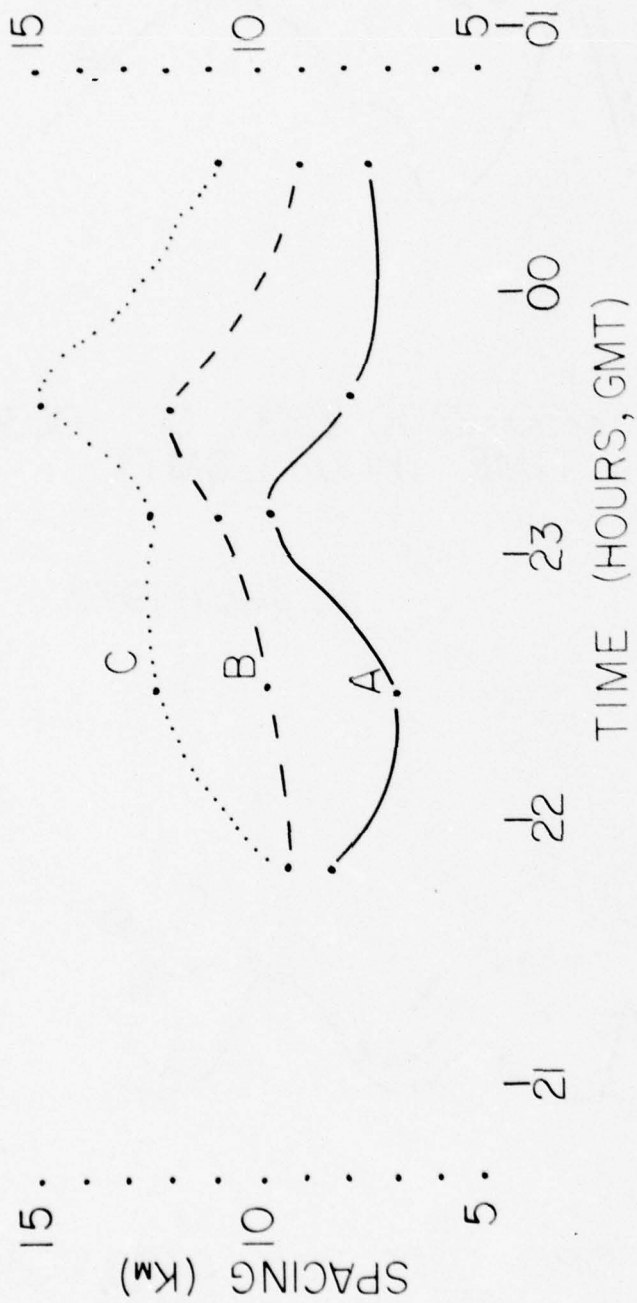
Figure 4 Cell Tracks for a 20-minute Interval Observed by the Wallops Island SPANDAR Radar (from Crane, 1976)

neighbor distributions were generated for each scan. The mode for each distribution was used to estimate the most probable cell spacing for that scan. Time histories of the modal values for the smallest, second and third shortest distances are given in Figure 5 for three days with relatively large numbers of cells (more than 20 per scan). These data show nearest neighbor distances to be on the order of 8 km. Some periodicity is evident in the nearest neighbor distance values but this is most likely due to the small number of samples used to generate a distance estimate. The data show a marked day to day consistency.

The most likely sites for the development of new cells in a cluster of cells should be at the nearest neighbor spacing from the extrapolated position of observed cells. A preliminary test of this hypothesis is illustrated in Figures 6 and 7. Figure 6 displays the locations of new, short-lived or decaying, and trackable cells observed at 2229 GMT on 18 June 1973 at Wallops Island. The trackable cells are depicted at mid-track. Since the observations are separated by more than 20 minutes, only long-lived cells are trackable and the majority of cells are depicted as new (first detection at 2229 GMT) or short-lived (detected on the previous scan). Figure 7 displays the situation more than an hour later, at 2337 GMT. The new cells depicted at this time are designated by N. The older cells shown on Figure 6 have been extrapolated to the time for Figure 7 using the mean cell velocity obtained from the trackable cells. It is noted that most of the cells have decayed by this time and the locations represent the extrapolated locations of the cell sites. The circles drawn about each of the extrapolated cell sites have radii equal to the most likely nearest neighbor distance. The results show that 23 (66%) of the new cells appear at or within 2 km of the nearest neighbor distance while 12 lie outside this range. These results show considerable promise given the relatively long time intervals between observations.

The new cell sites depicted on Figure 7 also show a number of cells approximately spaced from each other by the nearest neighbor distance but not connected to an older cell site. A forecast based upon a more complex pattern using the nearest neighbor distances in a more regular extended structure may be capable of predicting the locations of a larger number of cells. The structure may also reduce the size of the region

- A- NEAREST NEIGHBOR
- B- SECOND NEAREST
- C- THIRD NEAREST



18-19 JUNE 1973

Figure 5 Nearest Neighbor Distances

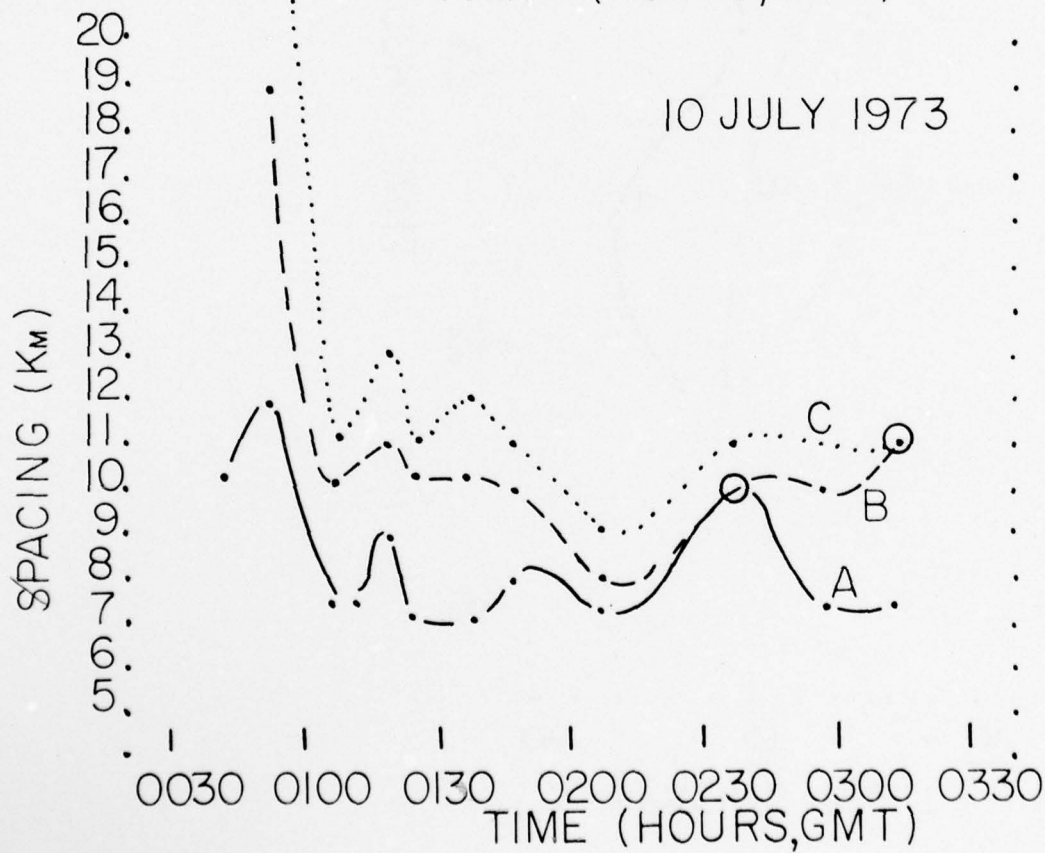
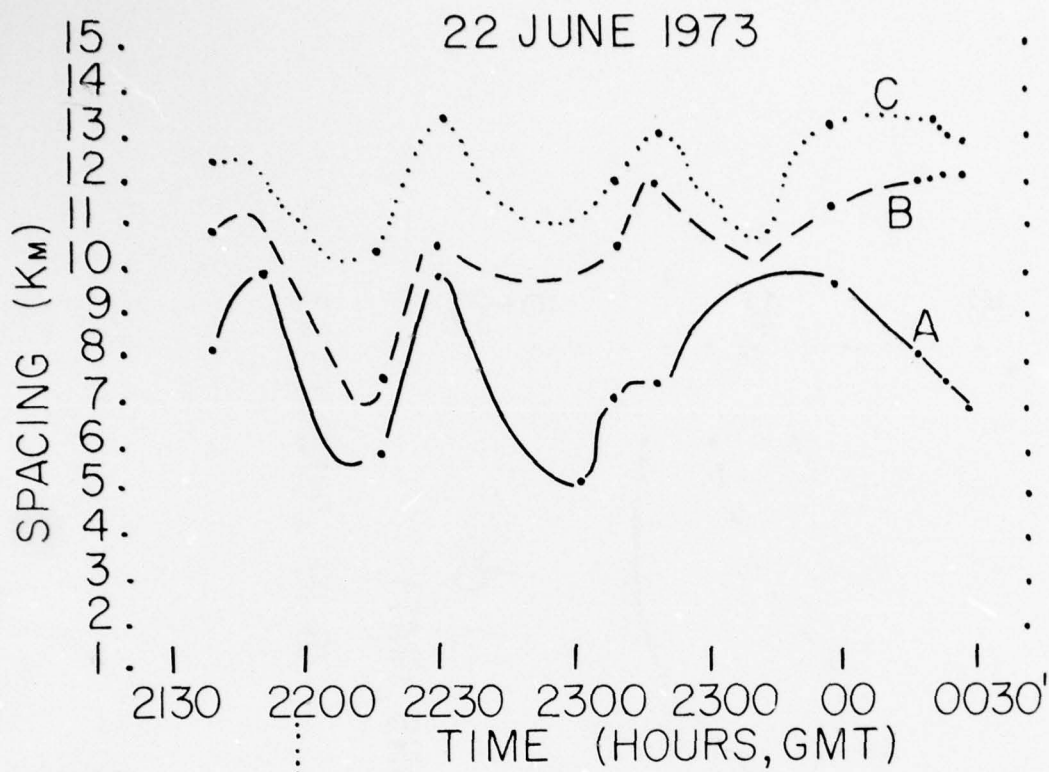


Figure 5 (cont) Nearest Neighbor Distances

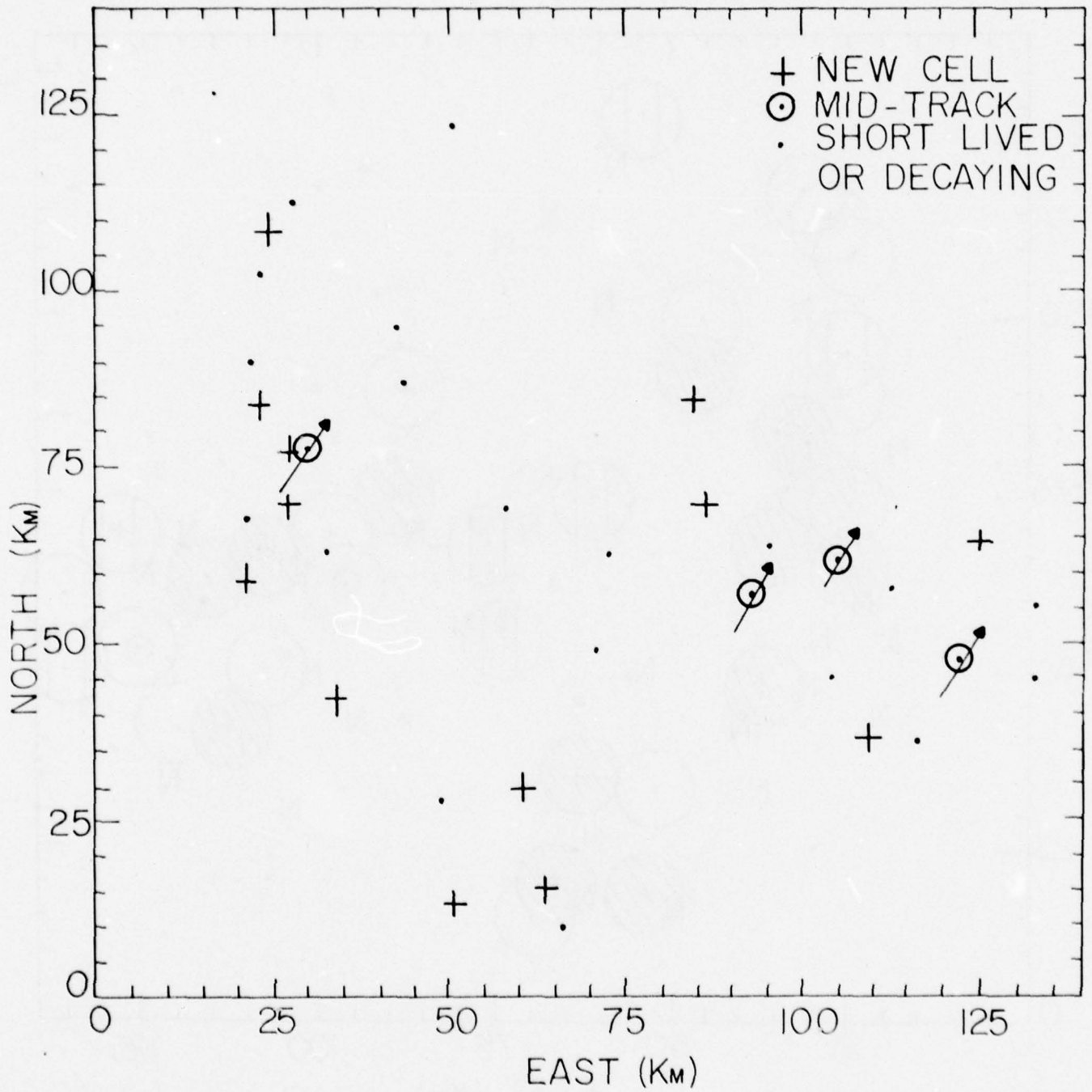


Figure 6 Cell Locations at 2229 GMT, 18 June 1975 at Wallops Island

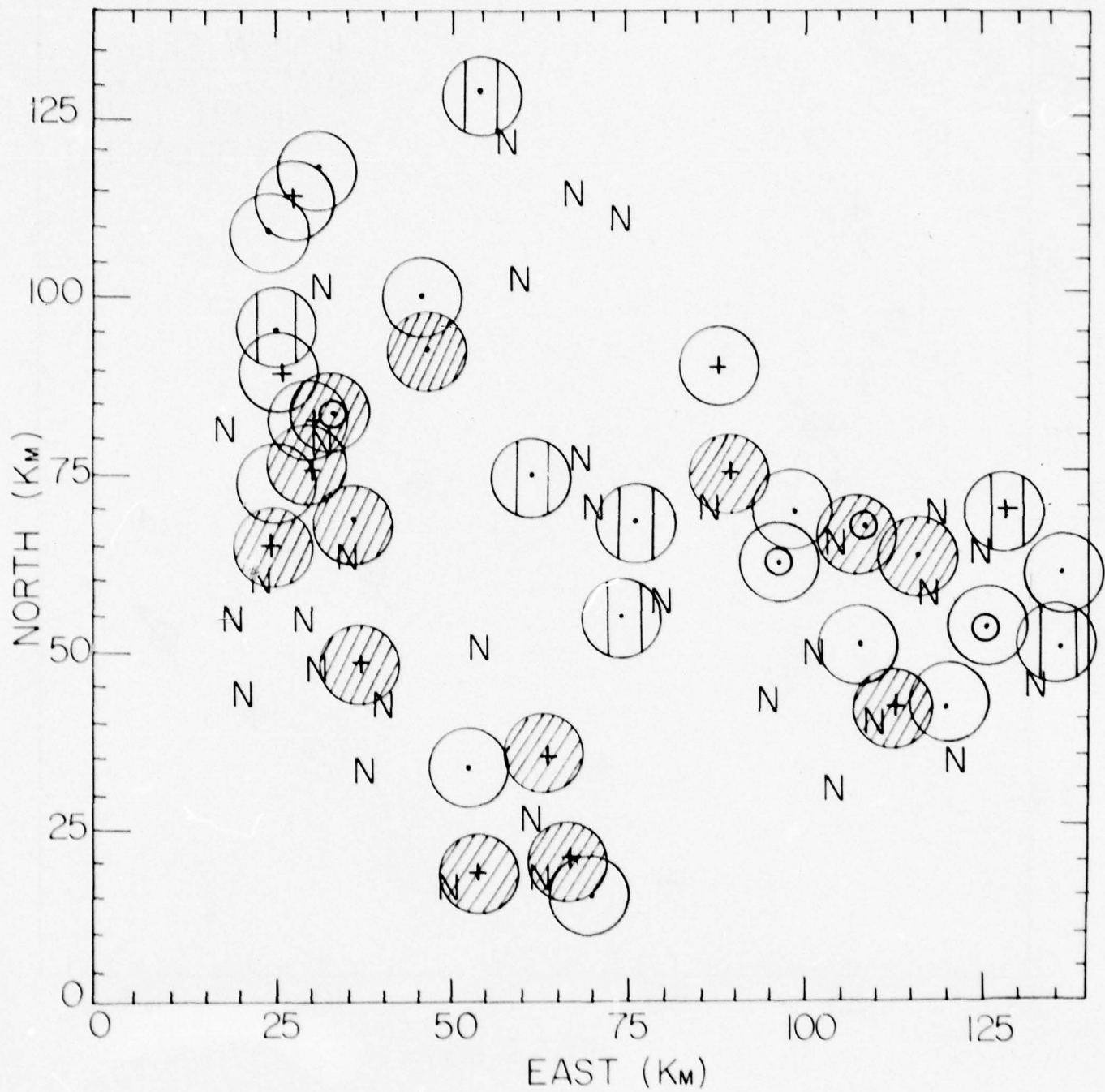


Figure 7 Cell Locations at 2337 GMT, 18 June 1973 at Wallops Island

forecast for probable new cell development by specifying a segment or segments of the nearest neighbor arc. A considerably larger sample of data with smaller time steps between observations is required before a procedure for new cell site forecasting can be developed and tested. The preliminary results presented here are encouraging and indicate that a new cell site forecasting procedure can be developed.

5. ANALYSIS OF SELECTED DATA SETS

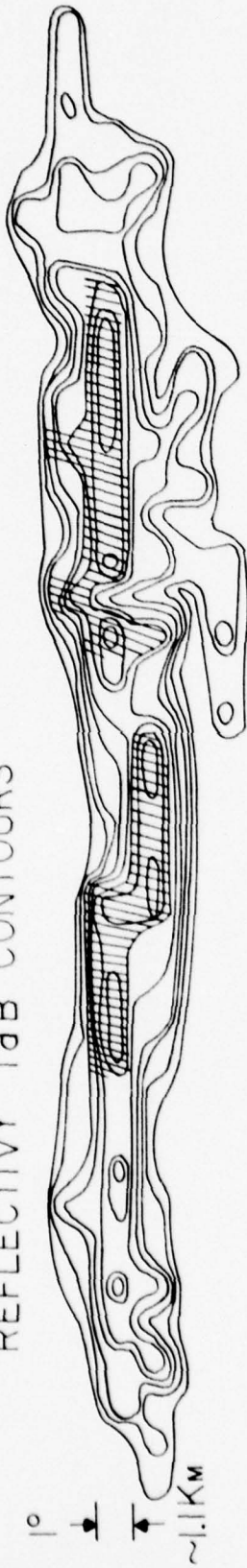
5.1 Use of the Computer Programs

The computer programs described above were developed as a prototype for a real-time processing system to be employed in reducing the number of data bits required to describe a set of radar observations. The objective of the program was to replace the large volumes of data obtained by a radar system to a set of fixed contour and peak referenced cell attributes capable of representing the same essential information. A prototype program is now available with optional choices for many of the processing parameters and for representing the cell and contour attributes. The major thrust of this contract has been program development and initial testing of critical hypotheses such as the possibility of forecasting the locations of new cell sites. A considerable amount of work still remains using the programs to optimize the processing parameters.

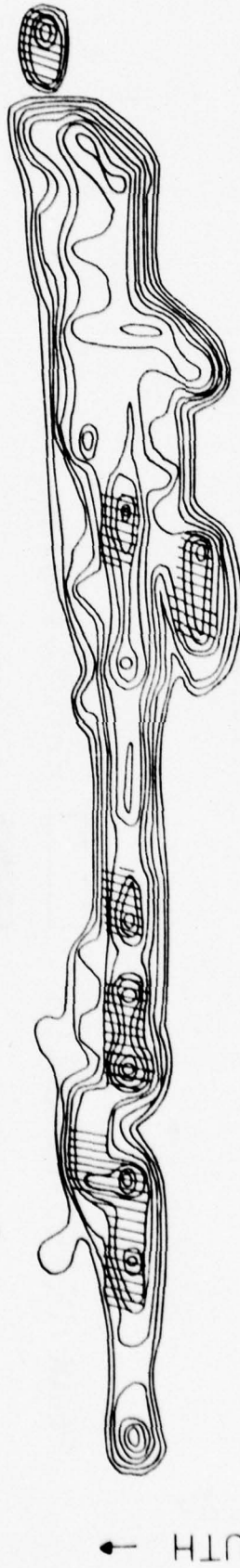
An example of the input radar data for a pair of fixed contours is given in Figure 1. The raw data are the three input parameters, reflectivity, radial velocity, and Doppler (or velocity) spread. An internally generated data field, tangential shear, is also depicted. Contoured data for the three fields used in further processing for one of the echo regions are depicted in Figure 8. In this figure, the quantization steps for each data field are 1 dB, 0.5 m/s, and 0.1 m/s/km for the reflectivity, spread, and tangential shear fields respectively. The reflectivity data show relatively long, thin contours. The basic resolution element for processing, 1° by 0.3 km, is a square on this figure. For more efficient processing, the resolution elements should be adjusted so the contours to be detected are nearly circular. The radar data are read into the computer in 1° by 0.15 km resolution elements. In this example, the data along a radial should be averaged by at least a factor of 6 (3 times the factor used for this figure) to produce 1° x 0.9 km resolution elements. This adjustment may be made automatically in the cell detection program. The spread and tangential shear data show large changes from one resolution element to the next although, with the quantization steps used, the data reveal the same tendency toward elongation as the reflectivity data.

Contours enclosing peak detected cells are indicated by the cross hatching on Figure 8 and on Figure 9. The contours are generated at

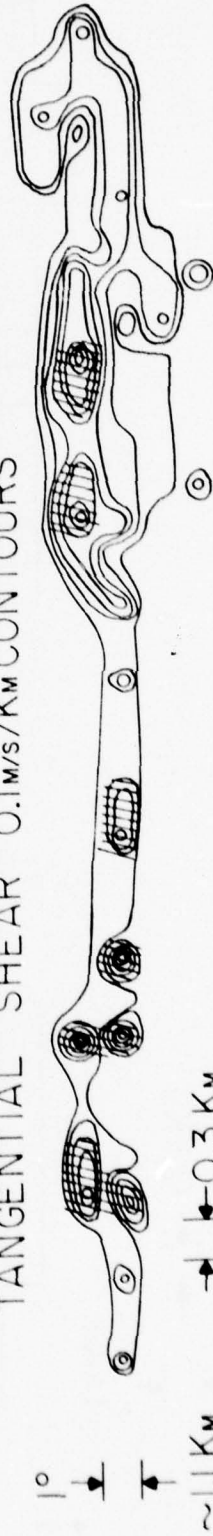
REFLECTIVITY 1dB CONTOURS



DOPPLER SPREAD 0.5m/s CONTOURS



TANGENTIAL SHEAR 0.1m/s/Km CONTOURS



RANGE →

PEAK
 /// DETECTED CELL

Figure 8 Contoured Data from the Sample Set Depicted in Figure 1

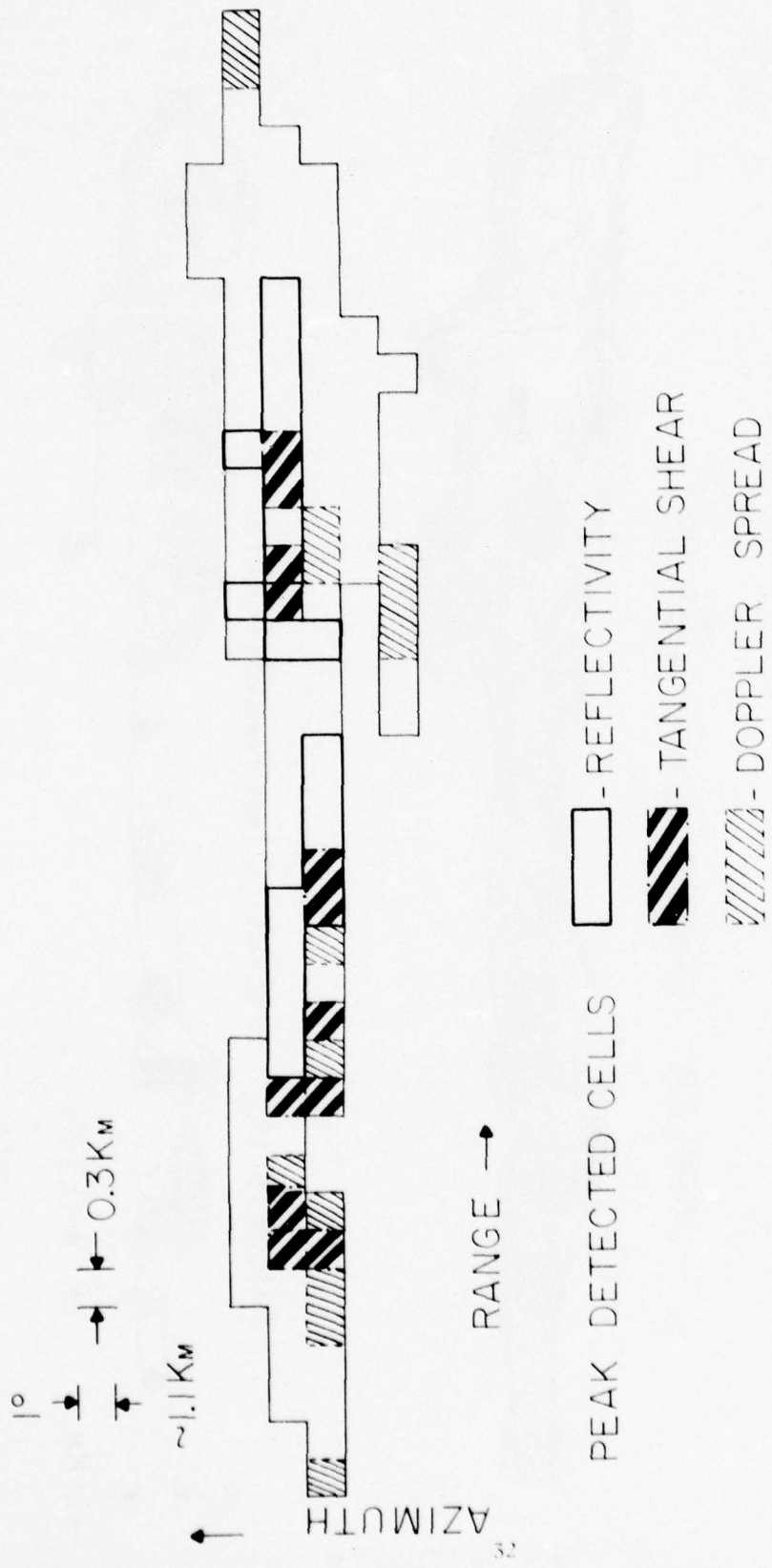


Figure 9 Composite of Fixed Contour Echo and Detected Reflectivity, Tangential Shear, and Doppler Spread Peaks for the Data Depicted in Figure 8

three quantization units below the peak values. The outer contour for reflectivity on Figure 8 and the outer contour on Figure 9 correspond to the 20 dBZ threshold used for processing. Two reflectivity peaks were detected although a shoulder on the first peak (in range, the shoulder is at shorter ranges) would have been detected as an individual cell if two quantization steps were used to define the cell. The shoulder would also be included with the two detected cells in a single cell if the 1° by 0.9 km resolution area were used.

The tangential shear and Doppler spread peaks are shown superimposed on the reflectivity contours in Figure 9. The two tangential shear peaks occur for each reflectivity peak if the shoulder were included. These peaks together with the reflectivity data appear to be delineating the updraft, down draft structure of the cell. With a change to a 1° by 0.9 km resolution area, these sub-cell structures would be averaged to a consistent, one cell picture for this echo region. The Doppler spread data reveal two types of peaks, four of the seven detected peaks coincide with the tangential shear peaks outlining regions of high shear and high spread. These peaks are also intimately related to the reflectivity structure. Three other Doppler spread peaks also are evident at the very edges of the 20 dBZ contour. These peaks correspond to regions of relatively low reflectivity (23 dBZ and lower) and ostensibly represent regions where low signal-to-noise values give rise to deceptively high Doppler spreads.

The number and shapes of the peak referenced cells will vary as the quantization step size, the number of quantization steps for peak detection, and the size of the resolution area are changed. More experience is required using these computer programs to select the optimum combination of these parameters for the detection of physically meaningful cells. As used in generating Figures 8 and 9, it appears that too much detail is present and some of the detected regions especially for spread and tangential shear data represent structure on too small a scale (for example, the individual updraft and downdraft regions within a cell).

5.2 Volume Cell Observations

The volume cell detection program is used to combine the data from a number of individual azimuth scans. Data obtained from the Sudbury radar, subsequent to 1928 GMT on August 13, 1975 using 1° by 0.9 km

resolution areas are depicted in Figures 10-14. These data show the centroid location of each reflectivity peak referenced cell coded both by average reflectivity and by area. The locations of the tangential shear peaks are denoted by X and the locations of Doppler spread peaks are denoted by +.

The data from each of the scans were combined to form volume cells shown in Figure 15. In this figure, the solid lines connect the cell locations as detected on each scan using the algorithms described in Section 3 (Track Program). Cells within 50 km of the radar were detected at elevation angles up to 5° ; cells at further ranges were only detected at elevation angles below 4° (heights less than 5 km). A limited set of volume cell attributes for this data set is listed in Table 2.

Figure 10 Reflectivity, Tangential Shear (X), and Doppler Spread (+)
Peak Locations for a 1° Elevation Angle

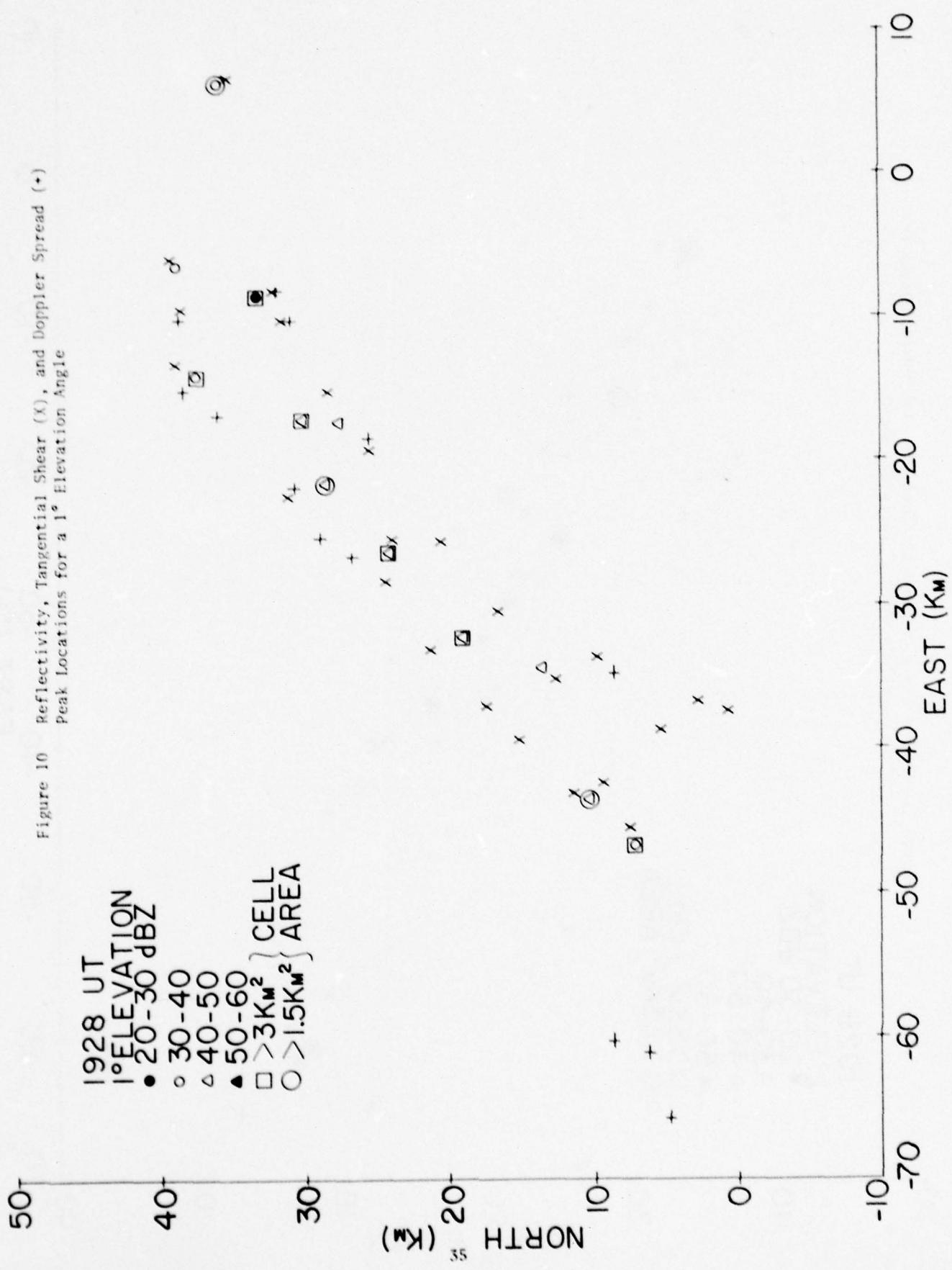


Figure 11 Reflectivity, Tangential Shear (X), and Doppler Spread (+)
Peak Locations for a 2° Elevation Angle

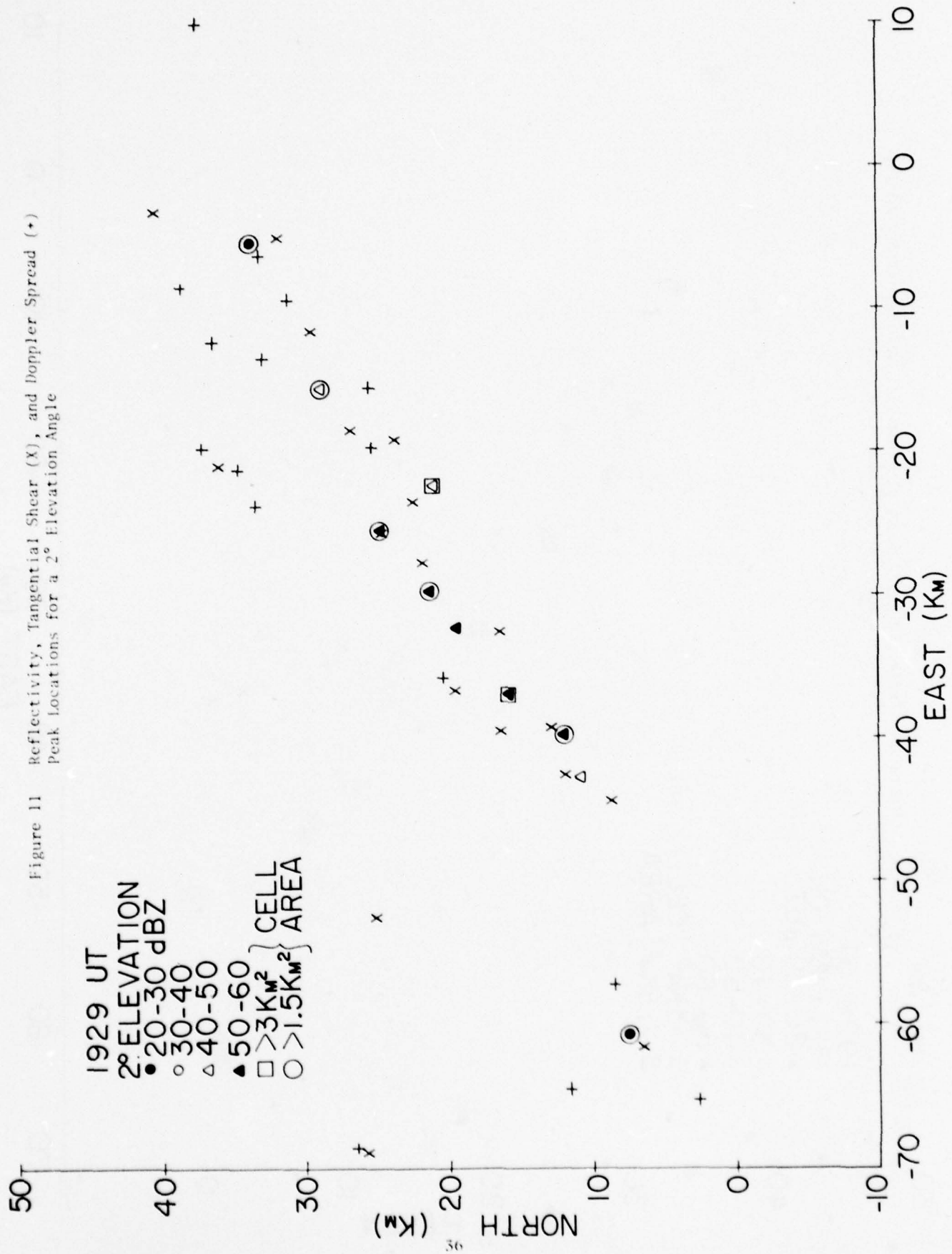
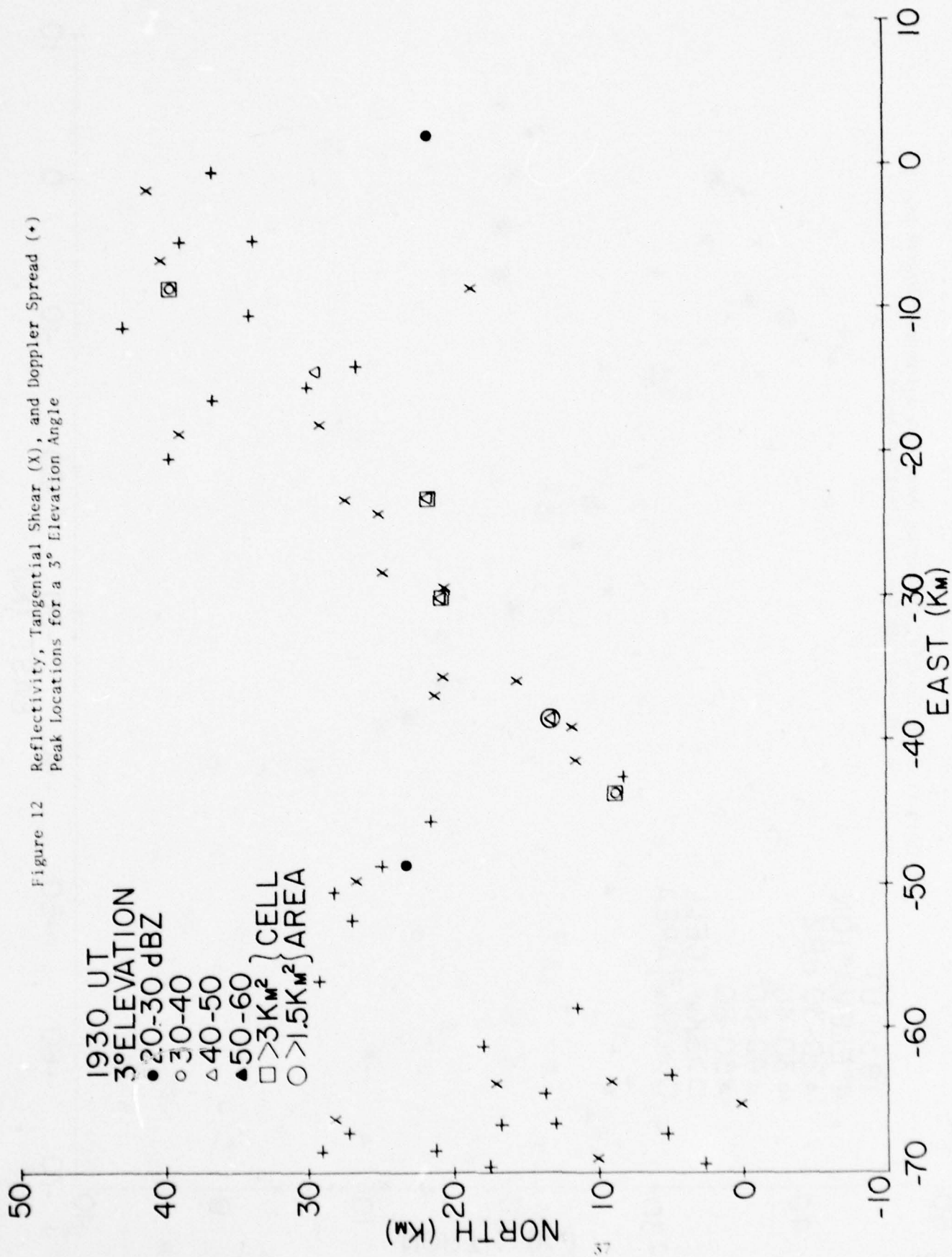


Figure 12 Reflectivity, Tangential Shear (X), and Doppler Spread (+)
Peak Locations for a 3° Elevation Angle



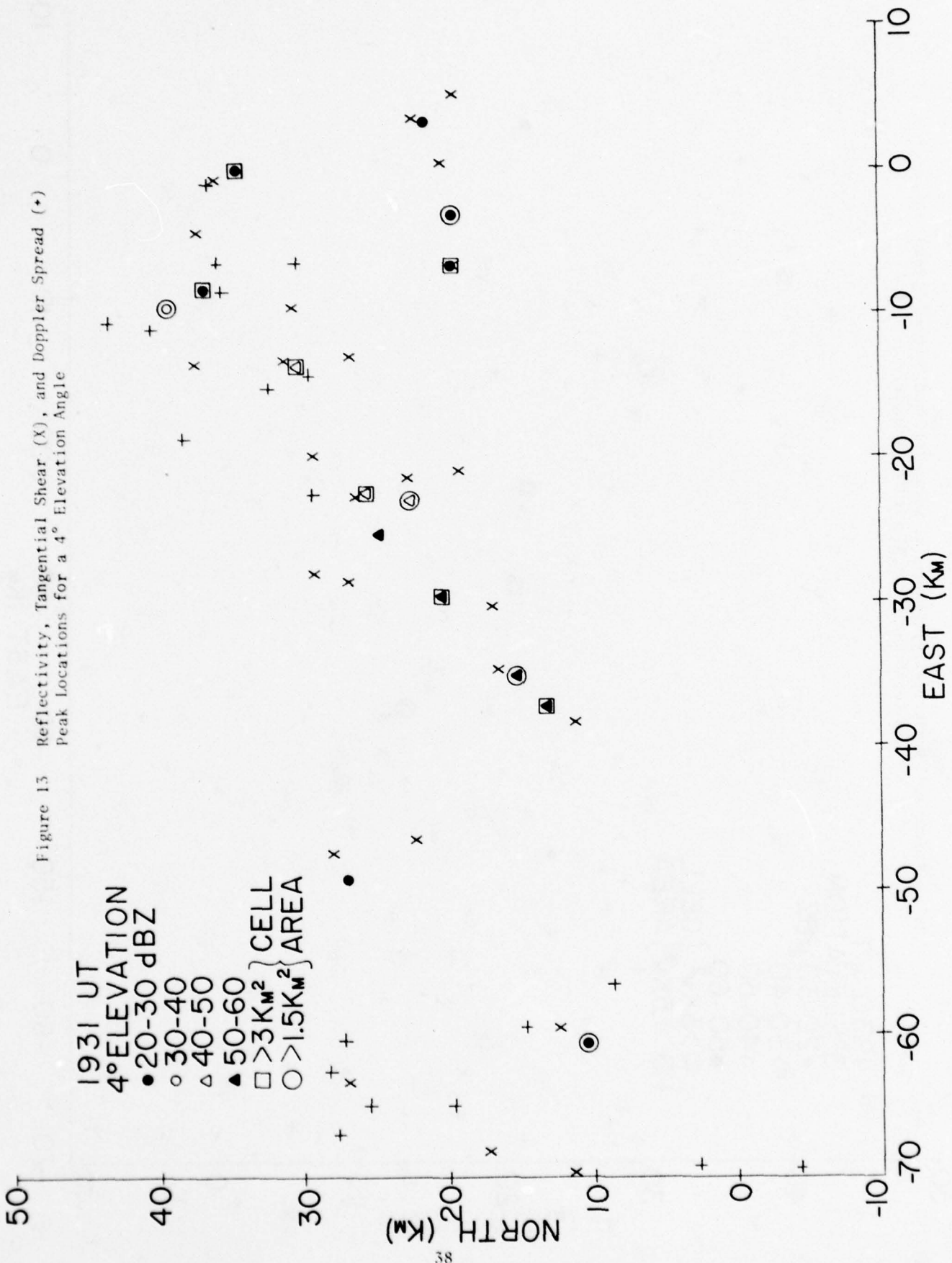


Figure 13

Reflectivity, Tangential Shear (X), and Doppler Spread (+)
Peak Locations for a 4° Elevation Angle

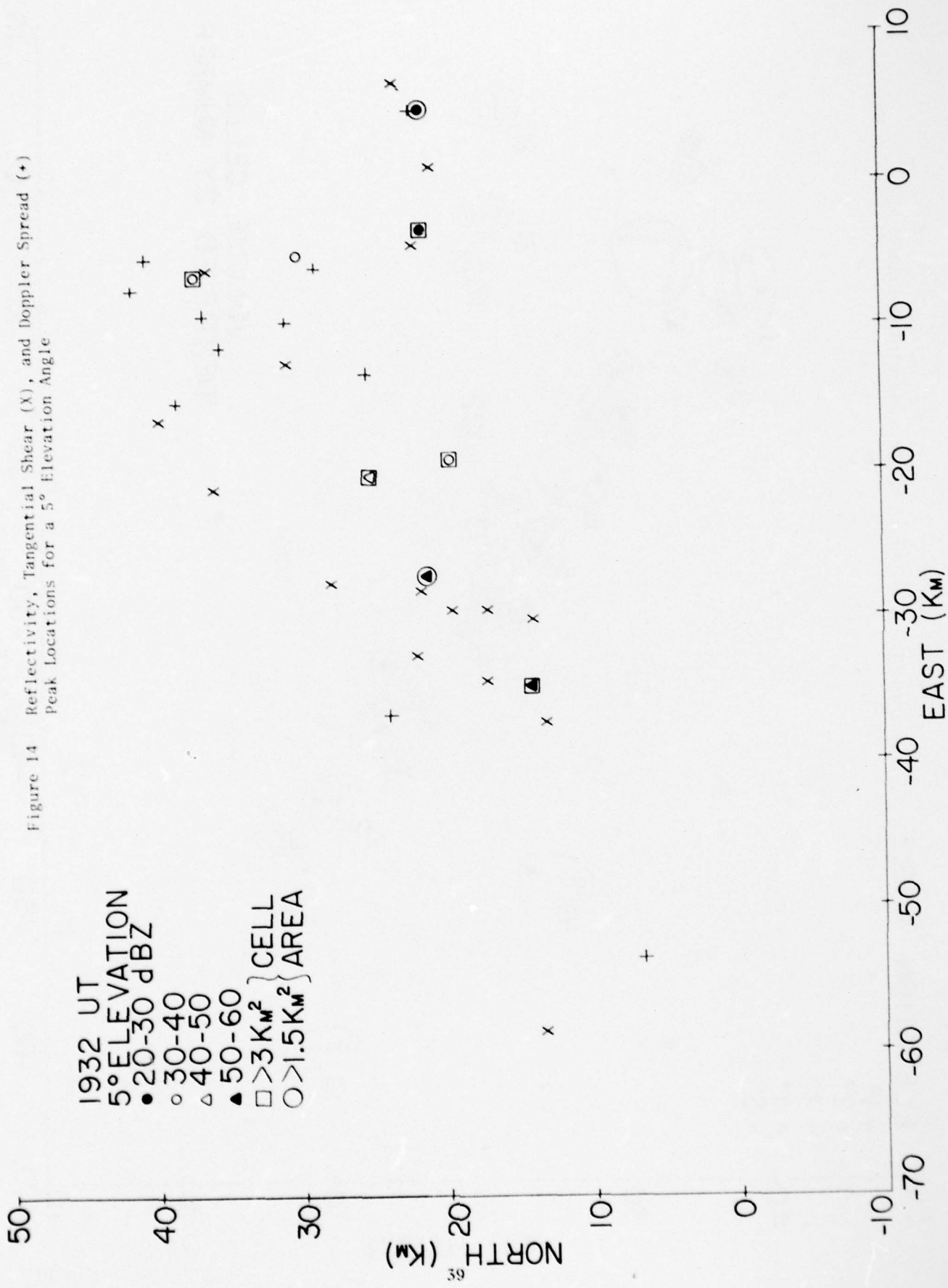


Figure 14 Reflectivity, Tangential Shear (X), and Doppler Spread (+) Peak Locations for a 5° Elevation Angle

ELEVATION ANGLE

- 1°
- 2°
- ▲ 3°
- △ 4°
- × 5°

Figure 15 Volume Cells for Data Depicted in Figures 11-14

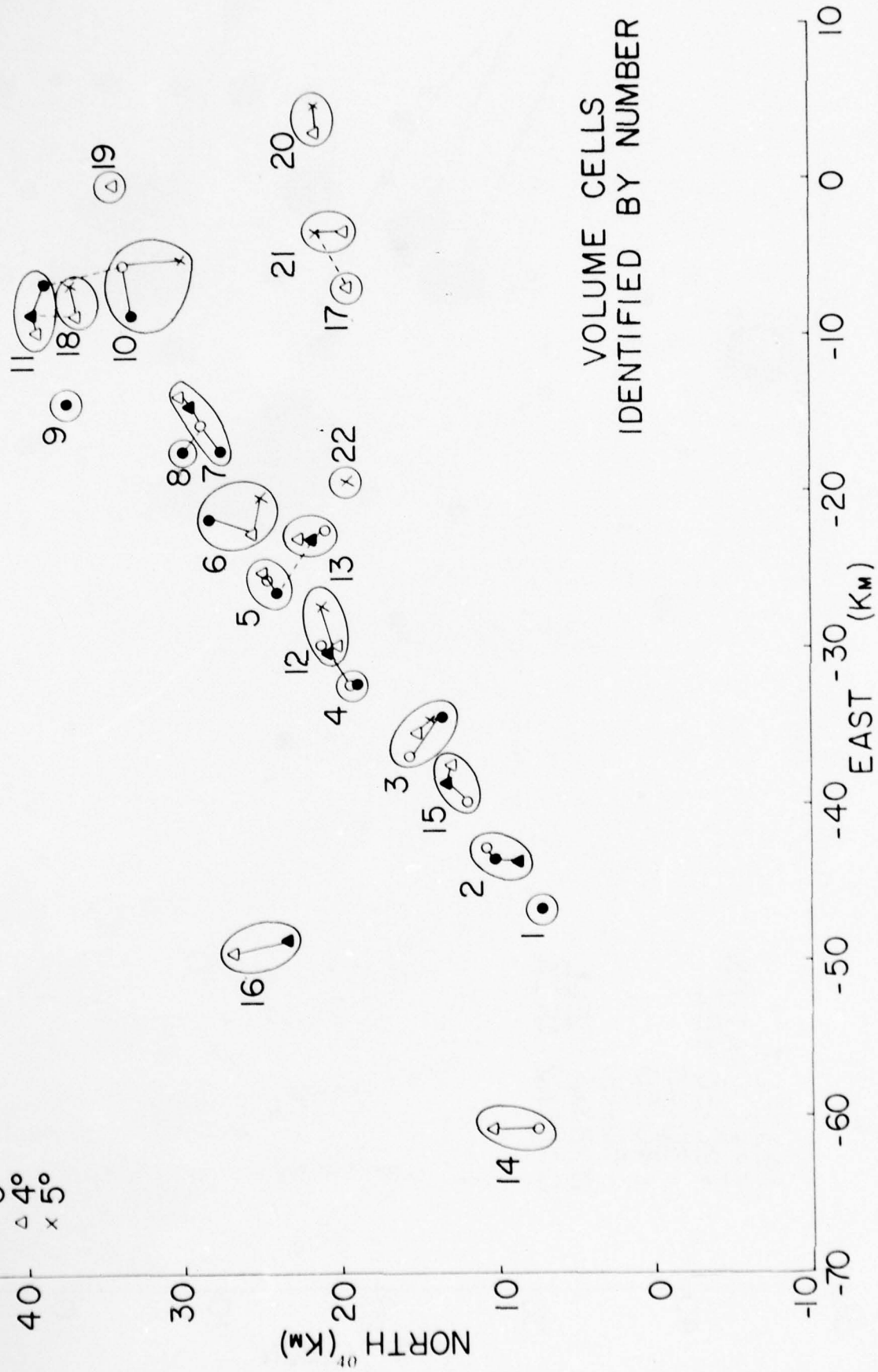


TABLE 2
VOLUME CELL ATTRIBUTES

ID*	X	Y	H _p	Z _p	H _b	H _T	ΔH	Δp	Volume
1	-46.8	7.3	0.9	39.9	0.9	0.9	0.5	4.0	2.0
2	-43.8	10.3	1.7	49.0	1.1	1.8	0.7	1.5	1.1
3	-34.4	13.7	3.4	54.9	2.9	-	-	3.5	-
4	-32.3	19.1	1.4	53.2	0.9	1.4	0.5	1.5	0.8
5	-26.4	24.1	2.5	52.9	1.0	2.4	1.4	5.4	7.6
6	-21.8	28.5	2.5	49.5	1.9	-	-	3.5	-
7	-17.4	27.8	2.4	47.8	0.7	2.4	1.7	3.2	5.4
8	-17.2	30.1	0.7	40.9	0.7	0.7	0.5	3.9	2.0
9	-14.2	37.5	0.8	33.0	0.8	0.8	0.5	4.4	2.2
10	- 8.9	33.1	2.7	30.7	1.8	-	-	1.4	-
11	- 6.8	38.8	2.2	31.9	0.8	2.9	2.1	2.0	4.2
12	-29.8	21.3	2.4	55.3	1.4	-	-	3.5	-
13	-22.4	21.1	2.3	44.6	1.1	2.3	1.2	1.4	1.7
14	-60.9	7.6	2.4	29.1	2.4	3.6	1.2	1.9	2.3
15	-39.9	12.0	2.2	53.6	1.7	2.8	1.1	1.2	1.4
16	-48.7	23.4	3.0	25.7	3.0	4.0	1.0	12.9	12.9
17	- 6.9	19.8	1.5	21.9	1.5	1.5	0.5	3.4	1.7
18	- 8.5	36.5	3.4	31.0	2.7	-	-	1.9	-
19	- 0.0	34.2	2.5	23.8	2.5	2.5	0.5	1.0	0.5
20	3.4	21.7	2.0	22.4	1.6	-	-	9.0	-
21	- 3.1	19.9	1.9	22.5	1.4	-	-	12.4	-
22	-19.3	-19.8	2.5	39.1	2.5	-	-	1.0	-

*See Figure 15

6. RECOMMENDATIONS

6.1 Parameter Optimization

A set of computer programs has been generated to provide an automatic means for the extraction of information from large volumes of radar data. The programs are written to be as general as possible to enable rapid changes in processing parameters. As indicated in Section 5, the optimum values for these parameters are not known and must be determined. It is expected that the parameters should change from one radar system to the next depending principally on the resolution volume and number of independent samples per resolution element. The first problem to be considered in the use of this set of programs is the optimization of parameters. This can only be done by processing a relatively large number of radar scans for different rain conditions.

Ideally, auxiliary data should be available to provide a standard of comparison for the output from the program. Many case studies such as the one reported in Section 5.1 should be performed to obtain the raw contour data to provide a comparison standard. For use in detecting severe weather events, auxiliary data on the severe events are also required.

6.2 Real Time Processing

The programs, although general in nature, were written with the ultimate goal of use in a real time processor. After the analysis for parameter optimization has been completed, specialization to a real time processor may be accomplished. Real-time processing requires the minimization of computer storage and operating time. Major steps can be made in this direction by increasing the resolution element area for processing (averaging over ≈ 1 km in range as recommended in Section 5.1) and by reducing the number of peak detection operations. The latter can be accomplished by processing either tangential shear or Doppler spread data but not both as is currently done. Another time saving step is to reduce the volume of output by not preparing the fixed level contour plotting displays in the computer but doing the fixed contouring in the color display processor as is currently done for the output of digital integrators.

Preprocessing of the data for calibration, velocity ambiguity resolution, and conversion from variance to velocity spread will also save some time.

Current running time for reflectivity processing only but including fixed contour generation for display is 2 minutes per azimuth scan. By just doing the preprocessing, the running time could be reduced by more than a factor of two. The other reductions recommended above plus internal programming changes to reduce the use of indirect array addressing should result in a program that will do at least two data fields, reflectivity and tangential shear or Doppler spread, in real time (30 seconds per scan).

6.3 Spatial Analysis of Cell Development

The initial considerations of the forecast of new cell site locations indicates that improvements should be possible if attention is focused on the structure or organization of the cell location patterns. Processing to date has used the determination of nearest neighbor distances to obtain information about cell spacings. The nearest neighbor distances provide estimates of the locations of secondary maxima in the spatial correlation function for cell locations. Information on structure can better be obtained from more refined correlation function (or spatial power spectra) of cell location. These analyses should be conducted using a much larger data sample preferably for a number of different locations and storm types.

6.4 Morphological and Climatological Analysis

The programs described above are used to extract the significant information from a large volume of radar data. The result is still a formidable data set comprised of a number of lists of volume cell attributes for each scan, storm, and day. These data must in turn be reduced to a manageable set to describe the morphology of cell development. This analysis must be performed before any meaningful cell forecast procedures can be developed and tested. The analysis entails both the construction of new programs and the processing of large volumes of data.

REFERENCES

- Crane, R.K. (1976): "Radar Detection of Thunderstorm Hazards for Air Traffic Control Vol. I Storm Detection", Project Report ATC-67, Vol. I, MIT Lincoln Laboratory, Lexington, Massachusetts.
- Crane, R.K. (1977): "Parameterization of Weather Radar Data for Use in the Prediction of Storm Motion and Development", Final Report, Contract No. F19628-76-C-0264, Environmental Research & Technology, Inc.; AFGL-TR-77-0216, Air Force Geophysics Laboratory, Hanscom Air Force Base, Massachusetts.

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APPENDIX A

CELL DETECTION AND TRACKING PROGRAM INSTRUCTIONS FOR OPERATION

A.1 Description of Input and Output

Program input and output are depicted in Figure A1. The tape input format is given in Table A1. The control cards are discussed in section A2. The program produces (a) tapes of computed attributes for input to a second program for computing volume scans; (b) a plot tape is generated that can be stored for input to another program "EXPAND" which is a general purpose plotting package for plotting the fixed contours, centroids, cell identification and peak locations expanded over selected areas; (c) B-scan maps are also produced as an option; and (d) at the completion of a scan the program will print out fixed contour attributes, peak detected cell attributes and tangential shear maxima attributes. All of the attributes printed have identifiers which can be associated with the identifiers displayed on the expanded plots.

A.2 Control Card Format

Control card input to the program is NAMELIST input which allows certain parameters in the program to default or to be set to different values. The variable names, type (LOGICAL L, INTEGER I, and REAL R), dimension, default value and their meanings are listed in Table A2.

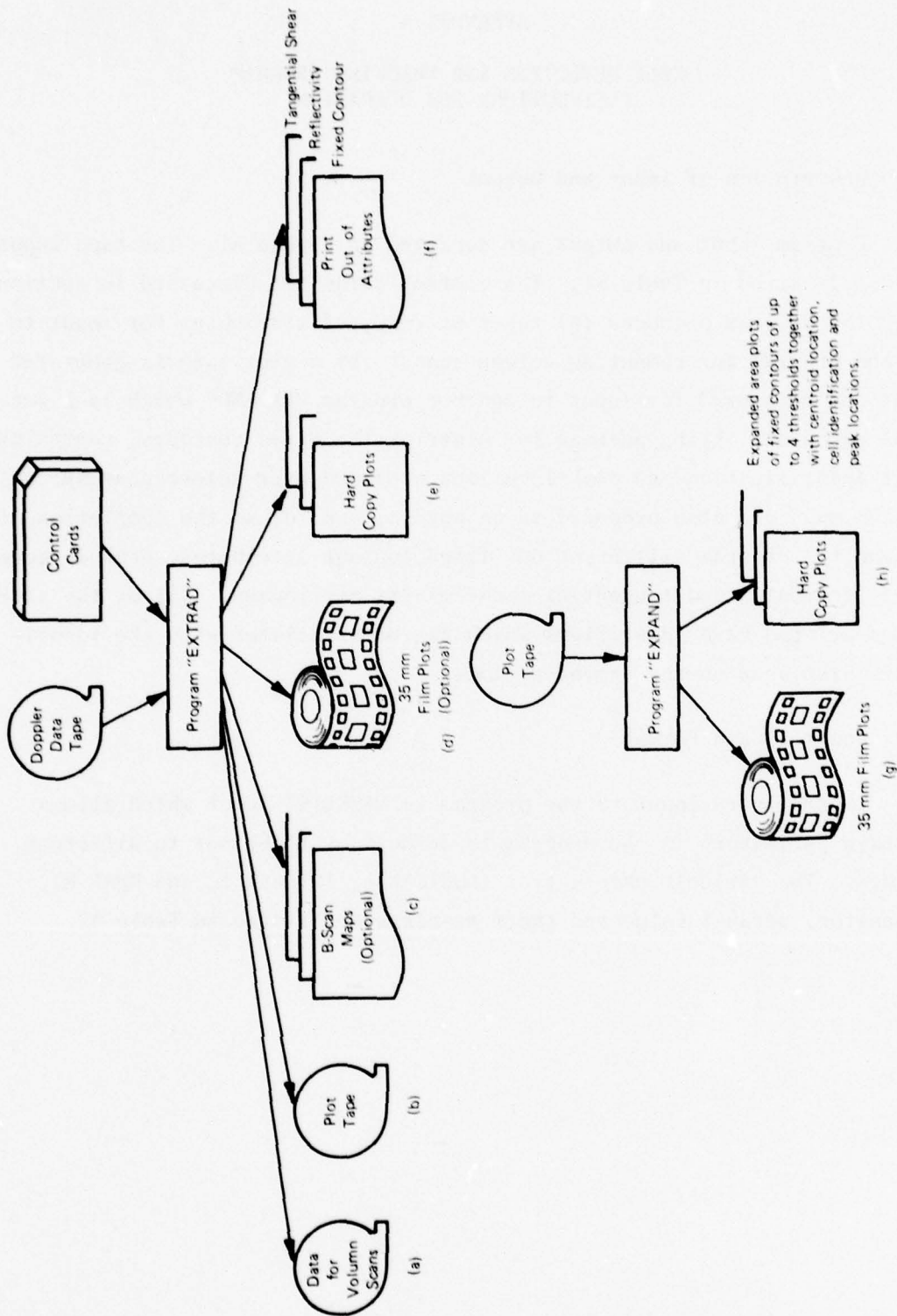


Figure A1 EXTRAD Products

	2 ¹¹	2 ¹⁰	2 ⁹	2 ⁸	2 ⁷	2 ⁶	2 ⁵	2 ⁴	2 ³	2 ²	2 ¹	2 ⁰	12 Bit Word Position
Day	800	400	200	100	80	40	20	10	8	4	2	1	1
Hour				20	10	8	4	2	1				2
Min			40	20	10	8	4	2	1				3
Sec						40	20	10	8	4	2	1	4
Status		T _p ¹	T _p ⁰	SF ₁	SF ₀		DD	¹⁾ NRC ₁	¹⁾ NRC ₀				5
*PRF		B		A									6
Azimuth		PRF ₁₁	PRF ₁₀	PRF ₉	PRF ₈	PRF ₇	PRF ₆	PRF ₅	PRF ₄	PRF ₃	PRF ₂	PRF ₁	PRF ₀
Spare		AZ ₁₁	AZ ₁₀	AZ ₉	AZ ₈	AZ ₇	AZ ₆	AZ ₅	AZ ₄	AZ ₃	AZ ₂	AZ ₁	²⁾ AZ ₀
Spare													8
Elevation		EL ₁₁	EL ₁₀	EL ₉	EL ₈	EL ₇	EL ₆	EL ₅	EL ₄	EL ₃	EL ₂	EL ₁	²⁾ EL ₀
Spare													11
Spare													12
Mean		⁵⁾ M ₁₁	⁵⁾ M ₁₀	M ₉	M ₈	M ₇	M ₆	M ₅	M ₄	M ₃	⁴⁾ M ₁	²⁾ M ₂	13 + (I-1)·3
Variance		⁵⁾ V ₈	V ₇	V ₆	V ₅	V ₄	V ₃	V ₂	V ₁	²⁾ V ₀			14 + (I-1)·3
Power		⁶⁾ P ₈	P ₇	P ₆	P ₅	P ₄	P ₃	P ₂	P ₁	²⁾ P ₀			15 + (I-1)·3

ANCILLARY DATA

VIDEO DATA
Repeated 256 times**

T_{p1} T_{p0}
0 0
0 1
1 0

Cell Width
0.5 μs
1 μs
2 μs

Subframe
SF₁ SF₀
0 0
0 1
1 0
1 1

Frequency of Dump Pulses DD
ALT 0
ALL 1

1) Number Range Cells	NRC ₁	NRC ₀
256	0	0
512	0	1
768	1	0
1024	1	1

- 2) Least Significant Bit
- 3) -----
- 4) Not Included in Parity
- 5) Sign
- 6) Parity

1 physical record = 158 sixty bit words

* If any group A bit = 1 and any group B bit = 1: PRF = 394
 If A has 1 bit and B has 3 bits: PRF = 794
 If A has 3 or more and B has 1 or less: PRF = 1613
 If A has 3 or more and B has 3 or more: PRF = 3333
 If A has 2 bits or B has 2 bits: PRF = Previous PRF
 If all zero for A and B groups: use an input PRF

** First cell is the 21st twelve bit data word.

TABLE A1

TABLE A2

CARD FORMAT FOR PROGRAM EXTRAD

Reads in program parameters via NAMELIST format.

NAMELIST VARIABLES: (Level 780415)

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
PRINT1	L	1	FALSE	Unused.
PRINT2	L	1	FALSE	If .TRUE. print B-scan maps of mean and variance.
PRINT3	L	1	FALSE	If .TRUE. print B-scan maps of dBz.
PRINT4	L	1	FALSE	Unused.
ICODES	I	36	Blank thru Z then 1 thru 9.	Codes for representing dBz categories for B-scan map output.
A1	R	1	.13779	In the linear equation $y = mx+b$ for computing coded dBz for B-scans, A1 = M and B1 = b.
B1	R	1	1.5	
A2	\$	1	.017	Unused.
B2	R	1	18.6	Unused.
CONTRZ	L	1	TRUE	If FALSE, do not process peak cell attributes.
CONTRV	L	1	TRUE	If FALSE, do not process reflectivity, shear, & spread.
CONTRS	L	1	TRUE	If FALSE, do not process shear and spread.
NFILE	I	1	0	Number of files on tape to skip before processing.
NUMF	I	1	1	Number of files on tape to process.
AC	R	4	-107.7, +1.97, -0.94, +.0018	Calibration coefficients for computing DBM below a threshold XCUT. (see XCUT)

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
COPLLOT	L	1	FALSE	If TRUE, output a tape for plotting.
VOLTAP	L	1	TRUE	If FALSE, do not output an attribute tape.
CALM	R	1	.332	In the calibration equation for DBM $y = mx+b$, CALM = M & CALB = b.
CALB	R	1	-98.3	
XCUT	R	1	10.0	Threshold value that determines which equation to use for calibration. (linear or non-linear)
CK	R	1	10.0	In the equation for computing dBz, $K+P+20\text{ALOG}_{10}(S(I-.5))$ K = CK.
ZMAX	R	1	0.0	Not currently used.
VMAX	R	1	0.0	Not currently used.
NREC	I	1	1	Not currently used.
NUMR	I	1	999	Number of radials to be processed. Use default value when doing full scan.
IRUN	I	1	0	Run number chosen by user.
INC	I	1	0	Not currently used.
STARTR	R	1	0.0	Where along a radial in kilometers processing is to start.
STOPR	R	1	300.0	Where along a radial in kilometers processing is to stop.
INPRF	I	1	3333	Value of PRF (Pulse Repetition Frequency) to be used when PRF cannot be obtained from the data tape.
SCALE	R	1	1.0	Scale factor for drawing fixed contours.
AE	R	1	1.21	Constant for computing heights of cells.
AA	R	1	300	Constant for computing rain rate.
BB	R	1	1.5	Exponent for computing rain rate.

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
X1	R	1	0.0	Frame size coordinates for fixed contour plotting. Less than or equal to 8 inches.
X2	R	1	8.0	Same as above.
Y1	R	1	0.0	Same as above.
Y2	R	1	8.0	Same as above.
TV	I	1	35	Mean wind velocity in a fixed echo contour is not computed for dBz greater than this value.
TSV	R	1	10 ⁶	Not currently used.
LDV	I	1	3	Cell detection threshold for reflectance peaks.
LTV	I	1	3	Cell detection threshold for velocity peaks.
LSV	I	1	3	Cell detection threshold for shear peaks.
ICOMP	I	1	6	Data compression factor. (range integration)
VMIN	R	1	0.0	Unused.
SVMIN	R	1	0.0	Unused.
AREAMN	R	1	1.0	Any completed contour having an area less than AREAMN will be ignored but is plotted if a fixed contour.
WAVEL	R	1	0.0542	Radar wavelength in meters.
VQUANT	R	1	10.0	Tangential shear quantization step (m/s/km) ⁻¹ .
SQUANT	R	1	2.0	Doppler spread quantization step (m/s) ⁻¹ .
RQUANT	R	1	1.0	Reflectivity quantization steps (in dB ⁻¹).
DAZM	R	1	1.0	Beam width (degrees).

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
ESTART	R	1	(1.5°)	Elevation start angle (degrees).
DELT	R	1	(.5°)	Delta elevation angle (degrees) defining next scan.

5
4
3
2
1

NORTH
39
(KM)

APPENDIX B

PLOTTING PROGRAM 'EXPAND' (VERSION 1.0)

B.1 Description of Input and Output

Program EXPAND utilizes the plot tape generated by program 'EXTRAD' as input to generate not only full scan plots of fixed contours and their centroids but on option will expand and plot certain areas of interest. Also on option, it will plot out locations of centroids of fixed contours, peak detected cells, Doppler spread and tangential shear locals. These plotting options apply to full scan plots as well as expanded plots.

The plots are generated on the CALCOMP ink pen drum plotter. The X axis are labeled negative kilometers west of the radar and positive east. Y axis are labeled negative kilometers south of the radar and positive north. The date and elevation angle are also annotated.

B.2 Control Card Format

Control card input to the program is NAMELIST input which allows certain parameters to default or to be set to different values. The variable names, type, dimension, default and meaning are listed in Table B1.

It is suggested that program EXPAND generate full scan plots of fixed contours from the entire EXTRAD tape first before generating expanded areas of view. This allows one to examine exactly what each scan contains and where expansion would be of interest. One set of NAMELIST input cards are needed for each scan. If, for example, it is desired to go into the third scan on tape, three NAMELIST set ups must occur.

TABLE B1

CARD FORMAT FOR PROGRAM EXPAND
 READS IN PROGRAM PARAMETERS VIA NAMELIST INPUT

NAMELIST VARIABLES:

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
IPLT	L	4		
IPLT(1)	L		.FALSE.	If .TRUE. plot a dot to locate peak detected cells.
IPLT(2)	L		.FALSE.	If .TRUE. plot a C to locate fix contour centroids.
IPLT(3)	L		.FALSE.	If .TRUE. plot a + to locate Doppler spread.
IPLT(4)	L		.FALSE.	If .TRUE. plot an X to locate tangential shear.
Z1	L	1	.TRUE.	Plot fix contours for first level contour.
Z2	L	1	.TRUE.	Plot fix contours for second level contour.
Z3	L	1	.TRUE.	Always set to .FALSE.
Z4	L	1	.TRUE.	Always set to .FALSE.
LS	L	1	.FALSE.	When .TRUE. expanded area plots are requested. When .FALSE. draw full scan only.
XK1	R	1	-320.0	Western plot area limit (km).
XK2	R	1	320.0	Eastern plot area limit (km).
YK1	R	1	-320.0	Southern plot area limit (km).
YK2	R	1	320.0	Northern plot area limit (km).
LK	L	1	.FALSE.	If .TRUE. plot centroids of given areas.

*Note: Expanded plots will always square off any rectangular area request to the largest axis requested.

APPENDIX C

TRACKING PROGRAM (ASOCCL)

C.1 Description of Input and Output

The input tape is the tape produced by program "EXTRAD". This program takes the cell attributes and associate cells for tracking volume cells. The output listing includes the location of volume cells and the updated cell ID.

C.2 Control Card Format

Control card input to the program is NAMELIST input which allows certain parameters in the program to default or to be set to different values. The variable names, type (LOGICAL L, INTEGER I, and REAL R), dimensions, default values and their meanings are listed in Table C1.

TABLE C1

CARD FORMAT FOR PROGRAM ASOCCL

Reads in Program Parameters via NAMELIST Format

NAMELIST VARIABLES:

<u>NAME</u>	<u>TYPE</u>	<u>DIMENSION</u>	<u>DEFAULT</u>	<u>MEANING</u>
PR1	L	1	FALSE	When .TRUE. program prints out the input attributes data.
PR2	L	1	FALSE	When .TRUE. program prints out the initial volume cell attributes and the total number of cells.
PR3	L	1	FALSE	When .TRUE. program prints out the associated update cell attributes and the total number of associated cells.
PR4	L	1	FALSE	Currently unused.
IDEV1	I	1	1	Input tape or file.
IDEV2	I	1	1	Currently unused.
ISTOP	I	1	1	Stop program, when "0" continue processing.

APPENDIX D
COMPUTER PROGRAM LISTINGS
AND SAMPLE OUTPUT

1	C	PROGRAM EXTRAD INPUT, OUTPUT, TIMES (IMP), TIMES OUTPUT (TAPE IN, TAPE2, TAPE3, DEBUG-OUTPUT, TAPE5, TAPE6)	EXTRAD
	C	PROGRAM EXTRAD EXT NO. 102	EXTRAD
	C	VERSION 2.8 LEVEL 761119	EXTRAD
3	C	MAIN PROGRAM SECTION.	EXTRAD
	C	JMW AFGL CDC 6688	EXTRAD
	C	LOGICAL PRINT1, PRINT2, PRINT3, COPLT, CONTRZ, CONTRY, CONTRS, VOL TAP	EXTRAD
	C	INTERCH/CHRTZ	TEST
10	C	COMMON /PARM/ PRINT1, PRINT2, PRINT3, COPLT, ICODES (B6), A1, B1, A2, B2, TEST	EXTRAD
	C	CONTRZ, CONTRY, CONTRS, MPLE, ROW, NREC, NROW, NCOLTRP	TEST
	C	DATA CHRD/4HPARA, 4MEXEC, 4MCDMM/	EXTRAD
	C	CALL DAY	EXTRAD
15	I	READ (5,10) KEY	EXTRAD
	11	FORMAT (A6)	EXTRAD
	21	IF (EQU(9)) 91, 21, 91	EXTRAD
	21	CALL PAGE	EXTRAD
20	31	WRITE (6,31) KEY	EXTRAD
		DO 51 K=1,3	EXTRAD
		IF (KEY.EQ.CHRD(K)) GO TO (61,71,81), K	EXTRAD
	51	CONTINUE	EXTRAD
	51	WRITE (6,51)	EXTRAD
	51	FORMAT (1GH ILLEGAL KEYJRD)	EXTRAD
		GO TO 91	EXTRAD
	C	* PARAMETERS * PACKAGE.	EXTRAD
	C		EXTRAD
30	61	CALL IMPARM	EXTRAD
		GO TO 1	EXTRAD
	C		EXTRAD
	C	* EXECUTION * PACKAGE.	EXTRAD
	C		EXTRAD
35	71	CALL EXTRAT	EXTRAD
		GO TO 1	EXTRAD
	C		EXTRAD
	C	* COMMENTS CAPJ * PACKAGE.	EXTRAD
	C		EXTRAD
40	91	CALL IME (5)	EXTRAD
		GO TO 1	EXTRAD
	C		EXTRAD
	C	END OF JOB.	EXTRAD
	C		EXTRAD
45	91	WRITE (6,101)	EXTRAD
	101	FORMAT (//Z1,7+ EMOJOB)	EXTRAD
	111	STOP	EXTRAD
		END	EXTRAD
			EXTRAD

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM
 22 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```
1 C BLOCK DATA
*****
C FOR PROGRAM EXTRAD ERT NO. 162
C VERSION 2.0 LEVEL 761119
C JHW C06500 MFCL
*****
C LOGICAL PRINT1,PRINT2,PRINT3,COPLDT,CONTRZ,CONTRV,CONTRS,VOLTAP
INTEGER TL ,IV,TSV
*****
C COMMON /PARM/ PRINT1,PRINT2,PRINT3,COPLDT,ICODES(36),A1,B1,A2,B2,
ICONTZ,CONTRV,CONTRS,FILE,NOMF,ANKE,NUMK,VOLTRP
COMMON /INSUB/ TL(2),LT,TC,ON,STARTR,STOPR,RN(4),SCON,CELMTH(3)
C /ICOMP,VMIN,SVMIN,TESTARR,DELT
COMMON /AZM/ AZMTH(460),NA,ELEVAT,PRF,KEEP
*****
C COMMON /AIBZ4/ MVPT(3,1024)
COMMON /VALMAX/ ZMAX,VMAX,AC(4),CALM,CALB,XCUT,CK,INC
COMMON /NDATA/ DORY,TRIDR,CTIN,ISECT,MP,NSF,NDOT,RC
COMMON /HEAD/ TITLE(6),ICODES,SECS,LEVEL,DAT,IRUN,NPAGE,NLOG
COMMON /LINDM/ LINE
*****
C COMMON /HORED/ INPRF,SCALE,LDIV,LTVALSV
COMMON /STORE/ AE,AA,AB,SL,CL,TV,TSV
COMMON /EXPAR/ XI,XZ,YA,YZ,XMIN,XMAX,YMIN,YMAX
COMMON /ERROR/ IERR
COMMON /FILTER/ FTRM,AREANN,DKZH
COMMON /VELEPRM/ WAVEI
COMMON /QUANTY/ QUANT,ROUANT
COMMON /PMORCK/ IPIC(22),IC(30,22),IPCNT(30,22),SMA X,I(50),JMXDB,
*****
C JMAX,IPIC(2640),IPC(2640),IPG(2640),IPMAX,
*****
C COMMON /FIXED/ IC(4,22,2),IB(4,22,2),MPA,EMKX,NFG,ICVNT(2),
IBVNT(2),ATR(5,120,2),IAT,MIDF,KDD(2),IDSLDT(120,2)
COMMON /PRSTORE/ OPT(20,3),NOP,TATR(70,29),NUMAX,ACT(70),
IOG(22),IPB(22),TB(30,22),IPBT(30,22),
IPSKG(50),IPB(2640),IPZ(2640),IPZ(2640),IPB(2640)
COMMON /PVSTORE/ UV(200,7),NUV,VATR(70,23),NPMAX,IACV(70),
IDVCT(27),IP(108,22),TV(130,22),IPB(130,22),
IPVANG(50),IPV(12640),IPV(12640),IPV(12640)
COMMON /PSSSTORE/ US(200,5),NUS,SATR(70,17),NSMAX,ZACS(70),
IOSC(22),IPISB(22),TSB(30,22),IPBSNT(30,22),
IPSKNG(50),IPST(2640),IPSZ(2640),IPST(2640)
COMMON /REFL/M(173),M(173),VJ(173),HR(173),NCL,MIDF,INCL
*****
C X2,IMX,IPM
*****
C DATA PRINT1,FALSE,PRINT2,FALSE,PRINT3,FALSE,COPLDT,TRUE,EL
+/A1,443/461,56/42/96,32/18.6,CONTRZ,TRUE,CONTRV/
+/VOLTAP,TRUE,
DATA VLZ(20,40)
DATA XL(0,0),XZ(0,0),Y1(0,0),Y2(0,0),AE/1.21,AA/400.7,BB/1.4/
DATA SL(0,0),CL(0,0),TV(357),TSV/1000007
DATA LT(2),START(20,1),STOP(150,1),ICOMP/6/
DATA PRIN(0,0),SVTR(70,3),AREANN(1,0),DREZ(76,0)
DATA DM(0,0),DN(0,0),RV(256,0),S1(2,0),764,0,1024,0/
DATA CELMTH(0,5),I(0,2),2.07
DATA ICODES /1M,1HA,1H3,1HP,1HG,1HR,1HS,1HT,1HU,1HV,1HW,1HX,1HY,
```

```

*      IMZ,IM1,IM2,IM3,IM4,IM5,IM6,IM7,IM8,IM9/
DATA ZMAX/0.0/,VMAX/0.0/,AC/-107.76555,1.9767838,-.094297528,.0801
TEST 32
88 18226317,CALH/0.332/,CALB/-38.3/,XCUT/10.0/
EXTRAD 92
DATA TITLE/PROGRAM,74 EXTRAD,1M,1M,1M,1M /
EXTRAD 94
DATA IRUN/0/,NPAGE/0/,LJODE/162/,VERS/2.0/,LEVEL/788501/
EL 6
DATA IMPRF/794/
EL 7
DATA CK/18.0/,INC/0/
EL 8
DATA SCALE/1.0/,LDW/3/,-10/3/,LSV/3/
TEST 33
DATA YERR/0/
EXTRAD 99
DATA WAVE/0.0542/
TEST 34
DATA VOURN/18.0/,SOURN/76.87/,ROURN/71.0/
EL 9
DATA M10F/120/,IAT/5/,N2A/4/,IEMAX/22/,MFC/2/
TEST 36
DATA KRX/30/,JRX/0/50/,JMX/50/,LMAX/2500/,IW/4/,JK/30/,KR/22/,
TEST 37
*      IWX/124/,NCL/123/
TEST1 5
DATA M10Z/200/,MOP/97/,M13/778/,MUMAX/25/
TEST 38
DATA MVMAX/23/,MUV/7/,M5HAX/17/,MUS/5/
TEST 40
DATA ESTPR/71.57/DELT/57
EL 10
-----
EXTRAD 102
END
EXTRAD 103

```



```

        JK=TL(I)+IK-1
    C PRESET PAIR RATE - 1 DBZ STEPS
    C DBZARY(IK)=X0.**((B0*FLOST(IK)-AK)
    C BUILD LINEAR Z TABLE
    C ZARV(IK)=I0.**((FLOST(IK)*RQUANT/I0.)
    10 CONTINUE
    IF (.NOT. COMPTIG) GOTO 21
    11 SCALE=8.0/(VZ-Y1)
    IF ((VZ-X1).GT.(VZ-Y1)) SCALE=8.0/(XZ-X1)
    XMIN=SCALE*X1
    XMAX=SCALE*X2
    YMIN=SCALE*Y1
    YMAX=SCALE*Y2
    21 IF (.NOT.PRINT2) GO TO 51
    C PRINT ICODES VALUES.
    C CALL PAGE
    31 WRITE (6,31)
    FORMAT (1M0,8Y,13MCODE FOR MEAN,7X,5MVALJE,5K,12MCODE FOR VAR,7X,5
    1MVALUE/4BX,7MHAND PRX)
    DO 41 I=1,36
    41 XA=(FLOST(I)-B1)/A1
    XB=(FLOST(I)-B2)/A2
    51 WRITE (6,51) ICODES(I),XA
    FORMAT (15X,A1,9X,F9.3,11X,A1,9X,F9.3)
    61 CONTINUE
    IF (.NOT.PRINT3) GO TO 101
    CALL PAGE
    71 WRITE (6,71)
    FORMAT (1M0,8X,13MCODE FOR DBZ,7X,5MVALJE)
    DO 81 I=1,36
    81 XA=(FLOST(I)-B1)/A1
    91 WRITE (6,91) ICODES(I),XA
    FORMAT (15X,A1,9X,F9.3)
    101 CONTINUE
    RETURN
    111 WRITE (6,121)
    121 FORMAT (30H END OF FILE IN NAMELIST INPUT)
    STOP
    END
    EXTRAD 145
    EXTRAD 146
    EXTRAD 147
    EXTRAD 148
    EXTRAD 149
    EXTRAD 150
    EXTRAD 151
    EXTRAD 152
    TEST 62
    EXTRAD 154
    TEST 63
    EXTRAD 168
    EXTRAD 169
    EXTRAD 170
    EXTRAD 171
    EXTRAD 172
    EXTRAD 173
    EXTRAD 174
    EXTRAD 175
    EXTRAD 176
    EXTRAD 177
    EXTRAD 178
    EXTRAD 179
    EXTRAD 180
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    EXTRAD 189
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    EXTRAD 192
    EXTRAD 193
    EXTRAD 194
    EXTRAD 195
    EXTRAD 196
    EXTRAD 197
    EXTRAD 198
    EXTRAD 199
    EXTRAD 200
    EXTRAD 201
    EXTRAD 202
    EXTRAD 203
    
```



```

115 29 CONTINUE
    NP=SHIFT(IN(1) .AND. NIPMSK,-9)
    NS=SHIFT(IN(1) .AND. NSMSK,-7)
    ND=SHIFT(IN(1) .AND. NDMSK,-5)
    NR=SHIFT(IN(1) .AND. NRMSK,-3)
120 C
    C UNPACK PRF AZI,UTH, AND ELEVATION.
    C
    K=SHIFT(IN(2) .AND. KMSK,4)
    N=SHIFT(IN(2) .AND. NMSK,11)
    PRF=IN(2)
    IF (K.EQ.0 .AND. N.EQ.0) GO TO 51
    JA=0
    JB=0
    DO 31 I=1,4
    IREF=2*(I-1)
    IF (IREF .AND. N) .NE. 0) JA=JA+1
    IF (IREF .AND. N) .NE. 0) JB=JB+1
    CONTINUE
    IF (JA.EQ.1 .AND. JB.EQ.1) PRF=194.
    IF (JA.EQ.1 .AND. JB.EQ.3) PRF=794.
    IF (JA.EQ.3 .AND. JB.EQ.1) PRF=1613.
    IF (JA.EQ.3 .AND. JB.EQ.3) PRF=3333.
    GO TO 51
130 51 CONTINUE
    IREF=SHIFT(IN(2) .AND. IZMSK,24)
    AZUTH(IN)=IREF*INTDGC
    IREF=SHIFT(IN(2) .AND. ELMSK,0)
    ELEVAT=IREF*INTDGC
    IF (ELEVAT.GT.180.) ELEVAT=ELEVAT-360.
145 C
    C UNPACK THE DATA.
    C NSF IS SUBFRAME.
    C
    KEMSF*256+1
    KEFPEK
    C UNPACK FIRST DATA WORD.
    C
    MVD(1,K)=SHIFT(IN(3) .AND. MEANML,-24)
    MVD(2,K)=SHIFT(IN(3) .AND. VZMSK1,-12)
    N=3
    C UNPACK REMAINING DATA.
    C
    DO 15 I=1,3
    NEM+1
    DO 163 J=1,5
    IF (I.EQ.1 .AND. (J.EQ.1 .OR. J.EQ.4)) K=K+1
    IF (I.EQ.1 .AND. (J.EQ.2 .OR. J.EQ.4)) N=1
    IF (I.EQ.2 .AND. (J.EQ.2 .OR. J.EQ.5)) K=K+1
    IF (I.EQ.2 .AND. (J.EQ.3 .OR. J.EQ.5)) N=1
    IF (I.EQ.3 .AND. (J.EQ.3)) K=K+1
    IF (I.EQ.3 .AND. (J.EQ.3)) N=1
    MVD(I,K)=SHIFT(IN(3) .AND. MVDMSK(I),INTDGC(I))
    NEM+1
155 C
    C UNPACK REMAINING DATA.
    C
    DO 163 J=1,5
    IF (I.EQ.1 .AND. (J.EQ.1 .OR. J.EQ.4)) K=K+1
    IF (I.EQ.1 .AND. (J.EQ.2 .OR. J.EQ.4)) N=1
    IF (I.EQ.2 .AND. (J.EQ.2 .OR. J.EQ.5)) K=K+1
    IF (I.EQ.2 .AND. (J.EQ.3 .OR. J.EQ.5)) N=1
    IF (I.EQ.3 .AND. (J.EQ.3)) K=K+1
    IF (I.EQ.3 .AND. (J.EQ.3)) N=1
    MVD(I,K)=SHIFT(IN(3) .AND. MVDMSK(I),INTDGC(I))
    NEM+1
170 C
    C UNPACK REMAINING DATA.
    C
    DO 163 J=1,5
    IF (I.EQ.1 .AND. (J.EQ.1 .OR. J.EQ.4)) K=K+1
    IF (I.EQ.1 .AND. (J.EQ.2 .OR. J.EQ.4)) N=1
    IF (I.EQ.2 .AND. (J.EQ.2 .OR. J.EQ.5)) K=K+1
    IF (I.EQ.2 .AND. (J.EQ.3 .OR. J.EQ.5)) N=1
    IF (I.EQ.3 .AND. (J.EQ.3)) K=K+1
    IF (I.EQ.3 .AND. (J.EQ.3)) N=1
    MVD(I,K)=SHIFT(IN(3) .AND. MVDMSK(I),INTDGC(I))
    NEM+1

```

```

53 CONTINUE EXTRAD 367
55 CONTINUE EXTRAD 368
   IF(N .LT. 155) GO TO 61 EXTRAD 369
   C ..... CLEAN OFF EXTRA BITS. EXTRAD 390
   C ..... EXTRAD 391
   C ..... EXTRAD 392
   C ..... EXTRAD 393
   C ..... EXTRAD 394
   C ..... EXTRAD 395
   C ..... EXTRAD 396
   C ..... EXTRAD 397
   C ..... EXTRAD 398
   C ..... EXTRAD 399
   C ..... EXTRAD 400
   C ..... EXTRAD 401
   C ..... EXTRAD 402
   C ..... EXTRAD 403
   C ..... EXTRAD 404
   C ..... EXTRAD 405
   C ..... EXTRAD 406
   C ..... EXTRAD 407
   C ..... EXTRAD 408
   C ..... EXTRAD 409
   C ..... EXTRAD 410
   C ..... EXTRAD 411
   C ..... EXTRAD 412
   C ..... EXTRAD 413
   C ..... EXTRAD 414
   C ..... EXTRAD 415
   C ..... TEST2 21
   C ..... EXTRAD 417
   C ..... TEST2 22
   C ..... TEST2 23
   C ..... TEST2 24
   C ..... EXTRAD 418
   C ..... EXTRAD 419
   C ..... EXTRAD 420
   C ..... EXTRAD 421
   C ..... EXTRAD 422
   C ..... EXTRAD 423
   C ..... EXTRAD 424
   C ..... EXTRAD 425
   C ..... EXTRAD 426
   C ..... EXTRAD 427
   C ..... EXTRAD 428
   C ..... EXTRAD 429
   C ..... EXTRAD 430
   C ..... EXTRAD 431
   C ..... EXTRAD 432
   C ..... EXTRAD 433
   C ..... EXTRAD 434
   C ..... TEST2 25
   C ..... TEST2 26
   C ..... TEST2 16
   C ..... EXTRAD 435
   C ..... TEST 76
   C ..... EXTRAD 441
   C ..... EXTRAD 442
   C ..... EXTRAD 443

```

```

C FINISHED SCAN EXTRAD 466
230 122 ISCANF=+1 TEST2 27
    GO TO 131 EXTRAD 466
    IEOF=1 EXTRAD 467
111 ISCANF=-1 EXTRAD 468
121 IF INA.LE.10)GO TO 132 EXTRAD 469
131 ISCANF=SCANF TEST1 18
235 ISCANF=0 TEST1 19
    ELEV=ELEV+ELEVAT TEST1 20
    DELTAZ=ABS((AZMUTHINA)-AZMUTHINA-133)*PPD TEST2 26
    CALL COMPZ TEST1 22
    CALL CONTOP TEST1 23
    ISCANF=ISCANF TEST1 24
    ELEVAT=ELEVAT+NA TEST1 25
    CALL CONTRZ TEST 77
132 PERIOD 4 EXTRAD 455
265 PERIOD 9 EXTRAD 456
    IF (COPLOT) WRITE(21)DAY,IM,MM,LEND TEST2 29
    IF (IEOF.EQ.1) GO TO 181 EXTRAD 457
    IF (NA.GE.NUMB) RETURN EXTRAD 458
    GO TO 5 EXTRAD 459
161 WRITE (6,191) EXTRAD 460
    IF (IEOF)ELEV TEST1 61
    IF (IFILE .LT. NUMB*NFIL) GO TO 2 EXTRAD 462
191 FORMAT (19H EOF RECD ON UNIT 1) EXTRAD 463
211 FORMAT (21H PAPITY ERR ON UNIT 1) EXTRAD 464
221 RETURN EXTRAD 465
    END EXTRAD 466

```



```

115 C COMPUTE V EXTRAD 567
C EXTRAD 568
IF(IABS(MVP(1,J)) .LT. VELMIN) V(JP)=0 EXTRAD 569
IF(IABS(MVP(2,J)) .LT. VARMIN) V(JP)=0 EXTRAD 570
IF(V(JP) .LE. 1E-17) GO TO 37 EXTRAD 571
120 V(JP)=IF(INCOMPFL0AT(MVP(1,J))) EXTRAD 572
IF(VL .EQ. -999) VL=VAV EXTRAD 573
IF(V(JP) .LT. VHX) V(JP)=V(JP)-VMD EXTRAD 574
IF(VL-V(JP) .GT. VHX) V(JP)=V(JP)+VMD EXTRAD 575
IF(VBL(JP) .EQ. -999 .OR. NA .EQ. 1) GO TO 37 EXTRAD 576
125 IF(V(JP)-V(JP) .GT. VHX) V(JP)=V(JP)+VMD EXTRAD 577
IF(VBL(JP)-V(JP) .GT. VHX) V(JP)=V(JP)+VMD EXTRAD 578
VAV=VAV + V(JP) EXTRAD 579
VMS=VMS+1 EXTRAD 580
GO TO 35 EXTRAD 581
130 37 IF(VLS .LE. 1) GO TO 33 EXTRAD 582
VAV=VAV/VLS EXTRAD 583
IF( IVA .EQ. 0) VAS =VAV EXTRAD 584
135 IVA =1 EXTRAD 585
VAV=0 EXTRAD 586
35 VL=V(JP) EXTRAD 587
IF(V(JP) .EQ. -999) GO TO 41 EXTRAD 588
IF(MVP(2,J) .LT. 0 .OR. MVP(2,J) .GT. 5) GO TO 4111 TEST1 40
SV(JP)=SV(MVP(2,J)+1) TEST1 41
140 4111 IF(VBL(JP) .EQ. -999 .OR. NA .EQ. 1) GO TO 41 TEST 95
R=SCOR*FLOAT(JP)-.5)*DELTA*(MTP*1) EXTRAD 592
VS(JP)=V(JP)-VBL(JP)/R*1000./DELTA TEST1 42
41 CONTINUE EXTRAD 594
DO 45 JP=3,N EXTRAD 595
145 IF(V(JP)-1) .EQ. -999 .OR. V(JP) .EQ. -999 .OR. V(JP)+1 .EQ. -999) EXTRAD 596
1 GOTO 45 EXTRAD 597
VMEAN=V(JP)+V(JP-1)/2 EXTRAD 598
IF(V(JP)-1) .EQ. -999 .OR. V(JP)+1 .EQ. -999) EXTRAD 599
IF(VMEAN-V(JP) .GT. VHX) V(JP)=V(JP)+VMD EXTRAD 600
150 45 CONTINUE EXTRAD 601
DO 51 J=1,N EXTRAD 602
51 VBL(J)=V(J) EXTRAD 603
IF(FLAG .EQ. 0 .OR. VHX .GT. 70) RETURN TEST1 43
WRITE(6,300)M,N,(M(J),V(LJ),VS(LJ),SV(LJ),J=N,N) EXTRAD 605
155 300 FORMATTY,214,7/(IX,2015/7) EXTRAD 606
RETURN EXTRAD 607
END EXTRAD 608

```



```

115 ICVNT(J)=0
    KOD(J)=0
    DO 52 K=I,MIDF
      IDSLOT(K,J)=0
    52 CONTINUE
128 KRID=1
    81 CONTINUE
    C
125 DO 71 K=I,IEMAX
    DO 71 J=1,MZH
      DO 71 L=I,MZH
        DO 81 K=I,IEMAX
          DO 81 J=1,MZH
            DO 81 L=I,MZH
              VI(J,L,K)=0.0
            DO 91 K=I,IEMAX
              DO 91 J=1,MFC
                DO 91 L=I,MFB
                  CI(L,K,J)=0.0
                DO 101 K=I,IEMAX
                  DI(K)=0.0
                IOWC(K)=0
                IOWC(K)=0
                IOWC(K)=0
            101 CONTINUE
          DO 102 J=1,MJAX
            IPANG(J)=0
          IPANG(J)=0
        102 CONTINUE
      IPANG(J)=0
    102 CONTINUE
    101 CONTINUE
    IP=0
    IPB=0
    IPB=0
    IPB=0
    IPB=0
    C
    C
    C
    FIMO EVENTS
135 DO 281 I=IMN,NCL
    DO 281 K=I,MFC
      IF (MI(I)-GT.TL(K)) GO TO 131
      GO TO 281
    131 IF (MI(I)-LE.TL(K)) GO TO 141
      GO TO 131
    141 ICVNT(K)=ICVNT(K)+1
      IF (ICVNT(K)-LE.IEMAX) GO TO 141
      WRITE(6,1412)IEMAX,K
    1412 FORMAT('X',EVENT,COUNTER EXCEEDED MAX VALUE, IEMAX='',16,5X,
      *'(K=,14)
    ICVNT(K)=IEMAX
    1411 IEVENT=ICVNT(K)
      IF (K.EQ.1) IE=IEVENT
    1411 IEVENT,K)=I-1
      IC(I,IEVENT,K)=I-1
      IC(I,IEVENT,K)=I-1

```

```

C
C TALLY ATTRIBUTES.
C
175 R=SCON*(FLOAT(I-1)-.5)*SELTH(M(NTP+1)
INDEX(I)-CL(I)*I)
IF (INDX.GT.61) INDX=61
IF (INDX.LE.0) INDX=1
NR=P*ZARY(INDX)
EVENT=ICWNT(K)
C(I).EVENT.K)=C(I).EVENT.K)+R
C(I).EVENT.K)=C(I).EVENT.K)+NR
C(I).EVENT.K)=C(I).EVENT.K)+NR
IF (K.NE.1) GO TO 231
185 C
C PEAK DETECTION, LOCATE AND COUNT PEAKS.
C
C
161 IF (M(I)-M(I-1)) I71,I74,I51
IPB=I-1
GO TO 181
171 IF (IPB.EQ.0) GO TO 191
IP=IP+1
IF (IP.LE.JMAX) GO TO 1711
WRITE(I,I71,I74,I51) IP,EVENT
GO TO 181
174 IPRNG(IP)=(IP*IP)/2
IPB=0
181 CONTINUE
IF (M(I).EQ.-999) GO TO 191
IF (M(I)-M(I-1).EQ.-999) GO TO 201
IF (IABS(M(I))-IABS(M(I-1))) I91,I11,201
IF (IPB.EQ.0) GO TO 211
IPV=IPV+1
IF (IPV.LE.JMAX) GO TO 1912
WRITE(I,I91,I11) IPV,EVENT
1913 FORMAT(I91,'NUMBER OF PEAKS EXCEEDS ARRAY SIZE',Z16)
EX1=29
GO TO 211
1912 IPRNG(IPV)=(IP*IPV)/2
IPB=0
GO TO 211
201 IPB=I-1
211 CONTINUE
IF (M(I).EQ.-999) GO TO 1911
IF (M(I-1).EQ.-999) GO TO 2011
IF (IABS(M(I))-IABS(M(I-1))) I911,I111,2011
IF (IPB.EQ.0) GO TO 2111
IP5=IP5+1
IF (IP5.LE.JMAX) GO TO 1914
WRITE(I,I911,I111) IP5,EVENT
GO TO 2111
1914 IPRNG(IP5)=(IP*IP5)/2
IP5=0
GO TO 2111
2011 IPB=I-1
2111 CONTINUE
IF (I71*I74*I51*I91*I11*I911*I111) I51
I51=EVENT
IF (I71.IE.0.OR.I91.GT.NZ4) GO TO 221

```

```

230 MZ(I,IM,IEI)=Z(I,IM,IEI)*R
    MZ(I,IM,IEI)=MZ(I,IM,IEI)+R
    IF (M(I)-I)*I*Q*SQ(I)*I*TS(I) GO TO 221
    IF (M(I)-I)*I*Q*SQ(I)*I*EQ*SQ(I) GO TO 221
235 MZ(I,IM,IEI)=MZ(I,IM,IEI)+R
    MZ(I,IM,IEI)=MZ(I,IM,IEI)+R
    IF (M(I)-I)*I*Q*SQ(I)*I*EQ*SQ(I) GO TO 231
    RAIN=OBZARY(INOX)
    MZ(I,IM,IEI)=MZ(I,IM,IEI)+R
240 MZ(I,IM,IEI)=MZ(I,IM,IEI)+R
    GO TO 241
241 DO 271 KL=K,MFC
    IF (M(I)-I)*I*Q*SQ(I)*I*EQ*SQ(I) GO TO 261
    IEVENT=ICVNT(KL)
265 C
    C
    C KEEP COUNT OF PEAKS WITH EVENT.
    C
    IF (M(I)-I)*I*Q*SQ(I)*I*EQ*SQ(I) GO TO 271
    IF (IPB*EQ.0) GO TO 251
    IP=IP+1
    IPRG(IP)=(I+IPB)/2
    IPB=0
251 IDC(IEVENT)=IP
    IF (IPB*EQ.0) GO TO 261
    IP=IP+1
    IPRG(IP)=(I+IPB)/2
    IPB=0
261 IDVC(IEVENT)=IPV
    IF (IPB*EQ.0) GO TO 2611
    IP=IP+1
    IPSRG(IP)=I+IPB/2
    IPB=0
2611 IDSC(IEVENT)=IPS
    GO TO 271
271 CONTINUE
281 CONTINUE
321 COST=COS(TEMP)
    SINT=SIN(TEMP)
    COSA=COS(TEMP)*R
    COSA=COSA+COSA
    SINA=SIN(TEMP)*R
    SINA=SINA+SINA
    SWACNA=SINA*COSA
275 C
    C PLOT FIXED CONTJRS.
    C
    DO 511 K=1,MFC
    IEVENT=ICVNT(K)
    IEVENT=ICVNT(K)
    IP=IP+K
    IEVENT=1
    IEVENT=1
331 IF (I8(I,IEVENT,K)*EQ.0.AND.(I2,KEVENT,K)*EQ.0) GO TO 601
    IF (I8(I,IEVENT,K)*I*Q*SQ(I)*I*EQ*SQ(I) GO TO 571

```

787 EXTRAD 788
 789 EXTRAD 790
 791 EXTRAD 792
 793 EXTRAD 794
 795 EXTRAD 796
 797 EXTRAD 798
 799 EXTRAD 800
 801 EXTRAD 802
 803 EXTRAD 804
 805 EXTRAD 806
 807 EXTRAD 808
 809 EXTRAD 810
 811 EXTRAD 812
 813 EXTRAD 814
 815 EXTRAD 816
 817 EXTRAD 818
 819 EXTRAD 820
 821 EXTRAD 822
 823 EXTRAD 824
 825 EXTRAD 826
 827 EXTRAD 828
 829 EXTRAD 830
 831 EXTRAD 832
 833 EXTRAD 834
 835 EXTRAD 836
 837 EXTRAD 838
 839 EXTRAD 840
 841 EXTRAD 842
 843 EXTRAD 844
 845 EXTRAD 846
 847 EXTRAD 848
 849 EXTRAD 850
 851 EXTRAD 852
 853 EXTRAD 854
 855 EXTRAD 856
 857 EXTRAD 858
 859 EXTRAD 860
 861 EXTRAD 862
 863 EXTRAD 864
 865 EXTRAD 866
 867 EXTRAD 868
 869 EXTRAD 870
 871 EXTRAD 872
 873 EXTRAD 874
 875 EXTRAD 876
 877 EXTRAD 878
 879 EXTRAD 880
 881 EXTRAD 882
 883 EXTRAD 884
 885 EXTRAD 886
 887 EXTRAD 888
 889 EXTRAD 890
 891 EXTRAD 892
 893 EXTRAD 894
 895 EXTRAD 896
 897 EXTRAD 898
 899 EXTRAD 900
 901 EXTRAD 902
 903 EXTRAD 904
 905 EXTRAD 906
 907 EXTRAD 908
 909 EXTRAD 910
 911 EXTRAD 912
 913 EXTRAD 914
 915 EXTRAD 916
 917 EXTRAD 918
 919 EXTRAD 920
 921 EXTRAD 922
 923 EXTRAD 924
 925 EXTRAD 926
 927 EXTRAD 928
 929 EXTRAD 930
 931 EXTRAD 932
 933 EXTRAD 934
 935 EXTRAD 936
 937 EXTRAD 938
 939 EXTRAD 940
 941 EXTRAD 942
 943 EXTRAD 944
 945 EXTRAD 946
 947 EXTRAD 948
 949 EXTRAD 950
 951 EXTRAD 952
 953 EXTRAD 954
 955 EXTRAD 956
 957 EXTRAD 958
 959 EXTRAD 960
 961 EXTRAD 962
 963 EXTRAD 964
 965 EXTRAD 966
 967 EXTRAD 968
 969 EXTRAD 970
 971 EXTRAD 972
 973 EXTRAD 974
 975 EXTRAD 976
 977 EXTRAD 978
 979 EXTRAD 980
 981 EXTRAD 982
 983 EXTRAD 984
 985 EXTRAD 986
 987 EXTRAD 988
 989 EXTRAD 990
 991 EXTRAD 992
 993 EXTRAD 994
 995 EXTRAD 996
 997 EXTRAD 998
 999 EXTRAD 999

```

C      IF (IB(2),IEVENT,K).LT.I(1,KEVENT,K)) GO TO 471
C      ASSOCIATED
C      LEFT SIDE PEN JP.
290  C      IID=IB(IMP,IEVENT,K)
      IF (IID.NE.0) GO TO 3311
3312 GO TO 471
3311 IC(INPA,KEVENT,K)=IID
      IF (.NOT.COPLOT) GO TO 341
      X=FLUXX(I,IEVENT,K)*I.0
      R=SCONC*X
      Y=SCALE*(R*SIN44.8)
      Z=SCALE*(R*COS44.0)
300  C      WRITE(21X,Y,IPU
C      LEFT SIDE PEN JOHN.
C
C      X=FLUXX(I,IEVENT,K)*I.0
R=SCONC*X
Y=SCALE*(R*SIN44.8)
Z=SCALE*(R*COS44.0)
WRITE(21X,Y,IPU
341 IF (ISCANP.NE.0) GO TO 3311
310  ATR(1,IID,K)=ATR(I,IID,K)+DELTAZ*CI(1,KEVENT,K)
      ATR(2,IID,K)=ATR(2,IID,K)+DELTAZ*CI(2,KEVENT,K)
      ATR(3,IID,K)=ATR(3,IID,K)+SINA*DELTAZ*CI(3,KEVENT,K)
      ATR(4,IID,K)=ATR(4,IID,K)+COSA*DELTAZ*CI(3,KEVENT,K)
      IE(1,3,KEVENT,K)
      IID=IC(IMP,IE,1)
315  IF (ATR(I,1,0).NE.0) GO TO 310
      IF (IC(1,KEVENT,K).LT.IM4.OR.IC(2,KEVENT,K).GE.IM4)
      XATRIAT(I,0,K)=ABSTATR(IAT,IID,K))
      IF (K.NE.1) GO TO 381
320  DO 361 I=1,NZM
      IF (HZ(2,IM,KEVENT).LE.0) GO TO 361
      IF (W(3,IM,KEVENT).LE.0) GO TO 351
      ZH(1,IM,MNE)=ZH(1,IM,MNE)+VI(1,IM,KEVENT)
      ZH(2,IM,MNE)=ZH(2,IM,MNE)+VI(2,IM,KEVENT)
      ZH(3,IM,MNE)=ZH(3,IM,MNE)+SINA*VI(1,IM,KEVENT)
      ZH(4,IM,MNE)=ZH(4,IM,MNE)+COSA*VI(1,IM,KEVENT)
      ZH(5,IM,MNE)=ZH(5,IM,MNE)+SINA2*VI(3,IM,KEVENT)
      ZH(6,IM,MNE)=ZH(6,IM,MNE)+COSK2*VI(3,IM,KEVENT)
      ZH(7,IM,MNE)=ZH(7,IM,MNE)+SNACNA*VI(3,IM,KEVENT)
      ZH(8,IM,MNE)=ZH(8,IM,MNE)+SINA*VI(3,IM,KEVENT)
      ZH(9,IM,MNE)=ZH(9,IM,MNE)+COSA*VI(3,IM,KEVENT)
      ZH(10,IM,MNE)=ZH(10,IM,MNE)+VI(3,IM,KEVENT)
      ZH(11,IM,MNE)=ZH(11,IM,MNE)+HZ(1,IM,KEVENT)*DELTAZ
      ZH(12,IM,MNE)=ZH(12,IM,MNE)+HZ(2,IM,KEVENT)*DELTAZ
335  CONTINUE
      DS(I,0)=DS(I,0)+DS(KEVENT)*DELTAZ
361 IF (IEVENT.GE.JEM) GO TO 441
C      IF (IB(1),IEVENT+1,K).GT.IC(2,KEVENT,K)) GO TO 441
C      DRAW DOWN TO PRESENT AZMUTH.
C
C      IF (.NOT.COPLOT) GO TO 6003

```

EXTRAD 849
EXTRAD 850
EXTRAD 851
EXTRAD 852
EXTRAD 853
EXTRAD 854
TEST2 49
TEST2 50
TEST2 51
TEST 155
EXTRAD 856
TEST 156
EXTRAD 858
EXTRAD 859
EXTRAD 861
EXTRAD 862
EXTRAD 863
EXTRAD 864
EXTRAD 865
TEST 157
EXTRAD 867
EXTRAD 868
EXTRAD 870
TEST2 52
TEST2 53
EXTRAD 872
EXTRAD 873
EXTRAD 874
EXTRAD 875
EXTRAD 876
EXTRAD 881
TEST2 54
TEST2 55
TEST2 56
EXTRAD 889
EXTRAD 886
EXTRAD 887
EXTRAD 888
EXTRAD 889
EXTRAD 890
EXTRAD 891
EXTRAD 892
EXTRAD 893
EXTRAD 894
EXTRAD 895
EXTRAD 896
EXTRAD 897
EXTRAD 898
EXTRAD 899
EXTRAD 900
EXTRAD 901
TEST1 58
TEST1 59
EXTRAD 905
EXTRAD 906
EXTRAD 907
TEST 158


```

400 IF (IATF(J,NUMP),EQ,RKNIDU)YATP(J,NUMP)=RKNIDY TEST 162
    413 CONTINUE EXTRAD 957
    IF (IACV(J),EQ,0)GO TO 414 EXTRAD 960
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST 75
    416 CONTINUE EXTRAD 962
    IF (IACV(J),EQ,0)GO TO 413 TEST1 76
    IF (IATF(J,NUMP),EQ,RKNIDU)SATF(J,NUMP)=RKNIDY TEST1 77
    414 DO 415 J=1,NIC TEST1 78
    415 DO 415 J=1,NIC TEST1 79
    IF (IACV(J),EQ,0)GO TO 416 TEST1 80
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST 166
    417 CONTINUE TEST 167
    EXTRAD 966 TEST 168
    418 CONTINUE TEST 169
    EXTRAD 970 TEST 170
    419 CONTINUE TEST 171
    IF (IACV(J),EQ,0)GO TO 416 TEST 172
    IF (IATF(J,NUMP),EQ,RKNIDU)SATF(J,NUMP)=RKNIDY TEST 173
    420 CONTINUE TEST 174
    IF (IACV(J),EQ,0)GO TO 416 TEST1 81
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST1 82
    421 CONTINUE TEST1 83
    IF (IACV(J),EQ,0)GO TO 416 TEST2 64
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST2 65
    422 CONTINUE TEST2 66
    IF (IACV(J),EQ,0)GO TO 416 TEST2 67
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST2 68
    423 CONTINUE TEST1 86
    424 CONTINUE EXTRAD 971
    IF (IACV(J),EQ,0)GO TO 416 EXTRAD 972
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY EXI 42
    425 CONTINUE EXTRAD 973
    IF (IACV(J),EQ,0)GO TO 416 TEST2 69
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST2 70
    426 CONTINUE TEST2 71
    IF (IACV(J),EQ,0)GO TO 416 TEST2 72
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST2 73
    427 CONTINUE TEST2 74
    IF (IACV(J),EQ,0)GO TO 416 TEST2 75
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST1 87
    428 CONTINUE TEST1 88
    IF (IACV(J),EQ,0)GO TO 416 EXTRAD 976
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY EXTRAD 977
    429 CONTINUE EXTRAD 978
    IF (IACV(J),EQ,0)GO TO 416 TEST 172
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST 173
    430 CONTINUE EXTRAD 979
    IF (IACV(J),EQ,0)GO TO 416 TEST 173
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY EXTRAD 981
    431 CONTINUE EXTRAD 982
    IF (IACV(J),EQ,0)GO TO 416 EXTRAD 984
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY EXTRAD 985
    432 CONTINUE TEST1 89
    IF (IACV(J),EQ,0)GO TO 416 EXTRAD 987
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY EXTRAD 988
    433 CONTINUE EXTRAD 990
    IF (IACV(J),EQ,0)GO TO 416 EXTRAD 998
    IF (IATK(J,NUMP),EQ,RKNIDU)YATK(J,NUMP)=RKNIDY TEST 175
    6001 KEVENT=KEVENT+1
    
```


515	C	STRAIGHT LINE IN IC.	EXTRAD 1059
	C		EXTRAD 1060
521	IF (IC(I,KEVENT,K).EQ.0) 50 TO 562		EXTRAD 1061
	DO 522 IIO=1,NIOF		TEST 165
	IF (IIO.SLOT(IIO,K).NE.0) 63 TO 5522		EXTRAD 1064
	IIO=IIC		TEST 166
520	IC(NPA,KEVENT,K)=IIO		TEST 187
	IF (K.NE.1) GO TO 5521		EXTRAD 1065
	IIO=SLOT(IIO,K)=KNIO		EXTRAD 1066
	KNIO=KNIO+1		EXTRAD 1067
521	IE=IC(I,KEVENT,K)		TEST 188
525	IIO=IC(NPA,IE,I,1)		TEST1 104
	IIO=SLOT(IIO,K)=IIO.SLOT(IIO,I,1)		TEST 190
	GO TO 5523		TEST1 105
	5522 CONTINUE		EXTRAD 1072
530	C** NOTE	WHEN ALL IIO'S ARE USED,	EXTRAD 1073
	C** IC(NIO,K) WILL BURDEN ALL OTHER CELLS		EXTRAD 1074
	IF (K.NE.1) GO TO 5524		TEST 191
	KNIO=KNIO+1		TEST1 106
535	IIO=SLOT(IIO,K)=KNIO		TEST2 76
	IIO=IIC		TEST2 79
	IERR=4		TEST2 80
5523	KOO(K)=MAX(KOO(K),IIO)		TEST2 81
	IIO=IIC		EXTRAD 1077
540	IIO=IIC		TEST2 82
	IF (IIO.NE.0) 50 TO 527		TEST2 83
	IF (IIO.NE.0) 50 TO 527		TEST2 84
	IF (IIO.NE.0) 50 TO 527		TEST 193
	IF (IIO.NE.0) 50 TO 527		TEST 194
545	X=SCALE*(R*SINA+4.0)		EXTRAD 1084
	Y=SCALE*(R*COSSA+4.0)		EXTRAD 1085
	WRITE(2),Y,IPU		EXTRAD 1087
	X=FLOOR(X/10.0)		EXTRAD 1088
	IF (X.NE.0) 50 TO 551		TEST 195
550	X=SCALE*(R*SINA+4.0)		EXTRAD 1090
	Y=SCALE*(R*COSSA+4.0)		EXTRAD 1091
	WRITE(2),Y,IPU		EXTRAD 1093
527	IF (IIO.NE.0) 50 TO 551		TEST2 66
	ATR(1,IIO,K)=DELTAZ*CI(I,KEVENT,K)+ATR(1,IIO,K)		TEST2 67
	ATR(2,IIO,K)=DELTAZ*CI(2,KEVENT,K)+ATR(2,IIO,K)		TEST2 68
555	ATR(3,IIO,K)=SINA*DELTAZ*CI(3,KEVENT,K)+ATR(3,IIO,K)		TEST2 69
	ATR(4,IIO,K)=COSA*DELTAZ*CI(4,KEVENT,K)+ATR(4,IIO,K)		EXTRAD 1102
531	IE=IC(I,KEVENT,K)		EXTRAD 1103
	IIO=IC(NPA,IE,I,1)		EXTRAD 1104
	ATP(IAT,IIO,K)=IIO.SLOT(IIO,I,1)		EXTRAD 1105
560	IF (K.NE.0) ATP(IAT,IIO,K)=ABS(ATP(IAT,IIO,K))		TEST2 90
	IF (K.NE.0) ATP(IAT,IIO,K)=ABS(ATP(IAT,IIO,K))		EXTRAD 1106
	IF (K.NE.0) ATP(IAT,IIO,K)=ABS(ATP(IAT,IIO,K))		EXTRAD 1109
565	IF (K.NE.0) ATP(IAT,IIO,K)=ABS(ATP(IAT,IIO,K))		EXTRAD 1110
	IF (K.NE.0) ATP(IAT,IIO,K)=ABS(ATP(IAT,IIO,K))		EXTRAD 1111
	ZH(1,I,PA,NNE)=VI(I,I,4,KEVENT)		EXTRAD 1112
	ZH(2,I,PA,NNE)=VI(2,I,4,KEVENT)		EXTRAD 1113
	ZH(3,I,PA,NNE)=VI(3,I,4,KEVENT)		EXTRAD 1114
570	ZH(4,I,PA,NNE)=VI(4,I,4,KEVENT)		EXTRAD 1115

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ZM15,IH,NNEI=SINA*VI(3,IH,KEVENT)
ZM16,IH,NNEI=COSA*VI(3,IH,KEVENT)
ZM17,IH,NNEI=SINCA*VI(3,IH,KEVENT)
ZM18,IH,NNEI=SINCA*VI(3,IH,KEVENT)
ZM19,IH,NNEI=COSA*VI(3,IH,KEVENT)
ZM20,IH,NNEI=COSA*VI(3,IH,KEVENT)
575 ZM10,IH,NNEI=VI(3,IH,KEVENT)
541 ZM11,IH,NNEI=HZ(1,IH,KEVENT)*DELTAZ
ZM12,IH,NNEI=HZ(2,IH,KEVENT)*DELTAZ
580 CONTINUE
551 OSI(1001)=OI(KEVENT)*DELTAZ
551 CONTINUE
561 KEVENT=KEVENT+1
562 IF(KEVENT.GT.IEM.AND.IEVEN.GT.JEM) GO TO 601
IF(KEVENT.GT.IEM) GO TO 481
IF(IEVEN.GT.JEM) GO TO 521
GO TO 331
601 CONTINUE
611 CONTINUE
IF(ISCANF.NE.0) GO TO 871
IF(.NOT.CONTRZ) GO TO 800
8003 IF(.NOT.CONTRZ) GO TO 8000
CALL PEAKO(LDV,TLID,ISUP,NCEL,YATR,NUMAX,IACCT,IDG,IP1B,IB,
+ IPBNT,IPRNG,4R,NMR,IPB1,IPB2,IPB3)
8000 IF(.NOT.CONTRZ) GO TO 8001
CALL PEAKO(VS,LTV,0,2,0J,NVDEL,VATR,NVMAX,IACV,IP1VB,IVB,
+ IPBNT,IPVRN,5R,NRV,IPV1,IPV2,IPV3)
8001 IF(.NOT.CONTRZ) GO TO 800
CALL PEAKO(TSV,LSV,0,0,US,NSEL,SATR,NSMAX,IACS,IUSC,IP1SB,ISB,
+ IPBSNF,IPSRNS,1S,NMS,IPS1,IPS2,IPS3)
C STORE PRESENT PARAMETERS IN PREVIOUS PARAMETERS.
C
600 CONTINUE
IF(ISCANF.NE.0) GO TO 8004
DO 801 K=1,NFC
JEM=IBVNT(K)
IEM=IC4NT(K)
IBVNT(K)=ICWNT(K)
ICWNT(K)=0
610 IF(JEM.EQ.0) GO TO 803
IEM1=MAX(1,IEM)
DO 802 I=1,IEM1
IF(18(NPA,J,KI.EQ.IC1NPA,I,K)IGO TO 802
I10=18(NPA,J,K)
IF(I10.LE.0) GO TO 802
IF(18(K1,I10,K7)GE.18(K7) GO TO 802
ABAR=ATR(I10,K1)*SCON*DELTA(NIP+1)
IDSL0T(I10,K)=0
DO 8005 I=1,I1AT
DO 8005 I=1,I1AT
8005 ATR(I10,K)=0.0
802 CONTINUE
803 DO 801 IEM=I,IERAK
DO 801 IEM=I,IERAK
IBVNT(K)=ICWNT(K)
ICWNT(K)=0
801 CONTINUE
FREE UP ATTR SPACE IF POSSIBLE
C

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815 IF(NA,NE.1) GO TO 886
    DO 895 K=1,NFC
    YERI=RYR(I,YBNT(K))
    DO 896 J=1,IEM1
    YDST(RNPA,J,K)
    IF(IID.LE.8) GO TO 865
    CTR(IID,K)=ATR(IAT,IID,K)
    895 CONTINUE
    886 RETURN
C
C
817 ENTRY CONTRZ
    IF(IISCAF,NE.1) IISCAF=-1
    GO TO 8003
888* IF(IISCAF.GT.8) GO TO 831
    DO 821 K=1,NFC
    IF(IE.LE.8) GO TO 821
    IDDS=(RINPA,IE,K)
    822 ATR(IAT,100,K)=-ABS(ATR(IAT,100,K))
    DO 823 J=1,IEM1
    DO 824 I=1,IE
    IF(ABS(CTR(I,K)).NE.ABS(CTR(IAT,J,K))) GO TO 823
    ATR(IAT,J,K)=-ABS(ATR(IAT,J,K))
    823 CONTINUE
    821 CONTINUE
C
855 PLOT FINAL RADIALS.
    IF(L.MOI.CO.PLOT) GO TO 871
    Y=SCALE*%
    WRITE(2)X,Y,IPO
    SCRA=SCONC/ICOMP
    P=SCRA*TRINPC*%*-757
    X=SCALE*(R+SIN(AZMUTH(I)*%P))%*8.0
    Y=SCALE*(R+COS(AZMUTH(I)*%P))%*8.0
    WRITE(2)X,Y,IPO
    X=SCALE*(R+SIN(AZMUTH(N4)*%P))%*8.0
    Y=SCALE*(R+COS(AZMUTH(N4)*%P))%*8.0
    WRITE(2)X,Y,IPO
    X=SCALE*%
    Y=X
    WRITE(2)X,Y,IPO
    GO TO 871
831 TEMP=AZMUTH(N4)*%PO
    DELYR=ZNS(CKYR(MUTH(I)*%P))-TEMP
    AZNOM=AZMUTH(1)
    DO 861 I=2,NCL
    W(I)=W(I)+1
    8611 V5(I)=V5(I)+X
    GO TO 81
871 DELR=SCONC*CELLWTH(MT*%1)
    DAPFL=DELR*OHZ*%1.E-3
    IF(ITER.EQ.8) GO TO 8711
    IF(ITER.EQ.1) PRINT 8712,5*HCELL,5*HPEAKO
    
```

TEST2 114
TEST2 115
TEST2 116
TEST2 117
TEST2 118
TEST2 119
TEST2 120
TEST2 121
TEST2 122
EXTRAD 1174
EXTRAD 1175
EXTRAD 1176
EXTRAD 1177
TEST2 123
TEST2 124
TEST2 125
EXTRAD 1179
EXTRAD 1180
TEST 216
TEST 217
TEST2 126
TEST2 127
TEST2 128
TEST2 129
TEST2 130
TEST2 131
TEST2 132
TEST 218
EXTRAD 1184
TEST 211
TEST2 133
TEST2 134
EXTRAD 1188
TEST1 117
TEST 213
EXTRAD 1192
EXTRAD 1193
EXTRAD 1195
EXTRAD 1196
EXTRAD 1197
EXTRAD 1199
TEST2 135
TEST2 136
EXTRAD 1203
EXTRAD 1204
TEST2 137
TEST2 138
EXTRAD 1215
EXTRAD 1218
EXTRAD 1219
TEST 214
EXTRAD 1220
TEST2 139
EXTRAD 1222
TEST1 118
EXTRAD 1223
EXTRAD 1224

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585 IF IERR .EQ. 2) PRINT 871Z, 871ADR, 871UPK
    IF IERR .EQ. 3) PRINT 871Z, 871ADR, 871SHPK
    IF IERR .EQ. 4) PRINT 871Z, 871ADR, 871CONTR
    871Z  FORMAT(2X, 'ARRAY OVERFLOW', 2X, 'VARIABLE', 2X, 'A5.2X, 'IN', 2X, 'A5)
C
599 C      WRITE FIXED CONTOR ATTRIBUTES
C
    8711 IF (KNTD.LE.1) GO TO 1413
    CALL PAGE
    WRITE(6,872)
595 872  FORMAT(2X, 'FIXED CONTOR ATTRIBUTES')
    WRITE(6,712)
    712  FORMAT(7, 28X, 7MAVERAGE, 7X, 5HLOCATION, 13X, 4HAREA, 8X, 5HTOTAL, 3X,
    17H AVERAGE, 6X, 5HFIXED, 7X, 9HTRESHOLD, 5X, 4HAREA, 2X, 12H REFLECTIVITY
    2, 1X, 4H EAST, 2X, 5H NORTH, 5X, 5H RANGE, 1X, 10H RESOLUTION, 2X, 6H PRECIP, 4X,
    3H PRECIP, 5X, 5H CONTOR, 7X, 2X, 2H I, 5X, 5H CONTOR, 7X, 2X, 2H I, 5X, 5H CONTOR,
    45X, 4H I, 3X, 4H (KMI, 7X, 4H (KMI, 1X, 8HELEMENTS, 2X, 3H IONS/MK), 1X,
    57H (M/R), 4X, 3H REFERENCE)
    IF (.NOT.VOLTAP) GO TO 6819
705 ITYPE=0
    WRITE (3) ITYPE, ITYPE
    WRITE (3) ITYPE, ITYPE
    K,NEL
    WRITE(3) ELEVAT, LON, I, HO, J, MIN, ISE, ELEVAT, AZMUT(1), AZMUT(MIN)
    700 17H AVERAGE, 6X, 5HFIXED, 7X, 9HTRESHOLD, 5X, 4HAREA, 2X, 12H REFLECTIVITY
    2, 1X, 4H EAST, 2X, 5H NORTH, 5X, 5H RANGE, 1X, 10H RESOLUTION, 2X, 6H PRECIP, 4X,
    3H PRECIP, 5X, 5H CONTOR, 7X, 2X, 2H I, 5X, 5H CONTOR, 7X, 2X, 2H I, 5X, 5H CONTOR,
    45X, 4H I, 3X, 4H (KMI, 7X, 4H (KMI, 1X, 8HELEMENTS, 2X, 3H IONS/MK), 1X,
    57H (M/R), 4X, 3H REFERENCE)
    IF (.NOT.VOLTAP) GO TO 6819
    ITYPE=0
    WRITE (3) ITYPE, ITYPE
    WRITE (3) ITYPE, ITYPE
    K,NEL
    WRITE(3) ELEVAT, LON, I, HO, J, MIN, ISE, ELEVAT, AZMUT(1), AZMUT(MIN)
710 5819 DO 931 J=1, NFO
    C CALCULATE NUMBER OF CONTOURS FOR LOWEST LEVEL
    NICKR=0
    IF (.NOT.VOLTAP) GO TO 9333
    ITYPE=
    ICOUNT=0
    DO 9311 J=1, NFO
    IF (IGSLGT(J,K).NE.0) ICOUNT=ICOUNT+1
    9311 CONTINUE
    IF (VOL_TAP) WRITE (3) ITYPE, ICOUNT
    725 CONTINUE
720 DO 9312 J=1, NFO
    IF (DLSLOT(J,K).EQ.0) GO TO 9312
    KNIDG=ATR(IAT, J, K)
    IBI=J
    IF (ATR(I, J, K).LT. TATPMN) GO TO 9312
    88R=DELTA*ATR(I, J, K)
    ZBAR=ATR(I, J, K)*DELTA/ZBAR
    YBAR=ATR(I, J, K)*DELTA/YBAR/ZBAR
    YBAR=ATR(I, J, K)*DELTA/YBAR/ZBAR
    XBAR=ATR(I, J, K)*DELTA**2
    XBAR=XBAR/1000**2
    XBAR=XBAR/1000.
    YBAR=YBAR/1000.
    ZBAR=5*PT(XBAR*YBAR*ZBAR)
    PCELLS=ZBAR/ZBAR*DELTA
    ZBAR=10.*ALOG(10/ZBAR)
    735 IF (I=1) 9313, 9313, 9315
    9313 IF (NBL-I) 9314, 9314, 9315
    9314 TPREC=DELTA*DELTA
    APPREC=TPREC/ZBAR*1000**2)
    TPREC=TPREC/ZBAR
    WRITE(6,716) I01, TL(K), ZBAR, ZBAR, YBAR, XBAR, PCELLS, TPREC,
    740 XAPREC, KNIDG

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715 FORMAT (IX,13,5X,12,4X,F9.2,4X,F5.1,4X,F6.1,1X,F6.1,2F10.1,
      1X,F6.2,2X,F6.2,4X,16)
      IF (VOL YAP) WRITE(3) K, YL(X), ABAR, ZBAR, XBAR, YBAR, XPREC, YPREC, KNIDQ
      GO TO 9316
745
9315 WRITE(6,722) IDI, YL(X), XBAR, ZBAR, XBAR, YBAR, XCELLS, KNIDQ
720 FORMAT (IX,13,5X,12,4X,F9.2,4X,F5.1,4X,F6.1,1X,F6.1,2F10.1,21X,16)
      IF (VOL YAP) WRITE(3) K, YL(X), ABAR, ZBAR, XBAR, YBAR, XPREC, YPREC, KNIDQ
9315 IF (.NOT. COPLDT) GO TO 9312
      XBAR = XBAR / FRNG * 4.
      YBAR = YBAR / FRNG * 4.
      IPUSIVDPIDITK = IPUSIVDP
      WRITE(2) XBAR, YBAR, IPU
9312 CONTINUE
931 CONTINUE
C
C
C
      WRITE WIND DATA
C
      CALL PAGE
      WRITE(6,711)
711 FORMAT (10H WIND DATA)
      WRITE(6,945) IDAY, IMHOUR, IMIN, ISEC, ELEVAT, AZMUTH(IM), AZMUTH(MA)
      M = NNE
      WRITE(6,713)
      DO 921 I = 1, NZH
      IF (ZRNZP = 1) M = EQ
      B1GO TO 921
      T2 = DEL * 2 * ZM(I), I, M)
      AVZ = ZH(I), I, M) / ZH(I), I, M)
      IF (AVZ .GT. 0.7) AVZ = 10. * AL(5) / 10 (AVZ)
      C
      COMPUTE AVG WIND SPEED AND DIR.
      DEL = ZH(I), I, M) * ZH(I), I, M) - ZH(I), I, M) * ZH(I), I, M)
      IF (DEL .EQ. 0.) GO TO 921
      VN = (ZH(I), I, M) * ZH(I), I, M) - ZH(I), I, M) * ZH(I), I, M) / DEL / QUANT
      VE = (ZH(I), I, M) * ZH(I), I, M) - ZH(I), I, M) * ZH(I), I, M) / DEL / QUANT
      VE = (ZM(I), I, M) * VN * 2 * ZM(I), I, M) + VE * 2 * ZM(I), I, M) * 2. * VN * VE * ZH(I), I, M)
      I = 2 * VN * ZH(I), I, M) - 2 * VE * ZH(I), I, M) / ZH(I), I, M) / ZH(I), I, M)
      VE = ZH(I), I, M) / ZH(I), I, M) - (ZM(I), I, M) / ZH(I), I, M) * 2
      VC = ZH(I), I, M) / ZH(I), I, M) - (ZM(I), I, M) / ZH(I), I, M) * 2
713 FORMAT (10H 10X, 7HAVERAGE, 5X, 5HTOTAL, 5X, 7HAVERAGE, 1X, 7HAVERAGE, 12X,
      XSWVELOCITY, 1X, 6HEIGHT, 1X, 12HREFLECTIVITY, 1X, 12HREFLECTIVITY, 4X,
      X1MU, 7X, 14V, 5X, 8HVARIANC, 14X, 3HDEL /
      X
      2X, 2H1KRT, 5X, 2H1DBZ, 15X, 11H105Z, 4X, 21X, 7H1M/SEC, 1X,
      X7H1M/SEC, 1X, 11H1M/SEC, 4X, 21)
      T2 = T2 / DBE15
      WRITE(6,717) I, AVZ, T2, VE, VN, VE, DEL
717 FORMAT (15, 6X, F5.1, 7X, F9.1, 2X, F6.1, 2X, F6.1, 2X, F6.1, 1X, 1X, E15.5)
921 CONTINUE
C
C
      WRITE PEAK CELL ATTRIBUTES
C
      IF (.NOT. CONTRZ) GO TO 6019
      CALL PAGE
      WRITE(6,932)
932 FORMAT (10H * PEAK DETECTED CELL ATTRIBUTES*)
      WRITE(6,945) IDAY, IMHOUR, IMIN, ISEC, ELEVAT, AZMUTH(I), AZMUTH(MA)
      WRITE(6,716)
714 FORMAT (1, 60X, 7HAVERAGE, 3X, 7HAVERAGE, 3X, 7HAVERAGE, 3X, 7HAVERAGE, 5X,
      X4HMEAN, /, 32X,

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5*ELEMENTS*,IX*(M/S)*.5X*.8H(M/S/KM))
IF (.NOT.VOLTAP) GO TO 6022
IYPE=4
ICOUNT=0
850 C CALCULATE NUMBER OF PEAK VELOCITY CELLS
DO 9943 IX=1,MSCEL
IF (US(IX,1).LE.0.0R.UV(IX,2).EQ.0.1GO TO 9943
ICOUNT=ICOUNT+1
9943 CONTINUE
WRITE (3) IYPE,ICOUNT
865 DO 943 N=1,MSCEL
IF (UV(N,1).LE.0.0R.UV(N,2).EQ.0.1GO TO 943
UF(N,4)=UV(N,4)/UV(N,2)/1.0E03
UF(N,3)=UV(N,3)/UV(N,2)/1.0E03
870 UF(N,2)=UV(N,2)/UV(N,1)/SQJANT
UF(N,5)=UV(N,5)/UV(N,1)/SQJANT
UF(N,6)=UV(N,6)/UV(N,1)/VJANT
UF(N,1)=UV(N,1)*DELZ/1.0E06
PEAR=SQRT(UV(N,3)*UV(N,3)+UV(N,4)*UV(N,4))
RCCELLS=UF(N,1)/(RBAR*DAZE.)
TUV=UF(N,7)
WRITE(6,719) N,UF(N,2),UF(N,3),UF(N,4),RBAR,RCCELLS,
TUVMS,TUVIN,6,TUV
880 IF (VOLTAP) WRITE(3)UF(N,2),UF(N,3),UF(N,4),UF(N,5),UF(N,6),
+TUV
IF (.NOT.COPLT) GO TO 943
XREG=UV(N,3)/RANG+.0
YREG=UV(N,4)/RANG+.0
IPOS=UP*N
885 WRITE(2)XREG,YREG,IPOS
719 FORMAT (IX,I6,ZX,PF,1,3X,FF,1,IX,FF,1,1X,FF,1,3X,FF,1,6F7.1,
+3X,FF,1,5X,FF,1,4X,14)
943 CONTINUE
C
890 C OUTPUT SPREAD CELLS
EX2 111
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EX2 999
EX2 1000

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USIN,3)=USIN,3)/USIN,2)/I,DEU3      TEST 283
USIN,2)=USIN,2)/USIN,1)/SQUANT      TEST 284
915  USIN,1)=USIN,1)/DEL/I,DEU6        TEST 285
      RBAR=SQRT(USIN,3)*USIN,3)+USIN,4)*USIN,4)  TEST1 183
      RCELLS=USIN,1)/RBAR*DEU2EL      TEST1 186
      IUS=USIN,5)                     TEST 286
920  WRITE(72)I,N,USIN,2),JS(N,1),USIN,3),USIN,4),RBAR,RCELLS,IUS  TEST1 185
      FORMAI(1,4),F,1.5X,F6.1,2A,F6.1,1X,F6.1,5X,F7.1,2X,F7.1,5X,I4)  TEST1 186
      IF(PLT)PRINTWRITE(3)USIN,2),USIN,3),USIN,4),USIN,5)  TEST 289
      IF(.NOT.COPLOT)GO TO 944        TEST 290
      XREG=USIN,3)/RANG*4.0          TEST1 187
      YREG=USIN,4)/RANG*4.0          TEST1 188
      IPU=ISSPAN                     TEST1 293
      WRITE(2)XREG, YREG, IPU        TEST 294
944  CONTINUE                         ENZ 180
1413 WRITE(6,950)KNID,NMR,NM,NMS    TEST 295
950  FORMAT(10,10)TOTAL IODS,418J  TEST 296
930  ISCANF=0                         EXTRAD 1354
      IF(PRINT2) CALL PRN2(2)        TEST1 189
      RETURN                         EXTRAD 1398
      END                             EXTRAD 1399

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102=1*(LMB-I)*LW          EXTRAD 1452
IF (NA.NE.-1.OR.ISCANF.NE.0) GO TO 2109  EXI 59
ZERO AREAYS              EXTRAD 1454
                            EXTRAD 1455
                            EXTRAD 1456
                            EXI 60
                            EXI 61
                            EXI 62
                            EXI 63
2108 TATRI(J)=0          TEST 315
2109 NGM=0              EXI 65
DO 2108 I=1,NICP        EXTRAD 1457
IACT(I)=0              EXTRAD 1458
DO 2105 J=1,NUMAX      EXTRAD 1459
TATRI(J)=0            EXTRAD 1460
                            EXTRAD 1461
21  IPCNT(K,I)=0       EXTRAD 1462
DO 22 J=1,IMAX        EXTRAD 1463
IPC1(J)=0             EXTRAD 1464
IPC2(J)=0             EXTRAD 1465
IPC3(J)=0             EXTRAD 1466
                            EXTRAD 1467
                            EXTRAD 1468
                            TESTI 194
                            TESTI 195
                            EXI 66
1044 JEM=IBVNI(1)      EXTRAD 1470
IF IEM.LC.0) GO TO 952  EXTRAD 1471
IF IEM.GT.KR) IEM=KR   EXTRAD 1472
DO 951 I=1,IEM        TESTI 196
I101=IC(MPA,IE,1)     TESTI 197
IF I101.NE.0) GO TO 9510 TESTI 198
WRITE(6,951) I101     TESTI 199
9511 FUPMNTW I101='I101' TESTI 200
GO TO 951             EXTRAD 1472
9510 CONTINUE         TESTI 201
IF INA.EQ.1 .AND. ISCANF.EQ.1) GO TO 940 TESTI 202
IPL=0                 EXTRAD 1474
IF IE.GT.1) IPL=IDC(IE-1) EXTRAD 1475
IPL=IDC(IET)         TESTI 203
IF IPL.EQ.0) OR IPL.EQ.IP) GO TO 951 TESTI 204
IF IPL.EQ.0) IPL=1    EXI 67
IF (IP.GT.JMAX) IP=JMAX EXTRAD 1476
JEM=0                 EXTRAD 1477
JEZ=0                 EXTRAD 1478
                            EXTRAD 1479
                            EXTRAD 1480
                            EXTRAD 1481
                            EXTRAD 1483
                            EXI 68
                            EXTRAD 1484
                            EXTRAD 1485
                            EXTRAD 1486
                            EXTRAD 1487
110 IF (JEM.GT.KR) JEM=KR
DO 31 J=1,JEM         EXTRAD 1489
IF (I101.GE.1) .LT. IC(1,IE,1)) GO TO 31
IF (I101.GE.1) .GT. IC(2,IE,1)) GO TO 41
JEZ=JE                EXTRAD 1488
IF (JEI.EQ.0) JEI=JE  EXTRAD 1489
CONTINUE              EXTRAD 1490
31 CONTINUE           EXTRAD 1491
C                     EXTRAD 1492
C                     FIND THRESHOLDS FOR IE EVENT
C

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115 41 DO 51 J=1,JMXD9 EXTRAD 1493
51 Y(J)=0 EXTRAD 1494
   NTHRES=1 EXI 69
   IF (IP.LT.IPL) GO TO 951 TEST1 205
   DO 71 L=1,PLXP EXTRAD 1495
120 1R1=IPCRNGIL TEST 316
   IF (1R1.LE.U-DR-1R1) GE.NC1) GO TO 951 TEST 317
   IF (1R1.LT.IC(1,IE,1)) GO TO 71 TEST 318
   IF (1R1.GT.IC(2,IE,1)) GO TO 712 TEST 320
   DO 711 K=1,LOB TEST 321
125 1Y=ABS(1Y1Y1)-1R-K*1 EXTRAD 1499
   IF (1Y.LE.0) GO TO 711 TEST 322
   IF (1Y.GT.JMXD8) IT=JMXD8 EXI 71
   IF (1Y1.EQ.0) NTHRES=NTRES+1 EXI 72
   Y(1Y)=1 EXI 73
130 711 CONTINUE TEST 323
71 CONTINUE TEST 324
712 IPSRT=0 TEST 325
   IF (NTHRES.GT.KMAX) IPSRT=NTHRES-KMAX EXI 75
   IPT=1 EXTRAD 1502
135 DO 91 L=1,JMXD8 EXTRAD 1503
   IF (1(L) 91,91,81 EXTRAD 1504
81 TC(CPT,IE)=ESTR-1 EXTRAD 1505
   IPSRT=IPSRT-1 EXI 76
140 IF (IPSRT.GT.0) GO TO 91 EXI 77
   IPT=IPT+1 EXTRAD 1506
91 CONTINUE EXTRAD 1507
   IPT=IPT-1 EXTRAD 1508
145 IF (IPT.GE.JR) IPT=JRK EXI 78
   IPTG(IE)=IPT EXTRAD 1509
   IF (IPT.LE.0) GO TO 951 EXTRAD 1510
C C C EXTRAD 1511
C C C LOOP ON RANGE IN IE EVENT TO FIND CONTOUR EXTRAD 1512
150 18G=1Y1Y1,IE,1Y1 EXTRAD 1513
   IND=IC(2,IE,1)+1 EXTRAD 1514
   DO 161 I=1BGN,IND EXTRAD 1515
C C C EXTRAD 1516
C C C LOOP ON THRESHOLD EXTRAD 1517
155 DO 131 K=1,IPT EXTRAD 1518
   IF (U(1).EQ.-999) GO TO 141 EXTRAD 1519
   IF (ABS(U(1)).GT.YC(K,IE)) GO TO 111 EXTRAD 1520
   GO TO 141 EXTRAD 1521
160 111 IF (U(1)-1).EQ.-999) GO TO 121 EXTRAD 1522
   IF (ABS(U(1)-1)).LE.YC(K,IE)) GO TO 121 EXTRAD 1523
   GO TO 131 EXTRAD 1524
C C C EXTRAD 1525
C C C START RANGE FOR SEGMENT (CONTOUR) EXTRAD 1526
165 121 1PCNT(K,IE)=1PCNT(K,IE)+1 EXTRAD 1527
   IF (1PCNT(K,IE).LE.IHJMK) GO TO 1211 EXTRAD 1528
   WRITE(6,1212)Y,K,IE WRITEL6,1212)Y,K,IE
170 1212 FORMAT(2X,'NUMBER OF SEGMENTS EXCEEDS IMX',3I10) EXTRAD 1529
   1211 1PE=1PCNT(K,IE) EXTRAD 1530
   IREG=I-1 EXI 79
   CALL 1PK(1PE,I,REG,IPE,K,IE,IK,JR) EXI 80
   EXTRAD 1531
   EXTRAD 1532
   EXTRAD 1533

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131 CONTINUE
50 TO 161
175 C END RANGE FOR SEGMENT
181 DO 151 KL=K,IPT
IF (ABS(U(I-1))-LE.FC(L,IE)) GO TO 161
IPE=IPCNT(KL,IE)
IREG=I-1
CALL IPK(IPC2,IREG,IPE,L,IE,IR,IR)
151 CONTINUE
161 CONTINUE
185 C ASSOCIATE CELLS LOOP ON THRESHOLD HIGHEST TO LOWEST
C
900 DO 961 LC=1,IPT
KC=IPT-LC+1
IF (KC.LE.0) GO TO 961
NPC=IPCNT(KC,IE)
IF (NPC.LE.0) GO TO 961
LOOP ON SEGMENTS
DO 931 IPE=1,NPC
IAB=IUPK(IPC2,IPE,KC,IE,IR,IR)+1
IAB=IAB-1
K=KC+1
MPK=0
200 IATHEW=
IF (K.GT.IPT) GO TO 193
IPE=IPCNT(K,IE)
IF (IPE.LE.0) GO TO 193
197 DO 191 L=1,IPE
IF (IUPK(IPC2,L,K,IE,IR,IR).LT.IAB) GO TO 191
NPCEL=IUPK(IPC2,L,K,IE,IR,IR)
IF (NPCEL.EQ.0) GO TO 191
IATH=MAX(IATH,IAT(IAB,NPCEL))
IF (IATH.EQ.IATH) NPCEL=IATH
210 C
C NPCEL IS FOR NEXT HIGHER ENCLOSED THRESHOLD OR C RADIAL
C
231 IF (ABS(IAT(NPCEL,IJ).GT.(TC(KC,IE)+LOB))) GO TO 932
191 CONTINUE
50 TO 193
932 MPK=-NPCEL
50 TO 193
1911 MPK=-(INTD*1)
C
C ASSOCIATE CELLS ON B RADIAL, TOP DOWN
C
193 MPK=0
IF (IATH.EQ.1) GO TO 361
IATH=0
IF (JE2.EQ.0) GO TO 361
DO 261 JE=JEL,JE2
IF (IAB(2,JE,1).LT.IABM) JJ TO 261

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EXTRAD 1534
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EXTRAD 1555
EXTRAD 1556
EX1 83
TEST1 206
EX1 84
EXTRAD 1557
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EXTRAD 1561
EXTRA 1562
EXTRAD 1563
EXTRAD 207
TEST1 208
EXTRAD 1568
EXTRAD 1569
TEST 327
TEST 328
EXTRAD 1572
EXTRAD 1573
EXTRAD 1574
TEST 329
EXTRAD 1576
EXTRAD 1577
EXTRAD 1578
EXTRAD 1579
EX1 85
EXTRAD 1581
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EXTRAD 1584
EXTRAD 1586
EXTRAD 1587
EXTRAD 1594
EXTRAD 1595
TEST1 209

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230 C IF (IB(1,JE,1)-GT,IMD) GO TO 361
C C JE EVENT ON B RADIAL IS ASSOCIATED
C C
271 IPB=IPB(JE)
IF (IPB-LE,0) GO TO 261
DO 251 LB=1,IPB
KB=IPB-LB+1
NPI=IPBNT(KB,JE)
IF (NPI-LE,0) GO TO 231
DO 281 JPE=1,NPI
IF (IUP(KIPB2,JEL,K3,JE,IP,J3),LT,IMBM) GO TO 281
IF (IUP(KIPB1,JPE,K3,JE,IP,J3),GT,IMD) GO TO 231
LPCEL=IUP(KIPB3,JPE,K3,JE,IP,J3)
IF (LPCEL-EG,0) GO TO 281
IF (IC(KC,IE) .LE. T3(KB,JE)) GO TO 282
282 IATM=AMAX1(IATM,IATRI,LPCEL,IPJGO TO 281
MPK=LPCEL
KBP=KB
JBM=JE
281 CONTINUE
291 CONTINUE
251 CONTINUE
IF (MPK-NE,0) GO TO 3661
DO 154 I=IMB,IMD
IF (IMB(I)-EG,-999) GO TO 134
IF (IMB(IMB(I))-GT,IC(KC,IE) IPJGO TO 934
154 CONTINUE
GO TO 361
260 7661 IF (ABS(IATR(MPK,1)) .GT. T3(KC,IE) +LOB) MPK=-MPK
GO TO 361
934 MPK=-I(NIDP+1)
C C HAVE B COMPARE WITHIN RANGE
C C
261 CONTINUE
IF (MPK-EG,0 .AND. NPK-EG,0) GO TO 631
C C
270 C MPK=0 .AND. NPK=J - NO COMPARE
C MPK=0 .AND. NPK-NE,0 - NO B COMPARE
C NPK=0 .AND. MPK-NE,0 - B COMPARE
C C HIGHEST THIS RADIAL
C C
275 IF (MPK-EG,0 .AND. NPK-LE,0) GO TO 931
IF (MPK-NE,0) GO TO 921
C C
C C NO PRIOR RADIA. FOR COMPARISON, INCREMENT NPCEL
C C
381 NPCEL=MPK
IF (NA-EG, 1 .AND. ISCANF .EQ. 1) GO TO 392
IF (NA,EG,0) GO TO 351
DO 352 I=IMB,IMD
IF (IMB(I)-EG,-999) GO TO 352
IF (IMB(I)-GT, IC(KC,IE)) GO TO 931
352 CONTINUE

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357 INDX=TATR(NPCEL,I)-TC(K),IEJ-I TEST 334
391 IF (INDX.GE.LDB.OR.INDX.LE.0)GO TO 366 EXTRAD 1653
392 IN=I*INDX*LM TEST 335
IN=ID*INDX*LM EXTRAD 1657
290 IF (TATR(NPCEL,IN).NE.0)X=VAR.EQ.UIGO TO 392I TEST 336
IF (TATR(NPCEL,IN-LMH).LE.0)GO TO 931 TEST 337
MPC=NPCEL TEST 338
NPCEL=TATR(NPCEL,IN-LMH) TEST 339
295 IF (MPC.EQ.NPCEL)GO TO 931 TEST 340
GO TO 359 EXTRAD 1662
392I CALL IPKTIPOS,NPCEL,TYPE,K,IE,IK,JKI TEST 341
ISP=IMH TEST 214
DO 411 I=1ST,ISP TEST 215
R=SCOND*(FLOAT(I)-.5) TEST 215
RU=R*ABS(FLOAT(U(I))) EXTRAD 1665
TATR(NPCEL,IN+I)=TATR(NPCEL,IN+I)+DAZ*R TEST 344
TATR(NPCEL,IN+2)=TATR(NPCEL,IN+2)+DAZ*R TEST 346
TATR(NPCEL,IN+3)=TATR(NPCEL,IN+3)+DAZ*SZ*R*R*ZJ TEST 347
TATR(NPCEL,IN+4)=TATR(NPCEL,IN+4)+DAZ*SAZ*R*R*ZJ TEST 348
IF (ITY.EQ.0)GO TO 411 EXZ 154
IF (ISV(I).NE.-999) TEST 349
TATR(NPCEL,IN+5)=TATR(NPCEL,IN+5)+URZ*R*SV(I) TEST 350
IF (ITY.GE.2)GO TO 401 TEST 351
IF (ITY.EQ.-999)GO TO 401 EXTRAD 1672
TATR(NPCEL,IN+6)=TATR(NPCEL,IN+6)+DAZ*R*V(I) TEST 216
IF (C=-1)EQ.-999)GO TO 401 EXTRAD 1674
TATR(NPCEL,IN+7)=TATR(NPCEL,IN+7)+DAZ*R*V(I)-V(I-1)) TEST 352
401 IF (VSTI).EQ.-999) GO TO 411 EXTRAD 1676
TATR(NPCEL,IN+6)=TATR(NPCEL,IN+6)+R*VS(I)+DAZ TEST 353
CONTINUE EXTRAD 1678
411 TATR(NPCEL,INX)=SIGN(FLOAT(INA),TATR(NPCEL,INX)) TEST 354
IF (INA.EQ.1)TATR(NPCEL,INX)=SIGN(TATR(NPCEL,INX),-1.0) TEST 355
IF (1ST.LE.IMH.OR.ISP.GE.IMX) TATR(NPCEL,LOX)=-999. TEST 2 154
IF (VSTI.LE.IMH.OR.ISP.GE.IMX) TATR(NPCEL,LOX)=-999. TEST 2 155
GO TO 366 EXTRAD 1682
366Z NPCEL=MPK EXTRAD 1683
365 IF (NPCEL.GT.NIOP.OR.NPCEL.LE.0)GO TO 931 EX1 94
C INDX=TATR(NPCEL,I)-TC(K),IEJ-I TEST 357
C COMBINE LPCEL WITH NPCEL AT THIS LEVEL EXTRAD 1686
C COMBINE BY SETTING AREA AS POINTER AND IOX TO NA = 0 EXTRAD 1688
C EXTRAD 1689
C DO 365 L=1,LPCE EXTRAD 1690
IF (TUPKIPCEL,K,IE,IR,RI,L,I,IRHM) GO TO 365 TEST 217
IF (LUPKIPCI,L,K,IE,IR,RI,G,I,IND) GO TO 931 TEST 218
LPCEL=IUPKIPCI,L,K,IE,IR,RI EXTRAD 1695
341 IF (LPCEL.EQ.0)GO TO 365 TEST 358
IF (TATR(LPCEL,IOX).EQ.0)GO TO 365 TEST 359
351 IF (NPCEL.EQ.LPCEL)GO TO 365 EXTRAD 1698
INDX=TATR(LPCEL,I)-TC(K),IEJ-I TEST 359
IF (INDX.GE.LDB)GO TO 365 EXTRAD 1700
IF (INDX.LE.0)INDX=0 EXTRAD 1701
IND=ID*INDX*LM EXTRAD 1702
IF (TATR(LPCEL,IND).EQ.0)GO TO 365 TEST 360
IND=INDX*3 EXTRAD 1704
IPG=0 EXTRAD 1705

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DO 3663 J=IND,LOB
IN=(J-1)*LM+1
IF (IATR(LPCEL,IND,LM).EQ.NA) PG=1PG+1
DO 3663 I=1,LM
3663 TATR(LPCEL,IND)=0
IF (IPG.EQ.0.OR.IE.LE.1) GO TO 3664
IE=IE-1
DO 3665 I=1,IET
IPIY=IPICTI
IF (IPII.LE.0) GO TO 3665
DO 3666 KY=1,IPTI
MPC1=IPGNT(KY,I)
DO 3667 LP=1,NPCI
IF (LPCEL.NE.IUPK(IPC3,LP,KY,I,IR,JR)) GO TO 3667
INDX=TATR(NPCEL,I)-IPI(KY,I)-1
IF (INDX.LT.CLOB1GO TO 3668
GO TO 3667
3669 CALL IPK(IPC3,IZERO,LP,KY,I,IR,JR)
EXTRAD 1706
EXTRAD 1707
TEST 361
EXTRAD 1709
TEST 362
EXTRAD 1711
EXTRAD 1712
EXTRAD 1713
EXTRAD 1714
EXTRAD 1715
EXTRAD 1716
EXTRAD 1717
EXTRAD 1718
TEST1 219
TEST1 220
TEST 363
EXTRAD 1722
TEST1 221
EXTRAD 1724
EXTRAD 1725
EXTRAD 1726
TEST1 222
EXTRAD 1727
EXTRAD 1728
EXTRAD 1729
EXTRAD 1730
EX1 95
EXTRAD 1732
EXTRAD 1733
EXTRAD 1734
EX1 96
EXTRAD 1735
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EX1 97
EXTRAD 1746
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EXTRAD 1761
EXTRAD 1762

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400 C EXTRAD 1763
C EXTRAD 1764
C EXTRAD 1765
4213 IF (INDX.GE.A0B)GO TO 4221 EXTRAD 1766
      IN=INDX*LM EXTRAD 1768
405 512 IF (TATR(NPCEL,IN*IDX).NE.0)GO TO 5311 TEST 369
      IF (TATR(NPCEL,2*IN)-LE.J..AND.NGM.EQ.0)53 TO 4221 EXTRAD 1771
      IF (NGM.NE.1)GO TO 5312 EXTRAD 1772
406 5314 IN=INDX*LM TEST 223
      IF (IN.LT.0) GO TO 5311 TEST 224
      IF (LPCEL.LE.UOR.LPCEL.JT.NNY) GO TO 931 TEST 371
      IF (TATF(LPCEL,IN*IDX).NE.0)GO TO 5311 TEST 372
      IF (TATR(LPCEL,2*IN)-GT.J)GO TO 5313 EXTRAD 1775
      LPCEL=NPCEL EXTRAD 1776
      GO TO 4221 TEST 373
415 5313 LPCEL=TATR(LPCEL,2*IN) EXTRAD 1778
      IF (LPCEL.EQ.NPCEL)GO TO 5314 TEST 374
      INDX=TATR(LPCEL,1)-TC(K2,IE)-1 EXTRAD 1780
      GO TO 5314 TEST 375
420 5312 NPCEL=TATR(NPCEL,2*IN) EXI 59
      IF (NPCEL.LE.UOR.NPCEL.JT.NNY)GO TO 4221 TEST 376
      INDX=TATR(NPCEL,1)-TC(K2,IE)-1 TEST 377
425 5311 CALL IPK(IPC3,NPCEL,IE,K2,IE,IR,JK) EXTRAD 1783
      LSTE=IB TEST 225
      ISP=IMD TEST 226
      DO 531 I=IST,ISP EXTRAD 1785
      R=SCNG*(FLOAT(I)-1)-.51 EXTRAD 1787
      ROR=IBS(FLOAT(I)) TEST 379
      TATR(NPCEL,2*IN)=TATR(NPCEL,2*IN)+CAZ*R TEST 380
      TATR(NPCEL,3*IN)=TATR(NPCEL,3*IN)+DAZ*R TEST 381
      TATR(NPCEL,4*IN)=TATR(NPCEL,4*IN)+DAZ*SAZ*R*RU TEST 382
      TATR(NPCEL,5*IN)=TATR(NPCEL,5*IN)+DAZ*CAZ*RU*RU TEST 383
      IF (IY.EQ.0)GO TO 531 EX2 161
      IF (IY.NE.-999) TEST 384
      +TATR(NPCEL,6*IN)=TATR(NPCEL,6*IN)+DAZ*P*SV(I) TEST 385
      IF (IY.GE.2)GO TO 521 TEST 386
      IF (IY) .EQ. -999)GO TO 531 EXTRAD 1794
      TATR(NPCEL,7*IN)=TATR(NPCEL,7*IN)+DAZ*P*V(I) TEST 387
      IF (IY-1) .EQ. -999)GO TO 521 EXTRAD 1796
440 TATR(NPCEL,8*IN)=TATR(NPCEL,8*IN)+DAZ*P*V(I)-V(I)-I) TEST 388
      IF (WS(I).EQ.-999) GO TO 531 EXTRAD 1798
      TATR(NPCEL,7*IN)=TATR(NPCEL,7*IN)+DAZ*P*V(I) TEST 389
445 531 CONTINUE EXTRAD 1800
      TATR(NPCEL,IN*IDX)=SIGN(FLOAT(NAT),TATR(NPCEL,IN*IDX)) TEST 390
      IF (NA.EQ.1)TATR(NPCEL,1*IDX)=SIGN(TATR(NPCEL,IN*IDX),-1.0) TEST 391
      LPCEL=NPCEL EXTRAD 1804
      GO TO 4221 EXTRAD 1805
450 C COMBINE WITH B-RADIAL, C-LEVEL HIGHER EXTRAD 1806
C EXTRAD 1807
C IF FIRST COMBINE, AREA=0, IF SECOND OR HIGHER, AREA=-1. EXTRAD 1808
C TEST AREA TO ESTABLISH NEW NUMBERS EXTRAD 1809
455 481 INDX=-INDX EXTRAD 1810
      INDX=NUMP-1 EXTRAD 1811
      INDX=LCB EXTRAD 1812
      EXTRAD 1813
      EXTRAD 1814

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AD-A057 153

ENVIRONMENTAL RESEARCH AND TECHNOLOGY INC CONCORD MASS F/G 4/2
DEVELOPMENT OF TECHNIQUES FOR SHORT-RANGE PRECIPITATION FORECAS--ETC(U)
DEC 77 R K CRANE F19628-77-C-0058

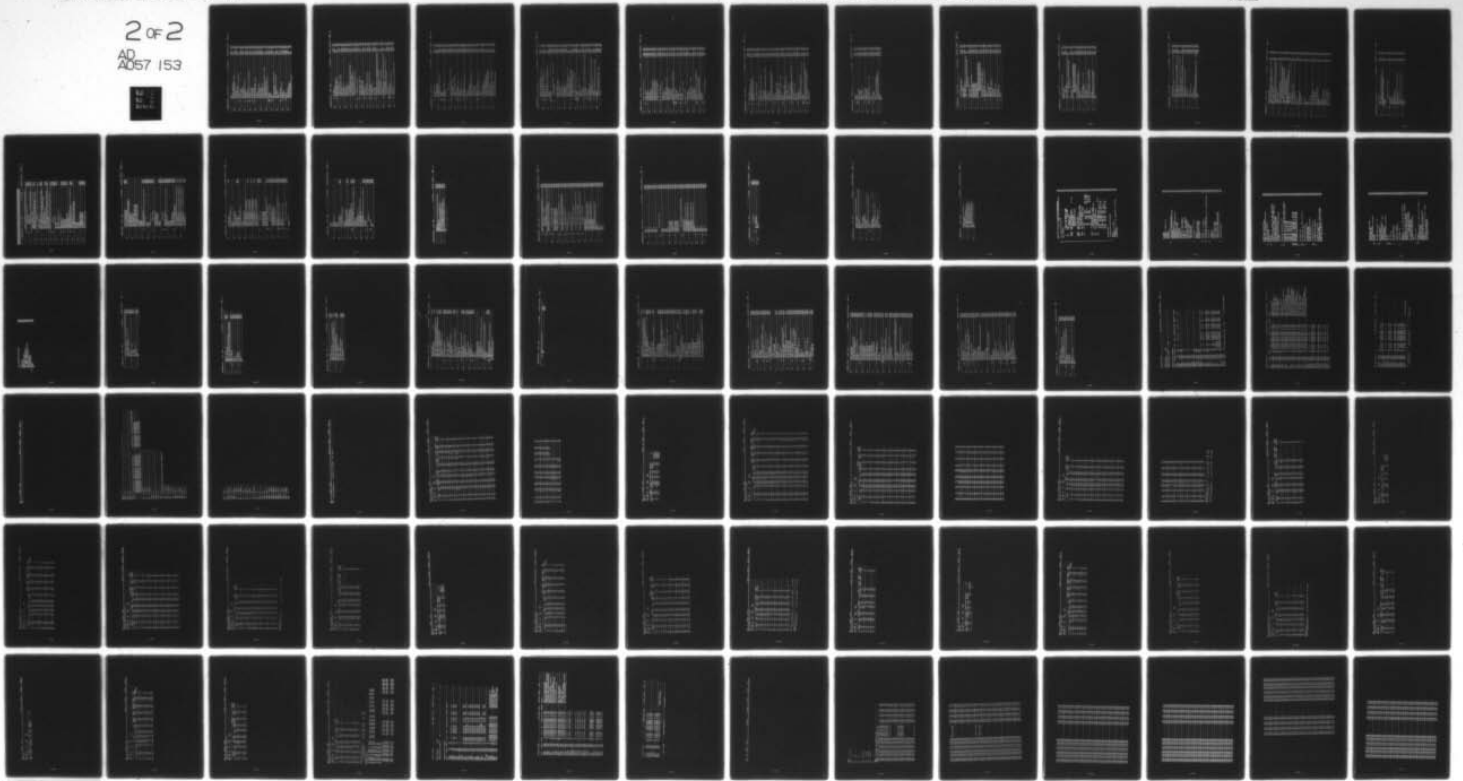
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INS=2
IPG=0
TATR(LPCEL,1)=TG(KC,IEI)+1
TATR(LPCEL,NUMP)=ASSIAT(IAT,1I01,1I)
460 IF(LNDC*GE*LOBT)GO TO 482
IND=LOB-INDX
DO 483 I=INDX,LOBH
IF (TATR(LPCEL,IDX+I)*LM).EQ.(NA)IPG=IPG+1
465 CONTINUE
DO 483 I=1,IND
DO 483 J=1,LM
IN=1+J+(LOB-I)*LM
IM=I*J+IND-1)*LM
470 TATR(LPCEL,IN)=TATR(LPCEL,IM)
IND=INDX*LM+1
INDP=INDX
482 DO 4835 I=1,LOB
IF (TATR(LPCEL,IDX+(I-1)*LM).EQ.(NA))IPG=IPG+1
485 CONTINUE
DO 484 I=INS,IND
TATR(LPCEL,I)=0.
484 DO 484.1 I=1,INDP
484.1 TATR(LPCEL,I)*LM+I)=NA
488 IF (IFG.EQ.0.OR.IE.LE.1)GO TO 488
IE=IE-1
IPII=IPI(I)
IF (IPII.LE.0)GO TO 4831
DO 4833 KI=1,IPII
NPCI=IPI(I,KI)
DO 4834 LPEI,NPCI
IF (NPCI.LE.0)GO TO 4833
INDX=TATR(LPCEL,I)-TG(KC,I)-1
IF (LPCEL.NE.I)FKI=IPC3,LP,(I,I,IR,JR)) GO TO 4834
IF (INDX.LY.LOBT)GO TO 4834
CALL YPK(IPC3,ZERO,LP,I,I,IR,JR)
4834 CONTINUE
4833 CONTINUE
4831 CONTINUE
4895 IPGE=0
488 IN=0
IF (LPCEL.LE.0.OR.LPCEL.GT.NHX)GO TO 931
TATR(LPCEL,IDX)=NA
CALL YPK(IPC3,LPCEL,IPE,KC,IE,IR,JR)
NPCI=LPCEL
NHN=0
GO TO 512
485 DO 485 I=1,NIP
IF (IAC(I).EQ.0)GO TO 487
486 CONTINUE
WRITE(6,644)
GO TO 931
487 LPCEL=I
IAC(I)=I
NWX=NA*(NHX,I+1)
IF (NWX.GT.NIP)NWX=NIP
TATR(LPCEL,1)=TG(KC,IE)+1
TATR(LPCEL,NUMP)=ASSIAT(IAT,1I01,1I)

```

EXTRAD 1815
 EXTRAD 1816
 TEST 393
 TEST 227
 TEST 1819
 EXTRAD 1820
 EXTRAD 1821
 TEST 395
 EXI 100
 EXTRAD 1824
 EXTRAD 1825
 EXTRAD 1826
 EXTRAD 1827
 TEST 396
 EXTRAD 1829
 EXTRAD 1830
 EXTRAD 1831
 TEST 397
 EXTRAD 1833
 EXTRAD 1834
 TEST 398
 EXTRAD 1836
 TEST 399
 EXTRAD 1838
 EXTRAD 1839
 EXTRAD 1840
 EXTRAD 1841
 EXTRAD 1842
 EXTRAD 1843
 EXTRAD 1844
 TEST 228
 TEST 229
 TEST 400
 EXTRAD 1848
 TEST 230
 EXTRAD 1851
 EXTRAD 1852
 EXTRAD 1853
 EXTRAD 1854
 EXI 181
 TEST 401
 EXTRAD 1856
 EXTRAD 1857
 EXI 182
 EXTRAD 1858
 EXI 183
 EXTRAD 1860
 EXTRAD 1861
 EXTRAD 1862
 EXTRAD 1863
 EXTRAD 1864
 EXTRAD 1865
 EXTRAD 1866
 EXI 184
 TEST 402
 TEST 231


```

591      YATR(NPCEL,ND+1)=0.
        CONTINUE
        YATR(NPCEL,ND+LM)=0.
        YATR(NPCEL,ND+1)=LPCEL
        YATR(NPCEL)=LPCEL
595      CALL IPK(IPB3,LPCEL,JPE,63+JE,IP,JK)
        CONTINUE
        CONTINUE
        CONTINUE
580      IF(INP*LE.0)GO TO 5662
        NPDEL=NPCEL
        GO TO 566
C
C      UNASSOCIATED
C
631      IF(INA.EQ.1.AND. ISCANF.EQ.0) GO TO 539
        IF (N1.EQ.1) GO TO 533
        GO 644 IF=LMB,ICD
        IF (N1.EQ.-593) GO TO 541
        IF (N1.EQ.57. TC(KC,IE))GO TO 931
590      CONTINUE
        GO 642 IF=L,NIOP
        IF (ACTY)EQ.0)GO TO 543
        CONTINUE
        WRITE(6,544)
544      FORMAT(5X,'* TOO MANY CE...S*')
        GO TO 531
630      NCELT=NCELT+1
        CALL IPK(IPB3,NCELT,PE,C,IE,IP,JF)
        GO TO 531
543      NPCEL=J
        NKE=AYC(NM,J+1)
        IF (N1.GT.NIOP)NM=NIOP
        CALL IPK(IPB3,NPCEL,PE,C,IE,IP,JF)
        IN=ELM+1
        IN=ELM-3)NLM*NI
        GO 671 IF=IN,IN
        YATR(NPCEL,1)=0.0
610      CONTINUE
        YATR(NPCEL,3)=YC(NC,IE)+1
        YATR(NPCEL,NUMP)=ABS(ATR(IAT,1)D1,1)
        IAT=THE
        IPE=IME
        GO 621 IF=IST,ICP
        R=SCON*(FLOAT(I-1)-.5)
        YU=WRRES(FLOAT(I))
        YATR(NPCEL,2)=CAZ*YATR(NPCEL,2)
        YATR(NPCEL,3)=CAZ*YU*YATR(NPCEL,3)
        YATR(NPCEL,4)=CAZ*YATR(NPCEL,4)
        YATR(NPCEL,5)=YATR(NPCEL,5)+CAZ*YATR(NPCEL,5)
        IF (ITY.EQ.0)GO TO 621
        IF (ITY.EQ.-999)
        *YATR(NPCEL,6)=YATR(NPCEL,6)+CAZ*YATR(NPCEL,6)
        IF (ITY.EQ.2)GO TO 621
        IF (ITY.EQ.-999)GO TO 621
        YATR(NPCEL,9)=YATR(NPCEL,9)+CAZ*YATR(NPCEL,9)

```

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TEST 416
EXTRAD 1927
TEST 417
TEST 418
EXTRAD 1930
EXTRAD 1931
EXTRAD 1932
EXTRAD 1933
EXTRAD 1934
EXTRAD 1935
EXTRAD 1936
EXTRAD 1937
EXTRAD 1938
EXTRAD 1939
EXTRAD 1940
EXTRAD 1941
EXTRAD 1942
EXTRAD 1943
EXTRAD 1944
EXTRAD 1945
EXTRAD 1946
EX1 113
EXTRAD 1948
EXTRAD 1949
EXTRAD 1950
EXTRAD 1951
EXTRAD 1952
EXTRAD 1953
EXTRAD 1954
EXTRAD 1955
EXTRAD 1956
EXTRAD 1957
EXTRAD 1958
EX1 114
EXTRAD 1959
EXTRAD 1961
EXTRAD 1962
EXTRAD 1963
TEST 419
EXTRAD 1965
TEST 420
TEST1 236
TEST1 235
TEST1 240
EXTRAD 1971
EXTRAD 1972
TEST 422
TEST 423
TEST 424
TEST 425
TEST1 241
EX1 166
TEST 427
TEST 428
TEST 429
EXTRAD 1978
TEST 430

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```

685 C COMBINE LAST TO FIRST CELL ATTR.
C
958 DO 959I I=1, IEM
IPT=IPIC(IIE)
DO 959J J=1, IPI
KC=IPT-LC+1
NPG=IPIC(IIC, IET)
DO 959I IPE=1, NPC
NPGCE=IOPK(IPE, IPE, KC, IET, I, J)
LPCCE=IOPK(IPE, IPE, KC, IET, I, J)
IF (NPGCE .LE. 0) GO TO 959I
IF (LPCCE .LE. 0) GO TO 959I
INDX=IATR(LPCEL, I) - IATR(NPCEL, I)
IF (INDX .LT. 0) GO TO 958
700 C PEAK LPCEL -GE. PEAK NPCEL.
C
IF (INDX .GE. LOB) GO TO 955
IND=LOB-INDX
DO 9592 I=1, IND
IM=I+IND-IT*LM
IF (IATR(NPCEL, IM) .GE. 0.100 TO 9592
IATR(LPCEL, IM)=MAX-1
DO 9593 J=1, IWN
IN=I+J+(LOB-I)*LM
IMS=J+(IND-IT)*LM
IATR(LPCEL, IM)=IATR(NPCEL, IM)+IATR(LPCEL, IM)
9593 CONTINUE
9592 DO 9594 I=1, NUMP
9593 IATR(NPCEL, I)=N.
9594 IACT(NPCEL)=0
955 IATR(LPCEL, LOB)=MAX-1
720 958 INDI=INDX
C IF (INDX .GE. LOB) GO TO 959I
C PEAK NPCEL .GT. LPCEL
C
IND=LOB-INDY
DO 959I I=1, IND
IN=I+IND-IT*LM
IF (IATR(NPCEL, IN) .GE. 0.100 TO 959I
IATR(NPCEL, IN)=MAX-1
DO 9592 J=1, IWN
IMS=J+(IND-IT)*LM
IN=I+J+(IND-I)*LM
IATR(NPCEL, IN)=IATR(LPCEL, IN)+IATR(NPCEL, IN)
9592 CONTINUE
959I CALL IPR(IPE, NPCEL, IPE, KC, IET, I, J)
IATR(NPCEL, NUMP)=IATR(LPCEL, NUMP)
NPCEL=LPCEL
GO TO 9593
740 959I CONTINUE
C
C END OF ASSOCIATION LOOPS

```

```

C
952 DO 991 I=1,NMX
   IF (ACT(I).EQ.0) GO TO 991
   IF (ATP(I,LDX).EQ.-999) GO TO 9982
745   IF (ATP(I,LDX).EQ.-999) GO TO 9912
   IF (ABS(TATP(I,LDX)).EQ.NAX-1) GO TO 971
   GO TO 991
C
750   CHECK BACKGROUND COMING DOWN
C
971 INBRED
   DO 9716 J=1,LOBM
   IF (ATP(I,IRIJ-1)*L4).C.0) GO TO 9982
755   CONTINUE
   DO 9711 J=1,JEM
   ICI=I*(NPA+J)
9712   IF (ATP(I,NUMP).NE.ABS(ATR(I,ICI))) GO TO 9711
   DO 9713 K=1,IPB
   NP=I*PNTK+J
   DO 9713 N=1,NP
   IF (I.NE.IUPK(IPB3,N,K,IR,JK)) GO TO 9713
765   IF (ATP(I,IRI)-TB(K,JK).EQ.CB765) GO TO 9713
   CONTINUE
   GO TO 9711
9714 IN3K=1*99+1
   IST=IUPK(IPB1,N,K,IR,JK)
   ISP=IUPK(IPB2,N,K,IR,JK)+1
770   DO 9715 L=1,ISP
   IF (L).EQ.-999) GO TO 9715
   IF (ABS(T(L)) .GT. TB(K,JK)) GO TO 9982
   CONTINUE
775   IF (IND).EQ.0) GO TO 9982
   IF (ATP(I,CKT) .GT. 1) GO TO 991
   IF (IAT+1).I02+1).LE.IAT) GO TO 9582
   DO 981 J=1,LMW
   UPINCELL(J)=IATP(I,I02+J)
   CONTINUE
780   UPINCELL(M)=IATP(I,NUM?)
   IF (I*MG+EQ.1) WRITE(5,9917) INCELL,UPINCELL,J,I,J,I,LM
9918   FORMAT (1X,2MC,14,4X,9F13.2)
785   MCELL=CELL*1
   MCELL=ND
   GO TO 9982
9912 DO 9913 J=1,LDL
   INDI=I+J*LM
790   IF (ABS(TATP(I,INDI)).EQ.NMIG) GO TO 991
   IF (ATP(I,INDI).LT.0.) GO TO 991
   CONTINUE
9913   CONTINUE
9982   CONTINUE
795   IF (I*MG+EQ.1) WRITE(5,9918) I,ACT(I),I,ICI,NUMP
999   FORMAT (1X,2MX,14,16,F7.2,6F13.2,/(20X,6F13.2))
999   FORMAT (3X,14,16,F7.2,6F13.2,/(20X,6F13.2))
   DO 992 J=1,NUMP
992   TATP(I,JI)=0.

```

EXTRAD 2094
 EXTRAD 2095
 EXTRAD 2096
 TEST 455
 TEST 456
 TEST 457
 EXTRAD 2100
 EXTRAD 2101
 EXTRAD 2102
 EXTRAD 2103
 EXTRAD 2104
 EXTRAD 2105
 TEST 458
 EXTRAD 2108
 EXTRAD 2109
 TEST 242
 EXTRAD 2111
 EXTRAD 2112
 EXTRAD 2113
 EXTRAD 2114
 EXTRAD 2115
 TEST 460
 EXTRAD 2117
 EXTRAD 2118
 EXTRAD 2119
 EXTRAD 2120
 EXTRAD 2121
 EXTRAD 2122
 EX 117
 EXTRAD 2123
 EXTRAD 2124
 EXTRAD 2125
 EXTRAD 2126
 TEST 461
 TEST 462
 EXTRAD 2129
 TEST 243
 EXTRAD 2131
 TEST 244
 TEST 245
 EX 2 175
 EXTRAD 2135
 EXTRAD 2136
 EXTRAD 2137
 EXTRAD 2138
 EXTRAD 2139
 EXTRAD 2140
 TEST 466
 TEST 467
 EXTRAD 2143
 EXTRAD 2144
 TEST 467
 EXTRAD 2146
 EXTRAD 2147
 EXTRAD 2148
 TEST 468

```

991 IACT(I)=9
992 CONTINUE
993 DO 1041 I=1,ITEMA
994   IPB(I)=IPB(I)
995   DO 1042 K=1,ITEMB
996     YB(K,I)=YB(K,I)
997     IPBNT(K,I)=IPBNT(K,I)
998   CONTINUE
999   DO 1043 IA=1,IAMAX
1000     IPB(I)=IPB(I)
1001     IPB2(I)=IPB2(I)
1002     IPB3(I)=IPB3(I)
1003   IF (ISCANF.NE.1.CM.NB.EQ.1) GO TO 1040
1004   NA=I
1005   MCEL=1
1006   GO TO 1045
1007 1045 DO I 1 22, MCLM
1008     MH=-999
1009     IF (U(I-1).NE.-999) MH=IABS(U(I-1))
1010     IF (U(I).NE.-999) MH=MAX(MH,IABS(U(I)))
1011     IF (U(I+1).NE.-999) MH=MAX(MH,IABS(U(I+1)))
1012     RETURN
1013   END

```



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1  SUBROUTINE PRANG                                EXTRAD 2247
   .....                                         EXTRAD 2248
   .....                                         EXTRAD 2249
   .....                                         EXTRAD 2250
   .....                                         EXTRAD 2251
   .....                                         EXTRAD 2252
   .....                                         EXTRAD 2253
   .....                                         TEST 157
   .....                                         TEST2 157
   .....                                         EXTRAD 2256
   .....                                         EXTRAD 2257
   .....                                         EXTRAD 2258
   .....                                         EXTRAD 2259
   .....                                         EXTRAD 2260
   .....                                         EXTRAD 2261
   .....                                         EXTRAD 2262
   .....                                         EXTRAD 2263
   .....                                         EXTRAD 2264
   .....                                         EXTRAD 2265
   .....                                         EXTRAD 2266
   .....                                         EXTRAD 2267
   .....                                         EXTRAD 2268
   .....                                         EXTRAD 2269
   .....                                         EXTRAD 2270
   .....                                         EXTRAD 2271
   .....                                         EXTRAD 2271

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1 SUBROUTINE PRN2(MODE)
2 PRINTS OUT DATA IN CODES MAP FORM AZIMUTH BY AZIMUTH.
3 VERSION 1.0 LEVEL 768320.
4 JMW CDC 800V AFSL
5 LOGICAL PRINTS,PRINTS,COPLOT,CONTRZ,CONTRF,CONTRF,VOLTAP
6 DIMENSION IC(164),LUNIT(3)
7 DIMENSION TYPE(3)
8 INTERP N,T,V,S,Y,C,W,J,M,E,WI,NCL
9 COMMON /PARM/ PRINT1,PRINT2,PRINT3,COPLOT,ICODES(16),A1,A2,A3,
10 CONTRZ,CONTRF,CONTRF5,NFILE,NUMF,NRES,NUMR,VOLTRF,
11 COMMON /REFL/ M1(73),M1(73),M1(73),M1(73),M1(73),M1(73),M1(73),
12 COMMON /VEL/ V1(73),V1(73),V1(73),V1(73),V1(73),V1(73),V1(73),
13 COMMON /AZW/ AZIMUTHS(73),AZIMUTHS(73),AZIMUTHS(73),
14 COMMON /ADAT/ DAY,TIME,IM,ISEC,NRP,NSF,NDQ,NRC
15 COMMON /INSUB/ TL(2),LT,YCH,ON,STARTR,STOPR,ZN(6),SECON,CELTR(3)
16 1,ICOMP,PHIN,SPMIN
17 DATA LUNIT/6,9,14/
18 DATA TYPE/MBE,MBE,MBE,MBE,MBE/
19 IF(MODE.GT.1)GO TO 30
20 DO 40 I=1,64
21 ICATI=I*8
22 ICDCR=ICATI/ICOMP
23 INT=(NCON-1)/6441
24 DO 28 K=1,3
25 I=1
26 L=1
27 IO=JUNIT(I)
28 DO 30 N=1,INT
29 I=10
30 I=10
31 I=10
32 I=10
33 I=10
34 I=10
35 I=10
36 I=10
37 I=10
38 I=10
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5 ICHIS=ICODS(IY)
6 I=1+1
50 IF(L-CL,NCCL,AND,C.LT,NEG,AND,I.LT,64) GO TO 3
WRITE(IU,100)AZMTH(NA),ELEVAT,IDAY,IMOUR,IMIN,ISEC,IC
100 FORMAT(IX,F5.1,F6.1,I4,IX,Z12,13,5X,6NAI)
20 CONTINUE
30 RETURN
65 C
C
C
30 DO 35 K2,3
IU=IUNIT(K)
70 31 REWIND IU
CALL PAGE
WRITE(IU,101)TYPE(K)
101 FORMAT(940 MAP OF ,A10)
CALL PRNG
75 34 READ(IU,100)AZMUT2,ELEVAT,IDAY,IMOUR,IMIN,ISEC,IC
355 CONTINUE
WRITE(IU,101)35,355,35
80 35 CONTINUE
END

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115 IF(EOF(2))999,11 000990
11 IF(KA.NE.-999) GO TO 31
   CALL LABEL(IXA,IYA,ELEVAT,XSIZ)
   GO TO 3
31 CONTINUE
120 IF(IXA.GT.1000)BACKSPACE 2
   IF(IXA.GT.1000)GO TO 18
   IF(IXA.GE.4000)GO TO 50
   PRINT(1)B,YB,KB 001010
   IF(EOF(2))999,11 001020
125 IF(IXB.NE.-999) GO TO 32
   CALL LABEL(IXB,IYB,ELEVAT,XSIZ)
   GO TO 3
32 CONTINUE
130 IF(IXB.GE.4000)GO TO 50
   XAS=IA-4,5*LEN(XMIN)
   IYVA=LY-5,5*YAS=YB-4,5*YLEN(XMIN)+DIFF1
   IF(IXA.GT.5)DIAS=IA-4,5*LEN(XMIN)-DIFF2 001030
   YBS=YB-4,5*YLEN(XMIN)
   IF(IXB.LT.5)DIYBS=YB-4,5*YLEN(XMIN)+DIFF1
   IF(IXB.GT.5)DIYBS=YB-4,5*YLEN(XMIN)-DIFF2
   XAS=YA-4,5*YLEN(YMIN)
   IF(IXA.LT.5)DIYAS=YA-4,5*YLEN(YMIN)+DIFF1
   IF(IXA.GT.5)DIYAS=YA-4,5*YLEN(YMIN)-DIFF2
   YBS=YB-4,5*YLEN(YMIN)
   IF(IXB.LT.5)DIYBS=YB-4,5*YLEN(YMIN)+DIFF1
   IF(IXB.GT.5)DIYBS=YB-4,5*YLEN(YMIN)-DIFF2
   IF(.NOT.LS)GO TO 18 001070
C 001080
C 001090
C 001100
145 XAS=(XAS-XI1)*SFXXMIN
   XBS=(XBS-XI1)*SFXXMIN
   YAS=(YAS-YI1)*SFYYMIN
   YBS=(YBS-YI1)*SFYYMIN
   WRITE(6,100)XAS,XBS,YAS,XBS,YBS
   FORMAT(I1,ZI2F7.3,I5I,150,4F6.3) 001150
C 001160
C 001170
C 001180
C 001190
155 IF(Z1.AND.(KA.EQ.388350)TO 15 001200
   IF(Z2.AND.(KA.EQ.388210)TO 19 001210
   IF(Z3.AND.(KA.EQ.388350)TO 19 001220
   IF(Z4.AND.(KA.EQ.388450)TO 15 001230
   GO TO 28 001240
160 CALL EXPAN(IXAS,YAS,XBS,YBS),RETURNS(20,12,40)
   WRITE(6,101) 001250
101 FORMAT(1H*,40X,'*OUTSIDE PLOT AREA*')
   GO TO 12 001270
102 WRITE(6,102) 001280
   FORMAT(1H*,40X,'*ERROR, SKIP PLOT*')
   GO TO 12 001300
C 001310
C 001320
C 001330
170 IF(.NOT.LK)GO TO 3 001340
   YAS=YK

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YBAR=YA
IO=KA
GO TO 53
175 500 IF (.NOT.LK) GO TO 3
YBAR=YA
YBAR=YA
IO=KB
GO TO 53
180 51 READ(I)XBAR,YBAR,IO
IF (.EOF) 599, 52
52 IF (I) GOTO 53
CALL LABEL(I,XBAR,IYR,ELEMT,XSIZ)
GO TO 3
185 53 CONTINUE
YBAR=YBAR-4.5*YLEN*YIN
YBAR=YBAR-4.5*YLEN*YIN
IF (.NOT.LSTGO) GO TO 60
XBAR=(XBAR-XI)*SF*YIN
YBAR=(YBAR-YII)*SF*YIN
60 WRITE(6,103)XBAR,YBAR,IO,XBAR,YBAR
103 FORMAT(IX,2Y7.3,I5,TSU,2F8.3)
IF (.OR.(XBAR.LT.XI.OR.XBAR.GT.XI.OR.YBAR.LT.YI.OR.YBAR.GT.YI))
GO TO 61
195 IJKID=ID/1800
JINDEX=JXID-3
IF (.NOT.IPLT(JINDEX)) GO TO 51
ISYM=JYH(JINDEX)
CALL SYMBOL(XBAR,YBAR,SSIZ,ISYM,XMETA,0)
200 IF (JINDEX.GE.3) GO TO 51
FIO=IO-IJKID*1800
CALL NUMBER(YBAR,SYCSIZ,YBAR,SYCSIZ,FIO,XMETA,-1)
GO TO 51
205 61 WRITE(6,IUI)
C
C TERMINATE PLOT
C
999 CALL EMOPLT
210 STOP
END
001400
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1      BLOCK DATA
      COMMON/HEAD/TITLE(6),ICDDE,VERS,LEVEL,DAT,IRUN,NPAGE,MLOG
      COMMON/LINUM/LINE
      COMMON/EXPAR/X1,R2,Y1,Y2,KMIN,XMAX,YMIN,YMAX
2      DATA XI/1.0,Y1/9.0,Y2/9.0,Y17/1.0,Y27/9.0/
3      DATA KMIN/1.0,XMAX/9.0,YMIN/1.0,YMAX/9.0/
      DATA TITLE/'PROGRAM: M EXPAND'/' IN 'IN '/
      IRUN/0,NPAGE/1,ICDDE/175,VERS/1.0,LEVEL/770331/
      END
    
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1  C..... SUBROUTINE EAPAN1(XA,XB,YA,YB,X1,X2,X3,RETURNS,INI,NC,N3) 001699
   C..... VERSION 1.0 LEVEL 7778337 001700
   C..... AFGL COS6698 001720
   C..... SPECIAL EXPANDET (NICE PLOTTING) 001730
   C..... COMMON/EXPAN/X1,X2,Y1,Y2,XMIN,XMAX,YMIN,YMAX 001740
   C..... 001750
   C..... 001760
10  C..... TEST IF LINE IS IN THE AREA 001770
   C..... 001780
   C..... 001790
   C..... IF(XA.LT.X1.AND.XB.LT.X1)RETURN N1 001800
   C..... IF(YA.GT.Y2.AND.YB.GT.Y2)RETURN N1 001810
   C..... IF(YA.LT.Y1.AND.YB.LT.Y1)RETURN N1 001820
   C..... IF(YA.GT.Y2.AND.YB.GT.Y2)RETURN N1 001830
   C..... 001840
   C..... TEST IF LINE IS TIRCELY IN THE AREA 001850
   C..... 001860
   C..... IF(XA.GE.X1.AND.XA.LE.X2.AND.YB.GE.Y1.AND.YB.LE.Y2)GO TO 49 001870
   C..... 1YA.GE.Y1.AND.YA.LE.Y2.AND.Y3.GE.Y1.AND.Y3.LE.Y2)GO TO 49 001880
   C..... TEST IF SLOPE IS INFINITE 001890
   C..... 001900
   C..... IF((XB-XA).EQ.0.0)GO TO 17 001910
   C..... 001920
   C..... TEST IF SLOPE IS ZERO 001930
   C..... 001940
   C..... IF((YB-YA).EQ.0.0)GO TO 18 001950
   C..... 001960
   C..... TEST IF POINT A IS IN THE AREA 001970
   C..... 001980
   C..... IF(YA.GE.X1.AND.XA.LE.X2.AND.YA.GE.Y1.AND.YA.LE.Y2)GO TO 20 001990
   C..... 002000
   C..... TEST IF POINT B IS IN THE AREA 002010
   C..... 002020
   C..... IF(XB.GE.X1.AND.XB.LE.X2.AND.YB.GE.Y1.AND.YB.LE.Y2)GO TO 10 002030
   C..... 002040
   C..... 002050
   C..... 002060
   C..... 002070
   C..... 002080
   C..... 002090
   C..... SLOPB=(YB-YA)/(XB-XA) 002100
   C..... REYB=SLOPB*(YB-Y1) 002110
   C..... IF(B.GE.Y1.AND.B.LE.Y2.AND.XB.LT.X1)GO TO 4 002120
   C..... IF(B.GE.Y1.AND.B.LE.Y2.AND.XB.LT.X1)GO TO 5 002130
   C..... 9=YB-SLOPB*(XB-X2) 002140
   C..... IF(B.GE.Y1.AND.B.LE.Y2.XYJ.XB.GT.X2)GO TO 8 002150
   C..... IF(B.GE.Y1.AND.B.LE.Y2.AND.XA.GT.X2)GO TO 9 002160
   C..... SLOPB=X1/SLOPB 002170
   C..... A=XB-SLOPB*(YB-Y1) 002180
   C..... IF(A.GE.X1.AND.A.LE.X2.AND.YB.LT.Y1)GO TO 6 002190
   C..... IF(A.GE.X1.AND.A.LE.X2.AND.YA.LT.Y1)GO TO 7 002200
   C..... RETURN N3 002210
   C..... XB=X1 002220
   C..... YB=B 002230
   C..... GO TO 10 002240
   C..... XA=X1 002250
   C..... YA=B 002260
   C..... GO TO 20 002270

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6   YB=YI      002260
   XB=A       002270
   GO TO 10   002280
7   YA=YI      002290
   XB=YI      002300
   GO TO 28   002310
8   XB=XZ      002320
   YB=B       002330
   GO TO 18   002340
9   XA=XZ      002350
   YB=B       002360
   GO TO 20   002370
70  C          002380
   C          002390
   C          002400
10  KS=XA     002410
   YSEYA     002420
   XA=XB     002430
   YA=YB     002440
   XB=XS     002450
   YB=YS     002460
   GO TO 20   002470
80  IF(YA.LT.YI)YA=YI  002480
   IF(YB.LT.YI)YB=YI  002490
   IF(XA.GT.YZ)XA=YZ  002500
   IF(YB.GT.YZ)YB=YZ  002510
   GO TO 49   002520
85  IF(XA.LT.XI)XA=XI  002530
   IF(XB.LT.XI)XB=XI  002540
   IF(XA.GT.XZ)XA=XZ  002550
   IF(YB.GT.XZ)YB=XZ  002560
   GO TO 49   002570
90  C          002580
   C          002590
   C          002600
20  SLOP=(YB-YA)/(XB-XA)  002610
   B=YB-SLOP*(XB-XI)  002620
   IF(B.GE.YI.AND.B.LE.Y2.AND.XB.LT.XI)GO TO 22  002630
   B=YB-SLOP*(XB-XZ)  002640
   IF(B.GE.Y1.AND.B.LE.Y2.AND.XB.GT.XZ)GO TO 24  002650
   SLOPA=1/7/SLOPB  002660
100 A=XB-SLOPA*(YB-Y1)  002670
   IF(A.GE.X1.AND.A.LE.X2.AND.YB.LT.Y1)GO TO 26  002680
   A=XB-SLOPA*(YB-Y2)  002690
   IF(A.GE.X1.AND.A.LE.X2.AND.YB.GT.Y2)GO TO 28  002700
   RETURN M3  002710
22  YB=YI      002720
   XB=YI      002730
   GO TO 49   002740
24  YB=B       002750
   XB=XZ      002760
   GO TO 49   002770
26  YB=YI      002780
   XB=YI      002790
   GO TO 49   002800
28  XB=A       002810
   YB=YZ      002820

```

TEST FOR SIDE POINT A TO POINT B INTERSECTS

115	C		002030
	C	PLOT THE LINE	002040
	C		002050
	49	CALL PLOT(XA,YA,3)	002060
		CALL PLOT(XB,YB,2)	002070
120		RETURN M2	002080
		END	002090

```

1 SUBROUTINE MUSCAL(XI,X2,KLEN,XSTART,XEND,DELX)
  DIMENSION DELTA(15)
  DATA DELTA /1.,2.,5.,10.,20.,25.,40.,50.,75.,100.,150.,200.,
  *250.,350.,500./
5 XMAX=X2
  XMIN=X1
  IF (X2.LT.X1) XMAX=X1
  IF (X2.LT.X1) XMIN=X2
  DIFF=(XMAX-XMIN)/KLEN
  DO 10 J=2,15
  IF (DIFF.GT.DELTA(J-1).AND.DIFF.LE.DELTA(J)) GO TO 20
  *10 CONTINUE
  J=15
15 DELX=DELTA(J)
  ISTART=XMIN/DELX
  ISTART=ISTART*DELX
  IF (XMIN.LT.0.) ISTART=(ISTART-1)*DELX
  IEND=XMAX/DELX
  IEND=IEND*DELX
  IF (XMAX.LT.0.) IEND=IEND*DELX
  RETURN
  END
  
```

```
1 SUBROUTINE LABEL(IX,IY,ELEVAT,XSIZ)
  DIMENSION LABL(3)
  DATA LABL/MDKY ,NHTIME,SREL /
  CALL SYMBOL(5,0,01,XSIZ,LABL(1),0,0,4)
  CALL NUMBER(6,0,0,01,XSIZ,IX,W,0,0,0)
  CALL SYMBOL(6,0,0,01,XSIZ,LABL(2),0,0,4)
  CALL NUMBER(5,0,0,01,XSIZ,IY,0,0,0)
  CALL SYMBOL(7,0,0,01,XSIZ,LABL(3),0,0,4)
  CALL NUMBER(6,5,0,01,XSIZ,ELEVAT,0,0,0)
  RETURN
  END
```

```

100 SUBROUTINE LINLOG (X,Y,BCD,N,PLTEN,NUMBUS,BEGNUM,ENDNUM,
110 DEL , NUMDEC, THETA, BCD5IZ,DRAM,XMOD,ITYPE)
120
130 PLOT LABELED LINEAR OR LOG AXIS
140
150 INPUT PARAMETERS
160
170 X X CORD OF POINT BEGNUM IN INCHES
180 Y Y CORD OF POINT ENDNUM IN INCHES
190 BCD TITLE MAILO FORMAT
200 N NUMB. CHARACTERS IN BCD
210 PLTEN LENGTH IN INCHES ENTIRE AXIS
220 NUMBUS NUMB. SUBDIV. BETWEEN MAJOR DIV. (N.A. LOG)
230 <del>=NO SUBDIVISIONS
240 2=DIVIDE MAJOR DIV. IN 1/2
250 3=DIVIDE MAJOR DIV. IN 1/3
260 ETC
270
280 VALUE AT AXIS ORIGIN
290 ENDNUM VALUE AT AXIS END
300 DEL ABS OF DELTA VALUE BETWEEN MAJOR DIV.
310 NUMDEC -DEL = START DIVISIONS AT ENDNUM
320 .LT. -1 = SUPPRESS NUMBERS
330 THETA AXIS ANGLE
340 0 X-AXIS BOTTOM LEFT TO RIGHT
350 -180 X-AXIS TOP LEFT TO RIGHT
360 +180 X-AXIS USED AS Y LEFT TO RIGHT
370 90 Y-AXIS LEFT BOT TO TOP
380 -90 Y-AXIS RIGHT BOT TO TOP
390 270 Y-AXIS USED AS X BOT TO TOP
400
410 BCD5IZ LETTER SIZE IN INCHES
420 CLEARANCE NEEDED 3.1 *BCD5IZ
430 DRAM LENGTH IN INCHES OF MAJOR DIVISION LINES
440 0.=SUPPRESS LINES
450 XMOD MODULO VALUE FOR MAJOR DIVISION
460 0.=NON-CYCLICAL
470 ITYPE 1= LINEAR AXIS NORMAL TITLE EXP ONLY DEFAULT=1
480 2= LOG AXIS NORMAL TITLE EXP ONLY
490 3= LOG AXIS NORMAL TITLE BASE 10 & EXP
500 4= LOG AXIS NORMAL TITLE BASE E & EXP
510 -1= LINEAR AXIS VERT TITLE
520 -2= LOG AXIS VERT TITLE EXP ONLY
530 -3= LOG AXIS VERT TITLE BASE 10 & EXP
540 -4= LOG AXIS VERT TITLE BASE E & EXP
550
560 DIMENSION BCD(1)
570
580 SET ORIENTATION AND SIZE PARAMETERS
590
600 ISPEC=0
610 IF(DEL .LT. 0.0) ISPEC=1
620 KIND=ITYPE
630 IF((IABS(ITYPE) .LT. 1) .OR. (IABS(ITYPE) .GT. 4)) KIND=1
640 DELNUM=ABS(DEL)

```

```

650 ON #BEGNUM
660 ON #ENDNUM
670 IF(BEGNUM .LT. ENDNUM) GO TO 5
680 ON #ENDNUM
690 OFF#BEGNUM
700 DELNUMS=DELNUM
710
720
730
740
750
760
770
780
790
800
810
820
830
840
850
860
870
880
890
900
910
920
930
940
950
960
970
980
990
1000
1010
1020
1030
1040
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1070
1080
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1100
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1120
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1170
1180
1190

C 5
NUMDIV=ABS((ENDNUM-BEGNUM)/DELNUM)
DIVLEN=PTLEN/ ABS((ENDNUM-BEGNUM)/DELNUM)
HEIGHT=COBIZ*0.75
VTRIZ=COBIZ*(0.25+COBIZ)
SUPERHEIGHT/2.0 * SIZEMHEIGHT*0.75
SINANG=ABS((THETA/37.2950)
COSANG=COS(THETA/37.2950)
SINI=ABS(SINANG)
COSI=ABS(COSANG)
THETA=THETA
IF(THETA .EQ. -180.0) THETA=0.0
IF(THETA .EQ. 270.0) THETA=90.0
SIGNER1.0
IF(THETA .LE. 45.0) SIGNER=-1.0
IF(THETA .EQ. -90.0) SIGNER=1.0
TICANG=THETA*(90.0+SIGNER)
TICBIZ = (0.20 * HEIGHT) * .10
SIZIC = 0.50 * TICBIZ
XENDM=(PTLEN*COBIZ)
YENDM=(PTLEN*SINI)

C
C IF(ABS(XEND) .GE. 2) GO TO 10
C
C SUBDIV = 0
IF(NUMSUB .LE. 0) GO TO 99
SUBDIV=DIVLEN/FLOAT(NUMSUB)
SUBNUM=DELNUM/FLOAT(NUMSUB)
GO TO 99

C 10
NUMTIC=1
IF(DIVLEN .LT. 1.0) NUMTIC=2

C 99
DIVOFF=HEIGHT*((1.25+SIGNER)-0.5)
IF((THETA .EQ. -180.) .OR. (THETA .EQ. 270.)) DIVOFF=DIVOFF+HEIGHT

C
C CYCLING LOOP
M1=NUMDIV +1
DO 999 I=1,M1
CYCLE=I-1
DIVTIC = CYCLE * DIVLEN
TICK = X +(DIVTIC * COSI)
TICK = Y +(DIVTIC * SINI)
IF(ISPEC .EQ. 1) TICX=END-(DIVTIC*COBIZ)
IF(ISPEC .EQ. 1) TICY=END-(DIVTIC*SINI)

C
C DRAW DIVISION NUMBERS

```

```

1200 IF (NUMDEC .LT. (-1)) GO TO 101
1210 DIVNUM = BEGNUM + (CYCLES * DELNUM)
1220 IF (ISPEC .EQ. 1) DIVNUM=ENDNUM-(CYCLES*DELNUM)
1230 IF (XMOD .EQ. 0.0) GO TO 102
1240 IF (DIVNUM .LT. XMOD) GO TO 192
1250 DIVNUM=DIVNUM-XMOD
1260 GO TO 101
1270 PLACES = 0.
1280 IF (DIVNUM .NE. 0.) PLACES = AINT (ALOG10 (ABS (DIVNUM)))
OFFSET = -.50 * HEIGHT * (PLACES + FLOAT (NUMDEC) * 1.25)
1290 IF ((THETA.EQ.-180.) .OR. (THETA.EQ. 270.)) OFFSET=OFFSET
1300 IF ((THETA.EQ.-180.) .OR. (THETA.EQ. 270.)) OFFSET=OFFSET
1310 XP=TIC*(OFFSET+COSANG)-(DIVOFF*BINANG)
1320 YP=TIC*(OFFSET+SINANG)+(DIVOFF*CSINANG)
1330 IF (IABS(KIND) .GT. 2) GO TO 201
1340 CALL NUMBER (XP,YP,HEIGHT,DIVNUM,THETA,NUMDEC)
1350 GO TO 301
1360
1370 SPECIAL LABEL LOG BASE 10 OR E & EXP
1380
1390 IF (IABS(KIND) .EQ. 3) CALL NUMBER (XP,YP,SIZE*10.,THETA,-1)
1400 IF (IABS(KIND) .EQ. 4) CALL SYMBOL (XP,YP,SIZE*1ME,THETA, 1)
1410 IF (THETA .EQ. 0.0) GO TO 202
1420 IF (THETA .EQ. -180.0) GO TO 202
1430 IF (THETA .EQ. 90.0) GO TO 203
1440 IF (THETA .EQ. 270.0) GO TO 203
1450 IF (THETA .EQ. 180.0) GO TO 204
1460 IF (THETA .EQ. -90.0) GO TO 205
1470 XP=XP+HEIGHT * YPS*YP+HEIGHT * 60 TO 299
1480 YP=YP+HEIGHT * YPS*YP+HEIGHT * 60 TO 299
1490 XP=XP-HEIGHT * YPS*YP+HEIGHT * 60 TO 299
1500 YP=YP-HEIGHT * YPS*YP+HEIGHT * 60 TO 299
1510 CALL NUMBER (XPS,YPS,SUPER,DIVNUM,THETA,NUMDEC)
1520
1530 C
1540 C
1550 C
1560 C
1570 C
1580 C
1590 C
1600 IF (DRAW .EQ. 0.0) GO TO 302
1610 XXXTIC*(DRAM+SINANG)
1620 YYYTIC*(DRAM+CSINANG)
1630 IF (THETA .EQ. 180.0) YYYTIC*Y*DRAM
1640 CALL PLOT (XXXX,YYYY,2)
1650
1660 IF (IABS(KIND) .GE. 2) GO TO 304
1670
1680 C
1690 C
1700 C
1710 IF (NUMSUB .LE. 1) GO TO 999
1720 DO 303 J = 2, NUMSUB
1730 TEST=(BEGNUM+(CYCLES*DELNUM)) + (FLOAT(J-1)*SUBNUM)
1740 IF ((TEST .LT. 0N) .OR. ((TEST .GT. OFF)) GO TO 303
SUBSTIC = SUBDIV * FLOAT (J - 1)

```

```

1750 IF(18PEC .EQ. 1) SUBTIC=SUBTIC
1760 XB=TIC*(SUBTIC*COB1)
1770 YB=TIC*(SUBTIC*BIN1)
1780 CALL SYMBOL (18, YB, 81ZTIC, 15, TICANG, =1)
1790 CONTINUE
1800 GO TO 999
1810
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2250
2260
2270
2280
2290

IF(18PEC .EQ. 1) SUBTIC=SUBTIC
XB=TIC*(SUBTIC*COB1)
YB=TIC*(SUBTIC*BIN1)
CALL SYMBOL (18, YB, 81ZTIC, 15, TICANG, =1)
CONTINUE
GO TO 999

DRAW SUBDIVISION TICS LOG AXIS
IF(1 .GE. M1) GO TO 999
DO 305 J=2, 9, NUMTIC
TICLOG=DIVLEN*ALOS10(FLOAT(J))
IF(DELMUM .LT. 0) TICLOG= -TICLOG
XB=TIC*(TICLOG*COB1)
YB=TIC*(TICLOG*BIN1)
CALL SYMBOL (18, YB, 81ZTIC, 15, TICANG, =1)
CONTINUE
305
C
999 CONTINUE
C
DRAW AXIS LINE
CALL PLOT (XEND, YEND, 3)
CALL PLOT (X, Y, 2)
C
IF (N .EQ. 0) RETURN
IF(KIND .LT. 0) GO TO 1001
C
CENTER NORMAL TITLE
SIGN1=1.0
IF((THETA .EQ. 0.0) .OR. (THETA .EQ. 270.0)) SIGN1=-1.0
SIGN2=-SIGN1
IF((THETA .LT. 0.0) .OR. (THETA .EQ. 270.0)) SIGN2=SIGN1
SCOFF=(HEIGHT*(1.25*SIGN1)-0.5)*SIGN2
OFFCEN=0.5*(PLEN-(FLOAT(N)-0.5)*SCOBIZ)
IF((THETA .EQ. 180.) .OR. (THETA .EQ. -90.))
* OFFCEN=OFFCEN*(SCOBIZ*FLOAT(N))
XC=X+(OFFCEN*COB1)*(SCDOFF*BIN1)
YCY=Y+(OFFCEN*BIN1)*(SCDOFF*COB1)
CALL SYMBOL (XC, YC, SCOBIZ, 8CD, THET2, N)
RETURN
C
CENTER VERT. TITLE
THET3=90.0
IF((ABS(THETA) .EQ. 90.0) .OR. (THETA .EQ. 270.0)) THET3= 0.0
SIGN3=SIGN(THET3/57.2958)
COB3=COB1*(THET3/57.2958)
OFFCEN=(0.5*(PLEN-(FLOAT(N)*VRTSIZ)))*SCOBIZ
OFFCEN=OFFCEN*(COB3*(FLOAT(N)-2)*VRTSIZ)
SIGN3=1.0
IF((THETA .EQ. 0.0) .AND. (THETA .LT. 270.0)) SIGN3=-1.0
SCDOFF=HEIGHT*(1.25*SIGN3)-0.5
YCY=(OFFCEN*COB3)*(SCDOFF*BIN1)

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2300
2310
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2440

```
C  
      XCR1*(OFFCEN+SIN3)*(BCDOFF+COS3)  
      ZI=1  
      DO 1002 I=1,N  
      JCM=MOD(I,10)  
      IF(JCM.EQ.0) JCM=10  
      IRIGHT=NGETX (BCD(I),JCM,1)  
      LEFT  =NGPUTX (IRIGHT,LEFT,1)  
      CALL SYMON (IC,YC,BCOSIZ,LEFT,TIME3,1)  
      IF(MOD(I,10).EQ.0) I=I+1  
      XCR1C*(VRTSIZ+SIN3)  
      YC=YC-(VRTSIZ+COS3)  
      1002 CONTINUE  
      RETURN  
      END
```

```

1  PROGRAM ASOCC1 (INPUT,OUTPUT,TAPE1,TAPE2,TAPE3,TAPE5,INPUT,TAPE6=OUTPUT) 000100
   LOGICAL PR1,PR2,PR3,PR4
   COMMON /PLG3/ ITYPE,PR1,PR2,PR3,PR4,ISTOP
   COMMON /INPUT/ IDE1,IDE2
   CALL INIY
   CALL PR4
   5  IF(ISTOP .EQ. 1) STOP
   CALL INPUT
   CALL TRACK
   IELIYDE=61-60 IO 5
-10 REMIND IDEV2
   GO TO 5
   END
000147
000148
000149

```

```

1      SURROUTINE INIT      000170
      LOGICAL PR1,PR2,PR3,PR4,PR5,PR6      000171
      COMMON /FLGS/ ITYPE,PREI,PR2,PR3,PR4,ISTOP      000176
      COMMON /CNIRS/ IELSCN,IWLSCH,IJXZIS,MAXR,IJCLMX,IJOMIX,ICMPIX
5      COMMON /DATA/ WCL (13,100,3),ECL (10,200),IMVCL (25),ICMPL (10)      000185
      TEJBBAL,ORINE,100      000188
10     FORMAT (1X,'INI1')      000191
      ISTOP=0      000194
      IELSCN=0      000196
      IWLSCH=0      000197
10     DO 10 IX=1,3      000200
      DO 10 JX=1,100      000203
15     DO 10 KX=1,13      000206
      WCL(KX,IX,IX)=0.      000209
      RETURN      000210
      END      000212

```

1 BLOCK DATA 000270
LOGICAL /ERR1,ERR2,ERR,ERRA 000280
COMMON /DATA/ VOL(13,100,3),ECL(10,200),IMVCL(25),ICMPRL(10)
COMMON/ERRS/ INCL,INCL1,INCL2,INCL3,INCL4,INCL5,INCL6,INCL7,INCL8,INCL9,INCL10
5 COMMON /CNTRS/ IELSCN,IIVLSCN,IATR(5),MATE,IIVLWY,IMPWX,ICMPWX
COMMON/ANCL1/ ELANK,IOAL,IMM,MIN,ISEC
COMMON /FLGS/ ITYPE,PR1,PR2,PR3,PR4,ISTOP 000320
COMMON /IMPW1/ IDEK1,IDEK2 000330
DATA IATR(3,7,9,7,5)
DATA IIEZL1,INCLM/1014,IMDMX/254
DATA PR1,PR2,PR3,PR4,PR5,PR6,PR7,PR8,PR9,PR10
DATA IDEK1,IDEK2,IDEK3,IDEK4,IDEK5,IDEK6
DATA ICMPWX/10/
END
000350
000355
000357
000360

SUBROUTINE INPUT IN/ZA OPI=1 FTN A-66828 26/28/7A 12-58-52 PAGE 2

60 238 FORMAT(2X,'EOF REACHED ON TAPE1')
60 66 RETURN
60 END

000790
000800
000810

```

1  SUBROUTINE TRACK                                00020
COMMON /DATA/ VOL(13,180,3),ECL(13,200),IIVCL(12,5),ICMPRL(18)
COMMON /PTRS/ IVCL5,IIVCL5,IECLM,IVCLP,IVCLC,ICMPR
COMMON /CMRS/ IELSCM,IIVLSCM,IIECLM,IIVLCP,IIVLCC,ICMPM
COMMON /ANGC/ ELANG,ITAY,ITM,MIN,ISEC
COMMON /ELCS/ IIEBE,PRL,PB2,PB1
LOGICAL PRI,PR2,PR3,PR4
DATA PBD/317.51/
PRINT 430,ITYPE
IF(ITBE.NE.3) RETURN
400  FORMAT(IX,'TRACK',I7)
IELSCM=EQ.0.AND.IELSCM.EQ.01.ELANG.PD.
0  ASSUME VFL=30 W/SEC
VEL=.03
SINE=1/SIN(ELANG*PPI)
TANLSTAN=(ELANG*PPI)
COSPHI=COS(ELANG*PPI)
COSPHI2=COSPHI**2
PRINT 410,TANEL,COSPHI,COSPHI2,ELANG,ELANGP,IELSCM,IIVLSCM
410  FORMAT(IX,11X,F10.6),1X,F7.3),2I6)
IF(ELANGP.GT.ELANG) IELSCM=0
IF(ELANGP.LT.ELANG) GO TO 45
IELSCM=IELSCM+1
01010
IELSCM=EQ.1.AND.IIVLSCM.EQ.01.GOTO 5
01030
IF(ELSCM.EQ.1) GOTO 15
GOTO 25
0  INITIALIZE VOL. CELL TABLE POINTERS
5  IIVCL=1
IIVCL=1
IIVCL=1
IIVCL=1
0  ENTRY FOR FIRST SCAN OF NEW VOLUME SCAN
PRINT 420,IECLM
420  FORMAT(IX,'TRACK',I6)
15  DO 13 JX=1,IECLM
0  INITIAL CELLS
C  CALCULATE SURFACE COORDINATES
I=(IDAY*24+IMH)*60+IMIN*60+ISEC
Y=EQ(1,JX)*COSPHI
Z=EQ(1,JX)*COSPHI
M=SI*ANGL
VOL(1,IIVCL,ITYPE)=X5
VOL(2,IIVCL,ITYPE)=X5
VOL(3,IIVCL,ITYPE)=R5
VOL(4,IIVCL,ITYPE)=M
VOL(5,IIVCL,ITYPE)=ECL(2,JX)
VOL(6,IIVCL,ITYPE)=EQM
VOL(7,IIVCL,ITYPE)=IMR
VOL(8,IIVCL,ITYPE)=MIN
VOL(9,IIVCL,ITYPE)=ISEC
VOL(10,IIVCL,ITYPE)=ECL(2,JX)*COSPHI
VOL(11,IIVCL,ITYPE)=ECL(1,JX)
VOL(12,IIVCL,ITYPE)=ECL(2,JX)
N=1
IF(PB2) PRINT 300,JX,IIVCL5,IIVCL5,IIVCL5,KU=1,13
0  CHECK FOR OVERFLOW OF VOL
01130
01130

```

60	IVCL=IVCL+1 IF(IVCL=16, IVCL=1) GOTO 11 PRINT 310 IVCL=IVCL+1	001350 001360 001370 001380 001390 001400
65	310 FOR=172Y, VCL LIMIT REACHED 11 CONTINUE C MOVE UP VCL SEGMENT PNR(ENP) IVCL=IVCL+1 FLANG=ELANG IF(ENP) PRINT A30, IVCL, IVCL, IVCL 1-10, IX, IY, IZ, IZ	001410 001420 001430 001440 001450 001460
70	60Y 100 C ASSOCIATE ELEV. CELLS TO BUILD VOL CELLS 25 PRINT *35 A35 FORMAT(IX, *ASSOC. EL. CELLS) DO 40 JX=1, IECLM I2=((IDAY*24+IHR)*60+IMIN)*60+ISEC DIZ=I2	001470 001480 001490 001500 001510 001520
75	ELKS=ECL(3, JX)*COSPHI ELYS=ECL(6, JX)*COSPHI PS=SQRT((ELXS*ELYS)+(ELYS*ELYS)) IX=PS*IX AREAS=ECL(2, JX)*COSPHI ICMPRS=1 DO 305 IX=1, ICMPIX ICMQR=IX+8 IF(OR3) PRINT 450, 2MEL, JX, ELYS, ELXS, RS, MT, AREAS FORMAT(IX, A2, IX, 2E12, IX, IX, SE12, A)	001530 001540 001550 001560 001570 001580 001590 001600 001610 001620
80	DO 70 IX=IVCLP, IVCLC VCLRS=SQRT(VCL(18, IX, IY, IZ)+VCL(18, IX, IY, IZ)+VCL(18, IX, IY, IZ)) YS1=VCL(1, IX, IY, IZ) YS2=VCL(2, IX, IY, IZ) YS3=VCL(3, IX, IY, IZ)	001630 001640 001650 001660 001670 001680 001690 001700
85	IF(OR4) PRINT 500, IX, VCLDIS, YS2, YS1, YS2, YS1 FORMAT(IX, IX, IX, SE12, A) IF(ELXS .LT. YS1 .OR. E.XS .GT. YS2) GOTO 30 IF(ELYS .LT. YS1 .OR. E.YS .GT. YS3) GOTO 30 C COMPARE-INSERT VCL INDEX INTO ICMPLR LIST ICMQR=ICMQR+1 IF(ELXRS .LE. ICMQR) GOTO 301 ERR=2 ICMPRS=ICMPRS 301 CONTINUE 30 CONTINUE	001710 001720 001730 001740 001750 001760 001770 001780 001790 001800
100	ICMQR=ICMQR+1 IF(ELXRS .LE. ICMQR) GOTO 301 ERR=2 ICMPRS=ICMPRS 301 CONTINUE 30 CONTINUE KX2=2 IF(ELXRS .LE. ICMQR) GOTO 301 IF(ELXRS .LE. ICMQR) GOTO 301 GOTO 35 301 CONTINUE 302 ICM=ICMPLR(KX2) I1=VCL(1, ICMQR, IY, IZ) I2=VCL(2, ICMQR, IY, IZ)	001810 001820 001830 001840 001850 001860 001870 001880 001890 001900 001910 001920 001930 001940 001950 001960 001970 001980 001990 002000


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02050 IF(IHVCL5 .LE. IIMDY)GOTO 52
02060 PRINT 588,IMDMX
02070
02080
02090
02100
02110
02120
02130
02140
02150
02160
02170
02180
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1  SUBROUTINE PRM
   LOGICAL PR1,PR2,PR3,PR4
   COMMON /FLGS/ ITYPE, PR1, PR2, PR3, PR4, ISTOP
   COMMON /INPUT1/ IOE1, IOE2
5  NAMELIST /PARAM/ PR1, PR2, PR3, PR4, IOE1, IOE2, ISTOP
   PRINT *, IOE1
10  FORMAT (IX, *INPUT ...PR1, PR2, PR3, PR4, IOE1, IOE2, I(TOP*))
   READ(*,PARAM)
   IF(EOF(5)) 15, 3
10  3  WRITE(*,PARAM)
   GOTO 20
15  PRINT *, IOE1
10  FORMAT (IX, *EOF ON UNIT 5*)
20  RETURN
15  END

```

FMA OF THE LOAD 111
 LMA+1 OF THE LOAD 227071
 TRANSFER ADDRESS -- EXTRAD 16574

PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROGSSK	PER	LEVEL	MARK	MARKRE	COMMENTS
/PRNH/	111	64								
EXTRAD	175	14506	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
/INSUB/	16703	24								
/I2M/	16727	720								
/AI02N7/	15847	6000								
/VALHA/	23647	13								
/ADATA/	23562	10								
/HEAD/	23672	15								
/LTDUM/	23707	1								
/MGRED/	23710	5								
/STOPE/	23735	7								
/EJPN/	23724	10								
/ERRDP/	23734	1								
/FILPEP/	23735	3								
/HELPEM/	23740	1								
/QUANTX/	23741	3								
/PWORX/	23744	22158								
/FIXEO/	46114	3413								
/RESTOPE/	51527	31576								
/PWSOPE/	103425	30212								
/RSTOPE/	133537	25525								
/REFL/	162365	1272								
BCVORT.	163557	172	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
/LOOKUP/	163657	172								
INPAP	164951	460	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
/VEL/	164531	2550								
/A22/	167301	5								
EXTRAT	167306	1136	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
COMP7	170444	1555	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
CONTR	17221	11803	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
PELKO	203524	4270	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
/MCKVAL/	210014	6								
YJPK	210022	103	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
IPK	210125	104	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
PTANG	210231	50	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
PN2	210311	362	LGO	05/04/78	FTN	4.6	428	666X	I	OPT=2
PRC	210573	33	UL-ERTLIB	02/16/78	FTN	4.6	428	666X	I	OPT=1
LINES	210726	44	UL-ERTLIB	02/16/78	FTN	4.6	428	666X	I	OPT=1
DAY	211772	10	UL-ERTLIB	02/16/78	FTN	4.6	428	666X	I	OPT=1
ERX	211802	25	UL-ERTLIB	02/16/78	FTN	4.6	428	666X	I	OPT=1
INE	211827	125	UL-ERTLIB	02/16/78	FTN	4.6	428	666X	I	OPT=1
/STP.END/	211154	1								
/FCL.G./	211155	23								
/P.LO./	211200	133								
COMPBY=	211333	0	SL-FORTRAN	04/12/77	COMPASS	3.	3-428			FCL INITIALIZATION ROUTINE.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR	VER	LEVEL	HARDWARE	COMMENTS
BUFTN=	211333	46	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		BUFFERED INPUT PROCESSOR.
FECHSK=	211401	41	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		INITIALIZE CONSTANTS.
FLROUTE	211452	311	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMMON FLOATING OUTPUT CODE
FOPSYS=	211753	603	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		FORTRAN OBJECT LIBRARY UTILITIES.
INCONE	212556	276	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMMON INPUT FORMATTING CODE
INDC=	213054	160	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		FORMATTED HEAD FORTRAN RECORD.
KORER=	213234	456	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		OUTPUT FORMAT INTERFERER.
NAMOUT=	213712	274	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		NAMELIST OUTPUT ROUTINE.
214206	227								
OUTB=	214435	203	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		BINARY WRITE FORTRAN RECORD.
OUTCOM=	214500	154	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMMON OUTPUT CODE
REWLND=	215014	37	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		POSITION FILE AT BEGINNING-OF-INFO.
UNIT	215053	50	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		STATUS OF BUFFER I/C FILE.
CLOCK=	215123	31	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		ACCESS SYSTEM CLOCKS FOR FORTRAN.
FORTEPE	215154	14	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMPUTED GO TO ERROR PROCESSOR.
ALOC	215170	73	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMPUTE COMMON AND NATURAL LOGARITHMS. OPT=ALL.
EXP	215263	75	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		EXPONENTIAL FUNCTION. E TC POWER X. OPT=ALL.
ITOU=	215360	16	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		INTEGER TO INTEGER EXPONENTIATION.
SYNGOS=	215376	66	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		TRIGONOMETRIC SINE OR COSINE OF X. OPT=ALL.
SYSDIO=	215464	1	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		LINK BETWEEN SYS-AID AND INITIALIZATION CODE.
POPIC=	215465	125	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMMON SET-UP ROUTINE FOR BUFINP/BOPOUT.
COMIC=	215512	64	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMMON CODED I/O ROUTINES AND CONSTANTS.
FOF	215575	16	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		TEST FOR END OF FILE STATUS.
FLTN=	215714	154	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMMON FLOATING INPUT CONVERTER.
FRTPE=	216370	352	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		CRACK APLIST AND FCMAT FOR KCODE/KRAKER.
FOUTL=	216442	16	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		FOR MATH UTILITIES.
GFPLTE	216520	42	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		CREATE EN FIT GIVEN A FILE NAME.
KRAKER=	216522	406	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		PROCESS FORMATTED FORTRAN INPUT.
NAMINE	217130	523	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		NAMELIST INPUT ROUTINE.
OUTC=	217653	172	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		FORMATTED WRITE FORTRAN RECORD.
SORT	220045	43	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		COMPUTE THE SQUARE ROOT OF X. OPT=ALL.
SYSDST	220110	62	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		MATH LIBRARY LINK TO ERROR MESSAGE PROCESSOR.
TYOVS	220172	7	SL-FORTRAN	05/12/77	COMPASS	3.	3-428		REAL TO REAL EXPONENTIATION.
SDF.S0	220201	2	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
FCOR.PM	220203	5							
CIO.PM	220211	40	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
TAOS.PM	220251	10							
MOVE.PM	220261	64	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
ACT.PM	220345	233	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CHEK.P4	220360	107	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
OSUB.PM	220707	71	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
JMPS.PM	221000	11							
OPEN.F0	221011	7							
OPEN.S0	221020	254	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
OPEN.S0	221274	14	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
PUT.PM	221310	11							
PLEG.PM	221321	42	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CLSF.F0	221363	7							
CLSF.S0	221372	134	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
CLSM.F0	221526	7							
CLM.S0	221535	137	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
REM.F0	221674	7							
PEH.S0	221703	33	SL-SYSIO	05/03/76	COMPASS	3.	2-414		
TEMP.PM	221736	1							
GET.F0	221737	7							

LOAD MAP - EXTRAD	CP SECONDS	CM STORAGE USED	PROCESS SYSTEM REQUEST
GET.BY/	221746		
GET.RY/	221753		
GET.S0	221764	1134 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
Z.S0	223120	101 SL-SVSIO 09/03/76 COMPASS 3. 2-414	
F50.S0	223221	106 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
SKFL.FD/	223327	7	
SKSF.FD/	223336	1	
SKSE.S0	223337	50 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
SKRBL.FD/	223407	7	
SKSB.FD/	223416	1	
SKSB.S0	223417	101 SL-SVSIO 09/03/76 COMPASS 3. 2-414	
ERR.PH	223520	404 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
CHRP.S0	224124	7 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
MEMC.GM/	224133	3	
TOPES.FD/	224136	1	
OPEN.PM	224137	237 SL-SVSIO 09/03/76 COMPASS 3. 2-414	
OPES.S0	224176	121 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
PUT.FD/	224517	7	
PUT.S0	224526	1600 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
WAR.S0	226126	260 SL-SVSIO 09/03/76 COMPASS 3. 2-414	
CLSF.PH	226406	25 SL-SVSIO 09/03/76 COMPASS 3. 2-414	
GTMR.S0	226433	41 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
BTPF.S0	226474	115 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
MEMO.S0	226611	150 SL-SVSIO 09/03/76 COMPASS 3. 2-414	
SKFL.S0	226751	51 SL-SVSIO 03/03/76 COMPASS 3. 2-414	
SYS.RR	227032	37 SL-NUCLEUS 04/15/77 COMPASS 3. 2-414	

1.348 CP SECONDS 2437093 CM STORAGE USED 129 TABLE MOVES

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PARA

\$INPUT
 PRINT1 = F,
 PRINT2 = F,
 PRINT3 = F,
 COPLOT = T,
 ICOCES = -329406144173304950, 30091026016254029, 4099622425736413, 66910623035219797, 04525021544700781, 102939420954102765,
 120953318563664749, 136960217073146733, 156902615802620717,
 211025011111074669, 22904209529556653, 247054608130030637,
 301097003650444509, 319112202167966573, 33712660067444557,
 391169786205994509, 40918194715376493, 4271905922465877,
 481241780753304429, 51727048972268397, 535294984261759381,
 -563593324796650642, -545578926257168633, -527564527777686674,
 XI = .443E+00,
 BI = .56E+00,
 AZ = .86E+00,
 BZ = .186E+02,
 CONTRZ = I,
 CONTRV = I,
 CONTRS = I,
 WHILE = U,
 WOHF = 30,
 AC = -.10776555E+03, .19767838E+01, -.3929723E-01, .10226310E-03,
 CALM = .332E+00,
 CALB = -.983E+02,
 XCOT = .1E+02,
 CK = .1E+02,
 ZHAX = 0.0,
 VHRX = 0.0,
 NREC = 1,
 WOHF = 99999,
 TKON = 0,
 INC = 0,
 TT =

.TOW = 0.0,
 .DN = 0.0,
 .STARTM = .2E+02,
 .STOPR = .15E+03,
 .IMPRF = 7%,
 .SCALE = .1E+01,
 .XE = .121E+01,
 .XA = .6E+03,
 .BB = .16E+01,
 .XI = 0.0,
 .XZ = .0E+01,
 .YI = 0.0,
 .YZ = .0E+01,
 .YV = 35,
 .TSA = 1000000,
 .LDA = 3,
 .LYO = 3,
 .LSA = 3,
 .ICOMP = 5,
 .VMIN = 0.0,
 .SYMZN = 0.0,
 .MPCANN = .1E+01,
 .WAVEL = .562E-01,
 .VOLUME = .1E+02,
 .SOURNT = .5E+01,
 .RBOUNT = .1E+01,
 .VOLTRP = 1,
 .DASH = .1E+01,
 .ESTART = .15E+01,
 .DELY = .5E+00,
 .RENO

162 0 PROGRAM EXTRAD VERSION 2.0 (700501) 05/04/76 PAGE 2
EXEC NO OF RECORDS/RNDIAL 6 CELL WIDTH 937.2 METERS PRF 795.0

FIXED CONTOUR ATTRIBUTES

DAY MMH 55 ELE AZM1 AZM2
 226 1333 40 1.2 118.2 116.2

THRESHOLD	AREA	REFLECTIVITY	EAST	LOCATION	RANGE	RESOLUTION	PRECIP	TOTAL	AVERAGE	PRECIP	COMTOR	FIXED
(DBZ)	(KM ²)	(DBZ)	(KM)	(KM)	(KM)	(KM)	(MM/HR)	(MM/HR)	(MM/HR)	(MM/HR)	REFERENCE	
1	20	1.27	26.1	12.6	-15.7	28.1	3.3	1.22	.96	-4		
2	20	1.85	32.3	15.8	-19.3	27.7	4.1	6.72	2.56	2		
3	20	2.34	35.9	14.6	-18.3	23.9	5.0	18.48	4.44	5		
4	20	1.95	29.6	22.3	-33.1	39.9	2.8	3.86	1.88	6		
5	20	3.95	21.0	-36.7	-47.8	68.5	3.3	1.69	.44	10		
6	20	6.68	21.6	-37.9	-53.7	89.7	5.1	6.22	.63	9		
7	20	3.30	36.0	-18.4	-13.7	23.0	8.4	13.00	3.93	11		
8	20	3.61	38.3	-18.8	-9.7	21.1	9.3	5.88	1.72	-12		
9	20	14.93	25.5	-132.1	-67.3	144.5	6.1	13.15	.86	-13		
10	20	6.88	28.8	-36.7	-33.3	38.9	10.8	3.86	1.89	20		
11	20	8.14	34.0	-35.1	-10.3	36.6	13.5	26.21	3.22	19		
12	20	1.40	21.0	-64.5	-26.3	88.5	1.8	.61	.44	21		
13	20	326.28	36.0	-127.6	-44.5	135.1	419.8	354.87	3.82	-18		
14	20	2.89	31.6	-37.0	.5	37.8	6.3	5.26	1.82	25		
15	20	2.15	21.0	-147.8	-22.5	149.5	.9	.94	.44	-27		
16	20	328.32	28.1	-173.3	11.3	68.3	292.8	259.34	.79	34		
17	20	25.33	41.7	-132.3	6.7	132.4	11.7	21.86	.94	31		
18	20	397.33	41.0	-55.4	22.1	33.7	721.8	435.85	18.35	36		
19	20	10.18	41.0	-33.3	9.4	34.4	16.0	34.26	5.34	35		
20	20	2.08	21.0	-54.5	11.7	55.8	2.3	.91	.44	37		
21	20	9.11	24.7	-182.7	24.5	105.6	5.3	7.84	.77	38		
22	20	2.29	21.0	-123.7	31.3	32.6	1.1	1.88	.44	39		
23	20	2.50	21.0	-140.6	34.7	144.8	1.1	1.05	.44	40		
24	20	3.53	21.0	-126.7	34.7	129.3	1.7	1.55	.44	41		
25	20	9.42	22.7	-118.6	48.1	142.4	4.0	5.44	.58	42		
26	20	2.88	24.0	-133.4	39.3	135.2	1.2	2.11	.72	43		
27	20	1.49	21.0	-83.8	26.3	66.3	1.3	.65	.44	44		
28	20	1.96	37.6	-25.6	12.3	25.5	2.2	5.39	5.02	45		
29	20	4.30	21.5	-114.1	96.5	149.5	1.8	2.83	.47	-46		
30	20	2.24	22.0	-83.2	73.5	111.1	1.2	1.15	.52	47		
31	20	2.89	27.4	-51.3	51.4	72.6	1.8	2.61	1.25	48		
32	20	4.15	21.0	-76.5	76.3	108.8	2.5	1.84	.44	49		
33	20	4.24	21.0	-84.1	123.3	149.0	1.8	1.88	.44	-51		
34	20	1.84	24.0	-32.6	38.3	58.4	1.1	.75	.72	52		
35	20	31.27	24.2	-75.1	126.1	146.7	13.0	22.54	.72	-53		
36	20	3.94	22.0	-83.2	78.3	98.0	6.1	4.55	.51	54		
37	20	9.85	23.2	-69.1	64.3	101.5	5.4	5.63	.62	55		
38	20	1.66	22.0	-45.8	94.4	95.1	1.1	.86	.52	56		
39	20	118.95	29.7	-34.8	69.1	95.4	76.3	135.94	1.56	57		
40	20	2.51	21.5	-35.2	79.3	87.2	1.3	1.21	.48	58		
41	20	34.65	32.4	-27.4	70.7	75.8	28.0	88.01	2.54	59		
42	20	1.33	21.8	-7.2	18.5	28.1	4.0	.66	.58	-61		
43	20	1.52	21.0	-24.3	32.3	36.1	1.0	.67	.64	61		
44	20	77.46	25.0	-4.7	38.8	38.3	123.3	63.75	.52	62		
45	20	1.30	21.5	-3.2	19.3	29.1	4.0	.62	.48	-63		
46	20	14.45	21.7	-9.0	62.3	13.4	13.9	7.83	.49	64		
47	20	8.95	23.4	-15.2	93.8	94.4	5.8	5.78	.65	65		
48	20	5.75	22.1	-14.5	89.3	91.0	3.3	3.01	.52	66		
49	20	3.97	21.8	-3.3	62.7	62.8	3.3	1.97	.50	67		
50	20	1.55	25.2	-3.3	33.3	23.2	1.1	2.75	1.77	68		
51	20	2.98	21.6	3.8	22.3	22.8	8.0	1.45	.49	70		

58	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
59	99.1	125.63	3.29	3.29	9.82	5.51	4.54	15.55	4	6
60	98.1	11	7.98	3.6	9.82	5.51	4.54	9.82	4	8
61	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
62	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
63	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
64	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
65	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
66	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
67	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
68	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
69	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
70	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
71	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
72	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
73	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
74	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
75	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
76	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
77	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
78	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
79	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
80	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
81	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
82	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
83	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
84	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
85	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
86	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
87	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
88	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
89	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
90	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
91	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
92	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
93	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
94	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
95	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
96	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
97	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
98	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
99	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11
100	72.7	10.53	1.21	1.22	7.02	5.55	5.22	8.53	8	11

WIND DATA

DAY HMMH SS ELE AZM1 AZM2
 226 1933 60 1.2 118.2 118.2

HEIGHT (TRM)	AVERAGE REFLECTIVITY (DBZ)	TOTAL REFLECTIVITY (DBZ)	AVERAGE VELOCITY (M/SEC)	AVERAGE # (M/SEC)	VELOCITY VARIANCE (M/SEC ²)	DEL
1	22.0	67.3	0.0	0.0	112.4	-.64409E-15
2	27.1	9289.0	12.6	-18.1	60.3	-.57697E880
3	35.0	671779.4	5.1	-10.1	61.0	-.39223E801
4	31.0	219615.2	-38.6	26.8	76.6	-.21589E-871
5	23.4	21683.5	-5.0	-8.5	69.9	-.80681E801
6	28.1	75385.5	-7.1	-7.9	91.8	-.94582E880

PEAK DEFLECTED CELL ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
 226 1933 40 1.2 118.2 118.2

ID	REFLECTIVITY (DBZ)	AREA (KM*2)	LOCATION EAST NORTH (KM)	RANGE (KM)	RESOLUTION ELEMENTS	AVERAGE VELOCITY SPEED (M/S)	AVERAGE RADIAL SHEAR (M/S/KM)	AVERAGE TANGENTIAL SHEAR (M/S/KM)	AVERAGE RADIAL VELOCITY (M/S)	FIXED CONTOUR REFERENCE	MEAN
1	32.5	5.8	110.9	-44.5	119.5	2.8	1.93	.05	-4.54	12	12
2	44.0	6.3	124.1	-48.8	133.6	3.2	2.45	-.21	-3.13	18	18
3	51.5	6.5	135.2	-37.3	143.8	1.9	1.78	-1.35	-4.10	12	12
4	41.5	13.8	151.3	-36.8	187.4	7.4	1.60	-.32	-3.46	12	12
5	48.0	2.4	131.9	-44.3	139.2	1.1	1.83	-.84	-.20	10	10
6	37.6	1.8	151.1	-11.8	37.0	3.0	1.34	.14	0.00	15	15
7	41.0	8.3	132.6	-35.5	137.3	3.7	2.07	.88	-1.78	18	18
8	41.0	4.2	142.4	-36.9	147.1	1.8	1.58	.45	-.35	18	18
9	37.8	5.5	139.3	-38.5	143.5	2.8	1.98	-.28	-.41	12	12
10	33.5	5.8	143.2	-29.5	145.2	2.1	.92	-.54	-2.35	12	12
11	38.1	18.5	129.4	-23.7	131.5	5.8	1.81	.13	-3.17	18	18
12	25.0	2.1	134.5	2.5	134.5	1.0	0.80	1.32	0.00	31	31
13	32.8	2.7	132.4	6.3	132.6	1.2	.50	1.11	-2.30	31	31
14	27.0	3.5	182.6	24.4	185.4	2.1	.33	-.37	-2.50	30	30
15	27.5	35.1	159.1	14.5	157.5	31.7	1.20	-.82	-3.45	34	34
16	22.5	9.4	135.7	40.0	142.4	4.0	.75	.55	-1.15	42	42
17	25.8	2.8	133.4	39.8	139.2	1.2	.17	0.00	-1.50	43	43
18	43.5	1.5	135.6	13.2	36.0	2.5	2.20	-1.82	-3.63	36	36
19	48.0	1.3	134.4	15.4	37.7	3.2	1.54	.64	-2.73	36	36
20	49.6	9.8	126.0	20.0	33.5	17.8	1.74	-.13	-.26	35	35
21	27.4	7.1	151.3	31.8	72.5	1.8	.43	0.00	0.00	42	42
22	51.0	1.7	123.2	25.6	34.5	5.1	1.50	-1.11	-2.22	36	36
23	27.0	6.3	144.2	125.5	145.7	2.3	.61	-.37	-5.03	53	53
24	24.5	3.7	163.4	89.9	101.7	2.2	.64	-.19	-9.73	55	55
25	25.0	1.4	137.5	79.3	88.6	1.0	.57	0.00	-9.80	54	54
26	45.0	1.5	121.3	30.6	33.0	3.0	.74	-.34	-9.92	36	36
27	38.8	2.8	128.0	78.8	75.3	1.7	.92	-.48	-10.25	53	53
28	38.4	4.8	132.5	84.9	94.8	3.1	1.21	-.53	-10.16	57	57
29	28.5	1.1	147.7	32.1	33.3	1.3	1.08	-.27	-11.60	36	36
30	25.5	2.4	140.1	36.6	38.0	3.3	.75	-.16	-12.13	36	36
31	28.3	5.0	146.3	53.8	34.4	3.3	.88	.03	-11.57	65	65
32	22.0	5.7	144.5	84.8	90.9	3.9	.29	-.12	-11.75	66	66
33	28.3	9.4	154.5	40.3	43.7	15.2	1.05	-.10	-12.74	62	62
34	25.9	5.8	144.5	40.2	44.5	9.1	1.37	-.32	-12.23	62	62
35	28.0	1.1	134.4	39.5	41.7	1.7	1.65	-.51	-15.13	73	73
36	25.5	13.4	145.0	106.2	116.9	7.2	.64	-.00	-6.93	74	74
37	25.8	7.3	137.7	87.6	97.7	5.5	1.35	.11	-6.61	78	78
38	26.8	5.3	147.8	91.8	103.5	3.7	1.35	-.22	-7.23	72	72
39	21.5	33.7	114.8	182.1	182.1	9.3	1.61	.65	-7.21	51	51
40	25.8	12.4	144.7	97.0	111.4	12.3	1.26	-.34	-7.05	76	76
41	31.9	11.5	172.2	64.9	74.3	9.5	1.13	-.36	-4.42	82	82
42	37.0	1.1	149.7	56.4	74.5	.9	1.67	-.53	-2.40	85	85
43	37.5	5.9	145.1	53.7	75.2	5.8	1.67	-.23	-6.13	85	85
44	41.8	7.7	144.5	63.4	81.3	5.8	2.19	-.42	-2.70	85	85
45	34.8	2.3	181.5	136.7	147.5	1.8	2.83	-.11	-11.70	90	90
46	25.5	3.9	188.5	86.4	121.7	1.9	1.83	-.30	-9.15	85	85
47	32.5	5.3	171.2	68.5	98.9	3.9	2.79	1.03	-7.37	85	85
48	27.9	23.7	177.0	134.4	134.4	11.5	1.56	.44	-11.67	85	85

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HMMH SS ELE AZM1 AZM2
226 1933 40 1.2 118.2 118.2

ID	MAGNITUDE (M/S/KM)	LOCATION			RANGE (KM)	RESOLUTION ELEMENTS	AREA VELOCITY SPREAD (M/S)	AVERAGE SHEAR (M/S/KM)	FIXED CONTOUR REFERENCE
		AREA (KM**2)	EAST (KM)	NORTH (KM)					
1	1.7	2.3	-132.0	-57.1	164.3	1.0	1.3	1.7	15
2	1.8	2.1	-125.2	-51.6	135.4	1.0	2.3	1.6	16
3	1.8	2.4	-126.9	-51.6	137.7	1.9	2.4	1.8	18
4	1.5	1.9	-111.3	-45.9	128.4	1.0	1.9	1.5	18
5	1.8	2.8	-129.5	-53.4	148.1	3.0	2.7	1.5	16
6	2.6	1.6	-101.5	-37.7	108.2	.9	1.3	2.6	18
7	2.7	1.6	-105.8	-39.0	112.9	.9	2.0	2.7	18
8	2.4	3.3	-107.2	-39.9	114.4	1.8	2.0	2.4	18
9	1.8	3.5	-117.7	-43.8	125.5	1.8	.5	1.8	16
10	.5	9.4	-97.6	-35.4	103.1	5.5	1.2	.5	16
11	2.0	2.2	-132.9	-47.1	141.0	1.0	1.6	2.0	18
12	1.2	4.7	-128.0	-42.9	135.3	2.1	1.5	1.2	18
13	1.5	1.7	-102.3	-32.3	107.3	1.0	1.2	1.5	18
14	.5	1.6	-95.2	-30.0	99.3	1.0	2.3	.5	18
15	1.9	2.2	-135.5	-42.4	141.3	1.0	3.2	1.9	18
16	2.2	1.8	-100.2	-29.7	104.5	1.1	0.0	2.2	18
17	1.1	2.3	-129.8	-38.5	135.5	1.1	2.3	1.1	18
18	1.3	4.4	-134.6	-37.3	139.7	1.9	2.5	1.3	18
19	1.9	1.5	-98.8	-25.1	96.2	1.0	0.0	1.9	18
20	1.1	2.1	-139.3	-36.0	143.3	.9	1.7	1.1	18
21	.8	2.5	-142.2	-31.9	145.7	1.0	2.7	.8	18
22	.3	11.7	-137.4	-29.1	140.5	5.1	1.5	.3	18
23	.8	2.0	-124.8	-23.4	127.3	1.0	1.5	.8	18
24	.9	4.6	-143.7	-27.0	146.2	1.9	0.0	.9	18
25	.5	7.8	-131.4	-20.6	133.3	3.6	2.5	.5	18
26	.9	2.2	-128.6	-17.7	129.1	1.1	0.0	.9	18
27	.9	2.2	-125.8	-17.3	127.3	1.1	0.0	.9	18
28	.5	6.0	-66.1	3.4	66.2	3.7	1.7	.5	34
29	1.0	6.2	-131.4	9.7	131.7	2.9	0.0	1.0	31
30	.4	3.1	-69.2	5.4	69.4	2.7	1.4	.4	34
31	.3	3.4	-68.4	5.4	68.5	3.4	1.7	.3	34
32	.4	6.7	-67.5	8.8	68.3	6.0	1.4	.4	34
33	.8	1.0	-97.3	18.0	98.2	1.1	1.8	.8	34
34	.3	2.0	-75.4	13.2	76.5	1.6	1.3	.3	34
35	.3	3.2	-68.9	12.6	78.1	2.8	1.1	.3	34
36	.9	1.0	-57.8	14.3	59.7	1.1	1.7	.9	34
37	1.8	1.8	-102.4	29.3	105.4	1.1	.7	1.8	38
38	.3	12.3	-67.4	18.0	69.3	10.7	1.3	.3	34
39	.9	5.7	-136.5	40.7	142.4	2.5	0.0	.9	42
40	.6	2.8	-76.2	76.9	108.2	1.1	.3	.6	49
41	.3	6.7	-76.5	127.7	148.5	1.9	.3	.3	53
42	1.1	1.1	-17.2	29.0	33.7	1.9	.4	1.1	36
43	.2	7.7	-72.4	126.0	155.3	3.3	.7	.2	53
44	.4	3.5	-46.3	69.0	81.2	2.1	.5	.4	55
45	.5	2.7	-19.5	37.6	42.3	3.9	.8	.5	36
46	.6	2.4	-27.6	69.7	75.0	1.9	1.1	.6	59
47	.7	1.6	-32.9	87.2	93.2	1.1	.8	.7	57
48	.5	1.5	-38.1	89.2	94.2	1.0	.8	.5	57
49	.2	7.3	-23.7	72.8	76.5	5.8	1.5	.2	55
50	.5	1.4	-13.7	89.4	90.4	1.8	0.8	.5	66

51	4	1.4	-7.6	64.7	65.1	1.0	1.0	-1.4	64
52	4	1.4	-4	41.2	41.2	2.1	2.1	-1.6	62
53	8	2.1	1	35.8	34.8	3.7	3.7	-1.8	62
54	2.4	1.7	39.8	91.9	99.8	1.1	0.0	-2.4	78
55	1.6	1.8	39.8	93.6	101.7	1.1	1.1	-1.5	78
56	9	1.5	42.3	94.5	103.6	9	1.3	-1.9	78
57	1.5	1.6	46.1	103.1	112.9	9	9	-1.9	78
58	8	3.4	48.6	95.1	106.3	1.9	1.0	-1.8	78
59	8	1.4	47.8	88.9	108.7	9	1.3	-1.6	78
60	9	1.7	56.6	106.3	120.4	9	9	-1.9	78
61	9	3.5	54.6	114.7	118.1	1.8	1.0	-1.9	78
62	2.1	2.9	44.6	85.6	96.5	1.8	1.3	-2.1	78
63	3.1	1.4	39.6	71.0	82.3	1.1	1.3	-3.1	81
64	1.1	2.1	53.1	92.1	106.4	1.2	1.2	-1.1	78
65	2.7	1.3	56.6	93.4	109.2	9	0.0	-2.7	78
66	2.5	1.3	57.5	95.0	111.1	9	0.0	-2.5	78
67	3.3	1.1	48.1	58.1	64.2	1.1	2.7	-3.3	85
68	3.6	1.3	46.8	57.4	73.6	1.1	1.7	-3.6	85
69	2.9	1.1	38.9	88.7	82.3	1.1	0.0	-2.9	85
70	2.8	1.4	52.4	63.1	82.4	1.1	2.7	-2.8	85
71	3.4	1.3	48.2	58.0	75.4	1.1	1.7	-3.4	85
72	3.9	1.8	45.6	52.9	63.3	9	2.0	-3.9	85
73	1.2	1.6	55.8	62.7	83.3	1.1	1.3	-1.2	85
74	7	5.4	96.5	108.5	145.2	2.3	1.8	-1.7	90
75	9	2.7	64.3	89.4	94.5	1.8	2.5	-1.9	85
76	4.4	1.0	48.1	51.9	70.5	9	0.0	4.4	85
77	1.2	2.9	68.1	73.6	100.3	1.8	1.3	-1.2	85
78	1.2	1.1	50.6	54.7	74.5	9	2.2	1.2	85
79	1.0	1.5	69.7	78.3	102.5	9	1.0	-1.0	85
80	3.5	1.3	56.6	59.3	82.1	1.0	2.3	3.5	85
81	9	6.7	61.9	83.6	90.3	4.6	1.2	-1.9	85
82	3.1	1.3	55.0	55.7	78.3	1.1	0.0	-3.1	85
83	2.8	1.3	53.7	54.3	76.4	1.1	1.0	-2.8	85
84	1.1	3.2	67.6	69.5	97.0	2.0	2.8	-1.1	85
85	2.9	1.3	68.7	59.2	84.5	1.8	1.0	-2.9	85
86	1.1	1.7	76.1	74.3	106.4	1.0	2.5	1.1	85
87	1.1	5.6	84.9	82.8	118.3	2.9	9	-1.1	85
88	1.8	1.4	63.7	68.1	87.5	1.0	9	-1.8	85
89	1.5	1.5	67.8	64.0	93.2	1.0	0.0	-1.5	85
90	1.8	4.0	92.0	86.8	126.5	1.9	0.0	-1.8	85
91	1.9	2.0	93.7	88.4	128.3	1.0	0.0	-1.9	85
92	1.7	2.1	96.5	91.0	132.6	1.0	0.0	-1.7	85
93	1.7	2.2	99.2	93.6	136.4	1.0	1.0	-1.7	85
94	2.8	1.6	75.8	69.1	102.6	1.0	2.3	-2.8	85
95	2.3	1.6	73.1	66.6	98.3	1.0	1.0	-2.3	85

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY MONTH SS ELE AZM1 AZM2
276 1933 40 1.2 116.2 116.2

ID	SPREAD (MHz)	AREA (km ²)	EAST (km)	NORTH (km)	RANGE (km)	RESOLUTION ELEMENTS	AREA ELEMENTS	FIXED CONTOUR REFERENCE
1	1.2	1.6	14.1	-15.3	23.9	6.0	5	5
2	1.7	1.5	-36.1	-51.4	52.8	1.6	9	9
3	1.9	2.8	-38.5	-53.7	66.0	2.5	6	6
4	1.3	2.9	-131.9	-188.2	148.5	1.1	13	13
5	2.2	1.9	-122.4	-171.9	135.4	.9	18	18
6	1.5	4.5	-117.7	-153.5	129.3	2.1	13	13
7	2.9	9.9	-129.0	-195.8	140.5	3.9	18	18
8	1.8	2.8	-115.7	-150.0	126.8	1.8	18	18
9	2.2	1.6	-103.5	-142.7	112.0	1.0	16	16
10	1.3	1.7	-79.1	-105.6	105.4	1.1	18	18
11	2.8	9.3	-131.6	-191.1	141.2	4.0	18	18
12	2.8	3.3	-108.0	-148.2	115.3	1.8	18	18
13	2.4	13.9	-112.8	-143.7	121.0	7.0	18	18
14	2.1	14.5	-105.6	-138.8	118.6	6.8	18	18
15	3.1	6.6	-133.6	-192.1	148.1	2.9	18	18
16	2.3	17.6	-101.7	-134.5	117.4	10.8	18	18
17	2.8	21.6	-136.8	-195.9	144.3	9.1	18	18
18	1.8	1.8	-36.7	-10.7	36.4	3.0	13	13
19	2.7	4.6	-139.1	-191.5	144.3	1.9	18	18
20	1.6	7.5	-129.7	-181.5	127.6	3.6	18	18
21	2.6	19.2	-132.4	-187.7	135.9	8.6	18	18
22	2.6	15.2	-131.0	-182.3	134.6	6.9	18	18
23	2.7	5.7	-130.2	-191.9	131.7	2.6	18	18
24	1.9	1.9	-37.0	-22.6	37.1	3.1	25	25
25	2.2	5.3	-133.1	-191.0	133.2	2.9	31	31
26	1.3	2.5	-138.6	-191.8	138.7	1.2	31	31
27	1.7	4.7	-137.1	-191.1	137.6	4.2	34	34
28	1.7	2.1	-96.5	-131.7	95.8	2.3	37	37
29	1.6	5.5	-103.1	-141.9	106.8	3.2	38	38
30	1.5	4.8	-76.8	-101.3	77.2	3.8	34	34
31	1.8	1.7	-124.0	-181.1	128.9	.8	41	41
32	1.9	3.7	-137.1	-191.8	142.5	1.6	42	42
33	2.7	1.1	-17.2	-13.0	33.4	1.7	36	36
34	1.4	3.6	-109.3	-141.7	111.5	4.7	34	34
35	1.1	1.1	-26.7	-12.6	29.5	2.2	45	45
36	1.9	6.9	-133.6	-191.1	137.7	11.2	36	36
37	2.5	3.5	-101.4	-131.5	101.0	5.8	36	36
38	1.2	2.2	-87.2	-121.6	111.1	1.2	47	47
39	1.1	2.2	-166.7	-211.7	167.7	1.2	49	49
40	1.7	1.4	-101.1	-151.6	101.1	1.1	48	48
41	2.3	1.1	-21.9	-25.7	31.8	2.3	36	36
42	2.0	2.6	-16.7	-24.8	31.0	5.2	36	36
43	2.2	7.3	-76.8	-125.0	146.7	2.9	53	53
44	1.6	3.0	-15.5	-25.4	29.4	5.2	35	35
45	1.0	1.7	-66.0	-101.7	101.7	1.1	55	55
46	1.7	1.4	-101.5	-151.6	101.5	1.0	54	54
47	1.7	1.2	-16.3	-26.3	36.7	.9	58	58
48	2.0	3.8	-12.1	-27.4	27.9	6.8	36	36
49	1.2	2.5	-10.5	-21.1	21.3	2.0	59	59
50	1.8	3.1	-35.0	-65.9	65.9	2.8	57	57
51	1.7	7.5	-31.5	-62.8	68.6	5.2	57	57

52	1.4	7.4	-24.0	63.2	67.6	6.7	60
53	1.6	6.5	-9.9	30.3	31.9	0.7	36
54	1.7	9.7	-24.4	73.1	77.0	7.7	53
55	1.7	1.0	-8.1	30.8	31.8	1.9	36
56	6	2.9	-14.5	90.2	91.4	1.9	66
57	2.2	1.5	-14.3	93.1	94.2	1.0	65
58	1.8	1.0	-7.6	64.7	65.1	1.0	64
59	1.3	9.4	-8.5	62.6	63.2	0.1	64
60	1.3	2.0	-3.4	53.2	53.3	1.9	67
61	1.7	1.2	-4.4	23.6	23.6	3.1	68
62	2.0	1.1	3	25.7	25.7	2.7	69
63	1.9	3.0	3.8	22.5	22.5	5.0	70
64	2.4	1.2	12.1	35.7	35.5	2.7	73
65	9	4.5	17.7	54.8	57.5	4.7	74
66	7	1.6	37.6	92.4	99.8	9	78
67	9	1.7	36.3	50.1	47.9	1.1	76
68	1.7	5.3	56.5	104.7	113.8	3.2	78
69	1.8	1.4	38.6	85.8	95.1	9	78
70	1.7	1.7	48.8	109.2	119.5	9	78
71	1.8	3.4	52.1	106.0	118.1	1.8	76
72	1.5	3.6	49.2	104.5	115.5	4.6	78
73	1.9	7.8	45.0	58.0	48.9	4.8	78
74	2.2	3.0	48.4	91.0	103.1	1.8	78
75	2.3	3.1	40.9	72.2	82.9	2.3	81
76	1.7	25.3	52.3	98.2	111.5	13.9	78
77	1.7	1.3	38.5	65.1	75.7	2.6	82
78	1.0	1.1	44.8	64.2	78.3	9	83
79	1.0	2.4	52.2	71.0	86.1	1.9	84
80	3.0	1.1	42.1	54.5	58.9	1.0	55
81	3.0	2.1	40.1	50.8	64.7	2.0	85
82	2.9	12.7	96.1	111.4	147.1	5.3	90
83	2.6	12.4	51.2	62.0	80.5	9.4	85
84	1.9	3.9	58.5	77.0	103.1	2.3	85
85	2.7	2.6	57.6	60.3	81.4	1.9	85
86	2.5	2.3	100.0	104.7	144.8	1.0	50
87	2.4	12.6	95.7	96.7	121.9	6.3	85
88	2.8	4.9	73.4	71.7	102.6	2.9	85
89	2.3	8.4	94.6	92.3	132.1	3.9	85
90	2.5	2.0	30.3	68.7	127.0	1.0	85
91	2.5	2.3	92.2	50.0	120.9	1.0	85

TOTAL IOD= 101 15 29 28
 TOP RECORD DENSITY
 NO OF RECORDS/RADIAL 4 CELL WIDTH 937.2 METERS PRF 794.0

TOTAL IOD= 1 1 1 1
 NO OF RECORDS/RADIAL 4 CELL WIDTH 937.2 METERS PRF 794.0

FIXED CONTOUR ATTRIBUTES

DAY HMMH SS FLE AZM1 AZM2
 226 1914 38 6.1 160.1 111.0

ID	THRESHOLD	AREA (KMR*2)	AREA REFLECTIVITY (DBZ)	LOCATION		RANGE (KM)	RESOLUTION (KM)	APX ELEMENTS	TOTAL PRECIP (TNS/HRI)	AVERAGE PRECIP (MM/HRI)	FIXED CONTOUR REFERENCE
				EAST	NORTH						
1	20	17.32	21.4	-31.0	-50.1	59.0	18.9	1			1
2	20	2.96	21.0	-74.6	-45.0	56.8	3.2	3			3
3	20	1.10	21.0	-50.7	6.8	51.1	1.8	4			4
4	20	548.88	43.0	-25.8	21.2	33.3	1005.8	7			7
5	20	31.69	22.1	1.6	22.3	22.3	86.8	1			-1
6	20	1.15	21.0	-3.5	56.3	67.0	1.1	15			15
7	20	12.57	21.1	-6.3	67.0	67.4	11.4	12			12
8	20	1.47	21.5	-4.1	42.4	42.6	2.1	13			13
9	20	11.22	21.1	-1.9	64.0	64.0	10.7	14			14
10	20	16.17	21.9	5.1	47.3	47.8	20.7	17			17
11	20	1.50	21.5	6.4	25.1	25.9	3.5	18			18
12	20	2.61	21.3	10.2	20.3	22.7	7.0	20			20
13	20	11.93	22.5	22.0	43.5	40.9	14.9	21			21
14	20	2.19	21.8	14.5	21.3	26.2	5.1	23			23
15	20	111.17	28.3	70.4	67.3	97.8	69.5	27			27
16	20	20.35	22.3	65.4	76.3	100.3	12.5	28			28
17	20	341.36	34.3	44.3	53.3	70.1	297.9	26			26
18	20	1.05	21.0	22.2	20.3	30.5	2.1	33			33
19	20	15.07	22.7	34.3	38.5	52.1	17.7	30			30
20	20	2.13	22.0	96.0	31.2	134.5	1.0	34			34
21	20	67.00	26.6	73.3	79.3	106.0	43.2	32			32
1	40	145.21	48.1	-27.0	20.1	33.6	269.3	7			7
2	40	11.12	46.0	-10.9	31.4	33.2	20.4	7			7
3	40	9.74	45.6	41.0	50.1	64.8	9.2	7			7

WIND DATA

DAY HAMP SS FILE AZM1 AZM2
 226 1334 3R 4.1 160.1 111.0

HEIGHT (KM)	AVERAGE REFLECTIVITY (DBZ)	TOTAL REFLECTIVITY (DBZ.KM**2)	AVERAGE U (M/SEC)	AVERAGE V (M/SEC)	AVERAGE VELOCITY (M/SEC)**2	VARIANCE (M/SEC)**2	JEL
4	22.0	78.7	0.0	0.0	.1	.1	-.08819E-19
5	21.5	209.2	-2.7	-7.1	4.8	4.8	.76765E-01
7	21.6	1151.1	0.0	1.6	.3	.3	-.35827E-14
9	33.3	258537.7	6.4	0.0	11.2	11.2	-.35827E-14

PEAK DETECTED CELL ATTRIBUTES

DAY HMM SS FILE RZM1 AZM2
 226 1344 38 5.1 163.1 111.0

ID	REFLECTIVITY (DBZ)	AREA (KM*2)	EAST (KM)	NORTH (KM)	RANGE (KM)	RESOLUTION ELEMENTS	AVERAGE VELOCITY SPREAD (M/S)	AVERAGE RADIAL SHEAR (M/S/KM)	AVERAGE TANGENTIAL VELOCITY (M/S)	MEAN FIXED CONTOUR REFERENCE
1	21.4	15.4	-11.1	-52.2	52.0	16.3	1.91	-1.39	-0.13	1
2	51.3	6.2	-32.3	16.0	36.6	3.3	2.15	-2.55	-0.03	7
3	33.0	2.8	-35.4	22.9	42.2	6.0	1.27	.02	-0.45	7
4	32.3	2.3	-32.6	26.0	40.4	3.5	1.12	.42	-1.13	7
5	54.5	3.5	-25.2	21.7	33.3	5.7	2.01	1.74	-0.33	7
6	52.0	2.0	-19.5	26.0	30.9	3.9	1.59	-2.02	2.29	7
7	53.0	1.9	-16.2	21.8	27.2	4.3	1.05	-0.58	.29	7
8	49.0	1.6	-10.3	31.6	33.3	3.0	1.94	-6.37	-1.49	7
9	27.8	2.2	3.3	47.9	48.0	2.8	1.25	-1.27	-0.26	17
10	21.4	1.5	6.4	25.2	26.0	3.5	.78	-.36	-.12	10
11	23.5	18.9	2.1	27.5	22.6	51.0	1.11	-.37	-0.33	10
12	21.7	5.6	21.9	43.5	48.7	7.0	.92	-.08	.00	21
13	21.7	2.2	14.4	21.9	26.3	5.1	.88	1.00	-.11	23
14	43.1	1.8	40.3	50.0	64.2	1.6	2.59	1.01	-.29	26
15	39.0	7.8	32.5	62.3	81.5	2.1	2.57	-1.61	1.05	26
16	24.5	6.8	60.6	70.4	92.9	4.5	2.04	-.57	5.43	27
17	23.6	5.7	66.0	74.3	99.3	3.5	1.55	2.14	-.81	28
18	23.6	8.3	34.5	38.2	51.5	4.4	1.77	.00	-.10	30
19	31.0	5.3	43.5	51.3	70.6	5.4	2.20	.31	.78	30
20	31.3	7.3	75.6	77.6	102.1	4.8	2.71	1.49	2.34	32
21	22.7	9.9	58.3	56.8	81.4	7.5	1.20	-.31	-.32	26
22	35.4	8.3	70.6	68.2	95.1	5.2	2.54	.41	.67	27

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HMMH SS ELE AZM1 AZM2
 226 1934 38 5.1 169.1 111.8

ID	MAGNITUDE (M/S/KM)	AREA (KM**2)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AVERAGE		FIXED CONTOUR REFERENCE
			EAST (KM)	NORTH (KM)			VELOCITY SPREAD (M/S)	SHEAR (M/S/KM)	
1	3.2	1.5	-31.1	-48.8	37.2	1.6	2.1	-3.2	1
2	1.4	1.0	-25.5	25.5	36.1	1.6	1.1	-1.4	7
3	.9	2.5	-13.5	35.7	33.3	3.9	.9	.9	7
4	.5	1.4	-10.9	26.2	28.3	3.0	.6	.5	7
5	1.9	2.1	-12.2	38.7	33.3	4.0	1.2	.9	7
6	.7	1.8	-5.4	26.5	28.2	3.9	.7	.7	7
7	1.1	1.3	-12.8	39.2	31.2	1.9	1.2	-1.1	7
8	.6	1.5	-6.2	28.3	29.9	3.1	1.1	-0.6	7
9	1.7	1.2	-6.5	35.9	37.2	1.9	1.5	-1.7	7
10	1.7	1.8	-8.6	37.7	38.0	2.9	1.3	-1.7	7
11	.4	1.2	-5.1	63.6	59.3	1.1	1.0	.4	12
12	.2	2.3	-6.2	66.7	67.0	2.1	1.4	-0.2	12
13	.8	1.2	-1.2	63.2	63.3	1.1	.7	.8	14
14	.4	3.2	-0.8	64.6	64.3	3.0	1.0	-0.4	14
15	.9	1.1	1.2	22.9	22.7	3.0	1.2	.9	10
16	.8	1.1	2.4	22.3	22.4	3.0	1.3	.8	10
17	.3	1.7	4.7	24.8	24.3	4.2	1.0	.3	10
18	1.5	1.1	48.7	65.9	62.3	.6	1.5	-1.5	26
19	.9	1.2	39.4	51.6	55.1	1.1	2.3	.9	26
20	3.2	1.1	58.9	64.3	62.0	.9	2.3	3.2	26
21	3.4	1.1	42.6	58.5	55.1	1.1	2.2	-3.4	25
22	1.6	1.8	66.2	78.4	102.5	1.1	2.7	1.6	26
23	3.5	1.1	65.2	74.4	38.3	.7	.3	-3.5	28
24	2.3	1.4	52.5	59.9	79.7	1.4	2.5	.1	26
25	3.0	1.2	78.7	60.7	107.3	.7	1.8	-3.0	32
26	2.6	1.9	72.9	81.2	109.2	1.1	3.0	2.6	32
27	1.7	3.0	43.9	55.2	73.7	2.5	2.2	-1.7	26
28	1.2	1.5	56.7	63.1	94.3	1.1	2.3	1.2	26
29	3.0	1.6	62.3	69.4	93.2	1.1	2.2	-3.0	27
30	2.5	1.9	77.0	82.6	112.3	1.1	3.0	-2.5	32
31	1.0	2.8	56.2	60.3	62.4	2.1	2.1	-1.0	26
32	1.4	1.4	53.1	54.9	76.4	1.1	2.0	-1.4	26
33	.9	1.8	65.1	67.4	95.1	1.1	2.8	.9	27
34	.8	3.4	57.6	57.2	81.1	2.9	1.1	.8	26
35	.9	1.3	58.2	59.8	84.3	1.0	1.5	.9	26
36	1.8	1.7	76.5	74.6	106.3	2.1	1.1	-1.8	32
37	.9	1.3	61.6	56.9	63.3	1.0	1.5	.9	26
38	1.9	1.6	73.3	67.7	99.9	1.0	2.9	-1.9	27
39	.3	5.1	59.7	54.8	81.1	3.9	1.1	.3	25
40	3.1	1.5	73.1	65.2	97.9	1.0	2.1	3.1	27
41	.8	1.6	77.0	66.4	101.7	1.0	2.7	.8	27
42	.7	1.6	76.7	63.9	99.9	1.0	2.2	.7	27

162 0 PROGRAM EXTRAC

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY HHMM SS ELF ADM1 ADM2
 226 1734 36 6.1 165.1 111.0

ID	SPEED (KHZ)	AREA (KHZ)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA ELEMENTS	FIXED CONTOUR REFERENCE
			EAST (KM)	NORTH (KM)				
1	2.0	5.2	-10.7	-43.1	57.9	6.5	1	
2	2.2	1.1	-36.3	-46.3	57.5	1.1	3	
3	1.2	1.1	-58.7	6.0	51.1	1.3	4	
4	2.4	3.5	-33.2	33.9	36.3	5.2	7	
5	2.7	3.5	-32.2	19.0	37.4	5.2	7	
6	2.2	3.5	-27.6	17.6	32.7	5.8	7	
7	2.4	2.7	-28.5	21.0	35.4	4.7	7	
8	1.4	5.3	-34.7	24.3	42.4	9.1	7	
9	2.2	1.1	-25.1	21.9	33.3	2.1	7	
10	1.8	3.5	-20.6	28.0	35.5	7.5	7	
11	2.5	2.1	-15.7	25.3	33.3	2.0	7	
12	2.7	1.1	-18.2	35.1	33.3	1.9	7	
13	1.2	2.3	-15.5	40.9	44.1	4.0	7	
14	1.9	3.2	-10.6	21.8	33.4	5.3	7	
15	2.1	1.1	-7.3	22.3	33.3	1.9	7	
16	1.5	7.7	-5.8	25.1	35.5	12.1	7	
17	1.1	1.5	-4.1	42.4	42.5	2.1	13	
18	1.7	1.2	-3.5	65.9	57.3	1.1	15	
19	1.2	11.7	-3.4	35.6	50.5	23.2	7	
20	1.4	3.4	0.5	23.7	23.8	13.8	15	
21	1.1	2.2	2.4	41.6	47.5	2.8	17	
22	1.2	3.4	7.3	47.4	46.5	12.0	17	
23	1.4	1.5	6.3	25.1	25.3	3.5	18	
24	1.3	7.3	22.5	43.5	48.9	9.8	21	
25	1.0	1.6	13.4	20.3	22.8	4.3	20	
26	1.4	2.2	14.5	22.0	26.3	5.1	23	
27	2.7	4.5	50.2	55.0	93.3	3.4	26	
28	2.5	7.7	43.0	58.3	71.4	2.7	25	
29	2.7	1.4	56.2	74.4	102.5	1.1	24	
30	3.0	1.4	58.5	81.3	105.4	1.1	32	
31	2.6	13.0	42.3	50.3	65.7	3.3	25	
32	2.2	3.5	57.0	74.6	120.3	2.1	28	
33	2.6	11.6	53.5	41.5	31.5	9.7	26	
34	2.9	7.5	37.1	39.9	54.4	4.0	35	
35	3.0	33.4	75.7	43.3	110.1	15.5	32	
36	2.8	1.1	22.2	21.4	33.5	2.1	33	
37	2.3	15.3	71.2	57.4	98.0	10.2	27	

TOTAL IDD= 36 11 15 17
 FOR REF= 00 UNITS 1
 NO OF RECORDS/RADIAL 4

CELL HEIGHT 937.2 METERS

REF

794.0

FIXED CONTOUR ATTRIBUTES

DAY HMM SS ELE AZM1 AZM2
 285 1935 34 733 115.0 115.0

ID	THRESHOLD (DBZ)	AREA (KM ²)	REFLECTIVITY (DBZ)	LOCATION		RANGE (KM)	RESOLUTION (KM)	PRECIP (TONS/HR)	TOTAL PRECIP (MM/HR)	FIXED CONTOUR REFERENCE
				EAST (KM)	NORTH (KM)					
1	20	2.29	21.0	-27.7	-47.3	54.9	2.5	1074.8	1	
2	20	575.39	42.5	-24.3	21.3	32.7	1074.8	2.3	7	
3	20	1.44	23.0	-4.3	38.3	38.4	2.3	1.9	9	
4	20	1.27	21.0	-24.3	-32.1	40.3	1.9	6.2	5	
5	20	2.04	21.5	4.0	20.3	20.3	6.2	53.8	-11	
6	20	23.35	23.6	15.3	22.2	27.0	19.0	14.7	13	
7	20	11.33	22.1	4.5	46.3	47.0	19.0	46.2	20	
8	20	14.93	23.0	22.8	42.3	48.1	24.5	5.3	16	
9	20	18.75	22.1	8.3	45.4	46.2	24.5	26.8	21	
10	20	4.51	22.2	25.2	35.3	45.9	76.7	127.5	-16	
11	20	31.12	23.1	5.1	24.3	24.8	127.5	82.1	22	
12	20	144.52	33.0	46.2	53.3	53.3	46.0	58.4	23	
13	20	51.71	25.9	55.2	53.3	53.3	1.9	258.5	25	
14	20	4.35	22.6	35.5	37.0	35.7	33.2	33.2	26	
15	20	1.72	21.0	32.2	35.7	58.4	1.9	33.2	7	
1	40	144.10	46.0	-25.3	20.1	32.8	258.5	15.9	7	
2	40	4.66	45.9	-10.4	31.5	33.2	15.9	55.6	22	
3	40	2.53	44.6	42.1	53.3	55.6	2.5			

WIND DATA

DAY	HR	SS	ELE	AZM1	AZM2
226	1335	38	7.3	115.0	115.0

HEIGHT (M)	AVERAGE REFLECTIVITY (DBZ)	TOTAL REFLECTIVITY (DBZ)	AVERAGE VELOCITY (M/SEC)	U VELOCITY (M/SEC)	AVERAGE VARIANCE (M/SEC ²)	DEL
5	21.0	1337.0	3.2	0.1	1.5	-.00018E-15
6	22.5	155.5	1.5	-6.3	11.8	-.59763E-11
7	21.0	216.4	0.0	1.6	1.1	-.00018E-15
10	31.2	122873.5	215.5	-155.3	27.6	.381933E-02

PEAK DEFECTED CELL ATTRIBUTES
 DAY HHMM SS ELE AZM1 AZM2
 226 1935 38 7.8 115.0 115.0

ID	REFLECTIVITY (DBZ)	AREA (KM^2)	LOCATION (EAST (KM), NORTH (KM))	RANGE (KM)	AREA RESOLUTION ELEMENTS	AVERAGE VELOCITY SPREAD (% S)	AVERAGE RADIAL SHEAR (M/S/KM)	AVERAGE TANGENTIAL SHEAR (M/S/KM)	AVERAGE RADIAL VELOCITY (M/S)	MEAN FIXED CONTOUR REFERENCE
1	52.7	3.1	-32.3 13.0	34.6	5.4	2.21	-0.34	-0.50	-2.06	7
2	52.4	2.0	-32.0 18.6	37.0	3.3	2.33	-1.32	.36	.23	7
3	52.0	6.2	-25.8 18.6	32.6	11.5	2.20	2.12	-1.07	-0.53	7
4	54.5	2.0	-24.1 21.6	32.3	3.8	1.72	2.36	1.43	2.06	7
5	50.4	3.6	-18.6 24.6	31.0	7.1	1.71	.85	1.27	1.93	7
6	50.0	1.1	-11.1 31.4	33.3	2.0	1.43	2.21	.41	1.44	7
7	22.7	5.9	5.6 47.0	47.2	8.9	.98	-0.19	-0.29	-0.28	13
8	22.1	18.7	8.8 45.3	46.2	24.3	1.02	-0.11	-0.21	-0.59	16
9	25.5	2.4	8.7 28.9	25.7	5.3	.62	-0.15	-0.35	-0.53	16
10	24.0	7.8	23.1 42.2	40.1	9.9	.70	-0.13	.08	1.01	20
11	22.7	4.5	26.2 38.8	46.8	5.9	.76	-0.02	-0.11	.87	21
12	36.6	3.0	46.0 56.4	72.8	2.5	2.56	-0.30	2.07	1.64	22
13	25.5	6.0	16.4 22.4	27.6	13.2	.63	-0.26	-0.26	.74	13
14	33.5	2.9	52.5 62.1	61.5	2.1	2.25	.42	-2.50	-4.00	23
15	27.3	4.1	56.8 56.2	85.7	7.9	2.23	-0.96	-0.00	-8.18	23
16	22.6	4.3	35.4 37.0	51.2	5.2	1.32	.12	-0.15	-0.62	25
17	24.3	14.0	54.3 56.1	61.7	10.5	1.61	.16	-0.33	-5.21	23

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY M444 55 ELE AZMI A7P2
226 133F 38 7.0 115.0 115.0

ID	MAGNITUDE SHEAR (M/S/KM)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS (M/S)	AREA VELOCITY SPREAD (M/S/KM)	AVERAGE SHEAR (M/S/KM)	FIXED CONTOUR REFERENCE
		EAST (KM)	NORTH (KM)					
1	2.8	1.5	-33.4	30.7	2.0	0.5	-0.2	7
2	0.7	2.8	-28.7	39.4	4.4	0.8	0.7	7
3	0.9	2.6	-26.5	37.7	4.2	0.9	-0.3	7
4	3.6	1.6	-19.3	21.1	3.2	1.6	3.6	7
5	2.6	1.1	-17.5	30.3	2.1	2.1	-0.3	7
6	0.7	2.0	-23.6	42.6	2.9	1.1	-0.7	7
7	0.9	1.3	-21.2	41.2	1.9	1.5	-0.9	7
8	2.0	1.1	-18.3	35.1	1.9	1.5	0.1	7
9	2.1	1.5	-11.9	32.4	2.3	1.3	-2.1	7
10	0.7	1.6	-10.7	24.5	3.1	1.1	-0.7	7
11	0.9	1.4	-14.2	38.7	11.7	1.1	-0.9	7
12	0.9	1.2	-11.8	38.4	1.9	1.1	-0.9	7
13	1.8	1.3	-6.4	36.0	2.1	1.2	1.6	7
14	0.9	1.1	-4.4	33.1	2.0	1.3	0.9	7
15	0.6	1.6	1.1	24.1	6.0	0.8	-0.6	19
16	0.7	1.1	7.1	24.5	2.7	0.8	-0.7	18
17	0.5	1.8	14.5	22.8	27.1	4.0	-0.5	19
18	0.3	1.5	27.0	34.3	46.1	1.5	-0.3	21
19	0.7	1.3	16.6	22.7	24.1	3.5	-0.7	15
20	3.1	1.1	45.0	58.2	71.5	0.9	2.3	22
21	2.5	1.3	41.8	52.4	67.3	1.1	2.0	22
22	2.7	1.4	53.2	62.4	62.0	1.1	2.3	23
23	2.3	1.0	43.1	46.8	65.1	1.0	2.1	22
24	1.8	1.3	52.5	55.3	79.2	1.0	2.5	23
25	0.8	1.3	56.2	63.5	84.5	1.0	1.8	23
26	3.3	1.3	45.0	50.1	67.9	1.1	2.2	3.3
27	2.1	1.3	38.5	52.9	71.7	1.1	2.2	-2.1
28	0.3	1.0	19.5	21.3	29.1	2.2	1.0	-0.0
29	1.1	1.3	56.3	57.0	88.1	1.0	1.7	-1.1
30	0.4	1.6	36.1	36.6	51.4	1.9	1.3	0.4
31	1.9	1.1	49.7	50.3	70.9	1.0	2.2	1.9
32	1.0	1.2	60.2	57.0	82.3	0.9	1.8	-1.0

VELOCITY SPREAD MAXIMA ATTRIBUTES

DAY	HHMM	SS	ELE	AZMI	AZM2
226	1935	38	7.0	115.0	115.0

ID	SPREAD (WVST)	AREA (KM2)	EAST (KM)	NORTH (KM)	LOCATION	RANGE (KM)	RESOLUTION ELEMENTS	AREA	FIXED CONTOUR REFERENCE
1	1.7	1.6	-28.1	-47.6		55.3	1.8		1
2	2.6	3.3	-33.6	13.6		36.3	5.4		7
3	2.5	2.9	-28.4	18.2		33.7	5.2		7
4	2.6	3.3	-30.1	20.4		36.4	5.6		7
5	2.4	4.7	-25.2	20.3		32.4	3.0		7
6	2.0	1.5	-23.9	33.1		33.3	2.6		7
7	2.0	7.0	-20.9	24.5		32.2	13.3		7
8	1.6	7.9	-25.9	34.8		43.3	11.2		7
9	1.8	7.5	-19.3	29.8		35.5	12.9		7
10	2.0	1.0	-14.3	29.6		32.8	1.9		7
11	1.8	5.1	-9.4	32.3		33.7	11.1		7
12	1.5	1.4	-3.3	35.3		38.4	2.3		9
13	1.8	1.6	-3.0	29.1		29.2	3.2		7
14	1.3	2.2	5.7	46.0		46.4	2.9		13
15	1.0	3.3	3.0	25.5		25.6	7.6		18
16	1.3	4.5	8.3	43.2		43.3	5.3		16
17	1.0	1.6	6.8	24.4		25.3	3.9		18
18	1.0	2.5	6.6	25.6		27.8	5.6		18
19	1.0	5.6	23.7	41.7		48.0	7.2		20
20	1.0	2.8	12.8	21.6		25.1	5.9		19
21	1.0	1.1	14.3	21.4		25.7	2.6		19
22	1.0	1.5	27.0	39.3		48.9	1.9		21
23	2.7	5.5	46.4	57.8		74.1	4.6		22
24	2.6	2.9	36.7	65.5		46.7	2.0		23
25	2.7	14.1	44.1	51.0		67.5	12.7		22
26	2.5	14.3	33.1	61.2		81.0	11.3		23
27	1.2	1.7	35.9	37.0		51.5	4.0		25
28	1.7	1.7	36.2	39.6		54.3	1.9		26
29	2.5	2.6	58.9	57.7		82.4	1.9		23

TOTAL IDO= 20 9 10 12
 NO OF PFCORUS/RADIAL 4 CELL WIDTH 337.2 METERS PRF 794.0

TOTAL IDO= 1 1 1 1
 NO OF PFCORUS/RADIAL 4 CELL WIDTH 337.2 METERS PRF 794.0

DAY HMMH SS ELE AZM1 AZM2
 226 1936 41 8.0 167.2 132.1

ID	THRESHOLD (DBZ)	AREA (KM**2)	AVERAGE		LOCATION		RANGE (KM)	RESOLUTION (KM)	AREA ELEMENTS	TOTAL PRECIP (TONS/HW)	AVERAGE PRECIP (MM/HW)	FIXED CONTOUR REFERENCE
			REFLECTIVITY (DBZ)	AREA (KM**2)	EAST (KM)	NORTH (KM)						
1	20	1.87	21.0	-24.6	-45.3	52.0	2.2	1				1
2	20	1.01	21.0	-25.3	-47.2	53.3	1.1	2				2
3	20	589.18	42.5	-23.2	22.0	32.0	1126.2	5				5
4	20	13.18	21.7	-22.3	-33.3	50.3	19.9	4				4
5	20	2.38	21.8	-2	36.8	36.8	4.0	9				9
6	20	2.35	21.4	2.5	28.3	28.7	6.3	-13				-13
7	20	23.51	21.5	4.3	23.3	24.3	59.1	12				12
8	20	38.84	22.5	8.5	43.0	43.8	55.6	14				14
9	20	15.19	22.7	13.2	21.3	25.2	36.8	17				17
10	20	5.24	22.3	25.8	41.3	48.0	6.7	18				18
12	20	96.90	30.6	44.0	53.2	69.0	95.3	20				20
1	60	167.07	48.0	-23.8	21.2	31.9	281.9	5				5
2	60	9.01	43.1	-9.1	31.3	33.1	14.8	5				5

WIND DATA

DAY	HH	SS	ELE	AZM1	AZM2
226	1936	41	8.0	147.2	132.1

HEIGHT	AVERAGE REFLECTIVITY (DBZ)	TOTAL REFLECTIVITY (DBZ)	AVERAGE U (M/SEC)	AVERAGE V (M/SEC)	AVERAGE VELOCITY VARIANCE (M/SEC**2)	DEL
4	22.7	2826.0	-8.6	-5.5	34.3	.76157E+00
7	22.3	885.4	-2.0	-10.7	24.8	.92090E-01

PEAK DETECTED CELL ATTRIBUTES

DAY MMM SS ELE AZMI AZM2
 226 1936 61 5.3 167.2 132.1

ID	REFLECTIVITY (DBZ)	AREA (KM*2)	LOCATION EAST (KM)	NORTH (KM)	RANGE (KM)	AREA RESOLUTION ELEMENTS	AVERAGE VELOCITY SPREAD (M/S)	AVERAGE RADIAL SHEAR (M/S/KM)	AVERAGE TANGENTIAL SHEAR (M/S/KM)	AVERAGE RADIAL VELOCITY (M/S)	PEAK FIXED VELOCITY CONTOUR REFERENCE
1	21.6	13.2	-22.9	-33.3	40.4	19.9	1.38	-0.22	-0.38	-0.96	4
2	49.6	5.0	-30.9	13.7	33.9	9.1	1.97	-0.16	.15	-1.18	5
3	28.9	6.3	-35.2	23.7	42.5	7.0	1.02	.70	.06	-4.17	5
4	53.8	2.3	-26.6	18.6	32.4	4.4	2.35	3.15	1.55	3.05	5
5	57.0	1.1	-25.2	18.7	31.4	2.1	2.05	2.52	-1.15	2.14	5
6	55.6	1.3	-22.5	23.2	32.3	2.4	1.77	2.02	-1.90	.59	5
7	46.9	2.2	-9.7	31.3	32.8	6.1	1.21	-3.94	.53	-10.50	5
8	21.7	2.4	-7.1	36.8	36.8	4.0	.93	-0.11	-0.13	-2.55	5
9	29.8	2.0	2.0	28.6	24.7	4.3	.80	.59	3.76	-3.02	12
10	22.8	30.2	8.4	42.9	43.7	42.2	1.04	-0.53	.33	-5.78	14
11	22.2	5.2	25.8	48.5	48.0	6.7	.85	.72	.06	-9.46	14
12	40.6	2.9	42.5	51.4	66.7	2.6	2.22	1.36	1.21	-6.72	20
13	32.9	2.2	47.0	57.3	74.1	1.8	2.62	.23	1.21	-9.05	20
14	25.6	3.5	47.0	51.1	60.5	3.1	2.17	-1.61	-0.05	-7.94	20

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY MMM SS FLE AZMI AZM2
 226 1536 45 6.3 147.2 132.1

ID	MAGNITUDE SHEAR (M/S/KM)	AREA		LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA VELOCITY SPREAD (M/S)	FIXED CONTOUR REFERENCE	
		(K**2)	(K**2)	EAST (KM)	NORTH (KM)					
1	1.4	1.2	17.7	-33.0	17.7	37.5	1.9	.7	-1.4	5
2	.4	1.3	36.6	-36.6	25.3	44.5	1.8	1.2	-.4	5
3	5.3	1.2	25.3	-25.3	28.9	38.4	1.5	1.6	-.3	5
4	2.1	1.4	27.2	-27.2	31.6	41.7	2.0	1.2	.1	5
5	7.3	2.4	22.3	-22.3	28.9	35.5	4.0	.9	7.3	5
6	5.0	1.1	18.7	-18.7	24.7	31.0	2.1	1.6	5.0	5
7	2.5	1.1	18.5	-18.5	27.9	32.7	1.9	1.7	-2.5	5
8	.9	1.5	22.4	-22.4	35.7	42.1	2.1	1.2	-.9	5
9	2.2	1.1	16.3	-16.3	27.4	31.3	2.0	1.7	-2.2	5
10	1.0	1.1	13.2	-13.2	34.1	36.5	1.6	.3	-1.0	5
11	.6	1.8	15.0	-15.0	33.9	41.7	2.6	1.2	-.6	5
12	.9	1.1	10.6	-10.6	36.9	39.4	1.6	1.3	-.9	5
13	1.3	1.1	6.8	-6.8	35.9	35.5	1.8	.9	-1.3	5
14	1.1	1.1	11.3	-11.3	45.4	46.3	1.4	1.2	-1.1	14
15	.2	2.0	6.8	-6.8	22.4	23.3	2.5	.7	-.2	12
16	2.2	2.6	44.9	-44.9	60.0	75.0	2.1	2.3	-2.2	20
17	3.8	1.2	43.3	-43.3	53.6	68.3	1.1	2.5	-3.8	20

VELOCITY SPPREAD MAXIMA ATTRIBUTES

DAY MMM SS ELE AZM1 AZM2
 226 1536 41 9.0 147.2 132.1

ID	SPREAD (M/ST)	LOCATION			RANGE (KM)	RESOLUTION ELEMENTS	AREA ELEMENTS	FIVED COUNT REFERENCE
		ARCA (M/ST)	EAST (KM)	NORTH (KM)				
1	2.0	1.3	-24.6	-45.8	52.0	2.2	2.2	1
2	2.2	1.0	-25.9	-47.2	53.3	1.1	1.1	2
3	1.8	4.2	-22.6	-35.2	42.0	6.1	6.1	4
4	2.7	4.1	-33.9	15.2	37.1	6.7	6.7	5
5	1.9	1.4	-35.1	17.5	39.2	2.1	2.1	5
6	2.2	1.7	-28.0	16.9	32.7	3.3	3.3	5
7	2.7	1.1	-26.4	18.0	31.3	1.9	1.9	5
8	2.6	3.6	-26.6	20.6	33.7	17.4	17.4	5
9	2.2	1.3	-17.3	31.1	35.6	5.3	5.3	5
10	1.7	1.6	-14.2	28.7	32.0	3.0	3.0	5
11	2.4	1.0	-18.6	29.5	31.4	2.0	2.0	5
12	1.4	15.1	-12.9	36.5	40.6	24.3	24.3	5
13	1.6	3.6	-9.7	32.0	33.1	15.0	15.0	5
14	1.9	3.9	-6.1	33.4	33.9	7.1	7.1	5
15	1.3	1.9	-3.9	28.3	28.6	4.0	4.0	5
16	1.7	1.8	-1.1	35.7	36.7	3.1	3.1	9
17	.9	2.7	2.2	20.5	20.6	7.6	7.6	13
18	.3	5.4	2.9	24.5	25.0	15.7	15.7	12
19	1.1	2.2	7.2	21.8	22.3	5.9	5.9	12
20	1.1	2.8	11.9	21.1	24.2	5.9	5.9	17
21	1.1	1.6	27.1	39.9	48.3	2.3	2.3	19
22	1.0	1.8	15.6	21.7	26.7	4.2	4.2	17
23	2.6	11.4	44.3	52.0	68.3	10.2	10.2	20
24	2.6	18.3	48.0	56.4	74.0	15.6	15.6	20

TOTAL LIDS: Z1 6 5 9
 EOF RELO ON UNIT 1 NO OF RECORDS/RADIAL 4 CELL WIDTH 937.2 METERS PRF 794.0

FIXED CONTOUR ATTRIBUTES

DAY	MM	SS	ELE	AZM1	AZM2
226	1977	37	9.0	135.2	112.9

ID	THRESHOLD	AREA (KM ²)	AVERAGE REFLECTIVITY (DBZ)	EAST (KM)	NORTH (KM)	LOCATION	RANGE RESOLUTION (KM)	NUMBER OF ELEMENTS	TOTAL PRECIP (TMS/HR)	AVERAGE PRECIP (MM/HR)	FIXED CONTOUR REFERENCE
1	20	39.07	22.0	-21.7	-33.1		39.0	61.3			1
2	20	648.71	43.5	-22.6	22.7		31.6	1256.9			2
3	20	6.78	22.3	3.5	28.3		21.2	13.8			-7
4	20	9.70	21.8	7.5	19.3		21.3	16.8			-12
5	20	2.13	21.0	6.1	48.4		44.8	2.9			9
6	20	1.60	21.8	10.1	19.3		22.2	4.4			13
7	20	25.41	28.6	43.8	51.4		67.6	23.0			14
8	20	2.35	22.0	48.5	55.3		74.5	1.3			15
1	40	6.75	43.2	-6.0	32.3		33.0	8.3			2
2	40	137.18	43.9	-22.9	21.3		31.9	266.3			2

WIND DATA

DAY	HHH	SS	ELE	AZM1	AZM2
226	1937	37	9.0	135.2	112.9

HEIGHT	REFLECTIVITY	TOTAL	AVERAGE	VELOCITY	DEL
(RM)	(DBZ)	REFLECTIVITY	(M/SEC)	(M/SEC)	(M/SEC)
		U	V	W	

PEAK DETECTED CELL ATTRIBUTES

DAY MMH SS ELE AZMI AZM2
 226 1977 37 9.3 135.2 112.9

ID	REFLECTIVITY (DBZ)	RPEX (KM*2)	LOCATION		RANGE (KM)	RESOLUTION ELEMENTS	AREA		AVERAGE VELOCITY		AVERAGE TANGENTIAL VELOCITY		PEAK FIXED COURSE REFERENCE
			EAST (KM)	NORTH (KM)			SPREAD (M/S)	RADIAL SHEAR (M/S/KM)	SHEAR (M/S/KM)	RADIAL VELOCITY (M/S)			
1	22.3	26.9	-20.7	-33.5	33.4	81.6	1.98	-0.82	-0.95	-2.22	-0.95	1	
2	43.8	1.3	-33.6	17.7	36.0	2.1	2.53	3.41	-3.08	-2.22	-2.22	2	
3	48.3	1.2	-30.7	18.9	35.1	2.0	2.11	-2.92	3.37	0.79	0.79	2	
4	59.7	2.1	-24.4	16.8	30.9	4.2	2.21	3.30	.25	-6.19	-6.19	2	
5	57.6	2.8	-27.2	23.2	35.7	6.7	2.33	-0.57	3.88	-5.89	-5.89	2	
6	58.9	1.0	-21.6	24.9	32.3	1.9	1.65	-1.27	-0.54	-1.05	-1.05	2	
7	53.0	1.3	-18.2	23.5	23.8	1.3	1.83	-1.35	-0.52	-1.23	-1.23	2	
8	51.4	1.4	-16.6	25.6	30.5	2.3	1.83	1.89	-0.13	2.11	2.11	2	
9	23.2	8.8	-11.7	35.0	40.7	13.3	1.85	-0.28	-0.17	0.07	0.07	2	
10	44.2	2.1	-8.2	31.5	32.5	3.9	1.29	1.12	-0.19	0.44	0.44	2	
11	24.5	2.5	5.8	37.7	33.2	4.0	0.95	3.50	3.91	-4.03	-4.03	2	
12	22.8	3.0	3.8	21.1	21.4	8.6	0.77	-1.10	1.68	-4.67	-4.67	7	
13	21.8	5.7	7.5	19.9	21.3	15.3	0.83	-0.31	0.06	-7.30	-7.30	12	
14	21.7	1.5	10.2	19.3	22.3	4.4	1.94	-0.14	-0.26	-6.18	-6.18	13	
15	33.0	4.3	43.7	51.4	67.5	3.9	2.24	-0.31	-1.69	-6.92	-6.92	14	

TANGENTIAL SHEAR MAXIMA ATTRIBUTES

DAY HHMM SS FILE AZM1 AZM2
 226 1377 37 9.0 135.2 112.9

ID	MAGNITUDE SHEAR (M/S/KM)	AREA (KM**2)	LOCATION			RANGE (KM)	RESOLUTION ELEMENTS	AREA VELOCITY SPREAD (M/S)	AVERAGE SHEAR (M/S/KM)	FIXED CONTOUR REFERENCE
			EAST (KM)	NORTH (KM)	DEPTH (KM)					
1	1.3	1.3	-26.8	32.9	41.3	1.9	1.4	-1.3	2	
2	4.7	1.1	-18.0	25.2	30.3	2.1	2.1	4.7	2	
3	2.1	1.5	-18.9	25.9	29.3	3.2	1.3	-1.7	2	
4	1.0	1.4	-17.7	36.2	40.3	2.1	1.8	-1.0	2	
5	.9	1.8	-15.5	34.6	37.3	2.9	1.3	.4	2	
6	1.6	4.1	-18.1	39.2	41.7	6.0	1.0	-1.6	2	
8	3.8	1.1	-6.3	33.2	31.7	1.9	2.2	-3.8	2	
9	1.6	1.1	-6.3	31.6	31.3	2.0	1.7	-1.6	2	
10	.9	1.1	.1	34.2	34.2	1.9	1.1	-1.9	2	

PWA OF THE LOAD 111
 LWA#1 OF THE LOAD 34170
 TRANSFER ADDRESS -- EXPAND 6315

PROGRAM AND BLOCK ASSIGNMENTS.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSR	VER	LEVEL	MARKURE	COMMENTS
/HEAD/	111	15							
/EXPAN/	126	10							
/LINUM/	136	7463	LGO	05/03/78	FTN	4.5	428	666X I	OPT=1
BEQRY.	7621	1							
EXPANI	7622	0	LGO	05/03/78	FTN	4.6	428	666X I	OPT=1
MUSCAL	7822	343	LGO	05/03/78	FTN	4.6	428	666X I	OPT=1
LABEL	18165	77	LGO	05/03/78	FTN	4.6	428	666X I	OPT=1
/NAME/	10264	125	LGO	05/03/78	FTN	4.6	428	666X I	OPT=1
/NAMIT/	10511	6							
/CREXP/	10417	1							
/TAGIT/	10421	1							
/SARVOR/	10522	5							
PLT103	10427	171	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
BLOIT	10620	54	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
ENPLY	10674	325	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
CHEXIT	11221	160	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
FACTOR	11401	11	UL-PEN	10/14/76	COMPASS	3.2	414		
SYMBOL	11512	16	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0700	11530	307	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0600E	11737	432	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
OUTX	12371	425	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
WHERE	13016	41	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
ERXPL	13057	23	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
MEMPEM	13152	52	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0700	13154	233	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0700	13511	233	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0700	13644	66	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0700	13732	75	UL-PEN	10/14/76	FTN	4.5	414	666X I	OPT=2
PL0700	14027	467	UL-PEN	10/14/76	COMPASS	3.2	414		
PL0700	14516	4	UL-PEN	10/14/76	COMPASS	3.2	414		
PL0700	14922	1115	UL-LIB	02/16/78	FTN	4.6	428	666X I	OPT=1
PL0700	15637	10	UL-LIB	02/16/78	FTN	4.6	428	666X I	OPT=1
PL0700	15647	33	UL-LIB	02/16/78	FTN	4.6	428	666X I	OPT=1
PL0700	15702	1							
PL0700	15703	23							
PL0700	15726	133							
PL0700	16061	0	SL-FORTRAN	08/12/77	COMPASS	3.3	428		FCL INITIALIZATION ROUTINE.
PL0700	16151	41	SL-FORTRAN	08/12/77	COMPASS	3.3	428		INITIALIZE CONSTANTS.
PL0700	16122	311	SL-FORTRAN	08/12/77	COMPASS	3.3	428		COMMON FLOATING OUTPUT CODE
PL0700	16433	603	SL-FORTRAN	08/12/77	COMPASS	3.3	428		FORTRAN OBJECT LIBRARY UTILITIES.
PL0700	17236	276	SL-FORTRAN	08/12/77	COMPASS	3.3	428		COMMON INPUT FORMATTING CODE
PL0700	17534	274	SL-FORTRAN	08/12/77	COMPASS	3.3	428		NAMELIST OUTPUT ROUTINE.
PL0700	20030	172	SL-FORTRAN	08/12/77	COMPASS	3.3	428		FORMATTED WRITE FORTRAN RECORD.
PL0700	20222	487	SL-FORTRAN	08/12/77	COMPASS	3.3	428		EXTENDED ERROR HANDLING OPTION.

BLOCK	ADDRESS	LENGTH	FILE	DATE	PROCESSOR LEVEL	HARDWARE	COMMENTS
CLOCK=	20631	31	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	ACCESS SYSTEM CLOCKS FOR FORTRAN.
GOITER=	20662	14	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	COMPUTED GO TO ERROR PROCESSOR.
RCOG	20676	73	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	COMPUTE COMMON AND NATURAL LOGARITHMS. OPTIMIZE.
SINCOS=	20771	66	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	TRIGONOMETRIC SINE OR COSINE OF X. OPT-ALL.
SYSTEM=	21057	1	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	LINK BETWEEN SYSVARIO AND INITIALIZATION CODE.
BACKSP=	21060	56	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	BACKSPACE LOGICAL RECORD.
COMIO=	21136	65	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	COMMON CODED I/O ROUTINES AND CONSTANTS.
EOF	21222	16	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	TEST FOR END OF FILE STATUS.
FLTRN=	21248	154	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	COMMON FLOATING INPUT CONVERTER.
FRAP=	21414	352	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	CRACK APLIST AND FORMAT FOR KODES/MAKER.
FORPUL=	21766	16	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	FILE MISC. UTILITIES.
GETFIL=	22804	42	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	LOCATE AN FIT GIVEN A FILE NAME.
/IO.BUF./	22846	227					
INPB=	22275	314	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	BINARY READ FORTRAN RECORD.
KODES=	22611	556	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	OUTPUT FORMAT INTERPRETER.
MAJIN=	23267	523	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	NAMELIST INPUT ROUTINE.
OUTCOM=	24812	154	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	COMMON OUTPUT CODE
SYSTEM	24866	21	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	USER CALLABLE ERROR PROCESSOR.
SYS=IST	24887	52	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	MATH LIBRARY LINK TO ERROR MESSAGE PROCESSING.
XTOI=	24271	18	SL-FORTRAN	08/12/77	COMPASS 3.	3-426	REAL TO INTEGER EXPONENTIATION.
/CONV.RM/	24301	6					
CIO.RM	24307	40	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/RUB.RM/	24347	10					
MOVE.RM	24357	64	SL-SYSIO	03/03/76	COMPASS 3.	2-414	
WCL.RM	24443	233	SL-SYSIO	03/03/76	COMPASS 3.	2-414	
/JHPS.RM/	24676	11					
/REMG.RM/	24787	3					
/OPE.S.FD/	24712	1					
/OPEK.FD/	24713	7					
OPEN.RM	24722	237	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/PUT.RT/	25161	11					
PLEO.RM	25172	42	SL-SYSIO	03/03/76	COMPASS 3.	2-414	
/CECF.FD/	25238	1					
CLSF.SD	25243	134	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/CLSV.FD/	25377	7					
CLSP.SD	25406	137	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/REW.FD/	25545	7					
REN.SD	25554	33	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/TERM.PM/	25607	1					
/GET.FD/	25610	7					
/GET.BT/	25617	5					
/GET.RT/	25624	11					
GET.SD	25635	1134	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
Z.SD	26771	101	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
W.SD	27872	58	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
F.SD	27142	106	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/SKBL.FD/	27250	7					
/SMB.FD/	27257	1					
SKSB.SD	27268	181	SL-SYSIO	03/03/76	COMPASS 3.	2-414	
ERR.RM	27161	404	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
CHMR.SD	27785	7	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
OSUB.RM	27774	71	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
OPEN.SD	30065	254	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
OPEX.SD	30341	14	SL-SYSIO	09/03/76	COMPASS 3.	2-414	
/PUT.FD/	30355	7					

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SIMPUT

IPLT = T, T, T, T, T,

Z1 = T,

Z2 = F,

Z3 = F,

Z4 = F,

LS = T,

RK1 = -.7E+02,

RK2 = .1E+02,

YK1 = -.1E+02,

YK2 = .7E+02,

LK = T,

SEMO

RANGE= 512. CELLWIDTH= 1.042 ELEVATION= 10.02
 X1(KM)= -80. Y1(KM)= -20. X2(KM)= 20. Y2(KM)= 80.
 X1(IN)= 1.00 Y1(IN)= 1.00 X2(IN)= 9.00 Y2(IN)= 9.00

3.153	2.617	3001	3.126	2.779	2001	OUTSIDE PLOT AREA	6.047	.710	6.304	.649
3.153	2.617	3001	3.125	2.838	2001	OUTSIDE PLOT AREA	5.047	.710	6.001	.744
3.126	2.779	3001	3.068	2.763	2001	OUTSIDE PLOT AREA	6.004	.649	5.911	.624
3.125	2.838	3001	3.110	2.849	2001	OUTSIDE PLOT AREA	6.001	.744	5.375	.761
3.068	2.763	3001	3.024	2.738	2001	OUTSIDE PLOT AREA	5.911	.624	5.841	.583
3.110	2.849	3001	3.023	2.799	2001	OUTSIDE PLOT AREA	5.979	.751	5.835	.668
3.024	2.738	3001	2.994	2.762	2001	OUTSIDE PLOT AREA	5.841	.583	5.792	.622
3.023	2.799	3001	3.114	2.806	2001	OUTSIDE PLOT AREA	5.839	.668	5.825	.692
3.014	2.806	3001	2.994	2.762	2001	OUTSIDE PLOT AREA	5.825	.692	5.792	.622
3.144	3.068	3001	3.112	3.032	2001	OUTSIDE PLOT AREA	6.032	1.108	5.793	1.053
3.080	2.997	3001	3.045	2.963	2001	OUTSIDE PLOT AREA	5.930	.998	5.879	.943
3.144	3.068	3001	3.150	3.115	2001	OUTSIDE PLOT AREA	5.032	1.108	6.058	1.186
3.112	3.032	3001	3.096	3.047	2001	OUTSIDE PLOT AREA	5.941	1.053	5.955	1.077
3.080	2.997	3001	3.053	3.013	2001	OUTSIDE PLOT AREA	5.930	.943	5.903	1.023
3.063	3.013	3001	3.048	2.963	2001	OUTSIDE PLOT AREA	5.903	1.023	5.879	.943
3.158	3.115	3001	3.145	3.129	2001	OUTSIDE PLOT AREA	6.058	1.195	6.034	1.209
3.145	3.129	3001	3.096	3.047	2001	OUTSIDE PLOT AREA	6.034	1.209	5.955	1.077
2.159	2.125	3001	2.126	2.091	2001	OUTSIDE PLOT AREA	4.859	-.396	4.406	-.450
2.094	2.056	3001	2.028	1.991	2001	OUTSIDE PLOT AREA	4.354	-.503	4.249	-.510
2.159	2.125	3001	2.128	2.156	2001	OUTSIDE PLOT AREA	4.459	-.396	4.405	-.446
2.128	2.156	3001	2.126	2.091	2001	OUTSIDE PLOT AREA	4.409	-.346	4.406	-.450
2.094	2.056	3001	2.051	2.050	2001	OUTSIDE PLOT AREA	4.354	-.503	4.302	-.551
2.051	2.050	3001	2.028	1.991	2001	OUTSIDE PLOT AREA	4.302	-.451	4.249	-.510
3.013	3.063	3001	2.979	3.031	2001	OUTSIDE PLOT AREA	5.823	1.103	5.765	1.052
3.013	3.063	3001	3.033	3.110	2001	OUTSIDE PLOT AREA	5.823	1.103	5.856	1.178
2.979	3.031	3001	2.999	3.078	2001	OUTSIDE PLOT AREA	5.759	1.052	5.800	1.127
3.033	3.110	3001	3.028	3.125	2001	OUTSIDE PLOT AREA	5.956	1.178	5.834	1.202
2.999	3.078	3001	2.985	3.054	2001	OUTSIDE PLOT AREA	5.800	1.127	5.776	1.152
3.028	3.125	3001	3.004	3.143	2001	OUTSIDE PLOT AREA	5.634	1.202	5.608	1.231
2.985	3.094	3001	2.968	3.113	2001	OUTSIDE PLOT AREA	5.778	1.152	5.752	1.182
3.004	3.143	3001	2.990	3.160	2001	OUTSIDE PLOT AREA	5.908	1.231	5.786	1.258
2.968	3.113	3001	2.947	3.100	2001	OUTSIDE PLOT AREA	5.752	1.182	5.670	1.162
2.007	2.410	3001	2.551	2.361	2001	OUTSIDE PLOT AREA	4.344	.860	4.286	.812

2.990	3.158	3031	3.312	3.207	2001	5.785	1.258	5.822	1.333
2.917	3.180	3031	2.976	3.177	2001	5.670	1.162	5.751	1.266
2.887	3.438	3031	2.851	2.843	2001	4.356	.850	4.332	.912
2.861	2.443	3031	2.951	2.381	2001	4.302	.812	4.269	.872
2.812	3.287	3031	2.943	3.193	2001	5.822	1.333	5.783	1.311
2.976	3.177	3031	2.926	3.164	2001	5.763	1.286	5.684	1.265
2.963	3.193	3031	2.988	3.237	2001	5.743	1.311	5.703	1.332
2.926	3.164	3031	2.913	3.181	2001	5.684	1.265	5.664	1.291
2.988	3.237	3031	2.976	3.255	2001	5.733	1.332	5.763	1.409
2.913	3.181	3031	2.900	3.199	2001	5.664	1.241	5.642	1.321
2.976	3.255	3031	2.963	3.272	2001	5.763	1.409	5.743	1.437
2.909	3.199	3031	2.886	3.218	2001	5.642	1.321	5.621	1.351
2.953	3.272	3031	2.930	3.315	2001	5.743	1.437	5.766	1.507
2.886	3.218	3031	2.873	3.237	2001	5.621	1.351	5.604	1.381
2.990	3.315	3031	2.931	3.330	2001	5.735	1.507	5.771	1.529
2.887	3.237	3031	2.853	3.253	2001	5.600	1.481	5.583	1.466
2.941	3.330	3031	2.968	3.349	2001	5.771	1.529	5.752	1.560
2.863	3.253	3031	2.849	3.274	2001	5.583	1.486	5.561	1.440
2.958	3.349	3031	2.917	3.342	2001	5.752	1.550	5.670	1.543
2.849	3.274	3031	2.877	3.318	2001	5.551	1.440	5.506	1.510
2.917	3.342	3031	2.947	3.364	2001	5.675	1.543	5.717	1.616
2.877	3.318	3031	2.825	3.313	2001	5.606	1.510	5.528	1.502
2.947	3.384	3031	2.937	3.402	2001	5.717	1.616	5.701	1.644
2.825	3.313	3031	2.814	3.333	2001	5.523	1.502	5.505	1.534
2.978	3.419	3031	2.937	3.496	2001	5.729	1.672	5.764	1.736
2.837	3.482	3031	2.844	3.375	2001	5.505	1.534	5.487	1.566
2.814	3.333	3031	2.803	3.353	2001	5.429	1.487	5.430	1.524
2.878	3.419	3031	2.850	3.451	2001	5.553	1.566	5.537	1.633
2.844	3.375	3031	2.834	3.395	2001	5.487	1.524	5.470	1.593
2.803	3.353	3031	2.792	3.373	2001	5.429	1.487	5.412	1.512
2.826	3.402	3031	2.806	3.406	2001	5.487	1.524	5.470	1.593
2.836	3.395	3031	2.855	3.437	2001	5.537	1.633	5.516	1.612
2.792	3.373	3031	2.781	3.396	2001	5.470	1.599	5.452	1.634
2.826	3.402	3031	2.814	3.402	2001	5.435	1.445	5.445	1.435
2.884	3.496	3031	2.856	3.441	2001	5.435	1.445	5.412	1.468
2.841	3.455	3031	2.839	3.375	2001	5.375	1.415	5.362	1.453
2.865	3.455	3031	2.856	3.455	2001	5.409	1.479	5.461	1.561
2.781	3.396	3031	2.729	3.394	2001	5.286	1.381	5.273	1.429
2.858	3.482	3031	2.816	3.411	2001	5.452	1.534	5.430	1.632
2.836	3.411	3031	2.816	3.311	2001	5.445	1.435	5.422	1.468
2.836	3.411	3031	2.856	3.361	2001	5.422	1.419	5.410	1.466
2.982	3.500	3031	2.899	3.451	2001	5.672	1.602	5.719	1.693
2.841	3.495	3031	2.833	3.431	2001	5.419	1.368	5.452	1.451
2.933	3.513	3031	2.899	3.513	2001	5.708	1.733	5.655	1.622
2.856	3.455	3031	2.847	3.474	2001	5.695	1.622	5.641	1.761
2.729	3.394	3031	2.762	3.474	2001	5.573	1.573	5.558	1.760
2.793	3.221	3031	2.727	3.435	2001	5.370	1.432	5.422	1.697
2.809	3.251	3031	2.742	3.402	2001	5.472	1.535	5.435	1.733
2.857	3.482	3031	2.811	3.483	2001	5.621	1.642	5.635	1.733
2.847	3.474	3031	2.848	3.452	2001	5.559	1.551	5.546	1.637
2.762	3.435	3031	2.754	3.454	2001	5.422	1.468	5.408	1.728
2.293	3.221	3031	2.281	3.247	2001	4.672	1.355	4.653	1.597
2.707	3.182	3031	2.715	3.210	2001	4.535	1.233	4.516	1.537
2.195	3.210	3031	2.193	3.172	2001	4.516	1.337	4.378	1.277
2.109	3.172	3031	2.122	3.143	2001	4.378	1.277	4.399	1.231
2.066	3.153	3031	2.023	3.124	2001	4.310	1.247	4.241	1.217
1.994	3.085	3031	1.937	3.097	2001	4.136	1.137	4.103	1.157
2.640	3.492	3031	2.611	3.512	2001	5.546	1.788	5.522	1.713
2.754	3.454	3031	2.745	3.475	2001	5.489	1.728	5.394	1.752
2.281	3.247	3031	2.289	3.276	2001	4.653	1.497	4.633	1.444
2.132	3.240	3031	2.136	3.222	2001	4.495	1.366	4.425	1.357
2.066	3.153	3031	2.052	3.166	2001	4.310	1.247	4.287	1.239
2.052	3.146	3031	2.009	3.168	2001	4.287	1.299	4.218	1.270
2.009	3.168	3031	2.023	3.134	2001	4.218	1.270	4.241	1.217

1.937	3.097	3001	2.089	3.168	2001	4.103	1.157	4.218	1.270
2.831	3.512	3001	2.823	3.531	2001	5.532	1.613	5.519	1.951
2.765	3.475	3001	2.692	3.479	2001	5.336	1.762	5.310	1.768
2.344	3.340	3001	2.300	3.323	2001	4.793	1.545	4.684	1.518
2.268	3.276	3001	2.296	3.266	2001	4.633	1.444	4.514	1.491
2.182	3.240	3001	2.189	3.271	2001	4.495	1.386	4.475	1.435
2.169	3.271	3001	2.126	3.254	2001	4.875	1.435	4.805	1.807
2.126	3.254	3001	2.138	3.222	2001	4.405	1.407	4.425	1.457
2.009	3.168	3001	1.995	3.201	2001	4.213	1.270	4.196	1.324
2.823	3.531	3001	2.816	3.549	2001	5.513	1.651	5.508	1.880
2.692	3.479	3001	2.684	3.459	2001	5.310	1.768	5.295	1.800
2.344	3.340	3001	2.334	3.366	2001	4.793	1.546	4.737	1.587
2.300	3.323	3001	2.290	3.349	2001	4.684	1.518	4.667	1.560
2.266	3.306	3001	2.246	3.332	2001	4.614	1.491	4.597	1.533
1.995	3.201	3001	1.983	3.232	2001	4.196	1.324	4.177	1.373
2.816	3.549	3001	2.809	3.569	2001	5.508	1.680	5.496	1.912
2.684	3.499	3001	2.632	3.456	2001	5.298	1.800	5.214	1.810
2.334	3.366	3001	2.323	3.394	2001	4.737	1.587	4.721	1.632
2.270	3.349	3001	2.279	3.378	2001	4.567	1.550	4.550	1.805
2.246	3.332	3001	2.235	3.362	2001	4.537	1.533	4.540	1.581
2.058	3.298	3001	2.054	3.282	2001	4.298	1.479	4.227	1.453
1.983	3.232	3001	1.926	3.251	2001	4.177	1.373	4.086	1.402
2.809	3.569	3001	2.801	3.590	2001	5.495	1.912	5.485	1.944
2.713	3.559	3001	2.668	3.544	2001	5.343	1.836	5.272	1.671
2.632	3.506	3001	2.624	3.525	2001	5.214	1.610	5.201	1.847
2.446	3.468	3001	2.440	3.453	2001	4.917	1.750	4.847	1.726
2.323	3.394	3001	2.313	3.422	2001	4.721	1.632	4.705	1.677
2.279	3.378	3001	2.269	3.407	2001	4.650	1.606	4.634	1.653
2.269	3.407	3001	2.254	3.392	2001	4.634	1.653	4.563	1.623
2.224	3.392	3001	2.235	3.362	2001	4.553	1.629	4.580	1.561
2.180	3.377	3001	2.136	3.362	2001	4.492	1.604	4.421	1.580
2.058	3.298	3001	2.047	3.331	2001	4.298	1.479	4.279	1.531
2.014	3.282	3001	1.958	3.301	2001	4.227	1.453	4.137	1.493
1.926	3.251	3001	1.914	3.266	2001	4.086	1.402	4.066	1.453
2.801	3.590	3001	2.751	3.594	2001	5.485	1.944	5.404	1.951
2.713	3.559	3001	2.706	3.579	2001	5.343	1.836	5.332	1.927
2.706	3.579	3001	2.651	3.565	2001	5.332	1.927	5.261	1.904
2.661	3.565	3001	2.668	3.544	2001	5.261	1.904	5.272	1.671
2.624	3.529	3001	2.617	3.550	2001	5.201	1.847	5.190	1.881
2.446	3.468	3001	2.443	3.456	2001	4.917	1.750	4.976	1.811
2.402	3.453	3001	2.394	3.477	2001	4.847	1.726	4.833	1.765
2.394	3.477	3001	2.304	3.448	2001	4.833	1.765	4.691	1.719
2.306	3.448	3001	2.313	3.422	2001	4.631	1.719	4.705	1.677
2.260	3.434	3001	2.215	3.419	2001	4.620	1.695	4.548	1.672
2.180	3.377	3001	2.171	3.405	2001	4.537	1.606	4.477	1.569
2.171	3.405	3001	2.126	3.390	2001	4.477	1.649	4.406	1.626
2.126	3.390	3001	2.136	3.362	2001	4.406	1.626	4.421	1.580
2.047	3.331	3001	2.037	3.361	2001	4.279	1.531	4.263	1.579
1.995	3.301	3001	1.992	3.347	2001	4.137	1.483	4.192	1.556
1.914	3.246	3001	1.948	3.332	2001	4.066	1.459	4.120	1.533
2.013	3.697	3001	2.068	3.683	2001	5.823	2.116	5.751	2.094
2.751	3.594	3001	2.759	3.628	2001	5.404	1.951	5.465	2.006
2.617	3.550	3001	2.609	3.573	2001	5.190	1.881	5.178	1.918
2.443	3.506	3001	2.475	3.532	2001	4.976	1.811	4.963	1.852
2.430	3.518	3001	2.385	3.505	2001	4.891	1.830	4.820	1.808
2.250	3.434	3001	2.251	3.463	2001	4.620	1.695	4.605	1.742
2.251	3.463	3001	2.206	3.450	2001	4.605	1.742	4.533	1.720
2.206	3.450	3001	2.215	3.419	2001	4.533	1.720	4.548	1.672
2.286	3.450	3001	2.161	3.436	2001	4.533	1.720	4.461	1.698
2.037	3.361	3001	2.026	3.394	2001	4.263	1.573	4.246	1.633
2.026	3.394	3001	1.981	3.381	2001	4.266	1.633	4.175	1.611
1.981	3.381	3001	1.981	3.347	2001	4.175	1.611	4.192	1.556
1.948	3.352	3001	1.981	3.381	2001	4.120	1.583	4.175	1.611
1.443	3.216	3001	1.398	3.202	2001	3.315	1.347	3.243	1.325
3.813	3.697	3001	3.853	3.728	2001	5.823	2.116	5.867	2.166
2.968	3.683	3001	2.918	3.650	2001	5.751	2.094	5.670	2.104

2.789	3.620	3001	2.737	3.630	2001	5.465	2.006	5.302	2.021
2.609	3.573	3001	2.557	3.506	2001	5.170	1.910	5.004	1.939
2.875	3.532	3001	2.566	3.568	2001	4.963	1.852	4.750	1.897
2.630	3.510	3001	2.621	3.547	2001	4.691	1.830	4.670	1.677
2.385	3.505	3001	2.376	3.534	2001	4.820	1.808	4.806	1.856
2.206	3.509	3001	2.136	3.463	2001	4.661	1.815	4.517	1.773
2.206	3.559	3001	2.136	3.483	2001	4.533	1.720	4.517	1.773
2.196	3.403	3001	2.151	3.470	2001	4.517	1.773	4.445	1.753
2.151	3.470	3001	2.151	3.436	2001	4.445	1.753	4.445	1.698
1.943	3.301	3001	1.925	3.405	2001	4.175	1.611	4.005	1.649
1.843	3.216	3001	1.829	3.263	2001	3.915	1.467	3.292	1.622
1.929	3.263	3001	1.890	3.202	2001	3.292	1.622	3.243	1.325
1.853	3.728	3001	3.053	3.764	2001	5.887	2.156	5.879	2.192
2.310	3.690	3001	2.312	3.700	2001	5.670	2.104	5.662	2.133
2.737	3.630	3001	2.731	3.659	2001	5.382	2.021	5.373	2.055
2.557	3.566	3001	2.550	3.611	2001	5.094	1.939	5.083	1.970
2.557	3.611	3001	2.559	3.586	2001	5.083	1.970	4.938	1.939
2.559	3.566	3001	2.566	3.560	2001	4.938	1.939	4.950	1.897
2.821	3.547	3001	2.814	3.574	2001	4.878	1.877	4.866	1.919
2.414	3.574	3001	2.369	3.562	2001	4.866	1.919	4.793	1.900
2.359	3.562	3001	2.376	3.534	2001	4.793	1.900	4.806	1.856
2.286	3.589	3001	2.278	3.538	2001	4.661	1.815	4.649	1.861
2.278	3.538	3001	2.187	3.513	2001	4.649	1.861	4.504	1.822
2.167	3.513	3001	2.196	3.483	2001	4.504	1.822	4.517	1.773
1.925	3.505	3001	1.961	3.452	2001	4.085	1.682	4.162	1.725
3.040	3.744	3001	3.044	3.761	2001	5.879	2.192	5.873	2.217
2.912	3.708	3001	2.953	3.730	2001	5.662	2.133	5.727	2.101
2.731	3.659	3001	2.726	3.681	2001	5.373	2.055	5.364	2.090
2.607	3.681	3001	2.652	3.689	2001	4.855	1.962	4.782	1.945
1.861	3.652	3001	1.997	3.640	2001	4.142	1.725	4.200	1.790
3.044	3.761	3001	2.995	3.764	2001	5.873	2.217	5.794	2.224
2.955	3.730	3001	2.949	3.754	2001	5.727	2.101	5.721	2.207
2.726	3.681	3001	2.675	3.690	2001	5.364	2.055	5.283	2.104
2.601	3.601	3001	2.601	3.625	2001	4.655	1.962	4.645	2.001
2.382	3.589	3001	2.355	3.615	2001	4.782	1.964	4.772	1.986
1.997	3.490	3001	1.930	3.529	2001	4.200	1.790	4.106	1.847
2.995	3.764	3001	2.937	3.791	2001	5.796	2.226	5.761	2.267
2.949	3.754	3001	2.991	3.781	2001	5.721	2.207	5.700	2.251
2.675	3.690	3001	2.716	3.722	2001	5.283	2.104	5.348	2.156
2.491	3.625	3001	2.395	3.652	2001	4.645	2.001	4.835	2.045
2.349	3.642	3001	2.355	3.615	2001	4.762	2.029	4.772	1.984
2.120	3.593	3001	2.074	3.583	2001	4.396	1.949	4.323	1.933
1.990	3.529	3001	2.020	3.573	2001	4.189	1.847	4.249	1.910
3.037	3.791	3001	3.034	3.808	2001	5.861	2.257	5.856	2.293
2.991	3.781	3001	2.980	3.799	2001	5.780	2.251	5.782	2.270
2.716	3.722	3001	2.711	3.744	2001	5.348	2.156	5.341	2.190
2.120	3.593	3001	2.113	3.625	2001	4.396	1.949	4.385	2.000
2.113	3.625	3001	2.067	3.615	2001	4.385	2.000	4.312	1.985
2.067	3.615	3001	2.074	3.583	2001	4.312	1.985	4.323	1.933
2.020	3.573	3001	2.057	3.5615	2001	4.249	1.910	4.312	1.905
3.034	3.808	3001	3.031	3.821	2001	5.856	2.293	5.852	2.314
2.985	3.799	3001	2.985	3.813	2001	5.782	2.270	5.778	2.300
2.711	3.744	3001	2.662	3.753	2001	5.341	2.190	5.262	2.205
2.067	3.615	3001	2.106	3.651	2001	4.312	1.985	4.377	2.062
3.031	3.821	3001	3.028	3.837	2001	5.852	2.314	5.847	2.340
2.995	3.813	3001	2.982	3.830	2001	5.778	2.280	5.773	2.324
2.662	3.753	3001	2.612	3.760	2001	5.262	2.205	5.182	2.229
2.519	3.752	3001	2.573	3.745	2001	5.036	2.206	4.960	2.192
2.149	3.690	3001	2.103	3.683	2001	4.442	2.105	4.368	2.093
2.108	3.651	3001	2.030	3.667	2001	4.377	2.062	4.220	2.068
3.026	3.837	3001	3.026	3.854	2001	5.847	2.340	5.843	2.366
2.982	3.830	3001	2.933	3.830	2001	5.773	2.320	5.695	2.344
2.612	3.760	3001	2.654	3.790	2001	5.182	2.229	5.250	2.270
2.088	3.791	3001	2.092	3.784	2001	5.176	2.266	5.182	2.255
2.519	3.752	3001	2.515	3.777	2001	5.036	2.204	5.027	2.244

2.515	3.777	3.031	2.469	3.770	2.001	5.027	2.244	4.553	2.233
2.469	3.170	3.001	2.473	3.745	2.001	4.953	2.233	4.960	2.192
2.376	3.756	3.001	2.330	3.729	2.001	4.805	2.211	4.731	2.200
2.217	3.736	3.001	2.130	3.729	2.001	4.583	2.177	4.506	2.166
2.149	3.690	3.001	2.144	3.722	2.001	4.442	2.135	4.436	2.155
2.103	3.663	3.001	2.198	3.715	2.001	4.358	2.093	4.366	2.144
2.098	3.715	3.001	2.010	3.667	2.001	4.360	2.156	4.220	2.058
2.026	3.654	3.001	2.023	3.664	2.001	5.043	2.166	5.633	2.163
2.933	3.640	3.001	2.977	3.664	2.001	5.635	2.344	5.765	2.183
2.634	3.798	3.001	2.605	3.615	2.001	5.250	2.275	5.170	2.304
2.608	3.791	3.001	2.605	3.615	2.001	5.176	2.266	5.170	2.304
2.605	3.615	3.001	2.556	3.609	2.001	5.170	2.266	5.096	2.294
2.558	3.809	3.001	2.562	3.784	2.001	5.036	2.234	5.102	2.255
2.558	3.809	3.001	2.512	3.602	2.001	4.936	2.211	4.799	2.255
2.376	3.756	3.001	2.372	3.724	2.001	4.793	2.255	4.724	2.245
2.372	3.784	3.001	2.326	3.776	2.001	4.724	2.255	4.731	2.245
2.372	3.784	3.001	2.326	3.776	2.001	4.593	2.177	4.576	2.229
2.237	3.736	3.001	2.233	3.765	2.001	4.593	2.177	4.576	2.229
2.233	3.765	3.001	2.186	3.759	2.001	4.576	2.225	4.502	2.215
2.186	3.759	3.001	2.130	3.729	2.001	4.502	2.215	4.508	2.166
2.144	3.722	3.001	2.093	3.747	2.001	4.436	2.155	4.353	2.195
3.023	3.670	3.001	3.021	3.687	2.001	5.633	2.393	5.336	2.643
2.977	3.664	3.001	2.926	3.676	2.001	5.765	2.333	5.667	2.602
2.695	3.649	3.001	2.648	3.644	2.001	5.315	2.359	5.240	2.350
2.685	3.615	3.001	2.602	3.618	2.001	5.170	2.314	5.156	2.342
2.558	3.809	3.001	2.555	3.813	2.001	5.036	2.234	5.391	2.333
2.512	3.802	3.001	2.506	3.628	2.001	5.022	2.284	5.017	2.324
2.093	3.747	3.001	2.039	3.779	2.001	4.353	2.135	4.346	2.247
3.021	3.687	3.001	3.019	3.903	2.001	5.836	2.613	5.833	2.646
2.928	3.676	3.001	2.973	3.699	2.001	5.687	2.482	5.759	2.638
2.695	3.649	3.001	2.633	3.671	2.001	5.315	2.353	5.311	2.394
2.693	3.671	3.001	2.646	3.644	2.001	5.311	2.334	5.240	2.350
2.602	3.638	3.001	2.595	3.662	2.001	5.156	2.312	5.152	2.379
2.555	3.813	3.001	2.552	3.857	2.001	5.091	2.343	5.087	2.372
2.952	3.857	3.001	2.906	3.853	2.001	5.087	2.343	5.012	2.365
2.506	3.653	3.001	2.508	3.628	2.001	5.012	2.365	5.012	2.365
2.089	3.779	3.001	2.086	3.811	2.001	4.346	2.365	4.346	2.324
1.805	3.784	3.001	1.759	3.776	2.001	4.346	2.254	4.341	2.258
3.019	3.903	3.001	3.018	3.911	2.001	5.833	2.645	5.731	2.667
3.018	3.917	3.001	2.973	3.699	2.001	5.631	2.467	5.759	2.636
2.599	3.662	3.001	2.537	3.681	2.001	5.152	2.379	5.152	2.610
2.504	3.673	3.001	2.467	3.669	2.001	5.009	2.398	4.935	2.691
2.270	3.854	3.001	2.223	3.850	2.001	4.636	2.356	4.561	2.360
2.066	3.611	3.001	2.036	3.634	2.001	4.341	2.296	4.262	2.334
1.930	3.630	3.001	1.943	3.626	2.001	4.185	2.323	4.113	2.322
1.686	3.622	3.001	1.649	3.618	2.001	4.038	2.315	3.964	2.303
1.805	3.784	3.001	1.803	3.814	2.001	4.333	2.254	4.289	2.303
1.803	3.614	3.001	1.759	3.779	2.001	3.899	2.303	3.819	2.247
2.597	3.881	3.001	2.536	3.905	2.001	5.157	2.618	5.156	2.663
2.504	3.873	3.001	2.502	3.895	2.001	5.002	2.398	5.006	2.638
2.502	3.873	3.001	2.455	3.895	2.001	5.005	2.438	4.932	2.633
2.455	3.895	3.001	2.457	3.869	2.001	4.932	2.438	4.935	2.631
2.270	3.654	3.001	2.266	3.683	2.001	4.636	2.366	4.632	2.613
2.266	3.683	3.001	2.221	3.680	2.001	4.632	2.413	4.556	2.606
2.221	3.880	3.001	2.223	3.850	2.001	4.558	2.403	4.551	2.650
2.034	3.834	3.001	2.034	3.867	2.001	4.262	2.334	4.258	2.387
2.034	3.867	3.001	1.987	3.864	2.001	4.256	2.387	4.186	2.382
1.967	3.864	3.001	1.930	3.864	2.001	4.186	2.382	4.186	2.382
1.943	3.826	3.001	1.940	3.861	2.001	4.113	2.372	4.109	2.377
1.940	3.861	3.001	1.893	3.857	2.001	4.109	2.372	4.036	2.372
1.893	3.857	3.001	1.895	3.822	2.001	4.036	2.372	4.036	2.315
1.804	3.810	3.001	1.800	3.651	2.001	3.964	2.383	3.964	2.362
2.596	3.905	3.001	2.594	3.931	2.001	5.156	2.645	5.154	2.683
1.600	3.651	3.001	1.644	3.694	2.001	3.964	2.362	3.955	2.631
2.594	3.931	3.001	2.546	3.953	2.001	5.156	2.683	5.077	2.525
2.486	3.946	3.001	2.359	3.947	2.001	4.852	2.518	4.777	2.515

1.844	3.894	3.001	1.796	3.929	2.001	3.955	2.431	3.870	2.486
2.546	3.953	3.001	2.533	3.976	2.001	5.077	2.529	3.151	2.562
2.405	3.968	3.001	2.805	3.973	2.001	4.892	2.518	4.851	2.557
2.485	3.973	3.001	2.358	3.972	2.001	4.851	2.557	4.776	2.556
2.358	3.972	3.001	2.359	3.947	2.001	4.775	2.556	4.777	2.515
2.830	3.967	3.001	1.383	3.966	2.001	4.252	2.547	4.177	2.545
1.795	3.929	3.001	1.795	3.963	2.001	3.878	2.548	3.877	2.580
2.593	3.976	3.001	2.545	3.998	2.001	5.151	2.562	4.576	2.596
2.038	3.967	3.001	2.829	3.997	2.001	4.752	2.567	4.251	2.585
2.829	3.997	3.001	1.382	3.997	2.001	4.251	2.585	4.176	2.595
1.982	3.997	3.001	1.983	3.966	2.001	4.176	2.595	4.177	2.565
1.795	3.963	3.001	1.795	3.996	2.001	3.877	2.560	3.876	2.594
2.639	4.023	3.001	2.593	4.026	2.001	5.226	2.637	5.151	2.638
2.499	4.023	3.001	2.499	4.025	2.001	5.076	2.596	5.001	2.640
1.795	3.996	3.001	1.795	4.036	2.001	3.876	2.634	3.952	2.658
1.795	3.996	3.001	1.842	4.036	2.001	5.226	2.637	5.302	2.661
2.593	4.024	3.001	2.593	4.041	2.001	5.151	2.638	5.152	2.655
2.499	4.025	3.001	2.546	4.042	2.001	5.001	2.640	5.077	2.658
1.842	4.031	3.001	1.796	4.056	2.001	3.952	2.658	3.878	2.668
2.647	4.038	3.001	2.641	4.073	2.001	5.302	2.661	5.229	2.717
2.593	4.041	3.001	2.594	4.075	2.001	5.152	2.665	5.154	2.721
2.594	4.075	3.001	2.548	4.078	2.001	5.154	2.721	5.079	2.725
2.568	4.078	3.001	2.566	4.042	2.001	5.079	2.725	5.077	2.658
1.796	4.064	3.001	1.845	4.116	2.001	3.878	2.702	3.956	2.705
2.651	4.073	3.001	2.596	4.095	2.001	5.229	2.717	5.156	2.752
2.549	4.098	3.001	2.502	4.101	2.001	5.001	2.757	5.006	2.762
1.845	4.116	3.001	1.893	4.142	2.001	3.956	2.785	4.034	2.827
2.596	4.095	3.001	2.597	4.119	2.001	5.156	2.752	5.159	2.769
2.583	4.098	3.001	2.527	4.122	2.001	5.081	2.757	5.084	2.796
2.502	4.101	3.001	2.504	4.126	2.001	5.006	2.762	5.009	2.802
1.893	4.142	3.001	1.943	4.176	2.001	4.036	2.827	4.113	2.878
2.597	4.119	3.001	2.646	4.135	2.001	5.159	2.789	5.237	2.816
2.551	4.122	3.001	2.553	4.145	2.001	5.084	2.796	5.087	2.833
2.553	4.145	3.001	2.506	4.149	2.001	5.007	2.831	5.013	2.883
2.506	4.149	3.001	2.508	4.126	2.001	5.013	2.839	5.009	2.882
2.506	4.149	3.001	2.549	4.154	2.001	5.013	2.839	4.938	2.846
1.843	4.174	3.001	1.946	4.205	2.001	4.113	2.878	4.118	2.928
2.646	4.135	3.001	2.602	4.166	2.001	5.237	2.816	5.166	2.865
2.596	4.171	3.001	2.509	4.177	2.001	5.092	2.874	5.018	2.883
2.586	4.149	3.001	2.589	4.177	2.001	5.013	2.839	5.018	2.883
2.589	4.177	3.001	2.562	4.182	2.001	5.018	2.683	4.943	2.891
2.462	4.182	3.001	2.459	4.154	2.001	4.943	2.691	4.938	2.846
1.946	4.205	3.001	1.950	4.243	2.001	4.118	2.928	4.124	2.988
2.682	4.166	3.001	2.651	4.181	2.001	5.166	2.865	5.245	2.889
2.685	4.187	3.001	2.558	4.193	2.001	5.171	2.899	5.097	2.909
2.556	4.171	3.001	2.558	4.193	2.001	5.092	2.874	5.097	2.909
2.558	4.193	3.001	2.512	4.200	2.001	5.097	2.909	5.022	2.919
2.512	4.200	3.001	2.509	4.177	2.001	5.022	2.919	5.018	2.883
2.665	4.205	3.001	2.619	4.212	2.001	4.948	2.929	4.874	2.939
1.950	4.243	3.001	2.000	4.268	2.001	4.124	2.988	4.205	3.023
2.651	4.181	3.001	2.608	4.200	2.001	5.245	2.889	5.176	2.933
2.605	4.187	3.001	2.608	4.209	2.001	5.171	2.899	5.176	2.933
2.608	4.209	3.001	2.582	4.212	2.001	5.176	2.933	5.102	2.944
2.562	4.212	3.001	2.558	4.193	2.001	5.102	2.944	5.097	2.909
2.665	4.206	3.001	2.669	4.229	2.001	4.948	2.929	4.933	2.967
2.669	4.229	3.001	2.422	4.236	2.001	4.953	2.967	4.879	2.978
2.622	4.236	3.001	2.619	4.212	2.001	4.879	2.978	4.874	2.939
2.608	4.268	3.001	2.651	4.292	2.001	4.205	3.029	4.206	3.067
2.608	4.209	3.001	2.474	4.268	2.001	5.176	2.933	4.961	3.015
2.651	4.292	3.001	2.104	4.323	2.001	4.236	3.067	4.378	3.116
2.674	4.268	3.001	2.578	4.283	2.001	4.961	3.015	4.968	3.053
2.684	4.323	3.001	2.109	4.352	2.001	4.378	3.116	4.378	3.162
2.678	4.283	3.001	2.684	4.314	2.001	4.968	3.053	4.977	3.101
2.109	4.352	3.001	2.254	4.361	2.001	4.378	3.162	4.610	3.177
2.878	4.399	3.001	2.024	4.409	2.001	4.315	3.238	4.283	3.253
2.809	4.265	3.001	2.763	4.276	2.001	5.497	3.024	5.424	3.040

