

AD-A059 813

ARIZONA UNIV TUCSON

EXCITATION OF A WIRE IN A RECTANGULAR CAVITY. VOLUME II. COMPUT--ETC(U)

F/6 20/14

MAY 78 D B SEIDEL

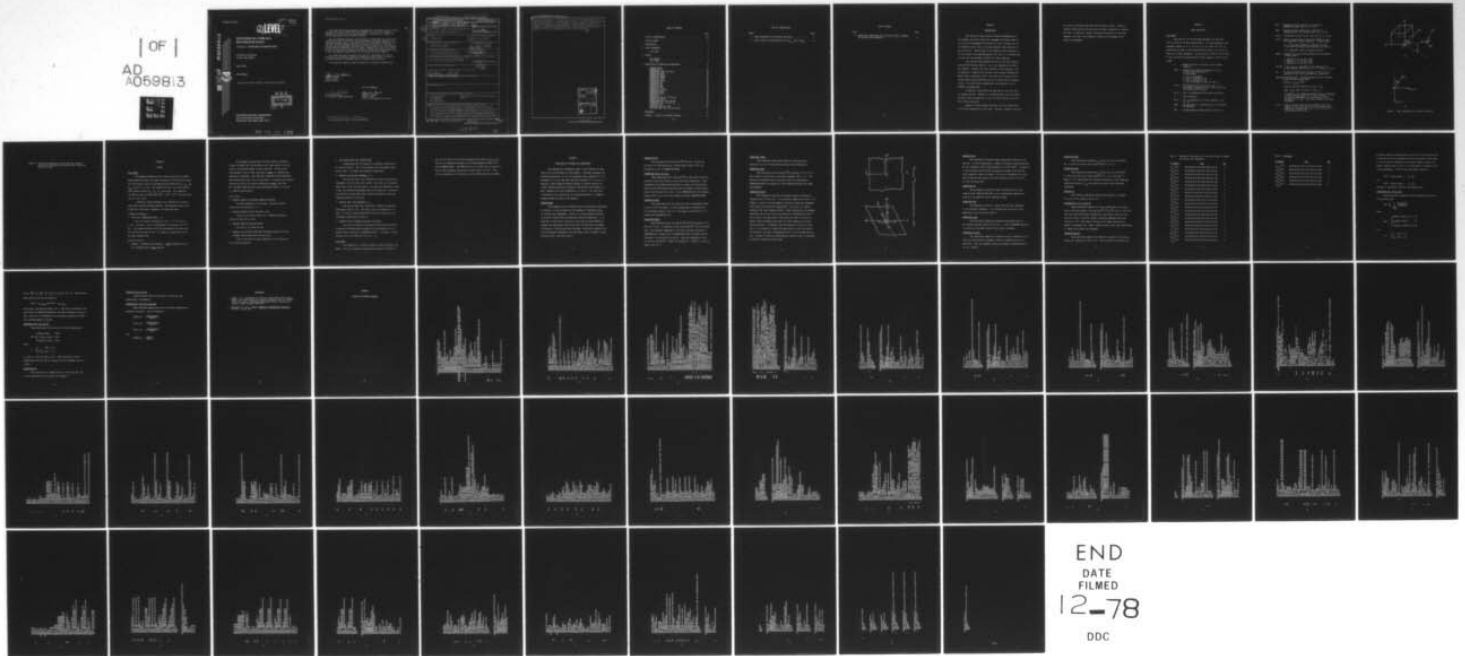
AFOSR-76-3009

UNCLASSIFIED

AFWL-TR-77-221-VOL-2

NL

[OF]
AD 69813



END
DATE
FILMED
12-78
DDC

AFWL-TR-77-221

AFWL-TR
77-221

ADE 200165

DDC
② LEVEL III
no

A050074

EXCITATION OF A WIRE IN A RECTANGULAR CAVITY

Volume II: COMPUTER DOCUMENTATION

University of Arizona
Tucson, AZ 85724

May 1978

Final Report

Approved for public release; distribution unlimited.

AD A059813

DDC FILE COPY



DDC
RECEIVED
OCT 17 1978
RECEIVED
SW
B

AIR FORCE WEAPONS LABORATORY
Air Force Systems Command
Kirtland Air Force Base, NM 87117

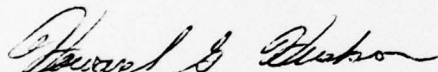
78 09 05 126

This final report was prepared by the University of Arizona, Tucson, Arizona, through AFOSR Grant 76-3009, Job Order 12090525 with the Air Force Weapons Laboratory, Kirtland Air Force Base, New Mexico. Capt Howard G. Hudson (ELT) was the Laboratory Project Officer-in-Charge.

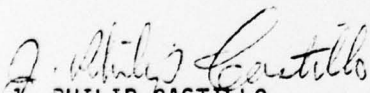
When US Government drawings, specifications, or other data are used for any purpose other than a definitely related Government procurement operation, the Government thereby incurs no responsibility nor any obligation whatsoever, and the fact that the Government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

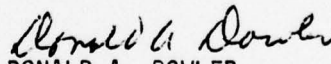
This report has been reviewed by the Office of Information (OI) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.


HOWARD G. HUDSON
Captain, USAF
Project Officer

FOR THE COMMANDER


J. PHILIP CASTILLO
Acting Chief, Technology Branch


DONALD A. DOWLER
Colonel, USAF
Chief, Electromagnetics Division

UNCLASSIFIED

AD-E200 165

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

19 REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM	
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER	
1 AFWL-TR-77-221, Vol II - Vol-2			
4. TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED		
EXCITATION OF A WIRE IN A RECTANGULAR CAVITY, Volume II, Computer Documentation.	Final Report.		
7. AUTHOR(s)	8. CONTRACT OR GRANT NUMBER(s)		
10 D. B. Seidel	15 AFOSR-76-3009		
9. PERFORMING ORGANIZATION NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS		
University of Arizona Tucson, Arizona 85724	16 64747F 12090525 1245		
11. CONTROLLING OFFICE NAME AND ADDRESS	12. REPORT DATE		
Air Force Weapons Laboratory (ELT) Kirtland Air Force Base, NM 87117	11 May 1978		
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)	13. NUMBER OF PAGES		
Air Force Office of Scientific Research (NP) Bolling Air Force Base, Wash D C 20332	58		
	15. SECURITY CLASS. (of this report)		
	UNCLASSIFIED		
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE		
16. DISTRIBUTION STATEMENT (of this Report)			
Approved for public release; distribution unlimited.			
18 AFWL, SBIE			
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)			
18. SUPPLEMENTARY NOTES			
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)			
Rectangular Cavity		Dyadic Green's Functions for Rectangular	
Small Aperture		Cavity	
Wire Scatterer			
Shielding Effects			
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) (UNCLASSIFIED)			
<p>In this work, the problem of determining the currents excited on a wire enclosed within a rectangular cavity is considered. The wire and cavity interior are excited by electromagnetic sources exterior to the cavity which couple to the cavity interior through a small aperture in the cavity wall. It is assumed that the wire is thin, straight and oriented perpendicular to one of the cavity walls. An integral equation is formulated for the problem in the frequency domain using equivalent dipole moments to approximate the</p>			

1264 p.

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

over

033 800

LB

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

effects of the aperture. This integral equation is then solved numerically by the method of moments. The dyadic Green's functions for this problem are difficult to compute numerically; consequently, extensive numerical analysis is necessary to render the solution tractable. Sample numerical results are presented for representative configurations of cavity, wire and aperture, and suggestions for future extensions of this work are discussed.



ACCESSION for	
NTIS	White Section <input checked="" type="checkbox"/>
DDC	Buff Section <input type="checkbox"/>
UNANNOUNCED	<input type="checkbox"/>
JUSTIFICATION _____	
BY _____	
DISTRIBUTION/AVAILABILITY CODES	
Dist.	_____ and/or SPECIAL
A	

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

TABLE OF CONTENTS

	Page
LIST OF ILLUSTRATIONS	iii
LIST OF TABLES	iv
1. INTRODUCTION	1
2. INPUT PARAMETERS	3
File INPUT	3
3. OUTPUT	7
File OUTPUT	7
File PUNCH	9
4. DESCRIPTION OF PROGRAM AND SUBPROGRAMS	11
PROGRAM START	11
SUBROUTINE FILL	12
SUBROUTINES FILL1 and FILL2	12
SUBROUTINE GETUM	12
SUBROUTINE MORFIL	12
SUBROUTINE INVERS	13
SUBROUTINE FIXUP	13
SUBROUTINE DPLFIX	13
SUBROUTINE EAP	15
SUBROUTINE INC	15
SUBROUTINE CONV	15
SUBROUTINE ALPHA	15
SUBROUTINE ELLIPTIC	15
SUBROUTINE MDIPL	16
SUBROUTINE EDIPL	16
FUNCTION S3	16
SUBROUTINES GA, GF, GM and GE	16
SUBROUTINE BADSUM	16
SUBROUTINES GM1, GM2 and GM3	19
SUBROUTINES NSS, NCC and NSC	20
SUBROUTINE NDE	20
FUNCTIONS COSH and SINH	21
FUNCTIONS RSS, RCC, RCS and RSINH	21
REFERENCES	22
APPENDIX - LISTING OF COMPUTER PROGRAMS	23

LIST OF ILLUSTRATIONS

Figure	Page
1. Input Parameters for Incident Plane Wave	5
2. Points Used for Interpolation of (a) $\hat{G}_{A_{nn}}$, and (b) $\hat{g}_{F_{11}}$. .	14

LIST OF TABLES

Table	Page
1. Appropriate subroutine call and value of GEZ to compute the various dyad components	17

CHAPTER 1

INTRODUCTION

This report has been written to provide documentation to the computer code which numerically implements the theory found in [1] for the electromagnetic excitation of a thin, straight wire in a rectangular cavity which is excited through a small aperture in the cavity wall. Because many of the equations and discussions in [1] are crucial to an understanding of this code, it is assumed that the user has that document available for ready reference.

This code has been prepared for use on a CDC 6400 computer using the RUN fortran compiler. It is also compatible with CDC's FTN compiler. However, for later versions of this compiler it may be necessary to suppress the non-fatal error message "ARGUMENT TOO SMALL" which is detected in EXP. This error will naturally occur during normal program execution and has no effect upon the program output. This error can be suppressed by an appropriate call to SYSTEMC in program START.

In addition, every effort has been made to write the code in standard fortran. However, it is expected that a few minor modifications might be needed for its use on non-CDC machines and with other fortran compilers.

Chapter 2 of this document provides a list and description of all input parameters for this code. Similarly, chapter 3 outlines

the various information which the code returns as output. These two chapters should provide the user with the needed information to operate the code. In addition, chapter 4 discusses the function of each sub-program in the code, and a complete listing of all programs can be found in the appendix.

CHAPTER 2

INPUT PARAMETERS

File INPUT

Note that all of the following parameters are read from the file INPUT in the main program START. All input parameters that represent lengths (A, B, C, XC, YC, R, ZL, ZU, LBDA, XPP, YPP, RA, DELFIX) may be input in any system of units desired, so long as the same unit is used throughout. Also note that if LBDA is set to unity, it has the effect of normalizing all other lengths in units of wavelength.

- N -- Number of pulses to be used in wire current expansion
- IGRD -- Integer which indicates connection of wire to one or both cavity walls.
If IGRD equals:
 - 0, wire is unattached
 - 1, wire is attached at $z=0$
 - 1, wire is attached at $z=c$
 - 2, wire is attached at both $z=0$ and $z=c$
- A,B,C -- The dimensions of the cavity in the x, y, z directions, respectively (note that cavity must be oriented such that $A \leq B$)
- XC,YC -- The x-y coordinates of the center of the wire
- R -- The wire radius
- ZL,ZU -- The z coordinates of the wire endpoints, with $ZL < ZU$
- LBDA -- The wavelength (λ) associated with the frequency of operation
- NSM -- Maximum number of terms used for the sum S3

- MAX -- Maximum value of m permitted in the sum of
SUBROUTINE BADSUM (See [1], p. 57-58)
- MAXX -- Maximum value of m permitted in the sums of
subroutines GM1, GM2, and GM3 (See [1], p. 57-58)
- CS,LS -- Convergence criteria for all sums (See [1], p. 57-59)
- ADYAD -- Logical variable which controls the method in which
the components of \bar{G}_e are computed. If ADYAD equals:
- (.T.) first-order difference techniques are used
to calculate \bar{G}_e from \bar{G}_A using equation (2.2) from [1].
- (.F.) components of \bar{G}_e are computed directly
- NWALL -- Indicates the cavity wall perforated by the aperture.
If NWALL equals:
- 1, aperture is in x=0 wall ($\hat{n}=\hat{x}$)
2, aperture is in y=0 wall ($\hat{n}=\hat{y}$)
3, aperture is in z=0 wall ($\hat{n}=\hat{z}$)
- XPP,YPP -- The x_1 and x_2 coordinates of the centerpoint of
of the aperture, such that $\hat{a}_1 \times \hat{a}_2 = \hat{n}$ (see [1], p. 23)
- RA -- An array containing the semi-axes of the elliptical
aperture in the x_1 and x_2 dimensions, respectively
- EMAG,PHASAP,THE,PHI,ANG -- Parameters controlling the incident
plane wave excitation, where
- $$\bar{E}^{inc}(\bar{r}) = \hat{a}_e |E_o| e^{-jk \cdot \bar{R}}$$
- where \hat{a}_e and \hat{k} are defined in Figure 1 with
- $$EMAG = |E_o|, THE = \theta^i, PHI = \phi^i, ANG = \psi^i.$$
- If PHASAP = (.F.), phase of incident field is referenced
to the coordinate origin ($\bar{R} = \bar{r}$) and if PHASAP = (.T.),
the phase is referenced to the centerpoint of the
aperture ($\bar{R} = \bar{r} - \bar{r}_a$). Note that all angles are input
in degrees.
- FIX -- Logical variable which controls whether or not the
effects of the cavity walls upon the aperture dipole
moments are included (See [1], p. 54). If FIX = (.T.),
such effects are included.

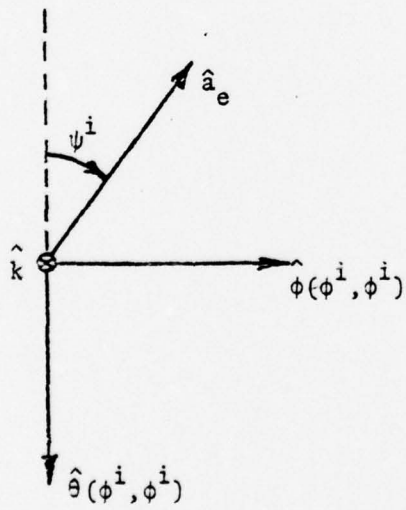
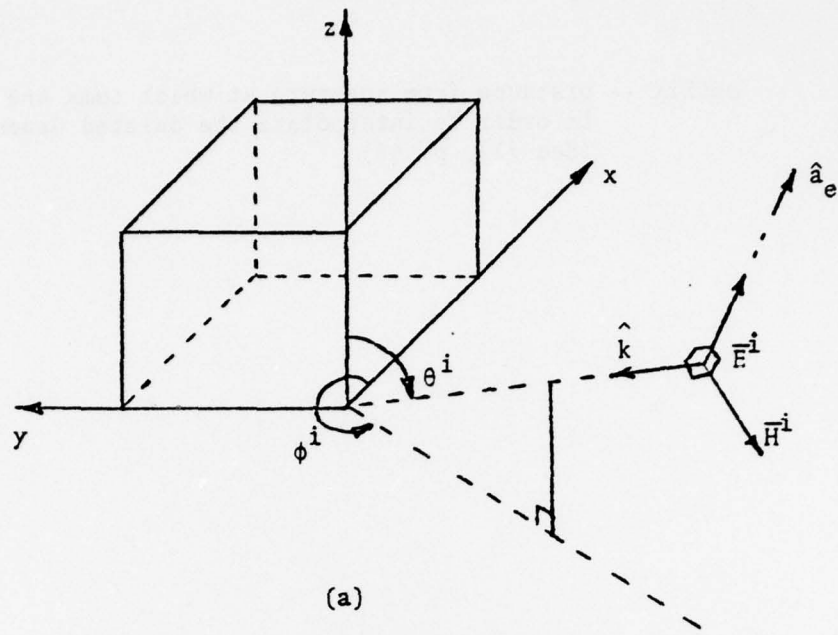


Figure 1. Input Parameters for Incident Plane Wave.

DELFIX -- Distance from aperture at which sums are computed
in order to interpolate the deleted Green's functions
(See [1], p. 68)

CHAPTER 3

OUTPUT

File OUTPUT

The program automatically will create the print file OUTPUT. During normal execution, the input information of the previous chapter will be printed, as well as the aperture polarizabilities α_e , α_{m11} and α_{m22} (see [1], p. 17-19). The solution for the wire current and the total aperture fields (E_{Tn} , H_{T1} , H_{T2}) are given. For comparison, the exterior short circuit fields (E_n^{sc} , H_1^{sc} , H_2^{sc}) are also given (see [1], pp. 20-26).

In addition, several messages of an informative or warning nature may be printed during execution. These messages which can be divided into three basic categories, are described below:

Informative messages --

1. NOTE--W(I) INTERPOLATED THRU I = n

W(I) is an array containing $P(\alpha)$ for $\alpha = (I-1)\Delta$ (see [1], p. 63). For small α , $P(\alpha)$ is interpolated as discussed on p.65 of [1]. This message indicates that this approximation has been made for the first n values of $P(\alpha)$. To reduce n, increase the size of the input parameter MAX.

Non-Fatal Errors --

1. WARNING -- DIMENSION SIZE EXCEEDED -- name1 TRUNCATED TO n. TO FIX, INCREASE SIZE OF name2 ARRAY(S).

This message indicates that the arrays used for temporary storage in BADSUM, GM1, GM2 and GM3 are not large enough to sum the series to the maximum number of terms specified. The particular input parameter (MAX or MAXX, specified by name1) is truncated and execution is continued. Note that this truncation could subsequently cause either fatal error 5 or 6 listed below. To rectify this problem, increase the size of the array(s) specified by name2, such that $MS1 > \max(\text{MAX}, \text{MAXX})$ and $MS2 > \max(c_1 \text{MAX}, c_2 \text{MAXX})$ where $c_1 = B/A$ and $c_2 = \max(A, B, C) / \min(A, B, C)$.

Fatal Errors --

1. WARNING--MATRIX SIZE EXCEEDS STORAGE ALLOCATION

The input parameter N is too large. Decrease N and/or increase MS such that $MS \geq N + 3$.

2. WARNING--REORIENT CAVITY SUCH THAT A.LE.B

A must be less than or equal to B. Redefine coordinate system such that this is true.

3. WARNING--ERROR IN WIRE END POINTS

Note that $ZL < ZU$ must be true

4. WARNING--ALL OR PART OF THE WIRE IS OUTSIDE THE CAVITY, OR UN-ATTACHED WIRE HAS END POINT ON CAVITY WALL

Check to see that the input parameters do not violate any of the above conditions.

5. NOT ENOUGH POINTS FOR INTERPOLATION

Interpolation of $P(\alpha)$ requires its numerical evaluation at at least two points. This is not possible with the present input value of MAX. To correct this problem, increase MAX.

6. WARNING--GMI SUM NOT CONVERGED \underline{c} \underline{l}

The value of MAXX is not sufficient to obtain the specified convergence (CS,LS) in GM1, GM2, or GM3. Note that \underline{c} is the convergence ratio at the last term and \underline{l} is the number of consecutive times, if any, the specified convergence ratio CS has been met. To rectify this problem, increase MAXX and/or reduce the severity of the convergence specified by CS and LS.

7. WARNING--SUM 3 NOT CONVERGED \underline{c} \underline{l}

The value of NSM is not sufficient to obtain the specified convergence (CS,LS) in S3. Note that \underline{c} and \underline{l} are defined as in 6 above. To rectify, increase NSM and/or reduce the severity of the convergence specified by CS and LS.

8. WARNING--CAVITY DIMENSION TOO SMALL FOR DPLFIX

This error is caused by insufficient room inside the cavity to perform the interpolation necessary for the evaluation of the deleted Green's functions in SUBROUTINE DPLFIX. To correct, either decrease the size of DELFIX or let FIX = (.F.).

File PUNCH

The program will in certain situations create the punch file PUNCH. This file contains the information from the file INPUT, as

well as the solution for the wire current and the fields ($E_{T_n}, H_{T_1}, H_{T_2}$).
The file is formatted according to the PUNCH statements found at the
end of PROGRAM START. The PUNCH file will be created only if execution
has not been abnormally halted and if sense switch 1 is "on". This
can be accomplished on CDC machines with the SCOPE control card ONSW(1).

CHAPTER 4

DESCRIPTION OF PROGRAM AND SUBPROGRAMS

The programs and subprograms listed in this chapter are those used in the code described in this document. Uniformly throughout the following description, it is to be understood that variables (X, Y, Z) represent \bar{r} or (x,y,z) and that (XP,YP,ZP) represent \bar{r}' or (x',y',z'). Similarly, other program variables (denoted in capital letters) obviously represent physical variables of the problem (for example, A, B and C represent the cavity dimensions a, b, and c). Only when such a connection is not obvious will it be explicitly noted. A complete program listing is given in the appendix.

PROGRAM START

This program's role is primarily that of input/output operations. In addition, it also provides for the checking of consistency among the various input parameters. Finally, it directs program execution by calling the basic matrix filling and inverting subprograms. It is important to note that if the size of the arrays in blank COMMON are changed, the appropriate values of MS, MS1, and MS2 should be changed accordingly to insure proper error checking. Sufficient dimension size can be obtained by adhering to the algorithms listed in chapter 3 under non-fatal error 1 and fatal error 1.

SUBROUTINE FILL

This subroutine fills the matrix \overline{Q}^a (see [1], p.52,63) for the case of an unattached wire. The necessary values of $P(\beta)$ are provided by a call to SUBROUTINE GETUM.

SUBROUTINES FILL1 and FILL2

These subroutines fill the matrix \overline{Q}^a for the cases of the wire attached to the cavity walls at one or both ends respectively. They incorporate the necessary modifications to account for non-zero half-pulse and the half-testing functions which are needed at the attached ends of the wire (see [1], p.50). As in SUBROUTINE FILL, the necessary values of $P(\beta)$ ([1], p.63) are provided by calling SUBROUTINE GETUM.

SUBROUTINE GETUM

This subroutine fills the array $W(I)$ with the necessary values of $P(\beta)$ to fill the matrix. It will automatically interpolate $P(\beta)$ for sufficiently small β (see [1], p.65) using a three-point fit to a second order polynomial in β .

SUBROUTINE MORFIL

This subroutine fills the matrices \overline{Q}^b and \overline{Q}^c according to (4.7) and (4.8) in [1]. In addition it also initializes \overline{Q}^d to \overline{I} , the identity dyad. The necessary components of the dyads have been calculated in SUBROUTINE EAP (through calls to SUBROUTINES EDIPL and MDIPL) and are contained in the arrays FP, G1 and G2. Note that advantage is taken of the fact that $\overline{G}_e(\overline{r}, \overline{r}') = \overline{G}_e(\overline{r}', \overline{r})$ and $\overline{g}_e(\overline{r}, \overline{r}') = -\overline{G}_H(\overline{r}', \overline{r})$ (see [1], Table 2 and (2.7)).

SUBROUTINE INVERS

This subroutine numerically solves the resulting matrix equation (4.5) in [1] using partial-pivoting Gauss Elimination.

SUBROUTINE FIXUP

This subroutine fills the matrix \bar{Q}^d according to (4.9) in [1]. This routine is called only if the input parameter FIX = (.T.). The values of the deleted Green's functions, which are calculated by SUBROUTINE DPLFIX, are supplied to this subprogram through the common block/WHYNOT/.

SUBROUTINE DPLFIX

This subroutine calculates the deleted Green's functions as outlined on pp. 67-70 of [1]. It is called by START only if FIX = (.T.). Figures 2 (a and b) show arrangement of points at which the components of \bar{G}_A and \bar{g}_F are calculated, respectively. Note that Δ in Figure 2 represents the input parameter DELFIX. These computations are somewhat complicated by the fact that if the aperture is sufficiently close to one or more of the side walls of the cavity the choice of points in Figure 2 must be modified such that all points remain on the cavity interior surface. In addition, when the aperture is close to a side wall, it is necessary to remove the image source in that wall before interpolation, and then to subsequently add it to the interpolated result. Because of these two complications, extensive logic is necessary in DPLFIX to adequately handle them.

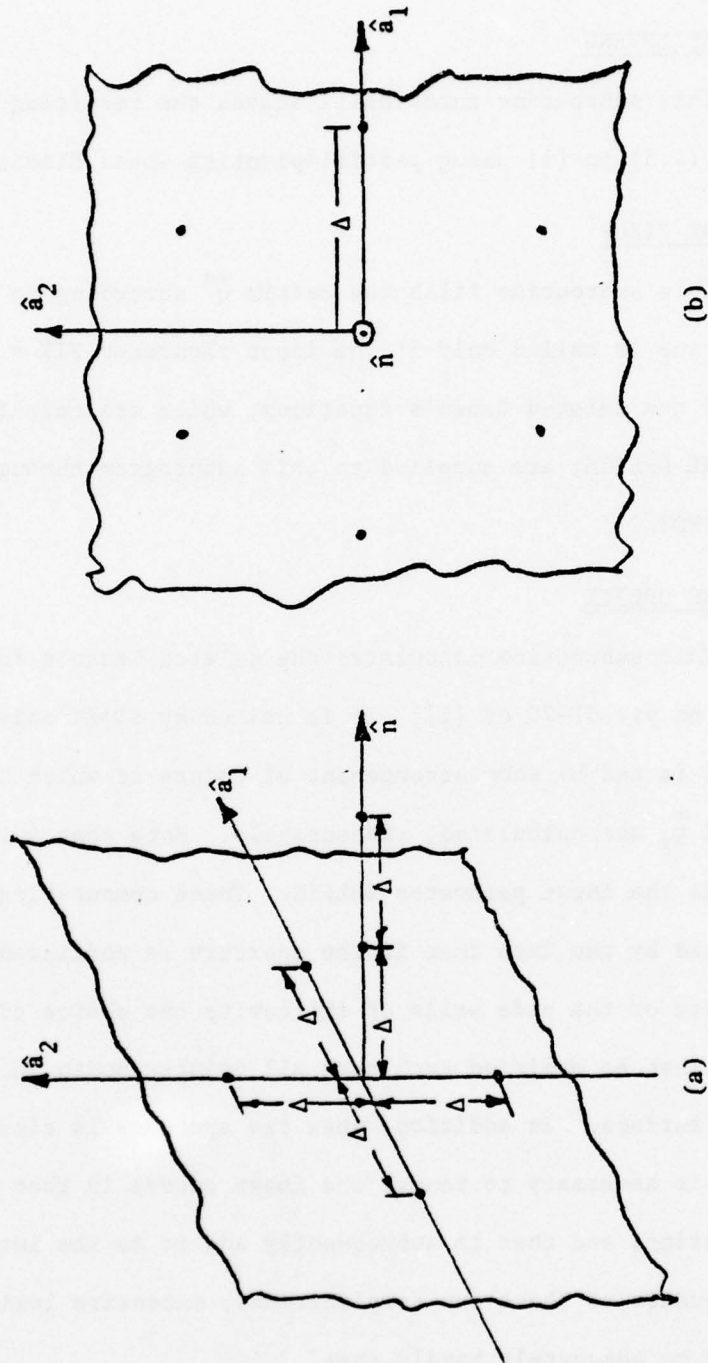


Figure 2. Points Used for Interpolation of (a) $\hat{G}_{A_{nn}}$, and (b) $\hat{G}_{F_{11}}$.

SUBROUTINE EAP

This subroutine calculates several quantities relating to the aperture. It calls subroutines to compute the aperture polarizabilities, and the components of \bar{G}_h and \bar{g}_e necessary to fill \bar{Q}^b and \bar{Q}^c . In addition it calls routines which convert the exterior incident field from the input parameters (shown in Figure 1) to the x,y,z components of E and H. These values are then used to fill the excitation vector in (4.5) of [1] into the array E(I).

SUBROUTINE INC

This subroutine converts the input specifications for the incident field (EMAG,ANG,THE,PHI) to the corresponding components of E and H in the spherical polar coordinate system.

SUBROUTINE CONV

This subroutine converts a vector from its polar components to its cartesian components. It is assumed that the vector is perpendicular to the polar unit vector \hat{r} .

SUBROUTINE ALPHA

This subroutine computes the aperture polarizabilities for the elliptic aperture using (2.15) of [1]. It calls SUBROUTINE ELLIPTIC to provide the necessary values of the elliptic integrals.

SUBROUTINE ELLIPTIC

This subroutine computes the complete elliptic integrals of the first and second kinds of argument X which are denoted EK and E, respectively. They are computed using the polynomial approximations of [2], pp. 591-592.

SUBROUTINE MDIPL

This subroutine calculates $G_{h_{Jz}}(\bar{r}_a, \bar{r}_p)$ for use in the matrix \bar{Q}^c . It fills the array E with these values for $p = 1, N$.

SUBROUTINE EDIPL

This subroutine calculates $G_{e_{Jz}}(\bar{r}_a, \bar{r}_p)$ for use in matrix \bar{Q}^c . It fills the array E with these values for $p = 1, N$. Note that if ADYAD = (.T.), these values are computed indirectly by first computing appropriate values of $G_{A_{zz}}$ and using first-order finite difference techniques.

FUNCTION S3

This function numerically computes the function S_3 , defined by (3.2c) in [1], using (3.16) in [1].

SUBROUTINES GA, GF, GM and GE

These subroutines compute the various components of the dyadic Green's functions needed in the matrices \bar{Q}^b , \bar{Q}^c and \bar{Q}^d (see [1], pp.52-54). Note that these subroutines automatically analytically reduce the sum that will result in the most rapidly converging remaining double sum (see [1], p. 55). Note that IN, SX and SY are dummy arrays and the answer is returned as SD. Table 1 shows the way to call these subroutines to compute any desired dyad component.

SUBROUTINE BADSUM

This subroutine computes the indefinite integral of the reduced kernel $P(\beta)$ defined by (4.22) in [1]. The m-n plane is subdivided into

Table 1. Appropriate subroutine call and value of GEZ to compute the various dyad components.

<u>To Compute</u>	<u>CALL</u>	<u>GEZ</u>
$G_{A_{xx}}(\bar{r}, \bar{r}')$	GA(IN, SX, SY, Y, YP, Z, ZP, X, XP, B, C, A, SD)	F
$G_{A_{yy}}(\bar{r}, \bar{r}')$	GA(IN, SX, SY, Z, ZP, X, XP, Y, YP, C, A, B, SD)	F
$G_{A_{zz}}(\bar{r}, \bar{r}')$	GA(IN, SX, SY, X, XP, Y, YP, Z, ZP, A, B, C, SD)	F
$g_{F_{xx}}(\bar{r}, \bar{r}')$	GF(IN, SX, SY, X, XP, Y, YP, Z, ZP, A, B, C, SD)	F
$g_{F_{yy}}(\bar{r}, \bar{r}')$	GF(IN, SX, SY, Y, YP, Z, ZP, X, XP, B, C, A, SD)	F
$g_{F_{zz}}(\bar{r}, \bar{r}')$	GF(IN, SX, SY, Z, ZP, X, XP, Y, YP, C, A, B, SD)	F
$G_{e_{xx}}(\bar{r}, \bar{r}')$	GA(IN, SX, SY, Y, YP, Z, ZP, X, XP, B, C, A, SD)	T
$G_{e_{xy}}(\bar{r}, \bar{r}')$	GE(IN, SX, SY, XP, X, ZP, Z, YP, Y, A, C, B, SD)	F
$G_{e_{xz}}(\bar{r}, \bar{r}')$	GE(IN, SX, SY, XP, X, YP, Y, ZP, Z, A, B, C, SD)	F
$G_{e_{yx}}(\bar{r}, \bar{r}')$	GE(IN, SX, SY, X, XP, Z, ZP, Y, YP, A, C, B, SD)	F
$G_{e_{yy}}(\bar{r}, \bar{r}')$	GA(IN, SX, SY, Z, ZP, X, XP, Y, YP, C, A, B, SD)	T
$G_{e_{yz}}(\bar{r}, \bar{r}')$	GE(IN, SX, SY, YP, Y, XP, X, ZP, Z, B, A, C, SD)	F
$G_{e_{zx}}(\bar{r}, \bar{r}')$	GE(IN, SX, SY, X, XP, Y, YP, Z, ZP, A, B, C, SD)	F
$G_{e_{zy}}(\bar{r}, \bar{r}')$	GE(IN, SX, SY, Y, YP, X, XP, Z, ZP, B, A, C, SD)	F
$G_{e_{zz}}(\bar{r}, \bar{r}')$	GA(IN, SX, SY, X, XP, Y, YP, Z, ZP, A, B, C, SD)	T
$-G_{h_{xy}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, XP, X, ZP, Z, YP, Y, A, C, B, SD)	F
$G_{h_{xz}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, XP, X, YP, Y, ZP, Z, A, B, C, SD)	F
$G_{h_{yx}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, YP, Y, ZP, Z, XP, X, B, C, A, SD)	F
$-G_{h_{yz}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, YP, Y, XP, X, ZP, Z, B, A, C, SD)	F
$-G_{h_{zx}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, ZP, Z, YP, Y, XP, X, C, B, A, SD)	F
$G_{h_{zy}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, ZP, Z, XP, X, YP, Y, C, A, B, SD)	F

Table 1.--Continued

<u>To Compute</u>	<u>CALL</u>	<u>GEZ</u>
$-g_{e_{xy}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, Y, YP, Z, ZP, X, XP, B, C, A, SD)	F
$g_{e_{xz}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, Z, ZP, Y, YP, X, XP, C, A, B, SD)	F
$g_{e_{yx}}(\bar{r}, \bar{r}')$	GM, IN, SX, SY, X, XP, Z, ZP, Y, YP, A, C, B, SD)	F
$-g_{e_{yz}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, Z, ZP, X, XP, Y, YP, C, A, B, SD)	F
$-g_{e_{zx}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, X, XP, Y, YP, Z, ZP, A, B, C, SD)	F
$g_{e_{zy}}(\bar{r}, \bar{r}')$	GM(IN, SX, SY, Y, YP, X, XP, Z, ZP, B, A, C, SD)	F

elliptical bands as discussed on pp. 55-59 of [1] and the double sum is evaluated using the convergence criteria discussed on those pages. If the sum does not converge in the allotted number of terms, the logical variable CIND is set to (.T.) and control is returned to the calling subprogram. SX and SY are input arrays defined as

$$SX(I) = \text{sink}_x x \text{ sink}_x x' , \quad k_x = \frac{\pi}{a} I$$

and

$$SY(I) = \text{sink}_y y \text{ sink}_y y' , \quad k_y = \frac{\pi}{b} I$$

The input X represents β and $P(\beta)$ is returned as SD.

SUBROUTINES GM1, GM2 and GM3

These subroutines numerically sum two dimensional series of the following form:

$$GM1 = \frac{1}{ab} \sum_{\substack{m=m_0 \\ n=n_0}}^{\infty} \frac{\varepsilon_m \varepsilon_n u v w}{\gamma_c \sinh \gamma_c c}$$

where

$$w_{mn} = \begin{cases} \sinh \gamma_c z < \sinh \gamma_c (c-z) , & I=1 \\ \gamma_c \sinh \gamma_c z \cosh \gamma_c z' , & I=2 \\ \Gamma_1 \cosh \gamma_c z < \cosh \gamma_c (c-z) , & I=3 \end{cases}$$

and

$$\Gamma_1 = \begin{cases} 1 , & \text{GEZ} = (.F.) \\ k_c^2 , & \text{GEZ} = (.T.) \end{cases}$$

for $k_x = \frac{m\pi}{a}$, $k_y = \frac{n\pi}{b}$, $k_c^2 = k_x^2 + k_y^2$ and $\gamma_c^2 = k_c^2 - k^2$. Note that the input arrays SX and SY are defined as

$$SX(I) = u_{(I-1+m_0)} \text{ and } SY(I) = v_{(I-1+n_0)}$$

and m_0 and n_0 can each be either 0 or 1. This sum is performed in the same fashion as SUBROUTINE BADSUM and the same convergence criteria is used. Note that if convergence is not achieved, execution is halted and a warning message is printed.

SUBROUTINES NSS, NCC and NSC

These subroutines fill the array D in the following ways:

$$D(I) = \begin{cases} \sin k_x x \sin k_x x', & (\text{NSS}) \\ \Gamma_2 \cos k_y y \cos k_y y', & (\text{NCC}) \\ k_z \sin k_z z \cos k_z z', & (\text{NSC}) \end{cases}$$

where

$$\Gamma_2 = \begin{cases} 1, & \text{GEZ} = (.F.) \\ k^2 - k_y^2, & \text{GEZ} = (.T.) \end{cases}$$

$k_x = \frac{\pi}{a} I$, $k_y = \frac{\pi}{b} (I-1)$ and $k_z = \frac{\pi}{c} I$. This subroutine is used to appropriately fill the SX and SY arrays for use in BADSUM, GM1, GM2 or GM3.

SUBROUTINE NDE

This subroutine is a dummy routine to call either NSS, NCC or NSC, depending upon the value of the integer L.

FUNCTIONS COSH and SINH

These functions compute the hyperbolic cosine and sine, respectively, of argument X.

FUNCTIONS RSS, RCC, RCS and RSINH

These functions compute the ratios of various combinations of hyperbolic functions. They are defined by

$$\text{RSS}(X,Y,Z) = \frac{\sinh X \sinh Y}{\sinh Z}$$

$$\text{RCC}(X,Y,Z) = \frac{\cosh X \cosh Y}{\sinh Z}$$

$$\text{RCS}(X,Y,Z) = \frac{\cosh X \sinh Y}{\sinh Z}$$

and

$$\text{RSINH}(X,Y) = \frac{\sinh X}{\sinh Y}$$

REFERENCES

1. Seidel, D. B., "Excitation of a Wire in a Rectangular Cavity, Part I: Theory," Air Force Office of Scientific Research, Grant No. AFOSR76-3009, Final Report, Engineering Experiment Station, University of Arizona, Tucson, Arizona, June 1977.
2. Abramowitz, M. and I. Stegun, Handbook of Mathematical Functions, New York: Dover, 1965.

APPENDIX

LISTING OF COMPUTER PROGRAMS

```

PROGRAM START(INPUT,OUTPUT,PUNCH)
LOGICAL GEZ,ADYAD,FIX,PHASAP
COMPLEX Q,D,S,ESC(3)
REAL K,KK,LBDA
DIMENSION RA(2)
COMMON/LAST2/RA,EMAG,ANG,THE,PHI,PHASAP
COMMON/SPEC/GEZ
COMMON/TYPE/ADYAD
COMMON/MN/K
COMMON/FSUM/A,B,C,MAX
COMMON/GM/MAXX
COMMON/GRD/IGRD
COMMON/SUMS/KK,NSM,CS,LS
COMMON/FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
COMMON/LAST/XPP,CHANG,APPR,VALS,MS,HSI AND/OR MS2!!!
C*****WARNING--DO NOT CHANGE DIMENSIONING OF ARRAYS IN BLANK COMMON
C*****WITHOUT CHANGING APPROPRIATE VALUES OF MS,HSI AND/OR MS2!!!
COMMON Q(36,36),SX(86),SY(285)
DATA HS,MS1,MS2/36,86,285/
C*****EIA/376.7/*****
DATA GEZ/.F./
DATA PI/3.1415927/
DATA XAM,XXAM/4H-MAX,4HMAXX/
CALL SSWTCH(1,IPUNCH)
READ IC0,N,IGRD
READ IC1,A,B,C,XC,YC,K,ZL,ZU
READ IC1,LBDA
READ I00,NSM,MAX,MAXX,LS,CS,ADYAD
READ 800,PHASAP,NWALL,XPP,YPP,RA,EMAG,ANG,THE,PHI
READ 202,FIX,DELFIX
N3=N+3
PRINT 99
PRINT 300
IF(IGRD)19,20,21
PRINT 129
ZL=0.23
GOTO 23
7U=C
IF(IGRD.EQ.1)GOTO 31
PRINT 132
GOTO 30
PRINT 131
GOTO 23
PRINT 130
IF(ZL.EQ.0...OR.ZU.EQ.C)GOTO 22

```

```

23      PRINT 301,A,R,C, LBDA
        PRINT 302,R,ZL,ZU,XC, YC
        PRINT 303,NSM,MAX,MAXX,CS,LS,ADYAD
        IF(ZL.LT.0)OR(ZU.GT.C)GOTO 22
        IF(ZU.GT.ZL)GOTO 17
        PRINT 116
        STOP
        IF(XC.LT.A.A.XC.GT.O..A.YC.LT.B.A.YC.GT.O.)GOTO 18
        PRINT 117
        STOP
        IF(A.LE.B)GOTO 11
        PRINT 110
        STOP
        IF(MS.GE.N3)GOTO 12
        PRINT 111
        STOP
        IF(MS1.GI.MAX)GOTO 13
        MAX=MS1-1
        PRINT 112, XAM,MAX
        CON=B/A
        MAX=CON*MAX
        IF(MS2.GI.NAX)GOTO 14
        MAX=(MS2-1)/CON
        PRINT 113, XAM,MAX
        IF(MS1.GI.MAXX)GOTO 15
        MAXX=MS1-1
        PRINT 112, XXAM,MAXX
        CON=AMAX1(A,B,C)/AMIN1(A,B,C)
        MAX=CON*MAXX
        IF(MS2.GI.NAX)GOTO 16
        MAXX=(MS2-1)/CON
        PRINT 113, XXAM,MAXX
        MAX=B/A*MAX
        KK=2.*PI/LBDA
        DEL=(ZU-ZL)/(N+1-IABS(IGRD))
        HDEL=.5*DEL
        CKD=2.*CKD*(K*DEL)
        CON=2.-CKD
        DQ=-.5*S3(YC, XC, XC+R, B, A)
        CALL NSS(SX, XC, XC+R, A, MAX)
        CALL NSS(SY, YC, YC, B, NAX)
        IF(IGRD)1,2,3
        IF(IGRD.EQ.1)GOTO 1
        CALL FILL2(IN, SX, SY, S, Q, MS, DQ)
        GOTO 4
17
22
18
11
12
13
14
15
16
3

```



```

1 2 300 *EXTERIOR*/25X*REAL*14X*IMAGINARY*18X*KEAL*14X*IMAGINARY*
301 /710X*EN: #2E20.5,5X,2E20.5/10X*H1: #2E20.5,5X,2E20.5/10X
302 *H2: #2E20.5,5X,2E20.5)
303 *FORMAT(20X*APERTURE DIMENSIONS: A = #E10.3,5X*8 = #E10.3,5X
304 *C = #E10.3,5X*LAMBDA = #E10.3/)
1 *FORMAT(5X*WIRE SIZE AND LOCATION: #/10X*RADIUS = #E10.3,5X
1 *ZL = #E10.3,5X*XC = #E10.3,5X*YC = #E10.3/)
2 *FORMAT(5X*NUMBER OF PULSES USED IN CURRENT EXPANSION: N = #I3/)
3 *FORMAT(5X*CONVERGENCE CRITERION, ETC. #/10X*MAXIMUM TERM FOR
4 *SUM 3: NSM = #I4/10X*MAXIMUM TERM SUM: *
1 *MAX = #I4/10X*CONVERGENCE RATIO: CS = #E10.3/10X
2 *MAXX = #I4/10X*CONVERGENCE RATIO: CS = #E10.3/10X METHOD *
3 *REPEAT IN CALCULATING INCIDENT FIELD (T/F): ADVAD = #L1/)
4 *FORMAT(10X*NOTE--DIPOLE APPROXIMATIONS ACCOUNT FOR WALL RE
1 *FLECTIONS (FIX=.T.) WITH DELFIX=#E10.3/)
2 *FORMAT(L1,11,8E9.2)
3 STOP
4 END

```

```

SUBROUTINE FILL(IN,SX,SY,D,S,Q,MS,DO,W)
1 DIMENSION IN(1),SX(1),SY(1),D(1),S(1),Q(MS,1),
  W(I),
  REAL X,Q,CE
  COMMON /MN/K
  COMMON /FSUM/A,B,C,MAX
  COMMON /FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
  DATA CE / (0.,-376.7) /
  NP=N+1
  NNP=NP+NP
  X=2.*ZL+HDEL
  CALL GETUM(D,DQ,X,NNP,IN,SX,SY)
  DO 2 I=2,NNP
  J=I-1
  S(J)=D(I)-D(J)
  X=HDEL
  CALL GETUM(W,DQ,X,NP,IN,SX,SY)
  D(I)=2.*W(I)
  DO 1 I=2,NNP
  D(I)=W(I)-W(I-1)
  DZ=2.*D(2)-CKD*D(1)
  DO 3 I=1,N
  IP=I+1

```

```

IJ=I+I
Q(I,I)=(DZ+S(IJ-1)+S(IJ+1)-CKD*S(IJ))*CE
IF(I.EQ.N)GOTO3
DO 4 J=IP,N
IJ=I+J
JI=J-I
Q(J,I)=(D(JI)+D(JI+2)+S(IJ-1)+S(IJ+1)
-CKD*(D(JI+1)+S(IJ)))*CE
CONTINUE
RETURN
END

```

1

4 3

```

SUBROUTINE FILLI(IN,SX,SY,S,Q,MS,DO)
DIMENSION IN(1),SX(1),SY(1),S(1),Q(MS,1)
REAL K
COMMON/WN/K
COMMON/FSUM/A,B,C,MAX
COMMON/FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
LOGICAL HI
COMMON/GRD/IGRD
DATA CE/10.,-376.7)/
HI=IGRD.EQ.1
NN=N+N
X=HDEL
NNP=NN+2
NP=N+1
CALL GETUM(S,DQ,X,NN,IN,SX,SY)
DO 1 I=2,NN
J=NNP-I
S(J)=S(J)-S(J-1)
S(1)=2.*S(1)
M=1
IF(HI)M=N
DZ=2.*S(2)-CKD*S(1)
Q(M,M)=CE*DZ
DO 6 J=2,N
JJ=J
IF(HI)JJ=NP-J
Q(JJ,M)=(S(J-1)+S(J+1)-CKD*S(J))*CE
Q(M,JJ)=Q(JJ,M)*2.
DO 2 I=2,N
II=I
IF(HI)II=NP-I

```

1

6

```

DO 2 J=I,N
JJ=J
JJ=NP-J
JI=Y+J
IF(I.EQ.J)GOTO10
IJ=J-I
Q(I,I,JJ)=(S(IJ+2)+S(JI-2)+S(IJ)+S(JI)-CKD*(S(IJ+1)+S(JI-1)))*CE
Q(JJ,II)=Q(II,JJ)
CONTINUE
RETURN
Q(II,II)=(DZ+S(JI-2)+S(JI)-CKD*S(JI-1))*CE
GOTO 3
END

```

3
2
10

```

SUBROUTINE FILL2(IN,SX,SY,S,Q,MS,DQ)
DIMENSION IN(1),SX(1),SY(1),S(1),Q(MS,1)
REAL Q,CE
COMMON/WN/K
COMMON/FSUM/AB,C,MAX
COMMON/FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
LOGICAL HI
COMMON/GRD/IGRD
DATA CE/(0.,-376.7)/
NP=N+1
NNP=NP+2
X=HDEL
NM=N-1
CALL GETUM(S,DQ,X,NP,IN,SX,SY)
DO 1 I=2,NP
J=NNP-I
S(J)=S(J)-S(J-1)
S(1)=2.*S(1)-CKD*S(1)
DZ=2.*S(2)-CKD*S(1)
Q(1,1)=CE*DZ
Q(N,N)=Q(1,1)
Q(1,N)=CE*(2.*S(NM)-CKD*S(N))
Q(N,1)=Q(1,N)
DO 6 J=2,NH
JJ=VP-J
Q(J,1)=(S(J-1)+S(J+1)-CKD*S(J))*CE
Q(JJ,N)=Q(J,1)
Q(1,J)=2.*Q(J,1)
Q(N,JJ)=Q(1,J)

```

1
6

```

DO 2 I=2,N
II=NP-I
IF(I.GT.II) GOTO 4
DO 2 J=i,II
JJ=NP-J
JI=I+J
IF(I.EQ.J)GOTO 10
IJ=J-I
Q(I,J)=(S(IJ+2)+S(JI-2)+S(IJ)+S(JI)-CKD*(S(IJ+1)+S(JI-1)))*CE
Q(I,I,J)=Q(I,J)
Q(J,I,I)=Q(I,J)
Q(J,J,II)=Q(I,J)
CONTINUE
CONTINUE
CONTINUE
RETURN
Q(I,I)=(DZ+S(JI-2)+S(JI)-CKD*S(JI-1))*CE
Q(II,II)=Q(I,I)
GOTO 3
END

```

3
2
4
10

```

SUBROUTINE GETUM(W,DQ,ST,NP,IN,SX,SY)
COMMON/FORMFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
LOGICAL CIND
COMMON/YES/CIND
DIMENSION W(1),IN(1),SX(1),SY(1)
DATA PI/3.1415927/
X=NP*DEL+ST
NP2=NP+1
CIND=.F.
DO 1 I=1,NP
J=NP2-I
X=X-DEL
CALL BADSUM(IN,SX,SY,X,SD)
IF(CIND)GOTO 10
RETURN
PRINT 11,J
FORMAT(10X*NOTE--W(I) INTERPOLATED THRU I=*I2/)
NS=J+1
X=X+DEL
J1=NS+1
X1=X+DEL
IF(J1.GT.NP)GOTO21
CD=.25/PI

```

1
10
11

```

XN=X/R
CC1=W(IN$)-CO*ALOG(XN+SQRT(XN*XN+1.))
XN=X1/R
CC2=W(J1)-CO*ALOG(XN+SQRT(XN*XN+1.))
B=(CC2-X1*CC1/X)/X1/DEL
A=(CC1-B*X)/X
DO 6 I=1,J
X=X+DEL
XN=X/R
W(I)=CO*ALOG(XN+SQRT(XN*XN+1.))+X*(A+B*X)
RETURN 31
STOP
FORMAT(10X*NOT ENOUGH POINTS FOR INTERPOLATION.*)
END

```

6
21
31

```

SUBROUTINE MORFIL(Q,MS,FP,G1,G2,CON)
DIMENSION Q(MS,1),FP(1),G1(1),G2(1),ALPM(2)
COMPLEX Q,CC,CE
COMMON/DIPOLE/XP,YP,ZP,ALPE,ALPM,NWALL
COMMON/GRD/IGRD
COMMON/FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
COMMON/NEXTRA/N1,N2,N3
DATA CE/(0.,-376.7)/
CC=CE*CON
DO 1 I=1,N
Q(I,N1)=CON*ALPE*FP(I)
Q(I,N2)=-CC*ALPM(1)*G1(I)
Q(I,N3)=-CC*ALPM(2)*G2(I)
Q(N1,I)=CE*DEL*FP(I)
Q(N2,I)=DEL*G1(I)
Q(N3,I)=DEL*G2(I)
DO 2 I=N1,N3
DO 3 J=N1,N3
Q(I,J)=(0.,0.)
IF(IGRD.EQ.0.0.IGRD.EQ.1)GOTO 5
DO 4 I=N1,N3
Q(I,1)=Q(I,1)*.5
IF(IGRD.LT.1)RETURN
DO 6 I=N1,N3
Q(I,N)=Q(I,N)*.5
RETURN
END

```

1
3
2
4
5
6

```

C SUBROUTINE INVERS (AM,M1,M2,NPTS,C,B)
SUBROUTINE INVERS INVERTS THE EQUATION AM(I,J) B(J) = C(I) AND RETURN
COMPLEX AM,B,C,TEMP,SUM,BETA
DIMENSION AM(M1,M2),C(M1),B(M2)
IF (NPTS.GT.M1.OR.NPTS.GT.M2) GO TO 1
NM1 = NPTS - 1
DO 690 KK = 1,NM1
KKPI = KK + 1
L = KK
DO 600 I = KKPI,NPTS
D=REAL(AM(I,KK))
P=AIMAG(AM(I,KK))
S=REAL(AM(L,KK))
T=AIMAG(AM(L,KK))
IF ( (L.EQ.KK) ) GT. (S*S+T*T) ) L = I
DO 610 J = KK,NPTS
TEMP=AM(KK,J)
AM(KK,J)=AM(L,J)
AM(L,J)=TEMP
TEMP=C(KK)
C(KK)=C(L)
C(L)=TEMP
DO 690 I = KKPI,NPTS
BETA = AM(I,KK) / AM(KK,KK)
DO 650 J = KKPI,NPTS
C(I,J) = AM(I,J) - BETA*AM(KK,J)
C(NPTS) = C(NPTS) / AM(NPTS,NPTS)
I = NM1
IPI = I + 1
SUM = (0.0,0.0)
DO 700 J = IPI,NPTS
SUM = SUM + AM(I,J)*B(J)
B(I) = ( C(I) - SUM ) / AM(I,I)
I = I - 1
IF ( I.GE.1 ) GO TO 710
PRINT 10
FORMAT (//)
RETURN
END
10 1

```

WARNING - MATRIX SIZE EXCEEDS STORAGE ALLOCATION*

```

SUBROUTINE FIXUP(Q,MS)
REAL K
COMPLEX Q, CHGA, CHGF(2), CE, CK, COK
DIMENSION Q(MS,1), DGX(2), DGYX(2), ALPM(2)
COMMON/WHYNOT/CHGA, CHGF, DGAX, DGAY, DGX, DGYX
COMMON/WN/K
COMMON/FORFILL/N, DEL, HDEL, ZL, XC, YC, R, CKD
COMMON/DIPOLE/XP, YP, ZP, ALPE, ALPM, NWALL
COMMON/NEXTRA/N1, N2, N3
DATA CE/(0., -376.71)
CK=CE*K
COK=K/CE
Q(N1,N1)=1.+ALPE*CHGA
Q(N1,N2)=CK*ALPM(1)*DGX(1)
Q(N1,N3)=-CK*ALPM(2)*DGX(2)
Q(N2,N1)=-COK*ALPE*DGAY
Q(N3,N1)=-COK*ALPE*DGAX
Q(N2,N2)=1.-ALPM(1)*CHGF(1)
Q(N3,N3)=1.-ALPM(2)*CHGF(2)
Q(N3,N2)=-ALPM(2)*DGYX(2)
Q(N2,N3)=-ALPM(1)*DGYX(1)
RETURN
END

```

```

SUBROUTINE DPLFIX(DEL, IN, SX, SY, XPF, YPP, NWALL)
COMPLEX CQ, CHGA, CHGF(2)
REAL K, KK
DIMENSION QX(6), QY(6), QA(6), QB(6), IN(1), SX(1), SY(1), XA(1)
, DGX(2), DGYX(2)
COMMON/WN/K
COMMON/FSUM/A, B, C, MAX
COMMON/SUMS/KK, NSM, CONV, LC
COMMON/WHYNOT/CHGA, CHGF, DGAX, DGAY, DGX, DGYX
DATA PI/3.1415927/
CN=CM/DEL
CQ=CHPLX(0., K/PI/3.)
XKD=K*DEL
CD=CN*COS(XKD)
CDD=.5*CN*COS(2.*XKD)
ZP=0.
XP=XPP
YP=YPP
IF(NWALL-2)1,2,3
CC=4

```

1

1

```

2      AA=B
      BB=C
      GOTO 4
3      CC=B
      AA=C
      RR=A
      GOTO 4
4      CC=C
      AA=A
      BB=B
      Z=ZP+DEL
      IXL=0
      IXU=0
      IYL=0
      IYU=0
      IF(XP+DEL.GE.AA)IXU=1
      IF(YP+DEL.GE.BB)IYU=1
      IF(XP-DEL.LE.0.)IYL=1
      IF(YP-DEL.LE.0.)IYL=1
      IX=IXU+IYL
      IY=IYU+IYL
      IF(IX.EQ.2.0.IY.EQ.2)GOTO 77
      ISUM=IX+IY
      IF(ISUM.EQ.0)GOTO 29
      IF(IXU.EQ.0)GOTO 21
      XS=AA+XP
      YS=Y
      IF(IXL.EQ.0)GOTO 22
      XS=-XP
      YS=Y
      IF(ISUM.EQ.2)GOTO 24
      YS=BB+YP
      XS=XP
      IF(IYL.EQ.0)GOTO 29
      YS=-YP
      XS=XP
      GOTO 29
      IF(IYU.EQ.0)GOTO 25
      YSI=Y+BB
      GOTO 29
      YSI=-YP
      CONTINUE
      CALL GA(IN,SX,SY,XP,YP,ZP,AA,BB,CC,SA)
      SA=SA-CD
      ZI=Z+DEL
      CALL GA(IN,SX,SY,XP,YP,ZI,ZP,AA,BB,CC,SB)

```

21
22
23
24
25
29

```

SB=SB-CDD
IF((ISUM.EQ.0)GOTO 26
ISE=-1
X=XP
Y=YP
XI=X
YI=Y
GOTO 70
DGNN=2.*(SB-SA)/DEL/DEL/3.
GAA=(4.*SA-SB)/9.
D1=DEL
X=XP+DEL
IF(X.LT.AA)GOTO 5
D1=AA-XP
X=AA
SA=0.
GOTO 6
CALL GA(IN,SX,SY,X,XP,YP,YP,ZP,AA,BB,CC,SA)
SA=SA-CM#COS(K*D1)/D1
D2=DEL
XI=XP-DEL
IF(XI.GT.0.)GOTO 7
D2=XP
XI=0.
SB=0.
GOTO 8
CALL GA(IN,SX,SY,XI,XP,YP,YP,ZP,AA,BB,CC,SB)
SB=SB-CM#COS(K*D2)/D2
IF((ISUM.EQ.0)GOTO 27
ISE=0
Z=ZP
ZI=Z
GOTO 70
DGAX=(SA-SB)/(D1+D2)
GAA=GAA+(SA+SB)/6.
D1=DEL
Y=YP+DEL
IF(Y.LT.BB)GOTO 9
Y=BB
D1=BB-YP
SA=0.
GOTO 10
CALL GA(IN,SX,SY,XP,XP,YP,YP,ZP,AA,BB,CC,SA)
SA=SA-CM#COS(K*D1)/D1
D2=DEL
YI=YP-DEL
IF(YI.GT.0.)GOTO 11

```

26

5
6

7
8

27

9
10

.

```

D2=YP
Y1=0.
GOTO 12
CALL GA(IN, SX, SY, XP, Y1, YP, ZP, AA, BB, CC, SB)
SB=SB-CM*COS(K*D2)/D2
IF(IISUM.EQ.0)GOTO 28
ISE=1
X=XP
X1=X
GOTO 70
DGAY=(SA-SB)/(D1+D2)
GAA=GAA+(SA+SB)/6.
IF(IISUM.NE.0)GOTO 72
CHGA=DGNN+K*(GAA+CO)
DD 49 IQD=1,2
CD=.586602540378444
SS=CO
CS=SD
DD 13 I=1,3
DY=CS*DEL
DX=SS*DEL
DY=YP+DY
IF(Y.GT.BB)GOTO 14
IF(Y.LI.0.)GOTO 15
X=XP+DX
DA=DX
IF(X.LI.AA)GOTO 17
DA=AA-XP
SA=0.
GOTO 18
CALL GF(IN, SX, SY, X, XP, Y, YP, ZP, AA, BB, CC, SA)
DAA=DAA+DA
D1=SQRT(DAA+DYY)
SA=SA-CM*COS(K*D1)/D1
QY(I)=DY
QB(I)=SA
X=XP-DX
DA=-DX
IF(X.GT.0.)GOTO 19
DA=-XP
SA=0.
GOTO 20
CALL GF(IN, SX, SY, X, XP, Y, YP, ZP, AA, BB, CC, SA)

```

11 12

28

79

16

17 18

19

```

20  UAA=DA*DA
    DI=SQRT(DAA+DYY)
    SA=SA-CM*COS(K*D1)/D1
    J=I+3
    QX(J)=DA
    QY(J)=DY
    QB(J)=SA
    SSS=SS*CD+CS*SD
    CS=CS*CD-SSS*SD
    ISUM=IXU+IXL+IYU+IYL
    FO=0.
    DFY=0.
    DFXX=0.
    DFXY=0.
    DD 50 I=1,6
    QA(I)=0.
    IF(IQD.EQ.2)GOTO 75
    DX=AA-XP
    IF(DX.GE.XP)IXL=1
    IF(DX.LE.XP)IXU=1
    DX=XB-YP
    IF(DX.GE.YP)IYL=1
    IF(DX.LE.YP)IYU=1
    IF(IXU.EQ.0)GOTO 92
    ISE=1
    XS=2.*AA-XP
    GOTO 30
    IF(IXL.EQ.0)GOTO 93
    ISE=0
    XS=-XP
    GOTO 30
    IF(IYU.EQ.0)GOTO 94
    ISE=1
    YS=2.*#BB-YP
    GOTO 40
    IF(IYL.EQ.0)GOTO 95
    ISE=0
    YS=-YP
    GOTO 40
    IF(IXU+IYU.NE.2)GOTO 96
    ISE=-1
    XS=2.*AA-XP
    YS=2.*#BB-YP
    GOTO 60
    IF(IXU+IYL.NE.2)GOTO 97

```

```

ISE=0 *AA-XP
XS=-YP
GOTO 60
IF(IXL+IYU.NE.2)GOTO 98
ISE=1
XS=-XP
GOTO 60
IF(IXL+IYL.NE.2)GOTO 99
ISE=2
XS=-XP
GOTO 60
I=1,6
QB(I)=QB(I)-QA(I)
D1=QX(1)-QX(4)
D2=QX(2)-QX(5)
D3=QX(3)-QX(6)
D4=QY(1)-QY(3)
G7=(-QX(4)+QB(1))+QX(1)*QB(4))/D1
G8=(-QX(6)+QB(3)+QX(3)*QB(6))/D3
DGY=(G7-G8)/D4
DGXY=((QB(1)-QB(4))/D1 - (QB(3)-QB(6))/D3)/D4
DGXX=2.*((QB(2)/QX(2)-QB(5)/QX(5))/D2+G0/QX(2)/QX(5))
IF(ISUM.EQ.0)GOTO 53
D0 52 I=1,6
QB(I)=QB(I)+QA(I)
G0=G0+FO
DGY=DGY+DFY
DGXX=DGXX+DFXX
DGXY=DGXY+DFXY
CHGF(I00)=DGXX+KK*(G0+CQ)
DGYX(I00)=DGY
XP=YPP
IT=IXU
IYU=IYU
IT=ITL
IYL=IYL
SSS=AA
AA=BB
BB=SSS

```

97

98

99
51
91

52

53

49

```

RETURN
Y=88
DY=Y-YP
DX=DEL
DYY=DY*DY
GOTO 16
Y=0.
DY=-YP
DX=DEL
DYY=DY*DY
GOTO 16
DO 31 I=1,6
DX=XP+QX(I)-XS
DY=QY(I)
R=SQRT(DX*DX+DY*DY)
QA(I)=QA(I)-CM/R
R=R*R*R
FO=FO-CM/R
DFXX=DFXX-2.*CM/R3
IF(I SE)93,93,92
DO 41 I=1,6
DY=YP+QY(I)-YS
R=SQRT(DX*DX+DY*DY)
QA(I)=QA(I)+CM/R
R=ABS(DY)
R3=R*R*R
FO=FO+CM/R
DFY=DFY-CM*DY/R3
DFXX=DFXX-CM/R3
IF(I SE)95,95,94
DO 61 I=1,6
DX=XP+QX(I)-XS
DY=YP+QY(I)-YS
R=SQRT(DX*DX+DY*DY)
QA(I)=QA(I)-CM/R
DX=XP-XS
DY=YP-YS
DXX=DX*DX
RR=SQRT(RR)
R3=R*R*R
R5=R3*RR
FO=FO-CM/R
DFY=DFY+CM*DY/R3

```

14

15

30

31

40

41

60

61

```

62 DFXY=DFXY-3.*CM*DX*DY/R5
77 DFXX=DFXX+CM*(1./R3-3.*DX/R5)
78 IF(ISE)96,97,62
70 IF(ISE.EQ.1)GOTO 98
PRINT 78
STOP
FORMAT(1X*WARNING--CAVITY DIMENSION TOO SMALL FOR DPLFIX*)
DX=X-YS
DY=Y-Z
ZZ1=Z1+Z1*Z1
R=SQR(ZZ1+DX*DX+DY*DY)
SA=SA+CM/R
DX=X1-YS
DY=Y1-ZS
R=SQR(ZZ1+DX*DX+DY*DY)
SB=SB+CM/R
IF(ISUM.EQ.1)GOTO 71
DX=Y-XP
DY=Y-YS1
R=SQR(ZZ1+DX*DX+DY*DY)
SA=SA+CM/R
DX=X1-XP
DY=Y1-YS1
R=SQR(ZZ1+DX*DX+DY*DY)
SB=SB+CM/R
DX=X1-XS
R=SQR(ZZ1+DX*DX+DY*DY)
SB=SB-CM/R
DX=X-XS
DY=Y-YS1
R=SQR(ZZ1+DX*DX+DY*DY)
SA=SA-CM/R
IF(ISE)26,27,28
DX=XP-XS
DY=Y-YS
R=SQR(RR)
R3=R*RR
GAA=GAA-CM/R
DGAX=DGAX+CM*DX/R3
DGAY=DGAY+CM*DY/R3
DGMN=DGMN+CM/R3
IF(ISUM.EQ.1)GOTO 79
DY=Y-YS1
RR=DY*DY

```

62
77
78
70

71
72

```

RR1=RR+DX+DX
R=SQRT(RR1)
R3=R+RR1
GAA=GAA-CM/DY+CM/R
DGAY=DGAY-CM+DX/R3
DGAY=DGAY+CM/RR-CM+DY/R3
DGNN=DGNN-CM/R3+CM/RR/DY
GOTO 79
END

```

```

SUBROUTINE EAP(IN, SX, SY, E, N, FP, G1, G2, CON)
LOGICAL PHASAP
COMPLEX E, C2, CE
DIMENSION E(1), FP(1), G1(1), G2(1), IN(1), SX(1), Y(1)
DIMENSION LN(3), RA(2), ALPHA(2), EC(3), HC(3)
DIMENSION AN(3)
COMMON/DIPOLE/XP, YP, ZP, ALPE, ALPH, NWALL
COMMON/GRD/IGRO
COMMON/LAST/XA, NWAL
COMMON/LAST2/RA, EMAG, ANG, THE, PHI, PHASAP
COMMON/NEXTRA/N1, N2, N3
DATA LN/1, 2, 3/
DATA AN/2HXX, 2HY, 2HZZ/
DATA CE/10., -376.71/
N1=N+1
N2=N+2
N3=N+3
NVAL=NWALL
WHERE=8HDIRIGIN
IF(PHASAP)WHERE=8HAPERTURE
I1=LT(1, NWALL)
I2=LT(2, NWALL)
RX=0.
RY=0.
RZ=0.
NI=N-NWALL-2
IF(NIN)I, 2, 3
XP=XA(1)
YP=YA(1)
ZP=XA(2)
RY=YA(2)
RZ=RA(1)
GOTO 4
YP=0.

```

1

2

```

XP=XA(2)
ZP=XA(1)
RX=RA(2)
RZ=RA(1)
GOTO 4
XP=XA(1)
YP=XA(2)
RY=RA(1)
RY=RA(2)
CALL ALPHA (RA,ALPE,ALPM)
PRINT 101,NWALL,XP,YP,ZP,RX,RY,RZ
PRINT 103,ALPE,AN(I),ALPH(I),AN(I2),ALPH(2)
PRINT 102,THE,PHI,EMAG,ANG,WHERE
J=LN(NWALL)
CALL EDIPL(J,FP,IN,SX,SY,GI,G2,CON)
DO 5 I=1,2
J=LT(I,NWALL)
IF(I.EQ.2) GOTO 6
CALL MDIPL(J,GI,IN,SX,SY)
GOTO 5
CALL MDIPL(J,G2,IN,SX,SY)
CONTINUE (EMAG,ANG,THE,PHI,ET,EP,HT,HP,PHASE)
CALL CONV(EC,ET,EP)
CALL CONV(HC,HT,HP)
J=LN(NWALL)
C2=(1.0)
IF(PHASAP) GOTO 8
C2=C2*CEXP(0.01)*PHASE)
DO 7 I=1,N
E(I)=(0.0)
E(N1)=2.*EC(J)*C2
E(N2)=2.*HC(I1)*C2
E(N3)=2.*HC(I2)*C2
RETURN
FORMAT(5X*APEPTURE LOCATION AND SIZE (WALL*I2)* /
10X*XA = *E10.3,5X*YA = *E10.3,5X*Z = *E10.3 /
10X*RX = *E10.3,5X*RY = *E10.3,5X*RZ = *E10.3 /
*PHI = (*E10.3**PI)/10X*WAVELENGTH FROM MAGNITUDE = *
E10.3/10X*AND E-FIELD POLARIZATION ANGLE = *E10.3/10X
*PHASE OF INCIDENCE POLARIZABILITIES:*/10X*ALPHA-E = *
E10.3,5X*ALPHA-M*2* = *E10.3,5X*ALPHA-M*2* = *E10.3 /
END

```

3

4

6 5

8 7

101

102

103

1 2 1 2 3 1

```

SUBROUTINE INC(E,A,T,P,ET,EP,HT,HP,PH)
DIMENSION ALPH(2)
COMMON/WN/K
COMMON/OVER/ST,CT,SP,CP
COMMON/DIPOLE/XP,YP,ZP,ALPE,ALPH,NWALL
REAL K
DATA PI/3.1415927/
RAD=PI/180.
RT=RAD*A
RP=RAD*P
H=E/376.7
ET=-E*COS(RA)
EP=-E*SIN(RA)
HT=H*SIN(RA)
HP=H*COS(RA)
CT= SIN(RT)
SP= COS(RT)
CP= SIN(RP)
PH=K*(XP*ST+CP+YP*ST+SP+ZP*CT)
RETURN
END

```

```

SUBROUTINE CONV(E,ET,EP)
DIMENSION E(1)
COMMON/OVER/ST,CT,SP,CP
E(1)=ET*CT*CP-EP*SP
E(2)=ET*CT*SP+EP*CP
E(3)=-ET*ST
RETURN
END

```

```

SUBROUTINE ALPHA(R,E,A)
REAL L
DIMENSION R(1),A(1)
DATA PI/3.1415927/
IF(R(2)-R(1))1,20,2
L=R(1)
W=R(2)
IBIG=1
ISM=2
GOTO 3

```

1

```

L=R(2)
W=R(1)
IBIG=2
IX=(L-W)/L
IF(X.LT.1.E-3)GOTO 20
RR=RAT/RAT
EE=1.-RR
CALL ELLIPTIC(EE,FK,FE)
CC=PI+LE*L/3.
A(IBIG)=CC/(FK-FE)
A(C*RR)/FE
RETURN
L=R(1)
E=2.*L*L/3.
A(2)=2.*E
A(1)=A(2)
RETURN
END

```

2

3

20

```

SUBROUTINE ELLIPTIC(X,EK,E)
DIMENSION A(4),B(4),C(4),D(4)
DATA A/.09666344259,.03590092383,.03742563713,.01451196212/
DATA B/.12498593597,.06880248576,.03328355346,.00441787012/
DATA C/.44325141463,.06260601220,.04757383546,.01736506451/
DATA D/.24998368310,.09200180037,.04069697526,.005226449639/
Y=1.-X
Z=ALOG(1./Y)
W=1./38629436112
Q=1.5
R=1.
S=0.
DO I,I=1,4
W=W+A(I)*W
Q=Q+B(I)*W
R=R+C(I)*W
S=S+D(I)*W
EK=P+Q+Z
E=R+S*Z

```

1

RETURN
END

```
SUBROUTINE MOIPL(J,E,IN, SX, SY)
DIMENSION E(1),IN(1),SX(1),SY(1),ALPH(2)
REAL K
COMMON/DIPOLE/XP,YP,ZP,ALPE,ALPH,NWALL
COMMON/FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
COMMON/FSUM/A,B,C,MAX
COMMON/GRD/IGRD
SD=0.
Z=71
IF(IGRD.EQ.-1.OR.IGRD.EQ.2)Z=Z-DEL
XD=XC+R
DO 1 I=1,N
Z=Z+DEL
IF(J.EQ.3)GOTO 1
IF(J.EQ.2)GOTO 2
CALL GM(IN,SX,SY,XD,XP,YP,Z,ZP,A,B,C,SD)
GOTO 1
CALL GM(IN,SX,SY,YP,XD,XP,Z,ZP,B,A,C,SD)
SD=-SD
E(I)=SD
RETURN
END
```

2
1

```
SUBROUTINE EDIPL(J,E,IN, SX, SY, DUM, BUM, CON)
DIMENSION E(1),IN(1),SX(1),SY(1),DUM(1),BUM(1),ALPH(2)
REAL K
LOGICAL GEZ,ADYAD
COMMON/TYPE/ADYAD
COMMON/SPEC/GEZ
COMMON/WN/K
COMMON/DIPOLE/XP,YP,ZP,ALPE,ALPH,NWALL
COMMON/FORFILL/N,DEL,HDEL,ZL,XC,YC,R,CKD
COMMON/FSUM/A,B,C,MAX
COMMON/GRD/IGRD
Z=ZL
IF(IGRD.EQ.-1.OR.IGRD.EQ.2)Z=Z-DEL
CC=1./K
XD=XC+R
IF(J.EQ.3)GOTO 30
```

```

IF(ADYAD)GOTO 20
DO 1 I=1,N
Z=Z+DEL
IF(J.EQ.1)CALL GE(IN,SX,SY,XO,XP,YP,Z,ZP,A,B,C,SD)
IF(J.EQ.2)CALL GE(IN,SX,SY,YC,YP,XO,XP,Z,ZP,A,B,C,SD)
E(I)=CC+SD
RETURN
XD=XO+HDEL
XM=XD-DEL
YM=YD+HDEL
YN=YD-DEL
NP=N+1
Z=ZL-HDEL/DEL
CC=CC/DEL/DEL
DO 2 I=1,NP
Z=Z+DEL
IF(J.EQ.2)GOTO 21
CALL GA(IN,SX,SY,YP,Z,ZP,XD,XP,B,C,A,SD)
CALL GA(IN,SX,SY,YP,Z,ZP,XH,XP,B,C,A,SH)
GOTO 22
CALL GA(IN,SX,SY,Z,ZP,XO,XP,YD,YP,C,A,B,SD)
CALL GA(IN,SX,SY,Z,ZP,XO,XP,YH,YP,C,A,B,SH)
DUM(I)=SD
BUM(I)=SH
DO 3 I=1,N
IP=I+1
E(I)=CC*(DUM(IP)-BUM(IP)-DUM(I)+BUM(I))
RETURN
NP=N+2
Z=ZL-DEL
CC=K/CON
DO 4 I=1,NP
Z=Z+DEL
CALL GA(IN,SX,SY,XO,XP,YP,Z,ZP,A,B,C,SD)
DUM(I)=SD
DO 5 I=1,N
E(I)=CC*(DUM(I)+DUM(I+2)-CKD*DUM(I+1))
RETURN
IF(ADYAD)GOTO 25
GEZ=.T.
DO 6 I=1,N
Z=Z+DEL
CALL GA(IN,SX,SY,XO,XP,YP,Z,ZP,A,B,C,SD)
E(I)=CC+SD
GEZ=.F.
RETURN
END
1
20
21
22
2
3
25
4
5
30
6

```

```

FUNCTION S3(Z,ZP,W,WP,C,D)
COMMON/PEEK/I
COMMON/SUMS/KK,N,CONV,LC
REAL KK,KW,KC,KWW
DATA PI/3.1415927/
X=PI/D
KW=0.
ZL=AMINI(Z,ZP)
ZG=C-AMAXI(Z,ZP)
ARG=X*(C-76-ZL)
CX=COSH(ARG)
SUM=
.125*ALOG((CX-COS(X*(W+WP)))/(CX-COS(X*(W-WP))))/X
L=0
DO 1 I=1,N
KW=KW+X
KWW=KW*KW
SKC=KK-KWW
IF(KWW.GT.KK)GOTO 2
KC=SQT(SKC)
T=SIN (KC*ZL)*SIN (KC*ZG)/SIN (KC*C)/KC
GOTO 3
KC=SQT(-SKC)
T=SINH(KC*ZL)*SINH(KC*ZG)/SINH(KC*C)/KC
TT=SIN(KW*W)*SIN(KW*WP)*(-I*ARG)/KW
SUM=SUM+TT
L=L+1
AB=ABS(TT/SUM)
IF(AB.GT.CONV)L=0
IF(L.EQ.LC) GOTO 4
CONTINUE
PRINT 5,AB,L
STOP
S3=SUM*2./D
FORMAT(10X*WARNING--SUM 3 NOT CONVERGED*E15.5I10)
RETURN
END

```

1

2

3

1

4

5

```

SUBROUTINE GM(IN,SX,SY,X,XP,Y,YP,Z,ZP,A,B,C,SD)
DIMENSION IN(1),SX(1),SY(1)
COMMON /NEUMAN/ MO,NO
LGM=-1
IF(Y.GT.YP)GOTO 5
AS=Y

```

```

5  SIG=-1.
   AC=B-YP
   GOTO 6
   AS=B-Y
   AC=Y-P
   SIG=1.
   GOTO 6
   ENTRY GA
   LGM=0
   GOTO 6
   ENTRY GF
   LGM=1
6  NO=1
   MO=NO
   DX=X-XP
   DY=Y-YP
   DZ=Z-ZP
   RA=1./A/A
   RB=1./B/B
   RC=1./C/C
   ALP=(RB+RC)*DX+DY
   GAM=(RA+RB)*DZ+DZ
   IF(ALP.GT.BET)GOTO 10
   IF(BET.GT.GAM)GOTO 2
   GOTO 3
   IF(ALP.LE.GAM)GOTO 3
   IF(B.GT.C)GOTO 4
   NAX=C*MAX/B
   NG=0
   IF(LGM.EQ.1)MO=0
   CALL NDE(SX,Y,YP,B,MAX,LGM)
   CALL NCC(SY,Z,ZP,C,MAX)
   CALL GHI(IN,SX,SY,X,XP,B,C,A,SD)
   RETURN
   NAX=B*MAX/C
4  MO=0
   IF(LGM.EQ.1)NO=0
   CALL NDE(SY,Y,YP,B,MAX,LGM)
   CALL NCC(SX,Z,ZP,C,MAX)
   CALL GHI(IN,SX,SY,X,XP,C,B,A,SD)
   RETURN
   IF(A.GT.C)GOTO 7
   NAX=C*MAX/A
2  NO=0
   CALL NSS(SX,X,XP,A,MAX)
   CALL NCC(SY,Z,ZP,C,MAX)

```

```

11 IF(LGM)12,11,21
    CALL GH1(IN,SX,SY,Y,YP,A,C,B,SD)
    GOTO 13
12 CALL GM3(IN,SX,SY,Y,YP,A,C,B,SD)
    GOTO 13
13 CALL GM2(IN,SX,SY,AS,AC,A,C,B,SD)
    SD=SIG*SD
    RETURN
    NAX=A*MAX/C
14 MO=0
    CALL NSS(SY,X,XP,A,NAX)
    CALL NCC(SX,Z,ZP,C,MAX)
    IF(LGM)15,14,22
15 CALL GH1(IN,SX,SY,Y,YP,C,A,B,SD)
    GOTO 13
22 CALL GM3(IN,SX,SY,Y,YP,C,A,B,SD)
    GOTO 13
15 CALL GM2(IN,SX,SY,AS,AC,C,A,B,SD)
    SD=SIG*SD
    RETURN
3 IF(A.GT.8)GOTO 8
    NAX=8*MAX/A
    IF(LGM.EQ.1)MO=0
    CALL NSS(SX,X,XP,A,MAX)
    CALL NDE(SY,Y,YP,B,NAX,LGM)
    CALL GM3(IN,SX,SY,Z,ZP,A,B,C,SD)
    RETURN
8 NAX=A*MAX/B
    IF(LGM.EQ.0)MO=0
    CALL NSS(SY,X,XP,A,NAX)
    CALL NDE(SX,Y,YP,B,MAX,LGM)
    CALL GM3(IN,SX,SY,Z,ZP,B,A,C,SD)
    RETURN
    END

```

```

SUBROUTINE GE(IN,SX,SY,X,XP,Y,YP,Z,ZP,A,B,C,SD)
DIMENSION IH(1),SX(1),SY(1)
COMMON /NEUMAN/ MO,NO
COMMON /GM/ MAX
MO=1
NO=1
SIG=1
DX=X-XP
DY=Y-YP
DZ=Z-ZP

```

```

10 RA=1./A/A
11 RB=1./B/B
12 RC=1./C/C
11 ALP=(RB+RC)*DX*DX
11 BET=(RA+RB)*DY*DY
11 GAM=(RA+RB)*DZ*DZ
11 IF(ALP.GT.BET)GOTO 10
11 IF(BET.GT.GAM)GOTO 2
11 GOTO 3
11 IF(ALP.LE.GAM)GOTO 3
11 IF(X.GT.XP)GOTO 12
11 AC=A-X
11 AS=X
11 SIG=-1.
11 GOTO 11
11 AC=XP
11 AS=A-X
11 IF(B.GT.C)GOTO 4
11 NAX=C*MAX/B
11 CALL NSS(SX,Y,YP,B,MAX)
11 CALL NSC(SY,ZP,Z,C,MAX)
11 CALL GM2(IN,SX,SY,AS,AC,B,C,A,SD)
11 SD=SIG*SD
11 GOTO 6
11 NAX=B*MAX/C
11 CALL NSS(SY,Y,YP,B,MAX)
11 CALL NSC(SX,ZP,Z,C,MAX)
11 CALL GM2(IN,SX,SY,AS,AC,C,B,A,SD)
11 SD=SIG*SD
11 GOTO 6
11 IF(A.GT.C)GOTO 7
11 NAX=C*MAX/A
11 CALL NSC(SX,X,XP,A,MAX)
11 CALL NSC(SY,ZP,Z,C,MAX)
11 CALL GM1(IN,SX,SY,Y,YP,A,C,B,SD)
11 GOTO 6
11 NAX=A*MAX/C
11 CALL NSC(SY,X,XP,A,MAX)
11 CALL NSC(SX,ZP,Z,C,MAX)
11 CALL GM1(IN,SX,SY,Y,YP,C,A,B,SD)
11 GOTO 6
11 IF(Z.GT.ZP)GOTO 5
11 AC=Z
11 AS=C-ZP
11 GOTO 13
11 AC=C-Z
11 AS=ZP

```

```

13  SIG=-1.
    IF(A.GT.B)GOTO 8
    NAX=B*MAX/A
    CALL NSC(SX,X,XP,A,MAX)
    CALL NSS(SY,Y,YP,B,MAX)
    CALL GM2(IN,SX,SY,AS,AC,A,B,C,SD)
    SD=SIG*SD
    GOTO 6
8    NAX=A*MAX/B
    CALL NSC(SX,X,XP,A,MAX)
    CALL NSS(SY,Y,YP,B,MAX)
    CALL GM2(IN,SX,SY,AS,AC,B,A,C,SD)
    SD=-SD
6    RETURN
    END

```

```

SUBROUTINE BADSUM(IN,SX,SY,X,SD)
REAL K,KK,KX
DIMENSION IN(1),SX(1),PX(1),SY(1)
LOGICAL CIND
COMMON/YES/CIND
COMMON/WN/K
COMMON/PEEK/M
COMMON/FSUM/A,B,C,MAX
COMMON/SUMS/KK,NSH,CONV,LC
DATA PI/3.1415927/
AR=PI/A
BR=PI/B

```

```

L=0
SBR=BR*BR
CW=C-X
DO 10 M=1,MAX
  IN(M)=0
  BSUM=0.
  DO 1 M=1,MAX
    KX=M*AR*KX
    RR=SKX+SBR
    SUM=0.
  I=M
  N=1
  GOTO 9
  I=I-1
  IF(I.EQ.0)GOTO 7

```

13

8

6

10

2

```

KX=I*AR
SKX=KX*KX
NF=IN(I)+1
IN(I)=SQRT((RR-SKX)/BR)
NL=IN(I)
IF(NF.GT.NL)GOTO 2
DO 3 N=NF,NL
GOTO 9
CONTINUE
GOTO 2
BSUM=BSUM+SUM
L=L+1
AB=ABS(SUM/BSUM)
IF(AB.GT.CONV)L=0
IF(L.EQ.LC)GOTO 4
CONTINUE
CIND=.T.
RETURN
SKY=N*N+SBR-KK
SGC=SKY+SKX-KK
IF(SGC.GT.0.)GOTO 11
GC=SQRT(-SGC)
T=SIN(GC*CW)/SIN(GC*C)
GOTO 12
GC=SQRT(SGC)
T=R*SINH(GC*CW,GC*C)
TT=T+SX(I)*SY(N)/SGC
SUM=SUM+TT
IF(I.EQ.M)GOTO 2
GOTO 6
SD=-BSUM*2./A/B
RETURN
END

```

6 3

7

1

9

11

12

4

```

SUBROUTINE GM1(IN,SX,SY,Z,P,A,B,C,SD)
REAL K,KK,KX,KXX
LOGICAL GEZ
DIMENSION IN(1),SX(1),SY(1)
COMMON /WN/K
COMMON /PEEK/M
COMMON /NEUMAN/MO,NO
COMMON /GH/MAX
COMMON /SUMS/KK,NSM,CONV,LC
COMMON /SPEC/GEZ

```



```

1  IF(AB.GT.CONV)L=0
   IF(L.EQ.LC)GOTO 4
   KXX=KXX+AR
   PRINT 5,IND,AB,L
   STOP
9  SKY=N*N*SBR
   SKC=SKY+SKX
   SGC=SKC-KK
   IF(SGC.GT.0.)GOTO11
   GC=SQRT(-SGC)
13  IF(INDM)13,14,15
   T=SIN(GC*ZL)*SIN(GC*ZG)/SIN(GC*C)/GC
14  T=COS(GC*AC)*SIN(GC*AS)/SIN(GC*C)
15  T=-COS(GC*ZL)*CDS(GC*ZG)/SIN(GC*C)/GC
   IF(GEZ)T=T*SKC
   GOTO 12
11  GC=SQRT(SGC)
   IF(INDM)16,17,18
16  T=RSS(GC*ZL,GC*ZG,GC*C)/GC
17  T=RCS(GC*AC,GC*AS,GC*C)
18  T=RCC(GC*ZL,GC*ZG,GC*C)/GC
12  IF(GEZ)T=T*SKC
   IT=T*SX(I)*SY(N+NN)
   IF(N.EQ.0) IT=.5*IT
   IF(MO+I.EQ.1) IT=.5*IT
   SUM=SUM+IT
   IF(I.EQ.M)GOTO 2
   GOTO 6
4  SD=4.*BSUM/A/B
5  FORMAT(10X*WARNING--GM*11* SUM NOT CONVERGED*E15.5I10)
   RETURN
   END

```

```

SUBROUTINE NSS(D,X,XP,A,M)
DIMENSION D(1)
DATA PI/3.1415927/
AR=PI/A
W=0.
DO 1 I=1,M
W=W+AR
D(I)=SIN(W*X)*SIN(W*XP)
1

```

RETURN
END

SUBROUTINE NCC(D,Z,ZP,C,M)
REAL KK GEZ
LOGICAL SUMS/KK,NSM,CONV,LC
COMMON/SPEC/GEZ
DIMENSION D(1)
DATA PI/3.1415927/
AR=PI/C
D(1)=1.
W=0.
DO I=1,M
W=W+AR
IP=I+1
D(IP)=COS(W+Z)*COS(W+ZP)
IF(GEZ) D(IP)=D(IP)*((KK-W*W)
CONTINUE
IF(GEZ) D(1)=KK
RETURN
END

1

55

SUBROUTINE NSC(D,YS,YC,B,M)
DIMENSION D(1)
DATA PI/3.1415927/
AR=PI/B
W=0.
DO I=1,M
W=W+AR
D(I)=W*SIN(W*YS)+COS(W*YC)
RETURN
END

1

SUBROUTINE NDE(D,Y,YP,B,M,L)
DIMENSION D(1)
IF(L1,2,3
CALL NSC(D,Y,YP,B,M)
RETURN
CALL NSS(D,Y,YP,B,M)
RETURN

1

2

```
3 CALL NCC(D,Y,YP,B,M)
  RETURN
  END
```

```
FUNCTION COSH(X)
  Y=EXP(X)
  COSH=.5*(Y+1./Y)
  RETURN
  END
```

```
FUNCTION SINH(X)
  Y=EXP(X)
  SINH=.5*(Y-1./Y)
  RETURN
  END
```

```
FUNCTION RSS(X,Y,Z)
  RSS=.5*(EXP(X+Y-Z)-EXP(X-Y-Z)-EXP(Y-X-Z)+EXP(-X-Y-Z))
  / (1.-EXP(-Z-Z))
  RETURN
  END
```

```
FUNCTION KCC(X,Y,Z)
  RCC=.5*(EXP(X+Y-Z)+EXP(X-Y-Z)+EXP(Y-X-Z)+EXP(-X-Y-Z))
  / (1.-EXP(-Z-Z))
  RETURN
  END
```

```
FUNCTION RCS(X,Y,Z)
  RCS=.5*(EXP(X+Y-Z)-EXP(X-Y-Z)+EXP(Y-X-Z)-EXP(-X-Y-Z))
  / (1.-EXP(-Z-Z))
  RETURN
  END
```

```
FUNCTION BSINH(X, Y)  
  BSINH=(EXP(X-Y)-EXP(-X-Y))/(1.-EXP(-Y-Y))  
  RETURN  
END
```