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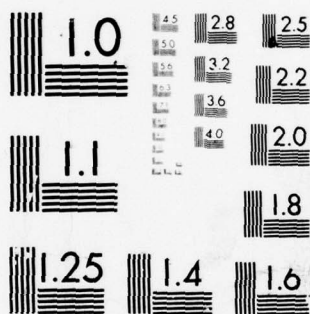
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TECHNICAL REPORT ARBRL-TR-02093

SOURCE: A FORTRAN-IV SUBROUTINE PACKAGE
THAT MODELS SEVERAL NATURALLY OCCURRING
ENERGY INPUTS TO THE MESOSPHERE.

Irving L. Chidsey

August 1978

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US ARMY ARMAMENT RESEARCH AND DEVELOPMENT COMMAND
BALLISTIC RESEARCH LABORATORY
ABERDEEN PROVING GROUND, MARYLAND

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INTRODUCTION

The interaction between the chemical species which make up the upper atmosphere and the energy sources which drive the atmospheric chemistry are primarily two-body 2nd order reactions between the resident chemical species and the flux of incoming photons and energetic particles. The rate constants for the reactions are expressed as interaction cross-sections which can and often do vary rapidly with available energy in addition to being different for each chemical species. Treating these reactions in a straightforward way as two-body reactions and adding them to any atmospheric reaction set would result in an essentially uncalculatable set. The deliberately broad band source models described in this report, which model energy inputs with only 47 solar bands plus photoelectrons, precipitated electrons, and galactic cosmic rays, would be prohibitively unwieldy if combined with the 45 basic chemical species-photon interaction reactions in the ECLIPSE-66 set,¹ or the 60 basic reactions in the BENCHMARK-76 set.² After allowing for those rate constants which are zero in the present sets, or would be zero in the full set, we get an increase from perhaps 40 basic reactions to about 2000 for these two cases.

It is therefore customary to reduce these photon-species reactions to psuedo-first order reactions by taking the sum

$$k_n = \sum_i \phi_i \sigma_{in}$$

where

$n \equiv$ the number of the pseudo first order reaction

$i \equiv$ the wavelength band number

$k \equiv$ psuedo-first order rate constant

$\phi \equiv$ photon flux

$\sigma \equiv$ interaction cross section.

¹F. E. Niles and I. L. Chidsey, "Comparison of Measured and Calculated D-Region Electron Density for Solar Eclipse of 12 November 1966," and I. L. Chidsey and F. E. Niles, "Comparison of Measured and Calculated D-Region Positive-Ion Number Density for Solar Eclipse of 12 November 1966," Trans. AGU 56, 997 (1975).

²J. M. Heimerl and F. E. Niles, "BENCHMARK-76 Model Computations for Disturbed Atmospheric Conditions, I. Input Parameters," BRL Report No. 2022, October 1977; "BENCHMARK-76 Model Computations for Disturbed Atmospheric Conditions, II. Results for the Stratosphere and Mesosphere," BRL Report ARBRL-TR-02050, March 1978; and "BENCHMARK-76 Model Computations for Disturbed Atmospheric Conditions, III. Results for Selected Excitation Parameters at 60 km," BRL Report ARBRL-TR-02051, April 1978. (AD Nos. A050355, A054325, and A054376)

This report documents how we obtained these psuedo-first order rate constants for two studies, ECLIPSE-66¹ and BENCHMARK-76.²

For the ECLIPSE-66 study the time variation of these reaction rate constants was critical, and they were computed by a subroutine package which was a part of the ECLIPSE-66 computer program.

For the BENCHMARK-76 study the time variations were not of interest and the subroutine package was used as a separate program. The output of this "stand-alone" program was a table of psuedo-first order rate constants as a function of altitude and is recorded as Table 9 of the Appendix. [See also Table 3 of reference 2 (I).]

ENERGY SOURCES

The code contains models of several sources of energy: the sun, including x-rays, and ultraviolet and visible light; precipitated electrons; and galactic cosmic rays. The solar model requires a separate atmospheric attenuation model; the precipitating electron model includes atmospheric attenuation; the cosmic ray model ignores it. The eclipse study also required an eclipse model.

NON-IONIZING SOURCES

The only source of non-ionizing energy in the code is the sun. Although the visible light and most of the ultraviolet light are unable to produce the ionization we are trying to study, the enormous amounts of non-ionizing radiation relative to the ionizing radiation drive most of the neutral chemistry and can strongly modulate the charged particle chemistry.

The Solar Model, which is given in Table 1 of the Appendix is based on that used in the OPTIR II code.³ The OPTIR II Solar Model covers the ultraviolet from 100 to 400 nm in 30 bands each 0.25 μm^{-1} wide. (The inverse micrometer (μm^{-1}) is a measure of wave number or energy similar to the inverse centimeter.) We chose to base our solar model on the OPTIR II model because it is made up of a few wide bands rather than many narrow bands and is given in units of photon flux rather than of energy flux. This model was extended on the short wavelength side by ten x-ray bands: three bands 0.2 nm wide from 0.4 to 1.0 nm, and seven bands nominally 1.0 nm wide from 3.1 to 10.0 nm. The x-ray photon fluxes for bands 1-3 were taken from Figure 3 of Sears review of November

³O. P. Manley, H. J. P. Smith, Y. M. Treve, J. W. Carpenter, T. C. Degges, and L. R. Doone, "OPTIR II," AFCRL-71-0528 (1), AFCRL, Bedford, MA, 1971.

1966 eclipse⁴ measurements with the conversion from $\text{ergs cm}^{-2} \text{sec}^{-1}$ to photons $\text{cm}^{-2} \text{sec}^{-1}$ computed for the center of each band. Because Sears' energy fluxes for bands 4-10 are approximately 5 times those recommended by Swider⁵ for 'quiet' solar conditions we used 5 times² Swider's 'quiet' model for our model. Again, we converted from $\text{ergs cm}^{-2} \text{sec}^{-1}$ to photons $\text{cm}^{-2} \text{sec}^{-1}$ at the band center.

The long wavelength limit of the OPTIR solar model was extended from 400 nm to 735 nm by adding seven bands, the width of each being about 10% of center wavelength. These were obtained by combining bands from Ackerman's⁶ model, as shown in Table 1.

Our 47 band model requires about 2200 words of memory when used with our 5 absorbing species and 60 photolytic reactions. Direct use of Ackerman's model would have quadrupled both memory requirements and the number of photon interaction calculations such as absorption, dissociation, etc.

IONIZING RADIATIONS

For computational purposes it was convenient to consider four sources of ionization: solar ultraviolet, solar x-rays, galactic cosmic rays, and precipitating electrons. The solar ultraviolet ionization source comprises bands 11-20 of the solar model mentioned above. The solar x-ray source comprises bands 1-10 of the solar model and includes ionization by two processes: primary photo-ionization and secondary ionization due to energetic photo-electrons.

The Photoelectron Pair Production Model supplements the x-ray portion of the solar model. The x-ray photons have considerable energy beyond that required to ionize atmospheric chemical species, and this energy appears as kinetic energy of the photoelectrons plus a small contribution from multiply-charged ions.⁵ These photoelectrons plus any multiply-charged ions create secondary ionization in the vicinity of the primary photon absorption.⁵ This secondary ion-pair production is given by

⁴R. D. Sears, "Analysis of the 1966 Solar Eclipse Data," LMSC D246526, Lockheed Palo Alto Research Lab, Palo Alto, CA, 1972.

⁵W. Swider, Jr., "Ionization Rates Due to the Attenuation of 1-100Å Nonflare Solar X-Rays," Rev. Geophys. 7, No. 3, 573-594 (August 1969).

⁶M. Ackerman, "Ultraviolet Solar Radiation Related to Mesospheric Processes," in Mesospheric Models and Related Experiments, G. Fiacco, ed., Springer Verlag, N.Y., 149-159 (1971).

TABLE 1. DERIVATION OF BRL BANDS 41 - 47 FROM ACKERMAN'S SOLAR MODEL⁶

Ackerman's Bands	BRL Band	Photons $10^{16}(\text{cm}^{-2}\text{sec}^{-1})$	Wavelength Range (nm)
113-118	41	1.145	400-435
119-126	42	1.851	435-470
127-134	43	2.015	470-510
135-144	44	2.581	510-560
145-156	45	3.237	560-620
157-165	46	3.040	620-680
166-171	47	3.528	680-735

$$\text{Pairs}_{\text{phe}} = 0.03 \left(\sum_i E_i \sigma_i I_i \right) - 1$$

where

$\text{Pairs}_{\text{phe}} \equiv$ photo-electron pair production

$E_i \equiv$ energy per photon in electron volts

$\sigma_i \equiv$ ionization cross section in 10^{-22} M^2

$I_i \equiv$ the attenuated photon flux in photons $\text{cm}^{-2} \text{ sec}^{-1}$

0.03 $\equiv$ the approximate ionization efficiency in ion-pairs per electron volt.

$i \equiv$ the solar x-ray band number.

The one in this expression accounts for the initial ionization reaction.

The Galactic Cosmic Ray ionization constant used was 3.6×10^{-18} molecules⁻¹ cm⁻³ sec⁻¹ and was obtained by linear interpolation between Sears' equations 1 and 2

$$Q_{\text{GCR max}} = 4(30 + 250 \sin^4 \lambda) \times 10^{-20} n$$

$$Q_{\text{GCR min}} = 4(30 + 1000 \sin^4 \lambda) \times 10^{-20} n$$

where $\lambda \equiv$ the geomagnetic latitude

$n \equiv$ number density per cm³

for a geomagnetic latitude of 32.4° ⁴ and is consistent with Swider's⁵ table 7d. A parameterization of cosmic ray ionization variation gives an ionization constant of 3.0×10^{-18} molecules⁻¹ cm³ sec⁻¹. The latitude given in Sears⁴ as the geomagnetic latitude appropriate for the eclipse data used is apparently the geographic latitude, and the appropriate geomagnetic latitude is 17.7° South.⁸ Thus, the value used for the Galactic Cosmic Ray ionization constant is probably high for the ECLIPSE and low for the BENCHMARK runs. However, the data tabulated by Swider⁵ indicate that this value of the ionization constant is not unreasonable.

The cosmic ray model makes no allowance for attenuation of the cosmic ray flux by the atmosphere, and therefore becomes increasingly inaccurate below 30 km.

⁷M. G. Heaps, "The Ion Pair Production Due to Cosmic Rays," BRL Memorandum Report 2641, June 1976. (AD #A027629)

⁸D. C. Baker, "Ionospheric D-Region Parameters from Blunt Probe Measurements during a Solar Eclipse," Scientific Report #334, pp. 45-46, Penn. State University, February 1, 1969.

The Precipitating Electron pair production model is based on that given by Sears.⁴ In his appendix B, which is reproduced in Table 3 of the appendix, he gives the average pair production rate versus altitude for the South Atlantic anomaly at eclipse time. In his Figure 1 he also plots the maximum pair production rate, which is about 12 times greater. Both of these rates are based on extrapolations from trapped electron flux measurements made on September 30, 1966, some six weeks before the eclipse.

Sears' table gives data from 54 to 100 km only and the model was extended above 100 km by assuming that the pair production fell with a constant scale height above 98 km. The model was extended below 54 km by assuming that the scale height decreased at a constant rate below 58 km.

ECLIPSE FUNCTIONS

One additional complication arises for the eclipse. The variation in energy input must be known if we are to accurately model the effects. Sears⁴ gives several eclipse functions: for visible light he gives a table of values computed from the expression for a uniformly bright circular disc eclipsed by a disc of the same subtended angle -

$$Q = Q_0 \left[2(\arcsin (t/d) + (t/d)(1 - (t/d)^2)^{1/2}) \right] / \pi$$

where

$Q_0 \equiv$ the uneclipsed flux

$t \equiv$ time before or after totality

$d \equiv$ the semiduration of the eclipse.

This eclipse function is strictly true only in the far infrared.⁹ For most wavelengths an optical depth of unity occurs below the temperature minimum in the solar atmosphere. Near the center of the solar disc the ray paths are vertical and the spectrum resembles that of a 6700 K black body.¹⁰ Near the limb the ray paths are oblique, unity optical depth occurs at a higher, cooler altitude, and the effective radiation temperature is 5400K at the limb.¹⁰ Sears' ultraviolet eclipse function, which reflects this limb darkening is given in Table 6 of the Appendix. For Lyman alpha the effects of limb darkening are counteracted by resonant scattering from the hydrogen in the solar corona and the geocorona and Sears recommends:

⁹G. Abetti, The Sun, Macmillan, N.Y., 1951, Fig. 85, p. 282.

¹⁰G. Abetti, *ibid.*, Fig. 86, p. 285.

$$Q_{Ly} = Q_{vis} + .001 \quad \text{for } t < 3400 \text{ seconds}$$

$$= Q_{vis} + .002 \quad \text{for } t < 1700 \text{ seconds.}$$

The x-ray flux originates to a large extent in the solar corona and is highly variable in space and time. Sears' recommended eclipse function is given in the Appendix (Table 6) and is quite asymmetric.

During totality the eclipse functions used were

$$Q_{visible} \equiv Q_{ultraviolet} \equiv 0.$$

$$Q_{Lyman \text{ alpha}} \equiv (.001 + .001 * t/d') Q_0$$

where $t \equiv$ time from the center of totality and $d' \equiv$ the semiduration of totality. For x-rays we interpolated linearly between the values at 2nd contact (the start of totality) and 3rd contact (the end of totality).

We were strongly influenced by Abetti's⁹ limb darkening curves when assigning our solar bands to these eclipse functions. We used the ultraviolet eclipse function for the near ultraviolet and throughout the visible (our bands 28-47, 174-740 nm). We used the Lyman alpha function for our bands 11-24, 100-148nm, and the "visible" eclipse function only for bands 25-27, 148-174 nm.

ATMOSPHERIC ATTENUATION COMPUTATIONS

The solar model gives us the photon flux at the top of the atmosphere, but the information we need is the photon flux at some lower level where we are simulating the atmospheric chemistry. We model the atmospheric attenuation of the solar flux by Beer's Law

$$I = I_0 e^{-N\sigma}$$

where $I_0 \equiv$ initial photon flux in photons - cm^{-2} - sec^{-1}

$N \equiv$ line of sight number density per square centimeter

$\sigma \equiv$ absorption cross section in square centimeters

$I \equiv$ the attenuated photon flux one band at a time.

Because there are more than one absorbing species we replace $N\sigma$

by $\sum_i N_i \sigma_i$ to get

$$I = I_0 e^{-\sum N_i \sigma_i}$$

Seven atmospheric species enter into the attenuation calculations: Argon, carbon dioxide, atomic and molecular nitrogen, atomic and molecular oxygen, and ozone. The absorption cross sections given in Table 1 of the Appendix were used both for the ECLIPSE calculations and for the BENCHMARK calculations. The x-ray cross sections are from Swider.⁵ The cross sections for the other wavelengths can be found by looking for the same species in the lists of photolytic reactions in the Appendix.

The species number densities are the same as those used as initial data for the AIRCHEM¹¹ and BENCHMARK computations,¹² but the absorbing species density model has been extended from 0-500 km using the DNA reaction rate handbook DNA 1948H.¹³ In some cases densities have been extrapolated beyond those given in the sources to avoid sudden jumps in the computed flux level for small changes in ray path.

The column densities of the absorbing species were found by integrating the column densities along the ray path from its lowest point until the OPTIR convergence criterion of a less than 1 percent change in the column density per integration step had been met for all absorbing species. The scale path length (i.e., the projection of the scale height on the ray path) was then computed for each absorbing species and was used to extrapolate the column density to the top of the atmosphere. The column densities were then checked again to ensure that either the extrapolated column density was less than .01 gm cm⁻² (i.e., negligible) or that the extrapolation caused an increase of less than 10 percent in the column density. If any species failed both of these criteria the OPTIR criterion was halved and integration along the ray path was resumed.

Two problems with the absorption computations must now be considered.

I. Time Variation of Absorbing Species

In general the chemistry may cause the number density of an absorbing species to change with time. For the present case, only one absorbing species, ozone, changes enough to cause a problem. If the ray path

¹¹E. L. Lortie, M. D. Kregel and F. E. Niles, "AIRCHEM: A Computational Technique for Modeling the Chemistry of the Atmosphere," BRL Report No. 1913, August 1976 (AD#A030157).

¹²F. E. Niles and J. M. Heimerl, "Selected Neutral Species Profiles 0-100 km," BRL Memo Report No. 2767, July 1977 (AD#A042620).

¹³DNA Reaction Rate Handbook, DNA 1948H, Chapter 2, Revision 1, DASIAC, GE-TEMPO, Santa Barbara, CA, 1972.

is nearly vertical so that most of the absorption occurs near the altitude of the chemical computations, and the species in question causes only a small amount of absorption, we may make the assumption that the variation in line of sight density is proportional to the variation in computed density. This assumption holds for the ECLIPSE¹ - the ray path was within 40° of vertical and the computations were for altitudes ≥ 60 km, well above the ozone maximum. For the BENCHMARK² runs the density of the absorbing ozone was held constant; the solar inputs were computed once for an overhead sun using the initial model densities. This assumption would not hold for ray paths which dipped below the ozone maximum, and would be grossly violated for sunrise/sunset studies.

11. Choice of Effective Cross Sections

The relatively wide bands in our solar model lead to another problem. The cross sections of absorbing species can vary by several orders of magnitude over one of our bands, making our choice of the proper effective cross section difficult. A particularly severe problem is presented by the Schuman-Runge bands of molecular oxygen,¹⁴ which roughly correspond to our bands 27-31 (167-210 nm). Oxygen also has a strongly varying cross section over our bands 13-17 and 19 (105-121 nm and 125-129 nm). For our band 18, which is dominated by Lyman alpha, we use cross sections for Lyman alpha. Parts of this discussion also apply to N₂ absorption, bands 11-23 (100-148 nm).

Fortunately, it can be shown^{15,16} that the absorption due to an isolated gaussian line which is narrow with respect to the measuring instrument has an effective absorption cross section which varies inversely with the square root of the absorber density, and that this relationship holds provided the optical density at the peak of the line is at least unity. It can also be shown¹⁷ that this relationship holds approximately for triangular lines, for randomly spaced arrays of lines, and for evenly spaced arrays of lines. This relationship has been experimentally verified by Blake *et al.*¹⁵ for a range of absorption sufficient to vary the light intensity in the Schuman-Runge bands by two orders of magnitude.

¹⁴G. Kockarts, "Penetration of Solar Radiation in the Schuman-Runge Bands of Molecular Oxygen," in Mesospheric Models and Related Experiments, G. Fiacco, ed., Springer Verlag, N.Y., pp. 160-176.

¹⁵A. J. Blake, J. H. Carver, and G. N. Haddad, "Photoabsorption Cross Sections of Molecular Oxygen Between 1250Å and 2350Å," *J. Quant. Spect. and Rad. Transfer* 6, 453-454 (1966).

¹⁶J. R. Nielson, V. Thornton, and E. B. Dale, "Absorption Laws for Gases in the Infrared," *Rev. Mod. Phys.* 16, 307 (1944).

¹⁷A. E. S. Green and P. J. Wyatt, Atomic and Space Physics, Sections 8-3 and 8-4, pp. 410-429, Addison-Wesley, N.Y., 1968.

We now consider what cross sections to use for those bands for which the cross section varies too widely for one cross section to be suitable. We assume that the unattenuated photon flux is relatively constant across the band. We also assume that there is some reasonable distribution of cross sections between $\sigma_{\max}$, the maximum cross section within the band, and $\sigma_{\min}$, the minimum cross section. Consider dividing a band into sub-bands whose boundaries are defined by $\sigma_{\max}$, $\sigma_{\max}/4$, $\sigma_{\max}/16$, ..., $4\sigma_{\min}$, $\sigma_{\min}$. We will accept a cross section distribution as reasonable if the sub-band intervals are approximately equal. If this is true

$$n = \frac{1}{1.4} \ln(\sigma_{\max}/\sigma_{\min})$$

$$\text{and } 1.4 = \ln(4) .$$

Then when the number density of an absorber along the line of sight is less than $1/\sigma_{\max}$ only the peaks are contributing to the absorption and

$$\sigma_e = 0.5 \sigma_{\max}/n$$

where $\sigma_e \equiv$ the effective cross section, i.e., the one we should use in our absorption calculations. In other words, $1/2$ of $\sigma_{\max}$ is effective over $1/n$ th of our band or $(1/2n)$ th of $\sigma_{\max}$ is effective over the whole band.

Hudson¹⁸ indicates that in much of the ultraviolet region the measured cross sections are instrumental bandwidth dependent, and that in general the peak cross sections should be greater and the minimum cross sections should be lower. We will therefore assume that for the most intense sub-band

$$\sigma_e = \sigma_{\max}/n = 1.4 \sigma_{\max}/\ln(\sigma_{\max}/\sigma_{\min}).$$

If the number density is such that $1/\sigma_{\max} \ll N \ll 1/\sigma_{\min}$ and if the inverse square law does hold, then $\sigma_e = \sigma_0 N_0^{1/2}/N^{1/2}$ where N_0 is the line of sight density when $\sigma_e = \sigma_0$. If we let $\sigma_0 = \sigma_e$ when $N = 1/\sigma_{\max}$

$$\begin{aligned} \sigma_e &= \sigma_{\max} \cdot 1.4/(\ln(\sigma_{\max}/\sigma_{\min})(\sigma_{\max} N)^{1/2}) \\ &= 1.4 \sigma_{\max}^{1/2}/(N^{1/2} \ln(\sigma_{\max}/\sigma_{\min})) . \end{aligned}$$

¹⁸R. D. Hudson, "Review of UV Cross Sections," Rev. Geophys. and Space Phys. 9, No. 2, 304-406 (1971).

If the number density is very large then $N \gg 1/\sigma_{\min}$ and $\sigma_e \gg \sigma_{\min}$. We now have 3 expressions; it would be simpler if we only had one.

Clearly, we can combine the latter two cases by simple addition to get

$$\sigma_e = 1.4 (\sigma_{\max}/N)^{1/2} / \ln(\sigma_{\max}/\sigma_{\min}) + \sigma_{\min}$$

for all $N \gg 1/\sigma_{\max}$.

Similarly, we can combine the first two cases by taking the harmonic sum $1/S = 1/a + 1/b$.

If we let

$$a = 1.4 \sigma_{\max} / \ln(\sigma_{\max}/\sigma_{\min})$$

$$b = 1.4 \sigma_{\max}^{1/2} N^{-1/2} / \ln(\sigma_{\max}/\sigma_{\min})$$

$$\text{and } S = \sigma_e,$$

then

$$\sigma_e = 1.4 \sigma_{\max} / (\ln(\sigma_{\max}/\sigma_{\min}) (\sigma_{\max}^{1/2} N^{1/2} + 1))$$

for $N < 1/\sigma_{\min}$.

Since $\sigma_e = \sigma_{\min}$ for $N > 1/\sigma_{\min}$ we can add this to get

$$\sigma_e = \sigma_{\min} + 1.4 \sigma_{\max} / (\ln(\sigma_{\max}/\sigma_{\min}) (\sigma_{\max}^{1/2} N^{1/2} + 1))$$

for all absorption calculations.

Because we now have two cross sections, $\sigma_{\max}$ and $\sigma_{\min}$, rather than one for some bands we now have a minor storage and retrieval problem. For O_2 , and only for those bands where the problem existed, $\sigma_{\max}$ was stored as an absorption cross section and $\sigma_{\min}$ as a dissociation cross section. For N_2 , $\sigma_{\max}$ was stored as an absorption cross section and $\sigma_{\min}$ was set to $3 \times 10^{-24} \text{ cm}^2$.

For CO_2 there is a different problem. The CO_2 absorption cross section decreases rapidly with increasing wavelength across the O_2 Schuman-Runge bands. The O_2 absorption is greater and strongly modulates the solar source seen by the CO_2 . The effective CO_2 absorption is therefore also modulated by the O_2 absorption. To simulate this modulation, the CO_2 cross section was made to vary by the same proportion of its range between $\sigma_{\max}$ and $\sigma_{\min}$ that the O_2 cross section did. Because the CO_2 cross section was decreasing monotonically with

increasing wavelength, $\sigma_{\min}$ for band n could be set to $\sigma_{\max}$ for band n+1 and so $\sigma_{\max}$ was stored for each band.

Note that these attempts to allow for square root low absorption result in some cross sections for O_2 , N_2 , and CO_2 which seem to have unusually high or low values.

Because of an algebraic error the factor 1.4 in the final expression for the cross section was replaced by a 2 in the computer program. The effect of this error will be discussed in the section on photolytic reactions.

Atmospheric attenuation of the precipitating electron flux is included in the model. Atmospheric attenuation of the galactic cosmic ray flux is small above 30 to 35 kilometers and the effects of attenuation are therefore ignored.

PHOTOLYTIC REACTIONS

These are reactions which are driven by photons and which decompose a chemical substance. The rate constants of the photolytic reactions are computed using the expression

$$R_n = \sum_j \sigma_{nj} I_j$$

where

$n \equiv$ reaction number

$j \equiv$ wavelength band number

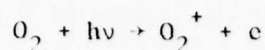
$R_n \equiv$ reaction rate constant

$\sigma_{nj} \equiv$ reaction and band specific cross section

$I_j \equiv$ attenuated photon flux.

The reactions, cross sections and references for the ECLIPSE study¹ are listed in Tables 4 and 5 of the Appendix, and those for the BENCHMARK study² are listed in Tables 7 and 8 of the Appendix.

Because the various ionizing mechanisms differ mainly in their energy sources we have been able to reduce the number of chemical reactions. Ionization by Energetic Particles can be described by chemical equations which are formally the same as the equivalent photo-ionization reaction equations. These equivalent reactions were combined and the rate constant for each combined reaction was obtained by adding those of its constituent reactions. For example, there is only one ionization reaction for molecular oxygen



with

$$R_n = R_{uv} + R_x + R_{phe} + R_{pre} + R_{gcr}$$

where

$h\nu$ $\equiv$ photons from all ionization sources

R $\equiv$ reaction rate constant

n $\equiv$ reaction number

uv $\equiv$ ultraviolet

x $\equiv$ x-rays (primary ionization only)

phe $\equiv$ photo-electrons

pre $\equiv$ precipitated electrons

gcr $\equiv$ galactic cosmic rays

The ionization due to energetic particles was computed by first adding the pair production rates of the source models of galactic cosmic rays, photo electrons, and precipitated electrons and then dividing this pair production among the atmospheric species. Following Swider⁵ we assumed that the cross section of an oxygen atom was 1.15 times that of a nitrogen atom, that the cross sections of molecules were stoichiometric multiples of the cross sections of their constituent atoms, and that these ratios were approximately valid for all three sources. We also chose to ignore all atomic species except Nitrogen and Oxygen.

Then

$$Pairs_{total} = Pairs_{gcr} + Pairs_{phe} + Pairs_{pre}$$

and

$$R'_n = \frac{<N> + 1.15 <O>}{[N] + 1.15 [O]} Pairs_{Total}$$

where

$Pairs_{total}$ = total pair production rate

gcr = galactic cosmic rays

phe = photo-electrons and multiply charged ions

pre = precipitating electrons

R'_n = ionization rate constant for species n by particles

< > indicates the number of N and O atoms in species n.

[] indicates the total local atomic number density of N or O.

Dyadichov and Kozlov¹⁹ give values for relative production rates and branching ratios which corroborate those given by Swider.⁵ The major difference is in the relative cross sections for photoelectron ionization. Dyadichov and Kozlov give cross sectional ratios of O: O₂ : N₂ = 0.56 : 1.5 : 1.15, while Swider gives O : O₂ : N₂ = 0.575 : 1.15 : 1.0, the ratios used in these studies.

Dyadichov and Kozlov¹⁹ also indicate that the photoelectron ionization of N₂ is accompanied by dissociation reactions with rates amounting to 40% - 90% of the ionization rate. They further indicate that all of the N produced by dissociative ionization and 75% of the N produced by dissociation by photoelectrons is N(¹D). In the code, the computed value for N(¹D) is expected to be low because these reactions forming N(¹D) were not included.

Dissociative Ionization was included only for the two species N₂ and O₂, whose branching ratios⁵ are 0.19 and 0.29, respectively. Similar branching ratios were found by Dyadichov and Kozlov.¹⁹

Predissociation is a reaction path which includes a molecule absorbing energy, being raised to an excited state, switching to another excited state, and then dissociating. This takes time, and radiation or collisional quenching are possible alternate paths. The branching ratio between radiation and predissociation is constant, but the collisional quenching rate is a function of M, the local number density, and hence is a strong function of altitude. Ideally this would be modelled by including a metastable species and the several decay paths. Because the reaction set was already large, the rates for the alternate paths were not well known, and these paths were only important for their effect on the dissociation path, we modelled predissociation by choosing a quantum efficiency, ϕ , which seemed reasonable over the altitude range of interest. For N₂ we chose a ϕ of zero because the rate is very slow²⁰ and is only effective at high altitudes. For NO we chose a ϕ of unity²¹ for our bands < 28, λ < 190 nm. For O₂ we chose a ϕ of one half²² for our bands

¹⁹V. N. Dyadichov and S. I. Kozlov, "Minor Ion Components in the Disturbed Ionosphere in the Altitude Range 100-200 km," Cosmic Res. 13, No. 2, 218-218 (1975).

²⁰P. M. Banks and G. Kockarts, Aeronomy, Part A, Academic Press, N.Y., 1973, p. 176 and p. 318.

²¹S. Cieslik and M. Nicolet, "The Aeronomic Dissociation of Nitric Oxide," Planet. Space Sci. 21, 925-938 (1973).

²²M. Ackerman, F. Biaume and G. Kockarts, "Absorption Cross Sections of the Schuman-Runge Bands of Molecular Oxygen," Planet. Space Sci. 18, 1639-1651 (1970).

27-29 (167-190 nm) and a ϕ of zero for our bands > 29 ($\lambda > 190$ nm) which corresponds to predissociation for $v' > 3$ in the Schuman-Runge bands.²³ For our bands < 27 the value of ϕ was absorbed into σ . The resulting O_2 dissociation had an altitude variation which agreed well with that given by Banks and Kockarts.²³

PHOTOLYTIC CROSS SECTIONS

The cross sections used in computing the photolytic reaction rate constants were chosen at times when our knowledge of negative ion cross sections was changing rapidly and hindsight indicates that some guesses and extrapolations from private communications were more fortunate than others. Several of the less fortunate choices and some other problems which arose in choosing cross sections will now be discussed. Reaction numbers without parentheses refer to the ECLIPSE reaction set and will be found with their references in Tables 4 and 5 of the Appendix. Reaction numbers within parentheses refer to the BENCHMARK reaction set and will be found with their references in Tables 7 and 8 of the Appendix. The actual rate constants computed for BENCHMARK are shown in Table 9 of the Appendix.

For the reaction:



a zero shift seems to have occurred in the conversion from cm^{-1} to band number. The cross sections are correct for the next, numerically higher band number. In effect, the cutoff has been shifted to a 10% shorter wavelength. The solar flux increases strongly in the cutoff region, so that the reaction rate constant was reduced by one third, and the rate constants for reaction (1)3, in Table 9 should be increased by 50% to obtain the correct value. We based our cross sections on those computed by Herbst *et al.*²⁴ for a vibrational temperature of 250 K. We did not use their measured cross sections because these were estimated to correspond to an effective temperature of 1750 K.²⁴ Use of the measured (1750 K) cross sections would increase the rate constants for Reaction 3(1) by an additional 20%. Herbst *et al.* did not include rotation effects in their cross section calculations. This neglect of rotation should be equivalent to lowering the effective temperature by an insignificant amount.

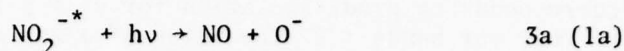
Herbst *et al.*²⁴ also measured a photodissociation cross section for the peroxy isomer of NO_2^- . This species is not in our reaction set, but

²³P. M. Banks and G. Kockarts, *Aeronomy*, Part A, 167-174, Academic Press, N.Y., 1973.

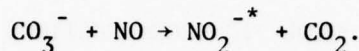
²⁴E. Herbst, T. A. Patterson, and W. C. Lineberger, "Laser Photodetachment of NO_2^- ," J. Chem. Phys. 61, No. 5, 1300-1304 (1974).

[†]Read as Reaction 3 of ECLIPSE studies and Reaction 1 of BENCHMARK studies.

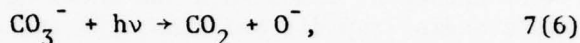
could be important^{25,26} because the photodissociation rate for



would be twice the corrected rate constant²⁵ for Reaction 3(1). One possible production path for NO_2^{-*} is the reaction

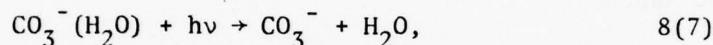


For the reaction



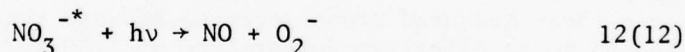
later measurements and estimates by Peterson²⁶ give values of σ which vary from 135% of our σ at longer wavelengths to 0.0% at shorter wavelengths. The net effect is that our computed rate constants²⁶ are 7-9% higher than they would have been if we had used Peterson's²⁶ cross sections.

For the reaction

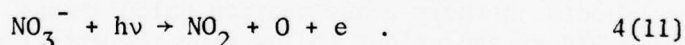


we used a constant 10 megabarn (10^{-17} cm^2) cross section throughout the visible ultraviolet wavelength range. Peterson²⁶ gives cross sections which are lower by 50% in the longest wavelength band, lower by 75-80% between 400 and 520 nm, and zero cm^2 for $\lambda < 390 \text{ nm}$. From Peterson's cross sections we would compute a rate constant for reaction 8(7) which is about 45% lower than the rate constants which we obtained from the cross sections we did use.

For the reaction



we used the same shape at cutoff as for the reaction



Because the solar photon flux decreases much more rapidly at the shorter wavelengths where the NO_3^- , 4(11), and NO_3^{-*} , 12(12), photodissociation reactions cut off than it does at the longer wavelengths where the NO_2^- , 3(1), and NO_2^{-*} , 3a(1a), reactions cut off, the difference between

²⁵J. H. Richardson, L. M. Stephenson, and J. I. Brauman, "Photodetachment of NO_2^{-*} , Experimental Evidence for a New Isomer," Chem. Phys. Lett. 25, No. 2, 318-320 (1974).

²⁶J. R. Peterson, "Sunlight Photodestruction of CO_3^- , $\text{CO}_3^-(\text{H}_2\text{O})$, and O_3^- : The Importance of Photodissociation to the D-Region Electron Densities at Sunrise," J. Geophys. Res. 81, 1433-1435 (1976).

the rate constants is much greater for the former reactions than for the latter reactions.

The effects of these changes to the rate constants in Table 9 of the Appendix are shown in Table 2.

Positive Ion Reactions

Positive ion photolytic reactions were formally included in the BENCHMARK-76 reaction set in Table 9 of the Appendix as reactions 18-32 but in practice the rate constants were set to zero. They were not included in the ECLIPSE-66 reaction set.

Neutral Species Reactions

The square root law variation in the absorption cross section of O_2 which is discussed under attenuation computations is also reflected in the O_2 dissociation cross sections. For normal, Beer's law absorption

$$I = I_0 e^{-n\sigma}$$

$$\text{and} \quad dI/dN = -I_0 \sigma e^{-n\sigma}$$

where σ is a constant. But, for square root law absorption

$$\sigma = \sigma_0 (N_0/N)^{1/2}$$

and

$$dI/dN = -1/2 I_0 \sigma e^{-n\sigma}$$

so that the effective cross section for the dissociation calculations is 1/2 of the effective cross section for the attenuation calculations. With this change the expression for the effective cross section for O_2 dissociation in the square root law region becomes

$$\sigma_e = 1.4 \sigma_{\max} / (\ln(\sigma_{\max}/\sigma_{\min}) (1 + 2N \sigma_{\max})^{1/2}) + \sigma_{\min}$$

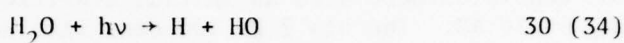
for all N .

Again, due to an algebraic error, the factor 2.0 rather than 1.4 was used in the actual computations. For O_2 this would tend to compensate for an identical error in the attenuation calculations. The absorption cross section error raises the altitude at which absorption occurs by 2-4 kilometers. The dissociation cross section error raises the contribution of the affected bands by 50%. For O_2 the latter effect would predominate above the altitude of unit optical depth and the former effect below that altitude.

TABLE 2. REVISED REACTION RATE CONSTANTS (s^{-1})

Remarks	Reaction No.	Altitude in km						
		80	70	60	50	40	30	20
250 K NO_2^- cross sections of ref. 24	3 (1)	.0524	.0524	.0524	.0522	.0511	.0488	.0485
250 K NO_2^{*-} cross sections of ref. 24	3a (1a)	.107	.107	.107	.107	.105	.102	.100
1500 K NO_2^- cross sections of ref. 24	3b (1b)	.0623	.0623	.0622	.0620	.0609	.0595	.0585
1500 K CO_3^- cross sections of ref. 26	7 (6)	.196	.196	.196	.196	.196	.195	.193
1500 K $CO_3^-(H_2O)$ cross sections of ref. 26	8 (7)	1.089	1.089	1.089	1.089	1.089	1.085	1.074

Effects similar to the interaction between the O_2 absorption cross section and the CO_2 absorption cross section in the Schuman-Runge region, our solar bands 27-31 (167-210 nm), should now be considered. Both CO_2 and H_2O have photodissociation cross sections which decrease very strongly with increasing wavelength in this region. Therefore for the two photodissociation reactions



we made adjustments in the photodissociation cross section identical to the adjustment in the CO_2 absorption cross section which was discussed under atmospheric attenuation calculations.

The solar flux is increasing moderately with increasing wavelength at the same time that the O_2 absorption cross section is decreasing, an effect which partially offsets the cross section interactions. A correction similar to the cross section correction was applied to the photon flux for the ECLIPSE 66 study.¹ It overcompensated at low absorption and was not used for BENCHMARK 76.

The X-Ray Ionization Cross Sections for the species N, N_2 , NO, NO_2 , O, O_2 and $O_2(^1\Delta)$ were computed from the N_2 and O_2 X-ray absorption cross sections using the formula

$$\sigma_{ij} = .5 \langle N \rangle \sigma_{N_2j} + .5 \langle O \rangle \sigma_{O_2j}$$

where

σ is the cross section

i is the reaction number

j is the solar band number

$\langle \rangle$ refers to the number of atoms of N or O in the species.

The cross section for ionization of O_2 by solar Lyman β was set at $1.6 \times 10^{-22} \text{ m}^2$ rather than $1.0 \times 10^{-22} \text{ m}^2$. This would have a maximum effect at 100 km where the total solar ionization rate was 25% high, but the effect was less than 1/2% at 90 km and negligible below that height.

[†]This reaction was not in the BENCHMARK-76 set because CO was not included in the species set.

COMMENTS ON THE CALCULATIONS

Atmospheric chemistry models are frequently allowed to run for several model weeks to eliminate all start up transients. The AIRCHEM models¹¹ were designed to study the reaction of the atmosphere to ionization shocks. They are zero dimensional, transportless, and make no claim to model slow chemistry. For the ECLIPSE-66¹ study we turned the sun on at 10 AM model time and let the program run till 2 PM model time. The 2 PM ion densities were used as initial densities for a second run starting at 10 AM. The new 2 PM ion densities were then used as initial densities for a third run with the ECLIPSE turned on. The 10:30 AM model densities usually agreed to better than 2-5% and the 2 PM densities for the first and second days agreed to a few tenths of a percent. The neutral densities stayed within their estimated error bars except for N(⁺D). This density fell to zero because several formation reactions¹⁹ were not considered. (See above for findings of Dyadichov and Kozlov.) For the ECLIPSE-66¹ study the SOURCE package was called to update the reaction rate constants at both the prediction and correction stages in the integrator.¹¹ For the BENCHMARK-76² study the package stood alone, and the initial neutral density model¹² was used to compute the rate constants, which are given in Table 9 of the Appendix, and which also appears as Table 3 of reference²⁷(I). The atmospheric temperature model was taken from the WEPH 4 code.

²⁷W. S. Knapp, R. L. Bogusch, M. I. Chock, "A FORTRAN Code for the Calculation of Ionization and Absorption Due to a Nuclear Detonation (WEPH 4)," GE-TEMPO, 68 TMP-44, DASA 2096, 30 April 1968.

REFERENCES

1. F. E. Niles and I. L. Chidsey, "Comparison of Measured and Calculated D-Region Electron Density for Solar Eclipse of 12 November 1966," and I. L. Chidsey and F. E. Niles, "Comparison of Measured and Calculated D-Region Positive-Ion Number Density for Solar Eclipse of 12 November 1966," Trans. AGU 56, 997 (1975).
2. J. M. Heimerl and F. E. Niles, "BENCHMARK-76 Model Computations for Disturbed Atmospheric Conditions, I. Input Parameters," BRL Report No. 2022, October 1977; "BENCHMARK-76 Model Computations for Disturbed Atmospheric Conditions, II. Results for the Stratosphere and Mesosphere," BRL Report ARBRL-TR-02050, March 1978; and "BENCHMARK-76 Model Computations for Disturbed Atmospheric Conditions, III. Results for Selected Excitation Parameters at 60 km," BRL Report ARBRL-TR-02051, April 1978. (AD Nos. A050355, A054325, and A054376)
3. O. P. Manley, H. J. P. Smith, Y. M. Treve, J. W. Carpenter, T. C. Degges, and L. R. Doone, "OPTIR II," AFCRL-71-0528 (1), AFCRL, Bedford, MA, 1971.
4. R. D. Sears, "Analysis of the 1966 Solar Eclipse Data," LMSC D246526, Lockheed Palo Alto Research Lab, Palo Alto, CA, 1972.
5. W. Swider, Jr., "Ionization Rates Due to the Attenuation of 1-100Å Nonflare Solar X-Rays," Rev. Geophys. 7, No. 3, 573-594 (August 1969).
6. M. Ackerman, "Ultraviolet Solar Radiation Related to Mesospheric Processes," in Mesospheric Models and Related Experiments, G. Fiacco, ed., Springer Verlag, N.Y., 149-159 (1971).
7. M. G. Heaps, "The Ion Pair Production Due to Cosmic Rays," BRL Memorandum Report 2641, June 1976.
8. D. C. Baker, "Ionospheric D-Region Parameters from Blunt Probe Measurements during a Solar Eclipse," Scientific Report #334, pp. 45-46, Penn. State University, February 1, 1969.
9. G. Abetti, The Sun, Macmillan, N. Y., 1951, Fig. 85, p. 282.
10. G. Abetti, *ibid.*, Fig. 86, p. 285.
11. E. L. Lortie, M. D. Kregel and F. E. Niles, "AIRCHEM: A Computational Technique for Modeling the Chemistry of the Atmosphere," BRL Report No. 1913, August 1976 (AD#A030157).
12. F. E. Niles and J. M. Heimerl, "Selected Neutral Species Profiles 0-100 km," BRL Memo Report No. 2767, July 1977 (AD#A042620).
13. DNA Reaction Rate Handbook, DNA 1948H, Chapter 2, Revision 1, DASIAC, GE-TEMPO, Santa Barbara, CA, 1972.

REFERENCES (CONTD)

14. G. Kockarts, "Penetration of Solar Radiation in the Schuman-Runge Bands of Molecular Oxygen," in Mesospheric Models and Related Experiments, G. Fiacco, ed., Springer Verlag, N.Y., pp. 160-176.
15. A. J. Blake, J. H. Carver, and G. N. Haddad, "Photoabsorption Cross Sections of Molecular Oxygen Between 1250Å and 2350Å," J. Quant. Spect. and Rad. Transfer 6, 453-454 (1966).
16. J. R. Nielson, V. Thornton, and E. B. Dale, "Absorption Laws for Gases in the Infrared," Rev. Mod. Phys. 16, 307 (1944).
17. A. E. S. Green and P. J. Wyatt, Atomic and Space Physics, Sections 8-3 and 8-4, pp. 410-429, Addison-Wesley, N.Y., 1968.
18. R. D. Hudson, "Review of UV Cross Sections," Rev. Geophys. and Space Phys. 9, No. 2, 304-406 (1971).
19. V. N. Dyadichov and S. I. Kozlov, "Minor Ion Components in the Disturbed Ionosphere in the Altitude Range 100-200 km," Cosmic Res. 13, No. 2, 218-218 (1975).
20. P. M. Banks and G. Kockarts, Aeronomy, Part A, Academic Press, N.Y., 1973, p. 176 and p. 318.
21. S. Cieslik and M. Nicolet, "The Aeronomical Dissociation of Nitric Oxide," Planet. Space Sci. 21, 925-938 (1973).
22. M. Ackerman, F. Biaumé and G. Kockarts, "Absorption Cross Sections of the Schuman-Runge Bands of Molecular Oxygen," Planet. Space Sci. 18, 1639-1651 (1970).
23. P. M. Banks and G. Kockarts, Aeronomy, Part A, 167-174, Academic Press, N.Y., 1973.
24. E. Herbst, T. A. Patterson, and W. C. Lineberger, "Laser Photodetachment of NO_2^- ," J. Chem. Phys. 61, No. 5, 1300-1304 (1974).
25. J. H. Richardson, L. M. Stephenson, and J. I. Brauman, "Photodetachment of NO_2^- , Experimental Evidence for a New Isomer," Chem. Phys. Lett. 25, No. 2, 318-320 (1974).
26. J. R. Peterson, "Sunlight Photodestruction of CO_3^- , $\text{CO}_3^-\cdot\text{H}_2\text{O}$, and O_3^- : The Importance of Photodissociation to the D-Region Electron Densities at Sunrise," J. Geophys. Res. 81, 1433-1435 (1976).
27. W. S. Knapp, R. L. Bogusch, M. I. Chock, "A FORTRAN Code for the Calculation of Ionization and Absorption Due to a Nuclear Detonation (WEPH 4)," GE-TEMPO, 68 TMP-44, DASA 2096, 30 April 1968.

APPENDIX

This appendix contains several tables of input data used in the ECLIPSE-66 and BENCHMARK-76 studies, and also, as a sample output the table of quiescent production rates used in the BENCHMARK study. Tables A1 through A9 apply to both studies; the other tables apply to only one study as noted.

Table A1 lists for each band in the solar model, the band limits in millimicrons (10^{-9} m), the absorption cross sections of the absorbing species, the solar flux in photons $\text{cm}^{-2} \text{sec}^{-1}$, and the model band number.

Table A2 lists for bands 11-20 the ultra-violet ionization cross sections in megabarns (10^{-22}M^2) for the species NO, NO_2 , O_2 , $\text{O}_2(^1\Delta)$ versus band number.

Table A3 lists the electron precipitation model⁴ in ion pairs $\text{cm}^{-3} \text{s}^{-1}$ versus altitude in km.

Table A4 lists for bands 11-47 the photodetachment and photodissociation cross sections in cm^{-2} for reactions 1-37 in the ECLIPSE-66 model.

Table A5 lists for all bands and photolytic reactions the references for the ECLIPSE-66 model.

Table A6 lists the uv and x-ray eclipse functions⁴ used in the ECLIPSE-66 model.

Table A7 lists for bands 11-47 the photodetachment and photodissociation cross sections in cm^{-2} for reactions 1-49 in the BENCHMARK-76 model.

Table A8 lists for all bands and photolytic reactions the references for the BENCHMARK-76 model.

Table A9 lists the quiescent production rates derived from the above mentioned data for the BENCHMARK-76 model.

TABLE A1. ABSORPTION CROSS SECTIONS AND SOLAR FLUX MODEL FOR ECLIPSE-66 AND BENCHMARK-76.

WAVELENGTH NANOMETERS	FROM TO	PHOTON-ABSORPTION CROSS SECTIONS (CM ²)				SPECIES	SOLAR FLUX PHOTONS/CM ² -SEC			SOLAR MODEL HAND NO.
		A	CULP	N2	N2		N2	N2	N2	
100.0	102.6	2.000E-20	0.	1.100E-20	1.400E-20	2.400E-20	9.600E+03	7.600E+04	4.500E+05	1
102.6	105.3	5.000E-20	0.	2.900E-20	5.000E-20	7.400E-20	7.600E+04	4.500E+05	1.200E+08	2
105.3	108.1	1.000E-19	0.	6.000E-20	9.000E-20	1.500E-19	1.200E+08	1.900E+08	3.700E+08	3
108.1	111.1	2.410E-18	0.	9.400E-19	1.640E-18	2.400E-18	1.900E+08	3.700E+08	4.000E+08	4
111.1	114.3	3.000E-18	0.	1.810E-18	3.040E-18	4.620E-18	3.700E+08	4.000E+08	6.000E+08	5
114.3	117.6	3.700E-18	0.	2.940E-18	5.090E-18	7.630E-18	4.000E+08	6.000E+08	8.000E+08	6
117.6	121.2	4.900E-18	0.	4.530E-18	7.730E-18	1.160E-17	6.000E+08	8.000E+08	1.000E+09	7
121.2	125.0	6.300E-18	0.	6.480E-18	1.100E-17	1.650E-17	8.000E+08	1.000E+09	1.300E+10	8
125.0	129.0	7.400E-18	0.	8.450E-18	1.510E-17	2.270E-17	1.000E+09	1.300E+10	1.600E+11	9
129.0	133.3	9.500E-18	0.	1.170E-17	2.000E-17	3.000E-17	1.300E+10	1.600E+11	2.000E+12	10
133.3	137.9	0.	4.400E-17	3.000E-22	1.400E-18	2.000E-18	2.000E+09	2.600E+09	3.200E+09	11
137.9	142.9	0.	1.800E-17	3.000E-22	1.000E-18	1.000E-18	2.600E+09	3.200E+09	4.000E+09	12
142.9	148.1	0.	1.000E-17	3.000E-22	3.700E-18	9.300E-18	3.200E+09	4.000E+09	5.000E+09	13
148.1	153.8	0.	5.000E-17	3.000E-22	2.900E-18	1.040E-17	4.000E+09	5.000E+09	6.000E+09	14
153.8	160.0	0.	1.500E-17	3.000E-22	3.000E-18	1.040E-17	5.000E+09	6.000E+09	7.000E+09	15
160.0	166.7	0.	4.000E-19	3.000E-22	7.000E-18	6.700E-18	6.000E+09	7.000E+09	8.000E+09	16
166.7	173.9	0.	9.000E-19	3.000E-22	1.500E-17	9.300E-18	7.000E+09	8.000E+09	9.000E+09	17
173.9	181.8	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	8.000E+09	9.000E+09	1.000E+10	18
181.8	190.5	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	9.000E+09	1.000E+10	1.100E+10	19
190.5	200.0	0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	1.100E+10	1.200E+10	1.300E+10	20
200.0	210.5	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	1.200E+10	1.300E+10	1.400E+10	21
210.5	222.2	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	1.300E+10	1.400E+10	1.500E+10	22
222.2	235.3	0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	1.400E+10	1.500E+10	1.600E+10	23
235.3	250.0	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	1.500E+10	1.600E+10	1.700E+10	24
250.0	266.7	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	1.600E+10	1.700E+10	1.800E+10	25
266.7	285.7	0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	1.700E+10	1.800E+10	1.900E+10	26
285.7	307.7	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	1.800E+10	1.900E+10	2.000E+10	27
307.7	333.3	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	1.900E+10	2.000E+10	2.100E+10	28
333.3	363.6	0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	2.000E+10	2.100E+10	2.200E+10	29
363.6	400.0	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	2.100E+10	2.200E+10	2.300E+10	30
400.0	430.0	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	2.200E+10	2.300E+10	2.400E+10	31
430.0	470.0	0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	2.300E+10	2.400E+10	2.500E+10	32
470.0	510.0	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	2.400E+10	2.500E+10	2.600E+10	33
510.0	560.0	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	2.500E+10	2.600E+10	2.700E+10	34
560.0	620.0	0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	2.600E+10	2.700E+10	2.800E+10	35
620.0	680.0	0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	2.700E+10	2.800E+10	2.900E+10	36
680.0	730.0	0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	2.800E+10	2.900E+10	3.000E+10	37
730.0		0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	2.900E+10	3.000E+10	3.100E+10	38
		0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	3.000E+10	3.100E+10	3.200E+10	39
		0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	3.100E+10	3.200E+10	3.300E+10	40
		0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	3.200E+10	3.300E+10	3.400E+10	41
		0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	3.300E+10	3.400E+10	3.500E+10	42
		0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	3.400E+10	3.500E+10	3.600E+10	43
		0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	3.500E+10	3.600E+10	3.700E+10	44
		0.	7.000E-19	3.000E-22	1.000E-17	1.500E-17	3.600E+10	3.700E+10	3.800E+10	45
		0.	4.000E-19	3.000E-22	1.000E-17	1.500E-17	3.700E+10	3.800E+10	3.900E+10	46
		0.	9.000E-19	3.000E-22	1.000E-17	1.500E-17	3.800E+10	3.900E+10	4.000E+10	47

TABLE A2. ULTRAVIOLET IONIZATION CROSS SECTIONS FOR ECLIPSE-66
AND BENCHMARK-76

SPECIES	NO	NO ₂	O ₂	O ₂ (¹ Δ)
ECLIPSE REACTION NO.	39	40	42	43
BENCHMARK REACTION NO.	51	52	57	60
BAND NO.				
11	14.	3.	1.6*	5.
12	8.5	3.	0.	5.
13	6.	3.	0.	4.
14	4.8	3.	0.	3.
15	3.2	1.6	0.	0.7
16	2.4	0.4	0.	0.
17	2.1	0.12	0.	0.
18	1.9	0.06	0.	0.
19	1.3	0.004	0.	0.
20	0.7	0.	0.	0.

*This was apparently a misprint which occurred when the program was key punched. 1.0×10^{22} meters² is the value indicated by the reference.

TABLE A3. ELECTRON PRECIPITATION MODEL FOR ECLIPSE-66 AND BENCHMARK-76

Altitude (km)	Pair Production Rate (ion-pairs $\text{cm}^{-3} \text{ s}^{-1}$)
100	.0047
98	.0060
96	.0077
94	.0097
92	.012
90	.016
88	.020
86	.026
84	.033
82	.042
80	.050
78	.057
76	.062
74	.064
72	.065
70	.063
68	.059
66	.053
64	.046
62	.038
60	.030
58	.022
56	.016
54	.011

TABLE A4. PHOTODETACHMENT AND PHOTODISSOCIATION CROSS SECTIONS FOR ECLIPSE-66.

WAVELENGTH RANGE (nm)		FRACTION NUMBERS									
FROM	TO	1	2	3	4	5	6	7	8	9	10
100.0	102.6	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
102.6	105.3	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
105.3	108.1	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
108.1	111.1	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
111.1	114.3	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
114.3	117.6	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
117.6	121.2	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
121.2	125.0	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
125.0	129.0	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
129.0	133.3	5.200E-18	5.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
133.3	137.9	5.300E-18	5.800E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
137.9	142.9	5.300E-18	5.800E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
142.9	148.1	5.300E-18	6.100E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
148.1	153.8	5.300E-18	6.300E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
153.8	160.0	5.400E-18	6.400E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
160.0	166.7	5.400E-18	6.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
166.7	173.9	5.400E-18	6.700E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
173.9	181.8	5.500E-18	6.900E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
181.8	190.5	5.500E-18	7.300E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
190.5	200.0	5.600E-18	7.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
200.0	210.5	5.700E-18	7.700E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
210.5	222.2	5.800E-18	7.800E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
222.2	235.3	5.800E-18	8.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
235.3	250.0	5.900E-18	8.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
250.0	266.7	6.000E-18	8.200E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
266.7	285.7	6.100E-18	8.500E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
285.7	307.7	6.100E-18	8.600E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
307.7	333.3	6.200E-18	8.700E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
333.3	363.6	6.200E-18	8.800E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
363.6	400.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
400.0	430.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
430.0	470.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
470.0	510.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
510.0	540.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
540.0	560.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
560.0	620.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
620.0	640.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18
640.0	730.0	6.300E-18	9.000E-18	1.000E-18	1.000E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-18	1.000E-18	1.000E-18

PHOTODISSOCIATION CROSSSECTIONS (CM²) USED IN SUBPRUGHAM HLKDAT - 75/12/16

		REACTION NUMBERS																		
WAVELENGTH RANGE (NM)	FROM	11	12	13	14	15	16	17	18	19	20									
	100.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	4.400E-18	1.000E-17	1.040E-18	1.000E-18	1.000E-18	0.								
	102.6	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-17	5.100E-18	1.000E-18	1.000E-18	0.								
	105.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-17	3.100E-18	1.000E-18	1.000E-18	0.								
	108.1	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-17	1.200E-18	9.000E-18	1.000E-18	0.								
	111.1	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	1.000E-17	1.000E-18	7.000E-19	7.000E-18	0.								
	114.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.500E-18	1.000E-20	4.000E-18	4.000E-19	7.300E-18	0.								
	117.6	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	4.000E-20	1.000E-20	3.000E-19	1.000E-19	1.000E-17	0.								
	121.2	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.300E-19	1.000E-19	1.000E-18	1.500E-17	1.000E-17	0.								
	125.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	4.000E-19	1.000E-19	1.000E-18	1.100E-17	1.000E-17	0.								
	129.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	8.000E-19	1.000E-19	2.000E-18	9.300E-18	1.000E-17	0.								
	133.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	9.000E-19	1.000E-19	1.000E-18	2.500E-18	1.300E-17	0.								
	137.9	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	8.000E-19	1.000E-19	1.000E-18	2.500E-18	1.300E-17	0.								
	142.9	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	9.000E-19	1.000E-19	1.000E-18	1.300E-17	1.000E-17	0.								
	148.1	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	7.000E-19	1.000E-19	1.000E-18	1.200E-18	1.300E-17	0.								
	153.8	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	4.000E-19	1.000E-19	1.000E-18	3.000E-19	1.500E-17	0.								
	160.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.500E-19	1.000E-19	1.000E-18	2.000E-19	1.500E-17	0.								
	166.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-20	1.000E-20	1.500E-19	1.500E-17	1.000E-17	0.								
	173.9	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-21	1.000E-21	2.000E-19	1.500E-17	1.000E-17	0.								
	181.8	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-22	1.000E-22	1.500E-19	1.500E-17	1.000E-17	0.								
	189.5	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-24	3.000E-24	9.100E-18	0.	2.000E-19	1.200E-23								
	190.5	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	3.000E-24	2.000E-24	2.500E-19	0.	4.000E-19	1.200E-23								
	200.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	2.000E-24	0.	0.	4.500E-19	1.000E-23	0.								
	210.5	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	5.400E-19	5.000E-24	0.								
	222.2	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	5.400E-20	1.000E-24	0.								
	235.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	1.900E-20	0.	0.								
	250.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	5.100E-20	0.	0.								
	266.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	1.200E-19	0.	0.								
	285.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	3.000E-19	0.	0.								
	307.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	5.100E-19	0.	0.								
	333.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	6.300E-19	0.	0.								
	363.6	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	400.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	430.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	470.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	510.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	560.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	620.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	680.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								
	730.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	0.	0.	0.	0.	0.	0.								

PHOTON ASSOCIATION CROSS SECTIONS (CM²) USED IN SUBPROGRAM PLKDAT - 75/12/16

REACTION NUMBERS												
FROM	TO	21	22	23	24	25	26	27	28	29	30	
100.0 -	102.6	4.000E-19	0.	0.	1.000E-18	0.	1.000E-20	0.	1.000E-18	1.000E-18	8.000E-18	
102.6 -	105.3	1.000E-18	0.	0.	1.000E-18	0.	1.000E-20	0.	1.000E-18	1.000E-18	4.000E-18	
105.3 -	108.1	5.000E-20	0.	0.	9.300E-18	0.	1.000E-20	0.	1.000E-18	1.000E-18	6.000E-18	
108.1 -	111.1	4.300E-21	0.	0.	9.300E-18	0.	1.000E-20	0.	1.000E-18	1.000E-18	5.000E-18	
111.1 -	114.3	1.000E-20	0.	0.	1.040E-17	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
114.3 -	117.6	1.000E-20	0.	0.	6.700E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
117.6 -	121.2	7.000E-21	0.	0.	9.300E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
121.2 -	125.0	1.000E-20	0.	0.	1.500E-17	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
125.0 -	129.0	6.500E-20	0.	0.	7.100E-17	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
129.0 -	133.3	1.000E-18	0.	0.	1.300E-17	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
133.3 -	137.9	6.000E-18	0.	0.	9.300E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
137.9 -	142.9	1.400E-17	0.	0.	7.400E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
142.9 -	148.1	1.400E-17	0.	0.	5.600E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
148.1 -	153.8	1.200E-17	0.	0.	3.300E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
153.8 -	160.0	8.000E-18	0.	0.	1.120E-17	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
160.0 -	166.7	3.500E-18	0.	0.	9.300E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
166.7 -	173.9	173.9	0.	0.	8.200E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
173.9 -	181.8	181.8	0.	0.	7.400E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
181.8 -	190.5	190.5	0.	0.	6.700E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
190.5 -	200.0	200.0	0.	0.	4.100E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
200.0 -	210.5	210.5	0.	0.	3.300E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
210.5 -	222.2	222.2	0.	0.	1.100E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
222.2 -	235.3	235.3	0.	0.	9.200E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
235.3 -	250.0	250.0	0.	0.	1.100E-17	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
250.0 -	266.7	266.7	0.	0.	5.600E-18	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
266.7 -	285.7	285.7	0.	0.	6.000E-19	0.	1.000E-20	0.	1.000E-18	0.	1.000E-18	
285.7 -	307.7	307.7	0.	0.	2.000E-20	0.	8.300E-21	0.	1.900E-20	0.	0.	
307.7 -	333.3	333.3	0.	0.	5.000E-22	0.	0.	0.	0.	0.	0.	
333.3 -	363.6	363.6	0.	0.	0.	0.	0.	0.	0.	0.	0.	
363.6 -	400.0	400.0	0.	0.	0.	0.	0.	0.	0.	0.	0.	
400.0 -	430.0	430.0	0.	4.140E-23	0.	0.	0.	0.	0.	0.	0.	
430.0 -	470.0	470.0	0.	1.920E-22	0.	0.	0.	0.	0.	0.	0.	
470.0 -	510.0	510.0	0.	8.750E-22	0.	0.	0.	0.	0.	0.	0.	
510.0 -	560.0	560.0	0.	2.440E-21	0.	0.	0.	0.	0.	0.	0.	
560.0 -	620.0	620.0	0.	4.250E-21	0.	0.	0.	0.	0.	0.	0.	
620.0 -	680.0	680.0	0.	8.450E-21	0.	0.	0.	0.	0.	0.	0.	
680.0 -	730.0	730.0	0.	8.400E-22	0.	0.	0.	0.	0.	0.	0.	

PHOTODISSOCIATION CROSSSECTIONS (CM²) USED IN SUPRUGRAM PLKDAT - 75/12/16

WAVELENGTH RANGE (NM)		REACTION NUMBERS						
FROM	TO	31	32	33	34	35	36	37
100.0 -	102.6	0.	1.000E-18	0.	0.	1.000E-18	0.	5.200E-18
102.6 -	105.3	0.	1.000E-18	0.	0.	1.000E-18	0.	5.200E-18
105.3 -	108.1	0.	1.000E-18	0.	0.	1.000E-18	0.	5.200E-18
108.1 -	111.1	0.	1.000E-18	0.	0.	3.700E-17	0.	5.200E-18
111.1 -	114.3	0.	1.000E-18	0.	0.	2.600E-17	0.	5.200E-18
114.3 -	117.6	0.	1.000E-18	0.	0.	1.100E-17	0.	5.200E-18
117.6 -	121.2	0.	1.000E-18	0.	0.	3.700E-18	0.	5.200E-18
121.2 -	125.0	0.	1.000E-18	0.	0.	5.600E-18	0.	5.200E-18
125.0 -	129.0	0.	1.000E-18	0.	0.	7.100E-17	0.	5.200E-18
129.0 -	133.3	0.	1.000E-18	0.	0.	5.600E-17	0.	5.300E-18
133.3 -	137.9	0.	1.000E-18	0.	0.	2.600E-18	0.	5.300E-18
137.9 -	142.9	0.	1.000E-18	0.	0.	1.700E-18	0.	5.300E-18
142.9 -	148.1	0.	1.000E-18	0.	0.	6.300E-18	0.	5.300E-18
148.1 -	153.8	0.	1.000E-18	0.	0.	9.300E-19	0.	5.400E-18
153.8 -	160.0	0.	1.000E-18	0.	0.	7.800E-20	0.	5.400E-18
160.0 -	166.7	0.	1.000E-18	0.	0.	4.800E-20	0.	5.400E-18
166.7 -	173.9	0.	1.000E-18	0.	0.	8.900E-20	0.	5.500E-18
173.9 -	181.8	0.	1.000E-18	0.	0.	1.400E-19	0.	5.500E-18
181.8 -	190.5	0.	1.000E-18	0.	0.	1.300E-19	0.	5.600E-18
190.5 -	200.0	0.	6.000E-19	0.	0.	8.000E-20	0.	5.700E-18
200.0 -	210.5	0.	4.600E-19	0.	0.	1.500E-20	0.	5.800E-18
210.5 -	222.2	0.	3.300E-19	0.	0.	1.500E-21	0.	5.800E-18
222.2 -	235.3	0.	2.200E-19	0.	0.	1.000E-22	0.	5.900E-18
235.3 -	250.0	0.	1.200E-19	0.	0.	1.300E-23	0.	6.000E-18
250.0 -	266.7	0.	7.000E-20	0.	0.	5.000E-24	0.	6.000E-18
266.7 -	285.7	0.	3.000E-20	0.	0.	6.000E-24	0.	6.100E-18
285.7 -	307.7	0.	1.200E-20	0.	0.	4.000E-24	0.	6.200E-18
307.7 -	333.3	0.	5.000E-21	0.	0.	1.000E-24	0.	6.300E-18
333.3 -	363.6	0.	2.000E-21	0.	0.	0.	0.	6.300E-18
363.6 -	400.0	0.	3.000E-22	0.	0.	0.	0.	6.300E-18
400.0 -	430.0	0.	0.	0.	0.	0.	0.	6.300E-18
430.0 -	470.0	0.	0.	0.	0.	0.	0.	6.300E-18
470.0 -	510.0	0.	0.	0.	0.	0.	0.	6.300E-18
510.0 -	560.0	0.	0.	0.	0.	0.	0.	5.800E-18
560.0 -	620.0	0.	0.	0.	0.	0.	0.	5.800E-18
620.0 -	680.0	0.	0.	0.	0.	0.	0.	5.400E-18
680.0 -	730.0	0.	0.	0.	0.	0.	0.	0.

REF. NO.	REACTION	WAVELENGTH REGION	REFERENCE	REF. NO.
31	H202 + HV = H20 + 0	140-200 NM, BAND 30	THOMPSON ET AL, ADV PHOTOCHEM V3, P192	30
32	H202 + HV = H0 + H0	100-125 NM, BANDS 11-18	NOT COMPUTED	31
		125-142 NM, BANDS 19-22	ESTIMATED, SEE TEXT	32
		138-200 NM, BANDS 22-30	HAMPSON, JPCO V2 P290-291 1973	32
33	N20 + HV = N + N0		UREY ET AL JACS V51 P1371-83 1929	33
34	N20 + HV = N2 + 0		NOT COMPUTED	34
35	N20 + HV = N2 + 01D		NOT COMPUTED	35
		100-104 NM, BANDS 11-13	ESTIMATED, SEE TEXT	36
		104-182 NM, BANDS 14-26	ZELIKOFF ET AL JCP V21 P1643-7 1953	37
		182-333 NM, BANDS 29-38	JOHNSTON + GRAHAM CAN J CHEM V52 P1415-23 1974	38
		0.4-10 NM, BANDS 1-10	NOT COMPUTED	39
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	40
		0.4-10 NM, BANDS 1-10	SEE IONIZATION SECTION OF TEXT	41
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	42
		0.4-10 NM, BANDS 1-10	SEE IONIZATION SECTION OF TEXT	43
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	44
		100-114 NM, BANDS 11-15	SEE IONIZATION SECTION OF TEXT	45
		114-135 NM, BANDS 16-20	WATANAHE ET AL APLD OPT V6 P391-6, P1220 1967	
		0.4-10 NM, BANDS 1-10	DNA 1948H RM 1972	
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	
		100-114 NM, BANDS 11-14	SEE IONIZATION SECTION OF TEXT	
		114-129 NM, BANDS 15-19	ESTIMATED	
		0.4-10 NM, BANDS 1-10	NAKAYAMA ET AL JCP V30 P1180-6 1959	
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	
		0.4-10 NM, BANDS 1-10	SEE IONIZATION SECTION OF TEXT	
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	
		100-103 NM, BAND 11	SEE IONIZATION SECTION OF TEXT	
		0.4-10 NM, BANDS 1-10	DNA 1948H RM 1972	
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	
		100-105 NM, BANDS 11-12	SEE IONIZATION SECTION OF TEXT	
		105-112 NM, BANDS 13-15	ESTIMATED	
		0.4-10 NM, BANDS 1-10	R P WAYNE IN MHRE G FIOCCO ED P 240-52 1971	
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	
		0.4-10 NM, BANDS 1-10	SEE IONIZATION SECTION OF TEXT	
		GAMMA- X-RAY PRE ELECT	W SWIDER RGP+SP V7 P573-94, 1969	
		0.4-10 NM, BANDS 1-10	SEE IONIZATION SECTION OF TEXT	

TABLE A6. ULTRAVIOLET AND X-RAY ECLIPSE FUNCTIONS FOR ECLIPSE-66

TIME	UV	x_{in}	x_{out}
0	.000	.170	.165
100	.008	.175	.165
200	.018	.180	.170
300	.033	.190	.170
400	.044	.200	.175
500	.068	.210	.185
600	.089	.225	.190
700	.112	.240	.200
800	.136	.255	.215
900	.161	.270	.225
1000	.188	.290	.240
1100	.215	.315	.250
1200	.243	.340	.265
1300	.272	.370	.285
1400	.302	.405	.300
1500	.331	.455	.320
1600	.360	.505	.340
1700	.390	.545	.365
1800	.420	.575	.380
1900	.449	.600	.395
2000	.479	.630	.410
2100	.509	.650	.430
2200	.538	.670	.445
2300	.568	.685	.460
2400	.598	.700	.470
2500	.628	.720	.485
2600	.656	.735	.495
2700	.683	.750	.505
2800	.709	.770	.520
2900	.735	.780	.535
3000	.760	.790	.555
3100	.784	.805	.585
3200	.807	.820	.625
3300	.828	.830	.700
3400	.849	.840	.745
3500	.869	.855	.785
3600	.888	.865	.810
3700	.906	.875	.830
3800	.922	.890	.850
3900	.937	.905	.870
4000	.950	.925	.880
4100	.962	.955	.905
4300	.881	.965	.915
4400	.988	.975	.925
4500	.993	.985	.935
4600	.997	.995	.940
4700	.999	1.0	.945
4800	1.0	1.0	.950

Time is time to or time from totality as appropriate.

TABLE A7. PHOTODETACHMENT AND PHOTOIONIZATION CROSS SECTIONS FOR BENCHMARK-76.

WAVELENGTH RANGE (NM)		REACTION NUMBERS								
FROM	TO	1	2	3	4	5	6	7	8	9
100.0	102.6	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
102.6	105.3	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
105.3	108.1	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
108.1	111.1	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
111.1	114.3	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
114.3	117.6	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
117.6	121.2	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
121.2	125.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
125.0	129.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
129.0	133.3	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
133.3	137.9	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
137.9	142.9	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
142.9	148.1	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
148.1	153.8	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
153.8	160.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
160.0	166.7	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
166.7	173.9	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
173.9	181.8	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
181.8	190.5	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
190.5	200.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
200.0	210.5	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
210.5	222.2	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
222.2	235.3	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
235.3	250.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
250.0	266.7	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
266.7	285.7	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
285.7	307.7	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
307.7	333.3	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
333.3	363.6	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
363.6	400.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
400.0	430.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
430.0	470.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
470.0	510.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
510.0	560.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
560.0	620.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
620.0	680.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18
680.0	730.0	1.000E-18	5.200E-18	5.500E-18	4.000E-18	1.000E-18	1.400E-18	1.000E-17	5.000E-20	1.000E-18

PHOTOISSION ASSOCIATION CROSSSECTIONS (CM*2) USED IN SIMPHOGRAM PLKDAT - 76/12/16

WAVELENGTH RANGE (NM)		REACTION NUMBERS							
FROM	TO	10	11	12	13	14	15	16	17
100.0	102.6	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
102.6	105.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
105.3	108.1	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
108.1	111.1	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
111.1	114.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
114.3	117.6	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
117.6	121.2	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
121.2	125.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
125.0	129.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
129.0	133.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
133.3	137.9	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
137.9	142.9	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
142.9	148.1	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
148.1	153.8	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
153.8	160.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
160.0	166.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
166.7	173.9	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
173.9	181.8	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
181.8	190.5	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
190.5	200.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
200.0	210.5	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
210.5	222.2	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
222.2	235.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
235.3	250.0	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
250.0	266.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
266.7	285.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
285.7	307.7	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
307.7	333.3	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
333.3	363.6	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
363.6	400.0	1.000E-18	0.	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
400.0	430.0	1.000E-18	0.	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
430.0	470.0	1.000E-18	0.	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
470.0	510.0	1.000E-18	0.	1.000E-18	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
510.0	560.0	1.000E-18	0.	0.	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
560.0	620.0	1.000E-18	0.	0.	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
620.0	680.0	1.000E-18	0.	0.	1.000E-18	1.000E-18	1.000E-18	5.000E-18	2.000E-18
680.0	730.0	1.000E-18	0.	0.	1.000E-18	1.000E-18	1.000E-18	5.000E-20	0.

PHOTODISSOCIATION CROSSSECTIONS (CM²) USED IN SUBPROGRAM PLKDAY - 7/6/12/16

WAVELENGTH RANGE (NM)	FROM	TO	REACTION NUMBERS								
			33	34	35	36	37	38	39	40	41
100.0 - 102.6	100.0	102.6	1.000E-18	1.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.040E-17	1.000E-18	0.
102.6 - 105.3	102.6	105.3	1.000E-18	4.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	5.100E-18	1.000E-18	0.
105.3 - 108.1	105.3	108.1	1.000E-18	6.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	3.100E-18	1.000E-18	0.
108.1 - 111.1	108.1	111.1	1.000E-18	5.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.200E-18	9.000E-18	0.
111.1 - 114.3	111.1	114.3	0.	1.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	7.000E-19	8.200E-18	0.
114.3 - 117.6	114.3	117.6	0.	1.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	4.000E-19	7.000E-18	0.
117.6 - 121.2	117.6	121.2	0.	1.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	3.000E-19	7.300E-18	0.
121.2 - 125.0	121.2	125.0	0.	6.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	4.000E-19	1.100E-17	0.
125.0 - 129.0	125.0	129.0	0.	7.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.100E-18	1.500E-17	0.
129.0 - 133.3	129.0	133.3	0.	6.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.900E-18	1.100E-17	0.
133.3 - 137.9	133.3	137.9	0.	3.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	2.000E-18	9.300E-18	0.
137.9 - 142.9	137.9	142.9	0.	7.000E-19	1.000E-18	1.000E-20	1.000E-18	1.000E-18	2.500E-18	1.300E-17	0.
142.9 - 148.1	142.9	148.1	0.	6.000E-19	1.000E-18	1.000E-20	1.000E-18	1.000E-18	2.500E-18	1.300E-17	0.
148.1 - 153.8	148.1	153.8	0.	1.200E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.200E-18	1.300E-17	0.
153.8 - 160.0	153.8	160.0	0.	2.000E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	3.000E-19	1.500E-17	0.
160.0 - 166.7	160.0	166.7	0.	4.500E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	2.000E-19	1.500E-17	0.
166.7 - 173.9	166.7	173.9	0.	3.200E-18	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.500E-19	1.500E-17	0.
173.9 - 181.8	173.9	181.8	0.	3.000E-19	1.000E-18	1.000E-20	1.000E-18	1.000E-18	2.000E-19	1.000E-17	0.
181.8 - 190.5	181.8	190.5	0.	5.000E-21	1.000E-18	1.000E-20	1.000E-18	1.000E-18	1.500E-19	2.200E-18	0.
190.5 - 200.0	190.5	200.0	0.	6.000E-23	1.000E-18	1.000E-20	1.000E-18	1.000E-18	4.200E-19	4.200E-19	0.
200.0 - 210.5	200.0	210.5	0.	0.	4.000E-19	1.000E-20	1.000E-20	1.000E-18	0.	4.000E-19	0.
210.5 - 222.2	210.5	222.2	0.	0.	3.300E-19	1.000E-20	2.500E-19	4.600E-18	0.	4.500E-19	0.
222.2 - 235.3	222.2	235.3	0.	0.	2.200E-19	1.000E-20	7.000E-20	4.200E-18	0.	2.500E-19	0.
235.3 - 250.0	235.3	250.0	0.	0.	1.200E-19	1.000E-20	2.400E-20	2.900E-18	0.	5.400E-20	0.
250.0 - 266.7	250.0	266.7	0.	0.	7.000E-20	1.000E-20	1.900E-20	1.100E-18	0.	1.900E-20	0.
266.7 - 285.7	266.7	285.7	0.	0.	3.000E-20	1.000E-20	1.400E-20	4.000E-19	0.	5.100E-20	0.
285.7 - 307.7	285.7	307.7	0.	0.	1.200E-20	1.000E-20	4.000E-21	1.000E-19	0.	1.200E-19	0.
307.7 - 333.3	307.7	333.3	0.	0.	5.000E-21	1.900E-20	2.000E-22	0.	0.	3.000E-19	0.
333.3 - 363.6	333.3	363.6	0.	0.	2.000E-21	4.200E-20	0.	0.	0.	5.100E-19	0.
363.6 - 400.0	363.6	400.0	0.	0.	3.000E-22	3.100E-20	0.	0.	0.	6.300E-19	0.
400.0 - 430.0	400.0	430.0	0.	0.	0.	0.	0.	0.	0.	6.000E-20	0.
430.0 - 470.0	430.0	470.0	0.	0.	0.	0.	0.	0.	0.	0.	0.
470.0 - 510.0	470.0	510.0	0.	0.	0.	0.	0.	0.	0.	0.	0.
510.0 - 560.0	510.0	560.0	0.	0.	0.	0.	0.	0.	0.	0.	0.
560.0 - 620.0	560.0	620.0	0.	0.	0.	0.	0.	0.	0.	0.	0.
620.0 - 680.0	620.0	680.0	0.	0.	0.	0.	0.	0.	0.	0.	0.
680.0 - 730.0	680.0	730.0	0.	0.	0.	0.	0.	0.	0.	0.	0.

PHOTODISSOCIATION CROSSSECTIONS (CM*2) USED IN SUBPROGRAM HLKDAT - 76/12/16

			REACTION NUMBERS							
WAVELENGTH RANGE (NM)	FROM	TO	42	43	44	45	46	47	48	49
100.0 - 102.6	100.0	102.6	1.000E-18	0.	4.000E-19	0.	0.	0.	0.	1.000E-18
102.6 - 105.3	102.6	105.3	1.000E-18	0.	1.000E-18	0.	0.	0.	0.	1.000E-18
105.3 - 108.1	105.3	108.1	1.000E-18	0.	5.000E-20	0.	0.	0.	0.	9.300E-18
108.1 - 111.1	108.1	111.1	3.700E-17	0.	4.300E-21	0.	0.	0.	0.	9.300E-18
111.1 - 114.3	111.1	114.3	2.600E-17	0.	1.000E-20	0.	0.	0.	0.	1.040E-17
114.3 - 117.6	114.3	117.6	1.000E-17	0.	1.000E-20	0.	0.	0.	0.	6.700E-18
117.6 - 121.2	117.6	121.2	3.700E-18	0.	7.000E-21	0.	0.	0.	0.	9.300E-18
121.2 - 125.0	121.2	125.0	5.400E-18	0.	1.000E-20	0.	0.	0.	0.	1.500E-17
125.0 - 129.0	125.0	129.0	7.100E-17	0.	6.500E-20	0.	0.	0.	0.	7.100E-18
129.0 - 133.3	129.0	133.3	5.600E-17	0.	1.000E-18	0.	0.	0.	0.	1.300E-17
133.3 - 137.9	133.3	137.9	2.600E-18	0.	1.000E-18	0.	0.	0.	0.	9.300E-18
137.9 - 142.9	137.9	142.9	1.700E-18	0.	1.400E-17	0.	0.	0.	0.	7.400E-18
142.9 - 148.1	142.9	148.1	6.300E-18	0.	1.400E-17	0.	0.	0.	0.	5.600E-18
148.1 - 153.8	148.1	153.8	9.300E-19	0.	1.200E-17	0.	0.	0.	0.	3.300E-18
153.8 - 160.0	153.8	160.0	7.800E-20	0.	8.000E-18	0.	0.	0.	0.	1.120E-18
160.0 - 166.7	160.0	166.7	4.800E-20	0.	3.500E-18	0.	0.	0.	0.	9.300E-18
166.7 - 173.9	166.7	173.9	8.900E-20	0.	3.000E-19	0.	0.	0.	0.	8.200E-19
173.9 - 181.8	173.9	181.8	1.400E-19	3.000E-22	3.000E-22	0.	0.	0.	0.	7.400E-19
181.8 - 190.5	181.8	190.5	1.300E-19	1.200E-23	1.200E-23	0.	0.	0.	0.	6.700E-19
190.5 - 200.0	190.5	200.0	8.000E-20	1.200E-23	1.200E-23	0.	0.	0.	0.	4.100E-19
200.0 - 210.5	200.0	210.5	1.500E-20	9.000E-24	9.000E-24	0.	0.	0.	0.	3.300E-19
210.5 - 222.2	210.5	222.2	1.500E-21	1.000E-23	1.000E-23	0.	0.	0.	0.	1.100E-18
222.2 - 235.3	222.2	235.3	1.000E-22	5.000E-24	5.000E-24	0.	0.	0.	0.	4.000E-18
235.3 - 250.0	235.3	250.0	1.300E-23	1.000E-24	1.000E-24	0.	0.	0.	0.	9.200E-18
250.0 - 266.7	250.0	266.7	5.000E-24	0.	0.	0.	0.	0.	0.	1.100E-17
266.7 - 285.7	266.7	285.7	6.000E-24	0.	0.	0.	0.	0.	0.	5.600E-18
285.7 - 307.7	285.7	307.7	4.000E-24	0.	0.	0.	0.	0.	0.	6.000E-19
307.7 - 333.3	307.7	333.3	1.000E-24	0.	0.	0.	0.	0.	2.000E-20	0.
333.3 - 363.6	333.3	363.6	0.	0.	0.	0.	0.	0.	0.	0.
363.6 - 400.0	363.6	400.0	0.	0.	0.	0.	0.	0.	0.	0.
400.0 - 430.0	400.0	430.0	0.	0.	0.	0.	0.	0.	0.	0.
430.0 - 470.0	430.0	470.0	0.	0.	0.	0.	0.	4.140E-23	0.	0.
470.0 - 510.0	470.0	510.0	0.	0.	0.	0.	0.	1.920E-22	0.	0.
510.0 - 560.0	510.0	560.0	0.	0.	0.	0.	0.	8.780E-22	0.	0.
560.0 - 620.0	560.0	620.0	0.	0.	0.	0.	0.	2.480E-21	0.	0.
620.0 - 680.0	620.0	680.0	0.	0.	0.	0.	0.	4.250E-21	0.	0.
680.0 - 730.0	680.0	730.0	0.	0.	0.	0.	0.	2.650E-21	0.	0.
			0.	0.	0.	0.	0.	8.900E-22	0.	0.

TABLE A8. PHOTOLYTIC REACTIONS AND REFERENCES FOR BENCHMARK-76.

REF. NO.	REACTION	WAVELENGTH REGION	REFERENCE	REF. NO.
1	$\text{NO}_2 \rightarrow \text{H}\nu = \text{NO}_2 + \text{E}$	100-430 NM, BANDS 11-41	ESTIMATED, SEE TEXT	1
2	$\text{O}_2 \rightarrow \text{H}\nu = \text{O} + \text{E}$	430-560 NM, BANDS 42-44	HERBST ET AL, JCP V61 P1300-4 FIG 3, 1974	1
3	$\text{O}_2 \rightarrow \text{H}\nu = \text{O}_2 + \text{E}$	100-116 NM, BANDS 11-16	EXTRAPOLATION FROM CHURCHILL, SEE TEXT	2
4	$\text{O}_2 \rightarrow \text{H}\nu = \text{O}_2 + \text{F}$	100-116 NM, BANDS 11-16	CHURCHILL ET AL, JQSRT V6, P371-442 1966	2
5	$\text{O}_3 \rightarrow \text{H}\nu = \text{O}_3 + \text{E}$	100-116 NM, BANDS 11-16	EXTRAPOLATION FROM CHURCHILL, SEE TEXT	3
6	$\text{CO}_3 \rightarrow \text{H}\nu = \text{CO}_2 + \text{O}$	100-450 NM, BANDS 43-46	CHURCHILL ET AL, JQSRT V6, P371-442 1966	3
7	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	4
8	$\text{CO}_4 \rightarrow \text{H}\nu = \text{CO}_2 + \text{O}_2$	100-450 NM, BANDS 43-46	BURCH ET AL, PHYS REV V112 P 171 1958	4
9	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	5
10	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	COSBY ET AL, JCP V63 P1612-20 1975	5
11	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	6
12	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	MOSELEY ET AL, JCP V65, P2512-7 1976	6
13	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	PETERSON, JGR V81 P1433-5 1975	6
14	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	7
15	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	PETERSON JGR V81 P1433-5 1975	7
16	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	8
17	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	J. MOSELEY, JCP V65 N12 P5267-74 1976	8
18	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	9
19	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	10
20	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	11
21	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT, USED NO2-SHAPE SHIFTED	11
22	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT, NO3-ISOMER	12
23	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	13
24	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	14
25	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	15
26	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	J. MOSELEY, JCP V65 N12 P5267-74 1976	15
27	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	16
28	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	16
29	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	COSBY ET AL, JCP V63 P1612-1620, 1975	17
30	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	ESTIMATED, SEE TEXT	17
31	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	COSBY ET AL JCP V63 P1612-1620 1975	17
32	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	NOT COMPUTED AT THIS TIME	18
33	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	NOT COMPUTED AT THIS TIME	19
34	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	NOT COMPUTED AT THIS TIME	20
35	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	NOT COMPUTED AT THIS TIME	21
36	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	NOT COMPUTED AT THIS TIME	22
37	$\text{H}_2 \rightarrow \text{H}\nu = \text{H}_2 + \text{E}$	100-450 NM, BANDS 43-46	NOT COMPUTED AT THIS TIME	23
			NOT COMPUTED AT THIS TIME	24
			NOT COMPUTED AT THIS TIME	25
			NOT COMPUTED AT THIS TIME	26
			NOT COMPUTED AT THIS TIME	27
			NOT COMPUTED AT THIS TIME	28
			NOT COMPUTED AT THIS TIME	29
			NOT COMPUTED AT THIS TIME	30
			NOT COMPUTED AT THIS TIME	31
			NOT COMPUTED AT THIS TIME	32
			ESTIMATED, SEE TEXT	33
			R D HUDSON, RGP-SP V9 P305-406 1971	34
			ESTIMATED, SEE TEXT	34
			K D HUDSON, J. OMA 1984M RRM REV 1972	34
			THOMPSON ET AL, ADV PHOTOCHEM V3, P192	35
			ESTIMATED, SEE TEXT	35
			HAMPSON JPCRD V2 P290-291 1973	35
			URFY ET AL JACS V51 P1371-83 1929	36
			ESTIMATED, SEE TEXT	36
			JOHNSTON, GRAHAM CAN J CHEM V52 P145-23 1974	37
			ESTIMATED, SEE TEXT	37

TABLE A9. BENCHMARK-76 PRODUCTION RATES FOR QUIESCENT CONDITIONS.
THE RATES ARE ZERO FOR REACTIONS 18-32, INCLUSIVE.

REACTION NO.	10 KM	20 KM	30 KM	40 KM	50 KM	60 KM	70 KM	80 KM
1	3.11E-02	3.13E-02	3.23E-02	3.36E-02	3.47E-02	3.49E-02	3.49E-02	3.50E-02
2	1.14E+00	1.15E+00	1.16E+00	1.17E+00	1.18E+00	1.18E+00	1.18E+00	1.18E+00
3	5.05E-02	5.21E-02	5.84E-02	6.70E-02	7.42E-02	7.57E-02	7.60E-02	7.60E-02
4	3.06E-01	3.08E-01	3.14E-01	3.20E-01	3.24E-01	3.25E-01	3.25E-01	3.25E-01
5	6.86E-02	6.89E-02	7.01E-02	7.14E-02	7.25E-02	7.28E-02	7.28E-02	7.28E-02
6	2.06E-01	2.07E-01	2.10E-01	2.12E-01	2.14E-01	2.14E-01	2.15E-01	2.15E-01
7	1.89E+00	1.90E+00	1.93E+00	1.94E+00	1.96E+00	1.96E+00	1.96E+00	1.96E+00
8	1.40E-02	1.41E-02	1.42E-02	1.43E-02	1.44E-02	1.44E-02	1.44E-02	1.44E-02
9	1.89E-01	1.90E-01	1.93E-01	1.94E-01	1.96E-01	1.96E-01	1.96E-01	1.96E-01
10	1.89E-01	1.90E-01	1.93E-01	1.94E-01	1.96E-01	1.96E-01	1.96E-01	1.96E-01
11	3.83E-04	4.16E-04	6.44E-04	1.14E-03	1.96E-03	2.16E-03	2.19E-03	2.20E-03
12	6.79E-02	6.82E-02	6.93E-02	7.06E-02	7.17E-02	7.20E-02	7.20E-02	7.20E-02
13	1.89E-01	1.90E-01	1.93E-01	1.94E-01	1.96E-01	1.96E-01	1.96E-01	1.96E-01
14	1.89E-01	1.90E-01	1.93E-01	1.94E-01	1.96E-01	1.96E-01	1.96E-01	1.96E-01
15	1.16E-01	1.17E-01	1.19E-01	1.20E-01	1.22E-01	1.22E-01	1.22E-01	1.22E-01
16	4.71E-01	4.74E-01	4.80E-01	4.87E-01	4.93E-01	4.94E-01	4.94E-01	4.95E-01
17	2.67E-01	2.69E-01	2.73E-01	2.76E-01	2.79E-01	2.79E-01	2.79E-01	2.79E-01
18	*****	*****	*****	*****	*****	*****	*****	*****
19	0.	0.	0.	0.	0.	0.	0.	0.
20	0.	0.	0.	0.	0.	0.	0.	0.
21	0.	0.	0.	0.	0.	0.	0.	0.
22	0.	0.	0.	0.	0.	0.	0.	0.
23	0.	0.	0.	0.	0.	0.	0.	0.
24	0.	0.	0.	0.	0.	0.	0.	0.
25	0.	0.	0.	0.	0.	0.	0.	0.
26	0.	0.	0.	0.	0.	0.	0.	0.
27	0.	0.	0.	0.	0.	0.	0.	0.
28	0.	0.	0.	0.	0.	0.	0.	0.
29	0.	0.	0.	0.	0.	0.	0.	0.
30	0.	0.	0.	0.	0.	0.	0.	0.
31	0.	0.	0.	0.	0.	0.	0.	0.
32	0.	0.	0.	0.	0.	0.	0.	0.
33	0.	0.	0.	0.	0.	0.	0.	0.
34	0.	0.	0.	0.	0.	0.	0.	0.
35	3.09E-05	3.25E-05	4.42E-05	7.49E-05	8.19E-05	8.61E-05	8.61E-05	8.61E-05
36	5.87E-04	5.92E-04	6.03E-04	6.16E-04	6.27E-04	6.29E-04	6.29E-04	6.30E-04
37	6.83E-07	9.46E-07	9.13E-06	4.71E-05	9.66E-05	1.33E-04	1.67E-04	1.91E-04
38	1.87E-13	8.03E-06	3.21E-05	3.35E-04	8.48E-04	9.89E-04	1.03E-03	1.03E-03
39	0.	0.	7.48E-21	1.38E-13	2.55E-10	1.25E-08	1.25E-07	4.84E-07
40	1.02E-02	1.03E-02	1.05E-02	1.07E-02	1.08E-02	1.08E-02	1.08E-02	1.08E-02
41	0.	0.	0.	0.	0.	0.	0.	0.
42	3.23E-09	3.75E-09	4.01E-08	2.29E-07	4.61E-07	7.35E-07	1.22E-06	2.48E-06
43	4.38E-19	1.75E-13	7.30E-11	6.61E-10	1.31E-09	1.58E-09	3.18E-09	1.54E-08
44	0.	0.	0.	0.	0.	0.	0.	0.
45	0.	0.	0.	0.	0.	0.	0.	0.
46	0.	0.	0.	0.	0.	0.	0.	0.
47	5.27E-04	5.30E-04	5.34E-04	5.35E-04	5.35E-04	5.35E-04	5.35E-04	5.35E-04
48	6.67E-05	7.03E-05	7.60E-05	7.81E-05	7.84E-05	7.85E-05	7.85E-05	7.85E-05
49	7.06E-06	3.77E-05	4.28E-04	2.15E-03	8.09E-03	9.67E-03	9.90E-03	9.93E-03
50	1.80E-18	1.80E-18	1.80E-18	1.80E-18	1.90E-18	1.93E-17	1.93E-16	3.17E-16
51	3.87E-18	3.87E-18	3.87E-18	3.87E-18	4.07E-18	4.12E-12	3.89E-08	3.16E-07
52	5.94E-18	5.94E-18	5.94E-18	5.94E-18	6.25E-18	2.88E-13	1.23E-09	1.01E-08
53	6.84E-19	6.84E-19	6.84E-19	6.84E-19	7.20E-19	1.55E-18	7.33E-18	1.21E-16
54	0.	0.	0.	0.	0.	0.	0.	0.
55	2.92E-18	2.92E-18	2.92E-18	2.92E-18	3.07E-18	6.60E-18	3.13E-17	5.14E-16
56	2.07E-18	2.07E-18	2.07E-18	2.07E-18	2.18E-18	4.86E-18	2.22E-17	3.67E-16
57	2.94E-18	2.94E-18	2.94E-18	2.94E-18	3.09E-18	6.65E-18	3.15E-17	5.21E-16
58	1.20E-18	1.20E-18	1.20E-18	1.20E-18	1.26E-18	2.72E-18	1.29E-17	2.13E-16
59	0.	0.	0.	0.	0.	0.	0.	0.
60	2.94E-18	2.94E-18	2.94E-18	2.94E-18	3.09E-18	6.65E-18	1.20E-14	8.28E-11

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