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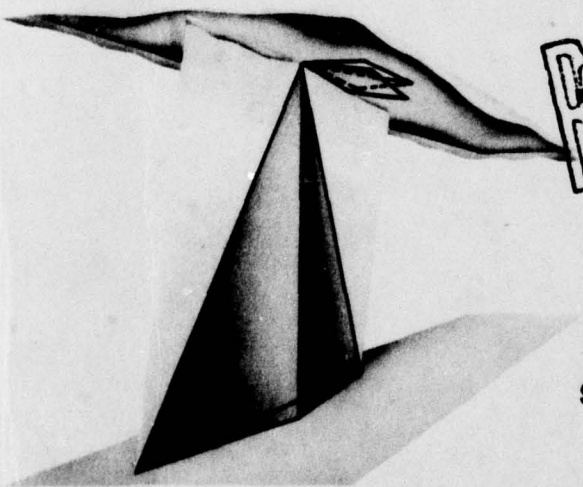
**LEVEL II**

NOSC TR 282

Technical Report 282

## EFFECTS OF STRONG LOCAL SPORADIC E on ELF PROPAGATION

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R. A. Pappert  
L. R. Shockey

15 August 1978

Interim Report: 1 February - 1 June 1978

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Technical Director

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J. H. RICHTER, Head  
EM Propagation Division

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Environmental Sciences Department

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## SUMMARY

### OBJECTIVE

Determine the effects of off path ionospheric inhomogeneities (sporadic-E patches) on the propagation of ELF waves by using a simple Kirchhoff-Huygens diffraction model.

### RESULTS

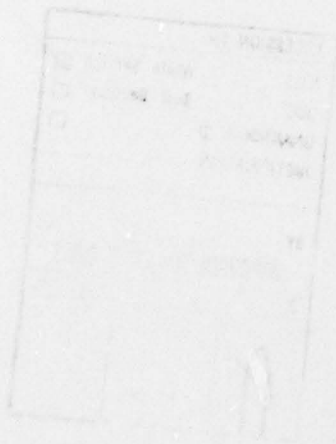
The results indicate that sporadic E patches of the order 1000 km by 1000 km which cause phase shifts and attenuation rate increases can account for the 6-8 dB fades observed over 1600 km transmission paths from the Navy's Wisconsin Test Facility ELF Transmitter. Such disturbances can be expected to produce 2 to 4 dB fades over paths as long as 10,000 km.

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## I. INTRODUCTION

In recent works (Barr, 1977; Pappert and Shockey, 1978; Pappert and Moler, to be published) it has been suggested that nighttime sporadic E layering could produce an order of magnitude enhancement of the earth ionosphere waveguide attenuation rate and thereby account for the 6 to 8 dB short path ( $\cong 1600$  km) fades reported in connection with transmissions from the Wisconsin Test Facility (WTF) (Davis and Meyers, 1975; Bannister, 1975; Davis, 1976). Since the signal from a remote transmitter is received over a range of azimuth angles, the extent of the effect produced by sporadic-E layering depends among other things, upon the size and shape of the disturbance, its proximity to the transmitter or receiver terminals, and its location relative to the great circle path. Although several authors have addressed the question of off path effects (Crombie, 1963; Wait, 1964a, 1964b; Galejs, 1971; Wilcox, 1974; Greifinger and Greifinger 1977; Shellman, 1977), principally on the basis of theoretical development, to the present authors' knowledge no computer code exists which can handle in generality the problem of off path effects associated with propagation in a spherical geometry with simultaneous allowance for vertical inhomogeneity and anisotropy of the ionosphere. Therefore, to obtain at least a semiquantitative estimate of the effect on signal level produced by sporadic E layering we use in this study, because of ease of implementation, a Kirchhoff-Huygens diffraction model (e.g., Marcuse, 1972). The model is similar to that used by Crombie. Unlike Crombie's work however, the Fresnel approximation to the diffraction integral is not invoked but rather the diffraction integral is evaluated by numerical integration. The latter is preferable because of the long wavelengths involved at ELF.

Propagation is assumed to occur along the surface of the earth and the disturbance is modeled by a screen, endowed with attenuation and phase shift properties, which is imagined to move along a great circle contour transverse to the great circle path connecting transmitter and receiver. Effort is concentrated on screens of 1000 km length. This seems to be a reasonable upper limit since the spectrum of reported lateral dimensions of sporadic E layering ranges to that order (Whitehead, 1970). Attenuation and phase shift properties assigned to the screen are selected to be in the range indicated by full wave solutions for ELF propagation in a laterally uniform guide with a superimposed sporadic E layer.

Basically the phase amplitude screen concept is tantamount to the assumption that although the sporadic E disturbance is three dimensional, its effect can be crudely represented by a lumped attenuation and phase shift bounded in the direction transverse to the great circle path connecting transmitter and receiver by the edges of the disturbance. Merit of the model as used in this study is its ease of implementation. Although we believe it is useful for predicting trends and giving an indication of the dependence of signal level on the size and location of the disturbance as well as pointing out the importance of phase shift in addition to attenuation enhancement associated with a disturbance, the model should in no way be construed as a substitute for a full wave treatment of the problem. Rather, the magnitude of the effect indicated in the present study fully supports the need for full wave algorithms capable of handling two dimensional lateral variations in a spherical geometry with simultaneous allowance for vertical inhomogeneity and anisotropy of the ionosphere.

## II. SUMMARY OF FORMULAS

Figure 1 shows the essential geometry consisting of a transmitter at O and receiver at P. A, B,  $A + \delta_1$ ,  $B + \delta_2$ , and Y are great circle arcs and their central angles will be denoted by  $\hat{a}$ ,  $\hat{b}$ ,  $\hat{a} + \delta_1$ ,  $\hat{b} + \delta_2$ , and  $\hat{y}$  respectively. P' represents a point on the great circle contour QQ' which is transverse to the transmitter receiver path OP and a distance Y from the latter. The phase amplitude screen to be introduced is assumed to lie along the contour QQ'. The great circle arc SS' is transverse to the great circle arc QQ' at point P'. The angles of intersection of the great circle arc SP' with the great circle arcs PP' and OO' are denoted by  $\gamma_1$  and  $\gamma_2$  respectively.

The point of departure for the present study is the Kirchhoff-Huygens diffraction integral along with the assumption that the channeled wave at P' due to O and the wave at P reradiated from P' are both described by an asymptotic outgoing Legendre function. Roughly this requires that

$$A, B \geq \lambda / (2\pi |S|) \quad (1)$$

where  $\lambda$  is the free space wavelength and S the sine of the complex eigenangle for the TEM (the only nonevanescant mode) mode which propagates at ELF in the earth ionosphere waveguide. Thus, the crucial assumption is made that the unperturbed field,  $E_{ZO}$ , at P is proportional to

$$E_{ZO} \sim \int_C \frac{\exp[-(\gamma/8.68 + i\omega/v)(A + B + \delta_1 + \delta_2)]}{[\sin(\hat{a} + \delta_1) \sin(\hat{b} + \delta_2)]^{1/2}} (\cos \gamma_1 + \cos \gamma_2) dY \quad (2)$$

where C is the great circle QQ',  $\gamma$  is an attenuation rate for the ambient guide and v a phase velocity for the ambient guide. Such subtleties as spatial or directional dependencies of those quantities as well as mode reflection or conversion due to lateral variation are completely

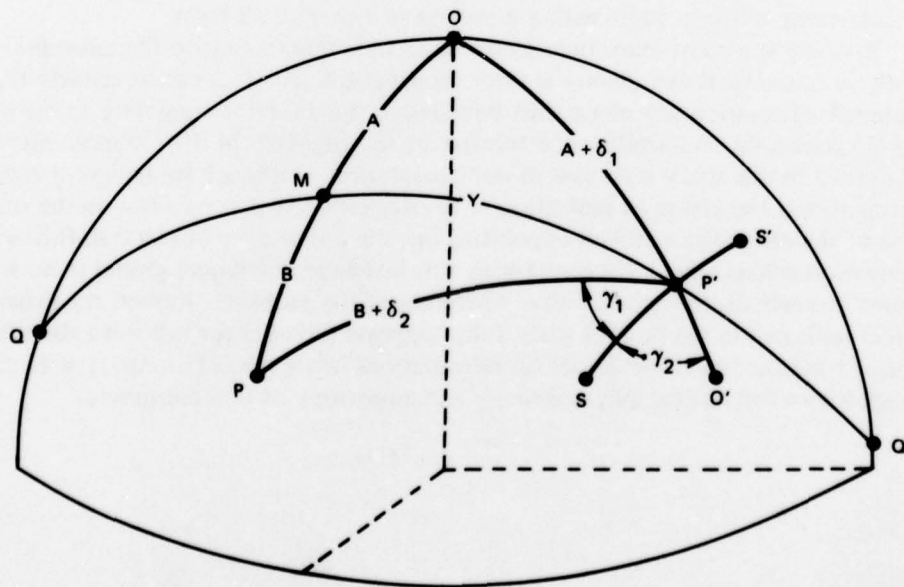


Figure 1. Propagation geometry.

ignored in this study. Observe that  $(\cos \gamma_1 + \cos \gamma_2)$  is an obliquity factor and that the  $Y$  dependence enters into the integrand through the  $\delta_1, \delta_2, \gamma_1,$  and  $\gamma_2$  dependencies. These dependencies are obtained from the following spherical trigonometric formulas:

$$\cos(\hat{a} + \hat{\delta}_1) = \cos \hat{y} \cos \hat{a} \quad (3)$$

$$\cos(\hat{b} + \hat{\delta}_2) = \cos \hat{y} \cos \hat{b} \quad (4)$$

$$\cos \gamma_1 = \sin \hat{a} / \sin(\hat{a} + \hat{\delta}_1) \quad (5)$$

$$\cos \gamma_2 = \sin \hat{b} / \sin(\hat{b} + \hat{\delta}_2) \quad (6)$$

In practice  $\hat{\delta}_1$  and  $\hat{\delta}_2$  are found from (3) and (4), respectively and  $\cos(\gamma_1, \gamma_2)$  is found from (5) or (6). Subject to the approximations

$$\hat{y} \ll 1 \quad (7)$$

$$\hat{\delta}_1 \ll 2 \tan \hat{a} \quad (8)$$

$$\hat{\delta}_2 \ll 2 \tan \hat{b}, \quad (9)$$

Equations (3) and (4) lead to a result given by Crombie:

$$\hat{\delta}_1 + \hat{\delta}_2 \cong \frac{\hat{Y}^2}{2} (\cot \hat{a} + \cot \hat{b}) \text{ or } \delta_1 + \delta_2 \cong \frac{Y^2}{2r} (\cot \hat{a} + \cot \hat{b}) \quad (10)$$

where  $r$  is the radius of the earth. In the limit  $\hat{a}, \hat{b} \ll 1$ , the flat earth limit

$$\delta_1 + \delta_2 \cong \frac{Y^2}{2} \frac{A+B}{AB} \quad (11)$$

is retrieved.

The attenuation rate,  $\gamma$ , and the obliquity factor in the integrand of (2) tend to reduce the off path contributions. With allowance for these factors it is expected that off path effects will damp out more rapidly than they would were Fresnel filtering alone considered.

Now suppose that the fictitious phase amplitude screen falls along the great circle contour  $QQ'$  between the limits (edges)  $Y_1$  and  $Y_2$  ( $Y_2 > Y_1$ ) and that the screen introduces an "enhanced" attenuation  $\beta$  (in dB) and an additional phase shift  $\phi$ . Then according to the crucial assumption of Equation (2) the ratio of the perturbed (by the screen) field,  $E_2$ , to the unperturbed field will be

$$E_2/E_{z0} \cong 1 + (\exp(-\beta/8.68 - i\phi) - 1) \frac{\int_{Y_1}^{Y_2} F(Y) dY}{\int_c F(Y) dY} \quad (12)$$

where

$$F(Y) = \frac{\exp[(-\gamma/8.68 - i\omega/v)(\delta_1(Y) + \delta_2(Y))]}{[\sin(\hat{a} + \hat{\delta}_1(Y)) \sin(\hat{b} + \hat{\delta}_2(Y))]^{1/2}} (\cos(\gamma_1(Y)) + \cos(\gamma_2(Y))) \quad (13)$$

Clearly, the attenuation,  $\beta$ , and phase shift,  $\phi$ , properties of the screen could be allowed to be a function of position along the screen ( $Y$ ) and the associated terms retained within the integral. This might be desirable; for example, if modeling for a specifically shaped perturbation, say circular, allowance could be provided for the different lengths of travel through the perturbed regions. If the attenuation "rate" and phase shift "rate" were constant through the perturbed region then the  $\beta$  and  $\phi$  would be proportional to the travel lengths and this could quite easily be accommodated with the model. Where to place the screen (i.e., what value of  $A$  to use) would remain a question best answered probably in empirical fashion by comparing with a selection of full wave results. In the present study such refinements are not attempted and all results given in the following section are based on Equation (12) which in turn is predicated on the constancy of  $\beta$  and  $\phi$  over the screen.

### III. RESULTS

In previous studies (Pappert and Shockey, 1977; Pappert and Moler, to be published) full wave outputs for an ambient nighttime profile and an ambient nighttime profile disturbed by a sporadic E layer (see Figure 2) have been analyzed as regards ionospheric absorption and reflection features of ELF waves. Figures 3 through 6 show comparisons between ambient and the ambient plus sporadic E modal properties and excitations in the frequency range from 45 to 100 Hz. In particular Figure 3 shows the attenuation rate (dB/1000 km), Figure 4 the phase velocity normalized to the free space velocity  $c$ , Figures 5 and 6 show the magnitude and phase respectively for the vertical E field excitation factor produced by end-on launch from a ground based horizontal dipole. Figure 3 illustrates the distinct possibility of an order of magnitude enhancement of the attenuation rate associated with the sporadic E layer and Figure 4 illustrates the possibility of substantial phase shift. Figures 5 and 6 illustrate the likelihood that should the sporadic E disturbance pass over the terminals, additional effects due to excitation factor fluctuations could be expected. However, effects attributable to the latter are not considered further in this study but certainly should be allowed for in full wave treatments. The subsequent plots are based on modal parameters consistent with those shown in Figures 3 and 4. Specifically, plots are shown for a number of transmitter receiver distances (denoted by  $D$  on the plots) for several values of beta and phi showing among other things signal variation with location of the phase amplitude screen on the great circle path transverse to the great circle path connecting the transmitter and receiver. The latter position is denoted by the midpoint

$$Y = \frac{Y_1 + Y_2}{2} \quad (14)$$

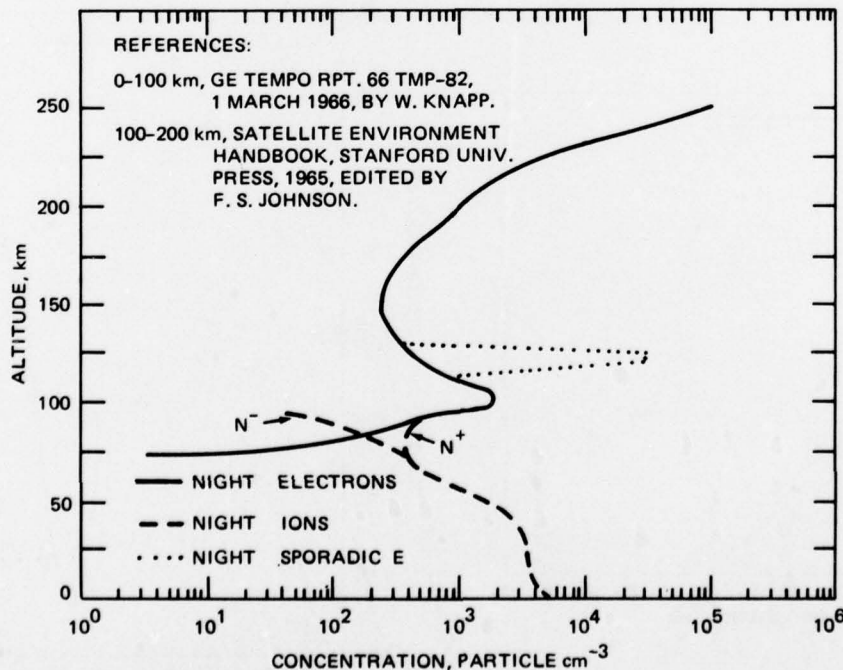


Figure 2. Night ambient profile and night sporadic E.

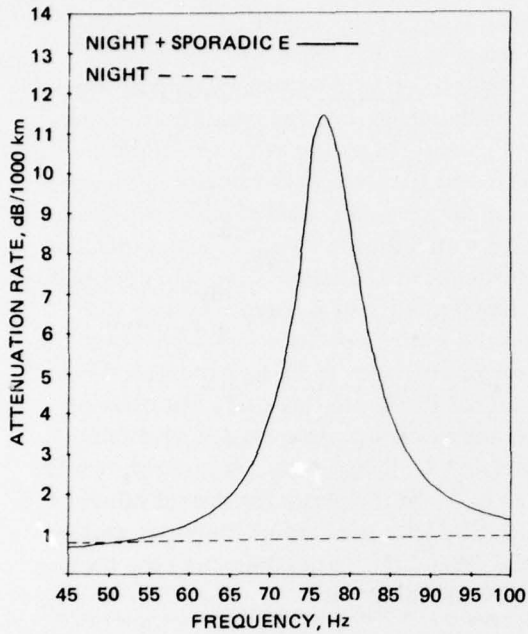


Figure 3. Attenuation versus frequency.

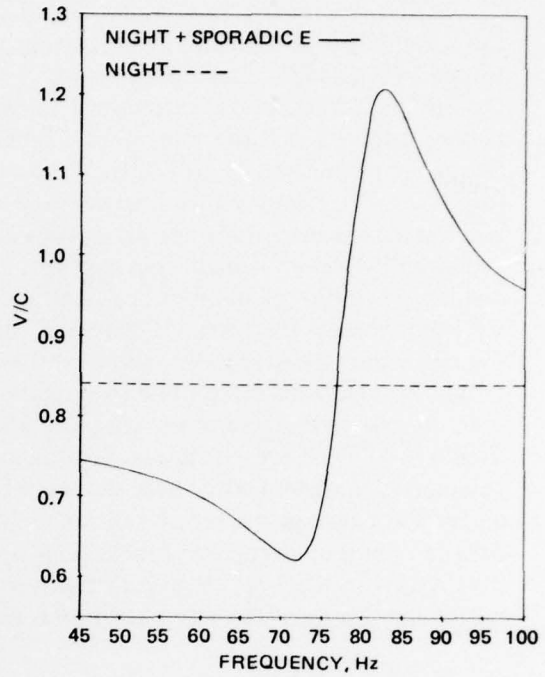


Figure 4. Phase speed over free space speed versus frequency.

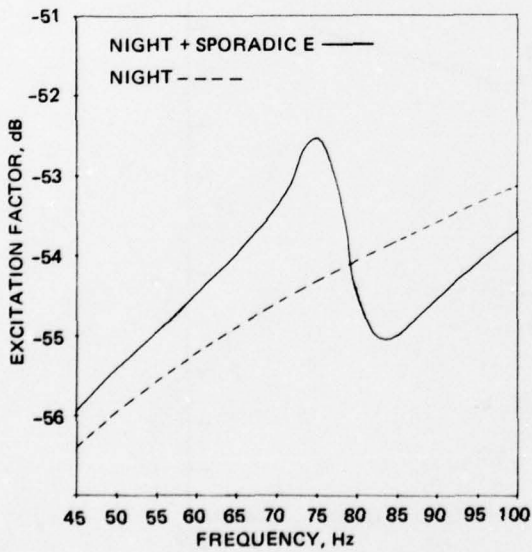


Figure 5. Excitation factor magnitude versus frequency.

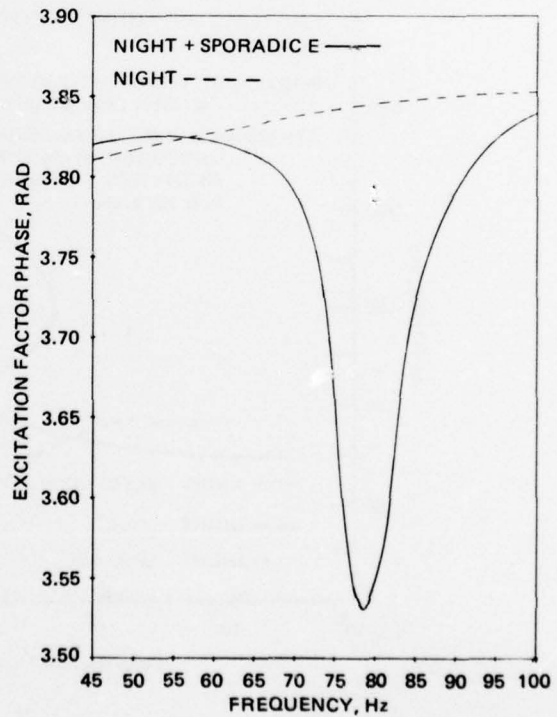


Figure 6. Excitation factor phase versus frequency.

and the length of the screen (i.e.,  $Y_2 - Y_1$ ) is denoted by  $T$ . Several values for the position of the screen,  $A$ , (see Figure 1) are considered and it should be realized that the interchange of  $A$ ,  $B$  leave the result invariant (e.g., the case  $A = 1000$  km,  $B = 5000$  km is mathematically identical to the case  $A = 5000$  km,  $B = 1000$  km). All of the subsequent figures are for a frequency of 75 Hz.

Figures 7 through 16 show results for a 1600 km path since 6 to 8 dB fades have been reported for paths of that length. Figures 7 and 8 show results for a screen length equal to 1000 km since the spectrum of lateral dimensions of sporadic E have been reported to that order. Shown on each figure are results for the field perturbation, in dB (Equation (12)) as a function of the center position of the screen (Equation (14)). Results are shown for total attenuation enhancement of 1, 5, and 10 dB and both figures are for a zero phase shift screen (i.e.,  $\phi = 0$ ). Since the magnitude of the sine of the eigenangle ( $S$ ), is typically in the range of 1.2, the smallest possible value of "A" consistent with the condition given in Equation (1) is 500 km and such a small value is marginal indeed. Nonetheless, in Figure 7 results are given for this value and in Figure 8 results are given for the midpoint value of 800 km. It will be seen that the fading in this instance is only slightly greater for  $A = 500$  km than it is for  $A = 800$  km. To approach even the reported 6 dB figure for fadings, it is clear that an order of magnitude enhancement in the attenuation is required for the parameters appropriate to Figures 7 and 8. Maximum fading occurs when the perturbation screen is centered about the great circle path connecting transmitter and receiver and the deviation from ambient is less than 0.5 dB for off path locations of the mid-point of the screen greater than about 1700 km. According to Equation (10) the first Fresnel zone size is 1079 km for  $A = 500$  km and 1165 km for  $A = 800$  km. The outer boundary of the second Fresnel zone is  $\sqrt{2}$  times these. The off path factors allowed for in the integrand of Equation (12) tend to damp the off path oscillations more rapidly than would have been the case had Fresnel filtering been employed.

Figures 3 and 4 illustrate the possibility of a substantial attenuation and phase shift occurring simultaneously. Table 1 shows the value

$$\psi = \frac{2\pi f}{c} \left[ \frac{1}{(v/c)_d} - \frac{1}{(v/c)_a} \right] \quad (15)$$

where "f" is the frequency, "c" the speed of light in vacuum, and  $v$  the phase velocity. The subscripts "d" and "a" stand for "disturbed" and "ambient," respectively. The table shows the results for the rate of phase retardation or advance in the neighborhood of the resonance along with the attenuation rate.

Table 1. Attenuation rate and rate of phase change close to resonance.

Freq, Hz	dB/1000 km	degrees/1000 km
72	5.99	38.25°
73	7.31	36.85°
74	8.83	32.25°
75	10.29	23.65°
76	11.24	11.17°
77	11.38	-2.39°
78	10.81	-14.08°
79	9.82	-22.66°
80	8.71	-27.96°
81	7.55	-31.07°
82	6.48	-32.23°
83	5.50	-32.05°

D = 1600 KM  
 A = 800 KM  
 T = 1000 KM  
 PHI = 0 DEGREES  
 FREQ = 75 HZ

BETA = 1 DB  
 BETA = 5 DB  
 BETA = 10 DB

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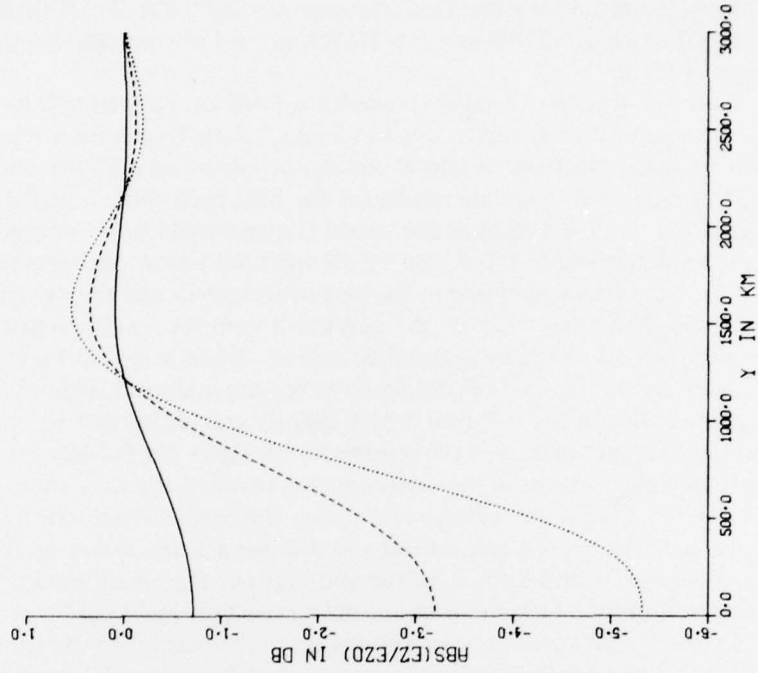


Figure 8. Signal level versus off path location (D = 1600 km, A = 800 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D = 1600 KM  
 A = 500 KM  
 T = 1000 KM  
 PHI = 0 DEGREES  
 FREQ = 75 HZ

BETA = 1 DB  
 BETA = 5 DB  
 BETA = 10 DB

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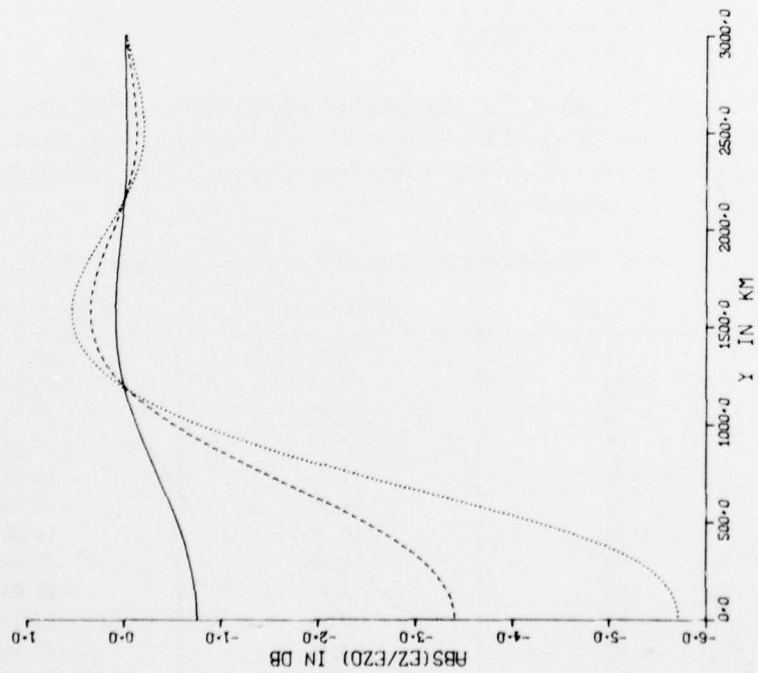


Figure 7. Signal level versus off path location (D = 1600 km, A = 500 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

An examination of the table shows that for a disturbance which extends 1000 km along the guide, it is quite within reason that an attenuation enhancement of 8 dB along with a  $30^\circ$  phase change can simultaneously occur. Thus, Figures 9 and 10 show results for the 1600 km path with a screen length equal to 1,000 km for values of  $\phi$  (Equation (12)) of  $-30^\circ$ ,  $0^\circ$ ,  $30^\circ$  and  $\beta = 8$  dB. In particular, Figure 9 is for  $A = 500$  km and Figure 10 for  $A = 800$  km. Again, there is not a great deal of difference between the results for the two  $A$  values. The significant feature is that the signal level for the  $-30^\circ$  case is down about another 1.5 dB from the results indicated in Figures (7) and (8) and definitely within the 6 to 8 dB range quoted in connection with the WTF transmissions to Connecticut and Maryland. As before, the phase-amplitude screen effects damp out when the midpoint of the screen exceeds the outer boundary of the second Fresnel zone. Also, note that the minimum signal level for  $\phi = 30^\circ$  occurs not for  $Y = 0$  but for  $Y \cong 400$  km. The latter feature, that is the minimum signal level occurring for  $Y \neq 0$ , is common to a number of the subsequent curves.

Figures 11 and 12 show, for the 1600 km path, signal level as a function of  $\phi$  for  $\beta = 6, 8$  and  $10$  dB and a screen length of 1,000 km. Figure 11 is for  $A = 500$  km and Figure 12 for  $A = 800$  km. The curves illustrate the significance of the phase shift although it must be remembered that  $\phi$  and  $\beta$  are not, as discussed previously, independent.

Figures 13 through 16 show results for the 1600 km path but with a screen length of 500 km. Since the screen is intended here as a lumped parameter model of a sporadic E disturbance of roughly 500 by 500 km, the total attenuation and phase shifts are halved from their previous values. Examination of the figures indicates that disturbances on that spatial scale even with order of magnitude enhancement of the attenuation rate cannot explain the 6 to 8 dB fades reported. Thus, in the subsequent figures the screen thickness is assigned the reasonable upper value of 1000 km. As shown, this thickness coupled with an order of magnitude enhancement of the attenuation rate can account for the observed short path fades.

Figures 17 through 38 show detailed off path behavior for transmitter-receiver distances,  $D$ , of 2000 km, 4000 km, 6000 km and 8000 km. For each value of  $D$  results are given for the combination  $\phi = 0^\circ$ ,  $\beta = 1, 5$ , and  $10$  dB, and for the combination  $\phi = -30^\circ$ ,  $0^\circ$ , and  $30^\circ$  with  $\beta = 8$  dB. Also for each  $D$  value results are given for  $A = 500$  km, 1000 km, and for the midpoint value  $A = D/2$ . The results indicate the following:

- a. For each value of  $A$  the deepest fades occur with the combination  $\phi = -30^\circ$ ,  $\beta = 8$  dB.
- b. For  $A$  values of 500 and 1000 km the deepest fades associated with (a) above always occur with the screen centered about the great circle path connecting transmitter and receiver.
- c. The perturbation is essentially damped out when the center of the screen exceeds the outer boundary of the second Fresnel zone.

Figures 39 through 41 show for  $D = 8000$  km the variation of signal level with  $\phi$  for  $\beta$ 's = 6, 8 and 10 dB. In particular, Figure 39 is for  $A = 500$  km, Figure 40 for  $A = 1000$  km, and Figure 41 for  $A = 4000$  km. Although the curves indicate that the phase shift can be as important or more important than the attenuation, it must be kept in mind that the two are not independent (i.e., it is unlikely that a  $45^\circ$  phase shift could occur simultaneously with a 6 dB attenuation enhancement).

The major results as far as depth of the fades is concerned are conveniently summarized in Figures 42 and 43. In particular, we have plotted the deepest fades for the cases ( $\beta = 10$ ,  $\phi = 0^\circ$  and  $\beta = 8$ ,  $\phi = -30^\circ$ ) as a function of  $D$  (going out to 16,000 km) for  $A$  values of 500 km, 1000 km, and the midpoint value  $A = D/2$ . The oscillatory nature of the curves

is a consequence of the round the world (long path) wave interfering with the diffracted short path field. This interference is probably somewhat magnified because the ambient attenuation rate of 1 dB/1000 km used in the present study is probably low for a global average. Also, the  $\pi/2$  advance of the long path wave as a consequence of passage through the antipode has not been allowed for in the present calculations. Nevertheless, the results are indicative of the behavior to be expected in a more refined treatment.

Even discounting the  $A = 500$  km case, as stretching the validity of the condition given in Equation (1) too far, and in spite of representing the oscillatory behavior of the results of Figures 42 and 43 by imaginary smooth average curves, it is clear that for ranges on the order of 10,000 km, fades in the range of 2 to 4 dB could be anticipated. Fades within the latter range have apparently been observed in connection with the WTF transmissions to Italy (John Davis private communications).

At several junctures in this report we have made reference to the fact that the total integrand of Equation (2) has been allowed for by means of numerical integration. It is legitimate to inquire into the differences to be expected if Fresnel filtering alone were considered. Figure 44 shows a comparison for  $D = 1600$  km,  $A = 800$  km,  $\phi = 0^\circ$  and  $\beta = 5$ , 10 dB between the numerical integration result and the Fresnel integral calculation. The major differences are that the additional terms in the integrand tend to damp out the off path effects more rapidly and tend to stabilize the behavior in the  $Y = 0$  range.

D= 1600 KM  
 A= 500 KM  
 T= 1000 KM  
 BETA= 8 DB  
 FREQ= 75 HZ

PHI= -30 DEGREES  
 PHI= 0 DEGREES  
 PHI= 30 DEGREES

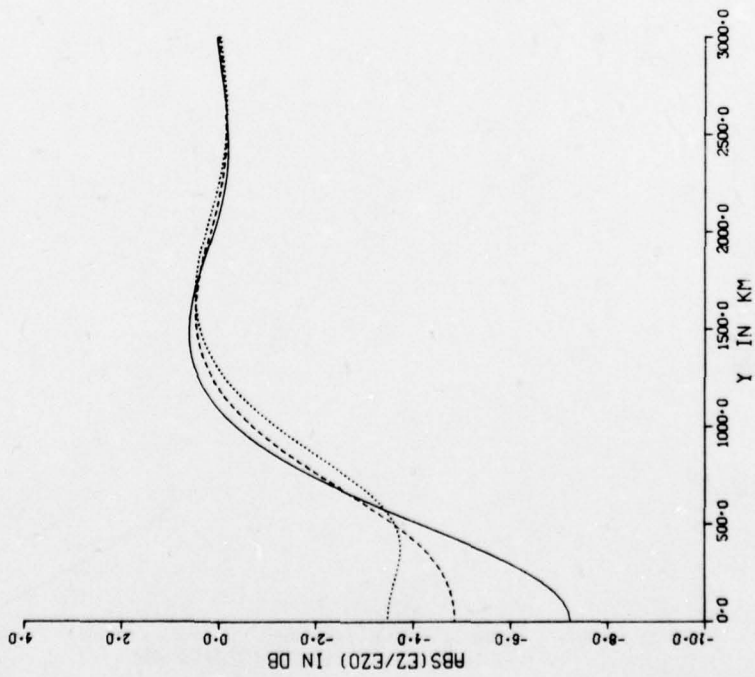


Figure 9. Signal level versus off path location (D = 1600 km, A = 500 km, T = 1,000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D= 1600 KM  
 A= 800 KM  
 T= 1000 KM  
 BETA= 8 DB  
 FREQ= 75 HZ

PHI= -30 DEGREES  
 PHI= 0 DEGREES  
 PHI= 30 DEGREES

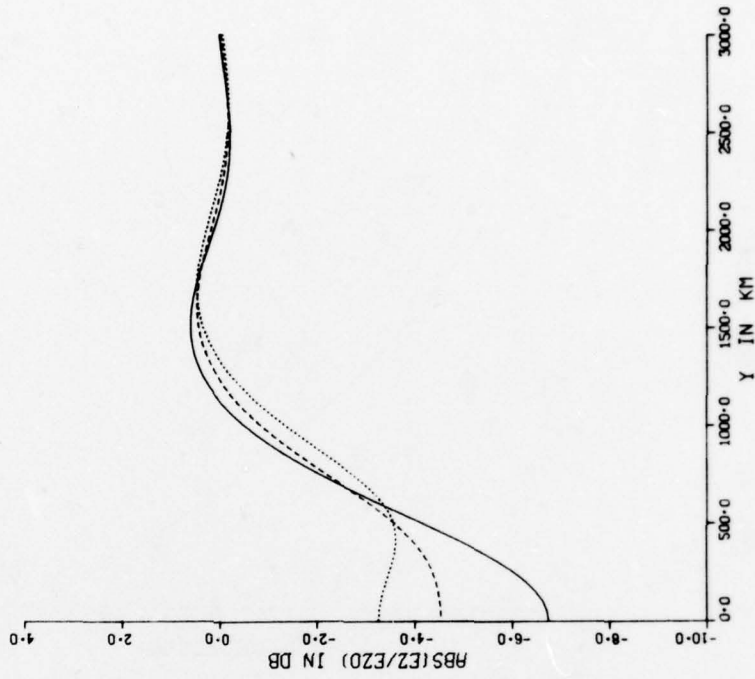


Figure 10. Signal level versus off path location (D = 1600 km, A = 800 km, T = 1,000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D = 1600 KM  
 A = 800 KM  
 T = 1000 KM  
 Y = 0 KM  
 FREQ = 75 HZ

BETA = 6 DB  
 BETA = 8 DB  
 BETA = 10 DB

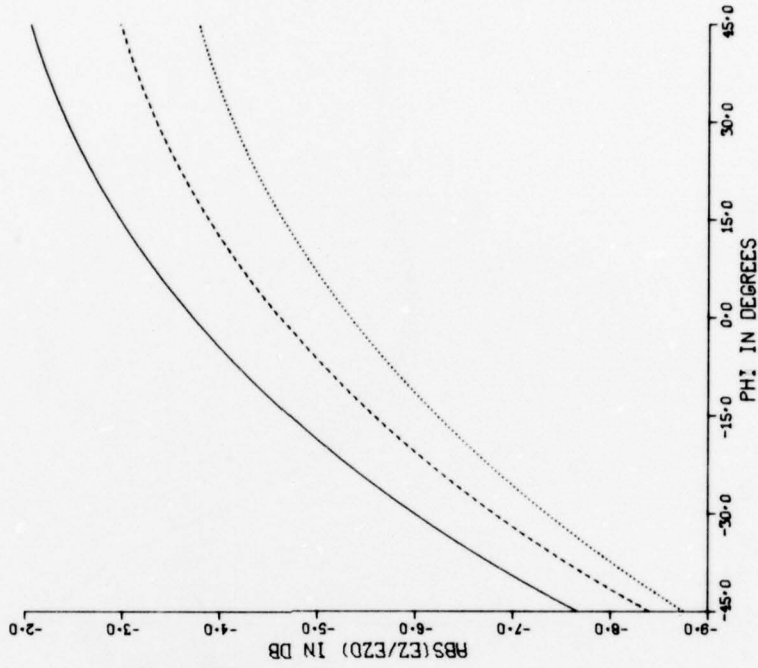


Figure 12. Signal level versus phi (D = 1600 km, A = 800 km, T = 1,000 km,  $\beta = 6, 8, 10$  dB).

D = 1600 KM  
 A = 500 KM  
 T = 1000 KM  
 Y = 0 KM  
 FREQ = 75 HZ

BETA = 6 DB  
 BETA = 8 DB  
 BETA = 10 DB

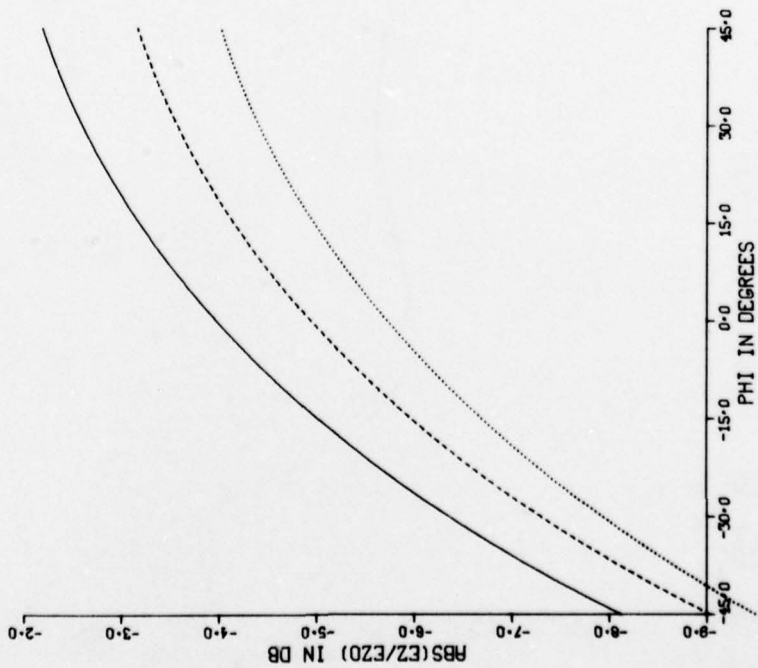


Figure 11. Signal level versus phi (D = 1600 km, A = 500 km, T = 1,000 km,  $\beta = 6, 8, 10$  dB).

D = 1600 KM  
 A = 500 KM  
 T = 500 KM  
 PHI = 0 DEGREES  
 FREQ = 75 HZ

BETA = 1 DB  
 BETA = 5 DB

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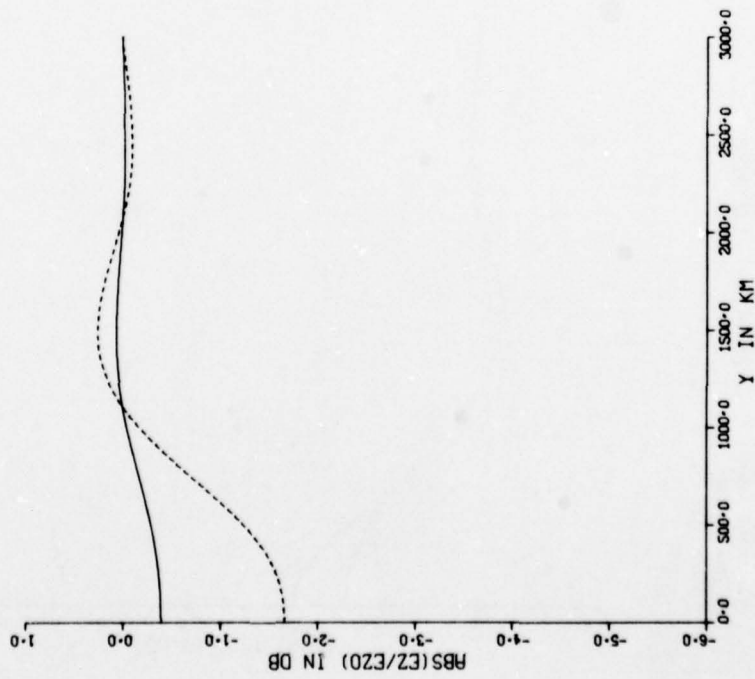


Figure 13. Signal level versus off path location (D = 1600 km, A = 500 km, T = 500 km,  $\beta = 1, 5$  dB,  $\phi = 0^\circ$ ).

D = 1600 KM  
 A = 800 KM  
 T = 500 KM  
 PHI = 0 DEGREES  
 FREQ = 75 HZ

BETA = 1 DB  
 BETA = 5 DB

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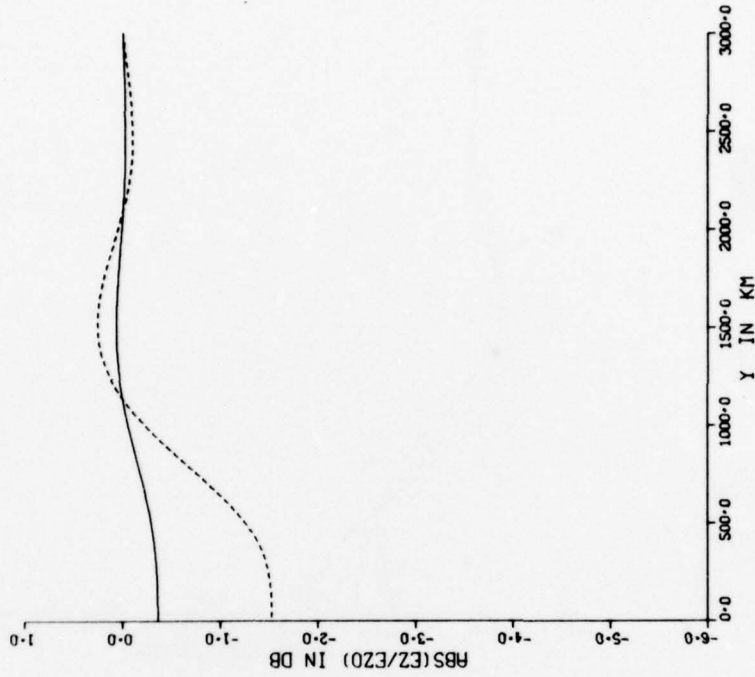


Figure 14. Signal level versus off path location (D = 1600 km, A = 800 km, T = 500 km,  $\beta = 1, 5$  dB,  $\phi = 0^\circ$ ).

D = 1600 KM  
 A = 800 KM  
 T = 500 KM  
 BETA = 4 DB  
 FREQ = 75 HZ

PHI = -15 DEGREES  
 PHI = 0 DEGREES  
 PHI = 15 DEGREES

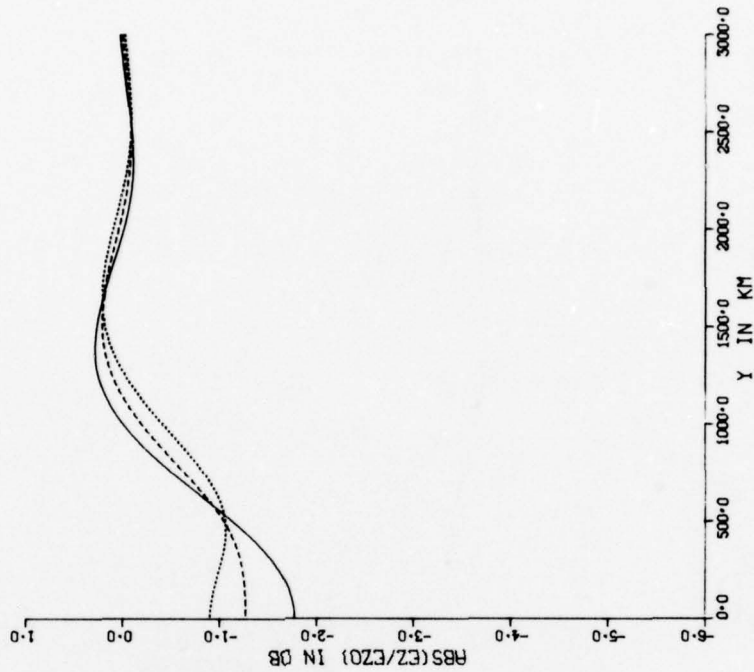


Figure 16. Signal level versus off path location (D = 1600 km, A = 800 km, T = 500 km,  $\beta = 4$  dB,  $\phi = -15^\circ, 0^\circ, 15^\circ$ ).

D = 1600 KM  
 A = 500 KM  
 T = 500 KM  
 BETA = 4 DB  
 FREQ = 75 HZ

PHI = -15 DEGREES  
 PHI = 0 DEGREES  
 PHI = 15 DEGREES

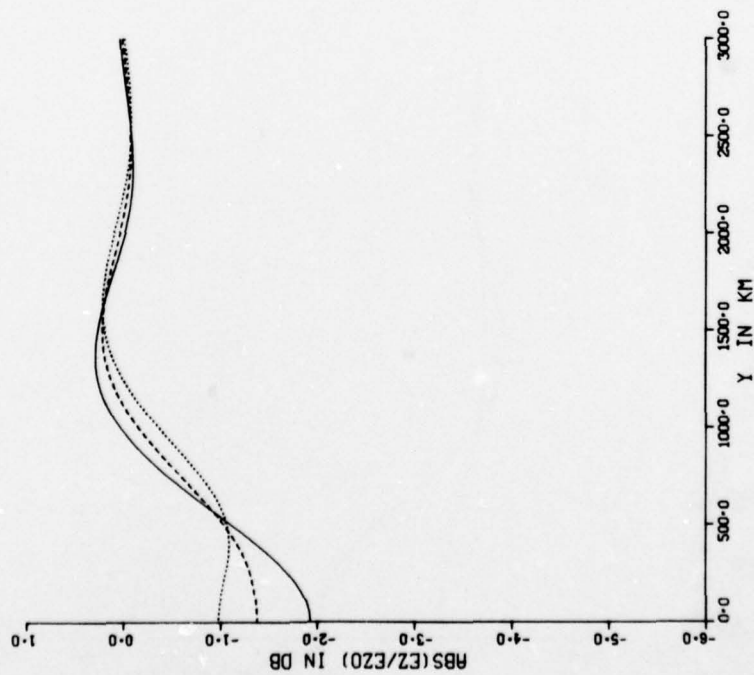


Figure 15. Signal level versus off path location (D = 1600 km, A = 500 km, T = 500 km,  $\beta = 4$  dB,  $\phi = -15^\circ, 0^\circ, 15^\circ$ ).

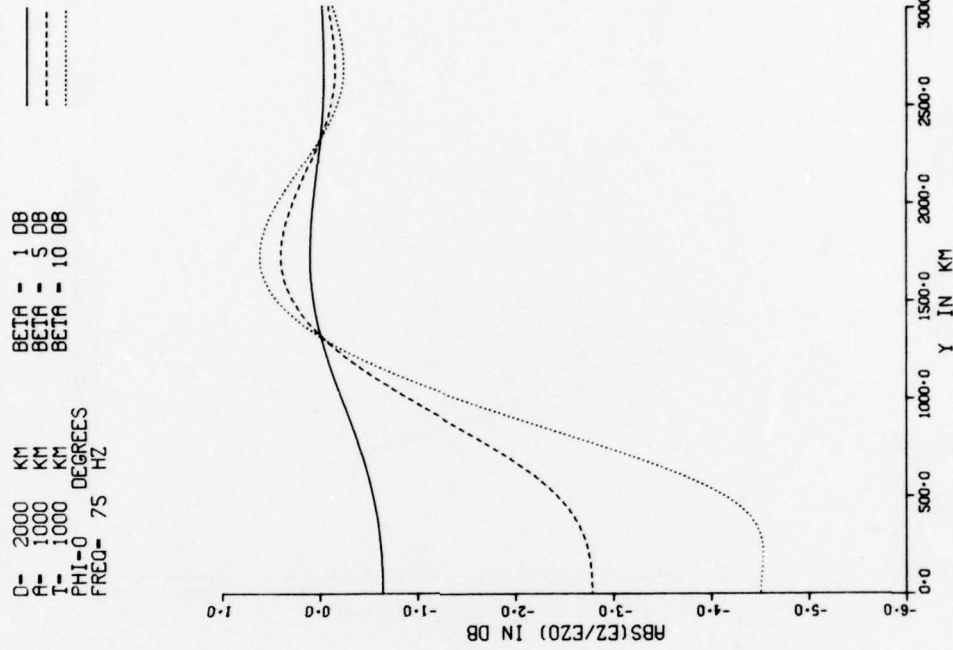


Figure 18. Signal level versus off path location ( $D = 2000$  km,  $A = 1,000$  km,  $T = 1,000$  km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

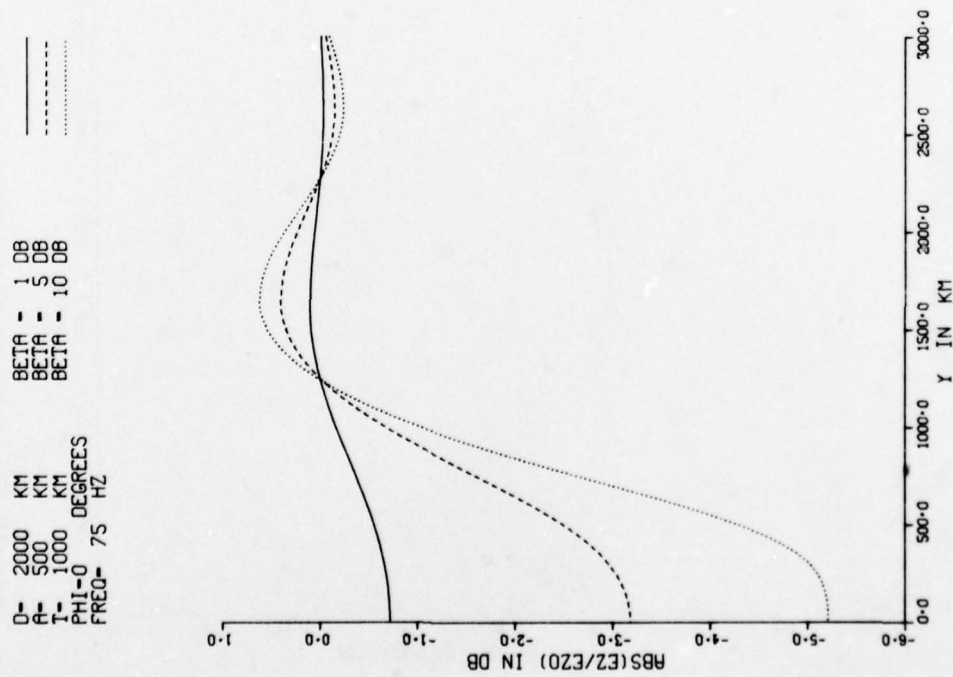


Figure 17. Signal level versus off path location ( $D = 2000$  km,  $A = 500$  km,  $T = 1,000$  km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D = 2000 KM  
 A = 1000 KM  
 T = 1000 KM  
 BETA = 8 DB  
 FREQ = 75 HZ

PHI = -30 DEGREES  
 PHI = 0 DEGREES  
 PHI = 30 DEGREES

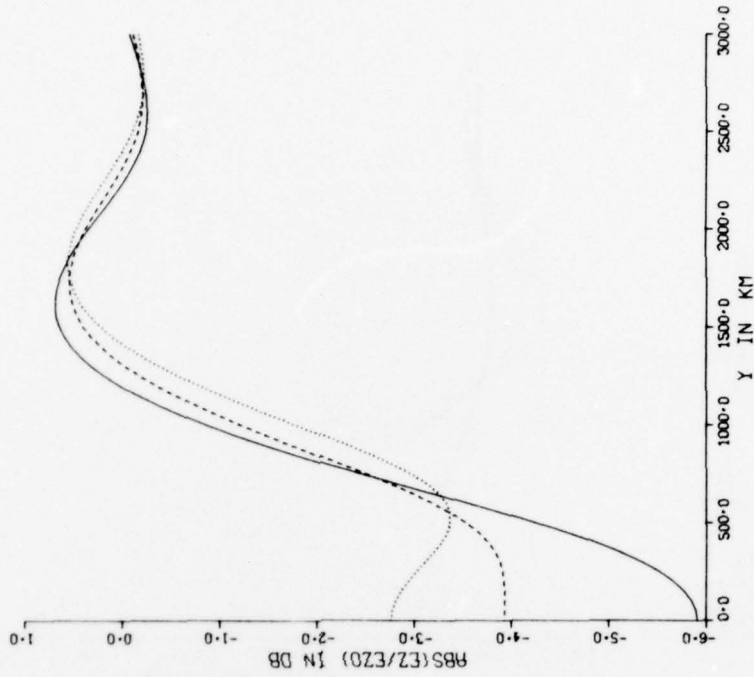


Figure 20. Signal level versus off path location (D = 2000 km, A = 1000 km, T = 1,000 km,  $\beta = 8$  dB,  $\phi = 30^\circ, 0^\circ, 30^\circ$ ).

D = 2000 KM  
 A = 500 KM  
 T = 1000 KM  
 BETA = 8 DB  
 FREQ = 75 HZ

PHI = -30 DEGREES  
 PHI = 0 DEGREES  
 PHI = 30 DEGREES

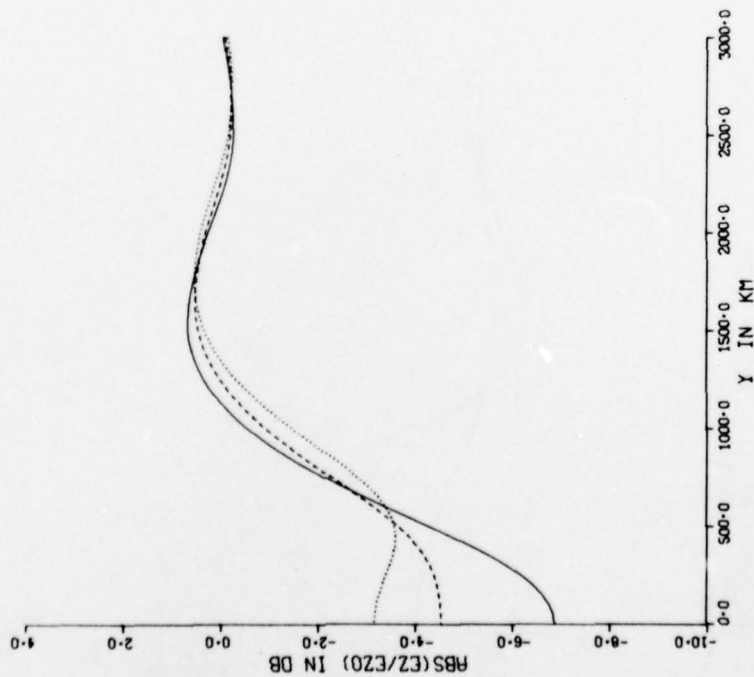


Figure 19. Signal level versus off path location (D = 2000 km, A = 500 km, T = 1,000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D- 4000 KM  
 A- 1000 KM  
 T- 1000 KM  
 PHI-0 DEGREES  
 FREQ- 75 HZ

BETA - 1 DB  
 BETA - 5 DB  
 BETA - 10 DB

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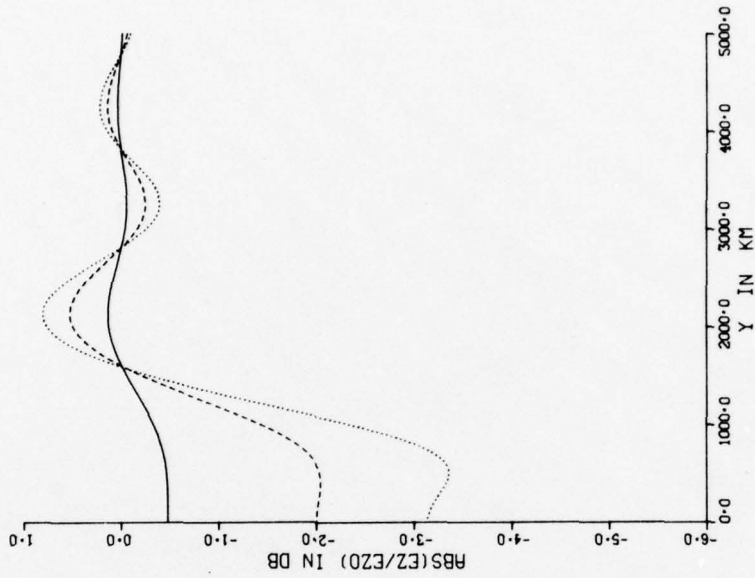


Figure 22. Signal level versus off path location (D = 4000 km, A = 1000 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D- 4000 KM  
 A- 500 KM  
 T- 1000 KM  
 PHI-0 DEGREES  
 FREQ- 75 HZ

BETA - 1 DB  
 BETA - 5 DB  
 BETA - 10 DB

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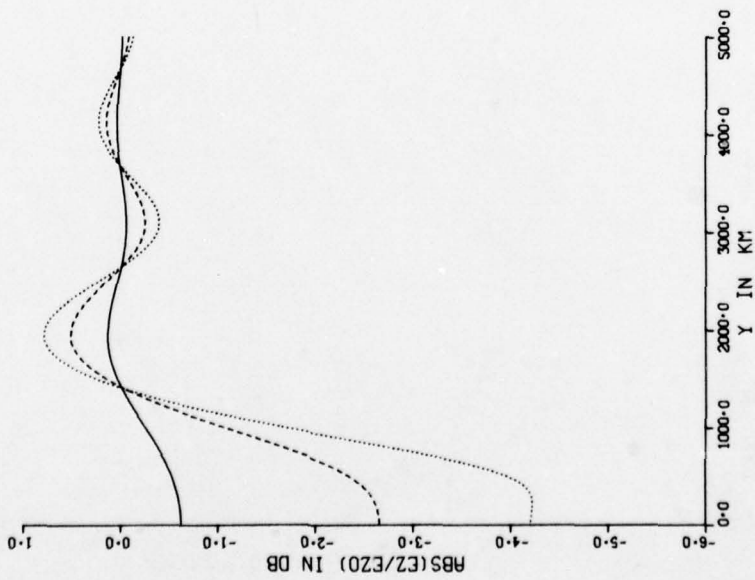


Figure 21. Signal level versus off path location (D = 4000 km, A = 500 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D- 4000 KM  
 A- 500 KM  
 T- 1000 KM  
 BETA- 8 DB  
 FREQ- 75 HZ

PHI- -30 DEGREES  
 PHI- 0 DEGREES  
 PHI- 30 DEGREES

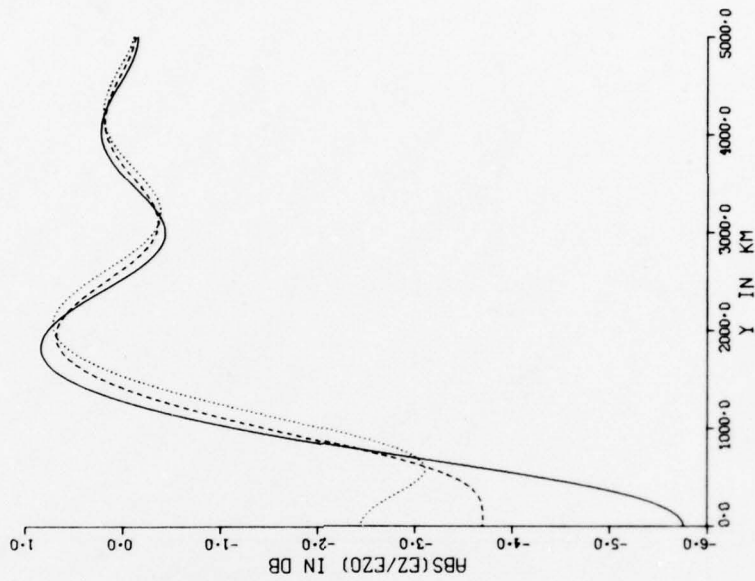


Figure 24. Signal level versus off path location (D = 4000 km, A = 500 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D- 4000 KM  
 A- 2000 KM  
 T- 1000 KM  
 PHI- 0 DEGREES  
 FREQ- 75 HZ

BETA - 1 DB  
 BETA - 5 DB  
 BETA - 10 DB

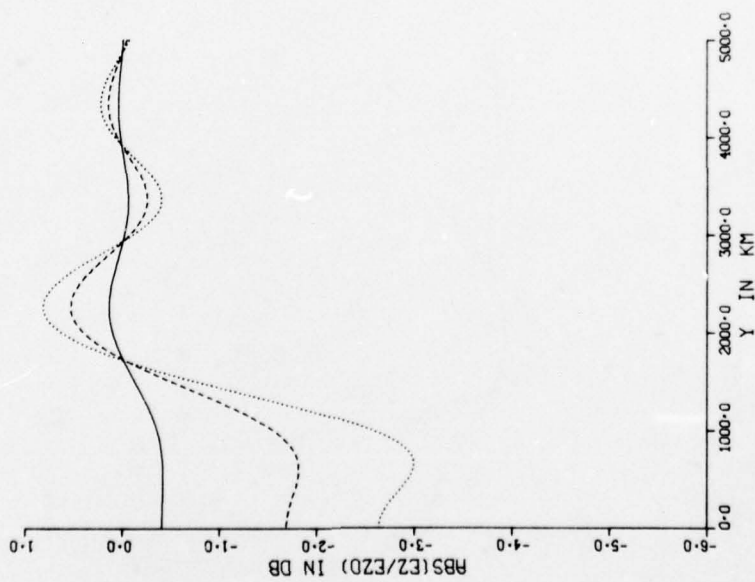


Figure 23. Signal level versus off path location (D = 4000 km, A = 2000 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D= 4000 KM  
 A= 2000 KM  
 T= 1000 KM  
 BETA= 8 DB  
 FREQ= 75 HZ

PHI= -30 DEGREES  
 PHI= 0 DEGREES  
 PHI= 30 DEGREES

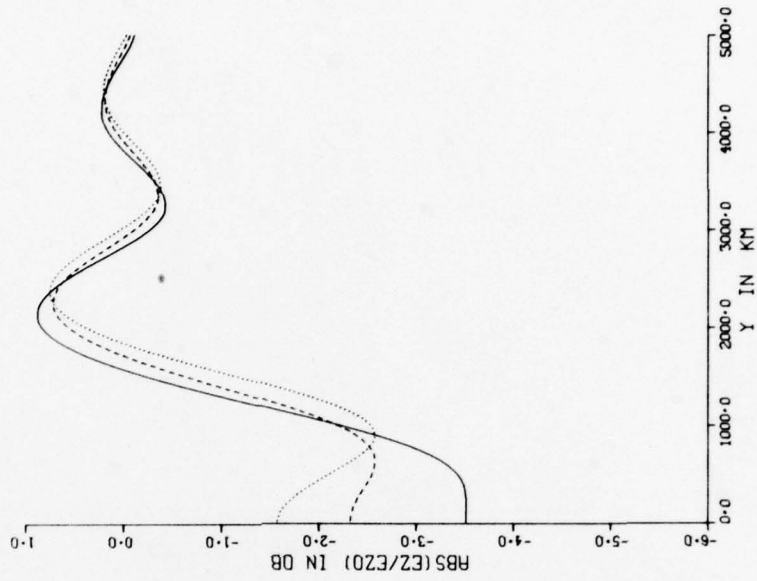


Figure 26. Signal level versus off path location (D = 4000 km,  
 A = 2000 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D= 4000 KM  
 A= 1000 KM  
 T= 1000 KM  
 BETA= 8 DB  
 FREQ= 75 HZ

PHI= -30 DEGREES  
 PHI= 0 DEGREES  
 PHI= 30 DEGREES

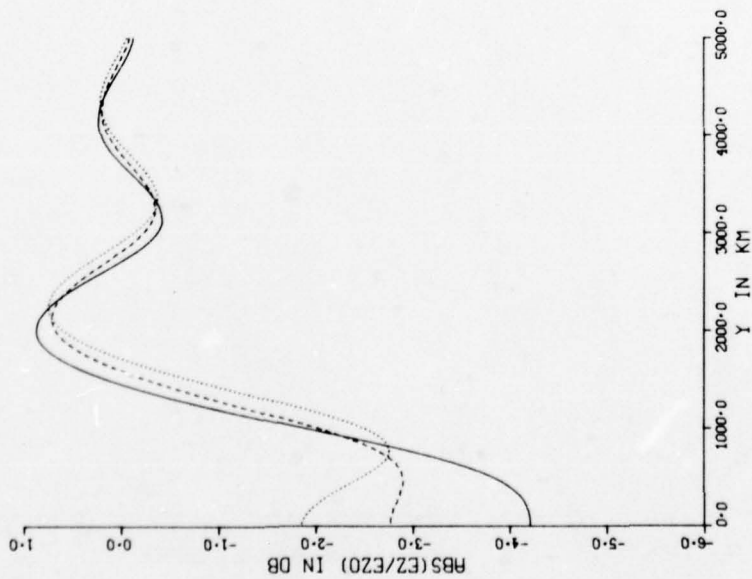


Figure 25. Signal level versus off path location (D = 4000 km,  
 A = 1000 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D- 6000 KM  
 A- 1000 KM  
 T- 1000 KM  
 PHI-0 DEGREES  
 FREQ- 75 HZ  
 BETA - 1 DB  
 BETA - 5 DB  
 BETA - 10 DB

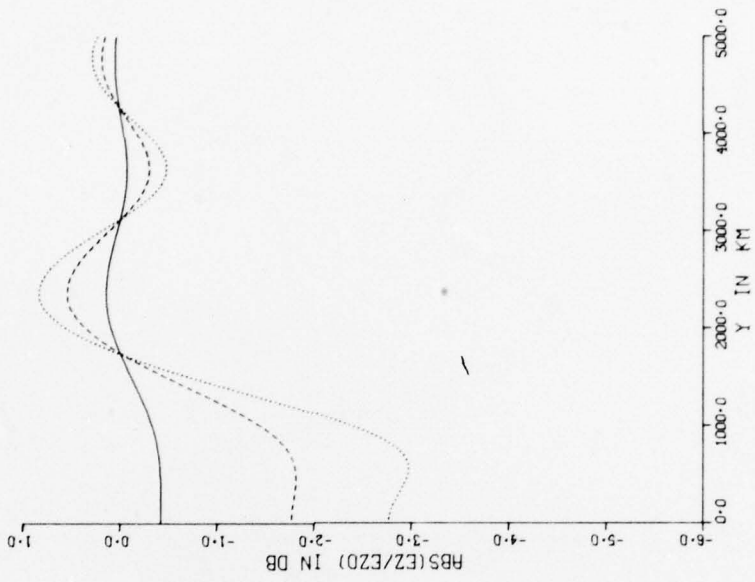


Figure 28. Signal level versus off path location (D = 6000 km, A = 1000 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D- 6000 KM  
 A- 500 KM  
 T- 1000 KM  
 PHI-0 DEGREES  
 FREQ- 75 HZ  
 BETA - 1 DB  
 BETA - 5 DB  
 BETA - 10 DB

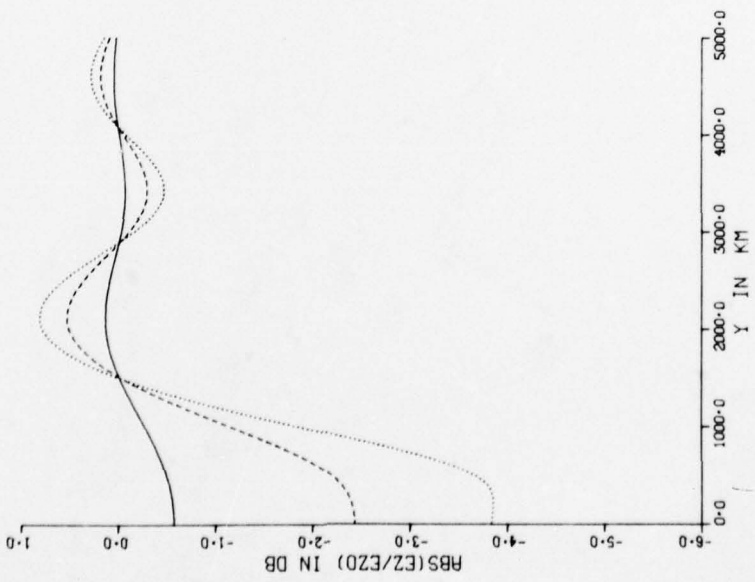


Figure 27. Signal level versus off path location (D = 6000 km, A = 500 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D = 6000 KM  
 A = 500 KM  
 T = 1000 KM  
 BETA = 8 DB  
 FREQ = 75 HZ

PHI = -30 DEGREES  
 PHI = 0 DEGREES  
 PHI = 30 DEGREES

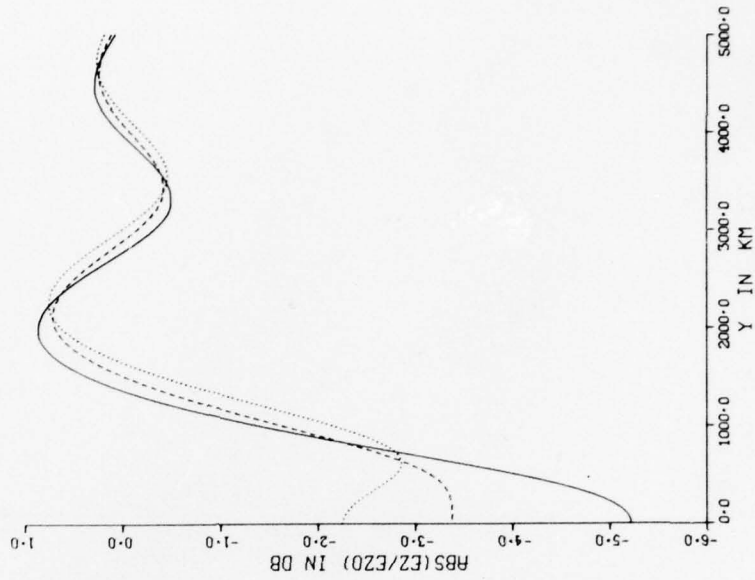


Figure 29. Signal level versus off path location (D = 6000 km, A = 3000 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D = 6000 KM  
 A = 3000 KM  
 T = 1000 KM  
 PHI = 0 DEGREES  
 FREQ = 75 HZ

BETA = 1 DB  
 BETA = 5 DB  
 BETA = 10 DB

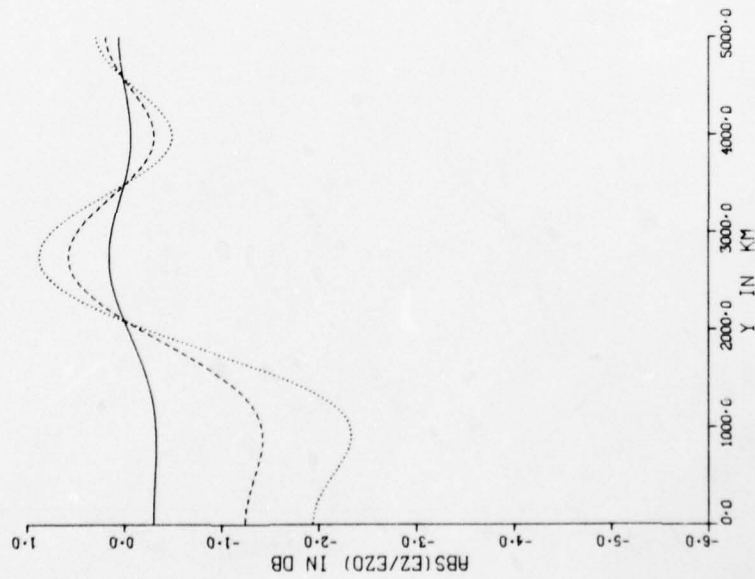


Figure 30. Signal level versus off path location (D = 6000 km, A = 500 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D = 6000 KM  
 A = 1000 KM  
 T = 1000 KM  
 BETA = 8 DB  
 FREQ = 75 HZ

PHI = -30 DEGREES  
 PHI = 0 DEGREES  
 PHI = 30 DEGREES

DEGREES  
 DEGREES  
 DEGREES

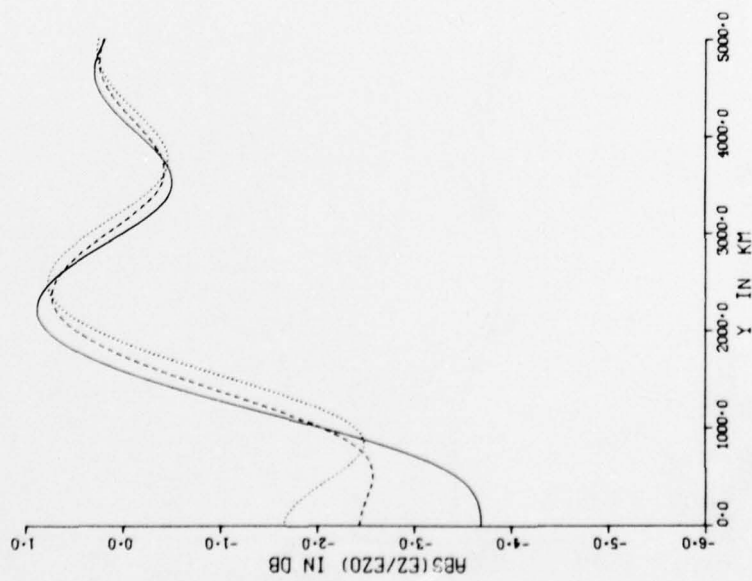


Figure 31. Signal level versus off path location (D = 6000 km, A = 1000 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D = 6000 KM  
 A = 3000 KM  
 T = 1000 KM  
 BETA = 8 DB  
 FREQ = 75 HZ

PHI = -30 DEGREES  
 PHI = 0 DEGREES  
 PHI = 30 DEGREES

DEGREES  
 DEGREES  
 DEGREES

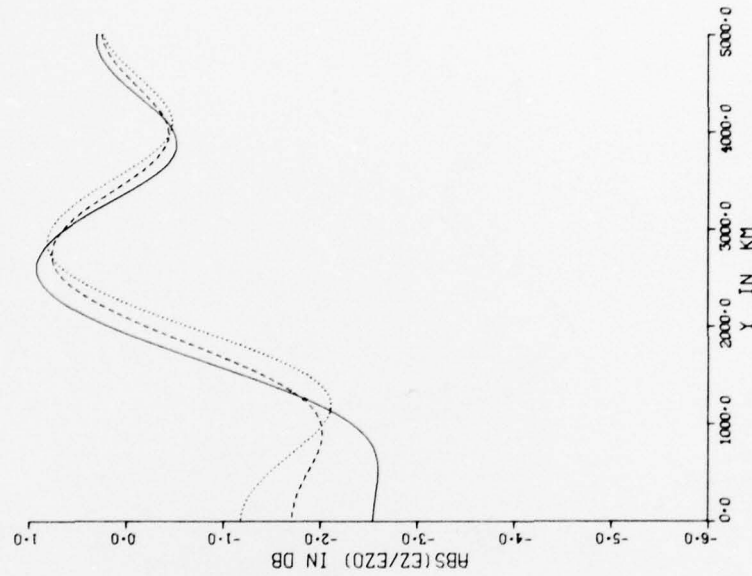


Figure 32. Signal level versus off path location (D = 6000 km, A = 3000 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D- 8000 KM  
 A- 1000 KM  
 T- 1000 KM  
 PHI=0 DEGREES  
 FREQ= 75 HZ

BETA = 1 DB  
 BETA = 5 DB  
 BETA = 10 DB

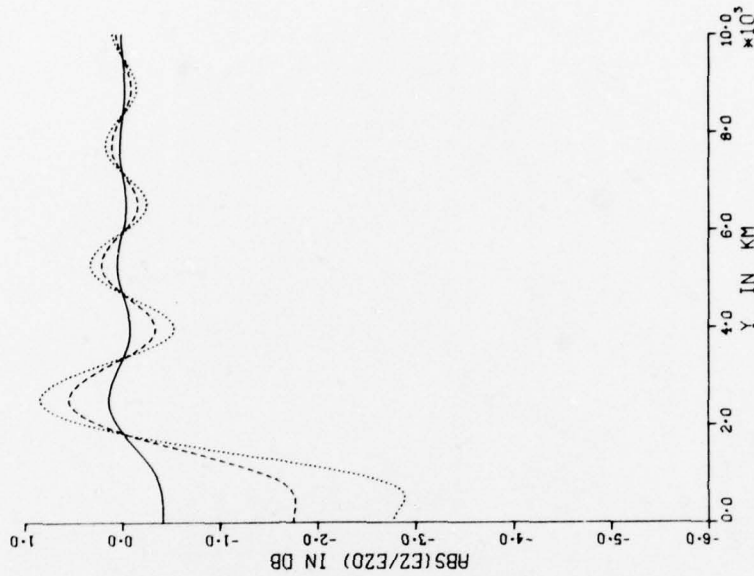


Figure 34. Signal level versus off path location (D = 8000 km, A = 1000 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D- 8000 KM  
 A- 500 KM  
 T- 1000 KM  
 PHI=0 DEGREES  
 FREQ= 75 HZ

BETA = 1 DB  
 BETA = 5 DB  
 BETA = 10 DB

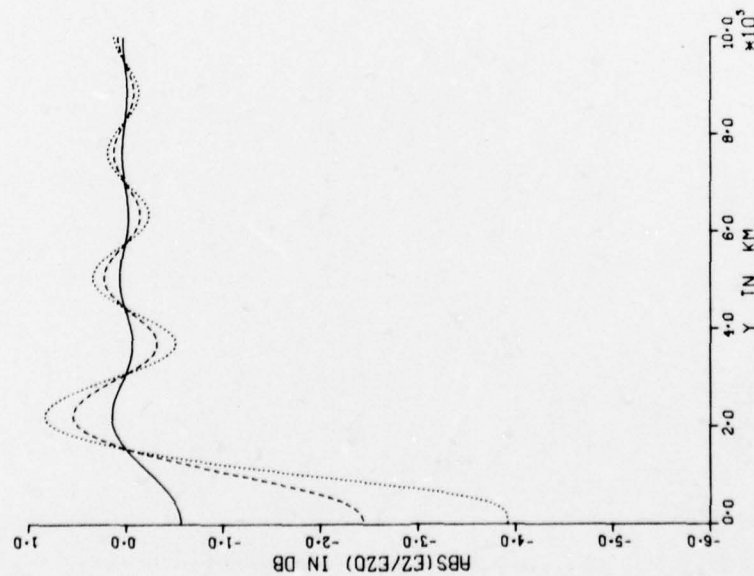


Figure 33. Signal level versus off path location (D = 8000 km, A = 500 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D- 8000 KM  
 A- 500 KM  
 T- 1000 KM  
 BETA- 8 DB  
 FREQ- 75 HZ  
 PHI- -30 DEGREES  
 PHI- 0 DEGREES  
 PHI- 30 DEGREES

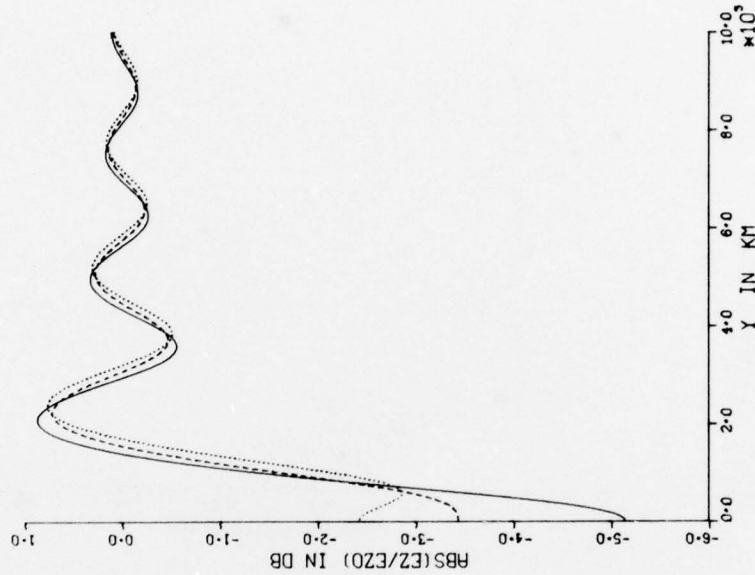


Figure 36. Signal level versus off path location (D = 8000 km, A = 500 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D- 8000 KM  
 A- 4000 KM  
 T- 1000 KM  
 PHI- 0 DEGREES  
 FREQ- 75 HZ  
 BETA - 1 DB  
 BETA - 5 DB  
 BETA - 10 DB

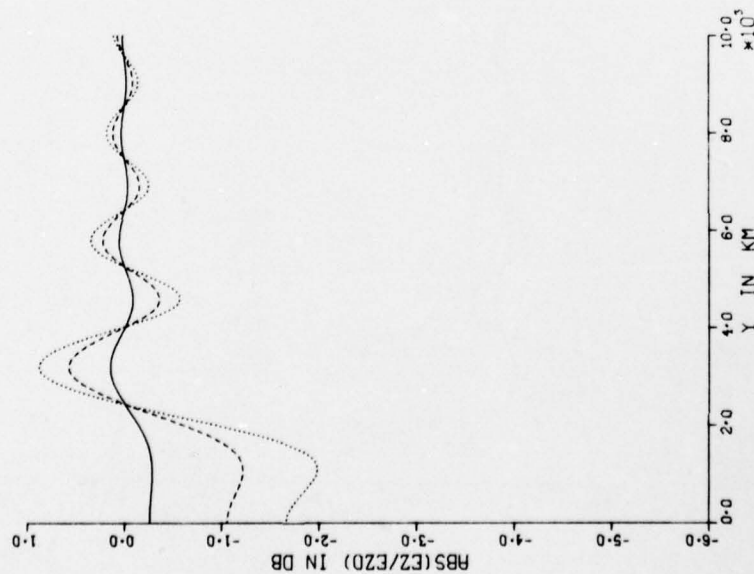


Figure 35. Signal level versus off path location (D = 8000 km, A = 4000 km, T = 1000 km,  $\beta = 1, 5, 10$  dB,  $\phi = 0^\circ$ ).

D= 8000 KM  
 A= 4000 KM  
 T= 1000 KM  
 BETA= 8 DB  
 FREQ= 75 HZ

PHI= -30 DEGREES  
 PHI= 0 DEGREES  
 PHI= 30 DEGREES

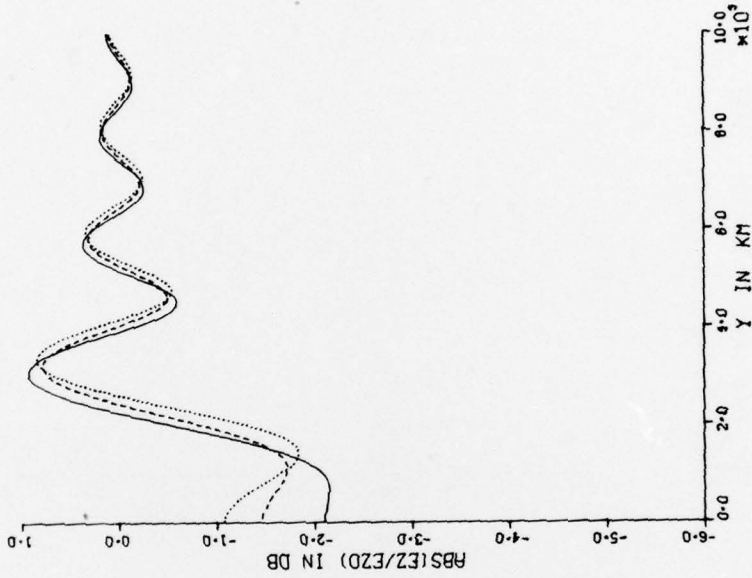


Figure 38. Signal level versus off path location (D = 8000 km, A = 4000 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D= 8000 KM  
 A= 1000 KM  
 T= 1000 KM  
 BETA= 8 DB  
 FREQ= 75 HZ

PHI= -30 DEGREES  
 PHI= 0 DEGREES  
 PHI= 30 DEGREES

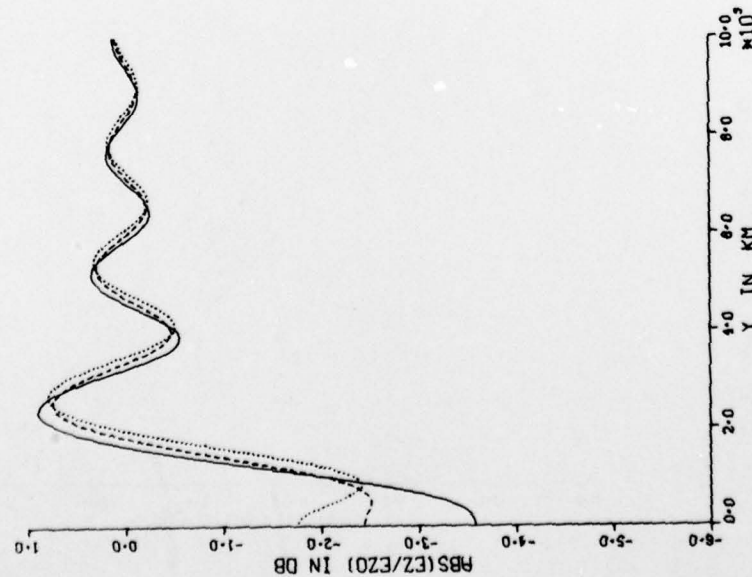


Figure 37. Signal level versus off path location (D = 8000 km, A = 1000 km, T = 1000 km,  $\beta = 8$  dB,  $\phi = -30^\circ, 0^\circ, 30^\circ$ ).

D = 8000 KM  
 A = 1000 KM  
 T = 1000 KM  
 Y = 0 KM  
 FREQ = 75 HZ

BETA = 6 DB  
 BETA = 8 DB  
 BETA = 10 DB

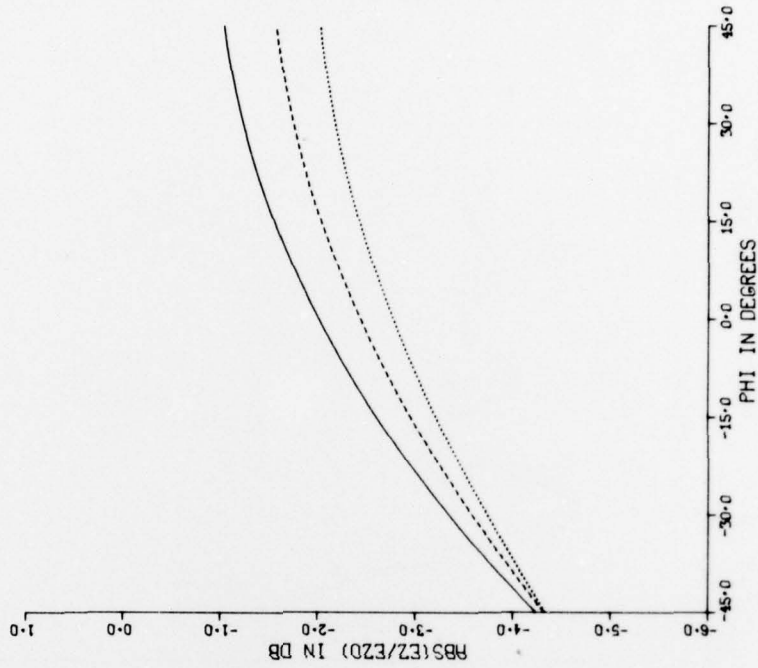


Figure 40. Signal level versus phi (D = 8000 km, A = 1000 km, T = 1000 km,  $\beta = 6, 8, 10$  dB).

D = 8000 KM  
 A = 500 KM  
 T = 1000 KM  
 Y = 0 KM  
 FREQ = 75 HZ

BETA = 6 DB  
 BETA = 8 DB  
 BETA = 10 DB

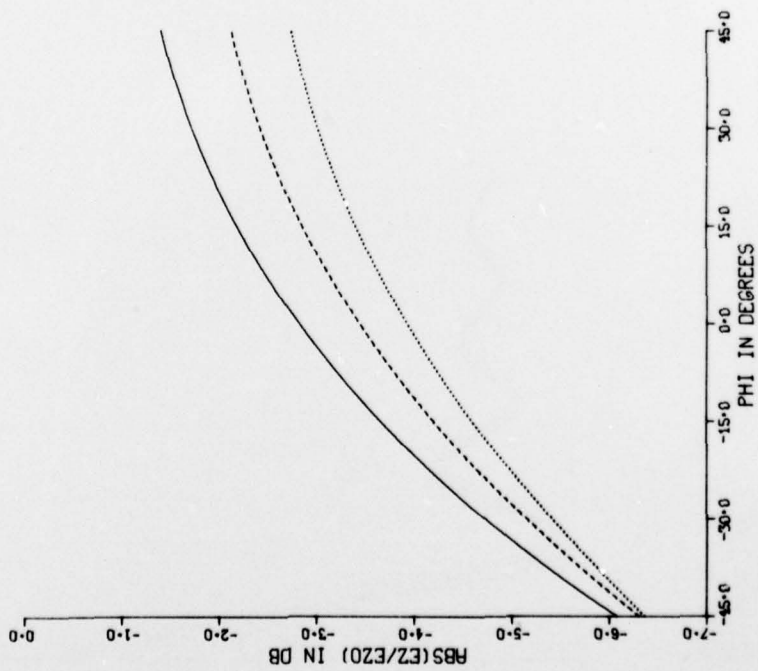


Figure 39. Signal level versus phi (D = 8000 km, A = 500 km, T = 1000 km,  $\beta = 6, 8, 10$  dB).

D- 8000 KM	BETA- 6 DB	———
A- 4000 KM	BETA- 8 DB	- - - - -
T- 1000 KM	BETA- 10 DB	.....
Y - 0 KM		
FREQ- 75 HZ		

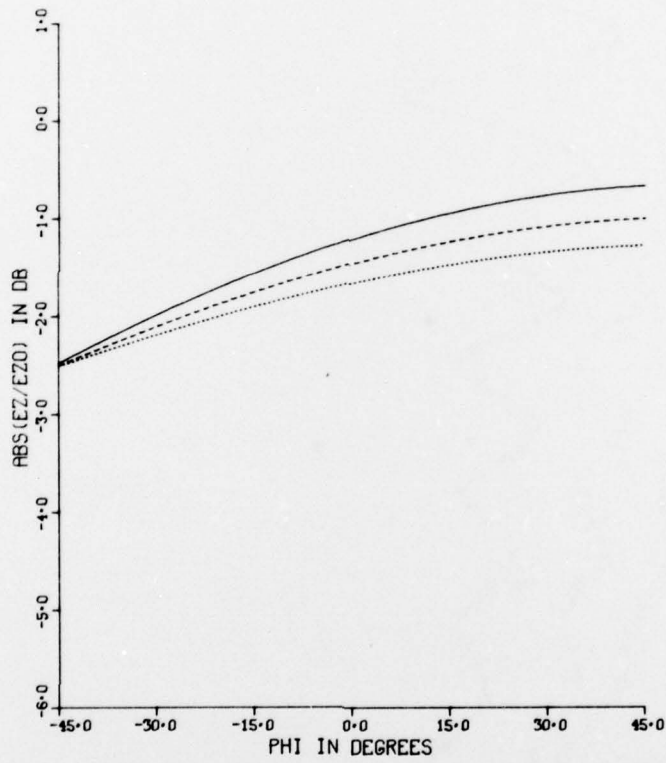


Figure 41. Signal level versus phi (D = 8000 km, A = 4000 km, T = 1000 km,  $\beta = 6, 8, 10$  dB).

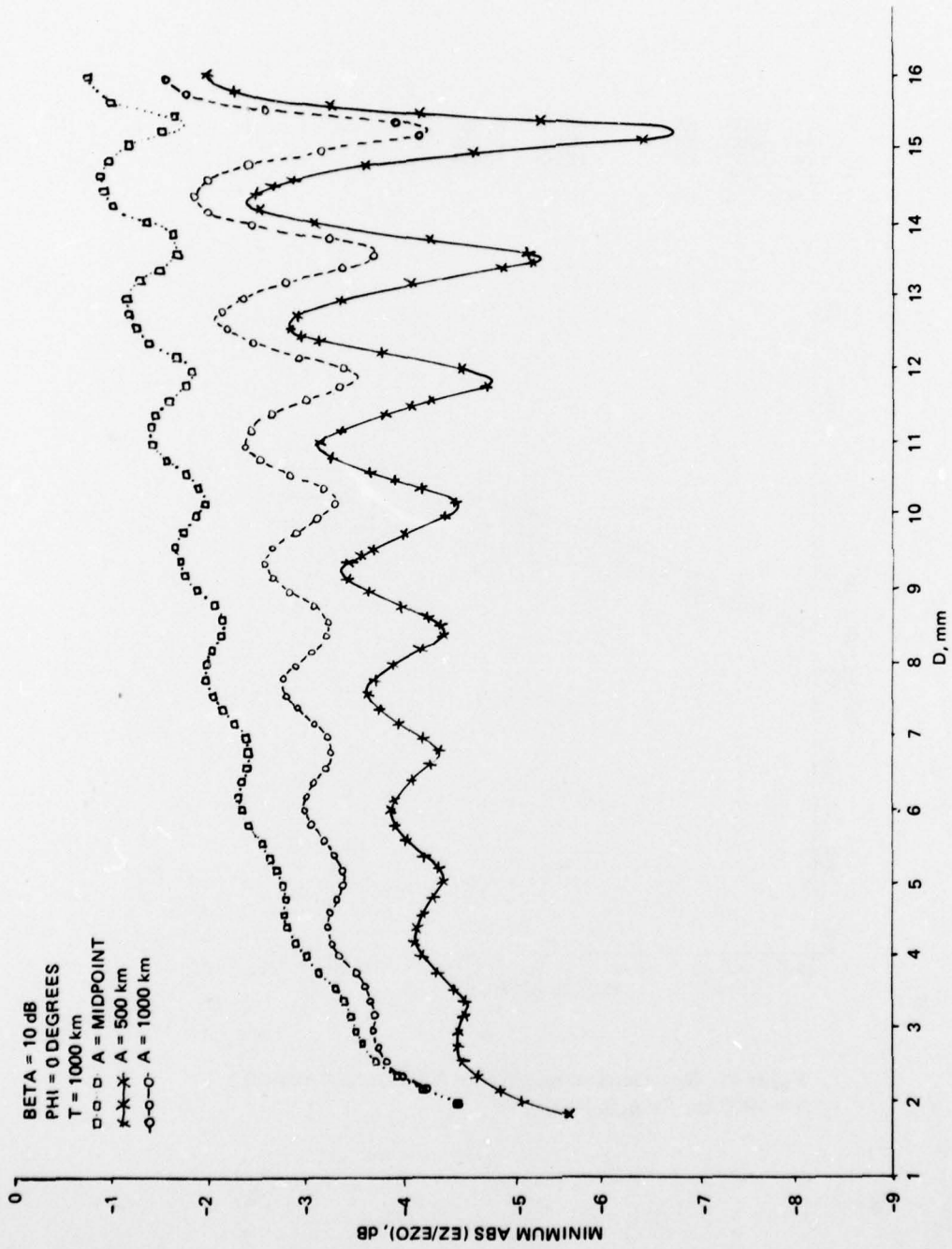


Figure 42. Minimum signal level versus transmitter-receiver distance.

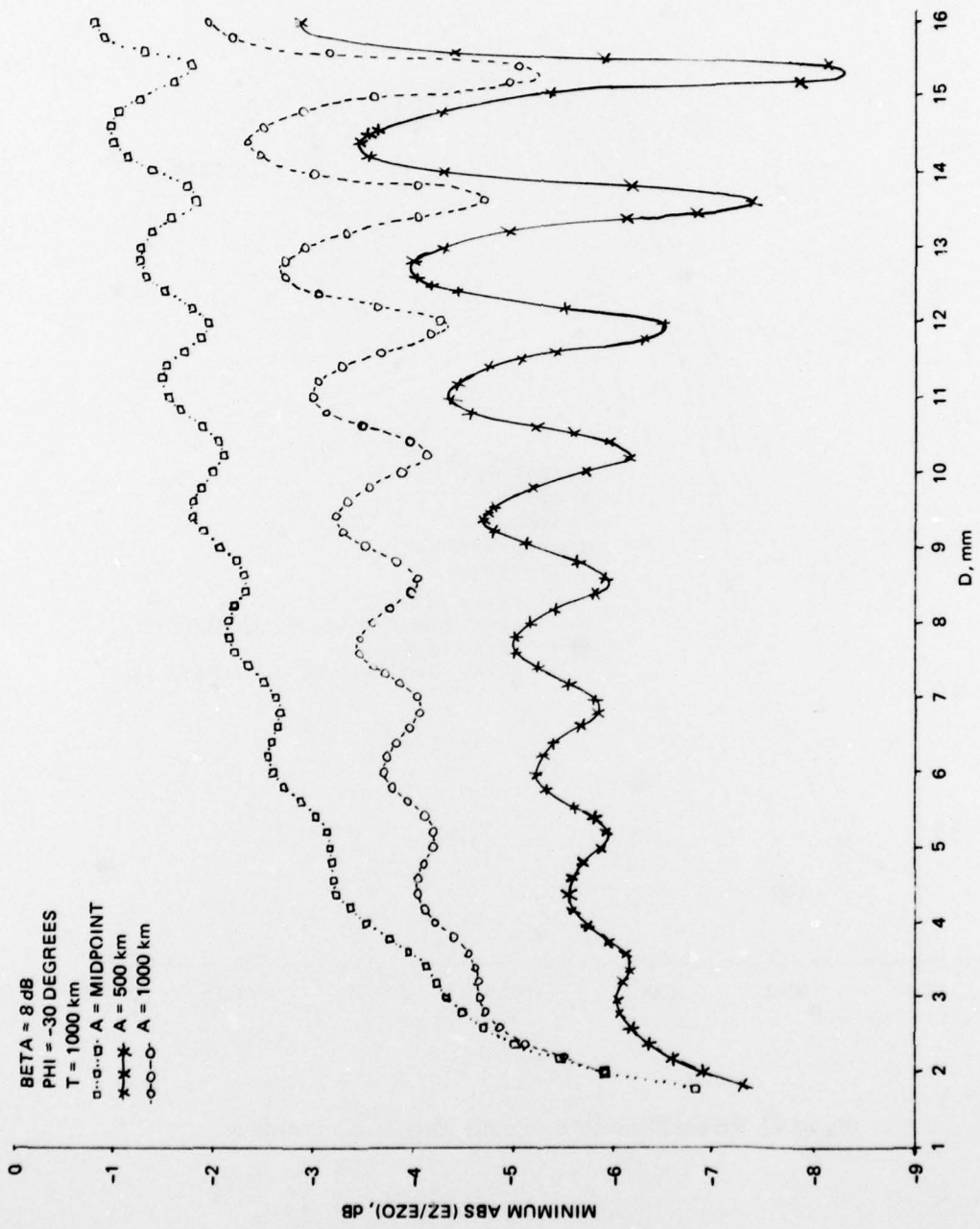


Figure 43. Minimum signal level versus transmitter-receiver distance.

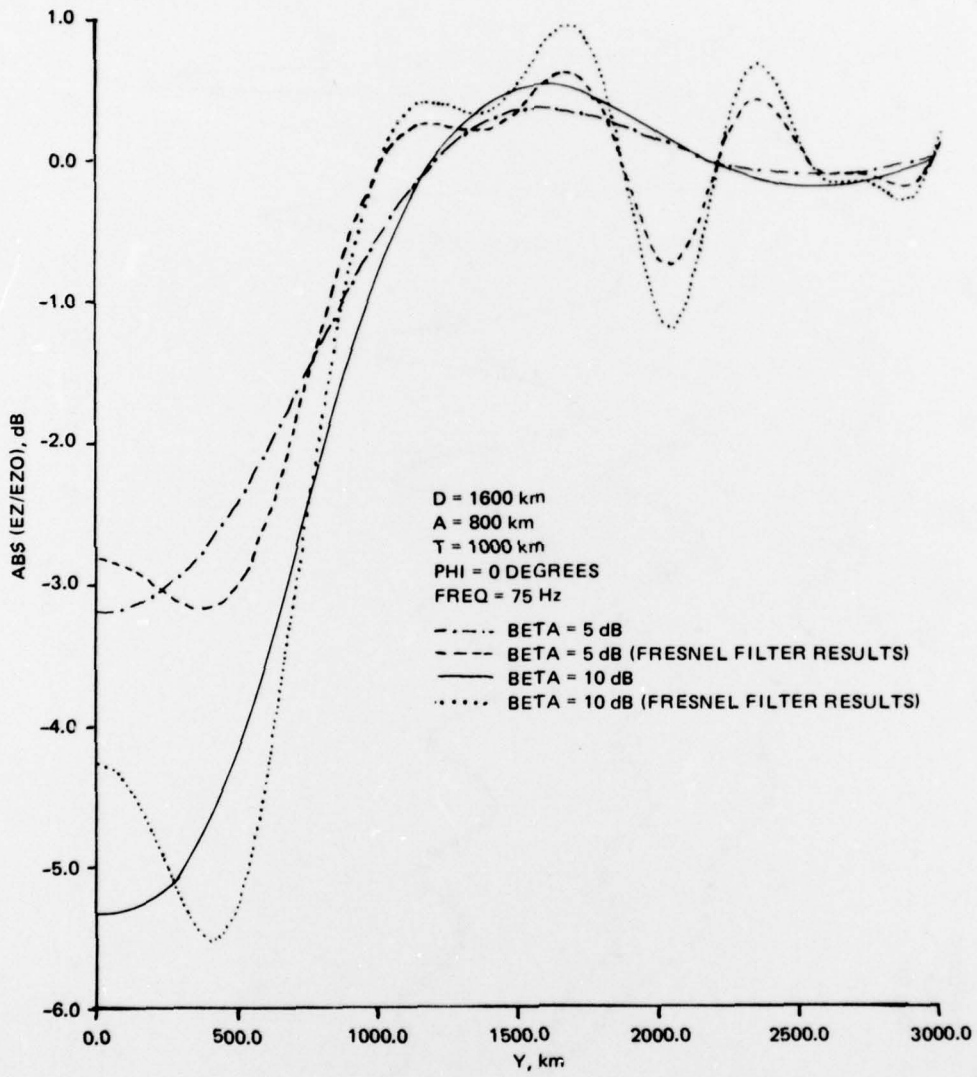


Figure 44. Fresnel filtering and numerical integration comparisons.

#### IV. CONCLUSIONS

A simple Kirchhoff-Huygens diffraction model has been used to estimate the effect of a finite sized patch of sporadic E on lower ELF propagation. The patch is approximated by a lumped parameter phase-amplitude screen allowed to move along a great circle path transverse to the transmitter-receiver great circle path.

The results indicate that sporadic E patches on the order of  $1000 \text{ km} \times 1000 \text{ km}$  causing phase rate shifts, and attenuation rate enhancements consistent with full wave modal evaluations, can account for the 6-8 dB fades observed in connection with the 1600 km WTF transmissions. The results suggest also that such disturbances can be expected to produce 2 to 4 dB fades over paths as long as 10,000 km. Deep fades require the center of the phase amplitude screen to be well within the first Fresnel zone and the effects of the disturbances are highly damped out when the center of the phase-amplitude screen exceeds about two Fresnel zones. It has been shown that phase shifts as well as attenuation enhancement can be influential in determining the perturbed signal. In fact, the deepest fades encountered in the present study were with the combination  $\phi = -30^\circ$ ,  $\beta = 8 \text{ dB}$ .

No allowance for excitation factor effects has been made in the study even though Figures 5 and 6 indicate that such effects could be important should the disturbed region fall over either the transmitter or receiver. Such effects would be best handled by a full wave treatment of the problem and the calculations presented in this study fully support the need for such programs. Development of the latter would benefit from a concurrent measurement program simultaneously involving nocturnal ELF propagation and sporadic E soundings over and about the path.

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Interservice Nuclear Weapons School  
Kirtland AFB, NM 87115  
O1CY ATTN Document Control

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Joint Strat TGT Planning Staff JCS  
Offutt AFB  
Omaha, NB 68113  
O1CY ATTN JPST CAPT D. G. Goetz

Chief  
Livermore Division Fld Command DNA  
Lawrence Livermore Laboratory  
P.O. Box 808  
Livermore, CA 94550  
O1CY ATTN FCPRL

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National Security Agency  
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The Pentagon  
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and Engineering  
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Washington, DC 20301  
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US Army Electronics Command  
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US Army Nuclear Agency  
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US Army Research Office  
P.O. Box 12211  
Triangle Park, NC 27709  
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O1CY ATTN Code 5404 J. Galet

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Naval Ocean Systems Center  
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O1CY ATTN Code 81 H.D. Smith  
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Fort Trumbull  
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ADC/DC  
ENT AFB, CO 80912  
O1CY ATTN DC Mr. Long

Commander  
ADCOM/XPD  
ENT AFB, CO 80912  
O1CY ATTN XPQDQ  
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Foreign Technology Division, AFSC  
Wright-Patterson AFB, OH 45433  
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HQ USAF/RD  
Washington, DC 20330  
O1CY ATTN RDQ  
Headquarters  
North American Air Defense Command  
1500 East Boulder  
Colorado Springs, CO 80912  
O1CY ATTN Chief Scientist

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Strategic Air Command  
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US Energy Research and Dev. Admin.

Department of Energy  
Albuquerque Operations Office  
P.O. Box 5400  
Albuquerque, NM 87115  
O1CY ATTN Doc Con for D. W. Sherwood

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Division of Military Application  
Department of Energy  
Washington, DC 20545  
O1CY ATTN Doc Con for Donald I. Gale

University of California  
Lawrence Livermore Laboratory  
P.O. Box 808  
Livermore, CA 94550  
O1CY ATTN Glenn C. Werth L-216  
O1CY ATTN Tech. Info Dept L-3

Los Alamos Scientific Laboratory  
P.O. Box 1663  
Los Alamos, NM 87545  
O1CY ATTN Doc Con for T. F. Taschek  
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Livermore Laboratory  
P.O. Box 969  
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Sandia Laboratories  
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Albuquerque, NM 87115  
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318 Electrical Engineering East  
University Park, PA 16802  
02CY ATTN Ionospheric Rsch Lab.

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Stanford, CA 94305  
01CY ATTN R. A. Helliwell  
01CY ATTN A. Fraser-Smith  
01CY ATTN J. Katsufraakis

TRW Defense & Space Sys. Group  
One Space Park  
Redondo Beach, CA 90278  
01CY ATTN Saul Altschuler  
01CY ATTN Dianna Dee

Jet Propulsion Laboratory  
4800 Oak Grove Drive  
Pasadena, CA 91103  
01 Cy ATTN: Ernest K. Smith  
Mail Code: 144-B13