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OREGON STATE UNIV CORVALLIS SCHOOL OF OCEANOGRAPHY
MARINE SEISMIC REFRACTION DATA BETWEEN WAINWRIGHT INLET AND PRU--ETC(U)
JUN 79 M BEE, S H JOHNSON, E F CHIBURIS

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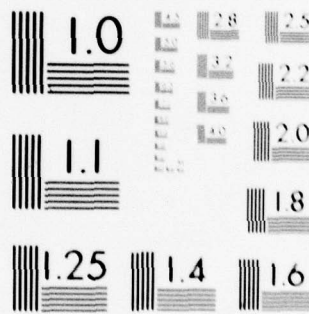
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SCHOOL OF OCEANOGRAPHY TECHNICAL REPORT No. 79-9

GEOPHYSICS TECHNICAL REPORT No. 790626

MARINE SEISMIC REFRACTION DATA BETWEEN WAINWRIGHT INLET AND PRUDHOE BAY, ALASKA.

BY

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RECEIVED
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12 12 pp.

- 1 SCHOOL OF OCEANOGRAPHY, OREGON STATE UNIVERSITY, CORVALLIS OR, 97331
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OFFICE OF NAVAL RESEARCH CONTRACTS N00014-76-C-0067 AND N00014-75-C-0714

272 268

79 08 31 053

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SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER 79-9	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) MARINE SEISMIC REFRACTION DATA BETWEEN WAINWRIGHT INLET AND PRUDHOE BAY, ALASKA		5. TYPE OF REPORT & PERIOD COVERED Technical report
		6. PERFORMING ORG. REPORT NUMBER
7. AUTHOR(s) Michel Bee Stephen H. Johnson Edward F. Chiburis, and Richard E. McAlister		8. CONTRACT OR GRANT NUMBER(s) N00014-76-C-0067 and N00014-75-C-0714 <i>ryan</i> <i>d. un.</i>
9. PERFORMING ORGANIZATION NAME AND ADDRESS School of Oceanography Oregon State University Corvallis, OR 97331		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS NR 083-102
11. CONTROLLING OFFICE NAME AND ADDRESS Office of Naval Research Ocean Science & Technology Division Arlington, Virginia 22217		12. REPORT DATE June 1979
		13. NUMBER OF PAGES 107
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The tectonic history of the Arctic Ocean Basin, and in particular the Canada Basin and the adjoining Beaufort Sea shelf, today remains unclear even after decades of geological and geophysical investigations. Reconstruction of the tectonic history of the margin requires information about the deep crustal structure of northern Alaska at the Beaufort Sea. In 1975 and 1976 a substantial amount of refraction data was successfully collected on the Alaskan shelf from an icebreaker. This technical report contains a detailed description		

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CONF of the methods and techniques used in the data collection and analysis. Interpretation of the data is the subject of articles to be submitted to professional journals.

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DATA BETWEEN WAINWRIGHT
INLET AND PRUDHOE BAY, ALASKA

by

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Office of Naval Research
Contracts N00014-76-C-0067
and N00014-75-C-0714

Geophysics Technical Report
No. 790626
June 1979

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ACKNOWLEDGEMENTS

It is our pleasure to acknowledge the assistance we received from both the Office of Polar Operations and the Eleventh District of the U.S. Coast Guard and to the divisions of Marine Geology and Geophysics (Code 480) and Arctic Programs (Code 461) of the Office of Naval Research for permission and encouragement to undertake these experiments.

We express our sincere appreciation to Captain Gillett, the officers and crew of the USCGC GLACIER in 1975 and to Captain Fournier, the officers and crew of the USCGC BURTON ISLAND in 1976 for their assistance and cooperation during data gathering at sea under difficult arctic conditions. We appreciate the use of the facilities at the Naval Arctic Research Laboratories at Barrow and assistance from laboratory personnel under the direction of Dr. Warren Denner for invaluable help with logistics. LCDR Bill Vinson directed and assisted in the essential helicopter operations.

Spencer Trombly, R.O. Ahner, Tim Graham, and Edward F. Chiburis, Jr. provided invaluable assistance and pleasant company during the field operations. This research was supported under ONR grants N00014-76-C-0067 to Oregon State University and N00014-75-C-0714 to the University of Connecticut.

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INTRODUCTION

The tectonic history of the Arctic Ocean Basin, and in particular the Canada Basin and the adjoining Beaufort Sea shelf, today remains unclear even after decades of geological and geophysical investigations. Reconstruction of the tectonic history of the margin requires information about the deep crustal structure of northern Alaska at the Beaufort Sea. In 1975 and 1976 a substantial amount of refraction data was successfully collected on the Alaskan shelf from an icebreaker. This technical report contains a detailed description of the methods and techniques used in the data collection and analysis. Interpretation of the data is the subject of articles to be submitted to professional journals.

DATA ACQUISITION

Location

Personnel from Oregon State University and the University of Connecticut conducted marine refraction studies in the eastern Chuckchi Sea and the western Beaufort Sea to obtain structural and velocity information on the continental margin. In contrast to most previous refraction studies in the region which were made from stations located on the ice, these data were obtained using standard marine seismic techniques during the Arctic Summer. Nineteen profiles were obtained between Wainwright Inlet and Prudhoe Bay in August 1975 from the USCG icebreaker Glacier and in August 1976 from the USCG icebreaker Burton Island with helicopter support. The profiles, ranging in length from 13 to 75 km, were roughly parallel to the coastline in about 20 m of water. Heavy ice cover forced many minor course changes and is the reason for the non-linear direction of individual profiles shown in Figure 1.

Techniques

A zone of ice-free or semi ice-free water exists along the northern continental shelf area out to a depth of approximately 2000 meters during one month of the year, and existence of this zone permitted operation of standard marine refraction techniques with sonobuoys and explosive charges.

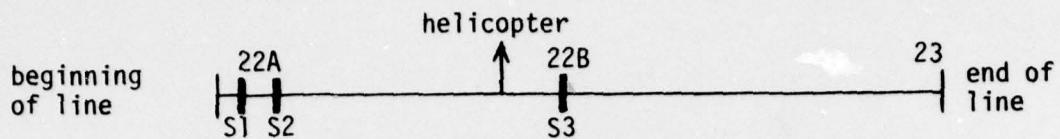
The lines were shot in the standard marine fashion by dropping charges in the water from the fantail of the icebreaker, using powder fuses and tilt table, while the ship was underway. Rotor-mounted yagi antennas received the sonobuoy signals which were recorded on a 4-channel tape recorder. Two of the four channels were sonobuoy signals, one was

a clock signal and one was a shot-break signal from a streamer 3 m long which was towed close behind the ship. When radio contact with the sonobuoys was lost, at a distance of about 30 km because of earth curvature, a portable recording unit consisting of a radio receiver, an amplifier, and strip-chart and tape recorders installed in a helicopter, monitored the sonobuoy. The helicopter remained within radio reception range of the sonobuoy during the shooting.

Expendable naval sonobuoys of the type AN/SSQ 41A were modified for extended time operation by addition of dry-cell batteries which worked well in spite of the cold water. Explosive charges of less than 10 pounds were made up of nitro-carbonitrate (Nitromon) in one pound metal cans. Explosive charges between 30 and 660 pounds were made up of Tovex in 30 pound plastic bags. Extra boosters (Dupont HDP-1) were required for large charges or for long burn times in order to insure complete detonation in the cold water.

Shots were detonated every three minutes at a ship speed of 10 kt which was slightly variable because of ice conditions. This resulted in a shot spacing of about 0.7 km. During the helicopter operations, shots were detonated at intervals of from 5 to 15 minutes resulting in a shot spacing of 1.4 to 4.3 km.

Sonobuoy deployments consisted of two sonobuoys (S1, S2) dropped at the beginning of each line and an intermediate sonobuoy (S3) deployed in the middle of long lines. This resulted in a special line numbering with letter A for the first sonobuoys and letter B for the intermediate one (for example, Lines 22A-23 and 22B-23)



The satellite navigation equipment was inoperative during the second half of the experiment, therefore most of the navigation was by radar fixes to land points at 15 minute intervals. The ice coverage ranged from 0 to 8 octas during the course of the experiment and required frequent course changes and caution on the part of the shooter not to drop the charge onto pieces of floating ice.

Sea-surface currents were not negligible and affected sonobuoy drift. The direction and magnitude of the drift was estimated by combining water wave travel time and navigation. The in-line component of drift ranged from 0 to 1.65 m/s and was quite variable from line to line.

DATA REDUCTION

A combination of manual and computer-aided manipulations shown in the flow chart of Figure 2 transform the raw data to record sections and velocity-depth profiles.

Arrival times for ground and water waves picked on each seismogram and other information such as bathymetry, ship velocity and streamer length, constitute an input data file for computer program TIMCORM. This program computes corrected ground and water wave arrival times to a datum, making corrections for the shot instant due to separation of shot and streamer and surface and bottom corrections at receiver and shot.

These results form an input file for the computer program REFPLTT which produces a travel time plot with the corrected arrival times of the ground waves at the distances calculated from corrected water wave arrival times. A first attempt is then made to interpret seismic velocities and the data examined for possible errors.

From the corrected output file obtained from program TIMCORM, the computer program REDPLOT2 produces a reduced time plot where arrival times reduced with a velocity of 5.00 km/s are plotted versus distance

A profile which includes some helicopter refraction data requires an additional routine. A data file is prepared from the ship navigation as an input to computer program UTMSTEVE and its two subroutine programs UTMGRIDB and UTM. These programs plot the navigation data on a Universal Transverse Mercator projection. Shot positions are added manually by interpolating time and arcs are drawn using a compass at a radius corresponding to the water wave travel time. Sonobuoy drift due to wind and currents appears as a non-coincidence of the arcs. A drift rate

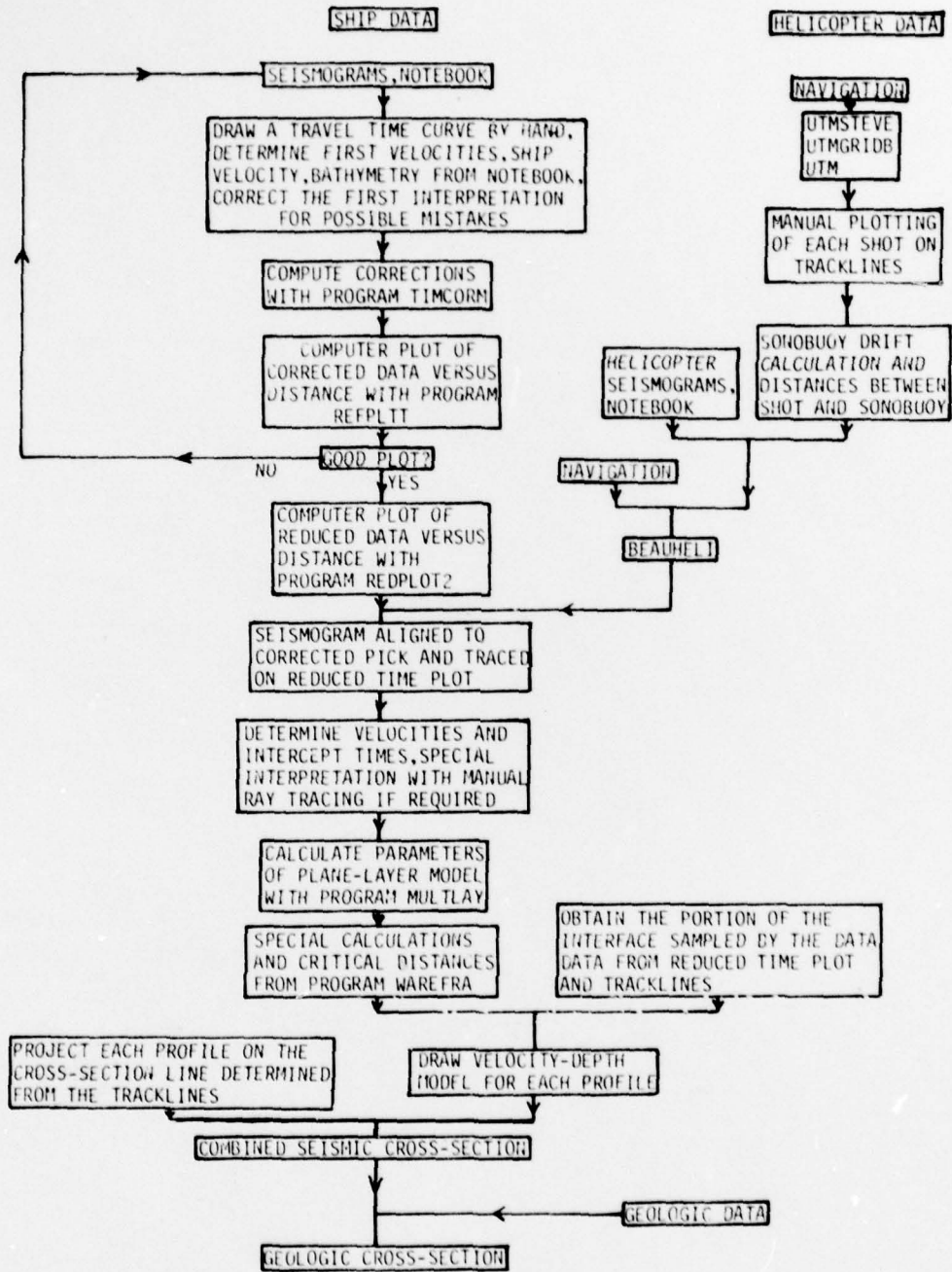


Figure 2. Flow chart of data analysis.

parallel to the trackline is assumed to apply to more distant shots where water wave arrival times may not be detected by the sonobuoy. The shot distance is then the distance between the shot location and the drift position of the sonobuoy at the time of the shot.

The drift distances between the shot and the sonobuoy and the ground wave arrival times from the helicopter refraction data constitute an input file for program BEAUHELI. Computer program BEAUHELI computes time corrections between the ship and the helicopter clocks, the corrected distance between the shot and the sonobuoy, and the corrected travel time for the ground arrival. The strip chart records played back from the helicopter recorder are then aligned to the corrected ground arrival times as plotted on the reduced time plot and traced to produce the record section.

Apparent velocities and intercept times are obtained from this record section and put into the computer program MULTLAY. The computer program MULTLAY computes a model composed of N dipping plane layers from reversed seismic refraction profile data using the formulation of Adachi (1954). The program requires two sets of apparent velocities and intercept times from single-ended refraction data. Complications such as non-reciprocal data or early intercept times require a manual ray tracing method based on the formulation of Adachi (1954).

On each seismic model obtained from MULTLAY the portion of an interface drafted with heavier lines on Figure 8 through Figure 26 represents only that portion of the layer which gives rise to observable seismograms. The offset distances of the rays are obtained from the program WAREFRA. The computer program WAREFRA is based also on the formulation of Adachi (1954) and requires the seismic model obtained from MULTLAY as an input data file.

For the combined velocity-depth section (Figure 27), each profile was projected onto a straight line drawn through the tracklines.

DATA INTERPRETATION

Because of the navigation difficulties, only five lines were reversed. These lines are Lines 1-2 and 6-7, Lines 3-4 and 4-5, Lines 10-11 and 12-13, Lines 22A-23 and 24B-25, and Lines 24A-25 and 22B-23 where the numbers indicate the end points of the lines (see for example Figures 10 and 11). The nine remaining lines (Lines GL-1, GL-2, 8A-9A, 8B-9B, 16-17, 18-19, 20-21, 26A-27A, 26B-27B) were interpreted as single-ended lines (see for example Figure 19). For complicated lines showing non-reciprocal data or early intercept times, a manual ray tracing method was used (see Figures 16 and 17).

Figures 8 to 26 show the nineteen profile plotted as reduced record sections where the reducing velocity is 5.0 km/s. The distance is plotted as water wave travel time seconds where the water velocity was estimated to be 1.44 km/s. All the velocities are in km/s. The seismic models determined from interpreted reduced sections are composed of plane horizontal or plane dipping layers. These are shown above the record sections with a vertical exaggeration of 3:1. Heavy lines on the refractors indicate the interfaces responsible for observed arrivals and contain the horizontal offsets for upgoing rays. Only the reversed profiles resulted in true velocities, and on all the single-ended profiles apparent velocities are assumed to be true velocities. A few estimated velocities are shown in parentheses.

The composite section shown in Figure 27 summarizes the subsurface velocity and depth information calculated from the refraction data. The heavy lines on the interfaces, corresponding to the observed arrivals as shown in Figures 16 through 26, were projected onto a composite section

which passes through the profiles. The small arrows along each interface correspond to the appropriate refraction lines shown at the top of the figure. The refraction layers from adjacent lines have been correlated on the basis of velocity as indicated in Figure 27 by light lines.

PRESENTATION OF DATA

I

MAP-GENERATING COMPUTER PROGRAMS (UTMSTEVE, UTMGRIDB, UTM)
NAVIGATION LISTING AND
TRACKLINE MAPS

```

UTMSTEVE
1.  COMPILER DOUBLE PRECISION
2.C  PROGRAM UTMMAP
3.C  THIS PROGRAM CALLS UTMGRID TO MAKE AN UNIVERSAL TRANSVERSE
4.C  MERCATOR GRID. IT THEN READS AN AEROMAS DATA FILE AND PLOTS
5.C  EITHER TRACKLINES OR ANNOTATED DATA POINTS ON THE GRID
6.  COMMON /UTM2/ MLAT, SLAT, ELONG, WLONG
7.  REAL LAT, LONG, MLAT, LX, LY, NX, NY, LATM, LONGM
8.  DIMENSION NAME (6), IVARI (2), FNAME (6)
9.C  CONSTANTS FOR THE CALCULATIONS
10.  PI = 3.1415926536
11.  PIB2 = PI / 2.0
12.  PID4 = PI / 4.0
13.  TWOPI = PI * 2
14.  RTOD = 180. / PI
15.  BTOR = PI / 180.
16.  ISIDE = 1
17.C  GO GET THE GRID PARAMETERS AND DRAW THE GRID
18.  CALL UTMGRID
19.  TYPE "ANNOTATE THE DATA PTS"
20.  READ (11, 101) IANS
21.  101 FORMAT (A2)
22.C  SET UP THE INPUT FILE
23.  3 TYPE "FILENAME"
24.  READ (11, 102) FNAME (1)
25.  102 FORMAT (S10)
26.  CALL FOPEN (1, FNAME)
27.C  GET A DATA POINT
28.  10 READ (1, 100, END=20) IVARI, LAT, LATM, LONG, LONGM
29.  100 FORMAT (7X, 2A2, 1X, F3.0, 1X, F5.0, 1X, F4.0, 1X, F5.0)
30.C  CHECK LAT AND LONG FOR WITHIN THE GRID
31.  LAT = LAT + SIGN (LATM/60., LAT)
32.  LONG = LONG + SIGN (LONGM/60., LONG)
33.  IF (LAT .EQ. 0.0) GO TO 10
34.  IF (LONG .LT. 0.0) LONG = 360. + LONG
35.  IF (LAT .LT. SLAT OR LAT .GT. MLAT) GO TO 10
36.  IF (LONG .LT. WLONG OR LONG .GT. ELONG) GO TO 10
37.C  CONVERT LAT AND LONG TO UTM X AND Y
38.  CALL UTM (LAT, LONG, X, Y)
39.C  IF NO ANNOTATION DON'T NEED THE ANGLES ETC
40.  IF (IANS .EQ. 2HNO) GO TO 16
41.C  FIGURE OUT WHERE AND WHAT ANGLE TO ANNOTATE THE DATA POINT
42.  ISIDE = ISIDE * (-1)
43.  YMLY = Y - LY
44.  THETA = ATAN (YMLY / (X-LX))
45.  LX = X
46.  LY = Y
47.  IF (ABS (THETA) .LT. PID4) GO TO 12
48.  ANGLE = 0
49.  NX = X
50.  IF (ISIDE .LT. 0) NX = NX - 0.3
51.  NY = Y
52.  GO TO 13
53.  12 ANGLE = 270.
54.  NX = X
55.  NY = Y
56.  IF (ISIDE .LT. 0) NY = NY + 0.3
57.C  LABEL THE DATA POINT
58.  13 CALL SYMBOL (NX, NY, 0.07, IVARI, ANGLE, 4)
59.  CALL PLOT (X, Y, 3)
60.C  PLOT THE DATA POINT
61.  16 CALL PLOT (X, Y, 2)
62.  CALL MARKER (1)
63.  GO TO 10
64.C  HERE ON EGF
65.  20 CONTINUE
66.  CALL FCLOS (1)
67.C  ANOTHER FILE ON THIS GRID
68.  TYPE "ANOTHER FILE"
69.  READ (11, 101) IFILE
70.  IF (IFILE .EQ. 2HYES) GO TO 5
71.  END

```

```

UTGRID
1.  COMPILER DOUBLE PRECISION
2.  SUBROUTINE UTGRID
3.  THIS SUBROUTINE DRAWS A UTM MERCATOR GRID ON THE PLOTTER IT
4.  QUERRIES THE USER FOR THE MAP PARAMETERS AND LEAVES THEM IN
5.  COMMON FOR THE CALLING PROGRAM
6.  SOUTHERN LATITUDES AND WESTERN LONGITUDES ARE NEGATIVE
7.  UTM MAP WILL WORK ACROSS BOTH THE DATELINE AND GREENWICH
8.  MERIDIAN.
9.  REAL  MINLAT, MAXLAT, MINLONG, MAXLONG
10.  COMMON /UTR1/ SCALE, X0, Y0, BTOR, NTOI, A, B, C, LA, LALA,
11.  1      LESS, ORLESS, CRESID, KO
12.  REAL  LA, LB, LESS, LALA, NTOI, KO
13.  REAL  MINLATR, MAXLATR, MINLONGR, MAXLONGR
14.  REAL  LAT, LONG, MLAT, MIN
15.  COMMON /UTR2/ MLAT, SLAT, ELONG, VLONG
16.  DIMENSION ABCD (40)
17.  CODES FOR THE PLOTTER SUBROUTINES
18.  INTEGER PENUP, PENDOWN, PLOTENB, PEN, ABCD
19.  PENDOWN = 2
20.  PENUP = 3
21.  PLOTENB = -PENUP
22.  CONSTANSY FOR CALCULATIONS
23.  BTOR = 3.1415926536 / 100.
24.  NTOI = 39.37
25.  PARAMETERS FOR A UTM GRID
26.  KO = 0.9996
27.  A = 1.0051092
28.  B = 0.0051202
29.  C = 0.0000100
30.  LA = 6370206.4
31.  LB = 6356583.0
32.  LALA = LA * LA
33.  LESS = (LALA - LB * LB) / LALA
34.  ORLESS = 1.0 - LESS
35.  X0 = 0.0
36.  Y0 = 0.0
37.  IO WRITE (10,100)
38.  LONGS WEST ARE NEGATIVE AND LATS SOUTH ARE NEGATIVE
39.  100 FORMAT ('GIVE THE FOLLOWING: ',//
40.  1      '      MLAT  SLAT  VLONG  ELONG  SCALE  GRID',//
41.  2      '      S  N  S  N  S  N  S  N  1.  N')
42.  READ (11,101) MAXLAT, MAXLATR, MINLAT, MINLATR,
43.  1      MINLONG, MINLONGR, MAXLONG, MAXLONGR,
44.  2      SCALE, MIN
45.  101 FORMAT ('F3.0, F2.0, F3.0, F2.0, F4.0, F2.0, F4.0,
46.  1      F3.0, F4.0, F6.0, F4.0')
47.  MAKE DECIMAL DEGREES OUT OF THE DEGREES AND MINUTES
48.  SLAT = MINLAT + SIGN (MINLATR, MINLAT) / 60.
49.  MLAT = MAXLAT + SIGN (MAXLATR, MAXLAT) / 60.
50.  VLONG = MINLONG + SIGN (MINLONGR, MINLONG) / 60.
51.  ELONG = MAXLONG + SIGN (MAXLONGR, MAXLONG) / 60.
52.  MIN = MIN / 60.
53.  IF (MLAT .LE. SLAT) GO TO 16
54.  MAKE LONGS 0 TO 360 TO THE EAST
55.  IF (VLONG .LT. 0.) VLONG = 360. + VLONG
56.  IF (ELONG .LT. 0.) ELONG = 360. + ELONG
57.  TAKE CARE OF CROSSING GREENWICH - MAKE LONGS GO TO 720 DEGS
58.  IF (VLONG .LT. ELONG) GO TO 12

```

```

59.      ELONG = ELONG + 360
60.      12 WRITE (10,117)
61.      117 FORMAT (' PLOTTER READY')
62.      READ (11,114) IANS
63.      114 FORMAT (A2)
64.      IF (IANS .EQ. 2HYE) GO TO 15
65.      GO TO 10
66.      16 TYPE 'NLAT, SLAT ERROR'
67.      GO TO 10
68.      17 TYPE 'LONGS NOT WITHIN + OR - 3 DEGREES OF CENTRAL MERIDIAN'
69.      GO TO 10
70.      15 CALL FOPEN (6, 'SPLT')
71. C INITIALIZE THE PLOTTER
72.      CALL INITIAL (6, 100, -0.5, 22)
73.      CALL PLOT (1, 1, PLOTENB)
74. C INITIALIZE PEN POSITIONS
75.      SCALE = 1.0 / SCALE
76. C LETS LABEL IT AGAIN WITH INFORMATION CONCERNING THE MAP.
77. C AREA, DATA, ETC
78.      WRITE (10,102)
79.      102 FORMAT ('GIVE THE PLOT LABEL -- UP TO 80 CHARS ')
80.      READ (11,103) ABCD
81.      103 FORMAT (40A2)
82.      CALL SYMBOL (0, -1, 21, ABCD, 0, 80)
83.      TEMP = WLONG
84.      IF (WLONG GE 100) TEMP = WLONG - 360
85.      IZONE = (TEMP + 186) / 6
86.      CNERID = MOD ((IZONE-1) * 6 + 103, 360)
87. C NOTE CNERID 0 TO 360 DEGREES TO THE EAST
88.      IF (DABS (CNERID - WLONG) GT 3) GO TO 17
89.      IF (DABS (CNERID - ELONG) GT 3) GO TO 17
90. C NOW WITHIN + OR - 3 DEGREES OF CNERID
91.      IF (WLONG GE CNERID) CALL UTR (SLAT, WLONG, X, Y)
92.      IF (ELONG LE CNERID) CALL UTR (SLAT, ELONG, X, Y)
93.      IF (WLONG LT CNERID AND ELONG GT CNERID)
94.      1 CALL UTR (SLAT, CNERID, X, Y)
95.      Y0 = Y
96. C NOW HAVE MIN Y VALUE (Y0) FOR THE MAP
97.      IF (WLONG GT CNERID) CALL UTR (NLAT, WLONG, X, Y)
98.      IF (WLONG LE CNERID) CALL UTR (SLAT, WLONG, X, Y)
99.      X0 = X
100. C NOW HAVE MIN X VALUE (X0) FOR THE MAP
101. C (X0, Y0) ARE THE SOUTH WEST CORNER OF THE MAP SUCH THAT THE GRID
102. C DOES NOT GO EITHER SOUTH OR WEST OF THIS POINT
103. C GUESS THAT WE CAN START MAKING THE GRID
104. C START THE GRID DRAWING THE LATS EAST AND WEST
105.      LONG = WLONG
106.      LAT = SLAT
107.      DLONG = (ELONG - WLONG) / 10.001
108.      CALL UTR (LAT, WLONG, X, Y)
109.      CALL NUMBER (X-75, Y, 14, MINLAT, 0, -1)
110.      CALL NUMBER (X-30, Y, 14, MINLAT, 0, -1)
111.      CALL PLOT (X, Y, PENUP)
112.      PEN = PENDOWN
113.      GO TO 25
114. C DRAWING A LAT FROM WEST TO EAST
115.      20 PEN = PENUP
116.      LAT = LAT + MIN

```

```

117.      DLONG = -DLONG
118.      LONG = WLONG
119.      IF (LAT GT NLAT) GO TO 40
120. 25 IF (LONG GT ELONG) GO TO 30
121.      CALL UTM (LAT, LONG, X, Y)
122.      CALL PLOT (X, Y, PEN)
123.      PEN = PENDOWN
124.      LONG = LONG + DLONG
125.      GO TO 25
126. C DRAWING A LAT FROM THE EAST TO WEST
127. 30 PEN = PENUP
128.      LAT = LAT + MIN
129.      IF (LAT GT NLAT) GO TO 40
130.      LONG = ELONG
131.      DLONG = -DLONG
132.      CALL UTM (LAT, LONG, X, Y)
133.      CALL PLOT (X, Y, PEN)
134.      PEN = PENDOWN
135. 35 LONG = LONG + DLONG
136.      IF (LONG LT WLONG) GO TO 20
137.      CALL UTM (LAT, LONG, X, Y)
138.      CALL PLOT (X, Y, PEN)
139.      GO TO 35
140. 40 CONTINUE
141. C DONE WITH EAST AND WEST PORTION OF THE GRID
142. C NOW LETS DO THE NORTH AND SOUTH LINES
143.      LONG = WLONG
144.      LAT = SLAT
145.      DLAT = (NLAT - SLAT) / 10 001
146.      CALL UTM (LAT, LONG, X, Y)
147.      CALL NUMBER (X- 40, Y- 25, 14, MINLONG, 0, -1)
148.      CALL NUMBER (X+ 10, Y- 25, 14, MINLONG, 0, -1)
149.      CALL PLOT (X, Y, PENUP)
150.      PEN = PENDOWN
151.      GO TO 50
152. C DRAWING A LONG FROM SOUTH TO NORTH
153. 45 PEN = PENUP
154.      LONG = LONG + MIN
155.      DLAT = -DLAT
156.      LAT = SLAT
157.      IF (LONG GT ELONG) GO TO 70
158. 50 IF (LAT GT NLAT) GO TO 55
159.      CALL UTM (LAT, LONG, X, Y)
160.      CALL PLOT (X, Y, PEN)
161.      PEN = PENDOWN
162.      LAT = LAT + DLAT
163.      GO TO 50
164. C DRAWING A LONG FROM NORTH TO SOUTH
165. 55 PEN = PENUP
166.      LONG = LONG + MIN
167.      IF (LONG GT ELONG) GO TO 70
168.      LAT = NLAT
169.      DLAT = -DLAT
170.      CALL UTM (LAT, LONG, X, Y)
171.      CALL PLOT (X, Y, PEN)
172.      PEN = PENDOWN
173. 60 LAT = LAT + DLAT
174.      IF (LAT LT SLAT) GO TO 45
175.      CALL UTM (LAT, LONG, X, Y)
176.      CALL PLOT (X, Y, PEN)
177.      GO TO 60
178. C DONE WITH THE GRID
179. 70 CONTINUE
180.      RETURN
181.      END

```

```

      UTM
1.  COMPILER DOUBLE PRECISION
2.  SUBROUTINE UTM (LAT, LONG, X, Y)
3.  THIS SUBROUTINE CONVERTS LAT (PHI), LONG (DLAMBDA) TO X, Y
4.  IN UTM COORDINATES IN INCHES FROM THE LOWER LEFT CORNER OF
5.  THE PLOT AT SCALE.
6.  REAL LA, LB, LESQ, LA, NU, LALA, MTOI, LAT, LONG, KB
7.  UTM HAS PROJECTION PARAMETERS THAT ARE PASSED FROM UTMGRID
8.  COMMON /UTM/ SCALE, X0, Y0, DTOR, MTOI, A, B, C, LA, LALA,
9.  LESQ, OMLESQ, CNERID, K0
9.  I
10. PHI = LAT * DTOR
11. SINPHI = SIN (PHI)
12. SPSP = SINPHI * SINPHI
13. RHO = LA * OMLESQ / (1.0 - LESQ * SPSP) ** 1.5
14. NU = LA / SQRT (1.0 - LESQ * SPSP)
15. LM = LA * OMLESQ * (A * PHI - B * SIN (2 * PHI) / 2 +
16. C * SIN (4 * PHI) / 4.)
17. DLAMBDA = (LONG - CNERID) * DTOR
18. DLDL = DLAMBDA * DLAMBDA
19. DLDL2L = DLDL * DLAMBDA
20. SINPHI = SIN (PHI)
21. COSPHI = COS (PHI)
22. TANPHI = TAN (PHI)
23. Y = K0 * (LM + DLDL * NU / 2.0 * SINPHI * COSPHI)
24. X = K0 * (DLAMBDA * NU * COSPHI + DLDL2L * NU / 6.0 * COSPHI ** 3 +
25. (NU / RHO - TANPHI * TANPHI))
26. SCALE X AND Y TO INCHES ON THE PAPER
27. X = X * SCALE + MTOI - X0
28. Y = Y * SCALE + MTOI - Y0
29. RETURN
30. END

```

RGNAY

1.750020	0440	71 15 63	-157 01 00	73.760012	1200	70 50 20	-151 29 00
2.750020	0500	71 10 17	-157 24 20	74.760012	1220	70 48 50	-151 19 00
3.750020	0512	71 08 78	-157 30 60	75.760012	1240	70 47 50	-151 10 00
4.750020	0540	71 04 59	-157 47 50	76.760012	1300	70 47 90	-151 05 00
5.750020	0600	71 02 54	-157 55 60	77.760012	1320	70 46 50	-150 55 00
6.750020	2000	71 10 73	-157 07 50	78.760012	1340	70 44 70	-150 48 00
7.750020	2015	71 12 08	-157 02 00	79.760012	1400	70 44 00	-150 40 00
8.750020	2025	71 14 02	-156 59 60	80.760012	1420	70 41 42	-150 32 90
9.750020	2035	71 15 07	-156 56 00	81.760012	1440	70 41 32	-150 21 30
10.750020	2040	71 15 70	-156 55 30	82.760012	1500	70 40 00	-150 10 40
11.760005	2240	70 50 70	-159 50 30	83.760012	1520	70 40 10	-150 02 00
12.760005	2300	70 48 50	-159 56 45	84.760012	1540	70 38 90	-149 52 90
13.760005	2315	70 47 20	-160 01 20	85.760012	1600	70 37 60	-149 43 00
14.760005	2330	70 45 00	-160 05 10	86.760015	0540	70 32 12	-148 39 50
15.760005	2340	70 45 23	-160 06 70	87.760015	0600	70 32 95	-148 46 00
16.760006	0001	70 45 54	-160 05 30	88.760015	0620	70 34 66	-148 56 20
17.760006	0104	70 45 56	-160 01 39	89.760015	0640	70 35 70	-149 05 40
18.760006	0115	70 44 00	-160 06 10	90.760015	0702	70 95	-149 15 30
19.760006	0130	70 44 50	-160 08 30	91.760015	0722	70 20	-149 25 00
20.760006	0145	70 43 95	-160 08 30	92.760015	0802	70 35 00	-149 30 00
21.760006	0200	70 43 70	-160 00 30	93.760015	0820	70 36 00	-149 37 50
22.760006	0215	70 44 00	-160 10 90	94.760015	0840	70 37 10	-149 30 75
23.760006	0230	70 46 70	-160 15 70	95.760015	0900	70 37 47	-149 56 00
24.760006	0245	70 47 90	-160 19 00	96.760015	0920	70 37 25	-150 07 20
25.760006	0300	70 50 00	-160 24 00	97.760015	0950	70 36 00	-150 23 50
26.760006	0316	70 52 20	-160 30 00	98.760015	1000	70 36 75	-150 30 00
27.760006	0340	70 45 00	-160 30 00	99.760015	1025	70 37 45	-150 39 00
28.760006	0600	70 44 00	-160 25 00	100.760015	1140	70 37 53	-150 30 60
29.760006	0630	70 42 50	-160 17 50	101.760015	1200	70 37 45	-150 27 00
30.760007	2100	70 44 60	-160 12 40	102.760015	1220	70 37 09	-150 16 91
31.760007	2156	70 46 50	-160 02 20	103.760015	1242	70 37 18	-150 03 65
32.760007	2210	70 48 60	-159 56 70	104.760015	1300	70 37 41	-149 59 10
33.760007	2225	70 50 70	-159 50 70	105.760015	1320	70 37 50	-149 57 20
34.760007	2235	70 52 25	-159 46 70	106.760015	1340	70 37 50	-149 57 20
35.760007	2250	70 54 60	-159 42 90	107.760015	1400	70 37 50	-149 57 20
36.760007	2300	70 55 20	-159 39 30	108.760015	1420	70 37 30	-149 54 00
37.760007	2310	70 56 50	-159 35 30	109.760015	1435	70 36 67	-149 46 05
38.760007	2320	70 57 60	-159 30 70	110.760015	1500	70 36 25	-149 36 25
39.760007	2330	70 58 40	-159 25 40	111.760015	1520	70 36 50	-149 30 75
40.760011	1045	71 06 45	-154 30 00	112.760015	1540	70 35 50	-149 20 00
41.760011	1900	71 05 63	-154 24 30	113.760015	1600	70 35 50	-149 09 00
42.760011	1915	71 04 44	-154 19 10	114.760017	0500	71 00 10	-152 00 20
43.760011	1930	71 03 15	-154 13 40	115.760017	0520	70 59 10	-151 54 40
44.760011	1945	71 02 45	-154 00 53	116.760017	0540	70 57 90	-151 47 10
45.760011	2000	71 01 40	-154 03 60	117.760017	0600	70 56 60	-151 38 20
46.760011	2015	71 00 45	-153 58 60	118.760017	0620	70 56 10	-151 27 70
47.760011	2030	71 00 00	-153 51 00	119.760017	0640	70 55 30	-151 17 70
48.760011	2045	71 00 55	-153 42 45	120.760017	0700	70 53 90	-151 00 30
49.760011	2100	70 59 50	-153 39 40	121.760017	0720	70 53 90	-151 00 30
50.760011	2115	71 00 30	-153 35 20	122.760017	0740	70 52 90	-151 00 40
51.760011	2315	71 01 00	-153 27 00	123.760017	0800	70 51 00	-150 50 70
52.760011	2330	71 01 10	-153 22 30	124.760017	0820	70 47 20	-150 50 06
53.760011	2345	71 01 10	-153 18 30	125.760017	0850	70 45 00	-150 42 00
54.760012	0000	71 01 56	-153 13 00	126.760017	0900	70 44 00	-150 39 00
55.760012	0015	71 01 70	-153 02 40	127.760017	0920	70 42 50	-150 24 50
56.760012	0030	71 00 60	-152 58 90	128.760017	0938	70 40 59	-150 12 70
57.760012	0045	71 00 00	-152 55 20	129.760018	0300	70 40 35	-150 00 20
58.760012	0100	70 59 50	-152 47 30	130.760018	0320	70 41 60	-150 10 70
59.760012	0115	70 59 20	-152 40 60	131.760018	0340	70 42 60	-150 20 20
60.760012	0130	70 58 30	-152 35 40	132.760018	0400	70 44 20	-150 29 00
61.760012	0145	70 58 70	-152 39 00	133.760018	0420	70 45 00	-150 39 20
62.760012	0200	70 59 30	-152 45 40	134.760018	0440	70 47 50	-150 40 00
63.760012	0215	70 59 00	-152 50 40	135.760018	0500	70 47 40	-150 50 00
64.760012	0230	71 00 50	-152 54 50	136.760018	0520	70 49 00	-150 52 00
65.760012	0245	71 01 30	-153 00 90	137.760018	0540	70 49 20	-151 05 00
66.760012	0300	71 01 50	-153 02 20	138.760018	0600	70 50 60	-151 15 00
67.760012	0315	71 02 10	-153 06 90	139.760018	0620	70 52 60	-151 24 50
68.760012	0330	71 02 10	-153 12 70	140.760018	0640	70 54 00	-151 33 00
69.760012	0345	71 02 70	-153 18 00	141.760018	0700	70 54 00	-151 44 00
70.760012	0400	71 02 90	-153 24 00	142.760018	0720	70 55 60	-151 55 00
71.760012	0740	71 00 90	-153 02 40	143.760018	0740	70 56 70	-152 00 00
72.760012	0800	71 00 40	-152 53 50	144.760018	1000	71 02 00	-152 59 40
73.760012	0820	70 59 35	-152 44 60	145.760018	1020	71 04 12	-153 05 10
74.760012	0900	70 58 65	-152 39 55	146.760018	1040	71 05 60	-153 13 20
75.760012	0922	70 58 00	-152 32 30	147.760018	1100	71 06 25	-153 26 10
76.760012	0940	70 56 95	-152 25 00	148.760018	1120	71 07 00	-153 35 20
77.760012	1000	70 55 65	-152 17 20	149.760018	1140	71 07 45	-153 36 50
78.760012	1020	70 55 00	-152 09 30	150.760018	1200	71 07 60	-153 42 20
79.760012	1040	70 54 20	-152 00 70	151.760018	1220	71 08 40	-153 52 00
80.760012	1100	70 53 45	-151 53 00	152.760018	1245	71 09 17	-154 05 00
81.760012	1120	70 53 20	-151 43 50	153.760018	1300	71 10 00	-154 14 40
82.760012	1140	70 51 10	-151 35 00	154.760018	1320	71 11 40	-154 26 55
83.760012	1160	70 51 10	-151 35 00	155.760018	1342	71 12 20	-154 30 40

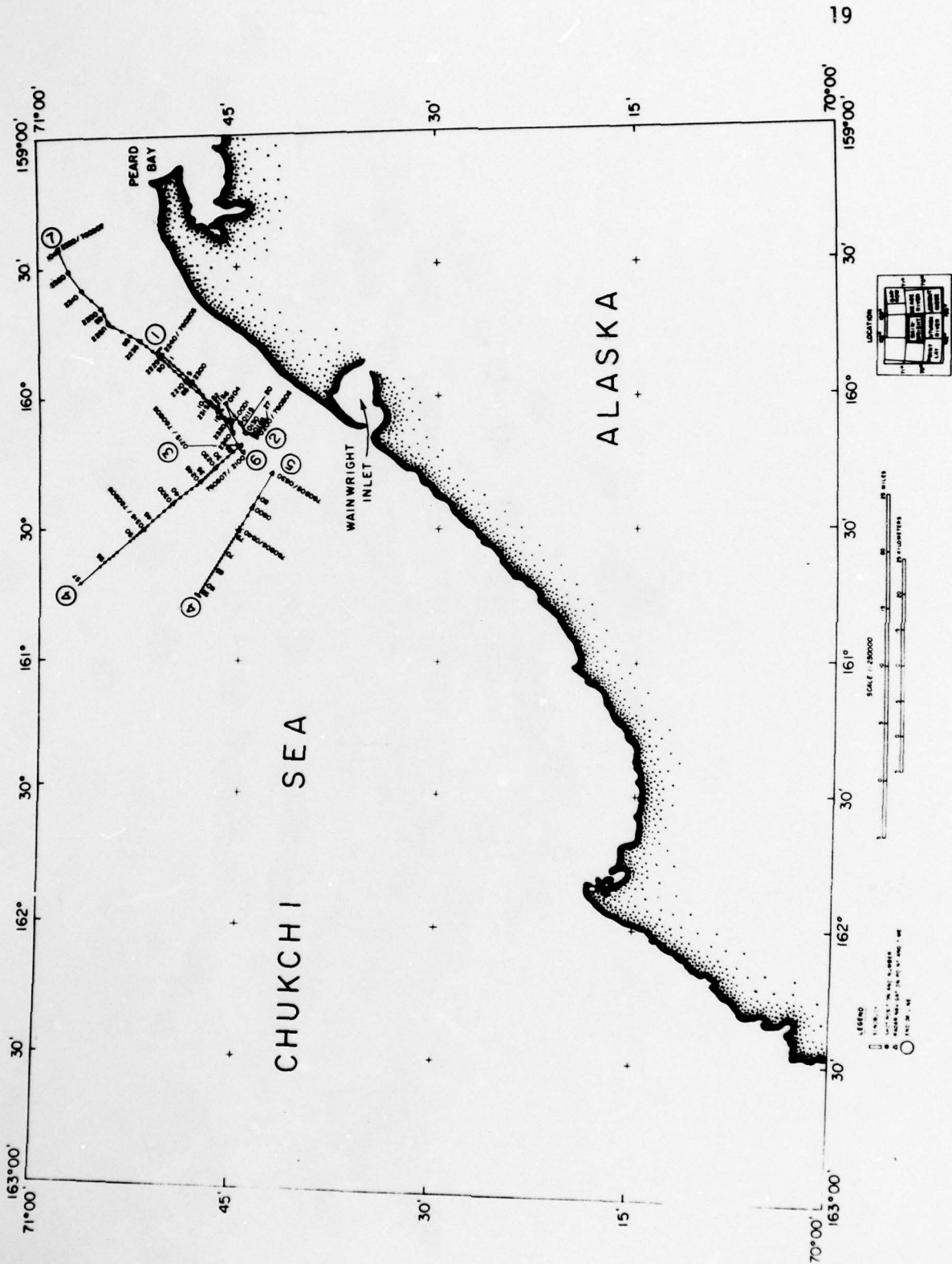


Figure 3. Tracklines and shot locations of Lines 1-2, 3-4, 4-5 and 6-7.

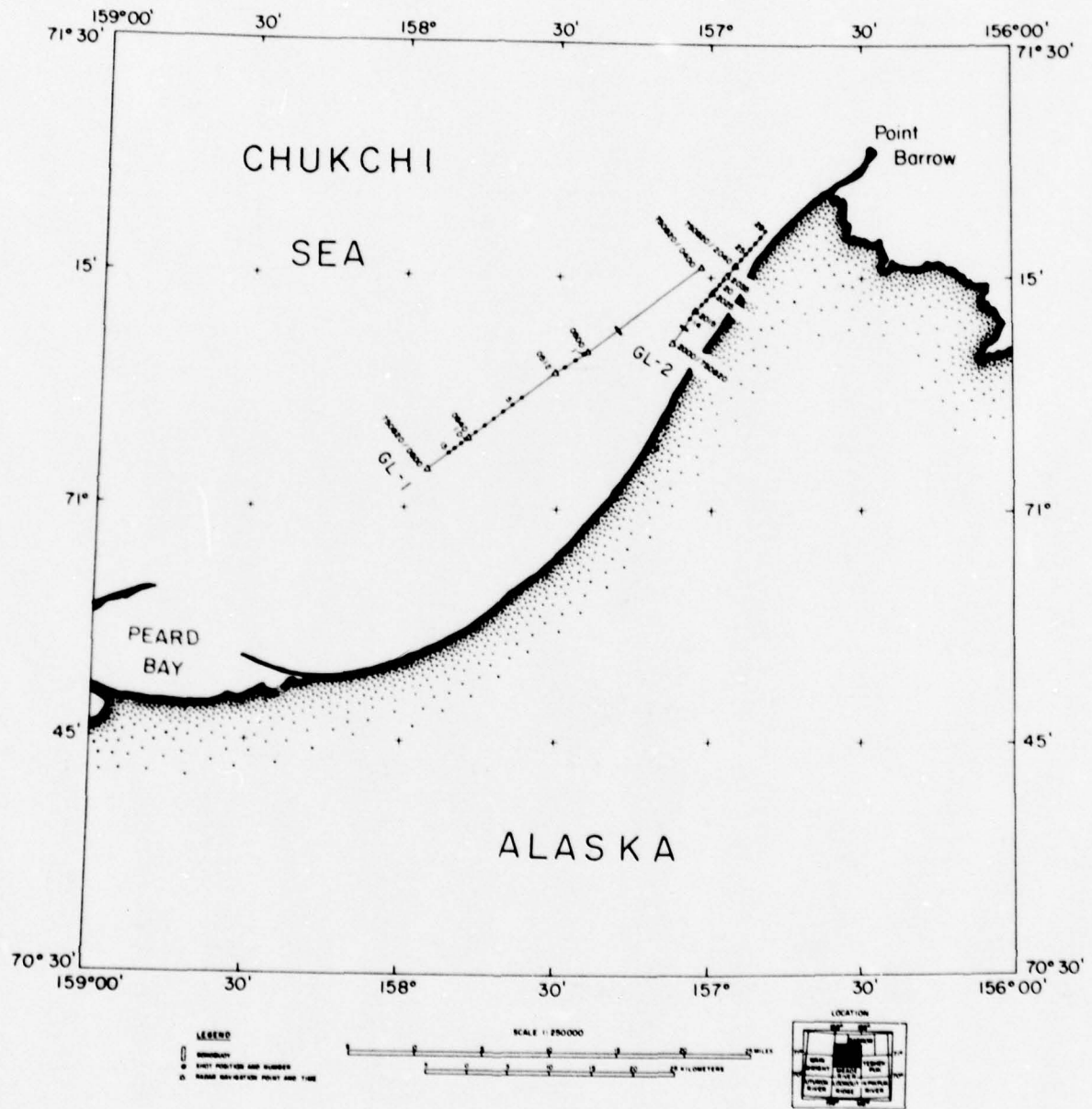


Figure 4. Tracklines and shot locations of Lines GL-1 and GL-2.

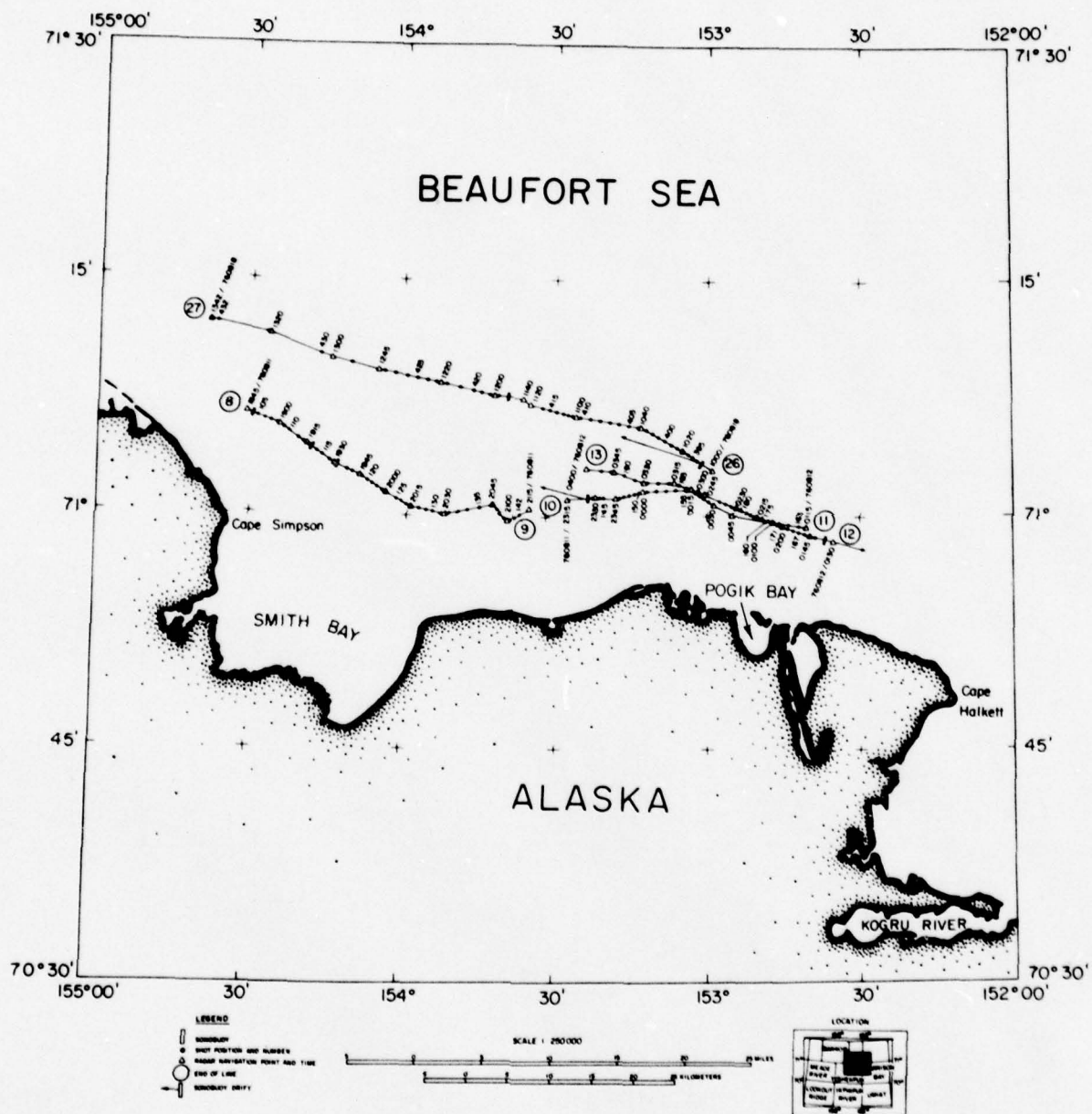


Figure 5. Tracklines and shot locations of Lines 8-9, 10-11, 12-13 and 26-27.

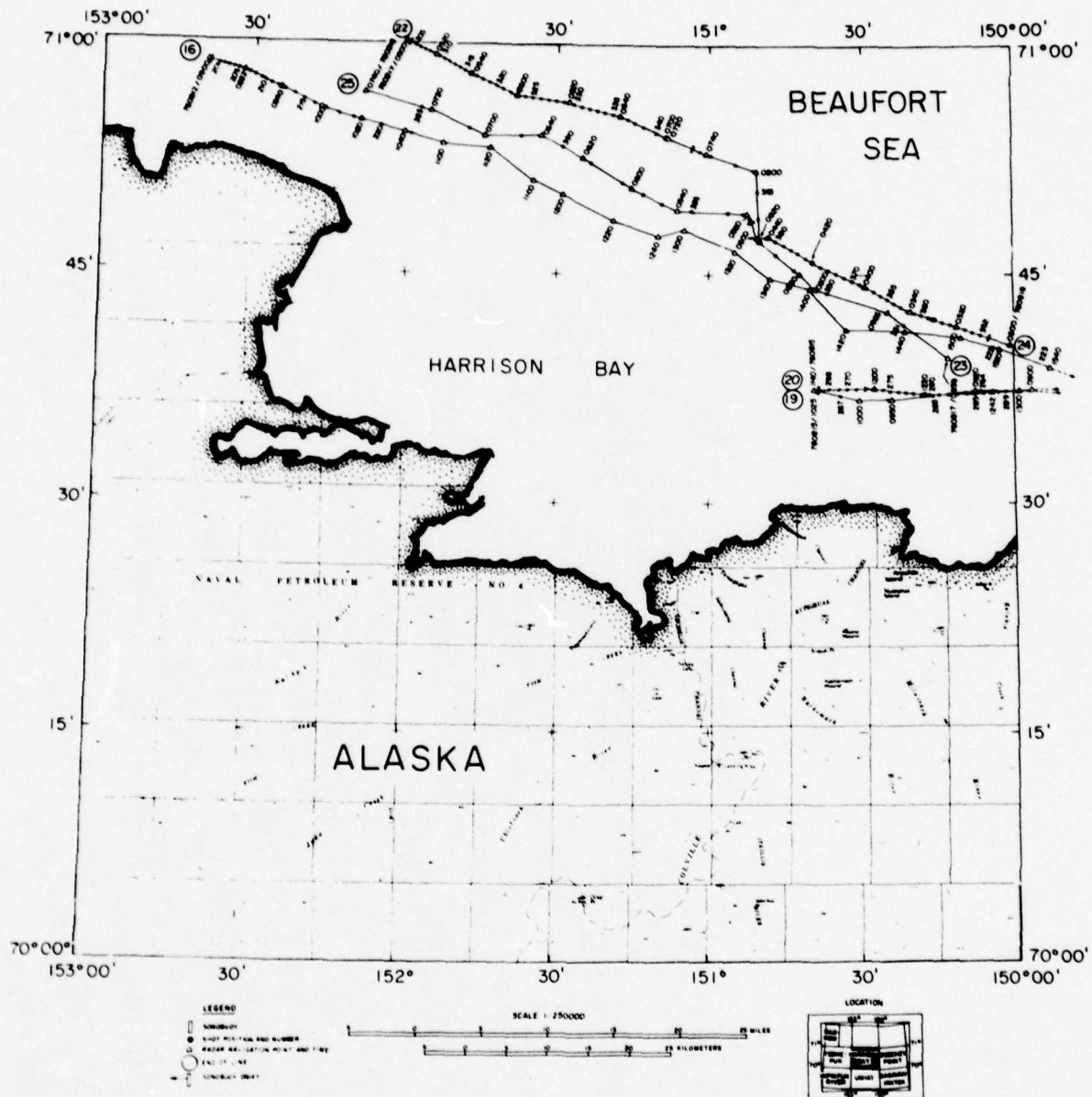


Figure 6. Tracklines and shot locations of Lines 16-17, 18-19 20-21, 22-23 and 24-25.

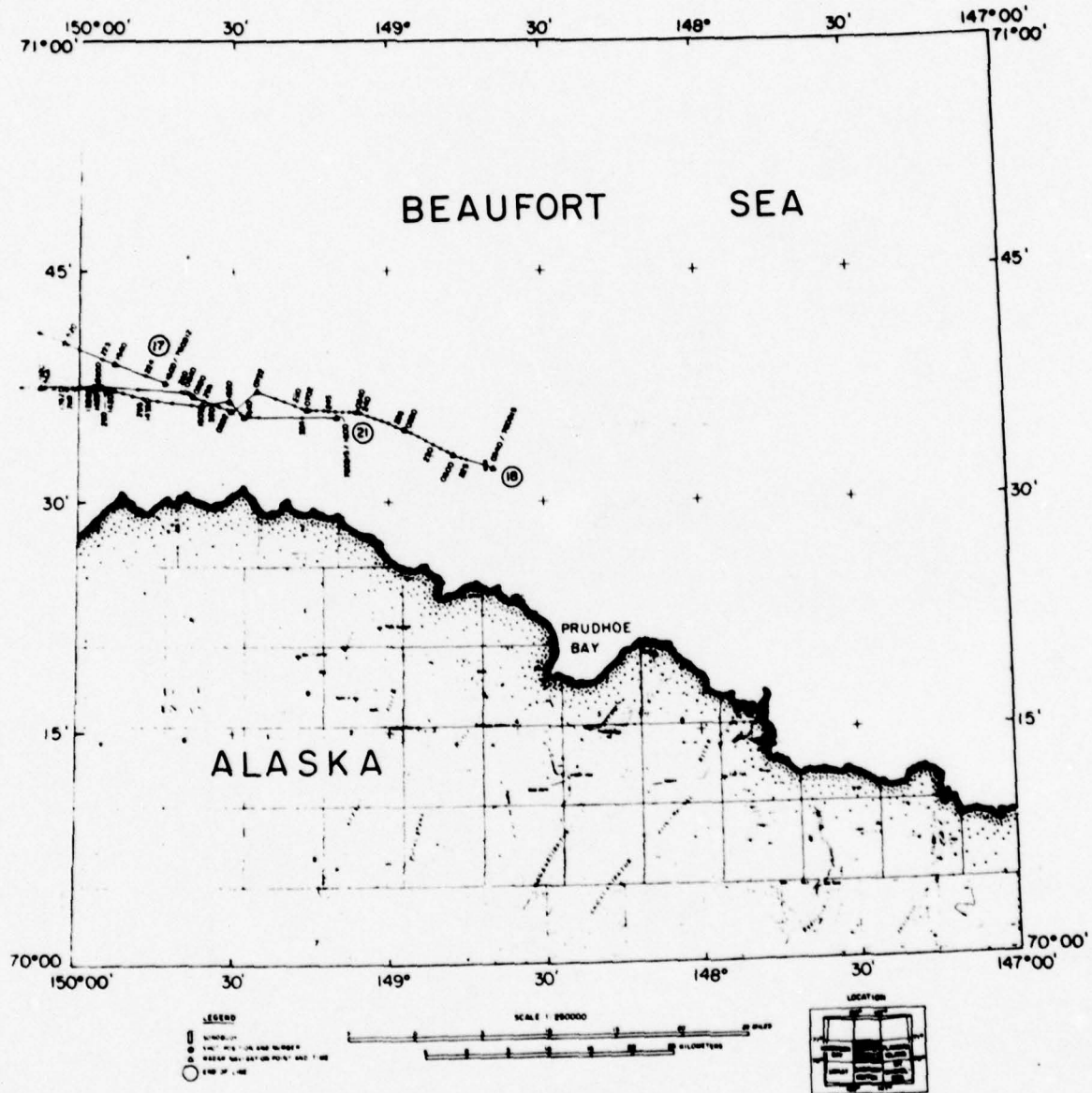


Figure 7. Tracklines and shot locations of Lines 16-17, 18-19 and 20-21.

II

COMPUTER PROGRAM TO FORM
ARRIVAL TIME CORRECTIONS (TIMCORM)
AND INPUT AND OUTPUT FILES
FOR ALL LINES

```

PROGRAM TIMCORN
DIMENSION G(22),GC(22),A(11),R(4)
READ(5,5)AID1,AID2
5 FORMAT(2A8)
6 READ(5,10)DBPM,DBBM,DBEM,TOTS,DRM,V1,SVMS,CLM,SLM,SDM
10 FORMAT(3F5.0,7F5.2)
WRITE(7,14)AID1,AID2
14 FORMAT(2A8)
WRITE(7,16)TOTS,V1
16 FORMAT(15X,F5.2,5X,F5.3)
15 FORMAT(1X,2A9,/)
WRITE(61,15)AID1,AID2
WRITE(61,17)
17 FORMAT(1X DBRM DBBM DBEM TOTS DRM V1 SVMS #,
1XCLM SLM SDM#)
WRITE(61,20)DBRM,DBBM,DBEM,TOTS,DRM,V1,SVMS,CLM,SLM,
1SDM
20 FORMAT(1X,1F6.0,2F6.2,F6.3,4F6.2)
WRITE(61,25)
25 FORMAT(1X SHOT TIME DISTS TS TC TCR G1 G2#,
1X G3 G4 G5 G6#)
N=0
ILL=0
30 READ(5,35)ACE,(A(I),I=1,11)
35 FORMAT(A5,11F5.0)
IF(EOF(5)) ILL=1
IF(N.EQ.11.AND.ILL.EQ.1) GO TO 40
IF(ILL.EQ.1) CALL EXIT
IF(ACE.EQ.5H99999) GO TO 6
IF(ACE.EQ.5H ) GO TO 135
ITYPE=0
40 IF(ITYPE.EQ.0.AND.N.EQ.0) GO TO 95
D=D+TC
DISTS=D+TS
DO 43 I=1,N
43 R(I)=R(I)+TC
WRITE(7,45)SHOT,ITYM,OBSM,TS,0,(R(I),I=1,N)
45 FORMAT(A5,15,F5.0,15X,6F5.2)
DO 46 I=1,N
G(I)=G(I)+TCR+TC
46 GC(I)=G(I)+TS
IF(N.GT.11)GO TO 55
WRITE(7,50)(G(I),I=1,N)
50 FORMAT(5X,11F5.2)
GO TO 60
55 WRITE(7,50)(G(I),I=1,11)
WRITE(7,50)(G(I),I=12,N)
50 KN=N
IF(N.GT.6)KN=5
WRITE(61,65)SHOT,ITYM, DISTS,TS,TC,TCR,(GC(I),I=1,KN)
IF (KN.EQ.N) GO TO 90
65 FORMAT(1X,A5,15,10F6.2)
KN=7
70 IF(N.GT.KN+6) GO TO 75
KN=N
GO TO 80
75 KN=KN+5
80 WRITE(61,85)(GC(I),I=KN,KN)
85 FORMAT(1X,13X,6F6.2)
IF(KN.EQ.N)GO TO 90
KN=KN+5
GO TO 70

```

```

90 IF (ILL.EQ.1) CALL EXIT
   IF (N.EQ.11) GO TO 96
   N=0
   GO TO 30
94 N=0
95 SHOT=ACE $ ITIM=A(1) $ DBSM=A(2) $ V2=A(3) $ VJ=A(4)
   BT=A(5) $ TS=A(6) $ TD=A(7)
   NR=0
   DO 100 I=1,4
   R(I)=A(I+7)
   IF (R(I).EQ.0.) GO TO 105
100 NR=I
105 S1=SQRT(1.-V1*V1/VJ/VJ)/V1
   S2=SQRT(1.-V1*V1/V2/V2)/V1
   SX=BT*SVMS
   SY=-40.54+1.513*BT
   IF (SY.GT.DBSM) SY=DBSM
   IF (SX.GT.CL) GO TO 110
   TC=SQRT((SX-CL)**2+(SY-SM)**2)*.001/V1
   GO TO 120
110 TLM=CL+SLM
   IF (SX.GT.TLM) GO TO 115
   WY=SM-SY
   TC=ABS(WY)*.001/V1
   GO TO 120
115 TC=SQRT((SX-TLM)**2+(SY-SM)**2)*.001/V1
120 CONTINUE
   ANG=ASINF(V1/VJ)
   OFFSET=DBSM*TANF(ANG)*.001/V1
   DMS=DRM+(DBEM-DRM)*(D+TS+TC-CFFSET)/TOTS
   OFFSET=DRM*TANF(ANG)*.001/V1
   DM=DRM+(DBEM-DRM)*OFFSET/TOTS
   C=(DMR-DRM+DM-DBSM)*.001
   IF (V2.NE.VJ) GO TO 125
   DT1=(SY+DRM)*S2*.001
   DT2=C*S2
   GO TO 130
125 S3=SQRT(1.-V2*V2/VJ/VJ)/V2
   DT1=(SY+DRM)*.001*S1
   DT2=C*(S1-S3)
130 CONTINUE
   TCR=DT1+DT2
   I*PE=1
   GO TO 30
135 NS=1
   IF (N.EQ.11) NS=12
   I=1
140 G(NS)=A(I)
   IF (G(NS).EQ.0) GO TO 40
   N=NS
   IF (N.EQ.11) GO TO 30
   IF (N.EQ.22) GO TO 40
   NS=NS+1
   I=I+1
   GO TO 140
END

```


OUTPUT FORMAT FOR PROGRAM TIMECORR

SHOT	SHOT TIME	DBBM	A1D2	DBEM	TDT5	DM	TCOR	V1	SWMS	G1	G2	CLM	G3	SLM	G4	SOM	G5	G6

A1D1, A1D2, DBBM, DBEM, TDT5, DM, V1, SWMS, CLM, SLM, SOM, SHOT, TIME : All the same as in input file.
 TS : Seismogram time correction : time in seconds between shot break and zeroth second ttc.
 TC : Shot instant correction due to separation of shot and streamer.
 TCOR : Surface and bottom corrections at shot and receiver.
 DIST5 : Corrected direct water wave travel time (includes TS and TC).
 G1, G2, ..., G6 : Corrected ground wave travel times (include TS, TC and TCOR).

LINE 1 CHUKCHI CORRECTED

DRPM	DRBM	DBEM	DRM	VI	SVMS	CLM	SLM	SOM
43	43	43	15.00	1.440	4.26	54.30	4.60	2.00
SHOT	TIME	DISTS	VS	TCOR	G1	G2	G3	G4
1	501	1.79	.73	.06	1.01	1.16		G5
2	505	2.93	.42	.06	1.52	1.61	2.09	2.45
3	509	3.96	.07	.06	1.80	1.95	2.00	2.30
4	523	7.82	.51	.06	2.74	3.21	3.69	4.14
					5.39	5.59		4.51
5	526	8.58	.11	.06	3.14	4.24	4.46	5.14
6	529	9.41	.02	.06	3.34	4.10	4.55	4.99
					6.02	6.40	6.50	6.76
7	532	10.19	.18	.06	5.51	6.03	6.55	6.89
					8.56			7.33
8	535	11.01	.03	.05	5.71	5.89	6.32	6.67
					7.94	9.09		7.46
9	538	11.82	.80	.06	6.28	6.63	6.96	7.28
					8.58	9.18	11.00	8.00
10	541	12.64	.27	.06	6.90	7.15	7.50	8.52
					10.35	11.67		9.00
11	544	13.44	.13	.06	6.58	7.31	7.56	8.26
					10.41	11.04	12.57	9.16
12	547	14.23	.22	.06	9.78	10.28	11.00	11.50
					10.89	11.20	12.76	12.15
13	550	15.02	.27	.05	8.46	9.24	9.59	9.99
					10.89	11.20	12.76	10.14
								13.64

LINE 1 CHUKCHI

42.7	42.7	42.7	15.0014.3	1.44	4.2654.3	4.6	2.
1	050142.7	3.25	3.2534.8	.73	1.00		
		.20	.35				
2	050442.7	3.25	3.2535.	.42	2.45		
		1.02	1.11	1.59	1.95		
3	050942.7	3.25	5.0335.	.07	3.03		
		1.65	1.80	1.85	2.15	2.62	3.42
4	052342.7	3.25	5.0334.2	.51	7.25		
		2.15	2.62	3.10	3.55	3.92	4.25
5	052642.7	3.25	5.0333.8	.11	8.41		
		2.95	4.05	4.27	4.95	5.72	5.87
6	052942.7	3.25	5.0335.	.82	1.53		
		2.44	3.20	3.65	4.09	4.22	4.60
7	053242.7	3.25	5.0334.0	.18	9.95		
		5.25	5.77	6.29	6.63	7.07	7.62
8	053542.7	3.25	5.0310.8	.0310.93			
		5.62	5.80	6.23	6.58	6.82	7.37
9	053842.7	3.25	5.0334.8	.010.96			
		5.40	5.75	6.08	6.40	7.12	7.32
10	054142.7	3.25	5.0333.8	.2712.31			
		6.55	6.80	7.15	8.17	8.65	9.3810.011.32
11	054442.7	3.25	5.0335.5	.1313.5513.48			
		6.17	7.10	7.35	8.05	8.95	9.4510.2810.812.36
12	054742.7	3.25	5.0334.4	.2213.5514.06			
		9.48	9.9810.7011.2011.8512.95				
13	055042.7	3.25	5.0332.2	.2714.7014.84			
		8.12	8.90	9.25	9.65	9.8010.1510.5510.8612.4213.30	

25 0140 26. 3.13 5.4381.5 .9316.31
 4.08 5.17 6.3810.86
 26 0144 26. 3.13 5.4311.5 .9916.79
 4.97 6.13 8.59 9.5810.1611.10
 27 0149 31. 4.13 5.4311.5 .5717.72
 5.53 6.7418.74

MURTON ISL 1-2
 37. 40. 40.18-3018.3 1.44 4.7961. 4.57 1.
 1 2245 37. 3.13 3.1348. .70 .56
 2 2248 37. 3.13 3.1337.5 .42 1.50
 .61
 3 2251 37. 3.13 3.1348.6 .86 1.68
 .42
 4 2254 37. 3.13 3.7447.6 .97 2.19
 .58 .98
 5 2257 37. 3.13 3.7445.6 .89 2.85
 .87
 6 2300 37. 3.13 3.7448.0 .65 3.73
 1.87 1.83 2.15
 7 2303 37. 3.13 3.7446.1 .51 4.44
 1.72 2.12
 8 2306 37. 3.13 3.7448.0 .57 4.54
 1.88 2.42 2.73
 9 2310 37. 3.13 3.7445.2 .48 5.79
 2.24 2.91 3.13
 11 2316 37. 3.13 5.4346.6 .23 7.20
 2.95 3.50 3.95 4.60
 12 2319 37. 3.13 5.4345.8 .88 7.15
 2.88 3.12 3.47 3.94
 13 2322 37. 3.13 5.4346.8 .92 7.71
 2.80 3.27 3.74 4.17 4.59 5.08
 14 2325 37. 3.13 5.4347. .87 8.48
 2.80 3.60 4.04 4.45 5.10
 15 2328 37. 3.13 5.4348.9 .23 9.65
 3.61 3.97 4.51 4.95 5.41 5.80 6.18
 16 2331 37. 3.13 5.4345.5 .4711.09
 3.56 3.98 4.60 5.94 6.27 6.45
 99999
 37. 40. 40.18-3018.3 1.44 2.7361. 4.57 1.
 17 0110 28. 3.13 5.4347.1 .6813.31
 4.23 4.56 5.61 6.10 7.01 7.70 8.65
 20 0120 28. 3.13 5.4372.5 .2514.61
 4.99 5.19 5.81 6.29 8.26
 21 0124 28. 3.13 5.4373. .5116.97
 4.82 5.64 6.80
 22 0128 28. 3.13 5.4373.8 .3015.63
 5.15 6.70 7.69 9.15
 23 0132 27. 3.13 5.4388.8 .8416.76
 5.54 6.59 7.10 8.59 8.99 9.6010.25
 24 0136 25. 3.13 5.4382.9 .7511.83
 4.89 5.92 6.58 7.80 7.91 8.58 8.98 9.71

MURTON ISL 1-2 CORR'CTED
 DRAM DBRM DBEM TOTIS DRM V1 SVMS CLM SLM SOM
 37 40 40 18.30 18.30 1.440 4.79 61.00 4.57 1.00
 SHOT TIME DTSTS IS IC TCO# G1 G2 G3 G4 G5 G6
 1 2245 1.35 .70 .09 .03 .83
 2 2248 2.01 .43 .08 .02 1.14
 3 2251 2.66 .86 .12 .04 1.43
 4 2254 3.27 .97 .11 .03 1.70 2.10
 5 2257 3.65 .69 .11 .03 1.90
 6 2300 4.50 .65 .12 .04 2.17 2.63 2.95
 7 2303 5.06 .51 .11 .03 2.37 2.77
 8 2306 5.61 .57 .12 .04 2.60 3.14 3.45
 9 2310 6.38 .48 .11 .03 2.86 3.53 3.75
 11 2316 7.54 .23 .11 .04 3.33 3.98 4.33 4.98
 12 2319 8.14 .88 .11 .04 3.50 4.14 4.49 4.96
 13 2322 8.74 .92 .11 .04 3.67 4.34 4.81 5.24 5.66 6.15
 14 2325 9.38 .87 .11 .04 3.82 4.62 5.06 5.47 6.12
 15 2328 10.00 .23 .12 .04 4.00 4.36 4.90 5.34 5.80 6.19
 16 2331 10.67 .47 .11 .04 4.17 4.59 5.21 6.55 6.88 7.06
 MURTON ISL 1-2
 DRAM DBRM DBEM TOTIS DRM V1 SVMS CLM SLM SOM
 37 40 40 18.30 18.30 1.440 2.73 61.00 4.57 1.00
 SHOT TIME DTSTS IS IC TCO# G1 G2 G3 G4 G5 G6
 17 110 14.07 .68 .08 .04 5.03 5.36 6.41 6.90 7.81 8.50
 9.65
 20 120 15.15 .25 .09 .04 5.37 5.57 6.19 6.67 8.64
 21 124 15.57 .51 .08 .04 5.46 6.28 9.44
 22 128 16.03 .30 .10 .04 5.58 7.13 8.12 9.58
 23 132 16.57 .04 .12 .04 5.73 6.78 7.29 8.78 9.19 9.79
 10.44
 24 136 16.89 .75 .11 .04 5.79 6.82 7.40 7.90 8.81 9.28
 9.84 10.63
 25 140 17.35 .93 .11 .04 5.96 6.25 9.46 11.14
 26 144 17.95 .99 .17 .04 6.16 7.32 9.68 10.77 11.35 12.29
 27 149 18.46 .57 .17 .04 6.31 7.52 11.52

BEAU76 BA-9A
 13. 13. 12.28.5 13. 1.44 4.1 61. 4.57 1.
 105 1950 13. 3.07 3.0745.3 -.33 1.21
 .86
 107 1956 13. 3.07 3.0745. -.28 2.93
 2.07 2.34
 108 1959 13. 3.07 3.0741.9 -.17 3.12
 1.72 2.36
 109 1902 13. 3.07 3.0739.1 -.31 4.27
 2.73 3.15 3.52
 111 1910 13. 3.07 5.6245.3 -.04 5.10
 2.45 3.03 3.70
 112 1913 13. 3.07 5.6245. .36 5.37
 2.54 2.6A
 113 1916 13. 3.07 5.6245.9 .3 5.58
 2.64 3.08 3.72
 114 1920 13. 3.07 5.6248. -.17 6.84
 3.49 3.82 4.6A
 115 1923 13. 3.07 5.6248.2 -.41 7.46
 3.49

BEAU76 BA-9A COMPLETED
 DRHM DBRM DBRM TDIS DRM V1 SWMS CLM SLM SDM
 13 13 12 24.50 13.00 1.440 4.10 61.00 4.57 1.00
 SHOT TIME DISTS TS TC ICOR G1 G2 G3 G4 G5 G6
 105 1950 1.62 .33 .08 .02 1.29
 107 1956 2.75 -0.2A .09 .02 1.09 2.16
 108 1959 3.36 .17 .07 .02 2.1A 2.62
 109 1902 4.03 -0.31 .07 .02 2.50 2.92 3.29
 111 1910 5.44 -0.04 .08 .02 2.91 3.09 3.76
 112 1913 5.81 .36 .08 .02 3.00 3.14
 113 1916 6.37 .30 .09 .02 3.24 3.44 4.12
 114 1920 6.76 -0.17 .09 .02 3.43 3.76 4.62
 115 1923 7.54 -0.41 .09 .02 3.59

BEAUF6 88-9R CORRECTED

OURM	ORBM	DREM	IDTS	GRM	VI	SVMS	CLM	SUM	SDM
113	13	12	24.50	13.00	1.440	4.10	61.00	4.57	1.00
SHOT TIME DIST S FS TC TCRP G1 G2 G3 G4 G5 G6									
119	1946	2.30	-0.50	.08	.02	1.64			
120	1949	2.07	.38	.08	.02	1.96			
122	1955	3.04	.53	.08	.02	2.36	2.05	3.16	
123	1958	4.24	0	.07	.02	2.49			
124	2000	4.59	.47	.17	.02	2.62	3.53		
125	2006	5.67	-0.34	.09	.02	2.09	3.41	3.09	
126	2009	6.28	.45	.09	.02	3.03	3.18	3.66	4.05
128	2015	7.15	-0.11	.09	.02	3.28	3.57	4.48	
128	2018	7.87	-0.20	.09	.02	3.48	3.77	4.17	4.72
132	2031	9.98	-0.07	.08	.02	3.96	4.87	5.58	6.36
134	2037	11.07	.07	.17	.02	4.15	5.75	6.56	
135	2041	11.72	.15	.16	.02	4.50			
136	2045	12.46	.45	.16	.02	4.49			
137	2049	13.17	.19	.17	.02	4.60	5.12	6.17	7.02
138	2053	13.87	-0.12	.17	.02	4.73	4.96	7.76	
139	2057	14.47	.35	.17	.02	4.87	5.11	8.03	
140	2101	15.17	.08	.17	.02	5.00	8.25		
141	2105	15.87	.52	.17	.02	5.28	5.63	6.64	
142	2109	16.56	.22	.16	.02	5.42			

BEAUF6 88-9R

113	13	12.24.5	13.1.44	4.1 61.	4.57 1.
119	1946	12. 3.07	5.6244.8	-5 2.72	
120	1949	12. 3.07	5.6244.2	.38 2.41	
122	1955	12. 3.07	5.6244.4	.53 3.23	
123	1958	12. 3.07	5.6239.5	0. 4.21	
124	2000	12. 3.07	5.6245.	.47 3.95	
125	2006	12. 3.07	5.6247.1	-.34 5.52	
126	2009	12. 3.07	5.6247.7	.45 5.74	
128	2015	11. 3.07	5.6248.0	-.11 7.17	
128	2018	11. 3.07	5.6247.7	-.2 7.98	
132	2031	11. 3.07	5.6243.2	-.07 9.97	
133	2034	11. 3.07	5.6268.	.1510.25	
134	2037	11. 3.07	5.6276.4	.0718.83	
135	2041	11. 3.07	5.6271.6	.1511.41	
136	2045	11. 3.07	5.6273.	.4511.85	
137	2049	11. 3.07	5.6276.5	.1912.81	
138	2053	11. 3.07	5.6277.	-.1213.82	
139	2057	11. 3.07	5.6276.8	.3513.55	
140	2101	11. 3.07	5.6276.9	.0814.92	
141	2105	11. 3.07	5.6276.7	.5215.18	
142	2109	12. 3.07	5.6273.7	.2216.14	
				5.02	

BEAU76 12-13

OPRM	DBBM	DBEM	TINTS	CRM	V1	SVMS	CLM	S1M	SDM
12	12	15	22.96	18.50	1.440	4.00	61.00	4.57	1.00
164	0142	12.	2.65	2.6537.2	-.07	.49			
	.74								
165	0145	12.	2.65	2.6538.9	-.02	1.34			
	1.15								
166	0148	11.	2.65	2.6540.1	-.04	1.87			
	1.58								
167	0151	11.	2.65	2.6542.5	.57	1.80			
	1.20								
168	0154	11.	2.65	2.6546.7	.06	2.42			
	1.94								
169	0157	10.	2.65	2.6547.7	.53	2.87			
	1.77								
171	0203	11.	2.65	5.8848.0	.69	3.77			
	2.05								
172	0206	11.	2.65	5.8844.5	.10	4.88			
	2.77								
173	0209	11.	2.65	5.8847.1	-.05	5.40			
	3.82								
175	0214	12.	2.65	5.8844.9	.18	6.0			
	3.0								
176	0217	12.	2.65	5.8847.4	.65	6.07			
	2.65								
177	0220	12.	2.65	5.8846.3	.13	7.11			
	3.32								
178	0223	12.	2.65	5.8844.2	-.17	8.83			
	3.76								
179	0226	13.	2.65	5.8846.4	.08	1.30			
	3.56								
180	0229	13.	2.65	5.8845.0	-.15	9.1			
	4.0								
181	0232	13.	2.65	5.8873.5	-.14	9.56			
	4.04								
182	0235	13.	2.65	5.8871.5	-.12	9.90			
	2.31								
183	0238	13.	2.65	5.8870.0	.1710.47				
	3.41								
184	0307	13.	2.65	5.8868.1	-.0714.91				
	4.74								
185	0312	13.	2.65	5.8872.5	-.4916.21				
	5.32								
186	0317	13.	2.65	5.8872.7	.6116.17				
	4.38								
188	0329	13.	2.65	5.88117.5	.3518.62				
	5.0								
190	0340	14.	2.65	5.88137.3	-.2021.13				
	6.0								
191	0346	14.	2.65	5.88138.1	.5821.57				
	5.45								

BEAU76 12-13 CORRECTED

OPRM	DBBM	DBEM	TINTS	CRM	V1	SVMS	CLM	S1M	SDM
12	12	15	22.96	18.50	1.440	4.00	61.00	4.57	1.00
164	142	.88	-0.07	.06	.02	.75			
165	145	1.39	-0.02	.07	.02	1.21			
166	148	1.90	-0.04	.07	.02	1.55			
167	151	2.45	.57	.08	.02	1.86			
168	154	2.97	.06	.09	.02	2.10			
169	157	3.49	.53	.09	.02	2.41			
171	203	4.55	.69	.09	.02	2.85			
172	206	4.98	.10	.08	.02	2.97			
173	209	5.44	-0.05	.09	.02	3.08			
175	214	6.26	.18	.08	.02	3.28			
176	217	6.81	.65	.09	.02	3.41			
177	220	7.33	.13	.09	.02	3.56			
178	223	7.94	-0.17	.09	.02	3.69			
179	226	8.47	.08	.09	.02	3.78			
180	229	8.83	-0.15	.08	.02	3.95			
181	232	9.58	-0.14	.16	.02	4.88			
182	235	9.94	-0.12	.16	.02	2.37			
183	238	10.79	.17	.15	.02	4.15			
184	307	16.99	-0.07	.15	.02	4.84			
185	312	18.84	-0.49	.16	.02	5.81			
186	317	16.84	.61	.16	.02	5.17			
190	329	19.26	.35	.29	.02	5.66			
190	340	21.27	-0.20	.34	.02	6.17			
191	346	22.48	.58	.33	.02	6.39			

G6

G5

G4

G3

G2

G1

IC

TC

IS

DISTS

FCOR

G1

G2

G3

G4

G5

G6

BEAUT6 18-19

15.	15.	14.28.5	14.	1.44	4.9861.	4.57	1.
225	0554	15.	1.94	1.9444.0	-10	1.62	
1.33							
226	0557	15.	1.94	1.9440.0	.37	1.57	
1.24							
227	0600	16.	1.94	2.5941.9	.33	2.27	
1.69							
228	0603	16.	1.94	2.5940.9	-.34	3.56	
2.70							
229	0606	17.	1.94	2.5939.3	.43	3.43	
2.36							
230	0609	17.	1.94	2.5940.7	-.30	4.83	
3.41							
231	0612	17.	1.94	2.5938.7	-.42	5.61	
3.82							
232	0615	18.	1.94	2.5944.0	.72	5.10	
2.93							
233	0618	18.	1.94	2.5939.3	.74	5.75	
3.14							
234	0621	18.	1.94	2.5940.4	.41	6.71	
3.66							
235	0624	18.	1.94	2.5939.6	.21	7.57	
4.05							
236	0627	18.	1.94	2.5943.6	.06	8.35	
4.30							
237	0630	18.	1.94	2.5943.0	.39	8.67	
4.14							
238	0633	18.	1.94	2.5944.9	.88	8.85	
3.82							
239	0636	17.	1.94	2.5944.1	-.04	10.40	
4.88							
240	0639	17.	1.94	2.5945.1	.41	10.58	
4.65							
242	0644	16.	1.94	2.5948.1	.18	11.58	
4.84							
243	0647	16.	1.94	2.5949.8	.39	12.20	
5.01							
244	0650	16.	1.94	2.5950.1	.39	12.79	
5.17							
246	0655	16.	1.94	2.5945.3	.21	13.98	
5.52							
247	0658	16.	1.94	2.5943.7	.80	13.93	
5.08							

BEAUT5 18-19 CORRECTED

DARM	DBRM	DRFM	DRIS	DRM	V1	SVMS	CLM	S1M	S0M
15	15	14	2A.50	14.00	1.440	4.98	61.00	4.57	1.00
SHOT TIME	DISTS	IS	TC	TCOR	G1	G2	G3	G4	G5
225	554	1.63	-0.10	.11	.01	1.35			
226	557	2.04	.37	.10	.01	1.72			
227	600	2.70	.33	.10	.02	2.14			
228	603	3.32	-0.34	.10	.02	2.47			
229	606	3.95	.43	.09	.02	2.90			
230	609	4.63	-0.30	.10	.02	3.22			
231	612	5.28	-0.42	.09	.02	3.51			
232	615	5.93	.72	.11	.02	3.77			
233	618	6.58	.74	.09	.02	3.99			
234	621	7.21	.41	.09	.02	4.18			
235	624	7.87	.21	.09	.02	4.37			
236	627	8.52	.06	.11	.02	4.48			
237	630	9.16	.39	.10	.02	4.65			
238	633	9.84	.88	.11	.02	4.83			
239	636	10.47	-0.04	.11	.02	4.96			
240	639	11.10	.41	.11	.02	5.19			
242	644	12.08	.38	.12	.02	5.36			
243	647	12.72	.39	.13	.02	5.54			
244	650	13.31	.39	.13	.02	5.71			
246	655	14.36	.21	.25	.02	6.00			
247	658	14.97	.81	.24	.02	6.14			
248	701	15.62	.72	.21	.02	6.29			
249	704	16.32	.47	.20	.02	6.46			
250	707	16.83	.18	.21	.02	6.61			
251	711	17.81	.70	.24	.02	6.64			
252	715	18.54	-0.06	.24	.02	6.91			

HRAU76 20-21 CORRECTED													
14	14	14	14	14	14	14	14	14	14	14	14	14	14
DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM
SHOT	TIME	DISTS	TS	TC	TCOR	G1	G2	G3	G4	G5	G6		
268	1145	1.10	.19	.10	.01	.91	.96						
269	1145	1.10	.19	.10	.01	.91	.96						
270	1151	2.42	1.10	.10	.02	1.96	2.07	2.19	2.35	2.47			
271	1154	2.78	.25	.10	.02	2.13	2.24	2.35	2.47				
272	1157	3.60	.66	.10	.02	2.42	2.70	2.83	3.04				
273	1200	4.11	.09	.10	.02	2.60	2.67	2.83	3.13				
274	1203	4.84	.35	.10	.02	2.81	3.24	3.94					
275	1206	5.39	.20	.11	.02	3.04	3.39	4.52					
276	1209	6.10	.15	.10	.02	3.27	3.72	3.79	3.85	4.29	5.05		
277	1212	6.78	.09	.12	.02	3.83	4.31						
278	1215	7.41	.07	.12	.02	3.78	4.21	4.46	4.93	5.69			
279	1218	8.05	.04	.12	.02	3.97	4.07	4.39	4.55	5.43			
280	1221	8.72	.02	.11	.02	4.15	4.40	4.90	5.07	5.72	6.02		
281	1224	9.39	.09	.12	.02	4.37	4.64	5.28	5.63	6.35			
282	1227	10.06	.09	.12	.02	4.61	5.53	5.98	6.51	6.85			
283	1230	10.79	.12	.22	.02	4.86	5.59	5.84	6.02	7.62			
284	1233	11.39	.04	.22	.02	5.05	5.56	5.65	6.01	6.75			
285	1236	12.03	.07	.21	.02	5.21	5.82	6.09	6.27	6.52			
286	1239	12.68	.03	.22	.02	5.44	6.14	6.71	7.54	7.82	8.04		
287	1242	13.94	.04	.47	.02	5.82	6.02	6.32	6.46	7.64	8.97		
288	1245	14.44	.04	.47	.02	6.05	6.16	7.24	7.92	9.47			
289	1250	15.73	.0	.47	.02	6.50	7.42	7.79	8.60	8.91			

HRAU76 20-21													
14	14	14	14	14	14	14	14	14	14	14	14	14	14
DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM	DRM
SHOT	TIME	DISTS	TS	TC	TCOR	G1	G2	G3	G4	G5	G6		
268	1145	1.10	.19	.10	.01	.91	.96						
269	1145	1.10	.19	.10	.01	.91	.96						
270	1151	2.42	1.10	.10	.02	1.96	2.07	2.19	2.35	2.47			
271	1154	2.78	.25	.10	.02	2.13	2.24	2.35	2.47				
272	1157	3.60	.66	.10	.02	2.42	2.70	2.83	3.04				
273	1200	4.11	.09	.10	.02	2.60	2.67	2.83	3.13				
274	1203	4.84	.35	.10	.02	2.81	3.24	3.94					
275	1206	5.39	.20	.11	.02	3.04	3.39	4.52					
276	1209	6.10	.15	.10	.02	3.27	3.72	3.79	3.85	4.29	5.05		
277	1212	6.78	.09	.12	.02	3.83	4.31						
278	1215	7.41	.07	.12	.02	3.78	4.21	4.46	4.93	5.69			
279	1218	8.05	.04	.12	.02	3.97	4.07	4.39	4.55	5.43			
280	1221	8.72	.02	.11	.02	4.15	4.40	4.90	5.07	5.72	6.02		
281	1224	9.39	.09	.12	.02	4.37	4.64	5.28	5.63	6.35			
282	1227	10.06	.09	.12	.02	4.61	5.53	5.98	6.51	6.85			
283	1230	10.79	.12	.22	.02	4.86	5.59	5.84	6.02	7.62			
284	1233	11.39	.04	.22	.02	5.05	5.56	5.65	6.01	6.75			
285	1236	12.03	.07	.21	.02	5.21	5.82	6.09	6.27	6.52			
286	1239	12.68	.03	.22	.02	5.44	6.14	6.71	7.54	7.82	8.04		
287	1242	13.94	.04	.47	.02	5.82	6.02	6.32	6.46	7.64	8.97		
288	1245	14.44	.04	.47	.02	6.05	6.16	7.24	7.92	9.47			
289	1250	15.73	.0	.47	.02	6.50	7.42	7.79	8.60	8.91			

9FAU76 228-23

19.	19.	70.21.0918.3	1.44	4.7461.	4.57 1.
305	0506	19. 2.16 2.1640.8	.15	.64	
58					
306	0509	19. 2.16 2.1639.9	.05	1.10	
1.00					
307	0512	19. 2.16 2.1640.4	-.12	1.96	
1.72					
308	0515	19. 2.16 2.1640.	-.54	2.57	
2.10					
309	0510	19. 2.16 2.1640.	-.05	2.44	
1.07					
310	0521	19. 2.16 2.1639.	.15	2.07	
2.08					
311	0524	19. 2.16 5.0541.7	.06	3.52	
2.45					
312	0527	19. 2.16 5.0540.4	-.10	4.34	
2.89					
313	0530	19. 2.16 5.0540.4	.11	4.60	
2.71					
314	0533	19. 2.16 5.0539.7	-.31	5.50	
3.25					
315	0536	19. 2.16 5.0539.2	-.17	6.02	
3.25					
316	0539	19. 2.16 5.0539.3	.53	5.89	
3.23					
317	0542	19. 2.16 5.0540.	-.08	7.05	
3.42					
318	0545	19. 2.16 5.0541.1	.62	7.06	
2.99					
319	0548	19. 2.16 5.0542.2	.31	7.65	
3.20					
320	0551	19. 2.16 5.0543.1	.32	8.27	
3.41					
321	0554	19. 2.16 5.0542.1	-.22	5.39	
4.05					
322	0557	19. 2.16 5.0542.9	.32	6.45	
3.66					
322	0600	19. 2.16 5.0544.9	.41	5.96	
3.68					
324	0603	19. 2.16 5.0542.6	-.20	11.12	
4.61					
325	0606	19. 2.16 5.0554.0	.41	11.19	
4.					
326	0609	19. 2.16 5.0560.	-.16	12.15	
4.70					
327	0612	19. 2.16 5.0560.3	-.15	12.66	
4.87					
328	0615	19. 2.16 5.0560.9	.18	13.19	
4.72					
330	0622	19. 2.16 5.0577.7	-.25	14.50	
4.93					

9FAU76 228-23

331	0625	19. 2.16 5.0507.5	.32	15.16	
5.06					
332	0628	19. 2.16 5.0501.3	-.35	16.45	
5.69					
333	0631	18. 2.16 5.0570.0	-.07	16.65	
5.62					
334	0634	18. 2.16 5.0572.4	-.11	17.49	
6.01					
335	0637	18. 2.16 5.0572.2	.28	17.76	
5.0					
336	0640	18. 2.16 5.0572.	-.24	18.39	
5.98					
337	0643	18. 2.16 5.05112.2	-.42	18.68	
7.07					
338	0646	19. 2.16 5.05112.4	-.05	19.69	
6.43					
339	0650	20. 2.16 5.05166.2	-.31	20.70	
6.40					
340	0655	20. 2.16 5.05134.5	-.40	21.09	
6.37					

9FAU76 228-23

20.	20.	20.22.6018.3	1.44	4.5661.	4.57 1.
341	0736	20. 1.94 1.94135.	-.62	.76	
.75					
342	0741	20. 1.94 1.94135.	.46	.01	
.44					
343	0751	20. 1.94 3.36190.	-.14	3.28	
2.21					
344	0759	20. 1.94 3.36192.3	.01	4.75	
2.72					
345	0805	20. 1.94 3.36190.3	-.29	6.40	
3.43					
346	0813	20. 1.94 3.36192.9	.50	7.30	
3.08					
347	0820	20. 1.94 3.36100.5	-.07	9.67	
4.14					
348	0832	20. 1.94 3.36265.7	-.10	10.74	
4.10					
349	0846	19. 1.94 3.36340.	-.14	13.29	
4.80					
350	0904	19. 1.94 3.36195.0	-.15	17.44	
6.16					
351	0929	20. 1.94 3.36192.9	-.42	22.60	
7.70					

DEAFU76 24A-25

17.	17.	16.44.63	17.	1.44	4.0261.	4.57	1.
352	0311	17.	1.99	1.9939.0	-12	1.27	
1.26							
353	0314	17.	1.99	1.9942.2	.32	1.14	
1.01							
354	0317	17.	1.99	1.9940.2	.03	2.15	
1.76							
355	0320	18.	1.99	1.9939.0	.07	2.63	
2.11	2.28						
356	0323	18.	1.99	3.3440.1	.12	3.21	
2.33	2.52						
357	0326	18.	1.99	3.3439.0	.12	3.62	
2.66	2.87						
358	0329	18.	1.99	3.3441.7	-.13	4.65	
3.15	3.32	3.5					
359	0332	18.	1.99	3.3439.0	.32	4.44	
2.97	3.72						
360	0335	18.	1.99	3.3439.4	.06	5.7	
3.47	4.18						
361	0338	18.	1.99	3.3439.6	-.21	6.1	
4.01	4.28	5.13					
362	0341	18.	1.99	3.3440.6	.46	6.56	
3.68	5.23						
363	0344	18.	1.99	3.3436.2	-.35	8.03	
4.72	5.66						
364	0347	18.	1.99	3.3443.8	.33	7.91	
3.89	6.19						
365	0350	18.	1.99	3.3444.4	-.01	8.91	
4.38	5.32	6.07	6.74				
366	0353	18.	1.99	3.3444.3	-.26	9.74	
4.86	5.87	6.47	7.67				
367	0356	18.	1.99	3.3445.	-.95	10.13	
4.60							
368	0359	18.	1.99	3.3455.0	.04	11.55	
4.73	6.77						
369	0402	18.	1.99	3.3459.	-.38	11.03	
5.31	8.97						
370	0405	18.	1.99	3.3458.9	-.28	12.1	
5.43	6.84						
371	0408	19.	1.99	3.3472.3	-.33	12.7	
5.52							
372	0411	19.	1.99	3.3473.2	.19	12.83	
5.27	8.53						
373	0414	19.	1.99	3.3470.6	.37	13.26	
5.18	9.1						
374	0417	19.	1.99	3.3483.3	-.42	14.6	
6.06	7.55						
375	0420	19.	1.99	3.3486.9	-.44	15.3	
6.06							

DEAFU76 24B-25

17.	17.	16.24.60	17.	1.44	4.0261.	4.57	1.
383	0521	18.	2.27	2.27138.5	-.12	1.31	
.83							
384	0525	18.	2.27	2.27138.2	.00	2.14	
385	0536	18.	2.27	6.02163.	.09	4.31	
2.40							
386	0547	18.	2.27	6.02192.1	-.04	6.50	
3.09							
387	0555	18.	2.27	6.02192.3	.35	7.77	
3.15							
388	0604	18.	2.27	6.02182.7	.14	9.97	
3.84							
389	0617	18.	2.27	6.02200.4	.06	12.79	
4.51							
390	0630	18.	2.27	6.02210.	.05	15.65	
5.17							
391	0647	18.	2.27	6.02211.2	.05	19.35	
6.01							
392	0706	16.	2.27	6.02217.8	-.02	23.50	
7.14							
393	0723	16.	2.27	6.02313.	.01	24.60	
7.69							

REAU76 268-278 CORRECTED
 OPDM DBM DBEM TOTS DRM W1 SVMS CLM SLM SOM
 23 23 18 23.92 18.00 1.440 5.30 61.00 4.57 1.00
 SMOI TIME DISIS IS TROP G1 G2 G3 G4 G5 G6
 417 1158 .88 -0.35 .25 .02 .92
 418 1202 1.69 -0.02 .24 .02 1.51
 419 1205 2.27 .03 .23 .02 1.92
 420 1208 2.85 -0.17 .20 .02 2.25
 421 1213 4.10 -0.24 .40 .03 2.78
 422 1218 5.16 -0.58 .32 .03 3.18
 423 1222 6.11 -0.01 .33 .03 3.51
 424 1226 7.10 -0.65 .44 .03 3.81
 425 1230 8.04 -0.73 .44 .03 4.12
 426 1234 8.96 -0.51 .43 .03 4.50
 427 1239 10.14 -0.57 .42 .03 4.82
 428 1243 11.03 -0.22 .42 .03 5.09
 429 1254 13.42 -0.22 .62 .02 5.64
 430 1304 15.76 .17 .61 .02 6.17
 431 1321 19.60 -0.14 .92 .02 6.97
 432 1340 23.92 -0.13 .92 .02 7.84

REAU76 268-278
 23. 23. 18.21.9218. 1.44 5.3061. 4.57 1.
 417 1158 23. 2.36 2.3481.5 -.35 .98
 .89
 418 1202 23. 2.34 2.3476.6 -.62 1.47
 1.27
 419 1205 22. 2.34 2.3474.0 .83 2.01
 1.64
 420 1208 22. 2.34 2.3467.8 -.17 2.62
 2.20
 421 1213 22. 2.34 4.23121.0 -.24 3.94
 2.59
 422 1218 22. 2.34 4.23100.5 -.56 5.42
 3.41
 423 1222 22. 2.34 4.23103.3 -.01 5.79
 3.16
 424 1226 22. 2.34 4.23138.6 -.65 7.31
 4.80
 425 1230 22. 2.34 4.23131.6 -.73 8.33
 4.39
 426 1234 21. 2.34 4.23129.1 -.51 9.04
 4.55
 427 1239 21. 2.34 4.23127.1 -.57 10.29
 4.94
 428 1243 20. 2.34 4.23126.0 -.22 16.68
 4.47
 429 1254 19. 2.34 4.23180.4 -.22 13.82
 5.22
 430 1304 19. 2.34 4.23176.4 .17 14.98
 5.36
 431 1321 18. 2.34 4.23263.3 -.18 18.86
 6.20
 432 1340 18. 2.34 4.23263.6 -.13 23.13
 7.82

III
COMPUTER PROGRAMS TO
PLOT DATA (REFPLOTT, REDPLOT2)
AND PROGRAM TO COMPUTE
STRUCTURE (MULTLAY)

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PROGRAM REFPLOTT
DIMENSION XAXIS(5),YAXIS(3),SHOT(1),AT(11),R(4)
INTEGER PLOTEND,PSUP,PSDOWN,PENUP,PENDOWN
PLOTEND=-3 $ PSUP=-1 $ PSDOWN=-2
PENUP=3 $ PENDOWN=2
XAXIS(1)=8HDISTANCE
XAXIS(2)=9H 2 SEC P
XAXIS(3)=8HER INCH
YAXIS(1)=8HYTE 1 S
YAXIS(2)=8HEC PER I
YAXIS(3)=9HNCH
READ(5,8) XAXIS(4),XAXIS(5)
8 FORMAT(A8,A8,)
9 FORMAT(15X,F5.2)
NX=IOTS/2.04
IF(NX.LV.13)NX=13
NXAXIS=40
NYAXIS=24
CALL PLOTINT(-6.,6.,10)
CALL PLOT(28.,0.,PLOTEND)
CALL ROTATEXY
DO 10 I=1,NX
X=I
10 CALL PLOTSYMB(X,3.,20,13,0.,PSDOWN)
C GO BACK TO (4,-1)
CALL PLOTSYMB(4.,-1.,25,XAXIS,0.,NXAXIS)
CALL PLOT(0.,0.,PENUP)
DO 20 I=1,27
Y=I
20 CALL PLOTSYMB(0.,Y.,20,13,90.,PSDOWN)
C GO BACK TO (-1,4)
CALL PLOTSYMB(-1.,4.,25,YAXIS,90.,NYAXIS)
30 READ(5,40)ACE,(AT(I),I=1,11)
40 FORMAT(A5,2F5.0,9F5.2)
IF(EOF(5))GO TO 80
IF(ACE.EQ.5H ) GO TO 60
SHOT(1)=ACE
ITIM=AT(1)
Z=27.-AT(2)*.001*2.
YS=AT(6)
DIST=AT(7)+YS
X=0IST/2.
CALL PLOTSYMB(X,1.,10,SHOT,90.,5)
C TIME=T(I)=1 SEC/INCH,DIST=2SEC/INCH,AND X AND Y IN INCHES
II=1
DO 100 I=1,4
R(I)=AT(I+7)
IF(R(II).EQ.0) GO TO 30
100 II=I
GO TO 30
60 DO 70 I=1,11
IF(AT(I).EQ.0.) GO TO 70
Y=AT(I)+YS
IF(Y.GT.28.) GO TO 70
CALL PLOTSYMB(X,Y.,10,3,0.,PSUP)
70 CONTINUE
CALL PLOTSYMB(X,2.,1,13,90.,PSUP)
GO TO 30
80 XN=NX+4
CALL PLOT(XN,30.,PLOTEND)
END

```

```

PROGRAM REDPLOT2
DIMENSION XAXIS(5),YAXIS(5),SHOT(1),AT(11),R(4)
DIMENSION DEPI(100),XD(100)
INTEGER PLOTEND,PSUP,PSDOWN,PENUP,PENDOWN
PLOTEND=-3 $ PSUP=-1 $ PSDOWN=-2
PENUP=3 $ PENDOWN=2 $ DEPTH=0. $ NC=0
WRITE(61,3)
3 FORMAT(4 GIVE REDUCING VELOCITY, F5.2)
READ(60,4)REDVEL
4 FORMAT(F5.2)
XAXIS(1)=8HDISTANCE
XAXIS(2)=8M 1 SEC P
XAXIS(3)=8HER INCH
YAXIS(1)=8HTIME .5
YAXIS(2)=8HSEC PER
YAXIS(3)=8MINCH
YAXIS(4)=8HT - X /
READ(5,8) XAXIS(4),XAXIS(5)
8 FORMAT(A8,A4)
9 READ(5,9)TOTS,V1
9 FORMAT(15X,F5.2,5X,F5.3)
NX=TOTS/1.04.
IF(NX.LT.13)NX=13
NXAXIS=40
NYAXIS=40
ENCODE(8,101,YAXIS(5))REDVEL
101 FORMAT(F5.2,3X)
CALL PLOTINT(-6.,6.,10)
CALL PLOT(29.,0.,PLOTEND)
CALL ROTATEXY
DO 10 I=1,NX
X=I
10 CALL PLOTSYMB(X,0.,20,13,0.,PSDOWN)
C GO BACK TO (4,-1)
CALL PLOTSYMB(4.,-1.,25,XAXIS,0.,NXAXIS)
CALL PLOT(8.,0.,PENUP)
DO 20 I=1,27
Y=I
20 CALL PLOTSYMB(0.,Y.,20,13,90.,PSDOWN)
C GO BACK TO (-1,4)
CALL PLOTSYMB(-1.,4.,25,YAXIS,90.,NYAXIS)
30 READ(5,40)ACE,(AT(I),I=1,11)
40 FORMAT(A5,2F5.0,9F5.2)
IF(EOF(5))GO TO 80
IF(ACE.EQ.5H 1 GO TO 60
SHOT(1)=ACE
ITIM=AT(1)
ND=ND+1
DEP(ND)=27.-AT(2)*.001*2.
YS=AT(6)
DIST=AT(7)+YS
REDUCE=DIST*V1/REDVEL
X=DIST/1.
XD(ND)=Y
IF(X.GT.37.) GO TO 55
CALL PLOTSYMB(X,1.,10,SHOT,90.,5)
C TIME=T(I)*.5 SEC/INCH,DIST=2 SEC/INCH,AND X AND Y IN INCHES
55 II=1
DO 100 I=1,4
P(I)=AT(I+7)
IF(R(I).EQ.0) GO TO 30
100 II=I
GO TO 30
60 DO 70 I=1,11
IF(AT(I).EQ.0.) GO TO 30
Y=AT(I)+YS
Y=(Y-REDUCE)*2.05.
IF(Y.GT.27.) GO TO 70
IF(X.GT.37.) GO TO 70
CALL PLOTSYMB(X,Y.,10,3,0.,PSUP)
70 CONTINUE
GO TO 30
80 DO 90 I=1,ND
X=XD(I)
DEPTH=DEP(I)
90 CALL PLOTSYMB(X,DEPTH.,1,13,90.,PSUP)
XN=NX+4
CALL PLOT(XN,30.,PLOTEND)
END

```

```

PROGRAM MULTLAY
DIMENSION W(20),V(20),VA(20),VB(20),ALPH(20),BETA(20),C(20),
1 A(20),B(20),TAI(20),TBI(20),HA(20),HB(20),DA(20),CB(20),P(20)
DIMENSION TITLE(N)
C IF TBI INTERCEPT TIMES ARE NOT READ IN, INSERT A BLANK
C CARD WHERE THEY ARE CALLED FOR IN THE DATA DECK. THEY
C WILL THEN BE COMPUTED BY FORMULA AFTER STEP 421. IF THEY
C ARE READ IN, THEY WILL BE CHECKED FOR CONSISTENCY WITHIN 10 PC
402 WRITE (61,401)

401 FORMAT (#0#)
C N=NUMBER OF LAYERS OR TRAVEL TIME SEGMENTS, X=END-TO-END
C SPREAD LENGTH
READ (5,405)N,X,(TITLE(I),I=1,6)
IF(EOF(5)) CALL EXIT
405 FORMAT (I4,F8.0,6A8)
IF (N) 640,640,407
407 READ (5,410)(VA(I),I=1,N)
410 FORMAT (9F8.0)
READ (5,410)(VB(I),I=1,N)
TAI(1) = .0
READ (5,410)(TAI(I),I=2,N)
TBI(1) = .0
READ (5,410)(TBI(I),I=2,N)
WRITE (61,415)X,(TITLE(I),I=1,6)
415 FORMAT (# #,#OVERSAL DISTANCE = # #,F10.3,3X,6A8,/)
WRITE (61,420)
420 FORMAT(# INPUT DATA### LAYER APPARENT APPARENT#,
1# INTERCEPT INTERCEPT### VELOCITIES A VELO#,
2#CITIES B TIMES A TIMES B#)
DO 425 I=2,N
TBB = TAI(I) + X*(1./VA(I) - 1./VB(I))
IF (TBI(I)) 422,422,423
422 TBI(I) = TBB
GO TO 425
423 TAEEND = TAI(I) + X/VA(I)
TBEEND = TBI(I) + X/VB(I)
ERROR = ABSF(TAEEND/TBEEND - 1.)
IF (ERROR - .10) 425,424,424
424 WRITE (61,1424) I
1424 FORMAT(#0APPARENT VELOCITY AND TIME INTERCEPT DATA ARE#,
1# INCONSISTENT AT LAYER ### NUMBER #,I2,# END-TO-END #,
2#TRAVEL TIMES DIFFER BY MORE THAN 10 PERCENT.##)
GO TO 425
425 CONTINUE
WRITE (61,1425) (I,VA(I),VB(I),TAI(I),TBI(I),I=1,N)
1425 FORMAT(# #,I4,F13.3,F14.3,F12.3,F10.3)
V(1) = (VA(1) + VB(1))*.5
DO 570 M = 2,N
K = 1
ALPH(1) = ASINF(V(1)/VB(M))
BETA(1) = ASINF(V(1)/VA(M))
IF (M-2) 500,500,510
500 A(1) = (ALPH(1) + BETA(1))*.5
W(2) = (ALPH(1) - BETA(1))*.5
V(2) = V(1)/SINF(A(1))
GO TO 550
510 A(1) = ALPH(1) - W(2)
B(1) = BETA(1) + W(2)
520 K = K+1
VV = V(K)/V(K-1)
P(K) = ASINF(VV*SINF(A(K-1)))

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```

Q(K) = ASINF(VV*SINF(B(K-1)))
IF (K+1-N) 530,540,540
530 A(K) = P(K) - W(K+1) + W(K)
R(K) = Q(K) + W(K+1) - W(K)
ALPH(K) = A(K) + W(K+1)
BETA(K) = B(K) - W(K+1)
GO TO 520
540 A(K) = (P(K) + Q(K))*0.5
B(K) = A(K)
W(K+1) = W(K) + (P(K) - Q(K))*0.5
ALPH(K) = A(K) + W(K+1)
BETA(K) = B(K) - W(K+1)
V(K+1) = V(K)/SINF(A(K))
550 KK = K-1
HMA = 0.
HMB = 0.
IF (K.EQ.1) GO TO 561
DO 560 I = 1, KK
HM = COSF(ALPH(I)) + COSF(BETA(I))
HH = HM/V(I)
HMA = HMA + HM*HA(I)
560 HMB = HMB + HM*HB(I)
561 R = V(K)/(COSF(ALPH(K)) + COSF(BETA(K)))
HA(K) = R*(TAI(K+1) - HMA)
HB(K) = R*(TBI(K+1) - HMB)
DA(1) = HA(1)
DB(1) = HB(1)
DA(K) = DA(K-1) + HA(K)
DB(K) = DB(K-1) + HB(K)
570 CONTINUE
RTOD=190./3.1415926
DO 580 J = 2, N
580 W(J) = W(J)*RTOD
WRITE (61,620)
620 FORMAT(20COMPUTED STRUCTURE### LAYER VELOCITY %,
1#THICKNESS A THICKNESS B DIP DEPTH A DEPTH B#)
I = 1
WRITE (61,625) I, V(I), HA(I), HB(I), DA(I), DB(I)
625 FORMAT(2#,I4,F12.3,F11.3,F14.3,9X,F8.3,F9.3)
VN = N-1
WRITE (61,630) (I, V(I), HA(I), HB(I), W(I), DA(I), DB(I),
1 I=2, NN)
630 FORMAT(2#,I4,F12.3,F11.3,F14.3,F9.3,F8.3,F9.3)
WRITE (61,635) N, V(N), W(N)
635 FORMAT(2#,I4,F12.3,23X,F11.3)
GO TO 402
640 CONTINUE
END

```

INPUT FORMAT FOR PROGRAM MULTLAY

N	X	TITLE(I)		
VA(1)	VA(2)	.	.	VA(N)
VB(1)	VB(2)	.	.	VB(N)
TAI(1)	TAI(2)	.	.	TAI(N)
TBI(1)	TBI(2)	.	.	TBI(N)

N : Number of layers (equal to number of velocities).

X : End to end profile length.

TITLE(I) : Line identification.

I=1,....,N : Layer number.

VA(I) : Apparent velocities from the A-end of the profile.

VB(I) : Apparent velocities from the B-end of the profile.

TAI(I) : Intercept times for layers 2 through N at A-end of the profile.

TBI(I) : Intercept times for layers 2 through N at B-end of the profile.

All distances in meters or kilometers.

All velocities in meters per seconds or kilometers per seconds.

All times in seconds.

With single-ended line : $VB(I) = VA(I)$ and $TBI(I) = TAI(I)$.

OUTPUT FORMAT FOR PROGRAM MULTLAY

REVERSEAL DISTANCE =		X		TITLE(I)		
INPUT DATA						
LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B	INTERCEPT	
1	VA(1)	VB(1)	TAI(1)	TBI(1)		
2	VA(2)	VB(2)	TAI(2)	TBI(2)		
...	
N	VA(N)	VB(N)	TAI(N)	TBI(N)		
COMPUTED STRUCTURE						
LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	V(1)	HA(1)	HB(1)	W(1)	DA(1)	DB(1)
2	V(2)	HA(2)	HB(2)	W(2)	DA(2)	DB(2)
...
N-1	V(N-1)	HA(N-1)	HB(N-1)	W(N-1)	DA(N-1)	DB(N-1)
N	V(N)	HA(N)	HB(N)	W(N)	DA(N)	DB(N)

X : End to end spread length.
 TITLE(I) : Line identification.
 I=1,...,N : Layer number.
 VA(I) : Apparent velocities from the A-end of the profile.
 VB(I) : Apparent velocities from the B-end of the profile.
 TAI(I) : Intercept times for layers 2 through N at A-end of the profile.
 TBI(I) : Intercept times for layers 2 through N at B-end of the profile.
 V(I) : True layer velocities.
 HA(I) : Layer thicknesses at A-end.
 HB(I) : Layer thicknesses at B-end.
 W(I) : Layer dips in degrees.
 DA(I) : Depths from surface to bottom of layers at A-end.
 DB(I) : Depths from surface to bottom of layers at B-end.

All times in seconds.
 All distances in meters or kilometers.
 All velocities in meters per seconds or kilometers per seconds.

IV
INTERCEPT TIMES AND APPARENT
VELOCITIES (INPUT OF MULTLAY)
AND COMPUTED STRUCTURES
(OUTPUT OF MULTLAY)
FOR ALL LINES

4 21.62 MGL1
 1.44 2.14 2.77 5.02
 1.44 2.14 2.77 5.02
 0.044 0.080 0.680
 0.044 0.080 0.680

REVERSAL DISTANCE = 21.620 MGL1S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TYPES A	INTERCEPT TYPES B
1	1.440	1.440	0	0
2	2.140	2.140	.044	.044
3	2.770	2.770	.080	.080
4	5.020	5.020	.680	.680

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1.440	.043	.043		.043	.043
2	2.140	.049	.049	0	.092	.092
3	2.770	.966	.966	0	1.058	1.058
4	5.020		0			

4 12.77 MGL2
 1.44 2.14 2.99 5.26
 1.44 2.14 2.99 5.26
 0.031 0.230 0.760
 0.031 0.230 0.760

REVERSAL DISTANCE = 12.770 MGL2S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TYPES A	INTERCEPT TYPES B
1	1.440	1.440	0	0
2	2.140	2.140	.031	.031
3	2.990	2.990	.230	.230
4	5.260	5.260	.760	.760

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1.440	.030	.030		.030	.030
2	2.140	.296	.296	0	.326	.326
3	2.990	.040	.040	0	1.175	1.175
4	5.260		0			

6 26.61 91 6 TO 1 M1267
 1.44 2.25 2.46 3.01 3.727 5.387
 1.44 2.25 2.46 3.01 3.716 5.259
 0.10 0.15 0.20 0.45 1.40
 0.10 0.15 0.20 0.43 1.28

REVERSAL DISTANCE = 26.610 91 6 TO 1 M1267S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1.440	1.440	0	0
2	2.250	2.250	.100	.100
3	2.460	2.460	.150	.150
4	3.010	3.010	.200	.200
5	3.727	3.716	.450	.430
6	5.387	5.259	1.400	1.280

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1.440	.094	.094		.094	.094
2	2.250	.124	.124	0	.217	.217
3	2.460	.027	.027	0	.244	.244
4	3.010	.578	.527	0	.823	.771
5	3.721	2.183	1.944	.116	3.006	2.715
6	5.322			.624		

6 29.39 91 4 TO 3 M345
 1.44 2.29 2.56 2.99 3.898 4.904
 1.44 2.29 2.56 2.99 3.867 4.674
 0.10 0.16 0.20 0.56 1.375
 0.10 0.16 0.20 0.50 1.080

REVERSAL DISTANCE = 29.390 91 4 TO 3 M345S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1.440	1.440	0	0
2	2.290	2.290	.100	.100
3	2.560	2.560	.160	.160
4	2.990	2.990	.200	.200
5	3.898	3.867	.560	.500
6	4.904	4.674	1.375	1.080

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1.440	.093	.093		.093	.093
2	2.290	.137	.137	0	.230	.230
3	2.560	.025	.025	0	.255	.255
4	2.990	.771	.630	0	1.026	.885
5	3.892	2.419	1.623	.276	3.665	2.568
6	4.784			1.707		

5 10958.ARC WEST 76 BEAUFORT #8A9A
 1440. 1600. 2230. 3020. 4680.
 1440. 1600. 2230. 3020. 4680.
 .010 .215 .575 1.255
 .010 .215 .575 1.255

REVERSAL DISTANCE = 10958.000 ARC WEST 76 BEAUFORT #8A9AS

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	2230.000	2230.000	.215	.215
4	3020.000	3020.000	.575	.575
5	4680.000	4680.000	1.255	1.255

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.519	16.510		16.510	16.510
2	1600.000	226.906	226.806	0	243.324	243.324
3	2230.000	519.810	519.810	0	763.142	763.142
4	3020.000	1100.723	1100.723		01863.865	1863.865
5	4680.000			0		

7 23846.ARC WEST 76 BEAUFORT #8B9B
 1440. 1600. 2230. 2830. 4240. 5630. 7070.
 1440. 1600. 2230. 2830. 4240. 5630. 7070.
 .010 .215 .470 1.050 1.440 1.925
 .010 .215 .470 1.050 1.440 1.925

REVERSAL DISTANCE = 23846.000 ARC WEST 76 BEAUFORT #8B9BS

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	2230.000	2230.000	.215	.215
4	2830.000	2830.000	.470	.470
5	4240.000	4240.000	1.050	1.050
6	5630.000	5630.000	1.440	1.440
7	7070.000	7070.000	1.925	1.925

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.519	16.510		16.510	16.510
2	1600.000	226.806	226.806	0	243.324	243.324
3	2230.000	391.899	391.899	0	635.223	635.223
4	2830.000	887.279	887.279		01522.501	1522.501
5	4240.000	906.128	906.128		02428.629	2428.629
6	5630.000	1750.786	1750.786		04179.415	4179.415
7	7070.000			0		

7 28.07 LINE 10-11 12-13 WITH 6.0 AND 7.0 LAYERS M1012
 1.440 1.650 2.509 3.044 4.056 6.000 6.906
 1.440 1.650 2.509 3.090 3.804 6.000 7.129
 0.008 0.440 0.675 1.130 1.760 1.805
 0.008 0.440 0.920 1.360 1.760 1.830

REVERSAL DISTANCE = 28.070 LINE 10-11 12-13 WITH 6.0 AND 7.0 LAYERS M1012S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1.440	1.440	0	0
2	1.650	1.650	.008	.008
3	2.509	2.509	.440	.440
4	3.044	3.090	.675	.820
5	4.056	3.804	1.130	1.360
6	6.000	6.000	1.760	1.760
7	6.906	7.129	1.805	1.830

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1.440	.012	.012		.012	.012
2	1.650	.467	.467	0	.479	.479
3	2.509	.400	.716	0	.879	1.195
4	3.067	.877	.966	-0.611	1.756	2.161
5	3.921	1.095	.362	2.615	2.841	2.523
6	5.994	-0.186	.063	-0.927	2.655	2.586
7	7.006			-2.886		

6 29736.ARC WEST 76 BEAUFORT M1617
 1440. 1600. 1820. 2440. 3620. 6080.
 1440. 1600. 1820. 2440. 3620. 6080.
 .010 .100 .380 1.025 1.745
 .010 .100 .380 1.025 1.745

REVERSAL DISTANCE = 29736.000 ARC WEST 76 BEAUFORT M1617S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	1820.000	1820.000	.100	.100
4	2440.000	2440.000	.380	.380
5	3620.000	3620.000	1.025	1.025
6	6080.000	6080.000	1.745	1.745

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.518	16.518		16.518	16.518
2	1600.000	144.306	144.306	0	160.824	160.824
3	1820.000	307.807	307.807	0	468.631	468.631
4	2440.000	907.949	907.945	0	1376.575	1376.575
5	3620.000	1226.193	1226.193		2602.768	2602.768
6	6080.000			0		

6 26699.ARC WEST 76 BEAUFORT M1819
 1440. 1600. 1840. 2320. 3310. 5660.
 1440. 1600. 1840. 2320. 3310. 5660.
 .010 .125 .465 1.205 2.310
 .010 .125 .465 1.205 2.310

REVERSAL DISTANCE = 26699.000 ARC WEST 76 BEAUFORT M1819S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	1840.000	1840.000	.125	.125
4	2320.000	2320.000	.465	.465
5	3310.000	3310.000	1.205	1.205
6	5660.000	5660.000	2.310	2.310

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.518	16.518		16.518	16.518
2	1600.000	179.367	179.367	0	195.885	195.885
3	1840.000	429.958	429.958	0	625.843	625.843
4	2320.000	975.136	975.136		01600.979	1600.979
5	3310.000	1762.815	1762.815		03363.796	3363.796
6	5660.000			0		

6 22651.ARC WEST 76 BEAUFORT M2021
 1440. 1600. 1890. 2350. 3390. 5680.
 1440. 1600. 1890. 2350. 3390. 5680.
 .010 .125 .490 1.105 2.075
 .010 .125 .490 1.105 2.075

REVERSAL DISTANCE = 22651.000 ARC WEST 76 BEAUFORT M2021S

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	1890.000	1890.000	.125	.125
4	2350.000	2350.000	.490	.490
5	3390.000	3390.000	1.105	1.105
6	5680.000	5680.000	2.075	2.075

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.518	16.518		16.518	16.518
2	1600.000	165.535	165.535	0	182.053	182.053
3	1890.000	509.354	509.354	0	691.407	691.407
4	2350.000	740.727	740.727		01432.134	1432.134
5	3390.000	1630.983	1630.983		03063.117	3063.117
6	5680.000			0		

6 45770.ARC WEST 76 BEAUFORT #22A24B REVERSE
 1440. 1600. 1932. 2348. 2932. 5781.
 1440. 1600. 1826. 2315. 2880. 6034.
 .010 .175 .450 .810 1.715
 .010 .100 .170 .525 2.050

REVERSAL DISTANCE = 41000.000 ARC WEST 76 BEAUFORT #24A22BS REVERSE

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	1937.000	1945.000	.120	.215
4	3395.000	3398.000	1.165	1.175
5	5687.000	5750.000	2.210	2.290

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.518	16.518		16.518	16.518
2	1600.000	147.839	282.887	0	164.357	298.605
3	1940.983	1160.407	997.175	-0.1721324	764	1295.781
4	3396.490	1869.649	2032.408	.0353194	413	3328.189
5	5718.294			-0.185		

5 41000.ARC WEST 76 BEAUFORT #24A22B REVERSE
 1440. 1600. 1937. 3395. 5687.
 1440. 1600. 1945. 3398. 5750.
 .010 .120 1.165 2.210
 .010 .215 1.175 2.290

REVERSAL DISTANCE = 45770.000 ARC WEST 76 BEAUFORT #22A24BS REVERSE

INPUT DATA

LAYER	APPARENT VELOCITIES A	APPARENT VELOCITIES B	INTERCEPT TIMES A	INTERCEPT TIMES B
1	1440.000	1440.000	0	0
2	1600.000	1600.000	.010	.010
3	1832.000	1826.000	.175	.100
4	2348.000	2315.000	.450	.170
5	2932.000	2880.000	.810	.525
6	5781.000	6034.000	1.715	2.050

COMPUTED STRUCTURE

LAYER	VELOCITY	THICKNESS A	THICKNESS B	DIP	DEPTH A	DEPTH B
1	1440.000	16.518	16.518		16.518	16.518
2	1600.000	265.613	141.769	0	282.131	158.287
3	1828.987	280.927	24.827	.170	563.058	192.315
4	2331.318	535.554	641.824	.4551098	612	833.338
5	2905.706	1100.886	2197.800	.3252198	698	3031.138
6	5903.385			-1.034		

V

PROGRAM TO COMPUTE THE OFFSET
DISTANCES OF THE RAYS (WAREFRA)
AND INPUT AND OUTPUT DATA
FOR PROCESSED LINES

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PROGRAM WAREFRA
C THIS PROGRAM COMPUTES PLANE DIPPING LAYER MODEL
C PARAMETERS, SECTIONS OF LAYERS ALONG WHICH RAY IS REFRACTED
C AND THE CRITICAL DISTANCE. THE INPUT DATA REQUIRES
C KNOWN OR APPARENT LAYER VELOCITIES (VA) AND EITHER
C INTERCEPT TIME FROM REFRACTED ARRIVAL OR LAYER THICKNESS
C VERTICALLY UNDER THE ORIGIN. LAYER DIP IS ASSUMED ZERO
C IF LEFT BLANK. IF LAYER THICKNESS IS GIVEN, GIVEN
C VELOCITY IS TAKEN TO BE THE TRUE LAYER VELOCITY.
  DIMENSION V(10), HDR(10), W(10), VA(10), TIA(10), HA(10)
  DIMENSION R (10), ALPHA (10), BETA (10), HB (10), A (10)
  DIMENSION XA(10), XB(10), YA(10), YB(10), XC(10), P(10)
  DIMENSION Q (10)
  RTOD = 180. / 3.14159265
  DTOR = 1. / RTOD
C READ HDR CARD
10 READ (5, 100) N, V(1), X, HDR
  IF (EOF(5)) CALL EXIT
C N IS NUMBER OF LAYERS, V(1) IS VELOCITY OF FIRST LAYER,
C X IS LENGTH OF LINE, HDR IS IDENTIFIER MAX LENGTH OF 8
100 FORMAT (I5, F5.3, F5.2, 10A8)
  IF (EOF(1)) CALL EXIT
  IF (N .LT. 10) GO TO 15
  WRITE (6, 110) N
110 FORMAT (2-N LARGER THAN DIMENSIONS N =#, I5)
  CALL EXIT
15 K = 2
  VA (1) = V (1)
  W (1) = 0.0
C READ SUCCEEDING CARDS
C IF HA(I) IS NOT GIVEN, COMPUTE MODEL FROM TIA INTERCEPT
  READ (5, 101) VA (2), TIA (2), W (2), HA (1)
101 FORMAT (4F5.3)
  W (2) = W (2) * DTOR
  BETA (1) = ASINF (V (1) / VA (2))
  A (1) = R (1) = BETA (1) * W (2)
  ALPHA (1) = A (1) + W (2)
  V (2) = V (1) / SIN (A (1))
  IF (HA(1) .NE. 0.0) V(2) = VA(2)
C FIND OUT IF THICKNESS GIVEN. IF NOT, CALCULATE VELOCITY AND
C ANGLES.
  IF (HA (1) .NE. 0.0) GO TO 30
  IF (TIA (2) .NE. 0.0) GO TO 25
  22 WRITE (6, 111)
111 FORMAT (2-HA AND TIA .EQ. 0.0#)
  CALL EXIT
C COMPUTE DEPTHS TO LAYERS
25 HA(1) = (TIA(2)*V(1)) / (COS(ALPHA(1))*COS(BETA(1)))
30 HB (1) = HA (1) - X * TANF(W (2))
C COMPUTE CRITICAL DISTANCES AND END POINTS IN LAYER
C WHERE RAY TRAVELS AS REFRACTED WAVE
  XA (1) = HA (1) * TANF(ALPHA (1))
  1 / (1.0 + TANF(W (2)) * TANF(ALPHA (1)))
  YA (1) = HA (1) - XA (1) * TANF(W (2))
  XC(1) = (HA(1) - XA(1) * TANF(W(2))) * TANF(B(1)) + XA(1)
  XR (1) = HB (1) * TANF(BETA (1))
  1 / (1.0 - TANF(BETA (1)) * TANF(W (2)))
  YB (1) = HB (1) + XB (1) * TANF(W (2))
  XB (1) = X - XB (1)
40 K = K + 1
C DO LAYERS 3 THROUGH N
  READ (5, 101) VA (K), TIA (K), W (K), HA (K-1)
C COMPUTE ANGLES
  W (K) = W (K) * DTOR
  BETA (1) = ASINF (V (1) / VA (K))
  P (1) = BETA (1) + W (2)
  I = 1
  KM1 = K - 1
50 I = I + 1
  Q (I) = ASINF (V (I) / V (I-1) * SIN (B (I-1)))
  BETA (I) = Q (I) - W (I)
  R (I) = BETA (I) + W (I+1)
  IF (I .LT. KM1) GO TO 50
  A (K-1) = B (K-1)
  ALPHA (K-1) = A (K-1) + W (K)
  V (K) = V (K-1) / SIN (A (K-1))
  IF (HA(K-1) .NE. 0.0) V(K) = VA(K)
  P (K-1) = A (K-1) - W (K-1) + W (K)
  I = K - 1
70 I = I - 1
  A (I) = ASINF (V (I) / V (I+1) * SIN (P (I+1)))
  ALPHA (I) = A (I) + W (I+1)
  P (I) = A (I) - W (I) + W (I+1)
  IF (I .NE. 1) GO TO 70
  KM2 = K - 2
  TEMP1 = TEMP2 = TEMP3 = 0.0
  DO 80 I = 1, KM2
  TEMP1 = TEMP1 + HA (I) / W (I) * (COS (ALPHA (I)))

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      1      + COS (BETA (I)))
      TEMP2 = TEMP2 + HA (I)
      TEMP3 = TEMP3 + HB (I)
80 CONTINUE
      IF (HA (K-1) .NE. 0.0) GO TO 85
C FIND OUT IF THICKNESS GIVEN. IF NOT COMPUTE VELOCITY AND
C MORE ANGLES
      IF (TIA (K) .EQ. 0.0) GO TO 22
C COMPUTE DEPTH TO LAYER
      HA (K-1) = (TIA (K) - TEMP1) * V (K-1)
      1      / (COS (ALPHA (K-1)) + COS (BETA (K-1)))
C COMPUTE DISTANCES IN LAYER WHERE WAVE IS REFRACTED
85 TEMP2 = TEMP2 + HA (K-1)
      HB (K-1) = TEMP2 - TEMP3 - X * TANF(W (K))
      TEMP3 = TEMP3 + HB (K-1)
      TEMPA = HA (I) * TANF(ALPHA (I))
      1      / (1.0 + TANF(W (2)) * TANF(ALPHA (1)))
      TEMPXB = HB (I) * TANF(BETA (I))
      1      / (1.0 - TANF(W (2)) * TANF(BETA (1)))
      DO 115 I = 2, KM1
      TEMPA = TEMPA + (HA (I) * TANF(ALPHA (I)) + TEMPA
      1      * TANF(ALPHA (I)) * (TANF(W (I)) - TANF(W (I+1))))
      2      / (1.0 + TANF(ALPHA (I)) * TANF(W (I+1)))
      TEMPXB = TEMPXB + (HB (I) * TANF(BETA (I)) - TEMPXB
      1      * TANF(BETA (I)) * (TANF(W (I)) - TANF(W (I+1))))
      2      / (1.0 - TANF(BETA (I)) * TANF(W (I+1)))
115 CONTINUE
      XA (K-1) = TEMPA
      XB (K-1) = X - TEMPXB
      YA (K-1) = TEMP2 - XA (K-1) * TANF(W (K))
      YB (K-1) = TEMP3 + TEMPXB * TANF(W (K))
      I = K
      DELTAXC = TEMPA
123 I = I - 1
      DELTAXC = DELTAXC + (HA (I) * TANF(BETA (I)) + DELTAXC
      1      * TANF(BETA (I)) * (TANF(W (I)) - TANF(W (I+1))))
      2      / (1.0 - TANF(W (I)) * TANF(BETA (I)))
      IF (I .GT. 2) GO TO 120
      XC (K-1) = DELTAXC + (HA (I) - DELTAXC * TANF(W (2)))
      1      * TANF(BETA (1))
C GO BACK FOR ANOTHER LAYER
      IF (K .LT. N) GO TO 40
C CONVERT ANGLES TO DEGREES
      DO 130 I = 1, N
      W (I) = W (I) * PTOD
130 CONTINUE
C PRINT OUT RESULTS
      WRITE (61, 102) HDR, N, X
102 FORMAT (A0#,10A#,/,# N = #,I2,# SPREAD = #,F6.1)
      WRITE (61, 103)
103 FORMAT (A0 N APPARENT DIP LAYER THICKNESS#,/,
      1      # VELOCITY AT ORIGIN#)
      NM1 = N - 1
      DO 140 I = 1, NM1
      WRITE (61, 104) I, VA (I), W (I), HA (I)
104 FORMAT (I3,F9.3,F8.3,6X,F6.3)
140 CONTINUE
      WRITE (61, 104) N, VA (N), W (N)
      WRITE (61, 105)
105 FORMAT (A0 N DEPTH A THICK A VELOCITY THICK B #
      1      #DEPTH B#)
      SHA = 0.0
      SHB = 0.0
      DO 150 I = 1, NM1
      SHA = SHA + HA (I)
      SHB = SHB + HB (I)
      WRITE (61, 106) I, SHA, HA (I), W (I), HB (I), SHB
106 FORMAT (I3,F8.3,F9.3,F10.3,F10.3,F9.3)
150 CONTINUE
      WRITE (61, 107) N, V (N)
107 FORMAT (I3,18X,F8.2)
      WRITE (61, 108) X
108 FORMAT (A0LAYER RAY TO LAYER CRITICAL DIST RAY FROM #,
      1#LAYER#,/,# X Y #,
      2# Y#,/,# 0.00 0.00 #,
      3 F7.2,# 0.00#)
      DO 160 I = 1, NM1
      IP1 = I + 1
      WRITE (61, 109) I, YA (I), YA (I), XC (I), XR (I), YB (I)
109 FORMAT (I3,F9.3,F8.3,F11.3,F14.3,F9.3)
160 CONTINUE
      GO TO 10
      END

```

INPUT FORMAT FOR PROGRAM WAREFRA

N	V1	X	TITLE(I)
VA(1)	TAI(1)		
VA(2)	TAI(2)	W(2)	HA(1)
...
VA(N)	TAI(N)	W(N)	HA(N-1)

N : Number of layers (equal to number of velocities).
 V1 : Water velocity.
 X : End to end spread length.
 TITLE(I) : Line identification.
 I=1,...,N : Layer number.
 VA(I) : Apparent velocities at A-end or true velocities.
 TAI(I) : Intercept times at A-end.
 W(I) : Layer dips in degrees.
 HA(I) : Layer thicknesses at A-end.

All times in seconds.

All distances in kilometers.

All velocities in kilometers per seconds.

The program needs intercept times or layer thicknesses.

The layer dip is assumed zero if left blank.

If the layer thickness is given, the given velocity is taken to be the true layer velocity.

OUTPUT FORMAT FOR PROGRAM WAREFRA

TITLE(I)						
N =	N	SPREAD =		X		
N	APPARENT DIP		LAYER THICKNESS			
VELOCITY		AT ORIGIN				
1	VA(1)	W(1)	HA(1)			
2	VA(2)	W(2)	HA(2)			
...			
N-1	VA(N-1)	W(N-1)	HA(N-1)			
N	VA(N)	W(N)				
N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B	
1	SHA(1)	HA(1)	V(1)	HB(1)	SHB(1)	
2	SHA(2)	HA(2)	V(2)	HB(2)	SHB(2)	
...	
N-1	SHA(N-1)	HA(N-1)	V(N-1)	HB(N-1)	SHB(N-1)	
N			V(N)			
LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER		
	X Y			X Y		
	0 . 0 0			0 . 0 0		
1	XA(1)	YA(1)	XC(1)	XB(1)	YB(1)	
2	XA(2)	YA(2)	XC(2)	XB(2)	YB(2)	
...	
N-1	XA(N-1)	YA(N-1)	XC(N-1)	XB(N-1)	YB(N-1)	

TITLE(I) : Line identification.
 N : Number of layers including the water layer.
 X : End to end spread length.
 I=1,.....,N : Layer number.
 VA(I) : Apparent velocities at the A-end of the profile or true velocities.
 W(I) : Layer dips in degrees.
 HA(I) : Layer thicknesses at A-end.
 HB(I) : Layer thicknesses at B-end.
 V(I) : True velocities.
 SHA(I) : Layer depths at A-end.
 SHB(I) : Layer depths at B-end.
 XA(I) : Offset distances from A-end.
 XB(I) : Offset distances from B-end.
 XC(I) : Critical distances.
 YA(I) : Layer depths at the offset distances at A-end.
 YB(I) : Layer depths at the offset distances at B-end.

All distances in kilometers.

All velocities in kilometers per seconds.

41.44 21.62 WGL1
 2.136 .044
 2.769 .080
 5.017 .690

WGL15
 N = 4 SPREAD = 21.6

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.043
2	2.136	0	.049
3	2.769	0	.966
4	5.017	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.043	.043	1.440	.043	.043
2	.092	.049	2.136	.049	.092
3	1.057	.966	2.769	.966	1.057
4			5.02		

LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER	
	X	Y		X	Y
	0.00	0.00		21.62	0.00
1	.039	.043	.078	21.581	.043
2	.085	.092	.171	21.535	.092
3	.675	1.057	1.350	20.945	1.057

41.44 12.77 WGL2
 2.136 .031
 2.994 .230
 5.255 .760

WGL25
 N = 4 SPREAD = 12.9

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.030
2	2.136	0	.294
3	2.994	0	.852
4	5.255	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.030	.030	1.440	.030	.030
2	.325	.294	2.136	.294	.325
3	1.177	.852	2.994	.852	1.177
4			5.26		

LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER	
	X	Y		X	Y
	0.00	0.00		12.77	0.00
1	.020	.030	.055	12.742	.030
2	.316	.325	.633	12.454	.325
3	.730	1.177	1.461	12.040	1.177

E1.44 26.61 RI 6 TO 1 W1267
 2.249 .100
 2.463 .150
 3.013 .200
 3.721 .116 .578
 5.322 .6242.183

RI 6 TO 1 W1267S
 N = 6 SPREAD = 26.6

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.094
2	2.249	0	.122
3	2.463	0	.028
4	3.013	0	.578
5	3.721	-.116	2.183
6	5.322	.624	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.094	.094	1.440	.094	.094
2	.216	.122	2.249	.122	.216
3	.244	.028	2.463	.028	.244
4	.422	.578	3.013	.524	.769
5	3.005	2.183	3.721	1.947	2.716
6			5.32		

LAYER	PAY TO X	LAYER Y	CRITICAL DIST	RAY FROM X	LAYER Y
1	0.00	0.00		26.61	0.00
1	.078	.094	.156	26.532	.094
2	.342	.216	.683	26.268	.216
3	.228	.244	.497	26.382	.244
4	.960	.820	1.912	25.727	.770
5	2.716	2.976	5.323	24.219	2.742

E1.44 29.39 RI 4 TO 3 W345
 2.289 .100
 2.556 .160
 2.993 .280
 3.882 .276 .771
 4.794 1.7072.419

RI 4 TO 3 W345S
 N = 6 SPREAD = 29.4

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.093
2	2.289	0	.138
3	2.556	0	.023
4	2.993	0	.771
5	3.882	.276	2.419
6	4.794	1.707	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.093	.093	1.440	.093	.093
2	.231	.138	2.289	.138	.231
3	.254	.023	2.556	.023	.254
4	1.025	.771	2.993	.629	.883
5	3.444	2.419	3.882	1.685	2.562
6			4.78		

LAYER	PAY TO X	LAYER Y	CRITICAL DIST	RAY FROM X	LAYER Y
1	0.00	0.00		29.39	0.00
1	.075	.093	.150	29.315	.093
2	.341	.231	.682	29.049	.231
3	.253	.254	.506	29.137	.254
4	1.105	1.020	2.191	28.464	.888
5	4.436	3.312	8.394	26.281	2.661

51.44 10.86 WAA9A
 1.600 .010 .016
 2.230 .215 .227
 3.020 .520 .520
 4.680 1.255 1.101

WAA9AS

N = 5 SPREAD = 10.9

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.016
2	1.600	0	.227
3	2.230	0	.520
4	3.020	0	1.101
5	4.680	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.016	.016	1.440	.016	.016
2	.243	.227	1.600	.227	.243
3	.763	.520	2.230	.520	.763
4	1.864	1.101	3.020	1.101	1.864
5			4.68		

LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER	
	X	Y		X	Y
	0.00	0.00		10.86	0.00
1	.033	.016	.066	10.927	.016
2	.247	.243	.495	10.613	.243
3	.720	.763	1.440	10.140	.763
4	1.300	1.864	2.599	9.560	1.864

71.44 23.85 WBB9B
 1.600 .010 .016
 2.230 .215 .227
 2.830 .392 .392
 4.240 1.050 .887
 5.630 1.440 .906
 7.070 1.925 1.751

WBB9BS

N = 7 SPREAD = 23.9

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.016
2	1.600	0	.227
3	2.230	0	.392
4	2.830	0	.887
5	4.240	0	.906
6	5.630	0	1.751
7	7.070	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.016	.016	1.440	.016	.016
2	.243	.227	1.600	.227	.243
3	.635	.392	2.230	.392	.635
4	1.522	.887	2.830	.887	1.522
5	2.428	.906	4.240	.906	2.428
6	4.179	1.751	5.630	1.751	4.179
7			7.07		

LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER	
	X	Y		X	Y
	0.00	0.00		23.85	0.00
1	.033	.016	.066	23.817	.016
2	.247	.243	.495	23.603	.243
3	.667	.635	1.333	23.183	.635
4	1.136	1.522	2.271	22.714	1.522
5	1.793	2.428	3.587	22.057	2.428
6	3.558	4.179	7.116	20.292	4.179

71.44 30.6 W1011
 1.650 .030 .044
 2.320 .365 .372
 3.030 .670 .429
 4.100 1.140 .821
 5.610 1.945 .787
 6.910 1.805 .782

W1011S

N = 7 SPREAD = 30.6

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.044
2	1.650	0	.372
3	2.320	0	.429
4	3.030	0	.821
5	4.100	0	.787
6	5.610	0	.782
7	6.910	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.044	.044	1.440	.044	.044
2	.416	.372	1.650	.372	.416
3	.845	.429	2.320	.429	.845
4	1.666	.821	3.030	.821	1.666
5	2.453	.787	4.100	.787	2.453
6	3.235	.782	5.610	.782	3.235
7			6.91		

LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER	
	X	Y		X	Y
	0.00	0.00		30.60	0.00
1	.079	.044	.157	30.521	.044
2	.411	.416	.822	30.189	.416
3	.776	.845	1.552	29.824	.845
4	1.375	1.666	2.750	29.225	1.666
5	1.691	2.453	3.381	28.989	2.453
6	2.322	3.235	4.644	28.279	3.235

71.44 32.4 W1213
 1.650 .030 .044
 2.540 .450 .433
 3.460 .960 .827
 4.000 1.290 .865
 5.980 1.755 .519
 7.140 1.940 .042

W1213S

N = 7 SPREAD = 32.4

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.044
2	1.650	0	.433
3	2.540	0	.827
4	3.460	0	.865
5	4.000	0	.519
6	5.980	0	.042
7	7.140	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.044	.044	1.440	.044	.044
2	.477	.433	1.650	.433	.477
3	1.304	.827	2.540	.827	1.304
4	2.169	.865	3.460	.865	2.169
5	2.688	.519	4.000	.519	2.688
6	2.730	.042	5.980	.042	2.730
7			7.14		

LAYER	RAY TO LAYER		CRITICAL DIST	RAY FROM LAYER	
	X	Y		X	Y
	0.00	0.00		32.40	0.00
1	.079	.044	.157	32.321	.044
2	.400	.477	.801	32.000	.477
3	1.149	1.304	2.298	31.291	1.304
4	2.384	2.169	4.768	30.016	2.169
5	1.604	2.688	3.208	30.796	2.688
6	1.321	2.730	2.648	31.079	2.730

E1.44 29.74 W1617
 1.600 .010 .016
 1.820 .100 .144
 2.440 .300 .308
 3.620 1.025 .908
 6.088 1.745 1.226

W1617S

N = 6 SPREAD = 29.7

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	1.440	0	.016	.016	.016	1.440	.016	.016
2	1.600	0	.144	.160	.144	1.600	.144	.160
3	1.820	0	.308	.468	.308	1.820	.308	.468
4	2.440	0	.908	1.376	.908	2.440	.908	1.376
5	3.620	0	1.226	2.602	1.226	3.620	1.226	2.602
6	6.080	0	6.08					

LAYER	RAY TO LAYER X	RAY TO LAYER Y	CRITICAL DIST	RAY FROM LAYER X	RAY FROM LAYER Y
1	0.00	0.00		29.74	0.00
2	.033	.016	.066	29.707	.016
3	.286	.160	.573	29.454	.160
4	.482	.468	.963	29.258	.468
5	1.086	1.376	2.171	28.654	1.376
6	1.446	2.602	2.892	28.294	2.602

E1.44 26.70 W1819
 1.600 .010 .016
 1.840 .125 .179
 2.320 .465 .430
 3.310 1.205 .975
 5.660 2.310 1.763

W1819S

N = 6 SPREAD = 26.7

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	1.440	0	.016	.016	.016	1.440	.016	.016
2	1.600	0	.179	.195	.179	1.600	.179	.195
3	1.840	0	.430	.625	.430	1.840	.430	.625
4	2.320	0	.975	1.600	.975	2.320	.975	1.600
5	3.310	0	1.763	3.363	1.763	3.310	1.763	3.363
6	5.660	0	5.66					

LAYER	RAY TO LAYER X	RAY TO LAYER Y	CRITICAL DIST	RAY FROM LAYER X	RAY FROM LAYER Y
1	0.00	0.00		26.70	0.00
2	.033	.016	.066	26.667	.016
3	.335	.195	.671	26.365	.195
4	.743	.625	1.486	25.957	.625
5	1.352	1.600	2.704	25.348	1.600
6	1.914	3.363	3.828	24.786	3.363

61.44 22.65 W2021
 1.600 .010 .016
 1.890 .125 .165
 2.350 .490 .509
 3.390 1.105 .741
 5.640 2.075 1.631

W2021S

N = 6 SPREAD = 22.6

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.016
2	1.600	0	.165
3	1.890	0	.509
4	2.350	0	.741
5	3.390	0	1.631
6	5.640	0	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.016	.016	1.440	.016	.016
2	.181	.165	1.600	.165	.181
3	.690	.509	1.890	.509	.690
4	1.431	.741	2.350	.741	1.431
5	3.062	1.631	3.390	1.631	3.062
6			5.64		

LAYER	RAY TO LAYER X	RAY TO LAYER Y	CRITICAL DIST	RAY FROM LAYER X	RAY FROM LAYER Y
1	0.00	0.00		22.65	0.00
1	.033	.016	.066	22.617	.016
2	.281	.181	.562	22.369	.181
3	.855	.690	1.709	21.795	.690
4	1.150	1.431	2.301	21.500	1.431
5	1.782	3.062	3.564	20.868	3.062

61.44 45.77 W22A24B
 1.600 .010 .016
 1.829 +0.17 .266
 2.331 +0.45 .281
 2.906 +0.32 .535
 5.903 -1.031 .100

W22A24BS

N = 6 SPREAD = 45.8

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN
1	1.440	0	.016
2	1.600	0	.266
3	1.829	.170	.281
4	2.331	.450	.535
5	2.906	.320	1.100
6	5.903	-1.030	

N	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	.016	.016	1.440	.016	.016
2	.292	.266	1.600	.130	.146
3	.563	.281	1.829	.057	.204
4	1.098	.535	2.331	.639	.842
5	2.198	1.100	2.906	2.179	3.021
6			5.90		

LAYER	RAY TO LAYER X	RAY TO LAYER Y	CRITICAL DIST	RAY FROM LAYER X	RAY FROM LAYER Y
1	0.00	0.00		45.77	0.00
1	.033	.016	.066	45.737	.016
2	.505	.281	1.003	45.513	.147
3	.633	.558	1.247	45.500	.205
4	1.162	1.092	2.303	44.752	.848
5	.967	2.215	2.014	44.281	2.993

51.44 41.00 W24A229
 1.600 .310 .016
 1.941 -0.17 .148
 3.396 +0.031.160
 5.718 -0.181.870

W24A229S

N = 5 SPREAD = 41.0

N APPARENT DIP LAYER THICKNESS
 VELOCITY AT ORIGIN

1	1.440	0	.016
2	1.600	0	.148
3	1.941	-0.170	1.160
4	3.396	.030	1.870
5	5.718	-0.181	

N DEPTH A THICK A VELOCITY THICK B DEPTH B

1	.016	.016	1.440	.016	.016
2	.164	.148	1.600	.270	.286
3	1.324	1.150	1.941	1.017	1.303
4	3.194	1.870	3.396	2.020	3.323
5			5.72		

LAYER RAY TO LAYER CRITICAL DIST RAY FROM LAYER

	X	Y		X	Y
	0.00	0.00		41.00	0.00
1	.033	.016	.066	40.967	.016
2	.231	.165	.466	40.591	.274
3	.894	1.324	1.786	40.141	1.303
4	1.825	3.290	3.672	39.067	3.317

51.44 32.14 W26A27A
 1.600 .310 .016
 2.130 .270 .307
 2.990 .750 .616
 4.140 1.340 1.013
 5.280 1.735 .866

W26A27AS

N = 5 SPREAD = 32.1

N APPARENT DIP LAYER THICKNESS
 VELOCITY AT ORIGIN

1	1.440	0	.016
2	1.600	0	.307
3	2.130	0	.616
4	2.990	0	1.013
5	4.140	0	.866
6	5.280	0	

N DEPTH A THICK A VELOCITY THICK B DEPTH B

1	.016	.016	1.440	.016	.016
2	.323	.307	1.600	.307	.323
3	.939	.616	2.130	.616	.939
4	1.952	1.013	2.990	1.013	1.952
5	2.818	.866	4.140	.866	2.818
6			5.28		

LAYER RAY TO LAYER CRITICAL DIST RAY FROM LAYER

	X	Y		X	Y
	0.00	0.00		32.14	0.00
1	.033	.016	.066	32.107	.016
2	.364	.323	.728	31.776	.323
3	.829	.939	1.657	31.311	.939
4	1.562	1.952	3.124	30.579	1.952
5	2.164	2.818	4.328	29.976	2.818

61.44 34.44 W268278
 1.600 .010 .016
 2.100 .360 .424
 3.430 1.060 .757
 4.430 1.959 .959
 6.880 2.830 3.243

W268278S

N = 6 SPREAD = 34.4

N	APPARENT VELOCITY	DIP	LAYER THICKNESS AT ORIGIN	DEPTH A	THICK A	VELOCITY	THICK B	DEPTH B
1	1.440	0	.016	.016	.016	1.440	.016	.016
2	1.600	0	.424	.440	.440	1.600	.424	.440
3	2.100	0	.757	1.197	1.197	2.100	.757	1.197
4	3.430	0	.959	2.156	2.156	3.430	.959	2.156
5	4.430	0	3.243	5.399	5.399	4.430	3.243	5.399
6	6.880	0	6.88					

LAYER	RAY TO LAYER X	RAY TO LAYER Y	CRITICAL DIST	RAY FROM LAYER X	RAY FROM LAYER Y
1	0.00	0.00		34.44	0.00
1	.033	.016	.066	34.407	.016
2	.514	.440	1.028	33.926	.440
3	.817	1.197	1.634	33.623	1.197
4	1.751	2.156	3.501	32.609	2.156
5	3.628	5.399	7.256	30.812	5.399

VI

PROGRAM TO COMPUTE CORRECTIONS TO
HELICOPTER-RECORDED DATA (BEAUHELI)
AND INPUT AND OUTPUT DATA FOR PROCESSED LINES

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PROGRAM PEAUHETI
PI=3.1415926536
DTR=PI/180.
RTD=180./PI
READ(5,100)AID1,AID2
100 FORMAT(2A8)
READ(5,105)IYRMO1,IDA1,IHR1,MIN1,DIF1,IYRMO2,
1 IDA2,IHR2,MIN2,DIF2
IF(IYRMO1.NE.IYRMO2)GO TO 5
105 FORMAT(2(I4,I2,X,2I2,X,F6.2))
GO TO 10
5 WRITE(6,110)IYRMO1,IYRMO2
110 FORMAT(2 CLOCK CORR YR #,I4,# DIFFERS FROM YR #,I4)
CALL EXIT
10 TIM1=IDA1*86200+IHR1*3600+MIN1*60
TIM2=IDA2*86200+IHR2*3600+MIN2*60
READ(5,115)ISBYN,ISBD,ISBH,ISBP,ISBN,ISBP
115 FORMAT(I4,I2,X,2I2,X,2I2)
SBTIM=ISBD*86200+ISBH*3600+ISBP*60
READ(5,120)CLK,SLK,WATVELK,DBE,DBE,TDIST,DR,DBR
120 FORMAT(8F8.3)
WRITE(6,125)AID1,AID2
125 FORMAT(2 #,2A8)
WRITE(6,130)IYRMO1,IDA1,IHR1,MIN1,DIF1
130 FORMAT(2 PRESHOT TIME CHECK #,I4,I2,X,2I2,# DELTA T= #,
1 F7.3)
WRITE(6,135)IYRMO2,IDA2,IHR2,MIN2,DIF2
135 FORMAT(2 POSTSHOT TIME CHECK #,I4,I2,X,2I2,
1 # DELTA T= #,F7.3)
WRITE(6,140)
140 FORMAT(2 ALL DISTANCES IN KILOMETERS, ALL VELOCITIES #,
1 # IN KM/SEC, ALL TIMES ARE UNIVERSAL TIME#)
WRITE(6,145)CLK,SLK,WATVELK
145 FORMAT(2 CARLE LENGTH= #,F8.3,# ACTIVE SECTION #,
1 # LENGTH= #,F8.3,# WATER VELOCITY= #,F8.3)
WRITE(6,147)DBE,DBE,TDIST,DR,DBR
147 FORMAT(2 START DEPTH= #,
1 F8.3,# END DEPTH= #,F8.3,# LINE LENGTH= #,F8.3,
2 # RECEIVER DEPTH= #,F8.3,# DEPTH AT RECEIVER= #,F8.3)
READ(4,150)NYRMO1,NDA1,NHR1,NMN1,NLAT1,ALATM1,NLON1,ALCNM1
150 FORMAT(I4,I2,X,2I2,X,I3,X,F5.2,X,I4,X,F5.2)
ANTIM1=(NLAT1+ALATM1/60.)*DTR
ALON1=(NLON1-ALONM1/60.)*DTR
KIT=0
15 READ(4,150)NYRMO2,NDA2,NHR2,NMN2,NLAT2,ALATM2,NLON2,ALCNM2
ANTIM2=(NLAT2+ALATM2/60.)*DTR
ALON2=(NLON2-ALONM2/60.)*DTR
IF(KIT.EQ.1) GO TO 20
IF(SBTIM.GE.ANTIM1.AND.SBTIM.LE.ANTIM2) GO TO 20
ANTIM1=ANTIM2
ALAT1=ALAT2
ALON1=ALON2
GO TO 15
20 FACTOR=(SBTIM-ANTIM1)/(ANTIM2-ANTIM1)
SBLON=(ALON2-ALON1)*FACTOR+ALON1
SBLAT=(ALAT2-ALAT1)*FACTOR+ALAT1
SBL0P=SBLON*RTD
SBLAP=SBLAT*RTD
WRITE(6,155)ISBN,ISBP,ISBYN,ISBD,ISBH,ISBM,SELAP,SBL0P
155 FORMAT(2 SONOBUOY #,I2,# AT POSITION #,I2,

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1 * TIME #,I4,I2,X,2I2,* LAT #,F7.3,* LONG #,F8.3)
WRITE(6,160)
160 FORMAT(=0YRMODEA SHOT LATITUDE LONGITUDE SIZE BURN #,
1 * DEPTH SDIST CADIS TRAVI TTRAW SURF BOTC #,
2 #CLKC SCOR SHOTTIME SPVEL SPVELC#)
KIT=1
25 READ(5,165) ISHOT,SIZE,BURN,DEPK,DIST,KSYM,KSDA,
1 KSHR,KSMN,SSEC,KHHR,KHMN,HSEC,SPVEL
IF(EOF(5)) CALL EXIT
165 FORMAT(I5,4F5.2,X,I4,I2,X,2I2,X,F5.2,X,2I2,X,F5.2,X,F6.5)
SHORTIM=KSDA*66200+KSHR*3600+KSMN*60+SSEC-BURN
28 IF(SHORTIM.GE.ANTIM1.AND.SHORTIM.LT.ANTIM2)GO TO 30
ANTIM1=ANTIM2
ALAT1=ALAT2
ALON1=ALON2
GO TO 15
30 FACTOR=(SHORTIM-ANTIM1)/(ANTIM2-ANTIM1)
SHLON=(ALON2-ALON1)*FACTOR+ALON1
SHLAT=(ALAT2-ALAT1)*FACTOR+ALAT1
ARG=SINF(ALAT1)*SINF(ALAT2)+
1 COSF(ALAT1)*COSF(ALAT2)*COSF(ALON2-ALON1)
PDIST=6359.059*ACOSF(ARG)
ARG=SINF(SBLAT)*SINF(SHLAT)+
1 COSF(SBLAT)*COSF(SHLAT)*COSF(SHLON-SBLON)
SDIST=6359.059*ACOSF(ARG)
SPVELC=PDIST/(ANTI2-ANTI1)
SHOTX=SPVEL*BURN-SLK-CLK
SHOTZ=(-40.95+1.513*BURN)/1000.
IF(SHOTZ.GT.0)SHOTZ=DEPK
SHCOR=SQRT(SHOTX*SHOTX+SHOTZ*SHOTZ)/WATVELK
STIMC=SSEC-SHGOR
SHTIMC=SHORTIM+BURN-SHGOR
CKCOR=DIF1+(DIF2-DYF1)*(SHCRTIP-TIM1)/(TIM2-TIM1)
ARTIMH=KSDA*66200+KHHR*3600+KHMN*60+HSEC+CKCOR
TTRAW=ARTIMH-SHTIMC
TDEP=DBB+(DBE-DBR)*DIST/TDIST
S1=SQRT(1.-WATVELK*WATVELK/5./5.)
SURFCOR=(DR+SHOTZ)*S1/WATVELK
BOTCOR=(TDEP-DEPK+DBE-CBR)*S1/WATVELK
TTCOR=TTRAW+SURFCOR+BOTCOR
SHLON=SHLON*PTD
LLON=SHLON
ALONM=-(SHLON-LLON)*60.
SHLAT=SHLAT*PTD
LLAT=SHLAT
ALATM=(SHLAT-LLAT)*60.
WRITE(6,170)KSYM,KSDA,ISHOT,LLAT,ALATM,LLON,ALONM,
1 SIZE,BURN,DEPK,SDIST,DIST,TTCOR,TTRAW,SURFCOR,BOTCOR,
2 CKCOR,SHCOR,KSHR,KSMN,STIMC,SPVEL,SPVELC
WRITE(7,175)KSYM,KSDA,ISHOT,LLAT,ALATM,LLON,ALONM,
1 SIZE,BURN,DEPK,SDIST,DIST,TTCOR,TTRAW,SURFCOR,BOTCOR,
2 CKCOR,SHCOR,KSHR,KSMN,STIMC,SPVEL,SPVELC
170 FORMAT(= #,I4,I2,X,I4,X,I3,X,F5.2,X,I4,X,F5.2,X,F5.1,F5.1,
1 F6.3,4F6.2,4F5.2,X,2I2,F6.2,2F7.5)
175 FORMAT(I4,I2,X,I4,X,I3,X,F5.2,X,I4,X,F5.2,X,F5.1,F6.1,
1 F6.3,4F6.2,4F5.2,X,2I2,F6.2,2F7.5)
GO TO 25
END

```

DATA INPUT FORMAT FOR PROGRAM BEAURELL

AID1	AID2	IYPM01	IYPM02	DA2	HR2	MIN2	DIF2	DBE	DBR
ISBH	ISBU	ISBH	ISBN	ISBN	ISBN	ISBN	ISBN	ISBN	ISBN
CLK	SLK	WATVELK	DBB	KSYM	SDA	KSHR	KSHN	DR	SPVEL
TSHOT	SIZE	DEPK	DIST	SSEC	HSEC				

AID1, AID2 : Line Identification.

IYPM01, IDA1, IHRI, MIN1: Year, month, day, hour and minute of the preshot time check.

IYPM02, IDA2, IHR2, MIN2: Year, month, day, hour and minute of the postshot time check.

DIF1 : Clock correction (Time difference between the ship's master clock and the helicopter's clock) of preshot time check.

DIF2 : Clock correction of postshot time check.

ISBYM, ISBU, ISBH, ISBN : Year, month, day, hour and minute of the sonobuoy's drop.

ISBN : Sonobuoy number.

ISBP : Sonobuoy position.

CLK : Cable length in kilometers.

SLK : Streamer length (active section only) in kilometers.

WATVELK : Water velocity.

DBB : Depth to the bottom at the beginning of the line.

DBE : Depth to the bottom at the end of the line.

TDIST : End to end spread length (Total distance).

DR : Depth of the receiver (Hydrophone depth).

DBR : Depth to bottom at the receiver (Offset depth based on some average basement velocity).

ISHOT : Shot number.

SIZE : Size of the shot in pounds.

BURN : Burn time.

DEPK : Depth to the bottom at the shot point in kilometers (Offset depth).

DIST : Estimated drift distance between shot and sonobuoy computed manually.

KSYM, KSDA, KSHR, KSHN, SSEC : Year, month, day, hour, minute and second of the shot.

KSHR, KSHN, HSEC : Hour, minute and second of the helicopter ground arrival.

SPVEL : Ship velocity.

NAVIGATION INPUT FORMAT FOR PROGRAM BEAUNELI

TITLE(I)							
NYRMOI	NDAI	NHRI	MMNI	NLATI	ALATMI	NLONI	ALONMI
.
.
NYRMOK	NDAK	NHRK	MMNK	NLATK	ALATMK	NLONK	ALONMK

TITLE(I) : Line identification.
 K : Number of ship's navigation points for the profile.
 I=1,.....,K : Ship's navigation points number.
 NYRMO(I) }
 NDA(I) } : Year, month, day, hour and minute of navigation points.
 NHR(I) }
 MMNI(I) }
 NLAT(I) } : Position in latitude (degrees and minutes) of the ship's navigation points.
 ALATMI(I) }
 NLON(I) } : Position in longitude (degrees and minutes) of the ship's navigation points.
 ALONMI(I) }

OUTPUT FORMAT FOR PROGRAM BEAUHELI

SBLAP,SBLOP : Sonubuy position in latitude and longitude.
KSYM,KSDA : Year,month and day of the shot.
LLAT,ALATM : Shot position in latitude (degrees and minutes).
LLON,ALONM : Shot position in longitude (degrees and minutes).
SDIST : Corrected distance between shot and sonubuy computed mathematically.
TTCOR : Corrected travel time including all corrections.
TTRAW : Travel time including shot and clock corrections but without any bottom or surface corrections.
SURFCOR : Surface correction.
BOTCOR : Bottom correction.
CLKCOR : Clock correction between ship and helicopter.
SHCOR : Total corrections for shot time.
KSHR,KSVM,STIME : Corrected shot time in hours,minutes and seconds.
SPVEL : Ship velocity.
SPVELC : Corrected ship velocity.
A1D1,A1D2,IYMMO1,IDA1,IHRT,MINT,IYMMO2,IDA2,IHR2,MIN2,DIF1,DIF2,JSBYM,JSB0,JSBH,JSBM,JSBP,CLK,SLK,MATVELK,DBB,
URE,TDIST,DR,DBR,ISHOT,SIZE,BURN,DEPK,DIST: All the same as in input file.

BEAU76 LINE 22A-23 HELICOPTER
 760817 0350 0.018 760817 1023 0.022
 760817 0500 522
 0.061 0.00457 1.440 0.019 0.014 70. 0.0163 0.020
 341 120.135.0 -0.20 37.6 760817 0730 55.61 0739 03.07 -0.0474
 342 120.135.0 -0.20 39.0 760817 0743 49.52 0743 58.07 -0.0474
 343 120.190.0 -0.20 42.2 760817 0754 51.11 0754 59.35 -0.0474
 344 240.192.3 -0.20 44.6 760817 0802 27.99 0802 36.84 -0.0474
 345 240.190.3 -0.20 45.6 760817 0807 46.29 0808 55.34 -0.0474
 346 240.192.9 -0.20 47.1 760817 0816 51.50 0817 00.75 -0.0474
 347 240.188.5 -0.20 48.5 760817 0825 03.07 0825 12.71 -0.0474
 348 360.265.7 -0.20 50.8 760817 0836 19.83 0836 29.79 -0.0474
 349 480.348.0 -0.19 54.4 760817 0852 00.14 0852 10.24 -0.0474
 350 480.199.8 -0.19 59.3 760817 0907 28.15 0907 39.70 -0.0474
 351 600.192.9 -0.20 69.0 760817 0932 22.44 0932 35.40 -0.0474

BEAU76 NAV22
 763817 0500 71 00.18 -152 00.20
 760817 0520 70 59.18 -151 56.48
 760817 0540 70 57.90 -151 47.10
 760817 0600 70 56.68 -151 38.20
 760817 0620 70 56.10 -151 27.70
 760817 0640 70 55.30 -151 17.70
 760817 0700 70 53.90 -151 08.30
 760817 0720 70 53.90 -151 08.30
 760817 0740 70 52.90 -151 00.40
 760817 0800 70 51.40 -150 58.70
 760817 0820 70 47.20 -150 58.00
 760817 0850 70 45.00 -150 42.00
 760817 0908 70 44.00 -150 39.00
 760817 0926 70 42.50 -150 24.50
 760817 0938 70 39.59 -150 12.70

PEAU76 HELI22
 PPESHOT TIME CHECK 760817 350 DELTA I = -0.18
 POSTSHOT TIME CHECK 760817 1023 DELTA I = -0.22
 ALL DISTANCES IN KILOMETERS, ALL VELOCITIES IN KM/SEC, ALL TIMES ARE UNIVERSAL TIME
 CABLE LENGTH= .061 ACTIVE SECTION LENGTH= .005 WATER VELOCITY= 1.440
 START DEPTH= .019 END DEPTH= .019 LINE LENGTH= 70.000 RECEIVER DEPTH= .018 DEPTH AT RECEIVER= .020
 SONARUOV 5 AT POSITION 22 TIME 760817 5 0 LAT 71.082 LONG -152.083
 WPMODA SHOT LATITUDE LONGITUDE SIZE BURM DEPTH SDIST CADIS TRAVT VFRAM SURF BOTC CLKC SCOR SHOTTIME SPVEL SPWELC
 760817 341 70 53.07 -151 1.71 120.0 135.0 -0.20 37.64 37.60 7.90 7.00 -0.3-0.00 -0.2 40 738 55.21 -0.0474 -0.0427
 760817 342 70 52.81 -150 59.64 120.0 135.0 -0.20 38.99 39.00 7.99 7.97 -0.3-0.00 -0.2 40 743 49.12 -0.0474 -0.0518
 760817 343 70 52.26 -150 54.73 120.0 190.0 -0.20 42.13 42.28 8.06 8.04 -0.3-0.01 -0.2 58 754 50.53 -0.0474 -0.0518
 760817 344 70 51.84 -150 51.06 240.0 192.3 -0.20 44.49 44.60 9.46 9.46 -0.3-0.00 -0.2 59 8 2 27.40 -0.0474 -0.0518
 760817 345 70 50.51 -150 50.50 240.0 190.3 -0.20 45.72 45.68 9.67 9.65 -0.3-0.00 -0.2 58 8 8 45.71 -0.0474 -0.0710
 760817 346 70 48.66 -150 50.22 240.0 192.9 -0.20 47.33 47.18 9.88 9.86 -0.3-0.00 -0.2 59 816 50.91 -0.0474 -0.0710
 760817 347 70 47.06 -150 49.49 240.0 188.5 -0.20 49.14 48.58 10.26 10.23 -0.3-0.00 -0.2 58 825 2.49 -0.0474 -0.0353
 760817 348 70 46.33 -150 46.83 360.0 265.7 -0.20 51.22 50.90 10.03 10.01 -0.3-0.01 -0.2 63 836 19.00 -0.0474 -0.0353
 760817 349 70 45.27 -150 42.98 480.0 348.0 -0.20 54.24 54.40 11.22 11.19 -0.2-0.00 -0.2 61 852 -0.93 -0.0474 -0.0353
 760817 350 70 43.76 -150 36.69 480.0 199.8 -0.20 58.97 59.38 12.21 12.18 -0.2-0.00 -0.2 61 9 7 27.54 -0.0474 -0.0353
 760817 351 70 41.73 -150 21.39 600.0 192.9 -0.20 68.91 69.00 13.59 13.57 -0.3-0.00 -0.2 59 932 21.85 -0.0474 -0.1251

BEAU76 LINE 24A-25 HELICOPTER
 760017 1023 0.022 760010 1400 0.04
 760010 0306 1624
 0.061 0.00857 1.440 0.017 70. 0.0103 0.016
 362 120.136.7 -0.1024.67 760010 0515 22.89 0519 30.34 -00402
 363 120.138.5 -0.1030.45 760010 0523 24.13 0523 31.56 -00402
 364 120.138.2 -0.1032.00 760010 0527 54.00 0528 01.61 -00402
 365 240.163.0 -0.1035.90 760010 0537 53.86 0539 02.04 -00402
 366 240.192.1 -0.1039.35 760010 0549 50.02 0550 06.57 -00402
 367 240.192.3 -0.1041.00 760010 0558 18.60 0558 27.05 -00402
 368 240.182.7 -0.1044.50 760010 0607 00.62 0607 10.37 -00402
 369 360.208.4 -0.1049.00 760010 0620 34.93 0620 44.99 -00402
 390 360.210.0 -0.1052.35 760010 0633 51.94 0634 02.29 -00402
 391 480.211.2 -0.1057.80 760010 0650 39.94 0650 51.29 -00402
 392 480.217.8 -0.1062.95 760010 0709 54.03 0710 06.24 -00402
 393 660.213.0 -0.1068.55 760010 0726 46.00 0726 59.25 -00402

BEAU76 HELI24
 PRESOT TIME CHECK 760017 1023 DELTA T = .022
 POSTSHOT TIME CHECK 760010 14 0 DELTA T = .040
 ALL DISTANCES IN KILOMETERS. ALL VELOCITIES IN KM/SEC. ALL TIMES ARE UNIVERSAL TIME
 CABLE LENGTH= .061 ACTIVE SECTION LENGTH= .017 LINE LENGTH= 78.000 RECEIVER DEPTH= 1.440
 START DEPTH= .017 END DEPTH= .017 LINE LENGTH= 78.679 LONG -150.056
 SONOBUOY 16 AT POSITION 24 TIME 760010 3 6 LAT 78.679 LONG -150.056
 YRMODEA SHOT LATITUDE LONGITUDE SIZE BUHM NDEPTH SDIST CADIS TRAWT TTRAW SURF BOTC CLKGC SCOR SHOTTIME SPVEL SPWELC
 760010 302 70 48.77 -150 51.71 120.0 136.7 -0.10 38.04 28.67 7.72 7.70 -02-00-00 -03 .41 519 22.48 -00402 -00267
 760010 303 70 49.01 -150 52.75 120.0 130.5 -0.10 33.01 30.45 7.91 7.88 -02-00-00 -03 .42 523 23.71 -00402 -00700
 760010 304 70 49.06 -150 55.86 120.0 130.2 -0.10 35.54 32.00 8.09 8.06 -02-00-00 -03 .42 527 53.58 -00402 -00700
 760010 305 70 49.16 -151 3.16 240.0 163.0 -0.10 39.68 35.90 8.74 8.71 -02-00-00 -03 .50 530 53.36 -00402 -00700
 760010 306 70 49.67 -151 A.91 240.0 192.1 -0.10 43.27 39.35 9.21 9.18 -02-00-00 -03 .60 549 57.42 -00402 -00513
 760010 307 70 50.26 -151 12.75 240.0 192.3 -0.10 45.83 41.80 9.71 9.68 -02-00-00 -03 .60 558 10.00 -00402 -00513
 760010 308 70 51.01 -151 16.95 240.0 182.7 -0.10 46.72 44.50 10.16 10.15 -02-00-00 -03 .57 6.7 8.25 -00402 -00571
 760010 309 70 52.31 -151 23.13 360.0 200.4 -0.10 53.11 49.00 10.77 10.75 -02-00-00 -03 .65 620 34.28 -00402 -00571
 760010 310 70 53.33 -151 24.91 360.0 210.0 -0.10 57.06 52.35 11.07 11.04 -02-00-00 -04 .66 633 51.20 -00402 -00480
 760010 311 70 54.00 -151 36.93 480.0 211.2 -0.17 62.02 57.00 12.07 12.05 -02 .00 .04 .66 658 39.20 -00402 -00555
 760010 312 70 54.50 -151 47.45 480.0 217.8 -0.16 68.20 62.95 12.95 12.93 -02 .00 .04 .68 7.9 53.35 -00402 -00607
 760010 313 70 55.79 -151 57.09 660.0 213.0 -0.15 74.57 68.55 13.99 13.96 -02 .00 .04 .67 726 45.33 -00402 -00679

BEAU76 NAV24

760010 0300 70 40.35 -150 00.20
 760010 0320 70 41.60 -150 10.70
 760010 0340 70 42.60 -150 20.20
 760010 0400 70 44.20 -150 29.00
 760010 0420 70 45.00 -150 39.20
 760010 0440 70 47.50 -150 48.00
 760010 0500 70 47.40 -150 50.00
 760010 0520 70 49.00 -150 52.00
 760010 0540 70 49.20 -151 05.00
 760010 0600 70 50.60 -151 15.00
 760010 0620 70 52.60 -151 24.50
 760010 0640 70 54.00 -151 33.00
 760010 0700 70 54.00 -151 44.00
 760010 0720 70 55.50 -151 55.00
 760010 0740 70 56.70 -152 00.00

BEAU76 HELI24

BEAU76 HELI24
 PRESOT TIME CHECK 760017 1023 DELTA T = .022
 POSTSHOT TIME CHECK 760010 14 0 DELTA T = .040
 ALL DISTANCES IN KILOMETERS. ALL VELOCITIES IN KM/SEC. ALL TIMES ARE UNIVERSAL TIME
 CABLE LENGTH= .061 ACTIVE SECTION LENGTH= .017 LINE LENGTH= 78.000 RECEIVER DEPTH= 1.440
 START DEPTH= .017 END DEPTH= .017 LINE LENGTH= 78.679 LONG -150.056
 SONOBUOY 16 AT POSITION 24 TIME 760010 3 6 LAT 78.679 LONG -150.056
 YRMODEA SHOT LATITUDE LONGITUDE SIZE BUHM NDEPTH SDIST CADIS TRAWT TTRAW SURF BOTC CLKGC SCOR SHOTTIME SPVEL SPWELC
 760010 302 70 48.77 -150 51.71 120.0 136.7 -0.10 38.04 28.67 7.72 7.70 -02-00-00 -03 .41 519 22.48 -00402 -00267
 760010 303 70 49.01 -150 52.75 120.0 130.5 -0.10 33.01 30.45 7.91 7.88 -02-00-00 -03 .42 523 23.71 -00402 -00700
 760010 304 70 49.06 -150 55.86 120.0 130.2 -0.10 35.54 32.00 8.09 8.06 -02-00-00 -03 .42 527 53.58 -00402 -00700
 760010 305 70 49.16 -151 3.16 240.0 163.0 -0.10 39.68 35.90 8.74 8.71 -02-00-00 -03 .50 530 53.36 -00402 -00700
 760010 306 70 49.67 -151 A.91 240.0 192.1 -0.10 43.27 39.35 9.21 9.18 -02-00-00 -03 .60 549 57.42 -00402 -00513
 760010 307 70 50.26 -151 12.75 240.0 192.3 -0.10 45.83 41.80 9.71 9.68 -02-00-00 -03 .60 558 10.00 -00402 -00513
 760010 308 70 51.01 -151 16.95 240.0 182.7 -0.10 46.72 44.50 10.16 10.15 -02-00-00 -03 .57 6.7 8.25 -00402 -00571
 760010 309 70 52.31 -151 23.13 360.0 200.4 -0.10 53.11 49.00 10.77 10.75 -02-00-00 -03 .65 620 34.28 -00402 -00571
 760010 310 70 53.33 -151 24.91 360.0 210.0 -0.10 57.06 52.35 11.07 11.04 -02-00-00 -04 .66 633 51.20 -00402 -00480
 760010 311 70 54.00 -151 36.93 480.0 211.2 -0.17 62.02 57.00 12.07 12.05 -02 .00 .04 .66 658 39.20 -00402 -00555
 760010 312 70 54.50 -151 47.45 480.0 217.8 -0.16 68.20 62.95 12.95 12.93 -02 .00 .04 .68 7.9 53.35 -00402 -00607
 760010 313 70 55.79 -151 57.09 660.0 213.0 -0.15 74.57 68.55 13.99 13.96 -02 .00 .04 .67 726 45.33 -00402 -00679

VII
RECORD SECTIONS AND
STRUCTURAL CROSS-SECTIONS

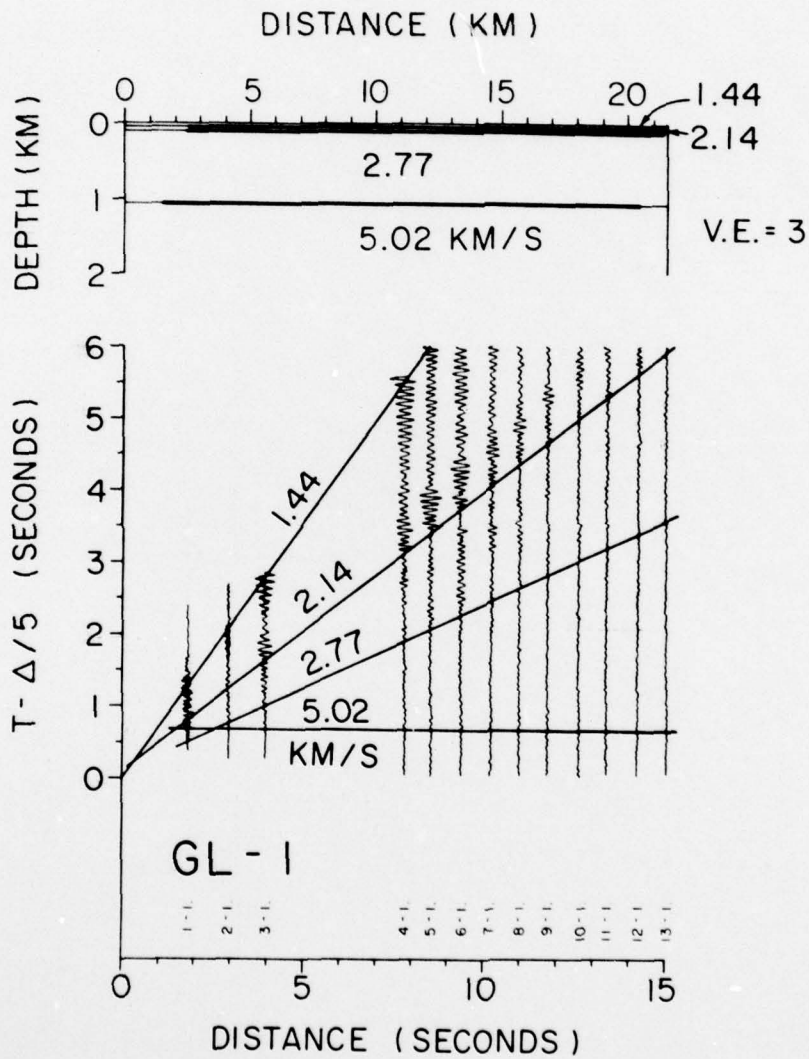


Figure 8. Line GL-1 record section and velocity-depth model interpretation. Below each seismogram is listed the shot number and the charge weight in pounds.

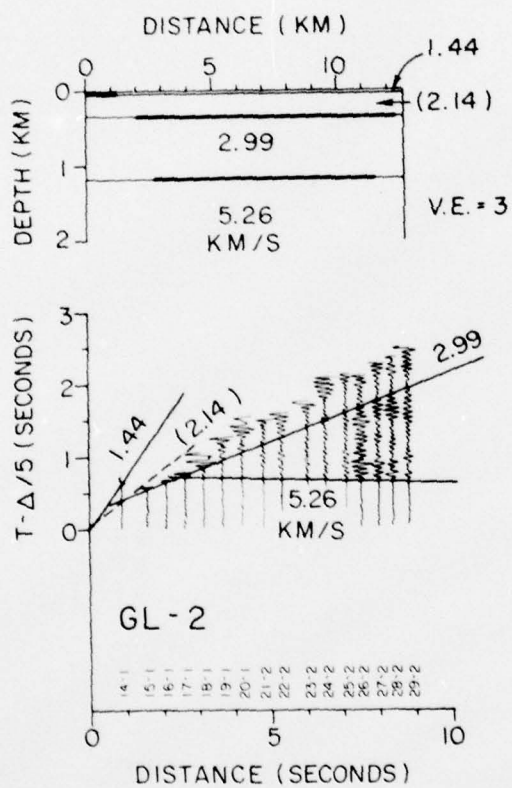


Figure 9. Line GL-2 record section and velocity-depth model interpretation.

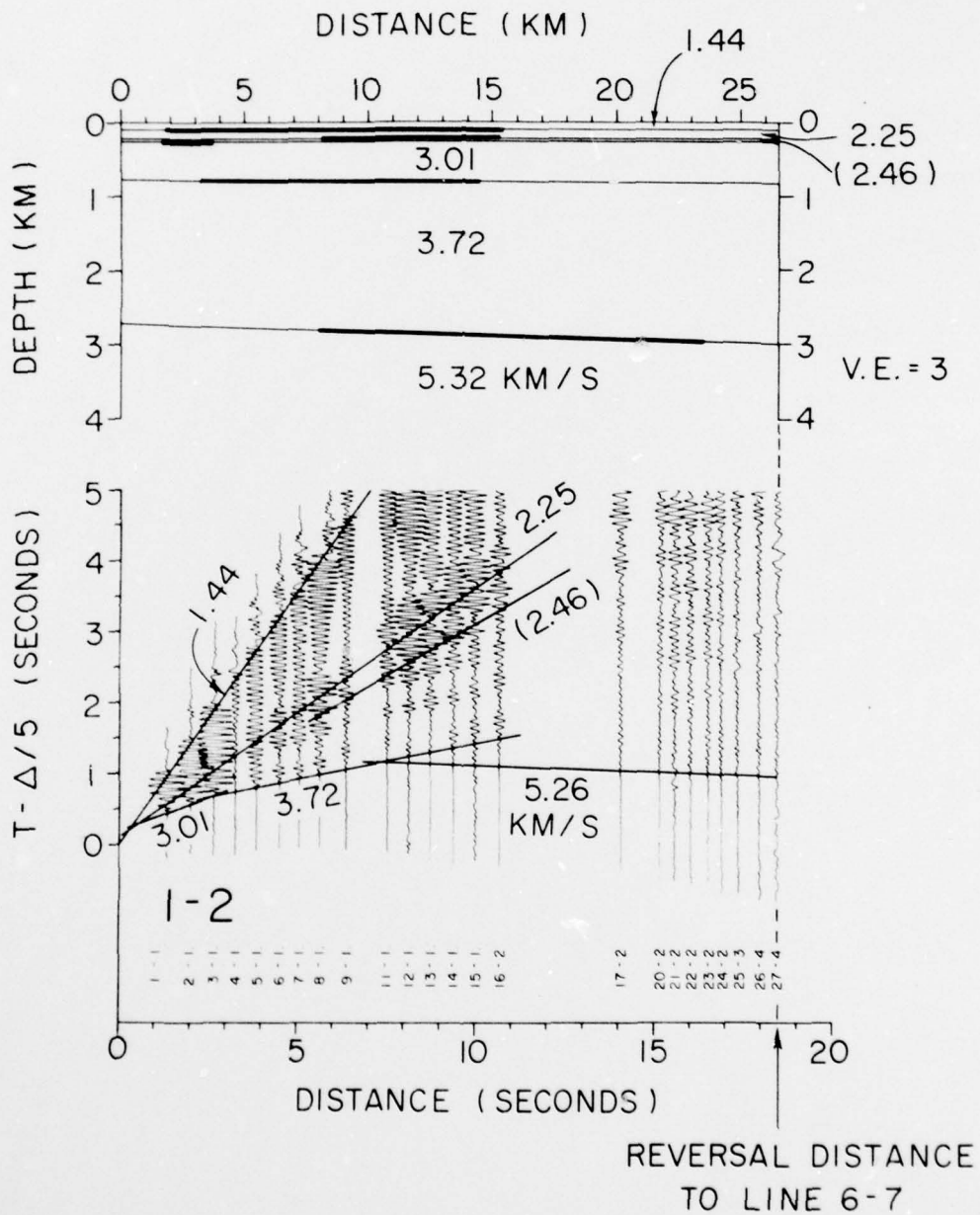


Figure 10. Line 1-2 record section and velocity-depth model interpretation.

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MARINE SEISMIC REFRACTION DATA BETWEEN WAINWRIGHT INLET AND PRU--ETC(U)

JUN 79 M BEE, S H JOHNSON, E F CHIBURIS

N00014-76-C-0067

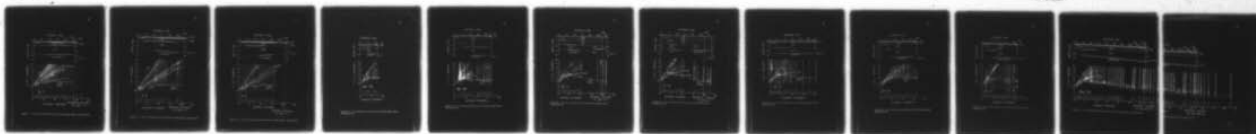
UNCLASSIFIED

79-9

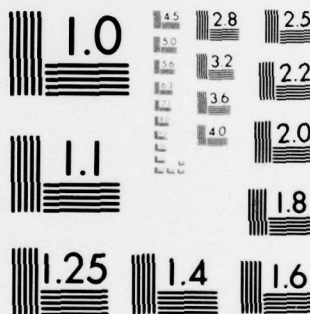
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2 OF 2

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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

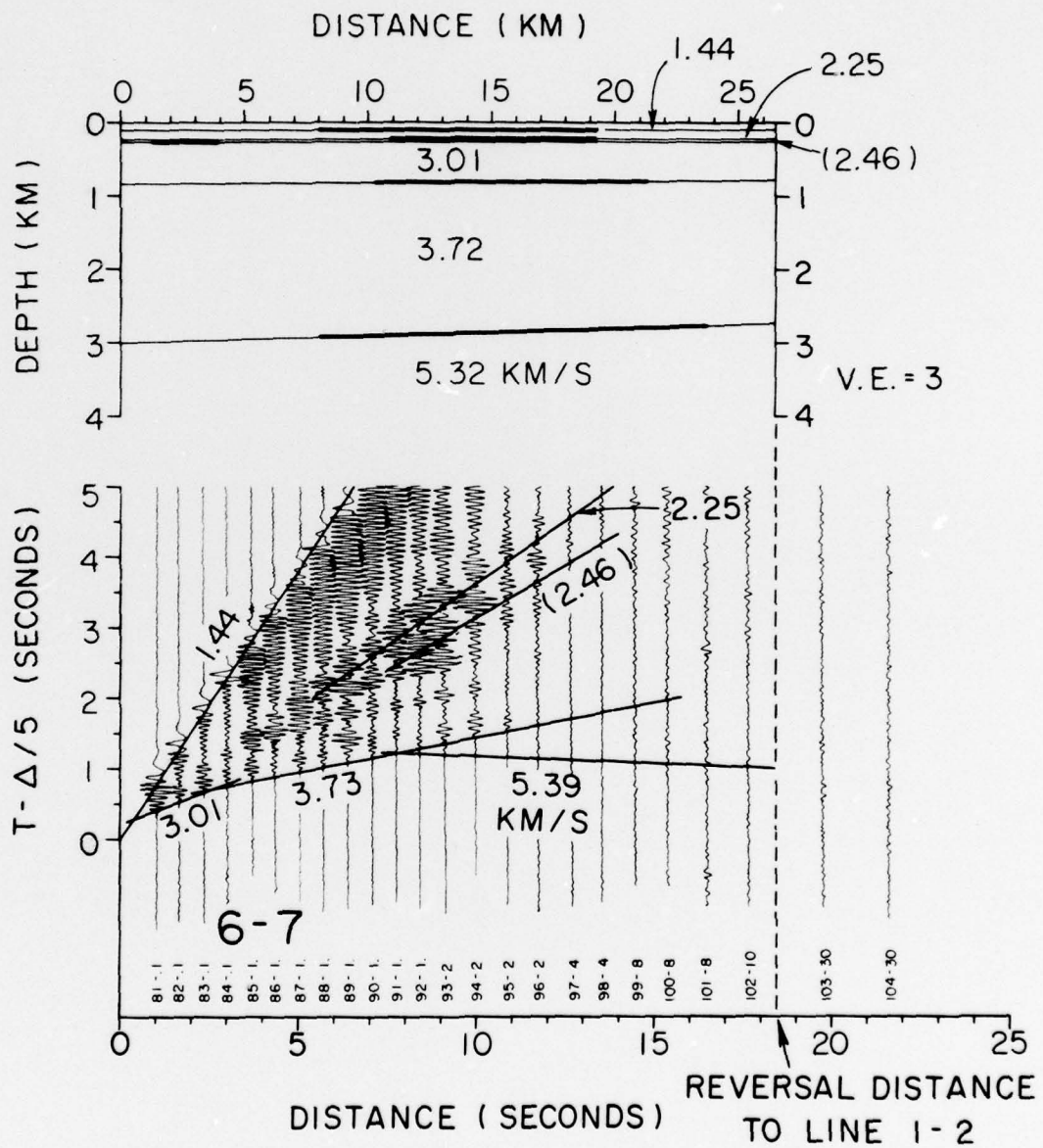


Figure 11. Line 6-7 record section and velocity-depth model interpretation.

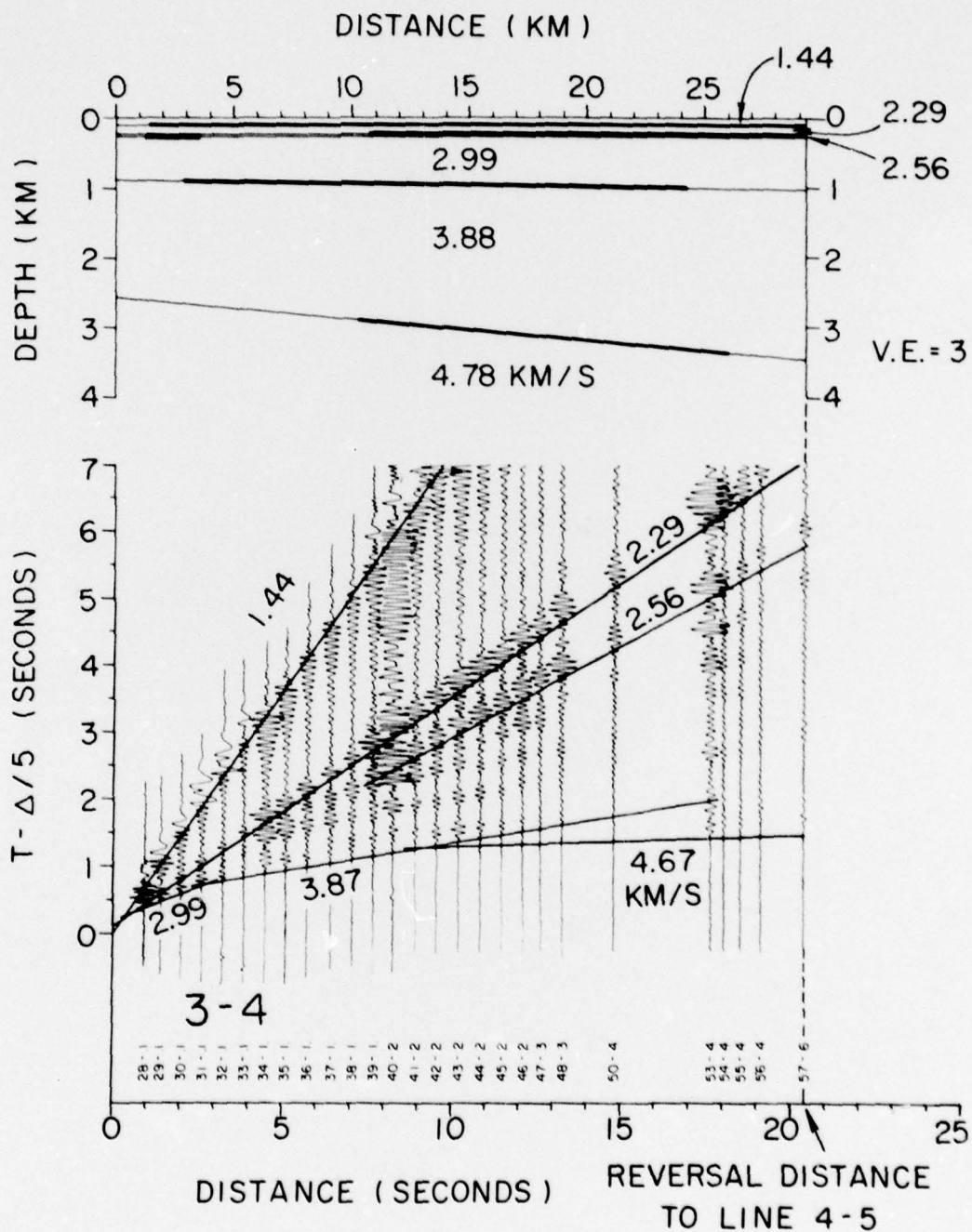


Figure 12. Line 3-4 record section and velocity-depth model interpretation.

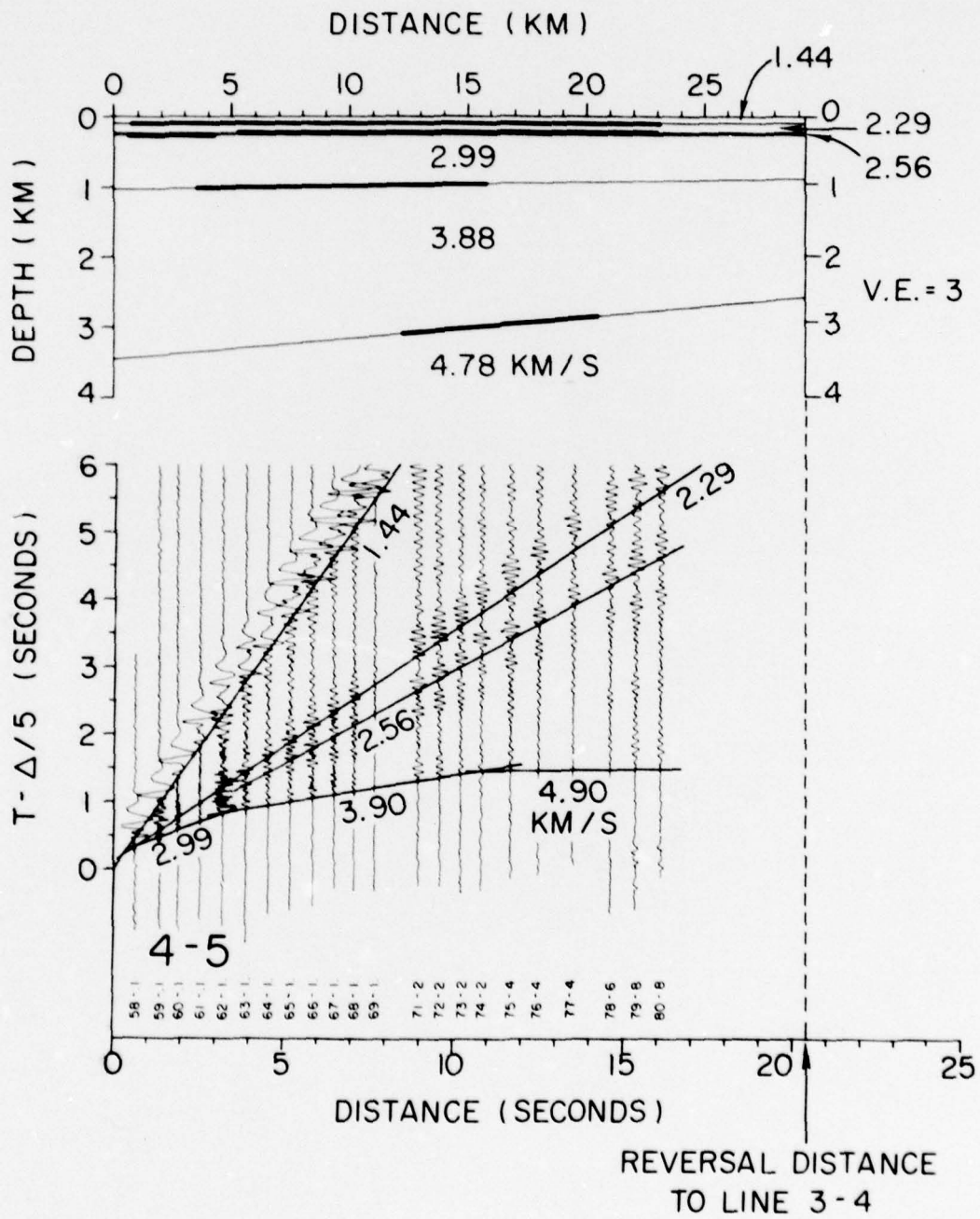


Figure 13. Line 4-5 record section and velocity-depth model interpretation.

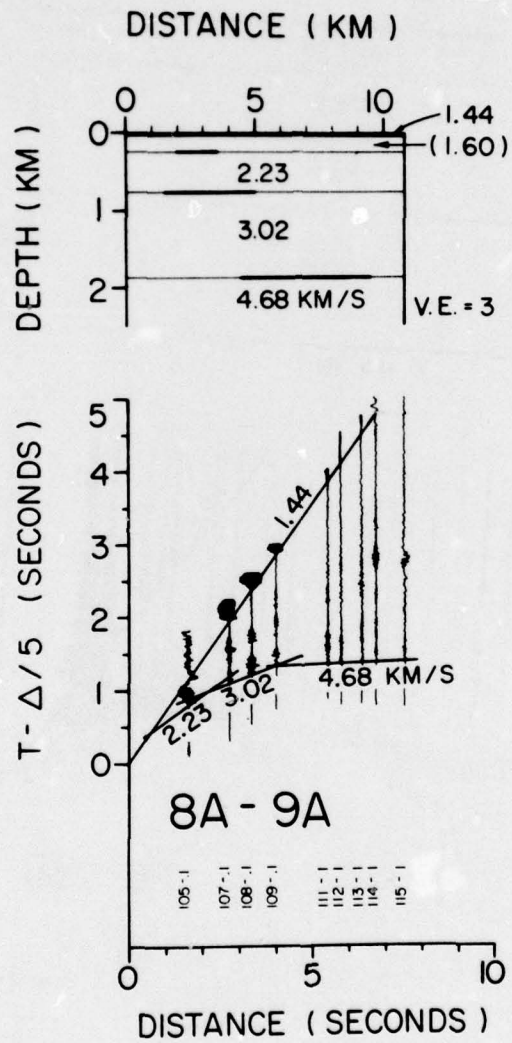


Figure 14. Line 8A-9A record section and velocity-depth model interpretation.

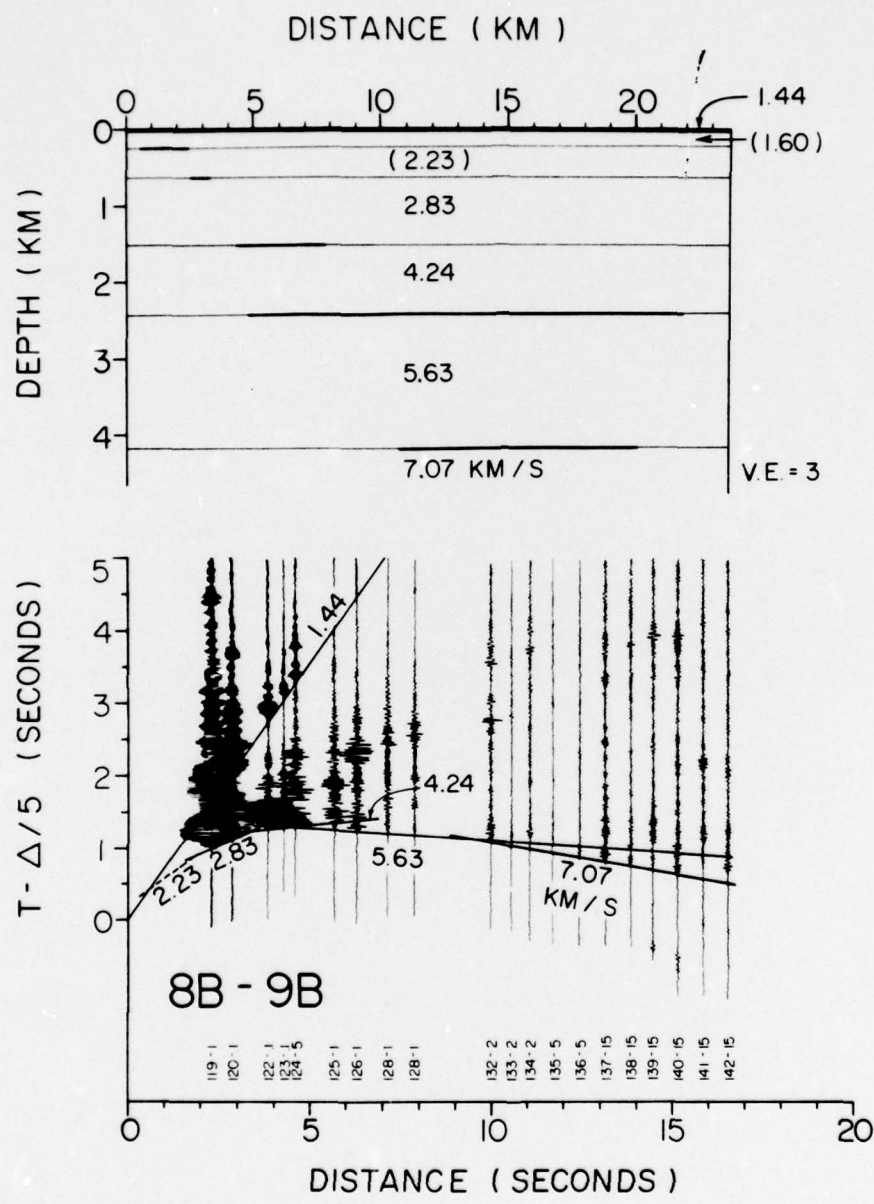


Figure 15. Line 8B-9B record section and velocity-depth model interpretation.

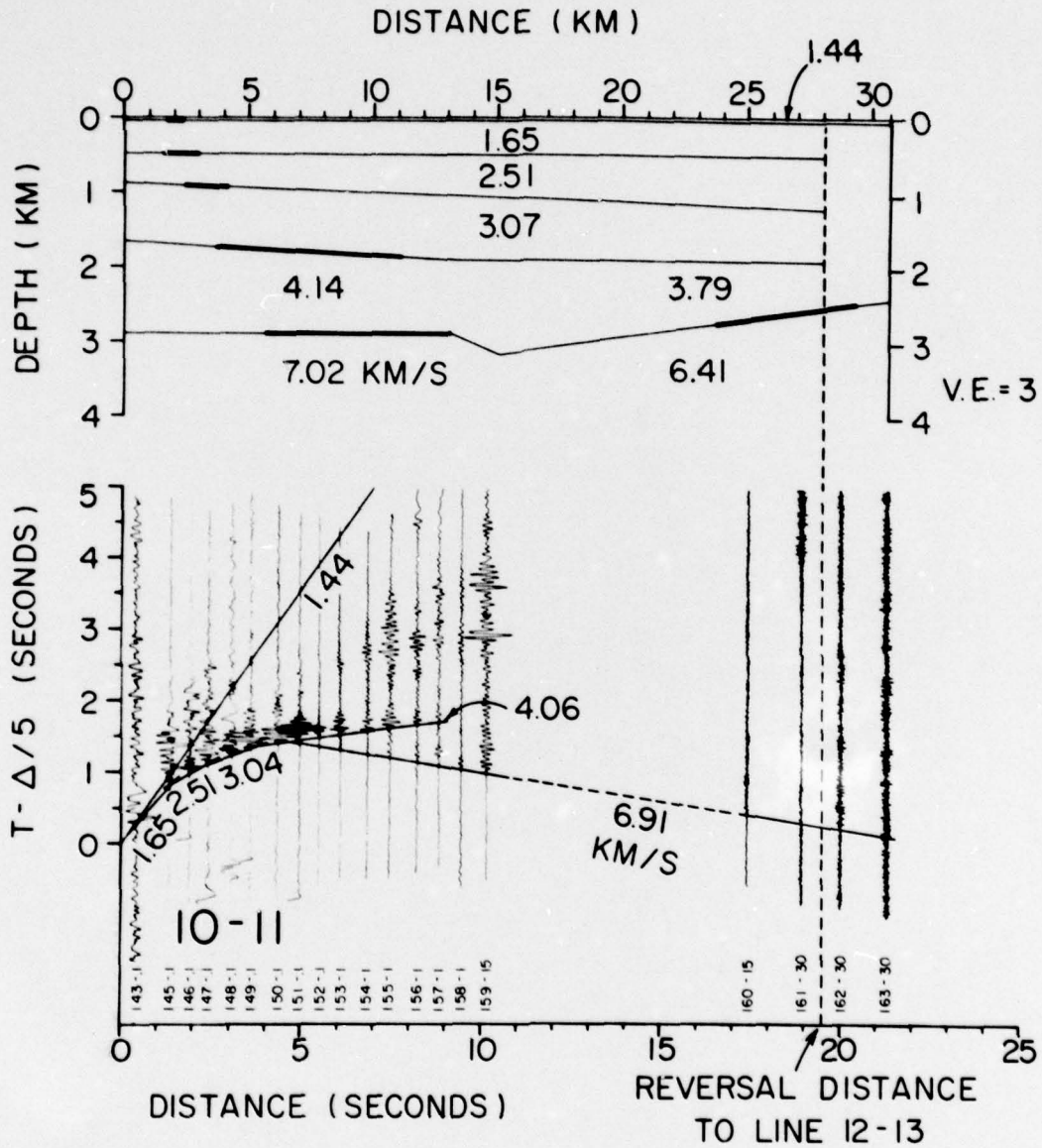


Figure 16. Line 10-11 record section and velocity-depth model interpretation.

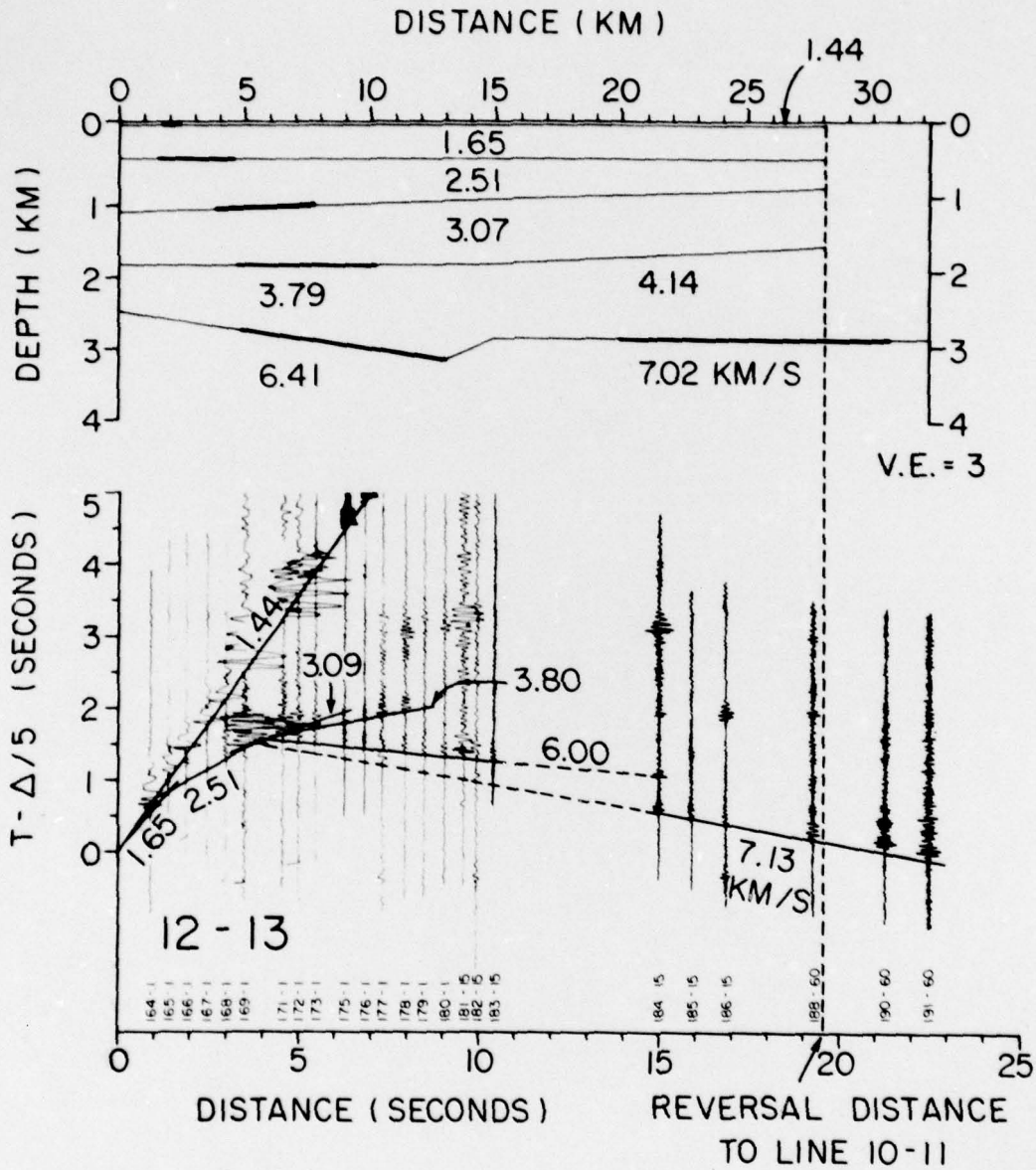


Figure 17. Line 12-13 record section and velocity-depth model interpretation.

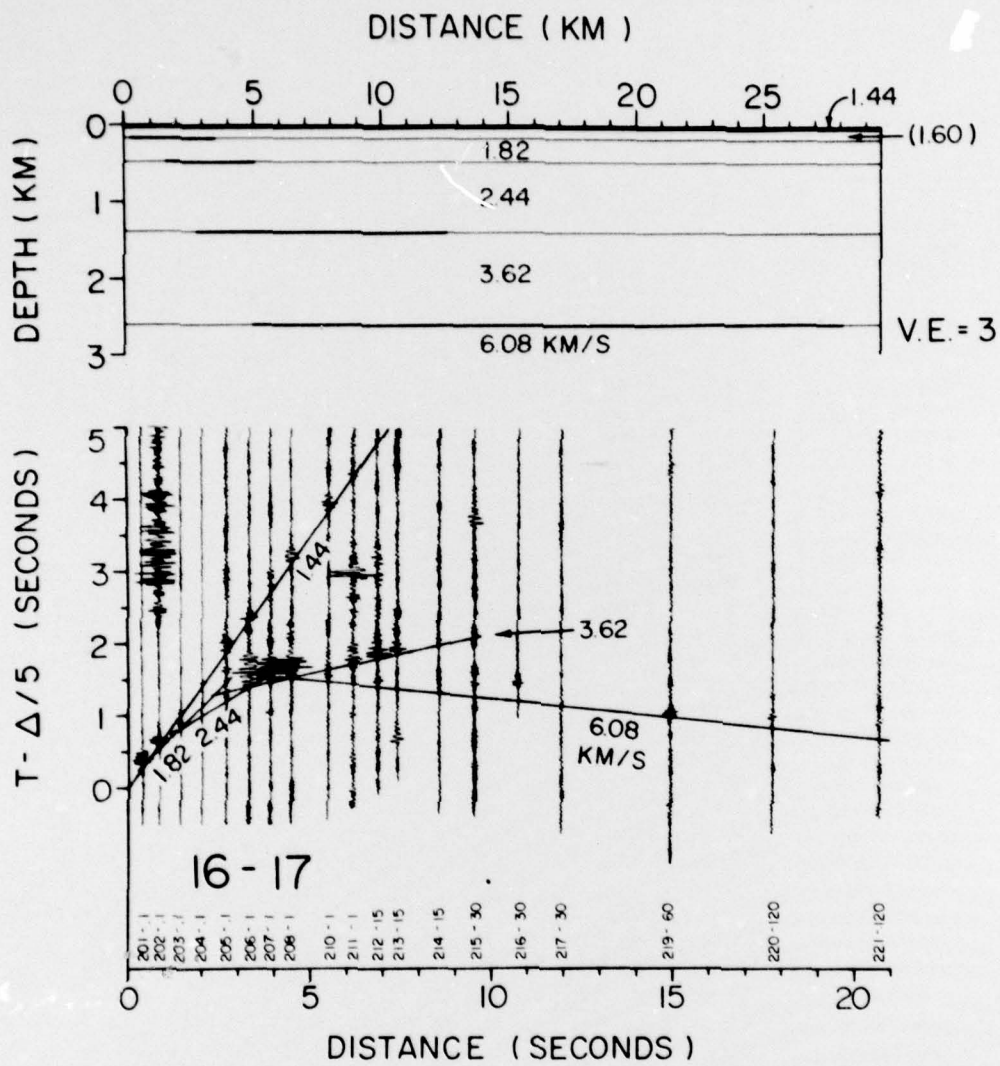


Figure 18. Line 16-17 record section and velocity-depth model interpretation.

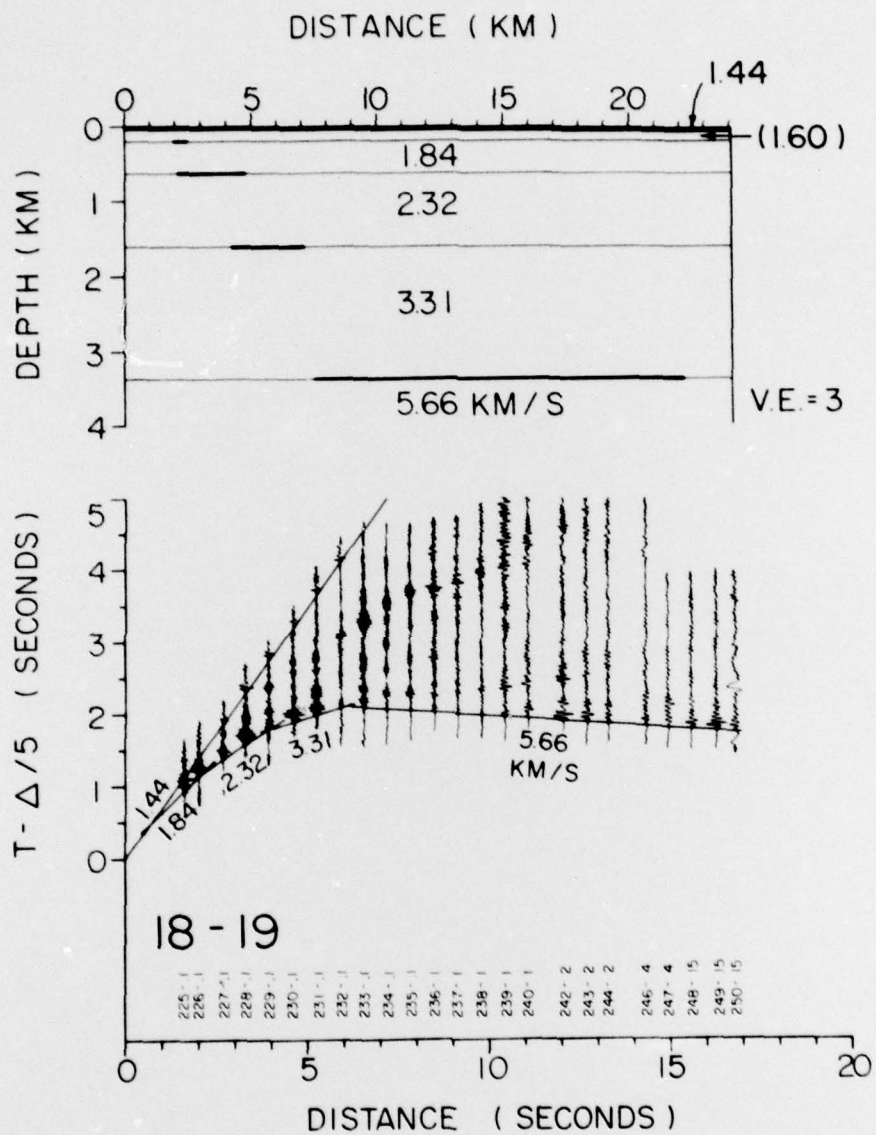


Figure 19. Line 18-19 record section and velocity-depth model interpretation.

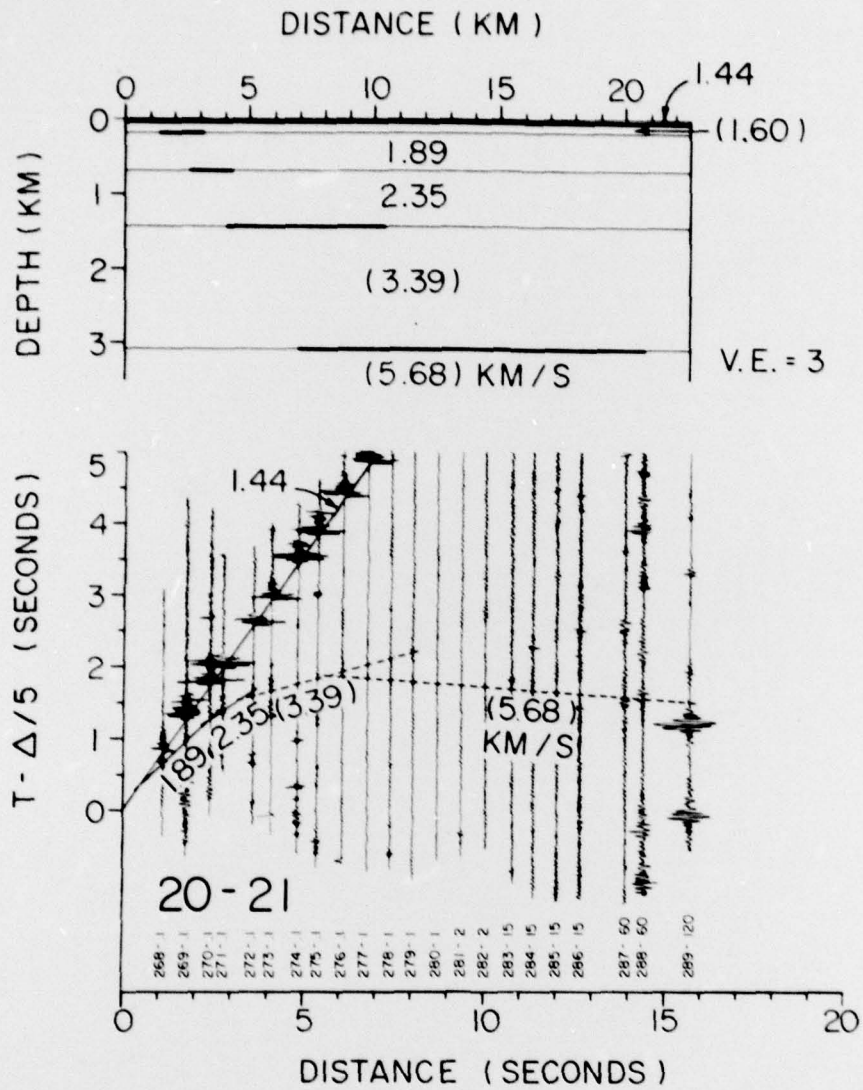


Figure 20. Line 20-21 record section and velocity-depth model interpretation.

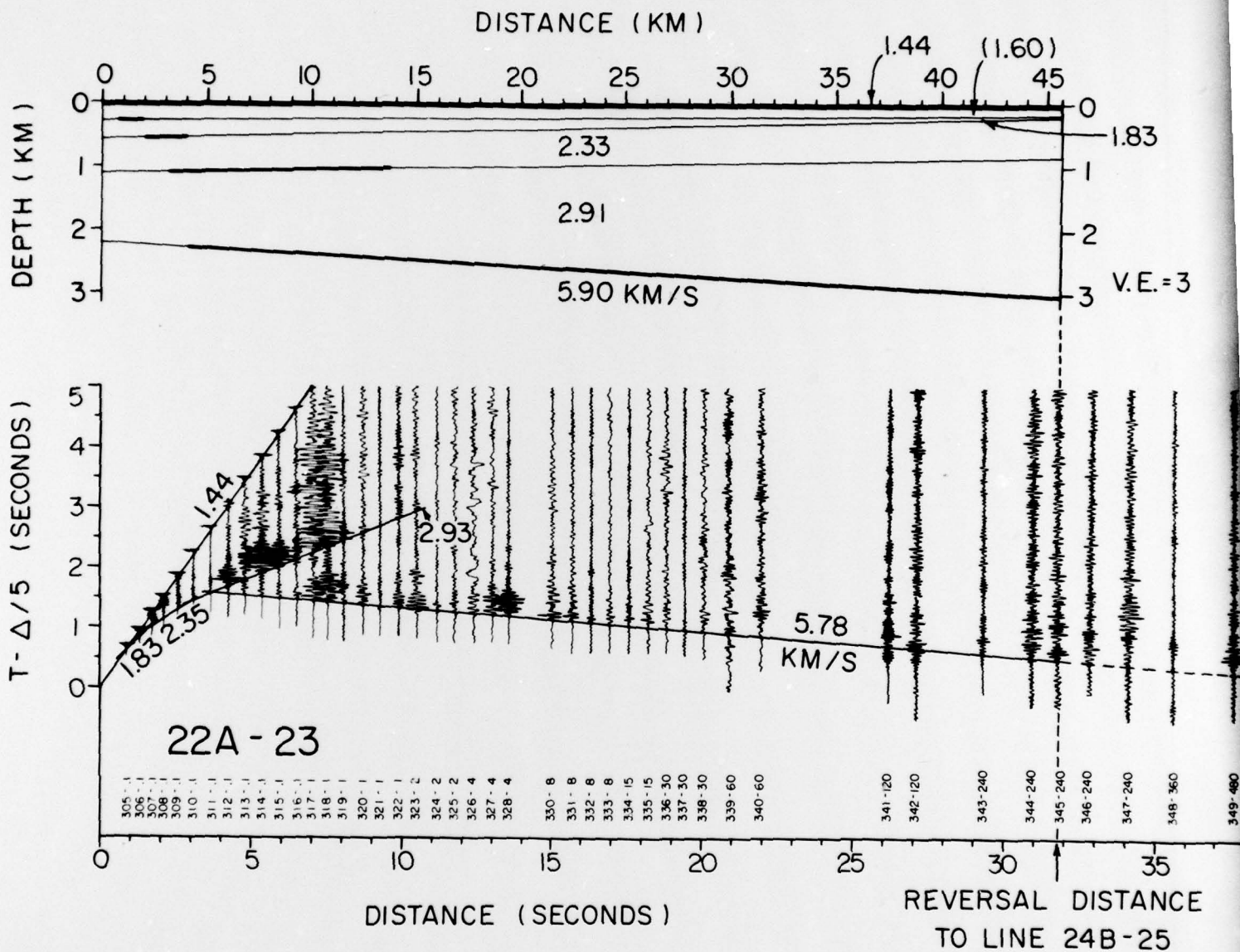
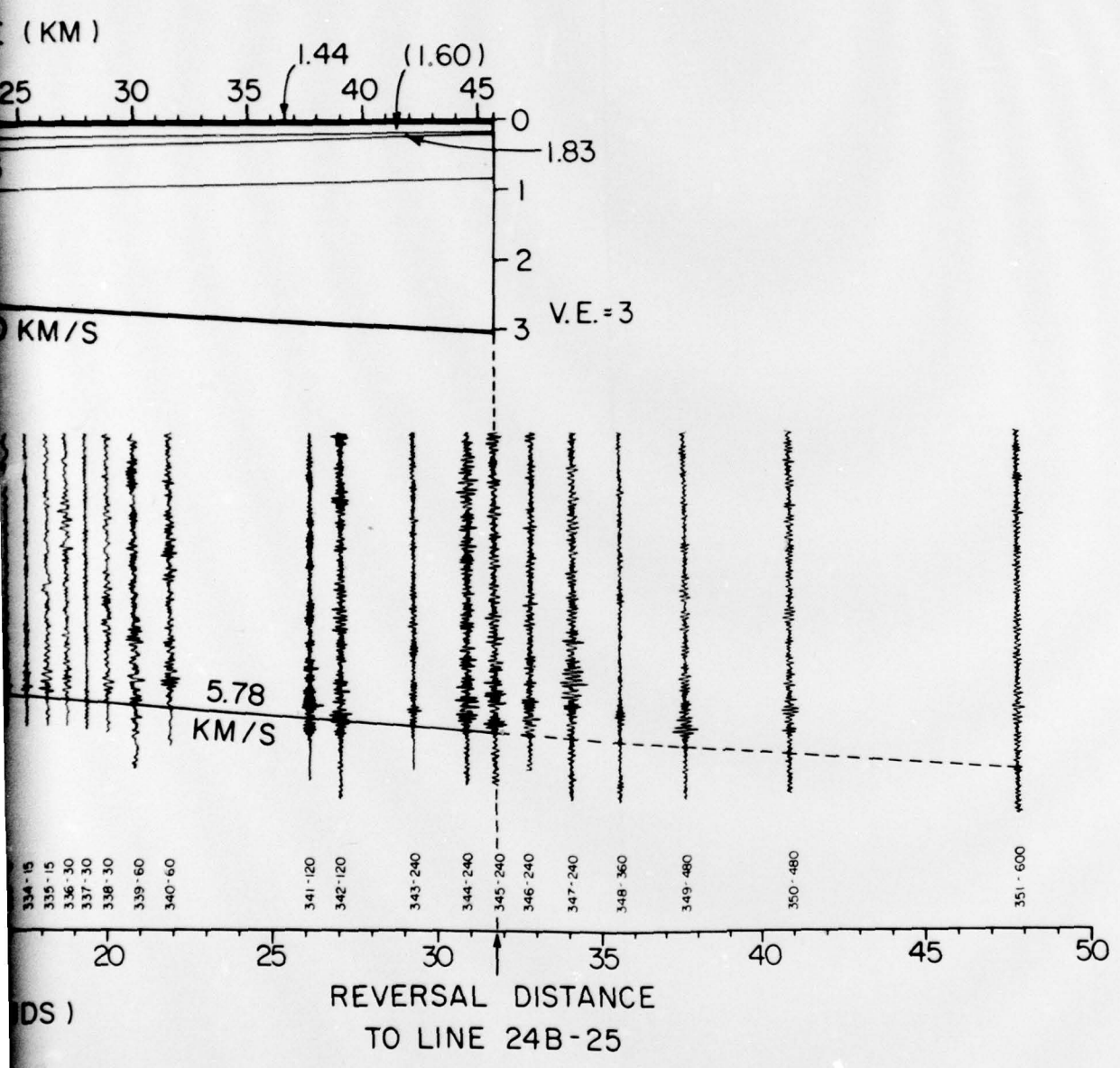


Figure 21. Line 22A-23 record section and velocity-depth model interpretation.



velocity-depth model interpretation.

a

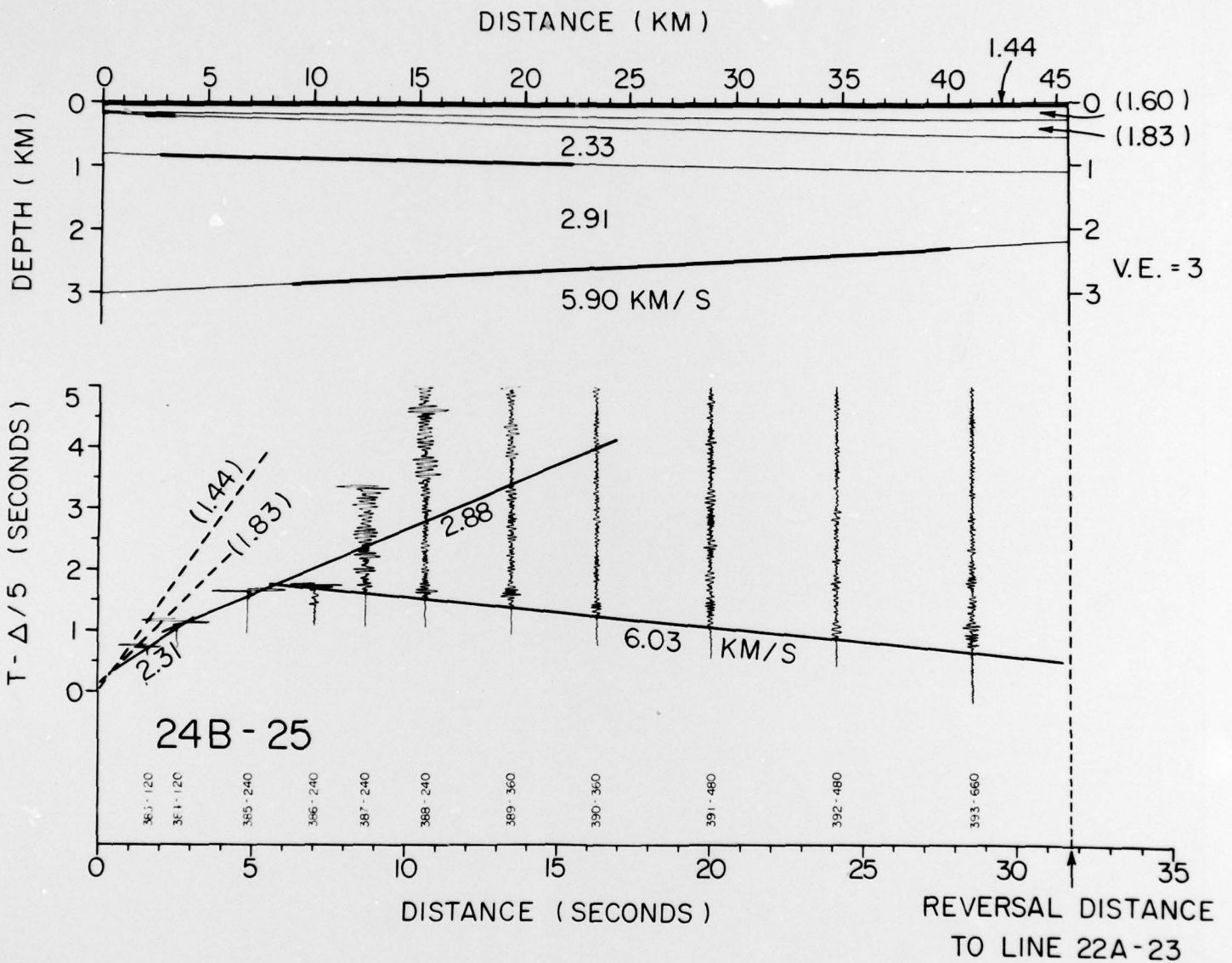


Figure 22. Line 24B-25 record section and velocity-depth model interpretation.

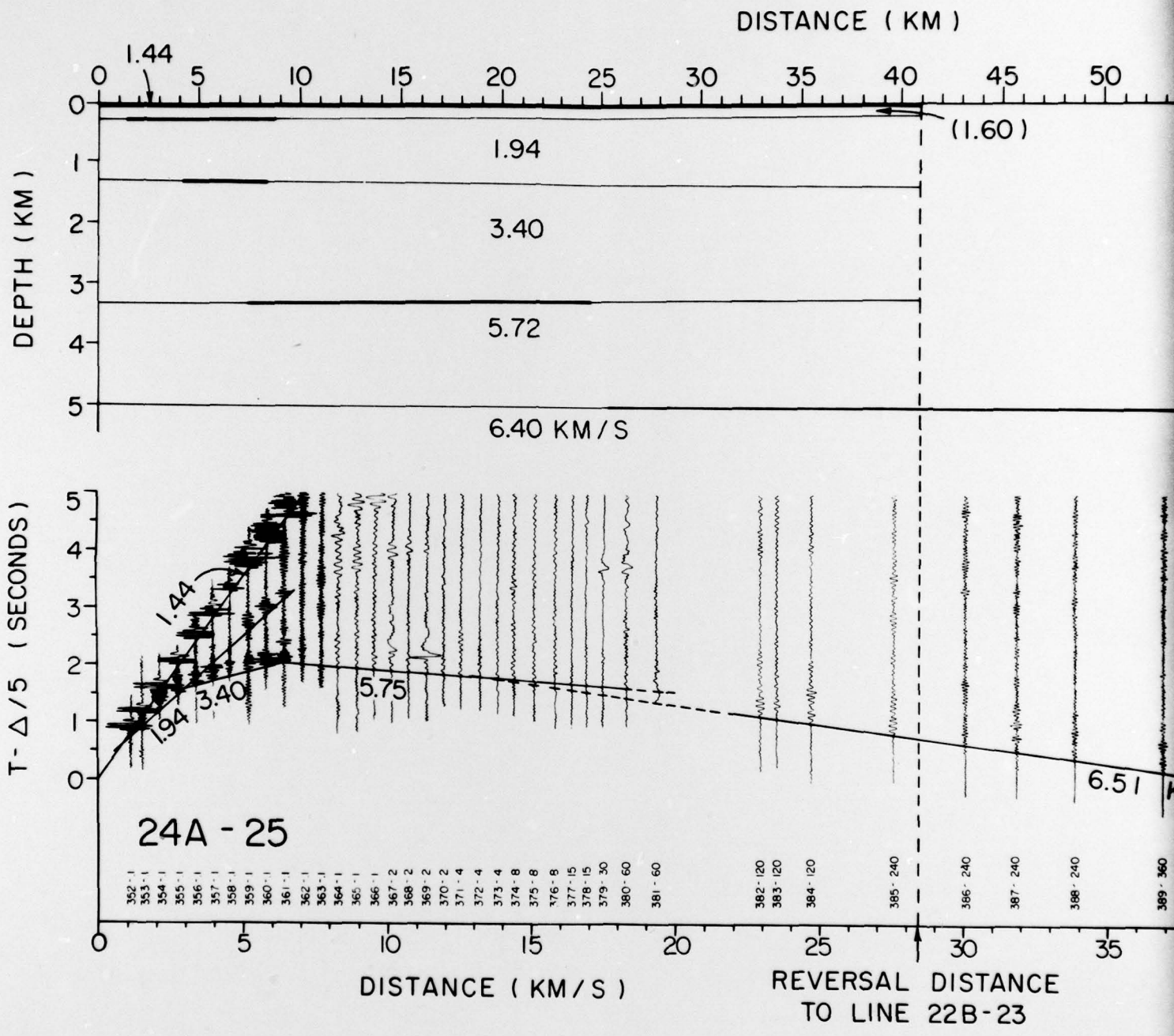


Figure 23. Line 24A-25 record section and velocity-depth model interpretation.

DISTANCE (KM)

30 35 40 45 50 55 60 65 70

(1.60)

0
1
2
3
4
5

6.40

6.51 KM/S

381 - 60
382 - 120
383 - 120
384 - 120
385 - 240
386 - 240
387 - 240
388 - 240
389 - 360
390 - 360
391 - 480
392 - 480
393 - 660

20 25 30 35 40 45 50 55

REVERSAL DISTANCE
TO LINE 22B-23

Velocity-depth model interpretation.

2

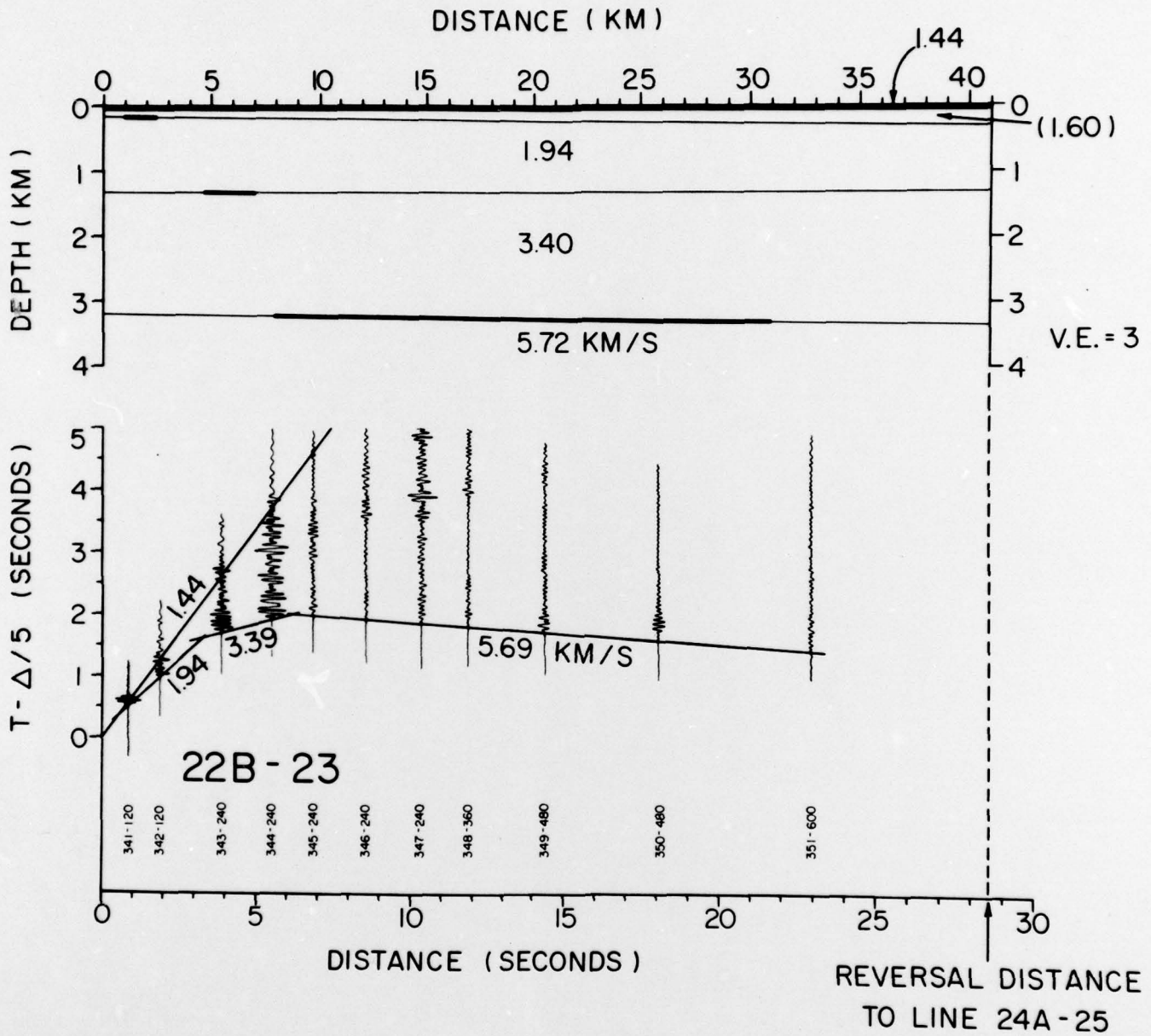


Figure 24. Line 22B-23 record section and velocity-depth model interpretation.

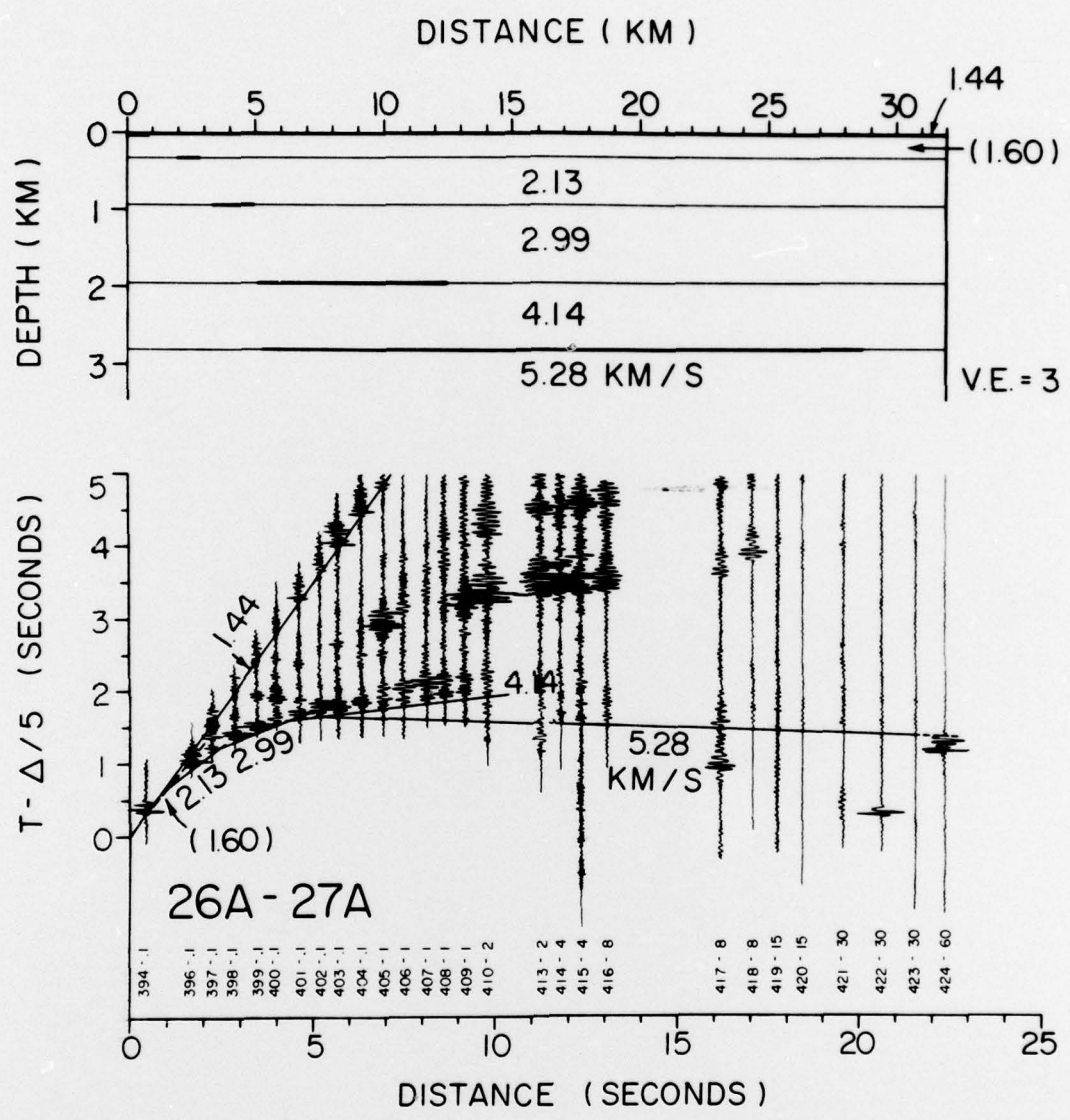


Figure 25. Line 26A-27A record section and velocity-depth model interpretation.

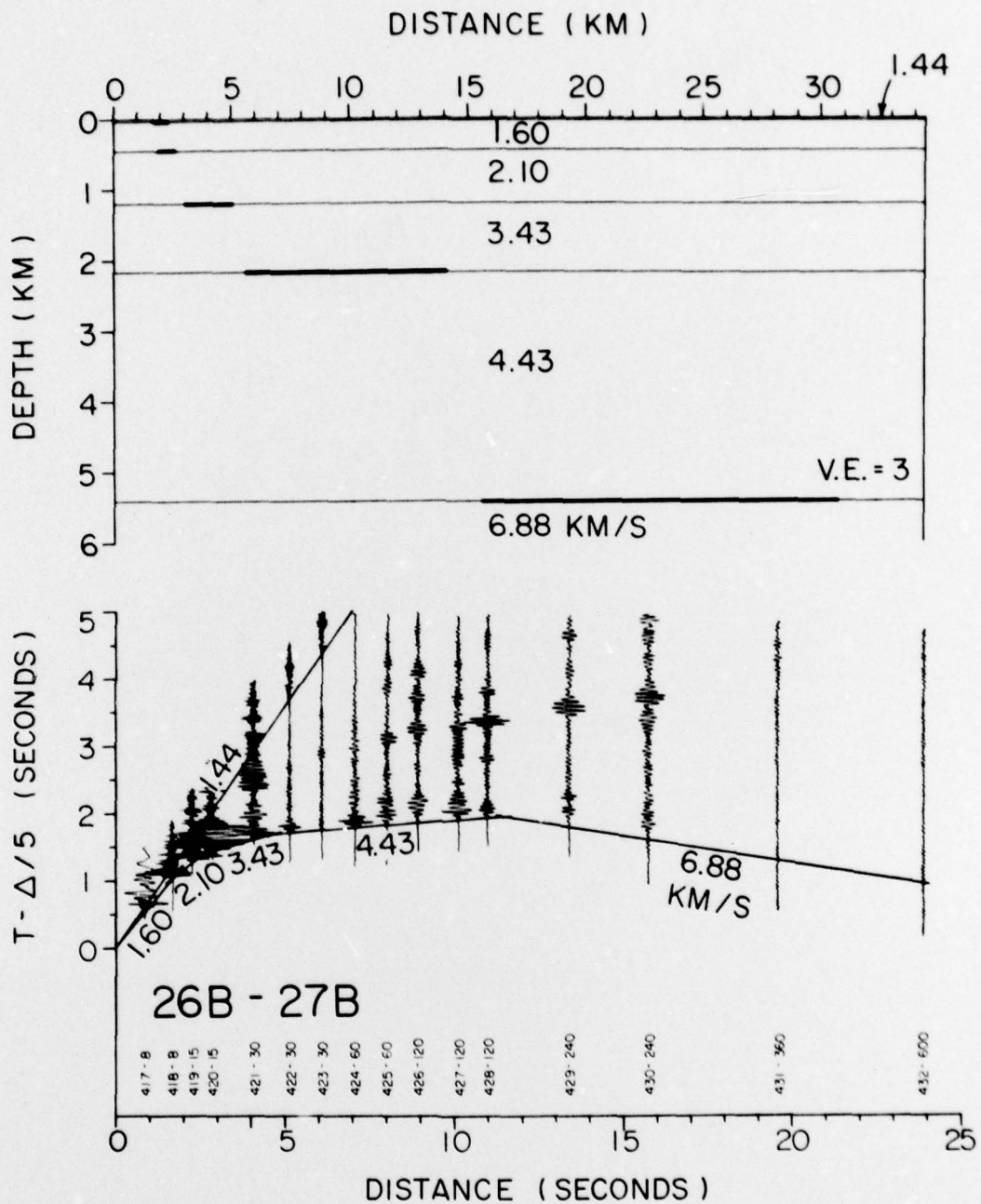


Figure 26. Line 26B-27B record section and velocity-depth model interpretation.

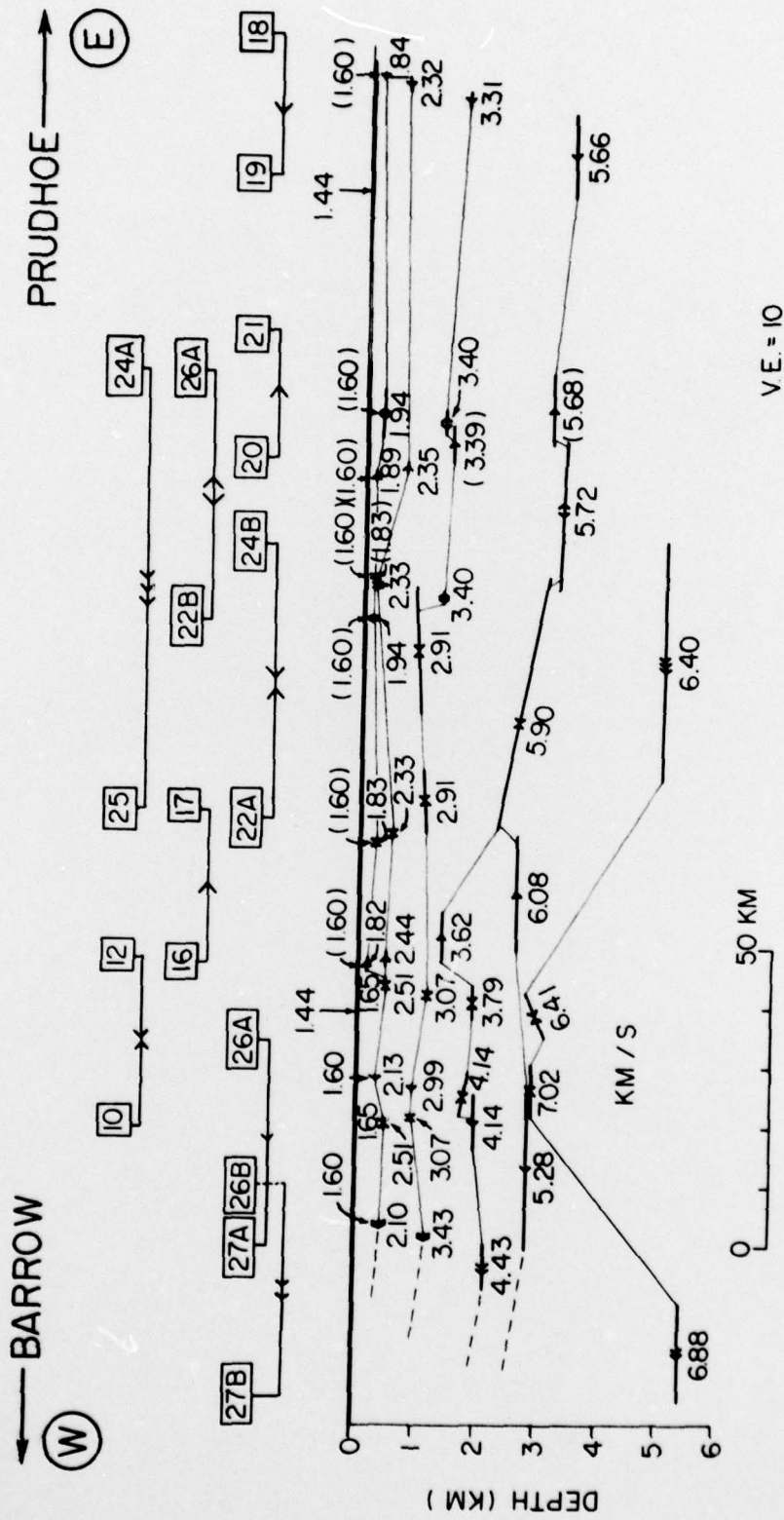


Figure 27. East-west velocity-depth section summarizing the subsurface velocity and depth information calculated from the refraction data.

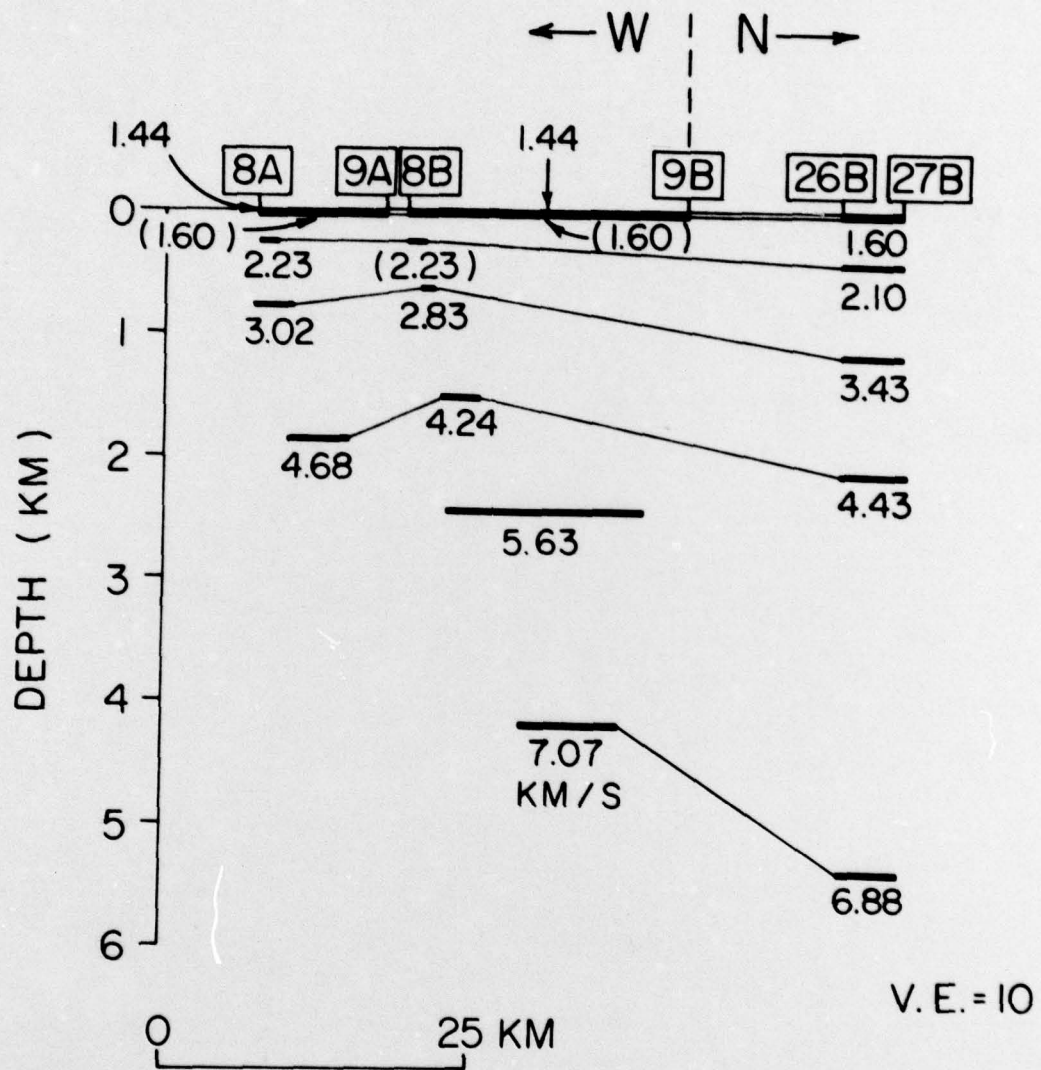


Figure 28. Velocity-depth section north of Smith Bay.

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Corvallis, Oregon.