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A SOFTWARE PACKAGE FOR ESTIMATING TIME DIFFERENCES FOR ARTILLERY SOUND RANGING APPLICATIONS

NOVEMBER 1979

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) The Fortran program entitled "Time Differences Estimator Program" is presented and documented. The program will accept a given number of microphone signals each containing a specified number of data points from a fixed data format and determine the time differences between signal bursts that appear within the record length. It also gives a measure of reliability to associate with the time differences and provides, through a least square error procedure, a consistent set of relative times that can be used as input data to a position			

20. ABSTRACT (cont)

estimator. Results from using the program on a number of recorded signals from C4 explosions approximately 12 km away are presented showing target location errors of approximately 200 meters.

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TABLE OF CONTENTS

	Page
ACKNOWLEDGEMENT	iii
I. INTRODUCTION	1
II. GENERAL DESCRIPTION TIME DIFFERENCES ESTIMATOR PROGRAM	2
A. Initialization and Acceptance of Data	2
1. Initializing	
2. Data File Format	
3. Bringing in Data from Master File	
B. Determination of Time Windows and Energies	7
1. Computation of Rough Arrival Times	
2. Computation of Fourier Window Starting Points	
3. Computation of Signal Energy within Fourier Window	
C. Prefiltering Operation	8
1. Determination of Starting Point for Noise Window	
2. Determination of Estimate of Noise Spectrum	
3. Determination of Estimate of Signal Plus Noise Spectrum	
4. Computation of Prefilter Values	
5. Application of Prefilter	
6. Application of Comb Filter for 60 HZ and Harmonics	
D. Pair by Pair Correlation	12
1. Positioning of Signals for Determining the Cross Correlation	
2. Finding the Raw Time Differences between Windowed Signals	
3. Determination of the Normalized Correlation Coefficient	
4. Determination of the Rough Time Differences between Signals I and L	
E. Determination of Least Square Time Fit	14
1. Establishment of Weights for Least Square Time Fit	
2. Determination of Least Square time Fit with MIC 1 as a Reference	
3. Adjustment of Time Differences	
4. Selection of MIC to be used as Reference	
5. Determination of Relative Times for the Position Estimator	
F. Printing the Output	18
1. Shot Information	
2. Window Information	
3. Time Differences Information	
4. Met and Timing for Position Estimator	

III. USING THE PROGRAM	18
IV. RESULTS	20
V. CONCLUSIONS	29
Appendix A Time Difference Estimator Program Listing	31
Appendix B Subroutine RDATA Program Listing	38
Appendix C An Estimate of the Noise Power Spectral Density for a PASS Run	39
Appendix D Derivation of Weighted Least Square Solution	40
Glossary of Program Variables	42
References	44

LIST OF FIGURES

Figure		Page
1.	Processing Structure of the Time Differences Estimator Program . .	3
2.	Illustration of the Data File Format	5
3.	Example of the Program Output Format	19
4.	Results from PASS Shot S1-D341-MB-1.	21
5.	Results from PASS Shot S1-D341-MB-2.	22
6.	Results from PASS Shot S2-D341-MB-1.	23
7.	Results from PASS Shot S2-D341-MB-2.	24
8.	Results from PASS Shot S2-D341-MB-4.	25
9.	Results from PASS Shot S3-D341-MB-2.	26
10.	Results from PASS Shot S7-D341-MB-2.	27

LIST OF TABLES

Table		Page
1.	Comb Filter Frequency Bands	12
2.	PASS Data Shots Used in Program Testing	20
3.	Miss Distances for PASS Data Examples	28

1. INTRODUCTION

The main problem of sound ranging is to determine the location of a transient sound source by examining the signals received at an array of microphones. The problem can be logically broken down into two main parts. First the determination of the relative arrival times of the sound at the microphones and second, the use of this information to estimate the position. In this paper we concentrate on the determination of relative arrival times.

In the past, the arrival times at each microphone were determined by visually selecting a point of change, the so-called "break point", from strip chart recorded signals [1]. Some methods used to determine these break points have been: first inflection, first maximum after inflection and first cross over after inflection. A comparative study of these methods is given in Dean [2]. In contrast to the break point methods, the author [3] proposed a procedure to obtain more accurate timing information from the received microphone signals by using the correlation between signals. The method when implemented on a digital computer would not only speed up the determination of the relative arrival times but provide more accurate results with less chance for reading errors than the visual techniques.

The purpose of this paper is to document a Fortran realization of the correlation technique described in [3] and present results from using field data from the PASS [4] experiment as input. These limited results indicate that, under a controlled experimental environment, the overall method provides reasonably good time differences estimates which, when used with the proper meteorological data, give good position estimates.

II. GENERAL DESCRIPTION OF TIME DIFFERENCES ESTIMATOR PROGRAM

The overall structure of the computer program for determining the relative time differences consists of the following basic sections: (A) Initialization and acceptance of input data, (B) a determination of the time windows that would enclose the signal received from the source and a calculation of the energies within the windows, (C) a prefiltering operation that would overcome wind and extraneous noise, (D) a pair by pair correlation to determine a rough time difference and a measure of correlation, (E) the determination of an overall least square time fit, and (F) an outputting of results. A general flow chart indicating processing structure is given in Figure 1, the program listing is given in Appendix A, and each main block is described in detail in the following sections. Each of the subheadings under the main blocks are set apart by comment cards in the program for ease in presentation.

A. Initialization and Acceptance of Data

1. Initializing. In the initialization portion of the program there are a number of parameters that must be specified and dimensioned. The main parameters are:

NMIC = Number of microphones

NL = Number of data points for each microphone

NSW = Number of points in the sliding window

NPFW = number of points in the Fourier window

The number of points in the sliding window is chosen to be approximately the number of points in the expected signal. By examining the C4 data from the PASS experiment, an example of which appears in Appendix C, it was seen that signals were in the 300-375 msec length and at a sample rate of 1 K samples/second this means approximately 350 samples. The number of points in the Fourier window was selected to be 1.5 times the number in the sliding

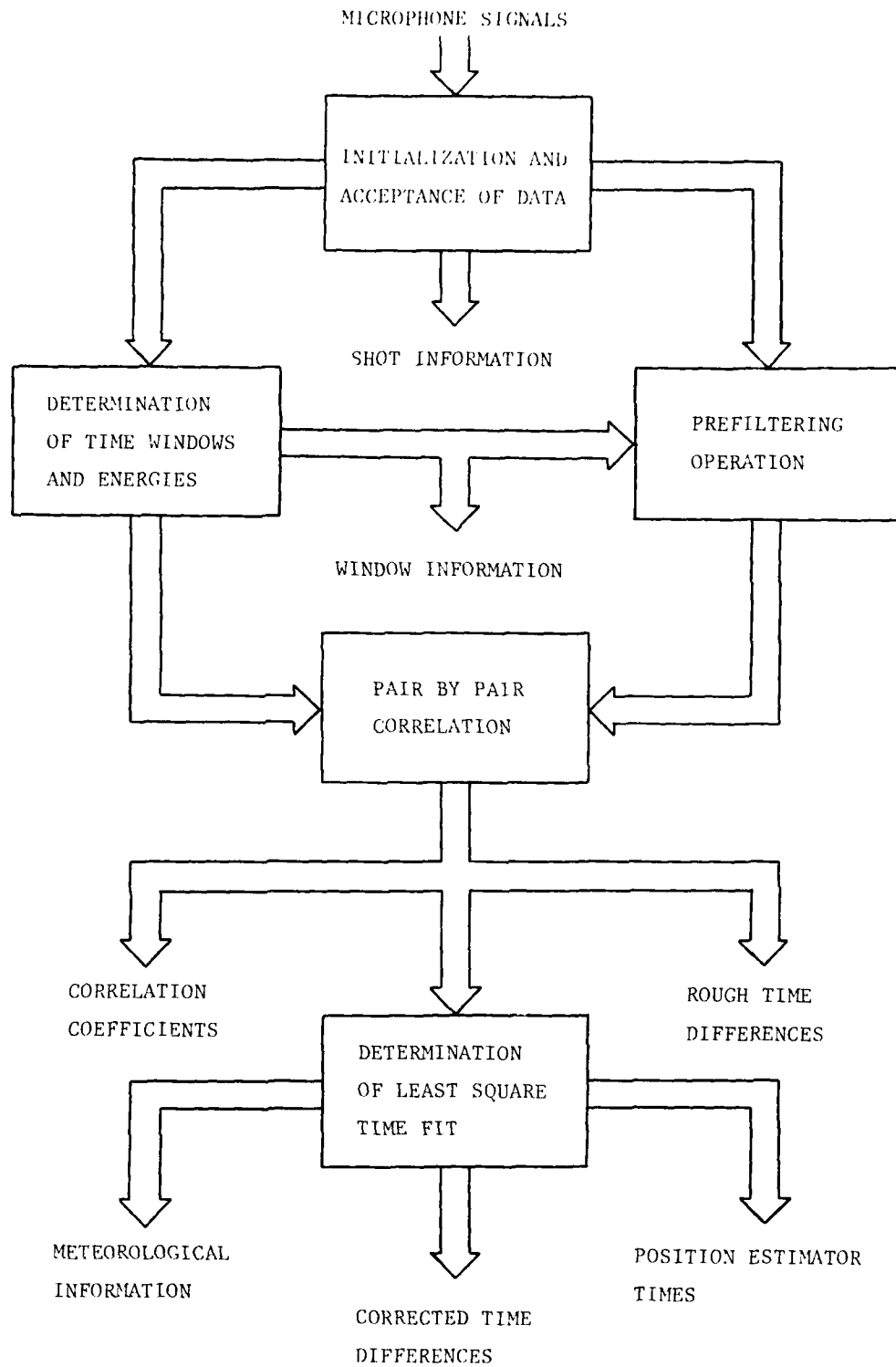


Figure 1. Processing structure of the Time Differences Estimator Program

window to make sure that most of the signal was within the window. For the C4 this meant approximately 500, and since the Fourier transform can be obtained faster for powers of 2 by the FFT, NPFW was selected to be 512 and NWS = 342. The data files provided by personnel from the Physical Sciences Laboratory (PSL), Las Cruces, New Mexico, were constructed to be 1920 samples per signal in length; therefore, NL is set equal to 1920. The following dimension and complex cards would then be required:

```

DIMENSION IDAY(NMIC), IHOURL(NMIC), IMIN(NMIC), SEC(NMIC), MIC(NMIC), TIME(NMIC)
DIMENSION TAU(NMIC,NMIC), IT(NMIC), NR(NMIC), E(NMIC), RTAU(NMIC,NMIC),
      CTAU(NMIC,NMIC), GAM(NMIC,NMIC)
DIMENSION SMIC(NMIC,NL,LRST(NMIC), G(NMIC,NMIC), AT(NMIC), A(NMIC,NMIC),
      JC(NMIC-1), V(2)
DIMENSION CMEAS(NMIC), MCOM(11).
COMPLEX X(2*NPFW), Y(2*NPFW), WORK(2*NPFW), XX(2*NPFW), YY(2*NPFW), ZZ(2*NPFW)

```

2. Data file Format. The input to the program was data taken from the PASS Experiment that had been transferred to files in the UNIVAC 1108 system by PSL personnel. The format modified slightly to include MET data and file identification for these data files is illustrated in Figure 2. Each data file is 728 lines in length with the first eight lines containing timing and shot information while the remaining lines contain the data for each microphone. To be more specific in the format we have the following line by line structure.

```

      I2   I2   I3   I2   I2   F6.3   F4.1   I4   I2
      ---  ---  ---  ---  ---  ---  ---  ---  ---
Line 1:  6   1  341  12  36  2.024  06.7  6380  09
          a   b   c   d   e   f       g   h   i

```

a = Number of microphones

b = PASS source number

c = Day of Pass shot

d = Hour of Pass shot

e = Min of Pass shot

In a similar fashion

Lines 129-248: values of microphone 2 at times $i = 1, 2, \dots, 1920$

249-368: values of microphone 3 at times $i = 1, 2, \dots, 1920$

369-488: values of microphone 4 at times $i = 1, 2, \dots, 1920$

489-608: values of microphone 5 at times $i = 1, 2, \dots, 1920$

609-728: values of microphone 6 at times $i = 1, 2, \dots, 1920$

3. Bringing in Data from Master File. In the original version of the program a subroutine was provided by PSL to read the data files and transfer this information to the SMIC(J,I) indexed array. In the present version the new subroutine RDATA(SMIC,MIC,IDAY,IHOUR,IMIN,SEC,TEMP,MILS,KNOTS) was written to obtain a desired output format and include meteorological and other cataloging information. A Fortran listing of the subroutine appears in Appendix B. To bring in the data to the program arrays simply requires the Fortran statement:

```
_____ CALL RDATA(SMIC,MIC,IDAY,IHOUR,IMIN,SEC,TEMP,MILS,KNOTS)
```

The indexed arrays: SMIC, MIC, IDAY, IHOUR, IMIN, SEC are described in the previous section and represent the values and starting time information for each microphone signal, while the TEMP, MILS, and KNOTS are defined below.

TEMP = Effective temperature at the time of the shot in degrees Centigrade

MILS = The angle of wind in mils at the time of the shot

KNOTS = The speed of the wind at the time of the shot

B. Determination of Time Windows and Energies

In many cases the time intervals of the received signals are much larger than the transient signal searched for and if the correlation procedure is used on the entire length of each signal an exorbitant amount of time would be consumed. Therefore, windows are established around the location of the signal bursts. This part of the procedure consists of computing rough arrival times, starting points for windows and the energies within the windows.

1. Computation of Rough Arrival Times. The rough arrival times are determined by the use of an energy detector for each signal. That is the energy within a sliding time window ($I, I+NSW$) is calculated for all values of time I equal 1 to $NL-NSW$. The point in time I_{MAX} for the J th microphone signal where the energy is maximum is called the rough starting time $LRST(J)$. If $X(J,I)$ $I = 1, 2, \dots, NL$ is the input to the energy detector for the J th signal, the running value of the energy within the J th sliding window becomes

$$E(J,I) = \sum_{k=I}^{I+NSW} SMIC^2(J,k) \quad I = 1, 2, \dots, NL-NSW$$

$LRST(J) =$ value of I such that $E(J,I)$ is maximized.

2. Computation of Fourier Window Starting Points. The starting point $NR(J)$ for the J th signal Fourier window is selected by bracketing the rough starting time on both sides by $NSW/4$. Care must be taken to make sure that the beginning and ending points of the window remain within 1 and NL . This is done by making the following assignment for $NR(J)$.

$$NR(J) = \begin{cases} 1 & \text{if } LRST(J) - NSW/4 \leq 1 \\ LRST(J) - NSW/4 & \text{if } 1 < (LRST(J) - NSW/4) \leq NL - 3NSW/2 \\ NL - 3 \cdot NSW/2 & \text{if } (LRST(J) - NSW/4) > NL - 3NSW/2 \end{cases}$$

3. Computation of Signal Energy within the Fourier Window. Once $NR(J)$ has been determined the energy within each Fourier window can be calculated as follows:

$$E(J) = \sum_{k=NR(J)}^{NR(J)+3NSW/2} SMIC^2(J,k)$$

The starting point of the Fourier window and signal energy are then printed out for each microphone.

C. Prefiltering Operation

In many cases there is noise present on the lines during the duration of the signals. The noise could come from a wide variety of sources including

wind noise, sixty cycle interference, and machine related noise. To characterize all these noises analytically becomes almost impossible. The program was designed, however, to try to minimize the effects these noises would have by prefiltering the data. This was done by using estimates of the spectrum of the noise, and the spectrum of the signal plus noise.

1. Determination of Starting Point for Noise Window. The noise window for each signal, selected to be before the Fourier window which contains the signal plus noise, consists of 512 points consistent with the Fourier window in size. By keeping the windows the same size the determination of the prefilter and application of the prefilter is simplified. The starting point for the noise window for each signal was determined by

$$\text{Start Point (J)} = \text{NR(J)} - 512$$

If this was less than zero for some J then the starting point for the Jth noise window was set equal to the first data point of that signal record. Since most of the data records had over 500 samples, i.e. 500 msec worth of noise preceding the signal, few cases of signal and noise window overlaps were reported.

2. Determination of Estimate of Noise Spectrum. For each pair of signals SMIC(I,L) and SMIC(J,L), and respective noise window starting points KXX and KYY, a rough estimate of the noise spectrum is desired. The estimation procedure used was that of obtaining the spectrum for each signal and simply averaging the results. To provide a spectrum compatible in samples the FOURG SUBROUTINE was used on each of the following signal vectors.

$$\begin{aligned} \text{XX} &= [\overbrace{\text{SMIC(I,KXX), SMIC(I,KXX+1), \dots, SMIC(I,KXX+511)}}^{512 \text{ samples}}, \overbrace{0, 0, \dots, 0}^{512 \text{ samples}}] \\ \text{YY} &= [\text{SMIC(J,KYY), SMIC(J,KYY+1), \dots, SMIC(J,KYY+511)}, 0, 0, \dots, 0] \end{aligned}$$

The addition of zeros will not alter the spectrum determined and provide the proper frequency indices. The spectrum was then estimated by

$$\text{Spectrum for noise} = \frac{\text{FOURG}(\text{XX}) \cdot \text{FOURG}^*(\text{XX}) + \text{FOURG}(\text{YY}) \cdot \text{FOURG}^*(\text{YY})}{2}$$

The noise spectrum was stored back in the real part of the complex array $\text{YY}(L)$, $L = 1, 2, \dots, 1024$.

3. Determination of Estimate of Signal Plus Noise Spectrum. For each pair of signals $\text{SMIC}(I, L)$ and $\text{SMIC}(J, L)$ and respective Fourier window starting points $\text{NR}(I)$ and $\text{NR}(J)$ the following signal vectors were defined.

$$\begin{aligned} \text{XX} &= [\overbrace{\text{SMIC}(I, \text{NR}(I)), \text{SMIC}(I, \text{NR}(I)+1), \dots, \text{SMIC}(I, \text{NR}(I)+511)}^{512 \text{ samples}}, \overbrace{0, 0, \dots, 0}^{512 \text{ samples}}] \\ \text{ZZ} &= [\text{SMIC}(J, \text{NR}(J)), \text{SMIC}(J, \text{NR}(J)+1), \dots, \text{SMIC}(J, \text{NR}(J)+511), 0, 0, \dots, 0] \end{aligned}$$

The signal plus noise spectrum was stored back in the real part of complex array $\text{XX}(L)$, $L = 1, 2, \dots, 1024$.

4. Computation of Prefilter Values. The prefilter that is to be applied to each pair of signals was selected to be of the form

$$H(L) = \phi_{\text{ss}}(L) / (\phi_{\text{ss}}(L) + \phi_{\text{nn}}(L)) \quad L = 1, 2, \dots, 1024$$

where $\phi_{\text{ss}}(L)$ and $\phi_{\text{nn}}(L)$ represent the value of the energy spectrum density of signal and noise respectively at index L . Since the $\phi_{\text{ss}}(L)$ was not known the prefilter frequency response was written in the following equivalent form

$$H(L) = 1 - \phi_{\text{nn}}(L) / (\phi_{\text{ss}}(L) + \phi_{\text{nn}}(L))$$

Since only the estimates of $\phi_{\text{nn}}(L)$ and $\phi_{\text{ss}}(L) + \phi_{\text{nn}}(L)$ are available, care must be taken to insure that $H(L)$ does not go negative. The program uses $\text{Real}(\text{XX}(L))$ and $\text{Real}(\text{YY}(L))$ to represent $\phi_{\text{ss}}(L) + \phi_{\text{nn}}(L)$ and $\phi_{\text{nn}}(L)$ respectively and defines PRC and PRD as

$$\text{PRC} = \text{REAL}(\text{YY}(L)) / \text{REAL}(\text{XX}(L))$$

$$\text{PRD} = \text{REAL}(\text{XX}(L))$$

The prefilter value $\text{ZZ}(L)$ at frequency index L is described as follows for $L = 1, 2, \dots, 1024$.

$$ZZ(L) = \begin{cases} (0,0) & \text{If } PRC > 1 \\ (1,1) & \text{If } PRD < .001 \\ CMLPX(H(L),H(L)) & \text{otherwise} \end{cases}$$

5. Application of Prefilter. Once the prefilter values have been determined and the product of the DFT of each positioned signal is eventually put in $Y(L)$ $L = 1, 2, \dots, 1024$ the prefiltering operation is done simply by multiplying each frequency component by $ZZ(L)$ that is

$$ZZ(L) = CMLPX (PREF, PREF)$$

$$Y(L) = Y(L) * ZZ(L)$$

6. Application of Comb Filter for 60 HZ and Harmonics

The power spectral density was obtained for microphone noise signals from the PASS experiment showing dc power, power in 60 HZ and harmonics, some low frequency wind noise, and some unidentified interference of approximately 7.8 HZ and higher harmonics. An example appears in Appendix C. To minimize the effects of these interferences a comb filter including a low pass filter was applied in the frequency domain. For the 1024 point Fourier transform the frequency indexes and corresponding analog and digital frequencies are given by:

index	digital frequency	corresponding analog frequency
k	$(k-1) \cdot 2\pi/1024$ radians	$(k-1) \cdot 2\pi/1024T$ radian/sec

Since the time T between samples is 1 msec for the PASS data the corresponding analog frequencies are spaced $2\pi/1.024$ rad/sec or .97656 HZ apart. The D.C. component index is one. Since 60 HZ and harmonics do not fall exactly on index numbers this causes a leakage to a band of frequencies that must be considered. The apparent index given in Table 1 is determined by:

$$\text{Apparent index} = \text{freq} \cdot (1.024) + 1.$$

The upper index band required because of symmetry of the DFT is determined by

$$k_u = 2 * NPFW + 2 - k = 1026 - k$$

TABLE 1 Comb Filter Frequency Bands

Identification	Frequency Band	Apparent Index	Lower Index Band k	Upper Index Band k _u
a	D.C.	1	1	1
b	0 ⁺ -7.8 HZ	1-8.9	2-10	1016-1024
c	60 HZ	62.44	60-65	961-966
d	120 HZ	123.88	121-126	900-905
e	180 HZ	185.32	183-188	838-843
f	140 HZ	246.76	244-249	777-782

The index information for the comb filter was given in the following data card

----- DATA MCOMB/1, 2, 10, 60, 65, 122, 126, 183, 188, 244, 249/

 a b c d e f

The comb filter was applied by setting the values corresponding to the index bands equal to zero in the frequency domain output of the pair by pair correlation.

D. Pair by Pair Correlation

The pair by pair cross correlation $R_{xy}(L)$ of the windowed signals is accomplished in the frequency domain by use of the FFT algorithm. That is

$$R_{xy}(L) = \text{IDFT}[\text{DFT}(X(L)) \cdot \text{DFT}^*(Y(L))]]$$

Since the above operation performs circular correlation it is necessary to position the data signals $X(L)$ and $Y(L)$ such that the circular and linear correlation are the same. The * means complex conjugate and is needed to provide correlation rather than convolution.

1. Positioning of Signals for Determining the Cross Correlation. To obtain linear convolution resulting in proper correlation, the signals $SMIC(I,L)$

and $SMIC(J,L)$ $L = 1,2,\dots,512$ are positioned as follows

L	1 ..	2	...	512	513	514	...	1024
Real X(L)	SMIC(I,1),SMIC(I,2),...,SMIC(I,512),				0	0	...	0
Imag X(L)	0	0	...	0	0	0	...	0
Real Y(L)	0	0	...	0	SMIC(J,1),SMIC(J,2),...,SMIC(J,512)			
Imag Y(L)	0	0	...	0	0	0	...	0

2. Finding the Raw Time Differences between Windowed Signals. Once the $DFT(X(L)) \cdot DFT^*(Y(L))$ is prefiltered and comb filtered the cross correlation $R_{xy}(L)$ is obtained back in the real part of array $Y(L)$ $L=1,2,\dots,1024$ by taking the Inverse Fourier Transform. The Fortran statement uses a +1 to indicate inverse as follows.

```
CALL FOURG(Y,1024,+1, WORK)
```

A search is then performed on $|\text{Real}(Y(L))|$, $L=1,2,\dots,1024$ to obtain the maximum value CMAX of the cross correlation and the time TMAX of the maximum value. Because of the positioning of the signals the raw time difference is then given by

$$TAU(I,J) = TMAX - NPFW - 1$$

3. Determination of the Normalized Correlation Coefficient. The normalized correlation coefficient $GAM(I,J)$ is obtained by dividing the maximum value by the square root of the product of the energies and is given by

$$GAM(I,J) = CMAX / ((E(J) * E(I)) ** 0.5)$$

If the signals $[SMIC(I,L)]$ and $[SMIC(J,L)]$ are identical in shape but of different amplitudes the $GAM(I,J)$ will be equal to 1. If there shapes are significantly different the value of $GAM(I,J)$ will be approximately zero. In this way the normalized correlation coefficient provides a measure of similarity of the two signals tested.

4. Determination of the Rough Time Differences between Signals I and L. The raw time difference represents the time difference between the signals in the windows. To obtain the rough time differences between microphone signals

the raw time difference $\text{TAU}(I,L)$ must be adjusted by the starting times of the windows as follows

$$\text{RTAU}(I,L) = \text{FLOAT}[\text{IT}(I) - \text{IT}(L)] + \text{TAU}(I,L)$$

These rough time differences $\text{TAU}(I,L)$ $I=1,2,\dots,\text{NMIC}$, and $L=I+1,\dots,\text{NMIC}$ are part of the input to the least square adjustment section.

E. Determination of Least Square Time Fit

The rough time difference $\text{RTAU}(I,J)$ and normalized correlation coefficient $\text{GAM}(I,J)$ $I=1,2,\dots,\text{NMIC}$ $J=1,2,\dots,\text{NMIC}$ are now used to obtain a consistent set of time differences by using a weighted least squares procedure. Each step in the procedure is described in the following paragraphs.

1. Establishment of Weights for Least Square Time Fit. A weight is attached to each one of the rough time differences indicating a measure of reliability of those estimates. The measure or weight $G(I,J)$ assigned to $\text{RTAU}(I,J)$ is defined to be a function of the normalized correlation coefficient $\text{GAM}(I,J)$. Different functional relationships have been played with, but at present no way of favoring one over the others has been established. The program in the present form uses the following weighting.

$$\begin{aligned} G(I,J) &= (\text{GAM}(I,J))^2 && \text{if } \text{GAM}(I,J) < 0.5 \\ &= (\text{GAM}(I,J))^{1/2} && \text{if } \text{GAM}(I,J) > 0.5 \end{aligned}$$

This attaches slightly more influence to time difference values that have a normalized correlation coefficient greater than 0.5 over those that have correlations less than 0.5.

2. Determination of Least Square Time Fit with MIC 1 as a Reference.

The weights $G(I,J)$ described above are used to define a measure of performance e given by

$$e = \sum_{I>J} \sum_{J=1}^{\text{NMIC}} G(I,J) (\text{RTAU}(I,J) - (\text{TIME}(I) - \text{TIME}(J)))^2$$

The objective is to find the times TIME(I) I=1,2,..., NMIC such that e is minimized. A solution of this problem for G(I,J)=1 is given by the Author [3] and requires solving for n microphone signals a set of simultaneous linear equations in n-1 unknowns when a given microphone has been selected as a reference. In Appendix C a solution for arbitrary G(I,J) with MIC1 as a reference is presented resulting in the following set of simultaneous equations in t_i where t_i is the relative time of arrival of the ith signal.

$$\begin{bmatrix} \alpha_2 \\ \alpha_3 \\ \alpha_4 \\ \alpha_5 \\ \alpha_6 \end{bmatrix} = - \begin{bmatrix} G(1,1) & G(2,3) & G(2,4) & G(2,5) & G(2,6) \\ G(2,3) & G(2,2) & G(3,4) & G(3,5) & G(3,6) \\ G(2,4) & G(3,4) & G(3,3) & G(4,5) & G(4,6) \\ G(2,5) & G(3,5) & G(4,5) & G(4,4) & G(5,6) \\ G(2,6) & G(3,6) & G(4,6) & G(5,6) & G(6,6) \end{bmatrix} \begin{bmatrix} t_1 \\ t_2 \\ t_3 \\ t_4 \\ t_5 \end{bmatrix}$$

where

$$G(1,1) = -(G(1,2) + G(2,3) + G(2,4) + G(2,5) + G(2,6))$$

$$G(2,2) = -(G(1,3) + G(2,3) + G(3,4) + G(3,5) + G(3,6))$$

$$G(3,3) = -(G(1,4) + G(2,4) + G(3,4) + G(4,5) + G(4,6))$$

$$G(4,4) = -(G(1,5) + G(2,5) + G(3,5) + G(4,5) + G(5,6))$$

$$G(5,5) = -(G(1,6) + G(2,6) + G(3,6) + G(4,6) + G(5,6))$$

and

$$\alpha_2 = - G(1,2)R(1,2) + G(2,3)R(2,3) + G(2,4)R(2,4) + G(2,5)R(2,5) + G(2,6)R(2,6)$$

$$\alpha_3 = - G(1,3)R(1,3) - G(2,3)R(2,3) + G(3,4)R(3,4) + G(3,5)R(3,5) + G(3,6)R(3,6)$$

$$\alpha_4 = - G(1,4)R(1,4) - G(2,4)R(2,4) - G(3,4)R(3,4) + G(4,5)R(4,5) + G(4,6)R(4,6)$$

$$\alpha_5 = - G(1,5)R(1,5) - G(2,5)R(2,5) - G(3,5)R(3,5) - G(4,5)R(4,5) + G(5,6)R(5,6)$$

$$\alpha_6 = - G(1,6)R(1,6) - G(2,6)R(2,6) - G(3,6)R(3,6) - G(4,6)R(4,6) - G(5,6)R(5,6)$$

with

$$R(I,J) = RTAU(I,J)$$

This set of equations was solved by using the GJR subroutine package from the 1108 Large Scale Systems Math Pack which is fully described in [5]. The subroutine is accessed with the following call

```

CALL GJR(A,6,5,5,6,$400,JC,V)
      a b c d e   f   g h

```

where

- a = augmented coefficient matrix
- b = maximum number of columns in A
- c = maximum number of rows in A
- d = the number of rows in A
- e = the number of columns in A
- f = statement number control is returned if an overflow is detected
- g = control array
- h = on input V(1) is the option indicator, which to solve equations is 4, on output V(2) contains the value of the natural log of the absolute value of the determinant and V(1) contains the sign of the determinant

On output the last column of A is the solution vector $[t_2, t_3 \dots t_6]$ and is called AT(2), AT(3), ..., AT(6). Since microphone 1 was defined to be the reference, AT(1) is set equal to zero. The AT[I] represents the starting time for the signal in the Ith window relative to the signal in window 1.

3. Adjustment of Time Differences. Using the AT vector, a raw corrected time difference can be found by the difference of the components

$$\text{TAU}(I,J) = \text{AT}(I) - \text{AT}(J) \quad I=1,2,\dots,6 \quad K \leq J \leq 6$$

The least square corrected time difference in milliseconds can then be formed by

$$\text{CTAU}(I,J) = \text{TAU}(I,J) + \text{FLOAT}[\text{IT}(I) - \text{IT}(J)]$$

4. Selection of MIC to be used as reference. To select a microphone as a reference for determining the relative times for the position estimator requires

a specification of a performance criterion. We would like to select the MIC as reference that gives the best possible relative times for the position estimator. Upon examining data, it was found that position estimates were sensitive to the selection of a MIC reference even though a least squares procedure had been performed on the time differences. No direct relationship was established however and the following procedure represents a reasonable way to select the reference with no sense of optimality implied. As the normalized correlation coefficient is a measure of reliability of the time differences determined, the sum of the correlation coefficients for all time differences associated with a particular microphone represents a measure of reliability of the time differences for that microphone. This measure was called CMEAS(I) $I=1,2,\dots,6$ and given by

$$\text{CMEAS}(I) \approx \sum_{\substack{J=1 \\ J \neq I}}^6 G(I,J)$$

The value K for which $\text{CMEAS}(K)$ $K=1,2,\dots,6$ is a maximum is called K_{MAX} and represents the number of the microphone to be used as a reference. In the output of the times for the position estimator the reference microphone is identified by having the time 0.000.

5. Determination of Relative Times for the Position Estimator. The position estimator `USRAN1[1]` requires six relative arrival times and the proper meteorological data as input to determine the position of the source. The number (K_{MAX}) of the microphone signal that was selected as a reference was determined previously. To find the times relative to this microphone could be easily accomplished by filling out the lower triangular part of the $\text{CTAU}(I,L)$ array with the negative of upper triangular part. In this way the time differences with respect to each microphone appear on the rows of $\text{CTAU}(I,L)$ and the selection of the K_{MAX} microphone corresponds to selecting a row.

F. Printing the Output

An example of the overall program output format is given in Figure 3 and consists of the four basic parts described below.

1. Shot Information. The header information is in reference to the data files from the PASS experiment and gives the day, time, and position of the shot as well as the position number, starting times and lengths (MSEC) of the data record for the microphones recording.

2. Window Information. The window starting time in MSEC determined by the program relative to the starting times for each microphone record are given along with the signal energy within the window. The microphones numbered 1 through 6 correspond to the normal ordering of the PASS microphone numbers. The window signal energy and starting time could be used in an interactive mode (not programmed at this time) to allow the operator to check if a signal appears in the window or not.

3. Time Differences Information. The normalized correlation coefficient, time differences in MSEC, and corrected time differences in seconds are given for each pair of microphone signals. These results may be used to infer the overall reliability provided by the normalized correlation coefficient and a measure of consistency by examining the changes made in the rough time differences $RTAU(I,J)$ to get the corrected time differences.

4. Met and Timing for Position Estimator. The times in seconds and the Met information that could be used as input to a position estimator are provided for interfacing purposes. The timing information appears in an array $TIME(J)$ $J=1,2,\dots,6$ while the temperature, wind direction and wind speed are labeled TEMP, MILS, and KNOTS respectively.

III. USING THE PROGRAM

The procedure given in this section will apply to the use of the program on the WSMR UNIVAC 1108 system. Presently the program is stored under file

```

DAY 341:  SHOOT TIME  8:15 HRS   1.89% SEC
SOURCE 2  MIC ARMY 6
MICS: 27+28+29+30+31+32      1920 VALUEN/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):  8:15 HRS  34.971 SEC      MIC(30):  8:15 HRS  35.379 SEC
MIC(28):  8:15 HRS  34.971 SEC      MIC(31):  8:15 HRS  37.659 SEC
MIC(29):  8:15 HRS  35.483 SEC      MIC(32):  8:15 HRS  39.451 SEC

THE WINDOW STARTING TIMES(SEC) RELATIVE TO ABOVE

MIC 1      MIC 2      MIC 3      MIC 4      MIC 5      MIC 6
  742       726       677       656       686       565

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1      MIC 2      MIC 3      MIC 4      MIC 5      MIC 6
1433159.   254966.   8322272.   21142409.   35415647.   34593679.

THE CORRELATION, TIME DIFFERENCES(SEC), AND CORRECTED TIME DIFFERENCES(SEC)
BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)= .678      RTAU(1,2)= -5.0      CTAU(1,2)= .014
GAMMA(1,3)= .703      RTAU(1,3)= -422.0    CTAU(1,3)= -.436
GAMMA(1,4)= .669      RTAU(1,4)= -1324.0   CTAU(1,4)= -1.340
GAMMA(1,5)= .653      RTAU(1,5)= -2652.0   CTAU(1,5)= -2.642
GAMMA(1,6)= .735      RTAU(1,6)= -4329.0   CTAU(1,6)= -4.319
GAMMA(2,3)= .674      RTAU(2,3)= -455.0    CTAU(2,3)= -.451
GAMMA(2,4)= .703      RTAU(2,4)= -1359.0   CTAU(2,4)= -1.354
GAMMA(2,5)= .730      RTAU(2,5)= -2656.0   CTAU(2,5)= -2.656
GAMMA(2,6)= .753      RTAU(2,6)= -4353.0   CTAU(2,6)= -4.333
GAMMA(3,4)= .774      RTAU(3,4)= -903.0    CTAU(3,4)= -.903
GAMMA(3,5)= .756      RTAU(3,5)= -2201.0   CTAU(3,5)= -2.206
GAMMA(3,6)= .724      RTAU(3,6)= -3877.0   CTAU(3,6)= -3.882
GAMMA(4,5)= .795      RTAU(4,5)= -1298.0   CTAU(4,5)= -1.303
GAMMA(4,6)= .753      RTAU(4,6)= -2974.0   CTAU(4,6)= -2.979
GAMMA(5,6)= .784      RTAU(5,6)= -1676.0   CTAU(5,6)= -1.676

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)= -4.319 SEC
TIME(2)= -4.333 SEC
TIME(3)= -3.882 SEC
TIME(4)= -2.979 SEC
TIME(5)= -1.676 SEC
TIME(6)= .000 SEC

THE BUT TO A POSITION ESTIMATOR INPUT TO POSITION ESTIMATOR

TEMP= 5.4 DEGS C.
WIND DIRECTION= 6180 MILS
WIND SPEED= 9 KNOTS

```

Figure 3. Example of the program output format

name and element LCLPF.SOUNDR in both a symbolic and absolute form. The following control statements will execute the program;

```
@ASC, AZ S3-D341-MB-1.      Assign data file to run
@USE 12., S3-D341-MB-1      Use file S3-D341-MB-1 as logical unit 12
@XQT LCLPF.SOUNDR          Execute program.
```

If the program is to be executed on another computer a duplicate of the symbolic form of SOUNDR must be obtained and if a different data structure is to be used the subroutine RDATA must be rewritten. The main program and subroutine can then be compiled on the computer to be used.

IV. RESULTS

The program LCLPF.SOUNDR was run using various signals from the PASS experiment as input. The results for the test shots given in Table 2 are shown in Figures 4 through 10. The times and Met data indicated in Figures 4 through 10 were used in a position estimator program resulting in the Miss distances given in Table 3.

TABLE 2. PASS Data Shots Used in Program Testing

UNIVAC 1108 File No.	Source	Day	MIC Array	Identification Number
S1-D341-MB-1.	1	341	B	1
S1-D341-MB-2.	1	341	B	2
S2-D341-MB-1.	2	341	B	1
S2-D341-MB-2.	2	341	B	2
S2-D341-MB-4.	2	341	B	4
S3-D341-MB-2.	3	341	B	2
S7-D341-MB-2.	7	341	B	2

DAY 341: SHOT TIME 5:36 HRS 2.024 SEC
 SOURCE 1 MINE ARRAY B
 MICS: 27,28,29,30,31,32 1920 VALUES/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):	5:36 HRS	35.611 SEC	MIC(30):	5:36 HRS	39.451 SEC
MIC(28):	5:36 HRS	36.507 SEC	MIC(31):	5:36 HRS	41.499 SEC
MIC(29):	5:36 HRS	37.787 SEC	MIC(32):	5:36 HRS	43.903 SEC

THE WINDOW STARTING TIMES(MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
808	603	658	716	701	747

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
3622710.	207322.	9752818.	26270144.	11659675.	13955643.

THE CORRELATION, TIME DIFFERENCES(MSEC), AND CORRECTED TIME DIFFERENCES(SEC) BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)=	.558	RTAU(1,2)=	-884.0	CTAU(1,2)=	-.884
GAMMA(1,3)=	.525	RTAU(1,3)=	-2181.0	CTAU(1,3)=	-2.182
GAMMA(1,4)=	.471	RTAU(1,4)=	-3860.0	CTAU(1,4)=	-3.861
GAMMA(1,5)=	.418	RTAU(1,5)=	-5878.0	CTAU(1,5)=	-5.883
GAMMA(1,6)=	.534	RTAU(1,6)=	-8218.0	CTAU(1,6)=	-8.216
GAMMA(2,3)=	.395	RTAU(2,3)=	-1295.0	CTAU(2,3)=	-1.297
GAMMA(2,4)=	.412	RTAU(2,4)=	-2977.0	CTAU(2,4)=	-2.977
GAMMA(2,5)=	.336	RTAU(2,5)=	-4993.0	CTAU(2,5)=	-4.998
GAMMA(2,6)=	.425	RTAU(2,6)=	-7334.0	CTAU(2,6)=	-7.331
GAMMA(3,4)=	.421	RTAU(3,4)=	-1677.0	CTAU(3,4)=	-1.679
GAMMA(3,5)=	.370	RTAU(3,5)=	-3695.0	CTAU(3,5)=	-3.701
GAMMA(3,6)=	.457	RTAU(3,6)=	-6037.0	CTAU(3,6)=	-6.034
GAMMA(4,5)=	.422	RTAU(4,5)=	-2017.0	CTAU(4,5)=	-2.022
GAMMA(4,6)=	.439	RTAU(4,6)=	-4356.0	CTAU(4,6)=	-4.355
GAMMA(5,6)=	.376	RTAU(5,6)=	-2310.0	CTAU(5,6)=	-2.337

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)=	.000 SEC
TIME(2)=	.884 SEC
TIME(3)=	2.182 SEC
TIME(4)=	3.861 SEC
TIME(5)=	5.883 SEC
TIME(6)=	8.216 SEC

THE MET TO A BE USED AS INPUT TO POSITION ESTIMATOR

TEMP=	6.7 DEGS C.
WIND DIRECTION=	6380 MILS
WIND SPEED=	9 KNOTS

Figure 4. Results from PASS shot S1-D341-MB-1.

DAY 341: SHOT TIME 0:55 HRS 1.640 SEC
 SOURCE 1 MIKE ARROY B
 MICS: 27,28,29,30,31,32 1/20 VALUES/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):	0:55 HRS	35.227 SEC	MIC(30):	0:55 HRS	37.967 SEC
MIC(28):	0:55 HRS	36.123 SEC	MIC(31):	0:55 HRS	41.115 SEC
MIC(29):	0:55 HRS	37.404 SEC	MIC(32):	0:55 HRS	43.419 SEC

THE WINDOW STARTING TIMES (MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
877	797	860	872	894	850

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
208128.	49282.	1073772.	15422260.	30297288.	18315863.

THE CORRELATION, TIME DIFFERENCES (MSEC), AND CORRECTED TIME DIFFERENCES (SEC) BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)=	.095	RTAU(1,2)=	-735.0	CTAU(1,2)=	-1.821
GAMMA(1,3)=	.130	RTAU(1,3)=	-2259.0	CTAU(1,3)=	-2.137
GAMMA(1,4)=	.233	RTAU(1,4)=	-3916.0	CTAU(1,4)=	-3.853
GAMMA(1,5)=	.206	RTAU(1,5)=	-5924.0	CTAU(1,5)=	-5.860
GAMMA(1,6)=	.197	RTAU(1,6)=	-7960.0	CTAU(1,6)=	-8.148
GAMMA(2,3)=	.160	RTAU(2,3)=	-1308.0	CTAU(2,3)=	-1.316
GAMMA(2,4)=	.307	RTAU(2,4)=	-3034.0	CTAU(2,4)=	-3.033
GAMMA(2,5)=	.306	RTAU(2,5)=	-5042.0	CTAU(2,5)=	-5.040
GAMMA(2,6)=	.271	RTAU(2,6)=	-7313.0	CTAU(2,6)=	-7.327
GAMMA(3,4)=	.435	RTAU(3,4)=	-1733.0	CTAU(3,4)=	-1.716
GAMMA(3,5)=	.496	RTAU(3,5)=	-3740.0	CTAU(3,5)=	-3.723
GAMMA(3,6)=	.503	RTAU(3,6)=	-6003.0	CTAU(3,6)=	-6.011
GAMMA(4,5)=	.835	RTAU(4,5)=	-2007.0	CTAU(4,5)=	-2.007
GAMMA(4,6)=	.771	RTAU(4,6)=	-4302.0	CTAU(4,6)=	-4.294
GAMMA(5,6)=	.807	RTAU(5,6)=	-2295.0	CTAU(5,6)=	-2.287

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)=	-5.860 SEC
TIME(2)=	-5.040 SEC
TIME(3)=	-3.723 SEC
TIME(4)=	-2.007 SEC
TIME(5)=	.000 SEC
TIME(6)=	2.287 SEC

THE NET TO BE USED AS INPUT TO POSITION ESTIMATOR

TEMP=	5.6 DEGS C.
WIND DIRECTION=	6380 MILS
WIND SPEED=	8 KNOTS

Figure 5. Results from PASS shot S1-D341-MB-2.

D341: SHOT TIME 12:15 HRS .768 SEC
 SOURCE: 2 MIKE OKKAY B
 MICS: 27,28,29,30,31,32 1920 VALUES/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27): 12:15 HRS 33.819 SEC	MIC(30): 12:15 HRS 35.227 SEC
MIC(28): 12:15 HRS 33.819 SEC	MIC(31): 12:15 HRS 36.567 SEC
MIC(29): 12:15 HRS 34.331 SEC	MIC(32): 12:15 HRS 38.299 SEC

THE WINDOW STARTING TIMES(MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
623	783	730	746	779	701

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
275637.	35194.	377331.	540671.	330844.	362904.

THE CORRELATION, TIME DIFFERENCES(MSEC), AND CORRECTED TIME DIFFERENCES(SEC)
 BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2) = .473	RTAU(1,2) = -14.0	CTAU(1,2) = -1.014
GAMMA(1,3) = .529	RTAU(1,3) = -498.0	CTAU(1,3) = -1.499
GAMMA(1,4) = .863	RTAU(1,4) = -1399.0	CTAU(1,4) = -1.399
GAMMA(1,5) = .420	RTAU(1,5) = -2708.0	CTAU(1,5) = -2.707
GAMMA(1,6) = .710	RTAU(1,6) = -4418.0	CTAU(1,6) = -4.418
GAMMA(2,3) = .441	RTAU(2,3) = -484.0	CTAU(2,3) = -1.484
GAMMA(2,4) = .472	RTAU(2,4) = -1384.0	CTAU(2,4) = -1.395
GAMMA(2,5) = .332	RTAU(2,5) = -2692.0	CTAU(2,5) = -2.692
GAMMA(2,6) = .421	RTAU(2,6) = -4404.0	CTAU(2,6) = -4.403
GAMMA(3,4) = .581	RTAU(3,4) = -901.0	CTAU(3,4) = -1.901
GAMMA(3,5) = .264	RTAU(3,5) = -2206.0	CTAU(3,5) = -2.209
GAMMA(3,6) = .581	RTAU(3,6) = -3920.0	CTAU(3,6) = -3.920
GAMMA(4,5) = .402	RTAU(4,5) = -1308.0	CTAU(4,5) = -1.308
GAMMA(4,6) = .626	RTAU(4,6) = -3018.0	CTAU(4,6) = -3.019
GAMMA(5,6) = .314	RTAU(5,6) = -1710.0	CTAU(5,6) = -1.711

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1) = -1.399 SEC
TIME(2) = -1.308 SEC
TIME(3) = -1.901 SEC
TIME(4) = .000 SEC
TIME(5) = 1.308 SEC
TIME(6) = 3.019 SEC

THE MICS TO BE USED AS INPUT TO POSITION ESTIMATOR

TEMP = 7.9 DEGS C.
 WIND DIRECTION = 6050 MILS
 WIND SPEED = 8 KNOTS

Figure 6. Results from PASS shot S2-D341-MB-1.

DAY 341: SHOT TIME 0:15 HRS 1.896 SEC
 SOURCE: MIKE ARRAY B
 MICS: 27,28,29,30,31,32 1920 VALUES/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):	0:15 HRS	34.971 SEC	MIC(30):	0:15 HRS	36.379 SEC
MIC(28):	0:15 HRS	34.971 SEC	MIC(31):	0:15 HRS	37.659 SEC
MIC(29):	0:15 HRS	35.483 SEC	MIC(32):	0:15 HRS	39.451 SEC

THE WINDOW STARTING TIMES(MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
742	726	677	666	686	565

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
1433169.	264966.	8322272.	21142428.	35415847.	34593879.

THE CORRELATION, TIME DIFFERENCES(MSEC), AND CORRECTED TIME DIFFERENCES(SEC) BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)=	.693	RTAU(1,2)=	5.0	CTAU(1,2)=	.014
GAMMA(1,3)=	.703	RTAU(1,3)=	-422.0	CTAU(1,3)=	-1.436
GAMMA(1,4)=	.667	RTAU(1,4)=	-1324.0	CTAU(1,4)=	-1.340
GAMMA(1,5)=	.653	RTAU(1,5)=	-2652.0	CTAU(1,5)=	-2.642
GAMMA(1,6)=	.765	RTAU(1,6)=	-1329.0	CTAU(1,6)=	-4.319
GAMMA(2,3)=	.674	RTAU(2,3)=	-455.0	CTAU(2,3)=	-1.451
GAMMA(2,4)=	.703	RTAU(2,4)=	-1359.0	CTAU(2,4)=	-1.354
GAMMA(2,5)=	.730	RTAU(2,5)=	-2656.0	CTAU(2,5)=	-2.656
GAMMA(2,6)=	.753	RTAU(2,6)=	-4333.0	CTAU(2,6)=	-4.333
GAMMA(3,4)=	.774	RTAU(3,4)=	-907.0	CTAU(3,4)=	-1.903
GAMMA(3,5)=	.756	RTAU(3,5)=	-2201.0	CTAU(3,5)=	-2.206
GAMMA(3,6)=	.724	RTAU(3,6)=	-3377.0	CTAU(3,6)=	-3.382
GAMMA(4,5)=	.795	RTAU(4,5)=	-1293.0	CTAU(4,5)=	-1.303
GAMMA(4,6)=	.753	RTAU(4,6)=	-2974.0	CTAU(4,6)=	-2.979
GAMMA(5,6)=	.784	RTAU(5,6)=	-1676.0	CTAU(5,6)=	-1.676

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)= -4.319 SEC
 TIME(2)= -4.333 SEC
 TIME(3)= -3.882 SEC
 TIME(4)= -2.979 SEC
 TIME(5)= -1.676 SEC
 TIME(6)= .000 SEC

THE MET TO BE USED AS INPUT TO POSITION ESTIMATION

TEMP= 5.4 DEGS C.
 WIND DIRECTION= 6100 MILS
 WIND SPEED= 9 KNOTS

Figure 7. Results from PASS shot S2-D341-MB-2.

DAY 341: SHOT TIME 9:15 HRS 1.768 SEC
 SOURCE 1: MKL ARMY B
 WIND: 27,28,29,30,31,32 1929 VALUES/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):	9:15 HRS	34.843 SEC	MIC(30):	9:15 HRS	36.251 SEC
MIC(28):	9:15 HRS	34.843 SEC	MIC(31):	9:15 HRS	37.531 SEC
MIC(29):	9:15 HRS	35.355 SEC	MIC(32):	9:15 HRS	39.323 SEC

THE WINDOW STARTING TIMES(MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
856	754	762	950	804	717

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
249470.	31231.	405041.	6196279.	2551576.	5881784.

THE CORRELATION, TIME DIFFERENCES(MSEC), AND CORRECTED TIME DIFFERENCES(SEC) BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)=	.144	RTAU(1,2)=	4.0	CTAU(1,2)=	-.020
GAMMA(1,3)=	.369	RTAU(1,3)=	-414.0	CTAU(1,3)=	-.416
GAMMA(1,4)=	.410	RTAU(1,4)=	-1483.0	CTAU(1,4)=	-1.498
GAMMA(1,5)=	.398	RTAU(1,5)=	-2624.0	CTAU(1,5)=	-2.631
GAMMA(1,6)=	.325	RTAU(1,6)=	-4374.0	CTAU(1,6)=	-4.353
GAMMA(2,3)=	.110	RTAU(2,3)=	-418.0	CTAU(2,3)=	-.396
GAMMA(2,4)=	.160	RTAU(2,4)=	-1490.0	CTAU(2,4)=	-1.478
GAMMA(2,5)=	.106	RTAU(2,5)=	-2519.0	CTAU(2,5)=	-2.611
GAMMA(2,6)=	.171	RTAU(2,6)=	-4334.0	CTAU(2,6)=	-4.333
GAMMA(3,4)=	.322	RTAU(3,4)=	-1109.0	CTAU(3,4)=	-1.083
GAMMA(3,5)=	.499	RTAU(3,5)=	-2208.0	CTAU(3,5)=	-2.215
GAMMA(3,6)=	.252	RTAU(3,6)=	-3938.0	CTAU(3,6)=	-3.937
GAMMA(4,5)=	.392	RTAU(4,5)=	-1142.0	CTAU(4,5)=	-1.132
GAMMA(4,6)=	.444	RTAU(4,6)=	-2844.0	CTAU(4,6)=	-2.854
GAMMA(5,6)=	.354	RTAU(5,6)=	-1702.0	CTAU(5,6)=	-1.722

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)=	-2.631 SEC
TIME(2)=	-2.611 SEC
TIME(3)=	-2.215 SEC
TIME(4)=	-1.132 SEC
TIME(5)=	.000 SEC
TIME(6)=	1.722 SEC

THE MET TO A BE USED AS INPUT TO POSITION ESTIMATOR

TEMP= 5.6 DEGS C.
 WIND DIRECTION= 6380 MILS
 WIND SPEED= 8 KNOTS

Figure 8. Results from PASS shot S2-D341-MB-4.

DAY 341: SHOT TIME: 6: 3 HRS 1.266 SEC
 SOURCE: 3 MILE ARRAY E
 MICS: 27,28,29,30,31,32 1920 VALUES/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):	6: 3 HRS	36.251 SEC	MIC(30):	6: 3 HRS	34.843 SEC
MIC(28):	6: 3 HRS	35.355 SEC	MIC(31):	6: 3 HRS	35.355 SEC
MIC(29):	6: 3 HRS	34.843 SEC	MIC(32):	6: 3 HRS	36.251 SEC

THE WINDOW STARTING TIMES(MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
799	747	824	713	709	529

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
5933733.	300650.	4848166.	19853956.	37227458.	25859578.

THE CORRELATION, TIME DIFFERENCES(MSEC), AND CORRECTED TIME DIFFERENCES(SEC) BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)=	.734	RTAU(1,2)=	908.0	CTAU(1,2)=	.902
GAMMA(1,3)=	.603	RTAU(1,3)=	1400.0	CTAU(1,3)=	1.401
GAMMA(1,4)=	.630	RTAU(1,4)=	1423.0	CTAU(1,4)=	1.429
GAMMA(1,5)=	.811	RTAU(1,5)=	1031.0	CTAU(1,5)=	1.033
GAMMA(1,6)=	.606	RTAU(1,6)=	119.0	CTAU(1,6)=	.115
GAMMA(2,3)=	.526	RTAU(2,3)=	492.0	CTAU(2,3)=	.499
GAMMA(2,4)=	.552	RTAU(2,4)=	548.0	CTAU(2,4)=	.526
GAMMA(2,5)=	.689	RTAU(2,5)=	123.0	CTAU(2,5)=	.131
GAMMA(2,6)=	.488	RTAU(2,6)=	-786.0	CTAU(2,6)=	-.787
GAMMA(3,4)=	.671	RTAU(3,4)=	22.0	CTAU(3,4)=	.027
GAMMA(3,5)=	.585	RTAU(3,5)=	-375.0	CTAU(3,5)=	-.368
GAMMA(3,6)=	.532	RTAU(3,6)=	-1281.0	CTAU(3,6)=	-1.286
GAMMA(4,5)=	.640	RTAU(4,5)=	-397.0	CTAU(4,5)=	-.395
GAMMA(4,6)=	.536	RTAU(4,6)=	-1302.0	CTAU(4,6)=	-1.313
GAMMA(5,6)=	.674	RTAU(5,6)=	-936.0	CTAU(5,6)=	-.918

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)=	1.033 SEC
TIME(2)=	.131 SEC
TIME(3)=	-.368 SEC
TIME(4)=	-.395 SEC
TIME(5)=	.000 SEC
TIME(6)=	.918 SEC

THE MET TO A BE USED AS INPUT TO POSITION ESTIMATOR

TEMP=	5.4 DEGS C.
WIND DIRECTION=	6180 MILS
WIND SPEED=	9 KNOTS

Figure 9. Results from PASS shot S3-D341-MB-2.

DAY 341: SHOT TIME 6:25 HRS 1.512 SEC
 SOURCE 7 MINE ARRAY B
 MICS: 27,28,29,30,31,32 1920 VOLS/MIC

THE STARTING TIMES FOR EACH MICROPHONE SIGNAL

MIC(27):	6:25 HRS	54.683 SEC	MIC(30):	6:25 HRS	50.075 SEC
MIC(28):	6:25 HRS	52.891 SEC	MIC(31):	6:25 HRS	49.051 SEC
MIC(29):	6:25 HRS	51.227 SEC	MIC(32):	6:25 HRS	48.411 SEC

THE WINDOW STARTING TIMES (MSEC) RELATIVE TO ABOVE

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
841	754	875	705	731	628

THE SIGNAL ENERGY WITHIN EACH WINDOW

MIC 1	MIC 2	MIC 3	MIC 4	MIC 5	MIC 6
1766708.	306684.	6485429.	18018153.	12667278.	12637918.

THE CORRELATION, TIME DIFFERENCES (MSEC), AND CORRECTED TIME DIFFERENCES (SEC) BETWEEN EACH PAIR OF MICROPHONE SIGNALS

GAMMA(1,2)=	.317	RTAU(1,2)=	1841.0	CTAU(1,2)=	1.874
GAMMA(1,3)=	.346	RTAU(1,3)=	3434.0	CTAU(1,3)=	3.462
GAMMA(1,4)=	.418	RTAU(1,4)=	4747.0	CTAU(1,4)=	4.785
GAMMA(1,5)=	.375	RTAU(1,5)=	5850.0	CTAU(1,5)=	5.863
GAMMA(1,6)=	.374	RTAU(1,6)=	6547.0	CTAU(1,6)=	6.496
GAMMA(2,3)=	.408	RTAU(2,3)=	1593.0	CTAU(2,3)=	1.588
GAMMA(2,4)=	.610	RTAU(2,4)=	2909.0	CTAU(2,4)=	2.911
GAMMA(2,5)=	.462	RTAU(2,5)=	3917.0	CTAU(2,5)=	3.929
GAMMA(2,6)=	.517	RTAU(2,6)=	4619.0	CTAU(2,6)=	4.624
GAMMA(3,4)=	.558	RTAU(3,4)=	1314.0	CTAU(3,4)=	1.323
GAMMA(3,5)=	.505	RTAU(3,5)=	2353.0	CTAU(3,5)=	2.341
GAMMA(3,6)=	.435	RTAU(3,6)=	3027.0	CTAU(3,6)=	3.036
GAMMA(4,5)=	.542	RTAU(4,5)=	1094.0	CTAU(4,5)=	1.018
GAMMA(4,6)=	.503	RTAU(4,6)=	1707.0	CTAU(4,6)=	1.713
GAMMA(5,6)=	.581	RTAU(5,6)=	599.0	CTAU(5,6)=	.650

THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION ESTIMATOR

TIME(1)=	4.785 SEC
TIME(2)=	2.911 SEC
TIME(3)=	1.323 SEC
TIME(4)=	.000 SEC
TIME(5)=	-1.018 SEC
TIME(6)=	-1.713 SEC

THE DATA TO BE USED AS INPUT TO POSITION ESTIMATOR

TEMP=	5.4 DEGS C.
WIND DIRECTION=	3180 MILS
WIND SPEED=	9 KNOTS

Figure 10. Results from PASS shot S7-D341-MB-2.

Table 3. Miss Distances for PASS Data Examples

File No.	Fig. No.	Miss Distance (Meters)	Distance to Center of Array (Meters)	Ratio of Miss Distance to Total Distance
S1-D341-MB-1.	4	430.0	12,678.5	.034
S1-D341-MB-2.	5	195.5	12,678.5	.015
S2-D341-MB-1.	5	176.4	11,784.8	.015
S2-D341-MB-2	7	192.8	11,784.8	.016
S2-D341-MB-4	8	1015.2	11,784.8	.086
S3-D341-MB-2.	9	395.54	11,471.9	.034
S7-D341-MB-2.	10	291.8	16,900.7	.017

V. CONCLUSIONS

The present edition of the "Time Difference Estimator Program" has been presented in the first three sections of this report and the results from its application to a number of arbitrarily selected signals from the PASS experiment was given in the fourth section. The results show good time duration estimates, based on the concept of miss distance; however, one should realize that with only seven samples not much can be said of the programs statistical performance other than it is looking very promising.

From Table 2 and Figures 4-10 it is seen that the program satisfactorily determined relative times such that target position could be estimated with miss distances around two hundred meters for targets of about twelve kilometers in range. It appears that as one would intuitively expect, correlation coefficients much lower than 0.5 for the time differences, Figure 4 and Figure 8, result in the considerable sized miss distances given in Table 2.

The application of the program to existing data has pointed out need for further research into several areas in order to improve the procedure.

- (1) In order to eliminate inaccurate data a threshold value for the correlation coefficient must be determined for which the associated time difference estimates with less than that threshold are claimed unreliable and discarded.
- (2) A procedure should be developed to assign realistic weights for use in the least squares procedure perhaps as a function of the normalized correlation coefficient.
- (3) The overall effectiveness of the procedure should be established by providing the variance or a bound on the variances of the time

difference estimates. This will require a theoretical development along with an examination of a large amount of data for experimental verification.

- (4) The program should be altered to present a workable procedure for handling the multiple target problem.

APPENDIX A

Time Differences Estimator Program Listing

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199C
200C

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TIME DIFFERENCES ESTIMATOR PROGRAM

GENERAL DESCRIPTION: THIS PROGRAM WILL ACCEPT A GIVEN NUMBER OF MICROPHONE SIGNALS EACH CONTAINING A SEQUENCE OF BURSTS OF DATA POINTS FROM A FIXED DATA LOGGING AND RECORDING THE TIME DIFFERENCES BETWEEN SIGNAL BURSTS THAT OCCUR WITHIN THE RECORD LENGTH.

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GLOSSARY OF VARIABLES:

NMIC= NUMBER OF MICROPHONES
 NL= NUMBER OF DATA POINTS FOR EACH MICROPHONE
 NSW= NUMBER OF POINTS IN SLIDING WINDOW
 NFW= NUMBER OF POINTS IN THE FOURIER WINDOW
 SMIC(J,I)= SIGNAL AMPLITUDE FOR MIC J AT TIME I RELATIVE TO TIC(I)
 TIC(I)= STARTING TIME FOR MICROPHONE J IN NSW RELATIVE TO BEATS
 LRST(I)= ROUGH STARTING POINT FOR MICROPHONE I RELATIVE TO TIC(I)
 NR(I)= START TIME FOR FOURIER WINDOW OF MIC I RELATIVE TO TIC(I)
 EC(I)= ENERGY WITHIN CORRELATION WINDOW FOR SIGNAL I
 TDIFF(J)= RAW TIME DIFFERENCE BETWEEN WINDOWED SIGNAL I AND J
 RTDIFF(J)= ROUGH TIME DIFFERENCE BETWEEN MICROPHONES I AND J
 DETERMINED BY CORRELATION
 CTDIFF(J)= IMPROVED TIME DIFFERENCE BETWEEN MICROPHONE I AND J BY
 LEAST SQUARES ERROR FIT(RELATIVE)
 GCMIC(J,I)= NORMALIZED CORRELATION COEFF. BETWEEN MIC I AND J SIGNALS
 GC(I)= RELIABILITY WEIGHT ASSIGNED TO RTDIFF(I) FOR THE
 LEAST SQUARE PROCEDURE
 AT(I)= TIME DIFFERENCE OF SIGNAL I RELATIVE TO MIC 1 SIGNAL
 TIME(I)= RELATIVE TIME OF THE I TH SIGNAL FOR POSITION ESTIMATOR
 ACC(I)= AUGMENTED COEFFICIENT MATRIX FOR LEAST SQUARE FIT
 VCC(I)= CONTROL VARIABLES FOR SUBROUTINE GCM
 V(1)= VARIABLES V(1) AND V(2) FOR INPUT TO GCM SUBROUTINE
 CORR(I)= OVERALL MEASURE OF CORRELATION FOR MIC I
 FREQ(I)= STARTING AND STOPPING FREQUENCY VALUES FOR 60 HZ
 CODE AND LOW PASS FILTER
 X(I)= I TH VALUE OF FIRST SIGNAL FOR CROSS CORRELATION INPUT
 I TH VALUE OF FOURIER TRANSFORM ON OUTPUT
 Y(I)= I TH VALUE OF SECOND SIGNAL FOR CROSS CORRELATION INPUT
 I TH VALUE OF FOURIER TRANSFORM ON OUTPUT
 WORK(I)= WORK PLACE SPECIFIED BY FOURG SUBROUTINE
 XX(I)= I TH VALUE OF ESTIMATE OF NOISE ENERGY SPECTRUM
 YY(I)= I TH VALUE OF ESTIMATE OF SIGNAL PLUS NOISE SPECTRUM
 ZZ(I)= VALUE OF PREDICTOR AT THE I TH FREQUENCY
 IDAY(I)= DAY OF THE START OF THE I TH MICROPHONE SIGNAL
 HOUR(I)= HOUR OF THE START OF THE I TH MICROPHONE SIGNAL
 MIN(I)= MINUTE OF THE START OF THE I TH MICROPHONE SIGNAL
 SEC(I)= SECOND OF THE START OF THE I TH MICROPHONE SIGNAL
 MIC(I)= PASS MICROPHONE NUMBER ASSOCIATED WITH MICROPHONE I

```

60:C   INITIALIZING
61:C
62:     DIMENSION IDAY(6), I HOUR(6), I MIN(6), SEC(6), MIC(6), TIME(6)
63:     DIMENSION IAU(6,6), IT(6), NR(6), F(6), RTAU(6,6), CTAU(6,6), HAU(6,6)
64:     DIMENSION SMIC(6,1920), I RST(6), G(6,6), AT(6), A(5,6), JC(6), V(2)
65:     DIMENSION CMEN(6), NCUMB(11)
66:     COMPLEX X(1024), Y(1024), WORK(1024), XX(1024), YY(1024), ZZ(1024)
67:     NML=5
68:     NL=1920
69:     NSW=342
70:     NFW=512
71:C
72:C   BRINGING IN DATA FROM MASTER FILE
73:C
74:     CALL RDATA(CMIC, MIC, IDAY, I HOUR, I MIN, SEC, TEMP, MILS, KNOTS)
75:     DO 50 I=1, NMIC
76:     ISEC=SEC(I)*1000
77:     IT(I)=I HOUR(I)*60*60*1000+I MIN*60*1000+ISEC
78:     50 CONTINUE
79:C
80:C   COMPUTATION OF ROUGH ARRIVAL TIMES
81:C
82:     DO 100 J=1, NMIC
83:     TE=0.0
84:     EMAX=0.0
85:     LMAX=0
86:     DO 90 K=1, NSW
87:     E=SMIC(J,K)*SMIC(J,K)
88:     TE=TE+E
89:     90 CONTINUE
90:     EMAX=TE
91:     LMAX=0
92:     NLF=NL-NSW
93:     DO 95 N=1, NLF
94:     TE=TE+SMIC(J,NSW+N)*SMIC(J,NSW+N)-SMIC(J,N)*SMIC(J,N)
95:     IF(TE.LT.EMAX) GO TO 95
96:     EMAX=TE
97:     LMAX=N
98:     95 CONTINUE
99:     LRST(J)=LMAX
100: 100 CONTINUE
101:C
102:C   COMPUTATION OF WINDOW STARTING POINTS
103:C
104:     DO 110 I=1, NMIC
105:     INSW=NSW/4
106:     MRST=LRST(I)-INSW
107:     IF(MRST.GT.0) GO TO 105
108:     NR(I)=0
109:     GO TO 110
110: 105 CONTINUE
111:     NF=NL-NFW
112:     IF(MRST.LT.NF) GO TO 106
113:     NR(I)=NF
114:     IT(I)=IT(I)+NF
115:     GO TO 110
116: 106 NR(I)=LRST(I)-INSW
117:     IT(I)=IT(I)+NR(I)
118: 110 CONTINUE
119:C

```

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1210C PRINTING THE WINDOW STARTING TIMES
1211C
122:      WRITE(6,2011)
123: 2011 FORMAT(22, ' THE WINDOW STARTING TIMES (MS/SEC) RELATIVE TO ABOVE ')
124:      WRITE(6,2013)
125: 2013 FORMAT(27, ' MIC 1      MIC 2      MIC 3      MIC 4      MIC 5      MIC 6')
126:      .IC 6'')
127:      WRITE(6,2010)NR
128: 2010 FORMAT(1X,6(110))
1291C
1301C COMPUTATION OF SIGNAL ENERGY WITHIN FOURIER WINDOW
1311C
132:      DO 115 J=1,NMIC
133:      SUM=0.0
134:      KSTAR=NR(J)+1
135:      KSTOP=NR(J)+NFW
136:      DO 112 K=KSTAR,KSTOP
137:      P=SMIC(J,K)*SMIC(J,K)
138:      SUM=SUM+P
139: 112 CONTINUE
140: 115 E(J)=SUM
1411C
1421C PRINTING THE SIGNAL ENERGY WITHIN EACH WINDOW
1431C
144:      WRITE(6,2007)
145: 2007 FORMAT(27, ' THE SIGNAL ENERGY WITHIN EACH WINDOW')
146:      WRITE(6,2014)
147: 2014 FORMAT(27, ' MIC 1      MIC 2      MIC 3      MIC 4      MIC 5      MIC 6')
148:      .IC 6'')
149:      WRITE(6,2008)E
150: 2008 FORMAT(6(F13.0))
1511C
1521C POSITIONING OF SIGNALS FOR DETERMINING THE CROSS CORRELATION
1531C
154:      DO 200 I=1,5
155:      NI=I+1
156:      DO 150 J=NI,NMIC
157:      KA=NR(I)
158:      DO 120 L=1,512
159:      KAL=KA+L
160:      SM=SMIC(I,KAL)
161:      X(L)=CMPLX(SM,0.0)
162:      Y(L)=CMPLX(0.0+0.0)
163: 120 CONTINUE
164:      DO 130 L=513,1024
165:      X(L)=CMPLX(0.0+0.0)
166:      KB=NR(J)
167:      KALP=KB+L-512
168:      SKAL=SMIC(J,KALP)
169:      Y(L)=CMPLX(SKAL,0.0)
170: 130 CONTINUE
171:      CALL FOURG(X,1024,-1,WORK)
172:      CALL FOURG(Y,1024,-1,WORK)
1731C
1741C DETERMINATION OF STATING POINT FOR NOISE WINDOW
1751C
176:      KXX=NR(I)-513
177:      KYY=NR(J)-513
178:      DO 125 L=1,512
179:      LI=L+512

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180:      XX(L)=CMPLX(0.0,0.0)
181:      YY(L)=CMPLX(0.0,0.0)
182:      IF (KXX.LT.1)GO TO 116
183:      MXX=1/XX(L)
184:      SXX=SMIC(1,MXX)
185:      XX(L)=CMPLX(SXX,0.0)
186: 118 CONTINUE
187:      IF (KYY.LT.1)GO TO 117
188:      MYX=YY(L)
189:      SYY=SMIC(1,MYX)
190:      YY(L)=CMPLX(SYY,0.0)
191:      GO TO 125
192: 116 XX(L)=CMPLX(0.0,0.0)
193:      GO TO 118
194: 117 YY(L)=CMPLX(0.0,0.0)
195: 125 CONTINUE
196:C
197:C DETERMINATION OF ESTIMATE OF NOISE SPECTRUM
198:C
199:      CALL FOURG(XX,1024,-1,WORK)
200:      CALL FOURG(YY,1024,-1,WORK)
201:      DO 135 L=1,1024
202:      ZZ(L)=CONJG(XX(L))
203:      XX(L)=XX(L)*ZZ(L)
204:      ZZ(L)=CONJG(YY(L))
205:      YY(L)=YY(L)*ZZ(L)
206:      YY(L)=(XX(L)+ZZ(L))/2.
207:C
208:C DETERMINATION OF ESTIMATE OF SIGNAL PLUS NOISE SPECTRUM
209:C
210:      ZZ(L)=Y(L)
211:      Y(L)=CONJG(Y(L))
212:      XX(L)=Y(L)*ZZ(L)
213:      ZZ(L)=CONJG(X(L))
214:      ZZ(L)=2*(L)*X(L)
215:      XX(L)=(XX(L)+ZZ(L))/2.
216:C
217:C COMPUTATION OF PREFILTER VALUES
218:C
219:      PRA=REAL(XX(L))
220:      PRB=REAL(YY(L))
221:      PRD=.001
222:      IF (PRA.GT.PRD)GO TO 716
223:      PREF=1.0
224:      GO TO 721
225: 716 CONTINUE
226:      PRC=PRB/PRA
227:      IF (PRC.GT.1.)GO TO 719
228:      PREF=1.0-PRC
229:      GO TO 721
230: 719 PREF=0.0
231: 721 CONTINUE
232:      ZZ(L)=CMPLX(PREF,PREF)
233:      Y(L)=X(L)*Y(L)
234:      Y(L)=Y(L)/1024.
235:C
236:C APPLICATION OF PREFILTER
237:C
238:      Y(L)=Y(L)*ZZ(L)
239:C

```

```

240:C APPLICATION OF COMB FILTER FOR 60 CYCLE AND HARMONICS
241:C
242: 130 CONTINUE
243: DATA MCOMB/1,1,10,60,65,121,126,183,188,244,249/
244: NX=MCOMB(1)
245: IF(NX.LE.0) GO TO 131
246: Y(1)=CMPLX(0.0,0.0)
247: 131 DO 133 N=2,10,2
248: NX=MCOMB(N)
249: IF(NX.LE.0) GO TO 138
250: NY=MCOMB(N+1)
251: DO 132 LL=NX,NY
252: Y(LL)=CMPLX(0.0,0.0)
253: MX=2*N*PFW+2-LL
254: Y(MX)=CMPLX(0.0,0.0)
255: 132 CONTINUE
256: 133 CONTINUE
257: 138 CONTINUE
258:C
259:C FINDING THE RAW TIME DIFFERENCES BETWEEN THE WINDOWED SIGNALS
260:C
261: CALL FOURG(Y,1024,+1,WORK)
262: CMAX=0.
263: TMAX=0.
264: DO 140 L=1,1024
265: CA=REAL(Y(L))
266: CA=ABS(CA)
267: IF(CA.LE.CMAX) GO TO 140
268: CMAX=CA
269: TMAX=L
270: 140 CONTINUE
271: TAU(1,J)=TMAX-PFW-1
272:C
273:C DETERMINATION OF THE NORMALIZED CORRELATION COEFFICIENT
274:C
275: G(I,J)=CMAX/((E(J)*E(I))**.5)
276: GAM(I,J)=G(I,J)
277: 150 CONTINUE
278: 200 CONTINUE
279:C
280:C DETERMINATION OF ROUGH TIME DIFFERENCES BETWEEN SIGNALS I AND L
281:C
282: WRITE(6,2016)
283: WRITE(6,2017)
284: 2017 FORMAT(' BETWEEN EACH PAIR OF MICROPHONE SIGNALS')
285: DO 250 I=1,5
286: KX=I+1
287: DO 240 L=KX,NMIC
288: RTAU(I,L)=FLOAT(IT(1)-IT(L))+TAU(I,L)
289: 2016 FORMAT(' THE CORRELATION, TIME DIFFERENCES(MSEC), AND CORRECTED
290: ,TIME DIFFERENCES(SEC) ')
291: 240 CONTINUE
292: 250 CONTINUE
293:C
294:C SELECTION OF MIC TO BE USED AS REFERENCE
295:C
296: CMEAS(1)=G(1,2)+G(1,3)+G(1,4)+G(1,5)+G(1,6)
297: CMEAS(2)=G(1,2)+G(2,3)+G(2,4)+G(2,5)+G(2,6)
298: CMEAS(3)=G(1,3)+G(2,3)+G(3,4)+G(3,5)+G(3,6)
299: CMEAS(4)=G(1,4)+G(2,4)+G(3,4)+G(4,5)+G(4,6)

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300:      COMEAS(5) =G(1,5)+G(2,5)+G(3,5)+G(4,5)+G(5,6)
301:      COMEAS(6) =G(1,6)+G(2,6)+G(3,6)+G(4,6)+G(5,6)
302:      CC =0.0
303:      DO 275 I=1,6
304:      IF (COMEAS(I).LT.CC) GO TO 255
305:      CC =COMEAS(I)
306:      K=I
307:      KMAX=K
308: 255 CONTINUE
309:C
310:C ESTABLISHMENT OF WEIGHTS FOR LEAST SQUARE TIME FIT
311:C
312:      DO 275 I=1,5
313:      KU=I+1
314:      DO 270 J=KU,6
315:      IF (G(I,J).LT.0.5) GO TO 266
316: 265 G(I,J)=GAM(I,J)*0.5
317:      GO TO 270
318: 266 G(I,J)=GAM(I,J)+GAM(1,J)
319: 270 CONTINUE
320: 275 CONTINUE
321:C
322:C DETERMINATION OF LEAST SQUARES TIME FIT WITH MIC(1) AS REFERENCE
323:C
324:      DO 290 I=1,4
325:      KX=I+1
326:      DO 280 J=KX,5
327:      A(I,J)=-G(I+1,J+1)
328:      A(J,I)=A(I,J)
329: 280 CONTINUE
330: 290 CONTINUE
331:      A(1,1)=G(1,2)+G(2,3)+G(2,4)+G(2,5)+G(2,6)
332:      A(2,2)=G(1,3)+G(2,3)+G(3,4)+G(3,5)+G(3,6)
333:      A(3,3)=G(1,4)+G(2,4)+G(3,4)+G(4,5)+G(4,6)
334:      A(4,4)=G(1,5)+G(2,5)+G(3,5)+G(4,5)+G(5,6)
335:      A(5,5)=G(1,6)+G(2,6)+G(3,6)+G(4,6)+G(5,6)
336:      AA=-G(1,2)*TAU(1,2)+G(2,3)*TAU(2,3)+G(2,4)*TAU(2,4)
337:      A(1,6)=AA+G(2,5)*TAU(2,5)+G(2,6)*TAU(2,6)
338:      BB=-G(1,3)*TAU(1,3)-G(2,3)*TAU(2,3)+G(3,5)*TAU(3,5)
339:      A(2,6)=BB+G(3,4)*TAU(3,4)+G(3,6)*TAU(3,6)
340:      CC=-G(1,4)*TAU(1,4)-G(2,4)*TAU(2,4)-G(3,4)*TAU(3,4)
341:      A(3,6)=CC+G(4,5)*TAU(4,5)+G(4,6)*TAU(4,6)
342:      DD=-G(1,5)*TAU(1,5)-G(2,5)*TAU(2,5)-G(3,5)*TAU(3,5)
343:      A(4,6)=DD-G(4,5)*TAU(4,5)+G(5,6)*TAU(5,6)
344:      EE=-G(1,6)*TAU(1,6)-G(2,6)*TAU(2,6)-G(3,6)*TAU(3,6)
345:      A(5,6)=EE-G(4,6)*TAU(4,6)-G(5,6)*TAU(5,6)
346:      V(1)=4
347:      CALL GJR(A,6,5,5,6,400,JC,V)
348:      AT(1)=0.
349:      DO 295 K=2,6
350:      AT(K)=A(K-1,6)
351: 295 CONTINUE
352:C
353:C ADJUSTMENT OF TIME DIFFERENCES
354:C
355:      DO 310 I=1,5
356:      KT=I+1
357:      DO 300 J=KT,6
358:      TAU(I,J)=AT(I)-AT(J)
359:      CTAU(I,J)=TAU(I,J) *FLOAT(IT(I)-IT(J))

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360:      CTAU(I,J)=CTAU(I,J)/1000.
361:C
362:C PRINTING CORRELATION COEF AND ROUGH AND CORRECTED TIME DIFFERENCES
363:C
364:      WRITE(6,2001)I,J,GAM(I,J),I,J,RTAU(I,J),T,I,CTAU(I,J)
365: 2001 FORMAT(6X,' GAMMA('11,'11,') 'F6.3,2X,'RTAU('11,'11,') 'F7.1,2X
366: .X,'CTAU('11,'11,')'F6.3)
367: 300 CONTINUE
368: 310 CONTINUE
369:C
370:C DETERMINATION OF RELATIVE TIMES FOR THE POSITION ESTIMATOR
371:C
372:      DO 620 I=1,5
373:      KX=I+1
374:      DO 610 L=KX,NMIC
375:      CTAU(L,I)=-CTAU(I,L)
376: 610 CONTINUE
377: 620 CONTINUE
378:      DO 640 J=1,6
379:      IF(J.NE.KMAX)GO TO 630
380:      TIME(J)=0.00
381:      GO TO 640
382: 630 CONTINUE
383:      TIME(J)=CTAU(J,KMAX)
384: 640 CONTINUE
385:C
386:C PRINTING THE RELATIVE TIMES FOR POSITION ESTIMATOR
387:C
388:      WRITE(6,2005)
389: 2005 FORMAT(' THE TIMES IN SEC TO BE USED FOR INPUT TO A POSITION EST
390: IMATOR')
391:      DO 503 I=1,NMIC
392:      WRITE(6,2003)I,TIME(I)
393: 2003 FORMAT(30X,'TIME('11,')='F7.3,' SEC')
394: 503 CONTINUE
395:      WRITE(6,2025)
396: 2025 FORMAT(')
397:C
398:C OUTPUTTING THE MET INFORMATION
399:C
400:      WRITE(6,2021)
401: 2021 FORMAT(' THE MET TO A BE USED AS INPUT TO POSITION ESTIMATOR')
402:      WRITE(6,2022)TEMP
403: 2022 FORMAT(32X,' TEMP='F4.1,' DEGS C.')
404:      WRITE(6,2023)MILS
405: 2023 FORMAT(22X,' WIND DIRECTION='14,' MILS')
406:      WRITE(6,2024)KNOTS
407: 2024 FORMAT(26X,' WIND SPEED='14,' KNOTS')
408:      GO TO 401
409: 400 WRITE(6,2015)
410: 2015 FORMAT(30H AN OVERFLOW HAS BEEN DETECTED )
411: 401 CONTINUE
412: STOP
413: END

```

APPENDIX B

Subroutine RDATA Program Listing

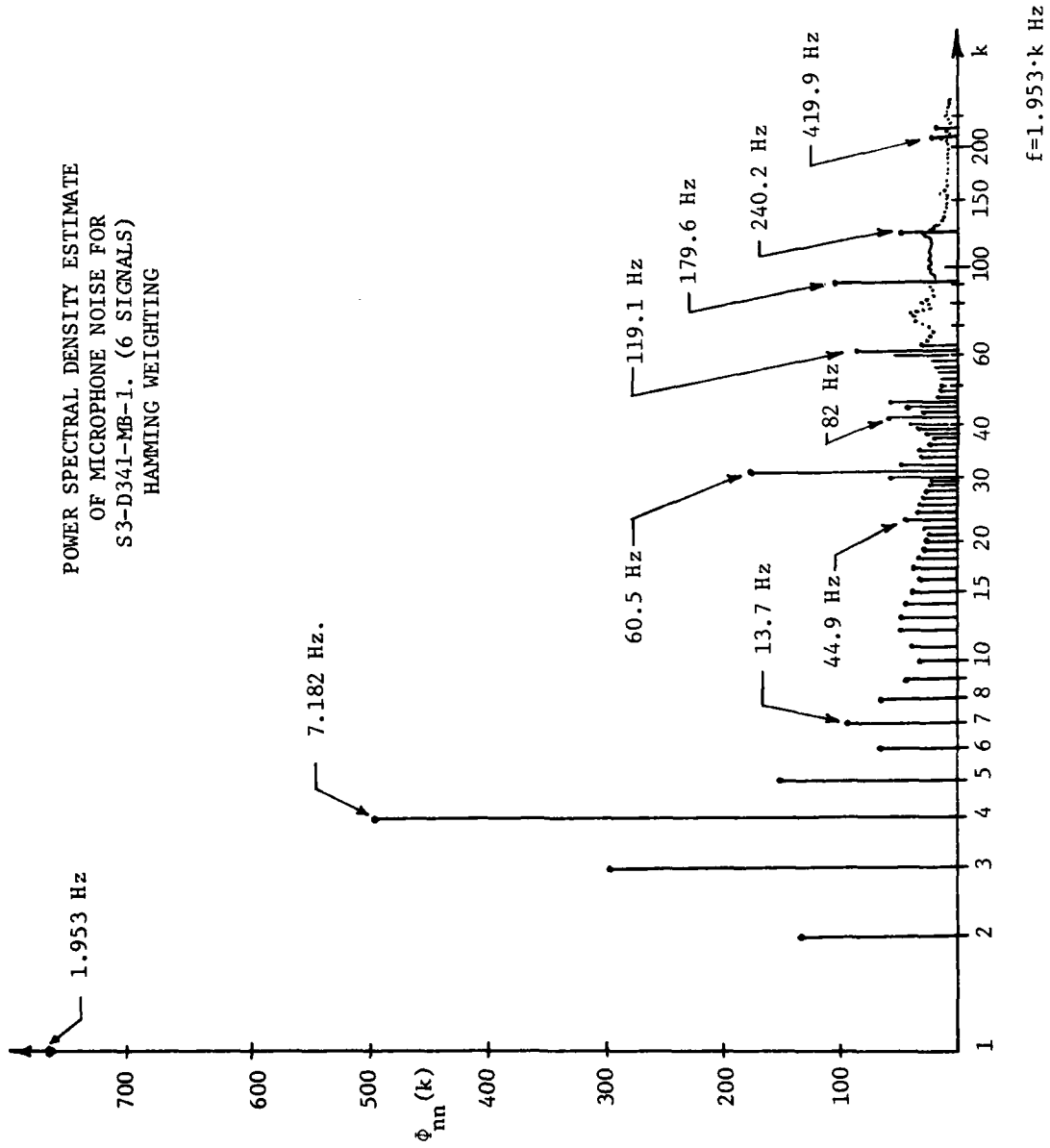
```

1:C
2:C
3:C
4:      SUBROUTINE RDATA(SMIC,M1 ,IDAY,THOUR,IMIN,SEC,TEMP,MILS,KNOTS)
5:      DIMENSION MIC(6),IDAY(6),THOUR(6),IMIN(6),SEC(6),SMIC(6,1920)
6:      INTEGER VALUES(6),VAL
7:      READ(12,111)MIKTOT,MSORC,MD,MH,MMIN,SSEC,TEMP,MILS,KNOTS
8:      111 FORMAT(I3,I3,1X,I3,1X,I2,1X,I2,1X,F6.3,3X,F4.1,1X,I4,1X,I2)
9:      MH=MH-7
10:     WRITE(6,115)
11:     115 FORMAT(////)
12:     WRITE(6,112)MD,MH,MMIN,SSEC
13:     112 FORMAT(4X,' DAY 'I3,': 'I2,': 'I2,': 'I2,': 'I2,': 'I2,': 'I2,3X,I6,' VALUES
14:     READ(12,221)
15:     221 FORMAT(5X,50H
16:     WRITE(6,221)
17:     DO 11 I=1,MIKTOT
18:     READ(12,333) VALUES(I),MIC(I),IDAY(I),THOUR(I),IMIN(I),SEC(I)
19:     THOUR(I)=THOUR(I)-7
20:     333 FORMAT(3X,I6,5X,I3,I4,I3,I3,F7.3)
21:     11 CONTINUE
22:     WRITE(6,225)MIC(1),MIC(2),MIC(3),MIC(4),MIC(5),MIC(6),VALUES(1)
23:     225 FORMAT(4X,' MICS: 'I2,': 'I2,': 'I2,': 'I2,': 'I2,': 'I2,3X,I6,' VALUES
24:     ./'MIC')
25:     WRITE(6,227)
26:     227 FORMAT(// ' THE STARTING TIMES FOR EACH MICROPHONE SIGNAL '//)
27:     DO 25 I=1,3
28:     J=I+3
29:     WRITE(6,229)MIC(I),THOUR(I),IMIN(I),SEC(I),MIC(J),THOUR(J),
30:     .IMIN(J),SEC(J)
31:     229 FORMAT(4X,' MIC('I2,'): 'I2,': 'I2,': 'I2,': 'I2,': 'I2,': 'I2,3X,I6,' VALUES
32:     .,'): 'I2,': 'I2,': 'I2,': 'I2,': 'I2,': 'I2,3X,I6,' VALUES
33:     25 CONTINUE
34:     DO 22 I=1,MIKTOT
35:     VAL=VALUES(I)
36:     READ(12,444) (SMIC(I,J),J=1,VAL)
37:     22 CONTINUE
38:     444 FORMAT(16F5.0)
39:     RETURN
40:     END

```

APPENDIX C

An Estimate of the Noise Power Spectral Density for a PASS Run



APPENDIX D

Derivation of Weighted Least Square Solution

The performance index to be minimized is given by

$$e = \sum_{i>j}^N \sum_{j=1}^N \gamma_{ij} [\tau_{ij} - (t_i - t_j)]^2$$

In this expression τ_{ij} represents the estimate of the rough time difference between signals from microphone i and j , γ_{ij} is the weight associated with that estimate, and t_i is the time of arrival of the signal at microphone i . If we select $t_1 = 0$ as a reference and use six microphones, e can be written as follows.

$$e = \gamma_{12}(\tau_{12} - (-t_2))^2 + \gamma_{13}(\tau_{13} - (-t_3))^2 + \dots + \gamma_{16}(\tau_{16} - (-t_6))^2 \\ + \sum_{i>j}^6 \sum_{j=2}^6 \gamma_{ij} [\tau_{ij} - (t_i - t_j)]^2$$

A necessary, in this case sufficient because of convexity, condition for e to be minimized is that

$$\frac{\partial e}{\partial t_i} = 0 \quad i = 2, 3, \dots, 6$$

Taking the partial derivatives of e we have the following set of simultaneous linear equations in t_2, t_3, \dots, t_6 that can be easily solved.

$$\begin{bmatrix} \alpha_2 \\ \alpha_3 \\ \alpha_4 \\ \alpha_5 \\ \alpha_6 \end{bmatrix} = - \begin{bmatrix} \gamma_{22} & \gamma_{23} & \gamma_{24} & \gamma_{25} & \gamma_{26} \\ \gamma_{23} & \gamma_{33} & \gamma_{34} & \gamma_{35} & \gamma_{36} \\ \gamma_{24} & \gamma_{34} & \gamma_{44} & \gamma_{45} & \gamma_{46} \\ \gamma_{25} & \gamma_{35} & \gamma_{45} & \gamma_{55} & \gamma_{56} \\ \gamma_{26} & \gamma_{36} & \gamma_{46} & \gamma_{56} & \gamma_{66} \end{bmatrix} \begin{bmatrix} t_2 \\ t_3 \\ t_4 \\ t_5 \\ t_6 \end{bmatrix}$$

where

$$\alpha_2 = -\gamma_{12}^T \gamma_{12} + \gamma_{23}^T \gamma_{23} + \gamma_{24}^T \gamma_{24} + \gamma_{25}^T \gamma_{25} + \gamma_{26}^T \gamma_{26}$$

$$\alpha_3 = -\gamma_{13}^T \gamma_{13} - \gamma_{23}^T \gamma_{23} + \gamma_{24}^T \gamma_{34} + \gamma_{35}^T \gamma_{35} + \gamma_{36}^T \gamma_{36}$$

$$\alpha_4 = -\gamma_{14}^T \gamma_{14} - \gamma_{24}^T \gamma_{24} - \gamma_{34}^T \gamma_{34} + \gamma_{45}^T \gamma_{45} + \gamma_{46}^T \gamma_{46}$$

$$\alpha_5 = -\gamma_{15}^T \gamma_{15} - \gamma_{25}^T \gamma_{25} - \gamma_{35}^T \gamma_{35} - \gamma_{45}^T \gamma_{45} + \gamma_{56}^T \gamma_{56}$$

$$\alpha_6 = -\gamma_{16}^T \gamma_{16} - \gamma_{26}^T \gamma_{26} - \gamma_{36}^T \gamma_{36} - \gamma_{46}^T \gamma_{46} - \gamma_{56}^T \gamma_{56}$$

and

$$\gamma_{22} = -(\gamma_{12} + \gamma_{23} + \gamma_{24} + \gamma_{25} + \gamma_{26})$$

$$\gamma_{33} = -(\gamma_{13} + \gamma_{23} + \gamma_{34} + \gamma_{35} + \gamma_{36})$$

$$\gamma_{44} = -(\gamma_{14} + \gamma_{24} + \gamma_{34} + \gamma_{45} + \gamma_{46})$$

$$\gamma_{55} = -(\gamma_{15} + \gamma_{25} + \gamma_{35} + \gamma_{45} + \gamma_{56})$$

$$\gamma_{66} = -(\gamma_{16} + \gamma_{26} + \gamma_{36} + \gamma_{46} + \gamma_{56})$$

In the present edition of the program this set of equations was solved by using a canned subroutine. If computer storage becomes a problem the solution vector can be obtained by using a form of the steepest descent algorithm.

GLOSSARY OF PROGRAM VARIABLES

NMIC = Number of Microphones

NL = Number of data points for each microphone

NSW = Number of points in the sliding window

NPFW = Number of points in the Fourier window

SMIC(J,I) = Signal amplitude for MIC J at time I relative to IT(J)

IT(I) = Starting time for microphone I in MSEC relative to blast

LRST(I) = Rough starting point for microphone I relative to IT(I)

NR(I) = Starting time (MSEC) for Fourier window for microphone signal I relative to IT(I)

E(I) = Energy within correlation window for signal I

TAU(J,I) = Raw time difference between windowed signals J and I

RTAU(J,I) = Rough time difference between signal from microphones J and I determined by correlation

CTAU(J,I) = Corrected time difference between microphone J and I by least squared error fit

GAM(J,I) = Normalized correlation coef between signals from microphones J and I

G(J,I) = Reliability weight assigned to RTAU(J,I) for the least square procedure

AT(I) = Time difference shift of signal I relative to MIC 1 signal

TIME(I) = Relative time of the Ith signal for position estimator

A(J,I) = Augmented coefficient matrix for least square fit

JC(I) = Control variable for Subroutine GJR

V(I) = Variables V(1) and V(2) for input to linear equation solution subroutine GJR

CMEAS(I) = Overall measure of correlation for microphone I

X(I) = Ith value of first signal for cross correlation on input
Ith value of Fourier transfer on output

Y(I) = Ith value of second signal for cross correlation on input
Ith value of Fourier tranform on output

WORK(I) = Work space specified by FOURG subroutine

XX(I) = Ith value of estimate of noise spectrum

YY(I) = Ith value of estimate of signal plus noise spectrum

ZZ(I) = Value at Ith freq for prefilter

IDAY(I) = Day of the start of the Ith microphone signal

IHOUR(I) = Hour of the start of the Ith microphone signal

IMIN(I) = Min of the start of the Ith microphone signal

SEC(I) = Sec of the start of the Ith microphone signal

MIC(I) = PASS microphone number associated with mic I

KMAX = Microphone number selected for reference

TEMP = Effective temperature at time of shot in Deg. C.

MILS = The effective wind direction at time of shot in mils

KNOTS = The effective wind speed at time of shot in knots

KXX = Noise window starting point for SMIC(I,L)

KYY = Noise window starting point for SMIC(J,L)

PREF = Real and imaginary value of prefilter

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