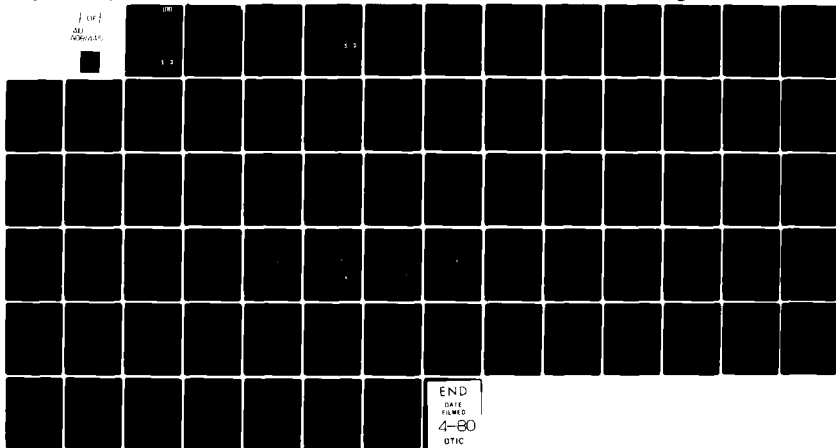


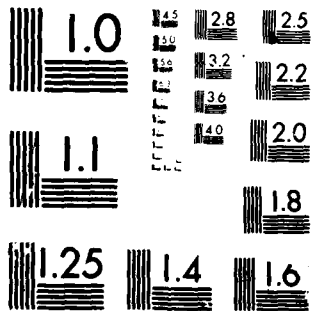
AD-A081 445

LOWELL UNIV RESEARCH FOUNDATION MA F/G 7/4  
MEASUREMENT OF NEUTRAL TEMPERATURE IN THE 120-180 KM REGION OF --ETC(U)  
MAY 79 D F KITROSSER F19628-77-C-0090  
ULRF-403/CAR AFGL-TR-79-0120 NL

UNCLASSIFIED

1 of 1  
DU  
UNCLASS





MICROCOPY RESOLUTION TEST CHART  
NATIONAL BUREAU OF STANDARDS-1963-A

AFGL-TR-79-0120

(12) LEVEL II

MEASUREMENT OF NEUTRAL TEMPERATURE IN THE  
120-180 KM REGION OF THE ATMOSPHERE FOLLOWING  
TMA RELEASES FROM A ROCKET

David F. Kitrosser

University of Lowell  
Center for Atmospheric Research  
450 Aiken Street  
Lowell, Massachusetts 01854

May 1979

Final Report for Period 17 January 1977 to 17 August 1978

Approved for public release; distribution unlimited.

AIR FORCE GEOPHYSICS LABORATORY  
AIR FORCE SYSTEMS COMMAND  
UNITED STATES AIR FORCE  
HANSCOM AFB, MASSACHUSETTS 01731

DTIC  
ELECTE  
MAR 6 1980  
S D B

THIS DOCUMENT IS BEST QUALITY PRACTICE  
THE COPY FURNISHED TO DDC CONTAINED A  
SIGNIFICANT NUMBER OF PAGES WHICH DO NOT  
REPRODUCE LEGIBLY.

80 3 4 010

AD A081445

DDC FILE COPY

Qualified requestors may obtain additional copies from the Defense Documentation Center. All others should apply to the National Technical Information Service.

## **DISCLAIMER NOTICE**

**THIS DOCUMENT IS BEST QUALITY  
PRACTICABLE. THE COPY FURNISHED  
TO DDC CONTAINED A SIGNIFICANT  
NUMBER OF PAGES WHICH DO NOT  
REPRODUCE LEGIBLY.**

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

| REPORT DOCUMENTATION PAGE                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                              |                       | READ INSTRUCTIONS<br>BEFORE COMPLETING FORM                                             |
|--------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------------|-----------------------|-----------------------------------------------------------------------------------------|
| 1. REPORT NUMBER<br>AFGL-TR-79-0120                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                    | 2. GOVT ACCESSION NO. | 3. REPORT'S CATALOG NUMBER                                                              |
| 4. TITLE (and Subtitle)<br>MEASUREMENT OF NEUTRAL TEMPERATURE IN THE<br>120-180 KM REGION OF THE ATMOSPHERE<br>FOLLOWING TMA RELEASES FROM A ROCKET                                                                                                                                                                                                                                                                                                                                                                                                    |                       | 5. TYPE OF REPORT & PERIOD COVERED<br>Final Technical Report<br>17 Jan 1977-17 Aug 1978 |
| 6. AUTHOR(s)<br>David F. Kitrosser                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                     |                       | 7. PERFORMING ORG. REPORT NUMBER<br>DLRF-403/CAR                                        |
| 8. PERFORMING ORGANIZATION NAME AND ADDRESS<br>University of Lowell, Center for<br>Atmospheric Research, 450 Aiken Street,<br>Lowell, Massachusetts 01854                                                                                                                                                                                                                                                                                                                                                                                              |                       | 9. CONTRACT OR GRANT NUMBER(s)<br>F19628-77-C-0090                                      |
| 10. CONTROLLING OFFICE NAME AND ADDRESS<br>Air Force Geophysics Laboratory<br>Hanscom AFB, Massachusetts 01731<br>Contract Monitor: Robert E. Good/LKD                                                                                                                                                                                                                                                                                                                                                                                                 |                       | 11. PROGRAM ELEMENT, PROJECT, TASK<br>AREA & WORK UNIT NUMBERS<br>61102F<br>2310/G3-AB  |
| 12. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)<br>1275                                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                       | 13. REPORT DATE<br>May 1979                                                             |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                       | 14. NUMBER OF PAGES<br>74                                                               |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                       | 15. SECURITY CLASS. (of this report)<br>Unclassified                                    |
|                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                        |                       | 15a. DECLASSIFICATION DOWNGRADING<br>SCHEDULE                                           |
| 16. DISTRIBUTION STATEMENT (of this Report)<br>Approved for public release; distribution unlimited.                                                                                                                                                                                                                                                                                                                                                                                                                                                    |                       |                                                                                         |
| 17. DISTRIBUTION STATEMENT (of abstract entered in Block 20, if different from Report)<br>DTIC ELECTE<br>MAR 6 1980<br>S D                                                                                                                                                                                                                                                                                                                                                                                                                             |                       |                                                                                         |
| 18. SUPPLEMENTARY NOTES<br>B                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                                           |                       |                                                                                         |
| 19. KEY WORDS (Continue on reverse side if necessary and identify by block number)<br>TMA Molecular Vibrational-Rotational<br>A10<br>Upper Atmosphere<br>Temperature<br>Resonance-Fluorescence                                                                                                                                                                                                                                                                                                                                                         |                       |                                                                                         |
| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number)<br>Atmospheric temperature measurements at approximately 160 km altitude over White Sands Missile Range on 24 September 1977 were made by the A10 sunlit resonance fluorescence technique. A rocket borne payload released trimethyl aluminum (TMA) in one large cloud at morning twilight. Twelve minutes of data were used to calculate temperatures at the top of the cloud averaging 628°K and at bottom averaging 578°K. The standard deviation of any one mea- |                       |                                                                                         |

DD FORM 1473  
1 JAN 73

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

409596

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

20. ABSTRACT

surement involving typically 40 seconds of data was generally between 5 and 11°K. Included in this report is the most detailed description to date of the procedures and statistical background underlying the 'A/Q Temperature' technique developed by the author over the last eleven years.

FILED  
20 0-AM  
2  
196

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

## ACKNOWLEDGEMENT

We take pleasure in acknowledging the encouragement and assistance of Dr. Dan Golomb from 1967 onward in the development of the overall technique of measuring upper atmosphere temperatures using A10.

|                                 |                                                   |
|---------------------------------|---------------------------------------------------|
| ACCESSION for                   |                                                   |
| NTIS                            | White Section <input checked="" type="checkbox"/> |
| DOC                             | Buff Section <input type="checkbox"/>             |
| UNANNOUNCED                     | <input type="checkbox"/>                          |
| JUSTIFICATION _____             |                                                   |
| BY _____                        |                                                   |
| DISTRIBUTION/AVAILABILITY CODES |                                                   |
| Dist. AVAIL. and/or SPECIAL     |                                                   |
| A                               | 23<br>G                                           |

## TABLE OF CONTENTS

|                                   | Page                                         |
|-----------------------------------|----------------------------------------------|
| 1.0 INTRODUCTION                  | 1                                            |
| 2.0 INSTRUMENTATION AND PROCEDURE | 4                                            |
| 3.0 DATA REDUCTION                | 8                                            |
| 4.0 RESULTS                       | 23                                           |
| 5.0 REFERENCES                    | 25                                           |
| APPENDIX A                        | STATISTICAL DEVELOPMENT OF FITTING PROCEDURE |
| APPENDIX B                        | VISUAL VERIFICATION OF MATCH RESULTS         |
| APPENDIX C                        | LISTING OF COMPUTER PROGRAMS                 |

## LIST OF FIGURES

| Figure No. |                                                                | Page |
|------------|----------------------------------------------------------------|------|
| 1          | The $B^2\Sigma^+$ and $X^2\Sigma^+$ Levels of the A10 Molecule | 2    |
| 2          | Observational Geometry                                         | 3    |
| 3          | Block Diagram of Field Instrumentation                         | 5    |
| 4          | Boresight TV Monitor (Typical)                                 | 6    |
| 5          | Block Diagram of Data Reduction                                | 9    |
| 6          | Dead Time Curves                                               | 13   |
| 7          | Quick Plot Sample (QPL)                                        | 14   |
| 8          | Sample of STPL Output                                          | 16   |
| 9          | Slit Function Curve                                            | 17   |
| 10         | Adjustments Used in MATCH                                      | 19   |
| 11         | Interpolation of MATCH Results (Example)                       | 21   |

## LIST OF TABLES

| Table No. |                                  | Page |
|-----------|----------------------------------|------|
| 1         | SAMPLE OUTPUT OF A10 DUMP        | 10   |
| 2         | LIGHT BOX AVERAGE (LBAVG) OUTPUT | 11   |
| 3         | WSMR A10 TEMPERATURE             | 24   |

## 1.0 INTRODUCTION

Over the last 17 years many uses of TMA (trimethyl aluminum) trails in the upper atmosphere have been made by various experimenters (Blamont et al, 1961; Armstrong, 1963; Rosenberg et al, 1964). In addition to measuring winds and diffusion rates, (Authier et al, 1962, 1963, 1964; Authier, 1964; Harang, 1964; Golomb et al, 1967, 1972; Fees et al, 1974) have also measured temperature by studying the temperature dependent vibrational-rotational intensity distribution of the blue-green system of  $\text{AlO} (\text{B}^2\Sigma^+ - \text{X}^2\Sigma^+)$  generated when TMA is exposed to sunlight in the presence of atomic oxygen (see Figure 1).

Recent experiments under the direction of AFGL (Aladdin, Aeolus, etc.) have centered around rocket released puffs of TMA on the downleg of a rocket trajectory from 180 km down to 120 km with approximately 10 km spacing (see Figure 2).

A program involving one rocket payload for winds and temperature studies was conducted at White Sands Missile Range on 24 September, 1977. In this case the rocket made only one release at approximately 160 km altitude at 5:00 A.M. local time during morning twilight ( $8^\circ$  solar depression). The experimental procedure consisted of observing the top and bottom of the cloud for 30 to 40 second periods. In general, adequate signal to noise ratio is maintained until 1 or  $2^\circ$  solar depression although, after this length of time (approximately 20 minutes) from an initial release at say  $8^\circ$  solar depression, only at the lowest altitudes 120-130 km are there "sharp" enough features to permit altitude discrimination in the spectrometer's line of sight and accurate photographic triangulation of altitude. In this program, only 12 minutes of data was taken with the above limitation being reached more quickly at the higher altitudes available in this particular experiment.

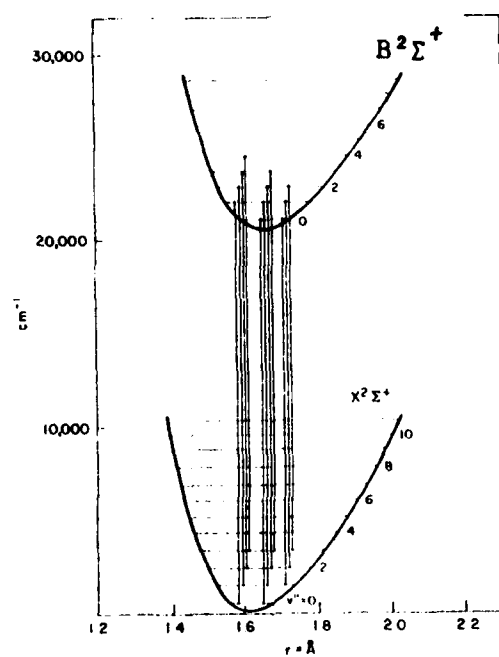


Figure 1. The  $B^2\Sigma^+$  and  $X^2\Sigma^+$  Levels of the AlO Molecule.

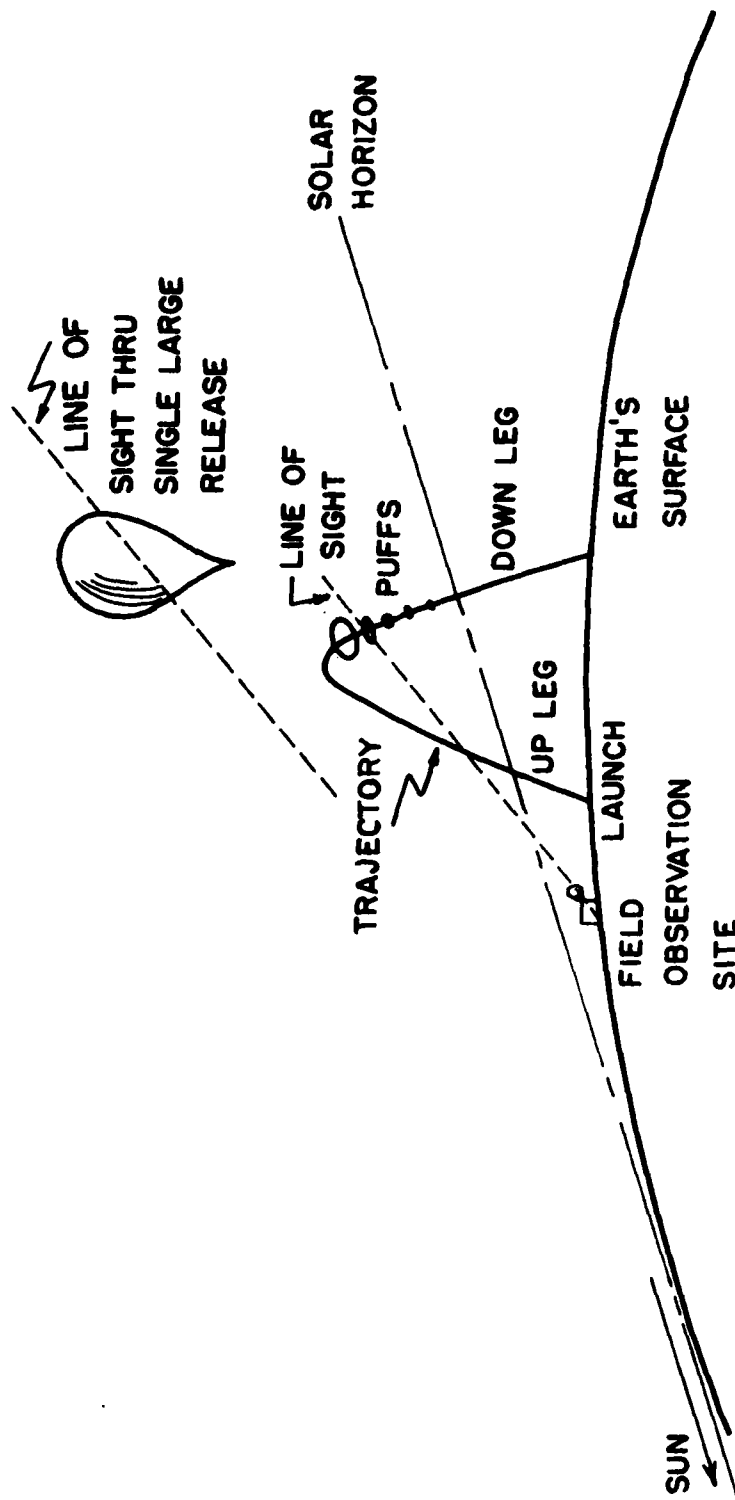


Figure 2. Observational Geometry

## 2.0 INSTRUMENTATION AND PROCEDURE

The heart of field instrumentation is a 1/2 meter Fastie-Ebert scanning spectrometer. The input optics is a 50 cm focal length F/5.0 lens which "images" the input slit upon the sky as a horizontal slit  $7^\circ$  wide by  $.06^\circ$  high. The spectrometer is co-mounted on a tripod adjustable in elevation and azimuth along with a secondary electron conduction (SEC) vidicon low light level television camera (and a 35 mm photographic camera as backup) for both boresight recording and real-time aiming of the spectrometer. The grating of the spectrometer is tilted to scan in wavelength by a synchronous motor through an adjustable cam mechanism at a rate of one scan every five seconds. Photoelectron pulses from the photomultiplier are processed with standard "nuclear" counting electronics and recorded on a high speed (60 ips) magnetic tape recorder. Also recorded are a sample of the 60 Hz waveform driving the synchronous motor scanning the spectrometer and audio comments of the person aiming the spectrometer. A block diagram of the Field Instrumentation is shown in Figure 3.

The boresight TV camera is recorded on a video tape recorder along with time from a digital clock superimposed on one corner of the video frame. Also recorded on the video tape recorder's audio channel is the commentary of the "aimer" describing what he is pointing the instrument at as well as when he is moving it or holding steady on some feature (see Figure 4).

The aimer makes use of a TV monitor for aiming in addition to various direct sights mounted on the tripod. He also has view of a chart recorder displaying the spectrum being recorded in order to ascertain the quality (amplitude) of the spectra from a particular feature.

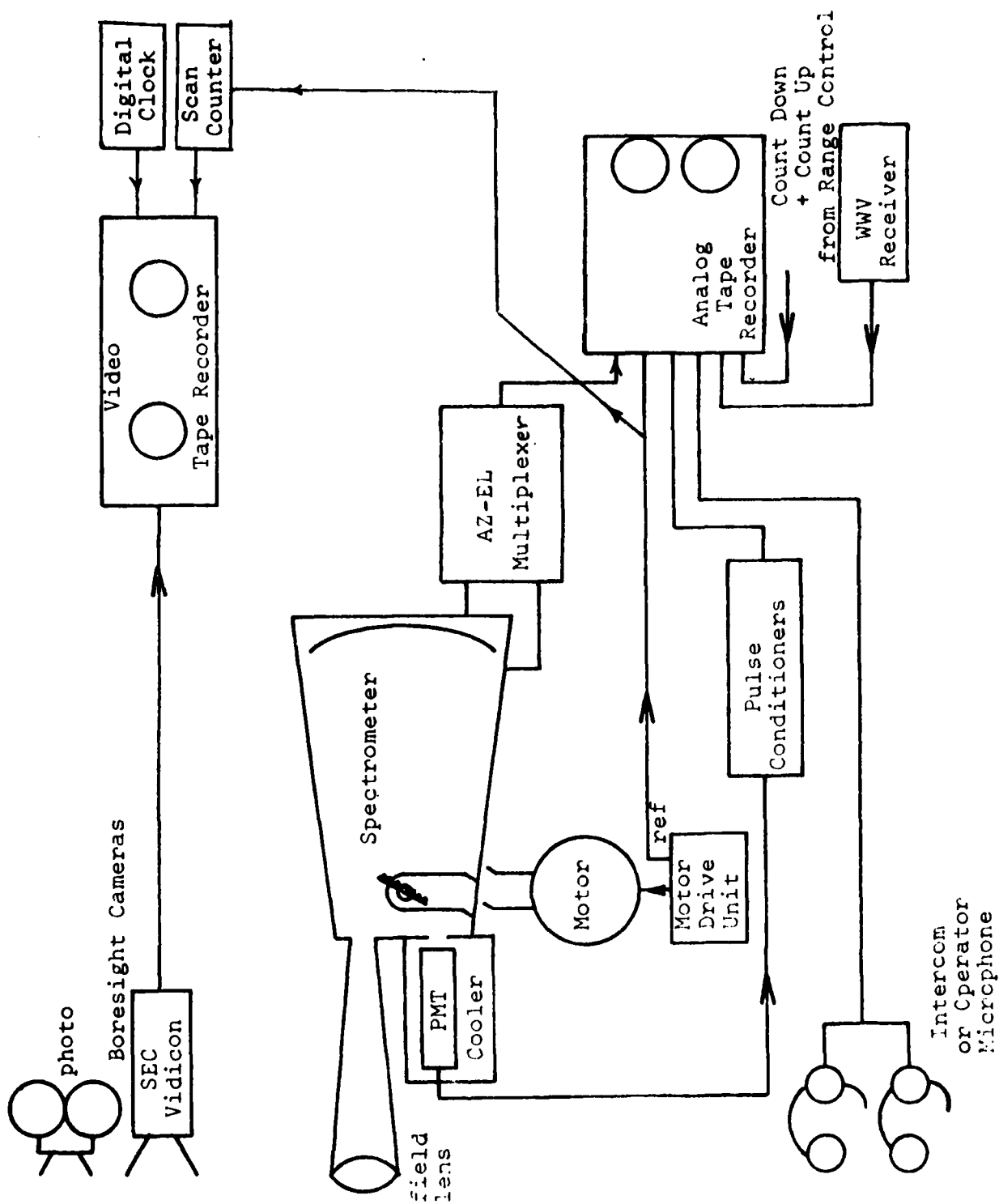


Figure 3. Block Diagram of Field Instrumentation

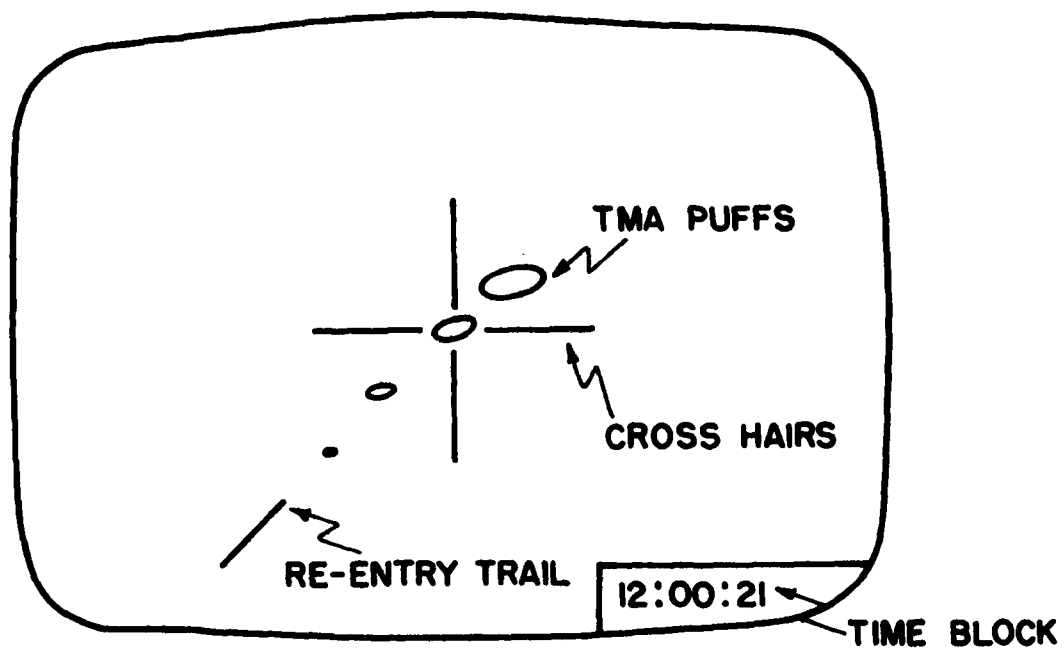


Figure 4. Boresight TV Monitor (Typical)

After the experiment certain calibrations are recorded. An iron-neon hollow cathode lamp is scanned to establish the wavelength calibration of the spectrometer and the shape of the spectrometer's slit function. A light box (LDF #6) with a radiance calibration traceable to an NBS quartz-iodine irradiance standard is scanned to establish the variation of the spectrophotometer's sensitivity with wavelength. Records of the photomultiplier output, with the spectrometer scan stopped, versus the step number of the calibrated apertures in the lightbox are used to establish the amplitude linearity of the counting-recording system. In a photon counting scheme such as this, counts are lost at higher counting rates due to "dead-time". Prior to the experiment boresight calibrations using a several kilometer distant light source are made to align all the sights as well as markers on the boresight TV monitor and fiduciarities on the photographic camera with the very narrow (vertically) field of view of the spectrometer. Later, during data reduction, playback of the TV recording of this boresight calibration will again allow us to place markers on the TV monitor used for playback.

### 3.0 DATA REDUCTION

Data reduction was carried out in the following steps. A block diagram of data reduction is shown in Figure 5.

1. Digitize Data - The tapes brought back from the field are "replayed" and the photon counts are totaled every 1/60th of a second using as a clock the recorded 60 Hz waveform originally driving the synchronous motor on the grating drive. The totaled counts are recorded on a digital tape recorder whose operation as well as the counting and interface to the analog "playback" tape recorder is handled by a microprocessor based system.

The following programs are used on the AFGL CDC 6600 computer:

2. Program CONVERS - The "stranger" type digital tape created above is converted to a SCOPE format file by CONVERS.
3. Program ALO TAPE DUMP - Prints all of the data on the high speed printer in an easy to examine format together with a running index to keep track of position along the tape (see Table 1).
4. Program LB AVG takes sections of data, that have been identified by examining the dump above as observations of the lightbox at various aperture steps, and computes the average count corresponding to the lightbox steps 0, 1, 2, 4, 8, 16, . . . ., 1024 (see Table 2).
5. Program LBT AU takes the averages computed above ( $k'$ ) plus the measured "hole factors" for each attenuator step on the light box ( $k$ ) and adjusts the parameters  $\alpha$ ,  $\beta$ ,  $\tau$  in the expression below for best fit to properly weighted values of  $k$  and  $k'$ .

$$k' = \frac{\alpha k + \beta}{1 + (\alpha k + \beta) \tau}$$



TABLE 1. SAMPLE OUTPUT OF A10 DUMP

|       | 1 | 2 | 3 | 4 | 5 | 6 | 7 | 8 | 9 | 10 | 11 | 12 | 13 | 14 | 15 | 16 | 17 | 18 | 19 | 20 | 21 | 22 | 23 | 24 | 25 | 26 | 27 | 28 | 29 | 30 | LAST WD |
|-------|---|---|---|---|---|---|---|---|---|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|----|---------|
| 11971 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11972 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11973 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11974 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11975 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11976 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11977 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11978 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11979 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11980 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11981 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11982 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11983 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11984 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11985 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11986 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11987 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11988 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11989 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |
| 11990 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0  | 0       |

TABLE 2.  
LIGHT BOX AVERAGE (LBAVG) OUTPUT

|                   | WORD                   | WORD                 | COUNT                    | APERTURE STEP  |
|-------------------|------------------------|----------------------|--------------------------|----------------|
| FILE 1            | START 12878            | END 13705            | AVERAGE 251.7            | 1024           |
| <del>FILE 1</del> | <del>START 13743</del> | <del>END 14466</del> | <del>AVERAGE 119.7</del> | <del>512</del> |
| FILE 1            | START 14475            | END 15140            | AVERAGE 63.0             | 256            |
| FILE 1            | START 15149            | END 15814            | AVERAGE 23.2             | 128            |
| FILE 1            | START 15935            | END 16646            | AVERAGE 12.7             | 64             |
| FILE 1            | START 16655            | END 17320            | AVERAGE 5.7              | 32             |
| FILE 1            | START 17409            | END 18072            | AVERAGE 3.1              | 16             |
| <del>FILE 1</del> | <del>START 18085</del> | <del>END 18722</del> | <del>AVERAGE 1.6</del>   | <del>8</del>   |
| FILE 1            | START 18809            | END 19465            | AVERAGE .9               | 4              |
| FILE 1            | START 19509            | END 20171            | AVERAGE .4               | 2              |
| FILE 1            | START 20275            | END 20977            | AVERAGE .2               | 1              |
| FILE 1            | START 21069            | END 21541            | AVERAGE .1               | 0              |
| FILE 1            | START 21740            | END 22520            | AVERAGE 29.6             | 1024           |
| <del>FILE 1</del> | <del>START 22546</del> | <del>END 23186</del> | <del>AVERAGE 11.6</del>  | <del>512</del> |
| FILE 1            | START 23170            | END 23710            | AVERAGE 6.2              | 256            |
| FILE 1            | START 23905            | END 24577            | AVERAGE 2.7              | 128            |
| FILE 1            | START 24600            | END 25267            | AVERAGE 1.0              | 64             |
| FILE 1            | START 25326            | END 26227            | AVERAGE .6               | 32             |
| FILE 1            | START 26310            | END 27177            | AVERAGE 171.7            | 1024           |
| <del>FILE 1</del> | <del>START 27120</del> | <del>END 27812</del> | <del>AVERAGE 56.0</del>  | <del>512</del> |
| FILE 1            | START 27847            | END 28577            | AVERAGE 20.7             | 256            |
| FILE 1            | START 28569            | END 29227            | AVERAGE 10.1             | 128            |
| FILE 1            | START 29280            | END 29947            | AVERAGE 5.7              | 64             |
| FILE 1            | START 29970            | END 30660            | AVERAGE 2.6              | 32             |
| FILE 1            | START 30720            | END 31377            | AVERAGE 1.0              | 16             |
| <del>FILE 1</del> | <del>START 31440</del> | <del>END 32152</del> | <del>AVERAGE .6</del>    | <del>8</del>   |
| FILE 1            | START 32160            | END 32797            | AVERAGE .3               | 4              |
| FILE 1            | START 32850            | END 33490            | AVERAGE .1               | 2              |
| FILE 1            | START 33570            | END 34177            | AVERAGE .1               | 1              |
| FILE 1            | START 34320            | END 34650            | AVERAGE .0               | 0              |
| FILE 1            | START 34320            | END 34650            | AVERAGE .0               |                |

where  $k'$  = measured counts

$k$  = output of lightbox

$\tau$  = dead time

$\alpha$  = constant of proportionality since the hole factors for the aperture steps of the lightbox are in arbitrary units, not counts

$\beta$  = an additive constant representing the dark current of the photomultiplier.

From this point forward in the data reduction the data can be corrected to remove the non-linearity introduced by the dead time inherent in the counting by the expression

$$k'' = \frac{k'}{1 - k'\tau} - \frac{\beta}{\alpha}$$

where  $k''$  is the corrected counts (see Figure 6).

6. Program KITQPL makes plots on the CRT plotter of the raw data once the starting points of the scans are established from examining the dump of data in ALO TAPE DUMP. These "quick plots" can be visually correlated with the video tape boresight record by comparing the relative amplitude of the quick plot with the apparent brightness of the ALO image in the field of view. Once this timing has been established, a table is created of sequential scan numbers on the data tape versus the identification numbers on the video boresight record (see Figure 7).
7. Program KITSTPL makes strip plots on computer printout of the data tapes. Groups of sequential scans of the same feature in the TMA release are summed. Summed scans of the lightbox are plotted this way to establish the variation of sensitivity with wavelength of the instrument using the known calibration curves of the lightbox (traceable to NBS). This slight variation of sensitivity

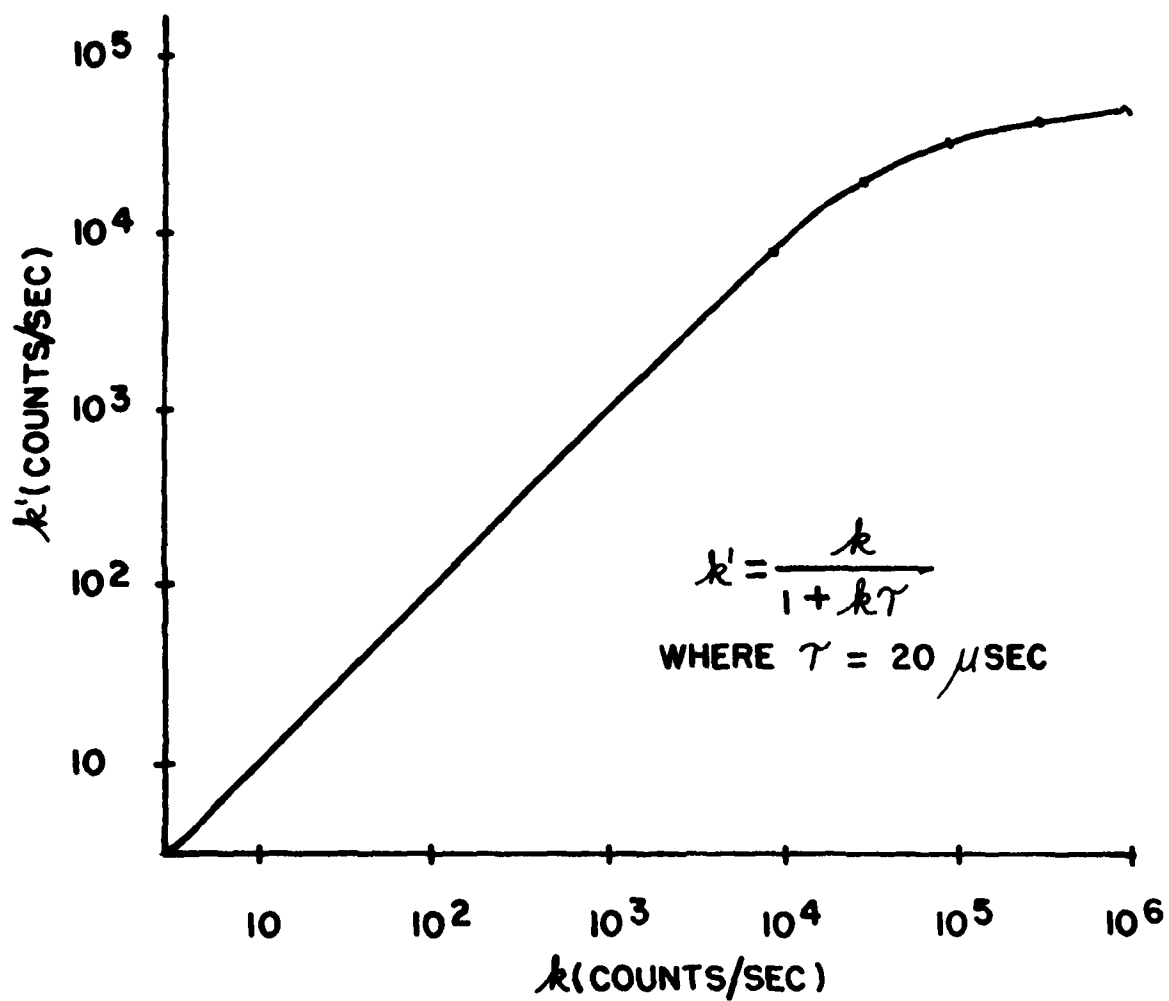


Figure 6. Dead Time Curves

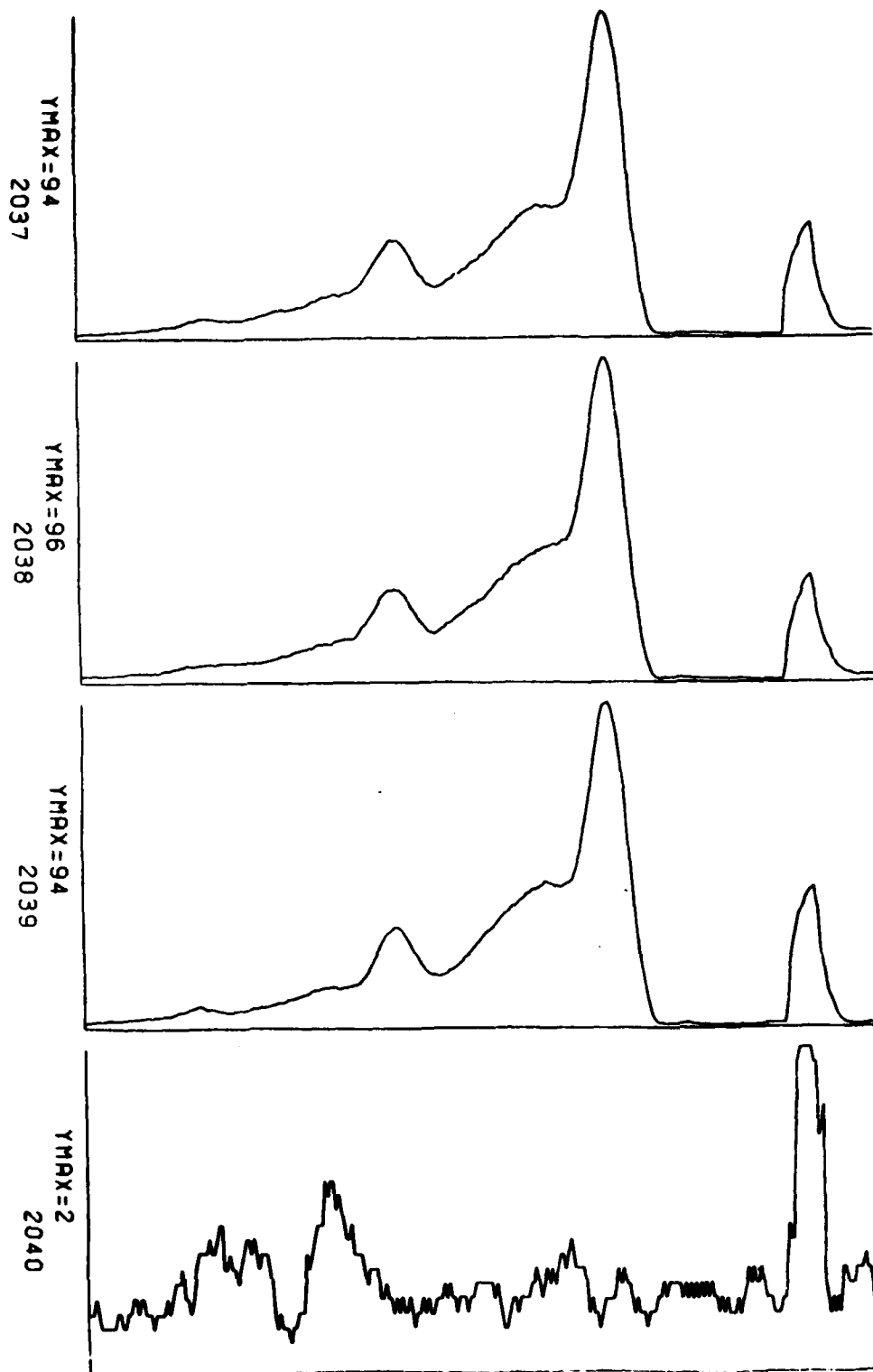


Figure 7. Quick Plot Sample (QPL)

(~5% over  $100 \text{ \AA}$ ) is used later to correct the data in MATCH (see Figure 8).

Scans of the iron hollow cathode lamp lines establish the wavelength calibration of the spectrometer system as well as the actual shape of the slit function.

8. Program KITSLIT takes the summed scans across selected lines and fits a triangular slit function to them, adjusting an arbitrary multiplicative constant, a background pedestal, the horizontal position and the width. Then scans of different lines can all be normalized and plotted on computer printout as shown in Figure 9. An accurate slit function can be deduced from this composite by hand drawing smoothed sections at the top and bottom of the straight line of the triangular function (physically, the sharp corners of the geometric optically correct triangular slit function are rounded off by diffraction).
9. Program SYN calculates a synthetic AlO spectra. The technique is similar to Harang (1966). The molecular parameters of Tyte and Nicholls (1964) are used to calculate the position of the rotational-vibrational lines. Populations of various rotational and vibrational levels are derived from the Boltzmann distribution law assuming thermal equilibrium with the ambient air which would appear to be a valid assumption up to approximately 170 km where the collision rate is 10/sec; the f-value of the AlO electronic transition is generally assumed to be 0.1 to 1.0 (Harang, 1966) implying that each molecule has 1 to 10 seconds or 10 to 100 collisions to attain thermal equilibrium between excitations. The solar excitation used is taken from the Utrecht Atlas (Minnaert et al, 1940). The band strength with Franck Condon factors is used to calculate absorption for various vibrational levels.

|     | 2     | 180 | 32 | 8 | 1 | 5077 | 110 | WSPR | DET | 1977 |
|-----|-------|-----|----|---|---|------|-----|------|-----|------|
| 91  | 9.250 |     |    | . |   |      |     |      |     |      |
| 92  | 8.750 |     |    | . |   |      |     |      |     |      |
| 93  | 7.875 |     |    | . |   |      |     |      |     |      |
| 94  | 8.750 |     |    | . |   |      |     |      |     |      |
| 95  | 9.125 |     |    | . |   |      |     |      |     |      |
| 96  | 8.500 |     |    | . |   |      |     |      |     |      |
| 97  | 9.125 |     |    | . |   |      |     |      |     |      |
| 98  | 8.625 |     |    | . |   |      |     |      |     |      |
| 99  | 8.875 |     |    | . |   |      |     |      |     |      |
| 100 | 9.625 |     | .  |   |   |      |     |      |     |      |
| 101 | 8.750 |     | .  |   |   |      |     |      |     |      |
| 102 | 9.125 |     | .  |   |   |      |     |      |     |      |
| 103 | 10.13 |     | .  |   |   |      |     |      |     |      |
| 104 | 9.000 |     | .  |   |   |      |     |      |     |      |
| 105 | 10.25 |     | .  |   |   |      |     |      |     |      |
| 106 | 9.125 |     | .  |   |   |      |     |      |     |      |
| 107 | 9.500 |     | .  |   |   |      |     |      |     |      |
| 108 | 9.875 |     | .  |   |   |      |     |      |     |      |
| 109 | 9.750 |     | .  |   |   |      |     |      |     |      |
| 110 | 11.13 |     | .  |   |   |      |     |      |     |      |
| 111 | 11.63 |     | .  |   |   |      |     |      |     |      |
| 112 | 11.38 |     | .  |   |   |      |     |      |     |      |
| 113 | 12.13 |     | .  |   |   |      |     |      |     |      |
| 114 | 13.63 |     | .  |   |   |      |     |      |     |      |
| 115 | 14.13 |     | .  |   |   |      |     |      |     |      |
| 116 | 15.25 |     | .  |   |   |      |     |      |     |      |
| 117 | 17.38 |     | .  |   |   |      |     |      |     |      |
| 118 | 16.75 |     | .  |   |   |      |     |      |     |      |
| 119 | 20.75 |     | .  |   |   |      |     |      |     |      |
| 120 | 21.00 |     | .  |   |   |      |     |      |     |      |
| 121 | 21.63 |     | .  |   |   |      |     |      |     |      |
| 122 | 22.25 |     | .  |   |   |      |     |      |     |      |
| 123 | 22.88 |     | .  |   |   |      |     |      |     |      |
| 124 | 23.50 |     | .  |   |   |      |     |      |     |      |
| 125 | 22.75 |     | .  |   |   |      |     |      |     |      |
| 126 | 22.13 |     | .  |   |   |      |     |      |     |      |
| 127 | 21.42 |     | .  |   |   |      |     |      |     |      |
| 128 | 19.36 |     | .  |   |   |      |     |      |     |      |
| 129 | 18.25 |     | .  |   |   |      |     |      |     |      |
| 130 | 16.25 |     | .  |   |   |      |     |      |     |      |
| 131 | 15.63 |     | .  |   |   |      |     |      |     |      |
| 132 | 13.50 |     | .  |   |   |      |     |      |     |      |
| 133 | 13.13 |     | .  |   |   |      |     |      |     |      |
| 134 | 12.13 |     | .  |   |   |      |     |      |     |      |
| 135 | 12.00 |     | .  |   |   |      |     |      |     |      |
| 136 | 11.38 |     | .  |   |   |      |     |      |     |      |
| 137 | 11.17 |     | .  |   |   |      |     |      |     |      |
| 138 | 11.63 |     | .  |   |   |      |     |      |     |      |
| 139 | 11.83 |     | .  |   |   |      |     |      |     |      |
| 140 | 10.33 |     | .  |   |   |      |     |      |     |      |
| 141 | 11.88 |     | .  |   |   |      |     |      |     |      |
| 142 | 11.00 |     | .  |   |   |      |     |      |     |      |
| 143 | 11.88 |     | .  |   |   |      |     |      |     |      |

Figure 8. Sample of STPL Output

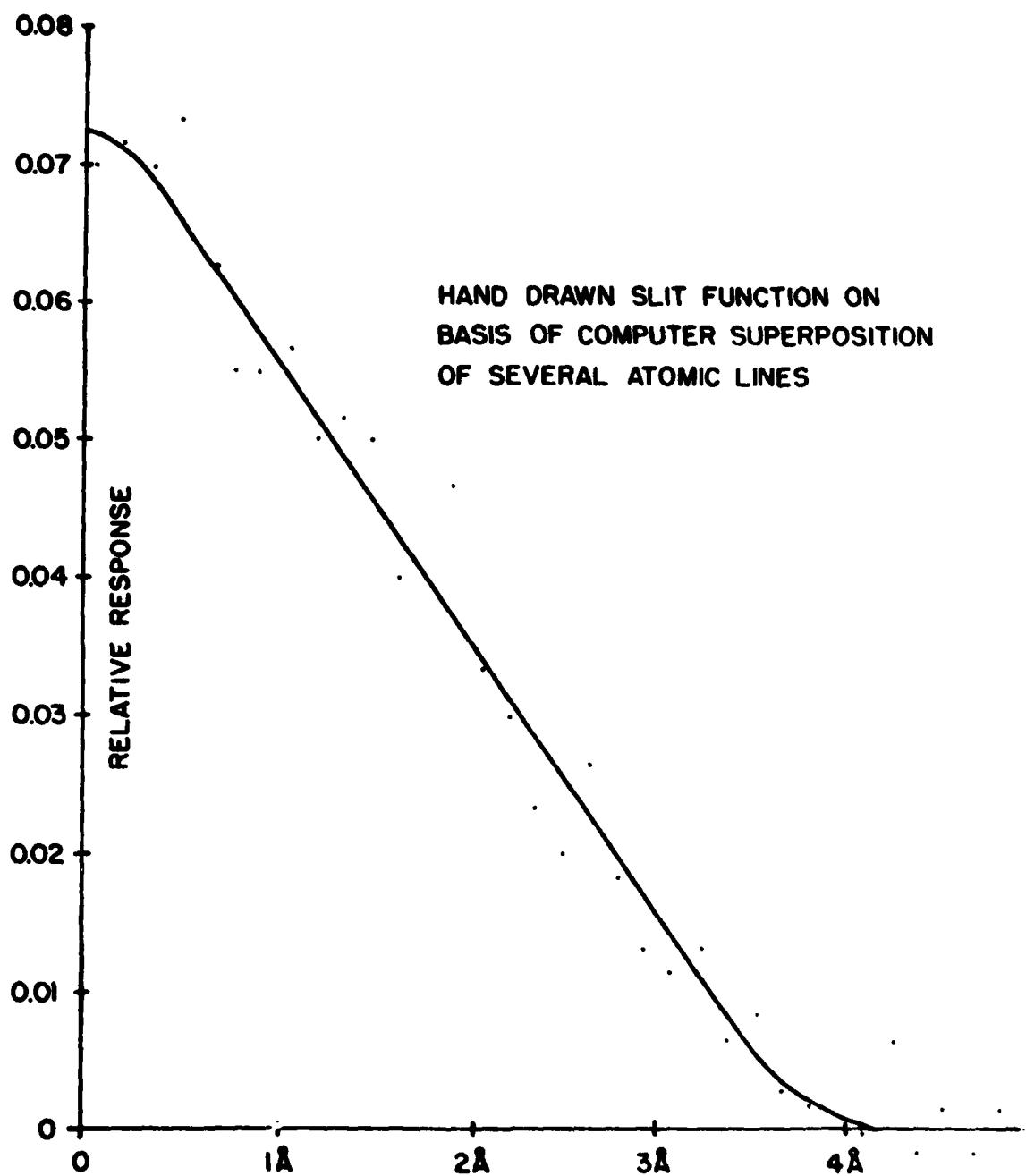


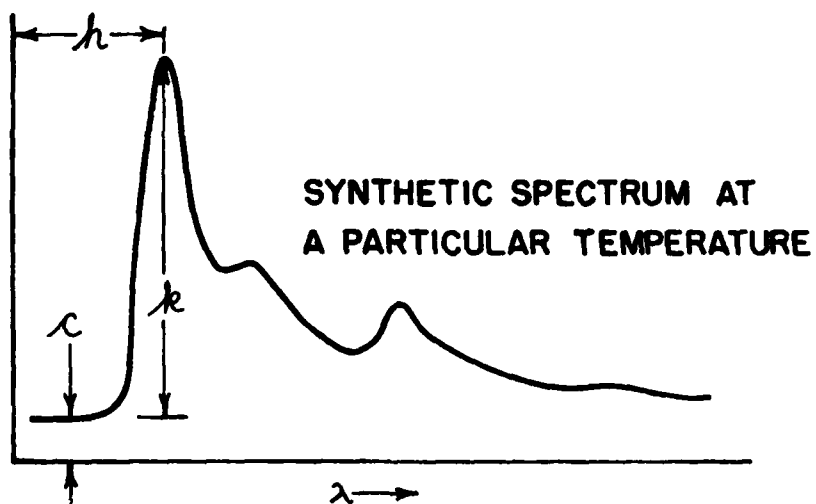
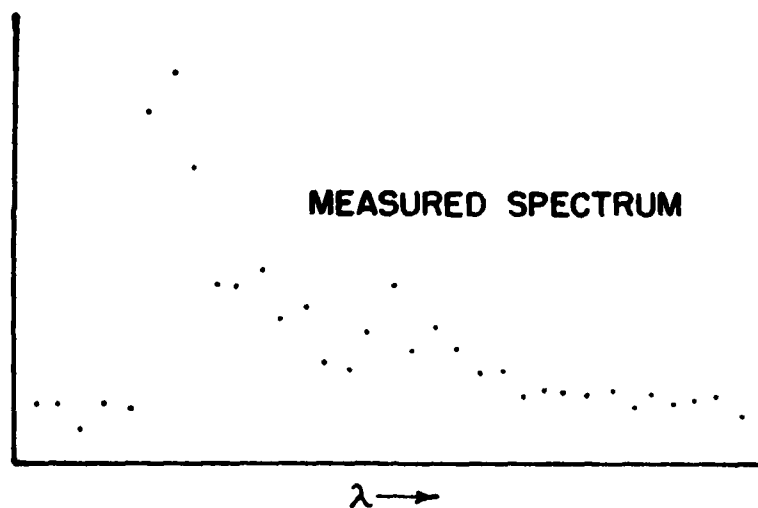
Figure 9. Slit Function Curve

Assuming dynamic equilibrium between vibrational levels and between rotational levels relative intensities can be assigned to each rotational line in the bands of a sequence.

The intensities of the first 75 rotational lines of each branch (P and R branches) in the first three bands of the  $\Delta V = 0$  sequence are then convolved with the experimentally measured slit function derived in KITSPLIT. This convolution is then tabulated every  $1/4 \text{ \AA}$  and every 50 degrees from 150°K to 1050°K and stored as a permanent file. Plots of synthetic spectra are shown in Appendix B.

10. Program MATCH is the heart of the data reduction scheme. Inputs to MATCH are synthetic spectra from SYN already convolved with the slit function at 19 temperatures and the digitized spectrometer output. Groups of scans are summed or lumped as determined by the examination of quick plots from KITQPL and the study of the boresight records. The spectrometer output is then corrected for amplitude non-linearity or dead-time with subroutine FKAY using constants supplied by program KITAU. Correction is then made for variation of sensitivity with respect to wavelength using a linear approximation derived from the calibration scans of the lightbox.

The data points in the lumped measured scans are then compared to each of the 19 synthetic spectra. Iterative adjustments are made to the exact horizontal (wavelength) position of the measured scan, a multiplicative factor which scales the synthetic spectra to the measured scan, and an additive constant which is added under the synthetic spectra as a pedestal. The iterative adjustments of the three variables described above and shown graphically in Figure 10 are made using as a criterion for best fit of the measured points to the synthetic curve the likelihood that the measured points result from a curve



**ADJUSTMENTS TO OBTAIN OPTIMUM FIT**

$c$  = ADDITIVE CONSTANT = BACKGROUND PEDESTAL

$k$  = MULTIPLICATIVE CONSTANT = SCALING FACTOR

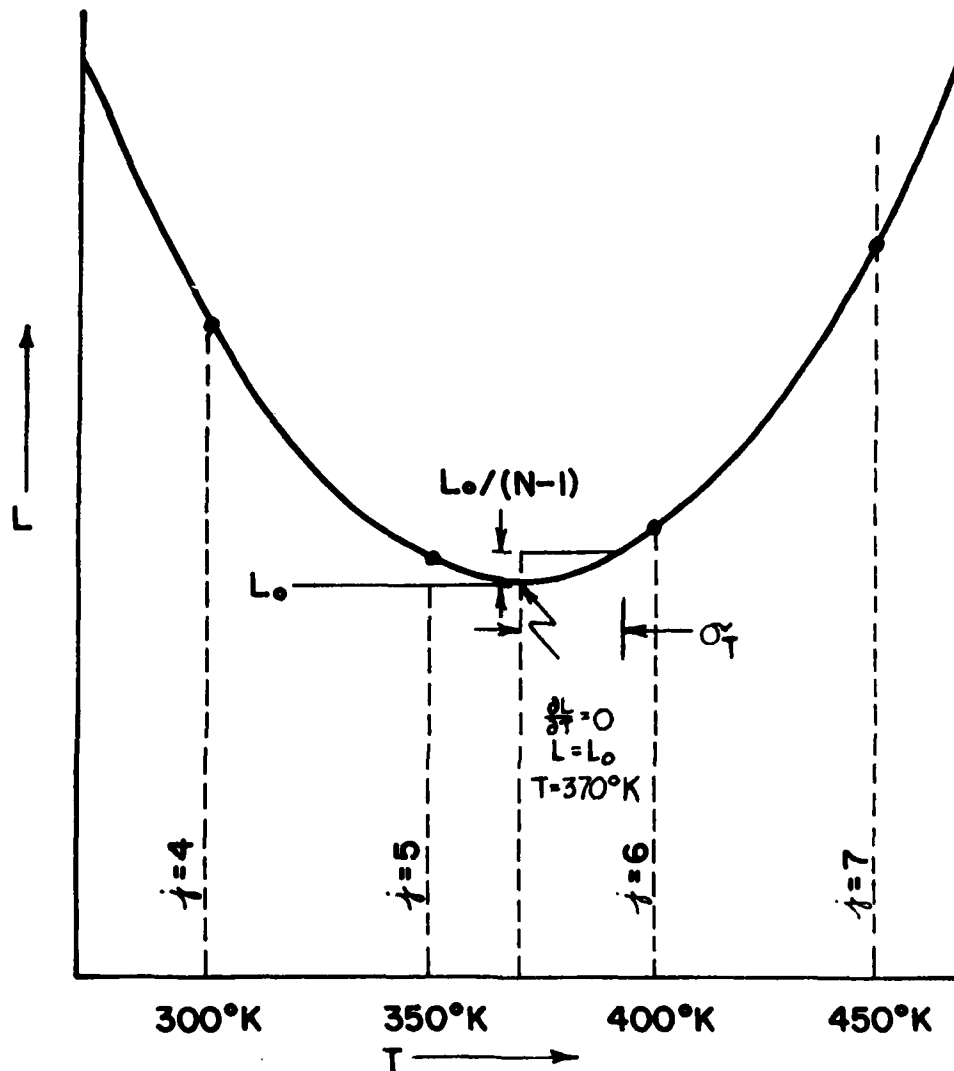
$h$  = HORIZONTAL SHIFT = WAVELENGTH ADJUSTMENT

Figure 10. Adjustments Used in MATCH

same as the synthetic but made noisy according to Poisson statistics. The likelihood function is the product of the probabilities at each point in the measured scan that the point results from Poisson distributed errors about a point at the same wavelength in the synthetic spectrum. Incidentally, this type of maximum likelihood function procedure simplifies to become a least square fit when the errors in the measurement are Gaussian. It has been determined that in this application, involving counting randomly arriving photons which is properly described by Poisson statistics, with a fairly low number of counts at each point in the measured spectrum, considering that Gaussian statistics become a poorer approximation to Poisson statistics at smaller counts with a consistent bias from the skewed nature of the Poisson distribution and that the temperature deduced by this technique varies monotonically with the slope of the data points, use of least squares fitting rather than the maximum likelihood technique based on Poisson statistics results in a systematic error of as much as 15 degrees.

The temperature of the synthetic spectrum producing the maximum likelihood function as well as the next higher and next lower temperature and the three corresponding values of the likelihood function are used to generate a parabolic curve for a parabolic interpolation (see Figure 11). The peak of this parabola is used as the interpolated temperature of best fit. More details are supplied in Appendix A.

In Appendix B plots of the fourteen "lumped" or summed scans of measured spectra are shown along with five synthetic spectra closest in temperature to each of the measured spectra. The measured spectra are corrected for dead-time amplitude non-linearity and the variation of instrumental sensitivity with respect to wavelength.



WHERE:

$N$  = NO. OF INDEPENDENT MEASUREMENTS

$\sigma_T$  = STD. DEVIATION OF TEMPERATURE MEASUREMENT

$L$  = SUM OF SQUARES (OR EQUIVALENT FOR POISSON STATISTICS)

$T$  = TEMPERATURE

Figure 11. Interpolation of MATCH Results (Example)

The measured spectra as well as the five synthetic spectra are normalized to peak at 100 on the two decade 1 to 100 scale. The synthetic spectra are shown "sitting on top of" a pedestal  $C_j/k_j$  where  $C_j$  and  $k_j$  are the constants derived by the fitting procedure for best match of the particular synthetic spectrum to the measured spectrum. Even though only the region from 4824 Å to 4886 Å is used in the fitting procedure, more of the measured spectrum including part of the spectrometer return sweep is shown on the plot.

#### 4.0 RESULTS

The results of the September 1977 White Sands temperature measurements are summarized in Table 3. Since there was only one puff or cloud, the data was taken from points near the top and near the bottom of the cloud rather than from the center of each in a series of small puffs as would usually be done in this sort of experiment. An average temperature for the observations of the top of the cloud weighted by  $1/\sigma^2$  is 622°K with an overall  $\sigma$  of 22°K. Disregarding the three weak measurements where there may have been instrumental problems, the average is 628°K with a  $\sigma$  of 16°K. An average temperature for the observations of the bottom of the cloud with or without the two weak measurements was 578°K with an overall  $\sigma$  of 14°K.

Some of the scatter of individual measurements, particularly at the bottom of the cloud, is a result of having in the line of sight to the bottom, the more rapidly diffusing upper part of the cloud. In general, only the earliest measurements of A10 at altitudes as high as these are accurate for reasons of altitude spread along the line of sight through the cloud.

Better altitude resolution could have been had if the elevation angle of the line of sight were to have been lower; however, in the case of the White Sands site the logistic requirements precluded moving the observation site back 100-200 km as would have been preferred. Also the accident of having a very large release over perhaps 7-10 km rather than the smaller "point" releases did not aid the altitude precision either.

# WSMR A10 TEMPERATURE

24 September 1977

File No. 2 AMUL = 0.3010

Calculations 19 June 78

| Description | Scan No. | Sum | Peak  | Max. Amp. | Time     | Temp. [°K] | $\sigma$ |
|-------------|----------|-----|-------|-----------|----------|------------|----------|
| TOP 1       | 8        | 7   | 210.5 | 117       | 11:59:38 | 650        | 6        |
| BOT 1       | 16       | 8   | 207.4 | 63        | 12:00:21 | 571        | 8        |
| BOT 2       | 24       | 8   | 204.2 | 80        | 12:01:01 | 574        | 7        |
| BOT 3       | 32       | 8   | 201.5 | 101       | 12:01:41 | 601        | 7        |
| TOP 2       | 49       | 5   | 194.9 | 210       | 12:02:58 | 621        | 6        |
| BOT 4       | 54       | 3   | 193.8 | 130       | 12:03:18 | 606        | 11       |
| BOT 5       | 58       | 9   | 191.5 | 13 Weak   | 12:03:53 | 600        | 20       |
| TOP 3       | 68       | 8   | 186.1 | 23 Weak   | 12:04:41 | 574        | 16       |
| TOP 4       | 76       | 9   | 183.5 | 23 Weak   | 12:05:23 | 594        | 13       |
| TOP 5       | 86       | 5   | 179.7 | 23 Weak   | 12:06:03 | 575        | 18       |
| BOT 6       | 93       | 6   | 177.9 | 11 Weak   | 12:06:41 | 572        | 29       |
| BOT 7       | 100      | 8   | 175.0 | 91        | 12:07:21 | 569        | 6        |
| BOT 8       | 122      | 11  | 166.2 | 78        | 12:09:18 | 570        | 5        |
| TOP 6       | 136      | 7   | 160.0 | 118       | 12:10:18 | 614        | 6        |

TABLE 3

## 5.0 REFERENCES

1. Armstrong, E. B., Planet. Space Sci., 11, 733 (1963).
2. Authier, B., Ann. Geophys., 20, No. 4, 356 (1964).
3. Authier, B., J. Blamont and G. Carpentier, Mesure de la temperature de l'ionosphere a partir du spectre de rotation de la molecule AlO, Compt. Rend., 255, 1974 (1962).
4. Authier, B., Blamont, J. E. and Carpentier, G., Ann. Geophys., 20, No. 3, 342 (1964).
5. Authier, B., Blamont, J. E., Carpentier, G. and Herse, M., C. R. Acad. Sc. Paris, 256, 3870 (1963).
6. Blamont, J. E., Hieblot, J. and Selzer, E., C. R. Acad. Sc. Paris, 252, 3317 (1961).
7. Dyer, G. L., private communication, AFCRL (1969).
8. Golomb, D., O. Harang and F. P. DelGreco, Upper atmosphere densities and temperatures at 105-165 km from diffusion and spectral intensity of AlO trails, J. Geophys. Res., 72, 2365 (1967).
9. Golomb, D., D. F. Kitrosser and R. H. Johnson, Thermosphere structure over Churchill and Hawaii, in Space Research XII, Akademie Verlag, Berlin (1972).
10. Harang, O., Planet. Space Sci., 12, 567 (1964).
11. Harang, O., AlO resonant spectrum for upper atmosphere temperature determination, AFCRL Tech. Report, AFCRL-36-314, May 1966.
12. Minnaert, M., Mulders, M. F. W. and Houtgast, J., Photometric Atlas of the Solar Spectrum ("Utrecht Atlas"), Kampert and Helm, Amsterdam (1940).
13. Rees, D., D. F. Kitrosser and D. Golomb, Combined temperature, diffusion coefficient and density measurements of photoluminescent AlO releases, in Space Research XIV, Akademie Verlag, Berlin (1974).
14. Rosenberg, N. W., Golomb, D. and Allen, E. F., Jr., J. Geophys. Res., 69, No. 7, 1451 (1964).
15. Tyte, D. C. and Nicholls, R. W., Identification Atlas of Molecular Spectra, Univ. of W. Ontario (1964).

A P P E N D I X    A

STATISTICAL DEVELOPMENT OF FITTING PROCEDURE

## APPENDIX A

The general likelihood function where the error distributions at each point are independent is

$$L_j = \prod_{i=1}^n P_{\lambda_{ij}}(y_i) \quad (1)$$

where  $y_i$  = table of values representing measurements at successive points in the measured spectrum.

$P_{\lambda_{ij}}(y_i)$  = the probability that a point in the spectrum having a long term average  $\lambda_{ij}$  would be measured as  $y_i$  in a single measurement.

$$\lambda_{ij} = k_j z_{ij} + C_j \quad (2)$$

where  $z_{ij}$  = table of values of synthetic spectra at wavelengths corresponding to  $y_i$  at the same  $i$  index and temperature  $j$ .

$k_j$  = an arbitrary multiplicative factor used to scale the synthetic spectrum to the measured spectrum and will be optimized to obtain the maximum likelihood at a given  $j$ .

$C_j$  = an arbitrary additive constant added to the synthetic spectrum to represent a constant background or pedestal under the measured spectrum. It will be optimized same as  $k_j$ .

In this case where the distribution of individual measurements about a long term average is a Poisson distribution

$$P_{\lambda_{ij}}(y_i) = \frac{(\lambda_{ij})^{y_i} e^{-\lambda_{ij}}}{(y_i)!} \quad (3)$$

Combining (1), (2) and (3) and taking the logarithm of both sides

$$\ln L_j = \sum_{i=1}^n [y_i \ln(k_j z_{ij} + C_j) - (k_j z_{ij} + C_j) - \ln(y!)] \quad (4)$$

It is necessary now to find the maximum likelihood of  $\ln L_j$  as a function of  $k_j$ ,  $C_j$  and  $j$  independently. The third term in (4) is not a function of the above so it can be ignored for the time being. At any given  $j$  then the optimum  $k_j$  and  $C_j$  are those which allow the partial derivatives below (5), (6) to be zero

$$\frac{\partial \ln L_j}{\partial k_j} = 0 = \sum_{i=1}^n \left[ \frac{y_i z_{ij}}{k_j z_{ij} + C_j} - z_{ij} \right] \quad (5)$$

$$\frac{\partial \ln L_j}{\partial C_j} = 0 = \sum_{i=1}^n \left[ \frac{y_i}{k_j z_{ij} + C_j} - 1 \right] \quad (6)$$

Unfortunately there is no analytic solution for  $k_j$  and  $C_j$  as in the analogous procedure for a Gaussian distribution (least squares). The Newton Rapsohn method will be used to effect a solution.

$$f_j(k_j, C_j) = 0 = \sum_{i=1}^n \frac{y_i z_{ij}}{k_j z_{ij} + C_j} - \sum_{i=1}^n z_{ij} \quad (7)$$

$$g_j(k_j, C_j) = 0 = \sum_{i=1}^n \frac{y_i}{k_j z_{ij} + C_j} - n \quad (8)$$

in general

$$\begin{aligned} f(k_0 + \delta_k, C_0 + \delta_C) = 0 &= f(k_0, C_0) + \delta_k \frac{\partial f(k_0, C_0)}{\partial k} \\ &+ \delta_C \frac{\partial f(k_0, C_0)}{\partial C} \end{aligned} \quad (9)$$

$$\begin{aligned} g(k_0 + \delta_k, C_0 + \delta_C) = 0 &= g(k_0, C_0) + \delta_k \frac{\partial g(k_0, C_0)}{\partial k} \\ &+ \delta_C \frac{\partial g(k_0, C_0)}{\partial C} \end{aligned} \quad (10)$$

solving the right-hand side of both equations.

$$\delta_k = \frac{g \frac{\partial b}{\partial c} - f \frac{\partial g}{\partial c}}{\frac{\partial b}{\partial k} \frac{\partial g}{\partial c} - \frac{\partial f}{\partial c} \frac{\partial g}{\partial k}} \quad (11)$$

$$\delta_c = \frac{f \frac{\partial g}{\partial k} - g \frac{\partial f}{\partial k}}{\frac{\partial f}{\partial k} \frac{\partial g}{\partial c} - \frac{\partial f}{\partial c} \frac{\partial g}{\partial k}} \quad (12)$$

initial values of  $k_0$  and  $C_0$  are

$$k_0 = y_{\max} - y_{\min} \quad (13)$$

$$C_0 = y_{\min} \quad (14)$$

new values for  $k$  and  $C$  are

$$k = k_0 + \delta_k \quad (15)$$

$$C = C_0 + \delta_c \quad (16)$$

which are iterated until  $\delta k/k$  and  $\delta C/C$  are both less than  $10^{-8}$  or so. Convergence to the  $10^{-8}$  criteria takes five or six iterations.

Once optimum  $k_j$  and  $C_j$  values are found corresponding to a particular  $T_j$  the actual likelihood function at each  $j$  can be computed. The  $T_j$  at which the likelihood function is maximum is the temperature of best fit. The preceding  $T_j$  along with  $T_{j+1}$  and  $T_{j+2}$  are used to generate a parabola

$$L = AT^2 + BT + C \quad (17)$$

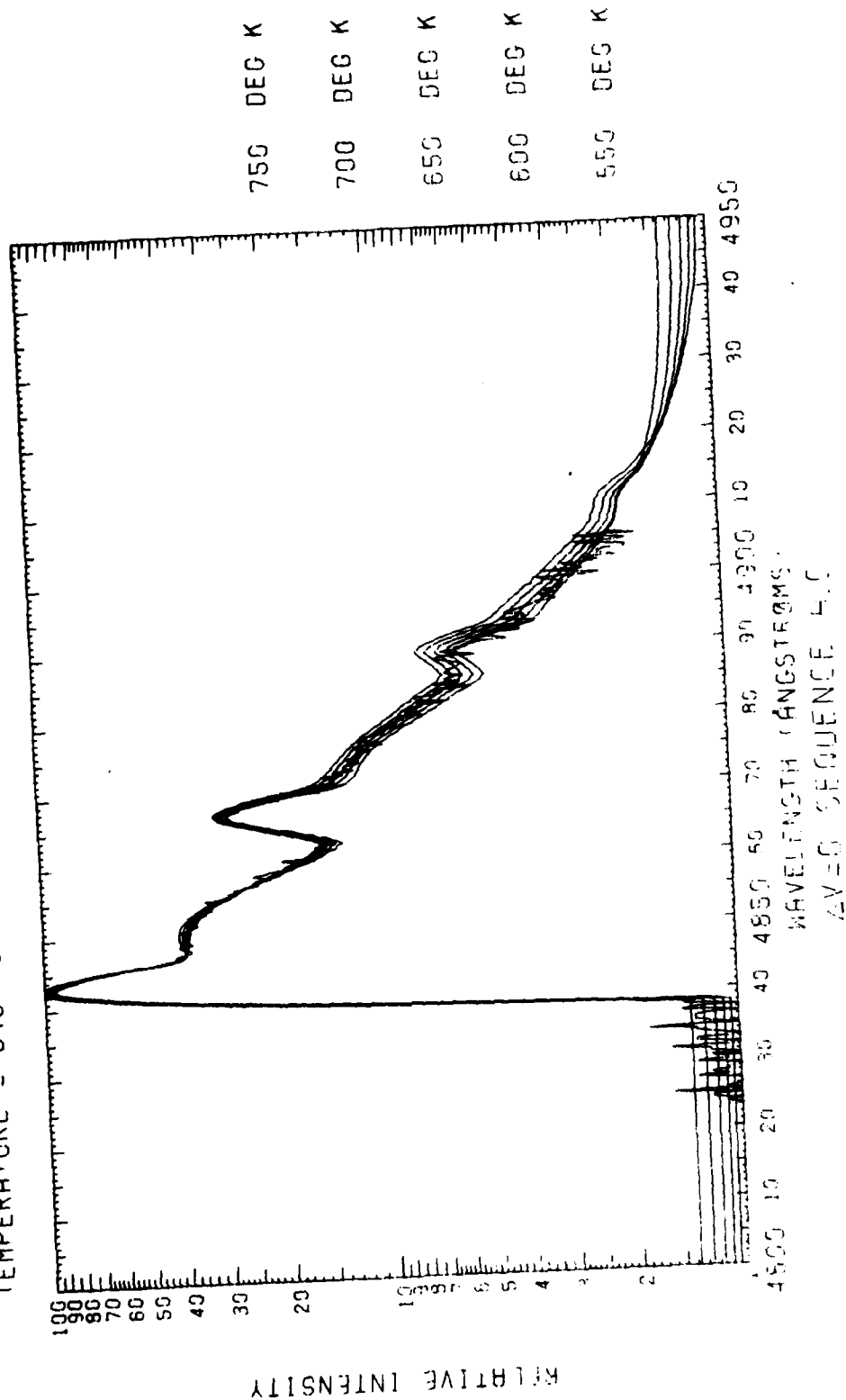
The peak of the parabola, where  $\partial L/\partial T = 0$  is used to indicate an interpolated value of  $T$ . The shape of the parabola near the peak is used to deduce a  $\sigma_T$  in a manner similar to Dyer (1970, unpublished) for least squares fitting (see Figure 11).

A P P E N D I X    B

VISUAL VERIFICATION OF MATCH RESULTS

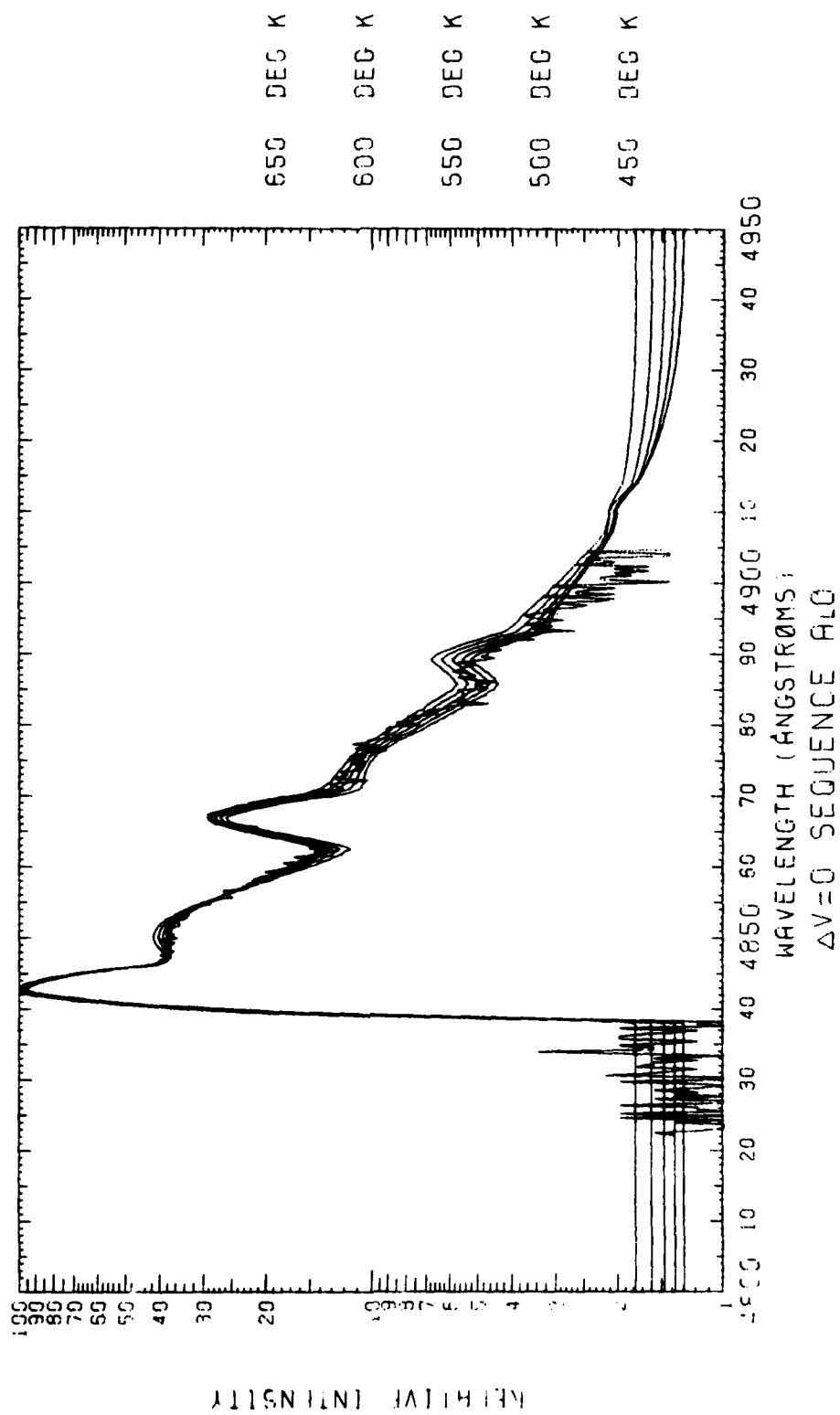
SCAN NOS. 2 8 7

TEMPERATURE = 648 +OR- 6 DEG K

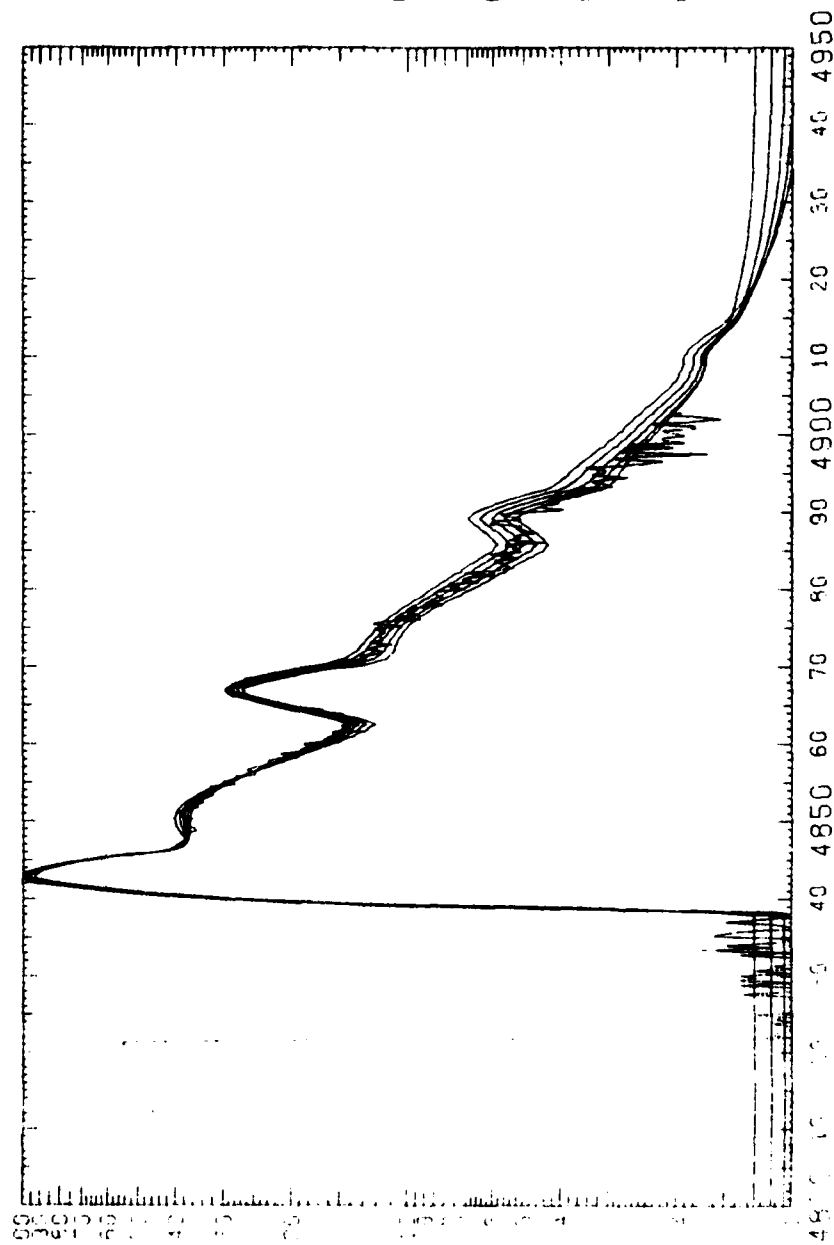


SCAN NOS. 2 16 8

TEMPERATURE = 573 +OR- 8 DEG K



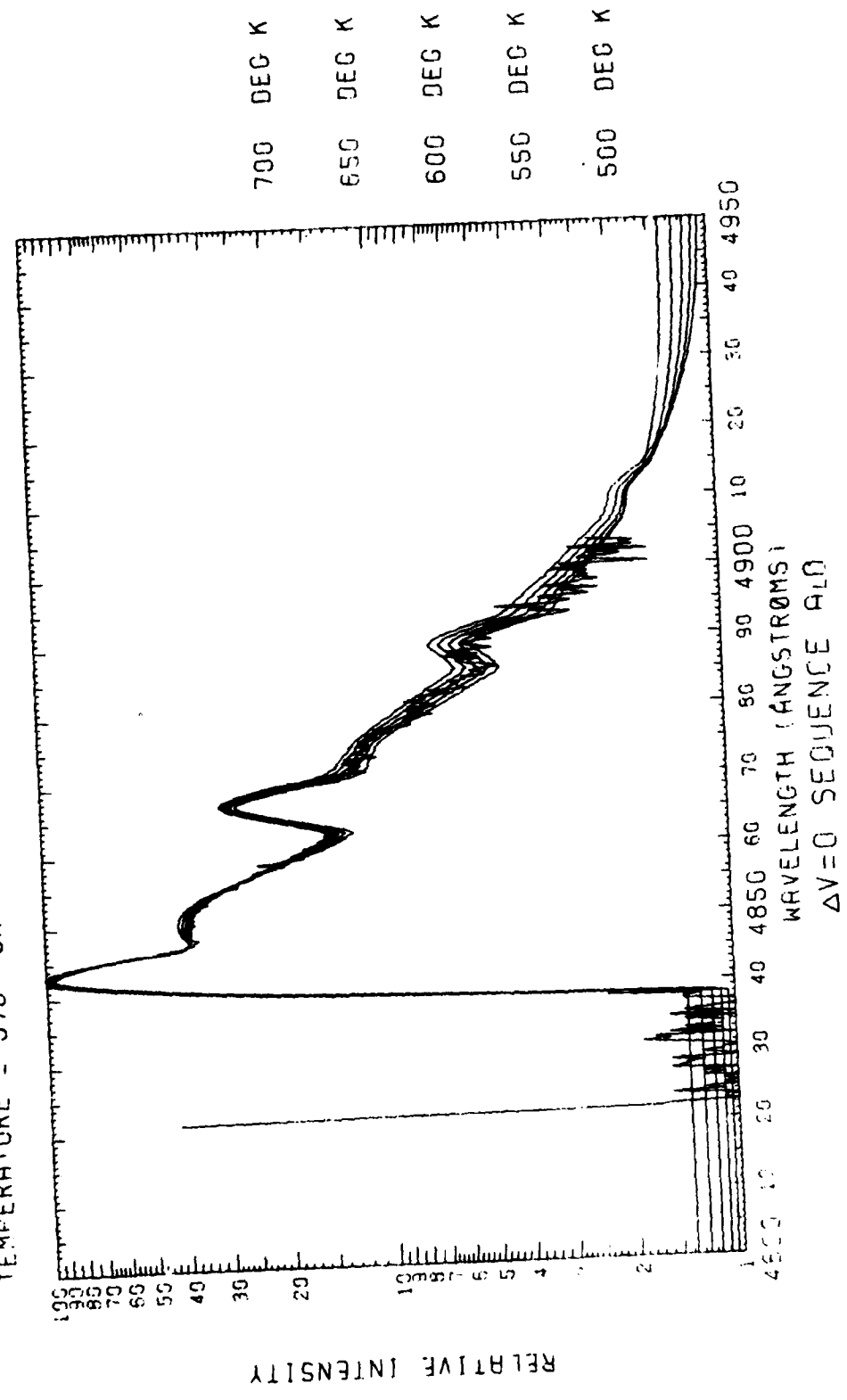
WAVELENGTH = 500 + OR - 5 DEG K



WAVELENGTH (ANGSTROMS)  
ΔV=0 SEQUENCE A10

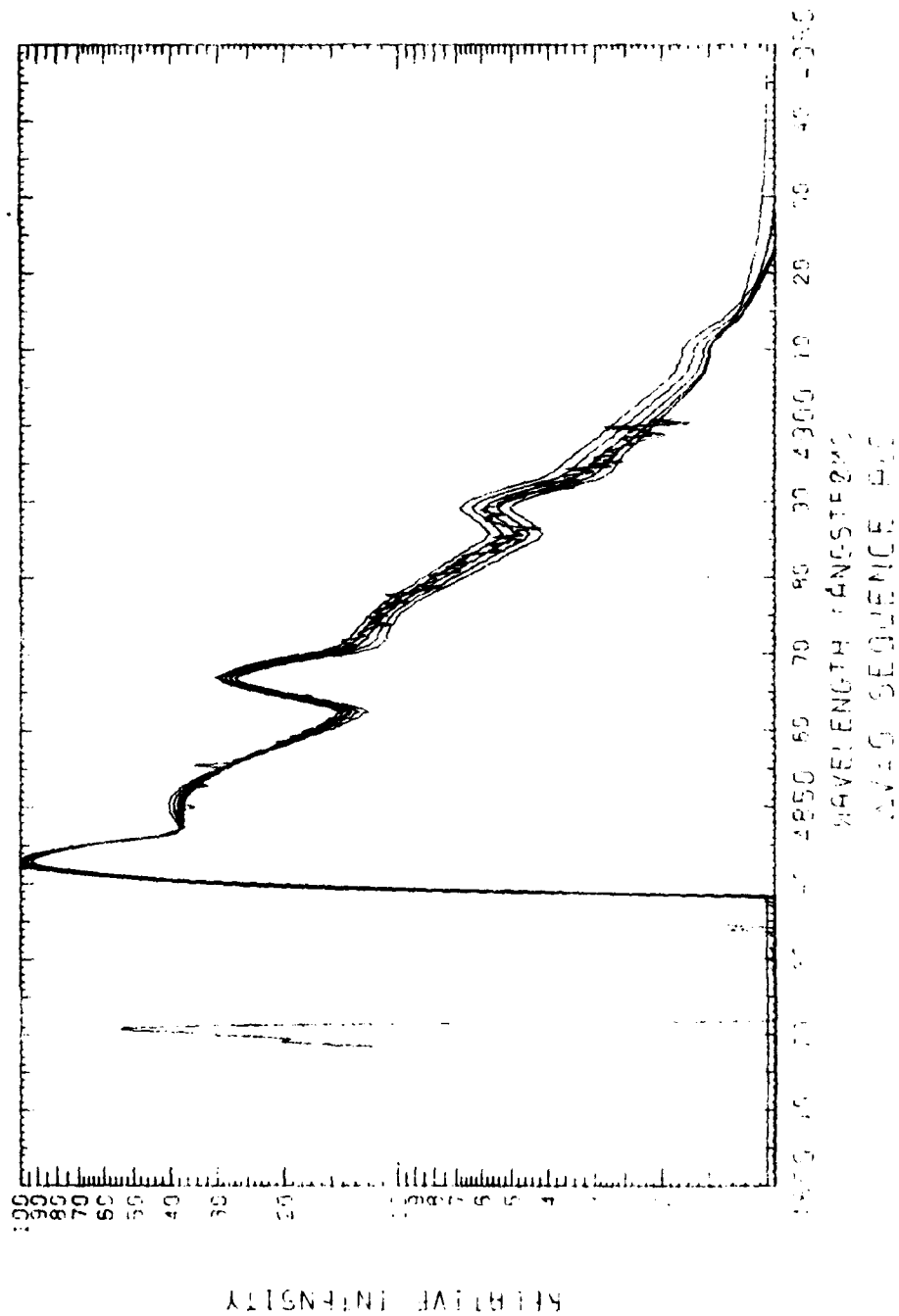
SCAN NOS. 2 24 8

TEMPERATURE = 578 +OR- 7 DEG K



SCAN NOS. 2 49 5

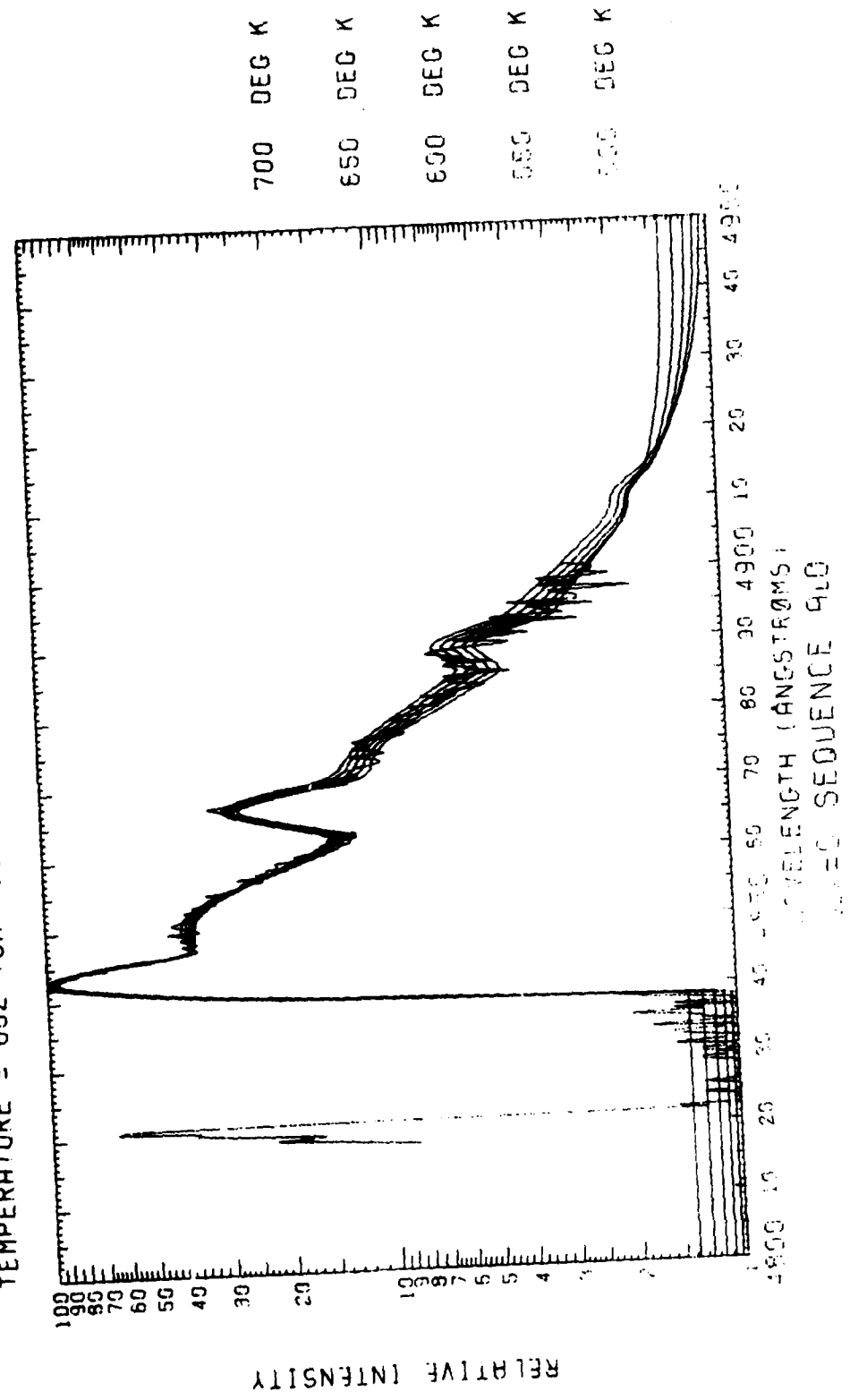
TEMPERATURE = 621 +OR- 6 DEG K



700 DEG K  
650 DEG K  
600 DEG K  
550 DEG K  
500 DEG K

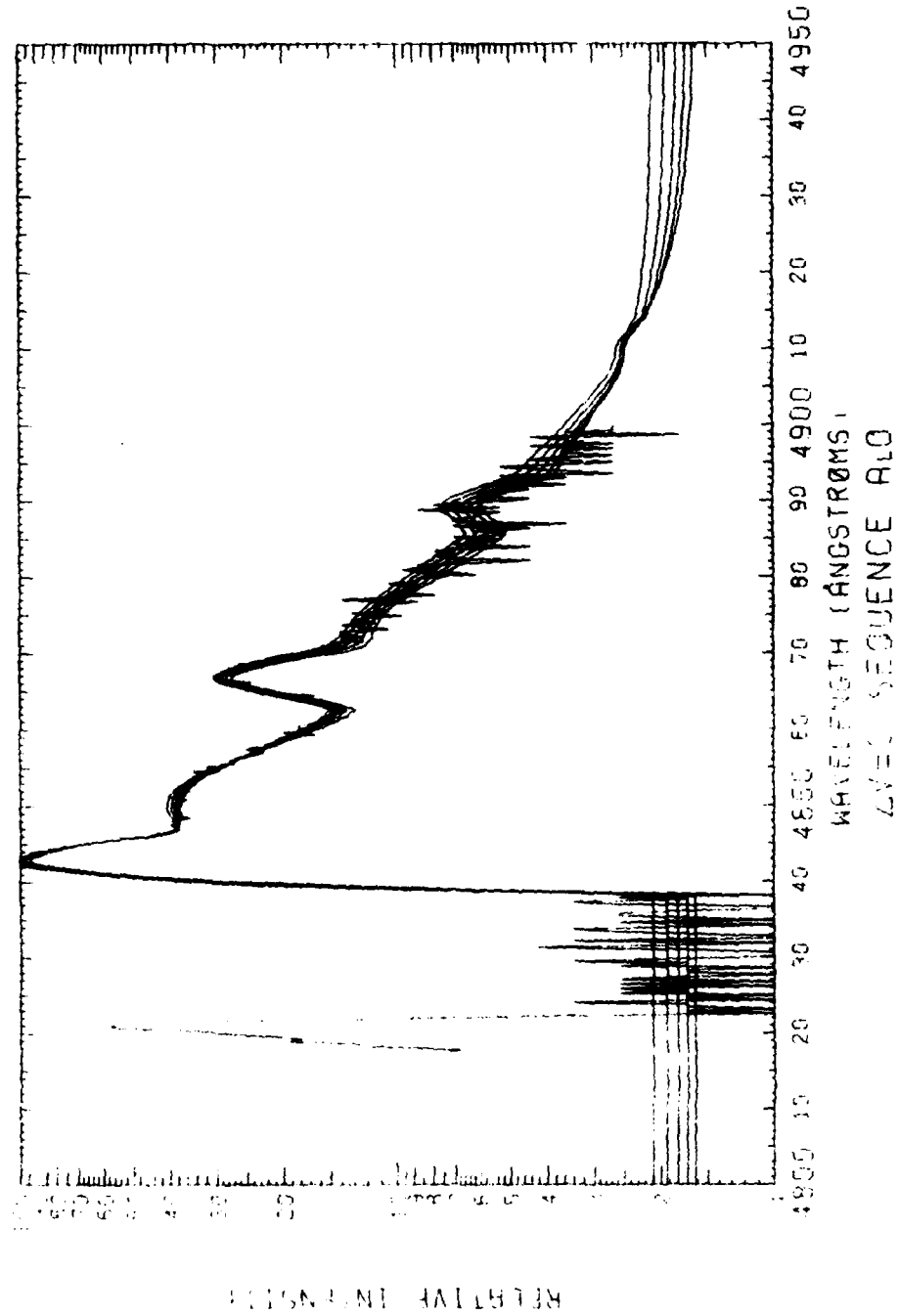
SCAN NOS. 2 54 3

TEMPERATURE = 602 +OR- 11 DEG K



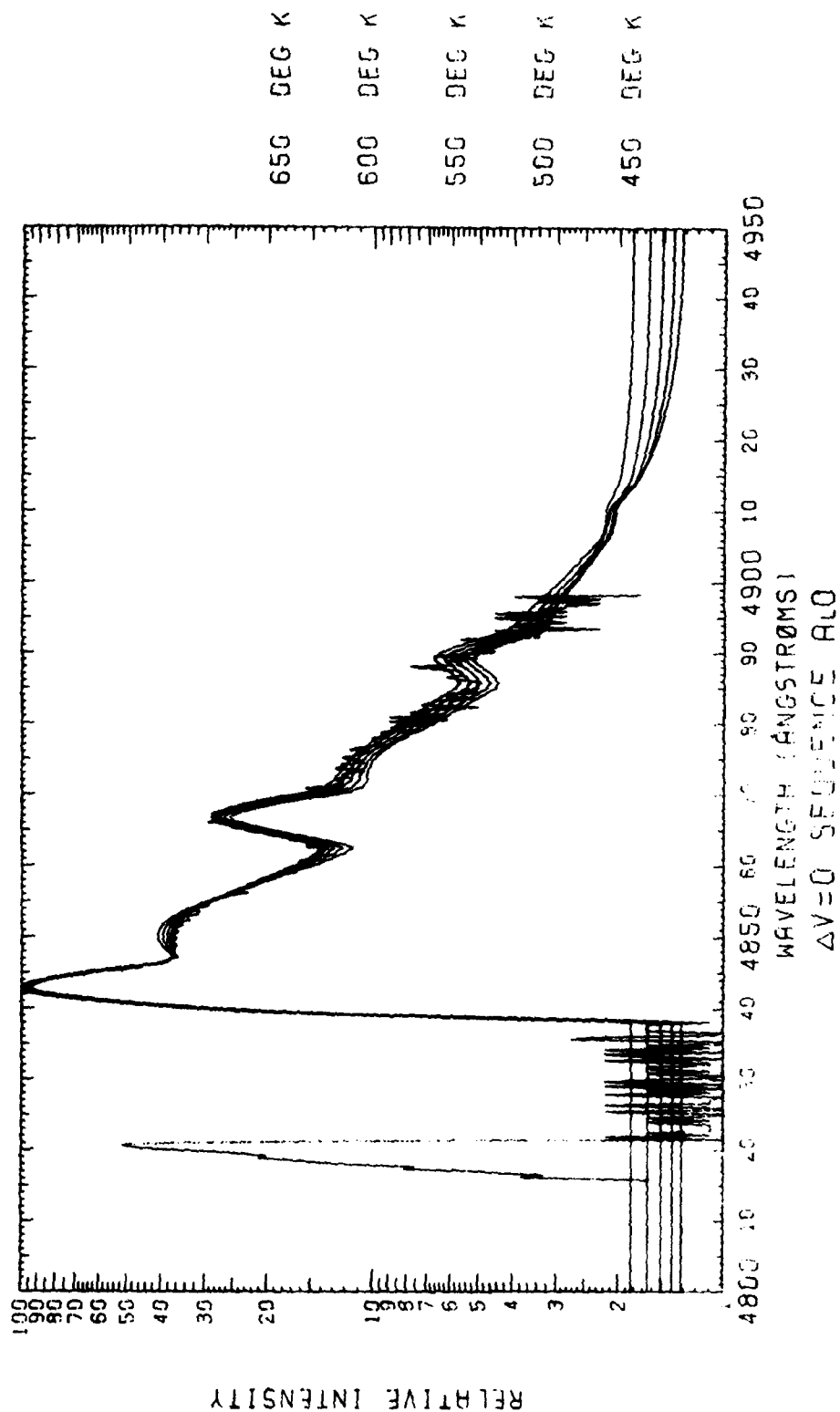
SIGN NOS: 2 58 9

TEMPERATURE = 600 +OR- 19 DEG K



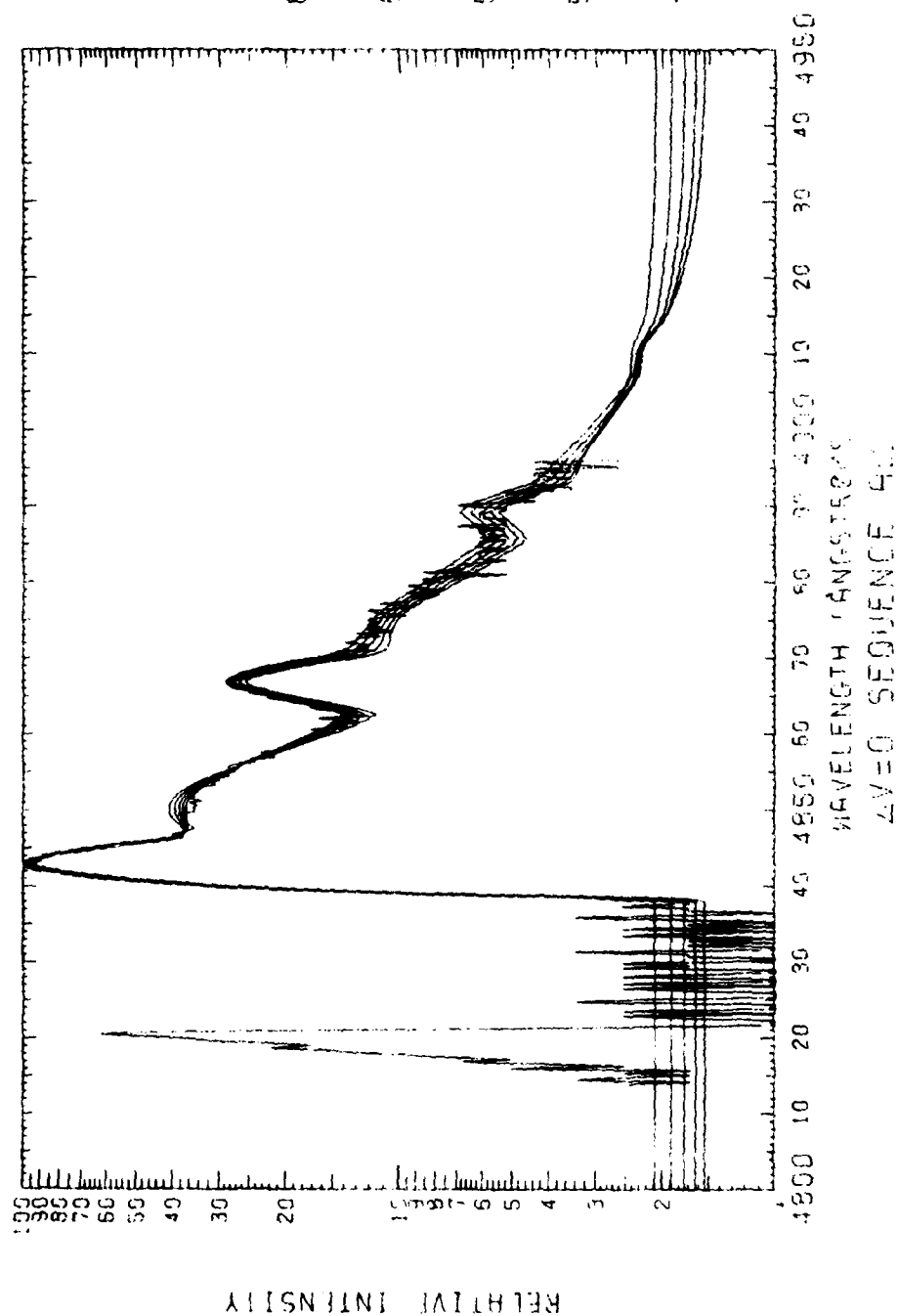
SCAN NOS. 2 68 8

TEMPERATURE = 574 +OR- 15 DEG K



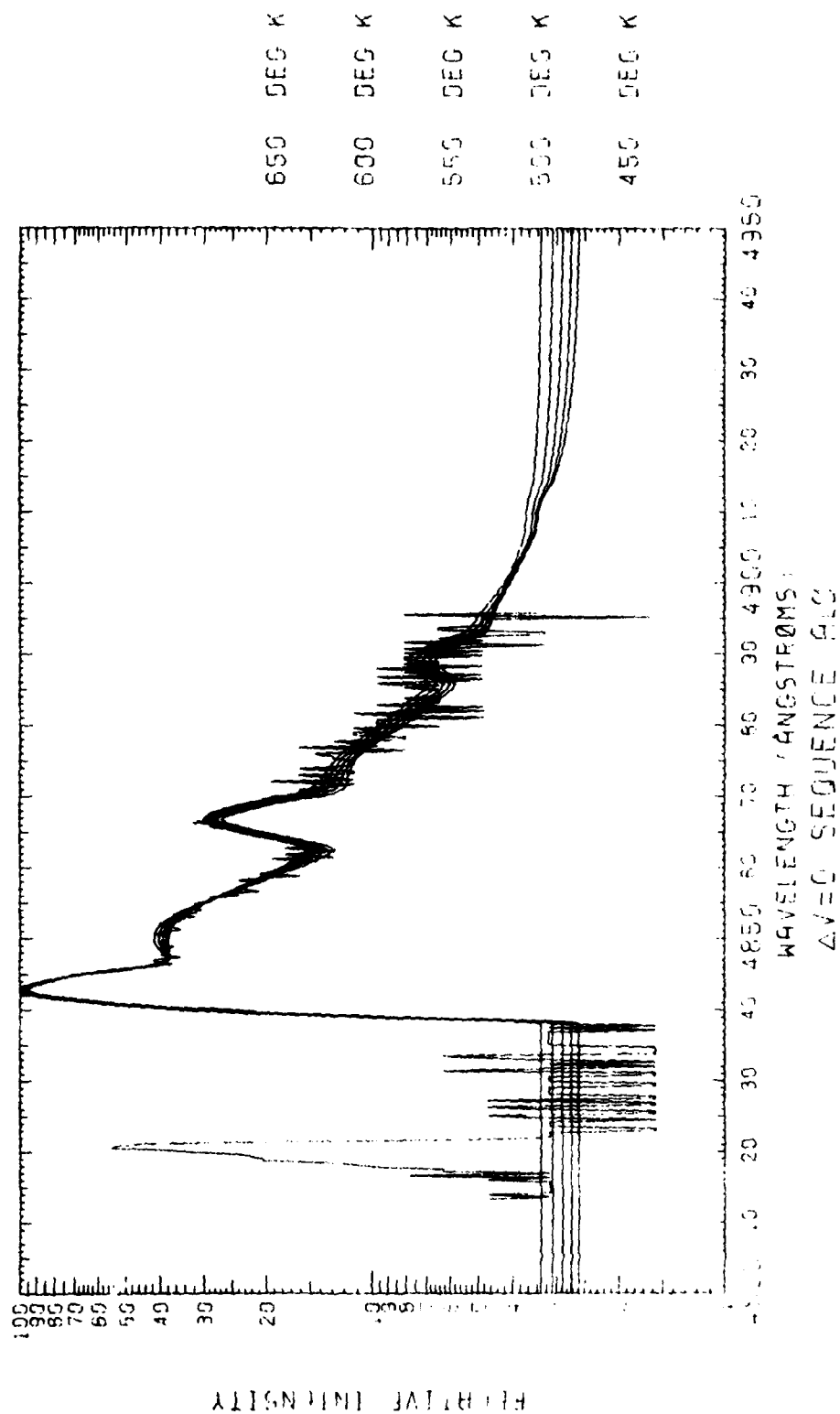
SCAN NOS. 2 86 5

TEMPERATURE = 573 +OR- 18 DEG K



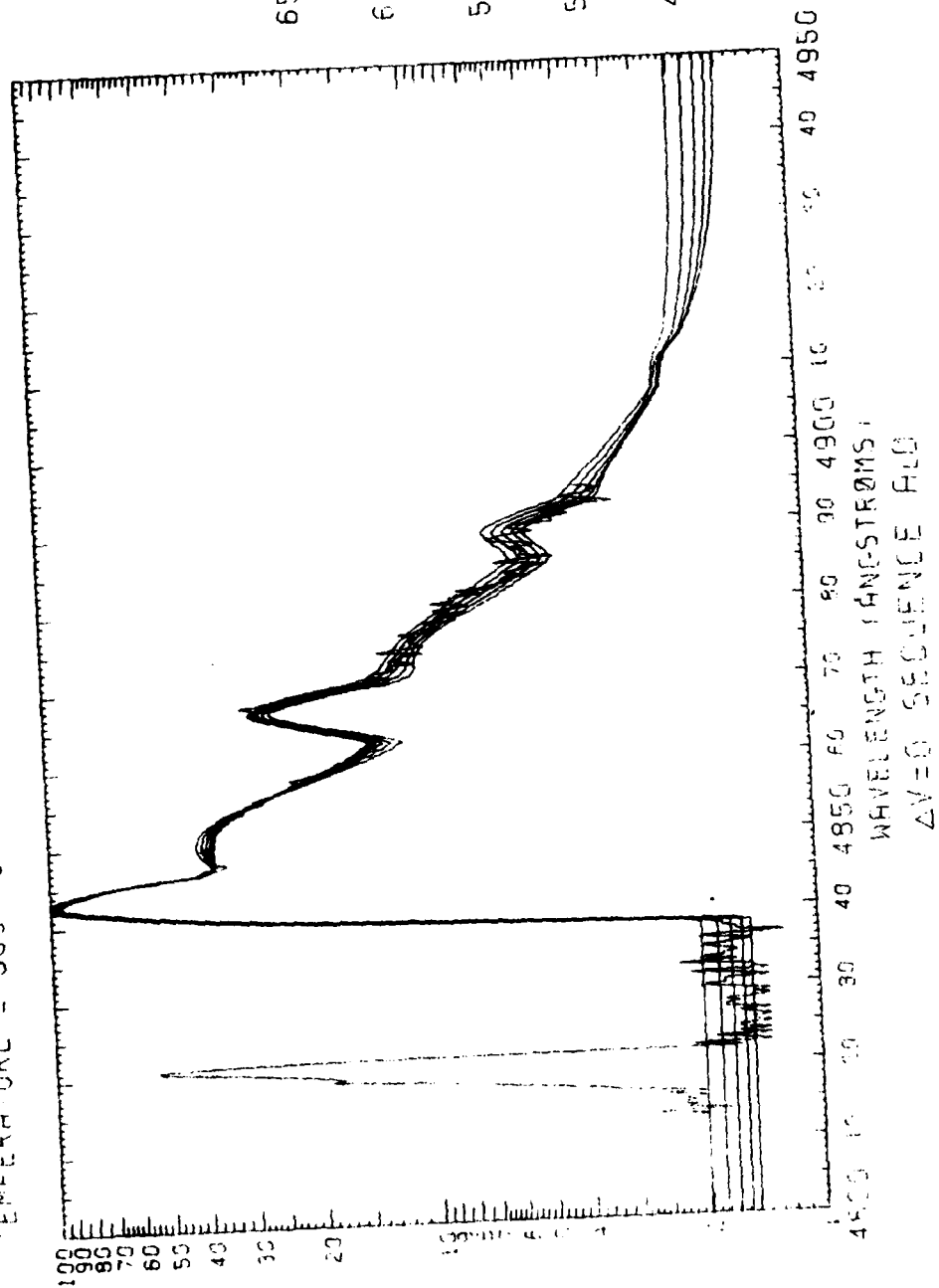
SCAN NOS. 2 93 6

TEMPERATURE = 572 +OR- 29 DEG K



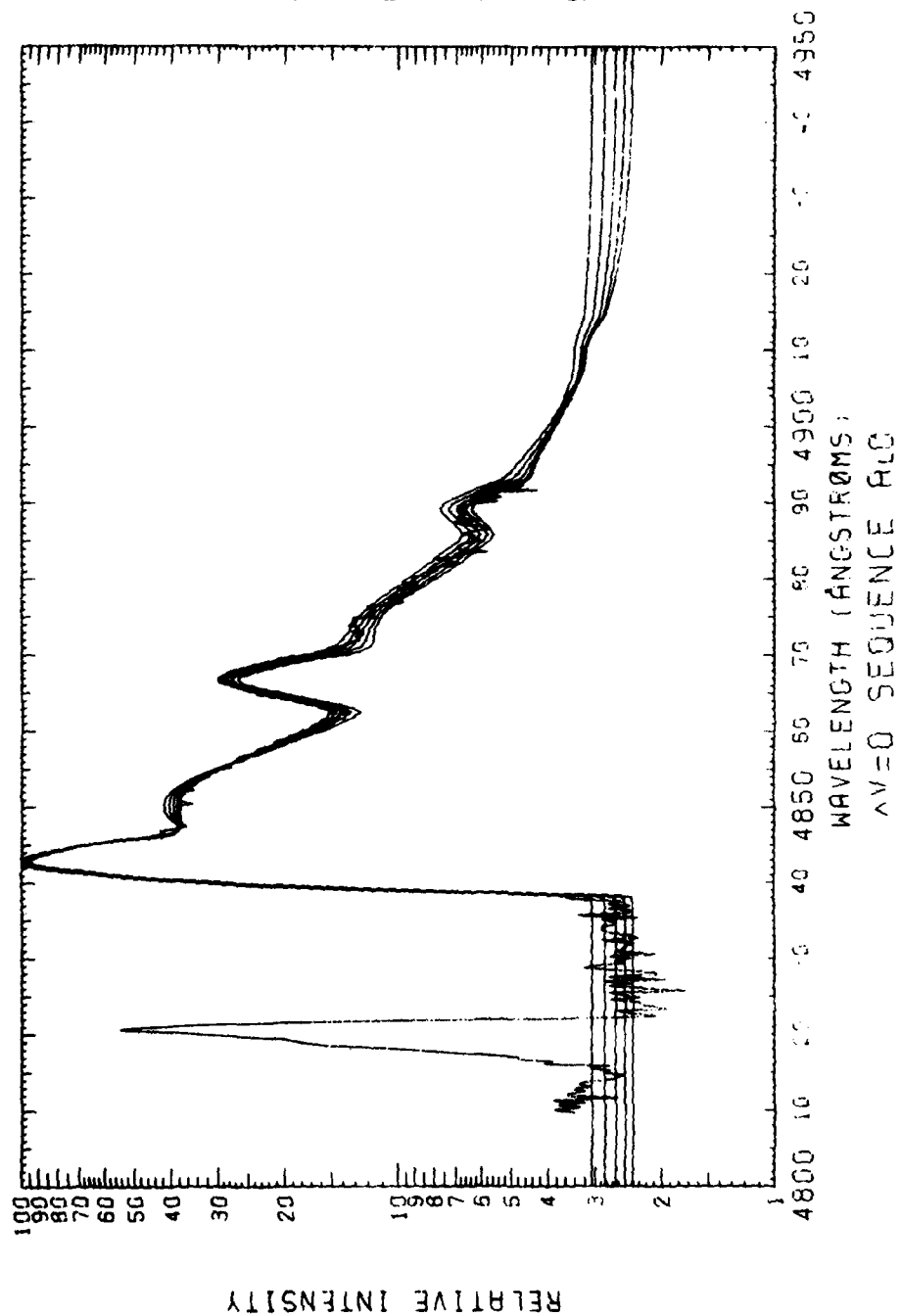
SCAN NOS. 2 100 8

TEMPERATURE = 559 +OR- 6 DEG K



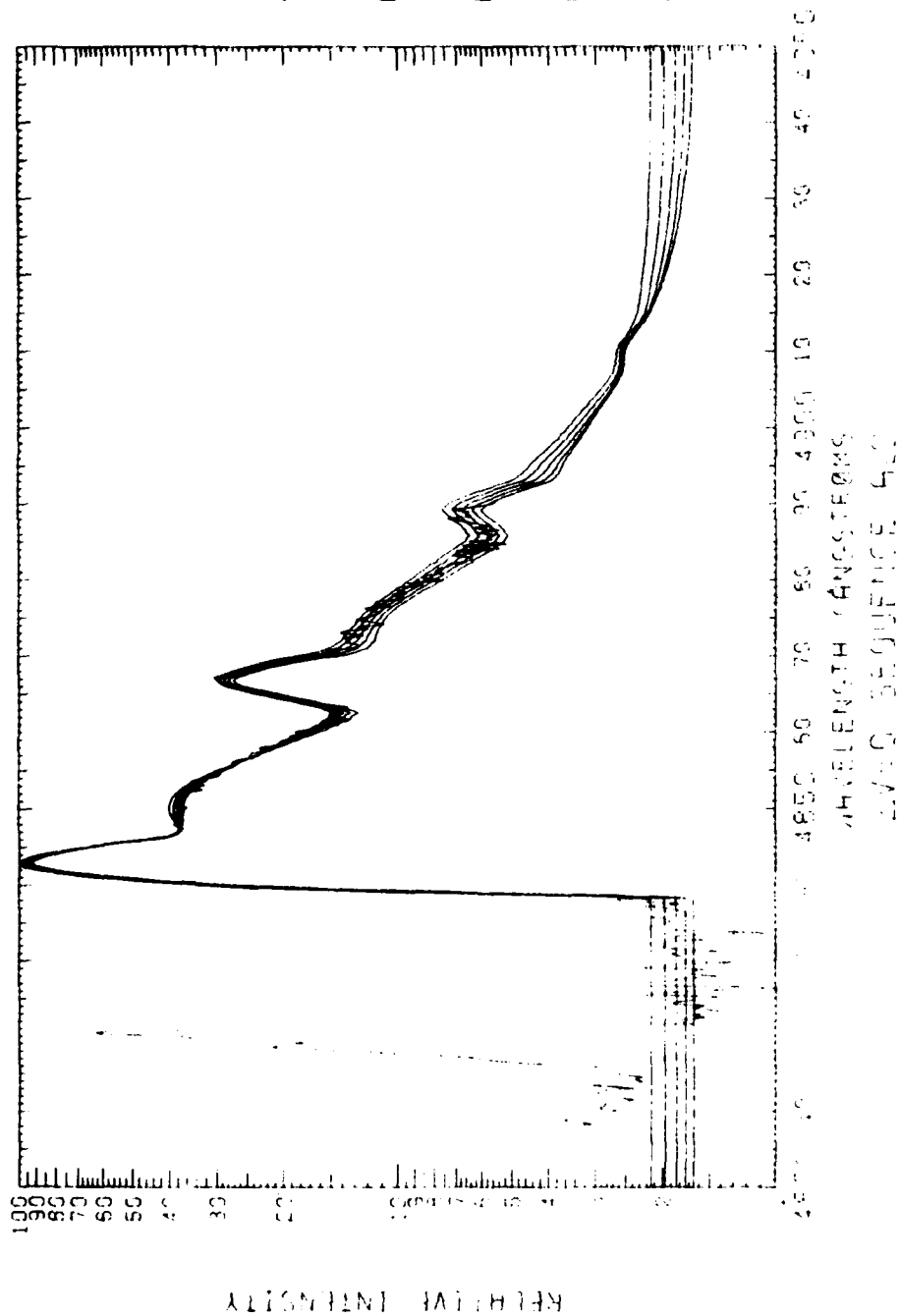
SCAN NOS. 2 122 11

TEMPERATURE = 570 +OR- 5 DEG K



SCAN NOS. 2 136 7

TEMPERATURE = 511 +OR- 6 DEG K



A P P E N D I X   C

LISTING OF COMPUTER PROGRAMS

|      |                                                               |        |
|------|---------------------------------------------------------------|--------|
|      | PROGRAM ASP(OUTPUT,TAPE5,TAPE6,TAPE3,TAPE7,TAPE39)            | 000720 |
| CC   | PROGRAM THEO                                                  | 000730 |
|      | DIMENSION TE(2),W(2),WX(2),WY(2),BE(2),ALFA(2),IZ(28),IIZ(28) | 000740 |
|      | DIMENSION FC(8,8),R(8,8),SNU(8),SNJ(8,80),EMI(8,80),APS(8,80) | 000750 |
|      | DIMENSION FR(3,3,80),FP(3,3,80),JEX(8)                        | 000760 |
|      | DIMENSION HJR(80),HJQ(80),HJP(80),BLAP(80),BIP(80),BLAR(80),  | 000770 |
|      | BIR(80)                                                       | 000780 |
|      | COMMON TE,W,WX,WY,BE,ALFA                                     | 000790 |
|      | COMMON/SPECTP/BLAP,BLAR,BIP,BIR                               | 000800 |
|      | WRITE(6,297)                                                  | 000810 |
| 297  | FORMAT (38H1ALO PROGRAM 1968 FOLLOWING DATA USED )            | 000820 |
|      | REWIND 7                                                      | 000830 |
|      | READ(5,295)IDATE,MOG                                          | 000840 |
|      | WRITE(6,2951)IDATE,MOG                                        | 000850 |
| 295  | FORMAT(I6,I2)                                                 | 000860 |
| 2951 | FORMAT(1X,I6,I2)                                              | 000870 |
|      | READ (5,296)(JEX(IJEX),IJEX=1,5)                              | 000880 |
|      | WRITE(6,296)(JEX(IJEX),IJEX=1,5)                              | 000890 |
| 296  | FORMAT(1H,5A10)                                               | 000900 |
|      | READ(5,109)TSOL,YSOL,SOLD                                     | 000910 |
|      | WRITE(6,1091)TSOL,YSOL,SOLD                                   | 000920 |
| 109  | FORMAT(2F10.0,E12.4)                                          | 000930 |
| 1091 | FORMAT(1X,2F10.0,E12.4)                                       | 000940 |
|      | READ(5,111)(TE(I),W(I),WX(I),WY(I),BE(I), ALFA(I),I=1,2)      | 000950 |
|      | WRITE(6,1111)(TE(I),W(I),WX(I),WY(I),BE(I), ALFA(I),I=1,2)    | 000960 |
| 111  | FORMAT(F12.4,F11.5,F12.7,F9.6,F9.7,F10.7)                     | 000970 |
| 1111 | FORMAT(1X,F12.4,F11.5,F12.7,F9.6,F9.7,F10.7)                  | 000980 |
|      | READ(5,112)G,IMAX,JMAX                                        | 000990 |
|      | WRITE(6,1121)G,IMAX,JMAX                                      | 001000 |
| 112  | FORMAT(F20.3,2I3)                                             | 001010 |
| 1121 | FORMAT(1X,F20.3,2I3)                                          | 001020 |
|      | DO 113 I=1,IMAX                                               | 001030 |
|      | DO 113 II=1,IMAX                                              | 001040 |
|      | READ(5,114)L,LL,FC(I,II),R(I,II)                              | 001050 |
|      | WRITE(6,1141)L,LL,FC(I,II),R(I,II)                            | 001060 |
| 114  | FORMAT (2I2,E11.4,F7.3)                                       | 001070 |
| 1141 | FORMAT(1X,2I2,E11.4,F7.3)                                     | 001080 |
| 113  | CONTINUE                                                      | 001090 |
|      | READ(5,122)M,IAX,IIAX,JMAX                                    | 001100 |
|      | WRITE(6,1221)M,IAX,IIAX,JMAX                                  | 001110 |
| 122  | FORMAT(4I3)                                                   | 001120 |
| 1221 | FORMAT(1X,4I3)                                                | 001130 |
|      | IF(M)127,127,1233                                             | 001140 |
| 127  | DO 128 I=1,IAX                                                | 001150 |
|      | DO 128 II=1,IIAX                                              | 001160 |
|      | DO 128 J=1,JMAX                                               | 001170 |
|      | READ(5,180)IA,IB,LQ,JP,TP,FP(I,II,J),JQ,JR,TR,FR(I,II,J)      | 001180 |
|      | WRITE(6,1801)IA,IB,LQ,JP,TP,FP(I,II,J),JQ,JR,TR,FR(I,II,J)    | 001190 |
| 180  | FORMAT(2I3,I4,I3,F10.2,F10.3,2I3,F10.2,F10.3)                 | 001200 |
| 1801 | FORMAT(1X,2I3,I4,I3,F10.2,F10.3,2I3,F10.2,F10.3)              | 001210 |
| 128  | CONTINUE                                                      | 001220 |
| 1233 | READ(5,193)LL,JKAX                                            | 001230 |
|      | WRITE(6,1931)LL,JKAX                                          | 001240 |
|      | READ (5,193 )(IZ(L),IIZ(L),L=1,LL)                            | 001250 |
|      | WRITE(6,1931)(IZ(L),IIZ(L),L=1,LL)                            | 001260 |
| 193  | FORMAT (14I4)                                                 | 001270 |
| 1931 | FORMAT(1X,14I4)                                               | 001280 |
|      | READ(5,115)T,DELT,TMAX                                        | 001290 |
|      | WRITE(6,1151)T,DELT,TMAX                                      | 001300 |
|      | TBEGIN=T                                                      | 001310 |
| 115  | FORMAT (3F10.1)                                               | 001320 |
| 1151 | FORMAT(1X,3F10.1)                                             | 001330 |
| 292  | FORMAT (26H THESE DATA ON TAPE IF 1 =,I2)                     | 001340 |
|      | WRITE(6,292)MOG                                               | 001350 |
|      | READ(5,193 )ISPECP,ILINE,ICON,IINU                            | 001360 |
|      | WRITE(6,1931)ISPECP,ILINE,ICON,IINU                           | 001370 |
| 123  | CONTINUE                                                      | 001380 |
|      | GT=1.0/(C.6952*T)                                             | 001390 |
|      | JAX=JMAX+1                                                    | 001400 |
|      | V=0.0                                                         | 001410 |
|      | Q=1.0                                                         | 001420 |
| 116  | V=V+1.0                                                       | 001430 |
|      | QQ=(W(2)-WX(2))*V-WX(2)*V*V                                   | 001440 |
|      | EX=EXP (-GQ*GT)                                               | 001450 |
|      | Q=Q*EX                                                        | 001460 |
|      | IF(EX*200.0-1.0)117,117,116                                   | 001470 |
| 117  | QV=Q                                                          | 001480 |
|      | DO 120 L=1,IMAX                                               | 001490 |
|      | UL=L-1                                                        | 001500 |
|      | QQQ=(W(2)-WX(2))*UL-WX(2)*UL*UL                               | 001510 |
|      | VN=(1.0/QV)*EX* (-GQ*GT)                                      | 001520 |
|      | SNU(L)=VN                                                     | 001530 |
| 120  | CONTINUE                                                      | 001540 |
|      | R=RF(2)-ALFA(2)*1.5                                           | 001550 |

|                                     |        |
|-------------------------------------|--------|
| D=4.08BF(2)*BE(2)*BE(2)/(W(2)*W(2)) | 001560 |
| AJ=0.0                              | 001570 |
| D=1.0                               | 001580 |
| 146 AJ=AJ+1.0                       | 001590 |
| A=AJ*(AJ+1.0)                       | 001600 |
| FJ=BSA-D*ASA                        | 001610 |
| F=EXP (-FJ*GT)                      | 001620 |
| FA=(AJ+AJ+1.0)*F                    | 001630 |
| D=D+FA                              | 001640 |
| IF((FA*100.0/D)-1.0)147,147,146     | 001650 |
| 147 DJ=D                            | 001660 |
| DO 148 I=1,IMAX                     | 001670 |
| V=I-1                               | 001680 |
| DB=BE(2)-ALFA(2)*(V+0.5)            | 001690 |
| DO 148 J=1,JAX                      | 001700 |
| SJ=J-1                              | 001710 |
| S=(SJ+1.0)*SJ                       | 001720 |
| FS=RR*S-D*S*S                       | 001730 |
| F=EXP (-FS*GT)                      | 001740 |
| SF=(SJ+SJ+1.0)*F/DJ                 | 001750 |
| 148 SNJ(I,J)=SF                     | 001760 |
| SO=0.6952*TSOL                      | 001770 |
| SOL=SLOF(YSOL,SO)                   | 001780 |
| C=SOL/SOL                           | 001790 |
| DO 355 I=1,IMAX                     | 001800 |
| DO 150 J=1,JMAX                     | 001810 |
| SUM=0.0                             | 001820 |
| DO 152 II=1,IMAX                    | 001830 |
| UR=1.0-G*RI(I,II)                   | 001840 |
| FK=UR*UR*FC(I,II)                   | 001850 |
| SU=SNV(II)                          | 001860 |
| SIV=SU*FK                           | 001870 |
| TYR=SNY(I,II,J,J-1)                 | 001880 |
| TYP=SNY(I,II,J,J+1)                 | 001890 |
| IF(M)179,179,154                    | 001900 |
| 179 IF(I-IA)174,174,154             | 001910 |
| 174 IF(II-IIAX)178,178,154          | 001920 |
| 178 IF(J-JMAX)176,176,154           | 001930 |
| 176 FRR=FR(I,II,J)                  | 001940 |
| FRP=FP(I,II,J)                      | 001950 |
| GO TO 153                           | 001960 |
| 154 FRR=1.0                         | 001970 |
| FRP=1.0                             | 001980 |
| 153 IF(J-1)155,155,156              | 001990 |
| 155 SIR=0.0                         | 002000 |
| GO TO 157                           | 002010 |
| 156 SJ=SNJ(II,J-1)                  | 002020 |
| CJ=J-1                              | 002030 |
| CCJ=2*(J-1)+1                       | 002040 |
| SR=CJ/CCJ                           | 002050 |
| SL=C*SLOF(TYR,SO)                   | 002060 |
| SIR=SJ*SR*TYR*SL*FRR                | 002070 |
| 157 SSJ=SNJ(II,J+1)                 | 002080 |
| DJ=J                                | 002090 |
| DDJ=2*J+1                           | 002100 |
| SP=DJ/DDJ                           | 002110 |
| SSL=C*SLOF(TYP,SO)                  | 002120 |
| SIP=SSJ*SP*SSL*TYP*FRP              | 002130 |
| SI=SIV*(SIP+SIR)                    | 002140 |
| SUM=SUM+SI                          | 002150 |
| 152 CONTINUE                        | 002160 |
| APS(I,J)=SUM                        | 002170 |
| 150 CONTINUE                        | 002180 |
| 355 CONTINUE                        | 002190 |
| DO 160 I=1,IMAX                     | 002200 |
| DO 161 J=1,JMAX                     | 002210 |
| SUM=0.0                             | 002220 |
| DO 162 II=1,IMAX                    | 002230 |
| UR=1.0-G*RI(I,II)                   | 002240 |
| FK=UR*UR*FC(I,II)                   | 002250 |
| IF(J-1)163,163,164                  | 002260 |
| 163 SIR=0.0                         | 002270 |
| GO TO 165                           | 002280 |
| 164 SR=J-1                          | 002290 |
| SYR=SNY(I,II,J-1)                   | 002300 |
| SJR=SYR*SYR*SYP                     | 002310 |
| SIR=SR*SJR                          | 002320 |
| 165 SP=J                            | 002330 |
| SYP=SNY(I,II,J,J+1)                 | 002340 |
| SJP=SYP*SYP*SYP                     | 002350 |
| SIP=SP*SJP                          | 002360 |
| SI=(SIP+SIR)*FA                     | 002370 |
| 162 SUM=SUM+SI                      | 002380 |
| 161 ENI(I,J)=SUM                    | 002390 |

|      |                                                                     |        |
|------|---------------------------------------------------------------------|--------|
| 160  | CONTINUE                                                            | 002400 |
|      | SDN=2.724E-04                                                       | 002410 |
|      | SDN=1.-SDN                                                          | 002420 |
|      | WLMAX=0.                                                            | 002430 |
|      | WLMIN=100000.                                                       | 002440 |
|      | AMPMAX=0.                                                           | 002450 |
|      | DO 194 I=1,LL                                                       | 002460 |
|      | I=IZ(L)+1                                                           | 002470 |
|      | II=IIZ(L)+1                                                         | 002480 |
| 1901 | FORMAT(IX,I6,F10.1,4I4, F10.3,E15.4,2I4,F10.3,E15.4)                | 002490 |
|      | RR=1.0-GBR(I,II)                                                    | 002500 |
|      | FK=FC(I,II)*RR*RR                                                   | 002510 |
|      | DO 168 J=1,JKAX                                                     | 002520 |
|      | AE=AFS(I,J)/EMI(I,J)                                                | 002530 |
| 170  | SR=J-1                                                              | 002540 |
| 172  | SP=J                                                                | 002550 |
|      | SNYP=SNY(I,II,J,J+1)                                                | 002560 |
|      | SNYR=SNY(I,II,J,J-1)                                                | 002570 |
|      | TJP=SNYP*SNYP*SNYP                                                  | 002580 |
|      | TJR=SNYR*SNYR*SNYR                                                  | 002590 |
|      | BLAP(J)=SDN*100000000/SNYP                                          | 002600 |
|      | BLAR(J)=SDN*100000000/SNYR                                          | 002610 |
|      | MJR(J)=J-2                                                          | 002620 |
|      | MJP(J)=J                                                            | 002630 |
|      | MJQ(J)=J-1                                                          | 002640 |
|      | BIP(J)=SP*AE*FK*TJP                                                 | 002650 |
|      | BIR(J)=SR*AE*FK*TJR                                                 | 002660 |
|      | IF(I,NE,II)GO TO 173                                                | 002670 |
|      | IF(BIP(J).GT.AMPMAX)AMPMAX=BIP(J)                                   | 002680 |
|      | IF(BIR(J).GT.AMPMAX)AMPMAX=BIR(J)                                   | 002690 |
|      | IF(BIP(J).LT..001*AMPMAX)GO TO 1725                                 | 002700 |
|      | IF(BLAR(J).GT.WLMAX)WLMAX=BLAR(J)                                   | 002710 |
|      | IF(BLAP(J).LT.WLMIN)WLMIN=BLAP(J)                                   | 002720 |
| 1725 | CONTINUE                                                            | 002730 |
|      | IF(BIR(J).LT..001*AMPMAX)GO TO 173                                  | 002740 |
|      | IF(BLAR(J).GT.WLMAX)WLMAX=BLAR(J)                                   | 002750 |
|      | IF(BLAR(J).LT.WLMIN)WLMIN=BLAR(J)                                   | 002760 |
| 173  | CONTINUE                                                            | 002770 |
|      | IF(J.EQ.20)WRITE(6,1901)IDATE,T,IZ(L),IIZ(L),MJQ(J),MJP(J),BLAP(J)  | 002780 |
|      | 1,BIP(J),MJQ(J),MJR(J),BLAR(J),BIR(J)                               | 002790 |
| 168  | CONTINUE                                                            | 002800 |
|      | IF(MOQ.EQ.1)WRITE(7, ) (IDATE,T,IZ(L),IIZ(L),MJQ(J),MJP(J),BLAP(J)  | 002810 |
|      | 1J),BIP(J),MJQ(J),MJR(J),BLAR(J),BIR(J),J=1,JKAX)                   | 002820 |
|      | IF(L.EQ.1.AND.T.EQ.500.)WRITE(6,1901) (IDATE,T,IZ(L),IIZ(L),MJQ(J), | 002830 |
|      | 1MJR(J),BLAP(J),BIP(J),MJQ(J),MJR(J),BLAR(J),BIR(J),J=1,JKAX)       | 002840 |
| 194  | CONTINUE                                                            | 002850 |
|      | IF(IINV.EQ.1)CALL INVEN(LL,JKAX)                                    | 002860 |
|      | IF(ISFECP.EQ.1)CALL SPECVC(WLMAX,WLMIN,LL,JKAX,JEX,T)               | 002870 |
|      | T=T+DELT                                                            | 002880 |
|      | IF(T.LE.TMAX)GO TO 123                                              | 002890 |
|      | BACKSPACE 7                                                         | 002900 |
|      | PRINT 1931, JKAX                                                    | 002910 |
|      | READ ( 7) (ID,T,I1,I2,MJQ(J),MJP(J),BLAP(J),BIP(J),MJQ(J),          | 002920 |
|      | 1MJR(J),BLAR(J),BIR(J),J=1,JKAX)                                    | 002930 |
|      | WRITE(6,1901) (ID,T,I1,I2,MJQ(J),MJP(J),BLAP(J),BIP(J),MJQ(J),      | 002940 |
|      | 1MJR(J),BLAR(J),BIR(J),J=1,JKAX)                                    | 002950 |
|      | REWIND 7                                                            | 002960 |
|      | IF(ICON.EQ.1)CALL HCON(TBEGIN,TMAX,DELT)                            | 002970 |
| 555  | CONTINUE                                                            | 002980 |
|      | IF(ISFECP.EQ.1)CALL PLOTV(4)                                        | 002990 |
|      | STOP                                                                | 003000 |
|      | END                                                                 | 003010 |
| C    |                                                                     | 003030 |
| C    |                                                                     | 003040 |
| C    | 4 SMALL SUBROUTINES                                                 | 003050 |
| C    |                                                                     | 003060 |
| C    |                                                                     | 003070 |
| C    | FUNCTION SLOF(A,SD)                                                 | 003080 |
| C    | THEORETICAL SPECTRA                                                 | 003090 |
|      | SLOF=A*A/(EXP(A/SD)-1.0)                                            | 003100 |
|      | RETURN                                                              | 003110 |
|      | END                                                                 | 003120 |
|      | FUNCTION SNY(I,II,J,JJ)                                             | 003130 |
|      | DIMENSION TE(2),W(2),WY(2),WY(2),PE(2),ALFA(2)                      | 003140 |
|      | COMMON T,TE,WX,WY,PE,ALF                                            | 003150 |
|      | V=1                                                                 | 003160 |
|      | WV=1                                                                | 003170 |
|      | ALF=1                                                               | 003180 |
|      | ALF=J-1                                                             | 003190 |
|      | BT=W(1)*W(V+0.5) WY(1)*W(V+0.5)*W(V+0.5)                            | 003200 |
|      | BT=W(2)*W(V+0.5) WY(2)*W(V+0.5)*W(V+0.5)                            | 003210 |
|      | BT=PE(1)*ALFA(1)*W(V+0.5)                                           | 003220 |
|      | BT=PE(2)*ALFA(2)*W(V+0.5)                                           | 003230 |
|      | BT=0.04*(1+BT*(1+BT*(1+W(1)*W(1)))                                  | 003240 |

|     |                                                                      |        |
|-----|----------------------------------------------------------------------|--------|
|     | D2=4.0#DE(2)*DE(2)*DE(2)/(W(2)*W(2))                                 | 003250 |
|     | AA=AJJ*(AJJ+1.0)                                                     | 003260 |
|     | A=AJ*(AJ+1.0)                                                        | 003270 |
|     | F1=P18A-D18AA                                                        | 003280 |
|     | F2=B28AA-D28AA8AA                                                    | 003290 |
|     | T1=TE(1)+G1+F1                                                       | 003300 |
|     | T2=TE(2)+G2+F2                                                       | 003310 |
|     | SNV=T1-T2                                                            | 003320 |
|     | RETURN                                                               | 003330 |
|     | END                                                                  | 003340 |
| C   |                                                                      | 001340 |
| C   |                                                                      | 001370 |
| C   | 5 HCON                                                               | 001380 |
| C   |                                                                      | 001390 |
| C   |                                                                      | 001400 |
|     | SUBROUTINE HCON(T1,T2,T3)                                            | 003410 |
|     | DIMENSION L(75),M(75),A(75),B(75),D(75),N(75),C(75)                  | 003420 |
|     | DIMENSION Y(801)                                                     | 003430 |
|     | REWIND 3                                                             | 003440 |
| C   | DO 100 IPAS=1,1                                                      | 003450 |
| C   |                                                                      | 003460 |
|     | REWIND 7                                                             | 003470 |
|     | IV=0                                                                 | 003480 |
|     | ST=4800.                                                             | 003490 |
|     | IT1=T1+.001 \$ IT2=T2+.001 \$ IT3=T3+.001                            | 003500 |
|     | DO 70 IT=IT1,IT2,IT3                                                 | 003510 |
|     | 5 READ(7)(ID,T,IX,IY,L(J),M(J),A(J),B(J),L(J),N(J),C(J),D(J),J=1,75) | 003520 |
|     | IF((IX-IY).NE.IV)GO TO 5                                             | 003530 |
|     | DO 6 K=1,801                                                         | 003540 |
|     | 6 Y(K)=0.                                                            | 003550 |
|     | DO 11 LL=1,4                                                         | 003560 |
|     | IF(LL.EQ.1)GO TO 7                                                   | 003570 |
|     | READ(7)(ID,T,IX,IY,L(J),M(J),A(J),B(J),L(J),N(J),C(J),D(J),J=1,75)   | 003580 |
|     | 7 IF((IX-IY).NE.IV)GO TO 110                                         | 003590 |
|     | ITT=T+.01                                                            | 003600 |
|     | IF(ITT.NE.IT)GO TO 110                                               | 003610 |
|     | DO 11 I=1,2                                                          | 003620 |
|     | DO 11 J=1,75                                                         | 003630 |
|     | IF(1.EQ.2)A(J)=C(J)                                                  | 003640 |
|     | IF(1.EQ.2)B(J)=D(J)                                                  | 003650 |
|     | K1=4.*(A(J)-ST)-15.                                                  | 003660 |
|     | K2=K1+30                                                             | 003670 |
|     | IF(K1.LT.1)K1=1                                                      | 003680 |
|     | IF(K1.GT.800)K1=800                                                  | 003690 |
|     | IF(K2.LT.2)K2=2                                                      | 003700 |
|     | IF(K2.GT.801)K2=801                                                  | 003710 |
|     | DO 11 K=K1,K2                                                        | 003720 |
|     | VK=K-1                                                               | 003730 |
|     | DLAM=A(J)-.25*VK-ST                                                  | 003740 |
|     | Y(K)=Y(K)+B(J)*SLITFN(IPAS,DLAM)                                     | 003750 |
| 11  | CONTINUE                                                             | 003760 |
|     | YM=0.                                                                | 003770 |
|     | DO 12 K=1,801                                                        | 003780 |
|     | IF(Y(K).GT.YM)KM=K                                                   | 003790 |
|     | IF(Y(K).GT.YM)YM=Y(K)                                                | 003800 |
| 12  | CONTINUE                                                             | 003810 |
|     | DO 13 K=1,801                                                        | 003820 |
| 13  | Y(K)=Y(K)/YM                                                         | 003830 |
|     | WRITE(3)IV,T,IPAS,KM,(Y(K),K=1,801)                                  | 003840 |
|     | PRINT 14,IV,T,IPAS,KM                                                | 003850 |
| 14  | FORMAT(1X,16HSEQUENCE DELT U=,I2,7H, TEMP=,F6.0,13H DEG A, IPAS=,    | 003860 |
|     | 114,30H BANDHEAD AT STEP NUM,14)                                     | 003870 |
| 70  | CONTINUE                                                             | 003880 |
|     | ENDFILE 3                                                            | 003890 |
|     | PRINT 71                                                             | 003900 |
| 71  | FORMAT(2H1#'                                                         | 003910 |
| 100 | CONTINUE                                                             | 003920 |
|     | GO TO 120                                                            | 003930 |
| 110 | PRINT 111                                                            | 003940 |
| 111 | FORMAT(1X,26HWRONG ORDER ON DISK,RETURN)                             | 003950 |
| 120 | RETURN                                                               | 003960 |
|     | END                                                                  | 003970 |
| C   |                                                                      | 003980 |
| C   |                                                                      | 004000 |
| C   | 6 SLITFN                                                             | 004010 |
| C   |                                                                      | 004020 |
| C   |                                                                      | 004030 |
| C   |                                                                      | 004040 |
|     | FUNCTION SLITFN(N,DLAM)                                              | 004050 |
|     | DIMENSION FN(3,100),ANUL(3),LIM(3)                                   | 004060 |
|     | DATA(FN(1,K),K=1,20)/5.54,5.50,5.40,5.22,4.90,4.56,4.12,3.64,3.22,   | 004070 |
|     | 12.76,2.30,1.06,1.42,1.00,1.74,1.48,1.28,1.16,1.06,0./               | 004080 |
|     | DATA(FN(2,K),K=1,14)/7.93,7.83,7.37,6.52,5.74,4.97,4.2,3.32,2.54,    | 004090 |
|     | 11.74,1.1,1.32,1.07,0./                                              | 004100 |

```

DATA(FN(3,K),K=1,18)/8.8,8.6,8.1,7.4,6.6,5.8,5.0,4.2,3.4,2.65, 004110
11.8,1.2,75,4,2,1,05,0./ 004120
DATA LIM/20,14,18/ 004130
DATA AMUL/.0794226,.6,.4062/ 004140
C FOLLOWING CONSTANTS FOR ALADDIN II CLARA & HOPE APR 1972 004150
DATA LIM/17/ 004160
DATA AMUL/.10640/ 004170
DATA(FN(1,K),K=1,17)/89.8,89,.84,.77,.68,4,59.4,50.8, 004180
142,.33,8,25,2,16.4,9.6,5.4,2.8,1.4,.6,0./ 004190
DATA LIM/13/ 004200
DATA AMUL/.1019/ 004210
DATA (FN(1,K),K=1,13)/227,.224,.209,.181,.153,.125,.98,.70. 004220
1.42,.16,.2,.0,0./ 004230
C ALADDIN 74 SLIT FN 004240
DATA LIM/30/ 004250
DATA AMUL/.15/ 004260
DATA (FN(1,K),K=1,30)/703,.701,.689,.671,.644,.616,.587,.558. 004270
1,529,.500,.472,.443,.414,.385,.356,.327,.298,.270,.241. 004280
2,212,.184,.155,.126,.97,.68,.41,.21,.9,.1,0./ 004290
C POST-ALADDIN JAN 75 SLIT FN AL BURNER 004300
DATA AMUL/.066175,.081125/,LIM/44,36/ 004310
DATA (FN(1,K),K=1,44)/.0949,.0948,.0945,.093,.091,.0885,.0859,.083004320
14,.0809,.0784,.0758,.0733,.0708,.0682,.0657,.0632,.0606,.0581,.055004330
26,.0531,.0505,.048,.0455,.0429,.0404,.0379,.0354,.0328,.0303,.0278004340
3,.0252,.0227,.0202,.0176,.0151,.0126,.0101,.0075,.0050,.0027,.0013004350
4,.0007,0,0,0./ 004360
C POST-ALADDIN JAN 75 SLIT FN TMA RELEASE 004370
DATA (FN(2,K),K=1,36)/.1176,.1173,.1156,.1120,.1083,.1045,.1008,.0004380
197,.0933,.0895,.0858,.082,.0783,.0745,.0708,.0670,.0633,.0596,.055004390
28,.0521,.0483,.0446,.0408,.0371,.0333,.0296,.0258,.0221,.0183,.014004400
36,.0108,.0071,.0034,.0005,0,0,0./ 004410
C AEOLUS JAN 1975 004420
DATA AMUL/.15345085/,LIM/29/ 004430
DATA (FN(1,K),K=1,29)/142.5,140,.134,.127.8,121.7,115.6,109.4,103,004440
12,97.2,91,.84.8,76.6,72.5,66.3,60.2,54.2,48.1,42.0,35.8,29.4,23.2,004450
217.0,11.5,6.5,4,.2,.7,0,0,0./ 004460
DS=ABS(DLAM)/AMUL(N)+1. 004470
IDS=DS 004480
IF (IDS.GE.LIM(N)-1)GO TO 20 004490
DDS=IDS 004500
RDS=DS-DDS 004510
SLITFN=(1.-RDS)*FN(N,IDS)+RDS*FN(N,IDS+1) 004520
GO TO 30 004530
20 SLITFN=0. 004540
30 RETURN 004550
END 004560

```

```

PROGRAM MATCH(OUTPUT,TAPE5,TAPE6,TAPE2,TAPE3)
DIMENSION NSF(8),NSTR(8),MICRON(8),IPLIST(3),AMUL(8)
DIMENSION AMBDAF(3),
DIMENSION WAC(20),WAA(20)
COMMON Y(300),X(300),YM(300),Z(801),WM(801),Y(19),DUM(801)
INTEGER OM
DATA ASKY/10HBLUE SKY /
C DATA AMUL/.397113,.397113,.32408,.32408,.32408,.340185,
C 11.62464,1.62464/
DATA AMUL/.2712,.2712,.2712,.2712,.2712,.2712,.2712,
DATA NSF/1,1,1,1,1,1,1,1/
C DATA NSTR/40,40,183,278,67,231,291/
C DATA NSTR/224,81,195,30,203,112,282,141/
C ALADDIN II CLARA AND MUPE
C DATA NSTR/170,149,144,230,0,0,0,0/
C GOLIAH MOV 71
DATA AMUL/.4076,.4076,0,0,0,0,0,0/
DATA NSTR/46,117,0,0,0,0,0,0/
DATA MICRON/135,135,135,176,176,176,176,176/
C ALADDIN 74
DATA NSTR/79,79,79,79,79,79,79,79/
DATA AMUL/.3055,.3055,.3055,.3055,0,0,0,0/
C POST-ALADDIN JAN 75
DATA NSF/1,1,2,2,2,2,2,2/
DATA NSTR/204,1,224,1,1,1,1,1/
DATA AMUL/.2647,1,.3245,1,.1,1,1,1/
DATA AMBDAF/4824.3,AMBDAF/4886.3,AMBDAF/384842.5/
DATA AMUL/.3069,.3069,.3069,.3069,.3069,.3069,.3069,.3069/
DATA NSF/1,1,1,1,1,1,1,1/
DATA NSTR/290,143,244,143,182,143,1,1/
C WSMR OCT 77
DATA NSTR/8*180/,AMUL/8*.3010/
REWIND 2
REWIND 3
REWIND 5
C IF NUMBA.GE.6 A CRT PLOT IS MADE, OTHERWISE A PEN PLOT
C IF NUMBA=0 NO PLOT IS MADE.
CC IAP IS PARAMETER FOR SCALE ON APLLOT.
C IF SM=0. NO SMOOTHING IS DONE.
C SM IS SMOOTHING PARABOLA HALF WIDTH IN ANGSTROMS.
C IF STPL = 0. NO STRIP PLOT IS MADE.
C STPL=1. MAKES STRIP PLOT ON OUTPUT WITH APLLOT.
C IF STPL=2. THE STRIP PLOT IS MADE BUT NO OTHER PROCESSING IS DONE.
C IF STPL=3. ONLY STRIP PLOT IS MADE AND VALUE READ IN AS PFAK IS USED
C FOR NSTR.
C IF STPL=4. ONLY STRIP PLOT IS MADE, PEAK IS USED FOR NSTR
C AND SHOT IS USED FOR SMOOTHING.
C IF OM=QUICK PLOT, QUICK CRT PLOT OF FILES N1, N2, OF DATA TAPE IS
C MADE BUT NO OTHER PROCESSING IS DONE.
READ(5,210)OM,N1,N2,STPL,IAP,SM,NUMBA1,NUMBA2
210 FORMAT(4X,I1,4X,I2,3X,I2,7X,F2.0,5X,I2,5X,F2.0,6X,I1,5X,I1)
PRINT 211,OM,N1,N2,STPL,IAP,SM,NUMBA1,NUMBA2
211 FORMAT(1X,3HOM=,I1,1X,5HFILES,I2,1X,2HIO,I2,7H, STPL=, I2,0,
11X,4HIAP=,I2,5H, SM=,F2.0,6H, PEN=,I1,1X,4HCRT=,I1)
NUMBA=NUMBA1+7*NUMBA2
IF(OM.NE.1)GO TO 1
CALL AL2(N1,N2,NSTR)
GO TO 100
1 CONTINUE
PRINT 201
201 FORMAT( 82H1FILE NO. SCAN NO. SCANS SUMMED TEMPERATURE(DEG. K)
1 STD DEVIATION DESCRIPTION,9X,9HPEAK SHOT)
XPEAK=0.
DO 3 K=1,801
3 ZW(K)=4800.+.25*FLOAT(K-1)
DO 5 L=1,19
5 Y(L)=50*L+100
7 READ (5,202)NF,NSC,NSUM,ALFH1,ALPH2,PEAK,ALPH3
IF(EOF(5))100,8
202 FORMAT(9X,I2,10X,I4,5X,I3,9X,A10,A9,F6.2,A5)
8 IF(STPL.LT.1,5)CALL ZSTORE(-NSF(NF))
CALL ISNN(NF,+1,IDUMMY)
NSUM=MAX0(NSUM,1)
DO 10 N=1,300
10 Y(N)=1.
NSTRNF=NSTR(NF)
C AEOLUS MARCH 1977
IF(NSC.GT.58)NSTRNF=NSTR(NF+2)
IF(NSC.GT.69)NSTRNF=NSTR(NF+4)
IF(STPL.GT.2,9)NSTRNF=PEAK
DO 22 N=1,NSUM
N4=300*(N+NSC)+NSTRNF -401
DO 20 K=1,300

```

```

      CALL ISNN(K+N4,-1,IWN3)
20 Y(K)=Y(K)+FNAAY(IWN3)
22 CONTINUE
   IF(STPL.LE..9)GO TO 25
   ANSUM=NSUM
   DO 23 K=1,300
23 Y(K)=Y(K)/ANSUM
   PRINT 201
   WRITE(6,201)
   PRINT 204,NF,NSC,NSUM,ALPH1,ALPH2,PEAK,ALPH3
   WRITE(6,204)NF,NSC,NSUM,ALPH1,ALPH2,PEAK,ALPH3
   IF(STPL.GE.3.9)GO TO 235
   CALL APL0T(300,IAP)
   IF(STPL.GE.1.9)GO TO 7
235 DO 24 K=1,300
24 Y(K)=Y(K)*ANSUM
25 NSFNF=NSF(NF)
C
C
C
C FOR INTERACTIVE ADJUSTMENT
  INPASS=1 $ GO TO 27
C
  INPASS=0
26 NUMBA=0 $ INPASS=INPASS+1
  PRINT 1002
262 READ 1001,APUT
   IF(APUT.NE.0.)GO TO 264 $ NUMBA=10 $ GO TO 262
264 PEAK=APUT
  PRINT 1003
  READ 1001,APUT
   IF(APUT.NE.0.)AMUL(NF)=APUT
1001 FORMAT(F13.2)
1002 FORMAT($ PEAK=*)
1003 FORMAT($ AMUL=*)
27 CONTINUE
C
C
C
C
DO 30 K=1,300
  YW(K)=AMBDAP(NSFNF) +AMUL(NF)*(PEAK-FLOAT(K))
  IF(INPASS.EQ.1)Y(K)=FRES(Y(K),YW(K))
30 CONTINUE
  IFITS=PEAK-(AMBDAP-AMRDAP(NSFNF))/AMUL(NF)
  IFITF=PEAK+(AMBDAP(NSFNF)-AMRDAS)/AMUL(NF)
  IFITS=MINO(IFITS,275)
  IFITF=MAXO(IFITF,1)
  IFITS=MAXO(IFITS,1)
  IFITF=MINO(IFITF,275)
  IF(STPL.GE.3.9)IFITS=1
  IF(STPL.GE.3.9)IFITF=300
  IF(STPL.LE.3.9)GO TO 37
  CALL APL0T(300,IAP)
  IF(STPL.GE.1.9)GO TO 7
37 IF(ASKY.NF,ALPH1)GO TO 50
DO 40 K=1,300
40 X(K)=Y(K)
  XPEAK=PEAK
  PRINT 204,NF,NSC,NSUM,ALPH1,ALPH2,PEAK,ALPH3
204 FORMAT(3X,I2,8X,I3,10X,I2,43X,A10,A9,F6.1,1X,A5)
  GO TO 7
50 CONTINUE
  CALL FIT(801,19,IFITS,IFITF,TF,TE,FN,WAC,WAK,0.,XPEAK,AMUL(NF))
  IDLIST(1)=NF*IDLIST(2)+NSC*IDLIST(3)+NSUM
  PRINT 203,NF,NSC,NSUM,TF,TE,ALPH1,ALPH2,PEAK,ALPH3
203 FORMAT(3X,I2,8X,I3,10X,I2,14X,F6.1,13X,F5.1,5X,A10,A9,F6.1,1X,A5)
C
C
C
C FOR INTERACTIVE ADJUSTMENT
  IF(NUMBA.NE.10)GO TO 26
C
C
C
C
  IF(NUMBA.EQ.0)GO TO 7
  CALL SHOT(YW,Y,1,275,SM)
  CALL NEWFIT(IDLIST,1,3,801, 1,275,TF,TE,MICRON(NF),19,WAC,WAK,
10,NUMBA,SM,XPEAK,AMUL(NF))
  GO TO 7
100 CONTINUE
  IF(NUMBA.EQ.1,OF,NUMBA.EQ.2)CALL ENDFIT
  STOP
  END

```

```

009050
009060
009070
009080
009090
009100
009110
009120
009130
009140
009150
009160
009170
009180
009190
009200
009210
009220
009230
009240
009250
009260
009270
009280
009290
009300
009310
009320
009330
009340
009350
009360
009370
009380
009390
009400
009410
009420
009430
009440
009450
009460
009470
009480
009490
009500
009510
009520
009530
009540
009550
009560
009570
009580
009590
009600
009610
009620
009630
009640
009650
009660
009670
009680
009690
009700
009710
009720
009730
009740
009750
009760
009770
009780
009790
009800
009810
009820
009830
009840
009850
009860
009870
009880

```

|   |                                              |        |
|---|----------------------------------------------|--------|
| L |                                              | 009900 |
| C |                                              | 009910 |
| C | 12 FRES                                      | 009920 |
| C |                                              | 009930 |
| C |                                              | 009940 |
|   | FUNCTION FRES(F,FLAND)                       | 009950 |
|   | FL=FLAND-4800.                               | 009960 |
| C | USED WITH HAWAII DATA                        | 009970 |
| C | FRES=F*(.930753+.0011915*FL-.00000504*FL*FL) | 009980 |
| C |                                              | 009990 |
| C |                                              | 010000 |
| C | USED WITH ALADDIN AND GENIE DATA             | 010010 |
|   | FRES=F*(1.+.0004903*FL)                      | 010020 |
| C |                                              | 010030 |
|   | RETURN                                       | 010040 |
|   | END                                          | 010050 |
| C |                                              | 010070 |
| C |                                              | 010080 |
| C | 13 FKAY                                      | 010090 |
| C |                                              | 010100 |
| C |                                              | 010110 |
|   | FUNCTION FKAY(KAYPRM)                        | 010120 |
| C | ALADDIN 74                                   | 010130 |
|   | DATA A/9818.9/.B/.0004572/.T/.0011618/       | 010140 |
| C | POST-ALADDIN JAN 75                          | 010150 |
|   | DATA A/1.7/.B/1.00788/.T/.0011621/           | 010160 |
| C |                                              | 010170 |
| C |                                              | 010180 |
| C | WSMR OCT 77                                  | 010190 |
|   | FKAY=KAYPRM                                  | 010200 |
|   | RETURN                                       | 010210 |
| C |                                              | 010220 |
| C |                                              | 010230 |
|   | FK=KAYPRM                                    | 010240 |
| C | USED UP TO APR 73 ON ALADDIN II DATA         | 010250 |
| C | FKAY=FK/(1.-FK/950.)                         | 010260 |
| C | SLIGHTLY DIFFERENT NO. FOR GOLIATH NOV 71    | 010270 |
| C | FKAY=FK/(1.-FK/949.217)                      | 010280 |
| C | AEOLUS MARCH 1975                            | 010290 |
|   | DATA A/2699.8/.B/.0002055/.T/.0010693/       | 010300 |
|   | FKAY=FK/(1.-FK*T)-BBA                        | 010310 |
|   | RETURN                                       | 010320 |
|   | END                                          | 010330 |

```

C
C
C 14 FIT POISSON
C
C SUBROUTINE FIT(N,NT,N1,N2,TF,TE,FM,WACC,WAKK,SM,XPEAK,ANUL)
C
C-----
C ZW WAVELENGTH ARRAY SYNTHETIC SPECTRA N ELEMENTS
C Z AMPLITUDE ARRAY NT BY N
C N
C T TEMPERATURE ARRAY NT ELEMENTS
C NT MUST BE LESS THAN 20
C YW MEASURED SPECTRA WAVELENGTH ARRAY NY ELEMENTS
C Y MEASURED SPECTRA AMPLITUDE ARRAY NY ELEMENTS
C NY
C IF BEST FIT TEMPERATURE
C TE ERROR BARS ON TEMPERATURE
C X = BACKGROUND ARRAY
C
C NOTE THE SYNTHETIC ARRAY MUST BE IN CONSTANT INCREMENTS IN WAVELENGTH
C-----
C
C DIMENSION WACC(20),WAKK(20),AA(20),AM(20),F(19)
C COMMON Y(300),X(300),YW(300),Z(801),ZW(801),T(19),DUM(801)
C AN=N-1
C I=N1
10 CONTINUE
C AK=AN*(YW(I)-ZW(I))/(ZW(N)-ZW(1))+1.
C IF(AK.GE.1. .AND. AK.LT.AN+1.) GO TO 20
C IF(AK-1.) 13,13,14
13 N1=I+1
C GO TO 20
14 N2=I-1
C GO TO 21
20 IF(I.GE.N2) GO TO 21
C I=I+1
C GO TO 10
21 D=N2-N1+1
C YMAX=0. $ YMIN=1.E+08 $ RYC=0.
C DO 40 I=N1,N2
C YMAX=AMAX1(YMAX,Y(I))
C YMIN=AMIN1(YMIN,Y(I))
C IF(Y(I).LT.5.) GO TO 4B1
C YII=Y(I)+1.
C RYC=RYC+(YII-.5)*ALOG(YII)-YII+1./((12.*YII)-1./((360.*YII**3)
C +1./((1260.*YII**5)-1./((1680.*YII**7)
C GO TO 4B5
4B1 KKY I
C KY=Y(I)+.5
C IF(KKY.EQ.2) KKY=2
C IF(KKY.EQ.3) KKY=6
C IF(KKY.EQ.4) KKY=24
C IF(KKY.EQ.5) KKY=120
C YKKY=FLOAT(KKY)
C RYC=RYC+ALOG(YKKY)
4B5 YIP=AMAX1(.01,Y(I))
C RYC=RYC-.5*ALOG(YIP)
40 CONTINUE
C WAK=YMAX-YMIN $ WAC=YMIN
C DO 50 J=1,NT
C CALL ZSTORE(J)
C LDDP=0
44 AZ=0. $ AYZ=0. $ AYD=0. $ AYZD2=0. $ AYD2=0. $ AYD2=0.
C LDDP=LDDP+1
C IF(LDDP.GT.50) F(J)=1.1117
C IF(LDDP.GT.50) GO TO 55
C DO 46 I=N1,N2
C AK=AN*(YW(I)-ZW(I))/(ZW(N)-ZW(1))+1.
C A=AK
C LK=K
C AK=AK-CK
C Z=Z+AK*Z(K) Z(K+1)=AK
C A=AZ/Z/D
C KA=WAK/Z/WAC
C B=Z(I)/(D*KA)
C BB=B/KK
C AYD=AYD+B
C AYD2=AYD2+B*B
C B=B/Z
C AYZD=AYZD+B

```

```

010350
010360
010370
010380
010390
010400
010410
010420
010430
010440
010450
010460
010470
010480
010490
010500
010510
010520
010530
010540
010550
010560
010570
010580
010590
010600
010610
010620
010630
010640
010650
010660
010670
010680
010690
010700
010710
010720
010730
010740
010750
010760
010770
010780
010790
010800
010810
010820
010830
010840
010850
010860
010870
010880
010890
010900
010910
010920
010930
010940
010950
010960
010970
010980
010990
011000
011010
011020
011030
011040
011050
011060
011070
011080
011090
011100
011110
011120
011130
011140
011150
011160
011170
011180

```

|     |                                                      |        |
|-----|------------------------------------------------------|--------|
|     | B=B/BA                                               | 011190 |
|     | AYZD2=AYZD2+B                                        | 011200 |
|     | B=B#ZZ                                               | 011210 |
|     | AYZD2=AYZD2+B                                        | 011220 |
| 44  | CONTINUE                                             | 011230 |
|     | DET=AYZD2*AYD2-AYZD2#82                              | 011240 |
|     | FNOT=AZ-AYZD 8 GNOT=1.-AYD                           | 011250 |
|     | DELK=(GNOT*AYZD2-FNOT*AYD2)/DET                      | 011260 |
|     | DELC=(FNOT*AYZD2-GNOT*AYZD2)/DET                     | 011270 |
|     | WAK=WAK+DELA 8 WAC=WAC+DELC                          | 011280 |
|     | IF(DELK.GT.1.E-108WAK.OR.DELC.GT.1.E-108WAC)GO TO 44 | 011290 |
|     | WACC(J)=WAC                                          | 011300 |
|     | WAKK(J)=WAK                                          | 011310 |
|     | IF(WAC.LT.0..OR.WAK.LT.0.)F(J)=1.E+13                | 011320 |
|     | IF(WAC.LT.0..OR.WAK.LT.0.)GO TO 55                   | 011330 |
|     | F(J)=0.                                              | 011340 |
|     | DO 50 I=N1,N2                                        | 011350 |
|     | AK=AN*(YU(I)-ZU(1))/(ZU(N)-ZU(1))+1.                 | 011360 |
|     | K=AK                                                 | 011370 |
|     | CK=K                                                 | 011380 |
|     | AK=AK-CK                                             | 011390 |
|     | ZZ=(1.-AK)*Z(K)+AK*Z(K+1)                            | 011400 |
|     | XI=1.                                                | 011410 |
|     | IF(XPEAK.LT..001)GO TO 48                            | 011420 |
|     | FK=XPEAK-(YU(I)-4861.34)/AMUL                        | 011430 |
|     | M=FK                                                 | 011440 |
|     | ACG=M                                                | 011450 |
|     | ACG=FK-ACG                                           | 011460 |
|     | XI=ACG*X(M+1)+(1.-ACG)*X(M)                          | 011470 |
| 48  | B=WAK#ZZ+WAC                                         | 011480 |
|     | B=B-Y(I)*ALOG(B)                                     | 011490 |
| 50  | F(J)=F(J)+B                                          | 011500 |
| 55  | F(J)=F(J)+BYC                                        | 011510 |
| 201 | FORMAT(IX,SE11.4)                                    | 011520 |
|     | FM=10.E+10                                           | 011530 |
|     | DO 60 J=1,NT                                         | 011540 |
|     | IF(F(J).LT.FM) JT=J                                  | 011550 |
|     | IF(F(J).LT.FM)FM=F(J)                                | 011560 |
| 60  | CONTINUE                                             | 011570 |
|     | IF(JT.EQ.1.OR.JT.EQ.NT) GO TO 71                     | 011580 |
|     | X1=T(JT-1)                                           | 011590 |
|     | X2=T(JT)                                             | 011600 |
|     | X3=T(JT+1)                                           | 011610 |
|     | DO 70 NN=1,3                                         | 011620 |
|     | GO TO (61,62,63),NN                                  | 011630 |
| 61  | Y1=F(JT-1)                                           | 011640 |
|     | Y2=F(JT)                                             | 011650 |
|     | Y3=F(JT+1)                                           | 011660 |
|     | GO TO 64                                             | 011670 |
| 62  | Y1=WACC(JT-1)                                        | 011680 |
|     | Y2=WACC(JT)                                          | 011690 |
|     | Y3=WACC(JT+1)                                        | 011700 |
|     | GO TO 64                                             | 011710 |
| 63  | Y1=WAKK(JT-1)                                        | 011720 |
|     | Y2=WAKK(JT)                                          | 011730 |
|     | Y3=WAKK(JT+1)                                        | 011740 |
| 64  | Y4=(Y2-Y1)/(X2-X1)                                   | 011750 |
|     | Y5=(Y3-Y2)/(X3-X2)                                   | 011760 |
|     | X4=(X2*X2-X1*X1)/(X2-X1)                             | 011770 |
|     | X5=(X3*X3-X2*X2)/(X3-X2)                             | 011780 |
|     | AQ=(Y5-Y4)/(X5-X4)                                   | 011790 |
|     | BQ=Y4-AQ*X4                                          | 011800 |
|     | CQ=Y1-AQ*X1+BQ*X1                                    | 011810 |
|     | GO TO (65,66,67),NN                                  | 011820 |
| 65  | TF=-BQ/(2.*AQ)                                       | 011830 |
|     | FM=AQ*TF*TF+BQ*TF+CQ                                 | 011840 |
|     | RM=FH*(1.+1./D)                                      | 011850 |
|     | TE=BQ*BQ-4.*AQ*(CQ-RM)                               | 011860 |
|     | TE=SQRT(TE)/(2.*AQ)                                  | 011870 |
|     | GO TO 70                                             | 011880 |
| 66  | WAC=AQ*TF*TF+BQ*TF+CQ                                | 011890 |
|     | GO TO 70                                             | 011900 |
| 67  | WAK=AQ*TF*TF+BQ*TF+CQ                                | 011910 |
| 70  | CONTINUE                                             | 011920 |
|     | GO TO 72                                             | 011930 |
| 71  | TF=T(JT)                                             | 011940 |
|     | TE=999.0                                             | 011950 |
| 72  | RETURN                                               | 011960 |
|     | END                                                  | 011970 |
|     |                                                      | 011980 |

|      |                                                                |        |
|------|----------------------------------------------------------------|--------|
| C    |                                                                | 012000 |
| C    |                                                                | 012010 |
| C 15 | ZSTORE                                                         | 012020 |
| C    |                                                                | 012030 |
| C    |                                                                | 012040 |
|      | SUBROUTINE ZSTORE(L)                                           | 012050 |
|      | COMMON Y(300),X(300),YM(300),Z(801),ZW(801),T(19),DUM(801)     | 012060 |
|      | IF(L.LT.1) GO TO 16                                            | 012070 |
|      | IF(L-LL)91,100,6                                               | 012080 |
| 6    | LM=LL+1                                                        | 012090 |
|      | DO 8 M=LM,L                                                    | 012100 |
| 8    | READ(3)IV,TT,MM,KK,( Z(JJ),JJ=1,801)                           | 012110 |
|      | LL=L                                                           | 012120 |
|      | GO TO 100                                                      | 012130 |
| 16   | N5=13267898122369                                              | 012140 |
|      | IF(N4.NE.N5)N2=N5                                              | 012150 |
|      | N4=N5                                                          | 012160 |
|      | NF=-L                                                          | 012170 |
|      | IF(NF.GT.N2)GO TO 22                                           | 012180 |
| 20   | REWIND 3                                                       | 012190 |
|      | N2=1                                                           | 012200 |
| 22   | N3=N2+1                                                        | 012210 |
|      | IF(NF.EQ.1) GO TO 28                                           | 012220 |
| 23   | DO 25 N1=N3,NF                                                 | 012230 |
| 24   | READ(3)IV,TT,MM,KK,( Z(JJ),JJ=1,801)                           | 012240 |
|      | IF(EOF(3))25,24                                                | 012250 |
| 25   | CONTINUE                                                       | 012260 |
| 28   | LL=0                                                           | 012270 |
| 90   | N2=NF                                                          | 012280 |
|      | IF(L-1)100,6,6                                                 | 012290 |
| 91   | BACKSPACE 3                                                    | 012300 |
| 92   | LL=LL-1                                                        | 012310 |
|      | BACKSPACE 3                                                    | 012320 |
|      | IF(L.LT.LL)GO TO 92                                            | 012330 |
|      | READ(3)IV,TT,MM,KK,( Z(JJ),JJ=1,801)                           | 012340 |
| 100  | CONTINUE                                                       | 012350 |
|      | RETURN                                                         | 012360 |
|      | END                                                            | 012370 |
| C    |                                                                | 012390 |
| C    |                                                                | 012400 |
| C 16 | SHOT RECTANGULAR                                               | 012410 |
| C    |                                                                | 012420 |
| C    |                                                                | 012430 |
|      | SUBROUTINE SHOT(X,Y,N1,N2,A)                                   | 012440 |
|      | COMMON YD(300),XD(300),YMD(300),ZD(801),ZMD(801),TD(19),Z(801) | 012450 |
|      | DIMENSION X(1),Y(1)                                            | 012460 |
|      | IF(A.LE..001)GO TO 100                                         | 012470 |
|      | AS=(X(N1)-X(N2))/(N1-N2)                                       | 012480 |
|      | AS=ABS(AS)                                                     | 012490 |
|      | II=.5*A/AS+.5001                                               | 012500 |
|      | NN=2*II-1                                                      | 012510 |
|      | II=II-1                                                        | 012520 |
|      | NN1=N1+II * NN2=N2-II                                          | 012530 |
|      | DO 30 I=NN1,NN2                                                | 012540 |
|      | Z(I)=Y(I)                                                      | 012550 |
|      | DO 30 J=1,II                                                   | 012560 |
|      | I=I-J * JI=I+J                                                 | 012570 |
|      | Z(I)=Z(I)+(Y(IJ)+(JI))                                         | 012580 |
| 30   | CONTINUE                                                       | 012590 |
|      | DO 40 I=NN1,NN2                                                | 012600 |
| 40   | Y(I)=Z(I)/FLOAT(NN)                                            | 012610 |
| 100  | RETURN                                                         | 012620 |
|      | END                                                            | 012630 |
| C    |                                                                | 012650 |
| C    |                                                                | 012660 |
| C 17 | ISNN                                                           | 012670 |
| C    |                                                                | 012680 |
| C    |                                                                | 012690 |
|      | SUBROUTINE ISNN(N,K,ISN)                                       | 012700 |
|      | DIMENSION II(30)                                               | 012710 |
|      | IF(K)20,20,10                                                  | 012720 |
| 10   | N6=132876981239                                                | 012730 |
|      | IF(N4.NF.N6) N2=N6                                             | 012740 |
|      | N4=N6                                                          | 012750 |
|      | NF=N                                                           | 012760 |
|      | GO TO 100                                                      | 012770 |
| 20   | IF(NF-N2)21,31,22                                              | 012780 |
| 21   | REWIND 2                                                       | 012790 |
|      | N5=-29                                                         | 012800 |
|      | IF(NF.FD.1)GO TO 32                                            | 012810 |
|      | N2=-1                                                          | 012820 |
| 22   | N5=-29                                                         | 012830 |
|      | N4=N5                                                          | 012840 |
|      | DO 30 N1=N4,N5                                                 | 012850 |

|     |                             |        |
|-----|-----------------------------|--------|
| 25  | READ(2,209)(II(NN),NN=1,30) | 012860 |
|     | IF(EOF(2))30,25             | 012870 |
| 30  | CONTINUE                    | 012880 |
|     | GO TO 32                    | 012890 |
| 31  | IF(N.LT.N5)GO TO 50         | 012900 |
|     | IF(N.GE.N5+30)GO TO 32      | 012910 |
|     | GO TO 81                    | 012920 |
| 32  | N2=NF                       | 012930 |
|     | N5=N5+30                    | 012940 |
|     | DO 40 N1=N5,N,30            | 012950 |
|     | N11=N1                      | 012960 |
| 40  | READ(2,209)(II(NN),NN=1,30) | 012970 |
| 209 | FORMAT(30I3)                | 012980 |
|     | N5=N11                      | 012990 |
|     | GO TO 81                    | 013000 |
| 50  | BACKSPACE 2                 | 013010 |
| 51  | N5=N5-30                    | 013020 |
|     | BACKSPACE 2                 | 013030 |
|     | IF(N.LT.N5) GO TO 51        | 013040 |
|     | READ(2,209)(II(NN),NN=1,30) | 013050 |
| 81  | NN=N-N5+1                   | 013060 |
|     | ISN=II(NN)                  | 013070 |
| 100 | RETURN                      | 013080 |
|     | END                         | 013090 |

|      |                                                                      |        |
|------|----------------------------------------------------------------------|--------|
| C    |                                                                      | 013140 |
| C    |                                                                      | 013150 |
| C    | SUBROUTINE NEWPLT(IDLIST,K1,K2,NSYP,N1,N2,TF,TE,MICRON,NT,ACC,       | 013160 |
|      | IAKK,IV,NUMBA,BN,XPEAK,AMUL)                                         | 013170 |
| C    |                                                                      | 013180 |
| C    | MAKES FANCY PLOT OF SYNTHETIC SPECTRA COMBINED WITH MEASURED SPECTRA | 013190 |
| C    | IDLIST(K1) TO IDLIST(K2) IS A LIST OF SCAN NUMBERS TO BE PLOTTED     | 013200 |
| C    | Z(NT,NSYP) IS AN ARRAY OF SYNTHETIC SPECTRA                          | 013210 |
| C    | ZW IS THE ARRAY OF WAVELENGTHS FOR THE ELEMENTS IN Z                 | 013220 |
| C    | Y IS AN ARRAY OF MEASURED SPECTRA WITH NYEL ELEMENTS                 | 013230 |
| C    | YW IS THE ARRAY OF WAVELENGTHS FOR THE ELEMENTS IN Y                 | 013240 |
| C    | IF IS THE BEST FIT TEMPERATURE FOR THAT SUM OF SCANS BY WFIT         | 013250 |
| C    | TE IS THE ERROR BAR ON TF                                            | 013260 |
| C    | MICRON IS THE SLIT WIDTH CODE IN MICRONS                             | 013270 |
| C    | T IS THE ARRAY OF TEMPERATURES USED IN THE SYNTHETIC CURVES          | 013280 |
| C    | NT IS THE NUMBER OF TEMPERATURES                                     | 013290 |
| C    | ACC AND AKK ARE THE BEST ADDITIVE AND MULTIPLICATIVE CONSTANTS       | 013300 |
| C    | IV SEQUENCE OF ALO USED                                              | 013310 |
| C    |                                                                      | 013320 |
|      | DIMENSION IDLIST(1)                                                  | 013330 |
|      | DIMENSION ACC(20),AKK(20)                                            | 013340 |
|      | COMMON Y(300),X(300),YW(300),Z(801),ZW(801),T(19),YP(801)            | 013350 |
|      | INTEGER H                                                            | 013360 |
| C    | DRAW AXIS                                                            | 013370 |
|      | IF(NUMBA.EQ.10)GO TO 5                                               | 013380 |
|      | CALL SUPAPL(IV,2,1,NUMBA,0,0)                                        | 013390 |
|      | GO TO 6                                                              | 013400 |
|      | 5 TID=IDLIST(3)                                                      | 013410 |
|      | CALL PLOT(1,ZW,Z,IDLIST(1),IDLIST(2),TID)                            | 013420 |
| C    | FIND NUMBER OF BEST FIT TEMPERATURE                                  | 013430 |
|      | 6 TT=T(NT)                                                           | 013440 |
|      | DO 1010 N=1,NT                                                       | 013450 |
|      | DT=ABS(T (N)-TF)                                                     | 013460 |
|      | IF(DT.LT.TT)LL=N                                                     | 013470 |
| 1010 | IF(DT.LT.TT)TT=DT                                                    | 013480 |
|      | YMAX=0.                                                              | 013490 |
|      | DO 8 M=N1,N2                                                         | 013500 |
| B    | YMAX=AMAX1(YMAX,Y(M))                                                | 013510 |
| C    | IF NUMBA=7 A CRT PLOT WILL BE MADE.                                  | 013520 |
| C    | IF NUMBA=10 A PRINT PLOT WILL BE MADE.                               | 013530 |
| C    | IF NUMBA=1 A PEN PLOT WILL BE MADE.                                  | 013540 |
| C    | FOR PEN PLOT PF NAMED PENPLOTS MUST BE LOADED.                       | 013550 |
| C    | FOR CRT PLOT PF NAMED CRTPLOTS MUST BE LOADED.                       | 013560 |
| C    | FOR PRINT PLOT PF NAMED KITMAPAD MUST BE LOADED.                     | 013570 |
|      | NDI=NYEL-3                                                           | 013580 |
| C    | PLOT SYNTHETIC SPECTRA                                               | 013590 |
|      | DO 32 I=1,NSYP                                                       | 013600 |
|      | I2=I-1                                                               | 013610 |
|      | IF(ZW(I).GT.YW(N1))GO TO 33                                          | 013620 |
| 32   | CONTINUE                                                             | 013630 |
| 33   | DO 34 I=1,NSYP                                                       | 013640 |
|      | I1=I                                                                 | 013650 |
|      | IF(ZW(I).GE.YW(N2))GO TO 35                                          | 013660 |
| 34   | CONTINUE                                                             | 013670 |
| 35   | DO 1100 MM=1,5                                                       | 013680 |
|      | L=LL+MM-3                                                            | 013690 |
|      | IF(L.LT.1.OR.L.GT.19)GO TO 1100                                      | 013700 |
|      | CALL ZSTORE(L)                                                       | 013710 |
| C    | SHOT CHANGES PRESENT Z ARRAY                                         | 013720 |
|      | CALL SHOT(ZW,Z,I1,I2,SH)                                             | 013730 |
|      | IF(MH.NE.1)GO TO 37                                                  | 013740 |
| 37   | DO 38 I=1,NSYP                                                       | 013750 |
|      | Z(I)=(Z(I)*AKK(L)+ACC(L))/YMAX                                       | 013760 |
|      | Z(I)=AMAX1(Z(I),.01)                                                 | 013770 |
| 38   | Z(I)=4.*ALOG10(Z(I))*R.                                              | 013780 |
|      | IF(NUMBA-10)40,39,40                                                 | 013790 |
| 39   | CALL PLOT(MH+1,ZW,Z,1,NSYP,T(L))                                     | 013800 |
|      | GO TO 1100                                                           | 013810 |
| 40   | IF=3                                                                 | 013820 |
|      | DO 1090 M=1,NSYP                                                     | 013830 |
|      | ZZ=Z(M)                                                              | 013840 |
|      | X3=(ZW (M)-4800.+200.*FLOAT(IV))*R.                                  | 013850 |
|      | IF(ZZ.GT.8..OR.ZZ.LT.0..OR.X3.LT.0.)GO TO 1090                       | 013860 |
|      | IF(X3.GT.12.)GO TO 1096                                              | 013870 |
|      | CALL PLOT(X3,ZZ,IP)                                                  | 013880 |
| 1090 | IP=2                                                                 | 013890 |
| 1096 | AL=MM                                                                | 013900 |
| C    | TABLE SYNTHETIC SPECTRA FOR TEMPERATURE                              | 013910 |
|      | CALL NUMBER(12.5,AL,.2,T (L),0.,-1)                                  | 013920 |
|      | CALL SYMBOL(13.5,AL,.2,SHDED K,0.,5)                                 | 013930 |
| 1100 | CONTINUE                                                             | 013940 |
| C    | PLOT MEASURED SPECTRA                                                | 013950 |
|      | IP=3                                                                 | 013960 |
|      | DO 1049 M=N1,N2                                                      | 013970 |

```

X2=(YM      (M)-4800.+200.*FLOAT(IV))*.08      013980
XM=1.      013990
IF(XPEAK.LT..001)GO TO 1055      014000
FK=XPEAK-(YM      (M)-4861.34)/AMUL      014010
I=FK      014020
ACG=I      014030
ACG=FK-ACG      014040
XM=ACG*X(I+1)+(1.-ACG)*X(I)      014050
1055 YY=100.*Y(M)/YMAX      014060
YY=AMAX1(YY,1.)      014070
Y3=4.*ALOG10(YY)      014080
YP(M)=Y3      014090
IF(X2.LT.0..OR.Y3.LT.0..OR.Y3.GT.9.)GO TO 1069      014100
IF(X2.GT.12.)GO TO 1070      014110
IF(NUMBA.EQ.10)GO TO 1069      014120
CALL FLOT(X2,Y3,IP)      014130
1069 IP=2      014140
1070 IF(NUMBA.NE.10)GO TO 1071      014150
CALL FPLOT(7,YM,YP,N1,N2,TF)      014160
CALL FPLOT(8,ZW,Z,1,NSYP,TE)      014170
GO TO 100      014180
C WRITE TEMPERATURE OF MEASURED SPECTRA      014190
1071 CONTINUE      014200
CALL SYMBOL(0.,8.5,.2,31HTEMPERATURE = +OR- DEG K,0.,.31)      014210
CALL NUMBER(2.8,8.5,.2,TF,0.,-1)      014220
CALL NUMBER(4.6,8.5,.2,TE,0.,-1)      014230
C WRITE SCAN NUMBERS      014240
YT=9.29      014250
XT=2.      014260
CALL SYMBOL(0.,9.29,.19,9HSCAN NOS.,0.,.9)      014270
DO 1080 K=K1,K2      014280
FPN=IDLIST(K)      014290
CALL NUMBER(XT,YT,.19,FPN,0.,-1)      014300
XT=XT+1.      014310
IF(XT.LT.12.)GO TO 1080      014320
XT=2.      014330
YT=YT-.35      014340
1080 CONTINUE      014350
C LABEL SLIT SIZE      014360
IF(MICRON.EQ.250)CALL SYMBOL(8.,8.5,.2,20HSLIT = 2.5 ANGSTROMS,0.,.14370
120)      014380
IF(MICRON.EQ.251)CALL SYMBOL(8.,8.5,.2,20HSLIT = 3.5 ANGSTROMS,0.,.14390
120)      014400
IF(MICRON.EQ.450)CALL SYMBOL(8.,8.5,.2,20HSLIT = 4.0 ANGSTROMS,0.,.14410
120)      014420
100 RETURN      014430
END      014440
C      014460
C      014470
C 19 PRINT PLOT      014480
C      014490
C      014500
SUBROUTINE FPLOT(KOD,X,Y,N1,N2,TITL)      014510
DIMENSION TITLE(70),X(1),Y(1)      014520
DATA MCTR/4860./,HGRD/12./,VCTR/4./,VGRD/1.7143/,FST/0./      014530
DATA TITLE/6HWAVELN,6H (ANG),6HAMPLIT,3HUDE,-1.,0.,6H FILE,      014540
+6H SCAN,6H SUMMED,0.,0.,0.,6HTEMPFRAT,3HURE,0.,0.,      014550
+6H(K) +OR-,0.,0.,0.,0.,1HE,0.,0.,1HR,0.,0.,1HC,0.,0.,1NR,      014560
+0.,0.,1HA/      014570
IF(FST.NE.0.)GO TO 11      014580
DO 10 J=35,70      014590
10 TITLE(J)=0.      014600
DO 101 J=50,62,3      014610
101 TITLE(J)=-1.      014620
DO 102 J=40,42      014630
102 TITLE(J)=-1.      014640
TITLE(48)=TITLE(46)+1.      014650
TITLE(64)=999.      014660
TITLE(34)=3HXXX      014670
11 FST=1.      014680
KOD=3      014690
IF(KOD.EQ.1)KOD=0      014700
IF(KOD.EQ.8)KOD=4      014710
TITLE(65)=KOD-1      014720
IF(KOD.EQ.7)TITLE(65)=29.      014730
IF(KOD.NE.1)GO TO 12      014740
TITLE(10)=N1 & TITLE(11)=N2 & TITLE(12)=TITL      014750
12 CONTINUE      014760
IF(KOD.EQ.7)TITLE(16)=TITL      014770
IF(KOD.EQ.8)TITLE(18)=TITL      014780
IF(KOD.GE.2.AND.KOD.LE.6)TITLE(-3&KOD+38)=TITL      014790
CALL MAF(X,Y,N1,N2,KOD,MCTR,HGRD,VCTR,VGRD,TITLE)      014800
RETURN      014810
END      014820

```

```

C
SUBROUTINE SUPAPL(IV,TYPE,IAxis,NUMBA,IDIM,ID)
C
C MAKES VARIOUS FORMS OF PLOTS FOR ALO TEMPERATURE PROBLEMS
C IV=0,1 FOR DELTA V = 0 OR DELTA V = 1
C TYPE=0,2,5, FOR A LINEAR, 2 CYCLE LOG OR SQUARE ROOT PLOTS, RESPECTIVELY
C IAXIS=0,1 FOR NO NEW AXIS OR NEW AXIS
C NUMBA=NO. OF PLOTS TO BE MADE (NOT NO OF AXIS)
C NUMBA 5 OR LESS IS PEN AND INK PLOT, 6 OR GREATER IS CRT PL
C IDIM=DIMENSION OF INPUT ARRAY, YARRAY, FROM LEFT TO RIGHT
C IF IDIM=0 NO CURVE IS PLOTTED
C YARRAY=ARRAY TO BE PLOTTED
C ID= IDENTIFICATION NUMBER TO BE PRINTED WITH AXIS(4 DIGITS)
C IF ID=0 NO NUMBER IS PRINTED AT ALL
C
C INTEGER TYPE
C DIMENSION YARRAY(1)
C DIMENSION FRID(3)
C FRID(1)=10HATROSSER
C FRID(2)=DATE(DDMM)
C FRID(3)=TIME(TDUM)
C IF(MSTART.NE.3624321061.AND.NUMBA.LE.5)CALL FLTID3(FRID,340.,11.,
11.)
C IF(MSTART.NE.3624321061.AND.NUMBA.LE.5)CALL NEWPEN(3)
C IF(MSTART.NE.3624321061.AND.NUMBA.GE.6)CALL CRTPLT(FRID,1.,17.)
C IF(MSTART.NE.3624321061)MEND=0
C IF(MSTART.NE.3624321061)CALL PLOT(1.,1.,-3)
C MSTART=3624321061
C MEND=MEND+1
C IF(IAXIS.EQ.0)GO TO 400
C AXIS
C IF(MEND.NE.1.AND.NUMBA.GE.6)CALL FRAME(1.5,1.5)
C IF(MEND.NE.1.AND.NUMBA.LE.5)CALL PLOT(17.,0.,-3)
C THE FOUR BORDER AXIS
C CALL PLOT(0.,0.,3)
C CALL PLOT(12.,0.,2)
C CALL PLOT(12.,8.,2)
C CALL PLOT(0.,8.,2)
C CALL PLOT(0.,0.,2)
C X AXIS FEDUCIARIES
C DO 120 K=1,2
C DO 120 I=1,149
C A=.05
C IF(I.EQ.5*(I/5))A=.1
C IF(I.EQ.10*(I/10))A=.15
C B=I
C B=.08*B
C C=0.
C IF(K.EQ.2)A=B.-A
C IF(K.EQ.2)C=B.
C CALL PLOT(B,A,3)
C CALL PLOT(B,C,2)
120 CONTINUE
C LABEL X AXIS
C IA=4800-200*IV
C IB=IA/150
C DO 303 M=IA,IB,10
C X=M-IA
C IF(M.LE.50*(M/50))GO TO 301
C FPN=M/100*(M/100)
C X=.08*X-.11
C CALL NUMBER(X,-.35,.15,FPN,0.,-1)
C GO TO 302
301 FPN M
C X=.08*X-.35
C CALL NUMBER(X,-.4,.2,FPN,0.,-1)
302 CONTINUE
303 CONTINUE
C CALL SYMBOL(3.8,-.8,.2,22HWAULENGTH (ANGSTROMS),0.,22)
C CALL SYMBOL(6.2,-.6,.2,1H.,0.,1)
C CALL SYMBOL(7.4,-.8,.2,1H./0.,1)
C CALL PLOT(3.8/, 1.25,3)
C CALL PLOT(4.0/, 1.25,2)
C CALL PLOT(3.9/, -1.07,2)
C CALL PLOT(3.8/, -1.25,2)
C CALL SYMBOL(4.12,-1.25,.25,14HV= SEQUENCE A,0.,14)
C CALL SYMBOL(7.62,-1.25,.15,1HL,0.,1)
C CALL SYMBOL(7.77,-1.25,.25,1HD,0.,1)
C FPN=IV
C CALL NUMBER(4.62,-1.25,.25,FPN,0.,-1)
C LABEL Y AXIS
C IF(ID)1004,1004,1005
1004 CONTINUE
C CALL SYMBOL(1.1,2.3,.2,24HRELATIVE INTENSITY ,90.,26)

```

```

014880
014890
014900
014910
014920
014930
014940
014950
014960
014970
014980
014990
015000
015010
015020
015030
015040
015050
015060
015070
015080
015090
015100
015110
015120
015130
015140
015150
015160
015170
015180
015190
015200
015210
015220
015230
015240
015250
015260
015270
015280
015290
015300
015310
015320
015330
015340
015350
015360
015370
015380
015390
015400
015410
015420
015430
015440
015450
015460
015470
015480
015490
015500
015510
015520
015530
015540
015550
015560
015570
015580
015590
015600
015610
015620
015630
015640
015650
015660
015670
015680
015690
015700

```

```

      GO TO 1006
1005 CONTINUE
      FIDNO=ID
      CALL SYMBOL(-1.1,1.1,.2,26HRELATIVE INTENSITY NUMBER,90.,26)
      CALL NUMBER(-1.1,6.5,.2,FIDNO,90.,-1)
1006 CONTINUE
C     LINEAR Y AXIS FEDUCIARIES
      IF (TYPE-2) 1020,200,1021
1020 DO 180 A=1,2
      DO 180 I=1,59
        A=.05
        IF (1.EQ.5*(1/5)) A=.1
        IF (1.EQ.10*(1/10)) A=.15
        B=I
        R=.08*B
        C=0.
        IF (K.EQ.2) A=12.-A
        IF (K.EQ.2) C=12.
        CALL PLOT(A,B,3)
        CALL PLOT(C,R,2)
180 CONTINUE
C     LABE Y AXIS LINEARLY
      CALL NUMBER(-.25,-.1,.2,0.,0.,-1)
      DO 340 M=10,90,10
        Y=M
        YY=.08*Y-.1
        CALL NUMBER(-.45,YY,.2,Y,0.,-1)
340 CONTINUE
      CALL NUMBER(-.65,7.9,.2,100.,0.,-1)
      GO TO 270
C     LOGARITHMIC Y AXIS FEDUCIARIES
200 DO 260 J=1,2
      DO 260 K=1,2
        DO 210 MA=1,4
          DO 210 M=1,4
            AMA=MA-1
            A=M
            A=4.*ALOG10(.1*A+1+.5*AMA)
            FK=K
            A=A+4.*FK-4.
            FJ=J
            B=11.95*FJ-11.95
            C=R+.05
            CALL PLOT(B,A,3)
            CALL PLOT(C,A,2)
210 CONTINUE
            DO 220 MA=3,6
              DO 220 M=2,8,2
                A=M
                AMA=MA
                A=4.*ALOG10(.1*A+AMA)
                FK=K
                A=A+4.*FK-4.
                FJ=J
                B=11.90*FJ-11.90
                C=R+.1
                CALL PLOT(B,A,3)
                CALL PLOT(C,A,2)
220 CONTINUE
                DO 230 M=1,8
                  A=M
                  A=4.*ALOG10(A+1.)
                  FK=K
                  A=A+4.*FK-4.
                  FJ=J
                  B=11.80*FJ-11.80
                  C=R+.2
                  CALL PLOT(B,A,3)
                  CALL PLOT(C,A,2)
230 CONTINUE
                DO 240 M=1,2
                  A=M
                  A=4.*ALOG10(A+.5)
                  FK=K
                  A=A+4.*FK-4.
                  FJ=J
                  B=11.85*FJ-11.85
                  C=R+.15
                  CALL PLOT(B,A,3)
                  CALL PLOT(C,A,2)
240 CONTINUE
                DO 250 M=1,3
                  A=M
                  A=4.*ALOG10(A+.5)

```

```

015710
015720
015730
015740
015750
015760
015770
015780
015790
015800
015810
015820
015830
015840
015850
015860
015870
015880
015890
015900
015910
015920
015930
015940
015950
015960
015970
015980
015990
016000
016010
016020
016030
016040
016050
016060
016070
016080
016090
016100
016110
016120
016130
016140
016150
016160
016170
016180
016190
016200
016210
016220
016230
016240
016250
016260
016270
016280
016290
016300
016310
016320
016330
016340
016350
016360
016370
016380
016390
016400
016410
016420
016430
016440
016450
016460
016470
016480
016490
016500
016510
016520
016530
016540
016550
016560
016570
016580
016590
016600
016610
016620
016630
016640
016650
016660
016670
016680
016690
016700
016710
016720
016730
016740
016750
016760
016770
016780
016790
016800
016810
016820
016830
016840
016850
016860
016870
016880
016890
016900
016910
016920
016930
016940
016950
016960
016970
016980
016990
017000

```

|                                            |        |
|--------------------------------------------|--------|
| FA-A                                       | 016550 |
| A=44.8FA-4.                                | 016560 |
| FJ=J                                       | 016570 |
| R=11.85*FJ-11.85                           | 016580 |
| C=R+.15                                    | 016590 |
| CALL PLOT(B,A,3)                           | 016600 |
| CALL PLOT(C,A,2)                           | 016610 |
| 250 CONTINUE                               | 016620 |
| A=4.                                       | 016630 |
| F=J                                        | 016640 |
| R=11.75*FJ-11.75                           | 016650 |
| C=R+.25                                    | 016660 |
| CALL PLOT(B,A,3)                           | 016670 |
| CALL PLOT(C,A,2)                           | 016680 |
| 260 CONTINUE                               | 016690 |
| C LABEL Y AXIS LOGARITHMICALLY             | 016700 |
| DO 310 M=1,9                               | 016710 |
| FFN=M                                      | 016720 |
| Y=4.*ALOG10(FFN)-.08                       | 016730 |
| CALL NUMBER(-.2,Y,.15,FFN,0.,-1)           | 016740 |
| 310 CONTINUE                               | 016750 |
| DO 320 M=10,90,10                          | 016760 |
| FFN=M                                      | 016770 |
| Y=4.*ALOG10(FFN)-.08                       | 016780 |
| CALL NUMBER(-.35,Y,.15,FFN,0.,-1)          | 016790 |
| 320 CONTINUE                               | 016800 |
| CALL NUMBER(-.5,7.93,.15,100.,0.,-1)       | 016810 |
| GO TO 270                                  | 016820 |
| 1021 CONTINUE                              | 016830 |
| C LABEL Y AXIS FOR SQUARE ROOT             | 016840 |
| CALL NUMBER(-.2,-.08,.15,0.,0.,-1)         | 016850 |
| DO 1022 M=10,90,10                         | 016860 |
| FFN=M                                      | 016870 |
| Y=.8*SQRT(FFN)-.08                         | 016880 |
| CALL NUMBER(-.35,Y,.15,FFN,0.,-1)          | 016890 |
| 1022 CONTINUE                              | 016900 |
| CALL NUMBER(-.5,7.92,.15,100.,0.,-1)       | 016910 |
| C SQUARE ROOT FEDUCIARIES                  | 016920 |
| DO 1028 K=1,2                              | 016930 |
| DO 1028 I=1,99                             | 016940 |
| A=.05                                      | 016950 |
| IF(MOD(I,5).EQ.0)A=.1                      | 016960 |
| IF(MOD(I,10).EQ.0)A=.15                    | 016970 |
| B=I                                        | 016980 |
| R=.8*SQRT(B)                               | 016990 |
| C=0.                                       | 017000 |
| IF(K.EQ.2)A=12.-A                          | 017010 |
| IF(K.EQ.2)C=12.                            | 017020 |
| CALL PLOT(A,B,3)                           | 017030 |
| CALL PLOT(C,B,2)                           | 017040 |
| 1028 CONTINUE                              | 017050 |
| 270 CONTINUE                               | 017060 |
| 400 CONTINUE                               | 017070 |
| IF(IDIM.EQ.0)GO TO 407                     | 017080 |
| C PLOT                                     | 017090 |
| IT=3                                       | 017100 |
| YMAX=0.                                    | 017110 |
| DO 401 I=1,IDIM                            | 017120 |
| IF(YARRAY(I).GT.YMAX)YMAX=YARRAY(I)        | 017130 |
| 401 CONTINUE                               | 017140 |
| DO 403 I=1,IDIM                            | 017150 |
| X=I                                        | 017160 |
| DIM IDIM=1                                 | 017170 |
| X=X+IDIM/DIM                               | 017180 |
| IF(I.EQ.2)402,403,406                      | 017190 |
| 402 Y=YARRAY(I)*(B./YMAX)                  | 017200 |
| GO TO 404                                  | 017210 |
| 403 IF(YARRAY(I).LT.0.)YARRAY(I)=YMAX/100. | 017220 |
| Y=4.*ALOG10(100.*(YARRAY(I)/YMAX))         | 017230 |
| GO TO 404                                  | 017240 |
| 406 IF(YARRAY(I).LT.0.)YARRAY(I)=0.        | 017250 |
| Y=.8*SQRT(YARRAY(I)/YMAX)                  | 017260 |
| 404 IF(Y.LT.0.)Y=0.                        | 017270 |
| CALL PLOT(X,Y,IT)                          | 017280 |
| IT=2                                       | 017290 |
| 405 CONTINUE                               | 017300 |
| 407 RETURN                                 | 017310 |
| END                                        | 017320 |

|      |                                                            |        |
|------|------------------------------------------------------------|--------|
| C 21 | AFLOT                                                      | 017360 |
| C    |                                                            | 017370 |
| C    |                                                            | 017380 |
|      | SUBROUTINE AFLOT(NE,ND)                                    | 017390 |
|      | DIMENSION IFO(3),B(121)                                    | 017400 |
|      | COMMON Y(300),X(300),YM(300),Z(801),ZW(801),T(19),DUM(801) | 017410 |
|      | DATA IFO/10H(1X,I3,1X,,10HF5,2,1X,12,10H1A1 )/             | 017420 |
| C    | NE=NUMBER OF ELEMENTS IN ARRAY TO BE PLOTTED.              | 017430 |
| C    | Y=ARRAY TO BE PLOTTED.                                     | 017440 |
| C    | ND=NUMBER OF DECARES FOR LOG PLOT.                         | 017450 |
| C    | ND=0 MAKES LINEAR PLOT.                                    | 017460 |
| C    | ND=NEGATIVE GIVES THAT FRACTION OF A DECAH.                | 017470 |
| C    | CALL AFLOT(-1,DUMMY,NSIZE) TO SET WIDTH OF PLOT.           | 017480 |
| C    | DEFAULT VALUE IS 120 SPACES.                               | 017490 |
| C    | MAXIMUM WIDTH IS 120 SPACES.                               | 017500 |
|      | DATA A0/1H /,A1/1H,/                                       | 017510 |
|      | NSIZE=120                                                  | 017520 |
|      | SIZE=NSIZE                                                 | 017530 |
|      | YM=0.                                                      | 017540 |
|      | DO 10 N=1,NE                                               | 017550 |
| 10   | YM=AMAX1(YM,Y(N))                                          | 017560 |
|      | IF(ND,NE,0)F=NSIZE/ND                                      | 017570 |
|      | IF(ND,LT,0)F=-NSIZE*ND                                     | 017580 |
|      | DO 40 N=1,NE                                               | 017590 |
|      | YN=Y(N)/YM                                                 | 017600 |
|      | IF(ND,EQ,0)GO TO 21                                        | 017610 |
|      | YN=AMAX1(YN,.0000000001)                                   | 017620 |
|      | NY=ALOG10(YN)*F+SIZE+1.000001                              | 017630 |
|      | GO TO 22                                                   | 017640 |
| 21   | NY=SIZE*YN+1.000001                                        | 017650 |
| 22   | NY=MAX0(1,NY)                                              | 017660 |
|      | NY=MIN0(NSIZE+1,NY)                                        | 017670 |
|      | NSIZE1=NSIZE+1                                             | 017680 |
|      | DO 30 J=1,NSIZE1                                           | 017690 |
| 30   | B(J)=A0                                                    | 017700 |
|      | B(NY)=A1                                                   | 017710 |
|      | YN=ABS(Y(N))                                               | 017720 |
|      | YN=AMAX1(YN,.000000000001)                                 | 017730 |
|      | IAL=ALOG10(YN)+1.0000000001                                | 017740 |
|      | IAL=J1-IAL                                                 | 017750 |
|      | IAL=MIN0(31,IAL)                                           | 017760 |
|      | IF(IAL,LE,26)GO TO 37                                      | 017770 |
|      | CALL MXPCTX(IAL,IFO(2),4)                                  | 017780 |
|      | WRITE(6,IFO)N,Y(N),(B(J),J=1,NY)                           | 017790 |
|      | GO TO 40                                                   | 017800 |
| 37   | NYN=Y(N)                                                   | 017810 |
|      | WRITE(6,292)N,NYN,(B(J),J=1,NY)                            | 017820 |
| 292  | FORMAT(1X,I3,1X,I5,1X,121A1)                               | 017830 |
| 40   | CONTINUE                                                   | 017840 |
|      | CONTINUE                                                   | 017850 |
|      | CONTINUE                                                   | 017860 |
|      | CONTINUE                                                   | 017870 |
|      | CONTINUE                                                   | 017880 |
|      | CONTINUE                                                   | 017890 |
|      | RETURN                                                     | 017900 |
|      | END                                                        | 017910 |
| C    |                                                            | 017930 |
| C    |                                                            | 017940 |
| C 22 | AL2                                                        | 017950 |
| C    |                                                            | 017960 |
| C    |                                                            | 017970 |
|      | SUBROUTINE AL2(N1,N2,NSTR)                                 | 017980 |
|      | DIMENSION NSTR(8)                                          | 017990 |
|      | COMMON Y(300),X(300),YM(300),Z(801),ZW(801),T(19),DUM(801) | 018000 |
|      | WRITE(6,201)                                               | 018010 |
| 201  | FORMAT(1X,13HENTER PROGRAM)                                | 018020 |
|      | NUM=1                                                      | 018030 |
|      | DO 110 NN=N1,N2                                            | 018040 |
|      | CALL ISNN(NN,1,DUMMY)                                      | 018050 |
|      | DO 100 M=1, 149                                            | 018060 |
|      | I=300*NN+NSTR(NN)-301                                      | 018070 |
|      | ISNMAX=0                                                   | 018080 |
|      | DO 20 K=1,300                                              | 018090 |
|      | II=I+K                                                     | 018100 |
|      | CALL ISNN(II,-1 ISN)                                       | 018110 |
|      | IF(ISNMAX,LT,ISN)ISNMAX=ISN                                | 018120 |
| 20   | Y(K)=ISN                                                   | 018130 |
|      | IF(ISNMAX,LE,0)GO TO 105                                   | 018140 |
|      | CALL SMOOTH( 300,11)                                       | 018150 |
|      | NID=1000*NN+N                                              | 018160 |
|      | CALL DWPL( NUM,NID,300)                                    | 018170 |
| 100  | CONTINUE                                                   | 018180 |
| 105  | CONTINUE                                                   | 018190 |
|      | PRINT ,0.1,NN,N,NUM                                        | 018200 |

|      |                                                            |        |
|------|------------------------------------------------------------|--------|
| 201  | FORMAT(1X,316)                                             | 018210 |
| 110  | CONTINUE                                                   | 018220 |
|      | CALL ENDPLT                                                | 018230 |
|      | RETURN                                                     | 018240 |
|      | END                                                        | 018250 |
| C    |                                                            | 018270 |
| C    |                                                            | 018280 |
| C 23 | SMOOTH                                                     | 018290 |
| C    |                                                            | 018300 |
| C    |                                                            | 018310 |
|      | SUBROUTINE SMOOTH( NDIM,NSM)                               | 018320 |
|      | COMMON Y(300),X(300),YW(300),Z(801),ZW(801),T(19),S(801)   | 018330 |
|      | IF(NSM.LE.1) GO TO 100                                     | 018340 |
|      | N=NSM/2                                                    | 018350 |
|      | FNSM=N*2+1                                                 | 018360 |
|      | DO 10 K=1,N                                                | 018370 |
|      | K2=N+K+1                                                   | 018380 |
|      | K3=NDIM+K-N                                                | 018390 |
|      | S(K+1)=Y(K3)                                               | 018400 |
| 10   | S(K2)=Y(K)                                                 | 018410 |
|      | DO 40 I=1,NDIM                                             | 018420 |
|      | DO 20 K=1,N                                                | 018430 |
| 20   | S(K)=S(K+1)                                                | 018440 |
|      | S(N+1)=Y(I)                                                | 018450 |
|      | Y(I)=0.                                                    | 018460 |
|      | DO 30 K=1,N                                                | 018470 |
|      | IF(I+K.GE.NDIM+1) GO TO 40                                 | 018480 |
| 30   | Y(I)=Y(I)+Y(I+K)                                           | 018490 |
| 40   | N1=N+1-NDIM+1                                              | 018500 |
|      | N1=MAX0(N1,1)                                              | 018510 |
|      | N1=N+1                                                     | 018520 |
|      | DO 50 K=1,N1                                               | 018530 |
| 50   | Y(I)=Y(I)+S(K)                                             | 018540 |
| 60   | Y(I)=Y(I)/FNSM                                             | 018550 |
| 100  | RETURN                                                     | 018560 |
|      | END                                                        | 018570 |
| C    |                                                            | 018590 |
| C    |                                                            | 018600 |
| C 24 | QWFL                                                       | 018610 |
| C    |                                                            | 018620 |
| C    |                                                            | 018630 |
|      | SUBROUTINE QWFL( NO,IO, ZE)                                | 018640 |
| C    | Y ARRAY IN                                                 | 018650 |
| C    | NO OF PLOTS OUTPUTTED EXCEPT MAKE NO=1 AT FIRST ENTRY      | 018660 |
| C    | ID OF PLOT IN                                              | 018670 |
| C    | IZE OF Y ARRAY                                             | 018680 |
|      | DIMENSION PROGID(3)                                        | 018690 |
|      | COMMON Y(300),X(300),YW(300),Z(801),ZW(801),T(19),DUM(801) | 018700 |
|      | PROGID(1)=10HKITROSSER                                     | 018710 |
|      | PROGID(2)=DATE(DDUM)                                       | 018720 |
|      | PROGID(3)=TIME(TDUM)                                       | 018730 |
|      | IF(NO.EQ.1)CALL CRTPLT(PROGID,1.,17.)                      | 018740 |
|      | IF(NO.EQ.1)CALL PLOT(3.65,0.,-3)                           | 018750 |
|      | IF(NO.EQ.1)GO TO 61                                        | 018760 |
|      | IF(NO-(NO/4)*4.EQ.1)CALL FRAME(4.15,.5)                    | 018770 |
|      | IF(NO-(NO/4)*4.EQ.1)GO TO 61                               | 018780 |
|      | CALL PLOT(4.25,0.,-3)                                      | 018790 |
| 61   | FID=ID                                                     | 018800 |
|      | CALL PLOT(-4.,.4,3)                                        | 018810 |
|      | CALL PLOT(0.,.4,2)                                         | 018820 |
|      | CALL PLOT(0.,10.4,2)                                       | 018830 |
|      | YMAX=0.                                                    | 018840 |
|      | DO 1 I=1,IZE                                               | 018850 |
|      | IF(Y(I).GT.YMAX)YMAX=Y(I)                                  | 018860 |
| 1    | CONTINUE                                                   | 018870 |
|      | IF(YMAX.IF.0.)GO TO 3                                      | 018880 |
|      | CALL NUMBER(-2.,-.4,.2,FID,0.,-1)                          | 018890 |
|      | CALL SYMBOL(-3.,0.,.2,5,YMAX=.0.,5)                        | 018900 |
|      | CALL NUMBER(-2.,0.,.2,YMAX,0.,-1)                          | 018910 |
|      | IF.3                                                       | 018920 |
|      | DO 2 I=1,IZE                                               | 018930 |
|      | YY=.4*Y(I)/YMAX                                            | 018940 |
|      | IF(YY.GT.0.)YY=0.                                          | 018950 |
|      | FI=I-1                                                     | 018960 |
|      | FIZ=IZE-1                                                  | 018970 |
|      | XX=.4+10.*FI/FIZ                                           | 018980 |
|      | CALL PLOT(YY,XX,IT)                                        | 018990 |
|      | IT=2                                                       | 019000 |
| 2    | CONTINUE                                                   | 019010 |
|      | NO=NO+1                                                    | 019020 |
| 3    | CONTINUE                                                   | 019030 |
|      | RETURN                                                     | 019040 |
|      | END                                                        | 019050 |

```

E
C 26 SLIT PROGRAM
C
PROGRAM SLIT(INPUT,OUTPUT,TAPE2,TAPE6=OUTPUT,TAPE7)
DIMENSION X(100),Z(100),V(10),D(10),G(10),DA(3)
PRINT 909
909 FORMAT(/# #####REMEMBER TO COPY TAPE7 AFTER EXECUTIO#
+ #DN,#### #/)
REWIND 2
READ(2,902)AAN
N=AAN+.0001
902 FORMAT(F9.3)
DO 5 I=1,N
5 X(I)=I
READ(2,902)(Z(I),I=1,N)
WRITE(6,904)
904 FORMAT(/5X##5X#Z#/)
WRITE(6,903)(X(I),Z(I),I=1,N)
903 FORMAT(1X,13.0,1X,F5.0)
D V(1)=1 V(2)=0 V(3)=W V(4)=A
V(2)=.5*(Z(1)+Z(N))
V(4)=0.
DO 10 I=1,N
IF(Z(I).GT.V(4))JX=I
IF(Z(I).GT.V(4))V(4)=Z(I)
10 CONTINUE
V(4)=V(4)-V(2)
V(1)=X(JX)
ZW V(2)=.5*V(4)
DO 15 I=1,N
JX=I
IF(ZW.LT.Z(I))GO TO 16
15 CONTINUE
DO 17 I=JX+1,N
JX=I
IF(ZW.GT.Z(I))GO TO 18
17 CONTINUE
V(1)=X(JX)-X(JX1)
D(3)=V(3) & D(1)=V(1) & D(2)=D(4)=V(4)
KK=0
WRITE(6,905)
905 FORMAT(/5X##5X#T#(1X#C#11X##11X#A#/)
DATA DA/10HVALUE ,10H RANGE ,10H FIT CRITER/
WRITE(6,906)KK,N,(V(K),K=1,4),DA(1)
WRITE(6,906)KK,N,(D(K),K=1,4),DA(2)
WRITE(6,907)
DO 30 KK=1,40
DO 20 K=1,4
CALL FERTI(N,X,Z,K,V,D(K),G(K))
20 CONTINUE
REWIND 2
WRITE(7,908)AAN,(V(K),K=1,4),(X(I),Z(I),I=1,N)
WRITE(6,906)KK,N,(V(K),K=1,4),DA(1)
WRITE(6,906)KK,N,(D(K),K=1,4),DA(2)
WRITE(6,906)KK,N,(G(K),K=1,4),DA(3)
WRITE(6,907)
906 FORMAT(2(1X,I2),4G12.6,1X,A10)
907 FORMAT(1X)
30 CONTINUE
908 FORMAT(5F10.4)
STOP
END
SUBROUTINE FERTI(N,X,Z,K,V,DG,GM)
DIMENSION X(1),Z(1),V(1)
GO V(K) & DG=ABS(DG) & GM=0.
IF(K.EQ.2.OR.K.EQ.4)GM=L.F10R
DO 10 I=1,20
F10R=1.
G=GO DG1=10R/10.
V(K)=G
IF(K.EQ.2.OR.K.EQ.4)GO TO 5
GH FGN(N,X,Z,V)
IF(GH.GT.GM)G1=V(K)
IF(GH.GT.GM)GM=GH
GO TO 10
5 GH FSN(N,X,Z,V)
IF(GH.LT.GM)G1=V(K)
IF(GH.LT.GM)GM=GH
10 CONTINUE
V(K)=G1
DG=.4*DG1/ABS(G1-GO)
RETURN
END

```

```

019360
019370
019380
019390
019400
019410
019420
019430
019440
019450
019460
019470
019480
019490
019500
019510
019520
019530
019540
019550
019560
019570
019580
019590
019600
019610
019620
019630
019640
019650
019660
019670
019680
019690
019700
019710
019720
019730
019740
019750
019760
019770
019780
019790
019800
019810
019820
019830
019840
019850
019860
019870
019880
019890
019900
019910
019920
019930
019940
019950
019960
019970
019980
019990
020000
020010
020020
020030
020040
020050
020060
020070
020080
020090
020100
020110
020120
020130
020140
020150
020160
020170
020180
020190
020200

```

|     |                                                        |        |
|-----|--------------------------------------------------------|--------|
|     | FUNCTION FCN(N,X,Z,U)                                  | 020200 |
|     | DIMENSION X(1),Z(1),U(1)                               | 020210 |
|     | T=U(1) \$ C=U(2) \$ M=U(3) \$ A=U(4) \$ RN=N \$ ZA=0.  | 020220 |
|     | DO 10 I=1,N                                            | 020230 |
| 10  | ZA=ZA+Z(1)-C                                           | 020240 |
|     | ZA=ZA/RN                                               | 020250 |
|     | YA=0.                                                  | 020260 |
|     | DO 12 I=1,N                                            | 020270 |
|     | XI=X(1)-I                                              | 020280 |
|     | YA=YA/(N(XI,A,M))                                      | 020290 |
| 12  | CONTINUE                                               | 020300 |
|     | YA=YA/RN                                               | 020310 |
|     | YS=0.                                                  | 020320 |
|     | DO 14 I=1,N                                            | 020330 |
|     | XI=X(1)-I                                              | 020340 |
|     | YI=YN(XI,A,M)-YA                                       | 020350 |
|     | YS=YS+YI*YI                                            | 020360 |
| 14  | CONTINUE                                               | 020370 |
|     | YS=YS/RN                                               | 020380 |
|     | YNH=0. \$ ZS=0.                                        | 020390 |
|     | DO 20 I=1,N                                            | 020400 |
|     | XI=X(1)-I                                              | 020410 |
|     | YNH=YNH+(Z(I)-C-ZA)*(YN(XI,A,M)-YA)                    | 020420 |
|     | ZS=ZS+(Z(I)-C-ZA)**2                                   | 020430 |
| 20  | CONTINUE                                               | 020440 |
|     | YNH=YNH/RN \$ ZS=ZS/RN                                 | 020450 |
|     | FD=ZS*YS                                               | 020460 |
|     | FCN=YNH/SQRT(FD)                                       | 020470 |
| 40  | RETURN                                                 | 020480 |
|     | END                                                    | 020490 |
|     | FUNCTION FSD(N,X,Z,U)                                  | 020500 |
|     | DIMENSION X(1),Z(1),U(1)                               | 020510 |
|     | T=U(1) \$ C=U(2) \$ M=U(3) \$ A=U(4) \$ RN=N \$ FSD=0. | 020520 |
|     | DO 10 I=1,N                                            | 020530 |
|     | XI=X(1)-I                                              | 020540 |
|     | FI=Z(1)-C-YN(XI,A,M)                                   | 020550 |
| 10  | FSD=FSD+FI*FI                                          | 020560 |
|     | FSD=FSD/RN                                             | 020570 |
|     | RETURN                                                 | 020580 |
|     | END                                                    | 020590 |
|     | FUNCTION YN(X,A,M)                                     | 020600 |
|     | IF(X,1,T,-M)GO TO 10                                   | 020610 |
|     | IF(X,GT,M)GO TO 10                                     | 020620 |
|     | AX=X                                                   | 020630 |
|     | IF(X,GT,0.1AX=-)                                       | 020640 |
|     | YN=AX*(AX/M)/M                                         | 020650 |
|     | GO TO 20                                               | 020660 |
| 10  | YN=0.                                                  | 020670 |
| 20  | RETURN                                                 | 020680 |
|     | END                                                    | 020690 |
|     |                                                        | 020710 |
|     |                                                        | 020720 |
|     |                                                        | 020730 |
|     |                                                        | 020740 |
|     |                                                        | 020750 |
|     | PROGRAM SLTIC(INPUT,OUTPUT,TAPE2,TAPE6,TAPE7=OUTPUT)   | 020760 |
|     | DIMENSION X(200),Z(200),TITLE(70)                      | 020770 |
|     | REWIND 6                                               | 020780 |
|     | REWIND 2                                               | 020790 |
|     | XMAX=0.                                                | 020800 |
|     | ZMAX=0.                                                | 020810 |
|     | ZMIN=-1.E+10                                           | 020820 |
|     | DO 15 J=1,10                                           | 020830 |
|     | READ(2,901)AAN,T,C,M,A                                 | 020840 |
|     | IF(CDE(2))20,10                                        | 020850 |
| 901 | FORMAT(5F10.4)                                         | 020860 |
| 10  | N=AAN*.00001                                           | 020870 |
|     | DATA L3/0.                                             | 020880 |
|     | L1=L3/1                                                | 020890 |
|     | L2=L1/N 1                                              | 020900 |
|     | L3=L2                                                  | 020910 |
|     | READ(2,901)(X(I),Z(I),I=L1,L2)                         | 020920 |
|     | DO 12 I=L1,L2                                          | 020930 |
|     | X(I)=ABS(X(I)-T)                                       | 020940 |
|     | Z(I)=(Z(I)-C)/(A*M)                                    | 020950 |
|     | IF(X(I),GT,XMAX)XMAX=X(I)                              | 020960 |
|     | IF(Z(I),GT,ZMAX)ZMAX=Z(I)                              | 020970 |
|     | IF(Z(I),LT,ZMIN)ZMIN=Z(I)                              | 020980 |
|     | WRITE(7,902)X(I),Z(I)                                  | 020990 |
| 12  | CONTINUE                                               | 021000 |
| 20  | FORMAT(2F10.5)                                         | 021010 |
| 15  | CONTINUE                                               | 021020 |
| 10  | CONTINUE                                               | 021030 |
|     | AM=ALOG10(2*XMAX)                                      | 021040 |

|    |                                                   |        |
|----|---------------------------------------------------|--------|
|    | M=AM                                              | 021050 |
|    | IF (AM.LT.0.)M=-INT(1.-AM)                        | 021060 |
|    | IM=.2*MAX/10.*M-.000000001                        | 021070 |
|    | HGRD=2.                                           | 021080 |
|    | IF (IH.GT.2.)HGRD=4.                              | 021090 |
|    | IF (IH.GT.4.)HGRD=10.                             | 021100 |
|    | HGRD=HGRD*10.*M                                   | 021110 |
|    | HCTR=HGRD*2.                                      | 021120 |
|    | AM=ALOG10(.2.*MAX/9.)                             | 021130 |
|    | M=AM                                              | 021140 |
|    | IF (AM.LT.0.)M=-INT(1.-AM)                        | 021150 |
|    | IM=(.2.*MAX/9.)/10.*M-.00000001                   | 021160 |
|    | VGRD=2.                                           | 021170 |
|    | IF (IV.GT.2.)VGRD=4.                              | 021180 |
|    | IF (IV.GT.4.)VGRD=10.                             | 021190 |
|    | VGRD=VGRD*10.*M                                   | 021200 |
|    | VCTR=VGRD*2.                                      | 021210 |
|    | DO 30 J=1,70                                      | 021220 |
| 30 | TITLE(J)=0.                                       | 021230 |
|    | TITLE(1)=AMWAVELEN   \$   TITLE(2)=6H STEPS       | 021240 |
|    | TITLE(3)=6HAMPLIT   \$   TITLE(4)=6HIDF           | 021250 |
|    | TITLE(5)=-1.                                      | 021260 |
|    | TITLE(6)=999.   \$   TITLE(65)=29.                | 021270 |
|    | TITLE(7)=3HXXX                                    | 021280 |
|    | DO 40 J=1,3                                       | 021290 |
|    | IF (J.EQ.1)KOM=0                                  | 021300 |
|    | IF (J.EQ.2)KOM=3                                  | 021310 |
|    | IF (J.EQ.3)KOM=4                                  | 021320 |
|    | CALL MAPA(X,Z,L,L3,KOM,HCTR,HGRD,VCTR,VGRD,TITLE) | 021330 |
| 40 | CONTINUE                                          | 021340 |
|    | CONTINUE                                          | 021350 |
|    | CONTINUE                                          | 021360 |
|    | CONTINUE                                          | 021370 |
|    | CONTINUE                                          | 021380 |
|    | STOP                                              | 021390 |
|    | END                                               | 021400 |

|                                     |        |
|-------------------------------------|--------|
| C                                   | 030420 |
| C                                   | 030430 |
| C 36 LIGHTBOX AVERAGE PROGRAM       | 030440 |
| C                                   | 030450 |
| C                                   | 030460 |
| PROGRAM AVERAGE OUTPUT INPUT        | 030470 |
| REWRITE                             | 030480 |
| PRINT 104                           | 030490 |
| READ 102,11                         | 030500 |
| IF 11                               | 030510 |
| CALL USNN(1,11,(BUNNY)              | 030520 |
| DO 30 I=1,100                       | 030530 |
| PRINT 101                           | 030540 |
| READ 102,15                         | 030550 |
| PRINT 103                           | 030560 |
| READ 102,11                         | 030570 |
| US 15, 11, 11                       | 030580 |
| ISUM 0                              | 030590 |
| DO 20 N=15,11                       | 030600 |
| CALL USNN(N,-1,10)                  | 030610 |
| ISUM ISUM+10                        | 030620 |
| CONTINUE                            | 030630 |
| ISUM ISUM                           | 030640 |
| ISUM ISUM/104*(11-15)               | 030650 |
| PRINT 105,ISUM                      | 030660 |
| CONTINUE                            | 030670 |
| 101 FORMAT(1X, #NO. OF FIRST MD. #) | 030680 |
| 102 FORMAT(12,3)                    | 030690 |
| 103 FORMAT(1X, #NO. OF LAST MD. #)  | 030700 |
| 104 FORMAT(1X, #FILE NO. #)         | 030710 |
| 105 FORMAT(1X, #AVERAGE = #,10,2)   | 030720 |
| STOP                                | 030730 |
| END                                 | 030740 |
| C                                   | 030750 |
| C                                   | 030760 |
| C 17 ISUM                           | 030770 |
| C                                   | 030780 |
| C                                   | 030790 |
| SUBROUTINE USNN(N,K,ISN)            | 030800 |
| DIMENSION I1(30)                    | 030810 |
| I1(1)=20,20,10                      | 030820 |
| 10 READ(2,209)I1(1),I1(2),I1(3)     | 030830 |
| I1(4)=I1(1)+I1(2)+I1(3)             | 030840 |
| N4=N4                               | 030850 |
| N1=N                                | 030860 |
| GO TO 100                           | 030870 |
| 20 IF (N1-N2) 21,31,22              | 030880 |
| 31 REWRITE                          | 030890 |
| N2=22                               | 030900 |
| IF (N1,10,100) 10,32                | 030910 |
| N2=1                                | 030920 |
| 32 N2=22                            | 030930 |
| N4=N2+1                             | 030940 |
| DO 30 N2=N3+N1                      | 030950 |
| 30 READ(2,209)(I1(NN),NN=1,30)      | 030960 |
| IF (I1(2)) 30,25                    | 030970 |
| CONTINUE                            | 030980 |
| GO TO 32                            | 030990 |
| 31 IF (N1,1,N2) 10,50               | 031000 |
| IF (N1,1,N2) 30,60,10,32            | 031010 |
| GO TO 31                            | 031020 |
| 32 N1=N1                            | 031030 |
| IF (N1,1,30)                        | 031040 |
| DO 40 N1=N1+30                      | 031050 |
| 31 N1                               | 031060 |
| 30 READ(2,209)(I1(NN),NN=1,30)      | 031070 |
| IF (I1(2)) 30,13                    | 031080 |
| 31 N1                               | 031090 |
| GO TO 31                            | 031100 |
| 50 DO 50,1,30                       | 031110 |
| 51 DO 50,1,30                       | 031120 |
| DO 50,1,30                          | 031130 |
| IF (N1,1,N2) GO TO 51               | 031140 |
| READ(2,209)(I1(NN),NN=1,30)         | 031150 |
| 31 N1=N1                            | 031160 |
| IF (I1(NN))                         | 031170 |
| 30 RETURN                           | 031180 |
| END                                 | 031190 |