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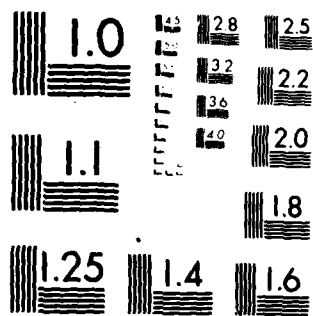
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FRAM I METEOROLOGY REPORT,

by

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Polar Science Center*
University of Washington

11 May 80

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1. INTRODUCTION

✓ The Fram experiment was conceived as a series of studies to study the geophysics and oceanographic characteristics of the eastern Arctic. The meteorological experiment was designed to provide basic data on wind velocities for the oceanographic experiments, to measure the drag coefficient of the pack ice in the area of the camp, and to collect standard weather data and transmit it to Thule for inclusion in the synoptic network and for planning flight support operations.

This report describes the experiment, the data analysis procedures and the data products which are available. The time series of half hour averages of wind speed, direction, and air temperature plus the air pressure every three hours are included as an appendix. Results of the drag coefficient calculations are also included.

2. THE EXPERIMENT

Measurements

During the experiment Ice Station Fram I was located northeast of Greenland, drifting southward from 84° 45' North Latitude and 10° 01' West Longitude on April 2, 1979 to 83° 27' North and 6° 42' West on May 9, 1979.

Wind speed and air temperature at two heights and wind direction at one height were recorded as continuously as possible during the experimental period. The variance of the wind speed signal in the frequency range 0.2 Hz to 1.0 Hz, from the upper height was also recorded. This was done using an analog circuit called a Near Inertial Subrange Stress Instrument (NISSI) as in Leavitt (1980). The wind speed signal is band pass filtered, squared and then integrated with a 90 second time constant. As described in Chapter 4 this signal is proportional to the surface air stress.

Atmospheric pressure was recorded every three hours and when possible a standard weather observation was transmitted to Thule twice daily.

Wind speed and direction were measured using anemometers and a wind vane respectively. Temperatures were measured using aspirated platinum resistance elements. These sensors were manufactured by Climet, Inc. and had been used during the AIDJEX experiment. The wind sensors were serviced and recalibrated by Climet before the experiment. The temperature sensor aspirator motors were also repaired.

The data was digitized and recorded on magnetic tape. Wind speed and direction data was sampled at 10 Hz and temperature data and wind variance data was sampled at 1 Hz.

Pressure was monitored by a Belfort microbarograph which was checked three times daily using a pair of Negretti and Zambra Precision Digital Barometers.

Chronology of Events

March

- 11 Fram I established, three men in a Parcoll tent.
- 14-17 Storm, SE winds to 40 knots.
- 19-24 Camp buildings erected, set up meteorology tower, checkout and troubleshoot system. Weather regime is periodic, multi-day storms with strong SE winds.
- 20 Pressure recording began.
- 28 Crack splits floe, dividing camp in two and opening a 200 meter lead, within 1 meter of 2 of the tower's 3 guylines.
- 29-April 1 Move meteorology program with radio shack and a few other buildings onto an adjacent floe, 1 kilometer south of the initial

April camp. Change of weather regime to light and variable winds, generally northerly.

2 Meteorological data recording begins.

3, 2300Z ADF beacon antenna and unit moved away from meteorology system to cure serious noise on temperature channels.

11, 2200Z Tower sensor booms reoriented to direct wind direction dead spot toward camp and consolidate wind directions contaminated by tower and camp.

29 Change of weather regime to steady winds over 10 knots from N or NW.

30 Small air-sampling hut moved from quite close to tower (27 meters) to a different side of "South Fram."

May

10 End of meteorological data recording.

15 Fram I evacuated.

Instrument Calibrations and Comparisons

The most useful calibration data for the temperature sensors was recorded during side-by-side comparisons at the same level. This compensated for the effect of differences in aspiration strength which cannot be seen in ice-bath sensor element calibrations. Table 1 summarizes the side-by-side comparisons which were performed approximately every four days. The anomalous result on day 114 appears due to a wind direction which directly opposed the aspirator intake direction. For the drag coefficient calculations the upper temperature sensor was taken to read 0.2°C higher than the lower one before day 114 and 0.1°C after day 114.

Similar comparisons were made with wind speed sensors at the beginning and end of the experiment. One unit, sensor/cups (3153/321), had been specially calibrated by CLIMET at different speeds and was used as the standard. The original sensor at the upper level failed at the end of day 96 and was replaced. Table 2 gives the height and comparison information for the anemometers.

Table 1: Side-by-side Temperature Comparisons

Both temperature sensors, normally at 7.8 meters and 1.1 meter, were set up side-by-side at the lower height. Each comparison period lasted several hours. Some editing proved necessary to remove obvious radio frequency noise. The following lists the average differences between the sensors for each comparison period.

<u>Julian Day</u>	<u>T(8M Sensor) - T(1M Sensor)</u>
97	0.18°C
100	0.23°C
103	0.25°C
107	0.25°C
114	-0.13°C
119	0.08°C
123	0.07°C
130	0.12°C
131	0.11°C

Table 2: Anemometer Height/Sensor Table

<u>Julian days</u>	<u>Height</u>	<u>Sensor/Cups</u>
92-96	9.2 meters	(3290/030)
97-130	9.2 meters	(3293/030)
92-130	2.0 meters	(3299/317)

Averaged comparison periods of several hours showed:

<u>Julian Day</u>	<u>Comparing</u>	<u>And</u>	<u>Speed Difference</u>
92	(3299/317) -	(3290/030)	= 0.05 m/sec
92	(3153/321) -	(3299/317)	= -0.16 m/sec
130	(3293/030) -	(3299/317)	= -0.07 m/sec
130	(3153/321) -	(3299/317)	= -0.03 m/sec

Sensor Location and Heights

Figure 1 shows the layout of "South Fram," the camp established one kilometer away from the original camp after the breakup on March 28. About a 60° arc of wind direction was not usable for drag coefficient calculations because of contamination by the camp buildings, the air sampling hut and the tower itself.

The wind speeds were measured at 9.2 m and 2.0 m, the wind direction height was 3.0 m and air temperatures were measured at 7.8 m and 1.1 m. These heights are relative to the height above the local snow surface.

3. DATA PRODUCTS

As mentioned above, wind speed and direction were sampled at 10 Hz and temperature and wind speed variance output were sampled at 0.125 Hz. The data was recorded on magnetic tape in forty second long records.

To reduce the amount of data that must be permanently stored on the tape, the wind speed and direction data was smoothed by averaging sequential sets of four samples. The averaged data is available for future spectral analysis or other studies.

All the data, including wind, temperature and NISSI, have been stored as record averages on a separate data tape. This product is available (on one magnetic tape) for users who may desire time information on shorter time scales than the half-hour period that is our principal data product.

Half-Hour Average Data

The 40-second record averages were accumulated in half-hour periods, centered on the whole hour and half-hour. Wind direction was corrected to true direction using tripod-mounted magnetic compass bearings of the direction sensor's zero direction, noted at least daily, and the local magnetic declination determined by sunshot at the main part of the camp.

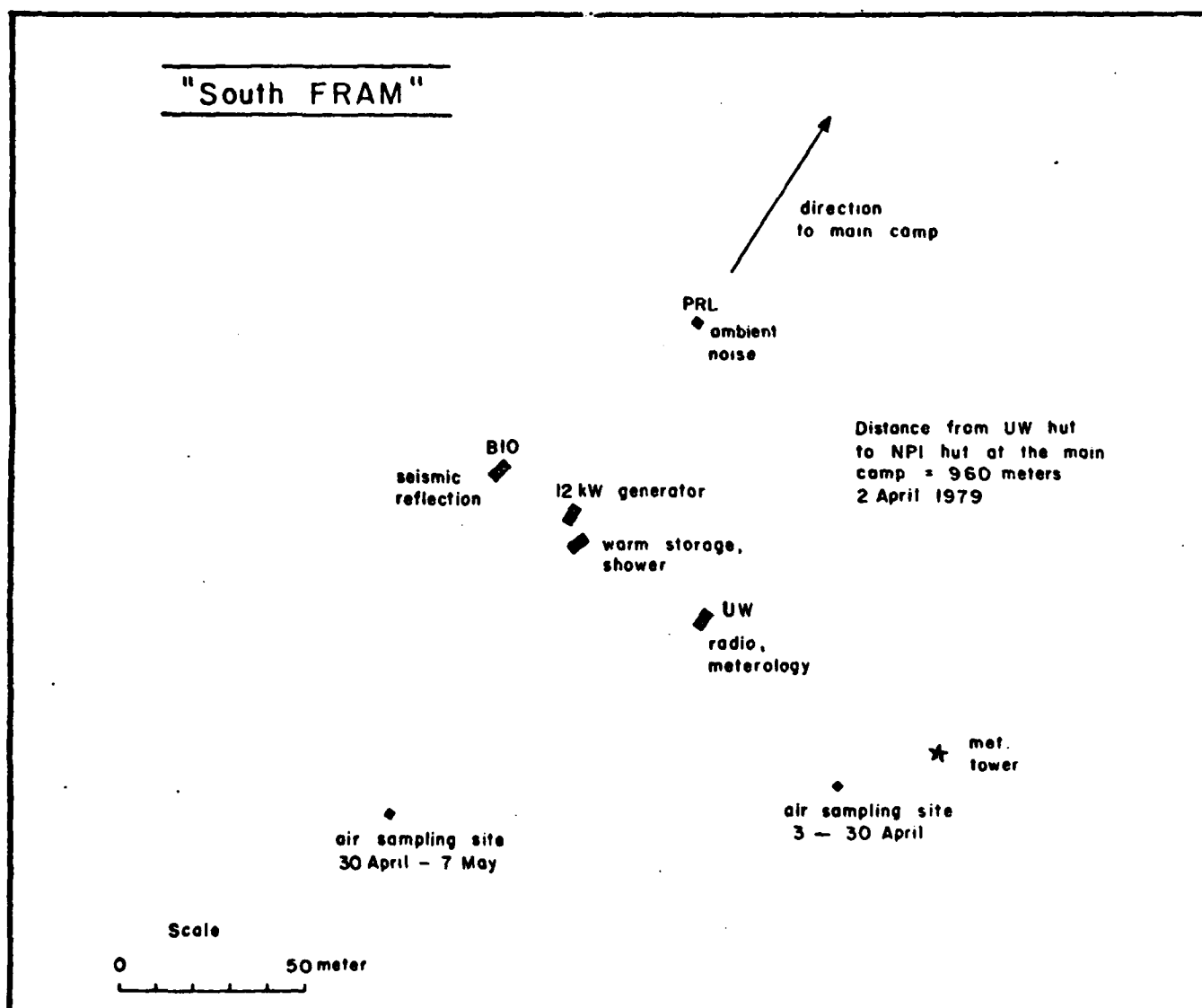


Figure 1 Camp layout map for South Fram. (From "Isdriftstasjonene Fram I Ekspedisjonsrapport", Yngve Kristoffersen, Norsk-Polarinstitutt, September 1979).

An effort was made during this averaging process to reduce the effect of noise, apparent in the temperature channels, whose principal source was the radio transmissions necessary for operation of the camp. A high value of the standard deviation of the temperature difference between the upper and lower sensors was taken to indicate serious noise. The records of noisy half-hours were sorted into 20 equal slots between the minimum and maximum vertical temperature differences. Temperatures from records outside of one slot on each side of the median were discarded, and new means calculated. If more than half the records were thus eliminated or if the new difference standard deviation was not less than the original standard, the improvement was not accepted and the original noisy mean was retained. This procedure resulted in a considerable improvement in the temperature values. The average data is plotted in Figures 2-9 and listed by time in the appendix.

Pressure Data

Pressure data was picked from the microbarograph charts every three hours and then calibrated by comparison with the N & Z standard barometers. The stability of the standards was demonstrated by comparisons with mercurial barometers at Thule and Nord before and after the experiment. These data were then reduced to sea level pressures and are included in the appendix..

4. DRAG COEFFICIENTS

Theory

The two techniques which were used to estimate the momentum flux from these data are the profile method and the inertial-dissipation method. The Monin-Obukhov similarity theory provides a framework for indirect estimates of the momentum flux. It proposes that over a horizontally homogeneous

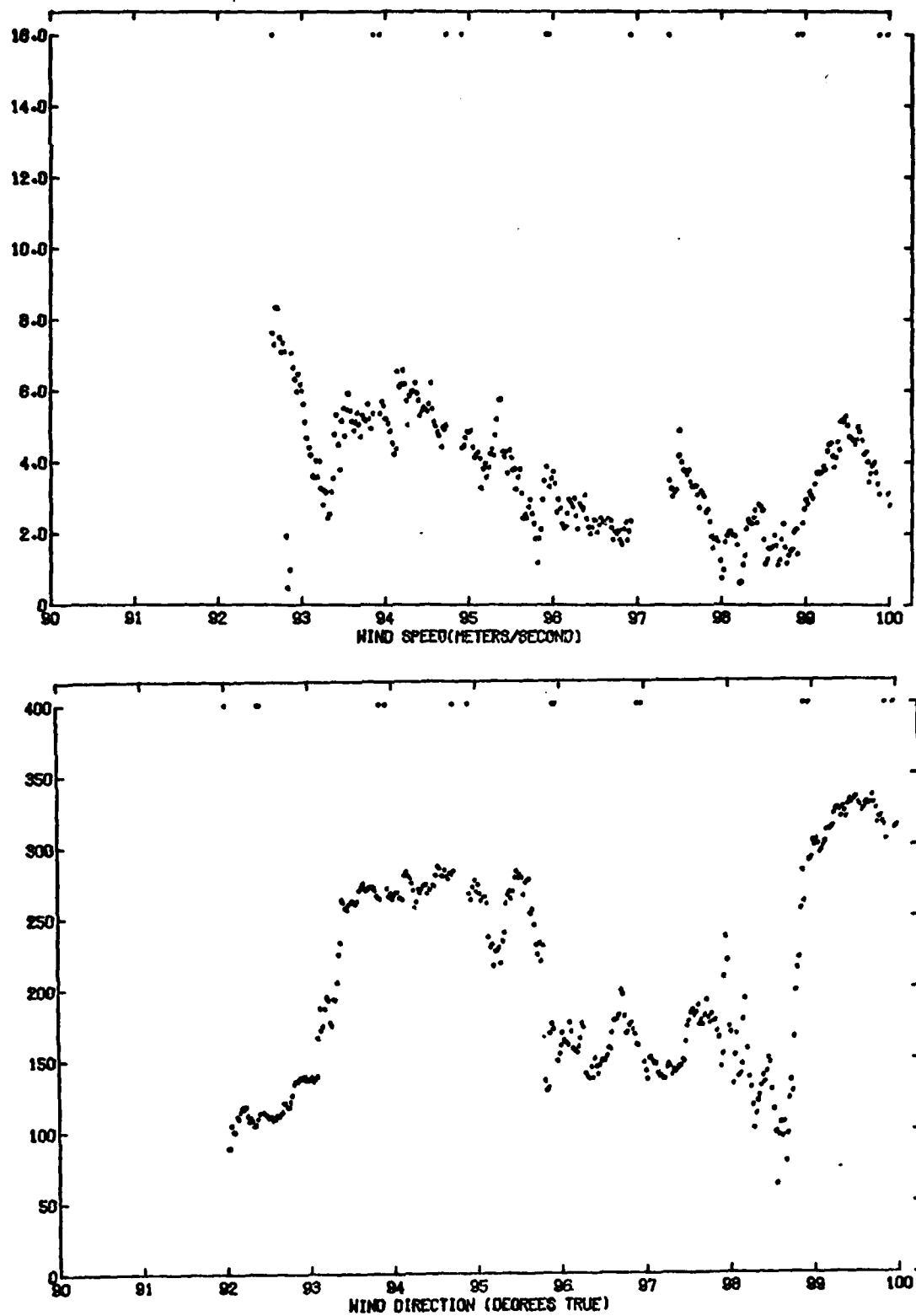


Figure 2 Half-hourly average wind speed and direction at Fram I, Julian days 90-100.

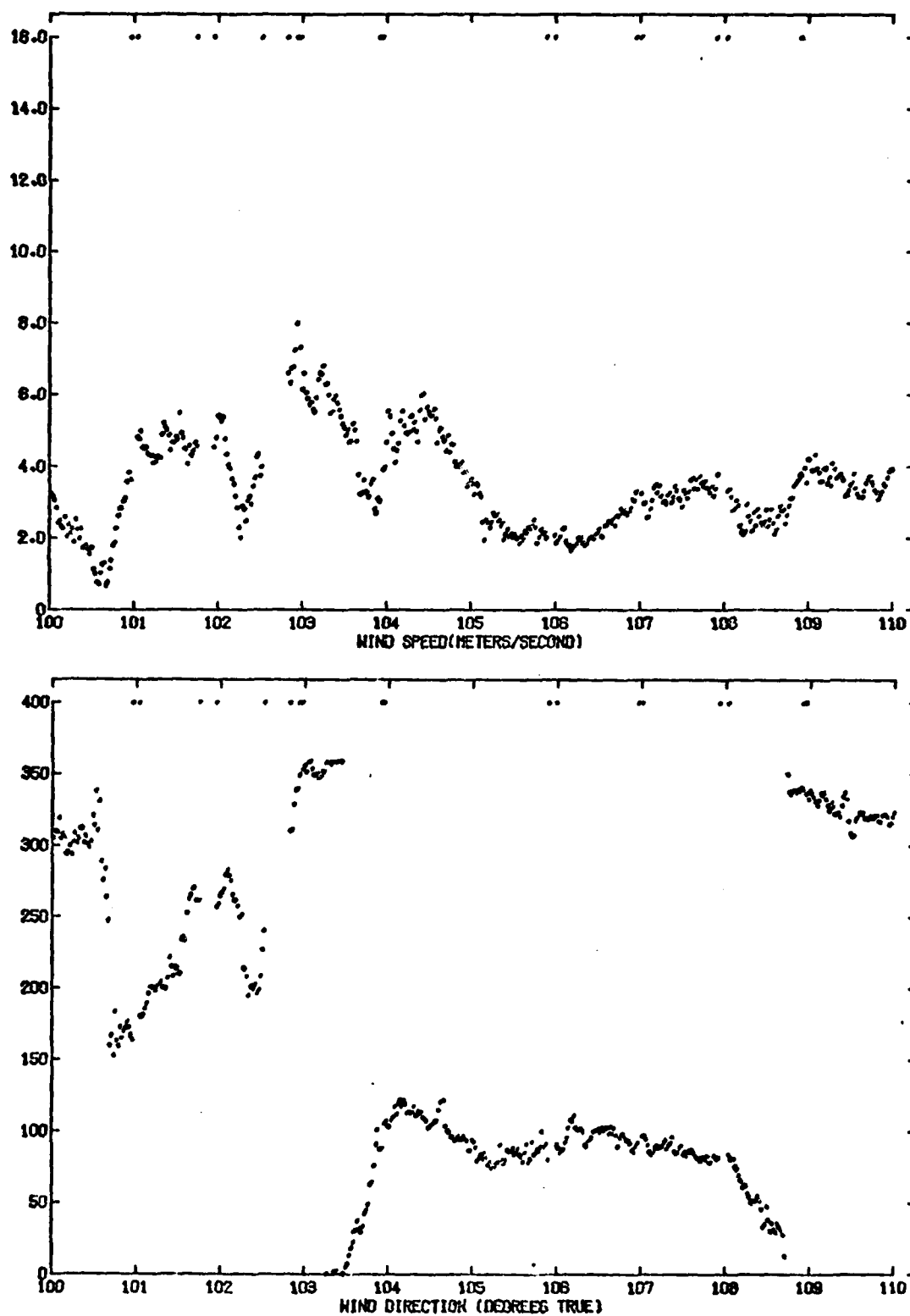


Figure 3 Half-hourly average wind speed and direction at Fram I, Julian days 100-110.

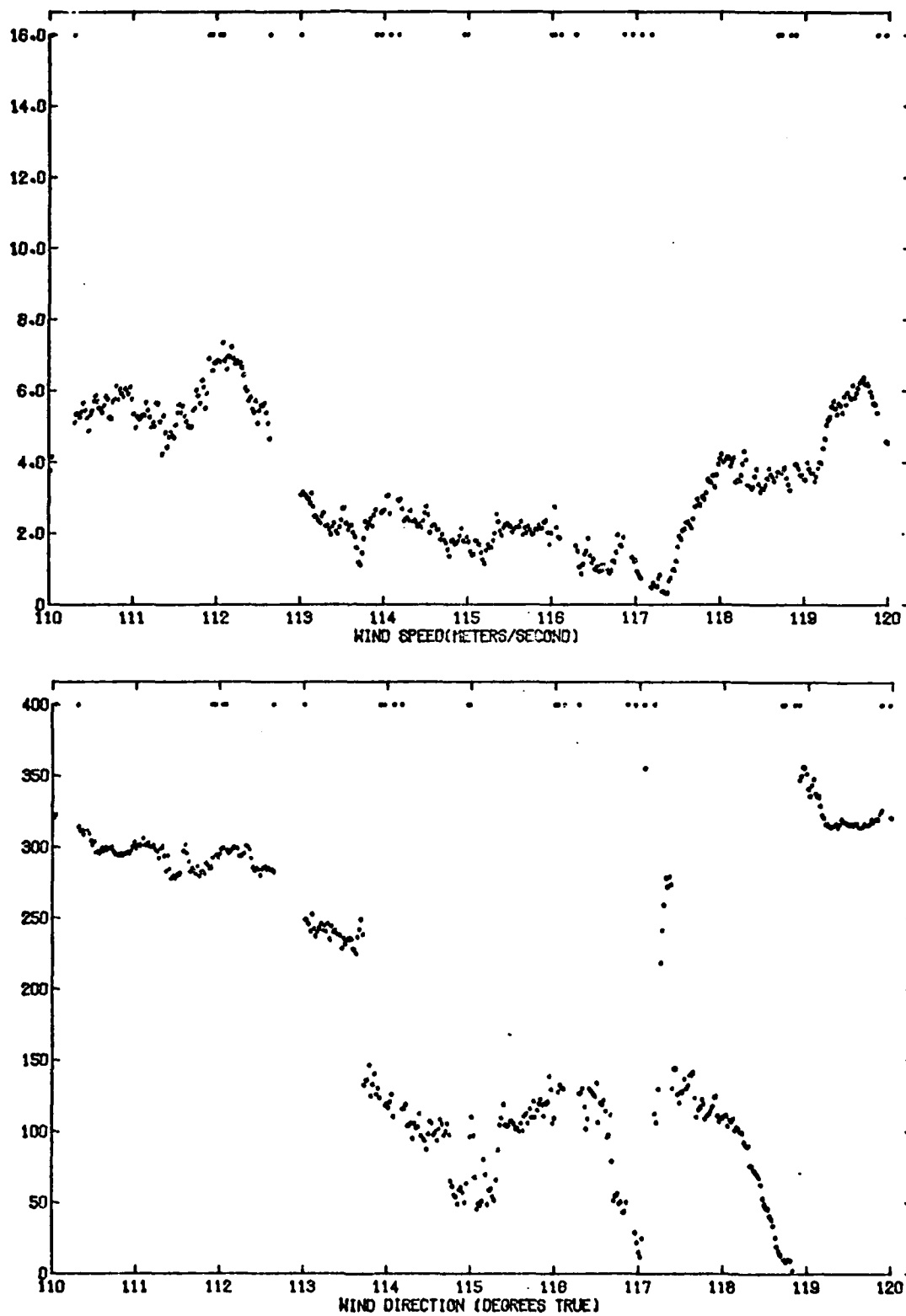


Figure 4 Half-hourly average wind speed and direction at Fram I, Julian days 110-120.

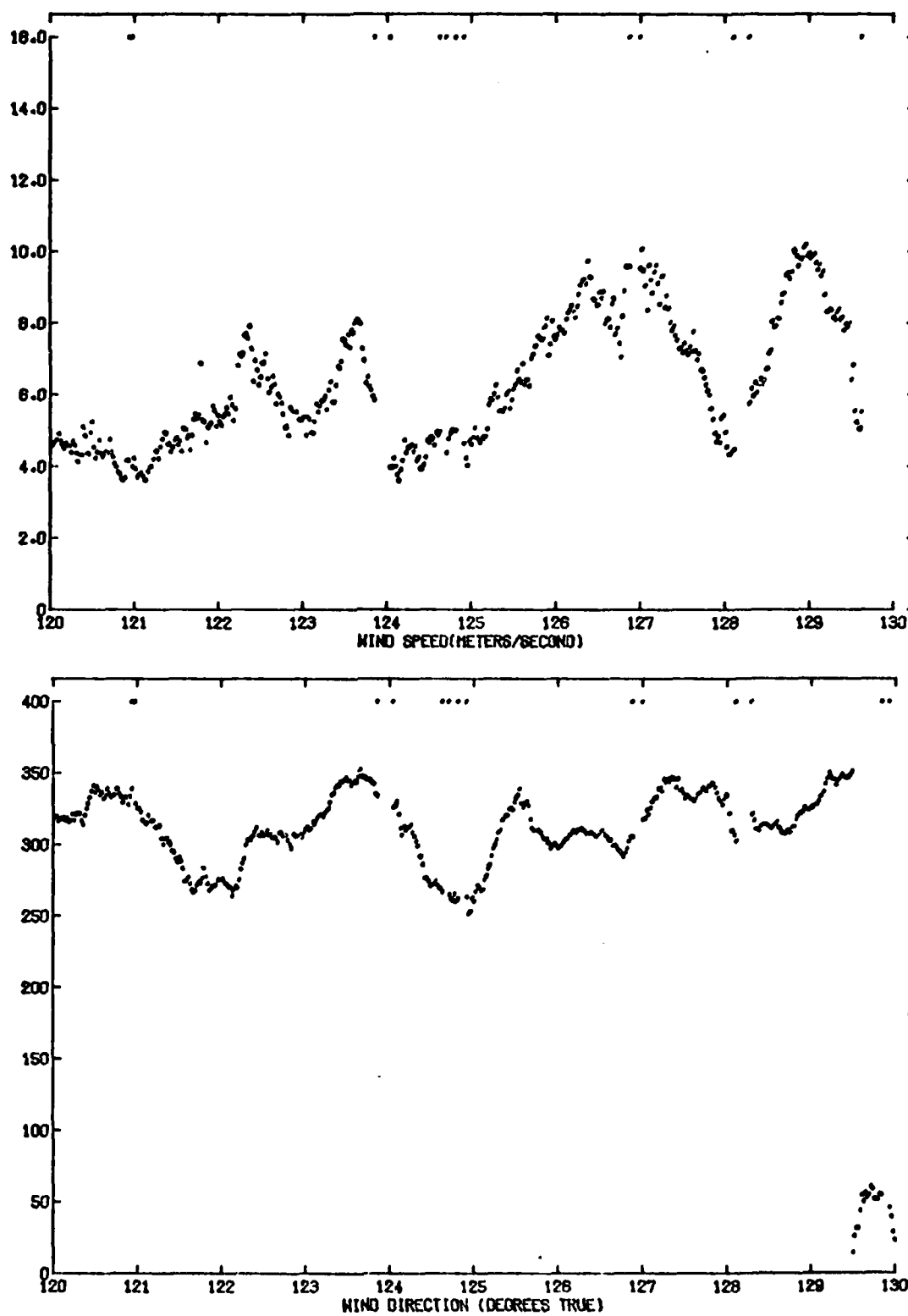


Figure 5 Half-hourly average wind speed and direction at Fram I, Julian days 120-130.

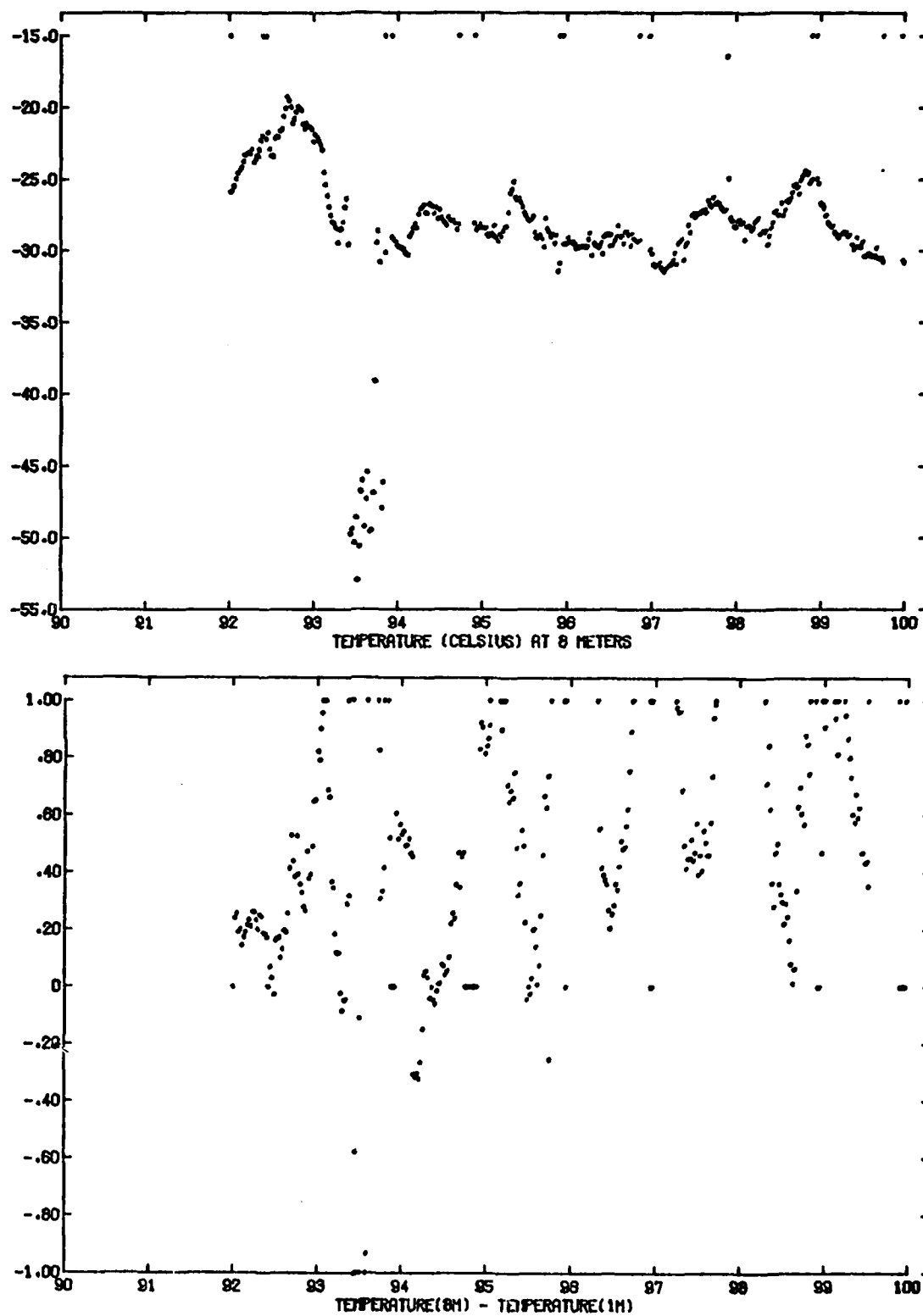


Figure 6 Half-hourly temperature and vertical temperature difference at Fram I, Julian days 90-100.

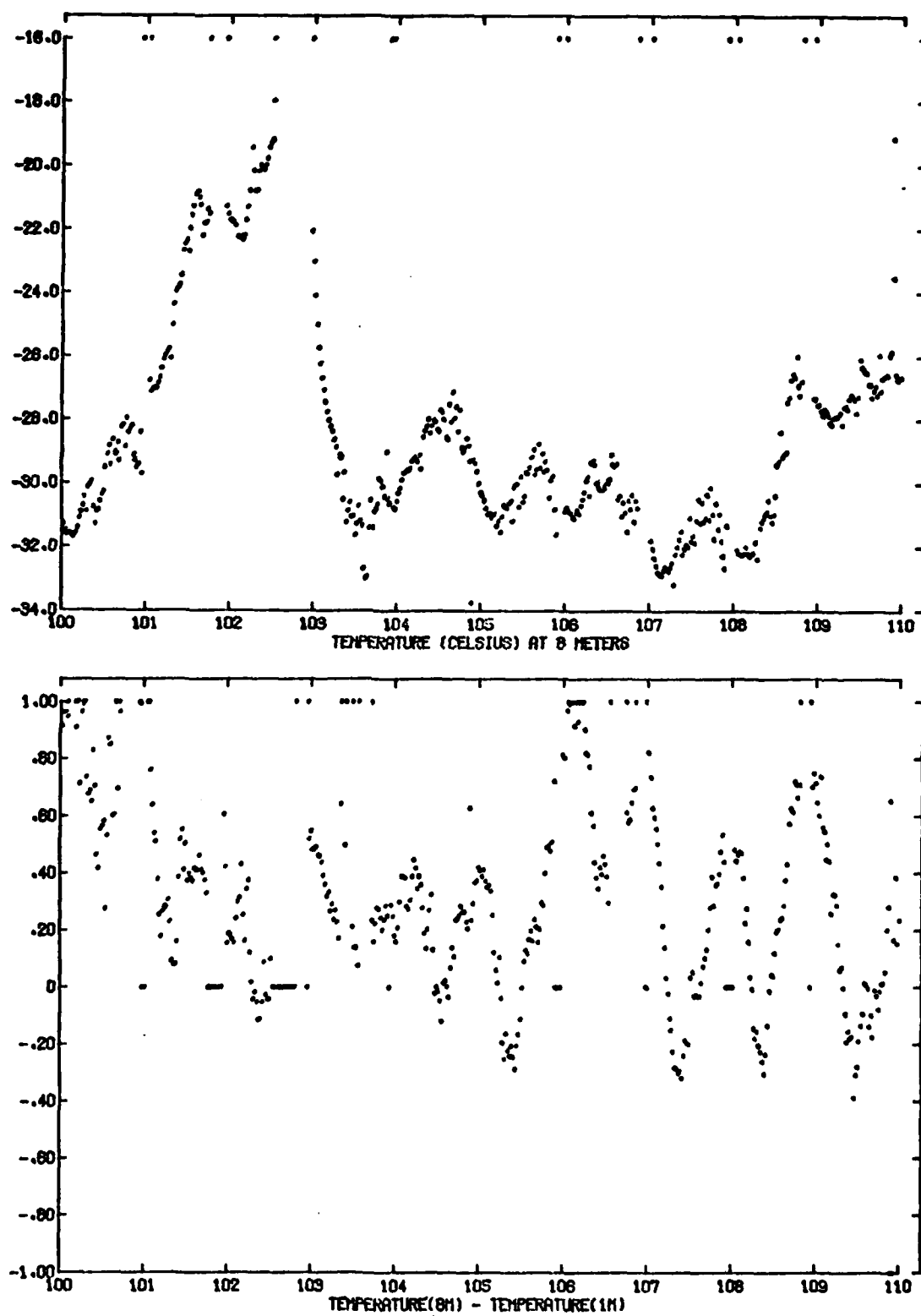


Figure 7 Half-hourly temperature and vertical temperature difference at Fram I, Julian days 100-110.

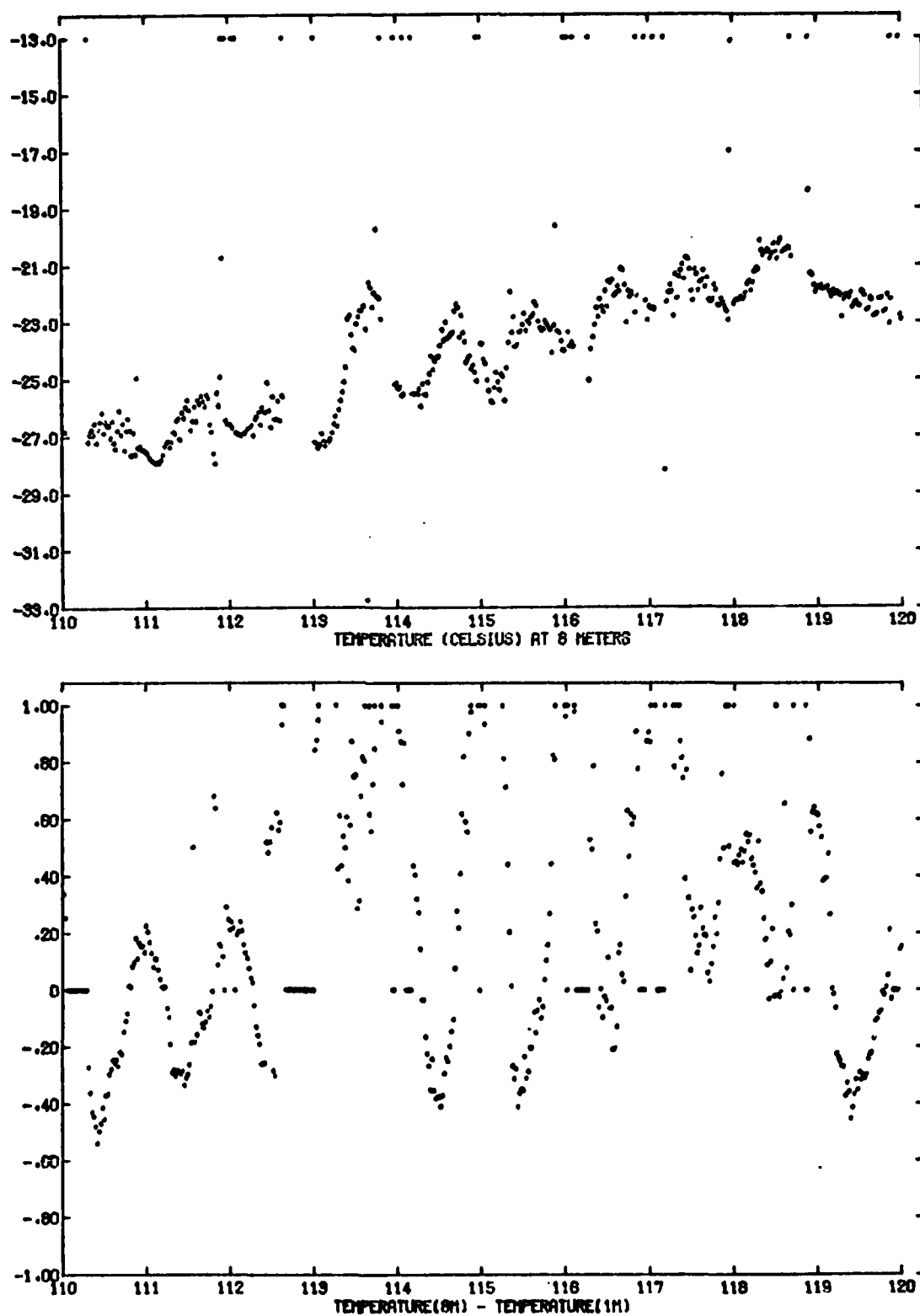


Figure 8 Half-hourly temperature and vertical temperature difference at Fram I, Julian days 110-120.

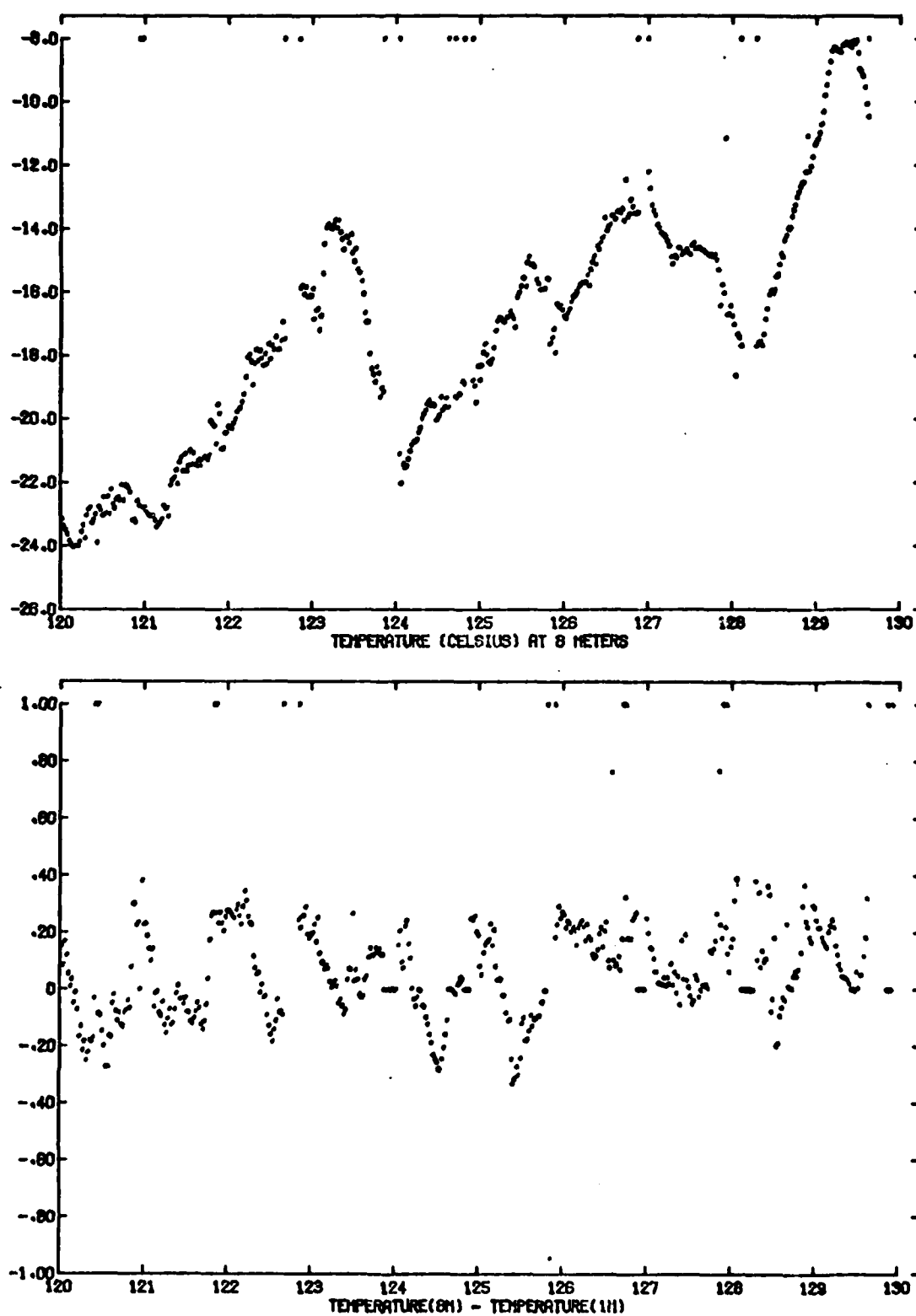


Figure 9 Half-hourly temperature and vertical temperature difference at Fram I, Julian days 120-130.

surface the turbulence structure is a function of the surface shear stress τ , the surface heat flux H_0 , the height from the surface z , and the buoyancy parameter g/T , where g is the acceleration due to gravity and T is the mean air temperature. From these variables we can form a velocity scale $u_* = \sqrt{\tau/\rho}$, a temperature scale $\theta_* = -H/\rho C_p u_*$, and a length scale z .

A given turbulence property should then depend only on these scales; for example, the mean vertical gradients of horizontal wind U , and potential temperature θ , can be written as

$$\left[\frac{kz}{u_*} \frac{\partial U}{\partial z} = \phi_m(z/L) \right], \quad \left[\frac{kz}{\theta_*} \frac{\partial \theta}{\partial z} = \phi_H(z/L) \right] \quad (1)$$

Here L is the Monin-Obukhov length ($z/L = -kz(g/T)(H/\rho C_p)u_*^{-3}$), k is von Karman's constant and ϕ_m and ϕ_H must be determined experimentally. Once these functions are known, the surface stress and the sensible heat flux can be calculated from the mean profiles as demonstrated in Leavitt, et al. (1977) using AIDJEX observations. For the profile analysis they chose

$$\phi_m = \phi_H = 1 + \gamma_1 z/L, \quad z/L > 0 \quad (2)$$

$$\phi_m = \phi_H^2 = (1 - \gamma_2 z/L)^{-0.25}, \quad z/L \leq 0 \quad (3)$$

Values of the constants which were used by Leavitt, et al. were $\gamma_1 = 4.5$, $\gamma_2 = 16.0$, and $k = 0.4$. Equations (2) and (3) can be integrated:

$$U = u_*/k (\log z/z_0 - \psi_1) \quad (4)$$

$$\theta - \theta_0 = \theta_*/k (\log z/z_0 - \psi_2) \quad (5)$$

where z_0 is the roughness length, θ_0 the temperature at height z_0 , and the forms of ψ_1 , ψ_2 , appropriate to (2) and (3) are given by Paulson (1970).

Equations (4) and (5) are solved using an iterative procedure. However because there are only two levels of observations of wind and temperature the computed fluxes will be extremely sensitive to errors in the data.

The inertial subrange hypothesis of Kolmogoroff suggests that there exists a region in wave number space where the velocity spectra are a function only of the rate of dissipation of the turbulent kinetic energy ϵ and the wave number κ_1 . Using Taylor's hypothesis, $\kappa_1 = 2\pi n/U$, this can be expressed as:

$$n S_u(n) = \alpha_1 \epsilon^{2/3} (2\pi n/U)^{-2/3} \quad (6)$$

where S_u is the spectral density, α_1 is a universal constant and n is frequency in Hertz. With some manipulation (6) can be rewritten as

$$n S_u(n) / u_*^2 \phi_\epsilon^{2/3} = C_{IN} f^{-2/3} \quad (7)$$

where $f = nz/U$ is a non-dimensional frequency, $C_{IN} = \alpha_1 / (2\pi k)^{2/3}$, and $\phi_\epsilon = \epsilon k z / u_*^3$ is the dimensionless dissipation rate. If a balance between production and dissipation of turbulent kinetic energy is assumed; $\phi_\epsilon = \phi_m - z/L$. Measurements suggest that this is a reasonable assumption for stable conditions but not for unstable conditions (Champagne, et al., 1977). For unstable conditions, we have assumed $\phi_\epsilon^{2/3} = 1.0 + .5|z/L|^{2/3}$ in agreement with Champagne, et al. The range of stratification is so limited that the effect of different assumptions about ϕ_ϵ is not very critical.

After applying corrections for the bandpass filter and anemometer response the output from the NISSI is equivalent to

$$\text{Output(NISSI)} = \int_{.2}^{1.0} S_u(n) dn \quad (8)$$

The frequency range of the NISSI (.2 to 1.0 Hz) only partially overlaps with the inertial subrange. An empirical spectral shape derived from Kaimal (1978)

is used in place of equation (7) for values of $f < .4$

$$\frac{nS_u(n)}{u_*^2 \phi_\epsilon^{2/3}} = C_s \cdot f^{-.4} \quad (9)$$

The value of C_s is chosen by matching equations (6) and (9) at $f = .4$.

From Kaimal (1978) $C_{IN} = 0.3$ and $C_s = 0.38$.

Substitution of equations (9) and (6) into (10) permits calculation of u_* and z/L . The temperature profile is used to calculate θ_* .

Errors

There are obviously several sources of errors in both methods. The values of the empirical constants have been taken from the literature and it should not be assumed that there is universal agreement about their values. Even the von Karman's constant is in dispute; estimates range from .35 to .43, although the value of 0.4 is probably the most universally accepted value. Similar statements could be made about the other constants.

Comparisons between the two methods during AIDJEX gave agreement between them of better than 20%. Limited comparison between the NISSI method and direct stress measurements also suggested that the estimates of mean drag coefficients are accurate to better than $\pm 20\%$.

The profile method will be very sensitive to errors in the mean wind speed measurement whether due to instrument problems or to interference to the flow from nearby camp structures. For example if the gradient in the wind speed is 10% of the mean wind speed a 5% error in one of the mean estimates causes a 50% error in the stress estimate. The spectral method, on the other hand, is insensitive to errors in mean wind speed measurement and is a superior method for sampling in relatively inhomogenous terrain.

Results

Estimates of the surface roughness (z_0) are presented in the form of 10 m drag coefficients

$$C_{10} = [k/\log(10/z_0)]^2$$

This value of C_{10} should be independent of z/L ; any dependence on z/L indicates errors in measurement or in specifying the empirical constants. An equivalent definition of C_{10} is

$$C_{10} = u_*^2 / U_n^2(10)$$

$$U(10)_n = U_m(10) + u_* \psi_1(10/L)/K$$

where $U_m(10)$ is the actual measured wind at 10 m and $U_n(10)$ is the equivalent neutral wind.

Values of C_{10} computed using the two methods on the half-hour averages are plotted versus relative wind direction in Figures 10 and 11. Relative wind direction is used rather than absolute wind direction because the ice on which the camp was located rotated during the experiment.

Computations were only done using data where the wind speed was greater than or equal to 5 m/sec. Data from wind directions between 330° and 30° is not plotted because the camp was upwind of the tower; unfortunately this excluded about 60% of the data with high enough wind speeds.

The range of values of C_{10} calculated from the NISSI data varies from about 1.3×10^{-3} to 2.5×10^{-3} . The profiles derived values of C_{10} vary from nearly 0.0 to about 2×10^{-3} .

Values of C_{10} calculated using the two methods are plotted versus z/L in Figures 12 and 13. The profile C_{10} shows a sharp variation with z/L . Whether this is due to errors in the wind profile or in the temperature

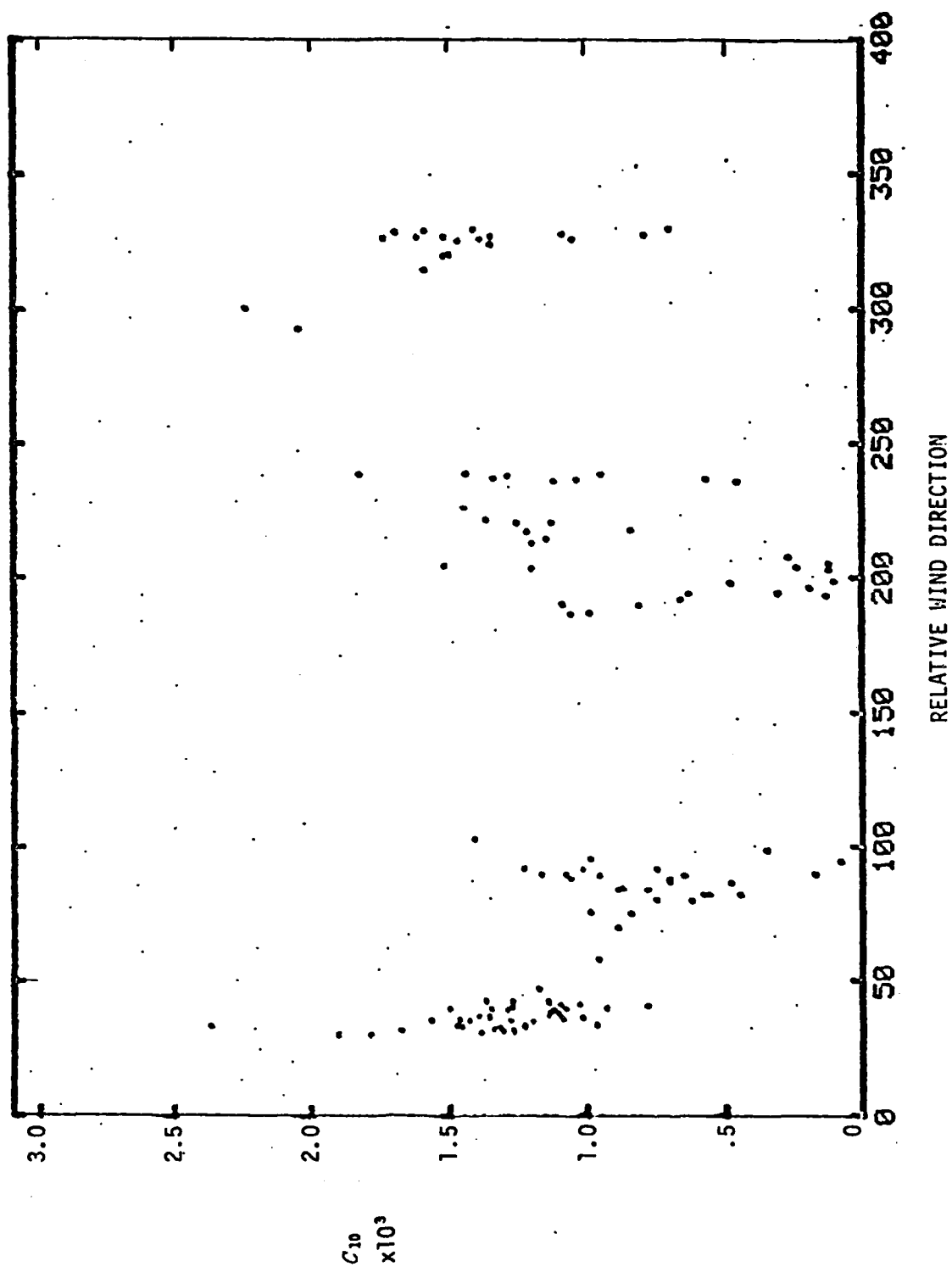


Figure 10. Drag coefficients compiled using the profile method plotted versus relative wind direction.

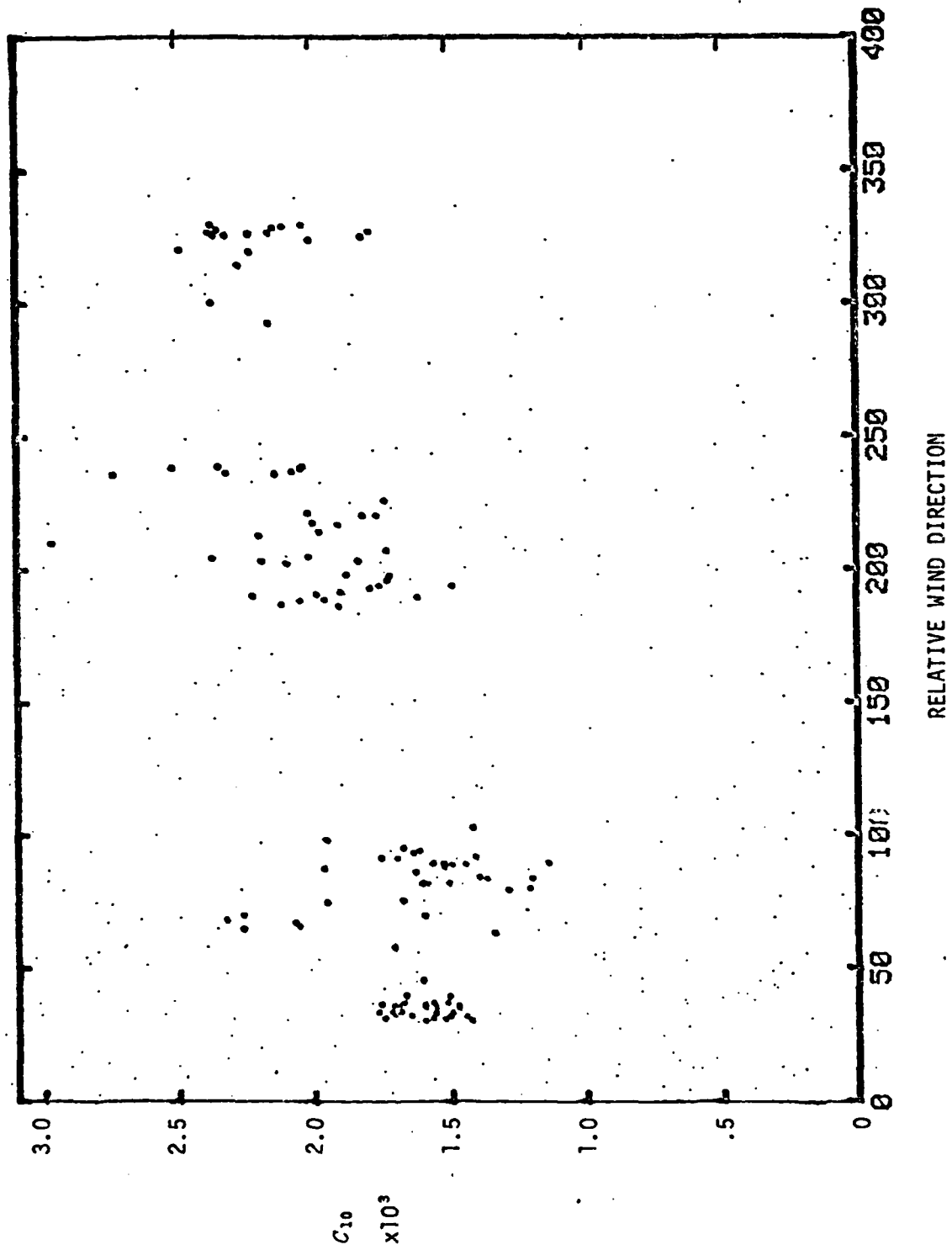


Figure 11. Drag coefficients compiled using the inertial subrange method (NISSI) plotted versus relative wind direction.

profile is impossible to verify from the profiles above. However the NISSI data does not show a similar variation, in fact the range of z/L values are only about 10% of the range of the former. This suggests that the problem may be in the mean wind speed gradient data.

The heat fluxes computed from both methods range between $\pm 30 \text{ W/m}^2$ and are extremely small. The uncertainty in the measurement is large because of the difficulty of measuring the small temperature gradient very accurately.

The mean value of C_{10} from the NISSI data is 1.7×10^{-3} with a standard deviation of about $.2 \times 10^{-3}$. There is a variation with direction, from a mean value of 1.5×10^{-3} for wind directions less than 100° to a value of 2×10^{-3} for wind direction greater than 100° . During AIDJEX the range of drag coefficients measured at the 10 m height using the NISSI system varied between 1.1×10^{-3} and 1.4×10^{-3} (Leavitt, 1980 and unpublished data).

5. CONCLUSIONS

The profile method did not produce valid drag coefficients, probably because of errors in the wind speed measurements. Some of this error may be due to interference of the flow by small surface relief features. In any case this is not surprising because of the sensitivity of the profile method to errors in estimating the mean wind speed gradient.

The mean value of the drag coefficient using the NISSI method is insensitive to small errors in measuring the wind speed. Unfortunately nearly 60% of the data had to be discarded because the fetch lay over the camp and the fuel dump. The remaining data indicates a trend with direction, however, this trend cannot be related to the local topography because only a general record of nearby surface features is available.

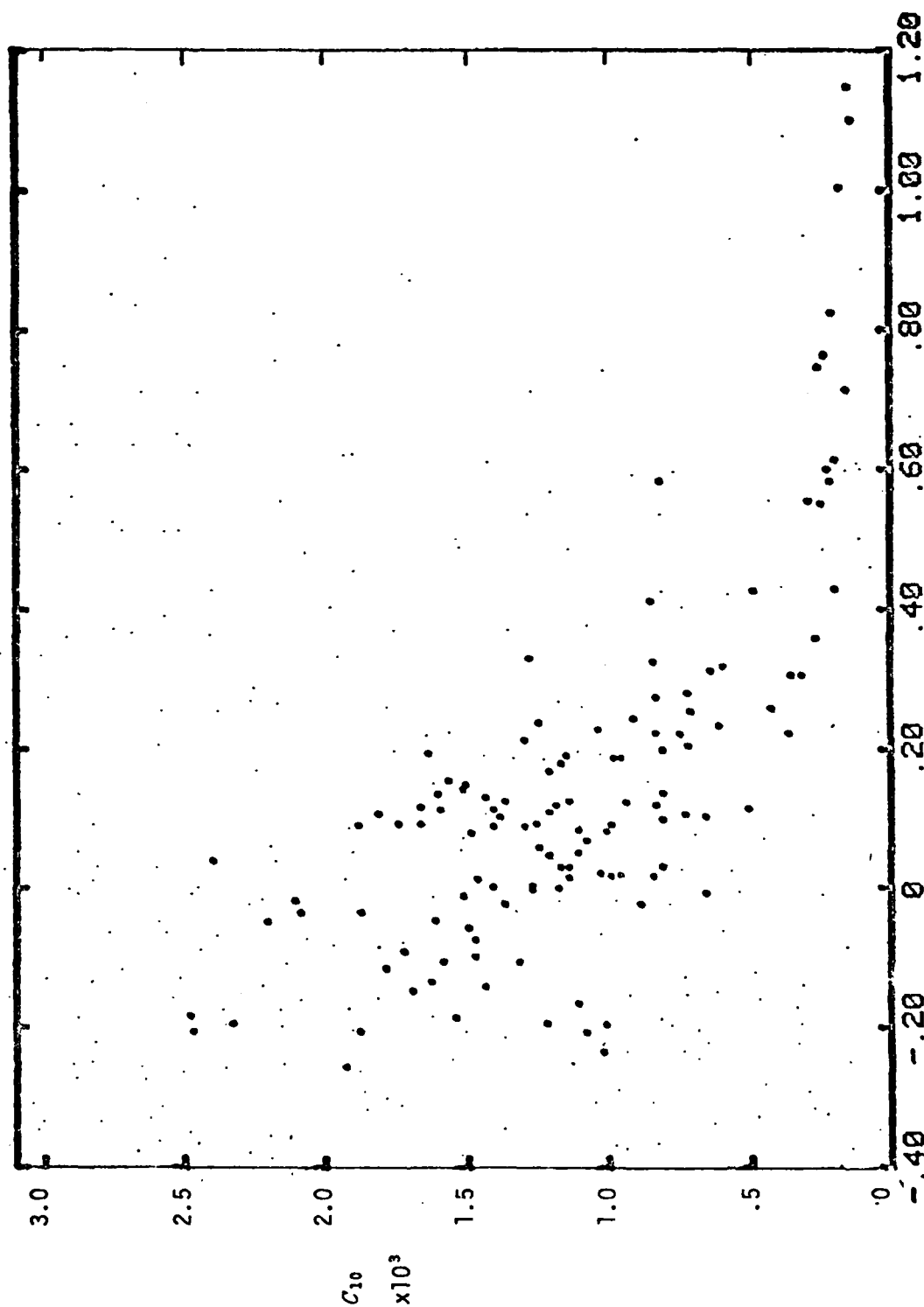


Figure 12. Profile drag coefficients plotted versus z/L .

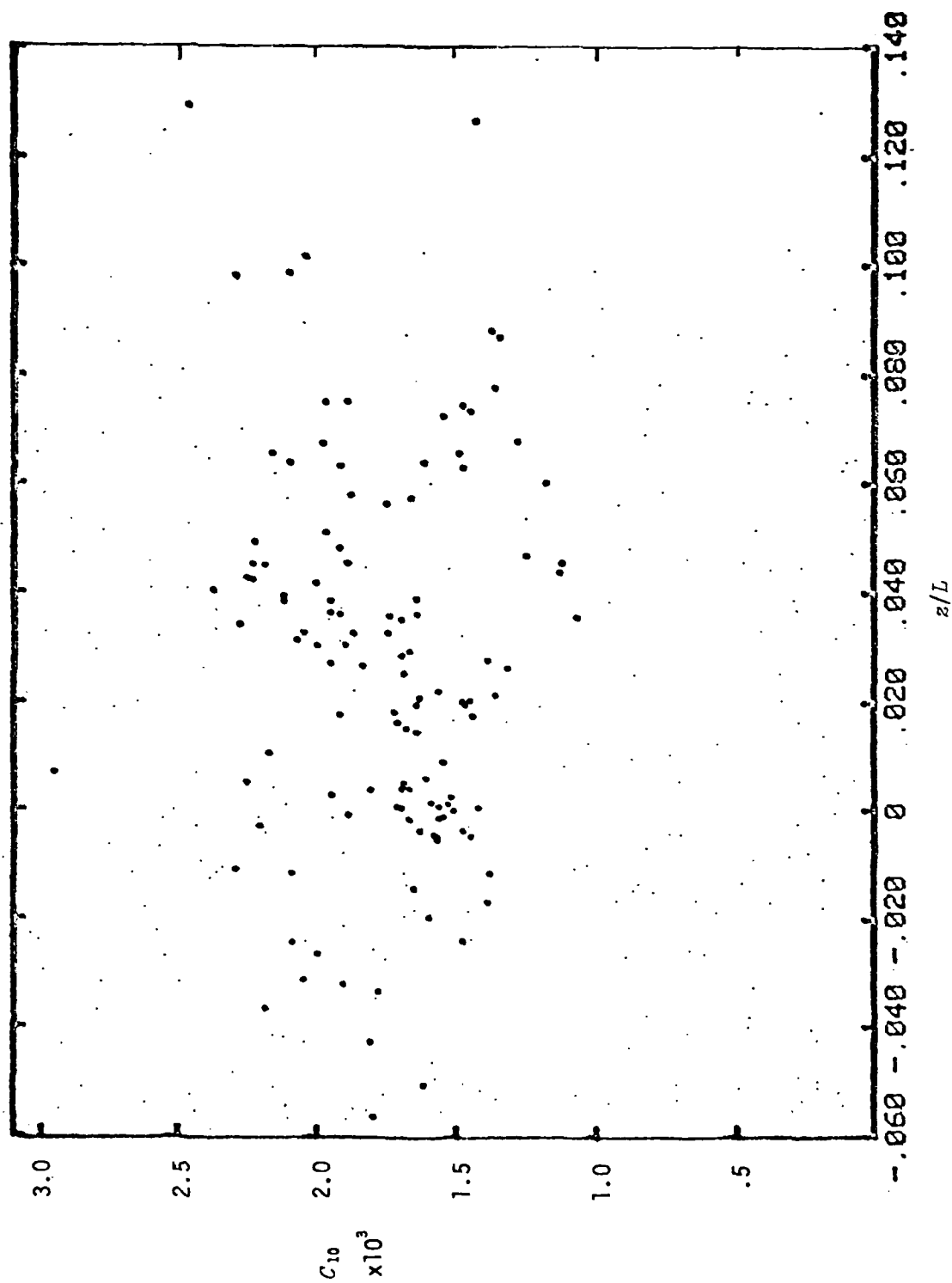


Figure 13. Drag coefficients computed using the NISSI data plotted versus z/L .

The mean value of the drag coefficient is about 30% greater than the values measured from the 10 m height at the AIDJEX camps. This agrees with the qualitative impression of observers present at both projects that the surface appeared distinctly rougher at the Fram site than it appeared at the AIDJEX sites.

Since "South Fram" was located on a floe as relatively smooth as any in the area, the true regional drag coefficient is probably considerably larger than the value of 1.7×10^{-3} . In conclusion the meteorological measurement program was successfully completed but the coefficient drag coefficient determination was only moderately successful.

6. ACKNOWLEDGMENTS

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APPENDIX: Time Series Printout

The following pages contain a listing of half-hourly averages of meteorological data recorded at Ice Station Fram 1. Each average period is centered on the half-hour. Units are meters per second for wind speed, degrees true for wind direction, and degrees Celsius for air temperature. Atmospheric pressure, in millibars, is not an average but a recorded observation every three hours. Missing or unrecorded data is indicated by a blank field.

APPENDIX: TIME SERIES PRINTOUT

MONTH	DAY	JULIAN DAY	HOUR	WIND SPEED @ 9.2 M (M/SEC)	WIND SPEED @ 2.0 M (M/SEC)	DIRECTION (DEG TRUE)	TEMPERATURE @ 7.8 M (DEG C)	TEMPERATURE @ 1.1 M (DEG C)	PRESSURE (MB)
APRIL	2	92	0						1032.3
		92	.5		1.8	88.	-25.9	-26.1	
		92	1.0		2.2	88.	-25.8	-26.0	
		92	1.5		2.7	105.	-25.5	-25.7	
		92	2.0		2.9	100.	-25.0	-25.2	
		92	2.5		2.8	100.	-24.6	-24.7	
		92	3.0		3.3	111.	-24.4	-24.5	1031.0
		92	3.5		3.5	109.	-24.2	-24.4	
		92	4.0		3.4	114.	-23.8	-24.0	
		92	4.5		3.4	117.	-23.3	-23.5	
		92	5.0		3.6	116.	-23.2	-23.5	
		92	5.5		3.5	118.	-23.2	-23.4	
		92	6.0		3.9	111.	-23.2	-23.5	1028.5
		92	6.5		4.0	107.	-22.9	-23.2	
		92	7.0		4.0	110.	-23.8	-24.0	
		92	7.5		3.4	108.	-23.6	-23.8	
		92	8.0		3.9	104.	-23.4	-23.6	
		92	8.5		4.7	105.	-23.0	-23.1	
		92	9.0		5.2	109.	-22.3	-22.5	1026.2
		92	9.5		4.8	113.	-22.0	-22.1	
		92	10.0						
		92	10.5		5.3	114.	-22.2	-22.2	
		92	11.0		5.6	113.	-21.7	-21.8	
		92	11.5		5.4	112.	-22.9	-22.8	
		92	12.0		5.7	110.	-23.4	-23.5	1024.0
		92	12.5		5.5	110.	-23.4	-23.5	
		92	13.0		5.9	111.	-22.1	-22.3	
		92	13.5		6.1	108.	-22.0	-22.1	
		92	14.0		5.7	109.	-22.1	-22.2	
		92	14.5		6.0	112.	-21.6	-21.8	
		92	15.0		6.1	111.	-21.5	-21.7	1021.5
		92	15.5	7.6	6.5	112.	-20.6	-20.9	
		92	16.0	7.3	6.2	114.	-20.1	-20.5	
		92	16.5	8.3	7.0	120.	-19.3	-19.8	
		92	17.0	8.3	7.0	120.	-19.5	-20.0	
		92	17.5	7.5	6.3	117.	-20.0	-20.4	
		92	18.0	7.1	6.0	117.	-21.1	-21.6	1019.3
		92	18.5	7.3	6.1	121.	-20.8	-21.2	
		92	19.0	7.1	5.9	126.	-20.3	-20.7	
		92	19.5	1.9	6.3	133.	-19.9	-20.3	
		92	20.0	.5	6.1	135.	-20.0	-20.3	
		92	20.5	1.0	6.4	135.	-20.2	-20.4	
		92	21.0	7.1	5.9	138.	-21.2	-21.6	1018.5
		92	21.5	6.6	5.5	137.	-21.5	-21.9	
		92	22.0	6.3	5.1	138.	-21.1	-21.5	
		92	22.5	6.0	4.9	139.	-21.3	-21.8	
		92	23.0	6.5	5.3	136.	-21.4	-22.0	
		92	23.5	6.2	5.0	136.	-21.5	-22.2	
APRIL	3	93	.0	6.0	4.9	136.	-22.4	-23.2	1018.0
		93	.5	5.6	4.5	138.	-21.9	-22.7	

93	1.0	5.1	4.0	135.	-22.0	-22.9			
93	1.5	4.7	3.6	137.	-22.3	-23.3			
93	2.0	4.4	3.3	139.	-22.6	-23.7			
93	2.5	4.2	3.1	166.	-22.9	-24.0			
93	3.0	3.6	2.6	187.	-24.5	-25.2	1017.8		
93	3.5	3.6	2.7	171.	-25.4	-26.0			
93	4.0	4.0	3.2	174.	-26.1	-26.5			
93	4.5	3.6	2.8	186.	-26.9	-27.3			
93	5.0	4.0	3.2	194.	-27.5	-27.7			
93	5.5	3.3	2.6	192.	-28.0	-28.1			
93	6.0	2.8	2.2	177.	-28.1	-28.2	1018.4		
93	6.5	3.2	2.6	174.	-28.4	-28.3			
93	7.0	3.2	2.6	193.	-29.5	-29.4			
93	7.5	2.4	1.9	192.	-28.5	-28.5			
93	8.0	2.5	2.0	205.	-28.4	-28.4			
93	8.5	3.2	2.7	224.	-28.0	-28.3			
93	9.0	3.5	3.0	233.	-26.9	-27.3	1018.7		
93	9.5	4.8	4.3	263.	-26.3	-31.5			
93	10.0	5.3	4.6	261.	-29.6	-36.9			
93	10.5	4.5	3.9	257.	-49.7	-48.5			
93	11.0	3.8	3.4	256.	-49.4	-48.8			
93	11.5	5.2	4.6	259.	-50.4	-48.7			
93	12.0	5.5	4.9	260.	-48.6	-48.5	1019.4		
93	12.5	4.7	4.3	262.	-53.0	-50.5			
93	13.0	5.5	4.9	261.	-50.6	-47.4			
93	13.5	5.9	5.3	260.	-46.8	-44.7			
93	14.0	5.4	4.8	262.	-46.0	-45.1			
93	14.5	5.2	4.5	270.	-49.2	-50.7			
93	15.0	4.9	4.2	272.	-47.3	-51.0	1020.1		
93	15.5	5.1	4.4	274.	-45.4	-50.8			
93	16.0	5.4	4.7	271.	-49.6	-51.3			
93	16.5	5.1	4.4	269.	-49.5	-51.5			
93	17.0	4.7	4.1	271.	-46.9	-51.1			
93	17.5	5.3	4.6	272.	-39.1	-39.9			
93	18.0	5.2	4.5	272.	-29.5	-29.8	1020.5		
93	18.5	5.2	4.4	271.	-28.6	-28.9			
93	19.0	5.6	5.0	269.	-30.8	-31.2			
93	19.5	5.2	4.5	265.	-47.9	-51.4			
93	20.0	4.9	4.3	264.	-46.1	-48.2			
93	20.5	5.4	4.4	263.	-30.1	-30.6			
93	21.0						1022.3		
93	21.5								
93	22.0								
93	22.5	5.4	4.6	271.	-29.0	-29.7			
93	23.0	5.7	4.9	265.	-29.2	-29.7			
93	23.5	5.6	4.8	267.	-29.4	-29.9			
APRIL	4	94	.0	5.2	4.5	263.	-29.7	-30.2	1023.8
		94	.5	5.2	4.5	266.	-29.7	-30.3	
		94	1.0	5.1	4.4	268.	-29.8	-30.3	
		94	1.5	4.8	4.1	268.	-29.9	-30.4	
		94	2.0	4.5	3.8	264.	-30.1	-30.6	
		94	2.5	4.2	3.5	263.	-30.2	-30.7	
		94	3.0	4.4	3.6	263.	-30.3	-30.7	1025.4
		94	3.5	6.5	5.5	279.	-29.0	-28.7	
		94	4.0	6.1	5.3	282.	-28.8	-28.4	
		94	4.5	6.2	5.2	279.	-28.4	-28.1	

94	5.0	6.6	5.5	278.	-28.1	-27.8	
94	5.5	6.2	5.3	274.	-28.4	-28.1	
94	6.0	5.7	4.9	269.	-27.4	-27.3	1027.7
94	6.5	5.0	4.4	257.	-27.1	-27.1	
94	7.0	5.8	5.0	261.	-27.0	-27.0	
94	7.5	6.0	5.2	270.	-26.8	-26.8	
94	8.0	6.0	5.2	268.	-27.4	-27.3	
94	8.5	6.2	5.5	270.	-27.4	-27.4	
94	9.0	5.9	5.1	273.	-26.7	-26.7	1030.3
94	9.5	5.7	4.9	273.	-26.8	-26.7	
94	10.0	5.3	4.6	267.	-26.9	-26.9	
94	10.5	5.4	4.7	271.	-27.4	-27.4	
94	11.0	5.5	4.7	270.	-27.0	-27.0	
94	11.5	5.5	4.6	273.	-27.8	-27.8	
94	12.0	5.4	4.6	272.	-27.1	-27.2	1032.0
94	12.5	5.6	4.7	280.	-27.7	-27.7	
94	13.0	6.2	5.2	286.	-27.9	-28.0	
94	13.5	5.5	4.5	285.	-28.0	-28.1	
94	14.0	5.1	4.1	279.	-28.2	-28.5	
94	14.5	5.0	4.0	279.	-27.6	-27.9	
94	15.0	4.8	3.9	283.	-27.9	-28.1	1033.4
94	15.5	4.7	3.7	279.	-27.9	-28.3	
94	16.0	4.4	3.4	277.	-27.9	-28.4	
94	16.5	5.0	4.0	281.	-28.1	-28.4	
94	17.0	4.9	3.9	281.	-28.5	-29.0	
94	17.5	5.0	4.0	282.	-28.1	-28.6	
94	18.0						1035.2
94	18.5						
94	19.0						
94	19.5						
94	20.0						
94	20.5						
94	21.0						1036.8
94	21.5						
94	22.0	4.4	3.5	267.	-28.1	-28.9	
94	22.5	4.4	3.5	262.	-28.6	-29.5	
94	23.0	4.7	3.8	271.	-28.4	-29.3	
94	23.5	4.8	3.8	276.	-28.2	-29.0	
APRIL 5	95 .0	4.8	3.8	268.	-28.4	-29.3	1038.0
	95 .5	4.9	3.9	273.	-28.4	-29.3	
	95 1.0	4.4	3.5	267.	-28.4	-29.3	
	95 1.5	4.1	3.1	262.	-28.9	-30.0	
	95 2.0	4.2	3.1	264.	-29.0	-30.1	
	95 2.5	4.3	3.3	264.	-28.8	-30.0	
	95 3.0	4.1	3.0	260.	-28.9	-30.1	1038.5
	95 3.5	3.3	2.3	236.	-28.3	-29.8	
	95 4.0	3.8	2.8	229.	-29.1	-30.1	
	95 4.5	3.9	2.9	231.	-29.3	-30.2	
	95 5.0	3.6	2.6	216.	-28.8	-30.0	
	95 5.5	3.8	2.8	226.	-29.0	-30.0	
	95 6.0	4.2	3.3	227.	-28.6	-29.3	1038.5
	95 6.5	4.4	3.3	228.	-28.3	-29.0	
	95 7.0	4.2	3.2	218.	-28.3	-29.0	
	95 7.5	4.7	3.6	233.	-27.3	-28.0	
	95 8.0	5.2	4.1	239.	-26.0	-26.7	
	95 8.5	5.7	4.8	260.	-25.7	-26.2	

	95	9.0	5.7	4.9	266.	-25.2	-25.5	1038.8
	95	9.5	4.3	3.6	268.	-26.3	-26.6	
	95	10.0	4.1	3.3	263.	-26.4	-27.0	
	95	10.5	4.3	3.5	268.	-26.3	-26.8	
	95	11.0	3.7	3.0	278.	-26.7	-26.9	
	95	11.5	4.3	3.6	282.	-26.9	-26.9	
	95	12.0	4.1	3.4	278.	-27.3	-27.3	1039.3
	95	12.5	3.8	3.1	280.	-27.5	-27.5	
	95	13.0	3.8	3.0	278.	-27.8	-27.8	
	95	13.5	3.2	2.7	266.	-27.9	-28.1	
	95	14.0	3.6	2.8	274.	-27.8	-28.0	
	95	14.5	3.8	3.1	276.	-27.6	-27.6	
	95	15.0	3.1	2.6	276.	-28.7	-28.8	1039.3
	95	15.5	2.4	2.0	252.	-29.1	-29.4	
	95	16.0	2.5	2.0	255.	-29.0	-29.4	
	95	16.5	2.4	1.8	244.	-28.9	-29.6	
	95	17.0	2.7	2.0	231.	-29.1	-29.8	
	95	17.5	2.9	2.2	224.	-29.7	-30.5	
	95	18.0	2.5	1.8	232.	-27.7	-27.5	1038.9
	95	18.5	2.3	1.5	219.	-28.5	-29.5	
	95	19.0	1.8	1.2	230.	-28.7	-30.1	
	95	19.5	1.2	1.4	135.	-29.0	-30.9	
	95	20.0	1.8	1.3	128.	-28.8	-31.2	
	95	20.5	2.1	1.3	130.	-29.5	-31.9	
	95	21.0	3.0	2.0	168.	-28.9	-30.7	1038.5
	95	21.5	3.5	2.4	175.	-31.4	-32.9	
	95	22.0	3.9	2.7	171.	-30.9	-32.3	
	95	22.5						
	95	23.0	3.3	2.2	149.	-29.5	-31.4	
	95	23.5	3.5	2.5	154.	-29.5	-31.2	
APRIL 6	96	.0	3.7	2.6	160.	-29.5	-31.0	1037.3
	96	.5	3.4	2.2	169.	-29.1	-30.8	
	96	1.0	2.6	1.8	163.	-29.4	-31.3	
	96	1.5	2.9	2.0	162.	-29.5	-31.2	
	96	2.0	2.7	1.9	160.	-29.6	-31.1	
	96	2.5	2.3	1.4	176.	-29.8	-31.5	
	96	3.0	2.1	1.5	169.	-29.8	-31.5	1036.6
	96	3.5	2.2	1.5	158.	-29.8	-31.8	
	96	4.0	2.6	1.7	156.	-29.7	-32.0	
	96	4.5	3.0	2.0	155.	-29.7	-31.7	
	96	5.0	2.9	2.1	159.	-29.7	-30.8	
	96	5.5	2.7	1.9	165.	-29.8	-31.0	
	96	6.0	3.0	2.0	175.	-29.2	-30.5	1036.0
	96	6.5	2.5	1.6	173.	-28.8	-30.3	
	96	7.0	2.1	1.5	140.	-30.3	-31.6	
	96	7.5	2.8	2.1	138.	-29.5	-30.5	
	96	8.0	2.7	2.2	137.	-29.6	-30.1	
	96	8.5	2.7	2.2	144.	-29.7	-30.1	
	96	9.0	3.1	2.4	137.	-29.8	-30.2	1035.5
	96	9.5	2.4	2.1	150.	-29.5	-29.9	
	96	10.0	2.2	1.9	144.	-30.2	-30.6	
	96	10.5	2.0	1.7	140.	-29.0	-29.3	
	96	11.0	2.2	1.9	146.	-28.9	-29.1	
	96	11.5	2.4	2.0	149.	-28.9	-29.2	
	96	12.0	2.4	2.0	149.	-29.7	-30.0	1034.9
	96	12.5	2.0	1.7	149.	-28.9	-29.2	

96	13.0	2.2	1.9	152.	-29.7	-30.0	
96	13.5	2.4	2.0	158.	-29.3	-29.7	
96	14.0	2.3	1.9	158.	-29.1	-29.6	
96	14.5	2.3	1.9	169.	-28.3	-28.7	
96	15.0	2.4	1.9	177.	-29.0	-29.4	1034.3
96	15.5	2.4	2.0	177.	-29.0	-29.6	
96	16.0	2.4	1.9	178.	-29.5	-30.1	
96	16.5	2.2	1.6	181.	-28.7	-29.4	
96	17.0	1.8	1.3	199.	-28.6	-29.5	
96	17.5	2.1	1.5	196.	-28.9	-29.9	
96	18.0	2.0	1.5	181.	-29.7	-30.9	1033.5
96	18.5	2.1	1.6	168.	-28.8	-30.1	
96	19.0	1.8	1.3	168.	-29.2	-30.6	
96	19.5	1.7	1.2	174.	-29.3	-31.0	
96	20.0	2.1	1.5	175.	-29.3	-31.2	
96	20.5	2.3	1.6	171.	-29.3	-31.0	
96	21.0	1.8	1.0	168.		-32.9	1033.6
96	21.5	2.1	1.4	160.		-29.0	
96	22.0	2.3	1.7	160.		-31.3	
96	22.5						
96	23.0						
96	23.5		1.7	148.	-29.9	-31.9	
APRIL 7	97 .0		1.7	142.	-30.2	-32.3	1032.7
	97 .5		2.1	136.	-30.9	-33.0	
	97 1.0		2.1	151.	-31.1	-32.7	
	97 1.5		1.9	151.	-30.9	-32.7	
	97 2.0		2.0	149.	-30.9	-32.8	
	97 2.5		2.2	147.	-31.2	-32.7	
	97 3.0		2.1	147.	-31.3	-32.7	1031.8
	97 3.5		2.1	140.	-31.4	-32.7	
	97 4.0		2.0	138.	-31.2	-32.4	
	97 4.5		1.9	138.	-31.1	-32.3	
	97 5.0		1.7	136.	-31.0	-32.1	
	97 5.5		2.0	136.	-30.9	-32.1	
	97 6.0		2.0	144.	-30.6	-31.6	1031.6
	97 6.5		2.2	147.	-30.2	-31.1	
	97 7.0		2.2	145.	-30.9	-31.9	
	97 7.5		2.2	139.	-29.5	-30.2	
	97 8.0		2.3	142.	-29.4	-29.9	
	97 8.5		2.6	141.	-29.2	-29.6	
	97 9.0	3.5	2.7	143.	-30.6	-31.1	1031.3
	97 9.5	3.3	2.5	145.	-29.7	-30.1	
	97 10.0	3.0	2.3	145.	-29.5	-30.0	
	97 10.5	3.2	2.5	150.	-28.2	-28.7	
	97 11.0	3.2	2.5	149.	-28.7	-29.2	
	97 11.5	4.2	3.2	162.	-27.5	-28.1	
	97 12.0	4.9	3.8	173.	-27.4	-27.8	1030.7
	97 12.5	4.0	3.0	177.	-27.6	-28.1	
	97 13.0	3.8	2.9	182.	-27.4	-27.8	
	97 13.5	3.8	2.8	184.	-27.4	-28.0	
	97 14.0	3.6	2.8	181.	-27.3	-27.8	
	97 14.5	3.8	2.9	183.	-27.2	-27.7	
	97 15.0	3.5	2.5	188.	-27.2	-27.6	1030.5
	97 15.5	3.3	2.4	174.	-27.3	-27.9	
	97 16.0	3.3	2.2	177.	-26.4	-27.2	
	97 16.5	3.3	2.2	174.	-26.8	-27.7	

	97	17.0	3.1	2.0	181.	-26.9	-27.9		
	97	17.5	2.7	1.7	191.	-26.3	-27.6		
	97	18.0	3.2	2.0	179.	-26.7	-28.2	1030.0	
	97	18.5	3.1	2.0	175.	-26.6	-27.9		
	97	19.0	3.0	1.9	182.	-26.6	-28.1		
	97	19.5	2.6	1.6	177.	-26.9	-28.7		
	97	20.0	2.7	1.7	177.	-27.0	-29.0		
	97	20.5	2.3	1.5	170.	-27.2	-29.0		
	97	21.0	1.9	1.5	165.	-27.1	-28.8	1029.5	
	97	21.5	1.6	1.4	145.	-16.4	-19.3		
	97	22.0	1.8	1.4	153.	-24.9	-27.5		
	97	22.5	1.9	1.0	208.	-27.7	-30.1		
	97	23.0	1.8	1.2	236.	-27.9	-29.8		
	97	23.5	1.2	.7	219.	-28.3	-29.8		
APRIL	8	98	.0	.7	.7	173.	-28.4	-29.5	1029.3
		98	.5	1.0	1.0	169.	-27.9	-29.3	
		98	1.0	1.8	1.7	132.	-27.9	-29.6	
		98	1.5	1.9	1.6	152.	-28.1	-29.9	
		98	2.0	2.0	1.2	167.	-28.0	-30.7	
		98	2.5	2.1	1.6	138.	-29.2	-31.6	
		98	3.0	2.0	1.3	139.	-28.3	-30.3	1028.4
		98	3.5	2.0	1.3	146.	-28.2	-30.4	
		98	4.0	1.9	1.3	178.	-28.3	-30.2	
		98	4.5	1.7	1.1	193.	-28.5	-30.2	
		98	5.0	.6	.4	157.	-28.4	-29.6	
		98	5.5	.6	.8	137.	-28.0	-29.2	
		98	6.0	1.1	1.2	130.	-27.8	-29.6	1028.4
		98	6.5	1.4	1.3	118.	-27.7	-29.3	
		98	7.0	2.1	1.9	102.	-28.8	-29.9	
		98	7.5	2.4	2.0	111.	-28.6	-29.4	
		98	8.0	2.3	1.7	120.	-28.6	-29.4	
		98	8.5	2.3	1.8	124.	-28.7	-29.3	
		98	9.0	2.4	1.9	131.	-29.6	-29.9	1028.4
		98	9.5	2.6	2.1	138.	-28.9	-29.2	
		98	10.0	2.3	1.8	133.	-28.4	-28.9	
		98	10.5	2.8	2.1	141.	-28.0	-28.5	
		98	11.0	2.8	2.2	151.	-27.3	-27.7	
		98	11.5	2.6	2.1	147.	-27.2	-27.5	
		98	12.0	1.8	1.5	128.	-27.5	-27.8	1028.4
		98	12.5	1.1	1.1	115.	-27.5	-27.7	
		98	13.0	1.3	1.2	99.	-26.7	-27.0	
		98	13.5	1.6	1.4	62.	-27.5	-27.8	
		98	14.0	1.6	1.5	97.	-27.2	-27.3	
		98	14.5	1.6	1.5	105.	-26.5	-26.6	
		98	15.0	1.9	1.9	96.	-26.6	-26.6	1028.9
		98	15.5	1.7	1.6	106.	-26.4	-26.4	
		98	16.0	1.1	1.0	78.	-25.9	-26.3	
		98	16.5	1.2	1.1	98.	-25.4	-26.1	
		98	17.0	1.8	1.5	122.	-25.4	-26.1	
		98	17.5	2.3	1.9	135.	-25.6	-26.2	
		98	18.0	1.6	1.4	127.	-26.0	-26.6	1029.7
		98	18.5	1.2	.8	165.	-25.1	-26.0	
		98	19.0	1.4	1.0	198.	-24.8	-25.6	
		98	19.5	1.5	1.1	214.	-24.5	-25.2	
		98	20.0	1.5	1.2	221.	-24.5	-25.5	
		98	20.5	2.0	1.5	256.	-24.6	-25.9	

	98	21.0	2.1	1.5	282.	-25.3	-26.3	1030.9	
	98	21.5	1.4	1.0	261.	-25.1	-26.2		
	98	22.0							
	98	22.5							
	98	23.0	2.3	1.7	290.	-25.0	-25.4		
	98	23.5	2.7	1.9	291.	-25.3	-26.3		
APRIL	9	99	.0	2.9	2.1	304.	-26.7	-27.6	1031.5
		99	.5	2.8	2.0	300.	-26.8	-27.9	
		99	1.0	3.2	2.4	304.	-27.0	-28.1	
		99	1.5	3.1	2.3	301.	-27.5	-28.6	
		99	2.0	3.0	2.2	295.	-28.0	-29.3	
		99	2.5	3.4	2.6	297.	-28.2	-29.3	
		99	3.0	3.7	3.1	300.	-28.3	-29.3	1032.2
		99	3.5	3.7	3.1	303.	-28.3	-29.1	
		99	4.0	3.7	3.0	311.	-28.7	-29.7	
		99	4.5	3.7	3.1	311.	-28.8	-29.8	
		99	5.0	3.9	3.2	311.	-29.1	-30.2	
		99	5.5	3.8	3.1	313.	-29.0	-30.0	
		99	6.0	4.3	3.6	322.	-28.8	-29.7	1033.3
		99	6.5	4.5	3.8	325.	-28.7	-29.6	
		99	7.0	4.5	3.9	326.	-28.7	-29.5	
		99	7.5	4.2	3.6	325.	-28.8	-29.5	
		99	8.0	3.9	3.3	320.	-29.0	-29.6	
		99	8.5	4.1	3.5	327.	-28.9	-29.5	
		99	9.0	4.6	4.0	324.	-29.6	-30.3	1035.4
		99	9.5	4.3	3.7	320.	-30.0	-30.6	
		99	10.0	5.1	4.6	328.	-29.8	-30.4	
		99	10.5	5.2	4.6	332.	-29.1	-29.6	
		99	11.0	5.1	4.6	329.	-29.7	-30.2	
		99	11.5	5.3	4.8	331.	-29.8	-30.2	
		99	12.0	5.0	4.5	334.	-29.4	-29.8	1036.5
		99	12.5	4.7	4.3	333.	-30.4	-30.7	
		99	13.0	4.7	4.2	330.	-30.4	-32.9	
		99	13.5	4.6	4.2	328.	-30.2	-32.7	
		99	14.0	4.5	4.0	324.	-30.3	-32.5	
		99	14.5	4.6	4.1	326.	-30.3	-32.6	
		99	15.0	5.0	4.5	329.	-30.4	-32.6	1038.3
		99	15.5	4.9	4.3	330.	-30.4	-32.5	
		99	16.0	4.6	4.1	329.	-29.8	-31.9	
		99	16.5	4.2	3.7	330.	-30.5	-32.8	
		99	17.0	4.3	3.8	335.	-30.5	-32.9	
		99	17.5	4.0	3.5	330.	-30.6	-33.0	
		99	18.0	3.5	2.9	326.	-30.8	-33.3	1040.0
		99	18.5	3.7	2.9	316.		-34.4	
		99	19.0	3.9	3.0	320.		-30.9	
		99	19.5	4.0	3.0	320.		-30.2	
		99	20.0	3.7	2.8	316.		-30.4	
		99	20.5	3.4	2.6	314.		-30.6	
		99	21.0	3.1	2.3	304.		-31.9	1041.5
		99	21.5						
		99	22.0						
		99	22.5						
		99	23.0						
		99	23.5	3.1	2.2	312.	-30.7	-31.8	
APRIL	10	100	.0	2.8	2.0	313.	-30.8	-32.0	1042.1
		100	.5	3.2	2.4	305.	-31.3	-32.2	

100	1.0	3.2	2.3	310.	-31.5	-32.4		
100	1.5	3.0	2.2	309.	-31.6	-32.6		
100	2.0	2.8	1.9	319.	-31.6	-32.5		
100	2.5	2.4	1.7	305.	-31.6	-32.7		
100	3.0	2.5	1.8	308.	-31.6	-32.8	1042.8	
100	3.5	2.3	1.7	306.	-31.7	-32.8		
100	4.0	2.3	1.6	294.	-31.6	-32.7		
100	4.5	2.6	1.8	295.	-31.4	-32.3		
100	5.0	2.0	1.4	300.	-31.1	-32.2		
100	5.5	2.4	1.7	294.	-30.9	-31.6		
100	6.0	2.1	1.5	302.	-30.7	-31.7	1043.4	
100	6.5	2.3	1.7	309.	-30.4	-31.4		
100	7.0	1.9	1.3	302.	-30.9	-31.9		
100	7.5	2.5	1.8	305.	-30.1	-30.9		
100	8.0	2.2	1.6	312.	-30.1	-30.7		
100	8.5	2.0	1.6	312.	-30.0	-30.7		
100	9.0	2.2	1.8	302.	-30.8	-31.4	1044.1	
100	9.5	1.7	1.3	307.	-31.3	-32.1		
100	10.0	1.7	1.2	302.	-30.9	-31.6		
100	10.5	1.8	1.3	299.	-30.9	-31.3		
100	11.0	1.7	1.3	303.	-30.6	-31.0		
100	11.5	1.5	1.3	321.	-30.4	-30.9		
100	12.0	1.7	1.4	314.	-30.3	-30.8	1044.5	
100	12.5	1.1	.8	338.	-29.5	-30.1		
100	13.0	1.0	.8	311.	-29.1	-29.4		
100	13.5	.7	.6	331.	-28.8	-29.4		
100	14.0	.7	.5	289.	-29.4	-30.3		
100	14.5	1.0	.9	276.	-28.6	-29.5		
100	15.0	1.2	1.0	283.	-29.0	-29.6	1044.7	
100	15.5	1.3	1.0	264.	-29.1	-29.7		
100	16.0	.6	.4	248.	-28.7	-30.1		
100	16.5	.8	.7	160.	-29.3	-30.0		
100	17.0	1.1	.9	167.	-28.2	-29.2		
100	17.5	1.4	1.1	153.	-28.2	-29.4		
100	18.0	1.8	1.3	184.	-28.9	-30.7	1044.8	
100	18.5	1.9	1.3	163.	-28.0	-29.9		
100	19.0	2.3	1.6	159.	-28.4	-30.1		
100	19.5	2.6	1.6	173.	-28.3	-30.1		
100	20.0	2.8	1.9	165.	-28.2	-29.9		
100	20.5	2.8	1.8	170.	-29.1	-30.7		
100	21.0	3.0	1.9	173.	-29.3	-30.7	1044.6	
100	21.5	3.1	1.9	177.	-29.5	-30.9		
100	22.0	3.6	2.4	172.	-29.4	-30.6		
100	22.5	3.8	2.8	167.	-28.4	-29.4		
100	23.0	3.6	2.6	164.	-29.7	-30.7		
100	23.5							
APRIL 11	101	.0					1043.9	
	101	.5						
	101	1.0	4.8	3.6	181.	-26.8	-28.0	
	101	1.5	4.8	3.5	180.	-27.1	-28.2	
	101	2.0	5.0	3.8	182.	-27.1	-27.8	
	101	2.5	4.5	3.5	186.	-27.0	-27.6	
	101	3.0	4.5	3.5	190.	-27.0	-27.6	1042.5
	101	3.5	4.5	3.5	196.	-26.8	-27.4	
	101	4.0	4.4	3.4	201.	-26.7	-27.0	
	101	4.5	4.3	3.5	201.	-26.4	-26.6	

101	5.0	4.3	3.5	201.	-26.1	-26.3		
101	5.5	4.1	3.3	198.	-26.0	-26.2		
101	6.0	4.3	3.4	202.	-25.9	-26.1	1041.6	
101	6.5	4.1	3.2	203.	-25.8	-26.1		
101	7.0	4.3	3.4	205.	-26.1	-26.4		
101	7.5	4.2	3.4	201.	-25.0	-25.3		
101	8.0	4.9	4.0	201.	-24.4	-24.5		
101	8.5	5.2	4.3	200.	-24.0	-24.0		
101	9.0	5.1	4.2	207.	-23.9	-24.0	1040.7	
101	9.5	5.0	4.2	221.	-23.8	-23.9		
101	10.0	4.9	4.1	215.	-23.5	-23.8		
101	10.5	4.4	3.6	209.	-22.7	-23.2		
101	11.0	4.7	3.9	215.	-22.5	-23.0		
101	11.5	4.7	4.0	214.	-22.4	-22.8		
101	12.0	4.8	4.0	211.	-22.7	-23.2	1040.5	
101	12.5	4.7	4.0	210.	-22.0	-22.4		
101	13.0	5.5	4.6	234.	-21.6	-22.0		
101	13.5	4.9	4.1	236.	-21.3	-21.7		
101	14.0	4.8	4.0	234.	-20.9	-21.3		
101	14.5	4.5	3.8	253.	-20.8	-21.2		
101	15.0	4.5	3.8	263.	-21.0	-21.4	1040.8	
101	15.5	4.1	3.4	266.	-21.2	-21.7		
101	16.0	4.6	3.9	270.	-22.2	-22.7		
101	16.5	4.3	3.7	271.	-21.8	-22.2		
101	17.0	4.4	3.9	262.	-21.8	-22.2		
101	17.5	4.6	4.1	262.	-21.4	-21.7		
101	18.0	4.5	4.0	262.	-21.5	-21.8	1040.8	
101	18.5							
101	19.0							
101	19.5							
101	20.0							
101	20.5							
101	21.0						1041.3	
101	21.5							
101	22.0							
101	22.5							
101	23.0	4.5	3.4	257.	-21.3	-21.9		
101	23.5	4.8	3.6	259.	-21.5	-21.9		
APRIL 12	102	.0	5.4	3.9	265.	-21.7	-21.9	1040.5
	102	.5	5.4	3.8	267.	-21.7	-21.9	
	102	1.0	5.2	3.6	270.	-21.8	-22.0	
	102	1.5	5.4	4.2	280.	-21.9	-22.0	
	102	2.0	4.8	4.0	282.	-22.2	-22.4	
	102	2.5	4.3	3.3	279.	-22.3	-22.5	
	102	3.0	4.0	2.9	275.	-22.2	-22.5	1039.3
	102	3.5	3.9	2.8	265.	-22.3	-22.6	
	102	4.0	3.6	2.6	261.	-22.2	-22.6	
	102	4.5	3.5	2.5	262.	-21.7	-22.0	
	102	5.0	3.2	2.6	258.	-21.3	-21.5	
	102	5.5	2.8	2.4	250.	-20.8	-21.1	
	102	6.0	2.3	1.8	251.	-19.4	-19.8	1037.5
	102	6.5	2.0	1.7	215.	-20.2	-20.3	
	102	7.0	2.9	2.5	213.	-20.8	-20.8	
	102	7.5	2.8	2.5	208.	-20.8	-20.7	
	102	8.0	2.5	2.1	195.	-20.2	-20.1	
	102	8.5	3.0	2.6	201.	-20.0	-19.9	

	102	9.0	3.2	2.8	201.	-20.1	-20.0	1035.3
	102	9.5	2.9	2.5	200.	-20.1	-20.0	
	102	10.0	3.4	2.9	202.	-20.0	-19.9	
	102	10.5	3.7	3.0	197.	-19.8	-19.9	
	102	11.0	4.3	3.5	199.	-19.4	-19.4	
	102	11.5	4.3	3.7	208.	-19.3	-19.2	
	102	12.0	3.7	3.2	227.	-19.2	-19.1	1032.1
	102	12.5	4.0	3.4	240.	-18.0	-18.1	
	102	13.0						
	102	13.5						
	102	14.0						
	102	14.5						
	102	15.0						1029.7
	102	15.5						
	102	16.0						
	102	16.5						
	102	17.0						
	102	17.5						
	102	18.0						1027.6
	102	18.5						
	102	19.0						
	102	19.5						
	102	20.0	6.6	5.6	310.		-18.1	
	102	20.5	6.3	5.4	311.		-18.3	
	102	21.0	6.7	5.8	329.		-18.9	1027.2
	102	21.5	6.8	5.9	339.		-19.2	
	102	22.0	7.2	6.3	340.		-19.5	
	102	22.5	8.0	6.9	349.		-19.3	
	102	23.0						
	102	23.5	7.3	6.3	353.	-22.1	-22.6	
APRIL 13	103	.0	6.1	5.2	356.	-23.0	-23.6	1028.6
	103	.5	6.6	5.6	351.	-24.1	-24.6	
	103	1.0	6.1	5.0	358.	-25.0	-25.5	
	103	1.5	5.9	4.9	358.	-25.7	-26.2	
	103	2.0	5.7	4.9	353.	-26.2	-26.7	
	103	2.5	5.8	4.9	349.	-26.7	-27.1	
	103	3.0	5.6	4.8	349.	-27.1	-27.5	1030.5
	103	3.5	5.5	4.7	350.	-27.5	-27.8	
	103	4.0	5.9	5.1	347.	-27.8	-28.1	
	103	4.5	6.4	5.6	348.	-28.0	-28.3	
	103	5.0	6.6	5.7	352.	-28.2	-28.6	
	103	5.5	6.6	5.7	352.	-28.4	-28.6	
	103	6.0	6.8	5.8	358.	-28.6	-28.9	1032.0
	103	6.5	6.3	5.4	0.	-28.9	-29.1	
	103	7.0	6.3	5.4	358.	-29.7	-30.0	
	103	7.5	6.0	5.2	357.	-29.1	-29.3	
	103	8.0	5.5	4.7	358.	-29.2	-29.4	
	103	8.5	5.5	4.8	2.	-30.5	-31.1	
	103	9.0	5.9	5.1	358.	-29.6	-38.5	1034.0
	103	9.5	6.0	5.2	2.	-31.2	-45.5	
	103	10.0	5.8	5.0	359.	-30.8	-31.3	
	103	10.5	5.6	4.8	358.	-30.6	-32.6	
	103	11.0	5.4	4.7	0.	-31.0	-35.2	
	103	11.5	5.2	4.6	0.	-31.0	-35.8	
	103	12.0	5.1	4.4	5.	-31.6	-31.8	1035.6
	103	12.5	4.9	4.2	7.	-31.3	-31.4	

	103	13.0	5.0	4.3	13.	-30.7	-30.8	
	103	13.5	4.7	4.0	18.	-31.2	-31.3	
	103	14.0	4.7	4.0	22.	-31.3	-36.5	
	103	14.5	5.2	4.6	30.	-32.7	-34.6	
	103	15.0	5.0	4.4	30.	-33.0	-34.4	1036.4
	103	15.5	4.7	4.1	37.	-32.9	-34.4	
	103	16.0	3.8	3.3	31.	-31.4	-34.1	
	103	16.5	3.2	2.8	29.	-30.5	-33.4	
	103	17.0	3.3	2.9	33.	-31.4	-34.5	
	103	17.5	3.6	3.1	42.	-30.9	-31.2	
	103	18.0	3.3	2.9	45.	-30.8	-30.9	1036.7
	103	18.5	3.3	2.8	49.	-30.6	-30.9	
	103	19.0	3.2	2.6	63.	-29.8	-30.1	
	103	19.5	3.5	2.9	64.	-29.9	-30.2	
	103	20.0	3.6	3.0	76.	-30.1	-30.3	
	103	20.5	2.8	2.4	91.	-30.4	-30.6	
	103	21.0	2.7	2.3	101.	-29.0	-29.2	1036.5
	103	21.5	3.1	2.7	88.	-30.5	-30.7	
	103	22.0	3.0	2.6	88.	-30.6	-30.9	
	103	22.5						
	103	23.0	3.9	3.5	106.	-30.7	-31.0	
	103	23.5	4.0	3.5	107.	-30.3	-31.0	
APRIL 14	104	.0	4.7	4.2	104.	-30.6	-30.7	1035.9
	104	.5	5.5	4.9	103.	-30.3	-30.5	
	104	1.0	5.4	4.8	108.	-30.2	-30.4	
	104	1.5	4.9	4.4	110.	-29.9	-30.2	
	104	2.0	4.5	4.0	117.	-29.7	-30.0	
	104	2.5	4.1	3.6	112.	-29.6	-30.0	
	104	3.0	4.4	3.9	120.	-29.6	-30.0	1035.0
	104	3.5	4.6	4.1	122.	-29.6	-29.9	
	104	4.0	5.3	4.7	118.	-29.5	-29.8	
	104	4.5	5.5	4.9	122.	-29.3	-29.6	
	104	5.0	5.1	4.5	119.	-29.2	-29.6	
	104	5.5	4.9	4.4	113.	-29.2	-29.7	
	104	6.0	4.9	4.4	113.	-29.3	-29.7	1034.3
	104	6.5	4.9	4.4	113.	-29.1	-29.5	
	104	7.0	5.4	4.8	113.	-29.5	-29.9	
	104	7.5	5.0	4.4	118.	-28.5	-28.9	
	104	8.0	5.2	4.7	111.	-28.3	-28.6	
	104	8.5	5.0	4.5	114.	-28.2	-28.4	
	104	9.0	4.7	4.3	113.	-28.0	-28.1	1034.5
	104	9.5	5.6	5.0	114.	-28.4	-28.6	
	104	10.0	6.0	5.4	110.	-28.2	-28.4	
	104	10.5	6.0	5.4	109.	-28.0	-28.3	
	104	11.0	5.3	4.8	108.	-28.1	-28.2	
	104	11.5	5.7	5.1	103.	-28.3	-28.3	
	104	12.0	5.5	5.0	103.	-28.4	-28.4	1034.8
	104	12.5	5.5	4.9	105.	-27.7	-27.7	
	104	13.0	5.4	4.9	106.	-27.8	-27.7	
	104	13.5	5.6	5.0	107.	-28.0	-27.9	
	104	14.0	5.3	4.8	107.	-28.5	-28.6	
	104	14.5	4.7	4.1	115.	-28.6	-28.6	
	104	15.0	5.0	4.5	121.	-27.5	-27.5	1035.5
	104	15.5	5.1	4.4	122.	-28.1	-28.0	
	104	16.0	4.8	4.2	122.	-27.1	-27.2	
	104	16.5	4.7	4.1	104.	-27.9	-28.1	

	104	17.0	4.4	3.9	101.	-27.6	-27.7	
	104	17.5	4.8	4.2	100.	-28.4	-28.6	
	104	18.0	4.4	3.8	97.	-27.7	-27.9	1036.5
	104	18.5	4.6	4.0	97.	-28.9	-29.1	
	104	19.0	4.6	4.0	94.	-29.0	-29.3	
	104	19.5	4.1	3.5	94.	-28.9	-29.1	
	104	20.0	4.0	3.4	96.	-28.6	-28.9	
	104	20.5	4.0	3.4	94.	-28.8	-29.0	
	104	21.0	4.0	3.4	94.	-29.3	-29.5	1037.8
	104	21.5	4.1	3.6	96.	-33.7	-34.4	
	104	22.0	3.8	3.3	95.	-29.2	-29.5	
	104	22.5	3.8	3.3	93.	-29.4	-29.7	
	104	23.0	3.4	2.9	87.	-29.6	-30.0	
	104	23.5	3.6	2.9	86.	-30.0	-30.4	
APRIL 15	105	.0	3.6	3.0	94.	-30.3	-30.7	1038.7
	105	.5	3.5	2.9	93.	-30.4	-30.8	
	105	1.0	3.2	2.6	89.	-30.5	-30.9	
	105	1.5	3.5	2.8	79.	-30.8	-31.2	
	105	2.0	3.5	2.8	81.	-31.0	-31.4	
	105	2.5	3.2	2.6	84.	-31.0	-31.3	
	105	3.0	3.1	2.6	81.	-31.1	-31.4	1039.7
	105	3.5	2.4	2.0	85.	-31.0	-31.3	
	105	4.0	1.9	1.5	82.	-31.0	-31.2	
	105	4.5	2.5	1.9	77.	-31.3	-31.5	
	105	5.0	2.4	1.9	79.	-31.2	-31.2	
	105	5.5	2.3	1.8	75.	-31.5	-31.6	
	105	6.0	2.4	1.8	76.	-31.0	-31.2	1040.5
	105	6.5	2.7	2.1	75.	-30.7	-30.6	
	105	7.0	2.6	2.1	78.	-30.7	-30.6	
	105	7.5	2.6	2.2	79.	-30.8	-30.5	
	105	8.0	2.5	2.1	91.	-30.6	-30.5	
	105	8.5	2.3	1.9	80.	-30.6	-30.3	
	105	9.0	2.4	2.0	78.	-31.2	-30.9	1041.3
	105	9.5	1.9	1.6	81.	-30.1	-29.9	
	105	10.0	2.1	1.9	87.	-30.0	-29.8	
	105	10.5	2.2	1.9	86.	-30.0	-29.7	
	105	11.0	2.0	1.7	86.	-30.7	-30.5	
	105	11.5	2.1	1.9	88.	-29.8	-29.6	
	105	12.0	2.0	1.7	83.	-30.6	-30.5	1041.6
	105	12.5	2.1	1.8	85.	-30.4	-30.4	
	105	13.0	2.0	1.7	88.	-29.6	-29.7	
	105	13.5	2.0	1.7	84.	-29.7	-29.8	
	105	14.0	1.8	1.6	82.	-29.5	-29.6	
	105	14.5	2.1	1.6	79.	-29.2	-29.3	
	105	15.0	2.0	1.6	85.	-28.9	-29.1	1041.6
	105	15.5	2.2	1.8	91.	-29.7	-29.9	
	105	16.0	2.1	1.7	78.	-29.6	-29.8	
	105	16.5	2.3	1.8	81.	-28.7	-29.0	
	105	17.0	2.3	1.8	93.	-29.5	-29.7	
	105	17.5	2.3	1.8	84.	-29.1	-29.3	
	105	18.0	2.5	2.0	85.	-29.6	-29.9	1041.5
	105	18.5	2.3	1.9	87.	-29.3	-29.6	
	105	19.0	1.9	1.5	86.	-29.6	-30.0	
	105	19.5	2.0	1.5	89.	-30.5	-30.9	
	105	20.0	2.2	1.7	100.	-29.9	-30.4	
	105	20.5	2.1	1.6	89.	-29.8	-30.3	

	105	21.0	2.1	1.6	91.	-30.8	-31.3	1041.7
	105	21.5	2.0	1.5	80.	-31.6	-32.3	
	105	22.0						
	105	22.5						
	105	23.0						
	105	23.5						
APRIL 16	106	0	2.1	1.6	91.	-30.9	-31.7	1041.6
	106	.5	1.9	1.4	89.	-30.8	-31.6	
	106	1.0	1.9	1.4	85.	-30.9	-31.8	
	106	1.5	2.0	1.5	87.	-30.9	-31.9	
	106	2.0	2.2	1.6	87.	-31.0	-32.1	
	106	2.5	2.3	1.7	92.	-31.1	-32.1	
	106	3.0	1.9	1.5	96.	-30.9	-31.8	1041.4
	106	3.5	1.9	1.3	103.	-30.8	-31.8	
	106	4.0	1.8	1.4	108.	-31.0	-31.9	
	106	4.5	1.7	1.3	107.	-30.7	-31.7	
	106	5.0	1.8	1.4	111.	-30.5	-31.7	
	106	5.5	1.7	1.4	103.	-30.3	-31.3	
	106	6.0	1.8	1.5	101.	-29.9	-30.8	1041.3
	106	6.5	2.0	1.7	102.	-29.8	-30.6	
	106	7.0	1.9	1.6	102.	-30.4	-31.2	
	106	7.5	2.0	1.7	100.	-29.3	-30.1	
	106	8.0	1.9	1.6	91.	-29.3	-29.9	
	106	8.5	1.8	1.5	89.	-29.4	-30.0	
	106	9.0	1.8	1.6	93.	-30.0	-30.4	1041.4
	106	9.5	1.9	1.8	94.	-30.1	-30.5	
	106	10.0	2.0	1.9	96.	-30.2	-30.5	
	106	10.5	2.0	1.9	100.	-30.2	-30.6	
	106	11.0	2.0	1.8	101.	-30.2	-30.6	
	106	11.5	2.1	2.0	101.	-30.0	-30.5	
	106	12.0	2.1	2.0	102.	-30.0	-30.4	1041.5
	106	12.5	2.3	2.2	100.	-29.9	-30.3	
	106	13.0	2.1	2.0	103.	-29.1	-29.4	
	106	13.5	2.0	1.9	101.	-29.4	-31.1	
	106	14.0	2.3	2.2	103.	-29.4	-30.6	
	106	14.5	2.4	2.2	103.	-29.4	-30.4	
	106	15.0	2.5	2.3	99.	-30.5	-31.5	1041.3
	106	15.5	2.5	2.3	104.	-30.4	-31.5	
	106	16.0	2.4	2.2	99.	-31.0	-32.1	
	106	16.5	2.5	2.3	102.	-30.6	-31.7	
	106	17.0	2.3	2.1	97.	-30.9	-32.3	
	106	17.5	2.6	2.3	89.	-31.5	-35.1	
	106	18.0	2.6	2.3	96.	-30.5	-31.2	1041.1
	106	18.5	2.8	2.5	98.	-30.8	-31.4	
	106	19.0	2.7	2.4	98.	-30.4	-31.0	
	106	19.5	2.8	2.4	96.	-31.2	-31.9	
	106	20.0	2.7	2.4	94.	-30.5	-31.2	
	106	20.5	2.6	2.3	94.	-30.8	-31.5	
	106	21.0	2.7	2.1	92.		-32.6	1041.2
	106	21.5	2.8	2.2	88.		-32.9	
	106	22.0	3.1	2.4	86.		-32.0	
	106	22.5	3.1	2.4	89.		-33.0	
	106	23.0	3.3	2.5	92.		-32.3	
	106	23.5						
APRIL 17	107	.0						1041.0
	107	.5	3.2	2.6	97.	-31.8	-32.6	

107	1.0	3.0	2.4	97.	-32.0	-32.8	
107	1.5	3.0	2.4	95.	-32.4	-33.0	
107	2.0	2.6	2.0	90.	-32.6	-33.2	
107	2.5	2.6	2.0	86.	-32.8	-33.4	
107	3.0	2.8	2.1	84.	-32.9	-33.4	1040.8
107	3.5	3.0	2.3	85.	-32.9	-33.3	
107	4.0	3.4	2.7	88.	-32.7	-33.1	
107	4.5	3.5	2.8	90.	-32.6	-32.8	
107	5.0	3.3	2.7	88.	-32.7	-32.8	
107	5.5	3.5	2.9	89.	-32.8	-32.8	
107	6.0	3.2	2.6	89.	-32.6	-32.6	1040.5
107	6.5	3.0	2.5	91.	-32.5	-32.4	
107	7.0	3.0	2.5	94.	-33.2	-33.0	
107	7.5	3.0	2.5	88.	-32.2	-32.0	
107	8.0	3.2	2.8	90.	-32.0	-31.7	
107	8.5	3.2	2.8	92.	-31.7	-31.5	
107	9.0	3.0	2.6	96.	-31.5	-31.2	1040.3
107	9.5	3.2	2.7	86.	-32.2	-31.9	
107	10.0	3.4	3.0	85.	-32.0	-31.7	
107	10.5	3.3	2.9	85.	-31.9	-31.7	
107	11.0	3.1	2.7	89.	-32.0	-31.8	
107	11.5	3.1	2.7	90.	-31.1	-30.9	
107	12.0	2.9	2.5	84.	-31.8	-31.6	1039.5
107	12.5	3.3	2.9	86.	-31.7	-31.7	
107	13.0	3.2	2.8	83.	-31.9	-31.9	
107	13.5	3.1	2.7	86.	-31.2	-31.1	
107	14.0	3.3	2.8	85.	-30.5	-30.5	
107	14.5	3.6	3.1	87.	-31.2	-31.2	
107	15.0	3.7	3.1	85.	-30.6	-30.6	1038.5
107	15.5	3.4	2.9	83.	-31.2	-31.2	
107	16.0	3.6	3.1	81.	-31.1	-31.2	
107	16.5	3.4	2.8	81.	-30.3	-30.4	
107	17.0	3.7	3.1	79.	-31.1	-31.3	
107	17.5	3.5	3.0	82.	-30.1	-30.3	
107	18.0	3.5	2.9	81.	-31.0	-31.3	1037.0
107	18.5	3.6	3.0	80.	-31.7	-32.1	
107	19.0	3.4	2.8	83.	-30.6	-30.9	
107	19.5	3.4	2.8	78.	-31.4	-31.8	
107	20.0	3.3	2.7	79.	-31.0	-31.3	
107	20.5	3.4	2.8	83.	-31.8	-32.2	
107	21.0	3.2	2.5	82.	-32.3	-32.8	1036.0
107	21.5	3.4	2.7	80.	-32.7	-33.2	
107	22.0	3.8	3.0	82.	-31.3	-31.8	
107	22.5						
107	23.0						
107	23.5						
APRIL 18	108	.0					1034.6
	108	.5					
	108	1.0	3.3	2.6	83.	-32.1	-32.6
	108	1.5	3.4	2.7	81.	-32.2	-32.6
	108	2.0	3.1	2.5	81.	-32.2	-32.7
	108	2.5	2.8	2.2	81.	-32.2	-32.7
	108	3.0	2.8	2.2	76.	-32.2	-32.7
	108	3.5	3.0	2.5	74.	-32.0	-32.4
	108	4.0	2.9	2.4	69.	-32.2	-32.4
	108	4.5	2.3	1.9	65.	-32.3	-32.5

108	5.0	2.2	1.9	61.	-32.2	-32.4	
108	5.5	2.1	1.9	62.	-32.2	-32.2	
108	6.0	2.2	1.9	62.	-31.8	-31.8	1031.3
108	6.5	2.9	2.7	57.	-31.8	-31.7	
108	7.0	2.6	2.4	54.	-32.4	-32.2	
108	7.5	2.5	2.3	50.	-31.4	-31.2	
108	8.0	2.2	2.1	51.	-31.2	-31.0	
108	8.5	2.7	2.6	51.	-31.1	-30.9	
108	9.0	2.3	2.2	52.	-31.0	-30.7	1029.7
108	9.5	2.8	2.6	54.	-30.9	-30.6	
108	10.0	2.6	2.5	52.	-30.5	-30.3	
108	10.5	2.4	2.3	46.	-31.0	-30.9	
108	11.0	2.4	2.2	33.	-31.2	-31.2	
108	11.5	2.4	2.3	34.	-31.0	-31.0	
108	12.0	2.8	2.7	47.	-30.4	-30.4	1027.6
108	12.5	2.3	2.1	38.	-29.4	-29.5	
108	13.0	2.5	2.3	30.	-29.3	-29.5	
108	13.5	2.8	2.6	36.	-28.4	-28.6	
108	14.0	2.4	2.2	31.	-29.1	-29.4	
108	14.5	2.1	1.8	29.	-29.1	-29.3	
108	15.0	2.2	1.8	35.	-29.0	-29.3	1025.4
108	15.5	2.6	2.2	33.	-27.4	-27.8	
108	16.0	2.9	2.4	31.	-27.3	-27.7	
108	16.5	2.7	2.2	28.	-26.7	-27.3	
108	17.0	2.8	2.3	13.	-26.5	-27.2	
108	17.5	2.4	1.9	350.	-26.7	-27.3	
108	18.0	2.6	2.1	338.	-26.0	-26.7	1023.3
108	18.5	2.9	2.3	336.	-26.9	-27.6	
108	19.0	3.1	2.5	338.	-27.2	-27.9	
108	19.5	3.1	2.5	338.	-26.8	-27.5	
108	20.0	3.5	2.5	337.		-22.9	
108	20.5	3.5	2.6	339.		-28.6	
108	21.0	3.6	2.7	339.		-27.8	1021.5
108	21.5	3.8	2.8	341.		-28.9	
108	22.0	3.7	2.7	340.		-29.3	
108	22.5						
108	23.0	4.0	3.0	336.	-27.3	-28.0	
108	23.5	3.5	2.6	333.	-27.3	-28.1	
APRIL 19	109	.0	4.2	339.	-27.5	-28.3	1019.8
	109	.5	4.2	336.	-27.5	-28.2	
	109	1.0	3.9	334.	-27.7	-28.3	
	109	1.5	3.9	331.	-27.9	-28.6	
	109	2.0	4.3	328.	-27.7	-28.2	
	109	2.5	3.9	332.	-27.7	-28.3	
	109	3.0	3.8	337.	-27.9	-28.3	1018.5
	109	3.5	3.6	335.	-28.1	-28.6	
	109	4.0	3.6	337.	-28.1	-28.6	
	109	4.5	4.0	333.	-27.9	-28.2	
	109	5.0	3.9	329.	-27.9	-28.2	
	109	5.5	3.5	325.	-27.9	-28.2	
	109	6.0	3.7	331.	-27.8	-28.1	1017.5
	109	6.5	3.4	327.	-27.8	-27.9	
	109	7.0	4.1	322.	-28.1	-28.2	
	109	7.5	3.9	322.	-27.6	-27.7	
	109	8.0	3.7	323.	-27.6	-27.5	
	109	8.5	3.7	320.	-27.5	-27.6	

	109	9.0	3.8	3.1	328.	-27.3	-27.1	1016.9
	109	9.5	3.7	3.0	334.	-27.2	-27.0	
	109	10.0	3.6	3.0	337.	-27.2	-27.1	
	109	10.5	3.2	2.6	333.	-27.3	-27.2	
	109	11.0	3.2	2.6	317.	-27.8	-27.4	
	109	11.5	3.3	2.6	309.	-27.2	-26.9	
	109	12.0	3.5	2.9	307.	-26.1	-25.8	1016.6
	109	12.5	3.5	2.9	307.	-26.3	-26.1	
	109	13.0	3.8	3.2	318.	-26.4	-26.3	
	109	13.5	3.4	2.9	320.	-26.5	-26.4	
	109	14.0	3.2	2.8	323.	-26.5	-26.5	
	109	14.5	3.1	2.7	323.	-26.9	-26.9	
	109	15.0	3.1	2.7	322.	-26.9	-26.9	1016.4
	109	15.5	3.1	2.6	319.	-27.3	-27.2	
	109	16.0	3.3	2.8	320.	-27.1	-27.0	
	109	16.5	3.5	3.0	319.	-26.9	-26.7	
	109	17.0	3.7	3.1	320.	-27.2	-27.2	
	109	17.5	3.7	3.2	320.	-25.9	-25.9	
	109	18.0	3.6	3.0	320.	-27.1	-27.0	1016.5
	109	18.5	3.5	3.0	321.	-26.7	-26.7	
	109	19.0	3.3	2.8	321.	-26.7	-26.7	
	109	19.5	3.3	2.6	317.	-26.6	-26.6	
	109	20.0	3.1	2.4	317.	-26.6	-26.6	
	109	20.5	3.2	2.6	321.	-26.0	-26.2	
	109	21.0	3.3	2.8	322.	-25.8	-26.1	1016.9
	109	21.5	3.5	2.9	322.	-19.1	-19.8	
	109	22.0	3.5	2.7	320.	-23.5	-19.6	
	109	22.5	3.7	2.8	315.	-26.6	-26.7	
	109	23.0	3.9	2.9	316.	-26.7	-27.1	
	109	23.5	3.9	3.2	320.	-26.7	-26.8	
APRIL 20	110	.0	3.9	3.3	323.	-26.7	-26.9	1017.5
	110	.5	3.7	3.0	321.	-26.8	-27.1	
	110	1.0	4.1	3.5	322.	-26.8	-27.1	
	110	1.5						
	110	2.0						
	110	2.5						
	110	3.0						1018.0
	110	3.5						
	110	4.0						
	110	4.5						
	110	5.0						
	110	5.5						
	110	6.0						1018.5
	110	6.5						
	110	7.0						
	110	7.5	5.1	4.0	314.	-27.2	-26.9	
	110	8.0	5.3	4.3	311.	-26.9	-26.6	
	110	8.5	5.3	4.3	311.	-26.8	-26.3	
	110	9.0	5.3	4.2	309.	-26.9	-26.5	1019.0
	110	9.5	5.4	4.3	311.	-26.5	-26.1	
	110	10.0	5.6	4.7	311.	-27.2	-26.7	
	110	10.5	5.4	4.5	309.	-26.7	-26.3	
	110	11.0	5.2	4.1	304.	-26.5	-26.0	
	110	11.5	4.9	3.6	302.	-26.2	-25.7	
	110	12.0	5.3	4.2	304.	-26.9	-26.4	1019.6
	110	12.5	5.4	3.7	296.	-26.5	-26.1	

	110	13.0	5.7	3.9	297.	-26.6	-26.2	
	110	13.5	5.8	3.9	296.	-26.6	-26.3	
	110	14.0	5.7	4.2	299.	-27.1	-26.8	
	110	14.5	5.5	3.9	297.	-26.5	-26.2	
	110	15.0	5.5	4.1	300.	-27.2	-27.0	1019.7
	110	15.5	5.4	4.0	298.	-27.4	-27.2	
	110	16.0	5.6	4.2	299.	-26.8	-26.5	
	110	16.5	5.8	4.3	299.	-26.1	-25.9	
	110	17.0	5.8	4.4	300.	-26.9	-26.7	
	110	17.5	5.3	3.7	297.	-26.5	-26.4	
	110	18.0	5.2	3.5	295.	-27.5	-27.3	1019.7
	110	18.5	5.7	3.8	295.	-26.8	-26.7	
	110	19.0	5.7	3.8	294.	-26.4	-26.4	
	110	19.5	6.1	4.0	295.	-26.8	-26.8	
	110	20.0	5.7	3.8	294.	-27.7	-27.7	
	110	20.5	6.0	3.9	295.	-26.9	-27.0	
	110	21.0	5.9	3.8	296.	-27.6	-27.8	1019.5
	110	21.5	5.8	3.8	296.	-24.9	-25.0	
	110	22.0	6.1	4.1	295.	-27.4	-27.6	
	110	22.5	6.0	3.9	297.	-27.4	-27.5	
	110	23.0	5.9	3.9	300.	-27.4	-27.6	
	110	23.5	6.1	4.2	303.	-27.5	-27.6	
APRIL 21	111	0	5.7	3.8	299.	-27.5	-27.7	1019.4
	111	.5	5.3	3.4	301.	-27.6	-27.8	
	111	1.0	5.0	3.3	302.	-27.7	-27.8	
	111	1.5	5.3	3.5	301.	-27.8	-27.9	
	111	2.0	5.2	3.6	306.	-27.8	-27.9	
	111	2.5	5.2	3.4	301.	-27.9	-28.0	
	111	3.0	5.3	3.6	301.	-27.9	-28.0	1018.7
	111	3.5	5.3	3.5	303.	-27.9	-28.0	
	111	4.0	5.7	3.7	300.	-27.9	-27.9	
	111	4.5	5.4	3.6	300.	-27.8	-27.8	
	111	5.0	5.3	3.4	301.	-27.6	-27.6	
	111	5.5	5.0	3.4	298.	-27.3	-27.3	
	111	6.0	5.1	3.6	297.	-27.2	-27.2	1018.2
	111	6.5	5.0	3.8	292.	-27.2	-27.1	
	111	7.0	5.6	4.0	299.	-27.3	-27.2	
	111	7.5	5.6	3.7	300.	-27.2	-26.9	
	111	8.0	5.1	3.9	294.	-26.8	-26.6	
	111	8.5	4.2	3.6	283.	-26.9	-26.6	
	111	9.0	5.3	4.0	294.	-26.4	-26.1	1018.1
	111	9.5	4.8	4.0	284.	-26.4	-26.1	
	111	10.0	4.4	3.9	276.	-27.1	-26.8	
	111	10.5	4.7	4.2	279.	-26.2	-25.9	
	111	11.0	4.8	4.3	278.	-26.4	-26.0	
	111	11.5	4.7	4.2	280.	-26.0	-25.7	
	111	12.0	4.7	4.1	281.	-25.7	-25.4	1018.0
	111	12.5	5.0	4.3	281.	-26.1	-25.8	
	111	13.0	5.4	4.3	290.	-26.8	-26.6	
	111	13.5	5.6	4.0	297.	-26.5	-27.0	
	111	14.0	5.4	3.7	301.	-25.9	-25.8	
	111	14.5	5.6	4.0	296.	-26.5	-26.3	
	111	15.0	5.3	4.2	290.	-25.7	-25.7	1017.7
	111	15.5	5.1	4.4	282.	-25.8	-25.8	
	111	16.0	5.0	4.2	285.	-25.6	-25.5	
	111	16.5	5.0	4.3	283.	-25.8	-25.6	

	111	17.0	5.0	4.3	281.	-25.9	-25.8	
	111	17.5	5.4	4.4	286.	-25.5	-25.5	
	111	18.0	5.5	4.8	280.	-25.7	-25.6	1017.5
	111	18.5	6.0	5.2	282.	-26.6	-26.5	
	111	19.0	5.8	5.0	283.	-26.8	-26.8	
	111	19.5	5.6	4.9	281.	-27.6	-28.3	
	111	20.0	6.3	5.0	288.	-27.9	-28.6	
	111	20.5	6.1	4.9	287.	-25.5	-25.6	
	111	21.0	5.5	4.7	284.	-25.9	-26.1	1017.3
	111	21.5	5.9	4.9	286.	-24.9	-25.1	
	111	22.0	6.9	5.3	292.	-20.7	-20.8	
	111	22.5						
	111	23.0	6.6	4.8	295.	-26.4	-26.7	
	111	23.5	6.8	5.1	293.	-26.6	-26.8	
APRIL 22	112	.0	6.8	5.0	295.	-26.6	-26.8	1017.0
	112	.5	6.8	4.8	298.	-26.6	-26.8	
	112	1.0	6.8	4.6	299.	-26.7	-26.9	
	112	1.5						
	112	2.0	7.3	5.3	298.	-26.9	-27.1	
	112	2.5	6.8	5.0	296.	-26.9	-27.1	
	112	3.0	6.6	4.8	297.	-26.9	-27.2	1016.6
	112	3.5	7.0	4.9	298.	-27.0	-27.2	
	112	4.0	6.9	4.8	300.	-26.9	-27.1	
	112	4.5	7.2	5.1	299.	-26.9	-27.0	
	112	5.0	6.9	4.9	299.	-26.8	-26.9	
	112	5.5	6.8	5.1	293.	-26.7	-26.8	
	112	6.0	6.8	5.3	294.	-26.7	-26.7	1016.0
	112	6.5	6.8	5.1	294.	-26.6	-26.7	
	112	7.0	6.8	5.1	295.	-27.0	-26.9	
	112	7.5	6.6	4.6	301.	-26.4	-26.3	
	112	8.0	6.4	4.5	300.	-26.3	-26.2	
	112	8.5	6.1	4.5	298.	-26.1	-26.0	
	112	9.0	6.0	4.7	292.	-26.6	-26.3	1015.9
	112	9.5	5.7	5.0	286.	-26.0	-25.7	
	112	10.0	5.8	5.2	283.	-26.2	-25.9	
	112	10.5	5.5	4.7	285.	-26.2	-26.7	
	112	11.0	5.4	4.8	284.	-25.1	-25.6	
	112	11.5	5.7	5.1	280.	-26.1	-26.6	
	112	12.0	5.1	4.5	284.	-26.7	-27.3	1015.8
	112	12.5	5.4	4.8	286.	-25.6	-25.3	
	112	13.0	5.6	4.9	286.	-26.4	-26.1	
	112	13.5	5.6	5.0	284.	-26.4	-27.0	
	112	14.0	5.6	5.0	285.	-25.8	-26.3	
	112	14.5	5.4	4.8	284.	-26.4	-27.0	
	112	15.0	5.1	4.5	284.	-25.6	-26.5	1014.9
	112	15.5	4.6	4.0	282.	-25.6	-27.1	
	112	16.0						
	112	16.5						
	112	17.0						
	112	17.5						
	112	18.0						1014.4
	112	18.5						
	112	19.0						
	112	19.5						
	112	20.0						
	112	20.5						

	112	21.0						1014.0
	112	21.5						
	112	22.0						
	112	22.5						
	112	23.0						
	112	23.5						
APRIL 23	113	.0						1013.5
	113	.5	3.1	2.1	249.	-27.2	-28.0	
	113	1.0	3.2	2.1	249.	-27.3	-28.1	
	113	1.5	3.1	2.0	246.	-27.4	-28.4	
	113	2.0	3.0	1.8	241.	-27.3	-28.6	
	113	2.5	3.0	1.9	252.	-26.9	-28.1	
	113	3.0	2.9	1.8	243.	-27.2	-28.5	1013.5
	113	3.5	3.1	1.9	237.	-27.3	-28.6	
	113	4.0	2.8	1.6	240.	-27.2	-28.6	
	113	4.5	2.5	1.5	243.	-27.2	-28.4	
	113	5.0	2.4	1.5	246.	-27.1	-28.1	
	113	5.5	2.3	1.4	241.	-26.9	-28.0	
	113	6.0	2.3	1.5	245.	-26.6	-27.6	1013.2
	113	6.5	2.5	1.5	241.	-26.3	-27.5	
	113	7.0	2.6	1.7	246.	-26.6	-27.1	
	113	7.5	2.2	1.4	235.	-26.1	-26.7	
	113	8.0	2.2	1.4	244.	-25.7	-26.2	
	113	8.5	2.1	1.4	240.	-25.4	-26.0	
	113	9.0	2.0	1.3	241.	-25.1	-25.6	1013.3
	113	9.5	2.2	1.4	239.	-24.6	-25.2	
	113	10.0	2.3	1.5	239.	-22.9	-23.3	
	113	10.5	2.1	1.3	238.	-22.8	-23.3	
	113	11.0	2.0	1.3	228.	-23.5	-24.3	
	113	11.5	2.2	1.4	236.	-23.9	-24.7	
	113	12.0	2.4	1.6	232.	-24.0	-24.7	1013.5
	113	12.5	2.7	1.9	235.	-23.1	-23.3	
	113	13.0	2.7	1.9	235.	-22.8	-23.1	
	113	13.5	2.3	1.4	236.	-22.6	-23.3	
	113	14.0	2.1	1.2	228.	-22.6	-23.4	
	113	14.5	2.2	1.4	228.	-22.4	-23.2	
	113	15.0	2.2	1.4	225.	-23.2	-24.3	1013.7
	113	15.5	2.0	1.2	237.	-32.8	-37.4	
	113	16.0	1.9	1.2	242.	-21.6	-22.2	
	113	16.5	1.6	.8	249.	-21.8	-22.3	
	113	17.0	1.2	.6	238.	-22.5	-23.2	
	113	17.5	1.1	1.1	133.	-22.0	-22.8	
	113	18.0	1.4	1.2	136.	-19.7	-21.3	1013.7
	113	18.5	1.8	1.4	136.	-22.1	-23.2	
	113	19.0	2.3	1.7	146.	-22.1	-23.5	
	113	19.5	2.1	1.5	125.	-22.9	-23.8	
	113	20.0	2.3	1.6	133.		-25.5	
	113	20.5	2.4	1.7	140.		-25.2	
	113	21.0	2.2	1.5	126.		-25.7	1014.4
	113	21.5	2.5	1.7	130.		-26.0	
	113	22.0	2.7	1.9	123.		-27.1	
	113	22.5						
	113	23.0						
	113	23.5	2.6	1.8	118.	-25.2	-26.3	
APRIL 24	114	.0	2.6	1.8	119.	-25.1	-26.2	1014.6
	114	.5	2.6	1.9	116.	-25.3	-26.2	

114	1.0	3.0	2.1	121.	-25.3	-26.2		
114	1.5	3.1	2.2	126.	-25.6	-26.3		
114	2.0	2.5	1.7	110.	-25.5	-26.4		
114	2.5							
114	3.0						1014.8	
114	3.5							
114	4.0							
114	4.5	2.9	2.1	116.	-25.5	-26.0		
114	5.0	2.9	2.1	116.	-25.5	-26.0		
114	5.5	2.7	2.0	119.	-25.5	-25.8		
114	6.0	2.3	1.7	104.	-25.5	-25.8	1015.2	
114	6.5	2.4	1.8	104.	-25.3	-25.5		
114	7.0	2.4	1.9	105.	-26.0	-25.9		
114	7.5	2.3	1.8	95.	-25.2	-25.1		
114	8.0	2.6	2.0	106.	-25.5	-25.4		
114	8.5	2.3	1.8	103.	-25.5	-25.3		
114	9.0	2.4	1.8	103.	-25.1	-24.8	1016.3	
114	9.5	2.3	1.7	112.	-24.8	-24.5		
114	10.0	2.2	1.8	97.	-24.2	-24.0		
114	10.5	2.3	1.8	95.	-24.7	-24.3		
114	11.0	2.2	1.7	93.	-24.4	-24.0		
114	11.5	2.3	1.9	87.	-24.2	-23.9		
114	12.0	2.6	2.0	98.	-24.2	-23.8	1017.3	
114	12.5	2.7	2.3	107.	-23.8	-23.4		
114	13.0	2.5	2.1	106.	-23.3	-22.9		
114	13.5	2.0	1.6	97.	-23.6	-23.3		
114	14.0	2.2	1.7	99.	-23.0	-22.8		
114	14.5	2.2	1.8	93.	-23.6	-23.3		
114	15.0	2.2	1.7	102.	-23.5	-23.3	1018.0	
114	15.5	2.1	1.6	108.	-23.4	-23.3		
114	16.0	2.1	1.6	105.	-23.3	-23.2		
114	16.5	1.8	1.3	97.	-22.6	-22.7		
114	17.0	2.0	1.4	100.	-22.4	-22.6		
114	17.5	1.8	1.3	105.	-22.5	-22.7		
114	18.0	1.7	1.3	98.	-23.5	-23.9	1018.6	
114	18.5	1.5	1.3	65.	-22.7	-23.4		
114	19.0	1.3	1.2	61.	-23.4	-24.2		
114	19.5	1.8	1.5	55.	-23.7	-24.3		
114	20.0	1.8	1.4	54.	-24.4	-25.0		
114	20.5	1.7	1.4	49.	-24.3	-25.2		
114	21.0	1.7	1.2	59.	-24.2	-25.2	1019.7	
114	21.5	1.8	1.1	61.	-24.6	-25.9		
114	22.0	1.9	1.3	57.	-24.5	-25.9		
114	22.5	2.1	1.6	50.	-24.8	-26.0		
114	23.0	1.8	1.1	63.	-25.1	-26.2		
114	23.5							
APRIL 25	115	0	1.9	1.2	96.	-23.7	-25.3	1020.5
	115	.5	1.7	1.0	110.	-23.8	-25.1	
	115	1.0	1.5	1.0	97.	-24.3	-25.3	
	115	1.5	1.4	1.1	67.	-24.5	-25.8	
	115	2.0	1.4	1.5	45.	-25.0	-26.4	
	115	2.5	1.8	1.4	49.	-25.4	-26.9	
	115	3.0	1.8	1.4	48.	-25.8	-27.2	1020.9
	115	3.5	1.7	1.3	51.	-25.8	-27.2	
	115	4.0	1.4	1.0	80.	-25.3	-26.4	
	115	4.5	1.2	1.0	69.	-24.8	-25.9	

115	5.0	1.1	1.3	49.	-25.1	-26.2	
115	5.5	1.5	1.2	59.	-25.4	-26.4	
115	6.0	1.7	1.3	60.	-24.8	-25.8	1021.4
115	6.5	1.6	1.3	54.	-24.9	-25.7	
115	7.0	1.6	1.3	51.	-25.8	-26.5	
115	7.5	1.8	1.4	66.	-24.6	-25.1	
115	8.0	2.0	1.4	87.	-23.7	-23.9	
115	8.5	2.5	1.9	105.	-21.9	-21.9	
115	9.0	2.3	1.8	110.	-23.4	-23.1	1021.9
115	9.5	2.1	1.6	119.	-22.8	-22.5	
115	10.0	1.9	1.6	105.	-23.9	-23.6	
115	10.5	2.1	1.7	104.	-23.8	-23.4	
115	11.0	2.2	1.8	105.	-23.3	-23.0	
115	11.5	2.3	1.8	107.	-23.3	-23.0	
115	12.0	2.2	1.9	107.	-23.1	-22.7	1022.4
115	12.5	2.2	1.8	105.	-22.7	-22.5	
115	13.0	2.0	1.7	102.	-23.3	-23.0	
115	13.5	2.1	1.8	103.	-23.0	-22.7	
115	14.0	2.2	1.8	100.	-23.0	-22.8	
115	14.5	2.2	1.8	105.	-22.8	-22.6	
115	15.0	2.2	1.8	100.	-22.7	-22.6	1022.2
115	15.5	2.3	2.0	111.	-22.3	-22.1	
115	16.0	1.9	1.6	113.	-22.4	-22.3	
115	16.5	2.1	1.7	106.	-23.0	-22.9	
115	17.0	2.0	1.7	116.	-23.2	-23.1	
115	17.5	2.2	1.8	110.	-23.3	-23.3	
115	18.0	2.1	1.7	121.	-23.3	-23.3	1021.5
115	18.5	2.0	1.5	110.	-23.0	-23.1	
115	19.0	2.0	1.5	115.	-23.1	-23.2	
115	19.5	2.1	1.5	119.	-23.2	-23.4	
115	20.0	2.1	1.5	123.	-23.3	-23.7	
115	20.5	2.2	1.6	119.	-24.1	-24.9	
115	21.0	2.1	1.5	111.	-23.1	-23.9	1021.4
115	21.5	2.2	1.5	120.	-19.6	-21.1	
115	22.0	2.3	1.6	121.	-23.3	-24.4	
115	22.5	2.3	1.6	138.	-23.4	-24.6	
115	23.0	2.0	1.5	129.	-23.7	-24.7	
115	23.5	1.7	1.2	106.	-24.0	-25.0	
APRIL 26	116 .0	2.0	1.3	109.	-24.0	-25.0	1021.0
	116 .5						
	116 1.0	2.7	1.8	127.	-23.4	-25.2	
	116 1.5	2.2	1.3	132.	-23.8	-25.2	
	116 2.0	1.9	1.2	130.	-23.7	-25.5	
	116 2.5	1.9	1.4	130.	-23.8	-24.8	
	116 3.0						1020.5
	116 3.5						
	116 4.0						
	116 4.5						
	116 5.0						
	116 5.5						
	116 6.0						1020.1
	116 6.5						
	116 7.0	1.6	1.3	126.	-25.0	-25.6	
	116 7.5	1.5	1.2	127.	-23.9	-24.4	
	116 8.0	1.1	.9	130.	-23.5	-24.3	
	116 8.5	.8	.9	117.	-23.1	-23.3	

116	9.0	1.1	1.1	102.	-22.5	-22.7	1020.5
116	9.5	1.4	1.2	109.	-22.8	-22.8	
116	10.0	1.5	1.3	130.	-22.2	-22.2	
116	10.5	1.9	1.6	128.	-22.5	-22.4	
116	11.0	1.4	1.1	126.	-22.6	-22.6	
116	11.5	1.2	.9	125.	-21.9	-21.9	
116	12.0	1.3	1.1	134.	-22.5	-22.6	1020.5
116	12.5	1.0	.8	106.	-21.6	-21.5	
116	13.0	1.0	.9	120.	-21.6	-21.5	
116	13.5	.9	.9	119.	-21.5	-21.3	
116	14.0	1.1	1.0	122.	-22.1	-21.9	
116	14.5	.9	.8	114.	-22.0	-21.9	
116	15.0	1.1	1.0	96.	-21.8	-21.9	1020.6
116	15.5	1.0	.9	97.	-21.9	-22.1	
116	16.0	1.0	.9	111.	-21.1	-21.2	
116	16.5	.9	.7	79.	-21.2	-21.2	
116	17.0	.9	.9	51.	-21.7	-22.0	
116	17.5	1.2	1.2	55.	-23.0	-23.7	
116	18.0	1.2	1.0	56.	-21.9	-22.4	1020.7
116	18.5	1.5	1.3	49.	-22.1	-22.7	
116	19.0	2.0	1.4	50.	-22.0	-22.5	
116	19.5	1.7	1.3	43.	-22.0	-22.6	
116	20.0	1.7	1.3	44.	-22.7	-23.6	
116	20.5	1.9	1.4	50.	-22.1	-22.9	
116	21.0						1021.4
116	21.5						
116	22.0						
116	22.5						
116	23.0	1.3	1.1	29.	-22.3	-23.1	
116	23.5	1.2	1.0	22.	-22.9	-23.8	
APRIL 27	117 .0	1.2	1.0	15.	-22.4	-23.3	1021.4
	117 .5	.9	.7	12.	-22.5	-23.7	
	117 1.0	.8	.6	25.	-22.5	-23.6	
	117 1.5	.7	.5	355.	-22.5	-23.6	
	117 2.0						
	117 2.5						
	117 3.0						1021.0
	117 3.5						
	117 4.0						
	117 4.5	.5	.4	112.	-28.2	-29.7	
	117 5.0	.6	.3	106.	-22.3	-23.7	
	117 5.5	.5	.4	130.	-22.0	-23.1	
	117 6.0	.5	.6	218.	-21.7	-23.0	1020.5
	117 6.5	.7	.5	241.	-21.9	-23.0	
	117 7.0	.8	.6	259.	-22.8	-23.6	
	117 7.5	.4	.3	278.	-21.3	-22.3	
	117 8.0	.4	.5	272.	-22.2	-23.3	
	117 8.5	.3	.3	279.	-21.4	-22.3	
	117 9.0	.3	.3	273.	-21.2	-22.0	1019.6
	117 9.5	.7	.7	130.	-21.0	-21.7	
	117 10.0	.7	.5	144.	-21.5	-21.9	
	117 10.5	1.0	.7	144.	-20.7	-21.5	
	117 11.0	1.0	.7	126.	-20.8	-21.1	
	117 11.5	1.2	1.2	120.	-21.1	-21.2	
	117 12.0	1.6	1.5	127.	-21.9	-22.2	1018.2
	117 12.5	1.9	1.6	128.	-22.3	-22.5	

	117	13.0	1.8	1.5	137.	-21.2	-21.3	
	117	13.5	2.1	1.7	130.	-21.3	-21.5	
	117	14.0	2.1	1.7	132.	-21.9	-22.1	
	117	14.5	2.3	1.9	139.	-21.6	-21.9	
	117	15.0	2.3	1.9	140.	-21.5	-21.8	1016.5
	117	15.5	2.2	1.8	141.	-21.2	-21.4	
	117	16.0	2.1	1.8	123.	-21.8	-22.0	
	117	16.5	2.4	1.9	110.	-21.5	-21.5	
	117	17.0	2.7	2.2	115.	-22.2	-22.3	
	117	17.5	3.0	2.4	117.	-22.3	-22.4	
	117	18.0	2.8	2.3	123.	-22.2	-22.4	1014.5
	117	18.5	2.8	2.1	119.	-21.7	-22.0	
	117	19.0	3.0	2.4	109.	-21.9	-22.1	
	117	19.5	3.0	2.2	111.	-22.4	-22.7	
	117	20.0	3.1	2.3	112.	-22.4	-22.9	
	117	20.5	3.5	2.7	115.	-22.2	-23.0	
	117	21.0	3.4	2.5	117.	-22.3	-22.8	1013.6
	117	21.5	3.4	2.6	124.	-22.5	-23.5	
	117	22.0	3.6	2.7	125.	-22.6	-23.6	
	117	22.5	3.3	2.4	111.	-22.9	-23.4	
	117	23.0	3.6	2.7	107.	-17.0	-28.4	
	117	23.5	3.9	3.0	110.	-13.1	-32.1	
APRIL 28	118	.0	4.1	3.2	109.	-22.4	-22.8	1012.9
	118	.5	4.2	3.3	111.	-22.3	-22.7	
	118	1.0	4.0	3.1	111.	-22.2	-22.6	
	118	1.5	4.1	3.2	104.	-22.2	-22.7	
	118	2.0	4.1	3.2	108.	-22.1	-22.6	
	118	2.5	4.1	3.2	107.	-22.2	-22.7	
	118	3.0	3.9	3.0	109.	-22.2	-22.7	1013.0
	118	3.5	4.0	3.0	101.	-22.0	-22.6	
	118	4.0	4.1	3.2	103.	-21.7	-22.2	
	118	4.5	3.4	2.5	102.	-21.6	-22.1	
	118	5.0	3.5	2.6	100.	-21.9	-22.4	
	118	5.5	3.5	2.6	99.	-21.6	-22.1	
	118	6.0	3.6	2.8	93.	-21.2	-21.6	1014.3
	118	6.5	3.9	3.1	90.	-21.1	-21.5	
	118	7.0	4.3	3.4	90.	-21.2	-21.7	
	118	7.5	4.1	3.2	89.	-20.1	-20.5	
	118	8.0	3.3	2.7	76.	-20.5	-20.8	
	118	8.5	3.3	2.7	75.	-20.7	-20.9	
	118	9.0	3.3	2.7	73.	-20.6	-20.7	1016.1
	118	9.5	3.3	2.8	71.	-20.5	-20.6	
	118	10.0	3.6	3.1	70.	-20.5	-20.5	
	118	10.5	3.8	3.2	67.	-20.8	-20.9	
	118	11.0	3.4	2.9	63.	-20.6	-20.8	
	118	11.5	3.2	2.7	53.	-20.3	-20.2	
	118	12.0	3.3	2.8	49.	-20.5	-21.6	1017.8
	118	12.5	3.3	2.8	46.	-20.8	-20.8	
	118	13.0	3.4	2.8	46.	-20.2	-20.2	
	118	13.5	3.5	3.0	40.	-20.1	-20.1	
	118	14.0	3.8	3.3	38.	-20.6	-20.6	
	118	14.5	3.7	3.0	34.	-20.5	-21.2	
	118	15.0	3.6	3.0	25.	-20.5	-20.6	1019.6
	118	15.5	3.5	2.9	19.	-20.4	-20.6	
	118	16.0	3.6	3.0	16.	-20.4	-20.6	
	118	16.5	3.7	3.1	14.	-20.7	-21.0	

	118	17.0							
	118	17.5	3.7	3.0	10.		-20.7		
	118	18.0	3.8	3.0	8.		-20.5	1021.3	
	118	18.5	3.8	3.1	10.		-19.9		
	118	19.0	3.5	2.7	10.		-20.1		
	118	19.5	3.4	2.5	9.		-20.3		
	118	20.0	3.2	2.4	2.		-20.5		
	118	20.5							
	118	21.0						1023.5	
	118	21.5	3.9	3.0	347.	-18.4	-19.2		
	118	22.0	3.9	2.9	350.	-21.3	-21.8		
	118	22.5	3.8	2.7	356.	-21.4	-22.0		
	118	23.0	3.6	2.5	356.	-21.7	-22.4		
	118	23.5	3.6	2.5	351.	-21.9	-22.6		
APRIL 29	119	.0	3.5	2.5	341.	-21.8	-22.4	1025.5	
	119	.5	3.5	2.6	336.	-21.8	-22.4		
	119	1.0	4.0	2.9	343.	-21.8	-22.3		
	119	1.5	3.8	2.8	348.	-21.9	-22.2		
	119	2.0	3.7	2.8	338.	-21.9	-22.3		
	119	2.5	3.7	2.7	336.	-21.8	-22.2		
	119	3.0	3.4	2.5	336.	-21.8	-22.3	1026.9	
	119	3.5	3.6	2.6	329.	-22.0	-22.2		
	119	4.0	3.8	2.7	323.	-22.1	-22.1		
	119	4.5	4.0	2.9	321.	-21.9	-21.9		
	119	5.0	4.0	3.0	316.	-22.0	-22.0		
	119	5.5	4.4	3.5	317.	-22.0	-21.7		
	119	6.0	4.6	3.7	315.	-22.0	-21.8	1028.3	
	119	6.5	5.0	4.0	314.	-22.1	-21.8		
	119	7.0	5.2	4.1	315.	-22.8	-22.6		
	119	7.5	5.3	4.3	316.	-22.2	-22.0		
	119	8.0	5.6	4.6	317.	-22.1	-21.7		
	119	8.5	5.7	4.5	314.	-22.1	-21.8		
	119	9.0	5.5	4.5	316.	-22.1	-21.8	1029.4	
	119	9.5	5.3	4.3	320.	-22.0	-21.5		
	119	10.0	5.6	4.6	319.	-22.5	-22.1		
	119	10.5	5.6	4.6	318.	-22.3	-22.0		
	119	11.0	5.4	4.4	317.	-22.3	-22.0		
	119	11.5	5.8	4.7	316.	-22.4	-22.0		
	119	12.0	5.6	4.5	316.	-22.5	-22.2	1030.5	
	119	12.5	6.0	4.8	317.	-21.9	-21.6		
	119	13.0	5.8	4.6	315.	-22.0	-21.7		
	119	13.5	5.8	4.7	317.	-22.1	-21.8		
	119	14.0	6.2	5.0	317.	-22.6	-22.3		
	119	14.5	5.8	4.5	314.	-22.6	-22.3		
	119	15.0	5.9	4.5	314.	-22.1	-21.9	1030.5	
	119	15.5	6.1	4.7	314.	-22.2	-22.0		
	119	16.0	6.2	4.9	317.	-22.8	-22.6		
	119	16.5	6.3	4.9	316.	-22.8	-22.7		
	119	17.0	6.4	4.9	316.	-22.7	-22.6		
	119	17.5	6.2	4.8	317.	-22.2	-22.1		
	119	18.0	6.2	5.0	320.	-22.2	-22.1	1030.5	
	119	18.5	6.2	4.8	317.	-22.2	-22.2		
	119	19.0	6.0	4.7	319.	-22.7	-22.6		
	119	19.5	5.8	4.7	320.	-22.6	-22.6		
	119	20.0	5.6	4.5	320.	-22.1	-22.1		
	119	20.5	5.6	4.6	324.	-23.1	-23.3		

		119	21.0	5.4	4.3	326.	-22.2	-22.2	1031.0
		119	21.5						
		119	22.0						
		119	22.5						
		119	23.0						
		119	23.5	4.6	3.6	321.	-22.8	-22.9	
APRIL	30	120	.0	4.5	3.5	321.	-22.9	-23.1	1031.3
		120	.5	4.6	3.5	319.	-23.2	-23.3	
		120	1.0	4.6	3.6	319.	-23.4	-23.5	
		120	1.5	4.7	3.4	317.	-23.5	-23.7	
		120	2.0	4.7	3.6	318.	-23.6	-23.8	
		120	2.5	4.9	3.8	319.	-23.8	-23.9	
		120	3.0	4.7	3.7	319.	-24.0	-24.0	1031.3
		120	3.5	4.6	3.4	317.	-24.0	-24.1	
		120	4.0	4.5	3.6	318.	-24.0	-24.0	
		120	4.5	4.6	3.5	316.	-24.0	-24.0	
		120	5.0	4.6	3.6	317.	-24.0	-23.9	
		120	5.5	4.6	3.7	321.	-23.9	-23.7	
		120	6.0	4.4	3.5	317.	-23.6	-23.4	1031.6
		120	6.5	4.7	3.8	321.	-23.4	-23.2	
		120	7.0	4.6	3.7	322.	-23.8	-23.6	
		120	7.5	4.4	3.5	322.	-23.0	-22.8	
		120	8.0	4.1	3.4	317.	-22.9	-22.6	
		120	8.5	4.3	3.4	314.	-22.8	-22.6	
		120	9.0	4.3	3.6	320.	-23.3	-23.1	1032.5
		120	9.5	5.1	4.1	325.	-23.2	-23.0	
		120	10.0	4.8	4.0	329.	-23.0	-23.0	
		120	10.5	4.4	3.6	333.	-23.9	-36.8	
		120	11.0	4.3	3.7	337.	-22.8	-22.7	
		120	11.5	4.9	4.3	341.	-22.9	-22.8	
		120	12.0	5.2	4.4	337.	-23.1	-22.9	1033.5
		120	12.5	4.5	3.9	340.	-22.5	-22.3	
		120	13.0	4.2	3.6	338.	-23.0	-22.7	
		120	13.5	4.4	3.7	334.	-22.4	-22.2	
		120	14.0	4.7	4.0	336.	-23.0	-22.8	
		120	14.5	4.4	3.6	332.	-22.2	-22.1	
		120	15.0	4.3	3.6	333.	-22.7	-22.6	1034.4
		120	15.5	4.3	3.7	339.	-22.8	-22.8	
		120	16.0	4.4	3.7	336.	-22.5	-22.5	
		120	16.5	4.4	3.6	333.	-22.5	-22.4	
		120	17.0	4.7	4.0	334.	-22.6	-22.5	
		120	17.5	4.4	3.6	335.	-22.1	-22.0	
		120	18.0	4.3	3.6	339.	-22.6	-22.5	1035.5
		120	18.5	4.1	3.4	339.	-22.1	-22.0	
		120	19.0	4.0	3.3	335.	-22.1	-22.0	
		120	19.5	3.8	3.1	333.	-22.2	-22.2	
		120	20.0	3.8	3.0	330.	-22.3	-22.2	
		120	20.5	3.6	2.9	333.	-23.2	-23.3	
		120	21.0	3.6	2.8	333.	-23.2	-23.5	1037.1
		120	21.5	3.7	2.8	328.	-23.3	-23.6	
		120	22.0	4.2	3.2	333.	-22.6	-22.8	
		120	22.5	4.2	3.4	339.	-22.7	-23.0	
		120	23.0						
		120	23.5	4.0	3.0	328.	-22.8	-23.2	
MAY	1	121	.0	4.2	3.2	325.	-22.8	-23.0	1037.9
		121	.5	3.9	2.9	325.	-22.9	-23.1	

121	1.0	3.7	2.8	323.	-23.0	-23.2	
121	1.5	3.8	2.8	317.	-23.1	-23.2	
121	2.0	3.8	2.8	316.	-23.1	-23.2	
121	2.5	3.7	2.6	315.	-23.1	-23.2	
121	3.0	3.6	2.7	320.	-23.2	-23.1	1038.5
121	3.5	3.6	2.7	317.	-23.4	-23.4	
121	4.0	3.9	2.9	317.	-23.4	-23.3	
121	4.5	4.0	3.0	317.	-23.3	-23.2	
121	5.0	4.0	2.8	312.	-23.2	-23.1	
121	5.5	4.2	3.0	312.	-22.7	-22.7	
121	6.0	4.4	3.2	313.	-22.8	-22.7	1038.6
121	6.5	4.4	3.3	313.	-22.8	-22.7	
121	7.0	4.2	3.0	304.	-23.1	-23.0	
121	7.5	4.5	3.3	300.	-22.1	-22.0	
121	8.0	4.8	3.4	304.	-21.9	-21.8	
121	8.5	5.0	3.5	304.	-21.9	-21.7	
121	9.0	4.9	3.6	302.	-21.5	-21.5	1038.8
121	9.5	4.6	3.4	300.	-22.1	-22.0	
121	10.0	4.6	3.7	296.	-21.4	-21.4	
121	10.5	4.4	3.6	295.	-21.2	-21.2	
121	11.0	4.5	3.8	290.	-21.6	-21.6	
121	11.5	4.7	4.1	288.	-21.1	-21.1	
121	12.0	4.8	4.1	291.	-21.5	-21.6	1038.4
121	12.5	4.6	3.9	289.	-21.5	-21.4	
121	13.0	4.7	4.1	283.	-21.0	-20.9	
121	13.5	4.4	3.9	274.	-21.4	-21.3	
121	14.0	5.0	4.4	275.	-21.1	-20.9	
121	14.5	5.0	4.4	277.	-21.4	-21.3	
121	15.0	4.8	4.2	273.	-21.5	-21.4	1036.6
121	15.5	4.8	4.1	268.	-21.3	-21.2	
121	16.0	4.5	3.8	267.	-21.4	-21.4	
121	16.5	4.9	4.1	268.	-21.3	-21.2	
121	17.0	5.3	4.6	272.	-21.2	-21.1	
121	17.5	5.5	4.7	273.	-21.2	-21.1	
121	18.0	5.3	4.5	273.	-21.3	-21.2	1034.8
121	18.5	5.4	4.7	276.	-21.1	-21.2	
121	19.0	6.9	6.0	284.	-20.1	-20.2	
121	19.5	5.3	4.6	277.	-20.2	-20.4	
121	20.0	5.2	4.4	273.	-20.2	-20.5	
121	20.5	4.7	3.7	268.	-20.8	-23.3	
121	21.0	5.1	4.2	269.	-19.6	-19.6	1033.0
121	21.5	5.1	4.2	270.	-19.8	-20.1	
121	22.0	5.2	4.3	271.	-21.0	-21.2	
121	22.5	5.7	4.6	272.	-20.9	-21.2	
121	23.0	5.5	4.6	276.	-20.4	-20.6	
121	23.5	5.1	4.1	275.	-20.4	-20.7	
MAY 2	122 .0	5.4	4.5	276.	-20.2	-20.5	1030.9
	122 .5	5.2	4.3	275.	-20.3	-20.6	
	122 1.0	5.2	4.2	273.	-20.3	-20.6	
	122 1.5	5.4	4.4	273.	-20.1	-20.4	
	122 2.0	5.5	4.5	271.	-20.0	-20.2	
	122 2.5	5.6	4.6	270.	-19.8	-20.0	
	122 3.0	5.5	4.4	264.	-19.7	-20.0	1028.5
	122 3.5	5.9	4.9	268.	-19.7	-19.9	
	122 4.0	5.7	4.7	271.	-19.5	-19.7	
	122 4.5	5.3	4.3	270.	-19.2	-19.5	

122	5.0	5.6	4.6	275.	-18.7	-19.0			
122	5.5	6.8	5.9	283.	-18.1	-18.4			
122	6.0	7.1	6.3	287.	-18.0	-18.2	1026.9		
122	6.5	7.1	6.1	290.	-18.2	-18.4			
122	7.0	7.2	5.6	300.	-18.9	-19.2			
122	7.5	7.7	5.6	303.	-18.3	-18.4			
122	8.0	7.7	5.7	303.	-17.8	-17.9			
122	8.5	7.6	5.7	303.	-18.2	-18.2			
122	9.0	7.9	5.7	306.	-17.8	-17.9	1026.0		
122	9.5	7.3	5.3	309.	-18.1	-18.1			
122	10.0	6.4	4.7	312.	-18.3	-18.3			
122	10.5	7.0	5.2	306.	-17.9	-17.9			
122	11.0	6.7	4.9	306.	-18.3	-18.2			
122	11.5	6.3	4.4	308.	-17.6	-17.5			
122	12.0	6.5	4.7	306.	-18.1	-18.0	1025.5		
122	12.5	6.9	4.9	307.	-17.7	-17.5			
122	13.0	6.9	4.9	310.	-17.8	-17.6			
122	13.5	7.1	5.1	307.	-17.4	-17.3			
122	14.0	6.4	4.6	307.	-17.8	-17.7			
122	14.5	6.1	4.4	305.	-17.8	-17.8			
122	15.0	6.2	4.6	305.	-17.5	-17.4	1024.9		
122	15.5	6.5	4.8	305.	-17.0	-16.9			
122	16.0	6.3	4.9	302.	-17.5	-17.4			
122	16.5	5.7	4.0	309.		-19.6			
122	17.0	6.0	4.3	308.		-17.2			
122	17.5	5.9	4.5	306.		-17.1			
122	18.0	5.8	4.2	307.		-17.1	1024.6		
122	18.5	5.5	3.9	307.		-16.7			
122	19.0	5.1	3.8	303.		-16.5			
122	19.5	5.1	3.9	300.		-16.7			
122	20.0	4.9	3.8	298.		-17.2			
122	20.5	5.6	4.0	308.	-15.9	-16.1			
122	21.0	5.6	4.1	306.	-15.8	-16.0	1024.6		
122	21.5	5.5	4.0	306.	-16.1	-16.3			
122	22.0	5.5	4.0	306.	-15.8	-16.1			
122	22.5	5.5	3.9	307.	-16.1	-16.4			
122	23.0	5.3	3.9	305.	-16.1	-16.3			
122	23.5	5.3	3.7	309.	-16.1	-16.3			
MAY	3	123	.0	5.3	3.6	311.	-15.9	-16.1	1024.9
		123	.5	5.4	3.7	312.	-16.8	-17.0	
		123	1.0	4.9	3.3	310.	-16.6	-16.8	
		123	1.5	5.4	3.7	311.	-16.5	-16.7	
		123	2.0	5.3	3.8	316.	-17.2	-17.4	
		123	2.5	4.9	3.5	314.	-16.7	-16.9	
		123	3.0	4.9	3.8	317.	-15.4	-15.5	1025.5
		123	3.5	5.2	4.2	320.	-14.5	-14.6	
		123	4.0	5.7	4.6	321.	-14.0	-14.0	
		123	4.5	5.5	4.5	321.	-13.8	-13.9	
		123	5.0	5.7	4.5	320.	-13.9	-14.0	
		123	5.5	5.8	4.8	322.	-14.0	-14.0	
		123	6.0	5.8	4.8	324.	-13.9	-13.9	1026.8
		123	6.5	5.9	4.9	325.	-13.7	-13.7	
		123	7.0	5.6	4.6	330.	-14.0	-14.0	
		123	7.5	6.1	5.1	335.	-13.7	-13.7	
		123	8.0	6.4	5.4	336.	-14.1	-14.0	
		123	8.5	5.8	5.0	340.	-14.3	-14.3	

123	9.0	5.8	5.0	341.	-14.6	-14.6	1029.3		
123	9.5	6.3	5.5	341.	-14.2	-14.1			
123	10.0	6.8	5.9	344.	-14.3	-14.2			
123	10.5	6.7	5.8	344.	-14.4	-14.5			
123	11.0	6.9	6.1	345.	-14.2	-14.2			
123	11.5	7.6	6.6	347.	-14.7	-14.8			
123	12.0	7.5	6.5	345.	-15.0	-15.3	1031.7		
123	12.5	7.4	6.4	345.	-14.6	-14.7			
123	13.0	7.7	6.7	341.	-15.3	-15.3			
123	13.5	7.3	6.4	343.	-15.4	-15.4			
123	14.0	7.8	6.7	345.	-15.6	-15.6			
123	14.5	7.7	6.8	344.	-16.0	-16.0			
123	15.0	8.0	6.9	347.	-16.6	-16.6	1034.0		
123	15.5	8.1	7.0	352.	-16.9	-17.0			
123	16.0	8.1	7.0	348.	-17.0	-17.0			
123	16.5	8.0	6.9	347.	-17.9	-18.1			
123	17.0	7.3	6.3	347.	-18.4	-18.6			
123	17.5	7.0	6.1	345.	-18.6	-18.7			
123	18.0	6.3	5.5	345.	-18.8	-18.9	1036.8		
123	18.5	6.5	5.6	345.	-18.4	-18.5			
123	19.0	6.2	5.3	343.	-18.6	-18.7			
123	19.5	6.1	5.3	342.	-19.3	-19.5			
123	20.0	5.9	5.0	335.	-19.0	-19.1			
123	20.5	5.8	4.8	334.	-19.1	-19.3			
123	21.0						1038.4		
123	21.5								
123	22.0								
123	22.5								
123	23.0								
123	23.5								
MAY	4	124	.0				1039.4		
		124	.5						
		124	1.0	4.0	3.1	326.	-21.1	-21.3	
		124	1.5	4.0	3.0	327.	-22.0	-22.2	
		124	2.0	4.2	3.1	330.	-21.4	-21.5	
		124	2.5	4.0	2.9	321.	-21.5	-21.6	
		124	3.0	3.8	2.5	311.	-21.5	-21.7	1039.5
		124	3.5	3.6	2.4	307.	-21.3	-21.5	
		124	4.0	3.9	2.6	313.	-21.0	-21.2	
		124	4.5	4.2	2.8	310.	-20.8	-20.9	
		124	5.0	4.7	3.3	312.	-20.7	-20.7	
		124	5.5	4.4	3.0	312.	-20.7	-20.7	
		124	6.0	4.5	3.2	314.	-20.6	-20.6	1039.0
		124	6.5	4.5	3.3	308.	-20.4	-20.4	
		124	7.0	4.6	3.4	306.	-20.3	-20.3	
		124	7.5	4.4	3.3	302.	-20.0	-20.0	
		124	8.0	4.6	3.6	299.	-19.8	-19.8	
		124	8.5	4.2	3.6	292.	-19.7	-19.7	
		124	9.0	4.2	3.7	292.	-19.5	-19.4	1038.0
		124	9.5	3.9	3.4	286.	-19.4	-19.3	
		124	10.0	3.9	3.5	277.	-19.6	-19.4	
		124	10.5	4.0	3.6	276.	-19.5	-19.3	
		124	11.0	4.3	3.8	274.	-19.6	-19.4	
		124	11.5	4.7	4.1	271.	-20.0	-19.8	
		124	12.0	4.7	4.1	271.	-20.0	-19.7	1036.4
		124	12.5	4.8	4.2	272.	-19.9	-19.6	

	124	13.0	4.8	4.2	274.	-19.3	-19.0		
	124	13.5	4.6	4.0	272.	-19.7	-19.5		
	124	14.0	5.0	4.3	270.	-19.6	-19.4		
	124	14.5	4.9	4.2	269.	-19.3	-19.2		
	124	15.0	5.0	4.3	267.	-19.7	-19.6	1034.0	
	124	15.5							
	124	16.0							
	124	16.5							
	124	17.0	4.4	3.8	265.	-19.3	-19.3		
	124	17.5	4.8	4.1	262.	-19.3	-19.3		
	124	18.0	4.9	4.2	261.	-19.2	-19.2	1031.4	
	124	18.5	5.0	4.3	265.	-19.2	-19.3		
	124	19.0	5.0	4.2	260.	-18.8	-18.9		
	124	19.5	5.0	4.2	262.	-18.9	-18.9		
	124	20.0							
	124	20.5							
	124	21.0						1029.3	
	124	21.5							
	124	22.0	4.6	3.8	263.	-18.8	-19.0		
	124	22.5	4.2	3.4	251.	-19.0	-19.2		
	124	23.0	4.0	3.2	253.	-19.5	-19.7		
	124	23.5	4.7	3.9	263.	-18.3	-18.5		
MAY	5	125	.0	4.6	3.9	260.	-18.8	-19.0	1027.2
		125	.5	4.8	4.0	267.	-18.3	-18.4	
		125	1.0	5.1	4.3	272.	-17.9	-18.0	
		125	1.5	4.8	4.0	270.	-17.6	-17.8	
		125	2.0	4.7	3.9	268.	-18.0	-18.1	
		125	2.5	4.7	3.8	268.	-18.2	-18.4	
		125	3.0	4.8	3.9	275.	-18.3	-18.4	1025.9
		125	3.5	4.8	3.8	278.	-18.1	-18.4	
		125	4.0	4.8	4.0	283.	-17.8	-17.9	
		125	4.5	5.0	4.2	286.	-17.2	-17.4	
		125	5.0	5.7	4.9	292.	-16.9	-17.0	
		125	5.5	5.9	4.8	297.	-16.8	-16.8	
		125	6.0	5.8	4.6	300.	-16.8	-16.7	1025.4
		125	6.5	6.0	4.6	303.	-16.9	-16.9	
		125	7.0	6.3	4.6	308.	-16.9	-16.9	
		125	7.5	5.9	4.3	310.	-16.8	-16.8	
		125	8.0	5.5	4.1	317.	-16.8	-16.7	
		125	8.5	5.5	4.2	318.	-16.6	-16.5	
		125	9.0	5.5	4.3	320.	-16.7	-16.6	1026.1
		125	9.5	5.6	4.4	320.	-16.8	-16.6	
		125	10.0	6.0	4.9	325.	-17.1	-16.8	
		125	10.5	6.1	5.0	326.	-16.2	-15.8	
		125	11.0	5.6	4.6	324.	-16.0	-15.7	
		125	11.5	5.9	4.8	329.	-15.8	-15.5	
		125	12.0	6.2	5.2	332.	-15.5	-15.3	1027.4
		125	12.5	6.3	5.2	334.	-15.5	-15.4	
		125	13.0	6.7	5.9	339.	-15.8	-15.7	
		125	13.5	6.4	5.4	329.	-15.1	-14.9	
		125	14.0	6.3	5.3	326.	-14.9	-14.7	
		125	14.5	6.9	5.6	329.	-15.1	-15.0	
		125	15.0	6.3	5.2	330.	-15.1	-15.0	1028.5
		125	15.5	6.4	5.2	327.	-15.2	-15.1	
		125	16.0	6.4	4.8	318.	-15.6	-15.5	
		125	16.5	6.2	4.5	311.	-15.7	-15.6	

	125	17.0	7.0	5.2	310.	-15.9	-15.8		
	125	17.5	7.1	5.2	310.	-15.9	-15.8		
	125	18.0	7.4	5.4	310.	-15.9	-15.8	1028.6	
	125	18.5	7.4	5.4	310.	-15.9	-15.9		
	125	19.0	7.6	5.8	309.	-15.5	-15.5		
	125	19.5	7.6	5.7	306.	-15.6	-15.6		
	125	20.0	7.6	5.8	304.	-17.6	-20.1		
	125	20.5	7.5	5.8	304.	-17.4	-20.0		
	125	21.0	7.9	6.2	302.	-17.2	-19.9	1028.8	
	125	21.5	8.1	6.5	301.	-17.9	-20.7		
	125	22.0	7.1	6.0	297.	-16.4	-16.5		
	125	22.5	7.4	6.0	300.	-16.4	-16.7		
	125	23.0	8.1	6.4	301.	-16.4	-16.7		
	125	23.5	7.6	6.3	299.	-16.5	-16.8		
MAY	6	126	.0	7.6	6.4	297.	-16.7	-17.0	1028.4
		126	.5	7.7	6.3	299.	-16.8	-17.1	
		126	1.0	7.9	6.4	300.	-16.7	-16.9	
		126	1.5	7.8	6.1	302.	-16.5	-16.7	
		126	2.0	7.8	6.0	303.	-16.3	-16.5	
		126	2.5	7.7	5.9	304.	-16.1	-16.3	
		126	3.0	8.1	6.1	307.	-16.1	-16.3	1027.7
		126	3.5	8.3	6.2	307.	-16.0	-16.2	
		126	4.0	8.4	6.2	310.	-15.8	-16.0	
		126	4.5	8.5	6.3	309.	-15.7	-16.0	
		126	5.0	8.3	6.2	308.	-15.7	-15.9	
		126	5.5	8.1	6.0	310.	-15.7	-15.9	
		126	6.0	8.5	6.2	311.	-15.7	-15.9	1027.5
		126	6.5	8.8	6.4	312.	-15.4	-15.6	
		126	7.0	9.1	6.7	310.	-15.8	-16.0	
		126	7.5	9.2	6.8	310.	-15.3	-15.5	
		126	8.0	9.2	6.9	308.	-15.0	-15.2	
		126	8.5	9.1	6.8	307.	-14.9	-15.0	
		126	9.0	9.7	7.2	308.	-15.1	-15.2	1027.7
		126	9.5	9.3	6.9	308.	-14.5	-14.7	
		126	10.0	9.3	7.0	307.	-14.7	-14.8	
		126	10.5	8.7	6.6	306.	-14.4	-14.6	
		126	11.0	8.6	6.6	306.	-14.3	-14.5	
		126	11.5	8.5	6.5	307.	-13.6	-13.8	
		126	12.0	8.5	6.3	310.	-14.0	-14.3	1027.7
		126	12.5	8.9	6.5	310.	-13.9	-14.1	
		126	13.0	8.7	6.5	308.	-13.9	-14.0	
		126	13.5	8.9	6.7	306.	-13.6	-13.7	
		126	14.0	8.0	6.2	305.	-13.6	-14.3	
		126	14.5	8.1	6.4	303.	-13.7	-13.8	
		126	15.0	8.1	6.4	303.	-13.4	-13.5	1027.4
		126	15.5	7.9	6.5	299.	-13.4	-13.5	
		126	16.0	8.5	7.1	300.	-13.5	-13.6	
		126	16.5	8.7	7.3	299.	-13.4	-13.4	
		126	17.0	7.7	6.6	297.	-13.7	-13.9	
		126	17.5	7.8	6.8	295.	-12.4	-15.1	
		126	18.0	7.4	6.6	294.	-13.6	-13.9	1025.7
		126	18.5	7.0	6.1	291.	-13.5	-13.7	
		126	19.0	8.2	7.2	294.	-13.1	-13.2	
		126	19.5	8.9	7.7	297.	-13.3	-13.5	
		126	20.0	9.6	7.8	302.	-13.5	-13.7	
		126	20.5	9.6	7.5	305.	-13.5	-13.7	

		126	21.0	9.6	7.5	305.	-13.5	-13.8	1023.8
		126	21.5						
		126	22.0						
		126	22.5						
		126	23.0						
		126	23.5						
MAY	7	127	.0	9.5	6.8	318.	-12.2	-12.4	1021.7
		127	.5	10.1	7.3	318.	-12.7	-12.9	
		127	1.0	9.5	7.4	324.	-13.3	-13.4	
		127	1.5	9.0	6.7	321.	-13.4	-13.6	
		127	2.0	8.4	6.7	326.	-13.6	-13.7	
		127	2.5	9.6	7.9	330.	-13.9	-13.9	
		127	3.0	9.2	7.6	332.	-14.0	-14.0	1022.4
		127	3.5	8.8	7.3	333.	-14.1	-14.1	
		127	4.0	9.4	7.7	333.	-14.1	-14.2	
		127	4.5	9.6	8.1	339.	-14.2	-14.2	
		127	5.0	9.1	7.6	340.	-14.3	-14.3	
		127	5.5	8.5	7.0	337.	-14.4	-14.4	
		127	6.0	9.3	7.9	346.	-14.5	-14.6	1023.9
		127	6.5	9.3	8.0	343.	-14.9	-14.9	
		127	7.0	8.4	7.3	346.	-15.1	-15.2	
		127	7.5	8.8	7.5	344.	-14.9	-14.9	
		127	8.0	8.4	7.2	347.	-14.9	-15.0	
		127	8.5	8.0	6.9	346.	-14.6	-14.6	
		127	9.0	7.8	6.7	345.	-14.6	-14.7	1025.8
		127	9.5	7.9	6.7	340.	-14.8	-14.8	
		127	10.0	7.6	6.6	346.	-14.7	-14.9	
		127	10.5	7.5	6.3	338.	-14.7	-14.8	
		127	11.0	7.3	6.2	339.	-14.6	-14.8	
		127	11.5	7.3	6.0	336.	-14.8	-14.8	
		127	12.0	7.2	6.0	332.	-14.8	-14.8	1027.7
		127	12.5	7.4	6.2	335.	-14.5	-14.5	
		127	13.0	7.2	6.0	333.	-14.4	-14.4	
		127	13.5	7.1	5.9	332.	-14.6	-14.6	
		127	14.0	7.3	6.1	332.	-14.6	-14.7	
		127	14.5	7.2	5.9	330.	-14.6	-14.6	
		127	15.0	7.8	6.3	332.	-14.6	-14.6	1028.8
		127	15.5	7.2	5.9	335.	-14.7	-14.7	
		127	16.0	7.0	5.8	336.	-14.7	-14.7	
		127	16.5	7.2	5.9	337.	-14.7	-14.8	
		127	17.0	6.7	5.6	340.	-14.8	-14.8	
		127	17.5	6.6	5.5	338.	-14.8	-14.8	
		127	18.0	6.5	5.3	337.	-14.8	-14.9	1029.7
		127	18.5	6.3	5.2	341.	-14.9	-15.0	
		127	19.0	6.1	5.1	340.	-14.8	-15.0	
		127	19.5	6.0	5.0	343.	-15.0	-15.1	
		127	20.0	5.6	4.7	342.	-15.3	-15.6	
		127	20.5	5.3	4.3	340.	-16.4	-17.2	
		127	21.0	4.9	3.9	336.	-15.8	-16.0	1030.3
		127	21.5	4.7	3.8	332.	-16.0	-16.2	
		127	22.0	4.8	4.0	330.	-11.1	-18.8	
		127	22.5	4.7	3.7	328.	-16.7	-16.9	
		127	23.0	5.3	4.4	332.	-16.7	-16.8	
		127	23.5	5.4	4.3	335.	-16.4	-16.5	
MAY	8	128	.0	4.9	4.0	334.	-16.7	-16.9	1030.3
		128	.5	4.5	3.4	322.	-17.0	-17.2	

128	1.0	4.3	3.1	310.	-18.6	-19.0	
128	1.5	4.3	3.1	310.	-17.3	-17.7	
128	2.0	4.4	3.2	307.	-17.4	-17.8	
128	2.5	4.5	3.5	303.	-17.7	-18.1	
128	3.0						1029.9
128	3.5						
128	4.0						
128	4.5						
128	5.0						
128	5.5						
128	6.0						1028.5
128	6.5						
128	7.0	5.8	4.1	321.	-17.7	-18.1	
128	7.5	6.2	4.6	317.	-17.6	-17.7	
128	8.0	6.0	4.6	311.	-17.6	-17.9	
128	8.5	6.3	5.0	311.	-17.7	-17.7	
128	9.0	6.0	4.8	310.	-17.3	-17.5	1027.8
128	9.5	6.3	4.9	313.	-16.8	-16.9	
128	10.0	6.4	4.9	314.	-16.5	-16.6	
128	10.5	6.3	4.8	314.	-16.1	-16.4	
128	11.0	6.4	4.9	314.	-15.9	-16.3	
128	11.5	6.7	5.2	314.	-16.0	-15.9	
128	12.0	6.7	5.3	313.	-15.9	-15.9	1026.7
128	12.5	7.2	5.8	311.	-15.5	-15.7	
128	13.0	7.2	5.7	313.	-15.4	-15.2	
128	13.5	8.1	6.3	314.	-15.1	-14.9	
128	14.0	7.9	6.1	316.	-14.8	-14.7	
128	14.5	7.9	6.4	312.	-14.9	-14.8	
128	15.0	8.1	6.6	311.	-14.4	-14.3	1024.7
128	15.5	8.1	7.0	309.	-14.2	-14.2	
128	16.0	8.6	7.4	308.	-14.0	-14.2	
128	16.5	8.8	7.6	308.	-13.9	-14.0	
128	17.0	8.8	7.3	310.	-13.6	-13.6	
128	17.5	9.4	7.8	310.	-13.4	-13.4	
128	18.0	9.4	7.6	308.	-13.2	-13.2	1021.8
128	18.5	9.3	7.4	312.	-13.0	-13.0	
128	19.0	9.4	7.4	313.	-12.8	-12.9	
128	19.5	10.1	7.6	318.	-12.6	-12.7	
128	20.0	10.0	7.4	321.	-12.5	-12.6	
128	20.5	9.9	7.1	322.	-12.5	-12.8	
128	21.0	9.6	7.0	321.	-12.2	-12.6	1019.7
128	21.5	9.8	7.1	323.	-11.1	-11.3	
128	22.0	9.8	7.2	326.	-12.2	-12.4	
128	22.5	10.1	7.3	324.	-12.0	-12.2	
128	23.0	10.2	7.4	324.	-11.7	-11.9	
128	23.5	9.9	7.2	325.	-11.3	-11.6	
129	24.0	9.9	7.3	327.	-11.2	-11.5	1017.2
129	.5	9.8	7.2	326.	-11.1	-11.4	
129	1.0	9.9	7.4	328.	-11.0	-11.2	
129	1.5	9.9	7.6	329.	-10.7	-10.9	
129	2.0	9.7	7.7	331.	-10.3	-10.5	
129	2.5	9.5	7.9	334.	-9.8	-10.0	
129	3.0	9.6	8.0	334.	-9.5	-9.6	1015.9
129	3.5	9.3	7.7	337.	-9.1	-9.2	
129	4.0	9.4	7.7	343.	-8.7	-8.9	
129	4.5	8.8	7.3	346.	-8.4	-8.6	

129	5.0	8.3	7.2	350.	-8.3	-8.5	
129	5.5	8.3	7.1	347.	-8.3	-8.5	
129	6.0	8.4	7.1	345.	-8.4	-8.5	1015.7
129	6.5	8.4	7.1	346.	-8.4	-8.5	
129	7.0	8.2	6.7	342.	-8.4	-8.5	
129	7.5	8.1	6.8	345.	-8.2	-8.3	
129	8.0	8.3	7.1	346.	-8.2	-8.2	
129	8.5	8.4	7.3	349.	-8.1	-8.2	
129	9.0	8.1	7.0	348.	-8.2	-8.2	1015.5
129	9.5	8.2	7.1	347.	-8.1	-8.2	
129	10.0	7.8	6.7	347.	-8.3	-8.3	
129	10.5	8.0	6.9	348.	-8.1	-8.1	
129	11.0	7.9	6.9	349.	-8.1	-8.1	
129	11.5	8.0	7.0	351.	-8.1	-8.1	
129	12.0	6.4	5.6	14.	-8.5	-8.5	1015.3
129	12.5	6.8	6.1	26.	-9.0	-9.0	
129	13.0	5.5	4.9	31.	-9.0	-9.1	
129	13.5	5.2	4.6	31.	-9.2	-9.2	
129	14.0	5.0	4.4	44.	-9.5	-9.7	
129	14.5	5.1	4.5	55.	-10.1	-10.3	
129	15.0	5.5	4.9	50.	-10.5	-10.8	1015.8
129	15.5		5.0	56.		-11.8	
129	16.0		4.8	53.		-12.3	
129	16.5		4.5	55.		-12.5	
129	17.0		4.9	60.		-13.2	
129	17.5		4.1	59.		-13.6	
129	18.0		4.3	52.		-14.0	1017.4
129	18.5		4.4	52.		-14.6	
129	19.0		4.6	52.		-14.9	
129	19.5		5.1	55.		-15.7	
129	20.0		4.2	55.		-16.6	
129	20.5						
129	21.0						1020.5
129	21.5						
129	22.0						
129	22.5		5.0	46.		-18.6	
129	23.0		4.3	39.		-18.8	
129	23.5		4.1	28.		-19.0	
130	24.0		4.1	23.		-19.2	1022.6
130	.5		4.2	12.		-19.6	
130	1.0		4.4	9.		-19.7	
130	1.5		5.1	12.		-19.7	
130	2.0		5.2	16.		-19.7	
130	2.5		5.5	15.		-19.7	
130	3.0		5.6	14.		-19.8	1024.1
130	3.5		5.9	18.		-19.5	
130	4.0		5.8	15.		-19.6	
130	4.5		5.7	14.		-19.6	
130	5.0		5.2	14.		-19.6	
130	5.5		5.5	9.		-19.4	
130	6.0		5.2	2.		-19.1	1025.1
130	6.5		4.9	0.		-19.1	
130	7.0		5.5	3.		-18.9	
130	7.5		5.7	3.		-17.9	
130	8.0		6.0	2.		-17.5	

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