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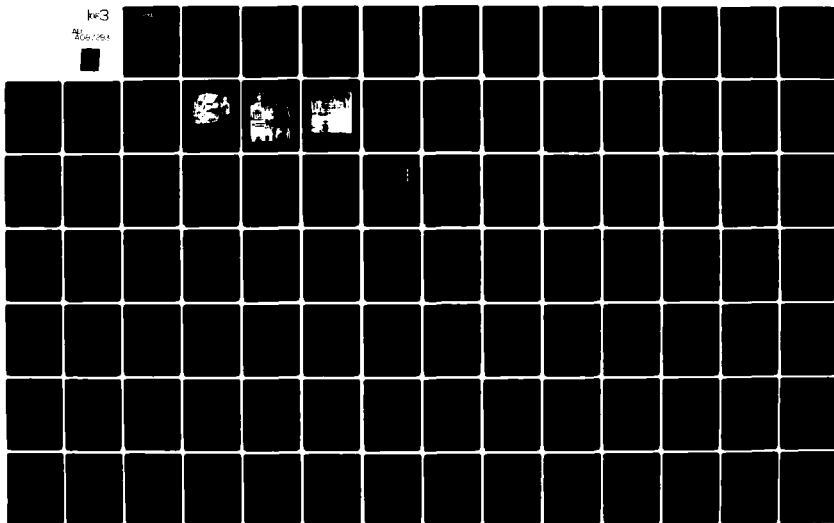
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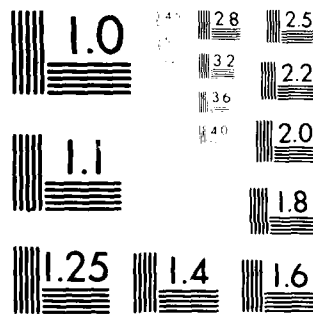
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REPORT NO. NADC-79141-80



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V/STOL EQUIVALENT SYSTEMS ANALYSIS

by
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and
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McDonnell Douglas Corporation
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May 1980

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) A fixed base manned V/STOL handling qualities simulation was performed to answer questions concerning: (a) the pilot's frequency range of interest, (b) the maximum allowable mismatch between high order systems and their low order equivalents, (c) acceptability of high order appearing responses and (d) the piloting effects of phase lag at the natural frequency versus time delay. Various high or low frequency terms were added to low order attitude systems. Pilot ratings and comments showed that the pilot's frequency range of interest was .5-4.0 rad/sec; the amount of mismatch allowed was dependent on the type		

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of high order dynamics added and the match frequency range; pilots did not accept high order appearing dynamics and; time delay is a better correlating parameter than phase lag at the configuration natural frequency. Equivalent systems analysis established criteria for the different flying qualities levels in terms of equivalent parameters.

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FOREWORD

This study was conducted under Contract No. N62269-79-C-0700 to the Naval Air Development Center, and was monitored by Mr. John W. Clark, Jr., Flight Dynamics Branch (Code 6053).

Mr. Roger H. Hoh of Systems Technology Incorporated (STI) and Mr. Rogers E. Smith of Calspan made significant contributions to the study. Mr. Smith also acted as an evaluation pilot.

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TABLE OF CONTENTS

<u>SECTION</u>	<u>PAGE</u>
I INTRODUCTION	1
II DESCRIPTION OF THE SIMULATION.	3
1. SIMULATOR AND DISPLAY.	3
2. CHOICE OF EXPERIMENTAL VARIABLES	7
a. Background	7
b. Choice of Baseline Dynamics.	7
c. Nominal Low Order Lateral Dynamics	9
d. Longitudinal Dynamics.	12
e. Directional Dynamics	12
f. Thrust-to-Throttle Dynamics.	12
3. EQUATIONS OF MOTION.	12
4. GUSTS AND TURBULENCE	12
5. PILOT TASK	18
6. PILOT COMMENT AND RATING SHEET	18
7. ADDED HIGH ORDER DYNAMICS.	18
8. LOW FREQUENCY DYNAMICS	18
9. HIGH FREQUENCY DYNAMICS.	22
a. First Order Lags	22
b. Second Order Lags.	22
c. Transport Lags	22
III RESULTS OF SIMULATION.	24
1. EFFECTS OF THE DISPLAY	24
2. PILOT COMMENTS AND RATINGS	24
3. CALCULATIONS OF MISMATCHES	24
4. LOW FREQUENCY DYNAMICS	28
5. HIGH FREQUENCY DYNAMICS.	31
a. First Order Lags	31
b. Second Order Lags.	34
c. Transport Lags	34
6. PILOTING EFFECTS OF PURE TIME DELAY VS. PHASE LAG.	34
7. HIGH ORDER FLIGHT PATH DYNAMICS.	38
8. EFFECT OF COMMAND GAIN/TIME DELAY INTERACTIONS	38
9. EQUIVALENT SYSTEMS ANALYSIS OF HIGH FREQUENCY EFFECTS.	41
IV SUMMARY AND CONCLUSIONS.	45
V RECOMMENDATIONS.	49
REFERENCES.	50

NADC-79141-60

TABLE OF CONTENTS (Concluded)

<u>SECTION</u>	<u>PAGE</u>
APPENDIX A CONFIGURATION DATA.	52
APPENDIX B PILOT COMMENTS.	123
APPENDIX C PILOT DATA.	209

LIST OF ILLUSTRATIONS

<u>FIGURE</u>		<u>PAGE</u>
1	AV-8B Fixed Base Simulator.	4
2	AV-8B Simulator Cockpit	5
3	AV-8B Cockpit and Vital IV Display.	6
4	Comparison of High Order and Low Order Equivalent YAV-8B Normalized Pitch Dynamics	8
5	Lateral Dynamics, ϕ/δ_{ST} - N1LAT	10
6	Lateral Dynamics, ϕ/δ_{ST} - N2LAT	11
7	Longitudinal Dynamics, θ/δ_{ST}	13
8	Directional Dynamics, ψ/δ_{ST}	14
9	Thrust-to-Throttle Dynamics	15
10	Typical Strip Chart Recordings of Wind Gusts and Crosswind "Spikes".	17
11	Description of Pilot Task	19
12	Pilot Comment Sheet	20
13	Cooper-Harper Pilot Rating Card	21
14	Effect of Dipole Frequency on Pilot Rating, N1LAT .	29
15	Effect of Dipole Frequency on Pilot Rating, N2LAT .	29
16	Comparison of Average Pilot Rating and Mismatch for a Dipole Mode Added to N1LAT and N2LAT.	30
17	Effect On Pilot Rating of Adding a 1st Order Lag to N1LAT.	32
18	Effect on Pilot Rating of Adding a 1st Order Lag to N2LAT.	32
19	Comparison of Average Pilot Rating and Mismatch for a 1st Order Lag Added to N1LAT.	33
20	Comparison of Average Pilot Rating and Mismatch for a 1st Order Lag Added to N2LAT.	33
21	Effect on Pilot Rating of Adding a 2nd Order Lag to N1LAT.	35

LIST OF ILLUSTRATIONS (Continued)

<u>FIGURE</u>		<u>PAGE</u>
22	Effect on Pilot Rating of Adding a 2nd Order Lag to N2LAT.	35
23	Comparison of Average Pilot Rating and Mismatch for a 2nd Order Lag Added to N1LAT.	36
24	Comparison of Average Pilot Rating and Mismatch for a 2nd Order Lag Added to N2LAT.	36
25	Effect of Pure Time Delay on Pilot Rating	37
26	Effect of Time Delay on Mismatch.	37
27	Effect of Phase Lag on Average Pilot Rating	39
28	Interaction of Command Gain and Time Delay.	40
29	Variation of Pilot Rating with Command Gain and Time Delay.	42
30	Variation of Average Pilot Rating with Equivalent Time Delay	44
31	Summary of Maximum Augmentation Added Without Affecting Rating.	47
A-1	Key to Configuration Listing.	53
A-2	List of Configurations and Pilot Ratings.	54
A-3	List of Configuration Transfer Functions.	59
A-4 through A-63	Frequency and Time Response	63 through 122

NADC-79141-60

LIST OF TABLES

<u>TABLE</u>		<u>PAGE</u>
1	Equations of Motion	15
2	List of Configurations and Pilot Ratings.	25
3	Time Delay vs Phase Lag - Summary of Results.	39
4	Equivalent Systems Parameters	43

NADC-79141-60
LIST OF SYMBOLS

F_s	Stick Force, N
HOS	High Order System
K	Command Gain, $\text{rad/sec}^2/\text{cm}$
LOS	Low Order System
m	Aircraft Mass, kg
n	Number of Frequencies
p	Body Angular Roll Rate, rad/sec
q	Body Angular Pitch Rate, rad/sec
s	Laplace Operator, sec^{-1}
u	Body-Axis Velocity, X-Direction, m/sec
v	Body-Axis Velocity, Y-Direction, m/sec
Y_v	$(\partial Y/\partial v)/m$, sec^{-1}
δ_{PED}	Rudder Pedal Displacement, cm
δ_{ST}	Stick Displacement, cm
ζ	Damping Ratio
ζ_e	Equivalent Damping Ratio
θ	Pitch Angle, rad
λ	Root of First Order Lag
τ	Time Delay, sec
τ_e	Equivalent Time Delay, sec
ϕ	Roll Angle, rad
$\dot{\psi}$	Yaw Rate, rad/sec
ω_B	Break Frequency of Turbulence Model, rad/sec
ω_{DP}	Dipole Frequency, rad/sec
ω_e	Equivalent Frequency, rad/sec
ω_L	Lag Frequency, rad/sec
ω_n	Natural Frequency, rad/sec

I INTRODUCTION

High order mathematical models are used to simulate the response of a vertical/short takeoff and landing (V/STOL) aircraft to pilot or turbulence inputs. A recent Naval Air Development Center (NADC) contract (N62269-77-C-0278), Reference 1, categorized high order V/STOL responses in terms of low order equivalent systems. Reference 1 then used equivalent parameters to propose modifications to the V/STOL flying qualities Military Specification, MIL-F-83300. It has become imperative to determine the capability of these low order equivalent systems to adequately approximate the high order dynamics.

This present study investigated equivalent system techniques for defining V/STOL handling qualities criteria in hover and low speed flight. It addressed four questions:

- 1) What is an allowable mismatch between the high order system and its low order equivalent?
- 2) What is the pilot's frequency range of interest, in which a good match should be assured?
- 3) Do pilots require low-order-appearing responses in attitude, velocity and position to control inputs, and will they reject more complicated higher order responses?
- 4) What are the piloting effects of time delay versus the effects of phase lag?

Considerable research has been performed on the flying qualities of augmented aircraft, using the equivalent systems approach. Much equivalent systems work has been done by Systems Technology Incorporated (for example the early Navy-sponsored studies of References 2 and 3) and by McDonnell Aircraft, MCAIR (for example, References 4 and 5). These references discuss the augmented dynamics of conventional takeoff and landing (CTOL) aircraft. In fact, low order equivalent systems have emerged as the most widely accepted technique for analyzing high order CTOL dynamics. This led to proposals that the CTOL flying qualities specification, MIL-F-8785B (ASG), should be written in terms of equivalent systems (References 4 and 6). NADC and the USAF Flight Dynamics Laboratory (AFFDL) then sponsored an in-flight simulation, using the variable stability NT-33 aircraft, to validate the CTOL equivalent systems concept. The simulation is described in Reference 7 and initial analytical results are presented in Reference 8.

This NT-33 study produced a surprising result. It was discovered that the pilots were relatively insensitive to large mismatches between high order dynamics and their low order

equivalents. For example, in performing analytical matching of CTOL dynamics, a mismatch function had been defined as

$$\frac{20}{n} \sum (\text{Gain}_{\text{HOS}} - \text{Gain}_{\text{LOS}})^2 + .02 (\text{Phase}_{\text{HOS}} - \text{Phase}_{\text{LOS}})^2$$

where the summation is performed over n frequencies equispaced on a Bode plot. A value of 10 for this mismatch had been arbitrarily chosen as a good match based on the visual Bode match quality. In the NT-33 simulation, high order systems were evaluated together with their low order equivalents. The pilots were unable to distinguish between pairs of systems with mismatches as high as 200.

The most likely explanation for the observed insensitivity of flying qualities to mismatch is that mismatch alone is not the critical parameter. This may stem from the fact that the range of frequency and damping values for good flying qualities is large. In other words mismatch will exist between two low order systems with parameters near the extremes of the Level 1 region. The pilot comments and ratings for these two low order systems are not expected to differ much in spite of the large mismatch between them.

It therefore may be necessary to specify how mismatch is generated, by defining what type of high order effect has been added to a low order response. Theoretically, a virtually infinite number of effects can be added to a low order response. Fortunately, a relatively small number of effects are encountered in practice.

The foregoing findings led to the approach (used in the present study) of systematically augmenting low order responses with high order effects and determining the flying qualities rating on the simulator. By adding augmentation progressively to increase mismatch, a mismatch threshold can be established for a given type of augmentation. This threshold is the mismatch level at which the rating just begins to degrade. An analyst then has a guideline for evaluating his augmented dynamics by using an equivalent system which should fall within the mismatch threshold. Alternatively, the analyst can increase the order of the equivalent system by adding a term of the same type added in this present study. In this case the mismatch will decrease and the parameters of the added term also become available for correlation. This latter approach has the disadvantage of increasing the dimension of the analyst's problem, but the advantage of reducing the mismatch. Both approaches were used in this present study.

The four questions on equivalence were therefore tackled by simulation of two nominal attitude control systems with various amounts of added low and high frequency dynamics. Section II describes the simulator and presents the justification for the parameter values chosen. Section III describes the results and Section IV presents a summary and conclusions. Section V gives recommendations for further work. The experimental data are documented fully in the Appendices.

II DESCRIPTION OF THE SIMULATION

1. Simulator and Display - The simulation was conducted in the McDonnell AV-8B fixed base simulator cockpit, shown in Figure 1. The external world display was produced by the VITAL IV three window display system (not shown in Figure 1).

The AV-8B simulator cockpit, shown in Figure 2, duplicates the actual aircraft in physical geometry, control and display layout, and function.

A minimum of cockpit instrumentation was used since the test was mainly visual. The altitude in 3.048 m (10 ft) increments was displayed by two digits on the heads-up display (HUD).

The stick force gradients used were approximately 3.07 Newtons/cm (1.75 pounds/in) in pitch control and 3.13 Newtons/cm (1.79 pounds/in) in left roll control and 4.05 Newtons/cm (2.31 pounds/in) in right roll control. A rudder force gradient of approximately 28.89 Newtons/cm (16.5 pounds/in) was used throughout. The stick deflections available were +13.716 cm (5.4 in) and -5.334 cm (-2.1 in) longitudinally and +7.62 cm (+3.0 in) laterally. The rudder pedal travel was +5.385 cm (+2.12 in).

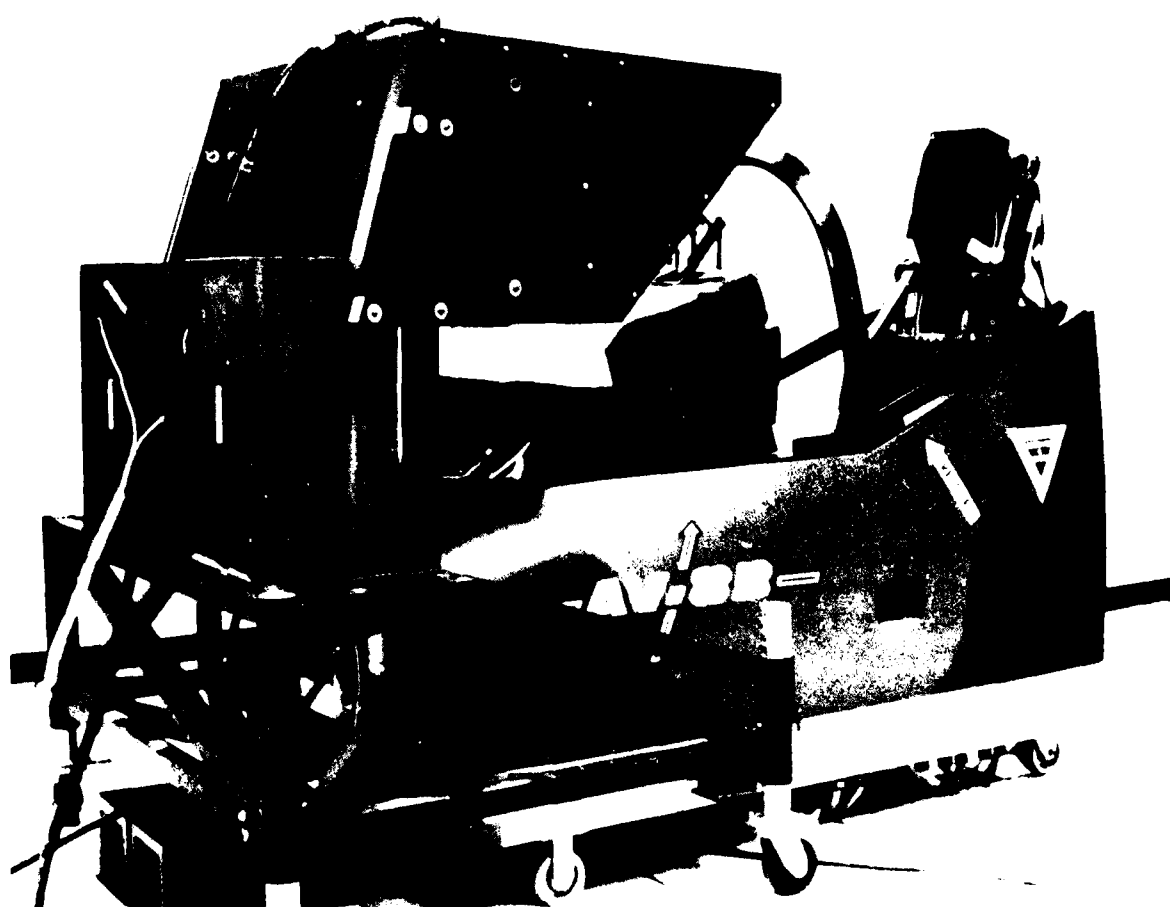
The thrust control was of the throttle type.

VITAL IV is a general purpose computer-generated simulation display system. The image is generated on a digital computer with a refresh rate of 20 Hz. The high-resolution, multi-color image is displayed in virtual image form.

For the AV-8B simulator application, three VITAL display units are arranged about the front of the cockpit to provide a wide angle scene. Each display unit has a field-of-view of approximately 35° by 45°. The total field-of-view is approximately +60° horizontally. The vertical field-of-view of the front unit is about 15° up to 20° over the nose. The side units provide a vertical field-of-view of about 5° up to 40° down. This arrangement is especially well suited for providing ground visibility for VTOL operations.

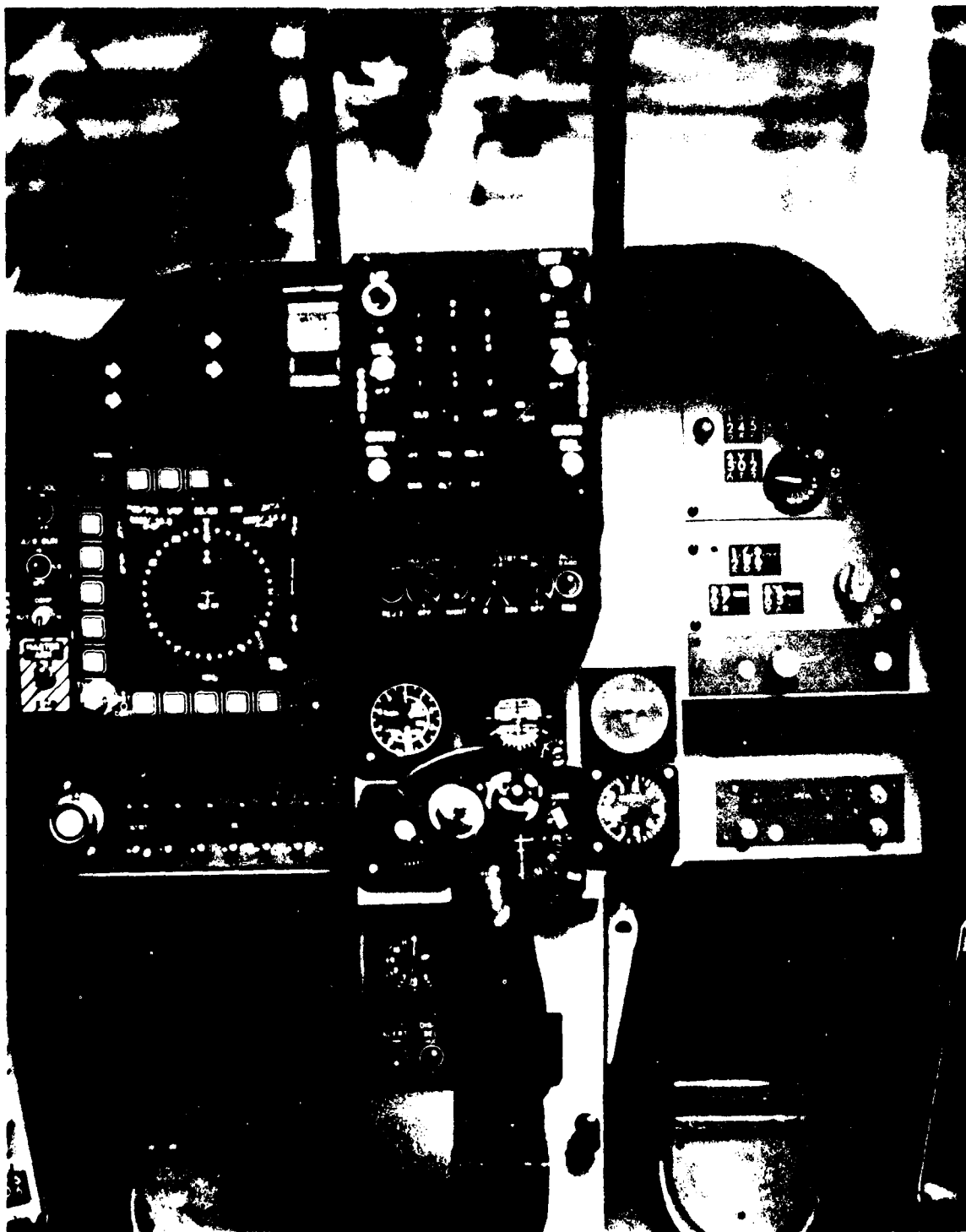
The visual display used was a twilight scene of the Minneapolis/St. Paul airport.

Figure 3 presents a "birds-eye" view of the AV-8B cockpit and the simulated VITAL IV display.



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Figure 1. AV-8B Fixed Base Simulator



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Figure 2. AV-8B Simulator Cockpit

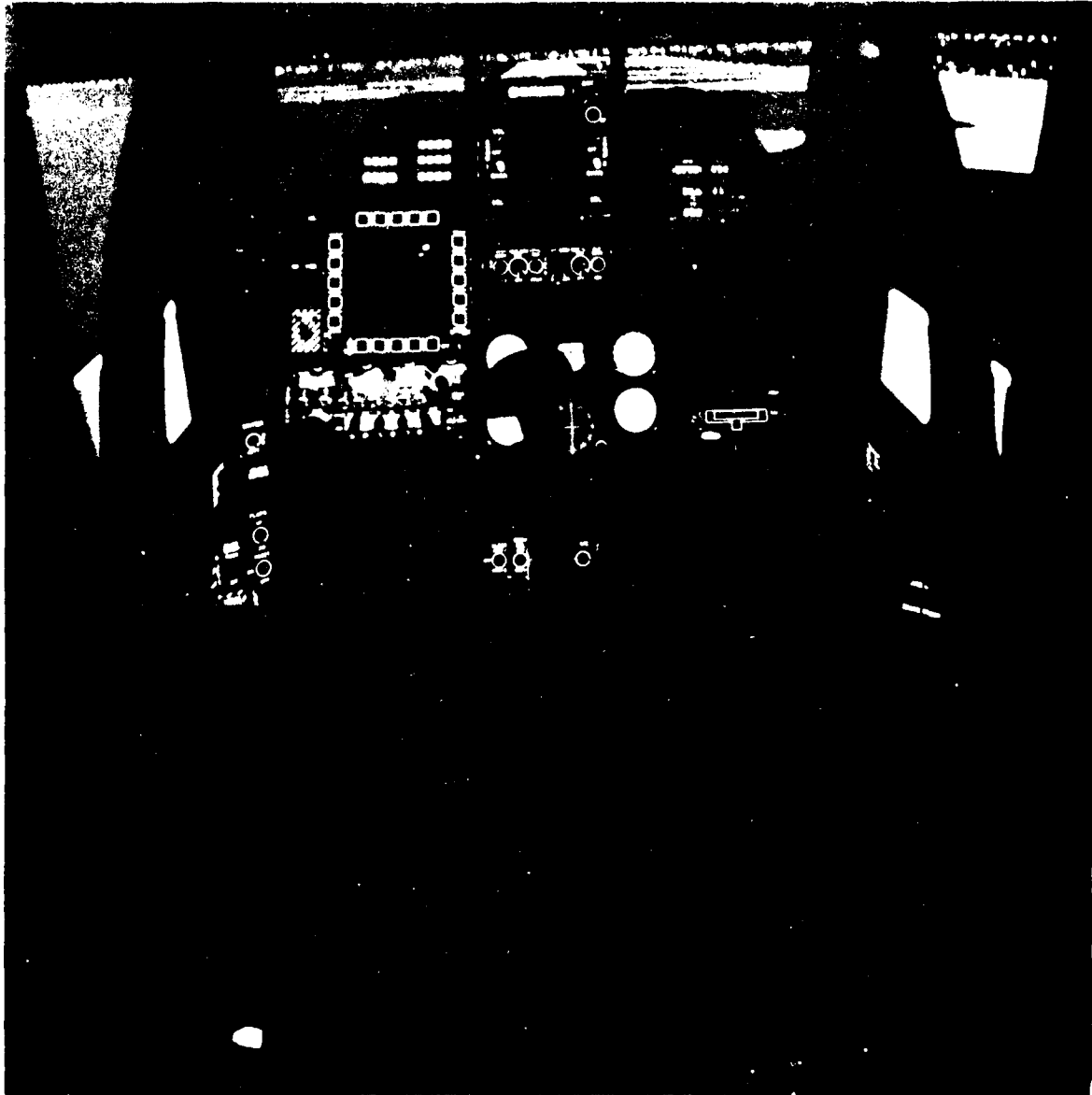


Figure 3. AV-8B Cockpit and VITAL IV Display

The following data were recorded on strip-chart recorders:

- Lateral Stick Position
- Longitudinal Stick Position
- Rudder Pedal Position
- Lateral Stick Force
- Longitudinal Stick Force
- Rudder Pedal Force
- Throttle Position
- Altitude
- Roll Rate
- Roll Angle
- Pitch Rate
- Pitch Angle
- Yaw Rate
- Yaw Angle
- Gust Response (Directions and Velocities)
- Body Angular Rates p and q
- Body-Axis Velocities u and v

The following data were recorded on magnetic tape:

- Roll, Pitch, Yaw and Thrust Cockpit Control Positions
- Altitude
- Computed Pitch, Roll and Yaw Angles
- Gust Response (Directions and Velocities)
- Body Angular Rates p and q

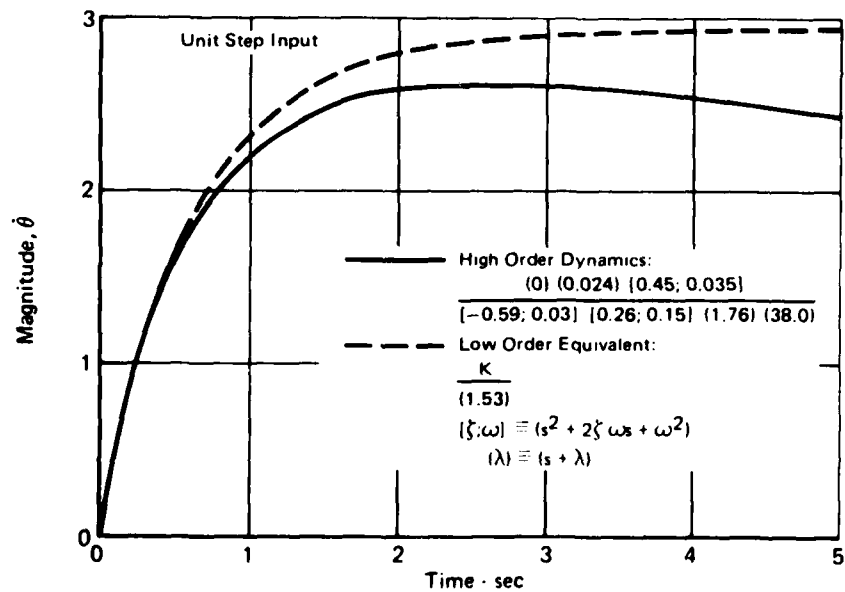
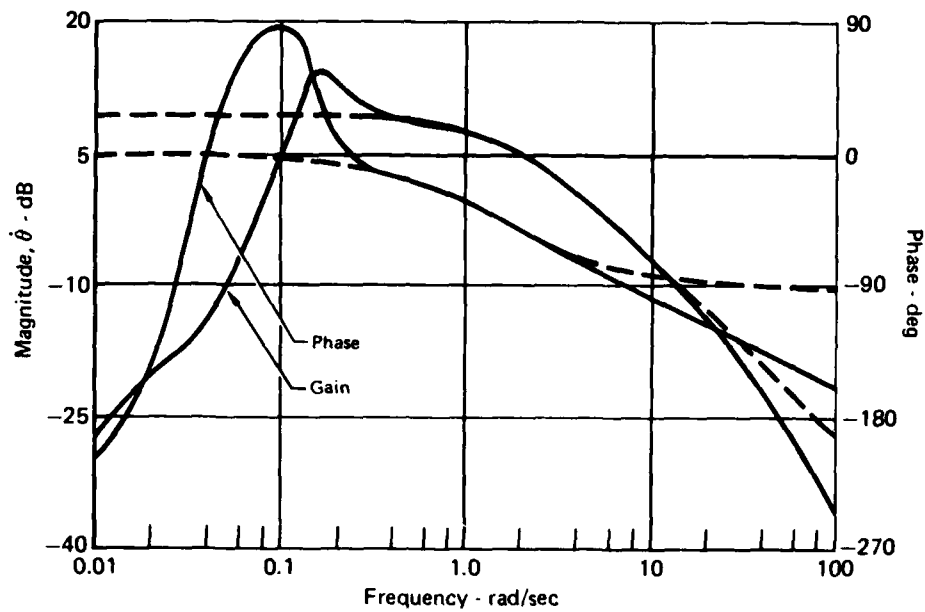
Fast Fourier analysis was used during checkout to verify the configurations.

Voice recordings were made throughout the simulation.

2. Choice of Experimental Variables

(a) Background - Figure 4 illustrates a YAV-8B pitch rate response which was used in establishing the experiment ground-rules. The response is a first order lag, with added modes at high and low frequency. In any arbitrary frequency range, the total high order response can be approximated by a baseline first order lag alone, together with a mismatch caused by the added modes. Since the pilot rating for the configuration is Level 1 these mismatches due to the added nuisance modes would be negligible to the pilot.

(b) Choice of Baseline Dynamics - The YAV-8B response is a rate system generated by a rate feedback. Other system types have been proposed in which, for example, attitude and velocity feedbacks are added. Examples of these systems, depending on the mechanization, have been described as attitude, translation rate, rate command attitude hold, and translation rate position hold. Examination of all these systems is beyond the scope of this present study. Attitude command dynamics were chosen as



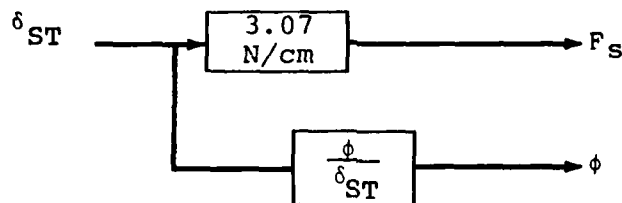
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Figure 4. Comparison of High Order and Low Order Equivalent YAV-8B Normalized Pitch Dynamics

the baseline for this study since previous studies (e.g., Reference 1) have indicated this to be the nominally acceptable augmentation for operation in the Navy environment. Bank angle dynamics were chosen as a suitable axis for study. To simplify the study further, only hover and very low speed dynamics were considered.

To prevent the pilot from being influenced by the longitudinal, directional and thrust-to-throttle dynamics, these systems remained constant throughout the simulation. They were chosen after investigation into previous simulations (Reference 9, 10 and 11).

(c) Nominal Low Order Lateral Dynamics - Two baselines were defined as below.



$$\text{where } \phi/\delta_{ST} = \frac{.708 \text{ rad/sec}^2/\text{cm}}{[.7;2.0]} \quad (\text{N1LAT})$$

$$\text{or } \phi/\delta_{ST} = \frac{2.95 \text{ rad/sec}^2/\text{cm}}{[.7;5.0]} \quad (\text{N2LAT})$$

$$\text{using the notation } \frac{K}{s^2 + 2\zeta\omega_n s + \omega_n^2} \triangleq \frac{K}{[\zeta; \omega_n]} .$$

Time history responses to step and impulse inputs for both nominal systems are shown in Figures 5 and 6. The impulse responses confirm that the dynamics are attitude systems when compared with the criterion of Reference 1.

The nominal systems were designated N1LAT (.708/[.7;2.0]) and N2LAT (2.95/[.7;5.0]) as shown. Note that the command gain values for N1LAT and N2LAT were .708 and 2.95 rad/sec²/cm respectively. Command gains of .472 and .944 rad/sec²/cm were used in a few cases for N1LAT.

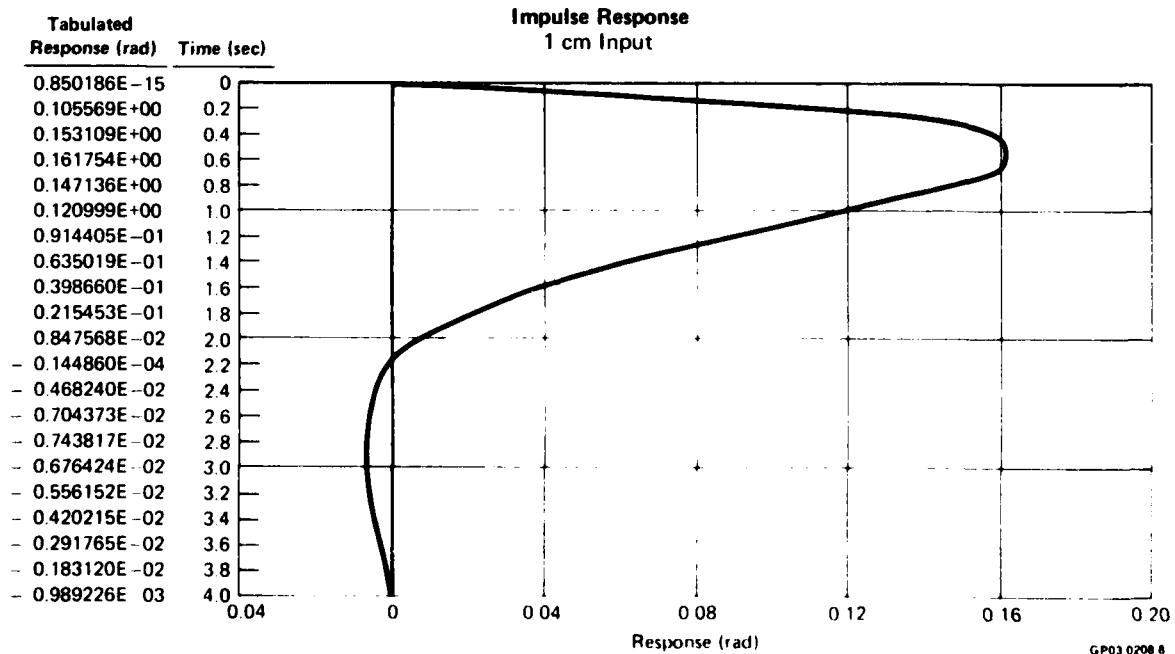
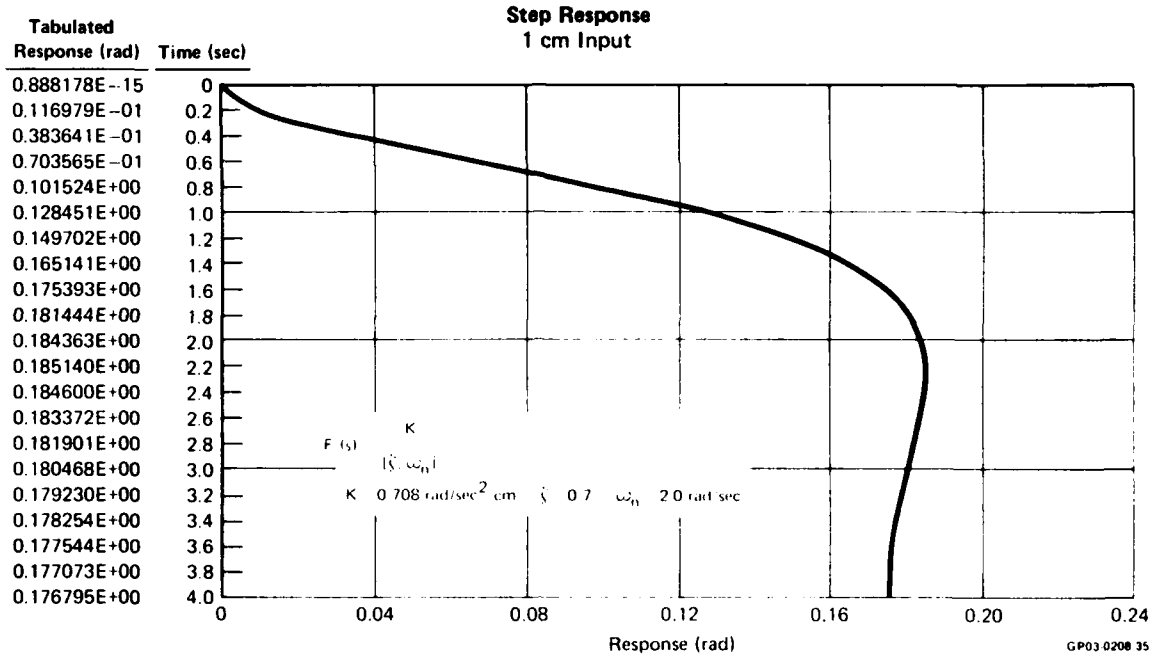


**Figure 5. Lateral Dynamics, ϕ/δ_{ST}
N1LAT**

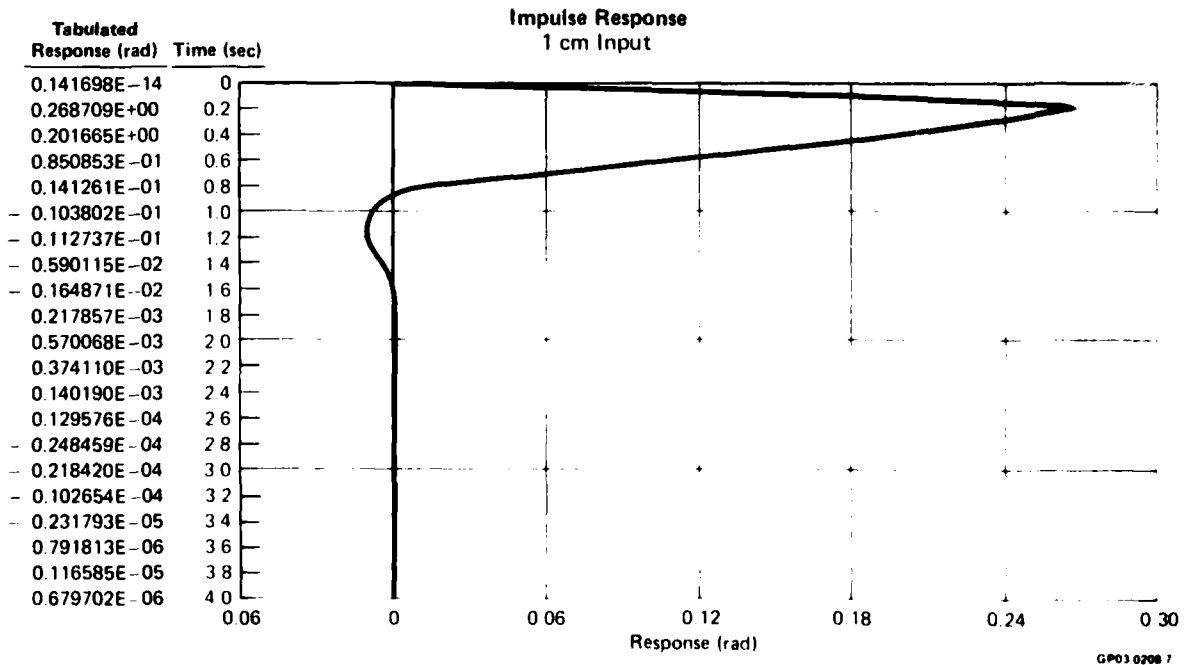
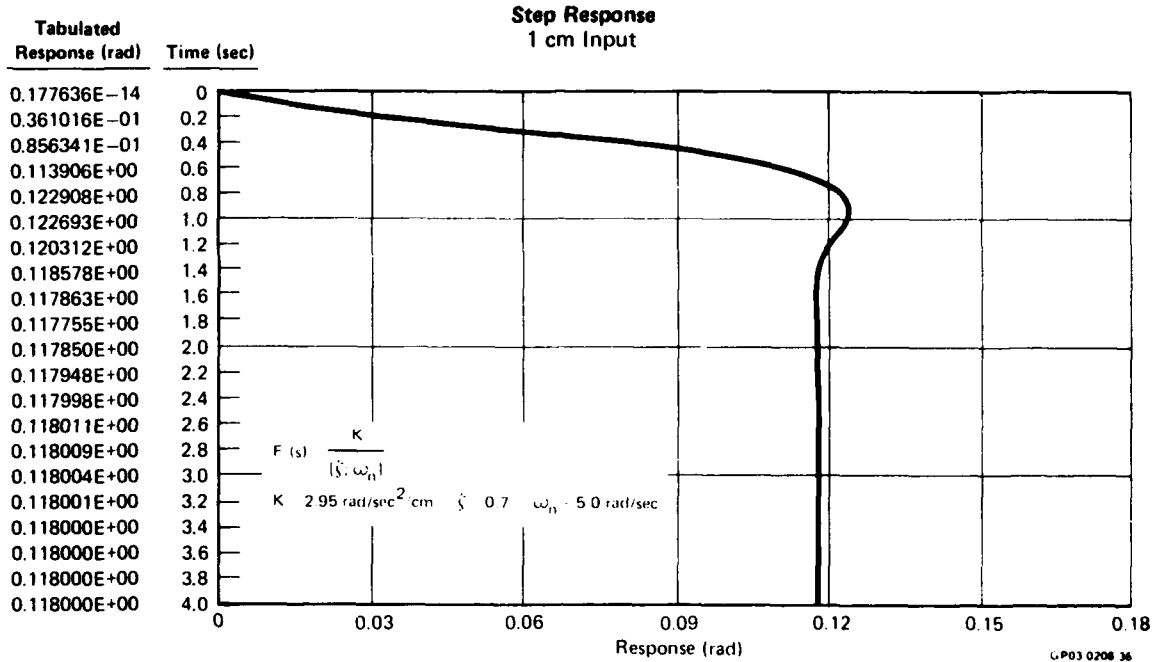


Figure 6. Lateral Dynamics, ϕ/δ_{ST}
N2LAT

(d) Longitudinal Dynamics - These were held constant in the experiment, and were modeled by a 0/2nd transfer function of the form:

$$\frac{\theta}{\delta_{ST}} = \frac{.591 \text{ rad/sec}^2/\text{cm}}{[.7;2.0]}$$

Time histories for step and impulse functions are presented in Figure 7. Again the impulse histories confirm that the longitudinal dynamics are categorized as attitude systems.

(e) Directional Dynamics - These were held constant in the experiment and were modeled by a 0/1st transfer function of the form:

$$\frac{\dot{\psi}}{\delta_{\text{Pedal}}} = \frac{.115 \text{ rad/sec}^2/\text{cm}}{(1.095)}$$

Time history responses for step and impulse functions are shown in Figure 8.

(f) Thrust-to-Throttle Dynamics - These were held constant in the experiment, and were modeled with a second order lag representative of the YAV-8B Pegasus response. The maximum thrust-to-weight ratio was 1.1. Trim was set at approximately 90% throttle.

The block diagram for thrust-to-throttle response is shown in Figure 9.

3. EQUATIONS OF MOTION - The equations of motion used in the simulation are presented in Table 1.

Simulator display motions were driven by six degree of freedom calculations.

4. GUSTS AND TURBULENCE - Continuous turbulence was simulated by passing the output of a random noise generator having a relatively uniform low-frequency power spectral distribution through a first order filter with a break frequency (ω_B) of 0.314 rad/sec:

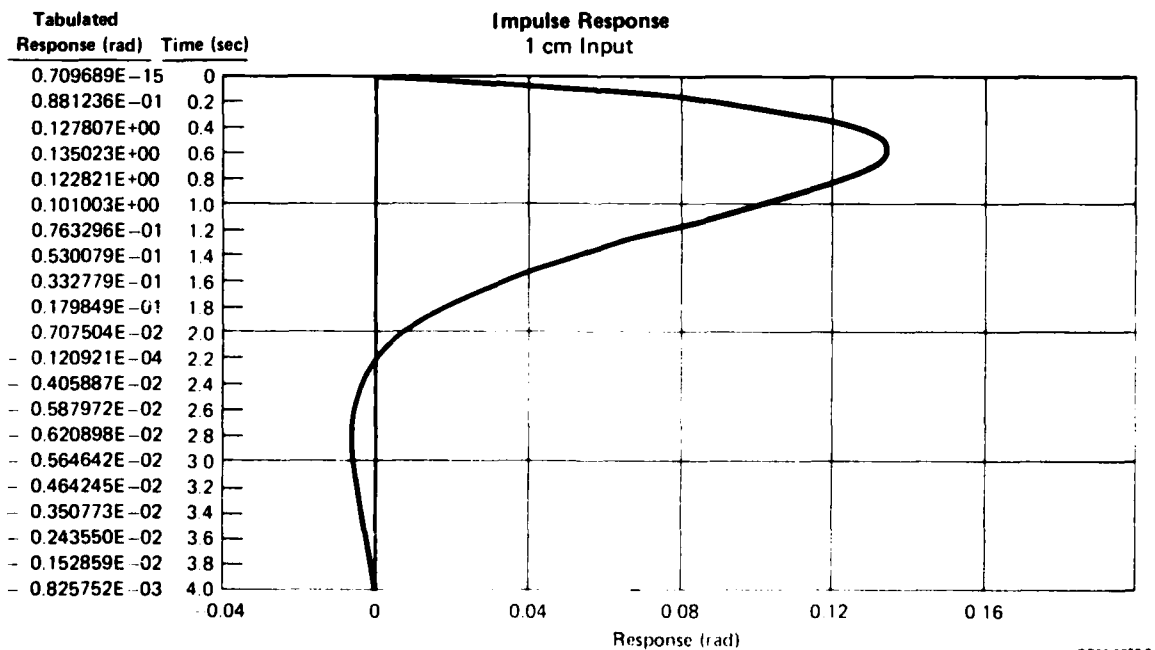
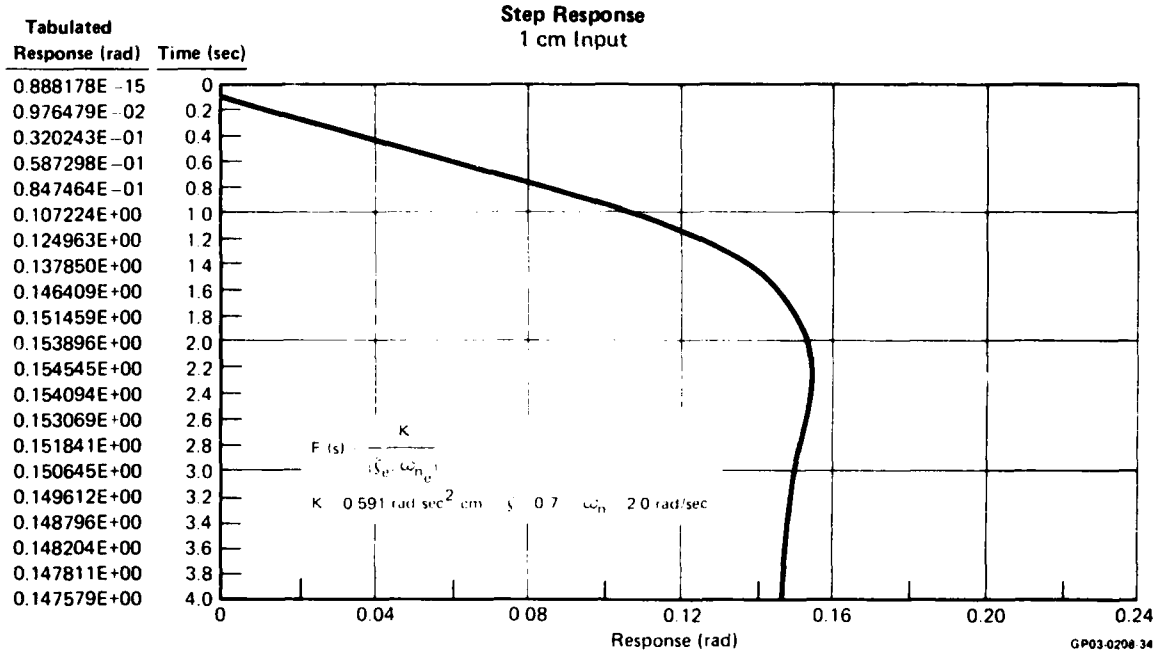
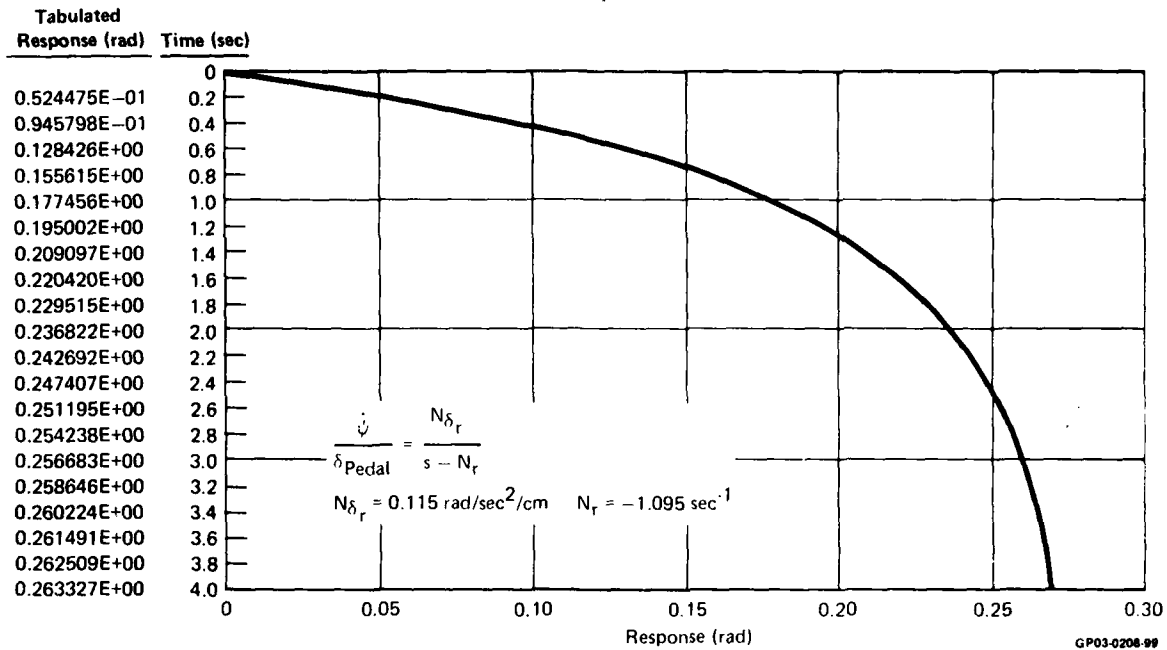


Figure 7. Longitudinal Dynamics, θ_{IST}

Step Response
1 cm Input



Impulse Response
1 cm Input

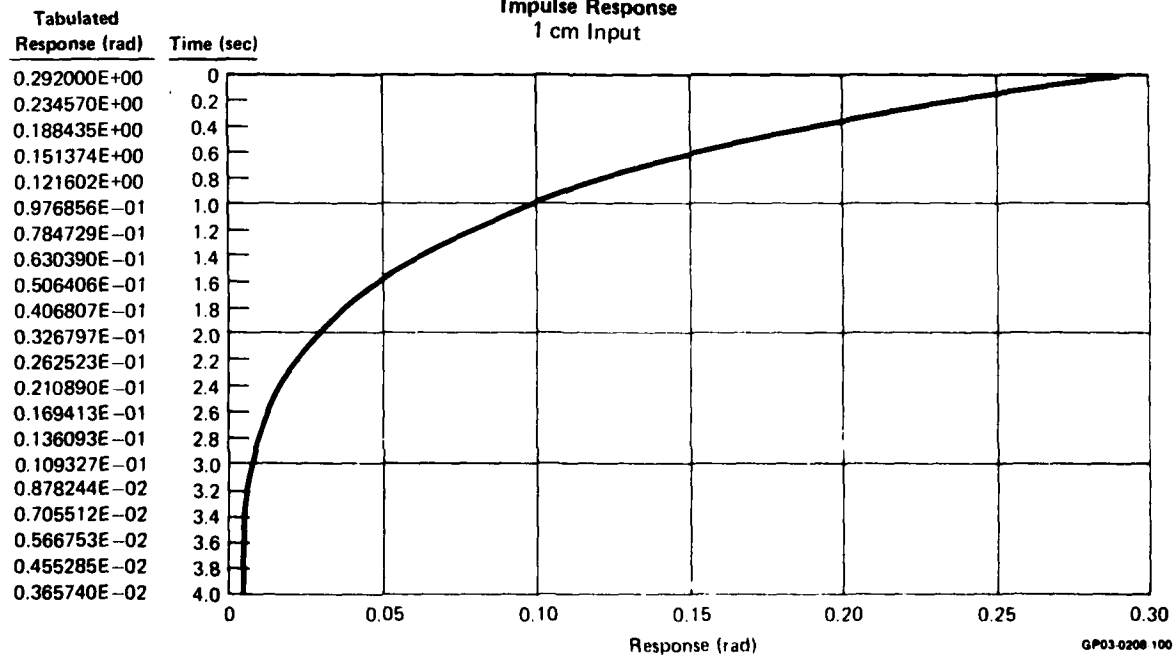
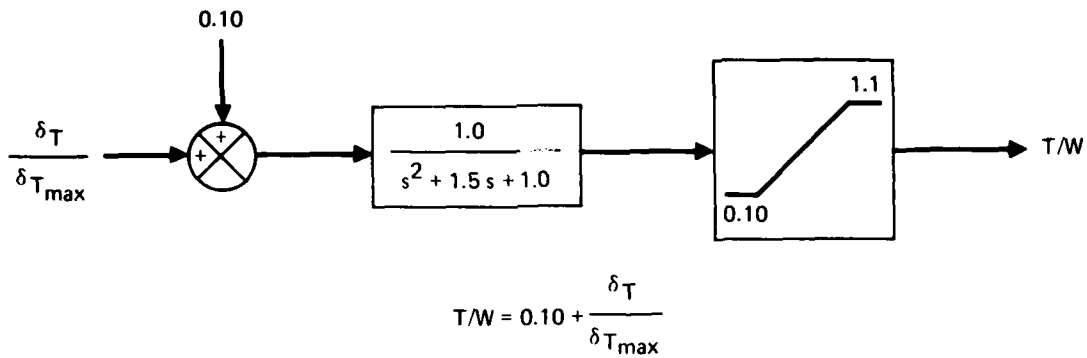


Figure 8. Directional Control, $\dot{\psi}/\delta_{\text{PED}}$



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Figure 9. Thrust-to-Throttle Dynamics

TABLE 1. EQUATIONS OF MOTION

1. Transfer functions yield p, q, r (body axis angular rates).

2. Body axis velocity components obtained from:

$$\begin{aligned}\dot{u} &= -g \sin \theta + rv - qw + X_u u & X_u &= -0.1 \\ \dot{v} &= g \sin \phi \cos \theta + pw - ru + Y_v v & Y_v &= -0.1 \\ \dot{w} &= -pv + qu - g (T/W - \cos \theta \cos \phi) + Z_w w & Z_w &= -0.75\end{aligned}$$

3. Inertial axis displacement determined from:

$$\begin{aligned}\dot{X} &= u \cos \psi \cos \theta + v [\cos \psi \sin \theta \sin \phi - \sin \psi \cos \phi] + w [\cos \psi \sin \theta \cos \phi + \sin \psi \sin \phi] \\ \dot{Y} &= u \sin \psi \cos \theta + v [\sin \psi \sin \theta \sin \phi + \cos \psi \cos \phi] + w [\sin \psi \sin \theta \cos \phi - \cos \psi \sin \phi] \\ \dot{Z} &= -u \sin \theta + v \cos \psi \sin \phi + w \cos \theta \cos \phi\end{aligned}$$

GP03-0208-16

$$\frac{u_g}{N_g} = \frac{K_{u_g}}{S + 0.314}$$

$$\frac{v_g}{N_g} = \frac{K_{v_g}}{S + 0.314}$$

where K_{u_g} and K_{v_g} were adjusted to yield desired rms values of turbulence. N_g is the output of the random noise generator.

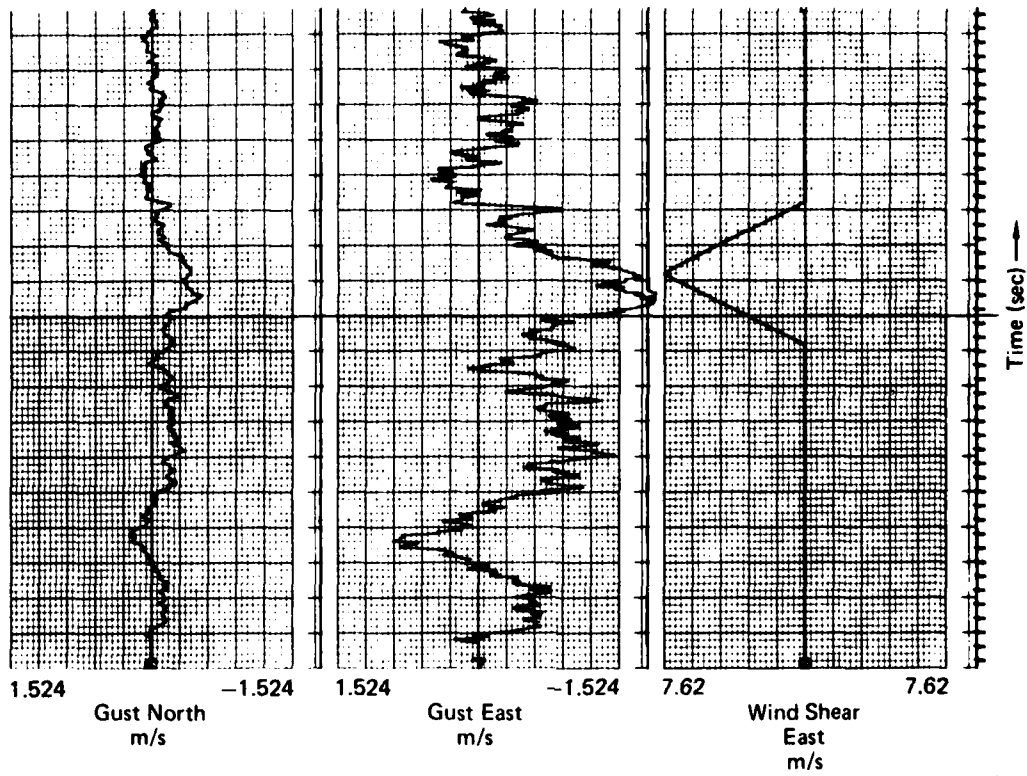
The continuous turbulence intensity level was $\sigma_g = 1.14$ kt (1.925 fps). For the lateral handling qualities study, the longitudinal component u_g was 25% of the lateral component v_g . The components were in phase. Turbulence was introduced along the aircraft X and Y body axes through the display. The continuous turbulence did not produce severe problems for the pilot and was rated as a minor nuisance.

In addition to the continuous turbulence, large discrete disturbances along the aircraft Y body axis were input to the display. These "spikes" appeared to the pilot as strong side gusts producing large excursions from the flight path.

The crosswind spike magnitude was established during the check-out phase by progressively increasing rate magnitudes from 0.6096 to 3.048 meters per second squared. A maximum spike rate of 1.524 meters per second squared for 5.0 seconds, followed by a decay at the same rate, gave a realistic but demanding external disturbance. This produced a maximum aircraft translation rate of 14.8 kts (25 fps).

The pilots were asked to maintain a constant heading when encountering the spike, which was input at random times by the engineer. Since the spike was a gross disturbance in the aircraft's position, it forced the pilot to evaluate both flight path control (outer loop) and attitude control (inner loop). Thus its implementation was analogous to the CTOL offset precision landings which have been shown to expose flying qualified problems very reliably.

A strip chart recording of the low frequency turbulence and crosswind spike (wind shear) is shown in Figure 10 for a typical run.



GP03-0208-101

Figure 10. Typical Strip Chart Recordings of Wind Gusts and Crosswind "Spikes"

5. PILOT TASK - The aircraft was initially at an altitude of 18.288m (60 ft) with a 14.8 kts (25 fps) forward speed and was centered on the runway approximately 30.48m (100 ft) laterally and 60.96m (200 ft) longitudinally from the hover point. The task was to translate forward and to the right and stabilize in hover over a point on the right edge of the runway and slightly displaced from the intersection of the runway with the taxi-way. A sketch depicting the task is shown in Figure 11. As a secondary task, the pilots tried to maintain a constant altitude of 18.288m (60 ft). The pilots were also asked to maintain a constant heading down the runway. Normal piloting technique would be to yaw into the wind spike. By maintaining a relatively constant heading instead, it was hoped to expose any piloting problems with the lateral axis.

6. PILOT COMMENT AND RATING SHEET - A pilot comment and rating sheet was used to stimulate the pilots thinking in the areas of interest. The sheet covered areas of general interest, e.g. attitude response, flight path response and wind and turbulence, with more precise topics under the general headings. A sample comment sheet is shown in Figure 12.

The pilots were also given a Cooper-Harper rating scale card to be used in rating each configuration. A sample rating card is shown in Figure 13.

7. Added High Order Dynamics - As discussed in the Introduction, high order terms were cascaded with (i.e. added to) the low order nominal dynamics at high and low frequencies, to gain information on the four basic questions of equivalence. Appendix A contains transfer function coefficient and root data, with frequency and time responses, for all configurations. The response of each configuration is compared with the corresponding nominal dynamics.

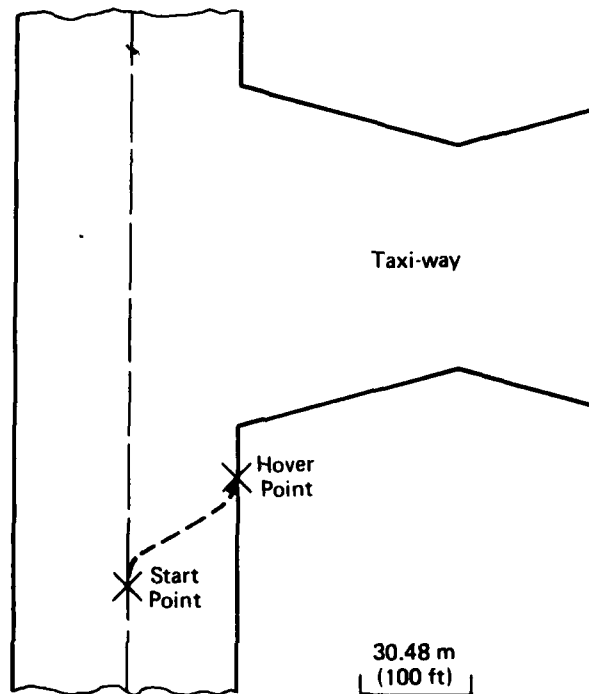
8. Low Frequency Dynamics - Two types of low frequency dynamics were added separately to the nominal dynamics.

The first was a second order element of the form

$$\frac{\omega_L^2 s^2}{[.05; \omega_L]} \quad \text{with } \omega_L = .1, .3, .5, .7 \text{ rad/sec}$$

It combines two low frequency effects which can be seen in practical flight control systems. The first is the localized amplitude resonance due to low damping, and the second is a 40 dB/decade low frequency gain roll-off. This roll-off is an exaggeration of the low frequency behavior of the 'rooftop' systems in Figure 28 of Reference 1. The advantage of the roll-off in this study is the smooth progressive increase in mismatch it introduces when ω_L is increased.

These data are presented in Appendix B as pilot comments and ratings only.



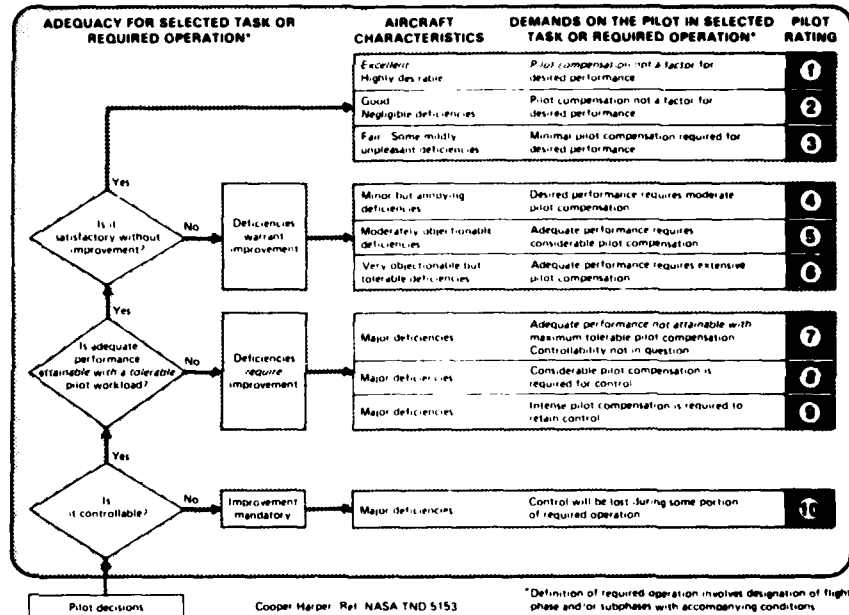
GP03-0208-14

Figure 11. Diagram of Pilot Task

	Translation	Hover
	Overall Rating:	Overall Rating:
Feel • Forces • Displacement • Sensitivity		
Attitude Response • Initial • Predictability • Special Inputs • PIO Tendency		
Flight Path Response • Initial • Predictability • Special Inputs • Flight Path and Attitude Trade-offs		
Height Response • Special Problems		
Wind and Turbulence • Effect on Attitude • Effect on Altitude, Flight Path and/or Height Response		
Summary Comments		

GP03-0208-15

Figure 12. Pilot Comment and Rating Sheet



DEFINITIONS FROM TN-D-5153

COMPENSATION

The measure of additional pilot effort and attention required to maintain a given level of performance in the face of deficient vehicle characteristics

HANDLING QUALITIES

Those qualities or characteristics of an aircraft that govern the ease and precision with which a pilot is able to perform the tasks required in support of an aircraft role

MISSION

The composite pilot vehicle functions that must be performed to fulfill operational requirements. May be specified for a role, complete flight, flight phase, or flight subphase

WORKLOAD

The integrated physical and mental effort required to perform a specified piloting task

PERFORMANCE

The precision of control with respect to aircraft movement that a pilot is able to achieve in performing a task (Pilot vehicle performance is a measure of handling performance. Pilot performance is a measure of the manner or efficiency with which a pilot moves the principal controls in performing a task.)

ROLE

The function or purpose that defines the primary use of an aircraft

TASK

The actual work assigned a pilot to be performed in completion of or as representative of a designated flight segment

GP03-0208-8

Figure 13. Cooper-Harper Pilot Rating Scale

The second type of low frequency dynamics was a dipole of the form

$$\frac{[.2; \omega_{DP}]}{[.7; \omega_{DP}]} \quad \text{with } \omega_{DP} = .1, .3, .5, .7 \text{ rad/sec}$$

This dutch roll-like, dipole mode was established after examining responses of the YAV-8B and Type A V/STOL. It adds a localized notch to the frequency response. By changing the frequency of the notch, ω_{DP} , information on the pilots' sensitivity to low frequency mismatches was gained.

9. High Frequency Dynamics - To generate high frequency mismatches, three types of high frequency dynamics (first order lag, second order lag, transport lag) were added separately to the two nominal systems. The frequency of the first and second order lags was decreased and the delay increased progressively. These dynamics are typical of the high order effects of prefilters, actuation, etc., which can be seen in many augmented systems. The form of each added term is indicated below:

a. First Order Lags

$$\frac{1}{(\lambda)} \quad \text{with } \lambda = 1., 2., 3., 4., 5., 6., 7. \text{ rad/sec}$$

b. Second Order Lags

$$\frac{\omega_L^2}{[.3; \omega_L]} \quad \text{with } \omega_L = 4., 5., 6., 7., 8., 9., 10., 11. \text{ rad/sec}$$

This damping ratio of .3 is lower than those usually due to high frequency control components, which have a damping ratio around .7. By introducing a mode with an oscillation, it was hoped to introduce a somewhat different piloting effect from the apparent delay which a well-damped second order mode would introduce.

c. Transport Lags - Pure time delay, e^{-sT} , was added to the nominal systems to investigate the effects of time delay on pilot performance. For N2LAT, the time delay was adjusted to produce the same amount of phase lag at the nominal frequency as was produced for N1LAT at its nominal frequency. For example, time delay of .2 sec will produce 23.0 degrees of phase lag at N1LAT's natural frequency of 2.0 rad/sec. Equivalently, a time delay of .08 sec will also produce 23.0 degrees of phase lag at N2LAT's natural frequency of 5.0 rad/sec. Time delay values of .2, .3 and .4 sec were also investigated for N2LAT. The time delays added to each nominal system, together with the added phase lag at the natural frequency, are tabulated below.

NADC-79141-60

Time delay for N1LAT, Sec	.1	.2	.3	.4			
Time delay N2LAT, Sec	.05*	.08	.12	.16	.2	.3	.4
Phase Lag At Natural Frequency, Degrees	11 (14*)	23	34	46	57	86	115

*A value of .05 seconds was used for computational simplicity instead of the true equivalent of .04 seconds.

III RESULTS OF THE SIMULATION

1. EFFECTS OF THE DISPLAY - The VITAL IV display was considered by the pilots to be very realistic. Of the types of display available, the twilight scene appeared the most realistic for simulating conditions close to the ground. In the bright daylight scene, additional surface detail and texture seemed to be needed. The night scene was highly realistic, with lights on surrounding runways, taxiways, structures and distant city lights, but the ground plane was not visible. In this respect, the night scene was an excellent simulation of operation close to the ground without a landing light. However, the twilight scene, with both ground plane simulation and the ground lights, offered the best combination of cues.

The refresh rate in the display was 20 Hz. The pilots commented that this produced slight but noticeable stair-stepping for N2LAT, which was deliberately chosen to be rapid. This effect did not appear to degrade the flying qualities. One pilot, who was experienced in the X-22 in-flight simulator, felt an additional unnatural effect, possibly due to vestibular conditioning, which he thought was not solely due to the high bandwidth of N2LAT.

Altitude cues were noticeably weaker in the outside world display than in actual flight. The heads-up display (HUD) replaced this cue to a large extent, however, additional information (for example altitude rate on the HUD) would be helpful for simulation of actual touchdown.

The pilots attempted to extrapolate the simulation to actual touchdown. In their opinion, some of the systems rated Level 1 and Level 2 for hovering and low speed conditions would be less satisfactory in actual touchdown. The following results should be viewed with this in mind.

2. PILOT COMMENTS AND RATINGS - Table 2 summarizes all the rating data for all configurations. Appendix B contains the pilot comments in full. All the pilot rating plots which follow show the average rating for each pilot.

3. CALCULATION OF MISMATCHES - Wherever mismatches are mentioned, a MCAIR frequency response computer program was used. This program calculates the mismatch between two systems expressed as the sum of squared differences in gain and phase, using

$$\frac{20}{n} \sum (\text{Gain}_{\text{HOS}} - \text{Gain}_{\text{LOS}})^2 + .02 (\text{Phase}_{\text{HOS}} - \text{Phase}_{\text{LOS}})^2$$

where n is the number of frequencies chosen within the frequency range of match.

TABLE 2. LIST OF CONFIGURATIONS AND PILOT RATINGS

Config	Nominal			Nuisance Mode					Pilot Rating			
	Gain	ζ	ω_n	τ (Equiv ϕ)	λ	ζ_N	ζ_D	ω_L or DP	A	B	C	D
N1LAT	0.6 0.45	0.7 ↓	2.0 ↓	— —	— —	— —	— —	— —	— 4,4,4,4,3,3,3,2,3, 3,3,3,4,3,3,3,2,2, 5,4	4.5,4,3.5 3.5,3,4,3.5 3.5	7,5	4,7,4
N2LAT	0.3 0.3	↓ ↓	↓ 5.0	— —	— —	— —	— —	— —	— 4,4,4,4,5,3,3,3,3, 3,3,5,4,4,5,4,3,	3.5,5 6.5,5,3.5,5 5.5	5,4	3 5
HF111	0.45	↓	2.0	—	1.0	—	—	—	7,7,9,7			
HF112	↓	↓	↓	—	2.0	—	—	—	5,8,6,6			
HF113	↓	↓	↓	—	3.0	—	—	—	6,4,3,5,6			
HF114	0.6 0.45	↓ ↓	↓ ↓	— —	4.0 ↓	— —	— —	— —	— 5,6	4		
HF115	0.3 0.45	↓ ↓	↓ ↓	— —	5.0 ↓	— —	— —	— —	— 5,4	3.5	6	
HF116	0.6 0.45	↓ ↓	↓ ↓	— —	6.0 ↓	— —	— —	— —	— 5	4,5 4,5		5
HF117	0.3	↓	↓	—	7.0	—	—	—	—	6		
HF124	0.6 0.45	↓ ↓	↓ ↓	— —	— —	— —	0.3 ↓	4.0 ↓	— 6	6 7,5		
HF125	0.6 0.45 0.3	↓ ↓ ↓	↓ ↓ ↓	— — —	— — —	— — —	— — —	5.0 ↓ ↓	— 5 6	— 6 —		7,5
HF126	0.45	↓	↓	—	—	—	—	6.0	6,5	4,4		
HF127	↓ 0.3	↓ ↓	↓ ↓	— —	— —	— —	— —	7.0 ↓	7,6	— 5,5		
HF128	0.45	↓	↓	—	—	—	—	8.0	4,5			
HF129	↓	↓	↓	—	—	—	—	9.0	3,4,4,4			
HF120	↓	↓	↓	—	—	—	—	10.0	5,5,3,4			
HF121	↓	↓	↓	—	—	—	—	11.0	6,4,5			

GP03-0208-33

TABLE 2. (Continued) LIST OF CONFIGURATIONS AND PILOT RATINGS

	Nominal			Nuisance Mode					Pilot Rating			
Config	Gain	ζ	ω_n	τ (Equiv ϕ)	λ	ζ_N	ζ_D	ω_L or DP	A	B	C	D
HF1T1	0.6	0.7	2.0	0.1 (11.46°)	—	—	—	—				6
	0.45			↓	—	—	—	—	4,2			
	0.3			↓	—	—	—	—		5		
HF1T2	0.45			0.2 (22.92°)	—	—	—	—	7,7	6.5	6	
HF1T3	0.6			0.3 (34.38°)	—	—	—	—		4		
	0.45			↓	—	—	—	—	7	5.5		
HF1T4	0.3			0.4 (45.84°)	—	—	—	—		7		
	0.45			↓	—	—	—	—	7			
LF121	0.45			—	—	0.2	0.7	0.1	3		4	
LF123	↓			—	—	↓	↓	0.3	2,3			
LF125	↓			—	—	↓	↓	0.5	3,4			
LF127	↓			—	—	↓	↓	0.7	4,7		8	
LF121*	0.6			—	—	—	0.05	0.1				3
LF123*	↓			—	—	—	↓	0.3				7
LF125*	↓			—	—	—	↓	0.5				10
LF127*	↓			—	—	—	↓	0.7				10
HF211	0.3		5.0	—	1.0	—	—	—	6,6,5,6,6			
HF212	↓		↓	—	2.0	—	—	—	2,3,3,5			
HF213	↓		↓	—	3.0	—	—	—	3,4,3,3			
HF214	↓		↓	—	4.0	—	—	—	3	3.5		
HF215	↓		↓	—	5.0	—	—	—	3	3,4,5	5	
HF216	↓		↓	—	6.0	—	—	—	3	4		
HF217	↓		↓	—	7.0	—	—	—	3		5	
HF224	↓		↓	—	—	—	0.3	4.0	7	5		
HF225	↓		↓	—	—	—	↓	5.0		7,8	7	
HF226	↓		↓	—	—	—	↓	6.0	6,6	5.5		
HF227	↓		↓	—	—	—	↓	7.0	6	5,6	6	
HF228	↓		↓	—	—	—	↓	8.0	8,4,4,6			
HF229	↓		↓	—	—	—	↓	9.0	5,4,3			
HF220	↓	↓	↓	—	—	—	↓	10.0	4,8,3			

*Exaggerated rooftop systems

GP03-0208 32

TABLE 2. (Concluded) LIST OF CONFIGURATIONS AND PILOT RATINGS

Config	Nominal			Nuisance Mode					Pilot Rating			
	Gain	ζ	ω_n	τ (Equiv ϕ)	λ	ζ_N	ζ_D	ω_L or DP	A	B	C	D
HF221	0.3	0.7	5.0	—	—	—	0.3	11.0	7,4,2,4			
HF2T1				0.05 (14.33°)	—	—	—	—	3	3,4,5	5	
HF2T2				0.08 (22.92°)	—	—	—	—	2,3	5		
HF2T3				0.12 (34.38°)	—	—	—	—	3	5		
HF2T4				0.16 (45.84°)	—	—	—	—	5,5,5,5	6.5		
HF2T5				0.2	—	—	—	—	6,6			
HF2T6				0.3	—	—	—	—	8,5,5			
HF2T7				0.4	—	—	—	—	8,9			
LF221				—	—	0.2	0.7	0.1	3			
LF223				—	—			0.3	4		8	
LF225				—	—			0.5	6			
LF227				—	—			0.7	6			
LF221*				—	—	—	0.05	0.1				5
LF223*				—	—	—		0.3				
LF225*				—	—	—		0.5				
LF227*				—	—	—		0.7				
G110	1.0		2.0	0 (0°)	—	—	—	—	3,2,3,2			
G111				0.1 (11.46°)	—	—	—	—	6,6			
G112				0.2 (22.92°)	—	—	—	—	8,5,8,7	6		
G113				0.3 (34.38°)	—	—	—	—	7	10		
G120	0.2			0 (0°)	—	—	—	—	7,7			
G121				0.1 (11.46°)	—	—	—	—	7,7			
G122				0.2 (22.92°)	—	—	—	—	7,7,4	7		
G180	0.8			0 (0°)	—	—	—	—	2,4			
G186				0.06 (6.88°)	—	—	—	—	4,4			
G188				0.08 (9.168°)	—	—	—	—	2,2			
G181				0.1 (11.46°)	—	—	—	—	6,5			

*Exaggerated rooftop systems

GP03-0208-31

4. LOW FREQUENCY DYNAMICS - The 'rooftop' system caused control difficulties for natural frequencies above 0.1 rad/sec. With an attitude system, and the need for steady state inputs, the reduction in low frequency gain due to the 40 dB/decade roll off appeared to be the culprit. A typical pilot comment was that the control system removed the pilots' input, and eventually the aircraft could be translating to the left, with the control held over to the right stop. These difficulties probably would not have occurred with a translation rate command system, since a steady attitude would not be required for a steady translation rate. This is confirmed by the good ratings obtained with rooftop systems and translation rate control systems in Reference 9.

For the low frequency dipole, the variation of pilot rating with increasing ω_{dp} is shown in Figures 14 and 15. This establishes the allowable low frequency mismatch. It also defines the low frequency threshold for this task, for these nominal dynamics, and for this dipole mode, as follows.

The mismatch between the high order system (nominal plus dipole) and the low order system (nominal alone) was determined for each simulated value of ω_{dp} using a MCAIR frequency response program in a frequency range of 0.1 to 10.0 rad/sec. Mismatch was then compared with the high order system average pilot rating. Figure 16 presents average pilot rating versus mismatch for increasing ω_{dp} . A large mismatch increase for ω_{dp} values between 0.1 to 0.3 rad/sec did not affect the pilot rating. Between 0.3 and 0.5 rad/sec a small change in mismatch occurred but the pilot rating began to be affected. Mismatch was constant for ω_{dp} values above 0.5 rad/sec because all the high order effect of the dipole was contained within the match range. Pilot rating had degraded significantly when ω_{dp} reached 0.7 rad/sec for N1LAT and 0.5 rad/sec for N2LAT. Mismatch values greater than 413 resulted in pilot rating degradation as indicated in Figure 16.

There are two ways of stating this result:

- (1) An added dipole of the form $\frac{[.2; \omega_{dp}]}{[.7; \omega_{dp}]}$ will not

significantly degrade nominal V/STOL attitude dynamics for $\omega_{dp} < .5$ rad/sec.

- (2) A nominal attitude equivalent system with a low frequency, dipole-like mismatch of less than about 400, will adequately model the attitude dynamics for flying qualities analysis of the V/STOL system.

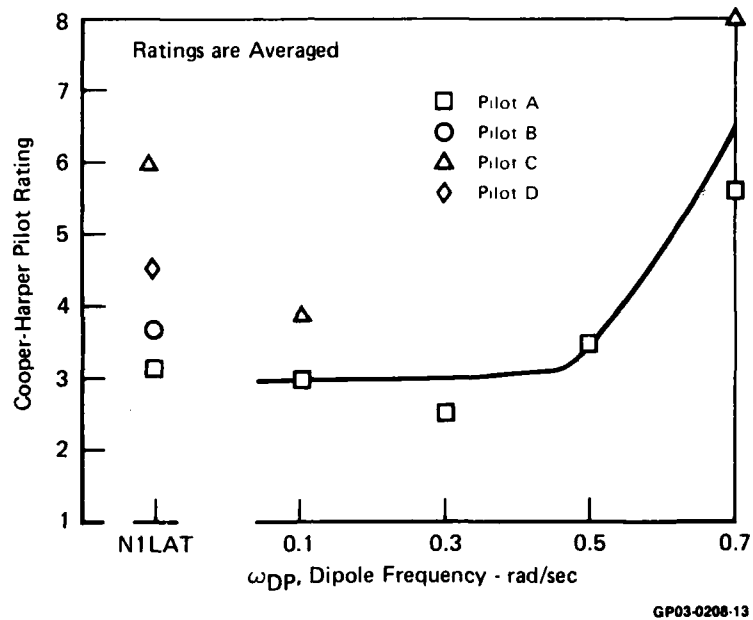


Figure 14. Effect of Dipole Frequency on Pilot Rating
N1LAT

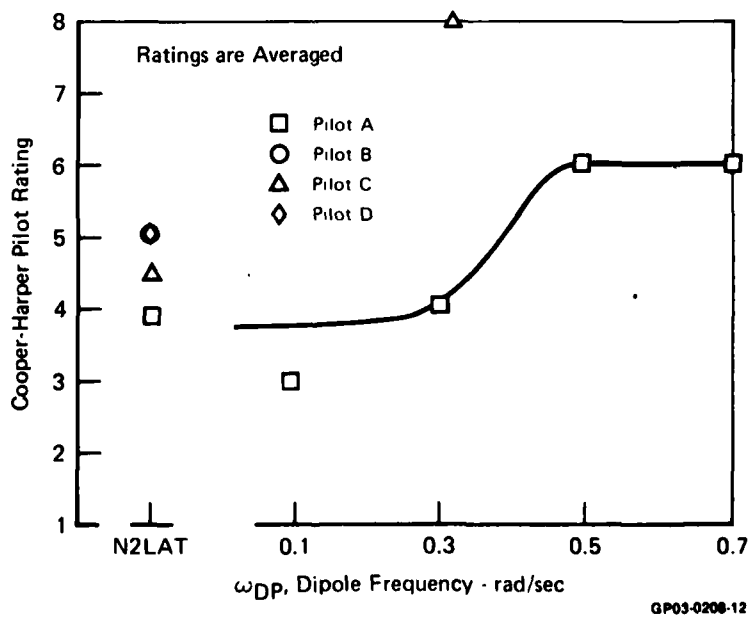
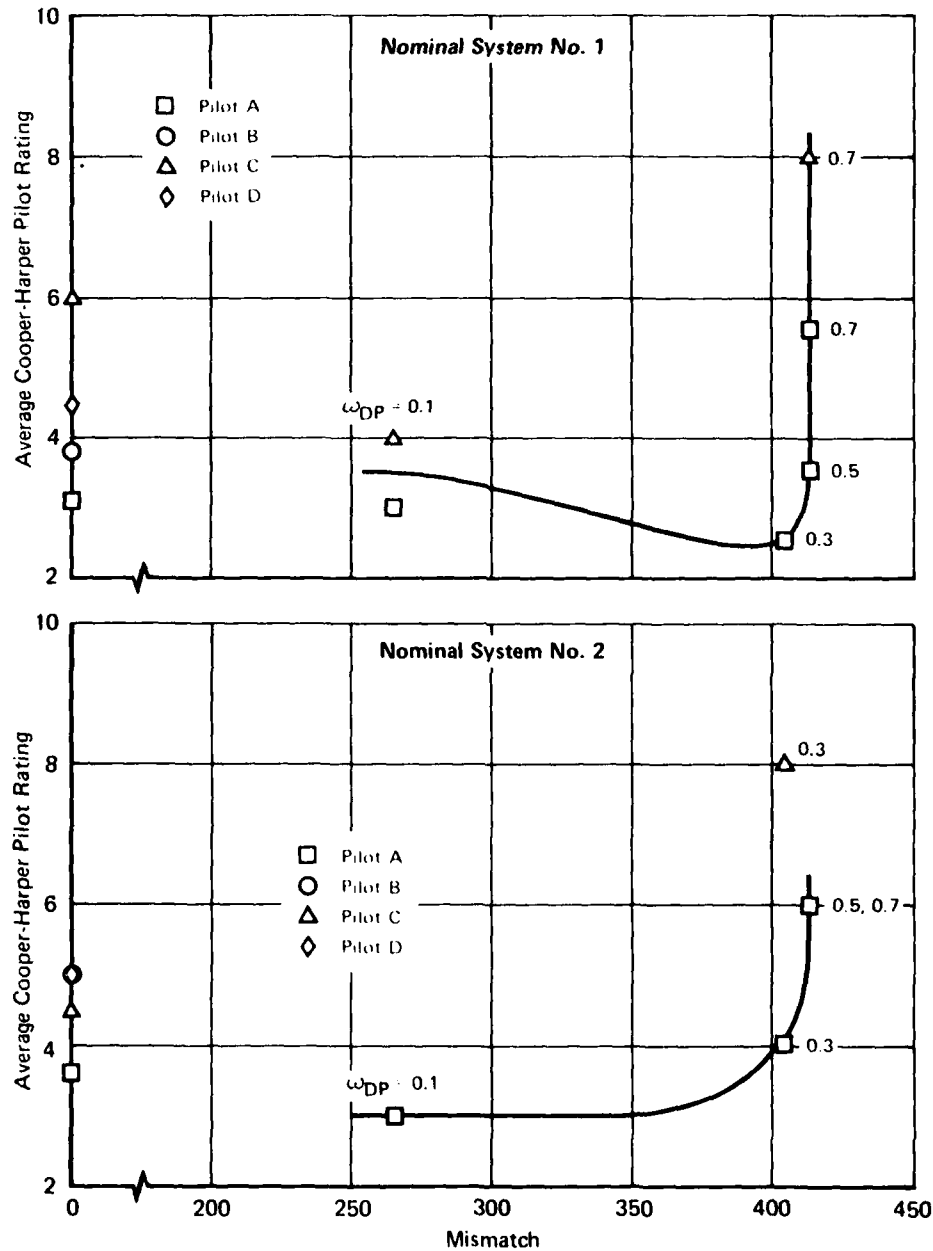


Figure 15. Effect of Dipole Frequency on Pilot Rating
N2LAT



GP03 0208 22

Figure 16. Comparison of Average Pilot Rating and Mismatch for a Dipole Mode Added to N1LAT and N2LAT
 Match Frequency Range: 0.1 — 10 Rad/Sec
 Ratings are Averaged

This result is reasonably consistent with the earlier MCAIR study of Reference 12. In that study, a lower match frequency of 0.4 rad/sec was used to eliminate a low frequency mode which, though an apparent contaminant to the basic rate response, did not affect the pilot ratings. It was a low frequency instability rather than a dipole. Expanding the match range to 0.1 rad/sec to 10.0 rad/sec and using a first order lag to match the Reference 12 pitch rate response produces a mismatch less than 400.

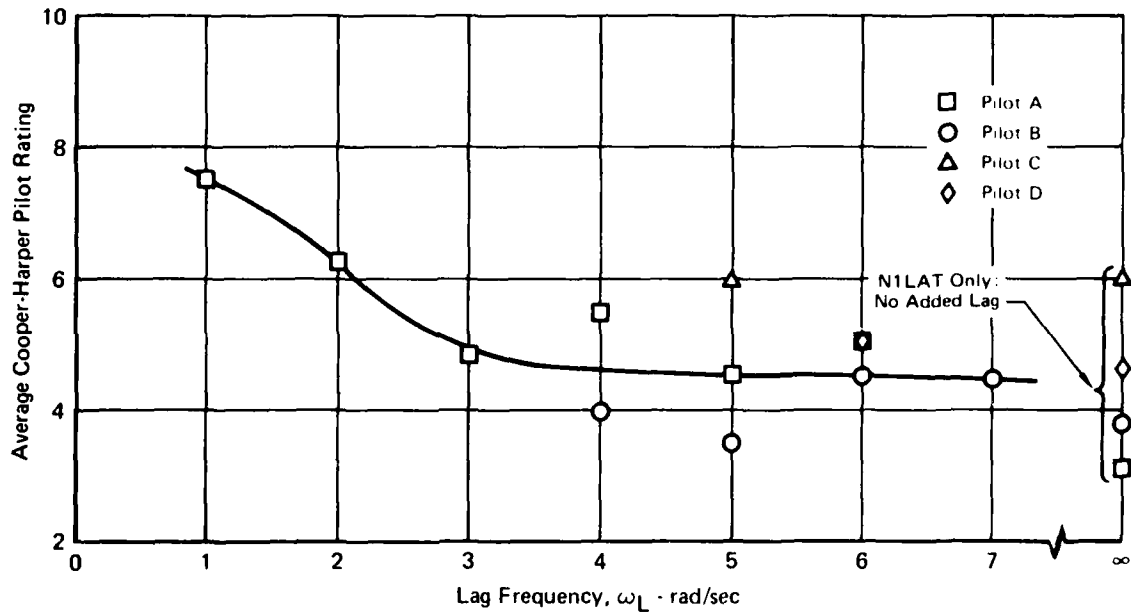
5. HIGH FREQUENCY DYNAMICS

a. First Order Lags - The effect on average rating of adding a first order lag to the nominal systems is shown in Figures 17 and 18. Adding lag to N1LAT (.708/[.7; 2.0]) degraded the pilot rating at all break frequencies investigated. The rating degraded sharply for break frequencies below 3 rad/sec and reached the Level 2-3 boundary for a break frequency of 2 rad/sec. The rating was 7.5, Level 3, when the break frequency was 1 rad/sec. Adding lag to N2LAT (2.95/[.7; 5.0]) at first improved the pilot rating, with an eventual degradation for large (low frequency) lags. This improved pilot rating is possibly because the lag acts as a prefilter and smoothes out the relatively abrupt N2LAT responses. However, CTOL experience suggests caution in evaluating the rating improvement due to the first order lag prefilter. A more demanding task, in particular an actual touchdown, might show severe piloting problems even for the higher break frequencies. Therefore, the degradation in rating of N1LAT for a break frequency of 7 rad/sec is taken as a minimum threshold for this type of added high frequency effect.

The mismatch between the high order system (nominal plus first order lag) and the low order system (nominal alone) was computed for each simulated value of λ using a MCAIR frequency response program in two frequency ranges of 0.1 to 10 rad/sec and 0.5 to 10.0 rad/sec. Mismatch was then compared with the average pilot rating. Figures 19 and 20 present average pilot rating versus mismatch for increasing λ for the nominal systems. Mismatch increased steadily with decreasing lag frequency. Using a threshold frequency of 7 rad/sec, the corresponding mismatches were:

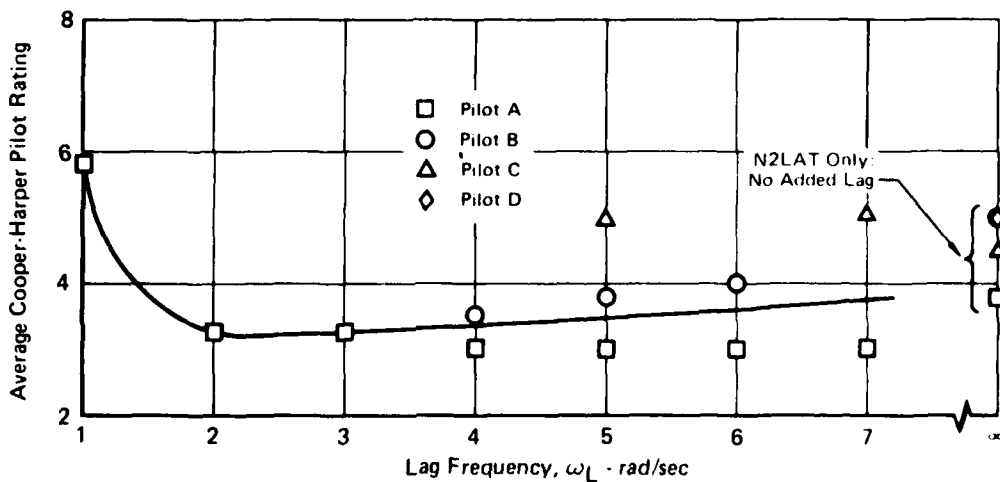
<u>Frequency Range</u>	<u>Maximum Allowable Mismatch</u>
0.1 to 10 rad/sec	230. (data not shown)
0.5 to 10 rad/sec	330.

Figure 20 presents the comparison of rating and mismatch for a first order lag added to N2LAT. Since the rating improvement with increasing mismatch may be due to the prefilter effect, the previous Figure, showing N1LAT data, was used to establish the threshold. Since the selected threshold frequency was at the limit of the available data, the maximum allowable mismatch may very well be lower than that listed above.



GP03-0208-30

Figure 17. Effect on Pilot Rating of Adding a 1st Order Lag to N1LAT



GP03-0208-29

Figure 18. Effect on Pilot Rating of Adding a 1st Order Lag to N2LAT

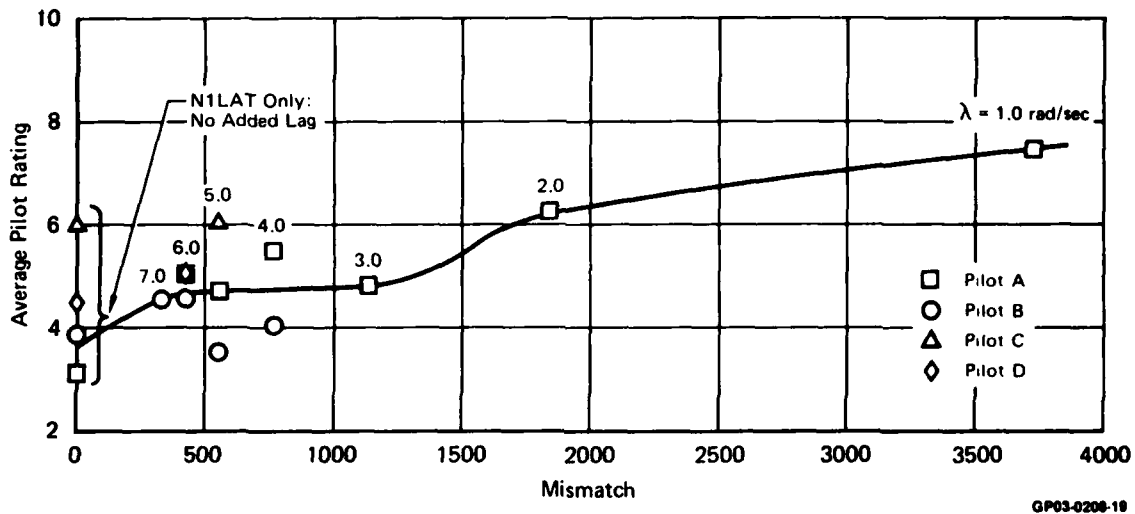


Figure 19. Comparison of Average Pilot Rating and Mismatch for a First Order Lag Added to N1LAT
Match Frequency Range: 0.5 - 10 Rad/Sec

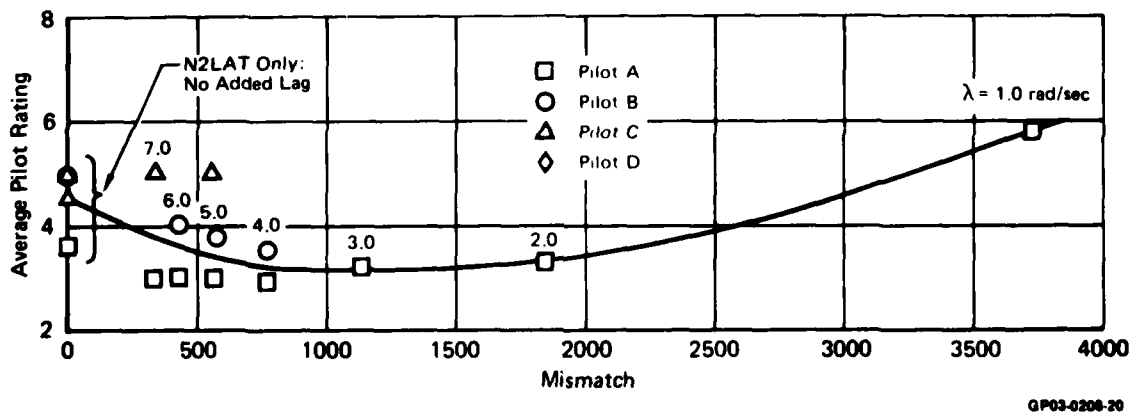


Figure 20. Comparison of Average Pilot Rating and Mismatch for a First Order Lag Added to N2LAT
Match Frequency Range: 0.5 - 10 Rad/Sec

b. Second Order Lags - Figures 21 and 22 present the effects of a second order lag added to the nominal systems. As the lag frequency was decreased, the pilot rating degraded. The N1LAT data indicate a slight degradation in rating even for the small (high frequency) lags, with N2LAT showing an initial slight improvement. However, a conservative threshold would be a limit on second order lags below 10 rad/sec. Again, the threshold here is defined as being where the pilot rating of the nominal plus second order lag is equivalent to the pilot rating of the nominal alone.

Mismatch was computed using the same method for the simulated values of ω_L as was used for first order lags. Figures 23 and 24 present pilot rating versus mismatch for the simulated ω_L for both nominal systems. As with the first order lags, mismatch increased steadily with decreasing ω_L and pilot rating degraded as mismatch increased. Using a threshold frequency of 10 rad/sec, the corresponding mismatches were:

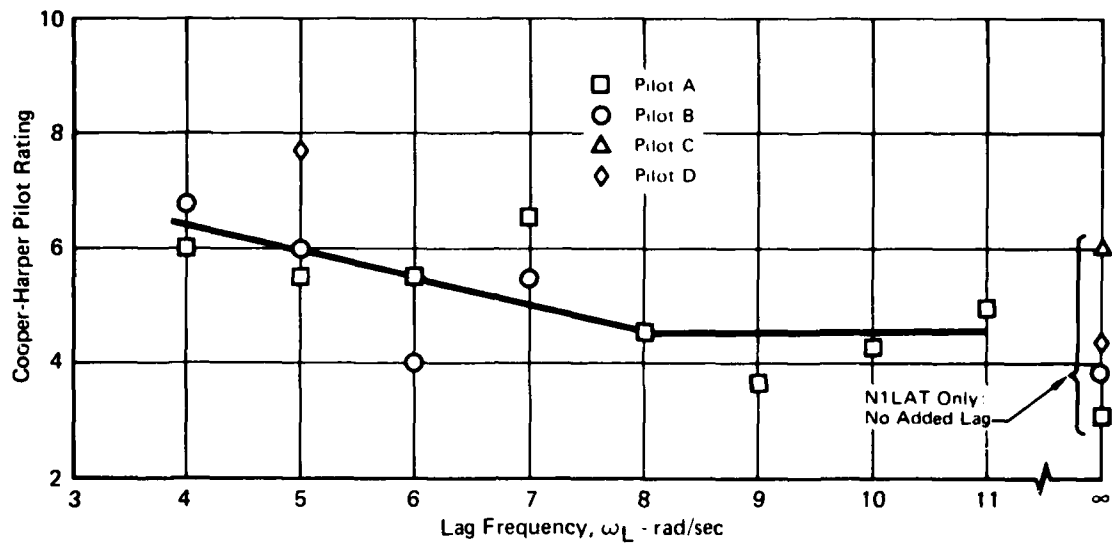
<u>Frequency Range</u>	<u>Maximum Allowable Mismatch</u>
0.1 to 10 rad/sec	260. (data not shown)
0.5 to 10 rad/sec	360.

c. Transport Lags - The effect of pure time delay on pilot opinion rating is presented for both nominal systems in Figure 25. Pilot rating degraded for $\tau > .10$ sec. The results follow a trend similar to that seen in CTOL landing data (Reference 8).

The time delay values do not include the computational time (.008 sec), the sample rate (20 Hertz) nor the equivalent delay due to the stick (.009 sec). The time delay values shown are only the amount of pure time delay added to the system. This is equivalent to ignoring an additional equivalent time delay of $.008 + 1/2(.05) + .009 = .042$ seconds.

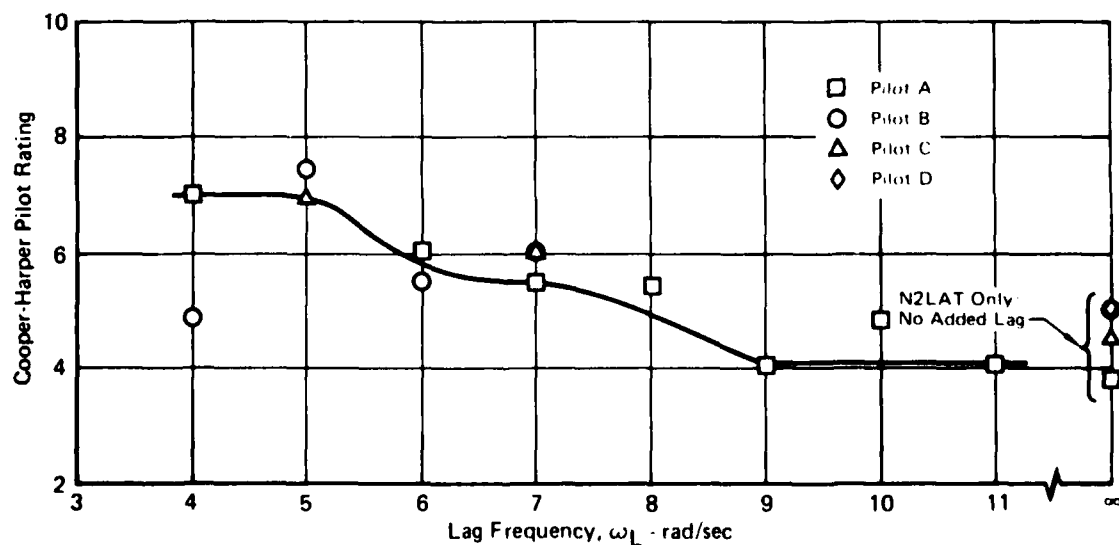
Mismatch was computed in the same manner as for first and second order lags. Time delay versus mismatch is shown in Figure 26. Average pilot ratings are listed next to each data point. The mismatch contribution due to a time delay is $57.3 (\omega\tau)^2$, with the summation taken over the chosen frequencies. The mismatch is in phase alone. Figures 25 and 26 indicate a mismatch value above 200 ($\tau = .10$) is significant.

6. PILOTING EFFECTS OF PURE TIME DELAY VS PHASE LAG - MCAIR research on augmented CTOL dynamics has investigated whether phase lag at the configuration natural frequency is a more appropriate correlating parameter than delay, (Reference 4). MIL-F-8785B requirements on surface phase lag at the configuration natural frequency imply that a given delay will be more troublesome at higher basic configuration natural frequencies. The requirements are based on the conventional airplane data of DiFranco (Reference 13). However, later results indicate that a given delay will produce a given rating degradation regardless of configuration natural frequency (References 4 and 14). The observed sensitivity of rating to delay is not consistent with the previously held observation that piloted crossover frequency is in the 1. -3. radians/second range, i.e., roughly in the usual range of configuration natural frequencies. At these relatively low frequencies, significant delays introduce apparently insignificant phase lags.



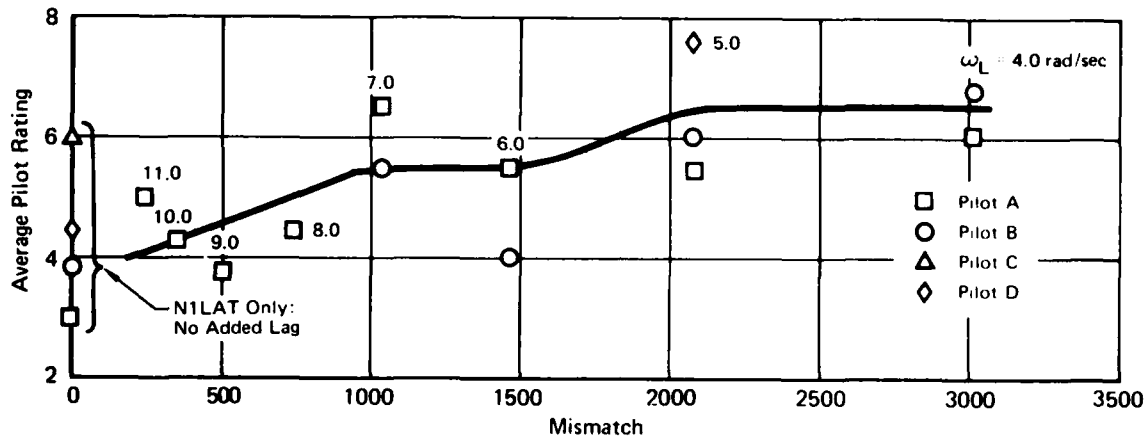
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Figure 21. Effect on Pilot Rating of Adding a 2nd Order Lag to N1LAT



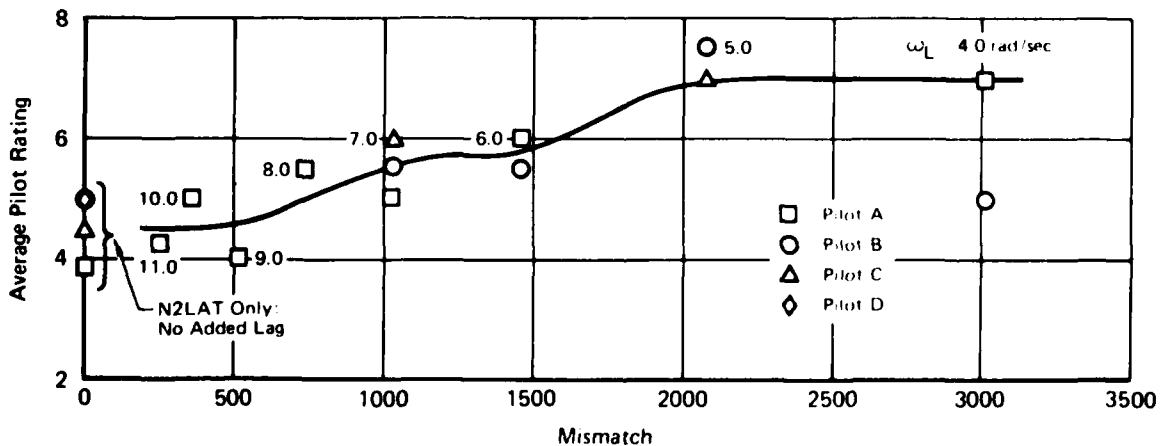
GP03-0208-27

Figure 22. Effect on Pilot Rating of Adding a 2nd Order Lag to N2LAT



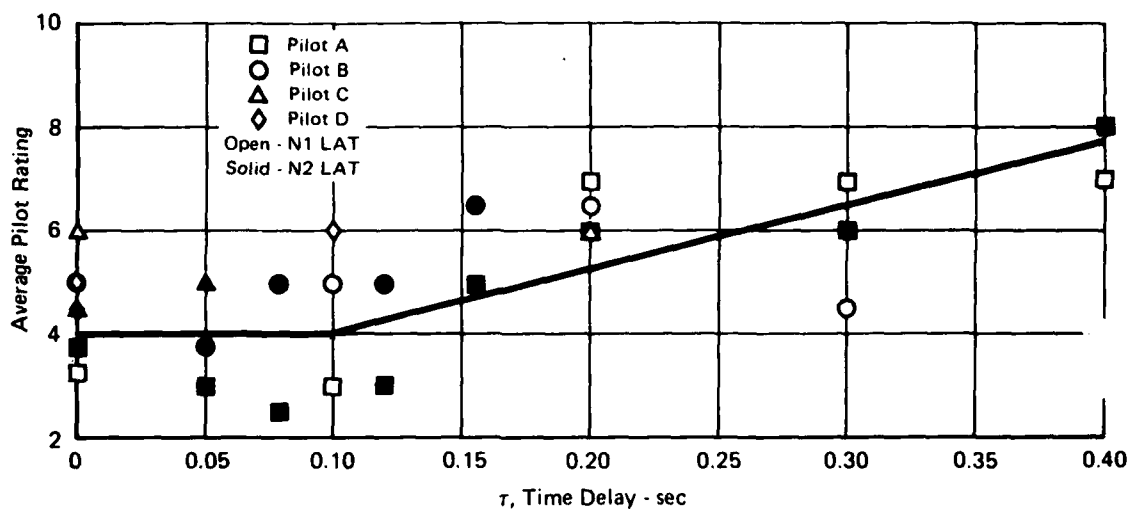
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Figure 23. Comparison of Average Pilot Rating and Mismatch for a 2nd Order Lag Added to N1LAT
Match Frequency Range: 0.5 - 10 Rad/Sec



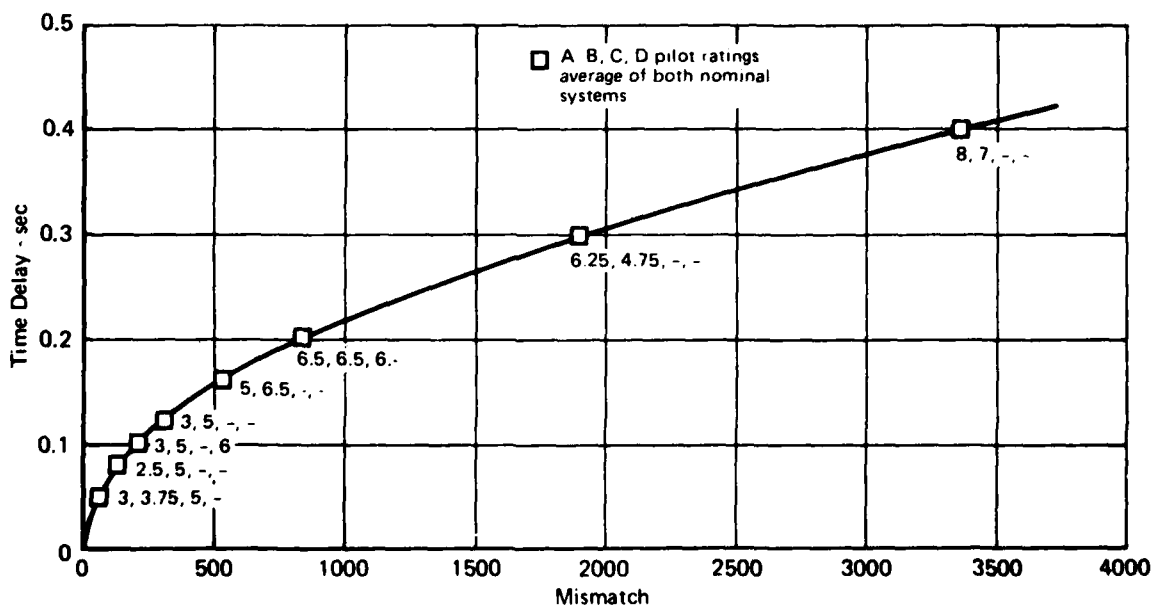
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Figure 24. Comparison of Average Pilot Rating and Mismatch for a 2nd Order Lag Added to N2LAT
Match Frequency Range: 0.5 - 10 Rad/Sec



GP03-0208-24

Figure 25. Effect of Pure Time Delay on Pilot Rating
Ratings from Both Nominal Systems



GP03-0208-23

Figure 26. Effect of Time Delay on Mismatch
Match Range: 0.5-10 Rad/Sec

To gather data in this area, pure time delay was added to N1LAT and N2LAT. The time delay added to N2LAT produced the same amount of phase lag at its nominal frequency as was produced for N1LAT at its nominal frequency as described in Section II-9-c.

Table 3 presents the time delay and phase lag values explored. Pilot rating versus phase angle is presented in Figure 27. The data show a rating degradation with lag but the pilot rating for a given lag is worse (larger) for the configuration with the lower natural frequency. Since a given delay produces a larger phase lag at a higher natural frequency, the rating is more likely a function of delay, not lag.

7. HIGH ORDER FLIGHT PATH DYNAMICS - The question of whether pilots desire low order attitude responses has been answered in Sections III-4, 5 and 6. Some configurations were evaluated to determine whether the results were dependent on the flight path characteristics. As is pointed out in Reference 1, there is an interaction between attitude and flight path dynamics which can result in high-order-appearing responses and degraded ratings.

The nominal lateral flight path bandwidth, Y_v , value was $-.1$ which was used through the majority of the simulation. A few representative runs were made with $Y_v = -.2$. The data indicate the pilot did not notice any type of degradation or improvement in the aircraft handling with the change in Y_v . Because of this result, the two data sets are combined with no distinction between the two. The configurations which were run with $Y_v = -.2$ are distinguished in the listing in Appendix B. Time did not permit further investigation of different Y_v values.

8. EFFECT OF COMMAND GAIN/TIME DELAY INTERACTIONS - The effects on pilot rating of a variation in command gain and time delay for N1LAT are shown in Figure 28. Command gains investigated were .079, .118, .177 (nominal), .236, .315 and .394 rad/cm with time delay varying from 0.0 to .4 sec.

Figure 28 shows that low gain (.079) causes a rating of 7 with no degradation due to time delay. Pilot comments showed that with low gain, the task required a large workload regardless of delay.

For a high gain (.394), the baseline dynamics were excellent but time delay produced an immediate degradation in pilot rating. The addition of only 0.1 sec time delay degraded the rating from 2.5 to 6. Further addition of time delay to the high gain case eventually caused loss of control.

With a high gain, the pilot was unable to detach himself from the task and time delay produced a sharp degradation in pilot rating. Ratings of low command gains were affected less by added time delay; the ratings remained poor. Up to 0.2 sec time delay can be tolerated in moderate command gain situations. This trend is also evident in CTOL data (Reference 8).

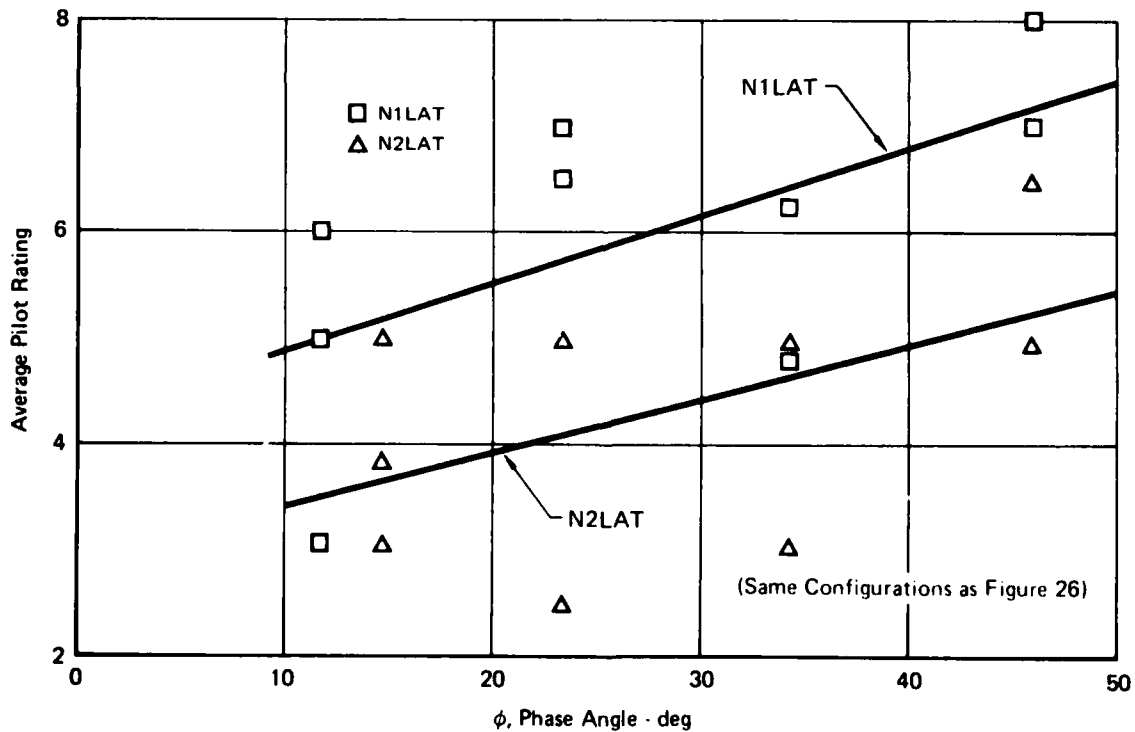
TABLE 3. TIME DELAY vs PHASE LAG

Summary of Results

τ	ω_n	ϕ^0	Pilot Rating
0.1	2.0 (N1LAT)	11.46	3, 5, 6
0.2		22.92	6.5, 6.5, 7
0.3		34.38	4.75, 6.25
0.4		45.84	8, 7
0.05	5.0 (N2LAT)	14.33	3, 3.75, 5
0.08		22.92	2.5, 5
0.12		34.38	3, 5
0.16		45.84	6.5, 5

$$\phi = \omega_n \tau (57.3)$$

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GP03-0208-10

Figure 27. Effect of Phase Lag on Average Pilot Rating

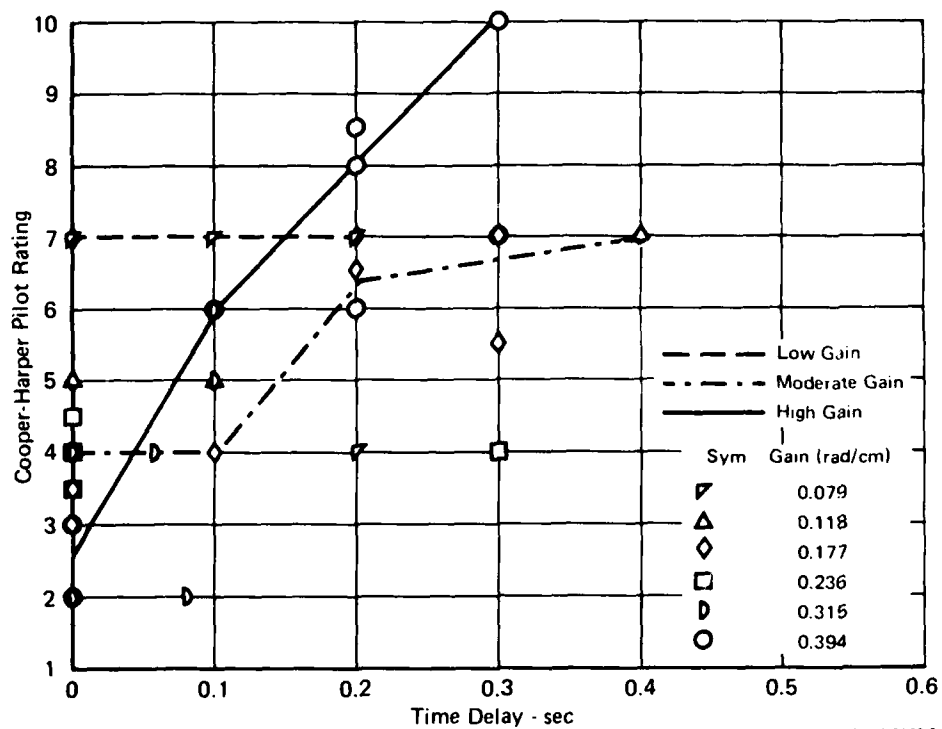


Figure 28. Interaction of Command Gain and Time Delay
Baseline Dynamics: [0.7; 2.0]

Figure 29 presents the same data as a set of curves for increasing time delay. This shows the expected U-shaped rating variation with gain as the gain progresses from insensitivity, through optimum, to oversensitivity.

9. EQUIVALENT SYSTEMS ANALYSIS OF HIGH FREQUENCY EFFECTS - As stated in Reference 1, a large class of attitude augmented VTOL's possess attitude dynamics which can be approximated by:

$$\frac{K e^{-\tau_e s}}{s^2 + 2\zeta_e \omega_e s + \omega_e^2}$$

This function was matched in the frequency range of 0.1 to 10.0 rad/sec to each high order configuration generated by adding high frequency lags or delays to N1LAT and N2LAT. The parameter τ_e is an equivalent time delay which chiefly approximates the phase lag contribution of the high frequency first and second order elements in the high order system. The results appear in Table 4. The great majority of cases were matched quite closely. Figure 30 presents average pilot rating versus τ_e . The shaded areas represent the three levels of flying qualities. The time delay boundaries for these areas were determined from the results of the transport lag (actual time delay) variation of Figure 25. The equivalent time delay data fall mostly within these transport lag boundaries, tending to validate equivalent delay as a flying qualities parameter. The data which lie outside the boundaries are good matches and, like all the equivalents, possess Level 1 gain values. However, they are borderline Level 1 according to the ω_n vs. $2\zeta_n \omega_n$ criteria established in Reference 1. This together with the additional flying qualities degradation due to equivalent time delay puts these data in Levels 2 and 3.

These data show that the total equivalent configuration (ζ_e , ω_e , τ_e , K) must be assessed very carefully. Even though each element of the equivalent configuration may meet its Level 1 criterion, the total equivalent configuration may not be Level 1. A cautionary note on this 'multiple degradation' effect should be included in any formal specification of VTOL flying qualities.

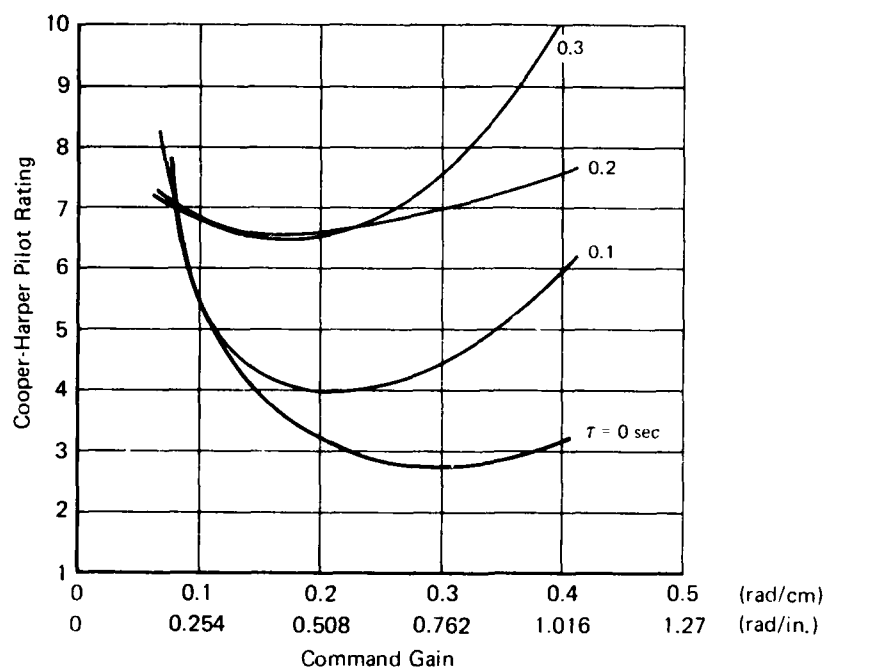


Figure 29. Variation of Pilot Rating with Command Gain and Time Delay

TABLE 4. EQUIVALENT SYSTEMS PARAMETERS

Configuration	HOS			LOS				Average Pilot Rating
	ζ	ω	λ	ζ	ω	τ	Mis-Match	
HF111	0.7	2	1	0.4793	1.0869	0.1585	159.0	7.5
HF112	0.7	2	2	0.4791	1.3499	0.1424	98.9	6.25
HF113	0.7	2	3	0.5039	1.5091	0.1290	63.4	4.8
HF114	0.7	2	4	0.5312	1.6166	0.1176	41.9	5.5, 4
HF115	0.7	2	5	0.5560	1.6938	0.1078	28.4	3.5, 6
HF116	0.7	2	6	0.5773	1.7511	0.0993	19.7	5, 4.5, 5
HF117	0.7	2	7	0.5951	1.7948	0.0919	14	4.5
HF211	0.7	5	1	0.9776	1.9995	0.1105	24.6	5.8
HF212	0.7	5	2	0.7826	2.6636	0.1022	17.1	3.25
HF213	0.7	5	3	0.7146	3.1080	0.0950	12	3.25
HF214	0.7	5	4	0.6853	3.4351	0.0887	8.55	3, 3.5
HF215	0.7	5	5	0.6722	3.6874	0.0830	6.17	3, 3.75
HF216	0.7	5	6	0.6669	3.8871	0.0779	4.51	3, 4
HF217	0.7	5	7	0.6654	4.0481	0.0733	3.35	3, 5
HF124	0.7	2	—	0.3722	1.9622	0.3113	453	6, 6.75
	0.3	4						
HF125	0.7	2	—	0.4992	2.1550	0.2847	256	6, 6, 7.5
	0.3	5						
HF126	0.7	2	—	0.6295	2.3167	0.2589	135	5.5, 4
	0.3	6						
HF127	0.7	2	—	0.7525	2.4422	0.2330	65.9	6.5, 5.5
	0.3	7						
HF128	0.7	2	—	0.8511	2.5136	0.2061	32.0	4.5
	0.3	8						
HF129	0.7	2	—	0.9058	2.5135	0.1777	18.9	3.75
	0.3	9						
HF120	0.7	2	—	0.9122	2.4519	0.1492	15.4	4.25
	0.3	10						
HF121	0.7	2	—	0.8888	2.3680	0.1237	13.8	5
	0.3	11						
HF224	0.7	5	—	0.2534	3.3367	0.2386	126	7
	0.3	4						
HF225	0.7	5	—	0.2935	3.9785	0.2270	90.6	7, 8, 7
	0.3	5						
HF226	0.7	5	—	0.3474	4.5775	0.2152	60	6, 5.5
	0.3	6						
HF227	0.7	5	—	0.4139	5.1556	0.2034	36.1	5, 5.5, 6
	0.3	7						
HF228	0.7	5	—	0.4914	5.7226	0.1915	19.1	5.5
	0.3	8						
HF229	0.7	5	—	0.5757	6.2526	0.1787	8.8	4
	0.3	9						
HF220	0.7	5	—	0.6565	6.6474	0.1640	3.71	5
	0.3	10						
HF221	0.7	5	—	0.7165	6.7795	0.1466	1.84	4.25
	0.3	11						

GP03-0208 105

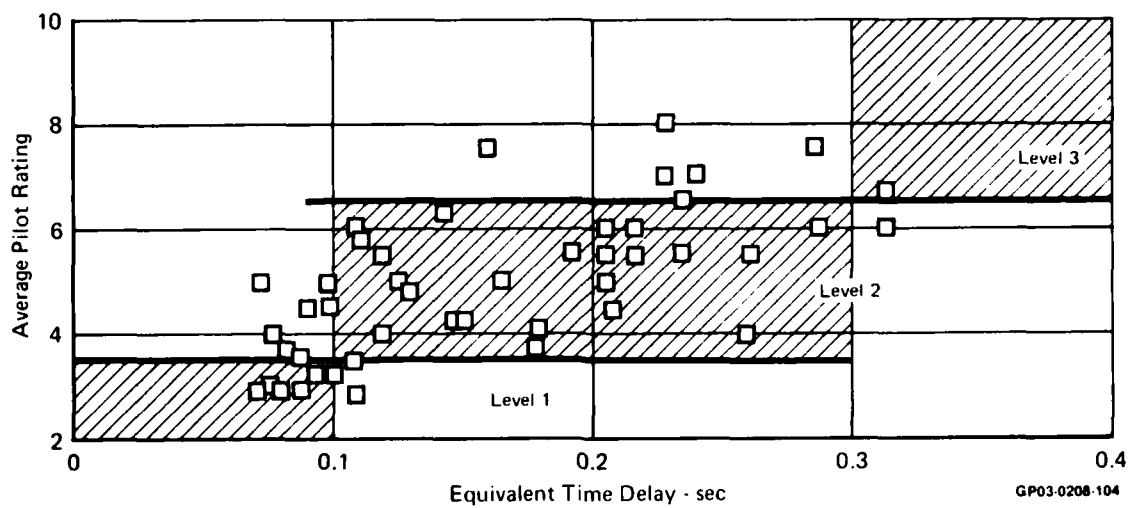


Figure 30. Variation of Average Pilot Rating with Equivalent Time Delay

IV SUMMARY AND CONCLUSIONS

A fixed-base simulation of attitude-type V/STOL dynamics in hovering and low speed flight was conducted. By adding high order effects to two nominal bank angle dynamic models, information was gained on allowable mismatches between high order and low order systems. The results show that it is reasonable to specify high order V/STOL dynamics in terms of low order equivalent system parameters. Mismatch levels for analytically derived equivalents will normally be far below the values of mismatch shown in this experiment to be noticeable to pilots. The general objective of gaining information on equivalents was tackled by asking four related questions. These are asked, and their answers given, below.

- (1) What is an allowable mismatch between the high order system and its low order equivalent?
- (2) What is the pilot's frequency range of interest?

Since mismatch is a function of frequency range, these questions are answered jointly.

The lower end of the frequency range was explored by adding two types of dynamics to the nominal systems. The first was a poorly damped mode with a low frequency gain roll-off and the second was a localized notch in the frequency response. Pilot comments indicated that both these high order effects ultimately degraded the nominal dynamics by reducing low frequency gain, or control effectiveness. The roll-off produced steadily decreasing gain, with zero steady state gain, and the notch produced a localized reduction of about 10dB. The flying qualities degradation due to the low frequency dynamics occurred when:

- (i) the local gain mismatch reached 10 dB in the frequency range .1 to .3 rad/sec (Figure A-24)
- (ii) similarly, a mismatch value of 400. due to low frequency effects alone was exceeded in the frequency range .1 to 10 rad/sec (Figure 16)
- (iii) a mismatch value of 100. was reached in the frequency range .5 to 10 rad/sec

Matching from .5 to 10 rad/sec is a way of de-emphasizing low frequency modes, i.e. a way of weighting the response match more towards the crossover region of piloted control.

The upper end of the pilot's frequency range was explored by adding one of three types of dynamics to the nominal systems; a first order lag, a second order lag, or a pure time delay. Values

of break frequency, natural frequency, and pure delay were established which caused a degradation in pilot rating.

The degradation due to the high frequency dynamics appeared when:

- (i) the local phase mismatch reached 20. degrees in the frequency range 4.0 to 10 rad/sec. (Figure A-17)
- (ii) similarly, a mismatch value of 260. due to high frequency effects alone was exceeded in the frequency range .1 to 10 rad/sec
- (iii) a mismatch value of 15. was reached in the frequency range .1 to 4 rad/sec

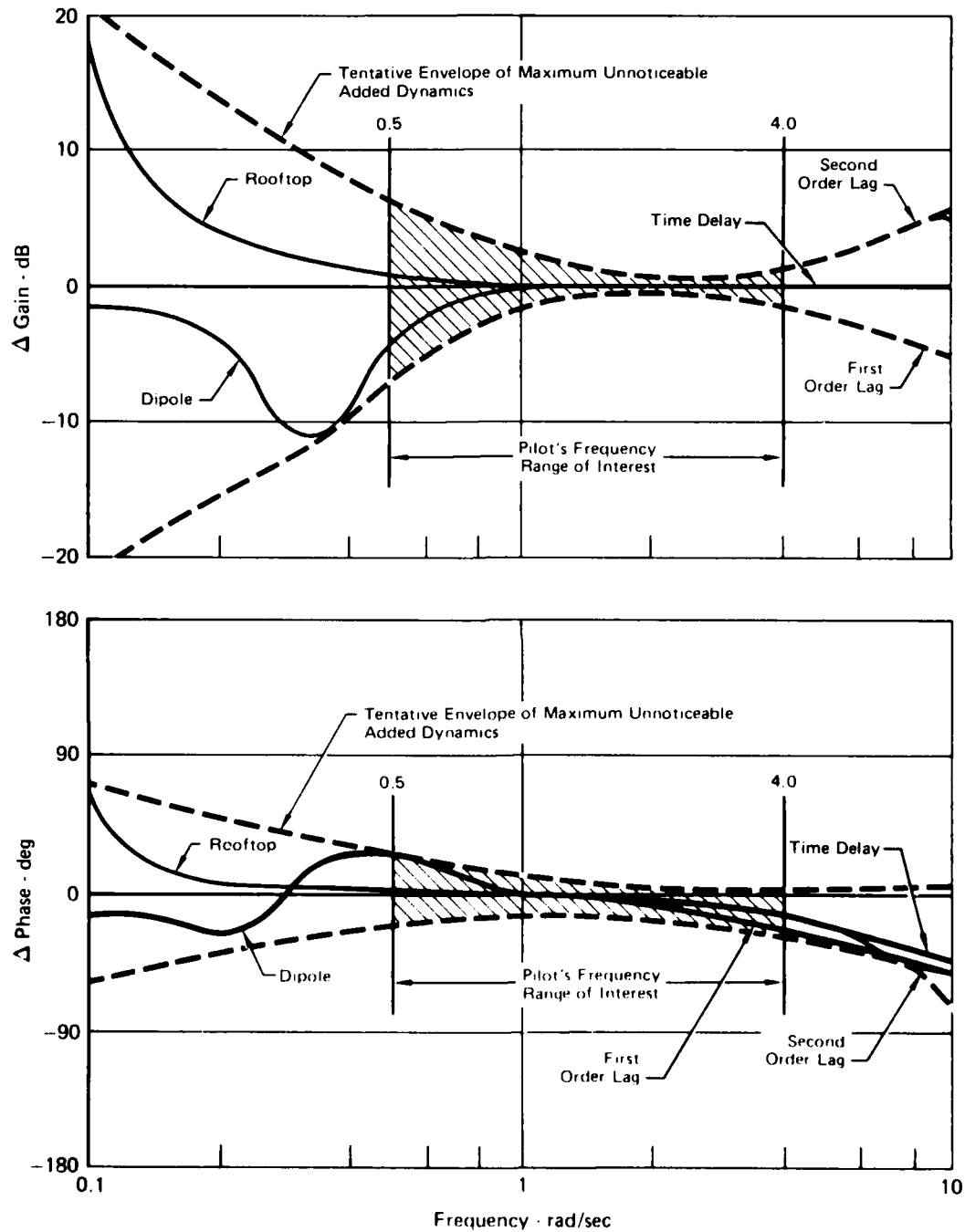
Matching from .1 to 4. rad/sec is a way of de-emphasizing high frequency modes, i.e. a way of weighting the response match more towards the crossover region of piloted control. From the foregoing, it is evident that the pilot's frequency range of interest can be defined as a tentative envelope of mismatch (Figure 31). This figure can be interpreted in two ways:

- (a) When a second order frequency response match to an attitude system has been obtained, the gain and phase mismatches at each frequency should be less than Figure 31. Caution should be exercised in using the envelope to interpret high order modes which differ from those used in this present study.
- (b) The envelope can be used to establish a weighting of gain and phase match as a function of frequency.

This range, as might be expected, is broadly the crossover region for piloted control. However, recent data suggest that some piloting tasks demand a higher crossover frequency than 4 rad/sec. The possibility of a higher crossover frequency for actual landing has been taken into account in establishing the above limits, however, caution should be exercised by allowing a reasonable margin of lag at higher frequencies.

- (3) Do pilots require low-order-appearing responses in attitude, velocity and position to control inputs, and will they reject more complicated high order responses?

It was shown from the pilot comments and ratings that handling qualities were degraded when high order effects were introduced into the pilot's frequency range of interest. This is described in detail in the answer to the first two questions.



GP03-0208 107

Figure 31. Summary of Maximum Augmentation Added Without Affecting Rating

- (4) What are the piloting effects of time delay versus the effects of phase lag?

By using two nominal system natural frequencies and judiciously chosen time delays, it was shown that pilots key more on the amount of pure time delay than on the amount of phase lag produced at the natural frequencies. Therefore, phase lag at the natural frequency is less suitable as a specification parameter. Time delay values of .10 and .30 second are suitable maxima for Levels 1 and 2.

V RECOMMENDATIONS

- (1) The conclusions of this study for hover and for low speed dynamics should be reexamined for the transition flight regime.
- (2) This present study focused on the flying qualities of attitude type dynamics. Examination of translation rate and other advanced systems should also be pursued.
- (3) The effects of command gain on the flying qualities degradation due to time delay should be explored. Ideally, a rule should be established for command gain in a ground-based simulation which will produce identical pilot rating degradation as that seen in actual flight.
- (4) This present study maintained excellent longitudinal characteristics while varying the lateral dynamics. The effects of degrading longitudinal and lateral dynamics simultaneously need evaluation.
- (5) The equivalent system tolerance rules (Figure 31) which have been established by this study should be incorporated in a computer program. A particularly suitable program feature would be to weight the mismatch as a function of frequency to stress the crossover region.
- (6) In future simulations, a stronger height cue would aid the pilot and compensate for the runway texture and other cues which are available in actual flight. A well-displayed analog HUD display of vertical situation should be adequate.
- (7) Verification of these and similar results in a flight test (variable-stability machine) with extension of the task to touchdown will be highly desirable.

REFERENCES

1. Hoh, Roger H., and Ashkenas, Irving L., "Development of VTOL Flying Qualities Criteria for Low Speed and Hover", Naval Air Development Center, NADC-77052-30, December 1979.
2. Stapleford, R. L., et al, "Outsmarting MIL-F-8785B(ASG), the Military Flying Qualities Specification", STI-TR-190-1, August 1971.
3. Craig, S. J., et al, "An Analysis of Navy Approach Power Compensator Problems and Requirements", STI 197-1, March 1971.
4. Hodgkinson, J., "Equivalent Systems Approach for Flying Qualities Specification", MCAIR Paper 79-017, SAE Aerospace Control and Guidance Systems Committee Meeting, Denver, Colorado, 7-9 March 1979.
5. Hodgkinson, J., Berger, R. L., and Bear, R. L., "Analysis of High Order Aircraft/Flight Control System Dynamics Using an Equivalent System Approach", Seventh Annual Pittsburgh Conference on Modeling and Simulation, 26-27 April 1976.
6. A'Harrah, R. C., et al, "Are Today's Specifications Appropriate for Tomorrow's Airplanes?", AGARD Flight Mechanics Panel Symposium on Stability and Control, Ottawa, Canada, September 1978.
7. Smith, R. E., "Equivalent System Verification and Evaluation of Augmentation Effects on Fighter Approach and Landing Flying Qualities", Calspan Report No. 6241-F-3, August 1979.
8. Hodgkinson, J., and Johnston, K. A., "Initial Results of an In-Flight Simulation of Augmented Dynamics in Fighter Approach and Landing", MCAIR Paper 79-019, AIAA Guidance and Control Conference, Boulder, Colorado, 6-8 August 1979.
9. McCormick, R. L., "VTOL Handling Qualities Criteria Study Through Moving-Base Simulation", AFFDL-TR-69-27, October 1969.
10. Miller, D. P., and Vinje, E. W., "Fixed-Base Flight Simulator Studies of VTOL Aircraft Handling Qualities in Hovering and Low-Speed Flight", AFFDL-TR-67-152, January 1968.
11. Vinje, E. W., and Miller, D. P., "Analytical and Flight Simulator Studies to Develop Design Criteria for VTOL Aircraft Control Systems", AFFDL-TR-68-165, April 1968.
12. Carpenter, C. G. and Hodgkinson, J., "Investigation into the Applicability of Equivalent Systems for V/STOL Flying Qualities Using the YAV-8B", MDC A6243, November 1979.

NADC-79141-60

13. DiFranco, D.A., "In-Flight Investigation of the Effects of Higher-Order System Dynamics on Longitudinal Handling Qualities", AFFDL-TR-69-90, August 1968.
14. Hodgkinson, J., "The Application of Equivalent Systems to MIL-F-8785B", Flying Qualities Symposium and Workshop, Dayton, Ohio, 12-15 September 1978.

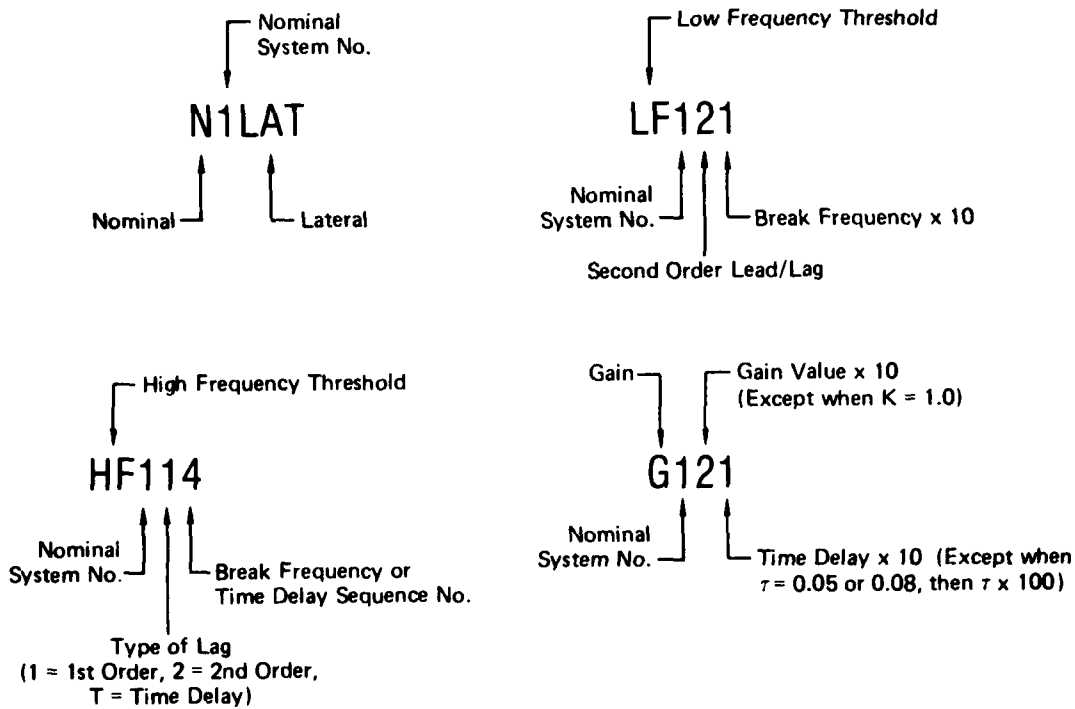
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APPENDIX A

CONFIGURATION DATA

A listing of each configuration is given accompanied by individual pilot ratings. The roots and coefficients of the transfer functions are listed separately. A configuration key is also presented. Frequency responses and time responses to a unit step input are presented for the nominal systems versus the HOS.

The frequency responses are shown on the same scale to allow overlaying data. The time responses are also on the same scale, with the exception of the gain variation cases (G-).



GP03-0208-1

Figure A-1. Key to Configuration Listing

Config	Nominal			Nuisance Mode					Pilot Rating			
	Gain	ζ	ω_n	τ (Equiv ϕ)	λ	ζ_N	ζ_D	ω_L or DP	A	B	C	D
N1LAT	0.6 0.45 0.3	0.7 ↓ ↓	2.0 ↓ ↓	— — —	— — —	— — —	— — —	— — —	4,4,4,4,3,3,3,2,3, 3,3,3,4,3,3,3,2,2, 5,4	4.5,4,3,5 3.5,3,4,3,5 3.5	7.5	4,7,4
N2LAT	0.3 0.3	↓ ↓	5.0 ↓	— —	— —	— —	— —	— —	4,4,4,4,5,3,3,3,3, 3,3,5,4,4,5,4,3,	3.5,5 6.5,5,3,5,5 5.5	5.1	3 5
HF111	0.45	↓	2.0	—	1.0	—	—	—	7,7,9,7	—	—	—
HF112	↓	↓	↓	—	2.0	—	—	—	5,8,6,6	—	—	—
HF113	↓	↓	↓	—	3.0	—	—	—	6,4,3,5,6	—	—	—
HF114	0.6 0.45	↓ ↓	↓ ↓	— —	4.0 ↓	— —	— —	— —	— 5,6	4 —	—	—
HF115	0.3 0.45	↓ ↓	↓ ↓	— —	5.0 ↓	— —	— —	— —	— 5,4	3,5 —	—	—
HF116	0.6 0.45	↓ ↓	↓ ↓	— —	6.0 ↓	— —	— —	— —	— 5	— 4,5	6 —	5
HF117	0.3	↓	↓	—	7.0	—	—	—	—	4,5	—	—
HF124	0.6 0.45	↓ ↓	↓ ↓	— —	— —	— —	0.3 ↓	4.0 ↓	— 6	6 7,5	—	—
HF125	0.6 0.45	↓ ↓	↓ ↓	— —	— —	— —	— —	5.0 ↓	— 5	— 6	—	7,5
HF126	0.3 0.45	↓ ↓	↓ ↓	— —	— —	— —	— —	6.0 ↓	6 6,5	— 4,4	—	—
HF127	↓ 0.3	↓ ↓	↓ ↓	— —	— —	— —	— —	7.0 ↓	7,6 —	— 5,5	—	—
HF128	0.45	↓	↓	—	—	—	—	8.0	4,5	—	—	—
HF129	↓	↓	↓	—	—	—	—	9.0	3,4,4,4	—	—	—
HF120	↓	↓	↓	—	—	—	—	10.0	5,5,3,4	—	—	—
HF121	↓	↓	↓	—	—	—	—	11.0	6,4,5	—	—	—

GP03 0208 33

Figure A-2. List of Configurations and Pilot Ratings

Config	Nominal			Nuisance Mode					Pilot Rating			
	Gain	ζ	ω_n	τ (Equiv ϕ)	λ	ζ_N	ζ_D	ω_L or DP	A	B	C	D
HF1T1	0.6	0.7	2.0	0.1 (11.46°)	-	-	-	-				6
	0.45			↓	-	-	-	-	4,2			
	0.3			↓	-	-	-	-		5		
HF1T2	0.45			0.2 (22.92°)	-	-	-	-	7,7	6.5	6	
HF1T3	0.6			0.3 (34.38°)	-	-	-	-		4		
	0.45			↓	-	-	-	-	7	5.5		
HF1T4	0.3			0.4 (45.84°)	-	-	-	-		7		
	0.45			↓	-	-	-	-	7			
LF121	0.45			-	-	0.2	0.7	0.1	3		4	
LF123	↓			-	-	↓	↓	0.3	2,3			
LF125	↓			-	-	↓	↓	0.5	3,4			
LF127	↓			-	-	↓	↓	0.7	4,7			
LF121*	0.6			-	-	-	0.05	0.1			8	
LF123*	↓			-	-	-	↓	0.3				3
LF125*	↓			-	-	-	↓	0.5				7
LF127*	↓			-	-	-	↓	0.7				10
HF211	0.3		5.0	-	1.0	-	-	-	6,6,5,6,6			10
HF212	↓			-	2.0	-	-	-	2,3,3,5			
HF213	↓			-	3.0	-	-	-	3,4,3,3			
HF214	↓			-	4.0	-	-	-	3	3,5		
HF215	↓			-	5.0	-	-	-	3	3,4,5	5	
HF216	↓			-	6.0	-	-	-	3	4		
HF217	↓			-	7.0	-	-	-	3		5	
HF224	↓			-	-	-	0.3	4.0	7	5		
HF225	↓			-	-	-	↓	5.0		7,8	7	
HF226	↓			-	-	-	↓	6.0	6,6	5,5		
HF227	↓			-	-	-	↓	7.0	6	5,6	6	
HF228	↓			-	-	-	↓	8.0	8,4,4,6			
HF229	↓			-	-	-	↓	9.0	5,4,3			
HF220	↓			-	-	-	↓	10.0	4,8,3			

*Exaggerated rooftop systems

GP03-0208 32

Figure A-2. (Continued) List of Configurations and Pilot Ratings

Config	Nominal			Nuisance Mode					Pilot Rating			
	Gain	ζ	ω_n	τ (Equiv ϕ)	λ	ζ_N	ζ_D	ω_L or DP	A	B	C	D
HF221	0.3	0.7	5.0	—	—	—	0.3	11.0	7,4,2,4			
HF2T1				0.05 (14.33°)	—	—	—	—	3	3,4,5	5	
HF2T2				0.08 (22.92°)	—	—	—	—	2,3	5		
HF2T3				0.12 (34.38°)	—	—	—	—	3	5		
HF2T4				0.16 (45.84°)	—	—	—	—	5,5,5,5	6,5		
HF2T5				0.2	—	—	—	—	6,6			
HF2T6				0.3	—	—	—	—	8,5,5			
HF2T7				0.4	—	—	—	—	8,9			
LF221				—	—	0.2	0.7	0.1	3			
LF223				—	—			0.3	4		8	
LF225				—	—			0.5	6			
LF227				—	—			0.7	6			
LF221*				—	—	—	0.05	0.1				5
LF223*				—	—	—		0.3				
LF225*				—	—	—		0.5				
LF227*				—	—	—		0.7				
G110	1.0		2.0	0 (0°)	—	—	—	—	3,2,3,2			
G111				0.1 (11.46°)	—	—	—	—	6,6			
G112				0.2 (22.92°)	—	—	—	—	8,5,8,7	6		
G113				0.3 (34.38°)	—	—	—	—	7	10		
G120	0.2			0 (0°)	—	—	—	—	7,7			
G121				0.1 (11.46°)	—	—	—	—	7,7			
G122				0.2 (22.92°)	—	—	—	—	7,7,4	7		
G180	0.8			0 (0°)	—	—	—	—	2,4			
G186				0.06 (6.88°)	—	—	—	—	4,4			
G188				0.08 (9.168°)	—	—	—	—	2,2			
G181				0.1 (11.46°)	—	—	—	—	6,5			

*Exaggerated rooftop systems

GP03 0208 31

FigureA-2. (Concluded) List of Configurations and Pilot Ratings

Configuration	Transfer Function	Description
N1LAT	$\frac{0.45}{0.25S^2 + 0.7S + 1.0}$	Nominal System No. 1 [0.7; 2.0]
N2LAT	$\frac{0.3}{0.04S^2 + 0.28S + 1.0}$	Nominal System No. 2 [0.7; 5.0]
High Frequency Threshold		
HF111	$\frac{0.45}{0.25S^3 + 0.95S^2 + 1.7S + 1.0}$	$\frac{1}{N1LAT (1.0)}$
HF112	$\frac{0.45}{0.125S^3 + 0.6S^2 + 1.2S + 1.0}$	$\frac{1}{N1LAT (2.0)}$
HF113	$\frac{0.45}{0.083S^3 + 0.483S^2 + 1.03S + 1.0}$	$\frac{1}{N1LAT (3.0)}$
HF114	$\frac{0.45}{0.0625S^2 + 0.425S^2 + 0.95S + 1.0}$	$\frac{1}{N1LAT (4.0)}$
HF115	$\frac{0.45}{0.05S^3 + 0.39S^2 + 0.9S + 1.0}$	$\frac{1}{N1LAT (5.0)}$
HF116	$\frac{0.45}{0.0417S^3 + 0.367S^2 + 0.867S + 1.0}$	$\frac{1}{N1LAT (6.0)}$
HF117	$\frac{0.45}{0.0357S^3 + 0.35S^2 + 0.843S + 1.0}$	$\frac{1}{N1LAT (7.0)}$
HF124	$\frac{0.45}{0.016S^4 + 0.081S^3 + 0.418S^2 + 0.85S + 1.0}$	$\frac{1}{N1LAT [0.3; 4.0]}$
HF125	$\frac{0.45}{0.01S^4 + 0.058S^3 + 0.374S^2 + 0.82S + 1.0}$	$\frac{1}{N1LAT [0.3; 5.0]}$
HF126	$\frac{0.45}{0.007S^4 + 0.044S^3 + 0.348S^2 + 0.8S + 1.0}$	$\frac{1}{N1LAT [0.3; 6.0]}$
HF127	$\frac{0.45}{0.005S^4 + 0.036S^3 + 0.33S^2 + 0.786S + 1.0}$	$\frac{1}{N1LAT [0.3; 7.0]}$
HF128	$\frac{0.45}{0.0039S^4 + 0.029S^3 + 0.318S^2 + 0.775S + 1.0}$	$\frac{1}{N1LAT [0.3; 8.0]}$

Figure A-3. List of Configuration Transfer Functions

GP03-0208-10

Configuration	Transfer Function	Description
	High Frequency Threshold	
HF129	$\frac{0.45}{0.0031S^4 + 0.25S^3 + 0.309S^2 + 0.767S + 1.0}$	N1LAT $\frac{1}{[0.3; 9.0]}$
HF120	$\frac{0.45}{0.0025S^4 + 0.022S^3 + 0.302S^2 + 0.76S + 1.0}$	N1LAT $\frac{1}{[0.3; 10.0]}$
HF121	$\frac{0.45}{0.0021S^4 + 0.019S^3 + 0.296S^2 + 0.755S + 1.0}$	N1LAT $\frac{1}{[0.3; 11.0]}$
HF1T1	$\frac{0.45e^{-0.1S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.1$)
HF1T2	$\frac{0.45e^{-0.2S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.2$)
HF1T3	$\frac{0.45e^{-0.3S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.3$)
HF1T4	$\frac{0.45e^{-0.4S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.4$)
HF211	$\frac{0.3}{0.04S^3 + 0.32S^2 + 1.28S + 1.0}$	N2LAT $\frac{1}{(1.0)}$
HF212	$\frac{0.3}{0.02S^3 + 0.18S^2 + 0.78S + 1.0}$	N2LAT $\frac{1}{(2.0)}$
HF213	$\frac{0.3}{0.013S^3 + 0.133S^2 + 0.613S + 1.0}$	N2LAT $\frac{1}{(3.0)}$
HF214	$\frac{0.3}{0.1S^3 + 0.11S^2 + 0.53S + 1.0}$	N2LAT $\frac{1}{(4.0)}$
HF215	$\frac{0.3}{0.008S^3 + 0.96S^2 + 0.48S + 1.0}$	N2LAT $\frac{1}{(5.0)}$
HF216	$\frac{0.3}{0.007S^3 + 0.87S^2 + 0.447S + 1.0}$	N2LAT $\frac{1}{(6.0)}$

GP03-0200-99

Figure A-3. (Continued) List of Configuration Transfer Functions

Configuration	Transfer Function	Description
HF217	$\frac{0.3}{0.006S^3 + 0.8S^2 + 0.423S + 1.0}$	$\frac{1}{N2LAT (7.0)}$
HF224	$\frac{0.3}{0.003S^4 + 0.024S^3 + 0.145S^2 + 0.43S + 1.0}$	$\frac{1}{N2LAT [0.3; 4.0]}$
HF225	$\frac{0.3}{0.002S^4 + 0.016S^3 + 0.114S^2 + 0.4S + 1.0}$	$\frac{1}{N2LAT [0.3; 5.0]}$
HF226	$\frac{0.3}{0.001S^4 + 0.012S^3 + 0.096S^2 + 0.38S + 1.0}$	$\frac{1}{N2LAT [0.3; 6.0]}$
HF227	$\frac{0.3}{0.0008S^4 + 0.009S^3 + 0.084S^2 + 0.366S + 1.0}$	$\frac{1}{N2LAT [0.3; 7.0]}$
HF228	$\frac{0.3}{0.000625S^4 + 0.00738S^3 + 0.0766S^2 + 0.355S + 1.0}$	$\frac{1}{N2LAT [0.3; 8.0]}$
HF229	$\frac{0.3}{0.000494S^4 + 0.0061S^3 + 0.071S^2 + 0.347S + 1.0}$	$\frac{1}{N2LAT [0.3; 9.0]}$
HF220	$\frac{0.3}{0.0004S^4 + 0.0052S^3 + 0.0668S^2 + 0.34S + 1.0}$	$\frac{1}{N2LAT [0.3; 10.0]}$
HF221	$\frac{0.3}{0.000331S^4 + 0.0045S^3 + 0.0635S^2 + 0.335S + 1.0}$	$\frac{1}{N2LAT [0.3; 11.0]}$
HF2T1	$\frac{0.3e^{-0.05}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.05$)
HF2T2	$\frac{0.3e^{-0.08S}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.08$)
HF2T3	$\frac{0.3e^{-0.12S}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.12$)
HF2T4	$\frac{0.3e^{-0.16S}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.16$)

GP03-0208-100

Figure A-3. (Continued) List of Configuration Transfer Functions

Configuration	Transfer Function	Description
High Frequency Threshold		
HF2T5	$\frac{0.3e^{-0.2S}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.2$)
HF2T6	$\frac{0.3e^{-0.3S}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.3$)
HF2T7	$\frac{0.3e^{-0.4S}}{0.04S^2 + 0.28S + 1.0}$	N2LAT ($\tau = 0.4$)
Low Frequency Threshold		
LF121:	$\frac{45.0S^2 + 1.8S + 0.45}{25.0S^4 + 73.5S^3 + 110.05S^2 + 14.7S + 1.0}$	N1LAT $\frac{[0.2; 0.1]}{[0.7; 0.1]}$
LF123:	$\frac{5.0S^2 + 0.6S + 0.45}{2.78S^4 + 8.94S^3 + 14.63S^2 + 5.37S + 1.0}$	N1LAT $\frac{[0.2; 0.3]}{[0.7; 0.3]}$
LF125:	$\frac{1.8S^2 + 0.36S + 0.45}{1.0S^4 + 3.5S^3 + 6.21S^2 + 3.5S + 1.0}$	N1LAT $\frac{[0.2; 0.5]}{[0.7; 0.5]}$
LF127:	$\frac{0.92S^2 + 0.26S + 0.45}{0.51S^4 + 1.93S^3 + 3.69S^2 + 2.7S + 1.0}$	N1LAT $\frac{[0.2; 0.7]}{[0.7; 0.7]}$
LF221:	$\frac{30.0S^2 + 1.2S + 0.3}{4.0S^4 + 28.56S^3 + 103.96S^2 + 14.28S + 1.0}$	N2LAT $\frac{[0.2; 0.1]}{[0.7; 0.1]}$
LF223:	$\frac{3.33S^2 + 0.4S + 0.3}{0.44S^4 + 3.3S^3 + 12.46S^2 + 4.95S + 1.0}$	N2LAT $\frac{[0.2; 0.3]}{[0.7; 0.3]}$
LF225:	$\frac{1.2S^2 + 0.24S + 0.3}{0.16S^4 + 1.23S^3 + 4.82S^2 + 3.08S + 1.0}$	N2LAT $\frac{[0.2; 0.5]}{[0.7; 0.5]}$
LF227:	$\frac{0.61S^2 + 0.17S + 0.3}{0.082S^4 + 0.65S^3 + 2.64S^2 + 2.28S + 1.0}$	N2LAT $\frac{[0.2; 0.7]}{[0.7; 0.7]}$

GP03-0208 101

Figure A-3. (Continued) List of Configuration Transfer Functions

Configuration	Transfer Function	Description
LF121*	$\frac{0.45S^2}{25.S^4 + 70.25S^3 + 100.95S^2 + 1.7S + 1.0}$	N1LAT $\frac{S^2}{[0.05, 0.1]}$
LF123*	$\frac{0.45S^2}{2.778S^4 + 7.86S^3 + 11.59S^2 + 1.033S + 1.0}$	N1LAT $\frac{S^2}{[0.05, 0.3]}$
LF125*	$\frac{0.45S^2}{S^4 + 2.85S^3 + 4.39S^2 + 0.9S + 1.0}$	N1LAT $\frac{S^2}{[0.05, 0.5]}$
LF127*	$\frac{0.45S^2}{0.51S^4 + 1.464S^3 + 2.39S^2 + 0.843S + 1.0}$	N1LAT $\frac{S^2}{[0.05, 0.7]}$
LF221*	$\frac{0.3S^2}{4S^4 + 28.04S^3 + 100.32S^2 + 1.28S + 1.0}$	N2LAT $\frac{S^2}{[0.05, 0.1]}$
LF223*	$\frac{0.3S^2}{0.444S^4 + 3.124S^3 + 11.243S^2 + 0.613S + 1.0}$	N2LAT $\frac{S^2}{[0.05, 0.3]}$
LF225*	$\frac{0.3S^2}{0.16S^4 + 1.128S^3 + 4.096S^2 + 0.48S + 1.0}$	N2LAT $\frac{S^2}{[0.05, 0.5]}$
LF227*	$\frac{0.3S^2}{0.0816S^4 + 0.5769S^3 + 2.12S^2 + 0.423S + 1.0}$	N2LAT $\frac{S^2}{[0.05, 0.7]}$

*Exaggerated rooftop systems

GP03-0200-100

Figure A-3. (Continued) List of Configuration Transfer Functions

Configuration	Transfer Function	Description
	Effect of Gains	
G120	$\frac{0.2}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0$, $K = 0.2$)
G121	$\frac{0.2e^{-0.1S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.1$, $K = 0.2$)
G122	$\frac{0.2e^{-0.2S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.2$, $K = 0.2$)
G110	$\frac{1.0}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0$, $K = 1.0$)
G111	$\frac{1.0e^{-0.1S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.1$, $K = 1.0$)
G112	$\frac{1.0e^{-0.2S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.2$, $K = 1.0$)
G113	$\frac{1.0e^{-0.3S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.3$, $K = 1.0$)
G180	$\frac{0.8}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0$, $K = 0.8$)
G185	$\frac{0.8e^{-0.05S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.05$, $K = 0.8$)
G188	$\frac{0.8e^{-0.08S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.08$, $K = 0.8$)
G181	$\frac{0.8e^{-0.1S}}{0.25S^2 + 0.7S + 1.0}$	N1LAT ($\tau = 0.1$, $K = 0.8$)

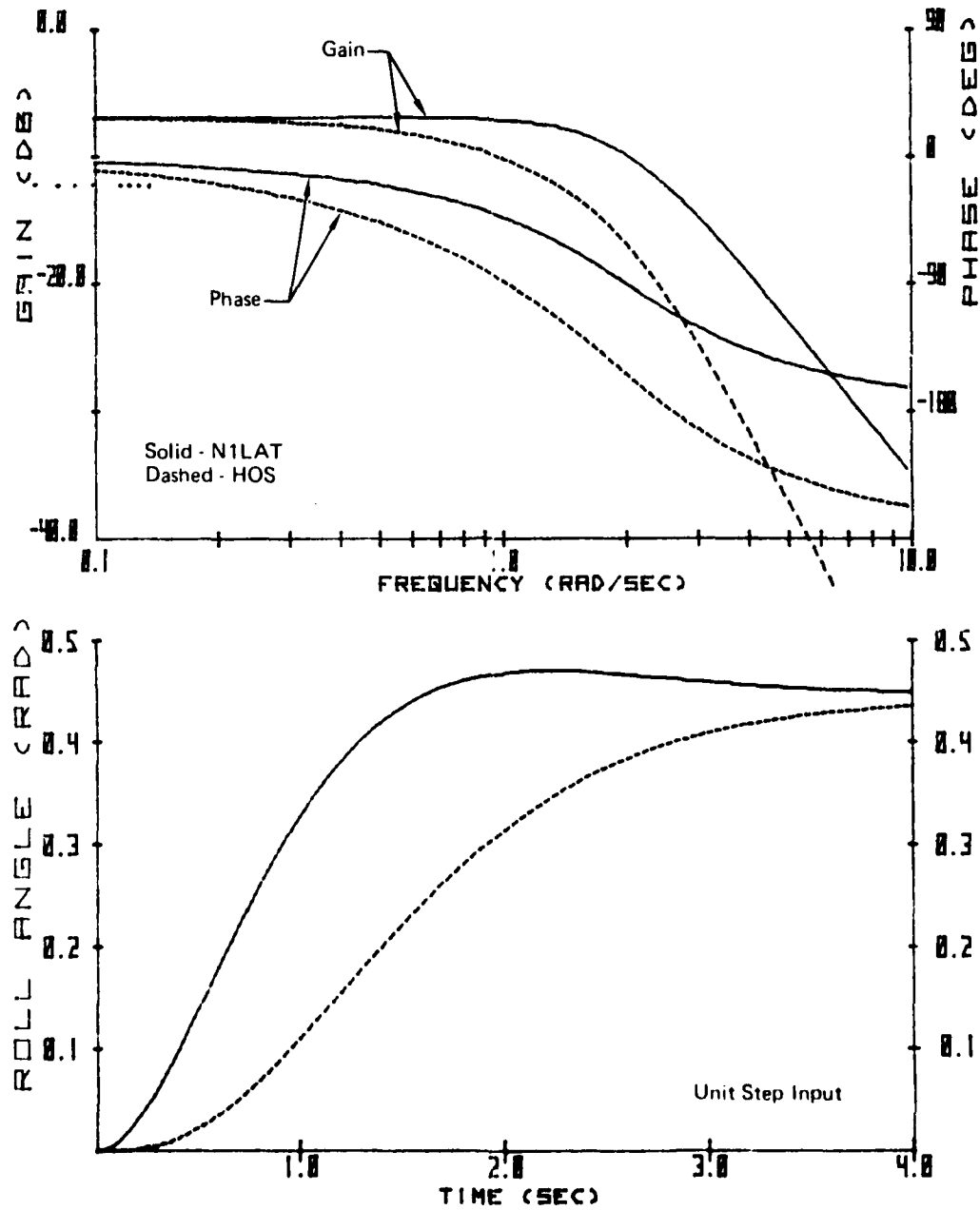
GP03 0208 102

Figure A-3. (Concluded) List of Configuration Transfer Functions

Config HF111

$\lambda = 1.0$

PR: 7.5, -, -, -



GP03-0200-30

Figure A-4. Frequency and Time Response

Config HF112
 $\lambda = 2.0$
 PR: 6.25, -, -, -

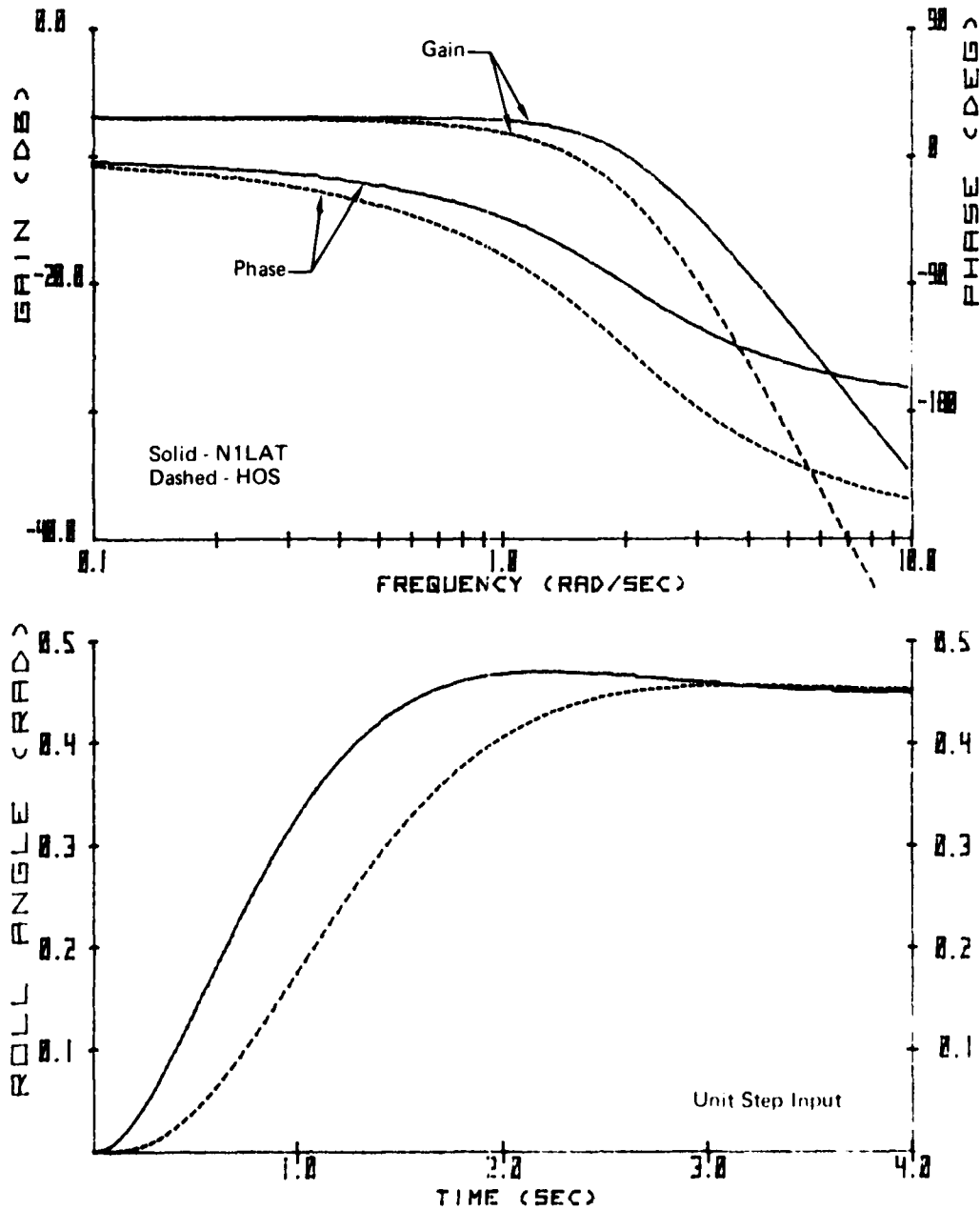
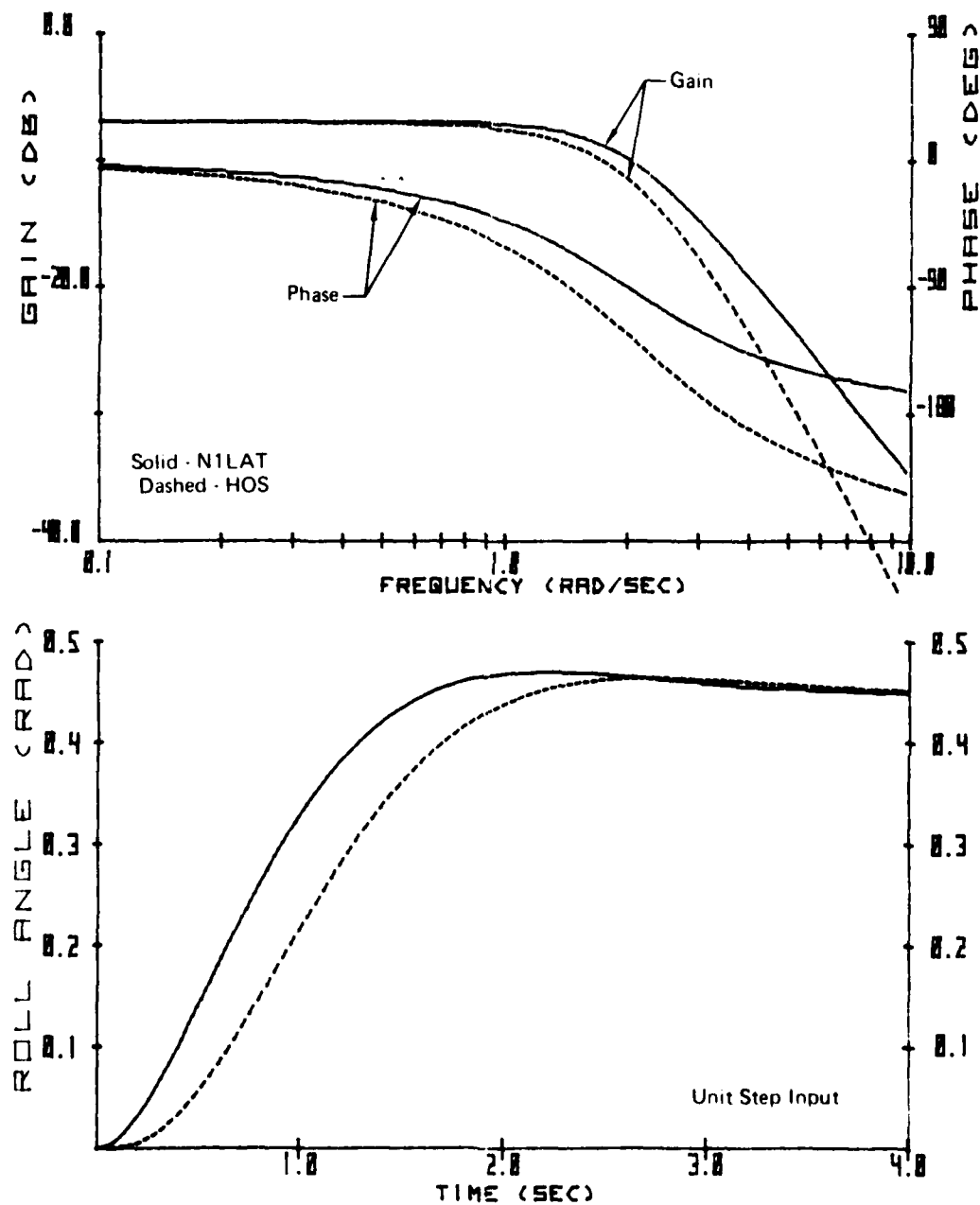


Figure A-5. Frequency and Time Response

GP03-0208 39

Config HF113
 $\lambda = 3.0$
 PR: 4.75, -, -, -



GP03-0208-40

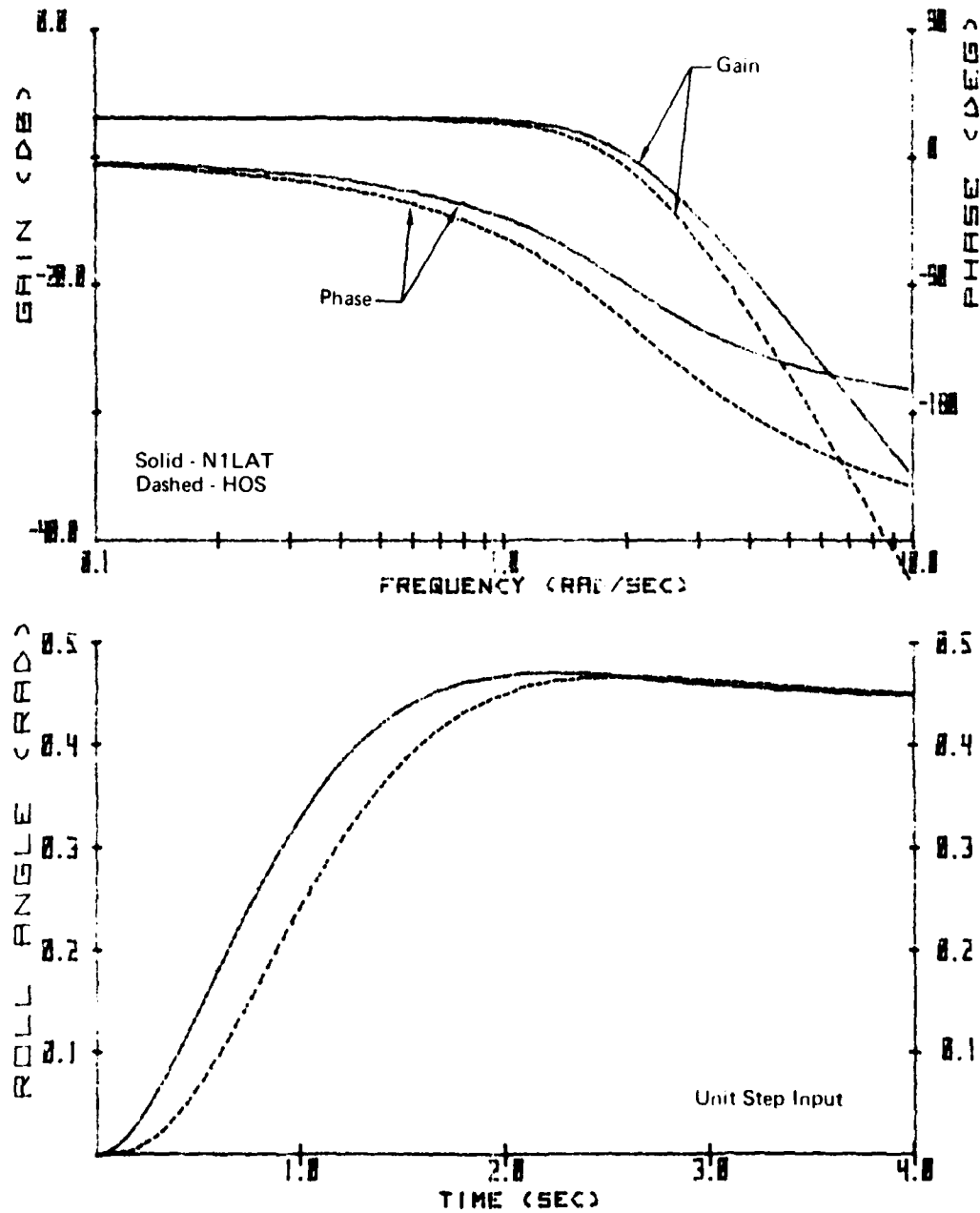
Figure A-6. Frequency and Time Response

NADC-79141-60

Config HF114

$\lambda = 4.0$

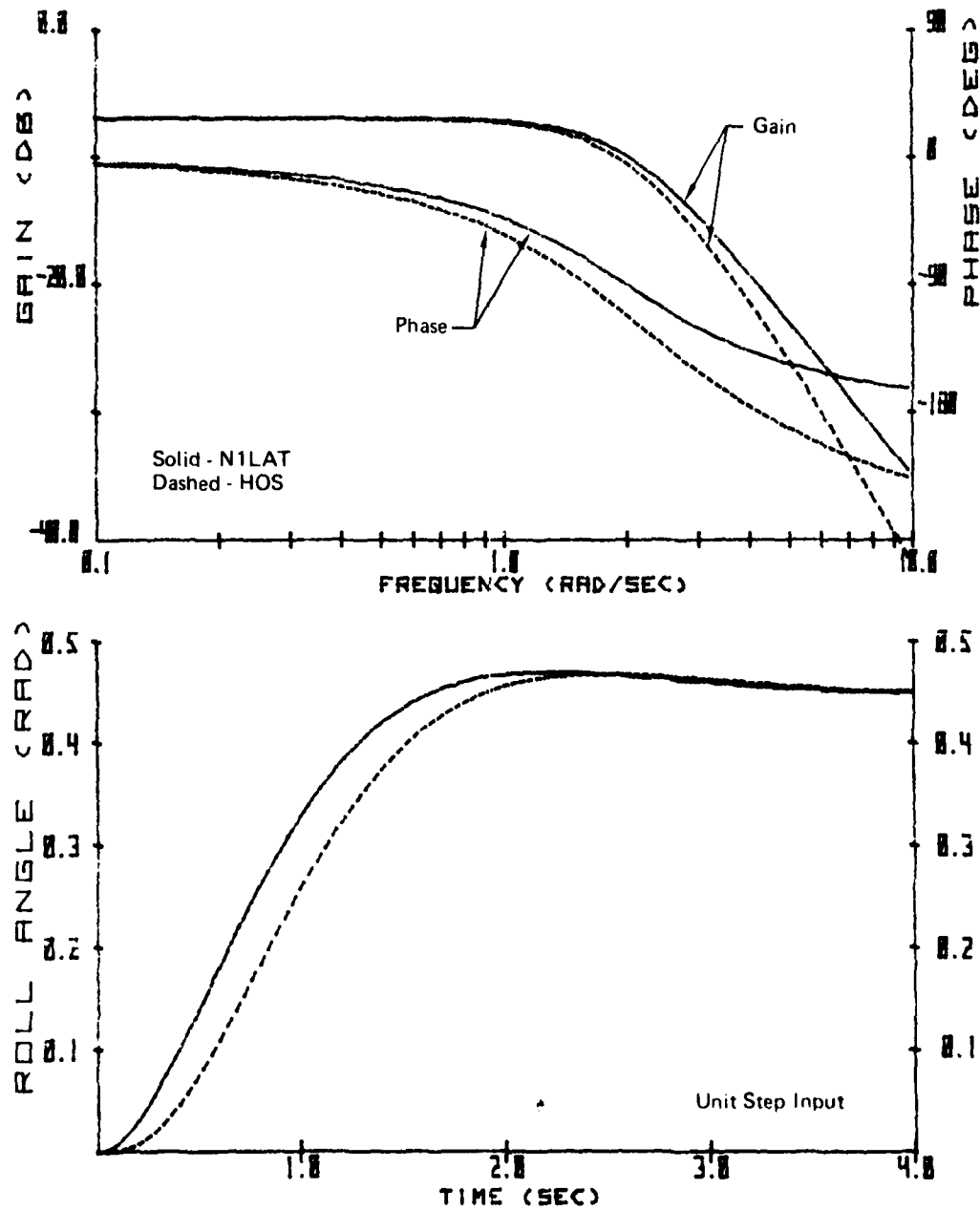
PR: 5.5, 4, -, -



GP03-0208-41

Figure A-7. Frequency and Time Response

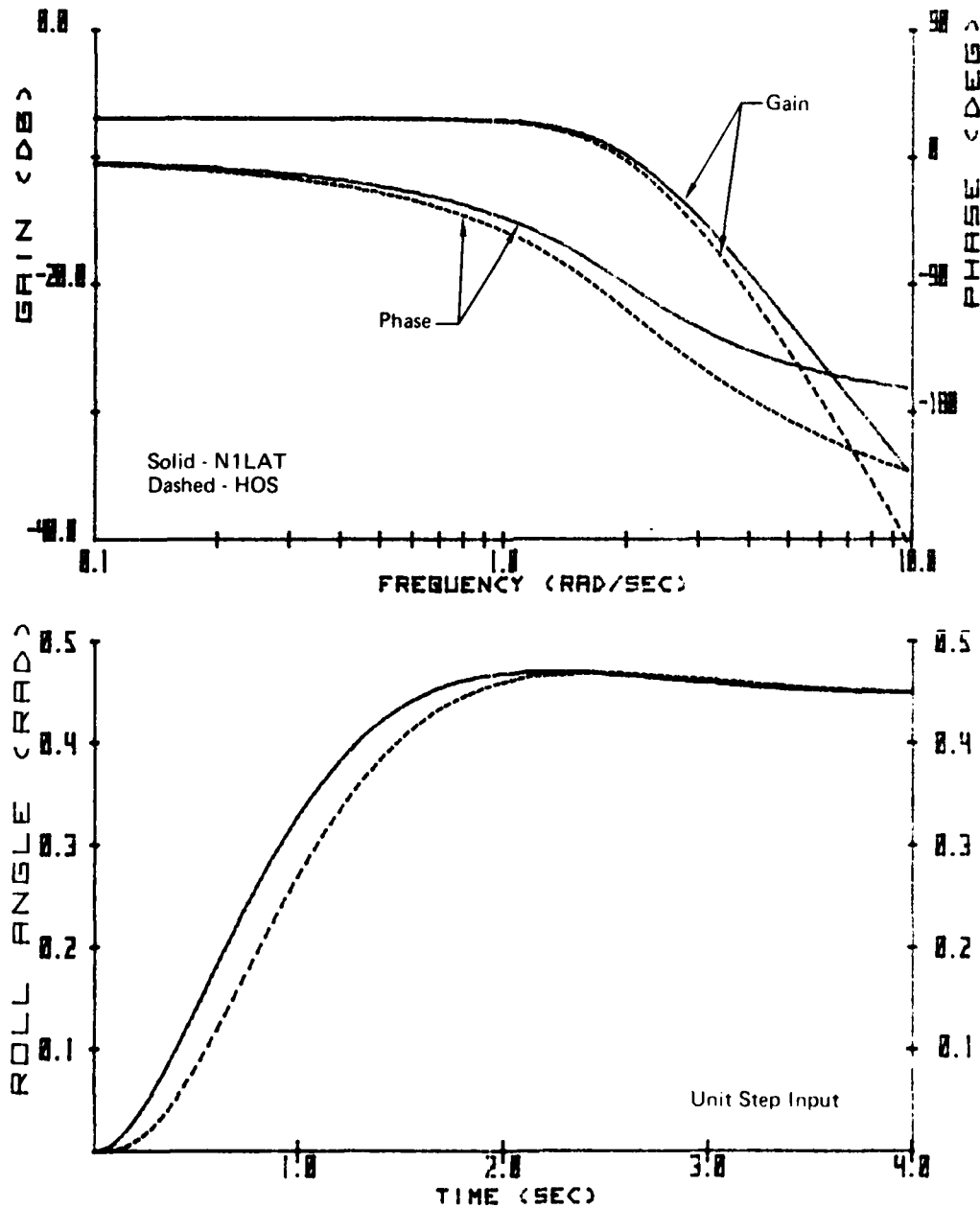
Config HF115
 $\lambda = 5.0$
 PR: -, 3.5, 6, -



GP03-0200-42

Figure A-8. Frequency and Time Response

Config HF116
 $\lambda = 6.0$
 PR: 5, 4.5, -, 5



GP03-0208-43

Figure A-9. Frequency and Time Response

Config HF117
 $\lambda = 7.0$
 PR: -, 4.5, -, -, -

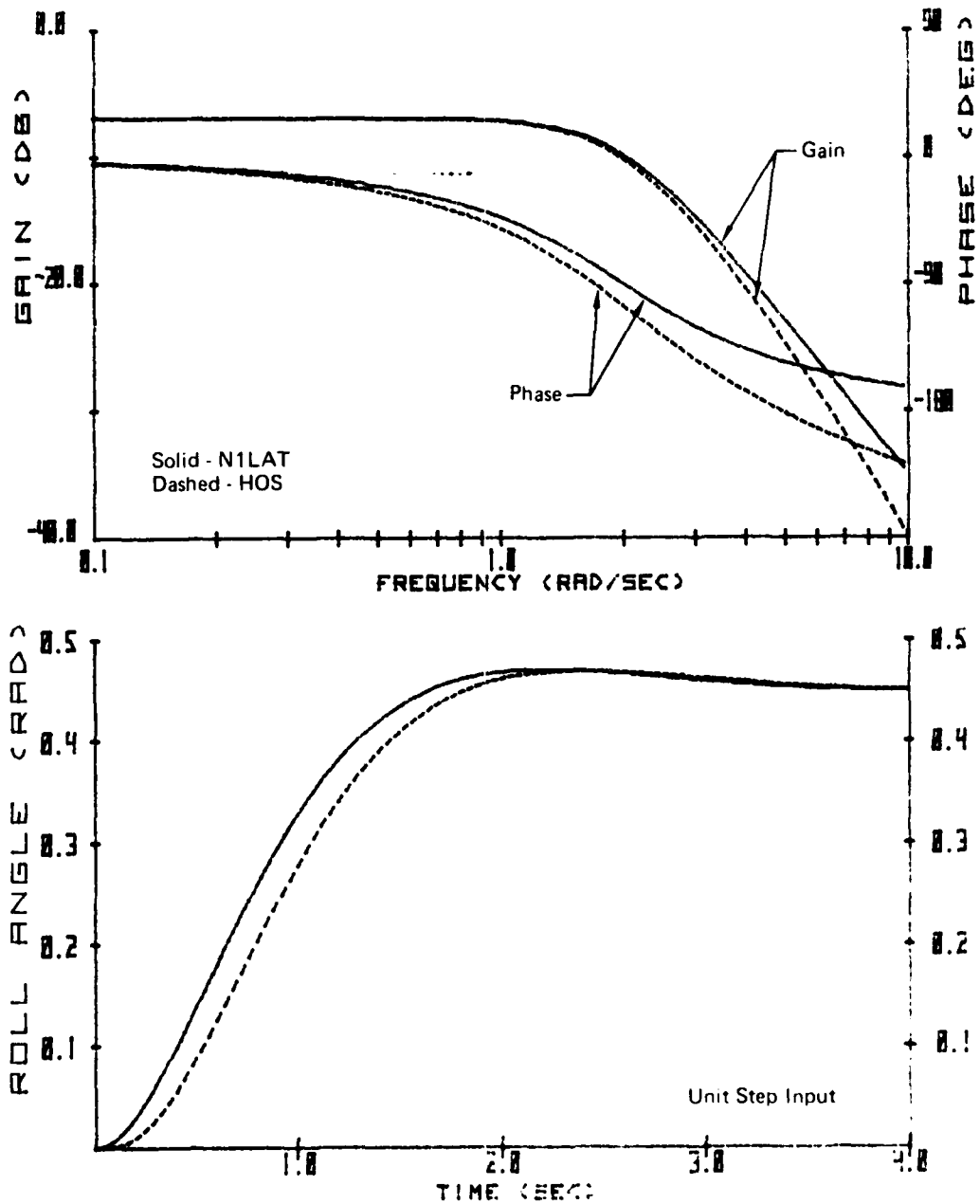


Figure A-10. Frequency and Time Response

GP03-0208-44

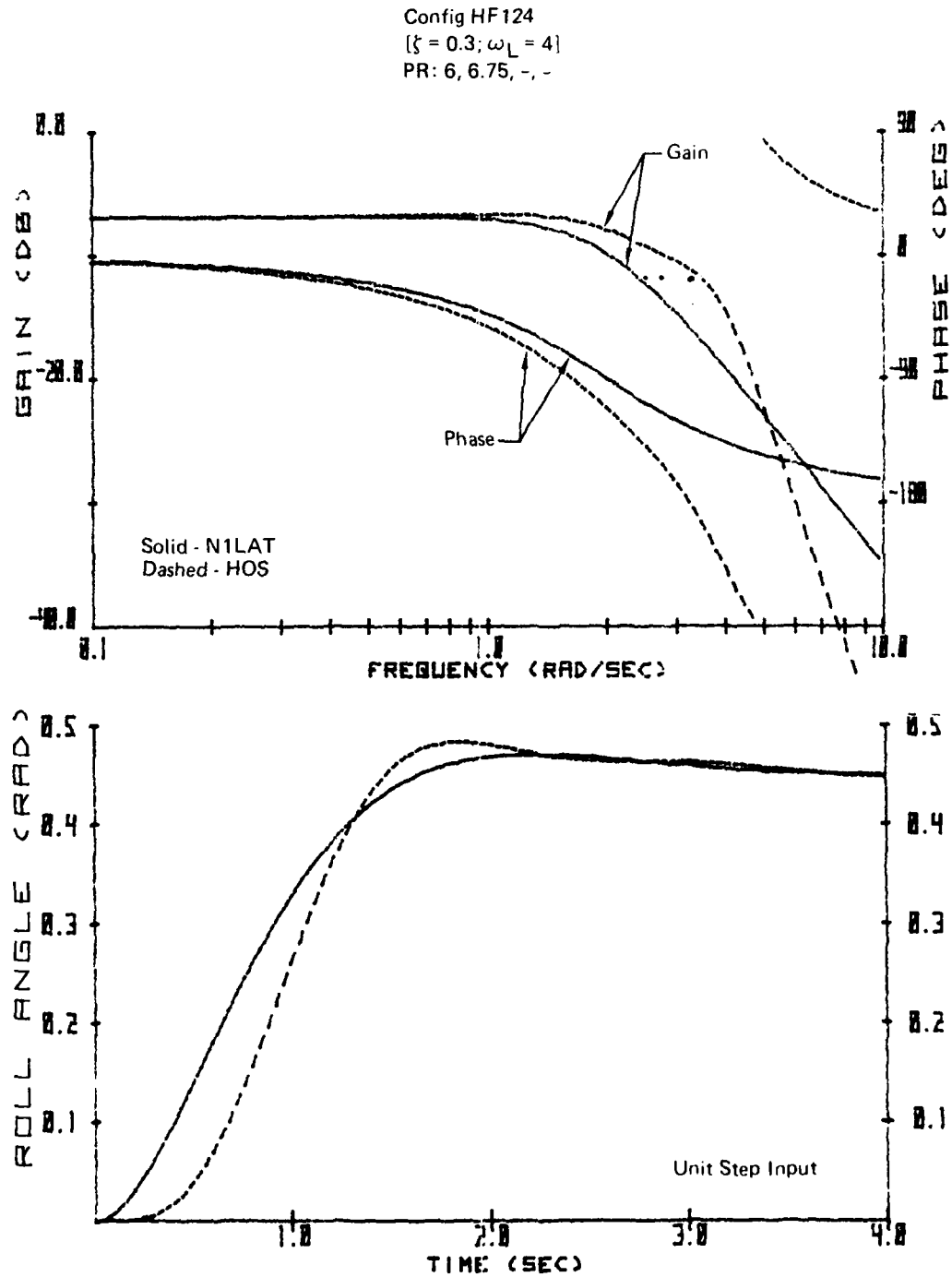


Figure A-11. Frequency and Time Response

GP03-0208 45

Config HF125
 $\zeta = 0.3; \omega_L = 5$
 PR: 5.5, 6, -, 7.5

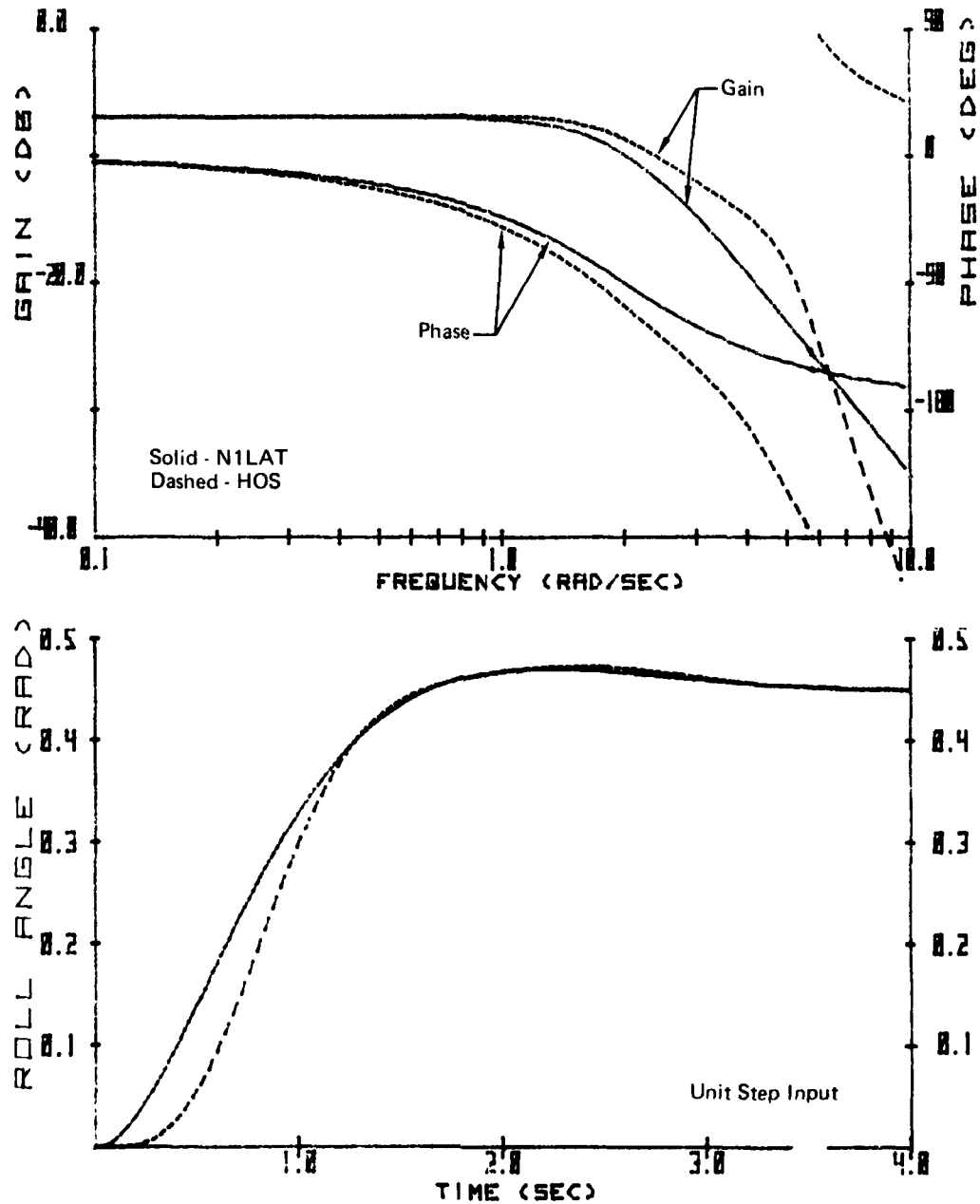


Figure A-12. Frequency and Time Response

GP03-0208-48

Config HF126
 $[\zeta = 0.3; \omega_L = 6]$
 PR: 5.5, 4, -, -

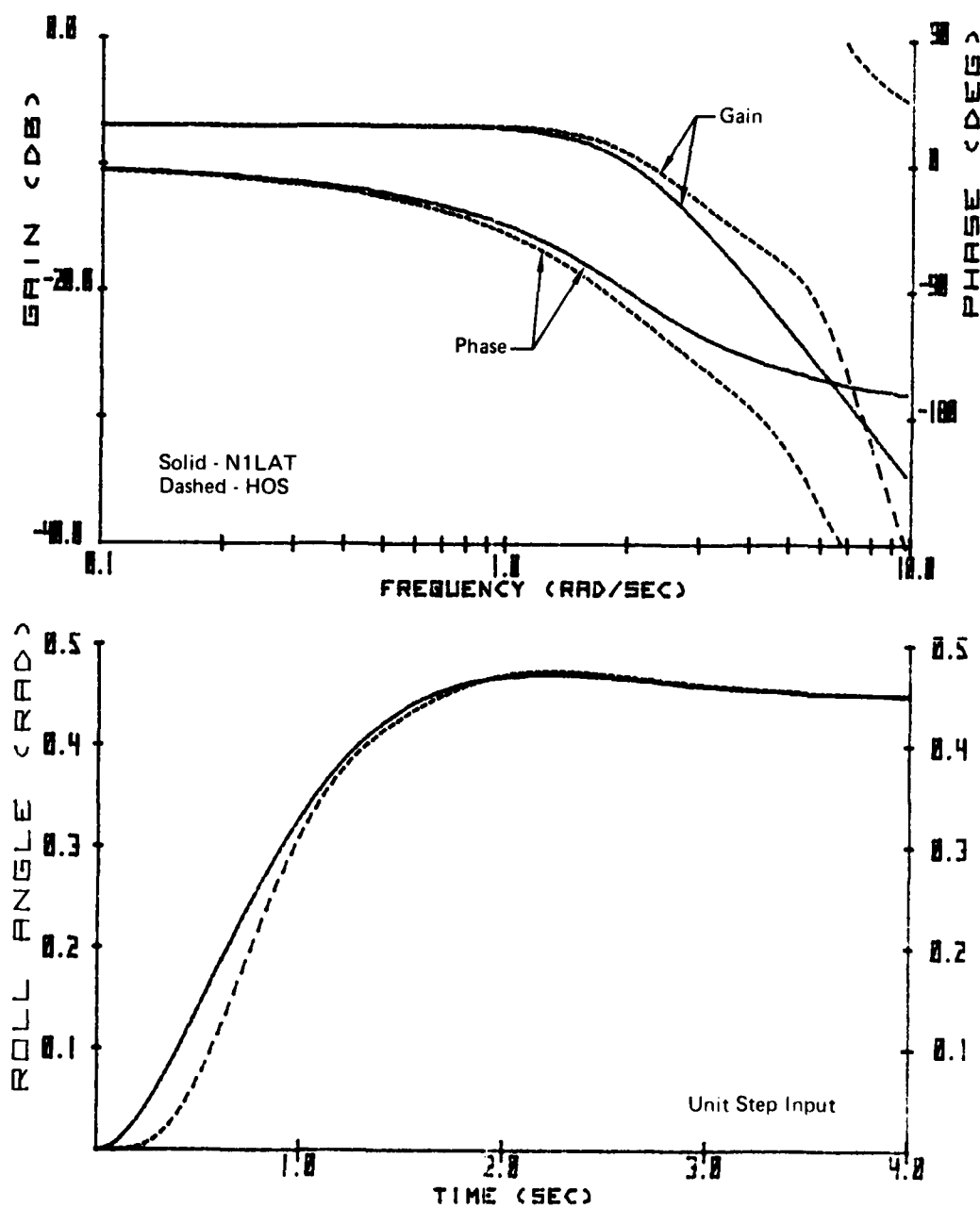


Figure A-13. Frequency and Time Response

GP03-0208-47

NADC-79141-60

Config HF127
 $\zeta = 0.3; \omega_L = 7$
 PR: 6.5, 5.5, -, -

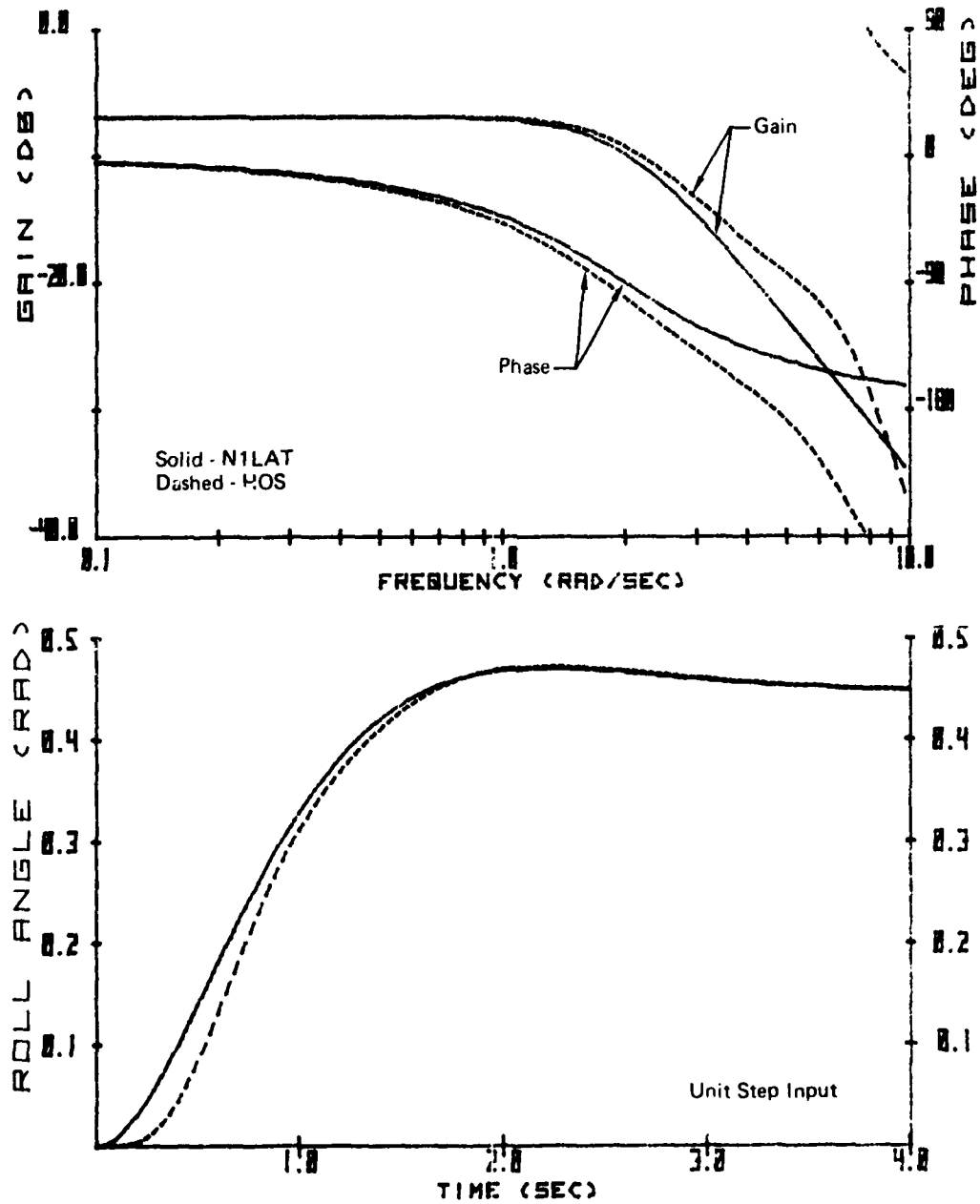
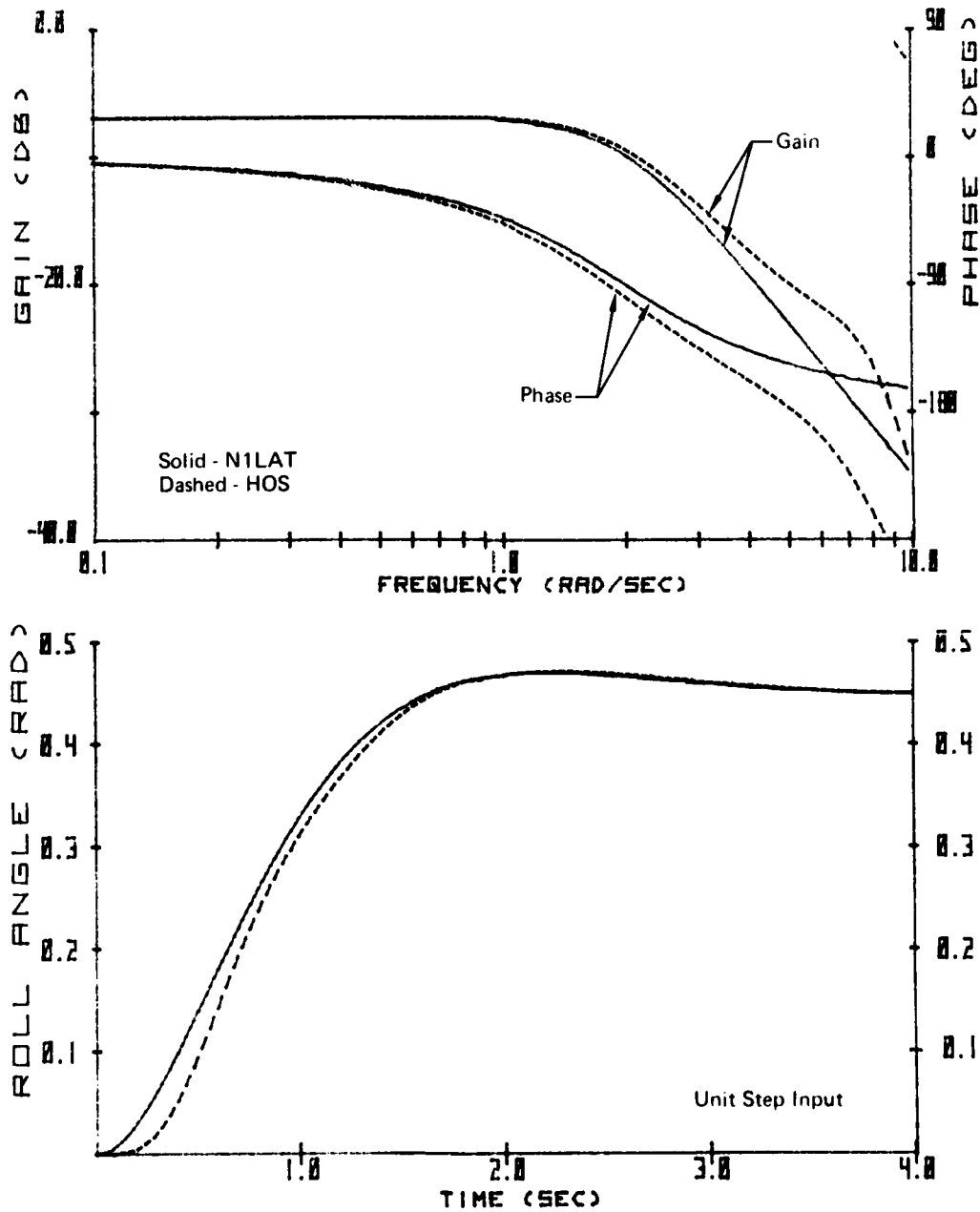


Figure A-14. Frequency and Time Response

GP03-0208-48

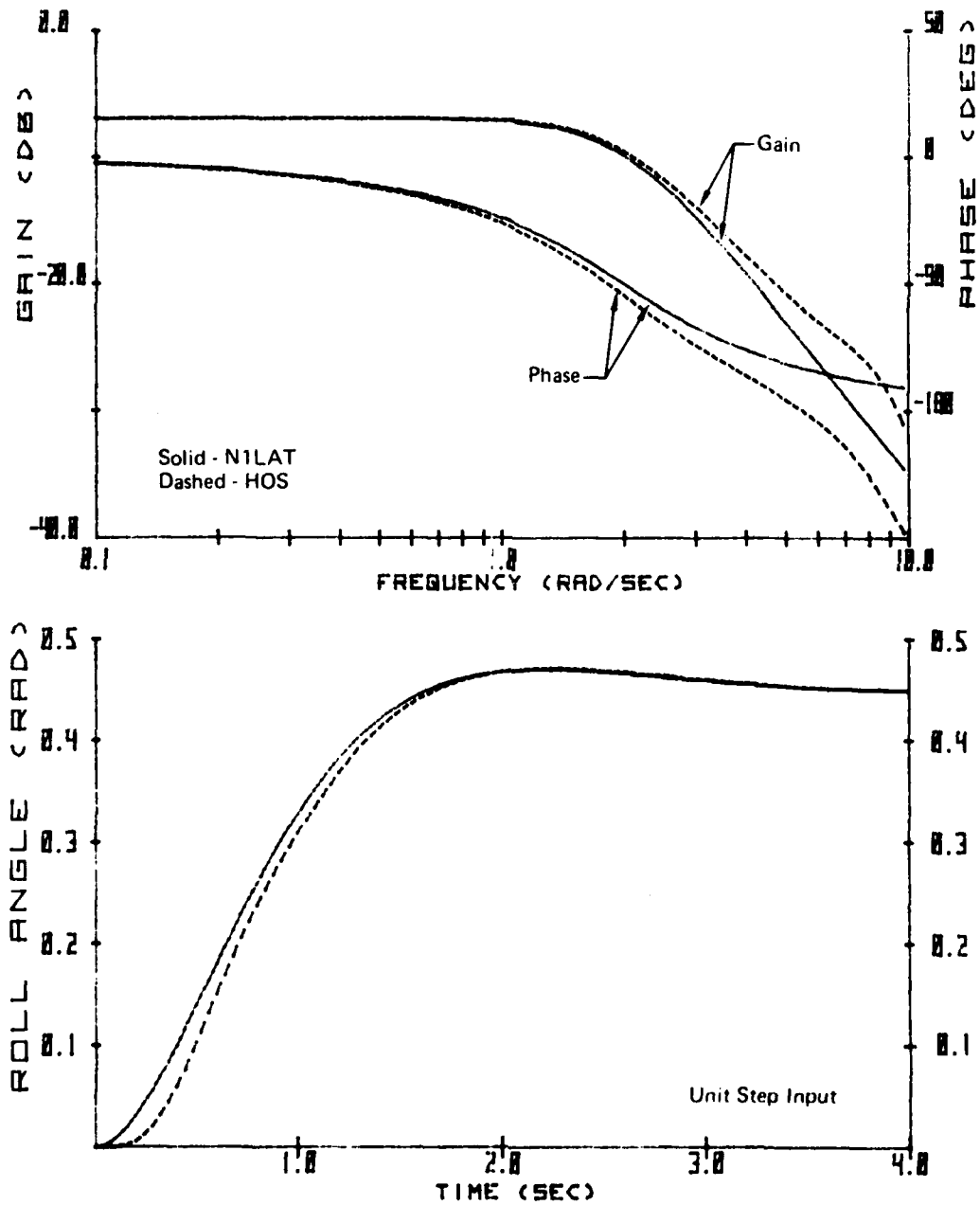
Config HF128
 $[\zeta = 0.3; \omega_L = 8]$
 PR: 4.5, -, -, -



QP03-0208-40

Figure A-15. Frequency and Time Response

Config HF129
 $[\zeta = 0.3; \omega_L = 9]$
 PR: 3.75, -, -, -

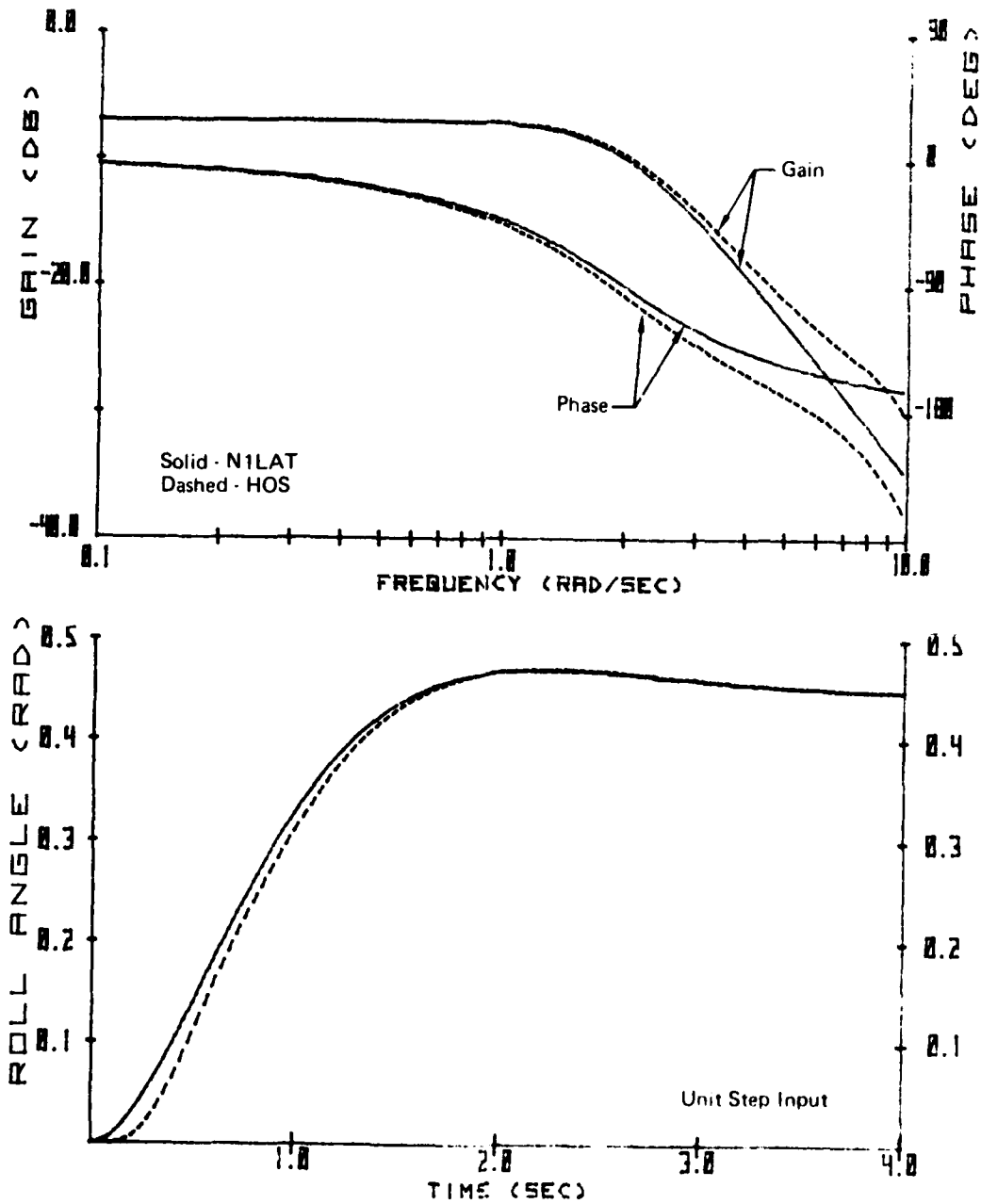


GP03-0208-50

Figure A-16. Frequency and Time Response

NADC-79141-60

Config HF120
 $[\zeta = 0.3; \omega_L = 10]$
 PR: 4.25, -, -, -

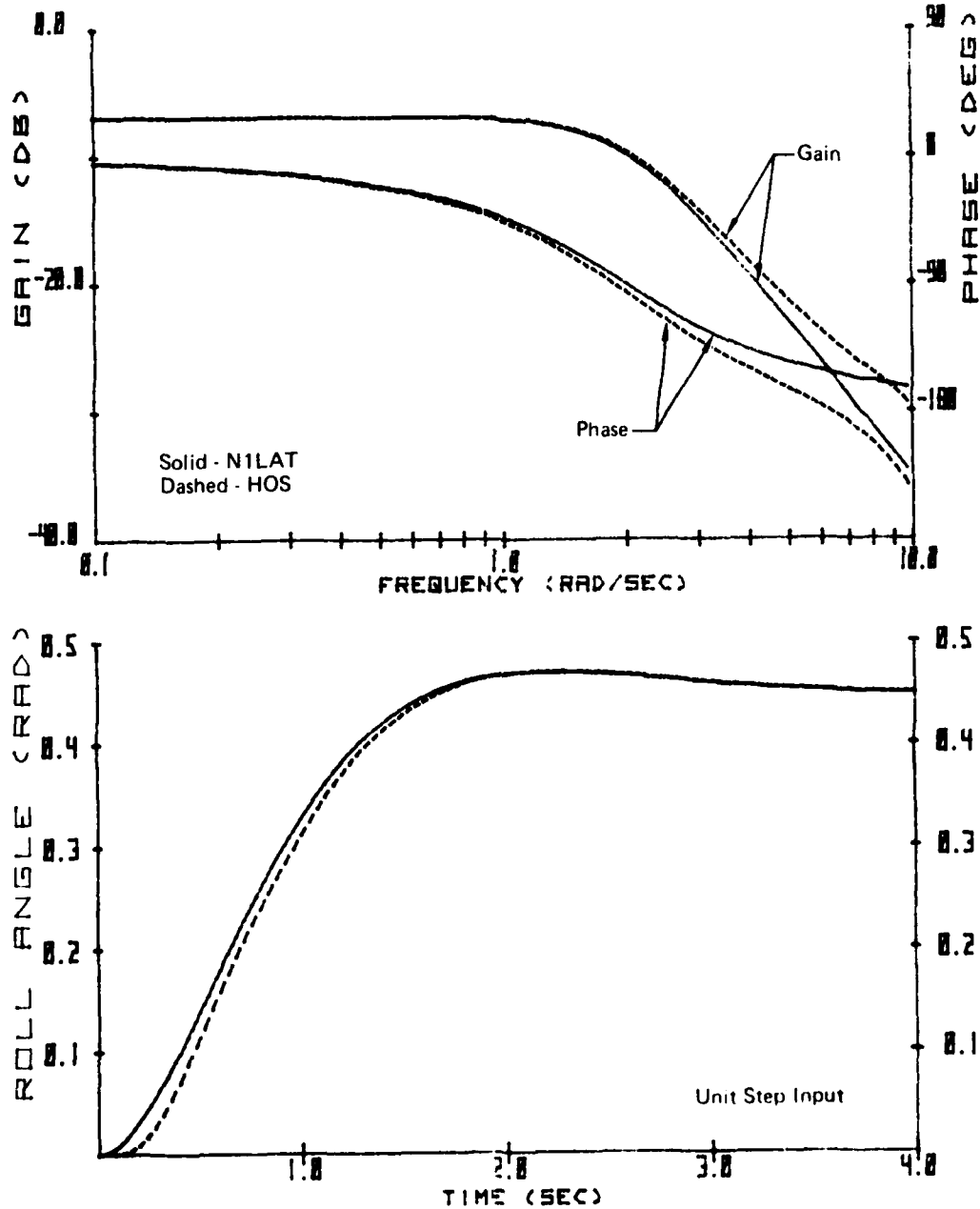


GP03-0208 51

Figure A-17. Frequency and Time Response

NADC-79141-60

Config HF121
 $\{\zeta = 0.3; \omega_L = 11\}$
 PR: 5, -, -, -



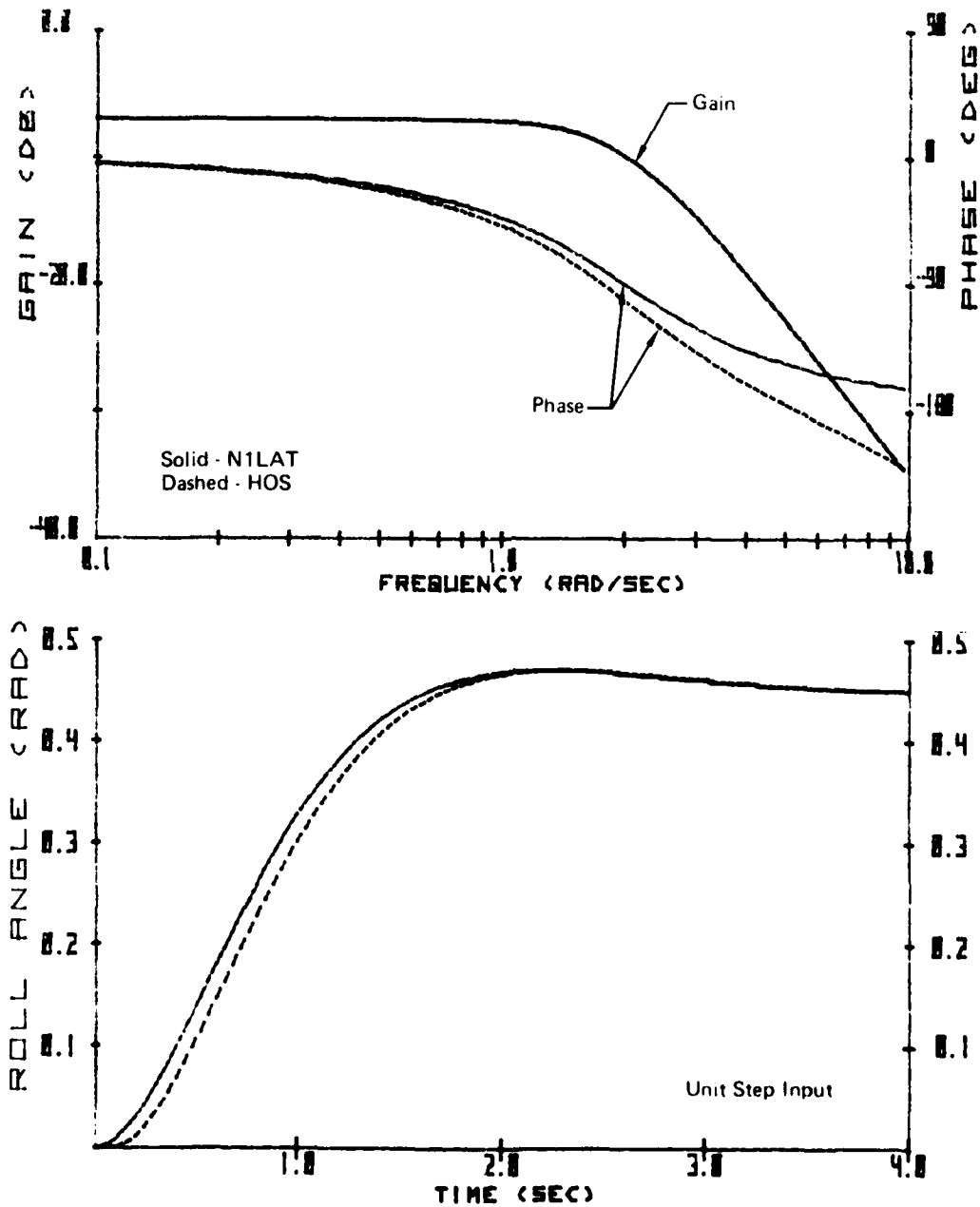
GP03-0200-02

Figure A-18. Frequency and Time Response

Config HF1T1

$\tau = 0.1$

PR: 3, 5, -, 6



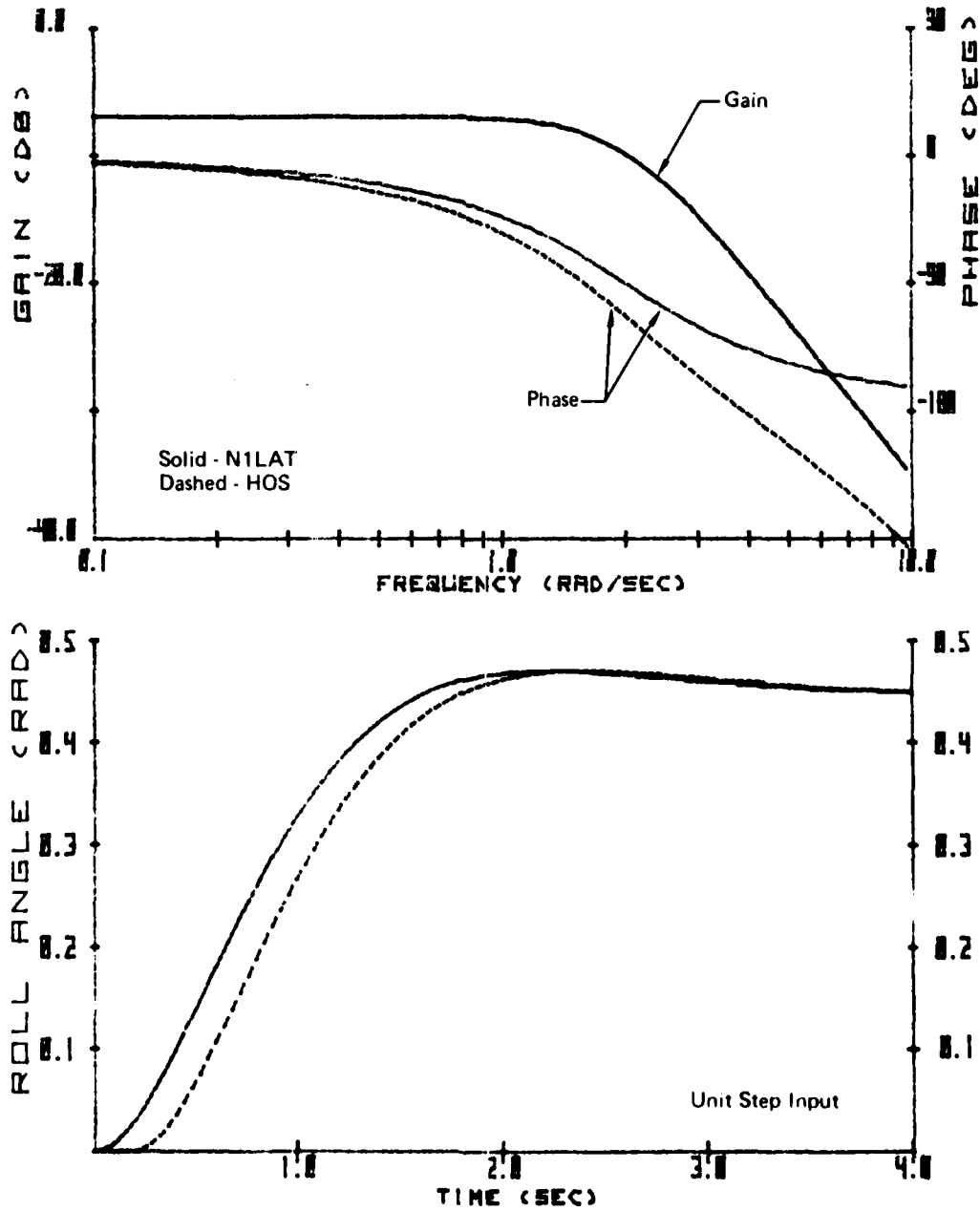
GP03-0208 53

Figure A-19. Frequency and Time Response

Config HF1T2

$\tau = 0.2$

PR: 7, 6.5, 6, -

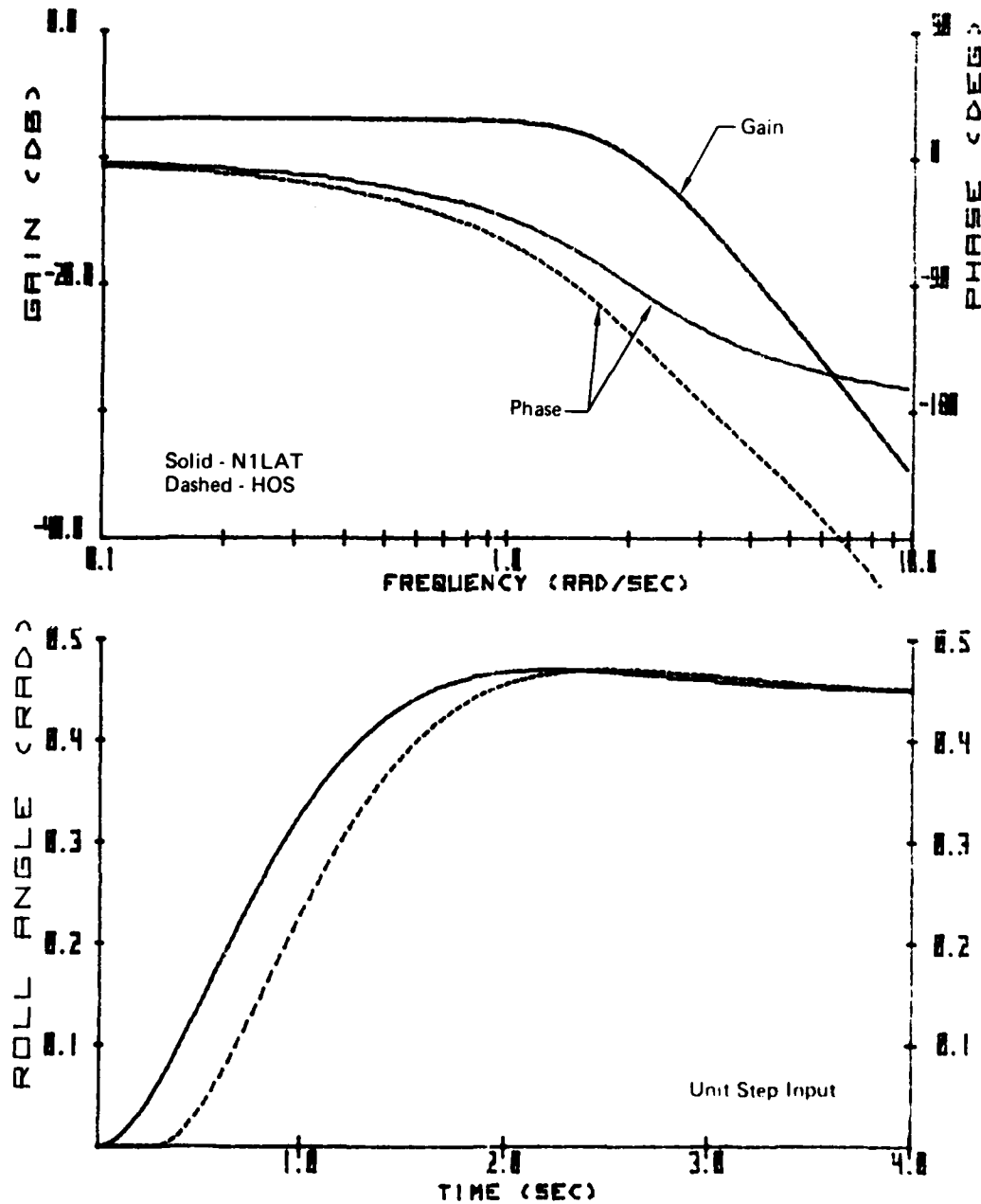


GP03-0208-54

Figure A-20. Frequency and Time Response

NADC-79141-60

Config HF1T3
 $\tau = 0.3$
PR: 7, 4.75, -, -



GP03-0208-55

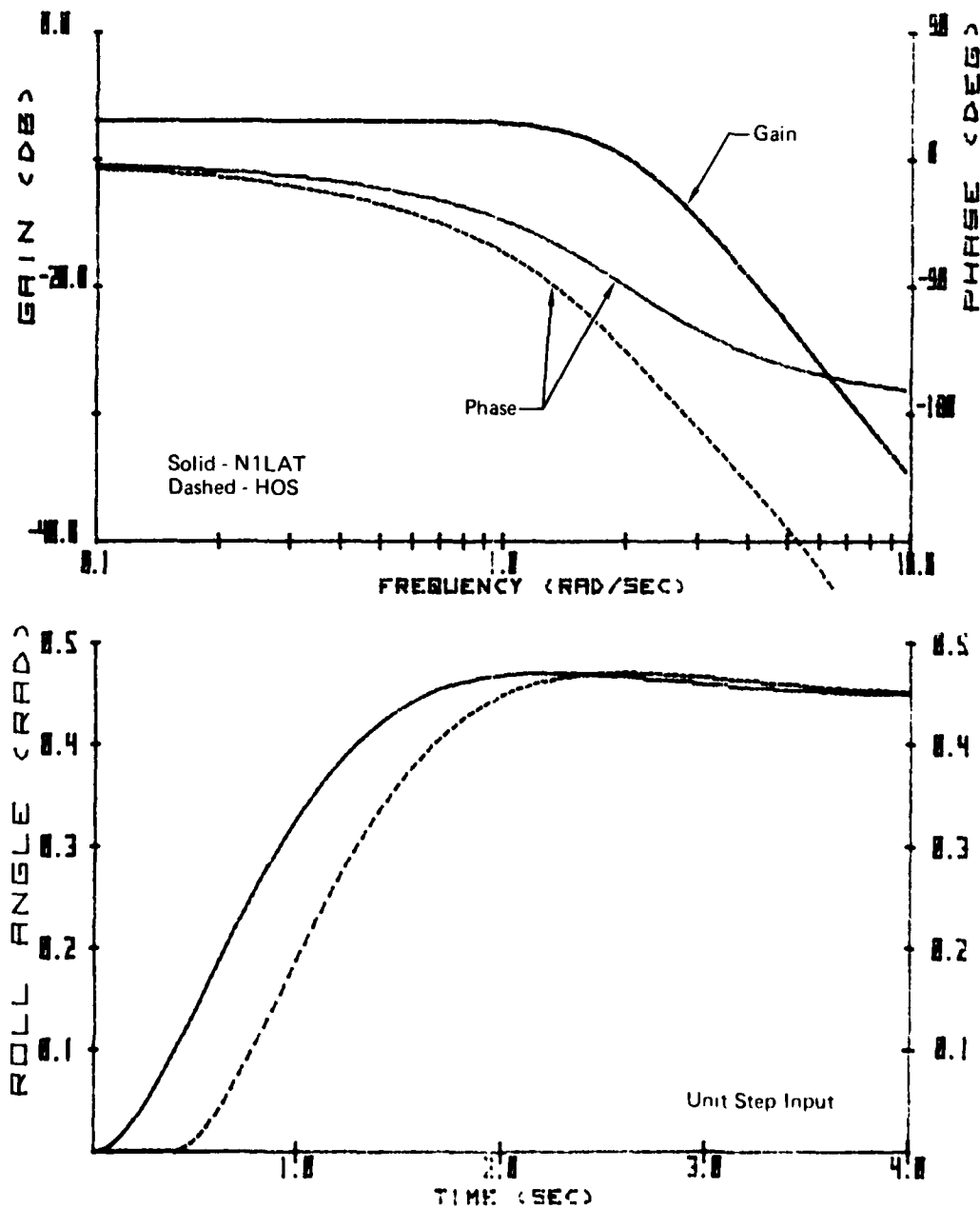
Figure A-21. Frequency and Time Response

NADC-79141-60

Config HF1T4

$\tau = 0.4$

PR: 7, 7, -, -



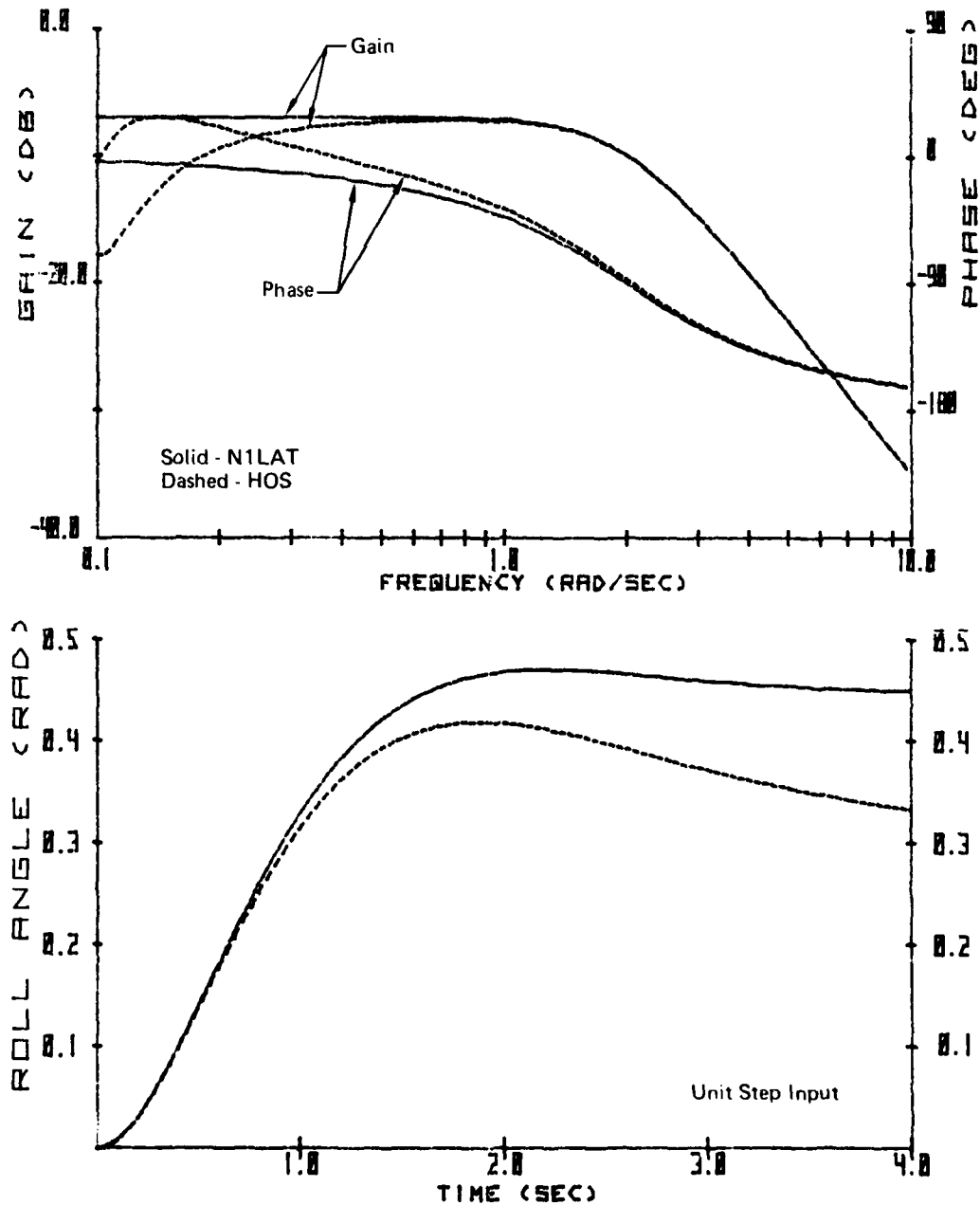
OP03-0208-96

Figure A-22. Frequency and Time Response

Config LF121

$[\zeta = 0.2; \omega_L = 0.3] / [\zeta = 0.7; \omega_L = 0.1]$

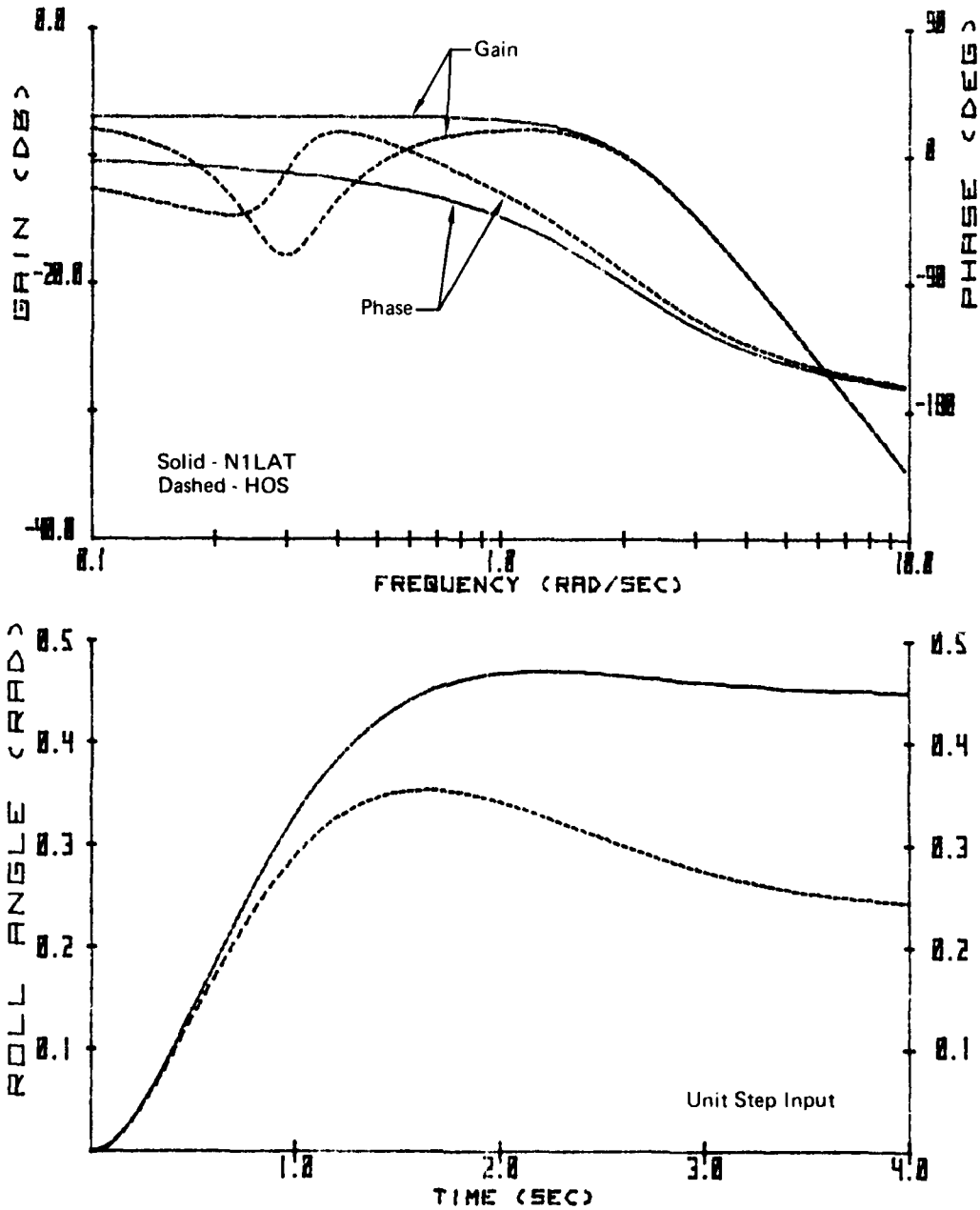
PR: 3, -, 4, -



GP03-0208-57

Figure A-23. Frequency and Time Response

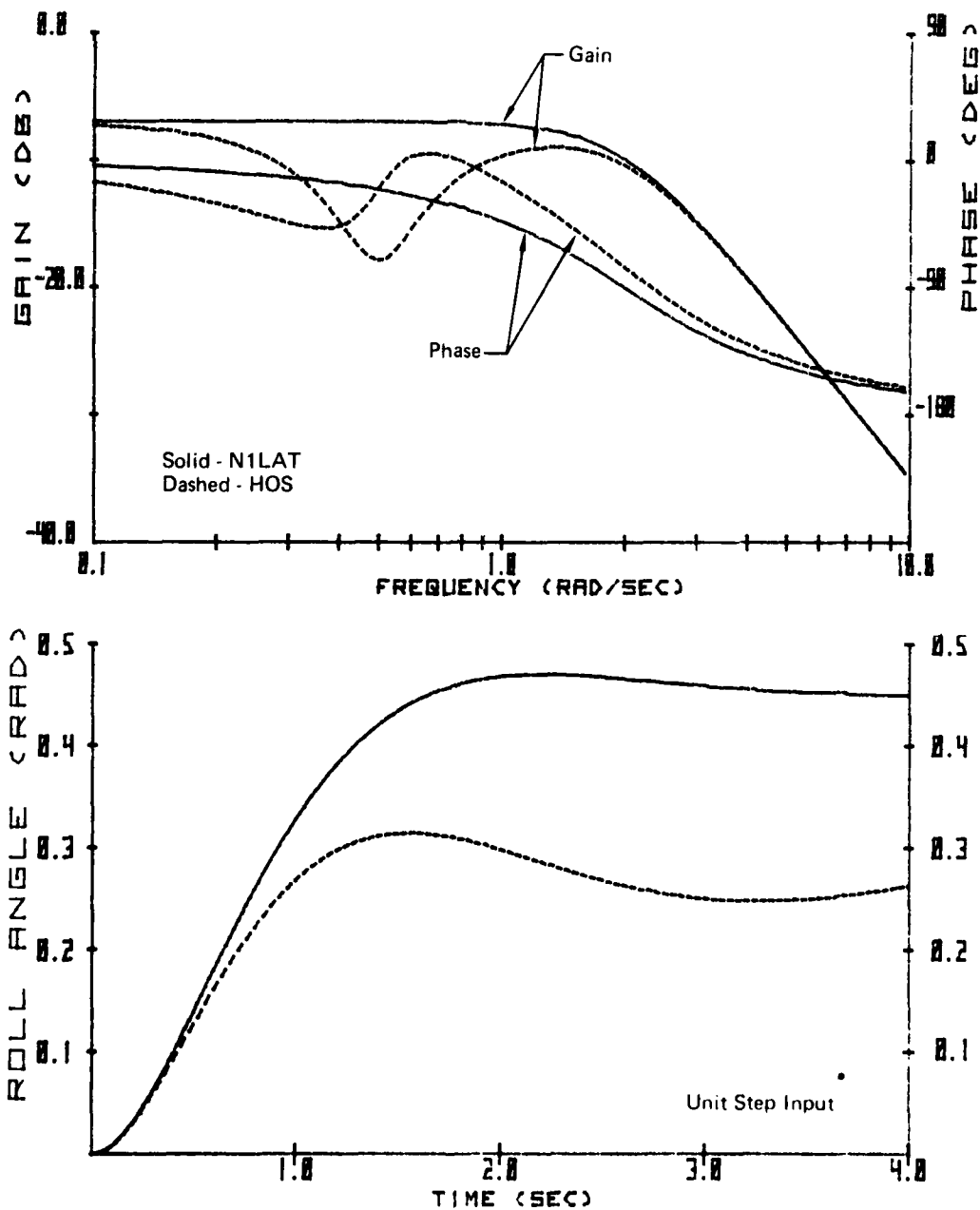
Config LF123
 $[\zeta = 0.2; \omega_L = 0.3] / [\zeta = 0.7; \omega_L = 0.3]$
 PR: 2.5, -, -, -



GP03-0208-58

Figure A-24. Frequency and Time Response

Config LF125
 $[\zeta = 0.2; \omega_L = 0.5] / [\zeta = 0.7; \omega_L = 0.5]$
 PR: 3.5, -, -, -



GP03-0208-59

Figure A-25. Frequency and Time Response

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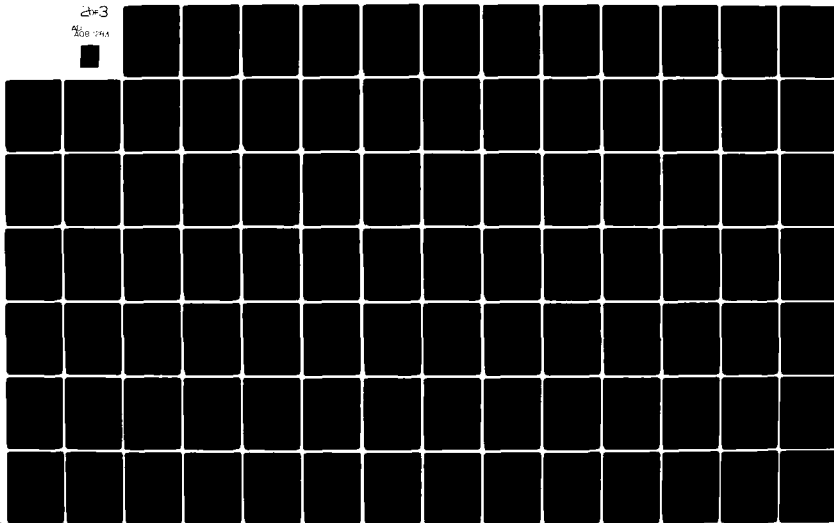
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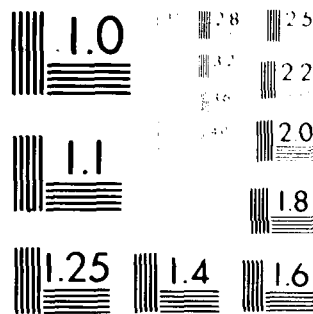
UNCLASSIFIED

NADC-79141-60

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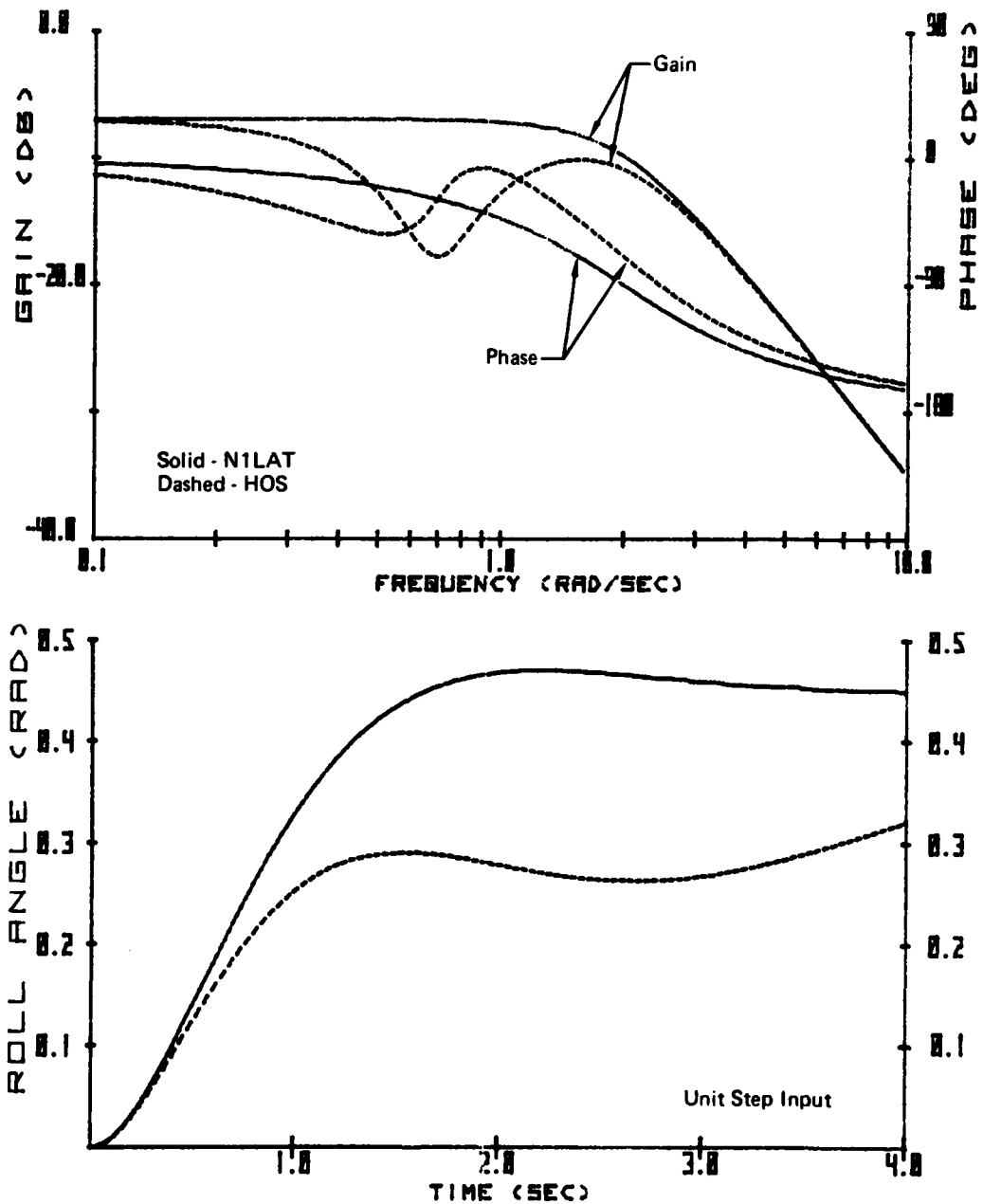
MICRO COPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

NADC-79141-60

Config LF127

$[\zeta = 0.2; \omega_L = 0.7] / [\zeta = 0.7; \omega_L = 0.7]$

PR: 5.5, -, 8, -



GP03-0200-00

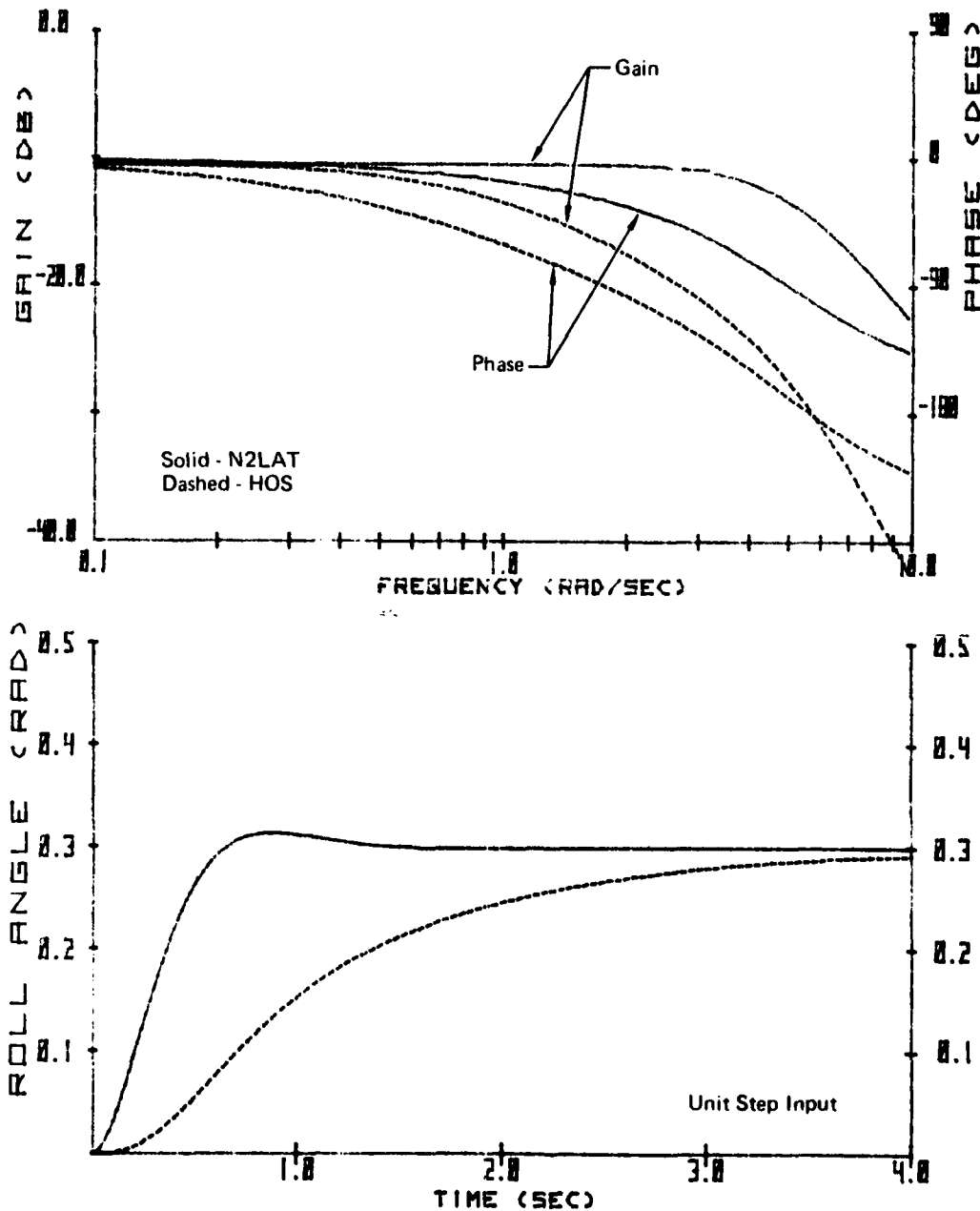
Figure A-26. Frequency and Time Response

NADC-79141-60

Config HF211

$\lambda = 1.0$

PR: 5.8, -, -, -



GP03-0206-01

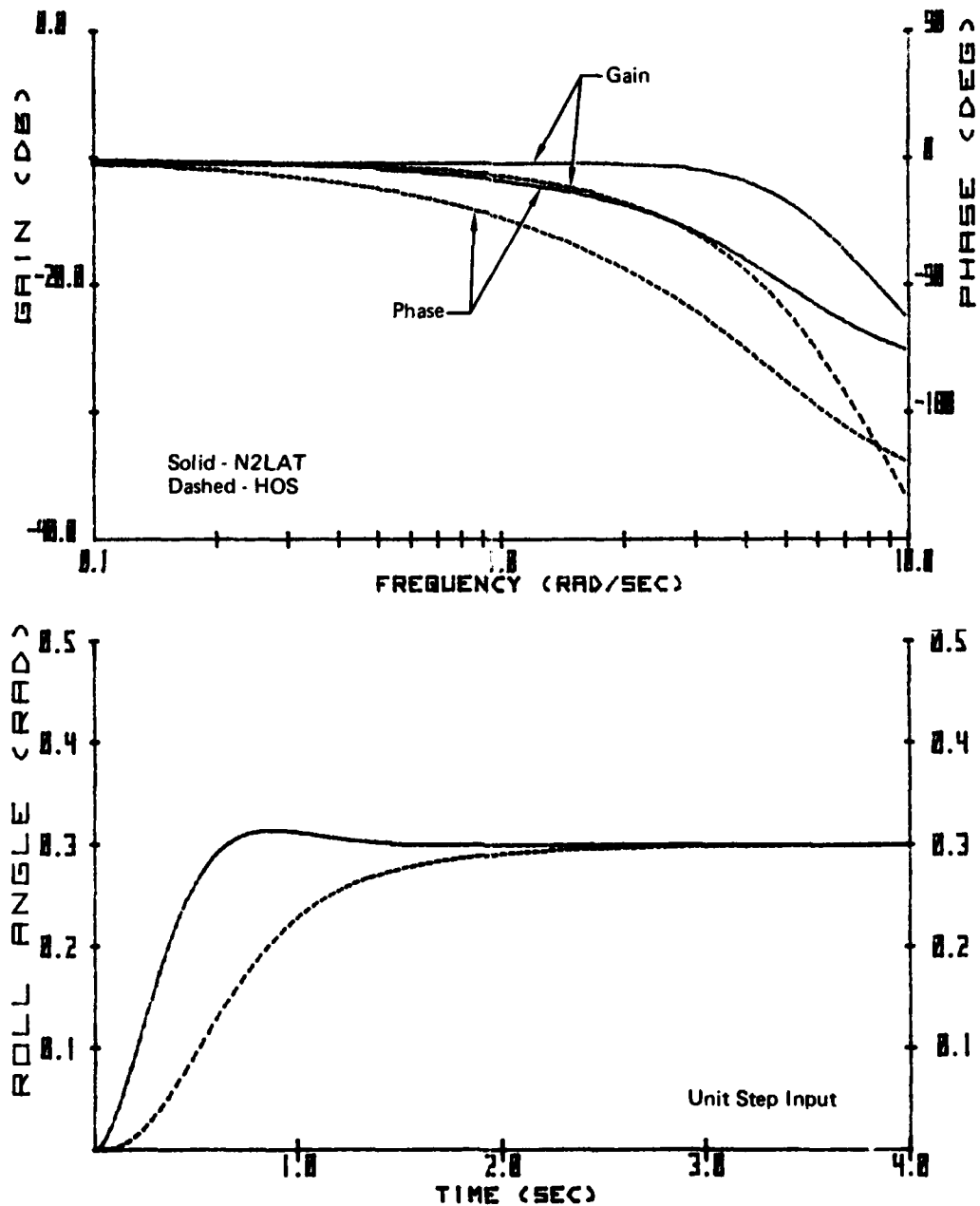
Figure A-27. Frequency and Time Response

NADC-79141-60

Config HF212

$\lambda = 2.0$

PR: 3.25, -, -, -



GP03-0200-02

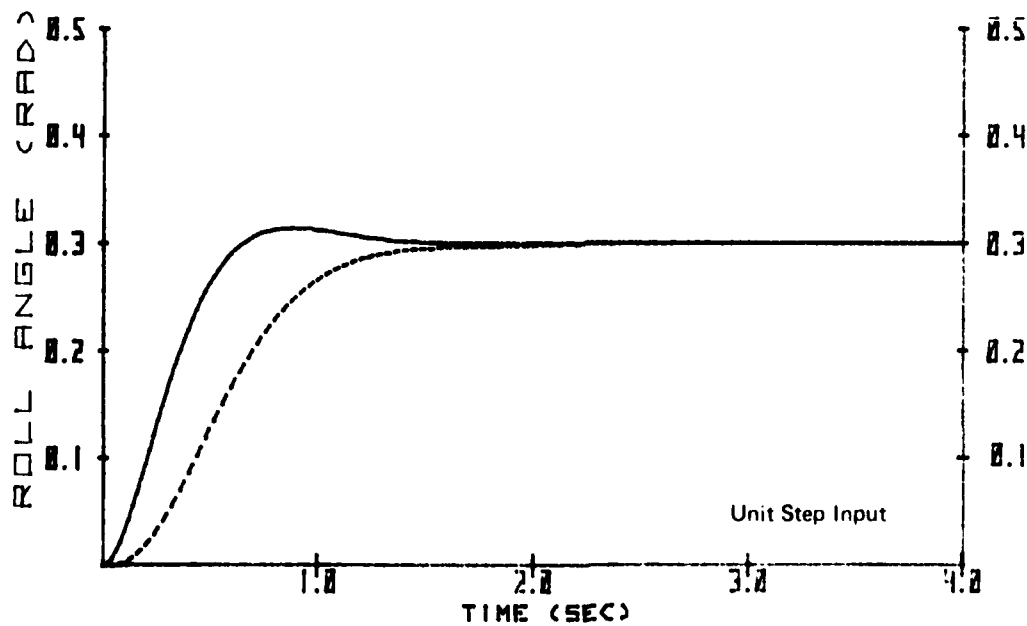
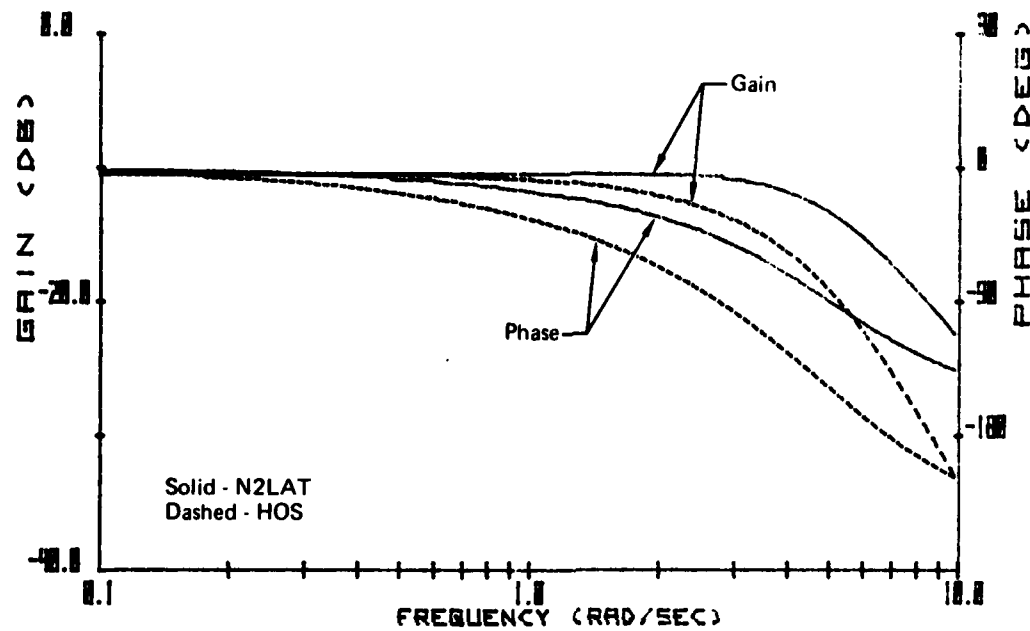
Figure A-28. Frequency and Time Response

NADC-79141-60

Config HF213

$\lambda = 3.0$

PR: 3.25, -, -, -



GP03-0208-43

Figure A-29. Frequency and Time Response

NADC-79141-60

Config HF214

$\lambda = 4.0$

PR: 3, 3.5, -, -

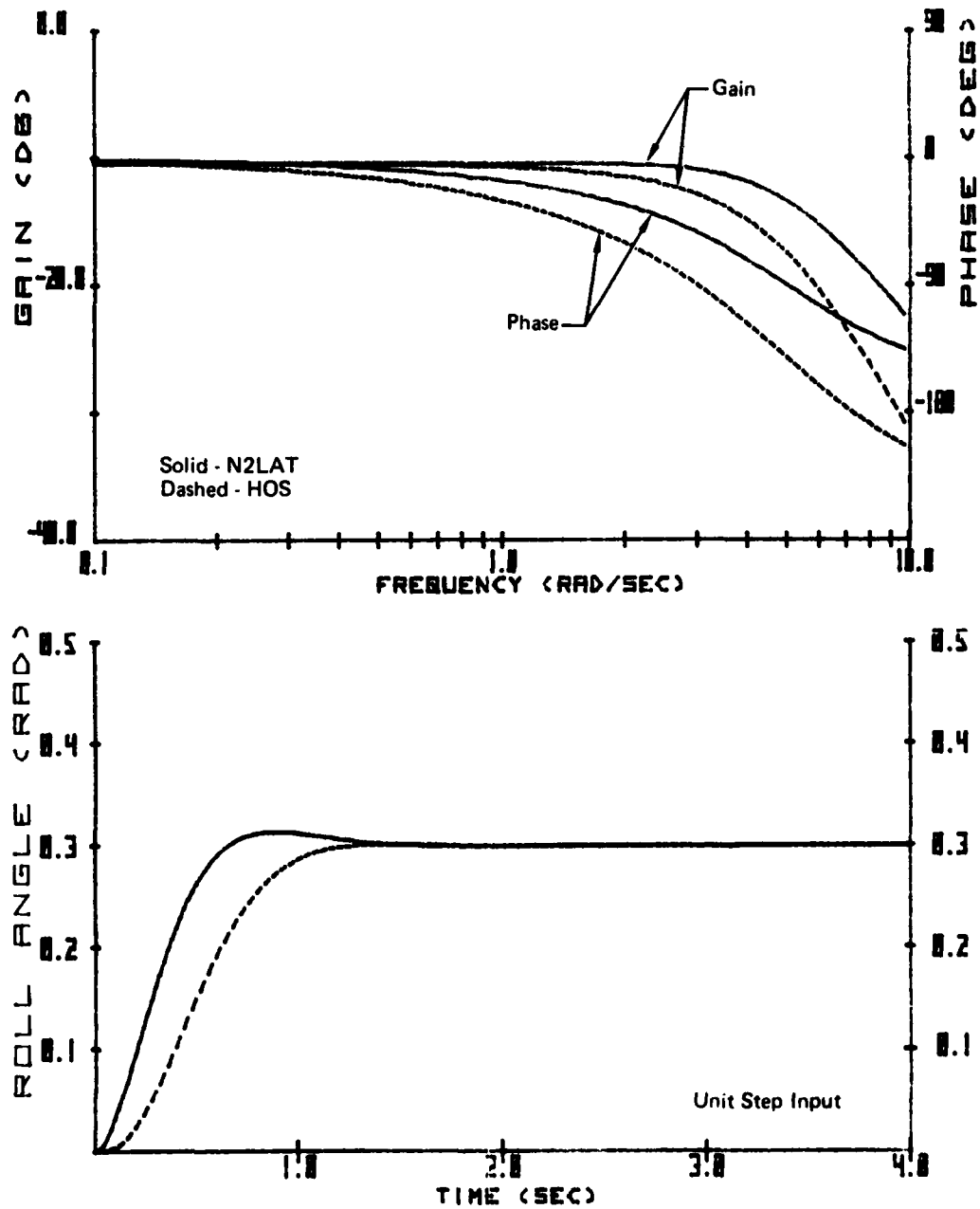


Figure A-30. Frequency and Time Response

GP03-0208-04

Config HF215
 $\lambda = 5.0$
 PR: 3, 3.75, 5, -

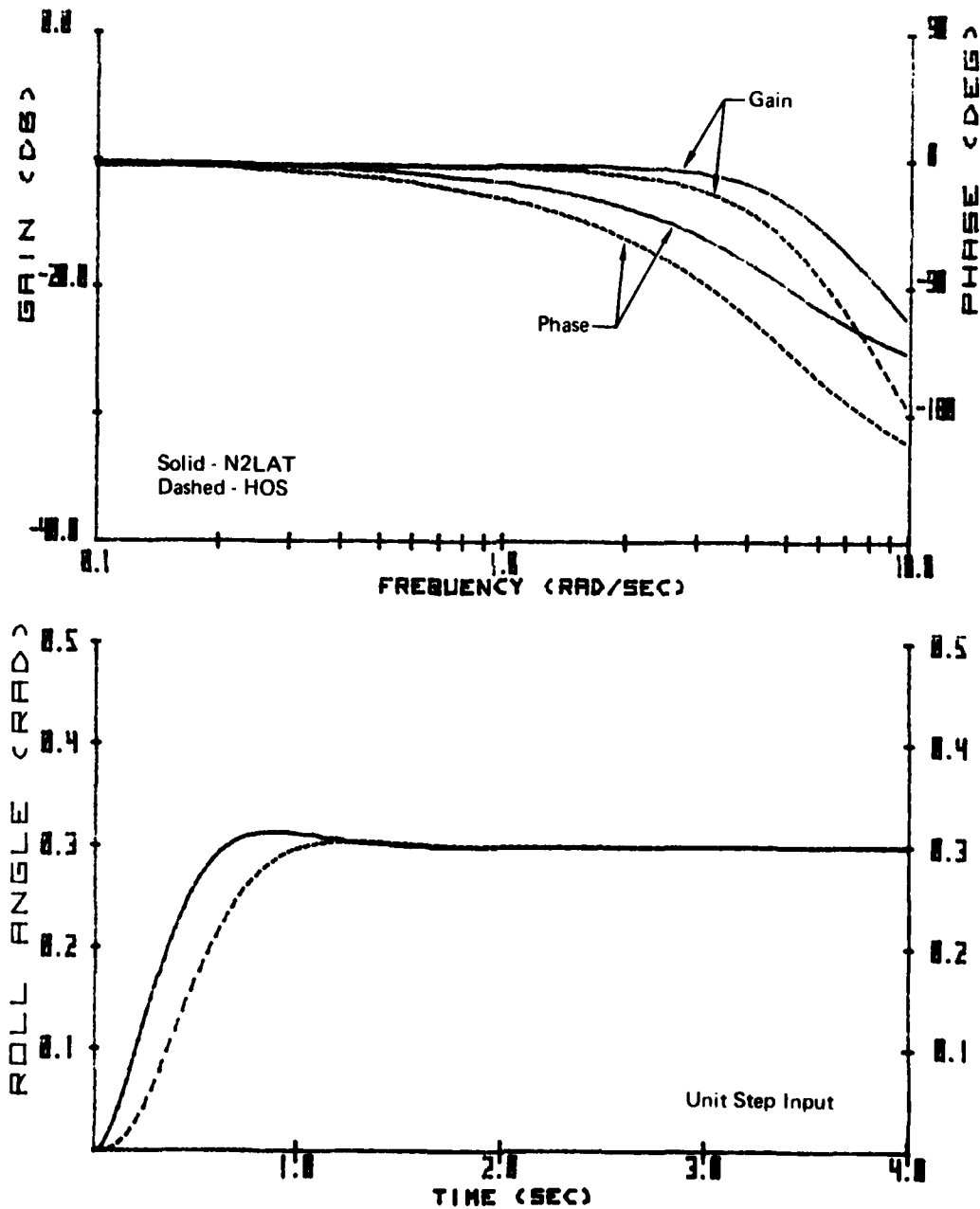


Figure A-31. Frequency and Time Response

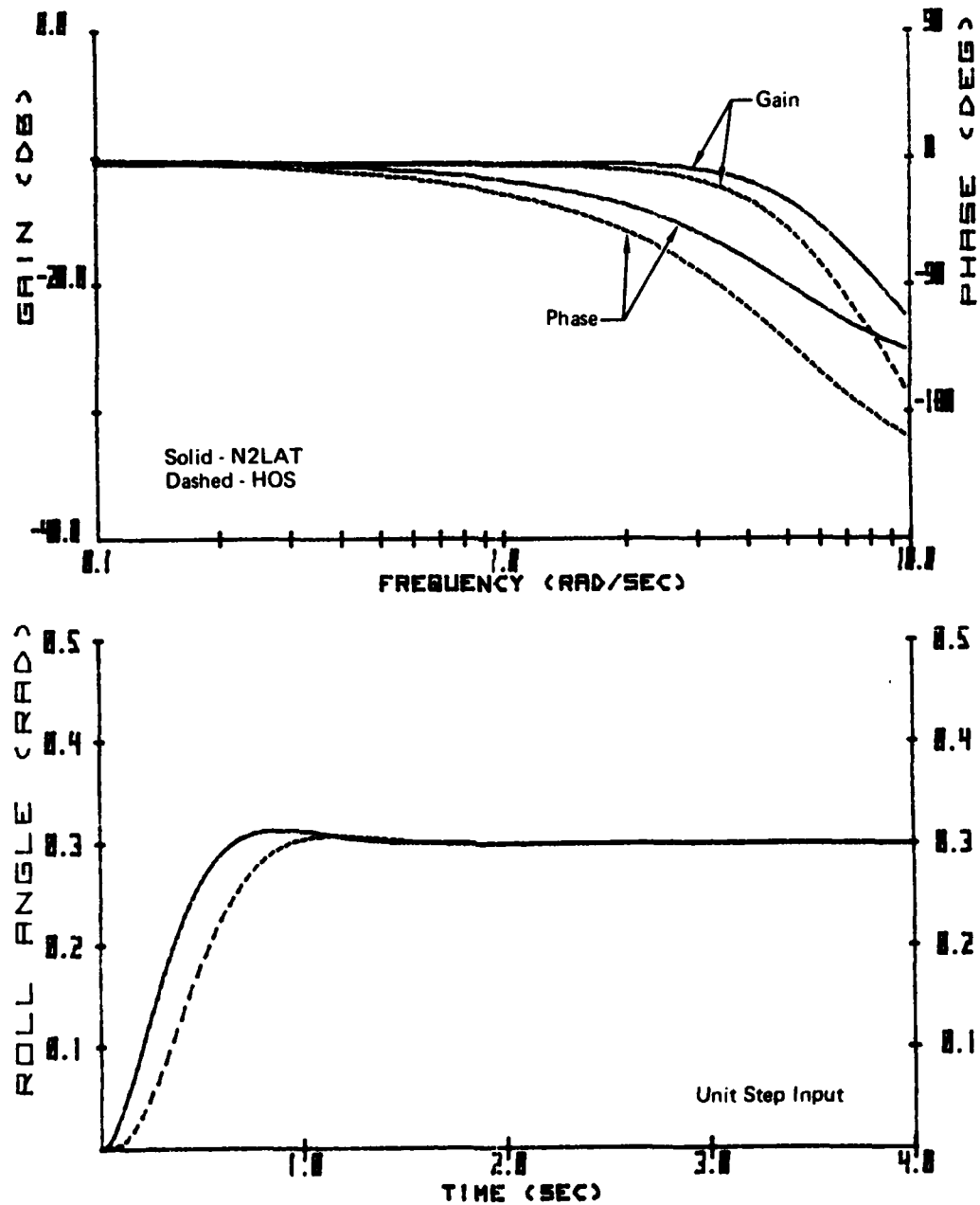
GP03-0200-05

NADC-79141-60

Config HF216

$\lambda = 6.0$

PR: 3, 4, -, -



QP03-0200-06

Figure A-32. Frequency and Time Response

NADC-79141-60

Config HF217

$\lambda = 7.0$

PR: 3, -, 5, -

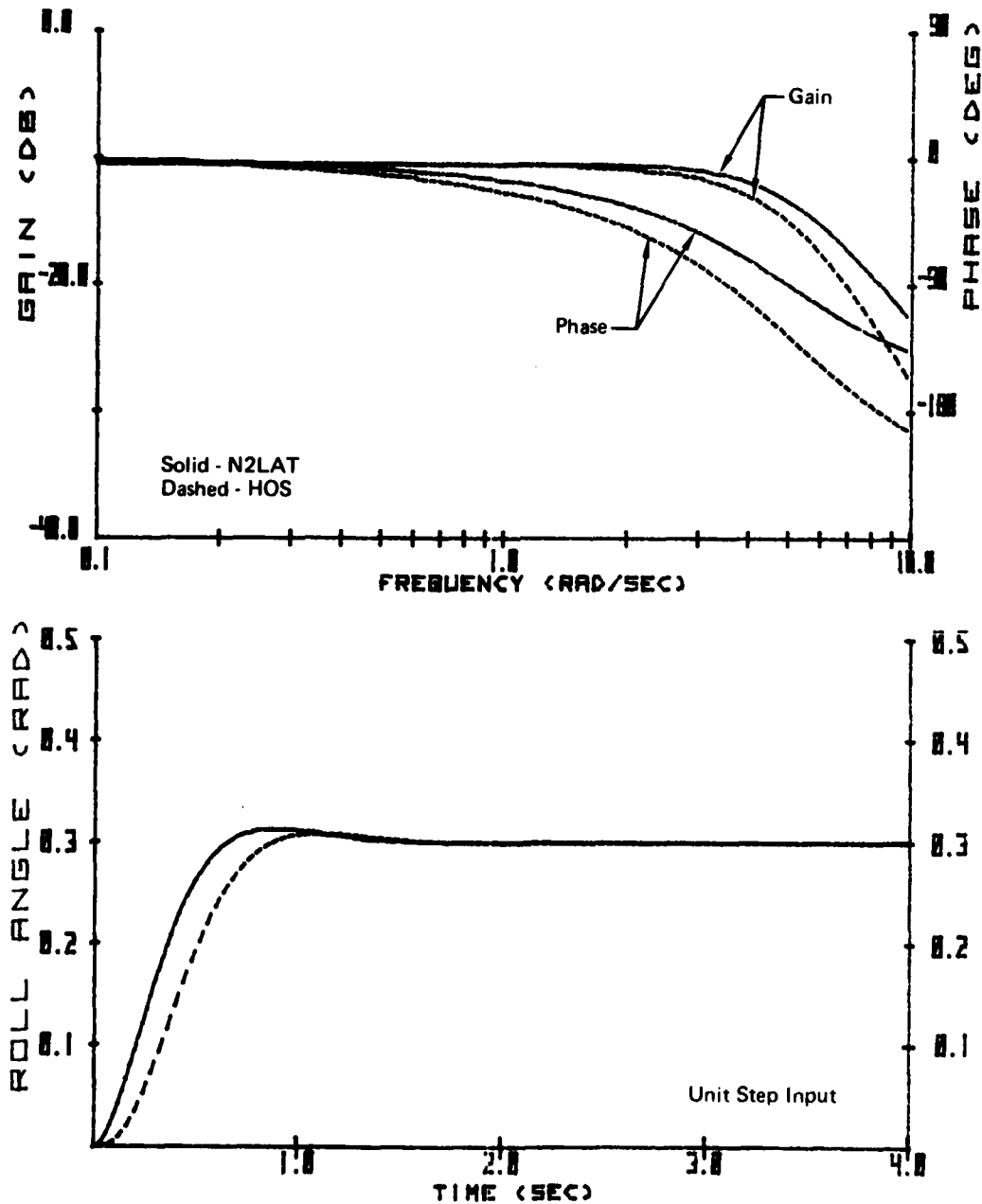
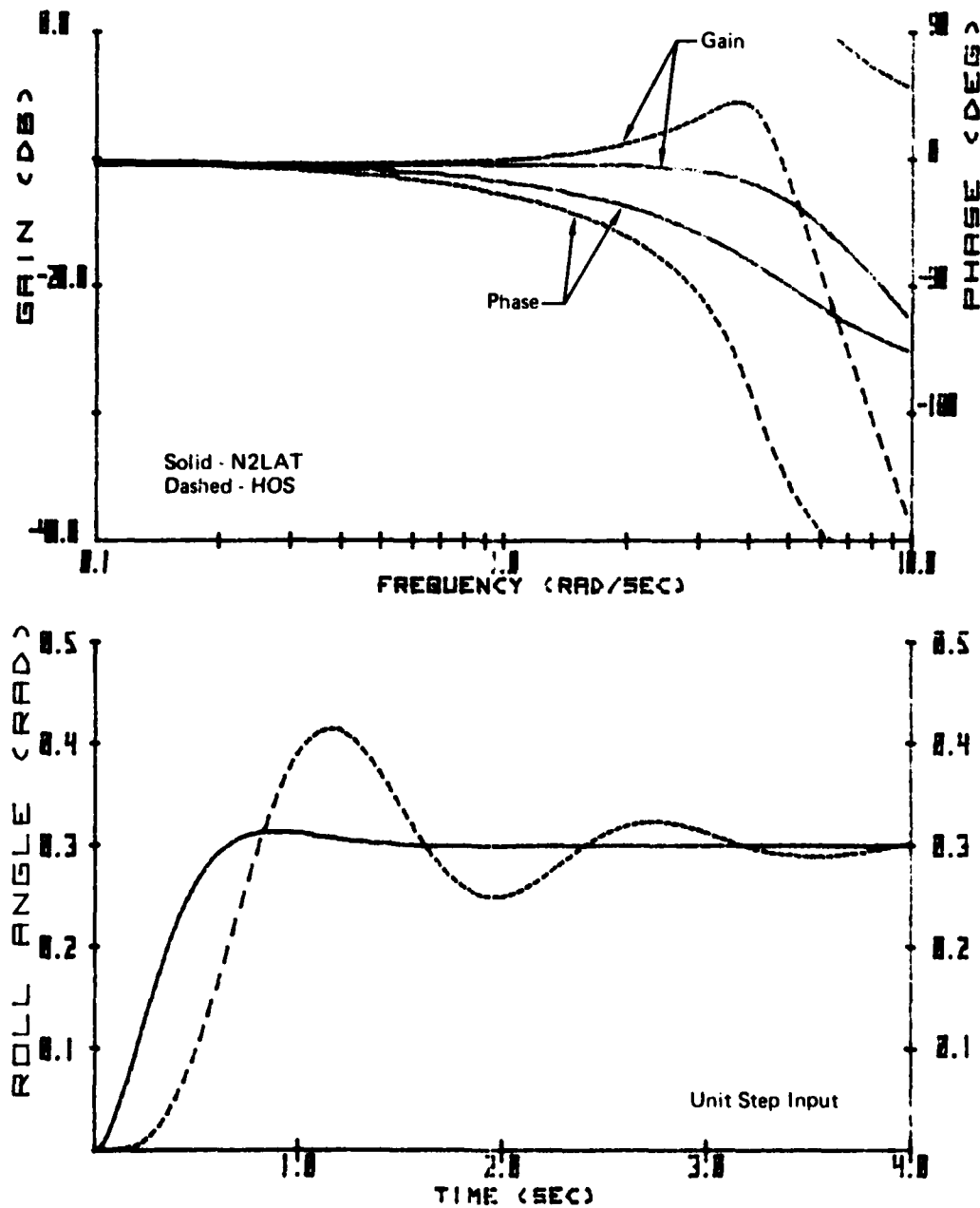


Figure A-33. Frequency and Time Response

GP03-0208-47

NADC-79141-60

Config HF224
 $\zeta = 0.3; \omega_L = 4$
PR: 7, 5, -, -

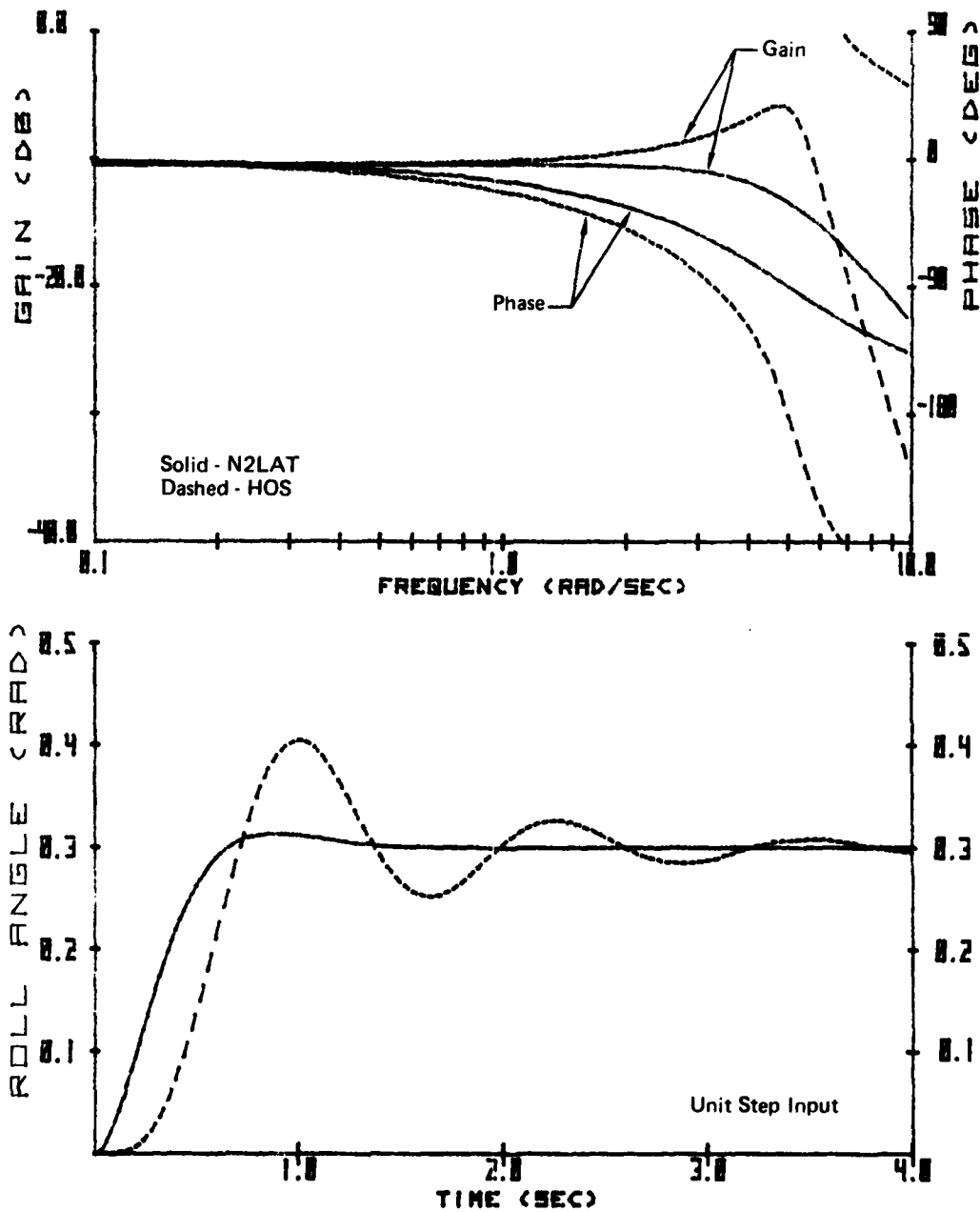


QP03-0208-00

Figure A-34. Frequency and Time Response

NADC-79141-60

Config HF225
 $\zeta = 0.3; \omega_L = 5$
 PR: -, 7.5, 7, -

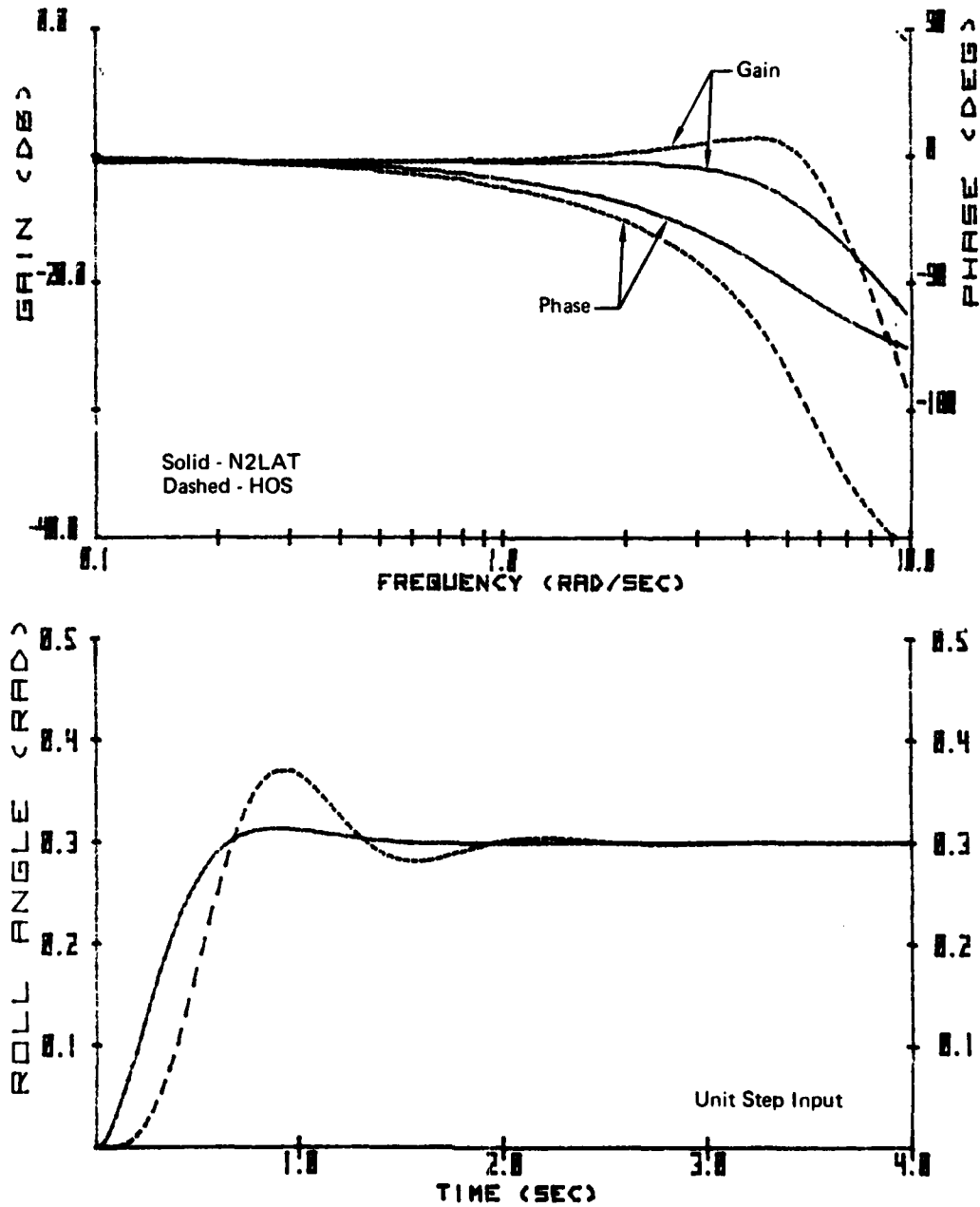


GP03-0208-00

Figure A-35. Frequency and Time Response

NADC-79141-60

Config HF226
 $\zeta = 0.3; \omega_L = 6$
 PR: 6, 5.5, -, -

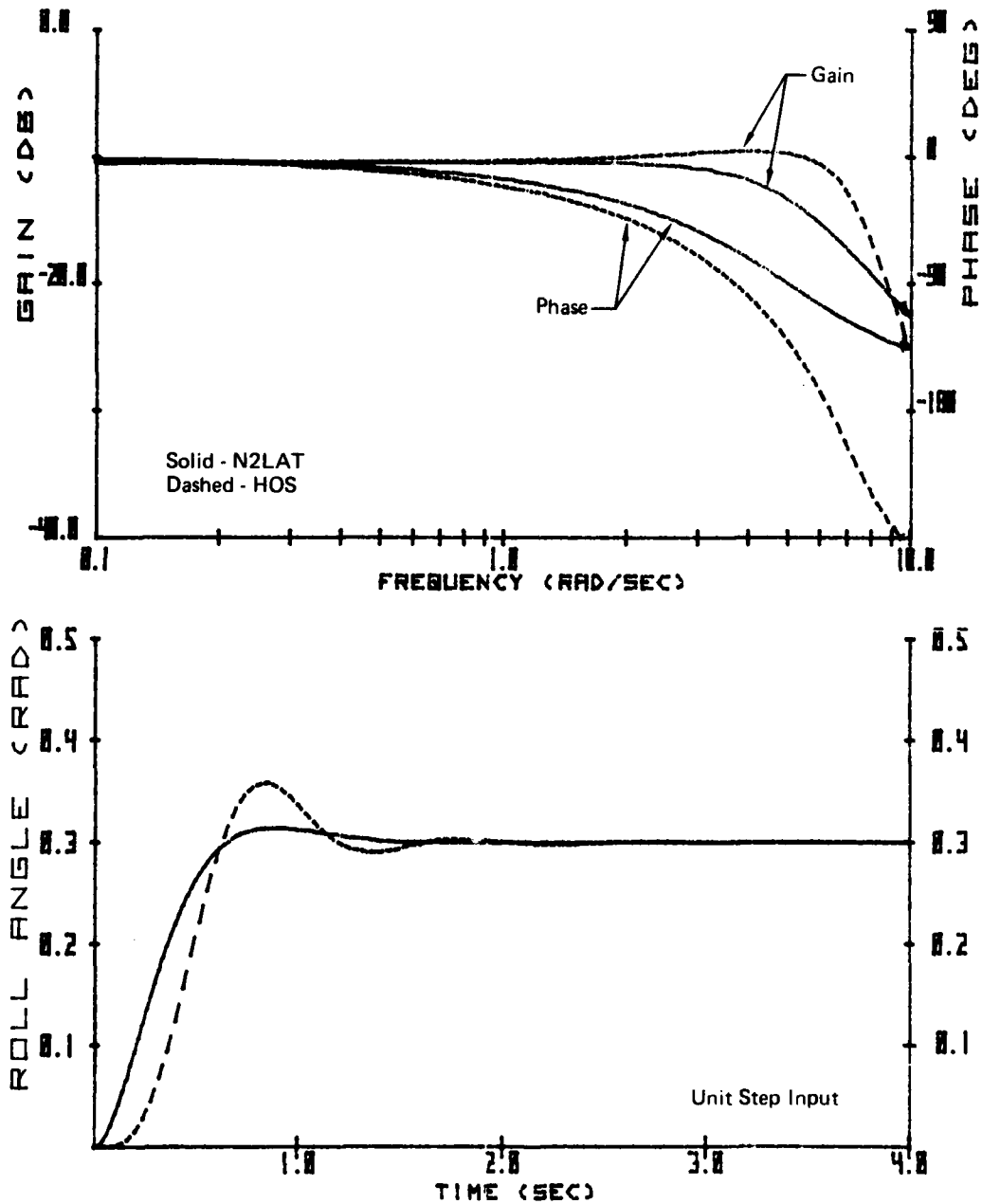


GP03-0200-70

Figure A-36. Frequency and Time Response

NADC-79141-60

Config HF227
 $[\zeta = 0.3; \omega_L = 7]$
 PR: 6, 5.5, 6, -

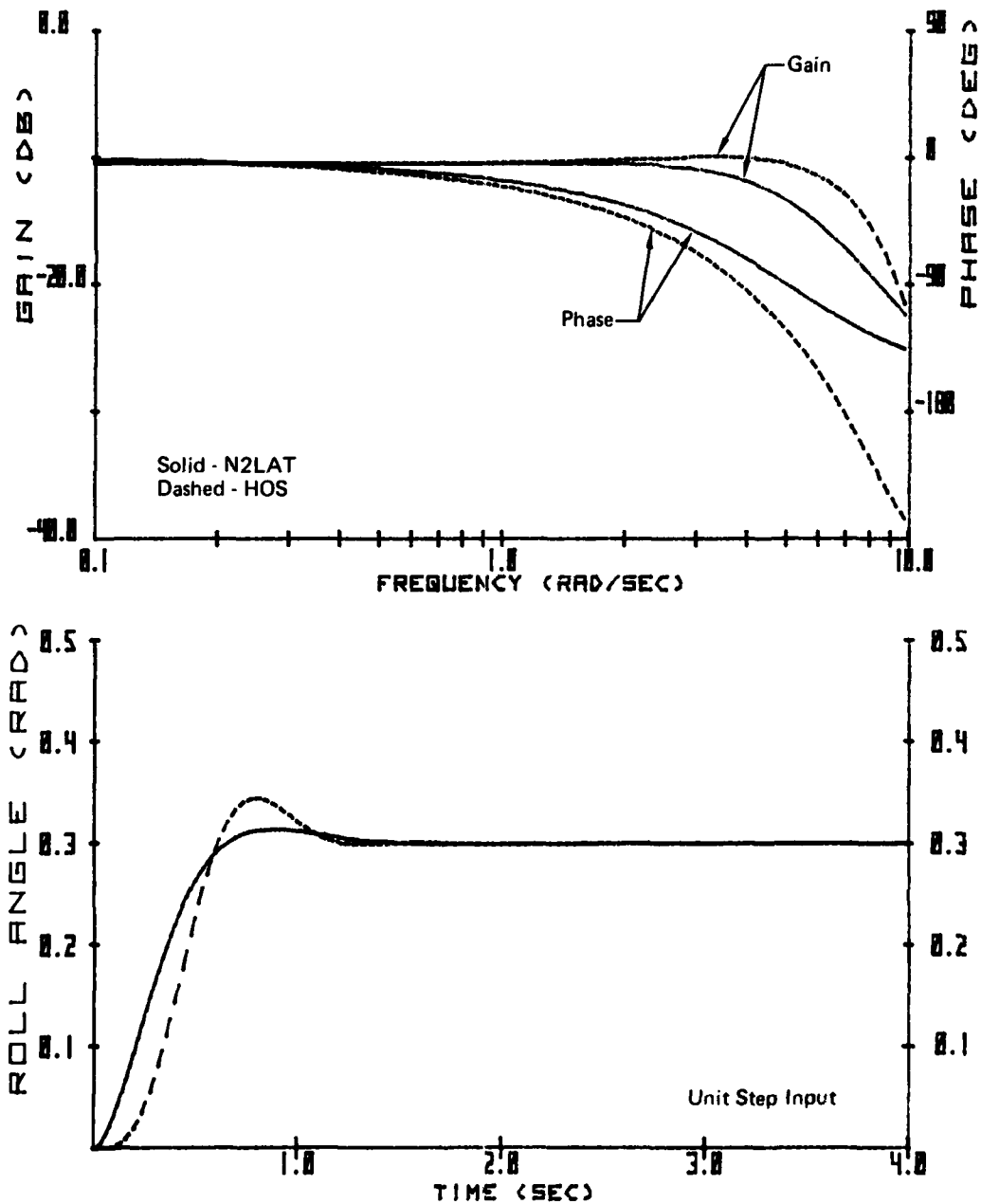


GP03-0200-71

Figure A-37. Frequency and Time Response

NADC-79141-60

Config HF228
[$\xi = 0.3$; $\omega_L = 8$]
PR: 5.5, -, -, -



GP03-0208-72

Figure A-38. Frequency and Time Response

NADC-79141-60

Config HF229
 $\zeta = 0.3; \omega_L = 9$
 PR: 4, -, -, -

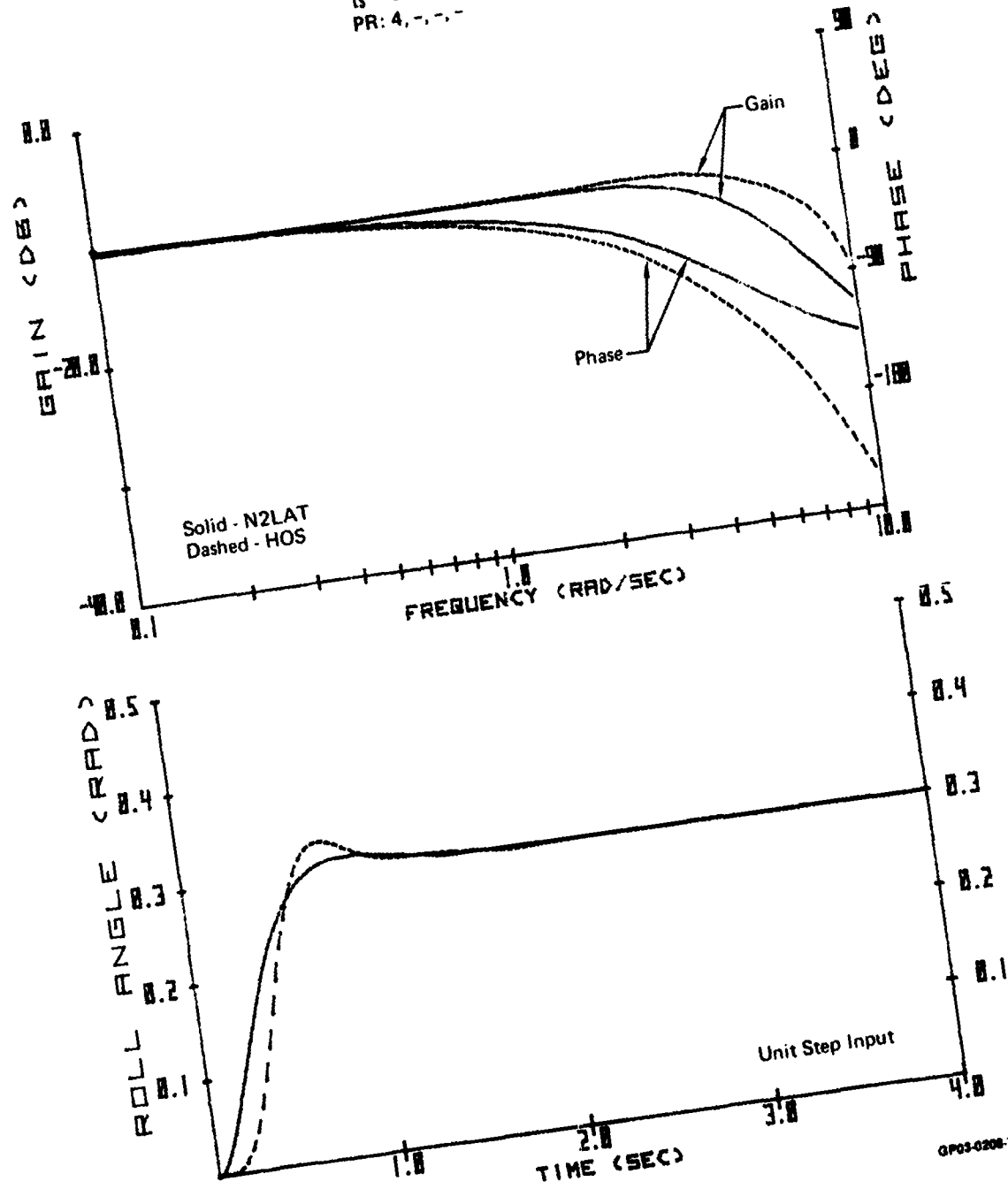


Figure A-39. Frequency and Time Response

NADC-79141-60

Config HF220
 $\zeta = 0.3; \omega_L = 10$
 PR: 5, -, -, -

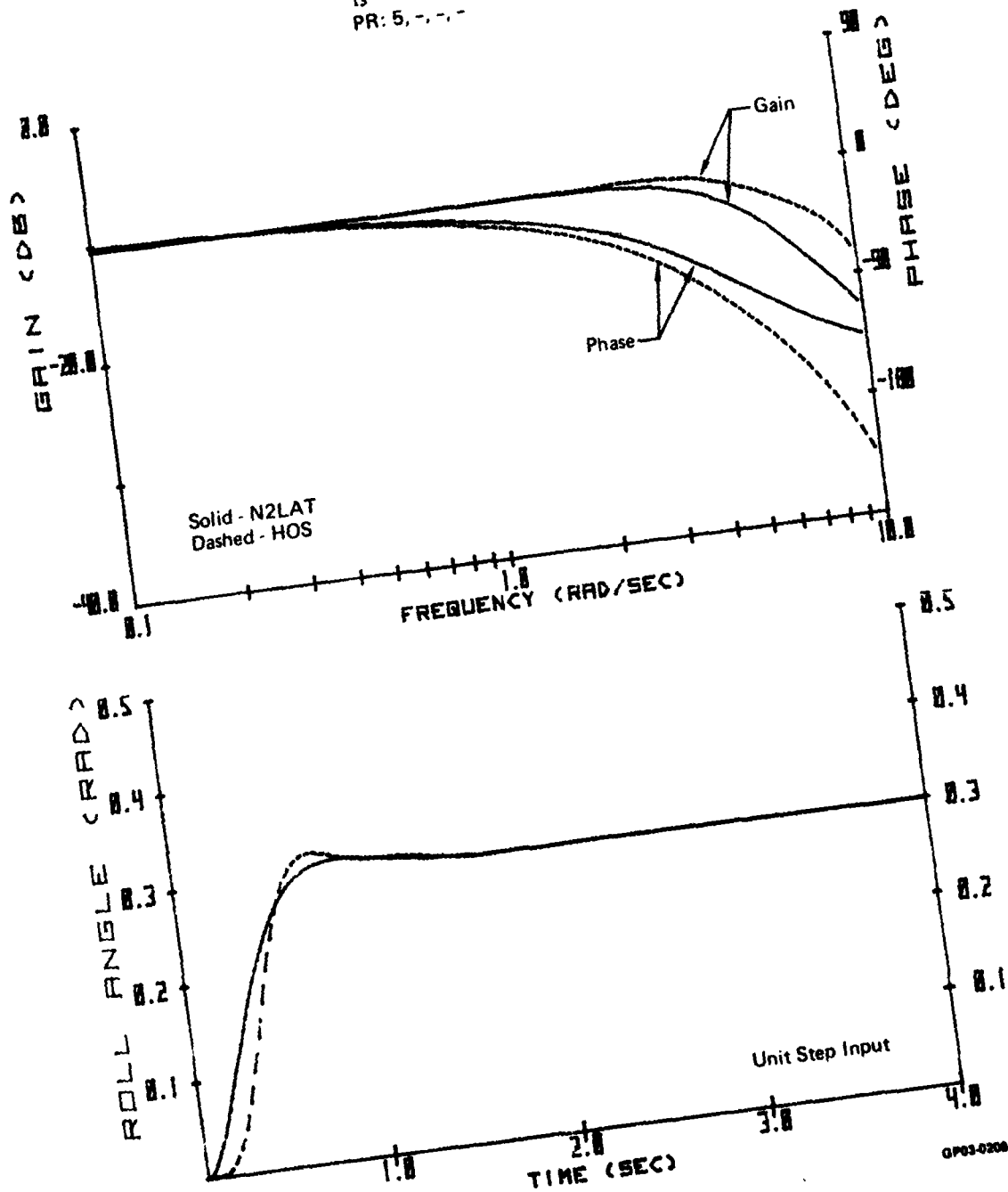


Figure A-40. Frequency and Time Response

NADC-79141-60

Config HF221
[$\zeta = 0.3$; $\omega_L = 11$]
PR: 4.25, -, -, -

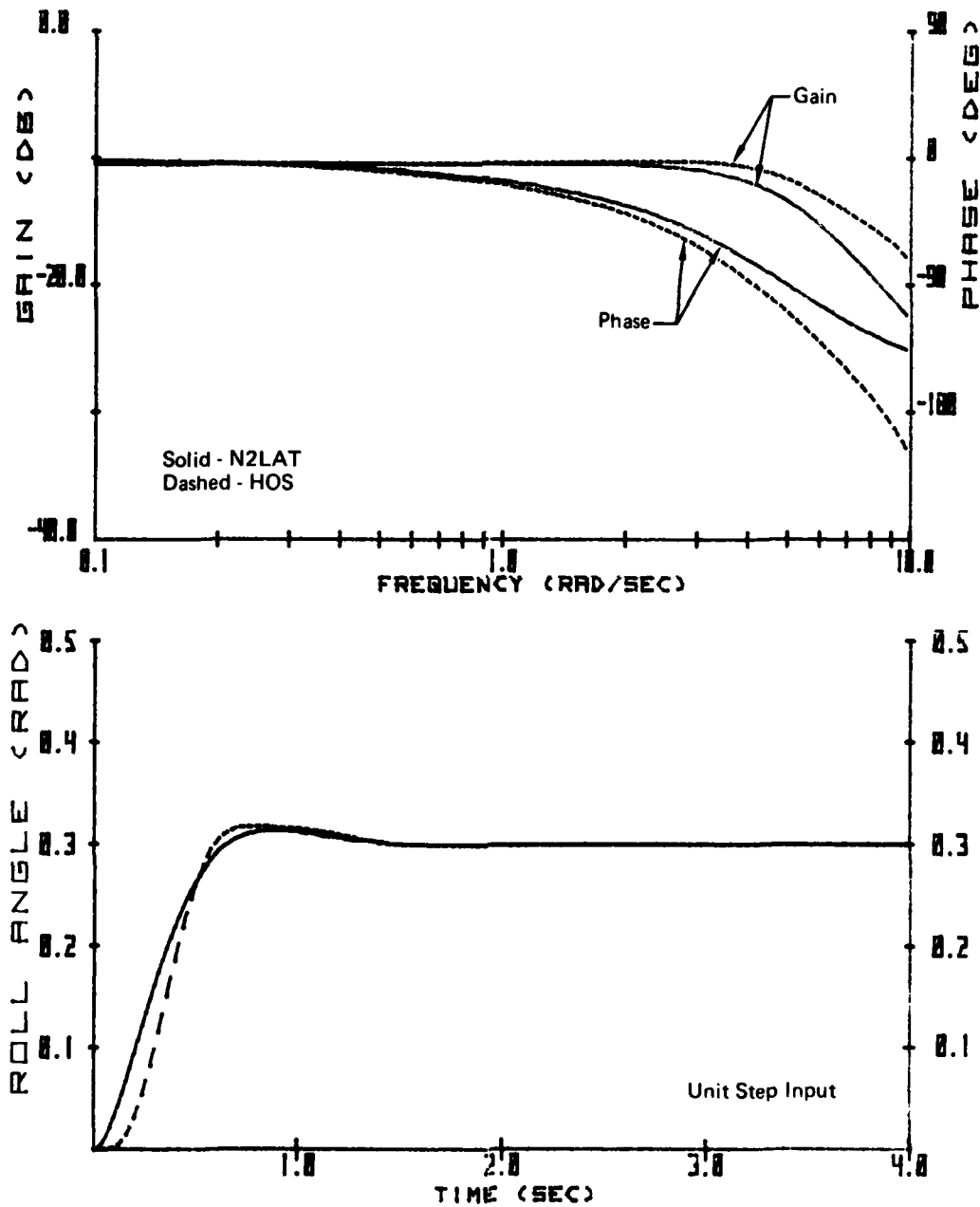


Figure A-41. Frequency and Time Response

GP03-0208-75

Config HF2T1
 $\tau = 0.05$
 PR: 3, 3.75, 5, -

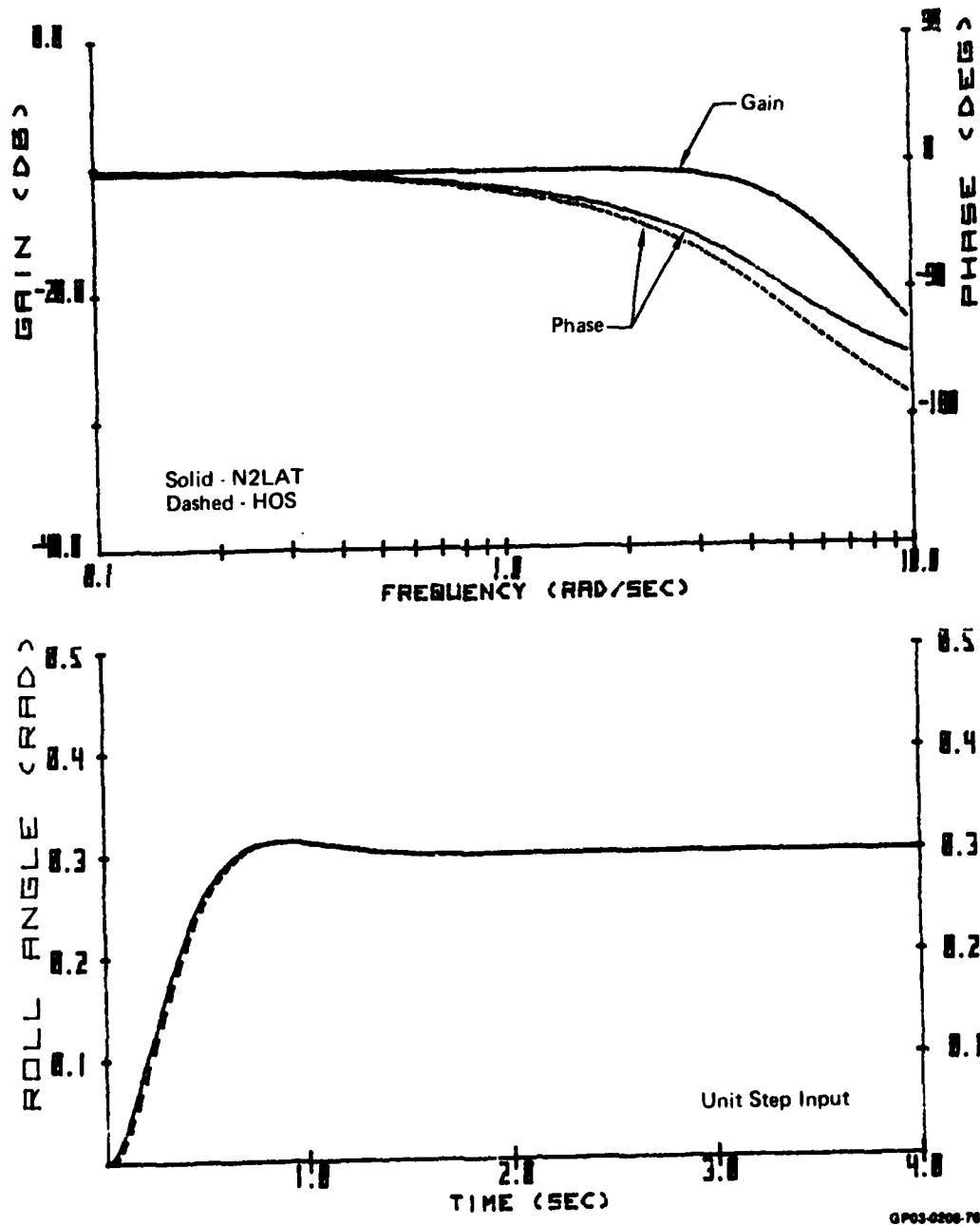


Figure A-42. Frequency and Time Response

NADC-79141-60

Config HF2T2
 $\tau = 0.08$
 PR: 2.5, 5, -, -

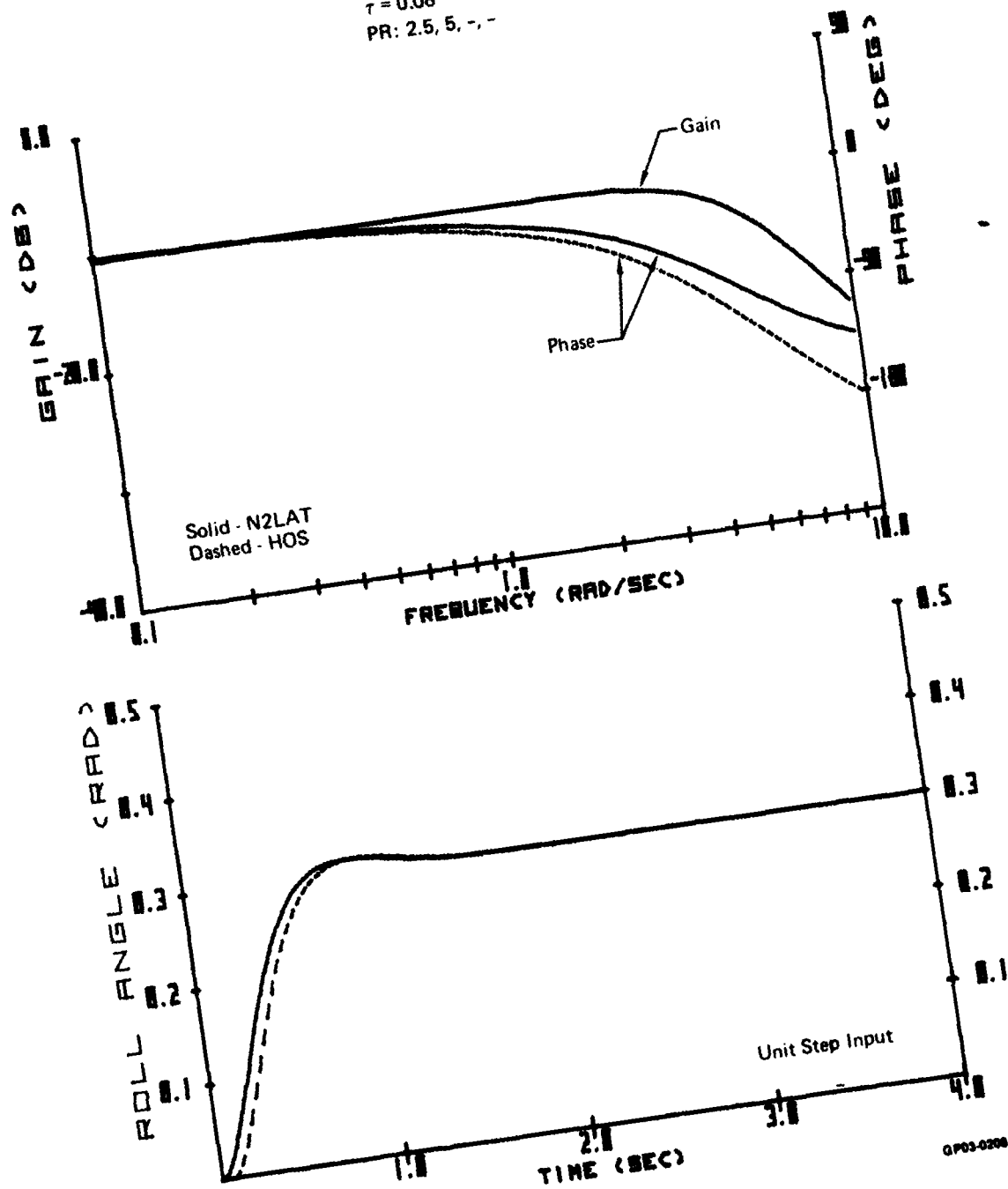


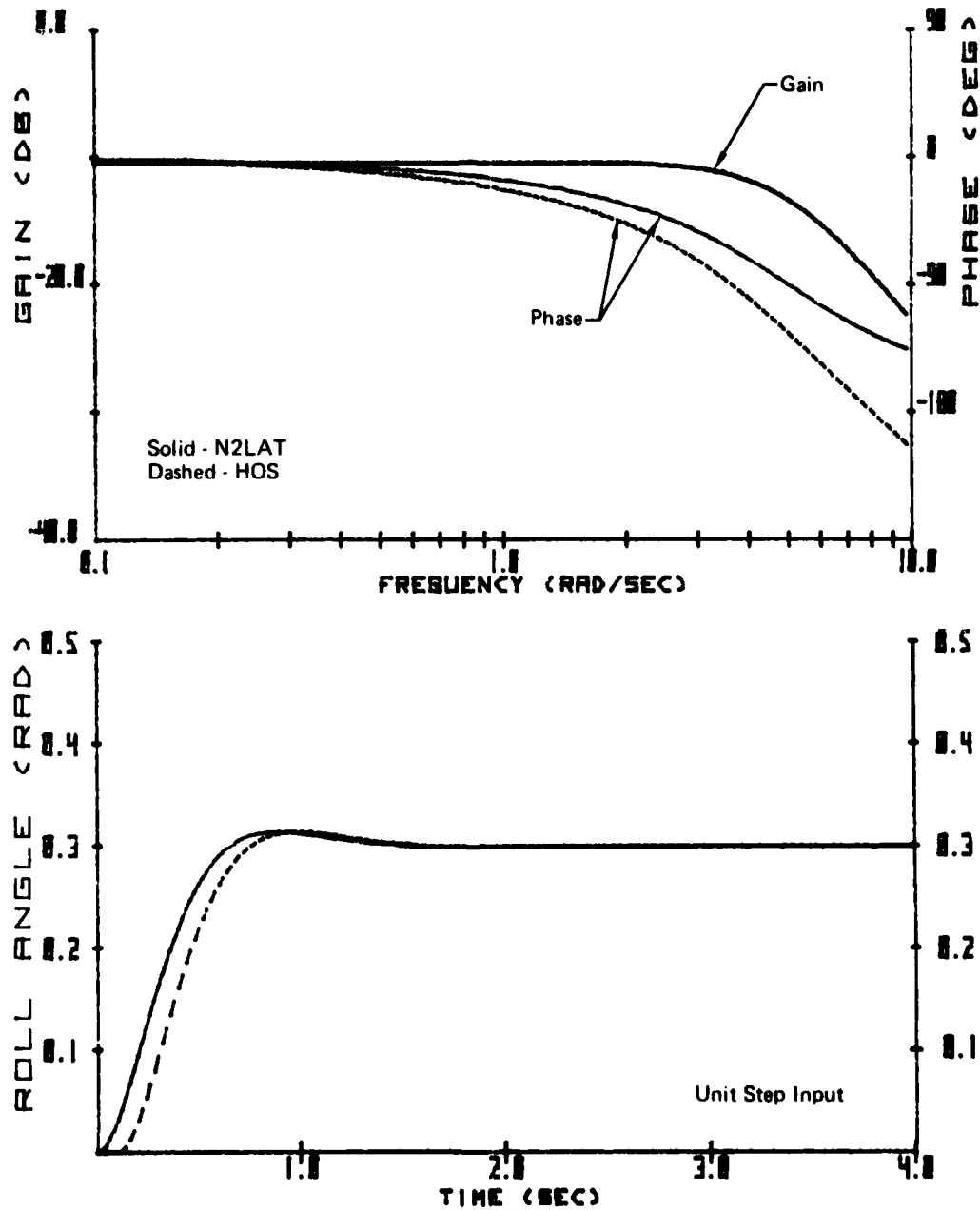
Figure A-43. Frequency and Time Response

NADC-79141-60

Config HF2T3

$\tau = 0.12$

PR: 3, 5, -, -



GP03-0208-78

Figure A-44. Frequency and Time Response

NADC-79141-60

Config HF2T4

$\tau = 0.16$

PR: 5, 4, -, -

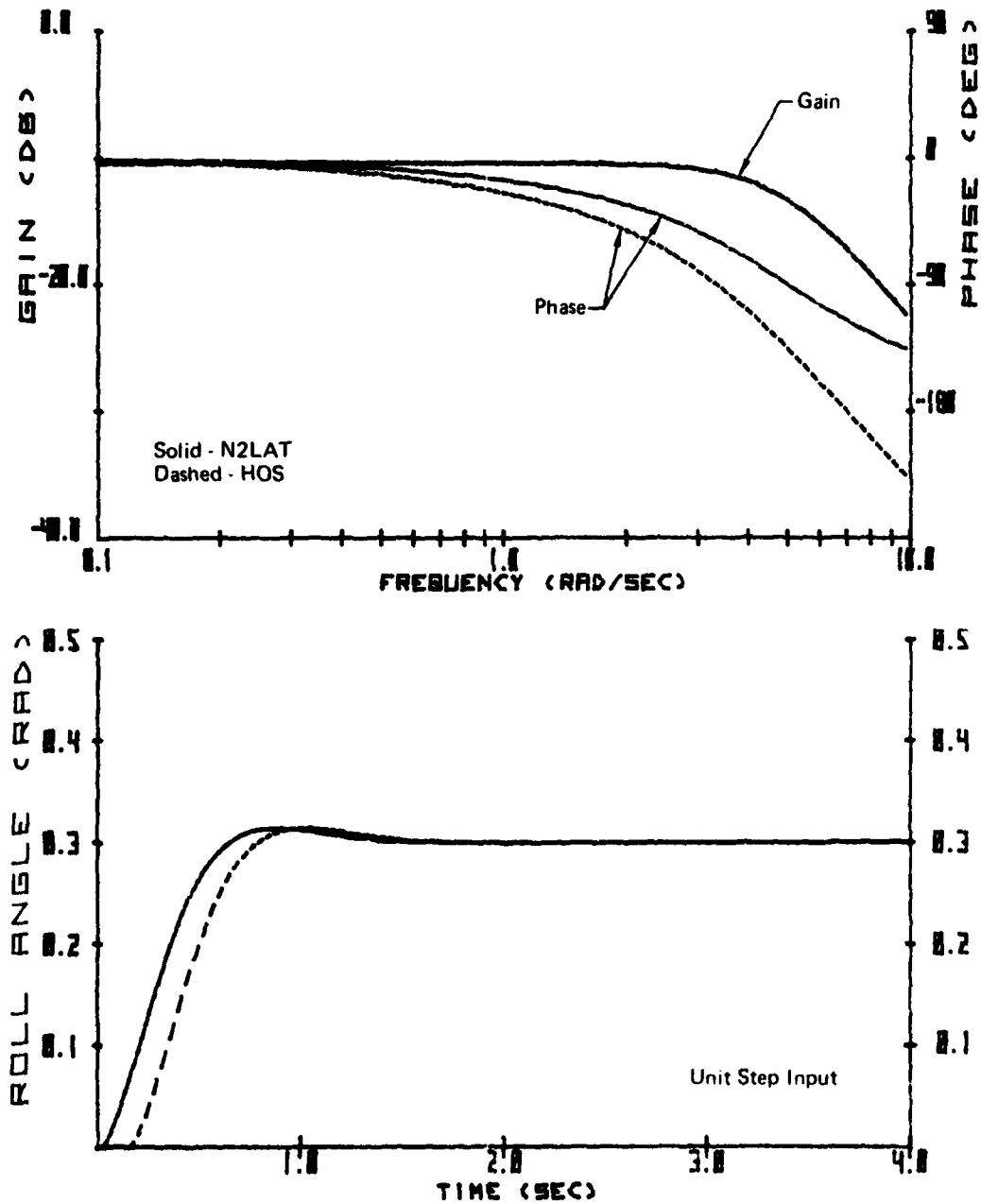


Figure A-45. Frequency and Time Response

GP03-0208-79

NADC-79141-60

Config HF2T5

$\tau = 0.2$

PR: 5, -, -, -

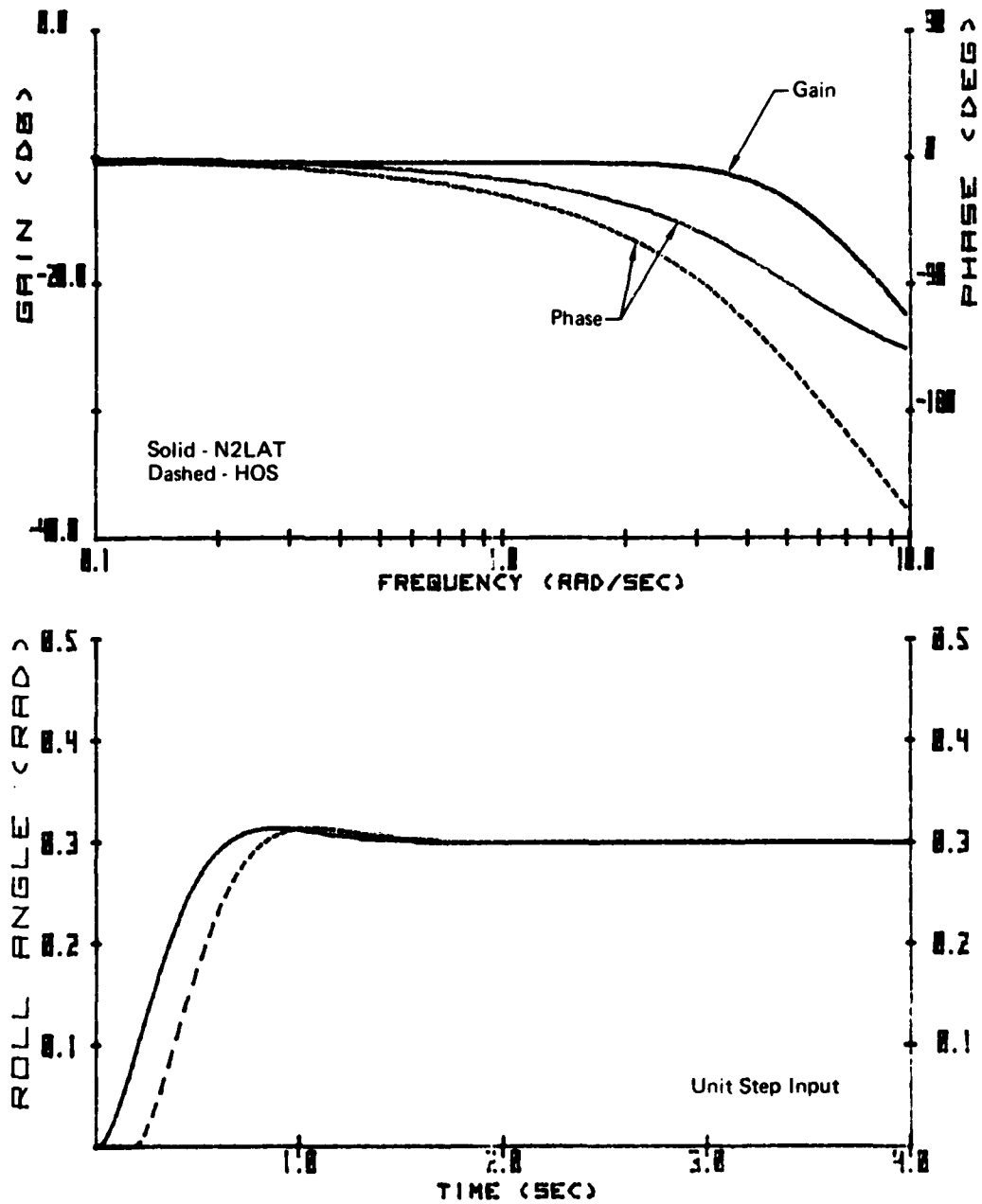


Figure A-46. Frequency and Time Response

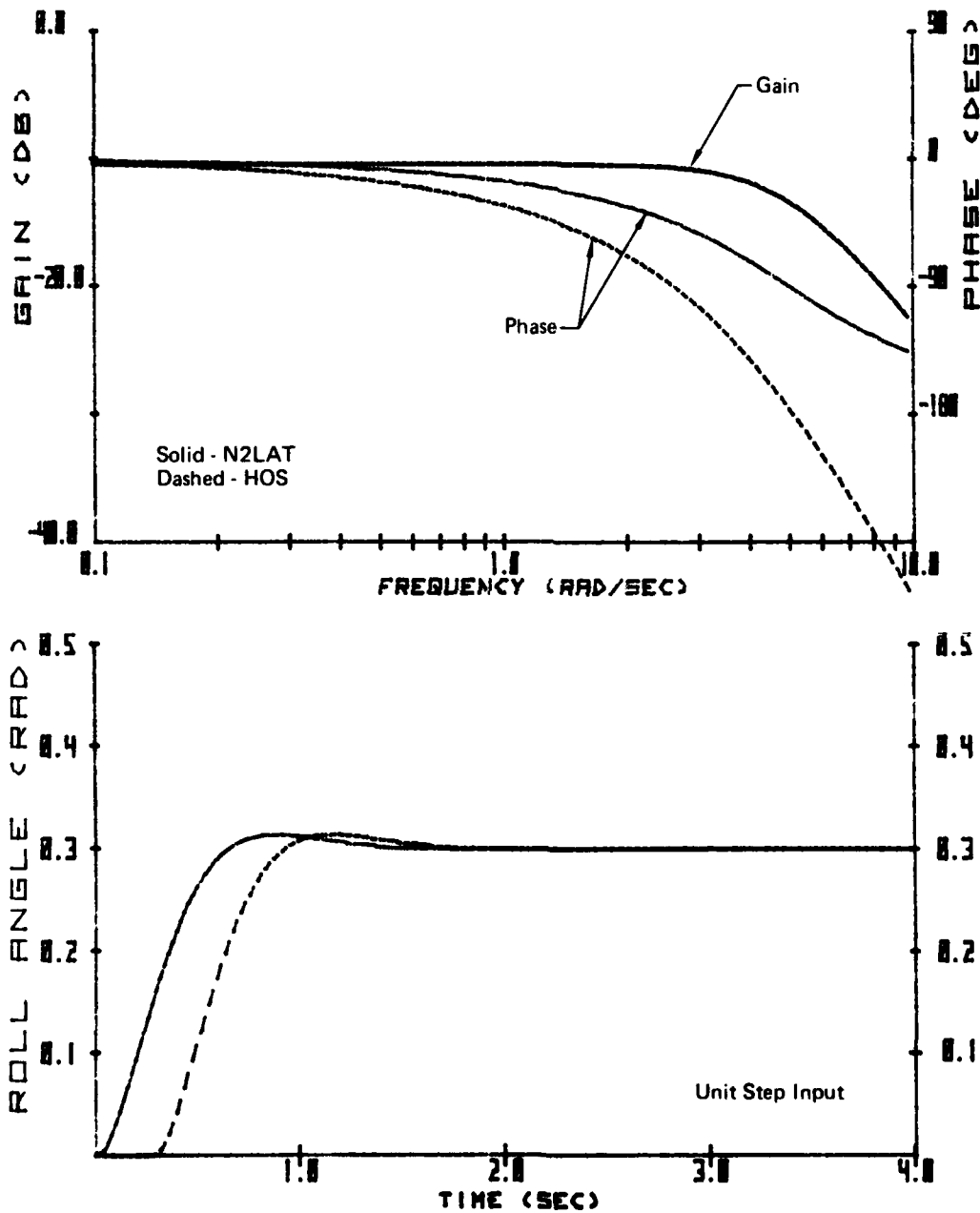
GP03-0200-00

NADC-79141-60

Config HF2T6

$\tau = 0.3$

PR: 6, -, -, -



GP03-0200-01

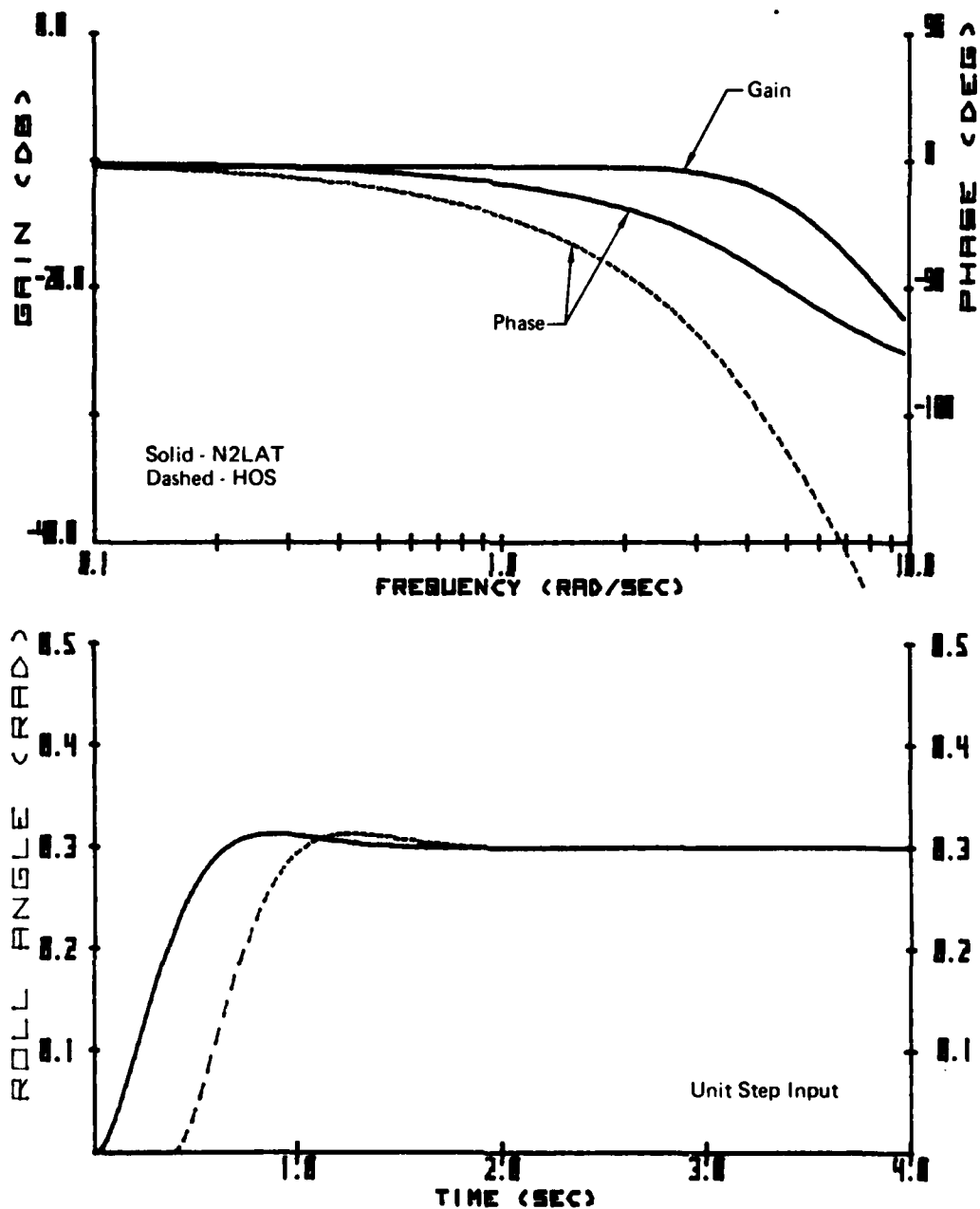
Figure A-47. Frequency and Time Response

NADC-79141-60

Config HF2T7

$\tau = 0.4$

PR: 8.5, -, -, -



GP03-0208-82

Figure A-48. Frequency and Time Response

Config LF221
 $[\xi = 0.2; \omega_L = 0.1] / [\xi = 0.7; \omega_L = 0.1]$
 PR: 3, -, -, -

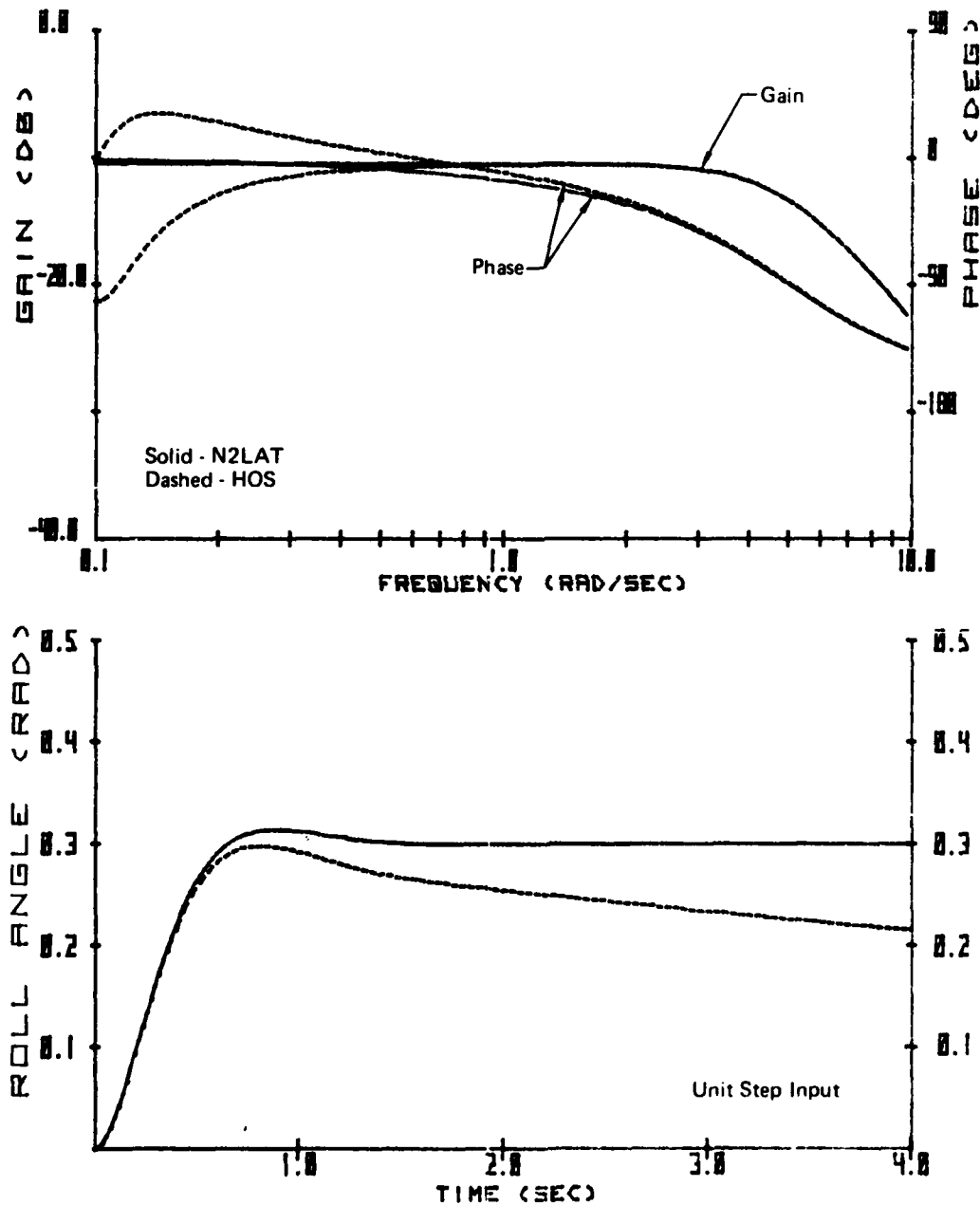


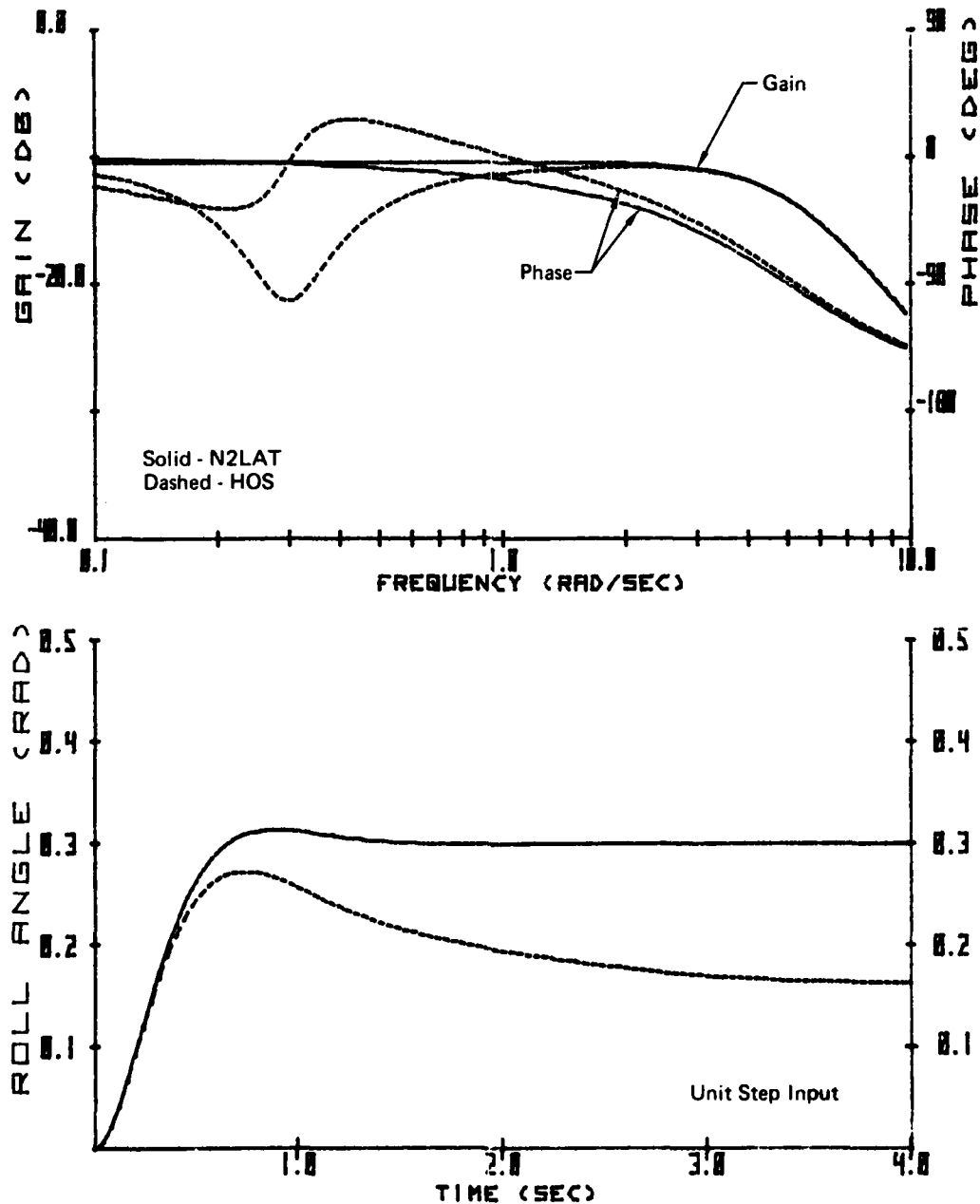
Figure A-49. Frequency and Time Response

GP03-0200-83

Config LF223

$[\zeta = 0.2; \omega_L = 0.3] / [\zeta = 0.7; \omega_L = 0.3]$

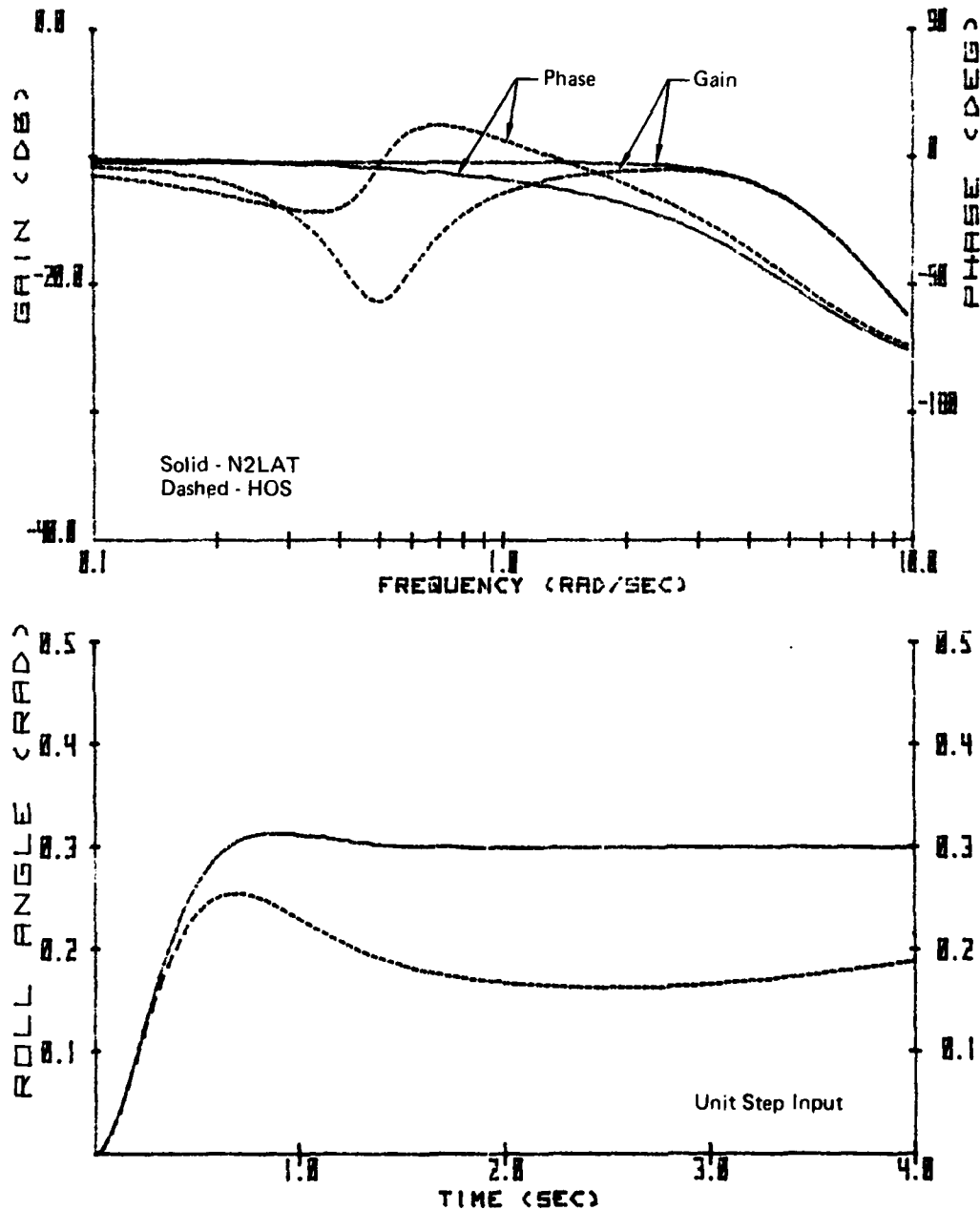
PR: 4, -, 8, -



GP03-0208-84

Figure A-50. Frequency and Time Response

Config LF225
 $[\zeta = 0.2; \omega_L = 0.5] / [\zeta = 0.7; \omega_L = 0.5]$
 PR: 6, -, -, -



OP03-0208-85

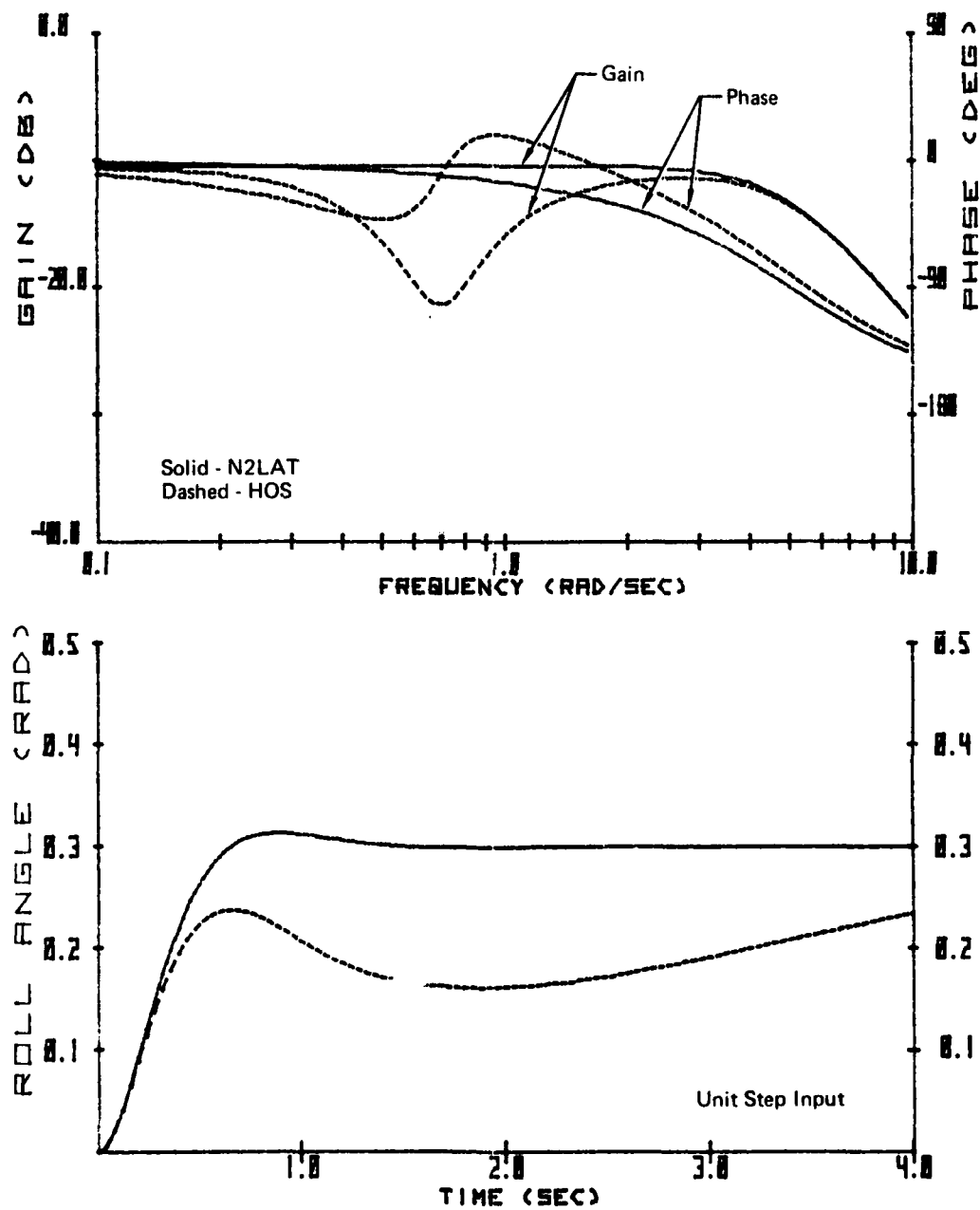
Figure A-51. Frequency and Time Response

NADC-79141-60

Config LF227

$\{\xi = 0.2; \omega_L = 0.7\} / \{\xi = 0.7; \omega_L = 0.7\}$

PR: 6, -, -, -

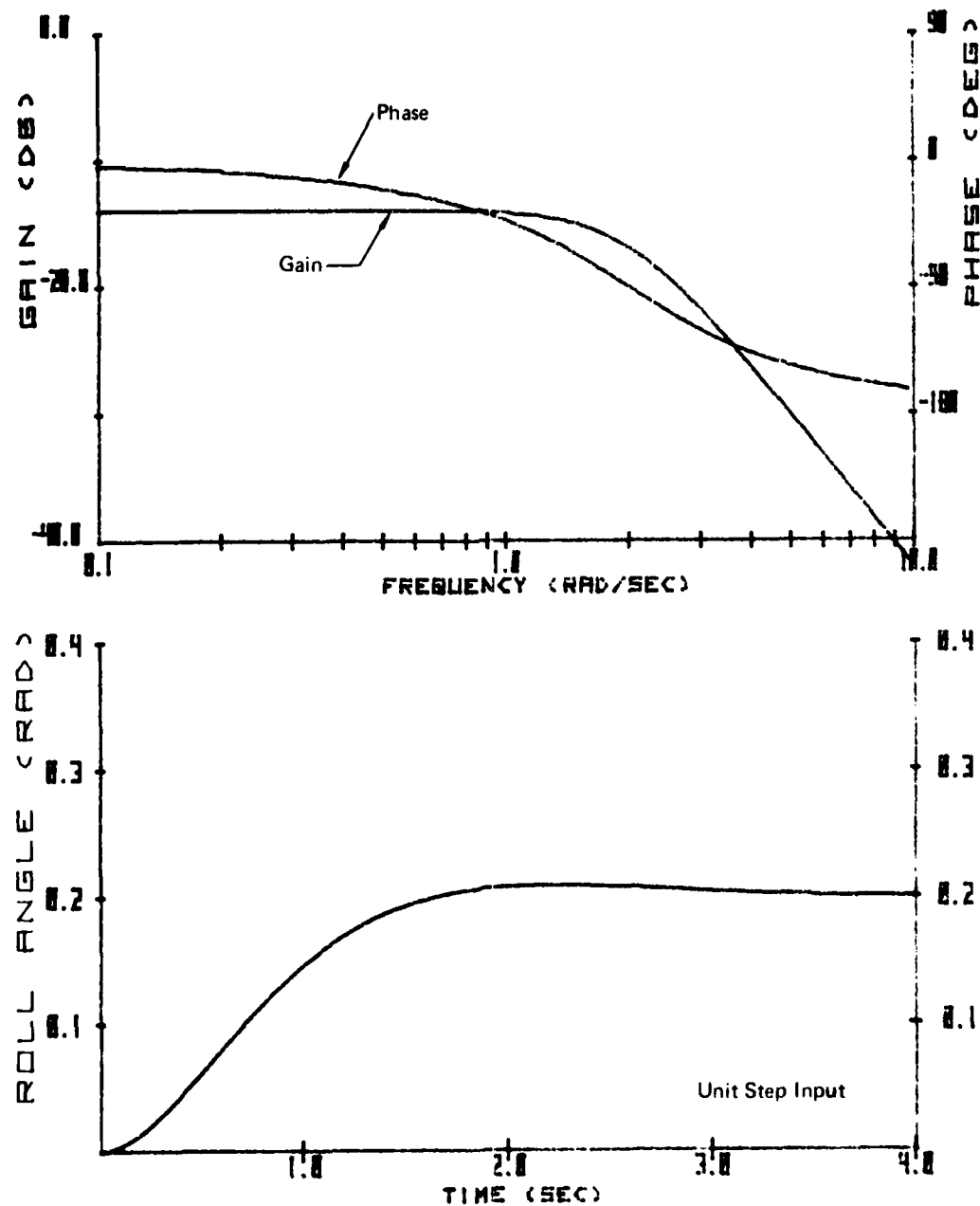


GP03-0200-06

Figure A-52. Frequency and Time Response

NADC-79141-60

Config G120
 $K = 0.2 \quad \tau = 0$
 PR: 7, -, -, -

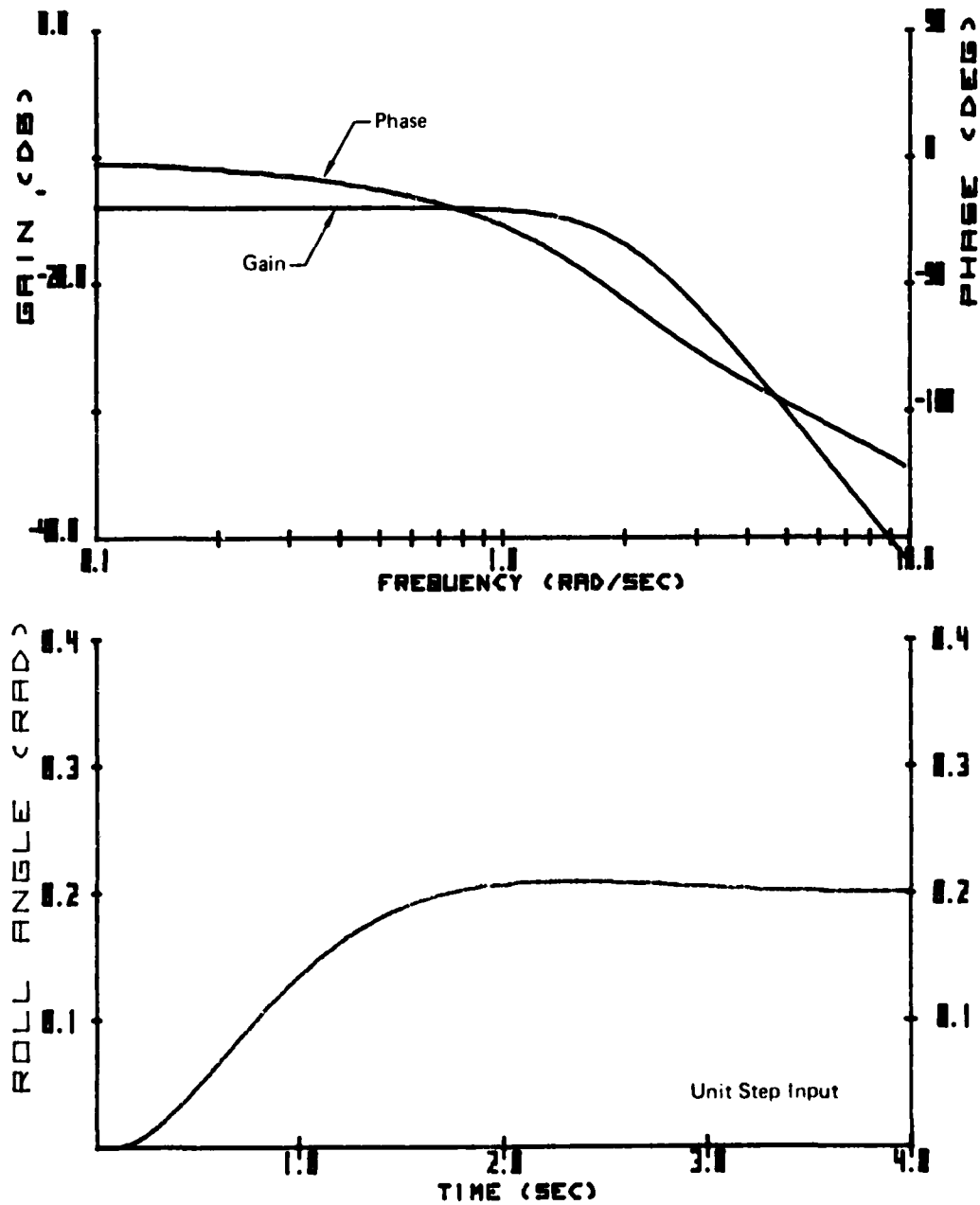


GP03-0208-87

Figure A-53. Frequency and Time Response

NADC-79141-60

Config G121
 $K = 0.2$ $\tau = 0.1$
PR: 7, -, -, -

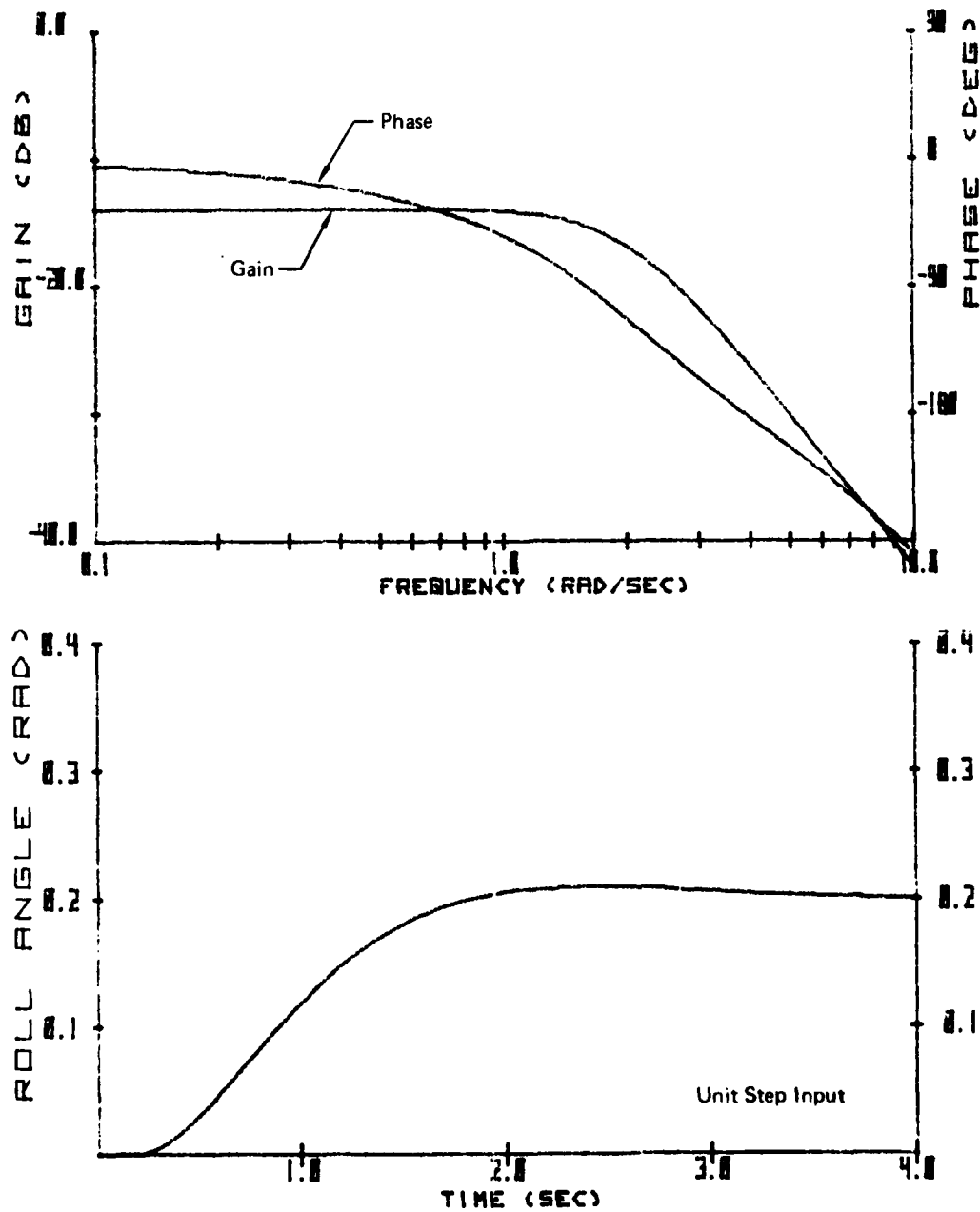


GP03-0208-00

Figure A-54. Frequency and Time Response

NADC-79141-60

Config G122
 $K = 0.2$ $\tau = 0.2$
PR: 6, 7, -, -

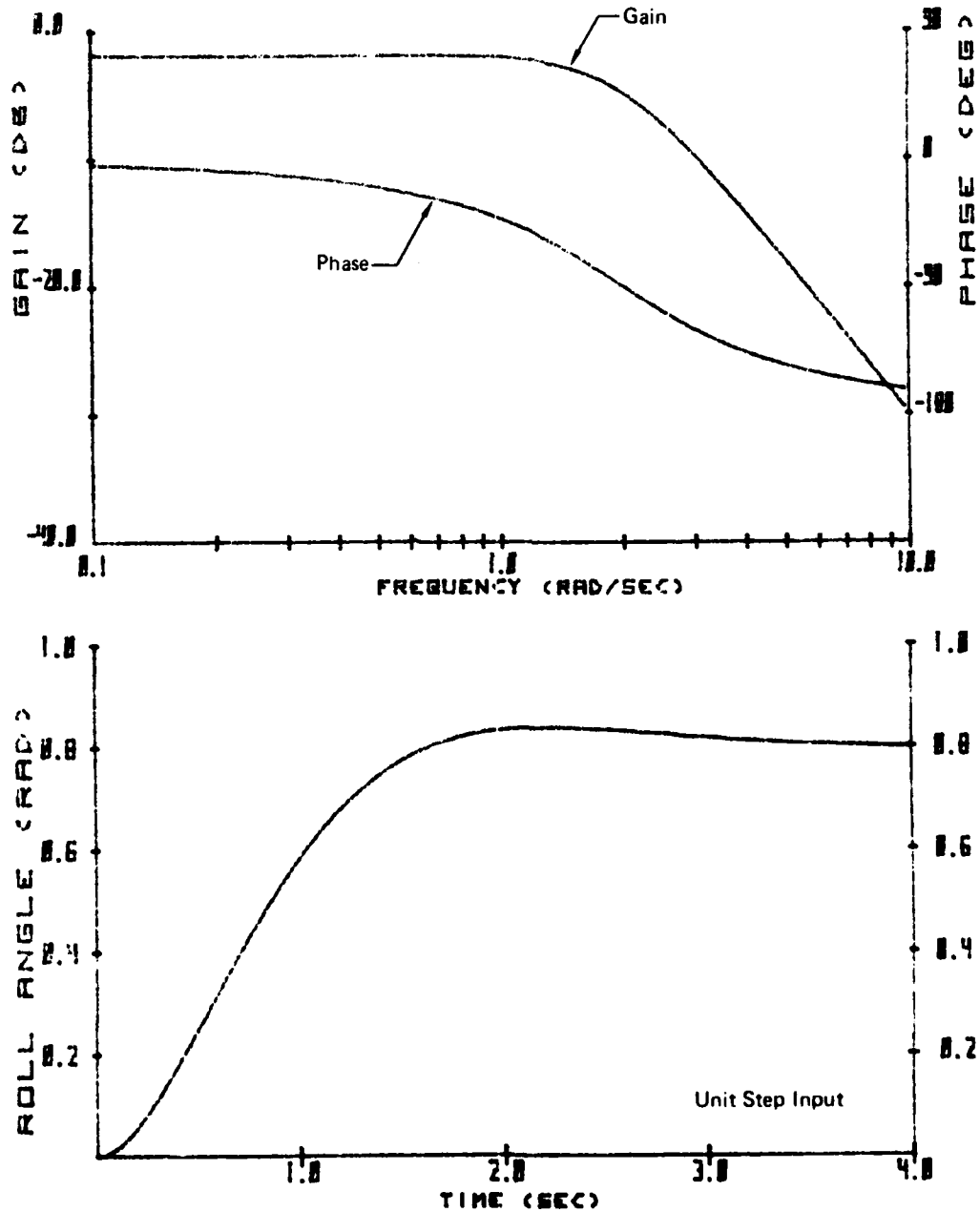


GP03-0208-00

Figure A-55. Frequency and Time Response

NADC-79141-60

Config G180
K = 0.8 $\tau = 0$
PR: 3, -, -, -

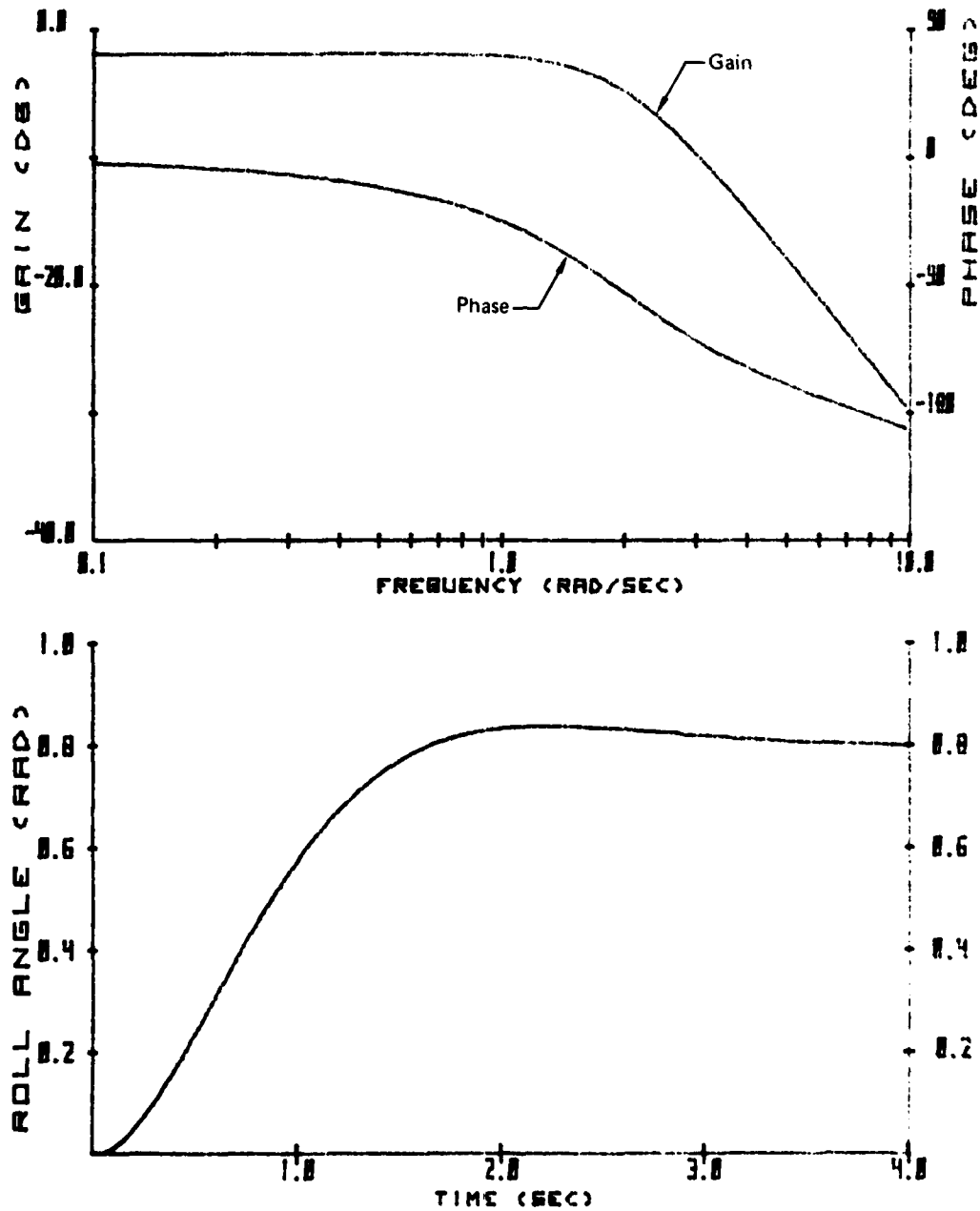


GP03-0208-00

Figure A-56. Frequency and Time Response

NADC-79141-60

Config G185
 $K = 0.8$ $\tau = 0.05$
PR: 4, -, -, -

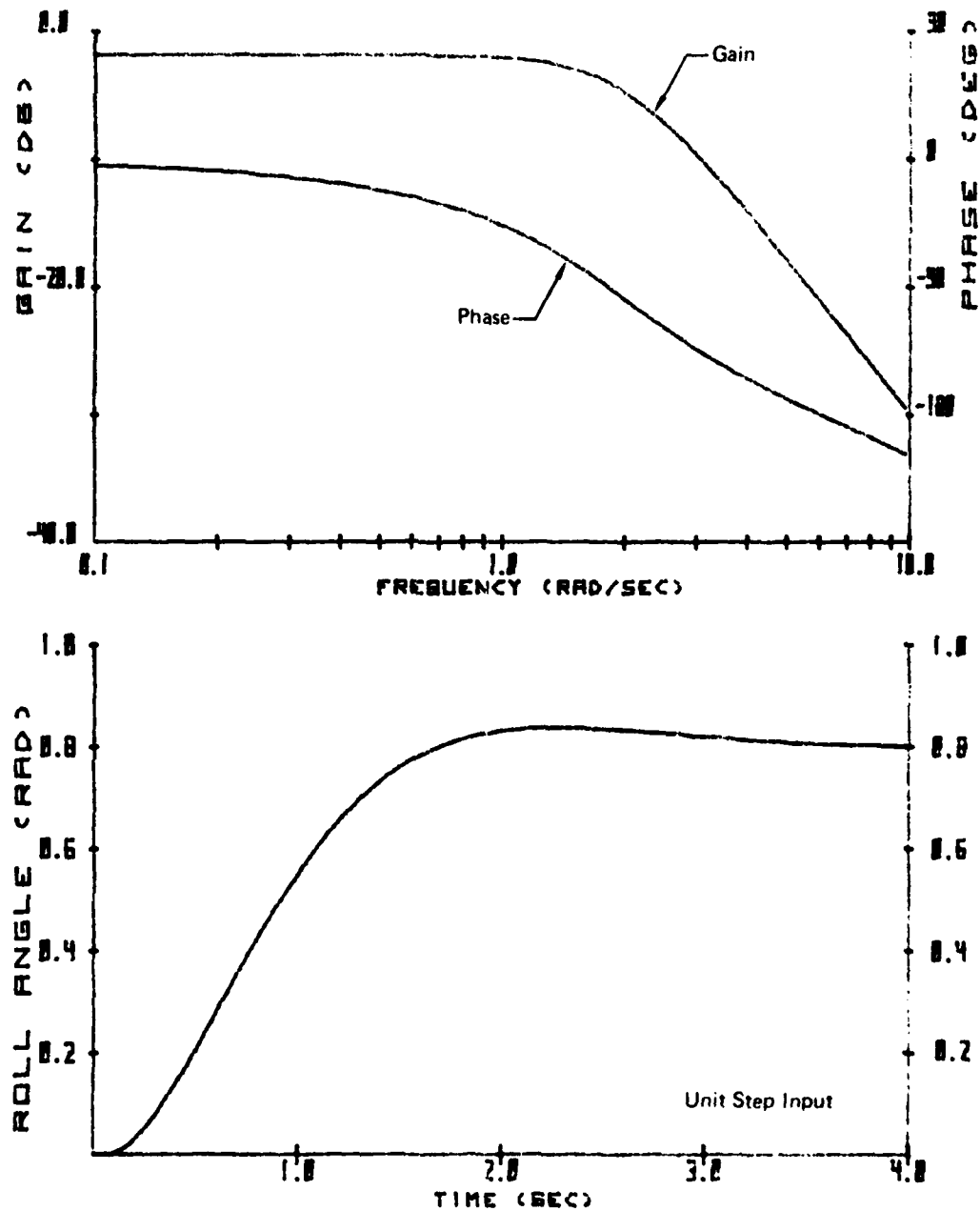


GP03-0200-01

Figure A-57. Frequency and Time Response

NADC-79141-60

Config G188
 $K = 0.8$ $\tau = 0.08$
PR: 2, -, -, 2

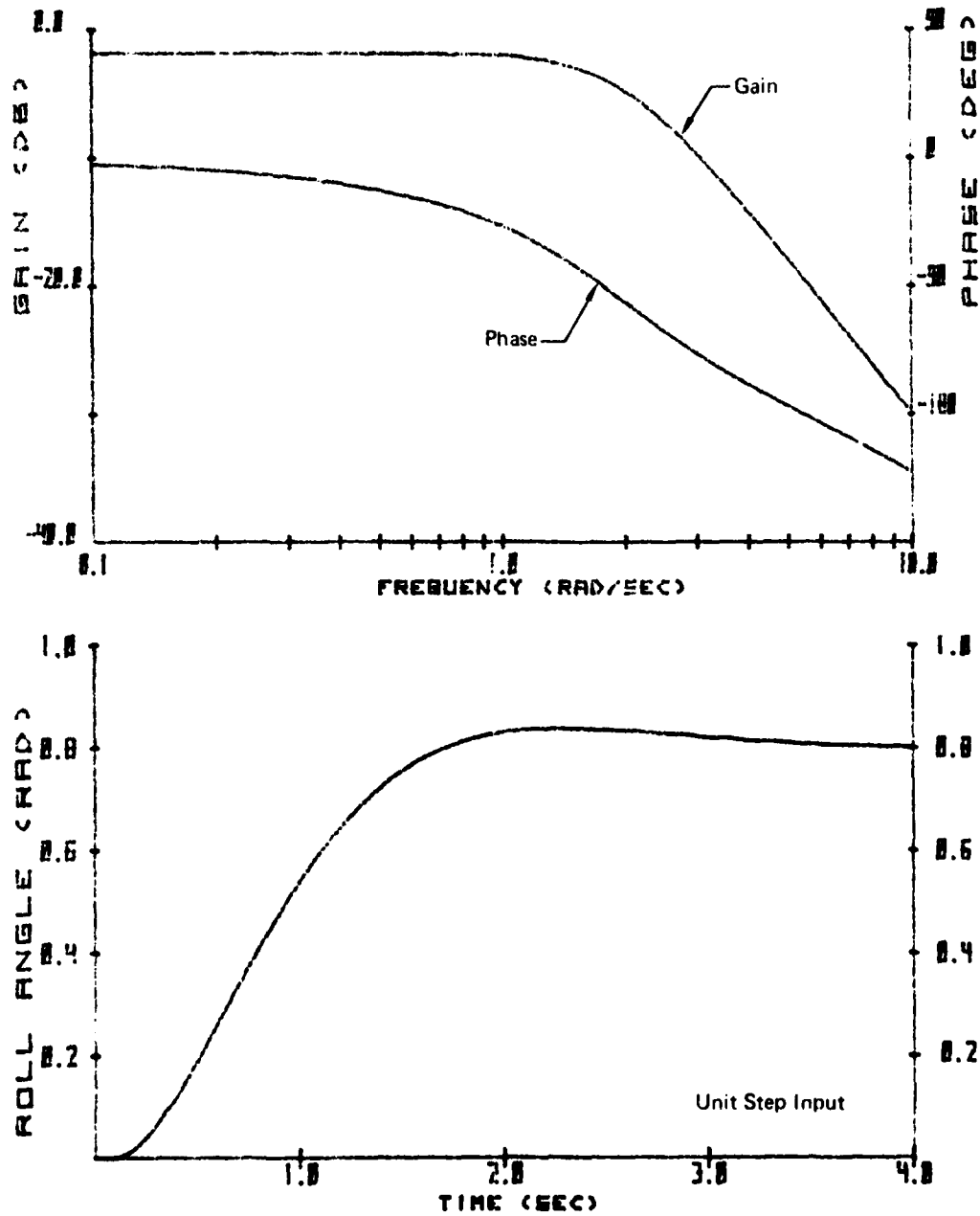


GP03-0200-02

Figure A-58. Frequency and Time Response

NADC-79141-60

Config G181
 $K = 0.8$ $\tau = 0.1$
PR: 5.5, -, -, -

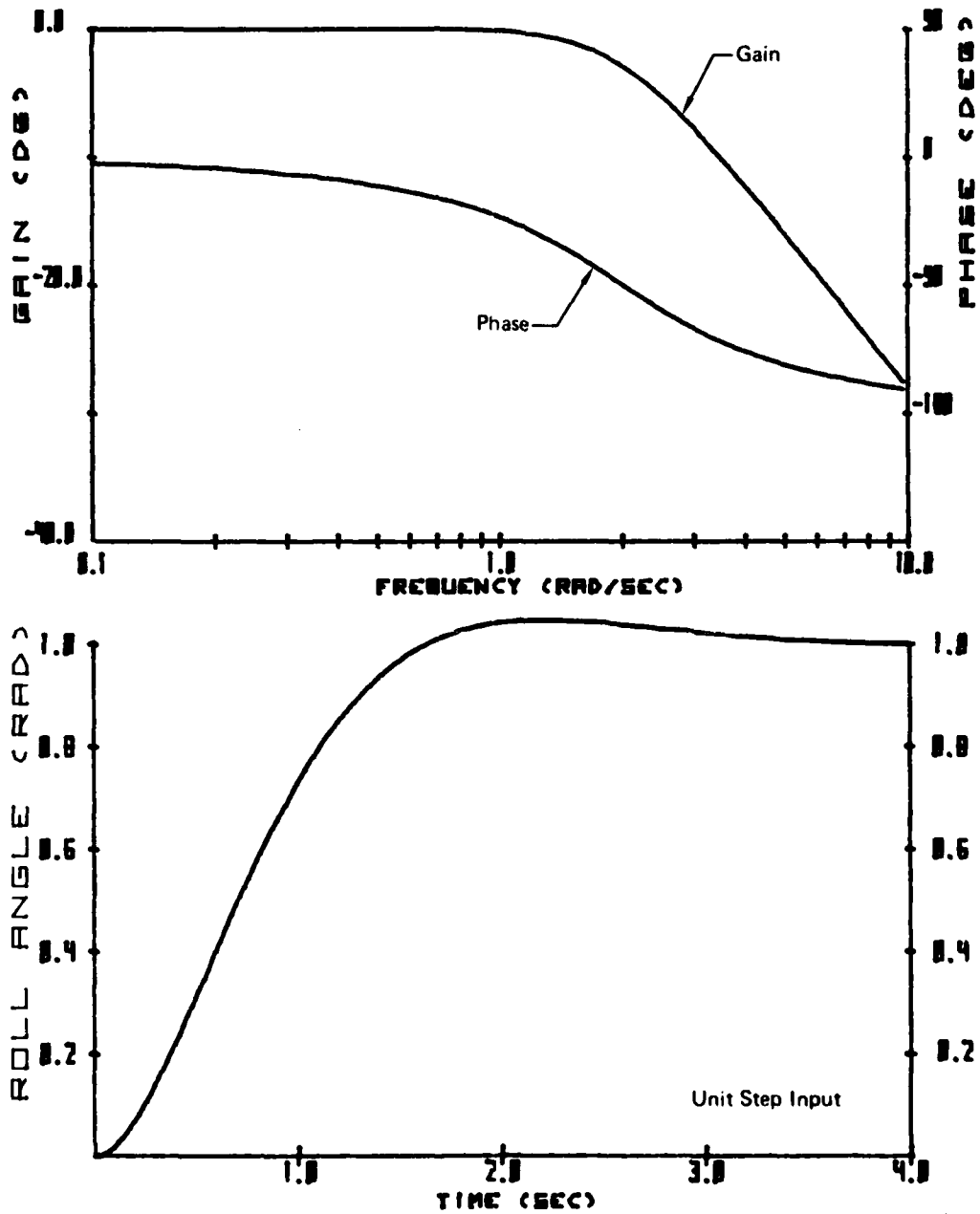


GP03-0200-03

Figure A-59. Frequency and Time Response

NADC-79141-60

Config G110
 $K = 1.0$ $\tau = 0$
PR: 2.5, -, -, -



GP03-0206-94

Figure A-60. Frequency and Time Response

NADC-79141-60

Config G111
 $K = 1.0$ $\tau = 0.1$
PR: 6, -, -, -

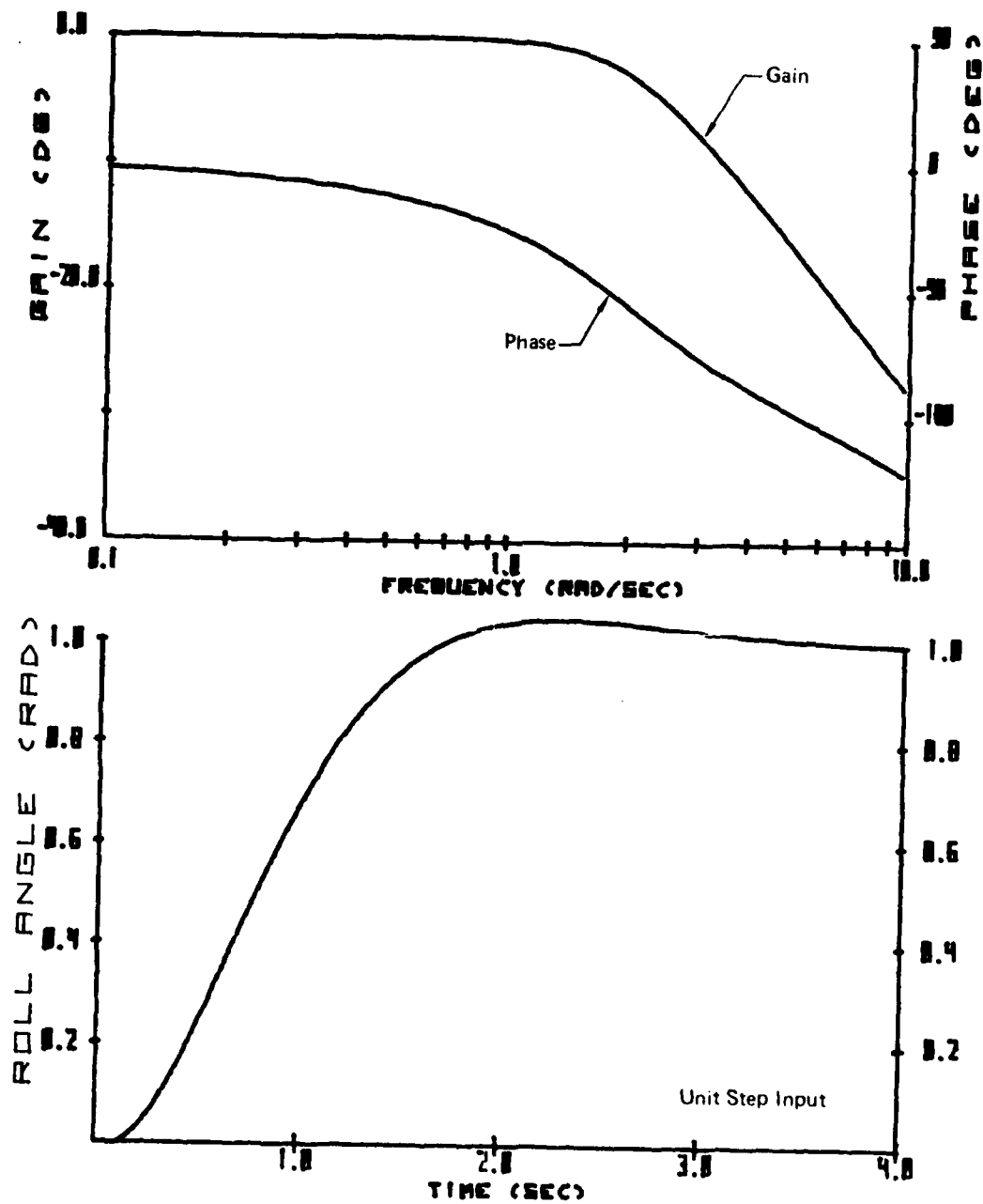
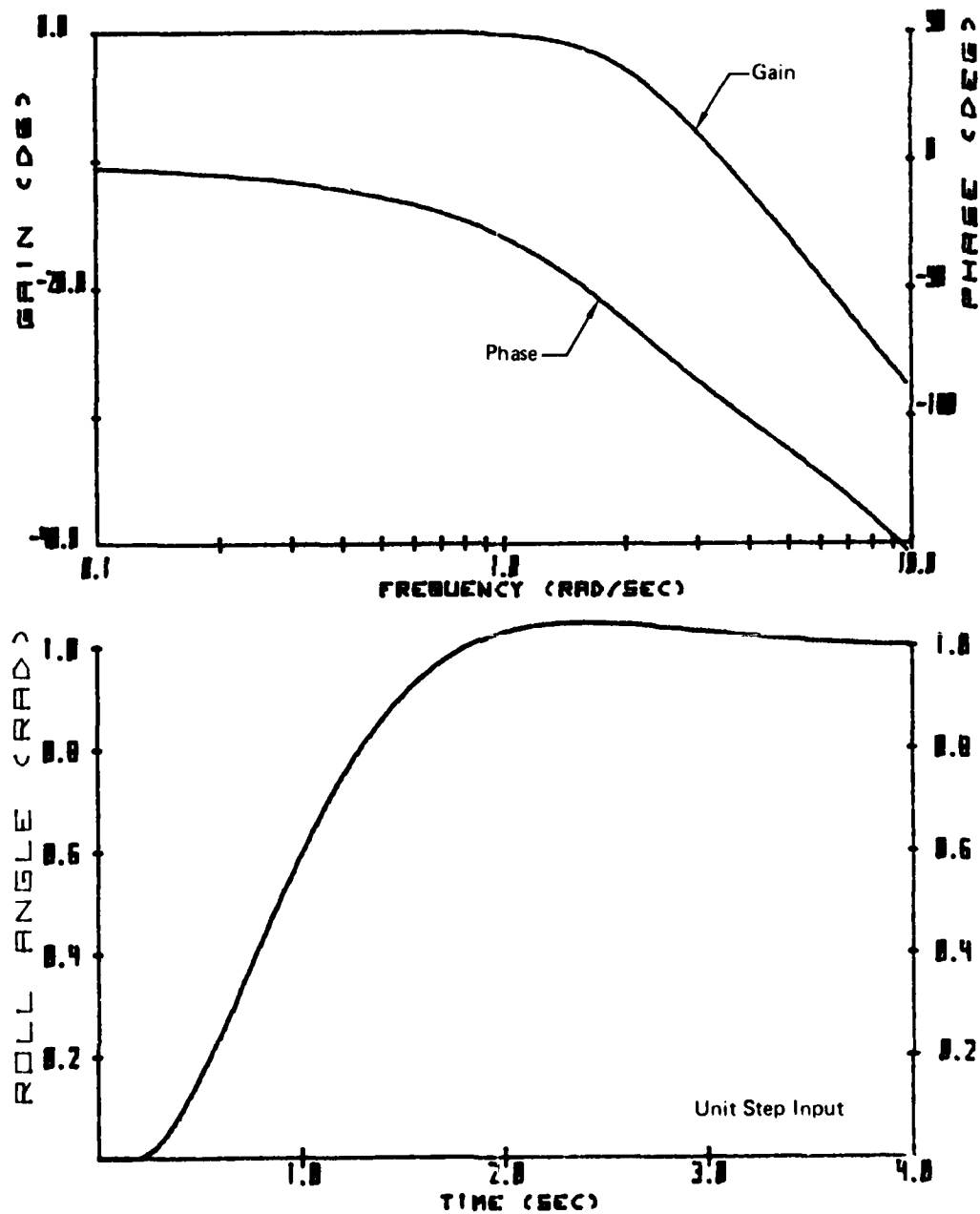


Figure A-61. Frequency and Time Response

GP03-0208-95

NADC-79141-60

Config G112
 $K = 1.0$ $\tau = 0.2$
PR: 7.8, 6, -, -

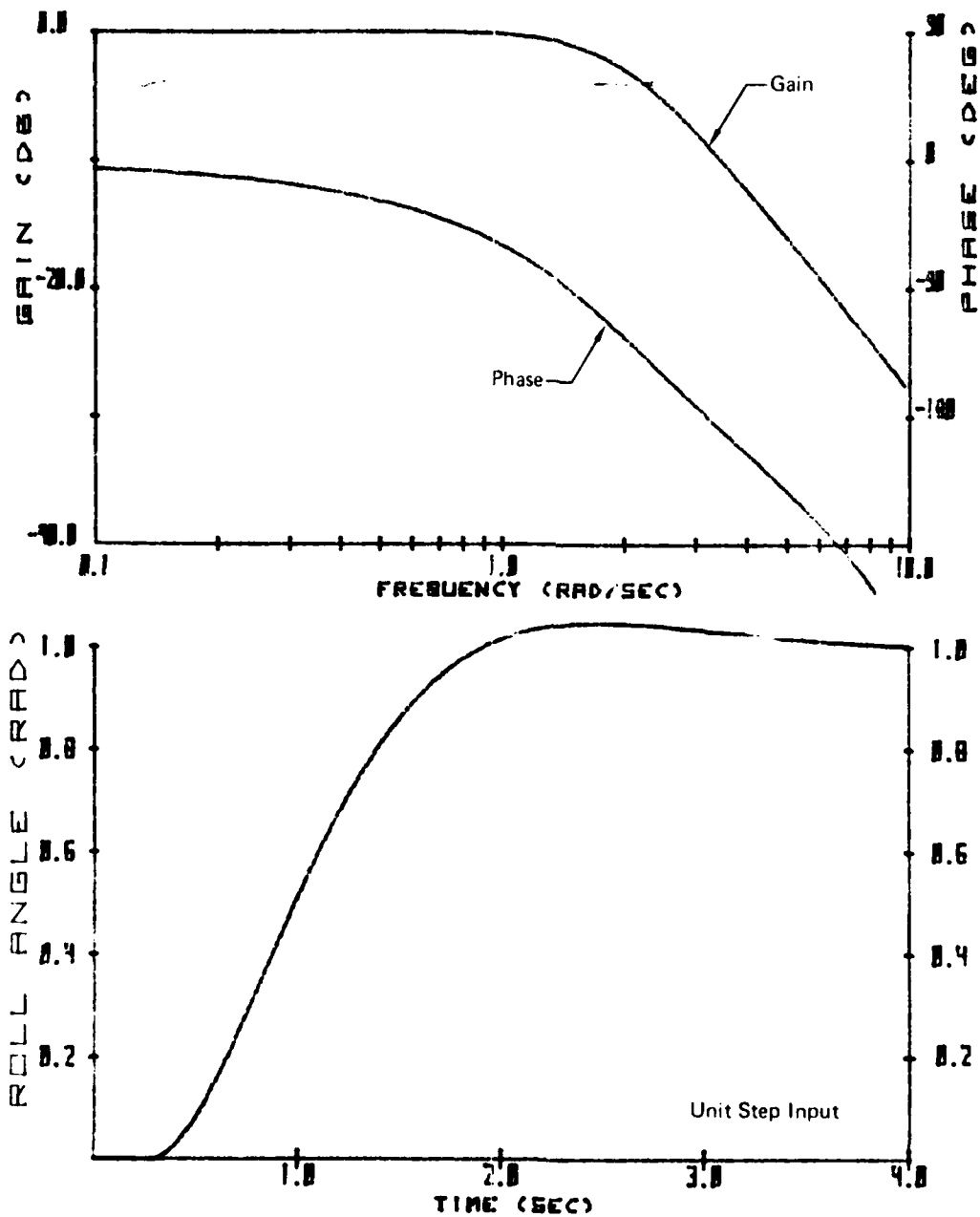


GP03-0208-96

Figure A-62. Frequency and Time Response

NADC-79141-60

Config G113
 $K = 1.0$ $\tau = 0.3$
PR: 7, 10, -, -



GP03-0208-97

Figure A-63. Frequency and Time Response

APPENDIX B

Pilot comments presented in this Appendix are shown essentially verbatim. Only minor editorial changes have been made.

Pilot C's comments and ratings in a few instances are colored by his experience with a rate system. The attitude system appeared unfamiliar.

Pilot D had extensive experience with in-flight simulation, however time did not permit a lengthy familiarization with the ground-based equipment. This makes his ratings and certainly his comments particularly interesting, however, when his ratings differ substantially from the mean, this should be borne in mind.

Finally, it is evident from the comments that the side gust was very severe and tended to reduce the number of Level 1 ratings in the experiment. This bias was considered a worthwhile price to pay for the demanding task needed to expose flying qualities problems.

The configurations denoted with an asterisk (*) are the exaggerated "rooftop" systems.

NILAT

- Pilot D: The hover itself, once I did get settled down, I could
4 stabilize reasonably well, so that as far as ratings
(K = .6) are concerned, I think the airplane's clearly control-
 lable. Is adequate performance attainable? I am a
 little bit doubtful about that.... I think that I
 could get the job done, but I wasn't really happy with
 it. My dominant feeling was that I was surprised at
 my inability to stop the airplane laterally where I
 wanted it.
- Pilot B: It's quite sensitive laterally. It feels very similar
4.5 to an AV-8A with the SAS on. It's no big problem.
(K = .6) Forces very light.... you've got to compensate quite a
 bit laterally.
- Pilot D: Initial response was okay.... I tended to over-control
7 and there was a mild tendency to PIO in trying to be
(K = .6) precise in coming to a hover laterally. The path
 response was initially okay.... I couldn't really get
 the job done to my satisfaction and I think it has
 major deficiencies. I don't really think that control-
 lability was a problem.
- Pilot D: General comments, I thought I could do a pretty
4 reasonable job. It certainly was controllable. I
(K = .6) thought I could get the job done whether it's satis-
 factory without improvement, I will hold out and say
 that I really still would like to be able to do the
 job a little bit more precisely than I could. So, I
 would say it's not satisfactory. I had just a slight
 tendency to not be able to do exactly what I wanted
 and when I wanted to do it with the bank angle. When
 I come to the end of the task getting hit with the
 gust and it takes awhile to get it settled down. Once
 I got it settled down, I could hold it reasonably
 precisely. I could fly the airplane precisely in
 attitude. The flight path response, I had problems
 stabilizing in the face of the gust in terms of hold-
 ing a position. Once I fought my way through the
 gust, I could get back where I wanted. Again, I
 noted the attitude, perhaps I ideally would like less
 attitude for the velocities I've got. If I just had
 to sit there, out of the presence of gust and so on,
 the airplane would be satisfactory and a 3.

NILAT

Pilot D:
3
(K = .3)

The airplane is controllable. I could do the job. I had a little trouble contending with this wind gust and in some respects it's not maybe a fair task, but I do think the airplane was, I had a feeling of confidence about the airplane and I haven't had on some, I'd say it's satisfactory. I could get the job done. Mildly unpleasant characteristics. I could control the airplane very well out of the presence of the gust. I got the gust like on the left edge of the runway and I scooted right across to the right quite rapidly, more rapidly than I had before and I was able to bring the airplane to a stop within reasonable distance of the line with a fairly aggressive input... I really don't know how to judge my capability to contend with the lateral upsets. It's a fairly severe upset. The attitude response, it felt like a well tuned airplane in the sense that I felt like I could fly one to one with it, so it was okay in the attitude. Path response, I can't perfectly stop where I want, but I did as good a job as I've done all day here.

Pilot B: The lateral is very comfortable. That's obviously
 3.5 a level deck command when I release it, it rolls
(K = .3) wings level, no problem holding it in the bank angle
 and although I never tried full control, I found it
 very comfortable.

Pilot B: I get the feeling that it just is not responding quite
5 fast enough. There's enough of a lag that I'm bothered
(K = .3) by them. I'm sitting there waiting, I need more
response to it. I called for more bank angle and it
seems to take a little bit longer than I think it
should.

Pilot B: 3.5 (K = .6) I'm sure that the ride qualities might feel a little bit crisp, a little bit sharp when you roll it, but it certainly is a lot easier to handle and it follows, does more like what I'm looking for.

Pilot B: It's a little less roll rate response than I would
3.5 like to see, but at the same time, I found it very
(K = .45) smooth and easy to control.

Pilot A: I'd say it's a little bit sluggish taking off. Seems
4 to be a little bit behind me. I don't know if
(K = .45) the gains down or you got a delay in it. I'm not real
wild about it.

NILAT

Pilot A: Seemed to be slower to react as opposed to the previous
 4 one. It's not a gain difference, because I'm putting
 (K = .45) the stick over, I get plenty of bank and it takes a
 while to get in there. The build-up in bank angle is
 not rapid. It's not real rapid, so it takes time to
 get to the bank angle I'm commanding and I can't sort
 out if it's a lag combined with a slow system, or just
 a slow system. I can get chasing cause I can leave it
 in too long and then have to over correct when I take
 it out, so I've got to compensate for it. All told,
 it's not too bad. I would say that it's got an
 annoying deficiency certainly.

Pilot C: In the gust, it doesn't respond too awfully well. I
 7 got the opinion that I was pushing, I made an input,
 (K = .45) I started to get something and in response to that
 input and then it would die off and then I would have
 to make another input and then I would get a lot of
 it. Sort of a stair step if you will, it wasn't a
 smooth gradient. As far as a rating, it seems sensi-
 tive enough at first, but it wouldn't fall out. Gust
 response was very poor.

Pilot C: There's something that's a little perplexing to me on
 6 this one. At first, I thought I was lightly damped
 (K = .45) and then because when I was on the stick, I put some-
 thing in and it would just continue to respond;
 however, when I got out of the loop a couple of times,
 it was fine.

Pilot A: What I'm seeing comes across to me as a lag in the
 4 response. That could be just a very slow rate
 (K = .45) build-up. It follows my commands going in pretty
 good. I notice it most when I try and take the
 command out and it takes awhile for the wings to get
 back level and therefore, I wind up overshooting and
 having to correct and come back. I don't know if it's
 lags or sluggish response or something like that, but
 it's coming across to me sort of sluggish, so I have
 to work harder than I think I should. It requires
 moderate compensation, I wouldn't say it's consider-
 able. I might have some problems if I got down to a
 low altitude. It's something you just have to try and
 stay a little bit ahead of, so you do have to
 compensate for the airplane.

N1LAT

Pilot A: Response seems down a little bit. I don't know if
 4 it's a matter of gain or rapidity. I guess I would
 (K = .45) like it either to be a little bit faster, or a little
 bit more sensitive as far as stick displacement. So,
 I usually wind up having to put in a correction and
 put in a little bit more than I originally put in.
 So, it takes me longer to damp out of oscillation. It
 takes me longer to get to where I want to go. I think
 it's something you could get used to, but it just
 comes across to me as being a little slow to answer
 the helm if you know what I mean. So, I guess I have
 to go back to saying that as far as I'm concerned, an
 annoying deficiency that I can't really put my finger
 on.

Pilot B: Slight lag in trying to get back to neutral, but other
 4 than that, not bad at all.
 (K = .45)

Pilot B: It would be a 3, if it was slightly more response.
 3.5 A little bit faster response, but other than that,
 (K = .45) it's nice and comfortable.

Pilot B: Well, it's pretty good up until you start pushing out
 3.5 very far and then it stiffens up.
 (K = .45)

Pilot A: I'm having some problems right around neutral. I just
 3 really can't find the neutral position. I don't know
 (K = .45) if it's weak centering, no breakout or what. I got to
 keep hunting to get that stick right in the center, so
 therefore, I'm constantly giving small lateral inputs
 and I think it's the feel system more than the dynam-
 ics. The airplane is going where I point it. I'm
 just having trouble feeling where the neutral point is
 on the stick and I sort of got to keep chasing the
 wing level position a little bit. Sensitivity is
 good, response is good and adequate, appropriate for
 the task. I have no problem making two axis correc-
 tions, I'm just having a little trouble in general
 finding the neutral point laterally. So, that gives
 me a small tendency for small oscillation in there
 that I don't think has anything to do with the dynam-
 ics. It's more having to do with the feel system.
 There is something in there that is annoying me. It's
 mildly unpleasant.

N1LAT

Pilot A: I would say I like the sensitivity better. I could
3 use a shade more response. I had no difficulty con-
(K = .45) trolling the airplane. The airplane certainly goes
where I point it. I have no major difficulty with the
airplane and I don't think I would get into difficulty
with it under any operation, so minimal pilot compensa-
tion is required.

Pilot A: Interesting. Sensitivity as far as stick gain goes is
3 good. Precision is good in so far as I see no
(K = .45) oscillatory tendencies, no secondary response tenden-
cies to roll back. There seems to be a little bit of
lag in there. It is no more than a nuisance. I could
get down fairly low there, so I did it intentionally
on that second run. It's a minor annoyance category.
I can make the airplane do almost exactly what I want
it to do. It just takes a fraction of a second longer
to get there than I think it should. So, it's got
some mildly unpleasant deficiencies. I don't really
have any major objections to the run.

Pilot A: I'm satisfied with this one.
2
(K = .45)

Pilot B: I don't see any big problem with that. I found it
3 very easy to do.
(K = .45)

Pilot A: The harmony and sensitivity is good. Perceived no
3 large or unusual problems. I've got an altitude
(K = .45) problem trying to split the difference when shown in
discrete ten foot intervals, so it will be a little
choppy on the altitude control.

Pilot A: I guess I finally got this doped out. There's no
3 problem with the lateral controllability in isolation.
(K = .45) However, compared to the longitudinal sensitivity, it
seems to me that lateral sensitivity is down just a
shade, therefore, there is a minor harmony problem. I
think if you made a longitudinal adjustment here, I'd
have to give it a Cooper-Harper 2. As it is, I'd say
the harmonization bothers me just a little bit.

N1LAT

Pilot A: No problems at all. Sensivity is good; no delays.
 3
 (K = .45)

Pilot A: I don't perceive any additional mode in the mid-frequency range. It's predictable. Sensitivity is pretty good. I might wish I had just a shade more response; however, I've got no gripes at all about the configuration.

Pilot A: On the first run, I seemed to get almost in a continual $\pm 20^\circ$ of bank oscillation. However, the two subsequent runs, I can't really perceive any real problem with it. The airplane is slightly sluggish and it may be caused by a bit of a delay; however, sensitivity is good and appropriate to the task. I guess as long as I fly the airplane properly, I can make it do pretty much what I want to do with it. I guess I wish I was just a little bit more rapid in response. I can make it go where I want it to with moderate pilot compensation.

Pilot A: I like that configuration. Sensitivity is good. Predictability is excellent. The only problem is I guess I wish the onset rate was a little faster. In other words, it comes across just slightly on the sluggish side. However, you can certainly make exactly what you want. I'd be tempted to give it a 2, except for the comment on sluggishness.

Pilot A: The airplane does what I want it to. What more can I say.
 3
 (K = .45)

Pilot A: The only problem with the configuration at all is it is just a shade slow on the response. Not bad at all. Definitely Level 1, the choice should be between a Cooper-Harper 2 and Cooper-Harper 3, but since I think I would like the response to come on just a little bit faster, I would say I am compensating for it so, therefore, I've got to put some small compensation in it.

Pilot A: We're back up to a Level 1 airplane. I can't really put my finger on anything that I would change. It's got very good flight characteristics, good sensitivity, good response, negligible deficiencies.

NLLAT

Pilot A: It seems like a very nice system. Sensitivity is
2 good. Control harmony is good. Control force is good.
(K = .45) Response is good. No noticeable lags. No sluggish-
ness. It's a very pleasant system to fly.

Pilot A: No controllability problems. The problem with it is,
5 the rate of onset is a little bit slow and therefore,
(K = .45) it takes a long time to get a correction in, which
 $Y_v = -.2$ means that by the time you sense that you need it and
put it in and the airplane reacts, you need more and
you can't station and keep exactly to that shear, so I
can't get the desired performance. It's certainly
adequate.

Pilot A: That's almost Level 1. The problem is that the onset
4 rate is just a little down, so the airplane comes
(K = .45) across as being a shade more sluggish than you would
 $Y_v = -.2$ really like. It might be real decent in flight, con-
sidering the ride quality, so a flight article might
be better. As far as the simulation goes and the
ability to make small corrections, I have to work
harder than I think I should.

HF111

Pilot A: Response is way down. It's certainly adequate for a
 7 DC-10 or B-52 (large aircraft). It's inadequate and
 (K = .45) inappropriate in a fighter sized airplane. So, I
 Y_v = -.2 cannot get desired performance, I cannot get adequate
 performance, so I'll have to say that adequate perform-
 ance is not obtainable with maximum tolerable pilot
 compensation, it's just not there. I've got no
 question about the control, controllability of the
 platform. You don't have enough to get in trouble
 with.

Pilot A: The airplane is just too sluggish, plus the response
 9 is down. Controllability is very definitely in
 (K = .45) question. I was in a continual bank to bank oscilla-
 Y_v = -.2 tion that I could not get out of. It was just like
 being on the end of a pendulum. There's no way I
 could have landed that machine. I question that I
 ever really had adequate control of it in the first
 place.

Pilot A: The airplane is just too sluggish. Definitely a Level
 7 3. I can't even get adequate performance. It just
 (K = .45) takes too long to get anything done and I do have some
 Y_v = -.2 qualms about control. With a differently defined
 task, there may be a controllability problem in that
 you could develop a large bank angle in close to the
 ground for instance, and just not be able to get it
 out in time. So, for the way we've got the task set
 up, and for what we're doing here, I'd have to say
 you're not bordering on loss of control. In a close
 confines environment or things like that, I think
 things could get pretty hairy in a hurry.

Pilot A: The problem here is a very, very sluggish response.
 7 Again, absolutely no question of being able to make
 (K = .45) small corrections. They're just not there. The
 question is again, can I even get adequate performance
 out of the configuration, added to a slight hedge on
 possible controllability. I'm getting into that
 factor being able to generate a fairly large bank
 angle and not be able to get rid of it in time, so I'm
 still back in that 6, 7, 8 ballpark. I don't think I
 can get what I would consider adequate performance out
 of the machine. It just isn't there. I wasn't really
 having a controllability problem, although I was oscil-
 lating from one side of the runway to the other and
 from +20/30° of Mag. For this task controllability
 wasn't a question. If you got a precision low
 altitude task, it might be.

HF112

Pilot A: The airplane is too sluggish. With a low response,
 8
 (K = .45) because you don't have enough to get into trouble.
 $Y_v = -.2$ What we have is the rate is too low. In that case,
 you can get into trouble because you can generate a
 very large bank angle and not be able to get it out in
 a hurry, which means that you're all the way over to
 the other side. You couple that with a little bit of
 lag in response and you've got a disaster. I think
 the pilot does have to stay on top of it in order to
 retain control and there's not even a question of
 being able to do any station keeping within a
 configuration.

Pilot A: Well now, response is very, very, very sluggish. It's
 6
 (K = .45) like flying a heavy. It might be typical of what you
 $Y_v = -.2$ could get into with some total configurations, however,
 compared to what we've been seeing as typical in this
 simulation, that is a very sluggish response. I found
 myself in almost continual bank to bank oscillation of
 about 20°. I never got real close to the ground, but
 I suspect in a close to the ground situation, with
 something upsetting you initially, it might be a
 little bit of a wild ride in there. I guess I'll say
 as far as I'm concerned, it's a very objectionable
 deficiency in that the sluggishness, I can get
 adequate performance, but because of the slowness, I
 certainly can't get the desired performance.

Pilot A: It might be an interesting configuration with a little
 6
 (K = .45) bit more time delay in it. As it is, the airplane is
 $Y_v = -.2$ just too sluggish. It's got very high sensitivity
 combined with a sluggish airframe. You got plenty of
 bank angle, it just takes a hell of a long time to get
 it. What that means is there is no such thing as a
 small correction, because by the time you get the bank
 into a small correction, you need a bigger one and by
 the time you get that in, you know a large one, so
 it's a process of continual fairly large amplitude
 corrections and the airplane is always way behind. I
 can't get the desired performance. I can barely get
 adequate performance. There is no question about
 control at all. I am getting adequate performance.

Pilot A: Moderately sluggish response, maybe some lag in there.
 5
 (K = .45) Again, I can't make the small corrections I would
 prefer to make, but I can get the corrections in, in a
 decent amount of time. I'm getting adequate
 performance.

HF113

Pilot A: I'm not quite sure what you got in this configuration
4 on that lateral control. It feels a little bit loose,
(K = .45) almost like there is a couple rates involved in the
Y_v = -.2 bank angle onset. I can control it and I don't have
any real problem with the lag. It seems to follow the
stick fairly precisely. I guess I wish I had a little
bit more response to small inputs, but I don't have
the problems of a constant bank to bank oscillation.
I feel I can get the job done. It's got some annoying
deficiencies.

Pilot A: In the process of keeping good altitude control on
3 these runs, I was very smooth and cautious on my
(K = .45) input, so I don't want any of the cosine effect on
Y_v = -.2 bank angle. Therefore, I can't really give you a good
evaluation on large scale maneuvers, I didn't make
any. The airplane responded well to what I was asking
it to do. I was getting pretty much what I asked for.

Pilot A: It's an almost good configuration. The problem here
5 is the airplane is sluggish. It's predictable, it
(K = .45) just takes a little bit too long to get in there and
Y_v = -.2 if you happen to make a mistake, it takes a long time
to correct for it, because you have to go the other
way and the airplane has to build-up rate and every-
thing, so the sensitivity seems good. I don't notice
any particular lags in it, although response is just
slow, so I guess I'll say it's a moderately
objectionable deficiency.

Pilot A: The airplane is just too sluggish. You know what
6 happens when you need a correction as it takes a long
(K = .45) time to build. Therefore, you need a bigger correc-
Y_v = -.2 tion and you get it in, you get everything stopped -
then you've got to take it out and by the time you
take it out, you're going the other way. So, you've
got to over correct and you get into an oscillation, a
real nuisance. A major problem with it. However, I
can get the adequate performance. I'm just not real
wild about it. Very objectionable, but tolerable
deficiencies.

HF113

Pilot A: Very sluggish. I don't know if it's sensitivity,
6 change in the lag or whatever. Although the configura-
(K = .45) tion is sluggish, I can get corrections in more
rapidly. I do have a tendency to get a constant sus-
tained low amplitude wing walk, but I can stop the
drift and I can get reasonable performance. There's
no question of being able to make small corrections.
It's just not there. But I think I can get reasonably
adequate performance. I can stop the drift in other
words. I'll say it's got the very objectionable, but
probable deficiencies.

HF114

Pilot B: A little bit light laterally, other than that I'm
4 compensating only slightly.
(K = .6)

Pilot A: That was interesting. When I first saw it, I was about
5 to say it was a pretty pleasant configuration and I
(K = .45) got into a pretty wild lateral overshoot. It's
pleasant and I think the harmony seems good, I'm
getting about the response I think I should be out of
the stick. I don't know if there's lag, or it's
sluggish or what. I got behind it in a hurry on a
couple of occasions it seems like, so it's a little
puzzling. The dynamics seem quite good. It's dead-
beat. I put stick over, it answers with about the
response I think it should. I guess it just takes
awhile getting there. Without the wind, I'd have
probably said that was a very good configuration, but
when the wind hit me, it took me awhile to damp it
out. Puzzling. So, I can't get to the desired
performance. I can certainly get an adequate perfor-
mance, the difference is that I can't make it do
exactly what I want to but, I can almost get there.

Pilot A: I'm trying to decide if adequate performance is or is
6 not obtainable. It's coming across to me as sluggish.
(K = .45) I don't know if it's just flat sluggish or if there's
sluggish plus a delay or just a delay. I'm consider-
ably ahead of the airplane which means that I can't
get into this overdrive situation. Got some oscilla-
tions in there, which I don't think qualifies as PIO
because I could back out of it so easy. I don't like
the configuration. It is very imprecise. It's
certainly moderately objectionable. I can't get the
desired performance. I'm in the adequate performance
category.

HF115

Pilot B: I don't see any big difference from the last three
3.5 runs.
(K = .3)

Pilot C: Continual small PIO problems with that one. It is very
6 nice really except in one place and that's when the
(K = .45) pilot is in the loop for small corrections and then
the airplane, the wings just sit there and oscillate
up and down and then you take your hand off the stick
and they quit.

Pilot A: It seems like there are several things wrong. There's
5 just a bit of lag. There seems to be some kind of
(K = .45) oscillatory or second stage response in there. It
comes across as being unpredictable. I never quite
get what I think I'm going to get out of the stick and
it takes awhile to get it all, and as a consequence,
I'm making larger corrections than I really feel are
necessary, and more of them. So, as a consequence, I
can't get what I would consider to be the desired
performance. I can get adequate performance certainly
and it doesn't require an awful lot of effort to get
that. It's a quirk, it's a nuisance, it's not
predictible. It's moderately objectionable.

Pilot A: I seem to have lost some mid to higher frequency per-
4 formance. It's ignoring small inputs. I'm having a
(K = .45) little bit more trouble getting small corrections in,
Y_v = -.2 because it tends to ignore some of them. I can get
the job done and it's a nuisance more than anything
else. It's not a question of extensive pilot
compensation, yet it's an annoyance.

HF116

Pilot D:

5

(K = .6)

In general, the airplane was controllable. I think you could get the job done. I was partly influenced by my last wandering around and trying to settle down on the position on the last evaluation. I don't think it's satisfactory. I think it's a smooth airplane. There's a tendency to not be able to learn how to precisely predict where I'm gonna stop over the ground and I felt like I tended to not have the right match between bank angle and the resulting translation that I wanted. In any event, there is not serious problems compared to some of it I've seen, but it is not satisfactory, but I think that we're talking about achieving adequate performance as opposed to desirable performance, but I could eventually salvage something here. When I'm stabilized in the hover, although in the face of these gusts, the wind shears I did have some difficulty at the end. Attitude response seemed smooth and predictable to me. I felt comfortable. I cannot really solve the problem of how to smoothly stop. That's why I gave it the unsatisfactory rating. No tendency to really PIO. I was able to in the face of the wind shear, which just about the time I'd get enough bank angle in to correct for what is a fairly large wind and stop from moving to the left, and move back to the right then it disappears and I end up over controlling and translating too far to the right, but despite that, I was able to recover from fairly large bank angles quickly and with reasonable predictability. The flight path response, I said in the face of the gust from the last one in particular, I was moving around more than I wanted to. Somehow I think that I would like to use less attitude to get translation. The wind affect seemed rather severe. Turbulence, I can't say that I really noticed anything.

Pilot B:

4.5

(K = .45)

There's enough lag in there that it bothers me a little bit. It's not hard to use or anything of that sort, and it's nice and smooth and tends to follow the stick pretty well, but at the same time, there's some sort of lag there that I can't sort out, but I don't like it very much.

HF116

Pilot A: I'm seeing a perceptible lag in the response. The
5 underlying dynamics are good. They're pleasant.
(K = .45) Rate build-up is good. It's predictable. You got to
stay ahead of the airplane and plan what your gonna do
in advance more or less and not try and make any rapid
corrections. As long as you keep your bandwidth down,
it's not a particular problem. If you got into a real
high gain situation, close to the ground, I think
you'd have problems controlling it. I don't like the
lag in the response. I think that I'd get in trouble
with it, so I've got to give it considerable pilot
compensation by staying ahead of it.

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HF117

Pilot B: That's a lot better. I can make smoother inputs. I'm
4.5 still getting some of that bang, bang effect, but I find
(K = .3) it to follow what I'm asking it to do much, much
better.

HF124

Pilot B: As far as the overall airplane is concerned, nothing
6 really different except the lateral system. The
(K = .6) lateral damping is obviously considerably reduced. Adequate performance requires extensive pilot compensation and that's true laterally, the thing oscillates unless I really determine that I can get it into the center and stop the lateral oscillation. It's not in the 7 category because I can attain adequate performance. It's objectionable to tolerable.

Pilot B: The lags are too high and it's totally uncomfortable.
• 7.5
(K = .45)

Pilot A: I think I could get myself in a dangerous PIO in a high
6 gain situation. As it was, I never really got out of
(K = .45) the loop. I was in a small amplitude PIO throughout the whole thing. The lags noticeable and objectionable. I certainly can't get desired performance and I'm not totally sure I want to call it adequate. It's a reasonable probability in a slight higher gain task I might want to go worse than that.

HF125

Pilot D: Controllable, yes, it's controllable. I can't do the
7.5 job, I get into a fast high frequency over control PIO
(K = .6) type situation anytime I try to be precise with the
airplane, so it has major deficiencies. The attitude
response was initially quick, but it was not predict-
able. I could not stop from seemingly putting inadver-
tent input. Special techniques would be to try and
keep yourself consciously from being too active on the
controls. There was a tendency to PIO. The path
response was bothered because I got preoccupied with
trying to stabilize the airplane in attitude, so the
predictability suffers there. When I did get it trans-
lating it seemed to be the attitudes were reasonable
for the translational velocities I was getting. The
lateral disturbance wind shear or whatever it is,
really upsets the apple cart with this thing, because
you get it almost stabilized and then you get this
task to compensate for the wind and several times, I
ended up translating back and forth and that's very
uncomfortable to fly because the motions are very
rapid in the simulator and I find my eye balls getting
a little bit crossed with whatever is going on the
display with the very rapid movement.

Pilot B: I move the stick and then there is a delay. Nah,
6 that's no good. You've got to have positive response
(K = .3) right away. This thing isn't stopping when the stick
moves. Good Lord, it's half a second or so. Maybe
even a second, yeah it's closer to a second delay in
there. It's not all that hard to do, because it's
basically flying itself, but the lag is what's getting
to me and I could get myself disoriented very easily
if I didn't have really good cues. I'm compensating
for that lag by saying okay, I'm gonna have to move it
now, because a second from now I'm gonna see something
happen or 1/2 second to a second someplace in there.

Pilot A: The problem here comes across as a transport lag. The
5 thing to consider is a modest amount of time before
(K = .45) the airplane responds. Therefore, I've lost the
Y_v = -.2 ability to make small corrections. Therefore, I can't
get the desired performance. Now, adequate perform-
ance, yeah, I can certainly obtain that. The differ-
ence being I just can't make small corrections. The
question of compensation is almost removed. Nothing
you can do about it. The vehicle just doesn't have it
with that much lag, so in order to get what I consider
adequate performance takes some amount of work load,
there's nothing I can do by increasing my own work
load, my own compensation, to improve the performance
of the vehicle.

HF126

Pilot B: I kind of like it in a lot of ways. I can't quite nail
4 it down as tight as I might like to, or as tight as
(K = .45) some of those others, but in the absolute hover it's
much more comfortable in maneuvering areas.

Pilot A: It does have a noticeable lag. That one comes across
6 as having a noticeable lag in the response. Under-
(K = .45) lying dynamics almost seem like there is something
else in there. My major objection is it takes awhile
to get anything out of the aircraft and therefore, by
the time I sense the motion starting and put a correc-
tion in and the airplane reacts, I've got an over
correct. I put in more, a rate, lateral rate, has
built-up, then the same thing goes taking it out. I
get a little bit behind, so I get into this lateral
oscillation, not only in bank, but actual lateral
position, so it was sliding back and forth, so that
one's got objectionable deficiencies. I certainly
can't get the desired performance. If I really back
away from the task, I wouldn't have any PIO type
problems. I've got to do two things, one, I've got to
continually over-correct, and two, I've got to simul-
taneously back down on my expectations, so I'm gonna
have to say that I can get adequate performance with
considerable compensation.

Pilot B: A little longer lag here. It's really not much dif-
4 ferent than the last one other than the slight change
(K = .45) change in lag.

Pilot A: I can sit there and oscillate the stick back and forth
5 as much as is comfortable, like say two inches either
(K = .45) side of center, at what I don't consider to be an
unreasonable frequency and get absolutely no lateral
response. I've got good prompt performance. The
steady state gain is good. I've got all the control
out there that I want. It takes awhile to get there,
but it totally ignores small corrections, so I've got
all the gain I could possibly ask for as far as
getting this thing stood up on its wing tip, but I
have lots of trouble making small corrections and it
just doesn't respond to small inputs. So, I can get
adequate, I can't get the desired performance, cause I
can't make small corrections I want to, I can get get
adequate performance and it's really not too hard.

HF127

Pilot B: I'm flying all of these in more of a bang, bang
5.5 fashion than the smooth control input that I'd like
(K = .3) to be able to make. I'm just chopping in there with
the stick waiting for something to happen and then
banging it back out waiting for it to happen, rather
than smoothly flying it. I might just as well have a
button here and press it for left/right and release it
for back to wings level. It's just I don't care for
this at all. I don't like the way you have to fly the
airplane in order to get done what you need to do. It
needs to be a smoother, more continuous effect, rather
than this bang, bang effect which is what I find
myself doing and I don't like that.

Pilot A: You got a perceptible lag in the system. Underlying
7 dynamics are good. Rate build-up is okay. The gains
(K = .45) okay as far as bank angle per stick deflection or such
like things. The lag creates a problem in that you
start over-correcting. You put in what you think you
should and it's a little late then you need more in
and you put that in, then you gotta get it out, so I
think you could get into pretty much of a sustained
PIO, in a high gain task. I think close to the
ground, that would definitely be Level 3. For the
task I'm doing up here, I can tolerate the workload,
but I can't really get what I consider to be adequate
performance.

Pilot A: If I ever got into a high gain situation, I would
6 follow the couple right into a PIO. It's very
(K = .45) objectionable. At this altitude it's tolerable. I
think in close proximity to the ground, there would be
a major problem with that.

HF128

Pilot A: Well let's see what we've got here. We got a small
4 lag in the response it seems like, combined with a
(K = .45) rather soft dynamics. The overall impression is the
airplane is just a shade sluggish. However, the lags
and the slow rate sort of blend together naturally, so
there is not a controllability problem. It just takes
a while getting what you want out of the airplane.
So, you can make it do what you want it to do, maybe
not quite as rapidly as you would like. I had no
problem making the airplane respond to what I think I
want out of it. So, although I wish it happened a
little bit quicker, I'll say that I can get the
desired performance.

Pilot A: You got a moderately slow responding airframe, coupled
5 with some lag. However, the lag seems to be appro-
(K = .45) priate to the airframe dynamics and sort of hard to
settle it out. It just comes across a little slug-
gish. Sensitivity is pretty good compared to the
previous configuration. I like the sensitivity fairly
well on that run. The problem is, I cannot make rapid
corrections. The airplane just does not get it on, so
therefore, I lose a bit of precision. I can certainly
get adequate performance. I can't get what I would
really like the airplane to do.

HF129

Pilot A: I don't know, sometimes I think I'm seeing a mid-
 3 frequency superimposed response in there. You know,
 (K = .45) like just a little oscillation in the mid-frequency
 range and sometimes I don't see it. Whatever, it's no
 more than a minor nuisance. I can certainly make the
 airplane go where I want to. I don't have any harmony
 sensitivity or lag problems.

Pilot A: I guess I would say that that's almost a good configur-
 4 ation. Sensitivity is good. Response rate is fairly
 (K = .45) good. It could be just a shade faster, but I guess
 I'm seeing a little bit of lag in the response that
 makes it a trifle less than optimum in predictability.
 If given a couple seconds, it goes where I want it to.
 I have minimum difficulty controlling it, but there is
 a quirk in there that I'm having some problem with. I
 will say it's a minor, but annoying deficiency.

Pilot A: I'm not quite sure what we've got here. It comes
 4 across to me as predictability as being down a little
 (K = .45) bit. I don't know if it's an additional mode or a bit
 of a lag or oversensitivity or a combination of all
 things. I'm just having a little bit of problem ques-
 sioning where the thing is going to or adapting myself to
 how much response I'm going to get, so it comes across
 as being less predictable than I would like. I have
 to provide more compensation in the form of having to
 make two or three corrections in order to get the job
 done than I would like. I can get the desired perform-
 ance, I just got to work harder for it.

Pilot A: Dynamics pretty good on that one. Sensitivity may be
 4 just a little bit low. I want to hedge that, not
 (K = .45) necessarily sensitivity, the rate might be just a
 Y_v = -.2 little bit low. In other words, from the time I
 perceive a correction until the airplane gets it in,
 is a little bit longer than I would really like. I
 can certainly do the job. I put it in the minor but
 annoying deficiencies category.

HF120

Pilot A: 5
(K = .45) There may be some lag in the response. It sort of ignores small rapid inputs. As a consequence, the response that I perceive is always stepy. I either get too much or not enough. Moderate size inputs, it almost seems like there's another mode in there that I'm not controlling, that's just sitting there bouncing around. I can make the airplane go more or less where I want to, but I find my inputs being step inputs, I'm going bang, bang on the control, I'm getting a very rapid step like response and I'm not real wild about it. I think it would be uncomfortable in a real airplane. It's definitely not the way I prefer to fly the airplane, so I'd say that deficiency certainly warrant improvement. There are at least moderately objectionable deficiencies. It's not so much a matter of extensive pilot compensation, as it involves a different mode of flying than I would really prefer to use. It does force me into a different mode of operations. I'll have to say it's a considerable pilot compensation.

Pilot A: 5
(K = .45) We've got a moderate size lag in this configuration, combined with a moderately sluggish response, it means that the pilot has to sort of stay on top of things. You never have serious doubts about your ability to control it. You just wish that you could get what you wanted a little bit quicker. Desired performance is not obtainable, because there's a lag in there, but adequate performance certainly is.

Pilot A: 3
(K = .45) No real qualms with that. I think there might be a minor lag in there, but the airplane does pretty much what I want it to. I guess there's something in there that's bothering me, but I don't know what. I can certainly get the job done. I wish it was a little bit crisper, so I'll say that it's got some mildly unpleasant deficiencies in that I've got to do some compensating for the lack of immediate response, but sensitivity wise and the whole schmeer, it's a pretty good airplane.

Pilot A: 4
(K = .45) The airplane does what you tell it, but it almost seems like there's an additional mode snuck in on top of it sometimes. It will get a quirk in the response and there's a modest amount of lag in the onset, but it's not a major problem. It's just a little difficult to be as precise as you'd like to be with the configuration; however, I can get the job done certainly, but there's something in there that's getting to me. I can get the desired performance, but I've got to work.

HF121

Pilot A: There is a perceptible lag in the lateral response on
 6 this configuration. There seems to also be another
 (K = .45) mode in there. I get almost a secondary response
 sometime. The primary problem is that with the lag in
 getting the attitude, I have to over correct and
 therefore, I'm always using a larger bank change than
 I think I need initially. Instead of being able to
 get away with corrections on the order of 10°, I'm
 usually using 20°, so I'm almost at a PIO situation;
 fairly large corrections. I can fly, but I don't have
 any great difficulty in controlling it. I have a
 problem with precision control. It can't be done.
 The deficiencies certainly warrant an improvement. I
 can get what I would consider adequate performance,
 but it does take a lot of pilot compensation. If you
 have a really tightly defined task, low altitude,
 hover control or something like that, it could get
 into the Cooper-Harper 7 area.

Pilot A: Fairly good configuration with a bit of delay in
 4 there. The delay comes across as a nuisance that I'm
 (K = .45) not real enthusiastic about, but it doesn't really
 impeded by ability to do anything except very, very,
 very tight tasks.

Pilot A: Sensitivity and rate seems good. You've got a
 5 distinct noticeable lag in the response which gets
 (K = .45) you immediately into an over correction situation.
 You can't make the small corrections immediately and
 you get into a wing rock, rocketing oscillation,
 constantly over correcting from one side to the other.
 It's not a PIO problem, it's just that in order to
 stop a drift, you put some in, then you put some more,
 you put some more and put some more then you got to
 leave it all out and it doesn't come out fast enough,
 so it's a definite nuisance. You can't get the
 desired performance certainly. You can get adequate
 performance. The airplane's just slow to respond.
 You don't have any controllability problems or any
 real PIO problems with it. It's definitely a very
 objectionable deficiency.

HF1T1

- Pilot D:
6
(K = .6) At times I felt like I was doing really well and other times I get into more trouble than the others. I had performance degradation that surprised me. In general, thought the airplane was controllable. I think I could get the job done, but I didn't think it was satisfactory without improvement and I don't think I was achieving desired performance, so we're talking about adequate performance. There was something about it I didn't like and that's for the translation, if I could stabilize the airplane, if I didn't have any of these wind shears and was just trying to stabilize in the hover, I could get it stabilized. Trying to contend with the disturbances and principally the wind shear, left something to be desired. I do find as I said, deterioration right at the end of the third approach. It seemed like I got hit by more gust, more wind shears and I had definitely less capability to stop and I was tending to over control.
- Pilot B:
5
(K = .3) It's a hard one to figure out. There's something I don't like about it and I'm not sure whether it is a differential in response as you move the stick out-board or whether there's a little more lag, or just what there is. I can't really figure out what's bothering me, but there's something I don't like about it.
- Pilot A:
4
(K = .45) The airplane seems quite loose. Not too many problems. Sensitivity/controllability what have you, are pretty good, almost a continual low amplitude, low frequency oscillation. It seems that the auto damping is down is what I perceive and I've gotta sort fight it a little bit to keep the wings level. So, you have to do something to fly the airplane. I'm not quite sure what it is, but I perceive it is an annoying deficiency.
- Pilot A:
2
(K = .3)
 $Y_v = -.2$ I've got no qualms about that one at all. Super configuration.

HF1T2

Pilot A: I'm not real happy with that one. You got a perceptable
7 lag. There's something that looks like a secondary
(K = .45) response. You really got to be smooth on your inputs
and you got to try to stay ahead of the airplane so
you need extensive compensation. It requires
improvement.

Pilot C: I got a bunch of response to the input that I had, it
7 seemed to me like for a very small input and then I
(K = .45) had to take it back out because it just began to build
up exponentially, I felt not to a great degree, but it
wasn't linear. This is very sensitive laterally.
Without the gust, it's a little better. It is sensi-
tive laterally, maybe too sensitive and probably would
be sensitive to gust.

Pilot B: There's a big lag in there.... I find myself making
6.5 an input-nothing happening and going into more input
(K = .45) and then starting to do the bang-bang routine. Also,
I find myself getting out of phase with it trying to
hover precisely. It's very disturbing and because of
the strange action laterally it feels like there is a
giant disharmony in pitch.

Pilot A: Reasonable underlying dynamics with a distinct notice-
7 able and objectionable lag in the response. Totally
(K = .45) wipes out your ability to make small corrections. I
Y_v = -.2 even got a little hesitation on it. The performance
is adequate at that level. We're somewhere in the 6
to 7 ballpark. I don't have a tendency to couple into
it. I guess the deciding factor is going to be that
in this case, I would say that that amount of lag
definitely requires improvement. It could be somehow
diastorous under certain conditions.

HF1T3

Pilot B: Maybe a slight difference in the lateral sensitivity.
4 Hover response maybe slightly different.
(K = .6)

Pilot A: OOOOH Help! I said the lag in the last configuration
7 was noticeable, this would have to be very noticeable.
(K = .45) Well definitely major deficiencies. I question
controllability. I think I could land it in an absolute
no wind situation. I'm not sure I could land it
with any turbulence, cross wind or anything like that.
Adequate performance was not attainable certainly. If
my task is properly defined as trying to stay somewhere
over the concrete and avoid sliding it, I would have to
say that for that, I could back away from it and get
high enough, controllability wouldn't be a question. If
you play the game and say that well yeah, but you're
operating in close proximity to the towers, platform
ships and what have you, I would say that controllability
is a question. It depends on how you define the task.
I'll go into this in detail, but the 7, 8, 9, ratings
are very, very task dependent. So, for the task you
gave me, well I didn't crash it really. For anything
that required a slightly tighter control, I think there
would have been serious questions.

Pilot B: I don't like the lags in it, but I can come closer than
5.5 I could with some of the other ones.
(K = .45)

HF1T4

Pilot B: This one has someone down in the control room that's
7 a little bit slow to answer when I holler at him.
(K = .3) That delay is long enough for me to see it. I can
easily get out of phase with it. I move it and I say
wait a minute it's not going far enough or fast
enough. I've got to use more control and I will start
to over-control. I'm deliberately not over-control-
ling here, but it would be very easy to do. It
wouldn't recover fast enough, from large changes here.
I'm getting out of phase with it when I'm trying to
really tie it down tight. I can't get it to where I
want it. Not with that kind of lag.

Pilot A: Distinct, very objectionable lags, controllability is
7 almost in question. At that altitude, I can avoid
(K = .45) getting into major difficulties. If I got close to
the ground, I would have serious questions about the
controllability. I think if you try to get this thing
down into a landing condition, it might possibly be an
8 where controllability is a distinct problem.

LF121

Pilot C: Part of the reasoning is that it handled the gust very
4 nicely. It handled large corrections nicely in and
(K = .45) out. The only thing that I did not like here again,
was the fact that once I got it into the hover and got
it stabilized, I still had to continue to fly the
machine. I couldn't take my hands off.

Pilot A: It flies good like an airplane should. Nice. That's
3 a pretty good configuration. I think I perceive a
(K = .45) small lag in rate onset, but the dynamics are very
good, stable, well damped, I get exactly the response
I call for and with reasonable repeatability. I would
say even a little pilot compensation is required for
desired performance. I can stay very close to my
desired spot.

Pilot A: Nothing dynamically wrong with that configuration.
3 I think I could use just a shade more sensitivity
(K = .45) on that, not a whole lot. I can certainly get the job
done. With maybe a little more sensitivity I'd have
to go with a 2.

LF123

Pilot A: I sort of like it. It goes where I want it to go.
3 Maybe there's a problem with the sensitivity. There's
(K = .45) something in there that's a minor nuisance. Maybe
right around neutral. It's giving me a little bit of
problem on very, very minor corrections, but it's very
pleasant to fly. It's predictable, it goes where I
want it to go. It's very pleasant to fly.

Pilot A: I think it goes where I want to. I don't notice any-
2 thing unusual in view of how well that performs. I'm
(K = .45) not having any trouble establishing wings level, it
does go where I want to point it. Sensitivity is
good.

LF125

Pilot A: You got something in there I'm not real enthusiastic
4 for. I don't know if I got enough bank angle at full
(K = .45) deflection. I can stay pretty close to where I want
to, but there's still something in there that's
annoying me. So, I'll say there's moderate pilot
compensation.

Pilot A: I've got adequate response for large inputs if I try
3 to couple fairly large maneuvers in there and response
(K = .45) comes from the large stick inputs, at a reasonable
rate. I don't seem to have as much response or sensi-
tivity for small inputs, so for small corrections, I
seem to have to use more stick than I think I ought to
and I wind up correcting twice more or less. I'm not
quite sure what that translates to. Precision is good
in that I can get there and hold it and I can get back
to wings level and things like that. It's precise in
as far as holding an attitude, but I am having to put
in a little bit more stick. Sometimes I put it in and
I have to put a little bit more, so I guess the sensi-
tivity.... I sense a sensitivity change for small
inputs. It certainly goes where I point it, but I do
have to compensate for it and I'm trying to decide if
I have to compensate, if it warrants improvement, or
if it's something I'll live with. I'm really not
having a great deal of problem with it, it's just
something I could adapt to. There is something in
there that I don't like as far as the sensitivity
goes. It's something I could certainly live with.

LF127

Pilot A: That was a nuisance. It feels sort of like there's
4 occasionally getting some kind of secondary response
(K = .45) in there. I'm getting what I ask for - almost a two
stage response. It's controllable, goes where I want.
Rate build-up might be a bit slow. I could handle
that with a little more sensitivity. It does what I
want it to do, I'm not really having any major prob-
lems with it, but it does require some compensation.

Pilot C: I don't like that one at all. That's too much work.
8 The thing that I didn't like was that it took a lot of
(K = .45) input to get a motion started and then slowing it down
took some input and then once you got it reasonably
sorted out, it would just sit there and wander and I'm
not sure whether those were pilot inputs or what, but
I couldn't get the system really stabilized and I was
just continually having to fly the machine. It took a
lot of pilot attention just to fly the machine and we
don't want that.

Pilot A: I no longer really feel I have enough control to get
7 the job done. Just comes across as both rate of onset
(K = .45) and also, the sensitivity in as far as bank angle per
degree stick, so I think I'm down in gain and fre-
quency both. I would have to say that for this task,
I do not believe I am getting adequate performance.
Controllability is not in question.

LF121*

Pilot D: That seemed to be getting closer to something that I
 3 think is satisfactory. No problems with the feel sys-
 (K = .6) tem. The attitude response was smooth, the initial
 response was okay and that was predictable. The
 capability was okay, I thought the initial response
 was a little bit quick. I was able to contend with
 what seems like a large lateral upset in terms of the
 wind and I was able to discern the existence of it
 which says that I was able to control the lateral.
 Flight path attitude trade-off; if you mean by that
 how much attitude I had to use to get the translation,
 I thought they were well matched. Height response; I
 paid a little more attention to the initial throttle
 setting and was able to stay around I think 75 feet, a
 little lower than I had been before. The gust disturb-
 ance seems of fairly large magnitude. I was able to
 get back and every time get over the line, so that in
 some way, I think the translation of the airplane is
 clearly controllable. I thought I could do the job
 and I felt like it was a smooth, reasonably precise
 airplane. So, I think it was satisfactory, the only
 complaints that I have is a little bit sensitive
 initially than I might like.

LF123*

Pilot D:

7

(K = .6)

It's very difficult to understand what's going on. It's a very strange airplane to fly. The first translation to the left and coming to a stop on the left edge of the runway was smooth and relatively predictable. (This was an early run with the partial objective of developing the task definition. The pilot first moved to the left side of the runway, with no wind, before completing the standard task.) I tended to stop earlier than I wanted to so that the bank angle seemed to be going in more discrete steps than I wanted. It was very rapid and stopped very rapidly, very quickly. Then, as I came back across and did the getting back to the right edge of the runway, I got into the gust. I would have increasing difficulty and it was very snappy when I would try to correct, and it really blows my mind with my visual scene here, but then I'd end up with an increasing steady state right stick requirement until it was surpassing my feeble right arm, and each time as I ended up roughly stabilized in over the line in the hover, I'd end up with really heavy lateral forces to the right, and the way we're doing the task, not changing the heading and so on, as we talked about, the airplane has deteriorated and was aggravating with a little sense of somebody else flying it on occasion. But getting to the rating, it was controllable. Attitude performance attainable and in a sense, I could - I thought I could - achieve the performance, but I sure had to work too hard to do it. But, I didn't think the compensation was tolerable in that sense that disconnection with the airplane, where you don't really correlate with what to do to get the job done, that was the disconcerting part. When I actually got stopped in the hover, on the second part of the lateral translation, I had that really heavy force, which is not acceptable. The initial one, I couldn't stabilize it in the lateral. It seemed very quick response with a funny sort of lateral trim problem interacting with attitude. If I had nothing else to do but just hover the airplane, as you give it to me, the initial conditions, and I stopped there and just hovered, I think I would say that I could do the job. But, the extraneous, what seemed like lateral trim, input build-up after a period of time made it unacceptable. So, I really have talked about the forces were a major problem near the end of the task. Sensitivity seemed overly sensitive in combination with that, which is a disconcerting combination. It

LF123*

moved very rapidly and I had to hold large forces, so it wasn't tuned properly. The attitude response, I didn't notice any tendency to oscillate, but these other factors dominated my problem. Flight path response, initially okay. I could get over to the left side, I tended not to be able to bleed off the bank angle and stop where I wanted, but that was okay, but it deteriorated going to the right side in the face of the wind shear. Although I didn't move as far as I have in some, I was more having a problem with the bank angle control and the extraneous trim that I was positioning. Height was not a problem. As I said in the hover, it would be a little better if you only hovered for a little while.

LF125*

Pilot D:
10
(K = .6)

That was a very strange airplane to fly. Controllability was a problem, especially on the third one. I just about lost control of the airplane. It seemed to start out alright, and then I was unable to get back over to the right and with increasing right stick, sliding to the left and the last of the three, I ended up just about sliding into the ground going left. The forces and displacements are very noticeable, once it got near the end of the task whether I was getting the wind from the right or whatever it was, I had large stick displacements and seemingly sluggish response. The attitude response initially seemed alright, but at the end I was really unable to increase the attitude in the face of sliding to the left and stop the slide, I didn't PIO, but controllability was a problem. Flight path response was not predictable, special inputs were; you use all the muscle you had to hold it over there. I got very confused between flight path and attitude; it seemed like things were changing very dramatically during the course of the task. Height response was diminished in that I felt myself up over a hundred feet and paying a lot of attention to everything. I felt the wind. I didn't feel any turbulence, but there must have been some very large wind effects, because I ended up sliding left across the runway while trying to go to the right. So both the translation and the hover problem, I could never get stabilized in the hover, although a couple of them I did get over to the left edge of the runway and stop it there. My ability to fly the task decreased as I went through the task and each time coming up to the right edge of the runway to try and stabilize I had great difficulty even staying in the right side of the runway, right half of the runway and the last one, I came perilously close to crashing, but I think the airplane is really not controllable. I could control the translation. Initially I could, but in the final, the last task I really was trying to hover and ended up translating it and unable to control the translation, so I think if I started out as we started the task and just do anything, it went along in the lateral axis stayed stable, but very disconcerting, very easy to get, it felt like you were horribly crash coordinated, although I wasn't, at one time I did inadvertently use the rudders. I wanted to turn to the right to see if I couldn't solve why I was getting the big lateral translation in almost the reversal, apparent reversal of the control pushing right and going left. I find that I push right and go left and I don't like, but that's like having a lot of adverse yaw with a high dihedral effect I guess, I just got disoriented flying the thing.

LF127*

Pilot D: I can track the center line for awhile anyway. Regard-
10 less of how it looks one way or the other, I'm start-
(K = .6) ing to build-up a bias with less translation. Now I'm
building in a lot of right stick, banking left, feel-
ing very uncomfortable. Further right stick, banking
left, going left, unflyable.

N2LAT

Pilot B: Pitch and yaw and height response all three reasonable.
 6.5 If all I want to do is hover it and nothing else, I
 (K = .3) can just sit there and not do anything, but if I want
 to change positions, the extreme overdamping is get-
 ting to me and I could go to lots and lots of lateral
 stick displacement with absolutely no increase in ro.
 Very high roll rates right around neutral, initial
 breakout, are unacceptable.

Pilot D: In general, it's a well behaved airplane except it's
 5 too quick. It's just too abrupt initially and it's
 (K = .3) doubly disconcerting because of the visual display.
 You really get yourself into a position where your
 trying to fly the airplane aggressively. The rapid
 movement for tiny inputs really slow my mind and
 visual mind, so that if I did consciously try to fly
 the airplane smoothly and I could achieve satisfactory
 performance, but in the face of the gust I couldn't
 always do that and I ended up with these very rapid,
 almost rachety type lateral responses which I didn't
 like, but I think it's controllable and I did think I
 could get the job done. It's not satisfactory because
 it's just too quick, too abrupt. So, it definitely
 should be improved and I don't think therefore, I'm
 gonna achieve a desirable performance, but I think all
 and all adequate performance and out of the gust
 environment, if you smooth yourself down a little bit,
 you could achieve desired performance. If I just had
 to hover without contending with those upsets, it
 would likely be a 4. You can fly smoothly and you get
 smooth performance. You can't fly smoothly when you
 have to contend with the gust.

Pilot B: Wow, a guy could make himself sick in here with that
 5 one. As far as getting the task done, it's so quick
 (K = .3) and positive that I could make instant corrections.
 However, I think it's way too quick. I'm being very
 careful not to over control here and I'm getting back
 into the very small bang, bang motion again, because I
 can't control it smoothly otherwise. The rapid bank
 angle; well the very, very sharp, almost instantaneous
 bank angle is bothering me.

Pilot B: I find that one quite comfortable. I don't know, still
 3.5 got a little bit of lag there and a little bit of
 (K = .3) jerkiness, but at the same time, it's very, very easy
 (No Wind) to do.

N2LAT

Pilot A: The airplane goes the way you want it to go, just sort
4 of instant bank angle, which is a little disconcert-
(K = .3) ing. Visual display just instantaneously almost goes
to commanded bank angle, so I'll occasionally get a
ratchet in the display, but usually just a bang, it's
there and it's a little disconcerting. I perceive
nothing unusual in the dynamics outside the repetitive
response. I would say that the repetitive of the
response is annoying. In fact, it is moderately
objective.

Pilot C: That one was responsive. It seemed heavily damped.
5 I put something in and it would pop right back out.
(K = .3) Maybe you put a control input in and then if you
didn't hold it in, it would come right back to neu-
tral. So, a lot of stability there I guess. It
wasn't bad. It's a little sensitive just for the
normal inputs I think with a 20 knot crosswind, ramped
in like that, it handled it reasonably well. The
thing that I didn't like was the normal sensitivity to
the stick inputs. It would just sit there and if you
made any kind of unusual movement at all, it was very
responsive to that and maybe slightly too responsive.

Pilot A: You move bang-bang. The response is right there.
4 There's no lags. It goes exactly where you want to.
(K = .3) So, it's not a problem mating the airplane to what you
want to, however, it is a very abrupt response. I
think you'd get used to it but it would have to hedge
on the ride qualities. It's got an annoying deficiency
there and that abrupt response.

Pilot C: It's very responsive. It does what I want it to do.
4 I put it someplace it stays there. I take it out, it
(K = .3) comes out and once I get it set where I want, I take
my hands off, I got a hands off hover capability.
It'll stay there. The only thing that's maybe a little
detrimental is it may be just slightly, ever so
slightly, and I hesitate even to say this, sensitive,
but not bad at all.

Pilot A: We're back to the very rapid rate onsets, which I
4 object to because of the display problems. When it
(K = .3) jumps around like that, you start getting vertigo, so
the response is more rapid than I would like. It's
too abrupt. No perceptible lags, no nuisance modes.
It's controllable. It goes where I want it. However,
I do object to the abruptness of the response, so it's
got an annoying deficiency.

N2LAT

Pilot A: The only objection is repetitive response. You start
4 to get the display problems and what have you. Very
(K = .3) controllable, goes where you want it to go. Just gets
there too quickly. So, it's not really a question of
compensation, it's a question of a deficiency that is
annoying in this case.

Pilot A: Overall, the response is just very, very rapid. Much
5 more rapid than I would like to fly. That makes it
(K = .3) sensitive to small inputs, so I had trouble making
small corrections. Repetitive response is almost a
vertigo into the simulator. Not real wild about the
sensitivity. I find myself getting into an over-
control situation because of the over-responsiveness.
So, I'll have to give that moderately objectionable
deficiencies.

Pilot B: At first it seemed very sensitive and as I got used to
5 it of course, that went away a little bit. Very light
(K = .3) and sensitive right around neutral with a very rapid
force build-up as you go out beyond neutral very far.
Not pleasant in that regard. I can release it and it
will come rapidly back to wings level, but I'm afraid
that's pretty jerky if you're actually flying it that
way and I found myself compensating considerably just
to detune the system. In other words, to be very
careful not to make much of an input.

Pilot B: It's not bad right around neutral, but when I get
5 outside of neutral, a half an inch or so, it feels
(K = .3) like the rate changes. In other words, the gains
change. I don't know exactly how to explain it, but
increases in lateral stick position do not give me a
corresponding increase in roll rate or roll angle, so
I'm having to compensate. Very, very small motion,
it's no problem at all, but once I try to get out
there and get a little bigger bank angle, a little
faster roll rate, I run into a wall.

Pilot B: It's a little bit quick, sharp, large force build-up
5 beyond some 10° of bank or so, trying to hold it on
(K = .3) there. Compensating for a little bit of lag that
doesn't seem to help out any.

N2LAT

Pilot A: The response is too rapid for my likes for the joint
 3 reason that I think it's unrealistically fast for
 (K = .3) flight and also, I get this minor case of vertigo with
 the display outside jumping up and down, but the
 response is quick and precise. I can put it exactly
 where I want to, and I don't have to pay a whole lot
 of attention to it. It's just very distracting with
 that high acceleration roll performance. I can
 certainly get the desired performance and I don't
 ... really have to compensate, although I would have to
 say that the display is a minor problem as far as I'm
 concerned and I think it's unrealistically fast for
 flight.

Pilot A: The problem here is the blindingly fast response given
 3 that vertigo inducing situation of the outside display
 (K = .3) flickering. On a couple runs ago, we flew one that
 had a very rapid onset, well a very rapid roll rate,
 but it seemed to be a slight softer onset. It appears
 quite harsh and you have to actually back away from
 your pilot inputs. The airplane follows the helm
 precisely, but too quickly and it would be very
 uncomfortable riding and I guess the big complaint I
 would have is it would probably be very bad ride
 quality. However, the airplane goes exactly where you
 want it to go. It just gets there too abruptly.
 Pilot compensation is required in that in order to
 keep the outside roll rate down, you got to sort of
 back away from your input, but that's about the only
 thing that you have to do.

Pilot A: No problems at all. The airplane quickly and precisely
 3 answers the helm. I'd say this one is down just
 (K = .3) slightly in response, sensitivity is down just a
 shade, so I'll say that I wish it was just a shade
 more response in there.

Pilot A: We're back to the very high rate configuration where
 3 when you bang your stick over, the airplane bangs over
 (K = .3) and the outside display goes bang, bang. It's a lit-
 tle disconcerting visually and it would probably be
 uncomfortable in flight, however, the airplane goes
 quickly and precisely where you point it with a mini-
 mum of delay. I think there is a modest amount of
 delay in that response. However, it certainly is no
 problem coping with it. My only objection to it is
 you got a possible ride quality type thing and cer-
 tainly is a little disconcerting watching the horizon
 going around at discrete 15° jumps more or less. So,
 I can get desired performance when I put the stick
 over, the airplane goes you know, what can I say?

N2LAT

Pilot A: We're back to the instant bank angle machine. No
 3 delays, certainly none that are perceptable. Sensitiv-
 (K = .3) ity is fair. Rate onset is instantaneous, therefore,
 we get the flickering outside display, the vertigo
 inducing jumping in the horizon and the possibility of
 a very, very poor ride. However, the airplane
 instantly goes where you point it. It means controll-
 ability is excellent, hedging of course as usual, the
 ride qualities.

Pilot A: No problem with sensitivity. No noticeable lags,
 3 delays and what have you. The problem is the abrupt-
 (K = .3) ness of the response which leads to the display prob-
 lem and the vertigo problem and everything associated
 with it. I can make the airplane to do precisely what
 I want. It's very precise. It's just a little bit
 too crisp. You don't couple into it or anything else.
 It's just I believe it would be an awfully uncomfort-
 able ride in a flight vehicle and you might possible
 get into some PIO just because you're getting bounced
 around, but you can certainly, precisely control it in
 the simulator. Hedging, of course, the ride quality.

Pilot A: Am making a very small input so I can get pretty much
 5 the performance I desired. There's some lag in there
 (K = .3) or whatever. It's giving me a little problem with
 position control. Can't really put my finger on it.

Pilot A: The big problem here is the very, very rapid rate. We
 4 start getting a display jumping and display flicker.
 (K = .3) It's instant bank angle and once you adapt to the
 sensitivity in terms of bank angle per stick deflec-
 tion, you tend to go to a bang-bang control mode where
 you pause a second to mentally figure out exactly what
 you need to put the stick there and just relax,
 because the airplane will do it. It would be an uncom-
 fortable ride and you have to adapt. I found myself
 adapting slightly different than normal piloting
 strategy on it. I can certainly make the small correc-
 tions I want to make. I don't like having to go to
 that bang-bang control mode, on the other hand, I
 don't really think I do, I just found myself doing it.
 I can get the desired performance, my two hedges are
 that I found myself doing something I wouldn't normal-
 ly do with an airplane going to a bang-bang control
 and also I hedged the ride quality.

N2LAT

Pilot A: Nice crisp response. Sensitivity is good, I guess I
4 see a barely preceptible lag in the response. Very
(K = .3) controllable, very predictable, it gets the job done.
Might be a shade harsh on the ride qualities. Got a
few oscillations going on the first flight, but I
really had to force that, so I wouldn't call it PIO
problems. I like the sensitivity. The rate may be
just a shade on the high side, but all told, not a
horrible configuration.

Pilot A: That one's a little puzzling. I'm getting occasional
5 oscillation on the inputs - small inputs and occasion-
(K = .3) ally on large inputs. I don't know if I'm inducing ot
or if there is an oscillatory movement. Dynamics is a
distinct nuisance. The airplane seems relatively sen-
sitive. The rate is a bit too high for flight. I
think I'd have to hedge on the ride quality of the way
the airplane gives you that instant bank angle, but
it's definitely got - I'm definitely having some
problems getting the oscillations out, it's a combina-
tion of high sensitivity and small lag or what.
Whatever, the airplane's oscillation prone, not PIO
prone. You don't tend to couple into it, it's just
you get almost like an underdamp response sometimes.
As I said before, I don't know if I'm inducing it or
if it's something in the dynamics. Because of that, I
can't make the fine corrections that I'd like to make,
so I guess I'd have to say I can't get the desired
performance. I can certainly get adequate performance
and it's just a nuisance in there.

Pilot A: Another good configuration; however, the rate is a
3 shade too high. I think you'd have a ride quality
(K = .3) problem in flight.
 $Y_v = -.2$

Pilot A: We're back to the very, very brisk dynamics that would
4 be a distinct nuisance in flight from a ride quality
(K = .3) point of view, definitely. I can make small correc-
tions. I don't know, there may be a little bit of a
lag in there. If there is, it's not enough to be
anything more than a distraction. My only major - my
major complaint with the configuration is the abrupt-
ness of the response. It does cause me to change my
pilot strategy, because I go to this bang-bang opera-
tion which I said before, I'm not particularly wild
about, but I can get the performance I think I want
out of the vehicle, but I'm not wild about it.

HF211

Pilot A: The problem here is just the response is down. Sensitivity primarily, although it's a combination of oversensitivity with the lower rate system it seems like, so you have to stay on top of it and even then, just because you have to move the stick so far in order to get the response, you always will be a little bit behind the requirements generated by the external disturbance. The airplane is controllable. You've got enough control, you just can't get it very rapidly. It feels like you're flying a very big airplane. Deficiencies warrant improvement, certainly. I'm going to have to say that adequate performance is obtainable, but it's borderline. If the response was down much more, we'd be in the 7 or 8 ballpark.

Pilot A: It seems to me that we've got two problems. One, the sensitivity is down in so far as absolute bank angle is concerned, and two, the response rate is down. The airplane is sluggish and doesn't have a hell of a lot there in the first place. I cannot get the desired performance, because it just takes too long to stop the drift and such like things I'm going bang/bang. I go to full input, then neutral, then full input the other way. I don't really have the tendency to couple into it or get into a controllability questions, things just don't happen quick enough. I don't perceive any lags in the responses, just a rate problem so, adequate performance I think is obtainable. I think you'd have a problem at low altitude precision hover, but I don't have any problems staying somewhere in the ballpark with it. Adequate performance is obtainable, but you have to stay on top of the machine. You can't get very far behind it.

Pilot A: The only problem with this configuration is it's too sluggish. Once you get everything together and the wind averages out at what have you, boy it stabilized as a rock. On a lot of tasks that would be quite appropriate for, however, there's no such thing as a small correction with this configuration by the time the airplane gets it in, you no longer need a small one, you need a large one, so it's a continual series of fairly large amplitude maneuvers to make a correction. We got a problem with not having nearly enough response. It's way too sluggish for a tactical airplane that would be exposed to a gusty environment. I can do this job, let's put it that way. I can do the job we're assigned here. I don't like it; however, if

HF211

you want to carry this down to a lower task, I don't think you've got the roll performance you need, so I'm going to have to say that it does have major deficiencies. For the task we're assigned here, the maintain station keeping at altitude. I certainly can't do it as precisely as I want to, however, I can do what I consider an adequate job. If we go down to the in close to the surface landing type task, I've got a question in my mind if you have sufficient control, for maneuvering and close to the ground in a gusty environment, so there is a question that down close to the ground or in close proximity to obstacle or something like this, it would definitely be a Level 3 airplane.

Pilot A: Major problem with the configuration is it is just too
6 sluggish. I don't have the tendency to get trapped
(K = .3) into this very large bank angle and not be able to get
Y_v = -.2 it out in time phenomenon. Although the airplane is
way too sluggish, with going in and coming out, I
don't really have the controllability question I had
earlier on some of those. I can get the job done. I
don't drift all the way across the runway. I don't
have the controllability problem. I guess I'll have
to put it in the bottom of Level 2.

Pilot A: We're back to a sluggish configuration. It takes a
6 long time to react to control inputs. Therefore, I
(K = .3) can no longer make the small corrections that I would
prefer to make and on top of that, I'm seeming to be
having more problems with the configuration than I
think I should. In other words, I'm oscillating
considerably in position. I'm running a right to left
much more than I should, not just in bank angle, I'm
actually sliding sideways more than I should. I'm
working harder than I should.

HF212

Pilot A: No particular problem. The response is down a bit,
 3 Sensitivity is down. On the other hand, it's a very,
 (K = .3) very precise airplane and no lags that I perceive, so,
 Y_v = -.2 therefore, I would say that I'm using perhaps more
 stick than I've averaged on some of the other configur-
 ations, but the aircraft response to the input is
 quick and is reasonably rapid, rapid enough and pre-
 cise. I guess I wish it had just a little bit more
 sensitivity, but I certainly have no controllability
 problems. I can't really say there are any problems
 at all.

Pilot A: Configuration is quite pleasant to fly. There may be
 3 a small lag or maybe it's just a soft response start-
 (K = .3) ing up. I guess the only problem I have with it, is I
 Y_v = -.2 guess I wish it just a little bit crisper. In other
 words, I think it could be just a shade more sensitive
 to control inputs. I have no problem at all making it
 do exactly what I want it to, so it's definitely Level
 1. If it had a shade more sensitivity, it might have
 gone to a 2.

Pilot A: It is a bit sluggish, therefore, as I said before,
 5 when you get into these configurations, there is no
 (K = .3) such thing as a small correction, which means I can't
 Y_v = -.2 get the precise performance I would like to get out of
 it. I have to accept a little bit more oscillation
 than I would consider desirable, so I'm in the
 category of adequate performance.

Pilot A: I've got no major objections to the configuration at
 2 all. Quick, precise, does what I want it to do with a
 (K = .3) minimum objection.

HF213

Pilot A: Sensitivity is alright, but the rate of onset is down,
 4 therefore, the airplane comes across as being a little
 (K = .3) bit sluggish in a roll and it's an annoyance, cer-
 Y_v = -.2 tainly, but wish it was better. I could live with it.
 The airplane is precise. I can get exactly what I
 want, I just wish I could get it just a little bit
 quicker. However, I can control it, I wouldn't have
 any qualms about handling the airplane in a cross wind
 or anything else. So, I'm going to say that yeah, I
 can get my desired performance, but I have to push for
 it.

Pilot A: Airplane does what I want it to do with a minimum of
 3 grips.
 (K = .3)
 Y_v = -.2

Pilot A: The dynamics are basically pretty good, but it seems
 3 to ignore small high frequency inputs. I have a
 (K = .3) little bit of a problem making very precise small
 Y_v = -.2 corrections. However, I can certainly get the job
 done. No major problems at all. It's got what I call
 some nuisance modes in there, so it's got some defi-
 ciencies. I'm trying to split the difference between
 mildly unpleasant to annoying here. Well, let's go on
 the basis of compensation. I do have to work to get
 the small corrections in, but I don't have to do a
 hell of a lot to get what I want out of the
 configuration.

Pilot A: All told, I like it. I might notice a little hesita-
 3 tion in the response on occasion. I don't think it's
 (K = .3) quite as clean a performance as I have seen.

HF214

Pilot B: I find that one reasonably comfortable.
3.5
(K = .3)

Pilot A: That's pretty good. I don't have any problems with
3 that one. The rate onsets about what I like. Sensi-
(K = .3) tivity is good. I notice nothing perceptable in the
way of control lags or secondary responses. I have a
little problem with very small inputs, so I'll say
it's got some mildly unpleasant deficiencies and maybe
it's just the way I'm doing it.

HF215

- Pilot A: The airplanes goes where you point it. I don't notice
 3 any unusual characteristics. Response seems down
 (K = .3) which means it's not as abrupt and it feels like I'm
 getting more bank angle per unit stick. So, as far as
 the response to controls, as far as I'm concerned,
 it's pretty close to optimum. The dynamics aren't
 that shabby either. I can make the airplane go where
 I want it to, doesn't seem to have any lags, doesn't
 seem to have any bad damping characteristics, nothing
 else. Turn the wind off, 2.
- Pilot C: A large input over my spot, correct, stop, level the
 5 wings. Go forward small tiny corrections. It
 (K = .3) responded nicely to my inputs. The input stayed in
 there until I took them out. The only thing I didn't
 like is that it did not hold the fine once I put it
 there and it had a tendency to drift which required my
 continued -- for minor corrections - although I sup-
 pose if you let it go it really wouldn't have
 mattered. But it just didn't stay for fine correc-
 tions. It had a tendency to drift
- Pilot B: It's nice and smooth around neutral and so forth. I
 4.5 still get that rapid force build-up as I go out
 (K = .3) laterally in order to get anything to happen. I don't
 much care for that.

HF126

Pilot B: It feels much more comfortable. I don't know what, I
4 can't honestly tell you why. It still has the high
(K = .3) force build-up as you go out in bank angle, but every-
thing else in between seems to be smoother and more
responsive. It's much more comfortable.

Pilot A: Sensitivity is good, gain is good. I got good control
3 feel and the airplane does go where I want it to go.
(K = .3) I get the feeling it may be a very small lag in there.
Rate build-up is good and appropriate to the task. I
feel I've got good control over it. However, there is
something in there that I'm not really sure what it is
that bothers me a little bit; however, I can do the
task. I don't really feel I get any problems close to
the ground.

HF217

Pilot A: The dynamics are quite good, it's predictable. It
3 goes where you want to. It seems I see a little bit
(K = .3) of a second response. It's almost like there's an
under damped mode in there someplace. I can't really
sort it out. I don't have any problems making the
airplane go where I want to but there's something in
there that's getting to me. I can sure make it do
what I want to but it's got something I don't like.

Pilot C: It's responsive to my inputs, I easily corrected the
5 gust, wasn't over responsive. I felt like I was in
(K = .3) full control and if I'm gonna put this thing down in
200 foot tall pine trees, which I've done many times,
it's reasonable. Of the ones that I've seen so far.
Well, what I saw was for small corrections and easy
corrections it was reasonable, when I made an input I
got what I was after. If I made large corrections it
took a little more of an input than what I am used to
but I don't think you are going to be horsing around
like that.

HF224

Pilot B: The thing over corrected and it's coming back and
5 I can't stop that. It's a lot more comfortable. You
(K = .3) really got some sudden changes here, but I just, as
long as I don't move it much, it's alright. It's like
a little bit of large motion in it and you tend to
over correct back the other way.

Pilot A: Yes I could get into trouble with this one, couldn't
7 I? That one comes close to being a little bit under-
(K = .3) damped. I've got almost a continual oscillation. I
think there's some lags in the response. I can easily
couple into the motion. I got into a lateral PIO
there for a few seconds. I lost a lot of altitude. I
don't like that one worth a darn. That does require
improvement if you get close to the ground.

Pilot A: We've got very, very PIO prone configuration, lots of
8 lag, no fun to fly at all. I think this would be
(K = .3) potentially disastrous. Got at least one crash out
of it. Controllability is definitely a question. You
have to back away from the task, because as soon as
you go to a high gain activity, you couple in and get
out of phase and it's bang-bang, back to back 180°
rolls and the whole smear. Major deficiencies
definitely. Pilot compensation is required for
control, but I guess I wouldn't say it's intense as
long as I remember to keep it slow. I can almost do
the job.

HF225

Pilot A: My perception is that damping is down, but what I
7 think it is, is you've got another damped mode in
(K = .3) there someplace. I think that if I was at a lower
altitude, I could couple into that one quite easily
and get into a lateral PIO. I am noticing in at least
one oscillation sometimes two oscillation on every
stick input. I don't like it, deficiencies do warrant
an improvement.

Pilot C: I don't like this one at all. It has a tendency to
7 PIO. Any large movements manifest themselves with
(K = .3) overshoots, laterally, both with and without the
gusts. It just sat there and you are just moving that
stick all day long and you don't need it.

Pilot B: This thing has a tendency to rebound each time I roll,
8 put the stick position in and it goes over and bounces
(K = .3) back. Well as you can see, I get out of phase with it
a little bit and start oscillating back and forth and
I'm not doing that deliberately.

HF226

- Pilot B: 5.5
(K = .3) All I wanted to do is just hover, not make any big motions here. It would be alright, but as soon as I start to make motion laterally, then I discover that the thing is much too sensitive and it seems to be very nice just right around neutral and then it seems to gain response very, very quickly and I wind up oscillating a little bit. It's not comfortable.
- Pilot A: 6
(K = .3) That one has still got a fairly sensitive response when it takes off, so I got to try and stay up with it and I think there's some kind of lag in it. I find out what I'm noticing most is when I put a control input in, I get a rebound, it's over to some angle, comes back and sits there and oscillates there a little bit and I think I could couple into; the fact that I did couple into it a couple times and I was never really sure if the airplane was doing its own thing or if I was driving it. I think I can get into a PIO on this one in a hurry. I'm never really sure if the airplane is doing something or if I'm doing something. I got to wait in order for it to settle down before I can make a correction. I could get into a PIO, but I'm sure the wind wasn't inductive, but it was me. So, I guess as far as I'm concerned, it has major deficiencies. I could stay somewhere in the vicinity of what I wanted. I can stay about where I want to, but I really got to stay on top of it. I think if I got close proximity to the ground, I'd have to go a 7.
- Pilot A: 6
(K = .3) I don't think I like it very much. I can't notice any real lags in response but what I do notice mostly and object to is a secondary response. It seems poorly damped. I don't know if it's the primary or if there's another mode in there that I get some oscillation out of, so therefore, when I start getting into an activity where I'm pacing it with a stick, I never really know where the airplane is at, how far it is behind my input. The airplane is quite PIO prone. I have to make a conscious effort not to chase it to avoid a PIO. If I keep my control inputs down, I can do a reasonable job. The problem with that is, that I can get what I consider to be adequate performance, as long as I really stay on top of it. The airplane is quite PIO prone....the PIO sensitivity would be very bad on a PIO scale. In a high gain task like landing, I think I would be very seriously concerned about controllability.

HF227

- Pilot A: 5
(K = .3) The frequency content seems different. I don't think I'd couple into this one. I am getting some rebound. In other words, I put a step in and I'll get say 20° of mag then five of it will roll off. It's not, I don't perceive it as a damping phenomenon so much as something like rebound. A second stage in there. It's a nuisance, but it, I don't think I'd couple onto it, so I guess I'd have to say that's a moderately objectionable deficiency.
- Pilot C: 6
(K = .3) It is not very good in gusts. You put it in and it wants to come back out, and you put it in and it wants to come back out. However, out of gust it seems to be a little more sensitive than I prefer. But once you get it all sorted out, it will stay there or it did for me anyway in both cases. It is reasonable I guess.
- Pilot B: 6
(K = .3) I cannot find the bank angle I want. It goes further than I expect it to each time I move the stick. It's just not following me. There's too much lag. I'm not comfortable with it.
- Pilot A: 6
(K = .3) It's oscillatory with a lag; however, the response rate is down far enough on this one that I don't have the tendency to couple into it. Controllability is not a question in this case; however, adequate performance, I can get it. I'm not real wild about the oscillations in there. What we've got is objectionable, but tolerable deficiencies. I can get adequate performance, but not desired performance out of it.
- Pilot A: 6
(K = .3)
 $Y_v = -.2$ The airplane has got some PIO tendencies. I think I could couple into it under some circumstances. It's not as easy as some I've seen to couple into, but PIO is definitely lurking around the corner. There's an oscillatory mode in there. Therefore, predictability is non-existent. You put the stick over and you're never quite sure where it's going to stop. Everything is over and done with fairly rapidly and you can make a reasonable size correction, you can't make the small precision corrections you'd like to make. If you do, you're in a constantly oscillating situation, so I'll have to put it in the category of very objectionable, but tolerable deficiencies.

HF228

- Pilot A: 8
(K = .3) Wasn't a question of losing control, because there was a question of whether or not I ever had control. The problem is that you got a distinct two stage response that comes across as either being low in damping or having an overshoot, plus a roll back, plus a time delay. The pilot stands a very good chance of coupling into that particular combination and getting into a totally wild PIO situation. I didn't quite, but I could see very easily that I could have. I don't like this configuration worth a darn. It's definitely Level 3. Is controllability in question? Well, yeah, I guess it is in my mind. Controllability is in question.
- Pilot A: 4
(K = .3) I guess I see a little bit of secondary response here, like somewhat under damped. Get a little bit of oscillation sometimes on control input that's a minor nuisance.
- Pilot A: 4
(K = .3) Get what looks like a bit of a secondary response in there. Sensitivity is fairly good. Rate onset is fairly high. I don't think this is a real, real fast rate or maybe there's something else buried in there I'm almost but not quite having a display flicker problem out there. It's certainly controllable, however, there's that quirk. You put the stick over and the airplane banks over and seems to roll back about 20%, so it's got a quirk in there that I'm not real wild about, but I can certainly get the job done. It's just a matter of adapting a little bit to it. I'd have to say that I've got to compensate and remember that roll back's in there and I'm not real wild about the rate of onset and what have you. The problem as I say is a moderately objectionable or a minor deficiency. I think I can get the job done.
- Pilot A: 6
(K = .3) The airplane has got some PIO tendencies. It seems to be oscillatory with a bit of a lag. Therefore, I wind up on corrections usually oscillating my way through them and chasing it. However, I don't really tend to couple into it for large amplitude maneuvers. I can induce them, but I back right out. It's not a sustaining type phenomenon, but in the process of making corrections, I do get some oscillation in bank angle that I don't like, so I guess I'll have to put this in the category of moderately - well it's a very objectionable deficiency, but it's certainly tolerable. You can get adequate performance, but you can't make the desired small corrections.

HF229

Pilot A: I'm not quite sure what it is I've got here. I think
 5 there's a bit of lag or a mid-frequency secondary
 (K = .3) response or something in there. What it translates to
 is, I can't all the time predict exactly what I want
 to get. Sometimes it comes across as a rebound, some-
 times I don't quite get what I wanted. It depends a
 little bit on how I put the inputs in. The response
 is fairly brisk. Sensitivity is fair. The problem is
 predictability, so it comes across to me as an
 objectionable deficiency.

Pilot A: I got fair sensitivity, very rapid roll response,
 4 coupled with a modest transport lag. It's a little
 (K = .3) disconcerting sometimes to be able to spike the stick
 - then watch the airplane spike with a modest amount
 of delay in there. From the time you perceive that a
 correction is necessary and move the stick and the
 airplane gets there, that amount of time is appropri-
 ate to be able to make the desired small corrections.
 However, what you've got is a lag followed by a fairly
 hefty roll acceleration. As long as you put the stick
 in the right place, in the first place, you're
 alright. You make the desired corrections, but I
 don't like it. I will put it in the category of
 minor, but annoying deficiencies, because I do have to
 compensate a little bit and be right in the first
 place. However, I can get the desired performance.

Pilot A: That's a pretty good configuration. Also, I can
 3 notice minor hesitation in the onset, but the combina-
 (K = .3) tion of sensitivity and rate and everything else makes
 it a minor nuisance. I can get the job done with a
 normal amount of compensation. It's a quirk, I don't
 like about it, but all told, it's pretty good
 configuration.

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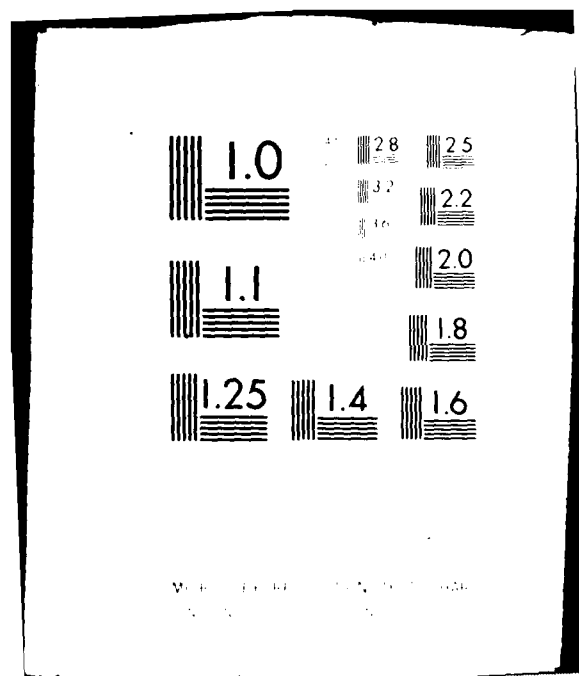
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HF220

Pilot A:

4

(K = .3)

The problem is that there seems to be something else in there other than the basic airplane. To a moderate large input, I get the bank angle, and then I get some roll back. I put the stick over and I might get my initial goal of 30° and then roll back to 20 say. Now, that can get to be a problem on some inputs, because about the time I perceive that it went further than I want to, I take the stick out, then it comes out, then I get into an oscillation situation. However, the majority of the time, the response is considerably more rapid than I am putting my average input in, so therefore, it sort of takes care of itself and I don't tend to couple into it. I can control the airplane, but I've got to remember what I'm doing, so I've got to definitely compensate for that additional mode in there. I think if the frequency of the whole thing was slowed down just a little bit to make it more compatible with the way I'm putting my inputs in, I think I could get into a PIO situation in a hurry. However, with this particular configuration, I don't have the PIO problem. I'm going to have to say though, that flying the airplane does require the pilot to remember what he's doing, make a conscious effort to let the airplane go ahead and roll back before he makes the second correction, so it requires somewhere between moderate and considerable pilot compensation, but I can certainly get the job done.

Pilot A:

8

(K = .3)

Well, that's what you might call a close encounter of the pilot induced kind, as you might notice from your strip charts. You've got the worse of several combinations. I see you've got that very rapid response coupled by a lag that is at least, for my pilot patterns, a PIO inducer. In other words, it is very easy for me to couple in and get 180° out of phase of the airplane. I can do it easily and repeatedly, rather amazing how easy it is to get into that. However, I can back out of it by just slowing down my inputs, because the airplane is so blindingly fast in response, you can damp the oscillation out by getting out of the loop. It's not a controllability problem that you wind up in some wierd attitude. It's when you go to a high gain task, it's quite easy to get out of phase of the airplane. However, because the thing's so blindingly fast, you can back out and make it do what you want to. It's rather an unusual situation. Well, I guess I'd have to say that at least for

HF220

my pilot technique for that configuration, there is the controllability question and hedge it by saying I can back out of it, but there are times you get into that situation in close to the ground, in close to an obstacle, where you can't back out of it right away. There you've got a controllability question hanging around the corner on this configuration that could prove disastrous under some circumstances. There's very definitely PIO problems.

Pilot A: It's an almost very good configuration, although I
3 occasionally get some oscillation in the response,
(K = .3) which takes it away from a 2. I'll have to say it's
got some mildly unpleasant deficiencies.

HF221

Pilot A: I don't like it worth a darn. I'm not sure exactly
 7 what you've done there, but there is a mode that I
 (K = .3) got into at least twice, maybe three times, that is a
 moderate frequency - very sharp PIO mode, but it's a
 very sharp frequency band. It seems to be mostly for
 small inputs around neutral in the mid-frequency range
 I get an oscillation. Larger inputs it's okay. It
 seems to be maybe a slight delay and then an oscilla-
 tion, and for very rapid inputs, it's okay because it
 sort of ignores them, but I find this mode in there
 that I can couple into and get into a PIO situation
 which I don't like. I'm not real wild about the
 overall response of the airplane and because of the
 problem of coupling into that PIO and I don't quite
 understand how I do it all the time, I'd have to say
 you've got major deficiencies in the airplane that
 under some circumstances at least, I can't get what I
 consider adequate performance, because I get into that
 oscillation mode.

Pilot A: Sensitivity is good. The response is quite brisk. I
 4 do sense that there's something in there that's inter-
 (K = .3) ferring with reliability, to predict exactly where
 it's going to go, but I can't really sort it out with
 the small inputs I'm using. I'll say it's got a minor
 deficiency that I'm not real wild about. I can make
 it do what I want.

Pilot A: Everything sort of comes together on that one. It's a
 2 very pleasant configuration. It may be slightly brisk
 (K = .3) in a roll acceleration. You might get jostled around
 a little bit, but it does what you ask it to do
 quickly and precisely and with a minimum of fuss and
 bother.

Pilot A: I guess I perceive a bit of lag in the response on
 4 this. Rates - fair, sensitivity is fair. I can get
 (K = .3) the desired performance out of the machine, but I
 think you could get yourself into PIO situation
 occasionally with the vehicle. I'm not real wild
 about the dynamics; however, I can get the job done.

HF2T1

- Pilot A:
3
(K = .3) I think I could use a little bit more gain on that one; however, the response is quick. I think I would just like to see more bank angle per unit of stick deflection. Response is quick, but not too quick. Some mildly unpleasant deficiencies.
- Pilot C:
5
(K = .3) It is doing what you want it to do. I don't particularly care for it personally, that type of approach, I don't like the machine taking out something that I put in, but it is reasonable.
- Pilot B:
4.5
(K = .3) Around neutral and for small changes, it's quite comfortable, beyond that I get rapid stick force build-up and reduced response. It's comfortable as long as you don't try to do much with it.

HF2T2

Pilot B: I don't know what to say about that one. Some of it I
5 like and some of it I don't. I get the impression
(K = .3) that beyond about 10° of bank angle, maybe even 5°, I
really get a large stick force build-up before any
response that I get, but right around neutral, it's a
little bit sensitive, but it's extremely damped. I
don't have the tendency to oscillate that I had on
some of the others. It's great in the absolute hover,
but any maneuvering is bad. Can't predict it, it's
just too big a change.

Pilot A: That's nice. That one's quite pleasant. It goes
2 where I want it to go. It doesn't get there too
(K = .3) rapidly, the gain seemed about right. I can find
myself trying to make, well, easily making two axis
corrections and not having an awful lot of difficulty
with three axis simultaneous corrections, which means
that workload is down in lateral axis. It's good,
negligible deficiencies.

Pilot A: How sweet it is. The airplane might be a shade
3 sensitive, but it certainly goes where you want it to
(K = .3) go with a minimum of effort.

HF2T3

Pilot B: I can do a pretty good job of hovering it, it responds
5 smoothly around neutral, but at the same time, I wind
(K = .3) up moving it in little steps. Don't quite understand
what's going on, cause I really have to be careful
when I move the stick, otherwise it tends to be moved
in jerky steps.

Pilot A: I think the airplane goes where I want it to go. It's
3 not overly sensitive. The sensitivity is about what I
(K = .3) like. It might be a little bit rapid, but not bad. I
don't notice any glitches in the response, maybe
there's a little secondary oscillation, but it might
be just a display flickering on me. I can make the
airplane do what I want to, I can make a multi-axis
correction. Therefore, it's imminently controllable.
I really don't see anything in there I object to
horribly, so I have to say minimal pilot compensation
is required.

HF2T4

Pilot B: A little bit of wind I'll let it drift over the center-
 6.5 line. Don't want to drift that far, okay we'll come
 (K = .3) back. Quite controllable laterally. Within strictly
 in the hover, there is a limit to the bank angle. I'm
 not sure why it's being limited or if you want it to
 be limited. I can't get the bank angles I want. The
 thing just stops and of course, that would be an
 unacceptable operational condition.

Pilot A: I now have got a lag in the response. The airplane is
 5 a little bit more sensitive than I think I would enjoy
 (K = .3) flying in flight. With the lag in the response, I
 think the lag and then the jump in the outside display
 is even more distracting in this case. I can get
 reasonably good performance as long as I remember to
 lean and stay backed away from it a little bit and not
 try and get too tense about staying right on top of
 the airplane. I don't see any PIO tendencies. I'm
 not sure I want to call that a desired performance. I
 can certainly get adequate performance out of it.

Pilot A: My major perception there is a mid-size lag in the
 5 response. It presents a problem in responding to a
 (K = .3) rapidly changing situation in that I have to wind up
 over correcting. However, the overall response to the
 airplane is precise, so although I can't get the
 immediate precision control I want under all circum-
 stances, I can certainly do the task adequately, so
 I'm going to back down to the moderate, or minor to
 moderately annoying deficiencies. I'm not real wild
 about the lag in the response. It's not so much
 really, a matter of pilot compensation, it's just I
 wind up having to use more control than I really like
 under some circumstances. You have to stay on top of
 it certainly.

Pilot A: The major problem here is a noticeable lag in the
 5 response. Sensitivity is good, response may be a
 (K = .3) shade on the brisk side. The lag is enough that you
 notice it and don't have the problem we have with the
 other configuration of coupling into it. It forces
 you to change your pilot technique and since you can't
 get the very small corrections and instantaneously you
 certainly can't get what you would call desired per-
 formance for small corrections. You can certainly
 make the airplane go very rapidly where you want to,
 as long as you wait for that small onset, lag and
 onset.

HF2T4

Pilot A: A little puzzling. There's lag in the response. The
5 rates of onset and what have you are fairly decent.
(K = .3) Sensitivity is good. All told, I can make reasonably
 $Y_v = -.2$ small corrections, but I'm forced to a difference mode
of operation that I would prefer. I go to a bang-bang
reaction, always reacting rather than a smooth continuous
input. I'm just trying to more or less trial and
error, hunt and peck on the amount of bank angle
required. I'm forced to adapt to the airplane. I
can't really get the precise small corrections I'd
like, but I can get better performance out of it than
I would have expected. I guess I'd have to say I
can't get the immediate small corrections I want and
I'm forced to change my strategy.

HF2T5

Pilot A: Sensitivity and such like things are pretty nice.
6 You've got an intermediate lag here. That means it's
(K = .3) not on the nuisance category, but it's not a disaster
either. Let me philosophize on that a bit; the lag
that we have in this case, is perceptible, and forces
the pilot to change his normal control strategy. If
the lag was a slight bit less, I think there would be
a PIO possibility of the pilot coupling into it by
trying to obtain performance that he just couldn't
get. In this case, it's blatantly obviously that the
airplane is not going to respond instantaneously and
the pilot just has to go to sort of a bang-bang
strategy and when he wants to make a correction, he
just tries something and waits a few seconds and sees
if that was enough and if not, he puts it in again.
So, he's in a bang-bang reaction, always reacting.
Cut and fit, trial and error, whatever you want to
call it. Certainly not the desired way to want to fly
the airplane. I cannot get adequate performance, but
I've got to think about it. I can't make the airplane
react fast enough to instantaneously stop that drift,
it's just not there. But, if I allow myself to loosen
up on the task a little bit and say that stopping the
drift instantaneously would be what I desired to do
and stopping it not quite so instantaneously would be
adequate. Well that's what I'm getting.

Pilot A: We've got a distinct noticeable lag. My impression is
6 it's a little bit longer than would be necessary to
(K = .3) couple into. In other words, I've got no problem at
all determining it is there. There is a possibility
that I could find myself in some task where I'd couple
into it. However, I tried to get into it a couple
times and I just back right out of it immediately, so
there as no real problem. However, the lag is severe
enough that you definitely can't get the response you
want out of the airplane. The question in my mind is,
can you get adequate response. Well, that's border-
line. The possibility exists that if that lag got
anymore perceptible, or slightly less perceptible, in
other words, you could couple into it and get into a
PIO situation.

HF2T6

Pilot A: 8
(K = .3) There does exist a possibility coupling into this one, it's fairly brisk response with a lag and I think a pilot could very easily get himself coupled into it, and so borderline lose control of the airplane. I can't certainly, get the desired performance. I'm not even sure I can get adequate performance. Controllability begins to rear its ugly head a little bit here, because I think the possibility exist for a PIO. I think you've got a very distinctly PIO prone platform here.

Pilot A: 5
(K = .3) Sensitivity is good. Response rate is okay, however, there is a lag in the response that interferes with reliability to precisely control the machine. It's not a big problem on the small inputs that I put in fairly slowly, but it does lead to a little bit of overshoot additional bank angle required, so I can't really get my desired performance; certainly get adequate performance. Again, with small inputs, it's hard to tell if I'd couple into it if I really got intense, but trying to maintain the altitude control sort of leads you to have to make small lateral corrections.

Pilot A: 5
(K = .3) Well, that's interesting. I got about the same dynamics that as I had before, fairly very brisk response, high sensitivity and the whole smear. However, there is a substantial time delay involved, so you don't really perceive it as that instant bank angle and to a certain extent, it's almost more flyable than the previous configuration. So, I would be tempted to say it's a better airplane, because the major way that comes across to me is, I don't, I'm not tempted to change my control strategy. It comes across as being a slightly softer response. On the other hand, I think you could quickly get into trouble with that much lag, so although it doesn't impact the way I fly the airplane like the previous configuration did, I'd have to hedge and say that in addition to the blinding fast response in getting coupled into it, it flickers and what have you, that would be uncomfortable in the real airplane. I think I'd have to say that you could probably get into trouble with this because of the delay involved.

HF2T7

Pilot A: Controllability rears it's ugly head. I guess I'll
8 have to say that I wasn't losing control and so there-
(K = .3) fore, it's not intense, it's borderline with that much
lag, you could very rapidly get into a very bad PIO
situation. I do have some question about the
controllability of it.

Pilot A: There is enough lag in that configuration to present a
9 major problem. I question if I'm really in control of
(K = .3) the vehicle at sometimes. I didn't crash. I didn't
lose control, but I sure couldn't make it do what I
wanted. Getting down close to the ground, I was in a
continual large amplitude bank to bank oscillation. I
have to stay on top of it and back away from it and
lead all the inputs to avoid getting out of phase and
into an oscillation. In close to the ground, I don't
think I can even do that, so if the task was say a
landing with any external disturbance, I think it
would have been a 10. I don't think I could have
landed the machine.

LF221

Pilot A: The lateral response is a little sharper. It goes
 3 where I want it to go. The gradient's good, gain is
(K = .3) good. It might just be a little sharper in the
 response. I'm not quite sure. It seems like I've
 been having a little more trouble with it than I did
 the previous configuration. There's just something in
 there I can't put my finger on, but I'm not having any
 real trouble with it.

LF223

Pilot C: What I'm simulating in the rapid movement just for
 8 your info, I'll go ahead and talk my way through this
(K = .3) one. What I've been doing is many times in Harriers,
 you'll come into a runway and you'll come over the
 middle and you have a wingman behind you and then
 you'll have to translate very rapidly from one side to
 the other. It's not uncommon to make a big input to
 get over there quickly, because he's probably minfuel,
 you're minfuel and he's got to have a place to land
 also. Then once I get past that, I'm trying to fine
 tune a spot to land and simulate coming down on a
 taxiway while my other three wingmen are landing
 behind me on the right, left, etc. I can't control
 it. It's totally unsafe, there's too much work.

Pilot A: There's something in there that I don't like. Some
 4 kind of additional response it seems like. I don't
(K = .3) see any perceptible lags. I still think rate onset is
 a little rapid. I have some difficulty sorting out
 what it is there that I like. There is something in
 there that's a nuisance. It goes where I want it to,
 but I'm having more trouble with it than I think I
 should. Requires moderate pilot compensation and I'm
 not quite sure why.

LF225

Pilot A: Wow. Let's see, I hit the stops a couple times on
 6 that, so I'm not getting any the full response that I
(K = .3) would like. Rate build-up was quick. I don't feel
 that I have enough control over it. I've got using
 too much stick to get the bank angle, bank angle was
 just really rapid. Might be a small lag in build-up,
 but I can't really tell. I get the feeling I'm not
 totally in control of the aircraft. To me, that it
 comes across as a very objectionable but tolerable
 deficiency. I can almost make it do what I want to,
 but I sure don't like it.

LF227

Pilot A: Just a little bit of rebound. I'm getting a little bit
6 of rebound on the rapid input. It gets over to a bank
(K = .3) angle and rolls out a little bit. It's not really in
oscillation, cause it just goes over then comes back a
little bit. It's a trifle unpredictable in that
characteristic. I think there might be some lag in
it. Also, the response is quite rapid when it comes
on. I find myself working harder than I think I
should. I think I could get in trouble with that if I
got down to a low altitude and got into a real
precision task.

LF221*

Pilot B: The roll force build-up is way too high, once you get
 5 past a little bit of roll and it tends to be, don't
(K = .3) want to damp itself out very hard, but as far as
 actually maintaining the position, the response is
 good enough and it wants to hold itself there.

G120

Pilot A: Adequate performance is not attainable but controllability is not a factor. You just don't have any.
7
(K = .2) Adequate performance is not attainable. It just is not there. You do not have sufficient gains or authority whatever you want to call it. Put it all the way over to the stop and continue to blow across the runway. However, because it is so unresponsive, it's not a matter of controllability becoming in question. You don't get into the PIO problems; loss of control. It just doesn't do what you want it to do. You're not going to get into serious loss of control problems, you just do not have sufficient control.

Pilot A: Your problem here is the gain is way down. You've got the worst of several thing going. I say it's controllable, but it's certainly not adequate.
7
(K = .2)

G121

- Pilot A: I think the underlying dynamics are good. It feels to
4 me like the gain's down, I don't have the control
(K = .2) response I've been seeing before by a long shot. I
don't notice any lags. The airplane is a shade on the
sluggish side, but the response comes on pretty quick.
It just seems like I don't really have enough lateral
control power and that if the wind was any stiffer,
I'd run out. However, with the wind conditions that
we've got, I've got adequate control margin. I wish
it had more sensitivity. I can get the desired
performance out of it, but I have to compensate.
- Pilot B: That's lousy. Very, very big lag in it. Very sluggish.
7 It takes lots of stick to roll it. I'm finding myself
(K = .2) putting in big leads here trying to get it where I
want it. I can't make it do what I want to do,
because there's too much lag.
- Pilot A: The response is down, sluggish and I'm not gonna feel
7 I'm getting enough sensitivity. I can't do what I
(K = .2) consider an adequate job. The controllability is not
in question.
- Pilot A: I just do not have sufficient lateral control to stop
7 the drift. I've almost got enough, but not quite.
(K = .2)

G123

Pilot A: It's pleasant as long as you don't have any wind on.
7 I do not have enough response, so not only do I not
(K = .2) have enough response, what I do have, I don't get fast
enough. Therefore, I can no longer get adequate
performance. There is a controllability problem
because of a large lag.

Pilot A: I can almost stop the drift. I just have to put in
7 more work than I really think is necessary, so that
(K = .2) takes it out of the class of tolerable deficiencies.
I have to give it a major deficiency even though I
can't stop the drift. I guess it's semi-adequate, but
at an intolerable pilot workload as far as I'm
concerned.

G180

Pilot A: If anything, it's a shade too responsive laterally. I
2 get a little bit of oscillation right around neutral.
(K = .8) I don't know if it's stick sensitivity or the rate of
bank angle onset. However, that's a very, very minor
objection. The airplane follows quickly and
precisely. As I said before, if anything it might be
just a shade too rapid, but I can certainly make it go
where I want and make it do what I want. I sort of
like the configuration.

Pilot A: That's puzzling configuration. I don't quite know
4 what's in there, but what comes across to me is a
(K = .8) combination of a not very brisk airframe, with a very
high stick sensitivity. I seem to be not in a PIO
situation, but I'm constantly exciting a small wing
rock type phenomenon. That's reasonably predictable
and the sensitivity is reasonable, I can make it do
pretty much what I want to, it's just got something in
there that's annoying to me, so I have to say it's got
a minor deficiency. You've got sufficient control
authority of this configuration to get yourself in
trouble if you really tried. Well, you can do that
with anything, so I'll say as far as I'm concerned,
I've got to compensate for the configuration, but I
think I can get the job done.

G185

Pilot A: The problem here is we keep shifting sensitivity
 4 scales more or less. We've got very, very responsive
 (K = .8) airplane and like I said before, we may have too much
 attainable response for an attitude command system.
 However, in this case, it's combined with just a
 barely perceptible lag, so I never really got any
 oscillation problems or PIO, so I don't think there's
 anything lurking in the weeds. I can more or less
 quickly and precisely make the airplane go where I
 want, but I will say that it does have a bit too much
 attainable response and maybe either mid frequency
 effect or a bit of a lag or something in there that's
 an annoyance superimposed. I'll have to say I can get
 the desired performance if I compensate for it, but
 it's got some annoying deficiencies.

Pilot A: It's almost good. However, it's a totally different
 4 class of dynamics. Response is much more brisk.
 (K = .8) Sensitivity is considerably higher. I don't quite
 know what is annoying me about it. It might be a
 minor lag, or something at high frequency. I don't
 quite know. I have difficulty with small, very small
 corrections, because for very small stick inputs I
 guess I'm getting surprised a little bit about how
 much response I'm getting, so I'm having some problems
 around neutral. Maybe it's a slight response lag.
 Maybe it's just a pilot technique. Almost a pretty
 good airplane. It's in a minor but annoying category.

G188

Pilot A: That's about what I want to see. Sensitivity is good,
2 harmony is good, no perceptible lags, everything just
(K = .8) sort of came together.

Pilot A: I guess I'd say that I think in flight the sensitivity
2 might be a little bit high. I think you'd be in a
(K = .8) constant little bit of wing walk on touchdown, because
of the sensitivity problem. However, as far as the
simulator task goes, oh man, it's nice. Light control
pressures and instantly answers the helm. No delays
and what have you. It was very pleasant in the
simulator. Hedging the possibility of being too
sensitive in flight.

G181

Pilot A: 6
(K = .8) You got a combination here which could present some problems under some conditions. You've got a very high bank angle capability, probably too high for an altitude control system, combined with some lags in response. On the first run on this one, I got myself into a fairly large amplitude PIO, bank to bank type thing for several oscillations. In close to the ground, it would have been utterly disastrous. Now, keeping in mind that you can get in trouble on any machine, on the other runs by backing away from it, I didn't particularly have that PIO problem. What I came across is noticing primarily the lag in response. So, making due allowance for the response character of the dynamics, you can compensate for the potential problem; however, it's lurking in the corner, so I'll have to say that adequate performance requires considerable pilot compensation. It certainly doesn't have a desired characteristic there. It might even have to say extensive pilot compensation. I does have the potential for disaster.

Pilot A: 5
(K = .8) You've definitely got too much sensitivity in bank angle per stick deflection, for an attitude command system, I get the feeling I could do an aileron roll on this. This would be interesting if I stopped half way around. What that translates to is I have trouble making small corrections... Go over there and hold it there for a second, you're going to lose control of the vehicle. So, you read the warning, don't put stick over to side of cockpit and you'll be alright on not losing control. I think you've definitely got too much sensitivity. I do have trouble making the small corrections, however, I can get them done. I get what I consider adequate performance, but not the desired performance.

G110

Pilot A: There's something in here that bothers me a little bit.
 3 I don't know quite what it is. It goes where I want
(K = 1.0) it to go. I don't have a whole lot of trouble with
 it. There's something in there that's annoying me.

Pilot A: Piece of cake. Gee, I like that. That HUD just went
 2 up to full brightness. (The HUD brightness increased
(K = 1.0) during this particular run. HUD brightness was con-
 stant for all other runs.) I think that was distract-
 ing me a little bit during that run. It goes where I
 want it to go with a minimal of effort. It's
 absolutely a Level 1 airplane. I can't really put my
 finger on anything that I object to.

Pilot A: I don't have any trouble getting the job done and it
 3 does what I want it to do. It might be a little soft
(K = 1.0) in there.

Pilot A: No problem with harmony. The airplane does what you
 2 tell it. Sensitivity is good and appropriate to the
(K = 1.0) task. I have no problem making it do exactly what I
 want and I have to really look to even get a suspicion
 of the lag, so it doesn't really bother me at all.

G111

Pilot A: Just in precision, I sort of got to hunt and peck for
6 it. The biggest problem I have is the inprecision in
(K = 1.0) control. If that's something like time delay, I would
say you're bordering on the ragged edge of a bad
rating. It wouldn't have to get very much worse
before I would have not very great difficulties with
it. Adequate performance is I think attainable, but
you got to really work for it.

Pilot A: We've got a very rapid response with - you know it's
6 a rate, with a lag in there. Fairly high sensitivity,
(K = 1.0) the combination makes the aircraft PIO prone. Because
of the sensitivity, I find myself constantly over
correcting small inputs. In other words, getting more
response than I thought I was going to get and having
to take it out, so I get into an oscillation. If you
ever get into a large amplitude maneuver, you've got a
very PIO prone configuration, because you can couple
right into it immediately. I can get the job done as
long as I'm very, very careful about what I'm doing.
There is some controllability possibilities or some
PIO possibilities lurking around the corner.

G112

Pilot B: I can't even figure that one out. I'm working hard
6 trying to get things settled down. I haven't gotten
(K = 1.0) what I would consider adequate performance out of it.

Pilot A: Very definitely PIO prone configuration. On the first
8.5 run, I definitely got into a PIO that I had to just
(K = 1.0) sort to put the stick back in center and politely take
my hand off and wait for the thing to damp out, so
controllability was very definitely a factor in terms
of pilot compensation, yeah, I had to just get off the
stick. It was necessary to retain control; however, I
do not impact the ground. The second time at it,
realizing that was coming, there were a couple times
where I could see the PIO beginning to develop, but
just by backing away from it in a hurry, I could avoid
the control problem getting into a full blown PIO.

Pilot A: I've got major objections already. I'll make a couple
8 comments on that. If I really back away from it and
(K = 1.0) just consciously keep my inputs down, I can do a fair
job. I got to stay on top of it, because it's very
responsive and I think I can perceive some lags, so
what I mean is I have to consciously sneak up on it as
long as I keep my own inputs under control, I think I
could get the job done. However, I also have some
question about controllability on that one. If you
start getting intense, you couple right into it and
get into a PIO that you cannot get out of easily. So,
compensation as far as I'm concerned is required for
control. I've got to make a conscious effort to avoid
rapid inputs. If I don't, I immediately get into a
PIO that I really have trouble breaking.

G112

Pilot A: I got several things wrong with this configuration.
7 You got way too much sensitivity for a bank angle
(K = 1.0) command system. That combined with a lag, I think you
could easily wind yourself up in a major problem of
inadvertently putting in too much input, and winding
up in some horrendous bank angle before you could get
it out. The lag and the sensitivity and the response
and everything else makes the aircraft PIO prone. In
this case, I wasn't chasing a correction, it was just
a constant low amplitude bank to bank oscillation, may-
be 10° of bank. Very easy to fall right into. I
think the sensitivity problem is extreme. It definite-
ly requires improvement. That takes it out of the
ballpark of the Level 2. I think puts it in Level 3.
I'll say that you can get adequate performance as far
as the task goes. However, I think you've got way too
much sensitivity that could get you into a controlla-
bility problem in a hurry. Therefore, I think that
sensitivity absolutely requires improvement.

G113

Pilot A: Well if I back away from the control inputs, I don't
7 get that horrendous PIO I started with. There is a
(K = 1.0) bunch of things wrong with it. A very sharp response,
laggy, imprecise. I can't put it where I want it
exactly. I got to keep hunting for it, but of course
it answers the helm, fairly briskly. I can do it, but
I say it may be overly sensitive cause I sure got into
a PIO there initially. But again, I can get what I
would consider adequate performance, but I got to walk
on tippy toes to do it. There could be task so
defined as to excite that lateral PIO and controllabil-
ity would distinctly come into question, but I didn't
lose control and I could do the task.

Pilot B: It's deceptive. If you don't move the controls very
10 much, it's no problem, but boy once you get over a
(K = 1.0) little bit of bank angle, it suddenly seems to just
get all fuzzy. I could put the stick in the middle
and stop it, but I can't control it.

APPENDIX C

PILOT DATA

Very briefly, the pilots' background were as follows:

- Pilot A - Ex-military A-4 pilot, current in light aerobatic aircraft, some VSTOL and helicopter time. Current assignment as flying qualities engineer.
- Pilot B - MCAIR test pilot, extensive AV-8 V/STOL experience.
- Pilot C - MCAIR test pilot, extensive AV-8 V/STOL experience.
- Pilot D - Calspan research and engineering pilot, very extensive variable stability CTOL and V/STOL aircraft experience.

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