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author: S. Sergev

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20. Continued

As written, DECEL1 should be compilable on most Fortran IV compilers with Boolean algebra capabilities.

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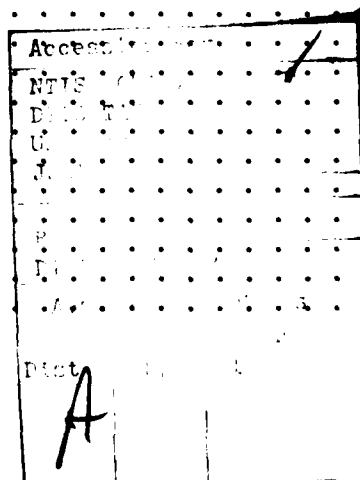
DECEL1 is a Fortran IV program for computing the ocean current-induced static deflections of undersea structural cable arrays. As dimensioned, the program can handle arbitrarily configured arrays of up to 22 cables. The cables can be electromechanical, wire rope, or synthetic. Any number of discrete devices (buoyancy elements, current meters, tensiometers, etc.) can be incorporated in the array. An option for parametric studies is included in the program, as is an option for incorporating arbitrary current fields. As written, DECEL1 should be compilable on most Fortran IV compilers with Boolean algebra capabilities.

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PREFACE

The Civil Engineering Laboratory (CEL), under sponsorship of the Naval Facilities Engineering Command, is engaged in a program of developing numerical tools for analyzing cable systems. As part of this work the NRL-written DESADE program has been used. In the course of using DESADE several improvements and additions have been made. The modifications are for the most part minor and serve to increase the accuracy of the mathematical modeling and to add user conveniences.

This report documents these modifications in the form of a revised users manual. (Much of the text of the original manual is used without modification.) To distinguish the updated program from the original NRL version, the program has been renamed DECEL1 for DESADE, CEL version one.

CEL's modifications were in five general areas:

1. Force calculations
2. Current field definition
3. Plotting options
4. Miscellaneous user conveniences
5. Iteration control

Force Calculations

Drag force and weight of cable sections covered by in-line devices have been deleted. (This assumes an in-line device that terminates the cable at each end of the device; floats that are in-line and envelope the cable must have their buoyancy adjusted by the weight of the enveloped cable segment.) This addition has a relatively minor effect except when in-line devices envelope a significant portion of a cable.

Calculation of tangential drag has been added to both cables and in-line devices.

Current Field Definition

The capability to accept a current field defined by 2, 3 or 4 current meter strings of up to 25 meters each has been added. Since much current meter data is referenced to magnetic north, the cable structure can be referenced to the current field by specifying the angle between the structure's X-axis and magnetic north.

The specification of current direction has been changed to be consistent with oceanographic terminology: a 90° current flows due east.

An option has been added to specify the input current velocity units; all velocities within an NDAT case must be the same units.

Plotting Options

Options have been added to plot the current field defined by two or more current meter strings and to plot the cable structure in either its deformed or undeformed configuration. Perspective or plan or elevation views can be depicted.

Miscellaneous User Conveniences

Required title cards have been added for the cable structure source deck and for each parametric case.

The specification of indexed and unindexed devices has been simplified. User selected devices now are automatically indexed, in order, by their location along a cable.

The changes allowed in a parametric study deck are such that the physical appearance of the array could be altered in the parametric case so much that referencing displacements to the original no-current case is illogical. An option has been added to declare any parametric case as the new no-current reference case. Displacements are printed referenced to both the original no-current case and to the present parametric reference case. The reference parametric case can be redefined any number of times since the original no current case is retained for the duration of the problem.

The error detection and display scheme has been altered. Errors that are detected by DECEL1 cause the entire input deck to be listed. Then, the cards with errors are flagged with a coded error number. The coded error message text is printed below the input card listing. All cards are scanned for errors; however, only the first error on a particular card is detected. The error messages are identical to those in the original DESADE manual except that only the portion of the message applicable to the card type is printed.

In some cases it is desirable to be able to punch on cards the locations of particular devices for input to other programs. An option has been added to select, based on device weight, the devices whose location is to be punched.

Iteration Control

Under some circumstances that have not been well defined, DECEL1 may either fail to converge or converge very slowly. To protect the user from high execution costs, iteration limits have been imposed. Iterative techniques are used to satisfy the imaginary reaction displacement constraints and to obtain the structure shape. Both iteration processes have had limits imposed because both have been the cause of excessively high execution costs.

These modifications have added to the capabilities of DECEL1 and have made it a more useful tool for the cable structure analyst.

INTRODUCTION

DECEL1 is a Fortran IV program for computing the ocean current-induced static deflections of undersea structural cable arrays. The solution algorithm is the Method of Imaginary Reactions (Refs 1,2)

combined with the method of successive approximations for treating position and configuration dependent forces (Refs 3,4).

As dimensioned, the program can handle arbitrarily configured arrays of up to 22 cables. The cables can be electromechanical, wire rope, or synthetic. Any number of discrete devices (buoyancy elements, current meters, tensiometers, etc.) may be incorporated in the array.

Certain limitations are placed on the structural characteristics of the arrays which can be analyzed by this program. These limitations are as follows:

1. No cables or cable segments may lie on the ocean floor. (No surface or bottom interaction is modeled, thus a cable may hang below the lowest anchor point.)
2. The dimensions of each discrete device must be small compared to overall array dimensions. Thus, for example, the application of this program to the analysis of an anchorage for a submerged submarine is not valid.
3. All parts of the array must be submerged. Thus, an array containing a surface buoy cannot be validly analyzed using this program. (The reason for this is that a surface buoy generates only one geometric constraint on its location.) An exception occurs when all three coordinates of a device on the surface can be specified - for example, the coordinates of a ship handling a crown line.

Also, certain hydromechanical assumptions are incorporated in the program as written. These are as follows:

1. The only hydrodynamic force considered to be acting on the discrete devices is a drag force. For in-line devices a normal drag coefficient and a tangential drag coefficient can be specified. For a free device, only the normal drag coefficient is to be specified. Lift forces are neglected as being small compared to the weight, buoyancy, and drag forces on these devices.
2. The only hydrodynamic force considered to be acting on the cable is a drag force. This drag force consists of both normal and tangential components and consequently two drag coefficients (normal and tangential) are to be specified for each cable.
3. The current option 1 is depth dependent in magnitude, unidirectional and horizontal. The current option 2 permits direction and magnitude variation as a function of depth. The current option 3 also permits magnitude and direction variation as a function of depth. This option requires two, three or four "strings" of depth dependent velocity data (where the strings are located at arbitrary points). These velocity data are used within the code via interpolation or extrapolation to obtain the velocity at any arbitrary point in space. In all cases the vertical component of velocity is assumed to be zero.

An option for parametric studies (changes in weights, diameters, cable lengths, anchor locations, etc.) is included in the program. DECEL1 also contains a series of error checks which insure that all input data are properly formulated.

Perspective plotting package SSP has been incorporated into DECEL1 to plot the deformed and/or undeformed configuration of the array.

The program uses the internally generated nodal points of the cables as the points to be plotted.

Scratch files 3, 4 and 10 must be available for use in the plotting package SSP.

Computer Requirements

As written, DECEL1 should be compilable on most Fortran IV compilers with Boolean algebra capabilities. Memory requirements for the program are approximately 206,000 (octal) words in single precision. Access to one, two, or three magnetic tape units, depending on the I/O options chosen, is required by the program.

Program Operation

The overall operation of the program DECEL1 is shown in the flow diagram in Figure 1. Numerical examples in Appendix A and the source language listing of the program is given in Appendix B.

Array Description

Typical cable arrays which can be analyzed using DECEL1 are shown in Figures 2a-2d. The figures also show the numbering and coordinate system conventions required for transmitting the array geometry to DECEL1. These conventions are as follows:

1. The cables comprising the array must be numbered consecutively from one to the total number of cables in the array (C1, C2, ... in Figure 2). Each cable so designated must have uniform properties (weight, drag coefficients, diameter, and constitutive relation) along its length. A change in property also requires a change in cable number as illustrated in Figure 2a.
2. The termination points of the cables in the array are called junctions. A junction may designate an anchor, the intersection point of two or more cables, or the free end of a cable such as illustrated by junction J9 in Figure 2c. The junctions must also be numbered consecutively from one to the total number of junctions in the array (J1, J2, ... in Figure 2).
3. A fixed, right-handed (X, Y, Z) Cartesian coordinate system must be chosen to describe the configuration of the array in space. This coordinate system is called the array-referenced coordinate system. The origin of the coordinate system can be arbitrarily located. The Z axis must be defined parallel to the direction of gravity and increasing upward. All distances are measured in feet.

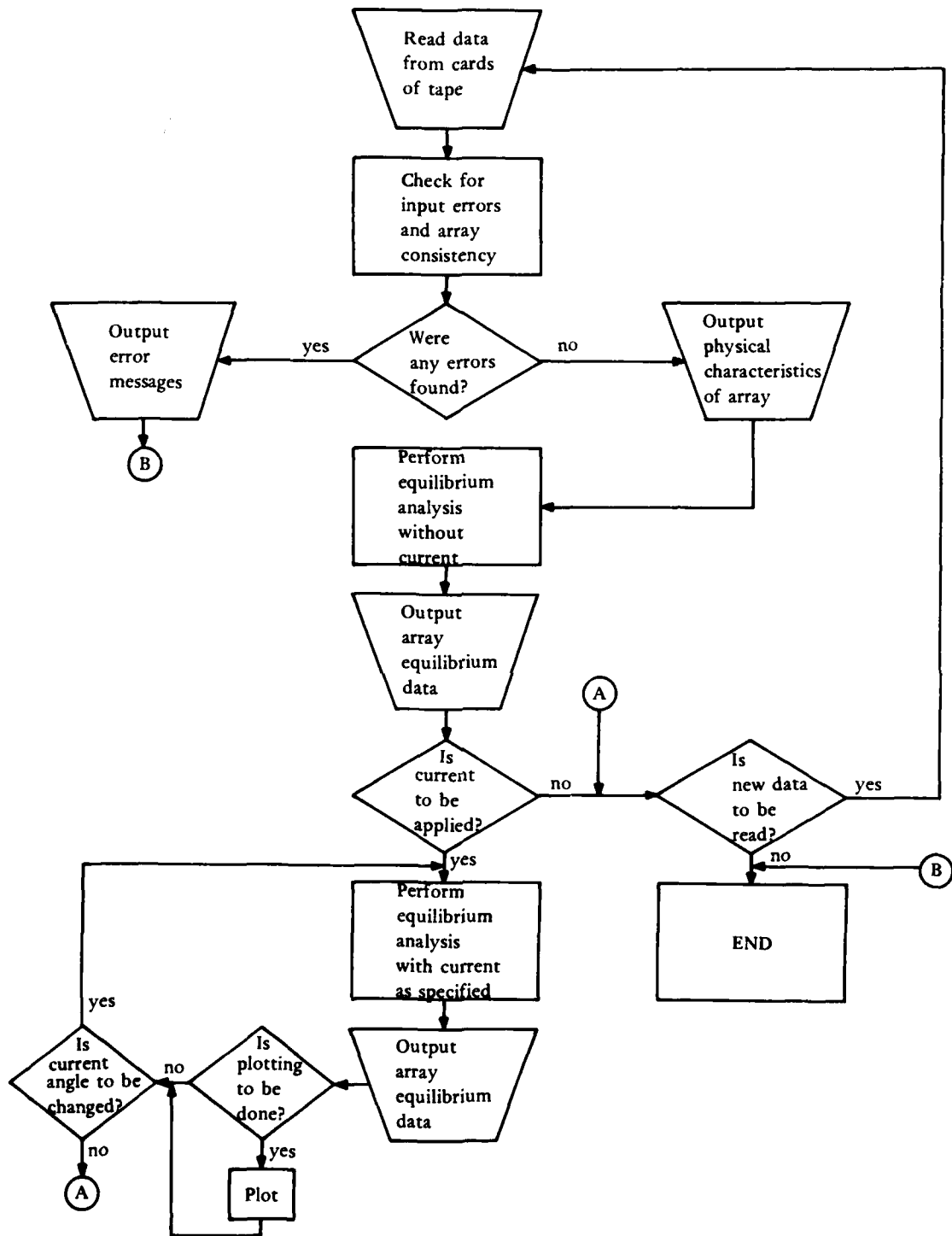


Figure 1. Generalized flow diagram of DECEL1 operation.

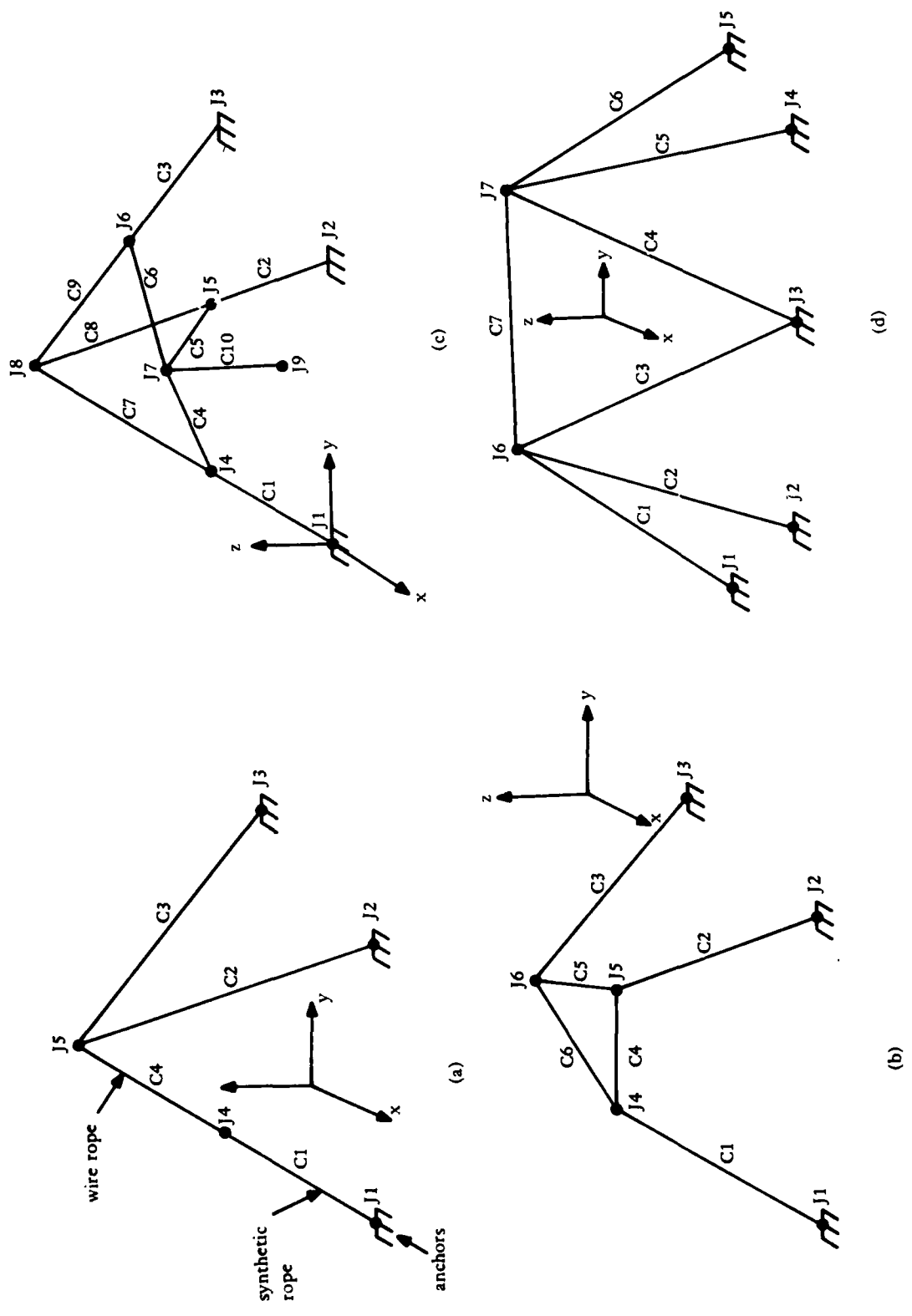


Figure 2. Typical cable arrays which can be analyzed using DECELL.

4. The junction numbers corresponding to anchors and the coordinate of the anchors must be tabulated according to the scheme illustrated in Table 1.

Table 1. Anchor Tabulation

<u>Column 1</u>	<u>Column 2</u>	<u>Column 3</u>	<u>Column 4</u>
Junction number of Anchor	X coordinate (ft)	Y coordinate (ft)	Z coordinate (ft)

Anchors are defined to be any fixed end point of a cable; thus an "anchor" can be placed on the bottom or at the surface or anywhere within the water column.

Reduction to a Statically Determinate Array

Before an arbitrary cable array can be analyzed by DECELL, a sufficient number of cuts must be made in the array to reduce it to a statically determinate structure. The effects of the constraints removed by these cuts are replaced by imaginary and equilibrating reactions (Refs 1,2).

The number of cuts required to reduce a cable array to a statically determinate structure is determined uniquely from the relation

$$\begin{aligned} \text{number of cuts} &= \text{number of cables} + \text{number of anchors} \\ &\quad - \text{number of junctions} \end{aligned} \quad (1)$$

Certain rules must be adhered to as the required cuts are made. These rules are as follows:

1. All required cuts must be made at points directly adjacent to array junctions - that is at end points of the cables comprising the array.
2. The first group of cuts must be made so as to release all but one cable from an anchor.
3. The remaining cuts (if required) are made within the array structure and must be located so as not to break the array into two (or more) parts.
4. As cuts are made, each new cut must be assigned a consecutive junction number, continuing from the last-used junction number. Also, the junction number (in the original array) at which the cut is made must be tabulated.

In effect, applying rules 1-3 reduces the array to the equivalent of a topological tree. As the name implies, this is a continuous structure containing only one fixed point and for which a unique (nonduplicative) path exists from any point to any other point.

Examples of proper reductions to statically determinate structures for the arrays illustrated in Figures 2a-2d are shown in Figures 3a-3d, respectively. In each of these figures, the left-hand schematic shows the reduced array while the right-hand schematic depicts the topological tree representation of the reduced array. The information required by rule 4, which represents geometric constraints on the reduced array, is tabulated below the left-hand schematic in each figure.

Finally, it is necessary to define directions of increasing arc length along the cables comprising the array. The tree representation of the reduced array is used primarily for this purpose. These directions, indicated by the arrowheads in the right-hand schematic of each figure, are identified by starting from the base of the tree and climbing "up" the tree.

Let the measure of arc length along a cable be denoted by s which increases from zero to the total length of the cable L . Then, the required information on increasing directions of arc length can be summarized in terms of array junctions as shown in the table below the right-hand schematic in each figure.

Once an array has been reduced to the state represented by Figure 3, it is amenable to analysis by the program DECEL1.

Coordinate Systems

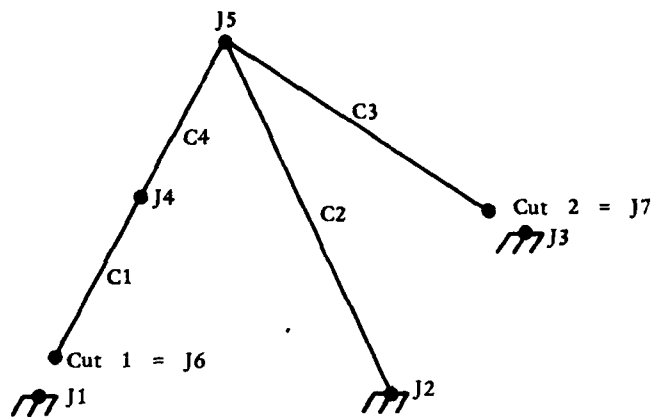
There are two coordinate systems used for inputting the data to DECEL1. They are the magnetically aligned reference coordinate system (N, W, Z) and the array or laboratory reference coordinate system (X, Y, Z). The two coordinate systems share the same origin and the same Z-axis; Z is positive upward. Consequently, the two coordinate systems can differ from one another by an arbitrary angular rotation in the horizontal plane which is denoted by ϕ . For arbitrary locations on the earth, the magnetic axes N-S and E-W are preestablished. Consequently, the angular rotation of the array-referenced coordinate system is referenced to the magnetic axes. In particular, ϕ is the angle between the N-axis and the positive X-axis. A positive rotation of the X-axis with respect to the N-axis is in the clockwise sense. Figure 4 illustrates the two coordinate systems.

The direction of positive rotation is in the clockwise sense in the magnetically aligned coordinate system. The zero degree reference is taken as the N-axis.

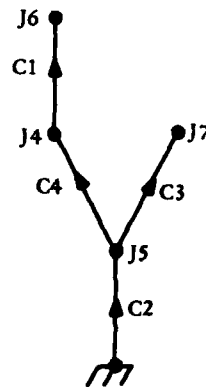
All current data to be input into the program are to be referenced with respect to the magnetic coordinate system. For example, a current having an inclination of 0° is flowing due north; a current with 270° inclination is flowing due west.

When current field input option 3 is selected, it is necessary to specify the locations on the ocean surface (horizontal plane) of the stations where current data have been gathered (relative to the N,W,Z coordinate origin). Typical examples of locations of such stations might be:

100 ft N by 3000 ft W = (100, 3000)
700 ft S by 1500 ft E = (-700, -1500)
0 ft N by 800 ft E = (0, -800)
400 ft N by 450 ft W = (400, 450)

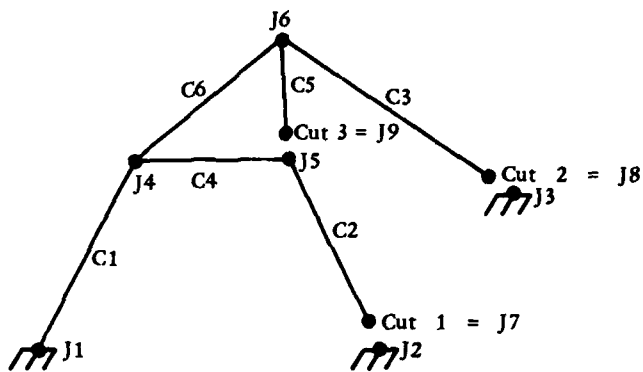


Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made
1	6	1
2	7	3

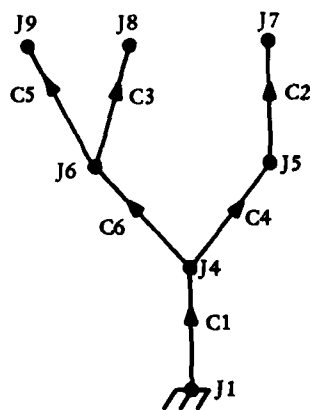


Cable No.	Junction No. At $s = 0$	Junction No. At $s = L$
1	4	6
2	2	5
3	5	7
4	5	4

(a)



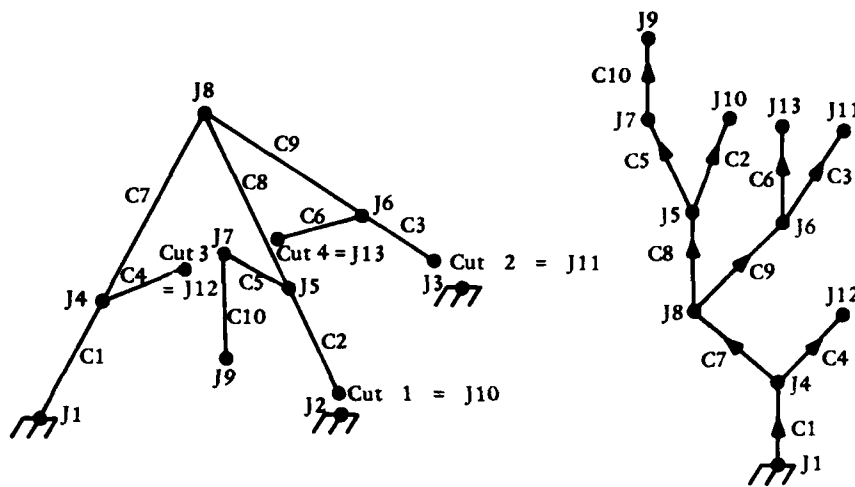
Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made
1	7	2
2	8	3
3	9	5



Cable No.	Junction No. At $s = 0$	Junction No. At $s = L$
1	1	4
2	5	7
3	6	8
4	4	5
5	6	9
6	4	6

(b)

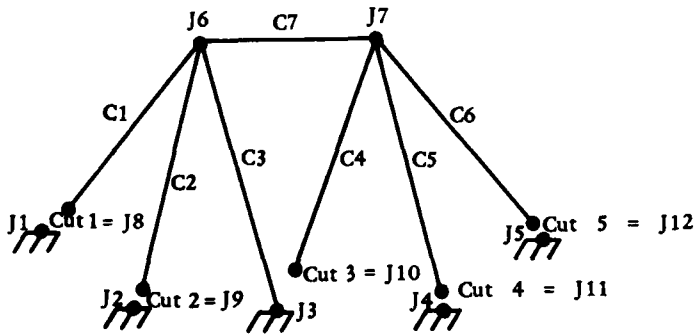
Figure 3. Examples of proper reductions to statically determinate structures for the arrays shown in Figures 2a and 2b.



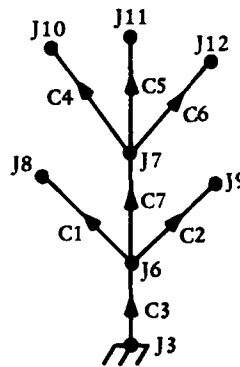
Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made
1	10	2
2	11	3
3	12	7
4	13	7

Cable No.	Junction No. At $s = 0$	Junction No. At $s = L$
1	1	4
2	5	10
3	6	11
4	4	12
5	5	7
6	6	13
7	4	8
8	8	5
9	8	6
10	7	9

(c)



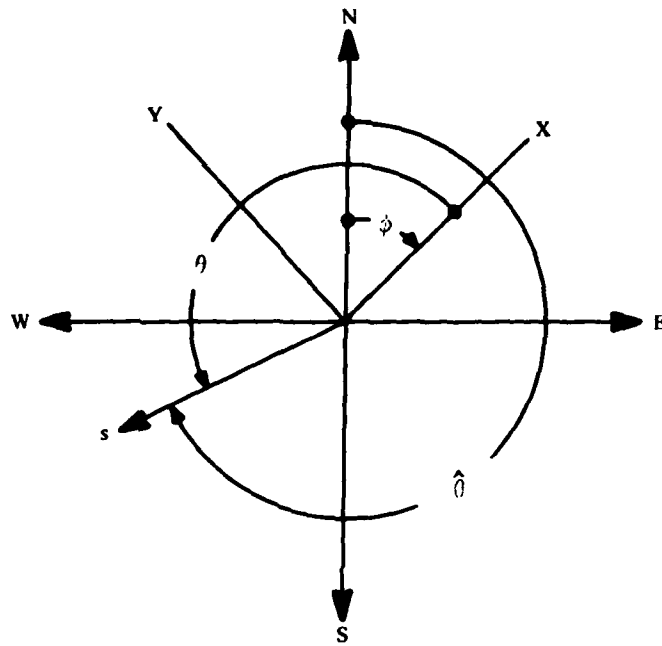
Cut No.	Junction No. Assigned To Cut	Junction No. At Which Cut Made
1	8	1
2	9	2
3	10	3
4	11	4
5	12	5



Cable No.	Junction No. At $s = 0$	Junction No. At $s = L$
1	6	8
2	6	9
3	3	6
4	7	10
5	7	11
6	7	12
7	6	7

(d)

Figure 3. Examples of proper reductions to statically determinate structures for the arrays shown in Figures 2c and 2d.



$$s = \sqrt{N^2 + W^2}$$

$$\theta = 360 + \gamma - \hat{\theta}$$

$$X = s \cos \theta$$

$$Y = s \sin \theta$$

In the magnetic coordinate system the N,W axes are positive. (N,W) form a coordinate pair of a right handed coordinate system. The positive direction of rotation $\hat{\theta}$ in the (N,W) coordinate system is clockwise with the zero degree reference being the N - axis. The array coordinate system (X,Y) system. The relationship between the two systems is given above.

Figure 4. Description and relationship between the magnetic and array referenced coordinate systems.

Above (on the right), is an example of how such locations should be interpreted for input preparation as coordinate pairs. Note that the north-west quadrant is the first quadrant of a right-handed coordinate system. Consequently, north and west are positive axes while south and east are the negative axes. When current field input option 3 is selected, the current data are printed out in both the magnetic and array-referenced coordinate systems.

The specification of the anchor locations is accomplished with respect to the array-referenced (X, Y, Z) coordinate system. All internal calculations within DECELL are performed with respect to the array-referenced coordinate system. The (X, Y, Z) coordinate system is also right-handed. In the horizontal plane in this frame of reference the direction of positive rotation is counter-clockwise with the positive X-axis being the zero degree reference.

Directions of Positive Rotation

<u>Reference System</u>	<u>0° Reference</u>	<u>Positive Rotation</u>
Magnetic	N-axis	clockwise
Array	X-axis	counter-clockwise

Current Field - Input Option 0

There is an input option for determining the static deflections of a cable system immersed in a currentless environment. This is current field input option 0. This option is automatically processed when any of the subsequently described current field input options are exercised. It can be exercised independently.

Current Field - Input Option 1

The current field option 1 is taken to be unidirectional and horizontal, though depth dependent in magnitude. The direction of the current is specified from the magnetic north axis by using the ANG card. [Within the code, the current is referenced to the array coordinate system for calculation purposes. Thus, if the direction of the flow with respect to the X-axis is denoted by θ , the current field is expressed by:

$$V_1 = V(Z)(\underline{e}_1 \cos \theta + \underline{e}_2 \sin \theta)$$

Here, \underline{e}_1 , \underline{e}_2 are unit base vectors with respect to the X- and Y- axes, respectively.] $V(Z)$ specifies the magnitude of the current as a function of depth, Z. This functional relationship must be tabulated as in Table 2.

Table 2. Current Tabulation - Option 1

<u>Column 1</u>	<u>Column 2</u>
Z coordinate (ft)	V(Z) knots

Up to 25 rows are permitted in Table 2. At least one of the Z-coordinates in Table 2 must be less than or equal to the Z-coordinate of the lowest anchor. A sorting scheme is invoked within the program that arranges Table 2 data according to ascending values of Z. Such sorting is necessary within the program for the determination of the current of an arbitrary depth. This is accomplished via a linear interpolation of the currents using the data at the two depths encompassing the depth of interest.

Figure 5 illustrates the magnetic-referenced coordinate system and the linear interpolation of the velocity between given data points.

For current field input option 1, the directionality of the current is a constant for the entire velocity field. Also, for any point (X, Y) on the plane (Z = constant), the value of velocity is invariant.

Current Field - Input Option 2

Current field input option 2 is a slight generalization of the current field input option 1. The generalization involves allowing the current direction θ to vary with depth. The input specification for this option requires depth Z, current magnitude and current direction from the magnetic north axis. The positive direction of rotation is clockwise in the magnetically-aligned reference coordinate system and a zero degree current flows due north. The current specification for option 2 requires a tabulation as in Table 3.

Table 3. Current Tabulation - Option 2

<u>Column 1</u>	<u>Column 2</u>	<u>Column 3</u>
Z-coordinate	V(Z) magnitude, knots	$\theta(Z)$ direction, degrees from magnetic N-axis, positive in clockwise sense

Up to 25 rows are permitted in Table 3. The velocity sorting scheme is invoked by the program. One entry for this data must correspond to a depth less than or equal to the Z-coordinate of the lowest anchor. The above current magnitude and direction data are used to generate velocity components along the (X, Y) axes. To obtain the velocity at an arbitrary depth, linear interpolation is performed using the (X, Y) velocity components above and below the depth of interest; the angular direction of the current is also found by interpolation.

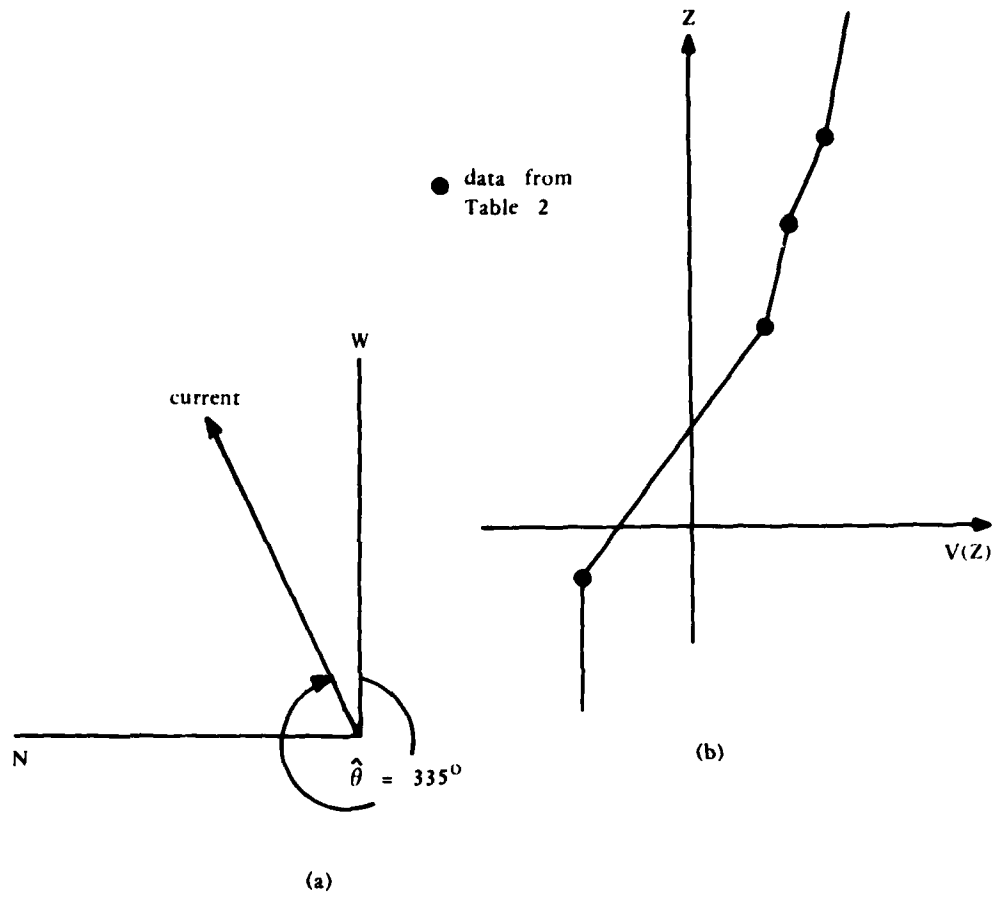


Figure 5. Current field option 1 used in DECEL1 (a) Current angle, θ , (b) Current profile, $V(Z)$.

For current option 2, the value of velocity at any (X, Y) point on the plane $Z = \text{constant}$ is invariant.

An ANG card can be used to rotate the entire current profile in the same manner that a unidirectional current profile is rotated.

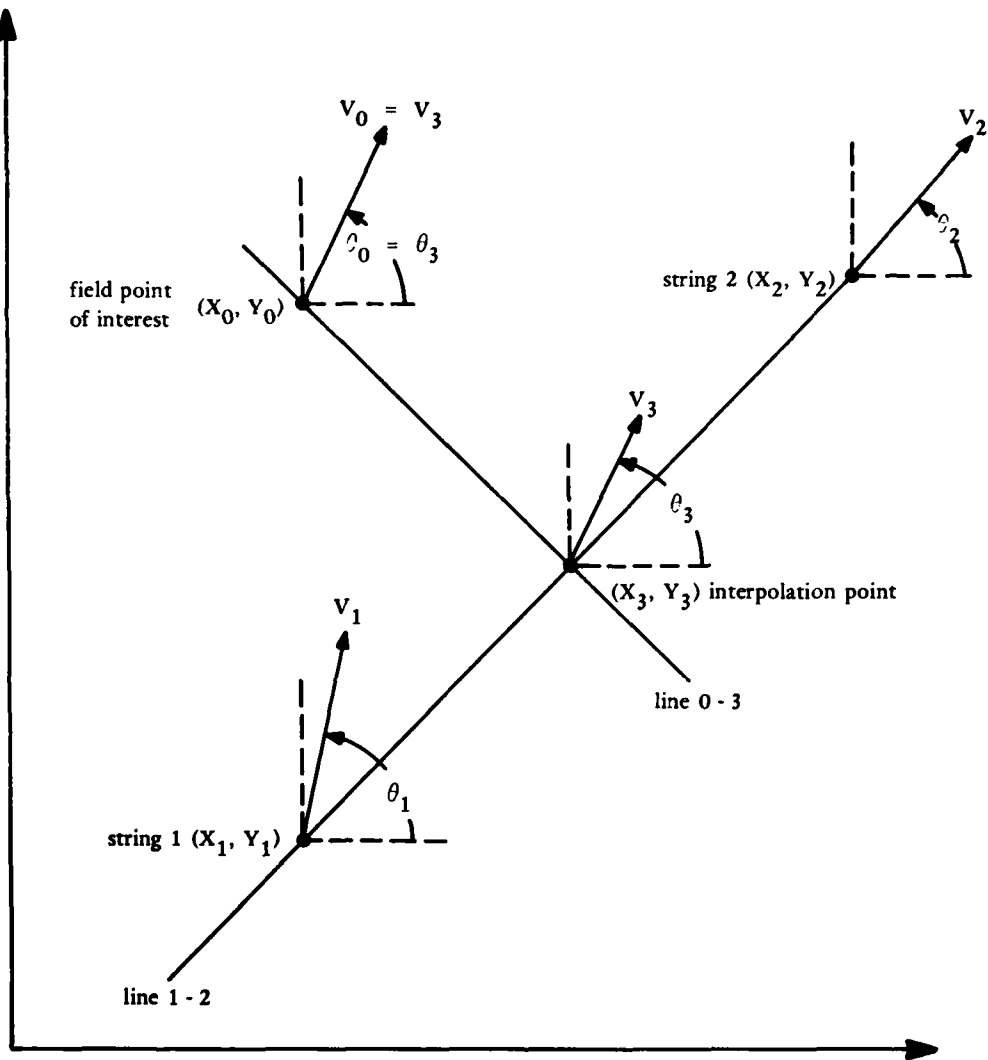
Current Field - Input Option 3

The current field input option 3 employs a linear interpolation/extrapolation scheme on current (magnitude and direction) data to give velocity variation in horizontal planes. When this option is invoked the program expects current data from 2, 3 or 4 current meter strings. Up to 25 measurements of current data can be contained on each string. For each string the first data entry must be at a depth equal to or less than the lowest anchor. The depth dependent data on the various strings do not have to correspond one to the other. That is, if on one string current data are obtained at $Z_1, Z_2, Z_3, \dots, Z_n$, then on the other strings data can be collected at completely different depths. This current field input option has been designed to treat mildly varying current fields. It does not provide acceptable results for eddy currents or reverse shear flows. The interpolation/extrapolation scheme to obtain the velocity at an arbitrary point in the field works as follows:

Case of 2 Strings. The field point (X_o, Y_o, Z_o) is determined where the velocity is to be found. On the plane $Z=Z_o$ there are three points of interest. They are (X_o, Y_o, Z_o) , (X_1, Y_1, Z_o) and (X_2, Y_2, Z_o) where the last two points denote the location on the plane $Z=Z_o$ at the meter strings. At each of these locations current magnitude and direction data are determined by a straight line interpolation of the data values given directly above and below the Z_o elevation. Figure 6 illustrates the situation after this linear interpolation. There, (V_1, θ_1) and (V_2, θ_2) are obtained from the vertical interpolation just mentioned.

A line normal to the line connecting (X_1, Y_1) and (X_2, Y_2) through the field point (X_o, Y_o) is constructed to locate the interpolation point (X_3, Y_3) . The point (X_3, Y_3) lies on the line joining (X_1, Y_1) and (X_2, Y_2) . Linear interpolations are now performed to find V_3 and θ_3 from the corresponding values at (X_1, Y_1) and (X_2, Y_2) . The current (V_3, θ_3) are assumed to prevail at all points along the normal line. Hence, (V_3, θ_3) provide the description of the current at the field point (X_o, Y_o) .

Case of 3 Strings. Suppose the field point is (X_o, Y_o, Z_o) . The current magnitude and direction are determined by linear vertical interpolation at the three string locations (X_1, Y_1, Z_o) , (X_2, Y_2, Z_o) and (X_3, Y_3, Z_o) . The corresponding velocity data obtained at these locations are (V_1, θ_1) , (V_2, θ_2) and (V_3, θ_3) . At the string location on the horizontal plane $(Z=Z_o)$ V_1, V_2 and V_3 are amplitudes through which a velocity plane can be passed. (A unique plane can be passed through any three non-collinear points.) The velocity V_o at the field point (X_o, Y_o, Z_o) then can be obtained by determining the amplitude on the velocity plane corresponding to the position (X_o, Y_o, Z_o) . The procedure is exactly the same for the determination of the current direction θ_o . For this quantity a direction plane has to be established using the direction amplitudes θ_1, θ_2 and θ_3 .



Line 0 - 3 is orthogonal to line 1 - 2. The velocities (V_1, θ_1) and (V_2, θ_2) are obtained by linearly interpolating string 1 and string 2 data, respectively. The velocity of any point along line 1 - 2 can be obtained by linear interpolation/extrapolation of the velocities (V_1, θ_1) , (V_2, θ_2) . The assumption is made that the velocity (V_3, θ_3) of an arbitrary point (X_3, Y_3) on line 1 - 2 is propagated along the orthogonal trajectory to that line at that point.

Figure 6. Interpolation/extrapolation in the case of 2-string data.

Case of 4 Strings. The field point is (X_0, Y_0, Z_0) . The string points are (X_1, Y_1, Z_1) , (X_2, Y_2, Z_2) , (X_3, Y_3, Z_3) and (X_4, Y_4, Z_4) . Through any three of the string points the procedure used in the preceding case can be repeated exactly. There are four independent ways that three points can be selected from four points, namely: (1, 2, 3); (1, 3, 4); (1, 2, 4); (2, 3, 4). The current is determined at the field point by averaging the results obtained by applying the case of three strings four times to the four combinations of points just indicated.

TANGENTIAL DRAG

The tangential drag computation on the cable is straightforward and is based on the expression

$$\Delta F_{TD} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix} = \frac{1}{2} \rho [\pi D(1+\epsilon)] C_{DT} V_{TM} V_T \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$$

where $\Delta F_{TD} \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$ = tangential drag force component per unit length in the direction X, Y or Z

$V_T \begin{pmatrix} X \\ Y \\ Z \end{pmatrix}$ = tangential velocity component along X, Y or Z axis

V_{TM} = $\sqrt{V_T^2(X) + V_T^2(Y) + V_T^2(Z)}$, magnitude of tangential velocity

C_{DT} = tangential drag coefficient

ρ = density of fluid

D = cable diameter

ϵ = strain developed by cable tension

The above calculation forms a part of the hydrodynamic cable drag force. The hydrodynamic force is comprised of a normal drag and a tangential drag.

CABLE DEVICES

In FUNCTION EFORCE (I, M, N) the tangential drag contribution to in-line devices is included in the drag calculation. It is required therefore to supply a tangential drag coefficient for each in-line device as input.

For in-line cable devices the weight of the cable and the hydrodynamic drag over a portion of the cable covered by an in-line device is deleted. Cable devices are referred to as in-line or free devices (two types). All cable devices are numbered automatically within the program. The numbering is accomplished sequentially with respect to cable number

and location of the device away from its $s=0$ end. That is, if on cable 1 there are three cable devices located at $s=s_1$, $s=s_2$, and $s=s_3$ with a $s_3 > s_2 > s_1$, then cable device indices 1, 2, 3 refer to devices located on cable 1 at $s=s_1, s_2, s_3$, respectively.

REFERENCE CONFIGURATION

An option exists to specify a particular parametric study case as a new no current reference configuration. Displacements with respect to the new no current reference configuration as well as the displacement from the original no current reference configuration are part of the output.

ITERATION CONTROL AND EXECUTION ERROR MESSAGES

To protect the user from excessively high execution costs coupled with the risk of not receiving any output, iteration limits have been added to DECEL1. Two separate iteration processes are involved: one attempts to satisfy the displacement constraints, where the cuts are made, imposed by the COMP card; where the other determines the structure's shape. Both iteration processes have been observed on rare occasions to converge very slowly, if at all.

The first iteration process deals with the imaginary reactions. The associated displacement errors have been observed to be large and to change slowly in some slowly convergent problems. An arbitrary definition of slow convergence coupled with a maximum iteration limit is used to terminate execution of a particular parametric case. Slow convergence has been defined to occur when, after half of the iteration limit is achieved, the displacement error is large (100 times the COMP value) and the error is changing by less than the COMP value per iteration. Iteration is terminated due to slow convergence with the message: SLOW CONVERGENCE AFTER XXX ITERATIONS. The previous and present displacement error values are printed to aid in determining how closely the solution has converged. If only one of the slow convergence criteria is satisfied iteration will continue until convergence occurs or the iteration limit is reached. Iteration is terminated due to reaching the iteration limit with the message: NO CONVERGENCE IN XXX ITERATIONS and the present and previous displacement error values are printed.

The second iteration process to determine the structure's shape occurs after the imaginary reaction iteration has been successful. This process has been observed on some occasions to oscillate about the correct solution. The normal iteration process is allowed to continue until half of the nodal position iteration limit is reached. At this point, the solution is arbitrarily assumed to be oscillating and a half-step iteration scheme is imposed (the iteration process is unchanged except that each node is allowed to move only half as far as calculated). This half-step technique continues until the iteration limit is reached or convergence occurs. Execution of the parametric case is terminated with the message: PROGRAM DID NOT CONVERGE AFTER XXX ITERATIONS, PARAMETRIC CASE TERMINATED. The displacement error is printed and the full output for the case is printed preceded by the message: APPROXIMATE RESULTS PRINTED. The user must judge if an adequate displacement error has been achieved for the results to be meaningful.

What To Do If . . .

When execution has been terminated by reaching the imaginary reaction iteration limit, several options are still available. The iteration limit (field 4 of the COMP card) can be increased; however, this probably will have to be done in conjunction with an increase in the COMP value. The COMP value should still be kept in a range that will be judged to produce usable results. The error values printed upon execution termination will give an idea of how much the COMP value will have to be increased.

In some cases, the desired current is too strong to apply in one step; strong currents have caused the imaginary reaction iteration limit to be reached. To handle this and other sensitive cases, an option has been added to apply the current in increments (field 11 of the NDAT card). Using this option, the program iterates to a solution for the first current increment as if this were the total current to be applied. Then the current is incremented and the process is repeated. An option exists to print the solution for each increment of the current (see field 11 of the NDAT card). This technique has been highly effective in obtaining solutions in high currents up to 10 knots.

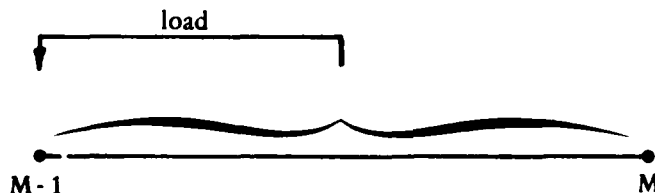
DECEL1 USER EXPERIENCE

In the course of using DECEL1 a wide variety of structures in various current profiles have been analyzed. Some results have been compared with experimental data with close agreement (Ref 7). Other cases have been cross-checked against other computer models again with good agreement. The program is easy to use to the point that a user with a general engineering background can use the manual to formulate the required input and expect to receive back usable results once obvious input errors are corrected. The ease of use is an exceptional attribute of the program.

In the course of making modifications to the program a great deal of insight has been gained regarding the mathematical modeling. Many of the details are of no importance to the user. However there are several characteristics that the user should be aware of; these deal with the internal distribution of loads, non-convergent problems, and the convergence parameter.

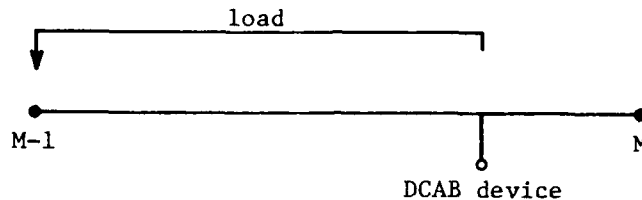
Load Distribution

Loads (weight and drag) are generated from three sources: cables, cable devices, and junction devices. Cable forces due to drag and weight are calculated for the cable length between two nodes [length = (total cable length)/(no. of elements in the cable)]. (See CAB card.) The forces are assigned to the M-1 node as shown below:



Clearly, the smaller the distance between the nodes, the more accurate the mathematical representation.

Loads due to devices on the cable (DCAB card) are modeled in a similar way except that the device is physically located at a specific point along the cable between the two nodes. The DCAB loads are modeled as shown below:



This is a good representation when the device is actually near node (M-1). However, when the device is near node M and the distance between the nodes is large, this may be a poor representation. This is not to say the computer results will be grossly in error; this depends upon the size and number of DCAB devices. If the devices are few and/or small such that the system is cable-load dominated, the results should be acceptable.

Probably the most serious error will arise when there are few elements and the DCAB devices produce large static or drag loads. In this case large loads may be assigned to locations quite distant from their actual point of application.

Loads due to DJNC devices are most accurately modeled. The loads are assigned exactly where the device is located.

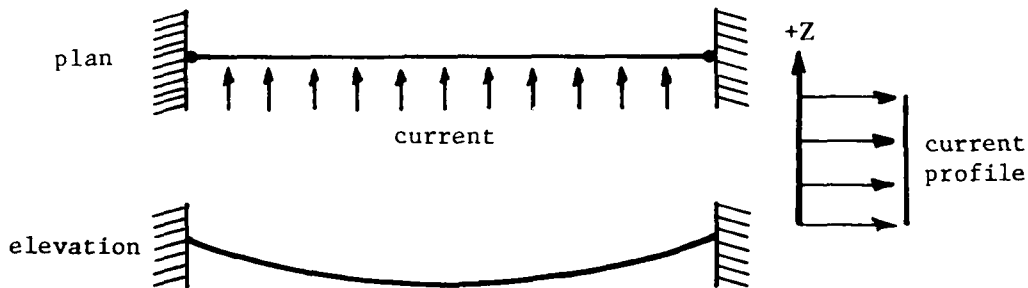
It may appear that a better modeling of cable and DCAB loads could be achieved by proportioning the loads between the appropriate adjacent nodes. However, this single change is not consistent with other internal force accounting schemes. To implement force proportioning, a major re-write of the program would be required; this has not been done.

As the program stands, the majority of problems can be analyzed with wholly satisfactory results even ignoring the way loads are distributed. Where the load distribution scheme is judged by the user to pose a problem in obtaining a satisfactory model, the following suggestions are presented.

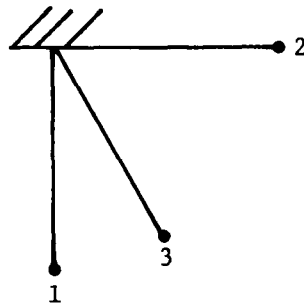
1. Model all cables with as many elements as possible (50). This will make the distance between nodes least so that DCAB loads will be assigned as close to the actual device location as possible.
2. Model large bodies as DJNC devices - loads will be assigned exactly where the device is located.
3. Model long cables as a series of shorter series-connected cables. This will aid in making elements short.

Non-Convergent Problems

DECEL1 treats statically determinate and statically indeterminate problems differently. The indeterminate problems are solved using the imaginary reaction technique (Ref 1). This is a powerful method and usually converges rapidly to a solution. (Reference 1 shows that the method is unconditionally convergent.) However, at least one case has been encountered where the method is at best very slowly convergent. The case involves a nearly neutrally buoyant cable hung in a catenary between two fixed points with a strong current acting perpendicular to the plane of the catenary:

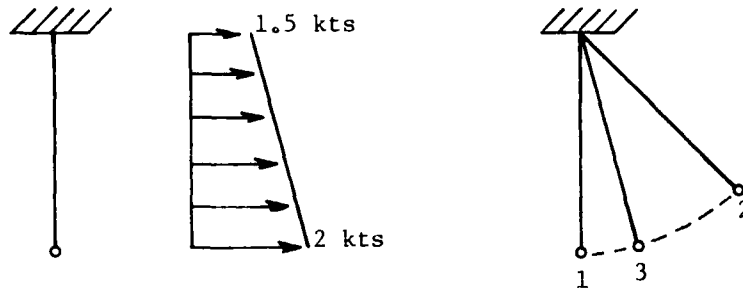


The positions attained by the cable during the iteration procedure are sketched below.



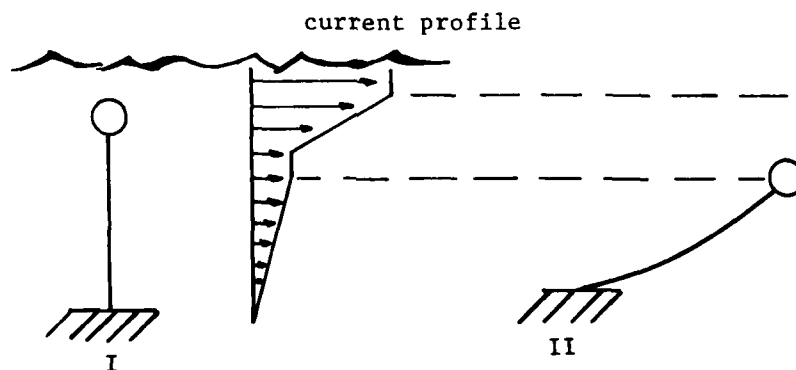
The cable is initially driven from the no-current position (1) to a nearly horizontal position (2). Here there is low- or no-normal drag to support the cable so in the next iteration it falls to position (3) (which may be coincident with position (1)). Internally, the iterations appear to oscillate between positions (2) and (3), and the solution fails to converge. Convergence can be achieved by reducing the current or by increasing the weight of the cable.

Statically determinate cases bypass the imaginary reaction routine, thus convergence is not as certain. There are combinations of current and geometry that interact in such a way as to appear to be unstable. An example is a lightweight anchor suspended from the surface in a current that increases with depth.



From the no-current position (1), the first iteration is to position (2) where the normal drag force is reduced both because of the orientation change (toward horizontal) and the reduced current in the new position. The reduced loading causes the system to attain position (3). The solution then oscillates between positions (2) and (3). Whether another case using this configuration will converge or not depends on both the magnitude of the current and the system weight. The particular case in question probably would converge in a more uniform current field or if the system weight were to be increased.

Another non-convergent case involved a sharp change in the velocity profile.



The subsurface buoy was initially in a high current zone (sketch I); in the first iteration it moved to a lower current region (sketch II). Here the high current was no longer acting on the system so on the next iteration the buoy was moved back into the high current regime. This case failed to converge primarily because the current shear was very near the initial depth of the buoy. Thus the buoy moved in and out of the high current on subsequent iterations. If the current shear had been much below the buoy and always acted only on the cable the solution most likely would have converged.

The above cases are presented simply to illustrate non-convergent problems. They by no means represent all non-convergent cases; however, they serve to illustrate what kinds of situations can be difficult to solve. If a user encounters a case that does not converge, the discussion of the examples here will help guide his reasoning in determining why non-convergence occurs.

In an attempt to improve the iteration technique, a half-step iteration technique has been introduced. The process is implemented only after 100 standard iterations have occurred. (The 100 iteration number has been relatively arbitrarily judged to be an indicator of oscillation during iteration.) After the first 100 iterations have occurred the next 100 iteration steps are calculated in the same way but the allowed displacement is reduced by one-half. This approach has not yet (as of this writing) been user tested; however, initial tests indicate that formerly oscillating cases will converge to a solution. As part of the half-step technique, an informative printout has been added that states the number of iterations required to achieve convergence. After 200 total iterations have occurred, iteration will be stopped, a message printed and the next parametric case will be analyzed. (The 200 iteration limit is arbitrarily taken as an indicator that the solution is not converging.)

Convergence Parameters

The variable on the COMP card is used as the convergence test parameter. The discussion of the COMP card defines a lower limit for the parameter that can be quite small. Iteration continues until two consecutive calculated positions for each node on the structure differ by less than the convergence parameter. Very small values of the convergence parameter can cause certain "sensitive" cases (such as some of those discussed above) to appear to oscillate. Adequate solutions and more rapid convergence can be obtained by picking a convergence parameter value that is consistent with the size of the structure being analyzed. The table below lists suggested convergence parameter values that are consistent with the structure size as determined by cable length.

<u>Cable Length (ft)</u>	<u>Convergence Parameter (ft)</u>
<10	<0.01
<100	0.01-0.1
<1000	0.1-1.0
<10,000	1.0-10.0
>10,000	5.0-20.0

These are only suggested values that may be used as initial values in order to insure that successful convergence does occur. For particular problems the user must judge for himself the adequacy of the convergence tolerance chosen. However, the user must realize that an unnecessarily small convergence parameter can cause a case to fail to converge mathematically even though a physically adequate solution has been reached in the iteration process.

INPUT CARDS

Input cards to DECEL1 contain a 4-digit integer (-999 to 9999) card number in columns 1-4, a 4-character card type identifier in columns 5-8, and descriptive properties of the array in the remaining fields with the exception of the following input cards.

- 1 - Main Descriptive Title Card
- 2 - Parametric Descriptive Title Card
- 3 - Continuation Card for CAB
- 4 - Velocity Field for Current Option 3

The card number has two uses. First, it is used as a convenience for the user to define the order of the cards in the deck, should the deck be dropped. Secondly, it is used as a cross-check in changing parameters in the Parametric Study Source Deck: when a parameter on a card is to be changed, both the card number and type must match the card in the Cable Array Source Deck or an error will occur. In the Cable Array Source Deck, duplicate card numbers are detected as errors; however, any number of input cards may have the card number omitted with no errors.

**** CABLE ARRAY SOURCE DECK CARDS ****

LUN CARD (optional card; if used it must be the first card in the deck)

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^LUN	Right adjust
3	9-16	I8	Unit number of card reader	
4	17-24	I8	Unit number of line printer	
5	25-32	I8	Unit number of temporary storage tape	
6	33-40	I8	Input option (0 or 1)	See notes
7	41-48	I8	Blank if input option = 0. Unit number of source tape if input option = 1.	
8	49-56	I8	Output option (0, 1 or 2)	See notes
9	57-64	I8	Blank if output option = 0. Unit number of output tape or card punch if output option = 1 or 2.	
10	65-72		Not used	See notes
11	73-77		Not used	
12	78-80		Not used	

- NOTES: 1. The carot symbol (^) is used to indicate one blank column in the position shown.
2. The LUN card is used to transmit the logical unit numbers of of the I/O devices and the I/O options. The LUN card is optional. If it is omitted then input option 0 and output option 0 are the default options.

Two input options are available:

- 0 - The physical characteristics of the array are to be read from the cable array source deck (see CABLE ARRAY SOURCE DECK)
- 1 - The physical characteristics of the array are to be read from the cable array source tape (see CABLE ARRAY SOURCE TAPE)

Three output options are available:

- 0 - A structural output to the line printer (see
STRUCTURAL OUTPUT)
- 1 - A device location output to tape or cards (see
DEVICE LOCATION OUTPUT)
- 3 - both of the above

MAIN DESCRIPTIVE TITLE CARD

Field	Columns	Format	Contents	Comments
1-10	1-80	8A10	Main descriptive title	See notes

NOTE: A single "Main Descriptive Title Card" must always follow the LUN card. If no title is desired a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type, so that the entire card can be utilized for a title. If the LUN card is omitted then this must be the first input card.

NJNC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	NJNC	
3	9-16	I8	Number of junctions in original (unreduced) array	2-44
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The NJNC card is used to transmit the number of junctions in the original (unreduced array).

ANC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^ANC	Right adjust
3	9-16	I8	Junction number of anchor	1-44
4	17-24	F8.0	X coordinate of anchor	ft
5	25-32	F8.0	Y coordinate of anchor	ft
6	33-40	F8.0	Z coordinate of anchor	ft
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The ANC cards are used to transmit the data in Table 1.
There must be one ANC card for each anchor in the array.

IR CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^^IR	Right adjust
3	9-16	I8	Junction number assigned to a cut in the reduced array	1-44
4	17-24	I8	Junction number at which cut is made in the original array	1-44
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The IR cards are used to transmit the information contained in the table below the left-hand schematic of each of Figures 3a-3d. There must be one IR card for each cut made in going from the original to the reduced array.

CAB CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	.CAB	Right adjust
3	9-16	I8	Cable number	1-22
4	17-24	I8	s=0 junction number	1-44
5	25-32	I8	s=L junction number (after required cuts are made)	1-44
6	33-40	F8.0	Cable weight per length in surrounding fluid; + if positively buoyant, - if nega- tively buoyant	lb/ft
7	41-48	F8.0	Normal drag coefficient of cable	
8	49-56	F8.0	Cable diameter	in.
9	57-64	F8.0	Total cable length (unstressed)	ft
10	65-72	F8.0	Cable rigidity, C (see notes) if k=1, C=EA	lb
11	73-77	F5.0	Exponent in constitu- tive relation, k (see notes)	<u>>0</u>
12	78-80	I3	Number of straight ele- ments by which cable is to be represented	<u>>0, <50</u>

NOTE: The CAB cards are used to transmit the information contained in the table below the right-hand schematic in Figures 3a-3d (fields 3 to 5), the physical characteristics of the cables in the array (fields 6 to 11), and the fineness by which the cables in the array are to be modeled (field 12). There must be one CAB card and one continuation CAB card for each cable in the array. The constitutive relation for a cable can, in general, be written (6) as $\epsilon=(T/C)^k$ where ϵ is the

NOTES FOR CAB CARD (continued)

strain and T the tension. C and k are constants which depend on the cable material and construction. Fields 10 and 11 transmit the values of C and k , respectively. An inextensible cable is transmitted to DECEL1 by leaving fields 10 and 11 blank.

CONTINUATION CAB CARD

Field	Columns	Format	Contents	Comments
1	1-8	F8.0	Tangential drag coefficient of cable	See notes
2	9-80	9F8.0	Not used	

NOTE: Each CAB card must be followed by an additional card. If no tangential drag is desired a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type since it is in fact a continuation of the tangential drag coefficient. Default value is zero.

DCAB CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	DCAB	
3	9-16	I8	Number of cable to which device is attached	1-22
4	17-24	I8	Device type (1,2)	See notes
5	25-32	I8	Print flag for cable devices. If flag = 0, print device characteristics and location. If flag \neq 0, don't print.	
6	33-40	F8.0	Device weight in surrounding fluid; + if positively buoyant, - if negatively buoyant	lb (See note 3)
7	41-48	F8.0	Normal drag coefficient	
8	49-56	F8.0	Diameter on which drag coefficient is based (Type 1) Frontal area on which drag coefficient is based (Type 2).	in. ft ²
9	57-64	F8.0	Device length (Type 1)	ft
10	65-72	F8.0	Unstressed distance of device from $s=0$ junction of the cable	ft
11	73-77	F5.0	Tangential drag coefficient	
12	78-80		Not used	

NOTE: 1. The DCAB cards are used to transmit the physical characteristics of the discrete devices (buoyancy elements, current meters, etc.) attached to the cables in the array. There must be one DCAB card for each such device

NOTES FOR DCAB CARD (continued)

in the array. Two types of devices are permitted: (a) in-line (Type 1) any elongated device (cylinder, ellipse, etc.) attached so that its longitudinal axis is aligned with the cable axis; and (b) free devices (Type 2).

2. Dummy DCAB devices with no weight and zero drag can be used as conveniences to print the location of the device in the cable array's deformed state. With no DCAB devices, no information about the cable shape between junctions is printed.
3. Include cable weight in water if device covers segment of cable.

Each device is automatically assigned a unique number based on its location on the structure. Low numbered devices are located on low numbered cables. On each cable the lowest number device is nearest the $s=0$ end of the cable.

DJNC CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	DJNC	
3	9-16	I8	Number of junction to which device is attached	1-44
4	17-24	I8	Not used	
5	25-32	I8	Not used	
6	33-40	F8.0	Device weight in surrounding fluid; + if positively buoyant, - if negatively buoyant	lb
7	41-48	F8.0	Device drag coefficient	
8	49-56	F8.0	Frontal area on which drag coefficient is based	ft ²
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The DJNC cards are used to transmit the physical characteristics of the discrete devices attached to the junctions in the array. There must be one DJNC card for each such device in the array.

Since an in-line device cannot physically exist at a junction (cable termination), only free devices are permitted at a junction.

DJNC devices are indexed automatically for counting purposes only; they are counted in the total number of indexed devices.

DEN CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	.DEN	Right adjust
3	9-16	F8.0	Density of fluid in which array is suspended	$\text{lb s}^2 \text{ft}^{-4}$ (1.99 for seawater)
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The DEN card is used to transmit the density of the fluid in which the array is suspended.

EOD CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^EOD	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOD card is used to specify the end of data transmission.

** PARAMETRIC STUDY SOURCE DECK CARDS **

NDAT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	NDAT	
3	9-16	I8	Current field option	See note 1
4	17-24	I8	Number of stations at which current data is taken for current field option 3. Otherwise not used.	See note 2
5	25-32	I8	Option for defining a particular parametric study as the new no current reference configuration. Option = 0, no new ref. config. Option \neq 0, new ref. config.	
6	33-40	F8.0	PHI	degrees See note 3
7	41-48	F8.0	Device location punch output option; option \neq 0, punch device locations on cards	See note 4
8	49-56	F8.0	Weight of device whose location is to be punched	lb
9	57-64		Not used	
10	65-72	F8.0	Velocity units input option	See note 5
11	73-77	F5.0	Number of steps used to apply full current	See notes 6 and 7 (default value = 1.0)
12	78-80		Not used	

SEE NEXT PAGE FOR NOTES

NOTE:

1. The NDAT card is used to specify that new, modified, or additional data follow and to transmit the current field option. Three current field options are available.
 - 0 - No current.
 - 1 - Current field is unidirectional and horizontal. (There is no vertical component.) The current magnitude can vary with depth. At any point in the plane Z-constant, the velocity is invariant. The no-current configuration is also calculated as part of this option.
 - 2 - Same as current field option 1 except that the current can have a directionality that depends on depth. That is, this option relaxes the unidirectional constraint on the velocity field. At any point in the plane Z-constant, the velocity is invariant. An example of a possible current candidate requiring this option would be a helical current where the axis of the helix is aligned with gravity. The no-current configuration is also calculated as part of this option.
 - 3 - Interpolation/extrapolation scheme for field current (magnitude and direction) data. The current is assumed to have no vertical component. Two, three, or four stations can be selected in the horizontal plane and at each of these stations, current (direction and magnitude) data can be obtained at up to 25 elevations. This option affords current variation in horizontal planes. The no-current configuration is also calculated as part of this option.
2. For current option 3, the value in field 4 on the NDAT card must appear on all successive NDAT cards even if the velocity field is not to be varied in any of the parametric studies.
3. The angle ϕ specifies the rotation of the X-axis from the N-axis. ϕ is measured positive in the clockwise sense and the N-axis is $\phi=0$. That is, when $\phi=0$ then the (N,W) coordinate system is coincident with the (X,Y) coordinate system (see Figure 4). The ϕ value should appear on each NDAT card.
4. It is sometimes desirable to have the locations of particular devices punched on cards for input to other programs. For example, both hydrophones and buoys may be distributed as DCAB devices along the structure, but only the location of the hydrophones is important. By specifying field 7 \neq 0 and field 8 = hydrophone weight, DECEL1 will punch for each hydrophone: (a) device index, (b) cable number, (c) distance from the s = 0 end of the cable, and (d) x,y,z coordinates of the device. Preceding this punched output is a card totalling the number of cards in the punched output.

NOTES FOR NDAT CARD (continued)

5. Velocity units input option:
 - 0 - input magnitude of velocity in knots (default)
 - 1 - input magnitude of velocity in cm/sec
 - 2 - input magnitude of velocity in ft/sec

6. This is a coded value: the integer portion represents the number of steps used to apply the full current; the fractional part controls printed output: a non-zero fractional part (i.e., 10.1) causes the shape calculated for each increment of the current to be printed. For example: the value 10.1 will cause the current to be applied in ten equal increments and the structure shape will be printed for each increment. A 10.0 value will apply the current in ten increments but print only the shape with the full current value applied. If plotting is requested, only the shape with the full current applied is plotted.

7. This input option is intended to aid in obtaining solutions where high currents cause SLOW/NO CONVERGENCE messages to be printed.

PARAMETRIC DESCRIPTIVE TITLE CARD

Field	Columns	Format	Contents	Comments
1-10	1-80	8A10	Parametric descriptive title	See notes

NOTE: Descriptive Title Card must always follow an NDAT card. If no title is desired, then a blank card must be inserted. This card does not adhere to the convention requiring a card number and card type, so that the entire card can be utilized for a title.

COMP CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	COMP	
3	9-16	F8.0	Accuracy required in array equilibrium calculations (COMP value)	ft (0.01 typ)
4	17-24	F8.0	Nodal position iteration limit	See note 2 (200 default value)
5	25-32	F8.0	Imaginary reaction iteration limit	See note 2 (1000 default value)
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTES:

1. The COMP card is used to transmit the accuracy requirement imposed on the array equilibrium calculations. This accuracy requirement, specified in field 3, insures that the calculated coordinates of every point in the array are within \pm field 3 of their exact values.

The accuracy obtainable is limited by the significant figure capacity of the computer being used and by the largest linear dimension in the array. Let the number of significant figures carried in single precision be n , and let the characteristic of the common logarithm of the largest linear dimension be m . Then, the value of field 3 is usually bounded by field 3 $\geq 10^{m-n+3}$. (For example, suppose $n = 8$ and the largest dimension is 25,000 ft. Then, field 3 ≥ 0.1 ft.) Occasionally, a larger minimum value must be used. A

NOTES FOR COMP CARD (continued)

COMP card must appear after the first NDAT card. See PARAMETRIC STUDY SOURCE DECKS. Accuracy requirements can be changed in subsequent Parametric Study Decks by using new COMP cards.

2. See the descriptions in the text on pages 18 and 19.

VEL CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^VEL	Right adjust
3	9-16	F8.0	Z coordinate at which current velocity is specified	ft
4	17-24	F8.0	Magnitude of current at Z coordinate specified in field 3	knots; cm/sec; ft/sec (consistent with NDAT card)
5	25-32	F8.0	Direction of current at Z coordinate (current option 2 only)	degrees
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	56-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The VEL cards are used to transmit the data in Table 2. There must be one VEL card for each value of Z at which the current velocity is specified.

Up to 25 VEL cards are permitted. At least one of the Z coordinates transmitted by the VEL cards must be less than or equal to the minimum Z coordinate transmitted by the ANC cards. For further information see CURRENT FIELD INPUT OPTION 1.

The VEL cards must not appear after an NDAT card specifying a current field option = 0. All VEL cards required to transmit the current profile must appear after the first NDAT card specifying a current field option = 1. See PARAMETRIC STUDY SOURCE DECKS.

A given current profile will be applied in all subsequent parametric cases until a new field is defined.

NOTES FROM VEL CARD (continued)

Current Option 1 - Only the magnitude of the current is input (field 4). The direction is varied by the ANG card.

Current Option 2 - Both magnitude and direction of current are input fields 4 and 5, respectively. The direction of the field also may be modified by the ANG card. Current direction is to be specified from the magnetic north axis. Clockwise rotation is positive.

Current Option 3 - Fields 3, 4 and 5 are ignored. The velocity information is read from the velocity continuation group immediately following the VEL card.

The following is a brief description of the velocity cards under current option 3.

After a VEL card is encountered there will be 2, 3 or 4 sets of velocity data depending on the number of stations at which velocity profiles were measured.

Each set of data for a station will contain one Station Location Card and N Velocity Definition Cards. N is the number of Z-coordinates at which velocity is measured for the particular station. The maximum value of N is 25.

The 2, 3 or 4 sets of data are stacked as indicated in Figure 7.

The Station Location Cards and Velocity Definition Cards are defined on the next two pages.

To further clarify the velocity option 3 data requirements we present another example using 3 stations of current data. The data deck will be arranged as follows:

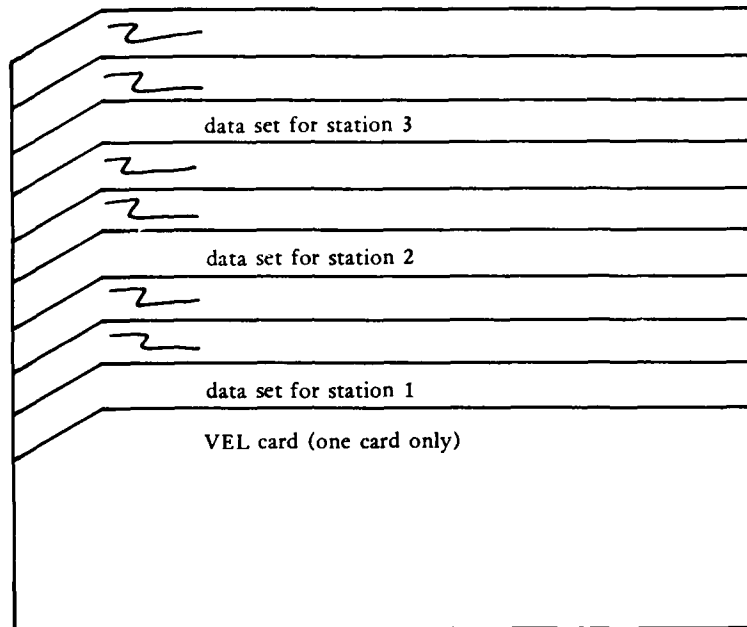


Figure 7. Arrangement of data sets for velocity option 3.

NOTES FROM VEL CARD (OPTION 3 ONLY) (continued)

Field	Columns	Format	Contents	Comments
1	1-5	I5	Station number at which velocity profile measured	
2	6-10	I5	Number of Z-coordinates at which velocity is measured for this station (field 1)	
3	11-20	F10.0	North coordinate of this station*	ft (see notes)
4	21-30	F10.0	West coordinate of this station**	ft (see notes)
5	31-80		Not used	

*Coordinate is positive for north, negative for south.

**Coordinate is positive for west, negative for east.

NOTES FROM VEL CARD (OPTION 3 ONLY) (continued)

Field	Columns	Format	Contents	Comments
1	1-5	I5	Station number	
2	6-10		Not used	
3	11-20	F10.0	Z-coordinate of velocity	ft
4	21-30	F10.0	Magnitude of velocity at Z-coordinate of this station (field 1)*	See notes
5	31-40	F10.0	Direction of current at Z-coordinate of this station (field 1)**	degrees (see notes)
6	41-80		Not used	

NOTE: There must be as many of this card as there are current readings at the station (= field 2 of preceding card).

*The magnitude of velocity may be input in three different units according to the option definition on the NDATA card.

Units Option 0 - knots (default)

Units Option 1 - cm/sec

Units Option 2 - ft/sec (see NDATA card)

**The direction of current is positive in the clockwise sense from the magnetic north axis (degrees).

ANG CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^ANG	Right adjust
3	9-16	F8.0	Initial current angle	degrees
4	17-24	F8.0	Increment in current angle	deg, > 0
5	25-32	F8.0	Final current angle	deg, ≥ field 3
6	33-40		Not used	
7	41-43		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The ANG card is used to transmit instructions for changing the angular direction of the current with respect to the N-axis for current options 1 and 2 only. DECEL1 calculates the array response to the specified current profile from the initial to the final current angles in increments transmitted by field 4. An ANG card must not appear after an NDAT card specifying a current field option = 0. One ANG card must appear after the first NDAT card specifying a current field option = 1, 2, or 3. See PARAMETRIC STUDY SOURCE DECKS.

If no parametric range of current direction variation is required, then Fields 3 and 5 should have identical values and field 4 should have a non-zero positive value.

When exercising the angular rotation option, it is important to recognize the difference between current options 1 and 2. For current option 1, the input value in field 3 of the ANG card establishes the directionality of the entire flow field. This is not the case for current option 2 since current directionality is established and specified as input on the VEL card.

NOTES FROM ANG CARD (continued)

For current option 2 the field 3 input value on the ANG card should be set equal to ϕ (the angle between the N- and X-axes) plus the initial angle of interest. The value in field 5 of the ANG card should be set equal to $\phi + \beta$ where β is the total angle through which the current is to be rotated. The value of field 4 is $\Delta\beta$, the increment. When current option 2 is selected and no rotation of the current field is desired, the fields 3 and 5 should be set equal to ϕ and any positive value set in field 4.

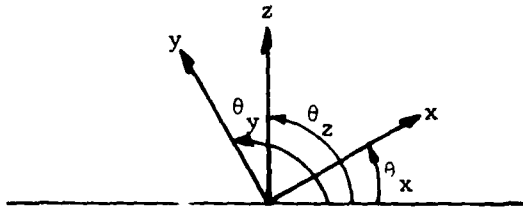
PPLT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	PPLT	
3	9-16	F8.0	Plotting option: 0 - Undeformed only 1 - Deformed only 2 - Both	Undeformed plotted as a dotted line. Deformed plotted as a solid line.
4	17-24	F8.0	Height of plot, y	in. (default 10)
5	25-32	F8.0	View angle, x (see note)	degrees (default 30)
6	33-40	F8.0	View angle, y (see note)	degrees (default 120)
7	41-48	F8.0	View angle, Z (see note)	degrees (default 90)

NOTE: For a plan or elevation view (not a perspective view) one view angle must be 361°. This is a code indicating which axis is perpendicular to the plot. For example, a plan view is specified by:

View Angle, x = 0.001 (0 gives the 30° default value)
View Angle, y = 90°
View Angle, z = 361°

The x, y and z view angles are shown below for the default configuration.



θ_x - View angle for x axis. 30 degrees.
 θ_y - View angle for y axis. 120 degrees.
 θ_z - View angle for z axis. 90 degrees.

Examples perspective plots are shown in Figures 8-10.

CPLT CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	CPLT	
3	9-16	F8.0	ZUP-Max. depth plane level	ft
4	17-24	F8.0	ZDN-Min. depth plane level	ft
5	25-32	F8.0	DZ -Delta depth	ft
6	33-40	F8.0	YIN-Height in Y direction of a single plane	in.
7	41-48	F8.0	XMIN	ft (If blank default values selected)
8	49-56	F8.0	XMAX	
9	57-64	F8.0	YMIN	
10	65-72	F8.0	YMAX	
11	73-77	F5.0	ANG-View angle Y	degrees default = 90
12	78-80	I3	NY -Number of mesh points in Y direction, including boundary	default = 6

NOTE: Current plots may be depicted at one or more depths by varying input parameters ZUP, ZDN, DZ. The vertical height for each plane of the plot is input as YIN, and the corresponding width is calculated by the program. The product of the number of planes and the vertical height of a single plane cannot exceed 10 inches.

The plots may vary in perspective view angle y over the range $0 < \text{ANG} < 180^\circ$, where $\text{ANG} = 90^\circ$ is the plan view. For purposes of plotting the current field, each plane is assumed to have z coordinate zero and view angle x equal to zero.

NOTES FROM CPLT CARD (continued)

The mesh for plotting current is controlled by input NY. NY is the number of mesh points in the y direction, for a plane, including the boundary. The corresponding number of mesh points, for the x direction, is calculated by the program. ($NY = 2 + \text{number of current arrows encountered when moving from YMIN to YMAX.}$)

The area covered by the current field plot may be selected in two ways. If the values XMIN, XMAX, YMIN, YMAX are left blank, the program determines the area to be plotted. The area is based on the maximum and minimum anchor point coordinates. The second method is to define XMIN, XMAX, YMIN, YMAX in terms of the x, y coordinate system. If there is only one anchor point XMIN, XMAX, YMIN, YMAX must be defined by the user. A star will be plotted at each anchor point within the defined area.

Examples of current field plots are shown in Figures 11 and 12.

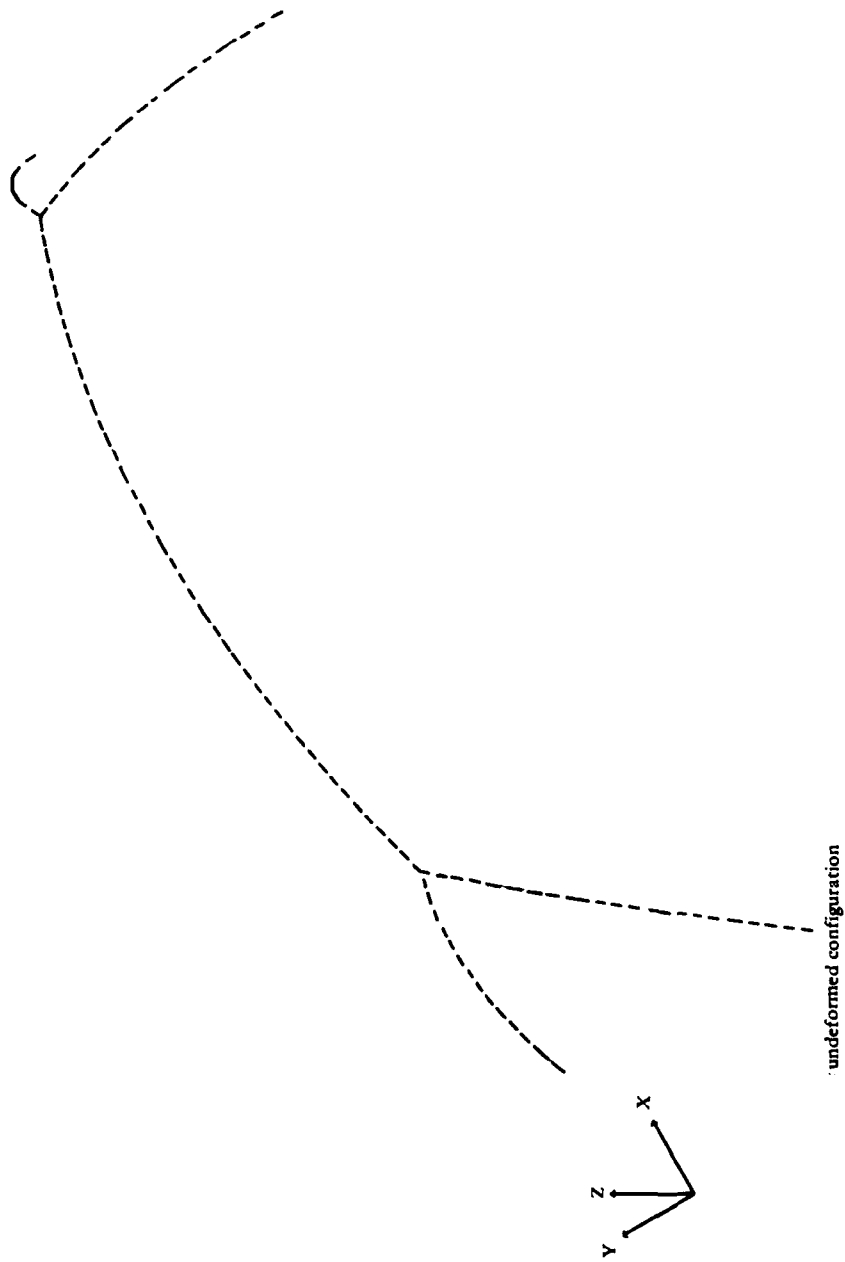


Figure 8. Perspective view of the undeformed structure (field $3 = 0$).

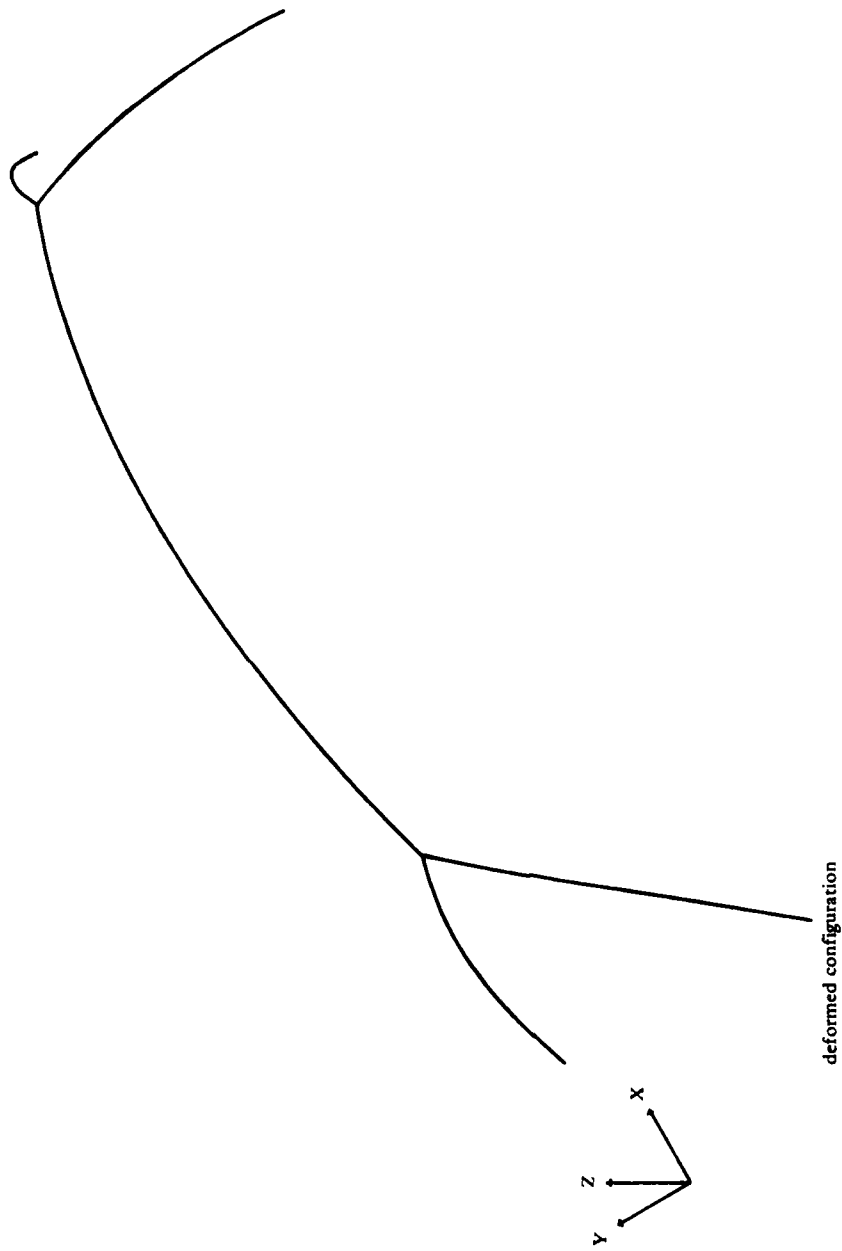


Figure 9. Perspective view of the deformed structure (field 3 = 1).

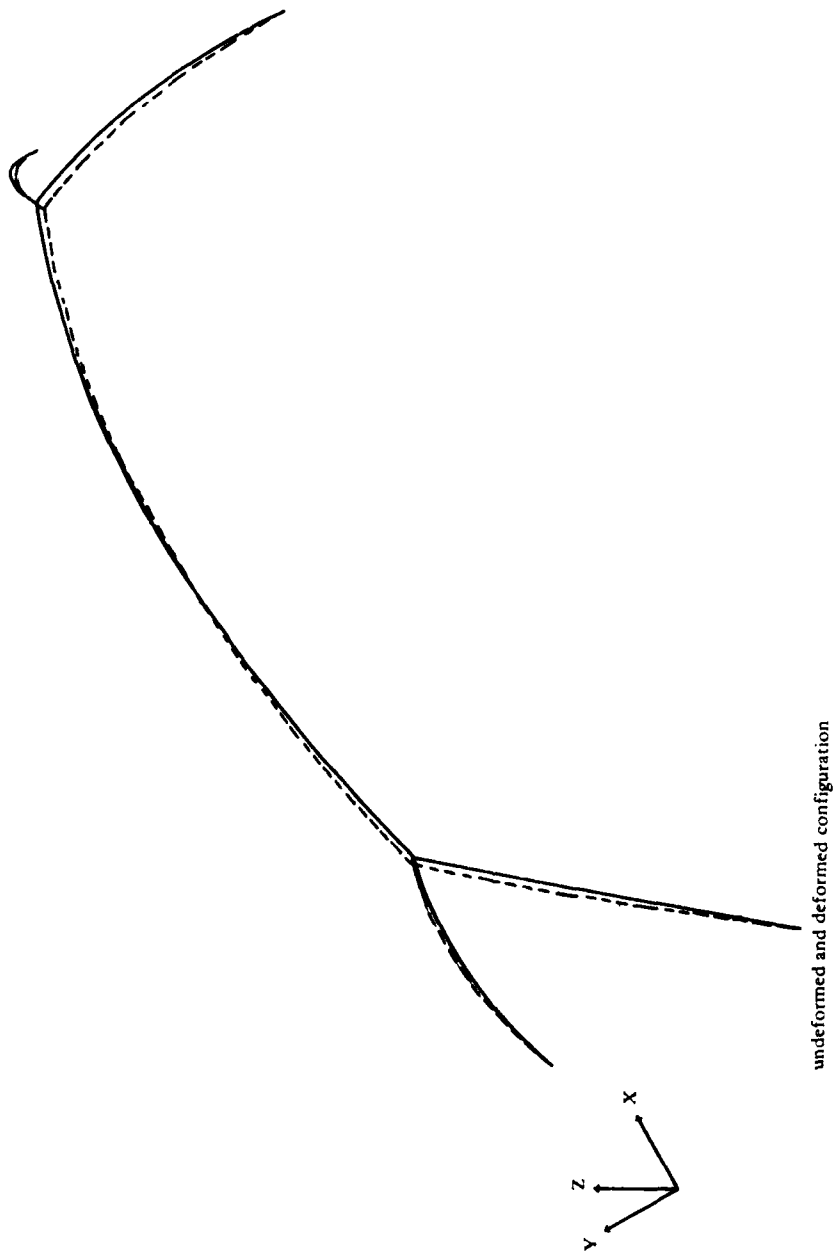


Figure 10. Perspective view of the deformed structure with the undeformed shape for comparison (field 3 = 2).

apply current profile at 45 dec increments

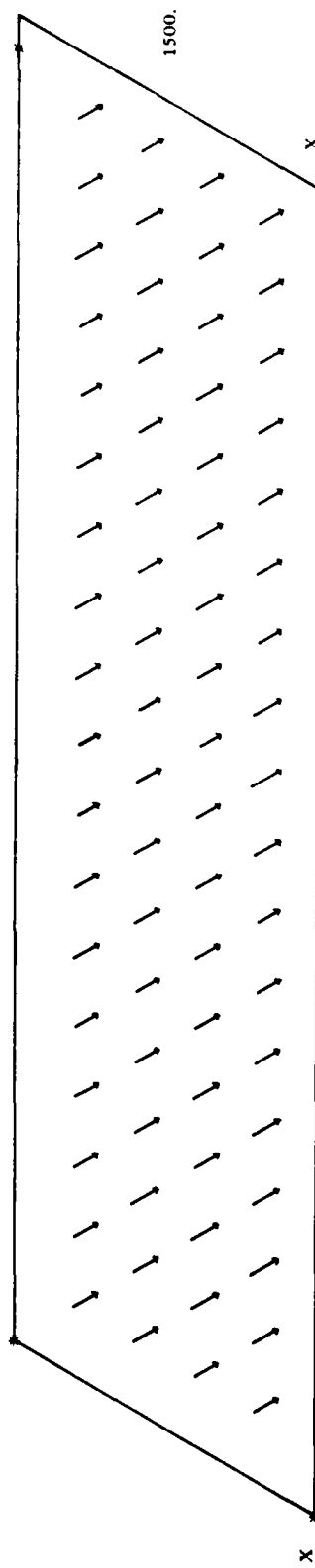
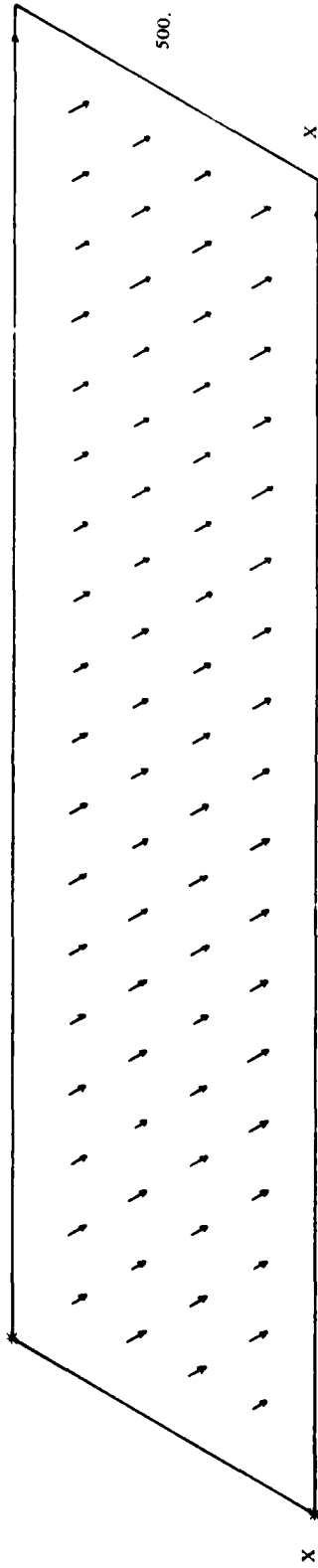


Figure 11. Unidirectional current field.

test for current option 3

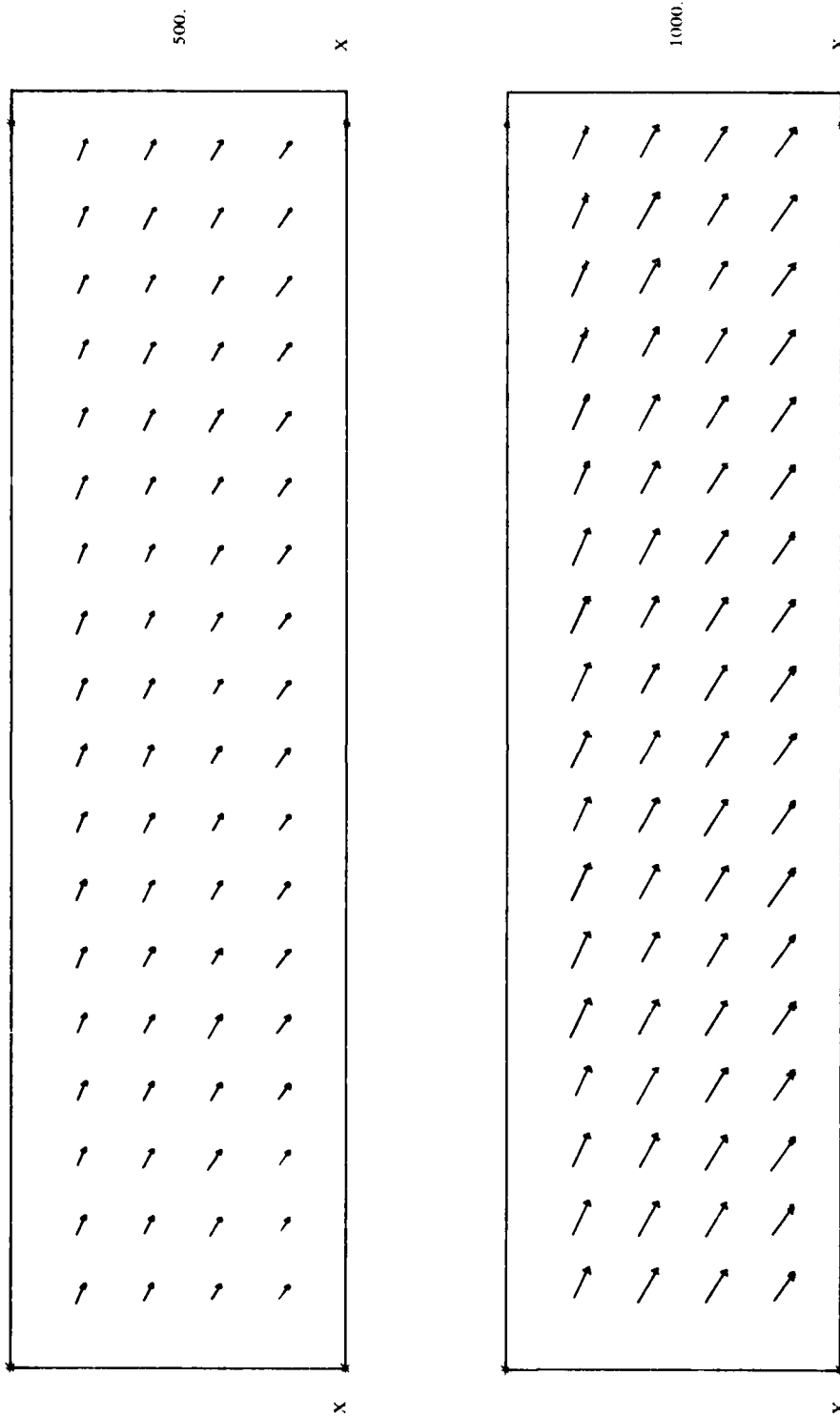


Figure 12. Non-unidirectional current field. (Note by sighting along the arrows that the field does curve.)

EOD CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	^EOD	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOD card is used to specify the end of data transmission or end of a parametric case.

EOP CARD

Field	Columns	Format	Contents	Comments
1	1-4	I4	Card number (optional)	-999 to 9999
2	5-8	A4	∟EOP	Right adjust
3	9-16		Not used	
4	17-24		Not used	
5	25-32		Not used	
6	33-40		Not used	
7	41-48		Not used	
8	49-56		Not used	
9	57-64		Not used	
10	65-72		Not used	
11	73-77		Not used	
12	78-80		Not used	

NOTE: The EOP card is used to specify the end of the problem and is required for a normal termination.

Cable Array Source Deck

The cable array source deck contains all of the cards required to describe the physical characteristics of the cable array under consideration. The last card in the cable array source deck must be an EOD card to signify the end of data transmission. The form of the cable array source deck is given below.

Cable Array Source Deck

<u>Card Type*</u>	<u>Comments</u>
NJNC	One card
ANC	One for each array anchor
IR	One for each cut going from original to reduced array
CAB	One (plus one continuation card) for each array cable
DCAB	One for each discrete device attached to a cable
DJNC	One for each discrete device attached at a junction
DEN	One card
EOD	Must be last card in source deck

Cable Array Source Tape

The cable array source tape is an alternate means of transmitting to DECEL1 the physical characteristics of the cable array under consideration. A recommended program for generating the cable array source tape from the cable array source deck is given below.

Cable Array Source Tape Generation

```
PROGRAM STAPE
DIMENSION DATA(10)
DATA(IREAD = Unit number of card reader)
DATA(ITAPE = Unit number of source tape)
1 READ(IREAD,10)(DATA(I),I=1,10),EX,NSEG
WRITE(ITAPE,11)(DATA(I),I=1,10),EX,NSEG
IF(DATA(2).NE.4HDCAB)GO TO 3
READ(IREAD,20)TANDRG
WRITE(ITAPE,21)TANDRG
```

(continued)

*These cards may be arbitrarily ordered except for the EOD card. It is strongly recommended that the cards in the cable array source deck be given unique card numbers (Field 1 of each card). Note that LUN, NDAT, COMP, VEL, ANG, and EOP cards are not permitted in the cable array source deck.

Cable Array Source Tape Generation (Continued)

```
3 CONTINUE
  IF(DATA(2).EQ.4H EOD)GO TO 2
  GO TO 1
10 FORMAT(F4.0,A4,8F8.0,F5.0,I3)
11 FORMAT(F4.0,A4,8E15.8,/,E12.5,I3)
20 FORMAT(F8.0)
21 FORMAT(E15.8)
2 REWIND TAPE
  END
```

Parametric Study Source Decks

The parametric study source decks are used to transmit to DECEL1 accuracy requirements, current fields, and changes in the physical properties of the cable array under consideration. Each parametric study source deck must begin with an NDAT card and a Parametric Descriptive Title card and end with an EOD card. The form of the parametric study source decks is given below.

Parametric Study Source Decks

<u>Card Type*</u>	<u>Comments</u>
NDAT	Must be first card in parametric study source deck. Field 3 (current option) can change as 0 1, 0 2, or 0 3. The changes 1 2, 1 3, and 2 3, even with intermediate zeros, are not permitted.
Parametric Title Card	NDAT card <u>must</u> be followed immediately by parametric title card.
COMP	Must appear after first NDAT card. The accuracy requirement transmitted is retained until the appearance of a COMP card in another parametric study source deck.
VEL	Must not appear after NDAT card containing current option 0. All VEL cards required to transmit a current profile must appear after the first NDAT card containing a current option 1 or 2 or 3. The current profile transmitted is retained until the appearance of a VEL card in another parametric study source deck. The appearance of the first VEL card in a parametric study source deck zeros the entire current profile. Thus, to change from one current profile to another, all VEL cards required to specify the new profile must appear in the appropriate parametric study source deck.
ANG	Must not appear after NDAT card containing current option 0. One ANG card must appear after the first NDAT card containing current option 1, 2 or 3. The current angles transmitted are retained until the appearance of an ANG card in another parametric study source deck.
ANC	Used to change anchor data. See Note.
CAB	Used to change cable data. See Note.
DCAB	Used to change discrete device on cable data. See Note.
DJNC	Used to change discrete device at junction data. See Note.
EOD	Must be last card in parametric study source deck.

*These cards may be arbitrarily ordered except for the NDAT, Parametric Title, and EOD cards. Note that LUN, JNC, IR, DEN, and EOP cards are not permitted in the parametric study source decks.

NOTE: The array design changes which are permitted are those changing the physical data of the array but not the overall geometric layout of, or the number of discrete devices on, the array. These changes are keyed by matching the card number and type appearing in a parametric study source deck to the card number and type appearing in changes in the array physical data is given below.

Summary of Changes in the Array Physical Data Permitted (P) and Not Permitted (NP)

Card Type	Field Number											
	1	2	3	4	5	6	7	8	9	10	11	12
ANC	NP	NP	NP	P	P	P	Not used					
CAB	NP	NP	NP	NP	NP	P	P	P	P	P	P	P
CONTINUATION CAB	P											
DCAB	NP	NP	NP	1≠2	NP	P	P	P	P	P	P	P
DJNC	NP	NP	NP	NP	NP	P	P	P	Not used			

OVERALL INPUT DECK

The overall input deck consists of a LUN card (optional) specifying the I/O options and the logical unit numbers of the required I/O devices, followed by the cable array source deck (or tape), followed by any number of parametric study source decks, and ended by an EOP card signifying the end of the problem. The form of the overall input deck is given below.

Overall Input Deck

- LUN Card (optional)
 - Cable Array Source Deck (or Tape)
 - Parametric Study Source Decks
- EOP Card

EXAMPLE

1. Compilation of cable array source deck errors only.

```
1000^LUN^^^^^^60^^^^^^61^^^^^^24 (or omit this card)
*****Main Title Card*****
      Cable Array Source Deck (or Tape)
1001^EOP
```

2. Deflections of the source deck cable array due to a current profile.

```
(LUN card omitted)
*****Main Title Card*****
      Cable Array Source Deck (or Tape)
1001NDAT^^^^^^1
*****Parametric Study 1 Title Card*****
1002COMP
1003^VEL
1010^VEL
1011^ANG
1012^EOD
1013^EOP
```

3. Deflections of the source deck cable array due to a current profile and effects of buoyancy changes on these deflections.

```
(LUN card omitted)
*****MAIN TITLE CARD*****
Cable Array Source Deck (or Tape) containing a card:
^^^9DJNC^^^^^^3^^^^^^10000.^^^1.95^^^35.3
1001NDAT^^^^^^1
*****Parametric (see note) Study 1 Title Card*****
1002COMP
1003^VEL
1010^VEL
1011^ANG
1012^EOD
1013NDAT^^^^^^1
*****Parametric Study 2 Title Card*****
^^^9DJNC^^^^^^3^^^^^^12500.^^^1.95^^^35.3
1014^EOD
1015^EOP
```

NOTE: In each case unique card numbers were assigned, otherwise an error would have resulted. However, any or all card numbers could have been omitted and no error would result.

ERROR MESSAGES

DECEL1 contains a series of internal error checks to insure that the original cable array is properly reduced to a statically determinate array; the input data are consistent; and the deck is properly structured.

If errors are found, the entire list of input cards is printed; and cards with errors are identified by an error code number. The text of the coded error message is printed after the card listing. All cards are scanned for errors; however, only the first error on a card is detected. A card with a DECEL1 detected error should be scanned visually to check for other errors.

DEFINITION OF ERRORS

Type 0 -

A type 0 error indicates that the card type identifier (Field 2) is not recognizable.

Type 1A - LUN

Field 6 not equal 0 or 1

Type 1B - LUN

Field 8 not equal 0,1,2

Type 1C - LUN

Non-unique numbers assigned to required I/O units.

Type 1A - NJNC

Field 3 greater than 44 or less than 2.

Type 1A - ANC

Field 3 greater than 44 or less than 1.

Type 1A - IR

Field 3 = Field 4.

Type 1B - IR

Fields 3 or 4 greater than 44 or less than 1.

Type 1A - CAB

Field 3 greater than 22 or less than 1.

Type 1B - CAB

Field 4 = Field 5.

Type 1C - CAB

Fields 4 or 5 greater than 44 or less than 1.

Type 1D - CAB

Fields 7, 8 or 9 less than or equal to 0.

Type 1E - CAB

Fields 10 or 11 less than 0

Type 1F - CAB

Field 10=0 and Field 11 not equal 0

Type 1G - CAB

Field 10 not equal 0 and Field 11=0.

- Type 1H - CAB
Field 12 greater than 50 or less than 1.
- Type 1A - DCAB
Field 3 greater than 22 or less than 1.
- Type 1B - DCAB
Field 4 greater than 2 or less than 1.
- Type 1C - DCAB
Field 5 greater than 1000 or less than 1.
- Type 1D - DCAB
Field 4=1 and Field 9 less than or equal to 0.
- Type 1E - DCAB
Field 4=2 and Field 9 not equal 0.
- Type 1F - DCAB
Fields 7,8 or 10 less than 0.
- Type 1A - DJNC
Field 3 greater than 44 or less than 1.
- Type 1B - DJNC
Field 7 or 8 less than 0.
- Type 1A - DEN
Field 3 less than 0.
- Type 1A - NDAT
Field 3 not equal 0,1, or 2.
- Type 1A - COMP
Field 3 less than or equal 0.
- Type 1A - ANG
Field 4 less than or equal 0.
- Type 1B - ANG
Field 5 less than Field 3.
- Type 2A - ANC
The junction number assigned to the anchor (Field 3) has been assigned to a preceding ANC card or to an S=L junction (Field 5) on a preceding CAB card.
- Type 2A - CAB
The junction number assigned to the S=L junction (Field 5) has been assigned on a preceding CAB card or to an anchor junction (Field 3) on a preceding ANC card.
- Type 3 - CAB
A Type 3 error appears only in conjunction with a CAB card and indicates that the number assigned to the cable (Field 3) has been assigned on a preceding CAB card.
- Type 4A - IR
The junction number assigned in Field 3 has been assigned in Fields 3 or 4 of a preceding IR card.

- Type 4B - IR
The junction number assigned in Field 4 has been assigned in Field 3 of a preceding IR card.
- Type 6A - NJNC
An NJNC card has previously appeared in the particular source deck.
- Type 6A - DEN
A DEN card has previously appeared in the particular source deck.
- Type 6A - COMP
A COMP card has previously appeared in the particular source deck.
- Type 6A - VEL
Twenty-five VEL cards have previously appeared in the particular source deck.
- Type 6B - VEL
The Z-coordinate at which the current velocity is specified (Field 3) has been used on a preceding VEL card in the particular source deck.
- Type 7 -
A Type 7 error indicates an inadequacy of information in cable array source deck (or tape). The other information column under the error heading contains a 1x3 matrix, the elements of which give respectively the number of NJNC cards read, the number of DEN cards read, and the number of ANC cards read. A zero element is an error (see cable array source deck).
- Type 8 -
A Type 8 error indicates a discontinuity in numbering the cables in the array. The other information column under the error heading contains a 1x22 matrix, the elements of which contain one or zero indicating, respectively, the use or non-use of the corresponding column number as a cable number. Zeros interspersed with ones are in error (see array description).
- Type 9 -
A Type 9 error indicates a discontinuity in numbering the junctions in the array. The other information column under the error heading contains a 1x44 matrix, the elements of which contain one or zero indicating respectively, the use or non-use of the corresponding column number as a junction number. Zeros interspersed with ones are in error (see array description and reduction to a statically determinate array).
- Type 11 -
A Type 11 error indicates an improper reduction of the original cable array to a statically determinate array or an absence of certain input cards in the cable array source deck (or tape). The other information column

under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of CAB cards read, the number of ANC cards read, the number of junctions in the original cable array (Field 3 of the NJNC card), the number of required cuts (Eq. (1)) calculated from the preceding information, and the number of IR cards read. Column 5 not equal to column 4 is an error (see reduction to a statically determinate array).

Type 12A - IR

The junction number assigned in Field 3 is less than or equal to the number of junctions in the original (unreduced) array (Field 3 of the NJNC card).

Type 12B - IR

The junction number assigned in Field 3 is greater than the number of junctions in the original (unreduced) array plus the number of cuts made in reducing the array (Eq. (1)).

Type 12C - IR

The junction number assigned in Field 4 is greater than the number of junctions in the original (unreduced) array.

Type 12A - CAB

The junction number assigned in Field 4 is greater than the number of junctions in the original (unreduced) array (Field 3 of the NJNC card) plus the number of cuts made in reducing the array (Eq. (1)).

Type 12A - DCAB

The cable number assigned in Field 3 does not correspond to a cable number assigned to a cable (Field 3 of the CAB cards).

Type 12B - DCAB

The distance of the discrete device from the S=0 junction of the cable (Field 10) is greater than or equal to the length of the corresponding cable (Field 9 of the CAB card).

Type 12A - DJNC

The junction number assigned in Field 3 does not correspond to either a junction number assigned to an anchor (Field 3 or the ANC cards) or a junction number assigned to an S=L junction of a cable (Field 5 of the CAB cards).

Type 13 -

A Type 13 error indicates that the original cable array has not been properly reduced to a statically determinate array or that junctions have been improperly numbered. The other information column under the error heading contains the message, improper array reduction or junction numbering. Check tree representation of array (see array reduction section of Users Manual) against junction numbering on ANC and CAB cards.

Type 14A -

A Type 14 error indicates an inadequacy of information in a parametric study source deck. The other information column under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of COMP cards read, the current field option, the number of VEL cards read, the number of VEL cards containing a Z-coordinate (Field 3) less than or equal to the minimum Z-coordinate transmitted by the ANC cards (Field 6 of the ANC cards), and the number of ANG cards read. If column 1 contains a zero, then a COMP card has not appeared after the first NDAT card (see parametric study source decks).

Type 14B -

A Type 14 error indicates an inadequacy of information in a parametric study source deck. The other information column under the error heading contains a 1x5 matrix, the elements of which give, respectively, the number of COMP cards less than or equal to the minimum Z-coordinate transmitted by the ANC cards (Field 6 of the ANC cards), and the number of ANG cards read. If column 2 contains a one and any of columns 3, 4 or 5 contain a zero, then the standard current field has not been properly formulated (see parametric study source decks and standard current field).

Type 15 -

A Type 15 error indicates that an unpermitted change has been attempted in a parametric study source deck. (See parametric study source decks.)

Type 16 -

A Type 16 error indicates an improper deck structure. See cable array source deck, parametric study source decks, and overall input deck.

Type 17 -

A Type 17 error indicates that the cable array source deck (or tape) contains more than 2150 records. The other information column under the error heading contains the message common/B1/bounds exceeded. See Users Manual. A Type 17 error is readily correctable if the machine being used has sufficient core storage. This correction is achieved by changing the row dimension of DATAT on cards DES025 and INFO22 from 2150 to a number exceeding the number of records in the cable array source deck (or tape). Simultaneously the comparison value on card INP615 must be changed from 2150 to the new row dimension of DATAT.

Type 18 -

A Type 18 error indicates that the accuracy required for the array equilibrium calculations (Field 3 of the COMP card) has not been obtained during the calculations. This is for one of two possible reasons.

- A. Some cable segments have gone slack (that is, the segments have near zero tension. An examination of the tensions printed out in conjunction with a Type 18 error will reveal if this is the reason. If it is, see the section on statically unstable cable arrays in Reference 2 for possible remedial actions. If it is not then ...
- B. The accuracy required for the equilibrium calculations is simply too stringent for the computer to handle (see COMP card). An examination of the final value of the accuracy obtained, printed out in conjunction with a Type 18 error, will reveal the best accuracy obtainable. Field 3 of the COMP card should be modified to reflect this information.

ARRAY DESCRIPTIVE OUTPUT

Following each error-free reading of a parametric study source deck, DECEL1 transmits to the line printer a description of the physical characteristics of the cable array under study. This printout includes anchor junctions and locations, information concerning the reduction of the original cable array to a statically determine array, properties of the cables in the array, properties of the discrete devices located at array junctions total number of Type 1 and 2 devices, current field option and current profile and calculational accuracy requirements.

The format of the array descriptive output is self-explanatory. A sample printout is given in Appendix A.

STRUCTURAL OUTPUT

If output option 0 or 2 is selected, DECEL1 transmits to the line printer a structural output. The structural printout follows and refers to the array characterized in the array descriptive output and contains information giving:

- a. A description of the current field (i.e., no current or current from xxx degrees)
- b. The cable forces and angles at each anchor
- c. The position coordinates of the original (unreduced) array junctions, the displacement of these coordinates from the no-current coordinates, and the cable forces and angles at each junction
- d. The maximum and minimum tensions and their locations for each array cable and the maximum displacement from the no-current condition and its location for each cable
- e. The position coordinates, the displacement of these coordinates from the no-current coordinates, and the tension at each Type 1 and 2 DCAB device in the array

This latter information is printed out in the same order that the Type 1 and 2 DCAB devices are numbered. Note that it is possible to obtain the latter information for any point on any cable in the array by defining a "dummy" Type 2 DCAB device to be located at the point. A dummy Type 2 DCAB device is simply one for which fields 6, 7, and 8 of the DCAB card are left blank so that the "device" has no effect on the array equilibrium calculations.

The format of the structural output is self-explanatory. A sample printout is given in Appendix A (Figure 17).

DEVICE LOCATION OUTPUT

If output option 1 or 2 is selected, DECEL1 transmits to tape or cards a device location output. The device location output contains information giving:

1. A description of the current field (i.e., no current or current from xxx degrees)
2. The position coordinates of each Type 1 and 2 discrete device in the array

Four types of records are associated with the device location output. Each of these records is written with the format:

(A4,I4,3F10.2)

REC Record

Field	Format	Contents
1	A4	^REC
2	I4	Record number
3	F10.2	Not used
4	F10.2	Not used
5	F10.2	Not used

NOTE: The REC record is used to identify the cable array under study. The record number (Field 2) is referenced in the array descriptive output in the statement, "DEVICE LOCATION OUTPUT RECORD XX REFERS TO THIS ARRAY." The information following a REC record refers to the identified array.

CUR Record

Field	Format	Contents
1	A4	^CUR
2	I4	0 if no current acting on array 1 if current is acting on array
3	F10.2	Blank if Field 2 = 0 Current angle if Field 2 = 1
4	F10.2	Not used
5	F10.2	Not used

NOTE: The CUR record is used to describe the current field (i.e., no current or current from xxx degrees). The information following a CUR record refers to the identified current field.

DEV Record

Field	Format	Contents
1	A4	^DEV
2	I4	Discrete device index (Field 5 of the DCAB and DJNC cards)
3	F10.2	X coordinate of device
4	F10.2	Y coordinate of device
5	F10.2	Z coordinate of device

NOTE: The DEV records are used to transmit the position coordinates of the Type 1 and 2 discrete devices in the array. There is one DEV record for each indexed (Types 1 and 2) device for each identified current field.

EOP Record

Field	Format	Contents
1	A4	^EOP
2	I4	Not used
3	F10.2	Not used
4	F10.2	Not used
5	F10.2	Not used

NOTE: The EOP record is used to signify the end of output transmission.

A typical overall device location output file is illustrated below.

```
^REC^^^1
^CUR^^^0
    DEV Records (one for each indexed device)
^CUR^^^1 current angle
    DEV Records
^CUR^^^1 current angle
    DEV Records
^REC^^^2
^CUR^^^0
    DEV Records
^EOP
```

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6. B. W. Wilson, "Elastic Characteristics of Moorings," Waterways and Harbors Div., ASCE, (Nov 1967), 93 (No. WW4), pp. 27-56.
7. Civil Engineer Laboratory, Technical Report R-848, Seafloor construction experiment, SEACON II - an instrument tri-moor for evaluating undersea cable structure technology by T. R. Kretschmer, G. A. Edgerton, and N. D. Albertsen, Port Hueneme, Calif., Dec 1976.

Appendix A
EXAMPLE PROBLEM

An example problem has been included both to illustrate actual input and output and as a test case. The test case can be used to confirm proper operation of DECEL1 when implemented on a particular host computer. The test case structure is shown in Figure 13. The structure represents an acoustic array in the horizontal leg; this leg has been buoyed at the center to keep it approximately horizontal. A signal cable rises from one anchor to a subsurface buoy. The applied current is unidirectional with the profile shown in Figure 14. The current is acting broadside to the structure. The DECEL1 model of the structure is shown in Figure 15; other details of the modeling are shown in Tables 4 through 8.

Input card images are shown in Figure 16. Note that one dummy-DCAB-device card was intentionally placed "out of sequence" just after the NJNC card. This illustrates that the card sequence is essentially arbitrary, except as noted elsewhere in the manual.

The output from DECEL1 is shown in Figures 17 and 18. Note that the "number of indexed devices" count includes the three DJNC devices. The "Array Equilibrium with no Current" portion defines both the initial positions of devices and the properties of the DCAB devices. If the "do not print" flag had been set on any DCAB card, that device would not have been tabulated here; however, its effects would have been accounted for in the solution.

In the portion of the output where the current was applied (Figure 18), the displacement of all junctions and devices is listed relative to the present no-current position and relative to the original no-current case. In this case both displacements are identical since the new no-current reference flag had not been set on the NDAT card.

Figure 19 shows the configuration of the array both in the no-current condition (dotted lines) and with current applied (solid lines). For this plot the default perspective view angles were used. Other views (plan or elevation) of the same structure in the same current could be obtained by additional identical NDAT cases with the perspective plotting angles changed accordingly.

Table 4. Cables

Cable No.	Junction		Length (ft)	Weight/Foot (lb/ft)	Diameter (in.)	Drag Coefficient
	From	To				
1	1	2	3,000	0.25	1.0	1.4
2	2	8	3,000	0.25	1.0	1.4
3	2	4	5,000	0.20	0.75	1.4
4	4	9	3,000	0.25	1.0	1.4
5	4	10	3,000	0.25	1.0	1.4
6	9	7	4,000	0.3	1.25	1.4

Table 5. Anchor Locations

Anchor No.	Junction No.	x	y	z
1	1	0	1,000	0
2	3	0	-1,000	0
3	5	7,000	-1,000	0
4	6	7,000	1,000	0

Table 6. Imaginary Reaction Cuts

Junction No.	Cut No.
3	8
5	9
6	10

Note: In the model the cables terminate at cuts rather than at anchors.

Table 7. DJNC Devices

Device Junction No.	Device Buoyancy (lb)	Device Drag Coefficient	Device Frontal Area (ft ²)
2	3,000	1.0	26.0
4	3,000	1.0	26.0
7	3,000	1.0	26.0

Table 8. DCAB Devices

Device Index	On Cable No.	S Coordinate (ft)	Device Buoyancy (lb)
9	3	2,500	1,000

Note: Other dummy devices are used to obtain a printout of the spatial location of the device; these devices have not been tabulated here. Dummy devices have a very small weight and no drag.

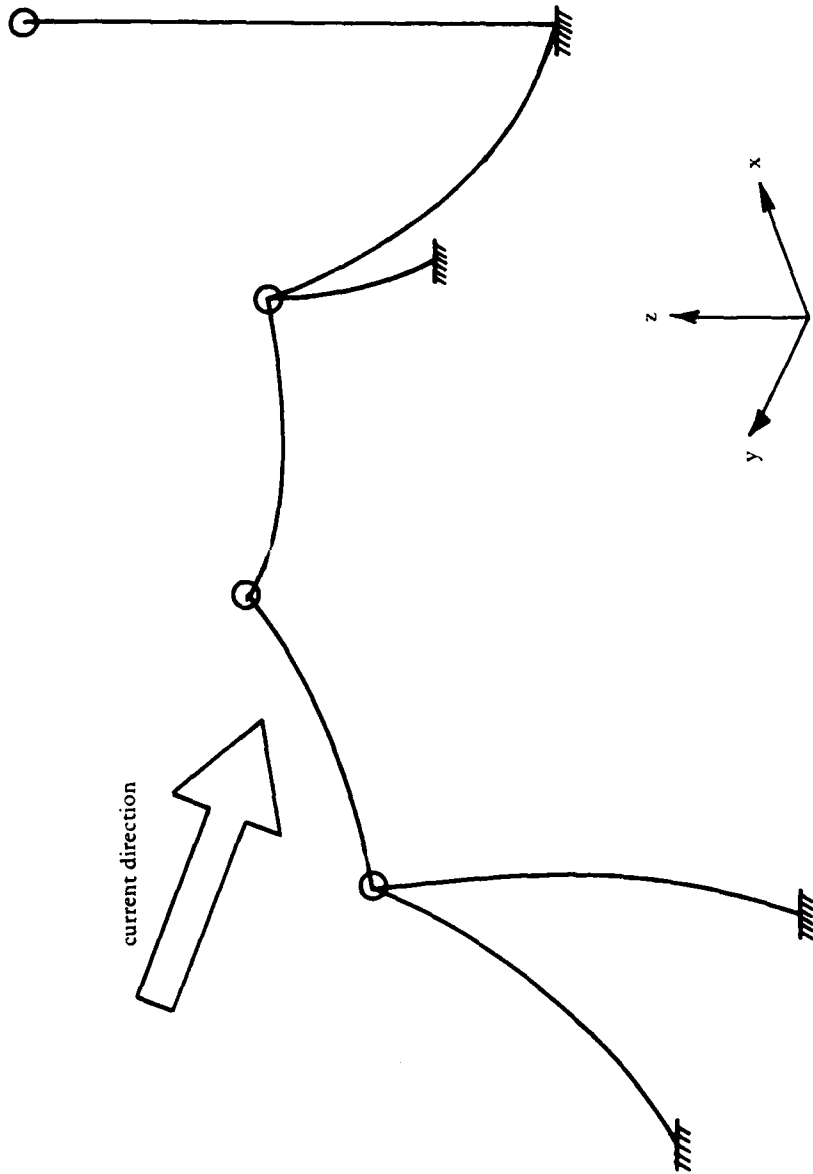


Figure 13. DECEL1 test case structure.

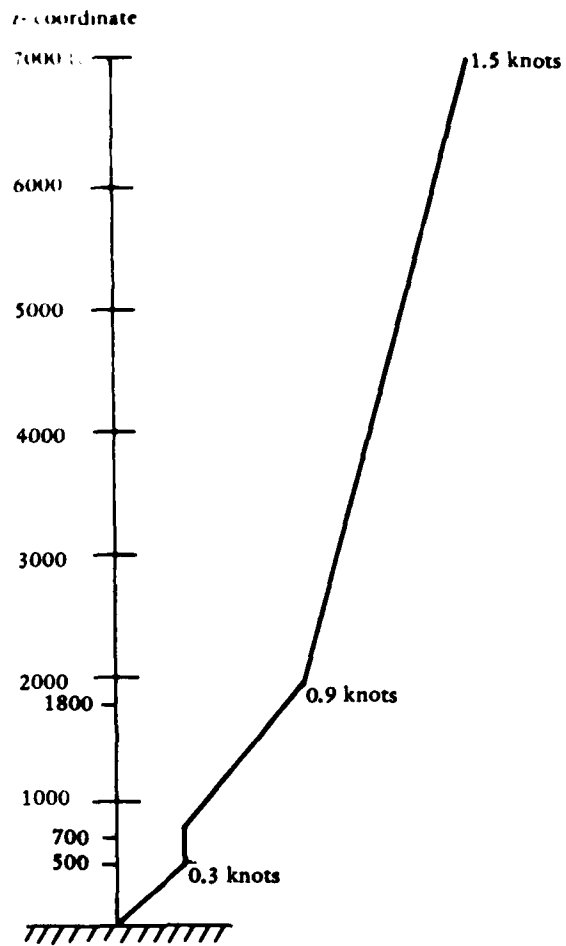


Figure 14. Current profile.

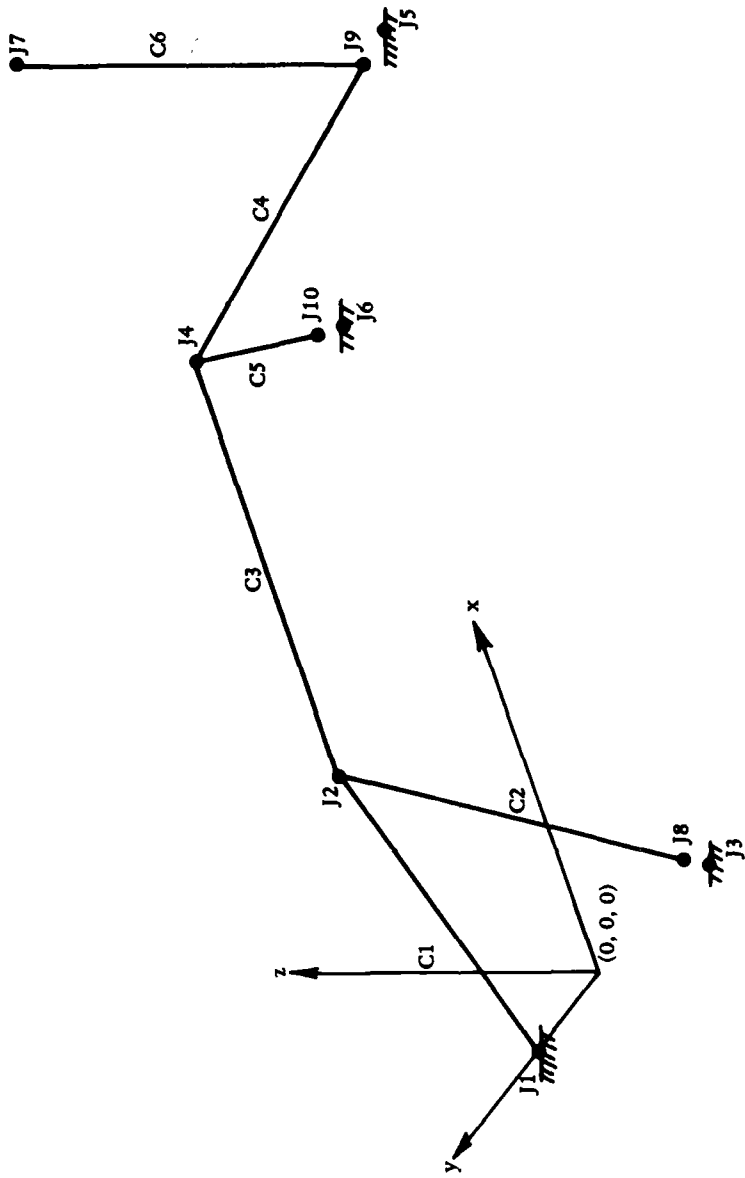


Figure 15. DECEL1 test case structure model.

UECFI TEST CASE

NJNC	7								
DCAB	1	2		0.001		0.01		750.	
ANC	1	0.0	1000.	0.0					
ANC	3	0.0	-1000.	0.0					
ANC	5	7000.0	-1000.	0.0					
ANC	6	7000.0	1000.	0.0					
IR	8	3							
IR	9	5							
IR	10	6							
CAB	1	1	2	-0.25	1.4	1.0	3000.		50
0.03 CAB									
CAH	2	2	8	-0.25	1.4	1.0	3000.		50
0.03 CAB									
CAB	3	2	4	-0.20	1.4	0.75	5000.		50
0.03 CAB									
CAB	4	4	9	-0.25	1.4	1.0	3000.		50
0.03 CAB									
CAB	5	4	10	-0.25	1.4	1.0	3000.		50
0.03 CAB									
CAB	6	9	7	-0.30	1.4	1.25	4000.		50
0.03 DCAB	1	2		0.001		0.01		1500.	
DCAB	1	2		0.001		0.01		2250.	
DCAB	2	2		0.001		0.01		750.	
DCAB	2	2		0.001		0.01		1500.	
DCAB	2	2		0.001		0.01		2250.	
DCAB	3	2		0.01		.1		1000.	
DCAB	3	2		0.01		.1		2000.	
DCAB	3	2		1000.	1.	5.		2500.	
DCAB	3	2		0.01		.1		3000.	
DCAB	3	2		0.01		.1		4000.	
DCAB	4	2		0.001		0.01		750.	
DCAB	4	2		0.001		0.01		1500.	
DCAB	4	2		0.001		0.01		2250.	
DCAB	5	2		0.001		0.01		750.	
DCAB	5	2		0.001		0.01		1500.	
DCAB	5	2		0.001		0.01		2250.	
DCAB	6	2		0.001		0.01		1000.	
DCAB	6	2		0.001		0.01		2000.	
DCAB	6	2		0.001		0.01		3000.	
DJNC	2			3000.	1.0	26.			
DJNC	4			3000.	1.0	26.			
DJNC	7			3000.	1.0	26.			
DEFN	1.59								
END									
NDAT	1								
APPLY 90 DEGREE CURRENT (TOWARD -Y AXIS)									
COMP	0.1								
VEL	0.0	0.0							
VFL	500.0	0.3							
VEL	700.0	0.3							
VEL	1800.0	0.9							
VEL	7000.0	1.5							
ANG	90.	1.	90.						
PPLT	2								
FCD									
ECP									

Figure 16. Input card images.

DECEL1 UPDATE INFORMATION

THIS IS THE JANUARY 1980 VERSION OF DECEL1 AS DESCRIBED IN THE USERS MANUAL
NO UPDATES HAVE BEEN ADDED

NO ERRORS DETECTED

DECEL1 TEST CASE

APPLY 90 DEGREE CURRENT (ICWAKU -Y AXIS)

PHYSICAL CHARACTERISTICS OF THE STRUCTURAL CABLE ARRAY

PHI= 0.00

SINCE PHI=0, THE MAGNETIC AND ARRAY REFERENCED COORDINATE SYSTEMS ARE IDENTICAL.

ALL X,Y,Z RESULTS AND DISPLACEMENTS ARE GIVEN IN TERMS OF THE ARRAY FIXED COORDINATE SYSTEM.

NO. OF ANCHORS IS 4

JUNCTION NO.	X-COORDINATE	Y-COORDINATE	Z-COORDINATE
1	0.00	1000.00	0.00
2	0.00	-1000.00	0.00
3	7000.00	-1000.00	0.00
4	7000.00	1000.00	0.00

NO. OF JUNCTIONS IN ORIGINAL ARRAY IS 7

NO. OF CUTS MADE IN ORIGINAL ARRAY IS 3

JUNCTION NO.	JUNCTION NO.
OF CUT	AT WHICH CUT MADE
4	3
5	5
6	6

Figure 17. Output from DECEL1 for the example problem.

NO. OF CABLES IS 6

CABLE NO.	S#0 JUNC	S#L JUNC	LENGTH	DIAMETER	WEIGHT/LENGTH	NORM DRAG COEFFICIENT	RIGIDITY	CONSTITUTIVE EXPONENT	NO. OF ELEMENTS	TANG DRAG COEFFICIENT
1	1	2	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
2	2	8	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
3	2	4	5000.00	.750	-.200	1.400	0.	0.000	50	.030
4	4	9	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
5	4	10	3000.00	1.000	-.250	1.400	0.	0.000	50	.030
6	9	7	4000.00	1.250	-.300	1.400	0.	0.000	50	.030

PROPERTIES OF THE DEVICES LOCATED AT JUNCTIONS ARE AS FOLLOWS

DEVICE JUNC. NO.	DEVICE WEIGHT	DEVICE COEFFICIENT	DEVICE AREA	FRONTAL AREA
2	3000.00	1.000	26.00	26.00
4	3000.00	1.000	26.00	26.00
7	3000.00	1.000	26.00	26.00

TOTAL NO. OF INDEXED DEVICES IS 20

ACCURACY REQUIRED IN CALCULATIONS IS .1000
DECEL TEST CASE

ARRAY EQUILIBRIUM WITH NO CURRENT

ARRAY ANCHORS

JUNC. NO. OF ANCHOR	CABLE AT ANCHOR	TENSION AT ANCHOR	X-COMP	Y-COMP	Z-COMP	MOR.-COMP	CABLE ANGLES WRT X-Y-PLANE
1	1	974.87	466.84	-420.50	745.39	628.30	-42.01 49.87
3	2	974.89	466.85	420.50	745.41	628.31	42.01 49.87
5	4	983.22	-466.83	423.53	754.60	630.33	137.78 50.13
6	5	983.28	-466.86	-423.53	754.65	630.35	-137.78 50.13

ARRAY CABLES

CABLE NO.	MAXIMUM TENSION	S-COORD OF TENSION	MINIMUM TENSION	S-COORD OF MINIMUM TENSION
1	1622.02	3000.00	574.87	0.00
2	1622.04	0.00	974.89	3000.00
3	1054.82	2500.00	933.69	46.01
4	1631.29	0.00	983.22	3000.00
5	1631.35	0.00	983.28	3000.00
6	3000.00	4000.00	1800.00	0.00

Figure 17. Continued.

ARRAY JUNCTIONS

JUNC. NO.	CABLE AT JUNCTION	TENSION AT JUNCTION	CABLE ANGLES WRT			JUNCTION LOCATION		
			X-AXIS	XY-PLANE	XY-PLANE	X-COORD	Y-COORD	Z-COORD
1	1	1622.02	137.99	-67.21	1110.22	-2.00	2588.59	
2	2	1652.04	-137.99	-67.21				
3	3	933.74	.00	-56				
4	4	1631.29	-180.00	.57	5897.72	.02	2592.27	
5	5	1631.35	-62.22	-67.27				
6	6	3000.00	42.21	-67.27				
7			0.00	-90.00	7000.00	-1000.00	4000.00	

INDEXED DEVICES ALONG ARRAY CABLES

DEVICE INDEX	CABLE NO.	S COORDINATE	TENSION AT DEVICE			DEVICE LOCATION			DEVICE HEIGHT	DEVICE LENGTH	NORMAL DMAG CU	TANG DRAG CO
			X-COORD	Y-COORD	Z-COORD	X-COORD	Y-COORD	Z-COORD				
1	1	750.00	1124.74	1284.54	1450.98	334.42	698.78	599.49	.00	0.00	0.000	0.000
2	1	1500.00	1284.54	1450.98	1450.98	625.66	436.45	1238.66	.00	0.00	0.000	0.000
3	1	2250.00	1450.98	1450.98	1450.98	882.06	205.51	1904.42	.00	0.00	0.000	0.000
4	2	750.00	1451.00	1284.56	1284.56	882.06	-205.51	1904.42	.00	0.00	0.000	0.000
5	2	1500.00	1284.56	1284.56	1284.56	625.66	-436.45	1238.66	.00	0.00	0.000	0.000
6	2	2250.00	1124.76	1284.56	1284.56	334.41	-698.79	599.49	.00	0.00	0.000	0.000
7	3	1000.00	952.99	1012.17	1012.17	2103.66	.00	2684.83	.01	0.00	0.000	0.000
8	3	2000.00	1012.17	1012.17	1012.17	3057.19	.01	2980.75	.01	0.00	0.000	0.000
9	3	2500.00	1054.82	1054.82	1054.82	3509.25	.01	3193.98	1000.00	0.00	0.000	0.000
10	3	3000.00	1019.43	1019.43	1019.43	3958.20	.01	3020.73	.01	0.00	0.000	0.000
11	3	4000.00	956.85	956.85	956.85	4906.32	.01	2707.82	.01	0.00	0.000	0.000
12	4	750.00	1460.14	1460.14	1460.14	8124.52	-215.74	1907.72	.00	0.00	0.000	0.000
13	4	1500.00	1293.56	1293.56	1293.56	6375.21	-436.45	1241.34	.00	0.00	0.000	0.000
14	4	2250.00	1133.51	1133.51	1133.51	6666.31	-699.02	601.17	.00	0.00	0.000	0.000
15	5	750.00	1460.21	1460.21	1460.21	6124.52	205.77	1907.72	.00	0.00	0.000	0.000
16	5	1500.00	1293.61	1293.61	1293.61	6379.21	436.42	1241.34	.00	0.00	0.000	0.000
17	5	2250.00	1133.57	1133.57	1133.57	6666.31	699.09	601.16	.00	0.00	0.000	0.000
18	6	1000.00	2100.00	2100.00	2100.00	7000.00	-1000.00	1000.00	.00	0.00	0.000	0.000
19	6	2000.00	2400.00	2400.00	2400.00	7000.00	-1000.00	2000.00	.00	0.00	0.000	0.000
20	6	3000.00	2700.00	2700.00	2700.00	7000.00	-1000.00	3000.00	.00	0.00	0.000	0.000

Figure 17. Continued.

DECEL1 TEST CASE

APPLY 90 DEGREE CURRENT (TOWARD -Y AXIS)

NUMBER OF ITERATIONS FOR CONVERGENCE - 12

CURRENT FIELD OPTION IS 1

Z-COORDINATE OF CURRENT (FEET)	MAGNITUDE OF CURRENT AT Z (KNOTS)	DIRECTION OF CURRENT AT Z FROM N-AXIS (DEGREES)
0.00	0.000	0.000
500.00	.300	0.000
700.00	.300	0.000
1000.00	.900	0.000
7000.00	1.500	0.000

*****CURRENT DIRECTION IS POSITIVE IN THE CLOCKWISE SENSE FROM THE N-AXIS*****

ARRAY EQUILIBRIUM WITH 270.00 DEGREE CURRENT

ARRAY EQUILIBRIUM WITH CURRENT DIRECTION
270.00 DEGREES FROM X-AXIS(+ IS COUNTERCLOCKWISE)
90.00 DEGREES FROM N-AXIS(+ IS CLOCKWISE)

ARRAY ANCHORS

JUNC. OF ANCHOR	CABLE AT ANCHOR	TENSION AT ANCHOR	X-COMP	Y-COMP	Z-COMP	HCR	MCR	COMP	ANGLE WRT XY-PLANE
1	1	2120.84	921.12	-1197.18	1488.71	1510.53	94.79	9.64	-52.42
3	2	105.56	93.45	15.88	-46.45	94.79	9.64	-26.10	44.58
5	4	104.64	-92.76	15.83	-45.78	94.10	9.64	-25.94	44.58
6	5	2135.04	-921.38	-1202.57	1509.41	1514.96	94.10	9.64	-127.46

ARRAY CABLES

CABLE NO.	MAXIMUM TENSION	S-COORD CF	MINIMUM TENSION	MAXIMUM DISP.	S-COORD CF	LOCATION OF THIS POINT	NO CURRENT	LOC. OF TWIS POINT
						X-COORD Y-COORD Z-COORD	X-COORD Y-COORD Z-COORD	X-COORD Y-COORD Z-COORD
1	2704.86	3000.00	2120.84	486.17	3000.00	1172.55 -421.42 2354.31	1110.22 -1.00 2588.59	1110.22 -1.00 2588.59
2	696.33	0.00	94.79	576.02	970.69	1027.61 -730.14 1451.71	809.61 3510.22 809.61	809.61 3510.22 809.61
3	1274.32	2500.00	1175.90	1098.62	2501.10	3508.36 -1038.93 2825.89	3510.22 3510.22 3510.22	3510.22 3510.22 3510.22
4	696.81	0.00	94.10	574.10	970.61	5978.03 -738.15 1457.38	6196.28 6196.28 6196.28	6196.28 6196.28 6196.28
5	2720.35	0.00	2135.04	463.26	0.00	5834.45 -418.76 2359.53	5897.72 5897.72 5897.72	5897.72 5897.72 5897.72
6	3001.43	4000.00	1891.74	1363.45	4000.00	7000.00 -2333.47 3715.67	7000.00 7000.00 7000.00	7000.00 7000.00 7000.00

Figure 18. Output from DECEL1.

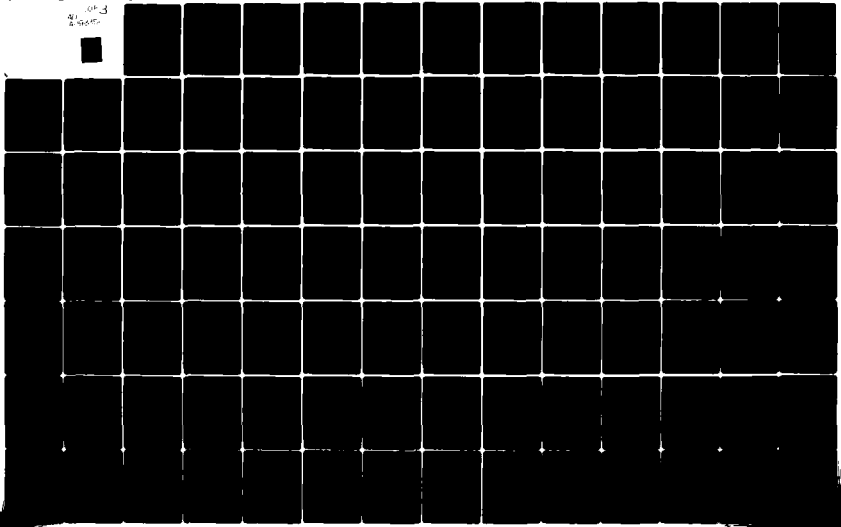
AD-A093 356

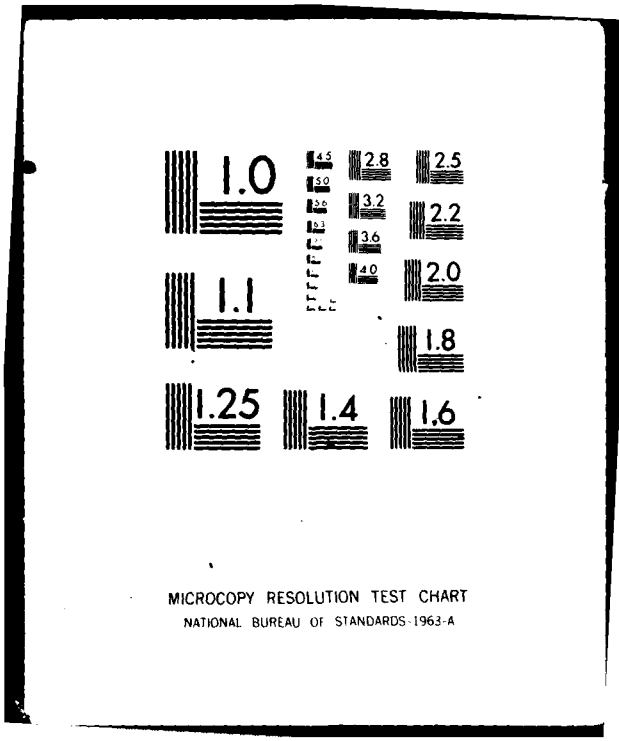
CIVIL ENGINEERING LAB (NAVY) PORT HUENEME CA F/G 13/13
DECEL1 USERS MANUAL. A FORTRAN IV PROGRAM FOR COMPUTING THE STA--ETC(U)
AUG 80 S SERGEV
CEL-TN-1584

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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

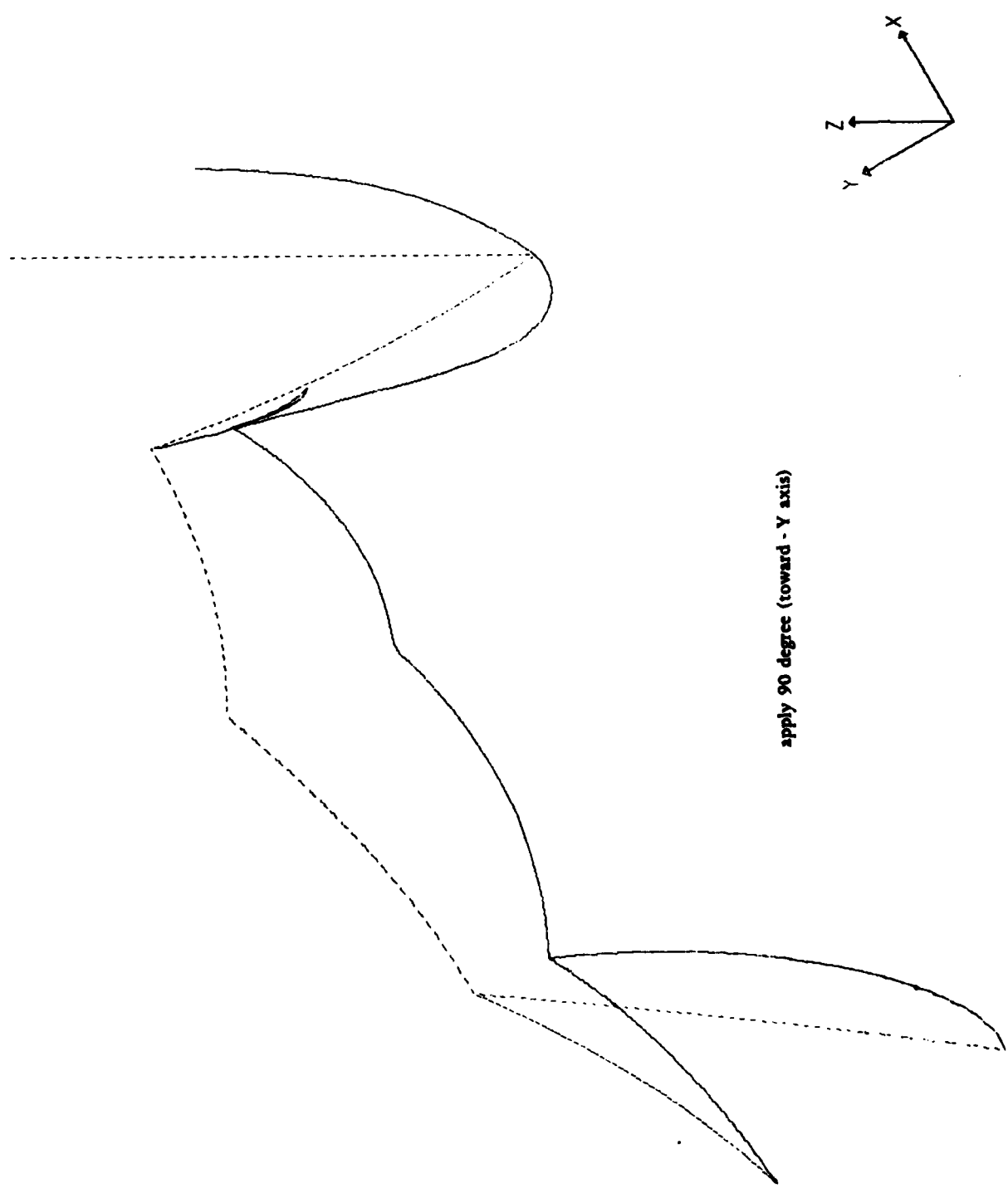
ARRAY JUNCTIONS		CABLE AT		TENSION AT		CABLE ANGLES WRT		JUNCTION LOCATION			DISP FROM NO CURRENT			DISP 1 JM ORIG NO CURRENT			
JUNC. NO.	CABLE AT JUNCTION	TENSION AT JUNCTION	X-AXIS	XY-PLANE	WRT XY-PLANE	X-COORD	Y-COORD	Z-COORD	X-DISP	Y-DISP	Z-DISP	X-DISP	Y-DISP	Z-DISP	X-DISP	Y-DISP	Z-DISP
2	2	696.39	-10.61	-63.07	-63.07	117.55	-421.42	2354.31	62.33	-421.42	-236.28	62.33	-421.42	-236.28	62.33	-421.42	-236.28
2	3	1183.16	-27.14	-1.28	-1.28	5834.45	-418.76	2359.53	-63.27	-418.76	-232.74	-63.27	-418.76	-232.74	-63.27	-418.76	-232.74
4	3	1183.49	-152.72	-0.50	-0.50												
4	4	696.11	-75.56	-63.00	-63.00												
4	5	272.35	43.31	-60.55	-60.55												
7	6	3181.43	90.00	-88.23	-88.23	7000.00	-2333.47	3715.67	.00	-1333.47	-264.34	.00	-1333.47	-264.34	.00	-1333.47	-264.34

INDEXED DEVICES ALONG ARRAY CABLES

INDEX	CABLE NO.	S COORDINATE	TENSION AT DEVICE			DEVICE LOCATION			DISP FROM NO CURRENT			DISP FROM ORIG NO CURRENT		
			X-COORD	Y-COORD	Z-COORD	X-COORD	Y-COORD	Z-COORD	X-DISP	Y-DISP	Z-DISP	X-DISP	Y-DISP	Z-DISP
1	1	750.00	2256.30	589.93	542.51	-18.43	-108.85	-56.97	-18.43	-108.85	-56.97	-18.43	-108.85	-56.97
2	1	1500.00	2398.83	614.23	1115.20	-11.43	-227.84	-123.46	-11.43	-227.84	-123.46	-11.43	-227.84	-123.46
3	1	2250.00	2547.87	898.33	1718.08	16.27	-340.47	-186.34	16.27	-340.47	-186.34	16.27	-340.47	-186.34
4	2	750.00	521.60	1067.69	1662.67	185.63	-482.83	-241.75	185.63	-482.83	-241.75	185.63	-482.83	-241.75
5	2	1500.00	341.51	906.55	943.19	280.89	-363.78	-295.48	280.89	-363.78	-295.48	280.89	-363.78	-295.48
6	2	2250.00	169.94	620.14	-894.13	285.72	-195.35	-342.41	285.72	-195.35	-342.41	285.72	-195.35	-342.41
7	3	1000.00	1193.47	2092.39	-802.26	2417.37	-11.28	-802.26	-11.28	-802.26	-267.46	-11.28	-802.26	-267.46
8	3	2000.00	1239.35	3040.22	-1006.85	2650.43	-16.97	-1006.86	-16.97	-1006.86	-330.32	-16.97	-1006.86	-330.32
9	3	2500.00	1214.32	3507.35	-1034.92	2825.47	-1.90	-1034.93	-1.90	-1034.93	-368.51	-1.90	-1034.93	-368.51
10	3	3000.00	1245.35	3972.33	-1007.15	2683.28	14.13	-1007.16	14.13	-1007.16	-337.45	14.13	-1007.16	-337.45
11	3	4000.00	1196.75	4916.46	-801.46	2436.58	10.14	-801.48	10.14	-801.48	-271.24	10.14	-801.48	-271.24
12	4	750.00	522.08	5938.34	-686.98	1668.23	-186.18	-481.25	-186.18	-481.25	-239.48	-186.18	-481.25	-239.48
13	4	1500.00	341.95	6098.03	-819.88	948.62	-281.18	-383.08	-281.18	-383.08	-292.72	-281.18	-383.08	-292.72
14	4	2250.00	170.11	6381.92	-894.01	261.42	-286.39	-194.93	-286.39	-194.93	-339.74	-286.39	-194.93	-339.74
15	5	750.00	2563.14	6107.12	-132.76	1722.43	-17.40	-338.53	-17.40	-338.53	-185.29	-17.40	-338.53	-185.29
16	5	1500.00	2413.83	6389.56	210.20	1118.42	10.35	-226.63	10.35	-226.63	-122.92	10.35	-226.63	-122.92
17	5	2250.00	2270.95	6686.00	590.79	544.31	17.69	-108.30	17.69	-108.30	-56.85	17.69	-108.30	-56.85
18	6	1000.00	2149.66	7000.00	-1507.81	861.12	.00	-507.81	.00	-507.81	-138.88	.00	-507.81	-138.88
19	6	2000.00	2419.27	7000.00	-1930.95	1766.54	.00	-930.95	.00	-930.95	-233.46	.00	-930.95	-233.46
20	6	3000.00	2704.36	7000.00	-2215.68	2723.92	.00	-1215.68	.00	-1215.68	-276.09	.00	-1215.68	-276.09

ANALYSIS COMPLETED

Figure 18. Continued.



apply 90 degree (toward - Y axis)

Figure 19. Undeformed and deformed configurations of the test case structure.

Appendix B
DECEL1 PROGRAM LISTING


```

58      KDUKMT=0
59      KSUMMY=0
60      KCURT=0
61
62      I1IME=1
63      CALL INPUT TO READ DATA AND IDENTIFY ERRORS
64
65      10 CALL INPUT
66         IF (NOCUR.NE.0.) IFIRST=0
67
68      CHECK TO SEE IF ANY ERRORS IN DATA
69
70      IF (EATE.NE.0.) GO TO 305
71
72      GET HERE IF NO ERRORS -- PRINT OUT PHYSICAL CHARACTERISTICS OF ARR
73
74      ABIEE.(IPRINT,310)
75      CALL PHSOUT
76
77      KMULT IS A MULTIPLIER FOR CHANGING CURRENT ANGLE THETA
78
79      KMULT=0
80      IF (IFIRST.NE.0) GO TO 15
81
82      JUMP=0--NO CURRENT  JUMP=1--CURRENT
83
84      JUMP=0
85      15 IF (I1VOP1.EG.0) GO TO 20
86      KCURT=0
87      THN=THETA+KMULT*THETAS
88      IMETA=360.*PHI-INTN
89      IF TH=0
90         IF (NSTEPS.GT.1) ISTEP=1
91
92      GET HERE TO CALCULATE FORCES AND IF SUCCESSIVE APPROXIMATION ROUTE
93      NOT SATISFIED -- ZERO FORCES
94
95      20 DO 25 J=1,NJUNC
96         DO 25 I=1,IJ
97            FEJUNC(I,J)=0.
98            DO 30 N=1,NCAP
99               INNENQUEIN
100              DO 30 N=1,INNA
101                 DO 30 I=1,IJ
102                    FCAB(I,POINT)=0.
103
104      PICK UP DISCRETE DEVICE DATA FROM TEMPORARY STORAGE TAPE AND
105      CALCULATE DEVICE FORCES -- DJAC FORCES ARE STORED IN FEJUNC --
106      UCAR FORCES IN FCAR -- FORCE(1) IS ROUTINE FOR CALCULATING
107      DEVICE FORCES IN DIRECTION I
108
109      35 READ (INPAP,315) (DATA(K),K=1,10)
110      IF (DATA(2).EG.TEST(3)) GO TO 40
111      IF (DATA(2).EG.TEST(4)) GO TO 50
112      IF (DATA(2).EG.TEST(9)) GO TO 60
113      GO TO 35
114      40) N=DATA(3)

```

```

115 DC 45 J=1,3
116 I=J
117 45 FFJUNC(I,M,K)=FFJUNC(I,M,K)+CFORCE(I,M,DUMMY,KDUMMY)
118 GO TO 35
119 50 N=DATA(I,3)
120 45 DAT(I,3)/H(K)+1.000001
121 DC 55 J=1,3
122 I=J
123 55 FCAB(I,M,K)=FCAB(I,M,K)+CFORCE(I,M,K)
124 GO TO 35
125 C
126 C GET HERE AT END OF TAPE
127 C
128 60 MEWIND INTAPE
129 C
130 C NOW CALCULATE THE FORCE/LENGTH IN DIRECTION I AT NODE M ON CABLE N
131 C (FONCE(I,P,N)) IS ROUTINE FOR DOING THIS -- INTEGRATE BY TRAPEZOIDA
132 C WHILE OVER SEGMENT TO GET TOTAL FORCE AND ADD TO DCAB FORCES
133 C
134 DO 65 J=1,NCAB
135 K=J
136 INRM=NNODE(K)-1
137 DO 65 MM=1,INRM
138 M=MM
139 DO 65 II=1,3
140 65 FCAB(I,M,K)=FCAB(I,M,K)+CFORCE(I,M+1,K)*H(K)*0.5
141 C
142 C ALL FORCES ARE NOW CALCULATED AND EQUILIBRIUM CAN BE DETERMINED
143 C LEAP = 1 FIRST TIME THROUGH IMAGINARY REACTION ROUTINE
144 C LEAP = 2 ANY OTHER TIME
145 C SKIP THIS SECTION IF NO IRAS
146 C
147 IF (NIR.EG.0) GO TO 70
148 IF (JUMP.EG.0) CALL START
149 LEAP=1
150 C
151 C INITIALIZE DELTA
152 C DELTA=DELTA1
153 C
154 C
155 C GET HERE TO INITIALIZE TOTAL FORCES AT THE JUNCTIONS, TFJUNC, AND
156 C IF THE IMAGINARY REACTION ITERATION NOT SATISFIED -- ALSO IF NO IR
157 C
158 DO 75 J=1,3
159 DO 75 I=1,3
160 75 TFJUNC(I,J)=FFJUNC(I,J)
161 C
162 C ADD APPROPRIATE REACTIONS TO TFJUNC -- SKIP THIS SECTION IF NO IRP
163 C
164 IF (NIR.EG.0) GO TO 95
165 DO 90 J=1,3
166 DO 90 K=1,3
167 IF ((J.EQ.1+JUNC(K)) OR (J.EQ.2+JUNC(K))) GO TO 80
168 GO TO 90
169 DO 85 I=1,3
170 85 IF JUNC(I,J)=1F JUNC(I,J)+IR(I,J)

```

86

```

172 96 CONTINUE
173 C
174 C IF JUNC IS NOW DETERMINED, AND THE REACTIVE FORCES IN THE ARRAY, HCA
175 C CAN BE CALCULATED BY SUPPING FROM THE FREE ENDS TO THE FIXED ANCHO
176 C
177 C
178 DC 130 A=1,NCAB
179 IALM=NCAB-I-A
180 KPATH(INDL,K)
181 INN=NODE(K)
182 ILLJ=LJUNC(K)
183 DO 100 I=1,3
184 HCA(I,INN,K)=TFJUNC(I,ILLJ)
185 IF (LJUNC(K).EQ.ZJUNC(L)) GO TO 105
186 GO TO 115
187 DO 110 I=1,3
188 HCA(I,INN,K)=HCA(I,INN,K)+RCAB(I,I,L)
189 115 CONTINUE
190 DO 125 M=1,INNN
191 H=INN+I-M
192 IF (H.EQ.0) GO TO 130
193 DO 124 I=1,3
194 HCA(I,M,K)=HCA(I,M,K)+FCAB(I,M-K)
195 125 CONTINUE
196 130 CONTINUE
197 C
198 C ALL REACTIVE FORCES ARE NOW DETERMINED AND THE CONFIGURATION OF TH
199 C ARRAY, PCAB AND PJUNC, CAN BE FOUND BY INTEGRATING FROM THE FIXED
200 C ANCHOR TO THE FREE ENDS -- INTEGRATION BY THE TRAPEZOIDAL RULE IS
201 C AGAIN USED
202 C
203 DO 155 M=1,NCAB
204 KPATH(M)
205 IALM=LJUNC(M)
206 INN=NODE(K)
207 IAZJ=LJUNC(K)
208 DO 135 I=1,3
209 PCAB(I,INN)=PJUNC(I,INZJ)
210 M=MM
211 DC 145 I=1,3
212 IF (TCAB(M,K).NE.0.) GO TO 140
213 PCAB(I,INN)=PCAB(I,M-K)
214 GO TO 145
215 PCAB(I,M,K)=PCAB(I,M-K)+(EXCAB(M-K)+HCA(I,M,K))/TCAB(M-K)
216 IF (KOUTH.LI.MI/2) GO TO 175
217 145 CONTINUE
218 DC 150 I=1,3
219 PJUNC(I,IALM)=PCAB(I,INN)
220 155 CONTINUE
221 IF (JUMP.EQ.0) GO TO 175
222 IF (KOUTH.LI.MI/2) GO TO 175
223 C 170 M=1,NCAB
224 KPATH(M)
225 IALM=LJUNC(K)
226 INN=NODE(K)
227
228

```

```

230      DC 160 M=1,INM
231      DC 160 I=1,J
232      160 PCAB(I,K,M)=0.5*(PCAB(I,M,K)+PCAB(I,M,K))
233      DO 165 I=1,3
234      165 PJUNC(I,IALN)=PCAB(I,INM)*K
235      170 CONTINUE
236      175 CONTINUE
237      C
238      C ARRAY CONFIGURATION NOW DETERMINED -- CHECK TO SEE IF IT SATISFIES
239      C GEOMETRIC CONSTRAINTS -- SKIP THIS SECTION IF NO IR#S
240      C
241      IF (NIR.EC.0) GO TO 245
242      C
243      C CALCULATE ERROR E
244      C
245      E2=0.
246      DO 180 M=1,NR
247      KIN=IRJUNC(M)
248      DO 180 I=1,J
249      180 E2=E2+(PJUNC(I,KEN)-PJUNC(I,KIN))**2
250      E=ESQRT(E2)
251      C
252      C COMPARE ERROR TO ACCURACY REQUIREMENTS
253      C
254      IF (E.LE.COMPD/10.) GO TO 245
255      C
256      C GET HERE IF GEOMETRIC CONSTRAINTS NOT SATISFIED
257      C
258      GO TO (185,220), LEAP
259      C
260      C GET HERE FIRST TIME THROUGH IMAGINARY REACTION ROUTINE
261      C
262      185 LEAP=2
263      KIN=0
264      EPREV=0.0
265      C
266      C STORE SUCCESSFUL POSITIONS AND REACTIONS
267      C
268      190 FS=F
269      C
270      KIN=KNIN*
271      ALLOW=MAX(F,1/2) ITERATIONS THEN BEGIN THE CHECK FOR SLOW CONVERGENCE
272      IF (NTR.LE.MAXITER/2) GO TO 218 CONVERGENCE - IF THE DISPLACEMENT
273      ERROR IS LARGE COMPARED TO THE CONVERGENCE TOLERANCE AND IS
274      CHANGING SLOWLY - SLOW CONVERGENCE IS INDICATED AFTER MAXITER/2
275      ITERATIONS
276      IF (KNTR.GT.I.AND.E.GT.COMPD*100.AND.EPREV.E.LI.COMPD) GO TO 195
277      LIMIT THE ITERATIONS TO SATISFY THE DISPLACEMENT TOLERANCE AT THE
278      CUTS TO MAXITER
279      IF (NTR.GT.MAXITER) GO TO 200
280      GO TO 210
281      195 WRITE (IPRNT,320) NTR
282      GO TO 205
283      205 WRITE (IPRNT,325) WRITE
284      WRITE (IPRNT,330) TITLE
285      WRITE (IPRNT,335) EPREV,E*COMPD

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286 IPCTVEL=EKCNIV*100.
287 IF (NSTEIS.GT.1) WRITE (IPRNT,340) IPCTVEL
288 WRITE (IPRNT,345)
289 GO TO 300
290 EPRCV=C
291 I=1
292 KEN=EKJUNC(N)
293 NIM=IMJUNC(N)
294 DO 215 I=1,3
295 PJUNCS(I,KEN)=PJUNC(I,KEN)
296 PJUNCS(I,KIN)=PJUNC(I,KIN)
297 IFS(I,KIN)=IFS(I,KIN)
298 GO TO 225
299
300 C GET HERE ANY OTHER TIME THROUGH IMAGINARY REACTION ROUTINE
301 C SEE IF ITERATION SUCCESSFUL
302 C
303 220 IF (E.LT.E5) GO TO 190
304 C
305 C REDUCE DELTA IF NOT SUCCESSFUL INTERATION
306 C
307 DELTA=DELTA/2.
308 C
309 C CALCULATE NEW IMAGINARY AND EQUILIBRATING REACTIONS AND GO BACK TO
310 C RECALCULATE ARRAY EQUILIBRIUM
311 C
312 DO 230 N=1,NIR
313 KEN=EKJUNC(N)
314 DO 231 I=1,3
315 IR(I,KEN)=0.
316 DO 235 N=1,NIR
317 KEN=EKJUNC(N)
318 NIM=IMJUNC(N)
319 DO 235 I=1,3
320 IR(I,KIN)=JRS(I,KIN)*DELTA*(PJUNCS(I,KEN)-PJUNCS(I,KIN))/ES
321 IFS(I,KEN)=IFS(I,KEN)-IR(I,KIN)
322 C
323 C CHECK CHANGES IN IMAGINARY REACTIONS
324 C
325 DO 240 N=1,NIR
326 KIM=IKJUNC(N)
327 DO 241 I=1,3
328 IF (IR(I,KIN).NE.IRS(I,KIN)) GO TO 70
329 C
330 C
331 C MIC CHANGES -- TIME TO QUIT
332 C
333 CALL ERROR
334 GO TO 305
335 C
336 C GET HERE IF ACCURACY REQUIREMENTS SATISFIED OR NO IRFS
337 C OUTPUT EQUILIBRIUM IF NO CURRENT -- IF CURRENT, FIRST CHECK TO SEE
338 C IF ACCURACY REQUIREMENT SATISFIED BY SUCCESSIVE APPROXIMATIONS
339 C
340 C
341 IF (JUMP.C.EQ.0) GO TO 250
342 250 CONTINUE

```

```

343 JUM=JUMP+1
344 GO TO (255,235),JUM
345 IF (OFLG.EQ.0).OR.(OFLG.EQ.2) CALL STROUT
346 IF (KPLT.NE.0.AND.JUM.EQ.1) CALL PERPLT (IVOPT,NCAB,NNODE,PCAB,PC
347 JAM,ITITLE)
348 IF (OFLG.EQ.1).OR.(OFLG.EQ.2) CALL TAPOUT
349 IF (OFLG.EQ.1) GO TO 270
350 IF (JUM.NE.1) GO TO 270
351 UC 25, N=1,NCAB
352 IN=NRNGUE(N)
353 UC 260 M=1,INNN
354 UC 260 I=1,3
355 PCAB(I,M,N)=FCAB(I,M,N)
356 HCAHU(I,M,N)=HCAH(I,M,N)
357 UC 265 N=1,NJUNC
358 UC 265 I=1,3
359 PJUNC(I,N)=PJUNC(I,N)
360 IF (KPLT.NE.0.AND.IVOPT.EQ.0) CALL PERPLT (IVOPT,NCAB,NNODE,PCAB,
361 IPCAB,ITITLE)
362 C
363 C
364 C
365 C
366 C
367 C
368 C
369 C
370 C
371 C
372 C
373 C
374 C
375 UC 260 N=1,NCAB
376 IN=NRNGUE(N)
377 UC 280 M=1,INNN
378 UC 280 I=1,3
379 PCABE(I,M,N)=FCAB(I,M,N)
380 C
381 C
382 C
383 C
384 C
385 C
386 C
387 C
388 C
389 C
390 C
391 C
392 C
393 C
394 C
395 C
396 C
397 C
398 C
399 C

```

```

400 DC 230, J=1, J1
401 UED*(PCAB(I,M,N)-PCAB(I,M,N))**2
402
403 IF NOT ACCURATE STORE CONFIGURATION AND RECALCULATE FORCES
404
405 IF (SQRT(U).GT.COMPD) GO TO 275
406 CONTINUE
407
408 GET HERE IF POSITION ACCURATE AND OUTPUT POSITION
409
410 IF (INCHMT.EQ.1.AND.ISTEP.LT.NSTEPS) CALL STROUT
411 CHECK TO SEE IF CURRENT IS TO BE INCREMENTED
412 IF (NSTEPS.EQ.1) GO TO 285
413 IF (ISTEP.LE.NSTEPS) ISTEP=ISTEP+1
414 IF (ISTEP.GT.NSTEPS) GO TO 255
415 GO TO 275
416
417 GO BACK FOR MORE DATA
418
419
420 300 IFIRST=1
421 NOUNTR=0
422 GO TO 10
423 CONTINUE
424 WRITE (IPRINT,355)
425 GO TO 5
426
427 310 FORMAT (///5X,'BAND ERRORS DETECTED')
428 FORMAT (F4.3,4X,'E15.8')
429
430 320 FORMAT (1P1,23X'SLOW CONVERGENCE AFTER 15,11H ITERATIONS/')
431 325 FORMAT (1P1,18X'CONVERGENCE IN 15,11H ITERATIONS/')
432 330 FORMAT (11H CASE TITLE/1X,10(1H=)/1X,8A10/)
433 335 FORMAT (24H PREVIOUS ERROR VALUE = ,E15.5/24H PRESENT ERROR VALUE
434 1 = ,E15.5/33H ACCEPTABLE ERROR (COMP VALUE) = ,E15.5)
435 340 FORMAT (1/23H PRESENT VALUE OF CURRENT = ,14.22H PERCENT OF FULL VA
436 ILLU)
437 345 FORMAT (//39H PARAMETRIC CASE TERMINATED, SEE MANUAL)
438 350 1 PARAMETRIC CASE TERMINATED/26H BEST ACCURACY OBTAINED = ,E15.4/2
439 27H DESIRED ACCURACY (COMP) = ,E15.4//28H APPROXIMATE RESULTS PRIN
440 31ED/1X,27(1P=)
441 355 FORMAT (1P1)
442 END

```

CARD NO.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM
254	I		AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
341	I	250	THIS IF DEGENERATES INTO A SIMPLE TRANSFER TO THE LABEL INDICATED.
344	I		AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1      *DECK INFURM          INF 1
2      SUBROUTINE INFORM    INF 2
3      =====             INF 3
4      C                    INF 4
5      C                    INF 5
6      C                    INF 6
7      C                    INF 7
8      C                    INF 8
9      C                    INF 9
10     C                    INF 10
11     C                    INF 11
12     C                    INF 12
13     C                    INF 13
14     C                    INF 14
15     C                    INF 15
16     C                    INF 16
17     C                    INF 17
18     C                    INF 18
19     C                    INF 19-

```

THIS SUBROUTINE IS USED TO INFORM THE USER OF UPDATES THAT HAVE BEEN ADDED TO DECEL THAT MAY AFFECT INPUT OR CALCULATIONS OR OUTPUT. ANY NEW UPDATES SHOULD BE DESCRIBED HERE BY ADDING TO THE INFORMATIVE PRINT STATEMENTS

PRINT 5
 PRINT 10
 RETURN

5 FORMAT (1P1,26H DECEL) UPDATE INFORMATION/2X,25(1H=)//
 10 FORMAT (76H THIS IS THE JANUARY 1990 VERSION OF DECEL) AS DESCRIBE
 10 IN THE USERS MANUAL/26H NO UPDATES HAVE BEEN ADDED)

END

```

1  *DECK CFORCE
2  FUNCTION CFORCE (I,M,N)
3
4  C THIS ROUTINE CALCULATES THE FORCE/LENGTH IN DIRECTION I AT NODE M
5  C VIA CABLE N USING THE NORMAL DRAG FORCE APPROXIMATION
6
7  C COMMON /B3/ VELX(25),VELY(25)
8  COMMON /B1/ FEJUNC,IR,DELTAI,DELTA,IRSF,IFJUNC,E,ES,FCAB,RCAB,JUMP,CFO
9  LPJUNCS,PCAB,PLABE,PCABO,RCABO,THETA,PJUNCO
10 COMMON /B2/ NCAB,NNODE,ERJUNC,IRJUNC,DAII,DATN,P,PJUNC,CCOCAB,OCAB,CFO
11 IFATE,NANJ,ANJUNC,IHEAD,IPRINT,INTAPE,OUTAPE,ITIME,IFLG,OFELG,NIR,THECFO
12 ZTAS,THETRC,CUMPO,THETAB,NJUNC,RHO,TEST,NVSEG,ZVEL,ZPI,ECICAB,CFO
13 3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WCAR,IDEV,ICHECK,NDEV,NDATC
14 COMMON /TANDRE/ TDCAB(22),TDCAB(1000)
15 COMMON /PIBLN/ PI
16 DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNCO(CFO
17 13,44)
18 DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)
19 1)
20 DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABU(3,51,22)
21 DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DAII(10), DATN(10), MCFO
22 1(22)
23 DIMENSION PJUNC(3,44), COCAB(22), DCAB(22), ANJUNC(44), TEST(14)
24 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
25 DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IUEV(1000)
26 DIMENSION ICHECK(44)
27 DIMENSION WTCAB(3), VADHM(3), PSPACE(3)
28 DIMENSION W(3), VT(3)
29 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OELG
30 INTEGER PATH
31 REAL IR,IRS
32
33 C CALCULATE THE WEIGHT/LENGTH VECTOR
34
35 WTCAB(1)=0.
36 WTCAB(2)=0.
37 WTCAB(3)=WCAB(N)
38
39 C CHECK TO SEE IF CURRENT OR NO CURRENT
40 JUM=JUMP+1
41 GC TO (5,10), JUM
42
43 C GET HERE IF NO CURRENT
44
45 S CFORCE=WTCAB(1)
46 RETURN
47
48 C GET HERE IF CURRENT
49
50 CALCULATE LOCATION OF NODE IN SPACE
51
52 UC 15 K=1,3
53 IF PSPACE(K)=PCAB(K,M,N)
54 IF (IVOPT.EG.3) CALL INTVEL (W,PSPACE)
55 IF (IVOPT.EG.3) GC TO 25
56 UC 20 K=1,3
57 WTKR=VELCC(K,PSPACE)

```

```

25 CONTINUE
C
C CALCULATE THE TANGENTIAL PROJECTION OF THE CURRENT ON THE CABLE
C
VPRQJ=0
DC 30 KK=1+3
K=KK
33 VPROJ=VPRQJ*W(K)*RCAB(K,M,N)/TCAB(M,N)
C
C CALCULATE THE NORMAL COMPONENT OF THE CURRENT AND ITS MAGNITUDE
C
DC 35 KK=1+3
K=KK
35 VNORM(K)=W(K)-VPROJ*RCAB(K,M,N)/TCAB(M,N)
VMAG=SQRT(VNORM(1)**2+VNORM(2)**2+VNORM(3)**2)
C
C CALCULATE THE FORCE/LENGTH
C
C CALCULATE TANGENTIAL COMPONENT OF CURRENT AND ITS MAGNITUDE
VT(1)=W(1)-VNORM(1)
VT(2)=W(2)-VNORM(2)
VT(3)=W(3)-VNORM(3)
VIM=SQRT(VT(1)**2+VT(2)**2+VT(3)**2)
CFORCE=I*CAH(1)*RHO*5*(UCAB(N)/12)*EXCAB(M,N)*(VMAG*VNORM(1)*CUCFO
ICAH(N)+VIP*V(1))*TUCAB(N)*PI
RETURN
END

```

CFO 54
CFO 55
CFO 60
CFO 61
CFO 62
CFO 63
CFO 64
CFO 65
CFO 66
CFO 67
CFO 68
CFO 69
CFO 70
CFO 71
CFO 72
CFO 73
CFO 74
CFO 75
CFO 76
CFO 77
CFO 78
CFO 79
CFO 80
CFO 81
CFO 82
CFO 83
CFO 84
CFO 85
CFO 86

CARD NO. SEVERELY DETAILS DIAGNOSIS OF PROBLEM
42 I AM IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1  *UECA EFORCE 1,PM,N)
2  FUNCTION EFORCE (I,PM,N)
3
4  C
5  C THIS ROUTINE CALCULATES THE DEVICE FORCES IN DIRECTION I
6  C USING THE NORMAL DRAG APPROXIMATION FOR IN-LINE DEVICES
7  C
8  C
9  COMMON /B3/ VELX(25),VELY(25)
10 COMMON /B1/ FEJUNC,IR,DELTAI,DELTA,IRHS,IFJUNC,E,ES,FCAB,RCAB,JUMP,EFO
11 IPJUNC,PCAB,PCABE,PCABU,MCABO,THETA,PJUNCO
12 COMMON /B2/ NCAB,NMODE,ERJUNC,IRJUNC,DAII,DATN,F,PJUNC,COCAB,DCAB,EFO
13 IFAT,ANANC,ANJUNC,IHEAD,IPRNI,INTAPE,OUTAPE,ITIME,IFLG,OF LG,NIR,THEEFO
14 ATAS,THETA,SCUPPD,THETAB,NJUNC,RHO,TEST,NVSEG,ZVEL,ZVEL,P,PCICAB,EFO
15 *EXPCAB,ZJUNC,LJUNC,PAIR,ICAB,IVOPT,WCAB,IDEV,ICHECK,NDEV,ADATC
16 COMMON /TANDRG/ TDICAB(22),TDICAB(1000)
17 COMMON /PI/DLK/ PI
18 DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNC(EFO
19 13,44)
20 DIMENSION FCAB(3,51,22), MCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)EFO
21 1)
22 DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABO(3,51,22)
23 DIMENSION ANODE(22), ERJUNC(44), IRJUNC(44), DATI(10), DAIN(10), HEFO
24 1(22)
25 DIMENSION PJUNC(3,44), CDCAU(22), DCAB(22), ANJUNC(44), TESI(14)
26 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
27 DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
28 DIMENSION ICHECK(44)
29 DIMENSION WTEL(3), VNOR*(3), PSPACE(3)
30 DIMENSION *(3), WTCAB(3), VT(3)
31 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OF LG
32 INTEGER PATH
33 HEAL IR,IRS
34
35 C INITIALIZE LOCAL VARIABLES
36
37 WTCAB(1)=0.
38 WTCAB(2)=0.
39 WTCAB(3)=*XCAB(N)
40 DC=DAII(8)
41 IF (DAII(4).EQ.1) DD=DAII(8)/12.
42 DL=DAII(5)
43 DD=DAII(7)
44
45 C CALCULATE THE WEIGHT VECTOR OF A DEVICE
46
47 WTEL(1)=(
48 WTEL(2)=L.
49 WTEL(3)=DAII(6)-DL*WTCAB(3)
50
51 CHECK TO SEE IF CURRENT UM NO CURRENT
52
53 JUM=JUMP*
54 GO TO (5+1), JUM
55
56 *FT HERE IF NO CURRENT
57
58 EFUNCE=WTEL(1)
59 RETURN
60

```

```

C          EFO 58
C          EFO 59
C          EFO 60
C          EFO 61
C          EFO 62
C          EFO 63
C          EFO 64
C          EFO 65
C          EFO 66
C          EFO 67
C          EFO 68
C          EFO 69
C          EFO 70
C          EFO 71
C          EFO 72
C          EFO 73
C          EFO 74
C          EFO 75
C          EFO 76
C          EFO 77
C          EFO 78
C          EFO 79
C          EFO 80
C          EFO 81
C          EFO 82
C          EFO 83
C          EFO 84
C          EFO 85
C          EFO 86
C          EFO 87
C          EFO 88
C          EFO 89
C          EFO 90
C          EFO 91
C          EFO 92
C          EFO 93
C          EFO 94
C          EFO 95
C          EFO 96
C          EFO 97
C          EFO 98
C          EFO 99
C          EFO 100
C          EFO 101
C          EFO 102
C          EFO 103
C          EFO 104
C          EFO 105
C          EFO 106
C          EFO 107
C          EFO 108
C          EFO 109
C          EFO 110
C          EFO 111
C          EFO 112
C          EFO 113
C          EFO 114

C          GET HERE IF CURRENT
C          CALCULATE LOCATION OF DEVICE IN SPACE
C          JJ DC 15 KK=1+3
C          K=KK
C          15 PSPACE(N)=SPACE(K)
C          IF (I(VOPI,EG-3) CALL INTVEL (NM,PSPACE)
C          IF (I(VOPI,EG-3) GO TO 25
C          DC 20 K=1+3
C          20 MM(K)=VELOC(K,PSPACE)
C          25 CONTINUE
C          CHECK IF DEVICE IS IN-LINE OR FREE
C          IJMP=DATI(14)
C          GO TO (35,30), IJMP
C          GET HERE IF FREE TYPE DEVICE -- CALCULATE MAGNITUDE OF THE CURRENT
C          30 VMAG=SORI(M(1)**2+M(2)**2+M(3)**2)
C          CALCULATE THE FORCE ON THE FREE DEVICE
C          EFORCE=TEL(1)*(M(0)/2.)*DATI(17)*VMAG*MM(1)
C          RETURN
C          GET HERE IF IN-LINE DEVICE
C          CALCULATE THE TANGENTIAL PROJECTION OF THE CURRENT ON THE DEVICE
C          TANG(I) EVALUATES THE UNIT TANGENT TO A CABLE AT ANY POINT
C          45 VPROJ=0.
C          DC 40 KK=1+3
C          K=KK
C          40 VPROJ=VPROJ+M(K)*TANG(K)
C          CALCULATE THE NORMAL COMPONENT OF THE CURRENT AND ITS MAGNITUDE
C          DO 45 KK=1+3
C          K=KK
C          45 VADHM(K)=M(K)-VPROJ*(ANG(K)
C          VMAG=SORI(VNORM(1)**2+VNORM(2)**2+VNORM(3)**2)
C          CALCULATE THE TANG. COMPONENT OF THE CURRENT AND ITS MAGNITUDE
C          VT(1)=MM(1)-VNORM(1)
C          VT(2)=MM(2)-VNORM(2)
C          VT(3)=MM(3)-VNORM(3)
C          VTM=SORI(VT(1)**2+VT(2)**2+VT(3)**2)
C          CALCULATE THE FORCE ON THE IN-LINE DEVICE
C          TERM1=TEL(1)
C          TERM2=VADHM(1)*M(1)*(DL*UND-CUCAB(N)*DCAB(N)/12.)
C          TERM3=VTM*VT(1)*PI*(DL*IDUCAB(N)-TOCAB(N)*DCAB(N)/12.)
C          EFORCE=TERM1+0.5*H*H0*DL*(TERM2+TERM3)
C          RETURN

```

106

03/07/80 11.41.06

FTN 4.6.433E

7474 OP1=1

EFO 115-

END.

115

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

52	1	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
74	1	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

31 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1  *ULCK EXCAR 1
2  FUNCTION EXCAR (M,K) 2
3  C 3
4  C 4
5  C 5
6  C 6
7  C 7
8  C 8
9  C 9
10 C 10
11 C 11
12 C 12
13 C 13
14 C 14
15 C 15
16 C 16
17 C 17
18 C 18
19 C 19
20 C 20
21 C 21
22 C 22
23 C 23
24 C 24
25 C 25
26 C 26
27 C 27
28 C 28
29 C 29
30 C 30
31 C 31
32 C 32

```

THIS ROUTINE CALCULATES (I * STRAIN) AT NODE M OF CAULE K
 COMMON /H3/ VELX(25),VELY(25)
 COMMON /B1/ FEJUNC,IR,DELTAI,DELTA,IRS,IFJUNC,E,ES,FCAB,MCAB,JUMP,EXC
 IPJUNC,PCAB,PCABE,FCABO,MCABO,THETA,PJUNCO
 COMMON /B2/ NCAB,NCODE,ERJUNC,IRJUNC,DATAI,DATAI*,PJUNC,CUCAB,DCAB,EXC
 I,FATE,NANC,ANJUNC,THEAD,IPRINT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEEXC
 2IAS,THEIAL,COMPD,THEIAB,ANJUNC,RMU,TEST,NVSEG,ZVEL,VELZ,PIPI,ECICAB,EXC
 3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,MCAB,IDEV,ICHECK,NDEV,NDATC
 DIMENSION FEJUNC(3,44), IH(3,44), IHS(3,44), IFJUNC(3,44), PJUNCO(EXC
 13,44)
 DIMENSION FCAB(3,51,22), MCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)EXC
 15
)
 DIMENSION PCABE(3,51,22), PCABO(3,51,22), MCABO(3,51,22)
 DIMENSION NNODE(2), ERJUNC(44), IRJUNC(44), DATAI(10), DATAI10), MEXC 18
 1(22)
 DIMENSION PJUNC(3,44), CCAB(22), DCAB(22), ANJUNC(44), FST(14) EXC 19
 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22) EXC 20
 DIMENSION LJUNC(22), PATH(22), ICAB(22), MCAB(22), IDEV(1000) EXC 21
 DIMENSION ICHECK(44) EXC 22
 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
 INTEGER PATH EXC 24
 INTEGER PATH EXC 25
 REAL IR,IRS
 IF (EXPCAB(K).EQ.0.) GO TO 5
 FCAB=1./((ICAB(M,K)/ECICAB(K))*EXPCAB(K)
 RETURN
 5 FCAB=1.
 RETURN
 END

```

1 INP 1
2 INP 2
3 INP 3
4 INP 4
5 INP 5
6 INP 6
7 INP 7
8 INP 8
9 INP 9
10 INP 10
11 INP 11
12 INP 12
13 INP 13
14 INP 14
15 INP 15
16 INP 16
17 INP 17
18 INP 18
19 INP 19
20 INP 20
21 INP 21
22 INP 22
23 INP 23
24 INP 24
25 INP 25
26 INP 26
27 INP 27
28 INP 28
29 INP 29
30 INP 30
31 INP 31
32 INP 32
33 INP 33
34 INP 34
35 INP 35
36 INP 36
37 INP 37
38 INP 38
39 INP 39
40 INP 40
41 INP 41
42 INP 42
43 INP 43
44 INP 44
45 INP 45
46 INP 46
47 INP 47
48 INP 48
49 INP 49
50 INP 50
51 INP 51
52 INP 52
53 INP 53
54 INP 54
55 INP 55
56 INP 56
57 INP 57

```

1 *DECK INPUT
2 SUBROUTINE INPUT
3
4 L
5 C
6 C
7 C
8 C
9 C
10 C
11 C
12 C
13 C
14 C
15 C
16 C
17 C
18 C
19 C
20 C
21 C
22 C
23 C
24 C
25 C
26 C
27 C
28 C
29 C
30 C
31 C
32 C
33 C
34 C
35 C
36 C
37 C
38 C
39 C
40 C
41 C
42 C
43 C
44 C
45 C
46 C
47 C
48 C
49 C
50 C
51 C
52 C
53 C
54 C
55 C
56 C
57 C

THIS ROUTINE READS ALL DATA AND IDENTIFIES ERRORS IN
DATA, DECK STRUCTURE, AND ARRAY REPRESENTATION

COMMON /B3/ VELX(25),VELY(25)
COMMON /H1/ FEJUNC,IR,DELTA,DELTA,IRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,
IPJUNC,PCAB,PCAB,PCAB,RCAB,THETA,PJUNCO
COMMON /B2/ NCAB,MODE,ERJUNC,IRJUNC,DATAI,DATAI,DATAI,PJUNC,DCAB,DCAB,
IFATE,NANC,ANJUNC,IKREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THE
2TAS,THETA,CUMPD,THETA,NJUNC,HHU,TEST,ANVSEG,ZVEL,VFLZ,PIP,ECICAB,
3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WGAB,IDEV,ICHECK,NDEV,NDATC
COMMON /CVEL/ VMAG(25,4),VDIR(25,4),ZPT(25,4),XPT(4),YPT(4),NPPS(4)
1),NSTA
COMMON /IVEL/ IFVEL
COMMON /REF/ NUCUR
COMMON /LANDNG/ IDCAB(22),TUDCAB(1000)
COMMON /ITL/ TITLE(8),PHI,CURITS,JUNIT,VELXP(25),VELYP(25)
COMMON /PL/ LPUNCH,IPACK,ITILEM(8),DEVMT
COMMON /BLN/ ISCH
COMMON /PLT/ KPPLT,SIZE,TH(3),IPOPT,KCPLT
COMMON /CPI/ ZUP,ZUN,ZC,XMIN,XMAX,YMIN,YMAX,YIN,ANGNY
COMMON /PIHLK/ PI
COMMON /NITER/ KOUNTR,NII,MAXITER,NSTEPS,ISTEP,PERCNTV,INCPRT
DIMENSION FEJUNC(3,4,4), IR(3,4,4), IRS(3,4,4), IFJUNC(3,4,4), PJUNCO(
13,4,4)
DIMENSION FCAB(3,51,22), HCAB(3,51,22), PJUNCS(3,4,4), PCAB(3,51,22)
1)
DIMENSION PCAHE(3,51,22), PCABO(3,51,22), RCABU(3,51,22)
DIMENSION IRULE(22), ERJUNC(4,4), IRJUNC(4,4), DATAI(10), MINP
1(22)
DIMENSION PJUNC(3,4,4), CUCAB(22), DCAB(22), ANJUNC(4,4), TEST(14)
DIMENSION ZVEL(25,4), VFLZ(25,4), ECICAB(22), EXPCAB(22), LJUNC(22)
DIMENSION ICHECK(4,4), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
DIMENSION DATIT(2150,10)
DIMENSION ITEST(14)
DIMENSION STOR(8)
EQUIVALENCE (DATIT(1),FEJUNC(1))
EQUIVALENCE (ITEST(1),TEST(1))
INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
INTEGER PATH
REAL IR,IRS

THIS IS THE BEGINNING OF THE INPUT SECTION
INITIALIZE ALL CONSTANTS, FLAGS, ARRAYS, AND COUNTERS

IF (ITIME.NE.1) GO TO 20
ITEST(1)=4H R
ITEST(2)=4H ANC
ITEST(3)=4H DJNC
ITEST(4)=4H DCAB
ITEST(5)=4H CAH
ITEST(6)=4H DEN
ITEST(7)=4H CUMP
ITEST(8)=4H ANG

```

60 ITEST(7)=4H EOD
   ITEST(10)=4H NJNC
   ITEST(11)=4H VEL
   ITEST(12)=4H NCAT
   ITEST(13)=4H LUN
   ITEST(14)=4H EOP
   PIP=PI/180.
   INTAPE=24
   ISCR=25
   IREAD=60
   IPNT=61
   IFEUD=0
   INDEY=0
   MDATC=0
   KFLG=0
   NCJUNC=0
   KCUP=0
   DO 5 I=1,1000
     5 IDDCAB(I)=0
     DO 10 J=1,4
       10 ICHECK(J)=0
       DO 15 J=1,22
         15 ICAB(J)=0
         NANC=0
         IFRHO=0
         IFJNC=0
         NIN=0
         IROW=1
         IPNCH=8
         KPLT=0
       20 FATE=0
         KCPLT=0
         KPPLT=0
       C CHECK LOGICAL UNITS
       C
       C IF (IIME.GI.1) GO TO 50
       ITIME=2
       C
       C IF READING FROM TAPE LUN MUST BE INCLUDED AS A CARD
       C
       C HEAD (IREAD=620) TITLEM
       C
       C SAVE INPUT ON TAPP
       C
       IREAD=0
       IFORM=1
       WRITE (ISCH) IFORM,IBAD
       WRITE (ISCH,620) TITLEM
       IF (EOP(IREAD)) 25,30
       25 STOP
       30 DECODE (B,625,TITLEM) IST1,IST2
       C
       C CHECK IF FIRST CARD IS LUN OR MAIN TITLE CARD
       C
       C IF (IST2.EQ.3HLUN) GO TO 35
       C

```

INP 58
 INP 59
 INP 60
 INP 61
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 INP 114

```

115 C FIRST CARD IS TITLE CARD SET DEFAULTS FOR LUN CARD
      C
      DATA(1)=4M
      DATA(2)=4M LUN
      DATA(3)=60
      DATA(4)=61
      DATA(5)=24
      DATA(6)=0.
      DATA(7)=0.
      DATA(8)=0.
      DATA(9)=0.
      DATA(10)=0.
      GC TO 40
120 C FIRST CARD IS LUN CARD
      C
125 C
      C
130 C J5 DECODE (80,630,TITLEM) DATA
      READ (IHEAD,620) TITLEM
135 C SAVE INPUT ON TAPE
      C
      IPAD=0
      IFORM=1
      WRITE (ISCR) IFORM,IBAD
      WRITE (ISCR,620) TITLEM
140 C
      40 IPRNT=DATA(4)+0.1
      45 IF (IIFEOD.AL=0) GC TO 320
      IF (IIFEOD.NE=0) GC TO 160
145 C HEAD ONE INPUT RECORD INTO DATA ARRAY
      C
150 C
      50 CONTINUE
      IF (IFLG.EQ.0) READ (IHEAD,620) STORE
      IF (IFLG.EQ.1) READ (IHEAD,635) (DATA(I),I=1,10),EX,NSEG
155 C SAVE INPUT ON TAPE
      C
      IHAD=0
      IFORM=2
      WRITE (ISCR) IFORM,IBAD
      IF (IFLG.EQ.0) WRITE (ISCR,620) STORE
      IF (IFLG.EQ.0) DECODE (80,630,STORE) DATA,EX,NSEG
160 C TYPE AND BRANCH
      C
      IF (IIFEOD.EQ.0) GC TO 55
      IF ((DATA(12).EQ.TEST(12)).OR.(DATA(2).EQ.TEST(14))) GO TO 55
      GC TO 615
165 C
      55 UC 60 J=1,14
      IF (DATA(12).EQ.TEST(1)) GO TO (65,65,100,105,120,130,615,615,135,1
      150,615,155,615,325), I
      61 CONTINUE
170 C GET HERE IF CARD UNIDENTIFIABLE
      C

```

INP 115
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INP 170
INP 171

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1

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172 GO TO 540
173 C
174 C
175 C
176 C
177 C
178 C
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181 C
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183 C
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224 C
225 C
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227 C
228 C

```

GET HERE IF IR CARD READ
 65 IF ((DATI(3).NE.DATI(4)) GO TO 70
 IBAD=7
 70 DC 75 I=3,4
 IF ((DATI(1).LT.1).OR.(DATI(1).GT.44.)) IRAD=8
 IF ((DATI(1).LT.1).OR.(DATI(1).GT.44.)) GO TO 545
 75 CONTINUE
 GET HERE IF DATA OK
 COUNT IR AND STORE DATA
 NIR=NIR+1
 IRJUNC(NIR)=DATI(3)
 ERJUNC(NIR)=DATI(4)
 DO 80 N=1,14
 IF ((IRJUNC(NIR).EQ.ERJUNC(NIR)) IBAD=33
 IF ((IRJUNC(NIR).EQ.ERJUNC(NIR)) GO TO 560
 IF ((IRJUNC(NIR).EQ.ERJUNC(NIR)).AND.(NIR.NE.NI)) IBAD=33
 IF ((IRJUNC(NIR).EQ.ERJUNC(NIR)).AND.(NIR.NE.NI)) GO TO 560
 IF ((ERJUNC(NIR).EQ.ERJUNC(NIR)) IBAD=34
 IF ((ERJUNC(NIR).EQ.ERJUNC(NIR)) GO TO 560
 80 CONTINUE
 GO TO 500
 GET HERE IF AC CARD READ
 85 INDEX=DATI(3)
 IF ((DATI(3).LT.1).OR.(DATI(3).GT.44.)) IBAD=6
 IF ((DATI(3).LT.1).OR.(DATI(3).GT.44.)) GO TO 545
 IF ((CHECK(INDEX).NE.0) IBAD=30
 IF ((CHECK(INDEX).NE.0) GO TO 550
 GET HERE IF DATA OK -- COUNT ANCHOR AND STORE DATA
 NANC=NANC+1
 ANJUNC(NANC)=DATI(3)
 ICHECK(INDEX)=1
 90 DO 95 I=1,3
 95 PJUNC(I,INDEX)=DATI(I+3)
 GO TO 500
 GET HERE IF DJMC CARD READ
 100 DATI(4)=2
 IF ((DATI(3).LT.1).OR.(DATI(3).GT.44.)) IRAD=23
 IF ((DATI(3).LT.1).OR.(DATI(3).GT.44.)) GO TO 545
 IF ((DATI(7).LT.0).OR.(DATI(8).LT.0.)) IRAD=24
 IF ((DATI(7).LT.0).OR.(DATI(8).LT.0.)) GO TO 545
 INDEV=INDEV+1
 INDEX=INDEX
 GO TO 500
 GET HERE IF UCAB CARD READ

```

230 C 105 DC 110 I=1,2
      ID=DATI(4)
      IF (ID.EQ.1) GO TO 115
      110 CONTINUE
      IBADE=18
      GO TO 545
235 115 IF ((DATI(3).LT.1.) .OR. (DATI(3).GT.22.)) IBADE=17
      IF ((DATI(3).LT.1.) .OR. (DATI(3).GT.22.)) GO TO 545
      INDEV=INDEV+1
      INDEX=INDEX
      IF ((INDEX.LT.1.) .OR. (INDEX.GT.1000)) IBADE=19
      IF ((INDEX.LT.1.) .OR. (INDEX.GT.1000)) GO TO 545
      IF ((DATI(7).LT.0.) .OR. (DATI(8).LT.0.)) IBADE=22
      IF ((DATI(7).LT.0.) .OR. (DATI(8).LT.0.)) GO TO 545
      IF ((DATI(4).EQ.2.) .AND. (DATI(9).NE.0.)) IBADE=21
      IF ((DATI(4).EQ.2.) .AND. (DATI(9).NE.0.)) GO TO 545
      IF ((DATI(4).EQ.1.) .AND. (DATI(9).LE.0.)) IBADE=20
      IF ((DATI(4).EQ.1.) .AND. (DATI(9).LE.0.)) GO TO 545
      IF ((DATI(10).LT.0.) .OR. (DATI(10).GT.50)) IBADE=22
      IF ((DATI(10).LT.0.) .OR. (DATI(10).GT.50)) GO TO 545
      IDCCAB(INDEX)=EX
      GO TO 530
240 C
      C GET HERE IF CAB CARD READ
      C
      C
250 120 INDEX=DATI(3)
      IF (IFLG.EQ.0) READ (IREAD,620) STORE
      IF (IFLG.EQ.1) READ (IREAD,645) IDCCAB(INDEX)
      C
      C SAVE INPUT ON TAPE
      C
      C
      IBADE=0
      IFORM=3
      WRITE (ISCH) IFORM,IBADE
      IF (IFLAG.EQ.0) WRITE (ISCP,620) STORE
      IF (IFLAG.EQ.0) WRITE (ISCP,640) STORE TOCCAB(INDEX)
      DECODE (I0,640,STORE) TOCCAB(INDEX)
      IF ((DATI(3).LT.1.) .OR. (DATI(3).GT.22.)) IBADE=9
      IF ((DATI(3).LT.1.) .OR. (DATI(3).GT.22.)) GO TO 545
      IF ((DATI(4).EQ.0.) .OR. (DATI(5).LE.0.)) IBADE=10
      IF ((DATI(4).EQ.0.) .OR. (DATI(5).LE.0.)) GO TO 545
      IF ((DATI(4).GT.44.) .OR. (DATI(5).GT.44.)) IBADE=11
      IF ((DATI(4).GT.44.) .OR. (DATI(5).GT.44.)) GO TO 545
      IF ((DATI(4).LT.1.) .OR. (DATI(5).LT.1.)) IBADE=11
      IF ((DATI(4).LT.1.) .OR. (DATI(5).LT.1.)) GO TO 545
      IF ((DATI(7).LE.0.) .OR. (DATI(8).LE.0.)) IBADE=12
      IF ((DATI(7).LE.0.) .OR. (DATI(8).LE.0.)) GO TO 545
      IF ((DATI(7).LE.0.) .OR. (DATI(8).LE.0.)) IBADE=15
      IF ((DATI(7).LE.0.) .OR. (DATI(8).LE.0.)) GO TO 545
      IF ((EX.LT.0.) .OR. (DATI(10).LT.0.)) IBADE=13
      IF ((EX.LT.0.) .OR. (DATI(10).LT.0.)) GO TO 545
      IF ((DATI(10).EQ.0.) .AND. (EX.NE.0.)) IBADE=14
      IF ((DATI(10).EQ.0.) .AND. (EX.NE.0.)) GO TO 545
      IF ((DATI(10).NE.0.) .AND. (EX.EQ.0.)) IBADE=15
      IF ((DATI(10).NE.0.) .AND. (EX.EQ.0.)) GO TO 545
      IF ((INSEG.LT.1.) .OR. (INSEG.GT.50)) IBADE=16
      IF ((INSEG.LT.1.) .OR. (INSEG.GT.50)) GO TO 545

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IF (ICAB(INDEX).NE.0) GO TO 555
ICAB(INDEX)=1
INDEX=DATI(5)
IF (ICHECK(INDEX).NE.0) IBAD=31
IF (ICHECK(INDEX).NE.0) GO TO 550
ICHECK(INDEX)=1

```

```

C GET HERE IF DATA CK
C
C

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```

INDEX=DATI(3)
ZJUNC(INDEX)=DATI(4)
LJUNC(INDEX)=DATI(5)
125 MCODE(INDEX)=NSEG+1
WCAB(INDEX)=DATI(6)
CDCAB(INDEX)=DATI(7)
DCAB(INDEX)=DATI(8)
H(INDEX)=DATI(9)/NSEG
ECICAB(INDEX)=DATI(10)
EXPCAB(INDEX)=EX
GO TO 500

```

```

C GET HERE IF UEN CARD READ
C
C

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```

130 IF (DATI(3).LE.0.) IBAD=25
IF (DATI(3).LE.0.) GO TO 545
IFRHO=IFRHO+1
IF (IFRHO.GT.1) IBAD=36
IF (IFRHO.GT.1) GO TO 565
MMU=DATI(3)
GO TO 50

```

```

C GET HERE IF EOD CARD READ
C
C

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```

135 IFEUD=IFEUD+1
DC 140 J=1,10
140 DATI(INOM+J)=DATI(J)
IMAX=IMOL

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```

IF (FATE.NE.0.) GO TO 450
IF (IFLG.EQ.1) GO TO 145
GO TO 335

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145 IREAD=ISAVI
IFLG=0
GO TO 335

```

```

C GET HERE IF NUNC CARD READ
C
C

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```

150 IF ((DATI(3).LI.2.).OR.(UATI(3).GT.44.)) IBAD=5
IF ((UATI(3).LI.2.).OR.(UATI(3).GT.44.)) GO TO 545
IFJNC=IFJNC+1
IF (IFJNC.GT.1) IBAD=35
IF (IFJNC.GT.1) GO TO 565
MCJUNC=DATI(3)
GO TO 50

```

```

C GET HERE IF NCAT CARD READ
C
C

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155 NCATC=NCATC+1

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399 C

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DEFINE CURRENT UNITS OPTION AND CONVERSION FACTOR
 IUNIT=DAT1(10)+1.E-9
 CUNITS=1
 IF (IUNIT.EG.1) CUNITS=0.01943
 IF (IUNIT.EG.2) CUNITS=0.5921
 DEWTE=DAT1(8)
 NSTEPS=1
 ISTEP=1
 PERCENTIV=0.
 INCPRT=0
 IF (EX.NE.0.0) NSTEPS=EX
 IF (FLOAT(NSTEPS).NE.EA.AND.NSTEPS.GT.1) INCPRT=1
 IF (DAT1(7).NE.0.0) IPUNCH=8H YES
 NCCUR=DAT1(5)
 HEAD=(IHEAD+620) TITLE
 SAVE INPUT ON TAPE
 IBAD=0
 IFORM=1
 WRITE (ISCR,620) TITLE
 IF (INDAIC.NE.IFEOD) GO TO 615
 PHIS=DAT1(6)
 GC TO 45
 IFCOMP=0
 INDAT=C
 IFVEL=0
 IFANG=C
 IF ((DAT1(3).LT.0.0).OR.(DAT1(3).GT.3.)) IBAD=26
 IVOPT=DAT1(3)
 IF (IVOPT.EG.3) NSTA=DAT1(4)
 IF (INDAIC.EG.1) GC TO 165
 IF (IVOPT.EG.0) GC TO 180
 IF (KFLG.EG.0) GO TO 170
 IF (IVOPT.EG.KCUR) GO TO 180
 GC TO 610
 165 IF (IVOPT.EG.0) GO TO 175
 170 KFLG=1
 KCUR=IVOPT
 GC TO 180
 175 KFLG=0
 HEAD ONE INPUT RECORD FROM PARAMETRIC STUDY SOURCE DECK
 IM HEAD (IHEAD+620) STORE
 IF (EOF(IHEAD)) 185+190
 185 CALL MACA1A
 STOP

```

400 C
401 C SAVE INPUT ON TAPE
402 C
403 C
404 C
405 C
406 C
407 C
408 C
409 C
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414 C
415 C
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454 C
455 C
456 C

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460      HANG=HANG+1
         IF (NANG.GT.1) IBAD=40
         IF (NANG.GT.1) GO TO 505
         GO TO 180
C
C      GET HERE IF COMP CARD READ
C
230      IFCOMP=IFCOMP+1
         CALL SWITCH
         IF (IFCOMP.EQ.1) NCOMP=0
         IF (DATI(3).LE.0.) IBAD=27
         IF (DATI(3).LE.0.) GO TO 545
NCOMP=NCOMP+1
         IF (NCOMP.GT.1) (BAD=37
         IF (NCOMP.GT.1) GO TO 565
COMP=DATI(3)
NIT=200
         IF (DATI(4).NE.0.0) NIT=DATI(4)
         MAXITER=1000
         IF (DATI(5).NE.0.0) MAXITER=DATI(5)
         GO TO 180
C
C      GET HERE TO PLOT VELOCITY FIELD
C
235      IF (KPLT.EQ.0) CALL PLOTS (0.0,6LNPFIL)
         KPLT=1
         KCPLI=1
         CALL SWITCH
         ZUP=DATI(3)
         ZDN=DATI(4)
         DZ=DATI(5)
         YIN=DATI(6)
         YMIN=DATI(7)
         YMAX=DATI(8)
         YMIN=DATI(9)
         YMAX=DATI(10)
         ANGE=EXX
         IF (ANGE.LE.0.0) ANGE=90.
         NY=NNSEG
         IF (NY.LE.0) NY=0
C
C      FIND MAX AND MIN FOR DEFAULT
C
         DEFAULT=XMIN+YMIN+XMAX+YMAX
         IF (DEFAULT.NE.0.) GO TO 180
         BIG=1.E10
         XMIN=BIG
         YMIN=BIG
         XMAX=-BIG
         YMAX=-BIG
         UC 240 ISF=1,NANIC
         ISA=ANJUNC(1SF)
         YMIN=AMINI(XMIN,PJUNC(1,ISA))
         YMAX=AMAXI(XMIN,PJUNC(1,ISA))
         XMIN=AMINI(YMIN,PJUNC(2,ISA))
         XMAX=AMAXI(YMIN,PJUNC(2,ISA))
         YMIN=AMINI(XMAX,PJUNC(1,ISA))
         YMAX=AMAXI(XMAX,PJUNC(1,ISA))
         UC 240
         KX=ABS(XMAX-XMIN)
INP 457
INP 458
INP 459
INP 460
INP 461
INP 462
INP 463
INP 464
INP 465
INP 466
INP 467
INP 468
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515      HY=HYS(YMAX-Y*IN)
        IF (RY.EQ.0.) YMIN=YMIN-0.15*RX
        IF (RY.EQ.0.) YMAX=YMAX+0.15*RX
        IF (RX.EQ.0.) XMIN=XMIN-0.15*RY
        IF (RX.EQ.0.) XMAX=XMAX+0.15*RY
        GO TO 180
520      C
        C GET HERE FOR PERSPECTIVE PLOTTING
        C
525      245 CALL SWITCH
        IFOPT=DAT1(3)*.01
        SIZE=DAT1(4)
        IH(1)=DAT1(5)
        IH(2)=DAT1(6)
        IH(3)=DAT1(7)
        DEFAULT=IH(1)+IH(2)+IH(3)
        IF (DEFAULT.NE.0.) GO TO 250
        IH(1)=302
        IH(2)=120
        IH(3)=90
530      250 IF (KPLT.EQ.0) CALL PLOIS (0,0,6LNPFIL)
        KPLT=1
        KPLT=1
        GO TO 180
535      C
        C GET HERE IF PARAMETERS ARE BEING CHANGED
        C LOCATE RECORD TO BE CHANGED AND BRANCH
        C
540      255 IF ((INDA1.NE.0) GO TO 260
        HEAD (INTAPE,660) ((DAT1(I),J),J=1,10),I=1,IRMAX)
        REWIND INTAPE
        I(KDATE)=1
545      260 DO 265 I=1,IRMAX
        IROW=1
        IF ((DATN(1).EQ.DAT1(ROW,1)).AND.(DATN(2).EQ.DAT1(ROW,2))) GO
        110 270
        IF (DAT1(ROW,2).EQ.TEST(9)) GO TO 605
        265 CONTINUE
        270 DO 275 J=1,10
        275 DAT1(J)=DAT1(ROW,J)
        DO 280 I=1,5
        IF (DATA(2).EQ.TEST(1)) GO TO (280,285,290,295,305), I
        280 CONTINUE
550      C
        C GET HERE IF ANC CARD READ
        C
555      285 IF (DAT1(3).NE.DATN(3)) GO TO 605
        CALL SWITCH
        INDEX=DAT1(3)
        GO TO 90
560      C
        C GET HERE IF DUNC CARD READ
        C
565      290 IF (DAT1(3).NE.DATN(3)) GO TO 605
        CALL SWITCH
        DAT1(4)=2
        IF ((DAT1(7).LT.0.)OR.(DAT1(8).LT.0.)) IHAD=24
570

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575 IF ((DATI(17).LT.0.).OR.(DATI(8).LT.02)) GO TO 545
    GO TO 500
C
C
C
580 GET HERE IF NCAB CARD READ
    295 IF (DATI(13).NE.DATI(3)) GO TO 605
    IDDCAB(INCM)=IXX
    IF ((DATI(4).EQ.1).OR.(DATI(4).EQ.2)).AND.((DATI(4).EQ.1).OR.(DATI(
    1(4).EQ.2)) GO TO 300
    GO TO 605
300 CALL SWITCH
    IF ((DATI(4).EQ.2).AND.(DATI(9).NE.0.)) IHAD=21
    IF ((DATI(4).EQ.2).AND.(DATI(9).NE.0.)) GO TO 545
    IF ((DATI(7).LT.0.).OR.(DATI(8).LT.02)) IHAD=22
    IF ((DATI(7).LT.0.).OR.(DATI(8).LT.02)) GO TO 545
    IF ((DATI(4).EQ.1).AND.(DATI(8).LT.02)) IHAD=20
    IF ((DATI(4).EQ.1).AND.(DATI(9).LE.0.)) IHAD=20
    IF ((DATI(4).EQ.1).AND.(DATI(9).LE.0.)) GO TO 545
    IF ((DATI(10).LT.0.).OR.(DATI(10).LT.0.)) IHAD=20
    IF ((DATI(10).LT.0.).OR.(DATI(10).LT.0.)) GO TO 545
    GO TO 500
C
C
C
595 GET HERE IF CAB CARD READ
    305 DC 310 I3.5
    IF (DATI(11).NE.DATI(1)) GO TO 605
310 CONTINUE
    CALL SWITCH
    EX=EXX
    INSEG=INSEG
    INDEX=DATI(3)
    HEAD (IREAD=620) STORE
    SAVE INPUT ON TAPE
C
C
C
605 IBAD=J
    IFORH=3
    WRITE (ISCR) IFORH,IBAD
    WRITE (ISCR=620) STORE
    DECODE (IV=0.0,STCR) IBCAR(INDEX)
    IF ((DATI(17).LE.0.).OR.(DATI(8).LE.0.).OR.(DATI(9).LE.0.)) IHAD=12
    IF ((DATI(17).LE.0.).OR.(DATI(8).LE.0.).OR.(DATI(9).LE.0.)) GO TO 511
    145 IF ((EX.LI.0.).OR.(DATI(10).LT.0.)) IHAD=13
    IF ((EX.LI.0.).OR.(DATI(10).LT.0.)) GO TO 545
    IF ((DATI(10).EQ.0.).AND.(EX.NE.0.)) IHAD=14
    IF ((DATI(10).EQ.0.).AND.(EX.NE.0.)) GO TO 545
    IF ((DATI(10).NE.0.).AND.(EX.EQ.0.)) IHAD=15
    IF ((DATI(10).NE.0.).AND.(EX.EQ.0.)) GO TO 545
    IF ((INSEG.LI.1.).OR.(INSEG.GT.50)) IBAD=10
    IF ((INSEG.LI.1.).OR.(INSEG.GT.50)) GO TO 545
    GO TO 125
C
C
C
625 GET HERE IF PCD CARD READ
    315 IF (FATE.PT.0.) GO TO 45
    GO TO 740

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630 C GET HERE IF LUN CAMD HEAD
C
C 320 INTAPE=DA11(5)
IFLG=DA11(6)
IF ((IFLG.LT.0).OR.(IFLG.GT.1)) IBAD=2
IF ((IFLG.LT.0).OR.(IFLG.GT.1)) GO TO 545
ISAVI=DA11(3)
IF ((IFLG.EQ.0) IHEAD=DA11(3)
IF ((IFLG.EQ.1) IHEAD=DA11(7)
OFLG=DA11(8)
IF ((OFLG.LT.0).OR.(OFLG.GT.2)) IBAD=3
IF ((OFLG.LT.0).OR.(OFLG.GT.2)) GO TO 545
IF (OFLG.EQ.0) OUTAPE=DA11(4)
IF (OFLG.NE.0) OUTAPE=DA11(9)
IF ((IPRINT.EQ.IREAD).OR.(IPRINT.EQ.INTAPE).OR.(OFLG.NE.0).AND.(IPRINT.EQ.
INTAPE).OR.(IPRINT.EQ.IREAD).OR.(INTAPE.EQ.IREAD).OR.(INTAPE.EQ.OUTAPE).OR.(IREA
20.EQ.OUTAPE).OR.(IFLG.EQ.1).AND.(IREAD.EQ.ISAVI))) IBAD=4
IF ((IPRINT.EQ.IREAD).OR.(IPRINT.EQ.INTAPE).OR.(OFLG.NE.0).AND.(IPRINT.EQ.
INTAPE).OR.(INTAPE.EQ.IREAD).OR.(INTAPE.EQ.OUTAPE).OR.(IREA
20.EQ.OUTAPE).OR.(IFLG.EQ.1).AND.(IREAD.EQ.ISAVI))) GO TO 545
GO TO 50
650 C GET HERE FOR EOP
C
C 325 IF (FATE.NE.0) CALL BADATA
IF (OFLG.EQ.0) GO TO 330
WRITE (OUTAPE,650) TEST(14)
330 IF (FATE.EQ.0) WRITE (IPRINT,655)
FATE=1.
RETURN
660 C CHECK TO SEE IF SUSPENDED ARRAY SOURCE DECK COMPLETE
C
C 335 IF ((IFJRC.EQ.0).OR.(IFRHU.LQ.0).OR.(NANC.EQ.0)) GO TO 570
GO TO 395
665 C CHECK TO SEE IF PARAMETRIC STUDY SOURCE DECK COMPLETE
C
C 340 IF ((IVOPT.EQ.0).OR.(IVUPJ.LQ.0.3)) GO TO 390
NZL=N
IF (INVSIG.EQ.0) IRAU=54
IF (INVSIG.EQ.0) GC TO 575
IF ((IFVEL.EQ.0) GC TO 370
IF (IVOPT.EQ.2) GO TO 355
670 C SORT VELOCITY PROFILE BY Z-COORDINATE
C
C DC 345 I=1,NVSEF
K=1
DC 345 J=K,NVSEF
IF (ZVEL(I).LE.ZVFL(J)) GO TO 345
TEMP=ZVEL(I)
ZVEL(I)=ZVEL(J)
ZVEL(J)=TEMP
TEMP=ZVEL(I)

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685 VELZ(I)=VELZ(J)
686 VELZ(J)=TEMP
687
688 345 CONTINUE
689
690 C UNITS CONVERSION
691
692 DO 350 I=1,NVSEG
693 VELXP(I)=VELZ(I)
694 VELYP(I)=C
695 VELZ(I)=VELZ(I)*CUNITS
696 VELX(I)=VELZ(I)
697 VELY(I)=0
698 GO TO 370
699
700 C SORT VELOCITY FOR CURRENT OPTION 2
701
702 DO 355 DO 360 I=1,NVSEG
703 N=I
704 DO 360 J=K,NVSEG
705 IF (ZVEL(I).LE.ZVEL(J)) GO TO 360
706 TEMP=ZVEL(I)
707 ZVEL(I)=ZVEL(J)
708 ZVEL(J)=TEMP
709 TVX=VELX(I)
710 TVY=VELY(I)
711 VELX(I)=VELX(J)
712 VELX(J)=TVX
713 VELY(I)=VELY(J)
714 VELY(J)=TVY
715 GO TO 360
716
717 C UNITS CONVERSION
718
719 DO 365 I=1,NVSEG
720 VELXP(I)=VELX(I)
721 VELYP(I)=VELY(I)
722 AMAG=VELX(I)
723 DIR=360-VELY(I)/PHI
724 VELX(I)=COS(DIR*PI)*AMAG*CUNITS
725 VELY(I)=SIN(DIR*PI)*AMAG*CUNITS
726 INDEX=ANJUNC(I)
727 ZANCM=PJUNC(3,INDEX)
728 IF (NANG.EQ.1) GO TO 380
729 UC 375 N=2,NANC
730 INDEX=ANJUNC(N)
731 IF (PJUNC(3,INDEX).LT.ZANCM) ZANCM=PJUNC(3,INDEX)
732
733 375 CONTINUE
734 380 IF (IVOPT.EG.1) ZVEL(I)=/ANCM
735 UC 385 N=1,NVSEG
736 IF (ZVEL(N).LE.ZANCM) NZL=N/L+1
737 385 CONTINUE
738 IF ((NZL.EQ.0).OR.(NANG.FU.0)) IRAD=54
739 IF ((PZL.EG.0).OR.(NANG.EQ.0)) GO TO 575
740 IF (HCOMP.EG.0) IRAD=53
741 IF (NCOMP.EG.0) GO TO 575
742 IF (INDAT.EQ.0) GO TO 415
743 RETURN

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C      CHECK ON CONTINUITY OF CABLE NUMBERING AND COUNT CABLES
C
C      395 NCAB=ICAB(22)
      DC 400 N=1,21
      NCAB=NCAB+ICAB(N)
      J=ICAB(N)-ICAB(N+1)
      IF (J.LT.0) GO TO 580
      400 CONTINUE
      IF (NCAB.EQ.0) GO TO 580
C
C      CHECK ON CONTINUITY OF JUNCTION NUMBERING AND COUNT JUNCTIONS
C
C      NJUNC=ICHECK(44)
      DC 405 N=1,43
      NJUNC=NJUNC+ICHECK(N)
      J=ICHECK(N)-ICHECK(N+1)
      IF (J.LT.0) GO TO 585
      405 CONTINUE
C
C      SORT DEVICES ON CABLE NO.(DATI(3))
C      AND DISTANCE FROM 0 JUNCTION(DATI(10))
C
      NDEV=INDEX
      CALL SORT (NDEV,INTAPE)
      IF (FATE.EQ.0.) GO TO 410
      GO TO 530
C
C      GET HERE IF ARRAY NUMBERED CORRECTLY
C      CHECK TO SEE IF NIR CONSISTENT
C
C      410 NIRC=NCAB+NANC-NOJUNC
      IF (NIRC.NE.NIRC) GO TO 590
C
C      GET HERE TO MAKE FINAL CHECK ON INTAPE
C
C      415 I=1
      420 DO 425 J=1,10
      425 DATI(J)=DATI(I,J)
      J=I+1
      IF (DATI(2).EC.TEST(1)) GO TO 430
      IF (DATI(2).EC.TEST(3)) GO TO 435
      IF (DATI(2).EC.TEST(4)) GO TO 440
      IF (DATI(2).EC.TEST(5)) GO TO 445
      IF (DATI(2).EC.TEST(9)) GO TO 450
      GO TO 420
C
C      GET HERE FOR IR
C
C      430 I=DATI(3)
      J2=DATI(4)
      IF (I01.LE.NOJUNC) IBAD=45
      IF (I01.LE.NOJUNC) GO TO 505
      IF (I02.GT.NOJUNC) IBAD=46
      IF (I02.GT.NOJUNC) GO TO 505
      IF (I03.GT.NOJUNC) GO TO 505
      IF (I03.GT.NOJUNC) IBAD=47
      IF (I03.GT.NOJUNC) GO TO 595
  
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800      GO TO 420
      C   GET HERE FOR CJNC
      C
      C 43E ID=UATI(3)
      IF (ID.GI.NJUNC) IBAD=51
      IF (ID.GI.NJUNC) GO TO 595
      GO TO 420
      C
      C   GET HERE FOR UCAB
      C
      C 440 ID=UATI(3)
      IF (ID.GI.NCAR) IBAD=49
      IF (ID.GI.NCAR) GO TO 595
      PL=H(ID)*(MODE(ID)-1)
      IF (UATI(10).GE.HL) IBAD=50
      IF (UATI(10).GE.HL) GO TO 595
      GO TO 420
      C
      C   GET HERE FOR CAB
      C
      C 445 ID=UATI(4)
      IF (ID.GI.NJUNC) IBAD=48
      IF (ID.GI.NJUNC) GO TO 595
      GO TO 420
      C
      C   GET HERE FOR EOD
      C
      C 450 WRITE (INTAPE,660) ((UATI(I,J),J=1,10),I=1,(RMAX)
      REMIND INTAPE
      IF (INDATC.NE.0.AND.FATE.EQ.0.) RETURN
      IF (FATE.EQ.0.) GO TO 455
      GO TO 50
      C
      C   GET HERE IF ALL OK AND CALCULATE PATH
      C
      C   K IS CABLE COUNTER
      C
      C 455 K=0
      C
      C   LOOP=1 LOOKING FOR CABLES LEAVING ANCHORS
      C
      C   LOOP=1
      C
      C   JMINP REMEMBERS FIRST VALUE OF K ON A LEVEL OF TREE
      C
      C   JMINP=1
      C
      C   JMAX REMEMBERS NUMBER OF CABLES ON A LEVEL OF TOPOGRAPHIC TREE
      C
      C   JMAX=NAC
      IF (LOOP.EQ.1) GO TO 465
      C
      C 460 JMAX=
      IF ((LOOP.EQ.1).AND.(K.NE.1)) GO TO 600
      C
      C   ( (LOOP.EQ.2).AND.(JMINP.GE.JMINP)) GO TO 600
      C   (K.NE.NCAR) GO TO 50
      C
      C   LOOP=2
      C   JMIN=JMINP
      C
      C 465

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      DC 495 J=JMIN,JMAX
      LOOKING FOR CABLES LEAVING A JUNCTION
      DC 490 N=1,NCAH
      GC TO (470,475), LOOP
      470 IF (ZJUNC(N).EQ.AJUNC(J)) GO TO 480
      GC TO 490
      475 IPATHJ=PATH(J)
      IF (ZJUNC(N).EQ.LJUNC(IPATHJ)) GO TO 480
      GC TO 490
      C
      C GET HERE IF CABLE N STARTS AT JUNCTION M
      C
      C 480 K=K+1
      PATH(K)=N
      GC TO (490,485), LOOP
      C
      C REMEMBER HERE FIRST VALUE OF K ON TREE LEVEL
      C
      485 IF (JMAX.EQ.(K-1)) JMINP=K
      490 CONTINUE
      495 CONTINUE
      GC TO 460
      C
      C PUT DATA INTO DATA ARRAY
      C
      C
      500 IF (IFCUD.NE.0) GO TO 515
      IF ((DATA(2).EQ.TEST(3)).OR.(DATA(2).EQ.TEST(4))). GO TO 505
      GC TO 515
      505 ID=INDEX
      DC 510 J=1,10
      DATI(IROW,J)=DATI(ID,J)
      510 DATI(ID,J)=DATI(J)
      GC TO 525
      515 DC 520 J=1,10
      520 DATI(IROW,J)=DATI(J)
      525 IROW=IROW+1
      IF (IROW.EQ.0) GO TO 180
      IF (IROW.LE.2150) GO TO 50
      *RIPE (IPRINT,665)
      GC TO 50
      C
      C THIS SECTION GENERATES ALL ERROR MESSAGES
      C
      C
      530 FATE=1.
      IFORNE=4
      WRITE (ISCK) (FORP,IBAD
      535 IF (NDATC.EQ.0) GC TO 50
      GC TO 180
      540 IFM=6
      IBAD=1
      GC TO 530
      545 IFM=1
      GC TO 530
      550 IFM=2
      GC TO 530

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555 IER=3
    IBAU=32
    GC TO 530
915
560 IER=4
    GC TO 530
565 IER=6
    GC TO 530
920
570 IER=7
    FATE=1
    IFORM=5
    IBAU=41
    WRITE (ISCR) IFORM,IBAD
925
    WRITE (ISCR) IFUNC,IFRMO,NANC
    GC TO 535
575 IER=14
    FATE=1
    IFORM=6
    WRITE (ISCR) IFORM,IBAD
930
    WRITE (ISCR) ACUMP,IVORI,NVSEG,NZL,NANG
    GC TO 535
580 IER=8
    FATE=1
    IBAU=42
    IFORM=7
935
    WRITE (ISCR) IFORM,IBAD
    WRITE (ISCR) (ICAB(I),I=1,22)
    GC TO 535
585 IER=9
    FATE=1
    IBAU=43
    IFORM=8
940
    WRITE (ISCR) IFORM,IBAD
    WRITE (ISCR) (ICHECK(I),I=1,44)
    GC TO 535
590 IER=11
    FATE=1
    IBAU=44
    IFORM=9
945
    WRITE (ISCR) IFORM,IBAD
    WRITE (ISCR) ACAB,NANC,NDJUNC,NIRC,NIH
    GC TO 535
595 IER=12
    GC TO 530
600 IER=13
    FATE=1
    IBAU=52
950
    GC TO 530
    DATA(1)=DATA(1)
960
    DATA(2)=DATA(2)
    IER=15
    IBAU=55
965
    GC TO 530
    IER=14
    IBAU=56
    IF(ODL.EQ.0) GC TO 530
    DATA(1)=DATA(1)
    DATA(2)=DATA(2)

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970 C GO TO 530
 624 FORMAT (A16)
 625 FORMAT (A5,A3)
 630 FORMAT (F4.0,A4,DF8.0,F15.0,F13)
 975 635 FORMAT (F4.0,A4,RE15.8,F17.5,I3)
 640 FORMAT (I8,F8.0)
 645 FORMAT (RE15.8)
 650 FORMAT (A4,I4,3E15.8)
 980 655 FORMAT (I1,I18,ANALYSIS COMPLETED)
 660 FORMAT (F4.0,A4,RE15.8)
 665 FORMAT (BX,PH17,18X,45HC,COMMON/B1/
 BOUND EXCEEDED. SEE USERS MANUAL
 INP 982
 INP 983-
 IL.)
 END

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

861 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
 872 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

FIN 4.6.433E

SUBROUTINE PHS001 7/774 DPT=1

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1 PHS 1
2 PHS 2
3 PHS 3
4 PHS 4
5 PHS 5
6 PHS 6
7 PHS 7
8 PHS 8
9 PHS 9
10 PHS 10
11 PHS 11
12 PHS 12
13 PHS 13
14 PHS 14
15 PHS 15
16 PHS 16
17 PHS 17
18 PHS 18
19 PHS 19
20 PHS 20
21 PHS 21
22 PHS 22
23 PHS 23
24 PHS 24
25 PHS 25
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48 PHS 48
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50 PHS 50
51 PHS 51
52 PHS 52
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55 PHS 55
56 PHS 56
57 PHS 57

*DECK PHS001
SUBROUTINE PHS001
C
C THIS ROUTINE GENERATES INFORMATION CONCERNING THE PHYSICAL
C CHARACTERISTICS OF THE STRUCTURAL CABLE ARRAY.
C
COMMON /H3/ VEX(25),VELY(25)
COMMON /H1/ FEJUNC,IR,DELTAI,DELTA,IRS,TFJUNC,E,ES,FCAB,KCAB,JUMP,PMS
1PJUNCS,PCAB,PCABE,PCABU,PCABO,THETA,PJUNCO
COMMON /H2/ NCAB,MODE,ERJUNC,IRJUNC,DATA1,DATA2,PJUNC,DCAB,DCABPMS
IFATE,NANC,ANJUNC,INEAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEPMS
2IAS,THETA,CMPD,THEIAB,NJUNC,RHO,TEST,NVSEF,VELZ,VELZPIP,ECICAB,PMS
3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IYOPT,MCAB,IDEV,ICHECK,NDEV,NDATC
COMMON /IANC/ ICAB(22),TUDCAB(1000)
COMMON /IITL/ IITL(8),PHI
COMMON /PL/ IPUPCH,IPACK,IITLEM(8),DEVMT
DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), TFJUNC(3,44), PJUNCO(PMS
13,44)
DIMENSION FCAB(3,51,22), KCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)PMS
1)
DIMENSION PCABE(3,51,22), PCABO(3,51,22), PCABU(3,51,22)
DIMENSION MODE(22), ERJUNC(44), IRJUNC(44), DATA(10), DATN(10),
1122)
DIMENSION PJUNC(3,44), DCAB(22), DCAB(22), ANJUNC(44), TEST(14)
DIMENSION VEL(25), VELY(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
DIMENSION CJUNC(22), PATH(22), ICAB(22), *CAR(22), *DEV(1000)
DIMENSION ICHECK(44)
INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
REAL IR,IFS
WRITE (IPRNT,40) TITLEM
IF (INDAIC.NE.0) WRITE (IPRNT,45) TITLE
WRITE (IPRNT,50)
*WRITE (IPRNT,55) PMS
IF (PHI.NE.0) WRITE (IPRNT,60)
IF (PHI.LG.0) WRITE (IPRNT,65)
WRITE (IPRNT,70)
*WRITE (IPRNT,75) NANC
DC 5 N=1,NANC
INDEX=ANJUNC(N)
5 WRITE (IPRNT,80) INDEX,(PJUNC(I,INDEX),I=1,3)
NCJUNC=NCZB+NARC-NIR
WRITE (IPRNT,85) NJUNC
WRITE (IPRNT,90) NIR
IF (NIR.LG.0) GO TO 15
DC 10 N=1,NIR
10 WRITE (IPRNT,95) INJUNC(N),ERJUNC(N)
15 *WRITE (IPRNT,100) NCAB
DC 20 N=1,NCAB
NSEG=MODE(N)-1
PL=H(N)*NSLC
*WRITE (IPRNT,105) (ZJUNC(N),LJUNC(N),PL,DCAB(N),*CAR(N),CDCAB(N),PMS
20 JFCICAB(N)+EXPCAB(N),NSEL,ICAB(N)
*WRITE (IPRNT,110)
25 *READ (IR,115) (DATA(I),I=1,10)
IF (DATA(2).EQ.TEST(3)) GO TO 30
IF (DATA(2).EQ.TEST(9)) GO TO 35

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60      GC TO 25
        30 JUNC=DAT1(3)
        WRITE (IPRINT,120) JUNC,(UATI(K),K=6,8)
        GC TO 25
        35 REMIND INTAKE
        WRITE (IPRINT,125) NCEX
        65      WRITE (IPRINT,130) CONFD
        IF (OFLG*E=0) WRITE (IPRINT,135) NDAIC
        RETURN
C
        40 FORMAT (1P1,8A10)
        45 FORMAT (//1A,8A10)
        50 FORMAT (//155H PHYSICAL CHARACTERISTICS OF THE STRUCTURAL CABLE APHS
        1ARRAY)
        55 FORMAT (//,1H,PHI=#F10.2)
        60 FORMAT (//,117H THE ANGLE PHI IS THE ANGLE BETWEEN THE MAGNETIC NOPS
        17TH AXIS AND THE X-AXIS OF THE ARRAY REFERENCED COORDINATE SYSTEM,PHS
        2/128H THE ANGLE IS GIVEN IN DEGREES AND IS POSITIVE FOR A CLOCKWPHS
        31SE ROTATION OF THE X-AXIS WITH RESPECT TO THE MAGNETIC NORTH AXISPHS
        4.)
        65 FORMAT (//,81P SINCE PHI=0, THE MAGNETIC AND ARRAY REFERENCED COORPHS
        10INATE SYSTEMS ARE IDENTICAL.)
        70 FORMAT (//,94P ALL X,Y,Z RESULTS AND DISPLACEMENTS ARE GIVEN IN IPHS
        80)
        75 FORMAT (//,19H NO. OF ANCHORS IS ,12,//5A,64HJUNCTION NO. X-COPHS
        1,12HJUNCTION NO.),//48X,6HOF CUT,16X,17HAI WHICH CUT MADE)
        80 FORMAT (10X,12,4X,315X,F10.2,3X))
        85 FORMAT (//,34P NO. OF JUNCTIONS IN ORIGINAL ARRAY IS ,12)
        90 FORMAT (//,39P NO. OF CUTS MADE IN ORIGINAL ARRAY IS ,12//1H ,2(51XPHS
        1,12HJUNCTION NO.),//48X,6HOF CUT,16X,17HAI WHICH CUT MADE)
        95 FORMAT (10Y,12,15X,12)
        100 FORMAT (//,18P NO. OF CABLES IS ,12,//5X,16HCABLE S=0 $=L,41X,9PHS
        1MORUM DRAG,16X,22P-CONSTITUTIVE NO. OF,5X,9HANG DRAG,16X,3HNO,PHS
        21X,2(2X,4HJUNC),3X,6HLENGTH,03X,8HDIAMETER,3X,13HWEIGHT/LENGTH,3X,PHS
        311HCOEFFICIENT,3X,8HSTIFFIDITY,6X,8HEXPOONENT,5X,8HELEMENTS,3X,11HCOEPHS
        4FFICIENT)
        105 FORMAT (5X,12,5X,12,4X,12,11X,F9.2,3(3X,F7.3,4X),F10.0,7X,F6.3,9X,1,PHS
        12,6X,F11.2)
        110 FORMAT (//,63H PROPERTIES OF THE DEVICES LOCATED AT JUNCTIONS ARE PHS
        1AS FOLLOWS //76X,6HDEVICE,10X,6HDEVICE,9X,11HDEVICE DRAG,4X,14HDEVPHS
        2ICE FRONTAL,15X,9HJUNC. NO.,8X,6HWEIGHT,9X,11HCOEFFICIENT,9X,4HMAPHS
        3EA)
        115 FORMAT (F4.0,9A,HE15.8)
        120 FORMAT (8X,12,9X,F10.2,6X,F10.3,6X,F10.2)
        125 FORMAT (//,12P TOTAL NO. OF INDEXED DEVICES IS,14)
        130 FORMAT (//,39H ACCURACY REQUIRED IN CALCULATIONS IS ,F8.4)
        135 FORMAT (//,20H DEVICE LOCATION OUTPUT RECORD,1J,21H REFERS TO THISPHS
        1 ARRAY)
        105      1 EPD
        PHS 58
        PHS 59
        PHS 60
        PHS 61
        PHS 62
        PHS 63
        PHS 64
        PHS 65
        PHS 66
        PHS 67
        PHS 68
        PHS 69
        PHS 70
        PHS 71
        PHS 72
        PHS 73
        PHS 74
        PHS 75
        PHS 76
        PHS 77
        PHS 78
        PHS 79
        PHS 80
        PHS 81
        PHS 82
        PHS 83
        PHS 84
        PHS 85
        PHS 86
        PHS 87
        PHS 88
        PHS 89
        PHS 90
        PHS 91
        PHS 92
        PHS 93
        PHS 94
        PHS 95
        PHS 96
        PHS 97
        PHS 98
        PHS 99
        PHS 100
        PHS 101
        PHS 102
        PHS 103
        PHS 104
        PHS 105
        PHS 106-
    
```

```

1  *DECK HPCLY
2  SUBROUTINE HPCLY (C,RR,RI)
3
4  C
5  C THIS ROUTINE FINDS REAL ROOTS OF POLYNOMIAL EQUATIONS UP TO
6  C  $C(4) \cdot (X^4) + C(3) \cdot (X^3) + C(2) \cdot (X^2) + C(1) \cdot X + C(0) = 0$  FOR USE IN
7  C EVALUATING MAXIMUM CABLE DISPLACEMENTS AND TENSION EXTREMA
8  C
9  C REAL PARTS OF ROOTS ARE PLACED IN RR, IMAGINARY PARTS IN RI
10 C SINCE ONLY REAL ROOTS ARE OF INTEREST, ALL NON-REAL OR
11 C NON-EXISTING ROOTS RETURN RR=0, RI=1
12 C
13 C DIMENSION C(4), RR(3), RI(3)
14 C IF (C(4).NE.0.) GO TO 40
15 C IF (C(3).NE.0.) GO TO 30
16 C IF (C(2).NE.0.) GO TO 15
17 C
18 C GET HERE IF EQUATION IDENTICALLY SATISFIED.
19 C
20 C 5  DO 10 I=1,3
21 C   RR(I)=0.
22 C   RI(I)=1.
23 C   RETURN
24 C
25 C GET HERE IF EQUATION LINEAR
26 C
27 C 15  RR(1)=-C(1)/C(2)
28 C   RI(1)=0.
29 C   DO 25 I=2,3
30 C     RR(I)=0.
31 C     RI(I)=1.
32 C   RETURN
33 C
34 C GET HERE IF EQUATION QUADRATIC
35 C
36 C 30  DTSC=C(2)**2-4.*C(1)*C(3)
37 C   IF (DTSC.GE.0.) GO TO 35
38 C   GO TO 5
39 C 35  RR(1)=(-C(2)+SQRT(DTSC))/(2.*C(3))
40 C   RI(1)=0.
41 C   RR(2)=(-C(2)-SQRT(DTSC))/(2.*C(3))
42 C   RI(2)=0.
43 C   RR(3)=0.
44 C   RI(3)=1.
45 C   RETURN
46 C
47 C GET HERE IF EQUATION CUBIC
48 C
49 C 40  P=C(3)/C(4)
50 C   Q=C(2)/C(4)
51 C   R=C(1)/C(4)
52 C   A=(3.*Q-P**2)/3.
53 C   H=(2.*P**3-9.*P*Q+27.*R)/27.
54 C   DTSC=(H**2)/4.+(A**3)/27.
55 C   F=DTSC
56 C   IF (F.LE.0.) GO TO 50
57 C   IF (H/2.*F**0.5) CAPA=1.
58 C   IF (H/2.*F**0.5) CAPA=1+((-B/2.+DTSC)**0.5)/((-B/2.-DTSC)

```

131

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60 CAPB=((1+P/2,-DISC)**4)**(1./3.)/(-B/2.-DISC)
   RH(1)=CAPB*CAFU-P/3.
   RI(1)=0.
   IF (DISC.GT.0.) GO TO 20
   RH(2)=-CAFA-P/3.
   RI(2)=0.
   RH(3)=RH(2)
   PI(3)=0.
65 RETURN
50 DISC=2.*SGT(-A/3.)
   PH=ACOS(1+3.*B)/(A*DISC)/3.
   RF(1)=-P/3.+DISC*COS(PH)
   RH(2)=-P/3.+DISC*COS(PH+3.14159265*(2./3.))
   RH(3)=-P/3.+DISC*COS(PH+3.14159265*(4./3.))
   PI(1)=0.
   PI(2)=0.
   PI(3)=0.
70 RETURN
75 END

```

RPO 58
RPO 59
RPO 60
RPO 61
RPO 62
RPO 63
RPO 64
RPO 65
RPO 66
RPO 67
RPO 68
RPO 69
RPO 70
RPO 71
RPO 72
RPO 73
RPO 74
RPO 75
RPO 76-


```

1      *DECK START
2      SUBROUTINE START
3
4
5      C
6      C THIS ROUTINE CALCULATES THE INITIAL GUESSES AT THE IMAGINARY
7      C AND EQUILIBRATING REACTIONS AND THE INITIAL DELTA BASED ON
8      C THE TOTAL WEIGHT OF THE ARRAY
9
10     COMMON /B3/ VELX(25),VELY(25)
11     COMMON /B1/ FEJUNC,IR,DELTA1,DELTA,IRMS,IFJUNC,E,ES,FCAB,RCAB,JUMP,STA
12     IPJUNCS,PCAB,PCABE,PCABU,RCABU,TRETA,PJUNCO
13     COMMON /B2/ NCAB,NNODE,ERJUNC,IRJUNC,DATI,DATN,P,PJUNC,CUCAB,DCAB,STA
14     IFATE,NANC,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THESTA
15     ZIAB,THETA,CUPPD,THFTAB,HJUNC,RHO,TEST,NVSE,VELZ,VELZ,PIP,ECICAB,STA
16     DEPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WCA,IOEV,ICHECK,NDEV,NUATC
17     DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNCO(STA
18     13,44)
19     DIMENSION FCAB(3,51,22), HCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)
20     1)
21     DIMENSION PCABE(3,51,22), PCABU(3,51,22), RCABU(3,51,22)
22     DIMENSION NNODE(22), ERJUNC(44), IHJUNC(44), DATI(10), DATN(10), HSTA
23     1(22)
24     DIMENSION PJUNC(3,44), DCAB(22), DCAB(22), ANJUNC(44), TEST(14)
25     DIMENSION VELZ(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
26     DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(100)
27     DIMENSION ICHECK(44)
28     INTEGER OLTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
29     INTEGER PATH
30     REAL IR,IFS
31     WEIGHT=0.
32     DO 5 J=1,PJUNC
33     5 WEIGHT=WEIGHT+FEJUNC(3,J)
34     DC 10 WEI,NCAB
35     IANN=NNODE(N)-1
36     DC 10 WEI,IANN
37     10 WEIGHT=WEIGHT+FCAB(3+M*N)
38     DC 15 WEI,NIR
39     KER=ERJUNC(N)
40     DC 15 IEL,J
41     IR(1,KER)=0.
42     DC 20 NEI,NIR
43     KIH=IRJUNC(N)
44     KER=ERJUNC(N)
45     IR(1,KIH)=0.
46     IR(2,KIH)=0.
47     IR(3,KIH)=WEIGHT/(NIR+1.101)
48     IR(3,KER)=IR(3,KER)-IR(3,NTH)
49     DELTAI=ABS(WEIGHT)/(NIR+1)
50     RETURN
51     FNO

```

```

1      *DECK STROUT
2      SUBROUTINE SHOUT
3
4      C
5      C      THIS ROUTINE GENERATES THE ARRAY STRUCTURAL OUTPUT
6
7      COMMON /B3/ VELX(25),VELY(25)
8      COMMON /B1/ FEJUNC,IR,DELTA,DELTA,IRS,IFJUNC,E,ES,FCAB,H CAB,JUMP,STR
9      IPJUNC,PCAB,PCAB,PCAB,RCAB,THE TA,PJUNC
10     COMMON /B2/ H CAB,ANODE,ERJUNC,IRJUNC,DATI,DATI,F,PJUNC,CUCAB,DCAB,STR
11     IFATE,NANC,ANJUNC,INHEAD,IPHNT,INTAPE,OUTAPE,ITIME,IFLG,DFLG,NIR,THESTR
12     2TAS,THE TAE,CUMPO,THE TAJ,ANJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,STR
13     3EPCAB,ZJUNC,ZJUNC,FATH,ICAB,IVOPT,WCAB,IDEV,ICHECK,NDEV,NDATC
14     COMMON /CVEL/ VMAG(25,4),VDIR(25,4),XPT(25,4),YPT(4),NPPS(4,STR
15     1),NSTA
16     COMMON /LEVEL/ IFVEL
17     COMMON /PCUR/ XNPT(4),YMP1(4)
18     COMMON /TAUKG/ IDCAB(22),TDDCAB(1000)
19     COMMON /TITL/ TITL(8),PHI,CURVITS,IUNIT,VELXP(25),VELYP(25)
20     COMMON /PL/ IPUNCH,IPKCH,IILEM(8),DEW1
21     COMMON /KILLER/ KOUNTN,NIT,MAITER,NSTEPS,ISTEP,PERCNTV,INCPRT
22     DIMENSION FEJUNC(3,4), IH(3,4), IHS(3,4), IFJUNC(3,4), PJUNCO(STR
23     13,4)
24     DIMENSION FCAB(3,5),22), H CAB(3,5),22), PJUNCS(3,4), PCAB(3,5),22)STR
25     1)
26     DIMENSION PCABE(3,5),22), PCABU(3,5),22), RCABU(3,5),22)
27     DIMENSION RMODE(22), ERJUNC(44), IRJUNC(44), DATI(10), UATN(10), HSTR
28     1(22)
29     DIMENSION PJUNC(3,4), CUCAB(22), DCAB(22), ANJUNC(44), TEST(14)
30     DIMENSION /VEL(25), VELZ(25), ECICAB(22), [XPCAB(22), ZJUNC(22)
31     DIMENSION ICHECK(44)
32     DIMENSION SPACE(3,1000), PJORIG(3,4), DISPO(3)
33     DIMENSION NSEW(4)
34     DIMENSION UBITS(3)
35     INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,DFLG
36     INTEGER PATH
37     REAL IR,IHS
38     DIMENSION TEMP1(3), TEMP2(3), TEMP3(3), DISP(3), PSPACE(3)
39     DIMENSION A(3), H(3), D(3), U(3), V(3), W(3), C(4), RI(3)
40     DATA NSEW/5,6,7,8,9,10,11,12,13,14,15,16,17,18,19,20,21,22,23,24,25/
41     DATA UNITS/24 (KNOTS),86 (CM/SEC),86 (FT/SEC)/
42     NCJUNC=NCAB+NANC-NIR
43     JUM=JUMP+1
44     FACTOR=1
45     PCT=PERCNTV*100.
46     IF (INCPRT.EQ.1) FACTOR=PERCNTV
47     GO TO (5,10), JUM
48     5 WRITE (IPRNT,465) TITL
49     IF (IPUNCH.EQ.8H YES) WRITE (IPNCH,470) TITL,FM
50     GO TO 55
51     10 WRITE (IPRNT,475) TITL,FM,IILE
52     WRITE (IPRNT,480) KOUNTN
53     IV=IVORT+1
54     GO TO (15,20,30,40), IV
55     C
56     C      CURRENT OPTION 0
57     C

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115 WRITE (IPRINT,545)
    IF (IPUNCH.EQ.8H) YES) WRITE (IPNCH,490) TITLE
    IF (IPUNCH.EQ.8H) YES) WRITE (IPNCH,495) IVOPT.
    C
    C
    C
120 GENERATE ANCHOR HEADERS
    C
    C
    C
125 WRITE (IPRINT,550)
    WRITE (IPRINT,555)
    WRITE (IPRINT,560)
    WRITE (IPRINT,565)
    C
    C THIS SECTION CALCULATES FORCES AND ANGLES AT ANCHORS
    C
    C
    C DO 110 J1=1,NANC
      J2=0
      J2=1
    60 IF (ANJUNC(J1).EQ.2JUNC(J2)). GO TO 100
    65 J2=J2+1
      IF (J2.LE.NCAD) GO TO 60
      IF (NIR.EQ.0) GO TO 110
    70 J3=1
    75 IF (ANJUNC(J1).EQ.ERJUNC(J3)) GO TO 85
    80 J3=J3+1
      IF (J3.LE.NIH) GO TO 75
      GO TO 110
    85 INDEX=IRJUNC(J3)
    90 IF (INDEX.EG.LJUNC(J4)) GO TO 95
    95 CONTINUE
      GO TO 110
    100 MM=J2
      MX=NODE(J4)
      Y=TCAB(MX,MP)
      HY=RCAB(1,IX,MM)
      HZ=RCAB(2,IX,MM)
      AZ=RCAB(3,IX,MM)
      GO TO 105
    105 MM=J2
      Y=TCAB(1,PM)
      HY=RCAB(1,IX,MM)
      HZ=RCAB(2,IX,MM)
      AZ=RCAB(3,IX,MM)
      MM=J2
    110 MM=J2
      IF (RZ.EG.0.) RH=1.
      A1=ASIN(RY/RH)/PI
      IF (RZ.EG.0.) RH=0.
      A2=ASIN(HZ/1)/PI
      IF (HX.LI.0.) AND. (RY.GE.0.)) A1=180.-A1
      IF (HX.LI.0.) AND. (RY.LI.0.)) A1=-180.-A1
      WRITE (IPRINT,570) ANJUNC(J1),MM,1,PA,RY,RZ,RH,A1,A2
      IF (J2.EG.NCAD) AND. (J3.EG.0.) GO TO 70
      IF (J2.EG.NCAD) AND. (J3.NE.NJUNC)) GO TO 80
    111 CONTINUE
    C
    C GENERATE CARLF HEADERS

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172 STR 172
173 STR 173
174 STR 174
175 STR 175
176 STR 176
177 STR 177
178 STR 178
179 STR 179
180 STR 180
181 STR 181
182 STR 182
183 STR 183
184 STR 184
185 STR 185
186 STR 186
187 STR 187
188 STR 188
189 STR 189
190 STR 190
191 STR 191
192 STR 192
193 STR 193
194 STR 194
195 STR 195
196 STR 196
197 STR 197
198 STR 198
199 STR 199
200 STR 200
201 STR 201
202 STR 202
203 STR 203
204 STR 204
205 STR 205
206 STR 206
207 STR 207
208 STR 208
209 STR 209
210 STR 210
211 STR 211
212 STR 212
213 STR 213
214 STR 214
215 STR 215
216 STR 216
217 STR 217
218 STR 218
219 STR 219
220 STR 220
221 STR 221
222 STR 222
223 STR 223
224 STR 224
225 STR 225
226 STR 226
227 STR 227
228 STR 228

```

C
WRITE (IPRINT,575)
WRITE (IPRINT,580)
IF (JUM,61,1) GO TO 115
WRITE (IPRINT,595)
GO TO 120
115 WRITE (IPRINT,590)
WRITE (IPRINT,595)
120 CONTINUE
C
THIS SECTION CALCULATES MAXIMUM AND MINIMUM CABLE TENSIONS
AND MAXIMUM CABLE DISPLACEMENTS FROM NO CURRENT LOCATION
BY EXTRAPOLATION BETWEEN CABLE NODES
C
INITIALIZE EXTREMA
C
DO 295 MN=1,NCAB
N=NN
IPAX=ICAB(1,N)
SIMAX=0.
IMIN=IMAX
SIMIN=0.
130 DO 130 I=1,3
135 DO 135 I=1,3
140 DO 140 I=1,3
145 DO 145 I=1,3
150 DO 150 I=1,3
155 DO 155 I=1,3
160 DO 160 I=1,3
165 DO 165 I=1,3
170 DO 170 I=1,3
175 DO 175 I=1,3
180 DO 180 I=1,3
185 DO 185 I=1,3
190 DO 190 I=1,3
195 DO 195 I=1,3
200 DO 200 I=1,3
205 DO 205 I=1,3
210 DO 210 I=1,3
215 DO 215 I=1,3
220 DO 220 I=1,3
225 DO 225 I=1,3
230 DO 230 I=1,3
235 DO 235 I=1,3
240 DO 240 I=1,3
245 DO 245 I=1,3
250 DO 250 I=1,3
255 DO 255 I=1,3
260 DO 260 I=1,3
265 DO 265 I=1,3
270 DO 270 I=1,3
275 DO 275 I=1,3
280 DO 280 I=1,3
285 DO 285 I=1,3
290 DO 290 I=1,3
295 DO 295 I=1,3
300 DO 300 I=1,3
305 DO 305 I=1,3
310 DO 310 I=1,3
315 DO 315 I=1,3
320 DO 320 I=1,3
325 DO 325 I=1,3
330 DO 330 I=1,3
335 DO 335 I=1,3
340 DO 340 I=1,3
345 DO 345 I=1,3
350 DO 350 I=1,3
355 DO 355 I=1,3
360 DO 360 I=1,3
365 DO 365 I=1,3
370 DO 370 I=1,3
375 DO 375 I=1,3
380 DO 380 I=1,3
385 DO 385 I=1,3
390 DO 390 I=1,3
395 DO 395 I=1,3
400 DO 400 I=1,3
405 DO 405 I=1,3
410 DO 410 I=1,3
415 DO 415 I=1,3
420 DO 420 I=1,3
425 DO 425 I=1,3
430 DO 430 I=1,3
435 DO 435 I=1,3
440 DO 440 I=1,3
445 DO 445 I=1,3
450 DO 450 I=1,3
455 DO 455 I=1,3
460 DO 460 I=1,3
465 DO 465 I=1,3
470 DO 470 I=1,3
475 DO 475 I=1,3
480 DO 480 I=1,3
485 DO 485 I=1,3
490 DO 490 I=1,3
495 DO 495 I=1,3
500 DO 500 I=1,3
505 DO 505 I=1,3
510 DO 510 I=1,3
515 DO 515 I=1,3
520 DO 520 I=1,3
525 DO 525 I=1,3
530 DO 530 I=1,3
535 DO 535 I=1,3
540 DO 540 I=1,3
545 DO 545 I=1,3
550 DO 550 I=1,3
555 DO 555 I=1,3
560 DO 560 I=1,3
565 DO 565 I=1,3
570 DO 570 I=1,3
575 DO 575 I=1,3
580 DO 580 I=1,3
585 DO 585 I=1,3
590 DO 590 I=1,3
595 DO 595 I=1,3
600 DO 600 I=1,3
605 DO 605 I=1,3
610 DO 610 I=1,3
615 DO 615 I=1,3
620 DO 620 I=1,3
625 DO 625 I=1,3
630 DO 630 I=1,3
635 DO 635 I=1,3
640 DO 640 I=1,3
645 DO 645 I=1,3
650 DO 650 I=1,3
655 DO 655 I=1,3
660 DO 660 I=1,3
665 DO 665 I=1,3
670 DO 670 I=1,3
675 DO 675 I=1,3
680 DO 680 I=1,3
685 DO 685 I=1,3
690 DO 690 I=1,3
695 DO 695 I=1,3
700 DO 700 I=1,3
705 DO 705 I=1,3
710 DO 710 I=1,3
715 DO 715 I=1,3
720 DO 720 I=1,3
725 DO 725 I=1,3
730 DO 730 I=1,3
735 DO 735 I=1,3
740 DO 740 I=1,3
745 DO 745 I=1,3
750 DO 750 I=1,3
755 DO 755 I=1,3
760 DO 760 I=1,3
765 DO 765 I=1,3
770 DO 770 I=1,3
775 DO 775 I=1,3
780 DO 780 I=1,3
785 DO 785 I=1,3
790 DO 790 I=1,3
795 DO 795 I=1,3
800 DO 800 I=1,3
805 DO 805 I=1,3
810 DO 810 I=1,3
815 DO 815 I=1,3
820 DO 820 I=1,3
825 DO 825 I=1,3
830 DO 830 I=1,3
835 DO 835 I=1,3
840 DO 840 I=1,3
845 DO 845 I=1,3
850 DO 850 I=1,3
855 DO 855 I=1,3
860 DO 860 I=1,3
865 DO 865 I=1,3
870 DO 870 I=1,3
875 DO 875 I=1,3
880 DO 880 I=1,3
885 DO 885 I=1,3
890 DO 890 I=1,3
895 DO 895 I=1,3
900 DO 900 I=1,3
905 DO 905 I=1,3
910 DO 910 I=1,3
915 DO 915 I=1,3
920 DO 920 I=1,3
925 DO 925 I=1,3
930 DO 930 I=1,3
935 DO 935 I=1,3
940 DO 940 I=1,3
945 DO 945 I=1,3
950 DO 950 I=1,3
955 DO 955 I=1,3
960 DO 960 I=1,3
965 DO 965 I=1,3
970 DO 970 I=1,3
975 DO 975 I=1,3
980 DO 980 I=1,3
985 DO 985 I=1,3
990 DO 990 I=1,3
995 DO 995 I=1,3
1000 DO 1000 I=1,3

```

230      MM=0.
        DC 165 I=1,3
        V(I)=EXCAB(M,N)*RCAB(I,M,N)/TCAB(M,N)
        W(I)=(EXCAB(M,N)*RCAB(I,M,N)/TCAB(M,N)-V(I))/MIN
        V(I)=A(I)-V(I)
        W(I)=(R(I)-W(I))/2.
        UL=UU+U(I)*V(I)
        UV=UV+U(I)*V(I)
        VW=UVW+2.*U(I)*W(I)+V(I)*V(I)
        165      MM=MM+W(I)*W(I)
        DC 170 I=1,3
        RCAB(I,M,N)=TEMP1(I)
        170      RCAB(I,M,N)=TEMP2(I)
        175      C(4)=0.
        C(3)=0.
        C(2)=DU
        C(1)=R0
        CALL RPOLY (C,R0,PI)
C
C      CALCULATE TENSION EXTREMA IN SEGMENT
C
        JTIME=0
        180      CONTINUE
        DC 205 I=1,3
        IF (JTIME.EQ.1) GO TO 185
        IF (HI(I).NE.C) GO TO 205
        IF ((HO(I).LE.0.).OR.(RW(I).GE.M(N))) GO TO 205
        SIG=KG(I)
        185      T=SQRT(HR+2.*HD*SIG*DD*SIG**2)
        IF (T.E.GT.TMAX) GO TO 195
        IF (T.E.LT.TMIN) GO TO 200
        190      IF (JTIME.EQ.0) GO TO 205
        195      TMAX=T
        200      TMIN=T
        205      STMIN=(I)*(M-I)*SIG
        GO TO 190
        210      CONTINUE
        JTIME=1
        SJ=SM(N)
        215      GO TO 180
        210      GO TO (245,215)+JUM
        215      C(4)=2.*W
        C(3)=3.*VW
        C(2)=UVW
        C(1)=1
        CALL RPOLY (C,R0,PI)
C
C      CALCULATE MAXIMUM DISPLACEMENT IN SEGMENT
C
        JTIME=0
        220      CONTINUE
        DC 240 I=1,3
        IF (JTIME.EQ.1) GO TO 225

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STR 229
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 STR 285

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IF (PI(I).NE.0.) GO TO 240
IF ((HO(I).LE.0.)OH.(AG(I).GE.H(N))) GO TO 240
SIG=HU(I)
225 ZARG=UU*2.*LV*SIG*UVW*SIG**2.*VM*SIG**J*WV*SIG**4
C THESE STATEMENTS CHECK ZARG FOR ZERO AND NEGATIVE VALUES
C ZARG SHOULD BE POSITIVE, IF IT IS NOT IT IS COMPARED TO H(N).
C THE LENGTH OF ONE CABLE SEGMENT, IF IT IS SMALL BY COMPARISON, IT
C IS SET TO A SMALL POSITIVE VALUE
IF (ZARG.LI.(U.J.AND.ABS(ZARG/H(N)).LJ.0.0001) ZARG=ABS(ZARG)
IF (ZARG.EQ.0.) ZARG=0.000001*H(N)
DE=SUH(ZARG)
IF (DE.GT.DMAX) GO TO 235
230 IF (JTIME.LG.0) GO TO 240
GO TO 245
235 DMAX=DE
SDMAX=H(N)*(N-1)*SIG
GO TO 230
240 CONTINUE
JTIME=1
SIG=H(N)
GO TO 220
245 CONTINUE
C
C EXTREMA ALONG A CABLE NOW DETERMINED
C CALCULATE FINAL AND INITIAL COORDINATES OF MAXIMALLY DISPLACED POINTS
C
GO TO (290,250), JUM
250 KL=H(N)*MX
IF (SDMAX.LI.KL) GO TO 260
K=LJUNC(N)
DO 255 I=1,K
A(I)=FJUNC(I,K)
255 B(I)=FJUNC(I,K)
GO TO 285
260 DATA(2)=FEST(4)
DATA(3)=N
DATA(10)=SDMAX
J=J+1
UC 265 II=1*3
I=II
265 A(II)=SPACE(II)
DC 270 I=1*3
TEMP1(I)=HCAH(I,J,N)
TEMP2(I)=HCAH(I,J1,N)
TEMP3(I)=PCAB(I,J,N)
WCAB(I,J,N)=HCAH(I,J,N)
HCAH(I,J1,N)=HCAH(I,J1,N)
PCAB(I,J,N)=PCAB(I,J,N)
UC 275 II=1*3
I=II
275 H(II)=SPACE(II)
DC 280 I=1*3
HCAH(I,J,K)=TEMP1(II)
HCAH(I,J1,N)=TEMP2(II)
PCAB(I,J,N)=TEMP3(II)
280 PCAB(I,J,N)=TEMP3(II)
285 CONTINUE

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```

345 WRITE (IPRNT,600) N,IMAX,STMAX,IMIN,STMIN,DMAX,SDMAX,(A(I),I=1,3),STR 343
      1(B(I),I=1,3) STR 344
      GO TO 295 STR 345
350 WRITE (IPRNT,600) N,IMAX,STMAX,IMIN,STMIN STR 346
      295 CONTINUE STR 347
      C STR 348
      C STR 349
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      C STR 396
      C STR 397
      C STR 398
      C STR 399

345 WRITE (IPRNT,600) N,IMAX,STMAX,IMIN,STMIN,DMAX,SDMAX,(A(I),I=1,3),STR 343
      1(B(I),I=1,3) STR 344
      GO TO 295 STR 345
290 WRITE (IPRNT,600) N,IMAX,STMAX,IMIN,STMIN STR 346
295 CONTINUE STR 347
C STR 348
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C STR 396
C STR 397
C STR 398
C STR 399

345 WRITE (IPRNT,605)
      WRITE (IPRNT,610)
      IF (JUM.GT.1) GO TO 300
      WRITE (IPRNT,615)
      WRITE (IPRNT,620)
      GO TO 305
360 CONTINUE
      WRITE (IPRNT,625)
      WRITE (IPRNT,630)
365 CONTINUE
C THIS SECTION CALCULATES JUNCTION FORCES, LOCATIONS AND DISPLACEMENTS
C STR 362
C STR 363
C STR 364
IF=0
DO 395 J1=1,NJUNC
DO 310 K=1,NARC
      IF (ANJUNC(K).EQ.J1) GO TO 395
310 CONTINUE
      GO TO (325,315), JUM
315 DO 320 J2=1,J3
      DISP(J2)=PJUNC(J2,J1)-PJURIG(J2,J1)
      DISP(J2)=PJUNC(J2,J1)-PJUNC(J2,J1)
325 J6=1
      IF (NDATC.GT.1.OR.JUM.GT.1) GO TO 335
      DO 330 J2=1,J3
      PJURIG(J2,J1)=PJUNC(J2,J1)
335 CONTINUE
340 IF (J1.EQ.7)JUNC(J6) GO TO 360
345 IF (J1.EQ.7)JUNC(J6) GO TO 380
357 J6=J6+1
      IF (J6.IE.NCAR) GO TO 340
      IF (NIR.EQ.0) GO TO 395
      J7=1
355 IF (J1.EQ.7)JUNC(J7) GO TO 365
      J7=J7+1
      GO TO 355
360 M7=J6
      I=ICAR(1,M7)
      HX=RCAB(I,1,M7)
      HY=RCAB(I,2,M7)
      MZ=RCAB(I,3,M7)
      GO TO 395
365 IANEX=(MUNC(7)
      DO 370 J8=1,NCAR
      F (I,ANEX,EG,LJUNC(J8)) GO TO 375
370 CONTINUE
      M7=J8
      GO TO 385

```

```

400 300 NK=J5
401 385 MX=MODE (MH)
402 I=(CAR(MX,MK)
403 RX=RCAB(1,1,1,MM)
404 RY=RCAB(2,1,1,MM)
405 H7=RCAB(3,1,1,MM)
406 H7=RCAB(3,1,1,MM)
407 H7=RCAB(3,1,1,MM)
408 H7=RCAB(3,1,1,MM)
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453 H7=RCAB(3,1,1,MM)
454 H7=RCAB(3,1,1,MM)
455 H7=RCAB(3,1,1,MM)
456 H7=RCAB(3,1,1,MM)

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460      DO 425 I1=1,3
461      I=I1
462      PSPACE(I)=SPACE(I)
463      IF (NDATC.EG.1.AND.JUV.EG.1) SPACE(I,INDEX)=SPACE(I)
464      TEM2=IEN2*(RCAB(I,M,K)-RCAB(I,M,K)-SIGMA/M(K))*2
465      TEM=SUPT(TEM2)
466      GO TO (430,435), JUV
467      IF ((IPUNCH).EQ.8H YES).AND.(DATI(6).EQ.DEVNT)) WRITE (IPNCH,68)STR 457
468      10) INDEA,K,DATI(10),(PSPACE(I),I=1,3)
469      IF (DATI(5).EQ.0) WRITE (IPRNT,685) INDEX,K,DATI(10),TEN,(PSPACE(I)STR 458
470      1),I=1,3),DATI(6),DATI(9),DATI(7),IDOCAB(INDEX)
471      GO TO 455
472      DO 440 I=1,3
473      TEMPI(I)=RCAB(I,M,K)
474      TEMP2(I)=RCAB(I,M,K)
475      TEMP3(I)=PCAB(I,M,K)
476      RCAB(I,M,K)=RCABU(I,M,K)
477      RCAB(I,M+1,K)=RCABU(I,M+1,K)
478      PCAB(I,M,K)=PCABU(I,M,K)
479      I=I1
480      UISP(I)=PSPACE(I)-SPACE(I,INDEX)
481      DO 450 I=1,3
482      RCAB(I,M,K)=TEMPI(I)
483      RCAB(I,M+1,K)=TEMP2(I)
484      PCAB(I,M,K)=TEMP3(I)
485      IF ((IPUNCH).EQ.8H YES).AND.(DATI(6).EQ.DEVNT)) WRITE (IPNCH,68)STR 484
486      10) INDEA,K,DATI(10),(PSPACE(I),I=1,3)
487      IF (DATI(5).NE.0.) GO TO 455
488      WRITE (IPRNT,690) INDEX,K,DATI(10),TEN,(PSPACE(I),I=1,3),(DISP(I),STR 487
489      I=1,3),(UISPU(I),I=1,3)
490      CCONTINUE
491      HEMIND INIAPE
492      RETURN
493
494      *05 FORMAT (M1,8A10//,34H ARRAY EQUILIBRIUM WITH NC CURRENT//)
495      *70 FORMAT (B410/35H ARRAY EQUILIBRIUM WITH NO CURRENT )
496      *75 FORMAT (M1,8A10//,1X,8A10//)
497      *80 FORMAT (/,1X,39NUMBER OF ITERATIONS FOR CONVERGENCE = ,I5/)
498      *85 FORMAT (3PH ARRAY EQUILIBRIUM WITH CURRENT OPTION,I3//)
499      *90 FORMAT (8A10)
500      *95 FORMAT (38H ARRAY EQUILIBRIUM WITH CURRENT OPTION,I3)
501      *00 FORMAT (25H CURRENT FIELD OPTION IS ,I1)
502      *05 FORMAT (/,7X,12HZ-COORDINATE,6X,12HMAGNITUDE OF ,7X,12HDIRECTION OF,/STR 500
503      1,8X,10HCF CURRENT,7X,12PCURRENT AT 2,7X,12HCURRENT AT Z/4X,11HFRUSTR 502
504      2H N-AXIS//,10X,6HFEET//,11X,8B,10X,9H(DEGREES))
505      *10 FORMAT (7X,F10.2)10X,F8.3,10X,F8.3,11X,F8.3)
506      *15 FORMAT (/F10.1,24H PERCENT OF FULL CURRENT)
507      *20 FORMAT (/,1X,78H***CURRENT DIRECTION IS POSITIVE IN THE CLOCKWISE//)
508      *25 FORMAT (24H ARRAY EQUILIBRIUM WITH ,F8.2,15H DEGREE CURRENT,/,1X,4STR 508
509      10HARRAY EQUILIBRIUM WITH CURRENT DIRECTION,/F10.2,2X,42HDEGREES FRSTR 509
510      20H X-AXIS(= IS COUNTERCLOCKWISE)/F10.2,2X,35HDEGREES FROM N-AXIS(=STR 510
511      (IS CLOCKWISE)//)
512      *30 FORMAT (24H ARRAY EQUILIBRIUM WITH ,F8.2,15H DEGREE CURRENT)
513      *35 FORMAT (/,1X,26HLOCATION OF STRING NUMBER=,I1/1X,F8.0,1X,4HFEET,1XSTR 513

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STR 571-

END

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

47	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
194	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
212	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
219	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
270	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
312	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
369	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
463	I	AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1  *DECK SWITCH
2  SUBROUTINE SWITCH
3  C
4  C THIS ROUTINE SWITCHES INPUT DATA
5  C
6  COMMON /B3/ VELX(25),VELY(25)
7  COMMON /B1/ FEJUNC,IR,DELTA,DELTA,IRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,SWT
8  1PJUNCS,PCAB,PCAB,PCAB,PCAB,RCABO,RCABO,THETA,PJUNCO
9  COMMON /B2/ NCAB,NNODE,ERJUNC,IRJUNC,DATI,DATN,M,PJUNC,DCAB,DCAB,SWT
10 IFATE,NANG,ANJUNC,IHEAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THE,SWT
11 2TAS,THETA,CUMPD,THETA,B,NJUNC,RMO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,SWT
12 3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,W CAB,IDEV,ICHECK,NDEV,NDATC
13 DIMENSION FEJUNC(3,44), IR(3,44), IR5(3,44), IFJUNC(3,44), PJUNCO(SWT
14 13,44)
15 DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)SWT
16 1)
17 DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCAB(3,51,22)
18 DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DAT1(10), DATN(10), HSW
19 1(22)
20 DIMENSION PJUNC(3,44), DCAB(22), ANJUNC(44), TEST(14)
21 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
22 DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
23 DIMENSION ICHECK(44)
24 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
25 INTEGER PATH
26 REAL IR,IRS
27 DC 5 I=1,10
28 5 DAT1(I)=DATN(I)
29 RETURN
30 END

```

```

1  *DECK TANG
2  FUNCTION TANG (I)
3
4  C THIS ROUTINE CALCULATES THE UNIT TANGENT TO A CABLE AT ANY POINT
5  C
6  COMMON /B/ VELX(25),VELY(25)
7  COMMON /BI/ FEJUNC,IR,DELTA,IRSD,IRSF,IRJUNC,E,ES,FCAB,RCAB,JUMP,TAN
8  IPJUNC,PCAB,PCABE,PCABO,RCABO,THETA,PJUNCO
9  COMMON /BZ/ NCAB,NNODE,ERJUNC,IRJUNC,DATI,DATN,M,PJUNC,DCAB,DCAB,TAN
10 IFATE,NANC,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,OFFLG,NIR,THEI,TAN
11 ZIAS,THEIAE,COMP,THEIAB,NJUNC,RHQ,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,TAN
12 3EX,PCAB,ZJUNC,CJUNC,PATH,PCAB,IVOP,WCAB,IDEV,ICHECK,NDEV,NDATC
13 13,44)
14 DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), TFJUNC(3,44), PJUNCO(IAN
15 1)
16 DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNCS(3,44), PCAB(3,51,22)IAN
17 1)
18 DIMENSION PCABE(3,51,22), PCABO(3,51,22), RCABO(3,51,22)
19 DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DATI(10), DATN(10), HIAN
20 1(22)
21 DIMENSION PJUNC(3,44), CDCAB(22), DCAB(22), ANJUNC(44), TEST(14)
22 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXPCAB(22), ZJUNC(22)
23 DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(1000)
24 DIMENSION ICHECK(44)
25 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFFLG
26 INTEGER PATH
27 REAL IR,IRS
28 N=DATI(3)
29 M=IDATI(10)/H(N))+1
30
31 C CALCULATE DISTANCE, SIGMA, OF POINT FROM NODE M
32 C
33 SIGMA=DATI(10)-(M-1)*H(N)
34
35 C CALCULATE EXTRAPOLATION QUANTITIES
36 C
37 EM=RCAB(I,M,N)/TCAB(M,N)
38 EM1=RCAB(I,M+1,N)/TCAB(M+1,N)
39
40 C CALCULATE TANGENT
41 C
42 TANG=EM*((EM1-EM)/H(N))*SIGMA
43 RETURN
44 END

```

```

1  *DECK TAPOUT
2  SUBROUTINE TAPOUT
3
4  C THIS ROUTINE GENERATES THE TAPE OR CARDS GIVING
5  C THE LOCATIONS OF THE INDEXED DEVICES
6
7  COMMON /B3/ VELX(25),VELY(25)
8  COMMON /B1/ FEJUNC,IA,DELTA1,DELTA,IRS,TFJUNC,E,ES,FCAB,RCAB,JUMP,TAP
9  IPJUNCS,PCAB,PCABE,PCAB0,RCAB0,THETA,PJUNCO
10 COMMON /B2/ NCAB,NODE,ERJUNC,IRJUNC,DATI,DCAB(22),ANJUNC(44),TEST(14)
11 IFATE,NANC,ANJUNC,IREAD,IPRNT,INTAPE,OUTAPE,ITIME,IFLG,UFILG,NIR,THETA
12 ZTAS,THEIAC,COMPD,THETAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,TAP
13 3EXP,PCAB,LJUNC,PATH,ICAB,IVOP,WCAB,IDEV,ICHECK,NDEV,NDATC
14 DIMENSION FEJUNC(3+44), IR(3+44), IRS(3+44), TFJUNC(3+44), PJUNCO(TAP
15 13+44)
16 DIMENSION FCAB(3,51+22), RCAB(3,51+22), PJUNCS(3+44), PCAB(3,51+22)TAP
17 TAP
18 DIMENSION PCABE(3,51+22), PCAB0(3,51+22), RCAB0(3,51+22)
19 DIMENSION NNODE(22), ERJUNC(44), IRJUNC(44), DATI(10), DATN(10), HIAP
20 1(22)
21 DIMENSION PJUNC(3+44), CDCAB(22), DCAB(22), ANJUNC(44), TEST(14)
22 DIMENSION ZVEL(25), VELZ(25), ECICAB(22), EXP,PCAB(22), ZJUNC(22)
23 DIMENSION LJUNC(22), PATH(22), ICAB(22), WCAB(22), IDEV(100)
24 DIMENSION ICHECK(44)
25 DIMENSION PSPACE(3)
26 INTEGER OUTAPE,ZJUNC,ERJUNC,ANJUNC,OFLG
27 INTEGER PATH
28 REAL IR,IRS
29 ID1=4H CUR
30 ID2=4H DEV
31 ID3=4H REC
32 JUM=JUMP+1
33 GO TO (5+10), JUM
34 WRITE (OUTAPE,35) ID3,NDATC
35 WRITE (OUTAPE,35) ID1,JUMP
36 GO TO 15
37 WRITE (OUTAPE,35) ID1,JUMP,THETA
38 IF (NDEV.EQ.0) GO TO 30
39 DO 25 NK=1,NDEV
40 READ (INTAPE,40) (DATI(K),K=1,10)
41 INDEX=DATI(5)
42
43 C CALCULATE LOCATION OF DEVICE IN SPACE
44 C
45 DO 20 J=1,3
46 ISJ
47 PSPACE(I)=SPACE(I)
48 WRITE (OUTAPE,35) ID2,INDEX,(PSPACE(I),I=1,3)
49 25 CONTINUE
50 30 CONTINUE
51 RETURN
52
53 C
54 35 FORMAT (44,14,3F10.2)
55 40 FORMAT (F4.0,44,8E15.8)
56 END

```

PAGE 2

03/07/80 11.41.06

FTN 4.6.433E

74/74 OPT=1

SUBROUTINE TAPOUT

CARD NR. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

33 1 AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.


```

1  *DECK VELOC (1, PSPACE)
C  FUNCTION VELOC (1, PSPACE)
C  THIS ROUTINE SPECIFIES THE I COMPONENT OF THE CURRENT FIELD
C  AT AN ARBITRARY POINT IN SPACE, PSPACE(I)
C
COMMON /B3/ VELA(25),VELY(25)
COMMON /B1/ FEJUNC,IR,DELTAI,DELTA,IRS,IFJUNC,E,ES,FCAB,RCAB,JUMP,VEL
IPJUNC,PCAB,PCAB,PCAB,PCAB,HCAB,THETA,PJUNCO
COMMON /B2/ NCAB,NODE,ERJUNC,IRJUNC,DATAI,DATA,M,PJUNC,DCAB,DCAB,VEL
IFATE,NANC,ANJUNC,IHEAD,IPRNI,INTAPE,OUTAPE,ITIME,IFLG,OFLG,NIR,THEVEL
2IAS,THETA,COMPDS,THETA,NCAB,NJUNC,RHO,TEST,NVSEG,ZVEL,VELZ,PIP,ECICAB,VEL
3EXPCAB,ZJUNC,LJUNC,PATH,ICAB,IVOPT,WCAB,IDEV,ICHECK,NDEV,NDATC
COMMON /PIBLK/ PI
COMMON /KITER/ KOUNT,IR,NI,MMITER,NSTEPS,ISTEP,PERCNTY,INCRPT
DIMENSION FEJUNC(3,44), IR(3,44), IRS(3,44), IFJUNC(3,44), PJUNCO(VEL
13,44)
DIMENSION FCAB(3,51,22), RCAB(3,51,22), PJUNCS(3,51,22)
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03/07/80 11.41.06

F IN 4.6.433E

OPT=1

74/74

FUNCTION VELOC

VEL 58
VEL 59
VEL 60
VEL 61
VEL 62
VEL 63-

RETURN
35 VELOC=V*(G*SIN(A)*PERCENT)
RETURN
40 VELOC=0
RETURN
END

60

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

34 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.
56 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

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1      *DELK MEDVEL
2      SUBROUTINE RECVEL (IR,IM)
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1  *DECK INTVEL
2  SUBROUTINE INTVEL (NW, PSPACE)
3  COMMON /CVEL/ VMAG(25,4), VDIR(25,4), ZPT(25,4), XPI(4), YPI(4), NPPTS(4)
4  IJ=NSTA
5  COMMON /CLE1/ X,Y,DUMVY(9),VDR(4),VMG(4)
6  COMMON /PIBLK/ PI
7  DIMENSION NP(3), FSPACE(3)
8  DIMENSION V1(4), V2(4)
9  STAT(Y1,Y2)=Y1*(Y2-Y1)**H
10 X=PSPACE(1)
11 Y=PSPACE(2)
12 Z=PSPACE(3)
13 DC 20 J=1,NSTA
14 NP=NPPTS(J)
15 DO 5 I=1,NP
16 ZDIF=Z-ZPT(I,J)
17 IF (ZDIF.GT.0.) GO TO 5
18 I2=1
19 I1=I-1
20 GO TO 10
21 5 CONTINUE
22 10 IF (I1.EQ.0) GO TO 15
23 10 IF (I1.EQ.0) GO TO 15
24 VMG(J)=STAT(VMAG(I1,J),VMAG(I2,J))
25 VDR(J)=STAT(VDIR(I1,J),VDIR(I2,J))
26 GO TO 20
27 15 VMG(J)=VMAG(I2,J)
28 VDR(J)=VDIR(I2,J)
29 20 CONTINUE
30 NSENSTA=1
31 GO TO (25,45,50), NS
32 X1=XPI(1)
33 Y1=YPI(1)
34 X2=XPI(2)
35 Y2=YPI(2)
36 IF (X1-X2.NF.0.) GO TO 30
37 X3=X1
38 Y3=Y1
39 GO TO 40
40 IF (Y1-Y2.NE.0.) GO TO 35
41 X3=X1
42 Y3=Y1
43 GO TO 40
44 35 SP1=(Y2-Y1)/(X2-X1)
45 SP2=(Y2-Y1)/(X2-X1)
46 SP2=-1./SP1
47 I0=SM2-SM1
48 X3=(Y1-SP1*X1)-(Y-SM2*X1)/US
49 Y3=(X1-SP2*Y1)+(X-SM1*Y)/US
50 S1=SDMT((X2-X1)**2+(Y2-Y1)**2)
51 S2=SDRT((X3-X1)**2+(Y3-Y1)**2)
52 SCS=52/S1
53 V1(1)=S0S*(VMG(2)-VMG(1))+VMG(1)
54 V2(1)=S0S*(VDR(2)-VDR(1))+VDR(1)
55 GO TO 55
56 45 CALL SCT (I)
57 CALL CRAMEH (V1(1))

```

```

60      CALL SET (2)
        CALL CRAMER (V2(1))
        GO TO 55
50      CALL SET (1)
        CALL CRAMER (V1(1))
        CALL SET (2)
        CALL CRAMER (V2(1))
        CALL SET (3)
        CALL CRAMER (V2(2))
        CALL SET (4)
        CALL CRAMER (V1(2))
        CALL SET (5)
        CALL CRAMER (V1(3))
        CALL SET (6)
        CALL CRAMER (V2(3))
        CALL SET (7)
        CALL CRAMER (V2(4))
        CALL SET (8)
        CALL CRAMER (V1(4))
        V1(1)=-.25*(V1(1)+V1(2)+V1(3)+V1(4))
        V2(1)=-.25*(V2(1)+V2(2)+V2(3)+V2(4))
55      DTR=PI/180.
        TRT=V2(1)*DTR
        W1(1)=V1(1)*COS(TRT)+1.688
        W1(2)=V1(1)*SIN(TRT)+1.688
        W1(3)=0.0
        RETURN
        END

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INT 58
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INT 84
INT 85-

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CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

31 I AN IF STATEMENT MAY BE MORE EFFICIENT THAN A 2 OR 3 BRANCH COMPUTED GO TO STATEMENT.

```

1      *CHECK SET
2      SUBROUTINE SET (I)
3      COMMON /LEVEL/ VMAG(25,4),VDIR(25,4),ZPT(25,4),XPT(4),YPT(4),NPPS(4)
4      SET 4
5      1),NSTA
6      COMP/4 /CLET/ X,Y,X1,X2,X3,Y1,Y2,Y3,Z1,Z2,Z3,VDR(4),VMG(4)
7      GO TO (5,10,15,20,25,30,35,40), I
8
9      5 CONTINUE
10     X1=XPT(1)
11     X2=XPT(2)
12     X3=XPT(3)
13     Y1=YPT(1)
14     Y2=YPT(2)
15     Y3=YPT(3)
16     Z1=VMG(1)
17     Z2=VMG(2)
18     Z3=VMG(3)
19     RETURN
20
21     10 CONTINUE
22     Z1=VDR(1)
23     Z2=VDR(2)
24     Z3=VDR(3)
25     RETURN
26
27     15 CONTINUE
28     X3=XPT(4)
29     Y3=YPT(4)
30     Z3=VDR(4)
31     RETURN
32
33     20 CONTINUE
34     Z1=VMG(1)
35     Z2=VMG(2)
36     Z3=VMG(3)
37     RETURN
38
39     25 CONTINUE
40     X1=XPT(3)
41     Y1=YPT(3)
42     Z1=VMG(3)
43     RETURN
44
45     30 CONTINUE
46     Z1=VDR(3)
47     Z2=VDR(2)
48     Z3=VDR(4)
49     RETURN
50
51     35 CONTINUE
52     X2=XPT(1)
53     Y2=YPT(1)
54     Z2=VDR(1)
55     RETURN
56
57     40 CONTINUE
58     Z1=VMG(3)
59     Z2=VMG(1)
60     Z3=VMG(4)
61     RETURN
62
63     45
64     50
65     53-

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```

1  *DECK CRAMEX
2  SUBROUTINE CRAMEX (ANS)
3  COMMON /CLEI/ X1,X2,X3,Y1,Y2,Y3,Z1,Z2,Z3,VDM(4),VMG(4)
4  U=X1*(Y2*Z3-Y3*Z2)-Y1*(X2*Z3-X3*Z2)+Z1*(X2*Y3-Y2*X3)
5  AN=- (Y2*Z3-Y3*Z2)-Y1*(Z2-Z3)-Z1*(Y3-Y2)
6  HA=X1*(Z2-Z3)+X2*Z3-X3*Z2)+Z1*(X3-X2)
7  CN=X1*(Y3-Y2)-Y1*(X3-X2)-(X2*Y3-Y2*X3)
8  IF (U.NE.0) GO TO 5
9  AN.S=(AN*X+BN*Y)/CN
10 RETURN
11 5  A=AN/I
12  H=HN/I
13  C=CN/I
14  ANS=(1./C)*(1.+A*X+B*Y)
15 RETURN
16 EN)

```

CRA 1
CRA 2
CRA 3
CRA 4
CRA 5
CRA 6
CHA 7
CHA 8
CHA 9
CRA 10
CRA 11
CRA 12
CHA 13
CRA 14
CRA 15
CRA 16-

C SORT BY UNSTRESSED DISTANCE FORM S=0 JUNCTION UF CABLE

```

60      DO 65 I=1,NCCAB1
           K=I+1
           55 IF (UATII(I,3).NE.OATII(K,3)) GO TO 65
           IF (UATII(I,10).LE.OATII(K,10)) GO TO 63
           CALL SWAP (I,K)
           65 K=K+1
           IF (K.GT.NDCAB) GO TO 65
           GO TO 55
65      CONTINUE
           RETURN
70      C      70 FORMAT (F4.0,A4,BF8.0)
           END

```

```

SOR 58
SOR 59
SOR 60
SOR 61
SOR 62
SOR 63
SOR 64
SOR 65
SOR 66
SOR 67
SOR 68
SOR 69
SOR 70
SOR 71
SOR 72-

```

```

1      *LECK SWAP
2      SUBROUTINE SWAP (I,K)
3      COMMON /BI/ FEJUNC
4      COMMON /TANCHG/ TCCAB(22),TDDCAB(1000)
5      DIMENSION DATI(2150,10), TDATA(10), FEJUNC(3*44)
6      EQUIVALENCE (DATI(1),FEJUNC(1))
7      DC 5 J=1,10
8      TDATA(J)=DATI(I,J)
9      DATI(I,J)=TDATA(J)
10     DATI(K,J)=TDATA(J)
11     TEMP=TDDCAB(I)
12     TDDCAB(I)=TDDCAB(K)
13     TDDCAB(K)=TEMP
14     RETURN
15     END

```

SWA 1
SWA 2
SWA 3
SWA 4
SWA 5
SWA 6
SWA 7
SWA 8
SWA 9
SWA 10
SWA 11
SWA 12
SWA 13
SWA 14
SWA 15-


```

WRITE (IPRNT,360) TITLE
GC TO 10
C
C HEAD AND PRINT ERROR TYPES AND OTHER INFORMATION
C
25 WRITE (IPRNT,375) TYPE (IBAD)
GC TO 10
30 READ (ISCR) IFJNC,IFRHO,NANC
WRITE (IPRNT,375) TYPE (IBAD),IFJNC,IFRHO,NANC
GC TO 10
35 READ (ISCR) NCOMP,IVOP1,NVSEG,NZL,NANG
WRITE (IPRNT,375) TYPE (IBAD),NCOMP,IVOP1,NVSEG,NZL,NANG
GC TO 10
40 READ (ISCR) (ICAB(I),I=1,22)
WRITE (IPRNT,380) TYPE (IBAD), (ICAB(I),I=1,22)
GC TO 10
45 READ (ISCR) (ICHECK(I),I=1,44)
WRITE (IPRNT,380) TYPE (IBAD), (ICHECK(I),I=1,44)
GC TO 10
50 READ (ISCR) NCAB,NANC,NOJUNC,NIRC,NIR
WRITE (IPRNT,375) TYPE (IBAD),NCAB,NANC,NOJUNC,NIRC,NIR
GC TO 10

```

PRINT TEXT OF ERRORS

```

55 WRITE (IPRNT,370)
DC 350 1=1,NER
IF (IERR(I).EQ.0) GO TO 350
WRITE (IPRNT,385) TYPE (I)SCARD(I)
GC TO 10
1,145,150,155,160,165,170,175,180,185,190,195,200,205,210,215,220,225,230,235,240,245,250,255,260,265,270,275,280,285,290,295,300,305,310,315,320,325,330,335,340,345). 1
60 WRITE (IPRNT,390)
GC TO 350
65 WRITE (IPRNT,395)
GC TO 350
70 WRITE (IPRNT,400)
GC TO 350
75 WRITE (IPRNT,405)
GC TO 350
80 WRITE (IPRNT,410)
GC TO 350
85 WRITE (IPRNT,415)
GC TO 350
90 WRITE (IPRNT,420)
GC TO 350
95 WRITE (IPRNT,425)
GC TO 350
100 WRITE (IPRNT,430)
GC TO 350
105 WRITE (IPRNT,435)
GC TO 350
110 WRITE (IPRNT,440)
GC TO 350
115 WRITE (IPRNT,445)
GC TO 350

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BAD 58
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115	120	WRITE (IPRNT,450)	BAD 115
	GC TO 350		BAD 116
	125	WRITE (IPRNT,455)	BAD 117
	GC TO 350		BAD 118
	130	WRITE (IPRNT,460)	BAD 119
	GC TO 350		BAD 120
	135	WRITE (IPRNT,465)	BAD 121
	GC TO 350		BAD 122
	140	WRITE (IPRNT,470)	BAD 123
	GC TO 350		BAD 124
	145	WRITE (IPRNT,475)	BAD 125
	GC TO 350		BAD 126
	150	WRITE (IPRNT,480)	BAD 127
	GC TO 350		BAD 128
	155	WRITE (IPRNT,485)	BAD 129
	GC TO 350		BAD 130
	160	WRITE (IPRNT,490)	BAD 131
	GC TO 350		BAD 132
	165	WRITE (IPRNT,495)	BAD 133
	GC TO 350		BAD 134
	170	WRITE (IPRNT,500)	BAD 135
	GC TO 350		BAD 136
	175	WRITE (IPRNT,505)	BAD 137
	GC TO 350		BAD 138
	180	WRITE (IPRNT,510)	BAD 139
	GC TO 350		BAD 140
	185	WRITE (IPRNT,515)	BAD 141
	GC TO 350		BAD 142
	190	WRITE (IPRNT,520)	BAD 143
	GC TO 350		BAD 144
	195	WRITE (IPRNT,525)	BAD 145
	GC TO 350		BAD 146
	200	WRITE (IPRNT,530)	BAD 147
	GC TO 350		BAD 148
	205	WRITE (IPRNT,535)	BAD 149
	GC TO 350		BAD 150
	210	WRITE (IPRNT,540)	BAD 151
	GC TO 350		BAD 152
	215	WRITE (IPRNT,545)	BAD 153
	GC TO 350		BAD 154
	220	WRITE (IPRNT,550)	BAD 155
	GC TO 350		BAD 156
	225	WRITE (IPRNT,555)	BAD 157
	GC TO 350		BAD 158
	230	WRITE (IPRNT,560)	BAD 159
	GC TO 350		BAD 160
	235	WRITE (IPRNT,565)	BAD 161
	GC TO 350		BAD 162
	240	WRITE (IPRNT,570)	BAD 163
	GC TO 350		BAD 164
	245	WRITE (IPRNT,575)	BAD 165
	GC TO 350		BAD 166
	250	WRITE (IPRNT,580)	BAD 167
	GC TO 350		BAD 168
	255	WRITE (IPRNT,585)	BAD 169
	GC TO 350		BAD 170
	260	WRITE (IPRNT,590)	BAD 171

420 FORMAT (5X,17#FIELD 3 = FIELD 4)
 425 FORMAT (5X,4#FIELD 3 OR 4 GREATER THAN 44 OR LESS THAN 1)
 430 FORMAT (5X,3#FIELD 3 GREATER THAN 22 OR LESS THAN 1)
 435 FORMAT (5X,17#FIELD 4 = FIELD 5)
 440 FORMAT (5X,4#FIELD 4 OR 5 GREATER THAN 44 OR LESS THAN 1)
 445 FORMAT (5X,3#FIELD 7*8 OR 9 LESS THAN OR EQUAL TO 0)
 450 FORMAT (5X,2#FIELD 10 OR 11 LESS THAN 0)
 455 FORMAT (5X,3#FIELD 10*0 AND FIELD 11 NOT EQUAL 0)
 460 FORMAT (5X,3#FIELD 10 NOT EQUAL 0 AND FIELD 11=0)
 465 FORMAT (5X,3#FIELD 12 GREATER THAN 50 OR LESS THAN 1)
 470 FORMAT (5X,3#FIELD 3 GREATER THAN 22 OR LESS THAN 1)
 475 FORMAT (5X,3#FIELD 4 GREATER THAN 2 OR LESS THAN 1)
 480 FORMAT (5X,4#FIELD 5 GREATER THAN 1000 OR LESS THAN 1)
 485 FORMAT (5X,4#FIELD 4*1 AND FIELD 9 LESS THAN OR EQUAL TO 0)
 490 FORMAT (5X,3#FIELD 4*2 AND FIELD 9 NOT EQUAL 0)
 495 FORMAT (5X,2#FIELD 7*8 OR 10 LESS THAN 0)
 500 FORMAT (5X,3#FIELD 3 GREATER THAN 44 OR LESS THAN 1)
 505 FORMAT (5X,2#FIELD 7 OR 8 LESS THAN 0)
 510 FORMAT (5X,19#FIELD 3 LESS THAN 0)
 515 FORMAT (5X,27#FIELD 3 NOT EQUAL 0,1, OR 2)
 520 FORMAT (5X,28#FIELD 3 LESS THAN OR EQUAL 0)
 525 FORMAT (5X,28#FIELD 4 LESS THAN OR EQUAL 0)
 530 FORMAT (5X,25#FIELD 5 LESS THAN FIELD 3)
 535 FORMAT (5X,7#THE JUNCTION NUMBER ASSIGNED TO THE ANCHOR(FIELD 3) BAD 251
 HAS BEEN ASSIGNED TO A PRECEDING ANC CARD OR/5A,52HTO AN S=L JUNCTBAD 253
 2ION (FIELD 5) ON A PRECEDING CAB CARD)
 540 FORMAT (5X,15#THE JUNCTION NUMBER ASSIGNED TO THE S=L JUNCTION (F)BAD 254
 FIELD 5) HAS BEEN ASSIGNED ON A PRECEDING CAB CARD OR/5X,55SHTO AN BAD 255
 ANCHOR JUNCTION (FIELD 3) ON A PRECEDING ANC CARD)
 545 FORMAT (5X,8#A TYPE 3 ERROR APPEARS ONLY IN CONJUNCTION WITH A CABAD 258
 IN CARD AND INDICATES THAT THE /5X,60#NUMBER ASSIGNED TO THE CABLE BAD 259
 2(FIELD 3) HAS BEEN ASSIGNED ON A PRECEDING CAB CARD)
 550 FORMAT (5X,9#THE JUNCTION NUMBER ASSIGNED IN FIELD 3 HAS BEEN ASSBAD 260
 IIGNED IN FIELDS 3 OR 4 OF A PRECEDING IR CARD)
 555 FORMAT (5X,3#THE JUNCTION NUMBER ASSIGNED IN FIELD 4 HAS BEEN ASSBAD 263
 IIGNED IN FIELD 3 OF A PRECEDING IR CARD)
 560 FORMAT (5X,20#AN NJNC CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARBAD 265
 IAR SOURCE DECK)
 565 FORMAT (5X,4#A DEN CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 267
 I SOURCE DECK)
 570 FORMAT (5X,65#A COMP CARD HAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 269
 IR SOURCE DECK)
 575 FORMAT (5X,77# TWENTY FIVE VEL CARDS HAVE PREVIOUSLY APPEARED IN THHAD 271
 LE PARTICULAR SOURCE DECK)
 580 FORMAT (5X,74#THE Z COORDINATE AT WHICH THE CURRENT VELOCITY IS SPRAD 273
 ECIFIED (FIELD 3) HAS /5X,63#BEEN USED ON A PRECEDING VEL CARD IN HAD 274
 THE PARTICULAR SOURCE DECK)
 585 FORMAT (5X,65#AN ANG CARD WAS PREVIOUSLY APPEARED IN THE PARTICULARHAD 275
 IR SOURCE DECK)
 590 FORMAT (5X,11#A TYPE 7 ERROR INDICATES AN INADEQUACY OF INFORMATIONHAD 278
 ON IN THE CABLE ARRAY SOURCE DECK(OR TAPE). THE OTHER INFORMATION/BAD 279
 25X,11#HOLDING UNDER THE ERROR HEADING CONTAINS A 1X3 MATRIX, THE BAD 280
 ELEMENTS OF WHICH GIVE RESPECTIVELY THE NUMBER OF NJNC CARDS/5X,12#HAD 281
 #HEAD, THE NUMBER OF DEN CARDS READ, AND THE NUMBER OF ANC CARDS BAD 282
 READ. A ZERO ELEMENT IS AN ERROR(SEE CABLE ARRAY SOURCE DECK)) BAD 283
 595 FORMAT (5X,11#A TYPE 8 ERROR INDICATES A DISCONTINUITY IN NUMBERSHAD 284
 IN THE CABLES IN THE AREA). THE OTHER INFORMATION COLUMN UNDER /5X#HAD 285

230 BAD 229
 235 BAD 230
 240 BAD 231
 245 BAD 232
 250 BAD 233
 255 BAD 234
 260 BAD 235
 265 BAD 236
 270 BAD 237
 275 BAD 238
 280 BAD 239
 285 BAD 240
 290 BAD 241
 295 BAD 242
 300 BAD 243
 305 BAD 244
 310 BAD 245
 315 BAD 246
 320 BAD 247
 325 BAD 248
 330 BAD 249
 335 BAD 250
 340 BAD 251
 345 BAD 252
 350 BAD 253
 355 BAD 254
 360 BAD 255
 365 BAD 256
 370 BAD 257
 375 BAD 258
 380 BAD 259
 385 BAD 260
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 395 BAD 262
 400 BAD 263
 405 BAD 264
 410 BAD 265
 415 BAD 266
 420 BAD 267
 425 BAD 268
 430 BAD 269
 435 BAD 270
 440 BAD 271
 445 BAD 272
 450 BAD 273
 455 BAD 274
 460 BAD 275
 465 BAD 276
 470 BAD 277
 475 BAD 278
 480 BAD 279
 485 BAD 280
 490 BAD 281
 495 BAD 282
 500 BAD 283
 505 BAD 284
 510 BAD 285

290 600 FORMAT (5X,11) THE ERROR INDICATES A DISCONTINUITY IN NUMBER HEAD 290
 291 THE JUNCTIONS IN THE ARRAY. THE OTHER INFORMATION COLUMN /5X,12) HEAD 291
 292 UNDER THE ERROR HEADING CONTAINS A 1 X 4 MATRIX, THE ELEMENTS OF WHICH 292
 293 WHICH CONTAIN ONE OR ZERO INDICATING RESPECTIVELY, THE USE OF /5X,13) HEAD 293
 294 OR NON-USE OF THE CORRESPONDING COLUMN NUMBER AS A JUNCTION NUMBER 294
 295 DER. ZEROS INTERFERED WITH ONES ARE IN ERROR (SEE ARRAY DESCRIPTION) 295
 296 DESCRIPTION AND REDUCTION TO A STATICALLY DETERMINATE ARRAY.) 296
 297 605 FORMAT (5X,11) THE ERROR INDICATES AN IMPROPER REDUCTION OF BAD 297
 298 THE ORIGINAL CABLE ARRAY TO A STATICALLY DETERMINATE ARRAY OR AN 298
 299 25X,12) ABSENCE OF CERTAIN INPUT CARDS IN THE CABLE ARRAY SOURCE DEBAD 299
 300 (FOR TAPE). THE OTHER INFORMATION COLUMN UNDER THE ERROR HEADING/BAD 300
 301 45X,12) CONTAINS A 1 X 5 MATRIX, THE ELEMENTS OF WHICH GIVE, RESPECTIVELY, 301
 302 THE NUMBER OF CAR CARDS READ, THE NUMBER OF ANC CARDS /5X) HEAD 302
 303 612) HEAD, THE NUMBER OF JUNCTIONS IN THE ORIGINAL CABLE ARRAY (FIELD 303
 304 7) OF THE NUNC CARD), THE NUMBER OF REQUIRED CUTS (EQ.(11))/5X,11) HEAD 304
 305 5) CALCULATED FROM THE PRECEDING INFORMATION, AND THE NUMBER OF IR 305
 306 SCARDS READ. COLUMN 5 NOT EQUAL TO COLUMN 4 IS AN ERROR /5X,50) (SEE HEAD 306
 307 3) REDUCTION TO A STATICALLY DETERMINATE ARRAY.) 307
 308 610 FORMAT (5X,10) THE JUNCTION NUMBER ASSIGNED IN FIELD 3 IS LESS THAN 308
 309 IR, OR EQUAL TO THE NUMBER OF JUNCTIONS IN THE ORIGINAL /5X,43) (UNREDBAD 309
 310 2) ARRAY (FIELD 3 OF THE NUNC CARD)) 310
 311 615 FORMAT (5X,11) THE JUNCTION NUMBER ASSIGNED IN FIELD 3 IS GREATER 311
 312 THAN THE NUMBER OF JUNCTIONS IN THE ORIGINAL (UNREDBAD) ARRAY /5X,43) 312
 313 25) PLUS THE NUMBER OF CUTS MADE IN REDUCING THE ARRAY (EQ.(11)) 313
 314 620 FORMAT (5X,11) THE JUNCTION NUMBER ASSIGNED IN FIELD 4 IS GREATER 314
 315 THAN THE NUMBER OF JUNCTIONS IN THE ORIGINAL (UNREDBAD) ARRAY 315
 316 625 FORMAT (5X,10) THE JUNCTION NUMBER ASSIGNED IN FIELD 4 IS GREATER 316
 317 THAN THE NUMBER OF JUNCTIONS IN THE ORIGINAL (UNREDBAD) ARRAY /5X,43) 317
 318 2) (FIELD 3 OF THE NUNC CARD) PLUS THE NUMBER OF CUTS MADE IN REDU 318
 319 3) THE ARRAY (EQ.(11)) 319
 320 630 FORMAT (5X,12) THE CABLE NUMBER ASSIGNED IN FIELD 3 DOES NOT CORRE 320
 321 1) SPOND TO A CABLE NUMBER ASSIGNED TO A CABLE (FIELD 3 OF THE CAR 321
 322 2) HEAD) 322
 323 635 FORMAT (5X,11) THE DISTANCE OF THE DISCRETE DEVICE FROM THE 500 323
 324 JUNCTION OF THE CABLE (FIELD 10) IS GREATER THAN OR EQUAL TO /5X,63) 324
 325 2) THE LENGTH OF THE CORRESPONDING CABLE (FIELD 9 OF THE CAR CARD)) 325
 326 640 FORMAT (5X,11) THE JUNCTION NUMBER ASSIGNED IN FIELD 3 DOES NOT 326
 327 RESPOND TO EITHER A JUNCTION NUMBER ASSIGNED TO AN ANCHOR /5X,11) 327
 328 4) (FIELD 3 OF THE ANC CARD) OR A JUNCTION NUMBER ASSIGNED TO AN 328
 329 3) JUNCTION OF A CABLE (FIELD 2 OF THE CAR CARDS)) 329
 330 645 FORMAT (5X,10) THE TYPE 13 ERROR INDICATES THAT THE ORIGINAL CABLE 330
 331 ARRAY HAS NOT BEEN PROPERLY REDUCED TO A STATICALLY /5X,10) (DETERM 331
 332 2) STATE ARRAY OR THAT JUNCTIONS HAVE BEEN IMPROPERLY NUMBERED. CHECK 332
 333 3) THE INFORMATION COLUMN UNDER /5X,10) THE ERROR HEADING CONTAINS THE 333
 334 4) MESSAGE, THE NUMBER OF JUNCTIONS OR JUNCTION NUMBERING. CHECK 334
 335 5) THE MESSAGE AGAINST JUNCTION NUMBERING OR ANCHOR (ANC CARDS)) 335
 336 650 FORMAT (5X,11) THE TYPE 14 ERROR INDICATES AN INADEQUACY OF 336
 337 1) JUNCTION IN A PARAMETRIC STUDY SOURCE DECS. THE OTHER INFORMATION /5X,11) 337
 338 2) COLUMN UNDER THE ERROR HEADING CONTAINS A 1 X 5 MATRIX, THE 338
 339 3) ELEMENTS OF WHICH GIVE, RESPECTIVELY, THE NUMBER OF COMP CARDS /5X,12) 339
 340 4) HEAD, THE CORRECT FIELD COLUMNS, THE NUMBER OF VIL CARDS HEAD, 340
 341 5) NUMBER OF VIL CARDS CONTAINED IN A /5X,11) (FIELD 3) /5X,11) 341
 342

- 345 655 THAN OR EQUAL TO THE MINIMUM Z COORDINATE TRANSMITTED BY THE ANBAD 343
- 7C CARDS (FIELD 6 OF THE ANG CARDS), AND THE /5X,25PNUMBER OF ANG CARDS 344
- EMDS HEAD, /5X,12SMIF COLUMN 1 CONTAINS A ZERO, THEN A COMP CARL HASBAD 345
- 9 NOT APPEARED AFTER THE FIRST READ (AND USE PARAMETRIC STUDY SOURCEBAD 346
- XCE DECK).)
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1      *CHECK CPLT
2      SUBROUTINE CPLT (I,OPT,IPRNT,IPJUNC,NANC,TITLE,ANJUNC)
3      COMMON /CPLT/ ZUP,ZDN,ZL,ZR,XMIN,XMAX,YMIN,YMAX,YIN,PANG,INY
4      COMMON /PIBLK/ PI
5      DIMENSION KJUNC(3,44), ANJUNC(44)
6      DIMENSION X(100), Y(100)
7      DIMENSION PSPACE(3), W*(3), TITLE(8)
8      INTEGER ANJUNC
9
10     C SET UP PERSPECTIVE TRANSFORMATIONS
11     C
12     UP(XP,YP)=XF+YP*EX
13     VP(YP)=YP*EY
14
15     C INITIALIZATION
16     C
17     DTH=PI/180.
18     EX=COS(ANG*DTR)
19     EY=SIN(ANG*DTR)
20     HGT=0.07
21
22     C CALCULATE SPACE BETWEEN PLOTS
23     C
24     NZ=(ZUP-ZDN)/DZ+1.00001
25     PIN=VP(YIN)
26     IY=NZ*PIN
27     SPACE=(10.-(YI)/(NZ+1))
28     IF (SPACE.GT.0.) GO TO 5
29     WRITE (IPRNT,75)
30     RETURN
31
32     C 5 CONTINUE
33
34     C GET COORDINATES
35     C
36     NYI=NY-1
37     DELI=YIN/NYI
38     DELU=(YMAX-YMIN)/NYI
39     NX=(XMAX-XMIN)/DELU+2.00000
40     IF (NX.GE.3) GO TO 10
41     WRITE (IPRNT,80)
42     RETURN
43
44     C 10 NXI=NX-1
45     XI=DELI*NXI
46     DC 15 I=1,NX
47     X(I)=XMIN+(I-1)*DELU
48     DC 20 J=1,NY
49     Y(I)=YMIN+(I-1)*DELU
50
51     C DEFINE SCALE IN UNITS PER INCH
52     C
53     SCALE=DELU/DELI
54
55     C FIND NORMALIZATION FACTOR FOR CURRENT
56     C
57     SMAA=0.
58     DC 40 K=1,NZ
59     PSPACE(3)=ZLN*(K-1)*UZ

```

75 FORMAT (2F3.3,7F10.3) 80 FORMAT (4F4.0,10F10.3)

MAP 228

```

60      C      LOOP ON X AND Y
        C      DC 35 I=2,NX1
        C      DC 35 J=2,NY1
        C      PSPACE(1)=X(I)
        C      PSPACE(2)=Y(J)
65      IF (I.VOIT.NE.3) GO TO 25
        CALL INTVEL (NWP,PSPACE)
        XA=WM(1)
        YA=WM(2)
        GC TO 70
70      25 XA=VELOC(1),PSPACE)
        YA=VELOC(2),PSPACE)
        30 S=SQRT(XA**2+YA**2)
        35 SPAX=AMAX1(S,MAX,S)
        40 CONTINUE
        SD=0.50*DELI/SMAX
75      C      INITIALIZE AND SET PEN POSITION
        C      YC=SPACE
        C      CALL PLOT (0.,Y0,-3)
        C      DC 70 K=1,NZ
80      C      LOOP ON DEPTH LEVELS
        C      PSPACE(3)=ZDN+(K-1)*DZ
85      C      LABEL DEPTH LEVEL AND INDICATE X-AXIS
        C      IF (K.EQ.1) GC TO 45
        C      YC=PIN+SPACE
        C      CALL PLOT (C.0,Y0,-3)
90      C      DRAW B07
        C
95      45 CALL PLOT (0.,0.,3)
        C      PX=UP(0.,YIN)
        C      PY=VP(YIN)
        C      CALL PLOT (PX,PY,2)
        C      PX=UP(XIN,YIN)
        C      CALL PLOT (PX,PY,2)
        C      CALL PLOT (XIN,0.,2)
        C      CALL PLOT (0.,0.,2)
        C      XR=0.5*(XIN+PX)+0.25
        C      YR=0.5*(PY+PGT)
        C      CALL NUMBER (XIN,YN,PGT,PSPACE(3),0.,0.)
        C      CALL SYMBOL (XIN,.25,PGT,IMX,0.,1)
        C      CALL SYMBOL (-.25,0.,PGT,IMX,0.,1)
100      C      PLOT SYMBOL AT EACH ANCHOR POINT
        C      DC 50 H=1,NHIC
        C      F=NHJUN(C,1)
        C      XAN=(FJUN(C,1)+L)-AMIN)/SCALE
        C      YAN=(FJUN(C,1)+YIN)/SCALE
        C      PY=ONE (XAP,YAN)
110

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CPL 58
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CPL 110
CPL 111
CPL 112
CPL 113
CPL 114

CPL 172
CPL 173
CPL 174
CPL 175
CPL 176
CPL 177
CPL 178
CPL 179-

CALL PLOT (X0,Y0,-3)
RETURN

C

75 FCRMA1 (////IX,57H)TOTAL HEIGHT OF PLOT EXCEEDS 10. INCHES, PLOT NOCPL 175
IF (CREATED////)
80 FCRMA1 (////IX,8RH)THE NUMBER OF GRID POINTS IN THE X DIRECTION IS LCPL 177
LESS THAN 3, TO CORRECT THIS INCREASE NY////)
END

```

1  *CHECK PERPLT
2  SUBROUTINE PERPLT (IPOP1,NCAR,NNODE,PCAB,PCAB0,TITLE)
3  DIMENSION M(12),NPAR(14),X(2200),Y(2200),Z(2200),TITLE(8)
4  DIMENSION PCAB(3,51,22),PCAB0(3,51,22),ANODE(22)
5  COMMON /PLT1/ KPLI,SIZE,TH(3),IPOP1,KCPLI
6  DATA MDC/M ,6H ,6H ,6H ,6H ,6H /
7
8  IPOP1=0 ,6H ,6H ,6H /
9  IPOP1=1 ,6H ,6H ,6H /
10 IPOP1=2 ,6H ,6H ,6H /
11 IPOP1=3 ,6H ,6H ,6H /
12 IPOP1=4 ,6H ,6H ,6H /
13 IPOP1=5 ,6H ,6H ,6H /
14 IPOP1=6 ,6H ,6H ,6H /
15 IPOP1=7 ,6H ,6H ,6H /
16 IPOP1=8 ,6H ,6H ,6H /
17 IPOP1=9 ,6H ,6H ,6H /
18 IPOP1=10 ,6H ,6H ,6H /
19 IPOP1=11 ,6H ,6H ,6H /
20 IPOP1=12 ,6H ,6H ,6H /
21 IPOP1=13 ,6H ,6H ,6H /
22 IPOP1=14 ,6H ,6H ,6H /
23 IPOP1=15 ,6H ,6H ,6H /
24 IPOP1=16 ,6H ,6H ,6H /
25 IPOP1=17 ,6H ,6H ,6H /
26 IPOP1=18 ,6H ,6H ,6H /
27 IPOP1=19 ,6H ,6H ,6H /
28 IPOP1=20 ,6H ,6H ,6H /
29 IPOP1=21 ,6H ,6H ,6H /
30 IPOP1=22 ,6H ,6H ,6H /
31 IPOP1=23 ,6H ,6H ,6H /
32 IPOP1=24 ,6H ,6H ,6H /
33 IPOP1=25 ,6H ,6H ,6H /
34 IPOP1=26 ,6H ,6H ,6H /
35 IPOP1=27 ,6H ,6H ,6H /
36 IPOP1=28 ,6H ,6H ,6H /
37 IPOP1=29 ,6H ,6H ,6H /
38 IPOP1=30 ,6H ,6H ,6H /
39 IPOP1=31 ,6H ,6H ,6H /
40 IPOP1=32 ,6H ,6H ,6H /
41 IPOP1=33 ,6H ,6H ,6H /
42 IPOP1=34 ,6H ,6H ,6H /
43 IPOP1=35 ,6H ,6H ,6H /
44 IPOP1=36 ,6H ,6H ,6H /
45 IPOP1=37 ,6H ,6H ,6H /
46 IPOP1=38 ,6H ,6H ,6H /
47 IPOP1=39 ,6H ,6H ,6H /
48 IPOP1=40 ,6H ,6H ,6H /
49 IPOP1=41 ,6H ,6H ,6H /
50 IPOP1=42 ,6H ,6H ,6H /
51 IPOP1=43 ,6H ,6H ,6H /
52 IPOP1=44 ,6H ,6H ,6H /
53 IPOP1=45 ,6H ,6H ,6H /
54 IPOP1=46 ,6H ,6H ,6H /
55 IPOP1=47 ,6H ,6H ,6H /
56 IPOP1=48 ,6H ,6H ,6H /
57 IPOP1=49 ,6H ,6H ,6H /
58 IPOP1=50 ,6H ,6H ,6H /
59 IPOP1=51 ,6H ,6H ,6H /
60 IPOP1=52 ,6H ,6H ,6H /
61 IPOP1=53 ,6H ,6H ,6H /
62 IPOP1=54 ,6H ,6H ,6H /
63 IPOP1=55 ,6H ,6H ,6H /
64 IPOP1=56 ,6H ,6H ,6H /
65 IPOP1=57 ,6H ,6H ,6H /

```



```

1  *DECK SSP
2  SUBROUTINE SSP (MED)
3
4  DIMENSION MED(H), NF(118)
5  DIMENSION REL(2), XX(6), KK(14)
6  DIMENSION ITHIN(3), BUFF(60)
7
8
9  COMMON A(6090)
10 COMMON /PLIT/ KPFLT,SIZE,TH(3),IPOP,KCPLT
11
12 DATA IBIN(3),4,8/
13 IR=60
14 IP=61
15
16 ****
17 CALL FTNBIN (J,3,IBIN) *****C
18 ****
19 *****C
20 *****C
21 *****C
22 *****C
23 *****C
24 *****C
25 *****C
26 *****C
27 *****C
28 *****C
29 *****C
30 *****C
31 *****C
32 *****C
33 *****C
34 *****C
35 *****C
36 *****C
37 *****C
38 *****C
39 *****C
40 *****C
41 *****C
42 *****C
43 *****C
44 *****C
45 *****C
46 *****C
47 *****C
48 *****C
49 *****C
50 *****C
51 *****C
52 *****C
53 *****C
54 *****C
55 *****C
56 *****C
57 *****C

```

```

60 C RESTORE GLOBAL COORDINATES
60 C CALL READS (3,ACIN),N33)
60 C HEAD VIEW CONTROL CARD
60 C NFR=1
65 XX(1)=0.
65 XX(2)=0.
65 XX(3)=0.
65 XX(4)=0.
65 XX(5)=0.
65 XX(6)=0.
70 C TEST ANGLES FOR ADMISSIBILITY
70 C
75 L=0
75 DO 5 K=1,3
75 IF (ABS(H(K)).LT.360.1) GO TO 5
75 L=L+1
75 5 CONTINUE
75 IF (L.LT.2) GO TO 10
75 WRITE (IP,100)
75 STOP 21
75 10 CONTINUE
80 C DEFINE PLGI COORDINATES FOR THIS VIEW
80 C CALL P1 (AIN1),A(IN2),A(IN3),NUMPATH,XX)
80 C PLGI NFR FRAMES IN THIS VIEW
90 DO 90 N=1,NFR
90 K=WINO 4
90 READ FRAME DATA
90 KTYPE=1
95 HY-PASS BOUNDARY ELEMENT PLOTTING
95 IF (KTYPE.EQ.7) GO TO 90
95 TEST FOR ADMISSIBLE ELEMENT TYPE
100 IF (KTYPE.GT.0.AND.KTYPE.LE.8) GO TO 15
100 IF (KTYPE.EQ.12) GO TO 15
100 STOP 22
100 15 CONTINUE
105 ADVANCE ELEMENT TAPE4 TO THIS ELEMENT TYPE
105 DO 20 L=1,NELTY
105 K=L
105 IF (KEL(L).EQ.KTYPE) GO TO 25
105 20 CONTINUE
105 25 MARK=1
105 IF (M.LT.1) GO TO 40

```

SSP 58
SSP 59
SSP 60
SSP 61
SSP 62
SSP 63
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SSP 90
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SSP 97
SSP 98
SSP 99
SSP 100
SSP 101
SSP 102
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SSP 105
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SSP 107
SSP 108
SSP 109
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SSP 111
SSP 112
SSP 113
SSP 114

```

115 DC 35 J=1,M
    HEAD (4) IELTYP,NUMEL,LR2
    IF (LR2.EQ.0) GO TO 35
    DC 30 I=1,NUMEL
    CALL HEADS (4,MP,LR2)
120 30 CONTINUE
    35 CONTINUE
    40 HEAD (4) IELTYP,NUMEL,LR2
    IF (IELTYP.AE.KTYPE) STOP 24
125 C      SHIFT PEN TO NEW ORIGIN
    C
    C      CALL PLOT (3*0*0*0,-3)
    C      NCOUNT=NCOUNT+1
    C      IF (NCOUNT.EQ.1) CALL PLOT (1,0*0,7,-3)
130 C      READ AN ELEMENT PLOT SEQUENCE CARD
    C
    C      ME=0
    C      KK(1)=1
    C      KK(2)=NUMEL
    C      DO 45 I,J=3,14
135 45  KK(I,J)=0
    C      IF (KK(1).LT.1) GO TO 85
    C      DO 50 L=1,7
140 50  IF (KK(2*L).LT.1) KK(2*L)=KK(2*L-1)
    C      IF (KK(2*L).LT.KK(2*L-1)) GO TO 55
    C      GO TO 65
    C      ELEMENT SEQUENCE NOT IN ORDER
145 55  WRITE (1P,105) L
    C      60 CONTINUE
    C      IF (KK(1).GT.0) GO TO 60
    C      GO TO 85
    C      CHECK FOR INCREASING SEQUENCE ELEMENT NUMBERS
150 65  L=1
    C      IF (KK(1).LE.KNE) GO TO 55
    C      DC 70 L=2,7
    C      IF (KK(2*L-1).LT.1) GO TO 70
    C      IF (KK(2*L-1).LE.KK(2*L-3)) GO TO 55
155 70  CONTINUE
    C
    C      PLOT THE RANGE OF ELEMENTS IN SEQUENCE L
160 DC 80 L=1,7
    C      I1=KK(2*L-1)
    C      IF (I1.LT.1) GO TO 85
    C      I2=KK(2*L)
    C      IF (I2.GT.NUMEL) STOP 25
    C      DC 80 M=I1,I2
165 C      HEAD THE PAGES FROM TAPE
    C
    C      75 CALL HEADS (4,MP,LR2)
    C      ME=ME+1
    C      IF (M.GT.KNE) GO TO 75
170 C

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SSP 115
SSP 116
SSP 117
SSP 118
SSP 119
SSP 120
SSP 121
SSP 122
SSP 123
SSP 124
SSP 125
SSP 126
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SSP 128
SSP 129
SSP 130
SSP 131
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SSP 135
SSP 136
SSP 137
SSP 138
SSP 139
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SSP 164
SSP 165
SSP 166
SSP 167
SSP 168
SSP 169
SSP 170
SSP 171


```

1  *DECK POUTB
2  SUBROUTINE POUTB (NUMNP,NELTY,N1,N2,N3,N33,KEL)
3
4  DIMENSION HEDT(12), IX(19), NP(18), LOUT(12), LIN(12), NPAR(14),
5  KPL(12), AP(19)
6
7  COMMON A(6600)
8
9  EQUIVALENCE (IX(2),NP(1),AP(1))
10
11 DATA LIN/3,3,5,5,9,5,6,17,0,0,0,0,4,1,LOUT/2,2,4,4,8,4,0,16,0,0,0,18/POR
12 IP=60
13 IP=61
14
15 NTR=10
16
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HEAD AND REFORMAT THE POUTHOLE TAPE = NTR
 REWIND NTR
 1 HEAD AND CONTROL INFORMATION
 HEAD (NTR) (HEDT(K),K=1,12),NUMNP,NELTY
 2 EQUATION NUMBERS FOR RETAINED DEGREES OF FREEDOM
 READ (NTR)
 SET UP ARRAY SIZE FOR COORDINATES
 N1=1
 N11=NUMNP
 N2=N1*NUMNP
 N22=2*NUMNP
 N3=N2*NUMNP
 N33=3*NUMNP
 N4=N3*NUMNP
 I=LOC(A(N4))
 3 HEAD NODE COORDINATES
 HEAD (NTR) (A(K),K=N1,N11)
 HEAD (NTR) (A(K),K=N2,N22)
 HEAD (NTR) (A(K),K=N3,N33)
 PRINT FIRST AND LAST NODE COORDINATES
 SAVE NODE COORDINATES ON TAPE 3
 REWIND 3
 CALL WRITES (3,A(N1),N33)
 4 NODE TEMPERATURES

PRINT FIRST AND LAST NODE COORDINATES

```

60      C      HEAD (NTB)
        C      4
        C      5      ENCL-FILE MARK
        C      HEAD (NTU) NDU M
        C      5
65      C      USE PRVIOUS CARD FOR RUN COMPILER
        C      IF (EOF(NTB)) 10,5
        C      5      WRITE (IP,135)
        C      CALL EXJI
        C      10      CONTINUE
70      C
75      C      PROCESS ELEMENT DATA AND SAVE CONNECTIVITIES ON TAPE 4
        C      HEWIND,4
        C
        C      DO 130 M=1,NELTYP
80      C      6      ELEMENT CONTROL PARAMETERS
        C      HEAD (NTU) (NPAR(K),K=1,14)
        C      6
        C      IELTYP=NPAR(1)
        C      KEL(M)=IELTYP
        C      NUMEL=NPAR(2)
        C
        C      LR=LIN(IELTYP)
        C      LR2=LOU(IELTYP)
90      C      WRITE (4) IELTYP,NUMEL,LR2
        C
        C      GO TO (15,25,35,40,50,55,65,70,75,85,90,95), IELTYP
95      C      15      CONTINUE
        C
        C      7      MATERIAL PROPERTIES
        C      NUMMAT=NPAR(3)
        C      GO 20 ISK(IP=1,NUMMAT)
        C      HEAD (NTB)
        C      HEAD (NTB)
        C      20      CONTINUE
100      C      7      SECTION PROPERTIES
        C      HEAD (NTB)
        C
        C      A      LOAD MULTIPLIERS
        C      HEAD (NTU)
        C
        C      GO TO 100

```

```

POR 58
POR 59
POR 60
POR 61
POR 62
POR 63
POR 64
POR 65
POR 66
POR 67
POR 68
POR 69
POR 70
POR 71
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POR 74
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POR 112
POR 113
POR 114

```



```

230 LRR2=LR2
    IF (IELTYP.EQ.12) LRR2=3
    DC 125 K=1, NUPEL
    C
235 CALL HEADS (NIB, IX, LR)
    C
    BY-PASS THE BOUNDARY ELEMENTS
    IF (IELTYP.EQ.7) GO TO 120
    C
    CHECK FOR SEQUENTIAL INPUT ORDER
    IF (IX(1).EQ.N) GO TO 105
    WRITE (IP,145) IX(1),K,I
    CALL EX11
    C
    105 CONTINUE
    C
245 TEST FOR FOURTH MODE ZERO
    IF (LR2.NE.4) GO TO 110
    IF (NP(4),L1,1)...NP(4),LRP(3)
    C
250 110 IF (IELTYP.NE.12) GO TO 115
    C
    HEAD_RADIUS,KODE,X3P (BEND) OR JUNK (TANGENT)
    C
    HEAD (NIB) AP(4),NP(5),AP(6),AP(7),AP(8)
    IF (NP(1).EQ.1) GO TO 115
    C
255 HEND, READ THETA AND DC ARRAY
    C
    HEAD (NT8) (AP(IJL),I,JL=9,18)
    C
260 PIPE TAPE SAVE FORMATS (TAPE4)
    C
    TANGENT - 1,N1,N,J,XLN,JUNK(5)-JUNK(14)
    HEND - 2,N1,N,J,RADIUS,KODE,X3P,[META,DC(1,)]-DC(3,3)
    C
265 115 CALL WRITES (4,NP,LR2)
    C
    PRINT FIRST AND LAST ELEMENT CONNECTIONS
    C
270 120 CONTINUE
    C
    125 CONTINUE
    C
    130 CONTINUE
    C
275 RETURN
    C
135 FORMAT (////23H SOLUTION TERMINATED.../39H NO END-OF-FILE ENCOUNTERED 277-
    IERED ON TAPE 4(19))
140 FORMAT (//20H ***ERROR... ELEMENT TYPE (+12,23H) FINCOUNTERED ON TAPPOUR 279
    IFB.,/1X)
145 FORMAT (//43H ***ERROR... ELEMENTS ON TAPEB ARE NOT SEQUENTIAL,5X,3POR 281
    ITC)
    END
    POR 283-

```

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```
1 *DECK WRITES  
SUBROUTINE WRITES (ITAPE,A,LREC)  
DIMENSION A(LREC)  
WRITE (ITAPE) A  
RETURN  
5 END  
6-
```

```

1      *DECL. HEADS
      SUBROUTINE HEADS (ITAPE,A,LREC)
      DIMENSION A(LREC)
      READ (ITAPE) A
      RETURN
      END

```

```

HEA 1
HEA 2
HEA 3
HEA 4
HEA 5
HEA 6-

```


AD-A093 356

CIVIL ENGINEERING LAB (NAVY) PORT HUENEME CA F/G 13/13
DECEL1 USERS MANUAL. A FORTRAN IV PROGRAM FOR COMPUTING THE STA--ETC(U)
AUG 80 S SERGEV
CEL-TN-1584

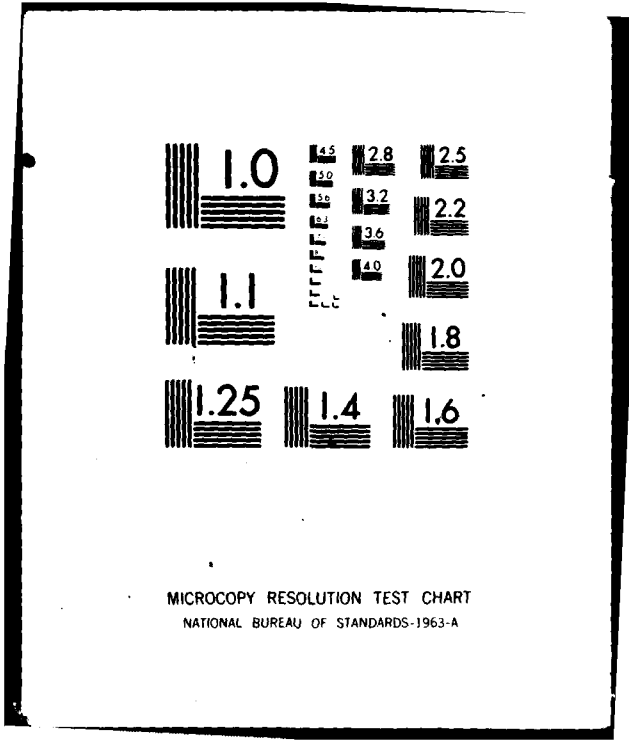
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END
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MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

```

115      ALEN=30.0          P1 115
        C
        C  SET SCALE PARAMETERS  P1 116
        C  P1 117
        C  P1 118
        C  P1 119
        C  50 CONTINUE      P1 120
        C  XX(11)=0.0      P1 121
        C  XX(12)=ALEN     P1 122
        C  YY(11)=0.0     P1 123
        C  YY(12)=YLEN    P1 124
        C  CONVERT PLOT ORDINATES TO RELATIVE VALUES  P1 125
        C  P1 126
        C  P1 127
        C  DO 55 I=1,NMAP   P1 128
        C  U(I)=U(I)-XFIN  P1 129
        C  V(I)=V(I)-YFIN  P1 130
        C  55 CONTINUE    P1 131
        C  RETURN          P1 132
        C  END             P1 133
    
```

CARD NO.	SEVERITY	DETAILS	DIAGNOSIS OF PROBLEM
36	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
38	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
39	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
40	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
41	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
42	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
43	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
44	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
45	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
46	I	XN	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
51	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
52	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
53	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
54	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
55	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
56	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
57	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
61	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
62	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
63	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
64	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
65	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
66	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
67	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
68	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
73	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.
75	I	W	ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.

```

1      *DECK P2
2      SUBROUTINE P2 (U,V,WP,RADIUS,KODE,XP,THETA,DC,NODES,ILINE)
3
4      C
5      C THIS SURROUTINE PLOTS A 2, 4, 8, OR 16-NODE ELEMENT
6
7      C
8      C DIMENSION U(1), V(1), NP(1), IT(9)
9      C DIMENSION DC(3,3), X3P(3)
10     C
11     C COMMON /MESH/ XX(12),YY(12),XLEN,XLENALEN,EX(3),EY(3),XMIN,YMIN
12     C
13     C DATA II/9,2,10,3,11,4,12,1,9/
14     C DATA RAD2/0.03490658/
15
16     C
17     C DETERMINE THE TYPE OF ELEMENT TO BE PLOTTED
18
19     C IF (NODES.EG.16) GO TO 40
20     C IF (NODES.EG.8) GO TO 25
21     C IF (NODES.EG.4) GO TO 15
22
23     N=0
24     IM=0
25     IN=0
26     IN=ILINE
27
28     C IF (NODES.NE.18) GO TO 5
29     C IF (NP(1).EG.2) GO TO 60
30
31     N=1
32     IM=1
33     IN=1
34
35     C TWO NODE ELEMENT
36
37     C
38     C 5 DC 10, M=1,2
39     C N=IN+1
40     C J=NP(N)
41     C XX(M)=U(J)
42     C YY(M)=V(J)
43     C XX(3)=XX(1)
44     C XX(4)=XX(2)
45     C YY(3)=YY(1)
46     C YY(4)=YY(2)
47
48     C
49     C CALL LINE (XX,YY,2,1,IM,IN)
50     C RETURN
51
52     C
53     C FOUR NODE ELEMENT (QUADRILATERAL OR TRIANGLE)
54
55     C
56     C 15 CONTINUE
57     C DC 20, M=1,4
58     C J=NP(M)
59     C XX(M)=U(J)
60     C YY(M)=V(J)
61     C XX(5)=XX(1)
62     C YY(5)=YY(1)
63     C XX(6)=XX(1)
64     C XX(7)=XX(2)
65     C YY(6)=YY(1)
66     C YY(7)=YY(2)
67
68     C
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70
71
72
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CALL LINE (XX,YY,5,1,0,0)
RETURN
60 C EIGHT NODE ELEMENT (BRICK OR WEDGE)
C
C 25 CONTINUE
DO 30 M=1,4
  JUMP(M)
  XX(M)=U(L)
  YY(M)=V(L)
30 C UC 35 M=5,8
  JUMP(J)
  JUMP(JJ)
  XX(M)=U(L)
  YY(M)=V(L)
35 C
  XX(9)=XX(1)
  YY(9)=YY(1)
  XX(10)=XX(4)
  YY(10)=YY(4)
80 C CALL LINE (XX,YY,10,1,0,0)
  XX(9)=XX(5)
  YY(9)=YY(5)
  XX(10)=XX(8)
  YY(10)=YY(8)
85 C CALL LINE (XX(9),YY(9),2,1,0,0)
  XX(9)=XX(6)
  YY(9)=YY(6)
  XX(10)=XX(3)
  YY(10)=YY(3)
90 C CALL LINE (XX(9),YY(9),2,1,0,0)
  XX(9)=XX(2)
  YY(9)=YY(2)
  XX(10)=XX(7)
  YY(10)=YY(7)
95 C CALL LINE (XX(9),YY(9),2,1,0,0)
  RETURN
C
C SIXTEEN NODE ELEMENT (THICK SHELL)
C
C 40 CONTINUE
C
C TOP AND BOTTOM (USING SYMBOL FOR MID-NODES)
IAC=0
DO 50 I=1,2
  IF (I=2) INC=4
  UC 45 M=1,9
  JUMP(I)*INC
  JUMP(JJ)
  XX(M)=U(J)
  YY(M)=V(J)
50 CALL LINE (XX(2),YY(2),9,1,2,1)
  EDGES
C
C

```

P2 58
P2 59
P2 60
P2 61
P2 62
P2 63
P2 64
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P2 104
P2 105
P2 106
P2 107
P2 108
P2 109
P2 110
P2 111
P2 112
P2 113
P2 114

```

115      DC 55,1,1,0,0
      J=NP(1)
      K=NP(1+4)
      X(9)=U(J)
      Y(9)=V(J)
      X(10)=U(K)
      Y(10)=V(K)
      55 CALL LINE (X(9),Y(9),2,1,0,0)
125      C
      MEIURA
      C
      MEMD (PIPE ELEMENT)
      C
      60 NSEG=THETA/RAD2
      IF (NSEG.LT.1) NSEG=1
      J=NP(2)
      X(2)=U(J)
      Y(2)=V(J)
      X(3)=X(1)
      X(4)=X(12)
      Y(3)=Y(1)
      Y(4)=Y(12)
      THETA=0.
      EDCL1=EX(1)*DC(1,1)+EX(2)*DC(2,1)+EX(3)*DC(3,1)
      EDCL2=EX(1)*DC(1,2)+EX(2)*DC(2,2)+EX(3)*DC(3,2)
      EDCL3=EX(1)*DC(1,3)+EX(2)*DC(2,3)+EX(3)*DC(3,3)
      EDC22=EV(1)*DC(1,2)+EV(2)*DC(2,2)+EV(3)*DC(3,2)
      CALL LINE (X(2),Y(2),1,1,-1,1)
      INTER=PI*RADIUS
      IE (KODE.EQ.1) RIEHM=RADIUS*TAN(0.5*(THETA)
      UCORH=EX(1)+X3P(1)*DC(1,KODE)+ETERM1+EX(2)+X3P(2)*DC(2,KODE)+RTEP2
      IMP1=EX(3)+X3P(3)*DC(3,KODE)+ETERM1)-XMIN
      VCOM=(Y(1)+X3P(1)*DC(1,KODE)+ETERM1)+Y(2)+X3P(2)*DC(2,KODE)+RTEP2
      IMP2=EV(3)+X3P(3)*DC(3,KODE)+ETERM1)-YMIN
      UO 70 I=1,NSEG
      X(1)=X(2)
      Y(1)=Y(2)
      T=TA=THETA/RAD2
      X=RADIUS*SIN(THTA)
      Y=RADIUS*(1-COS(THTA))
      X(2)=UCORH+EDC12+Y*UCOR
      Y(2)=EOC22+X*EDC22+Y*VCOM
      IF (1.LT.NSEG) GO TO 65
      J=NP(3)
      X(2)=U(J)
      Y(2)=V(J)
      65 CALL LINE (X(2),Y(2),1,0,0)
      70 CONTINUE
      CALL LINE (X(2),Y(2),1,1,-1,1)
      METURN
      C
      END
165      C
166      C
167      C

```

P2 115
P2 116
P2 117
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P2 161
P2 162
P2 163
P2 164
P2 165
P2 166
P2 167-

CARD NO. SEVERITY DETAILS DIAGNOSIS OF PROBLEM

131 I NP ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.

159 I NP ARRAY REFERENCE OUTSIDE DIMENSION BOUNDS.

```

1  CHECK P3 P3 1
   SUBROUTINE P3 (MED, IH) P3 2
C P3 3
C THIS ROUTINE COMPLETES THE PLOT FRAME P3 4
C P3 5
C DIMENSION MED(1), IH(1), M(3) P3 6
C P3 7
C COMMON /MESH/ XX(12),YY(12),XLEN,YLEN,ALEN,EX(3),EY(3) P3 8
C P3 9
C DATA W/IMX,IMY,IMZ/ P3 10
C IB=60 P3 11
C IP=61 P3 12
C PLOT TITLE AND AXES P3 13
C P3 14
C CALL SYMBOL (0.0,-.350,14,MED(1),0.0,0.0) P3 15
C CALL PLOT (-1.5,1.5,-3) P3 16
C DC 5, IP, 3 P3 17
C IF (IH(1).GT.270) GO TO 5 P3 18
C CALL SYMBOL (.5*EX(I),.5*EY(I),1.0,13,M(I),-1) P3 19
C CALL SYMBOL (EX(I),EY(I),0.1,6,IH(I),-1) P3 20
C CALL SYMBOL (1.2*EX(I),-.075,1.2*EY(I),-.075,.15,M(I),0.0,1) P3 21
C P3 22
C P3 23
C P3 24
C ADVANCE PAPER TO NEXT FRAME P3 25
C P3 26
C CALL PLOT (1.5,-1.5,-3) P3 27
C CALL PLOT (ALEN*7.0,0.0,-3) P3 28
C P3 29
C RETURN P3 30
C END P3 31-

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