

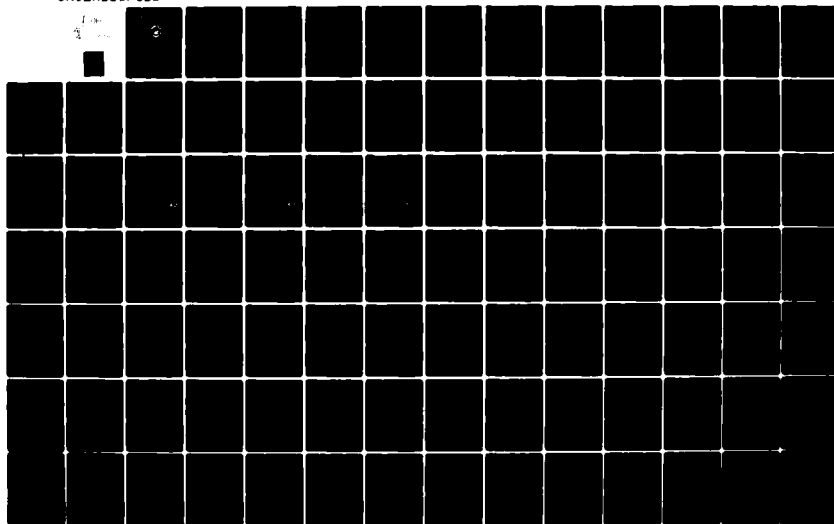
AD-A098 085

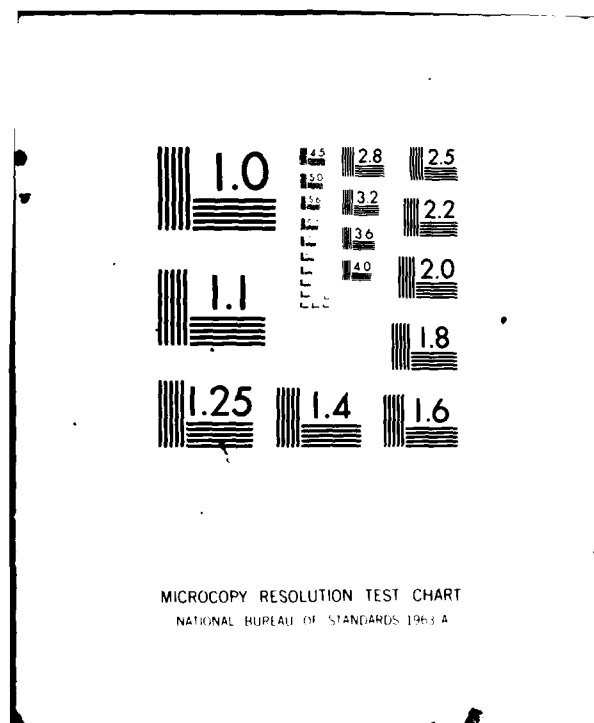
NAVAL POSTGRADUATE SCHOOL MONTEREY CA
COMPUTER INVESTIGATION OF VHF, UHF AND SHF FREQUENCIES FOR MARI--ETC(1
DEC 80 T G KANE

F/G 17/2.1

UNCLASSIFIED

NL





AD A 098085

NAVAL POSTGRADUATE SCHOOL
Monterey, California



DTIC
ELECTE
APR 23 1981

9/2/80

THESIS

COMPUTER INVESTIGATION OF VHF, UHF
AND SHF FREQUENCIES FOR
MARINE CORPS PACKET RADIO USAGE

by

(10) Thomas George Kane

December 1980

(12) 124

Thesis Advisor:

J. M. Wozencraft

Approved for public release; distribution unlimited.

DTIC FILE COPY

01 1 12 021

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER	2. GOVT ACCESSION NO.	3. RECIPIENT'S CATALOG NUMBER
	AD-A098085	
4. TITLE (and Subtitle)	5. TYPE OF REPORT & PERIOD COVERED	
Computer Investigation of VHF, UHF and SHF Frequencies for Marine Corps Packet Radio Usage	Master's Thesis; December 1980	
7. AUTHOR(s)	6. PERFORMING ORG. REPORT NUMBER	
Thomas George Kane		
9. PERFORMING ORGANIZATION NAME AND ADDRESS	8. CONTRACT OR GRANT NUMBER(s)	
Naval Postgraduate School Monterey, California 93940		
11. CONTROLLING OFFICE NAME AND ADDRESS	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
Naval Postgraduate School Monterey, California 93940		
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)	12. REPORT DATE	
Naval Postgraduate School Monterey, California 93940	December 1980	
	13. NUMBER OF PAGES	
	123	
	15. SECURITY CLASS. (of this report)	
	Unclassified	
	15a. DECLASSIFICATION/DOWNGRADING SCHEDULE	
16. DISTRIBUTION STATEMENT (of this Report)		
Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)		
Packet Radios Frequency Determination Link Equations Marine Amphibious Brigade Network Connectivity Interception Vulnerability		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number)		
This thesis is a computer investigation of the VHF, UHF and SHF frequency bands for possible use by Marine Corps Packet Radio systems. It uses the STAR Terrain Model to analyze the different connectivity patterns that appear as the units of the Marine Amphibious Brigade move across the battlefield. The problem of enemy intercept of friendly traffic is also discussed and the units with a high probability of being intercepted are displayed pictorially.		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE
S/N 6102-614-6001

Approved for public release; distribution unlimited.

Computer Investigation of VHF, UHF and SHF
Frequencies for Marine Corps Packet Radio Usage

by

Thomas George Kane
Captain, U.S. Marine Corps
B.S.I.M., Purdue University, 1974

Submitted in partial fulfillment of the
requirements for the degree of

MASTER OF SCIENCE IN ELECTRICAL ENGINEERING

from the

NAVAL POSTGRADUATE SCHOOL
December 1980

SEARCHED	INDEXED
SERIALIZED	FILED
DEC 1980	
NAVAL POSTGRADUATE SCHOOL	
DURHAM, N.C.	
A	

Author

Thomas G Kane

Approved by:

John R Wozencraft

Thesis Advisor

James K. Hartman

Second Reader

J. T. Kidd

Chairman, Department of Electrical Engineering

William M. Latta

Dean of Science and Engineering

ABSTRACT

This thesis is a computer investigation of the VHF, UHF and SHF frequency bands for possible use by Marine Corps Packet Radio systems. It uses the STAR Terrain Model to analyze the different connectivity patterns that appear as the units of the Marine Amphibious Brigade move across the battlefield. The problem of enemy intercept of friendly traffic is also discussed and the units with a high probability of being intercepted are displayed pictorially.

TABLE OF CONTENTS

I.	INTRODUCTION - - - - -	5
II.	LINK EQUATIONS FOR PACKET RADIOS - - - - -	7
	A. GENERAL - - - - -	7
	B. LINK EQUATION - - - - -	8
	C. PATH LOSS - - - - -	11
	D. ATTENUATION BY FOLIAGE - - - - -	14
	E. ATTENUATION OF MILLIMETER WAVES - - - - -	17
III.	STAR TERRAIN MODEL - - - - -	24
IV.	UNIT LOCATIONS - - - - -	36
V.	CONNECTIVITY - - - - -	60
	A. GENERAL - - - - -	60
	B. SHF CONNECTIVITY - - - - -	60
	C. UHF AND VHF CONNECTIVITY - - - - -	65
	D. CONNECTIVITY WITH UNIT MOVEMENT - - - - -	73
VI.	ENEMY INTERCEPT - - - - -	90
VII.	CONCLUSIONS AND RECOMMENDATIONS - - - - -	99
	APPENDIX A - COMPUTER PROGRAM LISTING - - - - -	102
	LIST OF REFERENCES - - - - -	121
	INITIAL DISTRIBUTION LIST - - - - -	123

I. INTRODUCTION

Packet Radio (PR) is a technology that extends the application of packet switching, which evolved for networks of point-to-point communication lines, into the area of broadcast radio. It offers a highly effective way of using a multiple-access radio channel, with potentially large numbers of mobile users, to support digital communications over a wide geographic area.

Users in a packet radio network are assumed to share common radio channels, access to which is controlled by microprocessors in the packet radios. The unit of transmission in a packet radio network is called a packet. It contains a number of data bits and is usually variable in length. A packet includes all addressing and control information necessary to correctly route the packet to its final destination. Each packet wends its way from node to node through the network until it arrives at its final destination and is delivered.

An essential attribute of any network is its ability to provide full connectivity among all network nodes [Ref. 1]. It is this connectivity that will be examined in this report. The nodes in this network will be the units that comprise the Marine Amphibious Brigade (MAB). The units will be spread over a battlefield such that their positions relative to one another will be in keeping with current doctrine. The battlefield will

be the STAR model of the Fulda Gap region in West Germany, which is currently being used by the U.S. Army for combat simulation [Ref. 2].

II. LINK EQUATIONS FOR PACKET RADIOS

A. GENERAL

Ground radio links are subject to severe variations in received signal strength due to local variations in terrain and foliage. In addition, reflections give rise to multiple signal paths which lead to distortion and fading as signals with different delays interfere at a receiver. As a result, RF connectivity is difficult to predict in detail and may change abruptly as units move about the battlefield.

If a packet radio network existed such that all radios were sited with a radio line-of-sight path to nearby neighbors, then the predictability and reliability of such a network would be greatly increased. Particularly if a packet radio network existed such that all radios possessed an optical line-of-sight to nearby neighbors, then analysis of the network would be greatly simplified.¹ The stringent requirement for an optical line-of-sight over the earth will be used in this report to simplify the calculations.

¹An optical line-of-sight exists when a straight line can be drawn between the two antennas, and the line is not intersected by the earth. A radio line-of-sight is an RF path between a transmitter and a receiver. This path can exist in the absence of an optical line-of-sight because of obstacle gain and diffraction.

B. LINK EQUATION

The link equation used in this report is:

$$\frac{P_T G_T G_R}{k T_o B_{Rf} F_s L} \geq \text{SNR}_{\min}$$

where P_T = transmitter output power (watts)
 G_T = transmitting antenna gain
 G_R = receiving antenna gain
 L = link loss
 k = Boltzman's constant (-228.6 dB)
 T_o = noise temperature (24.6 dB)
 B_{Rf} = RF bandwidth of receiver
 F_s = system noise figure
 $\text{SNR}_{\min}$ = signal-to-noise ratio at receiver input
corresponding to minimum acceptable
message quality

The link loss can consist of the following losses.

$$L = [L_s](L_{O_2 - H_2O})(L_{\text{Rain}})(L_T)(L_R)(L_P)(L_F)$$

Here:

- . $L_s = \left(\frac{4\pi d}{\lambda}\right)^2$ is the spreading loss (for free-space),
- . $L_{O_2 - H_2O}$ is the loss due to oxygen and water vapor absorption at frequencies above about 10 GHz,

- . L_{Rain} is the loss due to rainfall attenuation at frequencies above about 3 GHz
- . L_T and L_R are the losses associated with the transmitting and receiving stations,
- . L_p includes incidental losses, and
- . L_F is the loss associated with foliage penetration.

Therefore the link equation is:

$$\frac{P_T G_T G_R}{k T_o B_{\text{rf}} F_s [L_s] (L_{O_2 - H_2O}) (L_{\text{Rain}}) (L_T) (L_R) (L_p) (L_F)} \geq \text{SNR}_{\text{min}}$$

For the analysis of the connectivity of the MAB's radio network the following parameters were given.

- (1) Both transmit and receive antennas were omnidirectional in the horizontal plane and had a 30° beamwidth in the vertical plane.
- (2) The transmit power was 1 watt.
- (3) The data rate was 16 kbs with a $P_e \leq 10^{-6}$.
- (4) The system noise figure was 15 dB, $(L_T)(L_R)$ was 3 dB, and L_p was 1 dB.

To find the SNR_{min} that will give a $P_e \leq 10^{-6}$ we have

$$P_e \leq \frac{1}{2} \text{erfc } \sqrt{z}$$

where z is the $\text{SNR}_{\min}$ [Ref. 3]. This gives a $\text{SNR}_{\min}$ of 10.53 dB, or about 11 dB for PRK.

To get the gain of the transmit and receive antennas, which are omni-directional in the horizontal plane and have a 30° beamwidth in the vertical plane we have the following equation.

Directive Gain G_T, G_R

$$G_T = G_R = \frac{4\pi r^2}{\text{area}} = \frac{4\pi r^2}{(\theta r)(\phi r)} = \frac{4\pi}{\theta\phi} \text{ in radians}$$

or

$$G_T = G_R = \frac{4\pi}{\left[\frac{2\pi}{360} \theta^\circ\right] \left[\frac{2\pi}{360} \phi^\circ\right]} = \frac{360^2}{\pi \theta^\circ \phi^\circ} = \frac{41253}{\theta^\circ \phi^\circ} \text{ in degrees}$$

$$G_T = G_R = \frac{41253}{(30)(360)} = 3.8197 = 5.82 \text{ dB}.$$

Thus for $P_T = 1 \text{ watt} = 0 \text{ dBw}$ and $B_{RF} = 2 \times 16 \text{ kbps}$ the link equation becomes

$$\frac{0 \text{ dB} + 5.82 \text{ dB} + 5.82 \text{ dB}}{-228.6 \text{ dB} + 24.6 \text{ dB} + 45 \text{ dB} + 15 \text{ dB} [L_s] (L_{O_2-H_2O}) (L_{\text{Rain}}) + 3 \text{ dB} + 1 \text{ dB} + (L_F) \text{ dB}} \geq 11 \text{ dB}$$

or

$$L_{dB} = [L_s(L_{O_2} - H_2O)]_{dB} + [L_{Rain}]_{dB} + [L_F]_{dB} \leq 140.64 \text{ dB}$$

Therefore, the attenuation due to path loss, rain, and foliage must be less than or equal to about 141 dB. It is this link loss of 141 dB that was used in the model to determine whether or not a link "existed." All combinations of transmitters and receivers were analyzed to find links that had losses of less than 141 dB.

C. PATH LOSS

The minimum theoretical path loss on a radio link in free-space is given by the following formula.

$$L_s = \text{Loss}_{fs} = \left(\frac{4\pi d}{\lambda}\right)^2$$

For a ground radio link, the path loss of free-space may be approached on a link having a radio line-of-sight, although even under this desirable condition diffraction and multipath phenomena can greatly reduce received signal power. Average path attenuation exceeds that of a free-space radio link by a significant amount in the ground radio environment, depending on the type of terrain and the elevation of the radio antenna. The curves in Figures 1 and 2 show average path loss as a

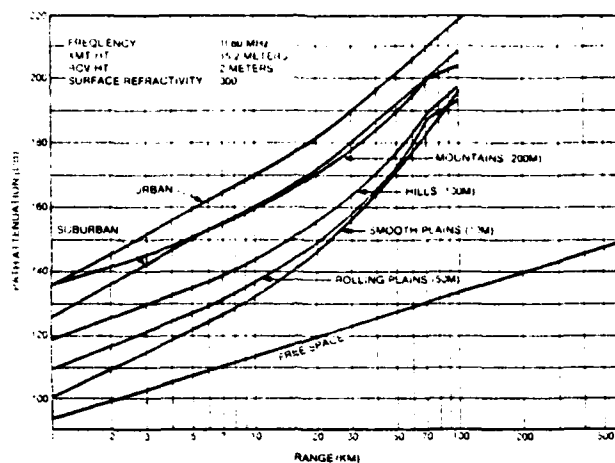
function of link range for a frequency of 1.080 GHz, and illustrate these dependencies for two different transmitter heights [Ref. 4]. These curves are typical also of propagation at UHF.

It is worth noting that the variation of mean path loss as a function of frequency is typically much less than the variations due to terrain at a particular frequency [Ref. 1]. The curves shown reflect average values of path loss which apply to a link of given length which is randomly selected without regard to user siting. Well sited radios will typically encounter less path loss than shown in the curves [Ref. 1].

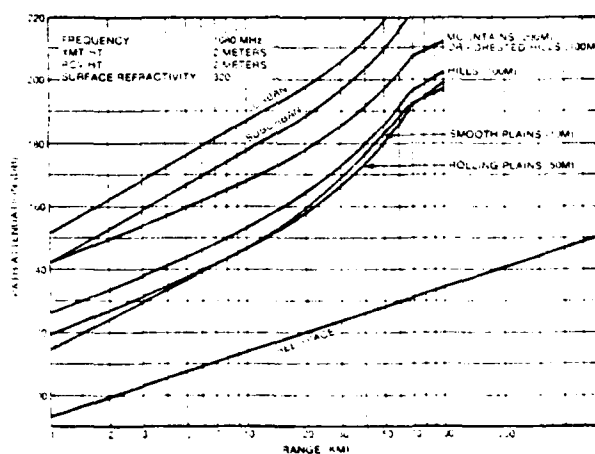
Bullington [Ref. 5] and later Jordan and Balmain [Ref. 6] have developed a simplified propagation formula for transmission in the VHF/UHF range when the elevated transmitting and receiving antennas are far apart. Their approximations are:

- (1) The surface wave can be neglected in comparison with the space wave.
- (2) The angle of incidence of the wave with the earth (hence the angle of reflection) is very small so that the reflection factor equals -1.

When the approximations used are valid, the received field strength is proportional to the height of the transmitting antenna, the height of the receiving antenna, and inversely proportional to the square of the distance between them [Refs. 5 and 6].



Path loss versus range. 15-m transmitter height.



Path loss versus range. 2-m transmitter height.

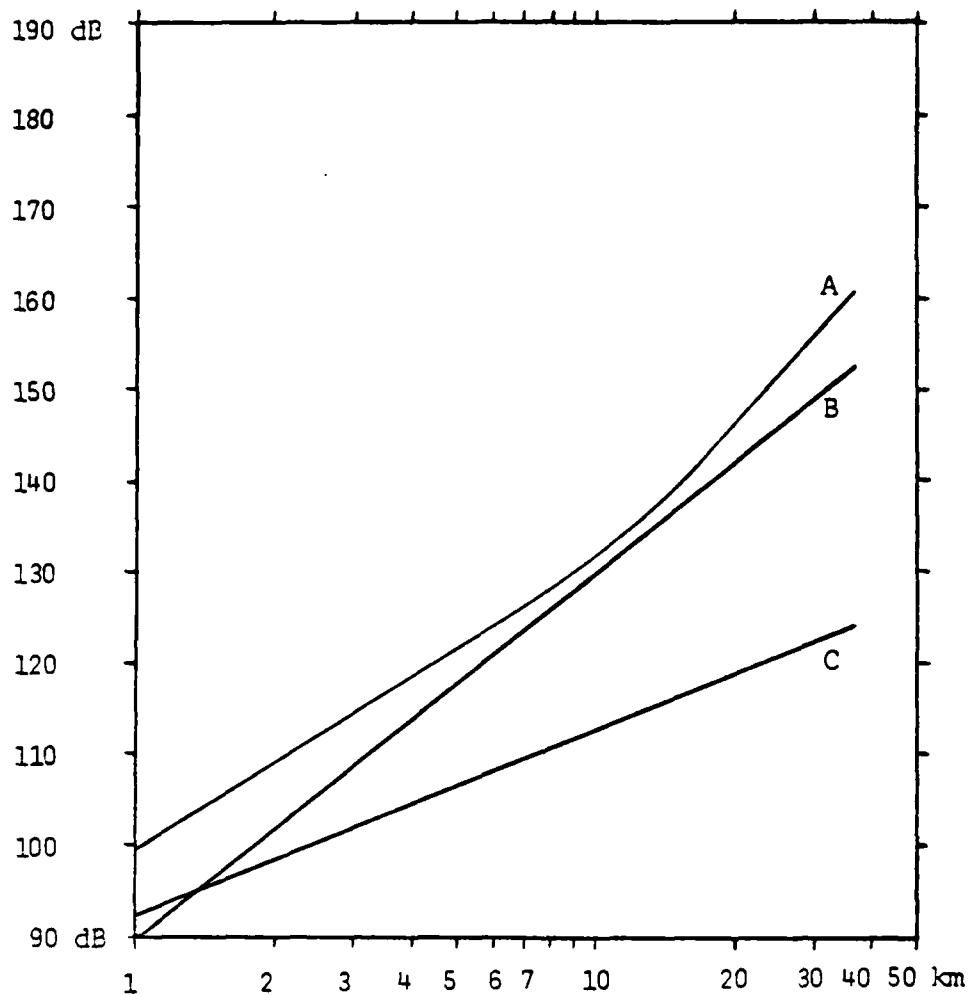
Figures 1 and 2. Path loss versus range [Ref. 4].

$$L_s = \text{Loss} = \left(\frac{d^2}{h_T h_R} \right)^2$$

where h represents the heights of the antennas and d represents the distance between them. This relation is independent of frequency and is valid as long as the loss is more than the free-space loss. Figure 3 shows the free-space loss, the loss encountered over "smooth plains" from Figure 1, and the loss associated with Bullington's equation for a transmit antenna height of 15.2 meters and a receive antenna height of two meters. Figure 4 represents the same data but with a transmit antenna height of two meters. For both graphs, the error is less than 5 dB over the range of interest, which is from a few to about 10 km. Therefore Bullington's equation was used in this thesis to predict path losses in the VHF and UHF regions. The equation is valid as long as it produces losses greater than the free-space loss. Therefore, the model uses the larger of the two losses in calculating link loss.

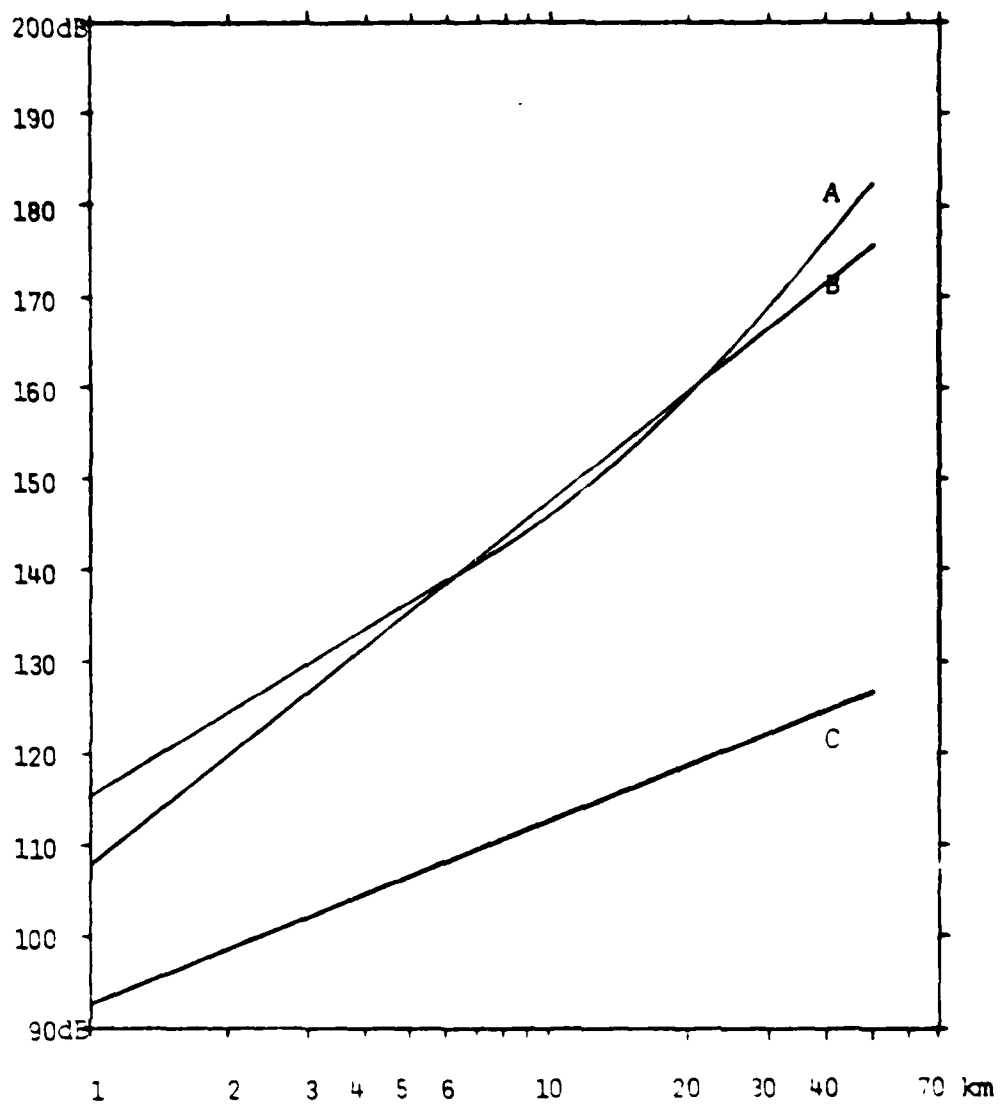
D. ATTENUATION BY FOLIAGE

Another factor that affects the link loss is the attenuation caused by foliage penetration. Nathanson [Ref. 7] referenced a previously defined equation by Saxton and Lane [Ref. 8] for attenuation in the frequency range from 100 MHz to 3 GHz. He stated that for either antenna polarization, attenuation by trees with leaves in that range is given



- A - Smooth plains
- B - Bullington's loss equation
- C - Free Space loss

Figure 3. Comparison of Bullington's loss equation vs. free space loss, for a transmitter height of 15.2 meters



- A - Smooth plains
- B - Bullington's loss equation
- C - Free Space loss

Figure 4. Comparison of Bullington's loss equation vs. free space loss, for a transmitter height of 2 meters

approximately by

$$A = 0.25 f^{3/4} \text{ (dB/m)}$$

where f is the carrier frequency in gigahertz and A is attenuation in dB per meter. This equation is used to calculate attenuation from foliage penetration in the model.

2. ATTENUATION OF MILLIMETER WAVES

As shown in Figure 5, at frequencies above about 10 GHz, transmission of millimeter waves through the atmosphere is subject to attenuation caused by resonances of oxygen and water vapor molecules. Attenuation by precipitation, primarily rain, and attenuation associated with penetrating tree foliage also play a key role.

For highly reliable operations at millimeter waves, attenuation by rain is the dominant factor in determining the reliability of the circuit. Figures 6a, b and c were developed by Dudzinsky [Ref. 9] and give required margins for three different levels of reliability. For various frequencies, Figure 6a has as abscissa the path length and gives as an ordinate the margin that will not be exceeded by attenuation due to rain for 99.9% of the time.

The attenuation over a free-space path through a clear atmosphere is simply the sum of the spreading loss $(4\pi d/\lambda)^2$ and the loss due to oxygen and water vapor absorption. The

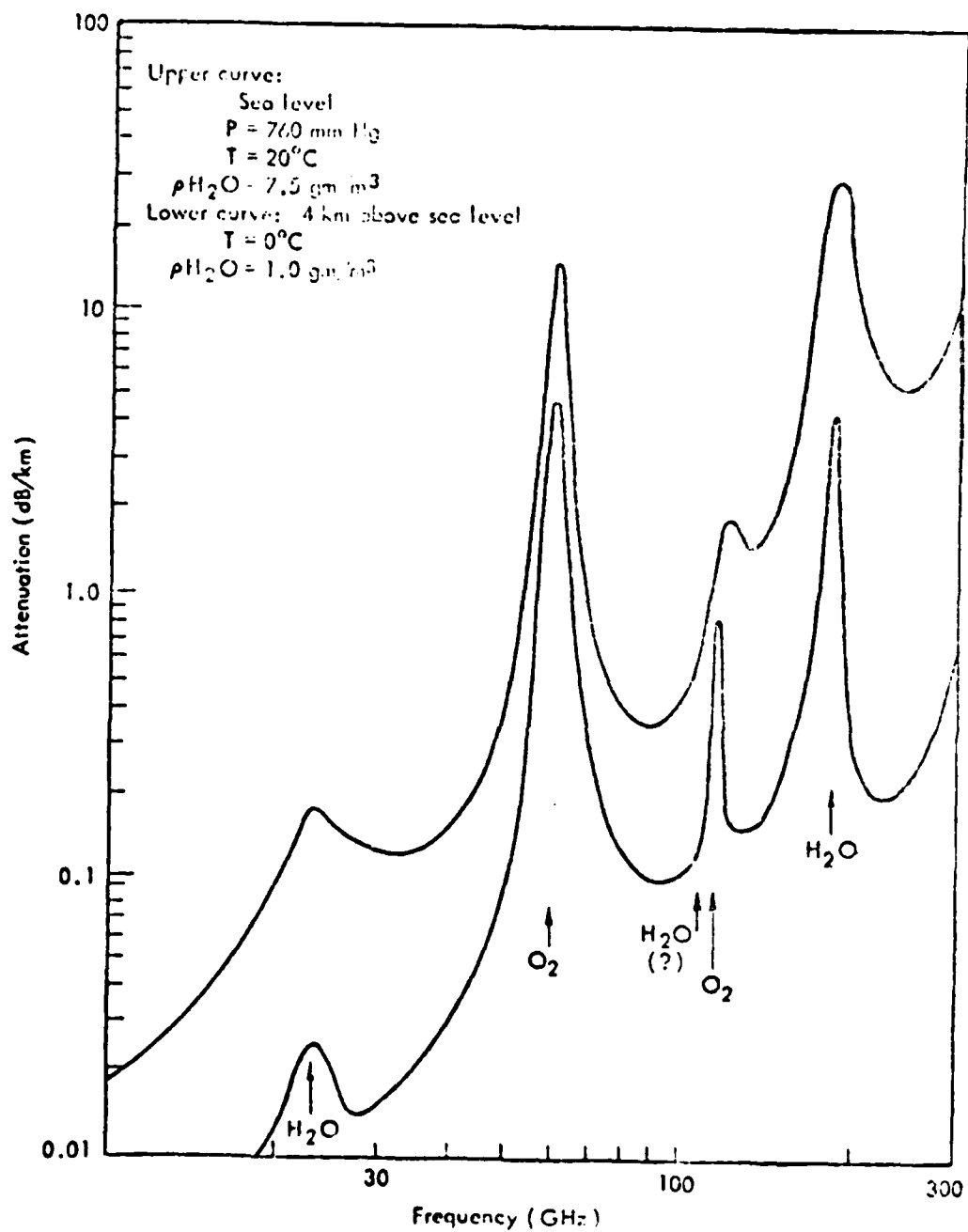


Figure 5. Horizontal attenuation due to oxygen and water vapor [Ref. 9].

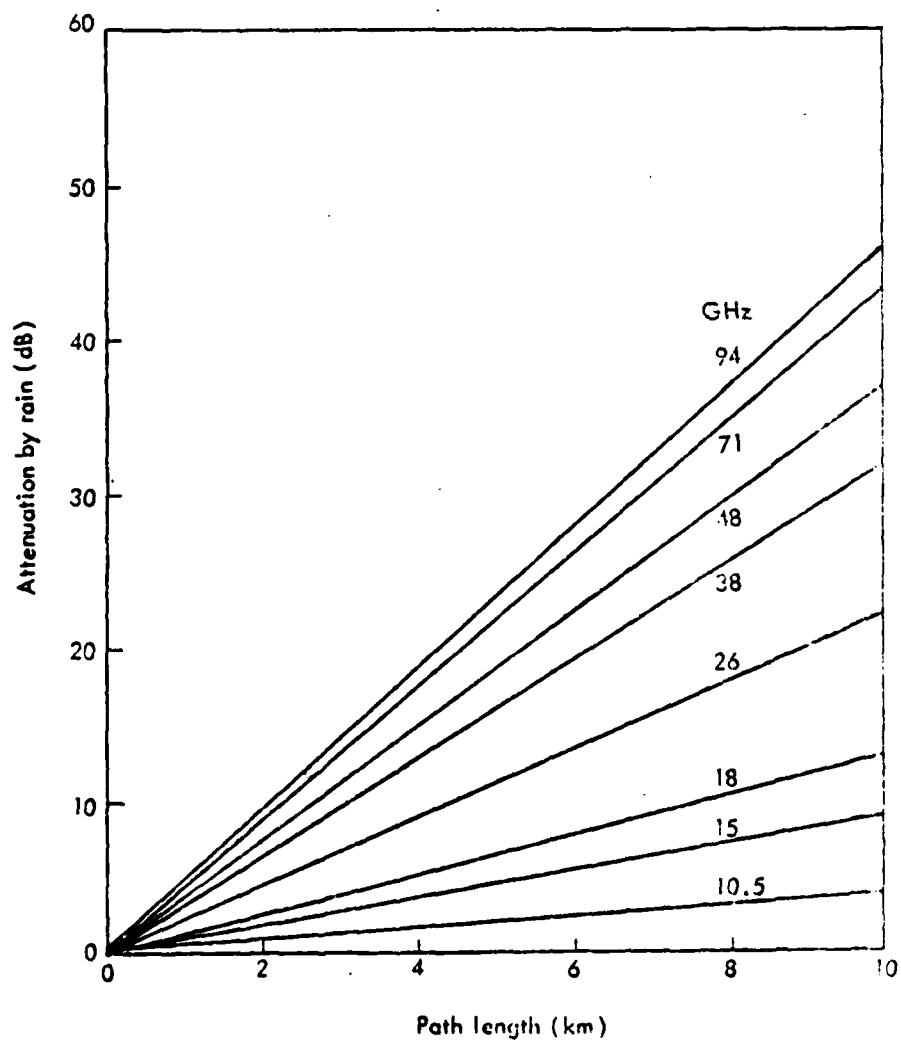


Figure 6a. Attenuation by rain as a function of path length for 99.9% reliability [Ref. 9].

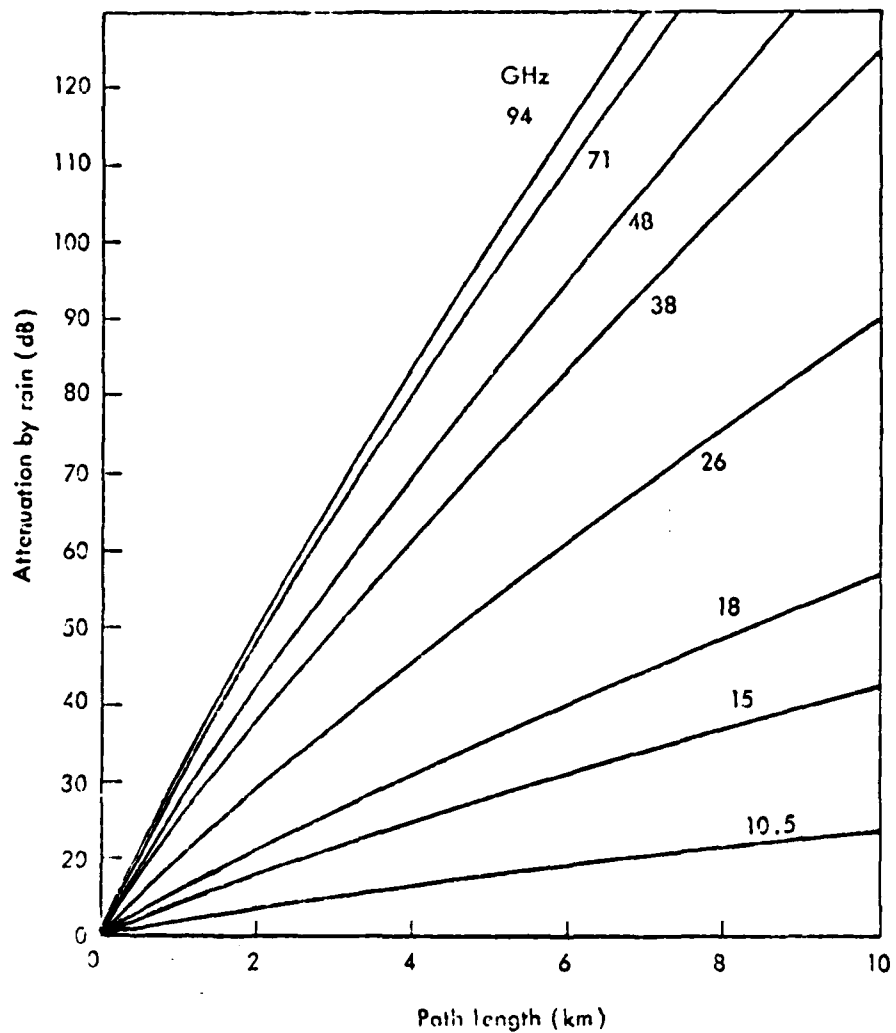


Figure 6b. Attenuation by rain as a function of path length for 99.99% reliability [Ref. 9].

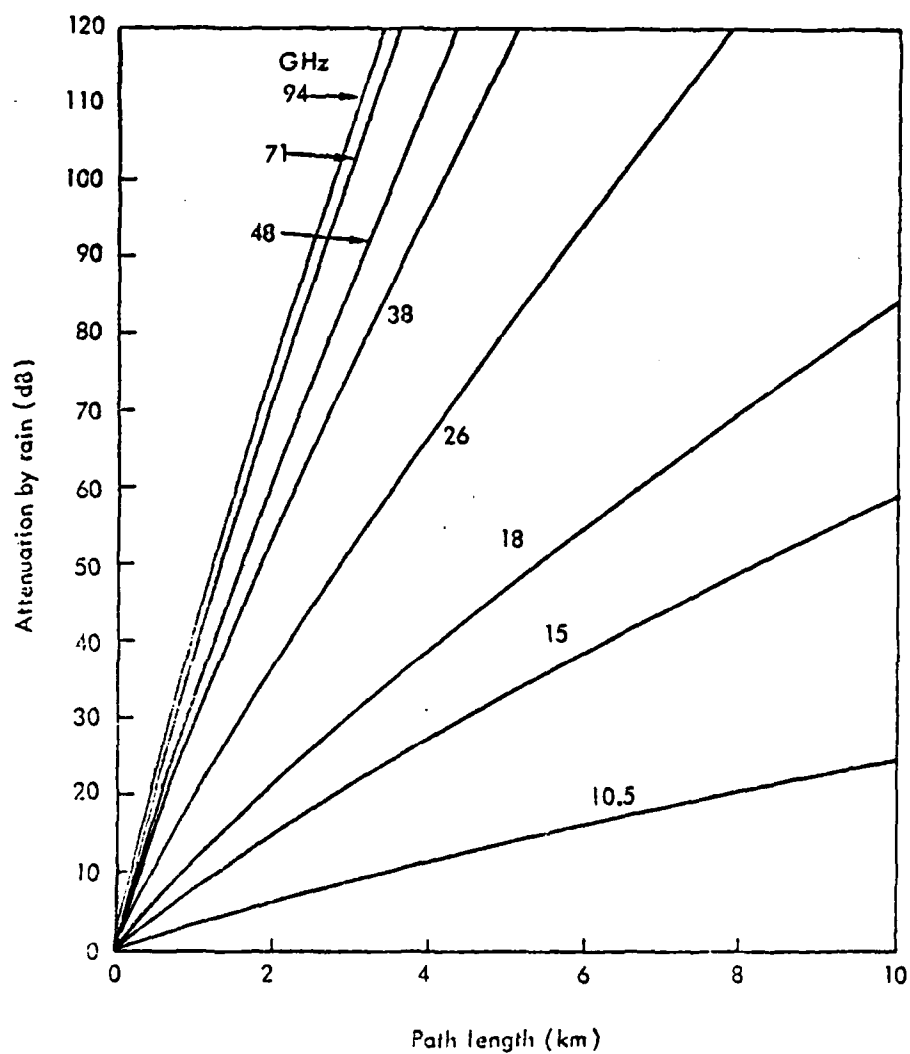


Figure 6c. Attenuation by rain as a function of path length for 99.999% reliability [Ref. 9].

dependence of this attenuation on path length can be represented by curves such as those of Figure 7 [Ref. 9]. These curves can be used together with curves from Figures 6 to estimate the performance of millimeter-wave communications links operating through the atmosphere and in the presence of rainfall.

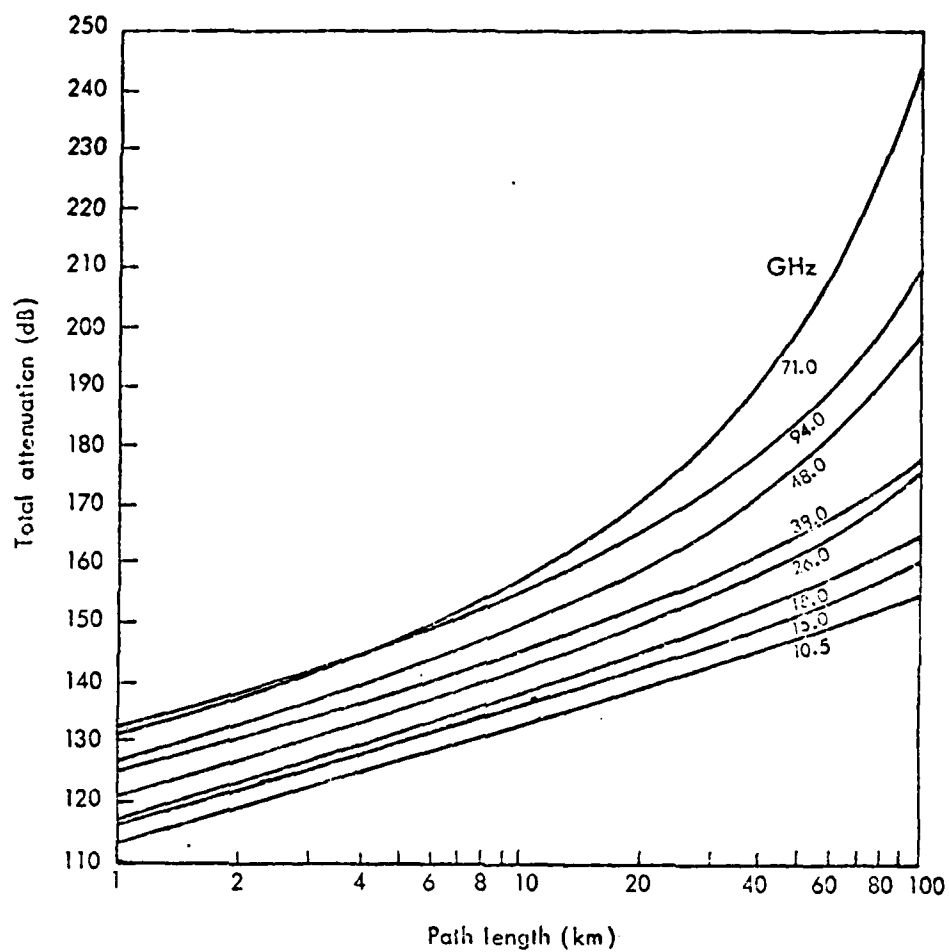


Figure 7. Total attenuation through a clear atmosphere at sea level [Ref. 9].

III. THE STAR TERRAIN MODEL

The STAR (Simulation of Tactical Alternative Responses) ground-air combat model is a computer simulation program developed at the Naval Postgraduate School during 1978-1979. STAR is written in SIMSCRIPT II.5 simulation language. The idea for the STAR terrain representation -- called parametric terrain -- was originally proposed by Major Chris Needels in his 1976 Master of Science Thesis at the Naval Postgraduate School [Ref. 10]. The model as used in this report is the work of Professor James K. Hartman [Ref. 2]. The subroutines that were developed specifically to analyze the MAB radio links are outlined in detail in Appendix A.

The basic function which any terrain representation must provide for a high-resolution combat simulation is, "for any x, y map coordinates on the battlefield, compute the elevation z of the terrain, and the height h of the forest if one exists." The elevation z is generally called the macro terrain.

The parametric terrain model used in STAR involves storing a function $f(x, y)$. The process of determining z for a given x, y then reduces to computing the function $z = f(x, y)$. Parametric terrain has the advantage that the function f can be stored using only a modest amount of computer storage. In addition, the parametric terrain is inherently continuous, so no interpolation is required for smoothing.

The parametric terrain model proposed by Needels represents terrain by modeling individual hill masses. Each hill mass is represented mathematically as a scaled bivariate normal probability density function. This gives a characteristic elliptic bell-shaped hill mass cross section as shown in Figure 8. By varying the parameters, a wide variety of different hill locations, sizes, and shapes can be modeled. By superposing several hill masses, the contour map can be fitted to real map contours remarkably well by using the maximum macro terrain.

In addition to the macro terrain, another factor that influences line-of-sight computations in the STAR model is the presence of forests. Forests in the model are represented by cover ellipses on the ground. Each ellipse has a tree height associated with it, and the forest is thus an elliptical "cylinder" with that fixed height above the ground. Actual forests with non-elliptical shapes and non-constant heights can be approximated by combining several overlapping ellipses. The tree height at a given point x,y is the maximum tree height for all the forest ellipses containing the point x,y .

Figures 11, 12, and 13 show the terrain model on which all computations have been performed. They are a 10 by 30 km section of terrain near the town of Hunfeld, West Germany. Hunfeld is located near the East German border in the Fulda Gap region of central West Germany.

The map symbols that resemble capital Y's represent forested areas. The contour lines are drawn every 10 meters with

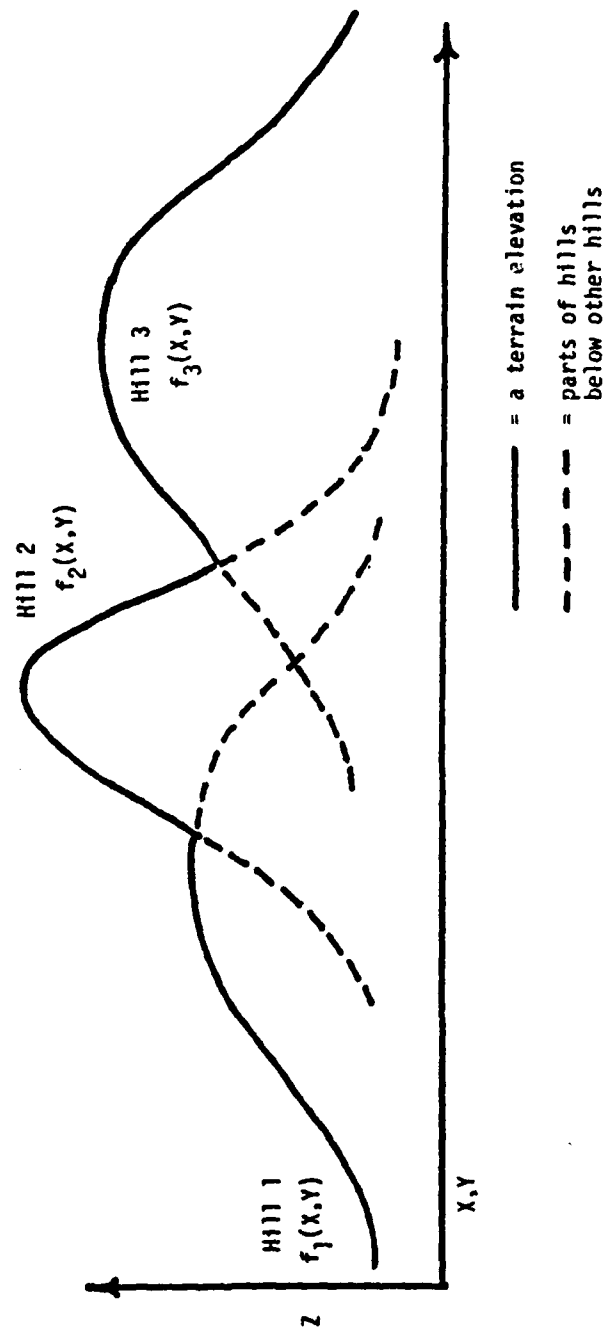


Figure 8. MACRO terrain is the maximum over all the hill masses.

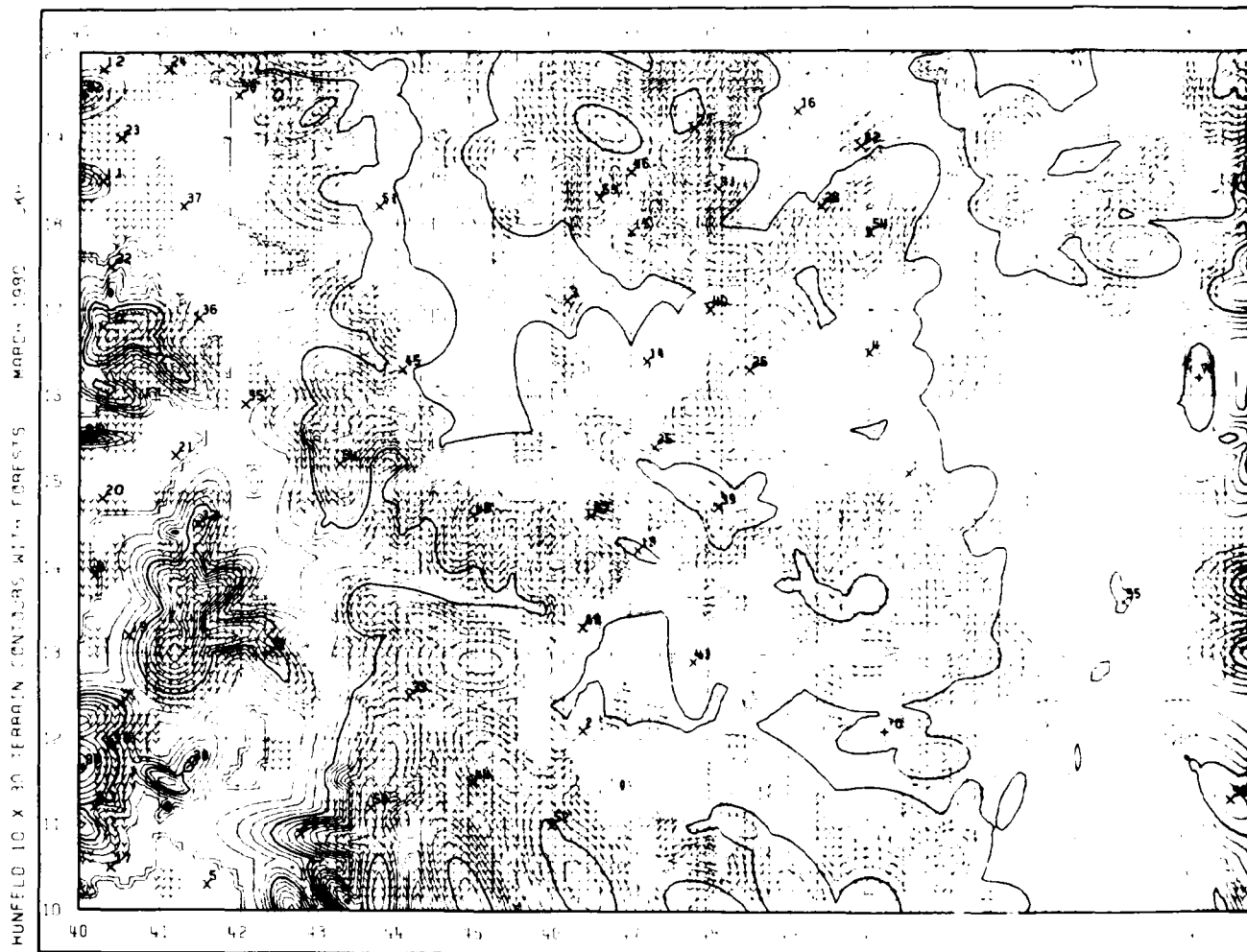
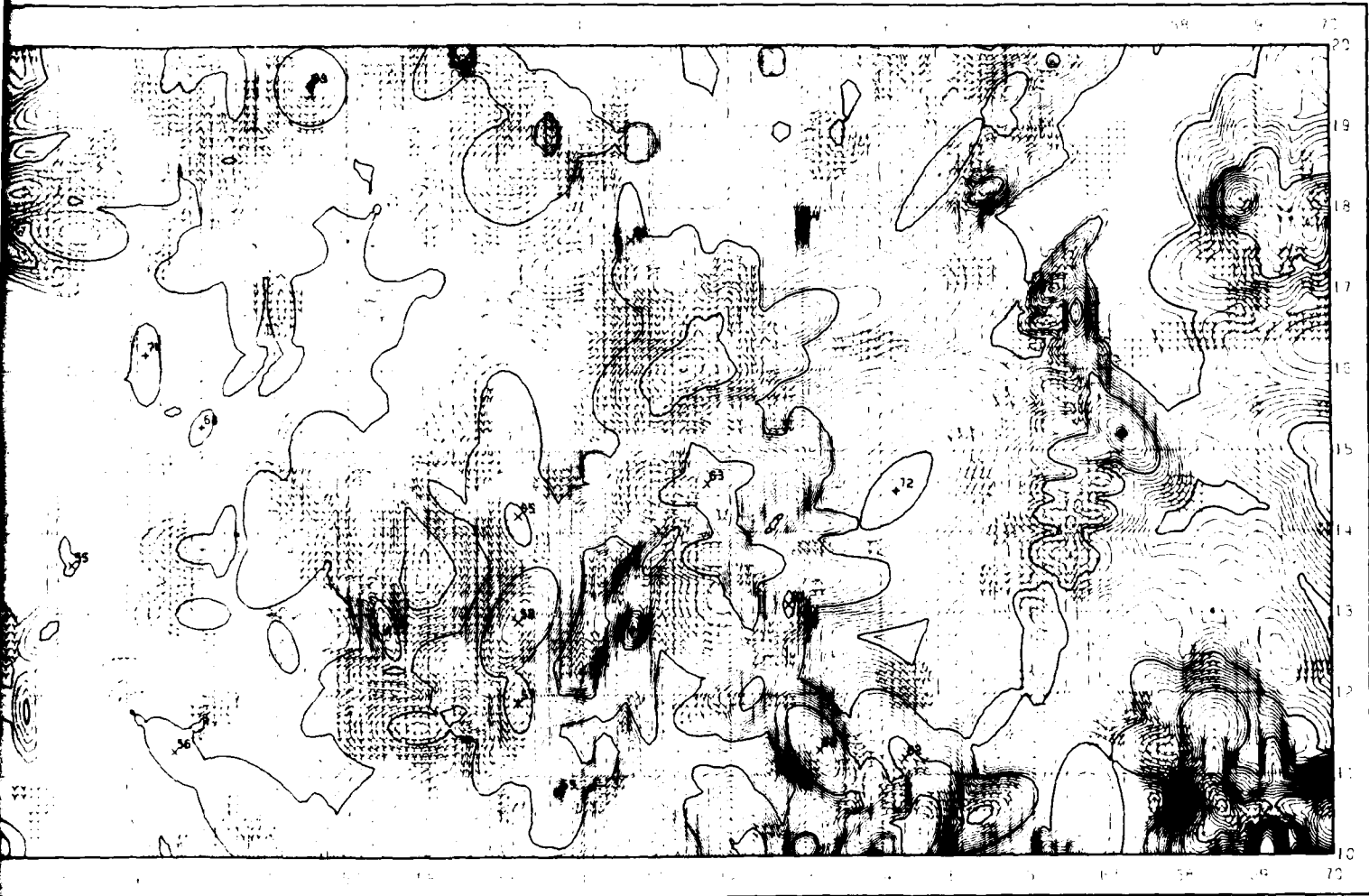


Figure 11. MAB Unit locations for the first set of data points.



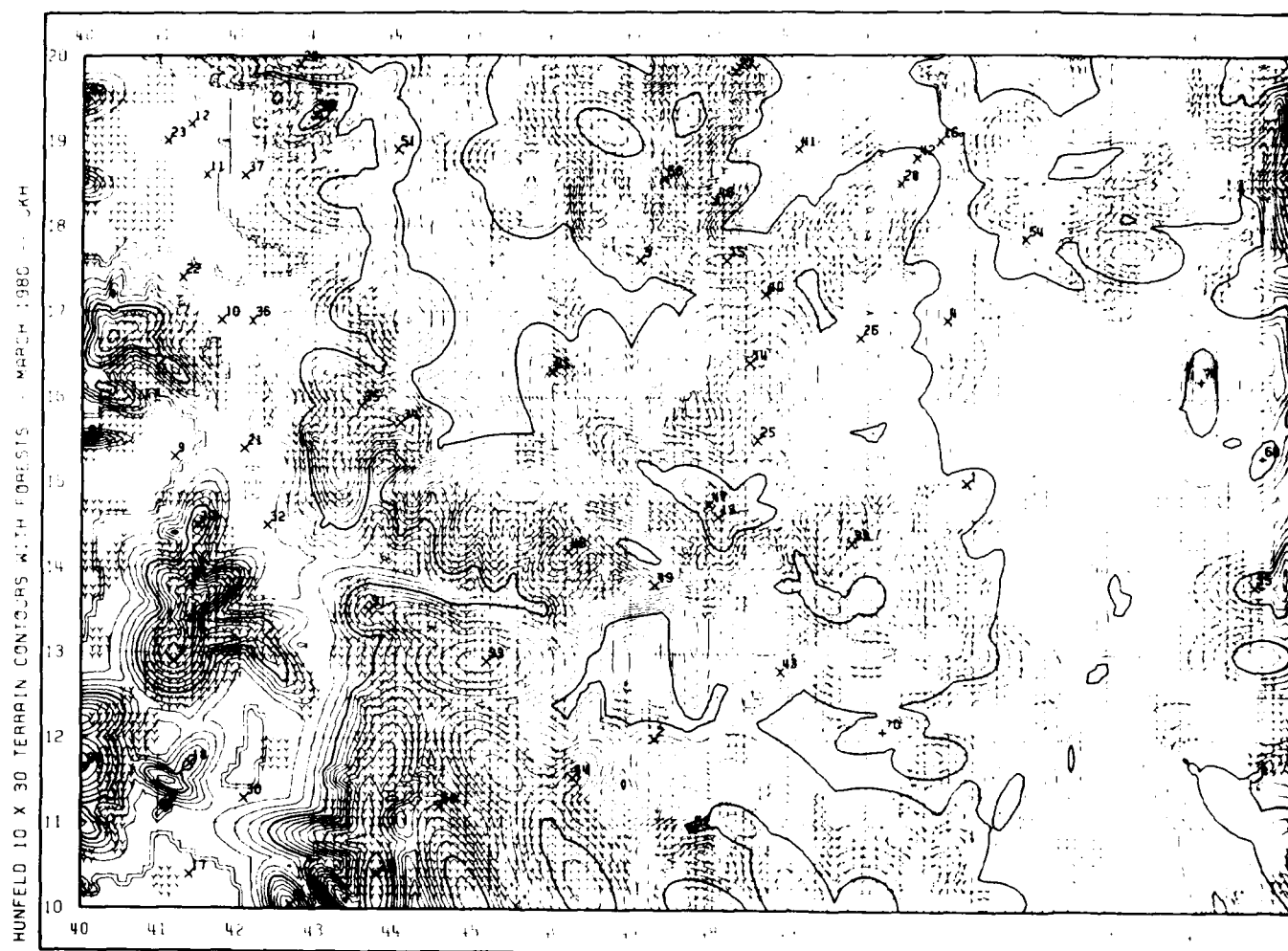
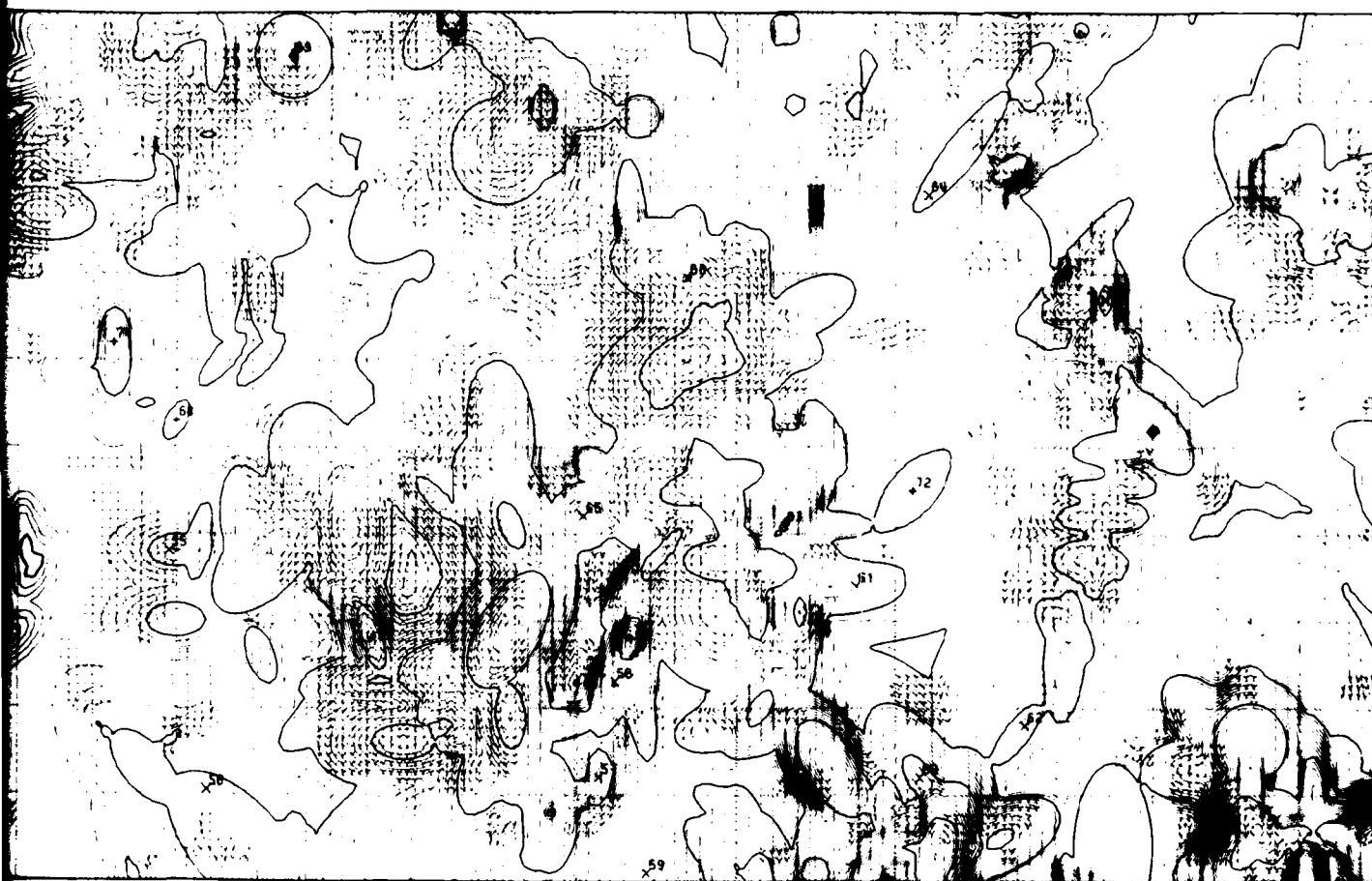


Figure 12. MAB Unit locations for the second set of data points.



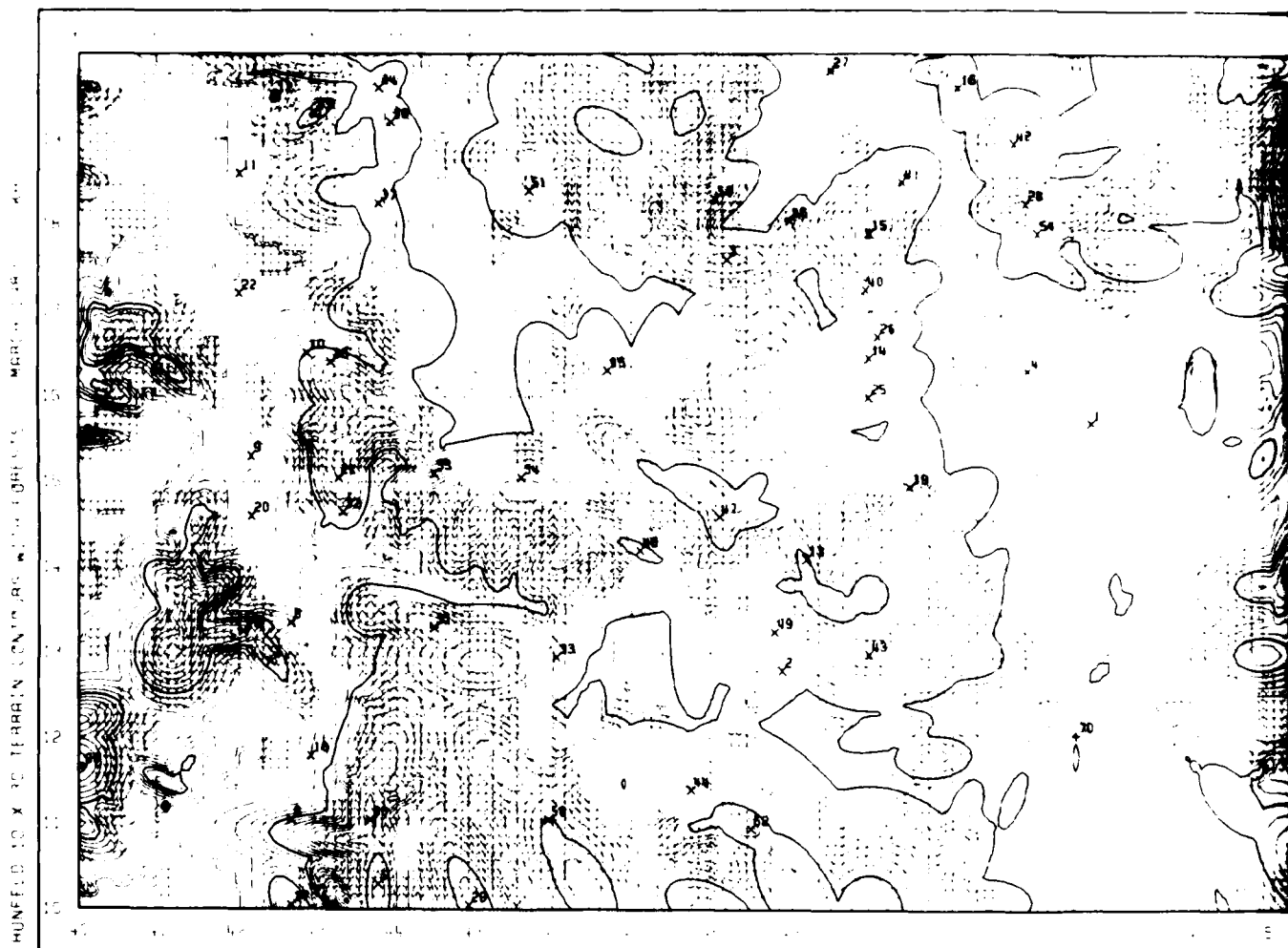
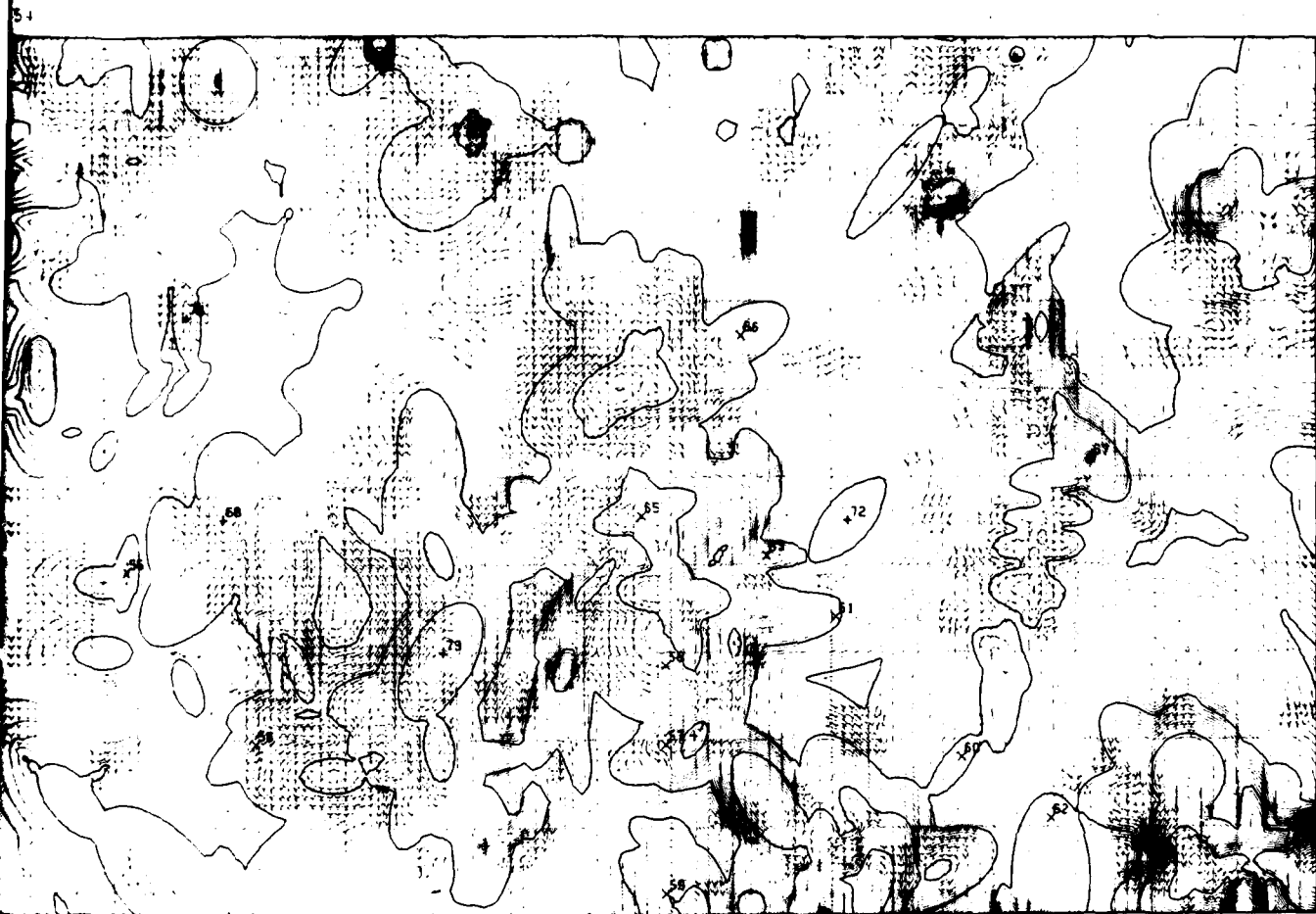


Figure 13. MAB Unit locations for the third set of data points.



100-meter contour lines accented. Grid lines in both the horizontal and vertical directions are every 1000 meters. The valley located at 41000 19000 has an elevation of 230 meters above sea level. The other two major valleys, located at 53000 15000 and 76000 19000, have elevations of 250 and 280 meters, respectively. The terrain represented in the model is highly forested and very irregular and is representative of many areas of the world.

The use of the STAR model has been simplified by the subroutine RES.TERR developed by Professor Hartman. This subroutine is called by the main program first and is set up to dynamically reserve and dimension the various arrays so that core requirements are minimized. The input to RES.TERR is parameter information on the hill masses and forest ellipses. This parameter information is currently stored on disk.

To use the model all that is needed is to read in two ten-digit grid coordinates and assign them to the variables XA.LS, YA.LS, XB.LS and YB.LS. The variable XA.LS is the five-digit x coordinate of the first point A and YA.LS is the five-digit y coordinate. Now the macro terrain elevation can be found by calling subroutine ELEV, or the height of the trees at point A can be found by calling the subroutine TREES.

To calculate the line-of-sight (LOS), the following information must be available for both points A and B:

- (1) The x and y coordinates on the battlefield expressed as XA.LS and YA.LS.

- (2) The macro terrain elevation (TMACA.LS) computed from the ELEV subroutine.
- (3) A micro terrain offset (TMICA.LS) of + or - from the macro terrain. The offset is used to place some of the antennas above the surrounding forest.
- (4) The last piece of information that is needed is the size of the antenna (SIZE.LS), which is specified as three meters in this report.

Now the LOS subroutine can be called which will return the percent visible of antenna B, i.e., the fraction of antenna B that can be seen from the top of antenna A. This is depicted in Figure 9 where point A's antenna is mounted on top of the radio and point B's antenna is mast mounted.

The preceding paragraphs provide an overview of Professor Hartman's report. Anyone wishing to use the STAR model should become familiar with Ref. 2 before proceeding.

Four routines were written as part of this thesis specifically to analyze the MAB's radio links. They are MAIN, REPORT.PRINT, LPI and FOREST. The purpose of the MAIN program is to determine if a radio transmission path exists between points A and B, at the specified high frequency, at the specified low frequency, or if no path exists at all. The program defines a low frequency (FREQ.L) and high frequency (FREQ.H). The maximum allowable loss between points A and B, as given in Chapter I, is then specified. The line-of-sight is specified as being from A to B (LATOB.LS=1).

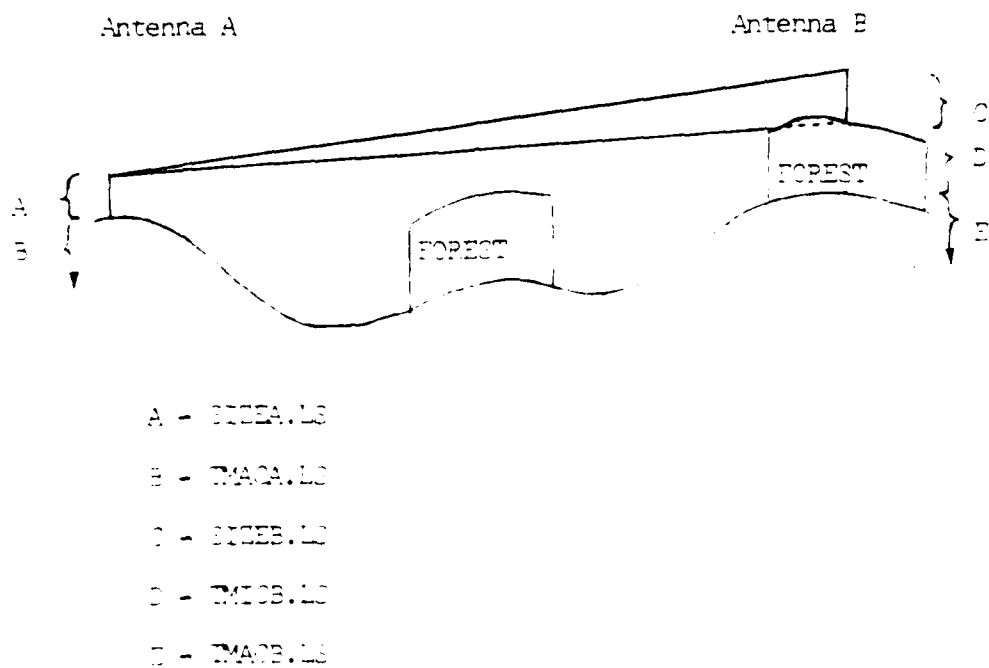


Figure 9. A Line-of-Sight Exists if the Top of Antenna A Can See the Top of Antenna B.

All of the points to be analyzed are read in at once with the x coordinate first followed by the y coordinate, the node number, the printing symbol code, and the "Mobility Factor."² Then each pair of points is analyzed. Since all pairs of points make up a symmetric matrix, only the upper half of the matrix is analyzed. The offset (TMICA.LS) is initially set to zero, but it can be changed to the tree height if the mobility factor is "1."

The macro terrain elevation is found along with the tree height at each pair of points. Antenna heights are also computed and some redefining is done in preparation for the first call of the LOS subroutine. The first call of LOS is done over a terrain model that is void of trees. If a line-of-sight exists over the ground then the forest ellipses are reinstated and another line-of-sight is shot. The loss for free-space and the loss associated with Bullington's equation are both computed and the greater loss is used. If a line-of-sight exists over the ground but not over the trees, then the subroutine FOREST is called. The output of FOREST is the amount of forests that lie between points A and B.

Now the total losses between A and B can be computed, since it is a function of the distance, frequency and amount of trees that intersect the line-of-sight. For each link, analysis is

²The Mobility Factor describes the unit's ability to erect a large antenna and is described in Chapter III.

done to determine if the link can operate at the high frequency, and then at the low frequency. For links that exist, the fading margin is given as the number of dBs above the required 11 dB, for a required $P_e = 10^{-6}$. If neither frequency produces a favorable margin, then the link is discarded and another pair of points (A,B) is looked at. For links that do exist, the distance between the two points is stored in matrix form for both (A,B) and (B,A). The distance is stored as a truncated number if the link is being carried by the higher frequency, and point one is added to the distance if it is being carried by the lower frequency.

Next, the matrix of distance is sorted and the five nearest neighbors to each point are displayed in table form. The nearest neighbor would appear in the table as 10 if it was accessible at the higher frequency and 11 if it was accessible by the lower frequency. Other valid entries in the table are 20, 21, 30, 31, 40, 41, 50, and 51.

The subroutine REPORT.PRINT prints out the contents of the matrix that contains the listing of the five nearest neighbors. It prints out the matrix in two separate formats. The first format is larger and easier to work with, while the second format is compatible with an 8-1/2" x 11" piece of paper.

The subroutine LPI determines the signal-to-noise ratio that an enemy listening post would receive if it used an antenna with a gain of 5.8 dB. This subroutine follows the

same procedures as the MAIN program except its output is the SNR and not the fading margin that the main program calculates.

The FOREST subroutine was designed to calculate the amount of forests that lie between points A and B. The routine checks the heights of the trees every 1/100 of the distance between the two end points. Every time that the height of the trees intersects the line-of-sight, it adds one more percent to its counter. When the routine is completed, it has a number that expresses the percent of the distance that the tree height exceeded the line-of-sight. This percent is returned to the main program where the depth of the forest in meters is determined by multiplication by the distance.

IV. UNIT LOCATIONS

On the battlefield are positioned sixty-six units that comprise the Marine Amphibious Brigade (MAB). There is also one point that represents an external connection with higher headquarters plus seven repeater stations. In addition to the one special point, any node near the boundary of the MAB could be used as an external connection point. These seventy-four points and their relative positions were furnished by Ref. 11. In their original form they had a frontage of 16 km and a depth of 26 km. Position number 1 was the Regimental Headquarters and also grid center for the map. All other positions were given coordinates relative to the Regimental Headquarters as shown in Table 1.

Since the STAR terrain model map of Hunfeld, West Germany, was only 10 km wide by 30 km in depth, there existed a need to decrease the frontage of the MAB. Each unit's lateral distance from grid center was decreased by $\frac{5}{8}$ and it was given coordinates that made it compatible with the Hunfeld map. Table 2 lists the new coordinates and Figure 10 shows the relative positions of all points on the map.

The reduced frontage of the MAB does make connectivity easier on this terrain model because of the reduction in the average amount of trees between nodes. Whether or not this frontage is realistic is a question that cannot be answered without knowledge of the density of the enemy units. It is

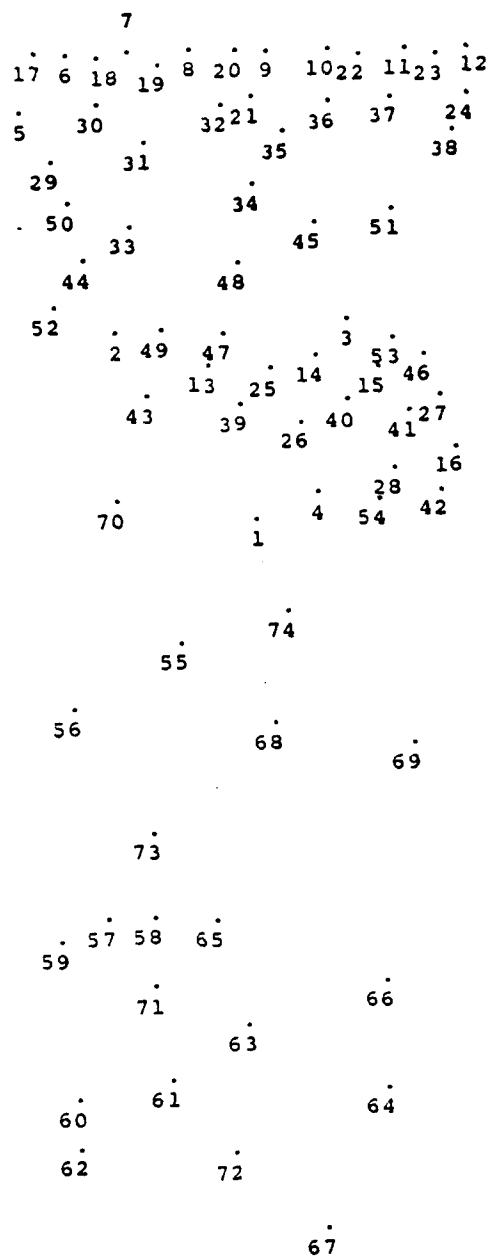


Figure 10. MAB Unit locations for the first set of data points, nodes.

worth noting that the 16 km front was for a situation in southern California where the lack of trees would have made the connectivity easier.

The points went through another transition when they were actually placed on the map. A term was used, called "antenna sight selection," whereby each antenna was placed within 200 - 300 meters from the unit's location in an area that was conducive to radio frequency communications. This kept the antennas out of the bottom of ravines and also prevented enemy direction finding systems from pinpointing unit locations, since the antenna and unit were not colocated.

A list of final coordinates is given as Table 3 along with their "Mobility Factor." Each unit has been given a mobility factor of either one or zero. If a unit has a mobility factor of zero, then it is assumed to be in almost constant motion and unable to erect an external antenna. Its antenna is defined as being three meters above the ground. If a unit has a mobility factor of one, then it is using an external antenna that is either three meters above the ground when the unit is in a clearing, or three meters above the forest when the unit is in a forest. Mobility factors of one have been given to units of battalion size and larger.

After all the units of the MAB were analyzed for connectivity in the first set of positions, described in Table 3 and Figure 11, they were moved back from the FEBA. The FEBA is near the grid line 40000. They were again analyzed in the second set of positions, described in Table 4 and

Figure 12, and moved again. The final set of positions used is described in Table 5 and Figure 13. Each time that the set of units was moved, their relative positions to one another were maintained. This was accomplished by requiring each unit to move backward into the next adjoining grid square. The units were permitted, however, to find an optimum position in that adjoining grid square. The movement of the repeaters, nodes 68 through 74, were not as strictly controlled as the units. When the units were moved into their second set of positions, the repeaters were not moved. The repeater positions were changed when the units were moved into the third set of positions. They were positioned on key terrain in positions relative to where they were at the start of the problem. Thus, their role of bridging the gap between distant units was again reinstated.

Three enemy listening posts were established along the FEBA and they were used to analyze what units could be intercepted. Analysis of RF interception is discussed in Chapter V.

Table 1. Marine Amphibious Brigade (MAB) Unit locations, all points relative to the infantry regiment.

NODE	NAME	LOCATION
1	Inf Regt	000 000
2	Inf Bn	-040 040
3	Inf Bn	040 040
4	Inf Bn	030 003
5	TACP 1	-074 084
6	TACP 2	-063 096
7	TACP 3	-040 097
8	TACP 4	-046 097
9	TACP 5	007 096
10	TACP 6	027 097
11	TACP 7	051 097
12	TACP 8	073 094
13	TACP 9	-009 027
14 :	TACP 10	024 027
15	TACP 11	046 028
16	TACP 12	062 010
17	FAAD 1	-074 095
18	FAAD 2	-045 097
19	FAAD 3	-028 092
20	FAAD 4	-006 096
21	FAAD 5	005 089
22	FAAD 6	034 096
23	FAAD 7	060 094

NODE	NAME	LOCATION
24	FAAD 8	074 086
25	FAAD 9	004 027
26	FAAD 10	025 018
27	FAAD 11	061 023
28	FAAD 12	052 007
29	Inf Co A	-073 069
30	Inf Co B	-055 083
31	Inf Co C	-029 077
32	Inf Co D	-008 081
33	Engr 1	-025 060
34	Engr 2	019 063
35	Inf Co E	011 079
36	Inf Co F	030 083
37	Inf Co G	050 083
38	Inf Co H	070 077
39	Inf Co I	-003 021
40	Inf Co K	032 023
41	Inf Co L	050 019
42	Inf Co M	059 003
43	Arty Bn	-026 022
44	Arty Bty A	-047 051
45	Arty Bty B	031 057
46	Arty Bty C	056 032

NODE	NAME	LOCATION
47	Arty Bty D	-003 037
48	LAAM	-006 051
49	Armor Bn	-018 032
50	Armor Co A	-041 062
51	Armor Co B	046 062
52	Mortar 1	-049 037
53	Mortar 2	050 039
54	Mortar 3	039 005
55	MAB (Fwd)	-006 -027
56	Helo Sqdn	-039 -037
57	MAG	-034 -085
58	TACC	-027 -091
59	Sqdn (VMF)	-047 -093
60	Sqdn (VMA)	-068 -133
61	TAOC	-043 -134
62	MATCU	-063 -143
63	MAB (Rear)	000 -114
64	LSG	044 -122
65	LSU 1	-012 -086
66	LSU 2	027 -093
67	External	017 -157
68	Repeater 1	-043 079
69	Repeater 2	-026 000

NODE	NAME	LOCATION
70	Repeater 3	-019 -054
71	Repeater 4	017 -055
72	Repeater 5	027 -110
73	Repeater 6	-024 -060
74	Repeater 7	019 -014

Table 2. MAB Unit locations, first set of data points

UNIT	NAME	LOCATION
1	Inf Regt	50300 15000
2	Inf Bn	46100 12200
3	Inf Bn	46200 17100
4	Inf Bn	50000 16500
5	TACP 1	41600 10300
6	TACP 2	40200 11200
7	TACP 3	40500 12400
8	TACP 4	40200 13900
9	TACP 5	40200 15700
10	TACP 6	40300 16800
11	TACP 7	40300 18500
12	TACP 8	40300 19800
13	TACP 9	47400 14000
14	TACP 10	47500 16500
15	TACP 11	47300 17100
16	TACP 12	49100 19300
17	FAAD 1	40400 10500
18	FAAD 2	40500 12000
19	FAAD 3	40600 13200
20	FAAD 4	40300 14800
21	FAAD 5	41200 15300
22	FAAD 6	40400 17500
23	FAAD 7	40500 19000

27	FAAD 7	41100 19800
28	FAAD 8	47300 15400
29	FAAD 10	48500 16300
30	FAAD 11	47800 19100
31	FAAD 12	49400 18200
32	Inf Co A	42800 10800
33	Inf Co B	41500 11500
34	Inf Co C	42400 12800
35	Inf Co D	41800 14300
36	Engr 1	44000 12500
37	Engr 2	43800 14900
38	Inf Co E	42100 15900
39	Inf Co F	41500 16900
40	Inf Co G	41300 18200
41	Inf Co H	42000 19500
42	Inf Co I	48100 14700
43	Inf Co K	48000 17000
44	Inf Co L	48200 18000
45	Inf Co M	49100 18900
46	Arty Bn	48000 12400
47	Arty Bty A	45000 11500
48	Arty Bty B	44400 16200
49	Arty Bty C	47000 18600

45	Artillery	46500	14600
46	ASPH	45100	14400
47	Armored	46900	13200
48	Armored A	44000	11200
49	Armored B	43900	17700
50	Mortar 1	46500	11200
51	Mortar 2	46300	18000
52	Mortar 3	49700	17400
53	MAB (Fwd)	53000	14500
54	Helicopter	54000	11100
55	MAG	5-000	11600
56	TACC	59500	12400
57	Sqdn (VMF)	59700	10300
58	Sqdn (VMA)	63600	10500
59	TACC	63500	13000
60	MATCU	64500	11300
61	MAB (Rear)	61800	15000
62	LSG	62300	19400
63	LSU 1	59000	13900
64	LSU 2	59700	17700
65	External	66000	17000
66	Repeater 1	55000	15000
67	Repeater 2	56500	19500

50000	12500
60500	12500
64000	1450
67000	12500
6400	16000

4. The first iteration, the first set of data points with antenna
position, elevation, and visibility data.

1	50500	15100
2	46400	12100
3	46200	17100
4	50000	16500
5	41600	10300
6	40200	11200
7	40500	12400
8	40200	13900
9	40200	15500
10	40300	16600
11	40300	18500
12	40300	19800
13	47100	14200
14	47200	16400
15	47300	17900
16	49100	19300
17	40400	10500
18	40400	11900
19	40600	13200
20	40300	14800
21	41200	15300
22	40400	17500
23	40500	19000

LINE	NAME	MOBILITY	QUANTITY
24	FAAD 7	0	41100 19800
25	FAAD 8	0	47300 15400
26	FAAD 10	0	48500 16300
27	FAAD 11	0	47800 19100
28	FAAD 12	0	49400 18200
29	Inf Co A	0	42800 10900
30	Inf Co B	0	41400 11700
31	Inf Co C	0	42400 13000
32	Inf Co D	0	41500 14500
33	Engr 1	1	44200 12500
34	Engr 2	1	43300 15200
35	Inf Co E	0	42100 15900
36	Inf Co F	0	41500 16900
37	Inf Co G	0	41300 18200
38	Inf Co H	0	42000 19500
39	Inf Co I	0	48100 14700
40	Inf Co K	0	48000 17000
41	Inf Co L	0	48100 18400
42	Inf Co M	0	49900 18900
43	Arty Bn	1	47800 12900
44	Arty Bty A	1	45000 11500
45	Arty Bty B	1	44100 16300
46	Arty Bty C	1	47000 18600

LINE	NAME	AVAILABILITY	LOCATION
47	Arty Coy B	1	46500 14600
48	LAAM	1	45000 14600
49	Armor En	1	46400 13300
50	Armor Co A	1	43700 11200
51	Armor Co B	1	43800 18200
52	Mortar 1	1	46000 11000
53	Mortar 2	1	46600 18300
54	Mortar 3	1	50000 17900
55	MAB (Fwd)	1	53200 13600
56	Helo Sqdn	1	54600 11300
57	MAG	1	59200 11900
58	TACC	1	59200 12900
59	Sqdn (VMF)	1	59700 10800
60	Sqdn (VMA)	1	63200 11300
61	TAOC	1	62800 13100
62	MATCU	1	64300 11200
63	MAB (Rear)	1	61700 14600
64	LSG	1	63000 17800
65	LSU 1	1	59200 14200
66	LSU 2	1	60700 17600
67	External	1	66000 16600
68	Repeater 1	1	55000 15300
69	Repeater 2	1	56500 19500

NODE	NAME	MOBILITY	LOCATION
70	Repeater 3	1	50200 12100
71	Repeater 4	1	60700 12800
72	Repeater 5	1	64200 14500
73	Repeater 6	1	57500 12800
74	Repeater 7	1	54190 16200

Table 4. MAB Unit locations, the second set of data points with antenna sight selection, and mobility factor.

UNIT	NAME	MOBILITY	LOCATION
1	Inf Regt	1	51250 15000
2	Inf Bn	1	47300 12000
3	Inf Bn	1	47100 17600
4	Inf Bn	1	51000 16900
5	TACP 1	0	42700 10050
6	TACP 2	0	41100 11200
7	TACP 3	0	41200 12900
8	TACP 4	0	41400 13800
9	TACP 5	0	41200 15300
10	TACP 6	0	41800 16900
11	TACP 7	0	41600 18600
12	TACP 8	0	41400 19200
13	TACP 9	0	48100 14600
14	TACP 10	0	48500 16400
15	TACP 11	0	48200 17600
16	TACP 12	0	50900 19000
17	FAAD 1	0	41400 10400
18	FAAD 2	0	41400 11700
19	FAAD 3	0	41200 13000
20	FAAD 4	0	41500 14500
21	FAAD 5	0	42100 15400
22	FAAD 6	0	41300 17400
23	FAAD 7	0	41100 19000

FILE	NAME	MOBILITY	LOCATION
24	FAAD 8	0	42300 19900
25	FAAD 9	0	48600 15500
26	FAAD 10	0	49900 16700
27	FAAD 11	0	48300 19800
28	FAAD 12	0	50400 18500
29	Inf Co A	0	43800 10400
30	Inf Co B	0	42100 11300
31	Inf Co C	0	43700 13500
32	Inf Co D	0	42400 14500
33	Engr 1	1	45200 12900
34	Engr 2	1	44100 15700
35	Inf Co E	0	43600 15900
36	Inf Co F	0	42200 16900
37	Inf Co G	0	42100 18600
38	Inf Co H	0	43000 19300
39	Inf Co I	0	49800 14300
40	Inf Co K	0	48700 17200
41	Inf Co L	0	49100 18900
42	Inf Co M	0	50600 18800
43	Arty Bn	1	48900 12800
44	Arty Bty A	1	46250 11550
45	Arty Bty B	1	45990 16300
46	Arty Bty C	1	48050 18300

LINE	NAME	MOBILITY	LOCATION
47	Arty Bty D	1	47990 14750
48	LAAM	1	46200 14200
49	Armor Bn	1	47300 13800
50	Armor Co A	1	44600 11200
51	Armor Co B	1	44050 18900
52	Mortar 1	1	47800 10950
53	Mortar 2	1	47400 18550
54	Mortar 3	1	51990 17850
55	MAB (Fwd)	1	54900 13800
56	Helo Sqdn	1	55400 11050
57	MAG	1	60300 11200
58	TACC	1	60700 12800
59	Sqdn (VMF)	1	60900 10100
60	Sqdn (VMA)	1	64300 11200
61	TAOC	1	63500 13400
62	MATCU	1	65600 11800
63	MAB (Rear)	1	62600 14100
64	LSG	1	64400 17900
65	LSU 1	1	60100 14200
66	LSU 2	1	61400 16950
67	External	1	66600 16700
68	Repeater 1	1	55000 15300
69	Repeater 2	1	56500 19500

DATE	NAME	MOBILITY	LOCATION
70	Repeater 3	1	50200 12100
71	Repeater 4	1	60700 12800
72	Repeater 5	1	64200 14500
73	Repeater 6	1	57500 12800
74	Repeater 7	1	54190 16200

Table 5. MAB Unit locations, the third set of data points with antenna sight selection, and mobility factor.

Unit	Location	Mobility	Lat	Long
1	Inf Bgt	1	52800	15700
2	Inf Bn	1	48900	12800
3	Inf Bn	1	48200	17600
4	Inf Bn	1	51990	16300
5	TACP 1	0	43800	10300
6	TACP 2	0	42700	11050
7	TACP 3	0	42450	12900
8	TACP 4	0	42700	13350
9	TACP 5	0	42200	15300
10	TACP 6	0	42900	16500
11	TACP 7	0	42050	18600
12	TACP 8	0	42500	19500
13	TACP 9	0	49200	14100
14	TACP 10	0	49990	16450
15	TACP 11	0	49990	17900
16	TACP 12	0	51100	19600
17	FAAD 1	0	42700	10050
18	FAAD 2	0	42950	11800
19	FAAD 3	0	42100	13250
20	FAAD 4	0	42200	14600
21	FAAD 5	0	43300	15050
22	FAAD 6	0	42050	17200
23	FAAD 7	0	42990	19300

LINE	NAME	QUANTITY	LOCATION
24	FAAD 8	0	43800 19600
25	FAAD 9	0	49990 15990
26	FAAD 10	0	50100 16700
27	FAAD 11	0	49500 19800
28	FAAD 12	0	51950 18250
29	Inf Co A	0	44950 10050
30	Inf Co B	0	43700 11050
31	Inf Co C	0	44500 13300
32	Inf Co D	0	43350 14650
33	Engr 1	1	46050 12950
34	Engr 2	1	45600 15050
35	Inf Co E	0	44500 15100
36	Inf Co F	0	43200 16400
37	Inf Co G	0	43800 18250
38	Inf Co H	0	43950 19200
39	Inf Co I	0	50500 14950
40	Inf Co K	0	49950 17250
41	Inf Co L	0	50400 18500
42	Inf Co M	0	51800 18950
43	Arty Bn	1	49990 12990
44	Arty Bty A	1	47750 11400
45	Arty Bty B	1	46700 16300
46	Arty Bty C	1	48990 18050

LINE	NAME	QUANTITY	LOCATION
47	Army sty B	1	48100 14600
48	LAAM	1	47100 14200
49	Armor En	1	48800 13250
50	Armor Co A	1	45950 11050
51	Armor Co B	1	45700 18400
52	Mortar 1	1	48500 10950
53	Mortar 2	1	48050 18300
54	Mortar 3	1	52100 17900
55	MAB (Fwd)	1	55300 13900
56	Helo Sqdn	1	56950 11950
57	MAG	1	61950 11950
58	TACC	1	61950 12850
59	Sqdn (VMF)	1	61950 10250
60	Sqdn (VMA)	1	65600 11800
61	TACC	1	64050 13400
62	MATCU	1	66700 11100
63	MAB (Rear)	1	63200 14100
64	LSG	1	65100 17900
65	LSU 1	1	61650 14550
66	LSU 2	1	62900 16600
67	External	1	67200 15200
68	Repeater 1	1	56550 14500
69	Repeater 2	1	59600 18900

CALL	NAME	QUANTITY	LOCATION
70	Repeater 3	1	52600 12050
71	Repeater 4	1	62300 12050
72	Repeater 5	1	64200 14500
73	Repeater 6	1	59250 12990
74	Repeater 7	1	56100 16800

V. CONNECTIVITY

A. GENERAL

The operational characteristics of the radio frequency band have a major impact on the connectivity of the MAB's packet radio system. The lowest and highest frequencies which can be used for a packet radio system are determined primarily by considerations of bandwidth and propagation link loss. Practical, cost-effective radio equipment is difficult to find if the ratio of RF bandwidth to RF center frequency is much larger than about 15%. With a 16 kbs data rate and a 32 kHz RF bandwidth, this puts the lower bound of RF center frequencies at about 200 kHz. With pseudonoise modulation, the lowest usable frequency will be multiplied by the "spreading factor."

The upper limits of usable frequencies are determined by total link losses. As the operating frequency rises above about 10 GHz, absorptive losses due to the atmosphere, rain, and foliage penetration rapidly increase, and the resulting range is reduced accordingly.

B. SHF CONNECTIVITY

For a center frequency of 40 GHz and a percent reliability of 99.9%, Figures 6a and 7 give the maximum single hop distance such that the path loss does not exceed 141 dB as described in Chapter I.

$$141 \text{ dB} \geq \left[\left(\frac{4\pi d}{\lambda} \right)^2 \cdot L_{O_2 - H_2O} \right]_{\text{dB}} + (L_{\text{Rain}})_{\text{dB}}$$

$$141 \text{ dB} \geq 132 \text{ dB} + 8 \text{ dB}$$

For a maximum distance of 2.5 km a link can exist in the absence of any trees. From Figure 14 for a frequency of 40 GHz the attenuation due to trees is between 2 and 5 dB per meter of forest. At this frequency, a single tree could produce almost 50 dB of attenuation. Therefore, Figure 15 displays all links that are less than 2.5 km and whose line-of-sight is not obstructed by any trees. Only 53% of the units have a connection, and these connections are broken down into eight disjointed sets. It is obvious at 40 GHz that connectivity does not exist.

If 20 GHz is used as the center frequency with the same percent reliability, Figures 6a and 7 give the maximum single hop distance as 5 km. From Figure 14 for a frequency of 20 GHz, the attenuation due to trees is still about 2 to 5 dB per meter. Figure 16 displays all the links that are less than 5 km and whose line-of-sight is not obstructed by any trees. This is a noticeable improvement in that 69% of the units have a connection, but connectivity does not exist since there is a limited capability to pass traffic from the forward units to the units in the rear. A loss of key nodes

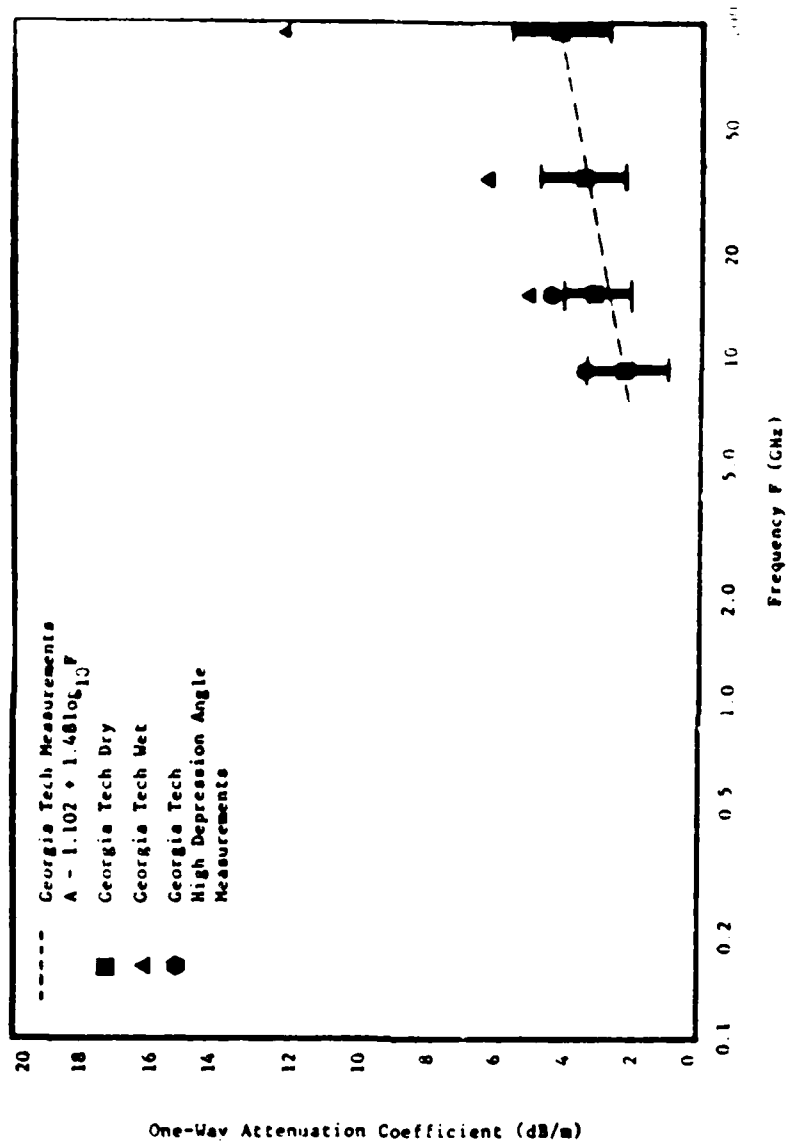


Figure 14. Attenuation due to foliage [Ref. 12].

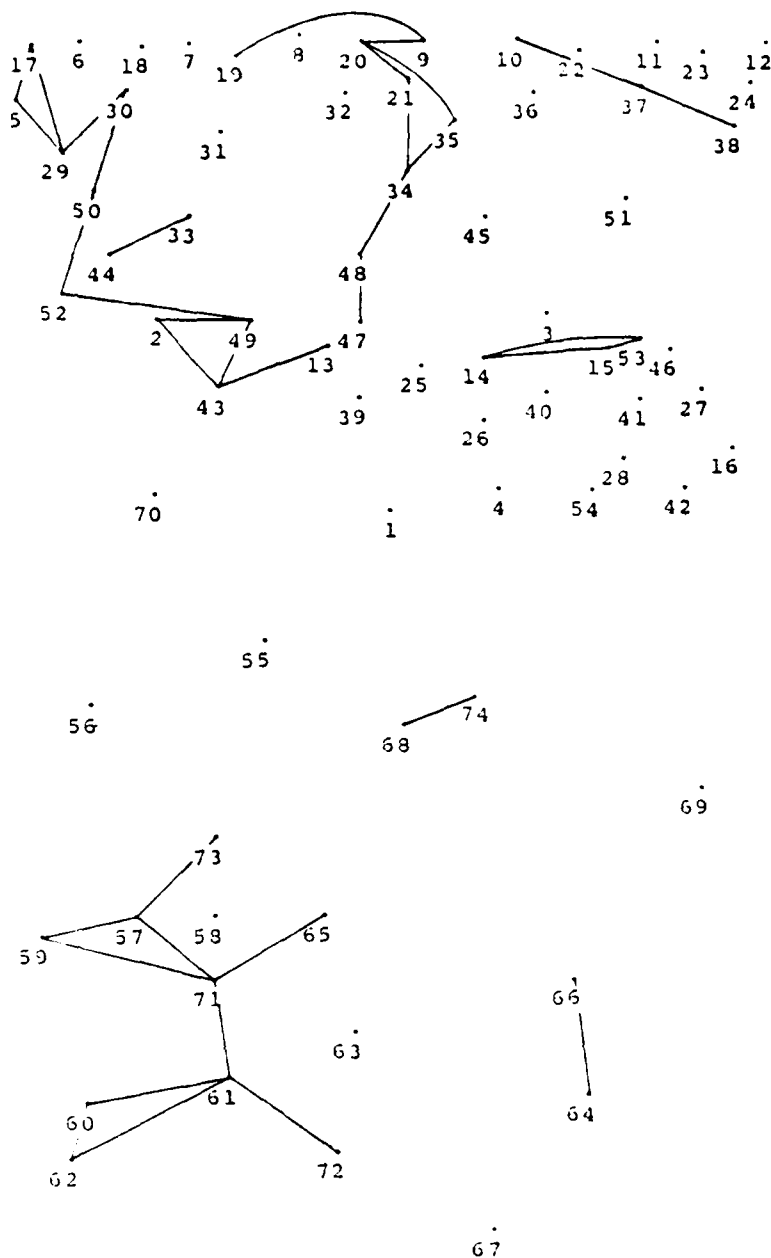


Figure 15. Connectivity at 40 GHz for the first data set.

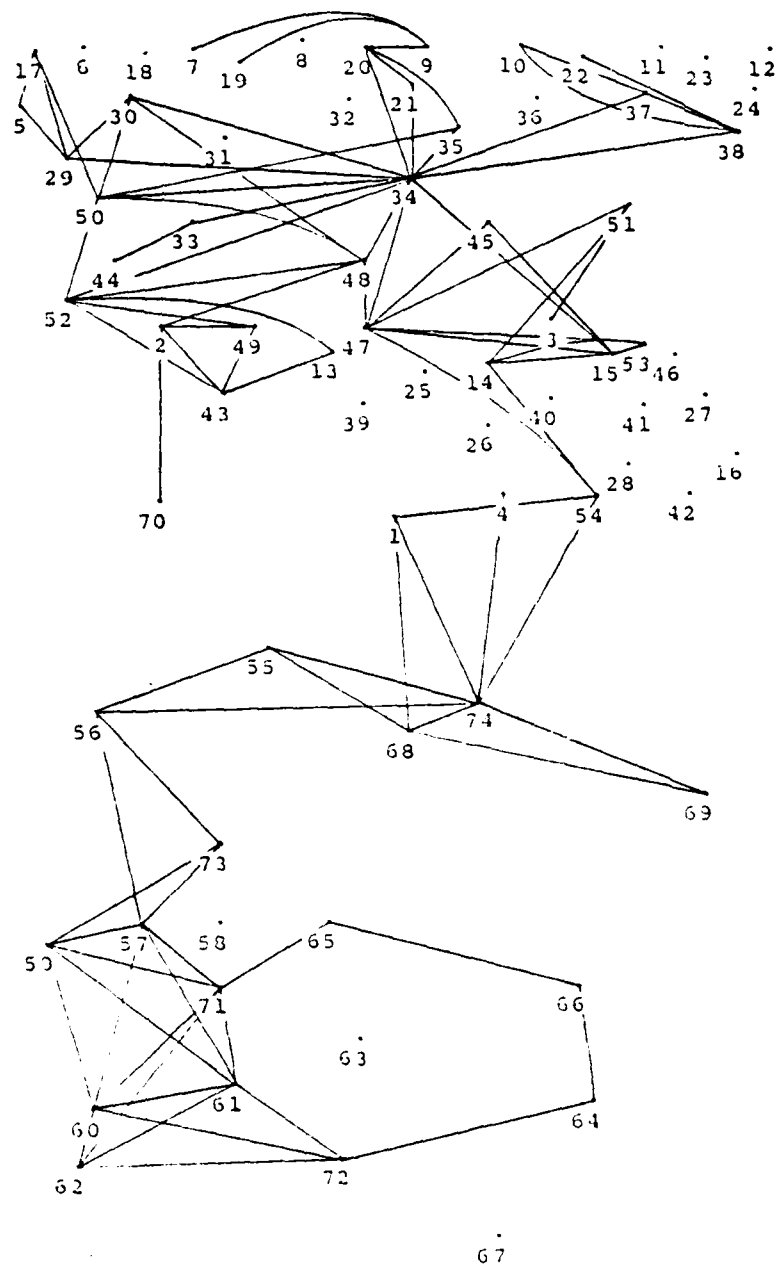


Figure 16. Connectivity at 20 GHz for the first data set.

such as 54 and 56 would cause the system to become disjointed. From Figure 16, it is obvious that a greater reduction in center frequency is still needed. Connectivity of the MAB's units in the SHF band is limited by the poor tree penetration quality and by the requirement to have short links. Units with antennas below the forest ceiling will never be able to connect at frequencies above about 10 GHz. Further analysis was therefore directed not only to finding a good frequency for connectivity but also to finding one with good tree penetration qualities.

C. UHF AND VHF CONNECTIVITY

At frequencies below SHF, Figures 6a, b, and c, and 7 cannot be used to determine path loss. At these lower frequencies the path loss is more accurately approximated by Bullington's equation as shown in Figures 3 and 4. The attenuation due to foliage penetration at VHF and UHF can be determined by Nathanson's equation. Therefore the link loss equation is

$$(\text{Attenuation})_{\text{dB}} = \left[\frac{d^2}{h_1 h_2} \right]_{\text{dB}}^2 + 0.25 f^{3/4}$$

Figure 17 displays the five nearest neighbors at a center frequency of 1.5 GHz that have a total link loss of less than or equal to 141 dB. The five nearest neighbors concept was

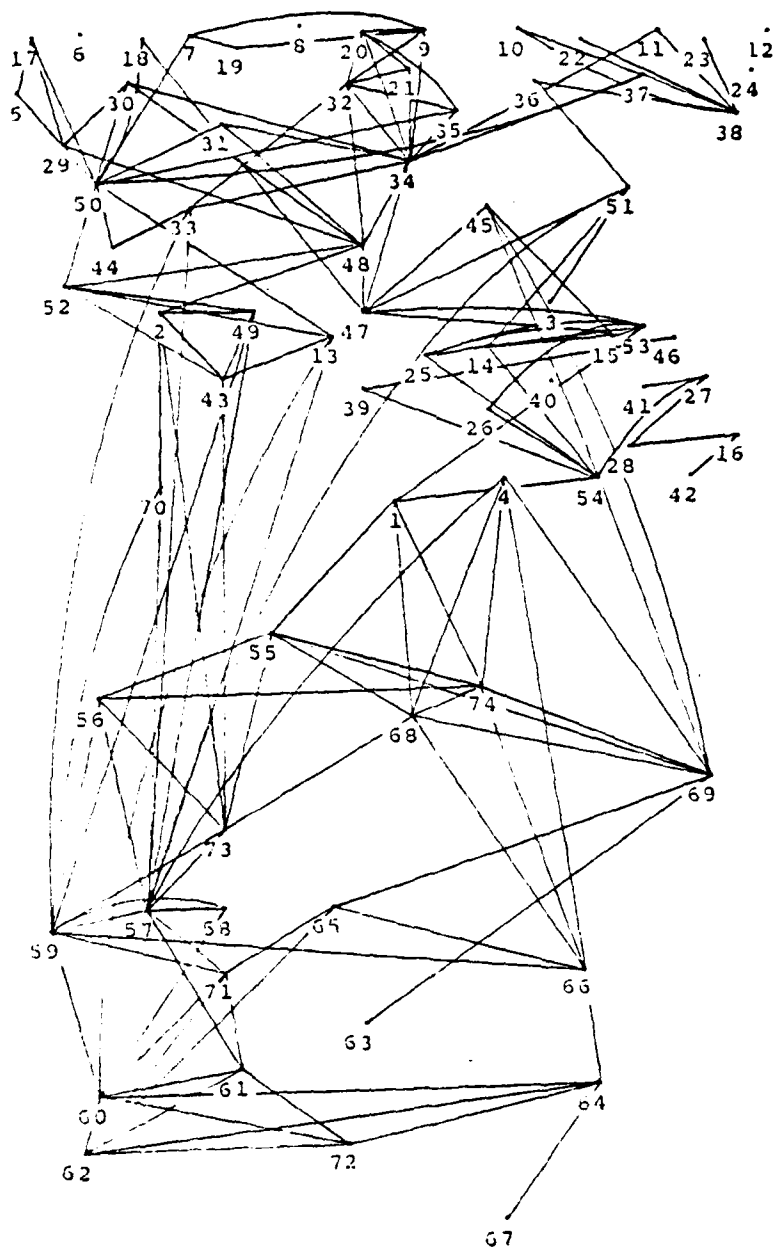


Figure 17. Connectivity for the five nearest neighbors at 1.5 GHz for the first data set.

developed because some nodes see over 20 other nodes. The five nearest neighbors concept functions such that a node displays the five nearest of all the links that it has. Nearest is determined as a function of the x and y coordinates only, and does not take into account changes in elevation. Figure 17 has only five nodes that do not have a single connection with another node, and all of these five have a mobility factor of zero. To connect these nodes, a lower frequency with a better tree penetration quality is needed.

In order to provide a high frequency with ample bandwidth for multi-channel operations, and a low frequency for tree penetration, a frequency pair was analyzed. The high frequency was 1.5 GHz and the low frequency was either 150 MHz or 300 MHz. These three frequencies were used throughout the remainder of the report. The five nearest neighbors concept was still used without regard to whether the link was being carried on the high or low frequency. One of the problems with this concept is that, as the number of low-frequency links increased, there was a decrease in the number of high-frequency links that fell within the five nearest neighbors rule. Though the use of lower-frequency links produced more of a direct path through the network, they were not beneficial to all nodes. Some nodes had high-frequency links capable of carrying multiple channels replaced by narrow-band, short links, capable of carrying only a few channels. This is evident when one compares Figures 17 and 18. Figure 17 is the five nearest high-frequency links, and

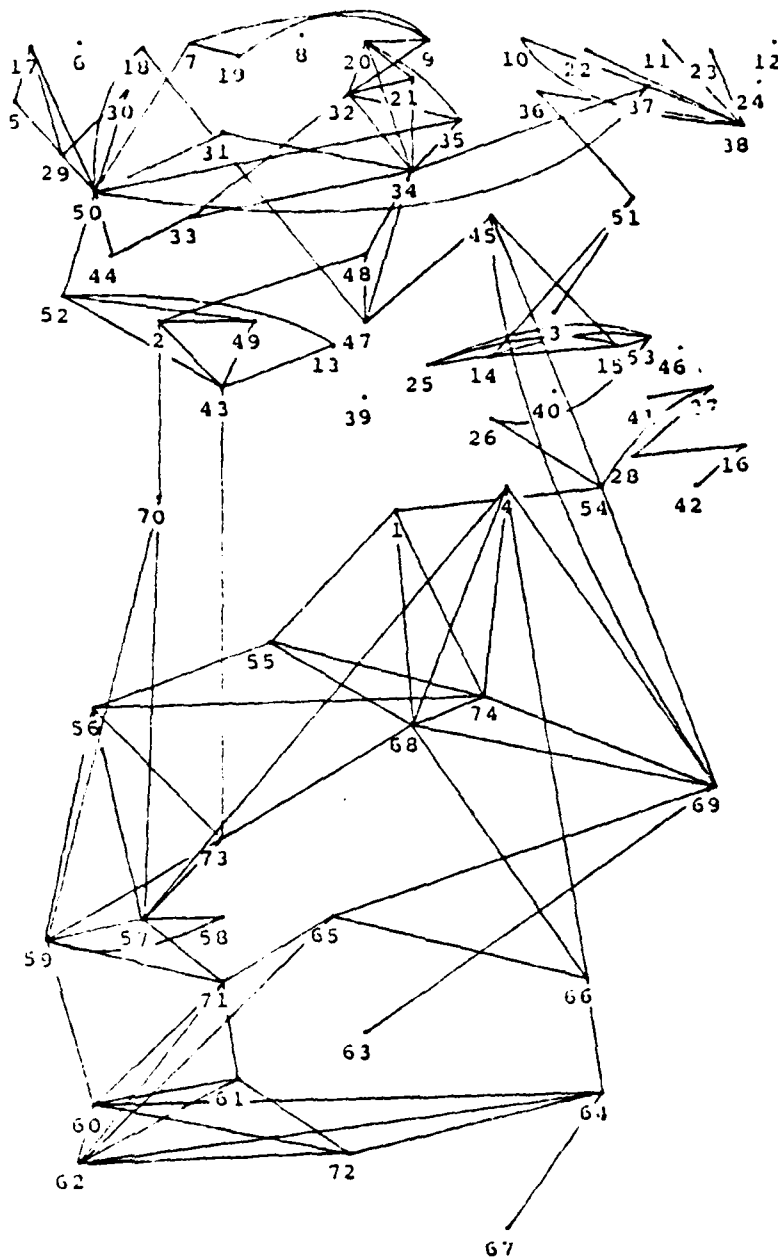


Figure 18. Connectivity for only the 1.5 GHz links from among the five nearest neighbors for 300 MHz and 1.5 GHz, for the first data set.

Figure 18 is the high-frequency links that fit the five nearest neighbors rule when the lower frequency is 300 MHz. There is a 21% reduction in the number of high-frequency links but a 27% increase in the number of total links. The total link connectivity is displayed in Figure 19 where the solid line represents a link that is being carried on the high frequency, and a solid line with a tick mark on it represents a link that is being carried on the low frequency. This is the first connection pattern that includes all the nodes. Figure 19 was generated from Table 6. Table 6 displays the transmit station on the left, the number of links that exist, and the five nearest receiving stations. The second digit under the receiving stations is a zero if the link is being carried on the high frequency and a one if the link is being carried on the low frequency.

If the low frequency is 150 MHz and the high frequency is maintained at 1.5 GHz the connectivity is described in Figure 20. On the average this produces more low-frequency links and reduces the number of high-frequency links that make up the backbone of wideband multi-channel links. The connectivity of the units near the FEBA is increased by the use of 150 MHz, but at the expense of channel capacity throughout the entire network. This decrease in high-frequency links can be seen by comparing Figure 18 for 300 MHz and 1.5 GHz, with Figure 21 for only 150 MHz and 1.5 GHz.

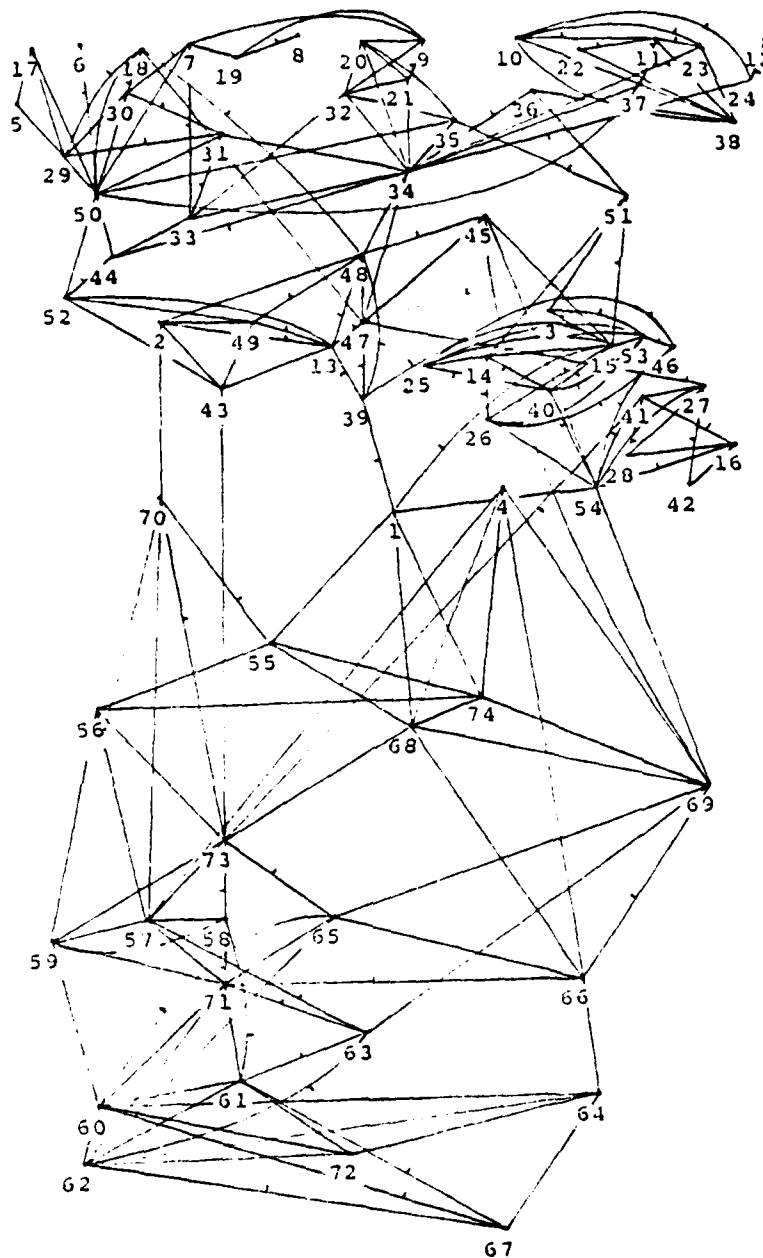


Figure 19. Connectivity for the five nearest neighbors for 300 MHz and 1.5 GHz, for the first data set. Links with tick marks are carried at the lower frequency.

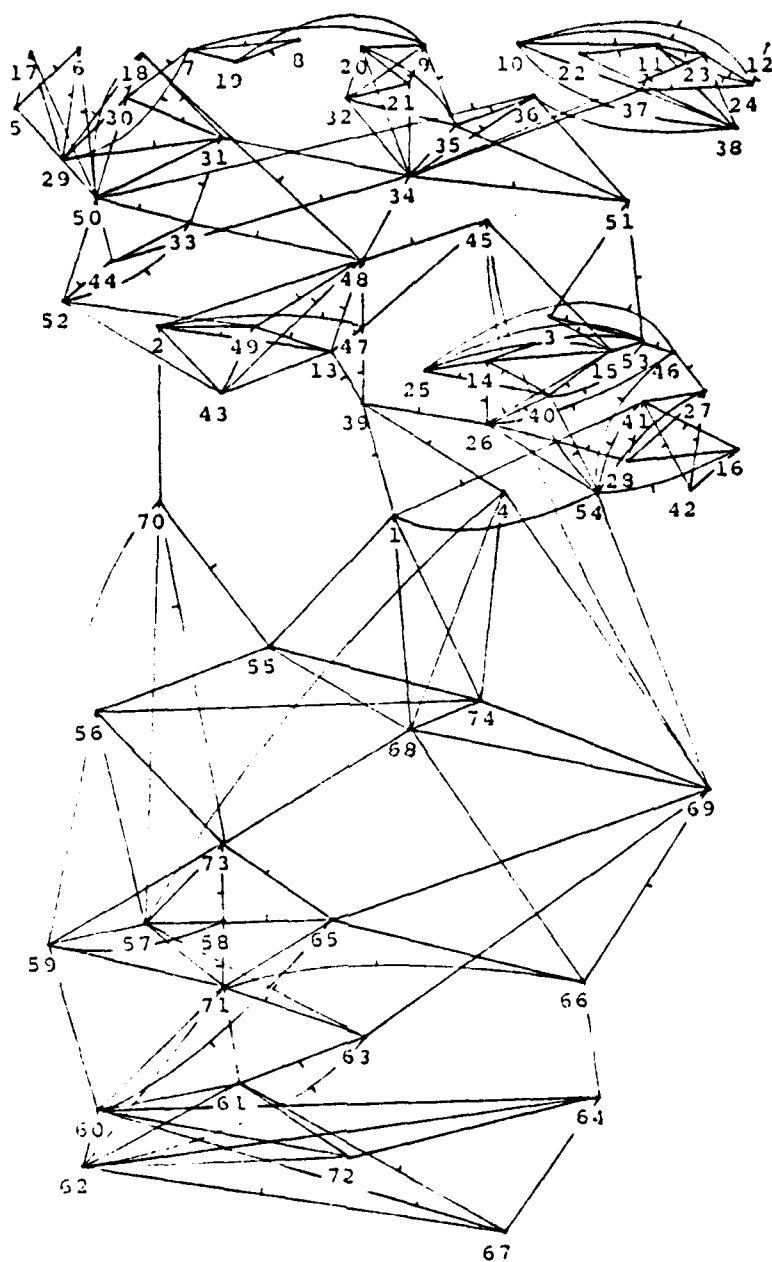


Figure 20. Connectivity for the five nearest neighbors for 150 MHz and 1.5 GHz, for the first data set. Links with tick marks are carried at the lower frequency.

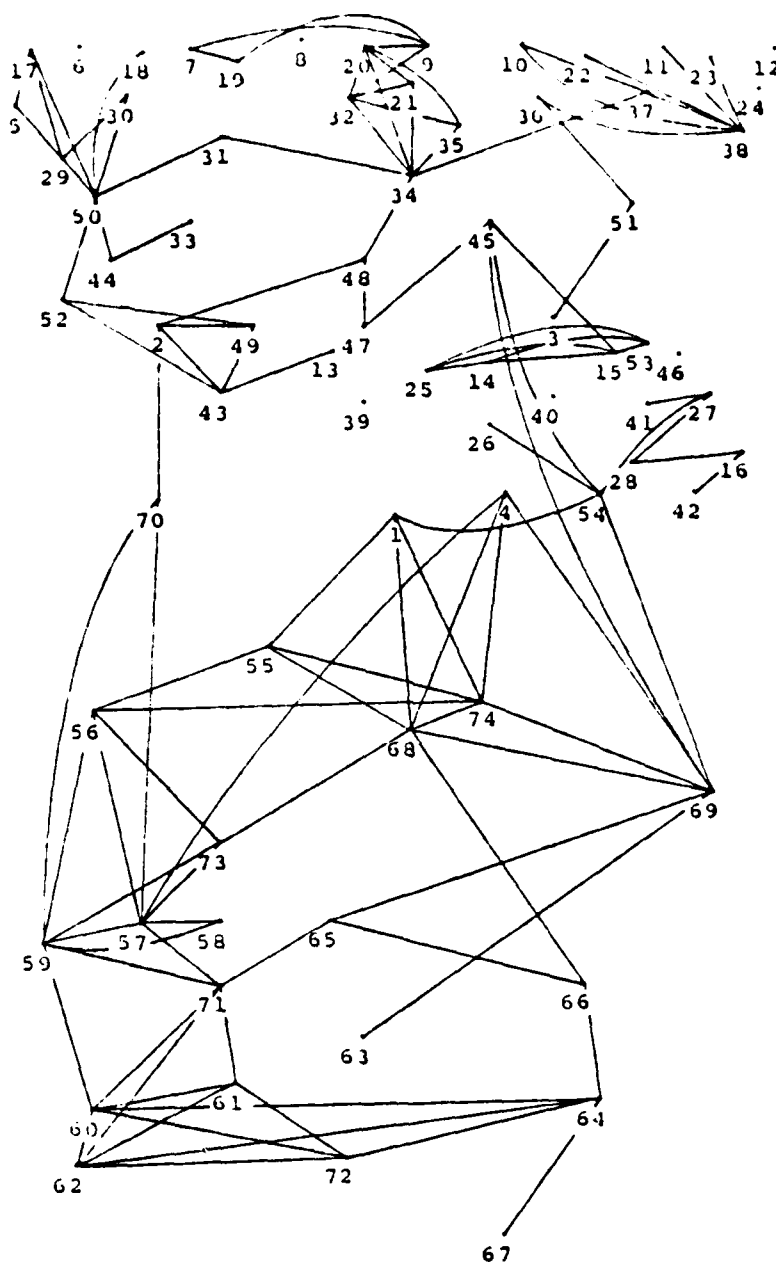


Figure 21. Connectivity for only the 1.5 GHz links from among the five nearest neighbors for 150 MHz and 1.5 GHz, for the first data set.

Both of these figures display the high-frequency links that meet the five nearest neighbors rule. By using 150 MHz as the low frequency vice 300 MHz, a 10% reduction in the number of high-frequency links is created.

D. CONNECTIVITY WITH UNIT MOVEMENT

In order to check the MAB's connectivity under different terrain conditions, all units were moved back off the FEBA into the next adjoining grid squares. Figure 22 displays the connectivity for a low frequency of 300 MHz and a high frequency of 1.5 GHz, with unit positions as described in Table 4 and Figure 12. Figure 23 also displays the five nearest neighbors but with a low frequency of 150 MHz. Both figures show evidence of the connectivity problem caused by the 6 km ridge that runs along grid line 59000, just forward of node 59. The connectivity problem caused by ridges and ravines will not be overcome solely by using packet radios. Care must be taken when assigning unit locations so that a repeater or unit is located with connectivity to both sides of the ridge.

The MAB units were moved a second time back into the next adjoining grid squares. The unit locations are described in Table 5 and Figure 13. The connectivity problem encountered by the ridge running along grid line 59000 has been eliminated by positioning repeater number 73 on top of the ridge. Figure 24 displays the five nearest neighbors when only the high frequency of 1.5 GHz is used. Figure 25 shows the

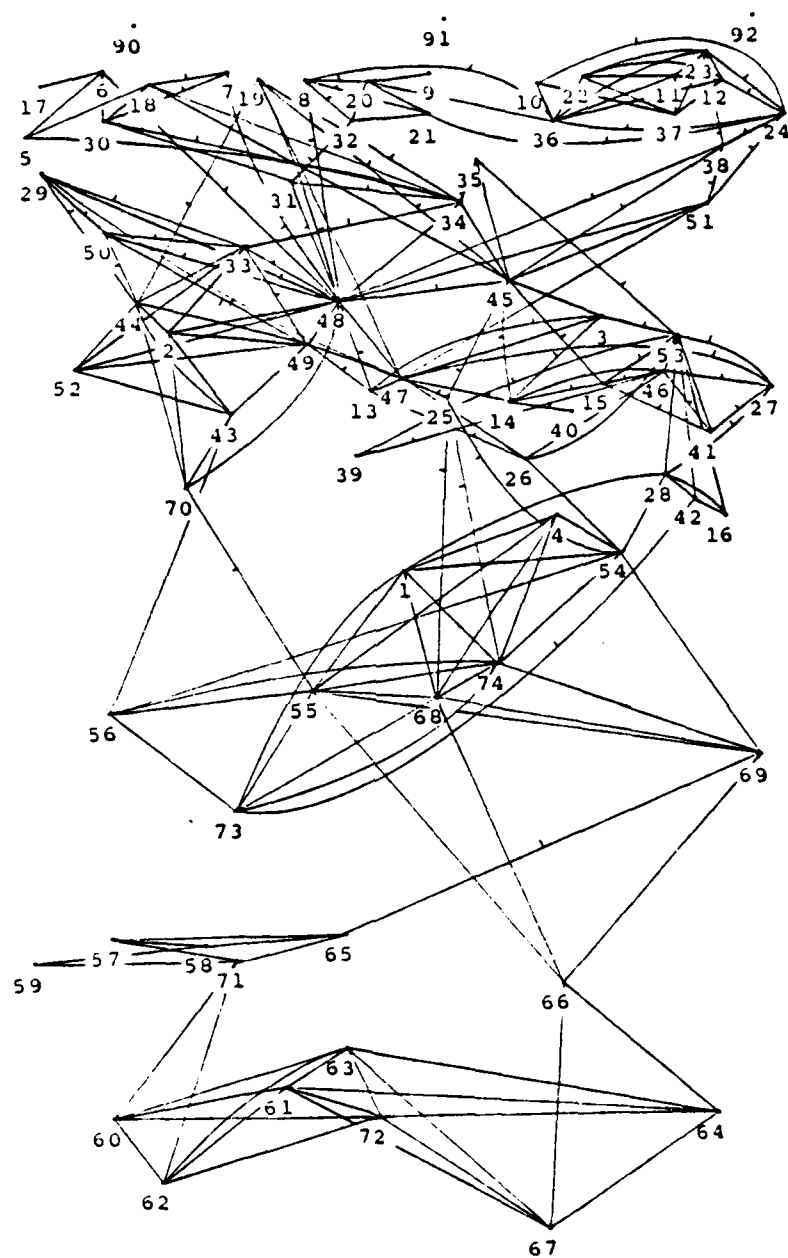


Figure 22. Connectivity for the five nearest neighbors for 300 MHz and 1.5 GHz, for the second data set. Links with tick marks are carried at the lower frequency.

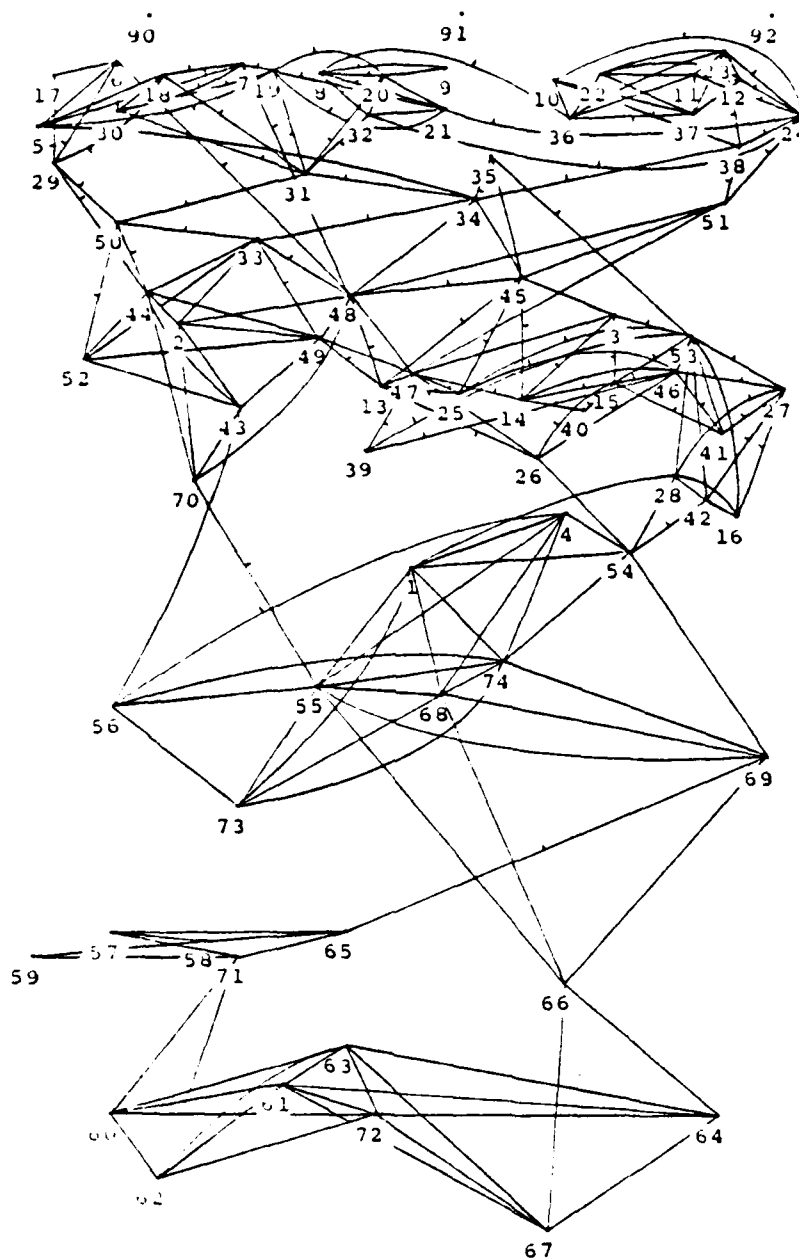


Figure 23. Connectivity for the five nearest neighbors for 150 MHz and 1.5 GHz, for the second data set. Links with tick marks are carried at the lower frequency.

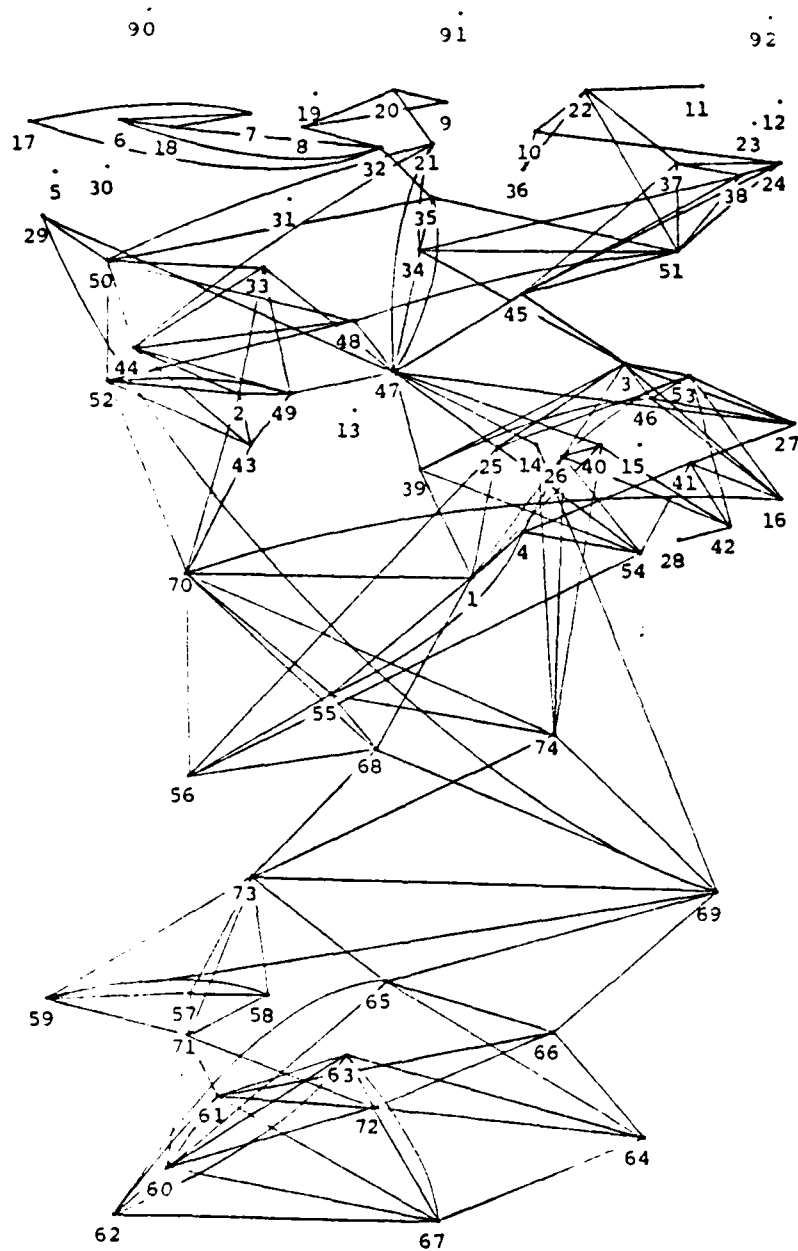


Figure 24. Connectivity for the five nearest neighbors at 1.5 GHz, for the third data set.

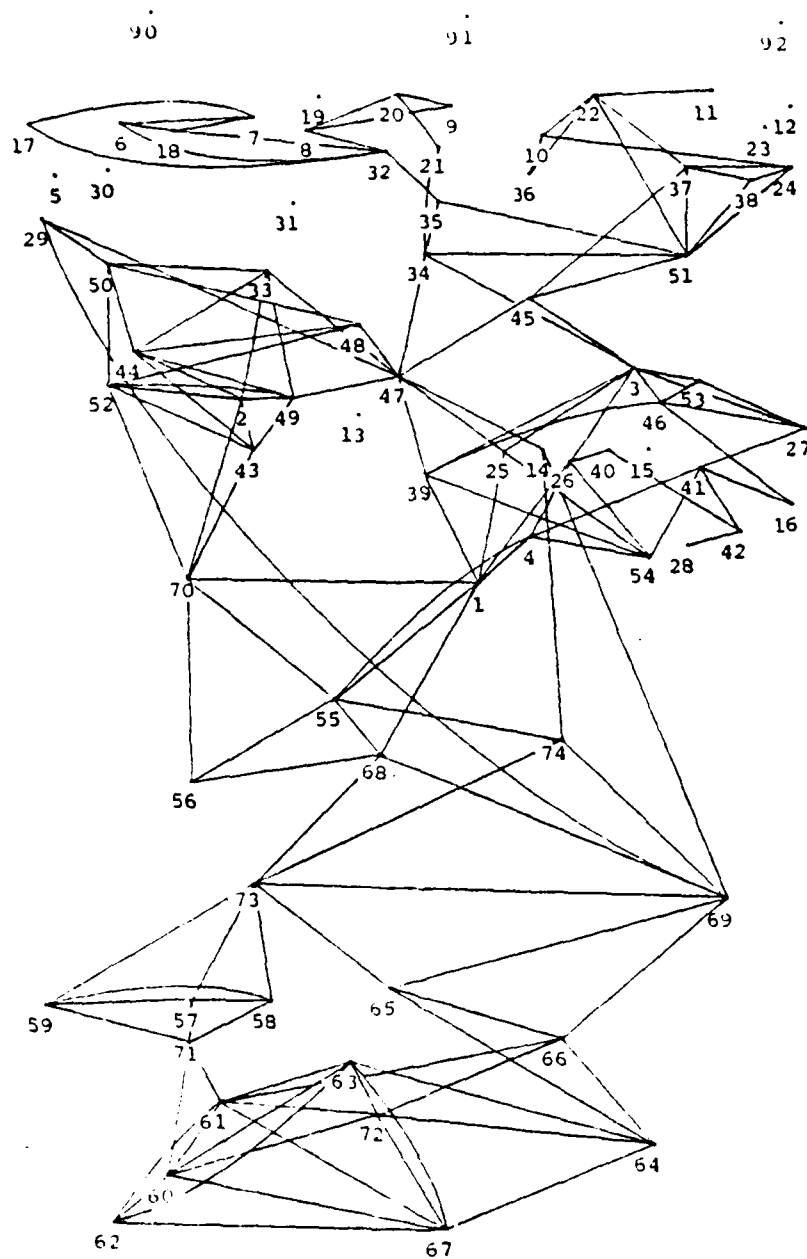


Figure 25. Connectivity for only the 1.5 GHz links from among the five nearest neighbors for 300 MHz and 1.5 GHz, for the third data set.

connectivity by the high-frequency links when the five nearest neighbors rule is employed with a low frequency of 300 MHz and a high frequency of 1.5 GHz. The total connectivity for these two frequencies is displayed in Figure 26.

These figures show good connectivity at the high frequency, which is the backbone of the high-volume, multi-channel system. They also provide ample routing capability for all nodes, even the units located near the FEBA with mobility factors of zero.

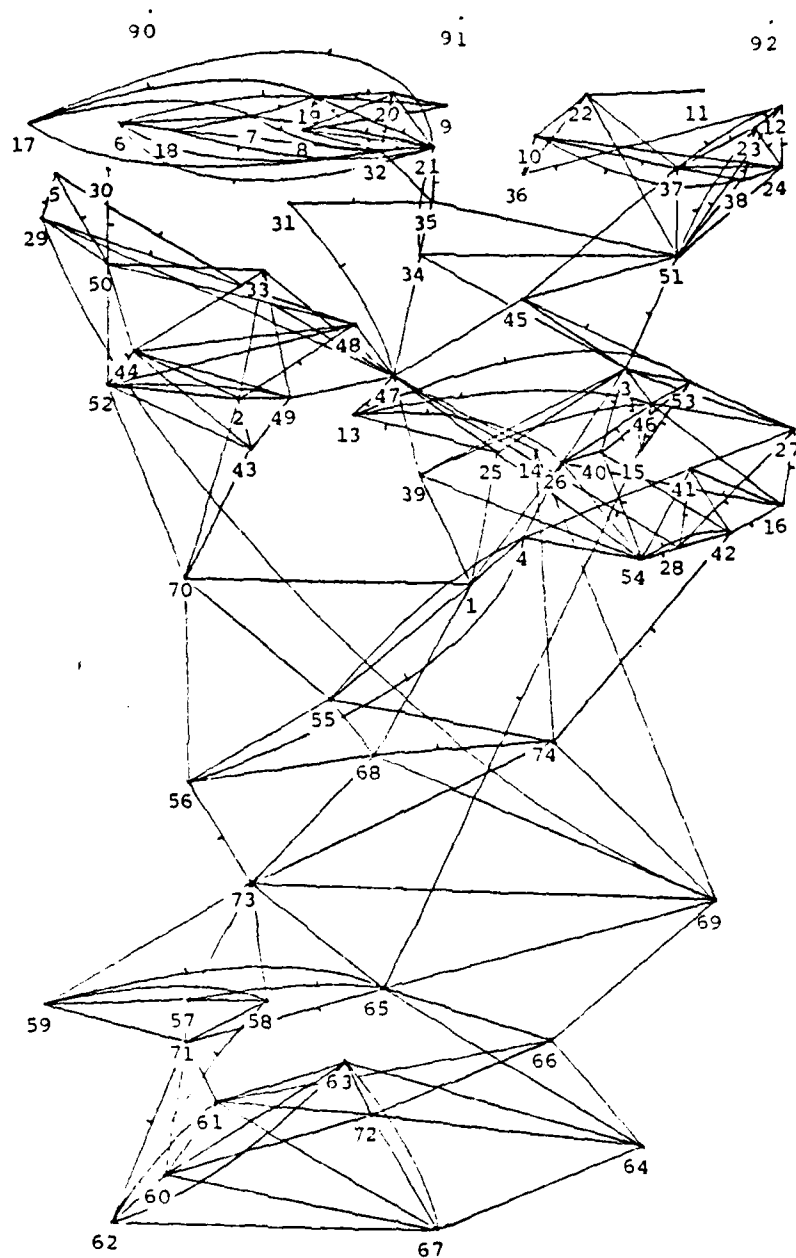


Figure 26. Connectivity for the five nearest neighbors for 300 MHz and 1.5 GHz, for the third data set. Links with tick marks are carried at the lower frequency.

Table 6. The five nearest neighbors for 300 MHz and 1.5 GHz, for the first data set.

[illegible]

1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100	101	102	103	104	105	106	107	108	109	110	111	112	113	114	115	116	117	118	119	120	121	122	123	124	125	126	127	128	129	130	131	132	133	134	135	136	137	138	139	140	141	142	143	144	145	146	147	148	149	150	151	152	153	154	155	156	157	158	159	160	161	162	163	164	165	166	167	168	169	170	171	172	173	174	175	176	177	178	179	180	181	182	183	184	185	186	187	188	189	190	191	192	193	194	195	196	197	198	199	200	201	202	203	204	205	206	207	208	209	210	211	212	213	214	215	216	217	218	219	220	221	222	223	224	225	226	227	228	229	230	231	232	233	234	235	236	237	238	239	240	241	242	243	244	245	246	247	248	249	250	251	252	253	254	255	256	257	258	259	260	261	262	263	264	265	266	267	268	269	270	271	272	273	274	275	276	277	278	279	280	281	282	283	284	285	286	287	288	289	290	291	292	293	294	295	296	297	298	299	300	301	302	303	304	305	306	307	308	309	310	311	312	313	314	315	316	317	318	319	320	321	322	323	324	325	326	327	328	329	330	331	332	333	334	335	336	337	338	339	340	341	342	343	344	345	346	347	348	349	350	351	352	353	354	355	356	357	358	359	360	361	362	363	364	365	366	367	368	369	370	371	372	373	374	375	376	377	378	379	380	381	382	383	384	385	386	387	388	389	390	391	392	393	394	395	396	397	398	399	400	401	402	403	404	405	406	407	408	409	410	411	412	413	414	415	416	417	418	419	420	421	422	423	424	425	426	427	428	429	430	431	432	433	434	435	436	437	438	439	440	441	442	443	444	445	446	447	448	449	450	451	452	453	454	455	456	457	458	459	460	461	462	463	464	465	466
---	---	---	---	---	---	---	---	---	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

[illegible]

REFERENCES

[illegible]

72 70

[illegible]

74	77	79	81	83	85	87	89	91	93	95	97	99	101	103	105	107	109	111	113	115	117	119	121	123	125	127	129	131	133	135	137	139	141	143	145	147	149	151	153	155	157	159	161	163	165	167	169	171	173	175	177	179	181	183	185	187	189	191	193	195	197	199	201	203	205	207	209	211	213	215	217	219	221	223	225	227	229	231	233	235	237	239	241	243	245	247	249	251	253	255	257	259	261	263	265	267	269	271	273	275	277	279	281	283	285	287	289	291	293	295	297	299	301	303	305	307	309	311	313	315	317	319	321	323	325	327	329	331	333	335	337	339	341	343	345	347	349	351	353	355	357	359	361	363	365	367	369	371	373	375	377	379	381	383	385	387	389	391	393	395	397	399	401	403	405	407	409	411	413	415	417	419	421	423	425	427	429	431	433	435	437	439	441	443	445	447	449	451	453	455	457	459	461	463	465	467	469	471	473	475	477	479	481	483	485	487	489	491	493	495	497	499	501	503	505	507	509	511	513	515	517	519	521	523	525	527	529	531	533	535	537	539	541	543	545	547	549	551	553	555	557	559	561	563	565	567	569	571	573	575	577	579	581	583	585	587	589	591	593	595	597	599	601	603	605	607	609	611	613	615	617	619	621	623	625	627	629	631	633	635	637	639	641	643	645	647	649	651	653	655	657	659	661	663	665	667	669	671	673	675	677	679	681	683	685	687	689	691	693	695	697	699	701	703	705	707	709	711	713	715	717	719	721	723	725	727	729	731	733	735	737	739	741	743	745	747	749	751	753	755	757	759	761	763	765	767	769	771	773	775	777	779	781	783	785	787	789	791	793	795	797	799	801	803	805	807	809	811	813	815	817	819	821	823	825	827	829	831	833	835	837	839	841	843	845	847	849	851	853	855	857	859	861	863	865	867	869	871	873	875	877	879	881	883	885	887	889	891	893	895	897	899	901	903	905	907	909	911	913	915	917	919	921	923	925	927	929	931	933	935	937	939	941	943	945	947	949	951	953	955	957	959	961	963	965	967	969	971	973	975	977	979	981	983	985
----	----	----	----	----	----	----	----	----	----	----	----	----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----	-----

[illegible]

AT 11 11 11 11 11 11

11 11

67	27	27	27
68	27	27	27
69	27	27	27
70	16	16	16
71	9	9	9
72	8	8	8
73	5	5	5
74	7	41	6
75	13	6	6
76	4	6	6
77	3	36	10
78	14	31	10
79	11	5	5
70	4	5	5
71	1	5	5
72	11	5	5

VI. ENEMY INTERCEPT

Three enemy listening posts (LP) were established in order to determine which units were capable of transmitting across the FEBA. The listening posts were numbered 90, 91 and 92, and were located at 40050 11650, 40050 15500, and 40050 19500. For each LP, an analysis was done to determine if an RF link existed to any one of the 74 nodes. If a link existed, then the SNR at the receiver input for an antenna gain of 5.83 dB was given. This SNR was given for both the low and high frequencies that the transmitter might be using. The distance between the LP and node was also given along with the amount of forests penetrated.

Table 7 shows all the links that exist for a low frequency of 150 MHz and a high frequency of 1.5 GHz. The units are located at the first set of data points as described in Figure 11. Figure 27 displays all the nodes that produce an SNR of greater than -30 dB at any one of the listening posts. The nodes with the large dots are the ones that can be intercepted. If the high frequency only is displayed as in Figure 28, there is a noticeable reduction in the number of nodes that produce an SNR > -30 dB at the FEBA. Therefore the high frequency is again recommended because of its bandwidth and low probability of intercept.

If the units are moved back off the FEBA one grid square to locations as in Figure 12, the stations that can be

Table 7. The nodes that can be intercepted for 150 MHz and 1.5 GHz, for the first data set. The distance and amount of forest between nodes is also displayed.

Node	Node	Distance	Forest	Node	Node
90	10	34.0	-51.7	90	10
90	13	37.0	-48.3	90	13
90	15	41.0	-16.6	90	15
90	15	45.0	-181.7	90	15
90	27	37.0	-53.7	90	27
90	27	45.0	-174.7	90	27
90	29	43.0	20.0	90	29
90	30	44.0	20.0	90	30
90	31	45.0	20.0	90	31
90	39	45.0	20.0	90	39
90	43	45.0	20.0	90	43
90	47	45.0	20.0	90	47
90	48	45.0	20.0	90	48
90	50	45.0	20.0	90	50
90	54	45.0	20.0	90	54
90	57	45.0	20.0	90	57
90	59	45.0	20.0	90	59
90	60	45.0	20.0	90	60
90	65	45.0	20.0	90	65
90	66	45.0	20.0	90	66
90	69	45.0	20.0	90	69
90	75	45.0	20.0	90	75
91	10	45.0	20.0	91	10
91	13	45.0	20.0	91	13
91	17	45.0	20.0	91	17
91	20	45.0	20.0	91	20
91	21	45.0	20.0	91	21
91	32	45.0	20.0	91	32
91	34	45.0	20.0	91	34
91	35	45.0	20.0	91	35
91	49	45.0	20.0	91	49
92	10	45.0	20.0	92	10
92	11	45.0	20.0	92	11
92	12	45.0	20.0	92	12
92	13	45.0	20.0	92	13
92	14	45.0	20.0	92	14
92	15	45.0	20.0	92	15
92	22	45.0	20.0	92	22
92	23	45.0	20.0	92	23
92	24	45.0	20.0	92	24
92	34	45.0	20.0	92	34
92	35	45.0	20.0	92	35
92	37	45.0	20.0	92	37
92	38	45.0	20.0	92	38
92	39	45.0	20.0	92	39
92	44	45.0	20.0	92	44
92	47	45.0	20.0	92	47
92	50	45.0	20.0	92	50
92	51	45.0	20.0	92	51
92	52	45.0	20.0	92	52
92	53	45.0	20.0	92	53
92	57	45.0	20.0	92	57
92	59	45.0	20.0	92	59
92	60	45.0	20.0	92	60

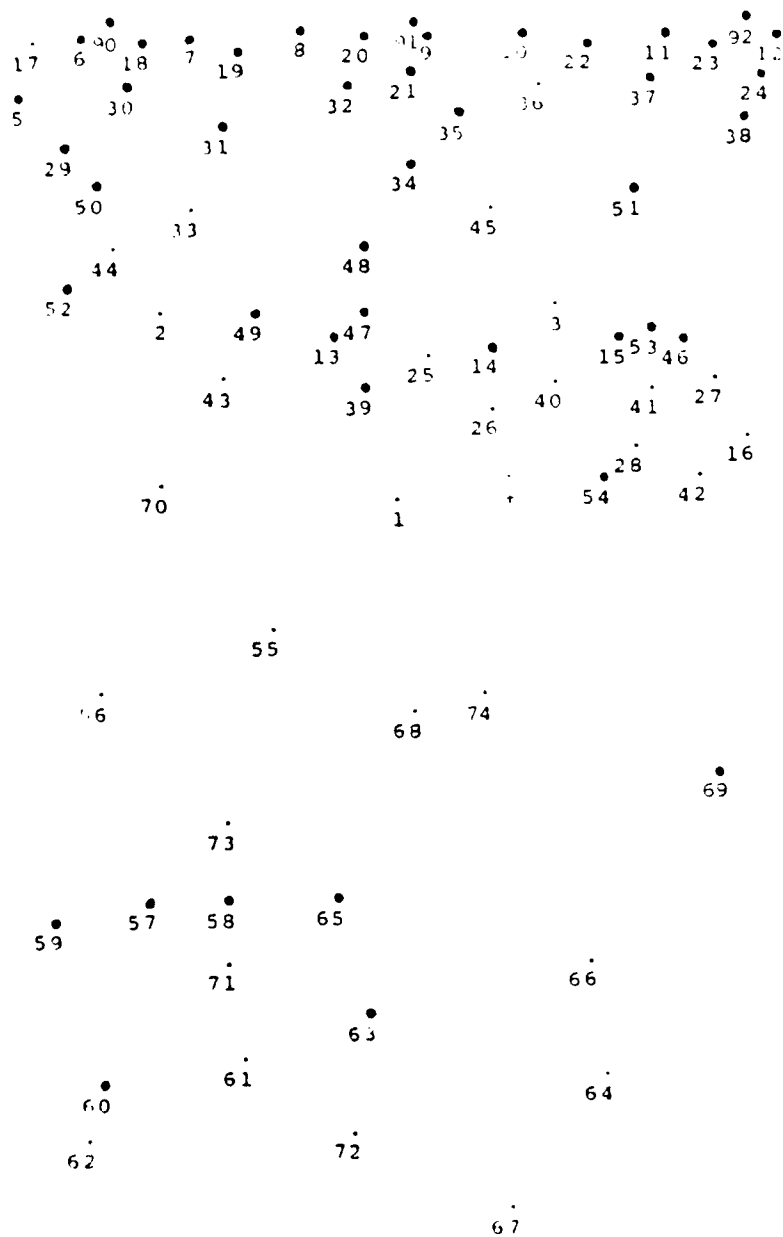


Figure 27. The nodes with the large dots can be intercepted with a CNR greater than -30 dB if they are transmitting at 150 MHz, first data set.

AD-A098 085

NAVAL POSTGRADUATE SCHOOL MONTEREY CA
COMPUTER INVESTIGATION OF VHF, UHF AND SHF FREQUENCIES FOR MARI--ETC(L)
DEC 80 T G KANE

F/G 17/2,1

UNCLASSIFIED

NL

200
3-81

1

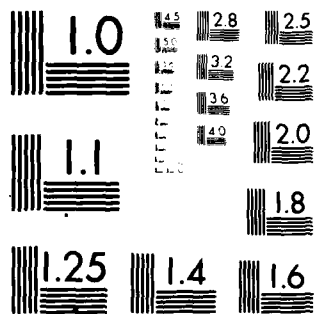
END

DATE

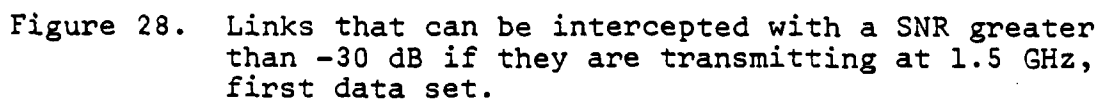
FILED

3-81

DTIC



MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A



intercepted at the low frequency appear in Figure 29 and the high frequency in Figure 30. Finally, if the units are again moved as in Figure 13, the units that can be intercepted at the low frequency appear in Figure 31 and the high frequency in Figure 32. These figures show that the probability of intercept decreases with increasing distance and frequency, as was expected. It is evident that, in order to decrease the amount of traffic intercepted, the low, tree-penetration frequencies should be used sparingly.



Figure 29. The nodes with the large dots can be intercepted with a SNR greater than -30 dB if they are transmitting at 150 MHz, second data set.

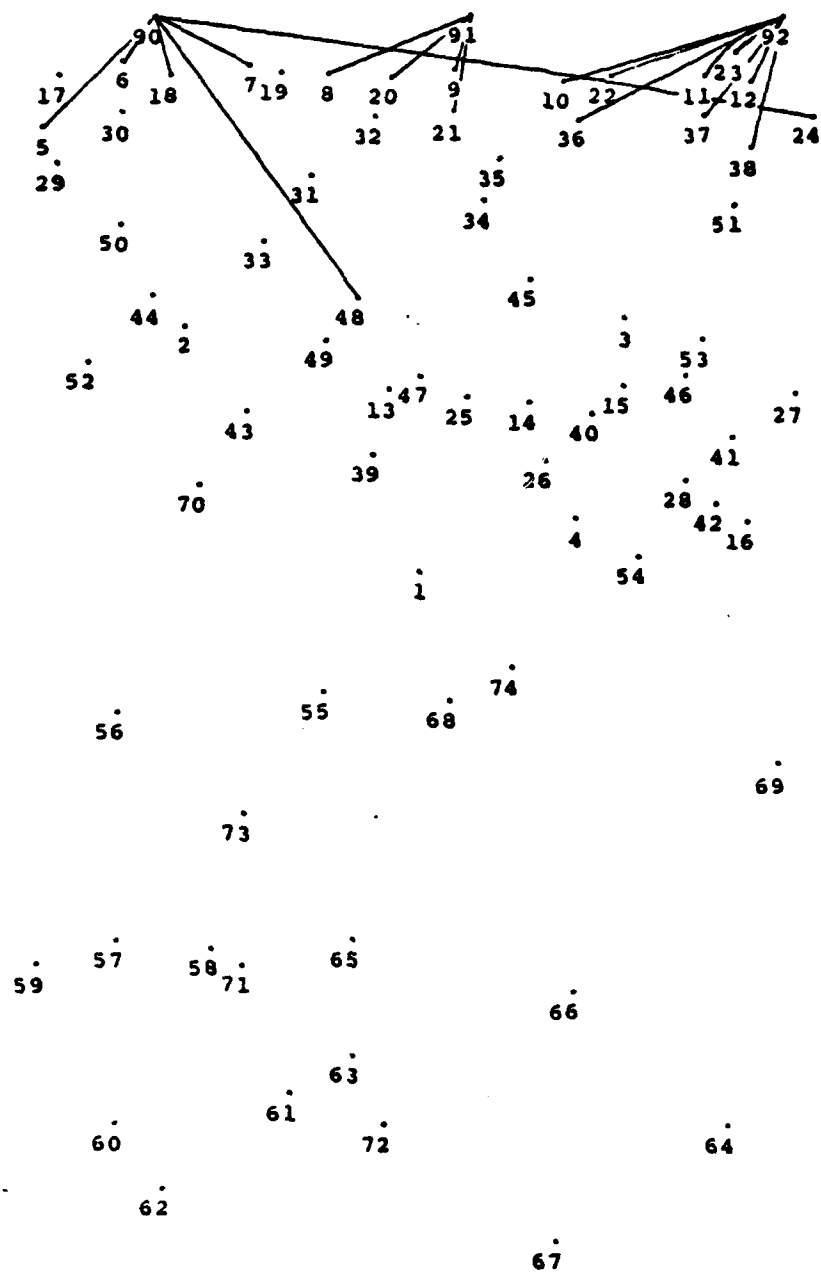


Figure 30. Links that can be intercepted with a SNR greater than -30 dB if they are transmitting at 1.5 GHz, second data set.



Figure 31. The nodes with the large dots can be intercepted with a SNR greater than -30 dB if they are transmitting at 150 MHz, third data set.



Figure 32. Links that can be intercepted with a SNR greater than -30 dB if they are transmitting at 1.5 GHz, third data set.

VII. CONCLUSIONS AND RECOMMENDATIONS

From the data presented in this report, it can be concluded that connectivity to support a practical packet radio system can be provided for terrain typical of western Europe. The system should have the capability of transmitting on at least two frequencies in the VHF and UHF bands. One of these frequencies should be in the high VHF range and would be needed as the tree-penetration frequency. The other frequency could be near 1.5 Hz and would be used as the wide-band, multi-channel frequency.

The algorithm used for selecting the frequency in the packet radio should make maximum use of the high frequency. The low frequency need only be used where the high frequency fails to connect with another node. Relying on the high frequency will not only increase the total system's channel capacity, but will also decrease the probability of being intercepted.

Figure 33 shows the connectivity under these constraints. The system is based on the five nearest neighbors rule for the third set of data points and a high frequency of 1.5 GHz. Then only the nodes without connectivity were permitted to use the lower frequency of 300 MHz. This network has 95% of the links being carried on the high frequency and only 35% of the nodes with the capability of being intercepted, as shown in Figure 34.

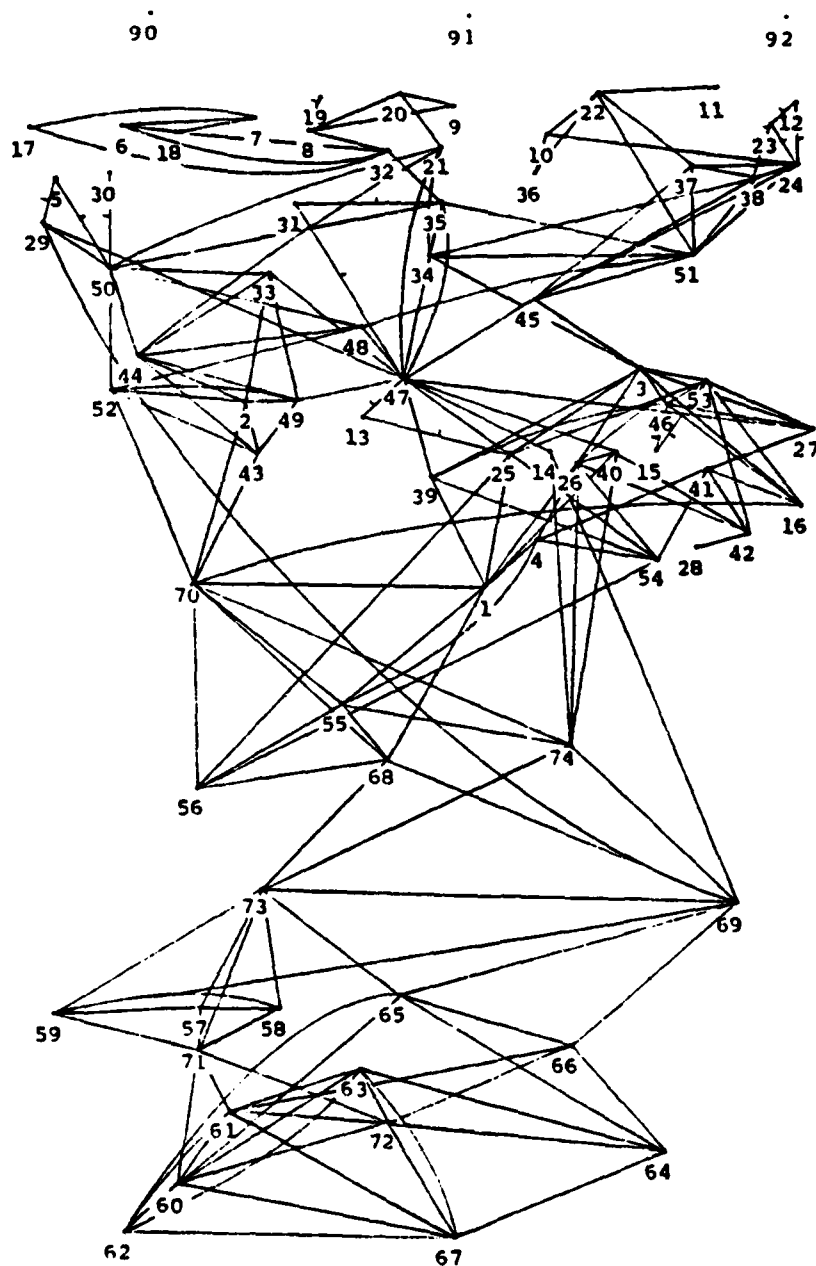


Figure 33. Connectivity for the five nearest neighbors at 1.5 GHz with selected nodes using 300 MHz, third data set. Links with tick marks are carried at the lower frequency.

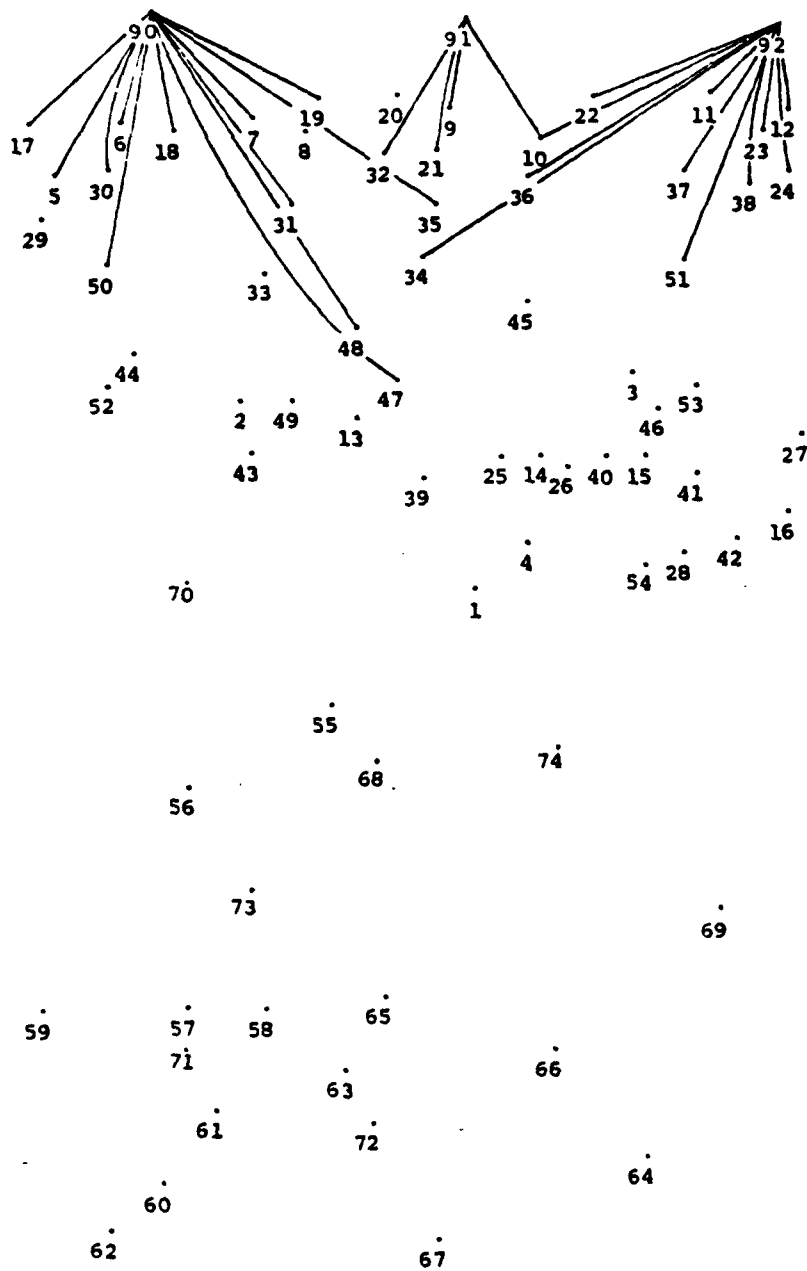


Figure 34. Links that can be intercepted with a SNR greater than -30 dB for 300 MHz and 1.5 GHz, third data set.

53

102

```

MAIN
DEFINE MAXLOS DISTANCE AS REAL VARIABLES
DEFINE LAND.VISFRB AS REAL VARIABLE
DEFINE I,J,K,II,JJ,SMALLEST,KK,
NODE.J,NODE.K,X,JX,XZ AS INTEGER VARIABLES
DEFINE MATRIX.DISTANCE AS A 2-DIMENSIONAL REAL ARRAY
DEFINE FREE.SPACE.L,FREE.SPACE.H,BULLINGTON.LOSS,MARGIN,LOSS.L,LOSS.H
AS REAL VARIABLES
LET LINES.V = 80
CALL RES.TERR
LET TEMP.NCVELS = NCVELS
READ SIZEA.LS,SIZEB.LS
RESERVE MAXLOS,NO.OF.PTS
RESERVE AX(*),AY(*),NODE.NO(*),NO.PER.ROW(*),MOBILITY(*) AS NO.OF.PTS
RESERVE MATRIX.DISTANCE(*,*),MATRIX.ORDER(*,*) AS NO.OF.PTS BY NO.OF.PTS
LET FREQ.L = 0.300 **GHZ OR 300MHZ
LET LAMDA.L = 0.3/FREQ.L
LET FREQ.H = 1.5 **GHZ
LET LAMDA.H = 0.3/FREQ.H
LET LINK.LOSS = 1
LET LAGB.LS = 1
LET LAGA.LS = 1
LET LBTOA.LS = 0
LET LATOB.LS = 1
FOR I = 1 TO NO.OF.PTS
  READ AX(I),AY(I),NODE.NO(I),J,MOBILITY(I)
  LET MATRIX.DISTANCE(J,J) = MAXLOS*10
  LET MATRIX.DISTANCE(NO.OF.PTS,NO.OF.PTS) = MAXLOS*10
  FOR K = J + 1 TO NO.OF.PTS
    LET NODE.K = NODE.NO(K)
    LET NCVELS = TEMP.NCVELS
    LET TMICA.LS = 0.
    LET TMICB.LS = 0.
    LET MATRIX.DISTANCE(NODE.K,NODE.J) = MAXLOS*10
    LET MATRIX.DISTANCE(NODE.J,NODE.K) = MAXLOS*10
    LET DISTANCE = SQRT.F((AX(J) - AX(K))**2 + (AY(J) - AY(K))**2)
    CALL ELEVEV GIVEN AX(J),AY(J) YIELDING TMACA.LS
    CALL ELEVEV GIVEN AX(K),AY(K) YIELDING TMACB.LS
    CALL TREES GIVEN AX(J),AY(J) YIELDING TREE.A.HT
    CALL TREES GIVEN AX(K),AY(K) YIELDING TREE.B.HT
    IF MOBILITY(J) EQ 1
      LET TMICA.LS = TREE.A.HT
    ALWAYS
    IF MOBILITY(K) EQ 1
      LET TMICB.LS = TREE.B.HT
  
```



```

FOR JJ = 1 TO 51 DO
  LET SMALLEST = 1
  FOR KK = 2 TO NO.OF.PTS, DO
    IF MATRIX.DISTANCE(II,SMALLEST) LE MATRIX.DISTANCE(II,KK), CYCLE
    ALWAYS
    LET SMALLEST = KK
  LOOP
  IF MATRIX.DISTANCE(II,SMALLEST) EQ MAXLOS*10, CYCLE
  ALWAYS
  LET MATRIX.ORDER(II,SMALLEST) = JJ*10 +
  INT.F(FRAC.F(MATRIX.DISTANCE(II,SMALLEST))*10)
  LET MATRIX.DISTANCE(II,SMALLEST) = MAXLOS*10
  JJ
LOOP
  CALL REPORT.PRINT
  CALL LPI
  STOP
END

```

```

ROUTINE REPORT.>PRINT
DEFINE IJ, JI AS INTEGER VARIABLES
BEGIN REPORT PRINTING FOR IJ = 1 TO NO.OF.PTS IN GROUPS OF 25 PER PAGE
BEGIN HEADING
PRINT 1 LINE AS FOLLOWS
  XT NO RECEIVERS
  SKIP 1 OUTPUT LINE
  PRINT 1 LINE WITH A GROUP OF IJ FIELDS THUS
  SKIP 1 OUTPUT LINE
  END
  FOR JI = 1 TO NO.OF.PTS, PRINT 1 LINE WITH JI, NO.PER.ROW(JI),
  ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** ** *
  ** ** ** REPORT
  LET LINES.V = 64
  BEGIN REPORT PRINTING FOR IJ = 1 TO NO.OF.PTS IN GROUPS OF 18 PER PAGE
  BEGIN HEADING
  SKIP 4 OUTPUT LINES

```

```

PRINT 1 LINE AS FOLLOWS
  XT NO RECEIVERS
SKIP 1 OUTPUT LINE
PRINT 1 LINE WITH A GROUP OF IJ FIELDS THUS
  ** ** ** **
SKIP 1 OUTPUT LINE
  ** ** **
END ** HEADING
FOR JI = 1 TO N3.DF.PTS, PRINT 1 LINE WITH JI, NO.PER.ROW(JI),
  AND A GROUP OF MATRIX.ORDER(JI,IJ) FIELDS THUS
  ** ** **
END ** REPORT
START NEW PAGE
RETURN
END

```

ROUTINE LPI

```

DEFINE I, SYMBOL AS INTEGER VARIABLES
DEFINE X, Y, NODE, MOBILITY.LPI, DISTANCE, SNR.L, SNR.H AS REAL VARIABLES
LET LINES = V = 80
START NEW PAGE
SKIP 4 OUTPUT LINES
PRINT 1 LINE AS FOLLOWS
  LP XMTR SNR.L SNR.H DISTANCE FOREST
SKIP 1 OUTPUT LINE
*START: READ X, Y, NODE, SYMBOL, MOBILITY.LPI
IF X EQ 9999 RETURN ALWAYS
FOR I = 1 TO N3.DF.PTS, DO
  LET TMICA.LS = 0.
  LET TMICB.LS = 0.
  LET DISTANCE = SQR T.F((X-AX(I))*2+(Y-AY(I))*2)
  CALL ELEV GIVEN X, Y YIELDING TMICA.LS
  CALL ELEV GIVEN X, Y YIELDING TMICB.LS
  CALL TREES GIVEN X, Y YIELDING TREE.A.HT
  CALL TREES GIVEN X, Y YIELDING TREE.B.HT
  IF MOBILITY.LPI EQ 1 LET TMICA.LS = TREE.A.HT ALWAYS
  IF MOBILITY.LPI EQ 1 LET TMICB.LS = TREE.B.HT ALWAYS
  LET XA.LS = X LET YA.LS = Y LET XB.LS = AX(I) LET YB.LS = AY(I)
  LET NCVELS = 0

```

```

CALL LOS
IF VISFRB.LS LE 0, CYCLE ALWAYS
LET NCVELS = TEMP.NCVELS
CALL LOS
LET WOODS = 0.0
IF VISFRB.LS LE 0.0, CALL FOREST YIELDING FOREST.PERCENT
IF FOREST.PERCENT LE 0.0 LET FOREST.PERCENT = 0.01 ALWAYS
LET WOODS = FOREST.PERCENT * DISTANCE
ALWAYS
LET SNR.L = LINK.LOSS+11-10*LOG.10.F(DISTANCE**4/(ANT.A.HT*ANT.8.HT)**2)-
WOODS*0.25*FREQ.L**0.75
LET SNR.H = LINK.LOSS+11-10*LOG.10.F(DISTANCE**4/(ANT.A.HT*ANT.8.HT)**2)-
WOODS*0.25*FREQ.H**0.75
PRINT 1 LINE WITH NODE, ***** SNR.L, SNR.H, DISTANCE, WOODS AS FOLLOWS
** **
LOOP **I**
GO TO START
END

```

ROUTINE FOR ELEV GIVEN X,Y YIELDING Z

```

**ROUTINE TO COMPUTE ELEVATION Z FOR GIVEN X,Y COORDINATES
DEFINE I,IX,IY,KOUNT,L AS INTEGER VARIABLES
DEFINE X,Y,Z,XS,YS,QI,FI AS REAL VARIABLES
DEFINE DUM,I AS A 1-DIMENSIONAL INTEGER ARRAY
LET IX=1+TRUNC.F((X-X.LO.BDRY)/GSIZE)
LET IY=1+TRUNC.F((Y-Y.LO.BDRY)/GSIZE)
IF IX LT 1 LET IX=1 ALWAYS
IF IX GT NGRIDX LET IX = NGRIDX ALWAYS
IF IY LT 1 LET IY=1 ALWAYS
IF IY GT NGRIDY LET IY = NGRIDY ALWAYS
LET DUM.I(*) = LIST.H(IX,IY,*) **DUMMY ARRAY TO SIMPLIFY INDEXING
LET KOUNT = DIM.F(DUM.I(*))
LET Z = DUM.I(1)
FOR L = 2 TO KOUNT DO
  LET I = DUM.I(L)
  LET XS=X-XC.H(I)
  LET QI=PX.XC.H(I)*XS*XS + PXY.H(I)*XS*YS
  IF QI LT CRIT.H(I) CYCLE
  ELSE LET FI=PEAK.H(I)+HT.H(I)*(EXP.F(QI)-1.)
  IF FI GT Z LET Z=FI ALWAYS
LOOP RETURN END

```

```

ROUTINE KOVER GIVEN ZO,IMACT,SIZET,ZT,S,HTS,ZS,VISFIN,YIELDING,VISFOUT
DEFINE ZO,IMACT,SIZET,ZT,S,HTS,ZS,VISFIN,VISFOUT,EVIST AS REAL VARIABLES
LET VISFOUT = VISFIN
IF S NE 0
  IF HTS GE ZS GO TO BLOCKED ELSE
    LET EVIST = MAX.F(I,IMACT,ZO+(HTS-ZO)/S)
    IF EVIST GE ZT GO TO BLOCKED ELSE
    IF EVIST LE ZT-SIZET RETURN ELSE
    LET VISFOUT = MIN.F(VISFOUT,(ZT-EVIST)/SIZET) RETURN
ELSE IF HTS LT ZO RETURN ELSE
  *BLOCKED* LET VISFOUT = 0. RETURN END

```

```

ROUTINE TREES GIVEN X AND Y YIELDING T
** ROUTINE TO COMPUTE TREE HEIGHT GIVEN A POINT ON THE BATTLEFIELD
DEFINE X,Y,T,XS,YS,QI,HT AS REAL VARIABLES
DEFINE IC,IX,IY,N,L AS INTEGER VARIABLES
DEFINE DUM,I AS A 1-DIMENSIONAL INTEGER ARRAY
LET T = 0.
IF NCVELS EQ 0 RETURN ELSE
  LET IX = 1 + TRUNC.F((X-X.LO.BDRY)/GSIZE)
  LET IY = 1 + TRUNC.F((Y - Y.LO.BDRY)/GSIZE)
  IF IX LT 1 LET IX = 1 ALWAYS
  IF IX GT NGRIDX LET IX = NGRIDX ALWAYS
  IF IY LT 1 LET IY = 1 ALWAYS
  IF IY GT NGRIDY LET IY = NGRIDY ALWAYS
  IF (IX LT 1) OR (IX GT NGRIDX) OR (IY LT 1) OR (IY GT NGRIDY) RETURN
  ELSE LET DUM.I(*) = LIST.C(IX,IY,*)

```

```

LET N = DUM.I(1) + 1
IF N EQ 1 RETURN ELSE
FOR L = 2 TO N DO
  LET IC = DUM.I(L) LET HT=HT.E(IC)
  IF HT LE 1 CYCLE
  ELSE
    XS = X-XC.E(IC) LET VS = Y-YC.E(IC)
    LET Q1 = PXX.E(IC)*XS**2 + PXY.E(IC)*XS*YS
    IF Q1 GE 1. CYCLE
    ELSE LET I = HT
  LOOP
RETURN
END

```

```

ROUTINE LOS
DEFINE I,K,N,LS,IC,M AS INTEGER VARIABLES
** ALL VARIABLES EXCEPT THOSE DECLARED ABOVE ARE GLOBAL FOR USE IN LOS AND
** ITS ASSOCIATED ROUTINES
LET VISFRA.LS = 1.0 - XA.LS LET VISFRB.LS = 1.0 LET YBA.LS = YB.LS - YA.LS
IF XBA.LS EQ 0 AND YBA.LS EQ 0 RETURN ELSE
IF (SIZEA.LS + TMICA.LS LE 0.) OR (SIZEB.LS + TMICB.LS LE 0.) GO TO NO.LOS ELSE
IF TMICA.LS LT 0. LET VISFRA.LS = 1. + TMICA.LS / SIZEA.LS ALWAYS
IF TMICB.LS LT 0. LET VISFRB.LS = 1. + TMICB.LS / SIZEB.LS ALWAYS
LET ZA.LS = TMACA.LS + TMICB.LS + SIZEA.LS
LET ZB.LS = TMACB.LS - ZA.LS ADD 1 TO IREP
LET XBASQ.LS = XBA.LS**2 LET YBASQ.LS = YBA.LS**2
LET XYBA.LS = XBA.LS * YBA.LS LET TWOYBA.LS = 2. * YBA.LS
LET TWOXBA.LS = 2. * XBA.LS LET LAGB.LS LET CHTMAX.LS = 0.
LET LAG.LS = LAGA.LS + LAGB.LS LET CHTMAX.LS = 0.
** COMPUTE LIST OF GRID SQUARES CROSSED BY A TO B LINE
LET NGRSQ.LS = 0
IF XBA.LS EQ 0. LET XBA.LS = 0.1 ALWAYS
IF XBA.LS GT 0.
  LET ISGX.LS = -1 LET XINC.LS = GSIZE/XBA.LS JUMP AHEAD
ELSE LET ISGX.LS = 1 LET XINC.LS = -GSIZE/XBA.LS
HERE IF YBA.LS EQ 0. LET YBA.LS = 0.1 ALWAYS

```

```

IF YBA.LS GT 0
  LET ISGY.LS = -1
  LET VINC.LS = -GSIZE/YBA.LS
  JUMP AHEAD
ELSE LET ISGY.LS = 1
  LET VINC.LS = GSIZE/YBA.LS
  JUMP AHEAD
HERE
  LET IX.LS = 1 + TRUNC.F((XB.LS-X.LO.BDRY)/GSIZE)
  LET IY.LS = 1 + TRUNC.F((YB.LS-Y.LO.BDRY)/GSIZE)
  LET XSTEP.LS = (XB.LS-X.LO.BDRY-GSIZE*(IX.LS-0.5*(ISGX.LS-1.0))/XBA.LS
  LET YSTEP.LS = (YB.LS-Y.LO.BDRY-GSIZE*(IY.LS-0.5*(ISGY.LS-1.0))/YBA.LS
  *GRID.LOOP
  IF (IX.LS LT 1) OR (IX.LS GT NGRIDX) OR (IY.LS LT 1) OR (IY.LS GT NGRIDY)
    JUMP AHEAD
  ELSE ADD 1 TO NGRSQ.LS
  LET IGX.LS(NGRSQ.LS) = IX.LS
  LET IGY.LS(NGRSQ.LS) = IY.LS
  HERE
  XSTEP.LS LE 1. OR YSTEP.LS LE 1.
  IF XSTEP.LS LT YSTEP.LS
    ADD ISGX.LS TO IX.LS
    ADD XINC.LS TO XSTEP.LS
    GO TO GRID.LOOP
  ELSE
    IF XSTEP.LS GT YSTEP.LS JUMP AHEAD
    ELSE ADD ISGY.LS TO IY.LS
    ADD YINC.LS TO YSTEP.LS
    GO TO GRID.LOOP
  *GRID.LIST NOW COMPLETE IN IGX.LS, IGY.LS WITH NGRSQ.LS ENTRIES
  ALWAYS *GRID.LIST EQ 0 GO TO NO.LOS ELSE
  IF NGRSQ.LS EQ 0 GO TO NO.LOS
  ** NOW FIND WHICH COVER ELLIPSES INTERSECT THE A TO B LINE
  ** AND CHECK LOS AT S1 AND S2 FOR EACH SUCH ELLIPSE
  LET NELS.LS = 0
  IF NCVELS EQ 0 GO TO HILL.PROCESSING ELSE
  FOR K = 1 TO NGRSQ.LS DO
    LET IX.LS = IGX.LS(K)
    LET IY.LS = IGY.LS(K)
    LET DUM.I(1) = LIST.C(IX.LS,IY.LS,*)
    LET N = DUM.I(1) + 1
    IF N EQ 1 CYCLE ELSE
    FOR L = 2 TO N DO
      LET IC = DUM.I(L)
      LET CPK.LS = HT.E(IC)
      IF KCREP(IC) EQ KIREP
        CYCLE ELSE
      LET RX.LS = XA.LS - XC.E(IC)
      LET RY.LS = YA.LS - YC.E(IC)
      LET PXX.LS = PXX.LS*XBASQ.LS + PXY.LS*VBASQ.LS
      LET PYY.LS = PYY.LS*XBASQ.LS + PXY.LS*VBASQ.LS
      LET AA.LS = PXX.LS*TXOXA.LS + PXY.LS*TXOYBA.LS
      LET BB.LS = PXX.LS*TXOXA.LS + PXY.LS*TXOYBA.LS
      LET CC.LS = (RX.LS*VBASQ.LS + RY.LS*XBASQ.LS)
      LET ARG.LS = BB.LS*2 - 4.0*AA.LS*CC.LS
      LET ARG.LS LE 0. CYCLE ELSE
      IF ARG.LS = SORT.F(ARG.LS)
      LET S1.LS = -(BB.LS+SQ.LS)/12.0*AA.LS)
      LET S2.LS = (SQ.LS-BB.LS)/12.0*AA.LS)

```

```

IF S1.LS GE 1.0 CYCLE ELSE
IF S2.LS LE 3.0 CYCLE ELSE
IF LAG.LS NE 0 GO TO AIR ELSE
**BOTH A AND B ARE GROUND PLATFORMS
IF S1.LS LT 0. GO TO NO.LOS ELSE
IF S2.LS GT 1. GO TO NO.LOS ELSE
**FOREST IS BETWEEN A AND B CALL TREE.CHECK
*GROUND* LET SS.LS = S2.LS CALL TREE.CHECK
LET TO SAVE = S1.LS
*AIR* GO TO SAVE = 11 AND S2.LS LE 1. GO TO GROUND ELSE
IF S1.LS LT 0. AND S2.LS LE 1. GO TO A.IS IN ELSE
IF S1.LS GE 0. AND S2.LS GT 1. GO TO B.IS IN ELSE
**BOTH A AND B ARE IN OR OVER TREES
IF LAG.LS LE 1 OR TMICA.LS LT CPK.LS OR TMICB.LS LT CPK.LS GO TO NO.LOS
ELSE GO TO SAVE.ELL
*A.IS.IN* **A IS IN OR OVER TREES B IS NOT
IF LAG.LS EQ 0 OR TMICA.LS LT CPK.LS GO TO NO.LOS ELSE
LET SS.LS = S2.LS CALL TREE.CHECK
GO TO SAVE.ELL
*B.IS.IN* **B IS IN OR OVER TREES A IS NOT
IF LAGB.LS EQ 0 OR TMICB.LS LT CPK.LS GO TO NO.LOS ELSE
LET SS.LS = S1.LS CALL TREE.CHECK
*SAVE.ELL* IF LATOB.LS EQ 1 AND VISFRB.LS LE 0. GO TO NO.LOS ELSE
IF LATOA.LS EQ 1 AND VISFRA.LS LE 0. GO TO NO.LOS ELSE
ADD 1 TO NELS.LS LET TEL.LS(NELS.LS) = IC
LET S1.LS(NELS.LS) = S1.LS LET CS2.LS(NELS.LS) = S2.LS
IF CPK.LS GT CHTMAX.LS LET CHTMAX.LS = CPK.LS ALWAYS
LOOP **BACK FOR NEXT GRID SQUARE
** ALL ELLIPSES CHECKED AND SAVED
** NOW STARTING ON THE HILLS
*HILL.PROCESSING*
FOR K = 1 TO NGRS Q.LS 00
LET IX.LS = IGX.LS(K) LET IV.LS = IGY.LS(K)
LET DUM.I(*) = LIST.H(IX.LS,IV.LS,*)
LET N = DIM.F(DJM.I(*))
LET BASE.LS = DJM.I(1)
FOR I = 2 TO N
LET I = DUM.I(1) ** GIVING THE HILL NUMBER
IF K*REP(1) EQ KTREP CYCLE ELSE
LET KHREP(1) = KILL I ALONG A TO B LINE
LET PXX.LS = PXX.H(1) LET PYY.LS = PYY.H(1) LET PXY.LS = PXY.H(1)
LET RX.LS = XA.LS - XC.H(1) LET RY.LS = YA.LS - YC.H(1)
LET GQ.LS = PXX.LS + XBASQ.LS + PYY.LS + YBASQ.LS + PXY.LS + XABA.LS
LET PQ.LS = 2.0*(PXX.LS*RX.LS + RY.LS*YBA.LS) +
PXY.LS*(RX.LS*YBA.LS + RY.LS*XBA.LS)

```

```

IF GQ.LS EQ 0.0 CYCLE ELSE
LET W.LS = -FJ.LS / (2.0*GQ.LS)
IF ABS.F(W.LS) GT 5. CYCLE ELSE
LET FQ.LS = FQ.LS*RX.LS*2 + PXY.LS*RY.LS*2 + PXY.LS*RX.LS*RY.LS
LET EQ.LS = PXX.LS - FQ.LS / (4.0*GQ.LS)
LET POW.LS = EQ.LS - 4.0 CYCLE ELSE
LET PK.LS = PEAK.H(I) LET HT.LS = HT.H(I)
LET HHW.LS = PK.LS + HT.LS*(EXP.F(POW.LS)-1.)
IF HHW.LS LE BASE.LS CYCLE ELSE
LET ZW.LS = ZA.LS + W.LS*ZBA.LS
LET W.LS = 0. OR W.LS GT 1. JUMP AHEAD ELSE
IF HHW.LS GE ZW.LS GO TO NO.LOS ELSE
IF NEL.LS EQ 0 JUMP AHEAD ELSE
LET CVHTW.LS = 0
FOR M = 1 TO NEL.LS DO
IF CS1.LS(M) GE W.LS OR CS2.LS(M) LE W.LS CYCLE ELSE
LET IC = IEL.LS(M)
IF CVHTW.LS LT HT.E(IC) LET CVHTW.LS = HT.E(IC) ALWAYS
LOOP
IF HHW.LS + CVHTW.LS GE ZW.LS GO TO NO.LOS ELSE
IF HHW.LS + CHIMAX.LS LT MIN.F(ZA.LS-SIZEA.LS,ZB.LS-SIZEB.LS) CYCLE ELSE
** IF WE GET TO HERE, THEN NEED TO FIND LOWEST SIGHT LINE OVER HILL
** NEWTON ITERATION FROM A TO B GIVING VISFRB.LS
IF LATOB.LS EQ 1
LET ZL.LS = ZA.LS + HT.LS - PK.LS LET VSUB.LS = 0.
CALL NEWTON
IF VISFRB.LS LE 0. GO TO NO.LOS ELSE
ALWAYS
** NEWTON ITERATION FROM B TO A GIVING VISFRA.LS
IF LBTOA.LS EQ 1
LET ZL.LS = ZB.LS + HT.LS - PK.LS LET VSUB.LS = 1.
CALL NEWTON
IF VISFRA.LS LE 0. GO TO NO.LOS ELSE
ALWAYS
LOOP ** BACK FOR NEXT HILL
RETURN ** BACK FOR NEXT GRID SQUARE
** NO.LOS. LET VISFRA.LS = 0. LET VISFRB.LS = 0.
ROUTINE END
DEFINE M.I.C AS INTEGER VARIABLES
** ALL VARIABLES ARE REAL AND GLOBAL EXCEPT M.I.C AS ABOVE AND
** NCT.LS, NEL.LS, IEL.LS WHICH ARE INTEGER GLOBAL
LET NCT.LS = 0
LET V.LS = W.LS LET VM.LS = V.LS - VSUB.LS
LET HHV.LS = HHW.LS + HT.LS - PK.LS
LET TWOGV.LS = 2.0*GQ.LS * V.LS

```

```

*TOP: LET FCNV.LS = ZZ.LS + HHV.LS*(FQ.LS+TWQGV.LS)*VM.LS-1.1
LET DFCNV.LS = HHV.LS*VM.LS*(TWQGV.LS**2 + 2.*(GQ.LS + TWQGV.LS*FQ.LS)+FSQ.LS)
IF ABS.(DFCNV.LS) LT 0.000000001 RETURN ELSE
LET V.LS = V.LS - FCNV.LS/DFCNV.LS
IF ABS.(F(V.LS)) GT 5. RETURN ELSE
LET VM.LS = V.LS - VSUB.LS
LET TWQGV.LS = 2.*GQ.LS*V.LS
LET POW.LS = EQ.LS + FQ.LS*V.LS + GQ.LS*V.LS**2
IF POW.LS LT -4. RETURN ELSE
LET HHV.LS = HT.LS*EXP.F(POW.LS)
LET ELV.LS = ZZ.LS + VM.LS*(HHV.LS*(FQ.LS+TWQGV.LS))
IF ABS.(F(ELV.LS - HHV.LS)) GT 1.
LET NCT.LS = NCT.LS + 1
IF NCT.LS LT 10 GO TO TOP ELSE
ALWAYS
IF V.LS LT 0. OR V.LS GT 1. RETURN ELSE
* WE HAVE A GOOD VALUE OF V -- CHECK IT FOR FOREST COVERAGE
LET CVHTV.LS = 0.
FOR M = 1 TO NELS.LS DO
IF CSI.LS(M) GE V.LS OR CS2.LS(M) LE V.LS CYCLE ELSE
LET IC = IEL.LS(M)
IF CVHTV.LS LT HT.E(IC) LET CVHTV.LS = HT.E(IC) ALWAYS
LOOP
LET HTV.LS = HHV.LS + PK.LS + CVHTV.LS - HT.LS
LET ZV.LS = ZA.LS + V.LS*ZBA.LS
IF VSUB.LS EQ 0.
CALL KOVER(ZA.LS, TMACB.LS, SIZEB.LS, ZB.LS, V.LS, HTV.LS, ZV.LS, VISFRB.LS) YIELDING
VISFRB.LS
ELSE
CALL KOVER(ZB.LS, TMACA.LS, SIZEA.LS, ZA.LS, -VM.LS, HTV.LS, ZV.LS, VISFRA.LS) YIELDING
VISFRA.LS
ALWAYS RETURN END

```



```

XXXXX INPUT DATA SEQUENCE ERROR IN COVER ELLIPSE NUMBER ***** XXXXX
ALWAYS
READ XC, YC, HT, E(I), ANG, AMAJ, AMIN
LET ANG = ANG/RADIAN.C LET SANG = SIN.F(ANG) LET CANG = COS.F(ANG)
LET PXX.E(I) = ((CANG/AMAJ)**2 + ((SANG/AMIN)**2
LET PYY.E(I) = ((SANG/AMAJ)**2 + ((CANG/AMIN)**2
LET PXY.E(I) = 2.*SANG*CANG*((1./AMAJ**2 - 1./AMIN**2)
LET XC.E(I) = XC * 100. LET YC.E(I) = YC * 100.
LET KCREP(I) = -INF.C

LOOP
FOR IX = 1 TO NGRIDX DO
FOR IY = 1 TO NGRIDY DO
READ JX, JY, KOUNT
IF IX NE JX OR IY NE JY PRINT 1 LINE WITH IX, IY AS FOLLOWS
XXXXX INPUT DATA SEQUENCE ERROR IN LIST.C DATA FOR GRID ***** XXXXX
ALWAYS RESERVE LIST.C(IX, IY, *) AS KOUNT+1
LET LIST.C(IX, IY, 1) = KOUNT
FOR I = 2 TO KOUNT + 1 READ LIST.C(IX, IY, I)
LOOP
USE UNIT 5 FOR INPUT
RETURN END

ROUTINE TREE.CHECK
LET XS.LS = XA.LS + SS.LS*XBA.LS LET YS.LS = YA.LS + SS.LS*YBA.LS
CALL ELEV GIVEN XS.LS, YS.LS YIELDING HTS.LS
ADD CPK.LS TO HTS.LS
LET ZS.LS = ZA.LS + SS.LS * ZBA.LS
IF LATOB.LS EQ 1
CALL KOVER(ZA.LS, IMACB.LS, SIZEB.LS, ZB.LS, SS.LS, HTS.LS, ZS.LS, VISFRB.LS)
YIELDING VISFRB.LS
ALWAYS
IF LBTOA.LS EQ 1
CALL KOVER(ZB.LS, IMACA.LS, SIZEA.LS, ZA.LS, 1.0-SS.LS, HTS.LS, ZS.LS, VISFRA.LS)
YIELDING VISFRA.LS
ALWAYS RETURN END

```

```

ROUTINE FOREST YIELDING FOREST.ATOB
DEFINE I AS INTEGER VARIABLE
DEFINE FOREST.ATOB,X,Y,ELEV.XY,TREE.XY,Z,Z.OT.LINE,DIF AS REAL VARIABLES
LET FOREST.ATOB = 0.0
FOR I = 1 TO 100, DO
  LET X = XA.LS + I/100*(XB.LS - XA.LS)
  LET Y = YA.LS + I/100*(YB.LS - YA.LS)
  CALL ELEV GIVEN X,Y YIELDING ELEV.XY
  CALL TREES GIVEN X,Y YIELDING TREE.XY
  LET Z = ELEV.XY + TREE.XY
  LET Z.OT.LINE = ZA.LS + I/100*(ZB.LS - ZA.LS)
  LET DIF = Z.OT.LINE - Z
  IF DIF LE 0.0, LET FOREST.ATOB = FOREST.ATOB + 0.01 CYCLE
  ALWAYS
LOOP
RETURN
END

```

```

//GO.SIMUL4 DD UNIT=2314,VOL=SER=PAT001,
// DSN=HUNTER,DISP=SHR
5000 3 74

```

```

99999 99999 99 99 9

```

```

//TGK1015 JOB (1420,0238,DC91,,15),*TRY ONE*,TIME=10
//EXEC FORTCLGM
//FORT-SYSIN DD *
C PLOT FOR 10 BY 30 KM HUNFELD TERRAIN BOX
1 DIMENSION IOPT(10),BX(7),BY(7),EX(7),EY(7),X(3600),Y(3600),
  ITR(100),ITITLE(20)
1 DATA BX/-500.,30500.,30500.,-500.,-500.,-500., 0.,1./,
  BY/-500.,-500.,10500.,10500.,-500.,-500., 0.,1./,
  EX/0.,30000.,30000.,0.,0.,0.,1./,
  EY/0.,0.,10000.,10000.,0.,0.,1./,
3 DATA LMASK1/20F0F/

C INPUT OPTIONS AS 1 = DESIRED, 0 = NOT DESIRED
C IOPT(1) -- COORDINATE GRID
C (2) -- LABEL COORDINATES
C (3) -- TERRAIN COORDINATES
C (4) -- ACCENT CONTOURS MAP
C (5) -- FORESTS SHADED
C (6) -- DRAW LINES (EG. ROUTES)
C (7) -- DRAW SYMBOLS (EG. POSITIONS)
C (8) -- TITLE

READ(5,7) IOPT
FORMAT(10,1)
C BATTLEFIELD LOWER LEFT CORNER COORDS IN METERS
XLOBY=40000.
YLOBY=10000.

C PLOT FRAME
C CALL PLOTS(0,2,0)
C CALL NEWPEN(5)
C CALL LINE(BX,BY,5,1,0,0)
C CALL LINE(EX,EY,5,1,0,0)
C CALL NEWPEN(1)

C PLOT COORDINATE GRID
C IF (IOPT(1).NE.1) GO TO 200
WRITE(6,107)
FORMAT(1,107)
CALL GRID(0.,0.,30,1000.,10,1000.,LMASK1)

C PLOT COORDINATE LABEL NUMBERS
C 107
C 200 IF (IOPT(2).NE.1) GO TO 300

```

PL000020
PL000030

PL000080
PL000090
PL000100
PL000110
PL000120
PL000130
PL000140
PL000150
PL000160
PL000170
PL000180
PL000190
PL000200
PL000360
PL000220

PL000250
PL000260
PL000270
PL000280
PL000290
PL000300
PL000310
PL000320
PL000330
PL000340
PL000350
PL000360

PL000380
PL000390
PL000400
PL000410

```

207 WRITE(6,207)
   FORMAT(1,OPTION 2 -- COORDINATE LABELS')
   CX=-100.
   CV=-315.
   CYT=10185.
   DX=-445.
   DXT=30055.
   DY=-65.
   XB=XL08Y/1000.
   YB=YL08Y/1000.
   HT=130.
   DQ 230 I=1,31
   CALL NUMBER(CX,CY,HT,XB,0.0,-1)
   CALL NUMBER(CX,CY,HT,XB,0.0,-1)
   CX=CX+1000.
   XB=XB+1
230 DQ 250 I=1,11
   CALL NUMBER(DX,DY,HT,YB,0.0,-1)
   CALL NJMBER(DXT,DY,HT,YB,0.0,-1)
   DY=DY+1000.
   YB=YB+1
250 C PLOT TERRAIN CONTJJR MAP
   C
300 IF(1OPT(3).NE.1) GO TO 500
   WRITE(6,307)
   FORMAT(1,OPTION 3 -- TERRAIN CONTOUR LINES')
307 IF (1OPT(4).EQ.1) WRITE(6,407)
407 FORMAT(1,OPTION 4 -- ACCENT 100 M. CONTOURS')
310 READ(3,317,END=390) NP,CV
317 FORMAT(15,F10.0)
327 READ(3,327) (X(I),Y(I),I=1,NP)
   FORMAT(8F10.2)
   X(NP+1)=0.
   X(NP+2)=1.
   Y(NP+1)=0.
   Y(NP+2)=1.
   Y(NP+2)=1.
   CALL NEWPEN(1)
   IF(1OPT(4).NE.1) GO TO 350
   C
   C ACCENT CONTOURS DIVISIBLE BY 100.
   C
   ICV=CV/100.
   XCV=CV-ICV*100.
   IF(ABS(XCV).LT.0.1) CALL NEWPEN(4)
350 CALL LINE(Y,X,NP,1,0,0)
   GO TO 310
   C OUT OF DATA

```

PL000420

PL000480
PL000490

PL000510
PL000520
PL000530
PL000540
PL000500
PL000550
PL000560
PL000570
PL000580
PL000590
PL000600
PL000610
PL000620

PL000630
PL000640
PL000650

PL000670
PL000680
PL000690
PL000700
PL000710
PL000720

PL000740

PL000760
PL000770
PL000780

PL000800
PL000810

```

390 CALL NEWPEN(1)
C SHADE FORESTED AREAS
C
500 IF(10PT(5).NE.1) GO TO 600
WRITE(6,517)
517 FORMAT(' OPTION 5 -- SHADE FORESTS')
HT=75.
XC=50.
DO 570 I=1, 300
READ(2,507) (1TR(J),J=1,100)
570 FORMAT(50I1,30X)
YC=50.
DO 540 J=1,100
540 IF(1TR(J).EQ.0) GO TO 520
CALL SYMBOL(XC,YC,HT, 9,0.,-1)
YC=YC+100.
520 CONTINUE
XC=XC+100.
540 CONTINUE
C PLOT LINES (EG. ROUTES)
C
600 IF(10PT(6).NE.1) GO TO 700
WRITE(6,627)
627 FORMAT(' OPTION 6 -- PLOT LINES')
CALL NEWPEN(2)
610 READ(5,607) NP
607 FORMAT(15)
IF(NP.EQ.999) GO TO 690
617 READ(5,617) (X(I),Y(I),I=1,NP)
FORMAT(8F10.0)
X(NP+1)=0.
X(NP+2)=1.
Y(NP+2)=1.
CALL LINE(X,Y,NP,1,0,0)
GO TO 610
CALL NEWPEN(1)
690
C PLOT SYMBOLS (EG. POSITIONS)
C
700 IF(10PT(7).NE.1) GO TO 800
WRITE(6,707)
707 FORMAT(' OPTION 7 -- PLOT POSITIONS')
HT = 100.
CALL NEWPEN(4)
710 READ(5,717) XC, YC, I, ISYM

```

```

PL000820
PL000830
PL000840
PL000850
PL000860

PL000870
PL000880

PL000900
PL000910
PL000920
PL000930
PL000940

PL000960
PL000970
PL000980
PL000990
PL001000
PL001010

PL001030

PL001040

```

```

717  FORMAT(F5.0,4X,F5.0,4X,12,4X,13)
      IF(1SY4.EQ.999) GO TO 800
      XC = XC - XLOBY
      YC = YC - YLOBY
      CALL SYMBOL(XC,YC,HT,ISYM,0.,-1)
      Z = 1
      XC = XC + 50.
      YC = YC + 50.
      CALL NUMBER(XC,YC,HT,Z,0.0,-1)
      GO TO 710

C  PLOT TITLE
C
800  IF(1OPT(8).NE.1) GO TO 900
      CALL NEWPEN(1)
      READ (5,807) ITITLE
      FORMAT(20A4)
      WRITE(6,817) ITITLE
      FORMAT(1,OPTION 8 -- TITLE ',20A4)
      XC=-700.
      YC=-400.
      HT=135.
      CALL SYMBOL(XC,YC,HT,ITITLE,90.0,80)
      CONTINUE
900  CALL PLOT(0.,0.,999)
      STOP
      END

//GO.PLOT Parm DD *
      &PLOT XMIN=-999.,XMAX=32000.,YMIN=-999.,YMAX=12000.,UNITS=.0254,
      SCALE=.00004,STRIP=14000. &END
      //GD.FT02F001 DD UNIT=2314,VOL=SER=PAT001,DSN=PLTHNTR,DISP=SHR
      //GD.FT03F001 DD UNIT=2314,VOL=SER=PAT001,DSN=PLTHNCL,DISP=SHR
      //GD.SYSIN DD *
      1111101100

```

```

00000 00000 02 999
HUNFELD 10 X 30 TERRAIN CONTOURS WITH FORESTS --- MARCH 1980 --- JKH

```

LIST OF REFERENCES

1. Kahn, Robert E., Gronemeyer, Steven A., Burchfiel, Jerry and Kunzelman, Ronald C., "Advances in Packet Radio Technology," Proceedings of the IEEE, v. 66, no. 11, p. 1468-1496, November 1978.
2. Naval Postgraduate School Report NPS55-79-018, Parametric Terrain and Line of Sight Modeling in the STAR Combat Model, By James K. Hartman, August 1979.
3. Ziemer, R. E. and Tranter, W. H., Principles of Communications Systems, Modulation, and Noise, Houghton Mifflin Co., 1976.
4. Okamura, Y. et al., "Field Strength Measurements and its Variability in VHF and UHF Land Mobile Radio Services," in Communication Channels: Characterization and Behavior, B. Goldberg, Ed., New York: IEEE Press, 1976.
5. Bullington, Kenneth, "Radio Propagation at Frequencies above 30 Megacycles," Proceedings of the IRE, p. 1122-1136, October 1977.
6. Jordan, E. C. and Balmain, K. G., Electromagnetic Waves and Radiating Systems, 2d ed., p. 653-654, Prentice-Hall, 1968.
7. Nathanson, Fred E., Radar Design Principles, p. 19, McGraw-Hill, 1968.
8. Saxton, J. A. and Lane, J. A., "VHF and UHF Reception Effects of Trees and other Obstacles," Wireless World, v. 61, p. 229-232, May 1955.
9. Rand Corporation Report R-1335-ARPA, Atmospheric Effects on Terrestrial Millimeter-Wave Communications, by Dudzinsky, S. J., Jr., March 1974.
10. Needels, C. J., Parameterization of Terrain in Army Combat Models, M.S. Thesis, Naval Postgraduate School, Monterey, March 1976.
11. Bond, J. E., Self Interference in a Packet Radio Network, M.S. Thesis, Naval Postgraduate School, Monterey, December 1980.

12. Georgia Institute of Technology, Atlanta Engineering Experiment GIT-A-1485-TR-4, Radar Foliage Penetration Measurements at Millimeter Wavelengths, by N. C. Currie, E. E. Martin and F. B. Dyer, December 1975.

INITIAL DISTRIBUTION LIST

	No. Copies
1. Defense Technical Information Center Cameron Station Alexandria, Virginia 22314	2
2. Library, Code 0142 Naval Postgraduate School Monterey, California 93940	2
3. Department Chairman, Code 62 Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	1
4. Professor J. M. Wozencraft, Code 74 Department of Electrical Engineering Naval Postgraduate School Monterey, California 93940	3
5. Professor J. K. Hartman, Code 55 Hh Department of Operations Research Naval Postgraduate School Monterey, California 93940	1
6. LtCol Adam Feit, IDF SMC #1073 Naval Postgraduate School Monterey, California 93940	1
7. Commander, Naval Ocean Systems Center Code 033 San Diego, California 92152	2
8. Capt. Edmund A. Lucke, USMC 2225 Montgomery Avenue Woodbridge, Virginia 22191	1
9. Capt. James E. Bond, USMC 1600 Indus Drive Woodbridge, Virginia 22191	1
10. Capt. Thomas G. Kane, USMC 407 Nob Hill Drive Stafford, Virginia 22554	3

