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USER'S MANUAL FOR THE PLUME SIGNATURE CODE EAPROF.(U)

JAN 81 S J YOUNG

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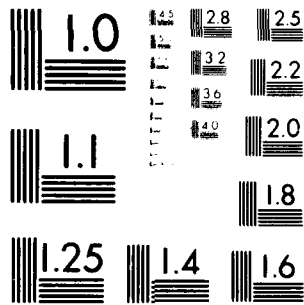
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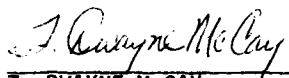
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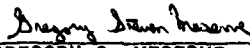
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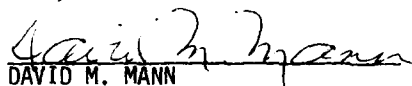
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1. INTRODUCTION

Program EAPROF (Emission Absorption Profiles) computes the transverse profiles of infrared emission and extinction for an axisymmetric, axially uniform, cylindrical plume from radial profiles of gas temperature, pressure, and concentration and particle temperature and number density. The radiation model treats gas radiation transfer with band model methods and particle radiation transfer with the single-scattering approximation. The radiation model correctly couples the gas and particle components into a single emitting, absorbing and scattering medium. The program treats just one gas species and one particle species at a time. Development of the model is made in Ref. 1.

The gas band model is the Malkmus statistical model and employs either the Curtis-Godson (CG) or derivative (DR) approximations to handle the inhomogeneity and nonisothermality of the plume. Lorentz, Doppler or Voigt line profiles may be used.

The single-scattering geometry used for particle radiation transport is shown in Fig. 1. The s -axis is the primary line of sight (LOS). (The LOS shown in Fig. 1 is the one that goes through the full plume diameter. As the LOS is scanned out across the lateral extent of the plume, it cuts progressively shorter chords of the cylindrical plume). The σ -axis is the scattering LOS.

-
1. S. J. Young, Retrieval of Flow-Field Gas Temperature and Concentration in Low-Visibility Propellant Rocket Exhaust Plumes, U.S. Air Force Rocket Propulsion Laboratory, Edwards Air Force Base, Calif. (to be published).

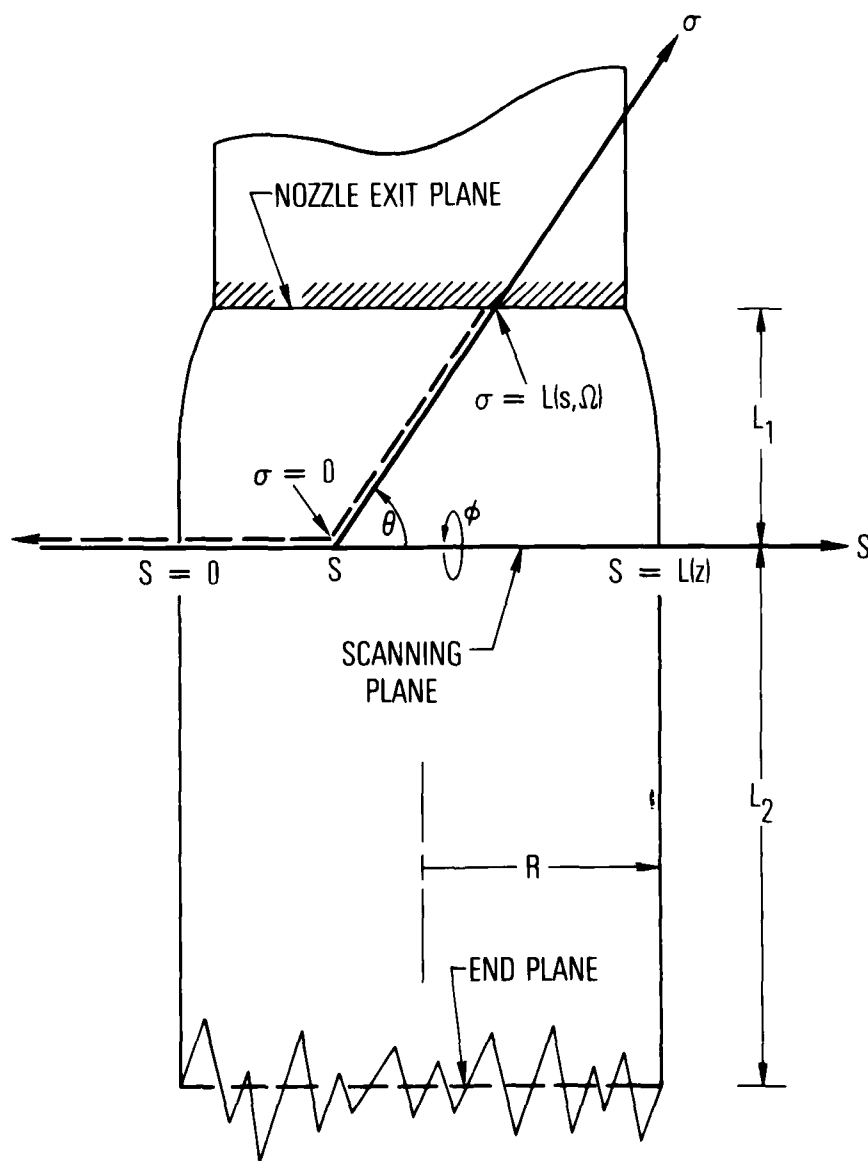


Fig. 1. Single-Scattering Plume Geometry.

It is described by the value of s where it branches off the primary LOS and by the scattering angle θ and the azimuthal angle ϕ . The single-scattering approximation includes radiation emitted along the primary LOS and radiation that has been scattered once from the scattering LOS into the primary LOS. If the scattering LOS terminates on the nozzle exit plane, motor radiation scattered into the primary LOS is also included. The exit plane is modeled as a solid disc with uniform temperature and emissivity.

Extinction of external radiation shown through the plume is assumed to be caused by gas absorption, particle absorption and particle outscattering. The single-scattering approximation does not allow inscattering to contribute to extinction calculations.

The structure of the code is described in Section 2, and a brief description of the function of each subprogram is given. Preparation of input data for the code is described in Section 3. An example application for a plume containing H_2O and Al_2O_3 as the gas and particle species, respectively, is given in Section 4. This example is taken from Ref. 1. A listing of the code is given in the Appendix.

2. CODE STRUCTURE

The organization of the code is shown in Fig. 2. EAPROF is the main program. The subroutine INPUT reads all data required for a run and processes it for compatibility with the rest of the code. The function ZONEFIT interpolates on input radial profiles and fits the data on a grid of N equal thickness radial zones. The function ANGLFIT interpolates on the input differential scattering cross section and fits the data to the scattering-angle integration grid (also part of input).

With the radial data fitted to a fixed radial grid, further interpolation is performed to fit the data to the primary and scattering lines of sight. These interpolations are performed by subroutines ZLOS and SLOS, respectively.

QTHERM is the main routine for computing the thermal radiation source function along the primary or scattering LOS. This radiation arises from gas and particle emission. The function KDPARAM interpolates for gas band model parameters along a LOS from input tables of these data. PLANCK computes the blackbody function. The remaining functions listed under QTHERM are radiation functions that are variously employed depending on the lineshape and nonuniformity modes selected for the gas radiation band model. They are described in more detail in Refs. 2 and 3.

2. S. J. Young, Description and Use of the Plume Radiation Code ATLES, SAMSO-TR-77-100, U.S. Air Force Space Division, El Segundo, Calif., 13 May 1977.
3. S. J. Young, Inversion of Plume Radiance and Absorptance Data for Temperature and Concentration, AFRPL-TR-78-60, U. S. Air Force Rocket Propulsion Laboratory, Edwards Air Force Base, Calif., 29 September 1978.

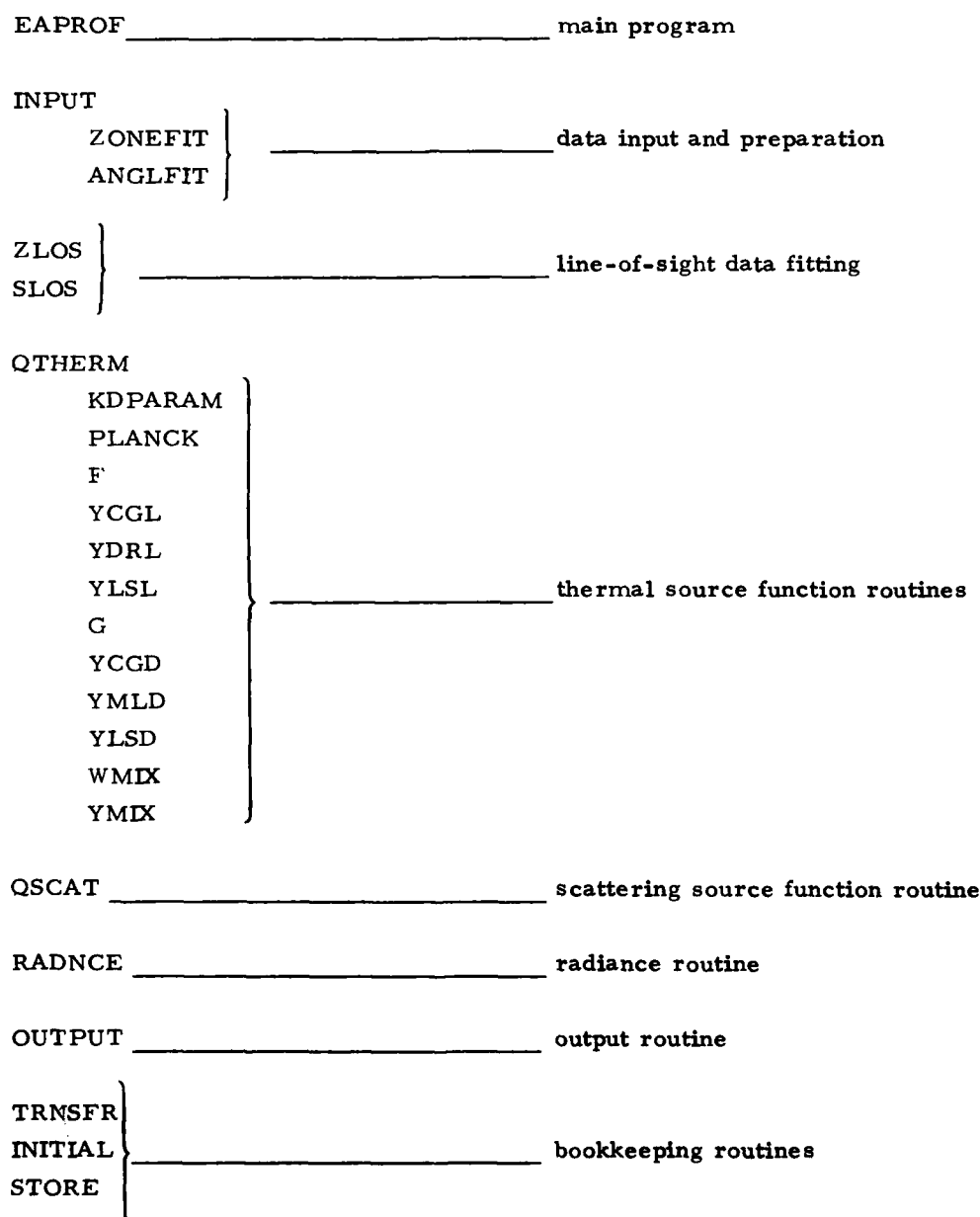


Fig. 2. Program EAPROF and Associated Subprograms.

The single-scattering source function is computed in QSCAT by an integration over all scattering angles θ and azimuthal angles ϕ . Thermal radiation from the nozzle exit plane is also treated here for scattering lines of sight that terminate on this plane.

The thermal source and scattering source functions are integrated over a LOS in subroutine RADNCE. The results are listed by OUTPUT.

The routines TRNSFR, INITIAL and STORE are bookkeeping routines.

3. PREPARATION OF INPUT DATA

A computational run of program EAPROF requires a set of program control cards to specify the mode of computation and to supply input data. Some program control cards simply specify a computation mode, some specify a computation mode and supply data, while others signal the code that blocks of auxiliary data are now to be read in. Each type of control card contains an alphanumeric name in the first ten card columns. These names must be spelled correctly and must be left-justified. If data are specified on a program control card, they must be entered in accordance with the format specification indicated in the detailed description of each card given below. All fields of the program control cards are 10 columns wide. In general, integer and alphanumeric data must be right-justified in their fields. Non-integer numerical data may be entered in either F or E formats (with decimal point and, for the latter, the exponential symbol E). E-formatted data must be right-justified in their field. These same rules apply to data entered on auxiliary card decks. The types of control cards and the data contained on them are illustrated in Fig. 3. A description of each type follows.

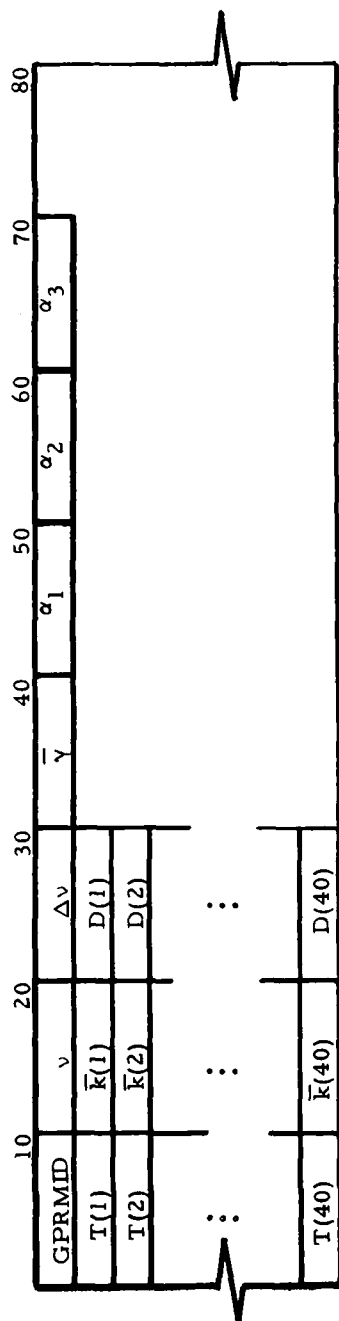
1. Title Card - The card name is TITLE. Columns 11-80 of this card may be used for any identification title desired.
2. Calculation Data Card - The card name is CALCDATA.
SHAPE (format A10) must be one of the alphanumeric values LORENTZ, DOPPLER, or VOIGT. INHOM (format A10) must have either the value CG (for the Curtis-Godson approximation) or DR (for the derivative approximation). NZONES (format I10) is the number of radial and transverse zones used by the spatial numerical integration routines. The maximum value of NZONES is 50. NSIGMA (format I10) is the number of equal-length segments that a scattering LOS is divided into for numerical integration.

TITLE	10	20	30	40	50	60	70	80
CALCDATA	SHAPE	INHOM	NZONES	NSIGMA	SFLAG			
PLMCDATA	L1	L2	TN	EN				
SPECIES	GCOL	PCOL						
GPARAM	PRINT							
GDATA	PRINT							
PPARAM	PRINT							
PDATA	PRINT							
GRID	NPHI	PRINT						
RUN								

Fig. 3. EAPROF Program Control Card Formats.

If SFLAG (format I10) has the value 1, full gas-particle calculations are carried out. If it has the value 0 (or blank), particle effects are ignored.

3. Plume Data Card - The card name is PLMDATA.
L1 (format E10) is the distance (cm) from the nozzle exit plane to the observation scanning plane. L2 (format E10) is the distance (cm) from the scanning plane to the end of the plume. TN (format E10) is the temperature (K) of the nozzle exit plane disc, and EN (format E10) is its emissivity.
4. Species Card - The card name is SPECIES. The GDATA card described under card type 6 allows the entry of up to four different gas species. The variable GCOL (format I10) on the SPECIES card selects the desired species by assuming a value of 1 to 4. Similarly, PCOL (format I10) selects one of the three particle species read in by the control card type 8 by assuming a value of 1 to 3.
5. Band Model Parameter Card - The card name is GPARAM. This card calls for the read-in of band model parameters for the gas species of interest. These parameters are listed if the variable PRINT (format A10) has the value PRINT. The card deck structure for the parameters is given in Fig. 4.
6. Gas Data Card - The card name is GDATA. This card calls for the read-in of the radial profiles of gas temperature, pressure and concentration. The required deck structure is shown in Fig. 5. If the variable PRINT (format A10) has the value PRINT, these data are listed.



All field formats are E10 or F10 except the GPRMID field which is A10.

GPRMID	Identification name.
ν	Spectral position (cm^{-1}).
$\Delta\nu$	Spectral resolution (cm^{-1}).
$\bar{Y}$	Pressure broadening coefficient ($\text{cm}^{-1}/\text{atm}$) for nonresonant self broadening at STP.
α_1	Ratio of resonant self broadening parameter to $\bar{Y}$ at STP.
α_2	Ratio of foreign gas broadening parameter to $\bar{Y}$ at STP.
α_3	Atomic weight of active gas species (amu).
T(i)	Temperature array (K). The array must be T(i) 100i, i 1, 2, ..., 40.
$\bar{k}(i)$	Absorption coefficient for ν , $\Delta\nu$ and T(i) ($\text{cm}^{-1}/\text{atm}$).
D(i)	Line density parameter for ν , $\Delta\nu$ and T(i) (lines/ cm^{-1}).
Note, $D \equiv 1/\bar{Y}$.	

Fig. 4. Input Card File Structure for Band Model Parameters.

10	20	30	40	50	60	70	80
GDTAID	N	R	GNAME1	GNAME2	GNAME3	GNAME4	
r(1)	p(1)	T(1)	c ₁ (1)	c ₂ (1)	c ₃ (1)	c ₄ (1)	
r(2)	p(2)	T(2)	c ₁ (2)	c ₂ (2)	c ₃ (2)	c ₄ (2)	
:	:	:	:	:	:	:	
:	:	:	:	:	:	:	
:	:	:	:	:	:	:	
r(N)	p(N)	T(N)	c ₁ (N)	c ₂ (N)	c ₃ (N)	c ₄ (N)	

All field formats are E10 or F10 except the GDTAID, GNAME1, GNAME2, GNAME3 and GNAME4 fields which are A10 and the N field which is I10.

GDTAID Gas data identification name.

N Number of radial points (N ≤ 201).

R Source radius (cm).

GNAME1 → GNAME4 Gas species identification names.

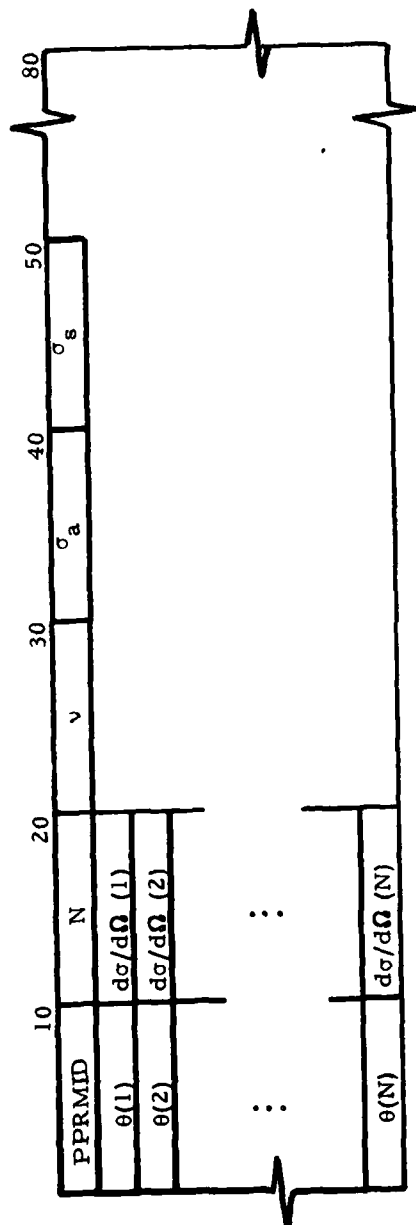
r(i) Radial positions (cm). $0 \leq r(1) < \dots < r(N) = R$.

T(i) Temperature (K) at r(i).

c_j(i) Concentration (mole fraction) of species j (j = 1, ..., 4) at r(i).

Fig. 5. Input Card File Structure for Radial Gas Data.

7. Particle Parameters Card - The card name is PPARAM. This card calls for the read-in of particle scattering data. The required deck structure is shown in Fig. 6. If the variable PRINT (format A10) has the value PRINT, these data are listed.
8. Particle Data Card - The card name is PDATA. This card calls for the read-in of the radial profiles of particle temperature and number density. The required deck structure is shown in Fig. 7. If the variable PRINT (format A10) has the value PRINT, these data are listed.
9. Angle Integration Grid - The card name is GRID. The card supplies and calls for the read in of data defining the grid over which angle integrations are carried out. NPHI (format I10) is the number of intervals over which the 360° azimuthal integration is carried out. The scattering angle integration over 180° is carried out on the grid defined in Fig. 8. If the variable PRINT (format A10) on the GRID card has the value PRINT, the scattering angle grid is listed.
10. Execution Card - The card name is RUN. When this card is encountered, computations are begun using the data entered up to that point, and an output listing of the results is made. When the computation and results listing are completed, the program continues to read program control cards until a new RUN card is encountered. A new computation is then begun for all of the conditions and data of the first run except those which have been changed by the intervening program control cards and auxiliary data decks. This process is repeated until an end-of-file card is encountered. With this feature, a large number of related runs can be made with one job submission.



All field formats are E10 or F10 except the PPRMID field which is A10 and the N field which is I10.

PPRMID Particle parameters identification name.

N Number of scattering angles ($N \leq 181$).

v Spectral position (cm^{-1}).

σ_a Absorption cross section (cm^2).

σ_s Total scattering cross section (cm^2).

θ(i) Scattering angle array (deg). 0 θ(1) < θ(2) < ... < θ(N) ≤ 180°.

dσ/dΩ(i) Differential scattering cross section for θ(i) (cm^2/sr).

Fig. 6. Input Card File Structure for Particle Scattering Parameters.

10	20	30	40	50	60	70	80
PDTAD	N	R	PNAME1	PNAME2	PNAME3		
r(1)	T ₁ (1)	c ₁ (1)	T ₂ (1)	c ₂ (1)	T ₃ (1)	c ₃ (1)	
r(2)	T ₁ (2)	c ₁ (2)	T ₂ (2)	c ₂ (2)	T ₃ (2)	c ₃ (2)	
⋮	⋮	⋮	⋮	⋮	⋮	⋮	⋮
r(N)	T ₁ (N)	c ₁ (N)	T ₂ (N)	c ₂ (N)	T ₃ (N)	c ₃ (N)	

All field formats are i10 or f10 except the PDTAD and PNAME 1 through PNAME3 fields which are A10, and the N field which is I10.

PDTAD Particle data identification name.
 N Number of radial points (N ≤ 201).
 R Source radius (cm).
 PNAME 1 → PNAME 3 Particle species identification names.
 r(i) Radial positions (cm). 0 = r(1) ≤ ... ≤ r(N) = R.
 T_j(i) Temperature (K) of species j (j = 1, ..., 4) at r(i).
 Note, if T₁(1) < 0, the particle temperature profile for the jth species is set equal to the gas temperature profile.
 c_j(i) Concentration (particles/cm³) of species j (j = 1, ..., 4) at r(i).

Fig. 7. Input Card File Structure for Radial Particle Data.

Other than the requirement that all required data be specified before a RUN card is encountered and that auxiliary data immediately follow the control card that calls for them, the program control cards may be arranged in any order.

Great care should be taken in the preparation of input data since very few checks of data consistency and setting of default values are provided. A general feature of data preparation is that, if particular data on a card are not required, they need not be specified. If none of the data on a control card is needed, that card need not be included.

4. EXAMPLE APPLICATION

An example application of EAPROF is made here for a plume containing H_2O as the active gas species and Al_2O_3 as the particle species. A discussion of this plume model is made in Ref. 1. The radial gas data are shown in Fig. 9. The particle radial profile is flat with the loading value $N_p = 10^5/cm^3$. The H_2O band model parameters are the NERD wideband parameters of Fig. 10 (Ref. 3) and are appropriate to a band center $\sim 3985\text{ cm}^{-1}$ and a bandpass of $\sim 300\text{ cm}^{-1}$. The nonresonant, self-broadening parameter is $\gamma_0 = .07394\text{ cm}^{-1}/\text{atm}$. The efficiency for resonant self-broadening is 6.53, and the efficiency for foreign gas broadening is 1.00.

Particle scattering cross sections were computed using Mie theory, the particle size distribution of Fig. 11 and the indexes of refraction $m = 2.51 - i0.0018$, $2.51 - i0.01$ and $2.51 - i0.05$. The first listed value is the accepted value for pure Al_2O_3 . The stuff of real plumes is not likely to be so pure. The two other values are simply arbitrary values selected to parametrically study the problem. The value $m = 2.51 - i0.01$ is used in this example. The results for the scattering cross sections are shown in Fig. 12.

Azimuthal integration was performed with a 16-point grid. The scattering angle integration grid and the manner in which it covers the weighting function $\sin \theta p(\theta)$ of the scattering source function integral $[p(\theta) \text{ is a scaled value of } d\sigma/d\Omega]$ are illustrated in Fig. 13.

Calculations were made for the Lorentz line shape and the CG approximation. The number of radial/transverse zones was 10, and scattering lines of sight were also divided into 10 segments for numerical integration. The distance from the exit plane to the observation plane was taken as 3 cm, and the distance from the observation plane to the end of the plume was fixed at 15 cm. The exit plane was modeled as a flat disc with uniform temperature $T = 800\text{ K}$ and emissivity $\epsilon = 0.75$.

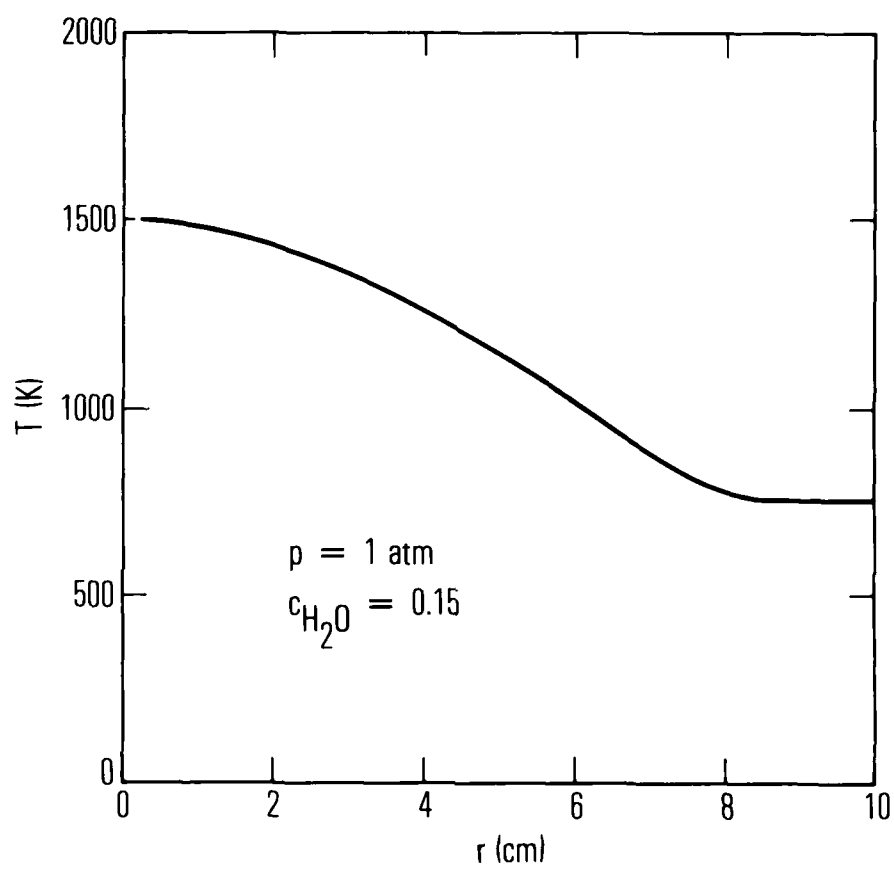
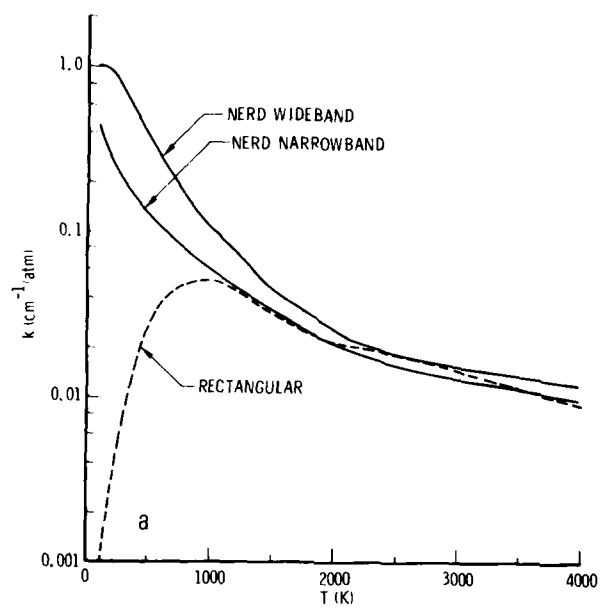
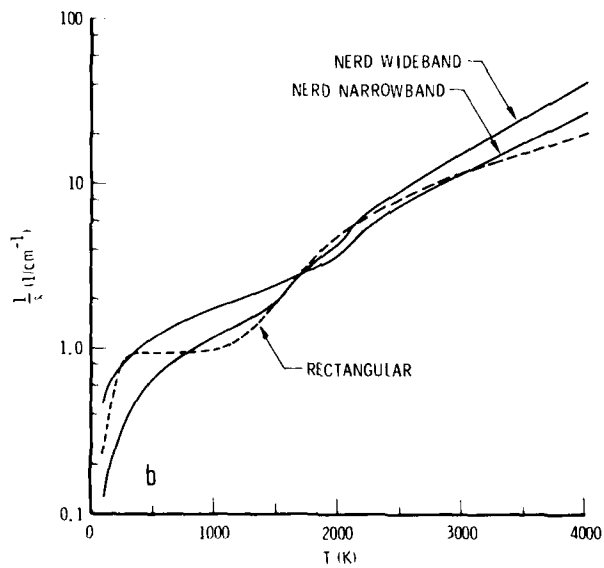


Fig. 9. Radial Gas Data.



a



b

Fig. 10. H₂O Band Model Parameters. a) Absorption Coefficient; b) Line Density.

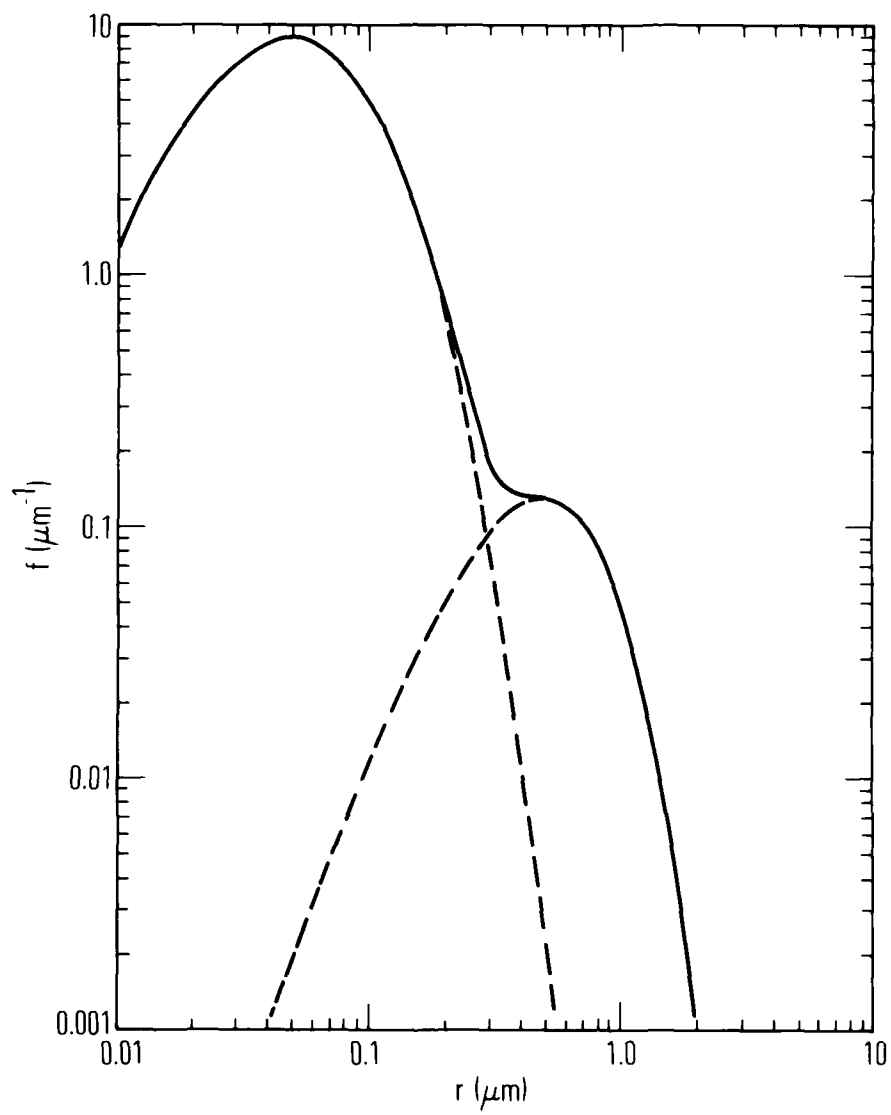


Fig. 11. Al_2O_3 Size Distribution.

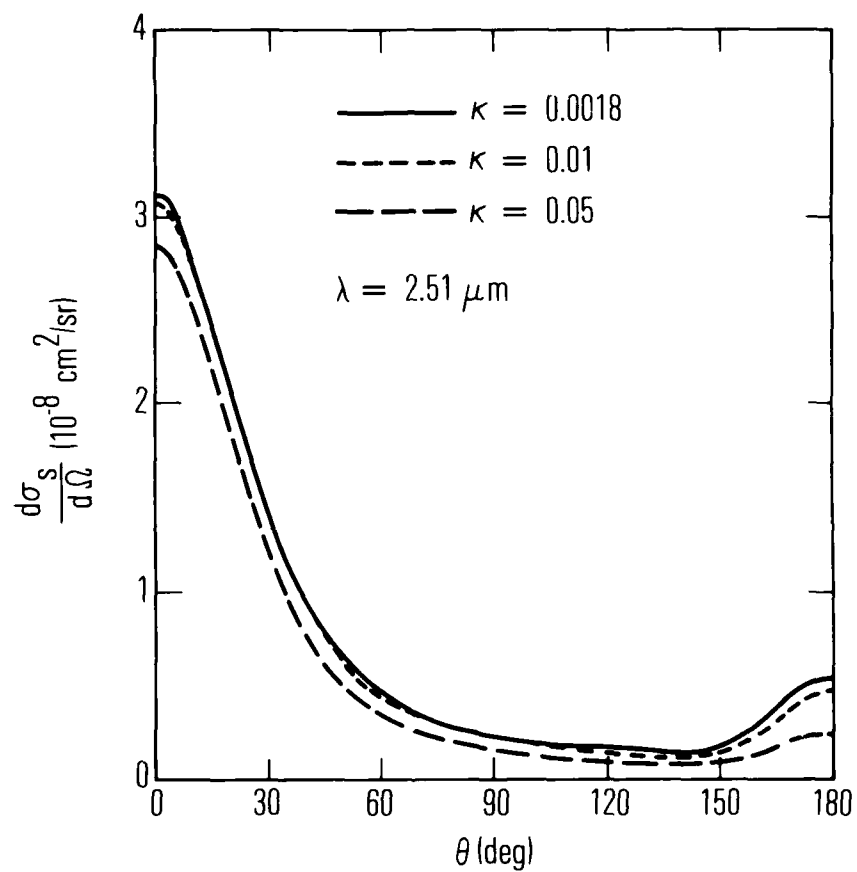


Fig. 12. Differential Scattering Cross Sections for Al_2O_3 .

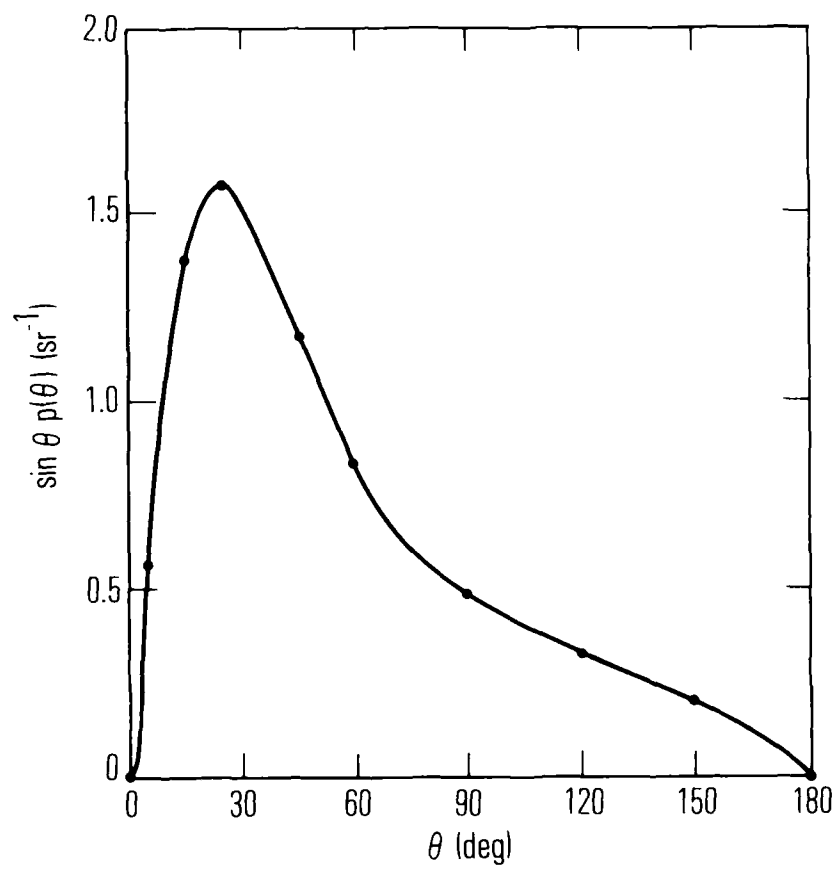


Fig. 13. Coverage of the Scattering Integral Weighting Function by the 11-Point Scattering Angle Grid.

A listing of the input data for these calculation conditions is shown in Fig. 14. The resulting output is shown in Figs. 15 and 16. Figure 16 also shows the results for computations assuming gas-only and particle only conditions. The gas-only results were obtained by changing the SFLAG value on the CALCDATA card from 1 to 0. The particle-only results were obtained by setting SFLAG back to 1 and substituting a band model parameter card deck in which the $\bar{k}$ values for all temperature were set to $\bar{k} = 10^{-40} \text{ cm}^{-1}/\text{atm}$.

Fig. 14. Input Data Listing.

HEADPROF EXAMPLE RUN -- AL2O3/H2O PLUME

```

JOB TITLE      EDIUS(CH)
SOURCE SHAPE   LINEAR
LINEAR GEN     ITY APPROXIMATION
NUMBER OF ZONES
GAS SPECIES    PARAMETER ICNAME
BAND MODEL     DNAMES
DATA ION NAME  SPECIES
PARTICLE CHARGING DATA ION NAME
SCATTERING     SCATTERING ANGLES
NUMBER OF SIGMA-AXES INTERVALS
NUMBER OF TO NOZZLE PLANE(CM)
DISTANCE FROM NOZZLE PLANE(CM)
NOZZLE VELOCITY TO END URVELOCITY
SCATTERING TEMPERATIVITY FLAG
```

*****E/A PROFILE RESULTS*****

[illegible]

Fig. 15. Output Listing.

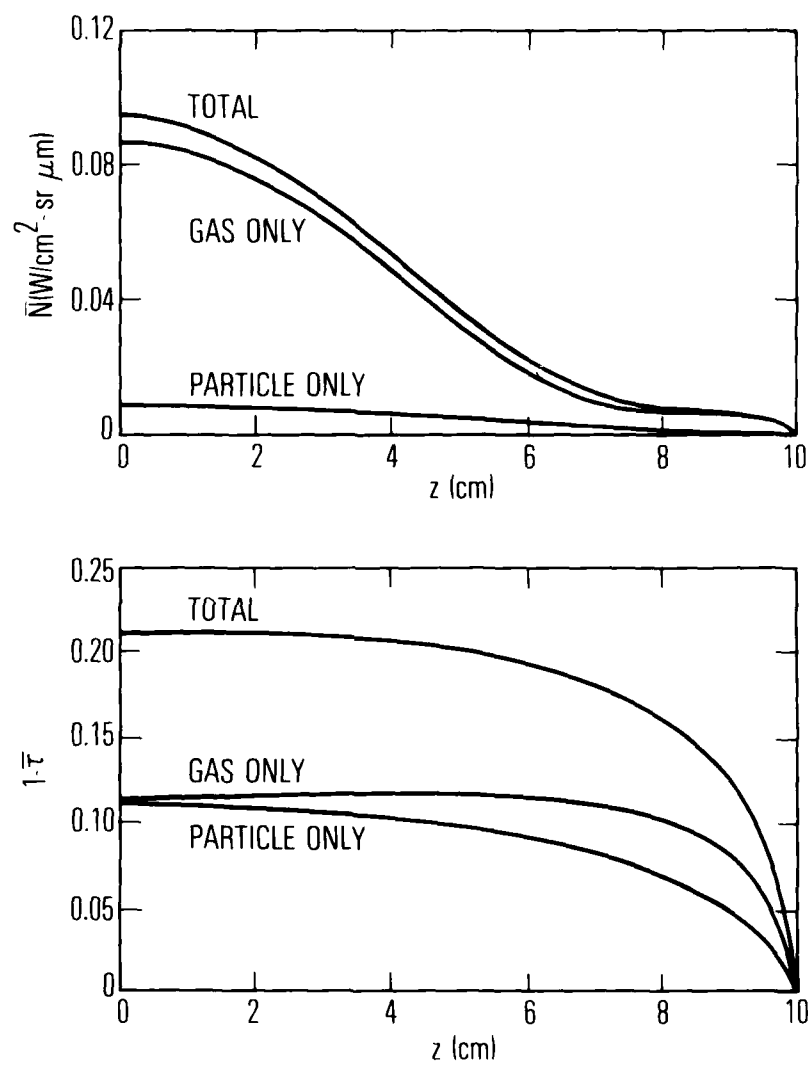


Fig. 16. Transverse Emission and Extinction Profiles.

APPENDIX

LISTING OF PROGRAM EAPROF

```

PROGRAM EAPROF(INPUT,OUTPUT,TAPE5=INPUT,TAPE6=OUTPUT)
      DIMENSION RAD(5),ABS(5)
      INTEGER SFLAG
      COMMON/OUTPT/RAD,ABS
      READ INPUT DATA
      DO 1 OVER TRANSVERSE POSITIONS
        DO 3 J=1,NZONES
          COMPUTE THERMAL SOURCE FUNCTION AND TRANSMITTANCE COMPONENTS
          CALL ZLCS(J,NLOS)
          CALL TRANSFER
          CALL INITIAL(0,NLOS)
          CALL OTHERY(I,SFLAG)
          CALL STORE
          COMPUTE SCATTERING SOURCE FUNCTION
          CALL Y(SFLAG,N,I) GO TO 2
          CALL INITIAL(I,NLOS)
          CALL QSCAT(J)
          COMPUTE LINE-OF-SIGHT RADIANCE AND EXTINCTANCE
          CALL LINESTORE
          CALL RATNCE(SFLAG,RTN1,RTN2)
          RAD(J)=RTN1
          ABS(J)=RTN2
          3 ABS(NZONES+1)=0.
          ABS(NZONES+1)=0.
        PRINT RESULTS
      END DO
      GOTO 1
      END

```


5 6 7 8 9 10 11 12 13 14 15 16 17 18 19 20 21 22 23 24 25 26 27 28 29 30 31 32 33 34 35 36 37 38 39 40 41 42 43 44 45 46 47 48 49 50 51 52 53 54 55 56 57 58 59 60 61 62 63 64 65 66 67 68 69 70 71 72 73 74 75 76 77 78 79 80 81 82 83 84 85 86 87 88 89 90 91 92 93 94 95 96 97 98 99 100

```

SUBROUTINE TRNSF2
  TRANSFER PTC VARIATION ALONG PRIMARY LOS INTO COMMON STORAGE
  LOCATION FOR SCATTERING LOS
  DIMENSION SP(113), PP(103), TGP(103), CGP(103), TPP(113), CPP(113)
  COMMON/PTCGRP/SP,PP,TGP,CGP,TPP,CGP,PP,NS
  COMMON/FTCSS/SS,PS,PS,TGS,CGS,TPS,CPS,NS
  DO 1 I=1,NP
    SS(I)=SP(I)
    PS(I)=PP(I)
    TGS(I)=TGP(I)
    CGS(I)=CGP(I)
    TPS(I)=TPP(I)
    CPS(I)=CPP(I)
  1 CONTINUE
  RETURN
END

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129      CO2=CR(I)
130      CALL PARAM(P2,TG2,CG2,K2,O2,ML2,W02)
131      DS=(S2-S1)/2
132      C COMPUTE BAND MODEL GAS TRANSMITTANCE
133      X1=CG1*F1
134      X2=CG2*F2
135      SUM1=SUM1+(X1+X2)*DS
136      U=SUM1
137      X1=X1*K1
138      X2=X2*K2
139      SUM2=SUM2+(X1+X2)*DS
140      KF=SUM2/SUM1
141      X3=X1/O1
142      X4=X2/O2
143      SUM3=SUM3+(X3+X4)*DS
144      DELE=1/O2
145      O2=SUM3/SUM2
146      DELE=DELE/CEL
147      IF (SHAPE.EQ.LORENTZ) GO TO 2
148      X3=2.12893*X1*W01*O1
149      X4=2.12893*X2*W02*O2
150      SUM4=SUM4+(X3+X4)*DS
151      Z=O=SUM4/SUM2
152      X3=U*KE/BED
153      X4=X4/X2
154      BED=BD/BED
155      IF (INMCM.EQ.OB) GO TO 1
156      Y02=YCGCL(X0,P0)
157      W02=BED*G(X0)
158      GO TO 2
159      Y02=YMLD(X0,P0,Q)
160      W02=W02*(X1+Y01+X2*Y02)*DS
161      IF (SHAPE.NE.DOPPLER) GO TO 3
162      Y2=Y02
163      W=W02
164      GO TO 7
165      X3=6.283185*X1*WL1*O1
166      X4=6.283185*X2*WL2*O2
167      SUM5=SUM5+(X3+X4)*DS
168      BEL=SUM5/SUM2
169      XL=U*KE/BEL
170      BL=X4/Y2
171      IF (INMCM.EQ.OB) GO TO 4
172      VL2=YCGCL(XL,PL)
173      WML=BL*F(XL)
174      GO TO 5
175      VL2=YORL(XL,PL,Z)
176      WML=WML*(X1+YL1+X2*YL2)*DS
177      IF (SHAPE.NE.LOPENVZ) GO TO 6
178      Y2=YL2
179      W=WML
180      GO TO 7
181      W=U*KE
182      W=MIX(W02,WML,W01)
183      Y2=YMIX(W02,WML,W01,Y02,YL2)
184      TK(L)=EXP(-M)

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RR=(I0-1)*DEL R
PR=(R-RG)/DEL R
P(L)=PR(I0)+ (TGR(I0+1)- PR(I0))*DR
TG(L)=TGR(I0)+ (TGR(I0+1)- TGR(I0))*DR
CG(L)=CGR(I0)+ (CGR(I0+1)- CGR(I0))*DR
TB(L)=TGR(I0)+ (TGR(I0+1)- TGR(I0))*DR
CALL CGR(I0)+ (CGR(I0+1)- CGR(I0))*DR
5 RETURN
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SUEROUTINE RADNCE(SFLAG,RAD,ABS)
      COMPUTE LINE OF SIGHT INTEGRAL OVER SOURCE FUNCTIONS
      DIMENSION S(103),TA(103),B(103),TK(103),2T(103),2S(103)
      COMMON/OTHPM/S,T,A,B,K,DT,NLOS
      COMMON/OSCAT/OS
      INTEGER SFLAG
      SUM=L, L=2,NLOS
      DO 1 L=2,NLOS
        OS=S(L)-S(L-1)
        P1=TA(L-1)*TK(L-1)
        P2=TA(L)*TK(L)
        S1=DT(L-1)
        S2=DT(L)
        IF(SFLAG.NE.1) GO TO 1
        P1=L*TK(L-1)
        P2=P2+TK(L)
        S1=S1+OS(L-1)
        S2=S2+OS(L)
        SUM=SUM+(P1*S1+P2*S2)*DS
      ABS=1.-F2
      AD=1./SUM
      RETURN
      END

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FUNCTION PLANCK(WN,T)
  COMPUTE THE PLANCK RADIATION FUNCTION(W/CM2*SR*CM-1) FOR
  WAVELENGTH WN(CM-1) AND TEMPERATURE T(DEGK)
  PLANCK=1.191E-12*WN**3/(EXP(1.4388*WN/T)-1.)
  RETURN
END
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FUNCTION YCGL(X,R)
  EQUIVALENT WIDTH DERIVATIVE FUNCTION FOR A BAND OF LORENTZ
  LINES WITH AN EXPONENTIAL-TAILED INVERSE LINE STRENGTH
  DISTRIBUTION AND FOR THE CURTIS-GOOSON APPROXIMATION
  YCGL=1.0
  IF (X.EQ.0.) RETURN
  Z=3.1415927*X
  XX=SQRT(1.+Z**2)
  YCGL=(2.-R)/XX*(2.-1.)*(XX-1.)/Z
  RETURN
END

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FUNCTION YCGD(X,R)
    EQUIVALENT WIDTH DERIVATIVE FUNCTION FOR A BAND OF DOPPLER
    LINES WITH AN EXPONENTIAL-TAILED INVERSE LINE STRENGTH
    DISTRIBUTION AND FOR THE CURTIS-GODSON APPROXIMATION
    YCGD=1.
    IF(X.EQ.0.) RETURN
    Z=1.415927*X
    YCGD=(2.-R)*YLSO(Z,1.)+(R-1.)*G(Z)/Z
    RETURN
END

```

YCGD

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FUNCTION YMLD(X,R,Q)
    EQUIVALENT WIDTH DERIVATIVE FUNCTION FOR A BAND OF DOPPLER
    LINES WITH AN EXPONENTIAL-TAILED INVERSE LINE STRENGTH
    DISTRIBUTION AND FOR THE MEAN-LINE DERIVATIVE APPROXIMATION
    YMLD=1.0
    IF (Q.EQ.0.) FETURN
    IF (X.EQ.0.) FETURN
    Z=3.1415927*X/Q
    YMLD=YLSQ(Z,R)
    RETURN
END

```

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[illegible]

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```

FUNCTION V*Y(WC, ML, MW, MV, YD, YL)
  COMPUTE DERIVATIVE FUNCTION Y FOR A VOIGT LINE BY A
  COMBINATION OF DERIVATIVE FUNCTIONS AND EQUIVALENT
  WIDTHS FOR PURE LORENTZ AND DOPPLER LINE SHAPES
  ACCORDING TO THE NASA HANDBOOK APPROXIMATION.

```

```

V4IX=1.0 C.O.1 RETURN
Q1=(M1/M)*2
Q2=(M2/M)*2
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Q5=(M5/M)*2
Q6=(M6/M)*2
Q7=(M7/M)*2
Q8=(M8/M)*2
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Q330=(M330/M)*2
Q331=(M
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FUNCTION F(X)
CURVE OF GROWTH FUNCTION FOR A BAND OF LORENTZ LINES
WITH AN EXPONENTIAL-TAILED INVERSE LINE STRENGTH
DISTRIBUTION.
F=0.3183099*(SORT(1.+6.283185*X)-1.)
RETURN
END

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```

W4IX=0.EQ.0.) RETURN **2+1./ (1.- (WD/WW) **2) **2-1.
W4Y=(W4I/(1.- (WL/WW) **2)- (WL/WW)) /SQR(1.-1./SQR(Y))
W4IX=W4Y**2
RETURN
END
```

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END

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