

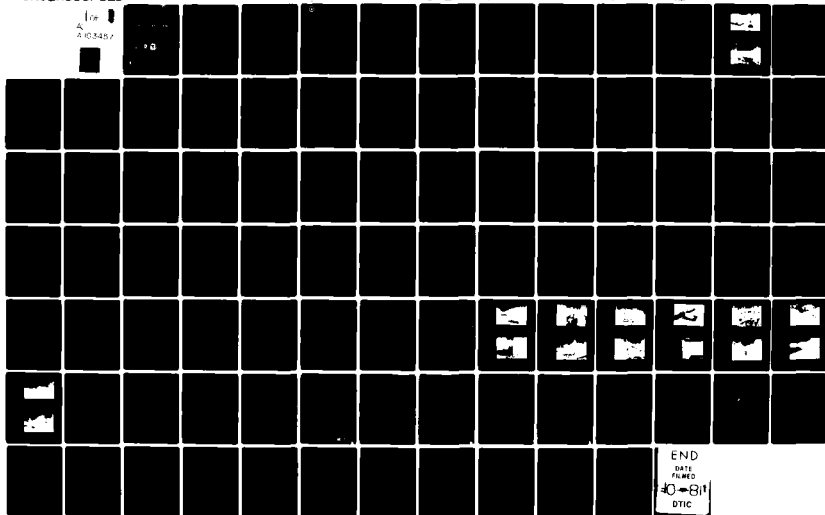
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NEW JERSEY DEPT OF ENVIRONMENTAL PROTECTION TRENTON F/8 13/13
NATIONAL DAM SAFETY PROGRAM, ECHO LAKE DAM (NJ00133), RAHWAY RI--ETC(U)
JUL 81 J J WILLIAMS DACW61-79-C-0011

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RAHWAY RIVER BASIN
NORMA HIGGIN BROOK
UNION COUNTY
NEW JERSEY

ECHO LAKE DAM

NJ 00133

PHASE 1 INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

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SELECTE
AUG 3 1 1981



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DEPARTMENT OF THE ARMY

Philadelphia District
Corps of Engineers
Philadelphia, Pennsylvania

JULY 1981

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19 REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER DAEN/NAP#53842/NJ00133-81/07	2. GOVT ACCESSION NO. AD-A103 457	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) Phase I Inspection Report National Dam Safety Program Echo Lake Dam, NJ00133 Union County, New Jersey	5. TYPE OF REPORT & PERIOD COVERED FINAL	
7. AUTHOR(s) Williams, John J.	8. CONTRACT OR GRANT NUMBER(s) DACW61-79-C-0011	
9. PERFORMING ORGANIZATION NAME AND ADDRESS O'Brien & Gere Engineers Inc. Suite 1760 1617 J.F. Kennedy Blvd. Philadelphia, PA 19103	10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS	
11. CONTROLLING OFFICE NAME AND ADDRESS NJ Department of Environmental Protection Division of Water Resources P.O. Box CN029 Trenton, NJ 08625	12. REPORT DATE 11 July, 1981	
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office) U.S. Army Engineer District, Philadelphia Custom House, 2d & Chestnut Streets Philadelphia, PA 19106	13. NUMBER OF PAGES 50	
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17. DISTRIBUTION STATEMENT Phase I Inspection Report. National Dam Safety Program. Echo Lake Dam (NJ00133), Rahway River Basin, Norma Higgin Brook, Union County, New Jersey.		
18. SUPPLEMENTARY NOTES Copies are obtainable from National Technical Information Service, Springfield, Virginia 22151.		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number)		
Dams Embankments Visual Inspection Structural Analysis	National Dam Safety Program Echo Lake Dam, N.J. Spillways	
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report cites results of a technical investigation as to the dam's adequacy. The inspection and evaluation of the dam is as prescribed by the National Dam Inspection Act, Public Law 92-367. The technical investigation includes visual inspection, review of available design and construction records, and preliminary structural and hydraulic and hydrologic calculations, as applicable. An assessment of the dam's general condition is included in the report.		



DEPARTMENT OF THE ARMY
PHILADELPHIA DISTRICT, CORPS OF ENGINEERS
CUSTOM HOUSE—2 D & CHESTNUT STREETS
PHILADELPHIA, PENNSYLVANIA 19106

IN REPLY REFER TO

NAPEN-N

11 AUG 1961

Honorable Brendan T. Byrne
Governor of New Jersey
Trenton, New Jersey 08621

Dear Governor Byrne:

Inclosed is the Phase I Inspection Report for Echo Lake Dam in Union County, New Jersey which has been prepared under authorization of the Dam Inspection Act, Public Law 92-367. A brief assessment of the dam's condition is given in the front of the report.

Based on visual inspection, available records, calculations and past operational performance, Echo Lake Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in good overall condition. The dam's spillway is considered inadequate because a flow equivalent to 27 percent of the Spillway Design Flood (SDF) would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated.

b. Within three months from the date of approval of this report the owner should engage a qualified professional consultant to perform detailed stability analyses to assess the stability of the structure and determine the need and the type of mitigating measures necessary to provide for a stable structure.

c. Within three months from the date of approval of this report the access well to the reservoir drain should be cleared of debris and the surface opening secured. The operational condition of the valve should be assessed.

d. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

NAPEN-N

Honorable Brendan T. Byrne

e. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

A copy of the report is being furnished to Mr. Dirk C. Hofman, New Jersey Department of Environmental Protection, the designated State Office contact for this program. Within five days of the date of this letter, a copy will also be sent to Congressman Rinaldo of the Twelfth District. Under the provision of the Freedom of Information Act, the inspection report will be subject to release by this office, upon request, five days after the date of this letter.

Additional copies of this report may be obtained from the National Technical Information Services (NTIS), Springfield, Virginia 22161 at a reasonable cost. Please allow four to six weeks from the date of this letter for NTIS to have copies of the report available.

An important aspect of the Dam Inspection Program will be the implementation of the recommendations made as a result of the inspection. We accordingly request that we be advised of proposed actions taken by the State to implement our recommendations.

Sincerely,



ROGER L. BALDWIN

Lieutenant Colonel, Corps of Engineers
Commander and District Engineer

1 Incl
As stated

Copies furnished:

Mr. Dirk C. Hofman, P.E., Deputy Director
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CN029
Trenton, NJ 08625

Mr. John O'Dowd, Acting Chief
Bureau of Flood Plain Regulation
Division of Water Resources
N.J. Dept. of Environmental Protection
P.O. Box CN029
Trenton, NJ 08625

ECHO LAKE DAM (NJ00133)

CORPS OF ENGINEERS ASSESSMENT OF GENERAL CONDITIONS

This dam was inspected on 24 April and 3 June 1981 by O'Brien & Gere Engineers, Inc., under contract to the U.S. Army Engineer District, Philadelphia, in accordance with the National Dam Inspection Act, Public Law 92-367.

Echo Lake Dam, initially listed as a high hazard potential structure, but reduced to a significant hazard potential structure as a result of this inspection, is judged to be in good overall condition. The dam's spillway is considered inadequate because a flow equivalent to 27 percent of the Spillway Design Flood (SDF) would cause the dam to be overtopped. To ensure adequacy of the structure, the following actions, as a minimum, are recommended:

a. The spillway's adequacy should be determined by a qualified professional consultant engaged by the owner using more sophisticated methods, procedures and studies within six months from the date of approval of this report. Within three months of the consultant's findings remedial measures to ensure spillway adequacy should be initiated.

b. Within three months from the date of approval of this report the owner should engage a qualified professional consultant to perform detailed stability analyses to assess the stability of the structure and determine the need and the type of mitigating measures necessary to provide for a stable structure.

c. Within three months from the date of approval of this report the access well to the reservoir drain should be cleared of debris and the surface opening secured. The operational condition of the valve should be assessed.

d. The owner should develop written operating procedures and a periodic maintenance plan to ensure the safety of the dam, within one year from the date of approval of this report.

e. An emergency action plan and warning system should be developed which outlines actions to be taken by the owner to minimize the downstream effects of an emergency at the dam within six months from the date of approval of this report.

APPROVED:



ROGER L. BALDWIN
Lieutenant Colonel, Corps of Engineers
Commander and District Engineer

DATE:

11 Aug 81

DELAWARE RIVER BASIN

Name of Dam: Echo Lake Dam
County and State: Union County, New Jersey
Inventory Number: 00133

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Prepared by:

O'BRIEN & GERE ENGINEERS, INC.

For:

DEPARTMENT OF THE ARMY
Philadelphia District, Corps of Engineers
Custom House-2nd & Chestnut Streets
Philadelphia, PA 19106

PREFACE

This report is prepared under guidance contained in the Recommended Guidelines for Safety Inspection of Dams, for Phase I Investigations. Copies of these guidelines may be obtained from the Office of Chief of Engineers, Washington, D.C. 20314. The purpose of a Phase I Investigation is to identify expeditiously those dams which may pose hazards to human life or property. The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigation, and analyses involving topographic mapping, subsurface investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I Investigation; however, the investigation is intended to identify any need for such studies.

In reviewing this report, it should be realized that the reported condition of the dam is based on observations of field conditions at the time of inspection along with data available to the inspection team. It is important to note that the condition of a dam depends on numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be any chance that unsafe conditions be detected.

Phase I inspections are not intended to provide detailed hydrologic and hydraulic analyses. In accordance with the established Guidelines, the Spillway Test flood is based on the estimated "Probable Maximum Flood" for the region (greatest reasonably possible storm runoff), or fractions thereof. The test flood provides a measure of relative spillway capacity and serves as an aid in determining the need for more detailed hydrologic and hydraulic studies, considering the size of the dam, its general condition and the downstream damage potential.

PHASE I REPORT

NATIONAL DAM INVENTORY PROGRAM

Name of Dam:	Echo Lake Dam ID # NJ 00133
State Located:	New Jersey
County Located:	Union
Stream:	Norma Higgin Brook
Coordinates:	Latitude N40°40.7', Longitude W74°20.1'
Dates of Inspection:	April 24 and June 3, 1981

ASSESSMENT

Echo Lake Dam is a concrete gravity structure about 130 feet long and 20 feet high. The surface area of the impoundment at normal pool is approximately 11 acres while storage capacity at maximum stage is estimated to be 69 acre-feet. Based on visual observations made during the field investigations, the structure appears to be in good condition.

Echo Lake Dam is classified as a "Small" size structure (height less than 40 feet, storage at maximum pool less than 1,000 acre-feet). The hazard potential for this dam is judged to be "Significant". The Spillway Design Flood (SDF) selected for this dam is fifty percent of the Probable Maximum Flood (PMF). A review of the hydrologic/hydraulic analyses indicates that the spillway is capable of passing about 13 percent of the PMF prior to overtopping the abutments. The Spillway is classified as "Inadequate".

Stability analyses were performed for the spillway sections of the dam. A review of these analyses indicates that the dam does not meet structural stability requirements with regard to resultant location as outlined in the Department of the Army publication Recommended Guidelines for Safety Inspection of Dams.

The Owner should retain the services of a licensed professional engineer experienced in the design and construction of dams to assist in complying with the following recommendations and remedial measures.

The recommendations and remedial measures which should be initiated very soon are as follows:

a. Facilities

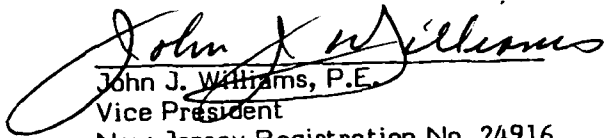
1. Detailed hydrologic and hydraulic analyses should be performed to determine the need and type of mitigating measures necessary to provide adequate spillway capacity.
2. Detailed stability analyses should be performed to assess the stability of the structure and determine the need and the type of mitigating measures necessary to provide for a stable structure.

3. The access well to the reservoir drain valve should be cleared of debris and the surface opening secured. The operational condition of the valve should be assessed.

b. Operation and Maintenance Procedures

1. A regular maintenance program should be developed and implemented.
2. An emergency action plan should be developed which outlines actions to be taken by the Owner to minimize the downstream effects of an emergency.

O'BRIEN & GERE ENGINEERS, INC.


John J. Williams, P.E.
Vice President
New Jersey Registration No. 24916

Date: 29 July 1981



OVERVIEW OF ECHO LAKE DAM FROM THE RIGHT ABUTMENT. (4/24/81)



UPSTREAM OVERVIEW OF ECHO LAKE DAM FROM THE LEFT ABUTMENT.
(4/24/81)

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PHASE I INSPECTION REPORT
NATIONAL DAM INSPECTION PROGRAM
ECHO LAKE DAM
INVENTORY NUMBER NJ 00133

SECTION 1

PROJECT INFORMATION

1.1 General

a. Authority. This report is authorized by the Dam Inspection Act, Public Law 92-367, and has been prepared in accordance with contract # DACW 61-80-D-0013 between O'Brien & Gere Engineers, Inc. and the United States Army Corps of Engineers, Philadelphia District.

b. Purpose of Inspection. The purpose of this inspection is to evaluate the structural and hydraulic condition of Echo Lake Dam and appurtenant structures and to determine if the dam constitutes a hazard to human life or property.

1.2 Project Description (Based on information provided by the New Jersey Department of Environmental Protection (NJDEP), Union County Park Commission (UCPC) and supplemented by field observations).

a. Description of Dam and Appurtenances. Echo Lake Dam is a concrete gravity overflow structure approximately 20 feet high and 130 feet long. The structure ties in at both abutments with concrete retaining walls. All exposed faces of the structure and retaining walls have been faced with cobble size stones set into the concrete.

An ornamental waterwheel is located near the left abutment. A diversion channel is constructed from the impoundment about 20 feet upstream of the dam to the waterwheel. A control gate is located at the end of the diversion channel immediately upstream of the waterwheel. The outlet channel downstream of the waterwheel, which is about 80 feet long, discharges into the pool downstream of the dam.

A reservoir drain structure is constructed in the right sidewall and abutment. The intake which extends into the impoundment is submerged. The 24-inch diameter ductile iron outlet pipe protrudes from the right side retaining wall about 7 feet downstream of the dam. Access to the control valve is by means of a vertical well, six inches in diameter located in the top of the right side retaining wall. The valve is operated by a long handled wrench which is stored by park personnel.

The spillway discharges into a pool which is formed by a small dam (about five feet high and 32 feet long) located about 100 feet downstream of the Echo Lake Dam. A small island is located in the center of the pool. A concrete cut-off wall, three feet deep by one foot wide is constructed about 35 feet downstream of Echo Lake Dam. The area between the dam and the cut-off wall is filled with riprap.

Flows from the small lower dam discharge onto an apron surfaced with riprap. A concrete cutoff wall about three feet deep by one foot wide is located at the downstream end of the 10-foot long apron.

b. Location. Echo Lake Dam is located in Union County, New Jersey in the Borough of Mountainside on Norma Higgin Brook. The dam site is shown in the USGS Quadrangle entitled "Roselle, New Jersey" at coordinates N 40° 40.7', W 74° 20.1'. A regional location map for Echo Lake Dam is enclosed as Figure 1, Appendix E.

c. Size Classification. Echo Lake Dam has a maximum height of approximately 20 feet and a maximum storage capacity of 69 acre-feet. Accordingly, it is classified as a "Small" size dam (height less than 40 feet, storage less than 1,000 acre-feet).

d. Hazard Classification. A restaurant is located about 200 feet left of Norma Higgin Brook an estimated 1,300 feet downstream of the dam. The floor elevation of this structure is about eight feet above the streambed. The retail store for a nursery is located about 300 feet right of Norma Higgin Brook an estimated 1,300 feet downstream of the dam. The floor elevation of the structure is about 9 feet above the streambed. Failure of the dam could possibly cause loss of life and appreciable damage in this area. Therefore, the dam is classified in the "Significant" hazard potential category.

e. Ownership. The dam is owned by the Union County Park Commission, Union County, New Jersey. Records are maintained by Union County, New Jersey, Department of Engineering and Planning.

f. Purpose of Dam. The dam was constructed to provide a lake for recreation.

g. Design and Construction History. Based on a review of information provided by the New Jersey Department of Environmental Protection (NJDEP), the original dam at the site was completely washed out as a result of an intense rainfall and subsequent flooding in July, 1938. The spillway for this structure was reported to have been about 60 feet long with one foot of freeboard.

The dam was replaced in 1939 in conjunction with the Public Works Administration effort. A construction drawing entitled "Echo Lake Park" dated November, 1938 was provided by the Owner and is reproduced in Appendix E as Figure 4. The spillway for this structure was 70 feet long with 2.8 feet of freeboard. This dam failed in August, 1973, as a result of intense rainfall and subsequent flooding.

The structure was reconstructed in 1975. A set of design drawings (two sheets) entitled "Walls at Lower Dam Across Norma Higgin Brook, Echo Lake Park", dated June 6, 1974 and January 9, 1975, were provided by the Owner. Both drawings are reproduced in Appendix E as Figures 2 and 3. The spillway was reconstructed to a length of 130 feet with approximately 2.8 feet of freeboard.

The configuration of the reconstructed dam is that of a retaining wall. No calculations relative to structural stability were provided. A review of boring logs indicates that the base of the dam may be founded on material which might be susceptible to piping and underdrainage.

h. Normal Operating Procedures. According to the Owner's representative, no restraint to flow over the spillway exists. The gate at the end of the sealed off diversion channel is in the closed position and is no longer used. The reservoir drain has not been operated since 1975.

1.3 Pertinent Data.

a. <u>Drainage Area.</u> (Square Miles)	2.5
b. <u>Discharge at Dam Site.</u> (CFS)	
Elevation 94.6 (low point, top of abutments)	1,280
c. <u>Elevations.</u> (Feet above NGVD)	
Spillway Crest 18 foot length	92.6
86 foot length	92.7
26 foot length	92.8
Low Point Top of Abutments	94.6
Reservoir Drain Invert	82.0
Streambed at Toe of Dam	80.0
Tailwater	+81.0
Base of Structure	+73.0
Diversion Channel to Waterwheel	+90.0
d. <u>Reservoir Length.</u> (Feet)	
Normal Pool Elevation 92.6	2,700
Low Point Top of Abutments Elevation 94.6	2,900
e. <u>Reservoir Storage.</u>	
Normal Pool, Elevation 92.6	45
Low Point Top of Abutment, Elevation 94.6	69
f. <u>Reservoir Surface Area.</u> (Acres)	
Normal Pool, Elevation 92.6	10.7
Low Point Top of Abutment, Elevation 94.6	13.5
g. <u>Dam.</u>	
Type	Concrete Gravity Overflow
Length	+130 feet
Height (above foundation)	+20 feet
Crest Width	7 inches

Slopes
Zoning
Impervious Core
Cut off
Grout Curtain

Refer to sheets 2 and 3, Appendix E
N/A
N/A
None
None

h. Diversion and Regulating Structure.

The diversion channel to the ornamental waterwheel is four feet wide and 12 feet long. The channel, which has an invert of approximately Elevation 90, is presently sealed off immediately upstream of the waterwheel.

i. Reservoir Drain.

The reservoir drain is a 24-inch diameter ductile iron pipe. The intake structure is submerged. The outlet protrudes from the right side retaining wall seven feet downstream of the dam. Access to the control valve is by means of a six-inch diameter vertical well. The top of the well is set in the crest of the retaining wall immediately above the pipe outlet.

SECTION 2
ENGINEERING DATA

2.1 Design.

a. Data Available. The engineering data provided includes the following:

1. Construction drawing entitled "Echo Lake Park" dated November 12, 1938. (Reproduced in Appendix E, Sheet 4.)
2. Construction drawings entitled "Walls at Lower Dam across Norma Higgin Brook, Echo Lake Dam Park" drawings numbered 24 and 25 of 25 (Reproduced in Appendix E, Sheets 2 and 3).
3. Hydraulic calculations prepared by Frank H. Lehr Associates.

b. Design Features. The principal design features for this structure are discussed in Section 1.2.a and shown on the drawings enclosed in Appendix E.

2.2 Construction.

No progress reports relative to the construction of the dam nor "as built" drawings were provided for review.

2.3 Operation.

According to the Owner's representative, Mr. Michael J. Cerra, Chief Engineer/Parks, no operational features are associated with this structure. The reservoir drain valve has not been operated since the time of reconstruction of the dam in 1975.

2.4 Evaluation.

a. Availability. The engineering data utilized in this report was provided by the Owner, Union County Park Commission (UCPC) and the New Jersey Department of Environmental Protection (NJDEP).

b. Adequacy. Based on the information provided by the NJDEP, the Owner and observations made during the field inspection, adequate information is available for a Phase I evaluation.

c. Validity. There is no reason to question the validity of the data provided.

SECTION 3

VISUAL INSPECTION

3.1 Findings.

a. General. Echo Lake Dam was inspected on April 24 and June 3, 1981. At the time of the inspections, the water surface elevation was less than 0.1 feet above the spillway crest. The observations and comments of the field inspection team are presented in Appendix B of this report. Elements of the structure which are under water were not inspected. The overall appearance of the dam is good.

b. Dam. The horizontal and vertical alignment of the dam appeared to be consistent with the construction drawings provided by the Owner. No settlement or displacement was evident. Water was discharging over 18 feet of the spillway length of from 26 to 44 feet from the left side retaining wall. The upstream face of the dam could not be observed because it was submerged. Some debris was evident along the spillway crest. The debris was essentially limited to leaves and brush.

No evidence of seepage was noted on the downstream face of the dam or at the dam and abutment junctions. The joints in all the stone masonry elements of the structure appear to be intact. No structural cracking was noted.

c. Appurtenant Structures.

The abutments of the dam are stabilized by retaining walls similar in appearance to the dam. The retaining walls extend upstream and downstream of the dam and appear to be in general conformance with the construction drawing provided by the Owner and reproduced in Appendix E, Sheets 2 and 3. The walls vary in height with the maximum wall height being about 15 feet above the water surface immediately downstream of the dam. No deflection or settlement in the walls was noted. Weepholes are located in the bottom half of the walls downstream of the dam. No flow was noted in the weepholes.

Most of the reservoir drain structure is not visible; however, no discharge was observed at the outlet. The Owner was unable to open the drain valve at the time of the inspection because the access well was filled with debris. According to the Owner's representative, the valve is not exercised regularly and has not been activated since completion of the reconstruction in 1975.

d. Reservoir Area.

The reservoir side slopes vary from a few percent up to a maximum of about 2H:1V. The perimeter grounds are well maintained in a grass and natural vegetative cover.

e. Downstream Channel.

The spillway discharges into a lower pool (lagoon) which is formed by a five-foot high by 32-foot long dam about 100 feet downstream from Echo Lake Dam. No settlement or displacement was noted in the aprons of either dam or in the lower dam. The channel downstream of both dams averages about 20 feet in width with about 4-foot high banks and side slopes approximating 1H:1V. Very little debris or obstructions were observed in the downstream channel.

SECTION 4
OPERATIONAL FEATURES

4.1 Procedures.

Based on a conversation with the Owner's representative, no formal operating procedures are established for Echo Lake Dam.

4.2 Maintenance of Dam

According to the Owner's representative, maintenance is performed on an "as required" basis.

4.3 Maintenance of Operating Facilities.

Based on a review of drawings provided by the Owner, the diversion channel to the ornamental waterwheel is sealed off immediately upstream of the waterwheel.

Based on a conversation with the Owner's representative, the reservoir drain is an operating part of the dam. Based on all information available, the drain was last utilized when the dam was reconstructed in 1975. An attempt was made by the Owner's representative to exercise the drain control valve during the field inspections; however, the vertical access well to the stem was clogged with debris and the effort was unsuccessful.

4.4 Description of Warning System in Effect.

According to the Owner's representative, no warning system, formal or informal, is in effect for Echo Lake Dam.

4.5 Evaluation of Operational Adequacy.

It is not known if the reservoir drain system is operational.

It appears that the dam is accessible under all weather conditions.

SECTION 5

HYDROLOGY AND HYDRAULICS

5.1 Evaluation of Features.

a. Design Data. Based on a review of the design data provided, the drainage area contributing to Echo Lake Dam is 2.5 square miles. The maximum length of the basin is about 2.5 miles and the maximum width is about 1.5 miles. Elevations within the basin vary from a maximum of about Elevation 480 to Elevation 92.6 at normal pool. The normal surface area of the lake is 10.7 acres and the associated storage is 45 acre feet. With the impoundment at the low point of the top of the dam Elevation 94.6, the storage capacity is 69 acre-feet and the spillway discharge capacity is 1,280 cfs. Most of the watershed is urbanized.

The spillway was designed to pass a flood flow of 1,150 cfs at a head of 1.8 feet with a freeboard of 1.0 feet. According to the material provided by the Owner's representative, the structure is designed for the one-hundred year event.

b. Experience Data. According to the Owner's representative, no records of reservoir stage or rainfall are maintained for this dam. It takes about 4 days to drawdown the reservoir. Refer to drawdown calculations to Appendix C.

c. Visual Observations. At the time of the inspection, some debris was accumulated at the spillway crest. The vertical access well to the reservoir control valve was obstructed with debris. The operational condition of the valve could not be assessed.

d. Overtopping Potential. Echo Lake Dam is classified as "Small" size, "Significant" hazard structure. Accordingly, the Spillway Design Flood (SDF) for this structure ranges from the one-hundred year flood to fifty percent of the Probable Maximum Flood (PMF). The SDF selected for use is fifty percent of the PMF.

The SDF hydrograph was developed using an SCS unit hydrograph which was routed through the reservoir with the starting water surface elevation at the spillway crest (Elevation 92.6). The peak inflow and outflow rates for the SDF were computed to be about 6,760 and 6,480 cfs, respectively. The maximum reservoir stage for this event is 3.1 feet above the low point of the top of the abutment and the duration of overtopping is about 5.2 hours. The spillway is capable of discharging approximately 13 percent of the PMF prior to overtopping the embankment (refer to Appendix C for computations and printout).

e. Spillway Adequacy. The spillway is considered "Inadequate" since it is not capable of discharging the SDF.

SECTION 6

STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations. The overall appearance of the dam at the time of the inspection was good. The horizontal and vertical alignment of the dam appeared to be consistent with the construction drawings provided by the Owner. No settlement or displacement was evident. The upstream face of the dam could not be observed because it was submerged.

No evidence of seepage was noted on the downstream face of the dam or at the dam and abutment junctions. The joints on all the masonry elements of the structure appear to be intact. No structural cracking was noted.

b. Design and Construction Data.

Sheets 2, 3 and 4 of Appendix E were provided by the Owner's representative. These drawings are the extent of the design and construction data which was provided to assist in preparation of this report.

c. Operating Records. According to the Owner's representative, no operating records are maintained for this dam.

d. Post-Construction Changes. Based on all available information, no records exist of any post-construction changes subsequent to the reconstruction of the dam in 1975.

e. Seismic Stability. Echo Lake Dam is located in Seismic Zone 1 on the Seismic Zone Map of Contiguous States. Spillway sections represented by Section A-A on Sheet 2 of Appendix E and Section C-C on Sheet 3 of Appendix E were analyzed for seismic stability with the water in the impoundment at the spillway crest Elevation 92.6 and no tailwater. Full uplift conditions varying from the impoundment elevation at the upstream end to the base of the dam at the downstream end were assumed for the analyses. The spillway sections meet the stability requirements for Zone 1 Seismic loading conditions according to the criteria outlined in the Recommended Guidelines for Safety Inspection of Dams. Refer to Appendix G for the seismic stability calculations.

f. Structural Stability. Spillway sections represented by Section A-A on Sheet 2 of Appendix E and Section C-G on Sheet 3 of Appendix E were analyzed for structural stability with the water in the impoundment at the spillway crest Elevation 92.6 and no tailwater. Full uplift conditions, varying from the impoundment elevations at the upstream end to the base of the dam at the downstream end were assumed for the analyses. The resultant of forces is located outside the middle third of the base for both sections. The criteria outlined in the Recommended Guidelines for Safety Inspection of Dams states that the resultant should be located within the middle third of the base width. Refer to Appendix G for the structural stability calculations.

SECTION 7

ASSESSMENT, RECOMMENDATIONS AND PROPOSED REMEDIAL MEASURES

7.1 Dam Assessment

a. Evaluation. Based on the visual inspection, Echo Lake Dam is judged to be in good condition. The access well to the reservoir drain is blocked with debris. It is not known if the valve is operational.

The selected SDF for Echo Lake Dam is fifty percent of the PMF. Based on the analyses performed for this report, the spillway is capable of passing 13 percent of the PMF prior to overtopping the abutment. The spillway is, therefore, classified as "Inadequate".

Seismic and structural stability analyses were performed for the spillway sections. Based on these analyses, the spillway sections of the dam meet the criteria for seismic stability but do not meet the requirements for structural stability according to the criteria outlined in the Recommended Guidelines for Safety Inspection of Dams.

b. Adequacy of Information. Based on the information provided by the NJDEP, the Owner and observations made during the field investigation, adequate data is available for a Phase I evaluation.

c. Urgency. The remedial measures recommended in Section 7.2 should be initiated very soon.

d. Necessity for Further Investigation. Further investigations should be performed in accordance with 7.2a, numbers 1 and 2.

7.2 Recommendations and Remedial Measures

The Owner should retain the services of a licensed professional engineer experienced in the design and construction of dams to assist in complying with the following recommendations and remedial measures.

Recommendations and remedial measures which should be initiated very soon are as follows:

a. Facilities

1. Detailed hydrologic and hydraulic analyses should be performed to determine the need and type of mitigating measures necessary to provide adequate spillway capacity.
2. Detailed stability analyses should be performed to assess the stability of the structure and determine the need and the type of mitigating measures necessary to provide for a stable structure.

3. The access well to the reservoir drain should be cleared of debris and the surface opening secured. The operational condition of the valve should be assessed.

b. Operation and Maintenance Procedures

1. A regular maintenance program should be developed and implemented.
2. An emergency action plan should be developed which outlines actions to be taken by the Owner to minimize the downstream effects of an emergency.

APPENDIX

A

Check List Engineering Data
Design, Construction, Operation
Phase I

CHECK LIST
ENGINEERING DATA
DESIGN, CONSTRUCTION, OPERATION
PHASE I

NAME OF DAM Echo Lake Dam
ID # NJ 00133

Sheet 1 of 4

ITEM

REMARKS

AS-BUILT DRAWINGS

Not available

REGIONAL VICINITY MAP

Refer to Appendix E, Figure 1

CONSTRUCTION HISTORY

No information available.

TYPICAL SECTIONS OF DAM

Refer to Appendix E, Figures 2 and 3

OUTLETS - PLAN

DETAILS

CONSTRAINTS

Refer to Appendix E, Figures 2 and 3

DISCHARGE RATINGS

None available

RAINFALL/RESERVOIR RECORDS

None available

ITEM	REMARKS
DESIGN REPORTS	None available.
GEOLOGY REPORTS	Boring logs (2 holes) were made available (Refer to Appendix F). The locations of the holes are unknown.
DESIGN COMPUTATIONS HYDROLOGY & HYDRAULICS DAM STABILITY SEEPAGE STUDIES	Limited information was made available relative to hydrology and hydraulics (Refer to section 5.1 a). No information relative to dam stability or seepage studies was made available.
MATERIALS INVESTIGATIONS BORING RECORDS LABORATORY } FIELD }	Refer to Appendix F for boring logs.
POST-CONSTRUCTION SURVEYS OF DAM	None available.
BORROW SOURCES	N/A

ITEM	REMARKS
MONITORING SYSTEMS	None
MODIFICATIONS	Refer to Section 1.2g.
HIGH POOL RECORDS	None available.
POST CONSTRUCTION ENGINEERING STUDIES AND REPORTS	None available.
PRIOR ACCIDENTS OR FAILURE OF DAM DESCRIPTION REPORTS	Refer to Section 1.2g.
MAINTENANCE OPERATION RECORDS	None available.

ITEM	REMARKS
SPILLWAY PLAN	
SECTIONS	Refer to Appendix E, Figures 2 and 3
DETAILS	
OPERATING EQUIPMENT PLANS & DETAILS	Refer to Appendix E, Figures 2 and 3
MISCELLANEOUS	

APPENDIX

B

Check List

Visual Inspection

Phase I

CHECK LIST
VISUAL INSPECTION
PHASE I

Sheet 1 of 8

Name Dam Echo Lake Dam County Union State New Jersey National ID # NJ 00133
Type of Dam Concrete Gravity Hazard Category Significant
Date(s) Inspection 4/24/81 Weather Cloudy w/rain Temperature 60 degrees
(6/2/81) (4/24/81) (4/24/81)

Pool Elevation at Time of Inspection 92.65 ± M.S.L. Tailwater at Time of Inspection 81 ± M.S.L.

Inspection Personnel:

L.R. Beck L.DeHeer (6/2/81)
J.F. Rauschkolb
R.E. Horvath R.E. Horvath Recorder

Remarks:

The inspection team was accompanied by Mr. Michael J. Cerra, Chief Engineer/Parks,
County of Union, New Jersey, Department of Engineering and Planning. (4/24/81)

CONCRETE/MASONRY DAMS

Sheet 2 of 8

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
ANY NOTICEABLE SEEPAGE	None observed	
STRUCTURE TO ABUTMENT/EMBANKMENT JUNCTIONS	No seepage or evidence or relative movement was noted. Minor erosion was evident at the left abutment. The erosion appears to be a result of foot traffic.	
DRAINS	No drains are evident in the dam. However, weepholes were noted in the retaining walls downstream of the dam. No flow was observed coming from any of the weepholes.	
WATER PASSAGES	A diversion channel to an ornamental water wheel is sealed. Surfaces visible appear to be in good condition.	
FOUNDATION	Not observed.	

CONCRETE/MASONRY DAMS

Sheet 3 of 8

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
SURFACE CRACKS CONCRETE SURFACES	None observed.	
STRUCTURAL CRACKING	None observed.	
VERTICAL AND HORIZONTAL ALIGNMENT	No evidence of settlement or deflection was noted.	
MONOLITH JOINTS	No leakage or evidence of movement was noted.	
CONSTRUCTION JOINTS	No leakage or evidence of movement was noted.	

OUTLET WORKS

Sheet 4 of 8

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CRACKING AND SPALLING OF CONCRETE SURFACES IN OUTLET CONDUIT	Not observed.	
INTAKE STRUCTURE	Submerged.	
OUTLET STRUCTURE	A 24 inch diameter cast iron pipe protrudes from retaining wall (right side) about 5 feet downstream of the dam. Only the outlet end is visible.	
OUTLET CHANNEL	Reservoir drain discharges to the spillway channel.	
EMERGENCY GATE	24 inch gate valve. Access well to gate is blocked with debris.	The well should be cleared of all debris.

UNIGATED SPILLWAY

Sheet 5 of 8

VISUAL EXAMINATION OF	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
CONCRETE WEIR	Surfaces appear to be in good condition.	
APPROACH CHANNEL	Impoundment.	
DISCHARGE CHANNEL	The spillway discharge channel is lined (with riprap and stone set in concrete) for a distance of about 100 feet downstream. A small dam is constructed at this location to form a plunge pool.	
BRIDGE AND PIERS	N/A	

INSTRUMENTATION

Sheet 16 of 8

VISUAL EXAMINATION	OBSERVATIONS	REMARKS OR RECOMMENDATIONS
--------------------	--------------	----------------------------

MONUMENTATION/SURVEYS

N/A

OBSERVATION WELLS

N/A

WEIRS

N/A

PIEZOMETERS

N/A

OTHER

N/A

RESERVOIR

Sheet 7 of 8

REMARKS OR RECOMMENDATIONS

OBSERVATIONS

VISUAL EXAMINATION OF

SLOPES

The impoundment is in a park environment. Maximum slopes are about 2 horizontal to one vertical and appear to be well maintain with a grass cover.

SEDIMENTATION

Not observed or assessed.

DOWNSTREAM CHANNEL

Sheet 8 of 8

REMARKS OR RECOMMENDATIONS

OBSERVATIONS

VISUAL EXAMINATION OF

CONDITION
(OBSTRUCTIONS,
DEBRIS, ETC.)

The downstream channel is the natural stream. The channel is approximately 4 feet deep and 20 feet wide with 1 horizontal to 1 vertical sideslopes. Very little debris or obstructions were observed in the channel.

SLOPES

The channel overbanks are relatively flat.

APPROXIMATE NO.
OF HOMES AND
POPULATION

A restaurant is located about 1,000 feet downstream of the dam. The floor elevation of this structure is located about 8 feet above the streambed. A number of inhabited homes are also located downstream of the dam. However, the floor elevations of these homes appear to be less critical than elevation of the restaurant.

APPENDIX

C

Hydrologic & Hydraulic Data

ECHO LAKE DAM
APPENDIX C
HYDROLOGIC AND HYDRAULIC
ENGINEERING DATA

TABLE OF CONTENTS

	<u>Sheet No.</u>
PMP Data	1
Lag Time Computation, Upper Reservoir	1 through 2
Lag Time Computations, Echo Lake	4 and 5
Stage-Area Computations, Upper Reservoir and Echo Lake	6
Upper Reservoir Stage-Discharge Computations	7
Echo Lake Stage-Discharge Computations	8
Stage-Discharge & Stage Storage Curves for Echo Lake Dam	9
Profile Top of Dam	10
Drawdown Analysis	11 and 12
HEC-1, Dam Safety Version, Computer Printout	13 through 18



SUBJECT	ECHO LAKE DAM - H/H	SHEET	1	BY	JFR	DATE	5-4-81	JOB NO	1800-006
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6/5/81

HYDROLOGY CALCULATIONS

Drainage Area = 12.49 sq. mi.

Upper Reservoir D.A. = 1.79 sq. mi.

Lower Reservoir (Echo Lake) D.A. = 0.70 sq. mi.

PMP DATA - HMS REPORT 33

Area is in Zone 6 of PMP ALL Season Envelope.

24 hr., 200 sq. mi. Rainfall = 22.5 in.

Storm Distribution

Hr.	%
6	113
12	124
24	132
48	142

BASIN LAG TIME - Upper Reservoir

1. SCS Upland Method:

Greatest hydraulic distance to upper reservoir consists of 5000 ft. of overland flow and 4500 ft. of stream flow.

$$\text{Avg. overland slope} = \frac{\Delta E I.}{d_o} = \frac{480 - 130}{5000} \times 100 = 7\%$$

Paved area & small upland gullies, $V_o = 5.3$ fps
(Fig 15.2, Pg 15-8, SCS NEH-4)

$$t_o = \frac{5000}{5.3} = 943 \text{ sec.} = 0.26 \text{ hr.}$$



SUBJECT

ECHO LAKE DAM - H₁'H

SHEET

2

BY

JFR

DATE

5-7-81

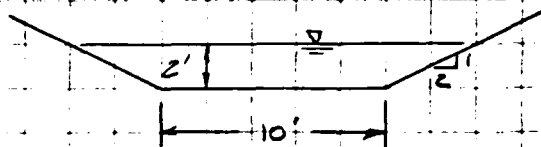
JOB NO

1800-006

v.f. 6/5/81

$$\text{Avg. stream slope} = \frac{130 - 98}{4500} = 0.007 \frac{\text{ft.}}{\text{ft.}}$$

$$\begin{aligned} V_s &= \frac{1.49}{n} R^{2/3} S^{1/2} \\ &= \frac{1.49}{.05} (1.48)^{2/3} (.007)^{1/2} \\ &= 3.2 \text{ fps} \end{aligned}$$



$$\begin{aligned} t_s &= \frac{4500}{3.2} = 1406 \text{ sec.} \\ &= 0.39 \text{ hrs.} \end{aligned}$$

$$n = .05, R = 18.9'$$

$$A = 28 \text{ ft}^2$$

$$T_c = 0.26 + 0.39 = 0.65 \text{ hr.}$$

$$\text{Lag, } L = 0.6 T_c = .6 (.65) = 0.39 \text{ hr.}$$

2. SCS Curve Number Method:

$$L = \frac{l^8 (S+1)^7}{1900 Y^5}$$

$$S = \frac{1000}{CN} - 10 = \frac{1000}{90} - 10 = 1.1$$

$$l = 9500 \text{ ft.}$$

$$Y = \frac{430 - 98}{9500} \times 100 = 4\%$$

$$L = \frac{(9500)^8 (1.1 + 1)^7}{1900 (4)^5} = 0.68 \text{ hr.}$$



3. California Highways Method:

$$T_c = \left(\frac{11.9 L^3}{H} \right)^{0.385}$$

$$L = 9500 / 5280 = 1.80 \text{ mi.}$$

$$H = \Delta E.L. = 480 - 98 = 382 \text{ ft.}$$

$$T_c = \left(\frac{11.9 (1.80)^3}{382} \right)^{0.385} = 0.52 \text{ hrs.}$$

$$L = 0.6 (0.52) = 0.31 \text{ hrs.}$$

4. Kenby Method:

$$T_c = \left(\frac{L}{3} \frac{L_n}{\sqrt{s}} \right)^{.467}$$

$$L = 9500'$$

$$n = 0.05$$

$$s = 0.04 \text{ ft/ft}$$

$$T_c = \left(\frac{L}{3} \frac{(9500)(.05)}{\sqrt{.04}} \right)^{.467} = 31 \text{ min.}$$

$$L = 0.6 (31/60) = 0.31 \text{ hrs.}$$

→ USE SCS LAG, $L = \underline{\underline{0.39 \text{ Hour.}}}$
(Lagging Method)



SUBJECT	SHEET	BY	DATE	JOB NO.
ECHO LAKE DAM - H.F.H	4	JFR	5-8-81	1800-006

✓ J

6/5/81

BASIN LAG TIME - ECHO LAKE

1. SCS Upland Method:

Greatest hydraulic distance to Echo Lake consists of 3000 ft. of overland flow.

$$\text{Avg. slope} = \frac{\Delta E}{d} = \frac{150 - 93}{3000} \times 100 = 1.9\%$$

Paved area & small upland gullies, $V = 2.8$ fps
(Fig 15.2, Pg 15-8, SCS IEH 4)

$$T_c = \frac{3000}{2.8} = 1071 \text{ sec.} = 0.30 \text{ hr.}$$

$$L = 0.6 T_c = 0.6 (.30) = 0.18 \text{ hr.}$$

2. SCS Curve Number Method:

$$L = \frac{l^8 (S+1)^7}{1900 Y^5}$$

$$S = \frac{1000}{90} - 10 = 1.1$$

$$l = 3000 \text{ ft.}$$

$$Y = 1.9\%$$

$$L = \frac{(3000)^8 (2.1)^7}{1900 (1.9)^5} = 0.39 \text{ hr.}$$



SUBJECT

ECHO LAKE DAM - H₂H

SHEET

5

BY

JFR

DATE

5-8-81

JOB NO

1900-006

✓ 3/4

6/5/81

3. California Highways Method:

$$T_c = \left(\frac{11.9 L^3}{H} \right)^{.385}$$

$$L = 3000 / 5280 = 0.57 \text{ mi.}$$

$$H = 150 - 93 = 57 \text{ ft.}$$

$$T_c = \left(\frac{11.9 (.57)^3}{57} \right)^{.385} = 0.29 \text{ hr.}$$

$$L = 0.6 T_c = 0.6 (.29) = 0.17 \text{ hr.}$$

4. Kerby Method:

$$T_c = \left(\frac{2}{3} \frac{L^n}{\sqrt{S}} \right)^{.467}$$

$$L = 3000'$$

$$n = .04$$

$$S = 0.019 \text{ ft/ft}$$

$$T_c = \left(\frac{2}{3} \frac{(3000)(.04)}{\sqrt{0.019}} \right)^{.467} = 19.5 \text{ min.}$$

$$L = 0.6 T_c = 0.6 (19.5 / 60) = 0.20 \text{ hr.}$$

→ USE SCS LAG, $L = \underline{\underline{0.18 \text{ hr.}}}$
(Upland Method)

**O'BRIEN & GERE**

SUBJECT	ECHO LAKE DAM - H/H	SHEET	6	BY	JFR	DATE	5-4-81	JOB NO	1800-006
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VJ

6/5/81

AREA - ELEVATION DATA, UPPER RESERVOIR

<u>W.S. ELEV.</u>	<u>AREA *</u>
97.65 (Norm. Pool)	8.0 ac.
100	18.7 ac.
120	33.0 ac.
140	59.7 ac.

AREA - ELEVATION DATA, ECHO LAKE

<u>W.S. ELEV.</u>	<u>AREA *</u>
80.0	0
92.65 (Norm. Pool)	10.7 ac.
100	27.3 ac.
120	80.6 ac.
140	684.6 ac.

* Planimetered from USGS Quad Sheets

**O'BRIEN & GERE**

SUBJECT

Echo Lake Dam - H&H

SHEET

7

BY

REH

DATE

5/11/81

JOB NO

1800.006.113

V.P. 4/5/81

HYDRAULICSFOR SPILLWAY AT UPPER RESERVOIRCrest Width = 2', Freeboard $\approx$ 4'

Crest Length = 60'

WSE	H (ft)	C	Q (cfs)
97.65	0	2.6	-
98.65	1	2.8	168
99.65	2	3.3	560
100.65	3	3.3	1029
101.65	4	3.3	1384
102.65	5	3.3	2214
103.65	6	3.3	2910
104.65	7	3.3	3667
105.65	8	3.3	4480

For overtopping, use 500 feet, $C = 2.6$ overtopping elevation $\approx$ 101.65



O'BRIEN & GERE

SUBJECT	SHEET	BY	DATE	JOB NO
Echo Lake Dam - H&H	8	REH	5/11/81	1800.006.113

✓

6/5/81

HYDRAULICS (Cont.)For Echo Lake Dam - Spillway

Based on a review of available drawings, the spillway crest elevation varies from 92.65 to 92.83, approximately 2 inches. For the hydrologic/hydraulic analyses, elev. 92.65 has been used for the full spillway length.

Crest Length = 130 feet

Crest elev = 92.65

Crest width = 7 inch

Coeff of Discharge C - from Hbk of Hydraulics, Table 5-11, slope of upstream face $\approx 2H:1V$

WSE	H(ft)	C	Q(cfs)
92.65	0	—	—
93.65	1	3.4	442
94.65	2	3.6	1324
95.65	3	3.7	2499
96.65	4	3.7	3848
97.65	5	3.7	5378
98.65	6	3.7	7069
99.65	7	3.7	8908
100.00	7.35	3.7	9585



O'BRIEN & GERE

SUBJECT

ECHO LAKE DAM - H.F.H

SHEET

9

BY

JFR

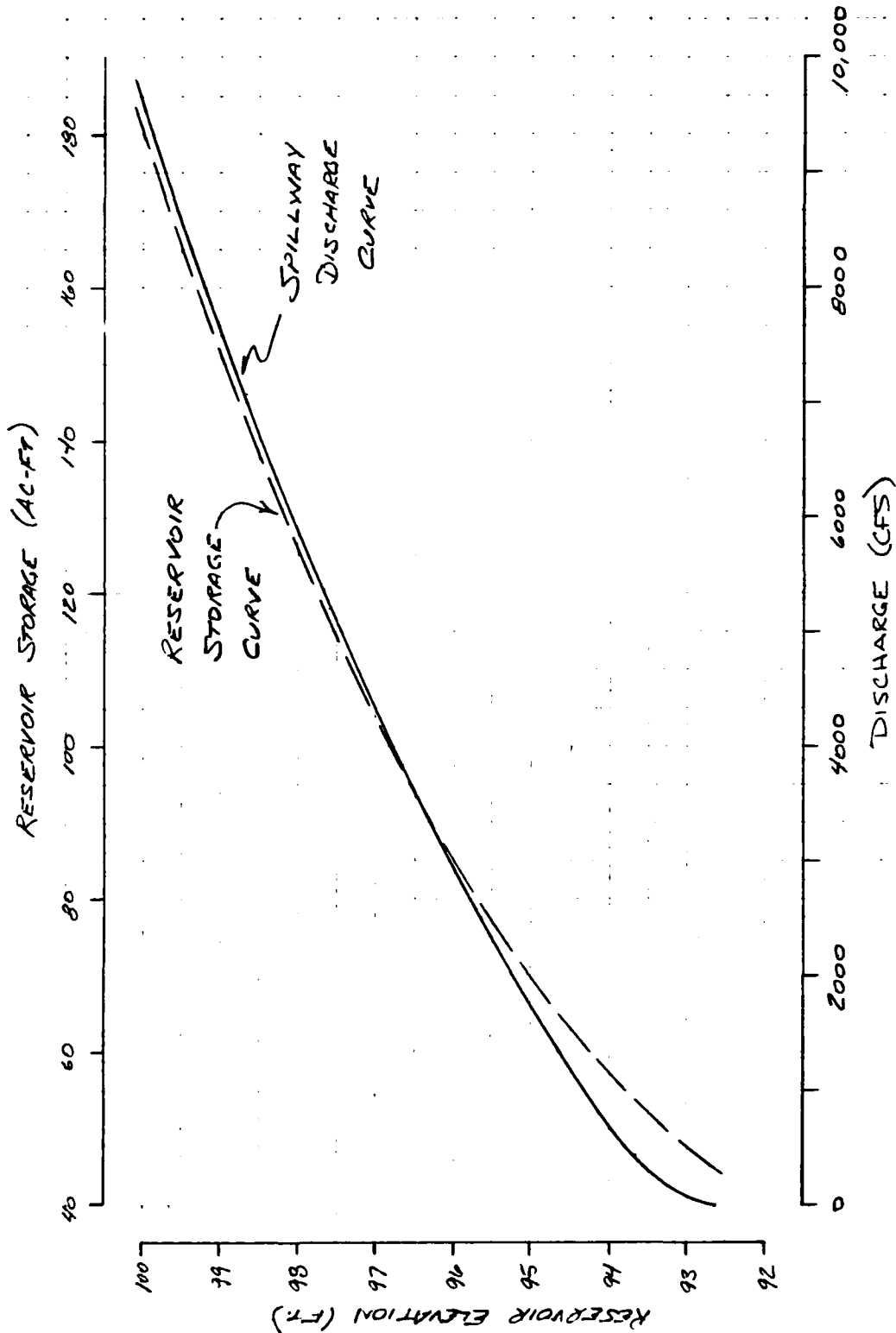
DATE

7-27-81

JOB NO

1800-006-113

STAGE DISCHARGE / STORAGE ECHO LAKE DAM





O'BRIEN & GERE

SUBJECT

Echo Lake Dam - H & H

SHEET

10

BY

REH

DATE

5/11/81

JOB NO

1800.006.113

✓ 6/5/81

For Overtopping

4400

3000

2000

1400

97.4

95.4

95.6

95.3

95.0

Spillway L=130

Looking Downstream

94.6

\$ L	0	8'	95'	115'	125'	130'	135'
\$ V	94.6	95	96	97	98	99	100

Spillway length not included.

scale 1" = 50' horiz
1" = 5' vert



SUBJECT	ECHO LAKE DAM - H/H	SHEET	11	BY	JFR	DATE	7-28-81	JOB NO	1800-006-113
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DRAWDOWN ANALYSIS24-inch ϕ reservoir drain - ductile iron pipeLength $\approx 54'$ 2 bends @ 90° 1 bend $> 90^\circ$

Outlet invert @ EL. 82.0, Inlet invert @ EL. 84.0

$$Q = \sqrt{\frac{2gH}{1 + K_e + EK_b + 29n^2L/R^{1.33}}} A_p$$

$$K_e \approx 0.5$$

$$EK_b \approx 0.2 + 0.2 + 0.1 = 0.5$$

$$n = 0.013$$

$$R = \frac{\pi(1)^2}{\pi(2)} = 0.50$$

$$Q = \sqrt{\frac{2(32.2)H}{1 + 0.5 + 0.5 + 29(.013)^2(54)/(0.5)^{1.33}}} \pi(12/12)^2$$

$$Q = 16.66 H^{1/2}$$

$$\text{Volume} = 970.89 (h_2^3 - h_1^3) \text{ ft}^3 \quad \dots \text{integration of vol. cone}$$

$$t = \frac{V}{Q} \quad \text{seconds}$$

$$\text{Normal Pool Elev.} = 92.65$$

$$\begin{aligned} \text{Base Flow} &= 1.5 \text{ cfm} \times 2.49 \text{ s.mi.} \\ &= 3.75 \text{ cfs} \end{aligned}$$

(OVER)

$$Q_{\text{NET}} = Q - 3.75$$



SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM - H&H	12	JFR	7-28-81	1800-006-113

DRAWDOWN (CONT'D)

RESERVOIR ELEVATION	ΔV (ft ³)	H _{AVG} (ft)	Q _{NET} (cfs)	t (sec)
92.65 - 92.0	287,659	9.325	47	6120
92.0 - 91.0	385,443	8.5	45	8565
91.0 - 90.0	321,364	7.5	42	7652
90.0 - 89.0	263,111	6.5	39	6746
89.0 - 88.0	210,683	5.5	35	6020
88.0 - 87.0	164,080	4.5	32	5123
87.0 - 86.0	123,303	3.5	27	4567
* { 86.0 - 85.0	88,351	2.5	17	5197
85.0 - 84.0	59,224	1.5	0.2	296,120

* Pipe flows partially full

@ AVG W.S.E. 85.5 , $R = 2.5274 / 5.9208 = 0.427$

$$Q = \left[\frac{64.4 H}{2 + 29 (.013)^2 (54) / (.427)^{1/3}} \right]^{1/2} 2.5274 = 13.38 H^{1/2}$$

@ AVG W.S.E. 84.5 , $R = .6142 / 3.8264 = 0.161$

$$Q = \left[\frac{64.4 H}{2 + 29 (.013)^2 (54) / (.161)^{1/3}} \right]^{1/2} .6142 = 3.22 H^{1/2}$$

Drawdown Time (to EL. 85) = $\frac{49,595}{3600} = \underline{\underline{14 \text{ hours}}}$

Drawdown Time (to EL. 84) = $\frac{346,115}{86,400} = \underline{\underline{4 \text{ Days}}}$

NATIONAL DAM INSPECTION PROGRAM
ECHO LAKE DAM
PMF HYDROGRAPH

JOB SPECIFICATION
NR 300 NHR 0 NMIN 10 IDAY 0 IHR 0 IMIN 0 METRC 0 IFLT 0 IPRT 0 NSTAN 0
JOPER 5 NWT 0 LROFT 0 TRACE 0

MULTI-PLAN ANALYSES TO BE PERFORMED

RTIOS= .10 .15 .20 .25 .30 .35 .40 .50 1.00
NPLAN= 1 NR110= 9 LRTIO= 1

SUB-AREA RUNOFF COMPUTATION

RUNOFF HYDROGRAPH FROM UPSTREAM DRAINAGE AREA

ISTAQ ICOMP IECON ITAPE JFLT JPRT INAME ISTAGE IAUTO
LAKE 1 0 0 0 0 0 1 0 0

HYDROGRAPH DATA

IHYDG 1 IUNG 2 TAREA 1.79 SNAP 0.00 TRSDA 2.49 TRSFC 0.00 RATIO 0.000 ISNOW 0 ISAME 1 LOCAL 0

PRECIP DATA

SFPE PMS R6 R12 R24 R48 R72 R96
0.00 22.50 113.00 124.00 132.00 142.00 0.00 0.00

TRSPC COMPUTED BY THE PROGRAM IS 1800

LOSS DATA

LROFT 0 STNR 0.00 ULTR 0.00 KTIOL 1.00 ERAIN 0.00 STKS 0.00 RTIOK 1.00 STATE 1.00 CNSTL 0.05 ALSHX 0.00 RTIMP 0.00

UNIT HYDROGRAPH DATA

TC= 0.00 LAG= .39

RECESSION DATA

SIRTO= -1.50 ORCSN= -.05 RTIOR= 2.00

END-OF-PERIOD FLOW

MO.DA HR.MN PERIOD RAIN EXCS LOSS COMP Q MO.DA HR.MN PERIOD RAIN EXCS LOSS COMP Q

SUM 25.56 23.17 2.39 164552.
(649.)(589.)(61.)(4659.59)

54 14

HYDROGRAPH ROUTING

ROUTING THROUGH UPSTREAM RESERVOIR

ISTAQ	ICOMP	IECON	ITAPE	JPLT	JPRI	INAME	ISTAGE	IAUID
DAM-1	1	0	0	0	0	1	0	0
QLOSS	CLOSS	AVG	IRTS	ISAME	IOPT	IPMP	LSTR	
0.0	0.000	0.00	1	1	0	0	0	
NSTPS	NSFIL	LAG	AMSKN	X	TSK	STORA	ISPRAT	
1	0	0	0.000	0.000	0.000	-98,	-1	
STAGE	97.65	98.65	99.65	100.65	101.65	102.65	103.65	104.65
FLOW	0.00	168.00	560.00	1029.00	1584.00	2214.00	2910.00	3667.00
SURFACE AREA	8.	19.	33.	60.				4480.00
CAPACITY	0.	30.	54.	145.				
ELEVATION	98.	100.	120.	140.				

CREL	SFWID	COBW	EXFW	ELEV	COOL	CAREA	EXPL
97.7	0.0	0.0	0.0	0.0	0.0	0.0	0.0

DAM DATA			
TOPEL	COOD	EXFO	DAMWID
101.7	2.6	1.5	300

PEAK OUTFLOW IS 800. AT TIME 40.33 HOURS

PEAK OUTFLOW IS 1209. AT TIME 40.33 HOURS

PEAK OUTFLOW IS 1638. AT TIME 40.33 HOURS

PEAK OUTFLOW IS 2336. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 2965. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 3533. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 4074. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 5121. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 10500. AT TIME 40.33 HOURS

SUR-AREA RUNOFF COMPUTATION

RUNOFF HYDROGRAPH FROM ECHO LAKE DRAINAGE AREA

ISTAQ ICOMP IECON ITAPE JPLT JFRT INAME ISTAGE IAUTO
LAKE-2 0 0 0 0 0 1 0 0

HYDROGRAPH DATA

IHYDG IUNG TAKEA SNAP TRSDA TRSPC RATIO ISNOW ISAME LOCAL
1 2 .70 0.00 2.49 0.00 0.000 0 1 0

PRECIP DATA

SFFE FMS R6 R12 R24 R48 R72 R96
0.00 22.50 113.00 124.00 132.00 142.00 0.00 0.00

TRSPC COMPUTED BY THE PROGRAM IS .800

LOSS DATA

LROFT STRKE DLTNR RTIOL ERAIN STRKS RTIOK STRTL CNSTL ALSMX RTIMP
0 0.00 0.00 1.00 0.00 0.00 1.00 1.00 0.05 0.00 0.00

UNIT HYDROGRAPH DATA

TC= 0.00 LAG= .18

RECESSION DATA

STRTO= 1.50 GRCSN= .05 RTIOR= 2.00

END-OF-PERIOD FLOW

MO.DA HR.MN PERIOD RAIN EXCS LOSS COMF Q MO.DA HR.MN PERIOD RAIN EXCS LOSS COMF Q

SUM 25.56 23.17 2.39 65280
(649.) (589.) (61.) (1848.52)

COMBINE HYDROGRAPHS

COMBINE DISCHARGE AND INFLOW HYDROGRAPHS

ISTAQ ICOMP IECON ITAPE JPLT JFRT INAME ISTAGE IAUTO
LAKE-2 2 0 0 0 0 1 0 0

HYDROGRAPH ROUTING

ROUTING THROUGH ECHO LAKE DAM

ISTAQ ICOMP IECON ITAPE JPLT JFRT INAME ISTAGE IAUTO
DAM-2 1 0 0 0 0 1 0 0

ROUTING DATA

QLOSS CLOSS AVG IRES ISAME IOFT IFMP LSTR
0.0 0.000 0.00 1 1 0 0 0
NSTPS NSTOL LAG AMSKK X ISK STORA ISFRAT
1 0 0 0.000 0.000 0.000 -93. -1

Sh 16

STAGE 92.65 93.65 94.65 95.65 96.65 97.65 98.65 99.65 100.00

FLOW 0.00 442.00 1324.00 2499.00 3848.00 5378.00 7069.00 8908.00 9585.00

SURFACE AREA= 0. 11. 27. 81. 485.

CAPACITY= 0. 45. 180. 1212. 7879.

ELEVATION= 80. 93. 100. 120. 140.

CREL SFWD COW EXPW ELEV COOL CAREA EXPL
92.7 0.0 0.0 0.0 0.0 0.0 0.0 0.0

DAM DATA
TOPEL COOL EXPD DAMWID
94.6 2.6 1.5 135.

CREST LENGTH 0. 8. 95. 115. 125. 130. 135.
AT OR BELOW
ELEVATION 94.6 95.0 96.0 97.0 98.0 99.0 100.0

PEAK OUTFLOW IS 1011. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 1523. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 2066. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 2774. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 3586. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 4352. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 5097. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 6484. AT TIME 40.17 HOURS

PEAK OUTFLOW IS 13539. AT TIME 40.00 HOURS

OPERATION	STATION	AREA	PLAN	RATIOS APPLIED TO FLOWS								
				RATIO 1	RATIO 2	RATIO 3	RATIO 4	RATIO 5	RATIO 6	RATIO 7	RATIO 8	RATIO 9
				.10	.15	.20	.25	.30	.35	.40	.50	1.00
HYDROGRAPH AT LAKE-1	(	1.79	1	1106.	1659.	2213.	2766.	3319.	3872.	4425.	5532.	11063.
		(4.64)	(	31.33)	(46.99)	(62.65)	(78.32)	(93.98)	(109.64)	(125.31)	(156.64)	(313.27)
ROUTED TO	(	1.79	1	800.	1209.	1638.	2336.	2965.	3533.	4074.	5121.	10500.
		(4.64)	(	22.66)	(34.24)	(46.30)	(66.14)	(83.96)	(100.05)	(115.36)	(145.01)	(297.33)
HYDROGRAPH AT LAKE-2	(	.70	1	559.	838.	1118.	1397.	1677.	1956.	2236.	2795.	5589.
		(1.81)	(	15.83)	(23.74)	(31.65)	(39.57)	(47.48)	(55.40)	(63.31)	(79.14)	(158.27)
2 COMBINED LAKE-2	(	2.49	1	1092.	1635.	2177.	2879.	3669.	4497.	5292.	6763.	13929.
		(6.45)	(	30.71)	(46.31)	(61.65)	(81.51)	(103.90)	(127.34)	(147.85)	(191.51)	(394.42)
ROUTED TO	(	2.49	1	1011.	1523.	2066.	2774.	3586.	4352.	5097.	6484.	13539.
		(6.45)	(	28.63)	(43.13)	(58.51)	(78.55)	(101.54)	(123.25)	(144.32)	(183.21)	(383.38)

SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	STORAGE	97.65	97.65	101.65
	OUTFLOW	0.	0.	62.
		0.	0.	1584.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF FAILURE	
						MAX OUTFLOW HOURS	FAILURE HOURS
.10	100.16	0.00	34.	800.	0.00	40.33	0.00
.15	100.97	0.00	49.	1209.	0.00	40.33	0.00
.20	101.72	.07	63.	1638.	.33	40.33	0.00
.25	102.26	.61	74.	2336.	.67	40.17	0.00
.30	102.63	.98	82.	2965.	1.00	40.17	0.00
.35	102.93	1.28	88.	3533.	1.17	40.17	0.00
.40	103.19	1.54	93.	4074.	1.50	40.17	0.00
.50	103.65	2.00	103.	5121.	2.50	40.17	0.00
1.00	105.58	3.93	145.	10500.	5.50	40.00	0.00

SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1	ELEVATION	INITIAL VALUE	SPILLWAY CREST	TOP OF DAM
	STORAGE	92.65	92.65	94.60
	OUTFLOW	45.	45.	69.
		0.	0.	1280.

RATIO OF PMF	MAXIMUM RESERVOIR W.S.ELEV	MAXIMUM DEPTH OVER DAM	MAXIMUM STORAGE AC-FT	MAXIMUM OUTFLOW CFS	DURATION OVER TOP HOURS	TIME OF FAILURE	
						MAX OUTFLOW HOURS	FAILURE HOURS
.10	94.30	0.00	65.	1011.	0.00	40.17	0.00
.15	94.82	.22	73.	1523.	1.00	40.17	0.00
.20	95.27	.67	80.	2066.	1.67	40.17	0.00
.25	95.79	1.19	88.	2774.	2.00	40.17	0.00
.30	96.28	1.68	97.	3586.	3.00	40.17	0.00
.35	96.70	2.10	104.	4352.	4.00	40.17	0.00
.40	97.05	2.45	111.	5097.	4.67	40.17	0.00
.50	97.67	3.07	124.	6484.	5.33	40.17	0.00
1.00	100.17	5.57	185.	13539.	6.50	40.00	0.00

5418

APPENDIX

D

Photographs

APPENDIX D
SELECTED PHOTOGRAPHS OF THE SITE

Site Plan	<u>Page No.</u>
	A
<u>PHOTOGRAPH NO.</u>	
1. Overview of impoundment, dam and the area immediately downstream of the dam. (4/24/81)	1
2. View from the right side of the dam showing discharge concentration at left side of spillway. (4/24/81)	1
3. View from the crest of the dam looking downstream. (4/24/81)	2
4. Stepped channel downstream of the dam. (4/24/81)	2
5. Channel and bank conditions approximately 100 feet downstream of the dam. (4/24/81)	3
6. Channel and bank conditions on the right side at the downstream end of the step channel spillway. (4/24/81)	3
7. Access to the reservoir drain pipe valve on the right side of the dam. (4/24/81)	4
8. Outlet of the reservoir drain pipe on the right side of the dam. (4/24/81)	4
9. Channel and bank conditions immediately downstream of stepped channel. (4/24/81)	5
10. Typical downstream channel conditions. (4/24/81)	
11. Decorative waterwheel and shelter at the left abutment of the dam. (4/24/81)	6
12. Spillway for impoundment which discharges directly into Echo Lake about 0.6 miles upstream of Echo Lake Dam. (4/24/81)	6
13. Potential damage area left of the channel about 0.25 miles downstream of Echo Lake Dam. (4/24/81)	7
14. Potential damage area right of the channel about 0.25 miles downstream of Echo Lake Dam. (4/24/81)	7

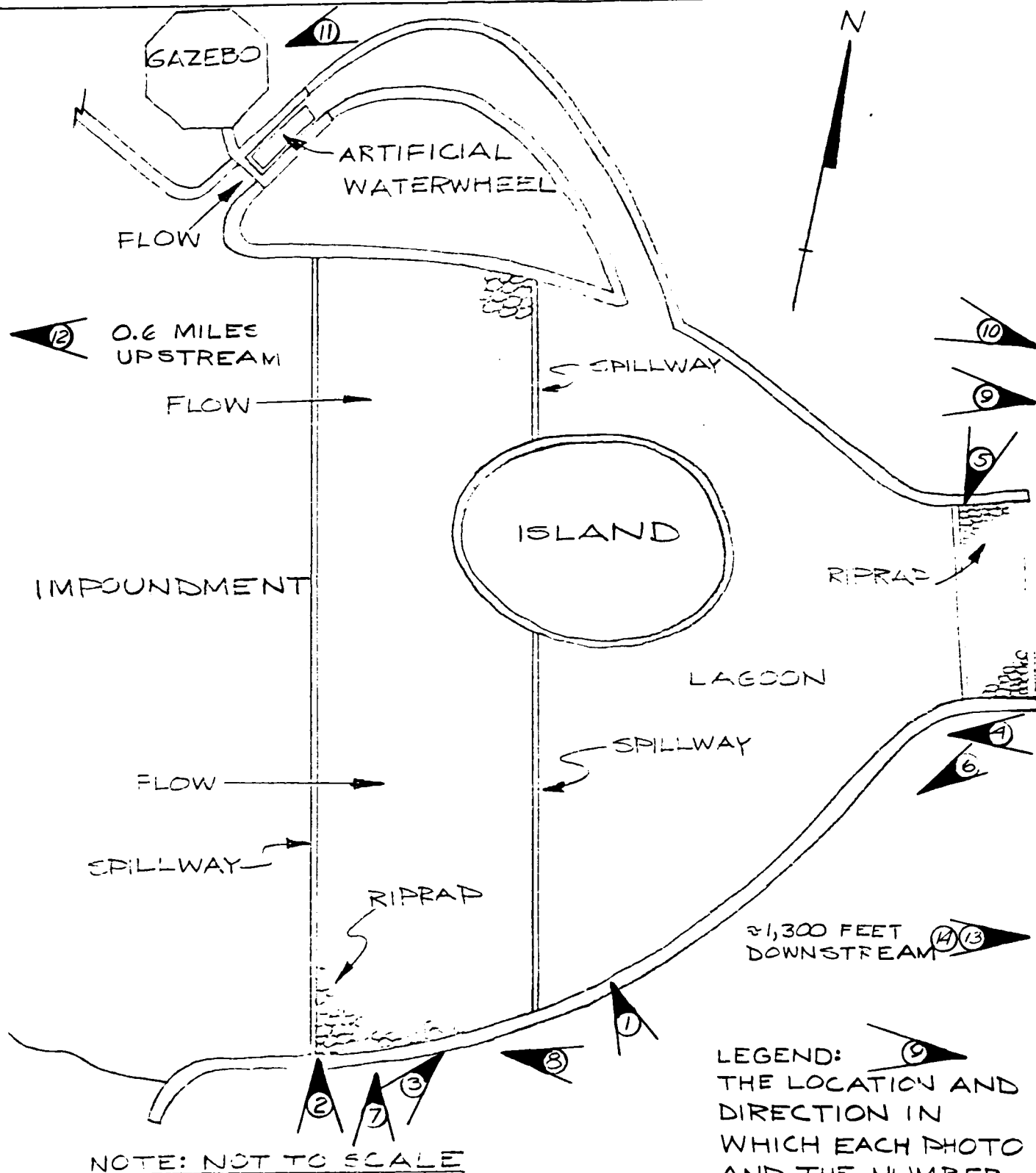
ECHO LAKE DAM

SHEET 4

FILE

DATE 6/24/81

JOB NO. 1500.006.113

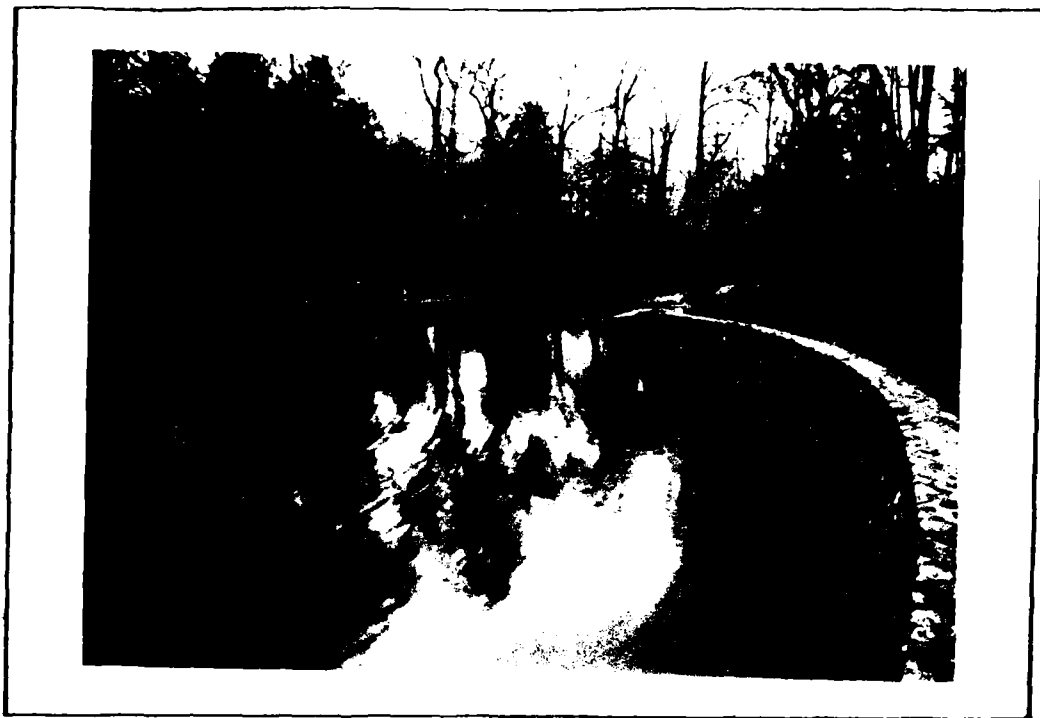




1. OVERVIEW OF IMPOUNDMENT, DAM AND THE AREA IMMEDIATELY DOWN-
STREAM OF THE DAM. (4/24/81)



2. VIEW FROM THE RIGHT SIDE OF THE DAM SHOWING DISCHARGE CONCEN-
TRATION OF LEFT SIDE OF SPILLWAY. (4/24/81)



3. VIEW FROM THE CREST OF THE DAM LOOKING DOWNSTREAM. (4/24/81)



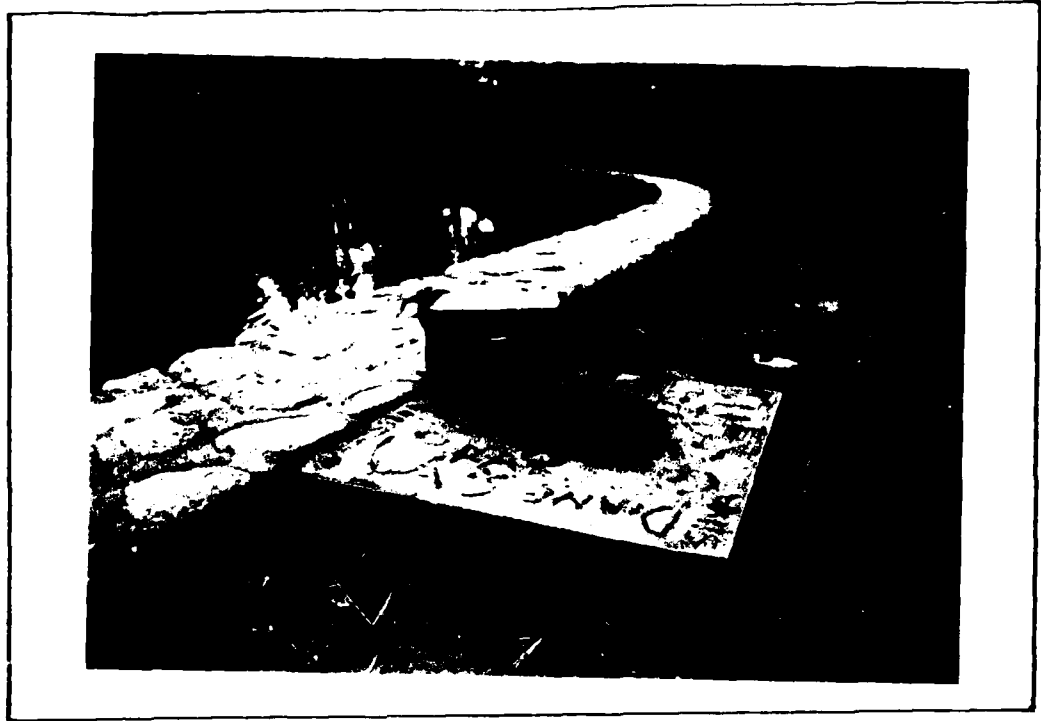
4. STEPPED CHANNEL DOWNSTREAM OF THE DAM. (4/24/81)



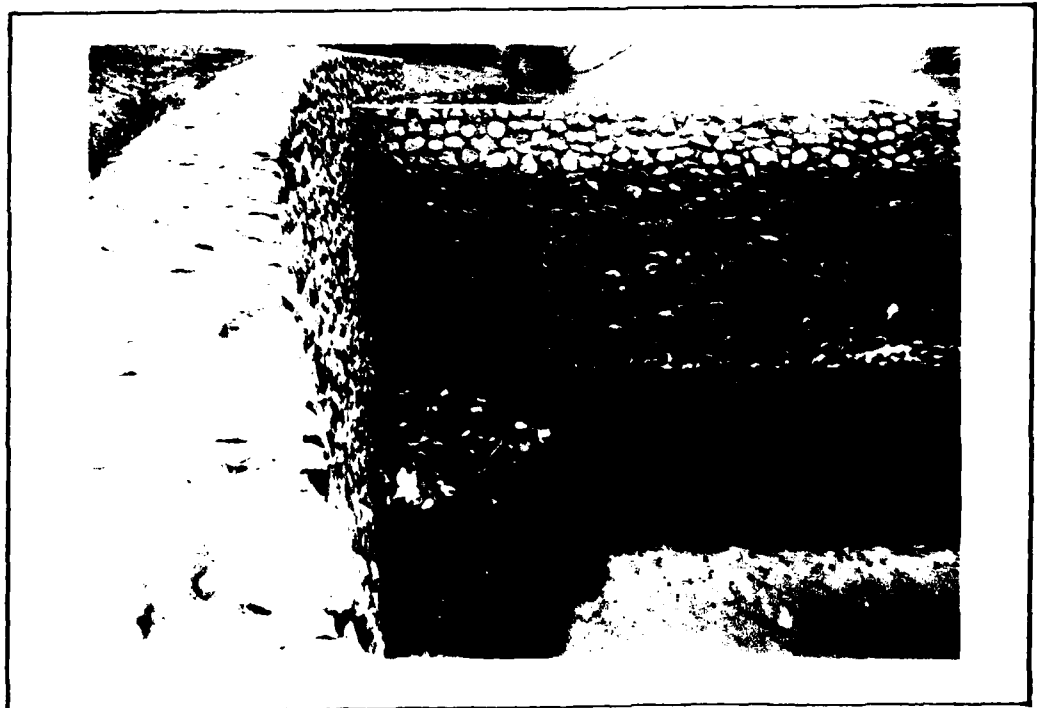
5. CHANNEL AND BANK CONDITIONS APPROXIMATELY 100 FEET DOWNSTREAM OF THE DAM. (4/24/81)



6. CHANNEL AND BANK CONDITIONS ON THE RIGHT SIDE AT THE DOWNSTREAM END OF THE STEP CHANNEL SPILLWAY. (4/24/81)



7. ACCESS TO THE RESERVOIR DRAIN PIPE VALVE ON THE RIGHT SIDE OF THE DAM. (4/24/81)



8. OUTLET OF THE RESERVOIR DRAIN PIPE ON THE RIGHT SIDE OF THE DAM. (4/24/81)



9. CHANNEL AND BANK CONDITIONS IMMEDIATELY DOWNSTREAM OF STEPPED CHANNEL. (4/24/81)



10. TYPICAL DOWNSTREAM CHANNEL CONDITIONS. (4/24/81)



11. DECORATIVE WATERWHEEL AND SHELTER AT THE LEFT ABUTMENT OF THE DAM. (4/24/81)



12. SPILLWAY FOR IMPOUNDMENT WHICH DISCHARGES DIRECTLY INTO ECHO LAKE ABOUT 0.6 MILES UPSTREAM OF ECHO LAKE DAM. (4/24/81)



13. POTENTIAL DAMAGE AREA LEFT OF THE CHANNEL ABOUT 0.25 MILES
DOWNSTREAM OF ECHO LAKE DAM. (4/24/81)



14. POTENTIAL DAMAGE AREA RIGHT OF THE CHANNEL ABOUT 0.25 MILES
DOWNSTREAM OF ECHO LAKE DAM. (4/24/81)

APPENDIX

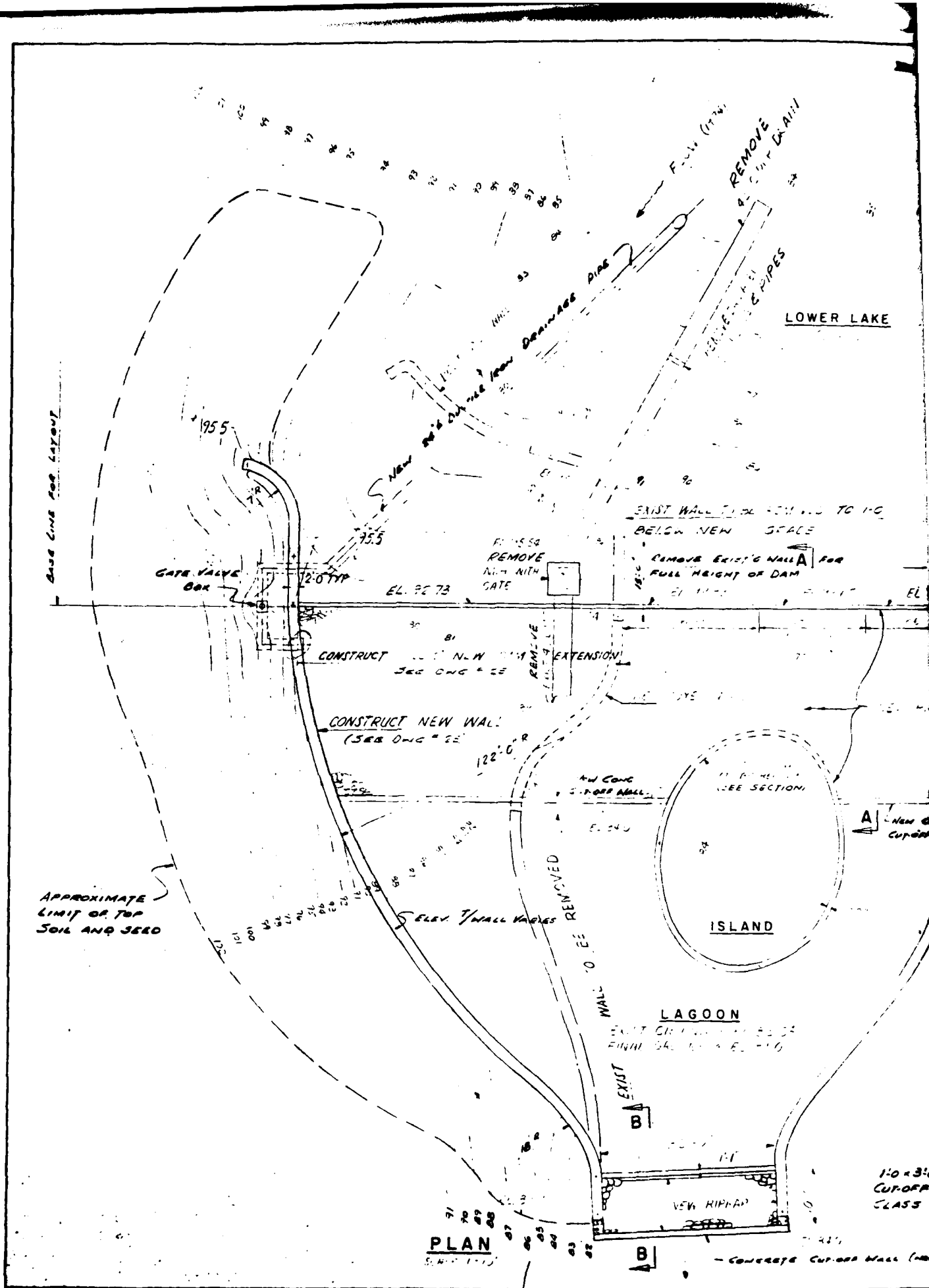
E

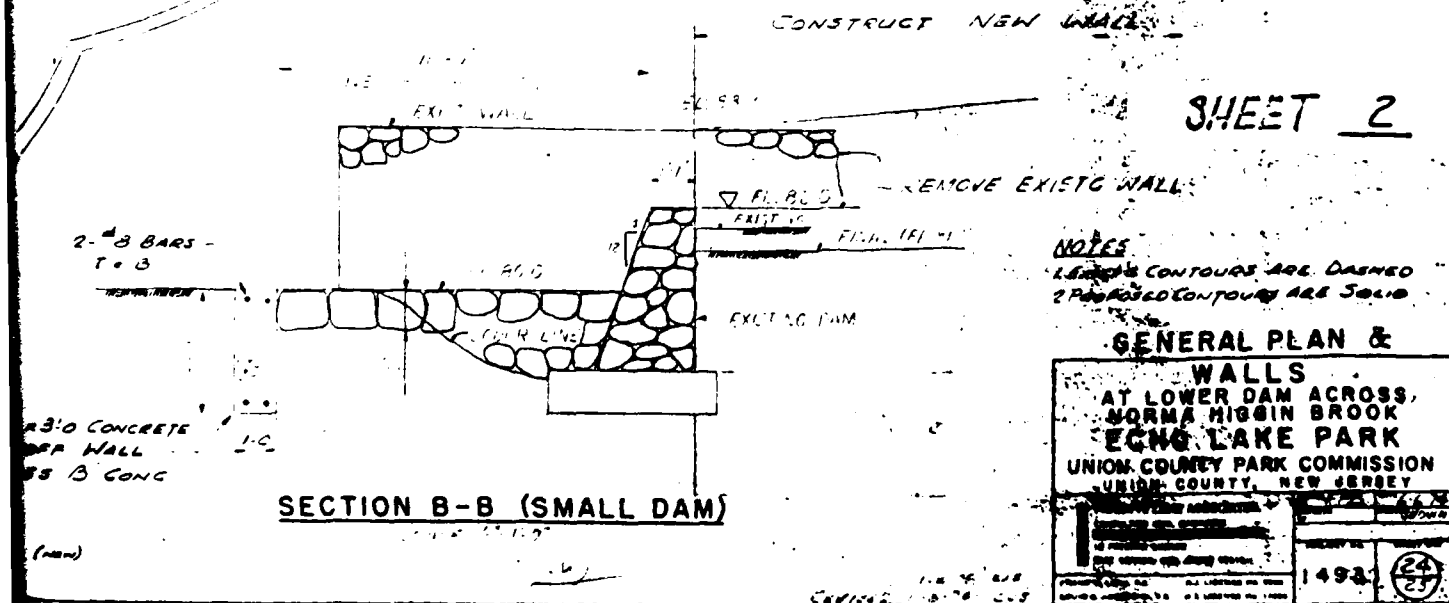
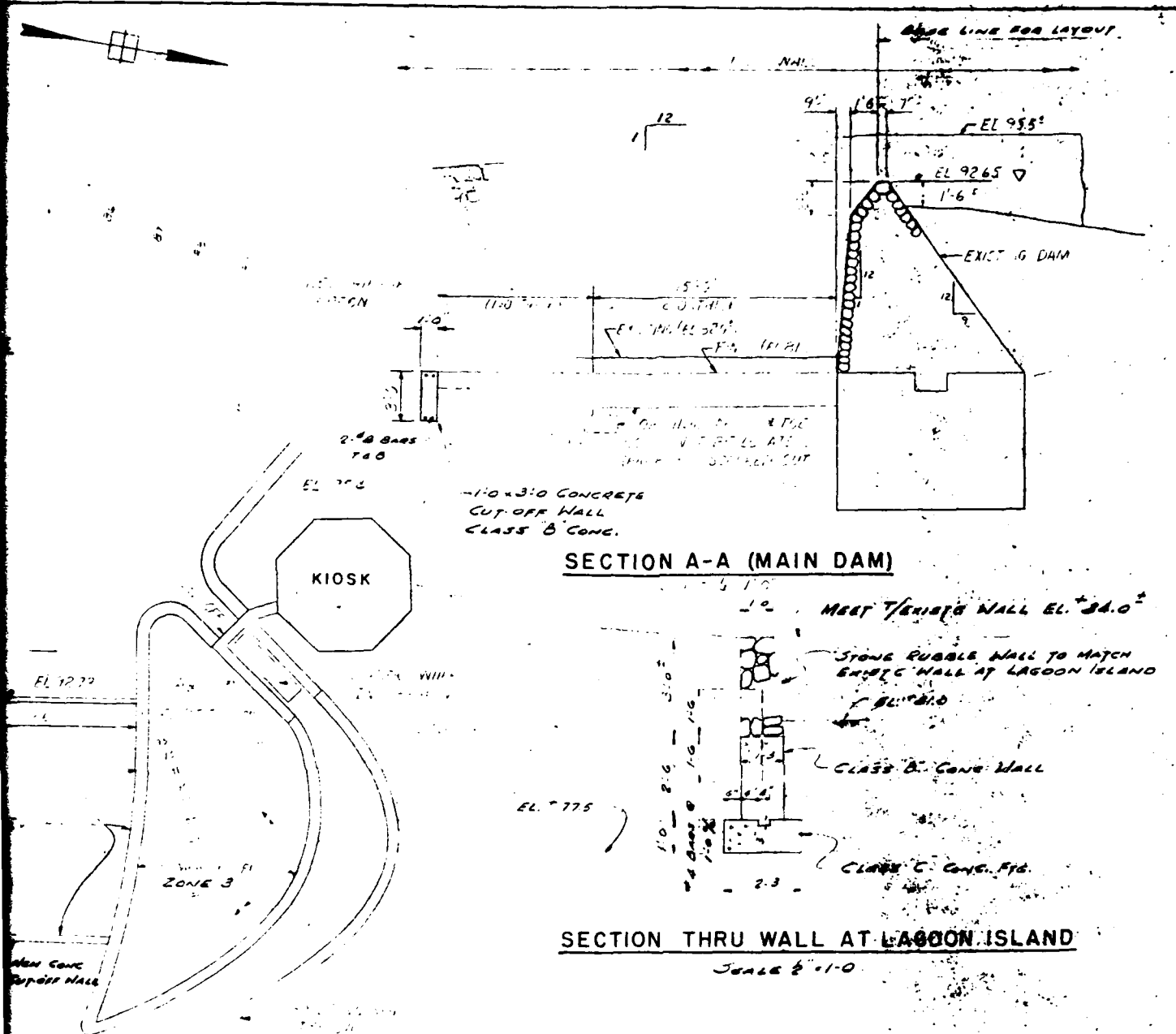
Drawings

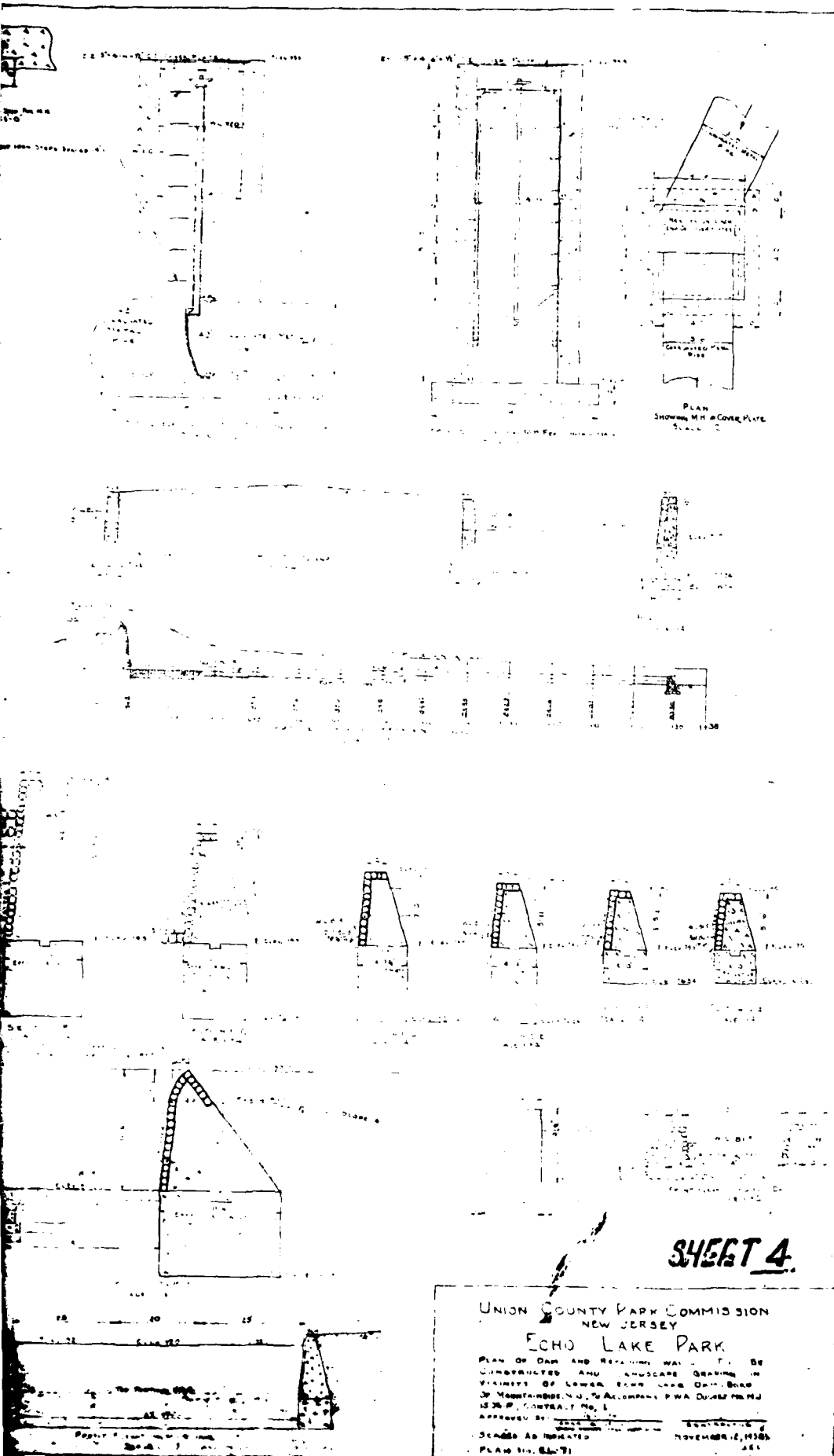
ECHO LAKE DAM
APPENDIX E
DRAWINGS

TABLE OF CONTENTS

	<u>Sheet No.</u>
Regional Vicinity Map, Figure 1	1
General Plan and Walls	2
Walls	3
Echo Lake Park, Plan of Dam and Retaining Walls (1938 Drawings)	4







SHEET 4.

UNION COUNTY PARK COMMISSION
NEW JERSEY

ECHO LAKE PARK

PLAN OF DAM AND RETAINING WALL TO BE
CONSTRUCTED AND LANDSCAPE GRADING IN
VICINITY OF LOWER ECHO LAKE DAM-BOND
30 MONTAGNES N.J. TO ACCOMMODATE PWA DUMP FILLING
IS 30.0 CONTRACT NO. 1

APPROVED BY: [Signature] ENGINEER
SCALES AS NOTED NOVEMBER 12, 1935
PLAN NO. E.L.W.1

APPENDIX

F

Site Geology

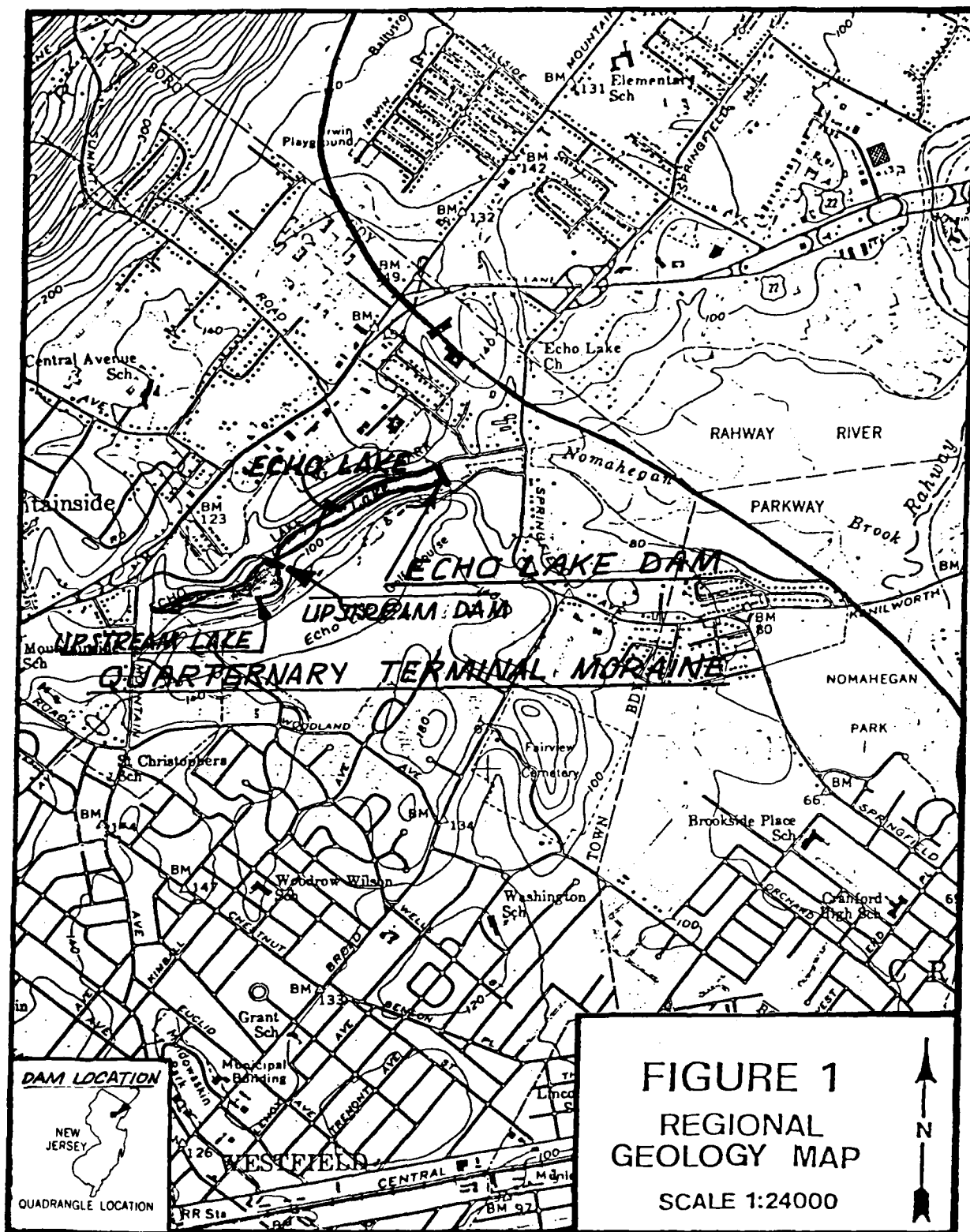
SITE GEOLOGY

ECHO LAKE DAM

Echo Lake Dam is located in Union County within the Triassic Lowland portion of the Piedmont physiographic province. The site of the dam and lake is underlain by Triassic age sedimentary rock units of the Brunswick formation, a series of brown to red siltstones and sandstones which strike predominantly NE-SW and dip about 10° to 20° NW. Although no major faults are known to occur near the site, the existence of minor offsets are possible in the Brunswick units. Fracturing and jointing occur throughout the formation.

Overburden consists of residual soils (S¹+) and remnant pockets of Wisconsin glacial epoch recessional moraine materials may mantle valley bottoms and hillside areas. Thickness and character of these glacially-derived materials will vary appreciably.

Some swampy conditions may occur within the recessional moraine areas in low-lying areas.



APPENDIX G
STRUCTURAL STABILITY

ECHO LAKE DAM
APPENDIX G
STRUCTURAL STABILITY DATA

TABLE OF CONTENTS

	<u>Sheet No.</u>
1. Assumption	1
2. Analysis of Portion of Dam Existing Since 1938	2 through 4
3. Analysis of Portion of Dam Existing Since 1975	5 through 7



O'BRIEN & GERE

SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM	1	REH	5/15/81	1800-006-113

✓ 6/5/81

STABILITY ANALYSIS

ASSUMPTIONS

Concrete Density	-	140 pcf
Silt Density	-	60 pcf (submerged)
At Rest Earth Coeff.	-	0.5
Shear Stress	-	50
Coeff of Friction	-	0.4



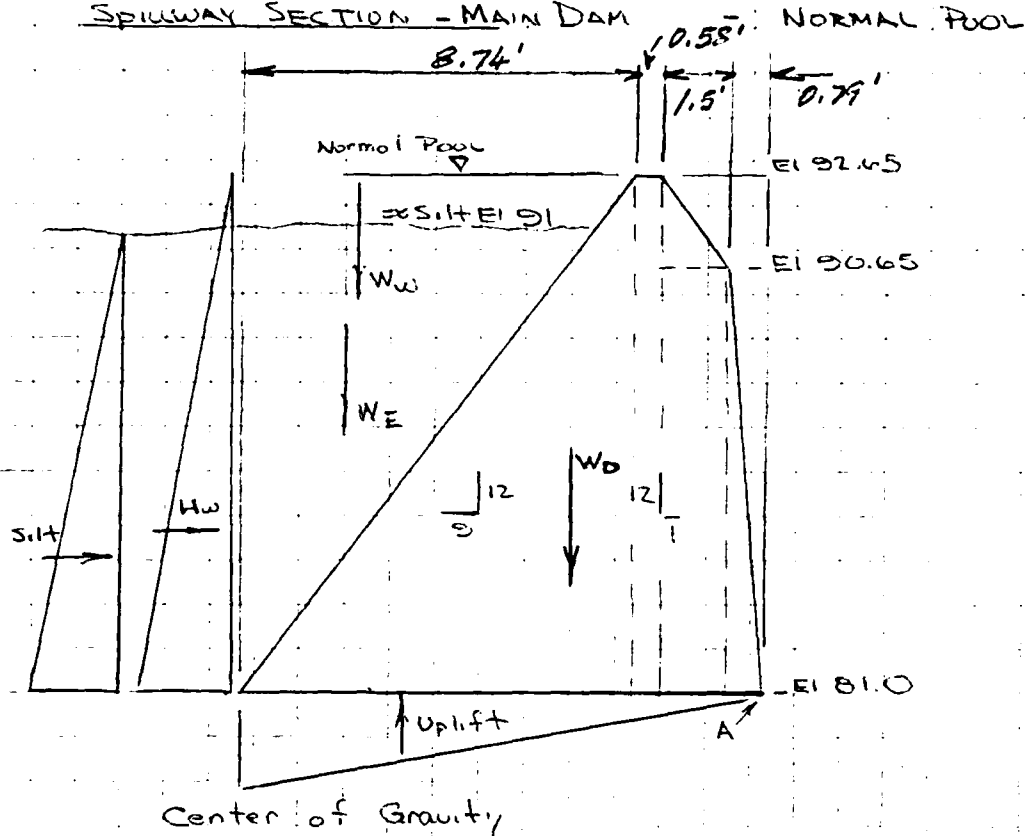
O'BRIEN & GERE

SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM	2	RGH	5/15/81	1800-006-113

✓
6/5/81

Existing Dam Since 1938

SPILLWAY SECTION - MAIN DAM



$$\frac{\sum M_A}{A} = \frac{\frac{1}{2}(9.65)(8.74)(5.3) + 1.5(9.65)(1.55) + \frac{1}{2}(1.5)(2)(1.8) + (5.8)(11.65)(2.59) + \frac{1}{2}(11.65)(8.74)(5.79)}{3.86 + 14.48 + 1.5 + 6.76 + 50.8}$$

$$= \frac{339.11}{77.40} = 4.38'$$



O'BRIEN & GERE

SUBJECT

ECHO LAKE DAM

SHEET

3

BY

REH

DATE

5/15/81

JOB NO

18W-006-113

✓ # 6/5/81

Normal Pool Loading

<u>Force</u>	<u>kips</u>	<u>Arm (feet)</u>	<u>Moment (ft.kips)</u>
Dam Wt -	$77.40(140) = 10.84 \uparrow$	4.38	+ 47.5
Water -	$\frac{1}{2}(11.65)8.73(0.62) = 3.15 \uparrow$	8.7	+ 27.4
WEARTH (Sediment) -	$\frac{1}{2}(10)(7.5)(0.60) = 2.25 \uparrow$	9.11	+ 20.5
HW -	$\frac{1}{2}(0.62)11.65^2 = 4.21 \rightarrow$	3.88	- 16.3
Silt -	$\frac{1}{2}(5)(0.60)10^2 = 1.50 \rightarrow$	3.33	- 5.0
Uplift -	$\frac{1}{2}(11.65)(0.62)11.62 = 4.2 \uparrow$	7.75	- 32.6

Resultant Location and Eccentricity

$$\Sigma M / \Sigma F_v = \frac{41.5}{12.04} = 3.45' < 3.87' \quad \begin{array}{l} \text{Resultant is located approx} \\ \text{0.4 feet outside middle} \\ \text{third of base width} \end{array}$$

$$e = \frac{11.61}{2} - 3.45 = 2.36$$

Foundation Stressess

$$p = \frac{\bar{y}}{b} \left(1 \pm \frac{6e}{b} \right) = \frac{12.04}{11.62} \left(1 \pm \frac{11.61}{11.62} \right) = 1.04 \left(1 \pm 1.26 \right)$$

$$= 7.2 \left(1 \pm 1.26 \right) = \begin{array}{l} + 16.3 \text{ psi } (+ 2.35 \text{ K/Ft}^2) \\ - 1.9 \text{ psi } (- 0.27 \text{ K/Ft}^2) \end{array}$$



O'BRIEN & GERE

SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM	4	REH	5/18/81	100-26-113

1 #

6/5/81

Shear

$$S.F. = \frac{\sum V_F (.4) + 7.2(11.62)}{\sum H_F} = \frac{12.4 + 7.2(11.62)}{5.71}$$

$$= \frac{4.82 + 83.6}{5.71} = 15.5$$



OBRIEN & GERE

SUBJECT

Echo Lake Dam

SHEET

4A

BY

REH

DATE

6/24/81

JOB NO

1800-006-113

Earthquake Loading Condition (Horizontal)

Center of Gravity (Vertical)

$$= \frac{\frac{1}{2}(79)(9.65)(\frac{9.65}{3}) + \frac{1}{2}(2)(1.5)(10.3) + 9.65(1.5)(\frac{9.65}{2}) + .58(11.65)(\frac{11.65}{2}) + \frac{1}{2}(11.65)(8.74)(\frac{11.65}{2})}{\frac{1}{2}(79)(9.65) + \frac{1}{2}(2)(1.5) + 9.65(1.5) + .58(11.65) + \frac{1}{2}(11.65)(8.74)}$$

$$= \frac{334.61}{77.46} = 4.3 \text{ feet}$$

Acceleration due to earthquake, Zone 1 $a = .025g$

<u>Force</u>	<u>kips</u>	<u>Arm (ft)</u>	<u>Moment (ft-kips)</u>
Dam $\rightarrow (.025)(10.84) = .271$		4.3	1.16

Water $\rightarrow$ (Refer to "Design of Small Dams" page 335)

$$P_e = C \lambda \gamma h = .4(.025)(.062)(11.65) = .0072 \text{ k/ft}$$

$$V_e = 0.726(.0072)(11.65) = .06 \text{ kips}$$

$$M_e = 0.299(.0072)(11.65)^2 = .29 \text{ ft-kips}$$

$$\begin{aligned} \text{Total negative Loading due to Earthquake} &= -.27 + -.06 \\ &= -.33 \text{ kips} \end{aligned}$$

$$\text{Total negative Moment due to Earthquake} = -1.45 \text{ ft-kips}$$

The effects of earthquake loadings on the dam are not significantly different from normal pool loadings

Structure meets current stability criteria for earthquake loading for analyses performed herein.

SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM	5	REH	5/15/81	1800 WOG-113

Built 1975 *Dr* 6/5/81

SPILLWAY SECTION - MAIN DAM

Normal Pool

1.5'

Shape of Section Analyzed

W_W

W_E

W_D

17'

H_W

5.7'

4'

3'

3'

14'

UPSET

A

Center of Gravity

$$\frac{\sum M_A^+}{A} = \frac{14(3)'7 + 17(4)'5}{14(3) + 17(4)} = \frac{634}{110} = 5.76'$$

**O'BRIEN & GERE**

SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM	6	REH	5/15/81	1800-006-113

✓ 6/5/81

NORMAL POOL LOADING

FORCE	kip	Arm (feet)	Moment (ft kips)
Dam Wt -	$110(14) = 15.4 \downarrow$	5.76'	+ 88.7
W _{water} -	$17(7)(.02) = 7.38 \downarrow$	10.5	+ 77.5
WEARTH -	$15.5(7)(.060) = 16.51 \downarrow$	10.5	+ 68.4
H _w -	$\frac{1}{2}(.062)(20^2) = 12.4 \rightarrow$	6.7	- 83.1
Silt -	$\frac{1}{2}(1.5)(.060)(18.5^2) = 5.1 \rightarrow$	6.2	- 31.6
Uplift -	$\frac{1}{2}(.062)(20)(14) = 8.7 \uparrow$	9.3	- 80.9

Resultant Location and Eccentricity

$$\Sigma M / \Sigma F_y = 39 / 20.6 = 1.89' \quad \text{- Resultant is located approx 4.4 feet outside middle third of base width}$$

$$e = \frac{14}{2} - 1.9 = 5.1'$$

Foundation Stresses

$$p = \frac{\bar{y}}{B} (1 \pm 6e/B) = \frac{20.6}{14} (1 \pm \frac{30.6}{14}) = 1.47 \pm (1 \pm 2.19)$$

$$= 10.2 (1 \pm 2.19) = \begin{matrix} 32.5 \text{ psi } (+4.68 \text{ K/F}^2) \\ - 12.1 \text{ psi } (-1.74 \text{ K/F}^2) \end{matrix}$$



O'BRIEN & GERE

SUBJECT	SHEET	BY	DATE	JOB NO
ECHO LAKE DAM	7	REH	5/12/81	1800-006.113

JH 6/5/81

Shear

$$S.F. = \frac{20.6(.4) + 7.2(14)}{17.5} = \frac{109.0}{17.5} = 6.2$$



O'BRIEN & GERE

SUBJECT	SHEET	BY	DATE	JOB NO
Echo Lake Dam	7A	REH	6/24/81	1800-006-113

✓ ~~JE~~ 6/24/81Earthquake Loading Condition (Horizontal)

Center of Gravity (Vertical)

$$= \frac{14(3)(1.5) + 17(4)(3 + \frac{17}{2})}{14(3) + 17(4)}$$

$$= \frac{63 + 782}{42 + 68} = \frac{845}{110} = 7.68'$$

Acceleration due to earthquake, Zone I $\alpha = .025g$

<u>Force</u>	<u>Kips</u>	<u>Arm (ft)</u>	<u>Moment (ft kips)</u>
Dam $\rightarrow$	$.025(15.4) = .385$	7.68	-2.96

Water $\rightarrow$ (Refer to "Design of Small Dams" page 335)

$$P_e = C \lambda \gamma h = .73(.025)(.062)(20) = .0226 \text{ k/sf}$$

$$V_e = 0.726 (.0226)(20) = .33 \text{ kips}$$

$$M_e = .299 (.0226)(20^2) = -2.7 \text{ ft kips}$$

Total negative loading due to earthquake = -.72 kips

Total negative moment due to earthquake = -5.66 kip ft



SUBJECT

Echo Lake Dam

SHEET

7B

BY

REH

DATE

6/24/81

JOB NO

1800-006-113

VLE 6/24/81

Resultant Location and Eccentricity

$$\Sigma M / \Sigma F_v = 39 - 5.66 / 20.6 = 1.62' \quad \text{Resultant is located approximately 3 feet outside middle third of base width}$$

$$e = 1\frac{1}{2} - 1.6 = 5.4$$

Foundation Stresses

$$\begin{aligned} p &= \frac{1}{B} \left(1 \pm \frac{6e}{B} \right) = \frac{20.6}{14} \left(1 \pm \frac{32.4}{14} \right) \\ &= 1.47 (1 \pm 2.31) \\ &= \begin{aligned} &+ 337 \text{ psi } (4.86 \text{ k/sf}) \\ &- 13.4 \text{ psi } (-1.93 \text{ k/sf}) \end{aligned} \end{aligned}$$

Sliding (shear)

$$SF = \frac{20.6(.4) + 7.2(14)}{17.5 + .72} = 5.98$$

Structure meets current stability criteria for earthquake loading for analyses performed herein.

