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NATIONAL DAM SAFETY PROGRAM. BENSON LAKE DAM (MO 30667), MISSOU--ETC(U)
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MISSOURI - KANSAS CITY RIVER BASIN

BENSON LAKE DAM
GASCONADE COUNTY, MISSOURI
MO. 30667

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PHASE I INSPECTION REPORT NATIONAL DAM SAFETY PROGRAM

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Corps of Engineers

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St. Louis District

PREPARED BY: U. S. ARMY ENGINEER DISTRICT, ST. LOUIS

FOR: STATE OF MISSOURI

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20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This report was prepared under the National Program of Inspection of Non-Federal Dams. This report assesses the general condition of the dam with respect to safety, based on available data and on visual inspection, to determine if the dam poses hazards to human life or property.		

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ATTENTION ON

DEPARTMENT OF THE ARMY
ST. LOUIS DISTRICT, CORPS OF ENGINEERS
210 TUCKER BOULEVARD NORTH
ST. LOUIS, MISSOURI 63101

SUBJECT: Benson Lake Dam Dam (Mo. 30667) Phase I Inspection Report

This report presents the results of field inspection and evaluation of the Benson Lake Dam (Mo. 30667).

It was prepared under the National Program of Inspection of Non-Federal Dams.

This dam has been classified as unsafe, non-emergency by the St. Louis District as a result of the application of the following criteria:

- 1) Spillway will not pass 50 percent of the Probable Maximum Flood
- 2) Overtopping could result in dam failure
- 3) Dam failure significantly increases the hazard to loss of life downstream

SUBMITTED BY: _____
Chief, Engineering Division Date

APPROVED BY: _____
Colonel, CE, District Engineer Date

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BENSON LAKE DAM
GASCONADE COUNTY, MISSOURI

MISSOURI INVENTORY NO. 30667

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

PREPARED BY
CONSOER, TOWNSEND AND ASSOCIATES, LTD.
ST. LOUIS, MISSOURI
AND
PRC ENGINEERING CONSULTANTS, INC.
ENGLEWOOD, COLORADO
A JOINT VENTURE

UNDER DIRECTION OF
ST. LOUIS DISTRICT, CORPS OF ENGINEERS
FOR
GOVERNOR OF MISSOURI

SEPTEMBER 1980

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

Name of Dam: Benson Lake Dam, Missouri Inv. No. 30667
State Located: Missouri
County Located: Gasconade
Stream: An unnamed tributary of the Frene Creek
Date of Inspection: April 24, 1980

Assessment of General Condition

Benson Lake Dam was inspected by the engineering firms of Consoer, Townsend and Associates, Ltd. and PRC Engineering Consultants, Inc. (A Joint Venture) of St. Louis, Missouri according to the U. S. Army Corps of Engineers "Engineer Regulation No. 1110-2-106" and additional guidelines furnished by the St. Louis District of the Corps of Engineers. Based upon the criteria in the guidelines, the dam is in the high hazard potential classification, which means that urban development with more than a small number of habitable structures could be affected in the event of failure of the dam. Within the estimated damage zone of three miles downstream of the dam are one dwelling, four buildings, two trailers, an oil depot, sewage lagoons and a state highway (Hwy 100) which may be subjected to flooding, with possible damage and/or destruction, and possible loss of life. Benson Lake Dam is in the small size classification since it is less than 40 feet in height and impounds less than 1000 acre-feet of water.

In general, the dam appears to be in poor condition. Our inspection and evaluation indicates that the spillway of Benson Lake Dam does not meet the criteria set forth in the guidelines for a dam having the above size and hazard potential. Benson Lake Dam being a small size dam with a high hazard potential is required by the guidelines to pass from one-half of the Probable Maximum Flood to the Probable Maximum Flood without overtopping. Considering the number of inhabited dwellings, a state highway, and an oil depot being located downstream of the dam, the PMF is considered the appropriate spillway design flood for Benson Lake Dam. It was determined that the reservoir/spillway system can accommodate approximately 20 percent of the Probable Maximum Flood without overtopping the dam. Our evaluation also indicates that the reservoir/spillway system can accommodate the one-percent chance flood (100-year flood) without overtopping.

The Probable Maximum Flood is defined as the flood discharge that may be expected from the most severe combination of critical meteorological and hydrologic conditions that are reasonably possible in the region.

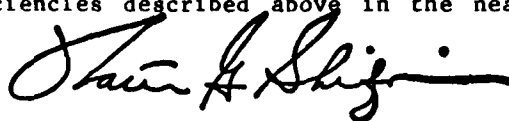
Another major deficiency with Benson Lake Dam is the three scarps observed on the downstream slope on the left side of the embankment and the seepage observed in the area. Two of the scarps were fairly shallow and approximately 3-feet wide. The other scarp was approximately 20-feet wide at the top and 30 feet wide at the bottom. These scarps and the seepage indicate instability of the slope.

Other deficiencies noted by the inspection team were the minor wave erosion on the upstream slope, the trees on the upstream and the downstream embankment slopes, the tall vegetation on the embankment, rodent activity on the embankment, the erosion on the left side slope of the spillway channel, tall grass growing within

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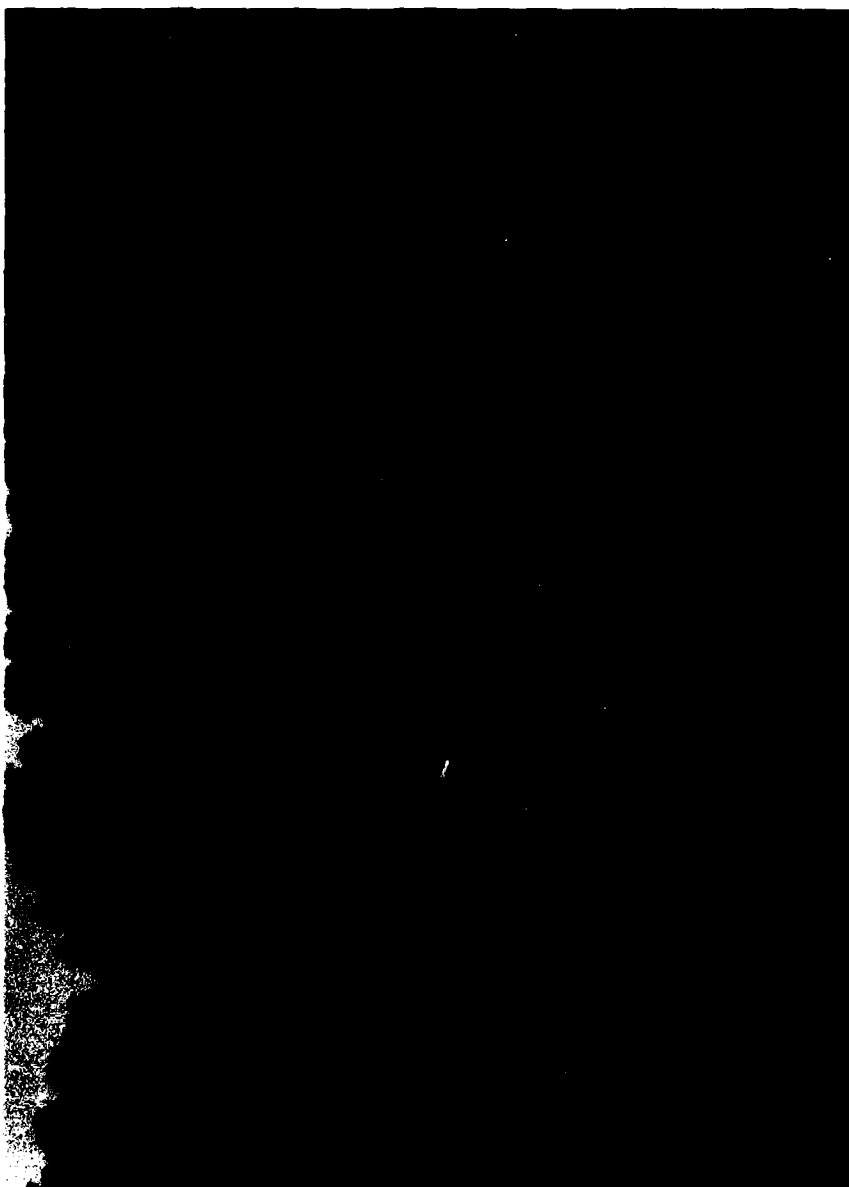
the spillway channel, a need for periodic inspection by a qualified engineer and a lack of maintenance schedule. The lack of seepage and stability analyses on record is also a deficiency that should be corrected.

It is recommended that the owner take immediate action to study the embankment seepage and stability problem and correct or control the several deficiencies described above in the near future.



Walter G. Shifrin, P.E.





Overview of Benson Lake Dam

PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

BENSON LAKE DAM, I.D. No. 30667

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PHASE I INSPECTION REPORT
NATIONAL DAM SAFETY PROGRAM

BENSON LAKE DAM, Missouri Inv. No. 30667

SECTION 1: PROJECT INFORMATION

1.1 General

a. Authority

The Dam Inspection Act, Public Law 92-367 of August, 1972, authorizes the Secretary of the Army, through the Corps of Engineers, to initiate a national program of dam inspections. Inspection for Benson Lake Dam was carried out under Contract DACW 43-80-C-0094 between the Department of the Army, St. Louis District, Corps of Engineers, and the engineering firms of Consoer, Townsend & Associates, Ltd., and PRC Engineering Consultants, Inc. (A Joint Venture), of St. Louis, Missouri.

b. Purpose of Inspection

The visual inspection of Benson Lake Dam was made on April 24, 1980. The purpose of the inspection was to make a general assessment as to the structural integrity and operational adequacy of the dam embankment and its appurtenant structures.

c. Scope of Report

This report summarizes available pertinent data relating to the project, presents a summary of visual observations made during the field inspection, presents an assessment of hydrologic and hydraulic conditions at the site, presents an assessment of the structural adequacy of the various project features and assesses the general condition of the dam with respect to safety.

Subsurface investigations, laboratory testing and detailed analyses were not within the scope of this study. No warranty as to the absolute safety of the project features is implied by the conclusions presented in this report.

It should be noted that in this report reference to left or right abutments is viewed as looking downstream. Where left abutment or left side of the dam is used in this report, this also refers to the west abutment or side, and right to the east abutment or side.

d. Evaluation Criteria

The inspection and evaluation of the dam is performed in accordance with the U.S. Army Corps of Engineers "Engineer Regulation No. 1110-2-106" and additional guidelines furnished by the St. Louis District office of the Corps of Engineers for Phase 1 Dam Inspection.

1.2 Description of the Project

a. Description of Dam and Appurtenances

The following description is based upon observations and measurements made during the visual inspection and from conversations with Wilbur Benson, a representative of the owner. Design drawings were not located for the dam or appurtenant structures.

The dam is an earthfill structure between earth abutments. The crest has a total length of 277 feet between the spillway and the right abutment. The maximum crest elevation is approximately 712 feet above mean sea level (MSL) at a point 100 feet to the right of the spillway. The crest elevation drops 6 inches from this point to the spillway and 2 feet from this point to the right abutment. The dam has a somewhat curved alignment convex in the downstream direction. The crest width is 12 feet. The maximum height of the embankment from the downstream creekbed is approximately 25 feet. The upstream slope was measured to be 1 vertical to 3 horizontal (1V to 3H) from the crest to the water surface. The downstream slope was measured to be 1V to 2H. No riprap was provided as slope protection on the upstream slope.

The spillway is constructed into the left abutment and functions as an open channel. The approachway provides a smooth transition from the lake to the spillway channel. Once over the crest the invert slope is approximately 1%. The crest area cross-section is trapezoidal in shape with a 68 foot top width and a 45 foot bottom width. The channel bottom has a small subchannel at its invert which carries most of the flow for normal conditions; this subchannel is four inches deep with a 5 foot top width. The spillway channel has a 1.5

foot drop about 100 feet downstream from the crest. Approximately 50 feet downstream from the drop the alignment has a sharp curve to the right before it empties into the downstream channel. There is about 50 feet of channel between the sharp curve and the downstream channel. Downstream from the 1.5 foot drop, the slope of the invert increases and the width of channel decreases.

The right rim of the reservoir is parallel to a road and both the rim and the road are at a lower elevation than the top of dam. Before the dam could be overtopped, water would spill over this right rim and into the roadway. This condition causes the right reservoir rim especially at the right abutment to serve as an emergency spillway. The roadway at the right abutment is approximately 2.5 feet lower than the top of dam at its maximum section, whereas the spillway crest is almost 4 feet lower than the top of dam elevation at its maximum section.

There are no low level drains or mechanically controlled outlet works provided for this dam.

b. Location

Benson Lake Dam is located in in the State of Missouri, Gasconade County, and crosses an unnamed tributary to Frene Creek, which is tributary to the Missouri River. The damsite is approximately five miles southwest of Hermann, a community on the Missouri River, and can be found on the 7.5 minute series of the Hermann, Mo. Quadrangle Sheet in Section 15 of Range 5 West and Township 45 North.

c. Size Classification

According to the "Recommended Guidelines for Safety Inspection of Dams" by the U.S. Department of the Army, Office of the Chief Engineer, the dam is classified in the dam-size category as being "small" since its storage is less than 1,000 acre-feet. The dam is also classified as "Small" in the dam-size category because its height is less than 40 feet. The overall size classification is therefore "Small".

d. Hazard Classification

The dam has been classified as having a "High" hazard potential in the National Inventory of Dams, on the basis that in the event of failure of the dam or its appurtenances, excessive damage could occur to downstream property, together with the possibility of the loss of life. Our findings concur with this classification. Within the estimated damage zone, which extends approximately three miles downstream of the dam, are one dwelling, four buildings, two trailers, an oil depot, sewage lagoons, and a state highway.

e. Ownership

Benson Lake Dam is owned privately by Mr. Clifford Benson. The mailing address is Mr. Clifford Benson, R.R. 1, Box 82, Hermann, Missouri 65041.

f. Purpose of Dam

The purpose of the dam is to impound water for recreational use as a private lake.

g. Design and Construction History

According to a neighbor, Mr. A.C. Schneider, the dam was built in 1966 (est.) by Mr. Glennon Epple of Hermann, Missouri. Efforts to contact the original builder were futile.

Mr. Elmer Kuhn, who was the soil conservationist for the Hermann, Missouri area, assisted with the initial planning for the dam. However, the dam wasn't built according to Mr. Kuhn's recommendations. The height of the dam and spillway were raised and the spillway width was decreased. The local Soil Conservation Service office doesn't have any records concerning Benson Lake. Benson Lake Dam was originally called Schneider Lake Dam.

h. Normal Operational Procedures

The dam is used to impound water for recreational use. Normal procedure is to allow the lake to remain as full as possible with the water level being controlled by rainfall, runoff, evaporation and the elevation of the spillway crest.

1.3 Pertinent Data

a. Drainage Area (square miles): 0.23

b. Discharge at Damsite

Estimated experienced maximum flood (cfs): 300

Estimated ungated spillway capacity with
reservoir at top of dam elevation (cfs): 338

c. Elevation (feet above MSL)

Top of dam (minimum): 710

Spillway crest: 708.2

Normal Pool: 708.2

Maximum Experienced Pool 710-

Observed Pool: 708.2

d. Reservoir

Length of pool with water surface
at top of dam (minimum) elevation (feet): 1000

e. Storage (Acre-Feet)

Top of dam (minimum) 20

Spillway crest: 14

Normal Pool: 14

Maximum Experienced Pool: 20-

Observed Pool: 14

f. Reservoir Surfaces (Acres)

Top of dam (minimum): 4.4

Spillway crest: 3

Normal Pool: 3

Maximum Experienced Pool: 4+

Observed Pool: 3

g. Dam

Type:	earthfill
Length:	227 feet
Structural Height:	25 feet
Hydraulic Height:	25 feet
Top width:	12 feet
Side slopes:	
Downstream	1V to 2H
Upstream	1V to 3H (crest to water surface)
Zoning:	Unknown
Impervious core:	Unknown
Cutoff:	Unknown
Grout curtain:	Unknown

h. Diversion and Regulating Tunnel None

i. Spillway

Type:	Trapezoidal open channel, uncontrolled
Length of crest:	45 feet (Bottom width)
Crest Elevation (feet above MSL):	708.2

j. Regulating Outlets None

SECTION 2: ENGINEERING DATA

2.1 Design

Design drawings or calculations are not available for the dam.

2.2 Construction

The dam was built by Mr. Glennon Epple of Hermann, Missouri. No construction records or data are available relating to the construction of the dam.

2.3 Operation

No operational records or data are available for the dam.

2.4 Evaluation

a. Availability

No design drawings, design computations, construction data, or operation data are available.

In addition, no pertinent data were available for review of hydrology, spillway capacity, flood routing through the reservoir, slope stability, seepage analyses, or foundation conditions.

b. Adequacy

The lack of engineering data did not allow for a definitive review and evaluation. Therefore, the adequacy of this dam could not be assessed from the standpoint of reviewing and evaluating design, operation and construction data, but is based primarily on visual inspection, past performance history, and sound engineering judgement.

Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available, which is considered a deficiency. These seepage and stability analyses should be performed for appropriate loading conditions (including earthquake loads) and made a matter of record.

c. Validity

No valid engineering data are available.

SECTION 3: VISUAL INSPECTION

3.1 Findings

a. General

A visual inspection of the Benson Lake Dam was made on April 24, 1980. The following persons were present during the inspection:

<u>Name</u>	<u>Affiliation</u>	<u>Disciplines</u>
Dr. M.A. Samad	PRC Engineering Consultants, Inc.	Project Engineer, Hydraulics and Hydrology
Mark R. Haynes	PRC Engineering Consultants, Inc.	Soils and Mechanical
Robert G. McLaughlin	PRC Engineering Consultants, Inc.	Civil
Razi Quraishi	PRC Engineering Consultants, Inc.	Geology
John Lauth	Consoer, Townsend & Assoc., Ltd.	Civil and Structural
Mr. Wilbur Benson	Representative of the Owner	

Specific observations are discussed below.

b. Dam

The dam crest supports an unmaintained vegetative cover which appears to be adequate protection against surface erosion. A comprehensive inspection of the crest was hampered due to the growth of vegetation. The curvature in the alignment and the crown in the crest do not appear to be due to an instability in the embankment. The dam was probably constructed this way. There was no evidence of significant settlement on the crest. No significant deviations in horizontal or vertical alignment were apparent. According to Mr. Wilbur Benson, the dam has never been overtopped and no evidence was observed indicating the contrary.

The upstream slope has no riprap protection. Some minor erosion due to wave action has occurred near the water surface. The slope above the water surface is adequately protected against surface erosion by a good growth of vegetation. No erosion gullies due to surface runoff were observed. Two trees were observed on the slope near the spillway. A comprehensive inspection of the slope was hampered due to the growth of vegetation. No settlements or bulges which would indicate an instability of the slope were apparent.

The downstream slope has a heavy growth of unmaintained vegetation which appeared to be adequate protection against surface erosion. No erosion due to surface runoff was observed. Considerable amount of trees were growing on the slope. In one area from approximately 50 feet to 100 feet to the right of the spillway, three scarps were observed. Two of the scarps were fairly shallow and approximately 3-feet wide. The other scarp was approximately 20-feet wide at the top and

30-feet wide at the bottom. The scarp extends from the toe of the dam to within 5 feet of the crest. The slope near the top of the scarp was near vertical. According to Mr. Benson, this area has been this way since 1977 when the Benson's took ownership of the property. Some indications indicate that the slough occurred fairly recently. The leaning of the young trees toward the slope in the area indicate that the slough had occurred fairly recently, however, grass has grown back on the steep sections of the scarp. Although seepage was observed on the slope in the area of the scarps, it was not possible to measure the flow rate for this investigation. Cattails were observed in the area which indicates that water (seepage) is present most of the time. No other depressions, bulges or cracks which would indicate an instability of the embankment were apparent on the slope.

Rodent activity was observed on the embankment. Several one inch diameter rodent holes were observed on the crest and the upstream slope. One large rodent hole was observed on the downstream slope. It was approximately 6 inches in diameter.

A small natural drainage channel was observed just downstream of the toe of the dam. The channel runs parallel to the embankment from the right abutment to the discharge channel of the spillway. The channel appeared to be used to drain the surface runoff of the right abutment area. Some flowing water was observed in the channel; however, it was not possible to determine whether or not this flow was due at least in part to seepage through the embankment or foundation.

Both abutments slope gently upward from the crest. No erosion which would affect the safety of the embankment or appurtenant structures was observed on either abutment. No seepage or instabilities which would affect the safety or stability of the dam were apparent on either abutment. The left abutment supports the spillway and the right abutment supports a gravel access road which runs perpendicular to the embankment. Rock outcrops were observed in the spillway discharge channel and on the right abutment.

c. Project Geology and Soils

(1) Project Geology

The damsite is located on an unnamed tributary of the Frene Creek in the Salem Plateau section of the Ozark Plateaus Physiographic Province. Deep dissection of topography by major streams is one of the important characteristics of the Salem Plateau section. There is a wide distribution of dolomites and limestones in the Salem Plateau. Cuestaform topography is exhibited in this plateau section, consisting of two major escarpments, namely the Crystal Escarpment and Burlington Escarpment. Deep dissection in dolomites and limestones is a major factor in the development of many springs in this area. The topography in the damsite vicinity is rolling to hilly with U to V shaped valleys. Elevation ranges from 927 feet above M.S.L. (nearly 0.5 miles northwest of the damsite) to 700 feet above M.S.L. at the Benson Lake. The reservoir slopes are generally 5° to 18° from horizontal. The reservoir appears to be watertight and free of any potential slide activity. The area at the damsite is covered with slope wash deposits of glacial-fluvial and loess in origin. These deposits consist of reddish-brown silty clay.

The inlet and outlet areas of the unnamed tributary of Frene Creek contain Quaternary Alluvium. Outcrops of Ordovician moderately weathered, hard Dolomitic rocks, horizontally interbedded with brown *Calcareous sandstones* and light gray shales, with a strike of N50E are exposed at the base of the spillway cut and at the downstream channel of the spillway. Each unit of these rocks is three feet thick, with horizontal to blocky joint pattern.

The areal bedrock geology beneath the slope wash deposits as shown on the geologic map of Missouri (1979), Plate 3 consists of Pennsylvanian rocks undifferentiated, Ordovician St. Peter's sandstone and Ordovician Dolomitic rocks. No faults have been identified in the vicinity of the damsite. The closest trace of a fault is the Cuba Fault nearly 22 miles south of the damsite. The Cuba Fault had its last movement in post-Pennsylvanian time. *This fault appears to have no effect on the damsite.*

Benson Lake Dam consists of an homogeneous earth-fill embankment and a spillway located at the right abutment end of the embankment. No boring logs or construction reports were available which would indicate foundation conditions encountered during the dam construction. It is assumed that the embankment probably rests on brownish-gray *Calcareous sandstone* interbedded with shales and dolomites. The spillway is cut into hard sandstone interbedded with shales and dolomites. The spillway rockcut slopes are relatively stable. Minor localized rock debris were observed at the foot of the slope at the downstream channel walls of the spillway.

(2) Project Soils

According to the "Missouri General Soil Map and Soil Association Descriptions" published by the Soil Conservation Service, the materials in the general area of the dam belong to the soil series of Gerald-Union-Goss in the Ozarks family. The soils were basically formed from loess and cherty limestone residuum. The permeability of these soils range from moderate to very slow.

Materials removed from the embankment on the upstream and downstream slopes approximately 1 foot below the vegetative cover appeared to be a light brown silty fine to medium sand. Based upon the Unified Soil Classification System, the soil probably be classified as a SM. This soil type generally has the following characteristics: semipervious to impervious with a coefficient of permeability less than 100 feet per year; medium to high shear strength; and a low to intermediate resistance to piping.

d. Appurtenant Structures

(1) Spillway

The banks of the spillway channel especially the left bank appear to be of easily erodible material as there are several erosion gullies forming along the slope. Although the channel is clear at the inlet area, the bottom of channel, a short distance downstream, becomes heavily laden with tall grass, bushes, and even a sapling or two. The bottom of channel seems to be in easily erodible soil also but, in an area where a rock outcropping occurs. There is much evidence of the erosion and rock downstream of the drop where the invert slope increases causing higher velocities. Sloughing

also seems to be present in this downstream portion. The entire bottom of channel is in bedrock through the sharp turn to the right and on down to the downstream channel.

(2) Outlet Works

There is no level drain or outlet works provided for this dam.

e. Reservoir Area

The water surface elevation was 708.2 feet above MSL on the day of the inspection. The reservoir rim is lined with trees along the right side which is also where a road runs adjacent to the reservoir. The remainder of the reservoir rim has mild grassy slopes. The slopes above the reservoir rim are mild and grass covered. The forested area begins a few hundred feet away from the reservoir rim. At least three drainage swales from the surrounding forest empty into the reservoir. There are no houses or other structures built in close proximity to the reservoir.

f. Downstream Channel

The downstream channel is well defined. The channel is 5 feet wide and 3 feet deep and has a side slope of 1V to 2H on the right side and 1V to 5H on the left side in the proximity of the damsite. Some trees and tall vegetation were observed growing on the channel. The trees and the tall vegetation will reduce the hydraulic efficiency of the channel.

3.2 Evaluation

The visual inspection did reveal one item which was significant enough to possibly warrant immediate remedial action. The scarps observed on the downstream slope indicate instability of the slope. The slope appeared to be stable at the time of the inspection, however, the potential of further sloughing of the slope is still there. The seepage observed in the area is also detrimental to safety and stability of the embankment. The seepage increases the potential for further failure in this area. The potential of the embankment to fail in this area is also increased if the dam is overtopped, the slope would probably erode faster in this area thus increasing the potential of failure. The embankment is also weaker in this area and the surcharge of water on the embankment as the reservoir level rises above the spillway crest could cause the embankment to fail.

The following conditions were observed which could affect the safety of the facility and will require maintenance within a reasonable period of time.

1. The minor wave erosion on the upstream slope does not appear to affect the stability of the dam in its present condition. Nevertheless, continual erosion of the slope could be detrimental to the stability of the dam.

2. The trees observed on the downstream and the upstream slopes pose a potential danger to the safety of the dam depending upon the extent of the root system. The roots of trees present possible paths for piping through the embankment. The root systems can also do damage to the embankment from being uprooted by a storm.

3. Rodent activities observed on the embankment could jeopardize the safety of the dam. The holes created by the animals make avenues for possible piping.

4. The vegetation on the embankment should be properly maintained. A heavy growth of vegetation on the embankment hinders a comprehensive inspection of the dam and potential problems could go undetected.

5. Although the spillway area does not seem to be in a condition that jeopardizes the safety of the dam, the following conclusions seem likely: (a) the erosion through the left bank will get worse and soil will be washed downstream if left in the "as is" condition, (b) the tall grass etc. growing within the channel slows the velocity of the flow thus causing some backwater effects, and (c) the channel banks downstream of the drop will continue to erode and slough into the bottom of channel.

6. If water overflows the roadway at the right abutment and flows down along the upstream right abutment contact, problems could arise due to a weakening between the dam and the abutment.

SECTION 4: OPERATIONAL PROCEDURES

4.1 Procedures

Benson Lake Dam is used to impound water from rainfall and runoff for recreation. The water level below the spillway crest is allowed to remain as high as possible.

4.2 Maintenance of Dam

The dam is maintained by the owner, Mr. Clifford Benson, and his brother, Mr. Wilbur Benson. The maintenance of the dam appears to be inadequate. The downstream slope is covered with dense vegetation, bushes, saplings and trees and on the upstream slope a few small trees and saplings are growing.

There is an erosion gully at the downstream side of the spillway. This erosion should be arrested before it can do any damage to the embankment.

There have not been any major repairs done to the dam since its original construction.

4.3 Maintenance of Operating Facilities

There are no operating facilities associated with this dam.

4.4 Description of Any Warning System in Effect

The inspection team is not aware of any existing warning system in effect.

4.5 Evaluation

The maintenance at Benson Lake Dam appears to be inadequate at this time. The remedial measures described in Section 7 should be undertaken to improve the condition of the dam.

SECTION 5: HYDRAULIC/HYDROLOGIC

5.1 Evaluation of Features

a. Design

The watershed area of Benson Lake Dam upstream from the dam axis consists of approximately 147 acres. There is an upstream dam above Benson Lake Dam. The watershed area between the upstream dam and Benson Lake Dam investigated in this report is about 93 acres. Most of the watershed area is wooded with some range and pasture land. Land gradients in the watershed average roughly 7 percent. Benson Lake Dam is located on an unnamed tributary of Frene Creek. The reservoir is about 2-1/4 miles upstream from the confluence of the unnamed tributary and Frene Creek. At its longest arm the watershed is approximately 0.8 mile long. A drainage map showing the watershed, the downstream hazard zone, and location of the upstream dam is presented as Plate 1 in Appendix B.

Evaluation of the hydraulic and hydrologic features of Benson Lake Dam was based on criteria set forth in Corps of Engineers' "Engineer Regulation No. 1110-2-106", and additional guidance provided by the St. Louis District of the Corps of Engineers. The Probable Maximum Flood (PMF) was calculated from the Probable Maximum Precipitation (PMP) using the methods outlined in the U.S. Weather Bureau Publication, Hydrometeorological Report No. 33. The probable maximum storm duration was set at 24 hours, and storm rainfall distribution was based on criteria given in EM 1110-2-1411 (Standard Project Storm). The SCS method was used for deriving the unit

hydrographs, utilizing the Corps of Engineers' computer program HEC-1 (Dam Safety Version). Two unit hydrographs were derived. One unit hydrograph was for the drainage above the Upstream Dam; another unit hydrograph was for drainage area between the Upstream Dam and Benson Lake Dam. The SCS method was used for determining loss rate. The hydrologic soil group of the watershed was determined by use of published soil maps. The hydrologic soil group of the watershed and the SCS curve number are also presented in Appendix B. The curve number, the unit hydrograph parameters, and the PMP rainfall were directly input to the HEC-1 (Dam Safety Version) computer program to obtain the PMF hydrograph. The computed peak discharges of the PMF and one-half of the PMF at the Upstream Dam reservoir are 1159 cfs and 579 cfs respectively. The peak discharges of the PMF and one-half of the PMF for the area between the Upstream Dam and Benson Lake Dam are 2026 and 1013 cfs respectively. Both the PMF and one-half of the PMF inflow hydrographs at the Upstream Dam were routed through the Upstream reservoir by the Modified Puls Method, also utilizing the HEC-1 (Dam Safety Version) computer program. A storm of 50 percent and 25 percent PMF, respectively, preceded the PMF and 50 percent PMF by four days. The reservoir was assumed at the mean annual high water level at the beginning of the antecedent storm. The mean annual high water level for the Upstream Dam was estimated to be at the crest of the spillway. The antecedent 50 percent PMF storm, when routed through the reservoir will leave the reservoir at the same elevation as the spillway crest at the end of four day period. Thus the reservoir was assumed at the crest level of the spillway at the start of the routing computation for PMF, one-half of the PMF and other PMF ratio floods. The failure elevation of the upstream dam was set at the minimum elevation of the top of dam. The breach dimension for the upstream dam was determined according to the guidelines furnished by the St. Louis Dis-

trict Corps of Engineers.

The peak outflow discharges with dam break for the PMF and one-half of the PMF at the Upstream Dam are 1091 cfs and 578 cfs, respectively. Both the PMF and one-half of the PMF when routed through the reservoir resulted in overtopping of the Upstream Dam. The outflow hydrographs at the Upstream Dam were routed through the channel between the Upstream Dam and Benson Lake Dam and then were combined with the PMF and one-half of the PMF hydrographs for Benson Lake Dam. The combined hydrographs for both the PMF and one-half of the PMF, were then routed through Benson Lake Dam reservoir. The reservoir was assumed at mean annual high water level at the beginning of the routing computation. The mean annual high water level for Benson Lake Dam Reservoir was estimated to be at the crest of the spillway. The peak outflow discharges for the PMF and one-half of the PMF at Benson Lake Dam are 2,887 cfs and 1,340 cfs, respectively. Both the PMF and one-half of the PMF, when routed through the reservoir resulted in overtopping of Benson Lake Dam.

The sizes of physical features utilized to develop the stage-outflow relation for the spillway and overtopping of the dams were prepared from field notes and sketches prepared during the field inspection. The reservoir elevation-area data were obtained from the U.S.G.S. Hermann, Missouri Quadrangle topographic map (7.5 minute series). The spillway and dam overtop-rating curve and the reservoir elevation-area curve for Benson Lake Dam are presented as Plates 2 and 3 in Appendix B.

From the standpoint of dam safety, the hydrologic design of a dam must aim at avoiding overtopping. Overtopping is especially dangerous for an earth dam because of its erodable characteristics. The safe hydrologic design of an embankment dam requires a spillway discharge capability combined with an embankment crest height that can handle a very large and exceedingly rare flood without overtopping.

The Corps of Engineers designs dams to safely pass the Probable Maximum Flood that could be generated from the dam's watershed. This is generally the standard for dam safety where overtopping would pose any threat to human life. Accordingly, the hydrologic requirement for safety for this dam is the capability to pass the Probable Maximum Flood without overtopping.

b. Experience Data

It is believed that records of reservoir stage or spillway discharge are not maintained for this site. However, according to Mr. Wilbur Benson, the maximum reservoir level was about a few inches above the roadway at the right abutment.

c. Visual Observations

Observations made of the spillway during the visual inspection are discussed in Section 3.1d(1) and evaluated in Section 3.2.

d. Overtopping Potential

As indicated in Section 5.1.a, both the Probable Maximum Flood, and one-half of the Probable Maximum Flood when routed through the reservoir, resulted in overtopping of the dam. The peak outflow discharges for the PMF are 2,887 and 1,340 cfs, respectively. The maximum capacity of the spillway just before overtopping the dam is 338 cfs. The PMF overtopped the dam by 2.33 feet and one-half of the PMF overtopped the dam by 1.35 feet. The total duration of overflow over the top of dam is 5.25 hours during the PMF and 1.17 hours during one-half of the PMF. The spillway/reservoir system of Benson Lake Dam is capable of accommodating a flood equal to approximately 20 percent of the PMF just before overtopping the dam. The reservoir/spillway system of Benson Lake Dam will accommodate the one-percent chance flood without overtopping.

The surface soils in the embankment and the spillway appear to be a sand-silt mixture. The dam is overtopped by over 2 feet during the occurrence of the PMF. The maximum velocity of flow in the spillway during the PMF will be about 8 ft/sec, which exceeds the permissible velocity (5 ft/sec) in the spillway. The dam itself would be susceptible to erosion due to high velocity of flow on its downstream slope, specially in the area of the scarps observed on the downstream slope, during overtopping of the dam.

SECTION 6: STRUCTURAL STABILITY

6.1 Evaluation of Structural Stability

a. Visual Observations

The evidence of the past sloughing and the present seepage observed on the downstream slope indicates a serious instability and potential for failure of the embankment in the area of the observed scarps. Seepage was observed in the area of the scarps. The scarps and the seepage observed on the slope indicate instability of the slope. The minor erosion of the upstream slope due to wave action was not serious enough to constitute an unsafe condition. Nevertheless, the erosion should be monitored and if the erosion continues, steps should be taken to control the problem. No other major signs of settlement or distress were observed on the embankment or foundation during the visual inspection. In the absence of seepage and stability analyses, no quantitative evaluation of the structural stability can be made.

The spillway crest area and the channel appear to be generally stable albeit in poor condition. The roadway, which will act as emergency spillway also appears to be in a stable condition.

b. Design and Construction Data

No design computations were uncovered during the report preparation phase. Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available. No embankment or foundation soil parameters were available for carrying out a conventional stability analysis on the embankment. No construction data or specifications relating to the degree of embankment compaction were available for use in a stability analysis.

c. Operating Records

No operating records are available relating to the dam or appurtenant structures. No regulated outlet works was provided for the dam. The water level on the day of the visual inspection was at the crest of the spillway. According to Mr. Wilbur Benson, the reservoir remains close to full at all times.

d. Post Construction Changes

No post construction changes are known to exist which will affect the structural stability of the dam.

e. Seismic Stability

The dam is located in Seismic Zone 1, as defined in "Recommended Guidelines For Safety Inspection of Dams" as prepared by the Corps of Engineers, and will not require a seismic stability analysis. An earthquake of the magnitude which would be expected in Seismic Zone 1 will not cause distress to a well designed and constructed earth dam.

Available literature indicates that no active faults exist near the vicinity of the damsite.

SECTION 7: ASSESSMENT/REMEDIAL MEASURES

7.1 Dam Assessment

The assessment of the general condition of the dam is based upon available data and visual inspections. Detailed investigations, testing, and detailed computational evaluations are beyond the scope of a Phase I investigation, however, the investigation is intended to identify any need for such studies.

It should be realized that the reported condition of the dam is based upon observations of field conditions at the time of inspection along with data available to the inspection team.

It is also important to note that the condition of a dam depends upon numerous and constantly changing internal and external conditions, and is evolutionary in nature. It would be incorrect to assume that the present condition of the dam will continue to represent the condition of the dam at some point in the future. Only through continued care and inspection can there be assurance that an unsafe condition could be detected.

a. Safety

The spillway capacity of Benson Lake Dam is found to be "Seriously Inadequate". The spillway/reservoir system will accommodate about 20 percent of the PMF without overtopping the dam. The surface soils in the embankment and the spillway appears to be a sand-silt mixture. The dam is overtopped by over 2 feet during the occurrence of the PMF. The maximum velocity of flow in the spillway during PMF will

be about 8 ft/sec. The velocity in the spillway will thus exceed the permissible velocity of 5 ft/sec (Kentucky Blue Grass-sandy silt). The dam would also be susceptible to erosion due to high velocity of flow on its downstream slope, due to overtopping of the dam during the occurrence of the PMF.

No quantitative evaluation of the safety of the embankment can be made in view of the absence of seepage and stability analyses. The present embankment, however, has reportedly performed satisfactorily since its construction without failure or evidence of instability, except for instability of the left side of the downstream slope. Reportedly, the dam has never been overtopped and there was no evidence indicating the contrary.

The safety of the dam can be improved if the deficiencies described in Sections 6.1a and 3.2 and below are properly corrected as described in Section 7.2. The trees observed on the downstream and upstream slopes pose a potential danger to the safety of the dam depending upon the extent of the root system. The roots of trees present possible paths for piping through the embankment. The root systems can also do damage to the embankment from being uprooted by a storm. Therefore, the trees should be removed from the embankment under the guidance of an engineer experienced in the design and construction of earthen dams.

The existence of burrowing animals on the embankment could jeopardize the safety of the dam. The holes created by the animals make avenues for possible piping. The extent of damage to the embankment done by the burrowing animals should be determined and corrective measures undertaken as required.

The spillway system seems to be functioning in a reasonably efficient manner and doesn't pose any hazards for the dam. The roadway at the right abutment, which will act as emergency spillway, was once overflowed during a flood. The roadway seems to be in good condition.

b. Adequacy of Information

Information relating to the design and construction of the dam is lacking. The conclusions presented in this report are based upon field measurement, past performance and present condition of the dam. Information on the design hydrology, hydraulic design, and the operation and maintenance of the dam were not available. Seepage and stability analyses comparable to the requirements of the "Recommended Guidelines for Safety Inspection of Dams" were not available, which is considered a deficiency.

c. Urgency

The steepness (almost vertical) of the scarps observed on the downstream slope, in conjunction with the seepage observed at the base of the scarps, poses a potential instability of the embankment, which should be investigated in the immediate future. The remaining remedial measures recommended in Section 7.2 should be accomplished within a reasonable period of time.

d. Necessity for Phase II Inspection

Based on results of the Phase I inspection, a Phase II inspection is not felt to be necessary. However, the remedial measures described in Paragraph 7.2 should be undertaken within the time frame recommended in Section 7.1(c).

7.2 Remedial Measures

a. Alternatives

There are several general options that may be considered to reduce the possibility of dam failure or to diminish the harmful consequences of such a failure. Some of these options are:

1. Increase spillway capacity to pass the Probable Maximum Flood without overtopping the dam.
2. Increase the height of the dam enough to pass the PMF without overtopping the dam. An investigation should also be done that includes studying the effects on the structural stability of the existing embankment and the spillway. The overtopping depth during the occurrence of the PMF, stated in Section 5.1d, is not the required or recommended increase in the height of the dam.
3. A combination of 1 and 2 above.

b. O & M Procedures

1. Perform an investigation of the stability and safety of the embankment due to the scarps and the seepage observed on the downstream slope.
2. The erosion due to wave action on the upstream slope should be monitored and if the erosion continues, protective measures should be employed to protect the slope from further damage.

3. Remove the trees from the downstream and upstream slopes of the dam. Removal of large trees should be under the guidance of an engineer experienced in the design and construction of earthen dams.
4. Determine the extent of damage done to the embankment by burrowing animals, and corrective repairs made as required. All burrowing animals should be eliminated from the embankment and their burrows properly backfilled and compacted.
5. The vegetation on the embankment should be properly maintained and an adequate vegetative cover retained on the embankment to protect it from surface erosion. A heavy growth of vegetation on the embankment could prevent a comprehensive inspection of the dam and potential problems could go undetected.
6. If during periods of spillage over the roadway at the right end of the dam, the water flows down the right upstream abutment contact area, a permanent berm should be constructed in order to direct this flow to a point beyond the abutment contact area and downstream toe. Once the flow is downstream from the abutment contact area and the toe of the dam, it may be directed towards the downstream channel.
7. The entire spillway should be watched and checked periodically for progressive erosion and sloughing which would be seriously detrimental to its proper functioning. If these things do occur, remedial action should be taken.

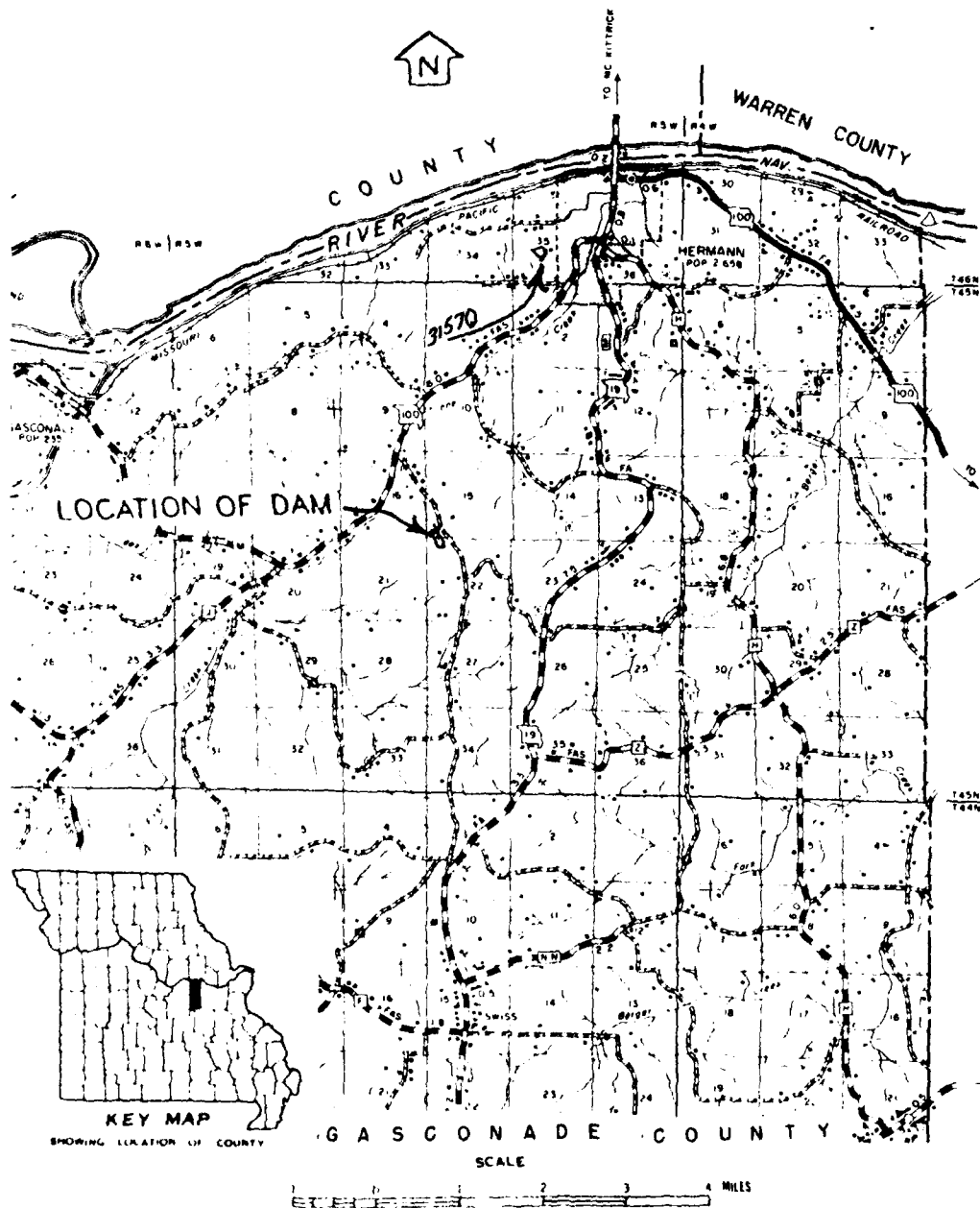
8. Seepage and stability analyses should be performed by a professional engineer experienced in the design and construction of earth dams.

9. The owner should initiate the following programs:

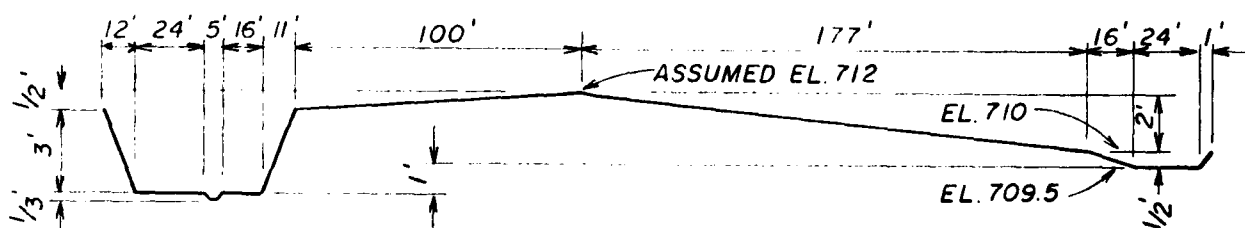
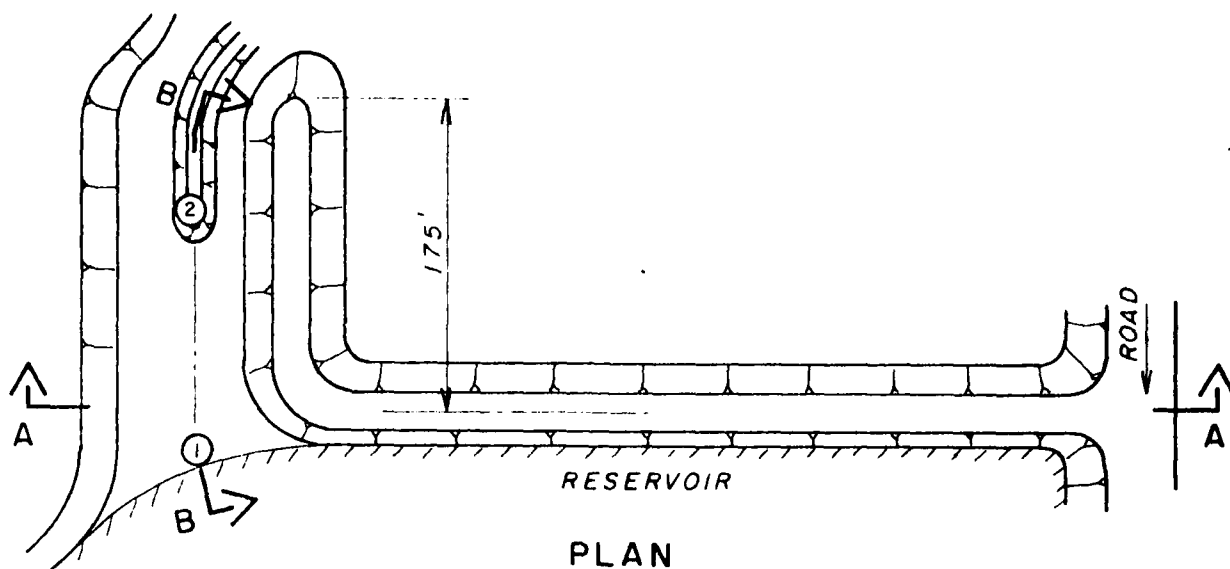
(a) Periodic inspection of the dam by a professional engineer experienced in the design and construction of earthen dams.

(b) Set up a maintenance schedule and log all visits to the dam for operation, repairs and maintenance.

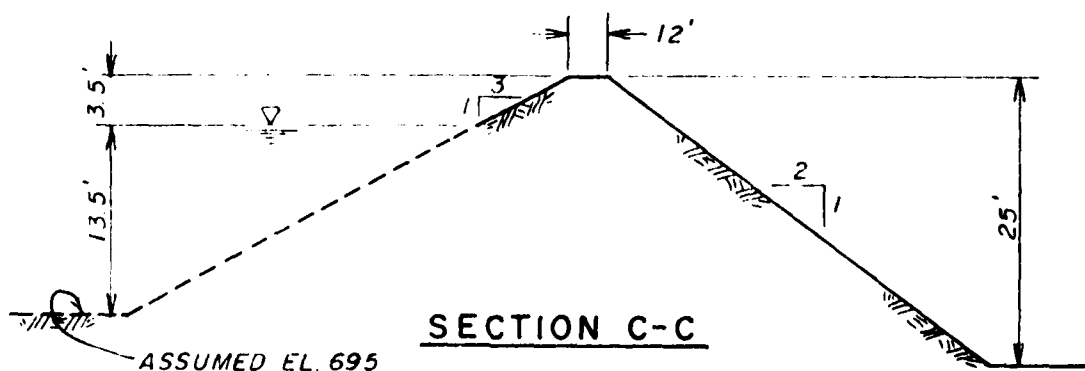
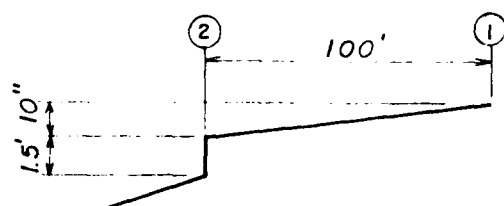
PLATES



LOCATION MAP - BENSON LAKE DAM
MO. 30667



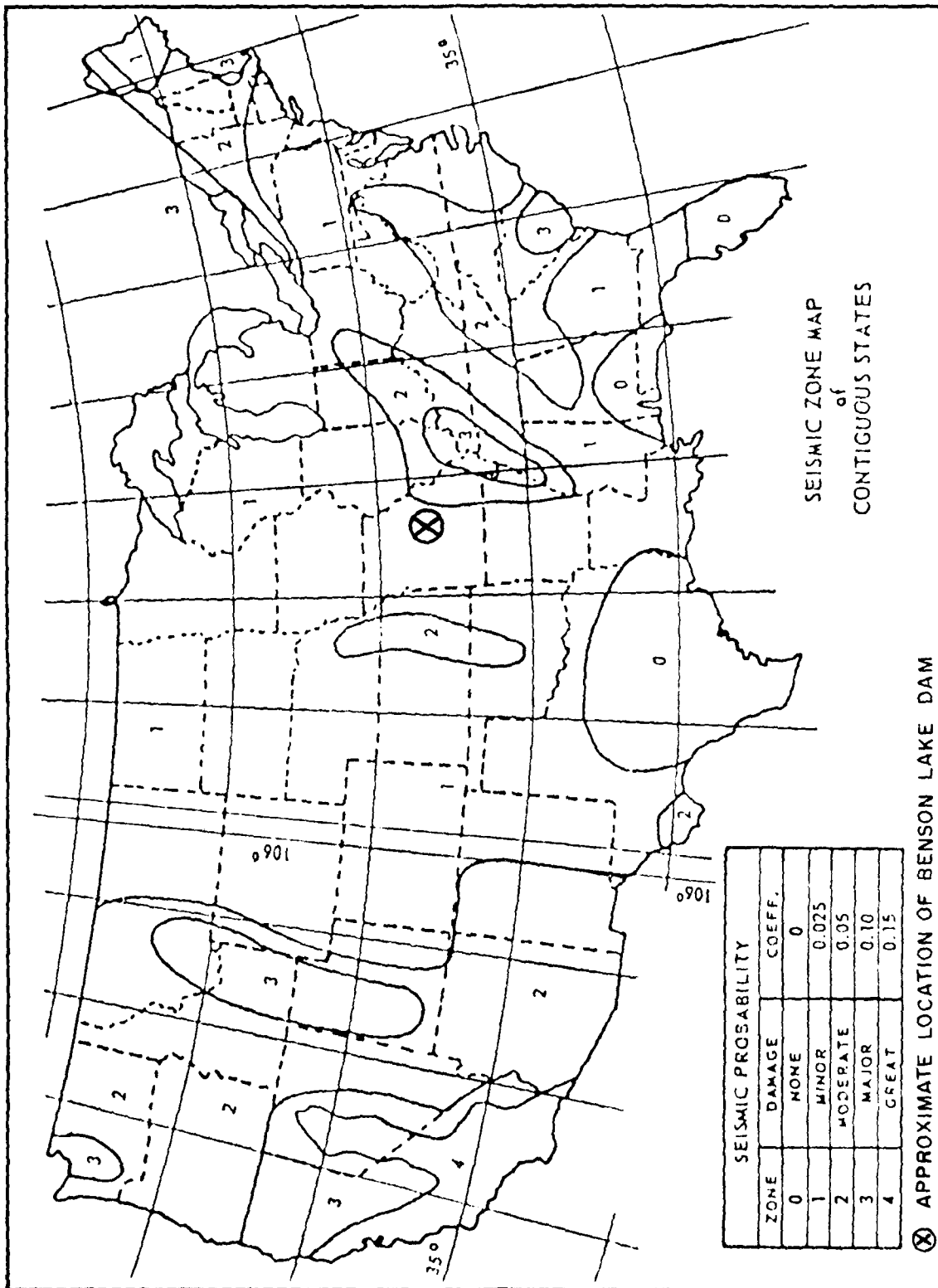
SCALE:
1" = 60' HORIZ.
VERT. - NOT TO SCALE



BENSON LAKE DAM (MO. 30667)
PLAN AND SECTIONS

LEGEND

<u>PERIOD</u>	<u>SYMBOL</u>	<u>DESCRIPTION</u>
QUATERNARY	Qal	ALLUVIUM: SAND, SILT, GRAVEL
	Pu	PENNSYLVANIAN UNDIFFERENTIATED
PENNSYLVANIAN	Pm	MARMATON GROUP: CYCLIC DEPOSITS OF SHALE, LIMESTONE AND SANDSTONE
	Pcc	CHEROKEE GROUP: CYCLIC DEPOSITS OF SHALE, LIMESTONE AND SANDSTONE
MISSISSIPPIAN	Mm	ST LOUIS FORMATION: LIMESTONE INTERBEDDED WITH SHALE.
		SALEM FORMATION: LIMESTONE INTERBEDDED WITH SHALE AND SILTSTONE
		WARSAW FORMATION: ARGILLACEOUS LIMESTONE AND CALCAREOUS SHALE
	Mo	KEOKUK - BURLINGTON FORMATION: CHERTY GRAYISH BROWN SANDY LIMESTONE
DEVONIAN	D	CHATTANOOGA SHALE, SYLAMORE SANDSTONE
ORDOVICIAN	Omk	MAQUOKETA SHALE, KIMMSWICK LIMESTONE
	Odp	DECORAH FORMATION: GREEN TO GRAY CALCAREOUS SHALE WITH THIN FOSSILIFEROUS LIMESTONE
	Osp	ST. PETER SANDSTONE
	Ojc	SMITHVILLE FORMATION POWELL DOLOMITE



APPENDIX A

PHOTOGRAPHS

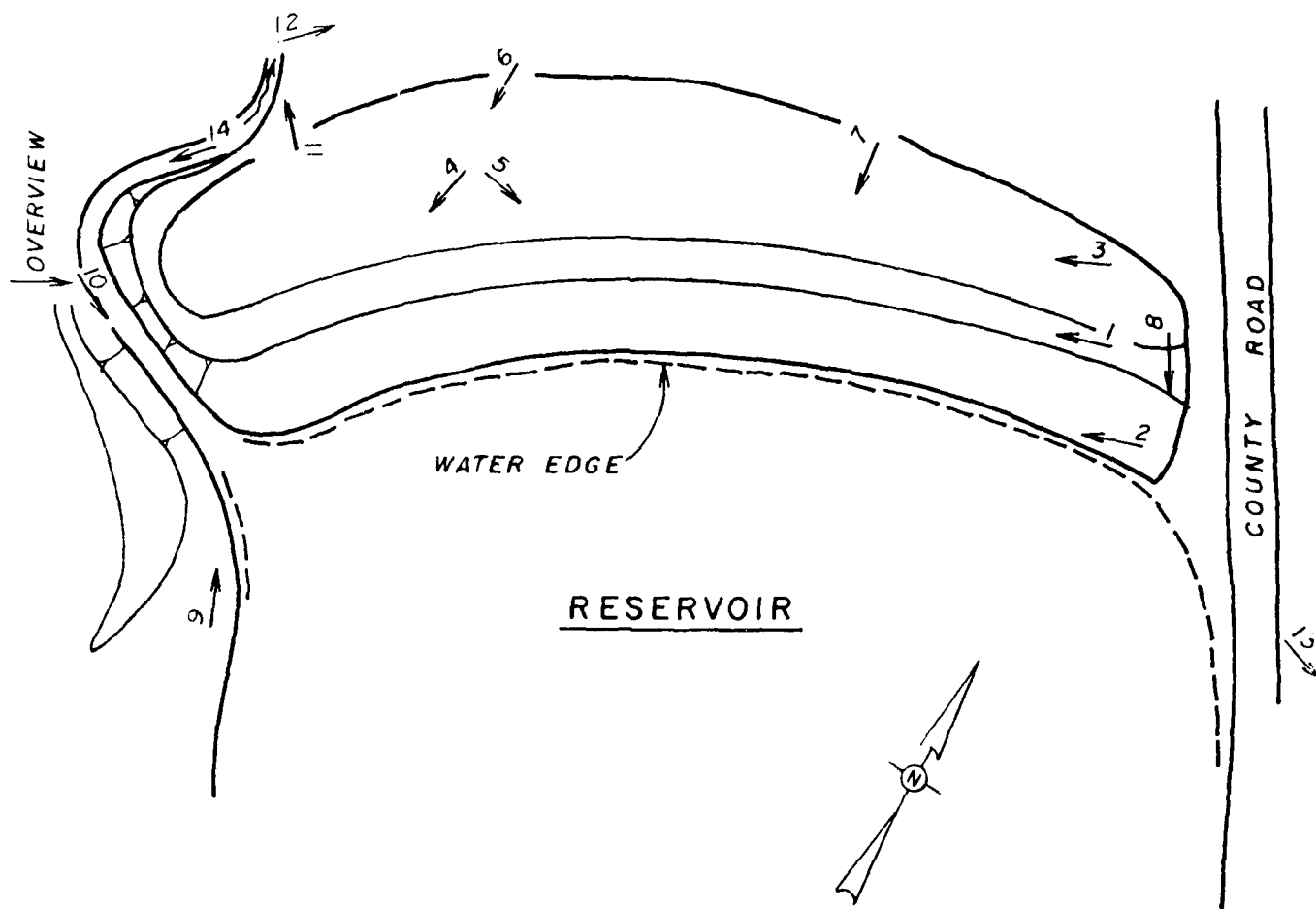


PHOTO INDEX
FOR
BENSON LAKE DAM

Benson Lake Dam

Photographs

- Photo 1 - Top of dam showing tall grass protection.
- Photo 2 - Upstream slope of dam showing dense grass protection with a tree and some small brush growing.
- Photo 3 - Downstream slope of dam showing dense grass protection adjacent to slope supporting trees and brush.
- Photo 4 - View of sloughed area on downstream slope of dam, supporting growth of cattail reeds; indicated continuous moisture condition.
- Photo 5 - View of sloughed area adjacent to area in photo 4.
- Photo 6 - View of very wet ground just below sloughed areas of photos 4 and 5.
- Photo 7 - View of hole indicating possible burrowing activity on downstream slope area.
- Photo 8 - Reservoir rim area showing adjacent road and mild grassy and tree-lined slopes.
- Photo 9 - Inlet to principal spillway showing small amount of rock slope protection.
- Photo 10 - Principal spillway channel showing brush, fence, sloughing, erosion, and dense grass growth.
- Photo 11 - Downstream channel area showing tree-lined banks and structure.

Photo 12 - Structures in area downstream of dam.

Photo 13 - Geology--Ordovician dolomite, horizontal, interbedded with brown, calcareous sandstone.

Photo 14 - Geology--Ordovician brown to light grey shale, interbedded with calcareous sandstone.

Benson Lake Dam

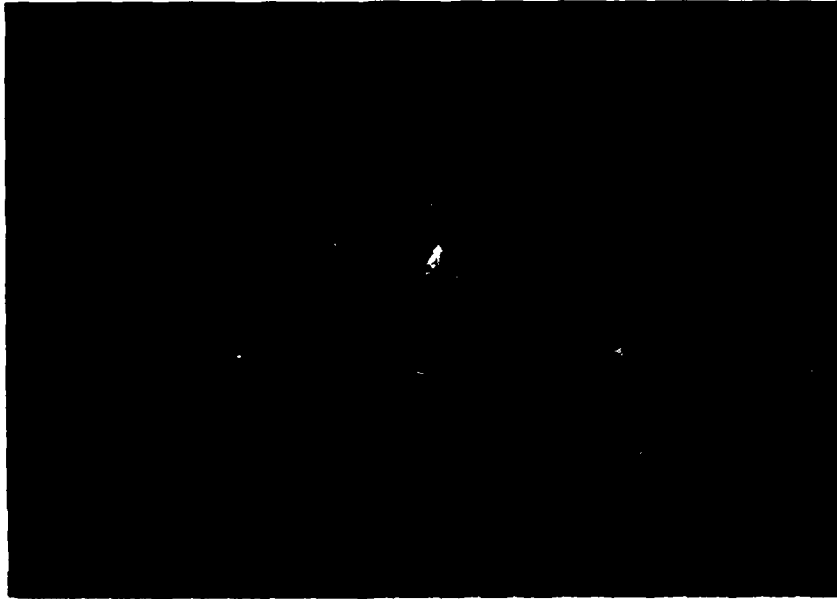


Photo 1



Photo 2

Benson Lake Dam

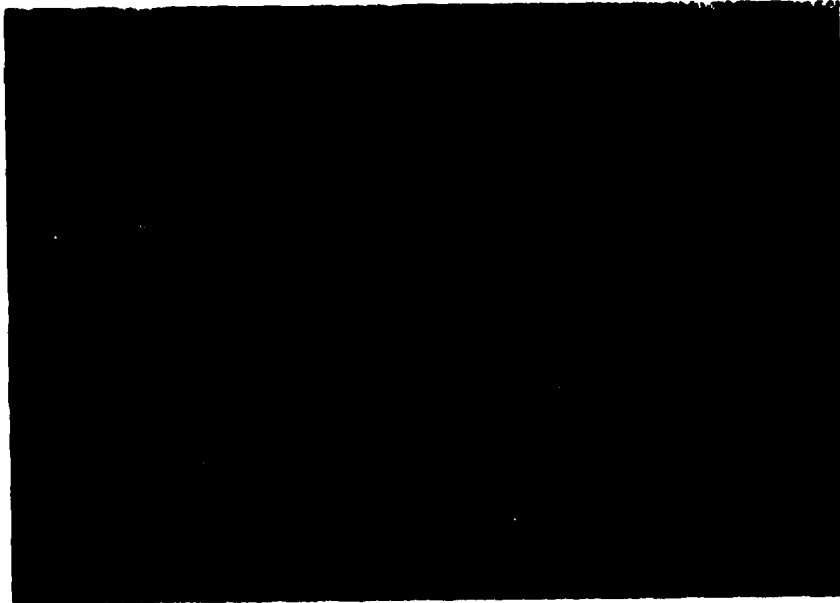


Photo 3



Photo 4

Benson Lake Dam



Photo 5

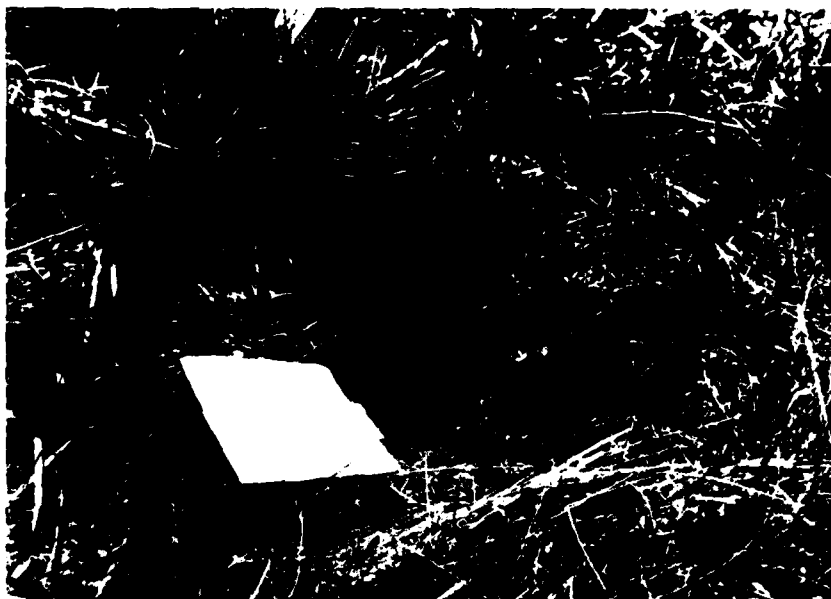


Photo 6

Benson Lake Dam



Photo 7



Photo 8

Benson Lake Dam

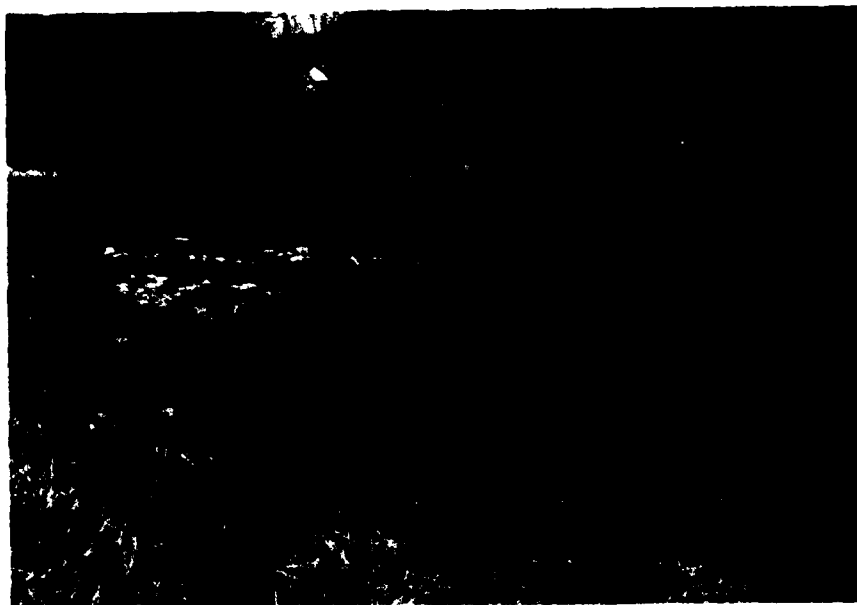


Photo 9



Photo 10

Benson Lake Dam



Photo 11

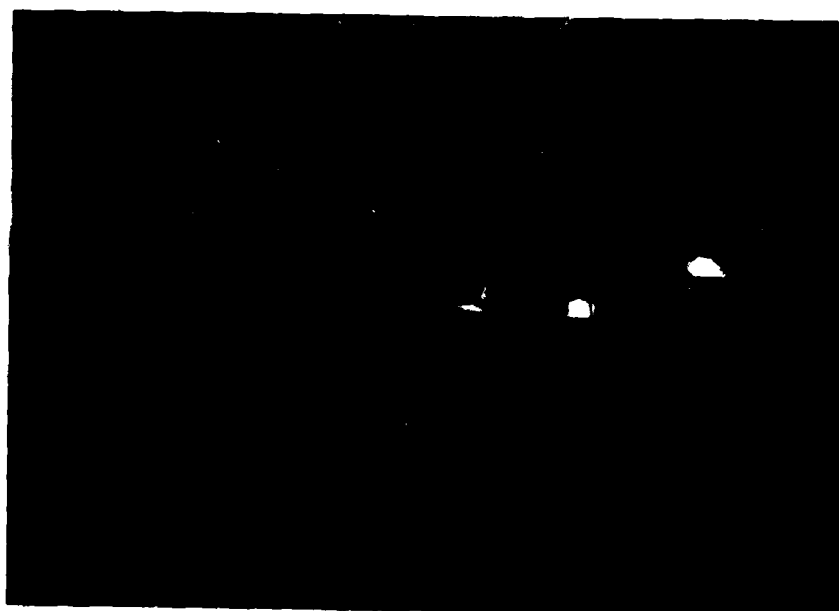


Photo 12

Benson Lake Dam



Photo 13

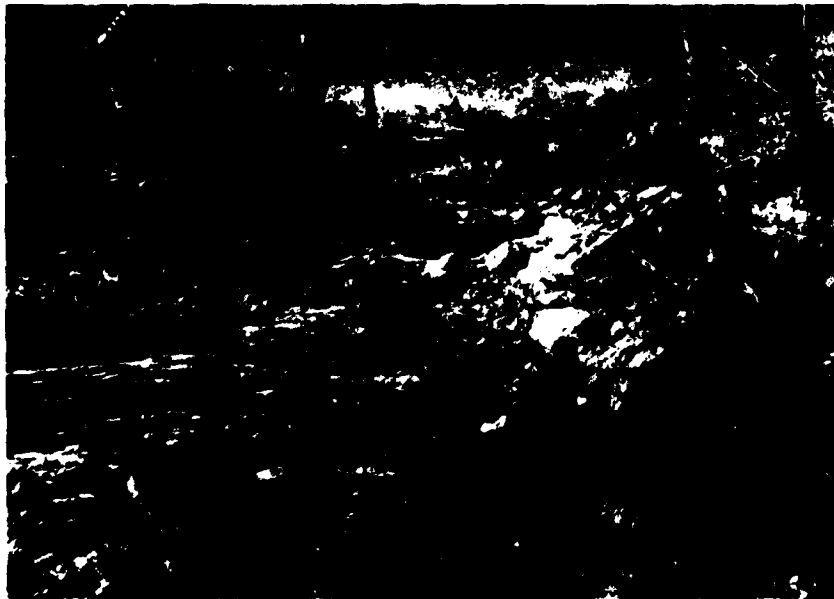
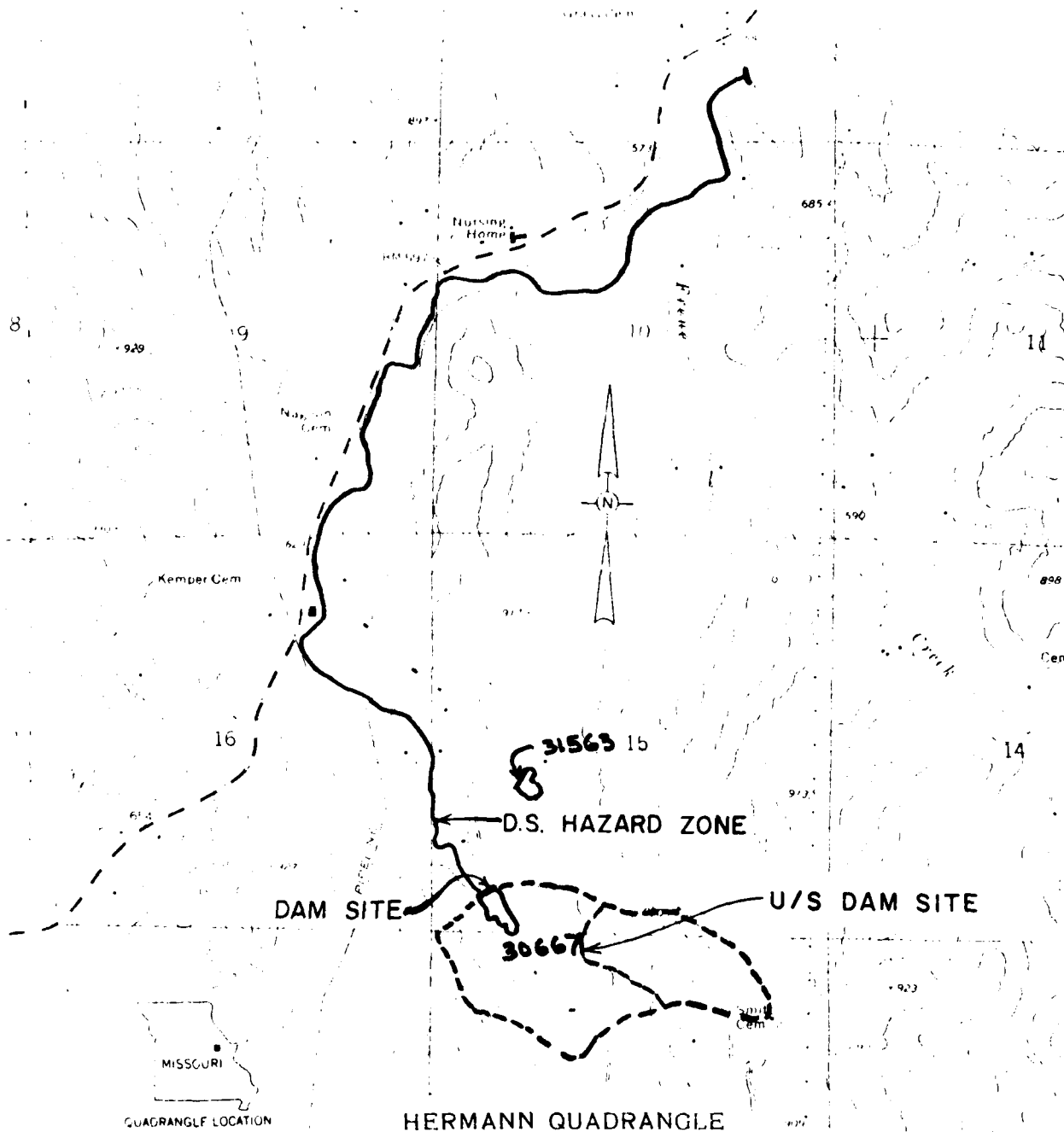


Photo 14

APPENDIX B

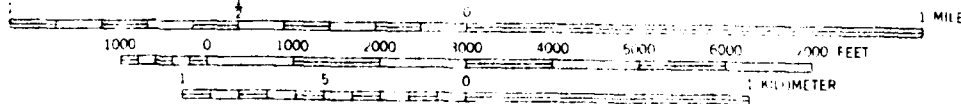
HYDROLOGIC AND HYDRAULIC COMPUTATIONS

PLATE I, APPENDIX B



HERMANN QUADRANGLE

SCALE 1:24,000



CONTOUR INTERVAL 10 FEET
DATUM IS MEAN SEA LEVEL

DRAINAGE BOUNDARY - - - - -

BENSON LAKE DAM MO 30667

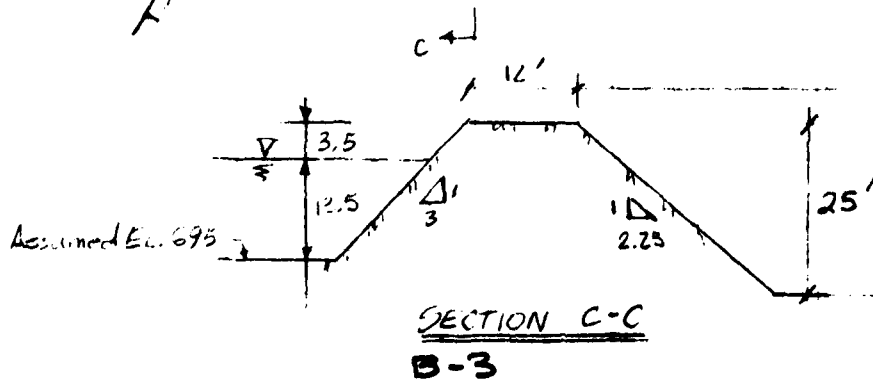
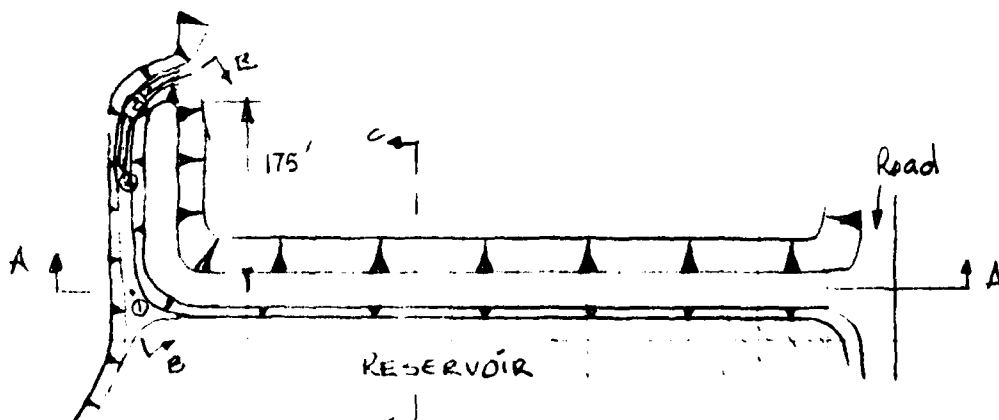
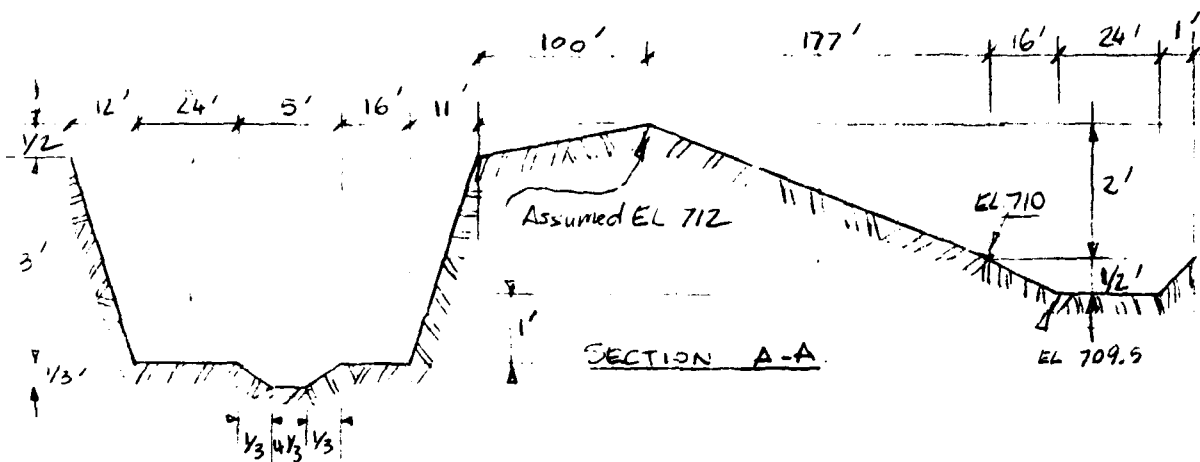
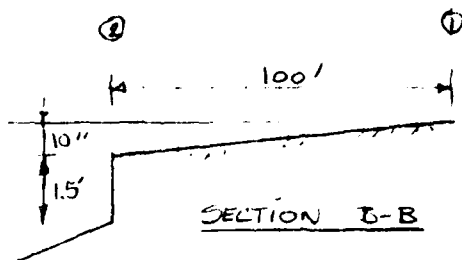
DRAINAGE BASIN

B-2

10-4

PRC ENGINEERING CONSULTANTS, INC.

DAM SAFETY INSPECTION / MISSOURI
 BENSON LAKE DAM #30667
 SLOTTED SPILLWAY RATING CURVE
 SHEET NO. 1 OF 5
 JOB NO. 1263
 BY FZ DATE MAY 80



B-3

PRC ENGINEERING CONSULTANTS, INC.

DESIGN OF INLET / MISSOURI

SHEET NO. 2 OF 5

BENEFIT LAKE

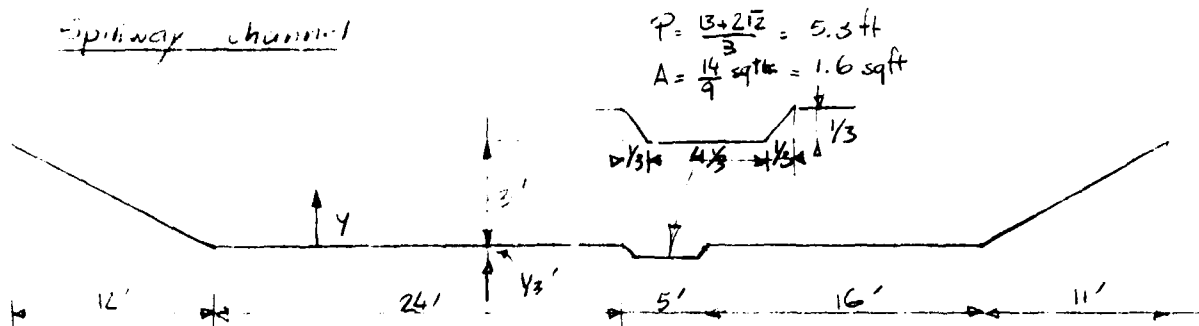
30667

JOB NO 1263

SMITHSONIAN OVER THE FALLING CURVE

BY FZ DATE MAY 80

Spillway channel



$$\text{Slope of channel} = \frac{10}{1200} = 0.0083$$

$$n = 0.03 \text{ assumed}$$

$$y \leq 3 \quad A = y(3.83y + 45) + 1.6$$

$$P = 45.3 + 7.2h$$

$$\frac{1.47 \times 5^{5/2}}{n} = \frac{1.47 \times 10.0033}{0.03} = 4.53$$

$$\left. \begin{array}{l} Q = 4.53 \frac{A^{5/3}}{P^{2/3}} \\ T = 45 + 7.67y \end{array} \right\}$$

$$T = 45 + 7.67y$$

$$y > 3 \quad A = 68y - 33$$

$$P = 64$$

$$\frac{1.47 \times 5^{5/2}}{n \cdot P^{2/3}} = 0.27$$

$$Q = 0.27 \frac{A^{5/3}}{P^{2/3}}$$

$$T = 68$$

$$y_c = \sqrt{\frac{A^3 g}{T}}$$

y_c	T_c	y_{NORMAL} for $Q = Q_c$	Remark
1'	280	1.16'	Subcritical
2'	303	2.17'	"
3'	1540	3.10'	"
4'	2542	4.05'	"
5'	3702	4.95'	Supercritical

PRC ENGINEERING CONSULTANTS, INC.

DAM SHEET: INLET / HIGGINS SHEET NO 3 OF 5
 KENSON LAKE DAM # 20667 JOB NO 1263
 SPIED AND CORRECTED BY J. C. R. E. BY FZ DATE MAY 80

Length required to go from critical depth to normal depth.

$$\Delta L = \frac{Y_N - Y_c}{0.0082 - \frac{N^2}{1.48 A_m R_m^{4/3}}} \cdot \frac{V_c^2}{g} \cdot \frac{N}{D} \cdot A_m R_m^{4/3} = \frac{\Delta_m^{5/3}}{T_m^{2/3}}$$

Y_c	Y_m	A_c	A_m	V_c	V_m	A_m	P_m	Q	N	D	ΔL
1	1.16	50.453	58.95	3.479	0.35	54.70	53.85	280	0.031	0.002	16'
2	2.17	106.44	117.31	0.887	0.737	112.13	61.81	808	0.020	0.0011	18'
3	3.10	171.12	172.45	1.258	1.103	174.54	69.46	1540	0.005	0.0008	6'

Conclusion the normal depth regime will be reached in a short distance and normal depth is to be considered for depth below 5'

PRC ENGINEERING CONSULTANTS, INC.

DAM SAFETY / MISSOURI

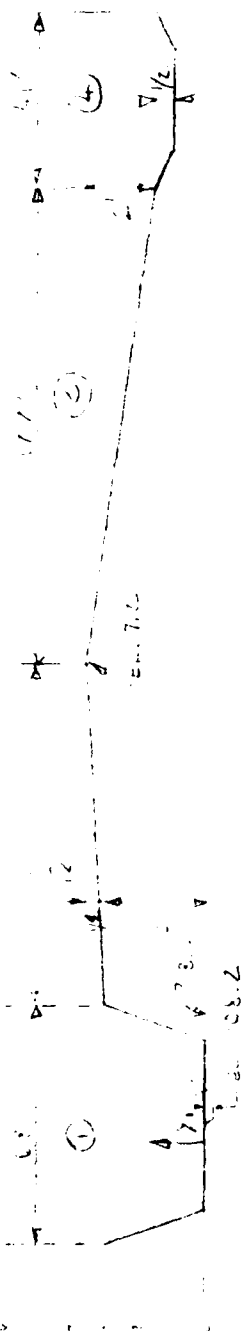
SHEET NO. 4 OF 5

LEMON LAKE DAM #3-667

JOB NO 1263

SPILLWAY & OVERTOP RATING CURVE

BY FR DATE MAY 80



$$\begin{aligned} \text{③ } d_{c3} &\leq 2 \Rightarrow d_{c3} = \frac{1}{2} H_3 \quad \left\{ \begin{array}{l} A_3 = \frac{177 d_{c3}}{4} \\ T_3 = \frac{177 d_{c3}}{2} \end{array} \right. \\ d_{c3} &> 2 \quad d_{c3} = (2H_3 + 1) \frac{1}{2} \quad \left\{ \begin{array}{l} A_3 = 177(d_{c3} - 1) \\ T_3 = 177 \end{array} \right. \\ Q_3 &= \sqrt{\frac{4.25}{T_3}} \end{aligned}$$

$$\begin{aligned} \text{② } H_2 &= H_1 - 3 \\ d_{c2} &= \frac{1}{4} (H_2 + \frac{1}{2} H_2) = \frac{8H_2 - 1}{12} \\ L_2 &= \frac{1}{T_2} (2d_{c2} - \frac{1}{2} H_2) = 25(4d_{c2} - 1) \\ Q_2 &= \sqrt{\frac{4.25}{T_2}} = 0.57 A_2^{3/2} \end{aligned}$$

Spillway ①					②					③				
Y_1	A_1	T_1	Q_1	$(\frac{H_1}{A_1})^{3/2}$	H_1	$\frac{H_2}{H_1 - 3}$	d_{c2}	A_2	Q_2	$\frac{H_3}{H_1 - 1.5}$	d_{c3}	T_2	A_3	Q_3
1	50.4	532	640	0.50	1.30	—	—	—	—	—	—	—	—	—
2	166.9	61.1	702	0.67	2.67	—	—	—	—	1.17	2.44	82.8	38.8	150
3	171.1	69.1	1418	1.07	4.07	1.07	0.80	54.7	229	2.57	2.05	177	185.3	1076
4	239.0	69.1	2473	1.66	5.66	2.66	1.86	160.7	1156	4.16	3.11	177	372.9	3071
5	327.0	—	3702	2.16	7.20	4.26	2.92	267.3	2480	5.76	4.17	177	561.7	5678
6	375.0	—	4997	2.76	8.76	5.76	3.92	367.3	3995	7.26	5.17	171	738.7	8563

PRC ENGINEERING CONSULTANTS, INC.

DAM SAFETY / MISSOURI

SHEET NO. 5 OF 5

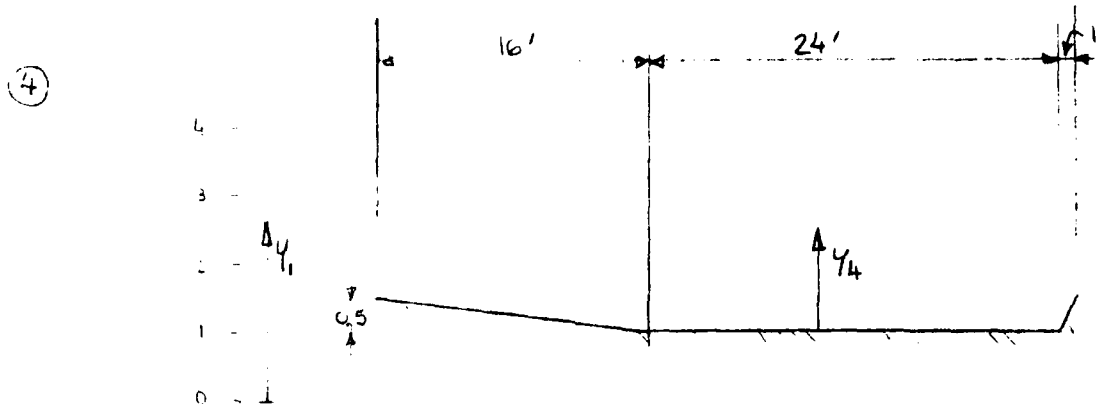
BERNARD LAKE DAM #30667

JOB NO. 1263

SPILLWAY & OVERTOP RATING CURVE (Cont'd)

BY FZ

DATE MAY 82



Assumed critical depth

$$A_4 = 41y_4 - 4.25$$

$$T_4 = 41'$$

$$V_4 = \sqrt{\frac{A_4 g}{T_4}}$$

$$Q_4 = A_4 V_4$$

$$\frac{V_4^2}{2g} = \frac{A_4}{2T_4}$$

$$H_4 = y_4 + \frac{V_4^2}{2g}$$

By iteration we have to find Q_4 for $H_4 + 1 = H_1$ (pg. 10)

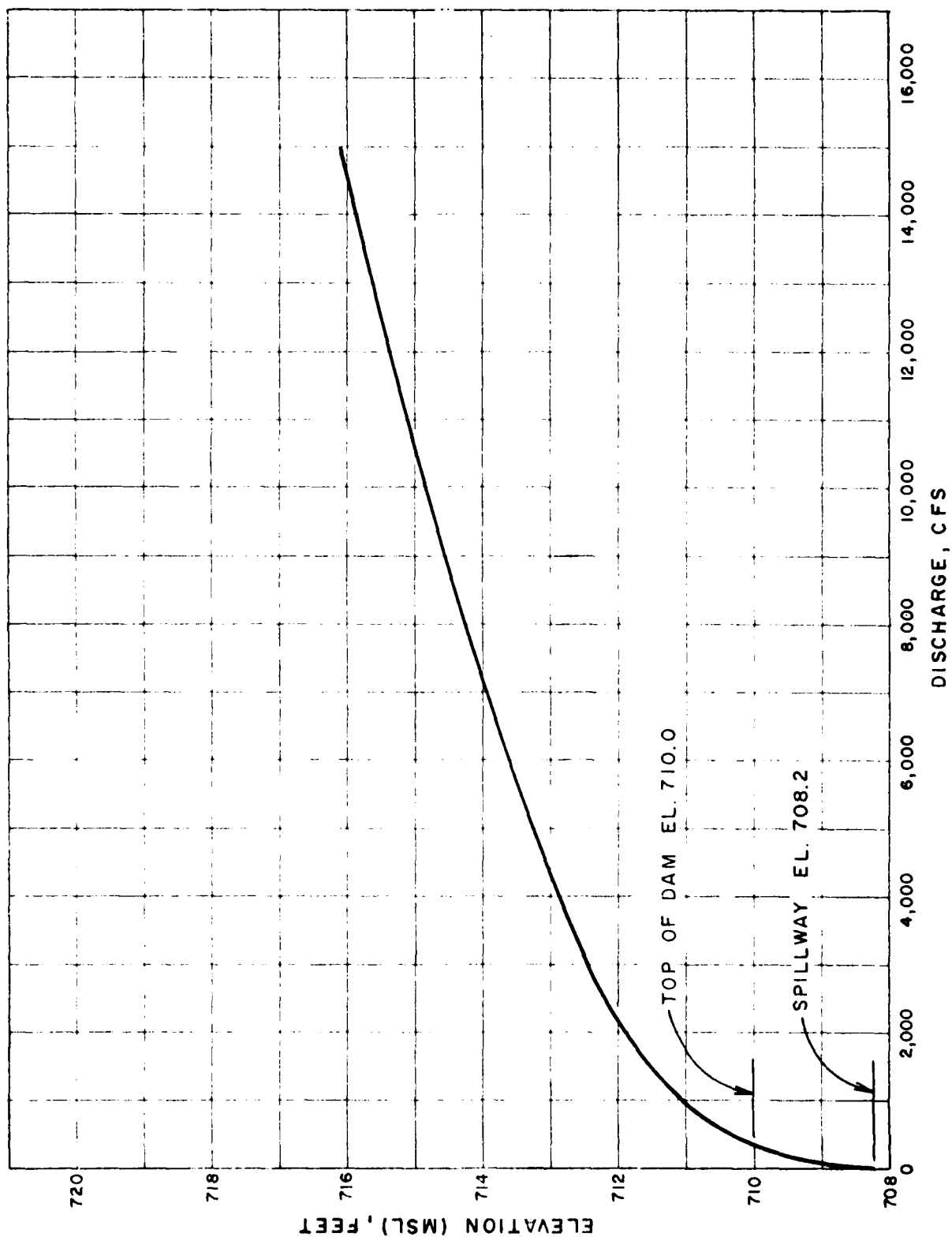
$$WSEL = 708.5 + H_1$$

1	H_1	y_4	A_4	$\frac{V_4^2}{2g}$	H_4	Q_4	$Q_1 + Q_2 + Q_3 + Q_4$	WSEL
1	1.3	0.258	5.73	0.092	0.30	14	233	709.80
2	2.67	1.148	46.02	0.522	1.67	248	1100	711.17
3	4.07	2.031	81.07	0.989	3.07	647	3370	712.57
4	5.47	2.842	124.57	1.511	4.66	1232	7932	714.16
5	6.87	3.608	168.28	2.052	6.26	1934	13794	715.76
6	8.26	4.268	207.28	2.552	7.76	2683	20238	717.26

$$y = 0.5$$

$$A = y(17y + 24)$$

$$T = 34y + 24$$



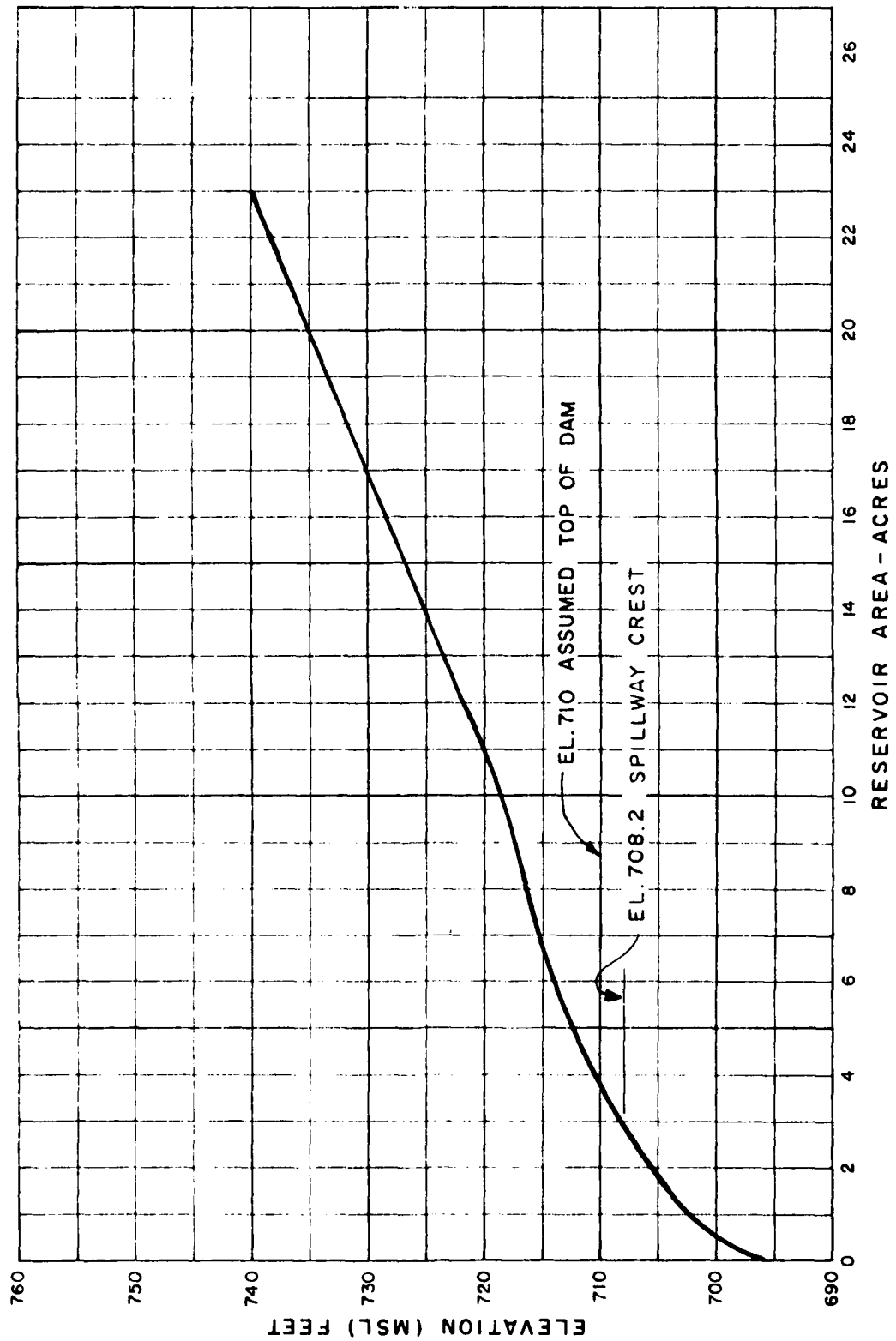
BENSON LAKE DAM (MO. 30667)
SPILLWAY & OVERTOP RATING CURVE
B-8

FORM 4

PRC ENGINEERING CONSULTANTS, INC.

DAM SAFETY INSPECTION - MISSOURI SHEET NO. 1 OF 1
 DAM NAME: BENSON LAKE DAM / ID NO.: 30661 JOB NO. 1263
 RESERVOIR ELEVATION AREA DATA BY FE DATE MAY 80

ELEV. (M.S.L.) (Fe.)	RESERVOIR SURFACE AREA (Acres)	REMARKS
610	0	Assumed bottom of lake
700	0.5	Interpolated.
708	3	- Assumed Spillway Crest
709.5	4	- Roadway acting as emergency spillway
712	5	- High point of dam
720	11	- Measured on USGS QUAD.
730	17	- Interpolated.
740	22	- Measured on USGS QUAD



BENSON LAKE DAM (MO. 30667)
 RESERVOIR ELEVATION - AREA CURVE
 B-10

PRC ENGINEERING CONSULTANTS, INC.

DAM SAFETY INSPECTION / MISSOURI

SHEET NO. 1 OF 1

DAM NAME: PENNSYLVANIA LAKE DAM # 30667

JOB NO. 1263

UNIT HYDROGRAPH PARAMETERS

BY FZ DATE 5/22/80

- 1) DRAINAGE AREA, $A = 0.145$ sq. mi. = (72.5 acres)
- 2) LENGTH OF STREAM, $L = (0.15 " \times 2000' = 1400') = 0.36$ mi.
- 3) ELEVATION AT DRAINAGE DIVIDE ALONG THE LONGEST STREAM,
 $H_1 = 810'$
- 4) ELEVATION OF RESERVOIR AT SPILLWAY CREST, $H_2 = 711.2$
- 5) ELEVATION OF CHANNEL BED AT $0.85L$, $E_{85} = 780$
- 6) ELEVATION OF CHANNEL BED AT $0.10L$, $E_{10} = 715$
- 7) AVERAGE SLOPE OF THE CHANNEL, $S_{AVG} = (E_{85} - E_{10}) / 0.75L = \frac{780 - 715}{0.75 \times 1400} = 0.046$
- 8) TIME OF CONCENTRATION:

A) BY KIRPICH'S EQUATION,

$$t_c = [(11.9 \times L^3) / (H_1 - H_2)]^{0.385} = \left[\frac{11.9 \times 0.36^3}{810 - 711.2} \right]^{0.385} = 0.136 \text{ hr.}$$

B) BY VELOCITY ESTIMATE,

$$\text{SLOPE} = 5\% \Rightarrow \text{AVG. VELOCITY} = 4 \text{ fps.}$$

$$t_c = L/V = \frac{1400'}{4} \times \frac{1}{3600} = 0.132 \text{ hr.}$$

$$\text{USE } t_c = 0.136 \text{ hr.}$$

$$9) \text{ LAG TIME, } t_L = 0.6 t_c = 0.6 \times 0.136 = 0.082$$

$$10) \text{ UNIT DURATION, } D \leq t_L / 3 = \frac{0.082}{3} = 0.027 < 0.083 \text{ hr.}$$

$$\text{USE } D = 0.033 \text{ hr}$$

$$11) \text{ TIME TO PEAK, } T_p = D/2 + t_L = \frac{0.033}{2} + 0.082 = 0.123 \text{ hr}$$

12) PEAK DISCHARGE,

$$q_p = (484 \times A) / T_p = \frac{484 \times 0.145}{0.123} = 570 \text{ cfs}$$

THE ENGINEERING CONSULTANTS, INC.

DAM SAFETY INSPECTION / MISSOURI

SHEET NO. 1 OF 3

DAM NAME: BENSON LAKE DAM # 30667

JOB NO. 1263

PROBABLE MAXIMUM PRECIPITATION

BY FR DATE 1/14/12

DETERMINATION OF PMP

1) Determine drainage area of the basin

D.A. = 92.5 A4

2) Determine PMP Index Rainfall (for D.A. = 200 sq. mi. & 24 hr. duration)

Location of centroid of basin,

Long. = 91° 28' 19"

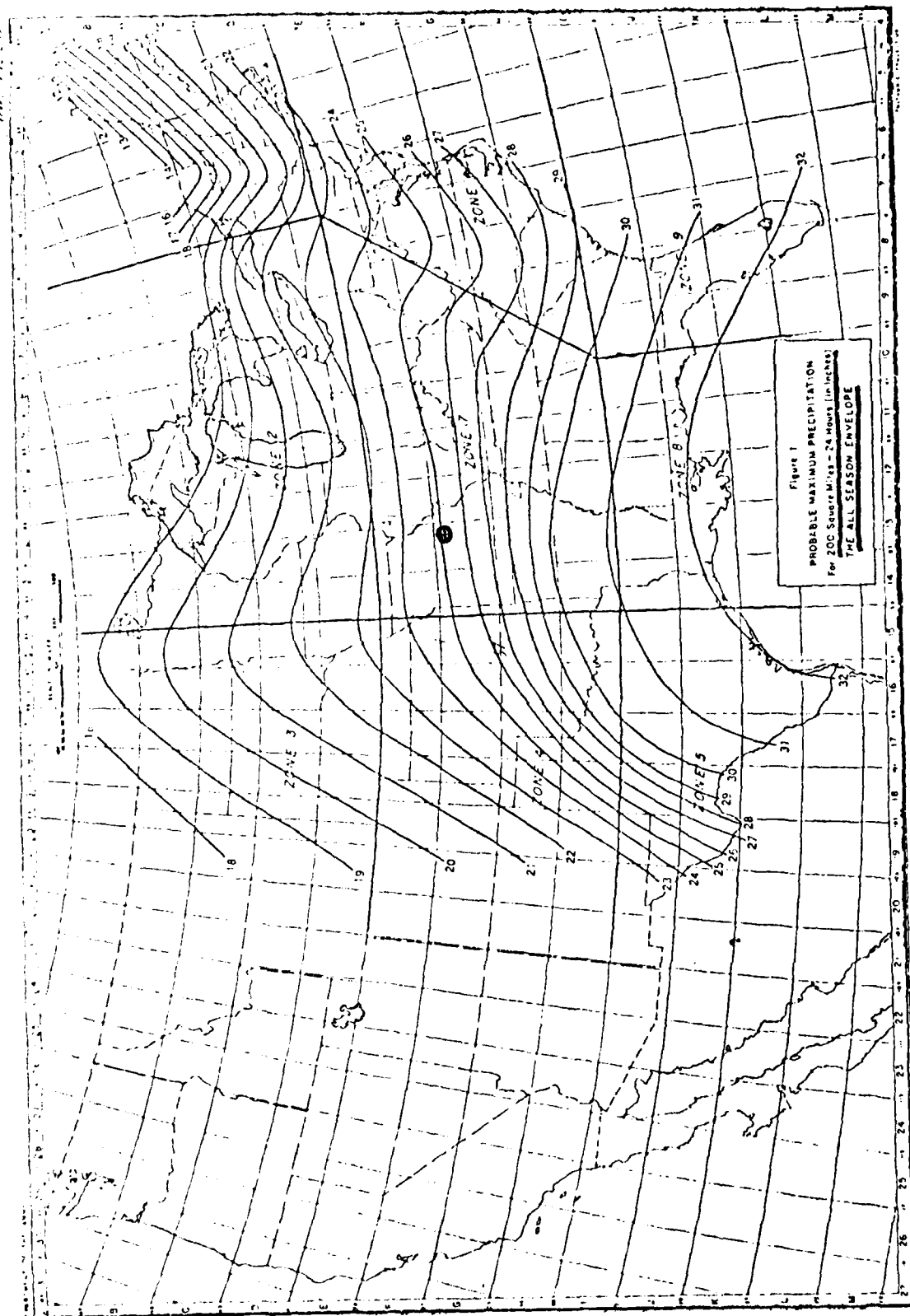
Lat. = 38° 38' 35"

PMP = 25.2 (from Fig. 1, HMR 33)

Zone = 7

3) Determine basin rainfall in terms of percentage of PMP Index
Rainfall for various durations.
(from Fig. 2, HMR 33)

Duration (Hrs.)	Percent of Index Rainfall (%)	Total Rainfall (Inches)	Rainfall Increments (Inches)	Duration of Increment (Hrs.)
6	100	25.2	25.2	6
12	140	30.2	5	6
24	150	32.8	2.6	12



● LOCATION OF CENTROID OF BASIN

BENSON LAKE DAM
DETERMINATION OF PMP

383

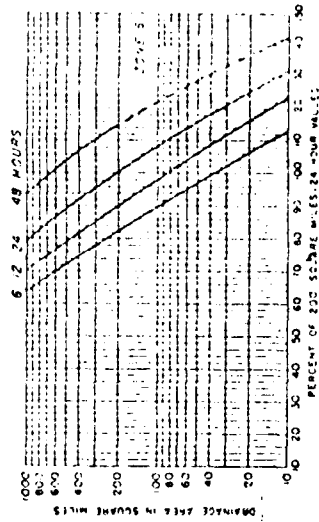
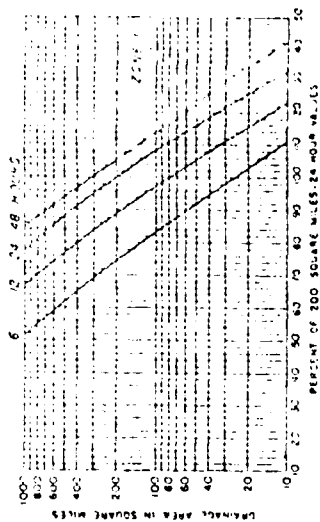
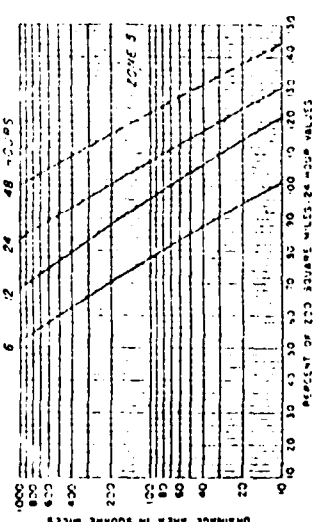
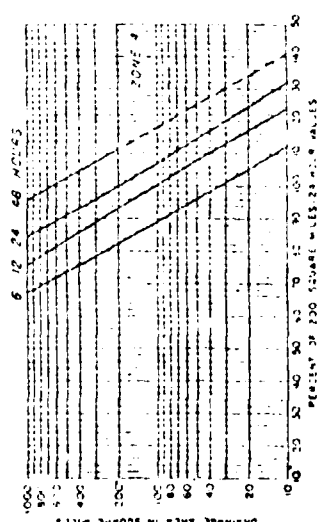
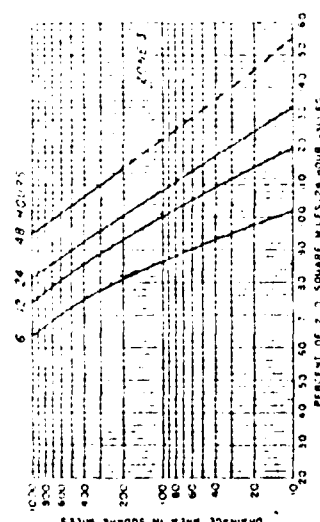
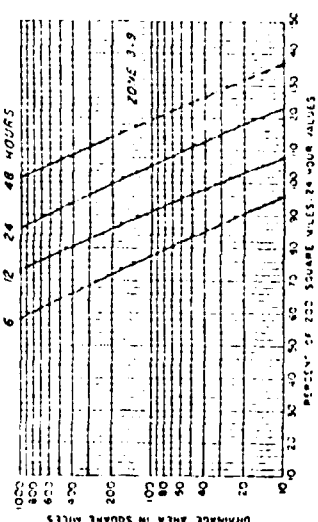
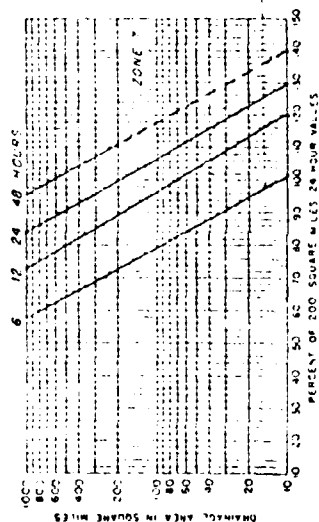
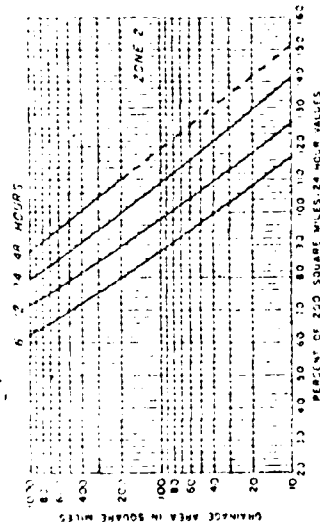


FIGURE 2
SEASONAL VARIATION
DEPTH-AREA-DURATION RELATIONS
Percentage to be applied to 200 square miles
24 hour probable maximum precipitation 10.45
for the all season envelope



PRC ENGINEERING CONSULTANTS, INC.

DAM SAFETY INSPECTION / MISSOURI - 1980 SHEET NO. 1 OF 1

DAM NAME: PEASON LAKE DAM # 30667 JOB NO. 1263

CURVE NUMBER DETERMINATION AT UPSTREAM PEASON LAKE DAM BY DATE

I) SOIL GROUP

WATERSHED SOILS IN THE BASIN CONSIST OF GROUP

A.
B.
C.
D.

GROUP B SOILS SEEM TO PREDOMINATE THE BASIN. THEREFORE,
ASSUME GROUP B SOILS FOR THE ENTIRE WATERSHED
FOR HYDROLOGIC PURPOSES.

II) COVER COMPLEX

ASSUMED
LAND USE

ASSUMED
HYDROLOGIC
CONDITION

PER CENT
AREA

CN
(AMC II)

FOREST

FAIR

70%

60

RANGE

FAIR

30%

69

III) CURVE NUMBER

WEIGHTED AVERAGE CN = 63 FOR AMC II

CURVE NUMBER = 80 FOR AMC III

PRC ENGINEERING CONSULTANTS, INC.

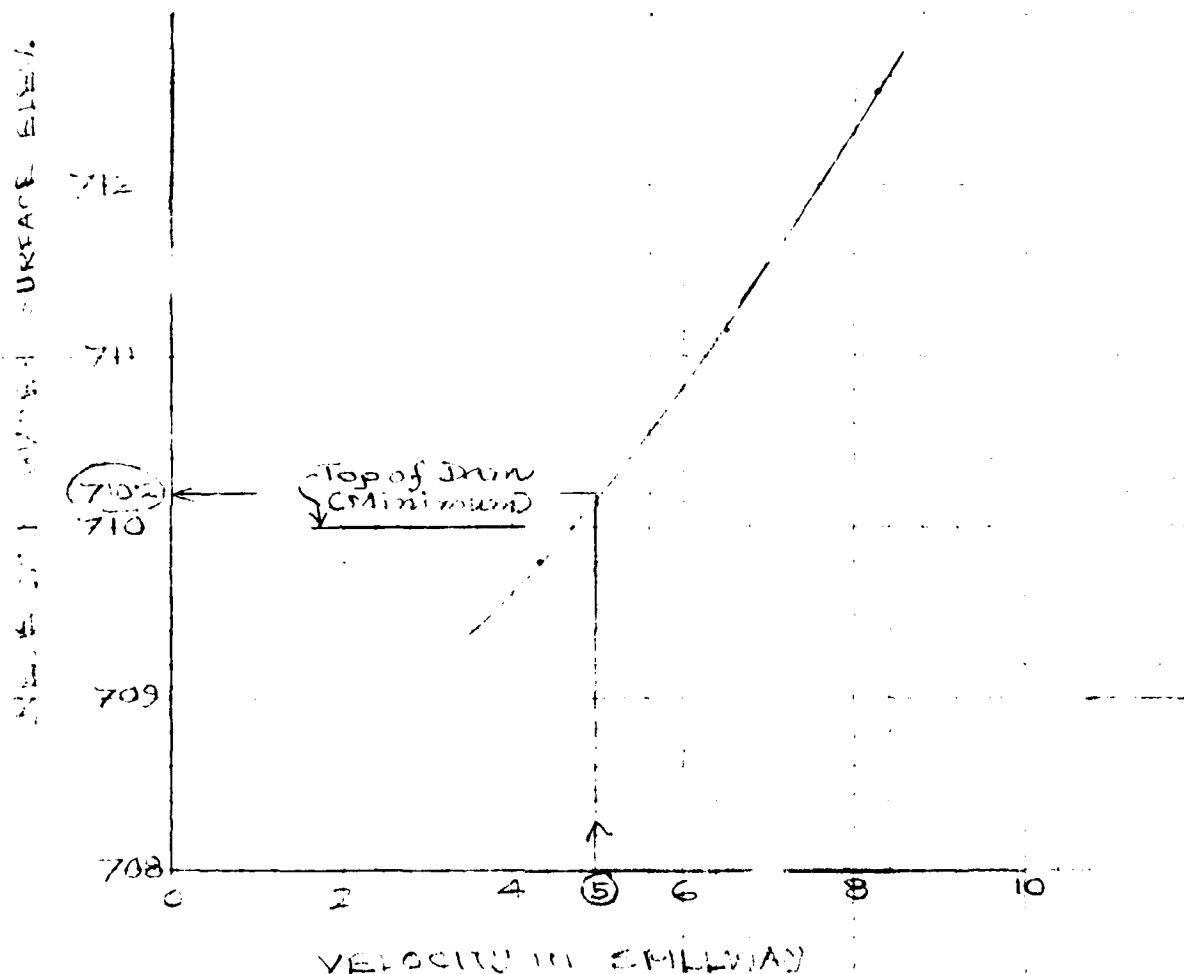
DAM SAFETY INSPECTION / MISSOURI

SHEET NO. 1 OF 1

REVISION NO. 1/11

JOB NO. 1263

DETERMINATION OF EFFECTIVE TOP OF DAM BY MAS DATE 6-9-80



Assuming a 5 ft/sec permissible velocity (Kentucky Blue Gravel-Sandy Silt) the effective top of dam is found to be 710.2 ft above U.S.L., which is higher than minimum top of dam elevation. Use the minimum top of dam elev. for overtopping analysis.

HEC1DB INPUT DATA

.....
 FLOOD HYDROGRAPH PACKAGE (MCH-1)
 DAM SAFETY VERIFICATION JULY 1978
 LAST MODIFICATION: 76 80 1 7

1	41	DAM SAFETY INSPECTION - MISSOURI									
2	42	HENSON LAKE DAM (NO 30657)									
3	43	D/F AND HALF D/F WITH U/S DAM BREAK IN CASE OF DAM OVERTOP									
4	44	300	0	0	0	0	0	0	0	0	0
5	45	1	1	2	1						
6	46	1	1	2	1						
7	47	1	1	2	1						
8	48	1	1	2	1						
9	49	1	1	2	1						
10	50	1	1	2	1						
11	51	1	1	2	1						
12	52	1	1	2	1						
13	53	1	1	2	1						
14	54	1	1	2	1						
15	55	1	1	2	1						
16	56	1	1	2	1						
17	57	1	1	2	1						
18	58	1	1	2	1						
19	59	1	1	2	1						
20	60	1	1	2	1						
21	61	1	1	2	1						
22	62	1	1	2	1						
23	63	1	1	2	1						
24	64	1	1	2	1						
25	65	1	1	2	1						
26	66	1	1	2	1						
27	67	1	1	2	1						
28	68	1	1	2	1						
29	69	1	1	2	1						
30	70	1	1	2	1						
31	71	1	1	2	1						
32	72	1	1	2	1						
33	73	1	1	2	1						
34	74	1	1	2	1						
35	75	1	1	2	1						
36	76	1	1	2	1						
37	77	1	1	2	1						
38	78	1	1	2	1						
39	79	1	1	2	1						
40	80	1	1	2	1						
41	81	1	1	2	1						
42	82	1	1	2	1						
43	83	1	1	2	1						
44	84	1	1	2	1						
45	85	1	1	2	1						
46	86	1	1	2	1						
47	87	1	1	2	1						
48	88	1	1	2	1						
49	89	1	1	2	1						
50	90	1	1	2	1						
51	91	1	1	2	1						
52	92	1	1	2	1						
53	93	1	1	2	1						
54	94	1	1	2	1						
55	95	1	1	2	1						
56	96	1	1	2	1						
57	97	1	1	2	1						
58	98	1	1	2	1						
59	99	1	1	2	1						
60	100	1	1	2	1						

LINE	DESCRIPTION	734	1	742	745	1
1	10/5 - 1/5					
2	CHANNEL ROUTING		1			
3						
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6						
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INFLOW PMF AND ONE-HALF PMF HYDROGRAPHS

• • • • •

• • • • •

.....
 FLOOD HYDROGRAPH FOR THE (HEC-1)
 DAM SAFETY VERIFICATION JULY 1991
 LAST MODIFICATION 26 FEB 92

RUN DATE 07/26/91
 TIME 14:06:31

ON SAFETY INSPECTION - MISSOURI
 FEDERAL DAM (NO. 1000)
 ONE AND HALF PPM WITH D/S DAM IN AREA OF DAM CONTROL

UNIT SPECIFICATION
 TO PPM 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14
 TO 0 0 0 0 0 0 0 0 0 0
 UNIT 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14

MULTI-PHASE UNIT SPECIFICATION
 UPDATE 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14 1.14

RTIME 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00

SUB-AREA RUNOFF COMPUTATION

RUNOFF CALCULATION FOR D/S DAM DRAINAGE AREA

ISTAG 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
 /S DAM 0 0 0 0 0 0 0 0 0 0

HYDROGRAPH DATA
 ITHG 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00 1.00
 TAREA 2 2 2 2 2 2 2 2 2 2
 SHAP 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
 TRSDR 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00
 TRSPE 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

PRECIP DATA
 SPM 25.20 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00 100.00
 R6 112 R24 R48 R72 R96
 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00 0.00

LOSS DATA
 LROPT STRM DLTAR RTIOL FRAL STRO RTIOA STUOL UNTL ALSPX RTIMO
 0 0.00 0.00 1.00 0.00 0.00 0.00 1.00 -1.00 -80.00 0.00 0.00

CURVE NO = 00.00 WITNESS = 1.00 EFFECT CN = 80.00

UNIT HYDROGRAPH DATA
 TC= 0.00 LAG= .09

RECESSION DATA
 SYRTO= 0.00 RECSN= 0.00 RTIOB= 1.00

TIME INCREMENT TOO LARGE--UNB IS GT LAG/2

UNIT HYDROGRAPH / END OF PERIOD ORIGINATES TC= 0.00 HOURS LAG= .09 VOL= 1.00

[illegible]

PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL VOLUME
1	24.0	68.	66.	198.7
2	1.9	2.	2.	5.8
3	33.	29.94	29.94	93.84
4	621.50	760.47	760.47	2142.44
5	111.	136.	136.	383.
6	17.	167.	167.	351.

HYDROGRAPH AT STA/S DAM FOR PLAN 1, RTIO 1

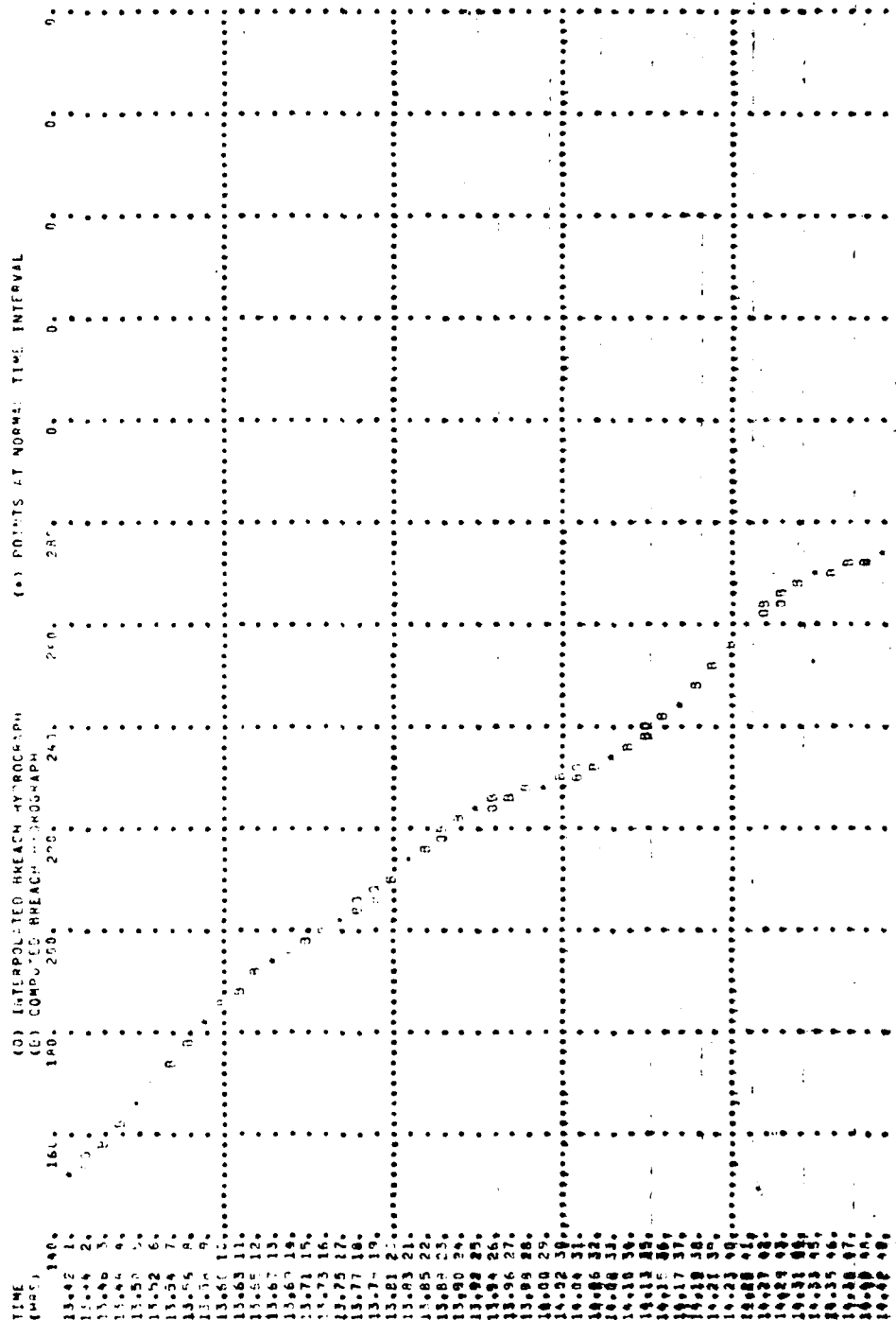
[illegible]

PEAK OUTFLOW IS 1091. AT TIME 15.67 HOURS

	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL	VOLUME
CFS	1091.	251.	78.	67.	1005.	569.
CMS	31.	7.	2.	2.	569.	3056.
INCHES		25.27	76.56	50.56	277.22	776.22
MM		641.86	1766.22	776.22	138.	138.
AC-FT		114.	138.	138.	171.	171.
THOUS CU M		141.	171.	171.	171.	171.

THE LEAK BREACH HYDROGRAPH WAS DEVELOPED USING A TIME INTERVAL OF .0121 HOURS DURING BREACH FORMATION. DOWNSTREAM CALCULATIONS WILL USE A TIME INTERVAL OF .005 HOURS. THIS TABLE PRESENTS THE HYDROGRAPH FOR DOWNSTREAM CALCULATION WITH THE COMPUTED BREACH HYDROGRAPH. INTERPOLATED VALUES ARE INDICATED FROM END-OF-PERIOD VALUES.

TIME (HOURS)	HYDROGRAPH (CFS)	INTERPOLATED (CFS)	CONJUGATE HYDROGRAPH (CFS)	ERROR (CFS)	ACCUMULATED ERROR (CFS)	ACCUMULATED ERROR (AC-FT)
13.432	152	152	152	0	0	0
13.444	154	154	154	0	0	0
13.456	156	156	156	0	0	0
13.468	158	158	158	0	0	0
13.480	160	160	160	0	0	0
13.492	162	162	162	0	0	0
13.504	164	164	164	0	0	0
13.516	166	166	166	0	0	0
13.528	168	168	168	0	0	0
13.540	170	170	170	0	0	0
13.552	172	172	172	0	0	0
13.564	174	174	174	0	0	0
13.576	176	176	176	0	0	0
13.588	178	178	178	0	0	0
13.600	180	180	180	0	0	0
13.612	182	182	182	0	0	0
13.624	184	184	184	0	0	0
13.636	186	186	186	0	0	0
13.648	188	188	188	0	0	0
13.660	190	190	190	0	0	0
13.672	192	192	192	0	0	0
13.684	194	194	194	0	0	0
13.696	196	196	196	0	0	0
13.708	198	198	198	0	0	0
13.720	200	200	200	0	0	0
13.732	202	202	202	0	0	0
13.744	204	204	204	0	0	0
13.756	206	206	206	0	0	0
13.768	208	208	208	0	0	0
13.780	210	210	210	0	0	0
13.792	212	212	212	0	0	0
13.804	214	214	214	0	0	0
13.816	216	216	216	0	0	0
13.828	218	218	218	0	0	0
13.840	220	220	220	0	0	0
13.852	222	222	222	0	0	0
13.864	224	224	224	0	0	0
13.876	226	226	226	0	0	0
13.888	228	228	228	0	0	0
13.900	230	230	230	0	0	0
13.912	232	232	232	0	0	0
13.924	234	234	234	0	0	0
13.936	236	236	236	0	0	0
13.948	238	238	238	0	0	0
13.960	240	240	240	0	0	0
13.972	242	242	242	0	0	0
13.984	244	244	244	0	0	0
13.996	246	246	246	0	0	0
14.008	248	248	248	0	0	0
14.020	250	250	250	0	0	0
14.032	252	252	252	0	0	0
14.044	254	254	254	0	0	0
14.056	256	256	256	0	0	0
14.068	258	258	258	0	0	0
14.080	260	260	260	0	0	0
14.092	262	262	262	0	0	0
14.104	264	264	264	0	0	0
14.116	266	266	266	0	0	0
14.128	268	268	268	0	0	0
14.140	270	270	270	0	0	0
14.152	272	272	272	0	0	0
14.164	274	274	274	0	0	0
14.176	276	276	276	0	0	0
14.188	278	278	278	0	0	0
14.200	280	280	280	0	0	0
14.212	282	282	282	0	0	0
14.224	284	284	284	0	0	0
14.236	286	286	286	0	0	0
14.248	288	288	288	0	0	0
14.260	290	290	290	0	0	0
14.272	292	292	292	0	0	0
14.284	294	294	294	0	0	0
14.296	296	296	296	0	0	0
14.308	298	298	298	0	0	0
14.320	300	300	300	0	0	0
14.332	302	302	302	0	0	0
14.344	304	304	304	0	0	0
14.356	306	306	306	0	0	0
14.368	308	308	308	0	0	0
14.380	310	310	310	0	0	0
14.392	312	312	312	0	0	0
14.404	314	314	314	0	0	0
14.416	316	316	316	0	0	0
14.428	318	318	318	0	0	0
14.440	320	320	320	0	0	0
14.452	322	322	322	0	0	0
14.464	324	324	324	0	0	0
14.476	326	326	326	0	0	0
14.488	328	328	328	0	0	0
14.500	330	330	330	0	0	0
14.512	332	332	332	0	0	0
14.524	334	334	334	0	0	0
14.536	336	336	336	0	0	0
14.548	338	338	338	0	0	0
14.560	340	340	340	0	0	0
14.572	342	342	342	0	0	0
14.584	344	344	344	0	0	0
14.596	346	346	346	0	0	0
14.608	348	348	348	0	0	0
14.620	350	350	350	0	0	0
14.632	352	352	352	0	0	0
14.644	354	354	354	0	0	0
14.656	356	356	356	0	0	0
14.668	358	358	358	0	0	0
14.680	360	360	360	0	0	0
14.692	362	362	362	0	0	0
14.704	364	364	364	0	0	0
14.716	366	366	366	0	0	0
14.728	368	368	368	0	0	0
14.740	370	370	370	0	0	0
14.752	372	372	372	0	0	0
14.764	374	374	374	0	0	0
14.776	376	376	376	0	0	0
14.788	378	378	378	0	0	0
14.800	380	380	380	0	0	0
14.812	382	382	382	0	0	0
14.824	384	384	384	0	0	0
14.836	386	386	386	0	0	0
14.848	388	388	388	0	0	0
14.860	390	390	390	0	0	0
14.872	392	392	392	0	0	0
14.884	394	394	394	0	0	0
14.896	396	396	396	0	0	0
14.908	398	398	398	0	0	0
14.920	400	400	400	0	0	0
14.932	402	402	402	0	0	0
14.944	404	404	404	0	0	0
14.956	406	406	406	0	0	0
14.968	408	408	408	0	0	0
14.980	410	410	410	0	0	0
14.992	412	412	412	0	0	0
15.004	414	414	414	0	0	0
15.016	416	416	416	0	0	0
15.028	418	418	418	0	0	0
15.040	420	420	420	0	0	0
15.052	422	422	422	0	0	0
15.064	424	424	424	0	0	0
15.076	426	426	426	0	0	0
15.088	428	428	428	0	0	0
15.100	430	430	430	0	0	0
15.112	432	432	432	0	0	0
15.124	434	434	434	0	0	0
15.136	436	436	436	0	0	0
15.148	438	438	438	0	0	0
15.160	440	440	440	0	0	0
15.172	442	442	442	0	0	0
15.184	444	444	444	0	0	0
15.196	446	446	446	0	0	0
15.208	448	448	448	0	0	0
15.220	450	450	450	0	0	0
15.232	452	452	452	0	0	0
15.244	454	454	454	0	0	0
15.256	456	456	456	0	0	0
15.268	458	458	458	0	0	0
15.280	460	460	460	0	0	0
15.292	462	462	462	0	0	0
15.304	464	464	464	0	0	0
15.316	466	466	466	0	0	0
15.328	468	468	468	0	0	0
15.340	470	470	470	0	0	0
15.352	472	472	472	0	0	0
15.364	474	474	474	0	0	0
15.376	476	476	476	0	0	0
15.388	478	478	478	0	0	0
15.400	480	480	480	0	0	0
15.412	482	482	482	0	0	0
15.424	484	484	484	0	0	0
15.436	486	486	486	0	0	0
15.448	488	488	488	0	0	0
15.460	490	490	490	0	0	0
15.472	492	492	492	0	0	0
15.484	494	494	494	0	0	0
15.496	496	496	496	0	0	0
15.508	498	498	498	0	0	0
15.520	500	500	500	0	0	0
15.532	502	502	502	0	0	0
15.544	504	504	504	0	0	0
15.556	506	506	506	0	0	0
15.568	508	508	508	0	0	0
15.580	510	510	510	0	0	0
15.592	512	512	512	0	0	0
15.604	514	514	514	0	0	0
15.616	516	516	516	0	0	0
15.628	518	518	518	0	0	0
15.640	520	520	520	0	0	0
15.652	522	522	522	0	0	0
15.664	524	524	524	0	0	0
15.676	526	526	526	0	0	0
15.688	528	528	528	0	0	0
15.700	530	530	530	0	0	0
15.712	532	532	532	0	0	0
15.724	534	534	534	0	0	0
15.736	536	536	536	0	0	0
15.748	538	538	538	0	0	0
15.760	540	540	540	0	0	0
15.772	542	542	542	0	0	0
15.784	544	544	544	0	0	0
15.796	546	546	546	0	0	0
15.808	548	548	548	0	0	0
15.820	550	550	550	0	0	0
15.832	552	552	552	0	0	0
15.844	554	554	554	0	0	0
15.856	556	556	556	0	0	0
15.868	558	558	558	0	0	0
15.880	560	560	560	0	0	0
15.892	562	562	562	0	0	0
15.904	564	564	564	0	0	0
15.916	566	566	566	0	0	0
15.928	568	568	568	0	0	0
15.940						

STATISTICS 7A^u

SECRETARY OF THE ARMY

[illegible][illegible]

AD-A106 167

PRC CONSOER TOWNSEND INC ST LOUIS MO F/G 13/13
NATIONAL DAM SAFETY PROGRAM. BENSON LAKE DAM (MO 30667), MISSOU--ETC(U)
SEP 80 W G SHIFRIN DACW43-80-C-0094

F/6 13/13

DACW43-80-C-0094

NL

UNCLASSIFIED

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END

DATE _____

511 MF

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DTIC

THE FOLLOWING TABLE WAS DEVELOPED USING A TIME INTERVAL OF .021 HOUR, USING BREACH FORMATION, COMPUTED CALCULATIONS AND USE A TIME INTERVAL OF .0013 HOUR. THIS TABLE COMPARES THE HYDROGRAPH FOR DOWNSTREAM CALCULATIONS WITH THE COMPUTED BREACH HYDROGRAPH. INTERPOLATE FLOODS ARE INTERPOLATED FROM END-GENERATED VALUES.

TIME (HOURS)	TIME FROM BEGINNING OF BREACH (HOURS)	INTERPOLATED BREACH HYDROGRAPH (CFS)	COMPUTED BREACH HYDROGRAPH (CFS)	ERROR (CFS)	ACCUMULATED ERROR (CFS)
15.000	0.000	121	121	0	0
15.021	.021	141	230	11	11
15.042	.042	161	366	26	37
15.063	.063	181	481	42	79
15.084	.084	201	581	61	140
15.105	.105	221	666	85	225
15.126	.126	241	737	96	321
15.147	.147	261	797	116	437
15.168	.168	281	847	136	573
15.189	.189	301	887	156	729
15.210	.210	321	917	176	905
15.231	.231	341	947	196	1101
15.252	.252	361	967	216	1317
15.273	.273	381	977	236	1553
15.294	.294	401	977	256	1809
15.315	.315	421	967	276	2085
15.336	.336	441	947	296	2381
15.357	.357	461	917	316	2697
15.378	.378	481	877	336	3033
15.399	.399	501	827	356	3389
15.420	.420	521	767	376	3765
15.441	.441	541	697	396	4161
15.462	.462	561	617	416	4577
15.483	.483	581	527	436	5013
15.504	.504	601	427	456	5469
15.525	.525	621	317	476	5945
15.546	.546	641	197	496	6441
15.567	.567	661	67	516	6957
15.588	.588	681	0	536	7493
15.609	.609	701	0	556	8049
15.630	.630	721	0	576	8625
15.651	.651	741	0	596	9221
15.672	.672	761	0	616	9837
15.693	.693	781	0	636	10473
15.714	.714	801	0	656	11129
15.735	.735	821	0	676	11805
15.756	.756	841	0	696	12501
15.777	.777	861	0	716	13217
15.798	.798	881	0	736	13953
15.819	.819	901	0	756	14709
15.840	.840	921	0	776	15485
15.861	.861	941	0	796	16281
15.882	.882	961	0	816	17097
15.903	.903	981	0	836	17933
15.924	.924	1001	0	856	18789
15.945	.945	1021	0	876	19665
15.966	.966	1041	0	896	20561
15.987	.987	1061	0	916	21477
16.008	1.008	1081	0	936	22413
16.029	1.029	1101	0	956	23369
16.050	1.050	1121	0	976	24345
16.071	1.071	1141	0	996	25341
16.092	1.092	1161	0	1016	26357
16.113	1.113	1181	0	1036	27393
16.134	1.134	1201	0	1056	28449
16.155	1.155	1221	0	1076	29525
16.176	1.176	1241	0	1096	30621
16.197	1.197	1261	0	1116	31737
16.218	1.218	1281	0	1136	32873
16.239	1.239	1301	0	1156	34029
16.260	1.260	1321	0	1176	35205
16.281	1.281	1341	0	1196	36401
16.302	1.302	1361	0	1216	37617
16.323	1.323	1381	0	1236	38853
16.344	1.344	1401	0	1256	40109
16.365	1.365	1421	0	1276	41385
16.386	1.386	1441	0	1296	42681
16.407	1.407	1461	0	1316	43997
16.428	1.428	1481	0	1336	45333
16.449	1.449	1501	0	1356	46689
16.470	1.470	1521	0	1376	48065
16.491	1.491	1541	0	1396	49461
16.512	1.512	1561	0	1416	50877
16.533	1.533	1581	0	1436	52313
16.554	1.554	1601	0	1456	53769
16.575	1.575	1621	0	1476	55245
16.596	1.596	1641	0	1496	56741
16.617	1.617	1661	0	1516	58257
16.638	1.638	1681	0	1536	59793
16.659	1.659	1701	0	1556	61349
16.680	1.680	1721	0	1576	62925
16.701	1.701	1741	0	1596	64521
16.722	1.722	1761	0	1616	66137
16.743	1.743	1781	0	1636	67773
16.764	1.764	1801	0	1656	69429
16.785	1.785	1821	0	1676	71105
16.806	1.806	1841	0	1696	72801
16.827	1.827	1861	0	1716	74517
16.848	1.848	1881	0	1736	76253
16.869	1.869	1901	0	1756	78009
16.890	1.890	1921	0	1776	79785
16.911	1.911	1941	0	1796	81581
16.932	1.932	1961	0	1816	83397
16.953	1.953	1981	0	1836	85233
16.974	1.974	2001	0	1856	87089
16.995	1.995	2021	0	1876	88965
17.016	2.016	2041	0	1896	90861
17.037	2.037	2061	0	1916	92777
17.058	2.058	2081	0	1936	94713
17.079	2.079	2101	0	1956	96669
17.100	2.100	2121	0	1976	98645
17.121	2.121	2141	0	1996	100641
17.142	2.142	2161	0	2016	102657
17.163	2.163	2181	0	2036	104693
17.184	2.184	2201	0	2056	106749
17.205	2.205	2221	0	2076	108825
17.226	2.226	2241	0	2096	110921
17.247	2.247	2261	0	2116	113037
17.268	2.268	2281	0	2136	115173
17.289	2.289	2301	0	2156	117329
17.310	2.310	2321	0	2176	119505
17.331	2.331	2341	0	2196	121701
17.352	2.352	2361	0	2216	123917
17.373	2.373	2381	0	2236	126153
17.394	2.394	2401	0	2256	128409
17.415	2.415	2421	0	2276	130685
17.436	2.436	2441	0	2296	132981
17.457	2.457	2461	0	2316	135297
17.478	2.478	2481	0	2336	137633
17.499	2.499	2501	0	2356	140000
17.520	2.520	2521	0	2376	142397
17.541	2.541	2541	0	2396	144825
17.562	2.562	2561	0	2416	147283
17.583	2.583	2581	0	2436	149761
17.604	2.604	2601	0	2456	152269
17.625	2.625	2621	0	2476	154807
17.646	2.646	2641	0	2496	157375
17.667	2.667	2661	0	2516	160000
17.688	2.688	2681	0	2536	162681
17.709	2.709	2701	0	2556	165429
17.730	2.730	2721	0	2576	168245
17.751	2.751	2741	0	2596	171129
17.772	2.772	2761	0	2616	174081
17.793	2.793	2781	0	2636	177101
17.814	2.814	2801	0	2656	180189
17.835	2.835	2821	0	2676	183345
17.856	2.856	2841	0	2696	186569
17.877	2.877	2861	0	2716	189861
17.898	2.898	2881	0	2736	193233
17.919	2.919	2901	0	2756	196685
17.940	2.940	2921	0	2776	200217
17.961	2.961	2941	0	2796	203829
17.982	2.982	2961	0	2816	207521
18.003	3.003	2981	0	2836	211293
18.024	3.024	3001	0	2856	215145
18.045	3.045	3021	0	2876	219077
18.066	3.066	3041	0	2896	223089
18.087	3.087	3061	0	2916	227181
18.108	3.108	3081	0	2936	231353
18.129	3.129	3101	0	2956	235605
18.150	3.150	3121	0	2976	240000
18.171	3.171	3141	0	2996	244500
18.192	3.192	3161	0	3016	249100
18.213	3.213	3181	0	3036	253800
18.234	3.234	3201	0	3056	258600
18.255	3.255	3221	0	3076	263500
18.276	3.276	3241	0	3096	268500
18.297	3.297	3261	0	3116	273600
18.318	3.318	3281	0	3136	278800
18.339	3.339	3301	0	3156	284100
18.360	3.360	3321	0	3176	289500
18.381	3.381	3341	0	3196	295000
18.402	3.402	3361	0	3216	300600
18.423	3.423	3381	0	3236	306300
18.444	3.444	3401	0	3256	312100
18.465	3.465	3421	0	3276	318000
18.486	3.486	3441	0	3296	324000
18.507	3.507	3461	0	3316	330100
18.528	3.528	3481	0	3336	336300
18.549	3.549	3501	0	3356	342600
18.570	3.570	3521	0	3376	349000
18.591	3.591	3541	0	3396	355500
18.612	3.612	3561	0	3416	362100
18.633	3.633	3581	0	3436	368800
18.654	3.654	3601	0	3456	375600
18.675	3.675	3621	0	3476	382500
18.696	3.696	3641	0	3496	389500
18.717	3.717	3661	0	3516	396600
18.738	3.738	3681	0	3536	403800
18.759	3.759	3701	0	3556	411100
18.780	3.780	3721	0	3576	418500
18.801	3.801	3741	0	3596	426000
18.822	3.822	3761	0	3616	433600
18.843	3.843	3781	0	3636	441300
18.864	3.864	3801	0	3656	449100
18.885	3.885	3821	0	3676	457000
18.906	3.906	3841	0	3696	465000
18.927	3.927	3861	0	3716	473100
18.948	3.948	3881	0	3736	481300
18.969	3.969	3901	0	3756	489600
18.990	3.990	3921	0	3776	498000
19.011	4.011	3941	0	3796	506500
19.032	4.032	3961	0	3816	515100
19.053	4.053	3981	0	3836	523800
19.074	4.074	4001	0	3856	532600
19.095	4.095	4021	0	3876	541500
19.116	4.116	4041	0	3896	550500
19.137	4.137	4061	0	3916	559600
19.158	4.158	4081	0	3936	568800
19.179	4.179	4101	0	3956	578100
19.200	4.200	4121	0	3976	587500
19.221	4.221	4141	0	3996	597000
19.242	4.242	4161	0	4016	606600
19.263	4.263	4181	0	4036	616300

STATION/ : 1344

(10) POINTS AT NORMAL TIME INTERVAL

(10) INTERPOLATED BEACH HYDROGRAPH

3614

[illegible]

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HYDROGRAPH ROUTING

CHANNEL ROUTING

IST40 ICOMP TEGG TTRG OPLT UPRT INAME I'PAGE I'AUOT
S -D/S 1 0 0 0 0 0
CLOS CLOSIS LAG TEGG ISAME IDPT ICOMP LSTR
0.0 0.010 0.00 1 1 0 0
NSTPS NSTEL LAG LAGS LAG TEGG I'PAGE I'AUOT
1 0 0 0.001 0.000 0.000 0.000

NORMAL DEPTH CHANNEL ROUTING

2N(1) GV(2) GV(3) FLWY FLWY FLWY SFL
0.000 0.000 0.000 720. 740.0 1.000 0.0000

CROSS SECTION COORDINATES--STA.ELEV--STA.ELEV--ETC
0.00 740.00 40.00 750.00 90.00 723.00
118.00 723.00 140.00 730.00 250.00 740.00

STORAGE	0.00	15.60	19.28	23.22	27.44	31.95	36.73	41.79	47.13	52.75	58.65	64.85	71.35	78.15	85.25	92.65	100.35	108.35	116.65	125.25
OUTFLOW	0.00	63.46	180.55	385.70	749.57	1324.89	2181.01	3376.07	4862.69	6659.72	8766.19	11182.01	13907.21	16941.81	20285.81	23939.21	27901.81	32173.61	36754.61	41645.01
STAGE	720.00	721.85	722.11	723.16	723.68	724.74	725.26	726.32	727.37	728.42	729.47	730.52	731.57	732.62	733.67	734.72	735.77	736.82	737.87	738.92
FLOW	0.00	53.46	180.55	385.70	749.57	1324.89	2181.01	3376.07	4862.69	6659.72	8766.19	11182.01	13907.21	16941.81	20285.81	23939.21	27901.81	32173.61	36754.61	41645.01

STATION S -D/S PLAN 1.0 PTD 1

OUTFLOW	0.00	63.46	180.55	385.70	749.57	1324.89	2181.01	3376.07	4862.69	6659.72	8766.19	11182.01	13907.21	16941.81	20285.81	23939.21	27901.81	32173.61	36754.61	41645.01
STAGE	720.00	721.85	722.11	723.16	723.68	724.74	725.26	726.32	727.37	728.42	729.47	730.52	731.57	732.62	733.67	734.72	735.77	736.82	737.87	738.92
FLOW	0.00	53.46	180.55	385.70	749.57	1324.89	2181.01	3376.07	4862.69	6659.72	8766.19	11182.01	13907.21	16941.81	20285.81	23939.21	27901.81	32173.61	36754.61	41645.01

[illegible][illegible]

	PEAK	6-HOUR	12-HOUR	TOTAL
CFS	539.	110.	36.	1028.
CBS	15.	1.	1.	290.
1-CBS		12.95	15.6	15.85
2-CBS		23.40	45.11	395.11
ACET		50.	70.	70.
THOUS. CU M		72.	97.	97.

MAXIMUM STORAGE = 1.

MAXIMUM STAGE IS 723.6

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SUB-AREA RUNOFF COMPUTATION

RUNOFF CALCULATION FOR ZENSON LAKE DAM RUNOFF AREA

ISTAG	ICOMP	IECON	ITAPE	JPLT	JPRY	ISNAME	ISTAGE	IAUTO
30667	0	0	0	0	0	1	0	0

HYDROGRAPH DATA			
ISNG	TAREA	SNAP	RATIO
2	0.15	8.00	0.000
3	0.15	8.00	0.000

ISNG	ISNG	ISNAME	LOCAL
2	0	0	0
3	0	0	0

PRECIP DAYA

DATE	TIME	NO.	NAME	AGE	SEX	PRICE
2042	25.20	100.00	K12	130.00	0.00	0.00
2043	25.20	100.00	K12	130.00	0.00	0.00
2044	25.20	100.00	K12	130.00	0.00	0.00
2045	25.20	100.00	K12	130.00	0.00	0.00
2046	25.20	100.00	K12	130.00	0.00	0.00
2047	25.20	100.00	K12	130.00	0.00	0.00
2048	25.20	100.00	K12	130.00	0.00	0.00
2049	25.20	100.00	K12	130.00	0.00	0.00
2050	25.20	100.00	K12	130.00	0.00	0.00
2051	25.20	100.00	K12	130.00	0.00	0.00
2052	25.20	100.00	K12	130.00	0.00	0.00
2053	25.20	100.00	K12	130.00	0.00	0.00
2054	25.20	100.00	K12	130.00	0.00	0.00
2055	25.20	100.00	K12	130.00	0.00	0.00
2056	25.20	100.00	K12	130.00	0.00	0.00
2057	25.20	100.00	K12	130.00	0.00	0.00
2058	25.20	100.00	K12	130.00	0.00	0.00
2059	25.20	100.00	K12	130.00	0.00	0.00
2060	25.20	100.00	K12	130.00	0.00	0.00
2061	25.20	100.00	K12	130.00	0.00	0.00
2062	25.20	100.00	K12	130.00	0.00	0.00
2063	25.20	100.00	K12	130.00	0.00	0.00
2064	25.20	100.00	K12	130.00	0.00	0.00
2065	25.20	100.00	K12	130.00	0.00	0.00
2066	25.20	100.00	K12	130.00	0.00	0.00
2067	25.20	100.00	K12	130.00	0.00	0.00
2068	25.20	100.00	K12	130.00	0.00	0.00
2069	25.20	100.00	K12	130.00	0.00	0.00
2070	25.20	100.00	K12	130.00	0.00	0.00
2071	25.20	100.00	K12	130.00	0.00	0.00
2072	25.20	100.00	K12	130.00	0.00	0.00
2073	25.20	100.00	K12	130.00	0.00	0.00
2074	25.20	100.00	K12	130.00	0.00	0.00
2075	25.20	100.00	K12	130.00	0.00	0.00
2076	25.20	100.00	K12	130.00	0.00	0.00
2077	25.20	100.00	K12	130.00	0.00	0.00
2078	25.20	100.00	K12	130.00	0.00	0.00
2079	25.20	100.00	K12	130.00	0.00	0.00
2080	25.20	100.00	K12	130.00	0.00	0.00
2081	25.20	100.00	K12	130.00	0.00	0.00
2082	25.20	100.00	K12	130.00	0.00	0.00
2083	25.20	100.00	K12	130.00	0.00	0.00
2084	25.20	100.00	K12	130.00	0.00	0.00
2085	25.20	100.00	K12	130.00	0.00	0.00
2086	25.20	100.00	K12	130.00	0.00	0.00
2087	25.20	100.00	K12	130.00	0.00	0.00
2088	25.20	100.00	K12	130.00	0.00	0.00
2089	25.20	100.00	K12	130.00	0.00	0.00
2090	25.20	100.00	K12	130.00	0.00	0.00
2091	25.20	100.00	K12	130.00	0.00	0.00
2092	25.20	100.00	K12	130.00	0.00	0.00

LOSS DATA

LAOPTY	SIRKS	OLVER	WITOL	ERAIN	SIRKS	RTIOX	STRIL	CNSTL	ALONE	RTIMP
0	0.00	0.00	1.00	0.00	0.00	1.00	-1.00	-0.00	-1.00	0.00

CURVE NO = 00.00 WEYNESS = -1.00 EFFECT CH = 00.00

UNIT HYDROGRAPH DATA

DATE: NOV 20 1964
YCS 0.00 LAGE 0.00

STRIKE 3.37 RECUSSION DATA RTIME 1.00
GREYNE 1.00

TIME INC (UNT) TO LARGE--(CNG IS ST 146/7)

RAIT HYPER KAP 7 END OF PERIOD OPTICALS ICE 5. 9.00 HOURS LA 2. 0.0R VOLE 1.00
102. 52.

HR.DA	HR.DV	PERIOD	RAIN	EXCS	LOSS	ENG-OF-PERIOD	HR.DA	HR.DV	PERIOD	RAIN	EXCS	LOSS	COMP Q
1.01	0.05	1	.31	0.00	.01	0.	1.01	12.35	151	.21	.20	.01	218.
1.01	0.10	2	.01	0.00	.01	0.	1.01	12.40	152	.21	.20	.01	219.
1.01	0.15	3	.01	0.00	.01	0.	1.01	12.45	153	.21	.20	.01	220.
1.01	0.20	4	.01	0.00	.01	0.	1.01	12.50	154	.21	.20	.01	221.
1.01	0.25	5	.01	0.00	.01	0.	1.01	12.55	155	.21	.20	.01	222.
1.01	0.30	6	.01	0.00	.01	0.	1.01	13.00	156	.21	.20	.01	223.
1.01	0.35	7	.01	0.00	.01	0.	1.01	13.05	157	.21	.20	.01	224.
1.01	0.40	8	.01	0.00	.01	0.	1.01	13.10	158	.21	.20	.01	225.
1.01	0.45	9	.01	0.00	.01	0.	1.01	13.15	159	.21	.20	.01	226.
1.01	0.50	10	.01	0.00	.01	0.	1.01	13.20	160	.21	.20	.01	227.
1.01	0.55	11	.01	0.00	.01	0.	1.01	13.25	161	.21	.20	.01	228.
1.01	1.00	12	.01	0.00	.01	0.	1.01	13.30	162	.21	.20	.01	229.
1.01	1.05	13	.01	0.00	.01	0.	1.01	13.35	163	.21	.20	.01	230.
1.01	1.10	14	.01	0.00	.01	0.	1.01	13.40	164	.21	.20	.01	231.
1.01	1.15	15	.01	0.00	.01	0.	1.01	13.45	165	.21	.20	.01	232.
1.01	1.20	16	.01	0.00	.01	0.	1.01	13.50	166	.21	.20	.01	233.
1.01	1.25	17	.01	0.00	.01	0.	1.01	13.55	167	.21	.20	.01	234.
1.01	1.30	18	.01	0.00	.01	0.	1.01	14.00	168	.21	.20	.01	235.
1.01	1.35	19	.01	0.00	.01	0.	1.01	14.05	169	.21	.20	.01	236.
1.01	1.40	20	.01	0.00	.01	0.	1.01	14.10	170	.21	.20	.01	237.
1.01	1.45	21	.01	0.00	.01	0.	1.01	14.15	171	.21	.20	.01	238.
1.01	1.50	22	.01	0.00	.01	0.	1.01	14.20	172	.21	.20	.01	239.
1.01	1.55	23	.01	0.00	.01	0.	1.01	14.25	173	.21	.20	.01	240.
1.01	2.00	24	.01	0.00	.01	0.	1.01	14.30	174	.21	.20	.01	241.
1.01	2.05	25	.01	0.00	.01	0.	1.01	14.35	175	.21	.20	.01	242.
1.01	2.10	26	.01	0.00	.01	0.	1.01	14.40	176	.21	.20	.01	243.
1.01	2.15	27	.01	0.00	.01	0.	1.01	14.45	177	.21	.20	.01	244.
1.01	2.20	28	.01	0.00	.01	0.	1.01	14.50	178	.21	.20	.01	245.
1.01	2.25	29	.01	0.00	.01	0.	1.01	14.55	179	.21	.20	.01	246.
1.01	2.30	30	.01	0.00	.01	0.	1.01	15.00	180	.21	.20	.01	247.
1.01	2.35	31	.01	0.00	.01	0.	1.01	15.05	181	.21	.20	.01	248.
1.01	2.40	32	.01	0.00	.01	0.	1.01	15.10	182	.21	.20	.01	249.
1.01	2.45	33	.01	0.00	.01	0.	1.01	15.15	183	.21	.20	.01	250.
1.01	2.50	34	.01	0.00	.01	0.	1.01	15.20	184	.21	.20	.01	251.
1.01	2.55	35	.01	0.00	.01	0.	1.01	15.25	185	.21	.20	.01	252.
1.01	3.00	36	.01	0.00	.01	0.	1.01	15.30	186	.21	.20	.01	253.
1.01	3.05	37	.01	0.00	.01	0.	1.01	15.35	187	.21	.20	.01	254.
1.01	3.10	38	.01	0.00	.01	0.	1.01	15.40	188	.21	.20	.01	255.
1.01	3.15	39	.01	0.00	.01	0.	1.01	15.45	189	.21	.20	.01	256.
1.01	3.20	40	.01	0.00	.01	0.	1.01	15.50	190	.21	.20	.01	257.
1.01	3.25	41	.01	0.00	.01	0.	1.01	15.55	191	.21	.20	.01	258.
1.01	3.30	42	.01	0.00	.01	0.	1.01	16.00	192	.21	.20	.01	259.
1.01	3.35	43	.01	0.00	.01	0.	1.01	16.05	193	.21	.20	.01	260.
1.01	3.40	44	.01	0.00	.01	0.	1.01	16.10	194	.21	.20	.01	261.
1.01	3.45	45	.01	0.00	.01	0.	1.01	16.15	195	.21	.20	.01	262.
1.01	3.50	46	.01	0.00	.01	0.	1.01	16.20	196	.21	.20	.01	263.
1.01	3.55	47	.01	0.00	.01	0.	1.01	16.25	197	.21	.20	.01	264.
1.01	4.00	48	.01	0.00	.01	0.	1.01	16.30	198	.21	.20	.01	265.
1.01	4.05	49	.01	0.00	.01	0.	1.01	16.35	199	.21	.20	.01	266.

1.01	4.10	5.9	7.1	7.9	7.1	2.	1.01	16.43	230	.29	.29	.00	327.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	16.45	231	.29	.29	.00	328.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	16.50	232	.29	.29	.00	329.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	16.55	233	.29	.29	.00	330.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.00	234	.29	.29	.00	331.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.05	235	.29	.29	.00	332.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.10	236	.29	.29	.00	333.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.15	237	.29	.29	.00	334.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.20	238	.29	.29	.00	335.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.25	239	.29	.29	.00	336.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.30	240	.29	.29	.00	337.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.35	241	.29	.29	.00	338.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.40	242	.29	.29	.00	339.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.45	243	.29	.29	.00	340.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.50	244	.29	.29	.00	341.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	17.55	245	.29	.29	.00	342.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.00	246	.29	.29	.00	343.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.05	247	.29	.29	.00	344.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.10	248	.29	.29	.00	345.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.15	249	.29	.29	.00	346.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.20	250	.29	.29	.00	347.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.25	251	.29	.29	.00	348.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.30	252	.29	.29	.00	349.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.35	253	.29	.29	.00	350.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.40	254	.29	.29	.00	351.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.45	255	.29	.29	.00	352.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.50	256	.29	.29	.00	353.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	18.55	257	.29	.29	.00	354.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.00	258	.29	.29	.00	355.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.05	259	.29	.29	.00	356.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.10	260	.29	.29	.00	357.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.15	261	.29	.29	.00	358.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.20	262	.29	.29	.00	359.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.25	263	.29	.29	.00	360.
1.01	4.00	5.1	7.0	7.0	7.0	2.	1.01	19.30	264	.29	.29	.00	361.</

	PRK	1-720R	3-190H	72-60R	1017	VOLUME
CPS	1716	1	58	56	1801	
CH	1716	1	58	56	1801	
1-CH	1716	1	58	56	1801	
AC-F	1716	10.94	14.5	16.97	476	
100S CH	1716	11.2	14.5	16.97	1497	
				SMO.74	360.24	
				116	116	
				143	143	

PMF AND ONE-HALF PMF ROUTING

RECEIVED TELETYPE UNIT - AUG 1961

ISTG	ICD9	PCON	TYPE	JFLY	JPRI	INAME	ISTAGE	IAUTO
1	1	Q	2	Q	Q	1	Q	2
3467								

CLASS	CLOS	AVG	RES	TSAME
0.0	0.050	0.00	1	1

STISN I C TULSA, LA6 :MSKK 0009

[illegible]

SUPPLEMENTAL

Case: 1:17-cv-00003

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TOP: L	DATA	NAMEID
Y1: 0	COG	EXP
	3.0	0.0
		J.

TATION 30667, FLAN 10, RAYC 1

FNC-OF-PERIOD HYDROGRAPH ORDINATES

MC71INC

[illegible]

PEAK JUTFC# 15 0.57. AT TIME 12.67 HOURS

STATION 30067, PLAN 1, RAY 22

END-OF-PERIOD HYPER-GRAPH ORDINATES

STORAGE

DEAD CUTOFF IS 1346. AT TIME 14.75 HOURS

	PEAK	6-HOUR	24-HOUR	72-HOUR	TOTAL	VOLUME
CFS	1340	305	34	97	2787	2787
CVS	34	7	3	3	165	165
PCFS		12	15	15	151	151
ACFS		13	185	185	385	385
THOUS CUM		151	230	186	186	186
		1	230	270	270	270

PEAK FLOW AND STORAGE (CUMULATIVE) SUMMARY FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUMULATIVE FEET PER SECOND, CUBIC METERS PER SECOND
 AREA IN SQUARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	AREA	RATIOS APPLIED TO FLOWS	
			PLAN RATIO 1	RATIO 2
			1.00	1.00
HYDROGRAPH AT 1/5 DAM			1	1159
		.20	(	32.60)(
ROUTED TO 1/5 DAM		.09	1	1091
		.20	(	3.90)(
ROUTED TO S-2/5		.05	1	1208
		.20	(	29.44)(
HYDROGRAPH AT 1/5		.15	1	1026
		.30	(	57.37)(
2 COMBINED		.07	1	2945
		.00	(	43.20)(
ROUTED TO		.23	1	2687
		.60	(	81.70)(

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SUMMARY OF PMF AND ONE-HALF PMF FLOOD ROUTING

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SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1	ELEVATION: STORAGE OUTFLOW	INITIAL VALUE 742.00 0.0 0.0	SPILLWAY CREST 742.00 0.0 0.0	TOP OF DAM 745.00 0.0 148.0	MAXIMUM DEPTH OVER DAM 0.0 0.0 0.0	MAXIMUM STORAGE 10.0 10.0 10.0	MAXIMUM OUTFLOW CFS 100.0 100.0 100.0	DURATION OVER THE HOURS 0.5 0.5 0.5	TIME OF MAX OUTFLOW HOURS 15.67 15.67 15.67	TIME OF FATIGUE HOURS 15.62 15.62 15.62
1.00	745.54	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.00	745.54	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0
1.00	745.54	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0	0.0

PLAN 1 STATION 5 +0/S

RATIO	MAXIMUM FLOW/CF	MAXIMUM STAGE/FT	TIME HOURS
1.00	100.0	7.07	15.67
0.50	50.0	7.23	15.67

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SUMMARY OF DAM SAFETY ANALYSIS

.....	ELEVATION	INITIAL VALUE	FILLWAY CREST	TOP OF DAM	TIME OF FAILURE
	STORAGE	704.20	104.20	71.20	
	OUTFLOW	14.	14.	20.	
		0.	0.	330.	
.....	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM	MAXIMUM
RATIO OF RESERVOIR WATER	STORAGE	DEPTH	OUTFLOW	OVER TOP	OUTFLOW
1.00	712.33	2.33	2487.	5.25	15.67
0.50	711.37	1.37	1390.	1.17	15.75
					0.00
					0.00

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C

PERCENT OF PMF FLOOD ROUTING
EQUAL TO SPILLWAY CAPACITY

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[illegible]

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Y9	10	.5	738	1	742	745	1
Y10	10/S -2/S						
Y11	CHANNEL ROUTING			1			
Y12	1						
Y13	.05	.05		720	740	1000	.025
Y14		740		730	90	723	95
Y15	110	723	190	730	250	740	
Y16	0	30667					1
Y17	1	2	.145		.145	1	
Y18	1	25.0	170	120	130		
Y19	1	.182					-1
Y20	0	0	1				
Y21	2	30667					1
Y22	1	30667					1
Y23	1	ROUTE HYDROGRAPH THROUGH BENSON LAKE DAM		1			
Y24	1	700.2	710.5	711.17	712	712.57	-700.2
Y25	0	233	500	1100	2200	3370	714.16
Y26	0	0	3	4	5	11	7932
Y27	0	0	700.2	700.5	712	720	17
Y28	0	0					733
Y29	0	0					
Y30	0	0					
Y31	0	0					
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Y99	0	0					
Y100	0	0					

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REVIEW OF USE OF NETWORK CALCULATIONS

ROUTE HYDROGRAPH BY FS DAN
ROUTE HYDROGRAPH TO FS DAN
ROUTE HYDROGRAPH TO S-17
ROUTE HYDROGRAPH AT 30667
ROUTE HYDROGRAPH AT 30667
ROUTE HYDROGRAPH TO 30667
END OF NETWORK

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CAPACITIVE	0.	1.	14.	18.	30.	92.	231.	425.
ELEVATIONS	695.	700.	708.	710.	717.	720.	730.	740.
	CHL	SPWD	CDW	EAU	ELEV	COI	CAREA	EAPL
	70.42	0.0	0.0	0.0	0.0	0.0	0.0	0.0

DATA
TUFEL 710.0
COWD 0.0
FIXED 0.0
HAMID 0.

PEAK OUTFLOW IS 241. AT TIME 15.03 HOURS

PEAK OUTFLOW IS 303. AT TIME 15.03 HOURS

PEAK OUTFLOW IS 340. AT TIME 15.75 HOURS

PEAK OUTFLOW IS 399. AT TIME 15.75 HOURS

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PLAN FL 2 AND STAGE 1 (END OF PERT) DATA FOR MULTIPLE PLAN-RATIO ECONOMIC COMPUTATIONS
 FLOWS IN CUBIC FEET PER SECOND (CUBIC METERS PER SECOND)
 AREA IN SQ. ARE MILES (SQUARE KILOMETERS)

OPERATION	STATION	AREA	PLAN	RATIO	RATIOS APPLIED TO FLOWS			
					1	2	3	4
					.16	.17	.18	.20
HYDROGRAPH AT /S DAM	1	.09	1	174.	127.	127.	209.	212.
ROUTED TO	1	.09	1	124.	127.	127.	127.	157.
ROUTED TO	1	.09	1	103.	124.	124.	124.	157.
HYDROGRAPH AT	1	.15	1	104.	124.	124.	124.	157.
2 COMBINED	1	.23	1	104.	124.	124.	124.	157.
ROUTED TO	1	.23	1	104.	124.	124.	124.	157.

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SUMMARY OF DAM SAFETY ANALYSIS

PLAN 1	ELEVATION		INITIAL VALUE		SPILLWAY CREST		TOP OF DAM	
	STORAGE	OUTFLOW	742.00	4.	742.00	4.	745.00	8.
			0.		0.		148.	
RATIO OF PHF	MAXIMUM RESERVOIR		MAXIMUM STORAGE		MAXIMUM OUTFLOW		DURATION OVER TOP	
	W.S.ELEV		AC-FT		CFS		HOURS	TIME OF MAX OUTFLOW HOURS
.15	744.59		7.		104.		0.00	15.75
.17	744.81		4.		127.		0.00	15.75
.18	744.90		3.		137.		0.00	15.75
.20	745.07		3.		150.		.15	15.79
								0.00
								0.00
								0.00
								15.75

PLAN 1 STATION S -D/S

RATIO	MAXIMUM		MAXIMUM		TIME	
	FLOW-CFS	STAGE-FT	STAGE-FT		HOURS	
.15	104.	721.5	721.5		15.83	
.17	127.	721.6	721.6		15.83	
.18	137.	721.7	721.7		15.83	
.20	150.	721.9	721.9		15.83	

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PLAN I

[illegible]

B-27

END

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