

AD-A108 051

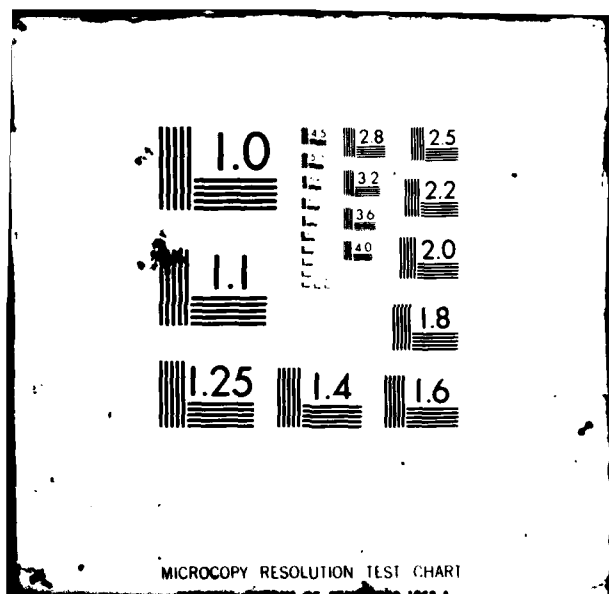
NAVAL SURFACE WEAPONS CENTER SILVER SPRING MD
NOTE ON PLANAR UNDULATOR WIGGLER SINGLE ELECTRON MOTION.(U)
JUN 81 R CAWLEY
NSWC/TR-81-227

F/G 20/5

UNCLASSIFIED

RL

END
DATE
FILMED
1 82
DTIC



AD A108051

NSWC TR 81-227

LEVEL

12

NOTE ON PLANAR UNDULATOR WIGGLER SINGLE ELECTRON MOTION

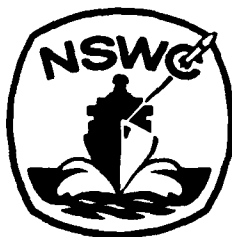
BY ROBERT CAWLEY

RESEARCH AND TECHNOLOGY DEPARTMENT

15 JUNE 1981

Approved for public release, distribution unlimited.

DTIC
ELECTE
S **DEC 2 1981** **D**
D



NAVAL SURFACE WEAPONS CENTER

Dahlgren, Virginia 22448 • Silver Spring, Maryland 20910

DTIC FILE COPY

81 12 02 040

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER NSWC/TR-81-227	2. GOVT ACCESSION NO. AD-A168051	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) NOTE ON PLANAR UNDULATOR WIGGLER SINGLE ELECTRON MOTION		5. TYPE OF REPORT & PERIOD COVERED Final
7. AUTHOR(s) Robert Cawley		6. PERFORMING ORG. REPORT NUMBER
9. PERFORMING ORGANIZATION NAME AND ADDRESS Naval Surface Weapons Center Code R41 White Oak, Silver Spring, MD 20910		8. CONTRACT OR GRANT NUMBER(s)
11. CONTROLLING OFFICE NAME AND ADDRESS		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 61152N; ZR00001; ZR01109; R01AA400
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE June 1981
		13. NUMBER OF PAGES 26
		15. SECURITY CLASS. (of this report) UNCLASSIFIED
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release, distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Free Electron Laser		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) Single particle motion in a planar undulator wiggler free electron laser magnetic field configuration is set up and examined for the construction of invariants, preparatory to specifying beam equilibria for input to a Maxwell-Vlasov analysis. Two invariants are immediately available, the energy (γ) and one component of transverse canonical momentum P_y . In an effort to find a third invariant, or a basis of determination for an advantageous approximate third invariant, which can be associated with the		

DD FORM 1 JAN 73 1473

EDITION OF 1 NOV 65 IS OBSOLETE
S/N 0102-014-6601

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

ITEM 20 (CONT)

axial periodicity of the field, a variable change having some interesting features is reported here. The axial motion between $z = 0$ is converted to the oscillations of a particle in an infinitely long, axially reflecting box. The transit of a half-cycle of wiggler oscillation, $(\Delta z) = \pi/k_0$, corresponds to a single bounce between $Z = +\infty$, where Z is the new coordinate. Transverse coordinates and velocities are continuous at each axial reflection from infinity.

α

$+ \infty - \text{infinity}$

Absolute value of
 Δz

$P_z / k_0 \sin \phi$

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

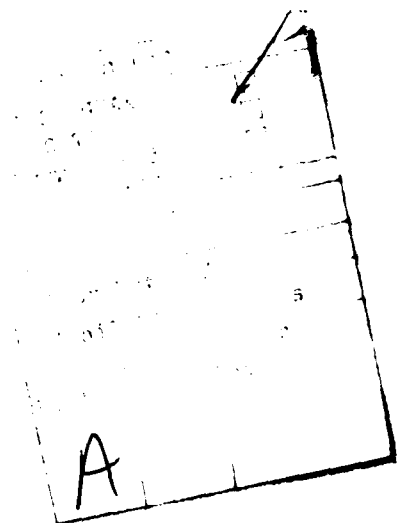
FOREWORD

Single particle motion in a planar undulator wiggler free electron laser magnetic field configuration is set up and examined for the construction of invariants, preparatory to specifying beam equilibria for input to a Maxwell-Vlasov analysis. Two invariants are immediately available, the energy γ and one component of transverse canonical momentum P_y . In an effort to find a third invariant, or a basis of determination for an advantageous approximate third invariant, which can be associated with the axial periodicity of the field, a variable change having some interesting features is reported here. The axial motion between $z = +\infty$ is converted to the oscillations of a particle in an infinitely long, axially reflecting box. The transit of a half-cycle of wiggler oscillation, $|\Delta z| = \pi/k_0$, corresponds to a single bounce between $Z = \pm\infty$, where Z is the new coordinate. Transverse coordinates and velocities are continuous at each axial reflection from infinity.

Ira M. Blatstein

IRA M. BLATSTEIN
By direction

DTIC
ELECTE
S DEC 2 1981 D
D



CONTENTS

<u>Chapter</u>		<u>Page</u>
I	INTRODUCTION	5
II	PLANAR UNDULATOR WIGGLER EQUATIONS OF MOTION	9
III	CHANGE OF VARIABLES	13
IV	CONCLUSION	17
REFERENCES		23

ILLUSTRATIONS

<u>Figure</u>		<u>Page</u>
1	PRINCIPAL BRANCH OF $g(\beta)$ FOR $A > 0$ AND $B = 1$	21
2	SKETCH OF $k_0 z$ <u>VS.</u> z FOR $A = + 2$	22

CHAPTER I

INTRODUCTION

Determination of beam equilibrium configurations forms the starting point in analysis of the free electron laser instability for an intense beam. For equilibrium distributions of beam electrons to be constructed which will take into account nonlinearities associated with beam electron motions in the prescribed magnetic field through which the beam passes, as well as effects of finite transverse geometry, the invariants of single particle motions in the given field are needed. When beam self-fields can be neglected, the determination of such invariants will constitute a solution for the single-particle motion; the equilibrium distribution will be a function of these invariants. Corresponding modulational influences on beam envelope can then be included automatically in the stability analysis.

In two different model field examples this has been done by Bernstein and Hirshfield,¹ Davidson and Uhm^{2,3} and Uhm and Davidson.⁴ In Refs. 1-3 the helical wiggler field was allowed to have only axial dependence,

$$\vec{B}_{\text{wigg}} = -\hat{B} \cos k_0 z \hat{x} - \hat{B} \sin k_0 z \hat{y} \quad (1.1)$$

where $k_0 = 2\pi/\lambda_0$, with λ_0 the wiggler wavelength, and where $\hat{B}$ is the constant amplitude of the wiggler field. In Ref. 3 a uniform axial guide field also was present. In Ref. 4 an axial undulator wiggler with a guide field was studied for the case of a hollow beam, which allowed radial variations of the field components again to be neglected,

$$\vec{B} = B_r \hat{r} + B_z \hat{z}, \quad (1.2)$$

where the axisymmetric components of $\vec{B}$ are got from the $\hat{\theta}$ - component of a vector potential given by $\vec{A} = A_\theta \hat{\theta}$,

$$B_r = -\partial A_\theta / \partial z, \quad B_z = r^{-1} \partial(r A_\theta) / \partial r, \quad (1.3)$$

with $A_\theta = A_\theta(r, z)$, and with also $\nabla \times \vec{B} = 0$. Setting $r = R_0$, the equilibrium beam mean radius, allowed B_r and B_z to be approximated as independent of r , and simplified the analysis of the single particle equations of motion. The field then has a form similar to eq. (1.1),

$$B_r \approx -\hat{B}_r \sin k_0 z, \quad B_z \approx B_0 - \hat{B}_z \cos k_0 z \quad (1.4)$$

where B_0 is the uniform guide field, and $\hat{B}_r, \hat{B}_z$ are constant wiggler amplitudes determined by $B_0, k_0 R_0$, and the mirror ratio $R \equiv B_z(r=0, k_0 z = \pm \pi) / B_z(r=0, k_0 z = 0)$.

In Refs. 1 and 2, three exact invariants of electron motion, the energy and two components of transverse canonical momentum, were available; and the same is true of Ref. 3, but where the invariants (C_1, C_h, C_z), now also allowed incorporation of helical and axial field effects together. In the undulator configuration of Ref. 4, only two exact invariants were available, the energy and canonical axial angular momentum, and a third approximate invariant, the axial component of particle momentum, p_z , was employed. So the undulator wiggler field single particle motions have also proved more difficult.

In the present report I describe a brief investigation of single particle motion in a planar undulator field, specified by a vector potential $\vec{A} = A_y(x, z)\hat{y}$. Only two invariants are immediately available, the energy and $\hat{y}$ -component of canonical momentum. As a starting point of the search for a third invariant with origin in the axial periodicity of the wiggler, or to produce a convenient basis of determination of an approximate third invariant better than p_z , I have transformed the axial coordinate z to a new coordinate Z , which ranges between $+\infty$ as z covers a half-cycle of wiggler oscillation. The transformation is fixed by specifying that the wiggler amplitude be absent from the axial equation (for zero guide field). After elimination of the y coordinate, the xZ -equations describe a particle oscillating in a box of infinite "length" and having axially reflecting walls, while also executing its transverse motions. In this way, the full motion along the beam axis is transformed into motion over only a single cycle of wiggler oscillation.

It is not clear whether the altered problem presents special calculational advantage, and time has not permitted more than a cursory examination of this. It has seemed appropriate nevertheless to record the present formulation as a slightly unusual and possibly

useful starting point of analysis in which features associated with wiggler periodicity receive explicit attention at the outset. The method is more generally applicable, e.g. to problems of cylindrical symmetry as well as to the present case of planar symmetry.

CHAPTER II

PLANAR UNDULATOR WIGGLER EQUATIONS OF MOTION

The vector potential is $\vec{A} = A_y \hat{y}$, and the magnetic field's nonvanishing components are

$$B_x = - \frac{\partial A_y}{\partial z}, \quad B_z = \frac{\partial A_y}{\partial x}, \quad (2.1)$$

The choice

$$A_y(x, z) = B_0 x - k_0^{-1} B_1 \sinh k_0 x \sinh k_0 z \quad (2.2)$$

models a static undulator configuration with mean guide field B_0 and undulator amplitude B_1 , where B_0 and B_1 are constants. Due to the symmetry

$$A_y(-x, z) = - A_y(x, z) \quad (2.3)$$

B_z has the sign of x , corresponding to like-pole magnet pairings successively alternating along the $\hat{z}$ - direction. The field satisfies the condition $\nabla \times \vec{B} = 0$. The Hamiltonian,

$$H = c \left[p_x^2 + p_z^2 + \left(p_y - qc^{-1} A_y(x, z) \right)^2 + m^2 c^2 \right]^{1/2} \quad (2.4)$$

where c is the speed of light in vacuo, q the charge on the electron and m its mass, is invariant to translations along the $\hat{y}$ -axis so p_y is a constant of the motion along with H ; and the problem of configuration motion is therewith reduced to a two-dimensional one in x and z .

It will be enough to study the configuration equations of motion. These are

$$\frac{d^2x}{dt^2} = \frac{q}{\gamma mc} B_z(x, z) \dot{y} \quad (2.5)$$

$$\frac{d^2z}{dt^2} = - \frac{q}{\gamma mc} B_x(x, z) \dot{y} \quad (2.6)$$

and

$$\begin{aligned} \frac{d^2y}{dt^2} &= \frac{q}{\gamma mc} (B_x(x, z) \dot{z} - B_z(x, z) \dot{x}) \\ &= - \frac{d}{dt} \left(\frac{q}{\gamma mc} A_y(x, z) \right), \end{aligned} \quad (2.7)$$

the last by the constancy of γ , whose value is H/mc^2 , and by eqs. (2.1). From eq. (2.7)

$$\dot{y} = \frac{P_y}{\gamma m} - \frac{q A_y(x, z)}{\gamma mc}, \quad (2.8)$$

where P_y is the constant of integration; whence, upon substitution into eqs. (2.5) and (2.6) one has

$$\frac{d^2x}{dt^2} = - \frac{\partial \psi}{\partial x}, \quad \frac{d^2z}{dt^2} = - \frac{\partial \psi}{\partial z} \quad (2.9)$$

where

$$\psi = \psi(x, z) = - \frac{q P_y}{\gamma^2 m^2 c} A_y + \frac{1}{2} \left(\frac{q A_y}{\gamma mc} \right)^2. \quad (2.10)$$

Eqs. (2.9) have the first integral

$$\frac{1}{2} (\dot{x}^2 + \dot{z}^2) + \psi(x, z) = C = \text{const.} \quad (2.11)$$

P_y , γ and C satisfy a relationship

$$C = -\frac{1}{2} \left(\frac{P_y}{\gamma m} \right)^2 + \frac{1}{2} (1 - \gamma^{-2}) c^2, \quad (2.12)$$

so only two of the three constants are independent, and γ can be exchanged for C if we wish.

Note from eq. (2.8), $P_y = 0$ corresponds to $\langle \dot{y} \rangle = 0$ for electron distributions even under $x \rightarrow -x$ owing to eq. (2.3). In this case also, $2C$ has the value v_0^2 , where v_0 is the constant speed of the charge.

I assume $B_0 = 0$ for simplicity now and expand eqs. (2.9) using (2.2) and (2.10),

$$\frac{d^2 x}{dt^2} = -\cosh k_0 x \cdot \sinh k_0 z \cdot (a + b \sinh k_0 x \cdot \sinh k_0 z) \quad (2.13)$$

$$\frac{d^2 z}{dt^2} = -\sinh k_0 x \cdot \cosh k_0 z \cdot (a + b \sinh k_0 x \cdot \sinh k_0 z), \quad (2.14)$$

where

$$a \equiv qB_1/(\gamma m)^2 c \cdot P_y = \frac{\Omega_1}{\gamma m} P_y \quad (2.15)$$

$$b \equiv (qB_1/\gamma mc)^2 k_0^{-1} = k_0^{-1} \Omega_1^2, \quad (2.16)$$

with $\Omega_1 \equiv qB_1/\gamma mc$; from eq. (2.11) also

$$\begin{aligned} \dot{x}^2 + \dot{z}^2 + 2 a k_0^{-1} \sinh k_0 x \cdot \sinh k_0 z \\ + b k_0^{-1} \sinh^2 k_0 x \cdot \sinh^2 k_0 z = 2C. \end{aligned} \quad (2.17)$$

CHAPTER III

CHANGE OF VARIABLES

If a new axial variable Z is introduced,

$$Z = k_0^{-1} g(k_0 z), \quad (3.1)$$

independent of t so the Hamiltonian will be unchanged in value, and with g a function at our disposal, we have the identities,

$$\dot{z} \equiv g'(k_0 z)^{-1} \dot{Z} \quad (3.2)$$

and

$$\frac{d^2 Z}{dt^2} \equiv g'(k_0 z)^{-1} \left[\ddot{Z} - k_0 g''(k_0 z) \dot{z}^2 \right], \quad (3.3)$$

where primes denote differentiation with respect to the argument. Eq. (2.14) becomes

$$\begin{aligned} \ddot{Z} - k_0 g'' \left[2C - \dot{x}^2 - 2ak_0^{-1} \sinh k_0 x \cdot \sinh k_0 z \right. \\ \left. - bk_0^{-1} \sinh^2 k_0 x \cdot \sin^2 k_0 z \right] = -g' \cdot a \sinh k_0 x \cdot \cosh k_0 z \\ - g' \cdot b \sinh^2 k_0 x \cdot \sinh k_0 z \cosh k_0 z. \end{aligned} \quad (3.4)$$

Note the choice $g(\beta) = \beta$, with $\beta \equiv k_0 z$ gives $Z = z$, and (3.4) reduces to (2.14) as it should.

The x -dependence of the coefficients of a , to be called a -terms, is the same on both sides of eq. (3.4); the same is true of the coefficients of b , viz. the b -terms. So the a -terms can be transformed away by a suitable choice of g ; or the b -terms can be

removed instead. (They cannot both be removed by a transformation of z .) The former is accomplished if g satisfies

$$2g''(\beta) \sin\beta = -g'(\beta) \cos\beta \quad (3.5)$$

i.e.

$$g'(\beta) = \pm A / \sqrt{|\sin\beta|}, \quad A > 0. \quad (3.6)$$

The transformation cannot be determined as an elementary function owing to the square root in eq. (3.6), whose cause was the factor 2 in eq. (3.5).

For the b-terms matters are different; the analogue of eq. (3.5) is

$$g''(\beta) \sin^2\beta = -g'(\beta) \sin\beta \cos\beta, \quad (3.7)$$

whence

$$|g'(\beta) \sin\beta| = |A|, \quad (3.8)$$

or, more serendipitously,

$$g'(\beta) = A \cos\beta, \quad (3.9)$$

where A is an arbitrary nonzero constant. Integrating,

$$k_0 z \equiv g(\beta) = A \log |B \tan \frac{1}{2} \beta|, \quad B = \text{const.}, \quad (3.10)$$

where, it will be recalled, $\beta = k_0 z$. B may be assumed positive without loss of generality; I assume further that $B = 1$ as there seems to be no gain resulting from its retention as a free parameter. (Figure 1 shows a sketch of $g(\beta)$ for $A > 0$, and $0 < \beta < \pi$.) Solving eq. (3.10) gives also,

$$\sin\beta = \pm \operatorname{sech} A^{-1} k_0 z, \quad \tan\beta = \mp \operatorname{csch} A^{-1} k_0 z, \quad (3.11)$$

the sign associations for fixed A depending upon the angular range in which β falls. From (3.11), also,

$$\cos \beta = - \tanh A^{-1} k_0 Z. \quad (3.12)$$

Hence, from eqs. (3.7), (3.9), (3.11) and (3.12),

$$g''(\beta) = A \sinh A^{-1} k_0 Z \cdot \cosh A^{-1} k_0 Z, \quad (3.13)$$

which, from inspection of eq. (3.4), suggests either $A = 2$ or $A = -2$. Each choice gives

$$g''(\beta) = + \sinh k_0 Z, \quad |A| = 2, \quad (3.14)$$

and eq. (3.4) becomes

$$\begin{aligned} \ddot{Z} - (2C - \dot{x}^2) k_0 \sinh k_0 Z \\ = \mp 2a \sinh k_0 x \cdot \sinh \frac{1}{2} k_0 Z; \end{aligned} \quad (3.15)$$

from eq. (2.13)

$$\begin{aligned} \ddot{x} + \frac{1}{2} b \operatorname{sech}^2 \frac{1}{2} k_0 Z \cdot \sinh 2k_0 x \\ = \mp a \operatorname{sech} \frac{1}{2} k_0 Z \cdot \cosh k_0 x. \end{aligned} \quad (3.16)$$

The "energy equation", eq. (2.17), reads

$$\begin{aligned} \dot{x}^2 + \dot{Z}^2 \pm 2ak_0^{-1} \sinh k_0 x \cdot \operatorname{sech} \frac{1}{2} k_0 Z \\ + bk_0^{-1} \sinh^2 k_0 x \cdot \operatorname{sech}^2 \frac{1}{2} k_0 Z = 2C, \end{aligned} \quad (3.17)$$

where

$$\dot{Z}^2 = \frac{1}{4} \operatorname{sech}^2 \frac{1}{2} k_0 Z \cdot \dot{Z}^2. \quad (3.18)$$

The upper and lower signs in eqs. (3.15) - (3.17) correspond to those in eqs. (3.11). Notice, finally, the periodic functions of z now are gone.

There is a consideration of domain, and we have a choice of procedures in defining the transformation further. Eqs. (3.2) and (3.9) give

$$\dot{z} = \epsilon(A) \cdot \frac{1}{2} \sin k_0 z \cdot \dot{Z} \quad (3.19)$$

while also, by definition of g ,

$$\frac{dZ}{dz} = g' = \epsilon(A) / \frac{1}{2} \sin k_0 z. \quad (3.20)$$

The second equation shows that Z , which takes all values as β varies between any two successive integer multiples of π (cf. eq. (3.10)), rises or falls monotonically with z , for fixed A , according to the sign of $\sin k_0 a$. We may choose $A > 0$ for $\sin \beta > 0$ and $A < 0$ for $\sin \beta < 0$. In this case also, eq. (3.19) shows that $\dot{z}$ and $\dot{Z}$ have the same sign always. There seems to be no special advantage to doing this, however, so I will just take $A = +2$ and allow Z to reverse sign relative to $\dot{z}$ each time β passes through an integer multiple of π . Each time it does the upper (lower) signs in eqs. (3.11), and (3.15) - (3.17) give way to the lower (upper) signs. For finite $\dot{z}$ both Z and $\dot{Z}$ are infinite across these points, while x and $\dot{x}$ are continuous. The system of equations of the axial motion along the z -axis from $-\infty$ to $+\infty$, coupled with the x -motion, has been replaced by a pair of systems corresponding to motion along succeeding half-cycles of $k_0 z$, covering a combined finite length $2\pi/k_0$. And in Z -space, there are axially reflecting mirrors at $\pm \infty$. The situation is illustrated in Figure 2.

For vanishing P_y , $a = 0$ and eqs. (3.15) and (3.16) become slightly simpler,

$$\ddot{Z} - (2C - \dot{x}^2) k_0 \sinh k_0 Z = 0 \quad (3.21)$$

$$\ddot{x} + \frac{1}{2} b \operatorname{sech}^2 \frac{1}{2} k_0 Z \cdot \sinh 2k_0 x = 0. \quad (3.22)$$

Note, once more, the absence of the periodic functions of z .

CHAPTER IV

CONCLUSION

A planar undulator wiggler field configuration has been constructed and examined from the standpoint of a transformation of the axial coordinate that sends the description of the single-electron motion between $z = \pm \infty$, to that of a particle in a box in which an oscillation cycle between $Z = \pm \infty$ corresponds to the traversal of a single cycle of wiggler period $|\Delta z| = 2\pi/k_0$.

A similar transformation is possible for the x-motion, but this has not been discussed as the resulting system does not appear especially interesting.

The special case $P_y = 0$ should be an interesting one physically (cf. remark in the paragraph following eq. (2.12)), so eqs. (3.21) and (3.22), in particular, might repay some effort of further investigation.

ACKNOWLEDGMENTS

The author wishes to thank H. S. Uhm for suggesting the importance of the problem of finding a third invariant for wiggler fields with dependence upon transverse as well as axial coordinates. This work was supported by the Independent Research Fund at the Naval Surface Weapons Center.

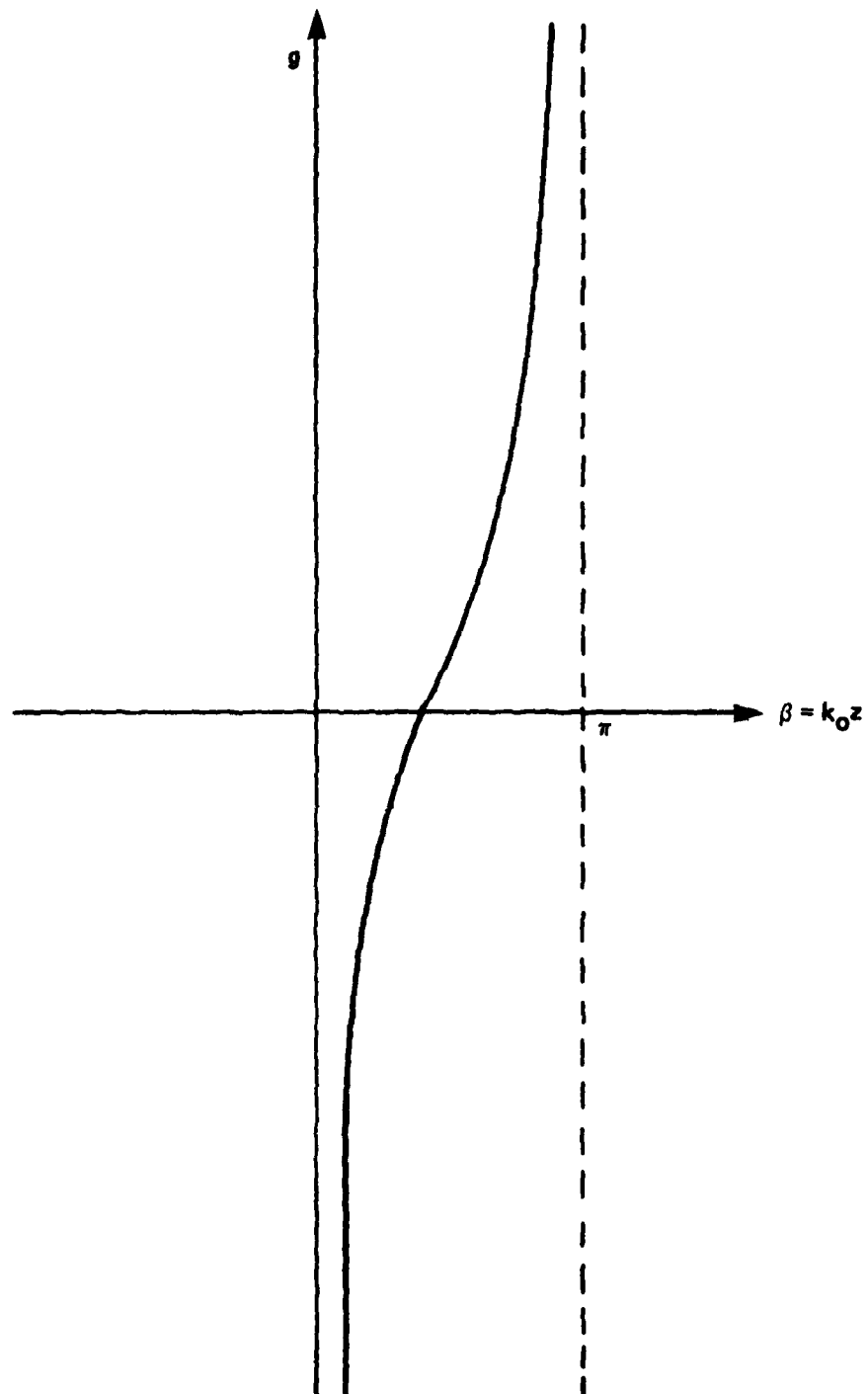


FIGURE 1 PRINCIPAL BRANCH OF $g(\beta)$ FOR $A > 0$ AND $B = 1$

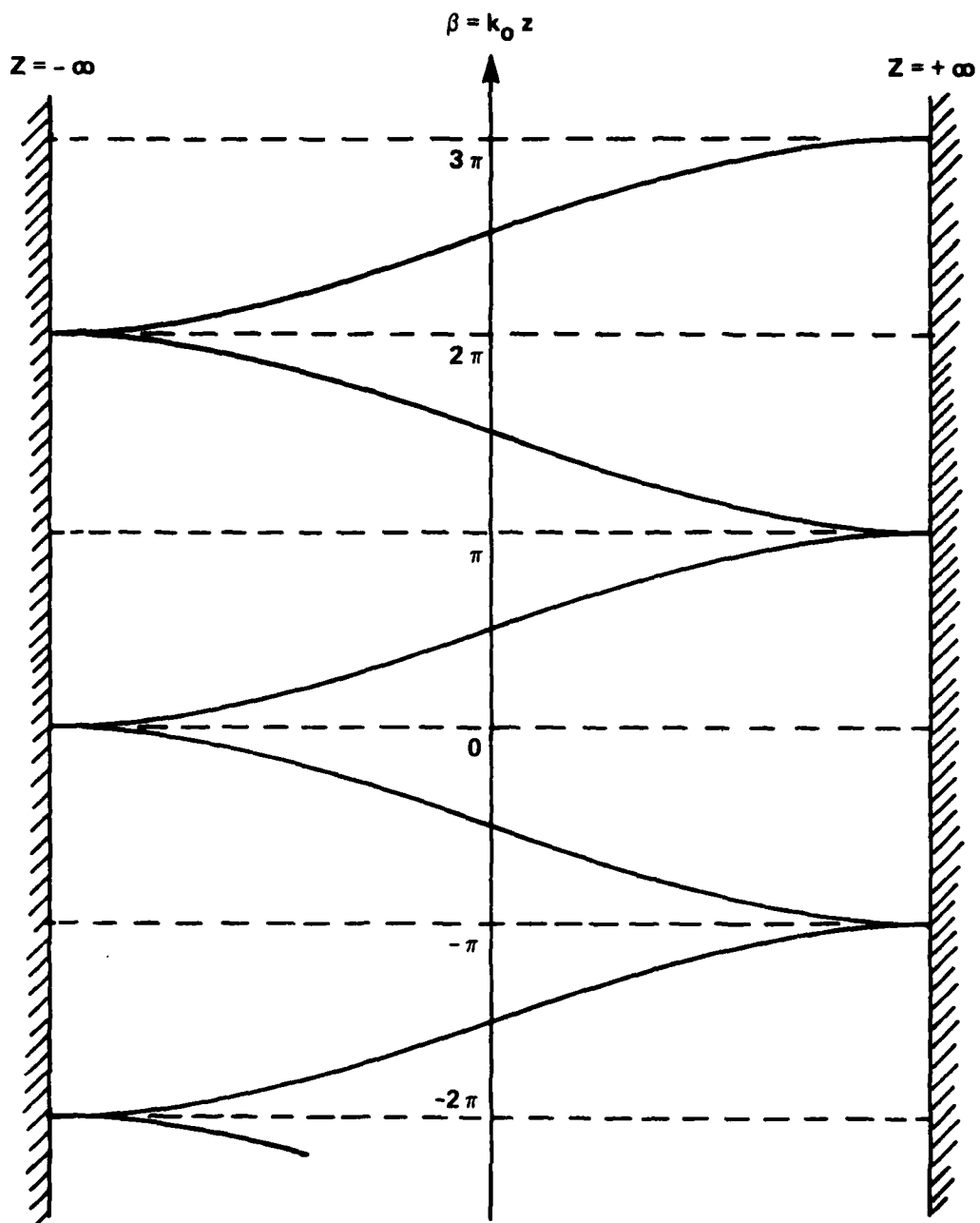


FIGURE 2 SKETCH OF $k_0 z$ VS Z FOR $A = +2$

REFERENCES

1. I. B. Bernstein and J. L. Hirshfield, Phys. Rev. A20, 1661(1979).
2. R. C. Davidson and H. S. Uhm, Phys. Fluids 23, 2076(1980).
3. R. C. Davidson and H. S. Uhm, "Helically Distorted Relativistic Electron Beam Equilibria for Free Electron Laser Applications" (MIT/NSWC Preprint).
4. H. S. Uhm and R. C. Davidson, "Theory of Free Electron Laser Instability in a Relativistic Annular Electron Beam" (NSWC/MIT Preprint).

DISTRIBUTION

	Copies
Naval Research Laboratory Attn: Dr. M. Lampe Washington, D.C. 20365	1
Office of Naval Research Attn: W. J. Condell (ONR-421) Washington, D.C. 20350	2
U. S. Army Ballistic Research Laboratory Aberdeen Proving Ground Attn: Dr. D. Eccleshall (DRDAR-BLB) Aberdeen, Maryland 21005	1
Air Force Weapons Laboratory Kirtland Air Force Base Attn: Maj. H. Dogliani Albuquerque, New Mexico 87117	1
Department of Energy Attn: Dr. T. Godlove (C-404) Washington, D.C. 20545	1
National Bureau of Standards Attn: Dr. J. M. Leiss Gaithersburg, Maryland 20760	1
Austin Research Associates, Inc. Attn: Dr. W. E. Drummond 1901 Rutland Drive Austin, Texas 78758	1
Ballistic Missile Defense Advanced Technology Center Attn: Dr. L. J. Harvard (BMDSATC-1) P. O. Box 1500 Huntsville, Alabama 35807	1
B-K Dynamics, Inc. Attn: Dr. R. Linz 15825 Shady Grove Road Rockville, Maryland 20850	1

DISTRIBUTION (cont)

	Copies
The Charles Stark Draper Laboratory, Inc. Attn: Dr. E. Olsson 555 Technology Square Cambridge, Massachusetts 02139	1
Director Defense Advance Research Projects Agency Attn: Dr. J. Mangano 1400 Wilson Boulevard Arlington, Virginia 22209	1
IRT Corporation Attn: Mr. W. Selph P. O. Box 81087 San Diego, California 92138	1
Los Alamos Scientific Laboratory Attn: Dr. G. Best P. O. Box 1663 Los Alamos, New Mexico 87545	1
Mission Research Corporation Attn: Dr. C. Longmire 735 State Street Santa Barbara, California 93102	1
Physical Dynamics, Inc. Attn: Dr. K. Breuckner P. O. Box 977 La Jolla, California 92037	1
Sandia Laboratories Attn: Mail Services Section for: Dr. R. B. Miller Albuquerque, New Mexico 87115	1
Science Applications, Inc. Attn: Dr. M. P. Fricke 1200 Prospect Street La Jolla, California 92037	1

DISTRIBUTION (cont)

	Copies
Science Applications, Inc.	
Attn: Dr. R. Johnston	1
Dr. J. Siambis	1
2680 Hanover Street	
Palo Alto, California 94304	
University of California	
Lawrence Livermore Laboratory	
Attn: Dr. R. J. Briggs	1
Dr. E. Lee	1
P. O. Box 808	
Livermore, California 94550	
Defense Technical Information Center	
Cameron Station	12
Alexandria, Virginia 22314	
Naval Sea Systems Command	
Washington, D.C. 20362	
Attn: SEA-09G32	2
SEA-03B	1

TO AID IN UPDATING THE DISTRIBUTION LIST
FOR NAVAL SURFACE WEAPONS CENTER, WHITE
OAK TECHNICAL REPORTS PLEASE COMPLETE THE
FORM BELOW:

TO ALL HOLDERS OF NSWC TR 81-227
By Robert Cavley
DO NOT RETURN THIS FORM IF ALL INFORMATION IS CURRENT

A. FACILITY NAME AND ADDRESS (OLD) (Show Zip Code)

NEW ADDRESS (Show Zip Code)

B. ATTENTION LINE ADDRESSES:

C.

☐ REMOVE THIS FACILITY FROM THE DISTRIBUTION LIST FOR TECHNICAL REPORTS ON THIS SUBJECT.

D.

NUMBER OF COPIES DESIRED

**DATA
FILM**