

AD-A119 945

GENERAL ELECTRIC CO CINCINNATI OH AIRCRAFT ENGINE BU--ETC F/G 11/6 -
MATERIAL CHARACTERIZATION. PART A. MECHANICAL PROPERTIES OF TWO--ETC(U)
MAY 82 S A EMERY
UOR-TR-79-98 F33615-77-C-5221
AFWAL-TR-82-2042-VOL-1 NL

UNCLASSIFIED

1-1
1-1

END
PAGE
FILMED
11 82
DT *

(12)

AFWAL-TR-82-2042
Volume I



MATERIAL CHARACTERIZATION, PART A MECHANICAL PROPERTIES OF
TWO METALS AT SEVERAL STRAIN RATES

S. A. EMERY

University of Dayton Research Institute
Dayton, Ohio 45469

May 1982

Interim Report for period 1 October 1977 - 30 November 1979

Approved for public release; distribution unlimited.

DTIC FILE COPY

AERO PROPULSION LABORATORY
AIR FORCE WRIGHT AERONAUTICAL LABORATORIES
AIR FORCE SYSTEMS COMMAND
WRIGHT-PATTERSON AIR FORCE BASE, OHIO 45433

DTIC
SELECTED
OCT 7 1982
A

82 10 07 008

NOTICE

When Government drawings, specifications, or other data are used for any purpose other than in connection with a definitely related Government procurement operation, the United States Government thereby incurs no responsibility nor any obligation whatsoever; and the fact that the government may have formulated, furnished, or in any way supplied the said drawings, specifications, or other data, is not to be regarded by implication or otherwise as in any manner licensing the holder or any other person or corporation, or conveying any rights or permission to manufacture, use, or sell any patented invention that may in any way be related thereto.

This report has been reviewed by the Office of Public Affairs (ASD/PA) and is releasable to the National Technical Information Service (NTIS). At NTIS, it will be available to the general public, including foreign nations.

This technical report has been reviewed and is approved for publication.

Sandra K. Drake

SANDRA K. DRAKE
Project Engineer

Isak J. Gershon

ISAK J. GERSHON
Technical Area Manager,
Propulsion Mechanical Design

FOR THE COMMANDER

James M. Shipman

J. SHIPMAN, MAJ, USAF
Deputy Director, Turbine Engine Division

"If your address has changed, if you wish to be removed from our mailing list, or if the addressee is no longer employed by your organization, please notify AFWAL/POTA, WPAFB OH 45433 to help us maintain a current mailing list."

Copies of this report should not be returned unless return is required by security considerations, contractual obligations, or notice on a specific document.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

REPORT DOCUMENTATION PAGE		READ INSTRUCTIONS BEFORE COMPLETING FORM
1. REPORT NUMBER AFWAL-TR-82-2042 Vol I	2. GOVT ACCESSION NO. AD-A119 985	3. RECIPIENT'S CATALOG NUMBER
4. TITLE (and Subtitle) MATERIAL CHARACTERIZATION, PART A MECHANICAL PROPERTIES OF TWO METALS AT SEVERAL STRAIN RATES		5. TYPE OF REPORT & PERIOD COVERED Technical Report October 1977 30 November 1979
7. AUTHOR(s) S. A. Emery		6. PERFORMING ORG. REPORT NUMBER UDR-TR-79-98
9. PERFORMING ORGANIZATION NAME AND ADDRESS University of Dayton Research Institute 300 College Park Ave. Dayton, Ohio 45469		8. CONTRACT OR GRANT NUMBER(s) 200-4BA-14K47844
11. CONTROLLING OFFICE NAME AND ADDRESS General Electric Company Evendale Plant - Aircraft Engine Group Evendale, OH 45215		10. PROGRAM ELEMENT, PROJECT, TASK AREA & WORK UNIT NUMBERS 62203F, 3066, 12, 33
14. MONITORING AGENCY NAME & ADDRESS (if different from Controlling Office)		12. REPORT DATE May 1982
		13. NUMBER OF PAGES 67
		15. SECURITY CLASS. (of this report) Unclassified
		15a. DECLASSIFICATION/DOWNGRADING SCHEDULE
16. DISTRIBUTION STATEMENT (of this Report) Approved for public release; distribution unlimited.		
17. DISTRIBUTION STATEMENT (of the abstract entered in Block 20, if different from Report)		
18. SUPPLEMENTARY NOTES		
19. KEY WORDS (Continue on reverse side if necessary and identify by block number) Stainless steel, titanium, foreign object damage, mechanical properties, low strain rate, intermediate strain rates, and dynamic strain rates.		
20. ABSTRACT (Continue on reverse side if necessary and identify by block number) >This report describes mechanical property data collected in support of a fan blade analysis model. The development of the blade model is part of a foreign object damage (FOD) study of jet engine fan blades. Use of the properties in the model allows one to evaluate potential fan blade materials. Part A of this report contains a discussion of the mechanical property tests conducted on two metallic materials: 410 stainless steel and 8Al-1Mo-1V titanium. These two materials were selected because		

DD FORM 1 JAN 73 1473

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE (When Data Entered)

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

of their use in the J-79 blade and the F-101 blade respectively. Part B of the report contains a discussion of mechanical property tests conducted on the two composite components of a hybrid composite blade: boron/2024 aluminum and stainless steel wire mesh. These two composites are used in the hybrid composite APSI blade.

Static, quasi-static and dynamic tensile tests were conducted on the metallic materials because (1) studies indicate that metallic mechanical properties exhibit strain rate dependence and (2) tests conducted on full scale blade, show that various locations on the fan blades load at different rates. The mechanical properties measured include Young's Modulus (when obtainable), Poisson's ratio (when obtainable), the yield strength, the ultimate strength, and the ultimate strain. The density of the materials was also measured.

UNCLASSIFIED

SECURITY CLASSIFICATION OF THIS PAGE(When Data Entered)

FOREWORD

This report describes a contractual work effort conducted for the General Electric Company, Aircraft Engine Group under Purchase Order No. 200-FBA-14K-47844 which is a subcontract of F33615-77-C-5221.

This report covers work conducted during the period of October 1977 to November 1979 and is part of Task IV-A.

The GE Program Manager was Mr. Joe McKenzie and the Principal Investigator was Mr. Al Storace. The work reported herein was performed under the direction of Susan A. Emery, Experimental and Applied Mechanics Division, University of Dayton Research Institute.

Technical support was provided by Mr. E. C. Klein. Program management for the University was provided by Mr. Robert Bertke.

This report covers work conducted for project 3066, task 12, entitled Foreign Object Impact Design Criteria. The contract was sponsored by the Aero Propulsion Laboratory, Air Force Systems Command, Wright-Patterson AFB, Ohio 45433 under the direction of Sandra K. Drake (AFWAL/POTA), Project Engineer.



Accession For	
NTIS GRA&I	☒
DTIC TAB	☐
Unannounced	☐
Justification	
By	
Distribution/	
Availability Codes	
Dist	Avail and/or Special
A	

TABLE OF CONTENTS

<u>SECTION</u>		<u>PAGE</u>
I	INTRODUCTION	1
II	EXPERIMENTAL PROCEDURES	3
	2.1 LOW AND INTERMEDIATE STRAIN RATE TESTS	3
	2.1.1 Test Specimen and Specimen Instrumentation	4
	2.1.2 Test Procedures and Test System	4
	2.1.2.1 Test System	4
	2.1.2.2 Test Procedure	7
	2.2 HIGH STRAIN RATE TESTS	7
	2.2.1 Experimental Apparatus	7
	2.2.2 Instrumentation	9
	2.2.3 Test Procedures and Mechanisms	11
III	ANALYSIS	15
	3.1 LOW AND INTERMEDIATE STRAIN RATE TESTS	15
	3.2 HIGH STRAIN RATE TESTS	17
IV	RESULTS AND DISCUSSION	19
	REFERENCES	27
	APPENDIX A: LOW AND INTERMEDIATE STRAIN RATE CURVES AND DIGITAL DATA	28
	APPENDIX B: HIGH STRAIN RATE CURVES AND DIGITAL DATA	57

LIST OF ILLUSTRATIONS

<u>FIGURE</u>		<u>PAGE</u>
1	Specimen for Low and Intermediate Strain Rate Tests.	5
2	Location of Measurement Instrumentation on the Low and Intermediate Strain Rate Specimens.	6
3	Schematic of Apparatus and Instrumentation for High Strain Rate Tests.	8
4	Specimen for High Strain Rate Tests.	10
5	Typical Oscilloscope Traces.	12
6	Lagrangian Displacement - Time Plot for High Strain Rate Tests.	13
7	Young's Modulus VS. Strain Rate.	23
8	Yield Stress VS. Strain Rate.	24
9	Ultimate Stress VS. Strain Rate.	25
10	Ultimate Strain VS. Strain Rate.	26

LIST OF TABLES

<u>TABLE</u>		<u>PAGE</u>
1	STRAIN RATES OF METALLIC MATERIAL CHARACTERIZATION TESTS	3
2	MECHANICAL PROPERTIES OBTAINED FOR 8Al-1Mo-1V TITANIUM	20
3	MECHANICAL PROPERTIES OBTAINED FOR 410 STAINLESS STEEL	21
4	DENSITY	22

SECTION I

INTRODUCTION

The material characterization tests discussed in this report are part of a foreign object damage (FOD) study of jet engine fan blades. The tests constitute a portion of the gross structural damage subtask of that study. The FOD study is designed to provide two resources necessary for the successful development of FOD resistant fan blades: (1) an analysis capability for predicting jet engine response to FOD impacts and (2) an understanding of the mechanisms of FOD failures. The fan blade analytical model uses inputs such as mechanical property data (of the material under consideration) and impact loads (representative of ice balls, ice spears, or small birds) to predict the fan blade response to the foreign object damage impacts. The model allows considerable evaluation of the blade design and material prior to the manufacturing and testing of a full stage of blades. This eliminates many costly experiments that have been necessary in the past.

The material characterization tests provide mechanical properties for use in the blade model discussed above. The materials tested include two metals, 410 stainless steel and 8Al-1Mo-1V titanium (used in the J-79 blade and F-101 blade, respectively) and two composites, boron/2024 aluminum and stainless steel wire mesh (used in the hybrid composite APSI blade). Part A of this report contains the description of the material characterization tests on the metals. Part B contains the discussion of the material characterization tests on the composite materials.

The mechanical properties of metals usually exhibit some strain rate dependence. ^(1,2,3) In addition, experiments have shown that the FOD impacts load various sections of the blades at different rates. For these reasons, tensile tests were conducted on the metals at strain rates ranging from 10^{-3} to

about 10^3 strain/second. The quasi-static and intermediate rate tests (10^{-3} to 1 strain/second), conducted with an MTS closed-loop hydraulic system, provide the following elastic and plastic region parameters: Young's modulus, Poisson's ratio (in the elastic region), 0.2 percent offset yield stress, ultimate stress, and ultimate strain. The dynamic tests (500 to 700 strain/second), conducted on a split-Hopkinson bar apparatus, provide only the plastic region parameters: yield stress, ultimate stress, and ultimate strain. The mechanical properties are summarized in this report as plots of the various parameters versus strain rate.

SECTION II

EXPERIMENTAL PROCEDURES

Tensile tests conducted at the strain rates shown in Table 1 provide the desired mechanical property data. This range of rates encompasses the range of strain rates measured at select locations on the full scale blade tests, 12-370 strain/second. (The full scale blade tests were conducted as part of the gross structural damage subtask IV-A but reported with similar tests in the Task VI report.) The quasi-static and intermediate rate tests (10^{-3} to 1 strain/second) were run on an MTS electrohydraulic closed-loop testing machine. They require different specimens and procedures than do the dynamic tests, which were run on the split-Hopkinson bar apparatus. Consequently, the two types of tests are described separately below.

TABLE 1
STRAIN RATES OF METALLIC MATERIAL
CHARACTERIZATION TESTS

Material	Strain Rates (strain/second)
8Al-1Mo-1V Titanium	10^{-3} , 10^{-1} , 1, 500
403 Stainless Steel	10^{-3} , 10^{-1} , 1, 700

2.1 LOW AND INTERMEDIATE STRAIN RATE TESTS

The information obtained from the low and intermediate strain rate tests include two elastic parameters, Young's modulus and Poisson's ratio, and three plastic parameters, the yield stress, the ultimate stress, and the ultimate strain. The following paragraphs describe the specimens used and how they were instrumented and tested. The full true stress-true strain curves appear in Appendix A.

2.1.1 Test Specimen and Specimen Instrumentation

The specimens were made from bar stock which had been worked the same amount as the finished blades. The specimen is illustrated in Figure 1. Its dimensions were per ASTM standard E8-69.⁽⁴⁾ Three specimens of each material were tested at each rate with one exception. Only one specimen of the titanium was tested at 1 strain/second.

Figure 2 shows the location of measurement instrumentation placed on the specimens. The extensometer supplied information for obtaining the entire stress-strain from test start to specimen failure. The high resistance foil strain gage placed in the longitudinal direction (the same direction as the applied load) provided high resolution measurements for the parameters in the elastic region and at yield. The strain gage in the transverse direction (to the applied load) supplied measurements for the calculation of Poisson's ratio. The transverse strain gages were applied to only one specimen of each material at each strain rate. The data reduction equations appear in the analysis section of this report.

2.1.2 Test Procedures and Test System

The following paragraphs contain a brief description of the test system and test procedures used for the low and intermediate strain rate tests.

2.1.2.1 Test System

The low and intermediate strain rate tests were conducted using the University's MTS electrohydraulic closed-loop testing system. This closed-loop test machine can be programmed in load, strain, or displacement control. The machine can produce displacement rates that range from less than 0.05 in/min. to 400 in/min. The signal conditioner used with the strain gage was a Honeywell 218 Bridge Amplifier. Included in the test system is an X-Y recorder and a multichannel transient recorder. An additional two pen X-Y recorder was used for these tests.

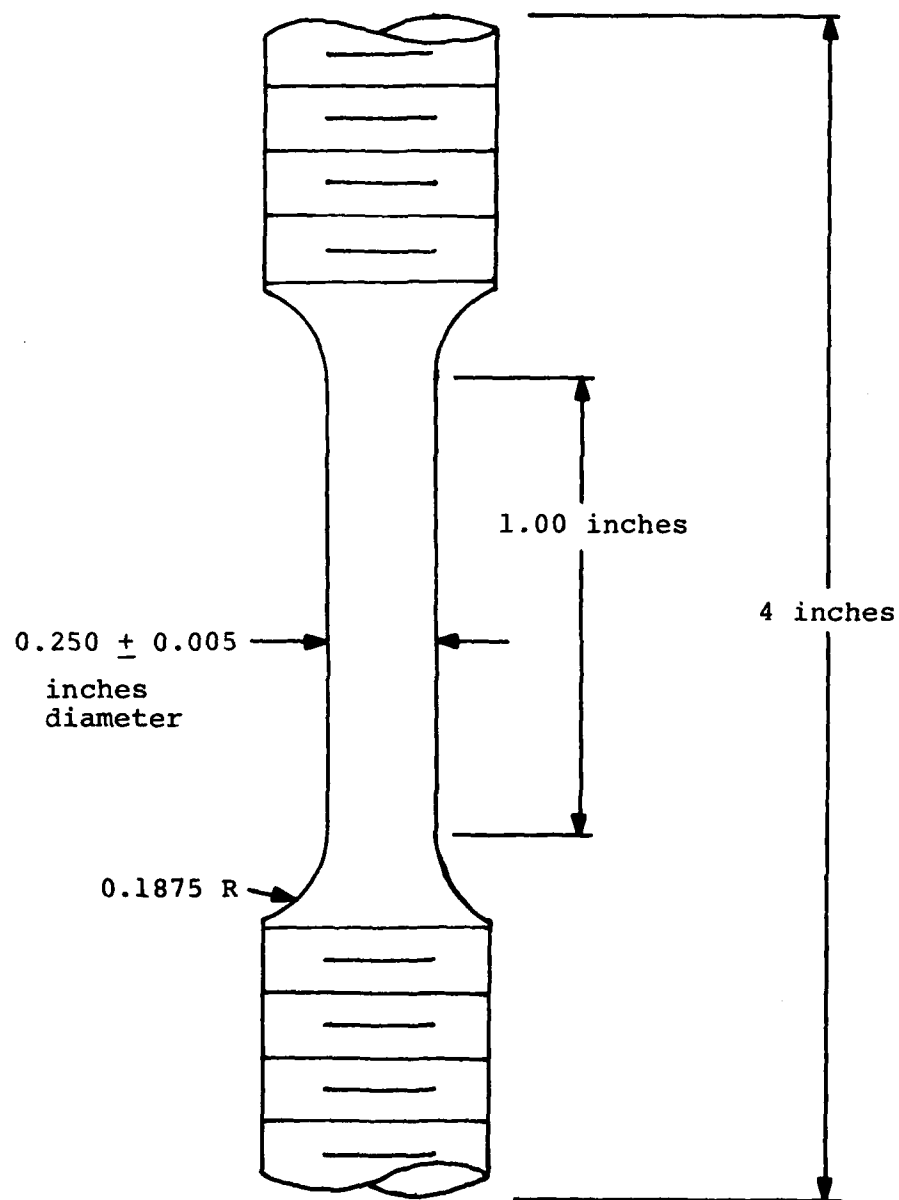
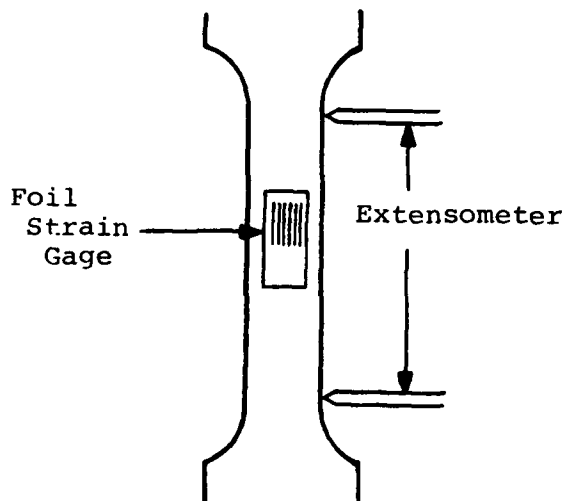
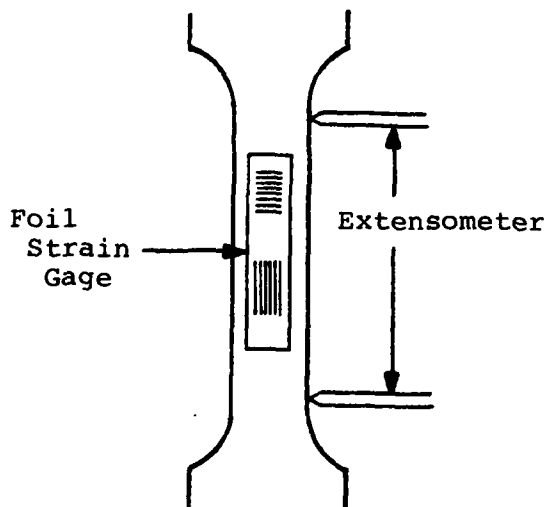


Figure 1. Specimen for Low and Intermediate Strain Rate Tests.



Specimen instrumented
for axial strain and
displacement
measurement



Specimen instrumented
for axial strain and
displacement measure-
ments and transverse
strain measurements

Figure 2. Location of Measurement Instrumentation on the Low and Intermediate Strain Rate Specimens.

2.1.2.2 Test Procedure

After tightening the strain gaged specimen in the grips, the extensometer was attached and adjusted to give the proper output voltage for the desired gage length. With the test machine in the load control mode a linear ramp function loaded the specimen to failure. Load and displacement were recorded directly on the system X-Y recorder for the lowest strain rate tests (10^{-3} strain/second). Load and strain were recorded directly on the additional X-Y recorder. For the higher strain rate tests (10^{-1} and 1 strain/second) the three parameters, load, strain, and displacement were recorded on three channels of the transient recorder for playback at slower speeds into the X-Y recorder.

2.2 HIGH STRAIN RATE TESTS

Mechanical properties obtained from the high strain rate tests include the following three plastic parameters: the yield stress, the ultimate stress, and the ultimate strain. Plastic region true stress-true strain curves were also acquired from the tests. (Elastic properties cannot be obtained from these tests because the pressure waves in the Hopkinson bar are not considered to be in equilibrium in the elastic region). The method (and apparatus) used is the same as that used in a study of the high strain rate tensile mechanical properties study of beryllium.⁽⁵⁾ The subsequent paragraphs provide a detailed description of the experimental apparatus, the instrumentation, and the test procedures and mechanisms. The analysis section of this report contains the brief explanation of the data reduction process. The results appear in Appendix B.

2.2.1 Experimental Apparatus

A schematic of the split Hopkinson bar apparatus and the associated instrumentation appears in Figure 3. Three parts of the apparatus are of major interest: two Hopkinson pressure bars (bar No. 1 and bar No. 2) and the striker bar.

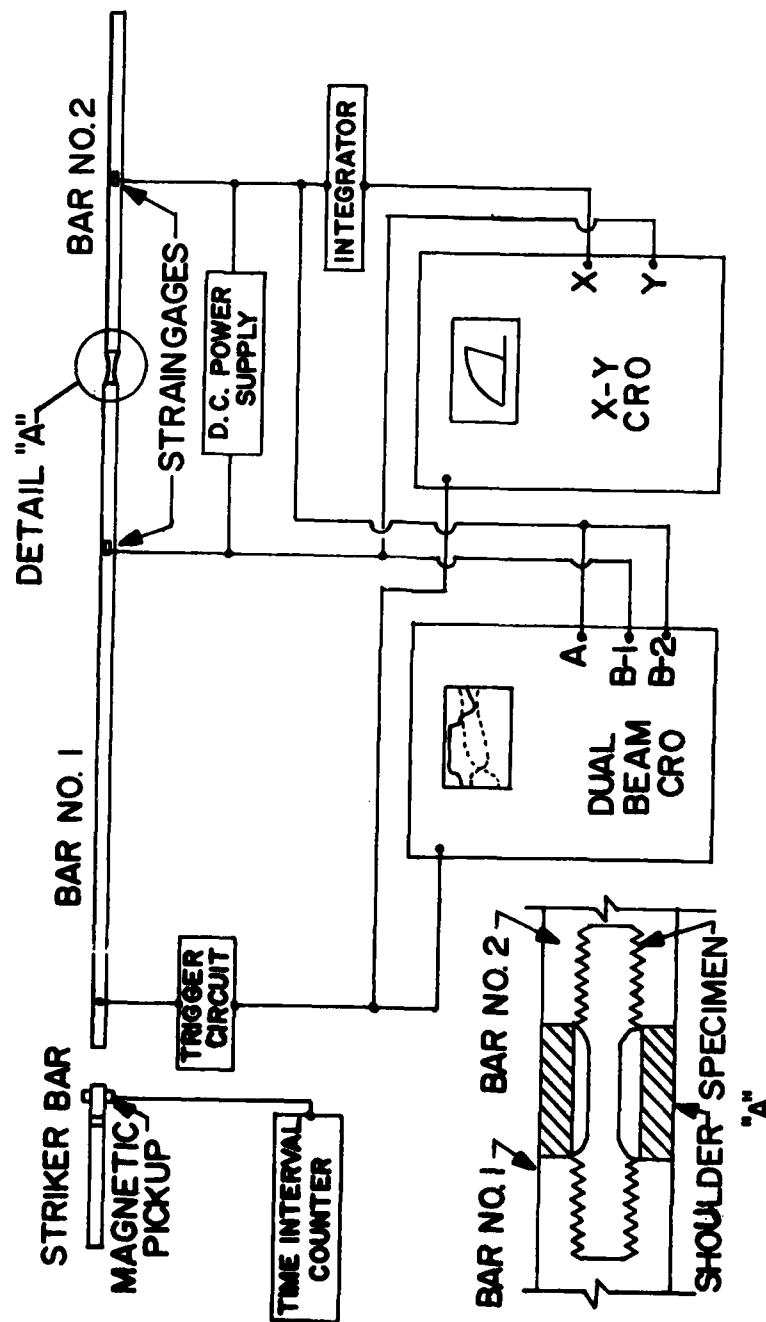


Figure 3. Schematic of Apparatus and Instrumentation for High Strain Rate Tests.

Bar No. 1 must be twice the length of bar No. 2 and the striker bar must be shorter than bar No. 2. For these experiments the bars are 0.06, 0.15, and 0.30 m lengths of 12.7 mm diameter AISI 4130 steel. They are mounted and aligned on a rigid base.

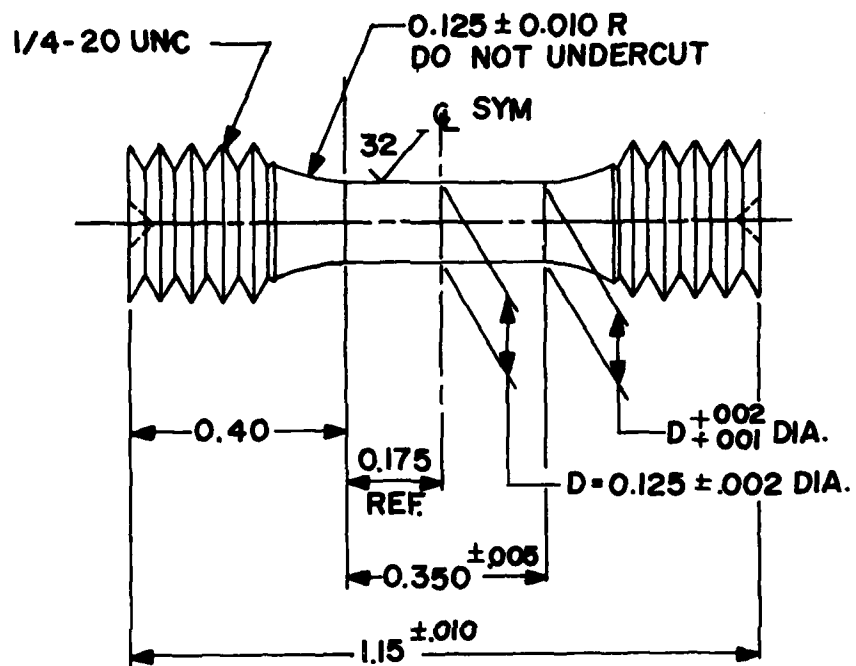
Detail "A" of Figure 3 shows an enlargement of a longitudinal section of the apparatus at the location of the specimen. To prepare for the test, the threaded tensile specimen, shown in Figure 4, is screwed partially into the pressure bars. Then a split shoulder is placed over the specimen, and the specimen is screwed in until the shoulder is snug against the pressure bars. The shoulder has the same outer diameter as the pressure bars (12.7 mm) and it has an inner diameter of 6.4 mm, just large enough to clear the specimen. The shoulder is made of the same material as the pressure bars, AISA 4130 steel. The ratio of the cross-sectional area of the shoulder to that of the pressure bar is 3:4, while the ratio of the area of the shoulder to the net cross-sectional area of the specimen is 12:1.

2.2.2 Instrumentation

The recording circuitry consists primarily of strain gages, two oscilloscopes, and a counter. See Figure 3. The recording system is triggered when the striker bar impacts bar No. 1. A brief review of the major parts of the recording system follows.

Bars No. 1 and 2 are instrumented with high resistance foil strain gages. The gages on each bar are placed equidistant from the specimen so that the reflected and transmitted wave signals are time coincident. They are far enough from the specimen that no spurious reflections interfere with the pulses being recorded. Gages are placed diametrically opposite each other on the pressure bars to cancel bending.

The two oscilloscopes record data. One, a dual beam Tektronix type 565 oscilloscope, records the complete



NOTE: ALL DIMENSIONS IN INCHES

THREADED TENSION HOPKINSON BAR SPECIMEN

Figure 4. Specimen for High Strain Rate Tests.

strain time history of the test. One beam records the incident pulse as it passes the first gage. The second beam is used in chopped mode to record both the transmitted pulse (which is proportional to load) and the reflected pulse (which is proportional to strain rate). Figure 5(a) shows a photo of typical traces.

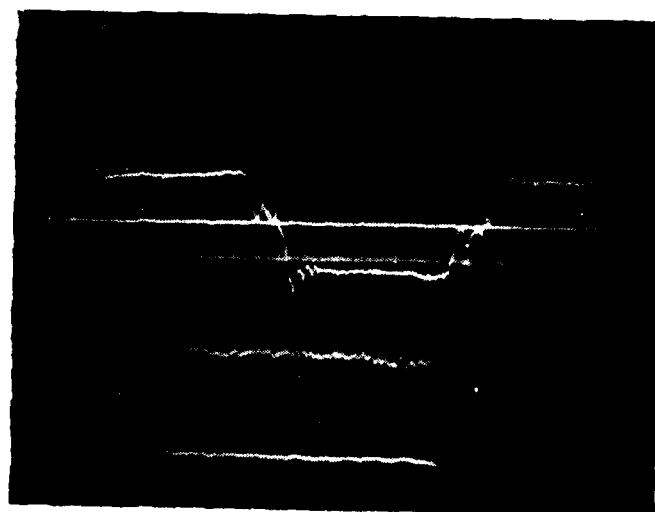
The second oscilloscope, an X-Y Tektronix, records a load-deflection curve. The reflected pulse (from gage No. 2) passes through an electronic integrator and is fed into the X axis of the scope. The signal is proportional to the displacement of the specimen. The signal from gage No. 1, proportional to the load in the specimen, is fed to the Y axis. Figure 5(b) shows the load-deflection trace.

2.2.3 Test Procedures and Mechanisms

The experiment begins when the striker bar is accelerated so that it impacts bar No. 1. The compression pulse generated travels down bar No. 1 to the specimen-shoulder junction. The pulse passes almost exclusively through the shoulder because of (1) the large area ratio of shoulder to specimen mentioned above and (2) the loose fit of the threaded joints (specimen and pressure bars). The portion of the pulse that passes through the specimen is below the elastic limit of the material. Then the compressive pulse travels through bar No. 2 to the free end, where it reflects as a tensile pulse. When this reflected pulse reaches the specimen, part of it is transmitted through the specimen and part is reflected back into bar No. 2 (because the shoulder doesn't carry the tensile pulse). The incident, transmitted and reflected pulses are recorded and analyzed for the required information.

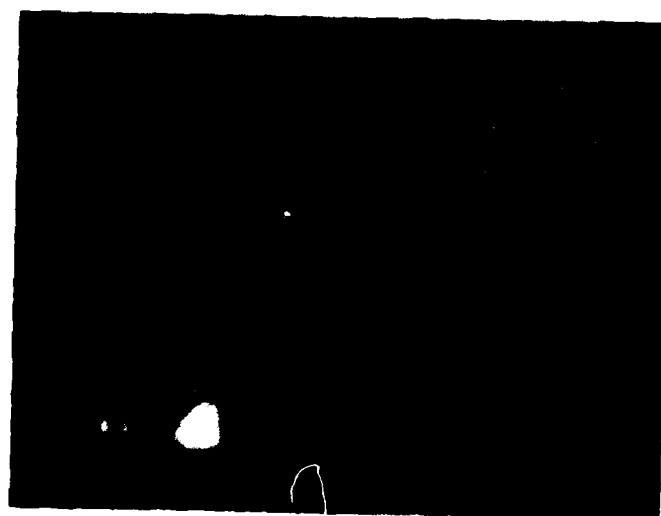
Figure 6 shows a Lagrangian x-t plot which illustrates the path of the pressure pulse during the test. The amplitude of the incident pressure pulse, generated by the striker bar impacting bar No. 1 is dependent on the striker bar velocity. Its length is twice the longitudinal elastic wave

E_i —
 E_r —
 E_t —



a

Specimen: Ti-3



b

Vert: 465 lb/div.
Horiz:
0.00155 in/div.

Figure 5. Typical Oscilloscope Traces.

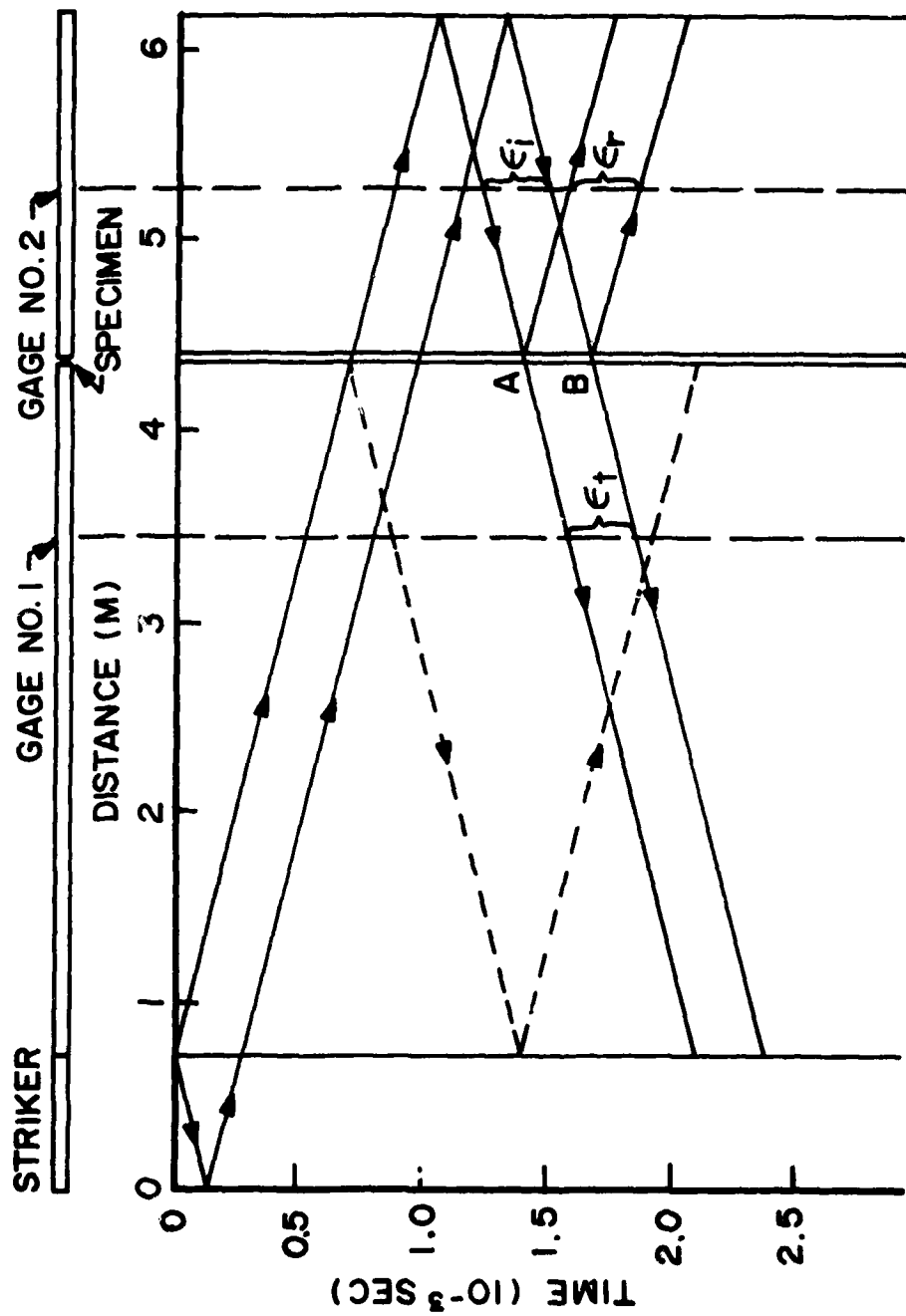


Figure 6. Lagrangian Displacement - Time Plot for High Strain Rate Tests.

transit time in the striker bar. The plot shows that the compressive pulse passes through the entire apparatus and is reflected from the free end of bar No. 2 as a tensile pulse, ϵ_i . The plot also illustrates the tensile pulse splitting when it reaches the specimen-shoulder junction and part of it, ϵ_t , being transmitted through the specimen while part, ϵ_r , is reflected back into bar No. 2.

SECTION III ANALYSIS

This section outlines the data reduction techniques and equations used to obtain the desired true stress-true strain curves and specific elastic and plastic parameters. All of the test data began as analog load-displacement curves that were then analyzed by various computer routines particular to the test type (low and intermediate, or high strain rate). The results appear in the appendices in analog and digital form.

3.1 LOW AND INTERMEDIATE STRAIN RATE TESTS

The low and intermediate strain rate tests resulted in (1) load-displacement curves from the extensometer and (2) load-strain curves from the strain gages. Converting the displacement measurement to true strain is relatively simple. Using u as displacement and l_0 as the initial gage length, one obtains the following:

$$\epsilon_E = \frac{u}{l_0} \quad (\text{engineering strain}) \quad (1)$$

$$\epsilon_T = \ln (1 + \epsilon_E) \quad (\text{true strain}) \quad (2)$$

where $\ln$ is the natural logarithm.

The extensometer gage length, l_0 , was 1 inch for these tests. Consequently, the digitized displacement value could be used directly in calculations as engineering strain.

The strain gage data was also simple to reduce. A correction factor was applied to the strain reading to account for the nonlinearity of the bridge circuit. The incremental error, n , is added to the indicated, $\hat{\epsilon}$, to obtain the actual strain, ϵ , causing the resistance change in the gage. For this case, a single active gage in a quarter-bridge arrangement, the

correction is

$$n = \frac{F (\hat{\epsilon})^2 \times 10^{-6}}{2 - F (\hat{\epsilon}) \times 10^{-6}} \quad (3)$$

where F is the gage factor. Equation 2 is then used to obtain true strain.

Obtaining true stress values for the low and intermediate strain rate tests is more complicated. True stress, σ_T , is proportional to engineering stress, σ_E , by the ratio of the initial area, A_0 , to the current area, A . In the elastic region, where one has small strains, the ratio of areas can be expressed in terms of the longitudinal engineering strain so that

$$\sigma_T = \frac{\sigma_E (1 + \epsilon_E)}{1 + \epsilon_E (1 - 2\nu)} \quad \begin{matrix} \text{(elastic region} \\ \text{true stress)} \end{matrix} \quad (4)$$

In the plastic region one assumes the material is incompressible, consequently the volume remains constant. Based on this assumption the true stress in the plastic region becomes

$$\sigma_T = \frac{\sigma_E (1 + \epsilon_E)}{1 + \bar{\epsilon}_E (1 - 2\nu)} \quad \begin{matrix} \text{(plastic region} \\ \text{true stress)} \end{matrix} \quad (5)$$

where $\bar{\epsilon}_E$ is the engineering strain evaluated at the yield point of the material.

Three elastic region parameters were calculated from the strain gage data. Young's modulus is the slope of the linear part of the curve. Poisson's ratio, ν , was obtained for one test per material per strain rate with the following relationship:

$$\nu = +\epsilon_{\text{transverse}} / \epsilon_{\text{longitudinal}}$$

The shear modulus, G , was calculated with the equation

$$G = \frac{E}{2(1 + \nu)}$$

The values of these mechanical properties appear in the results section. An additional parameter, the yield stress, was obtained from these curves. It was evaluated using the 0.2 percent (strain) offset method because neither of the metals exhibits a definite yield point. The load-displacement curves were analyzed using Equations 2, 4, and 5 to produce the full true stress-time strain curves. The ultimate strain was taken as the final strain value of the curve. However, the ultimate stress was calculated using the final load divided by the final reduced area of the specimens because Equation 5 is not accurate (complete) for large amounts of plasticity.

These curves were all digitized on the University of Dayton's Tektronix 4014-1 computer graphics terminal and associated digitizing board.

3.2 HIGH STRAIN RATE TESTS

The polaroid photographs of the load-deflection traces obtained from the high strain rate tests were digitized using a Hewlett Packard 9800 series calculator and digitizer (located at the AFML) to produce true stress-engineering strain curves. Those curves were then digitized on the Tektronix 4014-1 computer graphics terminal and digitizing board (located at the University) to produce true stress-true strain curves. A brief review of the analysis in the two data reduction programs follows. Details of the theory of the measurements appear in documents by U. S. Lindholm⁽⁶⁾ and by Lindholm and L. M. Yeakley.⁽⁷⁾

The average stress in the specimen is:

$$\sigma_s = E (A/A_s) \epsilon_t \quad (6)$$

where E and A are the elastic modulus and cross-sectional area of the pressure bars, A_s is the cross-sectional area of the specimen and ϵ_t is the transmitted wave. Using the assumption of no volume change after first yield, Equation (6) is modified to:

$$\sigma_T = E(A/A_s) \epsilon_t \frac{1}{(1 + \epsilon_t)} \quad (7)$$

for true stress.

Engineering strain was obtained from the deflection values using the following relationship:

$$\epsilon = 0.265 \delta - 0.5 (1 - \exp^{-0.55 \delta})$$

where ϵ represents strain in percent and δ represents the deflection in mils between the grips.⁽⁵⁾ This equation results from least-squares fitting many deflection-strain plots from several different materials. It is particular to the specimen size used, not to a material.

The yield stress was determined as the point on the stress-strain curve at which the increase in applied load essentially ceased. The ultimate stress and ultimate strain were selected as the final point on the stress-strain curve. Reasons for this selection procedure appear in the results and discussion section.

SECTION IV

RESULTS AND DISCUSSION

The mechanical properties acquired from the various strain rate tests on 8Al-1Mo-1V titanium and 410 stainless steel appear in Tables 2 and 3, respectively. Table 4 shows the measured density of each material. Figures 7 through 10 are plots of the mechanical properties versus strain rate. The points lacking standard deviation marks either represent one data point or they represent averaged data having a standard deviation smaller than the data symbol. The true stress-true strain curves for the low and intermediate tests (Appendix A) have two parts to the curve in the plastic region. The solid line represents the test data analyzed with the plastic region equations given in the analysis section. Obviously these are not complete for large strains. The dotted line joins the ultimate stress (calculated with the final load and reduced cross-sectional area)-ultimate strain point to the test curve.

Studying Figures 7 through 10, one concludes that all of the tensile mechanical properties determined by these tests vary with strain rate with the exception of the elastic modulus of titanium. Perhaps additional testing of the stainless steel would reveal that its elastic modulus also does not vary with strain rate. It is important to consider the comments in the following paragraphs when using the curves shown as data for calculations.

A very small specimen must be used for high strain rate tests to satisfy assumptions made in the Hopkinson bar theory equations. This presents problems in obtaining accurate data from the tests, particularly in the elastic region. One problem is that achievable machining tolerances on the specimen in relation to load surface alignment make it difficult to resolve small strains accurately. Secondly, an assumption made in developing the Hopkinson bar equations is that many stress

TABLE 2
MECHANICAL PROPERTIES OBTAINED FOR 8Al-1Mo-1V TITANIUM

Specimen	Strain Rate (ϵ/sec)	Elastic Modulus ($\times 10^6$ psi)	Shear Modulus ($\times 10^6$ psi)	Yield Stress (ksi)	Ultimate Stress (ksi)	Ultimate Strain (percent)
1-Ti	0.001	16.9	6.5	148.9	202.5	28.2
2-Ti	0.001	17.3	6.7	148.7	200.8	27.2
3-Ti	0.001	17.4	6.8	148.7	199.3	21.8
4-Ti	0.10	15.8	6.3	156.3	188.5	13.7
5-Ti	0.10	16.9	6.8	153.0	189.1	15.9
6-Ti	0.10	17.1	6.8	156.4	194.5	15.3
7-Ti	1.0	17.3	6.8	164.0	184.6	15.7
Ti-3	550	*	*	203.0	161.1	13.7
Ti-2	560	*	*	202.0	154.2	14.5
Ti-1	580	*	*	208.0	158.7	15.3

Poisson's Ratio = 0.279

* Elastic properties are not obtainable from the high strain rate tests.

TABLE 3
MECHANICAL PROPERTIES OBTAINED FOR 410 STAINLESS STEEL

Specimen	Strain Rate (ϵ/sec)	Elastic Modulus ($\times 10^6$ psi)	Shear Modulus ($\times 10^6$ psi)	Yield Stress (ksi)	Ultimate Stress (ksi)	Ultimate Strain (percent)
4-SS	0.001	27.4	10.6	84.2	207.2	26.7
5-SS	0.001	30.5	11.7	84.8	207.2	27.2
6-SS	0.001	33.7	12.9	84.9	211.9	26.9
9-SS	0.10	27.7	11.2	87.2	191.9	25.7
10-SS	0.10	26.4	10.2	87.0	188.3	26.8
11-SS	0.10	28.2	10.9	89.2	198.3	23.5
12-SS	1.0	27.2	10.4	86.6	182.7	23.8
13-SS	1.0	26.1	10.0	91.3	185.5	25.4
14-SS	1.0	27.2	10.4	94.5	183.8	24.6
15-SS	1.0	28.0	10.9	88.8	184.7	25.6
SS-5	680.0	*	*	124.0	129.5	16.9
SS-4	760.0	*	*	123.0	130.0	17.2
SS-3	700.0	*	*	131.0	131.4	18.0
SS-2	530.0	*	*	128.0	**	**
SS-1	340.0	*	*	126.0	**	**

Poisson's Ratio = 0.297

* Elastic properties are not obtainable from the high strain rate tests.

** These specimens did not fail.

TABLE 4
DENSITY

Material	Density
8Al-1Mo-1V Titanium	4.32 g/cm ³
410 Stainless Steel	7.57 gm/cm ³

wave reflections occur in the specimen before a state of dynamic equilibrium exists. This does not happen until some plastic deformation has taken place. In addition, once necking occurs in the specimen a uniform stress field no longer exists making the equations for stress and strain invalid. This is a significant factor for the small specimens.

However, the split-Hopkinson bar apparatus represents the state-of-the-art technique for obtaining stress-strain information at high strain rates. The curves are considered most accurate in the range of 2 to 10 percent strain. The yield stress values reported represent the point on the curves where the load ceases to increase significantly for a rather large increase in displacement. (The 0.2 percent offset method obviously cannot be used because of the lack of data in the elastic region.) The ultimate stress and ultimate strain values from these tests were the final point of the curve. Although the values from the high strain rate tests cannot be used as exact data points they are useful in establishing the trend of the strain rate dependence of the subject materials over nearly seven decades of strain rate.

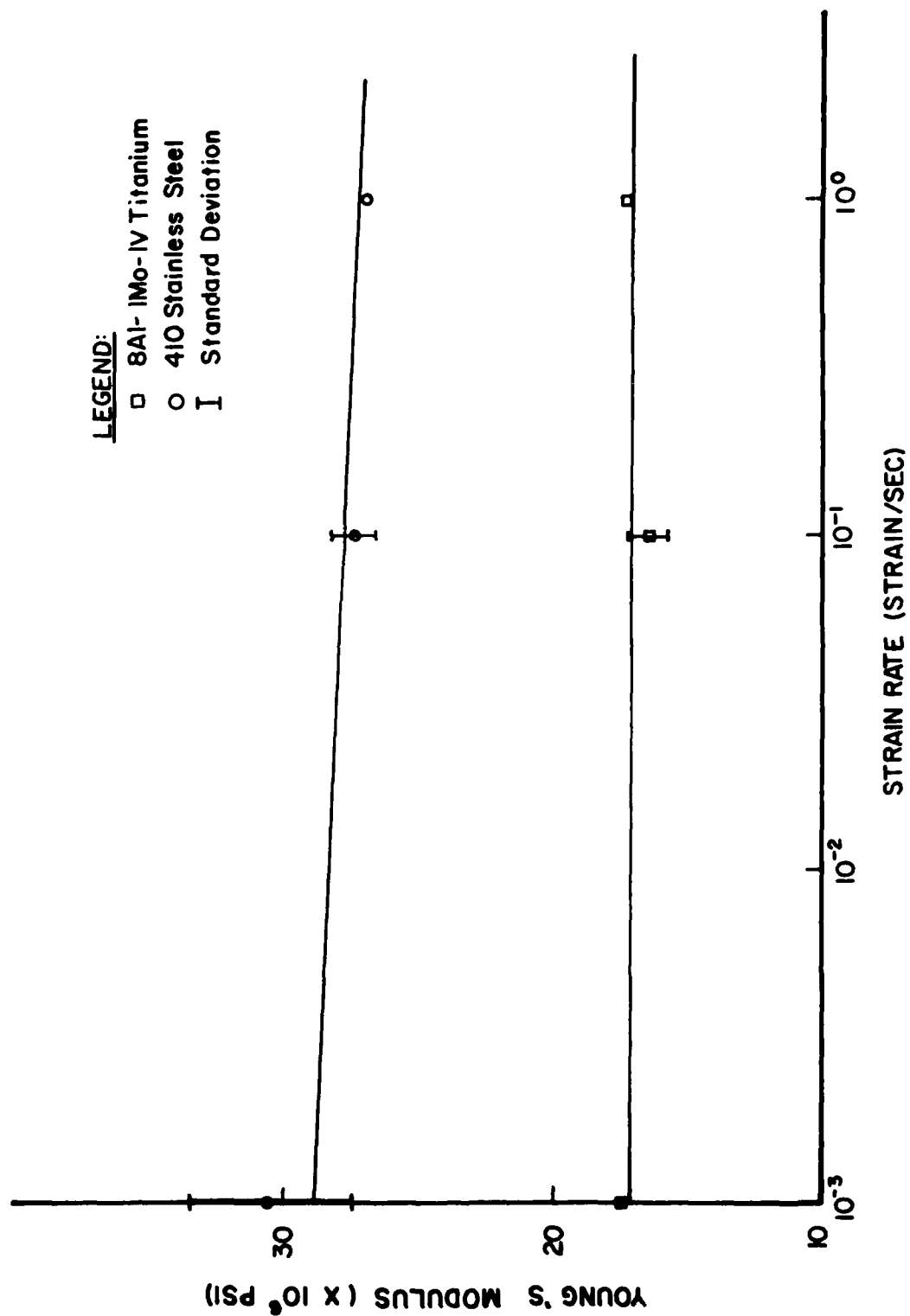


Figure 7. Young's Modulus VS. Strain Rate.

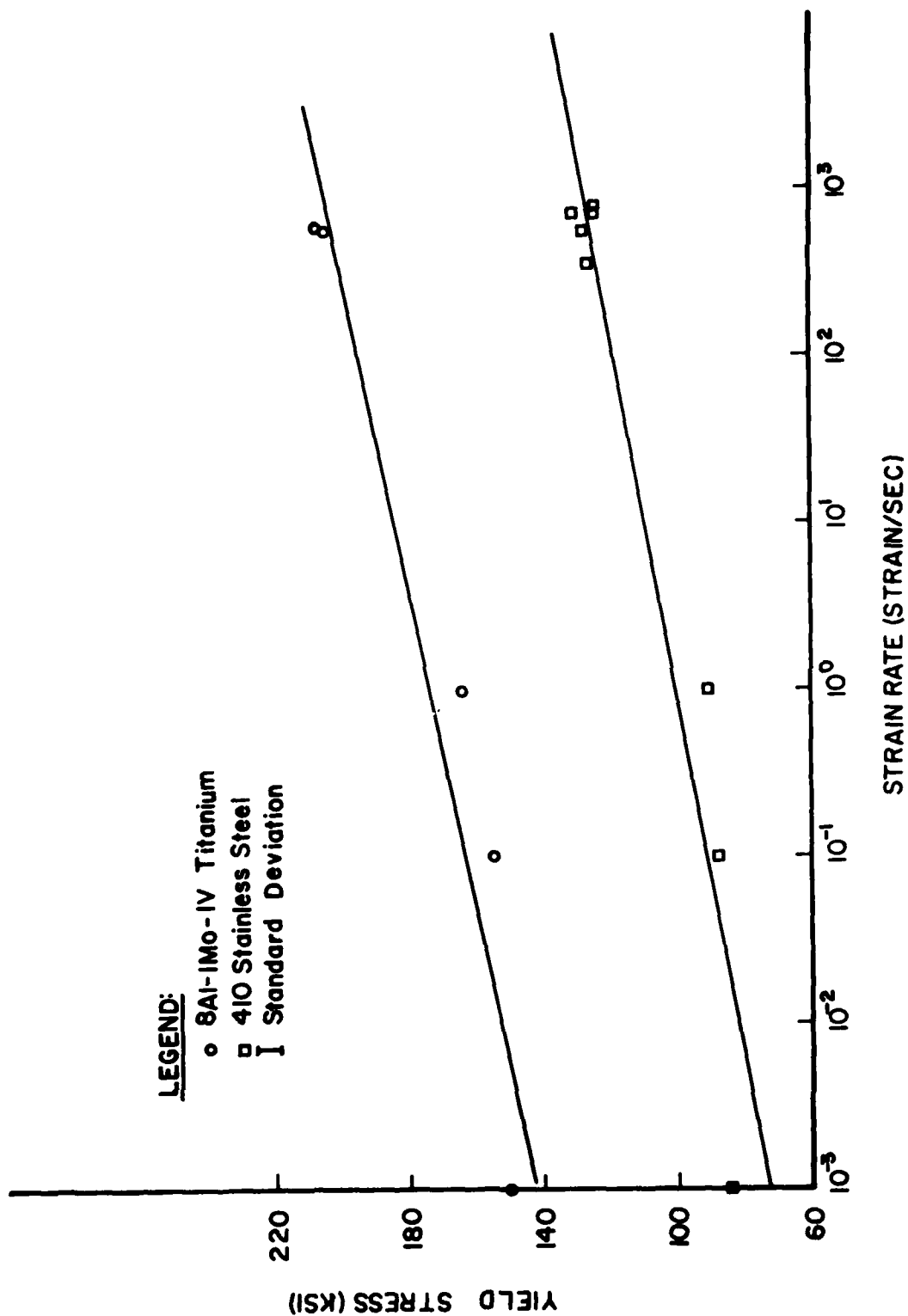


Figure 8. Yield Stress VS. Strain Rate

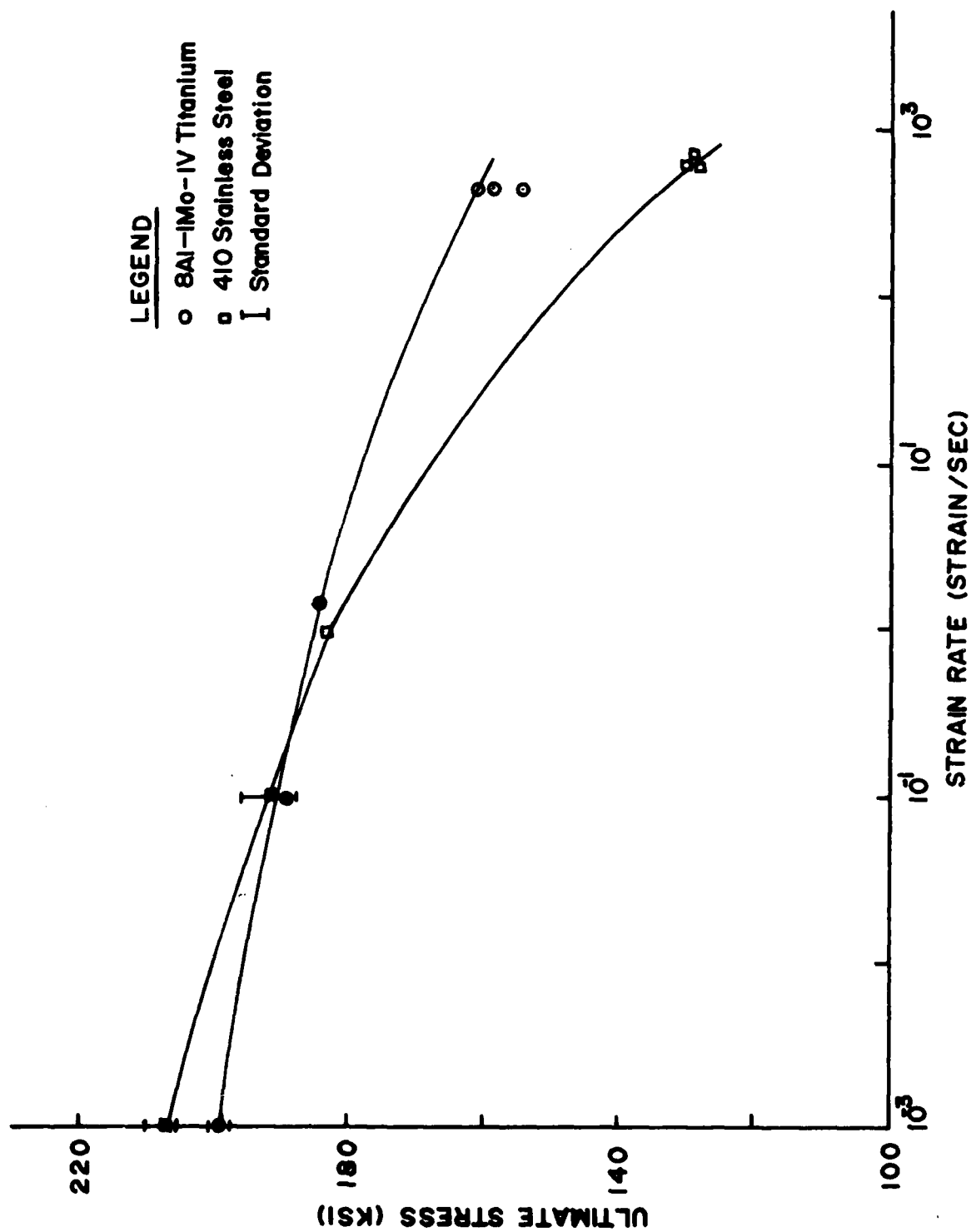


Figure 9. Ultimate Stress VS. Strain Rate.

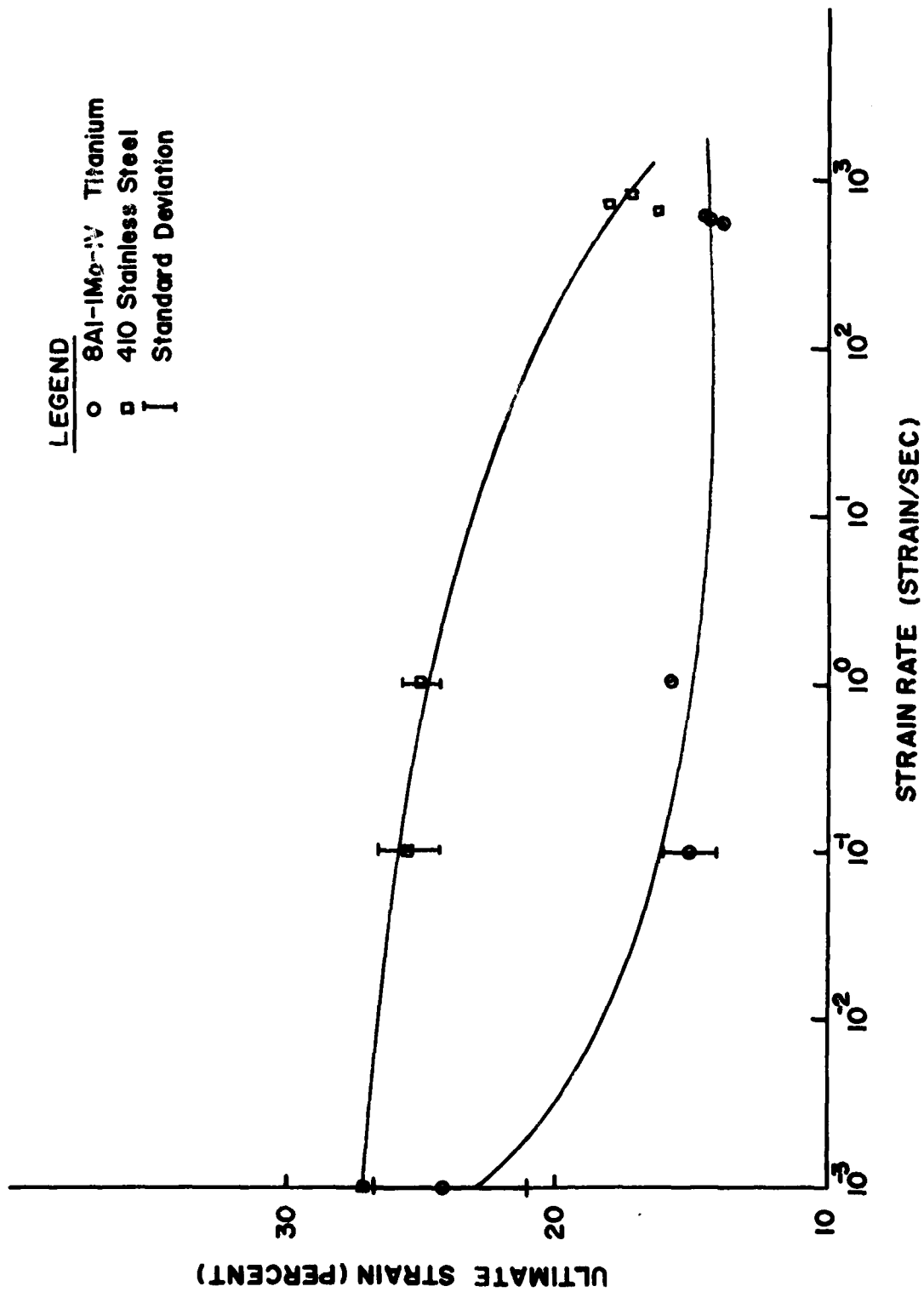


Figure 10. Ultimate Strain VS. Strain Rate.

REFERENCES

1. Mardirosian, M.M., "Strain Rate Effects in Brittle and Tough Materials," AMMRC-TR-74-34, December 1974.
2. Green, S.J. and S.G. Babcock, "Response of Materials to Suddenly Applied Stress Loads: Part I: High Strain-rate Properties of Eleven Reentry-vehicle Materials at Elevated Temperatures," TR66-83 Part I, November 1966.
3. Eleiche, Abdel-Salam M., "A Literature Survey of the Combined Effects of Strain Rate and Elevated Temperature on the Mechanical Properties of Metals," AMFL-TR-72-125, September 1972.
4. 1977 Annual Book of American Society for Testing and Materials Standards, Part 10: Metals Physical, Mechanical, Corrosion Testing, pp. 154-173.
5. Nicholas, T., "Mechanical Properties of Structural Grades of Beryllium at High Strain Rates," AFML-TR-75-168, October 1975.
6. Lindholm, U.S., "Some Experiments with the Split Hopkinson Pressure Bar," Journal of the Mechanics and Physics of Solids, 1964, Vol. 12, pp. 317-335.
7. Lindholm, U.S. and L.M. Yeakley, "High Strain-rate Testing: Tension and Compression, Experimental Mechanics, January 1968, pp. 2-9.

APPENDIX A

LOW AND INTERMEDIATE STRAIN RATE
CURVES AND DIGITAL DATA

STANDARD TENSILE		
0.001 STRAIN/SEC		
BAL-100-1U TITANIUM		
SPEC 1-T1		
1	.05808615	192.067
2	.13095612	191.729
3	.19177013	190.561
4	.25369049	189.072
5	.31774354	187.072
6	.39414203	185.434
7	.45869500	183.240
8	.51532190	180.949
9	.58442455	178.494
10	.66065961	177.242
11	.72509252	174.751
12	.79313489	172.950
13	.86556287	171.913
14	.92657194	
15	1.00219249	
16	1.11203352	
17	1.24609528	
18	1.39599318	
19	1.60598576	
20	1.79960876	
21	1.98463584	
22	2.16923089	
23	2.31751753	
24	2.51358850	
25	2.69730043	
26	2.91653145	
27	3.32579162	
28	3.54787803	
29	3.70994237	
30	3.89999825	
31	4.03346633	
32	4.21056616	
33	4.4237782	
34	4.63441857	
35	4.81654619	
36	4.98636415	
37	5.16559302	
38	5.34476368	
39	5.51947106	
40	5.6437597	
41	5.76375881	
42	18.36507948	
43	19.06724825	
44	19.86094865	
45	20.42284516	
46	20.80217157	
47	21.35157297	
48	21.89759880	
49	22.35689507	
50	22.81458814	
51	23.50988873	
STANDARD TENSILE		
0.001 STRAIN/SEC		
BAL-100-1U TITANIUM		
SPEC 2-T1		
1	.03439573	4.748
2	.06333684	10.304
3	.13626456	20.631
4	.19605711	30.739
5	.26735502	42.304
6	.36057480	58.211
7	.46522603	66.695
8	.52186549	75.591
9	.58173847	84.093
10	.63623282	93.835
11	.68336169	101.921
12	.73925781	109.409
13	.81140866	118.749
14	.87203732	128.750
15	.92116468	137.296
16	.97227816	144.385
17	1.0306337	148.820
18	1.0983378	150.428
19	1.20642624	149.593
20	1.36910988	149.061
21	1.52336818	149.394
22	1.70183256	149.495
23	1.8857076	150.296
24	2.0703259	150.713
25	2.3588535	151.784
26	2.54064246	152.769
27	2.70497600	153.328
28	2.9225051	154.006
29	3.1940427	154.840
30	3.26630093	155.098
31	3.41766243	156.023
32	3.5612205	156.127
33	3.72316532	156.817
34	3.857197	157.188
35	4.0425547	157.755
36	4.1390316	157.887
37	4.3982825	158.342
38	4.49355161	159.208
39	4.65903757	159.344
40	4.79191517	159.417
41		159.882

42	4.93667146	160.403	16.59235611	181.252
43	5.07349043	160.465	17.06298561	182.832
44	5.23000791	160.810	17.55088489	183.978
45	5.36627842	161.085	18.23478545	185.110
46	5.49437230	161.330	18.86348576	185.137
47	5.59835558	161.490	19.23840876	185.293
48	5.72201868	161.936	19.68592785	184.3285
49	5.76194818	161.937	20.09767138	182.884
50	5.79390030	161.980	20.71079176	180.538
51	5.79375274	162.140	20.71079176	177.843
52	17.39831956	182.551	21.05273283	174.627
53	17.91841989	183.520	21.2692783	172.109
54	18.5239766	184.941	21.43361443	169.461
55	19.23438722	185.642	21.68670513	165.992
56	19.65889960	185.420	21.9839834	163.207
57	20.12050715	184.534	STANDARD TENSILE	
58	20.49362849	183.179	0.001 STRAIN/SEC	
59	20.84923062	180.527	410 STRAINLESS STEEL	
60	21.16870509	178.270	SPEC 4-SS	
61	21.45459210	175.166	1	0.1040279
62	21.66894962	172.637	2	0.20522039
63	21.85567641	170.057	3	0.3824873
64	22.05201694	167.465	4	0.5214512
65	22.18952346	164.712	5	0.6627623
			6	0.8049998
			7	1.0195010
			8	1.1238959
			9	1.1876524
			10	1.3340770
			11	1.3780426
			12	1.4766870
			13	1.5551635
			14	1.6350264
			15	1.6780426
			16	1.7808040
			17	1.8766870
			18	1.9551635
			19	2.0340770
			20	2.1127623
			21	2.1915010
			22	2.2702910
			23	2.3490426
			24	2.4277910
			25	2.5065426
			26	2.5852910
			27	2.6640426
			28	2.7427910
			29	2.8215426
			30	2.9002910
			31	2.9790426
			32	3.0577910
			33	3.1365426
			34	3.2152910
			35	3.2940426
			36	3.3727910
			37	3.4515426
			38	3.5302910
			39	3.6090426
			40	3.6877910
			41	3.7665426
			42	3.8452910
			43	3.9240426
			44	4.0027910
			45	4.0815426
			46	4.1602910
			47	4.2390426
			48	4.3177910
			49	4.3965426
			50	4.4752910
			51	4.5540426
			52	4.6327910
			53	4.7115426
			54	4.7902910
			55	4.8690426
			56	4.9477910
			57	5.0265426
			58	5.1052910
			59	5.1840426
			60	5.2627910
			61	5.3415426
			62	5.4202910
			63	5.4990426
			64	5.5777910
			65	5.6565426
			66	5.7352910
			67	5.8140426
			68	5.8927910
			69	5.9715426
			70	6.0502910
			71	6.1290426
			72	6.2077910
			73	6.2865426
			74	6.3652910
			75	6.4440426
			76	6.5227910
			77	6.6015426
			78	6.6802910
			79	6.7590426
			80	6.8377910
			81	6.9165426
			82	6.9952910
			83	7.0740426
			84	7.1527910
			85	7.2315426
			86	7.3102910
			87	7.3890426
			88	7.4677910
			89	7.5465426
			90	7.6252910
			91	7.7040426
			92	7.7827910
			93	7.8615426
			94	7.9402910
			95	8.0190426
			96	8.0977910
			97	8.1765426
			98	8.2552910
			99	8.3340426
			100	8.4127910

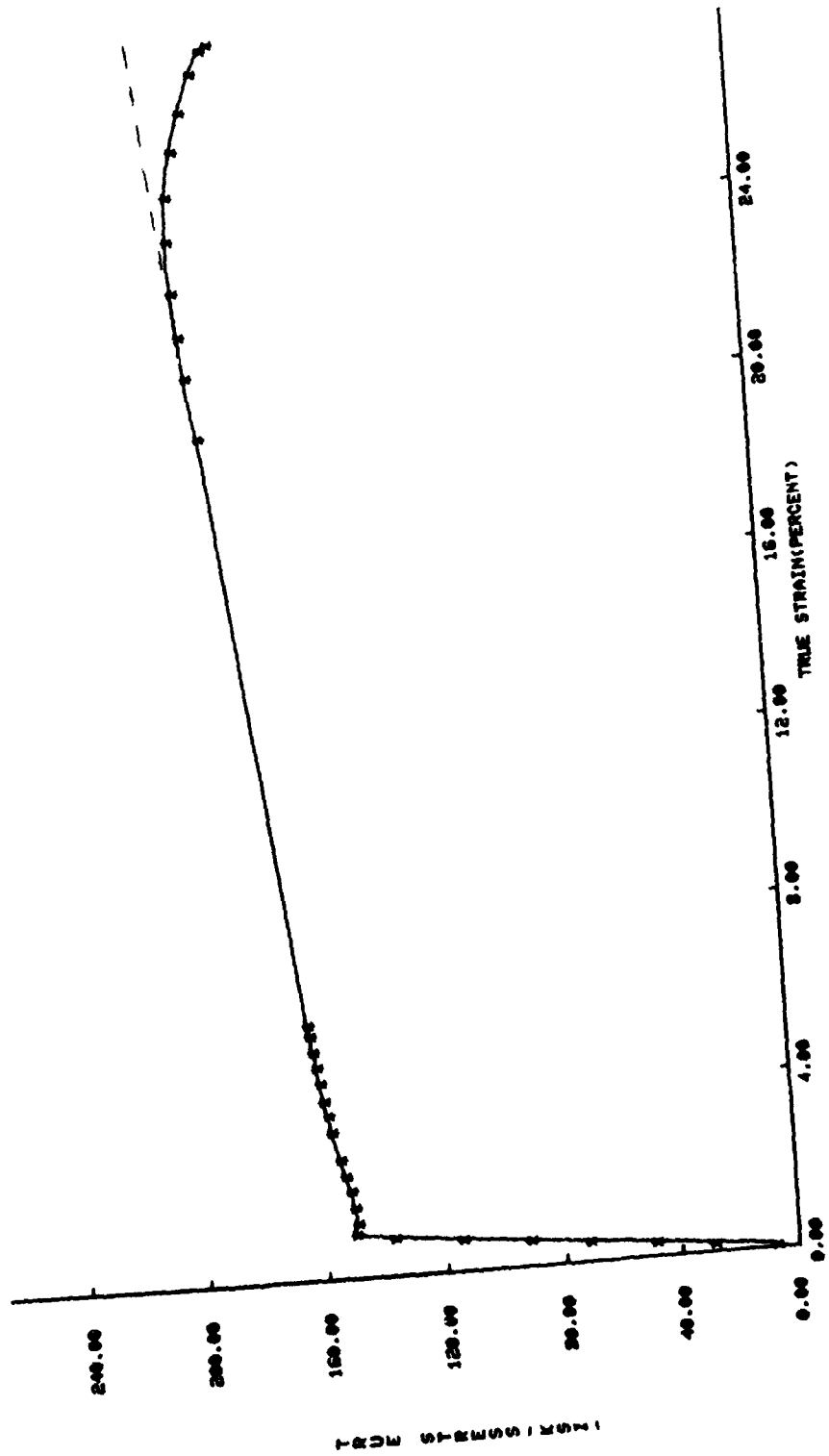
40	3.76963872	99.075	12	.15589810	48.009
41	3.98366369	99.358	13	.17658406	52.500
42	4.19333104	99.848	14	.19725574	56.991
43	4.40654272	99.919	15	.21397040	61.483
44	4.64955454	100.244	16	.23867162	66.284
45	4.85035264	100.512	17	.27928581	71.295
46	4.97955455	100.685	18	.31165099	74.673
47	5.10730128	101.071	19	.36002250	78.875
48	5.20546652	101.204	20	.43092758	82.375
49	5.28457515	101.311	21	.51966323	84.959
50	5.35247392	101.188	22	.62694926	87.288
51	13.07582100	109.921	23	.76567796	89.339
52	13.52256977	110.347	24	.90803160	90.680
53	14.02848708	111.198	25	1.08165585	92.050
54	14.63027639	111.820	26	1.29826164	93.253
55	15.17977981	112.381	27	1.56525307	94.089
56	15.62951275	112.703	28	1.76896874	95.288
57	16.05324169	112.873	29	2.01512792	96.129
58	16.37870745	113.160	30	2.27632310	96.497
59	16.76333720	113.282	31	2.46682236	96.862
60	17.11053232	113.477	32	2.65318220	97.130
61	17.38495616	113.701	33	2.84686707	97.631
62	17.71812483	113.878	34	3.06724456	97.986
63	18.01485193	113.888	35	3.23702333	97.986
64	18.32234909	114.033	36	3.39881806	98.334
65	18.40532138	113.771	37	3.59876485	98.716
66	22.4866068	113.714	38	3.77144280	98.865
67	22.87003031	112.023	39	3.82260193	98.172
68	23.36579787	109.282	40	3.95528677	98.917
69	23.73560876	107.275	41	16.43805428	113.243
70	24.08849560	104.586	42	16.97730314	114.200
71	24.49019167	101.542	43	17.58484123	115.119
72	24.84140932	98.157	44	18.17075977	115.655
73	25.15865730	94.711	45	18.71789881	115.904
74	25.50890054	90.359	46	19.54194813	116.589
75	25.74152234	87.570	47	20.22035414	116.738
76	25.97413504	84.373	48	20.75633392	116.847
77	26.19025726	81.014	49	21.49479097	116.553
78	26.38861546	78.417	50	22.1427383	115.639
79	26.53849205	75.504	51	22.59968014	114.242
80	26.70388300	72.860	52	23.07143095	112.461
81	26.83546185	71.109	53	23.54088878	110.529
82	26.90233717	69.436	54	23.87460523	108.692
			55	24.33962043	105.551
			56	24.62045519	103.287
			57	24.9350716	100.728
			58	25.62243481	94.388
			59	25.89944867	91.215
			60	26.12703423	88.642
			61	26.32146874	86.030
			62	26.53158584	83.022
			63	26.75751277	80.013
			64	27.0880156	74.660
			65	27.19091102	72.605
			66	27.31920534	70.823
			67	27.30389613	70.545
				STANDARD TENSILE	
				0.001 STRAIN/SEC	
				410 STAINLESS STEEL	
				SPEC 5-55	
1	.02079219	4.888			
2	.02540123	8.352			
3	.03776667	10.695			
4	.04217153	13.038			
5	.04672419	16.197			
6	.06334312	20.069			
7	.06809804	24.350			
8	.07668326	27.815			
9	.10178791	34.645			
10	.12646144	39.134			
11	.13914681	43.316			

410 STAINLESS STEEL
SPEC 6-SS

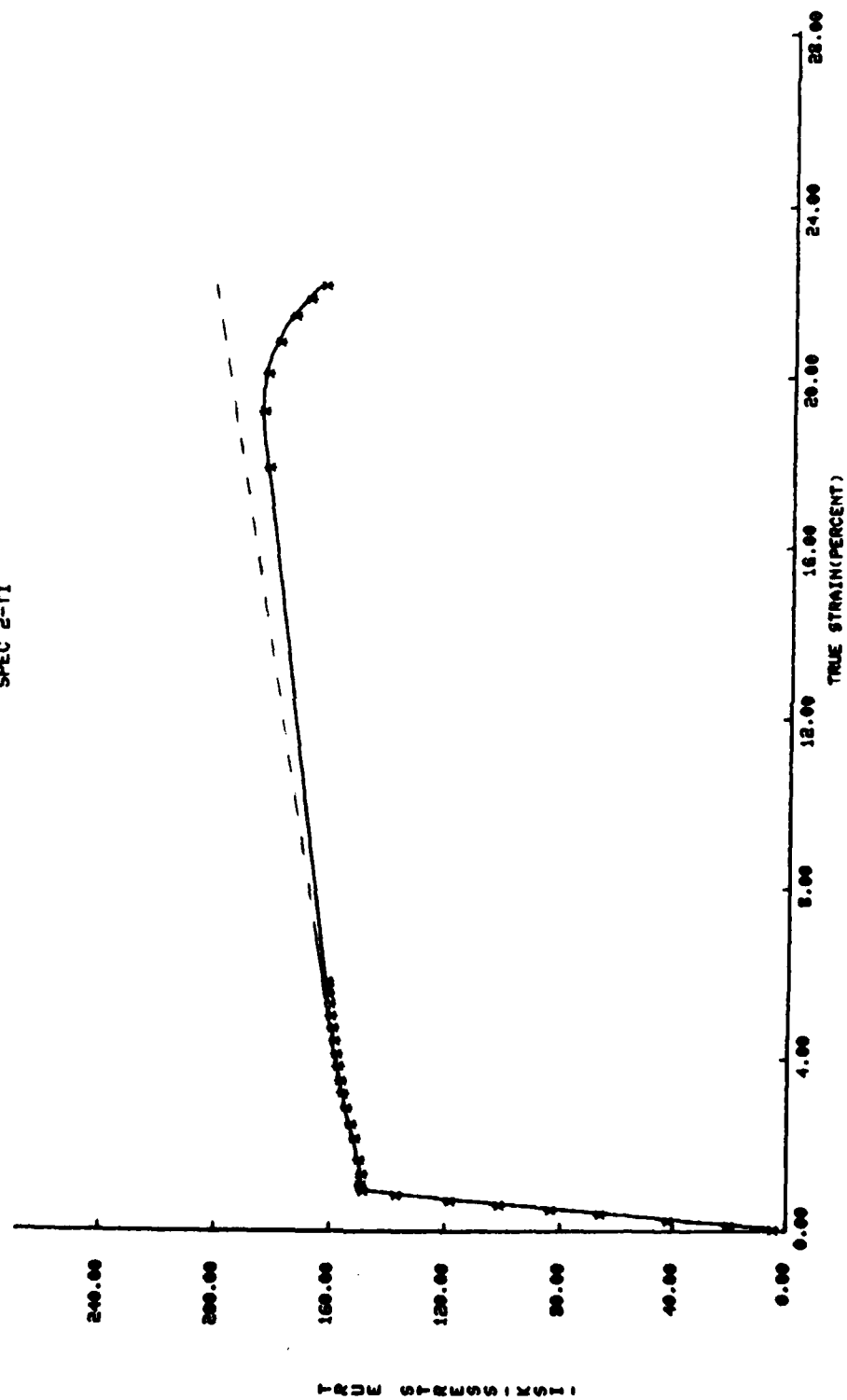
1 1.016
2 3.968
3 7.122
4 10.885
5 14.854
6 19.341
7 24.214
8 29.912
9 36.835
10 41.926
11 48.240
12 54.047
13 59.346
14 63.729
15 68.318
16 72.705
17 75.768
18 79.961
19 83.138
20 85.513
21 87.603
22 89.284
23 90.610
24 90.914
25 92.237
26 93.699
27 94.172
28 94.861
29 95.841
30 96.393
31 96.719
32 97.531
33 97.861
34 98.174
35 98.632
36 98.765
37 99.125
38 99.212
39 99.434
40 99.762
41 100.058
42 100.349
43 100.486
44 114.734
45 115.354
46 116.228
47 116.678
48 117.037
49 117.003
50 117.075
51 116.890
52 115.861
53 113.958
54 112.476
55 109.809
56 107.222

1 104.057
2 101.559
3 97.990
4 95.005
5 90.331
6 86.596
7 83.859
8 80.356
9 77.077
10 73.863
11 70.886
12 66.875
13 62.875
14 58.875
15 54.875
16 50.875
17 46.875
18 42.875
19 38.875
20 34.875
21 30.875
22 26.875
23 22.875
24 18.875
25 14.875
26 10.875
27 6.875
28 2.875
29 0.875
30 0.875
31 0.875
32 0.875
33 0.875
34 0.875
35 0.875
36 0.875
37 0.875
38 0.875
39 0.875
40 0.875
41 0.875
42 0.875
43 0.875
44 0.875
45 0.875
46 0.875
47 0.875
48 0.875
49 0.875
50 0.875
51 0.875
52 0.875
53 0.875
54 0.875
55 0.875
56 0.875

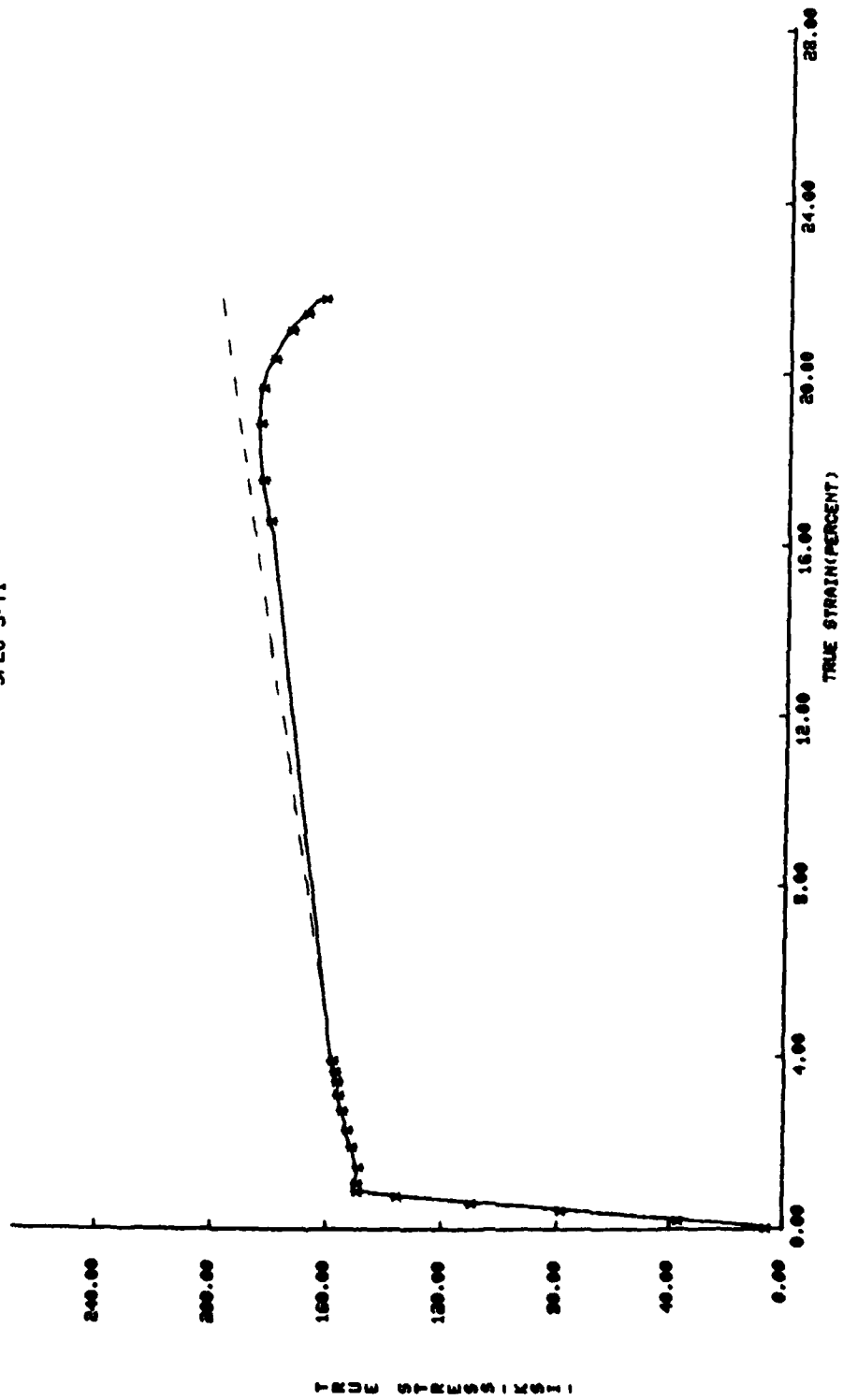
STANDARD TENSILE
0.001 STRAIN/SEC
BAL-100-10 TITANIUM
SPEC 1-T1



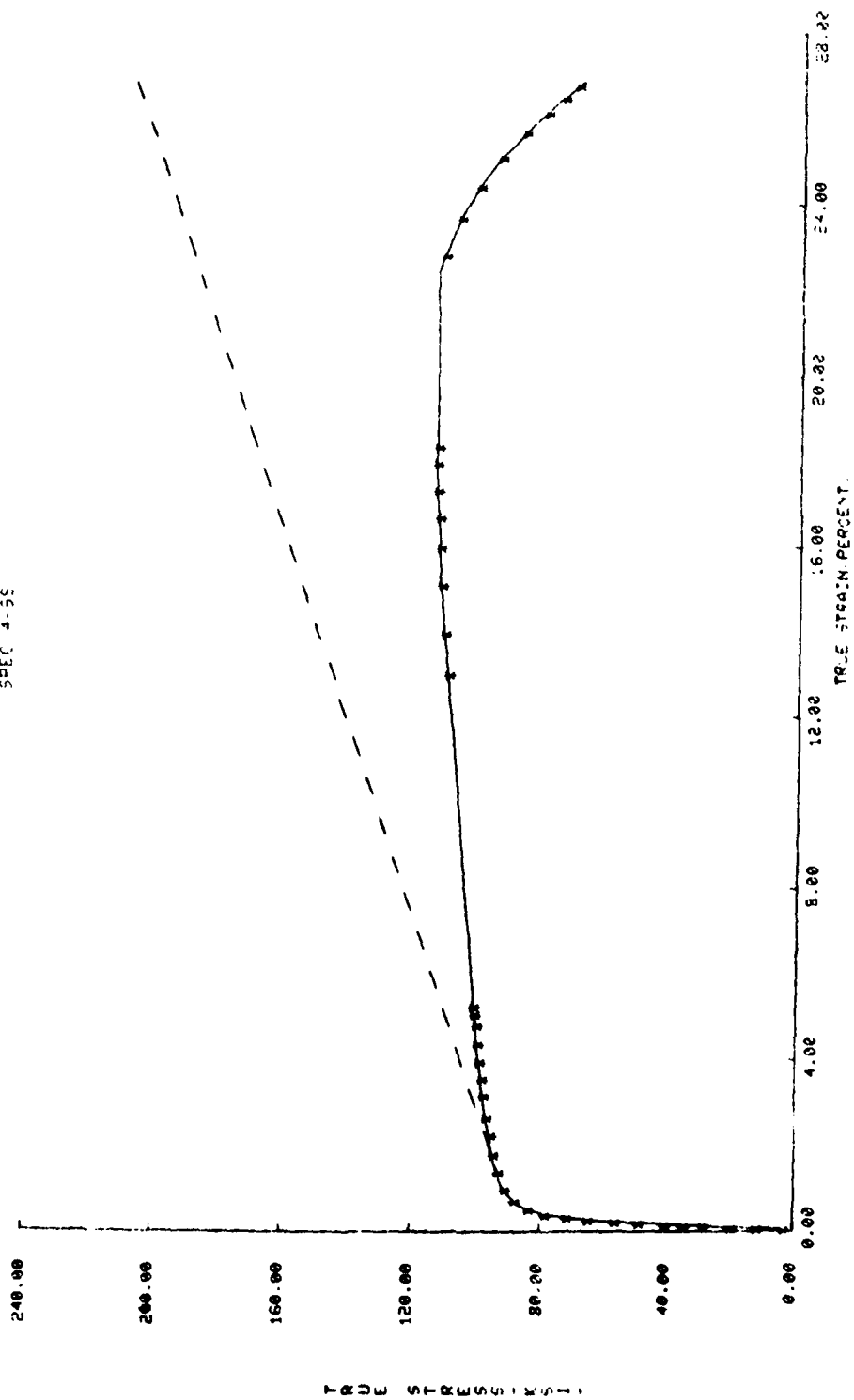
STANDARD TENSILE
0.001 STRAIN/SEC
BAL-INO-10 TITANIUM
SPEC 2-TI



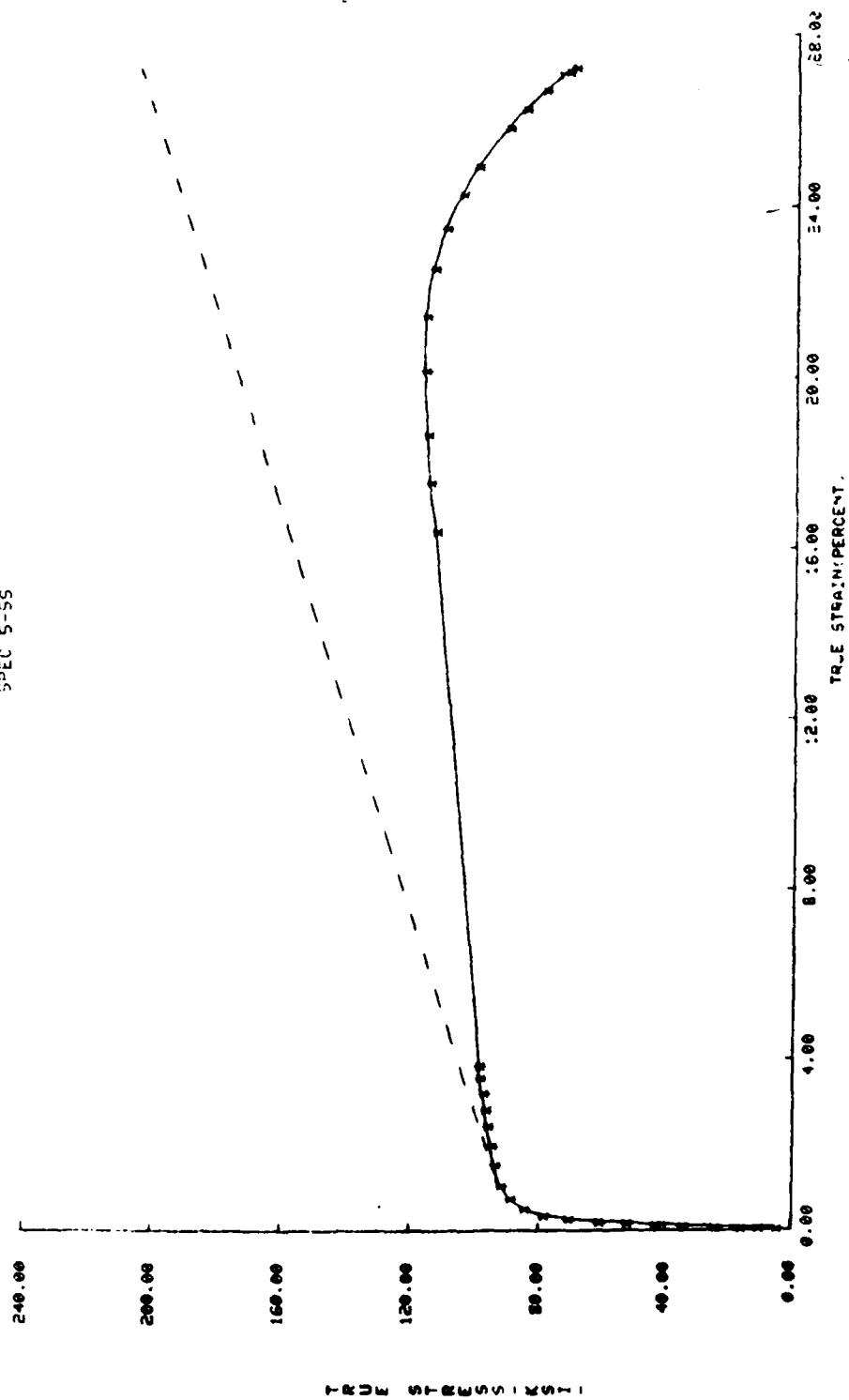
STANDARD TENSILE
0.001 STRAIN/SEC
8AL-1MO-1V TITANIUM
SPEC 3-TI



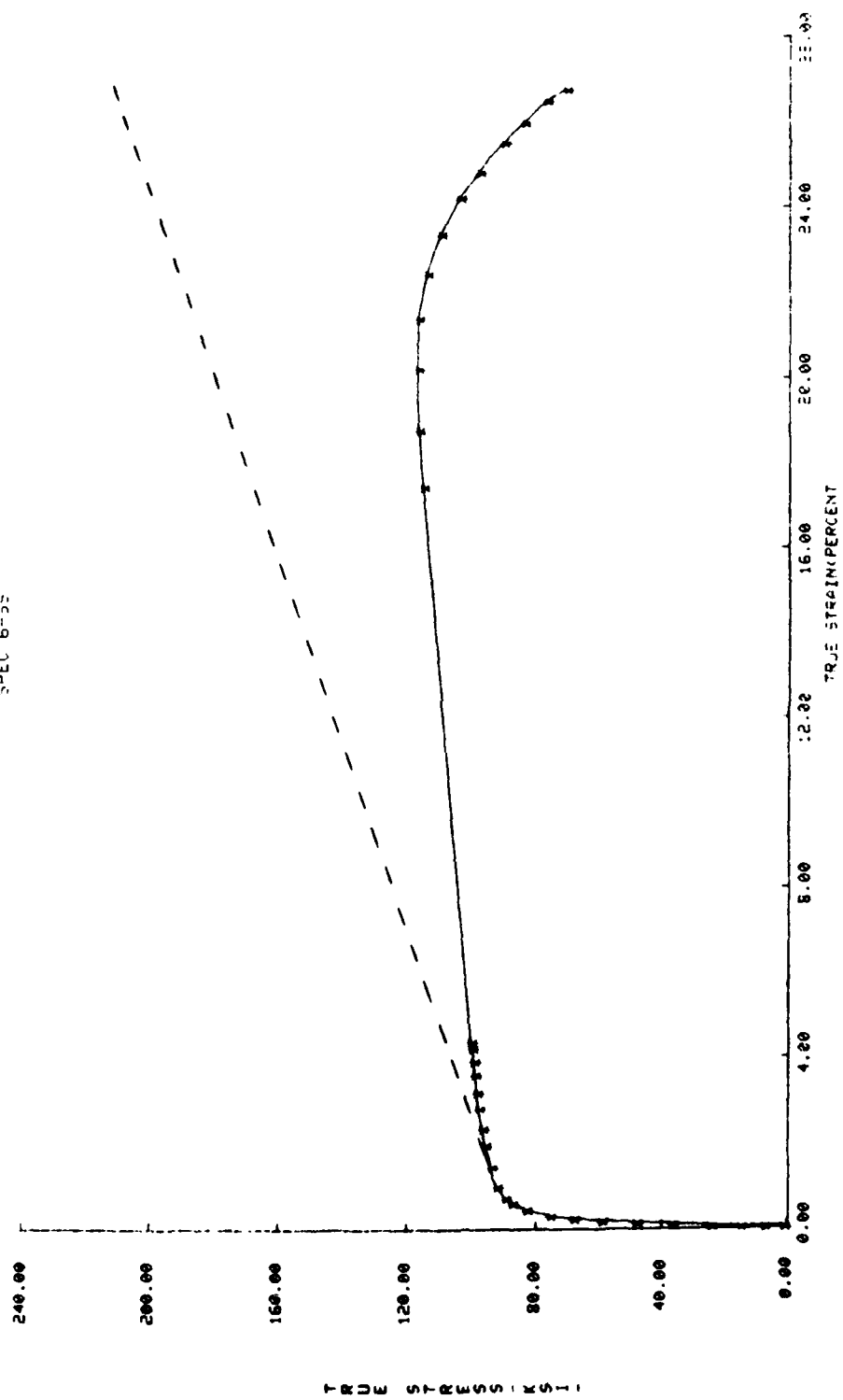
STANDARD TENSILE
 3.001 STRAIN SEC
 412 THINNESS STEEL
 SPEC 4-95



STANDARD TENSILE
0.001 STRAIN/SEC
410 STAINLESS STEEL
SPEC 5-55



STANDARD TENSILE
0.001 STRAIN/SEC
410 STAINLESS STEEL
SPEC 6-39



STANDARD TENSILE
0.100 STRAIN/SEC
BAL-IMO-1U TITANIUM
SPEC 4-TI

1	.0335636	3.257
2	.0900508	10.586
3	.15638171	19.547
4	.21490247	27.294
5	.25340253	35.854
6	.3139742	45.468
7	.3825160	57.491
8	.42774387	65.659
9	.46604360	75.053
10	.54001987	84.065
11	.60184056	95.112
12	.6460636	100.849
13	.65938212	107.800
14	.7177952	114.372
15	.7365080	121.735
16	.75545377	127.467
17	.81327086	137.725
18	.87152658	144.720
19	.89032801	151.276
20	.94877471	156.643
21	1.12597012	158.445
22	1.36217390	157.985
23	1.59776250	157.962
24	1.93054144	158.097
25	2.4268198	158.611
26	2.57369316	160.402
27	3.13423510	163.428
28	3.71172878	164.412
29	4.26676334	165.786
30	4.79374945	167.132
31	5.34901999	166.809
32	5.97021255	167.891
33	6.43831310	168.280
34	7.07130284	169.827
35	7.73724689	171.008
36	8.38344017	171.278
37	9.47307752	171.030
38	10.19656066	171.017
39	10.73485088	170.518
40	11.28830543	169.227
41	11.89194646	167.491
42	12.36882362	164.450
43	12.32591671	161.153
44	13.24538632	157.787
45	13.24538632	154.789

STANDARD TENSILE
0.100 STRAIN/SEC
BAL-IMO-1U TITANIUM
SPEC 5-TI

1	.05654797	3.271
2	.10870553	11.008

3	.1265188	17.106
4	.19257119	36.831
5	.24475782	34.641
6	.29444439	44.823
7	.34450159	54.625
8	.37627846	62.781
9	.42550477	73.394
10	.47620597	82.388
11	.52625225	92.199
12	.55599913	102.494
13	.58810322	110.171
14	.62098541	117.127
15	.65267456	125.307
16	.70451609	132.898
17	.73736615	140.070
18	.77177377	145.410
19	.82670694	149.961
20	.82355972	153.219
21	.94080533	154.591
22	1.07879180	154.766
23	1.21697999	154.611
24	1.35497748	154.473
25	1.5704257	155.306
26	1.98085383	156.529
27	2.31140082	158.013
28	2.67925197	159.996
29	3.10483700	160.861
30	3.4703574	161.809
31	3.91194067	162.936
32	4.44666631	164.045
33	4.96035564	164.209
34	5.52645895	166.310
35	6.22230569	166.499
36	6.65211026	166.982
37	7.33945767	168.020
38	7.91215402	168.381
39	8.37140514	168.936
40	8.73736618	169.290
41	9.17541029	168.917
42	9.70158121	169.176
43	10.17083419	169.756
44	10.56659295	169.280
45	11.03284015	168.501
46	11.56673857	169.221
47	12.15177187	168.690
48	12.69868228	167.807
49	13.22621626	165.083
50	13.62908264	162.723
51	14.08292549	159.521
52	14.44755739	157.500
53	15.24390454	149.787
54	15.55330532	147.591
55	15.81033547	145.748
56	15.96525145	143.217

STANDARD TENSILE
0.100 STRAIN/SEC
BAL-IMO-1U TITANIUM
SPEC 6-TI

1	0.3471539	3.667	59	15.31320832	142.215
2	.06552873	9.359		STANDARD TENSILE	
3	.13416839	17.916		0.100 STRAIN/SEC	
4	.17952807	28.084		4.00 STAINLESS STEEL	
5	.22429013	38.663		SPEC 9-55	
6	.27366970	46.410	1	.00035853	.203
7	.32124898	54.557	2	.00896298	5.063
8	.36710015	64.350	3	.03366054	13.368
9	.47082861	75.415	4	.0358711	20.356
10	.51661125	85.211	5	.08648913	28.339
11	.56697375	91.767	6	.09795168	32.825
12	.59804342	97.897	7	.15035226	39.928
13	.6282871	104.436	8	.12266335	46.814
14	.69349202	114.679	9	.13340555	52.898
15	.74032105	123.685	10	.18185101	57.777
16	.80693294	132.722	11	.14915893	61.821
17	.87464714	140.954	12	.19723884	66.500
18	.88640938	146.669	13	.24708391	72.197
19	.91967226	151.195	14	.29690415	77.897
20	.93372116	155.287	15	.38147019	80.774
21	1.12844386	157.609	16	.38789905	84.431
22	1.22766277	157.348	17	.47274506	87.516
23	1.32621259	157.500	18	.91840081	93.369
24	1.46515929	156.985	19	.127692285	95.530
25	1.64319673	156.553	20	1.00832474	97.753
26	1.93733236	157.193	21	2.16864879	100.011
27	2.17145361	158.115	22	3.58243795	101.836
28	2.42451498	159.084	23	4.46534833	103.329
29	2.67637448	160.467	24	5.40178148	104.984
30	3.14007390	162.747	25	6.54450526	106.257
31	3.44913410	163.444	26	7.28915843	106.794
32	3.98770165	164.666	27	8.21265215	107.736
33	4.42849011	165.253	28	9.23323846	108.827
34	4.7222466	165.620	29	10.3420005	109.543
35	5.22852417	166.249	30	11.46674946	109.983
36	5.68275105	166.876	31	12.42284052	110.755
37	6.20999722	167.677	32	13.12544181	111.495
38	6.62237795	167.785	33	13.95556107	111.487
39	6.95872451	168.574	34	14.93570225	111.608
40	7.42317698	169.673	35	15.67929211	111.385
41	7.94188394	170.038	36	16.52665221	110.611
42	8.40233466	170.702	37	17.26618215	109.703
43	8.76981055	170.706	38	17.86552894	108.392
44	9.22700084	170.925	39	18.66132649	106.526
45	9.69907468	171.406	40	19.4867614	103.633
46	9.95512767	170.467	41	20.13318117	101.580
47	10.40634295	170.669	42	20.81303257	99.488
48	10.88246422	171.183	43	21.32688160	96.964
49	11.19746146	171.797	44	21.97225420	93.540
50	11.66147829	171.028	45	22.72621590	89.606
51	12.05515430	168.814	46	23.48061967	84.863
52	12.53385115	168.157	47	24.04264046	81.188
53	13.10192704	164.035	48	24.50812256	77.659
54	13.36780151	161.452	49	24.97889934	73.575
55	13.80852118	157.880	50	25.21722951	70.356
56	14.24730702	154.271	51	25.49174514	67.922
57	14.59795432	150.426	52	25.76644683	64.959
58	14.98125574	147.095		STANDARD TENSILE	

0.100 STRAIN/SEC
410 STAINLESS STEEL
SPEC 10-SS

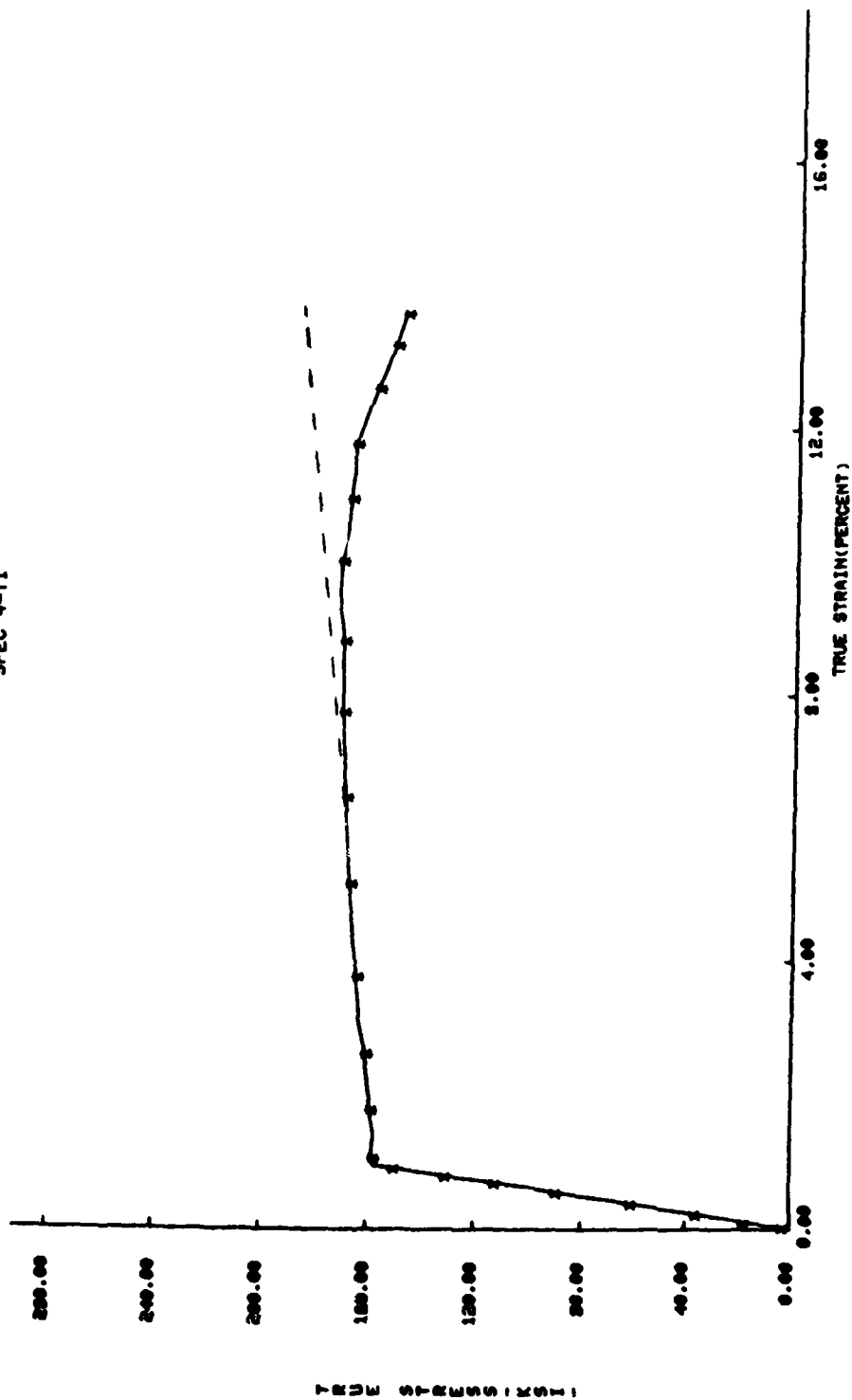
1	0.0000000	0.000
2	.01210789	3.239
3	.04877515	8.310
4	.06218912	15.403
5	.10791047	24.531
6	.11829335	32.438
7	.17355414	39.144
8	.18116430	47.661
9	.19682618	54.156
10	.17567809	59.823
11	.15754759	64.680
12	.22436764	68.160
13	.24757130	72.633
14	.27001492	77.311
15	.37350818	81.631
16	.47840062	85.550
17	.58468773	89.083
18	.61268690	91.957
19	1.12061854	94.519
20	1.54953608	96.403
21	2.20984863	98.348
22	3.96558705	100.354
23	3.63792577	101.586
24	4.25027029	102.695
25	5.06670736	104.071
26	5.95452543	105.286
27	6.76298396	106.375
28	7.59534481	107.210
29	8.58904225	108.393
30	9.39285159	108.917
31	10.19027116	109.435
32	11.01644387	110.216
33	11.86240655	110.271
34	12.85692657	111.073
35	14.05325846	110.738
36	15.09070747	111.087
37	16.15403901	110.515
38	17.31074385	108.593
39	18.15262109	107.204
40	18.85661755	105.132
41	19.82161320	101.853
42	20.58144965	98.768
43	21.17300813	95.044
44	22.4384566	92.864
45	23.12257405	89.268
46	24.11791677	85.141
47	24.50115880	81.819
48	24.81950740	75.177
49	25.13743427	72.618
50	25.32935102	69.782
51	25.48800529	67.343
52		65.390
53		

STANDARD TENSILE
0.100 STRAIN/SEC

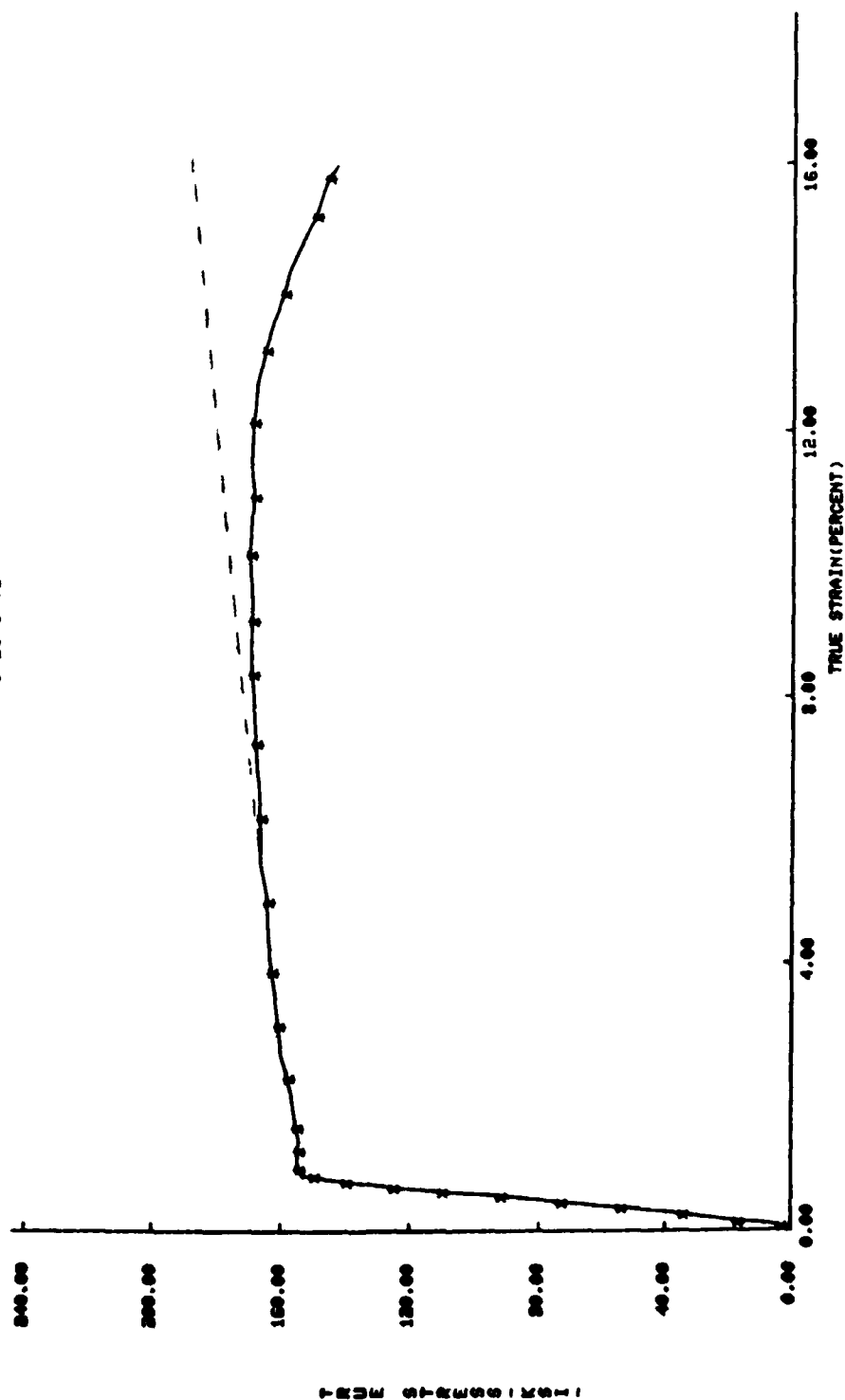
410 STAINLESS STEEL
SPEC 11-SS

1	0.00000000	.608
2	.03991219	7.090
3	.03991219	12.155
4	.05808846	18.237
5	.07980846	24.113
6	.07980846	30.800
7	.11968882	37.293
8	.11968882	43.968
9	.15955328	48.140
10	.15955328	53.722
11	.15955328	58.588
12	.19940186	61.831
13	.23923456	66.510
14	.27005141	71.596
15	.27005141	74.859
16	.27905141	77.659
17	.31885240	80.761
18	.31885240	83.350
19	.35863756	86.037
20	.47789816	88.290
21	.71593351	90.383
22	1.11153265	92.814
23	1.78046246	95.634
24	2.40596317	98.539
25	3.22101687	99.779
26	4.33575991	101.639
27	5.2490826	103.622
28	6.45385211	105.212
29	8.08714752	106.487
30	9.51287081	108.021
31	8.7111724	103.139
32	10.30824738	109.350
33	11.24015376	110.000
34	11.80934776	110.351
35	12.69227774	110.526
36	13.91542771	110.589
37	14.88388870	110.091
38	15.94403432	108.582
39	16.62246298	107.667
40	17.56459646	106.431
41	18.06568319	103.372
42	18.53110956	101.925
43	19.22521250	99.239
44	20.14335173	96.011
45	20.79337212	92.644
46	21.5606980	88.322
47	21.98647288	84.347
48	22.56155433	80.822
49	23.0066460	76.994
50	23.3232038	73.003
51	23.5448534	70.437
52	23.7338038	68.282
53		66.105

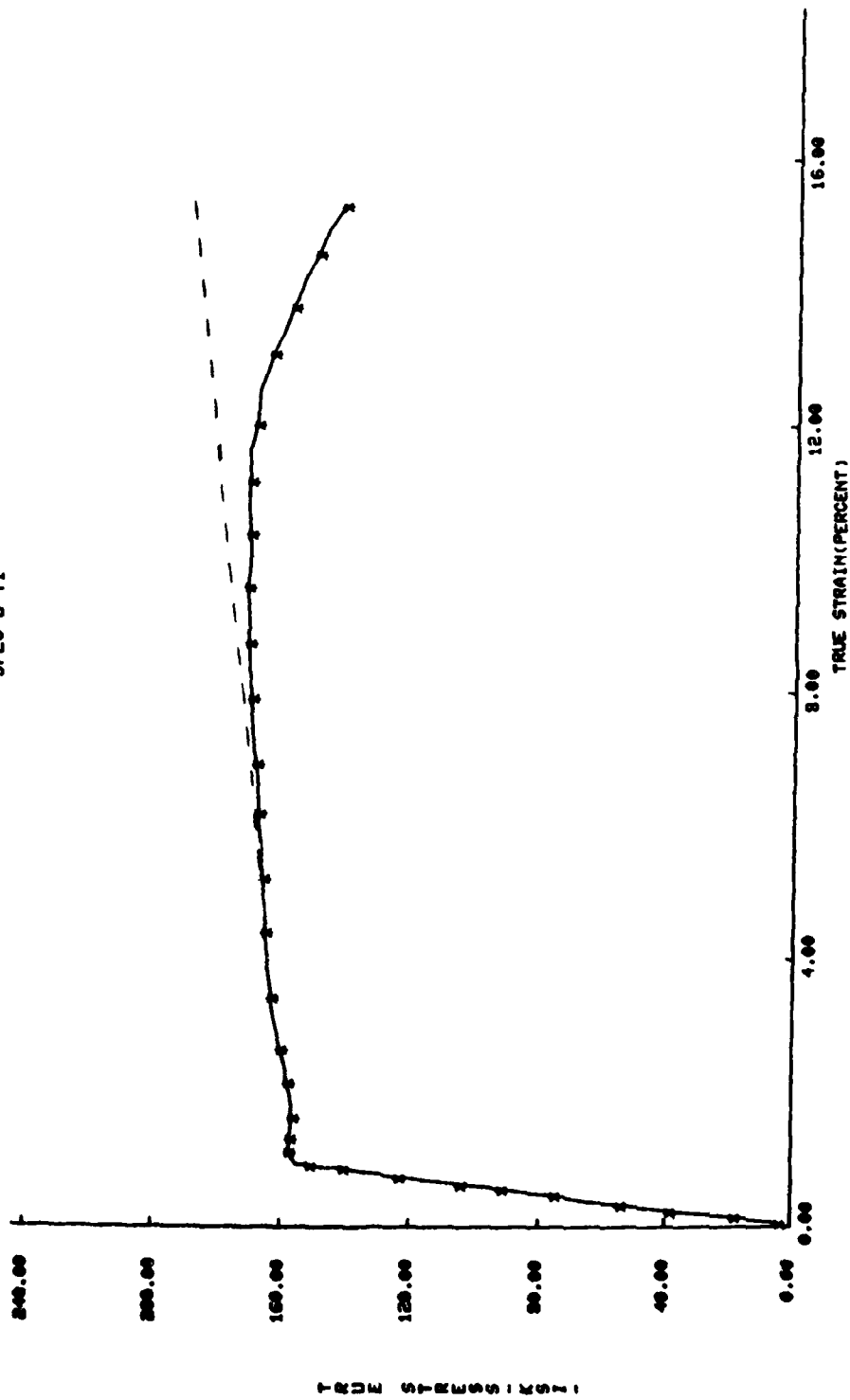
STANDARD TENSILE
0.100 STRAIN/SEC
BAL-INO-IU TITANIUM
SPEC 4-TI



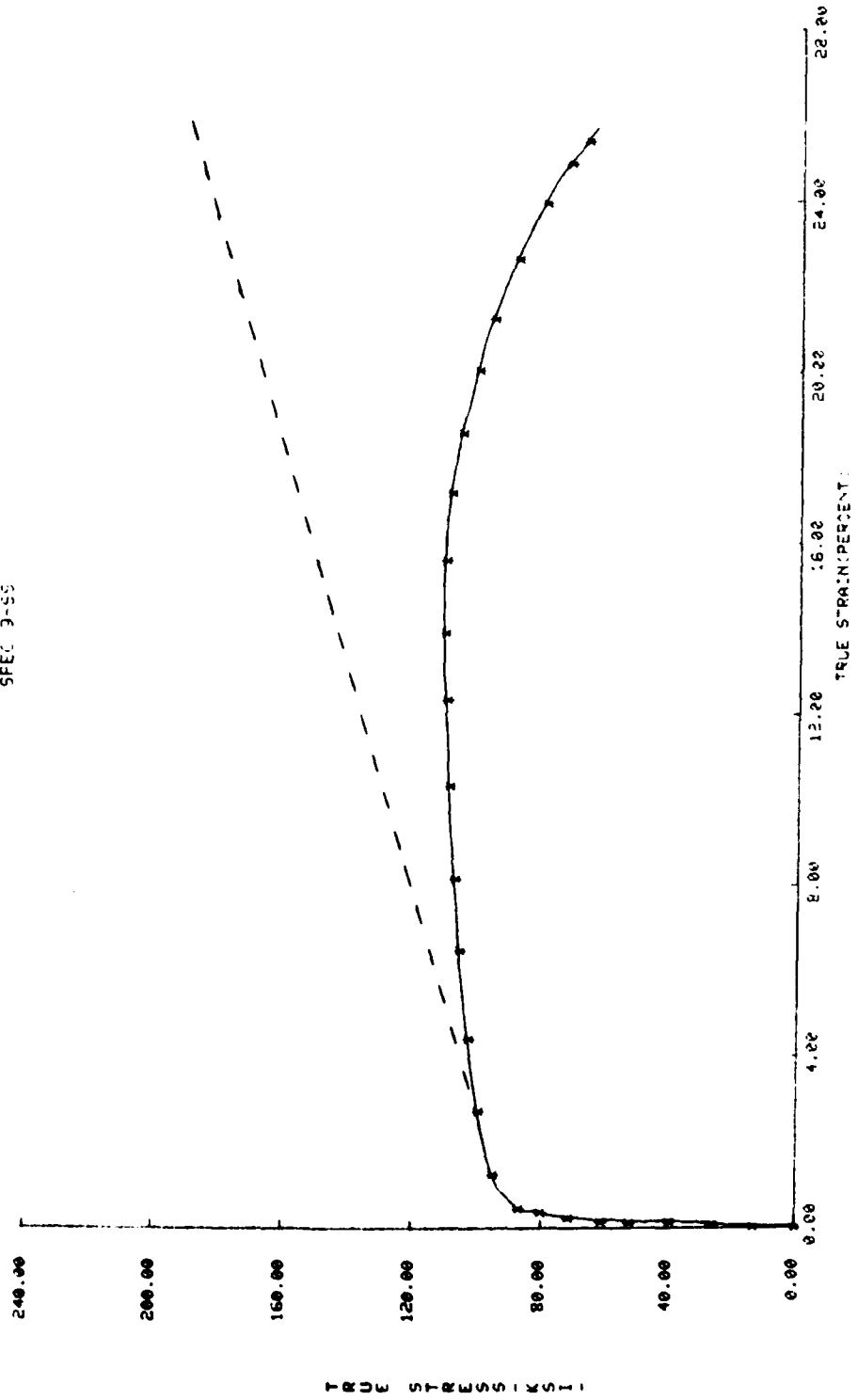
STANDARD TENSILE
0.100 STRAIN/SEC
BAL-100-10 TITANIUM
SPEC 5-TI



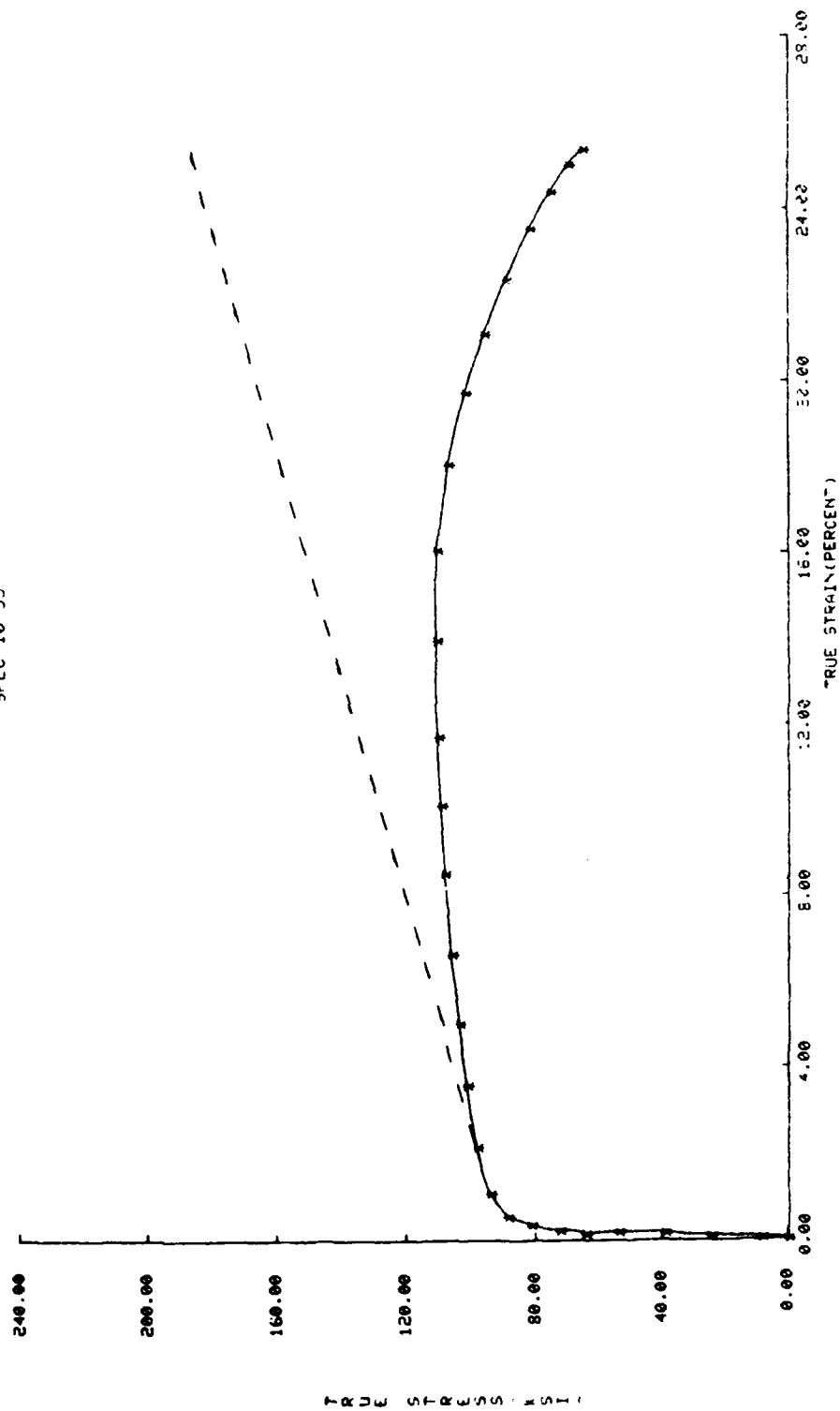
STANDARD TENSILE
0.100 STRAIN/SEC
BAL-100-1U TITANIUM
SPEC 6-TI



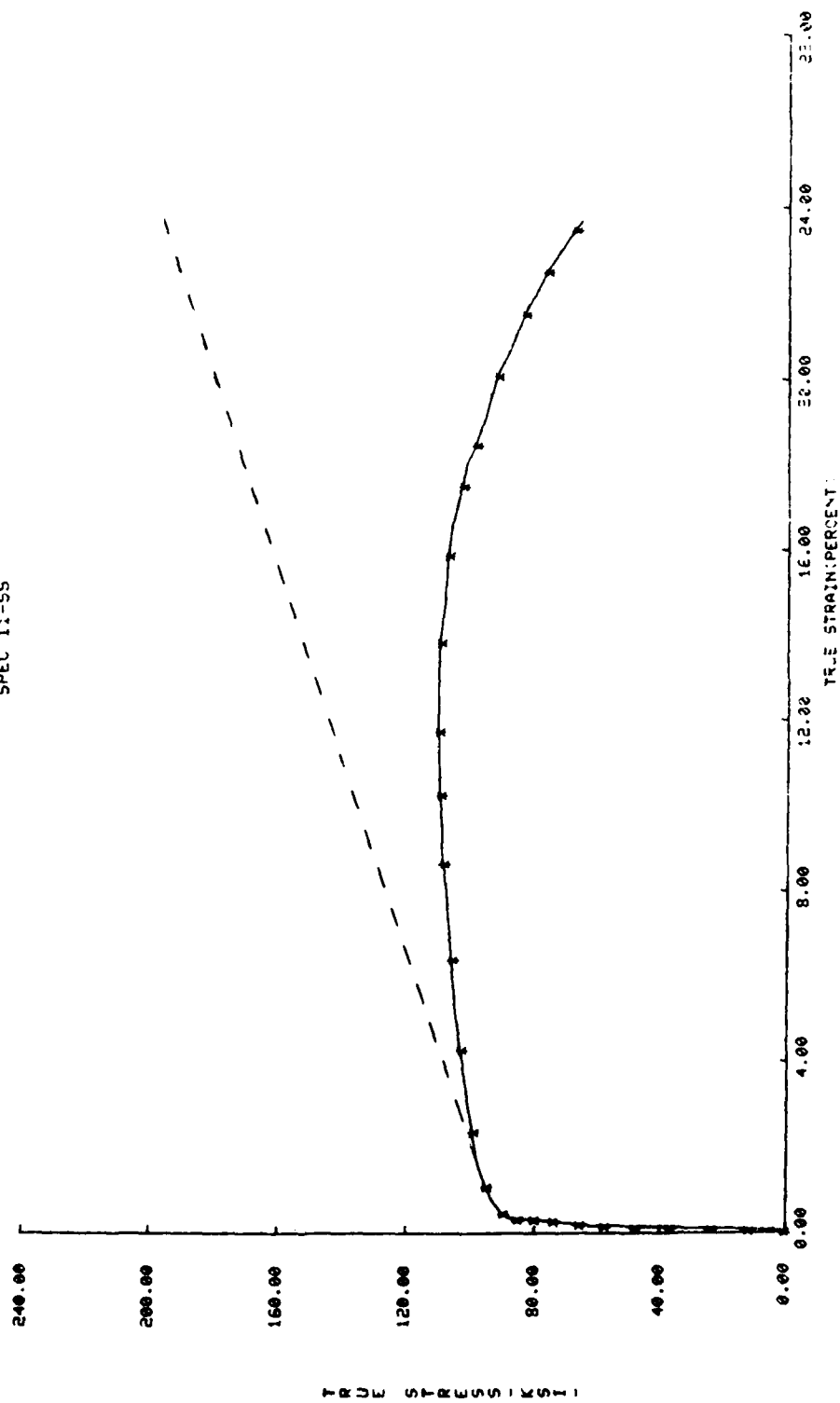
STANDARD TENSILE
0.100 STRAIN/SEC
410 STAINLESS STEEL
SPEC 3-55



STANDARD TENSILE
0.100 STRAIN/SEC
410 STAINLESS STEEL
SPEC 10-55



STANDARD TENSILE
0.100 STRAIN/SEC
410 STAINLESS STEEL
SPEC 11-55



STANDARD TENSILE
1 STRAIN/SEC
410 STAINLESS STEEL
12-55

0	0.0000000
1	.03375393
2	.02970882
3	.01959532
4	.0533264
5	.04120919
6	.07292752
7	.06551426
8	.05742644
9	.08946582
10	.07768440
11	.07364106
12	.06555391
13	.10063317
14	.09456950
15	.08783165
16	.12155595
17	.11414630
18	.10538873
19	.13843365
20	.12900468
21	.12092200
22	.14857474
23	.17891266
24	.16746771
25	.15938814
26	.19106900
27	.21937528
28	.20658896
29	.19851255
30	.23018102
31	.21806902
32	.24838586
33	.23829446
34	.23291196
35	.27062292
36	.38568597
37	.45963599
38	.61273456
39	.76559909
40	.99779722
41	1.30811156
42	1.73562019
43	2.12366414
44	2.54903252
45	3.08982778
46	3.62771417
47	4.23781135
48	5.03439341
49	6.03918727
50	6.24033942
51	

52	7.17148336
53	7.76414532
54	8.27815152
55	8.97236890
56	9.29953415
57	9.84244214
58	10.38302644
59	10.92070014
60	11.45618771
61	12.02458109
62	12.58865185
63	13.08087454
64	13.64021175
65	14.09947266
66	14.85378838
67	15.40448956
68	16.12409898
69	16.73751559
70	17.38186599
71	17.95382701
72	18.42432343
73	18.76063940
74	19.32868171
75	19.82765279
76	20.22273092
77	20.58658465
78	20.91571847
79	21.40739690
80	21.73438726
81	22.25395437
82	22.6495784
83	23.06446173
84	23.35616003
85	23.54944340
86	23.80462585
87	
88	
89	
90	
91	
92	
93	
94	
95	
96	
97	
98	
99	
100	

STANDARD TENSILE
1 STRAIN/SEC
410 STAINLESS STEEL
13-55

1	.00166925
2	.01085061
3	.01983012
4	.0898166
5	.05220655
6	.01545909
7	.04529750
8	.03111444
9	.05510926
10	.07159243
11	.08557121
12	.10621810
13	.09004367
14	.11185555
15	.1283100
16	.1563420
17	.1393355
18	.1593573
19	.18190014

107.92:
108.183
109.013
109.844
110.238
110.895
111.328
111.760
111.963
111.977
112.442
112.359
112.354
112.705
111.983
111.483
110.228
108.822
106.948
105.690
103.808
101.752
98.712
95.807
94.498
91.899
86.745
86.482
84.036
80.742
76.786
72.589
70.257
68.365
66.774

20	16190374	77.177	39772422	90.963
21	19536350	78.621	42745227	93.876
22	18836637	80.450	50752756	93.684
23	17836932	82.887	62076572	95.407
24	26649340	85.755	77486389	96.756
25	27270646	89.055	1.04573568	98.724
26	45549639	93.046	1.56238006	100.716
27	64707478	94.834	2.25916111	101.355
28	1.83326439	97.498	2.71474703	104.506
29	1.37948193	99.931	3.4854754	105.558
30	1.88366488	101.939	4.4805992	107.392
31	2.81238251	104.455	4.8037580	107.604
32	3.73341684	106.791	5.12429817	109.005
33	4.7237480	108.850	6.10425811	109.179
34	5.44437738	109.478	7.0190261	111.118
35	6.53241432	111.024	7.82246464	111.853
36	7.38916581	111.648	8.29434075	112.411
37	8.27303800	112.970	8.91620445	113.180
38	9.78625555	113.395	9.53422489	113.950
39	9.58853940	113.741	10.32903312	114.723
40	10.20386748	114.074	10.94097506	114.591
41	11.06489767	114.947	11.58152174	114.628
42	12.06664200	115.592	12.11462387	115.621
43	12.94370767	115.768	12.43198903	116.026
44	14.20827862	116.239	12.96058844	116.010
45	15.20113769	116.697	13.76472168	116.345
46	16.12637827	116.157	14.18260728	116.181
47	17.07674931	115.724	15.11420691	116.675
48	18.25590036	113.866	15.87031480	115.752
49	19.25859820	110.743	16.6906251	114.172
50	20.18654113	106.959	17.60530250	111.952
51	20.98059762	103.431	18.21123596	110.277
52	21.83011638	99.657	18.57906909	109.511
53			19.31541953	105.988
54			19.87960730	103.694
55			20.27859557	100.932
56			20.99988239	98.508
57			21.45859233	95.756
58			21.85249242	92.402
59			22.24312869	89.778
60			22.72814785	86.973
61			23.05265404	83.981
62			23.53546838	80.350
63			23.85962393	76.279
64			24.21178440	73.240
65			24.50087974	69.866
66			24.63177085	67.121
67				
68				
69				
70				
71				
72				
73				
74				
75				
76				
77				
78				
79				
80				
81				
82				
83				
84				
85				
86				
87				
88				
89				
90				
91				
92				
93				
94				
95				
96				
97				
98				
99				
100				
101				
102				
103				
104				
105				
106				
107				
108				
109				
110				
111				
112				
113				
114				
115				
116				
117				
118				
119				
120				
121				
122				
123				
124				
125				
126				
127				
128				
129				
130				
131				
132				
133				
134				
135				
136				
137				
138				
139				
140				
141				
142				
143				
144				
145				
146				
147				
148				
149				
150				
151				
152				
153				
154				
155				
156				
157				
158				
159				
160				
161				
162				
163				
164				
165				
166				
167				
168				
169				
170				
171				
172				
173				
174				
175				
176				
177				
178				
179				
180				
181				
182				
183				
184				
185				
186				
187				
188				
189				
190				
191				
192				
193				
194				
195				
196				
197				
198				
199				
200				
201				
202				
203				
204				
205				
206				
207				
208				
209				
210				
211				
212				
213				
214				
215				
216				
217				
218				
219				
220				
221				
222				
223				
224				
225				
226				
227				
228				
229				
230				
231				
232				
233				
234				
235				
236				
237				
238				
239				
240				
241				
242				
243				
244				
245				
246				
247				
248				
249				
250				
251				
252				
253				
254				
255				
256				
257				
258				
259				
260				
261				
262				
263				
264				
265				
266				
267				
268				
269				
270				
271				
272				
273				
274				
275				
276				
277				
278				
279				
280				
281				
282				
283				
284				
285				
286				
287				
288				
289				
290				
291				
292				
293				
294				
295				
296				
297				
298				
299				
300				
301				
302				
303				
304				
305				
306				
307				
308				
309				
310				
311				
312				
313				
314				
315				
316				
317				
318				
319				
320				
321				
322				
323				
324				
325				
326				
327				
328				
329				
330				
331				
332				
333				
334				
335				
336				
337				
338				
339				
340				
341				
342				
343				
344				
345				
346				
347				
348				
349				
350				
351				
352				
353				
354				
355				
356				
357				
358				
359				
360				
361				
362				
363				
364				
365				
366				
367				
368				
369				
370				
371				
372				
373				
374				
375				
376				
377				
378				
379				
380				
381				
382				
383				
384	</			

8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55										
0.08314563	0.0740583	0.0611511	0.0531527	0.0458013	0.0398924	0.0350058	0.0309920	0.02441315	0.01636861	0.00772123	0.0073255	0.0069779	0.003395526	0.002444	0.0023874	0.00190365	0.00171518	0.00279759	0.0077041	0.02214962	0.057359482	0.08100610	0.104694344	0.12658769	0.14740149	0.162340428	0.1745704594	0.186514684	0.196923764	0.2071817823	0.21784759224	0.2283359318	0.2394203004	0.250440322	0.260924109	0.27122431366	0.28174751395	0.29241357156	0.3037082995	0.31469807072	0.32531767822	0.335613718251	0.34574826724	0.3556463821	0.3652877786	0.3749025592	0.3844948970	0.3937375779	0.402466073	0.4117299021	0.42054636457	0.4288905083	0.436813802	0.4443512403			
20.726	25.398	30.890	36.384	41.270	46.146	50.425	54.503	59.380	63.866	68.964	73.232	77.519	82.012	84.248	84.923	88.404	90.561	92.343	94.169	96.246	97.837	99.040	101.045	102.622	104.126	105.473	107.254	108.872	108.557	109.756	110.656	111.371	112.338	112.864	113.087	113.432	113.478	113.812	114.249	114.423	114.228	114.505	114.048	113.175	110.818	109.245	106.927	102.087	102.685	100.141	75.180	72.027	69.663	67.428	65.381		
0.1983832	0.1904327	0.057611565	0.07625065	0.1160240	0.15244320	0.22007361	0.26667286	0.32363972	0.38037609	0.45222789	0.51378965	0.59014377	0.64702546	0.70407222	0.76059323	0.81772244	0.83616776	0.85485537	0.87363802	0.89310676	0.91717335	1.22820881	1.54285478	2.01287627	2.51959359	3.08177673	3.54473286	4.08205791	4.42592879	4.76871603	5.11023780	5.41130865	5.77145139	6.12851461	6.40962166	6.74559444	7.19174777	7.61753604	8.06028316	8.5001347	8.92115808	9.35809238	9.79294664	10.29816654	10.83636932	11.24721632	11.60330974	12.06361657	12.38123761	12.71541340	13.06623678	13.38104198	13.83438360	14.14712880			
1 STRAIN/SEC	BAL-IMO-1U-TITANIUM	7-11	1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55

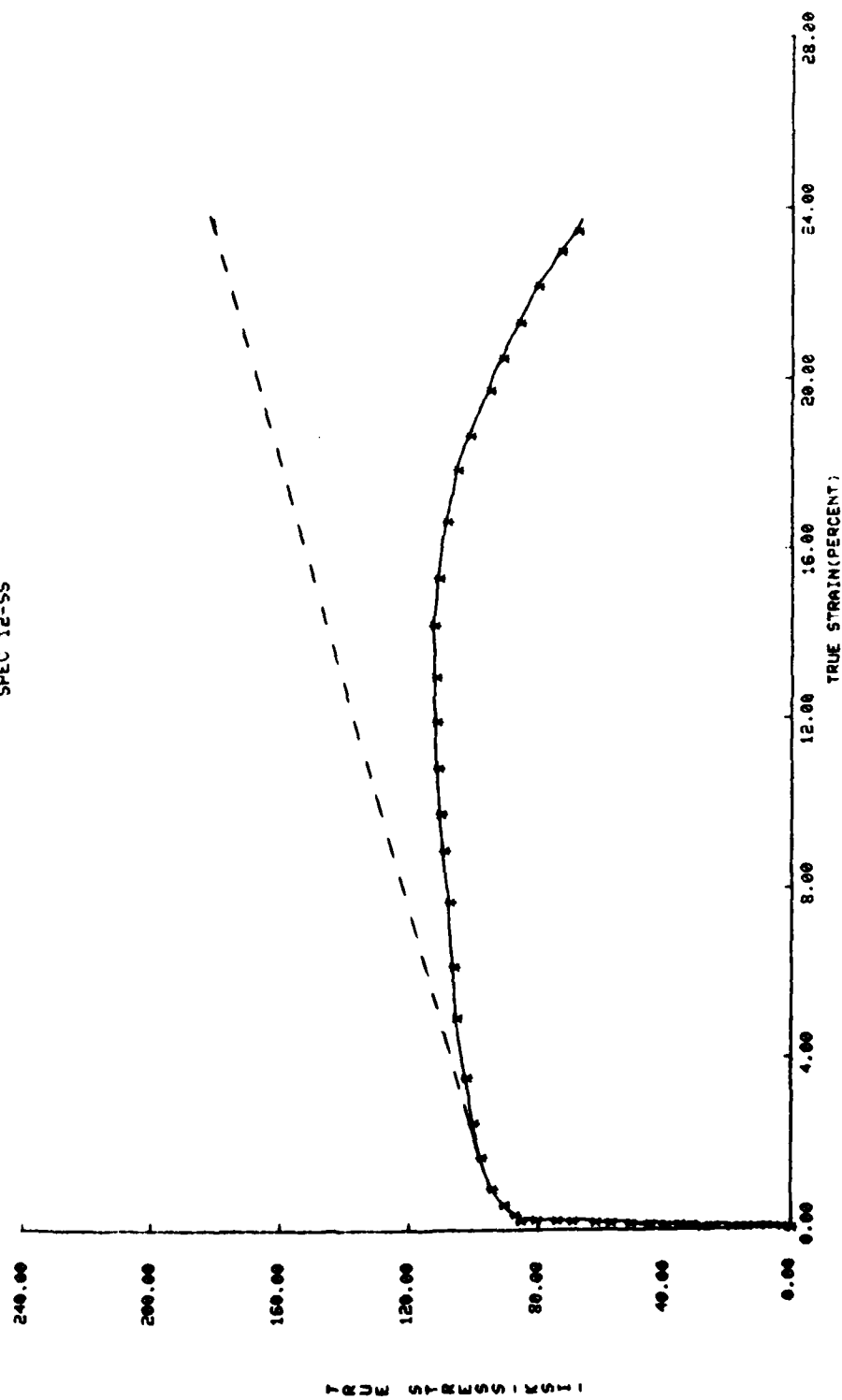
STANDARD TENSILE

170.453
166.432
161.938
158.970
155.960

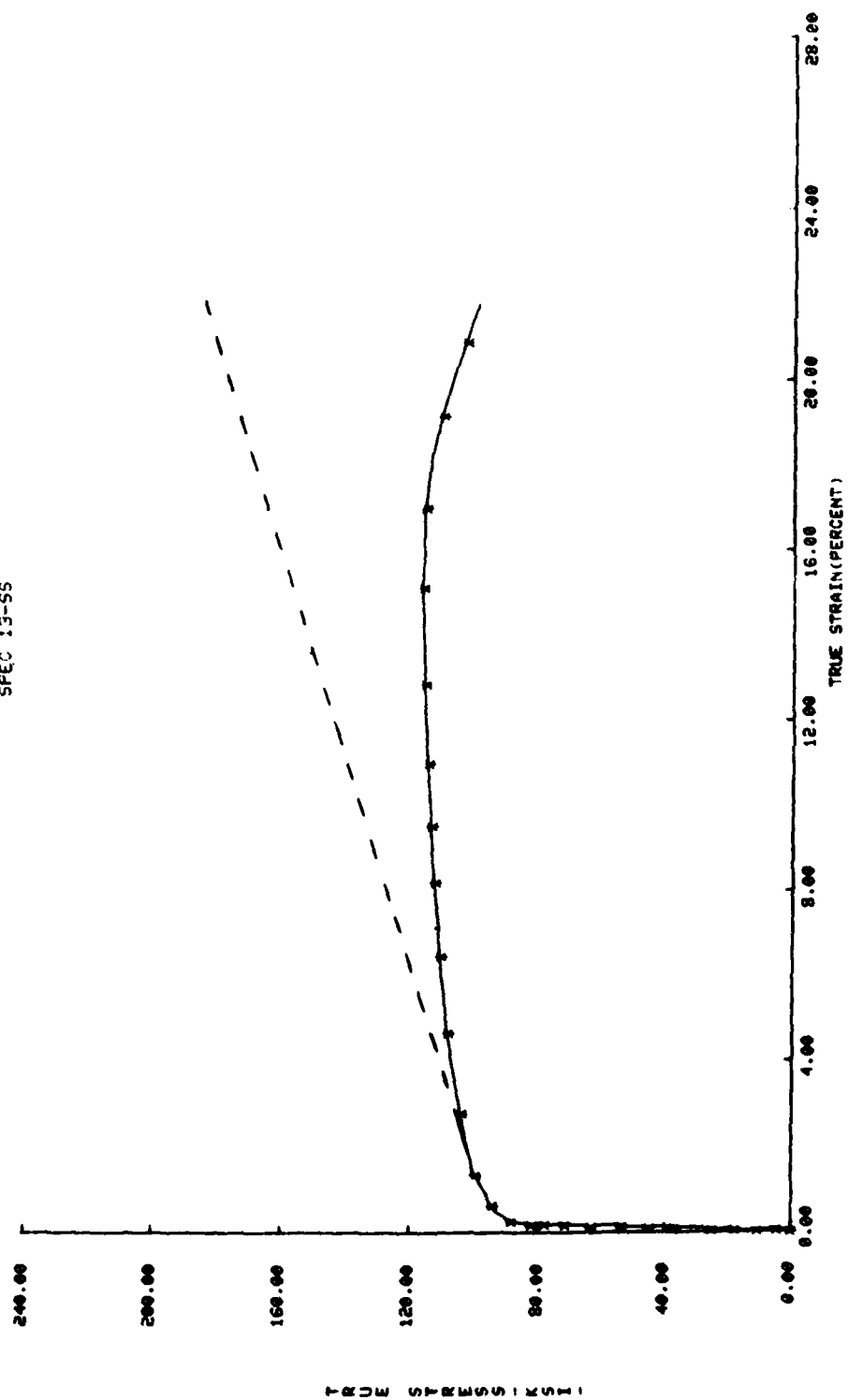
14.61450618
14.97650819
15.36439273
15.54238849
15.71407078

56
57
58
59
60

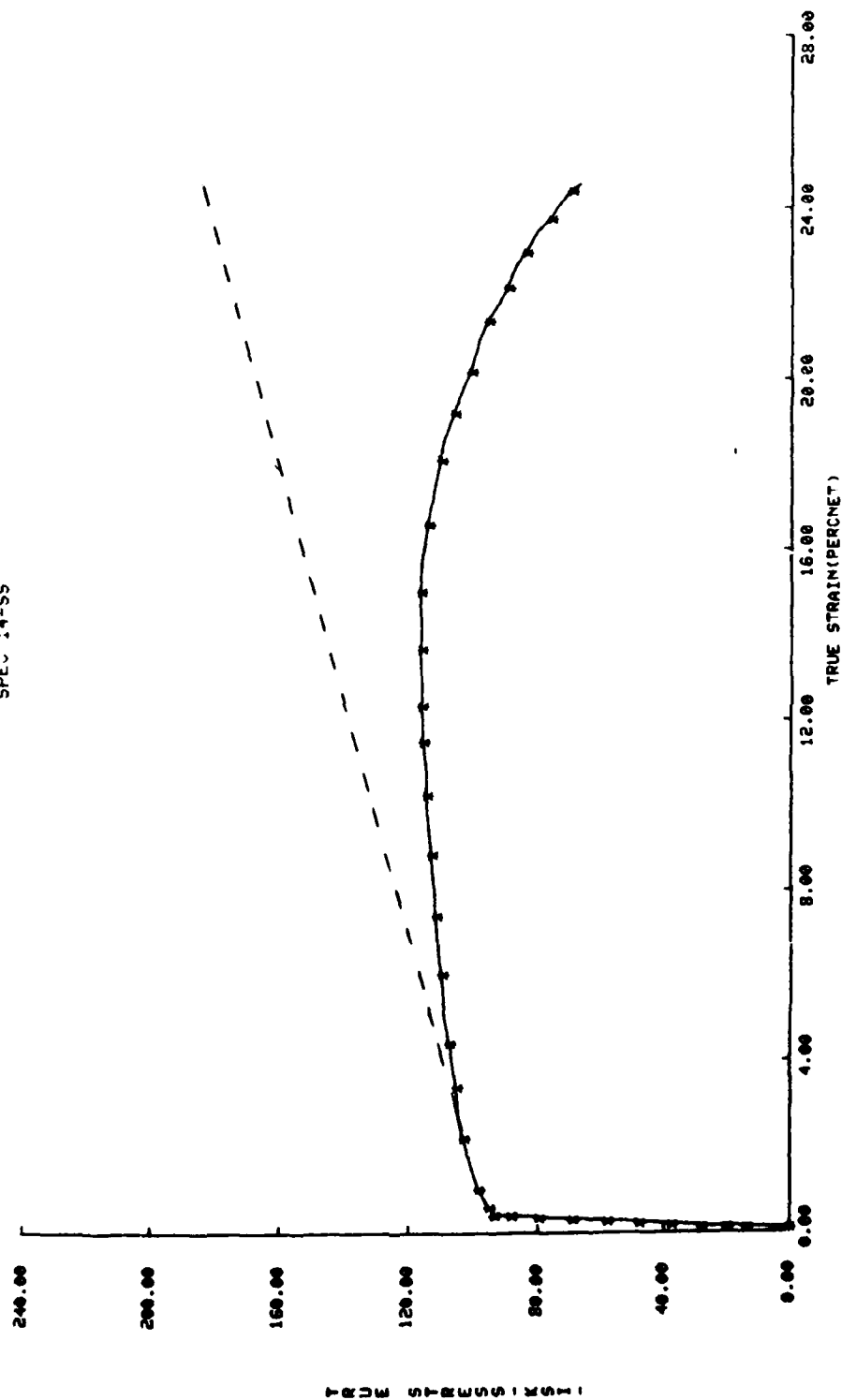
STANDARD TENSILE
1 STRAIN/SEC
410 STAINLESS STEEL
SPEC 12-55



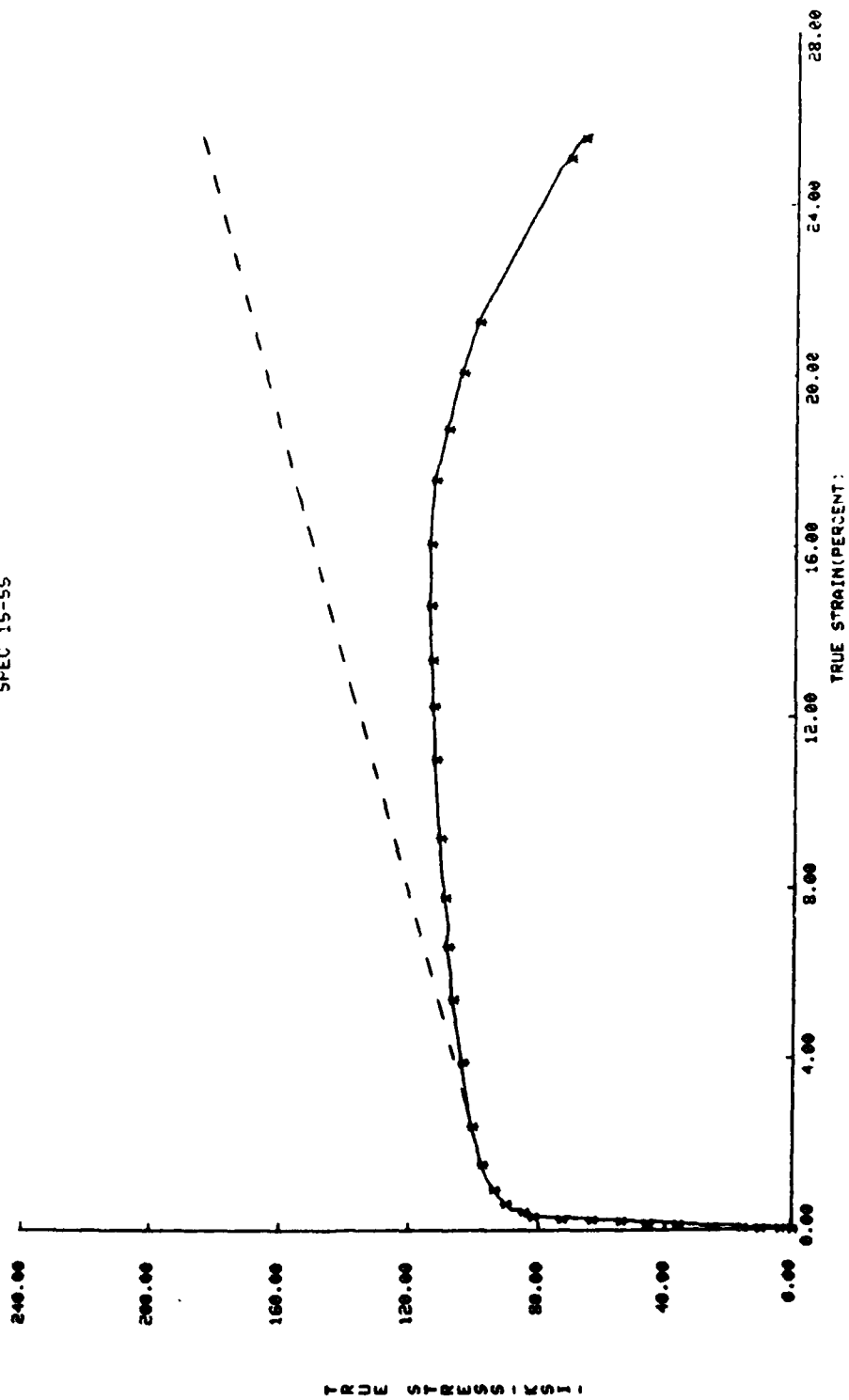
STANDARD TENSILE
1 STRAIN/SEC
410 STAINLESS STEEL
SPEC 13-SS



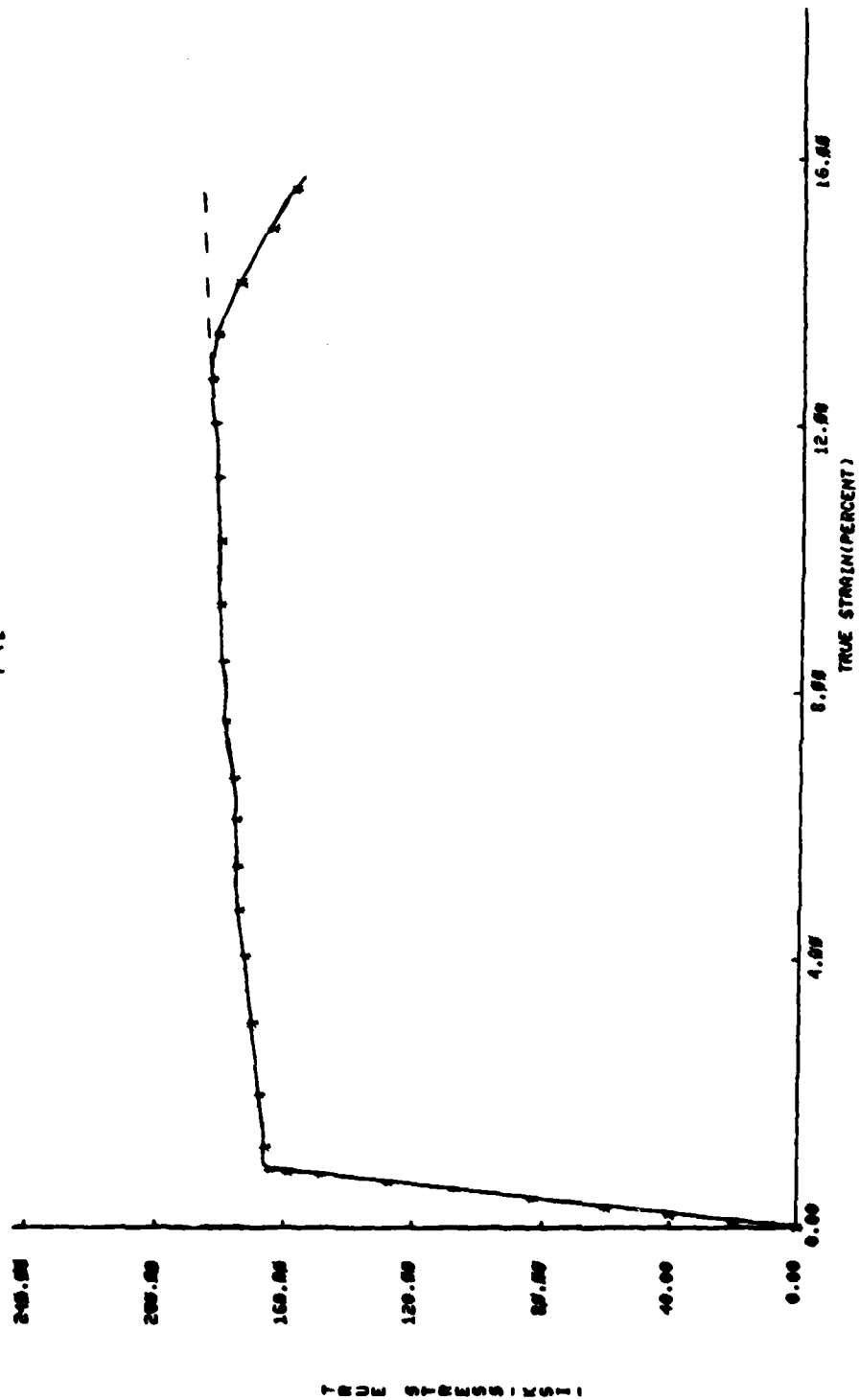
STANDARD TENSILE
1 STRAIN/SEC
410 STAINLESS STEEL
SPEC 14-SS



STANDARD TENSILE
1 STRAIN/SEC
410 STAINLESS STEEL
SPEC 15-55



STANDARD TENSILE
 1 STRAIN/SEC
 8AL-100-10-TITANIUM
 7-11



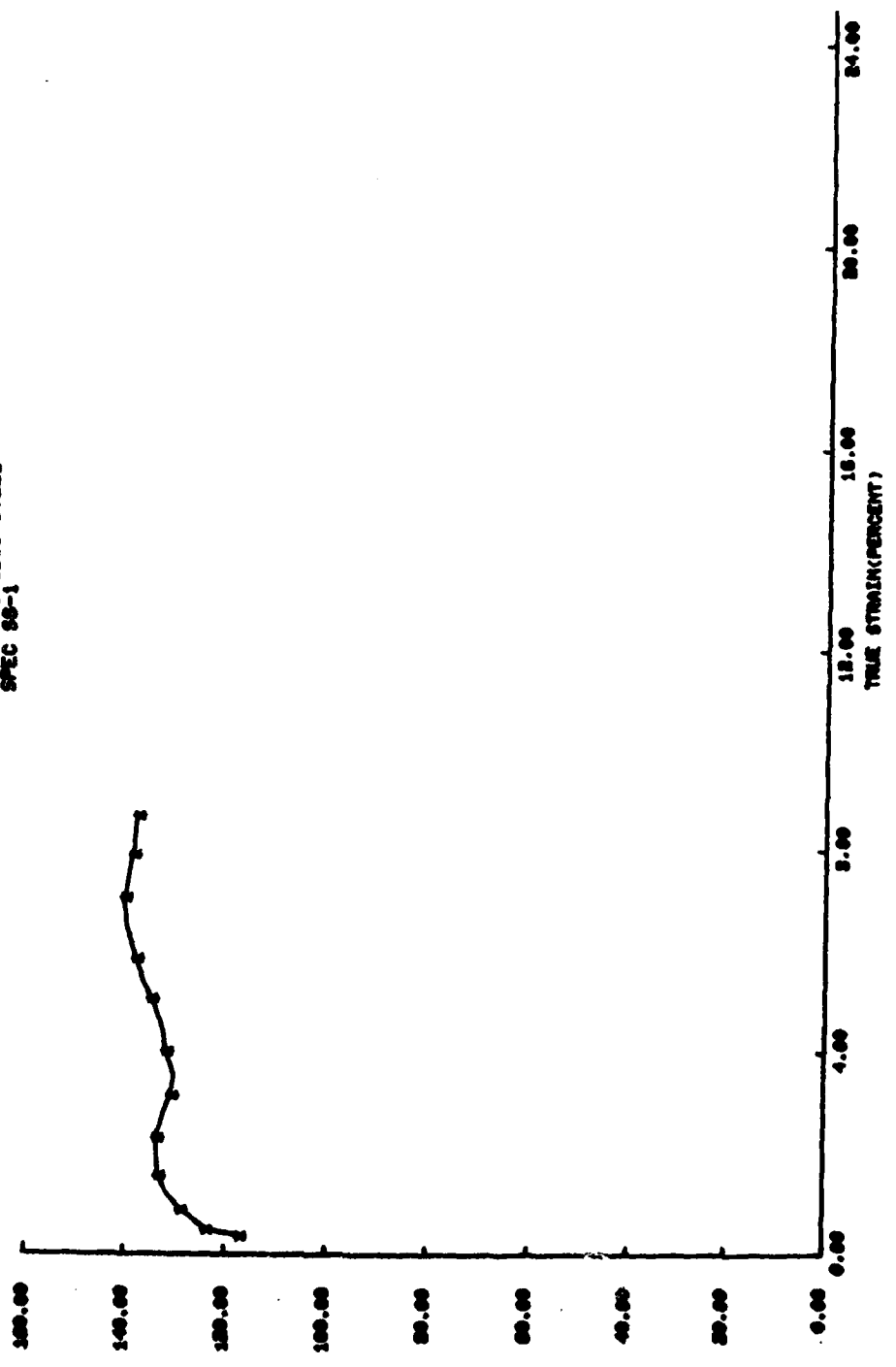
APPENDIX B
HIGH STRAIN RATE CURVES AND
DIGITAL DATA

1	131.853	1.94897857	1.18216133	182.695
2	136.814	2.00325116	1.2162579	185.479
3	201.123	2.13402188	1.24622894	188.254
4	208.746	2.26528111	1.27631782	190.641
5	209.136	2.39654036	1.31139596	193.821
6	208.747	2.52780061	1.34698239	197.001
7	207.903	2.65906086	1.42897555	199.776
8	207.181	2.79032111	1.73881692	201.306
9	205.608	2.92158136	2.23596459	203.432
10	204.036	3.05284161	2.54548973	205.517
11	202.850	3.18410186	2.85711875	205.580
12	201.664	3.31536211	3.16974777	205.847
13	201.000	3.44662236	3.48237679	206.046
14	201.000	3.57788261	3.79500581	206.281
15	201.000	3.70914286	4.10763483	206.463
16	201.000	3.84040311	4.42026385	206.641
17	201.000	3.97166336	4.73289287	206.869
18	201.000	4.10292361	5.04552189	207.051
19	201.000	4.23418386	5.35815091	207.271
20	201.000	4.36544411	5.67077993	207.491
21	201.000	4.49670436	5.98340895	207.654
22	201.000	4.62796461	6.29603797	207.895
23	201.000	4.75922486	6.60866699	208.095
24	201.000	4.89048511	6.92129601	208.295
25	201.000	5.02174536	7.23392503	208.495
26	201.000	5.15300561	7.54655405	208.695
27	201.000	5.28426586	7.85918307	208.895
28	201.000	5.41552611	8.17181209	209.095
29	201.000	5.54678636	8.48444111	209.295
30	201.000	5.67804661	8.79707013	209.495
31	201.000	5.80930686	9.10969915	209.695
32	201.000	5.94056711	9.42232817	209.895
33	201.000	6.07182736	9.73495719	210.095
34	201.000	6.20308761	10.04758621	210.295
35	201.000	6.33434786	10.36021523	210.495
36	201.000	6.46560811	10.67284425	210.695
37	201.000	6.59686836	10.98547327	210.895
38	201.000	6.72812861	11.29810229	211.095
39	201.000	6.85938886	11.61073131	211.295
40	201.000	6.99064911	11.92336033	211.495
41	201.000	7.12190936	12.23598935	211.695
42	201.000	7.25316961	12.54861837	211.895
43	201.000	7.38442986	12.86124739	212.095
44	201.000	7.51569011	13.17387641	212.295
45	201.000	7.64695036	13.48650543	212.495
46	201.000	7.77821061	13.79913445	212.695
47	201.000	7.90947086	14.11176347	212.895
48	201.000	8.04073111	14.42439249	213.095
49	201.000	8.17199136	14.73702151	213.295
50	201.000	8.30325161	15.04965053	213.495
51	201.000	8.43451186	15.36227955	213.695
52	201.000	8.56577211	15.67490857	213.895
53	201.000	8.69703236	15.98753759	214.095
54	201.000	8.82829261	16.29916661	214.295
55	201.000	8.95955286	16.61179563	214.495
56	201.000	9.09081311	16.92442465	214.695
57	201.000	9.22207336	17.23705367	214.895
58	201.000	9.35333361	17.54968269	215.095
59	201.000	9.48459386	17.86231171	215.295
60	201.000	9.61585411	18.17494073	215.495
61	201.000	9.74711436	18.48756975	215.695
62	201.000	9.87837461	18.79919877	215.895
63	201.000	10.00963486	19.11182779	216.095
64	201.000	10.14089511	19.42445681	216.295
65	201.000	10.27215536	19.73708583	216.495
66	201.000	10.40341561	20.04971485	216.695
67	201.000	10.53467586	20.36234387	216.895
68	201.000	10.66593611	20.67497289	217.095
69	201.000	10.79719636	20.98760191	217.295
70	201.000	10.92845661	21.29923093	217.495
71	201.000	11.05971686	21.61185995	217.695
72	201.000	11.19097711	21.92448897	217.895
73	201.000	11.32223736	22.23711799	218.095
74	201.000	11.45349761	22.54974701	218.295
75	201.000	11.58475786	22.86237603	218.495
76	201.000	11.71601811	23.17500505	218.695
77	201.000	11.84727836	23.48763407	218.895
78	201.000	11.97853861	23.79926309	219.095
79	201.000	12.10979886	24.11189211	219.295
80	201.000	12.24105911	24.42452113	219.495
81	201.000	12.37231936	24.73715015	219.695
82	201.000	12.50357961	25.04977917	219.895
83	201.000	12.63483986	25.36240819	220.095
84	201.000	12.76609011	25.67503721	220.295
85	201.000	12.89735036	25.98766623	220.495
86	201.000	13.02861061	26.29929525	220.695
87	201.000	13.15987086	26.61192427	220.895
88	201.000	13.29113111	26.92455329	221.095
89	201.000	13.42239136	27.23718231	221.295
90	201.000	13.55365161	27.54981133	221.495
91	201.000	13.68491186	27.86244035	221.695
92	201.000	13.81617211	28.17506937	221.895
93	201.000	13.94743236	28.48769839	222.095
94	201.000	14.07869261	28.79932741	222.295
95	201.000	14.20995286	29.11195643	222.495
96	201.000	14.34121311	29.42458545	222.695
97	201.000	14.47247336	29.73721447	222.895
98	201.000	14.60373361	30.04984349	223.095
99	201.000	14.73499386	30.36247251	223.295
100	201.000	14.86625411	30.67510153	223.495
101	201.000	14.99751436	30.98773055	223.695
102	201.000	15.12877461	31.29935957	223.895
103	201.000	15.26003486	31.61198859	224.095
104	201.000	15.39129511	31.92461761	224.295
105	201.000	15.52255536	32.23724663	224.495
106	201.000	15.65381561	32.54987565	224.695
107	201.000	15.78507586	32.86250467	224.895
108	201.000	15.91633611	33.17513369	225.095
109	201.000	16.04759636	33.48776271	225.295
110	201.000	16.17885661	33.79939173	225.495
111	201.000	16.31011686	34.11202075	225.695
112	201.000	16.44137711	34.42464977	225.895
113	201.000	16.57263736	34.73727879	226.095
114	201.000	16.70389761	35.04990781	226.295
115	201.000	16.83515786	35.36253683	226.495
116	201.000	16.96641811	35.67516585	226.695
117	201.000	17.09767836	35.98779487	226.895
118	201.000	17.22893861	36.29942389	227.095
119	201.000	17.36019886	36.61205291	227.295
120	201.000	17.49145911	36.92468193	227.495
121	201.000	17.62271936	37.23731095	227.695
122	201.000	17.75397961	37.54993997	227.895
123	201.000	17.88523986	37.86256899	228.095
124	201.000	18.01649011	38.17519801	228.295
125	201.000	18.14775036	38.48782703	228.495
126	201.000	18.27901061	38.79945605	228.695
127	201.000	18.41027086	39.11208507	228.895
128	201.000	18.54153111	39.42471409	229.095
129	201.000	18.67279136	39.73734311	229.295
130	201.000	18.80405161	40.04997213	229.495
131	201.000	18.93531186	40.36260115	229.695
132	201.000	19.06657211	40.67523017	229.895
133	201.000	19.19783236	40.98785919	230.095
134	201.000	19.32909261	41.29948821	230.295
135	201.000	19.46035286	41.61211723	230.495
136	201.000	19.59161311	41.92474625	230.695
137	201.000	19.72287336	42.23737527	230.895
138	201.000	19.85413361	42.54990429	231.095
139	201.000	19.98539386	42.86253331	231.295
140	201.000	20.11665411	43.17516233	231.495
141	201.000	20.24791436	43.48779135	231.695
142	201.000	20.37917461	43.79942037	231.895
143	201.000	20.51043486	44.11204939	232.095
144	201.000	20.64169511	44.42467841	232.295
145	201.000	20.77295536	44.73730743	232.495
146	201.000	20.90421561	45.04993645	232.695
147	201.000	21.03547586	45.36256547	232.895
148	201.000	21.16673611	45.67519449	233.095
149	201.000	21.29799636	45.98782351	233.295
150	201.000	21.42925661	46.29945253	233.495
151	201.000	21.56051686	46.61208155	233.695
152	201.000	21.69177711	46.92471057	233.895
153	201.000	21.82303736	47.23733959	234.095
154	201.000	21.95429761	47.54996861	234.295
155	201.000	22.08555786	47.86259763	234.495
156	201.000	22.21681811	48.17522665	234.695
157	201.000	22.34807836	48.48785567	234.895
158	201.000	22.47933861	48.79948469	235.095
159	201.000	22.61059886	49.11211371	235.295
160	201.000	22.74185911	49.42474273	235.495
161	201.000	22.87311936	49.73737175	235.695
162	201.000	23.00437961	50.04990077	235.895
163	201.000	23.13563986	50.36252979	236.095
164	201.000	23.26689011	50.67515881	236.295
165	201.000	23.39815036	50.98778783	236.495
166	201.000	23.52941061	51.29941685	236.695
167	201.000	23.66067086	51.61204587	236.895
168	201.000	23.79193111	51.92467489	237.095
169	201.000	23.92319136	52.23730391	237.295
170	201.000	24.05445161	52.54993293	237.495
171	201.000	24.18571186	52.86256195	237.695
172	201.000	24.31697211	53.17519097	237.895
173	201.000	24.44823236	53.48781999	238.095
174	201.000	24.57949261	53.79944901	238.295
175	201.000	24.71075286	54.11207803	238.495
176	201.000	24.84201311	54.42470705	238.695
177	201.000	24.97327336	54.73733607	238.895
178	201.000	25.10453361	55.04996509	239.095
179	201.000	25.23579386	55.36259411	239.295
180	201.000	25.		

185, 514
186, 265
191, 452
193, 235
197, 609
198, 192
199, 431
200, 409
201, 511
206, 573
208, 381
209, 471
210, 387
213, 471
213, 902
214, 428
214, 549
216, 459
216, 708
218, 118
218, 649
223, 187
223, 268
117, 423
113, 994
150, 423
157, 921
151, 559
178, 391
178, 148
180, 010
186, 558
193, 804
193, 115

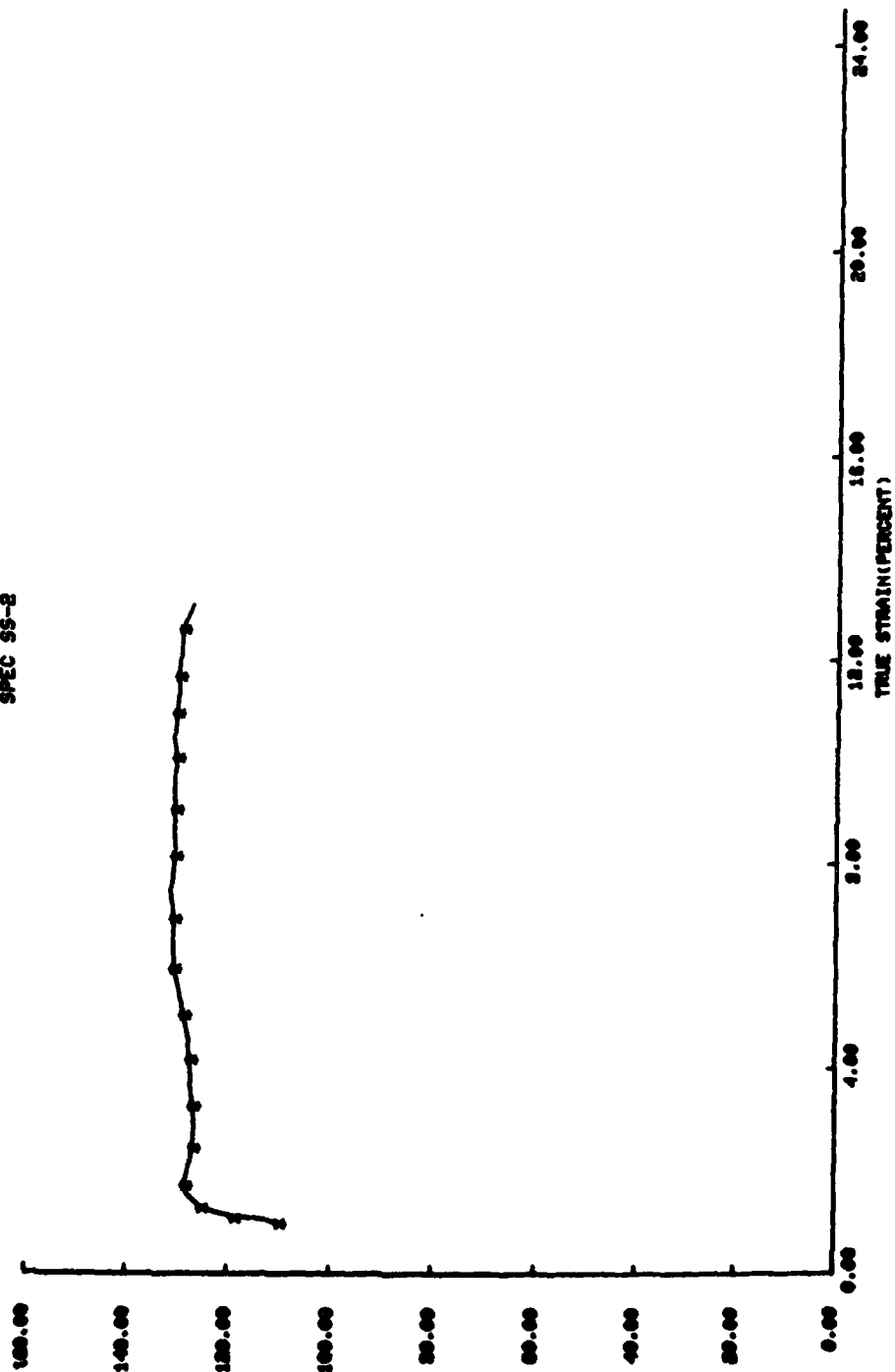
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87	88	89	90	91	92	93	94	95	96	97	98	99	100
1	2	3	4	5	6	7	8	9	10	11	12	13	14	15	16	17	18	19	20	21	22	23	24	25	26	27	28	29	30	31	32	33	34	35	36	37	38	39	40	41	42	43	44	45	46	47	48	49	50	51	52	53	54	55	56	57	58	59	60	61	62	63	64	65	66	67	68	69	70	71	72	73	74	75	76	77	78	79	80	81	82	83	84	85	86	87													

HOPKINSON BAR--TENSILE
 340 STRAIN/SEC
 410 STAINLESS STEEL
 SPEC 90-1



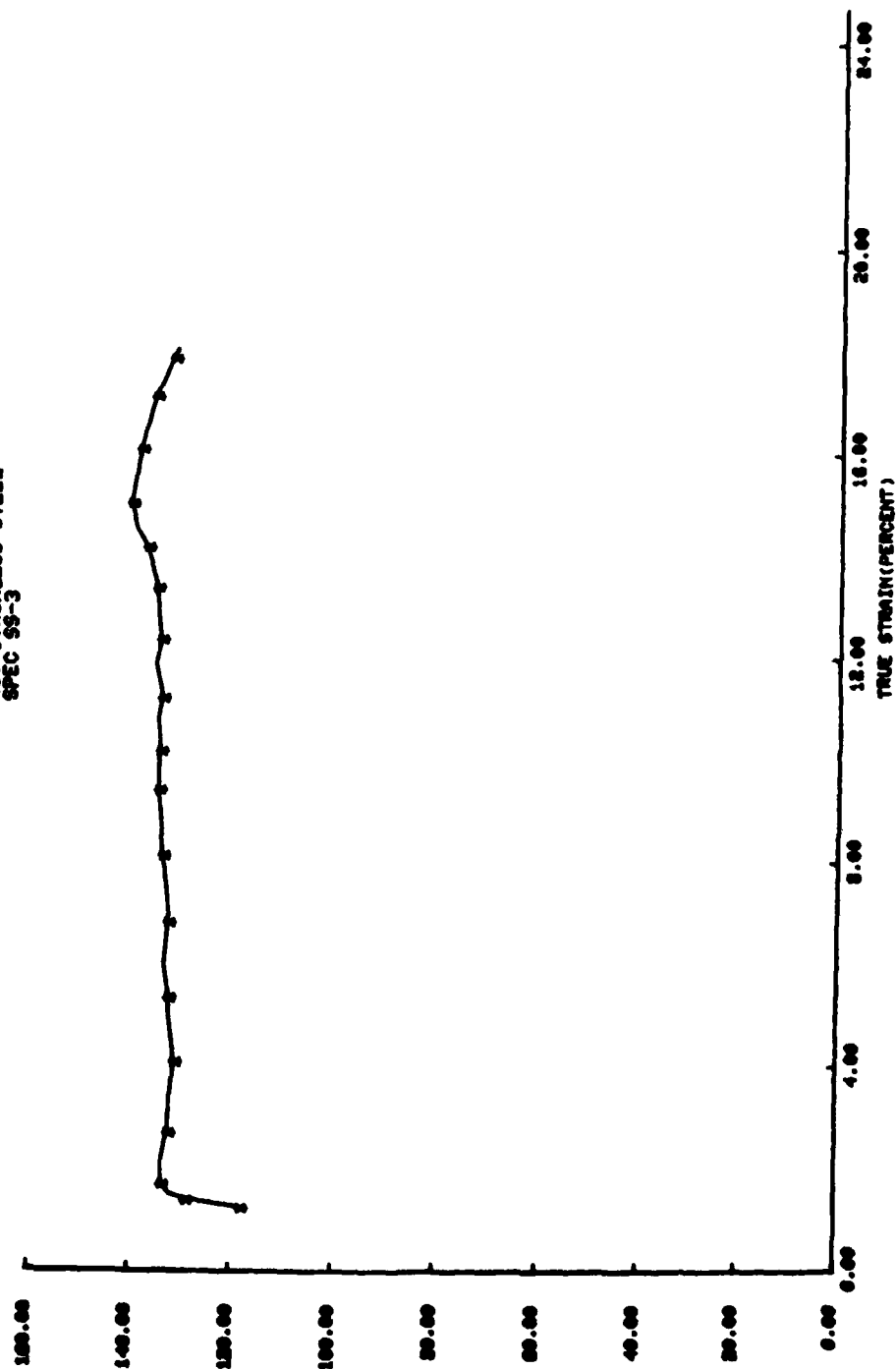
1-027-00000-00 FIG. 1

HOPKINSON BAR--TENSILE
 530 STRAIN/SEC
 410 STAINLESS STEEL
 SPEC SS-B

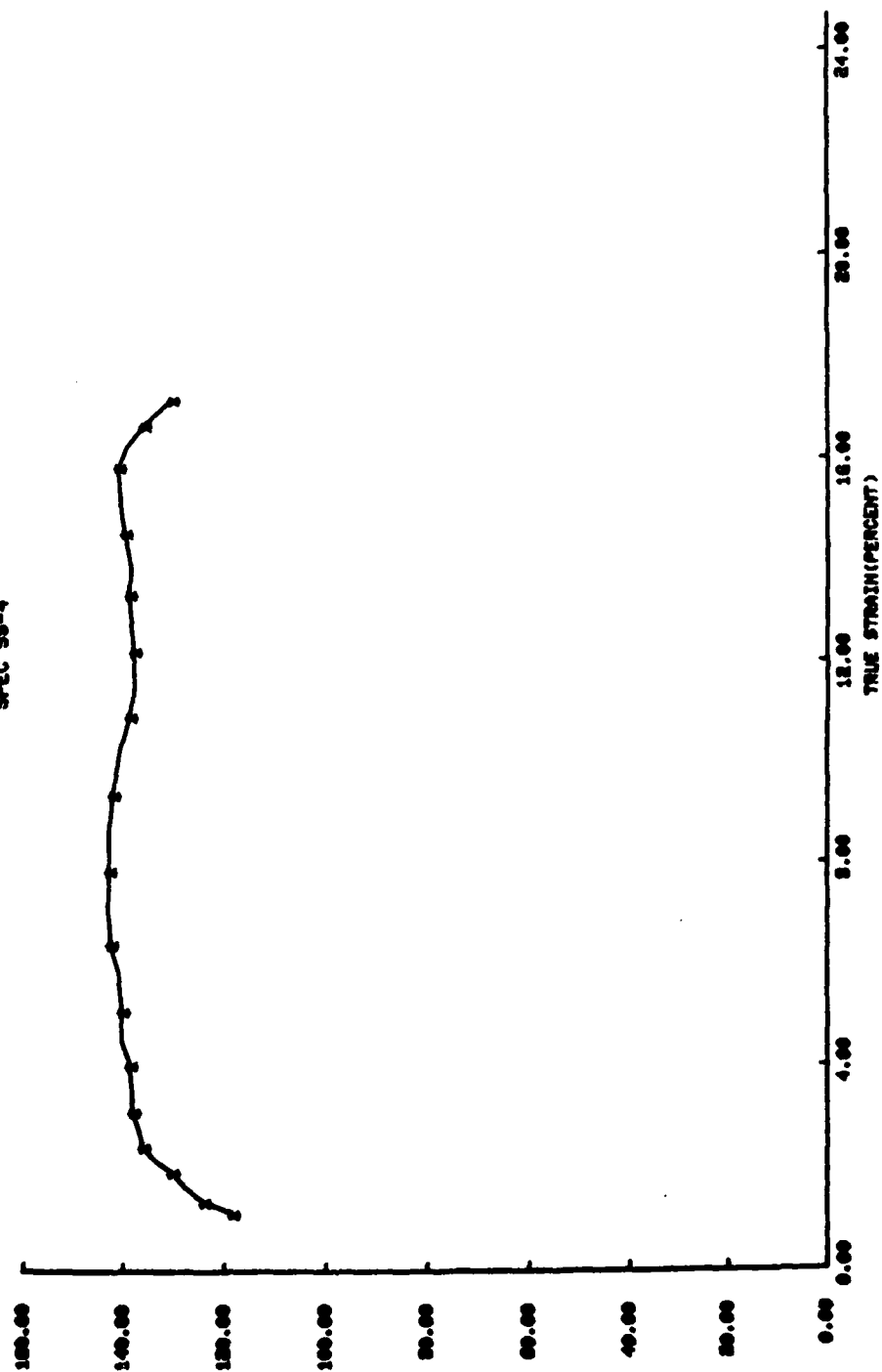


1-2-2-2 0-2-2-2-2-2 1-2-2-2-2-2

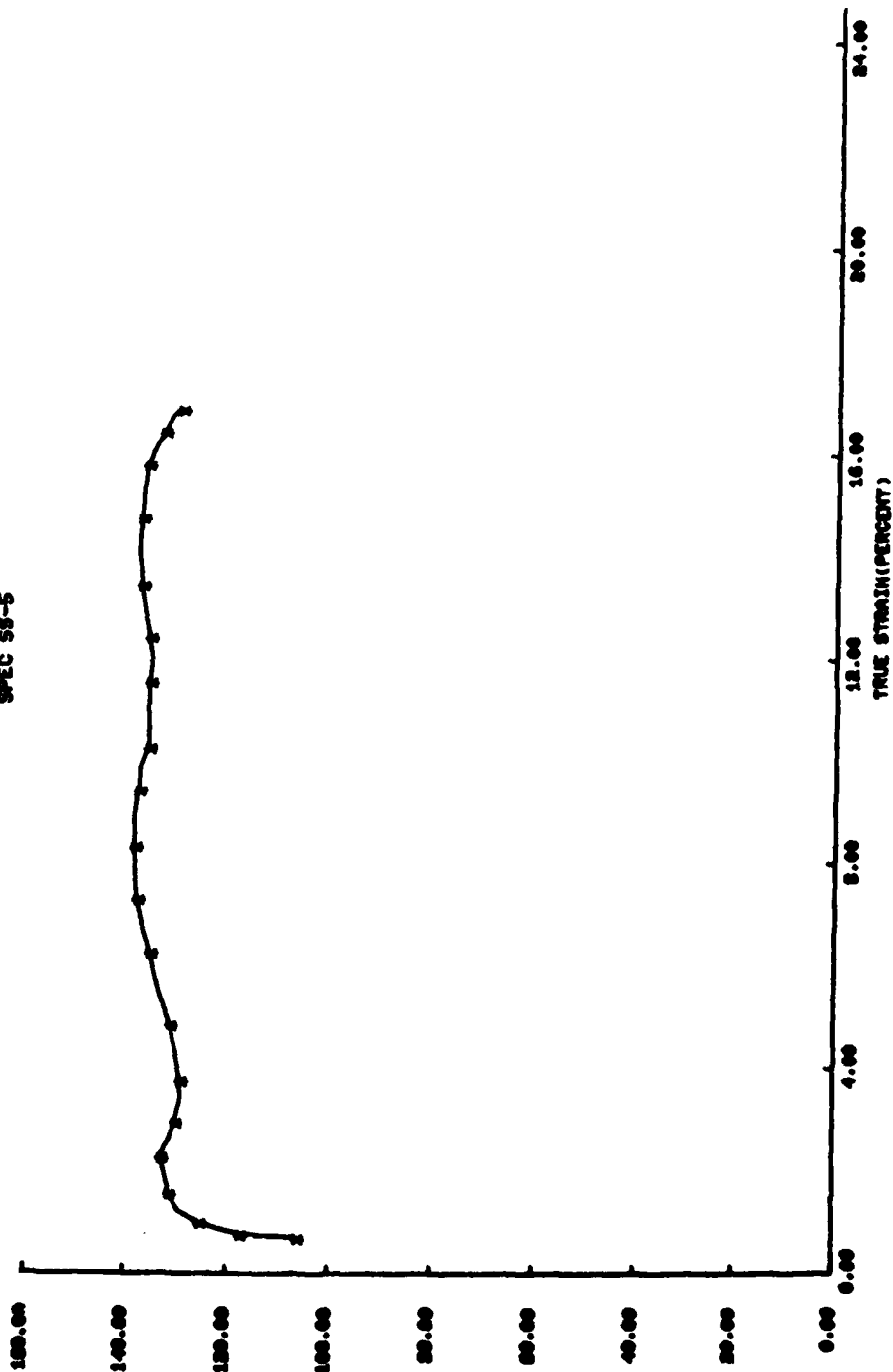
HOPKINSON BAR--TENSILE
700 STRAIN/SEC
410 STAINLESS STEEL
SPEC 99-3



HOPKINSON BAR--TENSILE
 760 STRAIN/SEC
 410 STAINLESS STEEL
 SPEC 58-4

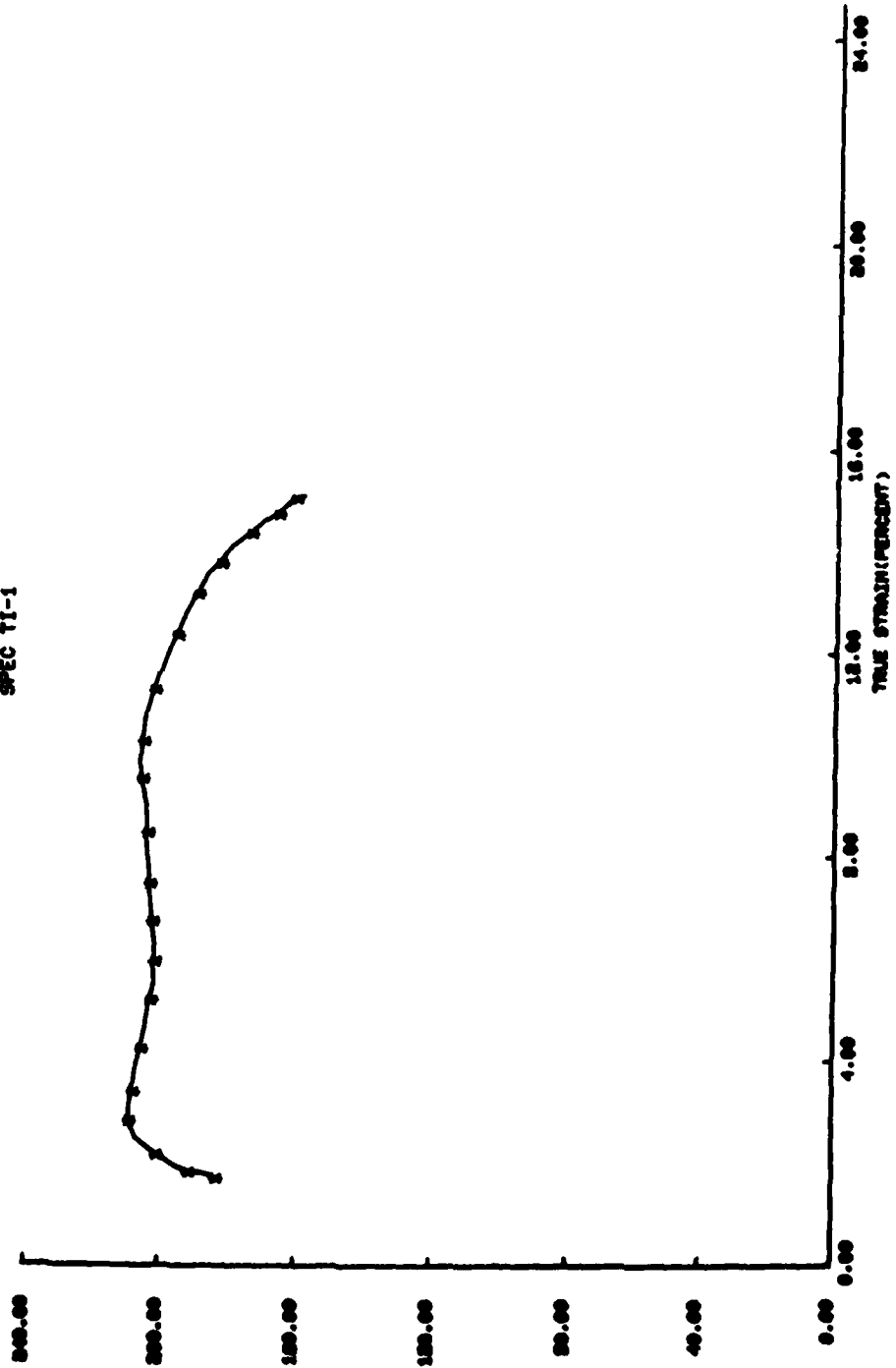


HOPKINSON BAR--TENSILE
 600 STRAIN/SEC
 410 STAINLESS STEEL
 SPEC S8-5

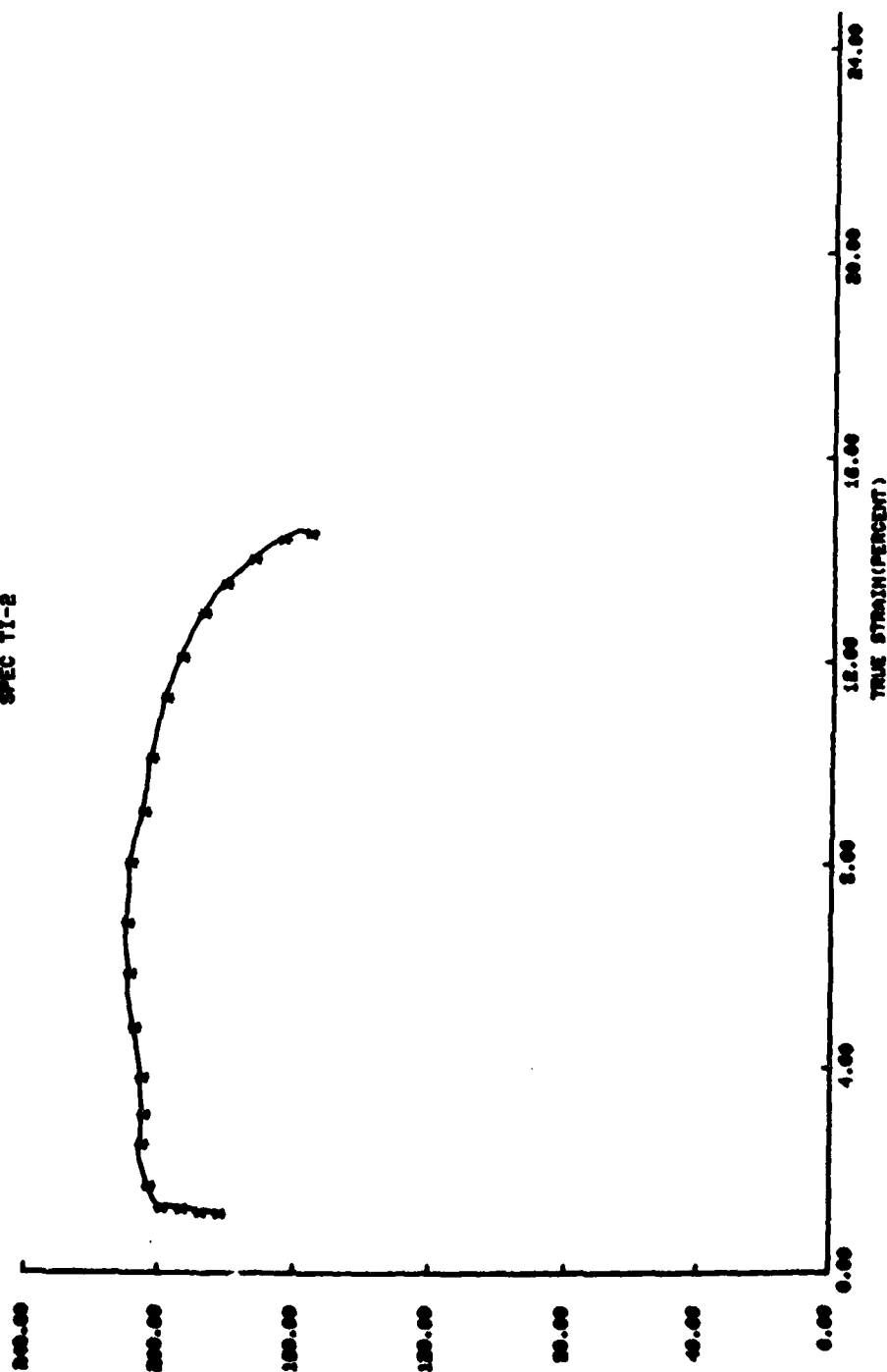


1-2222 00-222222 1222-1

HOPKINSON BAR--TENSILE
 500 STRAIN/SEC
 BAL-INO-10 TITANIUM
 SPEC TI-1

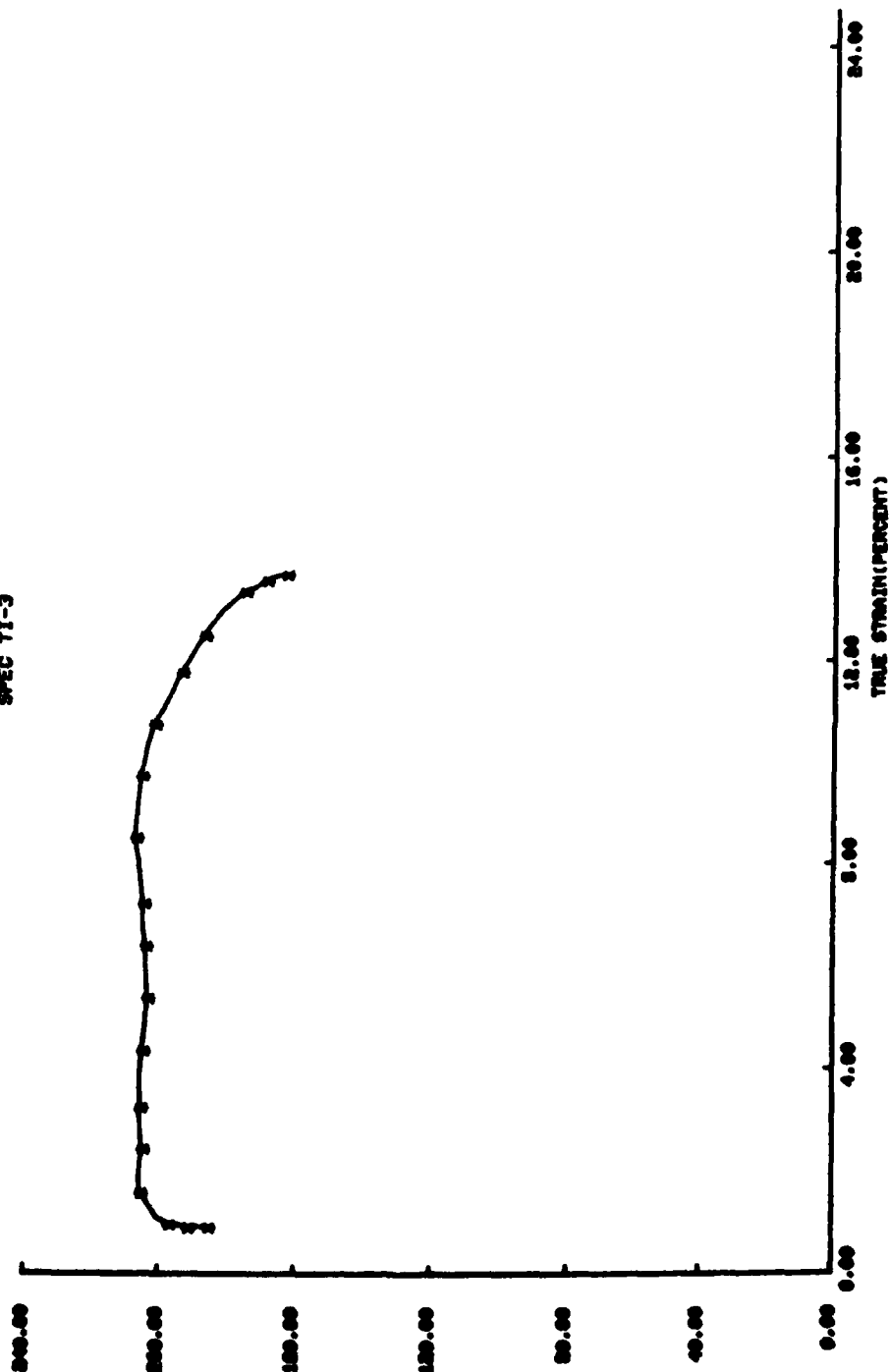


HOPKINSON BAR--TENSILE
 500 STRAIN/SEC
 BAL-100-10 TITANIUM
 SPEC TI-2



7-22-64 00-000000-1 100-10

HOPKINSON BAR--TENSILE
 550 STRAIN/SEC
 BAL-100-10 TITANIUM
 SPEC TI-3



1-10-68 10:00 AM

TE
MED
82