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LINEAR THEORY OF THE E X B INSTABILITY WITH AN
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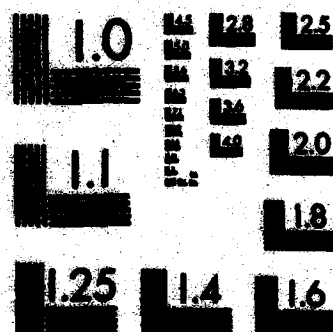
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20. Abstract (Continued)

of the analysis are as follows. First, the inhomogeneous velocity flow caused by the inhomogeneous electric field can stabilize the instability. Second, short wavelength modes are preferentially stabilized over longer wavelength modes. Third, the stabilization mechanism is associated with the x dependent, Doppler-shifted frequency $\omega - k_y V_y(x)$ where $V_y(x) = -cE_z(x)/B_0$ and not velocity shear terms proportional to $\partial V_y / \partial x$. And fourth, the marginal stability criterion is weakly dependent on the magnitude of B_0 . Applications of these results to ionospheric phenomena are discussed, viz., barium cloud structure and high latitude F region irregularities.

$V_{sub y}$

$$\frac{\omega - k_{sub y} V_{sub y}(x)}{\omega \sin \theta}$$

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LINEAR THEORY OF THE $E \times B$ INSTABILITY WITH AN INHOMOGENEOUS ELECTRIC FIELD

I. INTRODUCTION

An important instability associated with the structuring of ionospheric plasmas (e.g., high latitude F region and barium clouds) is the $E \times B$ instability, also known as the gradient drift instability. The instability is an interchange instability which can occur in an inhomogeneous, weakly collisional, magnetized plasma that contains an ambient electric field orthogonal to both the ambient magnetic field and the density gradient. A simple physical picture of the instability mechanism is shown in Fig. 1. We consider a plasma such that $B = B \hat{e}_z$, $E = E \hat{e}_y$, $n = n(x)$ with $\partial n / \partial x > 0$ and $v_{en} / \Omega_e \ll v_{in} / \Omega_i \ll 1$ where $v_{\alpha n}$ is the collision frequency between species α and neutrals, and Ω_α is the cyclotron frequency of species α . Upon this plasma we impose a density perturbation $\delta n \sim \delta n \sin(k_y y)$ as shown in Fig. 1. The influence of E on the plasma is to cause (1) the electrons and ions to $E \times B$ drift in the x direction and (2) an ion Pedersen drift in the y direction. The latter effect induces a space charge perturbation electric field denoted by δE . The response of the plasma to this perturbed electric field is to drift with a velocity $\delta v = c \delta E \times B / B^2$. For the configuration shown in Fig. 1, δv causes the "heavy" fluid perturbation to fall into the "light" fluid (region I), and the "light" fluid perturbation to rise into the "heavy" fluid (region II) - the classic interchange phenomenon. Of course, if the direction of $\partial n / \partial x$ or E_y were reversed then the density perturbation would be damped.

The original study of the $E \times B$ instability was by Simon (1963) and Boh (1963), who applied it to laboratory gas discharge experiments.

Subsequent to these first investigations, a considerable amount of

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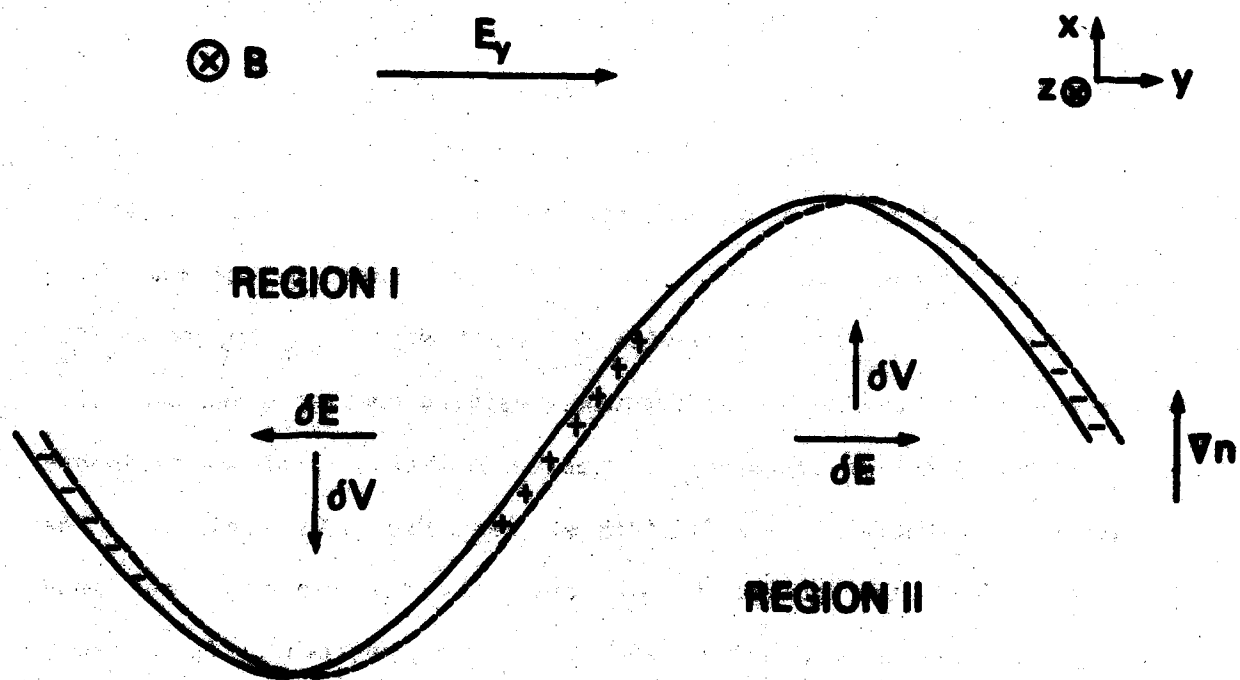


Fig. 1 Schematic of the physical mechanism of the $\mathbf{E} \times \mathbf{B}$ instability.

research has been devoted to explaining ionospheric phenomena based upon this instability (Linson and Workman, 1970 and references therein; Simon, 1970; Volk and Haerendel, 1971; Perkins et al., 1973; Zabusky et al., 1973; Shiau and Simon, 1972; Perkins and Doles, 1975; Scannapieco et al., 1976; Chaturvedi and Ossakow, 1979; Keskinen and Ossakow, 1982). Two areas of present interest concerning the instability are barium cloud striations (see for example the review papers Ossakow (1979) and Ossakow et al. (1982), and the references therein) and the structuring of plasma "blobs" in the high latitude F region (Vickrey et al., 1980; Keskinen and Ossakow, 1982).

The purpose of this paper is to present a general theory of the $\mathbf{E} \times \mathbf{B}$ instability which considers an ambient electric field at an arbitrary angle to the density gradient, and allows the electric field component parallel to the density gradient to be inhomogeneous. Some aspects of the problem have been treated by Perkins et al. (1973) and Perkins and Doles (1975). Perkins and Doles (1975) made the important discovery that the sheared velocity flow (resulting from an inhomogeneous electric field parallel to the density gradient) can stabilise the instability. Furthermore, short wavelength modes are preferentially stabilised over longer wavelength modes. The work of Perkins and Doles (1975) considered the strong collision limit ($v_{in} \gg \omega$), assumed a specific density profile amenable to analytical theory, and is valid only in the short wavelength regime, i.e., $k_y L \gg 1$ where L is the scale length of the boundary layer. The present study extends the theory of Perkins and Doles (1975) by removing these restrictions. Namely, we derive a differential equation which describes the mode structure of the $\mathbf{E} \times \mathbf{B}$ instability. Ion inertia effects are included so that the ratio v_{in}/ω is arbitrary. Moreover, we

solve this equation numerically so that arbitrary density and electric field profiles can be considered, and the regime $k_y L < 1$ can be investigated self-consistently.

The principal results of this work are the following.

1. The basic conclusions of Perkins and Doles (1975) are verified numerically. Specifically, the marginal stability criterion they derive analytically agrees well with our numerical result.

2. The marginal stability criterion is weakly dependent upon the magnitude of v_{in}/ω .

3. The stabilization mechanism is associated with the x dependent, Doppler-shifted frequency $\omega - k_y V_y(x)$, where $V_y(x) = -cE_x(x)/B$, and not velocity shear terms proportional to $\partial V_y/\partial x$ or $\partial^2 V_y/\partial x^2$.

4. When $E_x(x_0) \gtrsim E_y$, where x_0 is the position about which the mode is localized, the most unstable modes have $k_y L \lesssim 1$.

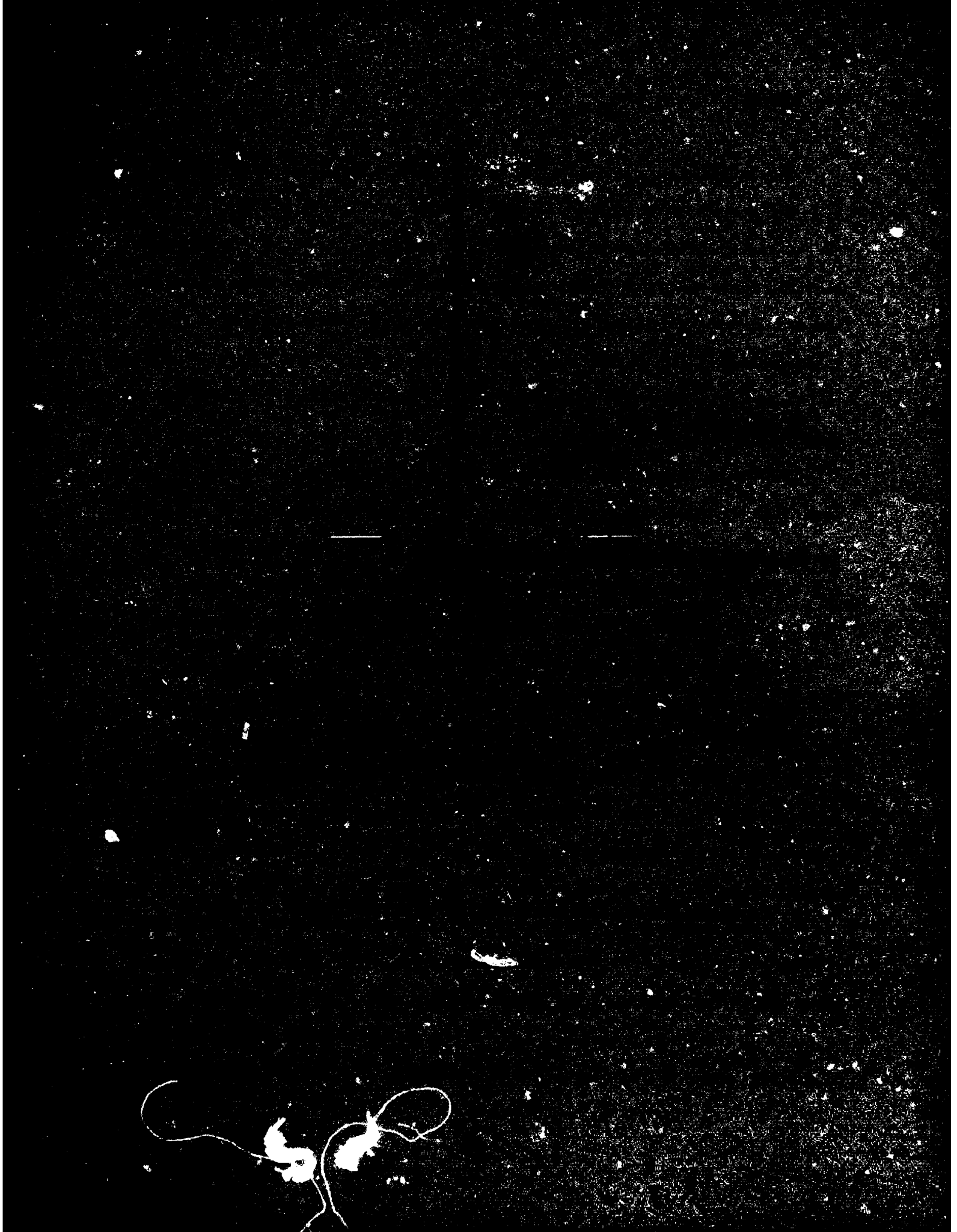
The organization of the paper is as follows. In Section II we derive the mode structure equation for the $E \times E$ instability. In Section III we present both analytical and numerical results based upon this equation. Finally, in Section IV we summarize our results and discuss applications to ionospheric phenomena, i.e., barium cloud striations and high latitude F region irregularities.

II. THEORY

The equilibrium configuration used in the analysis is shown in Fig. 2. The ambient magnetic and electric fields are in the z direction and the xy plane, respectively, where $\mathbf{B} = B \hat{\mathbf{e}}_z$ and $\mathbf{E} = E_x(x) \hat{\mathbf{e}}_x + E_y \hat{\mathbf{e}}_y$. The electric field in the y direction is constant, while the electric field in the x direction is allowed to be a function of x . This gives rise to an inhomogeneous velocity flow in the y direction, i.e., $V_y(x) = -cE_x(x)/B$. The density is taken to be inhomogeneous in the x direction ($n = n(x)$) and temperature effects are ignored.

The basic assumptions used in the analysis are as follows. We assume that the perturbed quantities vary as $\delta p \sim \delta p(x) \exp [i(k_y y - \omega t)]$, where k_y is the wave number along y direction and $\omega = \omega_r + i\gamma$, implying growth for $\gamma > 0$. The ordering in the frequencies is such that $\omega \ll \Omega_i$ and $\nu_{in} \ll \Omega_i$ (the F region approximation), where ν_{in} is the ion-neutral collision frequency and Ω_i is the ion gyrofrequency. We neglect terms of order ω/Ω_i and ν_{in}/Ω_i , but retain terms of order ν_{in}/ω . We ignore finite gyroradius effects by limiting the wavelength domain to $kr_{Li} \ll 1$, where r_{Li} is the mean ion Larmor radius. We neglect perturbations along the magnetic field ($k_z = 0$) so that only the two-dimensional mode structure in the xy plane is obtained. We retain ion inertial effects, thereby including the ion polarization drift, but ignore electron inertia.

A key feature of our analysis is that a nonlocal theory is developed. That is, the mode structure of the potential in the x direction, the direction in which density and the flow velocity are assumed to vary, is determined by a differential equation rather than an algebraic equation obtained by Fourier analysis. This is crucial to the



analysis since Perkins and Doles (1975) have shown that a nonlocal analysis is necessary to demonstrate the stabilizing influence of velocity shear, due to the inhomogeneous electric field parallel to the density gradient.

The fundamental equations used in the analysis are continuity and momentum transfer:

$$\frac{\partial n_\alpha}{\partial t} + \nabla \cdot (n_\alpha \mathbf{V}_\alpha) = 0 \quad (1)$$

$$0 = -\frac{e}{m_e} (\mathbf{E} + \frac{1}{c} \mathbf{V}_e \times \mathbf{B}) \quad (2)$$

$$\left(\frac{\partial}{\partial t} + \mathbf{V}_1 \cdot \nabla \right) \mathbf{V}_1 = \frac{e}{m_i} (\mathbf{E} + \frac{1}{c} \mathbf{V}_1 \times \mathbf{B}) - v_{in} \mathbf{V}_1 \quad (3)$$

where α denotes species (e : electrons, i : ions) and other variables have their usual meaning. Note that electron inertia terms are neglected, but ion inertia terms are included, and that the neutral wind is assumed to be zero. The equilibrium drifts are

$$\mathbf{V}_e = -cE_x(x)/B \hat{e}_y \quad (4)$$

$$\begin{aligned} \mathbf{V}_1 = & \left((v_{in}/\Omega_1) cE_x(x)/B + (cE'_x(x)/B\Omega_1) cE_y/B \right) \hat{e}_x \\ & + \left(-cE_x(x)/B + (v_{in}/\Omega_1) cE_y/B \right) \hat{e}_y \end{aligned} \quad (5)$$

where we have chosen a reference frame such that $\mathbf{V}_x = \mathbf{V}_x - cE_y/B$, $\Omega_1 = eB/m_1c$ and $E'_x(x) = \partial E_x/\partial x$. A relationship between $n(x)$ and $E_x(x)$ can be derived by assuming $\nabla \cdot \mathbf{J} = \nabla \cdot [n(\mathbf{V}_1 - \mathbf{V}_e)] = 0$ which reduces to

$$\nabla \cdot (n \underline{V}_1) = 0 \quad (6)$$

Equation (6) leads to

$$n(x) \left[(v_{in}/\Omega_1) cE_x(x)/B + (cE'_x(x)/B\Omega_1) cE_y/B \right] = \text{constant} \quad (7)$$

where we take the constant to be the LHS of Eq. (7) evaluated at $x = -\infty$. Thus, by specifying the density profile, the electric field profile $E_x(x)$ can be determined from Eq. (7). Of course, if there are sources and/or sinks in the plasma such that $\nabla \cdot (n \underline{V}_1) \neq 0$, then Eq. (7) is not applicable.

We now consider a linear perturbation analysis of Eqs. (1)-(3). We assume $n_\alpha = n_\alpha + \delta n_\alpha$, $\underline{V}_\alpha = \underline{V}_\alpha + \delta \underline{V}_\alpha$ and $\underline{E} = \underline{E} - \nabla \phi$ where ϕ is the perturbed electrostatic potential. Using Eqs. (2) and (3), we obtain

$$\delta V_{ex} = -ik_y \phi (c/B) \quad (8)$$

$$\delta V_{ey} = \phi' (c/B) \quad (9)$$

$$\delta V_{ix} = (-ik_y(1 - V'_{iy}/\Omega_1) \phi + i(\bar{\omega}/\Omega_1) \phi' - (V_{ix}/\Omega_1) \phi'') (c/B) \quad (10)$$

$$\delta V_{iy} = (-k_y(\bar{\omega}/\Omega_1 + i V'_{ix}/\Omega_1) \phi + (1 - ik_y V_{ix}/\Omega_1) \phi') (c/B) \quad (11)$$

where $\bar{\omega} = \omega + iv_{in} - k_y V_{iy}$, $V'_{iy} = \partial V_{iy}/\partial x$, $V'_{ix} = \partial V_{ix}/\partial x$, $\phi' = \partial \phi / \partial x$ and $\phi'' = \partial^2 \phi / \partial x^2$. Substituting Eqs. (8) - (11) into Eq (1), one can show that for the ions

$$\begin{aligned}
& -\frac{B}{c} \frac{\Omega_1}{\bar{\omega}} \left(\omega^* \frac{\delta n_1}{n} + i v_{1x} \frac{\delta n_1'}{n} \right) + i \frac{v_{1x}}{\bar{\omega}} \phi^{''''} + \left(1 + i \frac{n'}{n} \frac{v_{1x}}{\bar{\omega}} \right) \phi^{'''} \\
& + \left(-i k_y^2 \frac{v_{1x}}{\bar{\omega}} + \frac{n'}{n} + i \frac{v_{1x}}{\Omega_1} \left(\frac{n'}{n} \right)' \right) \phi'' + \left(-k_y^2 \left(1 + \frac{v_{1x}}{\bar{\omega}} \right) + \frac{k_y v_{1y}'}{\bar{\omega}} \right. \\
& \left. + \frac{n'}{n} \frac{k_y v_{1y}'}{\bar{\omega}} - \frac{n'}{n} \frac{k_y \Omega_1}{\bar{\omega}} \right) \phi = 0
\end{aligned} \tag{12}$$

and for the electrons

$$\frac{\delta n_e}{n} = -\frac{c}{B} \frac{k \phi}{(\omega - k_y v_{ey})} \frac{n'}{n} \tag{13}$$

where $\omega^* = \omega - k_y v_{1y} + i v_{1x}'$ and the superscripts ($'$, $''$, $'''$) indicate first, second and third derivatives with respect to x , respectively.

We assume quasineutrality and take $\delta n_e = \delta n_1$. The following equation is then obtained from Eqs. (12) and (13),

$$\begin{aligned}
& i \frac{v_{1x}}{\bar{\omega}} \phi^{''''} + \left(1 + i \frac{n'}{n} \frac{v_{1x}}{\bar{\omega}} \right) \phi^{'''} + \left(\frac{n'}{n} + i \frac{k_y v_{1x}}{\bar{\omega}} \left(-k_y + \frac{\bar{\omega}}{\Omega_1} \frac{1}{k_y} \left(\frac{n'}{n} \right)' \right) \right. \\
& \left. + \frac{\Omega_1}{\omega - k_y v_{ey}} \frac{n'}{n} \right) \phi'' + \left(-k_y^2 \left(1 + \frac{v_{1x}}{\bar{\omega}} \right) + \frac{k_y v_{1y}'}{\bar{\omega}} + \frac{n'}{n} \frac{k_y v_{1y}'}{\bar{\omega}} \right. \\
& \left. + i \frac{k_y v_{1x}}{\omega - k_y v_{ey}} \frac{\Omega_1}{\bar{\omega}} \frac{n'}{n} - i \frac{k_y v_{ey}'}{\omega - k_y v_{ey}} \frac{n'}{n} \frac{v_{1n}}{\bar{\omega}} \frac{\omega}{\omega - k_y v_{ey}} \right. \\
& \left. - \frac{v_{1n}}{\bar{\omega}} \frac{n'}{n} \frac{k_y}{\omega - k_y v_{ey}} k_y (c E_y / B) \right) \phi = 0
\end{aligned} \tag{14}$$

We simplify Eq. (14) by assuming the following ordering scheme: $\partial/\partial x \ll k_y$, $v_{in}/\Omega_1 \ll 1$, $V' = V/L$, $V'' = V/L^2$, $k_y L \ll \Omega_1/v_{in}$, $k_y L \ll \Omega_1/\omega$ where L is the scale length of the inhomogeneous plasma boundary layer. Equation (14) can now be written as

$$\begin{aligned} \phi'' + \left(\frac{n'}{n} \left(1 - \frac{iv_{in}}{\tilde{\omega}} \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \right) \right) \phi' \\ + \left(-k_y^2 - \frac{k_y (cE_y/B)}{\tilde{\omega} + iv_{in}} \frac{v_{in}}{\tilde{\omega}} \frac{k_y n'}{n} + \frac{n'}{n} \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \right. \\ \left. - \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \frac{iv_{in}}{\tilde{\omega}} \left(\frac{n''}{n} + \frac{V_{ey}}{V_{ey}} \frac{n'}{n} \frac{\omega}{\tilde{\omega}} \right) \right) \phi = 0 \end{aligned} \quad (15)$$

where $\tilde{\omega} = \omega - k_y V_{ey}(x) = \omega + k_y (cE_x(x)/B)$. Equation (15) describes the two-dimensional mode structure of ϕ for the $\underline{E} \times \underline{B}$ instability in a velocity sheared plasma for arbitrary v_{in}/ω .

III. RESULTS

A. Analytical Results

In general, Eq. (15) requires a numerical analysis for arbitrary density and electric field profiles. However, insight into the nature of the $\tilde{E} \times \tilde{E}$ instability can be gained by first considering several limiting cases.

1. Local Theory

We first reduce the differential equation, Eq. (15), to an algebraic equation by making use of local theory. That is, we let $\partial/\partial x \rightarrow ik_x$, and assume $k_x^2 L_n^2 \gg 1$ and $k_y^2 L_n^2 \gg 1$ where $L_n = (n'/n)^{-1}$ is the scale length of the density inhomogeneity evaluated at $x = x_0$. For simplicity, we also take $\tilde{E} = E_x \hat{e}_x + E_y \hat{e}_y = \text{constant}$. In this limit, Eq. (15) becomes

$$k_x^2 L_n^2 + k_y L_n \frac{v_{in}}{\tilde{\omega}} \frac{k \cdot \tilde{E} (c/B)}{\tilde{\omega} + i v_{in}} = 0 \quad (16)$$

where $\tilde{\omega} = \omega - k_y v_{ey}$ and $v_{ey} = -cE_x/B$. Equation (16) has the solution

$$\tilde{\omega} = -i \frac{v_{in}}{2} \left[1 \mp \left(1 + 4 \frac{k_y}{k} \frac{k \cdot \tilde{E} (c/B)}{v_{in} k L_n} \right)^{1/2} \right] \quad (17)$$

Instability occurs when

$$\frac{k_y}{k} \frac{k \cdot \tilde{E}}{k L_n} > 0. \quad (18)$$

The growth rates of the instability in the strong and weak collisional limits are, respectively,

$$\gamma = \frac{k_y}{k} \frac{k \cdot E (c/B)}{k L_n} \quad ; v_{in} \gg \omega \quad (19)$$

$$\gamma = \frac{k_y}{k} \left(\frac{k \cdot E (c/B)}{k L_n} v_{in} \right)^{1/2} \quad ; v_{in} \ll \omega \quad (20)$$

with a real frequency $\omega = k_y V_{ey}$ in each case. Note that instability can occur for $E_y = 0$ as long as $k_y \neq 0$ and $E_x \neq 0$ (Eq. (18); see also Maskinen and Ossakow (1982). For $k = k_y$, one obtains the usual $E \times B$ gradient drift instability growth rate (Linson and Workman, 1971) in Eq. (19), and the so-called high altitude limit (Ossakow et al., 1978) of the $E \times B$ gradient drift instability in Eq. (20).

2. Nonlocal Theory

In deriving Eq. (16) the local approximation is used. That is, the dispersion equation is solved based upon the plasma parameters at a particular value of x , say $x = x_0$; usually where n'/n is a maximum which leads to maximum growth. If we now assume $E_x = E_x(x)$ then a sheared $E \times B$ velocity flow arises $V_y = V_{ey}(x) = -cE_x(x)/B$. Applying local theory to this situation, one might expect that Eq. (16) is still valid with V_{ey} evaluated at x_0 , i.e., $V_{ey} = V_{ey}(x_0)$. Thus, Eqs. (19) and (20) follow accordingly, but the real frequency is now given by $\omega_r = k_y V_{ey}(x_0)$. However, Perkins and Doles (1975) have shown, both analytically and using numerical simulations, that this is not the case. We do not reproduce their detailed analysis here, but rather, point out the important result of their work.

Perkins and Doles (1975) consider the strong collision limit ($v_{in} \gg \omega$) so that ion inertia terms can be neglected. Furthermore,

they assume $\nabla \cdot (n \mathbf{V}) = 0$ which leads to

$$n(x) E_x(x) = n_0 E_{ox} = \text{constant} \quad (21)$$

where $n_0 = n(x = -\infty)$ and $E_{ox} = E_x(x = -\infty)$. This is evident from Eq. (7) by noting that $E'_x(x) \sim E_x/L_n$ and $v_{in} \gg \omega \sim cE_y/BL_n$. In this limit, Eq. (15) reduces to

$$\begin{aligned} \phi'' + \left[\frac{n'}{n} \left(1 - \frac{k v_{ey}}{\tilde{\omega}} \right) \right] \phi' \\ + \left[-k_y^2 + 1 - \frac{k_y (cE_y/B)}{\tilde{\omega}} \frac{k_y n'}{n} - \frac{k_y v_{ey}}{\tilde{\omega}} \left(\frac{n'}{n} + \frac{V'_{ey}}{v_{ey}} \frac{n'}{n} \frac{\omega}{\tilde{\omega}} \right) \right] \phi = 0 \end{aligned} \quad (22)$$

where $\tilde{\omega} = \omega - k_y v_{ey}$, $v_{ey} = -(cE_{ox}/B)(n_0/n(x))$ and $V'_{ey} = -(cE_{ox}/B)(n_0/n(x))'$. Perkins and Doles (1975) expand Eq. (22) about $x = x_0$ where x_0 is the position of maximum n'/n by taking

$$n'/n = [1 - (x - x_0)^2/D^2]/L_n \quad (23)$$

Assuming $k_y^2 L_n^2 \gg 1$ and $k_y^2 D^2 \gg 1$, and by making several variable changes, they solve Eq. (22) analytically. The important conclusion of their theory is that the $\mathbf{E} \times \mathbf{B}$ instability is stabilized when

$$\frac{E_x(x_0)}{E_y} > \frac{2}{k_y D} \quad (24)$$

Thus, the influence of velocity shear, i.e., an inhomogeneous E_x , is to preferentially stabilize the short wavelength modes, those with $k_y D \gg 1$.

B. Numerical Results

In order to solve Eq. (15) numerically, and also to gain insight into the nature of the solutions, we transform Eq. (15). First, we note that Eq. (15) is of the form

$$\phi'' + p(x) \phi' + q(x) \phi = 0 \quad (25)$$

where $p(x)$ and $q(x)$ are the coefficients of ϕ' and ϕ , respectively, in Eq. (15). We let

$$\phi = \tilde{\phi} \exp(-1/2 \int p(s) ds) \quad (26)$$

Substituting Eq. (26) into Eq. (25), we find that the transformed equation is

$$\tilde{\phi}'' - Q(x) \tilde{\phi} = 0 \quad (27)$$

where

$$Q(x) = -q(x) + 1/2 p'(x) + 1/4 (p(x))^2 \quad (28)$$

and

$$p(x) = \frac{n'}{n} \left(1 - \frac{iv_{in}}{\tilde{\omega}} \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \right) \quad (29)$$

$$p'(x) = \left(\frac{n''}{n} - \left(\frac{n'}{n} \right)^2 \right) \left(1 - \frac{iv_{in}}{\tilde{\omega}} \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \right)$$

$$- \frac{n'}{n} \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \frac{iv_{in}}{\tilde{\omega}} \left(1 + \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} + \frac{k_y V_{ey}}{\tilde{\omega}} \right) \quad (30)$$

$$q(x) = -k_y^2 - \frac{k_y (cE/B)}{\tilde{\omega} + iv_{in}} \frac{v_{in}}{\tilde{\omega}} \frac{k_y n'}{n} + \frac{n'}{n} \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}}$$

$$- \frac{k_y V_{ey}}{\tilde{\omega} + iv_{in}} \frac{iv_{in}}{\tilde{\omega}} \left(\frac{n''}{n} + \frac{V_{ey}}{V_{ey}} \frac{n'}{n} \frac{\omega}{\tilde{\omega}} \right) \quad (31)$$

Equation (27) has a simple form, albeit $Q(x)$ is a complicated function of x , which allows physical insight into the nature of the mode structure. As an example, if Q is real and has $Q > 0$ for $|x| > x_0$ and $Q < 0$ for $|x| < x_0$ then one would expect a bounded solution of $\tilde{\phi}$ in the region $|x| < x_0$ that exponentially decays for $|x| > x_0$.

We now solve Eq. (27) numerically for a variety of conditions to better understand the influence of an inhomogeneous electric field on the $E \times E$ instability. In all of the cases presented, the following density profile is assumed

$$n(x) = n_0 \frac{1 + \epsilon \tanh(x/L)}{1 - \epsilon} \quad (32)$$

where $0 < \epsilon < 1$, L characterizes the width of the boundary layer, and $n_0 = n(x = -\infty)$. By varying ϵ , the magnitude of the density gradient scale length L_n ($L_n = (n'/n)^{-1}$) can be changed. That is, as $\epsilon \rightarrow 0$, $L_n \rightarrow \infty$ (a constant density profile); as $\epsilon \rightarrow 1$, the value of $L_n \rightarrow 0$ (a rapidly changing density profile). We assume $\epsilon = 0.95$ for the results presented so that

$$\left(\frac{n'}{n}\right)_{\max} = 1.45 L^{-1} \quad \text{at } x/L = -0.9 \quad (33)$$

The maximum growth rate of the instability is expected to be

$$\gamma_m = 1.45 (V_0/L) \quad (34)$$

where $V_0 = cE_0/B$ and we have used Eq. (19) assuming $E = E_0 \hat{e}_y$.

The ambient electric field is chosen to be

$$\underline{E}(x) = E_x(x) \hat{e}_x + E_y \hat{e}_y \quad (35)$$

where

$$\underline{E}(x = -\infty) = E_0 \sin \theta \hat{e}_x + E_0 \cos \theta \hat{e}_y \quad (36)$$

so that $\theta = \tan^{-1} (E_x/E_y)$ at $x = -\infty$. The influence of the x component of the electric field is then studied by varying θ , the angle between $\underline{E}$ and $\hat{e}_y$ at $x = -\infty$. Two forms of $E_x(x)$ are considered in the analysis:

$$E_x(x) = E_0 \sin \theta = \text{constant} \quad (37)$$

and

$$E_x(x) = E_0 \sin \theta (n_0/n(x)) \neq \text{constant} \quad (38)$$

These allow us to contrast the effects of no velocity shear and velocity shear on the instability. We comment that Eq. (38) is an equilibrium solution which satisfies $\nabla \cdot (n \underline{V}_1) = 0$ in the strong collisional limit $v_{in} \gg \omega$ (i.e., Eq. (7)).

In Fig. 3 we plot $\tilde{\gamma} = \gamma/(V_0/L)$ vs $k_y L$ for $\theta = 0^\circ$ and 90° and $\tilde{v} = v/(V_0/L) = 1.0$ and 100.0 , where E_x is chosen to be constant (Eq. (37)) and $V_0 = cE_0/B$. A general comment on all of the curves shown is that $\tilde{\gamma}$ is an increasing function $k_y L$, but $\tilde{\gamma}$ asymptotes to a constant value independent of $k_y L$ for $k_y^2 L^2 \gg 1$. This is consistent with the predictions of local theory. The "standard" case is $\theta = 0^\circ$, that is, $\underline{E} = E_y \hat{e}_y$ and there is no component of $\underline{E}$ parallel to the density gradient. For this case, two values of $\tilde{v}$ are chosen: strong collisions ($\tilde{v} = 100.0$) and weak

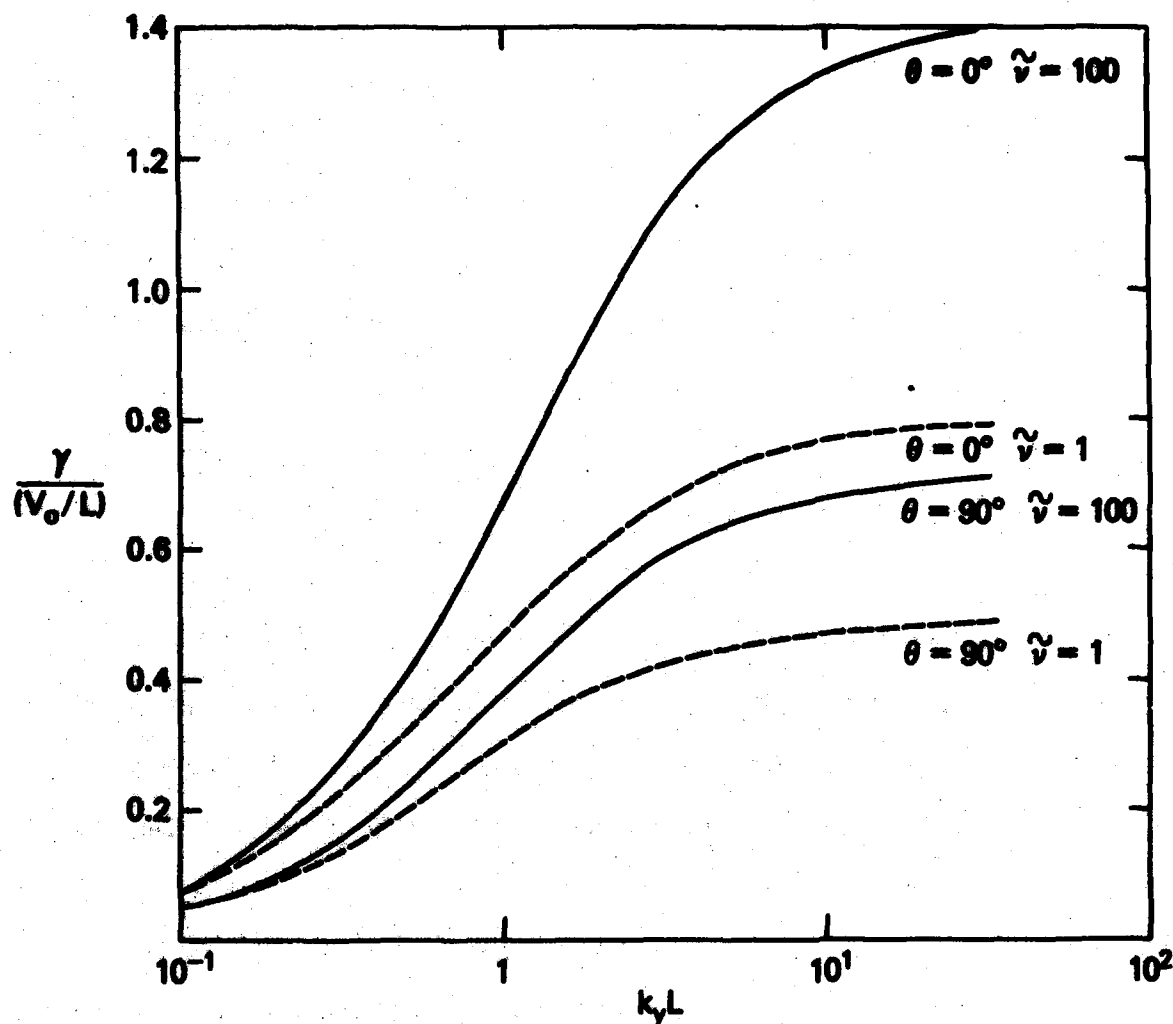


Fig. 3 Plot of $\tilde{\gamma} = \gamma/(V_0/L)$ vs. $k_y L$ for $\theta = 0^\circ$ and 90° , and for $\tilde{\nu} = v_{in}/(V_0/L) = 1.0$ and 100.0 . The electric field E_x is assumed to be constant (Eq. (37)).

collisions ($\tilde{\nu} = 1.0$). As is expected, the growth rate is larger for the larger value of $\tilde{\nu}$ in the short wavelength regime ($k_y L > 1$). Also, the growth rate for $\tilde{\nu} = 100.0$ at $k_y L = 30$ is $\tilde{\gamma} = 1.39$, and is still increasing, although slowly, as a function of $k_y L$. This value of $\tilde{\gamma}$ agrees well with the value obtained from local theory ($\tilde{\gamma} = 1.45$ from Eq. (33)). The growth rate for the weak collision case $\tilde{\nu} = 1.0$ asymptotes to a somewhat smaller value of $\tilde{\gamma}$ ($\tilde{\gamma} = 0.79$). However, note that the difference between the growth rates for the strong and weak collisional cases becomes smaller as $k_y L \rightarrow 0$, and that the growth rates are, in fact, comparable for $k_y L = 0.1$. The "non-standard" case is $\theta = 90^\circ$, or $\underline{E} = E_x \hat{e}_x$ and the only component of $\underline{E}$ is along the density gradient. The major result of this limit is simply that the instability can still persist even though $E_y = 0$. The overall influences of $\tilde{\nu}$ and $k_y L$ on the instability are the same as in the previous case, $\theta = 90^\circ$.

In Fig. 4 we plot $\tilde{\gamma}$ vs. $k_y L$ for $\theta = 0^\circ$ and 70° and $\tilde{\nu} = 1.0$ and 100.0 , but consider E_x to be a function of x as in Eq. (38) so that velocity sheared flows occur for $\theta \neq 0^\circ$. The curves for $\tilde{\nu} = 1.0$ and 100.0 and $\theta = 0^\circ$ are shown for comparative purposes. The important results in this figure are as follows. First, the mode is stable for $k_y L \gtrsim 12$ for both the strong and weak collisional cases when $\theta = 70^\circ$. This is in agreement with the conclusion of Perkins and Doles (1975); velocity shear effects tend to stabilize the short wavelength modes, those such that $k_y^2 L^2 \gg 1$. The influence of shear on the long wavelength modes ($k_y L < 1$) is weakly stabilizing. Second, the difference in the growth rate curves for $\tilde{\nu} = 1.0$ and 100.0 is much less than that of the case of no shear (i.e., $\theta = 0$). And finally, since velocity shear can stabilize short wavelength modes before long wavelength modes, velocity

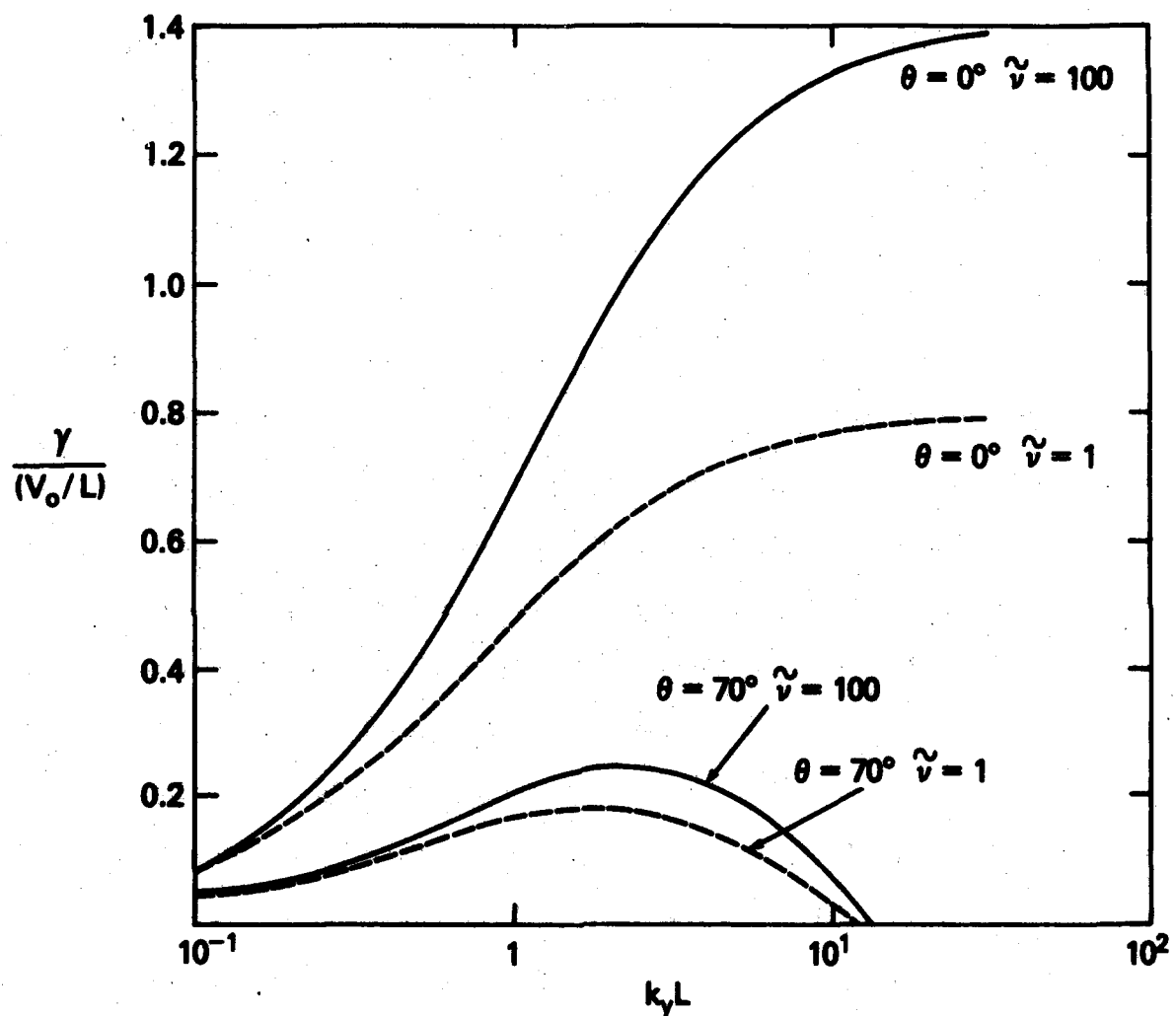


Fig. 4 Plot of $\tilde{\gamma} = \gamma/(V_0/L)$ vs. $k_y L$ for $\theta = 0^\circ$ and 70° , and for $\tilde{\gamma} = v_{in}/(V_0/L) = 1.0$ and 100.0 . The electric field E_x is assumed to be inhomogeneous (Eq. (38)).

small enough a differential wavelength λ is excited based upon linear theory. For the case above ($\lambda = 70^\circ$), the linear growth decreases as $\lambda \rightarrow 0$. Thus, velocity shear can lead to growth of long wavelength modes ($\lambda, \lambda = 1$), result from other wavelength modes ($\lambda, \lambda \gg 1$).

Figure 2 is a plot of Γ vs. λ, λ for $V = 100.0$ and $\epsilon = 10^2, 10^3, 10^4, 10^5$ and 10^6 . It is clear that a peak in the linear growth rate occurs because of velocity shear. However, as ϵ increases, the position of maximum growth decreases as a function of λ, λ . For $V = 10^2$ maximum growth occurs at $\lambda, \lambda = 10$ while for $V = 10^6$ maximum growth occurs at $\lambda, \lambda = 1.0$.

To further illustrate the influence of velocity shear on the $\lambda = 1$ instability, we consider the $\lambda = 1$ case at $V = 100.0$ and $\epsilon = 10^2, 10^3, 10^4, 10^5$ and 10^6 . For $\epsilon = 10^2$ and 10^3 , Γ is plotted in Figure 3 (a) and (b). Here, the value of Γ is plotted against λ, λ and the maximum value of Γ is plotted against λ, λ . For $\epsilon = 10^4, 10^5$ and 10^6 , Γ is plotted in Figure 3 (c), (d) and (e). For $\epsilon = 10^2$ and 10^3 , the maximum value of Γ is plotted against λ, λ and the maximum value of Γ is plotted against λ, λ . For $\epsilon = 10^4, 10^5$ and 10^6 , the maximum value of Γ is plotted against λ, λ and the maximum value of Γ is plotted against λ, λ . For $\epsilon = 10^2$ and 10^3 , the maximum value of Γ is plotted against λ, λ and the maximum value of Γ is plotted against λ, λ . For $\epsilon = 10^4, 10^5$ and 10^6 , the maximum value of Γ is plotted against λ, λ and the maximum value of Γ is plotted against λ, λ .

It is clear from the preceding discussion, an inhomogeneous electric field has a significant effect on the $\lambda = 1$ instability. However, for (27) to occur requires that a condition that naturally arises is, which can be taken to be (27) is responsible for stabilization of the

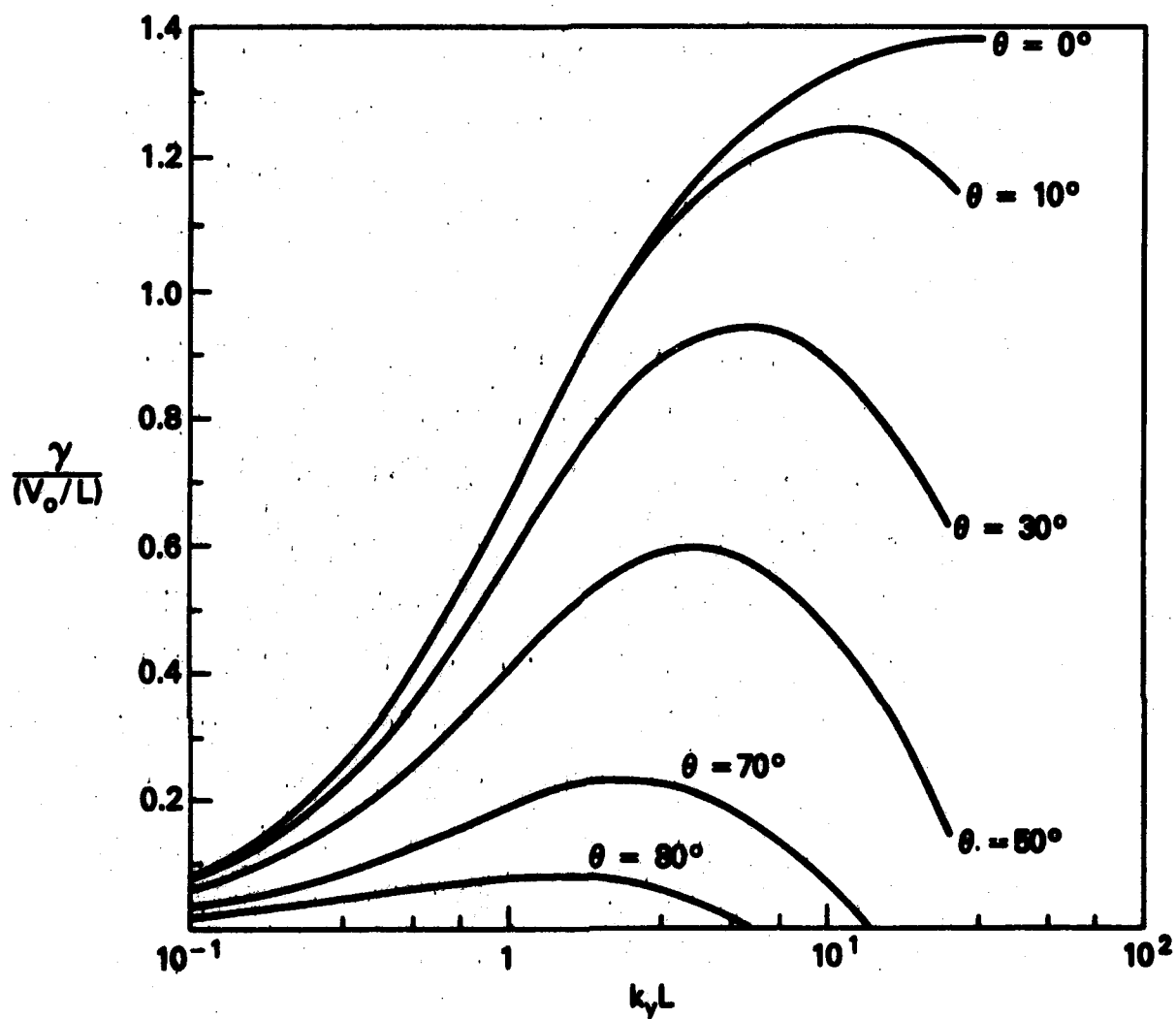


Fig. 5 Plot of $\tilde{\gamma} = \gamma/(V_0/L)$ vs. $k_y L$ for $\tilde{v} = v_{in}/(V_0/L) = 100.0$ and $\theta = 0^\circ, 10^\circ, 30^\circ, 50^\circ, 70^\circ$ and 80° .

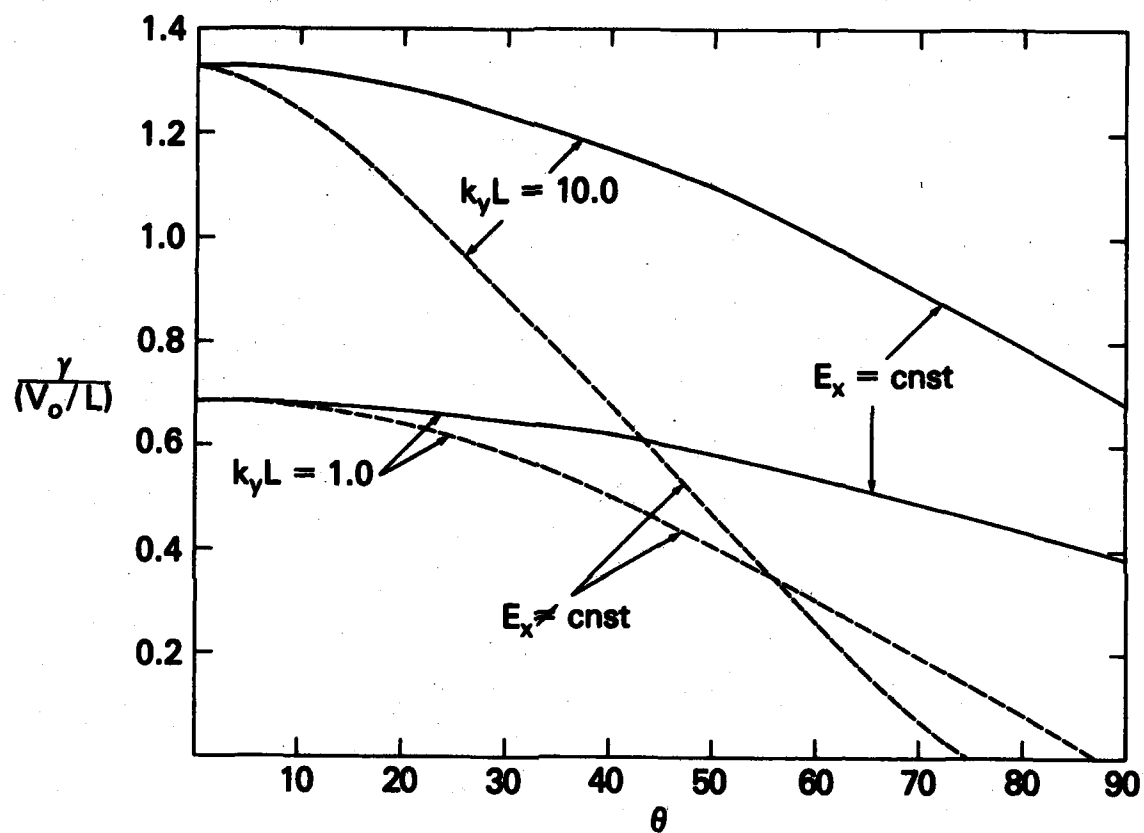


Fig. 6 Plot of $\tilde{\gamma} = \gamma / (V_o / L)$ vs θ for $\tilde{\gamma} = \gamma_{in} / (V_o / L) = 100.0$, $k_y L = 1.0$ and 10.0 , and $E_x = \text{cnst}$ (Eq. (37)) and $E_x \neq \text{cnst}$ (Eq. (38)).

mode? To shed light on this question, we consider the following simplified equation

$$\phi'' - \left[k_y^2 - i k_y \frac{k_y (cE_y/B)}{\omega - k_y V_{ey}(x)} \frac{n'}{n} \right] \phi = 0 \quad (39)$$

That is, we consider the limit $\tilde{\nu} \gg 1$ and retain the x -dependent, Doppler-shifted frequency $(\omega - k_y V_{ey}(x))$ as the only contribution of the inhomogeneous electric field profile. We neglect terms proportional to V_{ey}' , V_{ey}'' , and n'' . We emphasize that Eq. (39) is not the complete mode structure equation, but is solved and contrasted to the correct solution in order to isolate a single effect of the field inhomogeneity, viz., the x dependent resonance $\omega - k_y V_{ey}(x)$. In Fig. 7 we plot $\tilde{\gamma}$ vs. $k_y L$ for $\theta = 70^\circ$ and E_x is given by Eq. (38). The solid curve is the solution to Eq. (27) for $\tilde{\nu} = 100.0$, while the dashed curve is the solution to Eq. (39). Although there is a small difference between these curves for $k_y L < 1$, the important point is that the mode is stabilized at $k_y L = 13$ in both cases. Thus, the stabilization mechanism is related to the x dependent resonance $\omega - k_y V_{ey}(x)$, as opposed to velocity shear effects associated with terms proportional to V_{ey}' and V_{ey}'' . This is a key result of this analysis.

We now turn our attention to the mode structure associated with the $E_x \times B$ instability, and the influence of an inhomogeneous electric field on its structure. Figure 8 is a plot of the density profile $n(x)/n_0$ (Eq. (32) with $\epsilon = .095$) and the electric field profile $E_x(x)/E_{0x}$ (Eq. (38) with $E_{0x} = E_0 \sin \theta$) versus x/L . For $\theta = 0^\circ$, the electric field profile is simply $E_x(x)/E_{0x} = 0$. We present plots of Q and $\tilde{\phi}$ vs. x/L for these profiles. In the subsequent plots of Q and $\tilde{\phi}$, the subscript r denotes the

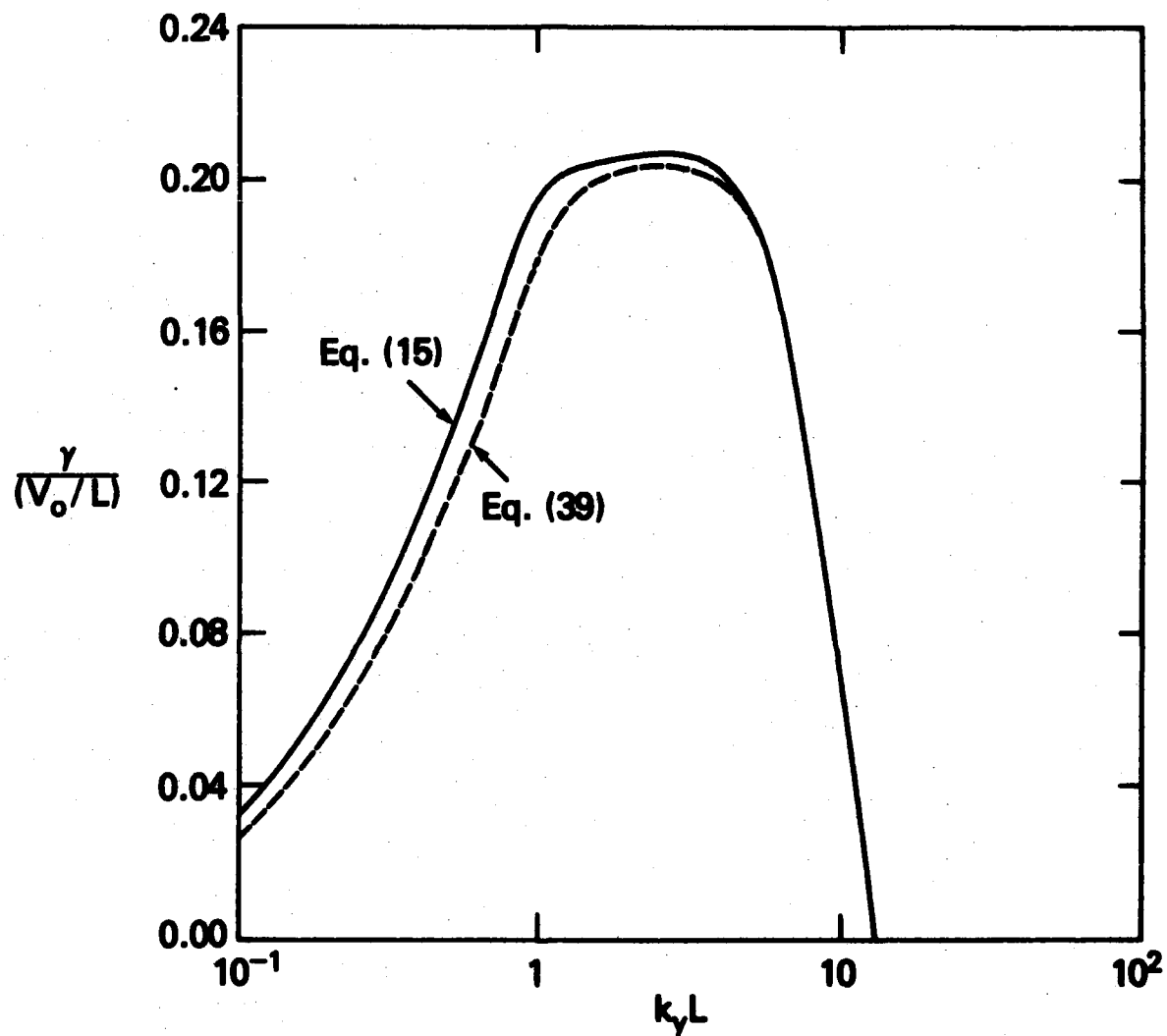


Fig. 7 Plot of $\tilde{\gamma} = \gamma/(V_0/L)$ vs $k_y L$ for $\tilde{\nu} = \nu_{in}/(V_0/L) = 100.0$ and $\theta = 70^\circ$ using Eq. (27) (solid curve) and Eq. (39) (dashed curve). The electric field E_x is assumed to be inhomogeneous (Eq. (38)).

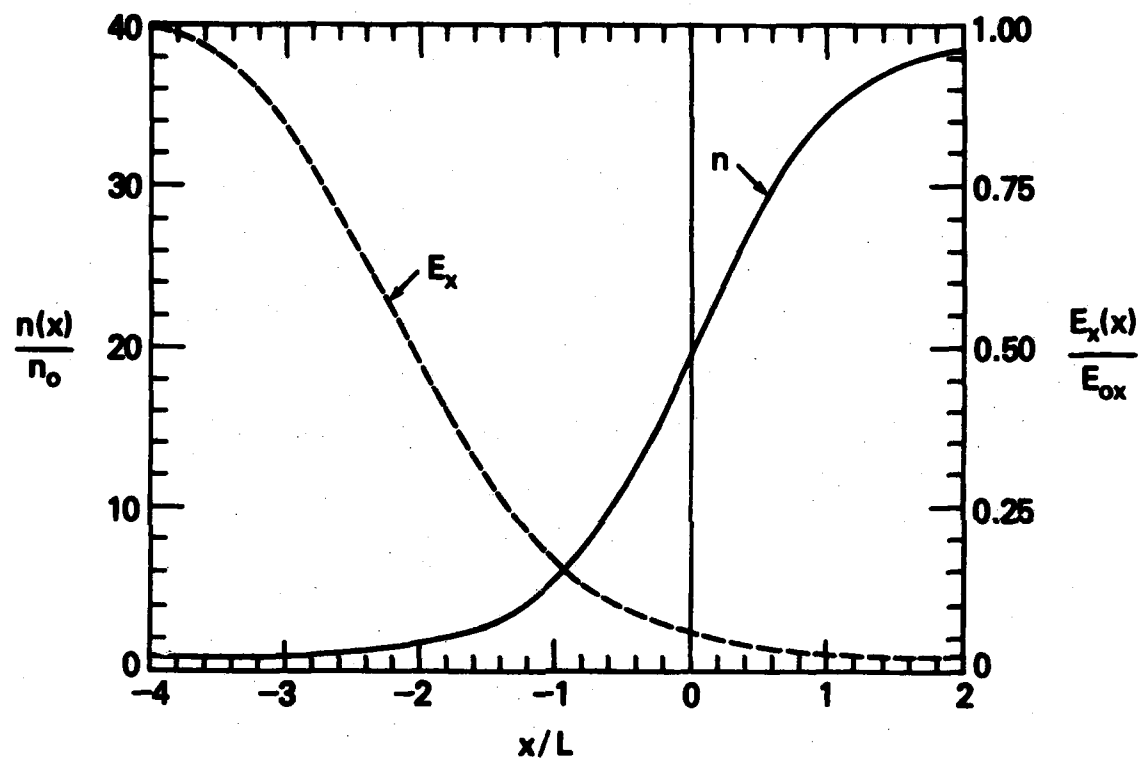


Fig. 8 Equilibrium density (Eq. (32)) and electric field (Eq. (38)) profiles for $\epsilon = 0.95$.

real part of Q or $\tilde{\phi}$, and i denotes the imaginary part of Q or $\tilde{\phi}$. The parameters considered for the first set of modes are $k_y L = 10.0$, $\tilde{\nu} = 100.0$, and $\theta = 0^\circ$ (Fig. 9) and $\theta = 70^\circ$ (Fig. 10). These modes are considered to be short wavelength modes since $k_y L \gg 1$.

Figure 9 is a plot of Q (Fig. 9a) and $\tilde{\phi}$ (Fig. 9b) versus x/L for the case of no electric field inhomogeneity ($\theta = 0^\circ$ or $E_x(x) = 0$). the eigenfrequency for the mode is $\tilde{\omega}_r = 0.0$ and $\tilde{\gamma} = 1.329$. the important points to note are the following. First, the wave potential Q is real and is such that $Q < 0$ for $-1.3 < x/L < -0.5$ and $Q > 0$ otherwise. Second, the wave potential Q achieves a minimum at $x/L = -0.9$, the position of maximum L_n (Eq. (33)). Third, consistent with this form of Q , the wave function $\tilde{\phi}$ is a bounded mode centered about $x/L = -0.9$ that falls off exponentially for $x/L > -0.5$ and $x/L < -1.3$. And finally, the wave function is reasonably broad in that its half-width at half maximum (Δx) is comparable to the width of the boundary layer, i.e., $\Delta x = L/2$.

Figure 10 is a plot of Q (Fig. 10a) and $\tilde{\phi}$ (Fig. 10b) versus x/L for the case of an inhomogeneous electric field ($\theta = 70^\circ$ and $E_x(x)$ is shown in Fig. 8). The eigenfrequency for this case is $\tilde{\omega}_r = 0.5307$ and $\tilde{\gamma} = 0.0716$. Note that the mode has a real frequency in contrast to the previous case and that the growth rate is smaller. Other important differences between this situation and the previous one are as follows. First, the wave potential Q is shifted to a larger value of x/L . The position of the minimum value of Q_r is at $x/L = -0.12$. Also, note that Q also has an imaginary component. Second, the wave function $\tilde{\phi}$ is the lowest order mode and has considerably more structure in x/L than the no shear case. Finally, the spatial extent of $\tilde{\phi}$ is somewhat narrower with $\Delta x = 0.1 L$.

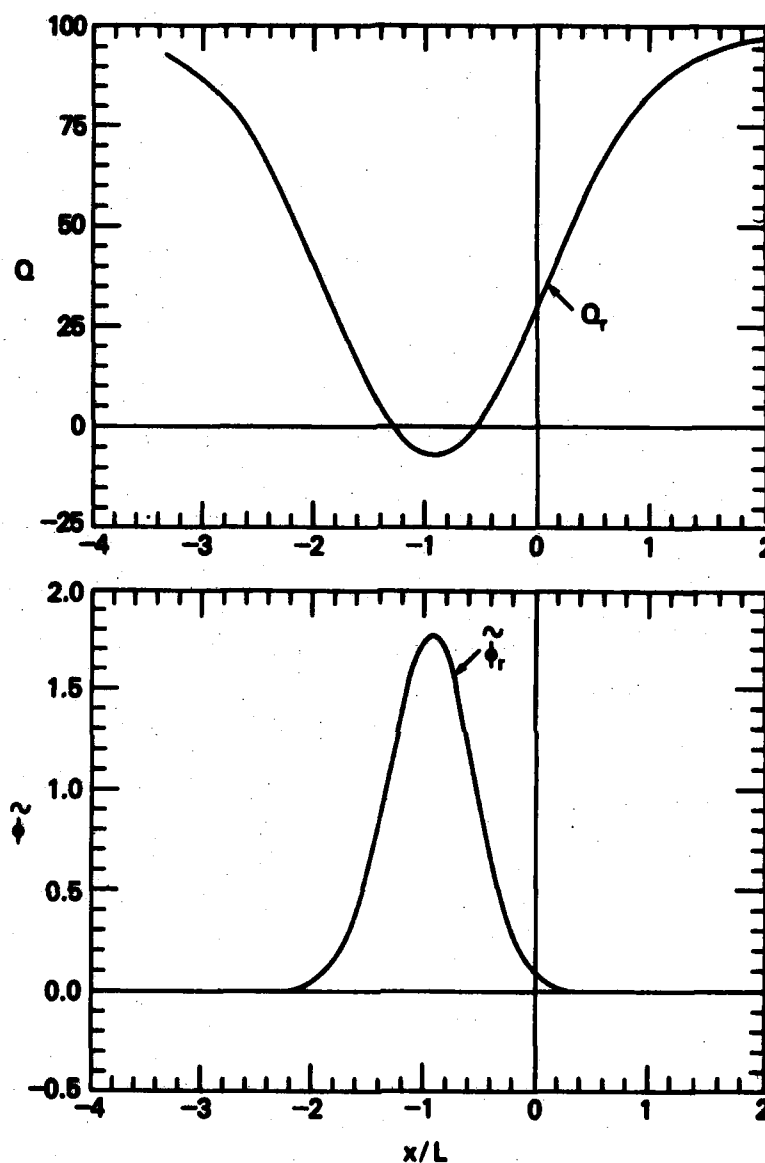


Fig. 9 Wave potential Q and wave eigenfunction $\tilde{\phi}$ as a function of x/L . The subscripts r and i denote real and imaginary, respectively. The parameters considered are $k_y L = 10.0$, $\tilde{\nu} = v_{in}/(v_o/L) = 100.0$ and $\theta = 0^\circ$ (i.e., $E_x = 0$). The eigenfrequency is $\tilde{\omega}_r = 0.0$ and $\tilde{\gamma} = 1.329$. (a) Q vs. x/L . (b) $\tilde{\phi}$ vs. x/L .

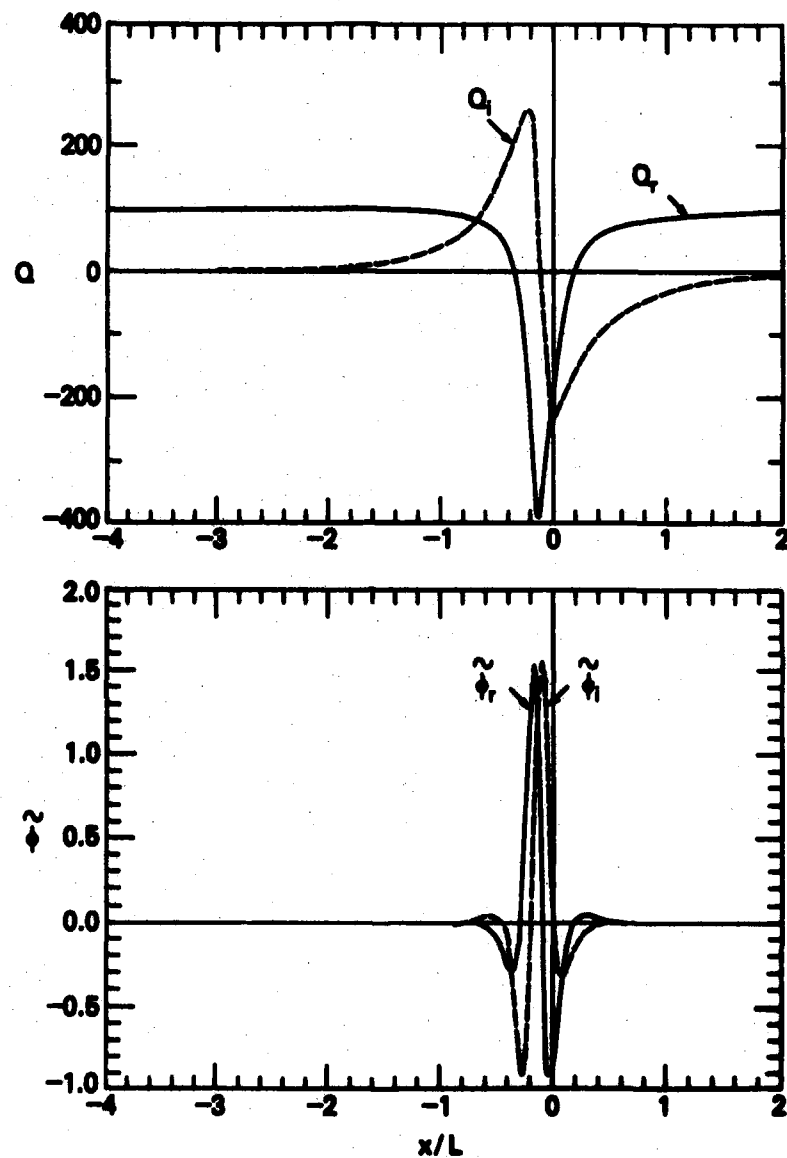


Fig. 10 Wave potential Q and wave eigenfunction as a function of x/L .

The subscripts r and i denote real and imaginary, respectively.

The parameters used are $k_y L = 10.0$, $\tilde{\nu} = \nu_{in}/(\nu_0/L) = 100.0$,

and $\theta = 70^\circ$ where k_x is given by Eq. (38). The eigenfrequency

is $\tilde{\omega}_r = 0.3307$ and $\tilde{\gamma} = 0.0716$. (a) Q vs. x/L . (b) $\tilde{\phi}$ vs. x/L .

A longer wavelength mode is now considered. We choose $k_y L = 0.1$ so that $k_y L \ll 1$, but still consider $\tilde{\nu} = 100.0$ as in the short wavelength case. Figure 11 is a plot of the density profile $n(x)/n_0$ and electric field profile $E_x(x)/E_{ox}$ for the same parameters as in Fig. 8. However, the range of x/L is expanded for comparison to the broadened mode structure. Figure 12 is a plot of Q (Fig. 12a) and $\tilde{\phi}$ (Fig. 12b) for the case of no electric field inhomogeneity ($\theta = 0^\circ$ or $E_x(x) = 0$). The eigenfrequency is $\tilde{\omega}_x = 0.0$ and $\tilde{\gamma} = 0.0930$. The character of Q is considerably different from the short wavelength case (Fig. 9a). The position of the minimum of the potential well is shifted to $x/L = 0.0$. Moreover, a "potential anti-well" exists for $-5.0 < x/L < 0.0$ which tends to inhibit mode penetration in this region. The corresponding eigenfunction $\tilde{\phi}$ (Fig. 12b) is also substantially different from the short wavelength case (Fig. 9b). First, the wave function has a surface wave character in that $\tilde{\phi} = \tilde{\phi}_0 \exp(-\kappa x)$. Second, the wavefunction is asymmetrical about the position of minimum Q_x , $x/L = 0.0$. The wavefunction falls off very rapidly in the region $-4.0 < x/L < 0.0$ which is due to the "potential anti-well" of Q in this region. For $x/L < -4.0$, $\tilde{\phi}$ falls off more gradually, similar to its behavior for $x/L > 10.0$. And finally, the wave function is very broad, extending out to $x/L = 50.0$.

Figure 13 is a plot of Q (Fig. 13a) and $\tilde{\phi}$ (Fig. 13b) versus x/L for the same parameters as Fig. 10, but now we take $\theta = 70^\circ$ so that the electric field is inhomogeneous (see Fig. 11). The eigenfrequency is $\tilde{\omega}_x = 0.0057$ and $\tilde{\gamma} = 0.0314$. Although both the wave potential Q and the wave eigenfunction $\tilde{\phi}$ now have imaginary components, Q and $\tilde{\phi}$ are quite similar to the no shear case. The wave function is centered about $x/L = 0.0$, has an asymmetrical nature, and extends up to $x/L = 50.0$. Thus, the

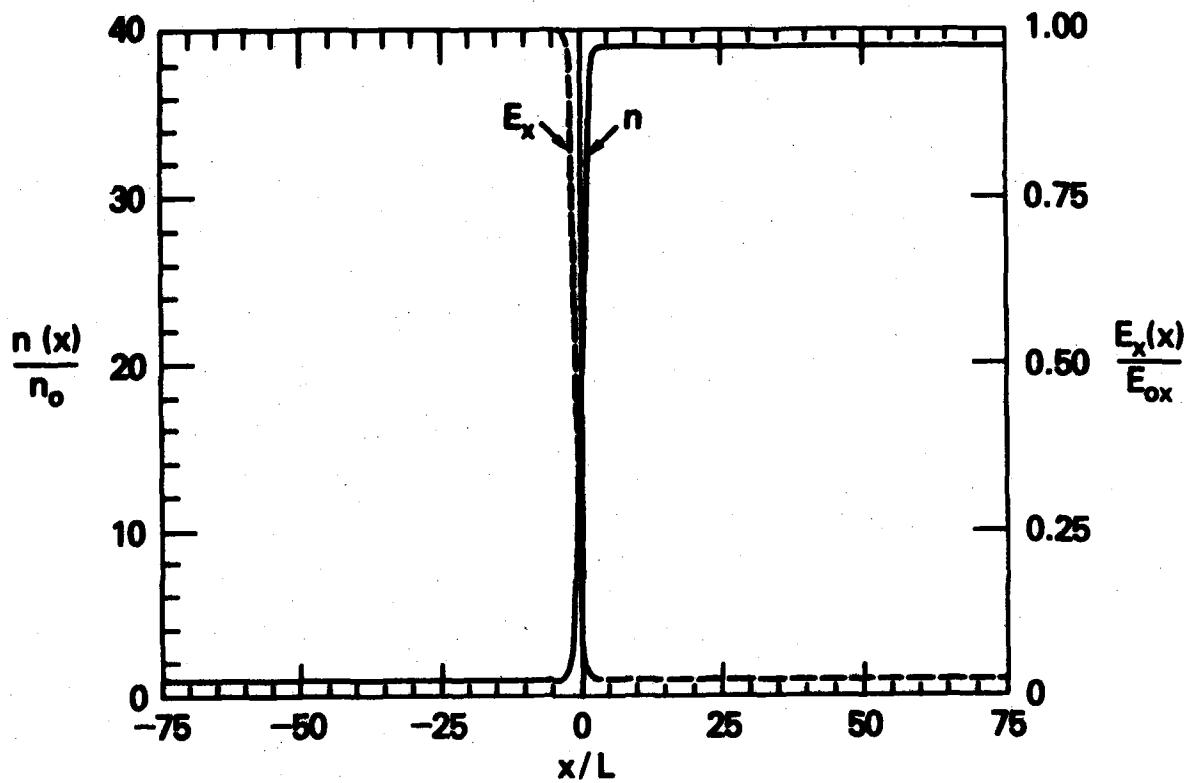


Fig. 11 Equilibrium density (Eq. (32) and electric field (Eq. (38)) profiles for $\varepsilon = 0.95$.

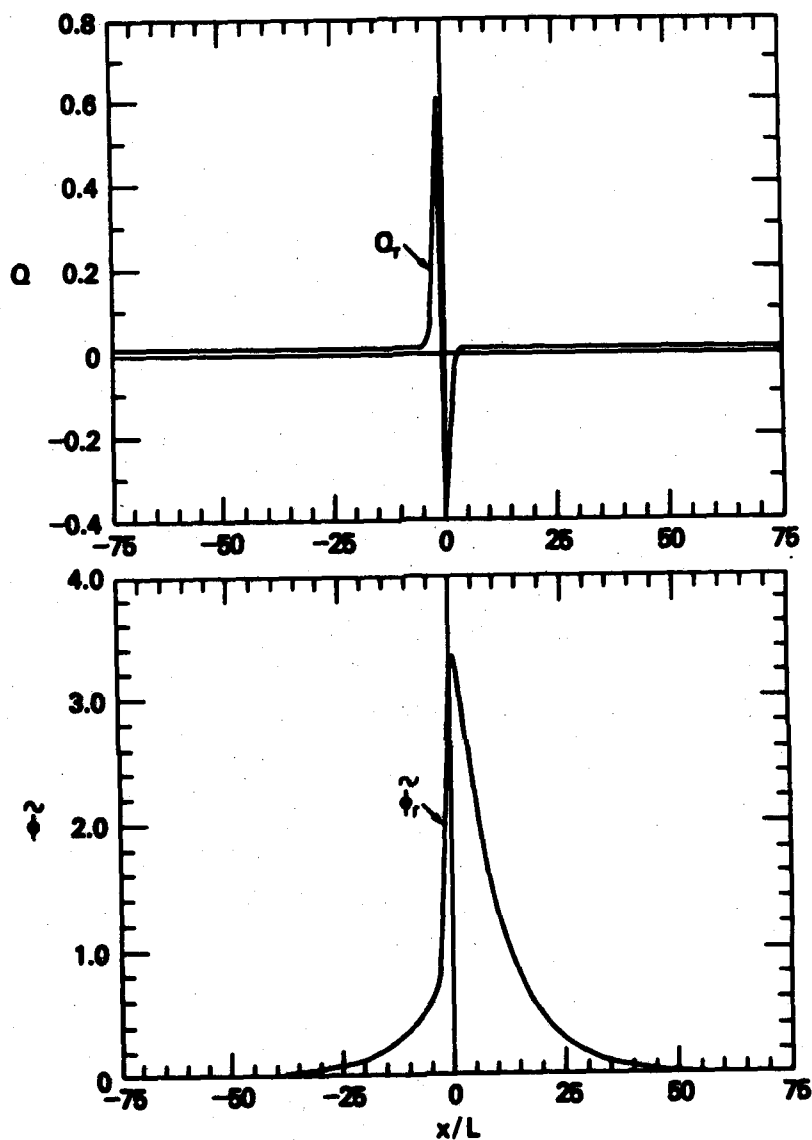


Fig. 12 Wave potential Q and wave eigenfunction $\tilde{\phi}$ as a function of x/L . The subscripts r and i denote real and imaginary, respectively. The parameters considered are $k_y L = 0.1$, $\tilde{\nu} = v_{in}/(v_o/L) = 100.0$, and $\theta = 0^\circ$ (i.e., $E_x = 0$). The eigenfrequency is $\tilde{\omega}_T = 0.0$ and $\tilde{\gamma} = 0.0930$. (a) Q vs. x/L . (b) $\tilde{\phi}$ vs. x/L .

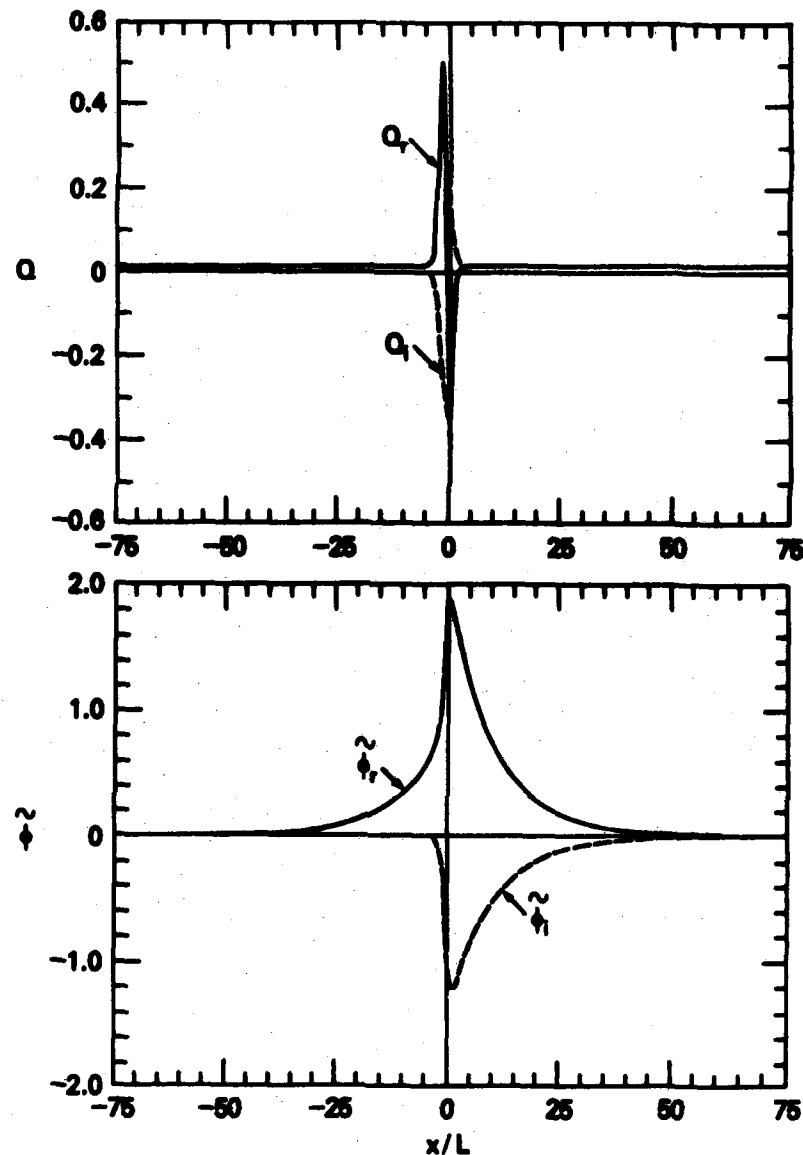


Fig. 13 Wave potential Q and wave eigenfunction $\tilde{\phi}$ as a function of x/L . The subscripts r and i denote real and imaginary, respectively. The parameters considered are $k_y L = 0.1$, $\tilde{\nu} = v_{in}/(V_0/L) = 100.0$, and $\theta = 70^\circ$ where E_x is given by Eq. (38). The eigenfrequency is $\tilde{\omega}_x = 0.0057$ and $\tilde{\gamma} = 0.0314$. (a) Q vs. x/L . (b) $\tilde{\phi}$ vs. x/L .

influence of the electric field inhomogeneity on the wave structure in the long wavelength regime ($k_y L \ll 1$) is much less pronounced than that in the short wavelength regime ($k_y L \gg 1$). However, the electric field inhomogeneity does reduce the growth rate of the mode significantly.

Finally we present Fig. 14 which is a marginal stability curve (i.e., $\gamma = 0$) of θ vs. $k_y L$ where we have taken $\tilde{v} = 1.0$ (dashed curve) and 100.0 (solid curve). Modes are stable ($\gamma < 0$) and unstable ($\gamma > 0$) above and below each of the curves, respectively. The ratio $E_x(x_0)/E_y$ is for the case $\tilde{v} = 100.0$ and has the following meaning. It is the ratio of E_x to E_y evaluated at $x = x_0$, where x_0 is the position of mode localization. The position of mode localization is defined as the position of the minimum value of Q_x , which corresponds to the maximum value of ϕ . For the parameters chosen, it is found that $x_0 = 0$. The marginal stability criterion is then given by

$$\frac{E_x(x_0)}{E_y} > 0.05 \tan \theta_{ms} \quad (40)$$

where θ_{ms} is the value of θ at marginal stability and we have used Eqs. (32) and (38) with $\epsilon = 0.95$. From Fig. 14 we find that

$$\theta_{ms} = 88 - 1.4 k_y L \quad (41)$$

where θ_{ms} is measured in degrees. Substituting Eq. (41) into Eq. (40), we obtain

$$\frac{E_x(x_0)}{E_y} > \frac{0.05}{\tan(1.4 k_y L)} \quad (42)$$

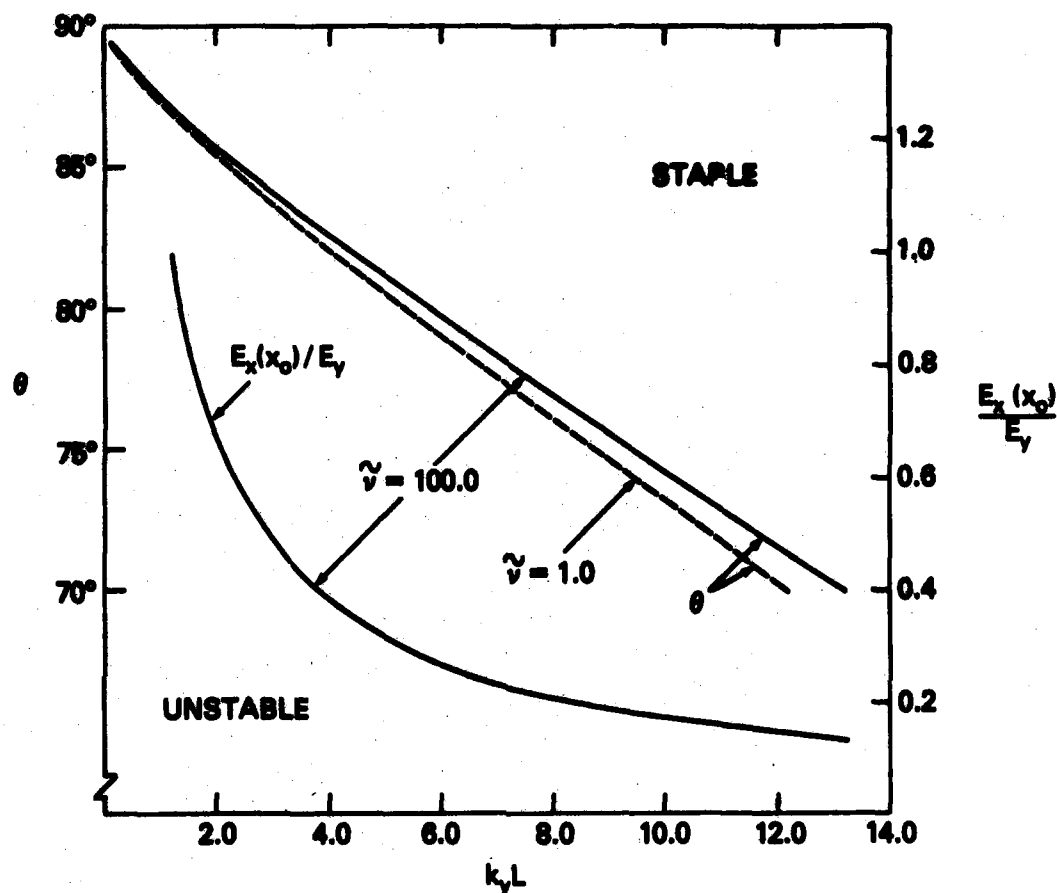


Fig. 14 Marginal stability curve of θ vs. $k_y L$ for $\tilde{\nu} = 1.0$ (dashed curve) and $\tilde{\nu} = 100.0$ (solid curve). The mode is stable ($\gamma < 0$) and unstable ($\gamma > 0$) above and below each of these curves, respectively. The ratio $E_x(x_0)/E_y$ vs. $k_y L$ is for the case $\tilde{\nu} = 100.0$ where $x_0/L = 0.0$ is the position of mode localization. In all of these curves, Eq. (38) has been used for $E_x(x)$.

or

$$\frac{E_x(x_0)}{E_y} > \frac{2.05}{k_y L} \quad (43)$$

for $k_y L \ll 36.0$. Note that Eq. (43) is qualitatively consistent with the result of Perkins and Doles (1975) in that there is an inverse relationship between $E_x(x_0)/E_y$ and k_y . Also, Eq. (43) is also quantitatively consistent (see Eq. (24)) since $D > L$ for the profiles used. Finally, as θ approaches 90° , i.e., $E_y \rightarrow 0$, the wavenumber of the last unstable mode approaches 0. There is no instability at $\theta = 90^\circ$; this has been demonstrated analytically by Perkins et al. (1973).

IV. DISCUSSION

We have presented a general theory of the $\underline{E} \times \underline{B}$ instability allowing for an arbitrary (1) density profile, (2) inhomogeneous electric field parallel to the density gradient, and (3) ratio of the collision frequency to the eigenfrequency (i.e., ν_{in}/ω). A differential equation is derived which describes the structure of the mode in the direction of the inhomogeneity, which we have considered to be the x direction. The theory is restricted to wave numbers such that $k_y L \ll \Omega_1/\nu_{in}$ and $k_y L \ll \Omega_1/\omega$; since it has also been assumed that $\nu_{in}/\Omega_1 \ll 1$ and $\omega/\Omega_1 \ll 1$ this restriction is not important. This work is basically an extension of the analysis of Perkins and Doles (1975), whose theory is restricted to the regime $\nu_{in}/\omega \gg 1$ and $k_y L \gg 1$, and considers a specific density and electric field profile. The principal results of this study are as follows.

1. For a constant electric field profile, instability persists even when $E_y = 0$ ($\theta = 90^\circ$). In fact, instability also occurs for $E_y < 0$ ($\theta > 90^\circ$) when $\partial n/\partial x > 0$; this is contrary to the simple one dimensional result (i.e., $\underline{k} = k_y \hat{e}_y$) which requires $E_y \partial n/\partial x > 0$ for instability. Thus, two-dimensional mode structure (i.e., $\underline{k} = k_x \hat{e}_x + k_y \hat{e}_y$) is crucial to the instability (Eq. (18)) (Linson and Workman, 1971).

2. For an inhomogeneous electric field, an inhomogeneous $\underline{E} \times \underline{B}$ velocity occurs ($V_y(x) = -cE_x(x)/B$) which has a stabilizing influence on the mode. Moreover, the short wavelength modes ($k_y L \gg 1$) are preferentially stabilized over long wavelength modes ($k_y L \lesssim 1$). This result is consistent with the work of Perkins and Doles (1975).

a. The functional form of $E_x(x)$ is not critical to stabilization of the mode. In the absence of any plasma sources or sinks, the ion continuity equation gives the equilibrium relationship between the density ($n(x)$) and the electric field $E_x(x)$, as given by Eq. (7) (also, see Fig. 8). Perkins and Doles (1975) use this relationship in their analysis. However, we have considered other electric field profiles (e.g., $E_x(x) = n(x)$ and $E_x(x) = \tanh(x)/n(x)$). We have found that the instability is still stabilized by the velocity inhomogeneity, again preferentially stabilizing the shorter wavelength modes, but that the marginal stability curves are different from Fig. (13).

b. The mode is stabilized because of the x-dependent resonance $\omega - k_y V_{ey}(x)$ in Eq. (15). Terms proportional to $\partial V_{ey}/\partial x$ and $\partial^2 V_{ey}/\partial x^2$ are not important for stabilization.

c. Perkins et al. (1973) have shown analytically that the mode is stable for $E_y = 0$ and E_x given by Eq. (21). The numerical results presented here are consistent with this conclusion. However, we add that as $E_y \rightarrow 0$ then $k_y L \rightarrow 0$. This is clear from Fig. (14) by noting that $k_y L \rightarrow 0$ as $\theta \rightarrow 90^\circ$.

d. In general, it is found that as v_{in} decreases the growth rate of the mode decreases; this is expected from linear theory (Eqs. (19) and (20)). However, in the case of an inhomogeneous electric field, the difference in growth rates between the strong and weak collisional limits considered is not significant (see Fig. (4)). Furthermore, the stabilization criterion is not sensitive to v_{in} (see Fig. (14)).

These results are applicable to the development of the $\underline{E} \times \underline{B}$ instability in both barium releases and the high latitude F region ionosphere. First, the important aspects of an inhomogeneous electric

field on barium cloud striations has been adequately addressed by Perkins and Doles (1975). In particular, they note that (1) the back side of a plasma cloud must steepen sufficiently so that it is almost one-dimensional to allow the mode to grow (i.e., $\underline{E} = E_y \hat{e}_y$) and (2) the stabilization of the mode due to $E_x(x)$ may explain why the sides of a plasma cloud do not become unstable. Furthermore, from our studies, we might hypothesize that the "freezing" phenomenon in plasma cloud striations (see McDonald et al., 1981) could be due to shear stabilization effects, since shear stabilization acts preferentially on short wavelength modes, i.e., $k_y L \gg 1$, but not on long wavelength modes, i.e., $k_y L < 1$. Second, the role of an inhomogeneous electric field in the $\underline{E} \times \underline{B}$ instability can be very important in the structuring of plasma "blobs" observed in the high latitude F region. Experimental observations (Vickrey et al., 1980; Tsunoda and Vickrey, 1982) indicate structuring in both the east-west and north-south directions. Moreover, small-scale structuring of the walls of the "blobs" have also been observed and is attributed to the $\underline{E} \times \underline{B}$ instability and/or the current convective instability. The plasma configuration is not well-known but the morphology of the "blobs" appears to be very complex. Not only are there inhomogeneities anticipated in the electric field, but there are also neutral wind effects, field-aligned plasma currents, and possible coupling effects between the E and F regions. A complete theoretical treatment incorporating these effects is beyond the scope of this paper. However, the results of this analysis strongly suggest that in order for the $\underline{E} \times \underline{B}$ drift instability to be a viable candidate for structuring in the high latitude F region, then the ambient electric field must be orthogonal or nearly orthogonal to the density gradient. A more complete

discussion of this problem will be deferred to a later report in which the influences of a field-aligned current and neutral wind are incorporated into this analysis.

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