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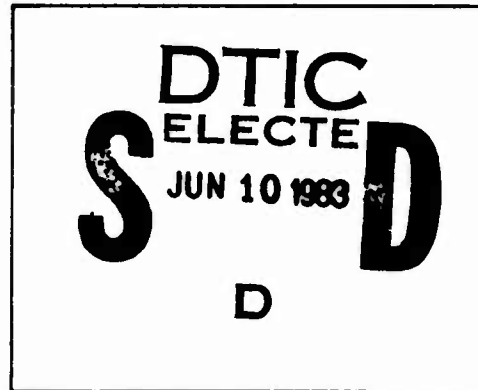
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**THERMOPHYSICAL PROPERTIES OF
SELECTED AEROSPACE MATERIALS
PART I: THERMAL RADIATIVE PROPERTIES**

T. S. FOULKEKIAN and G. T. HO, Editors

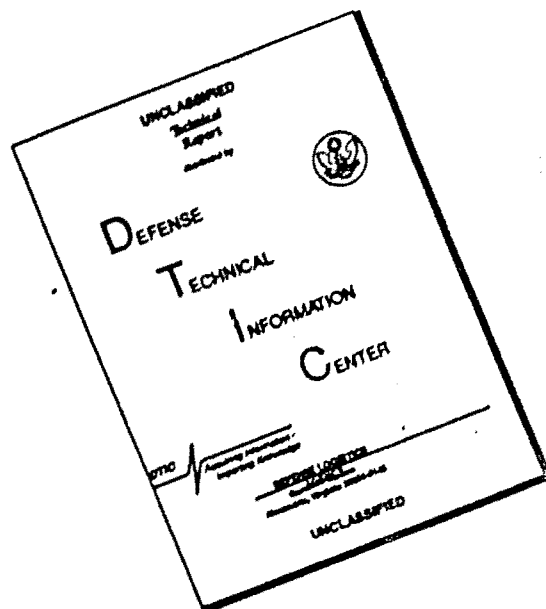
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| 20. ABSTRACT (Continue on reverse side if necessary and identify by block number) This volume presents the most comprehensively compiled experimental data and the critically evaluated and recommended values for the thermal radiative properties (hemispherical, normal, angular) spectral emittance, reflectance, absorptance, and transmittance of twenty-seven selected aircraft/spacecraft structural materials of technological interest. (continued on reverse side) | | |

magnesium fluoride--pyroceram--silica--silicon--silicon carbide--silicon nitride--acrylic resins--lucite--silicone resins--plastics--boron composites--graphite composites--glass composites--epoxy composites--aluminized grafoil

20. ABSTRACT (Cont)

Each subproperty is treated with respect to both wavelength and temperature dependences whenever possible. In the compilation of experimental data, all available data covering from the photographic region of the spectrum up to 100 microns are included. The recommended values resulting from critical evaluation, analysis, and synthesis of the available data and information cover the wavelength range of present interest from visible region to the infrared, if possible. Furthermore, the recommended values as a function of temperature are given for four particularly useful wavelengths.

The experimental data and the recommended values for each dependence of each subproperty of each material are presented in both tabular and graphical forms, together with a discussion text and a specification table. The former reviews and discusses the available data and information, the theoretical guidelines and other factors on which the critical evaluation, analysis, and synthesis of data are based, and the considerations involved in arriving at the final assessment and recommendations, and the latter gives the information on the specimen characterization and measurement method and condition for each set of experimental data.

In order to enable the user to fully utilize and property interpret the data and information presented in this reference work and also to enhance the usefulness of the data themselves, the theoretical background of thermal radiative properties is given at the beginning of the volume. Since most of the selected materials are not well known, a concise description of each of the materials is given at the beginning of each of the subsections.

PREFACE

This volume was prepared by the Thermophysical and Electronic Properties Information Analysis Center (TEPIAC), a DOD Information Analysis Center operated by the Center for Information and Numerical Data Analysis and Synthesis (CINDAS), Purdue University, West Lafayette, Indiana.

The overall program is aimed at providing data and information on all the important thermophysical properties of twenty-seven selected aerospace materials. This Part I contains data and information on thermal radiative properties only. Other parts are in preparation to cover other thermophysical properties.

Because of the extensive scope and highly specialized nature of the work, the staff who contributed to this volume were drawn not only from TEPIAC but also from other CINDAS programs. The following key personnel comprised the team responsible for the authorship (including data compilation, evaluation, and generation of recommended values) of the sections on the various selected materials: Mr. M. W. Johnson (Aluminum Alloy 2024), Dr. P. D. Desai (Aluminum Alloy 7075 and Titanium Alloy Ti-6Al-4V), Mr. T. Y. R. Lee (AISI 304 Stainless Steel), Dr. R. A. Matula (Aluminum oxide, boron nitride, calcium aluminum silicate, magnesium fluoride, Pyroceram, and vitreous silica), Mr. T. N. Havill (silicon), Dr. K. Y. Wu (silicon carbide), Dr. T. C. Chi (silicon nitride, acrylic resins, Lucite, polycarbonate plastics, and silicone resins), and Dr. H. H. Li (aluminized grafoil, boron fiber aluminum matrix composite, graphite fiber aluminum matrix composite, boron fiber epoxy composite, glass fiber epoxy composite, and graphite fiber epoxy composite). The Scientific Documentation Division of TEPIAC provided the in-depth search of the literature supplemental to its basic coverage.

We wish to take this opportunity to acknowledge the assistance provided by many of our friends both in governmental laboratories and in industry. In most cases this assistance has taken the form of providing reports or papers not readily available.

It is hoped that the present volume will prove useful to a large technical community as it provides a wealth of knowledge heretofore unknown or inaccessible to many. In particular, it is felt that the critical evaluation, analysis and reference data recommendation, whenever possible, constitute perhaps the most unique aspect of this work.

In putting a volume of this magnitude together it is nearly impossible to avoid some errors and omissions. It is hoped that we were able to keep these to a minimum. The editors and contributors would be most grateful if those who use this volume bring to their attention any additional known data or any possible errors that might have been inadvertently committed.

May 1976
West Lafayette, IN 47906

Y. S. TOULOUKIAN
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Distinguished Atkins Professor of
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SUMMARY

This volume presents the most comprehensively compiled experimental data and the critically evaluated and recommended values for the thermal radiative properties (hemispherical, normal, angular) spectral emittance, reflectance, absorptance, and transmittance of twenty-seven selected aircraft/spacecraft structural materials of technological interest.

Each subproperty is treated with respect to both wavelength and temperature dependences whenever possible. In the compilation of experimental data, all available data covering from the photographic region of the spectrum up to 100 μm are included. The recommended values resulting from critical evaluation, analysis, and synthesis of the available data and information cover the wavelength range of present interest from visible region (below 1 μm) to the infrared of 15 μm , if possible. Furthermore, the recommended values as a function of temperature are given for four particularly useful wavelengths (whenever possible): 2.8 μm , 3.8 μm , 5.0 μm , and 10.6 μm .

The experimental data and the recommended values for each dependence of each subproperty of each material are presented in both tabular and graphical forms, together with a discussion text and a specification table. The former reviews and discusses the available data and information, the theoretical guidelines and other factors on which the critical evaluation, analysis, and synthesis of data are based, and the considerations involved in arriving at the final assessment and recommendations, and the latter gives the information on the specimen characterization and measurement method and condition for each set of experimental data.

In order to enable the user to fully utilize and properly interpret the data and information presented in this reference work and also to enhance the usefulness of the data themselves, the theoretical background of thermal radiative properties is given at the beginning of the volume. Since most of the selected materials are not well known, a concise description of each of the materials is given at the beginning of each of the subsections.

The material and property coverage of this volume is summarized in the table entitled "Page Index to Materials and Properties" which appears on the next page.

| Page No. | Property | Emittance | | | | Reflectance | | | | Absorbance | | | | Transmittance | | | | | | | | | | | | |
|----------|---------------------------------|-----------|---------|---------|---------|-------------|---------|---------|---------|------------|---------|---------|---------|---------------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|---------|-----|
| | | HSE (λ) | HSE (T) | NSE (λ) | NSE (T) | ASE (λ) | ASE (T) | HSR (λ) | HSR (T) | NSR (λ) | NSR (T) | ASR (λ) | ASR (T) | HSA (λ) | HSA (T) | NSA (λ) | NSA (T) | ASA (λ) | ASA (T) | HST (λ) | HST (T) | NST (λ) | NST (T) | AST (λ) | AST (T) | |
| | Aluminum Alloy 2024 | | 28 | 38 | 41 | | | | | 46 | 61 | 64 | | | | 94 | 102 | 108 | | | 113 | 113 | 113 | 113 | 113 | 113 |
| | Aluminum Alloy 7075 | | 114 | | 120 | | | | | 126 | | 132 | | | | 135 | | 138 | | | 141 | 141 | 141 | 141 | 141 | 141 |
| | AISI 304 Stainless Steel | | 142 | 152 | | | | | | 155 | 161 | 164 | | | | 168 | 174 | | | | 180 | 180 | 180 | 180 | 180 | 180 |
| | Titanium Alloy Ti-6Al-4V | | 181 | 188 | 192 | | | | | 195 | 201 | 205 | | | | 211 | 217 | 221 | | | 224 | 224 | 224 | 224 | 224 | 224 |
| | Hadfield Manganese Steel | | | | | | | | | | | | | | | | | | | | 225 | 225 | 225 | 225 | 225 | 225 |
| | Aluminum Oxide | | 226 | 247 | | | | | | 253 | | 260 | | | | 265 | 269 | | | | 270 | | 274 | | | |
| | Boron Nitride | | 279 | 289 | | | | | | 295 | | 307 | | | | | | | | | | | | | | |
| | Calcium Aluminum Silicate | | 320 | 329 | | | | | | 332 | 342 | | | | | 345 | | | | | | | | | | |
| | Magnesium Fluoride | | 363 | 376 | | | | | | 379 | | 387 | | | | 391 | 399 | | | | | | | 402 | 415 | |
| | Pyroceram (Corning 9606) | | 419 | 423 | | | | | | 427 | | | | | | | | | | | 433 | | | | | |
| | Silica (Vitroous) | | 447 | | 468 | | | | | 477 | 488 | 491 | | | | 500 | | 509 | | | | | | 512 | 527 | |
| | Silicon | | 532 | 551 | | | | | | 558 | | | | | | 567 | 570 | | | | | | | 573 | 587 | |
| | Silicon Carbide | | 583 | 606 | | | | | | 613 | | | | | | 626 | | | | | | | | | | |
| | Silicon Nitride | | 647 | | | | | | | 654 | | | | | | 661 | | | | | | | | 667 | | |
| | Acrylic Resins | | 684 | | | | | | | 690 | | | | | | 699 | 705 | | | | | | | | | |
| | Lucite | | 728 | | | | | | | 731 | | 737 | | | | 743 | | | | | | | | 749 | | |
| | Polycarbonate Plastics | | 766 | | | | | | | 770 | | 776 | | | | 782 | | | | | | | | | | |
| | Polyphenylquinoxaline | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Silicone Resins | | 805 | | | | | | | 813 | | 822 | | | | | | | | | | | | | | |
| | Aluminized Grafoil | | 879 | 882 | | | | | | 885 | 888 | | | | | 891 | 894 | | | | | | | 897 | 897 | 897 |
| | Boron Fiber/Aluminum | | 900 | 903 | | | | | | 906 | 909 | | | | | 912 | 915 | | | | | | | 918 | 918 | 918 |
| | Graphite Fiber/Aluminum | | 921 | 924 | | | | | | 927 | 930 | | | | | 933 | 936 | | | | | | | 939 | 939 | 939 |
| | Boron Fiber/Epoxy | | 941 | 944 | | | | | | 947 | 953 | | | | | 956 | 959 | | | | | | | | | |
| | Glass Fiber/Epoxy | | 963 | 966 | | | | | | 969 | 975 | | | | | 978 | 981 | | | | | | | | | |
| | Graphite Fiber/Epoxy | | 985 | 989 | | | | | | 992 | 998 | | | | | 1001 | 1004 | | | | | | | | | |
| | Silicon Nitride/Graphite Fiber | | | | | | | | | | | | | | | | | | | | | | | | | |
| | Silicon Nitride/Vitreous Silica | | | | | | | | | | | | | | | | | | | | | | | | | |

* In the column headings, H = Hemispherical, N = Normal, A (in the first position) = Angular, S = Spectral, E = Emittance, R = Reflectance, A (in the third position) = Absorbance, T = Transmittance, (λ) = Wavelength dependence, and (T) = Temperature dependence. Blank space indicates that no information is available.

CONTENTS

| | Page |
|--|-------|
| PREFACE | iii |
| SUMMARY | iv |
| LIST OF TABLES | viii |
| LIST OF FIGURES | xxiii |
| LIST OF SYMBOLS | xxxv |
| 1. INTRODUCTION | 1 |
| 2. THEORETICAL BACKGROUND | 3 |
| 2.1. General Remarks | 3 |
| 2.2. Terminology | 5 |
| 2.3. Interrelationships between Thermal Radiative Properties | 9 |
| 2.4. Fresnel Equations for Specular Reflection | 11 |
| 2.5. Thermal Radiative Properties of Metals | 13 |
| 2.6. Thermal Radiative Properties of Nonmetallic Solids | 18 |
| 3. DATA EVALUATION AND GENERATION OF RECOMMENDED VALUES | 24 |
| 4. THERMAL RADIATIVE PROPERTIES OF SELECTED MATERIALS | 26 |
| 4.1. Aluminum Alloy 2024 M. W. Johnson | 27 |
| 4.2. Aluminum Alloy 7075 P. D. Desai | 114 |
| 4.3. AISI 304 Stainless Steel T. Y. R. Lee | 142 |
| 4.4. Titanium Alloy Ti-6Al-4V P. D. Desai | 181 |
| 4.5. Hadfield Manganese Steel | 225 |
| 4.6. Aluminum Oxide R. A. Matula | 226 |
| 4.7. Boron Nitride R. A. Matula | 279 |
| 4.8. Calcium Aluminum Silicate R. A. Matula | 320 |
| 4.9. Magnesium Fluoride R. A. Matula | 363 |
| 4.10. Pyroceram R. A. Matula | 418 |

| | | |
|-------|---|------|
| 4.11. | Silica (Vitreous) | 447 |
| | R. A. Matula | |
| 4.12. | Silicon | 530 |
| | T. N. Havill | |
| 4.13. | Silicon Carbide | 593 |
| | K. Y. Wu | |
| 4.14. | Silicon Nitride | 647 |
| | T. C. Chi | |
| 4.15. | Acrylic Resins | 683 |
| | T. C. Chi | |
| 4.16. | Lucite | 727 |
| | T. C. Chi | |
| 4.17. | Polycarbonate Plastics | 765 |
| | T. C. Chi | |
| 4.18. | Polyphenylquinoxaline | 802 |
| 4.19. | Silicone Resins | 804 |
| | T. C. Chi | |
| 4.20. | Aluminized Grafoil | 847 |
| | H. H. Li | |
| 4.21. | Boron Fiber Aluminum Matrix Composite | 898 |
| | H. H. Li | |
| 4.22. | Graphite Fiber Aluminum Matrix Composite | 919 |
| | H. H. Li | |
| 4.23. | Boron Fiber Epoxy Composite | 940 |
| | H. H. Li | |
| 4.24. | Glass Fiber Epoxy Composite | 962 |
| | H. H. Li | |
| 4.25. | Graphite Fiber Epoxy Composite | 984 |
| | H. H. Li | |
| 4.26. | Silicon Nitride with Chopped Graphite Fiber | 1007 |
| 4.27. | Silicon Nitride with Vitreous Silica | 1008 |
| 5. | REFERENCES | 1009 |

LIST OF TABLES

| | PAGE |
|---|------|
| 1. CLASSICAL MODELS FOR THE OPTICAL PROPERTIES OF METALS | 15 |
| 1- 1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 30 |
| 1- 2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 36 |
| 1- 3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 37 |
| 1- 4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE) | 39 |
| 1- 5. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 42 |
| 1- 6. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 47 |
| 1- 7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 53 |
| 1- 8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 57 |
| 1- 9. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE) | 62 |
| 1-10. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 65 |
| 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 72 |
| 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 83 |
| 1-13. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (INCIDENT ANGLE DEPENDENCE) | 92 |
| 1-14. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (INCIDENT ANGLE DEPENDENCE) | 93 |
| 1-15. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 95 |
| 1-16. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 100 |
| 1-17. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 101 |
| 1-18. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE) | 103 |
| 1-19. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE) | 106 |
| 1-20. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE) | 107 |

| | | |
|-------|---|-----|
| 1-21. | PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 109 |
| 2- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 115 |
| 2- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 118 |
| 2- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 119 |
| 2- 4. | RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 121 |
| 2- 5. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 124 |
| 2- 6. | EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 125 |
| 2- 7. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 127 |
| 2- 8. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 130 |
| 2- 9. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 131 |
| 2-10. | RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 133 |
| 2-11. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 136 |
| 2-12. | RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE) | 139 |
| 3- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 144 |
| 3- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 147 |
| 3- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 149 |
| 3- 4. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE) | 153 |
| 3- 5. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 156 |
| 3- 6. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF AISII 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 159 |
| 3- 7. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 160 |
| 3- 8. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE) | 162 |
| 3- 9. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF AISII 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 166 |

| | | |
|-------|---|-----|
| 3-10. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 167 |
| 3-11. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 169 |
| 3-12. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 172 |
| 3-13. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) | 173 |
| 3-14. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE) | 175 |
| 3-15. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE) | 178 |
| 3-16. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE) | 179 |
| 4- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 183 |
| 4- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 186 |
| 4- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 187 |
| 4- 4. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE) | 190 |
| 4- 5. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE) | 191 |
| 4- 6. | RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 193 |
| 4- 7. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 196 |
| 4- 8. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 199 |
| 4- 9. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 200 |
| 4-10. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE) | 203 |
| 4-11. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE) | 204 |
| 4-12. | RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 206 |
| 4-13. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 209 |
| 4-14. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 210 |
| 4-15. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 212 |

| | | |
|-------|---|-----|
| 4-16. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 215 |
| 4-17. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 216 |
| 4-18. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE) | 219 |
| 4-19. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE) | 220 |
| 4-20. | RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE) | 222 |
| 6- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE(COORS AD 99) (WAVELENGTH DEPENDENCE) | 228 |
| 6- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 235 |
| 6- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 240 |
| 6- 4. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE(COORS AD 99) (TEMPERATURE DEPENDENCE) | 248 |
| 6- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE) | 251 |
| 6- 6. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE) | 252 |
| 6- 7. | MEASUREMENT INFORMATION ON THE NCRMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 255 |
| 6- 8. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 257 |
| 6- 9. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 262 |
| 6-10. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 263 |
| 6-11. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 267 |
| 6-12. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 268 |
| 6-13. | MEASUREMENT INFORMATION ON THE HEMISPHERICAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 272 |
| 6-14. | EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPFNDENCE) | 273 |
| 6-15. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 276 |
| 6-16. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) | 277 |
| 7- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 281 |

| | | |
|-------|---|-----|
| 7- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 284 |
| 7- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 286 |
| 7- 4. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE) | 290 |
| 7- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE) | 293 |
| 7- 6. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE) | 294 |
| 7- 7. | TYPICAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 296 |
| 7- 8. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 299 |
| 7- 9. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 301 |
| 7-10. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 308 |
| 7-11. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 311 |
| 7-12. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 312 |
| 7-13. | TYPICAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 314 |
| 7-14. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 317 |
| 7-15. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) | 318 |
| 8- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (WAVELENGTH DEPENDENCE) | 322 |
| 8- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 326 |
| 8- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 327 |
| 8- 4. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (TEMPERATURE DEPENDENCE) | 330 |
| 8- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (WAVELENGTH DEPENDENCE) | 333 |
| 8- 6. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 336 |
| 8- 7. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 337 |
| 8- 8. | MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 340 |

| | | |
|-------|--|-----|
| 8- 9. | EXPERIMENTAL REFRACTIVE INDEX OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 341 |
| 8-10. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE(CORNING 9753) (TEMPERATURE DEPENDENCE) | 343 |
| 8-11. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF CALCIUM ALUMINUM SILICATE(CORNING 9753) (WAVELENGTH DEPENDENCE) | 346 |
| 8-12. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE(CORNING 9753) (WAVELENGTH DEPENDENCE) | 350 |
| 8-13. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 353 |
| 8-14. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) | 354 |
| 8-15. | PROVISIONAL NORMAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE(CORNING 9753) (TEMPERATURE DEPENDENCE) | 358 |
| 8-16. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE) | 361 |
| 8-17. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE) | 362 |
| 9- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (WAVELENGTH DEPENDENCE) | 365 |
| 9- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 368 |
| 9- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 369 |
| 9- 4. | MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 374 |
| 9- 5. | EXPERIMENTAL REFRACTIVE INDEX OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 375 |
| 9- 6. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (TEMPERATURE DEPENDENCE) | 377 |
| 9- 7. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (WAVELENGTH DEPENDENCE) | 380 |
| 9- 8. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 383 |
| 9- 9. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 384 |
| 9-10. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 389 |
| 9-11. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 390 |
| 9-12. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (WAVELENGTH DEPENDENCE) | 392 |
| 9-13. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 395 |

| | | |
|--------|--|-----|
| 9-14. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 396 |
| 9-15. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (TEMPERATURE DEPENDENCE) | 400 |
| 9-16. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (WAVELENGTH DEPENDENCE) | 404 |
| 9-17. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 407 |
| 9-18. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) | 409 |
| 9-19. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE(IRTRAN 1) (TEMPERATURE DEPENDENCE) | 416 |
| 10- 1. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 421 |
| 10- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 422 |
| 10- 3. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF PYROCERAM (TEMPERATURE DEPENDENCE) | 425 |
| 10- 4. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (TEMPERATURE DEPENDENCE) | 426 |
| 10- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM(CORNING 9606) (WAVELENGTH DEPENDENCE) | 428 |
| 10- 6. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 431 |
| 10- 7. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 432 |
| 10- 8. | MEASUREMENT INFORMATION ON THE HEMISPHERICAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 435 |
| 10- 9. | EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 436 |
| 10-10. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM(CORNING 9606) (WAVELENGTH DEPENDENCE) | 438 |
| 10-11. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 441 |
| 10-12. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) | 443 |
| 11- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 450 |
| 11- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 453 |
| 11- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 454 |
| 11- 4. | MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 460 |

| | | |
|--------|--|-----|
| 11- 5. | EXPERIMENTAL REFRACTIVE INDEX OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 462 |
| 11- 6. | MEASUREMENT INFORMATION ON THE ABSORPTION INDEX OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 466 |
| 11- 7. | EXPERIMENTAL ABSORPTION INDEX OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 467 |
| 11- 8. | PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 469 |
| 11- 9. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 472 |
| 11-10. | EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 473 |
| 11-11. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 478 |
| 11-12. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 481 |
| 11-13. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 483 |
| 11-14. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (TEMPERATURE DEPENDENCE) | 489 |
| 11-15. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 492 |
| 11-16. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 495 |
| 11-17. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 498 |
| 11-18. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 501 |
| 11-19. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 504 |
| 11-20. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 505 |
| 11-21. | PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 510 |
| 11-22. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 513 |
| 11-23. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 518 |
| 11-24. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) | 521 |
| 11-25. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (TEMPERATURE DEPENDENCE) | 528 |
| 12- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 535 |

| | | |
|--------|--|-----|
| 12- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) | 539 |
| 12- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) | 542 |
| 12- 4. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 553 |
| 12- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 556 |
| 12- 6. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 557 |
| 12- 7. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 560 |
| 12- 8. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) | 563 |
| 12- 9. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) | 565 |
| 12-10. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 568 |
| 12-11. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 571 |
| 12-12. | RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 575 |
| 12-13. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) | 578 |
| 12-14. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) | 580 |
| 12-15. | RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 588 |
| 12-16. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 591 |
| 12-17. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 592 |
| 13- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) | 595 |
| 13- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) | 599 |
| 13- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) | 601 |
| 13- 4. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE) | 607 |
| 13- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE) | 611 |
| 13- 6. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE) | 612 |

13- 7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 614

13- 8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 618

13- 9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 620

13-10. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 627

13-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 631

13-12. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 632

13-13. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 634

13-14. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 637

13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) 640

14- 1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 649

14- 2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 652

14- 3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 653

14- 4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 655

14- 5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 658

14- 6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 659

14- 7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 662

14- 8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 665

14- 9. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 666

14-10. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 668

14-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 672

14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) 674

15- 1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) 685

| | | |
|--------|---|-----|
| 15- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 688 |
| 15- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 689 |
| 15- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 691 |
| 15- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 694 |
| 15- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 695 |
| 15- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 700 |
| 15- 8. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 703 |
| 15- 9. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 704 |
| 15-10. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 708 |
| 15-11. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 712 |
| 15-12. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) | 714 |
| 16- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 729 |
| 16- 2. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 732 |
| 16- 3. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 735 |
| 16- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 736 |
| 16- 5. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 738 |
| 16- 6. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 741 |
| 16- 7. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 742 |
| 16- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 744 |
| 16- 9. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 747 |
| 16-10. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 748 |
| 16-11. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 750 |

| | | |
|--------|--|-----|
| 16-12. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 754 |
| 16-13. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) | 756 |
| 17- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 768 |
| 17- 2. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 771 |
| 17- 3. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 774 |
| 17- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 775 |
| 17- 5. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 777 |
| 17- 6. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 780 |
| 17- 7. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 781 |
| 17- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 783 |
| 17- 9. | MEASUREMENT INFORMATION ON THE SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 786 |
| 17-10. | EXPERIMENTAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 787 |
| 17-11. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 789 |
| 17-12. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 793 |
| 17-13. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) | 794 |
| 19- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE) | 807 |
| 19- 2. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 810 |
| 19- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 811 |
| 19- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 814 |
| 19- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 817 |
| 19- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 819 |
| 19- 7. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 823 |

| | | |
|--------|--|-----|
| 19- 8. | MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE) | 826 |
| 19- 9. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE) | 827 |
| 19-10. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 829 |
| 19-11. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 833 |
| 19-12. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) | 835 |
| 20- 1. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) | 849 |
| 20- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) | 850 |
| 20- 3. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) | 853 |
| 20- 4. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) | 859 |
| 20- 5. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) | 867 |
| 20- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) | 869 |
| 20- 7. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) | 873 |
| 20- 8. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) | 874 |
| 20- 9. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) | 876 |
| 20-10. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) | 877 |
| 20-11. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE) | 880 |
| 20-12. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE) | 883 |
| 20-13. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE) | 886 |
| 20-14. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE) | 889 |
| 20-15. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE) | 892 |
| 20-16. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE) | 895 |
| 21- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE) | 901 |

| | | | |
|--------|---|-----------|-----|
| 21- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE) | | 904 |
| 21- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE) | | 907 |
| 21- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE) | | 910 |
| 21- 5. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE) | | 913 |
| 21- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE) | | 916 |
| 22- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE) | | 922 |
| 22- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE) | | 925 |
| 22- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE) | | 928 |
| 22- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE) | | 931 |
| 22- 5. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE) | | 934 |
| 22- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE) | | 937 |
| 23- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 942 |
| 23- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | | 945 |
| 23- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 948 |
| 23- 4. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 951 |
| 23- 5. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 952 |
| 23- 6. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | | 954 |
| 23- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 957 |
| 23- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | | 960 |
| 24- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 964 |
| 24- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | | 967 |
| 24- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | | 970 |

| | | |
|--------|--|------|
| 24- 4. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 973 |
| 24- 5. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 974 |
| 24- 6. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | 976 |
| 24- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 979 |
| 24- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | 982 |
| 25- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 987 |
| 25- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | 990 |
| 25- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 993 |
| 25- 4. | MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 996 |
| 25- 5. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 997 |
| 25- 6. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | 999 |
| 25- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE) | 1002 |
| 25- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE) | 1005 |

LIST OF FIGURES

| | PAGE |
|---|------|
| 1. GEOMETRIC PARAMETERS DESCRIPTIVE OF REFLECTION FROM A SURFACE | 8 |
| 2. TYPICAL BEHAVIOR OF THERMAL RADIATIVE PROPERTIES OF METALS | 14 |
| 3. TYPICAL BEHAVIOR OF THERMAL RADIATIVE PROPERTIES OF A TRANSPARENT NON-SCATTERING NONMETALLIC SOLID. | 19 |
| 4. THE REFLECTIVITY AND TRANSMISSIVITY OF A SEMITRANSSPARENT SLAB | 22 |
| 1- 1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 31 |
| 1- 2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 32 |
| 1- 3. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 33 |
| 1- 4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF OXIDIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 34 |
| 1- 5. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 35 |
| 1- 6. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALCLAD ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE). | 40 |
| 1- 7. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 43 |
| 1- 8. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 44 |
| 1- 9. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 45 |
| 1-10. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 48 |
| 1-11. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 49 |
| 1-12. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 50 |
| 1-13. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 51 |
| 1-14. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF OXIDIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 52 |
| 1-15. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALCLAD ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE). | 63 |
| 1-16. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 66 |
| 1-17. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 67 |

| | | |
|-------|--|-----|
| 1-18. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 68 |
| 1-19. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 69 |
| 1-20. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 70 |
| 1-21. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 71 |
| 1-22. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (INCIDENT ANGLE DEPENDENCE). | 91 |
| 1-23. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 96 |
| 1-24. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 97 |
| 1-25. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE). | 98 |
| 1-26. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF OXIDIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 99 |
| 1-27. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALCLAD ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE). | 104 |
| 1-28. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE). | 105 |
| 1-29. | PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 110 |
| 1-30. | PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 111 |
| 1-31. | PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) | 112 |
| 2- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 116 |
| 2- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 117 |
| 2- 3. | RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 122 |
| 2- 4. | EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 123 |
| 2- 5. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 128 |
| 2- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 129 |
| 2- 7. | RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 134 |
| 2- 8. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 137 |

| | | |
|-------|--|-----|
| 2- 9. | RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE). | 140 |
| 3- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 145 |
| 3- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 146 |
| 3- 3. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE). | 154 |
| 3- 4. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 157 |
| 3- 5. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 158 |
| 3- 6. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE). | 163 |
| 3- 7. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 165 |
| 3- 8. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 170 |
| 3- 9. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE). | 171 |
| 3-10. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE). | 176 |
| 3-11. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE). | 177 |
| 4- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 184 |
| 4- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 185 |
| 4- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE). | 189 |
| 4- 4. | RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 194 |
| 4- 5. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 197 |
| 4- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 198 |
| 4- 7. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE). | 202 |
| 4- 8. | RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 207 |
| 4- 9. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 208 |
| 4-10. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 213 |

| | | |
|-------|---|-----|
| 4-11. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 214 |
| 4-12. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE). | 218 |
| 4-13. | RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE). | 223 |
| 6- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 229 |
| 6- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 230 |
| 6- 3. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 231 |
| 6- 4. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 232 |
| 6- 5. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 233 |
| 6- 6. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 234 |
| 6- 7. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE). | 249 |
| 6- 8. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE). | 250 |
| 6- 9. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 254 |
| 6-10. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 261 |
| 6-11. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 266 |
| 6-12. | EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 271 |
| 6-13. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE). | 275 |
| 7- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 282 |
| 7- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 283 |
| 7- 3. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE). | 291 |
| 7- 4. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE). | 292 |
| 7- 5. | TYPICAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 297 |
| 7- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 298 |

| | | |
|-------|--|-----|
| 7- 7. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 309 |
| 7- 8. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 310 |
| 7- 9. | TYPICAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 315 |
| 7-10. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE). | 316 |
| 8- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 324 |
| 8- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 325 |
| 8- 3. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE). | 331 |
| 8- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 334 |
| 8- 5. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM, SILICATE (WAVELENGTH DEPENDENCE). | 335 |
| 8- 6. | EXPERIMENTAL REFRACTIVE INDEX OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 339 |
| 8- 7. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE). | 344 |
| 8- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 348 |
| 8- 9. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 351 |
| 8-10. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE). | 352 |
| 8-11. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE). | 359 |
| 8-12. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE). | 360 |
| 9- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 366 |
| 9- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 367 |
| 9- 3. | EXPERIMENTAL REFRACTIVE INDEX OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 373 |
| 9- 4. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (TEMPERATURE DEPENDENCE). | 378 |
| 9- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 381 |
| 9- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 382 |

| | | |
|--------|---|-----|
| 9- 7. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 388 |
| 9- 8. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 393 |
| 9- 9. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 394 |
| 9-10. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (TEMPERATURE DEPENDENCE). | 401 |
| 9-11. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 405 |
| 9-12. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE). | 406 |
| 9-13. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (TEMPERATURE DEPENDENCE). | 417 |
| 10- 1. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE). | 420 |
| 10- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (TEMPERATURE DEPENDENCE). | 424 |
| 10- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE). | 429 |
| 10- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE). | 430 |
| 10- 5. | EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE). | 434 |
| 10- 6. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE). | 439 |
| 10- 7. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE). | 440 |
| 11- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 451 |
| 11- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 452 |
| 11- 3. | EXPERIMENTAL REFRACTIVE INDEX OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 459 |
| 11- 4. | EXPERIMENTAL ABSORPTION INDEX OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 465 |
| 11- 5. | PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 470 |
| 11- 6. | EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 471 |
| 11- 7. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 479 |
| 11- 8. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 480 |

| | | |
|--------|---|-----|
| 11- 9. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (TEMPERATURE DEPENDENCE). | 490 |
| 11-10. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 493 |
| 11-11. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 494 |
| 11-12. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 502 |
| 11-13. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 503 |
| 11-14. | PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 511 |
| 11-15. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 514 |
| 11-16. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 515 |
| 11-17. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 516 |
| 11-18. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE). | 517 |
| 11-19. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (TEMPERATURE DEPENDENCE). | 529 |
| 12- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 536 |
| 12- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE). | 537 |
| 12- 3. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF LOW-RESISTIVITY, DOPED SILICON (WAVELENGTH DEPENDENCE). | 538 |
| 12- 4. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH-RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 554 |
| 12- 5. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON (TEMPERATURE DEPENDENCE) | 555 |
| 12- 6. | RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 561 |
| 12- 7. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON OF VARIED PURITY (WAVELENGTH DEPENDENCE). | 562 |
| 12- 8. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 569 |
| 12- 9. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH-RESISTIVITY SILICON (TEMPERATURE DEPENDENCE) | 572 |
| 12-10. | RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE) | 576 |
| 12-11. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON OF VARIED SILICON (TEMPERATURE DEPENDENCE) | 577 |

| | | |
|--------|---|-----|
| 12-12. | RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH-RESISTIVITY PURITY (WAVELENGTH DEPENDENCE). | 589 |
| 12-13. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON (TEMPERATURE DEPENDENCE) | 590 |
| 13- 1. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 597 |
| 13- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 598 |
| 13- 3. | RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE). | 609 |
| 13- 4. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE). | 610 |
| 13- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 616 |
| 13- 6. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 617 |
| 13- 7. | RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 629 |
| 13- 8. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 630 |
| 13- 9. | RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 635 |
| 13-10. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE). | 636 |
| 14- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE). | 650 |
| 14- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE). | 651 |
| 14- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE). | 656 |
| 14- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE). | 657 |
| 14- 5. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE). | 663 |
| 14- 6. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE). | 664 |
| 14- 7. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE COATINGS (WAVELENGTH DEPENDENCE). | 669 |
| 14- 8. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE COATINGS (WAVELENGTH DEPENDENCE). | 670 |
| 14- 9. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE POWDERS (WAVELENGTH DEPENDENCE). | 671 |
| 15- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE). | 686 |

| | | |
|--------|---|-----|
| 15- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE). | 687 |
| 15- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE). | 692 |
| 15- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE). | 693 |
| 15- 5. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE). | 701 |
| 15- 6. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE). | 702 |
| 15- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATING (TEMPERATURE DEPENDENCE) | 706 |
| 15- 8. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE). | 709 |
| 15- 9. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE). | 710 |
| 15-10. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC THIN FILMS (WAVELENGTH DEPENDENCE). | 711 |
| 16- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 730 |
| 16- 2. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 733 |
| 16- 3. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 734 |
| 16- 4. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 739 |
| 16- 5. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 740 |
| 16- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 745 |
| 16- 7. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 746 |
| 16- 8. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 751 |
| 16- 9. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE). | 752 |
| 16-10. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE THIN FILMS (WAVELENGTH DEPENDENCE). | 753 |
| 17- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 769 |
| 17- 2. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 772 |
| 17- 3. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 773 |

| | | |
|--------|---|-----|
| 17- 4. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 778 |
| 17- 5. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 779 |
| 17- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 784 |
| 17- 7. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 785 |
| 17- 8. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 790 |
| 17- 9. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE). | 791 |
| 17-10. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS THIN FILMS (WAVELENGTH DEPENDENCE). | 792 |
| 19- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN COATING (WAVELENGTH DEPENDENCE). | 808 |
| 19- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE). | 809 |
| 19- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (WAVELENGTH DEPENDENCE). | 815 |
| 19- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE). | 816 |
| 19- 5. | PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (WAVELENGTH DEPENDENCE). | 824 |
| 19- 6. | EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE). | 825 |
| 19- 7. | PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE). | 830 |
| 19- 8. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE). | 831 |
| 19- 9. | EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESIN COATINGS (WAVELENGTH DEPENDENCE). | 832 |
| 20- 1. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE). | 848 |
| 20- 2. | EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE). | 852 |
| 20- 3. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE). | 866 |
| 20- 4. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE). | 872 |
| 20- 5. | EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE). | 875 |
| 20- 6. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE). | 881 |

| | | |
|--------|---|-----|
| 20- 7. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE). | 884 |
| 20- 8. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE). | 887 |
| 20- 9. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE). | 890 |
| 20-10. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE). | 893 |
| 20-11. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE). | 896 |
| 21- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE). | 902 |
| 21- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE). | 905 |
| 21- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE). | 908 |
| 21- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE). | 911 |
| 21- 5. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE). | 914 |
| 21- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE). | 917 |
| 22- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE). | 923 |
| 22- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE). | 926 |
| 22- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE). | 929 |
| 22- 4. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE). | 932 |
| 22- 5. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE). | 935 |
| 22- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE). | 938 |
| 23- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 943 |
| 23- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 946 |
| 23- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 949 |
| 23- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 950 |
| 23- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 955 |

| | | |
|--------|---|------|
| 23- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 958 |
| 23- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 961 |
| 24- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 965 |
| 24- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 968 |
| 24- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 971 |
| 24- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 972 |
| 24- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 977 |
| 24- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 980 |
| 24- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 983 |
| 25- 1. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 988 |
| 25- 2. | PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 991 |
| 25- 3. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 994 |
| 25- 4. | EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 995 |
| 25- 5. | PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 1000 |
| 25- 6. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE). | 1003 |
| 25- 7. | PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE). | 1006 |

LIST OF SYMBOLS

| | |
|-----|---|
| a | Absorption coefficient |
| c | Velocity of light in vacuum |
| CLA | Center line average |
| d | Specimen thickness |
| E | Irradiance |
| I | Radiant intensity |
| j | Unit imaginary number |
| k | Absorption index |
| K* | Complex dielectric constant |
| L | Radiance |
| m | Electron mass; RMS slope |
| M | Exitance |
| n | Refractive index |
| n* | Complex refractive index |
| N | Number density of free electrons |
| P | A quantity in Fresnel equations |
| q | Electron charge |
| Q | Radiant energy; A quantity in Fresnel equations |
| r | Electrical resistivity |
| R | Single surface reflectance |
| RMS | Root mean square |
| t | Time |
| T | Internal transmittance; Temperature |
| V | Volume |
| W | Radiant density |

| | |
|-------------------|--|
| α | Absorptance |
| α_p | Absorptance for incident radiation polarized parallel to plane of incidence |
| α_s | Absorptance for incident radiation polarized normal to plane of incidence |
| α_∞ | Absorptivity |
| β | Temperature coefficient of electrical resistivity |
| ϵ | Emittance |
| ϵ_0 | Permittivity of free space |
| ϵ_p | Emittance for radiation polarized parallel to plane of incidence |
| ϵ_s | Emittance for radiation polarized normal to plane of incidence |
| ϵ_∞ | Emissivity |
| θ | Zenith angle for incident conditions |
| θ' | Zenith angle for viewing conditions |
| $\Delta\theta$ | Half angle of acceptance of optical system |
| κ | Loss value factor |
| λ | Wavelength |
| ρ | Reflectance |
| ρ_p | Reflectance for incident radiant energy polarized parallel to plane of incidence |
| ρ_s | Reflectance for incident radiant energy polarized normal to plane of incidence |
| ρ_∞ | Reflectivity |
| σ | RMS roughness |
| τ | Transmittance; Relaxation time |
| φ | Azimuthal angle for incident conditions |
| φ' | Azimuthal angle for viewing conditions |
| Φ | Radiant flux |
| Φ_a | Absorbed flux |
| Φ_i | Incident flux |
| Φ_r | Reflected flux |

| | |
|-----------|-------------------------------------|
| Φ_t | Transmitted flux |
| ω | Solid angle for incident conditions |
| ω' | Solid angle for viewing conditions |

1. INTRODUCTION

This reference work presents the most comprehensively compiled experimental data and the critically evaluated and recommended values on the thermal radiative properties of twenty-seven selected aircraft/spacecraft structural materials.

The twenty-seven specific materials and generic groups of materials covered are the following:

| | <u>Melting Point (K)</u> |
|--|--------------------------------------|
| 1. Metals | |
| (1) Aluminum Alloy 2024 | 775-911 |
| (2) Aluminum Alloy 7075 | 750-911 |
| (3) AISI 304 Stainless Steel | 1670-1727 |
| (4) Titanium Alloy Ti-6Al-4V | 1803-1908 |
| (5) Hadfield Manganese Steel | 1470-1480 |
| 2. Dome Materials | |
| (6) Aluminum oxide (Wesgo Al-300) | 2315-2320 |
| (7) Boron nitride | 3273(sublimation) |
| (8) Calcium aluminum silicate (Corning 9753) | 1723-1773 |
| (9) Magnesium fluoride (Kodak IRTRAN 1) | 1528 |
| (10) Pyroceram (Corning 9606) | 1623(softening) |
| (11) Silica (vitreous) | 1950-2000 |
| (12) Silicon | 1687 |
| (13) Silicon carbide | >2400(sublimation) |
| (14) Silicon nitride | 2200(dissociation) |
| 3. Transparent Materials | |
| (15) Acrylic resins | 277-511(softening) |
| (16) Lucite | 397(softening) 520(decomposition) |
| (17) Polycarbonate plastics | 430(softening) 580(decomposition) |
| (18) Polyphenylquinoxaline | 780-830(decomposition) |
| (19) Silicone resins | 473-873(thermal degradation) |
| 4. Composites | |
| (20) Aluminized grafoil | 933.52(M. P. of Al) |
| (21) Boron fiber aluminum matrix composite | 933.52(M. P. of Al) |
| (22) Graphite fiber aluminum matrix composite | 933.52(M. P. of Al) |
| (23) Boron fiber epoxy composite | 590(epoxy decomposition) |
| (24) Glass fiber epoxy composite | 590(epoxy decomposition) |
| (25) Graphite fiber epoxy composite | 590(epoxy decomposition) |
| (26) Silicon nitride with chopped graphite fiber | |
| (27) Silicon nitride with vitreous silica | |

The thermal radiative properties covered include the four prime properties: emittance, reflectance, absorptance, and transmittance. Additionally, each of the

prime properties are divided into three subproperties: hemispherical spectral, normal spectral, and angular spectral, and each subproperty is treated with respect to both wavelength and temperature dependences, wherever possible.

In the compilation of experimental data, all available data covering from the photographic region of the spectrum up to $100\ \mu\text{m}$ are included. The recommended values resulting from critical evaluation, analysis, and synthesis of the available data and information cover the wavelength range of present interest from visible region (below $1\ \mu\text{m}$) to the infrared of $15\ \mu\text{m}$, if possible. Furthermore, the recommended values as a function of temperature are given for four particularly useful wavelengths (when ever possible); namely: 2.8 , 3.8 , 5.0 , and $10.6\ \mu\text{m}$.

In order to enable the user to fully utilize and properly interpret the data and information presented in this report and also to enhance the usefulness of the data themselves, Section 2 provides the theoretical background of thermal radiative properties, which is believed useful. In Section 3 the procedure for data evaluation and the generation of recommended values is briefly outlined. The original experimental data and the critically evaluated and recommended values in both tabular and graphical forms for the various subproperties of the selected materials are given in Section 4, together with a discussion text and a table on measurement information. The discussion text reviews and discusses the available data and information, the theoretical guidelines and other factors on which the critical evaluation, analysis, and synthesis of data are based, and the considerations involved in arriving at the final assessment and recommendations. In this discussion text the accuracy or uncertainty of the recommended values is also stated. The table on measurement information contains the information on the specimen characterization and measurement method and condition for each set of experimental data. Since most of the selected materials are not well known, a concise description of each of the materials is given at the beginning of each of the subsections in Section 4. The complete bibliographic citations for the 332 references are given in Section 5.

2. THEORETICAL BACKGROUND*

2.1. General Remarks

The purpose of this section is to briefly explain the theoretical background that is helpful in understanding thermal radiative properties and the material presented in this report.

When light or other forms of electromagnetic radiation is incident on a material, three things can happen: the light is reflected, the light is absorbed, or the light is transmitted. Materials in general exhibit selective reflectance, absorptance, and transmittance, which means that the reflectance, absorptance, and transmittance vary with the wavelength of the incident light. For example, if the fraction of the incident light or radiative energy transmitted is plotted against wavelength, it would show peaks and valleys. What is the significance of peaks in a transmittance curve as a function of wavelength? When looking through a piece of blue glass which is illuminated by white light, it would appear blue to an observer. This means that the blue light with its characteristic wavelengths passes through the material and is not absorbed. Red glass which is illuminated by white light will appear red to an observer meaning that the red light with its characteristic wavelengths is not absorbed and passes through the glass with little loss in intensity. Thus, as a generalization, it can be stated that the wavelengths of light that are transmitted by a material are those wavelengths at which the light is not selectively absorbed by the material. This generalization holds not only for visible light but also for thermal radiation. The peaks or high values of transmittance correspond to the thermal radiation which is not absorbed at those particular wavelengths and the valleys or low values of transmittance correspond to the thermal radiation which is absorbed at those particular wavelengths. What physically occurs when light or thermal radiation at certain wavelengths is absorbed? A material is made up of a large number of atoms and/or molecules. These atoms or molecules can undergo various kinds of motion or changes in condition by excitation with light or other electromagnetic radiation of certain wavelengths. When the wavelength of the incident radiation is the same as the wavelength necessary to excite various kinds of motion or changes in condition, the atoms or molecules absorb the radiation of those wavelengths and the remaining radiation with other wavelengths is transmitted through the material.

Radiation is one of the three fundamental means of heat transfer, the others being conduction and convection. Radiation differs from the other means in two important respects: first, no medium is required for the transport of energy by radiation, and second,

* For details, see the text in [T61238 and T66579].

the rate of heat dissipation by radiation varies approximately as the fourth power of the absolute temperature, while that by the other means varies approximately as the first power of temperature. For these reasons, radiation becomes the dominant means of heat transfer at high temperatures and in the absence of an atmosphere.

The thermal radiative properties - emittance, reflectance, absorptance, and transmittance - are the parameters which are descriptive of the energy transported by means of radiation. The properties can be prescribed in greater detail to account for the spectral or wavelength conditions and the geometrical or directional conditions in which the radiant energy interacts with the solid. This interaction can be phenomenologically described by other properties as well, such as the optical constants, complex dielectric constant, or propagation factor, each of which is especially convenient for studying various aspects of the interaction.

There is a marked contrast between the radiative properties of metallic and nonmetallic solids. The magnitude of the radiative properties of the metallic solid is determined to a large extent by the surface condition; due to the high absorption index radiant energy will not travel more than a few hundred angstroms into the metal before being totally absorbed. As a result, surface roughness, oxide layer formations, structural defects due to mechanical stresses, etc. can be predominating influences on the property variations. The nonmetallic or dielectric materials are known to be less sensitive to surface conditions; the absorption and emission processes are "bulk" or "volume" phenomena. This is a consequence of appreciable transparency of the nonmetallic solid to thermal radiation.

The understanding of the basic mechanism of interaction between radiant energy and metallic solids is reasonably well developed. The behavior of the metallic solid is fairly adequately described by the free electron models which indeed are only approximate, but do provide simple and useful tools. The more sophisticated theories, while still not useful as yet for the prediction of numerical values from structural parameters, do provide a means for evaluation of experimental data and a basis for developing empirical relations to meet specific conditions. Our understanding of the theory of nonmetallic behavior is less well developed. The simplest model ascribes the nonmetallic behavior as due to a combination of several types of free electrons and electrons bound to the lattice. The theory is useful for basic understanding of behavior but not tractable for direct computation of property values. The problem is further complicated by transparency, scattering phenomena, and temperature gradients within the solid, which can usually be treated only in a gross or oversimplified manner.

5

In summary, then, pertaining to the principal differences between the metallic and nonmetallic behaviors, it can be stated that there are two: (1) the contributions of the transparency of nonmetallic solids giving rise to "volume" effects rather than "surface" effects which predominate the behavior of metallic solids, and (2) the lack of theoretical tools and simplified models for nonmetallic solids as are available for metallic materials.

2.2. Terminology

In order to understand the many terms and the notation used to describe thermal radiation, an explanation of relevant processes, things, quantities, properties, and descriptors, etc. is called for.

a. Processes

Radiation. The process by which radiant energy is emitted by a body. This process is also called emission.

Reflection. The process by which radiant energy incident on a surface or medium leaves that surface or medium from the incident side.

Transmission. The process by which radiant energy incident on a surface or medium leaves that surface or medium on a side other than the incident side.

Absorption. The process by which radiant energy is converted into another form of energy.

Propagation. The process or processes by which radiant energy is transferred from one region to another region in space.

b. Things

Radiator. A source of radiant energy.

Thermal Radiator. A radiator that emits thermal radiant energy, as a consequence of its temperature only.

Blackbody. A body or surface that absorbs all of the radiant energy incident upon it, and emits the maximum possible amount of thermal radiant energy at each frequency for a body at its temperature.

Reflector. A body that reflects incident radiant energy.

Transmitter. A body that transmits incident radiant energy.

Transparent Body. A body that transmits radiant energy directly, without diffusion or scattering, and has a relatively high transmittance.

Translucent Body. A body that transmits radiant energy principally by diffuse transmission. Objects are not seen distinctly through such a body.

Absorber. A body that absorbs incident radiant energy.

c. Quantities

Radiant Energy, Q. Energy in the form of electromagnetic waves or photons. Joules, ergs, or kilowatt-hours.

Thermal Radiant Energy, Q. Radiant energy that is emitted by a thermal radiator.

Radiant Density, W. $W = dQ/dV$. Radiant energy per unit volume. Joule per cubic meter, erg per cubic centimeter.

Radiant Flux, Φ . $\Phi = dQ/dt$. Time rate of flow of radiant energy. Erg per second, watt.

Radiant Intensity, I. $I = d\Phi/d\omega$. Flux per unit solid angle from a source. Watt per steradian.

Radiance, L. $L = d^2\Phi/d\omega dA \cos \theta$. Flux propagated in a given direction, per unit solid angle about that direction and per unit area projected normal to the direction.

Exitance, M. $M = d\Phi/dA$. Flux per unit area leaving a surface.

Irradiance, E. $E = d\Phi/dA$. Flux per unit area incident on a surface.

d. Properties

Properties ending in "ance" are properties of real specimens, regardless of thickness or surface condition. Properties ending in "ivity" are intrinsic properties of the material of which the specimen is composed, and can only be approached by values measured on real specimens that have clean optically smooth surfaces and are opaque.

Reflectance, ρ . The ratio of reflected flux to incident flux.

Absorptance, α . The ratio of absorbed flux to incident flux.

Transmittance, τ . The ratio of transmitted flux to incident flux.

Internal Transmittance, T. The ratio of the radiant flux reaching the exit surface to the flux which leaves the entry surface of a transparent body.

Emittance, ϵ . The ratio of the radiant exitance of a body at a given temperature to that of a blackbody radiator at the same temperature.

Reflectivity, ρ, ρ_{∞} . The reflectance of a specimen that has an optically smooth surface and is thick enough to be opaque.

Absorptivity, α, α_{∞} . The absorptance of a specimen that has an optically smooth surface and is thick enough to be opaque.

Emissivity, $\epsilon, \epsilon_{\infty}$. The emittance of a specimen that has an optically smooth surface and is thick enough to be opaque.

Reflectance Factor, R . The ratio of the flux reflected by a specimen under specified conditions of irradiation and viewing to that reflected by the ideal completely reflecting, perfectly diffusing surface, identically irradiated and viewed.

For each of the four thermal radiative properties it is necessary to specify the wavelength conditions and the geometrical conditions applicable to the property.

e. Wavelength Descriptor

The only wavelength descriptor that is applicable to this report is the term "spectral". Used as a modifier for a thermal radiative property it means as a function of wavelength. For example, spectral transmittance means transmittance as a function of wavelength and is designated as $\tau(\lambda)$. Used in the context of a condition, the concept spectral means for a very narrow band of wavelength and is also referred to as monochromatic.

f. General Geometrical Descriptors

Figure 1 shows the general case of reflection at a surface and indicates the necessary geometric parameters required to fully describe the incident and reflected fluxes. The beams representing the incident and viewed flux are described by the zenith angles for θ and θ' and by the beam solid angles ω and ω' . The longitudinal angles Φ and Φ' relate the axes of the beams to each other and some reference line on the specimen; as a practical matter very few measurements so specify this angular descriptor. It is the convention in this report to distinguish three sets of general conditions as follows:

Normal - Conditions for incidence and/or viewing through a solid angle ω or ω' , normal to the specimen; that is θ or $\theta' < 15^\circ$.

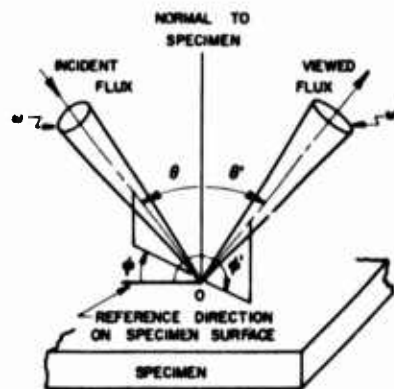


Figure 1. Geometric parameters descriptive of reflection from a surface. θ is the zenith angle, or colatitude, in degrees; Φ is the azimuthal angle, or longitude, in degrees; ω is the beam solid angle, in steradians; and the symbol ' refers to viewing conditions.

Angular - Conditions for incidence and/or viewing through a solid angle ω or ω' at some direction specified by θ or $\theta' \geq 15^\circ$

Hemispherical - Conditions for incidence and/or viewing of flux over a hemispherical region; that is ω or $\omega' = 2\pi$

The descriptors normal and angular do not fully describe the geometric conditions; ω and/or ω' and θ and θ' must be provided to fully specify the geometry.

g. Present Classification Scheme

In the classification scheme used in the data section of this report, reflectance, absorptance, and transmittance subproperties are grouped geometrically by incidence conditions and emittance is grouped by viewing conditions.

For absorptance, transmittance, and reflectance, hemispherical means the radiation is incident over a hemisphere, i. e., $\omega = 2\pi$, while normal means $\theta < 15^\circ$ and angular means $\theta \geq 15^\circ$. For emittance, hemispherical means $\omega' = 2\pi$, normal $\theta' < 15^\circ$, and angular $\theta' \geq 15^\circ$.

h. Symbolic Representation

The various subproperties are expressed according to the following convention. The symbols for the four primary properties ϵ , ρ , α , and τ have already been presented.

The geometric (incidence and viewing conditions) and wavelength descriptors, in that same order, are symbolically represented within the parentheses being separated by semicolons. The most general case would be (using reflectance as an example):

$$\rho(\theta, \Phi, \omega; \theta', \Phi', \omega'; \lambda)$$

where the wavelength descriptor, λ , used in this report has previously been defined.

As a practical matter not all the designations are always needed and many are omitted for convenience sake; usually Φ and Φ' are not used and, of course, for emittance and absorptance, the incidence and viewing geometry symbols, respectively, are not applicable.

It should be noted that for the subproperties of emittance and absorptance, only one geometric descriptor is required to designate the conditions of viewing and incidence, respectively. For the subproperties of reflectance and transmittance, two geometric descriptors are required since both incidence and viewing conditions need to be specified.

2.3. Interrelations Between Thermal Radiative Properties

All matter is continually emitting radiant energy as a result of the thermal vibration of the particles (electrons, ions, atoms, and molecules) of which it is composed. This process is called thermal radiation, and the radiant energy so emitted is called thermal radiant energy.

Each solid body is not only continually emitting thermal radiant energy, but it is also continually being bombarded by radiant energy from its surroundings, some of which is absorbed. The net rate of heat transfer by radiation to or from the body is equal to the difference in the rates of emission and absorption. Hence, the properties of the body that influence these rates are called thermal radiative properties.

When a body is irradiated, part of the incident radiant energy is reflected, part is absorbed, and the rest is transmitted. Nothing else can happen to it. The incident flux, Φ_i , is equal to the sum of the reflected flux, Φ_r , the absorbed flux, Φ_a , and the transmitted flux, Φ_t :

$$\Phi_i = \Phi_r + \Phi_a + \Phi_t \quad (2.3-1)$$

This is an example of the Law of Conservation of Energy.

The reflectance, ρ , is the ratio of reflected flux to incident flux; the absorptance, α , is the ratio of absorbed flux to incident flux; and the transmittance, τ , is the ratio of transmitted flux to incident flux. Dividing both sides of eq. (2.3-1) by Φ_i gives

$$1 = \rho + \alpha + \tau \quad (2.3-2)$$

For opaque materials, $\tau = 0$, hence for such materials

$$\rho + \alpha = 1 \quad (\tau = 0) \quad (2.3-3)$$

Kirchhoff's law states that the absorptance is equal to the emittance

$$\alpha = \epsilon \quad (2.3-4)$$

Thus, for an opaque material

$$\rho + \epsilon = 1 \quad (2.3-5)$$

and the thermal radiative properties of an opaque body are fully described by either the reflectance or the emittance. However, there are certain restrictions that apply to eqs. (2.3-2) through (2.3-5). They are restricted by the geometric and wavelength distribution of the reflected and emitted radiant energy. Considering the geometric distribution only, for opaque specimens

$$\alpha(\theta, \omega) = 1 - \rho(\theta, \omega; 2\pi) \quad (2.3-6)$$

where θ, ω are the same for α and ρ , and

$$\epsilon(\theta', \omega') = \alpha(\theta, \omega) \quad (2.3-7)$$

where $\theta = \theta'$ and $\omega = \omega'$. Equation (2.3-6) was derived on the basis of conservation of energy. Incident radiant energy that is not reflected must be absorbed and eq. (2.3-7) is a statement of Kirchhoff's law. Equations (2.3-6) and (2.3-7) can be used to convert one type of data (subproperty) to another. If normal emittance data are not available, for instance, normal absorptance or normal hemispherical reflectance can be used to compute the desired values.

The variation of the thermal radiative properties with temperature, wavelength, and geometric conditions (including polarization) of irradiation and viewing poses certain restrictions on eqs. (2.3-2) through (2.3-5). For eqs. (2.3-2) and (2.3-3) to be valid, α, ρ , and τ must be evaluated under the same conditions, which means that the temperature of the specimen must be the same, and the spectral composition, direction, solid angle, and degree and direction of polarization of the incident radiant energy must be identical, and all of the reflected and transmitted radiant energy must be measured.

Kirchhoff's law, eq. (2.3-4), is derived for the condition that the specimen is irradiated in a blackbody cavity with walls at the same temperature as the specimen, which means that the specimen is uniformly irradiated over a hemisphere with unpolarized radiant energy having the spectral distribution of that of a blackbody radiator at

the temperature of the specimen. However, it can be proved that eq. (2.3-4) is also valid for the two conditions: (1) any solid angle less than a hemisphere if the direction and solid angle of the incident beam for the absorption evaluation is identical to the direction and solid angle (but opposite in sense) of the emitted beam for the emittance evaluation, and (2) for plane-polarized radiant energy with the plane of polarization at any given angle to the plane of measurement, provided that it is the same for the incident radiant energy for the absorption evaluation and the emitted radiant energy for the emittance evaluation. Even with these modifications, eq. (2.3-4) applies strictly only provided the spectral composition of the incident radiant energy for the absorptance is that of blackbody radiant energy at the temperature of the specimen. This would appear to impose a severe restriction on the general applicability of eq. (2.3-5). However, it can also be shown that eq. (2.3-4) applies to any small wavelength band, as well as to total blackbody radiant energy. The properties of reflectance, absorptance, and transmittance do not vary with the amount of incident radiant energy until very high flux densities are reached. Within the narrow wavelength band used in measuring spectral thermal radiative properties the spectral distribution of radiant energy from almost any thermal source is approximately the same as that from a blackbody radiator at the temperature of the specimen. Also, polarization effects are completely absent for normally incident radiant energy and are negligible at angles near the normal. Hence eqs. (2.3-4) and (2.3-5) can be considered valid for normal spectral properties and can be used to convert normal hemispherical reflectance to normal emittance with but little error.

2.4. Fresnel Equations for Specular Reflection

When an electromagnetic wave in vacuum is incident on the plane surface of an optically homogeneous specimen, interaction of the wave with the material of the specimen will occur. The electrical and magnetic properties of the specimen will be different from those of the vacuum, and as a result, there may be a change in the direction of propagation of the wave, its velocity, amplitude, wavelength, and phase, and it may be separated into two portions, one reflected and one transmitted. The transmitted portion will be partially or totally absorbed. The only property of the wave that never changes is its frequency.

Similar changes in the wave will occur whenever it is incident on an interface between two media of different properties. The changes can be computed from the properties of the material, or the differences in properties on the two sides of the interface, and from the direction of propagation of the wave relative to the interface and the direction of its plane of polarization relative to the plane containing the direction of incidence and the normal to the interface at the point of incidence.

The optical properties describe the interaction of an electromagnetic wave with matter in terms of phase and amplitude, while the thermal radiative properties describe the energy transfer during the interaction. It is obvious that the two types of properties, optical and thermal radiative, are related. In some cases the relationships are simple.

One situation in which the relation is not simple is that for the general case of a wave incident on an interface. By solving the Maxwell equations for the boundary conditions, the Fresnel relations for specular reflection can be derived. The specular reflectance at the interface (fraction of incident flux reflected in the direction of mirror reflectance) is given as [see pp. 17 and 18 of A00012]

$$\rho_s(\theta) = \frac{Q^2 + P^2 - 2Q \cos \theta + \cos^2 \theta}{Q^2 + P^2 + 2Q \cos \theta + \cos^2 \theta} \quad (2.4-1)$$

$$\rho_p(\theta) = \rho_s(\theta) \frac{Q^2 + P^2 - 2Q \sin \theta \tan \theta + \sin^2 \theta \tan^2 \theta}{Q^2 + P^2 + 2Q \sin \theta \tan \theta + \sin^2 \theta \tan^2 \theta} \quad (2.4-2)$$

where

$$2Q^2 = [(n^2 - k^2 - \sin^2 \theta)^2 + 4n^2k^2]^{1/2} + (n^2 - k^2 - \sin^2 \theta) \quad (2.4-3)$$

$$2P^2 = [(n^2 - k^2 - \sin^2 \theta)^2 + 4n^2k^2]^{1/2} - (n^2 - k^2 - \sin^2 \theta) \quad (2.4-4)$$

The angle θ is the angle between the incident ray and the normal to the interface, ρ_s is the reflectance for plane-polarized incident radiant energy with its plane of polarization normal to the plane of incidence (the plane containing the incident ray and the normal to the interface at the point of incidence), ρ_p is the reflectance for plane-polarized incident radiant energy with its plane of polarization parallel to the plane of incidence, n is the refractive index, and k is the absorption index.

If the incident radiant energy is completely unpolarized

$$\rho(\theta) = \frac{1}{2} [\rho_s(\theta) + \rho_p(\theta)]. \quad (2.4-5)$$

For an opaque material the directional absorptance can be found and using Kirchhoff's law, eq. (2.3-4), the directional emittance can be found for the polarized components

$$\epsilon_s(\theta) = \alpha_s(\theta) = 1 - \rho_s(\theta) \quad (2.4-6)$$

$$\epsilon_p(\theta) = \alpha_p(\theta) = 1 - \rho_p(\theta) \quad (2.4-7)$$

and also for unpolarized light

$$\epsilon(\theta) = \alpha(\theta) = 1 - \rho(\theta) \quad (2.4-8)$$

The Fresnel eqs. (2.4-1) and (2.4-2) have been expressed in terms of n and k , but the relations are found in various forms in the literature. The simplest case occurs for normal incidence ($\theta = 0$), where the equations reduce to

$$\rho_p(0) = \rho_s(0) \quad (2.4-9)$$

and

$$Q = n \quad P = k \quad (2.4-10)$$

Hence, for radiant energy incident from vacuum or a medium of index of refraction of 1,

$$\rho(0) = \frac{(n - 1)^2 + k^2}{(n + 1)^2 + k^2} \quad (2.4-11)$$

2.5. Thermal Radiative Properties of Metals

a. General Behavior

The general behavior of the thermal radiative properties of metals is shown in Figure 2. For thicknesses greater than several hundred angstroms, metals are opaque, that is, they show zero transmittance for all wavelengths. The reflectance rises in the region of 1-2 μm to a large value which has a slightly increasing slope. The emittance and absorptance decrease rapidly in the region of 1-2 μm reaching a low value with a slight negative slope.

b. Classical Free-Electron Theory

The theoretical models for ideal metallic surfaces leads to help in predicting some thermal radiative properties.

The earliest attempts to predict the optical properties of metals were made by Lorentz, Drude [T20117], Kronig [A00023], and Mott and Zener [A00022], who assumed the metal to contain electrons which were essentially free to move under the influence of the electric field induced by the incident electromagnetic wave. These free electrons are the valence electrons in the outer shell of the atoms constituting the metal. When the wave is incident upon its surface, an oscillating electric field parallel to the surface is induced in the metal and the free electrons will oscillate under the influence of this field at the frequency of the incident wave. There is a phase difference between the

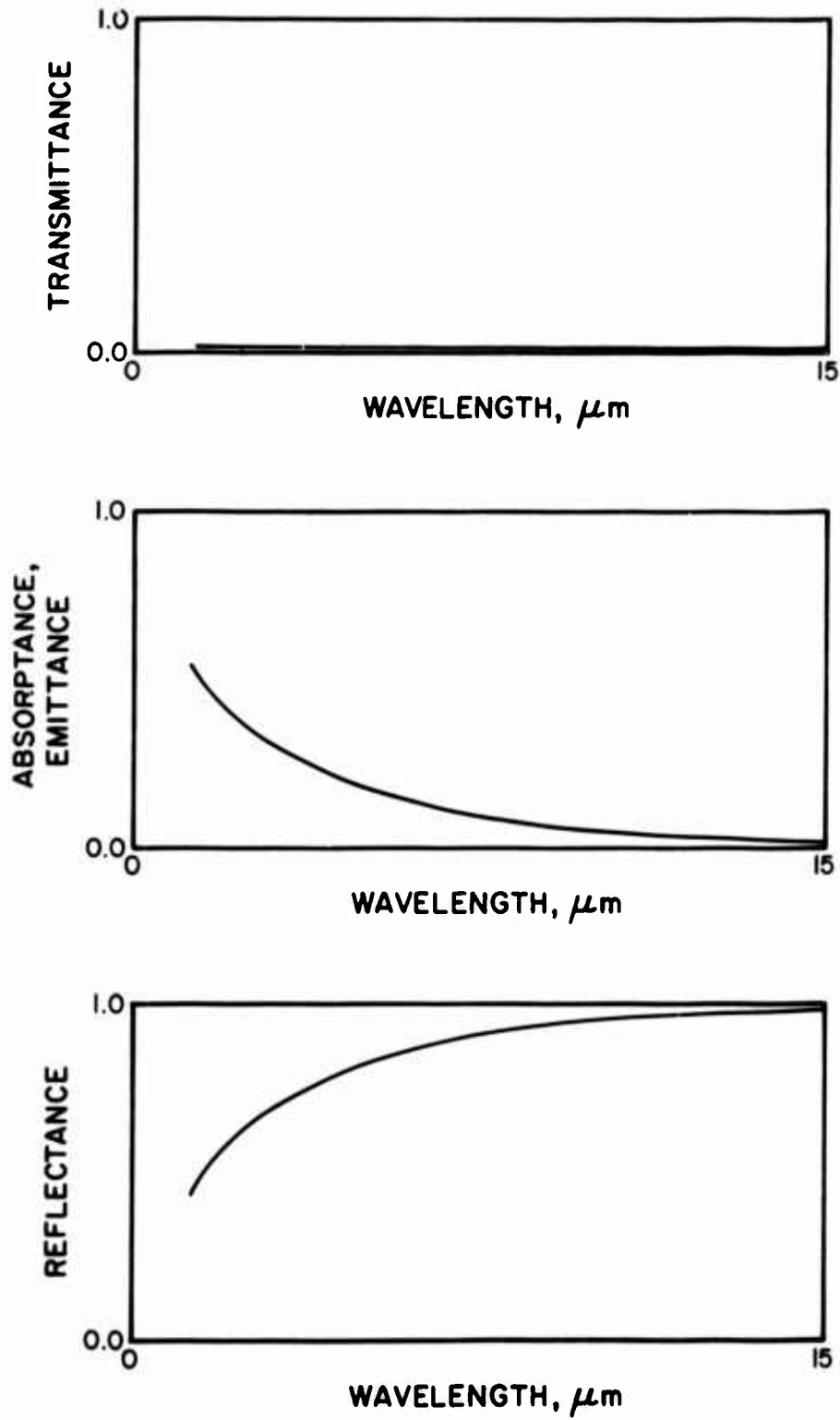


Figure 2. Typical behavior of thermal radiative properties of metals.

oscillation of the electrons and that of the field, caused by a viscous damping force arising from collisions between accelerated electrons and the atomic lattice. To describe the optical behavior of the material requires two parameters: the number density of free electrons, N , being excited by the induced field, and the average time (relaxation time, τ) between collisions of the electron with the atomic lattice. These two parameters can be estimated from the number of valence electrons per unit volume, the electrical conductivity and the assumption of a spherical Fermi surface. This is called the Drude Free Electron model, and is shown in Table 1 expressing the complex dielectric constant, K^* , as a function of the two parameters N and τ . See the List of Symbols for the meaning of other symbols.

If the phase change arising from electronic collisions can be neglected, the model describing the optical behavior of the material is greatly simplified. This situation occurs when the relaxation time is zero or when the time between electronic collisions is much less than the period of the induced electric field. For this condition, the optical behavior can be completely described by one material parameter - the dc electrical resistivity, r . Table 1 presents the resulting model for the complex dielectric constant, labeled the Simplified Drude Free Electron model.

This simplified model for the optical constants serves as the basis for relations used to compute the thermal radiative properties of materials from knowledge of the electrical resistivity (or conductivity) as a function of temperature. If the appropriate relation between the complex dielectric constant, K^* , and $\epsilon(0; \lambda)$ is used with the simplified Drude model, the normal spectral emissivity can be expressed as a function of the electrical resistivity, r , in the series form

$$\epsilon(0; \lambda) = 0.365(r/\lambda)^{1/2} - 0.0464(r/\lambda) + \dots \quad (2.5-1)$$

Table 1. Classical Models for the Optical Properties of Metals (MKS Units)

Drude Free Electron. Assumes the metal contains free electrons which are subjected to an oscillating electric field and a viscous damping force proportional to the velocity of the electrons arising from collisions between accelerated electrons and the atomic lattice.

$$K^* = 1 - \left(\frac{\lambda}{\lambda_0}\right)^2 \frac{1 + j(\lambda/\lambda_1)}{1 + (\lambda/\lambda_1)^2} \quad \begin{aligned} \lambda_1 &= 2\pi c\tau \\ \lambda_0 &= \left[\frac{\pi mc^2 \epsilon_0}{q^2 N}\right]^{1/2} \end{aligned}$$

Simplified Drude Free Electron. Drude theory valid for long wavelengths where currents in the metal are in phase with electric field.

$$K^* = -j \frac{\lambda}{c\epsilon_0 r}$$

where the units are r (ohm-m) and λ (m). This celebrated relation is frequently referred to as the Hagen-Rubens relation.

From the above discussions, the assumptions used to derive this basic model limit the Hagen-Rubens relation to long wavelengths (usually beyond $10 \mu\text{m}$) and high temperatures for metals in which the electronic structure can be approximated by one class of free electrons as the current carriers. This relationship has found extensive use in engineering applications.

An equation that can be used for the short wavelength region is developed by introducing a resonant wavelength into the denominator

$$\epsilon(0; \lambda) = A' \left(\frac{r}{\lambda - \lambda_0} \right)^{1/2} + B' \left(\frac{r}{\lambda - \lambda_0} \right) + \dots \quad (2.5-2)$$

where A' and B' are adjustable parameters. For metals, the resistivity is connected with temperature as

$$r = r_0 [1 + \beta (T - 293)] \quad (2.5-3)$$

where r_0 is the resistivity of the metal at 293 K and β is the temperature coefficient of the resistivity. Alternatively, the resistivity can be connected to the temperature by means of a power series

$$r = A' + B' T + C' T^2 + D' T^3 \quad (2.5-4)$$

Using eq. (2.5-3) in eq. (2.5-2), the Hagen-Rubens equation becomes

$$\epsilon(0, \lambda) = A + B \left[\frac{1 + \beta(T-293)}{\lambda - \lambda_0} \right]^{1/2} + C \left[\frac{1 + \beta(T-293)}{\lambda - \lambda_0} \right] + D \left[\frac{1 + \beta(T-293)}{\lambda - \lambda_0} \right]^{3/2} \quad (2.5-5)$$

where A , B , C , D , and λ_0 are adjustable parameters. By finding the normal spectral emittance, the normal spectral absorptance and reflectance can be computed from Kirchhoff's law, i. e.,

$$\alpha(0, \lambda) = \epsilon(0, \lambda) \quad (2.5-6)$$

and then, since a metal is opaque, the reflectance can be found from

$$\rho(0, 2\pi, \lambda) = 1 - \alpha(0, \lambda) \quad (2.5-7)$$

c. Non-Ideal Surfaces

The preceding discussion of the theoretical models used to predict radiative properties applied to ideal surfaces.

It has been understood for many years that the surface condition of metallic specimens plays a dominant role in the magnitude of the radiative properties. The literature abounds with examples of test surfaces shown to be very sensitive to methods of preparation, thermal history, and environmental conditions. Despite this awareness, descriptions of test surfaces are generally inadequate because of our modest understanding of the important mechanisms of real surface effects and how to properly characterize a surface.

Topographical, chemical, and physical (structural) characteristics all influence the properties of the metallic surface. The topographical characteristics describe the profile or geometry of the surface - the boundary between the material and the surrounding medium. The chemical characteristics describe the composition of the surface layer including such features as inhomogeneities and contaminants. The physical characteristics describe the structure of the surface such as crystal lattice orientation, particle size, strain, and other features which might affect the radiant energy exchange process.

To isolate the individual surface characteristics as outlined is a difficult task. For most materials it is not practical to alter one characteristic without causing an influence on another. The control of the many variables required to study surface characterization in a logical manner is a complex problem. As a result only the simplest of surface profiles or compositional effects have been studied or are understood.

The most important influences on the radiative properties of metals arise from surface roughness and films (oxide growth). The effect is most pronounced on the spectral radiative properties when the characteristic profile variation or film thickness is of the same order as the wavelength of interest. For some situations a thin dielectric film has a more significant influence on emittance properties than does surface roughness of the same dimension. These changes in spectral properties are also apparent as changes in angular distribution of reflected or emitted energy.

The influences of surface characteristics - topographical, chemical, physical - can be considerably dependent upon the energy spectrum of importance to the radiative property of interest. For example, the description of a surface for use as a room temperature absorber ($5 < \lambda < 40 \mu\text{m}$) will be quite different from that for a solar absorber ($0.25 < \lambda < 4 \mu\text{m}$). Also the techniques required to study each will be quite different.

The profiles of real metal surfaces are always shown as irregular patterns of peaks and valleys. Various parameters are in common use to describe the topography of a surface including RMS (root mean square) height, CLA (center line average) height,

lay, average slope, height distribution, etc. [A00021, T36500, A00020]. Such parameters are obtained primarily from stylus-type profilometers and to some extent from interferometry techniques.

The effect of surface roughness on the optical properties of materials was first studied by Lord Rayleigh, but only recently has this problem been of intense interest. If the size of the irregularities is of the order of the wavelength or larger, the interaction can be described by geometrical optics [T33896]. In this case, the facets of the surfaces reflect in various directions, and the properties/orientation of the facets must be described by some statistical process in order to explain the optical behavior of the surface. If, however, the surface irregularities are much smaller than the wavelength, the optical behavior can be explained by diffraction phenomena.

The diffraction problem was originally studied by Rice [A00019] and Davies [A00018] and their work was extended and experimentally verified by Bennett and Porteus [T45929]. Their expression for the relative reflectance ratio of the rough, ρ , to smooth, ρ_0 , surface at normal incidence is given as

$$\frac{\rho}{\rho_0} = \exp [-(4\pi\sigma/\lambda)^2] + 32\pi^4 (\sigma/\lambda)^4 (\Delta\theta)^2/m \quad (2.5-6)$$

where σ is the RMS roughness, m is the RMS slope, and $\Delta\theta$ is the half angle of acceptance of the optical system. The first term represents the coherently or specularly reflected fraction and the second term the incoherent or diffusely reflected term. The second term is shown proportional to $(\sigma/\lambda)^4$, and hence for longer wavelengths and smoother surfaces the first term predominates.

2.6. Thermal Radiative Properties of Nonmetallic Solids

a. General Behavior

The typical behavior for a nonmetallic solid which is transparent with little scattering is shown in Figure 3. The transmittance rises sharply in the region of 1-2 μm to a large constant value and drops sharply towards zero in the 8-9 μm region (the use of the 1-2 μm range and the 8-9 μm range is done only for illustrative purposes). Since the reflectance is of the order of 10% and decreases slowly in the entire range of interest, the emittance and absorptance show a behavior as if the transmittance were rotated 180° about the wavelength axis. The emittance decreases sharply in the 1-2 μm region, stays at a constant but low level and in the 8-9 μm region rises sharply to a level near 1.0.

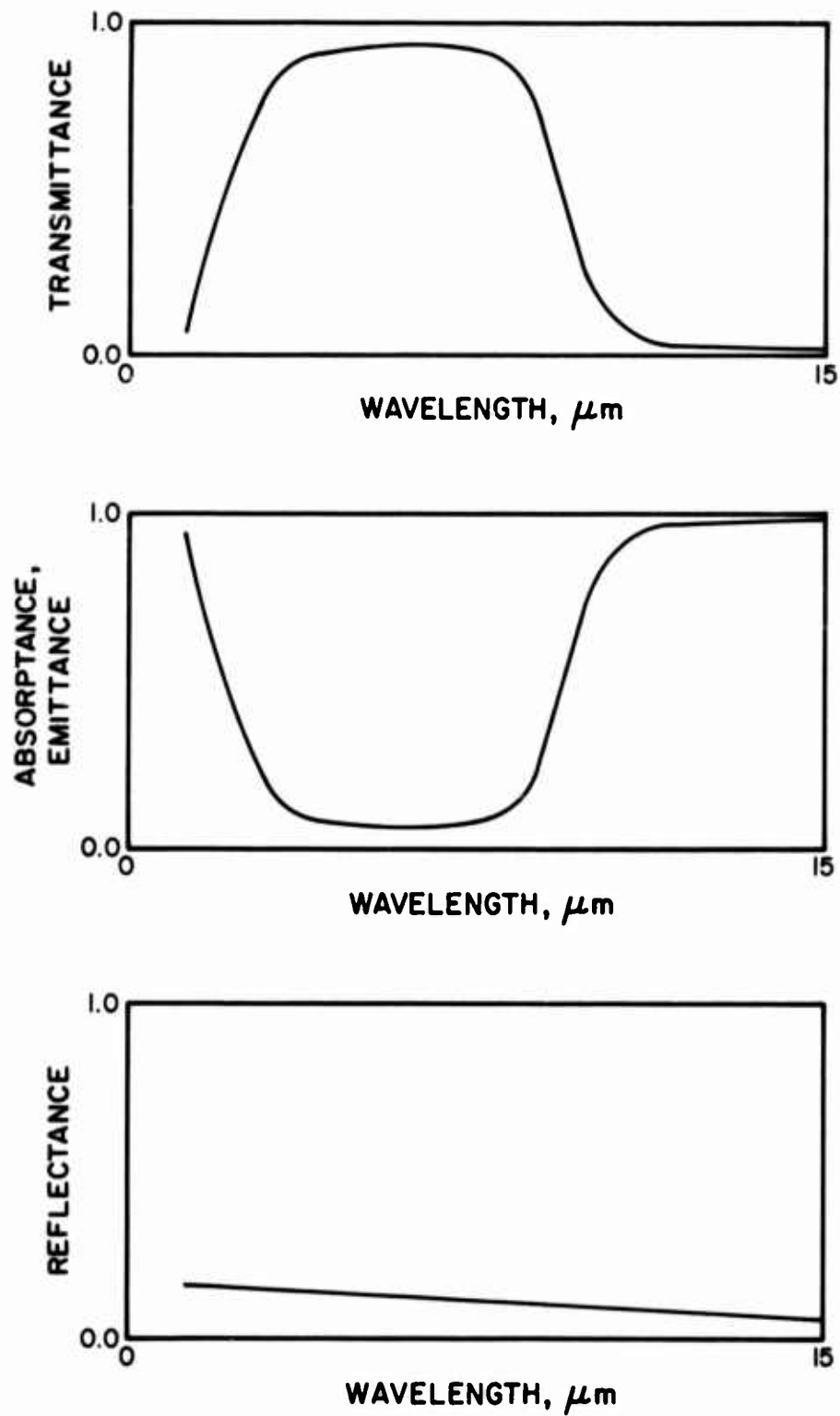


Figure 3. Typical behavior of thermal radiative properties of a transparent non-scattering nonmetallic solid.

b. Partially Transparent Material - Multiple Reflection Model

The simplest of the models to deal with the partially transparent nonscattering materials was developed by McMahan [T20468]. The theory is limited to only the passage of radiant energy normal to the surface but is useful to the very common problem of interpretation of reflectance or transmittance spectra of a partially reflecting slab sample.

Kirchhoff's law in its simplest form relates the spectral emissivity to spectral reflectivity of an opaque material as

$$\epsilon(\lambda, T) = 1 - \rho(\lambda, T) \quad (2.6-1)$$

For a body which is partially transparent because of its low absorption coefficient and/or thickness, Kirchhoff's law cannot be applied directly. Recall that the law derives from the existence of an energy balance between the emission and absorption of a body in thermal equilibrium within a uniformly heated enclosure. When the body is opaque, the incident flux is absorbed or reflected. If the body is partially transparent, the incident flux is absorbed and a significant fraction appears as reflected and transmitted flux after having undergone many internal reflections. For the general expression of Kirchhoff's law it is necessary to include the influence of transmittance.

McMahon shows the three measurable quantities emittance, reflectance, and transmittance are related to the single surface reflectance, R , and the internal transmittance, T , by the following expressions

$$\epsilon(\lambda) = \frac{[1-R(\lambda)] [1-T(\lambda)]}{[1-R(\lambda) T(\lambda)]} \quad (2.6-2)$$

$$\rho(\lambda) = R(\lambda) \left[1 + \frac{T^2(\lambda) [1-R(\lambda)]^2}{1-R^2(\lambda) T^2(\lambda)} \right] \quad (2.6-3)$$

$$\tau(\lambda) = T(\lambda) \frac{[1-R(\lambda)]^2}{[1-R^2(\lambda) T^2(\lambda)]} \quad (2.6-4)$$

The summation of these three equations is unity:

$$\epsilon(\lambda) + \rho(\lambda) + \tau(\lambda) = 1 \quad (2.6-5)$$

and this expression is the extension of Kirchhoff's law to partially transparent bodies.

Also, the results for ϵ , ρ , and τ can be understood by considering a collimated beam of radiant flux incident normally on a semitransparent slab of thickness d and complex index of refraction n^* . The incident flux upon first striking the interface is partially reflected and the balance passes through the interface. The reflected portion

R is computed from the Fresnel relations for normal incidence conditions

$$R = \left(\frac{n^* - 1}{n^* + 1} \right)^2 \quad (2.6-6)$$

It is important to recognize that this reflectance, R, is based upon a single reflection. The remaining flux that passes through the interface will traverse the thickness of the slab while being absorbed and eventually reach the back side. In the course of traversing the thickness of the slab, the radiant flux is diminished by a factor e^{-ad} , where a is the absorption coefficient and d is the specimen thickness. It is convenient to define the internal transmittance, T, as

$$T = e^{-ad} \quad (2.6-7)$$

which is the transmittance (frequently referred to as the transmissivity) within the material and is not affected by or inclusive of interface influences. Of the original flux striking the slab, the fraction $(1 - R)T$ has reached the near side of the slab upon first traversing the slab thickness. At this near interface, a fraction R is reflected and the balance passes through. This process of multiple reflection at the interfaces and traversing of the thickness must be considered to determine the overall transmittance and reflectance of the slab. Figure 4 represents the multiple processes occurring, giving the results

$$\rho = R \left[1 + \frac{T^2(1 - R)^2}{1 - R^2T^2} \right] \quad (2.6-8)$$

$$\tau = T \left[\frac{(1 - R)^2}{1 - R^2T^2} \right] \quad (2.6-9)$$

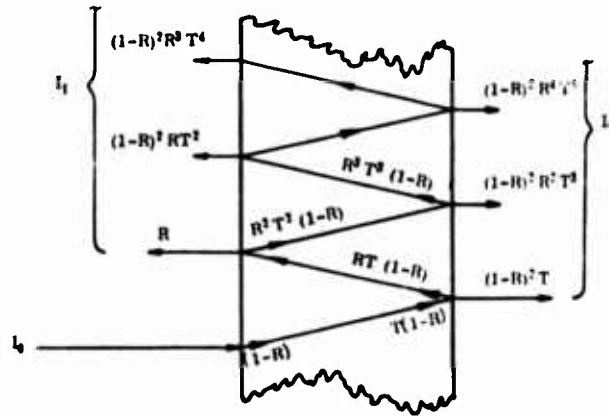
In terms of the single surface reflectance, R, absorption coefficient, a, and thickness, d, the relations are

$$\tau = \frac{(1 - R)^2 e^{-ad}}{1 - R^2 e^{-2ad}} \quad (2.6-10)$$

$$\rho = R \left[1 + \frac{e^{-2ad} (1 - R)^2}{1 - R^2 e^{-2ad}} \right] \quad (2.6-11)$$

$$\epsilon = \alpha = \frac{(1 - R) (1 - e^{-ad})}{1 - R e^{-ad}} \quad (2.6-12)$$

The above equations hold for $k \ll n$ where k is the absorption index ($\alpha = 4\pi k/\lambda$).



$$\rho = \frac{I_1}{I_0} = R + (1-R)^2 RT^2 + (1-R)^2 R^3 T^4 + \dots = R \left[1 + \frac{T^2(1-R)^2}{1-R^2 T^2} \right]$$

$$\tau = \frac{I_2}{I_0} = (1-R)^2 \{ T + R^2 T^3 + R^4 T^5 + \dots \} = T \frac{(1-R)^2}{1-R^2 T^2}$$

Figure 4. The reflectivity and transmissivity of a semitransparent slab.

A special case of the eqs. (2.6-10) through (2.6-12) is for the case of zero absorption ($\alpha \rightarrow 0$). In that case

$$\epsilon = \alpha = 0 \quad (2.6-13)$$

$$\tau = \frac{2n}{n^2 + 1} \quad (2.6-14)$$

$$\rho = \frac{(n-1)^2}{n^2 + 1} \quad (2.6-15)$$

The extension of eq. (2.6-10) that holds for k not being less than n is [p. 14 of A00024]

$$\tau = \frac{(1-R)^2 e^{-ad} \left(1 + \frac{k^2}{n^2} \right)}{1 - R^2 e^{-2ad}}$$

c. Kodak Scheme

Kodak has a method of calculating absorptance and reflectance from transmittance and refractive index data [E62600]. The energy impinging on a transparent slab is broken up into a reflected and transmitted beam. This is continued for three passes and the components added. The analysis is carried out in terms of the loss value factor, K , from which reflectance and absorptance are calculated. The value of the loss value factor in terms of the measured transmittance, T , and the single surface reflectance, R , is

$$\kappa = \frac{1 - T - 2R(1 - R + R^2)}{1 - 2R + 4R^2} \quad (2.6-16)$$

and

$$\rho = R [1 + (1 + \kappa)^2 (1 - R)^2] \quad (2.6-17)$$

$$\alpha = \epsilon = \kappa (1 - \kappa R) \quad (2.6-18)$$

d. Polymers

Pregelhof, Franey, and Haas [T77125] use a one-dimensional model for polycarbonate plastics, and assuming uniform properties, the emittance $\epsilon(\lambda)$, absorptance $\alpha(\lambda)$, transmittance $\tau(\lambda)$, and reflectance $\rho(\lambda)$ of a polymer sheet can be derived as follows.

$$\epsilon(\lambda) = \alpha(\lambda) = \frac{(1 - R) [(1 + R) \sinh ad + (1 - R) (\cosh ad - 1)]}{(1 + R^2) \sinh ad + (1 - R^2) \cosh ad} \quad (2.6-19)$$

$$\tau(\lambda) = \frac{(1 - R)^2}{(1 + R^2) \sinh ad + (1 - R^2) \cosh ad} \quad (2.6-20)$$

$$\rho(\lambda) = \frac{2R [R \sinh ad + (1 - R) \cosh ad]}{(1 + R^2) \sinh ad + (1 - R^2) \cosh ad} \quad (2.6-21)$$

where $R = (n - 1)^2 / (n + 1)^2$ and n is the refractive index, d is the thickness of the sample, and a is the absorption coefficient.

For the polycarbonate plastic bulk materials, it can be assumed that

$$e^{ad} \gg R^2 e^{-ad} \quad (2.6-22)$$

which enables eqs. (2.6-19) through (2.6-21) to become the following:

$$\epsilon(\lambda) = \alpha(\lambda) \cong (1 - R) [1 - (1 - R) e^{-ad} - R e^{-2ad}] \quad (2.6-23)$$

$$\tau(\lambda) \cong (1 - R)^2 e^{-ad} \quad (2.6-24)$$

$$\rho(\lambda) \cong R [1 + (1 - 2R) e^{-2ad}] \quad (2.6-25)$$

In a wavelength region when the material becomes opaque, i. e., $\tau = 0$, the absorptance can be obtained from

$$\alpha(\lambda) \cong (1 - R)$$

3. DATA EVALUATION AND GENERATION OF RECOMMENDED VALUES

As a result of comprehensive search of literature, numerous research documents of interest to this program are uncovered. These documents are procured and studied, from which pertinent data are extracted, scrutinized, organized, key-punched, homogeneously tabulated, and plotted in huge working graphs readied for data analysis and synthesis. The information on specimen characterization and measurement methods and conditions is recorded in a table specially designed for recording measurement information, which includes (to the extent provided in the original source document) the following:

- (1) Purity, chemical composition, dopant concentration, carrier concentration, defect concentration.
- (2) Type of crystal, crystal axis orientation.
- (3) Microstructure, grain size, inhomogeneity, additional phases.
- (4) Specimen shape and dimensions.
- (5) Method and procedure of fabrication.
- (6) Manufacturer and supplier, stock number, catalog number.
- (7) Heat, mechanical, irradiative, and other treatments.
- (8) Surface conditions.
- (9) Film thickness and substrate material.
- (10) Test environment, degree of vacuum or pressure.
- (11) Experimental method used in the measurement.
- (12) Reference standard used in data observation or reduction.
- (13) Form in which data are presented in the original source document other than tabular data.
- (14) Other pertinent remarks.

Due to the difficulties in accurate measurement of thermal radiative properties of materials and in exact characterization of test specimens and surface conditions, the available experimental data extracted from various research documents are usually widely divergent and subject to large uncertainty. Data evaluation and analysis is therefore very important. The procedure involves critical evaluation of the validity and reliability of the data and related information, resolution and reconciliation of disagreements in conflicting data, correlation of data in terms of various controlling parameters, curve fitting with theoretical or empirical equations, comparison of results with theoretical predictions or with results derived from theoretical relationships or from generalized empirical correlations, etc. Besides critical evaluation and analysis of existing data,

theoretical methods and semiempirical techniques are employed to fill data gaps and to synthesize fragmentary data so that the resulting recommended values are internally consistent and cover as wide a range of wavelength or temperature as possible.

Depending upon the level of confidence the data analyst has placed on the values and upon the degree of completeness of characterization of the test material and surface conditions for which the values are generated, the values are designated as "recommended values", "provisional values", or "typical values". In this report, all the values generated have been properly designated, and the accuracy or uncertainty of the values clearly stated.

4. THERMAL RADIATIVE PROPERTIES OF SELECTED MATERIALS

In each of the following subsections the thermal radiative property data and information for each dependence of each subproperty of each material are presented in the following order: (1) discussion text, (2) table of recommended values, (3) figure of recommended curves, (4) figure of experimental data, (5) table of measurement information, and (6) table of experimental data.

In the discussion text, a review and discussion of the available data and information for the particular dependence of the particular subproperty of the material is given, together with a discussion of the theoretical guidelines and other factors on which the critical evaluation, analysis, and synthesis are based and of the considerations involved in arriving at the final assessment and recommendations.

In the table of recommended values, the values are tabulated with small increments in temperature or wavelength so that linear interpolation of values is meaningful. The recommended values cover the spectrum from visible region (below $1\ \mu\text{m}$) up to the infrared of $15\ \mu\text{m}$, whenever possible. Those values as a function of temperature are, whenever possible, tabulated for four particular gas-laser wavelengths: $2.8\ \mu\text{m}$ (hydrogen fluoride laser), $3.8\ \mu\text{m}$ (deuterium fluoride laser), $5.0\ \mu\text{m}$ (carbon monoxide laser), and $10.6\ \mu\text{m}$ (carbon dioxide laser). The values may be designated as recommended, provisional, or typical values. The accuracy or uncertainty of the values is stated in the discussion text. In this report, the ranges of uncertainties of recommended, provisional, and typical values are less than $\pm 15\%$, between $\pm 15\%$ and $\pm 30\%$, and greater than $\pm 30\%$, respectively.

In the figure of recommended curves, experimental data (sometimes selected) are also shown as background for comparison. The curves and data are plotted only up to $14\ \mu\text{m}$, even though the recommended values or available experimental data may exist above $14\ \mu\text{m}$. Those values or data above $14\ \mu\text{m}$ not shown in the figure can always be found in the table.

In the figure of experimental data, similarly, data in the wavelength range above $14\ \mu\text{m}$ are not shown. They are, however, tabulated in the experimental data table. Corresponding to each set of data plotted in the figure and tabulated in the experimental data table, the information on the specimen characterization and measurement method and condition is given in the table of measurement information.

Since most of the selected materials are not well known, a concise description of each of the materials is given at the beginning of each of the subsections.

4.1. Aluminum Alloy 2024

Aluminum Alloy 2024, formerly known as Aluminum Alloy 24S, is a wrought alloy with copper as the principal alloying element. Its nominal composition [A00005] is (by weight) 4.5% Cu, 1.5% Mg, 0.6% Mn, and balance Al.

Some physical [T15906] and mechanical properties [A00006] of this material are as follows: solidus temperature, 775 K; liquidus temperature, 911 K; specific gravity, 2.77; tensile (ultimate) strength, 19.0-51.0 kg/mm²; Brinell hardness number (500 kg load, 10 mm ball), 47-130. These properties vary over a wide range due to differences in applied heat treatments.

In the heat treated condition, the mechanical properties of this alloy are similar to, and sometimes exceed, those of mild steel. This heat treatment is specified by a letter "T" after the 2024 designation. The "T", followed by the numerals 1-10, inclusive, designates one specific combination of basic treatments, thus Aluminum Alloy 2024-T4. Briefly, these heat treatments are broken down as follows [A00006]:

- T1 - cooled from an elevated temperature shaping process and naturally aged to a substantially stable condition.
- T2 - annealed (cast products only)
- T3 - solution heat-treated and then cold worked
- T4 - solution heat-treated and naturally aged to a substantially stable condition
- T5 - cooled from an elevated temperature shaping process and then artificially aged
- T6 - solution heat-treated and then artificially aged
- T7 - solution heat-treated and then stabilized
- T8 - solution heat-treated, cold worked, and then artificially aged
- T9 - solution heat-treated, artificially aged, and then cold worked
- T10 - cooled from an elevated temperature shaping process, artificially aged, and then cold worked.

Each of these thermal treatments [A00005] has a unique effect on the mechanical properties of the alloy. The symbol does not define the time and temperature of the thermal treatments; the details of the practice may be varied as desired or convenient if the end result as expressed by specified mechanical properties is unchanged. Should variation of the same basic operation be applied to the same alloy, resulting in different characteristics, other digits are added to the basic designation (Aluminum Alloy 2024-T81 or Aluminum Alloy 2024-T851). The second and third numbers in the heat treatment designation are arbitrary numbers, generally having no logical significance. With the

older nomenclature the specific heat treatments were not catalogued as above. An alloy may be described as Aluminum 24S-T, where the T only means that the material was tempered to a stable condition.

This alloy does not have as good corrosion resistance properties as most other aluminum alloys and under certain conditions may be subjected to intergranular corrosion. Therefore, it is widely used in the clad, anodized, or alodined states. In the clad [A00006] state the 2024 Aluminum Alloy is protected from corrosion by a thin surface of pure metal or an alloy with a higher solution potential than Aluminum Alloy 2024. In this report the term alclad was assumed to have meant the cladding material was pure aluminum. The anodizing [A00005] process involves forming a conversion coating on the metal surface by anodic oxidation. Alodining is also a conversion coating, with the coating being some other type of material such as a phosphate or chromate. These processes greatly increase Aluminum Alloy 2024's resistance to corrosion.

In this report data is actually reported for four different types of Aluminum Alloy 2024 for different subproperties. These types are as follows: Aluminum Alloy 2024 (either heat-treated or not heat-treated), alclad Aluminum Alloy 2024, alodined Aluminum Alloy 2024, and anodized Aluminum Alloy 2024. The provisional values for alclad Aluminum Alloy 2024 are from theoretical calculations using the relation discussed in subsection 4.20, based on Eq. (2.5-5), to calculate normal spectral reflectance. The data given for this alodined Aluminum Alloy 2024 is for a chromate conversion coating applied to the specimen. So, likewise, the provisional curves for the alodined specimen are for this same chromate coating. For the anodized specimen, the surface is actually a layer of aluminum oxide. Therefore, the provisional curves are for this same type of specimen.

No data was located for the following subproperties of aluminum alloy 2024: HSE(T), NSE(T), ASE(λ), ASE(T), HSR(λ), HSR(T), NSR(T), ASR(T), HSA(λ), HSA(T), ASA(λ), and ASA(T).

Data in the data tables also includes data for grooved surfaces of Aluminum Alloy 2024 for the subproperties ASR(λ) and NSR(λ). These data points are not plotted but are included in the report.

Aluminum Alloy 2024 is perhaps the best known and most widely used aircraft alloy.

a. Normal Spectral Emittance (Wavelength Dependence)

There are seven sets of experimental data available for the wavelength dependence (0.12-27.0 μm) of the normal spectral emittance of Aluminum Alloy 2024 under various

surface conditions. These are listed in Table 1-3 and shown in Figures 1-2 and 1-5.

(1) Highly Polished Aluminum Alloy 2024

The recommended values listed in Table 1-1 and shown in Figure 1-1 for highly polished Aluminum Alloy 2024 were generated from the absorptance data reported by Schriempf and Wieting [A00003] and are believed to be accurate to $\pm 10\%$ over the entire wavelength range at 293 K.

(2) Highly Polished Alclad Aluminum Alloy 2024

The recommended values listed in Table 1-1 and shown in Figure 1-3 for highly polished alclad Aluminum Alloy 2024 were generated with the relation discussed in subsection 4.20, based on Eq. (2.5-5), and are believed accurate to $\pm 10\%$ at the reported wavelength range at 293 K. These values are consistent with the normal spectral reflectance data of Grimm and Fannin [A00001] on a similar material. Provisional values at 450, 600, and 750 K tabulated in Table 1-1 and shown in Figure 1-3 were calculated with the relation discussed in subsection 4.20, based on Eq. (2.5-5), and are believed accurate to $\pm 20\%$ over the entire wavelength region for a highly polished (ideal) surface.

(3) Oxidized Aluminum Alloy 2024

Provisional values at 823 K listed in Table 1-1 and shown in Figure 1-4 were generated from the data of Blau, et al. [T16606] and are believed accurate to $\pm 20\%$ over the entire wavelength range.

TABLE 1-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| HIGHLY POLISHED ALCLAD T = 293 | | | HIGHLY POLISHED ALCLAD T = 450 | | | HIGHLY POLISHED ALCLAD T = 600 | | | HIGHLY FOLISHED ALCLAD T = 750 | | | OXIDIZED ALLOY T = 823 | | |
|--------------------------------------|------------|-----------|--------------------------------------|-----------|------------|--------------------------------------|------------|-----------|--------------------------------------|-----------|------------|------------------------------|------------|--|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | |
| 2.20 | 0.0980 | 2.5 | 0.067 | 2.5 | 0.071A† | 2.5 | 0.073A† | 2.5 | 0.075A† | 2.0 | 0.426A† | | | |
| 2.60 | 0.0760 | 2.8 | 0.057 | 2.8 | 0.063A | 2.8 | 0.067A | 2.8 | 0.069A | 2.2 | 0.418A | | | |
| 3.00 | 0.0697 | 3.0 | 0.052 | 3.0 | 0.059A | 3.0 | 0.063A | 3.0 | 0.066A | 2.5 | 0.410A | | | |
| 3.50 | 0.0575 | 3.5 | 0.044 | 3.5 | 0.052A | 3.5 | 0.056A | 3.5 | 0.060A | 2.0 | 0.403A | | | |
| 3.80 | 0.0524 | 3.8 | 0.041 | 3.8 | 0.048A | 3.8 | 0.053A | 3.8 | 0.057A | 3.0 | 0.399A | | | |
| 4.00 | 0.0438 | 4.0 | 0.039 | 4.0 | 0.046A | 4.0 | 0.051A | 4.0 | 0.055A | 3.2 | 0.394A | | | |
| 4.50 | 0.0440 | 4.5 | 0.035 | 4.5 | 0.043A | 4.5 | 0.047A | 4.5 | 0.051A | 3.5 | 0.386A | | | |
| 5.00 | 0.0402 | 5.0 | 0.033 | 5.0 | 0.040A | 5.0 | 0.044A | 5.0 | 0.048A | 3.0 | 0.381A | | | |
| 5.50 | 0.0375 | 5.5 | 0.031 | 5.5 | 0.037A | 5.5 | 0.042A | 5.5 | 0.046A | 4.0 | 0.376A | | | |
| 6.00 | 0.0355 | 6.0 | 0.029 | 6.0 | 0.035A | 6.0 | 0.040A | 6.0 | 0.043A | 4.2 | 0.374A | | | |
| 6.50 | 0.0338 | 6.5 | 0.027 | 6.5 | 0.034A | 6.5 | 0.038A | 6.5 | 0.042A | 4.5 | 0.366A | | | |
| 7.00 | 0.0323 | 7.0 | 0.026 | 7.0 | 0.032A | 7.0 | 0.037A | 7.0 | 0.040A | 4.0 | 0.362A | | | |
| 7.50 | 0.0310 | 7.5 | 0.025 | 7.5 | 0.031A | 7.5 | 0.035A | 7.5 | 0.039A | 5.0 | 0.360A | | | |
| 8.00 | 0.0298 | 8.0 | 0.024 | 8.0 | 0.030A | 8.0 | 0.034A | 8.0 | 0.037A | 5.2 | 0.356A | | | |
| 8.50 | 0.0287 | 8.5 | 0.023 | 8.5 | 0.029A | 8.5 | 0.033A | 8.5 | 0.036A | 5.5 | 0.351A | | | |
| 9.00 | 0.0278 | 9.0 | 0.023 | 9.0 | 0.028A | 9.0 | 0.032A | 9.0 | 0.035A | 5.0 | 0.346A | | | |
| 9.50 | 0.0272 | 9.5 | 0.022 | 9.5 | 0.027A | 9.5 | 0.031A | 9.5 | 0.034A | 6.0 | 0.342A | | | |
| 10.00 | 0.0270 | 10.0 | 0.021 | 10.0 | 0.026A | 10.0 | 0.030A | 10.0 | 0.033A | 6.2 | 0.340A | | | |
| 10.60 | 0.0262 | 10.5 | 0.021 | 10.5 | 0.026A | 10.5 | 0.029A | 10.5 | 0.032A | 6.5 | 0.336A | | | |
| 11.00 | 0.0258 | 11.0 | 0.020 | 11.0 | 0.025A | 11.0 | 0.029A | 11.0 | 0.032A | 7.0 | 0.330A | | | |
| 11.50 | 0.0254 | 11.5 | 0.020 | 11.5 | 0.025A | 11.5 | 0.028A | 11.5 | 0.031A | 7.2 | 0.328A | | | |
| 12.00 | 0.0250 | 12.0 | 0.019 | 12.0 | 0.024A | 12.0 | 0.028A | 12.0 | 0.030A | 7.5 | 0.323A | | | |
| 12.50 | 0.0246 | 12.5 | 0.019 | 12.5 | 0.024A | 12.5 | 0.027A | 12.5 | 0.030A | 8.0 | 0.317A | | | |
| 13.00 | 0.0242 | 13.0 | 0.019 | 13.0 | 0.023A | 13.0 | 0.026A | 13.0 | 0.029A | 8.5 | 0.310A | | | |
| 13.50 | 0.0239 | 13.5 | 0.018 | 13.5 | 0.023A | 13.5 | 0.026A | 13.5 | 0.029A | 9.0 | 0.303A | | | |
| 14.00 | 0.0235 | 14.0 | 0.018 | 14.0 | 0.022A | 14.0 | 0.025A | 14.0 | 0.028A | 9.5 | 0.296A | | | |
| 14.50 | 0.0232 | 14.5 | 0.017 | 14.5 | 0.022A | 14.5 | 0.025A | 14.5 | 0.028A | 10.0 | 0.290A | | | |
| 15.00 | 0.0228 | 15.0 | 0.017 | 15.0 | 0.021A | 15.0 | 0.025A | 15.0 | 0.027A | 10.5 | 0.284A | | | |
| | | | | | | | | | | 11.0 | 0.277A | | | |
| | | | | | | | | | | 11.5 | 0.271A | | | |
| | | | | | | | | | | 12.0 | 0.266A | | | |
| | | | | | | | | | | 12.5 | 0.261A | | | |
| | | | | | | | | | | 13.0 | 0.256A | | | |
| | | | | | | | | | | 13.5 | 0.252A | | | |
| | | | | | | | | | | 14.0 | 0.248A | | | |

†VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

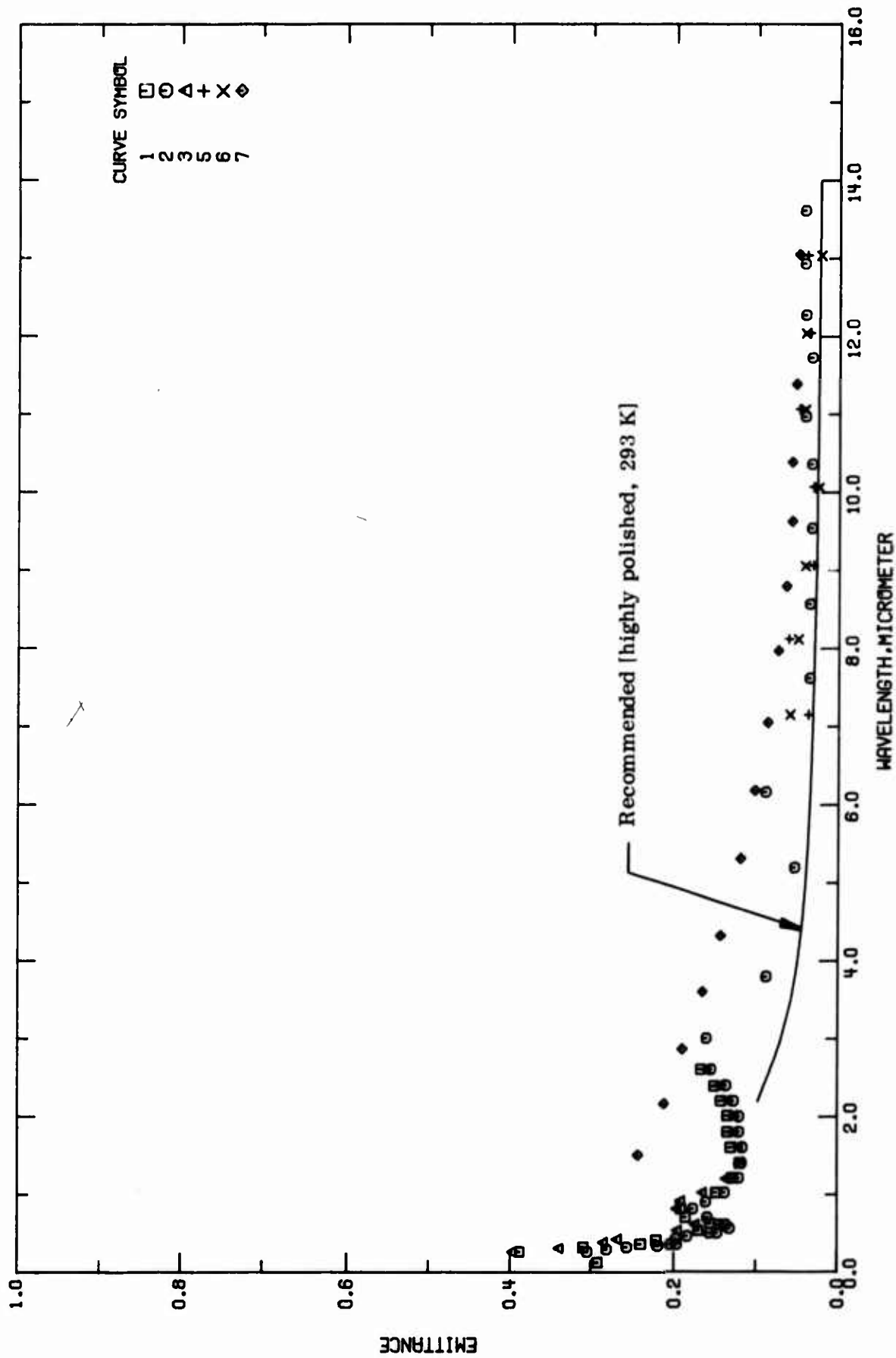


FIGURE 1-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

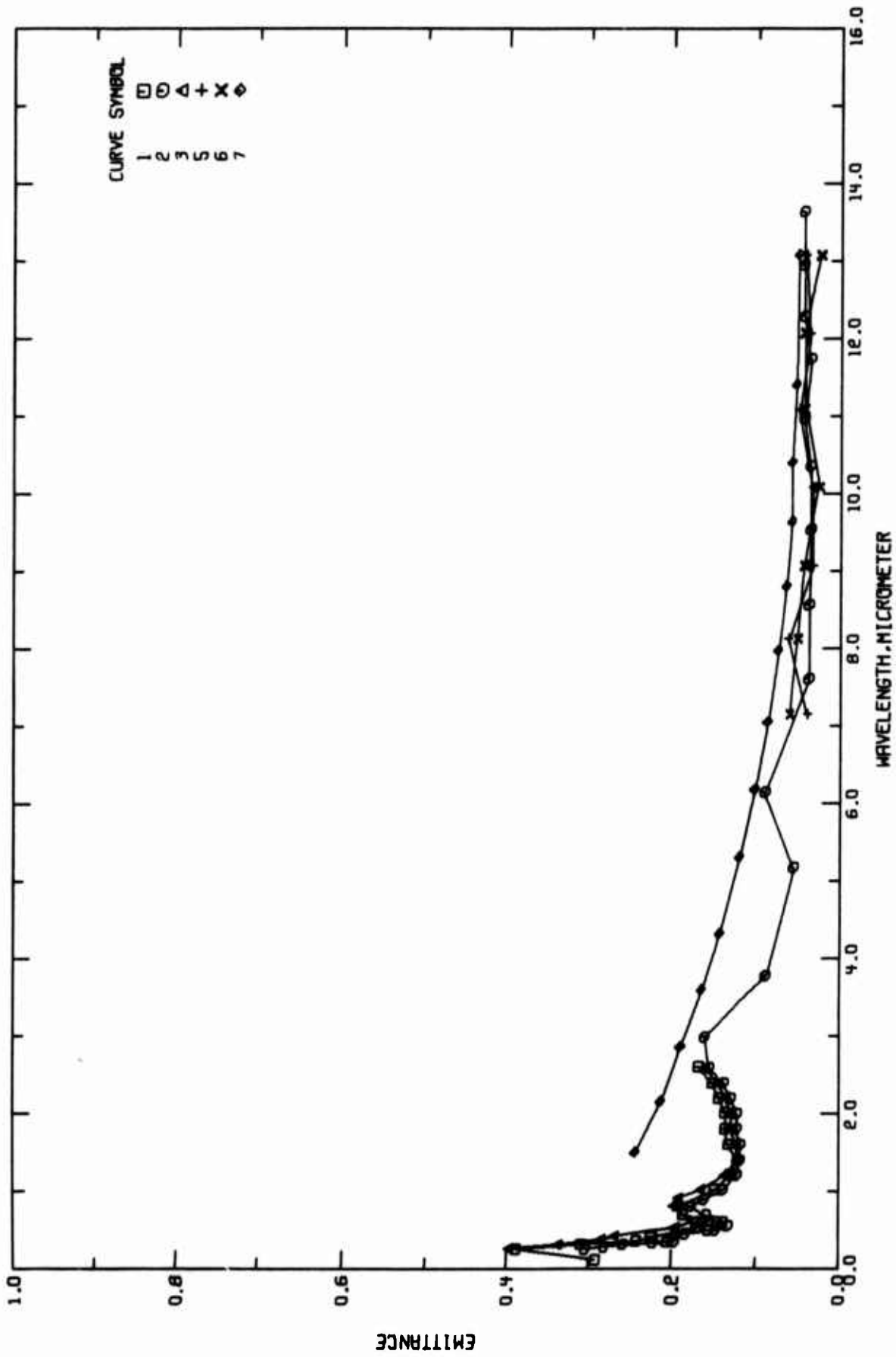


FIGURE 1-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

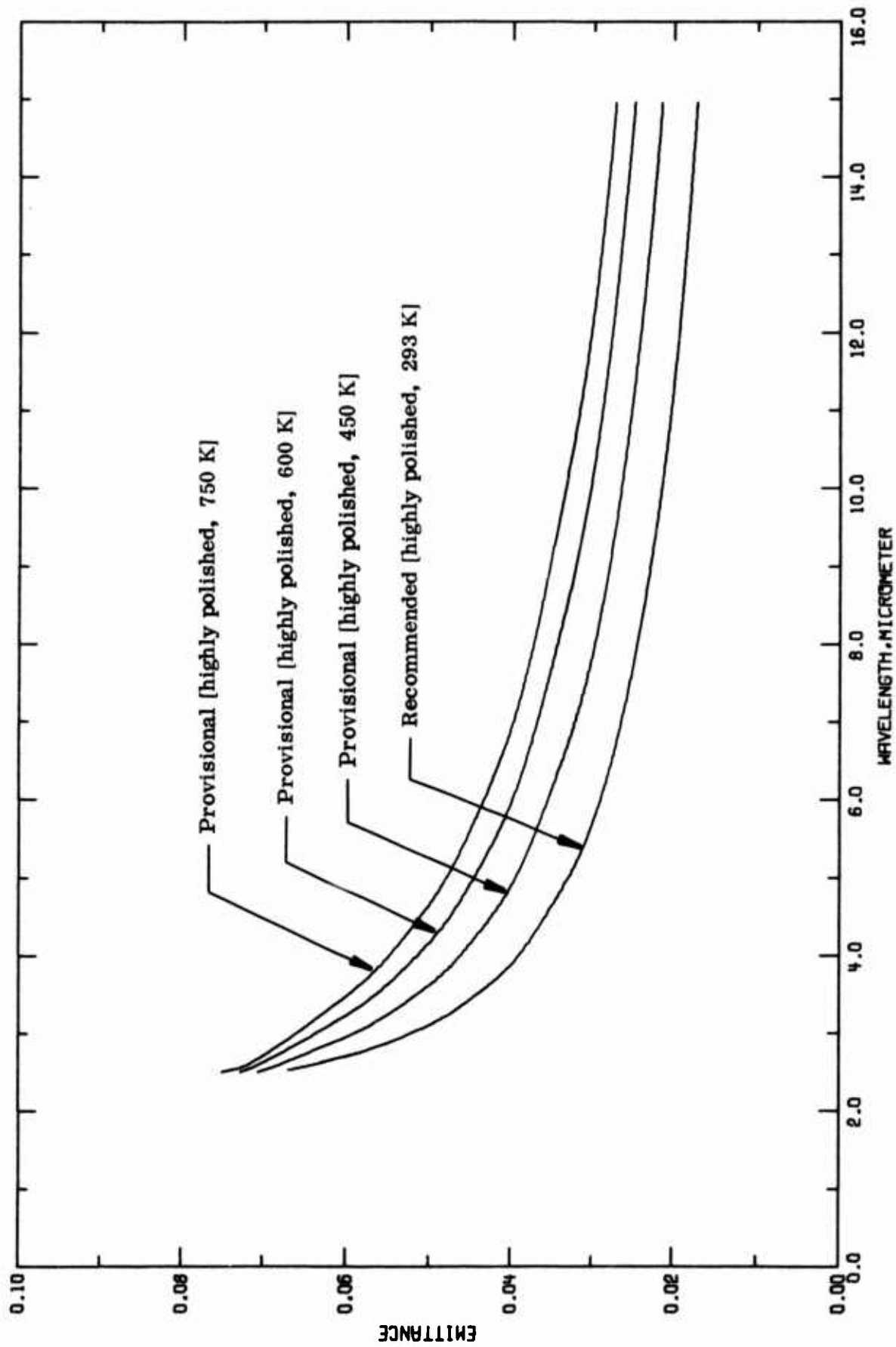


FIGURE 1-3. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

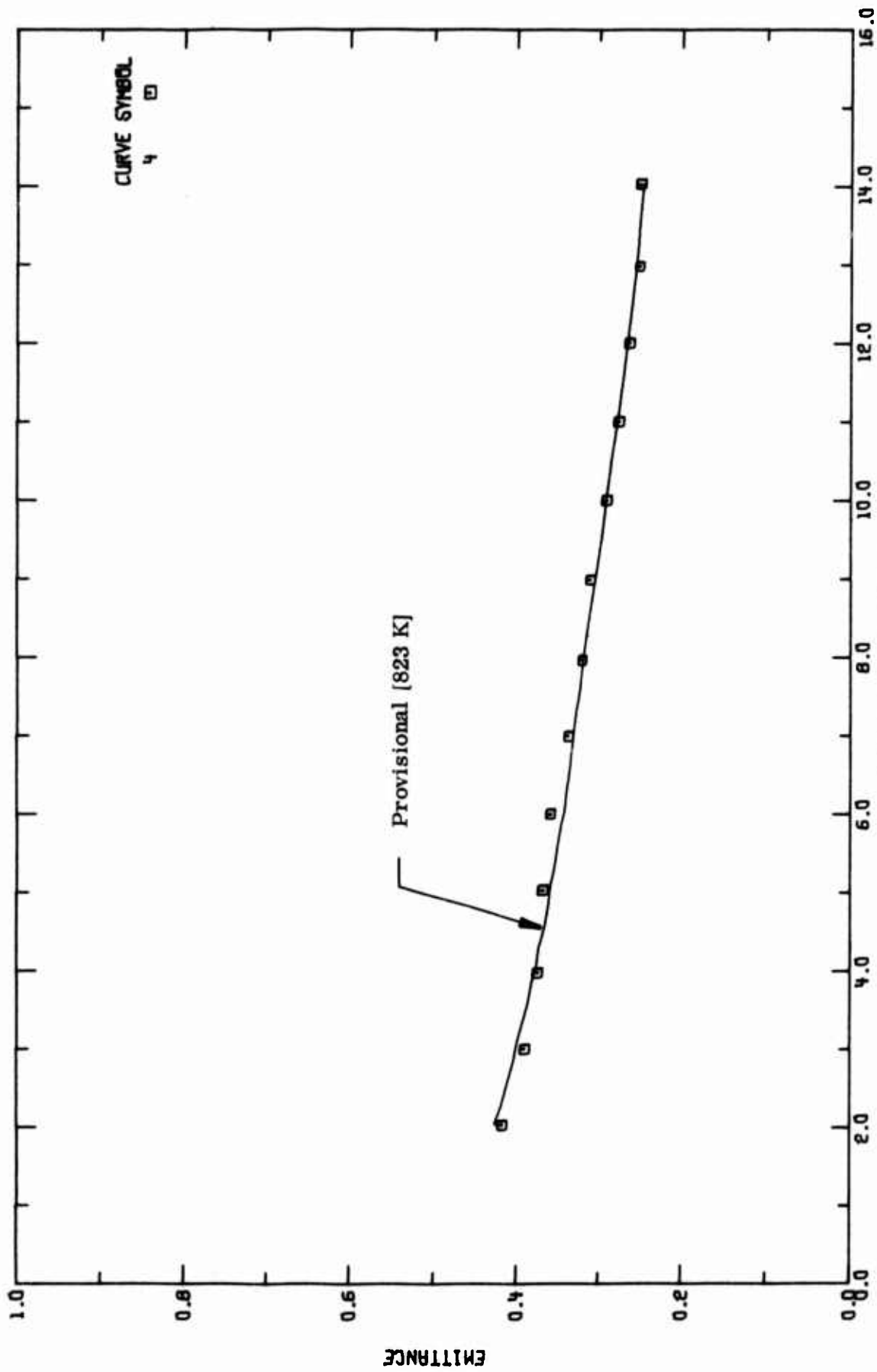


FIGURE 1-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF OXIDIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

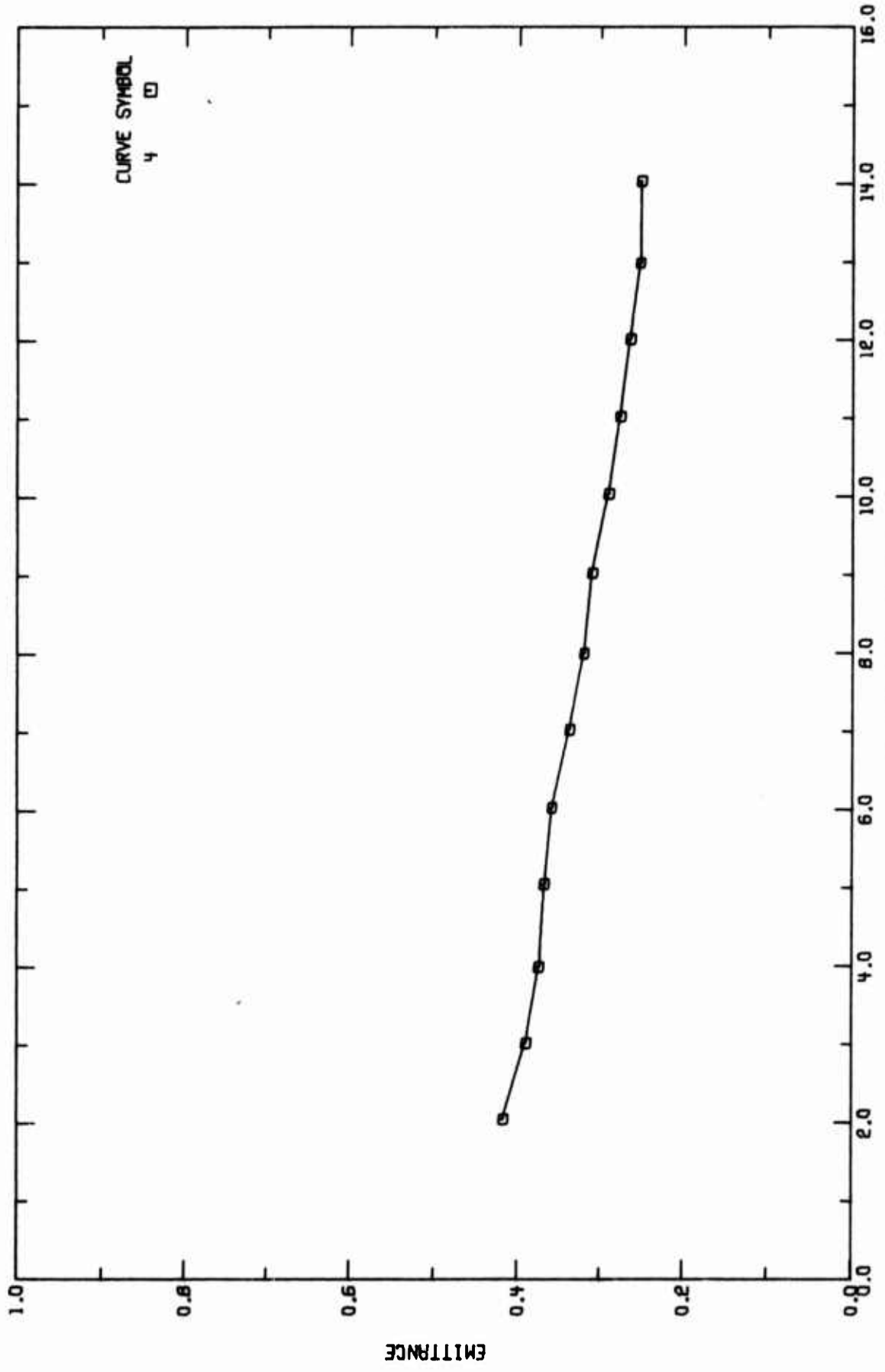


FIGURE 1-5. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

TABLE 1-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T29202 | Research Projects Div., G.C. Marshall Space Flight Center | 1963 | 0.12-2.6 | 323 | Specimen 1 | Front surface of sample was initially roughened with a variety of emery papers, sample then brought to a fine polish with grinding wheel and alumina powder; measurements made at equivalent time periods in temperature-humidity controlled room; measurements in 0.25-2.5 μm wavelength region were made with a Beckman 24500 reflectance unit and a Beckman DK-2 monochromator in conjunction with an integrating sphere; reported values of normal spectral emittance calculated from formula $\epsilon = 1 - r$; data extracted from figure. |
| 2 T29202 | Research Projects Div., G.C. Marshall Space Flight Center | 1963 | 0.26-27.0 | 323 | Specimen 3 | Different sample, the above specimen and conditions; measurements in infrared region of spectrum made with an energy detector. |
| 3 T29202 | Research Projects Div., G.C. Marshall Space Flight Center | 1963 | 0.26-2.6 | 323 | Specimen 4 | Different sample, the above specimen and conditions. |
| 4 T16606 | Blau, H.H., Chaffee, E., Marsh, J.D., Martin, W.J., and Jasperse, J.R. | 1960 | 2.0-14.0 | 823 | | Unpolished, oxidized in air for 2 hr; specimen heated by silicon carbide furnace, emittance measured by Perkin-Elmer Model 12C energy detector; data extracted from figure; $\theta \approx 0^\circ$, reported error $\pm 4\%$. |
| 5 T20470 | Weber, D. | 1959 | 7.15-15.06 | 383 | 24ST Aluminum (ANA13-352) | Specimen reported as flat and smooth; Perkin-Elmer Model 112 infrared spectrometer used for measurements; normal emissivity assumed; data extracted from figure; reported error $\pm 50\%$. |
| 6 T20470 | Weber, D. | 1959 | 7.15-15.06 | 303 | 24ST Aluminum (ANA13-362) | The above specimen and conditions. |
| 7 T21553 | Berry, J., Lee, T., and Shaw, C. | 1959 | 1.5-21.0 | 301 | | Specimen buffed on wheel with jewelers rouge for 17 min; data extracted from smooth curve; normal emissivity assumed. |

TABLE 1-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

| [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ] | | |
|--|------------|--|
| CURVE 1 | | |
| T = 323. | | |
| λ | ϵ | |
| 0.12 | 0.291 | |
| 0.26 | 0.387 | |
| 0.32 | 0.309 | |
| 0.36 | 0.240 | |
| 0.41 | 0.222 | |
| 0.53 | 0.170 | |
| 0.62 | 0.155 | |
| 0.70 | 0.186 | |
| 0.81 | 0.192 | |
| 1.02 | 0.148 | |
| 1.21 | 0.129 | |
| 1.40 | 0.120 | |
| 1.60 | 0.131 | |
| 1.80 | 0.135 | |
| 2.01 | 0.135 | |
| 2.20 | 0.143 | |
| 2.39 | 0.151 | |
| 2.60 | 0.168 | |
| CURVE 2 (CONT.) | | |
| λ | ϵ | |
| 1.21 | 0.121 | |
| 1.40 | 0.118 | |
| 1.60 | 0.117 | |
| 1.80 | 0.121 | |
| 2.00 | 0.121 | |
| 2.20 | 0.128 | |
| 2.40 | 0.137 | |
| 2.60 | 0.155 | |
| 3.00 | 0.161 | |
| 3.79 | 0.089 | |
| 5.19 | 0.054 | |
| 6.16 | 0.090 | |
| 7.62 | 0.036 | |
| 8.57 | 0.036 | |
| 9.54 | 0.034 | |
| 10.36 | 0.034 | |
| 10.97 | 0.042 | |
| 11.73 | 0.034 | |
| 12.28 | 0.042 | |
| 12.94 | 0.043 | |
| 13.62 | 0.043 | |
| 14.04 | 0.057 | |
| 14.08 | 0.052 | |
| 14.12 | 0.042 | |
| 14.65 | 0.060 | |
| 16.27 | 0.051 | |
| 16.27 | 0.044 | |
| 18.27 | 0.039 | |
| 20.10 | 0.038 | |
| 21.70 | 0.047 | |
| 24.32 | 0.064 | |
| 26.98 | 0.060 | |
| CURVE 3 (CONT.) | | |
| λ | ϵ | |
| 0.53 | 0.197 | |
| 0.61 | 0.175 | |
| 0.81 | 0.198 | |
| 0.91 | 0.193 | |
| 1.02 | 0.166 | |
| 1.20 | 0.137 | |
| 1.39 | 0.121 | |
| 1.61 | 0.123 | |
| 1.80 | 0.129 | |
| 2.01 | 0.129 | |
| 2.21 | 0.136 | |
| 2.40 | 0.145 | |
| 2.60 | 0.161 | |
| CURVE 4 | | |
| T = 823. | | |
| λ | ϵ | |
| 2.03 | 0.417 | |
| 3.00 | 0.390 | |
| 3.97 | 0.375 | |
| 5.02 | 0.369 | |
| 5.99 | 0.360 | |
| 6.98 | 0.338 | |
| 7.95 | 0.320 | |
| 8.97 | 0.310 | |
| 9.98 | 0.291 | |
| 10.98 | 0.277 | |
| 11.98 | 0.265 | |
| 12.95 | 0.253 | |
| 14.00 | 0.252 | |
| CURVE 5 | | |
| T = 383. | | |
| λ | ϵ | |
| 7.15 | 0.030 | |
| 8.12 | 0.062 | |
| 9.06 | 0.032 | |
| 10.07 | 0.032 | |
| 11.07 | 0.049 | |
| 12.05 | 0.036 | |
| CURVE 6 | | |
| T = 303. | | |
| λ | ϵ | |
| 7.15 | 0.060 | |
| 8.12 | 0.050 | |
| 9.06 | 0.042 | |
| 10.07 | 0.025 | |
| 11.07 | 0.042 | |
| 12.05 | 0.042 | |
| 13.05 | 0.023 | |
| 14.06 | 0.038 | |
| 15.06 | 0.047 | |
| CURVE 7 | | |
| T = 301. | | |
| λ | ϵ | |
| 1.50 | 0.243 | |
| 2.16 | 0.213 | |
| 2.86 | 0.191 | |
| 3.68 | 0.166 | |
| 4.32 | 0.144 | |
| 5.31 | 0.120 | |
| 6.18 | 0.103 | |
| 7.05 | 0.088 | |
| 7.97 | 0.075 | |
| 8.80 | 0.065 | |
| 9.63 | 0.058 | |
| 10.39 | 0.058 | |
| 11.39 | 0.053 | |
| 13.06 | 0.050 | |
| 14.31 | 0.050 | |
| 16.05 | 0.050 | |
| 18.39 | 0.050 | |
| 21.00 | 0.050 | |

b. Normal Spectral Emittance (Temperature Dependence)

There are no experimental data located in the literature. The provisional values tabulated in Table 1-4 and shown in Figure 1-6 were calculated with the relation discussed in subsection 4.20, based on Eq. (2.5-5), for highly polished alclad Aluminum Alloy 2024 for wavelengths of 2.8, 3.8, 5.0, and 10.6 μm . These values are believed accurate to $\pm 20\%$ over the entire wavelength range.

TABLE 1-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|------------------|------------|-------|------------|-------|------------|-------|------------|
| HIGHLY POLISHED | | | | | | | |
| ALCLAD | | | | | | | |
| $\lambda = 2.8$ | | | | | | | |
| 250.0 | 0.054 | 250.0 | 0.038 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.057 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.060 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.062 | 400.0 | 0.046 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.063 | 450.0 | 0.043 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.066 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.067 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.068 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 700.0 | 0.068 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| $\lambda = 3.0$ | | | | | | | |
| HIGHLY POLISHED | | | | | | | |
| ALCLAD | | | | | | | |
| $\lambda = 5.0$ | | | | | | | |
| 250.0 | 0.038 | 250.0 | 0.030 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.041 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.041 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.044 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.046 | 400.0 | 0.046 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.043 | 450.0 | 0.043 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.050 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.052 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.053 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.055 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 700.0 | 0.056 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.057 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| $\lambda = 10.6$ | | | | | | | |
| HIGHLY POLISHED | | | | | | | |
| ALCLAD | | | | | | | |
| 250.0 | 0.019 | 250.0 | 0.019 | 250.0 | 0.019 | 250.0 | 0.019 |
| 293.0 | 0.021 | 293.0 | 0.021 | 293.0 | 0.021 | 293.0 | 0.021 |
| 300.0 | 0.021 | 300.0 | 0.021 | 300.0 | 0.021 | 300.0 | 0.021 |
| 350.0 | 0.023 | 350.0 | 0.023 | 350.0 | 0.023 | 350.0 | 0.023 |
| 400.0 | 0.024 | 400.0 | 0.024 | 400.0 | 0.024 | 400.0 | 0.024 |
| 450.0 | 0.026 | 450.0 | 0.026 | 450.0 | 0.026 | 450.0 | 0.026 |
| 500.0 | 0.027 | 500.0 | 0.027 | 500.0 | 0.027 | 500.0 | 0.027 |
| 550.0 | 0.028 | 550.0 | 0.028 | 550.0 | 0.028 | 550.0 | 0.028 |
| 600.0 | 0.029 | 600.0 | 0.029 | 600.0 | 0.029 | 600.0 | 0.029 |
| 650.0 | 0.030 | 650.0 | 0.030 | 650.0 | 0.030 | 650.0 | 0.030 |
| 700.0 | 0.031 | 700.0 | 0.031 | 700.0 | 0.031 | 700.0 | 0.031 |
| 750.0 | 0.032 | 750.0 | 0.032 | 750.0 | 0.032 | 750.0 | 0.032 |

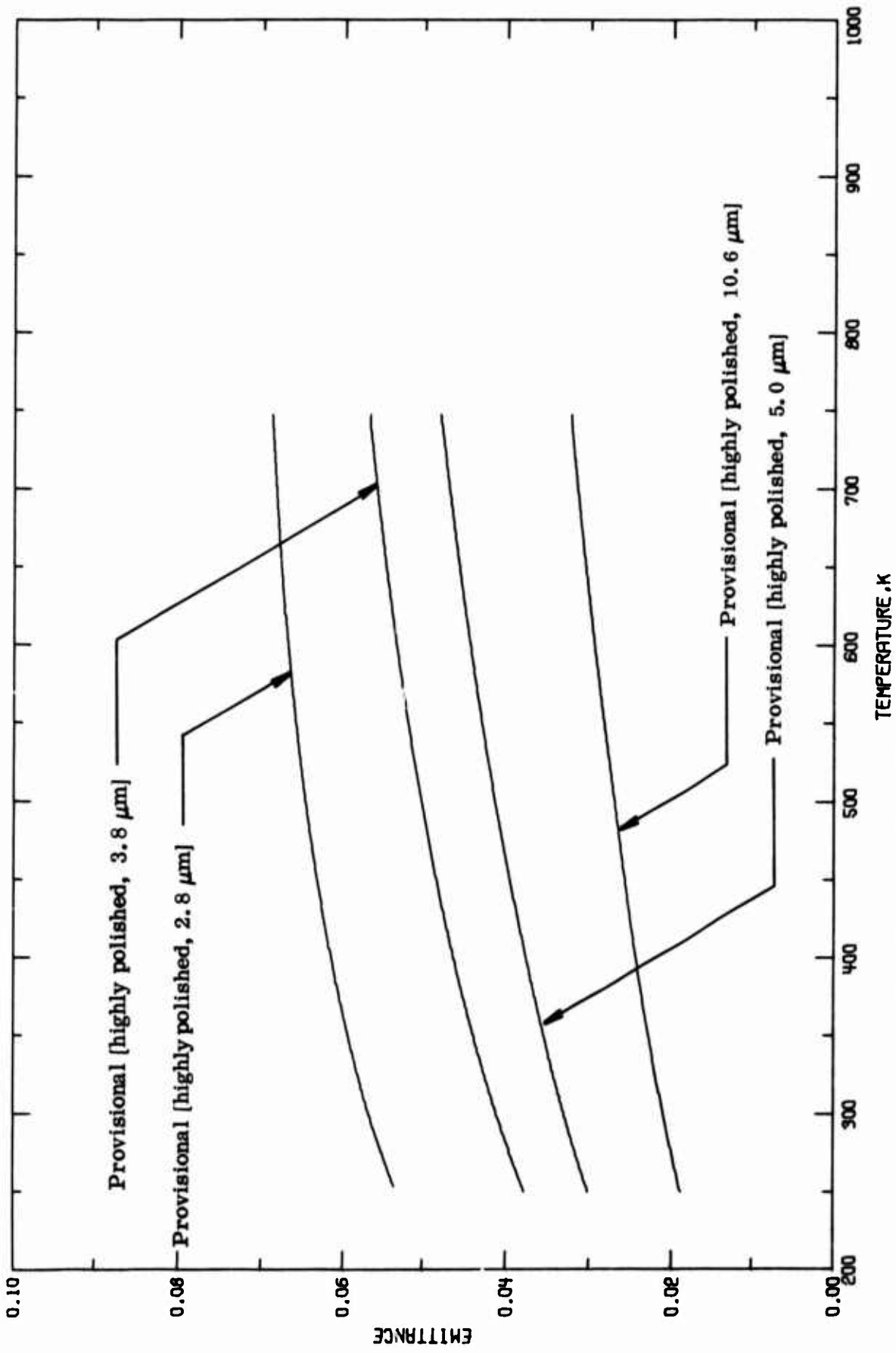


FIGURE 1-6. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALCLAD ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE).

c. Angular Spectral Emittance (Wavelength Dependence)

There are no data available for this subproperty but the provisional values listed in Table 1-5 and shown in Figures 1-7, 1-8, and 1-9 for anodized, alodined ($\theta = 15^\circ$), and alodined ($\theta = 45^\circ$) Aluminum Alloy 2024, respectively, were calculated from the angular spectral reflectance data (see Section 4.1.f). These values are believed accurate to $\pm 15\%$ over the entire wavelength range for the anodized and alodined Aluminum Alloy 2024 ($\theta = 15^\circ$) materials at 293 K. The provisional values for alodined Aluminum Alloy 2024 ($\theta = 45^\circ$) are accurate to $\pm 20\%$.

There are several methods which can be used to produce an anodized surface. The angular spectral emittance can vary widely with the anodizing process, i. e., porous or hard, secondary treatments such as sealing or dyeing of the surface layer, and thickness. Most of the authors do not clearly specify the nature of the anodizing process or surface conditions. So the provisional values reported in Table 1-5 are applicable only to the sulfuric acid anodized surface. Similarly, there are several alodining processes. Depending on this process the angular spectral emittance may vary. The provisional values apply only to the chromate conversion coating used in the references.

TABLE 1-5. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| SULFURIC ACID ANODIZED, $\theta = 15^\circ$ T = 293 | | SULFURIC ACID ANODIZED, $\theta = 15^\circ$ T = 293 (CONT.) | | CHROMATE ALODINED, $\theta = 15^\circ$ T = 293 | | CHROMATE ALODINED, $\theta = 15^\circ$ T = 293 (CONT.) | | CHROMATE ALODINED, $\theta = 45^\circ$ T = 293 | |
|--|------------|--|------------|---|------------|---|------------|---|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 0.30 | 0.740 | 6.10 | 0.464 | 2.34 | 0.517 | 12.00 | 0.142 | 2.00 | 0.240 |
| 0.35 | 0.640 | 6.20 | 0.473 | 2.50 | 0.531 | 12.50 | 0.135 | 2.20 | 0.258 |
| 0.40 | 0.550 | 6.40 | 0.410 | 2.80 | 0.604 | 13.00 | 0.129 | 2.40 | 0.280 |
| 0.50 | 0.482 | 6.60 | 0.398 | 3.00 | 0.677 | 13.50 | 0.123 | 2.60 | 0.350 |
| 0.60 | 0.474 | 6.80 | 0.405 | 3.05 | 0.685 | 14.00 | 0.118 | 2.80 | 0.552 |
| 0.70 | 0.475 | 7.00 | 0.426 | 3.10 | 0.689 | 14.50 | 0.113 | 3.00 | 0.620 |
| 0.80 | 0.481 | 7.20 | 0.514 | 3.15 | 0.682 | 15.00 | 0.109 | 3.10 | 0.618 |
| 0.83 | 0.482 | 7.40 | 0.640 | 3.20 | 0.682 | | | 3.20 | 0.606 |
| 0.90 | 0.434 | 7.60 | 0.740 | 3.25 | 0.673 | | | 3.40 | 0.550 |
| 1.00 | 0.380 | 7.80 | 0.820 | 3.30 | 0.655 | | | 3.60 | 0.470 |
| 1.20 | 0.320 | 8.00 | 0.875 | 3.50 | 0.589 | | | 3.80 | 0.400 |
| 1.40 | 0.292 | 8.20 | 0.918 | 3.70 | 0.528 | | | 4.00 | 0.366 |
| 1.60 | 0.274 | 8.40 | 0.942 | 3.80 | 0.502 | | | 4.20 | 0.338 |
| 1.80 | 0.268 | 8.60 | 0.949 | 4.00 | 0.480 | | | 4.40 | 0.320 |
| 2.00 | 0.279 | 8.80 | 0.947 | 4.20 | 0.458 | | | 4.50 | 0.316 |
| 2.20 | 0.301 | 9.00 | 0.941 | 4.50 | 0.431 | | | 4.60 | 0.320 |
| 2.40 | 0.341 | 9.20 | 0.920 | 4.56 | 0.426 | | | 4.70 | 0.400 |
| 2.60 | 0.422 | 9.40 | 0.893 | 4.61 | 0.427 | | | 4.72 | 0.412 |
| 2.80 | 0.779 | 9.60 | 0.864 | 4.70 | 0.461 | | | 4.76 | 0.414 |
| 2.85 | 0.807 | 9.80 | 0.855 | 4.74 | 0.472 | | | 4.80 | 0.412 |
| 2.90 | 0.810 | 10.00 | 0.864 | 4.77 | 0.481 | | | 4.90 | 0.320 |
| 2.95 | 0.808 | 10.20 | 0.900 | 4.81 | 0.472 | | | 5.00 | 0.290 |
| 3.00 | 0.797 | 10.40 | 0.935 | 4.87 | 0.440 | | | 5.20 | 0.280 |
| 3.20 | 0.677 | 10.60 | 0.960 | 4.93 | 0.405 | | | 5.40 | 0.270 |
| 3.40 | 0.592 | 10.80 | 0.972 | 4.95 | 0.397 | | | 5.60 | 0.260 |
| 3.60 | 0.526 | 11.00 | 0.975 | 5.00 | 0.394 | | | 5.80 | 0.252 |
| 3.80 | 0.484 | 11.20 | 0.963 | 5.50 | 0.362 | | | 6.00 | 0.246 |
| 4.00 | 0.454 | 11.40 | 0.955 | 6.00 | 0.334 | | | 7.00 | 0.220 |
| 4.20 | 0.428 | 11.60 | 0.949 | 6.50 | 0.308 | | | 8.00 | 0.200 |
| 4.40 | 0.410 | 11.80 | 0.943 | 7.00 | 0.285 | | | 9.00 | 0.181 |
| 4.60 | 0.396 | 12.00 | 0.938 | 7.50 | 0.263 | | | 10.00 | 0.164 |
| 4.80 | 0.389 | 12.50 | 0.928 | 8.00 | 0.244 | | | 10.60 | 0.156 |
| 5.00 | 0.384 | 13.00 | 0.920 | 8.50 | 0.227 | | | 11.00 | 0.150 |
| 5.20 | 0.382 | 13.50 | 0.915 | 9.00 | 0.210 | | | 12.00 | 0.136 |
| 5.40 | 0.390 | 14.00 | 0.909 | 9.50 | 0.195 | | | 13.00 | 0.127 |
| 5.60 | 0.406 | 14.50 | 0.905 | 10.00 | 0.182 | | | 14.00 | 0.116 |
| 5.80 | 0.442 | 15.00 | 0.902 | 10.60 | 0.167 | | | | |
| 5.90 | 0.476 | | | 11.00 | 0.158 | | | | |
| 6.00 | 0.484 | | | 11.50 | 0.150 | | | | |

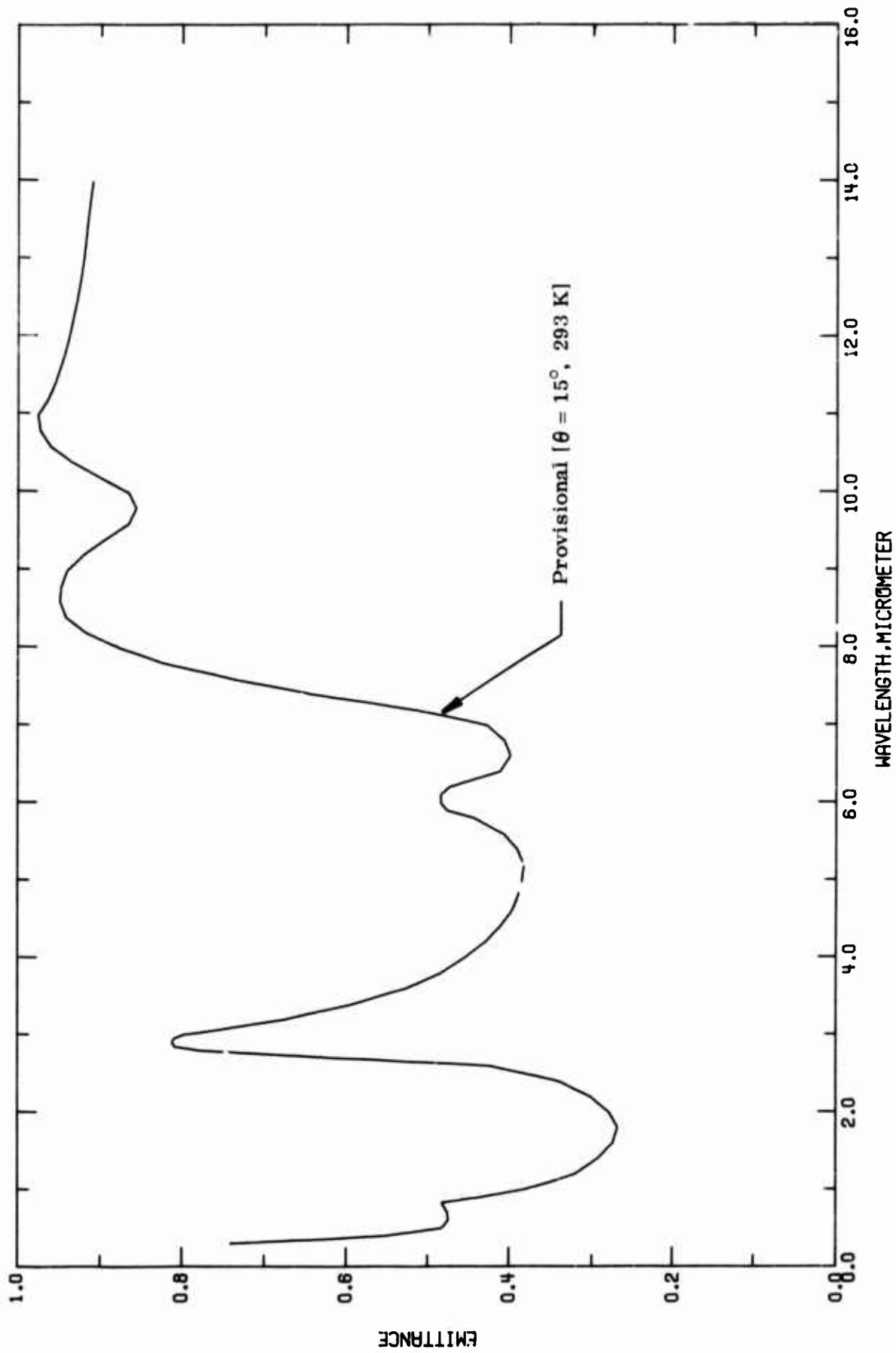


FIGURE 1-7. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

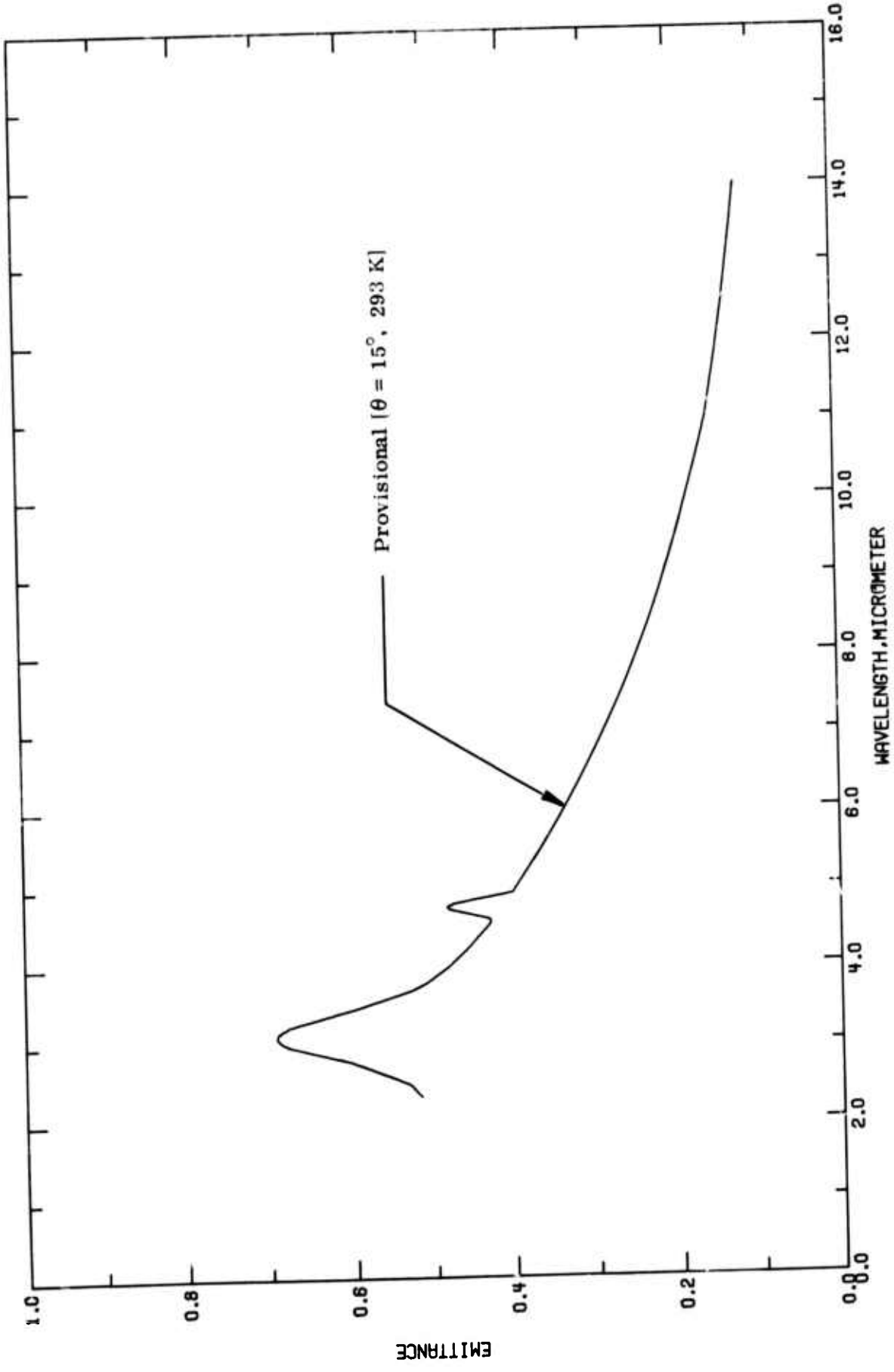


FIGURE 1-8. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

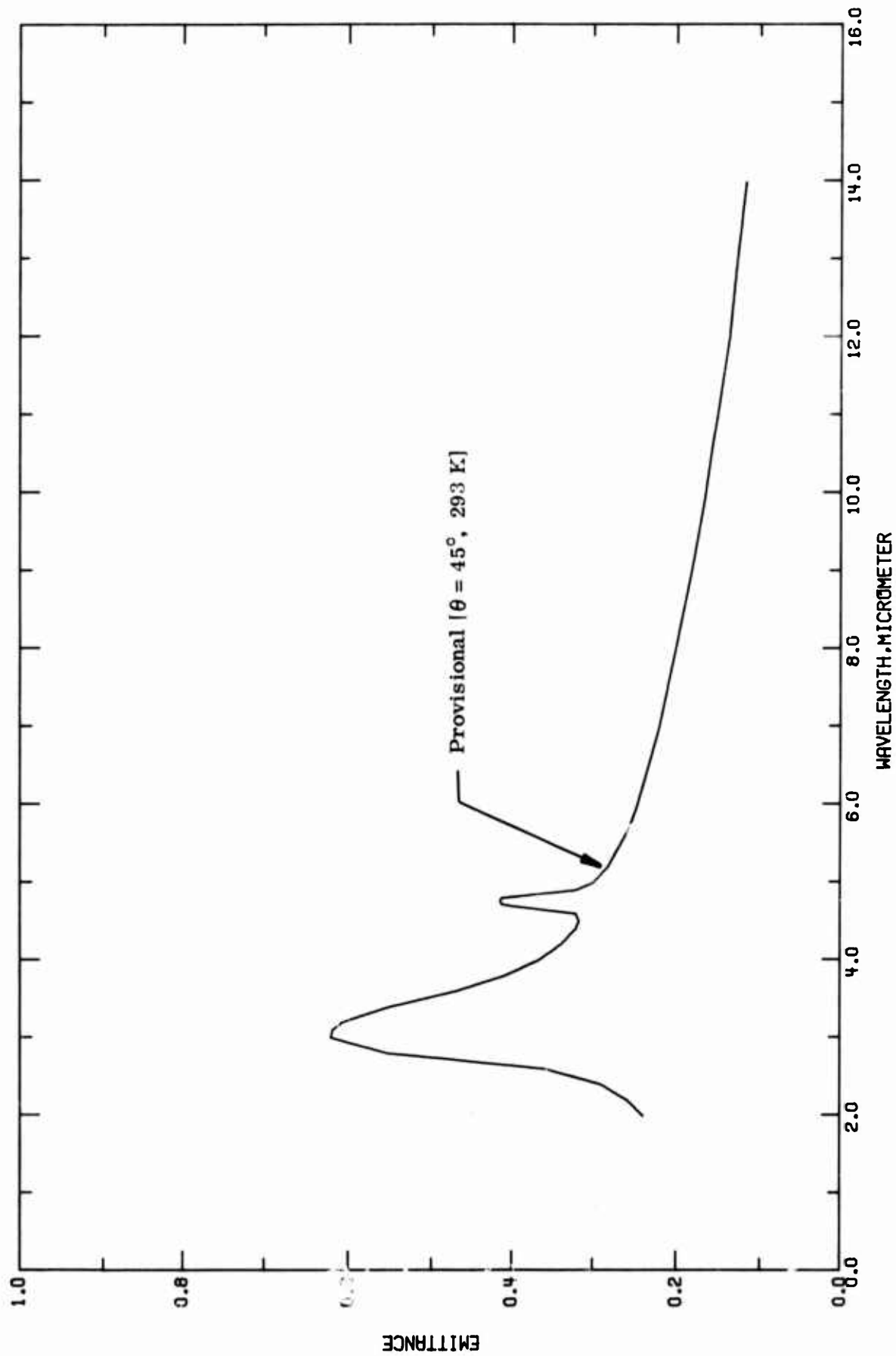


FIGURE 1-9. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

d. Normal Spectral Reflectance (Wavelength Dependence)

There are 47 sets of experimental data available for the wavelength dependence ($\lambda = 0.3\text{-}25.0\ \mu\text{m}$) of the normal spectral reflectance of Aluminum Alloy 2024 under various surface conditions. These are listed in Table 1-8 and most of them are shown in Figure 1-11. There are four sets of experimental data available for wavelength dependence ($\lambda = 2.0\text{-}15.0\ \mu\text{m}$) of the normal spectral reflectance of polished alclad Aluminum Alloy 2024 shown in Figure 1-13. Out of the total 47 data sets, 15 sets are for a polished material. Most of the measurements are for wavelengths between $0.3\text{-}3.0\ \mu\text{m}$.

(1) Highly Polished Aluminum Alloy 2024

The recommended values at 293 K listed in Table 1-6 and plotted in Figure 1-10 are primarily from the investigation of Schriempf and Wieting [A00003] and are believed to be accurate to $\pm 10\%$ over the entire wavelength range. These values are consistent with the normal spectral emittance measurements of the similar material.

(2) Alclad Aluminum Alloy 2024

There are four sets of data for the wavelength dependence ($2.0\text{-}14.7\ \mu\text{m}$) of the angular spectral reflectance of alclad Aluminum Alloy 2024. These are shown in Figure 1-13 and listed in Table 1-8. The incident angle reported is 15° . The normal spectral reflectance values for an ideal aluminum surface calculated using the relation discussed in subsection 4.20 and based on Eq. (2.5-5) agree extremely well with experimental results. These recommended values are believed accurate to $\pm 10\%$ over the entire wavelength range. The provisional values for highly polished alclad Aluminum Alloy 2024 reported at 450, 600, and 750 K shown in Figure 1-12 and listed in Table 1-6, were calculated from the relation discussed in subsection 4.20, based on Eq. (2.5-5). These values are believed accurate to $\pm 20\%$.

(3) Oxidized Aluminum Alloy 2024

The provisional values listed in Table 1-6 and shown in Figure 1-14 are for oxidized Aluminum Alloy 2024 at 823 K. These values are consistent with the provisional normal spectral emittance values (see Section 4.1a). These values are believed accurate to $\pm 20\%$.

TABLE 1-6. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| HIGHLY POLISHED T = 293 | | | HIGHLY POLISHED ALCLAD T = 293 | | | HIGHLY POLISHED ALCLAD T = 450 | | | HIGHLY POLISHED ALCLAD T = 600 | | | HIGHLY POLISHED ALCLAD T = 750 | | | OXIDIZED ALLOY T = 623 | | |
|----------------------------|--------|-----------|--------------------------------------|-----------|---------|--------------------------------------|---------|-----------|--------------------------------------|-----------|---------|--------------------------------------|---------|-----------|------------------------------|-----------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 2.20 | 0.9020 | 2.5 | 0.933 | 2.5 | 0.929A† | 2.5 | 0.927A† | 2.5 | 0.925A† | 2.5 | 0.925A† | 2.5 | 0.925A† | 2.00 | 0.574A† | | |
| 2.80 | 0.9240 | 2.8 | 0.943 | 2.8 | 0.937A | 2.8 | 0.933A | 2.8 | 0.931A | 2.8 | 0.931A | 2.8 | 0.931A | 2.20 | 0.582A | | |
| 3.00 | 0.9303 | 3.0 | 0.948 | 3.0 | 0.941A | 3.0 | 0.937A | 3.0 | 0.934A | 3.0 | 0.934A | 3.0 | 0.934A | 2.50 | 0.590A | | |
| 3.50 | 0.9425 | 3.5 | 0.956 | 3.5 | 0.948A | 3.5 | 0.944A | 3.5 | 0.940A | 3.5 | 0.940A | 3.5 | 0.940A | 2.80 | 0.597A | | |
| 3.80 | 0.9476 | 3.8 | 0.959 | 3.8 | 0.952A | 3.8 | 0.949A | 3.8 | 0.945A | 3.8 | 0.945A | 3.8 | 0.945A | 3.00 | 0.601A | | |
| 4.00 | 0.9502 | 4.0 | 0.961 | 4.0 | 0.954A | 4.0 | 0.949A | 4.0 | 0.945A | 4.0 | 0.945A | 4.0 | 0.945A | 3.20 | 0.606A | | |
| 4.50 | 0.9560 | 4.5 | 0.965 | 4.5 | 0.957A | 4.5 | 0.953A | 4.5 | 0.949A | 4.5 | 0.949A | 4.5 | 0.949A | 3.50 | 0.614A | | |
| 5.00 | 0.9538 | 5.0 | 0.967 | 5.0 | 0.960A | 5.0 | 0.956A | 5.0 | 0.952A | 5.0 | 0.952A | 5.0 | 0.952A | 3.80 | 0.619A | | |
| 5.50 | 0.9625 | 5.5 | 0.969 | 5.5 | 0.963A | 5.5 | 0.958A | 5.5 | 0.954A | 5.5 | 0.954A | 5.5 | 0.954A | 4.00 | 0.624A | | |
| 6.00 | 0.9645 | 6.0 | 0.971 | 6.0 | 0.965A | 6.0 | 0.960A | 6.0 | 0.957A | 6.0 | 0.957A | 6.0 | 0.957A | 4.20 | 0.626A | | |
| 6.50 | 0.9662 | 6.5 | 0.973 | 6.5 | 0.966A | 6.5 | 0.962A | 6.5 | 0.958A | 6.5 | 0.958A | 6.5 | 0.958A | 4.50 | 0.634A | | |
| 7.00 | 0.9677 | 7.0 | 0.974 | 7.0 | 0.968A | 7.0 | 0.963A | 7.0 | 0.960A | 7.0 | 0.960A | 7.0 | 0.960A | 4.80 | 0.638A | | |
| 7.50 | 0.9690 | 7.5 | 0.975 | 7.5 | 0.969A | 7.5 | 0.965A | 7.5 | 0.961A | 7.5 | 0.961A | 7.5 | 0.961A | 5.00 | 0.640A | | |
| 8.00 | 0.9702 | 8.0 | 0.976 | 8.0 | 0.970A | 8.0 | 0.966A | 8.0 | 0.963A | 8.0 | 0.963A | 8.0 | 0.963A | 5.20 | 0.644A | | |
| 8.50 | 0.9713 | 8.5 | 0.977 | 8.5 | 0.971A | 8.5 | 0.967A | 8.5 | 0.964A | 8.5 | 0.964A | 8.5 | 0.964A | 5.50 | 0.649A | | |
| 9.00 | 0.9722 | 9.0 | 0.977 | 9.0 | 0.972A | 9.0 | 0.968A | 9.0 | 0.965A | 9.0 | 0.965A | 9.0 | 0.965A | 5.80 | 0.654A | | |
| 9.50 | 0.9728 | 9.5 | 0.978 | 9.5 | 0.973A | 9.5 | 0.969A | 9.5 | 0.966A | 9.5 | 0.966A | 9.5 | 0.966A | 6.00 | 0.658A | | |
| 10.00 | 0.9730 | 10.0 | 0.979 | 10.0 | 0.974A | 10.0 | 0.970A | 10.0 | 0.967A | 10.0 | 0.967A | 10.0 | 0.967A | 6.20 | 0.660A | | |
| 10.60 | 0.9738 | 10.5 | 0.979 | 10.5 | 0.974A | 10.5 | 0.971A | 10.5 | 0.968A | 10.5 | 0.968A | 10.5 | 0.968A | 6.50 | 0.664A | | |
| 11.00 | 0.9742 | 11.0 | 0.980 | 11.0 | 0.975A | 11.0 | 0.971A | 11.0 | 0.968A | 11.0 | 0.968A | 11.0 | 0.968A | 7.00 | 0.670A | | |
| 11.50 | 0.9746 | 11.5 | 0.980 | 11.5 | 0.975A | 11.5 | 0.972A | 11.5 | 0.969A | 11.5 | 0.969A | 11.5 | 0.969A | 7.20 | 0.672A | | |
| 12.00 | 0.9750 | 12.0 | 0.981 | 12.0 | 0.976A | 12.0 | 0.972A | 12.0 | 0.970A | 12.0 | 0.970A | 12.0 | 0.970A | 7.50 | 0.677A | | |
| 12.50 | 0.9754 | 12.5 | 0.981 | 12.5 | 0.976A | 12.5 | 0.973A | 12.5 | 0.971A | 12.5 | 0.971A | 12.5 | 0.971A | 8.00 | 0.683A | | |
| 13.00 | 0.9758 | 13.0 | 0.981 | 13.0 | 0.977A | 13.0 | 0.974A | 13.0 | 0.971A | 13.0 | 0.971A | 13.0 | 0.971A | 8.50 | 0.690A | | |
| 13.50 | 0.9761 | 13.5 | 0.982 | 13.5 | 0.977A | 13.5 | 0.974A | 13.5 | 0.971A | 13.5 | 0.971A | 13.5 | 0.971A | 9.00 | 0.697A | | |
| 14.00 | 0.9765 | 14.0 | 0.982 | 14.0 | 0.978A | 14.0 | 0.975A | 14.0 | 0.972A | 14.0 | 0.972A | 14.0 | 0.972A | 9.50 | 0.704A | | |
| 14.50 | 0.9768 | 14.5 | 0.983 | 14.5 | 0.978A | 14.5 | 0.975A | 14.5 | 0.972A | 14.5 | 0.972A | 14.5 | 0.972A | 10.00 | 0.710A | | |
| 15.00 | 0.9772 | 15.0 | 0.983 | 15.0 | 0.979A | 15.0 | 0.975A | 15.0 | 0.972A | 15.0 | 0.972A | 15.0 | 0.972A | 10.50 | 0.716A | | |
| | | | | | | | | | | | | | | 11.00 | 0.723A | | |
| | | | | | | | | | | | | | | 11.50 | 0.729A | | |
| | | | | | | | | | | | | | | 12.00 | 0.734A | | |
| | | | | | | | | | | | | | | 12.50 | 0.739A | | |
| | | | | | | | | | | | | | | 13.00 | 0.744A | | |
| | | | | | | | | | | | | | | 13.50 | 0.748A | | |
| | | | | | | | | | | | | | | 14.00 | 0.752A | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

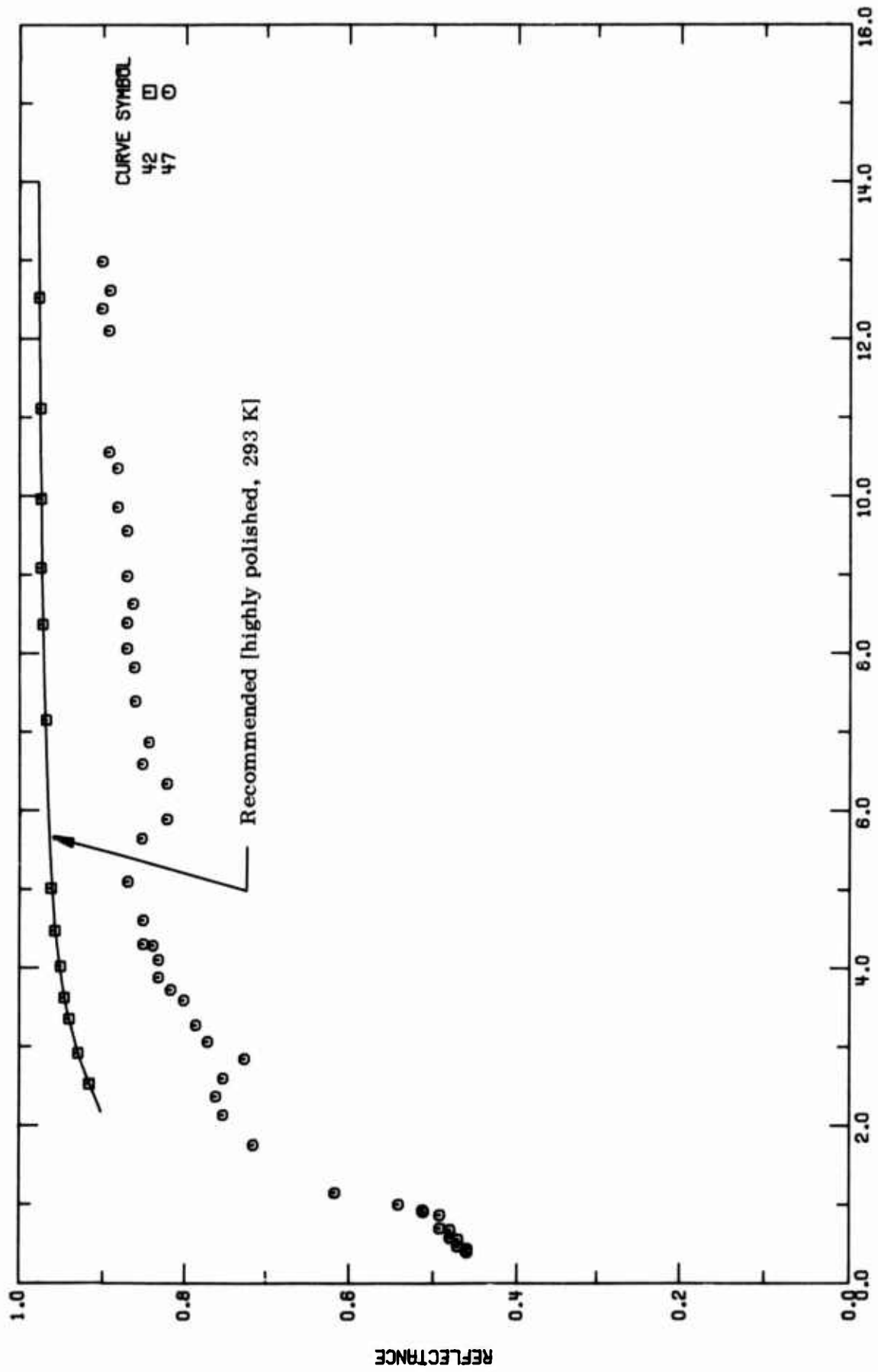


FIGURE 1-10. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

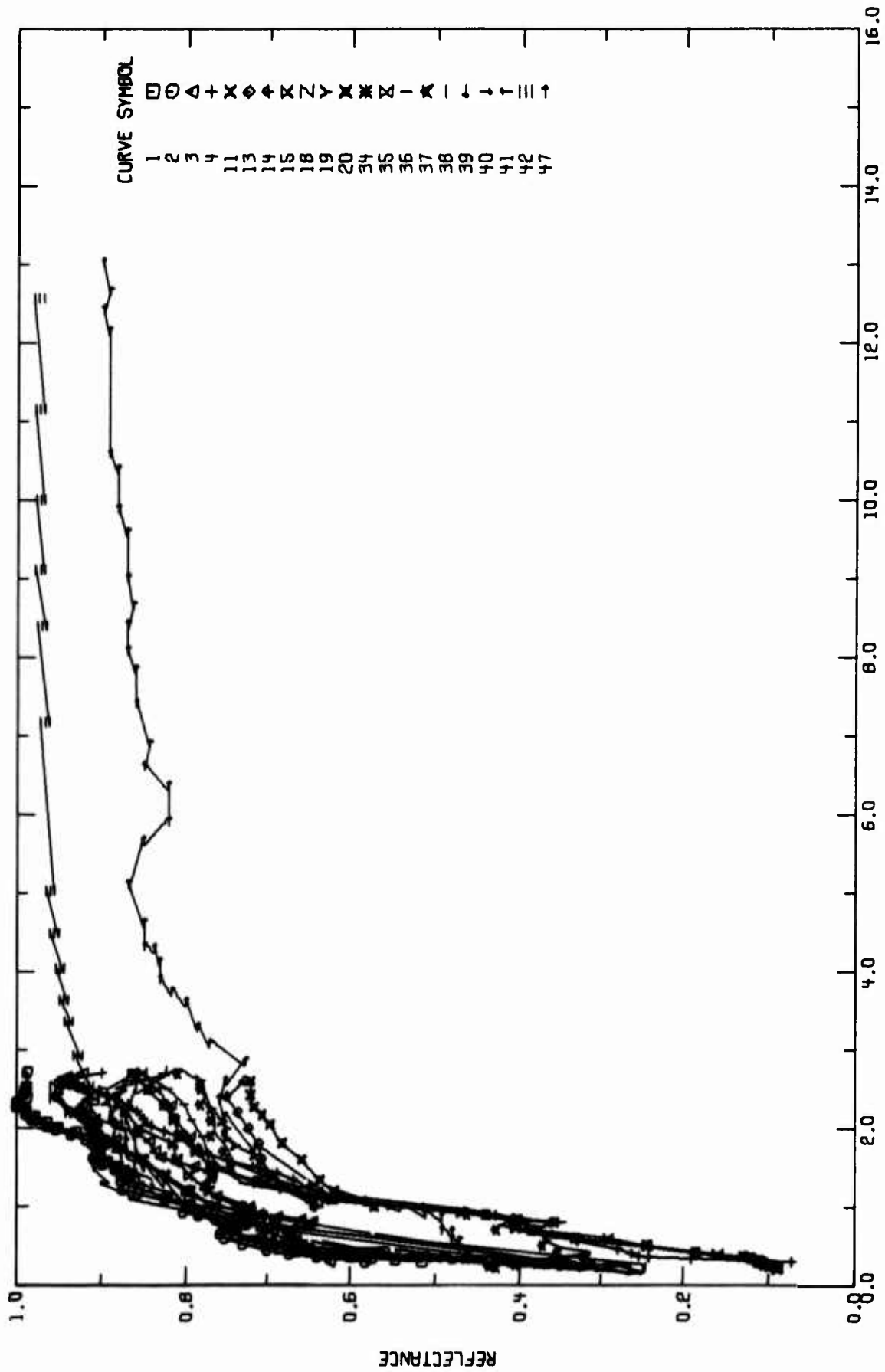


FIGURE 1-11. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

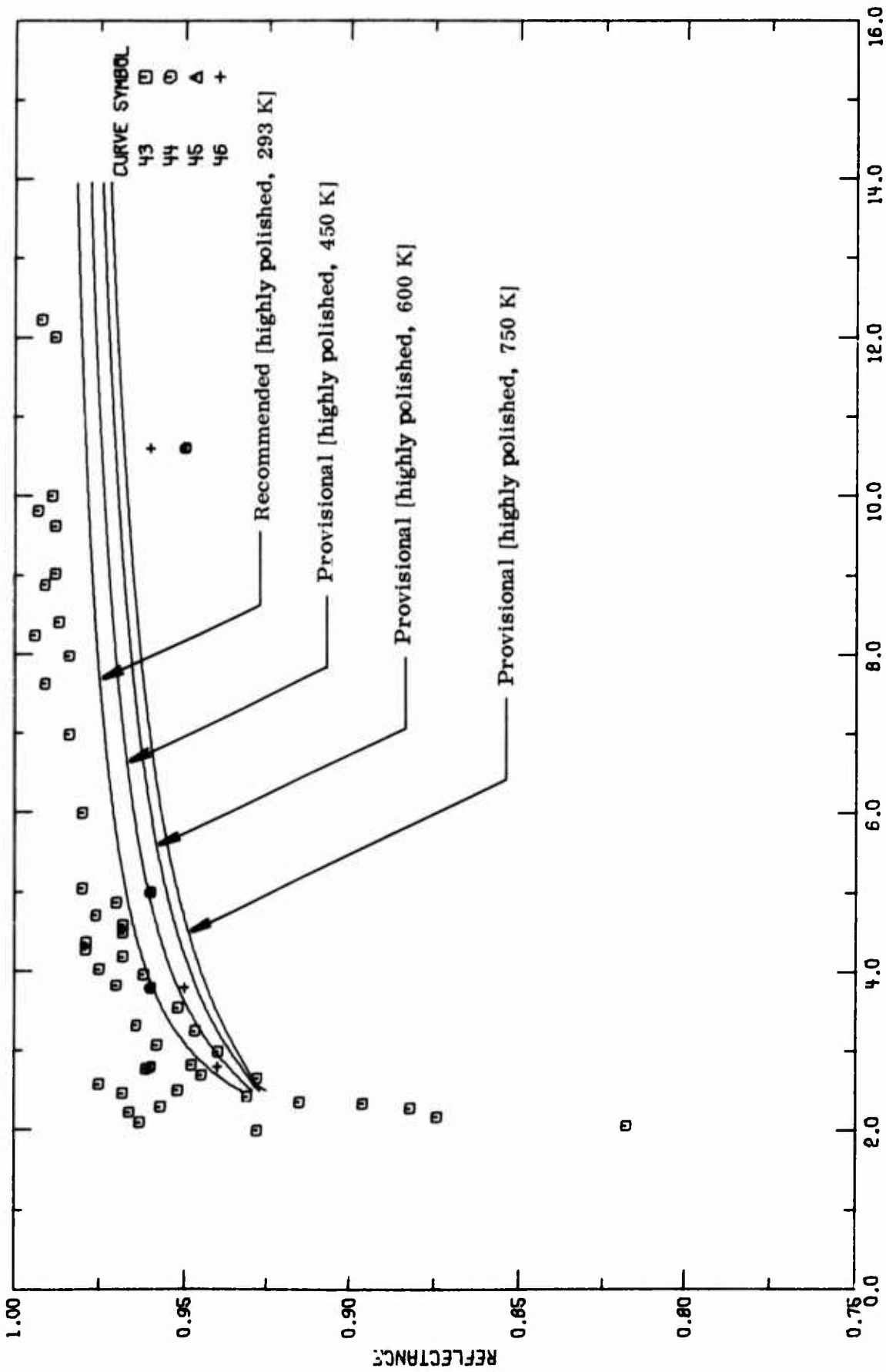


FIGURE 1-12. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

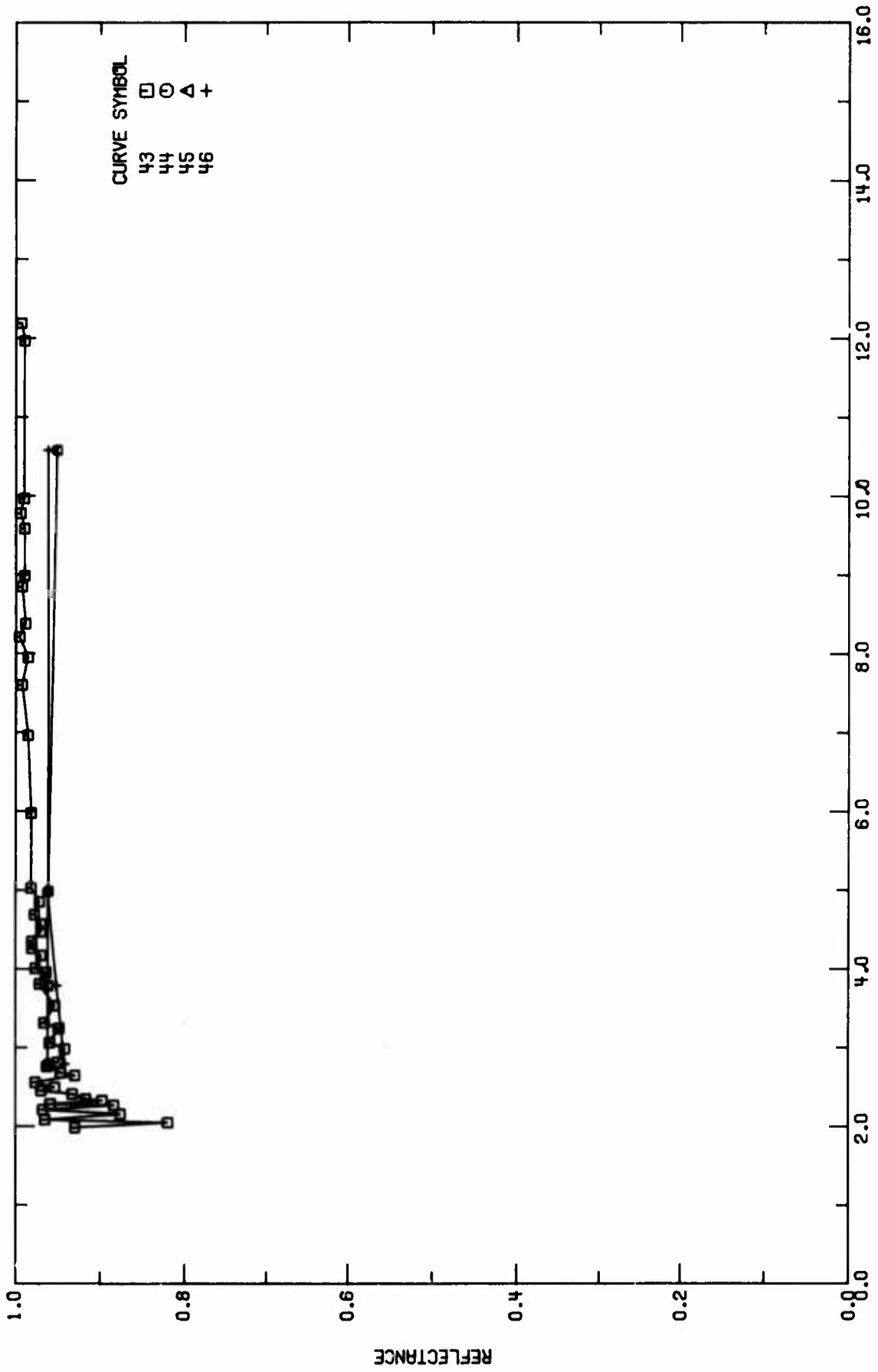


FIGURE 1-13. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

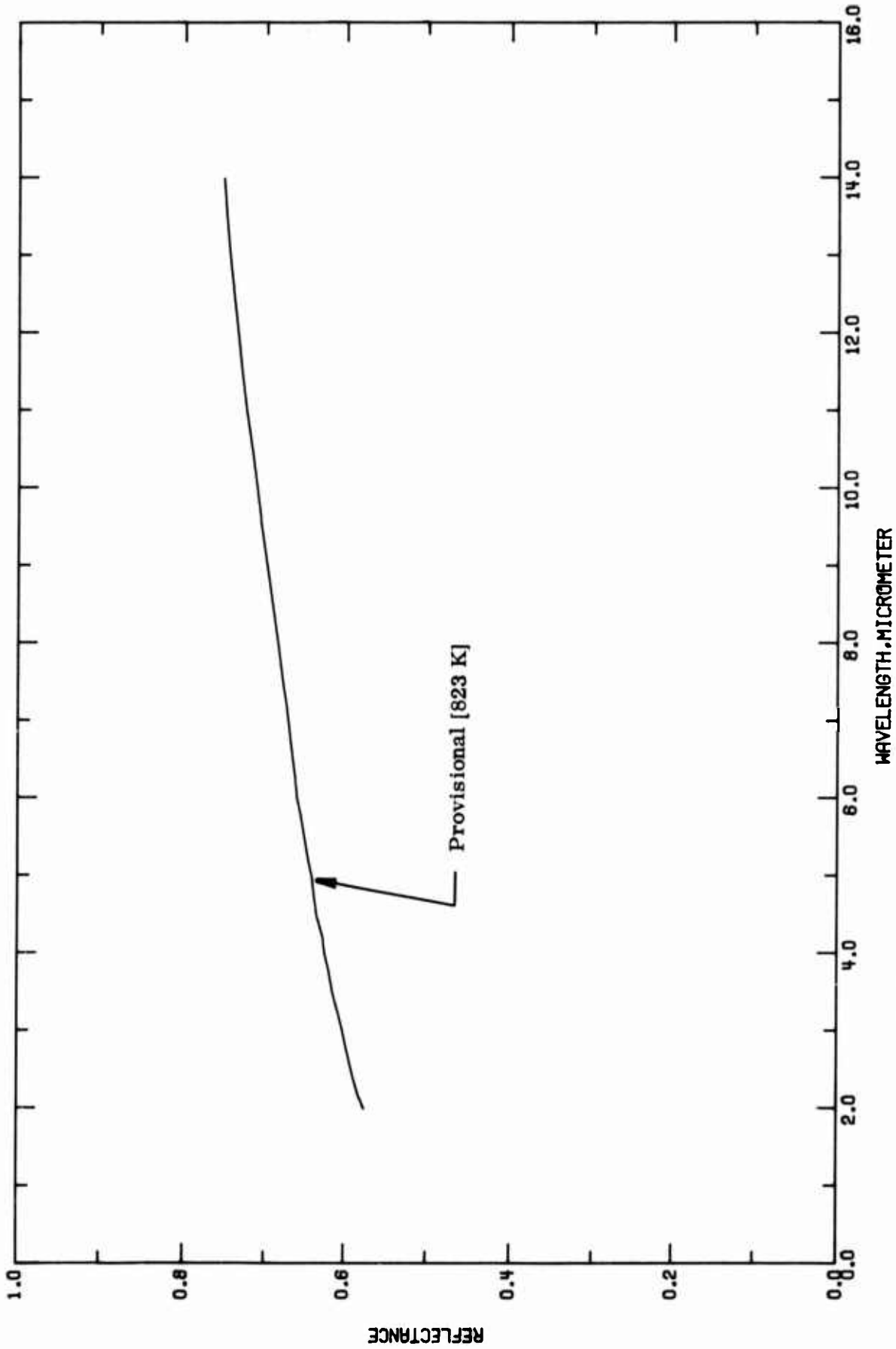


FIGURE 1-14. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF OXIDIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

TABLE 1-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent) | Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|----------------------------------|------------------------------|--|
| 1 T06979 | Betz, H. T., Morris, J. C., Olson, O. H., and Schurba, B. D. | 1957 | 0.3-2.7 | 293 | Aluminum 24-ST | | Surface conditions as received from supplier, may include oily film or plain dirt; a General Electric Recording Spectrophotometer is used in visible range and an integrating sphere reflectometer is used for ultraviolet and infrared regions; magnesium carbonate block used for standard; smooth values extracted from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta=6^\circ$ in visible region, $\theta=9^\circ$ in ultraviolet and infrared regions; reported error $\pm 4\%$. Similar to the above specimen except sample cleaned with liquid detergent to remove superficial dirt and oil films. |
| 2 T06979 | Betz, H. T., et al. | 1957 | 0.3-2.7 | 293 | Aluminum 24-ST | | Similar to the above specimen except sample polished with fine polishing compound on buffing wheel. |
| 3 T06979 | Betz, H. T., et al. | 1957 | 0.3-2.7 | 293 | Aluminum 24-ST | | Similar to the above specimen except sample allowed to oxidize in air at red heat for 30 min. |
| 4 T06979 | Betz, H. T., et al. | 1957 | 0.3-2.7 | 293 | Aluminum 24-ST | | Specimen was $15/16'' \times 1'' \times 1''$ with symmetric V-grooves cut into one $15/16'' \times 1''$ face; grooved surfaces made for this study with ruling machine of type used by Bausch and Lomb, loc.; specifications of grooved profiles and angle so reported by manufacturer, valley to valley distance (w), 83.33 μm , peak to valley height (h), 24.4 μm , and angle between faces, $119^\circ 13'$; source used is G.E. 30A/T20/4 tungsten ribbon strip lamp enclosed in H_2O cooled shield, monochromator used was Perkin-Elmer Model 83, detectors used were RCA 1P28 photomultiplier tube for visible (0.2-0.7 μm) and Perkin-Elmer lead sulfide photoconductive cell for near infrared (0.4-2.8 μm); incident beam and viewing path was perpendicular to groove; angle θ said to be negative if measured in same direction from normal as θ ; θ ' uncertainty $\pm 1^\circ$; reference was standard mirror; specimen appeared "bright and shining" to eye; measured temperature specified as room temperature, 293 K assigned; $\theta=0^\circ$, $\theta'=59^\circ$. |
| 5 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | | The above specimen except $\theta'=-60^\circ$. |
| 6 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | | Similar to the above specimen except $\theta'=59^\circ$. |
| 7 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | | The above specimen except $\theta'=-60^\circ$. |
| 8 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | | Similar to the above specimen except $w = 16.67 \mu\text{m}$, $h = 4.9 \mu\text{m}$, the angle of the V-groove = $119^\circ 6'$; $\theta'=58.0^\circ$. |
| 9 T39074 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | | The above specimen except $\theta'=-59.5^\circ$. |
| 10 T39074 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | | Specimen 2.22 cm discs, 0.16 to 0.32 cm thick; sample surface prepared by standard metallographic techniques, average horizontal peak to peak distance, 30 μm , groove depth is 0.40 μm ; integrating sphere used with PbS detector; reference standard MgO; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta=5^\circ$, $\omega'=27^\circ$. |
| 11 T29563 | Eberhart, R.C. | 1960 | 1.0-2.6 | 293 | Aluminum 24ST, Polished | | Similar to the above specimen except a phototube detector (RCA PM 128 photomultiplier tube) was used with an integrating sphere. |
| 12 T29563 | Eberhart, R.C. | 1960 | 0.4-1.0 | 293 | Aluminum 24ST, Polished | | |

TABLE 1-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 13 T29563 | Eberhart, R. C. | 1960 | 1.0-2.6 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except a Beckman DK-2 spectrophotometer was used for measurement; states values were uncorrected; reported error 10-15%. |
| 14 T29563 | Eberhart, R. C. | 1960 | 1.0-2.6 | 293 | Aluminum 24ST, Polished | Similar to specimen in curve 11. |
| 15 T29563 | Eberhart, R. C. | 1960 | 1.0-2.6 | 293 | Aluminum 24ST, Polished | Similar to the above specimen but a Beckman DK-2 spectrophotometer was used for measurement; states values were corrected. |
| 16 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to specimen in curve 11 except $\theta=0^\circ$. |
| 17 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=10^\circ$. |
| 18 T29563 | Eberhart, R. C. | 1960 | 1-2.6 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except data extracted from smooth curve; $\theta=5^\circ$. |
| 19 T29563 | Eberhart, R. C. | 1960 | 1-2.6 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except average horizontal peak to peak distance, 7 μm , groove depth (average displacement from mean surface line) is 3.48 μm ; sample surface prepared with sandpaper; data extracted from smooth curve. |
| 20 T29563 | Eberhart, R. C. | 1960 | 1-2.6 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except average horizontal peak to peak distance, 10 μm , groove depth (average displacement from mean surface line) is 4.52 μm ; sample surface prepared with sandpaper; data extracted from smooth curve. |
| 21 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to specimen in curve 11 except data extracted from smooth curve; $\theta=0^\circ$. |
| 22 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=5^\circ$. |
| 23 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=10^\circ$. |
| 24 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except average horizontal peak to peak distance, 7 μm , groove depth (average displacement from mean surface line) is 3.48 μm ; sample surface prepared with sandpaper; data extracted from smooth curve; $\theta=0^\circ$. |
| 25 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=5^\circ$. |
| 26 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=10^\circ$. |
| 27 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except average horizontal peak to peak distance, 10 μm , groove depth (average displacement from mean surface line) is 4.52 μm ; sample surface prepared with sandpaper; data extracted from smooth curve; $\theta=0^\circ$. |
| 28 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=5^\circ$. |
| 29 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=10^\circ$. |

TABLE 1-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 30 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Polished; Beckman DK-2 spectrometer integrating sphere used for measurement; MgO reference standard; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta=0^\circ$, $\omega=3\pi$. Similar to the above specimen except $\theta=10^\circ$. |
| 31 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | |
| 32 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Roughened sample; surface roughened with sandpaper, scratches parallel, coarse structure-peak to peak depth-6.35 μm , spacing-34 μm ; fine structure-peak to peak depth-1 μm ; Beckman DK-2 spectrometer integrating sphere used for measurement; MgO reference standard; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta=0^\circ$, $\omega=2\pi$. Similar to the above specimen except $\theta=10^\circ$. |
| 33 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | |
| 34 T24808 | Alexander, A.L., Cowling, J.E., and Noonan, F.M. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | Sample anodized; specimen irradiated in vacuum $\leq 1 \times 10^{-5}$ mm Hg at level of 0.75 cal/min for 100 hr; measurements made with Beckman DK-2 Spectrophotometer; data extracted from figure; measurement temperature not explicitly given, 293 K assigned; normal reflectance assumed; $\theta \sim 0^\circ$. Similar to the above specimen except irradiation applied for 60 hr. |
| 35 T24808 | Alexander, A.L., et al. | 1961 | 0.20-2.7 | 293 | Aluminum Alloy 24S-T | |
| 36 T24808 | Alexander, A.L., et al. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | Similar to the above specimen except irradiation applied for 20 hr. |
| 37 T24808 | Alexander, A.L., et al. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | Similar to the above specimen except not exposed to irradiation. |
| 38 T24808 | Alexander, A.L., et al. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | Sample clean rolled; specimen irradiated in vacuum $\leq 1 \times 10^{-5}$ mm Hg at level of 0.75 cal/min for 100 hr; measurements made with Beckman DK-2 spectrophotometer; data extracted from figure; measurement temperature not explicitly given, 293 K assumed; normal reflectance assumed; $\theta \sim 0^\circ$. Similar to the above specimen except irradiation applied for 60 hr. |
| 39 T24808 | Alexander, A.L., et al. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | |
| 40 T24808 | Alexander, A.L., et al. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | Similar to the above specimen except irradiation applied for 20 hr. |
| 41 T24808 | Alexander, A.L., et al. | 1961 | 0.22-2.7 | 293 | Aluminum Alloy 24S-T | Similar to the above specimen except not exposed to irradiation. |
| 42 A00003 | Schrieffer, J.T. and Wieting, T.J. | 1974 | 2.53-20.0 | 293 | Aluminum Alloy | Author states specimen was "aluminum alloy very similar to 2024 aluminum"; author describes surface as "high quality"; reflectance measured using grating spectrometer; a gold reference mirror was used as a standard; data extracted from figure; measurement temperature specified as room temperature, 293 K assigned; $\theta \sim 0^\circ$, reported error $\pm 0.1\%$. |

TABLE 1-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|--------------------------------------|------|---------------------------------|----------------------|---------------------------------|---|
| 43 A00001 | Grimm, F. C. and Farnia, E. R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. B-1 | Polished; sample thickness 99.0×10^{-3} cm; samples prepared by Organic Chemistry Laboratory of Dept. 255; measurements made with a Dunn Associates ellipsoidal mirror reflectometer; measurement temperature specified as ambient temperature, 293 K assigned; data extracted from smooth curve; relative reflectance reported, multiplied by 0.95 to convert to absolute (gold reference standard used); $\theta=15^\circ$, $\omega^*=2\pi$. |
| 44 A00001 | Grimm, F. C. and Farnia, E. R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen; reported values different from the values of above specimen for unknown reason. |
| 45 A00001 | Grimm, F. C. and Farnia, E. R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen. |
| 46 A00001 | Grimm, F. C. and Farnia, E. R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen except sample heat treated by heating to 644 K for 1 hr in air; absolute reflectance reported; data extracted from table. |
| 47 T40746 | Shipley, W. S. and Thostensen, T. O. | 1960 | 0.4-25.0 | 293 | 2024-T3 Aluminum Sample S4 | "125" finish; measurement temperature not given explicitly, 293 K assigned; data extracted from smooth curve; normal reflectance assumed; $\theta \sim 0^\circ$, $\omega^* = 2\pi$. |

TABLE 1-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 T = 293. | | CURVE 1 (CONT.) | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 (CONT.) | | CURVE 9* T = 293. | |
|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------------|--------|-----------------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 0.300 | 0.515 | 2.705 | 0.907 | 2.324 | 1.000 | 2.299 | 0.922 | 1.956 | 0.026 | 0.5 | 0.103 |
| 0.320 | 0.547 | CURVE 2 | | 2.377 | 0.987 | 2.360 | 0.917 | 2.026 | 0.042 | CURVE 10* T = 293. | |
| 0.339 | 0.575 | T = 293. | | 2.450 | 0.990 | 2.413 | 0.910 | 2.116 | 0.051 | CURVE 11 T = 293. | |
| 0.361 | 0.590 | 0.300 | 0.501 | 2.516 | 0.980 | 2.456 | 0.917 | 2.211 | 0.059 | CURVE 12* T = 293. | |
| 0.397 | 0.630 | 0.357 | 0.630 | 2.705 | 0.987 | 2.552 | 0.941 | 2.201 | 0.069 | CURVE 13 T = 293. | |
| 0.427 | 0.666 | 0.399 | 0.672 | CURVE 3 | | 2.611 | 0.950 | 2.351 | 0.080 | CURVE 5* T = 293. | |
| 0.466 | 0.685 | 0.450 | 0.700 | T = 293. | | 2.653 | 0.941 | 2.414 | 0.094 | CURVE 6* T = 293. | |
| 0.506 | 0.701 | 0.523 | 0.729 | 0.300 | 0.623 | 2.700 | 0.922 | 2.522 | 0.126 | CURVE 7* T = 293. | |
| 0.560 | 0.719 | 0.590 | 0.752 | 0.379 | 0.633 | CURVE 4 | | 2.562 | 0.136 | CURVE 8* T = 293. | |
| 0.640 | 0.730 | 0.654 | 0.758 | 0.449 | 0.640 | T = 293. | | 2.603 | 0.143 | CURVE 9* T = 293. | |
| 0.724 | 0.738 | 0.700 | 0.752 | 0.506 | 0.657 | 0.300 | 0.072 | 2.642 | 0.129 | CURVE 10* T = 293. | |
| 0.775 | 0.726 | 0.766 | 0.735 | 0.576 | 0.665 | 0.335 | 0.190 | 2.700 | 0.099 | CURVE 11 T = 293. | |
| 0.811 | 0.719 | 0.822 | 0.731 | 0.614 | 0.672 | 0.353 | 0.242 | CURVE 12* T = 293. | | CURVE 12* T = 293. | |
| 0.851 | 0.736 | 0.842 | 0.747 | 0.685 | 0.672 | 0.367 | 0.254 | CURVE 13 T = 293. | | CURVE 13 T = 293. | |
| 0.928 | 0.702 | 0.886 | 0.744 | 0.772 | 0.647 | 0.434 | 0.263 | CURVE 14* T = 293. | | CURVE 14* T = 293. | |
| 1.017 | 0.795 | 0.930 | 0.803 | 0.805 | 0.645 | 0.457 | 0.279 | CURVE 15* T = 293. | | CURVE 15* T = 293. | |
| 1.113 | 0.822 | 1.013 | 0.799 | 0.873 | 0.659 | 0.569 | 0.324 | CURVE 16* T = 293. | | CURVE 16* T = 293. | |
| 1.220 | 0.857 | 1.067 | 0.824 | 0.873 | 0.687 | 0.640 | 0.360 | CURVE 17* T = 293. | | CURVE 17* T = 293. | |
| 1.310 | 0.862 | 1.171 | 0.857 | 0.908 | 0.710 | 0.705 | 0.370 | CURVE 18* T = 293. | | CURVE 18* T = 293. | |
| 1.370 | 0.867 | 1.217 | 0.874 | 0.944 | 0.720 | 0.792 | 0.393 | CURVE 19* T = 293. | | CURVE 19* T = 293. | |
| 1.445 | 0.873 | 1.330 | 0.876 | 1.006 | 0.73E | 0.845 | 0.400 | CURVE 20* T = 293. | | CURVE 20* T = 293. | |
| 1.506 | 0.861 | 1.415 | 0.876 | 1.134 | 0.762 | 0.890 | 0.429 | CURVE 21* T = 293. | | CURVE 21* T = 293. | |
| 1.570 | 0.893 | 1.476 | 0.883 | 1.232 | 0.777 | 0.941 | 0.465 | CURVE 22* T = 293. | | CURVE 22* T = 293. | |
| 1.621 | 0.902 | 1.538 | 0.897 | 1.269 | 0.777 | 0.989 | 0.514 | CURVE 23* T = 293. | | CURVE 23* T = 293. | |
| 1.729 | 0.902 | 1.584 | 0.906 | 1.352 | 0.765 | 1.022 | 0.556 | CURVE 24* T = 293. | | CURVE 24* T = 293. | |
| 1.795 | 0.890 | 1.626 | 0.909 | 1.409 | 0.767 | 1.055 | 0.502 | CURVE 25* T = 293. | | CURVE 25* T = 293. | |
| 1.830 | 0.890 | 1.626 | 0.909 | 1.452 | 0.773 | 1.116 | 0.606 | CURVE 26* T = 293. | | CURVE 26* T = 293. | |
| 1.890 | 0.910 | 1.799 | 0.910 | 1.510 | 0.790 | 1.181 | 0.633 | CURVE 27* T = 293. | | CURVE 27* T = 293. | |
| 1.945 | 0.930 | 1.846 | 0.917 | 1.568 | 0.812 | 1.251 | 0.649 | CURVE 28* T = 293. | | CURVE 28* T = 293. | |
| 2.003 | 0.952 | 1.914 | 0.935 | 1.629 | 0.830 | 1.345 | 0.660 | CURVE 29* T = 293. | | CURVE 29* T = 293. | |
| 2.064 | 0.955 | 1.980 | 0.953 | 1.629 | 0.830 | 1.430 | 0.680 | CURVE 30* T = 293. | | CURVE 30* T = 293. | |
| 2.142 | 0.979 | 2.015 | 0.963 | 1.707 | 0.837 | 1.505 | 0.717 | CURVE 31* T = 293. | | CURVE 31* T = 293. | |
| 2.214 | 0.989 | 2.054 | 0.972 | 1.833 | 0.844 | 1.591 | 0.749 | CURVE 32* T = 293. | | CURVE 32* T = 293. | |
| 2.275 | 1.000 | 2.107 | 0.981 | 1.950 | 0.861 | 1.663 | 0.773 | CURVE 33* T = 293. | | CURVE 33* T = 293. | |
| 2.324 | 1.000 | 2.166 | 0.988 | 2.035 | 0.882 | 1.734 | 0.705 | CURVE 34* T = 293. | | CURVE 34* T = 293. | |
| 2.377 | 0.987 | 2.204 | 0.989 | 2.115 | 0.907 | 1.803 | 0.807 | CURVE 35* T = 293. | | CURVE 35* T = 293. | |
| 2.450 | 0.990 | 2.214 | 0.989 | 2.170 | 0.910 | 1.827 | 0.797 | CURVE 36* T = 293. | | CURVE 36* T = 293. | |
| 2.516 | 0.900 | 2.275 | 1.000 | 2.218 | 0.926 | 1.883 | 0.807 | CURVE 37* T = 293. | | CURVE 37* T = 293. | |

* NOT SHOWN IN FIGURE.

TABLE 1-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | | |
|------------------------|--------|----------------------|--------|-----------------------|--------|-----------------------|--------|-----------------------|--------|----------------------|--------|-----------------------|--|
| CURVE 13 (CONT.) | | | | | | | | | | | | | |
| 2.60 | 0.729 | CURVE 18 T = 293. | | | | | | | | | | | |
| CURVE 14 T = 293. | | | | | | | | | | | | | |
| 1.00 | 0.767 | 1.00 | 0.764 | CURVE 21* T = 293. | | | | | | | | CURVE 29* T = 293. | |
| 1.20 | 0.796 | 1.20 | 0.800 | 1.2 | 0.775 | CURVE 22* T = 293. | | CURVE 30* T = 293. | | CURVE 34 (CONT.) | | | |
| 1.40 | 0.827 | 1.40 | 0.828 | CURVE 23* T = 293. | | CURVE 23* T = 293. | | CURVE 31* T = 293. | | CURVE 35 T = 293. | | | |
| 1.60 | 0.856 | 1.60 | 0.855 | 1.2 | 0.806 | CURVE 24* T = 293. | | CURVE 32* T = 293. | | CURVE 36 (CONT.) | | | |
| 1.80 | 0.891 | 1.80 | 0.879 | 1.2 | 0.840 | CURVE 25* T = 293. | | CURVE 33* T = 293. | | CURVE 37 T = 293. | | | |
| 2.00 | 0.914 | 2.00 | 0.907 | 1.2 | 0.665 | CURVE 26* T = 293. | | CURVE 34 T = 293. | | CURVE 38 | | | |
| 2.20 | 0.936 | 2.20 | 0.937 | 1.2 | 0.678 | CURVE 27* T = 293. | | CURVE 35 T = 293. | | CURVE 39 | | | |
| 2.40 | 0.955 | 2.40 | 0.955 | 1.2 | 0.581 | CURVE 28* T = 293. | | CURVE 36 T = 293. | | CURVE 40 | | | |
| 2.60 | 0.942 | 2.60 | 0.946 | 1.2 | 0.594 | CURVE 29* T = 293. | | CURVE 37 T = 293. | | CURVE 41 | | | |
| CURVE 15 T = 293. | | | | | | | | | | | | | |
| 1.00 | 0.721 | 1.00 | 0.638 | CURVE 31* T = 293. | | | | | | | | CURVE 42 | |
| 1.20 | 0.772 | 1.24 | 0.680 | CURVE 32* T = 293. | | CURVE 32* T = 293. | | CURVE 33* T = 293. | | CURVE 43 | | | |
| 1.40 | 0.796 | 1.48 | 0.707 | 1.2 | 0.654 | CURVE 33* T = 293. | | CURVE 34 T = 293. | | CURVE 44 | | | |
| 1.60 | 0.811 | 1.66 | 0.715 | 1.2 | 0.665 | CURVE 34 T = 293. | | CURVE 35 T = 293. | | CURVE 45 | | | |
| 1.80 | 0.815 | 1.78 | 0.739 | 1.2 | 0.678 | CURVE 35 T = 293. | | CURVE 36 T = 293. | | CURVE 46 | | | |
| 2.00 | 0.856 | 1.87 | 0.750 | 1.2 | 0.687 | CURVE 36 T = 293. | | CURVE 37 T = 293. | | CURVE 47 | | | |
| 2.20 | 0.872 | 2.00 | 0.750 | 1.2 | 0.697 | CURVE 37 T = 293. | | CURVE 38 T = 293. | | CURVE 48 | | | |
| 2.40 | 0.887 | 2.09 | 0.755 | 1.2 | 0.707 | CURVE 38 T = 293. | | CURVE 39 T = 293. | | CURVE 49 | | | |
| 2.60 | 0.934 | 2.24 | 0.769 | 1.2 | 0.717 | CURVE 39 T = 293. | | CURVE 40 T = 293. | | CURVE 50 | | | |
| CURVE 16* T = 293. | | | | | | | | | | | | | |
| 1.2 | 0.794 | 2.60 | 0.783 | 1.2 | 0.721 | CURVE 41 T = 293. | | CURVE 42 T = 293. | | CURVE 51 | | | |
| 1.8 | 0.882 | CURVE 20 T = 293. | | | | | | | | | | | |
| CURVE 17* T = 293. | | | | | | | | | | | | | |
| 1.2 | 0.822 | 1.00 | 0.572 | CURVE 43 T = 293. | | | | | | | | CURVE 52 | |
| 1.8 | 0.914 | 1.20 | 0.619 | CURVE 44 T = 293. | | CURVE 44 T = 293. | | CURVE 45 T = 293. | | CURVE 53 | | | |
| * NOT SHOWN IN FIGURE. | | | | | | | | | | | | | |

TABLE 1-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM: ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | | |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|------|-------|
| CURVE 37 (CONT.) | | | | | | | | | | | | | | | |
| 1.696 | 0.755 | 0.220 | 0.263 | 0.320 | 0.470 | 0.700 | 0.746 | 2.00 | 0.928 | 2.00 | 0.928 | 6.00 | 0.991 | | |
| 1.895 | 0.771 | 0.240 | 0.306 | 0.340 | 0.504 | 0.800 | 0.755 | 2.06 | 0.818 | 2.06 | 0.818 | 9.02 | 0.988 | | |
| 2.093 | 0.771 | 0.260 | 0.353 | 0.360 | 0.528 | 0.200 | 0.323 | 2.10 | 0.963 | 2.10 | 0.963 | 9.62 | 0.988 | | |
| 2.289 | 0.784 | 0.280 | 0.371 | 0.420 | 0.565 | 0.301 | 0.464 | 2.17 | 0.874 | 2.17 | 0.874 | 9.81 | 0.993 | | |
| 2.488 | 0.784 | 0.300 | 0.409 | 0.500 | 0.666 | 0.399 | 0.592 | 2.23 | 0.966 | 2.23 | 0.966 | 10.00 | 0.989 | | |
| 2.690 | 0.812 | 0.320 | 0.443 | 0.600 | 0.705 | 0.497 | 0.703 | 2.28 | 0.966 | 2.28 | 0.966 | 12.00 | 0.988 | | |
| CURVE 38 | | | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | |
| 0.220 | 0.246 | 0.340 | 0.482 | 0.800 | 0.707 | 0.699 | 0.752 | 2.30 | 0.957 | 2.30 | 0.957 | 12.22 | 0.992 | | |
| 0.240 | 0.295 | 0.360 | 0.507 | 0.202 | 0.295 | 0.798 | 0.763 | 2.34 | 0.896 | 2.34 | 0.896 | 14.67 | 0.992 | | |
| 0.260 | 0.338 | 0.420 | 0.554 | 0.299 | 0.434 | 0.899 | 0.781 | 2.36 | 0.915 | 2.36 | 0.915 | CURVE 44 | | | |
| 0.285 | 0.366 | 0.500 | 0.652 | 0.400 | 0.513 | 1.099 | 0.863 | 2.43 | 0.931 | 2.43 | 0.931 | T = 293. | | | |
| 0.305 | 0.401 | 0.600 | 0.694 | 0.498 | 0.674 | 1.299 | 0.895 | 2.47 | 0.968 | 2.47 | 0.968 | | | | |
| 0.325 | 0.439 | 0.704 | 0.694 | 0.599 | 0.714 | 1.498 | 0.905 | 2.51 | 0.952 | 2.51 | 0.952 | | | | |
| 0.340 | 0.465 | 0.800 | 0.695 | 0.695 | 0.702 | 1.699 | 0.906 | 2.58 | 0.975 | 2.58 | 0.975 | | | | |
| 0.360 | 0.493 | 0.800 | 0.702 | 0.801 | 0.715 | 1.898 | 0.906 | 2.66 | 0.928 | 2.66 | 0.928 | | | | |
| 0.420 | 0.542 | 0.303 | 0.415 | 0.898 | 0.731 | 2.096 | 0.906 | 2.70 | 0.945 | 2.70 | 0.945 | | | | |
| 0.500 | 0.631 | 0.403 | 0.560 | 1.100 | 0.825 | 2.298 | 0.909 | 2.78 | 0.961 | 2.78 | 0.961 | | | | |
| 0.600 | 0.679 | 0.500 | 0.659 | 1.300 | 0.855 | 2.500 | 0.898 | 2.83 | 0.948 | 2.83 | 0.948 | CURVE 45 | | | |
| 0.700 | 0.679 | 0.603 | 0.702 | 1.697 | 0.882 | 2.694 | 0.858 | 3.00 | 0.948 | 3.00 | 0.948 | T = 293. | | | |
| 0.800 | 0.687 | 0.720 | 0.703 | 1.896 | 0.882 | CURVE 42 | | | | | | 2.8 | 0.96 | | |
| 0.900 | 0.687 | 0.804 | 0.719 | 2.096 | 0.887 | T = 293. | | | | | | 3.8 | 0.96 | | |
| 1.000 | 0.687 | 0.899 | 0.719 | 2.298 | 0.887 | | | | | | | 5.0 | 0.96 | | |
| 1.200 | 0.687 | 1.099 | 0.841 | 2.501 | 0.879 | | | | | | | 10.6 | 0.95 | | |
| 1.400 | 0.687 | 1.299 | 0.841 | 2.694 | 0.879 | | | | | | | CURVE 46 | | | |
| 1.600 | 0.687 | 1.499 | 0.862 | | | | | | | T = 293. | | | | | |
| 1.800 | 0.687 | 1.697 | 0.870 | | | | | | | | | | | | |
| 2.000 | 0.687 | 1.900 | 0.872 | | | | | | | | | | | | |
| 2.200 | 0.687 | 2.121 | 0.888 | | | | | | | | | | | | |
| 2.400 | 0.687 | 2.303 | 0.884 | | | | | | | | | | | | |
| 2.600 | 0.687 | 2.527 | 0.875 | | | | | | | | | | | | |
| 2.800 | 0.687 | 2.725 | 0.824 | | | | | | | | | | | | |
| 3.000 | 0.687 | | | | | | | CURVE 41 | | | | | | | |
| 3.200 | 0.687 | | | | | | | T = 293. | | | | | | | |
| 3.400 | 0.687 | 0.220 | 0.320 | 2.53 | 0.9150 | 3.97 | 0.962 | 4.03 | 0.975 | 4.03 | 0.975 | CURVE 46 | | | |
| 3.600 | 0.687 | 0.240 | 0.362 | 3.36 | 0.9391 | 4.03 | 0.975 | 4.19 | 0.968 | 4.19 | 0.968 | T = 293. | | | |
| 3.800 | 0.687 | 0.260 | 0.398 | 3.63 | 0.9449 | 4.28 | 0.979 | 4.28 | 0.968 | 4.28 | 0.968 | | | | |
| 4.000 | 0.687 | 0.300 | 0.429 | 4.03 | 0.9495 | 4.37 | 0.979 | 4.37 | 0.979 | 4.37 | 0.979 | | | | |
| 4.200 | 0.687 | 0.340 | 0.458 | 4.48 | 0.9561 | 4.49 | 0.968 | 4.49 | 0.968 | 4.49 | 0.968 | | | | |
| 4.400 | 0.687 | 0.360 | 0.489 | 5.02 | 0.9609 | 4.59 | 0.968 | 4.59 | 0.968 | 4.59 | 0.968 | | | | |
| 4.600 | 0.687 | 0.420 | 0.518 | 7.16 | 0.9671 | 4.71 | 0.976 | 4.71 | 0.976 | 4.71 | 0.976 | | | | |
| 4.800 | 0.687 | 0.480 | 0.550 | 8.38 | 0.9710 | 4.87 | 0.976 | 4.87 | 0.976 | 4.87 | 0.976 | | | | |
| 5.000 | 0.687 | 0.500 | 0.590 | 9.10 | 0.9734 | 5.05 | 0.980 | 5.05 | 0.980 | 5.05 | 0.980 | | | | |
| 5.200 | 0.687 | 0.560 | 0.628 | 9.98 | 0.9731 | 6.00 | 0.980 | 6.00 | 0.980 | 6.00 | 0.980 | | | | |
| 5.400 | 0.687 | 0.600 | 0.671 | 11.13 | 0.9735 | 6.99 | 0.984 | 6.99 | 0.984 | 6.99 | 0.984 | | | | |
| 5.600 | 0.687 | 0.660 | 0.719 | 12.54 | 0.9754 | 7.63 | 0.991 | 7.63 | 0.991 | 7.63 | 0.991 | | | | |
| 5.800 | 0.687 | 0.720 | 0.766 | 14.31 | 0.9771 | 7.98 | 0.984 | 7.98 | 0.984 | 7.98 | 0.984 | | | | |
| 6.000 | 0.687 | 0.800 | 0.828 | 16.66 | 0.9810 | 8.24 | 0.994 | 8.24 | 0.994 | 8.24 | 0.994 | | | | |
| 6.200 | 0.687 | 0.860 | 0.878 | 19.11 | 0.9805 | 8.41 | 0.987 | 8.41 | 0.987 | 8.41 | 0.987 | | | | |
| 6.400 | 0.687 | 0.900 | 0.928 | 20.00 | 0.9833 | CURVE 47 | | | | | | 0.44 | 0.460 | | |
| 6.600 | 0.687 | | | | | | | T = 293. | | | | | | 0.44 | 0.460 |
| 6.800 | 0.687 | | | | | | | | | | | | | 0.47 | 0.471 |
| 7.000 | 0.687 | | | | | | | | | | | | | 0.56 | 0.471 |

TABLE 1-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, P)

| λ | P | λ | P |
|------------------|-------|------------------|-------|
| CURVE 47 (CONT.) | | CURVE 47 (CONT.) | |
| 0.50 | 0.480 | 12.63 | 0.891 |
| 0.60 | 0.480 | 13.00 | 0.900 |
| 0.70 | 0.492 | 14.90 | 0.900 |
| 0.87 | 0.492 | 15.19 | 0.891 |
| 0.91 | 0.511 | 17.29 | 0.891 |
| 0.93 | 0.512 | 17.57 | 0.900 |
| 1.00 | 0.541 | 25.00 | 0.899 |
| 1.15 | 0.616 | | |
| 1.76 | 0.715 | | |
| 2.14 | 0.752 | | |
| 2.37 | 0.761 | | |
| 2.60 | 0.752 | | |
| 2.85 | 0.726 | | |
| 3.07 | 0.771 | | |
| 3.20 | 0.766 | | |
| 3.60 | 0.801 | | |
| 3.73 | 0.817 | | |
| 3.89 | 0.832 | | |
| 4.11 | 0.832 | | |
| 4.29 | 0.839 | | |
| 4.31 | 0.851 | | |
| 4.61 | 0.851 | | |
| 5.10 | 0.870 | | |
| 5.65 | 0.853 | | |
| 5.90 | 0.822 | | |
| 6.35 | 0.822 | | |
| 6.60 | 0.852 | | |
| 6.88 | 0.844 | | |
| 7.40 | 0.861 | | |
| 7.83 | 0.862 | | |
| 8.07 | 0.871 | | |
| 8.40 | 0.871 | | |
| 8.64 | 0.864 | | |
| 8.99 | 0.871 | | |
| 9.57 | 0.871 | | |
| 9.87 | 0.882 | | |
| 10.37 | 0.882 | | |
| 10.57 | 0.892 | | |
| 12.12 | 0.892 | | |
| 12.40 | 0.900 | | |

e. Normal Spectral Reflectance (Temperature Dependence)

There are no experimental data available. The provisional values listed in Table 1-9 and shown in Figure 1-15 are from the relationship discussed in subsection 4.20 and based on Eq. (2.5-5) for highly polished alclad Aluminum Alloy 2024 assuming that aluminum is the cladding material for wavelengths of 2.8, 3.8, 5.0, and 10.6 μm . These values are believed accurate to $\pm 20\%$.

TABLE 1-9. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ | T | ρ | T | ρ | T | ρ |
|-----------------|--------|-----------------|--------|-----------------|--------|------------------|--------|
| HIGHLY POLISHED | | HIGHLY POLISHED | | HIGHLY POLISHED | | HIGHLY POLISHED | |
| ALCLAD | | ALCLAD | | ALCLAD | | ALCLAD | |
| $\lambda = 2.8$ | | $\lambda = 3.0$ | | $\lambda = 5.0$ | | $\lambda = 10.6$ | |
| 250.0 | 0.946 | 250.0 | 0.962 | 250.0 | 0.970 | 250.0 | 0.981 |
| 293.0 | 0.943 | 293.0 | 0.959 | 293.0 | 0.967 | 293.0 | 0.979 |
| 300.0 | 0.943 | 300.0 | 0.959 | 300.0 | 0.967 | 300.0 | 0.979 |
| 350.0 | 0.940 | 350.0 | 0.956 | 350.0 | 0.964 | 350.0 | 0.977 |
| 400.0 | 0.938 | 400.0 | 0.954 | 400.0 | 0.962 | 400.0 | 0.976 |
| 450.0 | 0.937 | 450.0 | 0.952 | 450.0 | 0.960 | 450.0 | 0.974 |
| 500.0 | 0.935 | 500.0 | 0.950 | 500.0 | 0.959 | 500.0 | 0.973 |
| 550.0 | 0.934 | 550.0 | 0.948 | 550.0 | 0.957 | 550.0 | 0.972 |
| 600.0 | 0.933 | 600.0 | 0.947 | 600.0 | 0.956 | 600.0 | 0.971 |
| 650.0 | 0.932 | 650.0 | 0.945 | 650.0 | 0.954 | 650.0 | 0.970 |
| 700.0 | 0.932 | 700.0 | 0.944 | 700.0 | 0.953 | 700.0 | 0.969 |
| 750.0 | 0.931 | 750.0 | 0.943 | 750.0 | 0.952 | 750.0 | 0.968 |

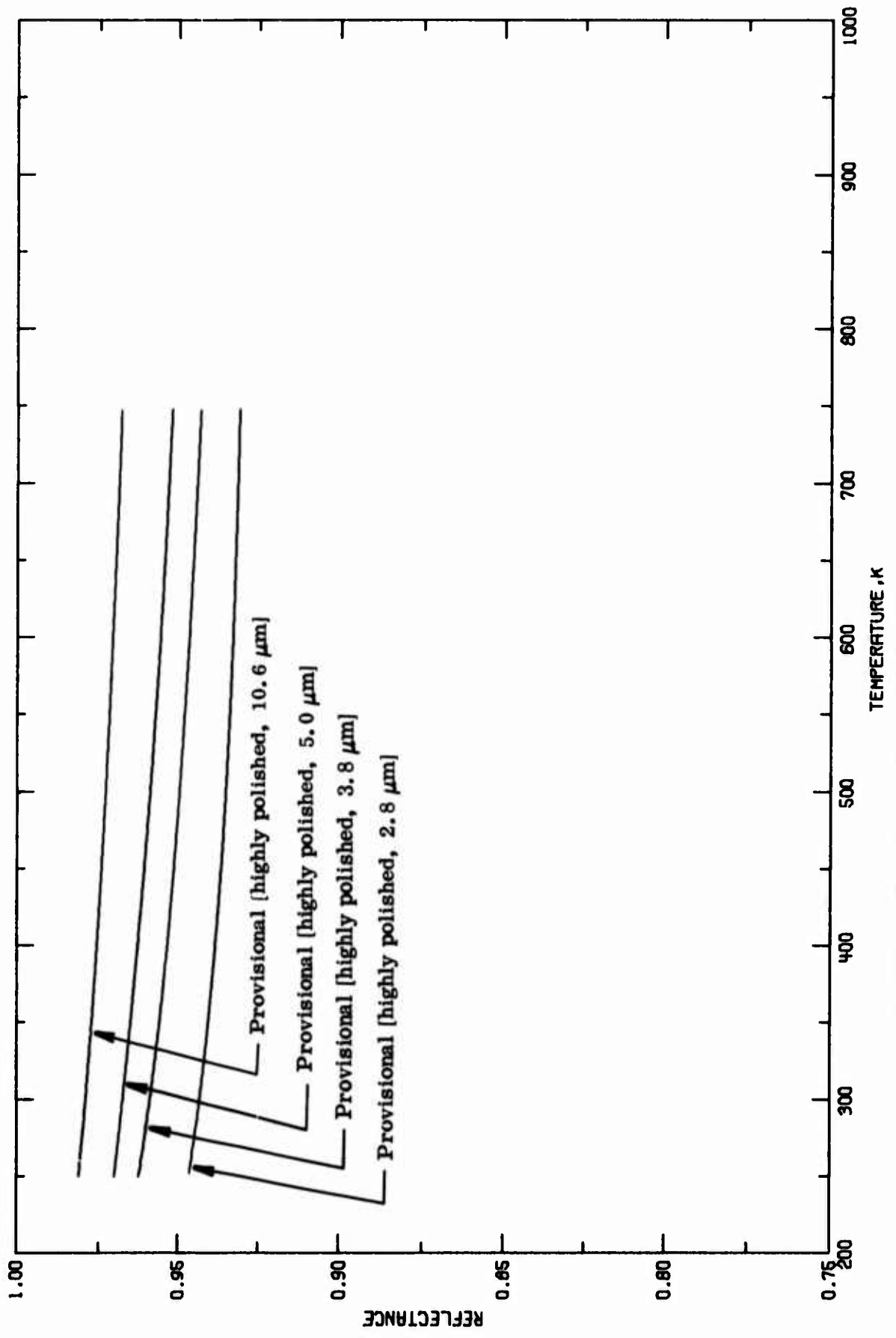


FIGURE 1-15. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALCLAD ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE).

f. Angular Spectral Reflectance (Wavelength Dependence)

There are 191 sets of experimental data for various surface conditions of Aluminum Alloy 2024. Of these sets 111 are for grooved surfaces by Zipin [T39074] which are included in the report as additional information. The analysis includes two types of Aluminum Alloy 2024, anodized and alodined.

There are seven sets of experimental data for anodized Aluminum Alloy 2024 and four sets of experimental data for alodined Aluminum Alloy 2024, both with the angle of incidence equal to 15° . For the alodined Aluminum Alloy 2024, there is one set of experimental data available for an incidence angle of 45° .

(1) Anodized Aluminum Alloy 2024

The experimental data sets are shown in Figure 1-17 and listed in Table 1-12. The provisional values for temperature 293 K are given in Table 1-10 and shown in Figure 1-16 and are considered accurate to within $\pm 15\%$ over the entire wavelength range at 293 K. These values show the absorption peaks near wavelengths 0.8, 2.9, 6.0, 9.9, and $11.0 \mu\text{m}$ and these values are considerably lower than those for polished alclad Aluminum Alloy 2024 and alodined Aluminum Alloy 2024 for wavelengths above $5.5 \mu\text{m}$. These provisional values apply only to the surface conditions cited in references, see Section 4.1c.

(2) Alodined Aluminum Alloy 2024

The experimental data sets are shown in Figure 1-19 and listed in Table 1-12 for an incidence angle of 15° . The provisional values at 293 K, shown in Figure 1-18 and listed in Table 1-10 are primarily from the investigations of Grimm and Fannin [A00001]. These are considered accurate to within $\pm 15\%$ over the entire wavelength range. These values show absorption peaks near wavelengths 3.1 and $4.8 \mu\text{m}$. The experimental data set is shown in Figure 1-21 and listed in Table 1-12 for an incidence angle of 45° . The provisional values of angular spectral reflectance from the investigation of Grimm and Fannin [A00001] are accurate to within $\pm 20\%$ over the entire reported wavelength range. These values also show absorption peaks near wavelengths 3.1 and $4.8 \mu\text{m}$. The provisional values apply only to the surface conditions cited in references, see Section 4.1c.

TABLE 1-10. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)
(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| SULFURIC ACID ANODIZED, $\theta=15^\circ$ T = 293 | | | SULFURIC ACID ANODIZED, $\theta=15^\circ$ T = 293 (CONT.) | | | CHROMATE ALODINED, $\theta=15^\circ$ T = 293 | | | CHROMATE ALODINED, $\theta=15^\circ$ T = 293 (CONT.) | | | CHROMATE ALODINED, $\theta=45^\circ$ T = 293 | | |
|--|--------|-----------|--|-----------|--------|---|--------|-----------|---|-----------|--------|---|--------|--|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
| 0.30 | 0.260 | 6.10 | 0.516 | 2.34 | 0.483 | 12.0 | 0.858 | 2.00 | 0.760 | | | | | |
| 0.35 | 0.360 | 6.20 | 0.527 | 2.50 | 0.469 | 12.5 | 0.865 | 2.20 | 0.742 | | | | | |
| 0.40 | 0.450 | 6.40 | 0.590 | 2.80 | 0.396 | 13.0 | 0.871 | 2.40 | 0.712 | | | | | |
| 0.50 | 0.518 | 6.60 | 0.602 | 3.00 | 0.323 | 13.5 | 0.877 | 2.60 | 0.642 | | | | | |
| 0.60 | 0.526 | 6.80 | 0.595 | 3.05 | 0.315 | 14.0 | 0.882 | 2.80 | 0.448 | | | | | |
| 0.70 | 0.525 | 7.00 | 0.574 | 3.10 | 0.311 | 14.5 | 0.887 | 3.00 | 0.380 | | | | | |
| 0.80 | 0.519 | 7.20 | 0.486 | 3.15 | 0.312 | 15.0 | 0.891 | 3.10 | 0.382 | | | | | |
| 0.83 | 0.518 | 7.40 | 0.360 | 3.20 | 0.318 | | | 3.20 | 0.394 | | | | | |
| 0.90 | 0.566 | 7.60 | 0.260 | 3.25 | 0.327 | | | 3.40 | 0.450 | | | | | |
| 1.00 | 0.620 | 7.80 | 0.180 | 3.30 | 0.345 | | | 3.60 | 0.530 | | | | | |
| 1.20 | 0.680 | 8.00 | 0.125 | 3.50 | 0.411 | | | 3.80 | 0.592 | | | | | |
| 1.40 | 0.708 | 8.20 | 0.082 | 3.70 | 0.472 | | | 4.00 | 0.634 | | | | | |
| 1.60 | 0.726 | 8.40 | 0.058 | 3.80 | 0.492 | | | 4.20 | 0.662 | | | | | |
| 1.80 | 0.732 | 8.60 | 0.051 | 4.00 | 0.520 | | | 4.40 | 0.680 | | | | | |
| 2.00 | 0.721 | 8.80 | 0.053 | 4.20 | 0.542 | | | 4.50 | 0.684 | | | | | |
| 2.20 | 0.699 | 9.00 | 0.060 | 4.50 | 0.569 | | | 4.60 | 0.680 | | | | | |
| 2.40 | 0.659 | 9.20 | 0.080 | 4.56 | 0.574 | | | 4.70 | 0.600 | | | | | |
| 2.60 | 0.578 | 9.40 | 0.107 | 4.61 | 0.573 | | | 4.72 | 0.588 | | | | | |
| 2.80 | 0.221 | 9.60 | 0.136 | 4.70 | 0.539 | | | 4.76 | 0.586 | | | | | |
| 2.85 | 0.193 | 9.80 | 0.145 | 4.74 | 0.522 | | | 4.80 | 0.538 | | | | | |
| 2.90 | 0.190 | 10.00 | 0.136 | 4.77 | 0.519 | | | 4.90 | 0.680 | | | | | |
| 2.95 | 0.192 | 10.20 | 0.100 | 4.81 | 0.528 | | | 5.00 | 0.702 | | | | | |
| 3.00 | 0.203 | 10.40 | 0.065 | 4.87 | 0.560 | | | 5.20 | 0.720 | | | | | |
| 3.20 | 0.323 | 10.60 | 0.040 | 4.93 | 0.595 | | | 5.40 | 0.730 | | | | | |
| 3.40 | 0.408 | 10.80 | 0.028 | 4.95 | 0.603 | | | 5.60 | 0.740 | | | | | |
| 3.60 | 0.474 | 11.00 | 0.025 | 5.00 | 0.606 | | | 5.80 | 0.748 | | | | | |
| 3.80 | 0.516 | 11.20 | 0.037 | 5.50 | 0.638 | | | 6.00 | 0.754 | | | | | |
| 4.00 | 0.546 | 11.40 | 0.045 | 6.00 | 0.666 | | | 7.00 | 0.780 | | | | | |
| 4.20 | 0.572 | 11.60 | 0.051 | 6.50 | 0.692 | | | 8.00 | 0.800 | | | | | |
| 4.40 | 0.590 | 11.80 | 0.057 | 7.00 | 0.715 | | | 9.00 | 0.819 | | | | | |
| 4.60 | 0.604 | 12.00 | 0.062 | 7.50 | 0.737 | | | 10.00 | 0.836 | | | | | |
| 4.80 | 0.613 | 12.50 | 0.072 | 8.00 | 0.756 | | | 10.60 | 0.844 | | | | | |
| 5.00 | 0.616 | 13.00 | 0.080 | 8.5 | 0.773 | | | 11.00 | 0.850 | | | | | |
| 5.20 | 0.618 | 13.50 | 0.085 | 9.0 | 0.790 | | | 12.00 | 0.864 | | | | | |
| 5.40 | 0.610 | 14.00 | 0.091 | 9.5 | 0.805 | | | 13.00 | 0.873 | | | | | |
| 5.60 | 0.594 | 14.50 | 0.095 | 10.0 | 0.818 | | | 14.00 | 0.884 | | | | | |
| 5.80 | 0.558 | 15.00 | 0.098 | 10.6 | 0.833 | | | | | | | | | |
| 5.90 | 0.524 | | | 11.0 | 0.842 | | | | | | | | | |
| 6.00 | 0.516 | | | 11.5 | 0.850 | | | | | | | | | |

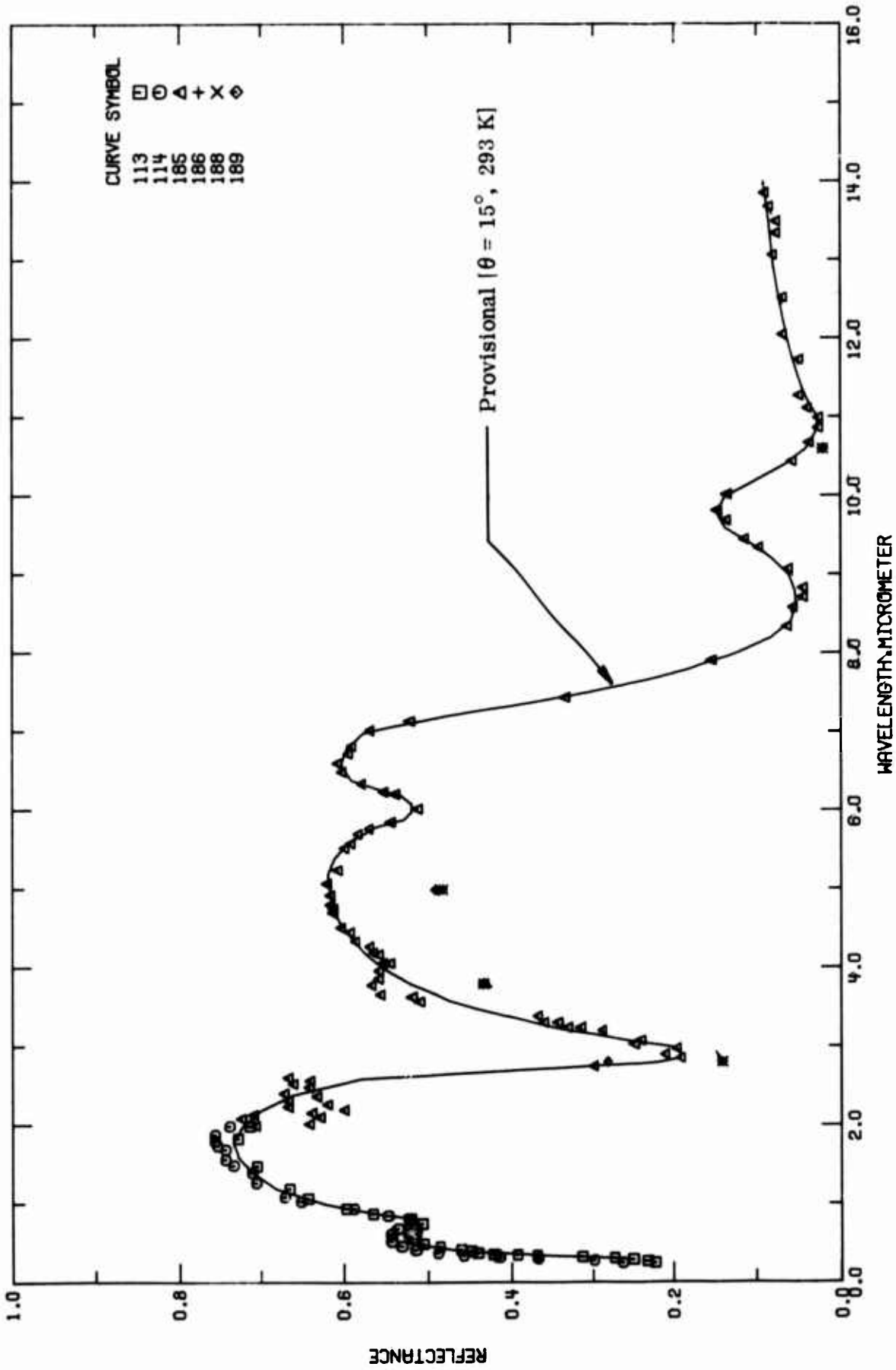


FIGURE 1-16. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

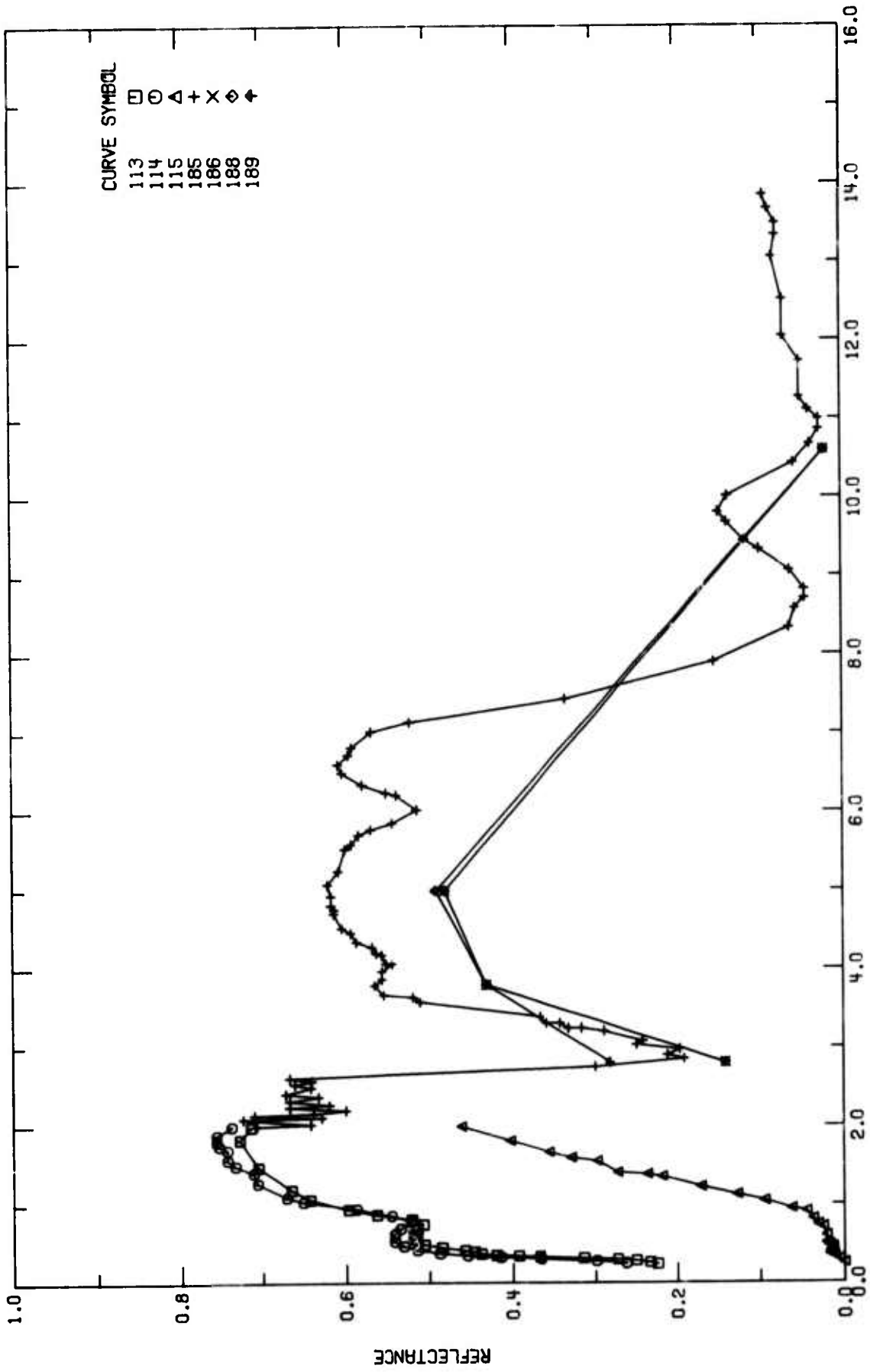


FIGURE 1.17. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

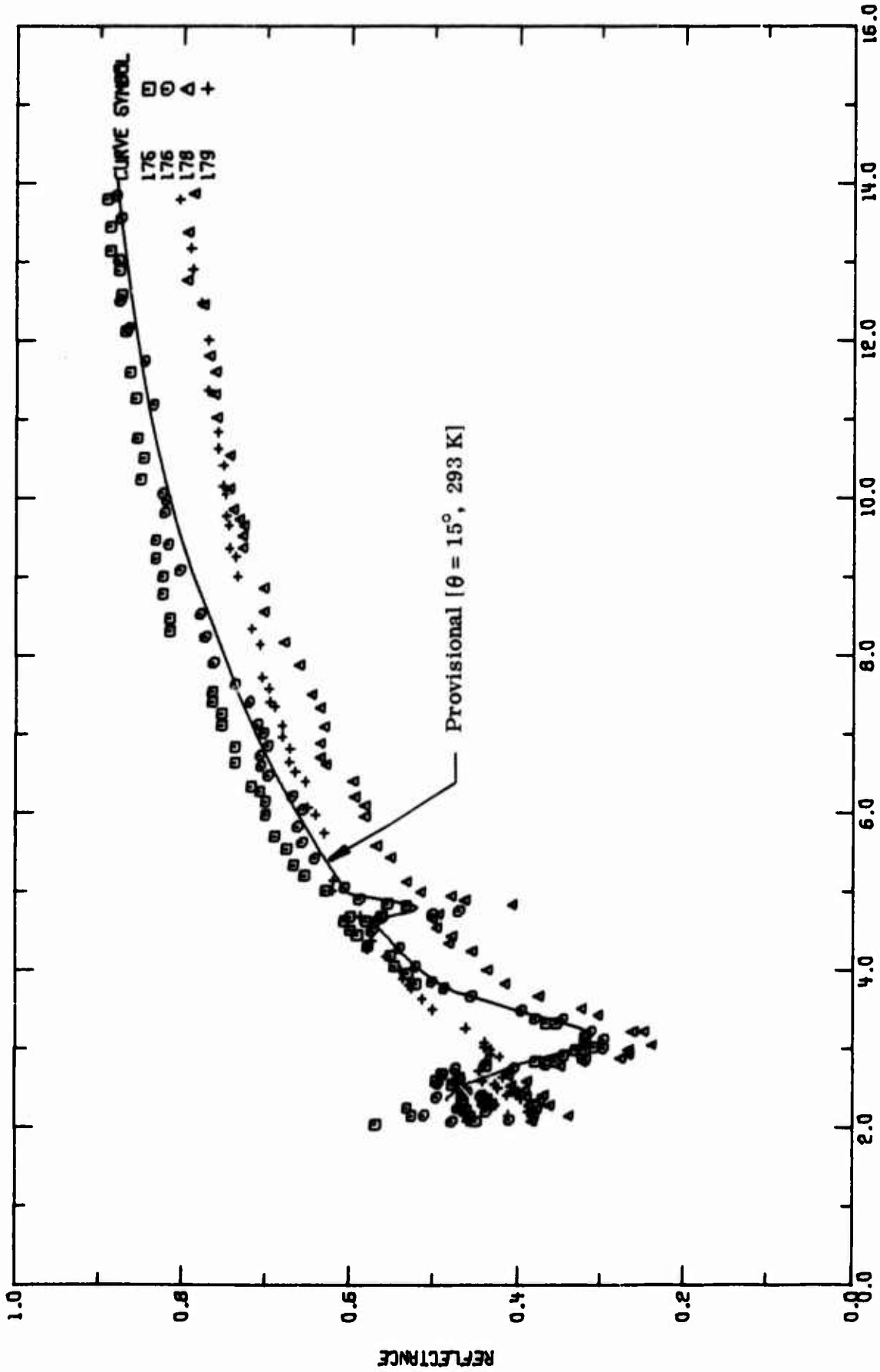
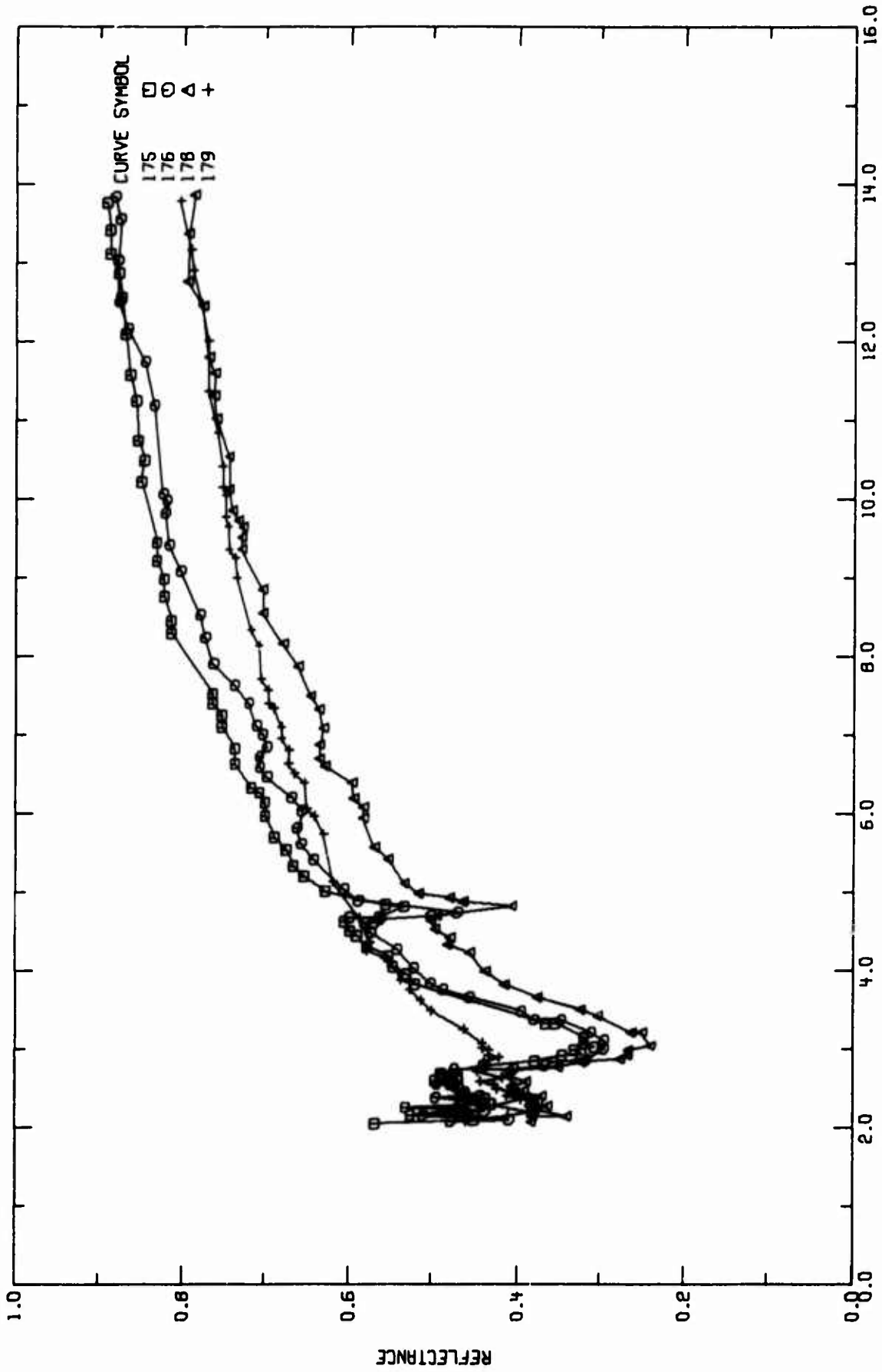


FIGURE 1-18. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).



WAVELENGTH, MICROMETER

FIGURE 1-19. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

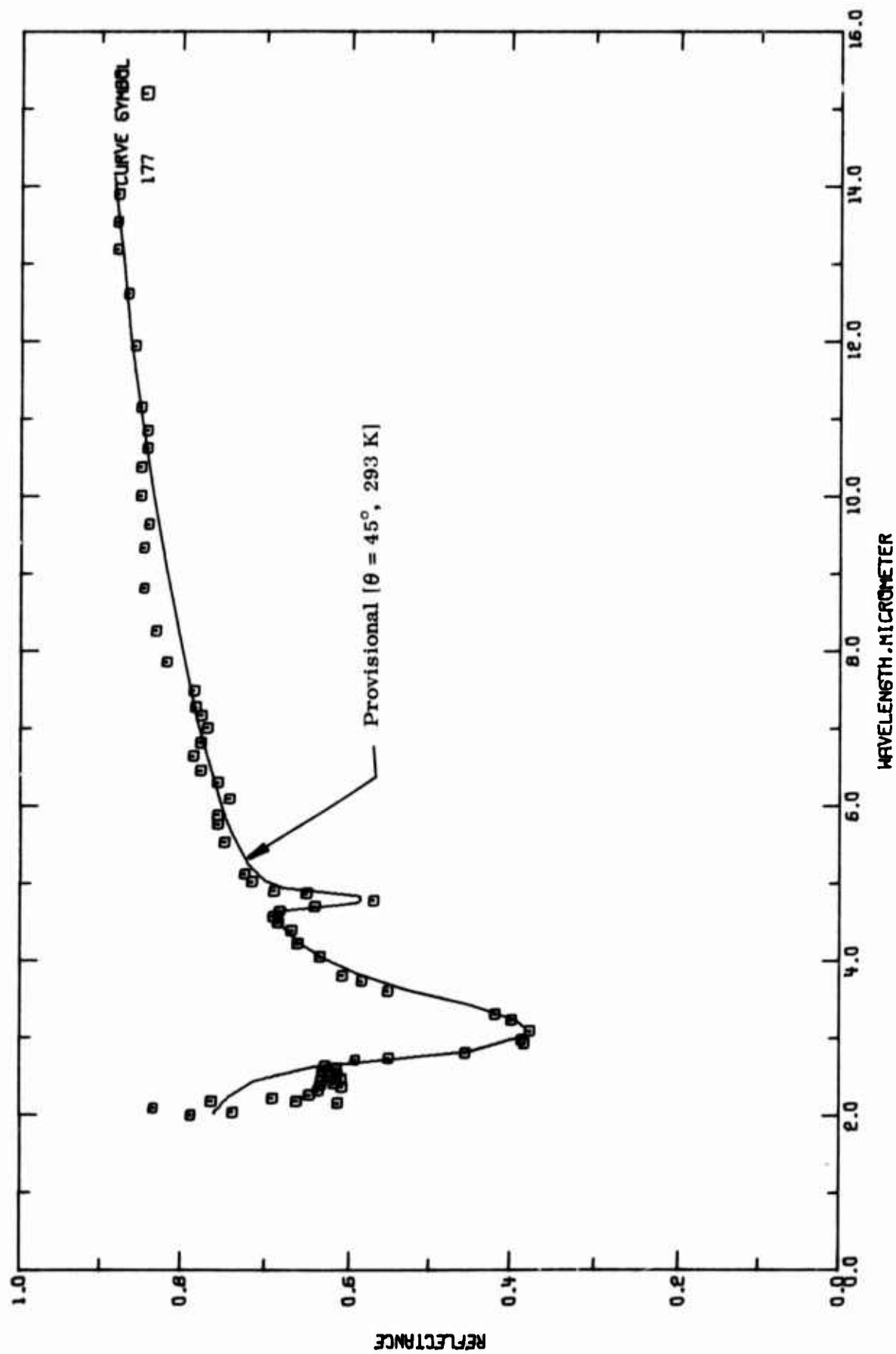


FIGURE 1-20. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

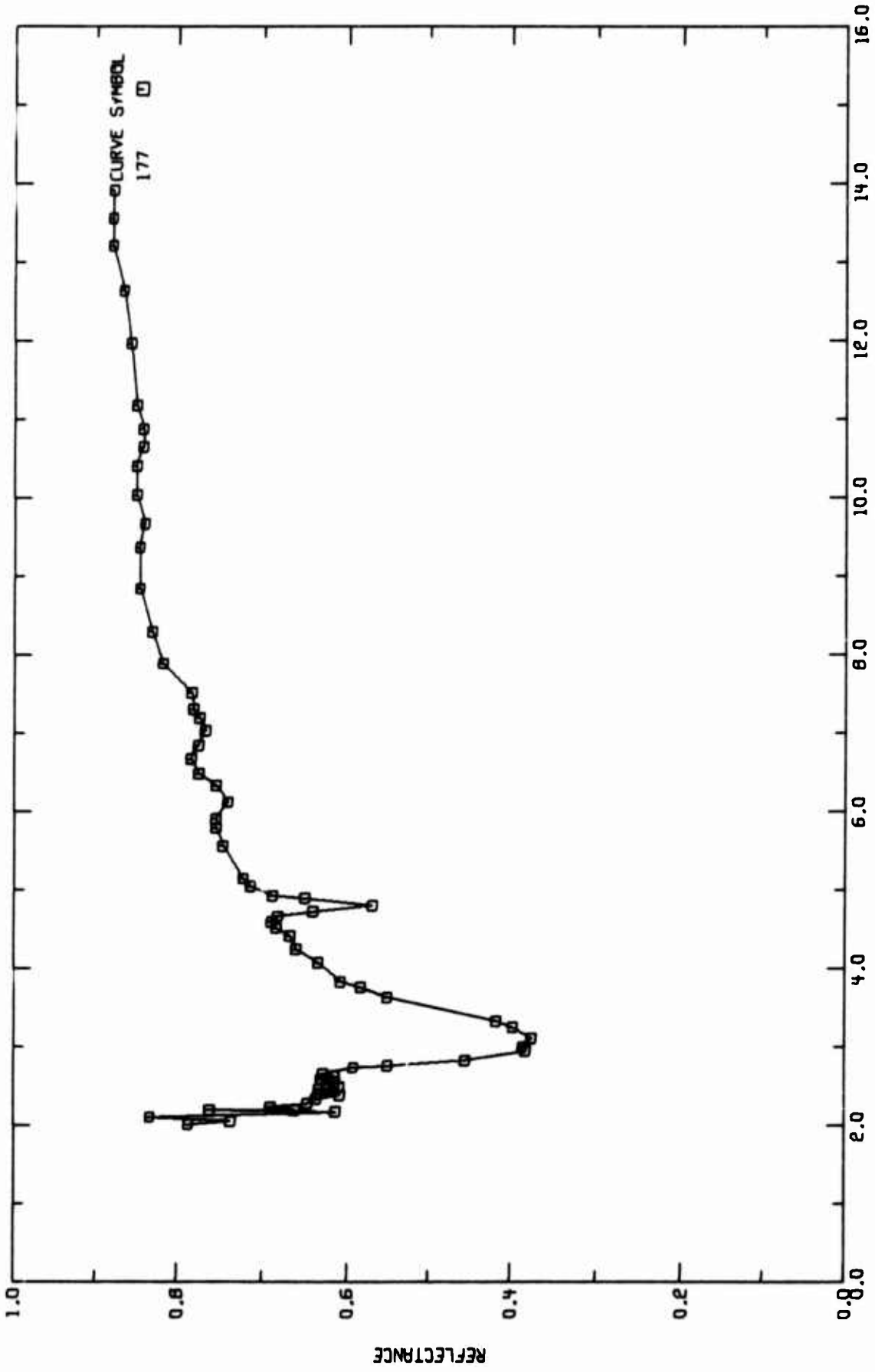


FIGURE 1-21. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGLULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, $^{\circ}\text{K}$ | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------------|------|---------------------------------|---------------------------------------|-----------------------------------|--|
| 1 | Aronson, J.R. and McLinden, H.G. | 1964 | 20.0-99.0 | 8.5 \pm 1 | Aluminum Alloy 2024 | Samples were 0.02 meter disks of a few mm thickness; measurement made by Perkin-Elmer Model 201-C spectrometer while temperature measured by carbon composition resistor; reflectance measured relative to Aluminum 2024 at room temperature; smooth values extracted from figure; $\theta = 45^{\circ}$, reported error $\pm 5\%$. |
| 2 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 3 | Specimen was 15/16" x 1" x 1" with symmetric V-grooves cut into one 15/16" x 1" face; grooved surfaces made for this study with ruling machine of type used by Bausch and Lomb, Inc.; specifications of grooved profiles and angle as reported by manufacturer, valley to valley distance (w), 80 μm , peak to valley height (h), 23.4 μm , and angle between faces, 89.9'; source used is G.E. 30A/T20/4 tungsten ribbon strip lamp enclosed in H ₂ O cooled shield, monochromator used was Perkin-Elmer Model 83, detectors used were RCA 1P28 photomultiplier tube for visible (0.2-0.7 μ) and Perkin-Elmer lead sulfide photoconducting cell for near infrared (0.4-2.8 μ); incident beam and viewing path was perpendicular to groove; angle θ' said to be negative if measured in same direction from normal as θ ; θ' uncertainty $\pm 1^{\circ}$; reference was standard mirror; specimen appeared "bright and shining" to eye; measured temperature specified as room temperature, 293 K assigned; $\theta = 75^{\circ}$, $\theta' = -15.25^{\circ}$, reported error $\pm 0.05\%$. The above specimen except $\theta = 15^{\circ}$, $\theta' = -74.5^{\circ}$. |
| 3 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 3 | The above specimen except $\theta = 75^{\circ}$, $\theta' = -15.5^{\circ}$. |
| 4 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 3 | Similar to the above specimen except w = 25 μm , h = 12.7 μm , the angle of the V-groove is 89.9'. |
| 5 | Zipin, F.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 4 | The above specimen except $\theta = 15^{\circ}$, $\theta' = -74.5^{\circ}$. |
| 6 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 4 | Similar to the above specimen except w = 16.67 μm , h = 2.19 μm , the angle of the V-groove is 150.30', incident and observation angle as specified, different wavelengths; $\theta = 45^{\circ}$. |
| 7 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta' = 38^{\circ}$. |
| 8 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | |
| 9 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | Similar to the above specimen except w = 83.33 μm , h = 24.4 μm , the angle of the V-groove is 119.15', $\theta = 75^{\circ}$, $\theta' = 15^{\circ}$. |
| 10 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta = 60^{\circ}$, $\theta' = 0^{\circ}$. |
| 11 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta = 45^{\circ}$, $\theta' = 13^{\circ}$. |
| 12 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta = 30^{\circ}$, $\theta' = 27^{\circ}$. |
| 13 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta = 15^{\circ}$, $\theta' = -74.5^{\circ}$. |
| 14 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta' = -42.5^{\circ}$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--------------------|------|---------------------------------|----------------------|-----------------------------------|---|
| 15 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta=75^\circ$, $\theta'=14.5^\circ$. |
| 16 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta=45^\circ$, $\theta'=14^\circ$. |
| 17 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta=15^\circ$, $\theta'=74^\circ$. |
| 18 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 7 | The above specimen except $\theta'=42^\circ$. |
| 19 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | Similar to the above specimen except $w = 41.67 \mu\text{m}$, $h = 12.2 \mu\text{m}$, the angle of the V-groove is $119^\circ 20'$; $\theta=75^\circ$, $\theta'=15^\circ$. |
| 20 | T39074 Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=60^\circ$, $\theta'=0^\circ$. |
| 21 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=45^\circ$, $\theta'=14^\circ$. |
| 22 | T39074 Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=30^\circ$, $\theta'=28^\circ$. |
| 23 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=15^\circ$, $\theta'=74.5^\circ$. |
| 24 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta'=43^\circ$. |
| 25 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=75^\circ$, $\theta'=14.5^\circ$. |
| 26 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=45^\circ$, $\theta'=15.5^\circ$. |
| 27 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta=15^\circ$, $\theta'=73^\circ$. |
| 28 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 8 | The above specimen except $\theta'=42^\circ$. |
| 29 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | Similar to the above specimen except $w = 16.67 \mu\text{m}$, $h = 4.9 \mu\text{m}$, the angle of the V-groove is $119^\circ 6'$; $\theta=60^\circ$, $\theta'=0.5^\circ$. |
| 30 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | The above specimen except $\theta=45^\circ$, $\theta'=16.5^\circ$. |
| 31 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | The above specimen except $\theta=30^\circ$, $\theta'=32.5^\circ$. |
| 32 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | The above specimen except $\theta=15^\circ$, $\theta'=72.5^\circ$. |
| 33 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 9 | The above specimen except $\theta'=49.5^\circ$. |
| 34 | T39074 Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | Similar to the above specimen except $w = 200 \mu\text{m}$, $h = 26.5 \mu\text{m}$, the angle of the V-groove is $150^\circ 16'$; $\theta=75^\circ$, $\theta'=45^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μ m | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------|------|---------------------------|----------------------|-----------------------------------|--|
| 35 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | The above specimen except $\theta=60^\circ$, $\theta'=60^\circ$. |
| 36 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | The above specimen except $\theta'=30^\circ$. |
| 37 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | The above specimen except $\theta=45^\circ$, $\theta'=74.5^\circ$. |
| 38 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | The above specimen except $\theta'=15^\circ$. |
| 39 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | The above specimen except $\theta=30^\circ$, $\theta'=60^\circ$. |
| 40 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 11 | The above specimen except $\theta=15^\circ$, $\theta'=45^\circ$. |
| 41 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | Similar to the above specimen except $w=100 \mu$ m, $h=13.25 \mu$ m, the angle of the V-groove is $150^\circ 17'$; $\theta=75^\circ$, $\theta'=45^\circ$. |
| 42 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | The above specimen except $\theta=60^\circ$, $\theta'=60^\circ$. |
| 43 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | The above specimen except $\theta'=30^\circ$. |
| 44 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | The above specimen except $\theta=45^\circ$, $\theta'=74.5^\circ$. |
| 45 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | The above specimen except $\theta'=15^\circ$. |
| 46 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | The above specimen except $\theta=30^\circ$, $\theta'=60^\circ$. |
| 47 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 12 | The above specimen except $\theta=15^\circ$, $\theta'=45^\circ$. |
| 48 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | Similar to the above specimen except $w=41.67 \mu$ m, $h=5.46 \mu$ m, the angle of the V-groove is $150^\circ 29'$; $\theta=44.5^\circ$. |
| 49 T39074 | Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=75^\circ$, $\theta'=45.75^\circ$. |
| 50 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=60^\circ$, $\theta'=60^\circ$. |
| 51 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta'=31^\circ$. |
| 52 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=45^\circ$, $\theta'=75^\circ$. |
| 53 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta'=16^\circ$. |
| 54 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=30^\circ$, $\theta'=60^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μ m | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------|------|---------------------------|----------------------|-----------------------------------|--|
| 55 T39074 | Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=15^\circ$, $\theta'=45^\circ$. |
| 56 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=75^\circ$, $\theta'=59^\circ$. |
| 57 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=55^\circ$. |
| 58 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=52^\circ$. |
| 59 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=48.5^\circ$. |
| 60 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=45.5^\circ$. |
| 61 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=42.5^\circ$. |
| 62 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=39.5^\circ$. |
| 63 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=37.5^\circ$. |
| 64 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=34.5^\circ$. |
| 65 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=60^\circ$, $\theta'=64.5^\circ$. |
| 66 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=56.5^\circ$. |
| 67 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=53^\circ$. |
| 68 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=50^\circ$. |
| 69 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=46.5^\circ$. |
| 70 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=41^\circ$. |
| 71 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=35.5^\circ$. |
| 72 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=33^\circ$. |
| 73 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=30.5^\circ$. |
| 74 T39074 | Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 13 | The above specimen except $\theta=28.5^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--------------------|------|---------------------------------|----------------------|-----------------------------------|--|
| 75 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | Similar to the above specimen except $w = 16.67 \mu\text{m}$, $h = 2.19 \mu\text{m}$, the angle of the V-groove is $150^\circ 30'$; $\theta = 23.5^\circ$. |
| 76 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 66.5^\circ$. |
| 77 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 62.5^\circ$. |
| 78 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 58.5^\circ$. |
| 79 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 55.5^\circ$. |
| 80 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 53.5^\circ$. |
| 81 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 50.5^\circ$. |
| 82 | T39074 Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 43^\circ$. |
| 83 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 39.5^\circ$. |
| 84 | T39074 Zipin, R.B. | 1965 | 0.5, 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 36^\circ$. |
| 85 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 32.5^\circ$. |
| 86 | T39074 Zipin, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 30.5^\circ$. |
| 87 | T39074 Zipin, P.E. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 28.25^\circ$. |
| 88 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 75^\circ$, $\theta' = 60.5^\circ$. |
| 89 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 51.25^\circ$. |
| 90 | T39074 Zipin, R.E. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 43.5^\circ$. |
| 91 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 36.5^\circ$. |
| 92 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 60^\circ$, $\theta' = 73.5^\circ$. |
| 93 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 59.5^\circ$. |
| 94 | T39074 Zipin, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta = 50^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-----------------------------------|--|
| 95 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=30^\circ$. |
| 96 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=24^\circ$. |
| 97 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=45^\circ$, $\theta'=75^\circ$. |
| 98 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=63^\circ$. |
| 99 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=52.5^\circ$. |
| 100 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=38^\circ$. |
| 101 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=31^\circ$. |
| 102 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=25.9^\circ$. |
| 103 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=20^\circ$. |
| 104 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=14.5^\circ$. |
| 105 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=9^\circ$. |
| 106 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=30^\circ$, $\theta'=68.5^\circ$. |
| 107 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=59^\circ$. |
| 108 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=51^\circ$. |
| 109 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=42.5^\circ$. |
| 110 T39074 | Zipka, R.B. | 1965 | 1.5 | 293 | Aluminum Alloy 2024T-4, Sample 14 | The above specimen except $\theta=15^\circ$, $\theta'=52^\circ$. |
| 111 T39074 | Zipka, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 5 | Similar to the above specimen except $w = 10 \mu\text{m}$, $b = 5 \mu\text{m}$, the angle of the V-groove is 90° ; grooves made by burnishing with weighted diamond; specimen did not appear "bright and shining" to eye; $\theta=75^\circ$, $\theta'=20^\circ$, reported error $\pm 0.05\%$. |
| 112 T39074 | Zipka, R.B. | 1965 | 0.5 | 293 | Aluminum Alloy 2024T-4, Sample 5 | The above specimen except $\theta=15^\circ$, $\theta'=74.5^\circ$. |
| 113 T43493 | Bevans, J.T., Brown, G.L., Luedke, E.E., W.D., Nelson, K.E., and Russell, D.A. | 1962 | 0.25-2.0 | 303 | Aluminum Alloy 2024T-4, Sample 5 | Sample materials prepared by Anadite Corp., South Gate, Calif.; sample discs were 19 mm in diameter; soft sulfuric acid anodize; 30 μm thick irradiation treatment; source used was GE B-H6 Mercury Arc Lamp at level of $5.5 \times 10^5 \text{ Watt/meter}^2$; spectral reflectance measured with either integrating sphere reflectometer or Beckman DK-2A modified reflectometer; data extracted from smooth curve; temperature not monitored for each sample, range 294-311, average temperature of 303 used; $\theta=15^\circ$, $\theta'=24^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 114 T43493 | Bevans, J. T., Brown, G. L., Luedke, E. E., Millue, W. D., Nelson, K. E., and Russell, D. A. | 1962 | 0.25-2.0 | 303 | | Similar to the above specimen except measurements made after exposure period of 2.2 hr at atm pressure. |
| 115 T43493 | Bevans, J. T., et al. | 1962 | 0.25-2.0 | 303 | | Similar to the above specimen except measurements made after exposure period of 96 hr at pressure of 10^{-6} Torr. |
| 116 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Specimen 2.22 cm discs, 0.16 to 0.32 cm thick; sample surface prepared by standard metallographic techniques, average horizontal peak to peak distance is 30 μm , groove depth (average displacement from mean surface line) is 0.40 μm , integrating sphere used with PbS detector; reference standard MgO; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta=20^\circ$, $\omega^2=2g$. |
| 117 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=30^\circ$. |
| 118 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=40^\circ$. |
| 119 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=50^\circ$. |
| 120 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=60^\circ$. |
| 121 T29563 | Eberhart, R. C. | 1960 | 1.2, 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=70^\circ$. |
| 122 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except data extracted from smooth curve; $\theta=15^\circ$. |
| 123 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=20^\circ$. |
| 124 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=25^\circ$. |
| 125 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=30^\circ$. |
| 126 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=35^\circ$. |
| 127 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=40^\circ$. |
| 128 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=45^\circ$. |
| 129 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=50^\circ$. |
| 130 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=55^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 131 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=60^\circ$. |
| 132 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=65^\circ$. |
| 133 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Similar to the above specimen except $\theta=70^\circ$. |
| 134 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except average horizontal peak to peak distance, 7 μm , groove depth, 3.18 μm ; sample surface prepared with sandpaper; data extracted from smooth curve; $\theta=15^\circ$. |
| 135 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=20^\circ$. |
| 136 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=25^\circ$. |
| 137 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=30^\circ$. |
| 138 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=35^\circ$. |
| 139 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=40^\circ$. |
| 140 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=45^\circ$. |
| 141 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=50^\circ$. |
| 142 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=55^\circ$. |
| 143 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=60^\circ$. |
| 144 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=65^\circ$. |
| 145 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=70^\circ$. |
| 146 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=75^\circ$. |
| 147 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 1 | Similar to the above specimen except $\theta=80^\circ$. |
| 148 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except average horizontal peak to peak distance, 10 μm , groove depth, 4.52 μm ; sample surface prepared with sandpaper; $\theta=15^\circ$. |
| 149 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=20^\circ$. |
| 150 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=25^\circ$. |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 151 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=30^\circ$. |
| 152 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=35^\circ$. |
| 153 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=40^\circ$. |
| 154 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=45^\circ$. |
| 155 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=50^\circ$. |
| 156 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=55^\circ$. |
| 157 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=60^\circ$. |
| 158 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=65^\circ$. |
| 159 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=70^\circ$. |
| 160 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=75^\circ$. |
| 161 T29563 | Eberhart, R.C. | 1960 | 1.2 | 293 | Aluminum 24ST, Grade 2 | Similar to the above specimen except $\theta=80^\circ$. |
| 162 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Polished; Beckman DK2 spectrometer integrating sphere used for measurement; MgO reference standard; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta=20^\circ$, $\omega=27^\circ$. Similar to the above specimen except $\theta=30^\circ$. |
| 163 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=40^\circ$. |
| 164 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=50^\circ$. |
| 165 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=60^\circ$. |
| 166 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=70^\circ$. |
| 167 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Roughened sample; surface roughened with sandpaper, scratches parallel; coarse structure - peak to peak depth 6.35 μm , spacing, 34 μm , fine structure - peak to peak depth, 1 μm ; Beckman DK2 spectrometer integrating sphere used for measurement; MgO reference standard; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta=20^\circ$, $\omega=27^\circ$. |
| 168 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence). (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|---------------------------------|--|
| 169 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=30^\circ$. |
| 170 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=40^\circ$. |
| 171 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=50^\circ$. |
| 172 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=60^\circ$. |
| 173 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=70^\circ$. |
| 174 T19294 | Rolling, R.E. and Seban, R.A. | 1960 | 1.2 | 293 | Aluminum 24ST | Similar to the above specimen except $\theta=80^\circ$. |
| 175 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. A-1 | Specimen brush-anodized; sample thickness 101.6×10^{-3} cm; samples prepared by Organic Chemistry Laboratory of Dept. 256; measurements made with a Dunn Associates ellipsoidal mirror reflectometer; measurement temperature specified as ambient temperature, 293 K assigned; data extracted from smooth curve; relative reflectance reported, multiplied by 0.95 to convert to absolute (gold reference standard used); $\theta=15^\circ$, $\omega=2\theta$; chromate conversion coating. The above specimen; reported values different from the values of above specimen for unknown reason. |
| 176 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. A-1 | The above specimen except $\theta=45^\circ$. |
| 177 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. A-1 | The above specimen; reported values different from the values of above specimen for unknown reason; $\theta=15^\circ$. |
| 178 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. A-1 | The above specimen except sample heat treated by heating to 644 K for 1 hr in air. |
| 179 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. A-1 | Polished; sample thickness 99×10^{-3} cm; samples prepared by Organic Chemistry Laboratory of Dept. 256; measurements made with a Dunn Associates ellipsoidal mirror reflectometer; measurement temperature specified as ambient temperature, 293 K assigned; data extracted from smooth curve; relative reflectance reported multiplied by 0.95 to convert to absolute (gold reference standard used); $\theta=15^\circ$, $\omega=2\theta$. |
| 180 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2-14.7 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen; reported values different from the values of above specimen for unknown reason; data extracted from table. |
| 181 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen except $\theta=45^\circ$. |
| 182 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen; reported values different from the values of above specimen for unknown reason; data extracted from table; $\theta=15^\circ$. |
| 183 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | The above specimen except sample heat treated by heating to 644 K for 1 hr in air. |
| 184 A00001 | Grimm, F.C. and Farnin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T81 Alclad, Sample No. B-1 | |

TABLE 1-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 185 A00001 | Grimm, F.C. and Fannin, E.R. | 1972 | 2-14.7 | 293 | 2024-T851 Al, Sample No. C-1 | Anodized with sulfuric acid; sample thickness ~ 0.254 cm; samples prepared by Organic Chemistry Laboratory of Dept. 256; measurements made with a Duann Associates ellipsoidal mirror reflectometer; measurement temperature specified as ambient temperature, 293 K assigned; data extracted from smooth curve; relative reflectance reported multiplied by 0.95 to convert to absolute (gold reference standard used); $\theta=15^\circ$, $\omega'=27^\circ$. |
| 186 A00001 | Grimm, F.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T851 Al, Sample No. C-1 | The above specimen; reported value different from the values of above specimen for unknown reason. |
| 187 A00001 | Grimm, F.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T851 Al, Sample No. C-1 | The above specimen except $\theta=45^\circ$. |
| 188 A00001 | Grimm, F.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T851 Al, Sample No. C-1 | The above specimen; reported values different from the values of above specimen for unknown reason; data extracted from table; $\theta=15^\circ$. |
| 189 A00001 | Grimm, F.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | 2024-T851 Al, Sample No. C-1 | The above specimen except sample heat treated by heating to 644 K for 1 hr in air. |
| 190 T73502 | Bowman, R.L., Jack, J.R., and Spisz, E.W. | 1973 | 0.35-2.0 | 293 | 2024 T4 Aluminum | Highly polished surface; measurements made in air with Gier-Dipple magnesium oxide coated integrating sphere reflectometer; data extracted from smooth curve; measured temperature specified as room temperature, 293 K assigned; $\theta=15^\circ$, $\omega'=27^\circ$. |
| 191 T73502 | Bowman, R.L., et al. | 1973 | 0.35-1.1 | 293 | 2024 T4 Aluminum | Similar to the above specimen except surface had diffuse finish provided by glass-bead blasting the surface. |

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|--|
| CURVE 1* | | CURVE 6* | | CURVE 14* | | CURVE 22* | | CURVE 30* | | CURVE 37 (CONT.)* | | | | | | | | | | |
| T = 0.5 | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | | | | | | | | | |
| 20.0 | 0.057 | 0.5 | 0.166 | 0.5 | 0.061 | 0.5 | 0.124 | 0.5 | 0.039 | 1.5 | 0.295 | | | | | | | | | |
| 20.9 | 0.066 | | | | | 1.5 | 0.000 | | | | | | | | | | | | | |
| 22.0 | 0.908 | CURVE 7* | | CURVE 15* | | | | CURVE 23* | | CURVE 31* | | | | | | | | | | |
| 23.7 | 0.934 | T = 293. | | T = 293. | | | | T = 293. | | T = 293. | | | | | | | | | | |
| 24.9 | 0.962 | | | | | | | | | | | | | | | | | | | |
| 25.0 | 0.962 | 1.5 | 0.20 | 1.5 | 0.437 | | | | | 0.5 | 0.0701 | | | | | | | | | |
| 27.4 | 0.947 | | | | | | | | | | | | | | | | | | | |
| 29.0 | 0.967 | CURVE 8* | | CURVE 16* | | | | CURVE 24* | | CURVE 32* | | | | | | | | | | |
| 33.0 | 0.967 | T = 293. | | T = 293. | | | | T = 293. | | T = 293. | | | | | | | | | | |
| 36.0 | 0.955 | | | | | | | | | | | | | | | | | | | |
| 40.0 | 0.960 | 1.5 | 0.001 | 1.5 | 0.0676 | | | 0.5 | 0.049 | 0.5 | 0.0995 | | | | | | | | | |
| 50.0 | 0.945 | | | | | | | | | | | | | | | | | | | |
| 62.1 | 0.965 | CURVE 9* | | CURVE 17* | | | | CURVE 25* | | CURVE 33* | | | | | | | | | | |
| 99.0 | 0.970 | T = 293. | | T = 293. | | | | T = 293. | | T = 293. | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| CURVE 2* | | 0.5 | 0.95 | 1.5 | 0.136 | | | 1.5 | 0.254 | 0.5 | 0.265 | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | | | | | | |
| 0.5 | 0.707 | CURVE 10* | | CURVE 18* | | | | | | | | | | | | | | | | |
| | | T = 293. | | T = 293. | | | | | | | | | | | | | | | | |
| CURVE 3* | | 0.5 | 0.915 | 1.5 | 0.05E | | | 0.5 | 0.024 | 0.5 | 0.024 | | | | | | | | | |
| T = 293. | | 1.5 | 0.75 | | | | | 1.5 | 0.0411 | 1.5 | 0.075 | | | | | | | | | |
| 0.5 | 0.223 | | | | | | | | | | | | | | | | | | | |
| 1.5 | 0.137 | CURVE 11* | | CURVE 19* | | | | CURVE 27* | | CURVE 35* | | | | | | | | | | |
| | | T = 293. | | T = 293. | | | | T = 293. | | T = 293. | | | | | | | | | | |
| CURVE 4* | | 0.5 | 0.095 | 0.5 | 0.355 | | | 1.5 | 0.070 | 0.5 | 0.164 | | | | | | | | | |
| T = 293. | | | | | | | | | | 1.5 | 0.13 | | | | | | | | | |
| 1.5 | 0.310 | CURVE 12* | | CURVE 20* | | | | CURVE 28* | | CURVE 36* | | | | | | | | | | |
| | | T = 293. | | T = 293. | | | | | | T = 293. | | | | | | | | | | |
| CURVE 5* | | 0.5 | 0.154 | 0.5 | 0.47 | | | 1.5 | 0.0335 | 0.5 | 0.500 | | | | | | | | | |
| T = 293. | | 1.5 | 0.166 | 1.5 | 0.46 | | | | | 1.5 | 0.625 | | | | | | | | | |
| 0.5 | 0.510 | CURVE 13* | | CURVE 21* | | | | CURVE 29* | | CURVE 37* | | | | | | | | | | |
| | | T = 293. | | T = 293. | | | | T = 293. | | T = 293. | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | 0.5 | 0.065 | 0.5 | 0.065 | | | 0.5 | 0.405 | 0.5 | 0.315 | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |
| | | | | | | | | | | | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm : TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-----------------------|--------|-----------------------|--------|-----------------------|--------|-----------------------|--------|-----------------------|--------|-----------------------|--------|
| CURVE 44* T = 293. | | CURVE 51* T = 293. | | CURVE 59* T = 293. | | CURVE 67* T = 293. | | CURVE 75* T = 293. | | CURVE 83* T = 293. | |
| 0.5 0.280 | | 0.5 0.55 | | 1.5 0.510 | | 1.5 0.035 | | 0.5 0.025 | | 0.5 0.0271 | |
| 1.5 0.211 | | CURVE 52* T = 293. | | CURVE 60* T = 293. | | CURVE 68* T = 293. | | CURVE 76* T = 293. | | CURVE 84* T = 293. | |
| CURVE 45* T = 293. | | 0.5 0.235 | | 1.5 0.640 | | 1.5 0.020 | | 0.5 0.015 | | 0.5 0.043 | |
| 0.5 0.615 | | CURVE 53* T = 293. | | CURVE 61* T = 293. | | CURVE 69* T = 293. | | CURVE 77* T = 293. | | 0.5 0.31 | |
| 1.5 0.505 | | 0.5 0.465 | | 1.5 0.376 | | 1.5 0.015 | | 0.5 0.0296 | | CURVE 85* T = 293. | |
| CURVE 46* T = 293. | | CURVE 54* T = 293. | | CURVE 62* T = 293. | | CURVE 70* T = 293. | | CURVE 78* T = 293. | | 0.5 0.245 | |
| 0.5 0.300 | | 0.5 0.305 | | 1.5 0.0475 | | 1.5 0.020 | | 0.5 0.0610 | | CURVE 86* T = 293. | |
| 1.5 0.312 | | CURVE 55* T = 293. | | CURVE 63* T = 293. | | CURVE 71* T = 293. | | CURVE 79* T = 293. | | 0.5 0.604 | |
| CURVE 47* T = 293. | | 0.5 0.337 | | 1.5 0.0150 | | 1.5 0.0675 | | 0.5 0.0334 | | CURVE 87* T = 293. | |
| 0.5 0.325 | | CURVE 56* T = 293. | | CURVE 64* T = 293. | | CURVE 72* T = 293. | | CURVE 80* T = 293. | | 0.5 0.342 | |
| CURVE 48* T = 293. | | 1.5 0.045 | | 1.5 0.0250 | | 1.5 0.354 | | 0.5 0.0303 | | CURVE 88* T = 293. | |
| 1.5 0.357 | | CURVE 57* T = 293. | | CURVE 65* T = 293. | | CURVE 73* T = 293. | | CURVE 81* T = 293. | | 1.5 0.232 | |
| CURVE 49* T = 293. | | 1.5 0.0702 | | 1.5 0.040 | | 1.5 0.442 | | 0.5 0.0109 | | CURVE 89* T = 293. | |
| 0.5 0.730 | | CURVE 58* T = 293. | | CURVE 66* T = 293. | | CURVE 74* T = 293. | | CURVE 82* T = 293. | | 1.5 0.547 | |
| CURVE 50* T = 293. | | 1.5 0.216 | | 1.5 0.050 | | 1.5 0.171 | | 0.5 0.013 | | CURVE 90* T = 293. | |
| 0.5 0.09 | | | | | | | | 1.5 0.045 | | | |
| 1.5 0.06 | | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-----------------------|--------|------------------------|--------|------------------------|--------|-----------------------|--------|-----------------------|--------|------------------------|--------|-----------|--------|
| CURVE 91* T = 293. | | CURVE 99* T = 293. | | CURVE 107* T = 293. | | CURVE 113 (CONT.) | | CURVE 114 (CONT.) | | CURVE 117* T = 293. | | | |
| 1.5 | 0.246 | 1.5 | 0.0267 | 1.5 | 0.179 | 0.404 | 0.445 | 1.690 | 0.742 | 1.2 | 0.020 | | |
| CURVE 92* T = 293. | | CURVE 100* T = 293. | | CURVE 108* T = 293. | | 0.420 | 0.484 | 1.745 | 0.752 | 1.6 | 0.910 | | |
| 1.5 | 0.075 | 1.5 | 0.023 | 1.5 | 0.036 | 0.460 | 0.505 | 1.803 | 0.755 | | | | |
| CURVE 93* T = 293. | | CURVE 101* T = 293. | | CURVE 109* T = 293. | | 0.497 | 0.514 | 1.800 | 0.755 | CURVE 110* T = 293. | | | |
| 1.5 | 0.0944 | 1.5 | 0.032 | 1.5 | 0.020 | 0.567 | 0.517 | 1.995 | 0.737 | | | | |
| CURVE 94* T = 293. | | CURVE 102* T = 293. | | CURVE 110* T = 293. | | 0.620 | 0.513 | CURVE 115 T = 303. | | | | | |
| 1.5 | 0.060 | 1.5 | 0.0167 | 1.5 | 0.030 | 0.690 | 0.519 | | | 1.2 | 0.690 | | |
| CURVE 95* T = 293. | | CURVE 103* T = 293. | | CURVE 111* T = 293. | | 0.751 | 0.506 | | | 1.6 | 0.741 | | |
| 1.5 | 0.479 | 1.5 | 0.217 | 1.5 | 0.0346 | 0.810 | 0.519 | | | | | | |
| CURVE 96* T = 293. | | CURVE 104* T = 293. | | CURVE 112* T = 293. | | 0.879 | 0.561 | | | CURVE 119* T = 293. | | | |
| 1.5 | 0.19 | 1.5 | 0.345 | 0.5 | 0.0089 | 0.946 | 0.596 | | | 1.2 | 0.662 | | |
| CURVE 97* T = 293. | | CURVE 105* T = 293. | | CURVE 113 T = 303. | | 1.071 | 0.642 | | | 1.6 | 0.731 | | |
| 1.5 | 0.097 | 1.5 | 0.110 | 0.249 | 0.260 | 1.196 | 0.664 | | | | | | |
| CURVE 98* T = 293. | | CURVE 106* T = 293. | | 0.272 | 0.290 | 1.405 | 0.704 | | | CURVE 120* T = 293. | | | |
| 1.5 | 0.053 | 1.5 | 0.0263 | 0.274 | 0.298 | 1.836 | 0.727 | | | 1.2 | 0.719 | | |
| | | | | 0.303 | 0.364 | 1.995 | 0.713 | | | 1.6 | 0.824 | | |
| | | | | 0.322 | 0.414 | CURVE 114 T = 303. | | | | | | | |
| | | | | 0.346 | 0.454 | | | | | | | | |
| | | | | 0.376 | 0.487 | | | | | | | | |
| | | | | 0.416 | 0.513 | | | | | | | | |
| | | | | 0.467 | 0.528 | | | | | | | | |
| | | | | 0.527 | 0.539 | | | | | | | | |
| | | | | 0.619 | 0.539 | | | | | | | | |
| | | | | 0.688 | 0.532 | | | | | | | | |
| | | | | 0.747 | 0.520 | | | | | | | | |
| | | | | 0.853 | 0.543 | | | | | | | | |
| | | | | 0.939 | 0.586 | | | | | | | | |
| | | | | 1.035 | 0.650 | | | | | | | | |
| | | | | 1.091 | 0.670 | | | | | | | | |
| | | | | 1.273 | 0.705 | | | | | | | | |
| | | | | 1.402 | 0.710 | | | | | | | | |
| | | | | 1.492 | 0.732 | | | | | | | | |
| | | | | 1.570 | 0.742 | | | | | | | | |
| | | | | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|------------|--------|------------|--------|------------|--------|------------|--------|------------|--------|------------|--------|
| CURVE 124* | | CURVE 132* | | CURVE 140* | | CURVE 148* | | CURVE 156* | | CURVE 164* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.671 | 1.2 | 0.638 | 1.2 | 0.633 | 1.2 | 0.612 | 1.2 | 0.512 | 1.2 | 0.782 |
| CURVE 125* | | CURVE 133* | | CURVE 141* | | CURVE 149* | | CURVE 157* | | CURVE 165* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.643 | 1.2 | 0.591 | 1.2 | 0.614 | 1.2 | 0.617 | 1.2 | 0.515 | 1.2 | 0.748 |
| CURVE 126* | | CURVE 134* | | CURVE 142* | | CURVE 150* | | CURVE 158* | | CURVE 166* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.753 | 1.2 | 0.607 | 1.2 | 0.602 | 1.2 | 0.617 | 1.2 | 0.510 | 1.2 | 0.716 |
| CURVE 127* | | CURVE 135* | | CURVE 143* | | CURVE 151* | | CURVE 159* | | CURVE 167* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.575 | 1.2 | 0.693 | 1.2 | 0.600 | 1.2 | 0.613 | 1.2 | 0.519 | 1.2 | 0.691 |
| CURVE 128* | | CURVE 136* | | CURVE 144* | | CURVE 152* | | CURVE 160* | | CURVE 168* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.524 | 1.2 | 0.694 | 1.2 | 0.604 | 1.2 | 0.604 | 1.2 | 0.520 | 1.2 | 0.698 |
| CURVE 129* | | CURVE 137* | | CURVE 145* | | CURVE 153* | | CURVE 161* | | CURVE 169* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.524 | 1.2 | 0.692 | 1.2 | 0.607 | 1.2 | 0.584 | 1.2 | 0.515 | 1.2 | 0.689 |
| CURVE 130* | | CURVE 138* | | CURVE 146* | | CURVE 154* | | CURVE 162* | | CURVE 170* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.591 | 1.2 | 0.681 | 1.2 | 0.609 | 1.2 | 0.541 | 1.2 | 0.637 | 1.2 | 0.658 |
| CURVE 131* | | CURVE 139* | | CURVE 147* | | CURVE 155* | | CURVE 163* | | CURVE 171* | |
| T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | | T = 293. | |
| 1.2 | 0.642 | 1.2 | 0.660 | 1.2 | 0.608 | 1.2 | 0.521 | 1.2 | 0.621 | 1.2 | 0.689 |

* NOT SHOWN IN FIGURE.

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | | |
|------------------------|--------|-----------|--------|-------------------|--------|-----------|--------|-------------------|--------|-----------|--------|-----------------------|--------|-----------|--------|-------------------|--------|--|--|
| CURVE 172* T = 293. | | | | CURVE 175 (CONT.) | | | | CURVE 176 (CONT.) | | | | CURVE 177 T = 293. | | | | CURVE 177 (CONT.) | | | |
| 1.2 | 0.595 | 3.81 | 0.521 | 12.84 | 0.678 | 4.49 | 0.575 | 2.00 | 0.707 | 4.90 | 0.609 | 2.07 | 0.477 | 4.40 | 0.582 | 4.40 | 0.575 | | |
| CURVE 173* T = 293. | | | | CURVE 176 | | | | CURVE 177 | | | | CURVE 178 | | | | CURVE 179 | | | |
| 1.2 | 0.603 | 3.94 | 0.532 | 13.09 | 0.688 | 4.61 | 0.582 | 2.09 | 0.410 | 5.04 | 0.606 | 2.07 | 0.410 | 4.61 | 0.582 | 4.61 | 0.582 | | |
| CURVE 174* T = 293. | | | | CURVE 177 | | | | CURVE 178 | | | | CURVE 179 | | | | CURVE 180 | | | |
| 1.2 | 0.601 | 4.03 | 0.549 | 13.39 | 0.688 | 4.61 | 0.571 | 2.15 | 0.511 | 5.41 | 0.642 | 2.15 | 0.511 | 4.61 | 0.571 | 4.61 | 0.571 | | |
| CURVE 175 | | | | CURVE 180 | | | | CURVE 181 | | | | CURVE 182 | | | | CURVE 183 | | | |
| 2.03 | 0.571 | 4.17 | 0.554 | 13.74 | 0.892 | 4.65 | 0.564 | 2.20 | 0.439 | 5.61 | 0.657 | 2.20 | 0.439 | 4.65 | 0.564 | 4.65 | 0.564 | | |
| 2.07 | 0.458 | 4.29 | 0.580 | 14.09 | 0.692 | 4.70 | 0.501 | 2.24 | 0.470 | 5.81 | 0.662 | 2.24 | 0.470 | 4.70 | 0.501 | 4.70 | 0.501 | | |
| 2.14 | 0.527 | 4.43 | 0.592 | 14.72 | 0.905 | 4.74 | 0.489 | 2.28 | 0.465 | 6.03 | 0.656 | 2.28 | 0.465 | 4.74 | 0.489 | 4.74 | 0.489 | | |
| 2.21 | 0.461 | 4.49 | 0.600 | CURVE 176 | | | | 4.89 | 0.589 | 6.20 | 0.668 | 2.37 | 0.689 | 4.89 | 0.589 | 4.89 | 0.589 | | |
| 2.24 | 0.533 | 4.61 | 0.607 | 12.84 | 0.678 | 5.04 | 0.606 | 2.37 | 0.689 | 6.20 | 0.668 | 2.37 | 0.689 | 5.04 | 0.606 | 5.04 | 0.606 | | |
| 2.28 | 0.432 | 4.66 | 0.565 | 13.09 | 0.688 | 5.41 | 0.642 | 2.41 | 0.619 | 6.46 | 0.697 | 2.41 | 0.619 | 5.41 | 0.642 | 5.41 | 0.642 | | |
| 2.34 | 0.465 | 4.66 | 0.565 | 13.39 | 0.688 | 5.61 | 0.657 | 2.44 | 0.634 | 6.58 | 0.706 | 2.44 | 0.634 | 5.61 | 0.657 | 5.61 | 0.657 | | |
| 2.35 | 0.438 | 4.80 | 0.534 | 13.74 | 0.892 | 5.81 | 0.662 | 2.51 | 0.460 | 6.72 | 0.707 | 2.51 | 0.460 | 5.81 | 0.662 | 5.81 | 0.662 | | |
| 2.40 | 0.455 | 4.82 | 0.558 | 14.09 | 0.692 | 6.03 | 0.656 | 2.55 | 0.493 | 6.84 | 0.697 | 2.55 | 0.493 | 6.03 | 0.656 | 6.03 | 0.656 | | |
| 2.54 | 0.476 | 4.99 | 0.629 | 14.72 | 0.905 | 6.20 | 0.668 | 2.60 | 0.460 | 7.00 | 0.702 | 2.60 | 0.460 | 6.20 | 0.668 | 6.20 | 0.668 | | |
| 2.58 | 0.496 | 5.18 | 0.654 | CURVE 176 | | | | 6.46 | 0.697 | 7.11 | 0.710 | 2.61 | 0.616 | 5.18 | 0.654 | 5.18 | 0.654 | | |
| 2.62 | 0.469 | 5.31 | 0.667 | 12.84 | 0.678 | 6.46 | 0.697 | 2.67 | 0.488 | 7.11 | 0.710 | 2.61 | 0.616 | 5.31 | 0.667 | 5.31 | 0.667 | | |
| 2.67 | 0.489 | 5.52 | 0.675 | 13.09 | 0.688 | 6.58 | 0.706 | 2.74 | 0.473 | 7.39 | 0.720 | 2.61 | 0.616 | 5.52 | 0.675 | 5.52 | 0.675 | | |
| 2.77 | 0.439 | 5.68 | 0.689 | 13.39 | 0.688 | 6.72 | 0.707 | 2.79 | 0.468 | 7.62 | 0.739 | 2.72 | 0.593 | 5.68 | 0.689 | 5.68 | 0.689 | | |
| 2.83 | 0.379 | 5.95 | 0.700 | 13.74 | 0.892 | 6.84 | 0.697 | 2.83 | 0.468 | 7.89 | 0.765 | 2.74 | 0.473 | 5.95 | 0.700 | 5.95 | 0.700 | | |
| 2.90 | 0.346 | 6.12 | 0.700 | 14.09 | 0.692 | 7.00 | 0.697 | 2.86 | 0.468 | 8.00 | 0.765 | 2.90 | 0.455 | 6.12 | 0.700 | 6.12 | 0.700 | | |
| 2.92 | 0.323 | 6.25 | 0.707 | 14.72 | 0.905 | 7.11 | 0.710 | 2.90 | 0.488 | 8.51 | 0.780 | 2.93 | 0.382 | 6.25 | 0.707 | 6.25 | 0.707 | | |
| 2.97 | 0.332 | 6.31 | 0.710 | CURVE 176 | | | | 7.39 | 0.460 | 8.51 | 0.780 | 2.98 | 0.386 | 6.31 | 0.710 | 6.31 | 0.710 | | |
| 3.01 | 0.307 | 6.61 | 0.739 | 12.84 | 0.678 | 7.62 | 0.739 | 2.98 | 0.468 | 9.07 | 0.803 | 3.09 | 0.375 | 6.61 | 0.739 | 6.61 | 0.739 | | |
| 3.05 | 0.320 | 6.81 | 0.755 | 13.09 | 0.688 | 7.89 | 0.765 | 3.00 | 0.468 | 9.40 | 0.817 | 3.23 | 0.398 | 6.81 | 0.755 | 6.81 | 0.755 | | |
| 3.13 | 0.320 | 7.00 | 0.755 | 13.39 | 0.688 | 8.00 | 0.765 | 3.11 | 0.468 | 9.60 | 0.822 | 3.23 | 0.398 | 7.00 | 0.755 | 7.00 | 0.755 | | |
| 3.13 | 0.320 | 7.23 | 0.755 | 13.74 | 0.892 | 8.22 | 0.774 | 3.17 | 0.468 | 9.96 | 0.822 | 3.31 | 0.418 | 7.23 | 0.755 | 7.23 | 0.755 | | |
| 3.31 | 0.354 | 7.30 | 0.766 | 14.09 | 0.692 | 8.51 | 0.780 | 3.24 | 0.468 | 10.05 | 0.825 | 3.61 | 0.552 | 7.30 | 0.766 | 7.30 | 0.766 | | |
| 3.31 | 0.366 | 7.51 | 0.766 | 14.72 | 0.905 | 8.51 | 0.780 | 3.29 | 0.468 | 11.17 | 0.836 | 3.74 | 0.505 | 7.51 | 0.766 | 7.51 | 0.766 | | |
| | | 7.62 | 0.739 | CURVE 176 | | | | 8.22 | 0.468 | 11.72 | 0.847 | 3.81 | 0.609 | 7.62 | 0.739 | 7.62 | 0.739 | | |
| | | 7.89 | 0.765 | 12.84 | 0.678 | 9.00 | 0.817 | 3.37 | 0.468 | 12.14 | 0.867 | 4.05 | 0.636 | 7.89 | 0.765 | 7.89 | 0.765 | | |
| | | 8.00 | 0.765 | 13.09 | 0.688 | 9.40 | 0.817 | 3.37 | 0.468 | 12.48 | 0.877 | 4.22 | 0.662 | 8.00 | 0.765 | 8.00 | 0.765 | | |
| | | 8.51 | 0.780 | 13.39 | 0.688 | 9.60 | 0.822 | 3.39 | 0.468 | 13.03 | 0.876 | 4.39 | 0.669 | 8.51 | 0.780 | 8.51 | 0.780 | | |
| | | 8.51 | 0.780 | 13.74 | 0.892 | 9.96 | 0.822 | 3.40 | 0.468 | 13.53 | 0.876 | 4.49 | 0.685 | 8.51 | 0.780 | 8.51 | 0.780 | | |
| | | 9.07 | 0.803 | 14.09 | 0.692 | 10.05 | 0.825 | 3.47 | 0.468 | 14.05 | 0.896 | 4.57 | 0.698 | 9.07 | 0.803 | 9.07 | 0.803 | | |
| | | 9.40 | 0.817 | 14.72 | 0.905 | 10.05 | 0.825 | 3.47 | 0.468 | 14.39 | 0.912 | 4.70 | 0.642 | 9.40 | 0.817 | 9.40 | 0.817 | | |
| | | 9.60 | 0.822 | CURVE 176 | | | | 10.80 | 0.468 | 14.67 | 0.915 | | | 9.60 | 0.822 | 9.60 | 0.822 | | |
| | | 9.96 | 0.822 | 12.84 | 0.678 | 11.17 | 0.836 | 3.51 | 0.468 | | | | | 9.96 | 0.822 | 9.96 | 0.822 | | |
| | | 10.05 | 0.825 | 13.09 | 0.688 | 11.72 | 0.847 | 3.51 | 0.468 | | | | | 10.05 | 0.825 | 10.05 | 0.825 | | |
| | | 11.17 | 0.836 | 13.39 | 0.688 | 12.14 | 0.867 | 3.57 | 0.468 | | | | | 11.17 | 0.836 | 11.17 | 0.836 | | |
| | | 11.72 | 0.847 | 13.74 | 0.892 | 12.48 | 0.877 | 3.57 | 0.468 | | | | | 11.72 | 0.847 | 11.72 | 0.847 | | |
| | | 12.14 | 0.867 | 14.09 | 0.692 | 13.03 | 0.876 | 3.59 | 0.468 | | | | | 12.14 | 0.867 | 12.14 | 0.867 | | |
| | | 12.48 | 0.877 | 14.72 | 0.905 | 13.53 | 0.876 | 3.66 | 0.468 | | | | | 12.48 | 0.877 | 12.48 | 0.877 | | |
| | | 13.03 | 0.876 | CURVE 176 | | | | 13.80 | 0.468 | | | | | 13.03 | 0.876 | 13.03 | 0.876 | | |
| | | 13.53 | 0.876 | 12.84 | 0.678 | 14.05 | 0.896 | 3.66 | 0.468 | | | | | 13.53 | 0.876 | 13.53 | 0.876 | | |
| | | 14.05 | 0.896 | 13.09 | 0.688 | 14.39 | 0.912 | 3.66 | 0.468 | | | | | 14.05 | 0.896 | 14.05 | 0.896 | | |
| | | 14.39 | 0.912 | 13.39 | 0.688 | 14.67 | 0.915 | 3.76 | 0.468 | | | | | 14.39 | 0.912 | 14.39 | 0.912 | | |
| | | 14.67 | 0.915 | 13.74 | 0.892 | 14.67 | 0.915 | 3.84 | 0.468 | | | | | 14.67 | 0.915 | 14.67 | 0.915 | | |
| | | 14.67 | 0.915 | 14.09 | 0.692 | 14.67 | 0.915 | 4.03 | 0.468 | | | | | 14.67 | 0.915 | 14.67 | 0.915 | | |
| | | 4.03 | 0.522 | 14.72 | 0.905 | 4.03 | 0.522 | 4.27 | 0.468 | | | | | 4.03 | 0.522 | 4.03 | 0.522 | | |
| | | 4.27 | 0.543 | CURVE 176 | | | | 4.27 | 0.543 | | | | | 4.27 | 0.543 | 4.27 | 0.543 | | |

* NOT SHOWN IN FIGURE.

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| CURVE 178 (CONT.) | | CURVE 178 (CONT.) | | CURVE 179 (CONT.) | | CURVE 179 (CONT.) | | CURVE 179 (CONT.) | | CURVE 180 (CONT.)* | | CURVE 180* | | CURVE 181* | |
|-------------------|--------|-------------------|--------|-------------------|--------|-------------------|--------|-------------------|--------|--------------------|--------|------------|--------|------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 2.28 | 0.386 | 6.60 | 0.629 | 2.54 | 0.428 | 0.32 | 0.717 | 3.00 | 0.940 | 3.00 | 0.940 | 2.00 | 0.706 | 2.00 | 0.706 |
| 2.33 | 0.374 | 6.69 | 0.636 | 2.50 | 0.443 | 0.90 | 0.736 | 3.08 | 0.958 | 3.08 | 0.958 | 2.02 | 0.641 | 2.02 | 0.641 |
| 2.38 | 0.390 | 6.87 | 0.636 | 2.63 | 0.418 | 9.23 | 0.739 | 3.26 | 0.947 | 3.26 | 0.947 | 2.09 | 0.723 | 2.09 | 0.723 |
| 2.40 | 0.370 | 7.08 | 0.631 | 2.71 | 0.446 | 9.34 | 0.746 | 3.33 | 0.964 | 3.33 | 0.964 | 2.11 | 0.628 | 2.11 | 0.628 |
| 2.44 | 0.405 | 7.32 | 0.636 | 2.83 | 0.439 | 9.63 | 0.747 | 3.55 | 0.952 | 3.55 | 0.952 | 2.14 | 0.709 | 2.14 | 0.709 |
| 2.47 | 0.392 | 7.49 | 0.646 | 2.89 | 0.422 | 9.75 | 0.750 | 3.83 | 0.978 | 3.83 | 0.978 | 2.16 | 0.638 | 2.16 | 0.638 |
| 2.52 | 0.408 | 7.86 | 0.661 | 2.92 | 0.433 | 10.02 | 0.750 | 3.97 | 0.962 | 3.97 | 0.962 | 2.20 | 0.599 | 2.20 | 0.599 |
| 2.58 | 0.389 | 8.15 | 0.679 | 2.98 | 0.433 | 10.13 | 0.754 | 4.03 | 0.975 | 4.03 | 0.975 | 2.24 | 0.666 | 2.24 | 0.666 |
| 2.65 | 0.412 | 8.54 | 0.703 | 3.01 | 0.440 | 10.39 | 0.754 | 4.19 | 0.968 | 4.19 | 0.968 | 2.27 | 0.619 | 2.27 | 0.619 |
| 2.72 | 0.412 | 8.84 | 0.703 | 3.07 | 0.440 | 10.61 | 0.760 | 4.28 | 0.979 | 4.28 | 0.979 | 2.32 | 0.666 | 2.32 | 0.666 |
| 2.77 | 0.351 | 9.35 | 0.730 | 3.25 | 0.461 | 11.34 | 0.771 | 4.37 | 0.979 | 4.37 | 0.979 | 2.37 | 0.632 | 2.37 | 0.632 |
| 2.83 | 0.323 | 9.50 | 0.730 | 3.49 | 0.500 | 11.98 | 0.771 | 4.49 | 0.968 | 4.49 | 0.968 | 2.41 | 0.671 | 2.41 | 0.671 |
| 2.87 | 0.275 | 9.53 | 0.728 | 3.62 | 0.513 | 12.45 | 0.779 | 4.59 | 0.968 | 4.59 | 0.968 | 2.49 | 0.641 | 2.49 | 0.641 |
| 2.92 | 0.266 | 9.71 | 0.734 | 3.76 | 0.527 | 12.88 | 0.789 | 4.71 | 0.976 | 4.71 | 0.976 | 2.53 | 0.668 | 2.53 | 0.668 |
| 2.98 | 0.266 | 9.84 | 0.742 | 3.85 | 0.527 | 13.14 | 0.791 | 4.81 | 0.976 | 4.81 | 0.976 | 2.57 | 0.640 | 2.57 | 0.640 |
| 3.04 | 0.240 | 10.10 | 0.746 | 3.88 | 0.538 | 13.76 | 0.804 | 5.05 | 0.980 | 5.05 | 0.980 | | | | |
| 3.21 | 0.250 | 10.52 | 0.746 | 3.98 | 0.541 | 14.17 | 0.808 | 6.00 | 0.980 | 6.00 | 0.980 | | | | |
| 3.21 | 0.262 | 11.00 | 0.762 | 4.16 | 0.558 | 14.53 | 0.808 | 6.99 | 0.984 | 6.99 | 0.984 | | | | |
| 3.42 | 0.302 | 11.29 | 0.765 | 4.26 | 0.580 | 14.63 | 0.805 | 7.63 | 0.991 | 7.63 | 0.991 | | | | |
| 3.50 | 0.324 | 11.58 | 0.764 | 4.36 | 0.576 | | | 7.98 | 0.994 | 7.98 | 0.994 | | | | |
| 3.66 | 0.375 | 11.78 | 0.771 | 4.67 | 0.588 | | | 8.24 | 0.994 | 8.24 | 0.994 | | | | |
| 3.82 | 0.416 | 12.43 | 0.778 | 5.13 | 0.619 | | | 8.41 | 0.997 | 8.41 | 0.997 | | | | |
| 3.99 | 0.438 | 12.74 | 0.796 | 5.73 | 0.630 | | | 8.68 | 0.991 | 8.68 | 0.991 | | | | |
| 4.23 | 0.455 | 13.35 | 0.795 | 5.96 | 0.641 | | | 9.02 | 0.988 | 9.02 | 0.988 | | | | |
| 4.33 | 0.481 | 13.84 | 0.788 | 6.05 | 0.650 | | | 9.62 | 0.988 | 9.62 | 0.988 | | | | |
| 4.42 | 0.478 | 14.05 | 0.781 | 6.38 | 0.653 | | | 10.00 | 0.989 | 10.00 | 0.989 | | | | |
| 4.53 | 0.496 | 14.16 | 0.777 | 6.50 | 0.665 | | | 12.00 | 0.988 | 12.00 | 0.988 | | | | |
| 4.64 | 0.501 | 14.50 | 0.780 | 6.63 | 0.672 | | | 14.67 | 0.992 | 14.67 | 0.992 | | | | |
| 4.70 | 0.493 | | | 6.80 | 0.671 | | | | | | | | | | |
| 4.82 | 0.407 | | | 6.95 | 0.680 | | | | | | | | | | |
| 4.88 | 0.463 | | | 7.09 | 0.688 | | | | | | | | | | |
| 4.93 | 0.479 | | | 7.09 | 0.688 | | | | | | | | | | |
| 4.98 | 0.516 | | | 7.33 | 0.689 | | | | | | | | | | |
| 5.11 | 0.534 | | | 7.39 | 0.695 | | | | | | | | | | |
| 5.42 | 0.554 | | | 7.56 | 0.696 | | | | | | | | | | |
| 5.57 | 0.571 | | | 7.70 | 0.704 | | | | | | | | | | |
| 5.94 | 0.584 | | | 7.70 | 0.704 | | | | | | | | | | |
| 6.08 | 0.584 | | | 8.12 | 0.707 | | | | | | | | | | |
| 6.19 | 0.595 | | | | | | | | | | | | | | |
| 6.39 | 0.597 | | | | | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 1-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-------------------|--------|-----------|--------|------------|--------|--------------------|--------|
| CURVE 185 (CONT.) | | | | | | | |
| 2.61 | 0.666 | 6.25 | 0.548 | CURVE 186 | | | |
| 2.75 | 0.299 | 6.35 | 0.577 | T = 293. | | | |
| 2.85 | 0.191 | 6.50 | 0.602 | 2.8 | 0.14 | CURVE 190 (CONT.)* | |
| 2.90 | 0.211 | 6.61 | 0.607 | 3.8 | 0.43 | 0.974 | 0.643 |
| 2.97 | 0.196 | 6.73 | 0.594 | 5.0 | 0.48 | 1.043 | 0.669 |
| 3.03 | 0.247 | 6.83 | 0.590 | 10.6 | 0.02 | 1.097 | 0.683 |
| 3.08 | 0.240 | 7.03 | 0.566 | CURVE 187* | | | |
| 3.20 | 0.208 | 7.15 | 0.519 | T = 293. | | | |
| 3.24 | 0.315 | 7.44 | 0.332 | 2.8 | 0.22 | 1.279 | 0.907 |
| 3.24 | 0.330 | 7.91 | 0.152 | 3.8 | 0.51 | 1.429 | 0.919 |
| 3.31 | 0.340 | 8.34 | 0.063 | 5.0 | 0.58 | 1.547 | 0.919 |
| 3.31 | 0.357 | 8.58 | 0.056 | 10.6 | 0.03 | 1.979 | 0.924 |
| 3.39 | 0.365 | 8.71 | 0.044 | CURVE 191* | | | |
| 3.58 | 0.509 | 8.83 | 0.044 | T = 293. | | | |
| 3.64 | 0.517 | 9.07 | 0.062 | 0.352 | 0.588 | CURVE 188 | |
| 3.67 | 0.552 | 9.34 | 0.098 | 0.455 | 0.616 | T = 293. | |
| 3.79 | 0.563 | 9.45 | 0.115 | 0.517 | 0.635 | CURVE 189 | |
| 3.87 | 0.554 | 9.69 | 0.136 | 0.572 | 0.656 | T = 293. | |
| 3.97 | 0.554 | 9.82 | 0.146 | 0.632 | 0.635 | CURVE 190* | |
| 4.07 | 0.541 | 10.02 | 0.135 | 0.690 | 0.615 | T = 293. | |
| 4.07 | 0.549 | 10.44 | 0.057 | 0.734 | 0.603 | CURVE 191* | |
| 4.10 | 0.554 | 10.68 | 0.037 | 0.760 | 0.603 | T = 293. | |
| 4.20 | 0.561 | 10.87 | 0.026 | 0.801 | 0.620 | CURVE 190* | |
| 4.20 | 0.566 | 11.00 | 0.026 | 0.858 | 0.627 | T = 293. | |
| 4.35 | 0.585 | 11.12 | 0.039 | 0.894 | 0.642 | CURVE 191* | |
| 4.46 | 0.592 | 11.28 | 0.049 | 0.939 | 0.666 | T = 293. | |
| 4.52 | 0.603 | 11.74 | 0.049 | 0.984 | 0.681 | CURVE 190* | |
| 4.71 | 0.613 | 12.06 | 0.069 | 1.038 | 0.700 | T = 293. | |
| 4.76 | 0.612 | 12.53 | 0.069 | 1.099 | 0.715 | CURVE 191* | |
| 4.81 | 0.616 | 13.07 | 0.081 | T = 293. | | | |
| 4.93 | 0.616 | 13.35 | 0.077 | 0.351 | 0.705 | CURVE 186 | |
| 5.00 | 0.620 | 13.50 | 0.077 | 0.454 | 0.73E | T = 293. | |
| 5.25 | 0.607 | 13.69 | 0.086 | 0.565 | 0.751 | CURVE 187* | |
| 5.53 | 0.599 | 13.86 | 0.091 | 0.680 | 0.746 | T = 293. | |
| 5.59 | 0.591 | 14.24 | 0.091 | 0.772 | 0.735 | CURVE 190* | |
| 5.71 | 0.582 | 14.63 | 0.102 | 0.844 | 0.771 | T = 293. | |
| 5.78 | 0.567 | | | 0.913 | 0.809 | CURVE 191* | |
| 5.86 | 0.540 | | | | | T = 293. | |
| 6.03 | 0.511 | | | | | CURVE 188 | |
| 6.22 | 0.535 | | | | | T = 293. | |

* NOT SHOWN IN FIGURE.

g. Angular Spectral Reflectance (Incident Angle Dependence)

Room temperature values of the angular spectral reflectance for wavelengths $1.2 \mu\text{m}$ and $1.8 \mu\text{m}$ as a function of incidence angle are listed in Table 1-14 and shown in Figure 1-22.

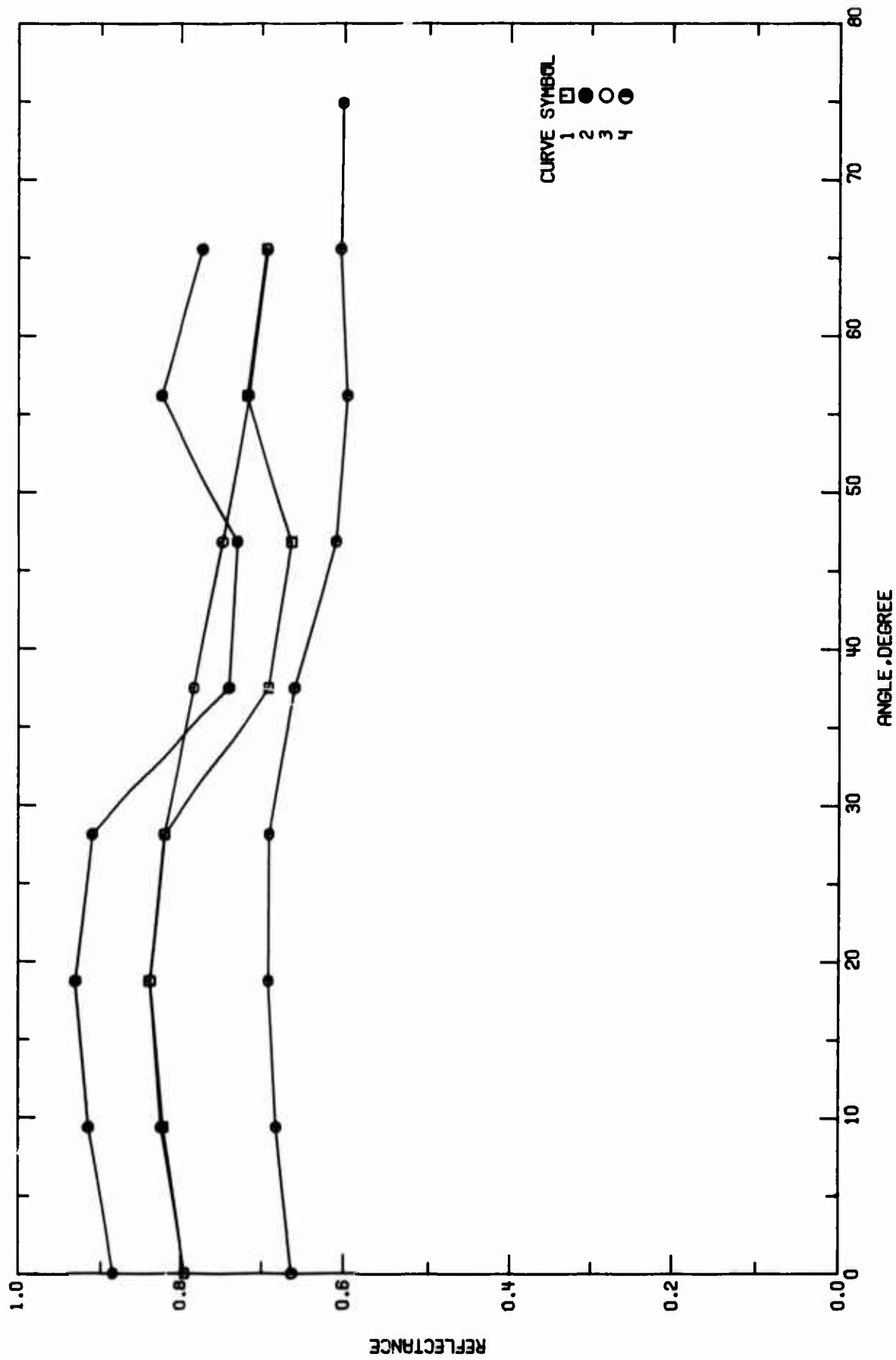


FIGURE 1-22. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (INCIDENT ANGLE DEPENDENCE).

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T29563 | Eberhart, R. C. | 1960 | 1.2 | 293 | Aluminum 24ST, Polished | Specimen 2.22 cm discs, 0.16 to 0.32 cm thick; sample surface prepared by standard metallographic techniques, average horizontal peak to peak distance is 30 μm , groove depth (average displacement from mean surface line) is 0.40 μm , integrating sphere used with PbS detector; reference standard MgO; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta = 30^\circ$, $\omega' = 2\pi$. |
| 2 T29563 | Eberhart, R. C. | 1960 | 1.8 | 293 | Aluminum 24ST, Polished | Similar to the above specimen |
| 3 T19294 | Folling, R. E. and Seban, R. A. | 1960 | 1.2 | 293 | Aluminum 24ST | Polished; Beckman DK2 spectrometer integrating sphere used for measurement; MgO reference standard; ω' s extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta = 0^\circ$ to 70° , $\omega' = 2\pi$. |
| 4 T19294 | Folling, R. E. and Seban, R. A. | 1960 | 1.2 | 293 | Aluminum 24ST | Roughened sample; surface roughened with sandpaper, scratches parallel; coarse structure - peak to peak depth 6.35 μm , spacing, 34 μm , fine structure - peak to peak depth, 1 μm ; Beckman DK2 spectrometer integrating sphere used for measurement; MgO reference standard; data extracted from figure; measurement temperature not given explicitly, 293 K assigned; $\theta = 0^\circ$ to 80° , $\omega' = 2\pi$. |

TABLE 1-14. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 2024 (INCIDENT ANGLE DEPENDENCE)
 [ANGLE, θ , DEGREE; TEMPERATURE, T, K; REFLECTANCE, ρ]

| θ | ρ | θ | ρ |
|----------|--------|----------|--------|
| CURVE 1 | | | |
| T = 293. | | | |
| 0. | 0.794 | 30. | 0.689 |
| 10. | 0.822 | 40. | 0.658 |
| 20. | 0.837 | 50. | 0.609 |
| 30. | 0.820 | 60. | 0.595 |
| 40. | 0.690 | 70. | 0.603 |
| 50. | 0.662 | 80. | 0.601 |
| 60. | 0.719 | | |
| 70. | 0.693 | | |
| CURVE 2 | | | |
| T = 293. | | | |
| 0. | 0.882 | | |
| 10. | 0.914 | | |
| 20. | 0.929 | | |
| 30. | 0.910 | | |
| 40. | 0.741 | | |
| 50. | 0.731 | | |
| 60. | 0.924 | | |
| 70. | 0.771 | | |
| CURVE 3 | | | |
| T = 293. | | | |
| 0. | 0.794 | | |
| 10. | 0.824 | | |
| 20. | 0.937 | | |
| 30. | 0.821 | | |
| 40. | 0.782 | | |
| 50. | 0.748 | | |
| 60. | 0.716 | | |
| 70. | 0.691 | | |
| CURVE 4 | | | |
| T = 293. | | | |
| 0. | 0.661 | | |
| 10. | 0.680 | | |
| 20. | 0.690 | | |

h. Normal Spectral Absorptance (Wavelength Dependence)

There are two sets of experimental data available for the wavelength dependence (2.53-20.0 μm) of the normal spectral absorptance of Aluminum Alloy 2024 for polished surface conditions. These are listed in Table 1-17 and shown in Figure 1-24.

(1) Highly Polished Aluminum Alloy 2024

The recommended values at 293 K listed in Table 1-15 and shown in Figure 1-23 for highly polished Aluminum Alloy 2024 were generated from the measurements of Schriempf and Wieting [A00003] and are believed accurate to $\pm 10\%$ over the entire wavelength range.

(2) Highly Polished Alclad Aluminum Alloy 2024

The recommended values at 293 K are listed in Table 1-15 and shown in Figure 1-25 for highly polished alclad Aluminum Alloy 2024. These values were generated with the relationship discussed in Section 4.20, based on Eq. (2.5-5), and are believed accurate to $\pm 10\%$ over the entire wavelength range. The provisional values for highly polished alclad Aluminum Alloy 2024 were calculated for temperatures of 450, 600, and 750 K by the relationship discussed in Section 4.20, based on Eq. (2.5-5), are listed in Table 1-15 and shown in Figure 1-25 and are believed accurate to $\pm 20\%$ over the entire wavelength range.

(3) Oxidized Aluminum Alloy 2024

The provisional values are listed in Table 1-15 and shown in Figure 1-26 for oxidized Aluminum Alloy 2024 at 823 K. These values are consistent with the normal spectral emittance values of Blau, et al. [T16606] and are believed accurate to $\pm 20\%$ over the entire wavelength range.

TABLE 1-15. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| HIGHLY POLISHED T = 293 | | HIGHLY POLISHED ALCLAD T = 293 | | HIGHLY POLISHED ALCLAD T = 450 | | HIGHLY POLISHED ALCLAD T = 600 | | HIGHLY POLISHED ALCLAD T = 750 | | OXIDIZED ALLOY T = 823 | |
|----------------------------|----------|--------------------------------------|----------|--------------------------------------|----------|--------------------------------------|----------|--------------------------------------|----------|------------------------------|----------|
| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α |
| 2.20 | 0.0980 | 2.5 | 0.067 | 2.5 | 0.071A† | 2.5 | 0.073A† | 2.5 | 0.075A† | 2.0 | 0.426A† |
| 2.60 | 0.0760 | 2.8 | 0.057 | 2.8 | 0.063A | 2.8 | 0.067A | 2.8 | 0.069A | 2.2 | 0.418A |
| 3.00 | 0.0697 | 3.0 | 0.052 | 3.0 | 0.059A | 3.0 | 0.063A | 3.0 | 0.066A | 2.5 | 0.410A |
| 3.50 | 0.0575 | 3.5 | 0.044 | 3.5 | 0.052A | 3.5 | 0.056A | 3.5 | 0.060A | 2.8 | 0.403A |
| 3.80 | 0.0524 | 3.8 | 0.041 | 3.8 | 0.049A | 3.8 | 0.053A | 3.8 | 0.057A | 3.0 | 0.399A |
| 4.00 | 0.0498 | 4.0 | 0.039 | 4.0 | 0.046A | 4.0 | 0.051A | 4.0 | 0.055A | 3.2 | 0.394A |
| 4.50 | 0.0460 | 4.5 | 0.035 | 4.5 | 0.043A | 4.5 | 0.047A | 4.5 | 0.051A | 3.5 | 0.386A |
| 5.00 | 0.0402 | 5.0 | 0.033 | 5.0 | 0.040A | 5.0 | 0.044A | 5.0 | 0.048A | 3.8 | 0.381A |
| 5.50 | 0.0375 | 5.5 | 0.031 | 5.5 | 0.037A | 5.5 | 0.042A | 5.5 | 0.046A | 4.0 | 0.376A |
| 6.00 | 0.0355 | 6.0 | 0.029 | 6.0 | 0.035A | 6.0 | 0.040A | 6.0 | 0.043A | 4.2 | 0.374A |
| 6.50 | 0.0338 | 6.5 | 0.027 | 6.5 | 0.034A | 6.5 | 0.038A | 6.5 | 0.042A | 4.5 | 0.366A |
| 7.00 | 0.0323 | 7.0 | 0.026 | 7.0 | 0.032A | 7.0 | 0.037A | 7.0 | 0.040A | 4.8 | 0.362A |
| 7.50 | 0.0310 | 7.5 | 0.025 | 7.5 | 0.031A | 7.5 | 0.035A | 7.5 | 0.039A | 5.0 | 0.360A |
| 8.00 | 0.0298 | 8.0 | 0.024 | 8.0 | 0.030A | 8.0 | 0.034A | 8.0 | 0.037A | 5.2 | 0.356A |
| 8.50 | 0.0287 | 8.5 | 0.023 | 8.5 | 0.029A | 8.5 | 0.033A | 8.5 | 0.036A | 5.5 | 0.351A |
| 9.00 | 0.0278 | 9.0 | 0.023 | 9.0 | 0.028A | 9.0 | 0.032A | 9.0 | 0.035A | 5.8 | 0.346A |
| 9.50 | 0.0272 | 9.5 | 0.022 | 9.5 | 0.027A | 9.5 | 0.031A | 9.5 | 0.034A | 6.0 | 0.342A |
| 10.00 | 0.0270 | 10.0 | 0.021 | 10.0 | 0.026A | 10.0 | 0.030A | 10.0 | 0.033A | 6.2 | 0.340A |
| 10.60 | 0.0262 | 10.5 | 0.021 | 10.5 | 0.026A | 10.5 | 0.029A | 10.5 | 0.032A | 6.5 | 0.336A |
| 11.00 | 0.0258 | 11.0 | 0.020 | 11.0 | 0.025A | 11.0 | 0.029A | 11.0 | 0.032A | 7.0 | 0.330A |
| 11.50 | 0.0254 | 11.5 | 0.020 | 11.5 | 0.025A | 11.5 | 0.028A | 11.5 | 0.031A | 7.2 | 0.328A |
| 12.00 | 0.0250 | 12.0 | 0.019 | 12.0 | 0.024A | 12.0 | 0.028A | 12.0 | 0.030A | 7.5 | 0.323A |
| 12.50 | 0.0246 | 12.5 | 0.019 | 12.5 | 0.024A | 12.5 | 0.027A | 12.5 | 0.030A | 8.0 | 0.317A |
| 13.00 | 0.0242 | 13.0 | 0.019 | 13.0 | 0.023A | 13.0 | 0.026A | 13.0 | 0.029A | 8.5 | 0.310A |
| 13.50 | 0.0239 | 13.5 | 0.018 | 13.5 | 0.023A | 13.5 | 0.025A | 13.5 | 0.029A | 9.0 | 0.303A |
| 14.00 | 0.0235 | 14.0 | 0.018 | 14.0 | 0.022A | 14.0 | 0.025A | 14.0 | 0.028A | 9.5 | 0.296A |
| 14.50 | 0.0232 | 14.5 | 0.017 | 14.5 | 0.022A | 14.5 | 0.025A | 14.5 | 0.028A | 10.0 | 0.290A |
| 15.00 | 0.0228 | 15.0 | 0.017 | 15.0 | 0.021A | 15.0 | 0.025A | 15.0 | 0.027A | 10.5 | 0.284A |
| | | | | | | | | | | 11.0 | 0.277A |
| | | | | | | | | | | 11.5 | 0.271A |
| | | | | | | | | | | 12.0 | 0.266A |
| | | | | | | | | | | 12.5 | 0.261A |
| | | | | | | | | | | 13.0 | 0.256A |
| | | | | | | | | | | 13.5 | 0.252A |
| | | | | | | | | | | 14.0 | 0.248A |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

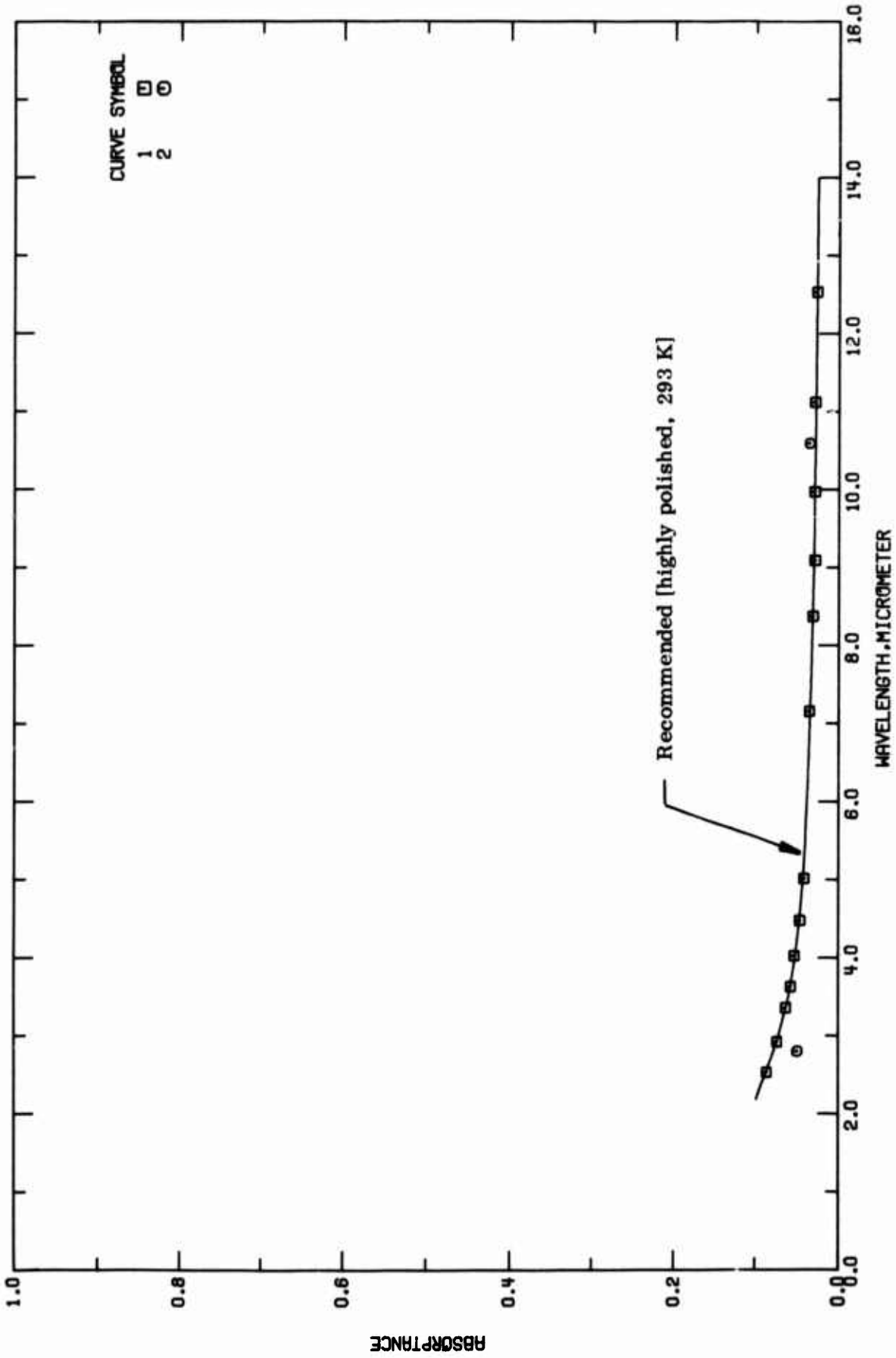


FIGURE 1-23. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

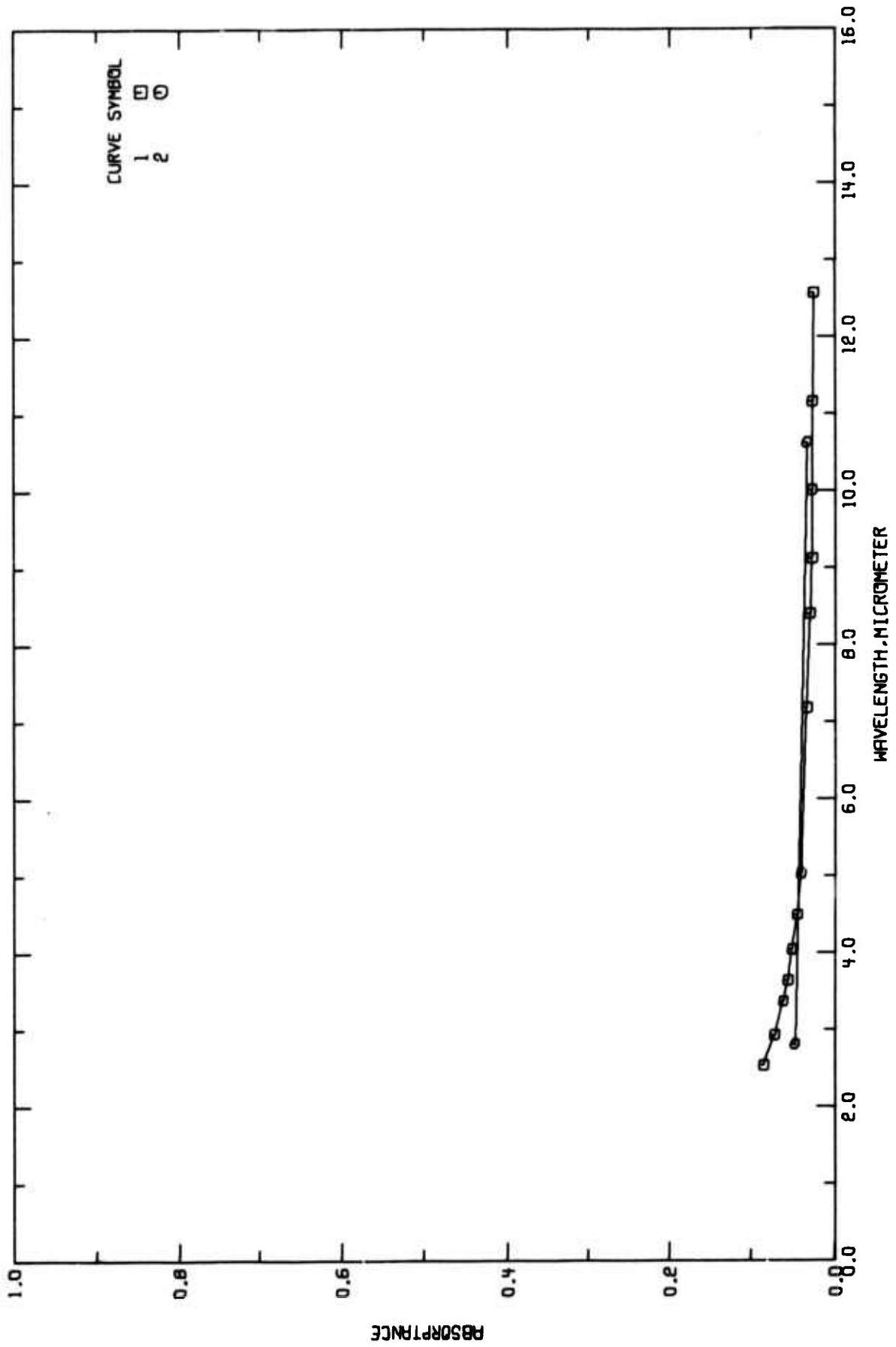


FIGURE 1-24. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

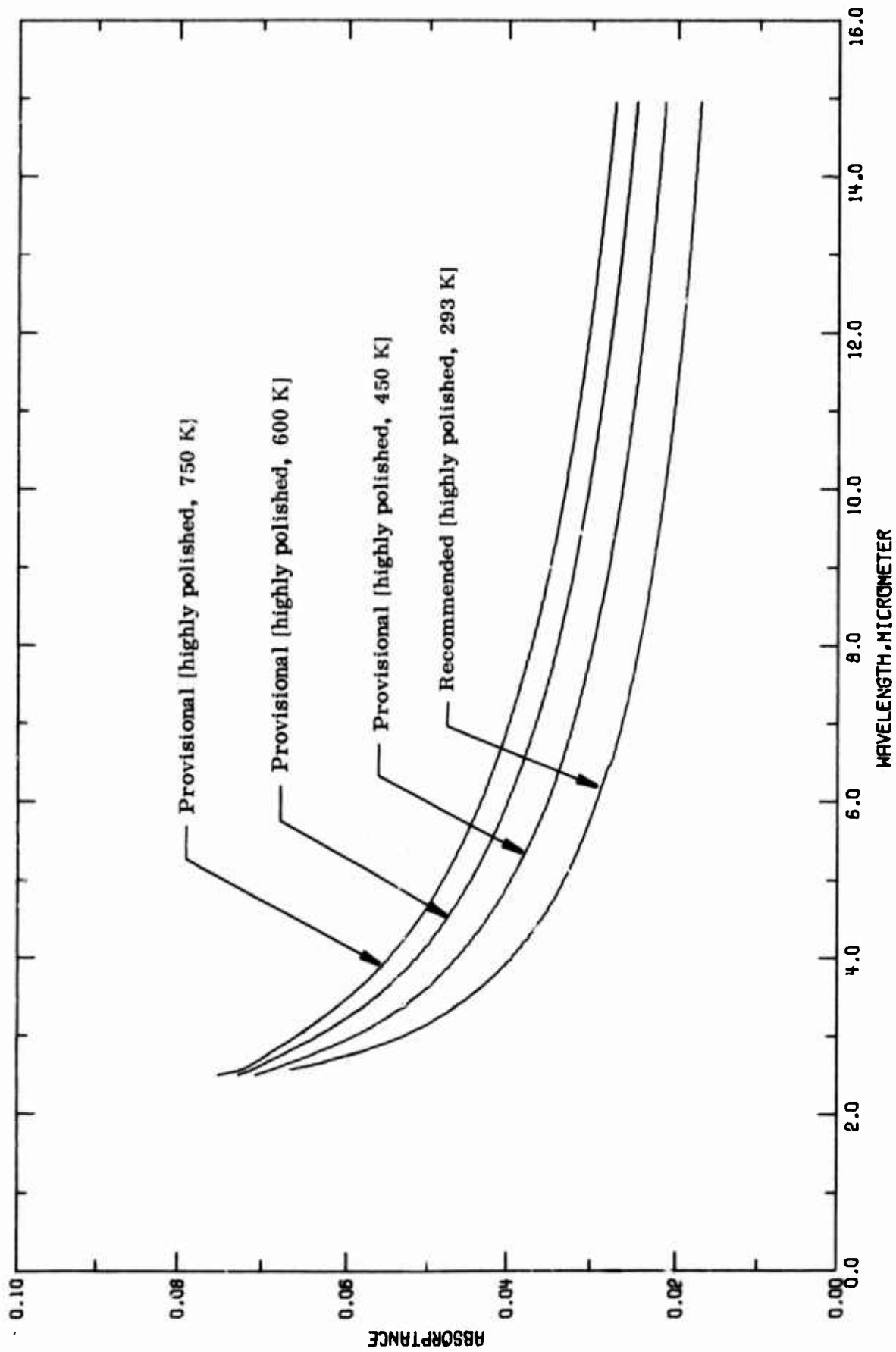


FIGURE 1-25. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALCLAD ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

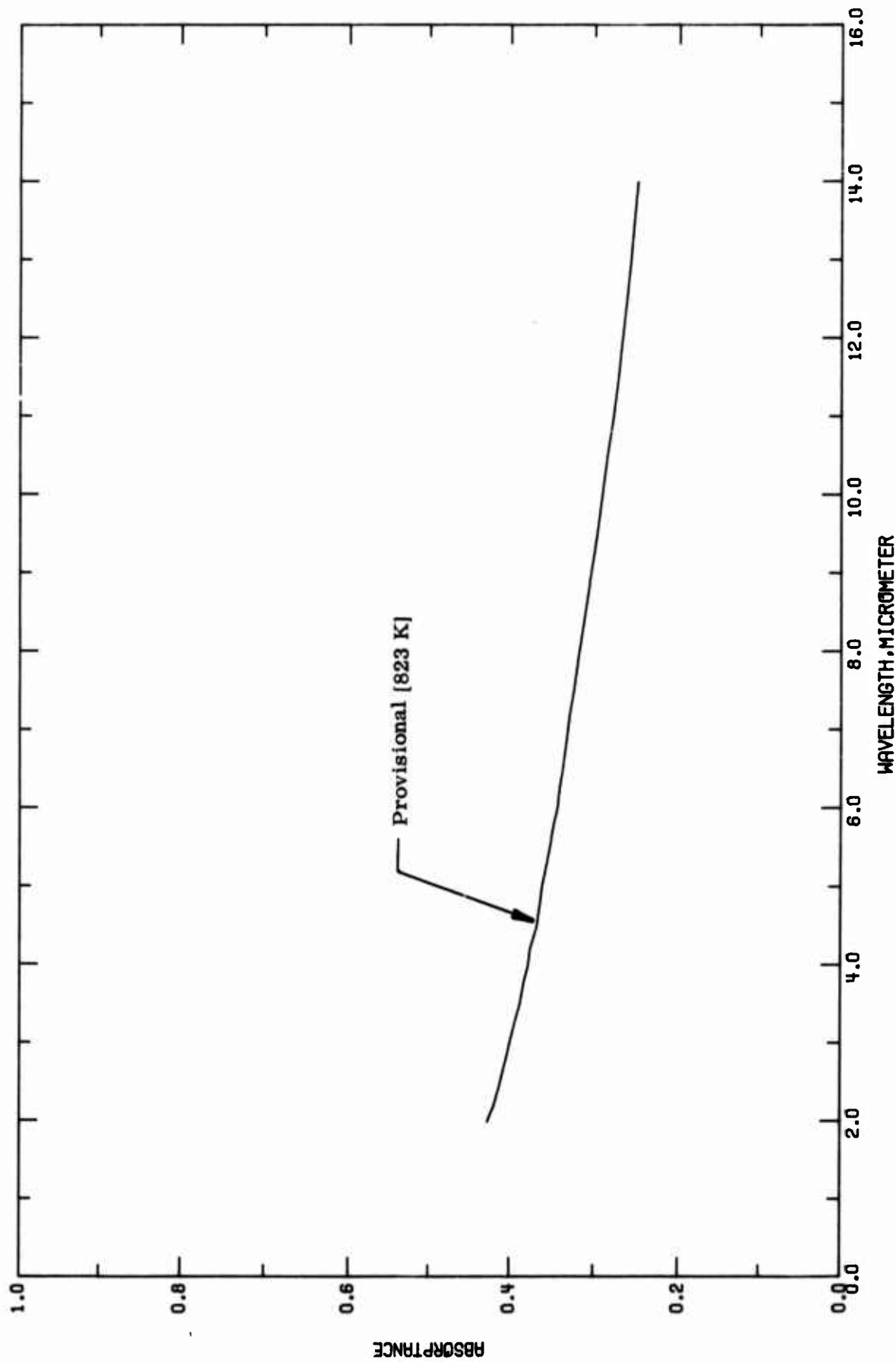


FIGURE 1-26. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF OXIDIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

TABLE 1-16. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (Wavelength Dependence)

| Cuc. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 A00001 | Schriempf, J.T. and Wieting, T.J. | 1974 | 2.53-20.0 | 293 | Aluminum Alloy | Author states specimen was "aluminum alloy very similar to 2024 aluminum"; author describes surface as "high quality"; reflectance was measured using a grating spectrometer, absorbance then calculated from $\alpha = 1 - \rho$; a gold reference mirror was used as a standard; data extracted from figure; measurement temperature specified as room temperature, 293 K assigned; $\theta = 0^\circ$, reported error $\pm 0.1\%$. |
| 2 A00016 | Neighbour, J.R., (Editor) | 1974 | 2.8, 10.6 | 293 | | Polished; measurement temperature specified as room temperature, 293 K assigned; $\theta = 0^\circ$. |

TABLE 1-17. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|-----------|----------|
| CURVE 1 | |
| T = 293. | |
| 2.53 | 0.0650 |
| 2.92 | 0.0717 |
| 3.36 | 0.0609 |
| 3.63 | 0.0551 |
| 4.03 | 0.0505 |
| 4.48 | 0.0439 |
| 5.02 | 0.0391 |
| 7.16 | 0.0329 |
| 8.38 | 0.0290 |
| 9.10 | 0.0266 |
| 9.98 | 0.0269 |
| 11.13 | 0.0265 |
| 12.54 | 0.0246 |
| 14.31 | 0.0229 |
| 16.66 | 0.0198 |
| 19.11 | 0.0195 |
| 20.88 | 0.0167 |

| λ | α |
|-----------|----------|
| CURVE 2 | |
| T = 293. | |
| 2.0 | 0.047 |
| 10.6 | 0.033 |

i. Normal Spectral Absorptance (Temperature Dependence)

There are two sets of experimental data available for the temperature dependence (325-593 K) of the normal spectral absorptance of Aluminum Alloy 2024. These are listed in Table 1-20 and shown in Figure 1-28. This available data was not sufficient to generate recommended values, but values were calculated by the relation discussed in subsection 4.20, based on equation (2.5-5), for highly polished alclad Aluminum Alloy 2024 for wavelengths of 2.8, 3.8, 5.0, and 10.6 μm . These values are believed accurate to $\pm 20\%$ over the entire wavelength range and are listed in Table 1-18 and shown in Figure 1-27.

TABLE 1-18. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α | T | α | T | α | T | α |
|-----------------|----------|-----------------|----------|-----------------|----------|------------------|----------|
| HIGHLY POLISHED | | HIGHLY POLISHED | | HIGHLY POLISHED | | HIGHLY POLISHED | |
| ALCLAD | | ALCLAD | | ALCLAD | | ALCLAD | |
| $\lambda = 2.0$ | | $\lambda = 3.0$ | | $\lambda = 5.0$ | | $\lambda = 10.6$ | |
| 250.0 | 0.054 | 250.0 | 0.038 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.057 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.060 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.062 | 400.0 | 0.046 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.063 | 450.0 | 0.047 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.066 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.067 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.068 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 700.0 | 0.068 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |

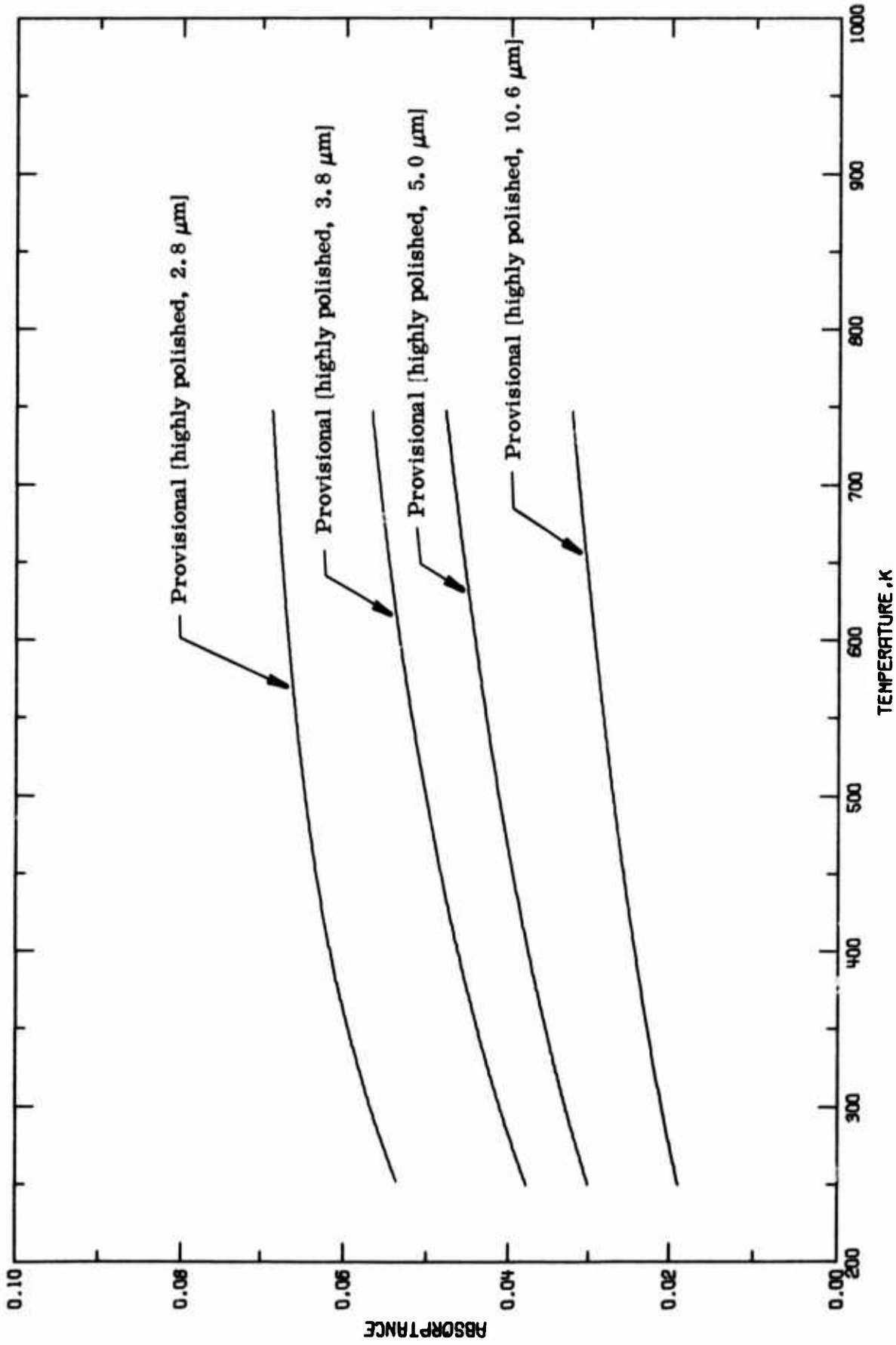


FIGURE 1-27. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALCLAD ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE).

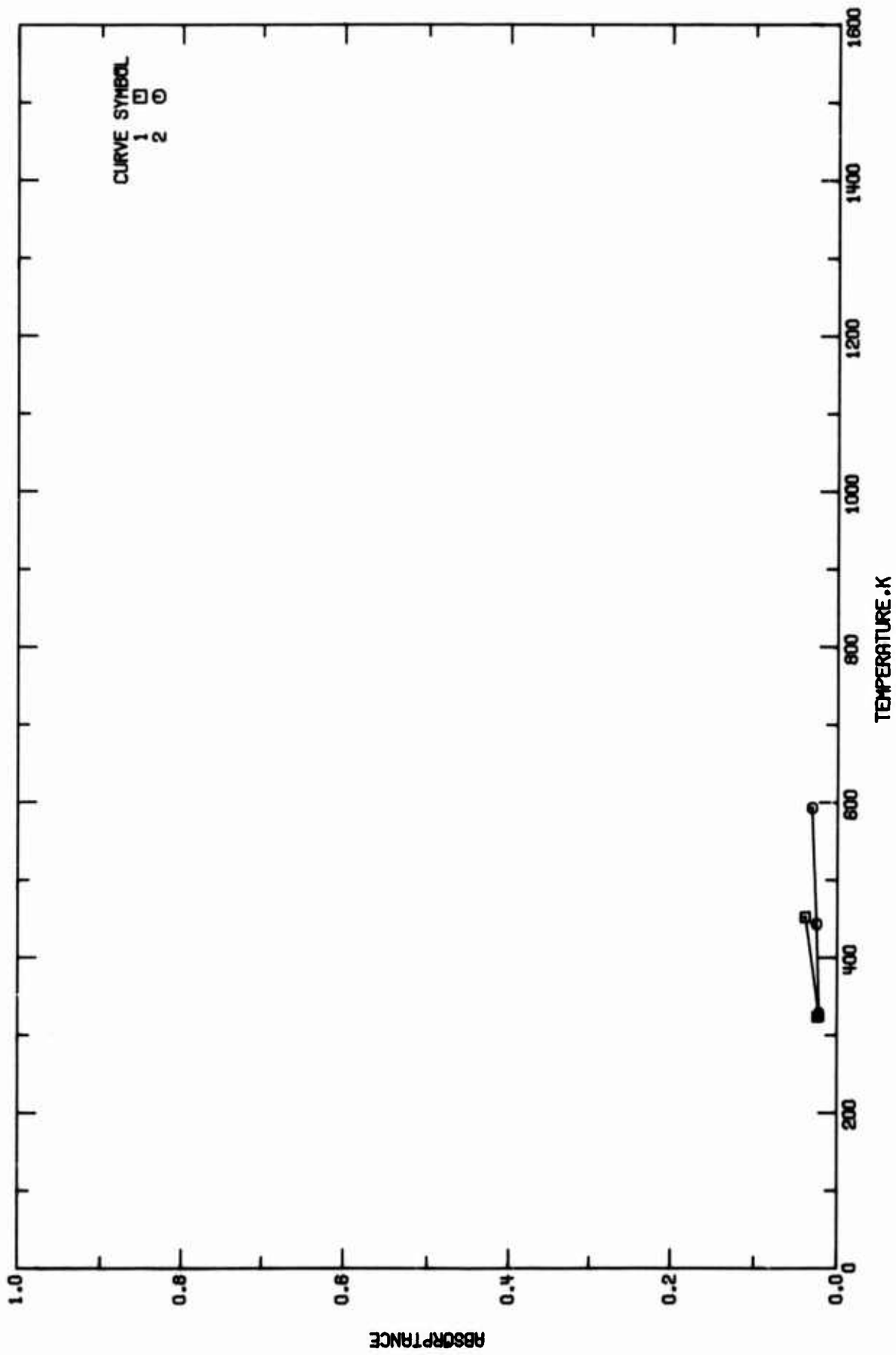


FIGURE 1-28. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE).

TABLE 1-19. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------------|-----------|---------------------------------|----------------------|-------------------------------|--|
| 1 E66194 | Cunningham, S.S. and Laughlin, W.T. | 1971-1973 | 10.6 | 325-453 | 2024 Alclad Aluminum | Specimen was circular; samples in as-received condition, then washed with methanol; room atm environment; sample irradiated with a 100 watt CO ₂ Laser with intensity from 60-165 watts/cm ² ; samples were uniformly heated by entire laser beam; thermocouples were attached to back of sample, one at center and one along perimeter; NSA calculated from temperature rise; author calls absorptance "coupling coefficient"; $\theta \sim 0^\circ$, reported error $\pm 0.3\%$. |
| 2 E66194 | Cunningham, S.S. and Laughlin, W.T. | 1971-1973 | 10.6 | 328-593 | 2024 Alclad Aluminum | Specimen was 12.7 x 12.7 cm flat plate; sample in as-received condition, then washed with methanol; room atm environment; sample irradiated with a 5000 watt CO ₂ Laser with intensity from 75-3700 watts/cm ² ; beam size varied depending on intensity, but beam was always in center of plate; three thermocouples were attached to sample back, one at center of plate, another along line between opposing corners of plate, and another along line between two other opposing corners; NSA calculated from temperature rise; author calls absorptance "coupling coefficient"; $\theta \sim 0^\circ$, reported error $\pm 0.4\%$. |

TABLE 1-20. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α |
|------------------|----------|
| CURVE 1 | |
| $\lambda = 10.6$ | |
| 324. | 0.024 |
| 325. | 0.022 |
| 453. | 0.039 |
| CURVE 2 | |
| $\lambda = 10.6$ | |
| 320. | 0.022 |
| 443. | 0.025 |
| 593. | 0.031 |

j. Angular Spectral Absorptance (Wavelength Dependence)

There are no experimental data available for this subproperty but provisional values are listed in Table 1-21 and shown in Figures 1-29, 1-30, and 1-31 for anodized, alodined ($\theta = 15^\circ$), and alodined ($\theta = 45^\circ$) Aluminum Alloy 2024, respectively. These were calculated from the provisional angular spectral reflectance data listed in Table 1-10 and shown in Figures 1-16, 1-18, and 1-20. The values are believed accurate to $\pm 15\%$ over the entire range for the anodized and alodined ($\theta = 15^\circ$) Aluminum Alloy 2024 materials at 293 K. The alodined ($\theta = 45^\circ$) Aluminum Alloy 2024 provisional values are accurate to $\pm 20\%$. These values apply only to the surface conditions cited in references, see Section 4.1-c.

TABLE 1-21. PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α | λ | α | λ | α |
|---|----------|---|----------|--|----------|-----------|----------|--|----------|
| SULFURIC ACID ANODIZED, $\theta=15^\circ$ T = 293 | 0.740 | SULFURIC ACID ANODIZED, $\theta=15^\circ$ T = 293 (CONT.) | 0.484 | CHROMATE ALODINED, $\theta=15^\circ$ T = 293 | 2.34 | 0.517 | 12.00 | CHROMATE ALODINED, $\theta=15^\circ$ T = 293 (CONT.) | 0.142 |
| 0.35 | 0.640 | 6.10 | 0.473 | 2.50 | 0.531 | 0.135 | 12.50 | 2.00 | 0.240 |
| 0.40 | 0.550 | 6.20 | 0.410 | 6.40 | 0.604 | 0.129 | 13.00 | 2.20 | 0.250 |
| 0.50 | 0.482 | 6.60 | 0.393 | 3.00 | 0.677 | 0.123 | 13.50 | 2.40 | 0.280 |
| 0.60 | 0.474 | 6.80 | 0.405 | 3.05 | 0.685 | 0.118 | 14.00 | 2.60 | 0.350 |
| 0.70 | 0.475 | 7.00 | 0.426 | 3.10 | 0.685 | 0.113 | 14.50 | 2.80 | 0.552 |
| 0.80 | 0.481 | 7.20 | 0.514 | 3.15 | 0.682 | 0.109 | 15.00 | 3.00 | 0.620 |
| 0.83 | 0.482 | 7.40 | 0.640 | 3.20 | 0.682 | | | 3.10 | 0.618 |
| 0.90 | 0.434 | 7.60 | 0.740 | 3.25 | 0.673 | | | 3.20 | 0.606 |
| 1.00 | 0.380 | 7.80 | 0.820 | 3.30 | 0.655 | | | 3.40 | 0.550 |
| 1.20 | 0.320 | 8.00 | 0.875 | 3.50 | 0.589 | | | 3.60 | 0.470 |
| 1.40 | 0.292 | 8.20 | 0.918 | 3.70 | 0.528 | | | 3.80 | 0.408 |
| 1.60 | 0.274 | 8.40 | 0.942 | 3.80 | 0.508 | | | 4.00 | 0.366 |
| 1.80 | 0.269 | 8.60 | 0.949 | 4.00 | 0.480 | | | 4.20 | 0.338 |
| 2.00 | 0.301 | 8.80 | 0.947 | 4.20 | 0.450 | | | 4.40 | 0.320 |
| 2.20 | 0.341 | 9.00 | 0.940 | 4.50 | 0.431 | | | 4.50 | 0.316 |
| 2.40 | 0.422 | 9.20 | 0.928 | 4.56 | 0.426 | | | 4.60 | 0.320 |
| 2.60 | 0.422 | 9.40 | 0.893 | 4.61 | 0.427 | | | 4.70 | 0.400 |
| 2.80 | 0.779 | 9.60 | 0.864 | 4.70 | 0.461 | | | 4.72 | 0.412 |
| 2.85 | 0.807 | 9.80 | 0.855 | 4.74 | 0.478 | | | 4.76 | 0.414 |
| 2.90 | 0.810 | 10.00 | 0.859 | 4.77 | 0.481 | | | 4.80 | 0.412 |
| 2.95 | 0.808 | 10.20 | 0.900 | 4.81 | 0.472 | | | 4.90 | 0.320 |
| 3.00 | 0.797 | 10.40 | 0.935 | 4.87 | 0.440 | | | 5.00 | 0.298 |
| 3.20 | 0.677 | 10.60 | 0.968 | 4.93 | 0.405 | | | 5.20 | 0.280 |
| 3.40 | 0.592 | 10.80 | 0.972 | 4.95 | 0.397 | | | 5.40 | 0.270 |
| 3.60 | 0.526 | 11.00 | 0.975 | 5.00 | 0.394 | | | 5.60 | 0.260 |
| 3.80 | 0.484 | 11.20 | 0.963 | 5.50 | 0.362 | | | 5.80 | 0.252 |
| 4.00 | 0.454 | 11.40 | 0.955 | 6.00 | 0.334 | | | 6.00 | 0.246 |
| 4.20 | 0.428 | 11.60 | 0.949 | 6.50 | 0.308 | | | 7.00 | 0.220 |
| 4.40 | 0.410 | 11.80 | 0.943 | 7.00 | 0.285 | | | 8.00 | 0.200 |
| 4.60 | 0.396 | 12.0 | 0.938 | 7.50 | 0.263 | | | 9.00 | 0.181 |
| 4.80 | 0.389 | 12.50 | 0.928 | 8.00 | 0.244 | | | 10.00 | 0.164 |
| 5.00 | 0.384 | 13.00 | 0.920 | 8.50 | 0.227 | | | 10.60 | 0.156 |
| 5.20 | 0.382 | 13.50 | 0.915 | 9.00 | 0.210 | | | 11.00 | 0.150 |
| 5.40 | 0.390 | 14.00 | 0.909 | 9.50 | 0.195 | | | 12.00 | 0.136 |
| 5.60 | 0.406 | 14.50 | 0.905 | 10.00 | 0.182 | | | 13.00 | 0.127 |
| 5.80 | 0.442 | 15.00 | 0.902 | 10.60 | 0.167 | | | 14.00 | 0.116 |
| 5.90 | 0.476 | | | 11.00 | 0.158 | | | | |
| 6.00 | 0.484 | | | 11.50 | 0.150 | | | | |

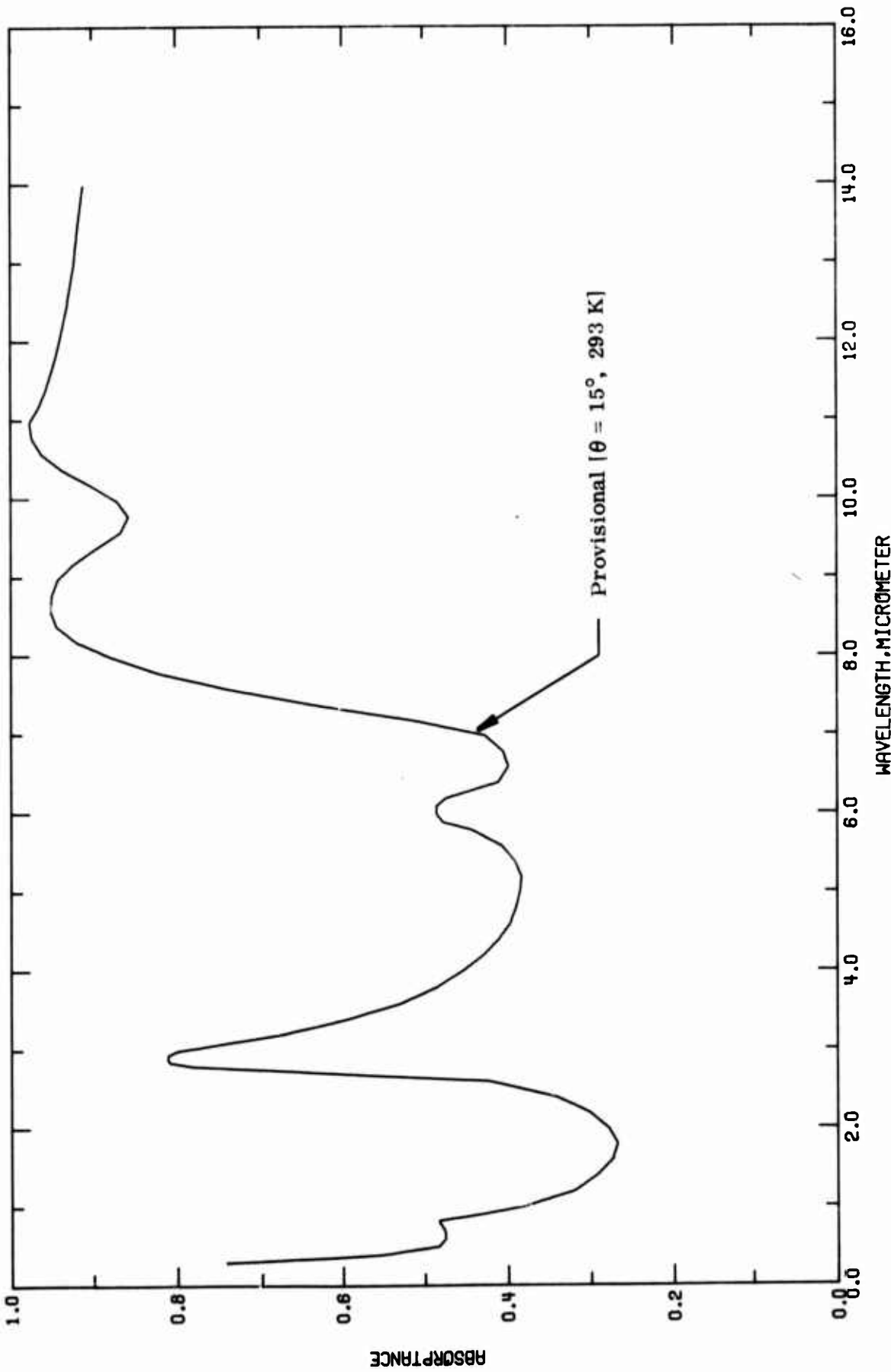


FIGURE 1-29. PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ANODIZED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

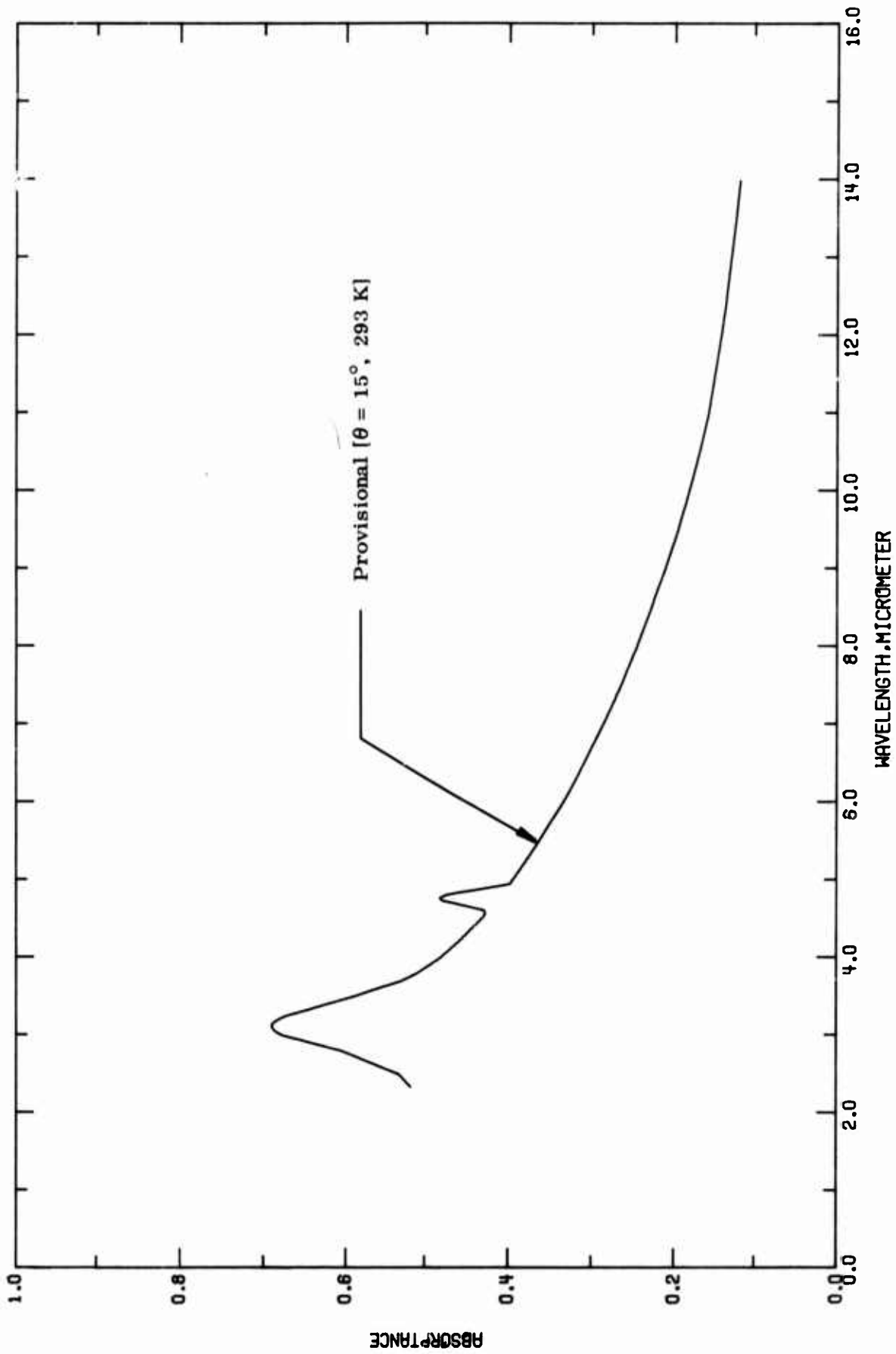


FIGURE 1-30. PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE)

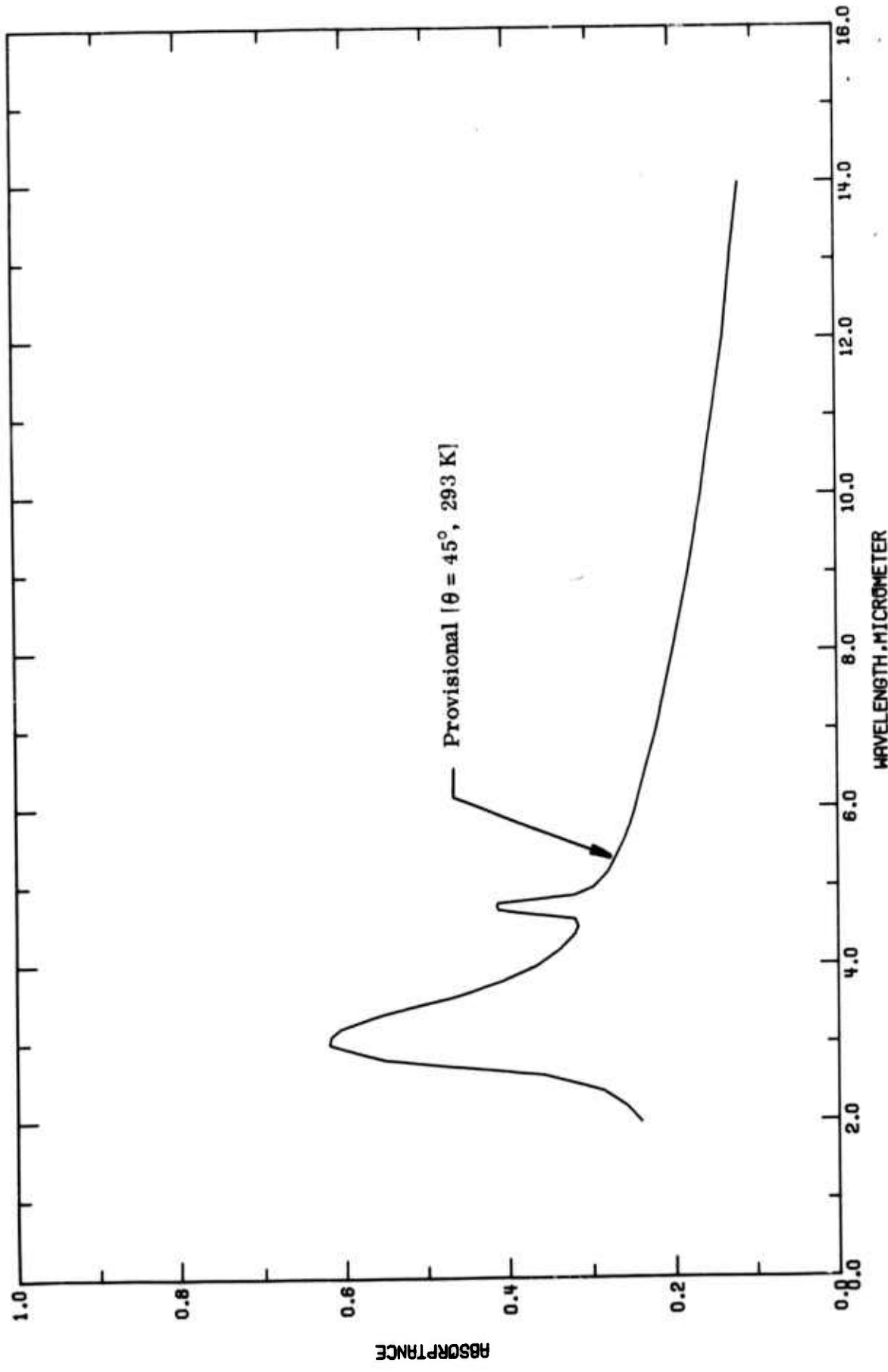


FIGURE 1-31. PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF ALODINED ALUMINUM ALLOY 2024 (WAVELENGTH DEPENDENCE).

k. Transmittance

Although it is true that metals and alloys in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms.

As an aircraft/spacecraft structural material, this alloy is not used in the form of extremely thin films and therefore is opaque; that is, its transmittance is zero.

4.2. Aluminum Alloy 7075

Aluminum 7075, formerly known as aluminum alloy 75S is a wrought alloy with zinc as the principal alloying element. Its nominal composition (by weight) is: 5.5% Zn, 2.5% Mg, 1.5% Cu, 0.3% Cr, and Al balance [A00005]. Various properties and usage of this alloy is discussed in [T15906] and [A00005].

In the solution-heat treated condition, this alloy is designated as 7075-T6. It is among the highest strength aluminum alloy which is commonly used in the aircraft structural parts. This alloy is also available in clad state.

Some physical and mechanical properties [A00005] of this alloy are as follows:

Liquidus temperature: 911 K

Solidus temperature: 749 K

Density at 293 K: 2.80 g cm^{-3}

Room-temperature tensile (ultimate) strength: 23 kg mm^{-2} (for annealed alloy)
 58 kg mm^{-2} (for 7075-T6)

Brinell hardness number: 60 (for annealed alloy)

(500 kg load, 10 mm ball) 150 (for 7075-T6)

a. Normal Spectral Emittance (Wavelength Dependence)

There are seven sets of experimental data available for the wavelength dependence (0.3-27 μm) of the normal spectral emittance of Aluminum Alloy 7075 under various surface conditions. These are tabulated in Table 2-3 and shown in Figure 2-2.

(1) Aluminum Alloy 7075

The recommended values tabulated in Table 2-1 and shown in Figure 2-1 for Aluminum Alloy 7075 with surface roughness of about 0.0005-0.0006 μm are primarily from the investigations of Schocken [T29202]. These are considered accurate to within $\pm 15\%$ over the entire wavelength range.

(2) Aluminum Alloy 7075-T6

The recommended values tabulated in Table 2-1 and shown in Figure 2-1 for Aluminum Alloy 7075-T6 rolled sheet were calculated from the normal spectral reflectance data (see Section 4.2.c).

TABLE 2-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ |
|---------------------------|------------|-------------------------|------------|
| POLISHED ALLOY T = 323 | | ROLLED SHEET T = 293 | |
| 0.3 | 0.260 | 2.8 | 0.043 |
| 0.4 | 0.165 | 3.0 | 0.040 |
| 0.5 | 0.136 | 3.8 | 0.030 |
| 0.6 | 0.131 | 4.0 | 0.029 |
| 0.7 | 0.150 | 5.0 | 0.024 |
| 0.8 | 0.164 | 6.0 | 0.023 |
| 0.9 | 0.148 | 7.0 | 0.022 |
| 1.0 | 0.120 | 8.0 | 0.021 |
| 1.2 | 0.090 | 9.0 | 0.020 |
| 1.4 | 0.078 | 10.0 | 0.019 |
| 1.6 | 0.075 | 10.6 | 0.018 |
| 1.8 | 0.078 | 11.0 | 0.018 |
| 2.0 | 0.083 | 12.0 | 0.018 |
| 2.4 | 0.088 | 13.0 | 0.018 |
| 2.8 | 0.092 | 14.0 | 0.017 |
| 3.0 | 0.092 | 15.0 | 0.017 |
| 3.4 | 0.090 | | |
| 3.8 | 0.082 | | |
| 4.0 | 0.078 | | |
| 4.5 | 0.070 | | |
| 5.0 | 0.064 | | |
| 6.0 | 0.054 | | |
| 7.0 | 0.048 | | |
| 8.0 | 0.046 | | |
| 9.0 | 0.045 | | |
| 10.0 | 0.045 | | |
| 10.6 | 0.044 | | |
| 11.0 | 0.043 | | |
| 12.0 | 0.043 | | |
| 13.0 | 0.043 | | |
| 14.0 | 0.042 | | |
| 15.0 | 0.042 | | |

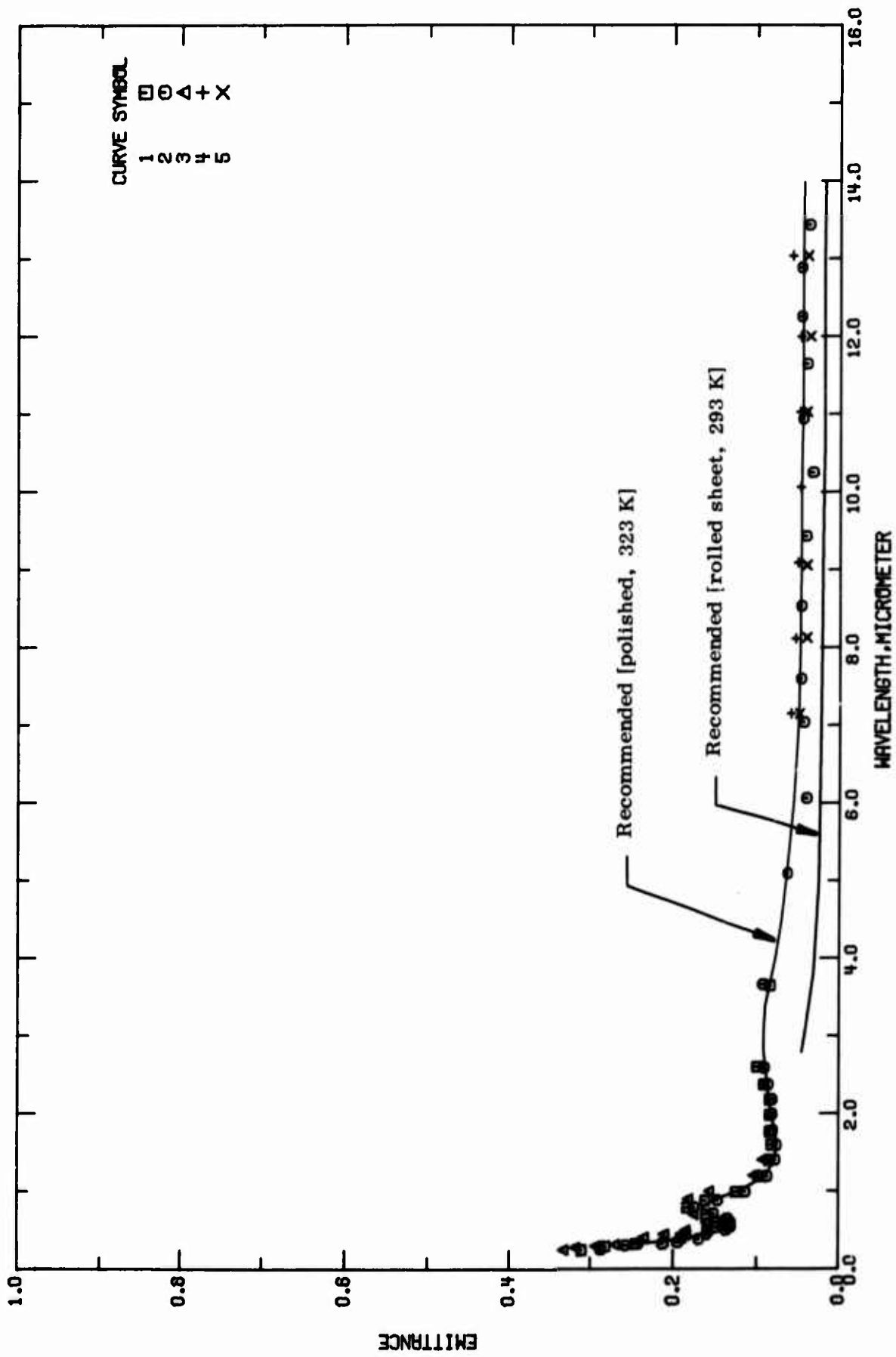


FIGURE 2-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

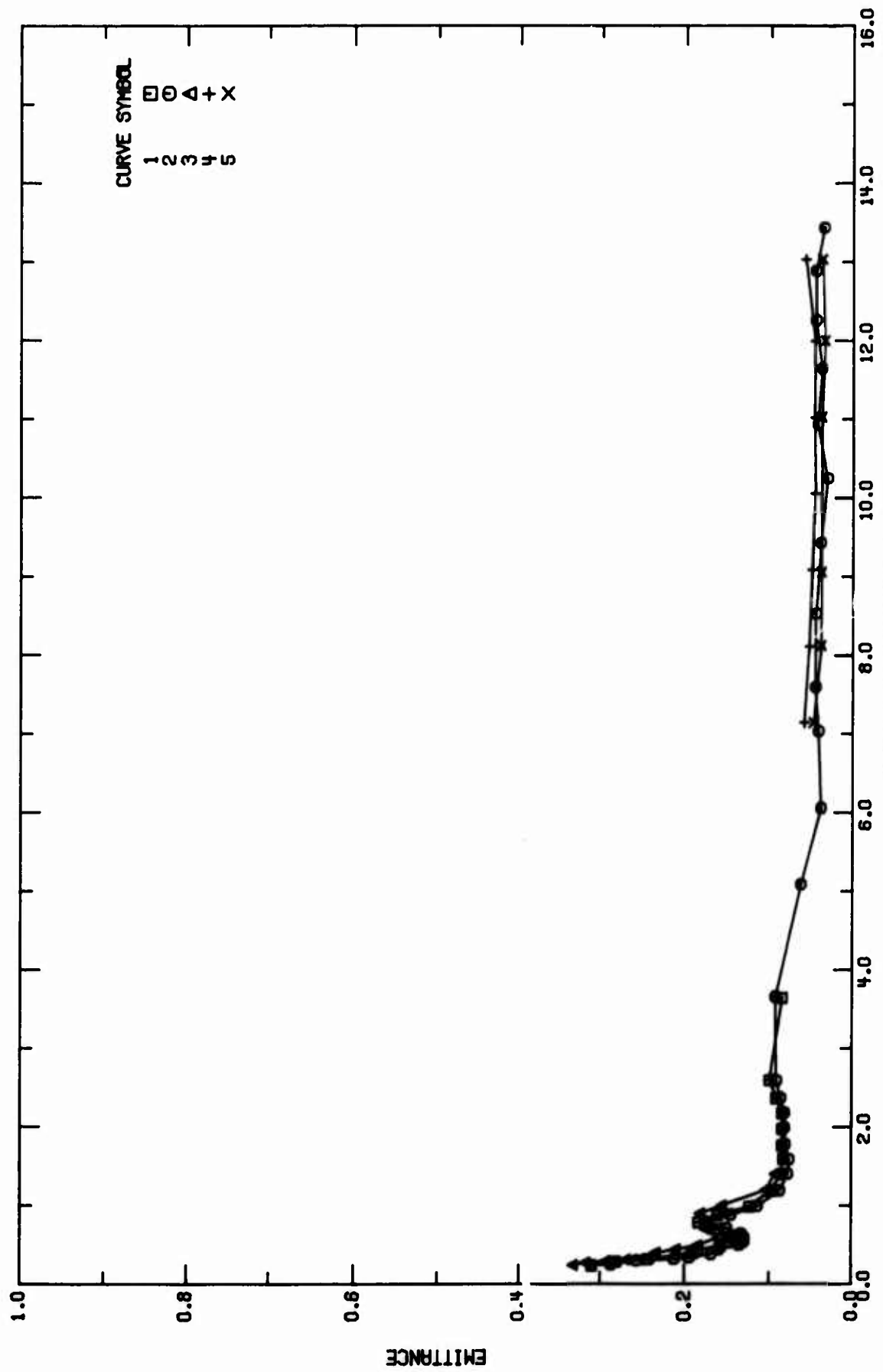


FIGURE 2-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

TABLE 2-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--------------|------|---------------------------------|----------------------|--------------------------------|---|
| 1 T29202 | Schocken, K. | 1963 | 0.29-3.65 | 323 | Aluminum Alloy 7075 Specimen 1 | Nominal composition: 5.6 Zn, 2.5 Mg, 1.6 Cu, 0.3 Cr, Al balance, surface roughness 3.2-4.4 microns, measurements in nitrogen. |
| 2 T29202 | Schocken, K. | 1963 | 0.24-26.9 | 323 | Aluminum Alloy 7075 Specimen 3 | Similar to the above specimen except surface roughness is 1.9-2.5 microns. |
| 3 T29202 | Schocken, K. | 1963 | 0.24-1.4 | 323 | Aluminum Alloy 7075 Specimen 4 | Similar to the above specimen except surface roughness is 3.2-4.5 microns. |
| 4 T20470 | Weber, D. | 1959 | 7.15-15.00 | 383 | 75 ST Aluminum | Specimen flat and smooth; reported error $\pm 50\%$. |
| 5 T20470 | Weber, D. | 1959 | 7.15-15.05 | 323 | 75 ST Aluminum | Similar to the above specimen. |

TABLE 2-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ |
|----------------|------------|----------------|------------|------------------------|------------|
| CURVE 1 | | | | | |
| T = 323. | | | | | |
| 0.24 | 0.310 | 0.80 | 0.144 | 0.34 | 0.240 |
| 0.29 | 0.280 | 0.99 | 0.113 | 0.40 | 0.233 |
| 0.32 | 0.242 | 1.19 | 0.087 | 0.44 | 0.210 |
| 0.40 | 0.190 | 1.40 | 0.077 | 0.49 | 0.185 |
| 0.44 | 0.184 | 1.59 | 0.075 | 0.60 | 0.159 |
| 0.49 | 0.157 | 1.78 | 0.080 | 0.70 | 0.175 |
| 0.54 | 0.148 | 1.99 | 0.081 | 0.90 | 0.182 |
| 0.60 | 0.145 | 2.18 | 0.081 | 1.09 | 0.155 |
| 0.70 | 0.159 | 2.37 | 0.086 | 1.20 | 0.103 |
| 0.79 | 0.183 | 2.59 | 0.091 | 1.40 | 0.093 |
| 0.88 | 0.160 | 3.66 | 0.093 | CURVE 3 (CONT.) | |
| 0.99 | 0.122 | 5.09 | 0.062 | T = 323. | |
| 1.19 | 0.097 | 6.06 | 0.038 | 7.15 | 0.058 |
| 1.40 | 0.085 | 7.04 | 0.041 | 8.12 | 0.052 |
| 1.60 | 0.082 | 8.54 | 0.045 | 9.10 | 0.049 |
| 1.77 | 0.084 | 9.44 | 0.039 | 10.07 | 0.046 |
| 1.98 | 0.084 | 10.26 | 0.031 | 11.04 | 0.047 |
| 2.18 | 0.094 | 10.95 | 0.043 | 12.01 | 0.046 |
| 2.37 | 0.091 | 11.66 | 0.038 | 13.05 | 0.057 |
| 2.60 | 0.099 | 12.27 | 0.045 | 14.02 | 0.053 |
| 3.65 | 0.084 | 12.90 | 0.045 | 15.00 | 0.078 |
| CURVE 2 | | | | | |
| T = 323. | | | | | |
| 0.24 | 0.310 | 13.45 | 0.035 | CURVE 4 | |
| 0.25 | 0.286 | 14.04 | 0.035 | T = 323. | |
| 0.30 | 0.255 | 14.04 | 0.043 | 7.15 | 0.058 |
| 0.32 | 0.211 | 14.65 | 0.053 | 8.12 | 0.052 |
| 0.34 | 0.194 | 16.19 | 0.029 | 9.10 | 0.049 |
| 0.38 | 0.168 | 18.26 | 0.035 | 10.07 | 0.046 |
| 0.44 | 0.158 | 19.95 | 0.031 | 11.04 | 0.047 |
| 0.50 | 0.134 | 21.71 | 0.037 | 12.01 | 0.046 |
| 0.54 | 0.129 | 24.35 | 0.037 | 13.05 | 0.057 |
| 0.59 | 0.129 | 26.80 | 0.061 | 14.02 | 0.053 |
| 0.60 | 0.136 | CURVE 3 | | 15.00 | 0.078 |
| 0.64 | 0.132 | T = 323. | | CURVE 5 | |
| 0.71 | 0.149 | 0.24 | 0.333 | T = 323. | |
| 0.79 | 0.174 | 0.27 | 0.318 | 7.15 | 0.047 |
| | | 0.29 | 0.293 | 8.13 | 0.038 |
| | | 0.31 | 0.268 | 9.06 | 0.038 |
| | | | | 11.04 | 0.038 |
| | | | | 12.01 | 0.034 |
| | | | | 13.05 | 0.037 |
| | | | | 14.02 | 0.037 |
| | | | | 15.00 | 0.044 |

b. Angular Spectral Emittance (Wavelength Dependence)

There are six sets of experimental data available for the wavelength dependence (0.3-15 μm) of the angular spectral emittance of Aluminum Alloy 7075-T6 for an incidence angle, $\theta = 25^\circ$. These values are tabulated in Table 2-6 and shown in Figure 2-4.

The recommended values tabulated in Table 2-4 and shown in Figure 2-3 for Aluminum Alloy 7075-T6 with surface roughness of about 0.0005-0.001 μm and the incident angle, $\theta = 25^\circ$, are primarily from the investigation of Edwards and Catton [T38391]. These values are considered accurate to within $\pm 15\%$ over the entire wavelength range. The angular spectral reflectance values for the similar material, but sandblasted with silicon carbide, are considerably higher than the values reported in Table 2-4. It is worth noting that Edwards and Catton [T38391] consider their values as the normal spectral emittance rather than the angular spectral emittance. Therefore, tabulated values from Table 2-4 may be applicable for the normal spectral emittance.

TABLE 2-4. RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ |
|---------------|------------|
| POLISHED | |
| 7075-T6 ALLOY | |
| T = 300 | |
| 0.4 | 0.178 |
| 0.5 | 0.160 |
| 0.6 | 0.151 |
| 0.7 | 0.149 |
| 0.8 | 0.143 |
| 0.9 | 0.124 |
| 1.0 | 0.102 |
| 1.2 | 0.074 |
| 1.4 | 0.057 |
| 1.6 | 0.047 |
| 1.8 | 0.041 |
| 2.0 | 0.038 |
| 2.8 | 0.035 |
| 3.0 | 0.035 |
| 3.8 | 0.035 |
| 4.0 | 0.035 |
| 5.0 | 0.035 |
| 6.0 | 0.034 |
| 7.0 | 0.034 |
| 8.0 | 0.033 |
| 9.0 | 0.032 |
| 10.0 | 0.031 |
| 10.6 | 0.030 |
| 11.0 | 0.030 |
| 12.0 | 0.030 |
| 13.0 | 0.030 |
| 14.0 | 0.029 |
| 15.0 | 0.029 |

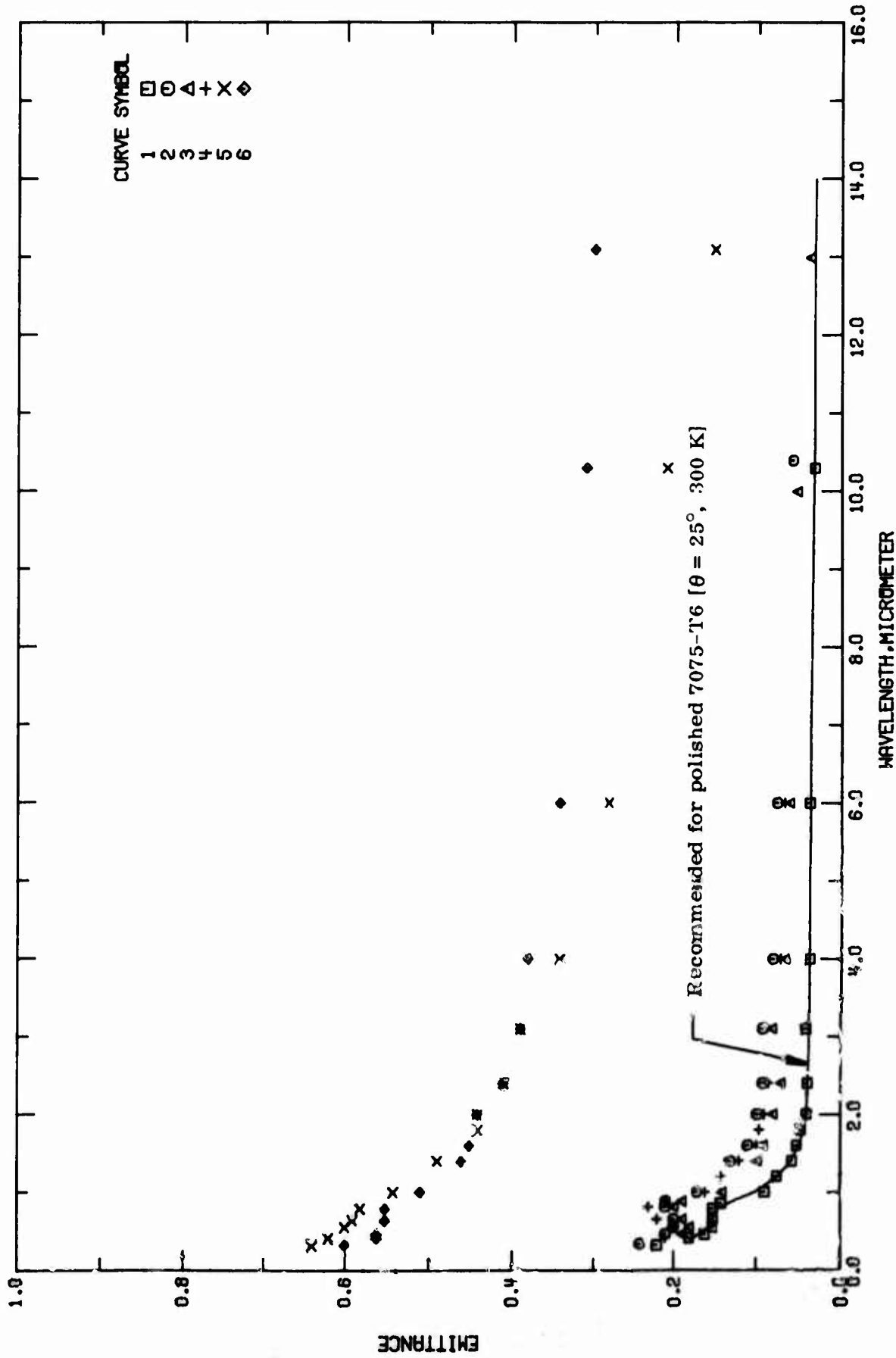
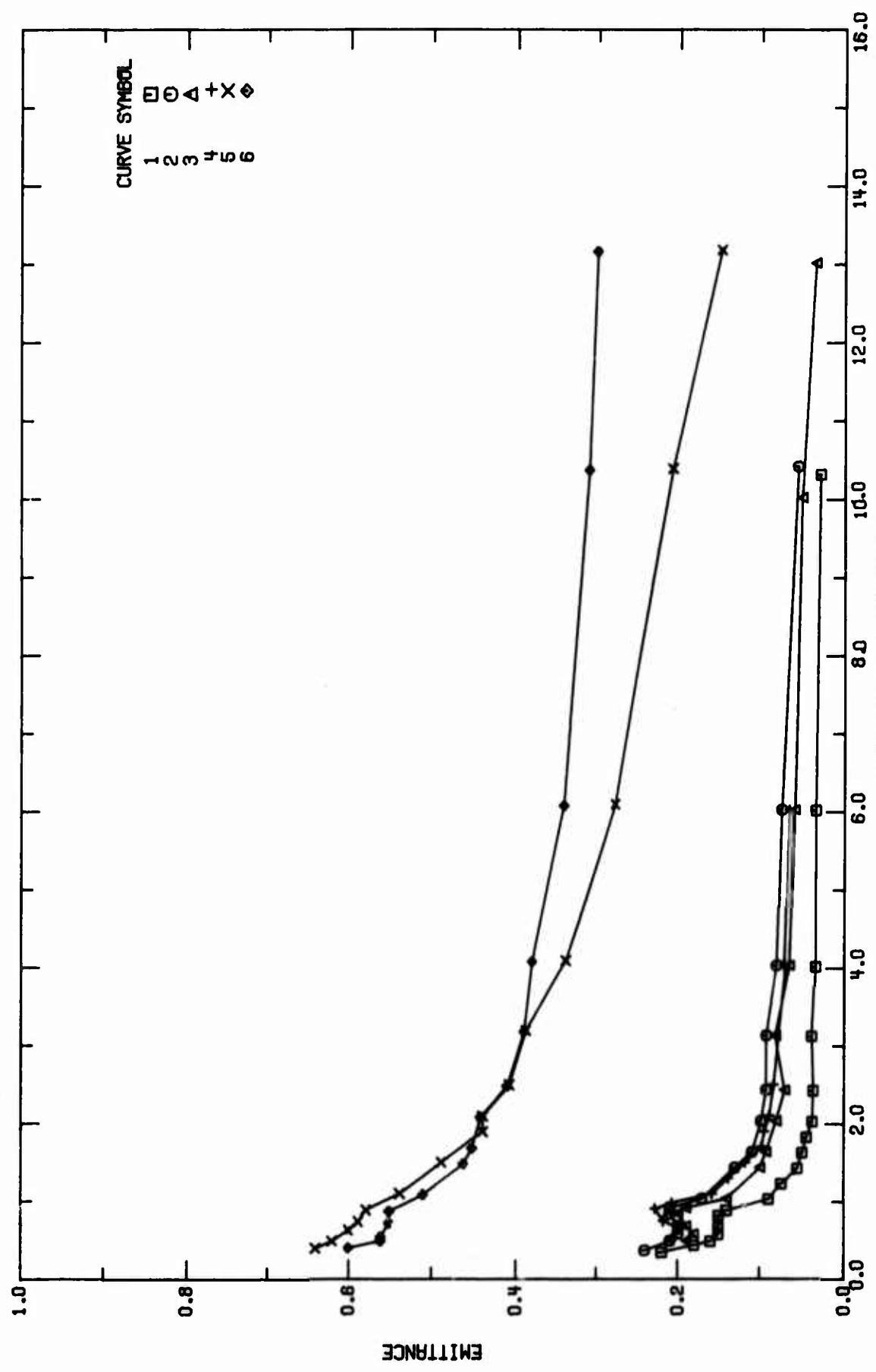


FIGURE 2-3. RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).



WAVELENGTH, MICROMETER

FIGURE 2-4. EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

TABLE 2-5. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T32391 | Edwards, D.K. and Catton, I. | 1965 | 0.32-15.0 | 306 | 7075-T6 | Polished specimen; Rms rough; 2-4 microinches; $\theta=25^\circ$. |
| 2 T36391 | Edwards, D.K. and Catton, I. | 1965 | 0.34-15.0 | 306 | 7075-T6 | Similar to the above specimen except sanded; grit mesh number is 150; grit sieve opening is 104 μ ; Rms roughness: 10-15 micro inches across, $\theta=25^\circ$. |
| 3 T38391 | Edwards, D.K. and Catton, I. | 1965 | 0.46-15.0 | 306 | 7075-T6 | Similar to the above specimen except grit mesh number is 80; grit sieve opening is 175 μ ; Rms roughness: 20-60 microinches in line and 150-170 microinches across; $\theta=25^\circ$. |
| 4 T38391 | Edwards, D.K. and Catton, I. | 1965 | 0.41-15.0 | 306 | 7075-T6 | Similar to the above specimen except grit mesh number is 40; grit sieve opening 42 μ ; Rms roughness: 50-100 microinches in line and 270-300 microinches across; $\theta=25^\circ$. |
| 5 T35391 | Edwards, D.K. and Catton, I. | 1965 | 0.32-15.0 | 306 | 7075-T6 | Similar to the specimen in curve 6 except sandblasted with 250 mesh silicon carbide; Rms roughness 10-15 microinches; $\theta=25^\circ$. |
| 6 T38391 | Edwards, D.K. and Catton, I. | 1965 | 0.32-15.0 | 306 | 7075-T6 | Similar to the above specimen except sandblasted with 60 mesh Silicon Carbide; Rms roughness 250-300 microinches. |

TABLE 2-6. EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|---------------------|------------|---------------------|------------|---------------------|------------|-----------------|------------|
| CURVE 1 T = 306. | | CURVE 3 T = 306. | | CURVE 5 T = 306. | | CURVE 6 (CONT.) | |
| 0.32 | 0.22 | 0.46 | 0.19 | 0.32 | 0.64 | 17.1 | 0.29 |
| 0.41 | 0.18 | 0.55 | 0.18 | 0.41 | 0.62 | 19.2 | 0.28 |
| 0.46 | 0.16 | 0.65 | 0.19 | 0.55 | 0.60 | 21.1 | 0.27 |
| 0.55 | 0.15 | 0.81 | 0.20 | 0.64 | 0.59 | | |
| 0.64 | 0.15 | 0.88 | 0.19 | 0.79 | 0.58 | | |
| 0.79 | 0.15 | 1.0 | 0.14 | 1.0 | 0.54 | | |
| 0.86 | 0.14 | 1.4 | 0.10 | 1.4 | 0.49 | | |
| 1.0 | 0.090 | 1.6 | 0.093 | 1.8 | 0.44 | | |
| 1.2 | 0.075 | 2.0 | 0.081 | 2.0 | 0.44 | | |
| 1.4 | 0.056 | 2.4 | 0.071 | 2.4 | 0.41 | | |
| 1.6 | 0.050 | 3.1 | 0.082 | 3.1 | 0.39 | | |
| 1.8 | 0.045 | 4.0 | 0.066 | 4.0 | 0.34 | | |
| 2.0 | 0.038 | 6.0 | 0.061 | 6.0 | 0.28 | | |
| 2.4 | 0.037 | 10.0 | 0.052 | 10.3 | 0.21 | | |
| 3.1 | 0.039 | 13.0 | 0.036 | 13.1 | 0.15 | | |
| 4.0 | 0.035 | 15.0 | 0.036 | 15.0 | 0.13 | | |
| 6.0 | 0.035 | | | 17.1 | 0.12 | | |
| 10.3 | 0.030 | CURVE 4 T = 306. | | 19.2 | 0.11 | | |
| 15.0 | 0.030 | | | 21.1 | 0.11 | | |
| CURVE 2 T = 306. | | CURVE 6 T = 306. | | | | | |
| 0.34 | 0.24 | 0.41 | 0.21 | 0.32 | 0.60 | | |
| 0.46 | 0.21 | 0.55 | 0.20 | 0.41 | 0.56 | | |
| 0.55 | 0.20 | 0.65 | 0.22 | 0.46 | 0.56 | | |
| 0.65 | 0.20 | 0.81 | 0.23 | 0.64 | 0.55 | | |
| 0.81 | 0.21 | 0.89 | 0.21 | 0.79 | 0.55 | | |
| 0.86 | 0.21 | 1.0 | 0.15 | 1.0 | 0.51 | | |
| 1.0 | 0.17 | 1.2 | 0.14 | 1.4 | 0.46 | | |
| 1.4 | 0.13 | 1.4 | 0.12 | 1.6 | 0.45 | | |
| 1.6 | 0.11 | 1.6 | 0.097 | 2.0 | 0.44 | | |
| 2.0 | 0.099 | 2.4 | 0.086 | 2.4 | 0.41 | | |
| 2.4 | 0.093 | 4.0 | 0.072 | 3.1 | 0.39 | | |
| 3.1 | 0.093 | 6.0 | 0.067 | 4.0 | 0.38 | | |
| 4.0 | 0.081 | 15.0 | 0.051 | 6.0 | 0.34 | | |
| 6.0 | 0.076 | | | 10.3 | 0.31 | | |
| 10.4 | 0.057 | | | 13.1 | 0.30 | | |
| 15.0 | 0.051 | | | 15.0 | 0.29 | | |

c. Normal Spectral Reflectance (Wavelength Dependence)

There are no experimental data sets available for Aluminum Alloy 7075, however only one set of experimental data is available for the wavelength dependence (2.8-15.0 μm) of the normal spectral reflectance of Aluminum Alloy 7075-T6 alloy. This is tabulated in Table 2-9 and shown in Figure 2-6.

(1) Aluminum Alloy 7075

The recommended values tabulated in Table 2-7 and shown in Figure 2-5 are for Aluminum Alloy 7075 with surface roughness of about 0.0005-0.0006 μm . These values calculated from the normal spectral emittance data (see Section 4.2. b) are considered accurate to about $\pm 15\%$ over the entire wavelength range.

(2) Aluminum Alloy 7075-T6

The recommended values tabulated in Table 2-7 and shown in Figure 2-5 for Aluminum Alloy 7075-T6 clad sheet are primarily from the investigation of Cunningham [A00027]. These values are considered accurate to within $\pm 15\%$ over the entire temperature range.

TABLE 2-7. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|--------------------------------------|--------|---|--------|
| AL ALLOY 7075 POLISHED T = 323 | | AL ALLOY 7075-T6 ROLLED SHEET T = 293 | |
| 0.3 | 0.740 | 2.0 | 0.957 |
| 0.4 | 0.815 | 3.0 | 0.960 |
| 0.5 | 0.864 | 3.8 | 0.970 |
| 0.6 | 0.869 | 4.0 | 0.971 |
| 0.7 | 0.850 | 5.0 | 0.976 |
| 0.8 | 0.836 | 6.0 | 0.977 |
| 0.9 | 0.852 | 7.0 | 0.978 |
| 1.0 | 0.820 | 8.0 | 0.979 |
| 1.2 | 0.910 | 9.0 | 0.980 |
| 1.4 | 0.922 | 10.0 | 0.981 |
| 1.6 | 0.925 | 10.6 | 0.982 |
| 1.8 | 0.922 | 11.0 | 0.982 |
| 2.0 | 0.917 | 12.0 | 0.982 |
| 2.4 | 0.912 | 13.0 | 0.982 |
| 2.8 | 0.908 | 14.0 | 0.983 |
| 3.0 | 0.908 | 15.0 | 0.983 |
| 3.4 | 0.910 | | |
| 3.8 | 0.910 | | |
| 4.0 | 0.922 | | |
| 4.5 | 0.930 | | |
| 5.0 | 0.936 | | |
| 6.0 | 0.946 | | |
| 7.0 | 0.952 | | |
| 8.0 | 0.954 | | |
| 9.0 | 0.955 | | |
| 10.0 | 0.955 | | |
| 10.6 | 0.956 | | |
| 11.0 | 0.957 | | |
| 12.0 | 0.957 | | |
| 13.0 | 0.957 | | |
| 14.0 | 0.958 | | |
| 15.0 | 0.958 | | |

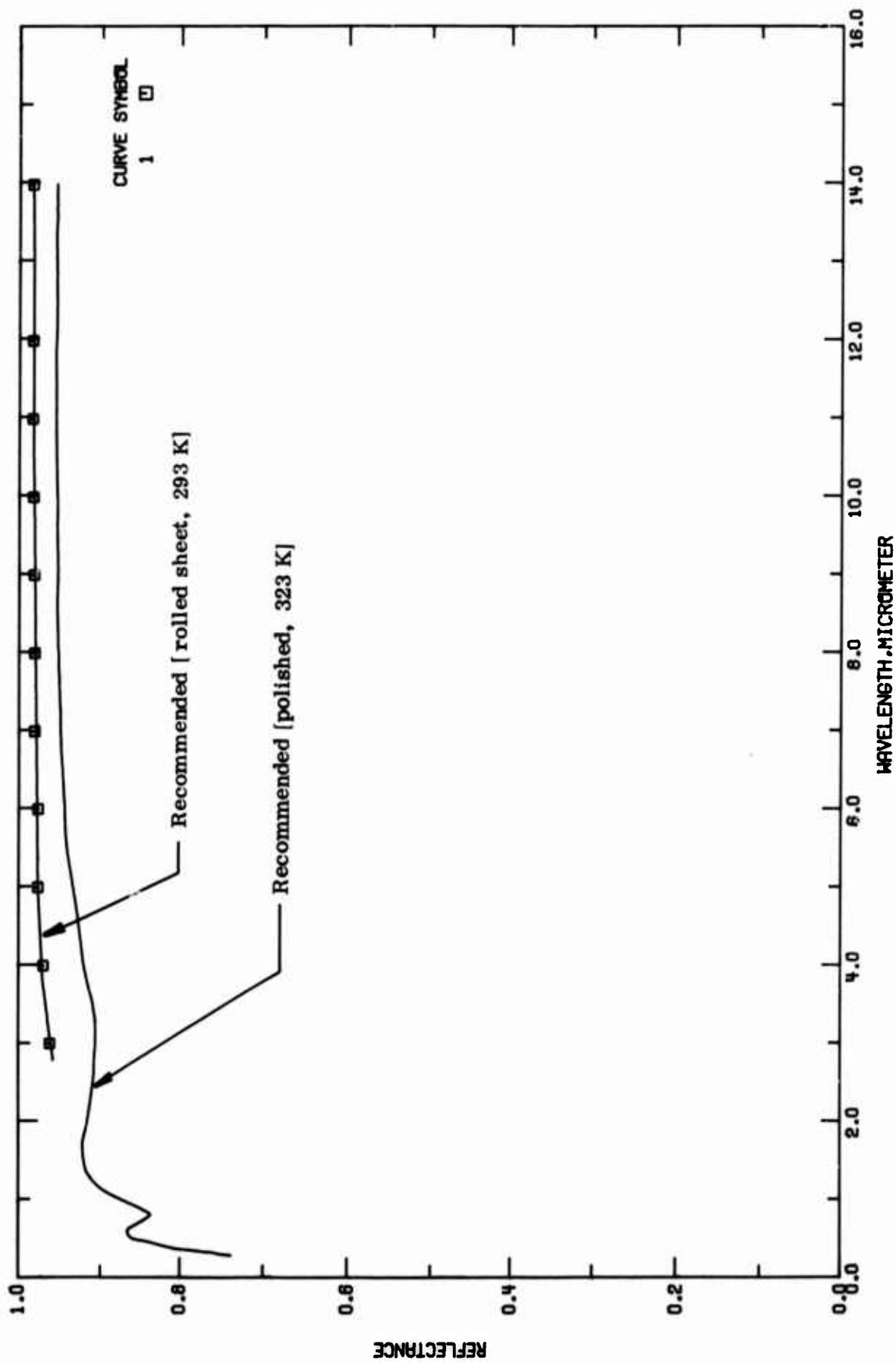


FIGURE 2-5. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

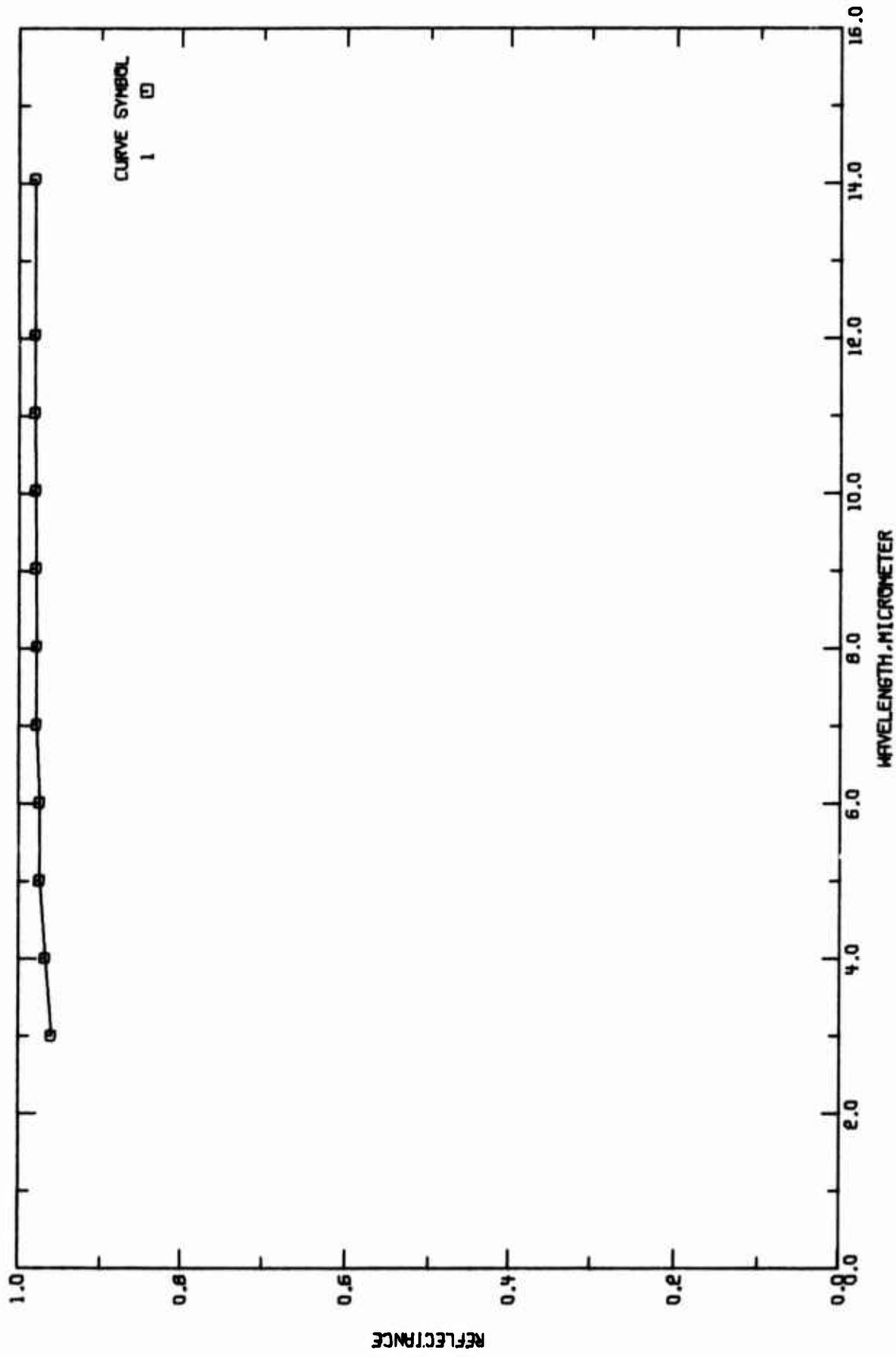


FIGURE 2-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY AL-7075 (WAVELENGTH DEPENDENCE).

TABLE 2-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (Wavelength Dependence)

| Cat. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00027 | Cumington, G.R. | 1975 | 3-15 | 293 | 7075 T6 | Rolled sheet. |

TABLE 2-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------|--------|
| CURVE 1 | |
| T = 293. | |
| 3. | 0.961 |
| 4. | 0.969 |
| 5. | 0.976 |
| 6. | 0.976 |
| 7. | 0.980 |
| 8. | 0.980 |
| 9. | 0.981 |
| 10. | 0.982 |
| 11. | 0.983 |
| 12. | 0.983 |
| 14. | 0.983 |
| 15. | 0.985 |
| 18. | 0.986 |
| 20. | 0.986 |
| 22. | 0.986 |
| 24. | 0.986 |

d. Angular Spectral Reflectance (Wavelength Dependence)

There are no experimental data available for this subproperty. The recommended values for Aluminum Alloy 7075-T6 with surface roughness 0.0005-0.001 μm and incidence angle, $\theta=25^\circ$, are calculated from the recommended values of the angular spectral emittance (see Section 4.2.b). These values tabulated in Table 2-10 and shown in Figure 2-7 are considered accurate to within $\pm 15\%$ over the entire wavelength range. As discussed in Section 4.2.b, these values may be applicable for the normal spectral reflectance.

TABLE 2-10. RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|---------------|--------|
| POLISHED | |
| 7075-T6 ALLOY | |
| T = 300 | |
| 0.4 | 0.822 |
| 0.5 | 0.840 |
| 0.6 | 0.849 |
| 0.7 | 0.851 |
| 0.8 | 0.857 |
| 0.9 | 0.876 |
| 1.0 | 0.892 |
| 1.2 | 0.926 |
| 1.4 | 0.943 |
| 1.6 | 0.953 |
| 1.8 | 0.959 |
| 2.0 | 0.962 |
| 2.8 | 0.965 |
| 3.0 | 0.965 |
| 3.8 | 0.965 |
| 4.0 | 0.965 |
| 5.0 | 0.965 |
| 6.0 | 0.966 |
| 7.0 | 0.966 |
| 8.0 | 0.967 |
| 9.0 | 0.968 |
| 10.0 | 0.969 |
| 10.6 | 0.970 |
| 11.0 | 0.970 |
| 12.0 | 0.970 |
| 13.0 | 0.970 |
| 14.0 | 0.971 |
| 15.0 | 0.971 |

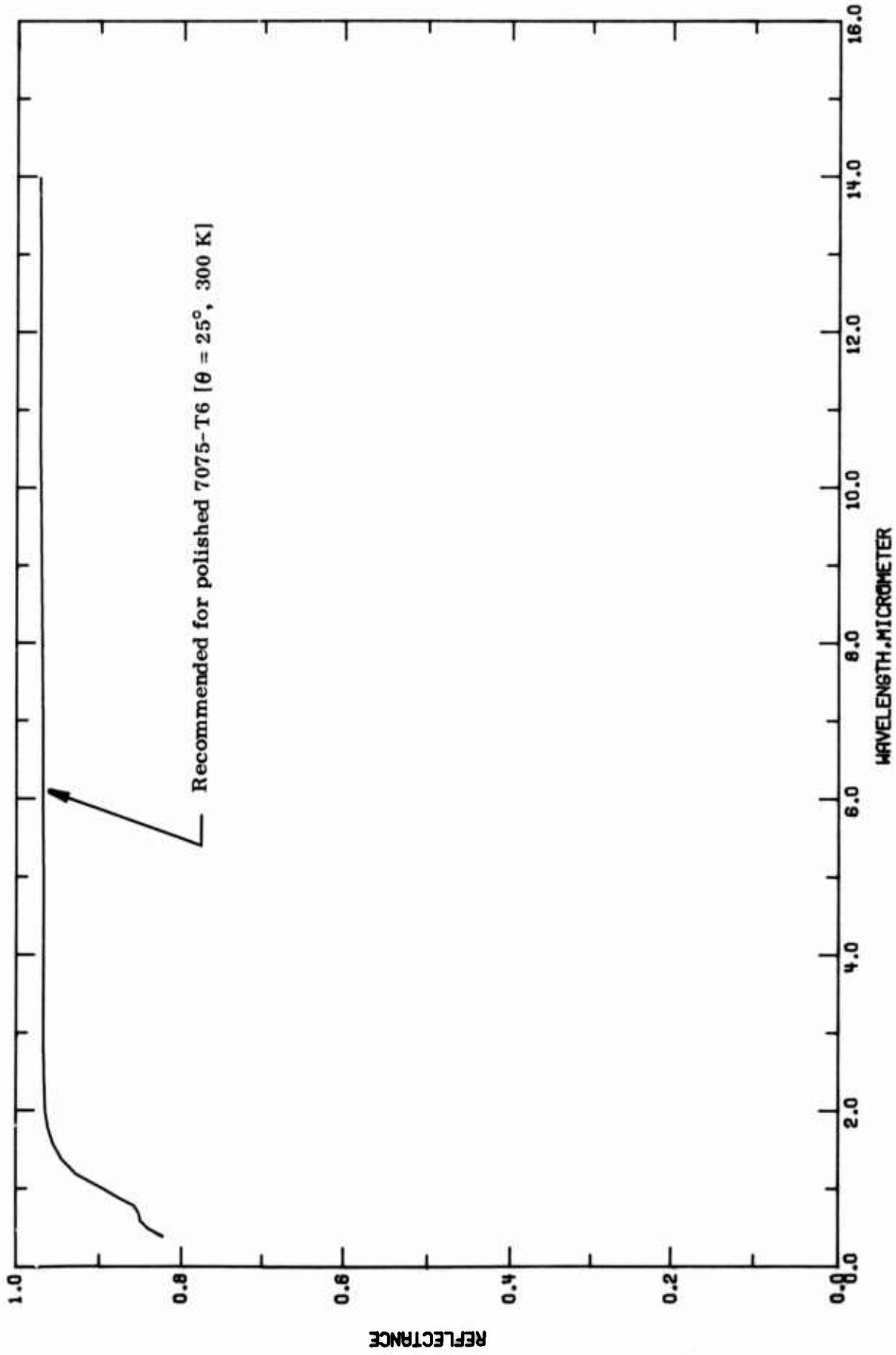


FIGURE 2-7. RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

There are no experimental data available for this subproperty.

(1) Aluminum Alloy 7075

The recommended values tabulated in Table 2-11 and shown in Figure 2-8 are for Aluminum Alloy 7075 with surface roughness of about 0.0005-0.0006 μm . These values calculated from the recommended values for the normal spectral emittance tabulated in Table 2-1 are considered accurate to about $\pm 15\%$ over the entire wavelength range.

(2) Aluminum Alloy 7075-T6

The recommended values tabulated in Table 2-11 and shown in Figure 2-8 are for Aluminum Alloy 7075-T6 clad sheet. These values calculated from the normal spectral emittance data tabulated in Table 2-1 are considered accurate to about $\pm 15\%$ over the entire wavelength range.

TABLE 2-11. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|---------------------------|----------|-------------------------|----------|
| POLISHED ALLOY T = 323 | | ROLLED SHEET T = 293 | |
| 0.3 | 0.260 | 2.8 | 0.043 |
| 0.4 | 0.185 | 3.0 | 0.040 |
| 0.5 | 0.136 | 3.8 | 0.030 |
| 0.6 | 0.131 | 4.0 | 0.029 |
| 0.7 | 0.150 | 5.0 | 0.024 |
| 0.8 | 0.164 | 6.0 | 0.023 |
| 0.9 | 0.148 | 7.0 | 0.022 |
| 1.0 | 0.120 | 8.0 | 0.021 |
| 1.2 | 0.090 | 9.0 | 0.020 |
| 1.4 | 0.078 | 10.0 | 0.019 |
| 1.6 | 0.075 | 10.6 | 0.018 |
| 1.8 | 0.078 | 11.0 | 0.018 |
| 2.0 | 0.083 | 12.0 | 0.018 |
| 2.4 | 0.088 | 13.0 | 0.018 |
| 2.8 | 0.092 | 14.0 | 0.017 |
| 3.0 | 0.092 | 15.0 | 0.017 |
| 3.4 | 0.090 | | |
| 3.8 | 0.082 | | |
| 4.0 | 0.078 | | |
| 4.5 | 0.070 | | |
| 5.0 | 0.064 | | |
| 6.0 | 0.054 | | |
| 7.0 | 0.048 | | |
| 8.0 | 0.046 | | |
| 9.0 | 0.045 | | |
| 10.0 | 0.045 | | |
| 10.6 | 0.044 | | |
| 11.0 | 0.043 | | |
| 12.0 | 0.043 | | |
| 13.0 | 0.043 | | |
| 14.0 | 0.042 | | |
| 15.0 | 0.042 | | |

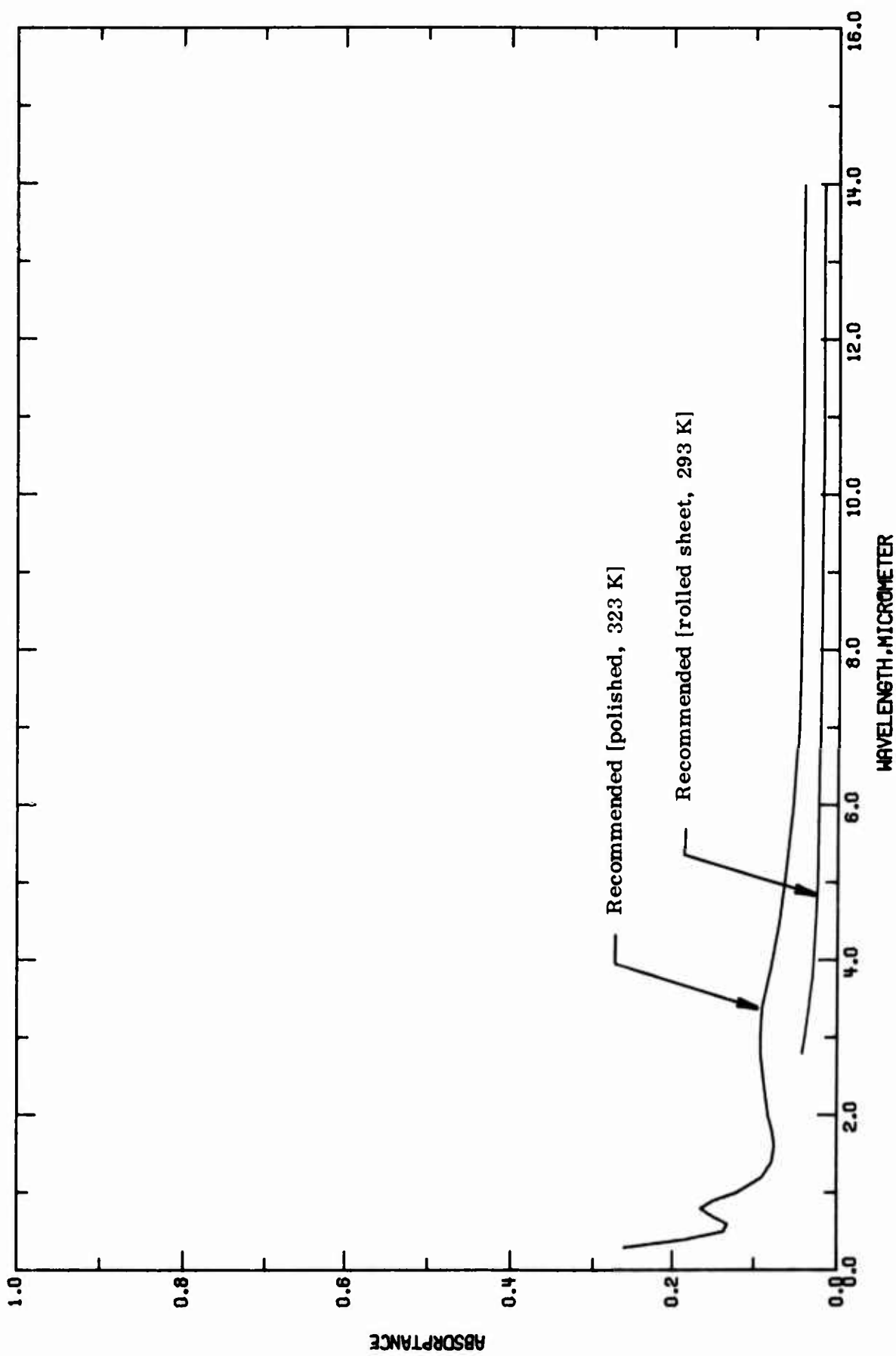


FIGURE 2-8. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

f. Angular Spectral Absorptance (Wavelength Dependence)

There are no experimental data available for this subproperty. The recommended values tabulated in Table 2-12 and shown in Figure 2-9 are for Aluminum Alloy 7075-T6 with surface roughness of about 0.0005-0.001 μm , and incidence angle, $\theta = 25^\circ$. These values calculated from the recommended values tabulated in Table 2-4 are considered accurate to about $\pm 15\%$ over the entire wavelength range. As discussed in Section 4.2.b these values may be applicable for the normal spectral absorptance.

TABLE 2-12. RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|---------------|----------|
| POLISHED | |
| 7075-T6 ALLOY | |
| T = 300 | |
| 0.4 | 0.170 |
| 0.5 | 0.160 |
| 0.6 | 0.151 |
| 0.7 | 0.149 |
| 0.8 | 0.143 |
| 0.9 | 0.124 |
| 1.0 | 0.102 |
| 1.2 | 0.074 |
| 1.4 | 0.057 |
| 1.6 | 0.047 |
| 1.8 | 0.041 |
| 2.0 | 0.038 |
| 2.6 | 0.035 |
| 3.0 | 0.035 |
| 3.8 | 0.035 |
| 4.0 | 0.035 |
| 5.0 | 0.035 |
| 6.0 | 0.034 |
| 7.0 | 0.034 |
| 8.0 | 0.033 |
| 9.0 | 0.032 |
| 10.0 | 0.031 |
| 10.6 | 0.030 |
| 11.0 | 0.030 |
| 12.0 | 0.030 |
| 13.0 | 0.030 |
| 14.0 | 0.029 |
| 15.0 | 0.029 |

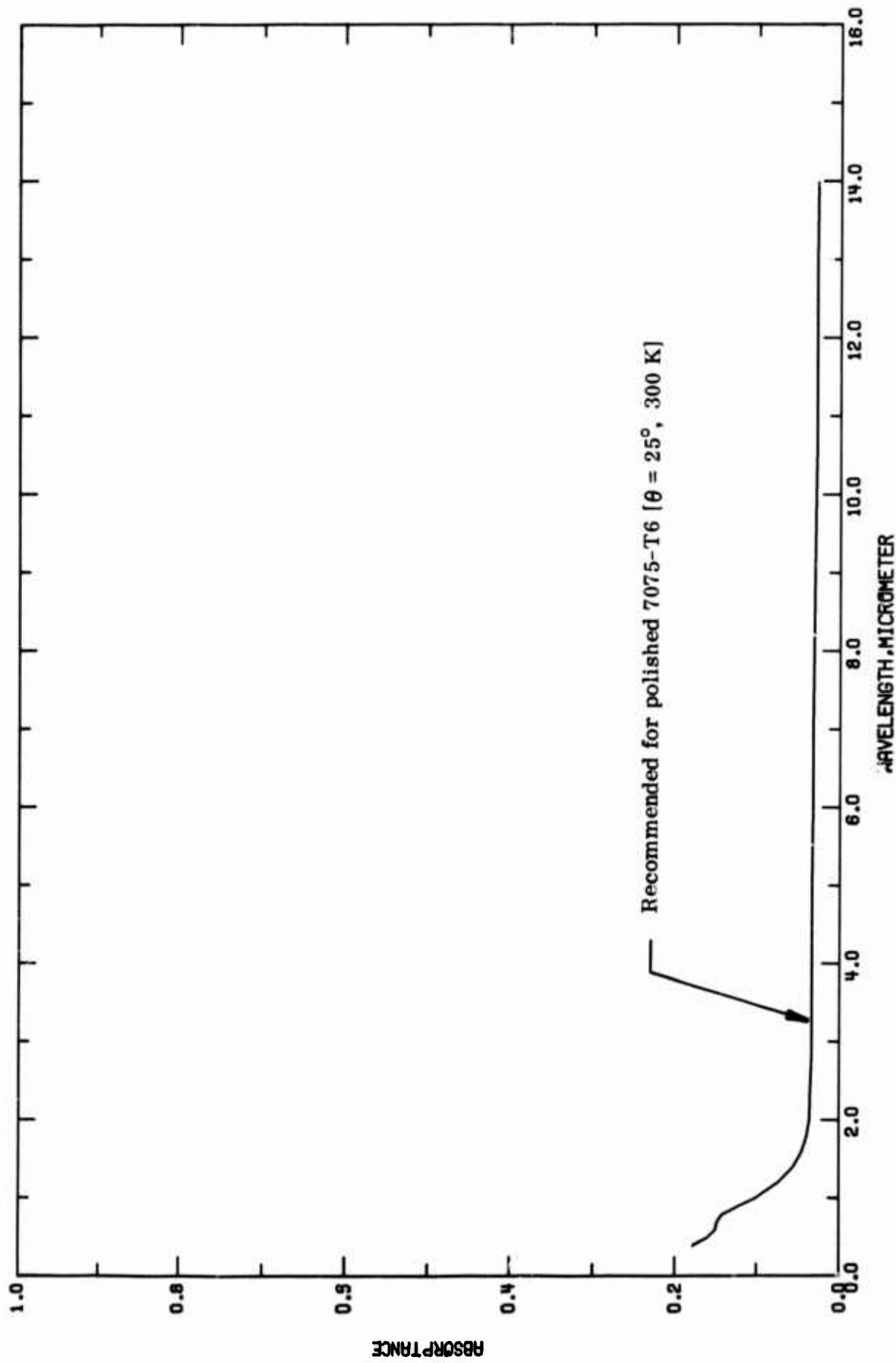


FIGURE 2-9. RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF ALUMINUM ALLOY 7075 (WAVELENGTH DEPENDENCE).

g. Transmittance

Although it is true that metals and alloys in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms.

As an aircraft/spacecraft structural material, this alloy is not used in the form of extremely thin films and therefore is opaque that is, its transmittance is zero.

4.3. AISI 304 Stainless Steel

The family of steel known as "stainless steel" covers an exceptionally wide range. About 35-40 different combinations of ingredients have been used by various manufacturers. Primarily all stainless steels have a base alloy of Fe and Cr. The nominal composition of s.s. 304 is (18-20%) Cr, (8-12%) Ni, 2% Mn, 1% Si, 0.08% C, and Fe balance. The composition of s.s. 304-L type is essentially the same except the composition of carbon is lowered to 0.03%.

Chromium, when added in excess of 10%, makes alloy heat and corrosion resistance. Other elements are added to obtain special characteristics. The most important of these in the case of stainless steel is nickel which increases its corrosion resistance and workability of the alloy. This addition causes a structural change which is known as austenitic which makes the alloy nonhardenable and nonmagnetic. It is possible to weld AISI 304 stainless in moderate thickness without subsequent heat treatment to restore corrosion resistance, whereas 304-L variety, due to its low carbon content, has lower hazard of carbide precipitation after welding or annealing.

Various properties and uses of this alloy are discussed in detail in [A00005]. Some of the physical properties can be summarized as follows:

| | |
|--|----------------------------|
| Density: | 7.9 g cm ⁻³ |
| Melting range: | 1670-1727 K |
| Electrical resistivity: at room temperature | 72 $\mu\Omega$ cm |
| Modulus of elasticity in tension: | 28 x 10 ⁶ psi |
| Modulus of elasticity in torsion: | 12.5 x 10 ⁶ psi |

a. Normal Spectral Emittance (Wavelength Dependence)

There are 31 sets of experimental data available for the wavelength dependence (0.20-27 μm) of the normal spectral emittance of AISI 304 Stainless Steel for oxidized and anodized surfaces covering the temperature range from room temperature to 1273 K. These are tabulated in Table 3-3 and shown in Figure 3-2.

(1) Polished AISI 304 Stainless Steel

The recommended values at 293 K tabulated in Table 3-1 and shown in Figure 3-1 are for polished and unoxidized surfaces are primarily from the investigations of Rolling and Funai [T47998, T29202]. These values are considered accurate to within $\pm 15\%$ over the entire wavelength range.

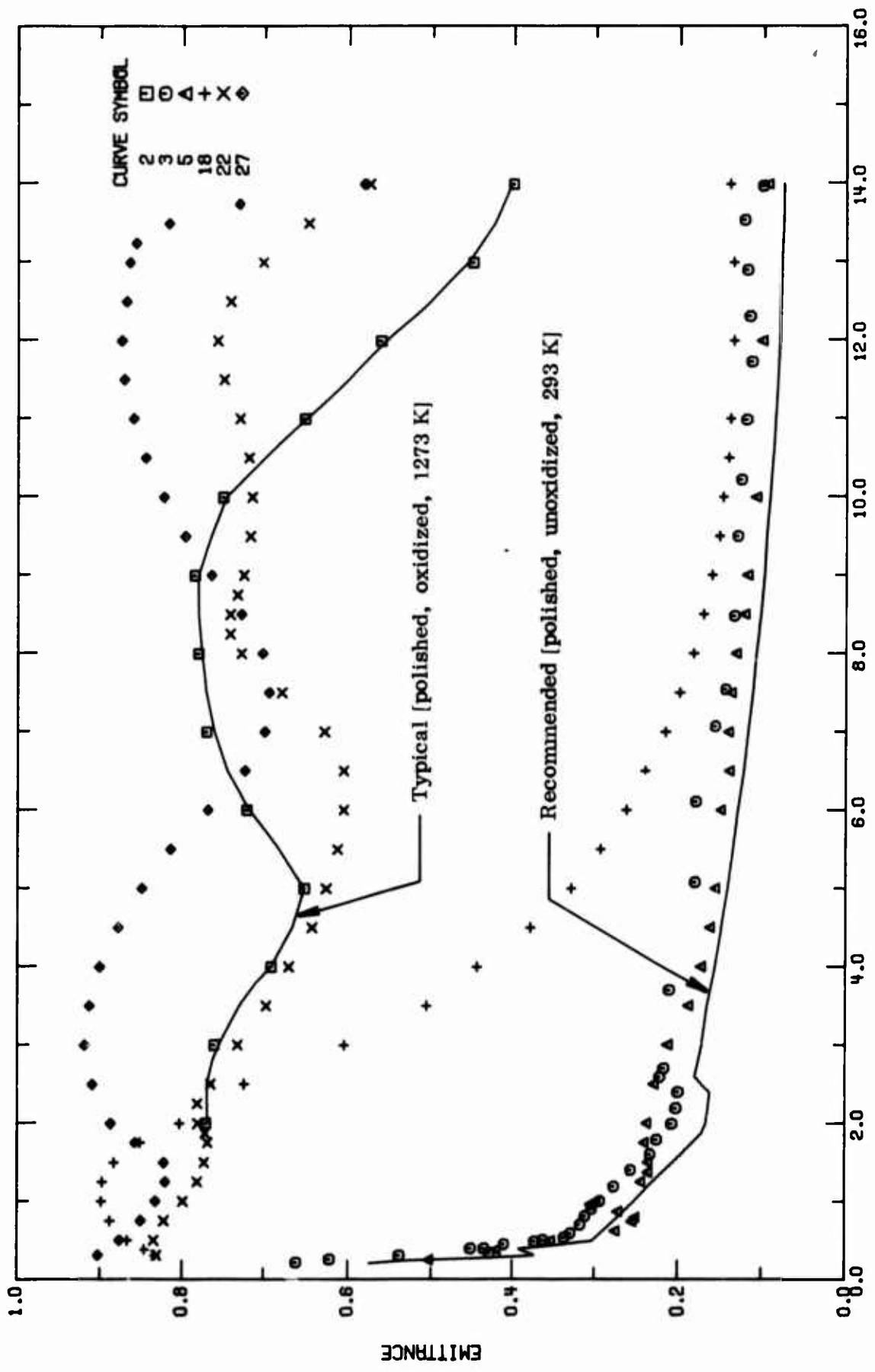
(2) Oxidized AISI 304 Stainless Steel

The typical values at 1273 K tabulated in Table 3-1 and shown in Figure 3-1 are for polished and oxidized surfaces of a sample heated in air for about six hours at 1273 K. These values, primarily from the investigations of Blau, et al. [T16606] are considered accurate to about $\pm 30\%$ over the entire wavelength range.

TABLE 3-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | POLISHED | | λ | ϵ |
|-----------|------------|-------------------------|---------------------------------|-----------|------------|
| | | NOT OXIDIZED T = 293 | NOT OXIDIZED T = 293 (CONT.) | | |
| 0.22 | 0.572 | 13.50 | 0.077 | 2.00 | 0.7648† |
| 0.25 | 0.532 | 14.00 | 0.076 | 2.50 | 0.7698 |
| 0.30 | 0.392 | | | 2.80 | 0.7628 |
| 0.32 | 0.372 | | | 3.00 | 0.7548 |
| 0.40 | 0.392 | | | 3.50 | 0.7298 |
| 0.50 | 0.302 | | | 3.80 | 0.7088 |
| 0.80 | 0.272 | | | 4.00 | 0.6908 |
| 1.00 | 0.252 | | | 4.50 | 0.6648 |
| 1.50 | 0.206 | | | 5.00 | 0.6508 |
| 1.80 | 0.172 | | | 5.50 | 0.6808 |
| 2.00 | 0.167 | | | 6.00 | 0.7178 |
| 2.20 | 0.164 | | | 6.50 | 0.7448 |
| 2.40 | 0.162 | | | 7.00 | 0.7688 |
| 2.50 | 0.172 | | | 7.50 | 0.7788 |
| 2.60 | 0.180 | | | 8.00 | 0.7768 |
| 2.80 | 0.176 | | | 8.50 | 0.7808 |
| 3.00 | 0.172 | | | 9.00 | 0.7818 |
| 3.50 | 0.165 | | | 9.50 | 0.7658 |
| 3.80 | 0.160 | | | 10.00 | 0.7468 |
| 4.00 | 0.156 | | | 10.60 | 0.6898 |
| 4.50 | 0.148 | | | 11.00 | 0.6488 |
| 5.00 | 0.140 | | | 11.50 | 0.6008 |
| 5.50 | 0.134 | | | 12.00 | 0.5548 |
| 6.00 | 0.128 | | | 12.50 | 0.5028 |
| 6.50 | 0.121 | | | 13.00 | 0.4568 |
| 7.00 | 0.116 | | | 13.50 | 0.4248 |
| 7.50 | 0.111 | | | 14.00 | 0.4028 |
| 8.00 | 0.107 | | | | |
| 8.50 | 0.102 | | | | |
| 9.00 | 0.098 | | | | |
| 9.50 | 0.096 | | | | |
| 10.00 | 0.092 | | | | |
| 10.50 | 0.089 | | | | |
| 10.60 | 0.086 | | | | |
| 11.00 | 0.086 | | | | |
| 11.50 | 0.083 | | | | |
| 12.00 | 0.081 | | | | |
| 12.50 | 0.080 | | | | |
| 13.00 | 0.079 | | | | |

† VALUE FOLLOWED BY A "B" IS TYPICAL.



WAVELENGTH, MICROMETER

FIGURE 3-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

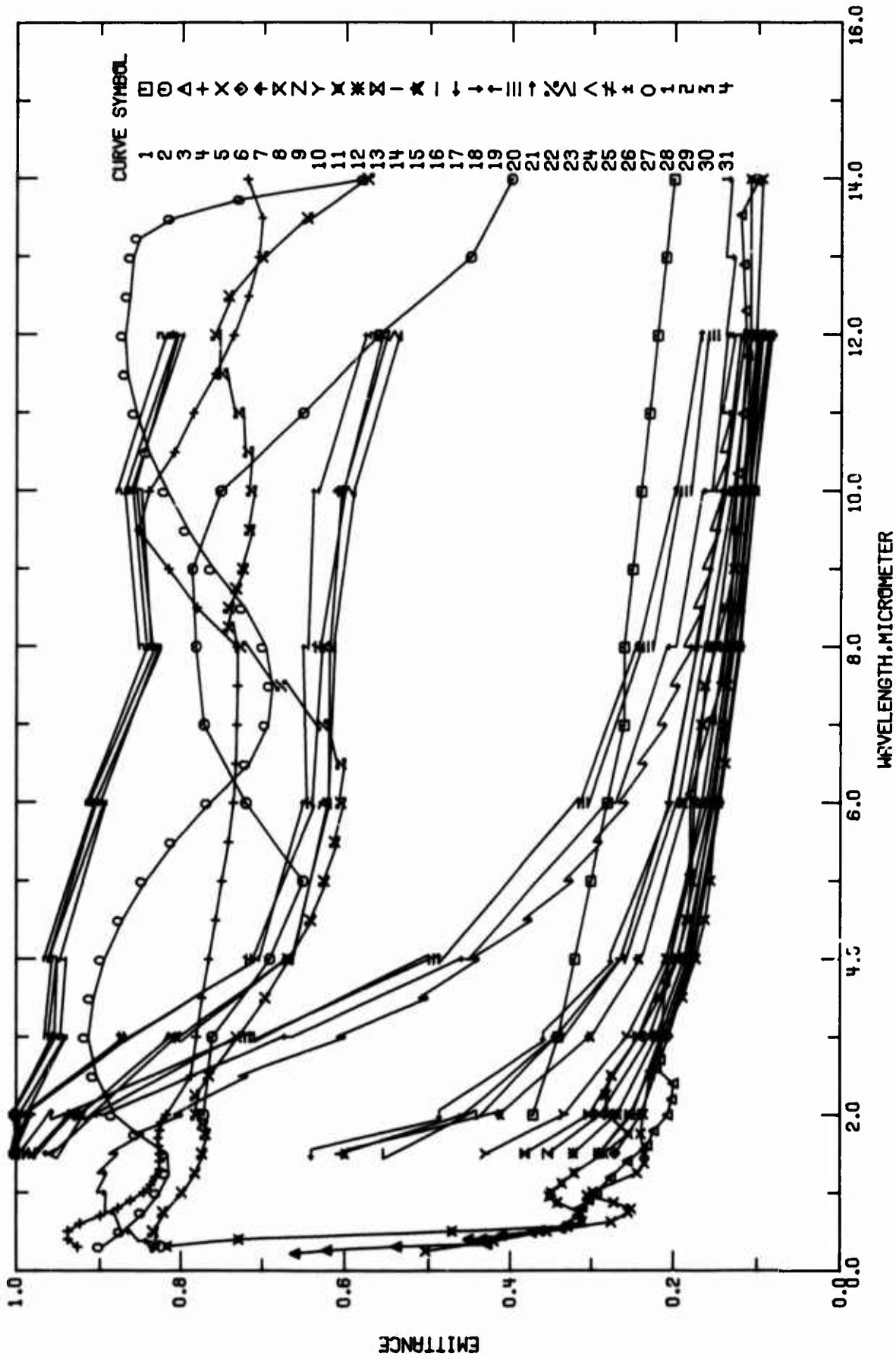


FIGURE 3-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

TABLE 3-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T16606 | Blau, H. H., March, J. B., Martin, W. S., Jasperse, J. R., and Chaffee, E. | 1960 | 2.0-14.0 | 873 | | Nominal composition: 18.00-20.00 Cr, 8.00-12.00 Ni; 2.00 max Mn, 1.00 max Si, 0.08 max C, Fe balance; oxidized in air for 3 hr at 873 K; measured in air; $\theta \sim 0^\circ$. |
| 2 T16606 | Blau, H. H., et al. | 1960 | 2.0-14.0 | 1273 | | Different sample, same as above specimen and conditions except oxidized in air for 6 hr at 1273 K. |
| 3 T29202 | NASA Technical Note No. D-1523 | 1963 | 0.20-27.00 | 323 | | Nominal composition: 18.00-20.00 Cr, 8.00-12.00 Ni; 2.00 max Mn, 1.00 max Si, 0.08 max C, Fe balance; surface roughness 0.75 micro-inches (center line avg); measured in nitrogen; computed from $\epsilon = 1 - R$ (29, 5); author indicated that slight error in transition region of 2.5 μ to 6.5 μ , deviation around 6 μ can be attributed to water vapor absorption, apparent rise at 24 to 27 μ due to scattered light; $\theta \sim 5^\circ$. |
| 4 T76814 | Conrardy, W. P. | 1963 | 0.3-21.0 | 1255 | | Chemical composition furnished by the supplier, 0.08 C, 1.0 Si, 2.0 Mn, 8-11 Ni, 18-20 Cr and Fe balance; disk specimen machined from rod stock obtained from Ducommun Metals and Supply Company; oxide formed by heating in air at 1255 K for 2 hr; stabilized after 30 days at 922 K. |
| 5 T47993 | Rolling, R. E. and Fusai, A. I. | 1967 | 0.25-18.9 | 300 | 1S | Sample 2 x 8 x 0.015 in. obtained with type 2B (bright, annealed) surface finish; 18.37 Cr, 8.89 Ni, 1.80 Mn, 0.50 Si, 0.055 C, 0.025 P, 0.007 S, and Fe balance; electropolished and cleaned using the following procedure: Step 1, soak 5 min. in $\text{Na}_2\text{P}_2\text{O}_7$ solution (60 g/liter) at 130 F, Step 2, electropolish for 20 min in a $\text{H}_2\text{PO}_4\text{-H}_2\text{SO}_4$ solution at 80 F, Step 3, rinse with distilled water, Step 4, dip in solution of nitric acid (100 ml per liter) and sodium dichromate (20 g per liter), Step 5, rinse and dry, rms roughness 0.33 μm ; not oxidized surface. |
| 6 T47993 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 811 | 1S-2 | Similar to the above specimen, first temperature cycle, time at this temperature 45 min. |
| 7 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 955 | 1S-2 | Similar to the above specimen, first temperature cycle, time at this temperature 35 min. |
| 8 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 807 | 1S-2 | Similar to the above specimen, second temperature cycle, surface appeared to be unoxidized at start of this cycle, time at this temperature 3 hr 15 min. |
| 9 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 946 | 1S-2 | Similar to the above specimen, time at this temperature 3 hr 15 min. |
| 10 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 948 | 1S-2 | Similar to the above specimen, time at this temperature 3 hr 50 min. |
| 11 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 300 | 2S | Similar to the above specimen except oxidized for 1/2 hr at 600 C in wet hydrogen furnace, average weight gain 2.1 $\mu\text{g}/\text{cm}^2$, approximate film thickness 0.015 μm based on weight gain data and assumption of uniform film of Fe_2O_3 with average density of 5.2 g/cm^3 , gold color of interference film, test pressure 4×10^{-6} torr. |
| 12 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 310 | 2S | Similar to the above specimen, first temperature cycle for 2 hr. |
| 13 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 952 | 2S | Similar to the above specimen, at this temperature for 3 hr 20 min. |
| 14 T47998 | Rolling, R. E. and Fusai, A. I. | 1967 | 1.5-12 | 1061 | 2S | Similar to the above specimen, at this temperature for 6 hr. |

TABLE 3-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF AISI 304-STAINLESS STEEL (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 15 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 1087 | 25 | Similar to the above specimen. |
| 16 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 803 | 25 | Similar to the above specimen except second temperature cycle, at this temperature for 2 hr 10 min, color of oxide film changed from gold to silver-gray. |
| 17 T47996 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 940 | 25 | Similar to the above specimen, at this temperature for 35 min. |
| 18 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 300 | 35 | Similar to the above specimen except oxidation temperature at 800 C for 30 min, average weight gain $24.3 \mu\text{g}/\text{cm}^2$, approximate film thickness $0.170 \mu\text{m}$, purple color of oxide film, test pressure 2.5×10^{-4} torr. |
| 19 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 807 | 35 | Similar to the above specimen except at this temperature for 2 hr. |
| 20 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 953 | 35 | Similar to the above specimen except at this temperature for 3 hr 15 min. |
| 21 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 1090 | 35 | Similar to the above specimen except at this temperature for 5 hr 30 min, instability of the oxide film observed. |
| 22 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 0.31-18.9 | 300 | 45 | Similar to the above specimen except oxidation temperature at 1000 C for 30 min, average weight gain $135.7 \mu\text{g}/\text{cm}^2$, approximate film thickness $0.95 \mu\text{m}$, dull gray color of oxide film; test pressure 4.5×10^{-4} torr. |
| 23 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 818 | 45 | Similar to the above specimen except first temperature cycle, at this temperature for 1 hr 40 min. |
| 24 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 957 | 45 | Similar to the above specimen except at this temperature for 5 hr. |
| 25 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 811 | 45 | Similar to the above specimen except second temperature cycle, at this temperature for 40 min. |
| 26 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 949 | 45 | Similar to the above specimen. |
| 27 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 0.31-19 | 500 | 55 | Similar to the above specimen except oxidation temperature at 1000 C for 90 min, average weight gain $200 \mu\text{g}/\text{cm}^2$, approximate film thickness $1.40 \mu\text{m}$, dark brownish gray color of oxide film, test pressure 3.5×10^{-4} torr. |
| 28 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 809 | 55 | Similar to the above specimen except first temperature cycle, at this temperature for 3 hr 15 min. |
| 29 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 950 | 55 | Similar to the above specimen except at this temperature for 3 hr 30 min. |
| 30 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 814 | 55 | Similar to the above specimen except second temperature cycle, at this temperature for 30 min. |
| 31 T47998 | Rolling, R.E. and Funai, A.I. | 1967 | 1.5-12 | 952 | 55 | Similar to the above specimen except at this temperature for 45 min. |

TABLE 3-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|----------------|------------|-----------|------------|-----------|------------|-----------------|------------|----------------|------------|-----------|------------|-----------|------------|
| CURVE 1 | | | | | | | | | | | | | |
| T = 873. | | | | | | | | | | | | | |
| 2.0 | 0.370 | 0.40 | 0.435 | 0.3 | 0.925 | 13.0 | 0.705 | 5.00 | 0.157 | 10.0 | 0.110 | 1.5 | 0.290 |
| 3.0 | 0.340 | 0.45 | 0.410 | 0.4 | 0.936 | 13.5 | 0.701 | 6.00 | 0.150 | 12.0 | 0.095 | 2.0 | 0.253 |
| 4.0 | 0.320 | 0.49 | 0.362 | 0.5 | 0.936 | 14.0 | 0.719 | 6.50 | 0.139 | CURVE 8 | | | |
| 5.0 | 0.300 | 0.51 | 0.337 | 0.6 | 0.922 | 14.5 | 0.730 | 7.00 | 0.140 | T = 807. | | | |
| 6.0 | 0.280 | 0.54 | 0.337 | 0.7 | 0.898 | 15.0 | 0.732 | 7.50 | 0.137 | | | | |
| 7.0 | 0.260 | 0.59 | 0.329 | 0.7 | 0.898 | 15.5 | 0.732 | 8.00 | 0.131 | | | | |
| 8.0 | 0.260 | 0.70 | 0.317 | 0.8 | 0.860 | 16.0 | 0.743 | 8.50 | 0.121 | | | | |
| 9.0 | 0.250 | 0.81 | 0.311 | 0.9 | 0.860 | 16.5 | 0.756 | 9.00 | 0.118 | | | | |
| 10.0 | 0.240 | 0.90 | 0.303 | 1.0 | 0.844 | 17.0 | 0.801 | 10.00 | 0.108 | | | | |
| 11.0 | 0.230 | 1.00 | 0.293 | 1.1 | 0.836 | 17.5 | 0.776 | 12.00 | 0.102 | | | | |
| 12.0 | 0.220 | 1.19 | 0.276 | 1.2 | 0.830 | 18.0 | 0.737 | 14.00 | 0.095 | | | | |
| 13.0 | 0.210 | 1.40 | 0.256 | 1.3 | 0.825 | 18.5 | 0.725 | 14.50 | 0.094 | | | | |
| 14.0 | 0.200 | 1.60 | 0.232 | 1.4 | 0.825 | 19.0 | 0.782 | 15.00 | 0.089 | | | | |
| | | 1.79 | 0.224 | 1.5 | 0.825 | 19.5 | 0.815 | 15.50 | 0.088 | | | | |
| | | 1.99 | 0.207 | 1.6 | 0.826 | 20.0 | 0.830 | 16.00 | 0.095 | | | | |
| | | 2.19 | 0.202 | 1.7 | 0.827 | 20.5 | 0.810 | 17.00 | 0.093 | | | | |
| | | 2.40 | 0.200 | 1.8 | 0.825 | 21.0 | 0.766 | 18.00 | 0.090 | | | | |
| CURVE 2 | | | | | | | | | | | | | |
| T = 1273. | | | | | | | | | | | | | |
| 2.0 | 0.770 | 1.9 | 0.823 | 2.0 | 0.817 | CURVE 5 | | | | | | | |
| 3.0 | 0.760 | 2.70 | 0.816 | 2.5 | 0.786 | T = 300. | | | | | | | |
| 4.0 | 0.690 | 3.70 | 0.810 | 3.0 | 0.779 | 0.25 | 0.503 | 1.5 | 0.271 | | | | |
| 5.0 | 0.650 | 5.08 | 0.772 | 3.5 | 0.772 | 0.38 | 0.420 | 2.0 | 0.240 | | | | |
| 6.0 | 0.720 | 6.11 | 0.764 | 4.0 | 0.764 | 0.50 | 0.354 | 3.0 | 0.206 | | | | |
| 7.0 | 0.770 | 7.54 | 0.741 | 4.5 | 0.741 | 0.62 | 0.275 | 4.0 | 0.177 | | | | |
| 8.0 | 0.700 | 8.48 | 0.735 | 5.0 | 0.741 | 0.74 | 0.255 | 6.0 | 0.146 | | | | |
| 9.0 | 0.705 | 9.50 | 0.735 | 5.5 | 0.735 | 0.79 | 0.251 | 6.0 | 0.121 | | | | |
| 10.0 | 0.750 | 10.22 | 0.731 | 6.0 | 0.732 | 0.87 | 0.272 | 8.0 | 0.104 | | | | |
| 11.0 | 0.650 | 10.99 | 0.730 | 6.5 | 0.730 | 0.96 | 0.305 | 10.0 | 0.084 | | | | |
| 12.0 | 0.560 | 11.73 | 0.730 | 7.0 | 0.731 | 1.00 | 0.290 | 12.0 | 0.084 | | | | |
| 13.0 | 0.450 | 12.31 | 0.730 | 7.5 | 0.730 | 1.25 | 0.244 | CURVE 7 | | | | | |
| 14.0 | 0.400 | 12.90 | 0.730 | 8.0 | 0.730 | 1.37 | 0.235 | T = 955. | | | | | |
| | | 13.54 | 0.730 | 8.5 | 0.730 | 1.50 | 0.235 | 1.5 | 0.290 | | | | |
| | | 13.98 | 0.730 | 9.0 | 0.730 | 1.75 | 0.235 | 2.0 | 0.251 | | | | |
| | | 16.23 | 0.730 | 9.5 | 0.730 | 2.00 | 0.237 | 3.0 | 0.215 | | | | |
| | | 18.26 | 0.730 | 10.0 | 0.730 | 2.50 | 0.228 | 4.0 | 0.183 | | | | |
| | | 21.76 | 0.730 | 10.5 | 0.730 | 3.00 | 0.212 | 6.0 | 0.155 | | | | |
| | | 24.34 | 0.730 | 11.0 | 0.730 | 3.50 | 0.189 | 8.0 | 0.130 | | | | |
| | | 26.92 | 0.730 | 11.5 | 0.730 | 4.00 | 0.174 | 10.0 | 0.116 | | | | |
| | | | 0.095 | 12.0 | 0.735 | 4.50 | 0.163 | 12.0 | 0.097 | | | | |
| | | | 0.095 | 12.5 | 0.718 | CURVE 10 | | | | | | | |
| | | | 0.095 | | | T = 948. | | | | | | | |
| | | | 0.095 | | | 1.5 | 0.431 | | | | | | |
| | | | 0.095 | | | 2.0 | 0.334 | | | | | | |
| | | | 0.095 | | | 3.0 | 0.257 | | | | | | |
| | | | 0.095 | | | 4.0 | 0.209 | | | | | | |
| | | | 0.095 | | | 6.0 | 0.161 | | | | | | |
| | | | 0.095 | | | 8.0 | 0.134 | | | | | | |
| | | | 0.095 | | | 10.0 | 0.116 | | | | | | |
| | | | 0.095 | | | 12.0 | 0.097 | | | | | | |

TABLE 3-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|----------------------|------------|-----------------------|------------|----------------------|------------|-----------|------------|----------------------|-----------------------|-----------|------------|-----------|------------|
| CURVE 11 T = 300. | | | | | | | | | | | | | |
| 0.31 | 0.816 | 1.5 | 0.322 | 4.0 | 0.243 | 1.75 | 0.850 | 10.0 | 0.161 | 2.50 | 0.764 | 10.0 | 0.161 |
| 0.40 | 0.728 | 2.0 | 0.269 | 6.0 | 0.190 | 2.00 | 0.802 | 12.0 | 0.132 | 3.00 | 0.731 | 12.0 | 0.132 |
| 0.50 | 0.471 | 3.0 | 0.221 | 8.0 | 0.157 | 2.50 | 0.723 | CURVE 20 T = 953. | | | | | |
| 0.56 | 0.329 | 4.0 | 0.187 | 10.0 | 0.132 | 3.00 | 0.604 | 1.5 | 0.990 | 4.00 | 0.668 | 1.5 | 0.990 |
| 0.62 | 0.311 | 6.0 | 0.153 | 12.0 | 0.114 | 3.50 | 0.506 | 2.0 | 0.923 | 4.00 | 0.641 | 2.0 | 0.923 |
| 0.75 | 0.314 | 8.0 | 0.129 | CURVE 16 T = 803. | | | | 4.00 | 0.444 | 3.0 | 0.715 | 4.00 | 0.715 |
| 0.87 | 0.342 | 10.0 | 0.110 | 1.5 | 0.553 | 4.50 | 0.378 | 4.00 | 0.494 | 5.00 | 0.612 | 4.00 | 0.494 |
| 0.95 | 0.351 | 12.0 | 0.088 | 2.0 | 0.442 | 5.00 | 0.329 | 5.50 | 0.262 | 6.00 | 0.605 | 5.50 | 0.262 |
| 1.00 | 0.349 | CURVE 13 T = 952. | | | | 6.50 | 0.239 | 6.00 | 0.311 | 6.00 | 0.627 | 6.00 | 0.311 |
| 1.12 | 0.336 | 1.5 | 0.381 | 7.00 | 0.215 | 7.00 | 0.215 | 6.00 | 0.232 | 7.50 | 0.677 | 6.00 | 0.232 |
| 1.25 | 0.321 | 2.0 | 0.303 | 8.00 | 0.195 | 7.50 | 0.199 | 8.00 | 0.186 | 8.00 | 0.727 | 8.00 | 0.186 |
| 1.50 | 0.284 | 3.0 | 0.243 | 8.00 | 0.163 | 8.00 | 0.171 | 10.0 | 0.154 | 8.25 | 0.741 | 10.0 | 0.154 |
| 1.75 | 0.255 | 4.0 | 0.204 | 10.0 | 0.130 | 8.50 | 0.161 | 12.0 | CURVE 21 T = 1090. | | | | |
| 2.00 | 0.279 | 6.0 | 0.167 | 12.0 | 0.107 | 9.00 | 0.152 | 1.5 | 1.000 | 8.75 | 0.732 | 1.5 | 1.000 |
| 2.25 | 0.282 | 8.0 | 0.141 | CURVE 17 T = 940. | | | | 9.50 | 0.147 | 9.00 | 0.724 | 9.50 | 0.147 |
| 2.50 | 0.275 | 10.0 | 0.119 | 10.50 | 0.140 | 10.00 | 0.147 | 10.50 | 0.140 | 10.50 | 0.716 | 10.50 | 0.140 |
| 3.00 | 0.243 | 12.0 | 0.101 | 11.00 | 0.138 | 11.00 | 0.138 | 11.00 | 0.138 | 11.00 | 0.714 | 11.00 | 0.138 |
| 3.50 | 0.217 | CURVE 14 T = 1081. | | | | 12.00 | 0.134 | 12.00 | 0.134 | 1.5 | 0.714 | 10.50 | 1.000 |
| 4.00 | 0.196 | 1.5 | 0.640 | 13.00 | 0.134 | 13.00 | 0.134 | 13.00 | 0.134 | 2.0 | 0.757 | 2.0 | 0.956 |
| 4.50 | 0.184 | 2.0 | 0.487 | 14.00 | 0.138 | 14.00 | 0.138 | 14.00 | 0.138 | 3.0 | 0.749 | 3.0 | 0.714 |
| 5.00 | 0.179 | 3.0 | 0.359 | 14.50 | 0.146 | 14.50 | 0.146 | 14.50 | 0.146 | 4.0 | 0.757 | 4.0 | 0.488 |
| 6.00 | 0.176 | 4.0 | 0.277 | 15.00 | 0.157 | 15.00 | 0.157 | 15.00 | 0.157 | 6.0 | 0.741 | 6.0 | 0.317 |
| 7.00 | 0.167 | 6.0 | 0.206 | 16.00 | 0.151 | 16.00 | 0.151 | 16.00 | 0.151 | 8.0 | 0.701 | 8.0 | 0.245 |
| 7.50 | 0.163 | 8.0 | 0.174 | 17.00 | 0.151 | 17.00 | 0.151 | 17.00 | 0.151 | 10.0 | 0.646 | 10.0 | 0.198 |
| 8.00 | 0.151 | 10.0 | 0.140 | 18.00 | 0.164 | 18.00 | 0.164 | 18.00 | 0.164 | 12.0 | 0.573 | 12.0 | 0.168 |
| 8.50 | 0.139 | 12.0 | 0.117 | 18.96 | 0.179 | 18.96 | 0.179 | 18.96 | 0.179 | 14.00 | 0.447 | 14.00 | 0.168 |
| 9.00 | 0.129 | CURVE 18 T = 300. | | | | 19.00 | 0.151 | 19.00 | 0.151 | 0.31 | 0.295 | 14.50 | 0.447 |
| 9.50 | 0.125 | 0.31 | 0.832 | 19.96 | 0.142 | 19.96 | 0.142 | 19.96 | 0.142 | 0.50 | 0.295 | 15.00 | 0.358 |
| 10.00 | 0.115 | 0.36 | 0.845 | 20.00 | 0.121 | 20.00 | 0.121 | 20.00 | 0.121 | 0.75 | 0.295 | 15.50 | 0.358 |
| 12.00 | 0.109 | 0.50 | 0.866 | CURVE 19 T = 807. | | | | 0.31 | 0.830 | 1.00 | 0.483 | 16.00 | 0.268 |
| 14.00 | 0.109 | 0.75 | 0.887 | 1.5 | 0.960 | 1.5 | 0.960 | 1.5 | 0.833 | 1.25 | 0.376 | 16.50 | 0.268 |
| 16.00 | 0.109 | 1.00 | 0.897 | 2.0 | 0.900 | 2.0 | 0.900 | 2.0 | 0.821 | 1.50 | 0.456 | 17.00 | 0.376 |
| 16.50 | 0.114 | 1.25 | 0.896 | 3.0 | 0.882 | 3.0 | 0.882 | 3.0 | 0.798 | 1.75 | 0.376 | 17.50 | 0.483 |
| 17.00 | 0.118 | 1.5 | 0.600 | 1.5 | 0.845 | 1.5 | 0.845 | 1.5 | 0.781 | 18.00 | 0.376 | 18.00 | 0.456 |
| 17.50 | 0.115 | 2.0 | 0.413 | 2.0 | 0.866 | 2.0 | 0.866 | 2.0 | 0.772 | 18.25 | 0.356 | 18.25 | 0.456 |
| 18.00 | 0.112 | 3.0 | 0.302 | 3.0 | 0.887 | 3.0 | 0.887 | 3.0 | 0.768 | 18.50 | 0.356 | 18.50 | 0.456 |
| 18.96 | 0.108 | 1.5 | 0.600 | 4.0 | 0.897 | 4.0 | 0.897 | 4.0 | 0.771 | 18.75 | 0.346 | 18.75 | 0.456 |
| | | 2.0 | 0.413 | 6.0 | 0.896 | 6.0 | 0.896 | 6.0 | 0.780 | 18.94 | 0.342 | 18.94 | 0.456 |
| | | 3.0 | 0.302 | 8.0 | 0.882 | 8.0 | 0.882 | 8.0 | 0.781 | 19.00 | 0.343 | 19.00 | 0.456 |

TABLE 3-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-------------------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|
| CURVE 23 | | | | | | | |
| T = 818. | | | | | | | |
| 1.5 | 0.979 | 4.0 | 0.707 | 13.50 | 0.816 | 1.5 | 1.000 |
| 2.0 | 0.930 | 6.0 | 0.648 | 13.75 | 0.730 | 2.0 | 1.000 |
| 3.0 | 0.809 | 8.0 | 0.637 | 14.00 | 0.580 | 3.0 | 0.960 |
| 4.0 | 0.665 | 10.0 | 0.635 | 14.25 | 0.447 | 4.0 | 0.961 |
| 6.0 | 0.620 | 12.0 | 0.573 | 14.50 | 0.387 | 6.0 | 0.910 |
| 8.0 | 0.615 | CURVE 27 | | | | | |
| 10.0 | 0.591 | T = 300. | | | | | |
| 12.0 | 0.536 | 0.31 | 0.901 | 15.00 | 0.333 | 8.0 | 0.845 |
| CURVE 24 | | | | | | | |
| T = 957. | | | | | | | |
| 1.5 | 0.955 | 0.50 | 0.875 | 15.75 | 0.347 | 10.0 | 0.874 |
| 2.0 | 0.921 | 0.75 | 0.849 | 16.00 | 0.352 | 12.0 | 0.823 |
| 3.0 | 0.805 | 1.00 | 0.831 | 16.25 | 0.357 | CURVE 29 | |
| 4.0 | 0.669 | 1.25 | 0.819 | 16.50 | 0.374 | T = 950. | |
| 6.0 | 0.625 | 1.50 | 0.821 | 16.75 | 0.426 | 1.5 | 1.000 |
| 8.0 | 0.624 | 1.75 | 0.856 | 17.00 | 0.511 | 2.0 | 0.992 |
| 10.0 | 0.609 | 2.00 | 0.886 | 17.30 | 0.638 | 3.0 | 0.947 |
| 12.0 | 0.553 | 2.50 | 0.908 | 17.42 | 0.638 | 4.0 | 0.955 |
| CURVE 25 | | | | | | | |
| T = 811. | | | | | | | |
| 1.5 | 1.000 | 3.00 | 0.912 | 17.50 | 0.629 | 6.0 | 0.901 |
| 2.0 | 1.000 | 3.50 | 0.918 | 17.59 | 0.362 | 8.0 | 0.830 |
| 3.0 | 0.872 | 4.00 | 0.899 | 17.79 | 0.350 | 10.0 | 0.853 |
| 4.0 | 0.717 | 4.50 | 0.877 | 18.00 | 0.376 | 12.0 | 0.810 |
| 6.0 | 0.642 | 5.00 | 0.848 | 18.25 | 0.406 | CURVE 30 | |
| 8.0 | 0.633 | 5.50 | 0.813 | 18.50 | 0.421 | T = 814. | |
| 10.0 | 0.606 | 6.00 | 0.768 | 18.75 | 0.428 | 1.5 | 1.000 |
| 12.0 | 0.561 | 6.50 | 0.722 | 19.00 | 0.424 | 2.0 | 0.992 |
| CURVE 26 | | | | | | | |
| T = 949. | | | | | | | |
| 1.5 | 1.000 | 7.00 | 0.698 | CURVE 28 | | | |
| 2.0 | 0.872 | 7.50 | 0.693 | T = 809. | | | |
| 3.0 | 0.717 | 8.00 | 0.701 | 1.5 | 1.000 | 3.0 | 0.955 |
| 4.0 | 0.642 | 8.50 | 0.727 | 2.0 | 0.986 | 4.0 | 0.955 |
| 6.0 | 0.633 | 9.00 | 0.764 | 3.0 | 0.943 | 6.0 | 0.900 |
| 8.0 | 0.606 | 9.50 | 0.796 | 4.0 | 0.944 | 8.0 | 0.835 |
| 10.0 | 0.561 | 10.00 | 0.822 | 6.0 | 0.897 | 10.0 | 0.864 |
| CURVE 27 (CONT.) | | | | | | | |
| T = 952. | | | | | | | |
| 1.5 | 1.000 | 10.50 | 0.844 | 1.5 | 1.000 | 12.0 | 0.810 |
| 2.0 | 0.955 | 11.00 | 0.859 | 2.0 | 0.986 | 1.5 | 1.000 |
| 3.0 | 0.955 | 11.50 | 0.871 | 3.0 | 0.943 | 2.0 | 0.992 |
| 4.0 | 0.955 | 12.00 | 0.874 | 4.0 | 0.944 | 3.0 | 0.947 |
| 6.0 | 0.900 | 12.50 | 0.868 | 6.0 | 0.897 | 4.0 | 0.955 |
| 8.0 | 0.835 | 13.00 | 0.864 | 8.0 | 0.831 | 6.0 | 0.900 |
| 10.0 | 0.864 | 13.25 | 0.856 | 10.0 | 0.859 | 8.0 | 0.835 |
| 12.0 | 0.810 | | | 12.0 | 0.802 | 10.0 | 0.864 |

b. Normal Spectral Emittance (Temperature Dependence)

There is no experimental data available for this property. The provisional values for the polished surface, tabulated in Table 3-4 and shown in Figure 3-3, for 3.8μ and 10.6μ , covering the temperature range from room temperature to the melting point, were calculated by using the Kirchhoff law, i. e., $\epsilon_{\lambda} = \alpha_{\lambda}$. Data for α_{λ} are available in Section 4.3.g. These are considered accurate to within $\pm 20\%$ over the entire temperature range.

TABLE 3-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ |
|------------------|------------|-------|------------|
| POLISHED | | | |
| $\lambda = 3.0$ | | | |
| 293. | 0.137 | 293. | 0.088 |
| 300. | 0.130 | 300. | 0.089 |
| 400. | 0.143 | 400. | 0.093 |
| 500. | 0.148 | 500. | 0.097 |
| 600. | 0.154 | 600. | 0.100 |
| 700. | 0.158 | 700. | 0.103 |
| 800. | 0.165 | 800. | 0.106 |
| 900. | 0.170 | 900. | 0.110 |
| 1000. | 0.176 | 1000. | 0.113 |
| 1100. | 0.180 | 1100. | 0.117 |
| 1200. | 0.186 | 1200. | 0.120 |
| 1300. | 0.192 | 1300. | 0.123 |
| 1400. | 0.196 | 1400. | 0.127 |
| 1500. | 0.202 | 1500. | 0.129 |
| 1600. | 0.207 | 1600. | 0.132 |
| 1700. | 0.212 | 1700. | 0.136 |
| 1727. | 0.213 | 1727. | 0.136 |
| POLISHED | | | |
| $\lambda = 10.6$ | | | |

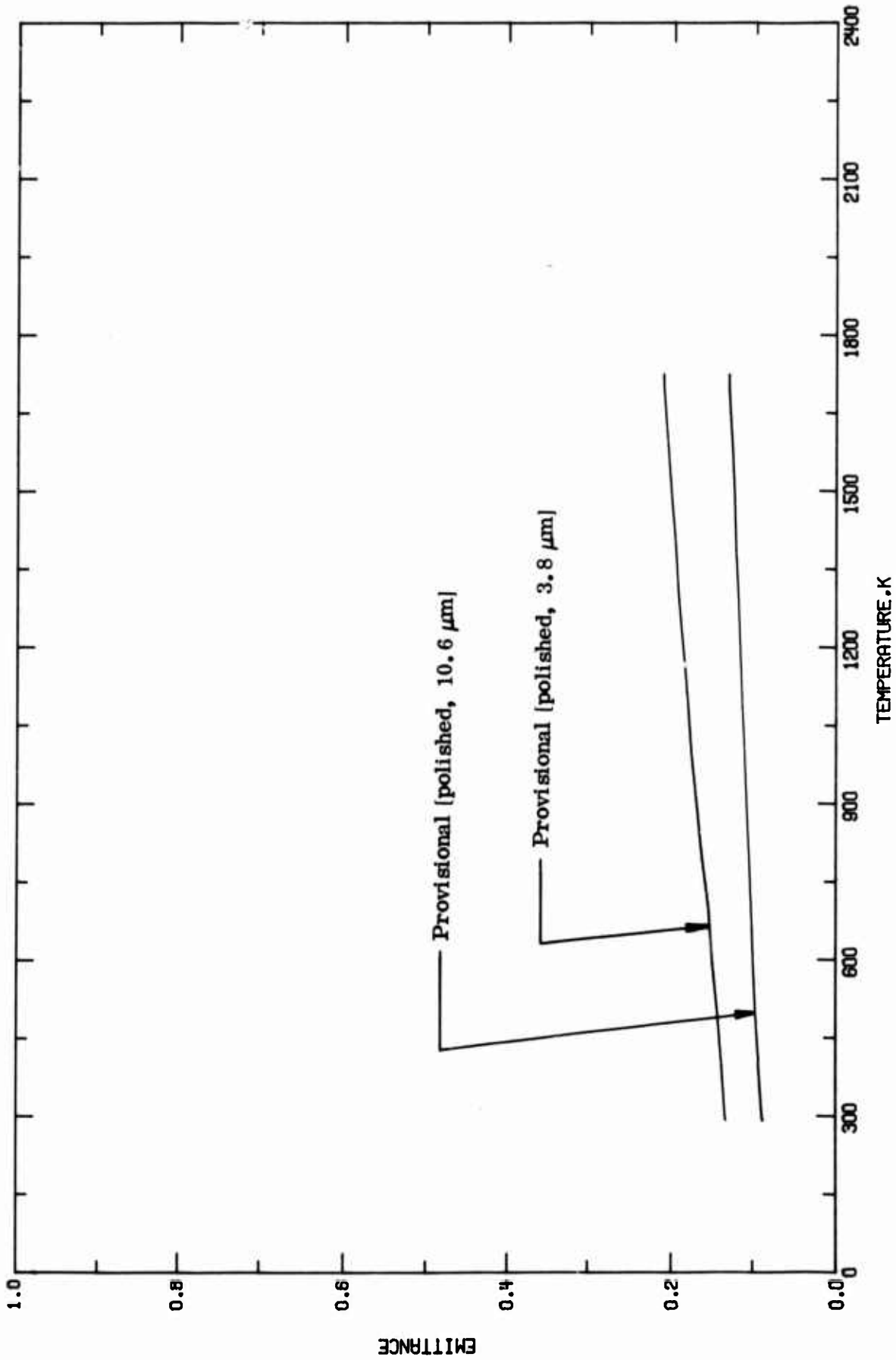


FIGURE 3-3. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

There are seven experimental data sets available for the wavelength dependence (0.97-295.9 μm) of the normal spectral reflectance of AISI 304 Stainless Steel from 77 K to room temperature. These are tabulated in Table 3-7 and shown in Figure 3-5.

The recommended values at 293 K, tabulated in Table 3-5 and shown in Figure 3-4, are for polished and unoxidized surfaces. These values, primarily from the investigations of Leigh [T33512] and Stockham [T45583], and the recommended values for the normal spectral emittance shown in Table 3-1 are considered accurate to within $\pm 15\%$ over the entire wavelength range.

The typical values at 1273 K, tabulated in Table 3-5 and shown in Figure 3-4, are for polished and oxidized surfaces. These values were calculated by using the Kirchhoff law, $\rho_{\lambda} = 1 - \alpha_{\lambda} = 1 - \epsilon_{\lambda}$, where the values for the normal spectral emittance are shown in Table 3-1. These values are considered accurate to about $\pm 30\%$ over the entire wavelength range.

TABLE 3-5. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | $T = 293$ | | λ | ρ |
|-----------|--------|-----------|-----------------|-----------|---------|
| | | POLISHED | T = 293 (CONT.) | | |
| 0.22 | 0.428 | 13.50 | 0.923 | 2.00 | 0.2328† |
| 0.25 | 0.468 | 14.00 | 0.924 | 2.50 | 0.2318 |
| 0.30 | 0.638 | | | 2.80 | 0.2368 |
| 0.32 | 0.628 | | | 3.00 | 0.2468 |
| 0.40 | 0.608 | | | 3.50 | 0.2718 |
| 0.50 | 0.698 | | | 3.80 | 0.2928 |
| 0.80 | 0.728 | | | 4.00 | 0.3108 |
| 1.00 | 0.748 | | | 4.50 | 0.3368 |
| 1.50 | 0.794 | | | 5.00 | 0.3508 |
| 1.88 | 0.828 | | | 5.50 | 0.3208 |
| 2.00 | 0.833 | | | 6.00 | 0.2638 |
| 2.20 | 0.836 | | | 6.50 | 0.2568 |
| 2.40 | 0.838 | | | 7.00 | 0.2408 |
| 2.50 | 0.828 | | | 7.50 | 0.2308 |
| 2.60 | 0.820 | | | 8.00 | 0.2248 |
| 2.80 | 0.824 | | | 8.50 | 0.2208 |
| 3.00 | 0.828 | | | 9.00 | 0.2198 |
| 3.50 | 0.834 | | | 9.50 | 0.2358 |
| 3.80 | 0.840 | | | 10.00 | 0.2548 |
| 4.00 | 0.846 | | | 10.60 | 0.3118 |
| 4.50 | 0.852 | | | 11.00 | 0.3528 |
| 5.00 | 0.860 | | | 11.50 | 0.4008 |
| 5.50 | 0.866 | | | 12.00 | 0.4468 |
| 6.00 | 0.872 | | | 12.50 | 0.4988 |
| 6.50 | 0.879 | | | 13.00 | 0.5448 |
| 7.00 | 0.884 | | | 13.50 | 0.5768 |
| 7.50 | 0.889 | | | 14.00 | 0.5988 |
| 8.00 | 0.893 | | | | |
| 8.50 | 0.898 | | | | |
| 9.00 | 0.902 | | | | |
| 9.50 | 0.904 | | | | |
| 10.00 | 0.908 | | | | |
| 10.50 | 0.911 | | | | |
| 10.60 | 0.912 | | | | |
| 11.00 | 0.914 | | | | |
| 11.50 | 0.917 | | | | |
| 12.00 | 0.919 | | | | |
| 12.50 | 0.920 | | | | |
| 13.00 | 0.921 | | | | |

† VALUE FOLLOWED BY A "8" IS TYPICAL.

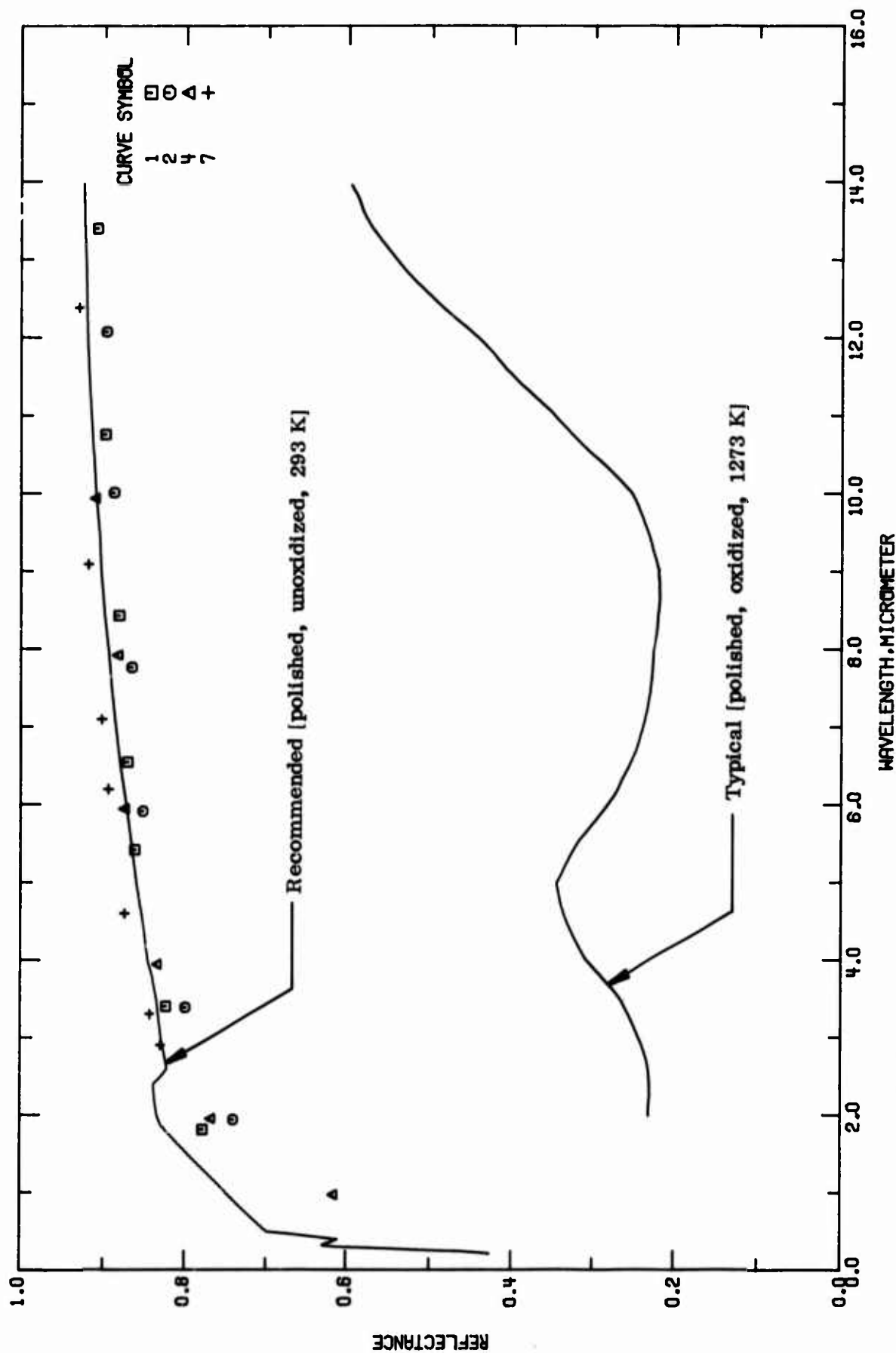


FIGURE 3-4. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

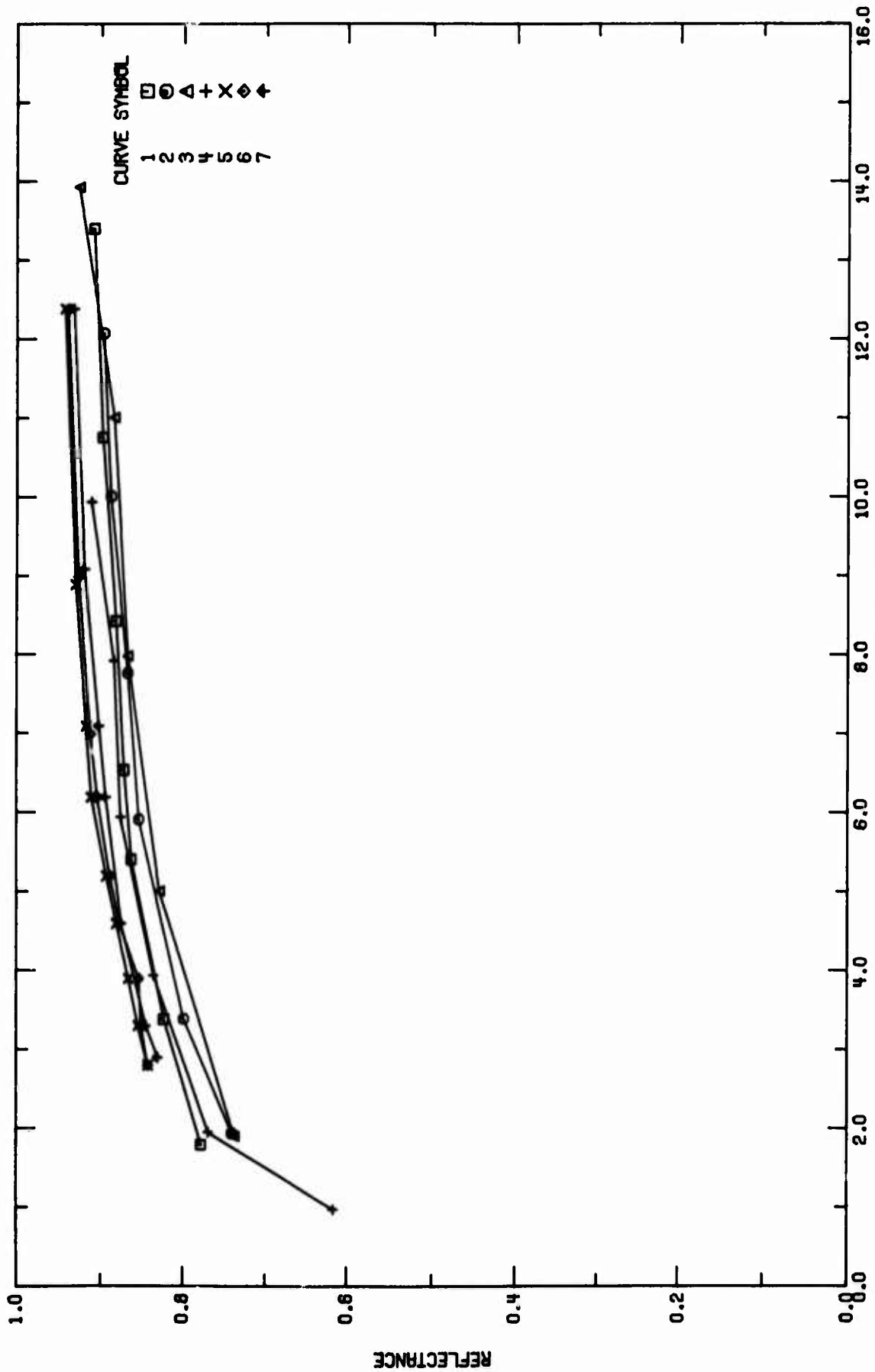


FIGURE 3-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

TABLE 3-6. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL. (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T33512 | Leigh, C.H. | 1962 | 1.81-26.01 | 298 | | Nominal composition: 18.00-20.00 Cr, 8.00-12.00 Ni, 2.00 max Mn, 1.00 max Si, 0.08 max C, Fe balance; polished; converted from $R(2\pi\theta^\circ)$; data extracted from smooth curve; $\theta=0^\circ$, $\omega^2=2g$. |
| 2 T33512 | Leigh, C.H. | 1962 | 1.94-26.01 | 298 | | Similar to the above specimen and conditions except damaged by particle impact. |
| 3 T33512 | Leigh, C.H. | 1962 | 1.90-25.99 | 77 | | Similar to the above specimen and conditions. |
| 4 T68866 | Stocckham, L.W. | 1972 | 0.97-9.95 | 300 | | Specimen cut from 1 1/2 in. bar stock, milled to thickness of 1/4 in. and polished using standard techniques; RMS roughness $0.03 \pm 0.005 \mu$. |
| 5 T45583 | Jones, M.C. and Palmer, D.C. | 1969 | 2.8-295.8 | 77 | | Sample ground in form of a flat disk 11/16 in. diameter and about 1/8 in. thick; relative measurement where energy reflected from a sample compared with that from a calibrated reference surface which is chosen to use films derived from very pure gold (999.999 pure) deposited from vapor on highly polished flat glass substrates under high vacuum or ultrahigh-vacuum conditions; commercial spectrophotometer having nominal wavelength range from 1-700 μm . |
| 6 T45583 | Jones, M.C. and Palmer, D.C. | 1969 | 2.8-295.8 | 105 | | Similar to the above specimen except measured at 105 K. |
| 7 T45583 | Jones, M.C. and Palmer, D.C. | 1969 | 2.8-295.8 | 297 | | Similar to the above specimen except measured at 297 K. |

TABLE 3-7. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ |
|----------------|--------|----------------|--------|----------------|--------|
| CURVE 1 | | | | | |
| T = 298. | | | | | |
| 1.81 | 0.777 | 22.01 | 0.889 | 2.8 | 0.841 |
| 3.48 | 0.822 | 23.98 | 0.895 | 3.3 | 0.849 |
| 5.42 | 0.862 | 25.99 | 0.899 | 3.9 | 0.852 |
| 6.55 | 0.871 | CURVE 4 | | | |
| 8.44 | 0.881 | T = 300. | | | |
| 10.77 | 0.897 | 0.97 | 0.615 | 5.2 | 0.888 |
| 13.42 | 0.907 | 1.95 | 0.768 | 6.2 | 0.903 |
| 15.90 | 0.908 | 3.94 | 0.834 | 7.0 | 0.911 |
| 18.98 | 0.919 | 5.95 | 0.875 | 9.0 | 0.925 |
| 21.65 | 0.923 | 7.93 | 0.883 | 12.4 | 0.937 |
| 26.01 | 0.924 | 9.95 | 0.910 | 14.1 | 0.942 |
| CURVE 2 | | | | | |
| T = 298. | | | | | |
| 1.94 | 0.739 | CURVE 5 | | | |
| 3.39 | 0.798 | T = 77. | | | |
| 5.92 | 0.852 | 2.8 | 0.841 | 28.4 | 0.959 |
| 7.77 | 0.866 | 3.3 | 0.853 | 33.1 | 0.961 |
| 10.02 | 0.887 | 3.9 | 0.865 | 56.1 | 0.966 |
| 12.09 | 0.896 | 4.6 | 0.880 | 65.3 | 0.964 |
| 14.02 | 0.898 | 5.2 | 0.892 | 78.5 | 0.964 |
| 16.65 | 0.902 | 6.2 | 0.910 | CURVE 6 | |
| 18.70 | 0.898 | 7.1 | 0.916 | T = 105. | |
| 20.67 | 0.890 | 8.9 | 0.928 | 2.9 | 0.829 |
| 22.32 | 0.895 | 12.4 | 0.946 | 3.3 | 0.843 |
| 24.41 | 0.899 | 14.1 | 0.954 | 4.6 | 0.874 |
| 26.01 | 0.899 | 21.7 | 0.949 | 6.2 | 0.893 |
| CURVE 3 | | | | | |
| T = 77. | | | | | |
| 1.90 | 0.736 | 25.4 | 0.951 | 7.1 | 0.901 |
| 5.01 | 0.827 | 28.4 | 0.949 | 9.1 | 0.918 |
| 7.99 | 0.866 | 33.1 | 0.963 | 12.4 | 0.930 |
| 11.02 | 0.883 | 39.2 | 0.962 | 14.3 | 0.934 |
| 13.95 | 0.924 | 49.4 | 0.967 | 21.8 | 0.942 |
| 15.81 | 0.903 | 56.1 | 0.966 | 25.5 | 0.949 |
| 18.02 | 0.888 | 65.3 | 0.963 | 29.0 | 0.949 |
| | | 79.5 | 0.969 | 33.1 | 0.952 |
| | | | | 39.2 | 0.955 |
| | | | | 49.3 | 0.958 |
| | | | | 56.1 | 0.962 |
| | | | | 65.3 | 0.959 |
| | | | | 78.5 | 0.965 |

d. Normal Spectral Reflectance (Temperature Dependence)

There is no experimental data available for this property. Two provisional values, tabulated in Table 3-8 and shown in Figure 3-6, were generated for 3.8 μ and 10.6 μ , respectively, covering the temperature range from room temperature to the melting point. The relation $\rho_\lambda + \alpha_\lambda = 1$ was employed for this case. Data for α_λ are available in Section 4.3.g. These values are considered accurate to about $\pm 20\%$ for the entire temperature range.

TABLE 3-8. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ | T | ρ |
|------------------|--------|-------|--------|
| POLISHED | | | |
| $\lambda = 3.0$ | | | |
| 293. | 0.863 | 293. | 0.912 |
| 300. | 0.862 | 300. | 0.911 |
| 400. | 0.857 | 400. | 0.907 |
| 500. | 0.852 | 500. | 0.903 |
| 600. | 0.846 | 600. | 0.900 |
| 700. | 0.842 | 700. | 0.897 |
| 800. | 0.835 | 800. | 0.894 |
| 900. | 0.83 | 900. | 0.890 |
| 1000. | 0.824 | 1000. | 0.887 |
| 1100. | 0.820 | 1100. | 0.883 |
| 1200. | 0.814 | 1200. | 0.880 |
| 1300. | 0.808 | 1300. | 0.877 |
| 1400. | 0.804 | 1400. | 0.873 |
| 1500. | 0.798 | 1500. | 0.871 |
| 1600. | 0.793 | 1600. | 0.868 |
| 1700. | 0.788 | 1700. | 0.864 |
| 1727. | 0.787 | 1727. | 0.864 |
| $\lambda = 10.6$ | | | |

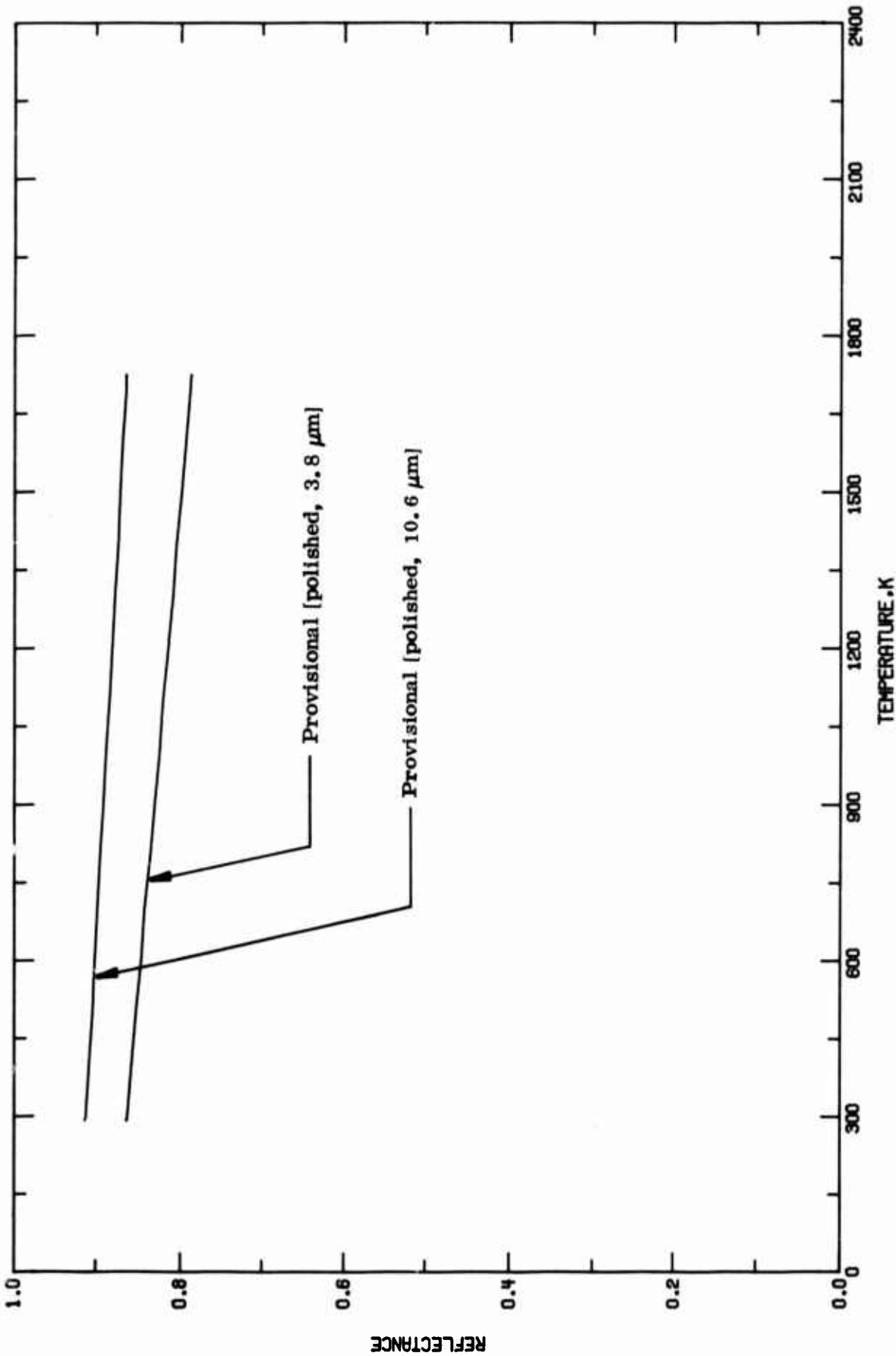


FIGURE 3-6. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE).

e. Angular Spectral Reflectance (Wavelength Dependence)

There are three sets of experimental data available for the wavelength dependence (0.1-0.2 μm) of the angular spectral reflectance of AISI 304 Stainless Steel at temperature 300 K. These are tabulated in Table 3-10 and shown in Figure 3-7.

No recommendations were made because of the lack of information in the wavelength range which we are interested in.

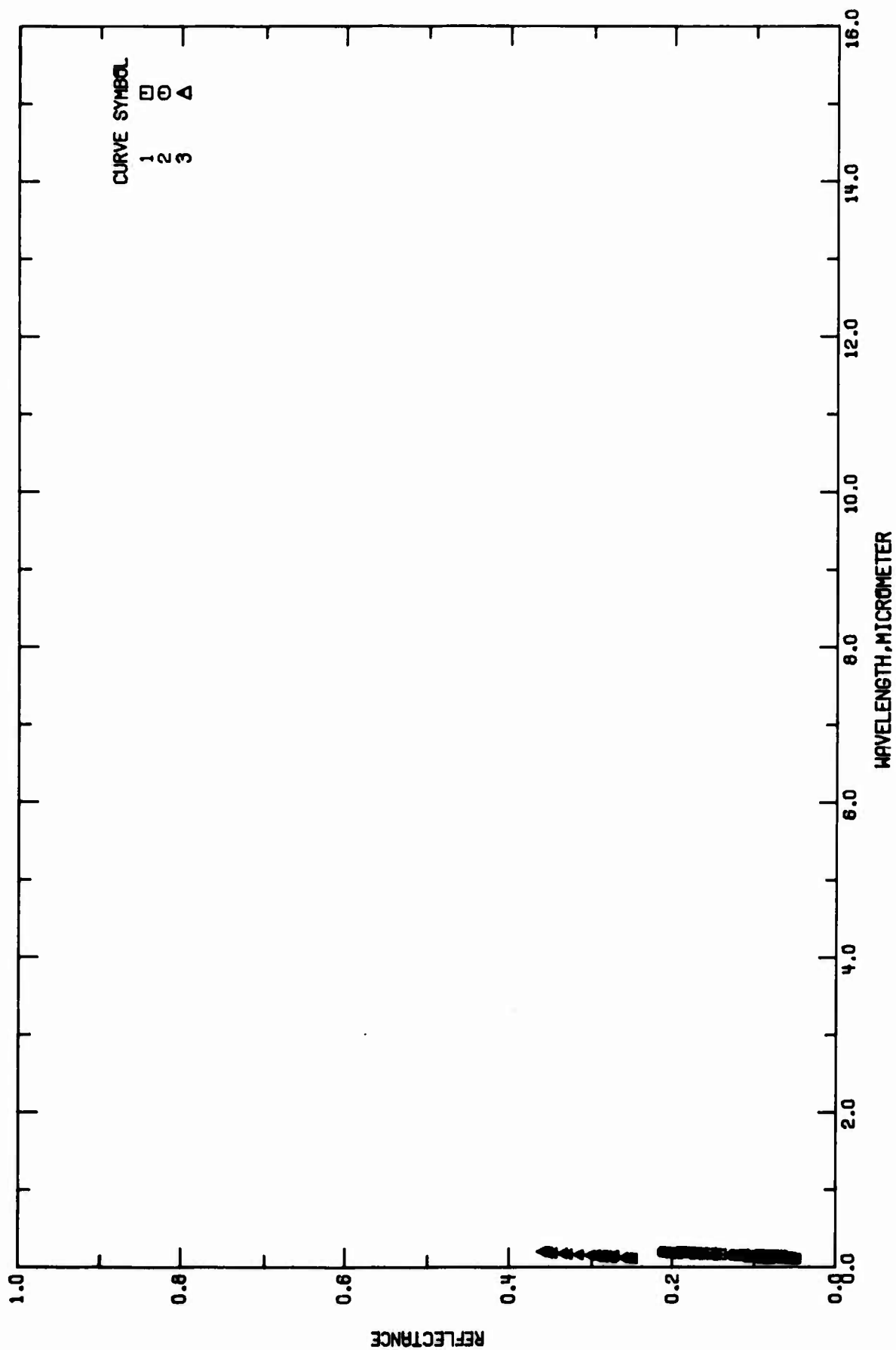


FIGURE 3-7. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

TABLE 3-9. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (Wavelength Dependence)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent). Specifications, and Remarks |
|-------------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T77362 | Marmo, F. F., Engelman, A., and Schultz, E. D. | 1967 | 0.1-0.2 | 300 | | The top and bottom parts of reflectometer contain a rotary push-pull vacuum cell with an indicating pointer and a fixed 360 degree protractor, angle of incidence of 20 degree; $\theta=30^\circ$. |
| 2 T77362 | Marmo, F. F., et al. | 1967 | 0.1-0.2 | 300 | | Similar to the above specimen except angle of incidence of 45 degree; $\theta=45^\circ$. |
| 3 T77362 | Marmo, F. F., et al. | 1967 | 0.1-0.2 | 300 | | Similar to the above specimen except angle of incidence of 70 degree; $\theta=70^\circ$. |

TABLE 3-10. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| CURVE 1 | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | |
|-----------|--------|-----------------|--------|-----------------|--------|
| λ | ρ | λ | ρ | λ | ρ |
| T = 300. | | | | | |
| 0.1115 | 0.050 | 0.1344 | 0.107 | 0.1544 | 0.302 |
| 0.1146 | 0.053 | 0.1357 | 0.109 | 0.1581 | 0.295 |
| 0.1161 | 0.056 | 0.1377 | 0.108 | 0.1608 | 0.316 |
| 0.1176 | 0.058 | 0.1395 | 0.103 | 0.1703 | 0.330 |
| 0.1189 | 0.060 | 0.1436 | 0.096 | 0.1753 | 0.336 |
| 0.1216 | 0.062 | 0.1464 | 0.095 | 0.1803 | 0.349 |
| 0.1254 | 0.066 | 0.1487 | 0.099 | 0.1853 | 0.354 |
| 0.1278 | 0.072 | 0.1517 | 0.108 | 0.1903 | 0.356 |
| 0.1344 | 0.076 | 0.1532 | 0.115 | 0.1903 | 0.358 |
| 0.1357 | 0.076 | 0.1544 | 0.121 | 0.1953 | 0.358 |
| 0.1377 | 0.076 | 0.1581 | 0.126 | 0.2003 | 0.361 |
| 0.1395 | 0.074 | 0.1608 | 0.146 | | |
| 0.1436 | 0.069 | 0.1703 | 0.164 | | |
| 0.1464 | 0.067 | 0.1753 | 0.175 | | |
| 0.1467 | 0.069 | 0.1803 | 0.190 | | |
| 0.1517 | 0.078 | 0.1853 | 0.197 | | |
| 0.1532 | 0.085 | 0.1903 | 0.205 | | |
| 0.1544 | 0.090 | 0.1953 | 0.208 | | |
| 0.1581 | 0.093 | 0.2003 | 0.212 | | |
| 0.1608 | 0.112 | | | | |
| 0.1703 | 0.140 | | | | |
| 0.1753 | 0.152 | | | | |
| 0.1803 | 0.163 | | | | |
| 0.1853 | 0.171 | | | | |
| 0.1903 | 0.178 | | | | |
| 0.1953 | 0.184 | | | | |
| 0.2003 | 0.188 | | | | |
| CURVE 2 | | | | | |
| T = 300. | | | | | |
| 0.1115 | 0.079 | 0.1115 | 0.250 | | |
| 0.1146 | 0.082 | 0.1146 | 0.251 | | |
| 0.1161 | 0.085 | 0.1161 | 0.255 | | |
| 0.1176 | 0.086 | 0.1176 | 0.258 | | |
| 0.1189 | 0.089 | 0.1189 | 0.262 | | |
| 0.1216 | 0.091 | 0.1216 | 0.276 | | |
| 0.1254 | 0.093 | 0.1254 | 0.279 | | |
| 0.1278 | 0.098 | 0.1278 | 0.286 | | |
| | | 0.1344 | 0.290 | | |
| | | 0.1357 | 0.294 | | |
| | | 0.1377 | 0.289 | | |
| | | 0.1395 | 0.262 | | |
| | | 0.1436 | 0.274 | | |
| | | 0.1464 | 0.274 | | |
| | | 0.1487 | 0.273 | | |
| | | 0.1517 | 0.286 | | |
| | | 0.1532 | 0.295 | | |

f. Normal Spectral Absorptance (Wavelength Dependence)

There are five sets of experimental data available for the wavelength dependence (2.8-20 μm) of the normal spectral absorptance of AISI 304 Stainless Steel near room temperature. These values are tabulated in Table 3-13 and shown in Figure 3-9.

The recommended values for polished surfaces at 293 K, tabulated in Table 3-11 and shown in Figure 3-8 are primarily based on the work by Harmon [A00003] and the recommended data for normal spectral emittance of wavelength dependence (see Section 4.3.a).

The accuracy for this recommended data is considered to within $\pm 15\%$ for the entire wavelength range.

The typical values at 1273 K, tabulated in Table 3-11 and shown in Figure 3-8, are for polished and oxidized surfaces. These values were calculated by using the Kirchhoff law, $\alpha_\lambda = \epsilon_\lambda$, where the values for the normal spectral emittance are shown in Table 3-1. These values are considered accurate to about $\pm 30\%$ over the entire wavelength range.

TABLE 3-11. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | POLISHED | | λ | α |
|-----------|----------|-----------|----------|-----------|---------------------|
| | | λ | α | | |
| T = 293 | | | | | |
| 0.22 | 0.572 | 13.50 | 0.077 | 2.00 | 0.7688 [†] |
| 0.25 | 0.532 | 14.00 | 0.076 | 2.50 | 0.7658 |
| 0.30 | 0.392 | | | 2.00 | 0.7628 |
| 0.32 | 0.372 | | | 3.00 | 0.7548 |
| 0.40 | 0.392 | | | 3.50 | 0.7298 |
| 0.50 | 0.302 | | | 3.00 | 0.7088 |
| 0.80 | 0.272 | | | 4.00 | 0.6908 |
| 1.00 | 0.252 | | | 4.50 | 0.6648 |
| 1.50 | 0.206 | | | 5.00 | 0.6508 |
| 1.80 | 0.172 | | | 5.50 | 0.6008 |
| 2.00 | 0.167 | | | 6.00 | 0.7178 |
| 2.20 | 0.164 | | | 6.50 | 0.7448 |
| 2.40 | 0.162 | | | 7.00 | 0.7608 |
| 2.50 | 0.172 | | | 7.50 | 0.7702 |
| 2.60 | 0.180 | | | 8.00 | 0.7768 |
| 2.80 | 0.176 | | | 8.50 | 0.7808 |
| 3.00 | 0.172 | | | 9.00 | 0.7818 |
| 3.50 | 0.166 | | | 9.50 | 0.7658 |
| 3.80 | 0.160 | | | 10.00 | 0.7468 |
| 4.00 | 0.156 | | | 10.60 | 0.6898 |
| 4.50 | 0.142 | | | 11.00 | 0.6488 |
| 5.00 | 0.140 | | | 11.50 | 0.6008 |
| 5.50 | 0.134 | | | 12.00 | 0.5548 |
| 6.00 | 0.128 | | | 12.50 | 0.5028 |
| 6.50 | 0.121 | | | 13.00 | 0.4568 |
| 7.00 | 0.116 | | | 13.50 | 0.4248 |
| 7.50 | 0.111 | | | 14.00 | 0.4028 |
| 8.00 | 0.107 | | | | |
| 8.50 | 0.102 | | | | |
| 9.00 | 0.098 | | | | |
| 9.50 | 0.096 | | | | |
| 10.00 | 0.092 | | | | |
| 10.50 | 0.089 | | | | |
| 10.60 | 0.080 | | | | |
| 11.00 | 0.086 | | | | |
| 11.50 | 0.083 | | | | |
| 12.00 | 0.081 | | | | |
| 12.50 | 0.080 | | | | |
| 13.00 | 0.079 | | | | |

[†] VALUE FOLLOWED BY A "8" IS TYPICAL.

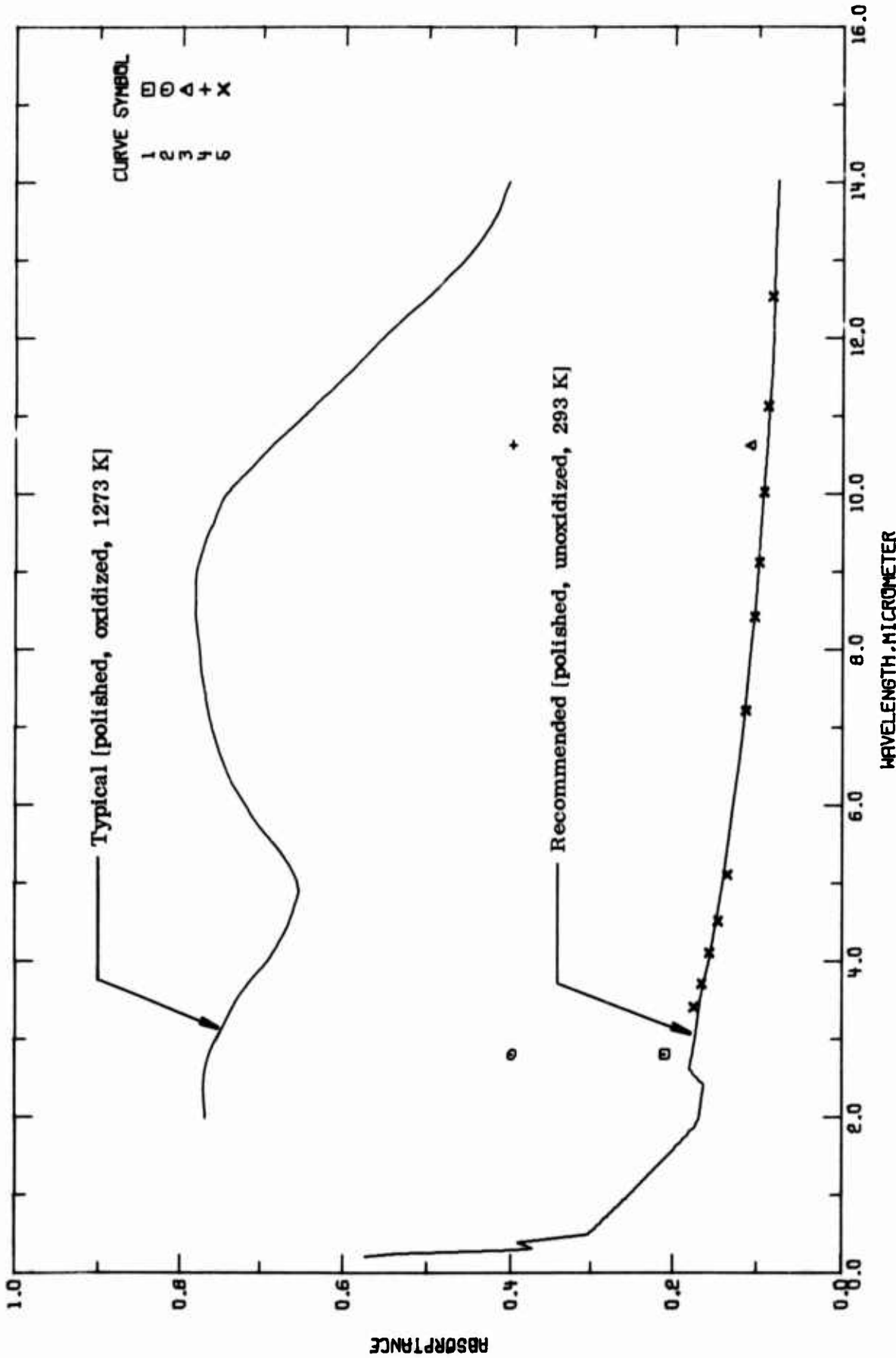


FIGURE 3-8. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

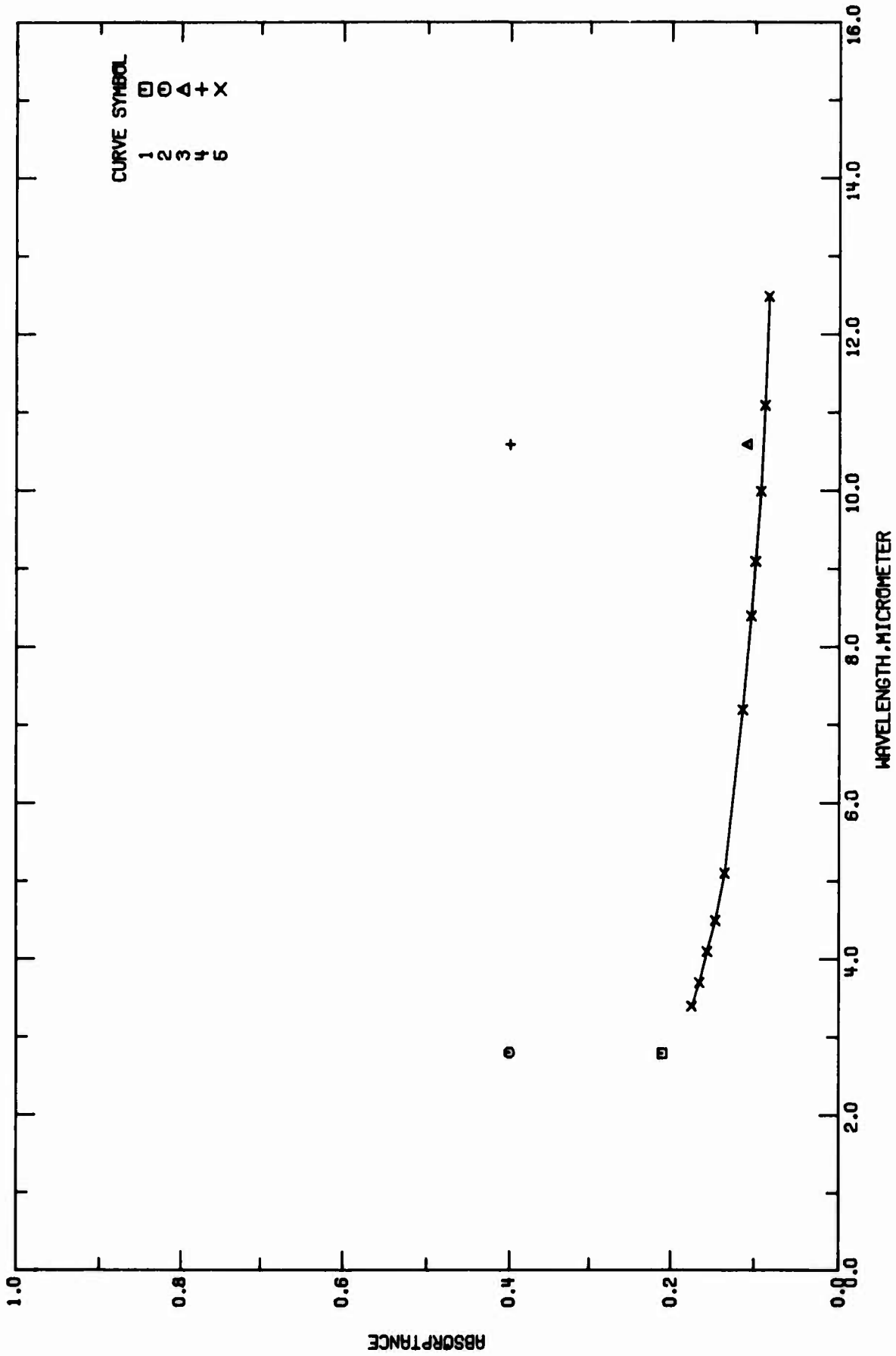


FIGURE 3-9. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE).

TABLE 3-12. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00016 | Neighbours, J.R., (Editor) | 1974 | 2.8 | 300 | | Polished surface condition. |
| 2 A00016 | Neighbours, J.R., (Editor) | 1974 | 2.8 | 300 | | As received surface condition. |
| 3 A00016 | Neighbours, J.R., (Editor) | 1974 | 10.6 | 300 | | Polished surface condition. |
| 4 A00016 | Neighbours, J.R., (Editor) | 1974 | 10.6 | 300 | | As received surface condition. |
| 5 A00003 | Hartman, N.F., (Editor) | 1974 | 3.42-20.00 | 293 | | High quality surface. |

TABLE 3-13. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|-----------|----------|
| CURVE 1 | |
| T = 300. | |
| 2.0 | 0.21 |
| CURVE 2 | |
| T = 300. | |
| 2.0 | 0.4 |
| CURVE 3 | |
| T = 300. | |
| 10.6 | 0.11 |
| CURVE 4 | |
| T = 300. | |
| 10.6 | 0.4 |
| CURVE 5 | |
| T = 293. | |
| 3.4 | 0.175 |
| 3.7 | 0.166 |
| 4.1 | 0.157 |
| 4.5 | 0.147 |
| 5.1 | 0.136 |
| 7.2 | 0.114 |
| 8.4 | 0.104 |
| 9.1 | 0.099 |
| 10.0 | 0.093 |
| 11.1 | 0.088 |
| 12.5 | 0.083 |
| 14.3 | 0.076 |
| 16.6 | 0.071 |
| 19.1 | 0.064 |
| 20.0 | 0.061 |

g. Normal Spectral Absorptance (Temperature Dependence)

There are eight sets of data available for the temperature dependence (293-1727 K) of the normal spectral absorptance of AISI 304 Stainless Steel covering the wavelength range from 2.8 μm to 10.6 μm . These values are tabulated in Table 3-16 and shown in Figure 3-11.

The provisional values for the polished surface for 3.8 μm and 10.6 μm are tabulated in Table 3-14 and shown in Figure 3-10 covering the temperature range from 293 to 1727 K.

The provisional values for 3.8 μm are primarily based on the work by Neighbours [A00016] who theoretically calculated the normal spectral absorptance from the equation $\alpha_\lambda = A_0 + A_2 T$ assuming that this AISI 304 Stainless Steel obeyed the Drude-Lorentz theory.

The provisional values at 10.6 μm were generated from the calculations of Neighbours [A00016] and Cunningham and Laughlin [E66194] who used the Hagen-Rubens relation, and the experimental values of Harmon [A00003]. The accuracy of both provisional curves is about $\pm 20\%$ over the entire temperature range.

TABLE 3-14. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α | T | α |
|-----------------|----------|------------------|----------|
| POLISHED | | | |
| $\lambda = 3.0$ | | $\lambda = 10.6$ | |
| 293. | 0.137 | 293. | 0.088 |
| 300. | 0.138 | 300. | 0.089 |
| 400. | 0.143 | 400. | 0.093 |
| 500. | 0.148 | 500. | 0.097 |
| 600. | 0.154 | 600. | 0.100 |
| 700. | 0.158 | 700. | 0.103 |
| 800. | 0.165 | 800. | 0.106 |
| 900. | 0.170 | 900. | 0.110 |
| 1000. | 0.176 | 1000. | 0.113 |
| 1100. | 0.180 | 1100. | 0.117 |
| 1200. | 0.186 | 1200. | 0.120 |
| 1300. | 0.192 | 1300. | 0.123 |
| 1400. | 0.196 | 1400. | 0.127 |
| 1500. | 0.202 | 1500. | 0.129 |
| 1600. | 0.207 | 1600. | 0.132 |
| 1700. | 0.212 | 1700. | 0.136 |
| 1727. | 0.213 | 1727. | 0.136 |

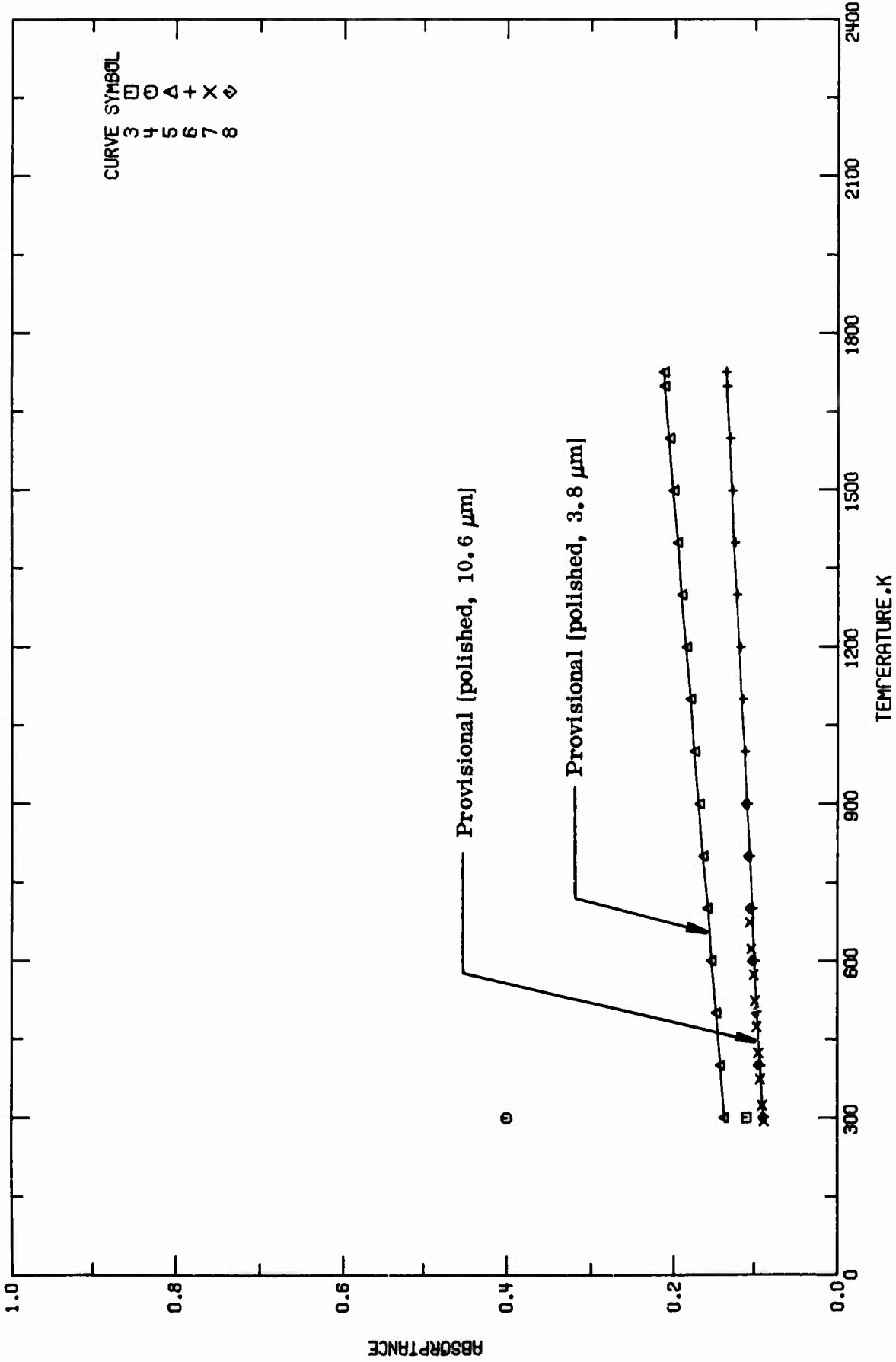


FIGURE 3-10. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE).

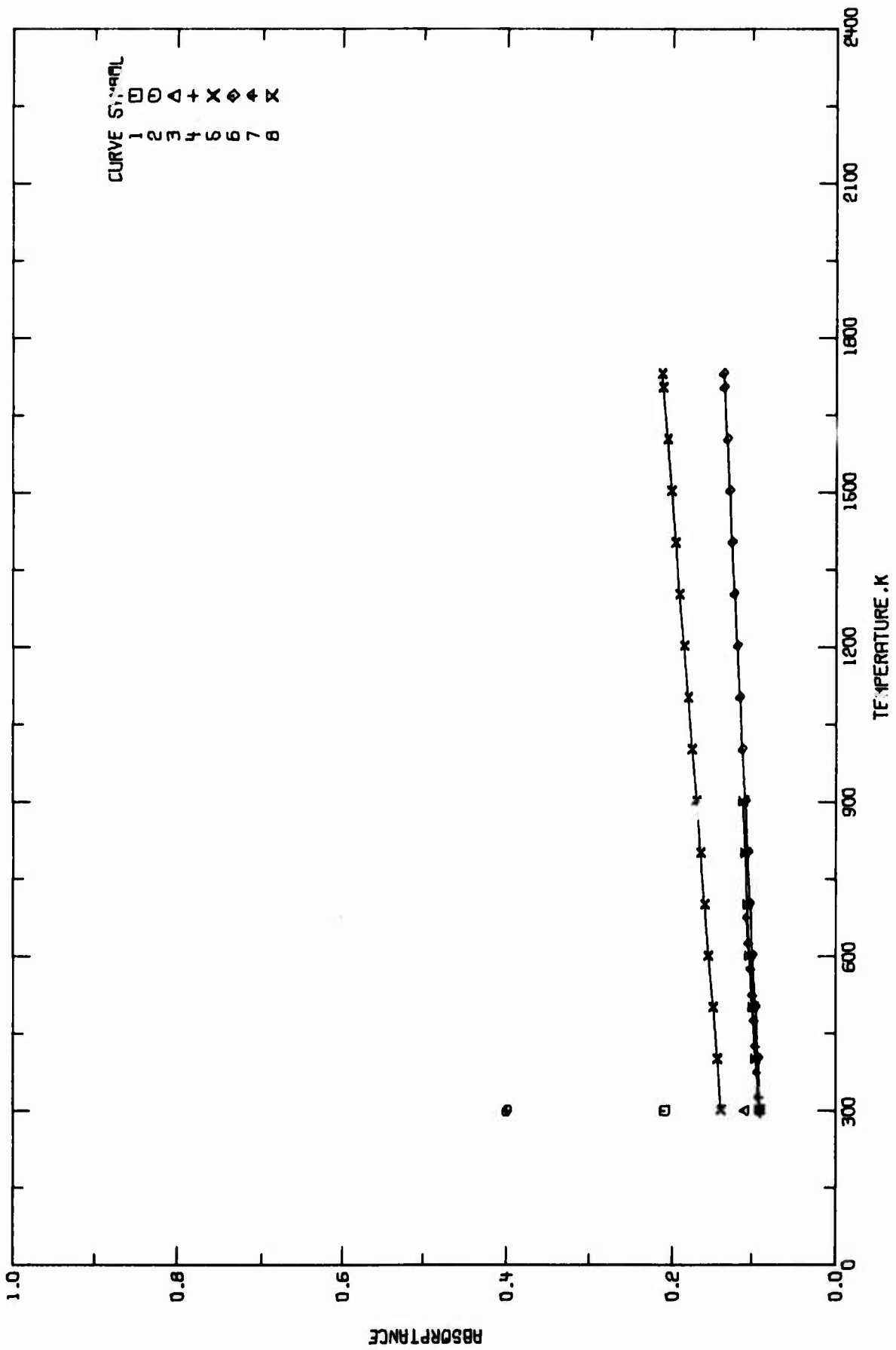


FIGURE 3-11. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE).

TABLE 3-15. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (Temperature Dependence)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|-------------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00016 | Neighbours, J.R., (Editor) | 1974 | 2.8 | 300 | | Polished surface condition. |
| 2 A00016 | Neighbours, J.R., (Editor) | 1974 | 2.8 | 300 | | As received surface condition. |
| 3 A00016 | Neighbours, J.R., (Editor) | 1974 | 10.6 | 300 | | Polished surface condition. |
| 4 A00016 | Neighbours, J.R., (Editor) | 1974 | 10.6 | 300 | | As received surface condition. |
| 5 A00016 | Neighbours, J.R., (Editor) | 1974 | 3.8 | 300-1727 | | Theoretical calculation of absorptance from 300 K to the melting point (1727 K) from the equation $A = A_0 + A_1 T$, based on the assumption that the alloys obey the Drude-Lorentz theory, where $A_0 = 0.122$ and $A_1 = 5.27 \times 10^{-5} \text{ K}^{-1}$ The above specimen except $A_0 = 7.91 \times 10^{-2}$ and $A_1 = 3.2? \times 10^{-5} \text{ K}^{-1}$. |
| 6 A00016 | Neighbours, J.R., (Editor) | 1974 | 10.6 | 300-1727 | | Averaged values of two runs. |
| 7 A00003 | Harmon, N.F., (Editor) | 1974 | 10.6 | 293-773 | | Calculated value of absorptance, which is obtained by evaluating the Hagen-Rubens relation. |
| 8 E66194 | Cunningham, S.S. and Laughlin, W.T. | 1974 | 10.6 | 300-900 | | |

TABLE 3-16. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF AISI 304 STAINLESS STEEL (TEMPERATURE DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| T | α | T | α | T | α |
|-----------------------------|----------|-----------------------------|----------|------|----------|
| CURVE 1 $\lambda = 2.8$ | | | | | |
| 300. | 0.21 | CURVE 6 $\lambda = 10.6$ | | | |
| | | 300. | 0.089 | 900. | 0.111 |
| | | 400. | 0.092 | | |
| CURVE 2 $\lambda = 2.8$ | | | | | |
| 500. | | 500. | 0.095 | | |
| 600. | | 600. | 0.099 | | |
| 700. | | 700. | 0.102 | | |
| 800. | 0.4 | 800. | 0.105 | | |
| 900. | | 900. | 0.108 | | |
| CURVE 3 $\lambda = 10.6$ | | | | | |
| 1000. | | 1000. | 0.112 | | |
| 1100. | | 1100. | 0.115 | | |
| 1200. | | 1200. | 0.118 | | |
| 1300. | 0.11 | 1300. | 0.122 | | |
| 1400. | | 1400. | 0.125 | | |
| CURVE 4 $\lambda = 10.6$ | | | | | |
| 1500. | | 1500. | 0.128 | | |
| 1600. | | 1600. | 0.131 | | |
| 1700. | | 1700. | 0.135 | | |
| 300. | 0.4 | 1727. | 0.136 | | |
| CURVE 5 $\lambda = 3.8$ | | | | | |
| 300. | 0.138 | CURVE 7 $\lambda = 10.6$ | | | |
| 400. | 0.143 | 293. | 0.088 | | |
| 500. | 0.148 | 323. | 0.090 | | |
| 600. | 0.154 | 373. | 0.093 | | |
| 700. | 0.159 | 423. | 0.095 | | |
| 800. | 0.164 | 473. | 0.097 | | |
| 900. | 0.169 | 523. | 0.099 | | |
| 1000. | 0.175 | 573. | 0.101 | | |
| 1100. | 0.180 | 623. | 0.104 | | |
| 1200. | 0.185 | 673. | 0.106 | | |
| 1300. | 0.191 | CURVE 8 $\lambda = 10.6$ | | | |
| 1400. | 0.196 | 300. | 0.069 | | |
| 1500. | 0.201 | 400. | 0.095 | | |
| 1600. | 0.206 | 500. | 0.099 | | |
| 1700. | 0.212 | 600. | 0.103 | | |
| 1727. | 0.213 | 700. | 0.106 | | |
| | | 800. | 0.108 | | |

h. Transmittance

Although it is true that metals and alloys in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms.

As an aircraft/spacecraft structural material, this alloy is not used in the form of extremely thin films and therefore is opaque; that is, its transmittance is zero.

4.4. Titanium Alloy Ti-6Al-4V

Titanium alloy Ti-6Al-4V was first introduced in 1954 [A00008]. Its nominal composition is 6% Al, 4% V, and balance Ti. The melting range of this alloy is 1803 to 1908 K. Its density is 4.424 g cm^{-3} , which is 56% of that of steel. It can be heat-treated to ultimate strength in excess of 170,000 psi and has excellent fatigue properties and crack propagation characteristics.

This alloy has an alpha lean beta composition. Addition of the six percent aluminum stabilizes the alpha phase resulting in an increase in $\alpha + \beta \rightarrow \beta$ transformation temperature from 1156 to 1266 K. It also increases the elevated temperature strength level. Addition of four percent vanadium increases the strength level by two mechanisms: firstly by substitutional solid solution hardening and secondly, by stabilizing the beta or high temperature phase, thereby making β to α hardening reaction possible through heat treatment. The addition of Vanadium improves hot workability by causing more of the ductile β -phase to be present at hot working temperatures.

Descaling of the alloy can be accomplished mechanically by methods such as grinding and grit blasting; and chemically by acid pickling or by immersion in molten caustic or hydride bath.

Pickling of the alloy is generally done either for dimensional reasons or for removing surface (oxygen) contamination. This is done in bath containing HNO_3 and HF with ratios of 10:1. HNO_3 acts as an inhibitor to prevent the titanium from picking up the free hydrogen from the Ti-HF reaction.

This alloy has the following different designations:

Republic Steel Co., Titanium Metal Division: Ti-6Al-4V
Special Metal Division: RS-120A

Crucible Steel Co., Titanium Division: C-120AV

Harvey Aluminum Co., Titanium Division: HA-6510

Reactive Metal Products: MST-6Al-4V

Aeronautical Material Specifications: 4928A

Military designation: OS-10737

a. Normal Spectral Emittance (Wavelength Dependence)

There are four sets of experimental data available for the wavelength dependence (0.3-15 μm) of the normal spectral emittance of Titanium Alloy Ti-6Al-4V for oxidized and anodized surfaces. These are tabulated in Table 4-3 and shown in Figure 4-2.

(1) 0.032 μm Finish Alloy

There are no experimental data available for this alloy; however, the recommended values are tabulated in Table 4-1 and shown in Figure 4-1 for Titanium Alloy Ti-6Al-4V alloy of nominal composition and 0.032 μm finish. These values were calculated from the normal spectral reflectance data for the similar material (see Section 4.5.d).

(2) Oxidized Titanium Alloy Ti-6Al-4V

The recommended values tabulated in Table 4-1 and shown in Figure 4-1 for oxidized material are primarily from the investigation of Gravina and Katz [T22613]. These values are considered accurate to within $\pm 15\%$ over the entire wavelength range. The values calculated from the normal spectral reflectance data of Grimm and Fannin [A00001] for a specimen after heating for 15 minutes in air are in good agreement with the recommended values.

(3) Anodized Titanium Alloy Ti-6Al-4V

The recommended values tabulated in Table 4-1 and shown in Figure 4-1 for chromic acid anodized surface are primarily from the investigation of Cunningham and Funai [T22613]. These values are considered accurate to within 15% over the entire wavelength range. It is very important to note that since different anodizing processes may produce entirely different surface finishes, which in turn will affect the radiative properties. This makes it impossible to give recommended values for general cases. Therefore, the above recommended values are for chromic acid anodized surface only. (See Section 4.1.c for further explanation.)

TABLE 4--1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ |
|---|------------|--|------------|--------------------------------------|------------|
| 0.032 μm ALLOY T = 293 | 0.657 | 0.032 μm ANODIZED T = 700 | 0.798 | OXIDIZED HEATED IN AIR T = 700 | 0.778 |
| 0.4 | 0.639 | 2.8 | 0.785 | 2.8 | 0.764 |
| 0.5 | 0.577 | 3.0 | 0.758 | 3.0 | 0.733 |
| 1.0 | 0.535 | 3.5 | 0.747 | 3.5 | 0.714 |
| 1.5 | 0.503 | 4.0 | 0.744 | 3.8 | 0.700 |
| 2.0 | 0.474 | 4.5 | 0.740 | 4.0 | 0.672 |
| 2.5 | 0.460 | 5.0 | 0.738 | 4.5 | 0.646 |
| 3.0 | 0.450 | 5.5 | 0.735 | 5.0 | 0.624 |
| 3.5 | 0.429 | 6.0 | 0.734 | 5.5 | 0.607 |
| 3.8 | 0.418 | 6.3 | 0.730 | 6.0 | 0.595 |
| 4.0 | 0.411 | 6.5 | 0.726 | 6.5 | 0.584 |
| 4.5 | 0.396 | 6.6 | 0.720 | 7.0 | 0.580 |
| 5.0 | 0.384 | 6.8 | 0.691 | 7.5 | 0.575 |
| 5.5 | 0.374 | 7.0 | 0.646 | 8.5 | 0.574 |
| 6.0 | 0.365 | 7.2 | 0.616 | 9.0 | 0.572 |
| 6.5 | 0.358 | 7.4 | 0.604 | 9.5 | 0.571 |
| 7.0 | 0.351 | 7.5 | 0.603 | 10.0 | 0.570 |
| 7.5 | 0.346 | 7.6 | 0.607 | 10.5 | 0.570 |
| 8.0 | 0.340 | 7.8 | 0.646 | 10.6 | 0.570 |
| 8.5 | 0.335 | 8.0 | 0.746 | | |
| 9.0 | 0.330 | 8.2 | 0.868 | | |
| 9.5 | 0.326 | 8.4 | 0.915 | | |
| 10.0 | 0.322 | 8.5 | 0.928 | | |
| 10.5 | 0.318 | 8.7 | 0.938 | | |
| 10.6 | 0.317 | 9.0 | 0.934 | | |
| 11.0 | 0.314 | 9.5 | 0.923 | | |
| 11.5 | 0.308 | 10.0 | 0.920 | | |
| 12.0 | 0.304 | 10.5 | 0.924 | | |
| 12.5 | 0.300 | 11.0 | 0.929 | | |
| 13.0 | 0.295 | 11.5 | 0.935 | | |
| 13.5 | 0.292 | 12.0 | 0.939 | | |
| 14.0 | 0.288 | 12.5 | 0.940 | | |
| 14.5 | 0.284 | 13.0 | 0.933 | | |
| 15.0 | 0.280 | 13.5 | 0.919 | | |
| | | 14.0 | 0.903 | | |
| | | 14.5 | 0.894 | | |
| | | 15.0 | 0.864 | | |

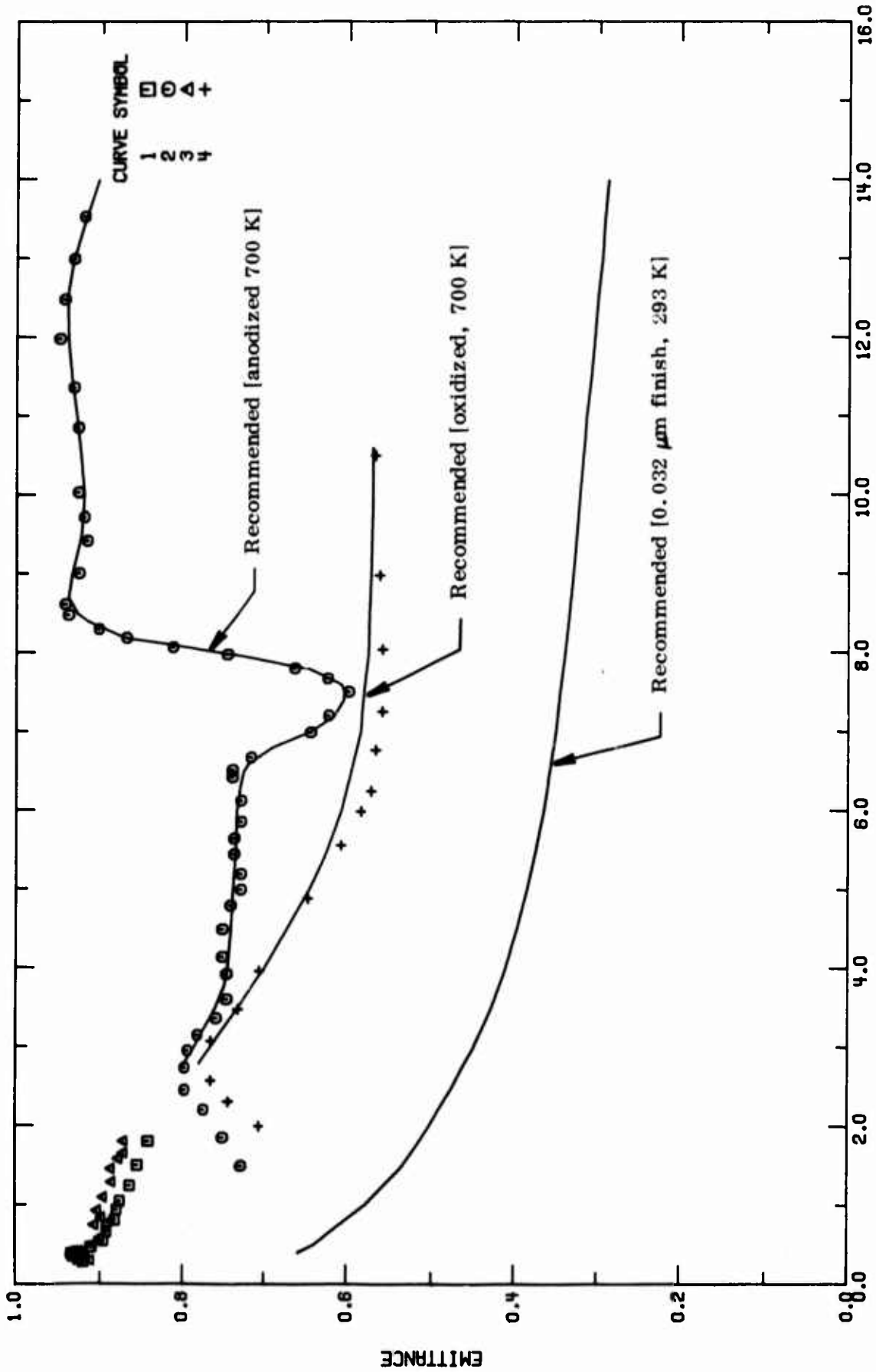


FIGURE 4-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

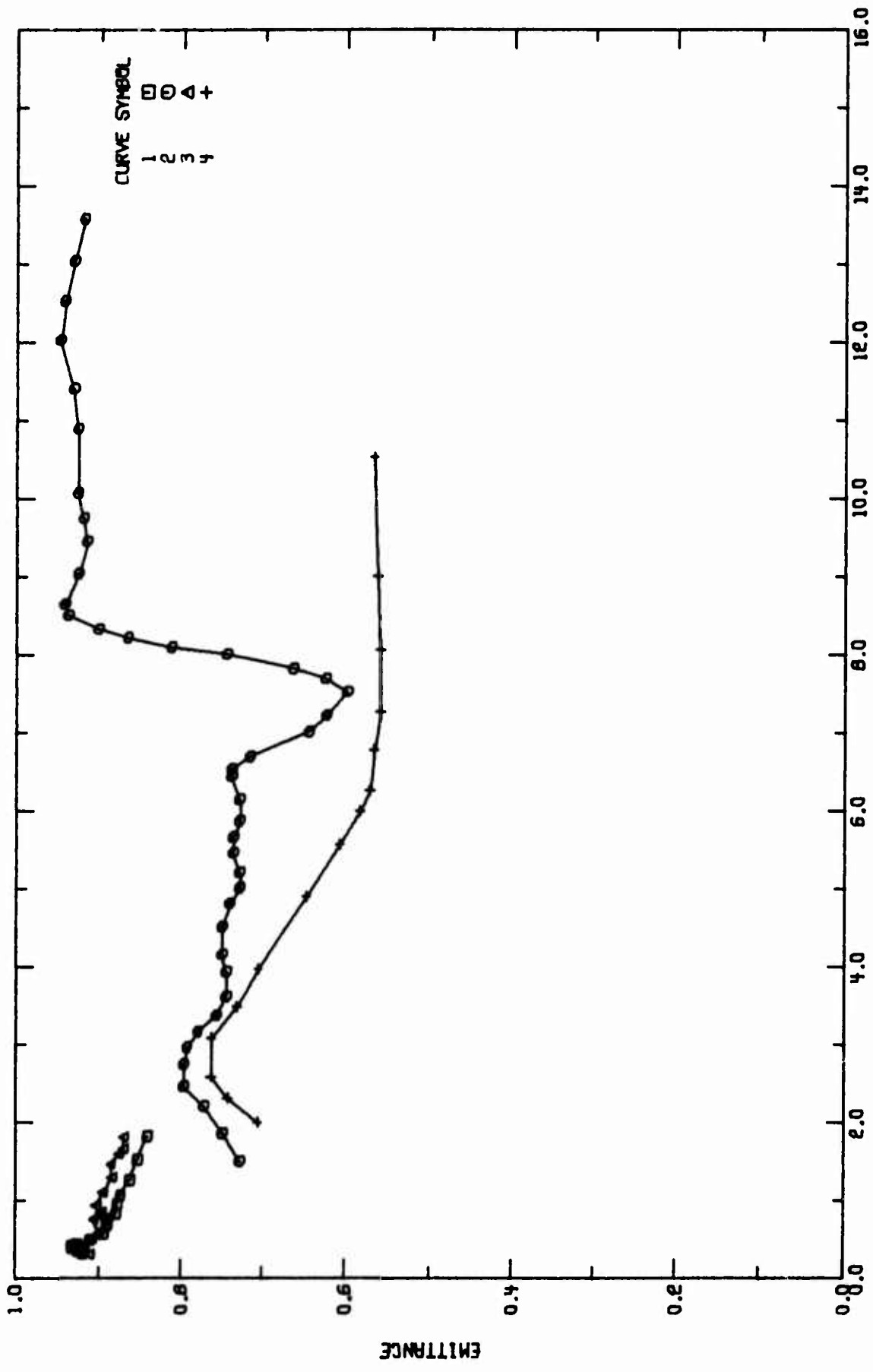


FIGURE 4-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

TABLE 4-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY Ti-6Al-4V (Wavelength Dependence)

| Cit. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T68303 | Cunnington, G.R. and Funai, A.J. | 1972 | 0.29-1.81 | 298 | | MSFC anodized Ti-6Al-4V; measurements before high temperature measurements. |
| 2 T68308 | Cunnington, G.R. and Funai, A.J. | 1972 | 1.5-15 | 700 | | The above specimen. |
| 3 T68308 | Cunnington, G.R. and Funai, A.J. | 1972 | 0.3-1.81 | 298 | | The above specimen; measurements after high temperature measurements. |
| 4 T22613 | Gravina, A. and Katz, M. | 1961 | 2-10.5 | 700 | | Oxidized specimen. |

TABLE 4-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ |
|----------------|------------|-----------|------------|----------------|------------|
| CURVE 1 | | | | | |
| T = 293. | | | | | |
| 0.29 | 0.919 | 6.52 | 0.739 | 1.10 | 0.896 |
| 0.32 | 0.924 | 6.68 | 0.717 | 1.29 | 0.885 |
| 0.36 | 0.930 | 7.00 | 0.644 | 1.46 | 0.886 |
| 0.39 | 0.932 | 7.21 | 0.623 | 1.59 | 0.876 |
| 0.41 | 0.925 | 7.51 | 0.598 | 1.66 | 0.870 |
| 0.47 | 0.910 | 7.68 | 0.624 | 1.81 | 0.870 |
| 0.55 | 0.894 | 7.81 | 0.663 | CURVE 4 | |
| 0.66 | 0.890 | 7.99 | 0.745 | T = 700. | |
| 0.73 | 0.890 | 8.08 | 0.813 | 2.00 | 0.706 |
| 0.81 | 0.890 | 8.20 | 0.866 | 2.31 | 0.743 |
| 0.94 | 0.877 | 8.31 | 0.902 | 2.58 | 0.763 |
| 1.05 | 0.873 | 8.49 | 0.938 | 3.08 | 0.763 |
| 1.25 | 0.861 | 8.63 | 0.942 | 3.48 | 0.732 |
| 1.51 | 0.852 | 9.02 | 0.926 | 3.96 | 0.706 |
| 1.81 | 0.840 | 9.43 | 0.916 | 4.89 | 0.647 |
| CURVE 2 | | | | | |
| T = 700. | | | | | |
| 1.50 | 0.728 | 10.05 | 0.927 | 5.56 | 0.607 |
| 1.86 | 0.749 | 10.87 | 0.927 | 5.99 | 0.583 |
| 2.21 | 0.772 | 11.38 | 0.932 | 6.25 | 0.571 |
| 2.46 | 0.797 | 12.00 | 0.948 | 6.77 | 0.566 |
| 2.74 | 0.797 | 12.50 | 0.943 | 7.26 | 0.559 |
| 2.96 | 0.793 | 13.01 | 0.932 | 8.05 | 0.559 |
| 3.16 | 0.780 | 13.55 | 0.920 | 8.99 | 0.562 |
| 3.37 | 0.757 | 14.18 | 0.909 | 10.51 | 0.567 |
| 3.61 | 0.745 | 14.60 | 0.887 | CURVE 3 | |
| 3.93 | 0.745 | 15.00 | 0.860 | T = 293. | |
| 4.15 | 0.750 | 0.30 | 0.912 | | |
| 4.80 | 0.741 | 0.34 | 0.918 | | |
| 5.00 | 0.729 | 0.37 | 0.922 | | |
| 5.20 | 0.729 | 0.41 | 0.922 | | |
| 5.45 | 0.737 | 0.50 | 0.909 | | |
| 5.65 | 0.737 | 0.58 | 0.900 | | |
| 5.86 | 0.729 | 0.75 | 0.907 | | |
| 6.13 | 0.729 | 0.80 | 0.886 | | |
| 6.43 | 0.739 | 0.84 | 0.890 | | |
| | | 0.93 | 0.904 | | |

b. Normal Spectral Emittance (Temperature Dependence)

There are 22 experimental data sets for the temperature dependence (1100-1700 K) at $\lambda = 0.65 \mu\text{m}$ of the normal spectral emittance of Titanium Alloy Ti-6Al-4V. These are tabulated in Table 4-5 and shown in Figure 4-3. Since no measurements are located at higher wavelengths, no recommendations are made.

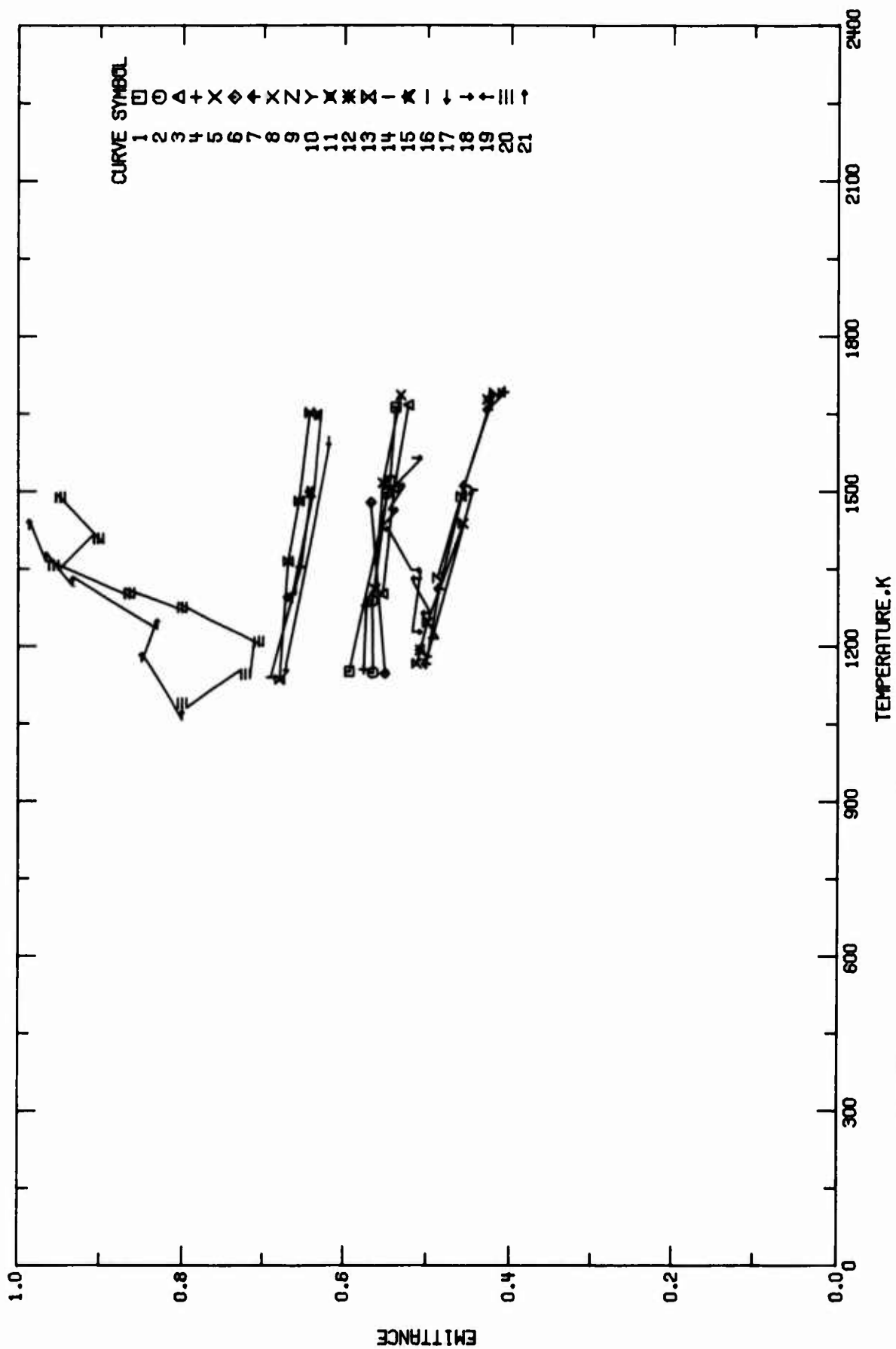


FIGURE 4-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE).

TABLE 4-4. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY Ti-6Al-4V (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T6979 | Betz, H. T., Olson, O. H., Schuriz, B. D., and Morris, J. C. | 1957 | 0.665 | 1153-1665 | | Nominal composition, specimen as received, cleaned with liquid detergent, measurements in vacuum (5×10^{-4} mm Hg) with increasing temperature, cycle one; $9 \sim 0^\circ$. |
| 2 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1150-1498 | | Similar to the above specimen and condition, decreasing temperature, cycle one. |
| 3 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1303-1669 | | Similar to the above specimen and condition, increasing temperature, cycle two. |
| 4 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1156-1280 | | Similar to the above specimen and condition, decreasing temperature, cycle two. |
| 5 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1312-1688 | | Similar to the above specimen and condition, increasing temperature, cycle three. |
| 6 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1148-1480 | | Similar to the above specimen and condition, decreasing temperature, cycle three. |
| 7 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1166-1693 | | Similar to the above specimen; polished with fine polishing compounds on a buffing wheel, increasing temperature cycle one. |
| 8 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1439-1167 | | Similar to the above specimen and condition, decreasing temperature, cycle one. |
| 9 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1334-1691 | | Similar to the above specimen and condition, increasing temperature, cycle two. |
| 10 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1504-1181 | | Similar to the above specimen and condition, decreasing temperature, cycle two. |
| 11 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1679 | | Similar to the above specimen and condition, cycle three. |
| 12 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1194 | | Similar to the above specimen and condition, cycle three. |
| 13 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1136-1654 | | Similar to the specimen from curve 1 except oxidized in air at red heat for 30 min, increasing temperature, cycle 1. |
| 14 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1491-1140 | | Similar to the above specimen and condition, decreasing temperature, cycle one. |
| 15 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1649-1296 | | Similar to the above specimen and condition, decreasing temperature, cycle one. |
| 16 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1312 | | Similar to the above specimen and condition, cycle two. |
| 17 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1597-1159 | | Similar to the above specimen and condition, cycle two. |
| 18 T6979 | Betz, H. T., et al. | 1957 | 0.665 | 1566-1229 | | Similar to the above specimen and condition, cycle three. |
| 19 T23145 | Skjarew, S. and Rabensteine, A. S. | 1963 | 0.65 | 1556-1229 | | Titanium alloy 6Al-4V; 5.5-6.5Al, 3.5-4.5V, 0.1 max C, 0.3 max Fe, 0.05 max N, 0.0125 max H, 0.15 max O ₂ , Ti balance; polished; surface roughness 2 to 3 μRMS ; measurements in vacuum (3 to 4×10^{-4} mm Hg); measurements with decreasing temperature. |
| 20 T23145 | Skjarew, S. and Rabensteine, A. S. | 1963 | 0.65 | 1216-1332 | | Similar to the above specimen and condition, measurements with increasing temperature. |
| 21* T23145 | Skjarew, S. and Rabensteine, A. S. | 1963 | 0.65 | 1490-1090 | | Similar to the above specimen except coated with Rokide "C", decreasing temperature. |
| 22* T23145 | Skjarew, S. and Rabensteine, A. S. | 1963 | 0.65 | 1066-1438 | | Similar to the above specimen except measurements with increasing temperature. |

* Not shown in figure.

TABLE 4-5. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|-------------------------------|------------|-------------------------------|------------|-------|------------|------------------------------|------------|
| CURVE 1 $\lambda = 0.665$ | | | | | | | |
| 1152. | 0.592 | 1166. | 0.500 | 1136. | 0.679 | 1216. | 0.491 |
| 1521. | 0.544 | 1312. | 0.485 | 1366. | 0.669 | 1265. | 0.501 |
| 1665. | 0.537 | 1512. | 0.455 | 1483. | 0.656 | 1332. | 0.513 |
| | | 1659. | 0.427 | 1654. | 0.643 | | |
| | | 1693. | 0.407 | | | | |
| CURVE 2 $\lambda = 0.665$ | | | | | | | |
| 1150. | 0.564 | CURVE 14 $\lambda = 0.665$ | | | | | |
| 1290. | 0.565 | | | | | 1090. | 0.800 |
| 1498. | 0.548 | | | | | 1147. | 0.722 |
| CURVE 3 $\lambda = 0.665$ | | | | | | | |
| 1303. | 0.553 | | | | | 1210. | 0.705 |
| 1508. | 0.539 | | | | | 1276. | 0.800 |
| 1669. | 0.522 | | | | | 1304. | 0.864 |
| CURVE 4 $\lambda = 0.665$ | | | | | | | |
| 1303. | 0.553 | | | | | 1358. | 0.955 |
| 1508. | 0.539 | | | | | 1410. | 0.901 |
| 1669. | 0.522 | | | | | 1490. | 0.947 |
| CURVE 5 $\lambda = 0.665$ | | | | | | | |
| 1156. | 0.575 | | | | | CURVE 21 $\lambda = 0.65$ | |
| 1280. | 0.572 | | | | | 1066. | 0.800 |
| CURVE 6 $\lambda = 0.665$ | | | | | | | |
| 1312. | 0.562 | | | | | 1179. | 0.850 |
| 1518. | 0.553 | | | | | 1244. | 0.832 |
| 1688. | 0.531 | | | | | 1327. | 0.932 |
| | | | | | | 1374. | 0.964 |
| | | | | | | 1438. | 0.985 |
| CURVE 7 $\lambda = 0.665$ | | | | | | | |
| 1166. | 0.500 | | | | | | |
| 1312. | 0.485 | | | | | | |
| 1512. | 0.455 | | | | | | |
| 1659. | 0.427 | | | | | | |
| 1693. | 0.407 | | | | | | |
| CURVE 8 $\lambda = 0.665$ | | | | | | | |
| 1167. | 0.512 | | | | | | |
| 1247. | 0.499 | | | | | | |
| 1439. | 0.456 | | | | | | |
| CURVE 9 $\lambda = 0.665$ | | | | | | | |
| 1334. | 0.487 | | | | | | |
| 1492. | 0.459 | | | | | | |
| 1691. | 0.420 | | | | | | |
| CURVE 10 $\lambda = 0.665$ | | | | | | | |
| 1161. | 0.499 | | | | | | |
| 1584. | 0.445 | | | | | | |
| CURVE 11 $\lambda = 0.665$ | | | | | | | |
| 1679. | 0.428 | | | | | | |
| CURVE 12 $\lambda = 0.665$ | | | | | | | |
| 1194. | 0.508 | | | | | | |
| CURVE 13 $\lambda = 0.665$ | | | | | | | |
| 1229. | 0.512 | | | | | | |
| 1349. | 0.513 | | | | | | |
| 1429. | 0.552 | | | | | | |
| 1466. | 0.541 | | | | | | |
| 1513. | 0.533 | | | | | | |
| 1566. | 0.512 | | | | | | |

c. Angular Spectral Emittance (Wavelength Dependence)

There are no experimental data located in the literature. The recommended values at 293 K tabulated in Table 4-6 and shown in Figure 4-4 are for pickled Titanium Ti-6Al-4V alloy of thickness 40 mil and the incident angle, $\theta = 45^\circ$. These values calculated from the angular spectral reflectance data tabulated in Table 4-12 are considered accurate to within $\pm 15\%$ at reported wavelengths. Unfortunately the authors gave only four data points, so no attempt was made to interpolate their data.

TABLE 4-6. RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ |
|-----------------------------|------------|
| PICKLED ALLOY T = 293 | |
| 2.6 | 0.42 |
| 3.8 | 0.37 |
| 5.0 | 0.31 |
| 10.6 | 0.22 |

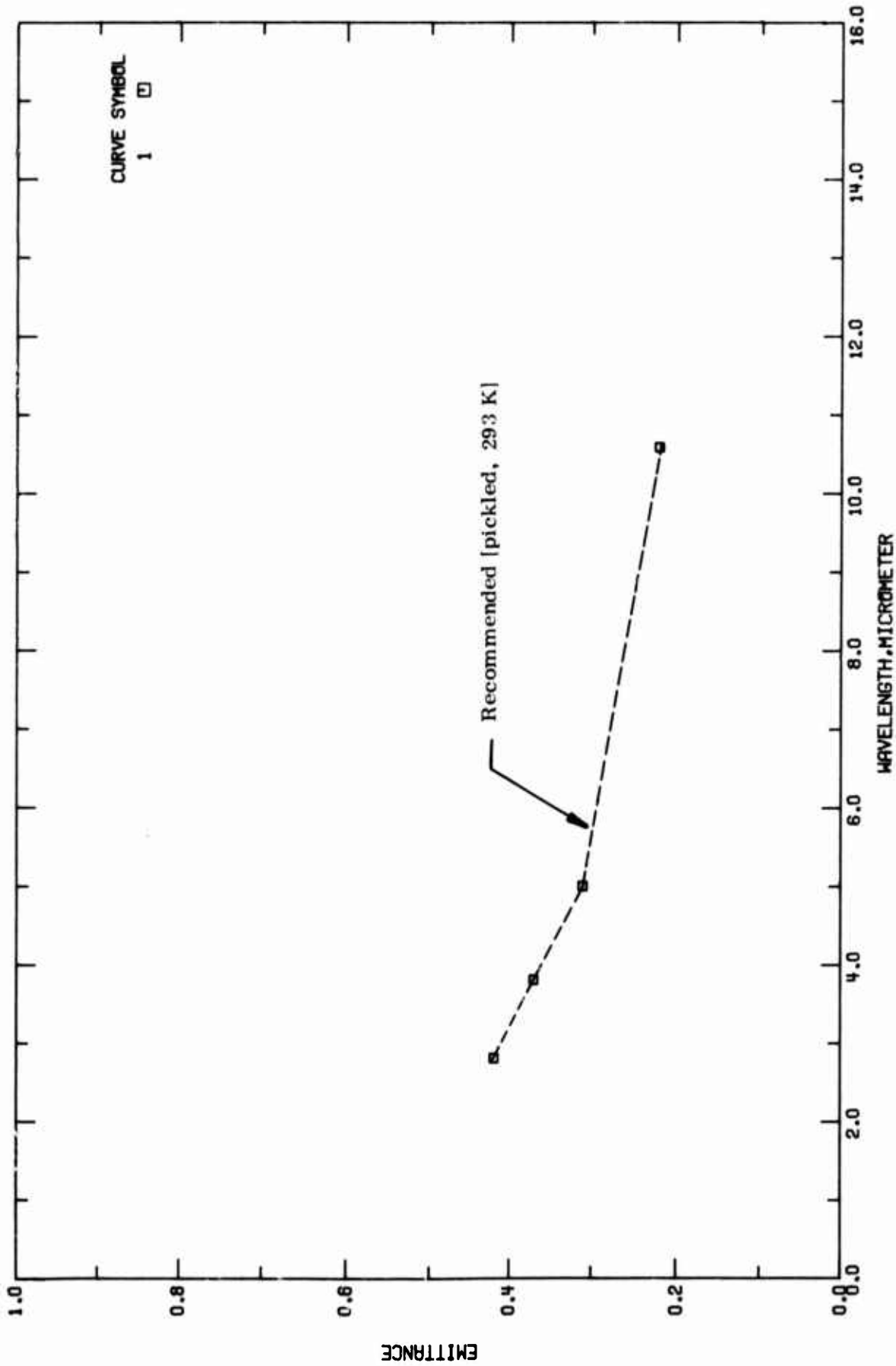


FIGURE 4-4. RECOMMENDED ANGULAR SPECTRAL EMITTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

d. Normal Spectral Reflectance (Wavelength Dependence)

There are 13 experimental data sets available for the wavelength dependence (2.8-10.6 μm) of the normal spectral reflectance of Titanium Alloy Ti-6Al-4V. These are tabulated in Table 4-9 and shown in Figure 4-6.

(1) 0.032 μm Finish Alloy

The recommended values at 293 K tabulated in Table 4-7 and shown in Figure 4-5 for Titanium Alloy Ti-6Al-4V with 0.032 μm finish are primarily from the investigations of Shipley and Thostesen [T40746]. These values are considered accurate to within $\pm 15\%$ over the entire wavelength range.

(2) Oxidized Titanium Alloy Ti-6Al-4V

The recommended values tabulated in Table 4-7 and shown in Figure 4-5 for oxidized Titanium Alloy Ti-6Al-4V are primarily from the investigation of Grimm and Fannin [A00001] and are for the material which has been heated in air for 15 minutes. These are considered accurate to within $\pm 15\%$ over the entire wavelength range. The values calculated from the normal emittance data of Gravina and Katz [T22613] for similar oxidized Titanium Alloy Ti-6Al-4V are in good agreement with the recommended values.

(3) Anodized Titanium Alloy Ti-6Al-4V

The recommended values tabulated in Table 4-7 and shown in Figure 4-5 for chromic acid anodized surface were calculated from the normal spectral emittance data of Cunnington and Funai [T22613]. These are considered accurate to about $\pm 15\%$ over the entire wavelength range. (See Section 4.1.c and 4.5.a for further details.)

TABLE 4-7. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|---------------------|--------|---------------------|--------|---------------|--------|---------------|--------|
| 0.032 μm | FINISH | 0.032 μm | FINISH | OXIDIZED | | OXIDIZED | |
| ALLOY | | ANODIZED | | HEATED IN AIR | | HEATED IN AIR | |
| T = 293 | | T = 700 | | T = 700 | | T = 700 | |
| 0.4 | 0.343 | 2.8 | 0.202 | 2.8 | 0.222 | 2.8 | 0.222 |
| 0.5 | 0.361 | 3.0 | 0.215 | 3.0 | 0.236 | 3.0 | 0.236 |
| 1.0 | 0.423 | 3.5 | 0.242 | 3.5 | 0.267 | 3.5 | 0.267 |
| 1.5 | 0.465 | 3.8 | 0.253 | 3.8 | 0.286 | 3.8 | 0.286 |
| 2.0 | 0.497 | 4.0 | 0.256 | 4.0 | 0.300 | 4.0 | 0.300 |
| 2.5 | 0.526 | 4.5 | 0.260 | 4.5 | 0.328 | 4.5 | 0.328 |
| 3.0 | 0.550 | 5.0 | 0.262 | 5.0 | 0.354 | 5.0 | 0.354 |
| 3.5 | 0.571 | 5.5 | 0.265 | 5.5 | 0.376 | 5.5 | 0.376 |
| 3.8 | 0.582 | 6.0 | 0.266 | 6.0 | 0.397 | 6.0 | 0.397 |
| 4.0 | 0.589 | 6.3 | 0.270 | 6.3 | 0.405 | 6.3 | 0.405 |
| 4.5 | 0.604 | 6.5 | 0.274 | 6.5 | 0.416 | 6.5 | 0.416 |
| 5.0 | 0.616 | 6.6 | 0.280 | 6.6 | 0.420 | 6.6 | 0.420 |
| 5.5 | 0.626 | 6.8 | 0.309 | 6.8 | 0.425 | 6.8 | 0.425 |
| 6.0 | 0.635 | 7.0 | 0.354 | 7.0 | 0.426 | 7.0 | 0.426 |
| 6.5 | 0.642 | 7.2 | 0.384 | 7.2 | 0.428 | 7.2 | 0.428 |
| 7.0 | 0.649 | 7.4 | 0.396 | 7.4 | 0.429 | 7.4 | 0.429 |
| 7.5 | 0.654 | 7.5 | 0.397 | 7.5 | 0.429 | 7.5 | 0.429 |
| 8.0 | 0.660 | 7.6 | 0.393 | 7.6 | 0.430 | 7.6 | 0.430 |
| 8.5 | 0.665 | 7.8 | 0.354 | 7.8 | 0.430 | 7.8 | 0.430 |
| 9.0 | 0.670 | 8.0 | 0.254 | 8.0 | 0.430 | 8.0 | 0.430 |
| 9.5 | 0.674 | 8.2 | 0.132 | 8.2 | 0.430 | 8.2 | 0.430 |
| 10.0 | 0.678 | 8.4 | 0.085 | 8.4 | 0.429 | 8.4 | 0.429 |
| 10.5 | 0.682 | 8.5 | 0.072 | 8.5 | 0.428 | 8.5 | 0.428 |
| 10.6 | 0.683 | 8.7 | 0.062 | 8.7 | 0.428 | 8.7 | 0.428 |
| 11.0 | 0.686 | 9.0 | 0.066 | 9.0 | 0.428 | 9.0 | 0.428 |
| 11.5 | 0.692 | 9.5 | 0.077 | 9.5 | 0.428 | 9.5 | 0.428 |
| 12.0 | 0.696 | 10.0 | 0.080 | 10.0 | 0.428 | 10.0 | 0.428 |
| 12.5 | 0.700 | 10.5 | 0.076 | 10.5 | 0.428 | 10.5 | 0.428 |
| 13.0 | 0.705 | 11.0 | 0.071 | 11.0 | 0.428 | 11.0 | 0.428 |
| 13.5 | 0.708 | 11.5 | 0.065 | 11.5 | 0.428 | 11.5 | 0.428 |
| 14.0 | 0.712 | 12.0 | 0.061 | 12.0 | 0.428 | 12.0 | 0.428 |
| 14.5 | 0.716 | 12.5 | 0.060 | 12.5 | 0.428 | 12.5 | 0.428 |
| 15.0 | 0.720 | 13.0 | 0.067 | 13.0 | 0.428 | 13.0 | 0.428 |
| | | 13.5 | 0.081 | 13.5 | 0.428 | 13.5 | 0.428 |
| | | 14.0 | 0.097 | 14.0 | 0.428 | 14.0 | 0.428 |
| | | 14.5 | 0.106 | 14.5 | 0.428 | 14.5 | 0.428 |
| | | 15.0 | 0.136 | 15.0 | 0.428 | 15.0 | 0.428 |

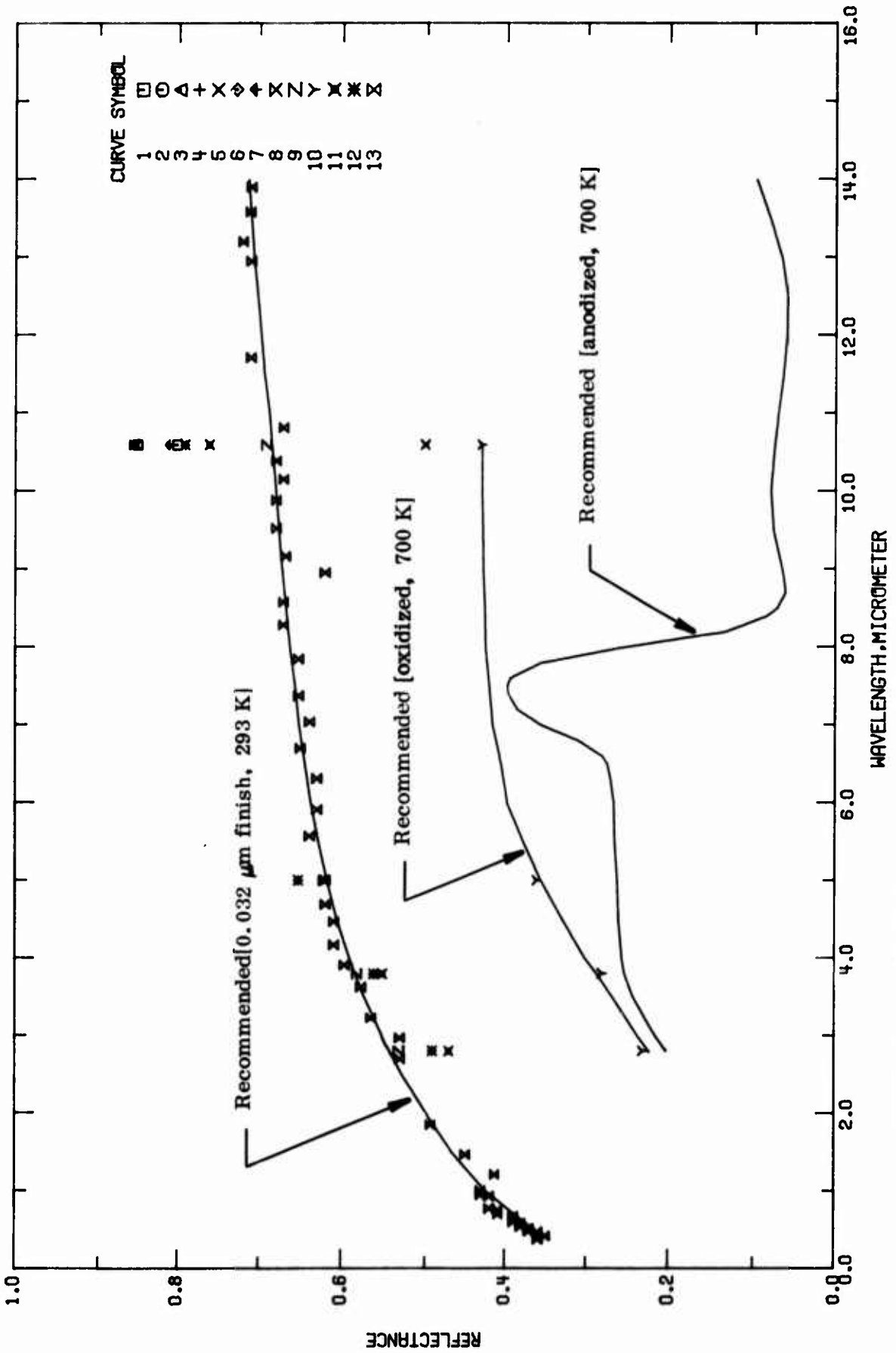


FIGURE 4-5. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

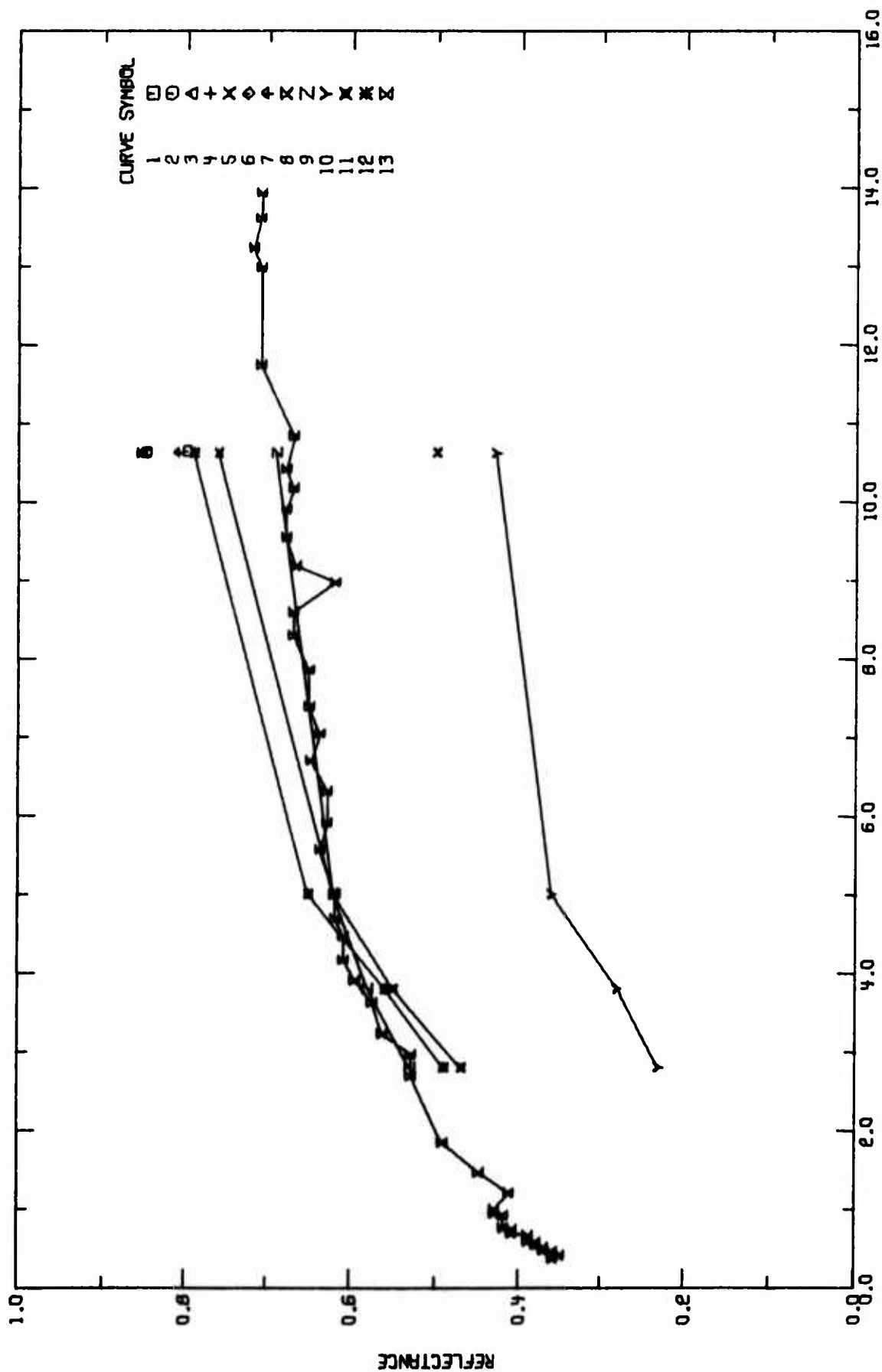


FIGURE 4-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

TABLE 4-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY Ti-6Al-4V (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney Metals, 4 mil. |
| 2 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 3 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney metals, 10 mil. |
| 4 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 5 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the specimen from curve 3 except sand blasted. |
| 6 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the specimen from curve 3 except chemically milled. |
| 7 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Timet Corp.; 15 mil. |
| 8 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 9 A00001 | Grimm, T.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | | Compilation, 125 $\mu\text{in.}$ finish. |
| 10 A00001 | Grimm, T.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 700 | | Measurements after being heated in air for 15 min. |
| 11 A00001 | Grimm, T.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | | Pickled Ti-6Al-4V; thickness: 40 mil; $\theta = 15^\circ$. |
| 12 A00001 | Grimm, T.C. and Fannin, E.R. | 1972 | 2.8-10.6 | 293 | | Similar to the above specimen except heat treated in air at 644 K for one hr. |
| 13 T40746 | Shipley, W.S. and Thorstesen, T.O. | 1960 | 0.38-25 | 300 | | Nominal composition; "125" finish. |

TABLE 4-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|---------------------|--------|----------------------|--------|------------------|--------|------------------|--------|------------------|--------|
| CURVE 1 T = 293. | | CURVE 9 T = 293. | | CURVE 13 (CONT.) | | CURVE 13 (CONT.) | | CURVE 13 (CONT.) | |
| 10.6 | 0.800 | 2.8 | 0.53 | 0.54 | 0.379 | 13.21 | 0.719 | 13.21 | 0.719 |
| | | 3.8 | 0.58 | 0.58 | 0.379 | 13.59 | 0.710 | 13.59 | 0.710 |
| CURVE 2 T = 293. | | 5.0 | 0.62 | 0.60 | 0.388 | 13.91 | 0.709 | 13.91 | 0.709 |
| | | 10.6 | 0.69 | 0.67 | 0.388 | 14.26 | 0.728 | 14.26 | 0.728 |
| 10.6 | 0.850 | | | 0.70 | 0.408 | 14.64 | 0.700 | 14.64 | 0.700 |
| | | CURVE 10 T = 700. | | 0.75 | 0.408 | 14.88 | 0.729 | 14.88 | 0.729 |
| | | | | 0.77 | 0.419 | 15.16 | 0.741 | 15.16 | 0.741 |
| CURVE 3 T = 293. | | | | 0.93 | 0.419 | 15.54 | 0.729 | 15.54 | 0.729 |
| | | | | 0.95 | 0.430 | 15.83 | 0.730 | 15.83 | 0.730 |
| | | | | 1.00 | 0.430 | 16.13 | 0.740 | 16.13 | 0.740 |
| 10.6 | 0.850 | | | 1.21 | 0.412 | 17.96 | 0.740 | 17.96 | 0.740 |
| | | | | 1.47 | 0.449 | 18.24 | 0.760 | 18.24 | 0.760 |
| | | | | 1.85 | 0.492 | 18.93 | 0.760 | 18.93 | 0.760 |
| CURVE 4 T = 293. | | | | 2.70 | 0.529 | 19.20 | 0.750 | 19.20 | 0.750 |
| | | | | 2.97 | 0.529 | 19.59 | 0.760 | 19.59 | 0.760 |
| | | | | 3.23 | 0.563 | 20.00 | 0.760 | 20.00 | 0.760 |
| 10.6 | 0.855 | | | 3.63 | 0.575 | 20.24 | 0.770 | 20.24 | 0.770 |
| | | | | 3.91 | 0.595 | 20.39 | 0.761 | 20.39 | 0.761 |
| CURVE 5 T = 293. | | | | 4.17 | 0.608 | 20.68 | 0.772 | 20.68 | 0.772 |
| | | | | 4.47 | 0.608 | 20.86 | 0.772 | 20.86 | 0.772 |
| | | | | 4.69 | 0.618 | 21.42 | 0.772 | 21.42 | 0.772 |
| 10.6 | 0.500 | | | 5.00 | 0.618 | 21.61 | 0.762 | 21.61 | 0.762 |
| | | | | 5.57 | 0.637 | 21.91 | 0.780 | 21.91 | 0.780 |
| CURVE 6 T = 293. | | | | 5.91 | 0.628 | 22.07 | 0.770 | 22.07 | 0.770 |
| | | | | 6.31 | 0.628 | 22.25 | 0.770 | 22.25 | 0.770 |
| | | | | 6.70 | 0.648 | 22.41 | 0.780 | 22.41 | 0.780 |
| 10.6 | 0.855 | | | 7.04 | 0.637 | 22.57 | 0.771 | 22.57 | 0.771 |
| | | | | 7.38 | 0.650 | 22.72 | 0.780 | 22.72 | 0.780 |
| CURVE 7 T = 293. | | | | 7.85 | 0.650 | 22.89 | 0.771 | 22.89 | 0.771 |
| | | | | 8.29 | 0.669 | 23.08 | 0.771 | 23.08 | 0.771 |
| | | | | 8.58 | 0.669 | 23.24 | 0.771 | 23.24 | 0.771 |
| 10.6 | 0.81 | | | 8.96 | 0.619 | 23.36 | 0.782 | 23.36 | 0.782 |
| | | | | 9.17 | 0.666 | 23.54 | 0.771 | 23.54 | 0.771 |
| CURVE 8 T = 293. | | | | 9.53 | 0.678 | 23.68 | 0.779 | 23.68 | 0.779 |
| | | | | 9.89 | 0.678 | 23.87 | 0.771 | 23.87 | 0.771 |
| | | | | 10.16 | 0.669 | 24.31 | 0.771 | 24.31 | 0.771 |
| 10.6 | 0.855 | | | 10.40 | 0.678 | 24.48 | 0.760 | 24.48 | 0.760 |
| | | | | 10.82 | 0.669 | 25.00 | 0.760 | 25.00 | 0.760 |
| | | | | 11.72 | 0.709 | | | | |
| | | | | 12.96 | 0.709 | | | | |

e. Normal Spectral Reflectance (Temperature Dependence)

There are 10 sets of experimental data available for the temperature dependence of the normal spectral reflectance of Titanium Alloy Ti-6Al-4V under various surface conditions. These are tabulated in Table 4-11 and shown in Figure 4-7. In the absence of sufficient data, no recommendations were made.

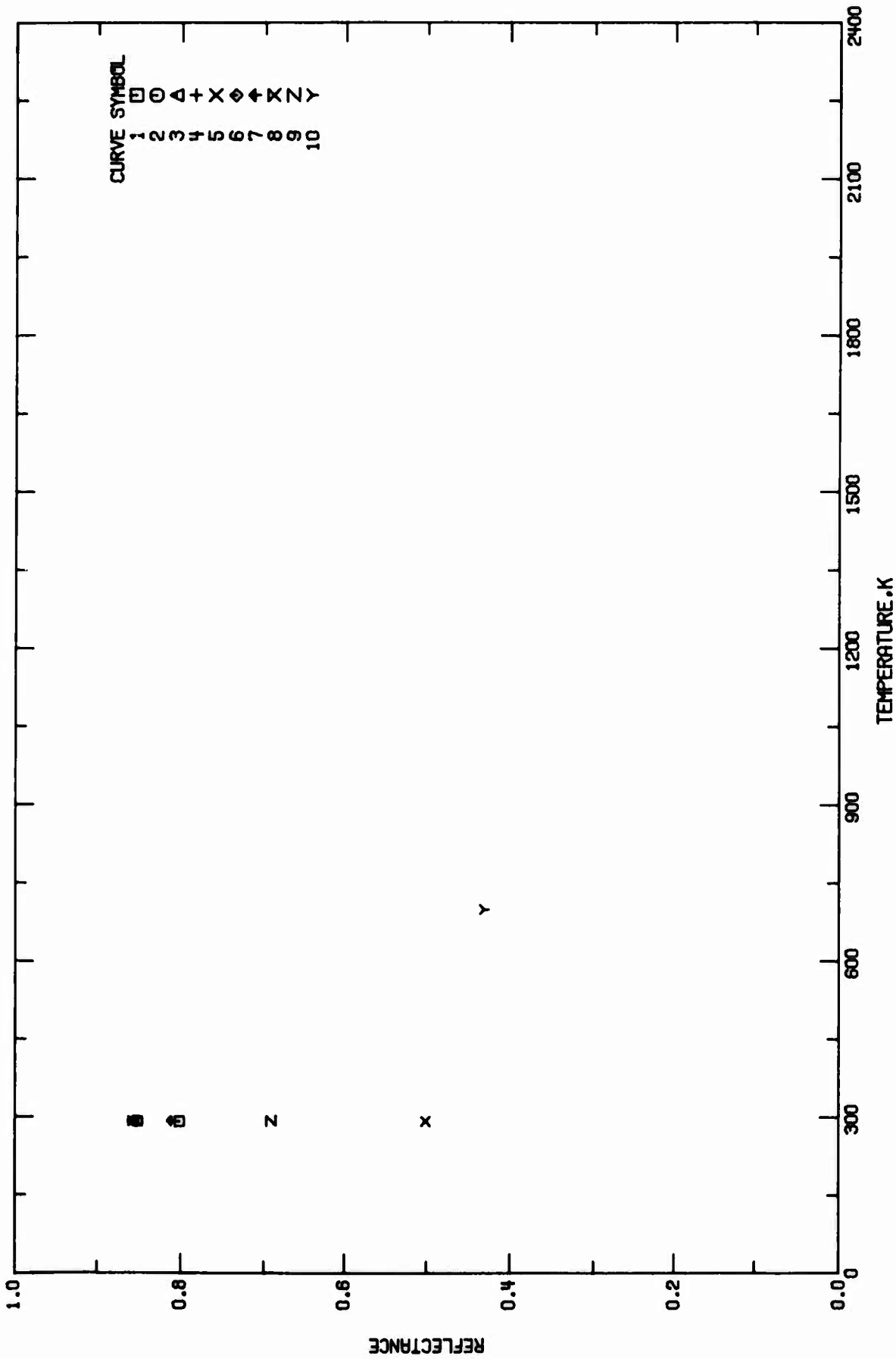


FIGURE 4-7. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE).

TABLE 4-10. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY Ti-6Al-4V (Temperature Dependence)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00002 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney Metals, 4 mil. |
| 2 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 3 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney metal, 10 mil. |
| 4 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 5 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the specimen from curve 3 except sand blasted. |
| 6 A00002 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the specimen from curve 3 except chemically milled. |
| 7 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Timet Corp.; 15 mil. |
| 8 A00003 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 9 A00001 | Grimm, T.C. and Farnir, E.R. | 1973 | 10.6 | 293 | | Compilation, 125 μ inch finish. |
| 10 A00001 | Grimm, T.C. and Farnir, E.R. | 1973 | 10.6 | 700 | | Similar to the above specimen, measurements after being heated in air for 15 min. |

TABLE 4-11. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| T | ρ | T | ρ |
|-----------------------------|--------|------------------------------|--------|
| CURVE 1 $\lambda = 10.6$ | | CURVE 9 $\lambda = 10.6$ | |
| 293. | 0.800 | 293. | 0.69 |
| CURVE 2 $\lambda = 10.6$ | | CURVE 10 $\lambda = 10.6$ | |
| 293. | 0.650 | 700. | 0.43 |
| CURVE 3 $\lambda = 10.6$ | | | |
| 293. | 0.650 | | |
| CURVE 4 $\lambda = 10.6$ | | | |
| 293. | 0.855 | | |
| CURVE 5 $\lambda = 10.6$ | | | |
| 293. | 0.500 | | |
| CURVE 6 $\lambda = 10.6$ | | | |
| 293. | 0.855 | | |
| CURVE 7 $\lambda = 10.6$ | | | |
| 293. | 0.810 | | |
| CURVE 8 $\lambda = 10.6$ | | | |
| 293. | 0.855 | | |

f. Angular Spectral Reflectance (Wavelength Dependence)

There is only one set of experimental data that is available. This one is tabulated in Table 4-14 and shown in Figure 4-9.

The recommended values tabulated in Table 4-12 and shown in Figure 4-8 are for 40 mil thick pickled Titanium Alloy Ti-6Al-4V with the incident angle, $\theta = 45^\circ$. These values primarily from the investigation of Grimm and Fannin [A00001] are considered accurate to within $\pm 15\%$ at the reported wavelengths.

TABLE 4-12. RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------------------------|--------|
| PICKLED ALLOY T = 293 | |
| 2.8 | 0.58 |
| 3.8 | 0.63 |
| 5.0 | 0.69 |
| 10.6 | 0.78 |

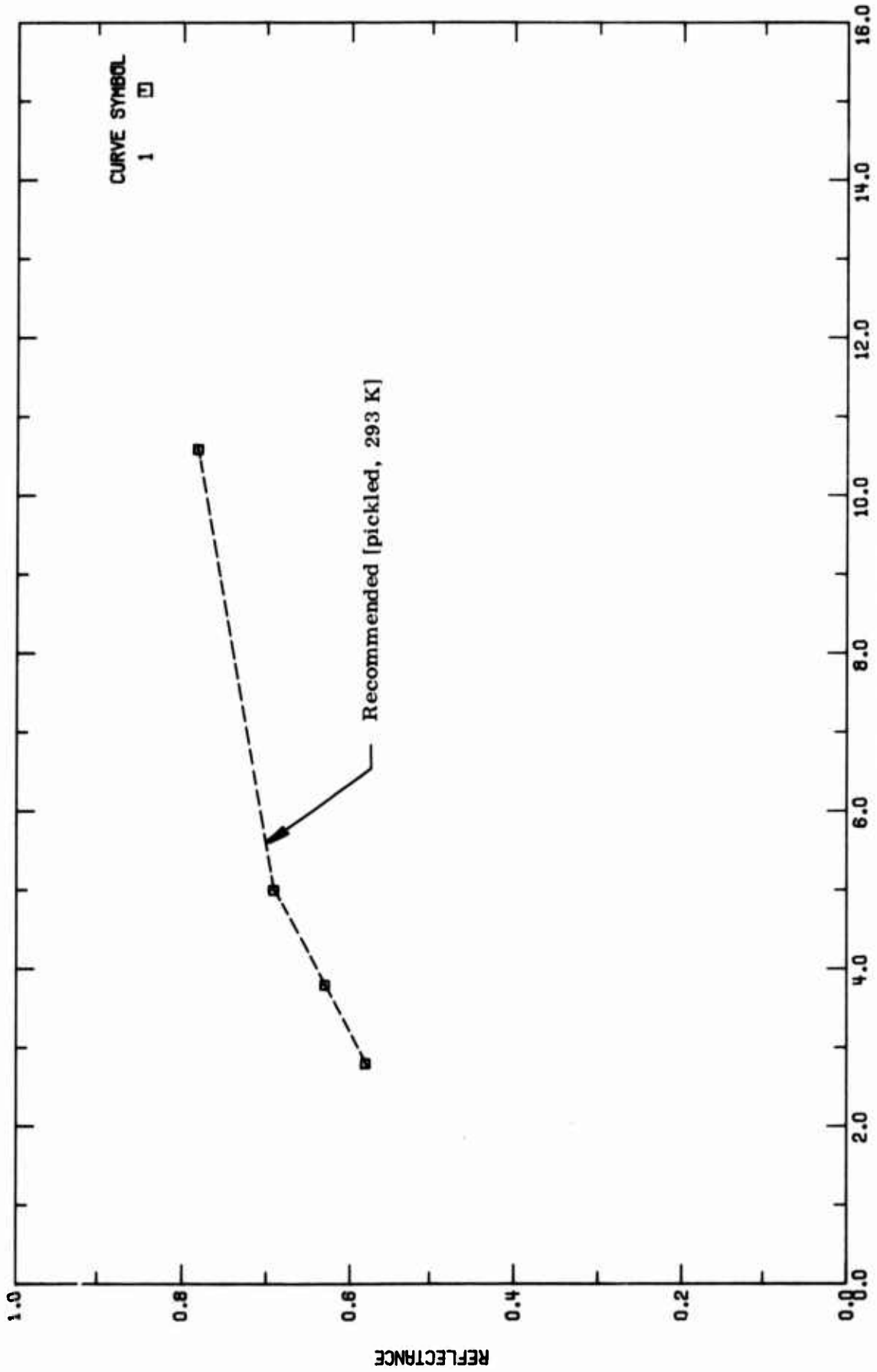


FIGURE 4-8. RECOMMENDED ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

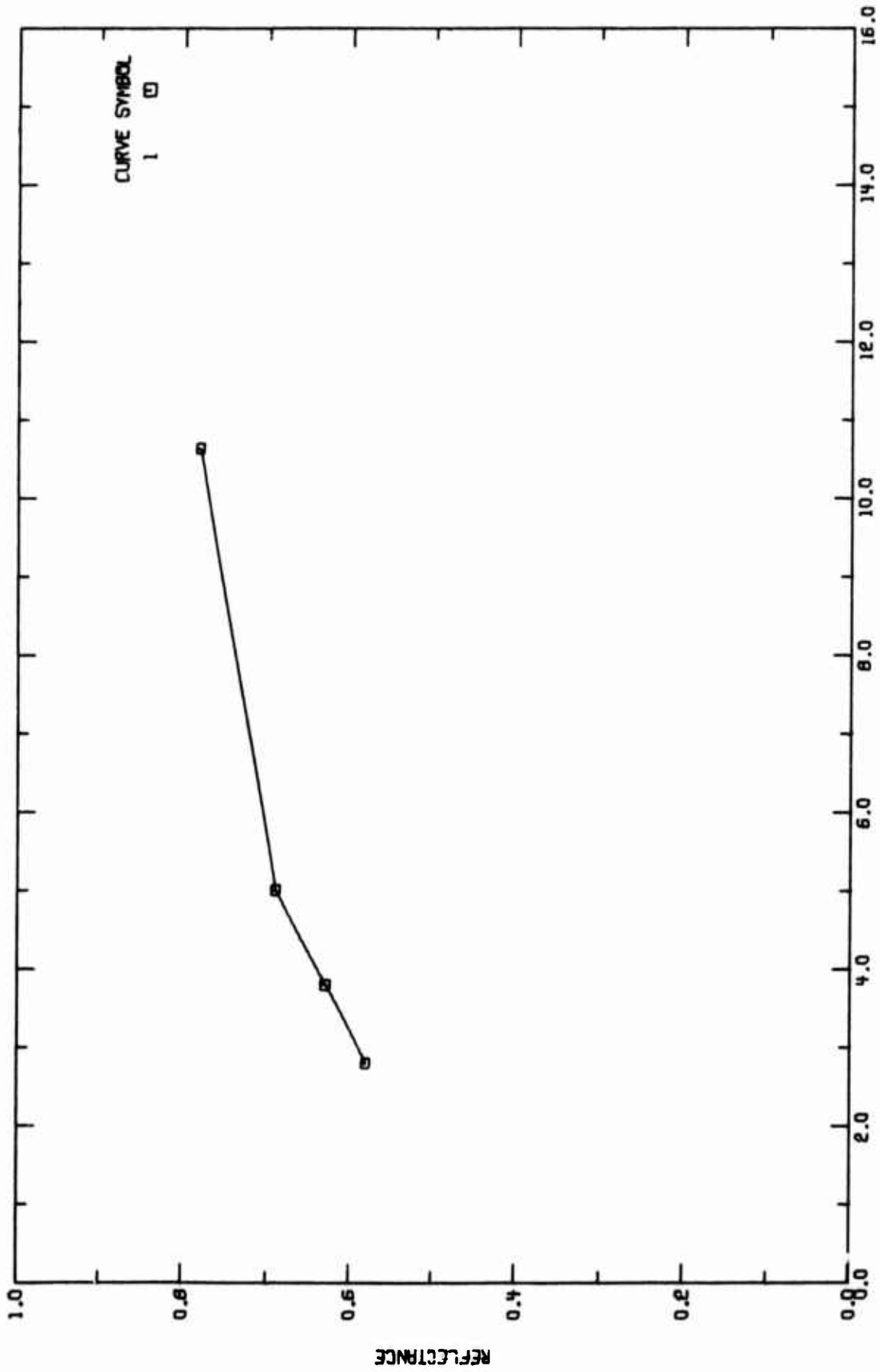


FIGURE 4-9. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY
TI-6AL-4V (WAVELENGTH DEPENDENCE).

TABLE 4-13. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY Ti-6Al-4V (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00001 | Grimm, T. C. and Fannin, E. R. | 1972 | 2.8-10.6 | 293 | | Pickled Ti-6Al-4V alloy, 40 mil. thickness; $\theta = 45^\circ$. |

TABLE 4-14. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------|--------|
| CURVE 1 | |
| T = 293. | |
| 2.8 | 0.58 |
| 3.8 | 0.63 |
| 5.0 | 0.69 |
| 10.6 | 0.78 |

g. Normal Spectral Absorptance (Wavelength Dependence)

There are 16 sets of experimental data available for the wavelength dependence (2.8 μm) of the normal spectral absorptance of Titanium Alloy Ti-6Al-4V under various surface conditions. These are tabulated in Table 4-17 and shown in Figure 4-11.

(1) 0.032 μm Finish Alloy

The recommended values tabulated in Table 4-15 and shown in Figure 4-10 calculated from the normal spectral emittance data on the identical material are considered accurate to about $\pm 15\%$ over the entire wavelength range (see Section 4.5.a).

(2) Oxidized Titanium Alloy Ti-6Al-4V

The recommended values tabulated in Table 4-15 and shown in Figure 4-10 calculated from the normal spectral emittance data on the identical material are considered accurate to about $\pm 15\%$ over entire wavelength range (see Section 4.5.a).

(3) Anodized Titanium Alloy Ti-6Al-4V

The recommended values for chromic acid anodized surface and tabulated in Table 4-15 and shown in Figure 4-10 calculated from the normal spectral emittance data on the identical material are considered accurate to about $\pm 15\%$ over the entire wavelength region (see Section 4.1.c and 4.5.a).

TABLE 4-15. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α |
|---|----------|--|----------|--------------------------------------|----------|
| 0.032 μm ALLOY T = 293 | FINISH | 0.032 μm ANODIZED T = 700 | FINISH | OXIDIZED HEATED IN AIR T = 700 | α |
| 0.4 | 0.657 | 2.8 | 0.798 | 2.8 | 0.778 |
| 0.5 | 0.639 | 3.0 | 0.785 | 3.0 | 0.764 |
| 1.0 | 0.577 | 3.5 | 0.758 | 3.5 | 0.733 |
| 1.5 | 0.535 | 3.8 | 0.747 | 3.8 | 0.714 |
| 2.0 | 0.503 | 4.0 | 0.744 | 4.0 | 0.700 |
| 2.5 | 0.474 | 4.5 | 0.740 | 4.5 | 0.672 |
| 2.8 | 0.460 | 5.0 | 0.738 | 5.0 | 0.646 |
| 3.0 | 0.450 | 5.5 | 0.735 | 5.5 | 0.624 |
| 3.5 | 0.429 | 6.0 | 0.734 | 6.0 | 0.607 |
| 3.8 | 0.418 | 6.3 | 0.730 | 6.5 | 0.595 |
| 4.0 | 0.411 | 6.5 | 0.726 | 7.0 | 0.584 |
| 4.5 | 0.396 | 6.6 | 0.720 | 7.5 | 0.580 |
| 5.0 | 0.384 | 6.8 | 0.691 | 8.0 | 0.575 |
| 5.5 | 0.374 | 7.0 | 0.646 | 8.5 | 0.574 |
| 6.0 | 0.365 | 7.2 | 0.616 | 9.0 | 0.572 |
| 6.5 | 0.358 | 7.4 | 0.604 | 9.5 | 0.571 |
| 7.0 | 0.351 | 7.5 | 0.603 | 10.0 | 0.570 |
| 7.5 | 0.346 | 7.6 | 0.607 | 10.5 | 0.570 |
| 8.0 | 0.340 | 7.8 | 0.646 | 10.6 | 0.570 |
| 8.5 | 0.335 | 8.0 | 0.746 | | |
| 9.0 | 0.330 | 8.2 | 0.868 | | |
| 9.5 | 0.326 | 8.4 | 0.915 | | |
| 10.0 | 0.322 | 8.5 | 0.928 | | |
| 10.5 | 0.318 | 8.7 | 0.938 | | |
| 10.6 | 0.317 | 9.0 | 0.934 | | |
| 11.0 | 0.314 | 9.5 | 0.923 | | |
| 11.5 | 0.308 | 10.0 | 0.920 | | |
| 12.0 | 0.304 | 10.5 | 0.924 | | |
| 12.5 | 0.300 | 11.0 | 0.929 | | |
| 13.0 | 0.295 | 11.5 | 0.935 | | |
| 13.5 | 0.292 | 12.0 | 0.939 | | |
| 14.0 | 0.288 | 12.5 | 0.940 | | |
| 14.5 | 0.284 | 13.0 | 0.933 | | |
| 15.0 | 0.280 | 13.5 | 0.919 | | |
| | | 14.0 | 0.903 | | |
| | | 14.5 | 0.894 | | |
| | | 15.0 | 0.864 | | |

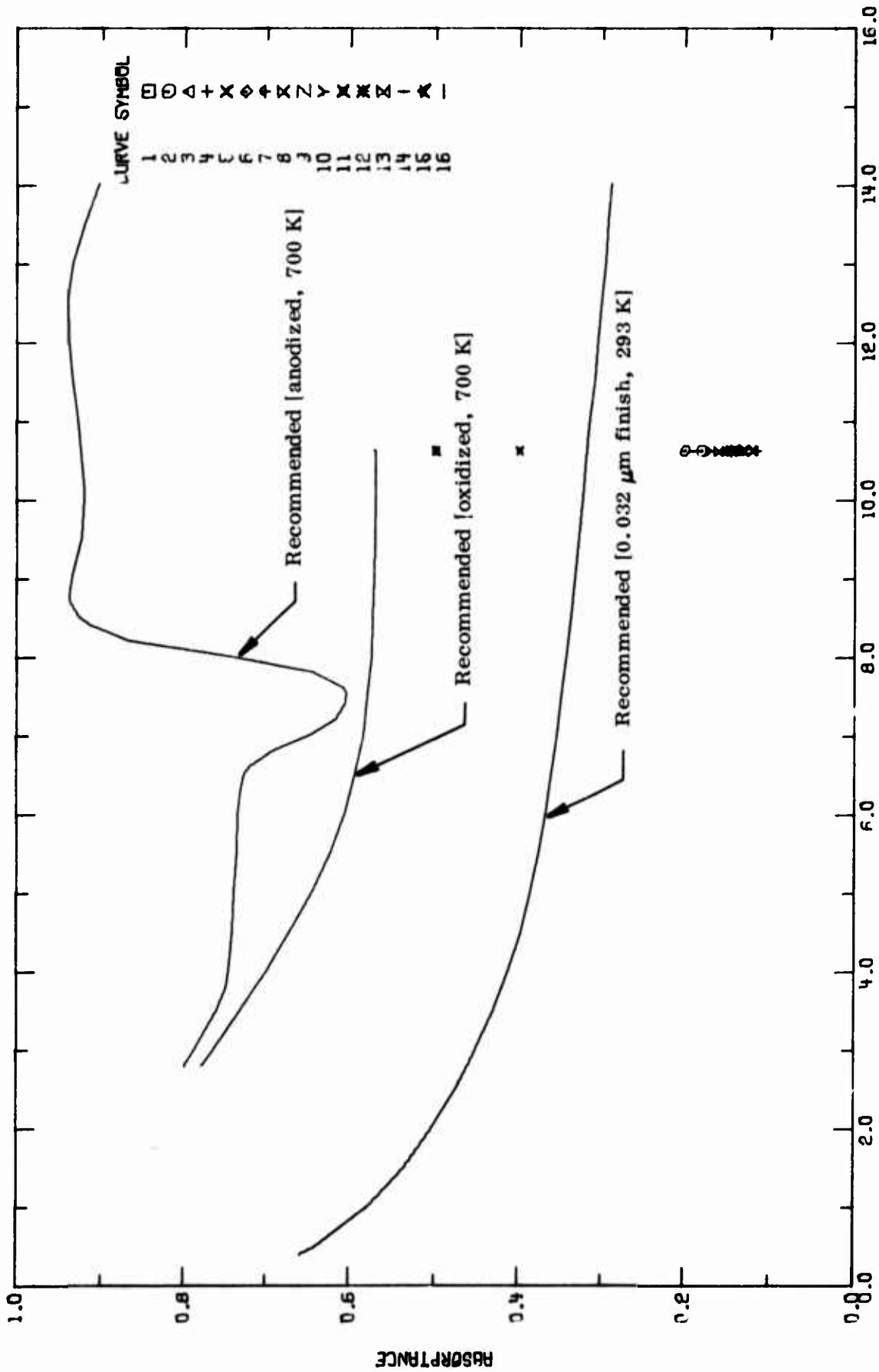


FIGURE 4-10. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

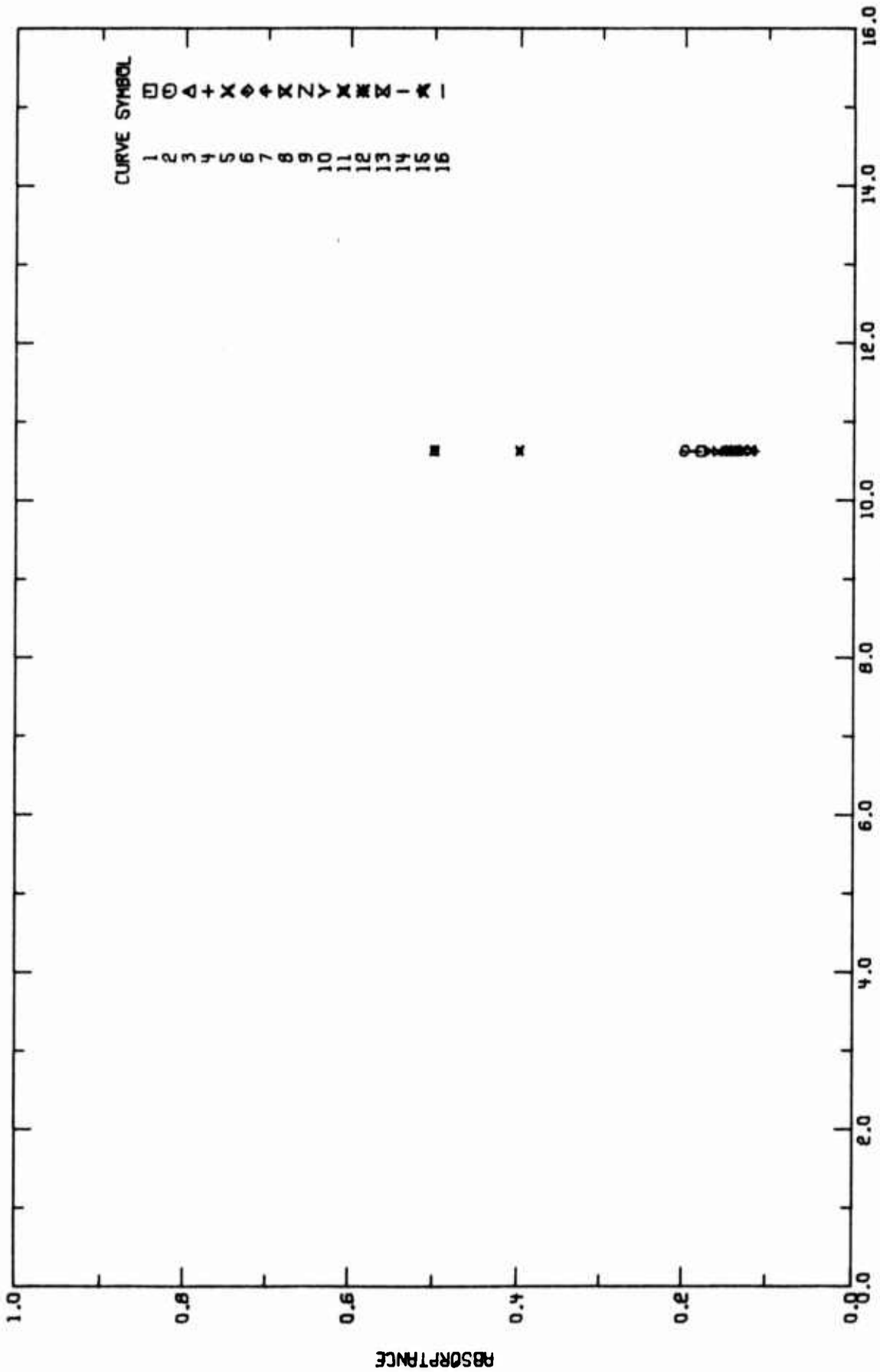


FIGURE 4-11. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

TABLE 4-16. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY Ti-6Al-4V (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney Metals, 4 mil. |
| 2 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except values for this and curves 4, 6, 8, 10, 12, 14, and 16 are calculated from reflectance data. |
| 3 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney Metals, mechanically polished. |
| 4 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen. |
| 5 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Rodney Metals, 10 mil. |
| 6 A00603 | Reichman, J. and Leib, K. | 1973 | 10.5 | 293 | | Similar to the above specimen. |
| 7 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 8 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen. |
| 9 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the specimen from curve 3 except chemically milled. |
| 10 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen. |
| 11 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the specimen from curve 3 except sand blasted. |
| 12 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen. |
| 13 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Specimen from the Timet Corp.; 15 mil. |
| 14 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen. |
| 15 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen except mechanically polished. |
| 16 A00603 | Reichman, J. and Leib, K. | 1973 | 10.6 | 293 | | Similar to the above specimen. |

TABLE 4-17. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY Ti-6Al-4V (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α | λ | α |
|---------------------|----------|----------------------|----------|
| CURVE 1 T = 293. | | CURVE 9 T = 293. | |
| 10.6 | 0.160 | 10.6 | 0.140 |
| CURVE 2 T = 293. | | CURVE 10 T = 293. | |
| 10.6 | 0.200 | 10.6 | 0.170 |
| CURVE 3 T = 293. | | CURVE 11 T = 293. | |
| 10.6 | 0.140 | 10.6 | 0.400 |
| CURVE 4 T = 293. | | CURVE 12 T = 293. | |
| 10.6 | 0.150 | 10.6 | 0.500 |
| CURVE 5 T = 293. | | CURVE 13 T = 293. | |
| 10.6 | 0.120 | 10.6 | 0.160 |
| CURVE 6 T = 293. | | CURVE 14 T = 293. | |
| 10.6 | 0.150 | 10.6 | 0.190 |
| CURVE 7 T = 293. | | CURVE 15 T = 293. | |
| 10.6 | 0.115 | 10.6 | 0.130 |
| CURVE 8 T = 293. | | CURVE 16 T = 293. | |
| 10.6 | 0.145 | 10.6 | 0.145 |

h. Normal Spectral Absorptance (Temperature Dependence)

There is only one set of data located for the temperature dependence (300-800 K) of the normal spectral absorptance of Titanium Alloy Ti-6Al-4V. This is tabulated in Table 4-19 and shown in Figure 4-12. These values were calculated using the Hagen-Rubens relationship. Due to lack of experimental evidence to support these calculations, no recommendations were made.

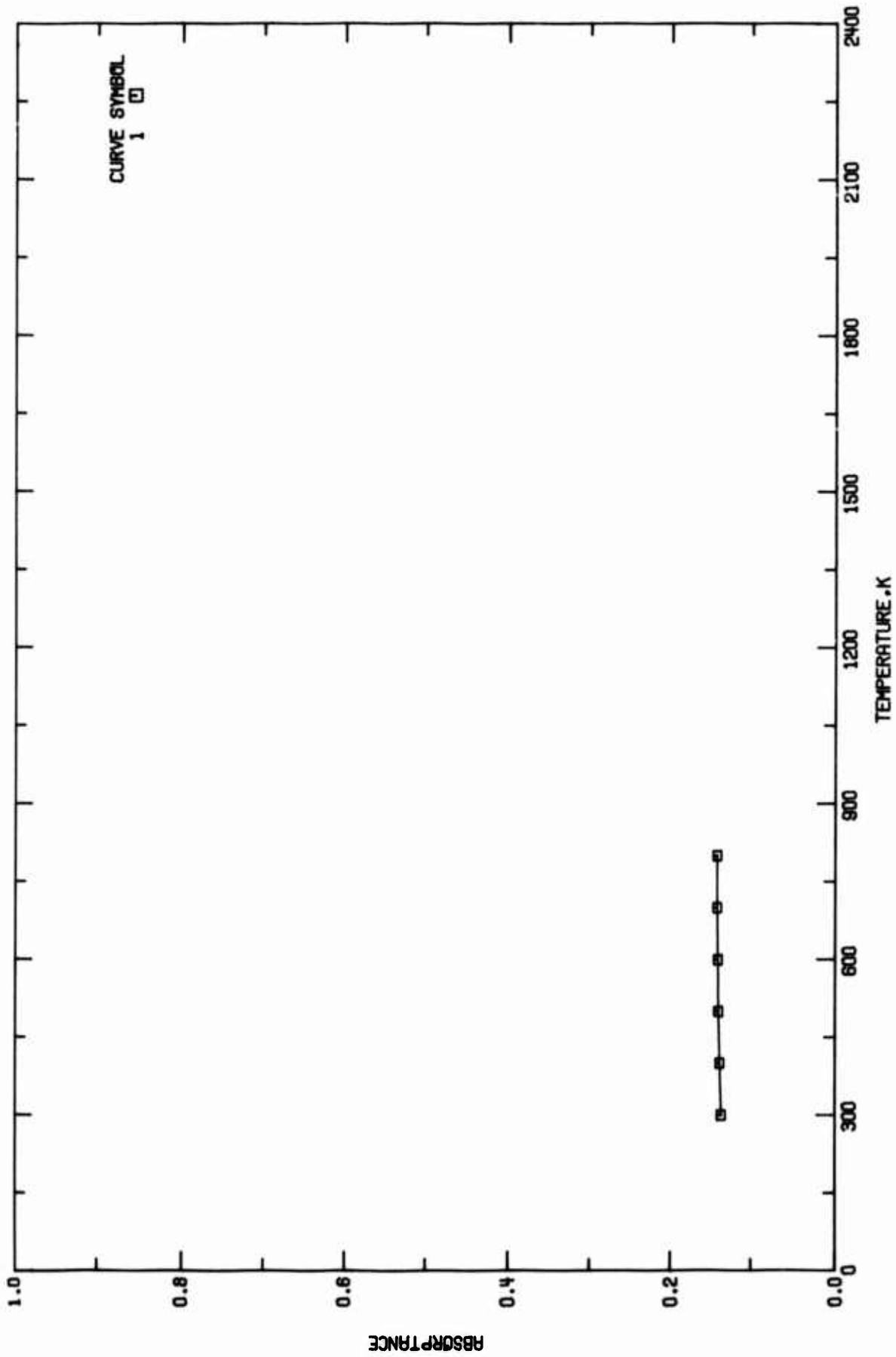


FIGURE 4-12. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE).

TABLE 4-16. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY Ti-6Al-4V (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 E66194 | Cunningham, S.S. and Laughlin, W.T. | 1974 | 10.6 | 300-800 | | Calculated from Hagen-Rubens relation. |

TABLE 4-19. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|------------------|----------|
| CURVE 1 | |
| $\lambda = 13.6$ | |
| 300. | 0.136 |
| 400. | 0.138 |
| 500. | 0.140 |
| 600. | 0.141 |
| 700. | 0.142 |
| 800. | 0.142 |

1. Angular Spectral Absorptance (Wavelength Dependence)

There are no experimental data available for this subproperty. The recommended values tabulated in Table 4-20 and shown in Figure 4-13 calculated from the recommended angular spectral emittance for the identical material are considered accurate to within $\pm 15\%$ at the reported wavelengths (see Section 4.5.c).

TABLE 4-20. RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|-----------|----------|
| PICKLED | |
| ALLOY | |
| T = 293 | |
| 2.8 | 0.42 |
| 3.8 | 0.37 |
| 5.0 | 0.31 |
| 10.6 | 0.22 |

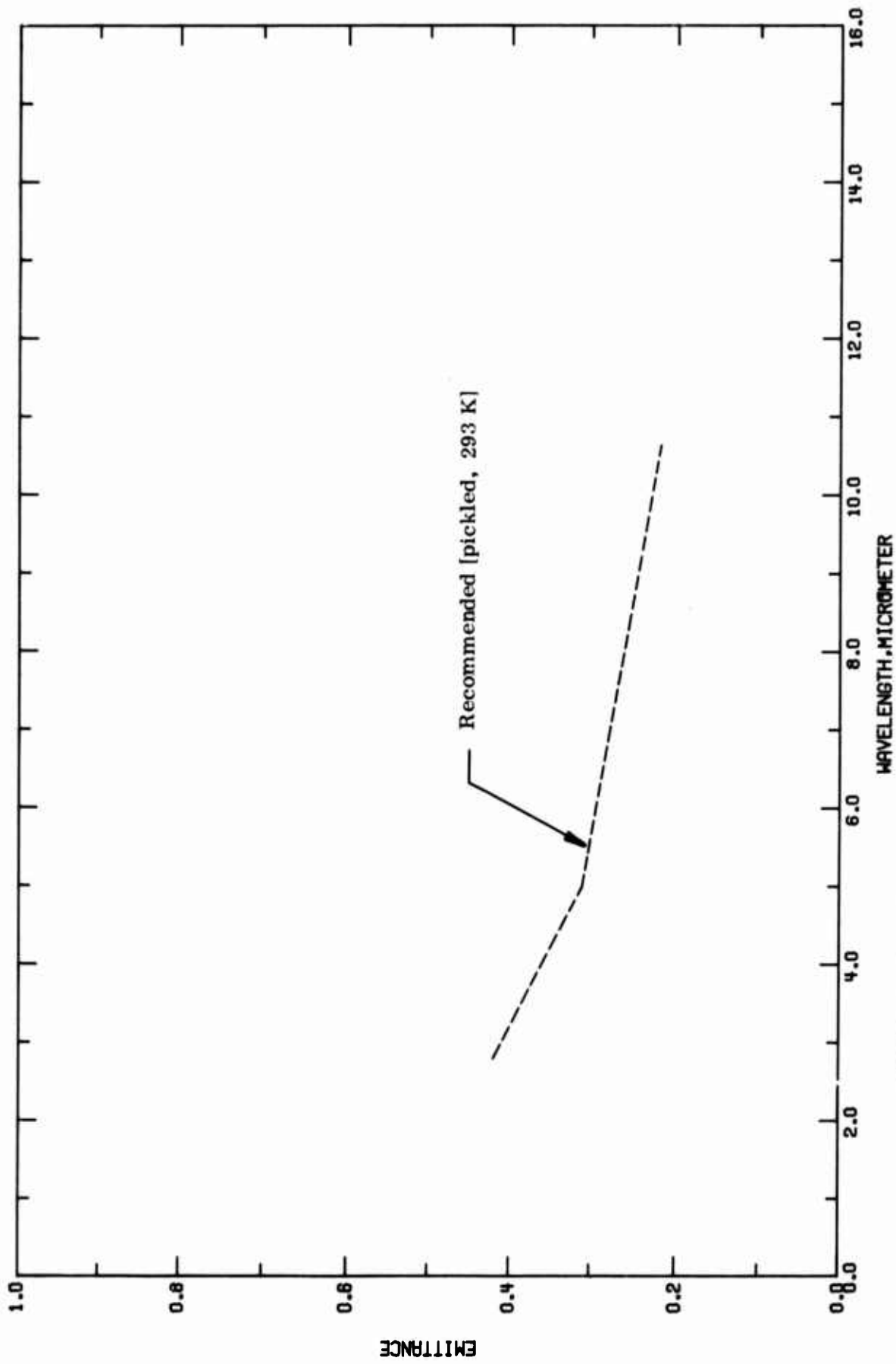


FIGURE 4-13. RECOMMENDED ANGULAR SPECTRAL ABSORPTANCE OF TITANIUM ALLOY TI-6AL-4V (WAVELENGTH DEPENDENCE).

j. Transmittance

Although it is true that metals and alloys in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms.

As an aircraft/spacecraft structural material, this alloy is not used in the form of extremely thin films and therefore is opaque; that is, its transmittance is zero.

4.5. Hadfield Manganese Steel

Hadfield manganese steel is an extremely tough nonmagnetic austenitic alloy. It was named after its inventor Sir Robert Abbott Hadfield (1858-1940), an English metallurgist, who was knighted in 1908 for his discovery of this steel in 1883 and many other metallurgical discoveries and inventions. This steel has a nominal composition of 10-14% Mn, 1.0-1.4% C, 0.1-0.3% Si, 0.1% P, and balance Fe. The melting range of this steel is estimated to be about 1470 to 1480 K. This steel is characterized by its high strength, high ductility, and excellent resistance to wear. In the form of castings or of rolled shapes, it serves many industrial requirements economically and has built up an enviable record as the outstanding material for resisting severe service that combines abrasion and heavy impact.

No information on the thermal radiative properties of this or other similar alloy was uncovered from the search of literature. Consequently, tabulation or recommendation of the thermal radiative properties of this alloy is not possible at this time. However, since a metal with thickness greater than several hundred angstroms is opaque, it can be safely stated that the transmittance of this alloy is zero in its bulk form for general applications.

4.6. Aluminum Oxide

The specific type of aluminum oxide for which evaluated data was requested is Wesgo Al-300 which is a dense, vacuum-tight alumina manufactured by the Western Gold and Platinum Company of Belmont, California [A00015]. Wesgo Al-300 contains 97.6% aluminum oxide and has a density of 3.76 g cm^{-3} which is about 95% of the theoretical value, although the manufacturer claims zero porosity. A 1/16 in. flat specimen of this material is white and translucent. The hardness is 75 (Rockwell 45N). The maximum working temperature is 1923 K while the melting point of pure alumina has been reported around 2315 to 2320 K [A00017]. Wesgo Al-300 is made by compacting at pressures higher than conventionally used. Its properties including high abrasion resistance, high thermal conductivity, and excellent dielectric characteristics lead to its use as R. F. windows, high voltage insulators, and vacuum tube envelopes.

A search of the technical literature did not turn up any data on the thermal radiative or optical properties of Wesgo Al-300. Therefore, with no specific data on Wesgo Al-300, no evaluated values can be given for it. However, to give some indication of the thermal radiative properties of alumina it was decided to give evaluated values, where the quantity and quality of data warrants it, for an alumina which has a purity close to Wesgo Al-300. Coors AD 99 is 99% pure aluminum oxide, while Coors AD 96 is 96% pure aluminum oxide and these specific materials are higher and lower in purity, respectively, than the 97.6% purity of Wesgo Al-300. It should be emphasized that any evaluated data for Coors is not a substitute for actual measurements on Wesgo Al-300 and is only given to give an indication of the behavior of another specific alumina. Because evaluated data was requested for Wesgo Al-300, data was generally not extracted for ruby or sapphire.

a. Normal Spectral Emittance (Wavelength Dependence)

A total of 86 sets of experimental data were located for the wavelength dependence of the normal spectral emittance of aluminum oxide as listed in Table 6-3 and shown in Figures 6-1 through 6-6. Curves 1 through 30 are shown in Figures 6-1 and 6-4. Curves 31 through 60 are shown in Figures 6-2 and 6-5. Curves 61 through 86 are shown in Figures 6-3 and 6-6. Specimen characterization and measurement information for the data are given in Table 8-2.

There is no data specifically for Wesgo Al-300, however, there are data for Coors AD 99 and Coors AD 96 which have a purity higher and lower, respectively, compared to Wesgo Al-300. Folweiler [T29570] (curves 22-26) has measured the normal spectral emittance of Coors AD 96. The data was presented in tabular form and for widely spaced

wavelengths leading to the conclusion that giving evaluated values is not justified. Data for Coors AD 99 was presented by Folweiler [T29570] (curves 17-21), Blau, et al. [T16606] (curves 3, 4, and 7), and Blau and Jasperse [T32045] (curve 62). The data for curves 17-20 was presented in tabular form with the remaining curves for Coors AD 99 given in graphical form. Curve 20 at 1423 K gives supporting evidence to curve 21, also at 1423 K, given in graphical form. These two curves form the basis for provisional values for the normal spectral emittance of Coors AD 99 at 1423 K with the values listed in Table 6-1 and shown in Tables 6-1, 6-2, and 6-3. The provisional curve continues only to 11 μm to keep the uncertainty to a 15% value. Curves 4 and 62 for a temperature of 1303 K are very similar to each other and form the basis of the provisional values for Coors AD 99 at 1303 K with the values listed in Table 6-1 and shown in Tables 6-1, 6-2, and 6-3; the uncertainty for this curve is 15%. Beyond 4.8 μm both provisional curves are the same since the stated uncertainty and the curves forming the basis of the provisional values do not justify separate provisional curves.

TABLE 6-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE(COORS AD 99) (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T = 1303 | | | T = 1303 (CONT.) | | | T = 1423 | | | T = 1423 (CONT.) | | |
|-----------|------------|-----------|------------------|-----------|------------|-----------|------------|-----------|------------------|-----------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 2.0 | 0.432 | 5.9 | 0.926 | 9.8 | 0.983 | 1.0 | 0.226 | 5.0 | 0.798 | 8.9 | 0.985 |
| 2.1 | 0.436 | 6.0 | 0.936 | 9.9 | 0.983 | 1.1 | 0.226 | 5.1 | 0.820 | 9.0 | 0.985 |
| 2.2 | 0.439 | 6.1 | 0.943 | 10.0 | 0.982 | 1.2 | 0.226 | 5.2 | 0.839 | 9.1 | 0.985 |
| 2.3 | 0.443 | 6.2 | 0.950 | 10.1 | 0.980 | 1.3 | 0.227 | 5.3 | 0.857 | 9.2 | 0.985 |
| 2.4 | 0.448 | 6.3 | 0.956 | 10.2 | 0.975 | 1.4 | 0.228 | 5.4 | 0.871 | 9.3 | 0.985 |
| 2.5 | 0.452 | 6.4 | 0.962 | 10.3 | 0.976 | 1.5 | 0.228 | 5.5 | 0.885 | 9.4 | 0.985 |
| 2.6 | 0.457 | 6.5 | 0.966 | 10.4 | 0.974 | 1.6 | 0.229 | 5.6 | 0.897 | 9.5 | 0.984 |
| 2.7 | 0.462 | 6.6 | 0.970 | 10.5 | 0.970 | 1.7 | 0.230 | 5.7 | 0.908 | 9.6 | 0.984 |
| 2.8 | 0.467 | 6.7 | 0.974 | 10.6 | 0.966 | 1.8 | 0.232 | 5.8 | 0.918 | 9.7 | 0.984 |
| 2.9 | 0.472 | 6.8 | 0.976 | 10.7 | 0.962 | 1.9 | 0.233 | 5.9 | 0.926 | 9.8 | 0.983 |
| 3.0 | 0.478 | 6.9 | 0.978 | 10.8 | 0.957 | 2.0 | 0.235 | 6.0 | 0.936 | 9.9 | 0.983 |
| 3.1 | 0.484 | 7.0 | 0.980 | 10.9 | 0.951 | 2.1 | 0.238 | 6.1 | 0.943 | 10.0 | 0.982 |
| 3.2 | 0.490 | 7.1 | 0.981 | 11.0 | 0.943 | 2.3 | 0.241 | 6.2 | 0.950 | 10.1 | 0.980 |
| 3.3 | 0.498 | 7.2 | 0.982 | | | 2.4 | 0.244 | 6.3 | 0.956 | 10.2 | 0.979 |
| 3.4 | 0.505 | 7.3 | 0.983 | | | 2.5 | 0.246 | 6.4 | 0.962 | 10.3 | 0.976 |
| 3.5 | 0.513 | 7.4 | 0.984 | | | 2.6 | 0.250 | 6.5 | 0.966 | 10.4 | 0.974 |
| 3.6 | 0.522 | 7.5 | 0.985 | | | 2.7 | 0.254 | 6.6 | 0.970 | 10.5 | 0.970 |
| 3.7 | 0.532 | 7.6 | 0.985 | | | 2.8 | 0.259 | 6.7 | 0.974 | 10.6 | 0.966 |
| 3.8 | 0.543 | 7.7 | 0.985 | | | 2.9 | 0.265 | 6.8 | 0.976 | 10.7 | 0.962 |
| 3.9 | 0.556 | 7.8 | 0.986 | | | 3.0 | 0.274 | 6.9 | 0.978 | 10.8 | 0.957 |
| 4.0 | 0.570 | 7.9 | 0.986 | | | 3.1 | 0.283 | 7.0 | 0.980 | 10.9 | 0.951 |
| 4.1 | 0.586 | 8.0 | 0.986 | | | 3.2 | 0.294 | 7.1 | 0.981 | 11.0 | 0.943 |
| 4.2 | 0.604 | 8.1 | 0.986 | | | 3.3 | 0.306 | 7.2 | 0.982 | | |
| 4.3 | 0.625 | 8.2 | 0.986 | | | 3.4 | 0.320 | 7.3 | 0.983 | | |
| 4.4 | 0.649 | 8.3 | 0.986 | | | 3.5 | 0.336 | 7.4 | 0.984 | | |
| 4.5 | 0.674 | 8.4 | 0.986 | | | 3.6 | 0.354 | 7.5 | 0.985 | | |
| 4.6 | 0.699 | 8.5 | 0.985 | | | 3.7 | 0.376 | 7.6 | 0.985 | | |
| 4.7 | 0.725 | 8.6 | 0.985 | | | 3.8 | 0.399 | 7.7 | 0.985 | | |
| 4.8 | 0.746 | 8.7 | 0.985 | | | 3.9 | 0.428 | 7.8 | 0.986 | | |
| 4.9 | 0.774 | 8.8 | 0.985 | | | 4.0 | 0.458 | 7.9 | 0.986 | | |
| 5.0 | 0.798 | 8.9 | 0.985 | | | 4.1 | 0.488 | 8.0 | 0.986 | | |
| 5.1 | 0.820 | 9.0 | 0.985 | | | 4.2 | 0.522 | 8.1 | 0.986 | | |
| 5.2 | 0.839 | 9.1 | 0.985 | | | 4.3 | 0.560 | 8.2 | 0.986 | | |
| 5.3 | 0.857 | 9.2 | 0.985 | | | 4.4 | 0.600 | 8.3 | 0.986 | | |
| 5.4 | 0.871 | 9.3 | 0.985 | | | 4.5 | 0.640 | 8.4 | 0.986 | | |
| 5.5 | 0.885 | 9.4 | 0.985 | | | 4.6 | 0.678 | 8.5 | 0.985 | | |
| 5.6 | 0.897 | 9.5 | 0.984 | | | 4.7 | 0.714 | 8.6 | 0.985 | | |
| 5.7 | 0.908 | 9.6 | 0.984 | | | 4.8 | 0.746 | 8.7 | 0.985 | | |
| 5.8 | 0.918 | 9.7 | 0.984 | | | 4.9 | 0.774 | 8.8 | 0.985 | | |

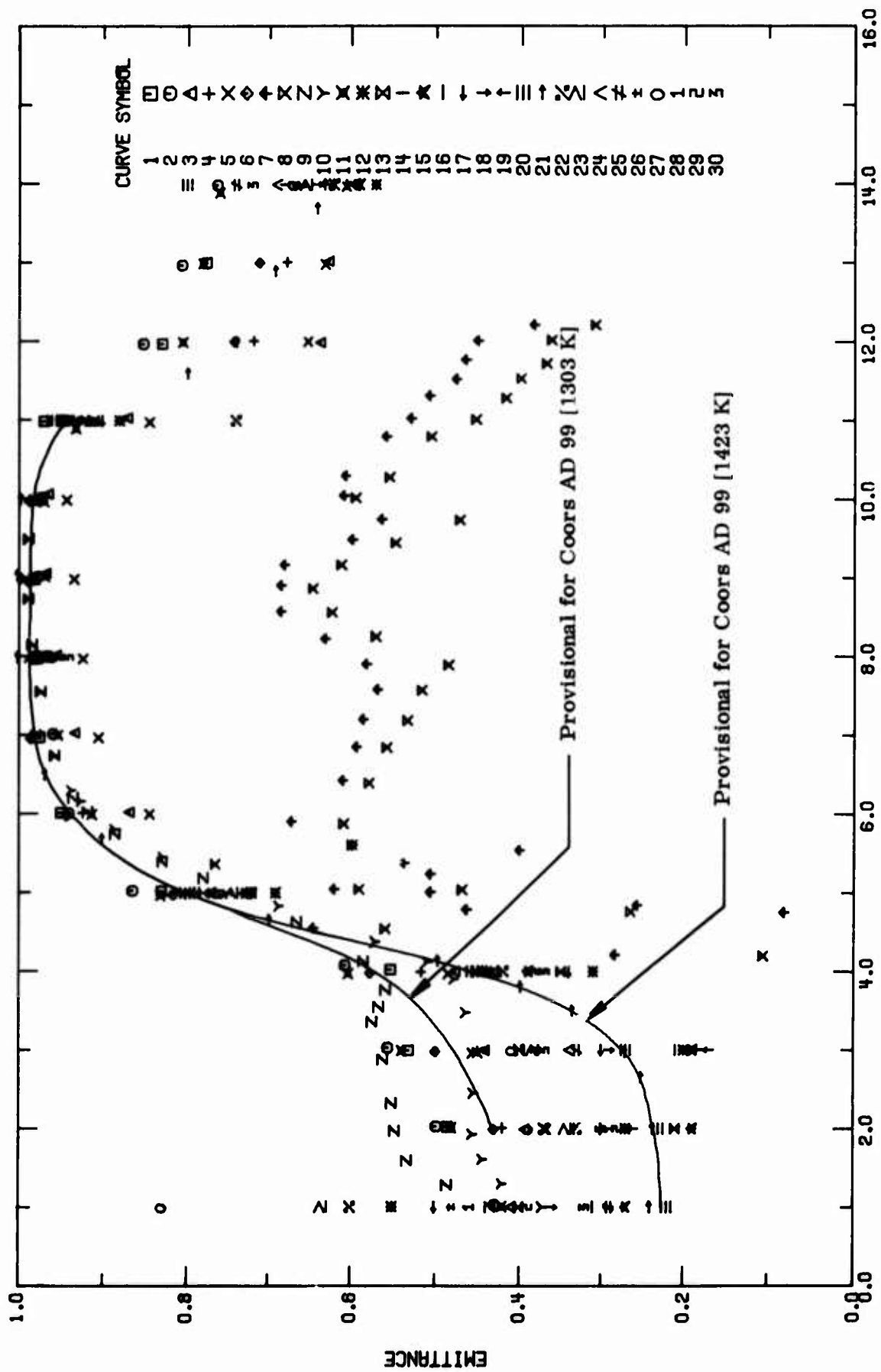


FIGURE 6-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

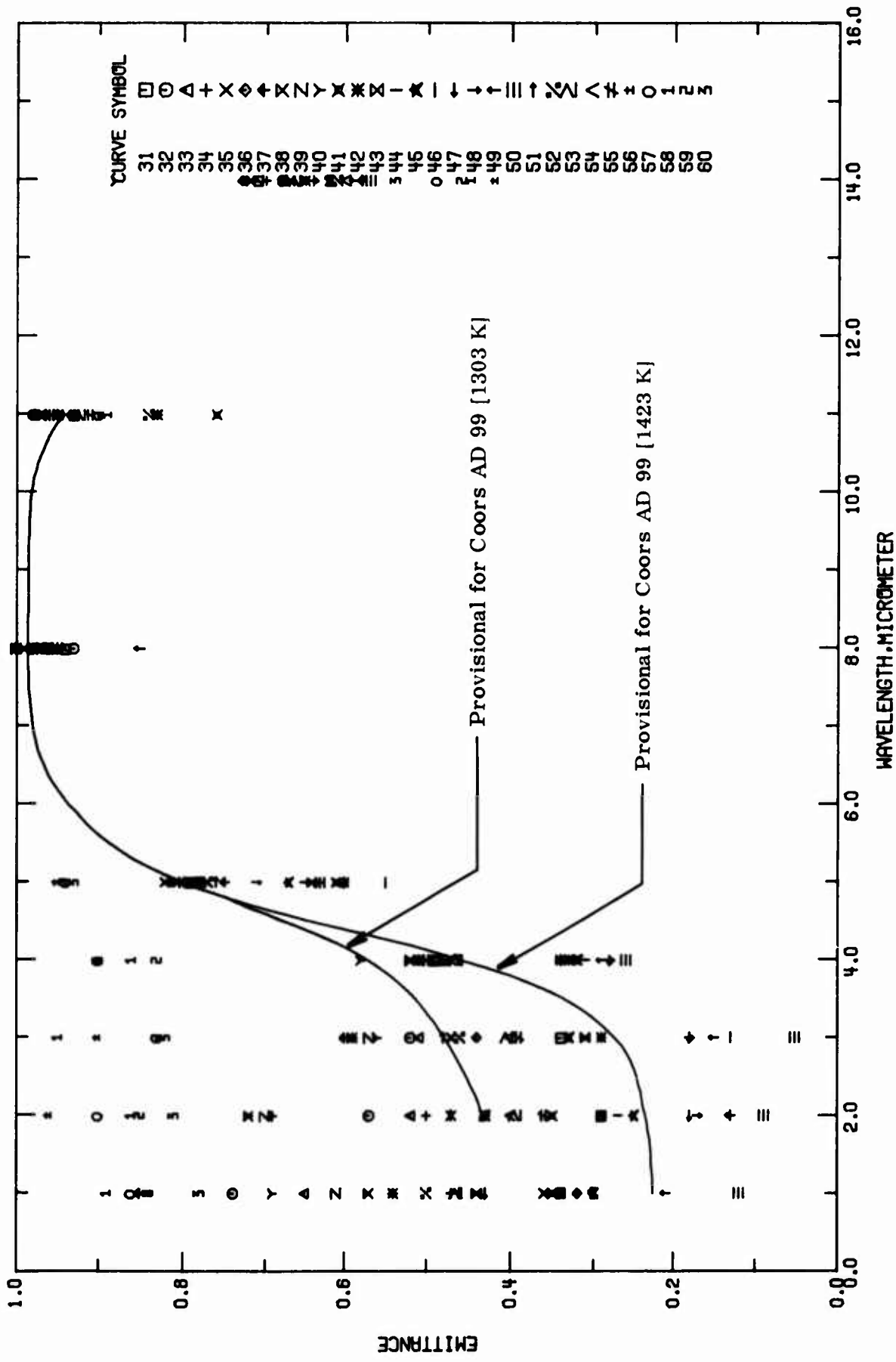


FIGURE 6-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

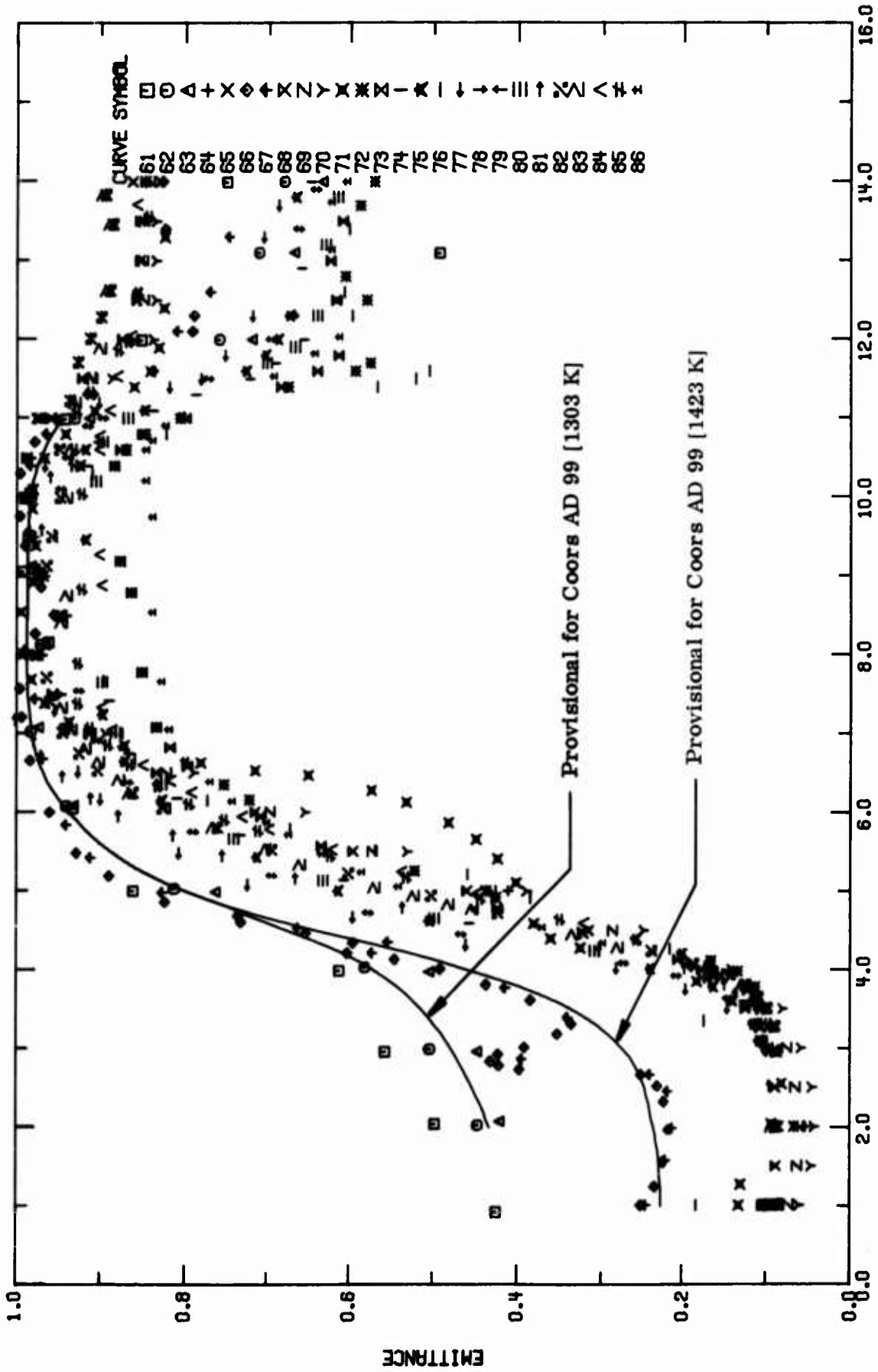


FIGURE 6-3. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

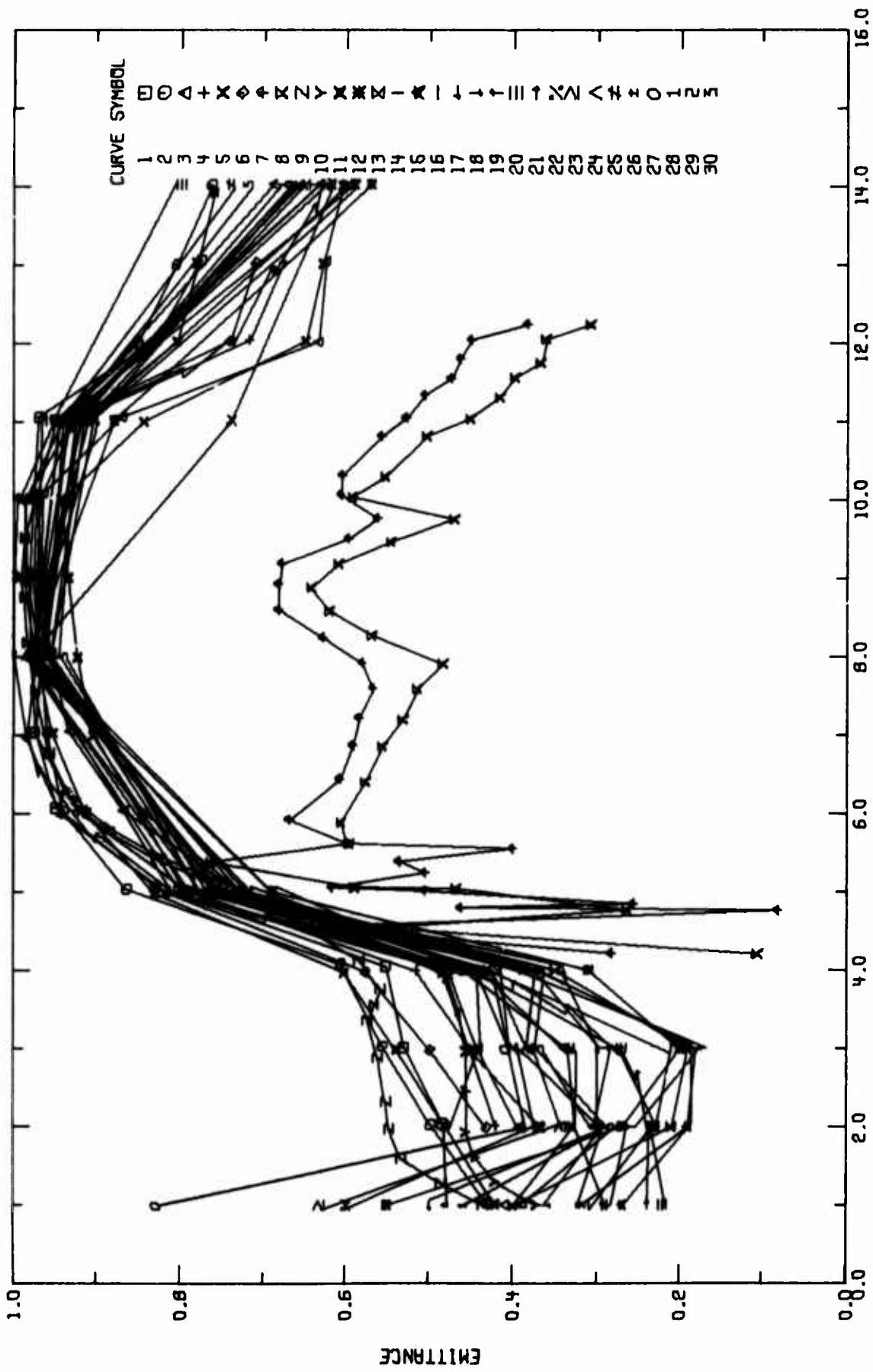


FIGURE 6-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

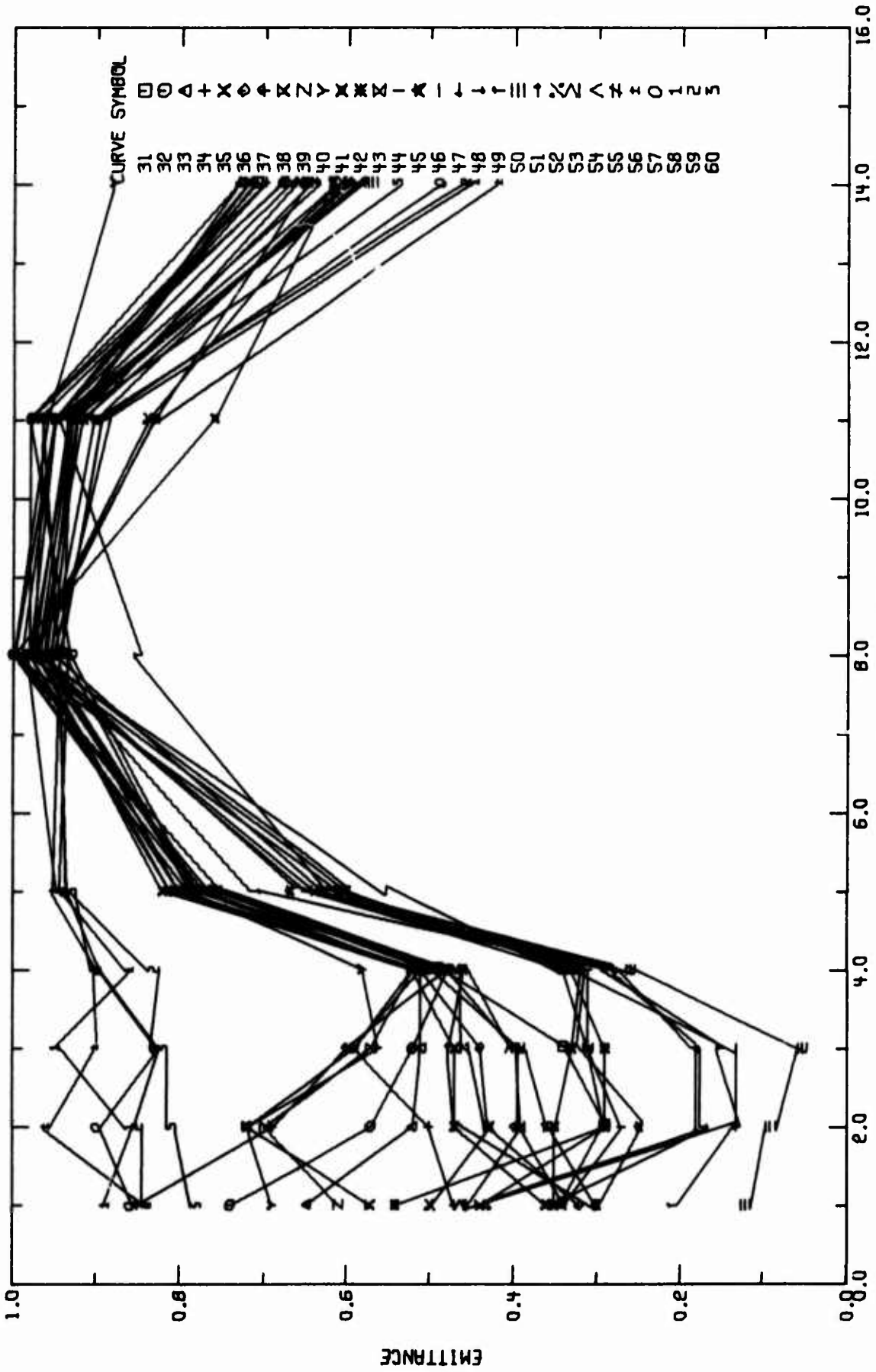


FIGURE 6-5. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

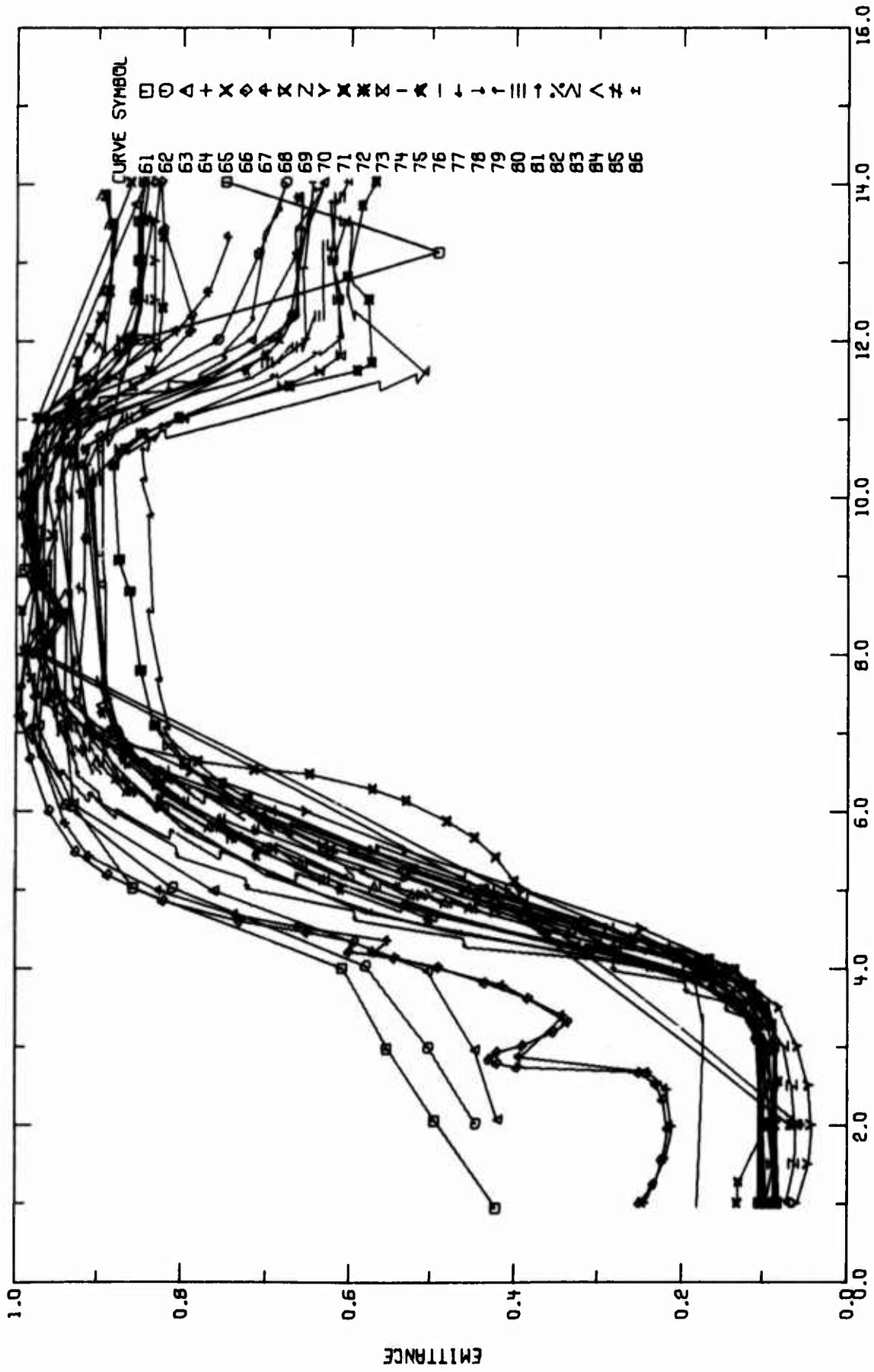


FIGURE 6-6. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

TABLE 6-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T16606 | Blau, H.H., Jr., Marsh, J.B., Martin, W.S., Jasperse, J.R., and Chaffee, E. | 1960 | 2.0-14 | 873 | Coors AD 85 | 95 Al_2O_3 ; measured in air; measurements made with Perkin-Elmer Model 12c infrared spectrometer with sodium chloride prism; data from figure; $\theta' = 0^\circ$; reported error $\pm 4\%$. |
| 2 T16606 | Blau, H.H., Jr., et al. | 1960 | 1.0-14 | 1303 | Coors AD 85 | Similar to the above specimen. |
| 3 T16605 | Blau, H.H., Jr., et al. | 1960 | 2.0-14 | 873 | Coors AD 99 | Similar to the above specimen except 99 Al_2O_3 . |
| 4 T16606 | Blau, H.H., Jr., et al. | 1960 | 2.0-14 | 1303 | Coors AD 99 | Similar to the above specimen. |
| 5 T16606 | Blau, H.H., Jr., et al. | 1960 | 2.0-14 | 873 | Norton TWA No. 2, A402 | Similar to the above specimen except 98.56 Al_2O_3 . |
| 6 T16606 | Blau, H.H., Jr., et al. | 1960 | 2.0-14 | 1323 | Norton TWA No. 2, A402 | Similar to the above specimen. |
| 7 T16606 | Blau, H.H., Jr., et al. | 1960 | 4.2-12 | 560 | Coors AD 99 | 99 Al_2O_3 ; specimen heated in air; solar furnace used to measure spectral reflectance; data not accurate; data from figure; $\theta' = 0^\circ$. |
| 8 T16606 | Blau, H.H., Jr., et al. | 1960 | 4.2-12 | 560 | Norton TWA No. 2, A402 | Similar to the above specimen except 98.56 Al_2O_3 . |
| 9 T25902 | Grenis, A.F. and Levitt, A.P. | 1965 | 1.0-10 | 1300 | | 98.55 Al_2O_3 , 0.58 SiO_2 , 0.31 Na_2O , 0.23 MgO , 0.19 CaO , 0.10 Fe_2O_3 , and 0.04 TiO_2 ; gamma type crystal form; from Norton Refractories; surface roughness 225 $\mu\text{in.}$; flame sprayed coating 12 mills thick on mild steel base; density of coating 3.3 g cm^{-3} ; porosity of coating 8-12%; measured in vacuum of 35 to 50 $\mu\text{ pressure}$; $\theta' = 0^\circ$. |
| 10 T35902 | Grenis, A.F. and Levitt, A.P. | 1965 | 1.0-10 | 1300 | | Similar to the above specimen except surface finished with polishing papers; flame sprayed coating 15 mills thick on mild steel base. |
| 11 T21920 | Stemp, W.S. and Wade, W.A. | 1962 | 1.0-15 | 923 | Norton 5190 alumina | Smooth values from figure; $\theta' \sim 0^\circ$; reported error $\pm 5\%$. |
| 12 T29570 | Folweiler, R.C. | 1964 | 1-14 | 814 | Coors AD 995 alumina | 99.5 Al_2O_3 ; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance determination; $\theta' \sim 0^\circ$; reported error 10%. |
| 13 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1055 | Coors AD 995 alumina | The above specimen. |
| 14 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1227 | Coors AD 995 alumina | The above specimen. |
| 15 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1410 | Coors AD 995 alumina | The above specimen. |
| 16 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1592 | Coors AD 995 alumina | The above specimen. |
| 17 T29570 | Folweiler, R.C. | 1964 | 1-14 | 813 | Coors AD 995 alumina | Similar to the above specimen except 99 Al_2O_3 . |
| 18 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1053 | Coors AD 99 alumina | The above specimen. |

TABLE 6-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence) (continued)

| Cat. No. | Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|----------|----------|-----------------|------|---------------------------------|----------------------|-------------------------------|--|
| 19 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1188 | Coors AD 99 alumina | The above specimen. |
| 20 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1423 | Coors AD 99 alumina | The above specimen. |
| 21 | T29570 | Folweiler, R.C. | 1964 | 1.0-15 | 1423 | Coors AD 99 alumina | Similar to the above specimen except smooth values from figure. |
| 22 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 822 | Coors AD 96 alumina | 96 Al ₂ O ₃ ; $\theta' \sim 0^\circ$; reported error, 10%. |
| 23 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1063 | Coors AD 96 alumina | The above specimen. |
| 24 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1183 | Coors AD 96 alumina | The above specimen. |
| 25 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1401 | Coors AD 96 alumina | The above specimen. |
| 26 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1526 | Coors AD 96 alumina | The above specimen. |
| 27 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 813 | Coors AD 94 alumina | 94 Al ₂ O ₃ ; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance determination; $\theta' \sim 0^\circ$; reported error 10%. |
| 28 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1035 | Coors AD 94 alumina | The above specimen. |
| 29 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1220 | Coors AD 94 alumina | The above specimen. |
| 30 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1413 | Coors AD 94 alumina | The above specimen. |
| 31 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1591 | Coors AD 94 alumina | The above specimen. |
| 32 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 811 | Coors AD 85 alumina | Similar to the above specimen except 85 Al ₂ O ₃ . |
| 33 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1053 | Coors AD 85 alumina | The above specimen. |
| 34 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1208 | Coors AD 85 alumina | The above specimen. |
| 35 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1413 | Coors AD 85 alumina | The above specimen. |
| 36 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 1513 | Coors AD 85 alumina | The above specimen. |
| 37 | T29570 | Folweiler, R.C. | 1964 | 1-14 | 813 | Coors AD 96 alumina | 1% CoCO ₃ ; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance determination; $\theta' \sim 0^\circ$; reported error 10%. |

TABLE 6-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (w'tght percent), Specifications, and Remarks |
|-------------------|-----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 38 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1053 | Coors AD 96 alumina | The above specimen. |
| 39 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1188 | Coors AD 96 alumina | The above specimen. |
| 40 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1423 | Coors AD 96 alumina | The above specimen. |
| 41 T29570 | Folweiler, R.C. | 1964 | 1-14 | 822 | McDaniel AP-35 alumina | 99 Al ₂ O ₃ ; slip cast; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance determinations; $\theta \sim 0^\circ$; reported error 10%. |
| 42 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1063 | McDaniel AP-35 alumina | The above specimen. |
| 43 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1183 | McDaniel AP-35 alumina | The above specimen. |
| 44 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1401 | McDaniel AP-35 alumina | The above specimen. |
| 45 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1523 | McDaniel AP-35 alumina | The above specimen. |
| 46 T29570 | Folweiler, R.C. | 1964 | 1-14 | 833 | McDaniel AP-35 alumina | Similar to the above specimen except isostatically pressed. |
| 47 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1037 | McDaniel AP-35 alumina | The above specimen. |
| 48 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1208 | McDaniel AP-35 alumina | The above specimen. |
| 49 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1395 | McDaniel AP-35 alumina | The above specimen. |
| 50 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1572 | McDaniel AP-35 alumina | The above specimen; value given in document at 2 μm was 0.9, which is probably an error, 0.09 presumed. |
| 51 T29570 | Folweiler, R.C. | 1964 | 1-14 | 814 | McDaniel AV-30 alumina | 96 Al ₂ O ₃ ; vitrified alumina; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance determination; $\theta \sim 0^\circ$; reported error 10%. |
| 52 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1053 | McDaniel AV-30 alumina | The above specimen. |
| 53 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1125 | McDaniel AV-30 alumina | The above specimen. |
| 54 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1408 | McDaniel AV-30 alumina | The above specimen. |
| 55 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1592 | McDaniel AV-50 alumina | The above specimen. |
| 56 T29570 | Folweiler, R.C. | 1964 | 1-14 | 813 | GE Lucalox alumina | Cold-pressed and sintered; MgO added to control grain growth; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance determination; $\theta \sim 0^\circ$; reported error 10%. |

TABLE 6-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 57 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1034 | GE Lucalox alumina | The above specimen. |
| 58 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1220 | GE Lucalox alumina | The above specimen. |
| 59 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1413 | GE Lucalox alumina | The above specimen. |
| 60 T29570 | Folweiler, R.C. | 1964 | 1-14 | 1595 | GE Lucalox alumina | The above specimen. |
| 61 T32045 | Biau, H.H., Jr., and Jasperse, J.R. | 1964 | 0.92-14 | 1303 | Coors AD 85 | 85 Al_2O_3 ; ultrasonically machined; measured in air; $\theta = 0^\circ$; reported error $\pm 4\%$. |
| 62 T32045 | Biau, H.H., Jr., and Jasperse, J.R. | 1964 | 2.0-14 | 1303 | Coors AD 99 | Similar to the above specimen except 99 Al_2O_3 . |
| 63 T32045 | Biau, H.H., Jr., and Jasperse, J.R. | 1964 | 2.1-14 | 1323 | Norton TWA No. 2; A402 | Similar to the above specimen except 98.5 Al_2O_3 . |
| 64 T38726 | Clark, H.E. | 1965 | 2-14 | 1400 | | Rotating specimen method with hollow cylinder of 7.94 mm wall thickness and diameter of 2.5 cm rotated at 100 rpm in front of a water cooled viewing port; separation distance between specimen and viewing port 0.127 mm; $\theta = 0^\circ$. |
| 65 T38726 | Clark, H.E. | 1965 | 2-14 | 1400 | | Similar to the above specimen except separation distance between specimen and viewing port 0.406 mm. |
| 66 T48368 | Richmond, J.C. | 1966 | 1.0-15 | 1073 | AD-5 alumina | Measured at NBS by rotating cylinder method; smooth values from figure; measurement temperature not given explicitly. 1073 K assigned because that figure mentioned in a related context; $\theta = 0^\circ$. |
| 67 T43368 | Richmond, J.C. | 1966 | 1.0-15 | 1073 | AD-5 alumina | The above specimen except grit blasted. |
| 68 T41606 | Clark, H.E. and Moore, D.G. | 1966 | 1.0-15 | 1600 | | >99 pure, 0.40 Fe_2O_3 , 0.10 SiO_2 , 0.07 CaO , and 0.02 Na_2O ; porosity 30 percent by volume; polycrystal; cylinder, 0.1875 in. wall thickness; outer surface smooth but not polished; sintered at 1865 K for 27 hr; average of two readings on each of three specimens; rotating specimen method used; $\theta = 0^\circ$. |
| 69 T41606 | Clark, H.L. and Moore, D.G. | 1966 | 1.0-15 | 1400 | | The above specimen. |
| 70 T41606 | Clark, H.E. and Moore, D.G. | 1966 | 1.0-15 | 1200 | | The above specimen. |
| 71 T50298 | Lewis, B.W., Wade, W.R., Siemp, W.S., and Progar, D.J. | 1966 | 1.0-15 | 1255 | | Al_2O_3 pure slab; 8.13 mm thick; smooth values from figure; $\theta = 0^\circ$. |
| 72 T37398 | Schatz, E.A., Cums, C.R., III, and Burks, T.L. | 1964 | 1.0-15 | 895 | | 99.9 pure powder; from Linde Co.; powder 1 μm particle size; sintered 2 hr at 2023 K; measurement made with help of Baird-Atomic Model NK-1 infrared double beam spectrophotometer; smooth values from figure; $\theta \sim 0^\circ$; reported error $\pm 5\%$. |
| 73 T37398 | Schatz, E.A., et al. | 1964 | 1.0-15 | 993 | | The above specimen. |
| 74 T37398 | Schatz, E.A., et al. | 1964 | 1.0-15 | 1148 | | The above specimen. |
| 75 T37398 | Schatz, E.A., et al. | 1964 | 1.0-15 | 1273 | | The above specimen. |

TABLE 6-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 76 T37398 | Schatz, E. A., Counts, C. R., III, and Burks, T. L. | 1964 | 1.0-15 | 373 | | The above specimen; calculated from spectral reflectance. |
| 77 T35840 | Schatz, E. A., Alvarez, G. H., Counts, C. R., III, and Hoppke, M. A. | 1965 | 1.0-15 | 1273 | | Sintered 1 hr at 1973 K; smooth values from figure; $\theta = 0^\circ$. |
| 78 T35640 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen except heated at 1273 K in measuring apparatus for 1 hr total in order to study emittance as a function of time of heating at 1273 K. |
| 79 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen except heated at 1273 K in measuring apparatus for 2 hr total. |
| 80 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen except heated at 1273 K in measuring apparatus for 4 hr total. |
| 81 T35940 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | Sintering conditions: 15 hr at 1273 K; after each sintering operation density measured by mercury displacement; density 1.58 g cm^{-3} ; $\theta = 0^\circ$. |
| 32 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen with additional 2 hr at 1273 K (to study effect of sintering, specimen removed from apparatus between measurements and heated at increasingly higher temperature) and density 1.60 g cm^{-3} . |
| 83 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen with additional 2 hr at 1473 K and density of 1.65 g cm^{-3} . |
| 84 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen with additional 2 hr at 1573 K and density of 1.71 g cm^{-3} . |
| 85 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen with additional 2 hr at 1673 K and density of 1.77 g cm^{-3} . |
| 86 T35840 | Schatz, E. A., et al. | 1965 | 1.0-15 | 1273 | | The above specimen with additional 2 hr at 1923 K and density of 3.34 g cm^{-3} . |

TABLE 0-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|---------------------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| CURVE 1 T = 873. | | | | | | | | | | | |
| 2.05 | 0.465 | 6.03 | 0.660 | 12.01 | 0.651 | 7.91 | 0.580 | 10.28 | 0.553 | 1.30 | 3.421 |
| 3.00 | 0.531 | 7.04 | 0.932 | 12.99 | 0.630 | 8.23 | 0.629 | 10.80 | 0.504 | 1.61 | 3.444 |
| 4.03 | 0.552 | 8.03 | 0.954 | 13.98 | 0.605 | 8.58 | 0.683 | 11.02 | 0.452 | 1.93 | 0.456 |
| 5.03 | 0.830 | 9.06 | 0.967 | CURVE 6 | | 8.91 | 0.683 | 11.29 | 0.417 | 2.45 | 0.455 |
| 6.03 | 0.349 | 10.07 | 0.964 | T = 1323. | 9.17 | 0.679 | 0.679 | 11.54 | 0.399 | 2.96 | 0.456 |
| 7.99 | 0.974 | 11.04 | 0.871 | 1.99 | 0.431 | 9.49 | 0.597 | 11.73 | 0.368 | 3.48 | 0.464 |
| 8.99 | 0.980 | 12.00 | 0.636 | 2.98 | 0.499 | 9.75 | 0.562 | 12.03 | 0.362 | 3.90 | 0.478 |
| 9.00 | 0.980 | 13.03 | 0.626 | 3.98 | 0.576 | 10.05 | 0.607 | 12.22 | 0.306 | 4.12 | 0.509 |
| 10.01 | 0.975 | 14.04 | 0.581 | 4.98 | 0.816 | 10.30 | 0.605 | CURVE 9 | | 4.33 | 0.570 |
| 11.01 | 0.969 | CURVE 4 | | 5.99 | 0.942 | 10.80 | 0.557 | T = 1300. | 5.46 | 0.535 | 0.535 |
| 11.99 | 0.830 | 2.01 | 0.420 | 6.97 | 0.984 | 11.03 | 0.529 | 1.00 | 0.435 | 5.61 | 0.695 |
| 13.02 | 0.776 | 3.09 | 0.420 | 7.98 | 0.972 | 11.32 | 0.506 | 1.28 | 0.486 | 6.17 | 0.924 |
| 14.04 | 0.724 | 3.99 | 0.420 | 8.95 | 0.986 | 11.73 | 0.464 | 1.59 | 0.533 | 6.31 | 0.936 |
| CURVE 2 | | | | | | | | | | | |
| T = 1303. | | | | | | | | | | | |
| 1.03 | 0.430 | 5.01 | 0.716 | 9.98 | 0.986 | 12.02 | 0.450 | 1.97 | 0.577 | 6.75 | 0.956 |
| 2.03 | 0.498 | 6.02 | 0.922 | 11.01 | 0.940 | 12.22 | 0.383 | 2.32 | 0.551 | 7.56 | 0.973 |
| 3.02 | 0.555 | 7.02 | 0.973 | 12.01 | 0.742 | CURVE 8 | | 2.88 | 0.561 | 8.74 | 0.987 |
| 4.08 | 0.505 | 8.02 | 0.957 | 13.01 | 0.711 | T = 560. | 3.55 | 0.574 | 9.00 | 0.991 | |
| 5.02 | 0.339 | 9.01 | 0.963 | 14.02 | 0.680 | 4.20 | 0.105 | 3.76 | 0.556 | 9.50 | 0.987 |
| 6.01 | 0.969 | 10.00 | 0.985 | 4.54 | 0.558 | 4.13 | 0.584 | 4.13 | 0.584 | 10.00 | 0.975 |
| 7.03 | 0.953 | 10.99 | 0.929 | 4.76 | 0.264 | 4.63 | 0.664 | 4.63 | 0.664 | CURVE 11 | |
| 8.01 | 0.969 | 12.02 | 0.713 | 5.04 | 0.468 | 5.19 | 0.779 | 5.19 | 0.779 | T = 923. | |
| 9.02 | 0.976 | 13.02 | 0.677 | 5.05 | 0.589 | 5.40 | 0.829 | 5.40 | 0.829 | | |
| 10.02 | 0.972 | 14.04 | 0.641 | 5.37 | 0.764 | 5.75 | 0.885 | 5.75 | 0.885 | | |
| 11.00 | 0.949 | CURVE 5 | | 5.61 | 0.597 | 6.03 | 0.917 | 6.03 | 0.917 | | |
| 12.98 | 0.852 | T = 873. | 6.64 | 5.88 | 0.607 | 6.21 | 0.934 | 6.21 | 0.934 | | |
| 14.00 | 0.763 | 1.99 | 0.367 | 6.40 | 0.577 | 6.75 | 0.956 | 6.75 | 0.956 | | |
| CURVE 3 | | | | | | | | | | | |
| T = 873. | | | | | | | | | | | |
| 1.99 | 0.393 | 2.97 | 0.453 | 6.85 | 0.556 | 7.56 | 0.973 | 7.56 | 0.973 | | |
| 3.00 | 0.442 | 3.97 | 0.484 | 7.19 | 0.532 | 8.16 | 0.983 | 8.16 | 0.983 | | |
| 4.00 | 0.477 | 5.00 | 0.720 | 7.58 | 0.515 | 8.74 | 0.937 | 8.74 | 0.937 | | |
| 5.00 | 0.729 | 6.01 | 0.844 | 7.90 | 0.484 | 9.00 | 0.891 | 9.00 | 0.891 | | |
| 6.00 | 0.393 | 6.99 | 0.904 | 8.26 | 0.569 | 9.50 | 0.987 | 9.50 | 0.987 | | |
| 7.00 | 0.442 | 7.98 | 0.922 | 8.57 | 0.621 | 10.00 | 0.975 | 10.00 | 0.975 | | |
| 8.00 | 0.477 | 8.97 | 0.933 | 8.87 | 0.644 | CURVE 10 | | 10.9 | 0.931 | | |
| 9.00 | 0.477 | 9.99 | 0.942 | 9.17 | 0.608 | T = 1300. | 12.0 | 12.0 | 0.805 | | |
| 10.00 | 0.729 | 10.98 | 0.845 | 9.45 | 0.592 | 1.00 | 0.372 | 13.0 | 0.781 | | |
| | | | | 9.74 | 0.584 | 13.9 | | 13.9 | 0.760 | | |
| | | | | 10.02 | 0.567 | 14.9 | | 14.9 | 0.722 | | |

TABLE 6-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------------|------------|-----------|------------|-----------------------|------------|-----------------------|------------|-----------------------|------------|-----------------------|------------|-----------|------------|
| CURVE 12 T = 614. | | | | | | | | | | | | | |
| 1. | 0.55 | 4. | 0.39 | 14. | 0.64 | 7.00 | 0.983 | 1. | 0.41 | 4. | 0.43 | 4. | 0.43 |
| 2. | 0.27 | 5. | 0.77 | CURVE 19 | | 8.00 | 1.000 | 2. | 0.33 | 5. | 0.76 | 5. | 0.76 |
| 3. | 0.20 | 8. | 0.97 | T = 1188. | | 9.03 | 1.000 | 3. | 0.34 | 8. | 0.96 | 8. | 0.96 |
| 4. | 0.31 | 11. | 1.94 | | | 10.0 | 0.995 | 4. | 0.45 | 11. | 0.91 | 11. | 0.91 |
| 5. | 0.69 | 14. | 0.59 | | | 11.0 | 0.948 | 5. | 0.69 | 14. | 0.67 | 14. | 0.67 |
| 6. | 0.98 | CURVE 10 | | 1. | 0.29 | 11.6 | 0.799 | 6. | 0.98 | CURVE 26 T = 1035. | | | |
| 11. | 0.83 | T = 1592. | | 2. | 0.26 | 12.0 | 0.739 | 8. | 0.98 | 1. | 0.46 | 1. | 0.46 |
| 14. | 0.57 | | | 3. | 0.17 | 12.9 | 0.691 | 11. | 0.95 | 2. | 0.29 | 2. | 0.29 |
| CURVE 13 T = 1055. | | | | | | | | | | | | | |
| 1. | 0.40 | 1. | 0.31 | 4. | 0.39 | 13.7 | 0.640 | 14. | 0.69 | 3. | 0.49 | 3. | 0.49 |
| 2. | 0.21 | 2. | 0.23 | 5. | 0.78 | 14.0 | 0.631 | CURVE 25 T = 1401. | | | | | |
| 3. | 0.19 | 3. | 0.21 | 8. | 0.98 | 14.5 | 0.639 | 1. | 0.29 | 1. | 0.35 | 1. | 0.35 |
| 4. | 0.35 | 4. | 0.44 | 11. | 0.94 | 15.0 | 0.662 | 2. | 0.33 | 2. | 0.42 | 2. | 0.42 |
| 5. | 0.72 | 5. | 0.79 | 14. | 0.63 | CURVE 22 T = 822. | | 3. | 0.33 | 3. | 0.33 | 3. | 0.33 |
| 8. | 0.98 | 8. | 0.96 | CURVE 20 T = 1423. | | 1. | 0.60 | 4. | 0.46 | 4. | 0.46 | 4. | 0.46 |
| 11. | 0.91 | 11. | 0.94 | 1. | 0.22 | 2. | 0.37 | 5. | 0.91 | 5. | 0.91 | 5. | 0.91 |
| 14. | 0.60 | 14. | 0.62 | 2. | 0.23 | 3. | 0.40 | 8. | 0.98 | 8. | 0.98 | 8. | 0.98 |
| CURVE 14 T = 1227. | | | | | | | | | | | | | |
| 1. | 0.32 | 1. | 0.50 | 3. | 0.27 | 4. | 0.42 | 11. | 0.95 | 11. | 0.95 | 11. | 0.95 |
| 2. | 0.19 | 2. | 0.30 | 4. | 0.45 | 5. | 0.72 | 14. | 0.74 | 14. | 0.74 | 14. | 0.74 |
| 3. | 0.18 | 3. | 0.30 | 5. | 0.79 | 8. | 0.98 | CURVE 26 T = 1526. | | | | | |
| 4. | 0.37 | 4. | 0.34 | 8. | 0.98 | 11. | 0.74 | 1. | 0.48 | 1. | 0.39 | 1. | 0.39 |
| 5. | 0.75 | 5. | 0.72 | 11. | 0.96 | 14. | 0.62 | 2. | 0.48 | 2. | 0.29 | 2. | 0.29 |
| 8. | 0.97 | 8. | 0.98 | 14. | 0.80 | CURVE 23 T = 1063. | | 3. | 0.44 | 3. | 0.38 | 3. | 0.38 |
| 11. | 0.92 | 11. | 0.90 | CURVE 21 T = 1423. | | 1. | 0.63 | 4. | 0.44 | 4. | 0.44 | 4. | 0.44 |
| 14. | 0.66 | 14. | 0.59 | 1. | 0.240 | 2. | 0.34 | 5. | 0.80 | 5. | 0.80 | 5. | 0.80 |
| CURVE 15 T = 1410. | | | | | | | | | | | | | |
| 1. | 0.27 | 1. | 0.36 | 2. | 0.237 | 3. | 0.38 | 6. | 0.98 | 6. | 0.98 | 6. | 0.98 |
| 2. | 0.19 | 2. | 0.30 | 2.65 | 0.251 | 4. | 0.43 | 11. | 0.93 | 11. | 0.93 | 11. | 0.93 |
| 3. | 0.19 | 3. | 0.29 | 2.97 | 0.271 | 5. | 0.74 | 14. | 0.66 | 14. | 0.66 | 14. | 0.66 |
| 4. | 0.38 | 4. | 0.38 | 3.50 | 0.336 | 8. | 0.98 | CURVE 27 T = 913. | | | | | |
| 5. | 0.77 | 5. | 0.77 | 3.80 | 0.399 | 11. | 0.92 | 1. | 0.83 | 1. | 0.32 | 1. | 0.32 |
| 8. | 0.92 | 8. | 0.96 | 4.13 | 0.497 | 14. | 0.65 | 2. | 0.30 | 2. | 0.30 | 2. | 0.30 |
| 11. | 0.92 | 11. | 0.96 | 4.65 | 0.698 | CURVE 24 T = 1183. | | 3. | 0.37 | 3. | 0.37 | 3. | 0.37 |
| 14. | 0.66 | 14. | 0.54 | 4.99 | 0.801 | 1. | 0.83 | 4. | 0.44 | 4. | 0.44 | 4. | 0.44 |
| CURVE 16 T = 1410. | | | | | | | | | | | | | |
| 1. | 0.27 | 1. | 0.27 | 5.68 | 0.90C | 2. | 0.39 | 5. | 0.77 | 5. | 0.77 | 5. | 0.77 |
| 2. | 0.19 | 2. | 0.19 | 6.51 | 0.968 | 3. | 0.41 | 8. | 0.94 | 8. | 0.94 | 8. | 0.94 |
| 3. | 0.19 | 3. | 0.19 | CURVE 18 T = 1053. | | 11. | 0.93 | 11. | 0.93 | 11. | 0.93 | 11. | 0.93 |

TABLE 6-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|------------------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| CURVE 30 (CONT.) | | | | | | | | | | | |
| T = 1206. | | | | | | | | | | | |
| 14. | 0.72 | | | | | | | | | | |
| CURVE 31 | | | | | | | | | | | |
| T = 1591. | | | | | | | | | | | |
| 1. | 0.34 | | | | | | | | | | |
| 2. | 0.29 | | | | | | | | | | |
| 3. | 0.34 | | | | | | | | | | |
| 4. | 0.49 | | | | | | | | | | |
| 5. | 0.79 | | | | | | | | | | |
| 8. | 0.94 | | | | | | | | | | |
| 11. | 0.93 | | | | | | | | | | |
| 14. | 0.71 | | | | | | | | | | |
| CURVE 32 | | | | | | | | | | | |
| T = 811. | | | | | | | | | | | |
| 1. | 0.74 | | | | | | | | | | |
| 2. | 0.57 | | | | | | | | | | |
| 3. | 0.52 | | | | | | | | | | |
| 4. | 0.48 | | | | | | | | | | |
| 5. | 0.76 | | | | | | | | | | |
| 6. | 0.93 | | | | | | | | | | |
| 11. | 0.38 | | | | | | | | | | |
| 14. | 0.68 | | | | | | | | | | |
| CURVE 33 | | | | | | | | | | | |
| T = 1053. | | | | | | | | | | | |
| 1. | 0.65 | | | | | | | | | | |
| 2. | 0.52 | | | | | | | | | | |
| 3. | 0.51 | | | | | | | | | | |
| 5. | 0.51 | | | | | | | | | | |
| 6. | 0.98 | | | | | | | | | | |
| 11. | 0.98 | | | | | | | | | | |
| 14. | 0.73 | | | | | | | | | | |
| CURVE 34 | | | | | | | | | | | |
| T = 1206. | | | | | | | | | | | |
| 1. | 0.47 | | | | | | | | | | |
| 2. | 0.50 | | | | | | | | | | |
| 3. | 0.59 | | | | | | | | | | |
| 4. | 0.51 | | | | | | | | | | |
| 5. | 0.81 | | | | | | | | | | |
| 8. | 0.98 | | | | | | | | | | |
| 11. | 0.98 | | | | | | | | | | |
| 14. | 0.70 | | | | | | | | | | |
| CURVE 35 | | | | | | | | | | | |
| T = 1413. | | | | | | | | | | | |
| 1. | 0.36 | | | | | | | | | | |
| 2. | 0.47 | | | | | | | | | | |
| 3. | 0.47 | | | | | | | | | | |
| 4. | 0.52 | | | | | | | | | | |
| 5. | 0.62 | | | | | | | | | | |
| 6. | 0.97 | | | | | | | | | | |
| 11. | 0.93 | | | | | | | | | | |
| 14. | 0.72 | | | | | | | | | | |
| CURVE 36 | | | | | | | | | | | |
| T = 1513. | | | | | | | | | | | |
| 1. | 0.32 | | | | | | | | | | |
| 2. | 0.43 | | | | | | | | | | |
| 3. | 0.44 | | | | | | | | | | |
| 4. | 0.51 | | | | | | | | | | |
| 5. | 0.81 | | | | | | | | | | |
| 6. | 0.97 | | | | | | | | | | |
| 11. | 0.93 | | | | | | | | | | |
| 14. | 0.73 | | | | | | | | | | |
| CURVE 37 | | | | | | | | | | | |
| T = 813. | | | | | | | | | | | |
| 1. | 0.65 | | | | | | | | | | |
| 2. | 0.69 | | | | | | | | | | |
| 3. | 0.60 | | | | | | | | | | |
| CURVE 37 (CONT.) | | | | | | | | | | | |
| T = 1206. | | | | | | | | | | | |
| 14. | 0.72 | | | | | | | | | | |
| CURVE 38 | | | | | | | | | | | |
| T = 1053. | | | | | | | | | | | |
| 1. | 0.57 | | | | | | | | | | |
| 2. | 0.72 | | | | | | | | | | |
| 3. | 0.59 | | | | | | | | | | |
| 4. | 0.52 | | | | | | | | | | |
| 5. | 0.77 | | | | | | | | | | |
| 8. | 0.99 | | | | | | | | | | |
| 11. | 0.95 | | | | | | | | | | |
| 14. | 0.72 | | | | | | | | | | |
| CURVE 39 | | | | | | | | | | | |
| T = 1188. | | | | | | | | | | | |
| 1. | 0.61 | | | | | | | | | | |
| 2. | 0.70 | | | | | | | | | | |
| 3. | 0.57 | | | | | | | | | | |
| 4. | 0.52 | | | | | | | | | | |
| 5. | 0.78 | | | | | | | | | | |
| 8. | 1.00 | | | | | | | | | | |
| 11. | 0.95 | | | | | | | | | | |
| 14. | 0.71 | | | | | | | | | | |
| CURVE 40 | | | | | | | | | | | |
| T = 1423. | | | | | | | | | | | |
| 1. | 0.69 | | | | | | | | | | |
| 2. | 0.72 | | | | | | | | | | |
| 3. | 0.56 | | | | | | | | | | |
| 4. | 0.58 | | | | | | | | | | |
| 5. | 0.79 | | | | | | | | | | |
| 8. | 1.00 | | | | | | | | | | |
| 11. | 0.96 | | | | | | | | | | |
| CURVE 40 (CONT.) | | | | | | | | | | | |
| T = 1401. | | | | | | | | | | | |
| 14. | 0.88 | | | | | | | | | | |
| CURVE 41 | | | | | | | | | | | |
| T = 822. | | | | | | | | | | | |
| 1. | 0.35 | | | | | | | | | | |
| 2. | 0.35 | | | | | | | | | | |
| 3. | 0.33 | | | | | | | | | | |
| 4. | 0.32 | | | | | | | | | | |
| 5. | 0.61 | | | | | | | | | | |
| 8. | 1.00 | | | | | | | | | | |
| 11. | 0.76 | | | | | | | | | | |
| 14. | 0.62 | | | | | | | | | | |
| CURVE 42 | | | | | | | | | | | |
| T = 1063. | | | | | | | | | | | |
| 1. | 0.54 | | | | | | | | | | |
| 2. | 0.29 | | | | | | | | | | |
| 3. | 0.29 | | | | | | | | | | |
| 4. | 0.33 | | | | | | | | | | |
| 5. | 0.60 | | | | | | | | | | |
| 8. | 0.98 | | | | | | | | | | |
| 11. | 0.83 | | | | | | | | | | |
| 14. | 0.65 | | | | | | | | | | |
| CURVE 43 | | | | | | | | | | | |
| T = 1183. | | | | | | | | | | | |
| 1. | 0.44 | | | | | | | | | | |
| 2. | 0.29 | | | | | | | | | | |
| 3. | 0.31 | | | | | | | | | | |
| 4. | 0.34 | | | | | | | | | | |
| 5. | 0.55 | | | | | | | | | | |
| 8. | 0.98 | | | | | | | | | | |
| 11. | 0.93 | | | | | | | | | | |
| 14. | 0.64 | | | | | | | | | | |
| CURVE 44 | | | | | | | | | | | |
| T = 1401. | | | | | | | | | | | |
| 1. | 0.34 | | | | | | | | | | |
| 2. | 0.27 | | | | | | | | | | |
| 3. | 0.31 | | | | | | | | | | |
| 4. | 0.31 | | | | | | | | | | |
| 5. | 0.65 | | | | | | | | | | |
| 8. | 0.96 | | | | | | | | | | |
| 11. | 0.95 | | | | | | | | | | |
| 14. | 0.70 | | | | | | | | | | |
| CURVE 45 | | | | | | | | | | | |
| T = 1523. | | | | | | | | | | | |
| 1. | 0.30 | | | | | | | | | | |
| 2. | 0.25 | | | | | | | | | | |
| 3. | 0.33 | | | | | | | | | | |
| 4. | 0.32 | | | | | | | | | | |
| 5. | 0.67 | | | | | | | | | | |
| 8. | 0.98 | | | | | | | | | | |
| 11. | 0.97 | | | | | | | | | | |
| 14. | 0.68 | | | | | | | | | | |
| CURVE 46 | | | | | | | | | | | |
| T = 833. | | | | | | | | | | | |
| 1. | 0.46 | | | | | | | | | | |
| 2. | 0.13 | | | | | | | | | | |
| 3. | 0.13 | | | | | | | | | | |
| 4. | 0.34 | | | | | | | | | | |
| 5. | 0.55 | | | | | | | | | | |
| 8. | 0.98 | | | | | | | | | | |
| 11. | 0.93 | | | | | | | | | | |
| 14. | 0.64 | | | | | | | | | | |
| CURVE 47 | | | | | | | | | | | |
| T = 1037. | | | | | | | | | | | |
| 1. | 0.43 | | | | | | | | | | |
| 2. | 0.18 | | | | | | | | | | |
| 3. | 0.18 | | | | | | | | | | |
| CURVE 47 (CONT.) | | | | | | | | | | | |
| T = 1208. | | | | | | | | | | | |
| 4. | 0.28 | | | | | | | | | | |
| 5. | 0.65 | | | | | | | | | | |
| 8. | 0.96 | | | | | | | | | | |
| 11. | 0.93 | | | | | | | | | | |
| 14. | 0.62 | | | | | | | | | | |
| CURVE 48 | | | | | | | | | | | |
| T = 1208. | | | | | | | | | | | |
| 1. | 0.35 | | | | | | | | | | |
| 2. | 0.17 | | | | | | | | | | |
| 3. | 0.18 | | | | | | | | | | |
| 4. | 0.28 | | | | | | | | | | |
| 5. | 0.71 | | | | | | | | | | |
| 8. | 0.97 | | | | | | | | | | |
| 11. | 0.94 | | | | | | | | | | |
| 14. | 0.64 | | | | | | | | | | |
| CURVE 49 | | | | | | | | | | | |
| T = 1395. | | | | | | | | | | | |
| 1. | 0.21 | | | | | | | | | | |
| 2. | 0.13 | | | | | | | | | | |
| 3. | 0.15 | | | | | | | | | | |
| 4. | 0.29 | | | | | | | | | | |
| 5. | 0.63 | | | | | | | | | | |
| 8. | 0.85 | | | | | | | | | | |
| 11. | 0.94 | | | | | | | | | | |
| 14. | 0.59 | | | | | | | | | | |
| CURVE 50 | | | | | | | | | | | |
| T = 1572. | | | | | | | | | | | |
| 1. | 0.12 | | | | | | | | | | |
| 2. | 0.09 | | | | | | | | | | |
| 3. | 0.052 | | | | | | | | | | |
| 4. | 0.26 | | | | | | | | | | |
| 5. | 0.63 | | | | | | | | | | |
| 8. | 0.95 | | | | | | | | | | |
| 11. | 0.96 | | | | | | | | | | |

TABLE 6-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------------|------------|-----------|------------|-----------------------|------------|-----------------------|------------|-----------------------|------------|
| CURVE 50 (CONT.) | | | | | | | | | |
| CURVE 54 T = 1468. | | | | | | | | | |
| 14. | 0.57 | 1. | 0.34 | 4. | 0.90 | 14. | 0.54 | 2.07 | 0.420 |
| CURVE 51 T = 814. | | | | | | | | | |
| 1. | 0.30 | 2. | 0.43 | 5. | 0.94 | CURVE 61 T = 1303. | | | |
| 2. | 0.47 | 3. | 0.40 | 8. | 0.95 | 0.92 | 3.424 | 2.92 | 0.372 |
| 3. | 0.48 | 4. | 0.49 | 11. | 0.90 | 2.04 | 0.497 | 7.68 | 0.964 |
| 4. | 0.46 | 5. | 0.78 | 17. | 0.49 | 3.96 | 0.556 | 8.13 | 0.981 |
| 5. | 0.70 | 6. | 0.97 | CURVE 56 T = 1220. | | | | 9.13 | 0.981 |
| 8. | 1.00 | 11. | 0.93 | 1. | 0.89 | 5.01 | 0.859 | 10.1 | 0.983 |
| 11. | 0.95 | 14. | 0.60 | 2. | 0.85 | 6.06 | 0.931 | 11.0 | 0.912 |
| CURVE 55 T = 1592. | | | | | | | | | |
| 1. | 0.58 | 1. | 0.30 | 3. | 0.95 | 7.07 | 0.941 | 12.0 | 0.720 |
| CURVE 52 T = 1053. | | | | | | | | | |
| 1. | 0.50 | 2. | 0.36 | 4. | 0.66 | 8.17 | 0.960 | 13.1 | 0.667 |
| 2. | 0.43 | 3. | 0.39 | 5. | 0.95 | 9.07 | 0.991 | 14.0 | 0.633 |
| 3. | 0.46 | 4. | 0.50 | 8. | 0.95 | 10.0 | 0.988 | CURVE 64 T = 1400. | |
| 5. | 0.77 | 5. | 0.60 | 11. | 0.89 | 11.0 | 0.941 | 2. | 0.053 |
| 8. | 0.98 | 6. | 0.96 | 14. | 0.45 | 12.0 | 0.850 | 5. | 0.410 |
| 11. | 0.94 | 11. | 0.91 | CURVE 59 T = 1413. | | | | 13.1 | 0.964 |
| 14. | 0.51 | 14. | 0.62 | 1. | 0.84 | 14.0 | 0.753 | 14. | 0.845 |
| CURVE 53 T = 1125. | | | | | | | | | |
| 1. | 0.46 | 1. | 0.34 | 2. | 0.85 | CURVE 62 T = 1303. | | | |
| 2. | 0.39 | 2. | 0.56 | 3. | 0.83 | 1.92 | 0.446 | CURVE 65 T = 1400. | |
| 3. | 0.40 | 3. | 0.93 | 4. | 0.94 | 2.99 | 0.503 | 2. | 0.066 |
| 4. | 0.46 | 4. | 0.90 | 5. | 0.94 | 4.03 | 0.581 | 5. | 0.436 |
| 5. | 0.76 | 5. | 0.95 | 8. | 0.90 | 5.03 | 0.811 | 8. | 0.976 |
| 8. | 0.97 | 8. | 0.98 | 11. | 0.46 | 6.38 | 0.939 | 11. | 0.975 |
| 11. | 0.92 | 11. | 0.83 | 14. | 0.42 | 7.03 | 0.991 | 14. | 0.861 |
| 17. | 0.66 | 14. | 0.42 | CURVE 60 T = 1595. | | | | 8.13 | 0.969 |
| CURVE 57 T = 1037. | | | | | | | | | |
| 1. | 0.57 | 1. | 0.78 | 1. | 0.78 | 10.0 | 0.981 | CURVE 66 T = 1073. | |
| 2. | 0.47 | 2. | 0.81 | 2. | 0.81 | 11.0 | 0.929 | 10.7 | 0.977 |
| 3. | 0.48 | 3. | 0.82 | 3. | 0.82 | 12.0 | 0.759 | 11.0 | 0.953 |
| 4. | 0.76 | 4. | 0.90 | 4. | 0.90 | 13.1 | 0.711 | 11.3 | 0.907 |
| 5. | 0.97 | 5. | 0.93 | 5. | 0.93 | 14.0 | 0.679 | 11.6 | 0.837 |
| 8. | 0.92 | 8. | 0.90 | 8. | 0.90 | CURVE 63 T = 1323. | | | |
| 11. | 0.66 | 11. | 0.66 | 11. | 0.95 | 14. | 0.845 | 12.1 | 0.791 |
| 17. | 0.66 | 17. | 0.66 | 14. | 0.93 | CURVE 64 T = 1400. | | | |
| CURVE 58 T = 1125. | | | | | | | | | |
| 1. | 0.57 | 1. | 0.66 | 1. | 0.66 | 2. | 0.066 | 12.3 | 0.789 |
| 2. | 0.47 | 2. | 0.81 | 2. | 0.81 | 5. | 0.436 | 13.4 | 0.822 |
| 3. | 0.48 | 3. | 0.82 | 3. | 0.82 | 8. | 0.976 | 14.0 | 0.825 |
| 4. | 0.76 | 4. | 0.90 | 4. | 0.90 | 11. | 0.975 | | |
| 5. | 0.97 | 5. | 0.93 | 5. | 0.93 | 14. | 0.861 | | |
| 8. | 0.92 | 8. | 0.90 | 8. | 0.90 | CURVE 65 T = 1400. | | | |
| 11. | 0.66 | 11. | 0.66 | 11. | 0.95 | 2. | 0.066 | 7.57 | 0.934 |
| 17. | 0.66 | 17. | 0.66 | 14. | 0.93 | 5. | 0.436 | 8.02 | 0.988 |
| CURVE 59 T = 1125. | | | | | | | | | |
| 1. | 0.57 | 1. | 0.78 | 1. | 0.78 | 8.27 | 0.976 | 8.51 | 0.954 |
| 2. | 0.47 | 2. | 0.81 | 2. | 0.81 | 8.86 | 0.822 | 8.86 | 0.869 |
| 3. | 0.48 | 3. | 0.82 | 3. | 0.82 | 9.38 | 0.532 | 9.38 | 0.588 |
| 4. | 0.76 | 4. | 0.90 | 4. | 0.90 | 9.76 | 0.934 | 9.76 | 0.934 |
| 5. | 0.97 | 5. | 0.93 | 5. | 0.93 | 10.3 | 0.977 | 10.3 | 0.977 |
| 8. | 0.92 | 8. | 0.90 | 8. | 0.90 | 10.7 | 0.953 | 10.7 | 0.953 |
| 11. | 0.66 | 11. | 0.66 | 11. | 0.95 | 11.0 | 0.953 | 11.0 | 0.953 |
| 17. | 0.66 | 17. | 0.66 | 14. | 0.93 | 11.3 | 0.907 | 11.3 | 0.907 |
| CURVE 60 T = 1125. | | | | | | | | | |
| 1. | 0.57 | 1. | 0.78 | 1. | 0.78 | 11.6 | 0.837 | 11.6 | 0.837 |
| 2. | 0.47 | 2. | 0.81 | 2. | 0.81 | 12.1 | 0.791 | 12.1 | 0.791 |
| 3. | 0.48 | 3. | 0.82 | 3. | 0.82 | 12.3 | 0.789 | 12.3 | 0.789 |
| 4. | 0.76 | 4. | 0.90 | 4. | 0.90 | 13.4 | 0.822 | 13.4 | 0.822 |
| 5. | 0.97 | 5. | 0.93 | 5. | 0.93 | 14.0 | 0.825 | 14.0 | 0.825 |
| 8. | 0.92 | 8. | 0.90 | 8. | 0.90 | CURVE 66 T = 1073. | | | |
| 11. | 0.66 | 11. | 0.66 | 11. | 0.95 | 1.00 | 0.251 | 1.00 | 0.251 |
| 17. | 0.66 | 17. | 0.66 | 14. | 0.93 | 1.24 | 0.234 | 1.24 | 0.234 |
| CURVE 61 T = 1303. | | | | | | | | | |
| 1. | 0.30 | 1. | 0.30 | 1. | 0.30 | 1.55 | 0.224 | 1.55 | 0.224 |
| 2. | 0.47 | 2. | 0.47 | 2. | 0.47 | 1.96 | 0.217 | 1.96 | 0.217 |
| 3. | 0.48 | 3. | 0.48 | 3. | 0.48 | CURVE 67 T = 1303. | | | |
| 4. | 0.46 | 4. | 0.46 | 4. | 0.46 | | | | |
| 5. | 0.70 | 5. | 0.70 | 5. | 0.70 | | | | |
| 8. | 1.00 | 8. | 1.00 | 8. | 1.00 | | | | |
| 11. | 0.95 | 11. | 0.95 | 11. | 0.95 | | | | |
| 14. | 0.58 | 14. | 0.58 | 14. | 0.58 | | | | |

TABLE 6-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | | |
|-----------------------|------------|-----------|------------|-----------------------|------------|-----------------------|------------|-----------|------------|----------------------|------------|------|-------|
| CURVE 66 (CONT.) | | | | | | | | | | | | | |
| 15.0 | 0.791 | | | | | | | | | | | | |
| CURVE 67 T = 1073. | | | | | | | | | | | | | |
| 1.00 | 0.245 | 1.0 | 0.097 | 7.5 | 0.169 | 7.5 | 0.945 | 7.15 | 0.936 | 11.4 | 0.674 | | |
| 1.57 | 0.221 | 1.5 | 0.086 | 4.5 | 0.237 | 8.0 | 0.968 | 7.39 | 0.965 | 11.6 | 0.593 | | |
| 1.96 | 0.212 | 2.0 | 0.085 | 5.0 | 0.431 | 8.5 | 0.939 | 7.69 | 0.951 | 11.7 | 0.575 | | |
| 2.45 | 0.213 | 2.5 | 0.089 | 5.0 | 0.572 | 9.0 | 0.965 | 8.52 | 0.990 | 12.5 | 0.579 | | |
| 2.86 | 0.394 | 3.0 | 0.097 | 6.5 | 0.695 | 9.5 | 0.978 | 8.55 | 0.993 | 12.8 | 0.605 | | |
| 3.39 | 0.341 | 3.5 | 0.125 | 7.0 | 0.821 | 10.0 | 0.984 | 8.93 | 0.978 | 13.7 | 0.587 | | |
| 3.77 | 0.414 | 4.0 | 0.177 | 7.5 | 0.910 | 10.5 | 0.982 | 9.39 | 0.976 | 14.0 | 0.570 | | |
| 4.30 | 0.491 | 4.5 | 0.316 | 8.0 | 0.956 | 11.0 | 0.958 | 9.86 | 0.980 | 14.6 | 0.561 | | |
| 4.81 | 0.572 | 5.0 | 0.459 | 8.5 | 0.975 | 11.5 | 0.885 | 10.1 | 0.979 | 15.0 | 0.551 | | |
| 5.33 | 0.553 | 5.5 | 0.595 | 9.0 | 0.947 | 12.0 | 0.836 | 10.5 | 0.966 | CURVE 73 T = 993. | | | |
| 5.88 | 0.652 | 6.0 | 0.715 | 9.5 | 0.973 | 12.5 | 0.833 | 10.8 | 0.941 | 1.00 | 0.104 | | |
| 6.42 | 0.725 | 6.5 | 0.832 | 10.0 | 0.989 | 13.0 | 0.833 | 11.1 | 0.906 | 3.09 | 0.104 | | |
| 6.97 | 0.825 | 7.0 | 0.912 | 10.5 | 0.987 | 13.5 | 0.828 | 11.4 | 0.859 | 3.53 | 0.112 | | |
| 7.54 | 0.910 | 7.5 | 0.955 | 11.0 | 0.972 | 14.0 | 0.814 | 11.6 | 0.840 | 3.74 | 0.122 | | |
| 8.12 | 0.939 | 8.0 | 0.973 | 11.5 | 0.909 | 14.5 | 0.799 | 11.9 | 0.830 | 3.98 | 0.163 | | |
| 8.72 | 0.967 | 8.5 | 0.944 | 12.0 | 0.860 | 15.0 | 0.799 | 12.4 | 0.824 | 4.13 | 0.236 | | |
| 9.35 | 0.975 | 9.0 | 0.957 | 12.5 | 0.849 | CURVE 71 T = 1255. | | | | | | | |
| 10.0 | 0.942 | 9.5 | 0.981 | 13.0 | 0.848 | 1.00 | 0.132 | 1.00 | 0.104 | 4.78 | 0.423 | | |
| 10.7 | 0.963 | 10.0 | 0.986 | 13.5 | 0.848 | 1.27 | 0.130 | 1.27 | 0.130 | 5.57 | 0.633 | | |
| 11.5 | 0.983 | 10.5 | 0.926 | 14.0 | 0.841 | 2.04 | 0.094 | 2.04 | 0.094 | 5.95 | 0.708 | | |
| 12.3 | 0.911 | 11.0 | 0.971 | 14.5 | 0.830 | 2.55 | 0.091 | 2.55 | 0.091 | 6.59 | 0.796 | | |
| 13.1 | 0.804 | 11.5 | 0.921 | 15.0 | 0.813 | 2.95 | 0.087 | 2.95 | 0.087 | 6.83 | 0.816 | | |
| 13.9 | 0.935 | 12.0 | 0.873 | CURVE 70 T = 1290. | | | | | | 3.09 | 0.134 | 7.08 | 0.932 |
| 14.7 | 0.986 | 12.5 | 0.856 | 1.0 | 0.060 | 3.27 | 0.107 | 3.27 | 0.107 | 7.78 | 0.849 | | |
| 15.5 | 0.983 | 13.0 | 0.852 | 1.5 | 0.046 | 3.85 | 0.183 | 3.85 | 0.183 | 8.79 | 0.362 | | |
| 16.3 | 0.983 | 13.5 | 0.852 | 2.0 | 0.042 | 4.28 | 0.326 | 4.11 | 0.166 | 9.19 | 0.875 | | |
| 17.1 | 0.983 | 14.0 | 0.842 | 2.5 | 0.045 | 4.40 | 0.361 | 4.92 | 0.425 | 10.4 | 0.882 | | |
| 17.9 | 0.983 | 14.5 | 0.833 | 3.0 | 0.045 | 4.59 | 0.380 | 5.26 | 0.521 | 10.6 | 0.875 | | |
| 18.7 | 0.983 | 15.0 | 0.813 | 3.5 | 0.058 | 5.11 | 0.401 | 6.16 | 0.722 | 10.8 | 0.849 | | |
| 19.5 | 0.983 | 15.5 | 0.813 | 4.0 | 0.058 | 5.41 | 0.423 | 6.35 | 0.753 | 11.0 | 0.799 | | |
| 20.3 | 0.983 | 16.0 | 0.813 | 4.5 | 0.080 | 5.66 | 0.448 | 7.08 | 0.832 | 11.4 | 0.683 | | |
| 21.1 | 0.983 | 16.5 | 0.813 | 5.0 | 0.141 | 5.87 | 0.481 | 7.78 | 0.849 | 11.6 | 0.639 | | |
| 21.9 | 0.983 | 17.0 | 0.813 | 5.5 | 0.248 | 6.13 | 0.531 | 8.79 | 0.862 | 11.8 | 0.613 | | |
| 22.7 | 0.983 | 17.5 | 0.813 | 6.0 | 0.389 | 6.28 | 0.573 | 9.19 | 0.875 | 12.5 | 0.616 | | |
| 23.5 | 0.983 | 18.0 | 0.813 | 6.5 | 0.530 | 6.47 | 0.649 | 10.4 | 0.882 | 13.0 | 0.623 | | |
| 24.3 | 0.983 | 18.5 | 0.813 | 7.0 | 0.653 | 6.53 | 0.715 | 10.6 | 0.868 | 13.5 | 0.608 | | |
| 25.1 | 0.983 | 19.0 | 0.813 | 7.5 | 0.785 | 6.63 | 0.781 | 10.8 | 0.846 | 14.1 | 0.597 | | |
| 25.9 | 0.983 | 19.5 | 0.813 | 8.0 | 0.892 | 6.85 | 0.870 | 11.0 | 0.805 | 14.7 | 0.571 | | |

TABLE 6-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|------------------|------------|------------------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| CURVE 73 (CONT.) | | | | | | | | | | | |
| 15.0 | 0.551 | 6.15 | 0.626 | 14.2 | 0.528 | 4.88 | 0.273 | 11.5 | 0.773 | 3.26 | 0.112 |
| CURVE 74 | | | | | | | | | | | |
| T = 1143. | | | | | | | | | | | |
| 3.09 | 0.104 | 6.05 | 0.870 | 15.0 | 0.440 | 4.45 | 0.466 | 12.0 | 0.696 | 3.52 | 0.128 |
| 3.33 | 0.115 | 7.24 | 0.896 | CURVE 77 | | 4.72 | 0.577 | 12.3 | 0.659 | 3.67 | 0.137 |
| 3.59 | 0.126 | 9.46 | 0.916 | T = 1273. | | 5.19 | 0.694 | 13.4 | 0.662 | 3.80 | 0.150 |
| 3.87 | 0.176 | 10.4 | 0.923 | 1.00 | 0.100 | 5.75 | 0.790 | 13.9 | 0.641 | 3.90 | 0.168 |
| 4.59 | 0.456 | 10.6 | 0.917 | 2.99 | 0.102 | 6.38 | 0.866 | 14.7 | 0.595 | 4.01 | 0.198 |
| 5.14 | 0.606 | 11.1 | 0.847 | 3.29 | 0.102 | 6.91 | 0.903 | 15.0 | 0.561 | 4.23 | 0.304 |
| 5.71 | 0.733 | 11.6 | 0.727 | 3.51 | 0.146 | 7.54 | 0.924 | CURVE 80 | | | |
| 6.18 | 0.808 | 11.8 | 0.703 | 3.75 | 0.196 | 10.1 | 0.946 | T = 1273. | | | |
| 6.75 | 0.864 | 12.0 | 0.687 | 4.02 | 0.282 | 10.5 | 0.938 | 1.00 | 0.100 | 5.15 | 0.665 |
| 7.42 | 0.888 | 12.3 | 0.673 | 4.32 | 0.460 | 10.9 | 0.914 | 3.30 | 0.114 | 5.44 | 0.755 |
| 10.4 | 0.914 | 13.8 | 0.665 | 4.67 | 0.595 | 11.5 | 0.896 | 3.54 | 0.114 | 5.70 | 0.813 |
| 10.7 | 0.901 | 14.5 | 0.641 | 5.08 | 0.724 | 12.0 | 0.773 | 6.17 | 0.910 | 5.95 | 0.877 |
| 11.1 | 0.858 | 15.0 | 0.614 | 5.48 | 0.806 | 12.3 | 0.696 | 6.45 | 0.944 | 6.71 | 0.959 |
| 11.3 | 0.757 | CURVE 76 (CONT.) | | | | | | | | | |
| 11.5 | 0.722 | 1.00 | 0.100 | 5.17 | 0.898 | 12.6 | 0.669 | 6.90 | 0.976 | 7.17 | 1.000 |
| 11.7 | 0.690 | 2.99 | 0.102 | 6.52 | 0.925 | 13.9 | 0.641 | 8.05 | 0.909 | 8.05 | 0.909 |
| 12.0 | 0.656 | 3.51 | 0.146 | 7.30 | 0.953 | 14.7 | 0.595 | 9.07 | 0.975 | 9.07 | 0.975 |
| 12.9 | 0.656 | 3.75 | 0.196 | 9.52 | 0.953 | 15.0 | 0.561 | 9.58 | 0.969 | 9.58 | 0.969 |
| 14.0 | 0.647 | 4.02 | 0.282 | 10.4 | 0.965 | CURVE 79 | | | | | |
| 14.7 | 0.608 | 4.32 | 0.460 | 11.0 | 0.952 | T = 1273. | | | | | |
| 15.0 | 0.501 | 4.67 | 0.595 | 11.2 | 0.900 | 1.00 | 0.100 | 10.2 | 0.996 | 10.60 | 0.951 |
| CURVE 75 | | | | | | | | | | | |
| T = 1273. | | | | | | | | | | | |
| 1.00 | 0.134 | 5.21 | 0.456 | 11.4 | 0.817 | 3.01 | 0.101 | 10.7 | 0.896 | 11.22 | 0.930 |
| 3.09 | 0.109 | 5.79 | 0.671 | 11.5 | 0.781 | 3.33 | 0.111 | 11.0 | 0.866 | 11.71 | 0.926 |
| 3.30 | 0.115 | 6.15 | 0.773 | 11.8 | 0.705 | 3.53 | 0.145 | 11.7 | 0.701 | 12.23 | 0.895 |
| 3.60 | 0.140 | 6.41 | 0.820 | 12.3 | 0.705 | 3.92 | 0.203 | 11.9 | 0.666 | 12.62 | 0.888 |
| 3.78 | 0.153 | 6.68 | 0.857 | 13.7 | 0.696 | 4.08 | 0.273 | 12.3 | 0.639 | 13.46 | 0.884 |
| 4.01 | 0.240 | 7.00 | 0.872 | 14.3 | 0.641 | 4.45 | 0.466 | 13.8 | 0.614 | 14.43 | 0.893 |
| 4.52 | 0.304 | 7.67 | 0.694 | 15.0 | 0.590 | 4.72 | 0.577 | 14.5 | 0.569 | 14.55 | 0.886 |
| 5.00 | 0.613 | 10.3 | 0.906 | CURVE 81 | | | | | | | |
| 5.43 | 0.713 | 10.6 | 0.867 | T = 1273. | | | | | | | |
| CURVE 82 | | | | | | | | | | | |
| T = 1273. | | | | | | | | | | | |
| 1.00 | 0.085 | 1.00 | 0.100 | 6.36 | 0.866 | 1.00 | 0.085 | 1.00 | 0.085 | 1.00 | 0.085 |
| 1.99 | 0.089 | 3.01 | 0.101 | 6.91 | 0.903 | 1.99 | 0.089 | 1.99 | 0.089 | 1.99 | 0.089 |
| 2.96 | 0.089 | 7.54 | 0.924 | 7.54 | 0.924 | 2.96 | 0.089 | 2.96 | 0.089 | 2.96 | 0.089 |
| 3.27 | 0.090 | 10.1 | 0.946 | 10.1 | 0.946 | 3.27 | 0.090 | 3.27 | 0.090 | 3.27 | 0.090 |
| | | 10.5 | 0.938 | 10.5 | 0.938 | | | | | | |
| | | 10.9 | 0.914 | 10.9 | 0.914 | | | | | | |
| | | 11.0 | 0.896 | 11.0 | 0.896 | | | | | | |

TABLE 6-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | | |
|-----------------------|------------|-----------------------|------------|-----------------------|------------|-----------|------------|-----------|------------|-------|-------|
| CURVE 82 (CONT.) | | | | | | | | | | | |
| 3.50 | 0.099 | 3.27 | 0.090 | 1.99 | 0.089 | 3.27 | 0.090 | 3.27 | 0.090 | | |
| 3.64 | 0.110 | 3.50 | 0.099 | 2.96 | 0.089 | 3.50 | 0.099 | 3.50 | 0.099 | | |
| 3.80 | 0.125 | 3.64 | 0.110 | 3.27 | 0.090 | 3.64 | 0.110 | 3.64 | 0.110 | | |
| 3.93 | 0.155 | 3.80 | 0.125 | 3.50 | 0.099 | 3.80 | 0.125 | 3.80 | 0.125 | | |
| 4.07 | 0.187 | 3.93 | 0.155 | 3.64 | 0.110 | 3.93 | 0.155 | 3.93 | 0.155 | | |
| 4.27 | 0.239 | 4.07 | 0.187 | 3.80 | 0.125 | 4.06 | 0.168 | 4.07 | 0.187 | | |
| 4.47 | 0.323 | 4.27 | 0.277 | 3.93 | 0.143 | 4.19 | 0.201 | 4.22 | 0.237 | | |
| 4.72 | 0.423 | 4.47 | 0.331 | 4.06 | 0.169 | 4.38 | 0.258 | 4.34 | 0.299 | | |
| 4.94 | 0.502 | 4.72 | 0.449 | 4.19 | 0.201 | 4.64 | 0.351 | 4.54 | 0.371 | | |
| 5.22 | 0.601 | 4.94 | 0.478 | 4.38 | 0.258 | 4.90 | 0.444 | 4.78 | 0.450 | | |
| 5.52 | 0.694 | 5.22 | 0.519 | 4.59 | 0.322 | 5.17 | 0.506 | 5.06 | 0.541 | | |
| 5.80 | 0.751 | 5.52 | 0.566 | 4.97 | 0.447 | 5.44 | 0.623 | 5.24 | 0.585 | | |
| 6.05 | 0.825 | 5.80 | 0.655 | 5.24 | 0.537 | 5.76 | 0.712 | 5.47 | 0.633 | | |
| 6.25 | 0.860 | 6.05 | 0.698 | 5.52 | 0.620 | 5.90 | 0.753 | 5.71 | 0.673 | | |
| 6.53 | 0.902 | 6.25 | 0.763 | 5.78 | 0.697 | 6.10 | 0.795 | 5.87 | 0.700 | | |
| 6.75 | 0.924 | 6.53 | 0.819 | 5.94 | 0.731 | 6.33 | 0.831 | 6.14 | 0.743 | | |
| 7.01 | 0.944 | 6.75 | 0.860 | 6.25 | 0.792 | 6.60 | 0.864 | 6.39 | 0.770 | | |
| 7.40 | 0.959 | 7.01 | 0.873 | 6.40 | 0.816 | 6.85 | 0.890 | 6.66 | 0.799 | | |
| 7.71 | 0.963 | 7.40 | 0.897 | 6.64 | 0.848 | 7.07 | 0.911 | 7.05 | 0.817 | | |
| 9.13 | 0.953 | 7.71 | 0.913 | 6.83 | 0.872 | 7.38 | 0.926 | 7.56 | 0.826 | | |
| 9.50 | 0.957 | 9.13 | 0.930 | 7.05 | 0.885 | 7.69 | 0.926 | 8.54 | 0.837 | | |
| 9.99 | 0.947 | 9.50 | 0.942 | 7.33 | 0.897 | 8.63 | 0.921 | 9.75 | 0.837 | | |
| 10.60 | 0.948 | 9.99 | 0.942 | 7.58 | 0.897 | 10.04 | 0.921 | 10.21 | 0.845 | | |
| 11.22 | 0.926 | 10.60 | 0.935 | 8.27 | 0.900 | 10.40 | 0.931 | 10.60 | 0.845 | | |
| 11.71 | 0.926 | 11.22 | 0.936 | 9.27 | 0.900 | 10.60 | 0.931 | 10.72 | 0.937 | | |
| 12.01 | 0.898 | 11.71 | 0.931 | 10.60 | 0.900 | 11.08 | 0.928 | 10.91 | 0.822 | | |
| 12.28 | 0.898 | 12.01 | 0.926 | 11.10 | 0.885 | 11.33 | 0.911 | 11.04 | 0.804 | | |
| 12.62 | 0.868 | 12.28 | 0.926 | 11.53 | 0.879 | 11.86 | 0.878 | 11.53 | 0.692 | | |
| 13.46 | 0.834 | 12.62 | 0.850 | 12.04 | 0.863 | 11.97 | 0.866 | 11.62 | 0.642 | | |
| 13.93 | 0.893 | 13.46 | 0.885 | 12.58 | 0.856 | 12.59 | 0.855 | 12.03 | 0.612 | | |
| 14.43 | 0.893 | 13.93 | 0.884 | 13.71 | 0.856 | 13.56 | 0.842 | 12.50 | 0.613 | | |
| 14.65 | 0.866 | 14.43 | 0.893 | 14.47 | 0.851 | 14.59 | 0.842 | 13.14 | 0.622 | | |
| 15.00 | 0.885 | 14.65 | 0.893 | 15.00 | 0.839 | 15.00 | 0.836 | 13.74 | 0.622 | | |
| 15.00 | 0.865 | 15.00 | 0.865 | CURVE 85 T = 1273. | | | | | | 14.00 | 0.603 |
| CURVE 83 T = 1273. | | | | | | | | | | | |
| 1.00 | 0.085 | CURVE 85 T = 1273. | | | | | | 14.48 | 0.562 | | |
| 1.99 | 0.089 | 1.00 | 0.085 | 1.00 | 0.085 | 1.00 | 0.085 | 14.62 | 0.543 | | |
| 2.96 | 0.089 | 1.99 | 0.089 | 1.99 | 0.089 | 1.99 | 0.089 | 14.81 | 0.516 | | |
| | | 2.96 | 0.089 | 2.96 | 0.089 | 2.96 | 0.089 | 15.00 | 0.489 | | |

b. Normal Spectral Emittance (Temperature Dependence)

A total of seven sets of experimental data were located for the temperature dependence of the normal spectral emittance of aluminum oxide as listed in Table 6-6 and shown in Figure 6-8. Specimen characterization and measurement information for the data are given in Table 6-5. All the data are for wavelengths of 1 μm or below.

However, provisional values at 3.8 and 10.6 μm for Coors AD 99 are shown in Figure 6-7 and are listed in Table 6-4. The values were obtained from the two provisional curves in the previous section. The uncertainty in each point is 15%. The lines connecting the two points for each wavelength are not to imply a smooth curve and are used merely as an aid in visualizing and integrating the values presented.

TABLE 6-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (COORS AD 99) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ |
|-----------------|------------|------------------|------------|
| $\lambda = 3.8$ | | $\lambda = 10.6$ | |
| 1303. | 0.543 | 1303. | 0.966 |
| 1423. | 0.399 | 1423. | 0.966 |

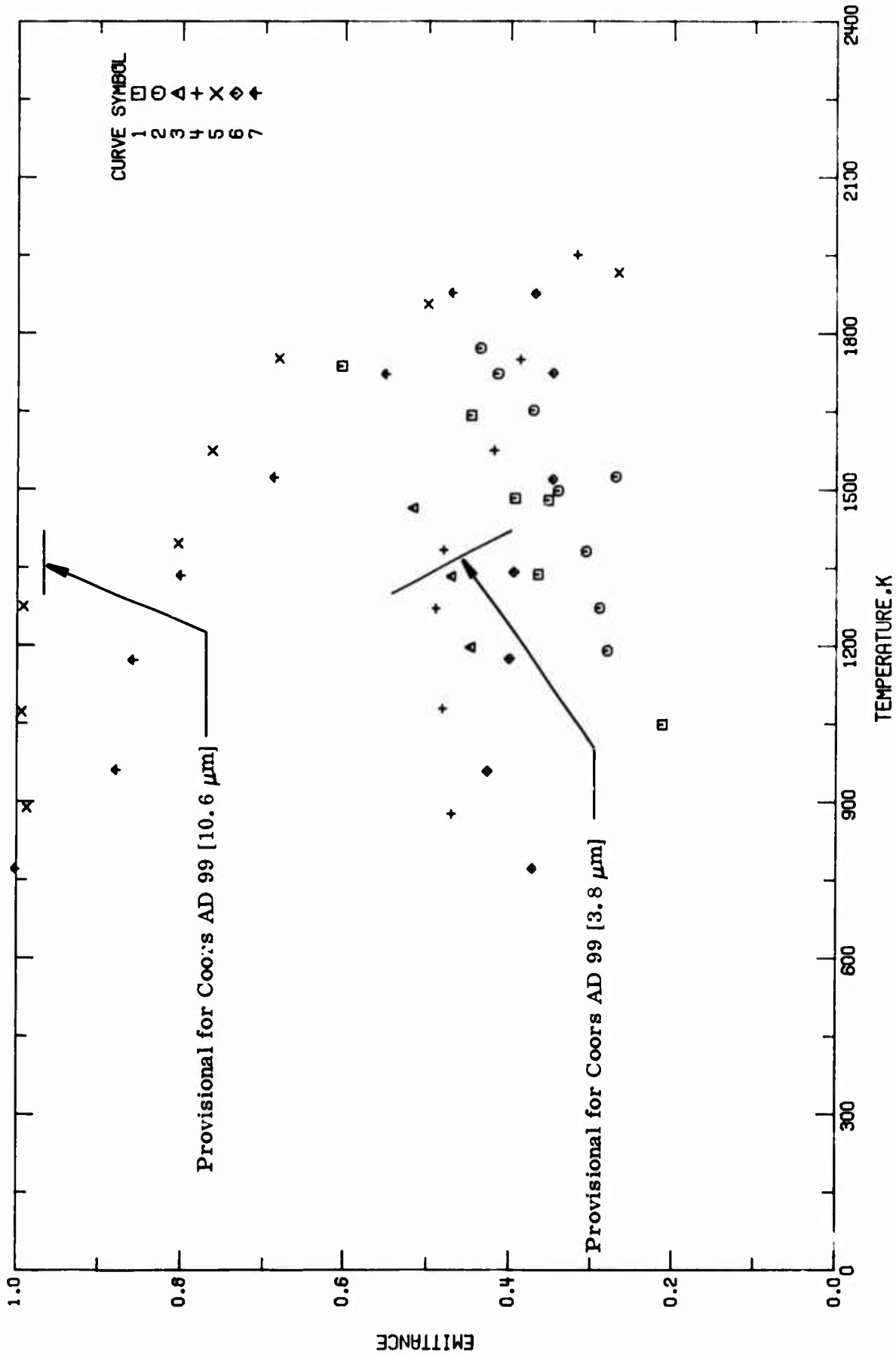


FIGURE 6-7. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE).

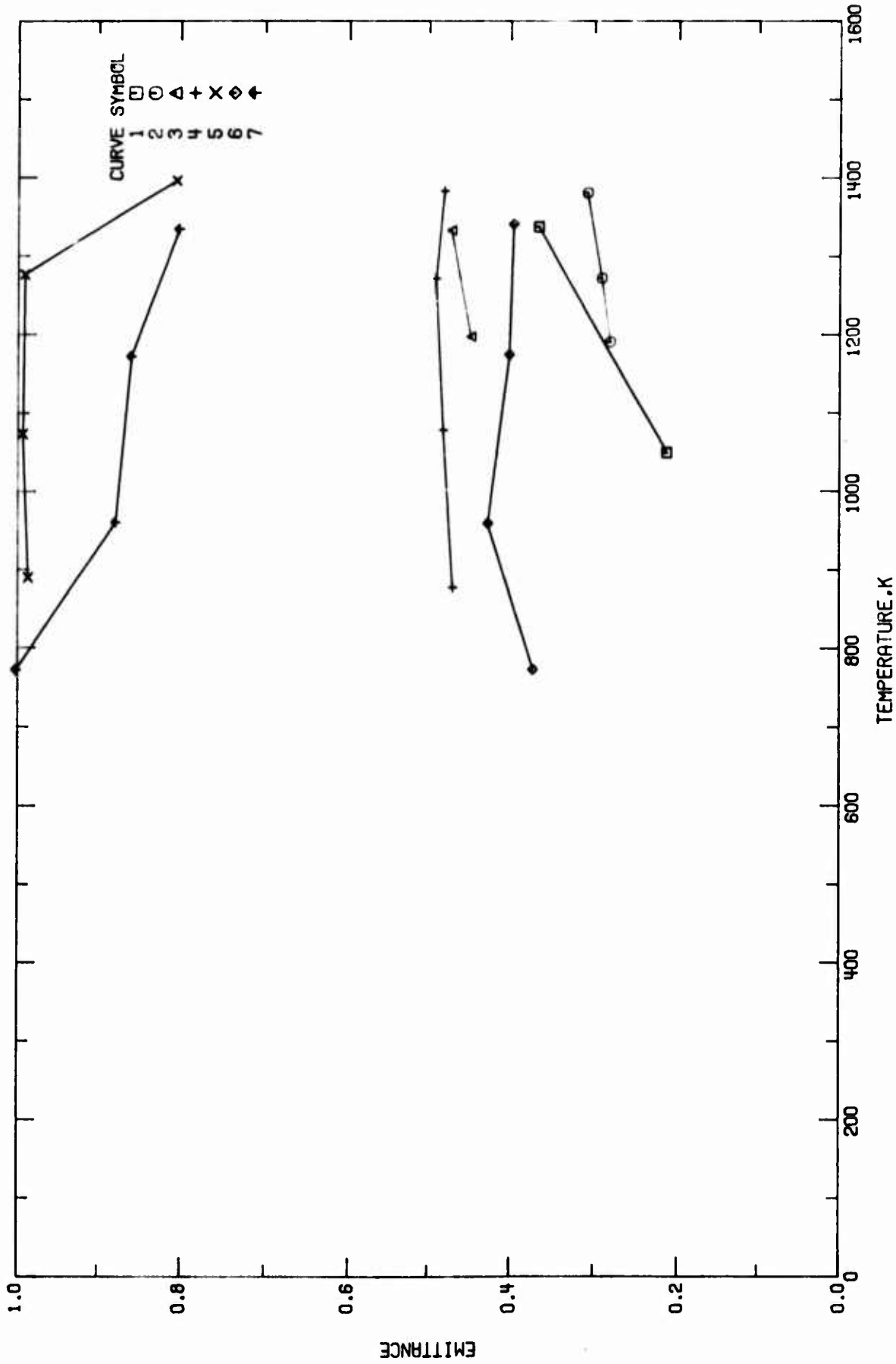


FIGURE 6-8. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE).

TABLE 6-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1050-1740 | Norton LA603 | Data from figure; $\theta' = 0^\circ$. |
| 2 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1191-1773 | Norton RA4213 | Data from figure; $\theta' = 0^\circ$. |
| 3 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1198-1465 | Norton Rokide A | Material on stainless steel No. 446; data from figure; $\theta' = 0^\circ$. |
| 4 T18630 | Blair, G.R. | 1960 | 0.640 | 878-1953 | Frenchtown alumina 4402 | Ground to size, ultrasonically cleaned, surface polished with 1-5 μm diamond polishing compound until normally mat surface began to reflect light; cleaned, polished with cloth charged with a paste of cerium oxide and kerosene; measured in vacuum; data from figure; emissivity reported; $\theta' = 0^\circ$; reported error $\sim 10\%$. |
| 5 T18630 | Blair, G.R. | 1960 | 1 | 891-1919 | Frenchtown alumina 4402 | The above specimen. |
| 6 T18630 | Blair, G.R. | 1960 | 0.640 | 773-1878 | Coors alumina AD 99 | Similar to the above specimen. |
| 7 T18630 | Blair, G.R. | 1960 | 1 | 773-1880 | Coors alumina AD 99 | The above specimen. |

TABLE 5-5. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM OXIDE (TEMPERATURE DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| T | ϵ | T | ϵ |
|-------------------|------------|-------------------|------------|
| CURVE 1 | | | |
| $\lambda = 0.665$ | | | |
| 1056. | 0.213 | 891. | 0.985 |
| 1339. | 0.366 | 1075. | 0.992 |
| 1482. | 0.353 | 1276. | 0.990 |
| 1485. | 0.394 | 1397. | 0.803 |
| 1645. | 0.445 | 1576. | 0.762 |
| 1740. | 0.603 | 1754. | 0.681 |
| | | 1858. | 0.500 |
| | | 1919. | 0.267 |
| CURVE 2 | | | |
| $\lambda = 0.665$ | | | |
| 1191. | 0.280 | CURVE 6 | |
| 1273. | 0.290 | $\lambda = 0.640$ | |
| 1382. | 0.307 | 773. | 0.372 |
| 1499. | 0.341 | 950. | 0.425 |
| 1526. | 0.270 | 1175. | 0.400 |
| 1654. | 0.372 | 1342. | 0.395 |
| 1724. | 0.414 | 1521. | 0.347 |
| 1773. | 0.434 | 1726. | 0.347 |
| | | 1879. | 0.370 |
| CURVE 3 | | | |
| $\lambda = 0.665$ | | | |
| 1198. | 0.445 | CURVE 7 | |
| 1334. | 0.470 | $\lambda = 1.0$ | |
| 1465. | 0.519 | 773. | 1.000 |
| | | 962. | 0.676 |
| | | 1173. | 0.657 |
| | | 1335. | 0.800 |
| | | 1524. | 0.687 |
| | | 1724. | 0.550 |
| | | 1880. | 0.468 |
| CURVE 4 | | | |
| $\lambda = 0.640$ | | | |
| 676. | 0.463 | | |
| 1079. | 0.430 | | |
| 1272. | 0.439 | | |
| 1364. | 0.479 | | |
| 1579. | 0.418 | | |
| 1751. | 0.388 | | |
| 1953. | 0.319 | | |

c. Normal Spectral Reflectance (Wavelength Dependence)

A total of 31 sets of experimental data were located for the wavelength dependence of the normal spectral reflectance of aluminum oxide as listed in Table 6-8 and shown in Figure 6-9. Figure 6-9 does not show the data for curves 4, 9-13, and 30-31. The data for these curves reported in the literature are relative values and some individual data points are over 1.0. The computer program handling the plotting divides any data over 1.0 by 100, and hence the curves having such data were not plotted. Specimen characterization and measurement information for the data are given in Table 6-7.

The data are predominately for wavelengths below $2.7 \mu\text{m}$. The data above $2.7 \mu\text{m}$ are not identified with any specific brand names nor are there confirmatory data for these data sets. For these reasons, taken together, it is not thought justified to pursue developing evaluated data.

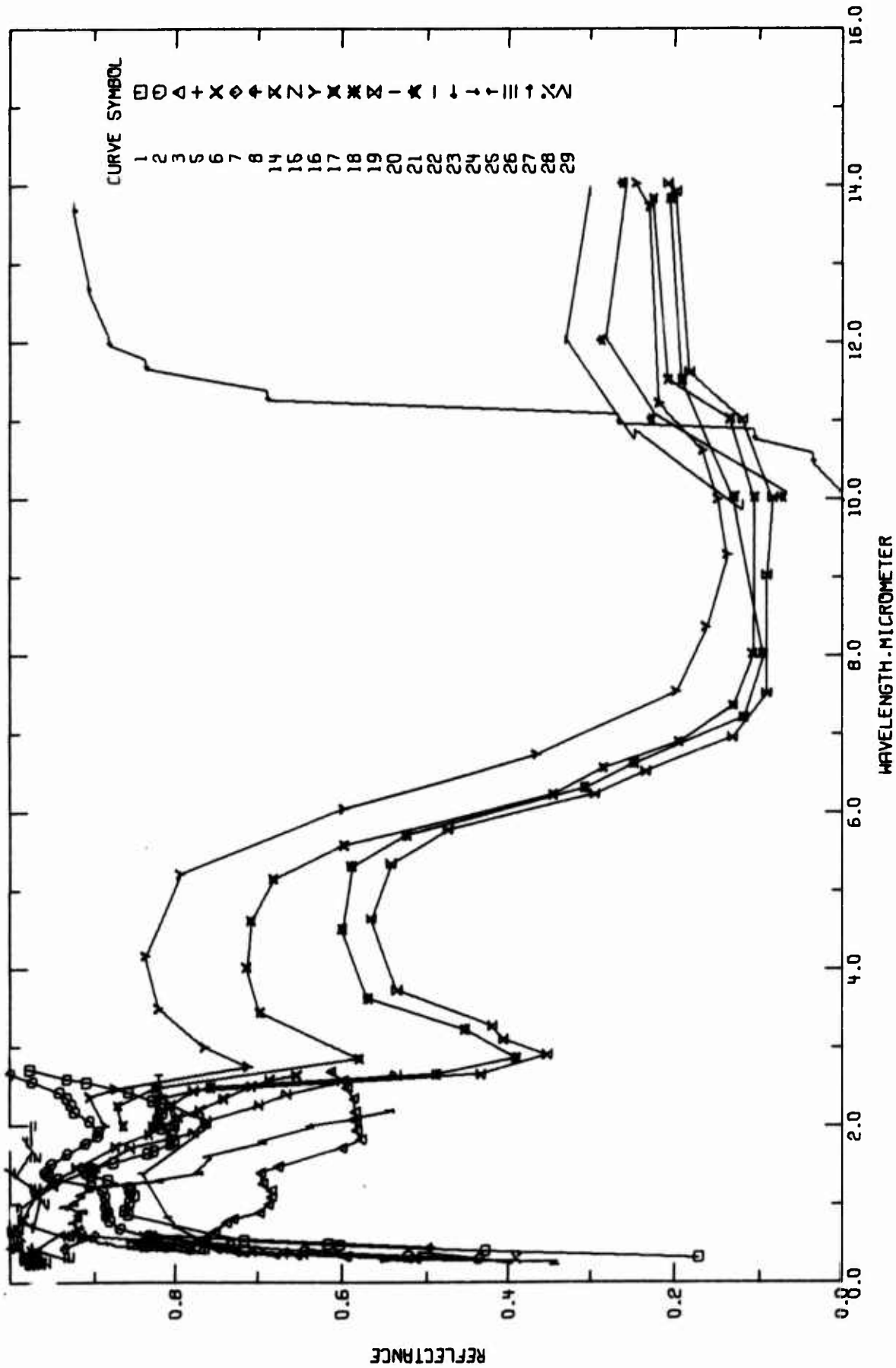


FIGURE 6-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

TABLE 6-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.30-2.7 | 293 | Norton LA603 | Working standard magnesium carbonate surface; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; integrating sphere reflectometer used, reflectance factor measured then values converted to absolute reflectance values; $\theta = 9^\circ$, $\omega' = 2\pi$; reported error 4%. |
| 2 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.30-2.7 | 293 | Norton RA4213 | Similar to the above specimen. |
| 3 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.31-2.7 | 293 | Norton Rokide A | Similar to the above specimen except material on stainless steel No. 446. |
| 4 T22272 | Schatz, E.A., Goldberg, D.M., Pearson, E.G., and Burks, T.L. | 1963 | 0.23-2.7 | 293 | Sample No. 112 | Sintered at 1923 K for 1 hr, setter material Al_2O_3 ; thickness 69 mils; density 3.45 g cm^{-3} , theoretical density 3.97 g cm^{-3} ; MgO reference standard, reflectance data measured and presented relative to MgO; spectral total reflectance reported; integrating sphere reflectometer, Beckman DK-2a spectroradiometer used; measurement temperature not given explicitly, 293 K assigned; smooth values from figure; $\theta = 5^\circ$, $\omega' = 2\pi$. |
| 5 T28755 | Zerlaut, G.A. and Harada, Y. | 1963 | 0.44, 0.60 | 293 | Alucer MC, alpha | Supplied by Gulton Industries; powder compacted at 10 000 psi; MgO used as standard, absolute values of reflectance reported; integrating sphere reflectometer used; measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 6 T28755 | Zerlaut, G.A. and Harada, Y. | 1963 | 0.44, 0.60 | 293 | Alucer MC, alpha | The above specimen except exposed to uv irradiation; 180 E.S.H. with solar factor 3. |
| 7 T28755 | Zerlaut, G.A. and Harada, Y. | 1963 | 0.44, 0.60 | 293 | Alucer MA, gamma | Supplied by Gulton Industries; powder compacted at 10 000 psi; MgO used as standard, absolute values of reflectance reported; integrating sphere reflectometer used; measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 8 T28755 | Zerlaut, G.A. and Harada, Y. | 1963 | 0.44, 0.60 | 293 | Alucer MA, gamma | The above specimen except exposed to uv irradiation; 75 E.S.H. with solar factor 1.5. |
| 9 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | > 99 pure; compacted powder; compaction pressure 290 psi; MgO reference standard; spectral total reflectance versus MgO presented; Beckman DK-2A spectroradiometer used; measurement temperature not given explicitly, assumed to be 293 K; smooth values from figure; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 10 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 1150 psi. |
| 11 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 2880 psi. |
| 12 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 3760 psi. |
| 13 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 11 500 psi. |
| 14 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 20 200 psi. |
| 15 T34908 | Schatz, E.A. | 1966 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 28 800 psi. |
| 16 T34908 | Schatz, E.A. | 1966 | 2.0-15 | 295 | | > 99 pure; compacted powder; compaction pressure 700 psi; absolute spectral total reflectance reported; blackbody reflectometer used in conjunction with Baird-Atomic model NK-1 spectrophotometer; smooth values from figure; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 17 T34908 | Schatz, E.A. | 1966 | 2.0-15 | 293 | | Similar to the above specimen except compacted at 7000 psi. |
| 18 T34908 | Schatz, E.A. | 1966 | 2.0-15 | 293 | | Similar to the above specimen except compacted at 28 000 psi. |
| 19 T34908 | Schatz, E.A. | 1966 | 2.0-15 | 293 | | Similar to the above specimen except compacted at 42 000 psi. |

TABLE 6-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 20 T40230 | Schatz, E. A. | 1967 | 0.23-2.7 | 293 | | Powder; commercially pure; -230 to +270 mesh, pressed at 24,300 Newtons cm^{-2} ; 1.6 mm thick and 22 mm in diameter stainless steel; Beckman DK-2A spectrophotometer used; curves presented relative to smoked MgO standard; measurement temperature not explicitly given, assumed to be 293 K; smooth values from figure; $\theta \sim 0^\circ$, $\omega' = 2\theta$. |
| 21 T40528 | Sulzbach, F. and Turner, A. F. | 1966 | 10.0-36.0 | 293 | | Clear film; electron beam deposited at normal incidence on glass at 423 K at 2 to 8×10^{-5} mm Hg; rate of deposit 1 quarterwave min^{-1} at $\lambda = 0.5 \mu\text{m}$; optical film thickness, index of refraction times thickness equals $10 \lambda/4$ at 2.3 μm ; measurement temperature specified as room temperature, 293 K assigned; Perkin Elmer model 21 and 221 spectrophotometers used for reflectance measurements; $\theta \sim 0^\circ$. |
| 22 T40528 | Sulzbach, F. and Turner, A. F. | 1966 | 9.9-37 | 293 | | Similar to the above specimen except elect on beam deposited at normal incidence on glass at 588 K; index of refraction times thickness equals $10 \lambda/4$ at 2.2 μm . |
| 23 T40528 | Sulzbach, F. and Turner, A. F. | 1966 | 10-37 | 293 | | Crystal; polished; smooth values from figure; measurement temperature specified as room temperature, 293 K assigned; Perkin Elmer models 21 and 221 spectrophotometers used for reflectance measurements; $\theta \sim 0^\circ$. |
| 24 T45667 | De la Perrelle, E. T., and Herbert, H. | 1962 | 0.4-2.2 | 293 | Specimen X64 | Integrating sphere reflectometer used with magnesium carbonate as inside liner of sphere; absolute reflectance factor ($\omega = 2\theta$; $\theta' = 0^\circ$) actually measured, equated to reflectance ($\theta = 0^\circ$; $\omega' = 2\theta$), angles θ and θ' presumed to be approx. 0° ; measurement temperature not given explicitly, assumed to be 293 K. |
| 25 T45700 | Wilcock, D. F. and Solier, W. | 1940 | 0.28-0.32 | 293 | | Dry pigment; packed in shallow steel cell; integrating sphere with magnesium oxide coating on inside used to measure absolute reflectance factor; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\omega' = 2\theta$. |
| 26 T49037 | Zerlaut, G. A., Tompkins, E. H., Harada, Y., and Marshall, G. C. | 1964 | 0.32-2.0 | 293 | Sample 34 | Pressed compact; Cary spectrophotometer used; presume $\theta = 0^\circ$, $\omega' = 2\theta$; measurement temperature not given explicitly, assumed to be 293 K. |
| 27 T34814 | Srinidheg, O. M. | 1966 | 0.43-0.54 | 293 | Reflector VIII | Sintered; Al23 and Al24 supplied by Tegussa; relative reflectance factor ($\omega = 2\theta$; $\theta' = 0^\circ$), compared to smoked MgO reference standard, actually measured, equated to reflectance factor ($\theta = 0^\circ$; $\omega' = 2\theta$); Zeiss Elrepho photometer used in reflectance measurement, diffuse illumination of specimen with white light and observation direction perpendicular to specimen; measurement temperature not explicitly given, 293 K assigned. |
| 28 T34814 | Srinidheg, O. M. | 1966 | 0.31-0.59 | 293 | Reflector VIII | The above specimen except PMQII spectrometer used with RA3 reflection attachment; RA3 used monochromatic light directed perpendicular to the specimen and integrating measurement of total diffuse reflection made. |
| 29 T34814 | Srinidheg, O. M. | 1966 | 0.43-0.54 | 293 | Reflector VIII | The above specimen except exposed to 423 K deionized water for 10 days and Elrepho photometer used for measurement. |
| 30 T35840 | Schatz, E. A., Alvarez, C. H., Counts, C. R., III, and Hoppe, M. A. | 1965 | 0.23-2.7 | 293 | | Sintered 15 hr at 1273 K; density 1.58; MgO reference standard; Beckman DK-2A spectrophotometer used; smooth values from figure; measurement temperature not explicitly given, assumed to be 293 K; $\theta = 5^\circ$, $\omega' = 2\theta$. |
| 31 T35840 | Schatz, E. A., et al. | 1965 | 0.23-2.7 | 293 | | The above specimen except sintered an additional 2 hr at 1923 K; density changed to 3.34. |

TABLE 6-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 T = 293. | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 (CONT.) | | CURVE 9 T = 293. | | CURVE 10 (CONT.) | |
|---------------------|--------|---------------------|--------|---------------------|--------|----------------------|--------|---------------------|--------|----------------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 0.394 | 0.171 | 0.588 | 0.834 | 1.177 | 0.684 | 1.04 | 0.928 | 0.230 | 1.000 | 1.88 | 1.014 |
| 0.429 | 0.429 | 0.678 | 0.668 | 1.263 | 0.694 | 1.15 | 0.934 | 0.243 | 1.000 | 2.07 | 1.020 |
| 0.452 | 0.603 | 0.779 | 0.681 | 1.390 | 0.697 | 1.24 | 0.940 | 0.270 | 1.000 | 2.20 | 1.011 |
| 0.473 | 0.616 | 0.852 | 0.686 | 1.481 | 0.676 | 1.39 | 0.952 | 0.280 | 1.021 | 2.30 | 1.012 |
| 0.519 | 0.717 | 0.887 | 0.684 | 1.710 | 0.600 | 1.55 | 0.956 | 0.289 | 1.033 | 2.45 | 1.000 |
| 0.349 | 0.659 | 0.970 | 0.667 | 1.829 | 0.578 | 1.75 | 0.968 | 0.318 | 1.020 | 2.65 | 0.972 |
| 0.900 | 0.563 | 1.00 | 0.697 | 1.945 | 0.583 | 1.84 | 0.976 | 0.347 | 1.020 | CURVE 11 T = 293. | |
| 0.999 | 0.857 | 1.17 | 0.690 | 2.375 | 0.584 | 1.95 | 0.976 | 0.350 | 1.022 | 0.230 | 0.994 |
| 1.09 | 0.651 | 1.22 | 0.905 | 2.188 | 0.585 | 2.15 | 0.995 | 0.371 | 1.031 | 0.243 | 0.995 |
| 1.16 | 0.855 | 1.31 | 0.944 | 2.356 | 0.566 | 2.24 | 1.00 | 0.571 | 1.031 | 0.254 | 0.999 |
| 1.19 | 0.858 | 1.36 | 0.955 | 2.492 | 0.594 | 2.44 | 1.01 | 0.849 | 1.030 | 0.262 | 0.997 |
| 1.29 | 0.864 | 1.40 | 0.959 | 2.585 | 0.599 | 2.55 | 1.26 | 1.01 | 1.038 | 0.280 | 1.015 |
| 1.35 | 0.904 | 1.50 | 0.952 | 2.702 | 0.613 | 2.65 | 1.05 | 1.15 | 1.034 | 0.293 | 1.019 |
| 1.39 | 0.900 | 1.63 | 0.933 | CURVE 4 T = 293. | | CURVE 5 T = 293. | | 1.47 | 1.036 | 0.262 | 0.997 |
| 1.43 | 0.904 | 1.77 | 0.911 | 0.231 | 0.260 | 0.440 | 1.000 | 1.69 | 1.047 | 0.280 | 1.015 |
| 1.51 | 0.877 | 1.87 | 0.896 | 0.241 | 0.259 | 0.600 | 1.000 | 1.90 | 1.038 | 0.311 | 1.006 |
| 1.63 | 0.834 | 1.93 | 0.895 | 0.250 | 0.242 | CURVE 6 T = 293. | | 2.26 | 1.047 | 0.331 | 1.006 |
| 1.66 | 0.827 | 2.06 | 0.906 | 0.266 | 0.238 | 0.440 | 1.000 | 2.43 | 1.042 | 0.356 | 1.001 |
| 1.75 | 0.806 | 2.17 | 0.924 | 0.274 | 0.246 | CURVE 7 T = 293. | | 2.51 | 1.044 | 0.810 | 1.015 |
| 1.79 | 0.801 | 2.25 | 0.933 | 0.280 | 0.205 | 0.440 | 0.740 | 2.65 | 1.029 | 1.15 | 1.013 |
| 1.87 | 0.805 | 2.35 | 0.942 | 0.285 | 0.375 | CURVE 8 T = 293. | | 0.230 | 0.995 | 1.41 | 1.001 |
| 1.95 | 0.817 | 2.42 | 0.942 | 0.290 | 0.435 | 0.600 | 0.915 | 0.249 | 0.996 | 1.72 | 0.999 |
| 2.07 | 0.822 | 2.55 | 0.974 | 0.300 | 0.517 | CURVE 9 T = 293. | | 0.260 | 1.000 | 1.90 | 0.972 |
| 2.14 | 0.817 | 2.65 | 1.000 | 0.310 | 0.573 | CURVE 10 T = 293. | | 0.281 | 1.017 | 2.12 | 0.966 |
| 2.21 | 0.819 | CURVE 3 T = 293. | | 0.320 | 0.608 | 0.440 | 0.935 | 0.295 | 1.023 | 2.33 | 0.937 |
| 2.30 | 0.829 | 0.307 | 0.513 | 0.330 | 0.634 | 0.600 | 0.900 | 0.319 | 1.010 | 2.55 | 0.900 |
| 2.41 | 0.859 | 0.332 | 0.595 | 0.340 | 0.662 | CURVE 11 T = 293. | | 0.344 | 1.011 | 2.65 | 0.854 |
| 2.53 | 0.910 | 0.395 | 0.727 | 0.350 | 0.678 | 0.440 | 0.935 | 0.459 | 1.020 | CURVE 12 T = 293. | |
| 2.57 | 0.933 | 0.439 | 0.750 | 0.450 | 0.805 | 0.600 | 0.900 | 0.654 | 1.029 | 0.230 | 0.984 |
| 2.69 | 0.977 | 0.565 | 0.763 | 0.503 | 0.844 | CURVE 12 T = 293. | | 0.763 | 1.021 | 0.239 | 0.990 |
| CURVE 2 T = 293. | | 0.647 | 0.752 | 0.561 | 0.867 | 0.440 | 0.495 | 0.970 | 1.023 | 0.252 | 0.983 |
| 0.301 | 0.437 | 0.766 | 0.738 | 0.651 | 0.895 | 0.600 | 0.825 | 1.24 | 1.027 | 0.260 | 0.994 |
| 0.334 | 0.524 | 0.809 | 0.730 | 0.800 | 0.917 | CURVE 13 T = 293. | | 1.44 | 1.019 | 0.270 | 0.989 |
| 0.398 | 0.645 | 0.892 | 0.698 | 0.815 | 0.914 | 0.440 | 0.495 | 1.55 | 1.025 | 0.288 | 1.002 |
| 0.472 | 0.733 | 0.995 | 0.687 | 0.890 | 0.913 | 0.600 | 0.825 | 1.72 | 1.025 | 0.310 | 0.991 |
| 0.533 | 0.796 | 1.091 | 0.664 | 0.912 | 0.923 | CURVE 14 T = 293. | | | | | |

TABLE 6-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| CURVE 12 (CONT.) | | | | | | | | | |
| 0.344 | 0.990 | | | | | | | | |
| 0.350 | 0.995 | | | | | | | | |
| 0.421 | 1.001 | | | | | | | | |
| 0.500 | 1.001 | | | | | | | | |
| 0.641 | 1.006 | | | | | | | | |
| 0.956 | 1.006 | | | | | | | | |
| 1.26 | 1.001 | | | | | | | | |
| 1.43 | 0.989 | | | | | | | | |
| 1.69 | 0.981 | | | | | | | | |
| 1.87 | 0.955 | | | | | | | | |
| 2.03 | 0.949 | | | | | | | | |
| 2.36 | 0.913 | | | | | | | | |
| 2.56 | 0.869 | | | | | | | | |
| 2.65 | 0.837 | | | | | | | | |
| CURVE 13 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 0.230 | 0.980 | | | | | | | | |
| 0.259 | 0.968 | | | | | | | | |
| 0.284 | 0.980 | | | | | | | | |
| 0.293 | 0.981 | | | | | | | | |
| 0.300 | 0.977 | | | | | | | | |
| 0.343 | 0.981 | | | | | | | | |
| 0.350 | 0.985 | | | | | | | | |
| 0.461 | 0.935 | | | | | | | | |
| 0.662 | 1.003 | | | | | | | | |
| 0.782 | 1.000 | | | | | | | | |
| 0.839 | 0.992 | | | | | | | | |
| 1.00 | 0.990 | | | | | | | | |
| 1.29 | 0.968 | | | | | | | | |
| 1.54 | 0.938 | | | | | | | | |
| 1.77 | 0.901 | | | | | | | | |
| 1.92 | 0.865 | | | | | | | | |
| 2.07 | 0.846 | | | | | | | | |
| 2.46 | 0.749 | | | | | | | | |
| 2.55 | 0.740 | | | | | | | | |
| 2.65 | 0.680 | | | | | | | | |
| CURVE 14 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 0.230 | 0.977 | | | | | | | | |
| 0.246 | 0.964 | | | | | | | | |
| 0.256 | 0.967 | | | | | | | | |
| 0.284 | 0.983 | | | | | | | | |
| 0.305 | 0.978 | | | | | | | | |
| 0.330 | 0.974 | | | | | | | | |
| 0.350 | 0.981 | | | | | | | | |
| 0.442 | 0.992 | | | | | | | | |
| 0.652 | 0.997 | | | | | | | | |
| 0.800 | 0.985 | | | | | | | | |
| 1.15 | 0.969 | | | | | | | | |
| 1.46 | 0.921 | | | | | | | | |
| 1.73 | 0.874 | | | | | | | | |
| 1.89 | 0.833 | | | | | | | | |
| 2.11 | 0.796 | | | | | | | | |
| 2.20 | 0.770 | | | | | | | | |
| 2.35 | 0.741 | | | | | | | | |
| 2.51 | 0.708 | | | | | | | | |
| 2.59 | 0.686 | | | | | | | | |
| 2.65 | 0.654 | | | | | | | | |
| CURVE 15 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 0.230 | 0.973 | | | | | | | | |
| 0.253 | 0.959 | | | | | | | | |
| 0.291 | 0.982 | | | | | | | | |
| 0.331 | 0.973 | | | | | | | | |
| 0.350 | 0.931 | | | | | | | | |
| 0.453 | 0.991 | | | | | | | | |
| 0.563 | 0.986 | | | | | | | | |
| 0.679 | 0.991 | | | | | | | | |
| 0.958 | 0.987 | | | | | | | | |
| 1.23 | 0.950 | | | | | | | | |
| 1.46 | 0.930 | | | | | | | | |
| 1.71 | 0.857 | | | | | | | | |
| 1.91 | 0.778 | | | | | | | | |
| 2.06 | 0.763 | | | | | | | | |
| 2.26 | 0.700 | | | | | | | | |
| CURVE 15 (CONT.) | | | | | | | | | |
| 2.40 | 0.667 | | | | | | | | |
| 2.57 | 0.600 | | | | | | | | |
| 2.65 | 0.537 | | | | | | | | |
| CURVE 16 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 2.00 | 0.887 | | | | | | | | |
| 2.36 | 0.906 | | | | | | | | |
| 2.47 | 0.874 | | | | | | | | |
| 2.76 | 0.712 | | | | | | | | |
| 3.01 | 0.764 | | | | | | | | |
| 3.50 | 0.821 | | | | | | | | |
| 4.17 | 0.837 | | | | | | | | |
| 5.21 | 0.794 | | | | | | | | |
| 6.04 | 0.598 | | | | | | | | |
| 6.73 | 0.365 | | | | | | | | |
| 7.53 | 0.198 | | | | | | | | |
| 8.35 | 0.162 | | | | | | | | |
| 9.27 | 0.137 | | | | | | | | |
| 9.98 | 0.146 | | | | | | | | |
| 10.6 | 0.166 | | | | | | | | |
| 11.2 | 0.219 | | | | | | | | |
| 13.7 | 0.230 | | | | | | | | |
| 14.0 | 0.246 | | | | | | | | |
| 15.0 | 0.246 | | | | | | | | |
| CURVE 17 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 2.00 | 0.865 | | | | | | | | |
| 2.25 | 0.872 | | | | | | | | |
| 2.48 | 0.826 | | | | | | | | |
| 2.36 | 0.580 | | | | | | | | |
| 3.45 | 0.698 | | | | | | | | |
| 4.02 | 0.714 | | | | | | | | |
| 4.62 | 0.705 | | | | | | | | |
| 5.15 | 0.682 | | | | | | | | |
| 5.58 | 0.598 | | | | | | | | |
| 6.22 | 0.345 | | | | | | | | |
| CURVE 17 (CONT.) | | | | | | | | | |
| 6.56 | 0.285 | | | | | | | | |
| 6.89 | 0.195 | | | | | | | | |
| 7.35 | 0.131 | | | | | | | | |
| 8.01 | 0.108 | | | | | | | | |
| 10.0 | 0.106 | | | | | | | | |
| 11.0 | 0.134 | | | | | | | | |
| 11.5 | 0.208 | | | | | | | | |
| 13.8 | 0.226 | | | | | | | | |
| 14.1 | 0.235 | | | | | | | | |
| 15.0 | 0.235 | | | | | | | | |
| CURVE 18 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 2.00 | 0.828 | | | | | | | | |
| 2.34 | 0.822 | | | | | | | | |
| 2.49 | 0.757 | | | | | | | | |
| 2.65 | 0.489 | | | | | | | | |
| 2.87 | 0.390 | | | | | | | | |
| 3.23 | 0.454 | | | | | | | | |
| 3.63 | 0.570 | | | | | | | | |
| 4.51 | 0.600 | | | | | | | | |
| 5.31 | 0.599 | | | | | | | | |
| 5.71 | 0.525 | | | | | | | | |
| 6.31 | 0.207 | | | | | | | | |
| 6.62 | 0.249 | | | | | | | | |
| 7.20 | 0.119 | | | | | | | | |
| 8.01 | 0.096 | | | | | | | | |
| 10.0 | 0.130 | | | | | | | | |
| 11.5 | 0.191 | | | | | | | | |
| 13.8 | 0.205 | | | | | | | | |
| 14.1 | 0.221 | | | | | | | | |
| 15.0 | 0.219 | | | | | | | | |
| CURVE 19 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 2.00 | 0.801 | | | | | | | | |
| 2.26 | 0.807 | | | | | | | | |
| 2.45 | 0.778 | | | | | | | | |
| CURVE 19 (CONT.) | | | | | | | | | |
| 2.66 | 0.435 | | | | | | | | |
| 2.91 | 0.352 | | | | | | | | |
| 3.11 | 0.406 | | | | | | | | |
| 3.28 | 0.420 | | | | | | | | |
| 3.74 | 0.536 | | | | | | | | |
| 4.65 | 0.566 | | | | | | | | |
| 5.35 | 0.543 | | | | | | | | |
| 5.78 | 0.475 | | | | | | | | |
| 6.23 | 0.295 | | | | | | | | |
| 6.52 | 0.235 | | | | | | | | |
| 6.95 | 0.132 | | | | | | | | |
| 7.51 | 0.092 | | | | | | | | |
| 9.01 | 0.092 | | | | | | | | |
| 10.0 | 0.085 | | | | | | | | |
| 11.0 | 0.120 | | | | | | | | |
| 11.6 | 0.182 | | | | | | | | |
| 13.0 | 0.198 | | | | | | | | |
| 14.0 | 0.208 | | | | | | | | |
| 15.0 | 0.206 | | | | | | | | |
| CURVE 20 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 0.230 | 0.342 | | | | | | | | |
| 0.259 | 0.344 | | | | | | | | |
| 0.266 | 0.354 | | | | | | | | |
| 0.274 | 0.406 | | | | | | | | |
| 0.285 | 0.459 | | | | | | | | |
| 0.294 | 0.500 | | | | | | | | |
| 0.316 | 0.559 | | | | | | | | |
| 0.335 | 0.613 | | | | | | | | |
| 0.346 | 0.643 | | | | | | | | |
| 0.350 | 0.684 | | | | | | | | |
| 0.373 | 0.711 | | | | | | | | |
| 0.456 | 0.741 | | | | | | | | |
| 0.560 | 0.770 | | | | | | | | |
| 0.708 | 0.797 | | | | | | | | |
| 0.838 | 0.809 | | | | | | | | |
| 1.39 | 0.841 | | | | | | | | |
| 1.99 | 0.762 | | | | | | | | |
| CURVE 20 (CONT.) | | | | | | | | | |
| 2.07 | 0.762 | | | | | | | | |
| 2.14 | 0.777 | | | | | | | | |
| 2.30 | 0.809 | | | | | | | | |
| 2.39 | 0.816 | | | | | | | | |
| 2.51 | 0.823 | | | | | | | | |
| 2.65 | 0.821 | | | | | | | | |
| CURVE 21 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 10.0 | 0.073 | | | | | | | | |
| 11.0 | 0.229 | | | | | | | | |
| 12.0 | 0.288 | | | | | | | | |
| 14.0 | 0.263 | | | | | | | | |
| 15.1 | 0.250 | | | | | | | | |
| 16.0 | 0.238 | | | | | | | | |
| 17.1 | 0.228 | | | | | | | | |
| 19.0 | 0.219 | | | | | | | | |
| 20.0 | 0.212 | | | | | | | | |
| 21.0 | 0.216 | | | | | | | | |
| 22.1 | 0.209 | | | | | | | | |
| 23.1 | 0.207 | | | | | | | | |
| 23.9 | 0.210 | | | | | | | | |
| 25.1 | 0.210 | | | | | | | | |
| 26.1 | 0.215 | | | | | | | | |
| 27.0 | 0.221 | | | | | | | | |
| 29.0 | 0.234 | | | | | | | | |
| 31.0 | 0.252 | | | | | | | | |
| 32.9 | 0.270 | | | | | | | | |
| 33.9 | 0.263 | | | | | | | | |
| 35.0 | 0.244 | | | | | | | | |
| 36.0 | 0.216 | | | | | | | | |
| CURVE 22 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 9.9 | 0.119 | | | | | | | | |
| 10.8 | 0.248 | | | | | | | | |
| 12.0 | 0.331 | | | | | | | | |
| 13.9 | 0.301 | | | | | | | | |

TABLE 6-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 22 (CONT.) | | | CURVE 23 (CONT.) | | | CURVE 24 (CONT.) | | | CURVE 28 | | | CURVE 30 (CONT.) | | | CURVE 31 (CONT.) | | |
|------------------|--------|--|------------------|--------|----------|------------------|----------|--------|-----------|--------|-------|------------------|--------|--|------------------|--------|--|
| λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | |
| CURVE 22 (CONT.) | | | CURVE 23 (CONT.) | | | CURVE 24 (CONT.) | | | CURVE 28 | | | CURVE 30 (CONT.) | | | CURVE 31 (CONT.) | | |
| 14.7 | 0.287 | | 21.9 | 0.935 | 1.2 | 0.906 | T = 293. | 0.3058 | 0.391 | 0.427 | 0.869 | 0.863 | 0.981 | | | | |
| 15.0 | 0.307 | | 23.0 | 0.854 | 1.3 | 0.82 | 0.3265 | 0.514 | 0.504 | 0.911 | 0.928 | 0.979 | | | | | |
| 18.0 | 0.239 | | 23.9 | 0.757 | 1.4 | 0.771 | 0.3589 | 0.646 | 0.565 | 0.932 | 1.52 | 1.03 | | | | | |
| 19.9 | 0.268 | | 25.6 | 0.556 | 1.6 | 0.761 | 0.3721 | 0.671 | 0.654 | 0.943 | 1.80 | 1.06 | | | | | |
| 21.9 | 0.245 | | 25.9 | 0.547 | 1.8 | 0.695 | 0.3957 | 0.708 | 0.777 | 0.962 | 1.96 | 1.07 | | | | | |
| 23.9 | 0.238 | | 26.3 | 0.591 | 2.0 | 0.639 | 0.4525 | 0.789 | 0.866 | 0.990 | 2.07 | 1.09 | | | | | |
| 25.9 | 0.247 | | 27.2 | 0.522 | 2.1 | 0.585 | 0.4984 | 0.829 | 1.16 | 1.03 | 2.17 | 1.09 | | | | | |
| 27.9 | 0.272 | | 27.9 | 0.489 | 2.2 | 0.544 | 0.5381 | 0.822 | 1.29 | 1.05 | 2.36 | 1.11 | | | | | |
| 30.5 | 0.313 | | 28.5 | 0.483 | | | 0.5644 | 0.828 | 1.40 | 1.04 | 2.65 | 1.11 | | | | | |
| 32.5 | 0.305 | | 29.8 | 0.427 | CURVE 25 | | | 0.5916 | 0.840 | 1.60 | 1.05 | | | | | | |
| 33.1 | 0.352 | | 30.5 | 0.431 | T = 293. | | | | 1.75 | 1.07 | | | | | | | |
| 33.9 | 0.288 | | 30.9 | 0.426 | | | | | 1.95 | 1.03 | | | | | | | |
| 35.9 | 0.293 | | 31.6 | 0.408 | 0.28 | 0.55 | | | 2.06 | 1.06 | | | | | | | |
| 36.9 | 0.275 | | 32.3 | 0.406 | 0.32 | 0.55 | | | 2.15 | 1.08 | | | | | | | |
| CURVE 23 | | | 32.8 | 0.415 | CURVE 26 | | | | | 2.25 | 1.08 | | | | | | |
| T = 293. | | | 33.1 | 0.456 | T = 293. | | | | 2.65 | 1.00 | | | | | | | |
| 10.0 | 0.000 | | 33.4 | 0.413 | 0.325 | 0.93 | 0.4260 | 0.762 | | | | | | | | | |
| 10.5 | 0.036 | | 34.0 | 0.407 | 0.375 | 0.97 | 0.4570 | 0.813 | | | | | | | | | |
| 10.9 | 0.106 | | 35.0 | 0.402 | 0.450 | 0.98 | 0.4950 | 0.844 | | | | | | | | | |
| 11.0 | 0.267 | | 37.0 | 0.388 | 0.600 | 0.93 | 0.5400 | 0.832 | | | | | | | | | |
| 11.3 | 0.689 | | | | 0.700 | 0.98 | | | | | | | | | | | |
| 11.7 | 0.837 | | | | 1.0 | 0.96 | | | | | | | | | | | |
| 12.0 | 0.883 | | | | 1.2 | 0.97 | | | | | | | | | | | |
| 12.7 | 0.907 | | | | 1.4 | 1.00 | | | | | | | | | | | |
| 13.7 | 0.924 | | | | 1.6 | 0.97 | | | | | | | | | | | |
| 14.6 | 0.926 | | | | 1.8 | 0.98 | | | | | | | | | | | |
| 15.1 | 0.913 | | | | 2.0 | 0.97 | | | | | | | | | | | |
| 15.4 | 0.938 | | | | | | | | | | | | | | | | |
| 15.8 | 0.836 | | | | | | | | | | | | | | | | |
| 16.2 | 0.856 | | | | | | | | | | | | | | | | |
| 19.2 | 0.164 | | | | | | | | | | | | | | | | |
| 19.5 | 0.129 | | | | | | | | | | | | | | | | |
| 19.7 | 0.685 | | | | | | | | | | | | | | | | |
| 20.0 | 0.698 | | | | | | | | | | | | | | | | |
| 20.4 | 0.680 | | | | | | | | | | | | | | | | |
| 20.8 | 0.512 | | | | | | | | | | | | | | | | |
| 20.0 | 0.899 | | | | | | | | | | | | | | | | |
| 21.3 | 0.955 | | | | | | | | | | | | | | | | |

CURVE 31
T = 293.

CURVE 30
T = 293.

CURVE 24
T = 293.

CURVE 27
T = 293.

d. Angular Spectral Reflectance (Wavelength Dependence)

A total of 10 sets of experimental data were located for the wavelength dependence of the angular spectral reflectance of aluminum oxide. These data are listed in Table 6-10 and shown in Figure 6-10. Specimen characterization and measurement information for the data are given in Table 6-9.

The data are all for a temperature of 293 K and none of the sets are for Coors alumina or other commercial alumina and, therefore, no data evaluation is possible.

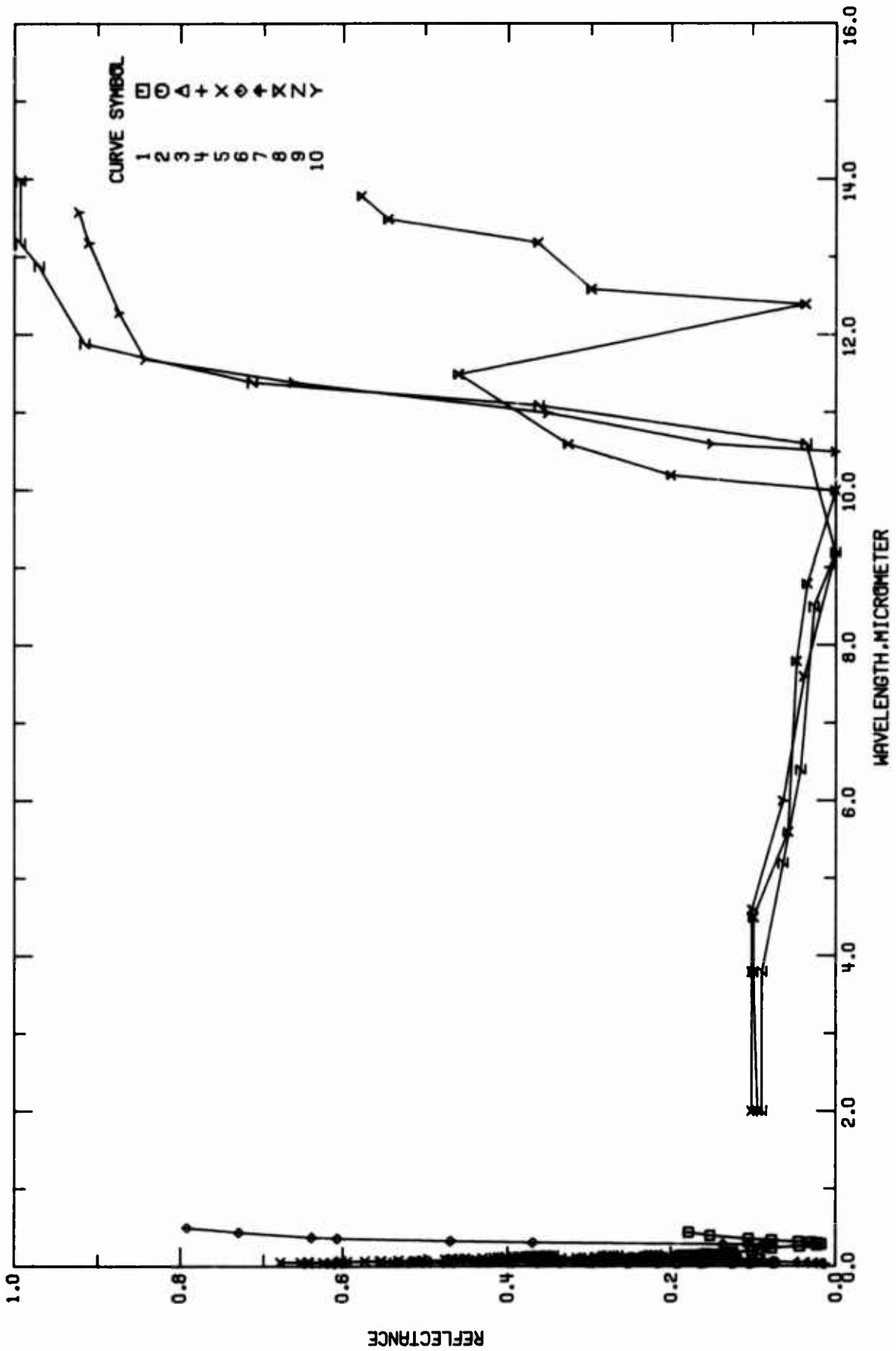


FIGURE 6-10. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

TABLE 6-9. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (Wavelength Dependence)

| Cat. No. | Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|----------|----------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | T32363 | Hass, G. and Tousey, R. | 1959 | 0.058-0.44 | 293 | | Al_2O_3 film on SiO coated glass; both films were effectively $\lambda/4$ thick at 3000 \AA ; angles θ and θ' determined by measurement from diagram of evaporator (see Fig. 1 in T32363); measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 18^\circ$, $\theta' \sim 18^\circ$. |
| 2 | T48912 | Arakawa, E. T. and Williams, M. W. | 1968 | 0.0473-0.16 | 293 | Corundum | Single crystal; cut with the optic axis parallel to the reflecting surface; polished using 6 μm diamond paste, followed by a final polish using 0.5 μm diamond paste on a Buchler microcloth wheel; measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 20^\circ$, $\theta' \sim 20^\circ$; reported error 2%. |
| 3 | T48912 | Arakawa, E. T. and Williams, M. W. | 1968 | 0.043-0.14 | 293 | Corundum | The above specimen; $\theta = 50^\circ$, $\theta' = 50^\circ$. |
| 4 | T48912 | Arakawa, E. T. and Williams, M. W. | 1968 | 0.043-0.14 | 293 | Corundum | The above specimen; $\theta = 60^\circ$, $\theta' = 60^\circ$. |
| 5 | T48912 | Arakawa, E. T. and Williams, M. W. | 1968 | 0.043-0.14 | 293 | Corundum | The above specimen; $\theta = 70^\circ$, $\theta' = 70^\circ$. |
| 6 | T34614 | Stralduhag, O. M. | 1966 | 0.25-6.50 | 293 | Reflector No. VII | Sintered Al23 and Al24 aluminum oxide; supplied by Degussa; relative reflectance factor determined; data reported relative to smoked MgO reference standard; PMQ II spectrometer used with RA2 reflection attachment; smooth values from figure; measurement temperature not explicitly given, 293 K assigned; $\theta = 45^\circ$, $\theta' = 0^\circ$. |
| 7 | T42891 | Stephan, G., Lezonier, J. C., and Robins, S. | 1967 | 0.029-0.15 | 293 | Corundum | Specimen cut perpendicular to the optic axis; measured in vacuum; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 20^\circ$, $\theta' = 20^\circ$. |
| 8 | T50100 | McCarthy, D. E. | 1963 | 2-50 | 293 | Sapphire | Synthetic; specimen 2 mm thick, ground and polished to a flatness of seven fringes or better; reference standard was aluminum mirror; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; Beckman IR-5A used in 2-16 μm range and Beckman IR-7 with CsI interchange used in 12.5-50 μm range; $\theta = 30^\circ$, $\theta' = 30^\circ$. |
| 9 | T36324 | McCarthy, D. E. | 1965 | 2-50 | 293 | Ruby | 0.05 Cr, essentially sapphire with the chromium impurity; synthetic; specimen 6.10 mm thick; flat to 10 fringes or better; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 30^\circ$, $\theta' = \theta'$. |
| 10 | T36324 | McCarthy, D. E. | 1965 | 2-50 | 293 | Sapphire | Synthetic; specimen 3.0 mm thick; flat to 10 fringes or better; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 30^\circ$, $\theta' = 30^\circ$. |

TABLE 6-13. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUE.)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 6 (CONT.) | | CURVE 8 (CONT.) | | CURVE 9 | | CURVE 9 (CONT.) | | CURVE 10 (CONT.) | |
|-----------------|--------|-----------------|--------|-----------|--------|-----------------|--------|------------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| CURVE 7 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 0.2825 | 0.135 | 5.6 | 0.057 | 2.0 | 0.088 | 43.6 | 0.306 | 24.2 | 0.554 |
| 0.3003 | 0.369 | 7.9 | 0.047 | 3.8 | 0.088 | 45.7 | 0.284 | 25.4 | 0.520 |
| 0.3255 | 0.468 | 8.8 | 0.034 | 5.2 | 0.063 | 46.7 | 0.257 | 26.4 | 0.547 |
| 0.3605 | 0.606 | 10.0 | 0.000 | 6.4 | 0.042 | 47.5 | 0.234 | 27.1 | 0.464 |
| 0.3732 | 0.638 | 10.2 | 0.200 | 8.5 | 0.026 | 50.0 | 0.244 | 27.5 | 0.439 |
| 0.4365 | 0.723 | 10.6 | 0.327 | 9.2 | 0.000 | CURVE 10 | | | |
| 0.4926 | 0.791 | 11.5 | 0.459 | 10.6 | 0.035 | T = 293. | | | |
| CURVE 8 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 0.0268 | 0.012 | 12.4 | 0.036 | 11.1 | 0.0713 | 2.0 | 0.100 | 34.3 | 0.363 |
| 0.0336 | 0.015 | 12.6 | 0.299 | 11.4 | 0.713 | 3.8 | 0.100 | 36.8 | 0.369 |
| 0.0355 | 0.022 | 13.2 | 0.363 | 11.9 | 0.914 | 4.6 | 0.100 | 41.4 | 0.369 |
| 0.0443 | 0.044 | 13.5 | 0.543 | 12.9 | 0.968 | 6.0 | 0.053 | 45.4 | 0.352 |
| 0.0474 | 0.044 | 13.8 | 0.576 | 13.2 | 0.991 | 7.6 | 0.638 | 50.0 | 0.340 |
| 0.0522 | 0.073 | 14.3 | 0.517 | 14.0 | 0.991 | 9.2 | 0.000 | | |
| 0.0553 | 0.087 | 15.3 | 0.428 | 15.1 | 0.944 | 10.5 | 0.000 | | |
| 0.0597 | 0.094 | 16.0 | 0.405 | 15.5 | 0.900 | 10.6 | 0.149 | | |
| 0.0640 | 0.097 | 16.6 | 0.442 | 15.6 | 0.804 | 11.0 | 0.351 | | |
| 0.0659 | 0.094 | 17.2 | 0.518 | 15.2 | 0.804 | 11.4 | 0.662 | | |
| 0.0713 | 0.085 | 17.7 | 0.552 | 16.7 | 0.705 | 11.7 | 0.841 | | |
| 0.0738 | 0.085 | 18.0 | 0.571 | 17.4 | 0.663 | 12.3 | 0.873 | | |
| 0.0786 | 0.094 | 18.7 | 0.571 | 17.6 | 0.494 | 13.2 | 0.909 | | |
| 0.0867 | 0.113 | 20.0 | 0.503 | 18.2 | 0.405 | 13.6 | 0.921 | | |
| 0.0896 | 0.116 | 21.0 | 0.451 | 19.3 | 0.258 | 14.5 | 0.930 | | |
| 0.0941 | 0.115 | 22.2 | 0.400 | 19.9 | 0.347 | 15.5 | 0.809 | | |
| 0.0985 | 0.120 | 23.5 | 0.364 | 20.5 | 0.265 | 16.0 | 0.825 | | |
| 0.109 | 0.134 | 25.1 | 0.320 | 20.9 | 0.227 | 16.8 | 0.590 | | |
| 0.116 | 0.146 | 26.6 | 0.300 | 21.0 | 0.790 | 17.7 | 0.543 | | |
| 0.126 | 0.172 | 28.7 | 0.274 | 21.5 | 0.876 | 18.5 | 0.410 | | |
| 0.131 | 0.175 | 31.0 | 0.259 | 22.3 | 0.771 | 19.0 | 0.303 | | |
| 0.153 | 0.127 | 33.6 | 0.234 | 22.6 | 0.616 | 19.5 | 0.375 | | |
| CURVE 9 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 2.0 | 0.093 | 35.0 | 0.227 | 23.9 | 0.461 | 19.9 | 0.485 | | |
| 3.8 | 0.098 | 41.4 | 0.226 | 25.7 | 0.414 | 20.4 | 0.430 | | |
| 4.5 | 0.098 | 46.6 | 0.244 | 26.4 | 0.502 | 20.8 | 0.781 | | |
| | | 47.8 | 0.265 | 27.4 | 0.441 | 21.2 | 0.853 | | |
| | | 48.8 | 0.308 | 28.6 | 0.399 | 21.6 | 0.882 | | |
| | | 50.0 | 0.339 | 30.0 | 0.362 | 22.1 | 0.859 | | |
| | | | | 30.0 | 0.364 | 22.6 | 0.798 | | |
| | | | | 30.5 | 0.364 | 23.0 | 0.727 | | |
| | | | | 40.9 | 0.351 | 23.8 | 0.657 | | |

e. Normal Spectral Absorptance (Wavelength Dependence)

A total of five sets of experimental data were located for the wavelength dependence of the normal spectral absorptance of aluminum oxide. This data is listed in Table 6-12 and shown in Figure 6-11. Specimen characterization and measurement information for the data are given in Table 6-11.

The data are all for wavelengths below 1 μm and, hence, no data evaluation is justified.

Since $\alpha = \epsilon$ by Kirchhoff's law (Eq. 2.3-7), the provisional values for normal spectral emittance of Coors AD 99 also apply to the normal spectral absorptance. See Table 6-1 for a listing of these provisional values and Figures 6-1, 6-2, and 6-3 for a graphical presentation.

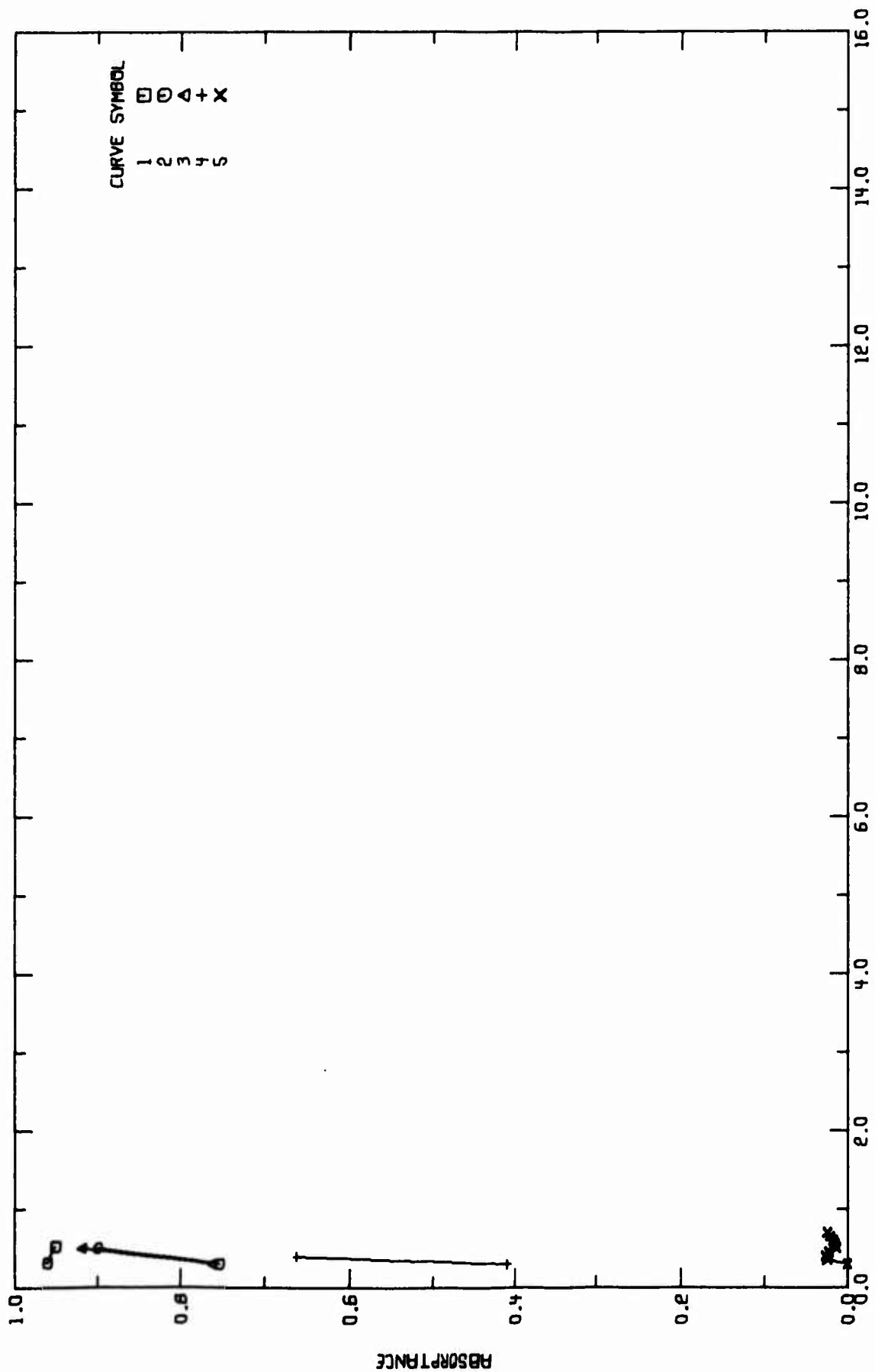


FIGURE 6-11. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

TABLE 6-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM OXIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T40412 | Schutt, J. B. and Macklin, B. A. | 1964 | 0.3-0.5 | 293 | | High purity γ - Al_2O_3 ; measured in vacuum; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$. |
| 2 T40412 | Schutt, J. B. and Macklin, B. A. | 1964 | 0.3-0.5 | 293 | | The above specimen except subjected to 50 solar actinic hr using Hanovia 673A high pressure mercury lamp in a vacion system. |
| 3 T40412 | Schutt, J. B. and Macklin, B. A. | 1964 | 0.3-0.5 | 293 | | High purity γ - Al_2O_3 ; slurried with 0.02 mole % H_2SO_4 , dried, pressed into a pellet; measured in vacuum; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$. |
| 4 T40412 | Schutt, J. B. and Macklin, B. A. | 1964 | 0.3-0.4 | 293 | | The above specimen except subjected to 50 solar actinic hr using Hanovia 673A high pressure mercury lamp in a vacion system. |
| 5 T40553 | Dube, C. W. | 1966 | 0.30-0.70 | 293 | Alucer MC | Compacted powder; data from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 0^\circ$. |

TABLE 6-12. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α |
|-----------|----------|
| CURVE 1 | |
| T = 293. | |
| 0.3 | 0.56 |
| 0.5 | 0.95 |
| CURVE 2 | |
| T = 293. | |
| 0.3 | 0.75 |
| 0.5 | 0.90 |
| CURVE 3 | |
| T = 293. | |
| 0.3 | 0.76 |
| 0.5 | 0.92 |
| CURVE 4 | |
| T = 293. | |
| 0.3 | 0.41 |
| 0.4 | 0.66 |
| CURVE 5 | |
| T = 293. | |
| 0.300 | 0.090 |
| 0.351 | 0.024 |
| 0.400 | 0.027 |
| 0.450 | 0.022 |
| 0.500 | 0.013 |
| 0.550 | 0.015 |
| 0.600 | 0.017 |
| 0.650 | 0.020 |
| 0.700 | 0.024 |

f. Normal Spectral Absorptance (Temperature Dependence)

No experimental data was found for the temperature dependence of the normal spectral absorptance of aluminum oxide.

By Kirchoff's law (Eq. 2.3-7) the provisional values for the temperature dependence of the normal spectral emittance are equal to the values for the temperature dependence of the normal spectral absorptance. See Table 6-4 for the listing of the provisional values and Figure 6-7 for a visual presentation.

g. Hemispherical Spectral Transmittance (Wavelength Dependence)

A total of 16 sets of experimental data were located for the wavelength dependence of the hemispherical spectral transmittance of aluminum oxide. These data are listed in Table 6-14 and shown in Figure 6-12. Specimen characterization and measurement information for the data are given in Table 6-13.

The data are all at room temperature and cover a wavelength range of 1 to 8 μm . The data are widely spaced, having come from tabular form, and drawing a smooth curve through the points for data evaluation is not justified. Lines are drawn between the data points in Figure 6-12 to aid in visualizing the data and do not imply a smooth curve connecting the data points.

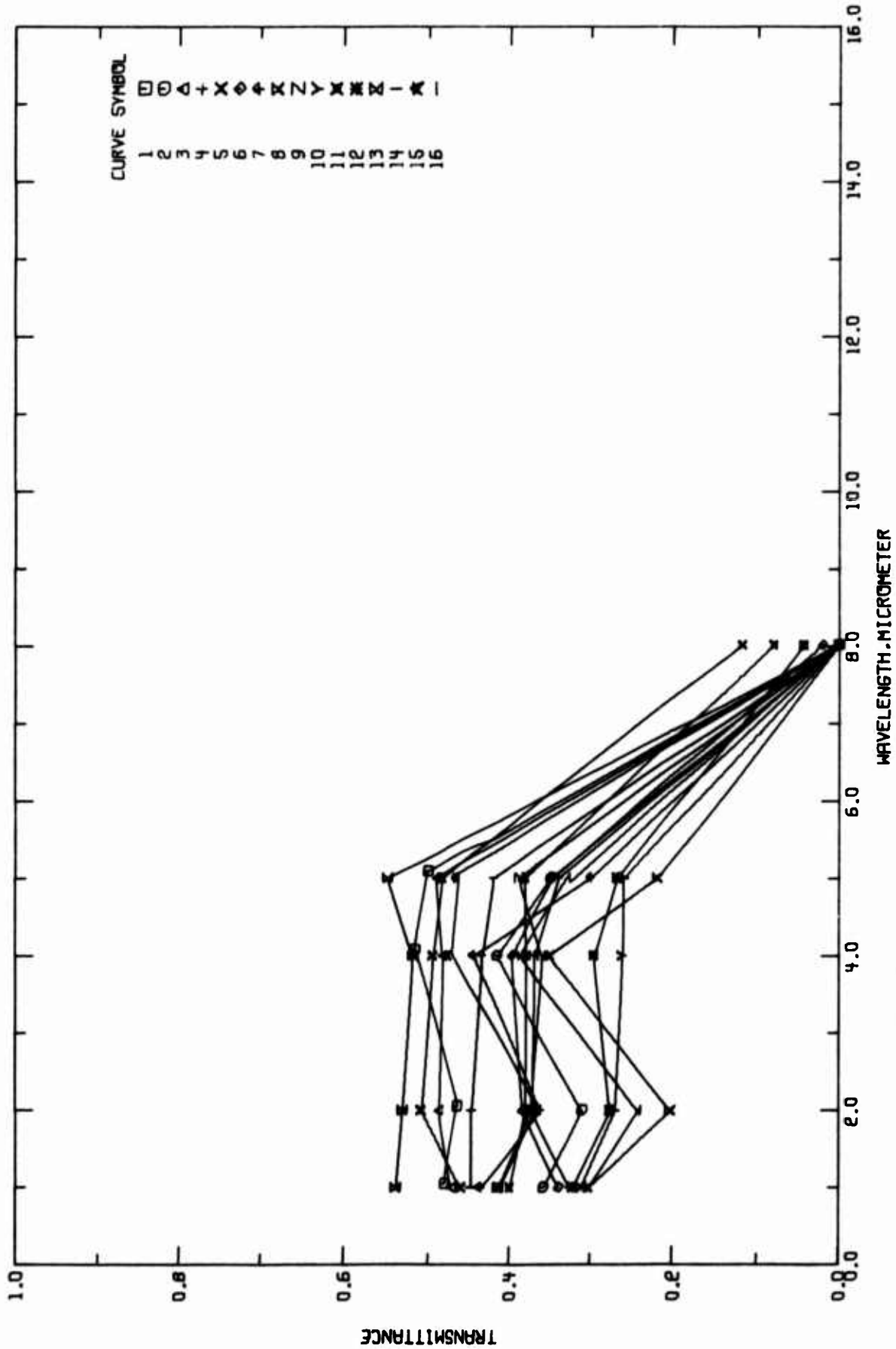


FIGURE 6-12. EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

TABLE 6-13. MEASUREMENT INFORMATION ON THE HEMISPHERICAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | McDaniel AV30 alumina | 96 pure; vitrified alumina; specimen 0.25 by 0.62 in. in cross section and 0.127 mm thick; measurement temperature not given explicitly, assumed to be 293 K; diffusing screen used in front of specimen; $\omega = 2\pi$, $\theta' \sim \theta$; reported error $\pm 5\%$. |
| 2 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | McDaniel AV30 alumina | Similar to the above specimen except 0.254 mm thick. |
| 3 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | McDaniel AP35 alumina, No. 3 | Similar to the above specimen except 99 pure and 0.127 mm thick. |
| 4 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | McDaniel AP35 alumina, No. 3 | Similar to the above specimen except 0.254 mm thick. |
| 5 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | McDaniel AP35 alumina, No. 4 | Similar to the above specimen except 0.127 mm thick. |
| 6 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | McDaniel AP35 alumina, No. 4 | Similar to the above specimen except 0.254 mm thick. |
| 7 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-85 alumina | Similar to the above specimen except 85 pure and 0.127 mm thick. |
| 8 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-85 alumina | Similar to the above specimen except 0.254 mm thick. |
| 9 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-94 alumina | Similar to the above specimen except 94 pure and 0.127 mm thick. |
| 10 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-94 alumina | Similar to the above specimen except 0.254 mm thick. |
| 11 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-96 alumina | Similar to the above specimen except 96 pure and 0.127 mm thick. |
| 12 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-96 alumina | Similar to the above specimen except 0.254 mm thick. |
| 13 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-99 alumina | Similar to the above specimen except 99 pure and 0.127 mm thick. |
| 14 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-99 alumina | Similar to the above specimen except 0.254 mm thick. |
| 15 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-96 alumina | Similar to the above specimen except 1 CoCO ₃ and 0.005 in. thick. |
| 16 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Coors AD-96 alumina | Similar to the above specimen except 0.010 in. thick. |

TABLE 6-14. EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T | λ | T | λ | T | λ | T |
|---------------------|-------|---------------------|-------|----------------------|-------|----------------------|-------|
| CURVE 1 T = 293. | | | | | | | |
| 1. | 0.490 | 5. | 0.483 | CURVE 10 T = 293. | | | |
| 2. | 0.453 | 8. | 0.119 | 1. | 0.312 | 5. | 0.420 |
| 4. | 0.517 | CURVE 6 T = 293. | | 2. | 0.270 | 8. | 0.000 |
| 5. | 0.501 | 1. | 0.338 | 4. | 0.261 | CURVE 15 T = 293. | |
| 8. | 0.000 | 2. | 0.383 | 5. | 0.259 | 1. | 0.415 |
| CURVE 2 T = 293. | | | | | | | |
| 1. | 0.357 | 4. | 0.397 | 8. | 0.000 | 2. | 0.370 |
| 2. | 0.310 | 5. | 0.346 | CURVE 11 T = 293. | | | |
| 4. | 0.410 | 8. | 0.020 | 1. | 0.400 | 4. | 0.476 |
| 5. | 0.348 | CURVE 7 T = 293. | | 2. | 0.390 | 5. | 0.466 |
| 8. | 0.000 | 1. | 0.435 | 5. | 0.378 | 8. | 0.000 |
| CURVE 3 T = 293. | | | | | | | |
| 1. | 0.470 | 2. | 0.360 | 6. | 0.380 | CURVE 16 T = 293. | |
| 2. | 0.487 | 4. | 0.443 | 8. | 0.080 | 1. | 0.306 |
| 4. | 0.462 | 5. | 0.300 | CURVE 12 T = 293. | | | |
| 5. | 0.490 | 8. | 0.000 | 1. | 0.322 | 2. | 0.237 |
| 8. | 0.000 | CURVE 8 T = 293. | | 2. | 0.276 | 4. | 0.390 |
| CURVE 4 T = 293. | | | | | | | |
| 1. | 0.325 | 1. | 0.303 | 5. | 0.296 | 5. | 0.326 |
| 2. | 0.371 | 2. | 0.202 | 8. | 0.043 | 8. | 0.000 |
| 4. | 0.369 | 4. | 0.350 | CURVE 13 T = 293. | | | |
| 5. | 0.339 | 5. | 0.216 | 1. | 0.539 | 2. | 0.531 |
| 8. | 0.000 | 8. | 0.000 | 2. | 0.531 | 4. | 0.519 |
| CURVE 5 T = 293. | | | | | | | |
| 1. | 0.456 | CURVE 9 T = 293. | | 5. | 0.548 | 5. | 0.548 |
| 2. | 0.509 | 1. | 0.414 | 8. | 0.000 | 8. | 0.000 |
| 4. | 0.495 | 2. | 0.373 | CURVE 14 T = 293. | | | |
| CURVE 5 T = 293. | | | | | | | |
| 1. | 0.456 | 4. | 0.358 | 1. | 0.446 | 1. | 0.446 |
| 2. | 0.509 | 5. | 0.388 | 2. | 0.445 | 2. | 0.445 |
| 4. | 0.495 | 8. | 0.000 | 4. | 0.433 | 4. | 0.433 |

h. Normal Spectral Transmittance (Wavelength Dependence)

A total of 18 sets of experimental data were located for the wavelength dependence of the normal spectral transmittance of aluminum oxide. These data are listed in Table 6-16 and shown in Figure 6-13. Specimen characterization and measurement information for the data are given in Table 6-15.

Because the data that are potentially useful are widely spaced, no evaluated data can be given. The lines connecting such data points do not imply a smooth curve.

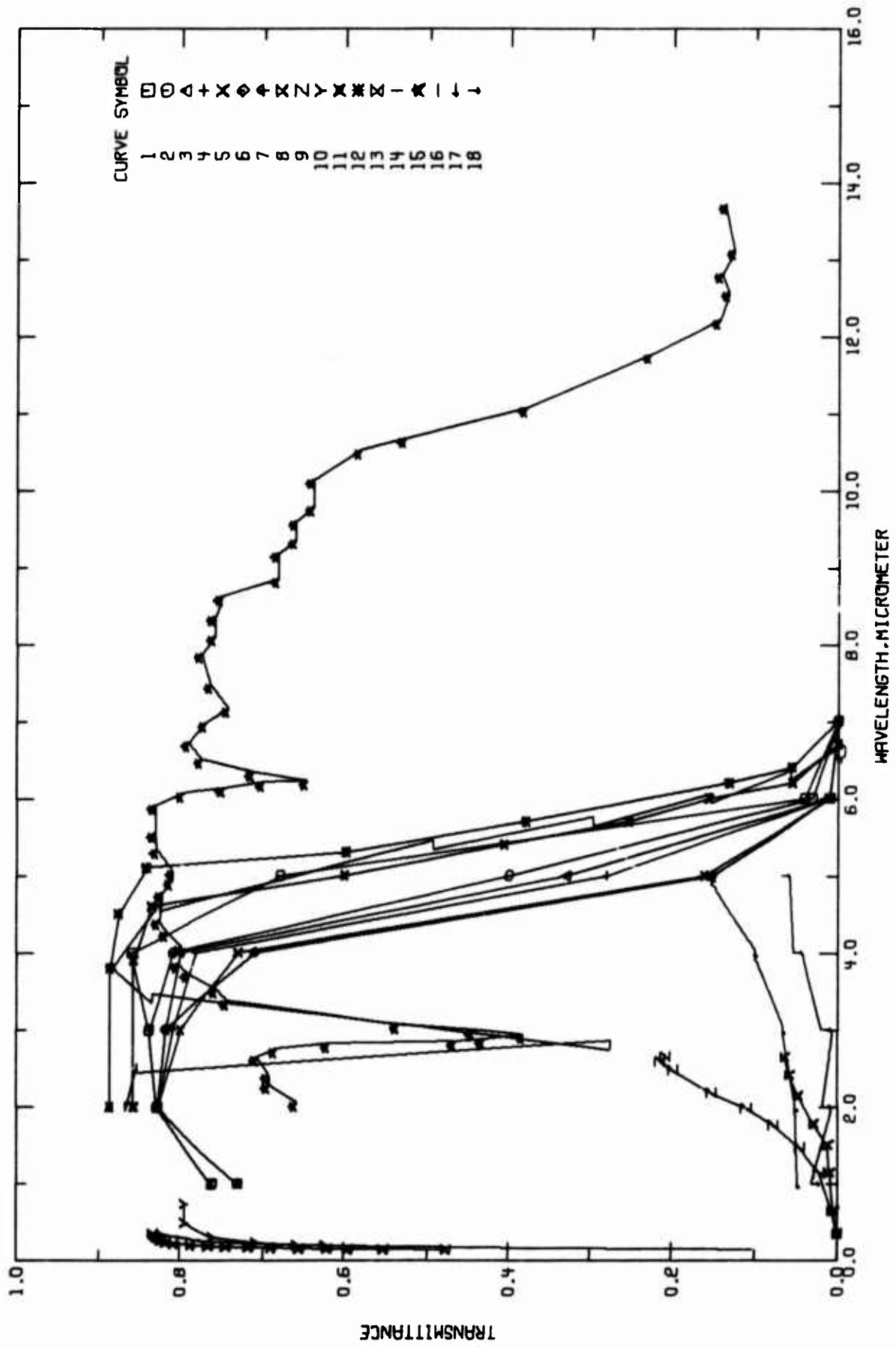


FIGURE 6-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE).

TABLE 6-15. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T29570 | Folweiler, R.C. | 1964 | 1-7 | 293 | Linde | Single crystal from Linde; specimen dimensions 0.125 by 0.5 by 1.5 in.; measurement temperature specified as room temperature, 293 K assigned; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$; reported error $\pm 5\%$. |
| 2 T29570 | Folweiler, R.C. | 1964 | 1-7 | 785 | Linde | The above specimen. |
| 3 T29570 | Folweiler, R.C. | 1964 | 1-7 | 960 | Linde | The above specimen. |
| 4 T29570 | Folweiler, R.C. | 1964 | 1-7 | 1177 | Linde | The above specimen. |
| 5 T29570 | Folweiler, R.C. | 1964 | 1-7 | 1411 | Linde | The above specimen. |
| 6 T29570 | Folweiler, R.C. | 1964 | 1-7 | 1567 | Linde | The above specimen. |
| 7 T29570 | Folweiler, R.C. | 1964 | 1-7 | 1671 | Linde | The above specimen. |
| 8 T24908 | Schätz, E.A. | 1966 | 0.35-2.7 | 293 | | >99 pure; specimen 0.0185 in. thick; compacted powder; compaction pressure 11 800 psi; smooth values from figure. |
| 9 T24908 | Schätz, E.A. | 1966 | 0.35-2.7 | 293 | | Similar to the above specimen except compaction pressure 75 500 psi. |
| 10 T34913 | Forestieri, A.F. and Grimes, H.H. | 1966 | 0.19-0.74 | 293 | | High purity $\alpha\text{-Al}_2\text{O}_3$; disc specimen 1/10 in. thick and 3/8 in. in diameter; c-axis 60° from the normal of the specimen surface; polished, notched for alignment purposes and annealed in air for 1 hr at 1773 K; surface reflections included; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 11 T36324 | McCarthy, D.E. | 1965 | 2.0-6.7 | 293 | Ruby | 0.05 Cr, essentially sapphire with the chromium impurity; synthetic; specimen 6.10 mm thick; flat to 10 fringes or better; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 12 T36324 | McCarthy, D.E. | 1965 | 2.0-7.0 | 293 | Sapphire | Synthetic; specimen 3.0 mm flat; flat to 10 fringes or better; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; lack of absorption band at 2.7 μ , compared to T30100 (see curve No. 39), attributed to this present specimen having impurities eliminated; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 13 T45481 | Boldt, G. | 1965 | 0.14-0.35 | 293 | | Specimen 0.5 mm thick; reflection losses included; smooth values from figure; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$. |
| 14 T45481 | Boldt, G. | 1965 | 0.14-0.35 | 293 | | Similar to the above specimen except 2 mm thick. |
| 15 T50470 | Brune, E.G., Jr., and Margrave, J.L., and Meloche, V.W. | 1957 | 2-16 | 293 | | 99% pure; rhombohedral crystal structure; disk 1 mm thick and 12 mm in diameter; Baird Associates Model B spectrophotometer used; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 16 T30100 | McCarthy, D.E. | 1953 | 2.0-6.6 | 293 | Sapphire | Synthetic; specimen 2 mm thick; ground and polished to a flatness of seven fringes or better; reference standard was aluminum mirror; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; Beckman IR-5A used in 2-16 μm range and Beckman IR-7 with CsI interchange used in 12.5-50 μm range; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 17 T39265 | Hobbs, H.A. and Folweiler, R.C. | 1966 | 1.0-5.0 | 293 | AD-995 | Author reports measured transmissivity; data from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$, $\omega' = 15/4^\circ$. |
| 18 T39265 | Hobbs, H.A. and Folweiler, R.C. | 1966 | 1.0-5.0 | 293 | AD-85 | Similar to the above specimen. |

TABLE 6-16. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|----------------------|--------|----------------------|--------|----------------------|--------|----------------------|--------|----------------------|--------|-----------|--------|-----------|--------|
| CURVE 1 T = 293. | | | | | | | | | | | | | |
| 1. | 0.76 | 7. | 0.00 | 1.149 | 0.009 | 6.0 | 0.154 | 0.144 | 0.107 | 3.60 | 0.606 | 8.79 | 0.688 |
| 2. | 0.83 | CURVE 5 T = 1411. | | 1.508 | 0.011 | 6.2 | 0.055 | 0.147 | 0.171 | 4.02 | 0.604 | 9.29 | 0.666 |
| 3. | 0.84 | 1. | 0.73 | 1.760 | 0.027 | 6.7 | 0.000 | 0.152 | 0.243 | 4.21 | 0.823 | 9.53 | 0.656 |
| 4. | 0.86 | 2. | 0.83 | 2.148 | 0.046 | CURVE 12 T = 293. | | 0.157 | 0.311 | 4.35 | 0.833 | 10.07 | 0.645 |
| 5. | 0.68 | 3. | 0.80 | 2.419 | 0.058 | 2.0 | 0.887 | 0.162 | 0.376 | 4.72 | 0.829 | 10.45 | 0.586 |
| 6. | 0.34 | 4. | 0.73 | 2.650 | 0.064 | 3.8 | 0.887 | 0.159 | 0.443 | 4.88 | 0.815 | 11.00 | 0.365 |
| 7. | 0.00 | 5. | 0.73 | CURVE 9 T = 293. | | 4.5 | 0.876 | 0.176 | 0.509 | 5.00 | 0.835 | 12.14 | 0.148 |
| CURVE 2 T = 785. | | | | | | | | | | | | | |
| 1. | 0.76 | 6. | 0.16 | 0.350 | 0.000 | 5.1 | 0.843 | 0.181 | 0.550 | 5.28 | 0.838 | 12.50 | 0.136 |
| 2. | 0.83 | 7. | 0.00 | 0.649 | 0.006 | 5.3 | 0.593 | 0.187 | 0.587 | 5.49 | 0.838 | 12.74 | 0.145 |
| 3. | 0.84 | CURVE 6 T = 1567. | | 1.147 | 0.021 | 5.7 | 0.379 | 0.192 | 0.617 | 6.01 | 0.832 | 13.04 | 0.129 |
| 4. | 0.81 | 1. | 0.75 | 1.475 | 0.045 | 6.2 | 0.130 | 0.198 | 0.646 | 6.08 | 0.752 | 13.63 | 0.140 |
| 5. | 0.40 | 2. | 0.73 | 1.765 | 0.079 | 6.4 | 0.056 | 0.206 | 0.678 | 6.15 | 0.756 | 14.26 | 0.124 |
| 6. | 0.03 | 3. | 0.63 | 1.984 | 0.110 | 7.0 | 0.000 | 0.223 | 0.728 | 6.20 | 0.718 | | |
| 7. | 0.00 | 4. | 0.71 | 2.185 | 0.151 | CURVE 13 T = 293. | | 0.233 | 0.746 | 6.45 | 0.778 | | |
| CURVE 3 T = 960. | | | | | | | | | | | | | |
| 1. | 0.76 | 5. | 0.15 | 2.479 | 0.199 | 0.144 | 0.476 | 0.248 | 0.766 | 6.67 | 0.795 | | |
| 2. | 0.82 | 6. | 0.01 | 2.593 | 0.215 | 0.147 | 0.552 | 0.261 | 0.779 | 6.92 | 0.773 | | |
| 3. | 0.80 | 7. | 0.0 | 2.650 | 0.208 | 0.149 | 0.595 | 0.289 | 0.793 | 7.11 | 0.746 | | |
| 4. | 0.33 | CURVE 7 T = 1671. | | CURVE 10 T = 293. | | 0.152 | 0.621 | 0.311 | 0.806 | 7.42 | 0.766 | | |
| 5. | 0.01 | 1. | 0.73 | 0.193 | 0.624 | 0.158 | 0.656 | 0.333 | 0.821 | 7.52 | 0.779 | | |
| 6. | 0.00 | 2. | 0.93 | 0.200 | 0.659 | 0.152 | 0.621 | 0.350 | 0.829 | 8.04 | 0.762 | | |
| 7. | 0.00 | 3. | 0.80 | 0.229 | 0.702 | 0.158 | 0.691 | CURVE 15 T = 293. | | 8.30 | 0.762 | | |
| CURVE 4 T = 1177. | | | | | | | | | | | | | |
| 1. | 0.73 | 4. | 0.52 | 0.191 | 0.794 | 0.165 | 0.691 | 2.00 | 0.664 | 8.56 | 0.754 | | |
| 2. | 0.83 | 5. | 0.15 | 0.204 | 0.808 | 0.173 | 0.718 | 2.23 | 0.699 | 8.79 | 0.688 | | |
| 3. | 0.81 | 6. | 0.01 | 0.222 | 0.819 | 0.182 | 0.744 | 2.36 | 0.699 | 9.12 | 0.688 | | |
| 4. | 0.28 | 7. | 0.00 | 0.239 | 0.825 | 0.191 | 0.764 | 2.59 | 0.713 | 9.29 | 0.666 | | |
| 5. | 0.01 | CURVE 8 T = 293. | | 0.266 | 0.829 | 0.204 | 0.808 | 2.70 | 0.690 | 9.53 | 0.656 | | |
| 6. | 0.01 | 1. | 0.73 | 0.301 | 0.858 | 0.222 | 0.819 | 2.76 | 0.625 | 9.72 | 0.645 | | |
| CURVE 5 T = 293. | | | | | | | | | | | | | |
| 1. | 0.73 | 2. | 0.83 | 0.326 | 0.833 | 0.239 | 0.819 | 2.92 | 0.470 | 10.45 | 0.586 | | |
| 2. | 0.83 | 3. | 0.81 | 0.350 | 0.800 | 0.266 | 0.825 | 2.98 | 0.436 | 10.60 | 0.533 | | |
| 3. | 0.78 | 4. | 0.78 | 0.650 | 0.004 | 0.301 | 0.829 | 3.01 | 0.386 | 10.87 | 0.533 | | |
| 4. | 0.78 | 5. | 0.28 | 0.650 | 0.004 | 0.326 | 0.833 | 3.04 | 0.340 | 11.00 | 0.533 | | |
| 5. | 0.28 | 6. | 0.01 | | | 0.350 | 0.835 | 3.32 | 0.240 | 11.69 | 0.533 | | |
| 6. | 0.01 | | | | | | | 3.48 | 0.148 | 12.14 | 0.533 | | |
| | | | | | | | | 3.68 | 0.136 | 12.50 | 0.533 | | |
| | | | | | | | | | 0.145 | 12.74 | 0.533 | | |
| | | | | | | | | | 0.129 | 13.04 | 0.533 | | |
| | | | | | | | | | 0.140 | 13.63 | 0.533 | | |
| | | | | | | | | | 0.124 | 14.26 | 0.533 | | |

TABLE 6-1b. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ALUMINUM OXIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T |
|------------------|--------|
| CURVE 15 (CONT.) | |
| 14.65 | 0.145 |
| 14.94 | 0.172 |
| 15.43 | 0.225 |
| 15.74 | 0.280 |
| 16.00 | 0.349 |
| CURVE 16 | |
| T = 293. | |
| 2.0 | 0.869 |
| 2.5 | 0.855 |
| 2.3 | 0.275 |
| 3.4 | 0.835 |
| 3.8 | 0.883 |
| 4.6 | 0.827 |
| 5.4 | 0.494 |
| 5.7 | 3.297 |
| 6.0 | 0.152 |
| 6.3 | 0.357 |
| 6.6 | 0.000 |
| CURVE 17 | |
| T = 293. | |
| 1.00 | 0.047 |
| 2.00 | 0.050 |
| 3.00 | 0.055 |
| 4.00 | 0.100 |
| 4.97 | 0.150 |
| CURVE 18 | |
| T = 293. | |
| 1.00 | 0.0254 |
| 2.00 | 0.0126 |
| 3.00 | 0.0115 |
| 4.00 | 0.0462 |
| 5.00 | 0.0029 |

4.7. Boron Nitride

Boron nitride is a material that is man-made and has no counterpart in nature. It exists in several forms. There is a soft hexagonal form, a hard cubic form, and a hard hexagonal form. Pure boron nitride sublimates at 3273 K and 1 atmosphere while the commercial forms sublime at 3003 K and one atmosphere [E12808].

The soft hexagonal form has a layer-lattice structure similar to graphite. It can be made in two ways. One method of manufacture is by hot pressing. The second method is by chemical vapor deposition (CVD) with this type also known as pyrolytic boron nitride.

The hard cubic form has a zincblende structure. The density is 3.45 g cm^{-3} [A00014]. Borazon, a trademark of the General Electric Company, is cubic boron nitride manufactured by the GE Specialty Materials Department, Worthington, Ohio. The Russian names for cubic boron nitride are Elbor and Cubonite. The cubic form is harder than diamond and is probably the hardest material on earth.

The hard hexagonal form has a wurtzite structure and only small amounts have been synthesized.

The application of boron nitride includes furnace insulation, high temperature lubrication (the graphite-like form), dielectrics, wave guides, heat shields for plasmas, and nose cone windows.

a. Normal Spectral Emittance (Wavelength Dependence)

A total of 19 sets of experimental data were located for the wavelength dependence of the normal spectral emittance of boron nitride. The data are listed in Table 7-3 and shown in Figures 7-1 and 7-2. Specimen characterization and measurement information for the data are given in Table 7-2.

Seven sets of data are for pyrolytic boron nitride (curves 11-17) specimens manufactured by High Temperature Materials, Inc., of Lowell, Massachusetts. Only for three data sets (curves 15-17) were specimen dimensions given. These three data sets cover a temperature range of 1280 to 2020 K and are very close to each other. A set of provisional values is, therefore, based on curves 15, 16, and 17 with these values valid within the following context: a 0.5 in. thick specimen of polished pyrolytic boron nitride manufactured by High Temperature Materials, Inc., with the surface parallel to the basal planes radiating. The values, within an uncertainty of 15%, hold for temperatures of 1280, 1670, and 2020 K. The provisional values are listed in Table 7-1 and shown in Figure 7-1.

Four sets of data (curves 7, 8, 10, and 18) are for 97% pure boron nitride manufactured by the Carborundum Corporation. The material for curve 9 reported by Browning, [T37476] had a density close to the density of the material for curves 7, 8, 10, and 18 and was, therefore, probably 97% pure.

The crystal structure for the remaining data sets was not reported and, therefore, these sets cannot be used for developing evaluated data.

TABLE 7-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| 2.5 | 0.759 | 6.3 | 0.848 | 9.6 | 0.834 | 13.2 | 0.834 |
| 2.6 | 0.762 | 6.4 | 0.808 | 9.7 | 0.838 | 13.3 | 0.841 |
| 2.7 | 0.765 | 6.5 | 0.754 | 9.8 | 0.842 | 13.4 | 0.847 |
| 2.8 | 0.770 | 6.6 | 0.680 | 9.9 | 0.845 | 13.5 | 0.853 |
| 2.9 | 0.774 | 6.7 | 0.620 | 10.0 | 0.848 | 13.6 | 0.858 |
| 3.0 | 0.778 | 6.8 | 0.535 | 10.1 | 0.851 | 13.7 | 0.863 |
| 3.1 | 0.781 | 6.9 | 0.480 | 10.2 | 0.854 | 13.8 | 0.868 |
| 3.2 | 0.785 | 7.0 | 0.442 | 10.3 | 0.857 | 13.9 | 0.872 |
| 3.3 | 0.789 | 7.05 | 0.422 | 10.4 | 0.860 | 14.0 | 0.876 |
| 3.4 | 0.792 | 7.12 | 0.404 | 10.5 | 0.863 | 14.1 | 0.880 |
| 3.5 | 0.796 | 7.15 | 0.389 | 10.6 | 0.866 | 14.2 | 0.884 |
| 3.6 | 0.799 | 7.20 | 0.377 | 10.7 | 0.869 | 14.3 | 0.888 |
| 3.7 | 0.803 | 7.25 | 0.371 | 10.8 | 0.872 | 14.4 | 0.892 |
| 3.8 | 0.806 | 7.30 | 0.369 | 10.9 | 0.875 | 14.5 | 0.896 |
| 3.9 | 0.810 | 7.35 | 0.370 | 11.0 | 0.878 | 14.6 | 0.900 |
| 4.0 | 0.814 | 7.40 | 0.377 | 11.1 | 0.881 | 14.7 | 0.904 |
| 4.1 | 0.819 | 7.45 | 0.387 | 11.2 | 0.884 | 14.8 | 0.907 |
| 4.2 | 0.824 | 7.50 | 0.400 | 11.3 | 0.887 | 14.9 | 0.911 |
| 4.3 | 0.831 | 7.55 | 0.416 | 11.4 | 0.890 | 15.0 | 0.914 |
| 4.4 | 0.839 | 7.60 | 0.443 | 11.5 | 0.893 | | |
| 4.5 | 0.848 | 7.70 | 0.495 | 11.6 | 0.896 | | |
| 4.6 | 0.856 | 7.8 | 0.543 | 11.7 | 0.898 | | |
| 4.7 | 0.865 | 7.9 | 0.592 | 11.8 | 0.900 | | |
| 4.8 | 0.874 | 8.0 | 0.651 | 11.9 | 0.902 | | |
| 4.9 | 0.884 | 8.1 | 0.690 | 12.0 | 0.903 | | |
| 5.0 | 0.892 | 8.2 | 0.718 | 12.1 | 0.904 | | |
| 5.1 | 0.901 | 8.3 | 0.737 | 12.2 | 0.904 | | |
| 5.2 | 0.909 | 8.4 | 0.752 | 12.3 | 0.904 | | |
| 5.3 | 0.916 | 8.5 | 0.763 | 12.4 | 0.904 | | |
| 5.4 | 0.924 | 8.6 | 0.774 | 12.5 | 0.903 | | |
| 5.5 | 0.931 | 8.7 | 0.783 | 12.6 | 0.900 | | |
| 5.6 | 0.935 | 8.8 | 0.791 | 12.7 | 0.889 | | |
| 5.7 | 0.938 | 8.9 | 0.798 | 12.8 | 0.871 | | |
| 5.8 | 0.943 | 9.0 | 0.805 | 12.9 | 0.847 | | |
| 5.9 | 0.939 | 9.1 | 0.811 | 12.95 | 0.833 | | |
| 6.0 | 0.935 | 9.2 | 0.816 | 12.95 | 0.829 | | |
| 6.05 | 0.930 | 9.3 | 0.820 | 13.0 | 0.828 | | |
| 6.1 | 0.921 | 9.4 | 0.825 | 13.05 | 0.827 | | |
| 6.2 | 0.890 | 9.5 | 0.830 | 13.1 | 0.828 | | |

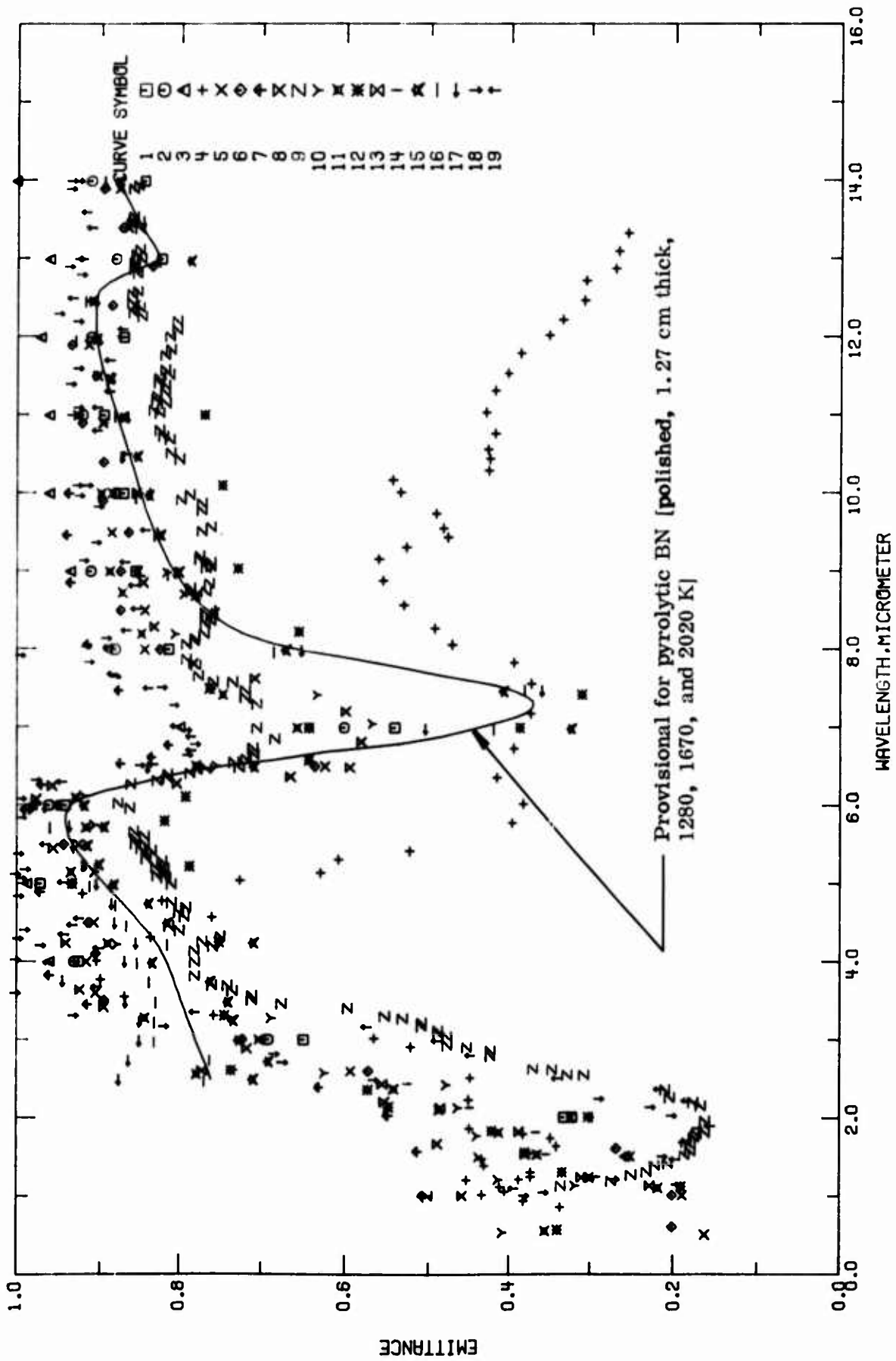


FIGURE 7-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

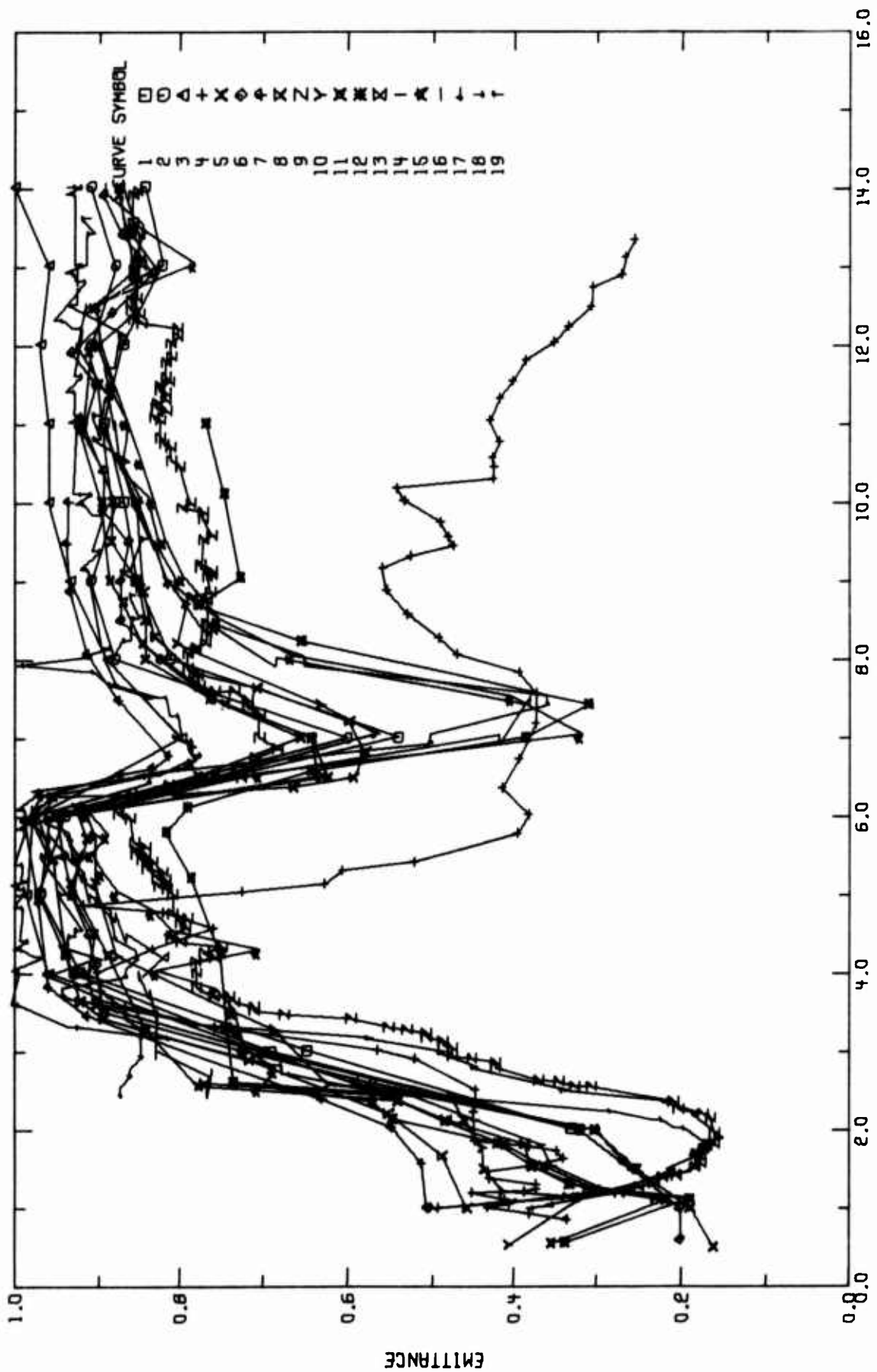


FIGURE 7-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 7-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T16606 | Blau, H. H., Jr., Marsh, J. B., Martin, W. S., Jasperse, J. R., and Chaffee, E. | 1960 | 2-14 | 873 | | Measured in air; measurements made with Perkin-Elmer Model 12C Infrared Spectrometer with sodium chloride prism; data from figure; $\theta' = 0^\circ$; reported error $\pm 4\%$. |
| 2 T16606 | Blau, H. H., Jr., et al. | 1960 | 2-14 | 1083 | | Similar to the above specimen. |
| 3 T16606 | Blau, H. H., Jr., et al. | 1960 | 1.5-14 | 1353 | | Similar to the above specimen. |
| 4 T16606 | Blau, H. H., Jr., et al. | 1960 | 0.85-13 | 2273 | | Specimen heated in air; solar furnace used in attempt to measure spectral reflectance in 1273-3273 K region; data not accurate; data from figure; $\theta' = 0^\circ$. |
| 5 T26088 | Walker, G. H. and Casey, F. W., Jr. | 1962 | 0.5-15 | 1033 | | Specimen 0.643 cm thick and in form of a semicircle; pressed; machined from 10.15 cm diameter round stock, initial specimens carefully polished on decreasing grits of emery paper to insure a uniform surface, dried at 373 K to remove any absorbed water; $\theta' = 0^\circ$. |
| 6 T26066 | Walker, G. H. and Casey, F. W., Jr. | 1962 | 0.6-15 | 1033 | | The above specimen, second test. |
| 7 T25502 | Grenis, A. F. and Levitt, A. P. | 1965 | 1-10 | 1300 | | 97.00 BN, 2.40 B ₂ O ₃ , 0.20 Al ₂ O ₃ and SiO ₂ , 0.10 alkaline earth oxides, and 0.008 C; hexagonal crystal structure; machine finished; from Carborundum Co., New Products Branch, Niagara Falls, N. Y.; surface roughness 110 μ in.; bulk density 2.15 g cm ⁻³ ; measured in vacuum of 35 to 50 μ of pressure; smooth values from figure; $\theta' = 0^\circ$. |
| 8 T25502 | Grenis, A. F. and Levitt, A. P. | 1965 | 1-10 | 1300 | | Similar to the above specimen except surface finished by polishing with silk cloth. |
| 9 T27478 | Browning, M. E. | 1963 | 1.0-15 | 1273 | | Sintered; from Carborundum Corp.; density 2.09 g cm ⁻³ ; reference standard NiO; smooth values from figure; $\theta' = 0^\circ$; reported error $\pm 5\%$. |
| 10 T25246 | Audio, G. W. and Scala, E. | 1968 | 0.53-11 | 1098 | | 97.0 BN, 2.40 methanol soluble borate, 0.10 alkaline earth oxides, 0.20 alumina and silica, and 0.008 carbon, polycrystal; hot-pressed; fabricated by Carborundum Co.; surfaces mechanically polished; density 2.1 g cm ⁻³ ; specimen temperature between 1093 and 1103 K; measured in purified hydrogen atm; probing technique used for measurement; data from figure; $\theta' = 0^\circ$. |
| 11 T25246 | Audio, G. W. and Scala, E. | 1968 | 0.55-11 | 1098 | Pyrolytic | Purity < 0.0010 total metallic impurities; measured from A-face (c-axis parallel to surface of (1010) faces); pyrolytic, made by vapor deposition process; prepared by High Temperature Materials, Inc.; surface mechanically polished; density ~ 2.2 g cm ⁻³ ; specimen temperature between 1093 and 1103 K; measured in purified hydrogen atm; probing technique used; data from figure; $\theta' = 0^\circ$. |
| 12 T25246 | Audio, G. W. and Scala, E. | 1968 | 0.56-11 | 1098 | Pyrolytic | Similar to the above specimen and conditions except measured from C-face (a-axis parallel to surface of (0001) face). |
| 13 T25246 | Audio, G. W. and Scala, E. | 1968 | 1.1-2.6 | 1103 | Pyrolytic | Similar to the above specimen and conditions except measured from A-face and polarizer axis parallel to c-axis. |
| 14 T25246 | Audio, G. W. and Scala, E. | 1968 | 1.1-2.6 | 1103 | Pyrolytic | Similar to the above specimen and conditions except polarizer axis perpendicular to c-axis. |

TABLE 7-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 15 T34724 | Durand, J. L. and Houston, K. C. | 1966 | 2.5-15 | ~1280 | Pyrolytic | Specimen size about 2 x 3 x 0.5 in.; manufactured by High Temperature Materials, Inc., Lowell, Mass.; surface polished to a 4-6 μm finish; AB surface (surface parallel to basal planes or planes of deposition) radiating; Beckman IR-9 spectrophotometer used; data from figure; $\theta' = 0^\circ$. Similar to the above specimen. |
| 16 T34724 | Durand, J. L. and Houston, K. C. | 1966 | 2.5-15 | 1670 | Pyrolytic | Similar to the above specimen. |
| 17 T34724 | Durand, J. L. and Houston, K. C. | 1966 | 2.5-15 | 2020 | Pyrolytic | Similar to the above specimen. |
| 18 T22272 | Schatz, E. A., Goldberg, D. M., Pearson, E. G., and Surks, T. L. | 1963 | 1-15 | 1273 | Sample No. 97 | 97 pure; sintered by Carborundum Co.; thickness 50 mils; density 2.09 g cm ⁻³ , theoretical density 2.27 g cm ⁻³ ; smooth values from figure; $\theta' = 0^\circ$. |
| 19 T22272 | Schatz, E. A., et al. | 1963 | 1-15 | 1223 | Sample No. 98 | 100 pure; sintered at 2123 K for 2 hr, sinter material BN; density 2.00 g cm ⁻³ , theoretical density 2.27 g cm ⁻³ ; smooth values from figure; $\theta' = 0^\circ$. |

TABLE 7-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|----------------|------------|----------------|------------|------------------------|------------|------------------------|------------|----------------|------------|
| CURVE 1 | | CURVE 2 | | CURVE 3 (CONT.) | | CURVE 4 (CONT.) | | CURVE 5 | |
| T = 873. | | T = 1083. | | T = 2273. | | T = 1033. | | T = 1300. | |
| 2.00 | 0.330 | 2.00 | 0.332 | 6.00 | 0.980 | 4.87 | 0.920 | 0.500 | 0.162 |
| 3.00 | 0.648 | 3.00 | 0.69 | 7.00 | 0.798 | 5.04 | 0.725 | 1.00 | 0.189 |
| 4.00 | 0.924 | 4.00 | 0.93 | 8.00 | 0.890 | 5.14 | 0.628 | 1.50 | 0.251 |
| 5.00 | 0.970 | 5.00 | 0.97 | 9.00 | 0.935 | 5.31 | 0.607 | 2.00 | 0.301 |
| 6.00 | 0.940 | 6.00 | 0.96 | 10.0 | 0.960 | 5.42 | 0.523 | 2.50 | 0.592 |
| 7.00 | 0.540 | 7.00 | 0.96 | 11.0 | 0.960 | 5.78 | 0.396 | 3.00 | 0.702 |
| 8.00 | 0.812 | 8.00 | 0.91 | 12.0 | 0.970 | 6.02 | 0.382 | 3.50 | 0.904 |
| 9.00 | 0.855 | 9.00 | 0.88 | 13.0 | 0.960 | 6.36 | 0.415 | 4.00 | 0.915 |
| 10.0 | 0.870 | 10.0 | 0.88 | 14.0 | 1.000 | 6.73 | 0.394 | 4.50 | 0.906 |
| 11.0 | 0.894 | 11.0 | 0.88 | CURVE 4 | | 7.18 | 0.373 | 5.00 | 0.933 |
| 12.0 | 0.870 | 12.0 | 0.88 | T = 2273. | | 7.56 | 0.372 | 5.50 | 0.925 |
| 13.0 | 0.822 | 13.0 | 0.88 | 0.85 | 0.335 | 8.06 | 0.471 | 6.00 | 0.952 |
| 14.0 | 0.844 | 14.0 | 0.88 | 0.93 | 0.381 | 8.27 | 0.491 | 6.50 | 0.623 |
| CURVE 3 | | CURVE 7 | | CURVE 6 (CONT.) | | CURVE 7 | | CURVE 8 | |
| T = 1353. | | T = 1273. | | T = 1300. | | T = 1300. | | T = 1300. | |
| 1.50 | 0.257 | 1.50 | 0.507 | 3.50 | 0.894 | 3.50 | 0.894 | 7.47 | 0.076 |
| 2.00 | 0.320 | 2.00 | 0.513 | 4.10 | 0.904 | 4.10 | 0.904 | 8.06 | 0.914 |
| 3.00 | 0.700 | 3.00 | 0.548 | 4.50 | 0.913 | 4.50 | 0.913 | 8.06 | 0.935 |
| 4.00 | 0.960 | 4.00 | 0.630 | 5.00 | 0.933 | 5.00 | 0.933 | 9.47 | 0.939 |
| 5.00 | 0.986 | 5.00 | 0.914 | 5.50 | 0.943 | 5.50 | 0.943 | 10.0 | 0.937 |
| 6.00 | 0.974 | 6.00 | 0.960 | 6.00 | 0.950 | 6.00 | 0.950 | CURVE 8 | |
| 7.00 | 0.874 | 7.00 | 0.960 | 6.50 | 0.635 | 6.50 | 0.635 | T = 1300. | |
| 8.00 | 0.822 | 8.00 | 0.960 | 7.00 | 0.642 | 7.00 | 0.642 | 1.00 | 0.450 |
| 9.00 | 0.855 | 9.00 | 0.960 | 7.50 | 0.761 | 7.50 | 0.761 | 1.67 | 0.488 |
| 10.0 | 0.870 | 10.0 | 0.960 | 8.00 | 0.824 | 8.00 | 0.824 | 2.21 | 0.552 |
| 11.0 | 0.894 | 11.0 | 0.960 | 8.50 | 0.874 | 8.50 | 0.874 | 2.89 | 0.716 |
| 12.0 | 0.870 | 12.0 | 0.960 | 9.00 | 0.874 | 9.00 | 0.874 | 3.42 | 0.894 |
| 13.0 | 0.822 | 13.0 | 0.960 | 9.50 | 0.864 | 9.50 | 0.864 | 3.64 | 0.923 |
| 14.0 | 0.844 | 14.0 | 0.960 | 10.4 | 0.896 | 10.4 | 0.896 | 4.24 | 0.940 |
| CURVE 3 | | CURVE 9 | | CURVE 7 | | CURVE 8 | | CURVE 9 | |
| T = 1353. | | T = 1273. | | T = 1300. | | T = 1300. | | T = 1273. | |
| 1.50 | 0.257 | 1.50 | 0.507 | 10.9 | 0.921 | 10.9 | 0.921 | 6.49 | 0.593 |
| 2.00 | 0.320 | 2.00 | 0.513 | 11.5 | 0.904 | 11.5 | 0.904 | 6.82 | 0.579 |
| 3.00 | 0.700 | 3.00 | 0.548 | 11.9 | 0.934 | 11.9 | 0.934 | 7.21 | 0.598 |
| 4.00 | 0.960 | 4.00 | 0.630 | 12.4 | 0.865 | 12.4 | 0.865 | 7.63 | 0.707 |
| 5.00 | 0.986 | 5.00 | 0.914 | 12.9 | 0.834 | 12.9 | 0.834 | 7.82 | 0.782 |
| 6.00 | 0.974 | 6.00 | 0.960 | 13.4 | 0.872 | 13.4 | 0.872 | 8.29 | 0.831 |
| 7.00 | 0.874 | 7.00 | 0.960 | 13.9 | 0.895 | 13.9 | 0.895 | 8.86 | 0.845 |
| 8.00 | 0.822 | 8.00 | 0.960 | 14.4 | 0.875 | 14.4 | 0.875 | 10.0 | 0.854 |
| 9.00 | 0.855 | 9.00 | 0.960 | 14.9 | 0.894 | 14.9 | 0.894 | CURVE 9 | |
| 10.0 | 0.870 | 10.0 | 0.960 | CURVE 7 | | CURVE 8 | | T = 1273. | |
| 11.0 | 0.894 | 11.0 | 0.960 | T = 1300. | | T = 1300. | | 1.00 | 0.500 |
| 12.0 | 0.870 | 12.0 | 0.960 | 1.57 | 0.513 | 1.57 | 0.513 | 1.13 | 0.334 |
| 13.0 | 0.822 | 13.0 | 0.960 | 2.03 | 0.548 | 2.03 | 0.548 | 1.19 | 0.273 |
| 14.0 | 0.844 | 14.0 | 0.960 | 2.39 | 0.630 | 2.39 | 0.630 | 1.27 | 0.250 |
| CURVE 3 | | CURVE 9 | | CURVE 7 | | CURVE 8 | | CURVE 9 | |
| T = 1353. | | T = 1273. | | T = 1300. | | T = 1300. | | T = 1273. | |
| 1.50 | 0.257 | 1.50 | 0.507 | 3.45 | 0.914 | 3.45 | 0.914 | 1.31 | 0.232 |
| 2.00 | 0.320 | 2.00 | 0.513 | 3.82 | 0.960 | 3.82 | 0.960 | 1.39 | 0.222 |
| 3.00 | 0.700 | 3.00 | 0.548 | 4.89 | 0.971 | 4.89 | 0.971 | 1.41 | 0.206 |
| 4.00 | 0.960 | 4.00 | 0.630 | 5.94 | 0.988 | 5.94 | 0.988 | | |
| 5.00 | 0.986 | 5.00 | 0.914 | 6.26 | 0.969 | 6.26 | 0.969 | | |
| | | | | 6.53 | 0.874 | 6.53 | 0.874 | | |
| | | | | 6.61 | 0.834 | 6.61 | 0.834 | | |
| | | | | 6.77 | 0.813 | 6.77 | 0.813 | | |

TABLE 7-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μms ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|------------------|
| CURVE 9 (CONT.) | CURVE 9 (CONT.) | CURVE 9 (CONT.) | CURVE 9 (CONT.) | CURVE 9 (CONT.) | CURVE 9 (CONT.) | CURVE 10 (CONT.) | CURVE 10 (CONT.) | CURVE 10 (CONT.) | CURVE 10 (CONT.) | CURVE 11 (CONT.) | CURVE 11 (CONT.) | CURVE 11 (CONT.) | CURVE 11 (CONT.) |
| 1.52 | 0.185 | 4.40 | 0.799 | 7.59 | 0.734 | 11.47 | 0.626 | 1.50 | 0.437 | 9.00 | 0.607 | 9.00 | 0.607 |
| 1.57 | 0.178 | 4.46 | 0.812 | 7.59 | 0.758 | 11.52 | 0.813 | 1.77 | 0.439 | 10.0 | 0.897 | 10.0 | 0.897 |
| 1.65 | 0.178 | 4.58 | 0.793 | 7.65 | 0.776 | 11.58 | 0.818 | 2.13 | 0.463 | 11.0 | 0.926 | 11.0 | 0.926 |
| 1.69 | 0.183 | 4.64 | 0.800 | 7.80 | 0.779 | 11.77 | 0.818 | 2.43 | 0.477 | CURVE 12 | | | |
| 1.75 | 0.174 | 4.70 | 0.791 | 7.88 | 0.791 | 11.84 | 0.811 | 2.58 | 0.623 | T = 1098. | | | |
| 1.79 | 0.171 | 4.76 | 0.809 | 8.07 | 0.781 | 12.01 | 0.812 | 3.28 | 0.687 | 0.560 | 0.338 | 0.560 | 0.338 |
| 1.81 | 0.161 | 5.00 | 0.809 | 9.11 | 0.781 | 12.09 | 0.803 | 4.22 | 0.878 | 1.12 | 0.190 | 1.12 | 0.190 |
| 1.96 | 0.166 | 5.11 | 0.827 | 8.15 | 0.769 | 12.20 | 0.803 | 5.15 | 0.905 | 1.30 | 0.332 | 1.30 | 0.332 |
| 2.15 | 0.166 | 5.11 | 0.827 | 8.20 | 0.769 | 12.26 | 0.848 | 5.75 | 0.905 | 1.55 | 0.376 | 1.55 | 0.376 |
| 2.20 | 0.175 | 5.15 | 0.818 | 8.33 | 0.768 | 12.31 | 0.859 | 6.12 | 0.918 | 1.83 | 0.420 | 1.83 | 0.420 |
| 2.26 | 0.203 | 5.20 | 0.818 | 8.37 | 0.768 | 12.31 | 0.859 | 6.51 | 0.753 | 2.14 | 0.547 | 2.14 | 0.547 |
| 2.36 | 0.209 | 5.21 | 0.829 | 8.45 | 0.766 | 12.44 | 0.861 | 7.05 | 0.566 | 2.36 | 0.571 | 2.36 | 0.571 |
| 2.55 | 0.306 | 5.29 | 0.821 | 8.74 | 0.767 | 12.55 | 0.861 | 7.42 | 0.632 | 3.31 | 0.743 | 3.31 | 0.743 |
| 2.55 | 0.326 | 5.33 | 0.841 | 8.75 | 0.786 | 12.58 | 0.854 | 8.20 | 0.604 | 4.25 | 0.750 | 4.25 | 0.750 |
| 2.62 | 0.345 | 5.38 | 0.841 | 8.79 | 0.763 | 12.61 | 0.854 | 8.71 | 0.793 | 5.22 | 0.786 | 5.22 | 0.786 |
| 2.63 | 0.369 | 5.42 | 0.834 | 8.85 | 0.763 | 12.87 | 0.858 | 8.99 | 0.815 | 5.80 | 0.817 | 5.80 | 0.817 |
| 2.80 | 0.423 | 5.45 | 0.848 | 9.05 | 0.767 | 12.95 | 0.858 | 10.0 | 0.852 | 6.11 | 0.791 | 6.11 | 0.791 |
| 2.86 | 0.423 | 5.51 | 0.843 | 9.07 | 0.761 | 13.00 | 0.849 | 10.9 | 0.895 | 6.50 | 0.642 | 6.50 | 0.642 |
| 2.91 | 0.453 | 5.52 | 0.855 | 9.12 | 0.761 | 13.06 | 0.856 | CURVE 11 | | | | | |
| 2.94 | 0.477 | 5.57 | 0.855 | 9.16 | 0.775 | 13.12 | 0.851 | T = 1098. | | | | | |
| 3.05 | 0.477 | 5.61 | 0.843 | 9.20 | 0.775 | 13.39 | 0.851 | 0.550 | 0.354 | 7.00 | 0.386 | 7.00 | 0.386 |
| 3.09 | 0.488 | 5.67 | 0.857 | 9.52 | 0.772 | 13.40 | 0.860 | 1.10 | 0.218 | 7.42 | 0.309 | 7.42 | 0.309 |
| 3.13 | 0.488 | 5.67 | 0.857 | 9.52 | 0.772 | 13.54 | 0.859 | 1.23 | 0.300 | 8.23 | 0.654 | 8.23 | 0.654 |
| 3.23 | 0.508 | 6.03 | 0.877 | 9.78 | 0.772 | 13.90 | 0.859 | 1.53 | 0.363 | 8.69 | 0.779 | 8.69 | 0.779 |
| 3.23 | 0.508 | 6.28 | 0.861 | 9.87 | 0.772 | 13.94 | 0.853 | 1.81 | 0.411 | 9.04 | 0.727 | 9.04 | 0.727 |
| 3.28 | 0.531 | 6.32 | 0.827 | 9.92 | 0.798 | 14.09 | 0.863 | 2.11 | 0.411 | 10.1 | 0.746 | 10.1 | 0.746 |
| 3.31 | 0.531 | 6.32 | 0.827 | 9.92 | 0.798 | 14.43 | 0.863 | 2.37 | 0.541 | 11.0 | 0.768 | 11.0 | 0.768 |
| 3.31 | 0.552 | 6.35 | 0.814 | 9.98 | 0.787 | 14.43 | 0.864 | 2.56 | 0.777 | CURVE 13 | | | |
| 3.42 | 0.596 | 6.40 | 0.814 | 10.44 | 0.800 | 14.49 | 0.859 | 3.23 | 0.842 | T = 1103. | | | |
| 3.47 | 0.675 | 6.42 | 0.786 | 10.52 | 0.811 | 14.56 | 0.862 | 4.28 | 0.889 | 1.13 | 0.228 | 1.13 | 0.228 |
| 3.52 | 0.711 | 6.47 | 0.766 | 10.69 | 0.812 | 14.82 | 0.862 | 5.15 | 0.934 | 1.23 | 0.309 | 1.23 | 0.309 |
| 3.57 | 0.711 | 6.49 | 0.726 | 10.73 | 0.820 | 14.87 | 0.861 | 5.72 | 0.915 | 1.53 | 0.378 | 1.53 | 0.378 |
| 3.63 | 0.734 | 6.56 | 0.732 | 10.81 | 0.825 | 14.94 | 0.881 | 6.10 | 0.928 | 1.82 | 0.386 | 1.82 | 0.386 |
| 3.70 | 0.740 | 6.60 | 0.718 | 11.03 | 0.825 | 15.00 | 0.886 | 7.00 | 0.778 | 2.13 | 0.484 | 2.13 | 0.484 |
| 3.70 | 0.759 | 6.66 | 0.709 | 11.07 | 0.833 | CURVE 10 | | | | 7.42 | 0.745 | 7.42 | 0.745 |
| 3.82 | 0.780 | 6.74 | 0.710 | 11.15 | 0.817 | T = 1098. | | | | 8.20 | 0.847 | 8.20 | 0.847 |
| 4.00 | 0.780 | 6.86 | 0.683 | 11.20 | 0.830 | 0.530 | 0.607 | 8.73 | 0.871 | 2.44 | 0.554 | 2.44 | 0.554 |
| 4.15 | 0.781 | 7.00 | 0.705 | 11.25 | 0.829 | 1.13 | 0.317 | 1.21 | 0.871 | 2.60 | 0.770 | 2.60 | 0.770 |
| 4.20 | 0.750 | 7.30 | 0.705 | 11.29 | 0.818 | 1.21 | 0.413 | | | | | | |
| 4.26 | 0.771 | 7.39 | 0.719 | 11.38 | 0.818 | | | | | | | | |
| 4.33 | 0.749 | 7.48 | 0.719 | 11.42 | 0.826 | | | | | | | | |

TABLE 7-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------------|------------|-----------|------------|-----------------------|------------|-----------|------------|-----------------------|------------|-----------|------------|
| CURVE 14 T = 1103. | | | | | | | | | | | |
| 1.14 | 0.196 | 12.97 | 0.786 | 14.46 | 0.884 | 1.00 | 0.380 | 9.14 | 0.919 | 4.35 | 0.943 |
| 1.24 | 0.292 | 13.46 | 0.861 | 14.99 | 0.917 | 1.04 | 0.356 | 9.37 | 0.904 | 4.47 | 0.933 |
| 1.53 | 0.352 | 13.99 | 0.877 | | | 1.21 | 0.279 | 9.83 | 0.901 | 4.55 | 0.925 |
| 1.81 | 0.365 | 14.48 | 0.854 | CURVE 17 T = 2020. | | 1.50 | 0.212 | 9.97 | 0.924 | 5.01 | 0.944 |
| 2.13 | 0.448 | 14.98 | 0.906 | | | 1.68 | 0.186 | 10.1 | 0.927 | 5.50 | 0.965 |
| 2.44 | 0.525 | | | 2.48 | 0.875 | 1.86 | 0.170 | 11.0 | 0.933 | 6.01 | 0.976 |
| 2.61 | 0.732 | | | 2.73 | 0.863 | 2.02 | 0.201 | 11.4 | 0.926 | 6.30 | 0.945 |
| CURVE 15 T = 1280. | | | | | | | | | | | |
| | | 2.46 | 0.768 | 2.98 | 0.849 | 2.13 | 0.227 | 11.4 | 0.935 | 6.52 | 0.832 |
| | | 2.73 | 0.830 | 3.23 | 0.849 | 2.24 | 0.288 | 11.6 | 0.926 | 6.70 | 0.785 |
| | | 2.96 | 0.830 | 3.75 | 0.944 | 2.49 | 0.565 | 12.2 | 0.926 | 6.88 | 0.785 |
| | | 3.21 | 0.830 | 4.00 | 0.868 | 2.71 | 0.673 | 12.3 | 0.949 | 7.01 | 0.804 |
| | | 3.47 | 0.828 | 4.23 | 0.854 | 2.82 | 0.683 | 12.8 | 0.922 | 7.50 | 0.839 |
| | | 3.73 | 0.852 | 4.49 | 0.881 | 3.17 | 0.818 | 12.9 | 0.937 | 7.60 | 0.884 |
| | | 3.97 | 0.852 | 4.74 | 0.885 | 3.31 | 0.931 | 13.0 | 0.925 | 8.24 | 0.867 |
| | | 4.21 | 0.814 | 4.99 | 0.903 | 3.63 | 1.000 | 13.9 | 0.935 | 8.52 | 0.855 |
| | | 4.45 | 0.866 | 5.23 | 0.918 | 4.03 | 1.000 | 14.0 | 0.926 | 8.82 | 0.858 |
| | | 3.98 | 0.833 | 4.71 | 0.932 | 4.21 | 0.970 | 14.5 | 0.934 | 8.94 | 0.849 |
| | | 4.24 | 0.709 | 5.49 | 0.932 | 4.30 | 0.997 | 14.7 | 0.927 | 9.12 | 0.869 |
| | | 4.49 | 0.814 | 5.73 | 0.936 | 4.41 | 0.989 | 14.8 | 0.927 | 9.53 | 0.843 |
| | | 4.74 | 0.838 | 5.98 | 0.965 | 4.84 | 0.996 | 14.0 | 0.945 | 10.0 | 0.852 |
| | | 4.98 | 0.882 | 6.48 | 0.839 | 5.07 | 0.993 | CURVE 19 T = 1223. | | | 0.867 |
| | | 5.24 | 0.900 | 6.98 | 0.504 | 5.12 | 1.000 | 10.8 | | 10.8 | 0.903 |
| | | 5.48 | 0.914 | 7.47 | 0.359 | 5.18 | 0.988 | 11.1 | | 11.1 | 0.903 |
| | | 5.72 | 0.894 | 7.98 | 0.651 | 5.38 | 0.996 | 11.3 | | 11.3 | 0.888 |
| | | 5.99 | 0.918 | 8.49 | 0.755 | 5.64 | 0.993 | 11.7 | | 11.7 | 0.888 |
| | | 6.49 | 0.708 | 8.98 | 0.805 | 5.93 | 0.985 | 12.0 | | 12.0 | 0.872 |
| | | 6.98 | 0.322 | 9.49 | 0.827 | 6.08 | 0.993 | 12.1 | | 12.1 | 0.872 |
| | | 7.46 | 0.407 | 9.99 | 0.837 | 6.32 | 0.975 | 12.5 | | 12.5 | 0.933 |
| | | 7.99 | 0.670 | 10.46 | 0.872 | 6.51 | 0.849 | 13.0 | | 13.0 | 0.921 |
| | | 8.46 | 0.757 | 10.97 | 0.865 | 6.64 | 0.789 | 13.4 | | 13.4 | 0.910 |
| | | 8.99 | 0.800 | 11.47 | 0.884 | 6.78 | 0.779 | 13.6 | | 13.6 | 0.917 |
| | | 9.46 | 0.823 | 11.97 | 0.899 | 6.96 | 0.790 | 14.1 | | 14.1 | 0.914 |
| | | 9.97 | 0.838 | 12.47 | 0.903 | 7.28 | 0.806 | 14.4 | | 14.4 | 0.902 |
| | | 10.47 | 0.853 | 12.98 | 0.859 | 7.51 | 0.821 | 14.6 | | 14.6 | 0.912 |
| | | 10.97 | 0.871 | 13.47 | 0.846 | 7.65 | 0.880 | 14.8 | | 14.8 | 0.903 |
| | | 11.46 | 0.887 | 13.99 | 0.894 | 7.84 | 0.912 | 14.9 | | 14.9 | 0.925 |
| | | 11.97 | 0.904 | 14.98 | 0.910 | 7.92 | 0.994 | | | | |
| | | 12.46 | 0.909 | | | 8.03 | 0.915 | | | | |
| | | | | | | 8.14 | 0.891 | | | | |

b. Normal Spectral Emittance (Temperature Dependence)

A total of two sets of experimental data were located for the temperature dependence of the normal spectral emittance. The data are listed in Table 7-6 and shown in Figures 7-3 and 7-4. Specimen characterization and measurement information for the data are given in Table 7-5.

Both sets of data are for $0.650\ \mu\text{m}$ and, therefore, no data from these sources can be used for evaluation at 3.8 and $10.6\ \mu\text{m}$. However, using the provisional values in the previous section for pyrolytic boron nitride, values for 3.8 and $10.6\ \mu\text{m}$ were obtained for temperatures of 1280 , 1670 , and $2020\ \text{K}$. The provisional values are listed in Table 7-4 and shown in Figure 7-3. The uncertainty is 15% . The context within which these values are valid is the following: a 0.5 in. thick specimen of polished pyrolytic boron nitride manufactured by High Temperature Materials, Inc., with the surface parallel to the basal planes radiating. Since the provisional values in the previous section are the same for 1280 , 1670 , and $2022\ \text{K}$, the emittance in this temperature range for either 3.8 or $10.6\ \mu\text{m}$ is temperature independent (see Figure 7-3).

TABLE 7-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ |
|---------------------|------------|-------|------------|
| PYROLYTIC, POLISHED | | | |
| 1.27CM THICK | | | |
| $\lambda = 3.8$ | | | |
| 1280. | 0.805 | 1280. | 0.866 |
| 1670. | 0.805 | 1670. | 0.866 |
| 2020. | 0.806 | 2020. | 0.866 |
| PYROLYTIC, POLISHED | | | |
| 1.27CM THICK | | | |
| $\lambda = 10.6$ | | | |

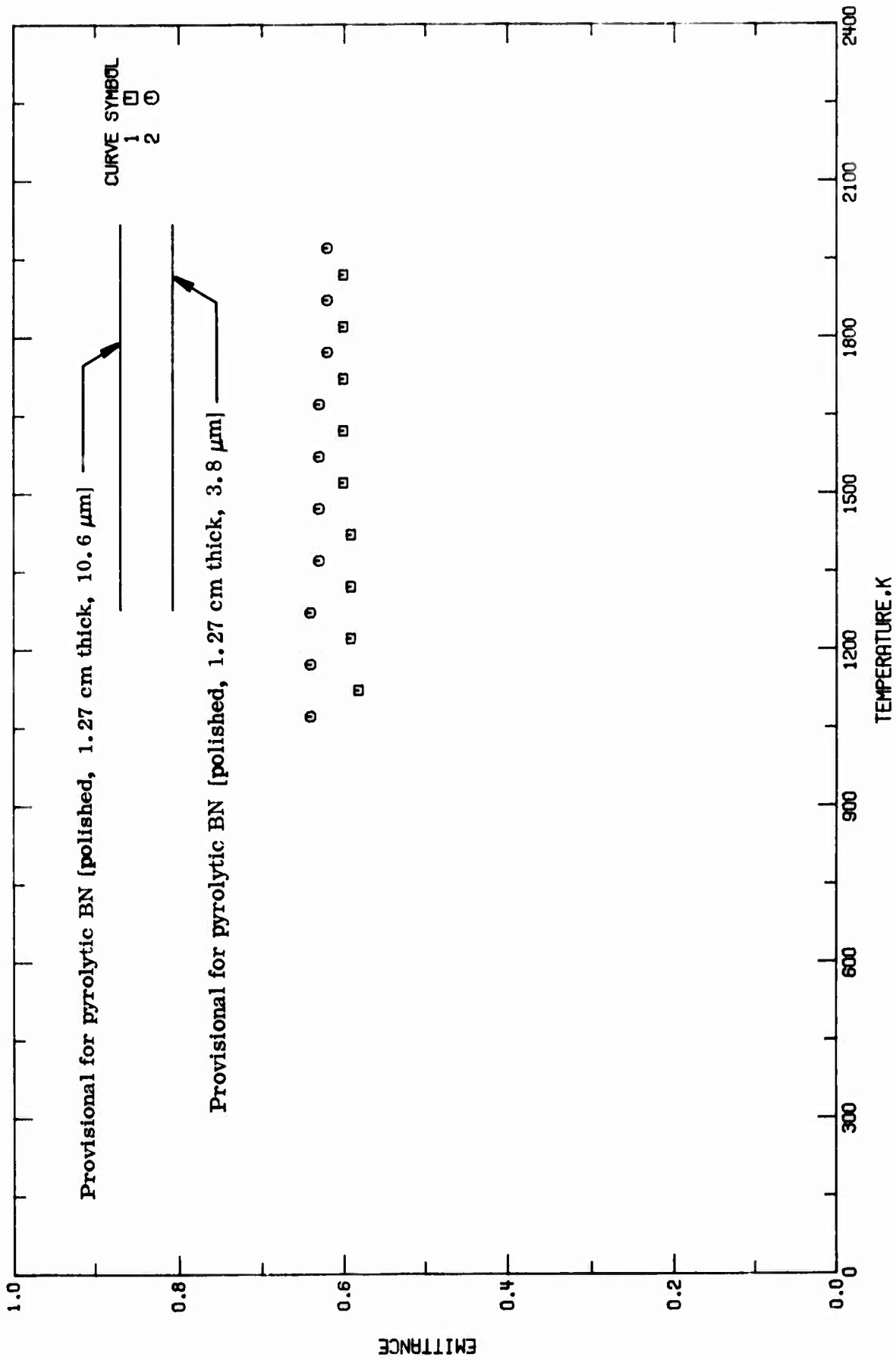


FIGURE 7-3. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE).

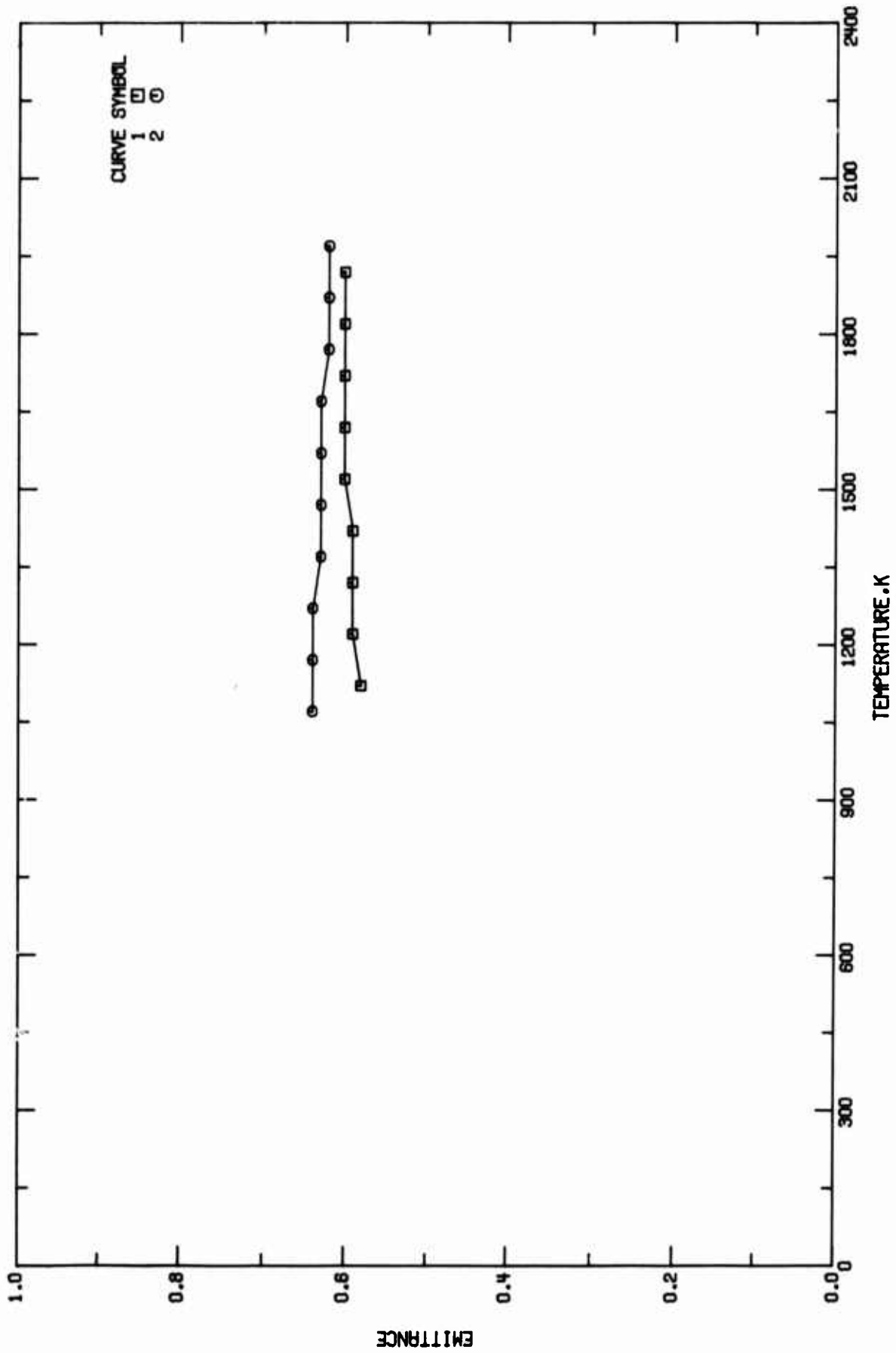


FIGURE 7-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE).

TABLE 7-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T14404 | Serebryakova, T. I., Paderno, Yu. B., and Samsonov, G. V. | 1960 | 0.650 | 1123-1923 | | Layer of paste, approx. 100 μm thick, on tantalum cylinder; paste prepared from fine powder, 2-3 μm , of BN suspended in nitrate binder and dried at 313 to 333 K; $\theta' = 0^\circ$. |
| 2 T32220 | Samsonov, G. V., Fomenko, V. S., and Paderno, Yu. B. | 1962 | 0.650 | 1073-1973 | | Similar to the above specimen except BN suspended in nitrocellulose binder, applied to outer surface of cylinder, and dried at 313 to 333 K. |

TABLE 7-b. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF BORON NITRIDE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ |
|-------------------|------------|
| CURVE 1 | |
| $\lambda = 0.650$ | |
| 1123. | 0.58 |
| 1223. | 0.59 |
| 1323. | 0.59 |
| 1423. | 0.59 |
| 1523. | 0.60 |
| 1623. | 0.60 |
| 1723. | 0.60 |
| 1823. | 0.60 |
| 1923. | 0.60 |
| CURVE 2 | |
| $\lambda = 0.650$ | |
| 1073. | 0.64 |
| 1173. | 0.64 |
| 1273. | 0.64 |
| 1373. | 0.63 |
| 1473. | 0.63 |
| 1573. | 0.63 |
| 1673. | 0.63 |
| 1773. | 0.62 |
| 1873. | 0.62 |
| 1973. | 0.62 |

c. Normal Spectral Reflectance (Wavelength Dependence)

A total of 28 sets of experimental data were located for the wavelength dependence of the normal spectral reflectance of boron nitride. The data are listed in Table 7-9 and shown in Figures 7-5 and 7-6. Specimen characterization and measurement information for the data are given in Table 7-8.

All sets of data, with the exception of one, are for 293 K. No data for higher temperatures was located. Two typical curves are given, one for a pyrolytic specimen and one for a cubic specimen. These are labeled typical because of the lack of complete specimen dimensions and the uncertainty of these values can be 30% or larger. The typical curve for pyrolytic boron nitride at 293 K is based on curve 2 and holds for a specimen from High Temperature Materials, Inc., for linearly polarized light with the electric field vector parallel to the c-axis of the crystal, and $\theta = 0^\circ$ and $\theta' = 0^\circ$. The typical curve for cubic boron nitride at 293 K is based on curve 5 and holds for a polished specimen with density approaching the theoretical value of 3.50 g cm^{-3} . The typical values are listed in Table 7-7 and shown in Figure 7-5.

TABLE 7-7. TYPICAL NORMAL SPECTRAL REFLECTANCE OF BOPON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| PYROLYTIC T = 293 | | | PYROLYTIC T = 293 (CONT.) | | | CURIC POLISHED T = 293 | | | CURIC POLISHED T = 293 (CONT.) | | |
|----------------------|--------|-----------|------------------------------|-----------|--------|------------------------------|--------|-----------|--------------------------------------|-----------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 5.00 | 0.092 | 13.0 | 0.114 | 5.040 | 0.096 | 9.268 | 0.817 | | | | |
| 5.10 | 0.089 | 10.2 | 0.110 | 5.260 | 0.097 | 9.320 | 0.817 | | | | |
| 5.21 | 0.087 | 10.6 | 0.098 | 5.457 | 0.094 | 9.407 | 0.816 | | | | |
| 5.33 | 0.084 | 11.0 | 0.098 | 5.747 | 0.089 | 9.434 | 0.806 | | | | |
| 5.44 | 0.081 | 11.2 | 0.082 | 5.956 | 0.080 | 9.569 | 0.737 | | | | |
| 5.56 | 0.071 | 11.4 | 0.065 | 5.00 | 0.077 | 9.691 | 0.661 | | | | |
| 5.68 | 0.064 | 11.7 | 0.044 | 6.101 | 0.075 | 9.814 | 0.586 | | | | |
| 5.80 | 0.056 | 11.9 | 0.025 | 5.245 | 0.067 | 9.950 | 0.501 | | | | |
| 5.95 | 0.042 | 12.0 | 0.010 | 5.447 | 0.059 | 10.00 | 0.487 | | | | |
| 6.0 | 0.039 | 12.1 | 0.049 | 5.540 | 0.047 | 10.12 | 0.451 | | | | |
| 6.09 | 0.036 | 12.3 | 0.478 | 5.784 | 0.039 | 10.33 | 0.410 | | | | |
| 6.17 | 0.050 | 12.3 | 0.702 | 6.354 | 0.025 | 10.62 | 0.373 | | | | |
| 6.24 | 0.085 | 12.7 | 0.774 | 7.00 | 0.021 | 10.88 | 0.350 | | | | |
| 6.29 | 0.120 | 12.9 | 0.580 | 7.082 | 0.016 | 11.00 | 0.342 | | | | |
| 6.33 | 0.168 | 13.0 | 0.490 | 7.143 | 0.012 | 11.14 | 0.332 | | | | |
| 6.37 | 0.219 | 13.1 | 0.408 | 7.225 | 0.012 | 11.55 | 0.313 | | | | |
| 6.39 | 0.268 | 13.2 | 0.333 | 7.299 | 0.019 | 12.00 | 0.297 | | | | |
| 6.44 | 0.305 | 13.5 | 0.291 | 7.364 | 0.020 | 12.02 | 0.296 | | | | |
| 6.47 | 0.329 | 13.6 | 0.262 | 7.402 | 0.059 | 12.56 | 0.280 | | | | |
| 6.58 | 0.345 | 14.0 | 0.224 | 7.452 | 0.165 | 13.00 | 0.271 | | | | |
| 6.66 | 0.328 | 14.3 | 0.212 | 7.524 | 0.307 | 13.30 | 0.264 | | | | |
| 6.76 | 0.289 | 14.8 | 0.200 | 7.570 | 0.410 | 14.27 | 0.249 | | | | |
| 6.84 | 0.260 | 15.3 | 0.194 | 7.628 | 0.537 | 15.02 | 0.240 | | | | |
| 6.93 | 0.238 | 16.2 | 0.175 | 7.675 | 0.641 | 16.03 | 0.231 | | | | |
| 7.0 | 0.228 | 17.3 | 0.172 | 7.722 | 0.721 | | | | | | |
| 7.05 | 0.221 | 18.6 | 0.157 | 7.740 | 0.771 | | | | | | |
| 7.12 | 0.202 | 20.1 | 0.162 | 7.843 | 0.785 | | | | | | |
| 7.26 | 0.189 | 21.7 | 0.159 | 7.987 | 0.805 | | | | | | |
| 7.47 | 0.177 | 23.9 | 0.159 | 8.00 | 0.806 | | | | | | |
| 7.69 | 0.163 | 26.4 | 0.157 | 9.091 | 0.816 | | | | | | |
| 7.94 | 0.160 | 29.9 | 0.153 | 9.137 | 0.820 | | | | | | |
| 8.0 | 0.157 | 33.3 | 0.152 | 9.333 | 0.820 | | | | | | |
| 8.22 | 0.148 | | | 8.496 | 0.810 | | | | | | |
| 8.50 | 0.144 | | | 8.643 | 0.801 | | | | | | |
| 8.84 | 0.143 | | | 8.787 | 0.798 | | | | | | |
| 9.0 | 0.137 | | | 8.929 | 0.798 | | | | | | |
| 9.10 | 0.133 | | | 9.00 | 0.801 | | | | | | |
| 9.46 | 0.126 | | | 9.107 | 0.806 | | | | | | |
| 9.83 | 0.116 | | | 9.200 | 0.813 | | | | | | |

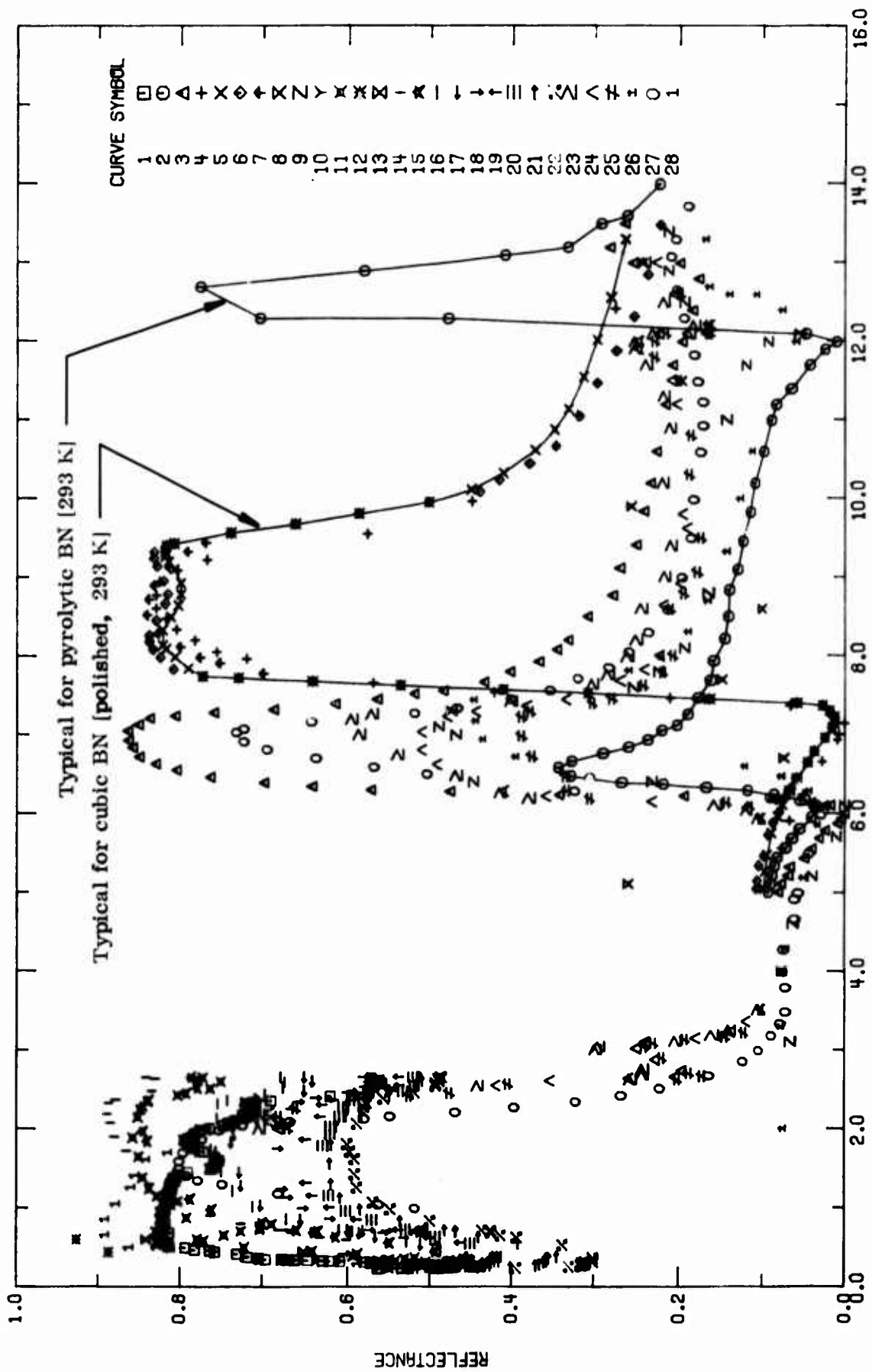


FIGURE 7-5. TYPICAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

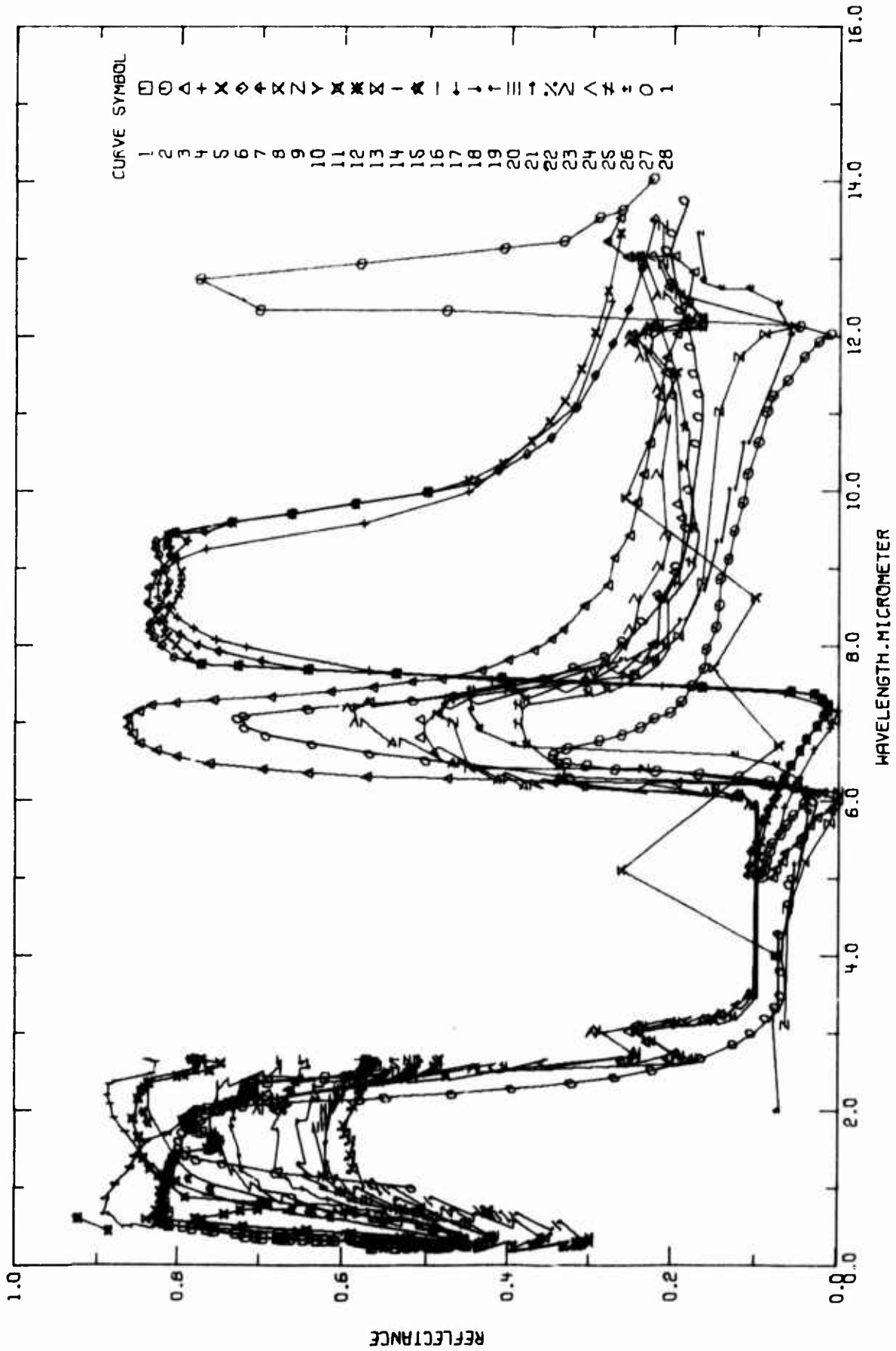


FIGURE 7-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 7-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent) | Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|------------------------------|--|
| 1 T37478 | Browning, M. S. | 1963 | 0.23-2.65 | 293 | | | Sintered; from Carborundum Corp.; density 2.09 g cm^{-3} ; reference standard MgO; smooth values from figure; integrating sphere reflectometer, Beckman DK-2a spectrophotometer, used; author reports spectral total reflectance; $\theta \sim 5^\circ$, $\omega' = 2\pi$. |
| 2 T29203 | Geick, R., Perry, C. H., and Rupprecht, G. | 1966 | 5-33 | 293 | Pyrolytic | | Hexagonal structure; samples supplied by High Temperature Materials, Inc.; linearly polarized light used with \vec{E} parallel to c-axis of crystal; Perkin-Elmer Model 521 spectrophotometer with reflection attachment used; measurement temperature not given explicitly, assumed to be 293 K; smooth values from figure; $\theta = 0^\circ$, $\theta' = 0^\circ$. Similar to the above specimen except linearly polarized light used with \vec{E} perpendicular to c-axis of crystal. |
| 3 T39203 | Geick, R., et al. | 1966 | 5-33 | 293 | Pyrolytic | | Cubic boron nitride; specimen approx. 6 mm in diameter; specimen manufactured by being subjected to very high pressures and temperatures; opaque; density approaches theoretical value of 3.50 g cm^{-3} ; ground and polished on one side with successively finer diamond powder to a perfectly flat, homogeneous, mirror-like finish; Perkin-Elmer Model 521 and 221 infrared spectrophotometers, together with appropriate attachments, used to measure reflectivity; data from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 4 T42872 | Gielisse, P. J., Mitra, S. S., Pinedi, J. N., Griffin, R. D., Marsur, L. C., Marshall, R., and Pascoe, E. A. | 1967 | 5.0-16 | 293 | | | Similar to the above specimen except smooth values from figure. |
| 5 T42872 | Gielisse, P. J., et al. | 1967 | 5.0-13 | 77 | | | Similar to the above specimen except measured at liquid nitrogen temperature, 77.3 K. |
| 7 T42872 | Gielisse, P. J., et al. | 1967 | 6.3-10 | 293 | | | Similar to the above specimen except annealed in air at 623 K for 15 min and subsequently measured at room temperature, 293 K assigned. |
| 8 T40523 | Sulzbach, F. and Turner, A. F. | 1966 | 4.0-34 | 293 | | | Film; optical thickness 10 quarterwaves at $\lambda = 1.7 \mu\text{m}$; electron beam deposited in vacuum, $2-8 \times 10^{-5} \text{ mm Hg}$, at normal incidence onto glass substrate heated to 588 K; rate of depositing 1 quarterwave per min at $\lambda = 0.5 \mu\text{m}$; clear dark brown in appearance; measurements made at room temperature, 293 K assigned; Perkin-Elmer Models 21 and 221 spectrophotometers used; data from figure; $\theta = 0^\circ$. |
| 9 T40523 | Sulzbach, F. and Turner, A. F. | 1966 | 3.1-37 | 293 | | | Polished; massive BN; measurements made at room temperature, 293 K assigned; Perkin-Elmer Models 21 and 221 spectrophotometers used; smooth values from figure; $\theta = 0^\circ$. |
| 10 T22272 | Schatz, E. A., Goldberg, D. M., Pearson, E. G., and Burks, T. L. | 1963 | 0.23-2.7 | 293 | Sample No. 97 | | 97 pure; sintered specimen; from Carborundum Co.; density 2.09 g cm^{-3} , theoretical density 2.27 g cm^{-3} ; thickness 50 mils; reference standard MgO, reflectance data measured and presented relative to MgO; spectral total reflectance reported; integrating sphere reflectometer, Beckman DK-2a spectrophotometer used; measurement temperature not given explicitly, 293 K assigned; smooth values from figure; $\theta \sim 5^\circ$, $\omega' = 2\pi$. |
| 11 T22272 | Schatz, E. A., et al. | 1963 | 0.23-2.7 | 293 | Sample No. 98 | | 100 pure; sintered at 2123 K for 2 hr, sinter material BN; density 2.00 g cm^{-3} , theoretical density 2.27 g cm^{-3} ; thickness 65 mils; reference standard MgO, reflectance data measured and presented relative to MgO; spectral total reflectance reported; integrating sphere reflectometer, Beckman DK-2a spectrophotometer used; measurement temperature not explicitly given, 293 K assigned; smooth values from figure; $\theta \sim 5^\circ$, $\omega' = 2\pi$. |

TABLE 7-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 12 T28755 | Zerlaut, G. A. and Harada, Y. | 1963 | 0.44, 0.60 | 293 | HC 0021 | Manufactured by Carborundum Co.; powder compacted at 10 000 psi; MgO used as standard, absolute values of reflectance reported; integrating sphere reflectometer used; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\omega' = 2\pi$. |
| 13 T28755 | Zerlaut, G. A. and Harada, Y. | 1963 | 0.44, 0.60 | 293 | HC 0021 | The above specimen and conditions except exposed to uv irradiation; 75 ESH with solar factor 1.5. |
| 14 T37398 | Schatz, E. A., Counts, C. R., III, and Burris, T. L. | 1964 | 0.23-2.7 | 293 | | 99.5 pure powder; from Carborundum Co.; mesh size 325; compacted at 290 psi with highly polished stainless steel ram; curves measured and presented relative to freshly prepared smoked MgO reference samples; Beckman DK-2A spectroradiometer used; measurement temperature not given explicitly, assumed to be 293 K; smooth values from figure; $\theta = 0^\circ$, $\omega' = 2\pi$; reported error $\pm 3\%$. |
| 15 T37399 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 1150 psi. |
| 16 T37398 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 2880 psi. |
| 17 T37398 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 5760 psi. |
| 18 T37395 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 11 500 psi. |
| 19 T37398 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 20 200 psi. |
| 20 T37399 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 28 800 psi. |
| 21 T37393 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 31 700 psi. |
| 22 T37398 | Schatz, E. A., et al. | 1964 | 0.23-2.7 | 293 | | Similar to the above specimen except compacted at 34 600 psi. |
| 23 T37399 | Schatz, E. A., et al. | 1964 | 2.0-15 | 293 | | Commercial sintered sample; surface machine grooved to roughness 55-40 μm ; black-body reflectometer used in conjunction with Baird-Atomic Model NK-1 spectrophotometer; reflectance factor ($\omega = 2\pi$, $\theta' = 0^\circ$) actually measured, equated to reflectance ($\theta = 0^\circ$; $\omega' = 2\pi$); smooth values from figure. |
| 24 T37398 | Schatz, E. A., et al. | 1964 | 2.0-15 | 253 | | Similar to the above specimen except surface roughness 300-400 μm . |
| 25 T37398 | Schatz, E. A., et al. | 1964 | 2.0-36 | 293 | | Similar to the above specimen except surface roughness 1800-2200 μm . |
| 26 T2756 | Martia, T. P., Massa, J. D., and Turner, A. F. | 1963 | 2-35 | 293 | | Pressed powder; measurement temperature not given explicitly, assumed to be 293 K; smooth values from figure; $\theta = 0^\circ$. |
| 27 A60027, A60002 | Cunnington, G. R. | 1975 | 1.0-24 | 293 | | 97.0 BN, 2.4 boric oxide, 0.2 alumina and silica, 0.1 alkaline earth oxides, and <0.01 carbon (this typical composition given by supplier); manufactured by Carborundum Co.; hot-pressed; no specification of density given; G. D. heated cavity used for measurement; reflectance factor with $\omega = 2\pi$, $\theta' = 20^\circ$ actually measured, equated here to reflectance with $\theta = 30^\circ$, $\omega' = 2\pi$; measurement temperature not given explicitly, assumed to be 293 K. |
| 28 A00027, A00002 | Cunnington, G. R. | 1975 | 0.29-2.11 | 293 | | 97.00 BN, 2.4 boric oxide, 0.2 alumina and silica, 0.1 alkaline earth oxides, and <0.01 carbon (this typical composition given by supplier); manufactured by Carborundum Co.; hot-pressed; no specification of density given; G. D. integrating sphere used for measurement; reflectance factor measured; direct or indirect made not explicitly given, direct made with $\theta = 20^\circ$, $\omega' = 2\pi$ presumed; measurement temperature not given explicitly, assumed to be 293 K. |

TABLE 7-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 T = 293. | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 2 T = 293. | | CURVE 2 (CONT.) | | CURVE 3 T = 293. | |
|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|---------------------|--------|-----------------|--------|---------------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 0.230 | 0.563 | 0.4170 | 0.729 | 1.461 | 0.782 | 2.437 | 0.594 | 8.22 | 0.146 | 5.00 | 0.080 | | |
| 0.2328 | 0.535 | 0.4440 | 0.755 | 1.594 | 0.760 | 2.471 | 0.574 | 8.50 | 0.144 | 5.11 | 0.077 | | |
| 0.2402 | 0.495 | 0.4620 | 0.762 | 1.521 | 0.752 | 2.498 | 0.574 | 8.84 | 0.143 | 5.21 | 0.069 | | |
| 0.2425 | 0.483 | 0.4720 | 0.780 | 1.536 | 0.753 | 2.545 | 0.568 | 9.10 | 0.133 | 5.32 | 0.067 | | |
| 0.2450 | 0.476 | 0.5020 | 0.792 | 1.579 | 0.753 | 2.587 | 0.559 | 9.46 | 0.126 | 5.43 | 0.051 | | |
| 0.2491 | 0.472 | 0.5210 | 0.811 | 1.607 | 0.750 | 2.620 | 0.562 | 9.83 | 0.116 | 5.55 | 0.042 | | |
| 0.2547 | 0.472 | 0.5550 | 0.813 | 1.638 | 0.756 | 2.650 | 0.571 | 10.2 | 0.110 | 5.68 | 0.033 | | |
| 0.2558 | 0.474 | 0.5690 | 0.824 | 1.650 | 0.755 | | | 10.6 | 0.098 | 5.78 | 0.025 | | |
| 0.2580 | 0.469 | 0.5950 | 0.824 | 1.721 | 0.769 | | | 11.0 | 0.088 | 5.87 | 0.009 | | |
| 0.2603 | 0.472 | 0.6070 | 0.822 | 1.728 | 0.774 | | | 11.2 | 0.082 | 5.93 | 0.004 | | |
| 0.2662 | 0.475 | 0.6500 | 0.822 | 1.764 | 0.781 | | | 11.4 | 0.065 | 6.00 | 0.000 | | |
| 0.2679 | 0.479 | 0.6700 | 0.821 | 1.783 | 0.785 | | | 11.7 | 0.044 | 6.10 | 0.010 | | |
| 0.2724 | 0.488 | 0.6840 | 0.811 | 1.815 | 0.785 | | | 11.9 | 0.025 | 6.09 | 0.026 | | |
| 0.2750 | 0.493 | 0.6960 | 0.824 | 1.827 | 0.783 | | | 12.0 | 0.010 | 6.13 | 0.043 | | |
| 0.2757 | 0.501 | 0.7500 | 0.819 | 1.841 | 0.785 | | | 12.1 | 0.049 | 6.18 | 0.087 | | |
| 0.2799 | 0.514 | 0.8140 | 0.816 | 1.864 | 0.792 | | | 12.3 | 0.478 | 6.22 | 0.194 | | |
| 0.2816 | 0.517 | 0.8280 | 0.820 | 1.888 | 0.782 | | | 12.3 | 0.702 | 6.23 | 0.344 | | |
| 0.2823 | 0.521 | 0.9510 | 0.820 | 1.897 | 0.784 | | | 12.7 | 0.774 | 6.28 | 0.476 | | |
| 0.2850 | 0.526 | 0.9730 | 0.816 | 1.911 | 0.783 | | | 12.9 | 0.580 | 6.30 | 0.572 | | |
| 0.2889 | 0.545 | 0.9860 | 0.817 | 1.921 | 0.780 | | | 13.1 | 0.408 | 6.39 | 0.697 | | |
| 0.2913 | 0.552 | 1.054 | 0.815 | 1.955 | 0.780 | | | 13.2 | 0.333 | 6.46 | 0.762 | | |
| 0.2938 | 0.552 | 1.066 | 0.813 | 1.994 | 0.774 | | | 13.5 | 0.291 | 6.55 | 0.803 | | |
| 0.2983 | 0.562 | 1.111 | 0.812 | 2.017 | 0.762 | | | 14.0 | 0.224 | 6.63 | 0.829 | | |
| 0.3006 | 0.571 | 1.125 | 0.814 | 2.051 | 0.745 | | | 14.8 | 0.200 | 6.72 | 0.849 | | |
| 0.3046 | 0.571 | 1.156 | 0.810 | 2.071 | 0.739 | | | 15.3 | 0.194 | 6.84 | 0.857 | | |
| 0.3069 | 0.569 | 1.176 | 0.810 | 2.084 | 0.739 | | | 16.2 | 0.175 | 6.93 | 0.862 | | |
| 0.3113 | 0.579 | 1.183 | 0.813 | 2.098 | 0.731 | | | 17.3 | 0.172 | 7.05 | 0.863 | | |
| 0.3200 | 0.608 | 1.193 | 0.813 | 2.115 | 0.731 | | | 18.6 | 0.157 | 7.13 | 0.858 | | |
| 0.3247 | 0.621 | 1.212 | 0.810 | 2.150 | 0.721 | | | 20.1 | 0.162 | 7.21 | 0.836 | | |
| 0.3258 | 0.629 | 1.238 | 0.810 | 2.166 | 0.717 | | | 21.7 | 0.159 | 7.24 | 0.805 | | |
| 0.3258 | 0.629 | 1.249 | 0.809 | 2.185 | 0.717 | | | 23.9 | 0.159 | 7.28 | 0.758 | | |
| 0.3276 | 0.629 | 1.266 | 0.809 | 2.223 | 0.711 | | | 26.4 | 0.157 | 7.32 | 0.686 | | |
| 0.3338 | 0.646 | 1.283 | 0.811 | 2.249 | 0.706 | | | 29.9 | 0.153 | 7.39 | 0.615 | | |
| 0.3400 | 0.660 | 1.296 | 0.808 | 2.269 | 0.706 | | | 33.3 | 0.152 | 7.45 | 0.565 | | |
| 0.3410 | 0.660 | 1.318 | 0.810 | 2.283 | 0.711 | | | | | 7.52 | 0.528 | | |
| 0.3436 | 0.660 | 1.345 | 0.804 | 2.308 | 0.718 | | | | | 7.56 | 0.484 | | |
| 0.3500 | 0.675 | 1.359 | 0.807 | 2.325 | 0.716 | | | | | 7.67 | 0.435 | | |
| 0.3500 | 0.694 | 1.359 | 0.807 | 2.344 | 0.710 | | | | | 7.80 | 0.402 | | |
| 0.3660 | 0.703 | 1.399 | 0.802 | 2.367 | 0.688 | | | | | | | | |
| 0.3750 | 0.716 | 1.428 | 0.802 | 2.423 | 0.620 | | | | | | | | |

TABLE 7-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED) [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

Table with columns for Curve number (3-8) and parameters (lambda, rho). The table is organized into sections for CURVE 3, CURVE 4, CURVE 5, CURVE 6, CURVE 7, and CURVE 8, each with its own set of lambda and rho values. Some curves include temperature T values.

TABLE 7-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|---------------------|--------|-----------|--------|----------------------|--------|----------------------|--------|----------------------|--------|----------------------|--------|-----------|--------|
| CURVE 9 T = 293. | | | | | | | | | | | | | |
| 3.10 | 0.066 | 0.280 | 0.514 | 2.60 | 0.559 | 1.89 | 0.856 | 0.350 | 0.467 | 0.976 | 0.760 | 0.350 | 0.467 |
| 4.60 | 0.063 | 0.290 | 0.550 | 2.65 | 0.570 | 2.15 | 0.850 | 0.360 | 0.477 | 1.11 | 0.786 | 0.360 | 0.477 |
| 5.20 | 0.041 | 0.300 | 0.570 | | | 2.25 | 0.847 | 0.589 | 0.600 | 1.32 | 0.808 | 0.589 | 0.600 |
| 5.70 | 0.010 | 0.310 | 0.570 | CURVE 11 T = 293. | | | | 0.618 | 0.632 | 1.84 | 0.839 | 0.618 | 0.632 |
| 6.10 | 0.000 | 0.320 | 0.607 | | | 2.43 | 0.801 | 0.681 | 0.664 | 1.97 | 0.844 | 0.681 | 0.664 |
| 6.40 | 0.233 | 0.330 | 0.635 | | | 2.51 | 0.761 | 0.703 | 0.662 | 2.29 | 0.844 | 0.703 | 0.662 |
| 6.40 | 0.448 | 0.340 | 0.660 | 0.230 | 0.550 | 2.60 | 0.748 | 0.717 | 0.671 | 2.36 | 0.837 | 0.717 | 0.671 |
| 7.00 | 0.469 | 0.345 | 0.663 | 0.233 | 0.529 | 2.65 | 0.770 | 0.717 | 0.679 | 2.45 | 0.791 | 0.717 | 0.679 |
| 7.10 | 0.481 | 0.350 | 0.675 | 0.236 | 0.499 | CURVE 12 T = 293. | | | | 2.52 | 0.777 | 0.800 | 0.724 |
| 7.30 | 0.474 | 0.350 | 0.700 | 0.245 | 0.452 | 1.05 | 0.801 | 0.901 | 0.761 | 2.62 | 0.770 | 0.901 | 0.761 |
| 7.60 | 0.255 | 0.447 | 0.757 | 0.260 | 0.486 | 1.30 | 0.835 | 1.30 | 0.835 | 2.65 | 0.785 | 1.30 | 0.835 |
| 7.80 | 0.225 | 0.513 | 0.813 | 0.280 | 0.472 | 0.440 | 0.885 | 1.72 | 0.864 | CURVE 16 T = 293. | | | |
| 8.10 | 0.193 | 0.548 | 0.813 | 0.290 | 0.476 | 0.600 | 0.925 | 1.90 | 0.878 | 0.230 | 0.526 | 1.90 | 0.878 |
| 8.80 | 0.166 | 0.569 | 0.827 | 0.294 | 0.473 | CURVE 13 T = 293. | | | | 2.08 | 0.883 | 2.08 | 0.883 |
| 11.0 | 0.146 | 0.673 | 0.823 | 0.300 | 0.467 | 0.310 | 0.504 | 2.19 | 0.887 | 0.230 | 0.526 | 2.19 | 0.887 |
| 11.7 | 0.122 | 0.683 | 0.811 | 0.319 | 0.543 | 0.327 | 0.562 | 2.33 | 0.885 | 0.236 | 0.492 | 2.33 | 0.885 |
| 12.0 | 0.092 | 0.700 | 0.828 | 0.327 | 0.550 | 0.440 | 0.650 | 2.37 | 0.876 | 0.252 | 0.450 | 2.37 | 0.876 |
| 12.1 | 0.056 | 0.789 | 0.818 | 0.340 | 0.550 | 0.600 | 0.840 | 2.48 | 0.833 | 0.261 | 0.452 | 2.48 | 0.833 |
| 12.5 | 0.193 | 0.854 | 0.823 | 0.350 | 0.531 | 0.600 | 0.840 | 2.63 | 0.829 | 0.288 | 0.462 | 2.63 | 0.829 |
| 12.9 | 0.213 | 0.950 | 0.823 | 0.360 | 0.518 | CURVE 14 T = 293. | | | | 2.65 | 0.840 | 2.65 | 0.840 |
| 13.4 | 0.213 | 1.05 | 0.819 | 0.387 | 0.592 | 0.440 | 0.885 | CURVE 15 T = 293. | | | | 0.230 | 0.526 |
| 14.3 | 0.179 | 1.15 | 0.812 | 0.413 | 0.587 | 0.600 | 0.925 | 0.230 | 0.540 | 0.230 | 0.526 | 0.230 | 0.540 |
| 14.9 | 0.135 | 1.35 | 0.807 | 0.448 | 0.641 | 0.240 | 0.479 | 0.236 | 0.475 | 0.236 | 0.492 | 0.236 | 0.475 |
| 15.4 | 0.101 | 1.44 | 0.799 | 0.497 | 0.720 | 0.243 | 0.475 | 0.252 | 0.450 | 0.252 | 0.450 | 0.252 | 0.450 |
| 16.1 | 0.087 | 1.50 | 0.762 | 0.551 | 0.772 | 0.245 | 0.460 | 0.261 | 0.452 | 0.261 | 0.452 | 0.261 | 0.452 |
| 33.4 | 0.082 | 1.53 | 0.754 | 0.582 | 0.765 | 0.249 | 0.462 | 0.288 | 0.462 | 0.288 | 0.462 | 0.288 | 0.462 |
| 34.8 | 0.062 | 1.60 | 0.749 | 0.603 | 0.777 | 0.253 | 0.453 | 0.300 | 0.453 | 0.300 | 0.453 | 0.300 | 0.453 |
| 35.5 | 0.043 | 1.79 | 0.786 | 0.652 | 0.724 | 0.259 | 0.457 | 0.330 | 0.459 | 0.330 | 0.459 | 0.330 | 0.459 |
| 36.4 | 0.045 | 1.83 | 0.785 | 0.702 | 0.724 | 0.254 | 0.454 | 0.350 | 0.459 | 0.350 | 0.459 | 0.350 | 0.459 |
| 37.0 | 0.057 | 1.86 | 0.794 | 0.721 | 0.701 | 0.272 | 0.460 | 0.441 | 0.493 | 0.441 | 0.493 | 0.441 | 0.493 |
| CURVE 10 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |
| 6.230 | 0.562 | 1.91 | 0.781 | 0.757 | 0.701 | 0.276 | 0.466 | 0.549 | 0.550 | 1.68 | 0.755 | 0.549 | 0.550 |
| 0.240 | 0.494 | 1.99 | 0.773 | 0.785 | 0.687 | 0.285 | 0.466 | 0.624 | 0.614 | 1.71 | 0.754 | 0.624 | 0.614 |
| 0.250 | 0.470 | 2.10 | 0.731 | 0.875 | 0.709 | 0.291 | 0.466 | 0.679 | 0.639 | 1.74 | 0.760 | 0.679 | 0.639 |
| 0.260 | 0.470 | 2.26 | 0.707 | 1.04 | 0.801 | 0.298 | 0.466 | 0.698 | 0.635 | 1.99 | 0.761 | 0.698 | 0.635 |
| 0.270 | 0.483 | 2.32 | 0.718 | 1.08 | 0.826 | 0.302 | 0.461 | 0.712 | 0.659 | 2.13 | 0.753 | 0.712 | 0.659 |
| | | 2.45 | 0.586 | 1.24 | 0.836 | 0.322 | 0.461 | 0.801 | 0.699 | 2.32 | 0.752 | 0.801 | 0.699 |
| | | 2.55 | 0.566 | 1.65 | 0.849 | 0.332 | 0.469 | | | | | | |

TABLE 7-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 16 (CONT.) | | | CURVE 17 | | | CURVE 18 | | | CURVE 19 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 21 (CONT.) | | | CURVE 22 (CONT.) | | | | | |
|------------------|--------|--|-----------|--------|--|-----------|--------|--|------------------|--------|--|------------------|--------|--|------------------|--------|--|------------------|--------|--|------|-------|--|
| λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | | | |
| CURVE 16 (CONT.) | | | | | | | | | | | | | | | | | | | | | | | |
| 2.36 | 0.740 | | 0.230 | 0.526 | | 0.310 | 0.423 | | 1.93 | 0.620 | | 2.60 | 0.509 | | 2.60 | 0.486 | | 2.60 | 0.486 | | | | |
| 2.44 | 0.695 | | 0.236 | 0.492 | | 0.350 | 0.423 | | 2.02 | 0.620 | | 2.65 | 0.512 | | 2.53 | 0.489 | | 2.53 | 0.489 | | | | |
| 2.52 | 0.674 | | 0.252 | 0.450 | | 0.553 | 0.463 | | 2.15 | 0.609 | | CURVE 22 | | | | | | | | | | | |
| 2.59 | 0.672 | | 0.261 | 0.452 | | 0.614 | 0.500 | | 2.27 | 0.604 | | T = 293. | | | | | | | | | | | |
| 2.65 | 0.677 | | 0.288 | 0.462 | | 0.676 | 0.519 | | 2.36 | 0.591 | | CURVE 23 | | | | | | | | | | | |
| CURVE 17 | | | | | | | | | | | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | | | | | | | | | |
| 0.230 | 0.526 | | 0.308 | 0.453 | | 0.700 | 0.514 | | 2.47 | 0.534 | | 0.230 | 0.394 | | 2.00 | 0.698 | | 2.12 | 0.706 | | 2.54 | 0.439 | |
| 0.236 | 0.492 | | 0.325 | 0.453 | | 0.713 | 0.519 | | 2.55 | 0.519 | | 0.244 | 0.331 | | 2.10 | 0.698 | | 2.62 | 0.439 | | 2.60 | 0.240 | |
| 0.252 | 0.450 | | 0.374 | 0.452 | | 0.846 | 0.588 | | 2.65 | 0.521 | | 0.262 | 0.314 | | 3.00 | 0.294 | | 2.75 | 0.240 | | 3.00 | 0.294 | |
| 0.261 | 0.452 | | 0.492 | 0.492 | | 0.998 | 0.621 | | CURVE 21 | | | | | | | | | | | | | | |
| 0.288 | 0.462 | | 1.15 | 0.641 | | 1.15 | 0.641 | | T = 293. | | | | | | | | | | | | | | |
| 0.324 | 0.455 | | 1.31 | 0.648 | | 1.31 | 0.648 | | 0.230 | 0.488 | | 0.291 | 0.314 | | 3.11 | 0.200 | | 3.11 | 0.200 | | 3.19 | 0.139 | |
| 0.330 | 0.458 | | 1.86 | 0.649 | | 1.86 | 0.649 | | 0.232 | 0.442 | | 0.302 | 0.310 | | 3.24 | 0.103 | | 3.24 | 0.103 | | 3.24 | 0.139 | |
| 0.360 | 0.456 | | 2.15 | 0.632 | | 2.15 | 0.632 | | 0.241 | 0.400 | | 0.304 | 0.300 | | 5.93 | 0.103 | | 5.93 | 0.103 | | 5.93 | 0.103 | |
| 0.360 | 0.456 | | 2.30 | 0.630 | | 2.30 | 0.630 | | 0.259 | 0.371 | | 0.350 | 0.330 | | 6.04 | 0.118 | | 6.04 | 0.118 | | 6.04 | 0.118 | |
| 0.527 | 0.511 | | 2.48 | 0.548 | | 2.48 | 0.548 | | 0.270 | 0.367 | | 0.350 | 0.330 | | 6.10 | 0.155 | | 6.10 | 0.155 | | 6.10 | 0.155 | |
| 0.627 | 0.566 | | 2.52 | 0.547 | | 2.52 | 0.547 | | 0.297 | 0.362 | | 0.350 | 0.330 | | 6.19 | 0.376 | | 6.19 | 0.376 | | 6.19 | 0.376 | |
| 0.679 | 0.585 | | 2.55 | 0.538 | | 2.55 | 0.538 | | 0.310 | 0.359 | | 0.350 | 0.330 | | 6.26 | 0.410 | | 6.26 | 0.410 | | 6.26 | 0.410 | |
| 0.700 | 0.581 | | 2.65 | 0.539 | | 2.65 | 0.539 | | 0.340 | 0.356 | | 0.350 | 0.330 | | 6.48 | 0.465 | | 6.48 | 0.465 | | 6.48 | 0.465 | |
| 0.712 | 0.599 | | CURVE 20 | | | | | | | | | 1.06 | 0.569 | | 6.74 | 0.537 | | 6.74 | 0.537 | | 6.74 | 0.537 | |
| 0.847 | 0.654 | | T = 293. | | | | | | | | | 1.25 | 0.588 | | 7.00 | 0.582 | | 7.00 | 0.582 | | 7.00 | 0.582 | |
| 1.03 | 0.700 | | 0.230 | 0.520 | | 0.233 | 0.489 | | 0.617 | 0.441 | | 1.42 | 0.591 | | 7.19 | 0.591 | | 7.19 | 0.591 | | 7.19 | 0.591 | |
| 1.20 | 0.724 | | 0.233 | 0.489 | | 0.240 | 0.440 | | 0.681 | 0.469 | | 1.61 | 0.591 | | 7.26 | 0.567 | | 7.26 | 0.567 | | 7.26 | 0.567 | |
| 1.45 | 0.726 | | 0.256 | 0.432 | | 0.293 | 0.430 | | 0.696 | 0.468 | | 1.70 | 0.597 | | 7.42 | 0.397 | | 7.42 | 0.397 | | 7.42 | 0.397 | |
| 1.63 | 0.736 | | 0.310 | 0.420 | | 0.350 | 0.420 | | 0.704 | 0.481 | | 1.80 | 0.600 | | 7.64 | 0.298 | | 7.64 | 0.298 | | 7.64 | 0.298 | |
| 1.92 | 0.733 | | 0.371 | 0.417 | | 0.420 | 0.420 | | 0.967 | 0.584 | | 2.06 | 0.588 | | 7.76 | 0.280 | | 7.76 | 0.280 | | 7.76 | 0.280 | |
| 2.03 | 0.734 | | 0.539 | 0.451 | | 0.625 | 0.492 | | 1.11 | 0.608 | | 2.20 | 0.580 | | 7.99 | 0.258 | | 7.99 | 0.258 | | 7.99 | 0.258 | |
| 2.17 | 0.727 | | 0.625 | 0.492 | | 0.684 | 0.510 | | 1.29 | 0.619 | | 2.27 | 0.580 | | 8.20 | 0.246 | | 8.20 | 0.246 | | 8.20 | 0.246 | |
| 2.33 | 0.723 | | 0.698 | 0.507 | | 0.717 | 0.530 | | 1.55 | 0.621 | | 2.32 | 0.577 | | 8.60 | 0.242 | | 8.60 | 0.242 | | 8.60 | 0.242 | |
| 2.38 | 0.707 | | 0.839 | 0.570 | | 0.839 | 0.570 | | 1.79 | 0.619 | | 2.37 | 0.557 | | 9.01 | 0.214 | | 9.01 | 0.214 | | 9.01 | 0.214 | |
| 2.40 | 0.650 | | 0.952 | 0.601 | | 0.952 | 0.601 | | 2.02 | 0.613 | | 2.45 | 0.519 | | 9.40 | 0.206 | | 9.40 | 0.206 | | 9.40 | 0.206 | |
| 2.60 | 0.641 | | 1.15 | 0.622 | | 1.15 | 0.622 | | 2.15 | 0.601 | | 2.54 | 0.493 | | 10.2 | 0.216 | | 10.2 | 0.216 | | 10.2 | 0.216 | |
| 2.65 | 0.650 | | 1.78 | 0.629 | | 1.78 | 0.629 | | 2.29 | 0.578 | | 2.57 | 0.492 | | 10.9 | 0.207 | | 10.9 | 0.207 | | 10.9 | 0.207 | |

TABLE 7-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 23 (CONT.) | | | CURVE 24 (CONT.) | | | CURVE 25 (CONT.) | | | CURVE 26 (CONT.) | | | CURVE 27 (CONT.) | | |
|------------------|--------|--|------------------|--------|--|------------------|--------|--|------------------|--------|--|------------------|--------|--|
| λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | |
| 11.3 | 0.215 | | 7.44 | 0.336 | | 5.93 | 0.103 | | 6.72 | 0.395 | | 1.36 | 0.777 | |
| 11.7 | 0.236 | | 7.68 | 0.271 | | 6.08 | 0.118 | | 6.94 | 0.437 | | 1.42 | 0.791 | |
| 11.9 | 0.249 | | 7.82 | 0.243 | | 6.13 | 0.147 | | 7.17 | 0.446 | | 1.51 | 0.800 | |
| 12.0 | 0.249 | | 8.00 | 0.225 | | 6.18 | 0.306 | | 7.44 | 0.448 | | 1.60 | 0.800 | |
| 12.1 | 0.228 | | 8.54 | 0.220 | | 6.28 | 0.335 | | 7.81 | 0.260 | | 1.71 | 0.795 | |
| 12.1 | 0.184 | | 8.92 | 0.199 | | 6.46 | 0.337 | | 7.99 | 0.223 | | 1.80 | 0.788 | |
| 12.2 | 0.178 | | 9.62 | 0.191 | | 6.62 | 0.377 | | 8.31 | 0.189 | | 1.88 | 0.772 | |
| 12.5 | 0.215 | | 9.80 | 0.196 | | 6.98 | 0.389 | | 8.70 | 0.167 | | 1.99 | 0.751 | |
| 13.0 | 0.239 | | 11.2 | 0.203 | | 7.22 | 0.389 | | 9.33 | 0.146 | | 2.05 | 0.723 | |
| 15.0 | 0.245 | | 11.5 | 0.210 | | 7.29 | 0.379 | | 10.0 | 0.130 | | 2.10 | 0.667 | |
| | | | 11.9 | 0.250 | | 7.39 | 0.303 | | 10.6 | 0.114 | | 2.14 | 0.580 | |
| | | | 12.0 | 0.250 | | 7.45 | 0.280 | | 12.0 | 0.060 | | 2.17 | 0.550 | |
| | | | 12.1 | 0.226 | | 7.62 | 0.244 | | 12.4 | 0.075 | | 2.22 | 0.470 | |
| | | | 12.1 | 0.191 | | 7.79 | 0.221 | | 12.6 | 0.108 | | 2.28 | 0.397 | |
| | | | 12.1 | 0.169 | | 8.00 | 0.204 | | 12.6 | 0.143 | | 2.35 | 0.323 | |
| 2.00 | 0.681 | | 8.00 | 0.211 | | 8.59 | 0.211 | | 12.7 | 0.165 | | 2.43 | 0.269 | |
| 2.09 | 0.691 | | 8.79 | 0.195 | | 8.79 | 0.195 | | 13.3 | 0.169 | | 2.52 | 0.224 | |
| 2.20 | 0.691 | | 9.06 | 0.179 | | 9.06 | 0.179 | | 15.2 | 0.128 | | 2.68 | 0.166 | |
| 2.54 | 0.423 | | 9.50 | 0.175 | | 9.50 | 0.175 | | 15.7 | 0.080 | | 2.86 | 0.127 | |
| 2.60 | 0.356 | | 10.3 | 0.188 | | 10.3 | 0.188 | | 16.2 | 0.077 | | 3.00 | 0.106 | |
| 2.63 | 0.261 | | 10.8 | 0.186 | | 10.8 | 0.186 | | 16.9 | 0.071 | | 3.19 | 0.089 | |
| 2.65 | 0.206 | | 11.5 | 0.201 | | 11.5 | 0.201 | | 17.3 | 0.073 | | 3.34 | 0.078 | |
| 2.73 | 0.197 | | 11.8 | 0.231 | | 11.8 | 0.231 | | 19.3 | 0.093 | | 3.49 | 0.072 | |
| 2.87 | 0.230 | | 12.0 | 0.231 | | 12.0 | 0.231 | | 21.4 | 0.122 | | 3.80 | 0.072 | |
| 3.01 | 0.252 | | 12.1 | 0.217 | | 12.1 | 0.217 | | 22.4 | 0.139 | | 4.00 | 0.076 | |
| 3.09 | 0.242 | | 12.1 | 0.166 | | 12.1 | 0.166 | | 23.5 | 0.143 | | 4.28 | 0.074 | |
| 3.14 | 0.181 | | 12.2 | 0.166 | | 12.2 | 0.166 | | 24.5 | 0.142 | | 4.67 | 0.062 | |
| 3.22 | 0.143 | | 12.2 | 0.166 | | 12.2 | 0.166 | | 28.0 | 0.118 | | 4.92 | 0.062 | |
| 3.35 | 0.123 | | 12.6 | 0.199 | | 12.6 | 0.199 | | 33.7 | 0.101 | | 5.00 | 0.058 | |
| 3.50 | 0.103 | | | | | | | | 34.6 | 0.093 | | 5.50 | 0.046 | |
| 3.53 | 0.103 | | | | | | | | 35.2 | 0.082 | | 5.99 | 0.031 | |
| 5.06 | 0.123 | | | | | | | | 35.9 | 0.064 | | 6.09 | 0.040 | |
| 6.14 | 0.234 | | | | | | | | | | | 6.16 | 0.056 | |
| 6.21 | 0.361 | | | | | | | | | | | 6.20 | 0.091 | |
| 6.28 | 0.410 | | | | | | | | | | | 6.29 | 0.325 | |
| 6.62 | 0.492 | | | | | | | | | | | 6.51 | 0.504 | |
| 6.80 | 0.511 | | | | | | | | | | | 6.60 | 0.569 | |
| 7.03 | 0.511 | | | | | | | | | | | 6.71 | 0.638 | |
| 7.23 | 0.480 | | | | | | | | | | | 6.82 | 0.694 | |
| 7.29 | 0.446 | | | | | | | | | | | 6.92 | 0.722 | |
| 7.36 | 0.383 | | | | | | | | | | | 7.00 | 0.731 | |
| | | | | | | | | | | | | 7.04 | 0.731 | |
| | | | | | | | | | | | | 7.08 | 0.722 | |
| | | | | | | | | | | | | 7.17 | 0.643 | |
| | | | | | | | | | | | | 7.28 | 0.520 | |
| | | | | | | | | | | | | 7.35 | 0.468 | |
| | | | | | | | | | | | | 7.46 | 0.401 | |
| | | | | | | | | | | | | 7.57 | 0.356 | |
| | | | | | | | | | | | | 7.72 | 0.321 | |
| | | | | | | | | | | | | 8.06 | 0.261 | |
| | | | | | | | | | | | | 8.31 | 0.236 | |
| | | | | | | | | | | | | 8.60 | 0.215 | |
| | | | | | | | | | | | | 9.01 | 0.197 | |
| | | | | | | | | | | | | 9.51 | 0.186 | |
| | | | | | | | | | | | | 10.00 | 0.183 | |
| | | | | | | | | | | | | 10.60 | 0.175 | |
| | | | | | | | | | | | | 10.94 | 0.172 | |
| | | | | | | | | | | | | 11.24 | 0.172 | |
| | | | | | | | | | | | | 11.50 | 0.178 | |
| | | | | | | | | | | | | 11.84 | 0.182 | |
| | | | | | | | | | | | | 12.31 | 0.194 | |
| | | | | | | | | | | | | 12.67 | 0.203 | |
| | | | | | | | | | | | | 13.09 | 0.210 | |
| | | | | | | | | | | | | 13.31 | 0.204 | |
| | | | | | | | | | | | | 13.73 | 0.189 | |
| | | | | | | | | | | | | 14.05 | 0.179 | |
| | | | | | | | | | | | | 14.51 | 0.176 | |
| | | | | | | | | | | | | 15.13 | 0.173 | |
| | | | | | | | | | | | | 16.02 | 0.167 | |
| | | | | | | | | | | | | 16.65 | 0.167 | |
| | | | | | | | | | | | | 17.01 | 0.172 | |
| | | | | | | | | | | | | 17.40 | 0.176 | |
| | | | | | | | | | | | | 17.66 | 0.182 | |
| | | | | | | | | | | | | 18.02 | 0.186 | |
| | | | | | | | | | | | | 18.73 | 0.187 | |
| | | | | | | | | | | | | 20.06 | 0.189 | |
| | | | | | | | | | | | | 22.00 | 0.180 | |
| | | | | | | | | | | | | 22.34 | 0.191 | |
| | | | | | | | | | | | | 22.99 | 0.194 | |
| | | | | | | | | | | | | 24.00 | 0.193 | |

CURVE 27
T = 293.

CURVE 26
T = 293.

CURVE 25
T = 293.

CURVE 24
T = 293.

TABLE 7-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------|--------|
| 0.29 | 0.589 |
| 0.29 | 0.493 |
| 0.35 | 0.477 |
| 0.41 | 0.605 |
| 0.47 | 0.811 |
| 0.50 | 0.828 |
| 0.50 | 0.862 |
| 0.66 | 0.891 |
| 0.86 | 0.891 |
| 1.05 | 0.876 |
| 1.26 | 0.860 |
| 1.41 | 0.855 |
| 1.61 | 0.842 |
| 1.70 | 0.815 |
| 1.91 | 0.790 |
| 2.01 | 0.770 |
| 2.11 | 0.741 |

CURVE 26
 T = 293.

d. Angular Spectral Reflectance (Wavelength Dependence)

A total of three sets of experimental data were located for the wavelength dependence of the angular spectral reflectance. The data are listed in Table 7-12 and shown in Figures 7-7 and 7-8. Specimen characterization and measurement information for the data are given in Table 7-11.

A provisional set of values, based on curve 2, is listed in Table 7-10 and shown in Figure 7-7. These room temperature values hold for a polished, 1/32 in. thick specimen of pyrolytic boron nitride manufactured by High Temperature Materials, Inc., with the angles θ and θ' both equal to 20° . An uncertainty of 30% or less is assigned.

TABLE 7-10. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm : TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ |
|------------------|--------|-----------|--------|-----------|--------|
| PYROLYTIC POLISH | | | | | |
| 0.79MM THICK | | | | | |
| T = 293 | | | | | |
| 3.0 | 0.101 | 6.6 | 0.352 | 10.2 | 0.155 |
| 3.1 | 0.092 | 6.7 | 0.424 | 10.3 | 0.153 |
| 3.2 | 0.085 | 6.8 | 0.496 | 10.4 | 0.151 |
| 3.3 | 0.080 | 6.9 | 0.574 | 10.5 | 0.150 |
| 3.4 | 0.076 | 6.95 | 0.620 | 10.6 | 0.148 |
| 3.5 | 0.073 | 6.98 | 0.631 | 10.7 | 0.147 |
| 3.6 | 0.071 | 7.0 | 0.635 | 10.8 | 0.145 |
| 3.7 | 0.069 | 7.04 | 0.630 | 10.9 | 0.143 |
| 3.8 | 0.067 | 7.1 | 0.595 | 11.0 | 0.142 |
| 3.9 | 0.066 | 7.2 | 0.540 | 11.1 | 0.140 |
| 4.0 | 0.065 | 7.3 | 0.490 | 11.2 | 0.139 |
| 4.1 | 0.064 | 7.4 | 0.444 | 11.3 | 0.137 |
| 4.2 | 0.063 | 7.5 | 0.404 | 11.4 | 0.136 |
| 4.3 | 0.062 | 7.6 | 0.364 | 11.5 | 0.134 |
| 4.4 | 0.061 | 7.7 | 0.332 | 11.6 | 0.132 |
| 4.5 | 0.060 | 7.8 | 0.302 | 11.7 | 0.131 |
| 4.6 | 0.059 | 7.9 | 0.277 | 11.8 | 0.129 |
| 4.7 | 0.058 | 8.0 | 0.256 | 11.9 | 0.128 |
| 4.8 | 0.056 | 8.1 | 0.240 | 12.0 | 0.126 |
| 4.9 | 0.055 | 8.2 | 0.226 | 12.1 | 0.124 |
| 5.0 | 0.054 | 8.3 | 0.214 | 12.2 | 0.123 |
| 5.1 | 0.052 | 8.4 | 0.204 | 12.3 | 0.120 |
| 5.2 | 0.050 | 8.5 | 0.196 | 12.4 | 0.122 |
| 5.3 | 0.048 | 8.6 | 0.190 | 12.5 | 0.126 |
| 5.4 | 0.044 | 8.7 | 0.184 | 12.6 | 0.135 |
| 5.5 | 0.041 | 8.8 | 0.180 | 12.7 | 0.148 |
| 5.6 | 0.037 | 8.9 | 0.177 | 12.8 | 0.159 |
| 5.7 | 0.032 | 9.0 | 0.176 | 12.9 | 0.169 |
| 5.8 | 0.026 | 9.1 | 0.174 | 13.0 | 0.175 |
| 5.85 | 0.023 | 9.2 | 0.172 | 13.1 | 0.180 |
| 5.90 | 0.022 | 9.3 | 0.170 | 13.2 | 0.184 |
| 5.93 | 0.021 | 9.4 | 0.168 | 13.3 | 0.185 |
| 5.98 | 0.027 | 9.5 | 0.167 | 13.4 | 0.186 |
| 6.0 | 0.032 | 9.6 | 0.165 | 13.5 | 0.184 |
| 6.1 | 0.074 | 9.7 | 0.163 | 13.6 | 0.182 |
| 6.2 | 0.122 | 9.8 | 0.162 | 13.7 | 0.177 |
| 6.3 | 0.172 | 9.9 | 0.160 | | |
| 6.4 | 0.228 | 10.0 | 0.158 | | |
| 6.5 | 0.288 | 10.1 | 0.156 | | |
| PYROLYTIC POLISH | | | | | |
| 0.79MM THICK | | | | | |
| T = 293 (CONT.) | | | | | |
| | | 6.6 | 0.352 | 10.2 | 0.155 |
| | | 6.7 | 0.424 | 10.3 | 0.153 |
| | | 6.8 | 0.496 | 10.4 | 0.151 |
| | | 6.9 | 0.574 | 10.5 | 0.150 |
| | | 6.95 | 0.620 | 10.6 | 0.148 |
| | | 6.98 | 0.631 | 10.7 | 0.147 |
| | | 7.0 | 0.635 | 10.8 | 0.145 |
| | | 7.04 | 0.630 | 10.9 | 0.143 |
| | | 7.1 | 0.595 | 11.0 | 0.142 |
| | | 7.2 | 0.540 | 11.1 | 0.140 |
| | | 7.3 | 0.490 | 11.2 | 0.139 |
| | | 7.4 | 0.444 | 11.3 | 0.137 |
| | | 7.5 | 0.404 | 11.4 | 0.136 |
| | | 7.6 | 0.364 | 11.5 | 0.134 |
| | | 7.7 | 0.332 | 11.6 | 0.132 |
| | | 7.8 | 0.302 | 11.7 | 0.131 |
| | | 7.9 | 0.277 | 11.8 | 0.129 |
| | | 8.0 | 0.256 | 11.9 | 0.128 |
| | | 8.1 | 0.240 | 12.0 | 0.126 |
| | | 8.2 | 0.226 | 12.1 | 0.124 |
| | | 8.3 | 0.214 | 12.2 | 0.123 |
| | | 8.4 | 0.204 | 12.3 | 0.120 |
| | | 8.5 | 0.196 | 12.4 | 0.122 |
| | | 8.6 | 0.190 | 12.5 | 0.126 |
| | | 8.7 | 0.184 | 12.6 | 0.135 |
| | | 8.8 | 0.180 | 12.7 | 0.148 |
| | | 8.9 | 0.177 | 12.8 | 0.159 |
| | | 9.0 | 0.176 | 12.9 | 0.169 |
| | | 9.1 | 0.174 | 13.0 | 0.175 |
| | | 9.2 | 0.172 | 13.1 | 0.180 |
| | | 9.3 | 0.170 | 13.2 | 0.184 |
| | | 9.4 | 0.168 | 13.3 | 0.185 |
| | | 9.5 | 0.167 | 13.4 | 0.186 |
| | | 9.6 | 0.165 | 13.5 | 0.184 |
| | | 9.7 | 0.163 | 13.6 | 0.182 |
| | | 9.8 | 0.162 | 13.7 | 0.177 |
| | | 9.9 | 0.160 | | |
| | | 10.0 | 0.158 | | |
| | | 10.1 | 0.156 | | |

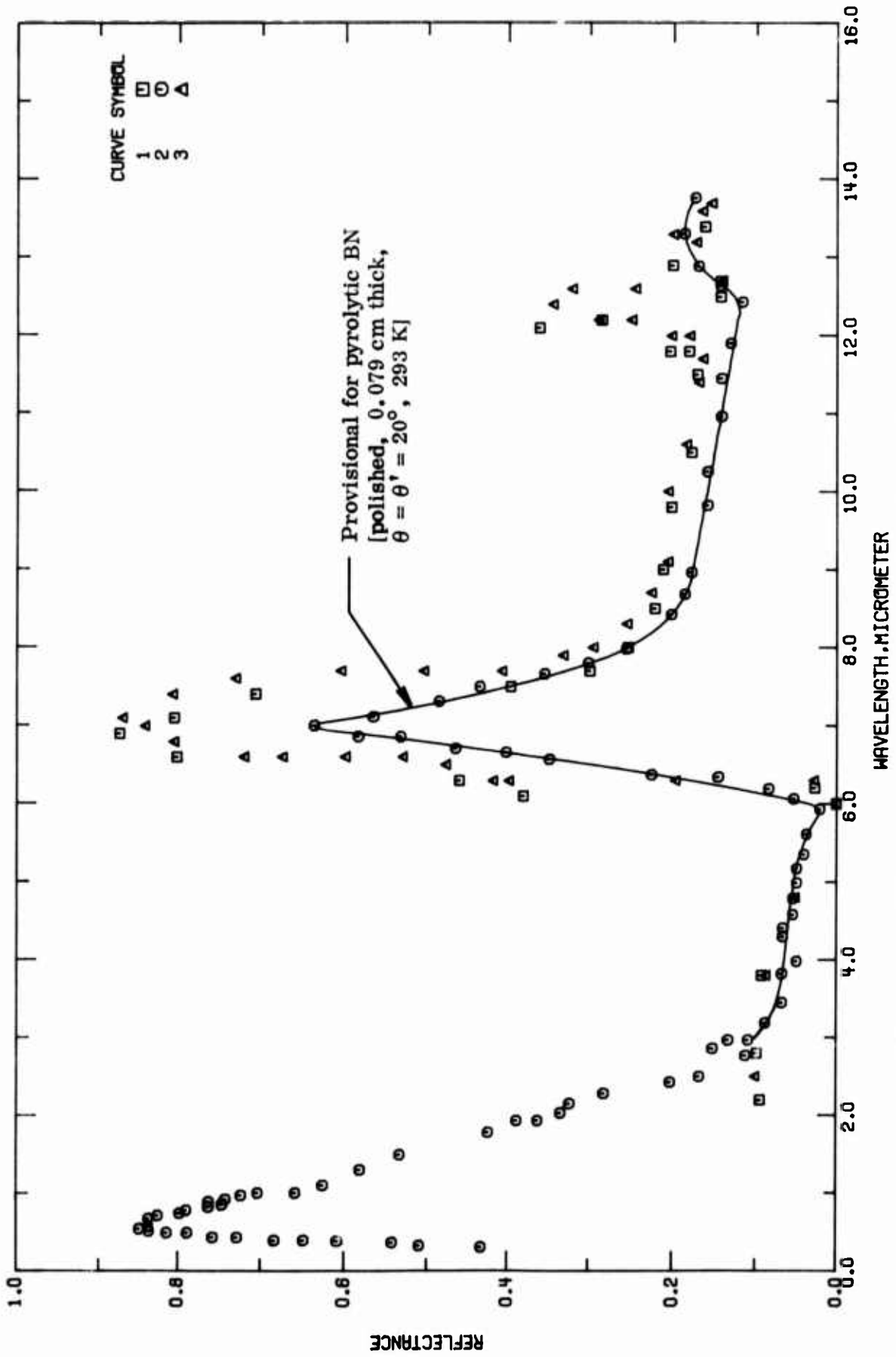
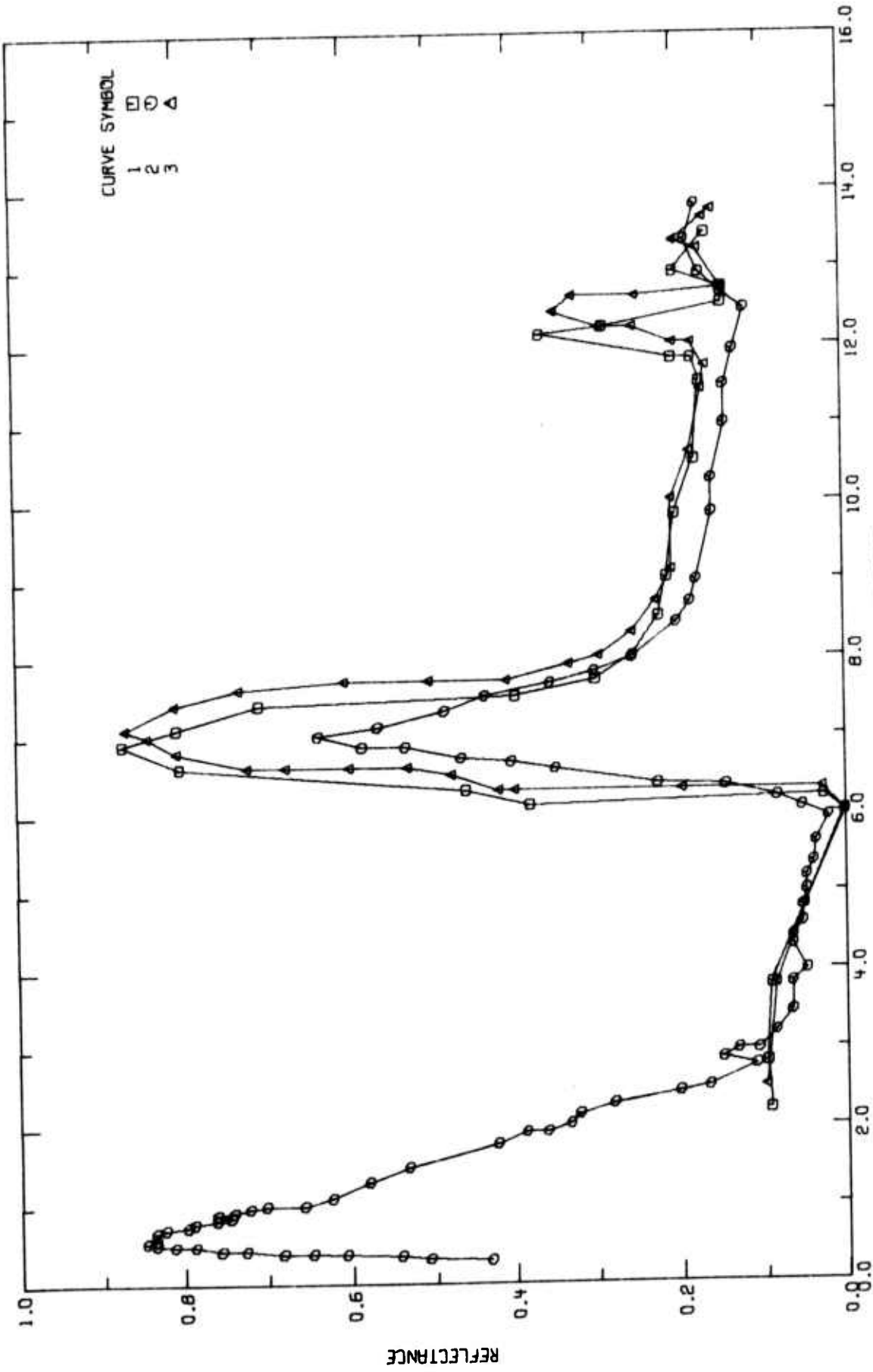


FIGURE 7-7. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).



WAVELENGTH, MICROMETER

FIGURE 7-8. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 7-11. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T31145 | McCarthy, D. E. | 1968 | 2.2-50 | 293 | | Synthetic specimen; thickness 6.0 mm; flat to 10 fringes or better; reference standard aluminum mirror; commercial double-beam instrument used; temperature not explicitly given, assumed to be 293 K; smooth values from figure; $\theta = 30^\circ$. |
| 2 T34724 | Durand, S. L. and Houston, K. C. | 1966 | 0.3-25 | 293 | Pyrolytic | Specimen size about $2 \times 3 \times 0.5$ in.; final dimensions 1 in. diameter, $1/32$ in. thick; manufactured by High Temperature Materials, Inc., Lowell, Mass.; both surfaces ground to a finish of approx. $18 \mu\text{in.}$; AB surface (surface parallel to basal planes or planes of deposition) radiating; Gier Dunkle Reflectometer used; data from figure; specimen cemented to 1 in. diameter aluminum disk with 3 M black low reflectivity paint which served as an opaque substrate; (no change in reflectivity from normal incidence to about 25° from normal); measurement temperature specified as room temperature, 293 K assigned; $\theta = 20^\circ$, $\theta' = 20^\circ$. |
| 3 T40525 | McCarthy, D. E. | 1966 | 2.5-50 | 313 | | Polycrystalline specimen; thickness 6 mm; ground and polished to 5 fringes or better; smooth values from figure; $\theta = 30^\circ$, $\theta' = 30^\circ$. |

TABLE 7-12. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| CURVE 1 T = 293. | | CURVE 2 T = 293. | | CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 3 (CONT.) | |
|---------------------|--------|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 2.20 | 0.094 | 0.30 | 0.432 | 3.19 | 0.068 | 13.31 | 0.186 | 7.1 | 0.069 | 38.1 | 0.153 |
| 2.80 | 0.096 | 0.32 | 0.508 | 3.45 | 0.068 | 13.77 | 0.173 | 7.4 | 0.806 | 40.1 | 0.153 |
| 3.80 | 0.092 | 0.36 | 0.542 | 3.82 | 0.068 | 16.58 | 0.174 | 7.6 | 0.730 | 41.1 | 0.151 |
| 6.00 | 0.000 | 0.38 | 0.607 | 3.98 | 0.050 | 17.21 | 0.181 | 7.7 | 0.504 | 42.0 | 0.151 |
| 6.20 | 0.027 | 0.39 | 0.647 | 4.41 | 0.067 | 17.68 | 0.194 | 7.7 | 0.507 | 43.2 | 0.154 |
| 6.10 | 0.379 | 0.39 | 0.682 | 4.58 | 0.055 | 18.08 | 0.205 | 7.7 | 0.407 | 44.2 | 0.154 |
| 6.30 | 0.453 | 0.43 | 0.727 | 4.79 | 0.055 | 18.40 | 0.205 | 7.9 | 0.331 | 45.5 | 0.154 |
| 6.60 | 0.800 | 0.43 | 0.756 | 4.99 | 0.050 | 18.85 | 0.199 | 8.0 | 0.295 | 45.8 | 0.154 |
| 6.90 | 0.872 | 0.49 | 0.787 | 5.17 | 0.050 | 19.43 | 0.220 | 8.3 | 0.255 | 46.9 | 0.154 |
| 7.10 | 0.803 | 0.49 | 0.812 | 5.35 | 0.041 | 19.97 | 0.202 | 8.7 | 0.226 | 48.1 | 0.154 |
| 7.40 | 0.705 | 0.51 | 0.834 | 5.61 | 0.038 | 20.40 | 0.223 | 9.1 | 0.206 | 50.0 | 0.154 |
| 7.50 | 0.395 | 0.54 | 0.847 | 5.93 | 0.021 | 20.99 | 0.213 | 10.0 | 0.206 | | |
| 7.70 | 0.298 | 0.57 | 0.835 | 6.06 | 0.054 | 21.47 | 0.220 | 10.6 | 0.184 | | |
| 8.00 | 0.253 | 0.67 | 0.835 | 6.19 | 0.084 | 21.99 | 0.220 | 11.4 | 0.169 | | |
| 8.50 | 0.221 | 0.71 | 0.823 | 6.34 | 0.145 | 22.38 | 0.230 | 11.7 | 0.164 | | |
| 9.00 | 0.211 | 0.74 | 0.796 | 6.37 | 0.225 | 22.69 | 0.230 | 12.0 | 0.180 | | |
| 9.80 | 0.201 | 0.78 | 0.788 | 6.57 | 0.347 | 23.14 | 0.220 | 12.0 | 0.202 | | |
| 10.5 | 0.177 | 0.82 | 0.761 | 6.66 | 0.401 | 23.65 | 0.222 | 12.2 | 0.250 | | |
| 11.5 | 0.170 | 0.85 | 0.745 | 6.71 | 0.464 | 24.01 | 0.209 | 12.2 | 0.289 | | |
| 11.8 | 0.180 | 0.89 | 0.761 | 6.86 | 0.532 | 24.38 | 0.219 | 12.4 | 0.344 | | |
| 11.8 | 0.203 | 0.92 | 0.741 | 6.86 | 0.583 | 25.00 | 0.235 | 12.6 | 0.321 | | |
| 12.1 | 0.360 | 0.97 | 0.722 | 7.00 | 0.635 | | | 12.6 | 0.246 | | |
| 12.2 | 0.285 | 1.00 | 0.702 | 7.11 | 0.565 | | | 12.7 | 0.142 | | |
| 12.5 | 0.143 | 1.00 | 0.657 | 7.31 | 0.485 | | | 13.2 | 0.172 | | |
| 12.7 | 0.143 | 1.10 | 0.624 | 7.50 | 0.434 | | | 13.3 | 0.200 | | |
| 12.9 | 0.200 | 1.30 | 0.580 | 7.66 | 0.353 | | | 13.6 | 0.165 | | |
| 13.4 | 0.161 | 1.49 | 0.533 | 7.80 | 0.300 | | | 13.7 | 0.154 | | |
| 14.9 | 0.154 | 1.78 | 0.423 | 7.88 | 0.255 | | | 15.0 | 0.154 | | |
| 22.7 | 0.172 | 1.93 | 0.387 | 8.42 | 0.201 | | | 17.3 | 0.158 | | |
| 25.3 | 0.190 | 1.93 | 0.361 | 8.68 | 0.185 | | | 20.0 | 0.167 | | |
| 26.5 | 0.190 | 2.03 | 0.333 | 8.95 | 0.177 | | | 22.2 | 0.172 | | |
| 28.2 | 0.168 | 2.15 | 0.322 | 9.82 | 0.158 | | | 25.0 | 0.187 | | |
| 29.7 | 0.143 | 2.28 | 0.281 | 10.25 | 0.158 | | | 26.3 | 0.187 | | |
| 31.7 | 0.132 | 2.43 | 0.202 | 10.96 | 0.142 | | | 28.3 | 0.167 | | |
| 35.0 | 0.154 | 2.50 | 0.167 | 11.45 | 0.142 | | | 30.1 | 0.137 | | |
| 50.0 | 0.156 | 2.77 | 0.112 | 11.90 | 0.131 | | | 30.8 | 0.134 | | |
| | | 2.86 | 0.151 | 12.43 | 0.117 | | | 31.6 | 0.133 | | |
| | | 2.97 | 0.133 | 12.64 | 0.143 | | | 33.4 | 0.142 | | |
| | | 2.97 | 0.109 | 12.89 | 0.169 | | | 35.0 | 0.154 | | |
| | | | | | | | | 37.1 | 0.150 | | |

CURVE 3
T = 313.

2.5 0.101
 3.8 0.088
 4.8 0.053
 6.0 0.000
 6.3 0.029
 6.3 0.197
 6.3 0.398
 6.3 0.418
 6.5 0.477
 6.6 0.530
 6.6 0.599
 6.6 0.674
 6.6 0.720
 6.8 0.804
 7.0 0.840

e. Normal Spectral Transmittance (Wavelength Dependence)

A total of seven sets of experimental data were located for the wavelength dependence of the normal spectral transmittance of boron nitride. The data are listed in Table 7-15 and shown in Figures 7-9 and 7-10. Specimen characterization and measurement information for the data are given in Table 7-14.

For the purposes of this report, the first four data sets are useless in aiding to arrive at evaluated data. Curve 5 forms the basis of a typical set of values which are valid at room temperature for platelets of yellow, undoped, single-crystals of cubic boron nitride. An assignment of typical is necessitated because of uninformed specimen dimensions. The uncertainty assigned is 30% or more.

TABLE 7-13. TYPICAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|------------------------------------|--|------------------------------------|--|------------------------------------|--|------------------------------------|--|------------------------------------|--|
| CUBIC, UNDOPE YELLOW T = 293 | CUBIC, UNDOPE YELLOW T = 293 (CONT.) | CUBIC, UNDOPE YELLOW T = 293 | CUBIC, UNDOPE YELLOW T = 293 (CONT.) | CUBIC, UNDOPE YELLOW T = 293 | CUBIC, UNDOPE YELLOW T = 293 (CONT.) | CUBIC, UNDOPE YELLOW T = 293 | CUBIC, UNDOPE YELLOW T = 293 (CONT.) | CUBIC, UNDOPE YELLOW T = 293 | CUBIC, UNDOPE YELLOW T = 293 (CONT.) |
| 0.20 | 0.000 | 2.0 | 0.739 | 5.43 | 0.253 | 9.0 | 0.000 | 12.9 | 0.565 |
| 0.24 | 0.014 | 2.1 | 0.738 | 5.47 | 0.191 | 9.1 | 0.000 | 13.0 | 0.567 |
| 0.26 | 0.030 | 2.2 | 0.738 | 5.50 | 0.206 | 9.2 | 0.000 | | |
| 0.28 | 0.040 | 2.3 | 0.733 | 5.55 | 0.236 | 9.3 | 0.000 | | |
| 0.30 | 0.053 | 2.4 | 0.738 | 5.6 | 0.256 | 9.4 | 0.000 | | |
| 0.31 | 0.058 | 2.5 | 0.738 | 5.7 | 0.284 | 9.5 | 0.000 | | |
| 0.33 | 0.079 | 2.6 | 0.738 | 5.8 | 0.304 | 9.6 | 0.000 | | |
| 0.36 | 0.108 | 2.7 | 0.738 | 5.9 | 0.319 | 9.7 | 0.000 | | |
| 0.38 | 0.132 | 2.8 | 0.738 | 6.0 | 0.322 | 9.8 | 0.000 | | |
| 0.40 | 0.156 | 2.9 | 0.738 | 6.1 | 0.344 | 9.9 | 0.000 | | |
| 0.41 | 0.169 | 3.0 | 0.738 | 6.2 | 0.356 | 10.0 | 0.000 | | |
| 0.44 | 0.203 | 3.1 | 0.738 | 6.3 | 0.367 | 10.1 | 0.056 | | |
| 0.48 | 0.256 | 3.2 | 0.738 | 6.4 | 0.378 | 10.2 | 0.102 | | |
| 0.50 | 0.303 | 3.3 | 0.738 | 6.5 | 0.389 | 10.3 | 0.146 | | |
| 0.53 | 0.352 | 3.4 | 0.738 | 6.6 | 0.399 | 10.4 | 0.186 | | |
| 0.57 | 0.414 | 3.5 | 0.738 | 6.7 | 0.419 | 10.5 | 0.226 | | |
| 0.60 | 0.470 | 3.6 | 0.738 | 6.8 | 0.446 | 10.6 | 0.252 | | |
| 0.61 | 0.489 | 3.7 | 0.738 | 6.9 | 0.476 | 10.7 | 0.293 | | |
| 0.63 | 0.543 | 3.8 | 0.738 | 7.0 | 0.507 | 10.8 | 0.326 | | |
| 0.65 | 0.585 | 3.9 | 0.737 | 7.1 | 0.574 | 10.9 | 0.354 | | |
| 0.68 | 0.620 | 4.0 | 0.735 | 7.2 | 0.618 | 11.0 | 0.380 | | |
| 0.70 | 0.651 | 4.1 | 0.733 | 7.3 | 0.656 | 11.1 | 0.403 | | |
| 0.72 | 0.680 | 4.15 | 0.730 | 7.4 | 0.714 | 11.2 | 0.427 | | |
| 0.74 | 0.693 | 4.20 | 0.726 | 7.5 | 0.076 | 11.3 | 0.449 | | |
| 0.77 | 0.717 | 4.25 | 0.722 | 7.6 | 0.016 | 11.4 | 0.467 | | |
| 0.80 | 0.726 | 4.30 | 0.714 | 7.63 | 0.000 | 11.5 | 0.483 | | |
| 0.803 | 0.736 | 4.4 | 0.675 | 7.7 | 0.000 | 11.6 | 0.496 | | |
| 0.806 | 0.7375 | 4.5 | 0.624 | 7.8 | 0.000 | 11.7 | 0.508 | | |
| 0.90 | 0.738 | 4.6 | 0.555 | 7.9 | 0.000 | 11.8 | 0.517 | | |
| 1.0 | 0.739 | 4.7 | 0.491 | 8.0 | 0.000 | 11.9 | 0.526 | | |
| 1.1 | 0.739 | 4.8 | 0.414 | 8.1 | 0.000 | 12.0 | 0.533 | | |
| 1.2 | 0.738 | 4.9 | 0.306 | 8.2 | 0.000 | 12.1 | 0.540 | | |
| 1.3 | 0.739 | 5.0 | 0.181 | 8.3 | 0.000 | 12.2 | 0.545 | | |
| 1.4 | 0.738 | 5.04 | 0.182 | 8.4 | 0.000 | 12.3 | 0.553 | | |
| 1.5 | 0.738 | 5.1 | 0.164 | 8.5 | 0.000 | 12.4 | 0.554 | | |
| 1.6 | 0.738 | 5.2 | 0.191 | 8.6 | 0.000 | 12.5 | 0.557 | | |
| 1.7 | 0.738 | 5.3 | 0.204 | 8.7 | 0.000 | 12.6 | 0.560 | | |
| 1.8 | 0.738 | 5.35 | 0.216 | 8.8 | 0.000 | 12.7 | 0.562 | | |
| 1.9 | 0.738 | 5.40 | 0.232 | 8.9 | 0.000 | 12.8 | 0.563 | | |

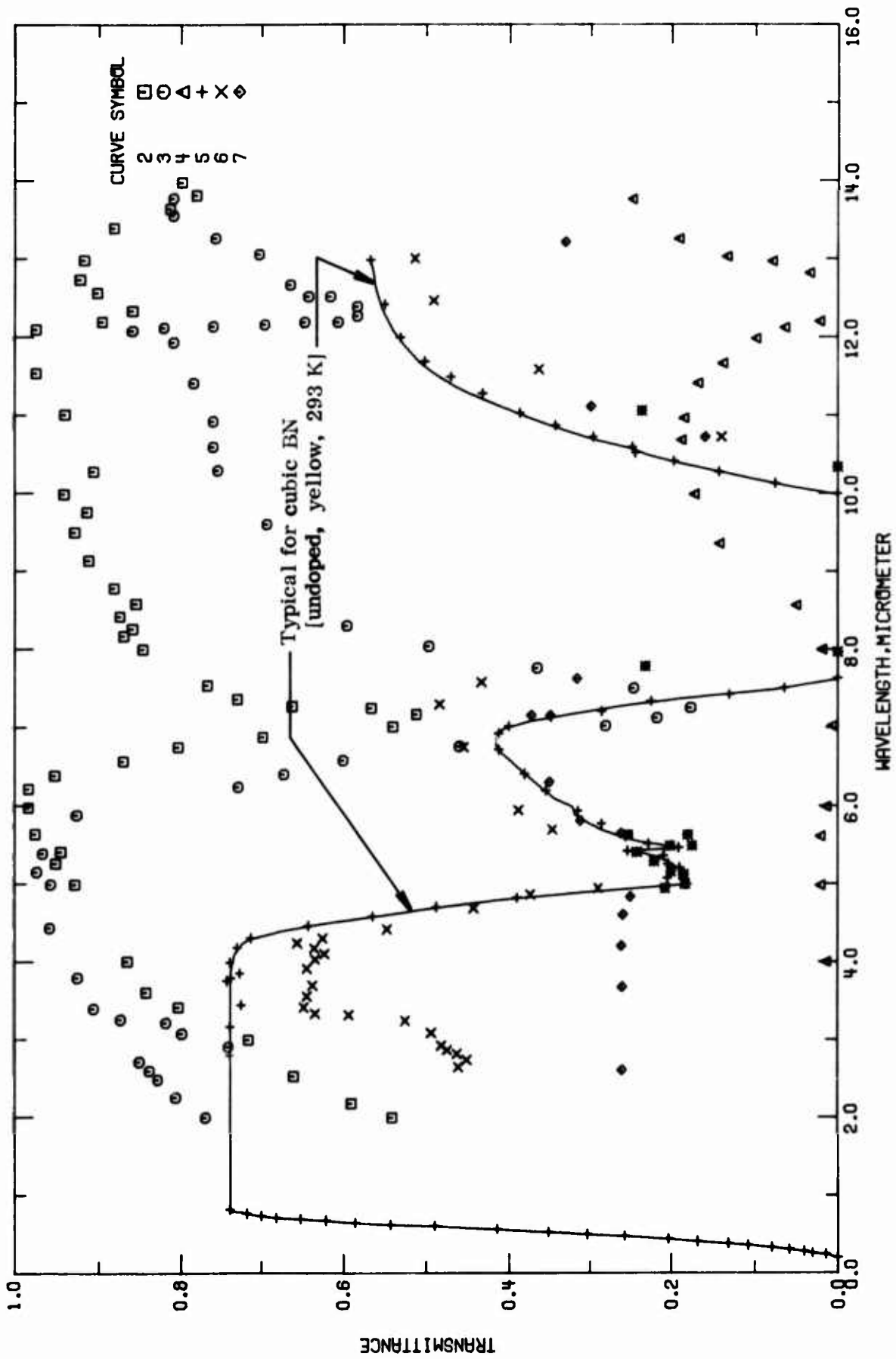


FIGURE 7-9. TYPICAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

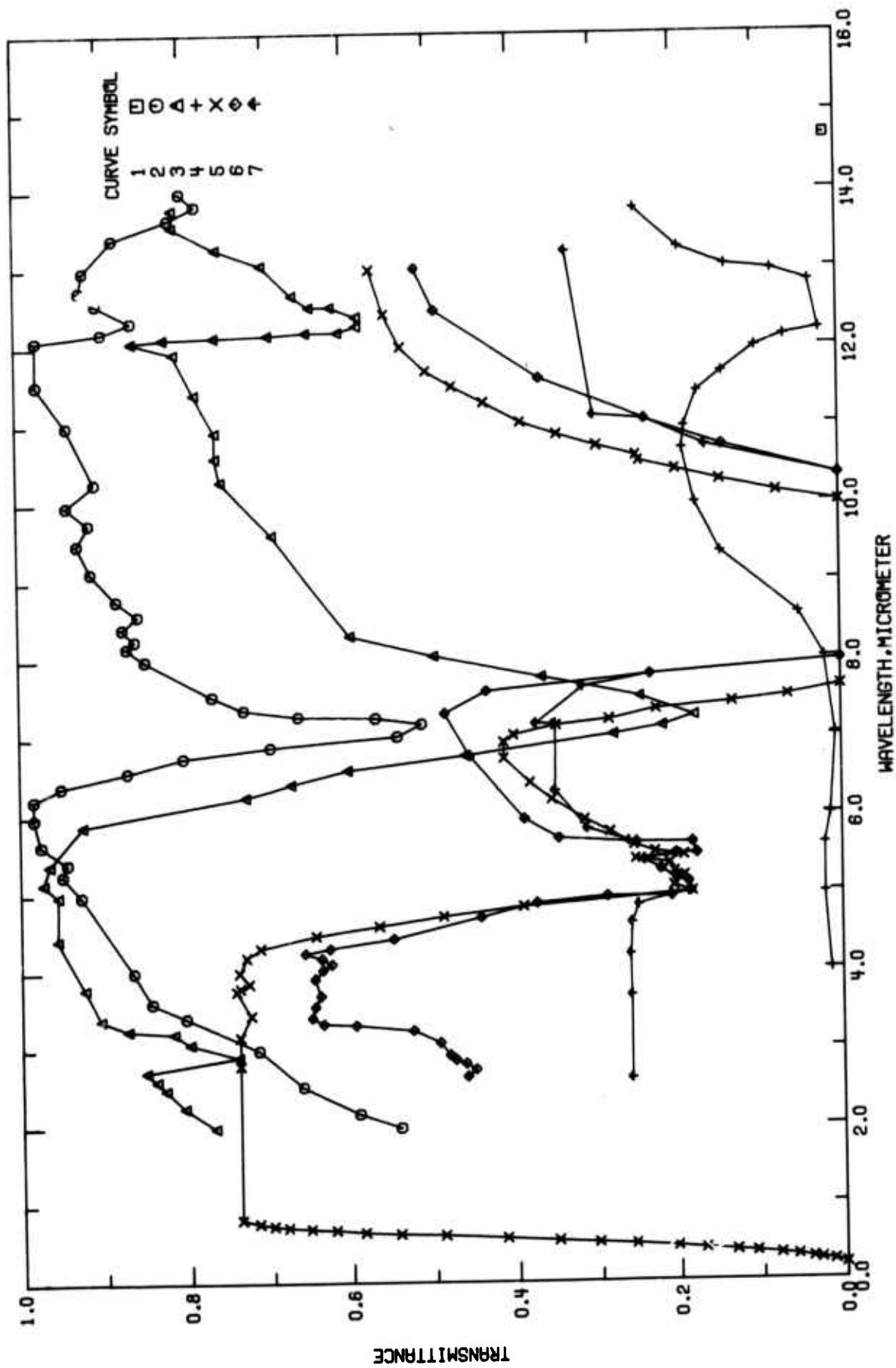


FIGURE 7-10. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 7-14. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T51145 | McCarthy, D. E. | 1968 | 15-50 | 293 | | Synthetic specimen; thickness 6.0 mm; flat to 10 fringes or better. Reference standard aluminum mirror; commercial double-beam instrument used; temperature not explicitly given, presumed to be 293 K; smooth values from I_{figure} ; $\theta = 0^\circ$, $\phi = 0^\circ$. |
| 2 T58818 | Miller, F. A. and Wilkins, C. H. | 1952 | 2.0-16 | 293 | | Pure; fine powder suspended in Nujol; measurements made with Baird Model A spectrophotometer; smooth values from figure; wavelength measurements accurate to approx. $\pm 0.03 \mu$; portion of spectra from 2 to just over 7 μm run in fluorolube; dip in spectra just below 14 μm a Nujol band; measurement temperature not given explicitly, assumed to be 293 K. |
| 3 T60470 | Brame, E. G., Jr., Martyr, J. L., and Meloche, V. W. | 1957 | 2-16 | 293 | | Hexagonal crystal structure; disk 1 mm thick and 12 mm in diameter; Baird Associates Model B spectrophotometer used; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 4 T29708 | Redfield, D. and Baum, R. L. | 1961 | 4-15 | 293 | | 1 mg BN in 300 mg KHS-5 pressed at 270 000 psi to an 0.375 in diameter and 0.025 in thickness; smooth values from figure. |
| 5 A00014 | DeVries, R. C. | 1972 | 0.2-13 | 293 | | Single-crystal (yellow, undoped); data taken on assemblage of small hexagonal-shaped platelets of cubic BN; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 6 T42972 | Gielisse, P. J., Mitra, S. S., Plendi, J. N., Griffis, R. D., Mansur, L. C., Marshall, R., and Pascoe, E. A. | 1967 | 2.7-24 | 293 | | Single crystal platelets with cubic structure (30 μm thick); grown at very high pressure and temperature; $10^{15} \Omega$ cm electrical resistivity; smooth values from figure; percent absorption reported on figure, normal spectral transmittance arrived at by equating percent normal spectral transmittance to 1.0 minus percent absorption. |
| 7 T42972 | Gielisse, P. J., et al. | 1967 | 2.6-27 | 293 | | Similar to the above specimen except beryllium doped. |

TABLE 7-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF BORON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | T | λ | T | λ | T |
|-----------------|-------|-----------------|-------|-----------------|-------|
| CURVE 6 (CONT.) | | CURVE 6 (CONT.) | | CURVE 7 (CONT.) | |
| 2.82 | 0.462 | 11.60 | 0.364 | 11.12 | 0.299 |
| 2.87 | 0.474 | 12.48 | 0.490 | 13.23 | 0.331 |
| 2.93 | 0.481 | 13.02 | 0.513 | 17.33 | 0.349 |
| 3.09 | 0.493 | 14.06 | 0.505 | 25.88 | 0.364 |
| 3.25 | 0.525 | 14.84 | 0.536 | | |
| 3.32 | 0.593 | 15.38 | 0.512 | | |
| 3.34 | 0.533 | 16.42 | 0.491 | | |
| 3.42 | 0.647 | 17.61 | 0.506 | | |
| 3.56 | 0.643 | 17.86 | 0.660 | | |
| 3.70 | 0.635 | 24.27 | 0.774 | | |
| 3.82 | 0.643 | | | | |
| 4.037 | 0.633 | | | | |
| 4.107 | 0.622 | | | | |
| 4.177 | 0.634 | | | | |
| 4.246 | 0.655 | | | | |
| 4.307 | 0.624 | 2.61 | 0.259 | | |
| 4.429 | 0.547 | 3.68 | 0.259 | | |
| 4.695 | 0.442 | 4.21 | 0.260 | | |
| 4.873 | 0.374 | 4.61 | 0.250 | | |
| 4.951 | 0.289 | 4.84 | 0.249 | | |
| 4.948 | 0.207 | 4.95 | 0.207 | | |
| 5.005 | 0.183 | 5.00 | 0.183 | | |
| 5.123 | 0.185 | 5.123 | 0.185 | | |
| 5.160 | 0.200 | 5.160 | 0.200 | | |
| 5.294 | 0.220 | 5.294 | 0.220 | | |
| 5.414 | 0.241 | 5.414 | 0.241 | | |
| 5.492 | 0.201 | 5.492 | 0.201 | | |
| 5.492 | 0.175 | 5.492 | 0.175 | | |
| 5.634 | 0.180 | 5.634 | 0.180 | | |
| 5.640 | 0.251 | 5.640 | 0.251 | | |
| 5.705 | 0.347 | 5.653 | 0.261 | | |
| 5.952 | 0.388 | 5.817 | 0.312 | | |
| 6.761 | 0.454 | 6.309 | 0.351 | | |
| 7.310 | 0.483 | 7.163 | 0.350 | | |
| 7.593 | 0.433 | 7.169 | 0.373 | | |
| 7.794 | 0.231 | 7.639 | 0.316 | | |
| 7.968 | 0.000 | 7.794 | 0.231 | | |
| 10.34 | 0.000 | 7.968 | 0.600 | | |
| 10.73 | 0.140 | 10.34 | 0.000 | | |
| 11.07 | 0.235 | 13.73 | 0.160 | | |
| | | 11.07 | 0.235 | | |

CURVE 7
 T = 293.

4.8. Calcium Aluminum Silicate

Since data evaluation was asked to be carried out on the specific kind of calcium aluminum silicate known as Corning 9753, the treatment in this section will concentrate on that material.

Corning 9753 is a solid solution of 30% CaO, 40% Al₂O₃, and 30% SiO₂ and is an infrared transmitting glass. It is a product of the Corning Glass Works, Corning, New York 14830. Other names by which it is known include Corning Code 9753, glass 9753, CGW-Glass 9753, Corning 9753 glass, and Cortran Code 9753. Cortran is a secondary trademark of the Corning Glass Works.

This material has several interesting physical properties which lead to its suitability for airborne applications. It melts around 1723 to 1773 K [T28664]. According to the Corning Glass Works specification sheet for Code 9753, copyrighted in 1970, other physical properties are as follows: It has a softening point (extrapolated) of 1254 K, an annealing point of 1105 K, and a strain point of 1073 K. The linear expansion coefficient between 298 and 573 K is $59.5 \times 10^{-7} \text{ C}^{-1}$ while between 29.8 and 973 K it is $72 \times 10^{-7} \text{ C}^{-1}$. Code 9753 has a density of 2.798 g cm^{-3} , a Young's modulus of $14.3 \times 10^6 \text{ psi}$, a shear modulus of $5.6 \times 10^6 \text{ psi}$, and a Poisson's ratio of 0.28. The Knoop hardness is 657.5 for a 100 g load and 601 for a 500 g load. These values of hardness makes this material highly suitable for high-speed airborne applications and coupled with its infrared transmitting properties leads to its use on heat-seeking missiles. The refractive index at $0.4867 \mu\text{m}$ is 1.61251, at $0.5893 \mu\text{m}$ is 1.60475, and at $0.6563 \mu\text{m}$ is 1.60151. The dielectric constant at 1 Mc and 298 K is 8.87 while for the same frequency it is 9.51 at 773 K; it is 8.28 at 298 K, 8.59 at 573 K, 8.66 at 673 K, and 8.76 at 773 K, all at 8600 Mc. The loss tangent at 1 Mc and 298 K is 0.0025 while for the same frequency it is 0.0029 at 773 K; it is 0.011 at 298 K, 0.01 at 573 K, 0.01 at 673 K, and 0.01 at 773 K, all at 8600 Mc. The log of the dc resistivity (ohm-cm) is 18.0 at 523 K, 15.0 at 623 K, and 11.8 at 773 K.

a. Normal Spectral Emittance (Wavelength Dependence)

There are six sets of experimental data available for the wavelength dependence of the normal spectral emittance, $\epsilon(\theta' \approx 0^\circ)$, of calcium aluminum silicate all of which apply to Corning 9753. The data is listed in Table 8-3 and shown in Figures 8-1 and 8-2. Specimen characterization and measurement information for the data are given in Table 8-2. Three data sets are for a specimen 0.3175 cm thick measured at temperatures 473 to 873 K. The remaining three data sets are for a 1.27 cm thick specimen covering the same temperature range.

It is observed that each of the six data sets is for a different combination of thickness and temperature and hence there is no direct confirmatory evidence for an individual data set. As a consequence of this lack of confirmatory evidence, only provisional values are justified. Two provisional curves are given for Corning 9753 for a specimen of 0.3175 cm with one curve applicable to 473 K and the other curve to 873 K. The provisional values are listed in Table 8-1 and shown in Figure 8-1. The thickness of 0.3175 cm is selected so as to be close to a thickness of 0.2 to 0.4 cm which is often used in reporting measurements. These two provisional curves are the same as curves 1 and 3 in Table 8-3 and Figure 8-1 with additional values reported. The uncertainty for the provisional values is within 30%.

It is noted that for curves 1-6 in Tables 8-2 and 8-3, data is not available for wavelengths below 1.5 μm and above 8.0 μm . In addition, data is unavailable over the entire wavelength region for temperatures above 873 K.

Assuming that the normal spectral emittance above 8.0 μm continues at a high and roughly constant value, the magnitude of emittance will be about 0.8 for a 3.175 mm thick specimen from 473 to 873 K.

Corroborating evidence of a high and roughly constant value above 8 μm for a slightly different thickness comes from the provisional values at 293 K for a specimen of 2 mm thick. These values are listed in Table 8-1 and shown in Figure 8-1. They were generated by using Eq. (2.3-2) to find α and using Kirchoff's law, Eq. (2.3-4), to find the normal spectral emittance. The values of the normal spectral transmittance used in Eq. (2.3-2) are the provisional values listed in Table 8-12 and shown in Figure 8-9; these values apply to a temperature of 293 K and a specimen thickness of 2 mm. From 5.0 to 15 μm it was assumed the transmittance was zero. The values of the normal spectral reflectance used in Eq. (2.3-2) are the provisional values listed in Table 8-5 and shown in Figure 8-4; these values apply to a temperature of 293 K and a thickness of 1.99 mm. The uncertainty is thought to be well within 30% over most of the wavelength region.

TABLE 8-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| 2.00MM THICK | | | 2.00MM THICK | | | 2.00MM THICK | | | 3.175MM THICK | | | 3.175MM THICK | | | |
|--------------|------------|-----------|-----------------|-----------|------------|-----------------|------------|-----------|---------------|-----------|------------|-----------------|------------|-----------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| T = 293 | | | T = 293 (CONT.) | | | T = 293 (CONT.) | | | T = 473 | | | T = 473 (CONT.) | | | |
| 0.40 | 0.101 | 5.10 | 0.966 | 3.00 | 0.973 | 12.9 | 0.916 | 2.40 | 0.110 | 4.60 | 0.676 | | | | |
| 0.50 | 0.029 | 5.20 | 0.966 | 3.10 | 0.965 | 13.0 | 0.915 | 2.47 | 0.103 | 4.64 | 0.700 | | | | |
| 0.60 | 0.017 | 5.30 | 0.967 | 9.29 | 0.954 | 13.1 | 0.915 | 2.50 | 0.099 | 4.70 | 0.758 | | | | |
| 0.80 | 0.015 | 5.40 | 0.967 | 9.30 | 0.934 | 13.2 | 0.915 | 2.59 | 0.090 | 4.71 | 0.775 | | | | |
| 0.90 | 0.023 | 5.50 | 0.968 | 9.40 | 0.902 | 13.3 | 0.915 | 2.60 | 0.089 | 4.74 | 0.805 | | | | |
| 1.00 | 0.024 | 5.60 | 0.968 | 9.50 | 0.886 | 13.4 | 0.916 | 2.73 | 0.080 | 4.77 | 0.823 | | | | |
| 1.10 | 0.026 | 5.70 | 0.969 | 9.60 | 0.873 | 13.5 | 0.915 | 2.73 | 0.077 | 4.80 | 0.832 | | | | |
| 1.20 | 0.027 | 5.80 | 0.969 | 9.70 | 0.864 | 13.6 | 0.914 | 2.80 | 0.070 | 4.82 | 0.841 | | | | |
| 1.30 | 0.028 | 5.90 | 0.970 | 9.80 | 0.856 | 13.7 | 0.912 | 2.81 | 0.069 | 4.87 | 0.854 | | | | |
| 1.40 | 0.028 | 6.00 | 0.970 | 9.90 | 0.848 | 13.8 | 0.910 | 2.90 | 0.065 | 4.90 | 0.858 | | | | |
| 1.50 | 0.028 | 6.10 | 0.971 | 10.0 | 0.841 | 13.9 | 0.909 | 2.91 | 0.065 | 4.91 | 0.860 | | | | |
| 1.60 | 0.027 | 6.20 | 0.971 | 10.1 | 0.832 | 14.0 | 0.906 | 3.0 | 0.061 | 4.96 | 0.869 | | | | |
| 1.70 | 0.027 | 6.30 | 0.972 | 10.2 | 0.825 | 14.1 | 0.901 | 3.04 | 0.060 | 5.00 | 0.870 | | | | |
| 1.80 | 0.026 | 6.40 | 0.973 | 10.3 | 0.825 | 14.2 | 0.895 | 3.10 | 0.059 | 5.08 | 0.869 | | | | |
| 2.00 | 0.026 | 6.50 | 0.974 | 10.4 | 0.820 | 14.3 | 0.890 | 3.20 | 0.060 | 5.10 | 0.868 | | | | |
| 2.30 | 0.025 | 6.60 | 0.975 | 10.5 | 0.820 | 14.4 | 0.885 | 3.21 | 0.060 | 5.20 | 0.862 | | | | |
| 2.40 | 0.026 | 6.70 | 0.976 | 10.6 | 0.820 | 14.5 | 0.882 | 3.30 | 0.064 | 5.22 | 0.860 | | | | |
| 2.50 | 0.027 | 6.80 | 0.977 | 10.7 | 0.821 | 14.6 | 0.879 | 3.31 | 0.065 | 5.30 | 0.851 | | | | |
| 2.60 | 0.031 | 6.90 | 0.978 | 10.8 | 0.822 | 14.7 | 0.877 | 3.40 | 0.073 | 5.40 | 0.840 | | | | |
| 2.70 | 0.036 | 7.00 | 0.979 | 10.9 | 0.823 | 14.8 | 0.873 | 3.46 | 0.079 | 5.42 | 0.838 | | | | |
| 2.80 | 0.049 | 7.10 | 0.980 | 11.0 | 0.826 | 14.9 | 0.865 | 3.50 | 0.084 | 5.50 | 0.832 | | | | |
| 2.90 | 0.062 | 7.20 | 0.981 | 11.1 | 0.837 | | | 3.57 | 0.095 | 5.53 | 0.828 | | | | |
| 3.20 | 0.066 | 7.30 | 0.982 | 11.2 | 0.835 | | | 3.60 | 0.101 | 5.60 | 0.823 | | | | |
| 3.30 | 0.064 | 7.40 | 0.983 | 11.3 | 0.844 | | | 3.70 | 0.122 | 5.65 | 0.820 | | | | |
| 3.40 | 0.064 | 7.50 | 0.984 | 11.4 | 0.849 | | | 3.80 | 0.144 | 5.70 | 0.818 | | | | |
| 3.50 | 0.064 | 7.60 | 0.986 | 11.5 | 0.855 | | | 3.90 | 0.167 | 5.76 | 0.820 | | | | |
| 3.60 | 0.086 | 7.70 | 0.987 | 11.6 | 0.860 | | | 4.00 | 0.190 | 5.80 | 0.822 | | | | |
| 3.90 | 0.100 | 7.80 | 0.989 | 11.7 | 0.866 | | | 4.02 | 0.195 | 5.85 | 0.824 | | | | |
| 4.00 | 0.116 | 7.90 | 0.990 | 11.8 | 0.871 | | | 4.09 | 0.227 | 5.90 | 0.828 | | | | |
| 4.10 | 0.151 | 8.00 | 0.996 | 11.9 | 0.876 | | | 4.10 | 0.229 | 5.98 | 0.835 | | | | |
| 4.20 | 0.202 | 8.10 | 1.00 | 12.0 | 0.880 | | | 4.18 | 0.278 | 6.00 | 0.837 | | | | |
| 4.30 | 0.272 | 8.20 | 1.00 | 12.1 | 0.885 | | | 4.20 | 0.294 | 6.18 | 0.858 | | | | |
| 4.40 | 0.391 | 8.30 | 1.00 | 12.2 | 0.890 | | | 4.24 | 0.332 | 6.10 | 0.849 | | | | |
| 4.50 | 0.543 | 8.40 | 1.00 | 12.3 | 0.897 | | | 4.30 | 0.363 | 6.20 | 0.860 | | | | |
| 4.60 | 0.715 | 8.50 | 1.00 | 12.4 | 0.905 | | | 4.38 | 0.453 | 6.29 | 0.869 | | | | |
| 4.70 | 0.824 | 8.60 | 1.00 | 12.5 | 0.910 | | | 4.40 | 0.469 | 6.30 | 0.870 | | | | |
| 4.80 | 0.900 | 8.70 | 0.998 | 12.6 | 0.914 | | | 4.46 | 0.534 | 6.38 | 0.876 | | | | |
| 4.90 | 0.944 | 8.80 | 0.993 | 12.7 | 0.916 | | | 4.50 | 0.580 | 6.40 | 0.877 | | | | |
| 5.00 | 0.965 | 8.90 | 0.982 | 12.8 | 0.916 | | | 4.58 | 0.648 | 6.43 | 0.879 | | | | |

TABLE 8-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | | ϵ | | λ | | ϵ | | λ | | ϵ | |
|-----------------|-------|---------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|
| 3.175MM THICK | | 3.175MM THICK | | 3.175MM THICK | | 3.175MM THICK | | 3.175MM THICK | | 3.175MM THICK | |
| T = 473 (CONT.) | | T = 873 | | T = 473 (CONT.) | | T = 873 (CONT.) | | T = 873 (CONT.) | | T = 873 (CONT.) | |
| 6.50 | 0.880 | 1.52 | 0.643 | 4.13 | 0.324 | 6.57 | 0.832 | 6.50 | 0.446 | 6.60 | 0.832 |
| 6.53 | 0.879 | 1.50 | 0.641 | 4.26 | 0.402 | 6.60 | 0.832 | 6.70 | 0.402 | 6.70 | 0.832 |
| 6.60 | 0.874 | 1.70 | 0.637 | 4.20 | 0.434 | 6.80 | 0.833 | 6.80 | 0.565 | 6.90 | 0.833 |
| 6.64 | 0.871 | 1.88 | 0.632 | 4.40 | 0.635 | 7.09 | 0.833 | 7.09 | 0.640 | 7.10 | 0.833 |
| 6.76 | 0.852 | 1.90 | 0.631 | 4.43 | 0.702 | 7.20 | 0.833 | 7.20 | 0.721 | 7.30 | 0.832 |
| 6.80 | 0.845 | 2.00 | 0.630 | 4.50 | 0.783 | 7.40 | 0.831 | 7.40 | 0.807 | 7.50 | 0.830 |
| 6.86 | 0.833 | 2.10 | 0.628 | 4.60 | 0.819 | 7.50 | 0.832 | 7.50 | 0.827 | 7.70 | 0.835 |
| 6.90 | 0.826 | 2.19 | 0.628 | 4.63 | 0.827 | 7.80 | 0.837 | 7.80 | 0.846 | 7.90 | 0.839 |
| 6.97 | 0.818 | 2.20 | 0.628 | 4.70 | 0.860 | 8.00 | 0.842 | 8.00 | 0.860 | | |
| 7.00 | 0.817 | 2.30 | 0.631 | 4.75 | 0.861 | | | | | | |
| 7.09 | 0.818 | 2.34 | 0.632 | 4.80 | 0.869 | | | | | | |
| 7.10 | 0.818 | 2.40 | 0.635 | 4.82 | 0.870 | | | | | | |
| 7.18 | 0.820 | 2.50 | 0.640 | 4.90 | 0.876 | | | | | | |
| 7.20 | 0.822 | 2.59 | 0.645 | 4.91 | 0.878 | | | | | | |
| 7.30 | 0.828 | 2.60 | 0.646 | 4.99 | 0.878 | | | | | | |
| 7.40 | 0.834 | 2.70 | 0.651 | 5.09 | 0.878 | | | | | | |
| 7.42 | 0.835 | 2.76 | 0.653 | 5.09 | 0.878 | | | | | | |
| 7.50 | 0.837 | 2.80 | 0.656 | 5.10 | 0.878 | | | | | | |
| 7.59 | 0.835 | 2.90 | 0.666 | 5.20 | 0.878 | | | | | | |
| 7.60 | 0.835 | 2.99 | 0.673 | 5.30 | 0.878 | | | | | | |
| 7.68 | 0.831 | 3.00 | 0.674 | 5.36 | 0.878 | | | | | | |
| 7.70 | 0.830 | 3.10 | 0.682 | 5.40 | 0.878 | | | | | | |
| 7.80 | 0.826 | 3.20 | 0.690 | 5.50 | 0.880 | | | | | | |
| 7.84 | 0.822 | 3.26 | 0.696 | 5.55 | 0.878 | | | | | | |
| 7.90 | 0.819 | 3.30 | 0.699 | 5.60 | 0.878 | | | | | | |
| 8.00 | 0.811 | 3.40 | 0.711 | 5.67 | 0.875 | | | | | | |
| | | 3.44 | 0.716 | 5.70 | 0.873 | | | | | | |
| | | 3.50 | 0.724 | 5.80 | 0.866 | | | | | | |
| | | 3.56 | 0.733 | 5.90 | 0.860 | | | | | | |
| | | 3.60 | 0.740 | 5.99 | 0.858 | | | | | | |
| | | 3.69 | 0.759 | 6.00 | 0.854 | | | | | | |
| | | 3.70 | 0.763 | 6.10 | 0.847 | | | | | | |
| | | 3.80 | 0.796 | 6.12 | 0.846 | | | | | | |
| | | 3.82 | 0.804 | 6.20 | 0.842 | | | | | | |
| | | 3.90 | 0.832 | 6.30 | 0.839 | | | | | | |
| | | 3.99 | 0.867 | 6.32 | 0.838 | | | | | | |
| | | 4.00 | 0.873 | 6.40 | 0.836 | | | | | | |
| | | 4.08 | 0.837 | 6.50 | 0.834 | | | | | | |

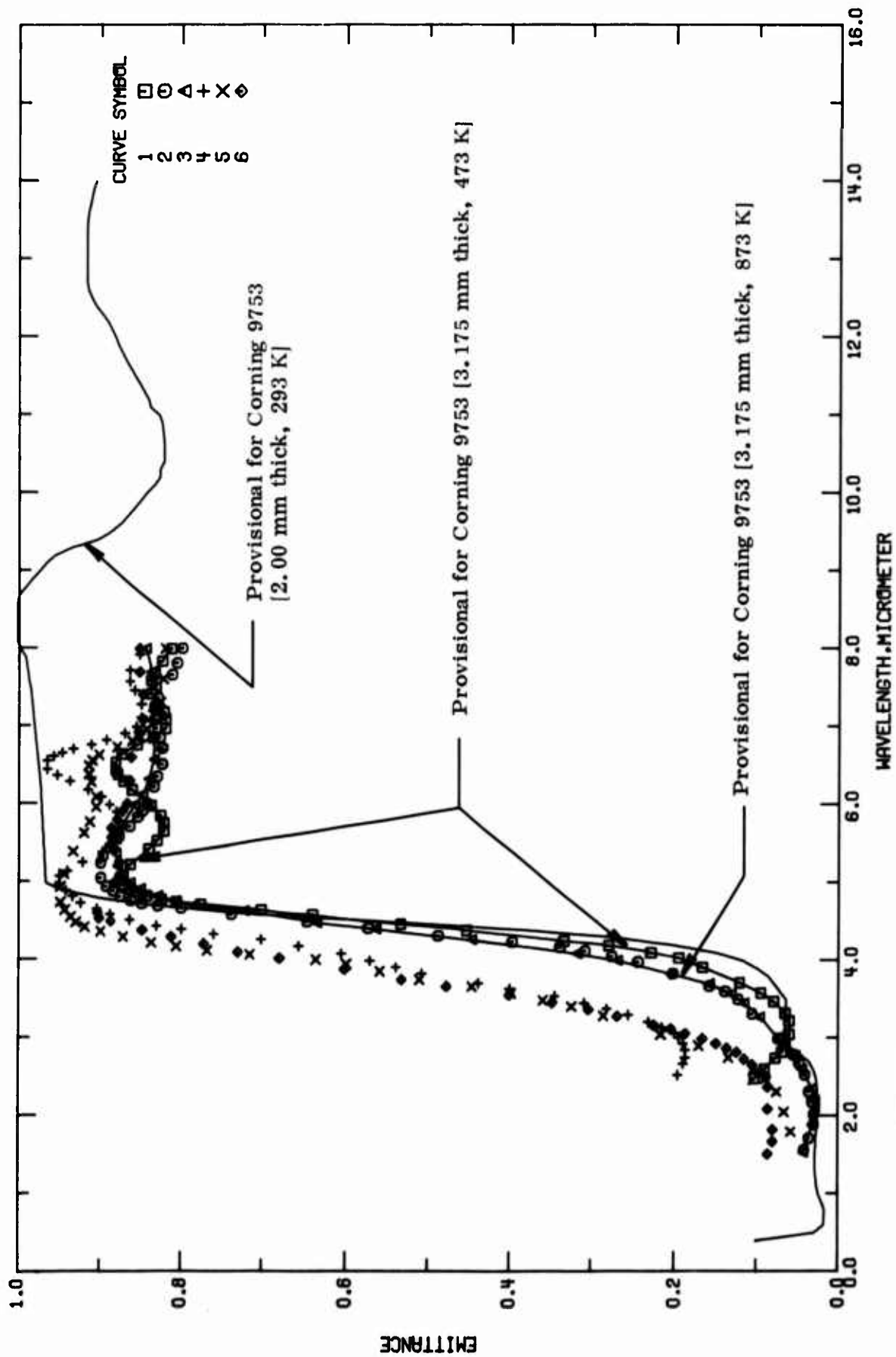


FIGURE 8-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

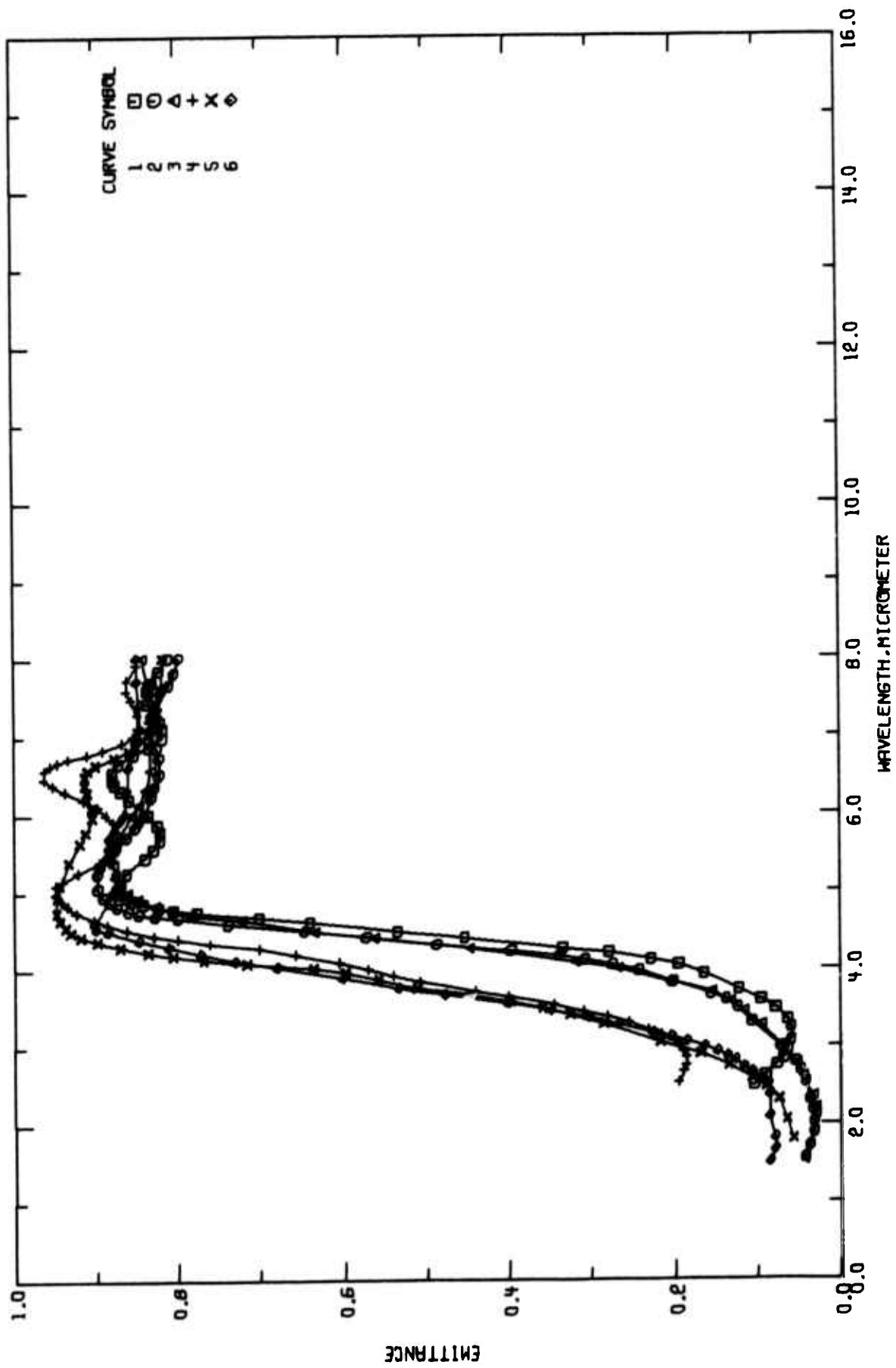


FIGURE 8-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

TABLE 8-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 A00009 | Kandrach, G.S. | 1975 | 2.5-8.0 | 473 | Corning 9753 | Specimen 0.3175 cm (1/8 in.) thick; spectral emittance; smooth values from figure. |
| 2 A00009 | Kandrach, G.S. | 1975 | 1.6-8.0 | 673 | Corning 9753 | Similar to the above specimen. |
| 3 A00009 | Kandrach, G.S. | 1975 | 1.5-8.0 | 873 | Corning 9753 | Similar to the above specimen. |
| 4 A00009 | Kandrach, G.S. | 1975 | 2.5-7.9 | 473 | Corning 9753 | Specimen 1.27 cm (1/2 in.) thick; spectral emittance; smooth values from figure. |
| 5 A00009 | Kandrach, G.S. | 1975 | 1.8-8.0 | 673 | Corning 9753 | Similar to the above specimen. |
| 6 A00009 | Kandrach, G.S. | 1975 | 1.5-8.0 | 873 | Corning 9753 | Similar to the above specimen. |

TABLE 8-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ |
|-----------------|------------|-----------------|------------|
| CURVE 5 (CONT.) | | CURVE 6 (CONT.) | |
| 4.48 | 0.929 | 2.92 | 0.151 |
| 4.55 | 0.935 | 2.98 | 0.167 |
| 4.64 | 0.942 | 3.05 | 0.187 |
| 4.74 | 0.947 | 3.11 | 0.204 |
| 4.94 | 0.947 | 3.16 | 0.224 |
| 5.10 | 0.943 | 3.27 | 0.267 |
| 5.39 | 0.932 | 3.36 | 0.303 |
| 5.63 | 0.919 | 3.45 | 0.346 |
| 5.77 | 0.912 | 3.55 | 0.400 |
| 5.96 | 0.904 | 3.66 | 0.478 |
| 6.09 | 0.904 | 3.75 | 0.533 |
| 6.28 | 0.910 | 3.88 | 0.601 |
| 6.38 | 0.913 | 4.02 | 0.679 |
| 6.49 | 0.913 | 4.10 | 0.729 |
| 6.56 | 0.909 | 4.20 | 0.771 |
| 6.63 | 0.900 | 4.29 | 0.811 |
| 6.73 | 0.877 | 4.38 | 0.845 |
| 6.81 | 0.859 | 4.49 | 0.885 |
| 6.88 | 0.850 | 4.53 | 0.900 |
| 6.96 | 0.841 | 4.60 | 0.902 |
| 7.03 | 0.834 | 4.98 | 0.861 |
| 7.17 | 0.829 | 5.08 | 0.874 |
| 7.31 | 0.824 | 5.25 | 0.874 |
| 7.61 | 0.821 | 5.42 | 0.880 |
| 8.00 | 0.818 | 5.50 | 0.882 |
| | | 5.57 | 0.884 |
| | | 5.69 | 0.884 |
| | | 5.80 | 0.877 |
| | | 5.91 | 0.870 |
| | | 6.00 | 0.864 |
| | | 6.30 | 0.861 |
| | | 6.60 | 0.859 |
| | | 6.91 | 0.849 |
| | | 7.03 | 0.845 |
| | | 7.41 | 0.845 |
| | | 7.70 | 0.849 |
| | | 8.00 | 0.845 |
| | | | |
| CURVE 6 | | | |
| T = 873. | | | |
| 1.50 | 0.086 | | |
| 1.65 | 0.080 | | |
| 1.81 | 0.080 | | |
| 2.08 | 0.095 | | |
| 2.36 | 0.085 | | |
| 2.49 | 0.083 | | |
| 2.56 | 0.095 | | |
| 2.65 | 0.106 | | |
| 2.72 | 0.116 | | |
| 2.81 | 0.126 | | |
| 2.86 | 0.138 | | |

b. Normal Spectral Emittance (Temperature Dependence)

No original experimental data were located for the temperature dependence of the normal spectral emittance of Corning 9753. However, using the interpolated values of curves 1, 2, and 3 of Figure 8-1 and Table 8-3, provisional values for a specimen thickness of 3.175 mm have been derived for 2.8, 3.8, and 5.0 μm . These provisional values are listed in Table 8-4 and shown in Figure 8-3. The uncertainty of the provisional values is within 30%. It is noted these values only go to 873 K and there are no values for higher temperatures for the thickness of 3.175 mm.

It is observed that the value of normal spectral emittance of Corning 9753 over the temperature range of 473 to 873 K is a constant, to a first approximation. Assuming that this constancy extends to the melting range of 1723 to 1773 K, it would be concluded that, in that temperature range, the numerical value of the normal spectral emittance of Corning 9753 would be 0.06 at 2.8 μm , 0.2 at 3.8 μm , and 0.9 at 5.0 μm .

TABLE 6-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ |
|-----------------|------------|-----------------|------------|-----------------|------------|
| 3.175MM THICK | | 3.175MM THICK | | 3.175MM THICK | |
| $\lambda = 2.8$ | | | | | |
| 473. | 0.068 | $\lambda = 3.6$ | | $\lambda = 5.0$ | |
| 673. | 0.057 | 473. | 0.144 | 473. | 0.869 |
| 873. | 0.057 | 673. | 0.198 | 673. | 0.895 |
| | | 873. | 0.199 | 873. | 0.861 |

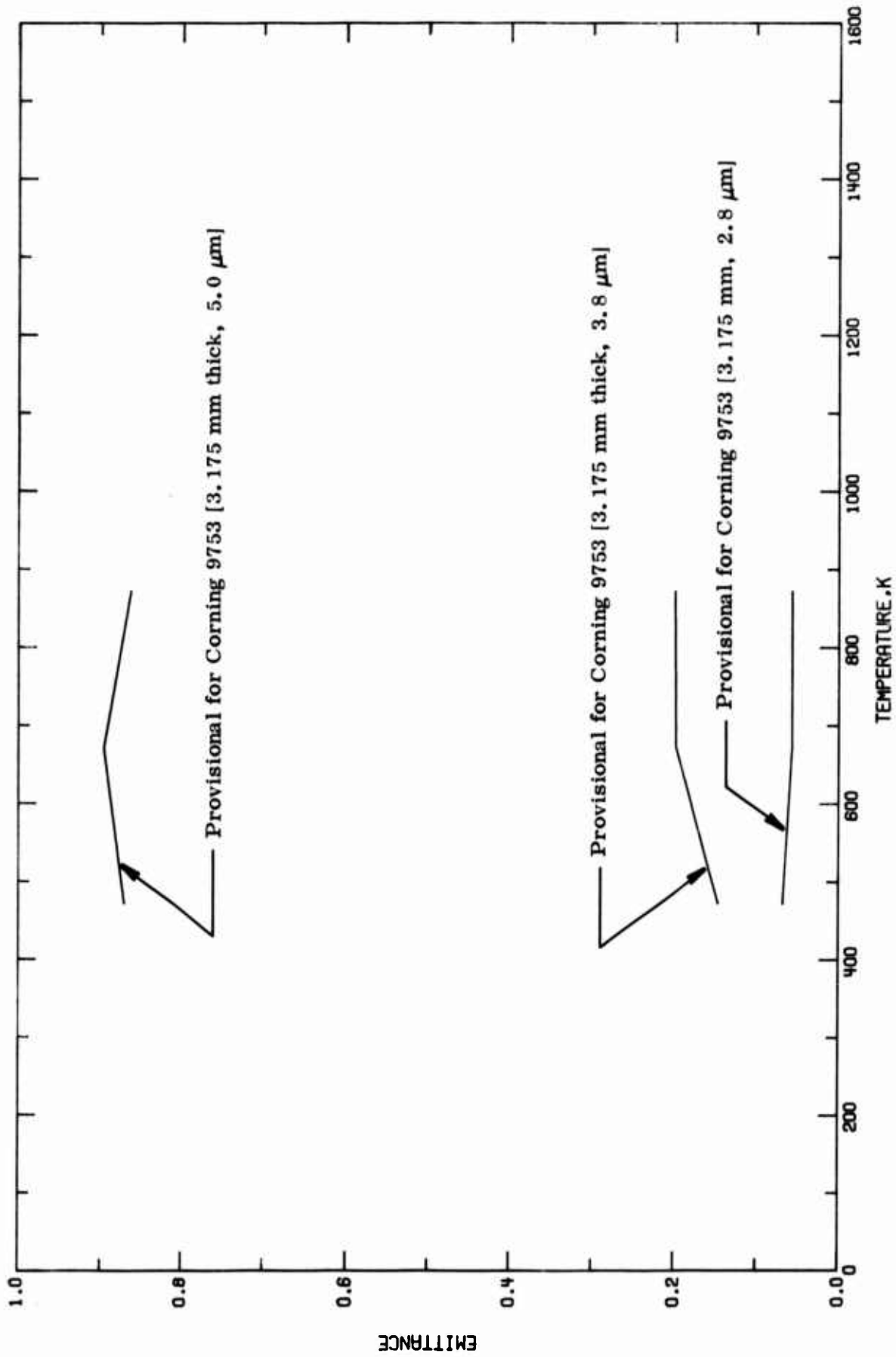


FIGURE 8-3. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

Only one data set was found for the wavelength dependence of the normal spectral reflectance. This is curve number 5 ($T = 293$ K, specimen thickness 1.99 mm) with the data listed in Table 8-7 and shown in Figures 8-4 and 8-5. Specimen characterization and measurement information for the data set are given in Table 8-6.

Values for other conditions have been generated for the normal spectral reflectance. Values for curve number 1 in Tables 8-6 and 8-7 were calculated using equation (2.6-15) which holds for a polished, uncoated, plane-parallel plate, taking into account multiple internal reflectance, and assuming zero absorption. The refractive index data was taken from curve number 1 in Table 8-9 and shown in Figure 8-6. Specimen characterization and measurement information for the refractive index data are given in Table 8-8.

Values of reflectance for a specimen thickness of 3.175 mm at 473, 673, and 873 K were calculated from normal transmittance and normal emittance data with details of the calculation mentioned in Table 8-6 for curves 2, 3, and 4.

Two provisional curves are given with one applicable to $T = 293$ K and a specimen thickness of 1.99 mm and the other for $T = 873$ K and a specimen thickness of 3.175 mm. The latter is shown to give an indication of the effect of temperature and thickness change. The uncertainty of these values can be large because of the small values of reflectance involved. However, over most of the wavelength region, the uncertainty should not exceed 30%. The provisional values are listed in Table 8-5 and shown in Figure 8-4.

It is noted that no reflectance data are available above 873 K and even the values for 473, 673, and 873 K do not go beyond $8 \mu\text{m}$.

TABLE 8-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE CORNING 9753 (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| 1.99MM THICK | | | 1.99MM THICK | | | 1.99MM THICK | | | 3.175MM THICK | | | 3.175MM THICK | | |
|--------------|--------|-----------|-----------------|-----------|--------|-----------------|--------|-----------|---------------|-----------|--------|-----------------|--------|--|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
| T = 293 | | | T = 293 (CONT.) | | | T = 293 (CONT.) | | | T = 873 | | | T = 873 (CONT.) | | |
| 0.40 | 0.104 | 4.30 | 0.075 | 9.20 | 0.000 | 12.1 | 0.115 | 2.00 | 0.125 | 6.00 | 0.146 | | | |
| 0.50 | 0.103 | 4.40 | 0.065 | 9.30 | 0.000 | 12.2 | 0.110 | 2.10 | 0.120 | 6.10 | 0.153 | | | |
| 0.60 | 0.102 | 4.50 | 0.047 | 9.40 | 0.000 | 12.3 | 0.103 | 2.20 | 0.115 | 6.20 | 0.158 | | | |
| 0.70 | 0.101 | 4.60 | 0.040 | 9.50 | 0.000 | 12.4 | 0.095 | 2.30 | 0.107 | 6.30 | 0.161 | | | |
| 0.80 | 0.100 | 4.70 | 0.038 | 9.60 | 0.000 | 12.5 | 0.090 | 2.40 | 0.099 | 6.40 | 0.164 | | | |
| 0.90 | 0.099 | 4.80 | 0.037 | 9.70 | 0.002 | 12.6 | 0.086 | 2.50 | 0.083 | 6.50 | 0.166 | | | |
| 1.00 | 0.099 | 4.90 | 0.036 | 9.80 | 0.010 | 12.7 | 0.084 | 2.60 | 0.077 | 6.60 | 0.168 | | | |
| 1.10 | 0.099 | 5.00 | 0.035 | 9.90 | 0.018 | 12.8 | 0.084 | 2.80 | 0.102 | 6.70 | 0.168 | | | |
| 1.20 | 0.099 | 5.10 | 0.034 | 9.99 | 0.027 | 12.9 | 0.084 | 2.90 | 0.105 | 6.80 | 0.168 | | | |
| 1.30 | 0.098 | 5.20 | 0.034 | 9.10 | 0.035 | 13.0 | 0.084 | 3.00 | 0.092 | 6.90 | 0.167 | | | |
| 1.40 | 0.098 | 5.30 | 0.033 | 9.20 | 0.045 | 13.1 | 0.084 | 3.10 | 0.082 | 7.00 | 0.167 | | | |
| 1.50 | 0.098 | 5.40 | 0.033 | 9.30 | 0.066 | 13.2 | 0.084 | 3.20 | 0.076 | 7.10 | 0.167 | | | |
| 1.60 | 0.098 | 5.50 | 0.032 | 9.40 | 0.098 | 13.3 | 0.084 | 3.30 | 0.071 | 7.20 | 0.167 | | | |
| 1.70 | 0.097 | 5.60 | 0.032 | 9.50 | 0.114 | 13.4 | 0.084 | 3.40 | 0.068 | 7.30 | 0.168 | | | |
| 1.80 | 0.097 | 5.70 | 0.031 | 9.60 | 0.127 | 13.5 | 0.085 | 3.50 | 0.078 | 7.40 | 0.169 | | | |
| 1.90 | 0.096 | 5.80 | 0.031 | 9.70 | 0.135 | 13.6 | 0.086 | 3.60 | 0.102 | 7.50 | 0.170 | | | |
| 2.00 | 0.096 | 5.90 | 0.030 | 9.80 | 0.144 | 13.7 | 0.088 | 3.70 | 0.092 | 7.60 | 0.168 | | | |
| 2.10 | 0.096 | 6.00 | 0.030 | 9.90 | 0.152 | 13.8 | 0.090 | 3.80 | 0.073 | 7.70 | 0.165 | | | |
| 2.20 | 0.095 | 6.10 | 0.029 | 10.0 | 0.159 | 13.9 | 0.092 | 3.90 | 0.058 | 7.80 | 0.163 | | | |
| 2.30 | 0.095 | 6.20 | 0.029 | 10.1 | 0.168 | 14.0 | 0.095 | 4.00 | 0.049 | 7.90 | 0.161 | | | |
| 2.40 | 0.094 | 6.30 | 0.028 | 10.2 | 0.175 | 14.1 | 0.099 | 4.10 | 0.040 | 8.00 | 0.158 | | | |
| 2.50 | 0.094 | 6.40 | 0.027 | 10.3 | 0.175 | 14.2 | 0.104 | 4.20 | 0.016 | | | | | |
| 2.60 | 0.093 | 6.50 | 0.026 | 10.4 | 0.180 | 14.3 | 0.110 | 4.30 | 0.022 | | | | | |
| 2.70 | 0.093 | 6.60 | 0.025 | 10.5 | 0.180 | 14.4 | 0.115 | 4.40 | 0.040 | | | | | |
| 2.80 | 0.092 | 6.70 | 0.024 | 10.6 | 0.180 | 14.5 | 0.118 | 4.50 | 0.064 | | | | | |
| 2.90 | 0.091 | 6.80 | 0.023 | 10.7 | 0.179 | 14.6 | 0.121 | 4.60 | 0.102 | | | | | |
| 3.00 | 0.091 | 6.90 | 0.022 | 10.8 | 0.178 | 14.7 | 0.123 | 4.70 | 0.105 | | | | | |
| 3.10 | 0.090 | 7.00 | 0.021 | 10.9 | 0.177 | 14.8 | 0.127 | 4.80 | 0.123 | | | | | |
| 3.20 | 0.090 | 7.10 | 0.020 | 11.0 | 0.174 | 14.9 | 0.134 | 4.90 | 0.139 | | | | | |
| 3.30 | 0.089 | 7.20 | 0.019 | 11.1 | 0.163 | | | 5.00 | 0.139 | | | | | |
| 3.40 | 0.088 | 7.30 | 0.018 | 11.2 | 0.161 | | | 5.10 | 0.130 | | | | | |
| 3.50 | 0.088 | 7.40 | 0.017 | 11.3 | 0.156 | | | 5.20 | 0.124 | | | | | |
| 3.60 | 0.086 | 7.50 | 0.016 | 11.4 | 0.151 | | | 5.30 | 0.122 | | | | | |
| 3.70 | 0.085 | 7.60 | 0.014 | 11.5 | 0.145 | | | 5.40 | 0.121 | | | | | |
| 3.80 | 0.084 | 7.70 | 0.013 | 11.6 | 0.140 | | | 5.50 | 0.120 | | | | | |
| 3.90 | 0.084 | 7.80 | 0.011 | 11.7 | 0.134 | | | 5.60 | 0.122 | | | | | |
| 4.00 | 0.084 | 7.90 | 0.010 | 11.8 | 0.129 | | | 5.70 | 0.127 | | | | | |
| 4.10 | 0.079 | 8.00 | 0.004 | 11.9 | 0.124 | | | 5.80 | 0.134 | | | | | |
| 4.20 | 0.075 | 8.10 | 0.000 | 12.0 | 0.120 | | | 5.90 | 0.140 | | | | | |

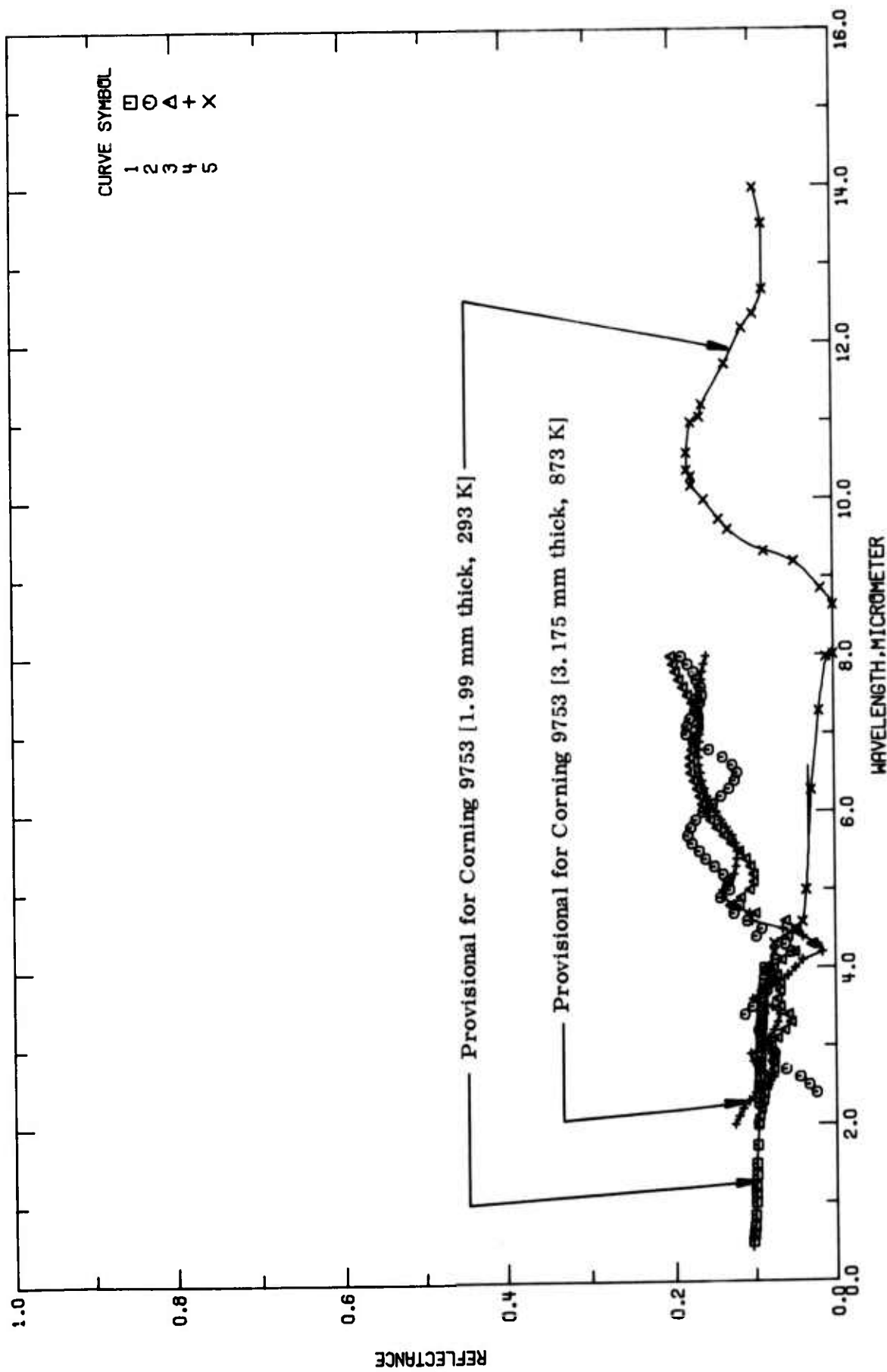


FIGURE 8-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

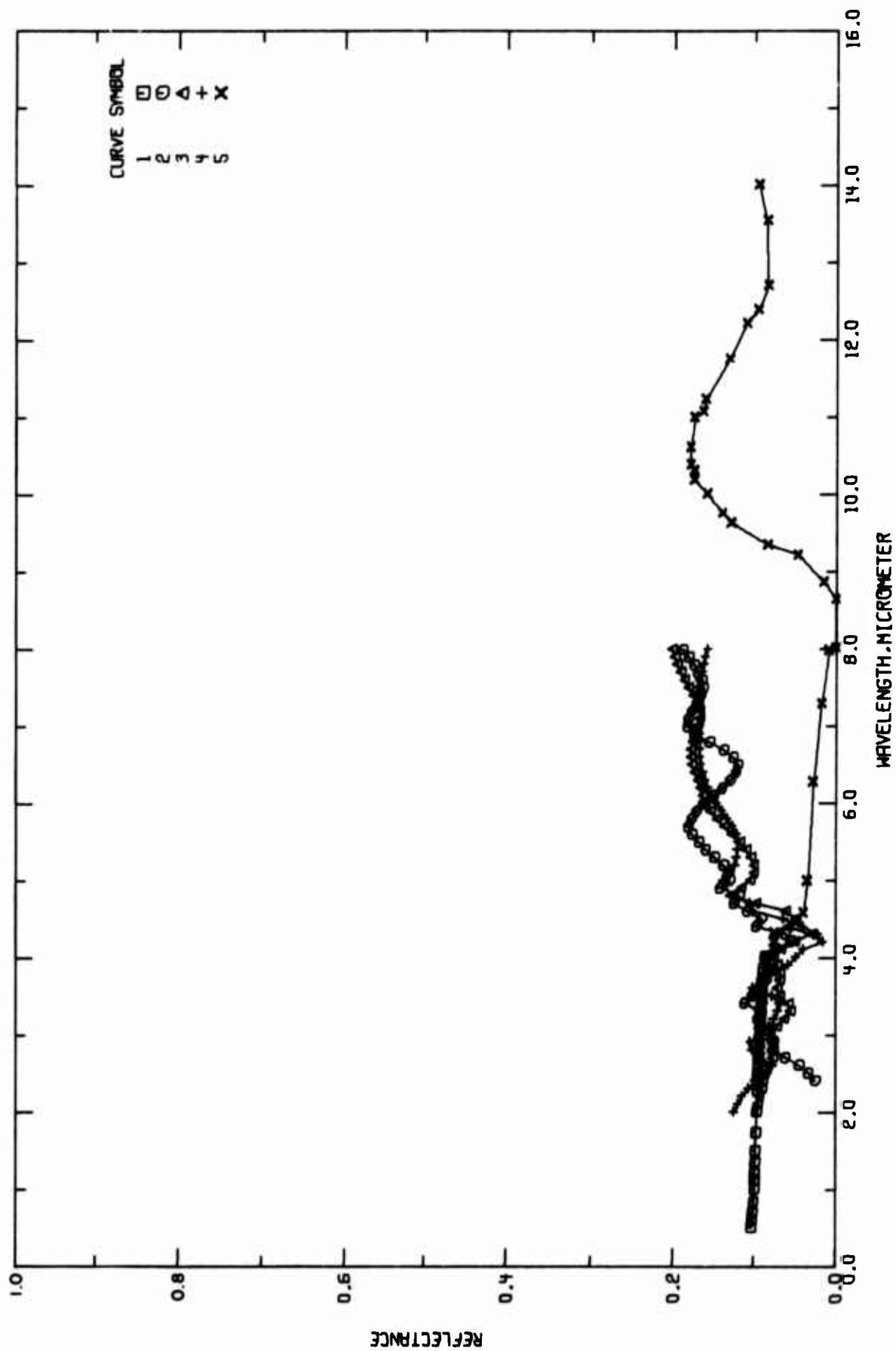


FIGURE 8-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

TABLE 5-6. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|------------------|---------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 E22600, A00009 | | | 0.50-4.0 | 293 | Glass 9753 | Calculated from refractive index data [see Ref. A00009] and using $(n-1)^2/(n^2+1)$ which applies to a polished, uncoated, plane-parallel plate, takes into account multiple internal reflections, and assumes zero absorption; measurement temperature for refractive index data not given explicitly, assumed to be 293 K. |
| 2 A00009 | | | 2.4-8.0 | 473 | Corning 9753 | Specimen thickness 0.3175 cm (1/8 in.); calculated using $\rho = 1.0 - \alpha - \tau$, and $\alpha = \epsilon$, where data for ϵ from curve no. 1 of Tables 8-2 and 8-3, data for τ from curve no. 7 of Tables 8-13 and 8-14, from 4.9 to 8.0 μm , τ taken to be 0.000. |
| 3 A00009 | | | 2.0-8.0 | 673 | Corning 9753 | Specimen thickness 0.3175 cm (1/8 in.); calculated using $\rho = 1.0 - \alpha - \tau$ and $\alpha = \epsilon$ where data for ϵ from curve no. 2 of Tables 8-2 and 8-3, data for τ from curve no. 8 of Tables 8-13 and 8-14, from 4.80 to 8.0 μm , τ taken to be 0.000. |
| 4 A00009 | | | 2.0-8.0 | 873 | Corning 9753 | Specimen thickness 0.3175 cm (1/8 in.); calculated using $\rho = 1.0 - \alpha - \tau$ and $\alpha = \epsilon$ where data for ϵ from curve no. 3 of Tables 8-2 and 8-3, data for τ from curve no. 9 of Tables 8-13 and 8-14, from 4.94 to 8.0 μm , τ taken to be 0.000. |
| 5 A00013 | Plummer, W.A. | | 2.5-15 | 293 | Code 9753 | Specimen 1.99 mm thick; reflectance vs. aluminum reported; Perkin-Elmer Model 221 infrared spectrophotometer used; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |

TABLE 3-7. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| CURVE 1 T = 293. | | CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 (CONT.) | | CURVE 4 (CONT.) | | |
|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|----------|-----------------|--------|-----------------|--------|-------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
| 2.500 | 0.103 | 3.40 | 0.112 | 7.40 | 0.166 | 4.90 | 0.116 | 2.40 | 0.099 | 6.50 | 0.166 | |
| 0.594 | 0.102 | 3.50 | 0.102 | 7.50 | 0.163 | 5.00 | 0.105 | 2.50 | 0.083 | 6.60 | 0.168 | |
| 0.694 | 0.101 | 3.60 | 0.092 | 7.60 | 0.165 | 5.10 | 0.100 | 2.60 | 0.077 | 6.70 | 0.168 | |
| 0.834 | 0.100 | 3.70 | 0.085 | 7.70 | 0.170 | 5.20 | 0.100 | 2.80 | 0.102 | 6.80 | 0.168 | |
| 1.001 | 0.099 | 3.80 | 0.081 | 7.80 | 0.174 | 5.30 | 0.104 | 2.90 | 0.105 | 6.90 | 0.167 | |
| 1.112 | 0.099 | 3.90 | 0.078 | 7.90 | 0.181 | 5.40 | 0.110 | 3.00 | 0.092 | 7.00 | 0.167 | |
| 1.202 | 0.099 | 4.00 | 0.081 | 8.00 | 0.189 | 5.50 | 0.118 | 3.10 | 0.082 | 7.10 | 0.167 | |
| 1.346 | 0.098 | 4.10 | 0.073 | CURVE 3 | | | 5.60 | 0.128 | 3.20 | 0.076 | 7.20 | 0.167 |
| 1.495 | 0.098 | 4.20 | 0.064 | T = 673. | | | 5.70 | 0.137 | 3.30 | 0.071 | 7.30 | 0.168 |
| 1.730 | 0.097 | 4.30 | 0.061 | | | | 5.80 | 0.146 | 3.40 | 0.068 | 7.40 | 0.169 |
| 2.000 | 0.096 | 4.40 | 0.057 | | | | 5.90 | 0.154 | 3.50 | 0.078 | 7.50 | 0.170 |
| 2.274 | 0.095 | 4.50 | 0.050 | | | | 6.00 | 0.160 | 3.60 | 0.102 | 7.60 | 0.165 |
| 2.489 | 0.095 | 4.60 | 0.125 | | | | 6.10 | 0.164 | 3.70 | 0.092 | 7.70 | 0.165 |
| 2.613 | 0.094 | 4.70 | 0.118 | | | | 6.20 | 0.167 | 3.80 | 0.073 | 7.80 | 0.163 |
| 2.767 | 0.094 | 4.80 | 0.142 | | | | 6.30 | 0.170 | 3.90 | 0.056 | 7.90 | 0.161 |
| 2.952 | 0.093 | 4.90 | 0.142 | | | | 6.40 | 0.174 | 4.00 | 0.049 | 8.00 | 0.158 |
| 2.987 | 0.093 | 5.00 | 0.130 | | | | 6.50 | 0.178 | 4.10 | 0.040 | | |
| 3.112 | 0.092 | 5.10 | 0.132 | | | | 6.60 | 0.179 | 4.20 | 0.016 | | |
| 3.260 | 0.091 | 5.20 | 0.130 | | | | 6.70 | 0.179 | 4.30 | 0.022 | | |
| 3.382 | 0.091 | 5.30 | 0.119 | | | | 6.80 | 0.177 | 4.40 | 0.040 | | |
| 3.495 | 0.090 | 5.40 | 0.160 | | | | 6.90 | 0.174 | 4.50 | 0.064 | | |
| 3.610 | 0.090 | 5.50 | 0.177 | | | | 7.00 | 0.171 | 4.60 | 0.102 | | |
| 3.723 | 0.089 | 5.60 | 0.182 | | | | 7.10 | 0.168 | 4.70 | 0.105 | | |
| 3.847 | 0.088 | 5.70 | 0.175 | | | | 7.20 | 0.168 | 4.80 | 0.123 | | |
| 4.000 | 0.087 | 5.80 | 0.172 | | | | 7.30 | 0.170 | 4.90 | 0.139 | | |
| | | 5.90 | 0.163 | | | | 7.40 | 0.176 | 5.00 | 0.130 | | |
| | | 6.00 | 0.151 | | | | 7.50 | 0.182 | 5.10 | 0.124 | | |
| | | 6.10 | 0.140 | | | | 7.60 | 0.187 | 5.20 | 0.122 | | |
| | | 6.20 | 0.130 | | | | 7.70 | 0.192 | 5.30 | 0.121 | | |
| | | 6.30 | 0.123 | | | | 7.80 | 0.196 | 5.40 | 0.120 | | |
| | | 6.40 | 0.120 | | | | 7.90 | 0.195 | 5.50 | 0.122 | | |
| | | 6.50 | 0.120 | | | | 8.00 | 0.202 | 5.60 | 0.127 | | |
| | | 6.60 | 0.138 | | | | CURVE 4 | | 5.70 | 0.134 | | |
| | | 6.70 | 0.155 | | | | T = 873. | | 5.80 | 0.140 | | |
| | | 6.80 | 0.174 | | | | | | 5.90 | 0.146 | | |
| | | 6.90 | 0.183 | | | | | | 6.00 | 0.153 | | |
| | | 7.00 | 0.182 | | | | | | 6.10 | 0.158 | | |
| | | 7.10 | 0.178 | | | | | | 6.20 | 0.161 | | |
| | | 7.20 | 0.172 | | | | | | 6.30 | 0.164 | | |
| | | 7.30 | 0.172 | | | | | | 6.40 | 0.164 | | |
| | | 7.40 | 0.172 | | | | | | 6.50 | 0.164 | | |
| | | 7.50 | 0.172 | | | | | | 6.60 | 0.164 | | |
| | | 7.60 | 0.172 | | | | | | 6.70 | 0.164 | | |
| | | 7.70 | 0.172 | | | | | | 6.80 | 0.164 | | |
| | | 7.80 | 0.172 | | | | | | 6.90 | 0.164 | | |
| | | 7.90 | 0.172 | | | | | | 7.00 | 0.164 | | |
| | | 8.00 | 0.172 | | | | | | 7.10 | 0.164 | | |
| | | 8.10 | 0.172 | | | | | | 7.20 | 0.164 | | |
| | | 8.20 | 0.172 | | | | | | 7.30 | 0.164 | | |
| | | 8.30 | 0.172 | | | | | | 7.40 | 0.164 | | |
| | | 8.40 | 0.172 | | | | | | 7.50 | 0.164 | | |
| | | 8.50 | 0.172 | | | | | | 7.60 | 0.164 | | |
| | | 8.60 | 0.172 | | | | | | 7.70 | 0.164 | | |
| | | 8.70 | 0.172 | | | | | | 7.80 | 0.164 | | |
| | | 8.80 | 0.172 | | | | | | 7.90 | 0.164 | | |
| | | 8.90 | 0.172 | | | | | | 8.00 | 0.164 | | |

TABLE 2-7. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ |
|-----------|-----------|
| CURVE | S (CONT.) |
| 10.00 | 0.159 |
| 10.15 | 0.175 |
| 10.30 | 0.175 |
| 10.38 | 0.180 |
| 10.60 | 0.180 |
| 10.99 | 0.175 |
| 11.06 | 0.164 |
| 11.22 | 0.161 |
| 11.74 | 0.132 |
| 12.20 | 0.110 |
| 12.36 | 0.095 |
| 12.59 | 0.084 |
| 13.53 | 0.065 |
| 13.99 | 0.055 |
| 14.21 | 0.105 |
| 14.49 | 0.118 |
| 14.79 | 0.125 |
| 14.87 | 0.136 |
| 14.92 | 0.133 |

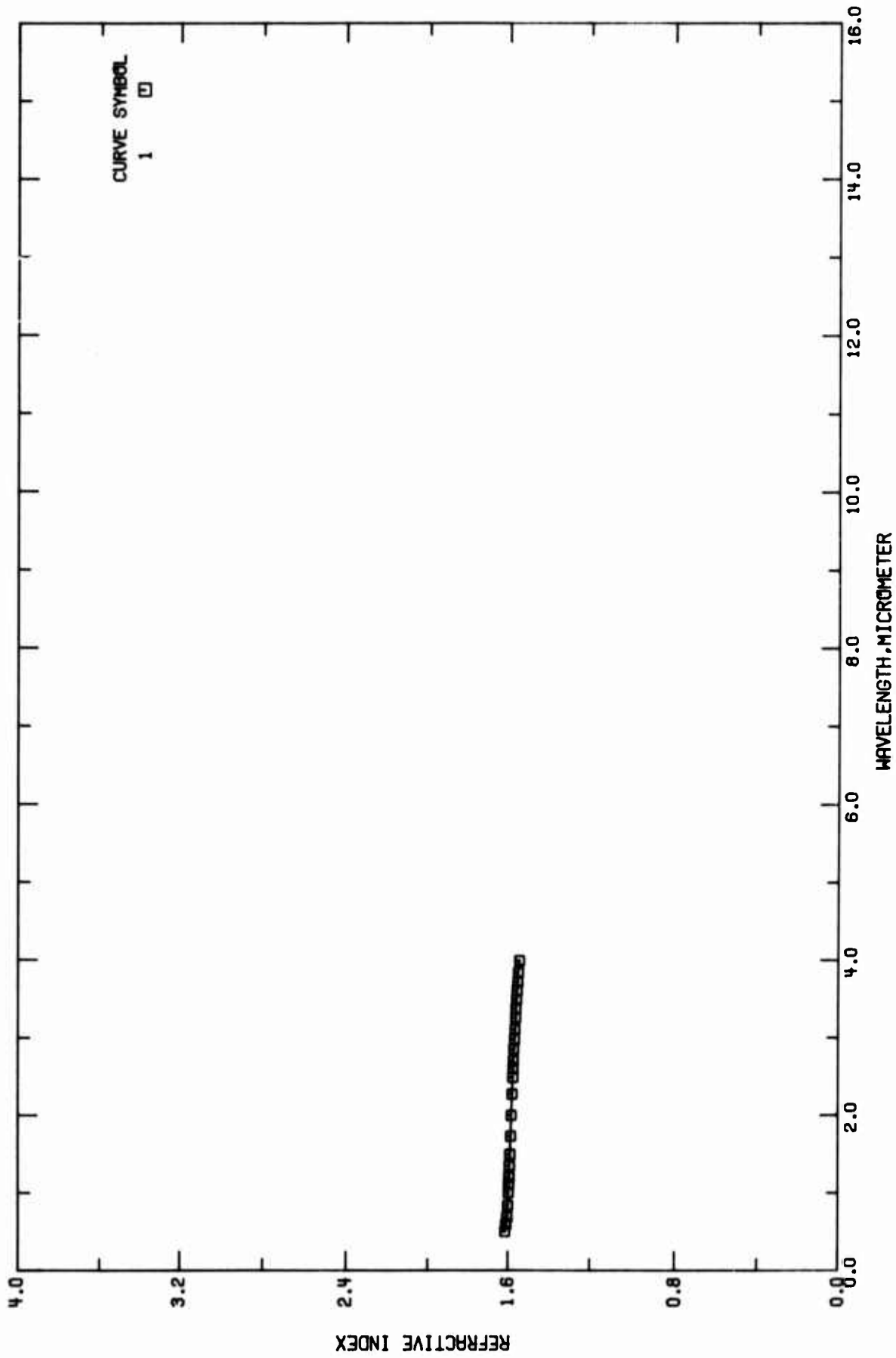


FIGURE 8-6. EXPERIMENTAL REFRACTIVE INDEX OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

TABLE 8-8. MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF CALCIUM ALUMINUM SILICATE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 | A00009 Kandrach, G. S. | 1975 | 0.50-4.0 | 293 | Class 9763 | Smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |

TABLE 8-9. EXPERIMENTAL REFRACTIVE INDEX OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE)
[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFRACTIVE INDEX, n]

| λ | n |
|-----------|--------|
| 0.500 | 1.6096 |
| 0.594 | 1.6140 |
| 0.697 | 1.6182 |
| 0.834 | 1.5965 |
| 1.001 | 1.5931 |
| 1.112 | 1.5914 |
| 1.252 | 1.5932 |
| 1.346 | 1.5883 |
| 1.495 | 1.5865 |
| 1.730 | 1.5837 |
| 2.000 | 1.5803 |
| 2.274 | 1.5767 |
| 2.469 | 1.5736 |
| 2.613 | 1.5717 |
| 2.707 | 1.5702 |
| 2.852 | 1.5679 |
| 2.967 | 1.5654 |
| 3.112 | 1.5630 |
| 3.260 | 1.5600 |
| 3.382 | 1.5576 |
| 3.495 | 1.5551 |
| 3.610 | 1.5525 |
| 3.723 | 1.5499 |
| 3.847 | 1.5467 |
| 4.000 | 1.5422 |

CURVE 1
T = 293.

d. Normal Spectral Reflectance (Temperature Dependence)

Using values from curves 2, 3, and 4 of the previous section, provisional values have been generated for 2.8, 3.8, and 5.0 μm . These values listed in Table 8-10 and shown in Figure 8-7 are valid for a thickness of 3.175 mm. The uncertainty should not exceed 30%. Note that for the three lowest wavelengths, values are not given above 873 K and no values are given for 10.6 μm above room temperature.

TABLE 8-10. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE(CORNING 9753) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ | T | ρ | T | ρ |
|------------------|--------|---------------|--------|---------------|--------|
| 3.175MM THICK | | 3.175MM THICK | | 3.175MM THICK | |
| $\lambda = 2.60$ | | | | | |
| 473. | 0.076 | 473. | 0.081 | 473. | 0.130 |
| 673. | 0.078 | 673. | 0.068 | 673. | 0.105 |
| 873. | 0.102 | 873. | 0.073 | 873. | 0.139 |
| $\lambda = 3.80$ | | | | | |
| $\lambda = 5.0$ | | | | | |

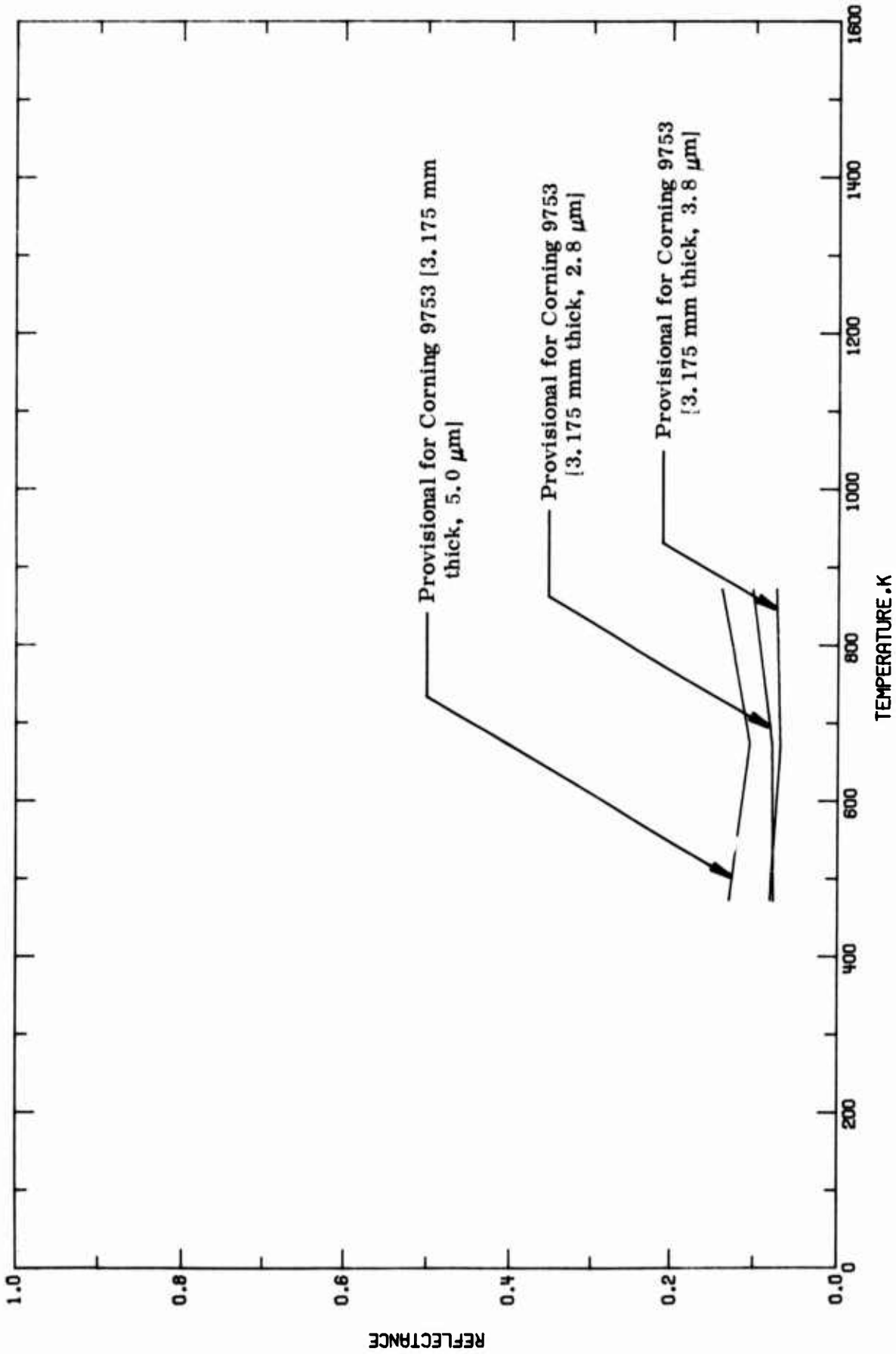


FIGURE 8-7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

No original experimental data were located for the normal spectral absorptance of Corning 9753. However, by applying Kirchhoff's law, the provisional values of the normal spectral absorptance are generated which are equal to the provisional values of the normal spectral emittance. For a discussion of the uncertainties see the section on the normal spectral emittance (wavelength dependence) of calcium aluminum silicate. The provisional values of the normal spectral absorptance are listed in Table 8-11 and shown in Figure 8-8.

For the temperature dependence of the normal spectral absorptance, see the section on the normal spectral emittance (temperature dependence) of calcium aluminum silicate.

TABLE 8-11. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF CALCIUM ALUMINUM SILICATE(CORNING 9/53) (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| 2.00MM THICK | | | 2.00MM THICK | | | 2.00MM THICK | | | 3.175MM THICK | | | 3.175MM THICK | | |
|--------------|----------|---------|--------------|----------|-----------------|--------------|----------|-----------------|---------------|----------|---------|---------------|----------|-----------------|
| λ | α | T = 293 | λ | α | T = 293 (CONT.) | λ | α | T = 293 (CONT.) | λ | α | T = 473 | λ | α | T = 473 (CONT.) |
| 0.40 | 0.101 | 0.966 | 5.10 | 0.973 | 12.9 | 0.916 | 2.40 | 0.110 | 4.60 | 0.675 | | | | |
| 0.50 | 0.029 | 0.956 | 3.10 | 0.965 | 13.0 | 0.916 | 2.47 | 0.103 | 4.64 | 0.700 | | | | |
| 0.60 | 0.017 | 0.967 | 9.20 | 0.954 | 13.1 | 0.916 | 2.50 | 0.099 | 4.70 | 0.750 | | | | |
| 0.80 | 0.016 | 0.967 | 9.30 | 0.934 | 13.2 | 0.916 | 2.59 | 0.090 | 4.71 | 0.775 | | | | |
| 0.90 | 0.023 | 0.968 | 9.40 | 0.902 | 13.3 | 0.916 | 2.60 | 0.089 | 4.74 | 0.805 | | | | |
| 1.00 | 0.024 | 0.968 | 9.50 | 0.886 | 13.4 | 0.916 | 2.70 | 0.080 | 4.77 | 0.823 | | | | |
| 1.10 | 0.026 | 0.969 | 9.60 | 0.873 | 13.5 | 0.915 | 2.73 | 0.077 | 4.80 | 0.832 | | | | |
| 1.20 | 0.027 | 0.969 | 9.70 | 0.864 | 13.6 | 0.914 | 2.80 | 0.070 | 4.82 | 0.841 | | | | |
| 1.30 | 0.028 | 0.970 | 9.80 | 0.856 | 13.7 | 0.912 | 2.81 | 0.069 | 4.87 | 0.854 | | | | |
| 1.40 | 0.029 | 0.970 | 9.90 | 0.848 | 13.8 | 0.910 | 2.90 | 0.065 | 4.90 | 0.858 | | | | |
| 1.50 | 0.028 | 0.971 | 10.0 | 0.841 | 13.9 | 0.908 | 2.91 | 0.065 | 4.91 | 0.860 | | | | |
| 1.60 | 0.027 | 0.971 | 10.1 | 0.832 | 14.0 | 0.905 | 3.00 | 0.061 | 4.96 | 0.869 | | | | |
| 1.70 | 0.027 | 0.972 | 10.2 | 0.825 | 14.1 | 0.901 | 3.04 | 0.060 | 5.00 | 0.870 | | | | |
| 1.80 | 0.026 | 0.973 | 10.3 | 0.820 | 14.2 | 0.896 | 3.10 | 0.059 | 5.08 | 0.869 | | | | |
| 2.00 | 0.026 | 0.974 | 10.4 | 0.820 | 14.3 | 0.890 | 3.20 | 0.060 | 5.10 | 0.868 | | | | |
| 2.30 | 0.025 | 0.975 | 10.5 | 0.820 | 14.4 | 0.885 | 3.21 | 0.060 | 5.20 | 0.862 | | | | |
| 2.40 | 0.026 | 0.976 | 10.6 | 0.820 | 14.5 | 0.882 | 3.30 | 0.064 | 5.22 | 0.860 | | | | |
| 2.50 | 0.027 | 0.977 | 10.7 | 0.821 | 14.6 | 0.879 | 3.31 | 0.065 | 5.30 | 0.851 | | | | |
| 2.60 | 0.031 | 0.978 | 10.8 | 0.822 | 14.7 | 0.877 | 3.40 | 0.073 | 5.40 | 0.840 | | | | |
| 2.70 | 0.036 | 0.979 | 10.9 | 0.823 | 14.8 | 0.873 | 3.46 | 0.079 | 5.42 | 0.838 | | | | |
| 2.80 | 0.048 | 0.980 | 11.0 | 0.826 | 14.9 | 0.866 | 3.50 | 0.084 | 5.50 | 0.832 | | | | |
| 2.90 | 0.062 | 0.981 | 11.1 | 0.837 | | | 3.57 | 0.095 | 5.53 | 0.828 | | | | |
| 3.20 | 0.066 | 0.982 | 11.2 | 0.839 | | | 3.60 | 0.101 | 5.60 | 0.823 | | | | |
| 3.30 | 0.064 | 0.983 | 11.3 | 0.844 | | | 3.70 | 0.122 | 5.65 | 0.820 | | | | |
| 3.40 | 0.064 | 0.984 | 11.4 | 0.849 | | | 3.80 | 0.144 | 5.70 | 0.818 | | | | |
| 3.50 | 0.064 | 0.986 | 11.5 | 0.855 | | | 3.90 | 0.167 | 5.76 | 0.820 | | | | |
| 3.80 | 0.086 | 0.987 | 11.6 | 0.860 | | | 4.00 | 0.190 | 5.80 | 0.822 | | | | |
| 3.90 | 0.100 | 0.989 | 11.7 | 0.866 | | | 4.02 | 0.195 | 5.85 | 0.824 | | | | |
| 4.00 | 0.118 | 0.990 | 11.8 | 0.871 | | | 4.09 | 0.227 | 5.90 | 0.828 | | | | |
| 4.10 | 0.151 | 0.996 | 11.9 | 0.876 | | | 4.10 | 0.229 | 5.98 | 0.835 | | | | |
| 4.20 | 0.202 | 1.000 | 12.0 | 0.880 | | | 4.18 | 0.270 | 6.00 | 0.837 | | | | |
| 4.30 | 0.272 | 1.000 | 12.1 | 0.885 | | | 4.20 | 0.294 | 6.10 | 0.849 | | | | |
| 4.40 | 0.391 | 1.000 | 12.2 | 0.890 | | | 4.24 | 0.332 | 6.18 | 0.858 | | | | |
| 4.50 | 0.543 | 1.000 | 12.3 | 0.897 | | | 4.30 | 0.383 | 6.20 | 0.860 | | | | |
| 4.60 | 0.715 | 1.000 | 12.4 | 0.905 | | | 4.38 | 0.453 | 6.29 | 0.869 | | | | |
| 4.70 | 0.824 | 1.000 | 12.5 | 0.910 | | | 4.40 | 0.469 | 6.30 | 0.870 | | | | |
| 4.80 | 0.900 | 0.998 | 12.6 | 0.914 | | | 4.46 | 0.534 | 6.38 | 0.876 | | | | |
| 4.90 | 0.944 | 0.996 | 12.7 | 0.916 | | | 4.50 | 0.580 | 6.40 | 0.877 | | | | |
| 5.00 | 0.965 | 0.982 | 12.8 | 0.916 | | | 4.58 | 0.640 | 6.43 | 0.879 | | | | |

E 8-11. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9733) (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α | λ | α |
|-----------------|----------|-----------|----------|-----------------|----------|-----------|----------|
| 3.175MM THICK | | | | 3.175MM THICK | | | |
| T = 473 (CONT.) | | | | T = 873 (CONT.) | | | |
| 6.50 | 0.890 | 1.52 | 0.043 | 4.10 | 0.328 | 6.57 | 0.832 |
| 6.53 | 0.973 | 1.60 | 0.041 | 4.20 | 0.402 | 6.60 | 0.832 |
| 6.60 | 0.874 | 1.70 | 0.037 | 4.26 | 0.446 | 6.70 | 0.832 |
| 6.64 | 0.871 | 1.80 | 0.034 | 4.30 | 0.560 | 6.80 | 0.832 |
| 6.70 | 0.862 | 1.98 | 0.032 | 4.40 | 0.565 | 6.90 | 0.833 |
| 6.76 | 0.852 | 1.90 | 0.031 | 4.48 | 0.635 | 7.00 | 0.833 |
| 6.80 | 0.845 | 2.00 | 0.030 | 4.50 | 0.640 | 7.10 | 0.833 |
| 6.86 | 0.833 | 2.10 | 0.028 | 4.60 | 0.702 | 7.20 | 0.833 |
| 6.90 | 0.826 | 2.19 | 0.028 | 4.63 | 0.721 | 7.30 | 0.832 |
| 6.97 | 0.818 | 2.20 | 0.028 | 4.70 | 0.783 | 7.40 | 0.831 |
| 7.00 | 0.817 | 2.30 | 0.031 | 4.75 | 0.807 | 7.50 | 0.830 |
| 7.09 | 0.818 | 2.34 | 0.032 | 4.80 | 0.819 | 7.60 | 0.832 |
| 7.10 | 0.818 | 2.40 | 0.035 | 4.82 | 0.827 | 7.70 | 0.835 |
| 7.18 | 0.820 | 2.50 | 0.040 | 4.90 | 0.846 | 7.80 | 0.837 |
| 7.20 | 0.822 | 2.59 | 0.045 | 4.91 | 0.848 | 7.90 | 0.839 |
| 7.30 | 0.828 | 2.60 | 0.046 | 4.99 | 0.860 | 8.00 | 0.842 |
| 7.40 | 0.834 | 2.70 | 0.051 | 5.00 | 0.861 | | |
| 7.42 | 0.835 | 2.76 | 0.053 | 5.09 | 0.869 | | |
| 7.50 | 0.837 | 2.80 | 0.056 | 5.10 | 0.870 | | |
| 7.59 | 0.835 | 2.90 | 0.066 | 5.20 | 0.876 | | |
| 7.60 | 0.835 | 2.99 | 0.073 | 5.33 | 0.878 | | |
| 7.68 | 0.831 | 3.00 | 0.074 | 5.36 | 0.878 | | |
| 7.70 | 0.830 | 3.10 | 0.082 | 5.40 | 0.879 | | |
| 7.80 | 0.825 | 3.20 | 0.090 | 5.50 | 0.880 | | |
| 7.84 | 0.822 | 3.26 | 0.096 | 5.55 | 0.878 | | |
| 7.90 | 0.819 | 3.30 | 0.099 | 5.60 | 0.878 | | |
| 8.00 | 0.811 | 3.40 | 0.111 | 5.67 | 0.875 | | |
| | | 3.44 | 0.116 | 5.70 | 0.873 | | |
| | | 3.50 | 0.124 | 5.80 | 0.866 | | |
| | | 3.56 | 0.133 | 5.90 | 0.860 | | |
| | | 3.60 | 0.140 | 5.99 | 0.855 | | |
| | | 3.69 | 0.159 | 6.00 | 0.854 | | |
| | | 3.70 | 0.163 | 6.10 | 0.847 | | |
| | | 3.80 | 0.196 | 6.12 | 0.846 | | |
| | | 3.82 | 0.204 | 6.20 | 0.842 | | |
| | | 3.90 | 0.232 | 6.30 | 0.839 | | |
| | | 3.99 | 0.267 | 6.32 | 0.838 | | |
| | | 4.00 | 0.273 | 6.40 | 0.836 | | |
| | | 4.08 | 0.317 | 6.50 | 0.834 | | |

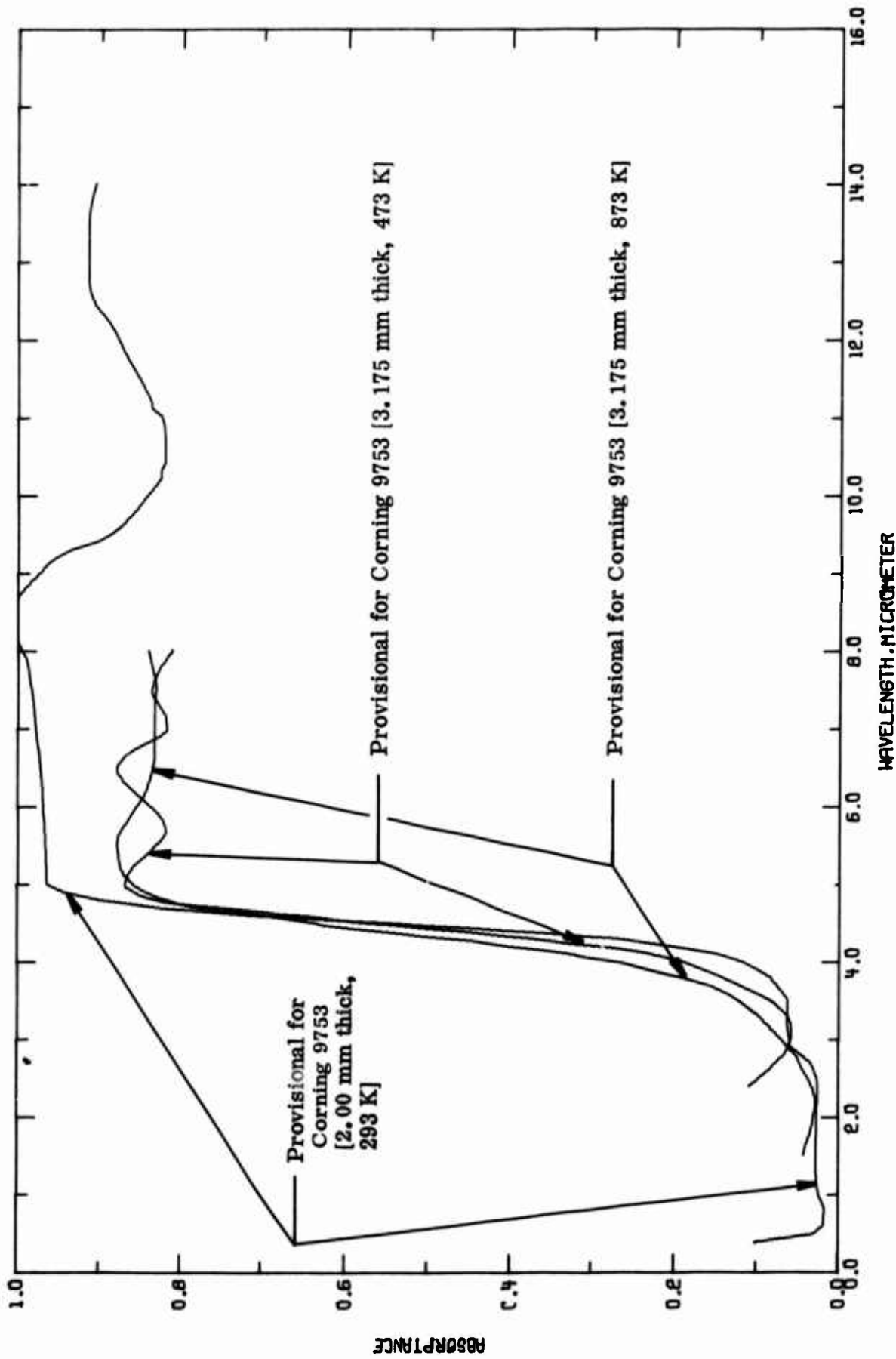


FIGURE 8-8. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

f. Normal Spectral Transmittance (Wavelength Dependence)

There are 17 sets of experimental data available for the wavelength dependence of the normal spectral transmittance of calcium aluminum silicate, 13 of which apply to Corning 9753. The data is listed in Table 8-14 and shown in Figures 8-9 and 8-10. Specimen characterization and measurement information for the data are given in Table 8-13.

There are three data sets which are for a specimen thickness of 2.00 mm at room temperature (curves 1, 4, and 5). These three curves were used to determine a provisional curve. The provisional values are listed in Table 8-12 and shown in Figure 8-9. For values of transmittance over 0.5, the uncertainty is within 5% but around a transmittance value of 0.1, the uncertainty can reach 20%. These uncertainties are determined taking into account the slightly different thicknesses and the slightly different temperatures of the specimens for the data sets that formed the basis of these provisional value sets.

In order to show the effect of temperature on the normal spectral transmittance of Corning 9753, another provisional curve is given and is applicable to a specimen 2.00 mm thick at a temperature of 1173 K. The provisional values are listed in Table 8-12 and shown in Figure 8-9. The uncertainty is within 20% for this set of values.

It is noted that the provisional curve for 1173 K is above the provisional curve for 293 K in the region 1 to about 2.7 μm . However, the provisional curve for 1173 K is below the provisional curve for 293 K in the wavelength region of 3.3 to 4.9 μm .

For a specimen of 2.00 mm thick there is no normal spectral transmittance data above 1173 K and only one set available between 1173 K and room temperature. For specimen thicknesses of 3.175 and 12.7 mm, the highest temperature for which normal spectral transmittance data is available is 873 K.

TABLE 8-12. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (CORNING 9753) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| .00MM THICK | | | 2.00MM THICK | | | 2.00MM THICK | | | 2.00MM THICK | | |
|-------------|-------|-----------|--------------|-----------|-------|--------------|-------|-----------|--------------|-----------|---|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 0.319 | 0.090 | 2.30 | 0.080 | 4.75 | 0.101 | 1.00 | 0.067 | 3.69 | 0.739 | | |
| 0.324 | 0.023 | 2.40 | 0.080 | 4.79 | 0.069 | 1.10 | 0.091 | 3.70 | 0.736 | | |
| 0.331 | 0.069 | 2.50 | 0.079 | 4.80 | 0.063 | 1.11 | 0.091 | 3.79 | 0.707 | | |
| 0.337 | 0.108 | 2.60 | 0.076 | 4.83 | 0.047 | 1.20 | 0.092 | 3.80 | 0.704 | | |
| 0.341 | 0.141 | 2.70 | 0.071 | 4.87 | 0.028 | 1.30 | 0.092 | 3.85 | 0.681 | | |
| 0.345 | 0.204 | 2.80 | 0.060 | 4.90 | 0.020 | 1.40 | 0.092 | 3.90 | 0.660 | | |
| 0.353 | 0.352 | 2.86 | 0.050 | 4.92 | 0.014 | 1.50 | 0.092 | 3.94 | 0.640 | | |
| 0.359 | 0.463 | 2.90 | 0.047 | 4.95 | 0.004 | 1.60 | 0.091 | 4.00 | 0.610 | | |
| 0.364 | 0.538 | 2.98 | 0.043 | 5.00 | 0.000 | 1.62 | 0.091 | 4.02 | 0.602 | | |
| 0.371 | 0.626 | 3.08 | 0.042 | | | 1.70 | 0.090 | 4.10 | 0.555 | | |
| 0.377 | 0.674 | 3.16 | 0.043 | | | 1.80 | 0.090 | 4.17 | 0.506 | | |
| 0.387 | 0.734 | 3.20 | 0.044 | | | 1.90 | 0.089 | 4.20 | 0.486 | | |
| 0.394 | 0.771 | 3.30 | 0.047 | | | 2.00 | 0.089 | 4.26 | 0.440 | | |
| 0.400 | 0.795 | 3.40 | 0.048 | | | 2.10 | 0.087 | 4.30 | 0.404 | | |
| 0.42 | 0.824 | 3.50 | 0.048 | | | 2.20 | 0.086 | 4.40 | 0.314 | | |
| 0.45 | 0.843 | 3.58 | 0.046 | | | 2.30 | 0.085 | 4.41 | 0.300 | | |
| 0.48 | 0.862 | 3.61 | 0.045 | | | 2.36 | 0.085 | 4.50 | 0.212 | | |
| 0.50 | 0.868 | 3.69 | 0.040 | | | 2.43 | 0.085 | 4.57 | 0.140 | | |
| 0.53 | 0.874 | 3.74 | 0.036 | | | 2.50 | 0.085 | 4.60 | 0.110 | | |
| 0.54 | 0.876 | 3.80 | 0.030 | | | 2.56 | 0.085 | 4.61 | 0.103 | | |
| 0.56 | 0.878 | 3.86 | 0.022 | | | 2.60 | 0.084 | 4.64 | 0.074 | | |
| 0.60 | 0.881 | 3.90 | 0.016 | | | 2.70 | 0.080 | 4.70 | 0.049 | | |
| 0.64 | 0.883 | 3.96 | 0.006 | | | 2.71 | 0.079 | 4.79 | 0.021 | | |
| 0.67 | 0.884 | 4.00 | 0.798 | | | 2.80 | 0.070 | 4.80 | 0.017 | | |
| 0.73 | 0.885 | 4.04 | 0.788 | | | 2.88 | 0.057 | 4.87 | 0.000 | | |
| 0.80 | 0.884 | 4.10 | 0.770 | | | 2.90 | 0.053 | 4.90 | 0.000 | | |
| 0.90 | 0.880 | 4.16 | 0.744 | | | 2.97 | 0.047 | 5.00 | 0.000 | | |
| 1.00 | 0.977 | 4.20 | 0.723 | | | 3.00 | 0.046 | | | | |
| 1.04 | 0.876 | 4.25 | 0.690 | | | 3.04 | 0.047 | | | | |
| 1.10 | 0.875 | 4.30 | 0.653 | | | 3.10 | 0.051 | | | | |
| 1.20 | 0.874 | 4.36 | 0.590 | | | 3.19 | 0.049 | | | | |
| 1.30 | 0.874 | 4.40 | 0.544 | | | 3.20 | 0.048 | | | | |
| 1.40 | 0.874 | 4.47 | 0.460 | | | 3.26 | 0.043 | | | | |
| 1.50 | 0.874 | 4.50 | 0.410 | | | 3.30 | 0.038 | | | | |
| 1.60 | 0.875 | 4.53 | 0.358 | | | 3.34 | 0.031 | | | | |
| 1.70 | 0.876 | 4.63 | 0.245 | | | 3.40 | 0.018 | | | | |
| 1.80 | 0.877 | 4.65 | 0.193 | | | 3.45 | 0.001 | | | | |
| 2.00 | 0.878 | 4.69 | 0.148 | | | 3.50 | 0.791 | | | | |
| 2.14 | 0.879 | 4.70 | 0.136 | | | 3.60 | 0.766 | | | | |

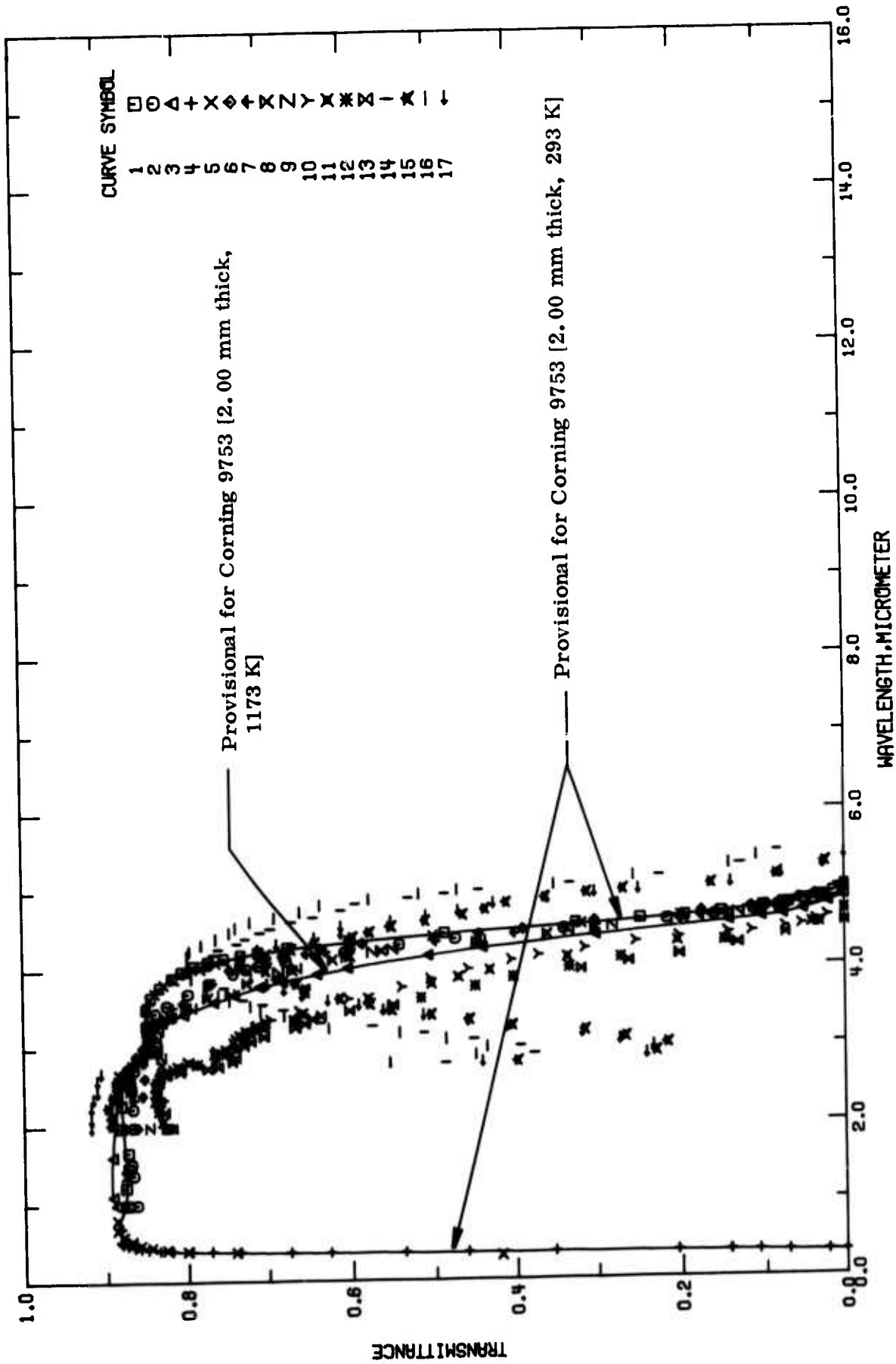


FIGURE 8-9. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

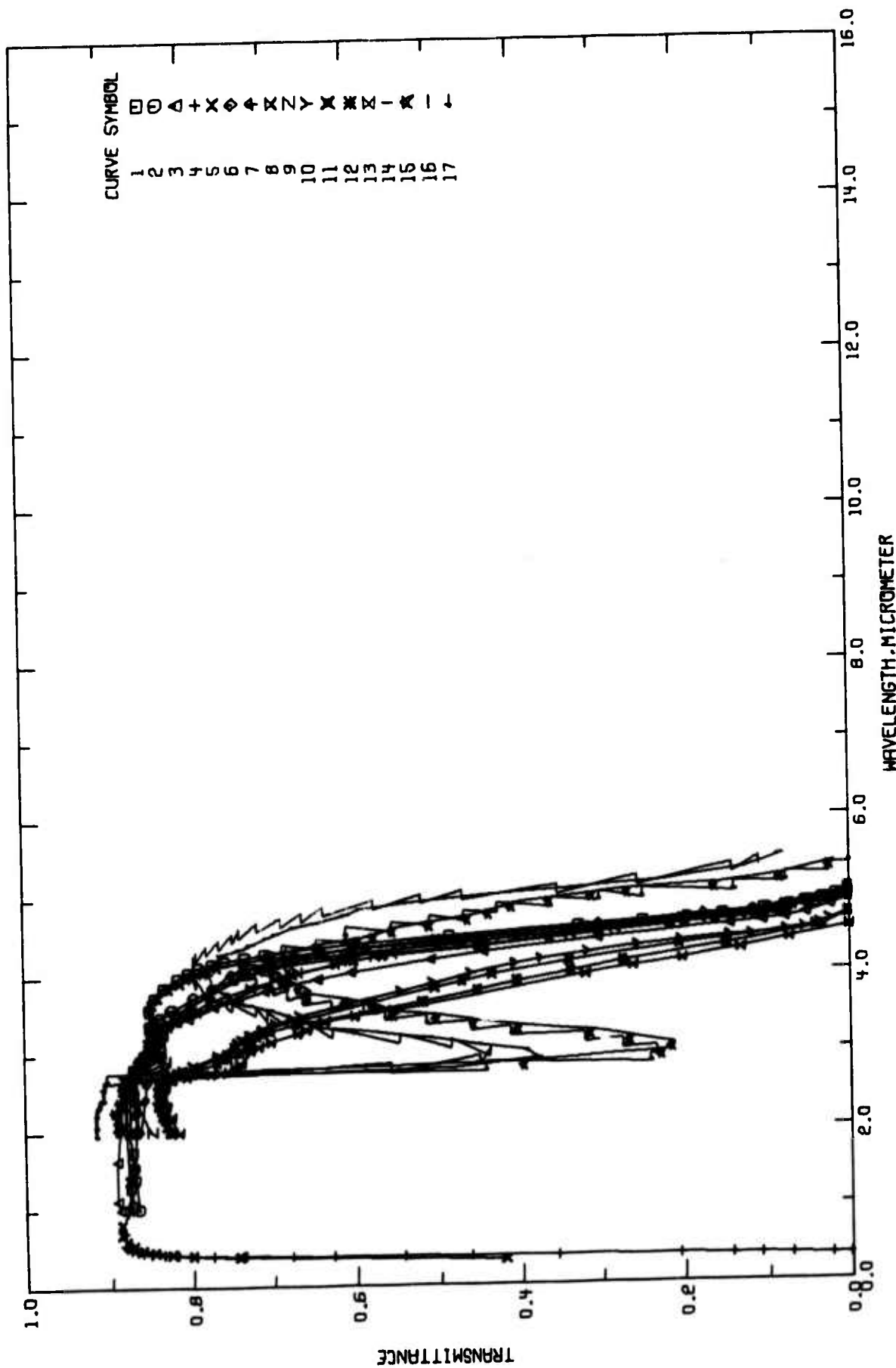


FIGURE 8-10. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE).

TABLE 8-13. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 A00009 | Kandrach, G.S. | 1975 | 1.0-5.0 | 298 | Corning 9753 | Specimen 2.02 mm thick; spectral transmittance; smooth values from figure. |
| 2 A00009 | Kandrach, G.S. | 1975 | 1.0-4.9 | 773 | Corning 9753 | Similar to the above specimen. |
| 3 A00009 | Kandrach, G.S. | 1975 | 1.0-4.9 | 1173 | Corning 9753 | Similar to the above specimen. |
| 4 A00009 | Kandrach, G.S. | 1975 | 0.52-0.70 | 293 | CGW-Glass 9753 | Specimen 2.02 mm thick; spectral transmittance; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 5 A00009 | Kandrach, G.S. | 1975 | 0.31-4.7 | 293 | Corning 9753 glass | Specimen typically 2.00 mm thick; spectral transmittance; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 6 A00009 | Kandrach, G.S. | 1975 | 2.0-5.0 | 293 | Corning 9753 | Specimen 0.3175 cm (1/8 in.) thick; spectral transmittance; smooth values from figure; measurement temperature specified as ambient temperature, 293 K assigned. |
| 7 A00009 | Kandrach, G.S. | 1975 | 2.0-4.9 | 473 | Corning 9753 | Specimen 0.3175 cm (1/8 in.) thick; spectral transmittance; smooth values from figure. |
| 8 A00009 | Kandrach, G.S. | 1975 | 2.0-4.7 | 673 | Corning 9753 | Similar to the above specimen. |
| 9 A00009 | Kandrach, G.S. | 1975 | 2.0-4.9 | 873 | Corning 9753 | Similar to the above specimen. |
| 10 A00009 | Kandrach, G.S. | 1975 | 2.0-4.7 | 293 | Corning 9753 | Specimen 1.27 cm (0.5 in.) thick; spectral transmittance; smooth values from figure; temperature called ambient temperature, 293 K assigned. |
| 11 A00009 | Kandrach, G.S. | 1975 | 2.0-4.7 | 473 | Corning 9753 | Specimen 1.27 cm (0.5 in.) thick; spectral transmittance; smooth values from figure. |
| 12 A00009 | Kandrach, G.S. | 1975 | 2.0-4.7 | 673 | Corning 9753 | Similar to the above specimen. |
| 13 A00009 | Kandrach, G.S. | 1975 | 2.0-4.5 | 873 | Corning 9753 | Similar to the above specimen. |
| 14 T39835 | Florence, J.M., Glaze, F.W., and Black, M.H. | 1955 | 2.0-5.5 | 293 | C-1458 | 52.0 CaO, 41.2 Al ₂ O ₃ , and 6.8 SiO ₂ ; specimen 2.18 mm thick; data from figure. |
| 15 T39835 | Florence, J.M., et al. | 1955 | 2.0-5.3 | 293 | C-1458 | Similar to the above specimen except thickness 4.10 mm. |
| 16 T39835 | Florence, J.M., et al. | 1955 | 2.0-5.4 | 293 | C-1474 | 49.5 CaO, 43.7 Al ₂ O ₃ , and 6.8 SiO ₂ ; specimen 2.02 mm thick; data from figure. |
| 17 T39835 | Florence, J.M., et al. | 1955 | 2.0-5.4 | 293 | C-1474 | Similar to the above specimen except thickness 4.16 mm. |

TABLE 6-14. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| CURVE 1 T = 298. | | CURVE 2 T = 773. | | CURVE 3 (CONT.) | | CURVE 4 (CONT.) | | CURVE 5 (CONT.) | | CURVE 6 T = 293. | | CURVE 7 (CONT.) | | | |
|---------------------|-------|---------------------|-------|-----------------|-------|-----------------|-------|-----------------|---------|---------------------|----------|-----------------|-------|-------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | | |
| 1.00 | 0.873 | 1.00 | 0.662 | 2.60 | 0.870 | 0.400 | 0.795 | 4.42 | 0.500 | 4.42 | 0.861 | 2.59 | 0.654 | | |
| 1.23 | 0.875 | 1.39 | 0.856 | 2.88 | 0.857 | 0.409 | 0.817 | 4.55 | 0.317 | 4.55 | 0.854 | 2.83 | 0.654 | | |
| 1.48 | 0.872 | 1.53 | 0.868 | 2.97 | 0.847 | 0.417 | 0.833 | 4.64 | 0.198 | 4.64 | 0.854 | 2.91 | 0.852 | | |
| 1.66 | 0.872 | 2.00 | 0.866 | 3.04 | 0.849 | 0.429 | 0.848 | 4.74 | 0.090 | 4.74 | 0.848 | 3.01 | 0.854 | | |
| 2.00 | 0.880 | 2.24 | 0.865 | 3.19 | 0.843 | 0.443 | 0.856 | CURVE 6 | | | | | 3.12 | 0.848 | |
| 2.29 | 0.889 | 2.53 | 0.870 | 3.26 | 0.843 | 0.461 | 0.866 | T = 293. | | | | | 3.23 | 0.844 | |
| 2.61 | 0.876 | 2.65 | 0.870 | 3.34 | 0.831 | 0.484 | 0.874 | 2.00 | 0.861 | 3.31 | 0.844 | 3.31 | 0.844 | | |
| 2.74 | 0.871 | 2.74 | 0.864 | 3.45 | 0.861 | 0.510 | 0.860 | 2.41 | 0.854 | 3.41 | 0.814 | 3.41 | 0.814 | | |
| 2.86 | 0.861 | 2.97 | 0.834 | 3.60 | 0.766 | 0.532 | 0.862 | 2.63 | 0.851 | 3.54 | 0.814 | 3.54 | 0.814 | | |
| 3.00 | 0.845 | 3.05 | 0.834 | 3.69 | 0.739 | 0.700 | 0.882 | 2.83 | 0.853 | 4.01 | 0.725 | 4.01 | 0.725 | | |
| 3.19 | 0.845 | 3.23 | 0.844 | 3.79 | 0.707 | CURVE 5 | | | | | 4.10 | 0.698 | | | |
| 3.30 | 0.849 | 3.33 | 0.844 | 3.85 | 0.681 | T = 293. | | | | | 4.15 | 0.679 | | | |
| 3.52 | 0.849 | 3.52 | 0.836 | 3.94 | 0.640 | 0.31 | 0.410 | 3.01 | 0.845 | 4.20 | 0.652 | 4.20 | 0.652 | | |
| 3.67 | 0.842 | 3.55 | 0.822 | 4.02 | 0.622 | 0.38 | 0.410 | 3.28 | 0.836 | 4.23 | 0.629 | 4.23 | 0.629 | | |
| 3.80 | 0.831 | 3.56 | 0.822 | 4.17 | 0.506 | 0.40 | 0.799 | 3.36 | 0.801 | 4.26 | 0.598 | 4.26 | 0.598 | | |
| 3.92 | 0.815 | 3.71 | 0.796 | 4.26 | 0.440 | 0.42 | 0.824 | 3.59 | 0.770 | 4.35 | 0.496 | 4.35 | 0.496 | | |
| 4.00 | 0.803 | 3.96 | 0.741 | 4.41 | 0.300 | 0.45 | 0.843 | 4.01 | 0.746 | 4.44 | 0.399 | 4.44 | 0.399 | | |
| 4.07 | 0.769 | 4.02 | 0.724 | 4.57 | 0.140 | 0.48 | 0.856 | 4.39 | 0.733 | 4.53 | 0.299 | 4.53 | 0.299 | | |
| 4.12 | 0.772 | 4.06 | 0.706 | 4.61 | 0.103 | 0.53 | 0.669 | 4.44 | 0.702 | 4.64 | 0.173 | 4.64 | 0.173 | | |
| 4.16 | 0.753 | 4.12 | 0.676 | 4.64 | 0.074 | 0.59 | 0.679 | 4.44 | 0.636 | 4.67 | 0.141 | 4.67 | 0.141 | | |
| 4.20 | 0.731 | 4.22 | 0.605 | 4.70 | 0.049 | 0.68 | 0.879 | 4.44 | 0.584 | 4.72 | 0.102 | 4.72 | 0.102 | | |
| 4.24 | 0.708 | 4.31 | 0.542 | 4.79 | 0.021 | 0.81 | 0.886 | 4.44 | 0.498 | 4.78 | 0.051 | 4.78 | 0.051 | | |
| 4.29 | 0.674 | 4.38 | 0.472 | 4.97 | 0.000 | 1.00 | 0.986 | 4.44 | 0.444 | 4.84 | 0.026 | 4.84 | 0.026 | | |
| 4.37 | 0.599 | 4.49 | 0.339 | CURVE 4 | | | | | 4.49 | 0.389 | CURVE 8 | | | | |
| 4.46 | 0.485 | 4.60 | 0.214 | T = 293. | | | | | 4.59 | 0.301 | T = 673. | | | | |
| 4.57 | 0.324 | 4.65 | 0.155 | 0.319 | 0.000 | 2.68 | 0.882 | 4.70 | 0.172 | 2.00 | 0.874 | 2.00 | 0.874 | | |
| 4.57 | 0.324 | 4.76 | 0.112 | 3.24 | 0.023 | 2.81 | 0.829 | 4.74 | 0.115 | 2.76 | 0.873 | 2.76 | 0.873 | | |
| 4.65 | 0.193 | 4.81 | 0.070 | 3.31 | 0.069 | 3.31 | 0.847 | 4.76 | 0.096 | 2.79 | 0.866 | 2.79 | 0.866 | | |
| 4.69 | 0.148 | 4.89 | 0.037 | 3.37 | 0.108 | 3.54 | 0.844 | 4.79 | 0.079 | 2.93 | 0.852 | 2.93 | 0.852 | | |
| 4.75 | 0.101 | 4.79 | 0.060 | 3.41 | 0.141 | 3.72 | 0.837 | 4.88 | 0.035 | 3.01 | 0.844 | 3.01 | 0.844 | | |
| 4.79 | 0.069 | CURVE 3 | | | | | 3.83 | 0.825 | 5.00 | 0.000 | 3.20 | 0.842 | 3.20 | 0.842 | |
| 4.83 | 0.047 | T = 1173. | | | | | 3.90 | 0.812 | CURVE 7 | | | | | 3.29 | 0.839 |
| 4.87 | 0.028 | 1.00 | 0.287 | 3.97 | 0.352 | 3.97 | 0.797 | 2.00 | 0.861 | 3.35 | 0.834 | 3.35 | 0.834 | | |
| 4.92 | 0.014 | 1.11 | 0.891 | 4.03 | 0.460 | 4.03 | 0.782 | 2.36 | 0.824 | 3.41 | 0.824 | 3.41 | 0.824 | | |
| 5.00 | 0.000 | 1.62 | 0.891 | 4.10 | 0.538 | 4.10 | 0.763 | 2.36 | 0.865 | 3.54 | 0.798 | 3.54 | 0.798 | | |
| | | 2.36 | 0.885 | 4.17 | 0.674 | 4.17 | 0.732 | 2.46 | 0.868 | 3.66 | 0.773 | 3.66 | 0.773 | | |
| | | 2.71 | 0.879 | 4.21 | 0.734 | 4.21 | 0.699 | | | | | | | | |
| | | | | 4.32 | 0.771 | 4.32 | 0.600 | | | | | | | | |

TABLE 8-14. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ |
|------------------|--------|-----------|--------|-----------|--------|
| CURVE 15 (CONT.) | | | | | |
| 4.54 | 0.552 | 4.25 | 0.794 | 3.82 | 0.698 |
| 4.61 | 0.510 | 4.33 | 0.780 | 3.91 | 0.718 |
| 4.68 | 0.464 | 4.40 | 0.763 | 4.02 | 0.736 |
| 4.75 | 0.437 | 4.48 | 0.746 | 4.10 | 0.736 |
| 4.83 | 0.410 | 4.54 | 0.738 | 4.16 | 0.709 |
| 4.89 | 0.382 | 4.62 | 0.719 | 4.26 | 0.709 |
| 4.95 | 0.351 | 4.67 | 0.699 | 4.33 | 0.687 |
| 4.99 | 0.266 | 4.74 | 0.660 | 4.40 | 0.643 |
| 5.05 | 0.160 | 4.82 | 0.636 | 4.47 | 0.610 |
| 5.15 | 0.084 | 4.89 | 0.576 | 4.55 | 0.610 |
| 5.30 | 0.024 | 4.96 | 0.518 | 4.61 | 0.552 |
| CURVE 16 (CONT.) | | | | | |
| | | 5.00 | 0.470 | 4.68 | 0.509 |
| | | 5.06 | 0.351 | 4.74 | 0.468 |
| | | 5.16 | 0.253 | 4.83 | 0.426 |
| | | 5.30 | 0.139 | 4.89 | 0.359 |
| | | 5.39 | 0.109 | 4.96 | 0.301 |
| | | | | 4.99 | 0.247 |
| | | | | 5.05 | 0.137 |
| | | | | 5.17 | 0.076 |
| | | | | 5.28 | 0.026 |
| | | | | 5.40 | 0.000 |
| CURVE 17 | | | | | |
| T = 293. | | | | | |
| 2.00 | 0.317 | 2.00 | 0.917 | | |
| 2.11 | 0.917 | 2.11 | 0.917 | | |
| 2.26 | 0.317 | 2.26 | 0.917 | | |
| 2.37 | 0.314 | 2.37 | 0.914 | | |
| 2.46 | 0.335 | 2.46 | 0.909 | | |
| 3.10 | 0.484 | 2.60 | 0.909 | | |
| 3.18 | 0.543 | 2.70 | 0.904 | | |
| 3.25 | 0.626 | 2.80 | 0.441 | | |
| 3.33 | 0.649 | 2.88 | 0.239 | | |
| 3.41 | 0.679 | 2.98 | 0.231 | | |
| 3.46 | 0.706 | 3.07 | 0.271 | | |
| 3.54 | 0.719 | 3.16 | 0.318 | | |
| 3.61 | 0.746 | 3.25 | 0.410 | | |
| 3.68 | 0.763 | 3.33 | 0.458 | | |
| 3.75 | 0.774 | 3.41 | 0.513 | | |
| 3.81 | 0.777 | 3.48 | 0.561 | | |
| 3.90 | 0.792 | 3.55 | 0.589 | | |
| 4.00 | 0.797 | 3.61 | 0.627 | | |
| 4.10 | 0.797 | 3.68 | 0.658 | | |
| 4.19 | 0.797 | 3.75 | 0.679 | | |

g. Normal Spectral Transmittance (Temperature Dependence)

There are 10 sets of experimental data available for the temperature dependence of the normal spectral transmittance of calcium aluminum silicate all of which apply to Corning 9753. The data is listed in Table 8-17 and shown in Figures 8-11 and 8-12. Specimen characterization and measurement information for the data are given in Table 8-16.

The 10 data sets are all for a thickness of 2 mm and cover a wavelength range of 3.5 to 4.7 μm . The temperature range covered is from slightly over 300 K to about 1175 K which is above the strain point (1073 K) but below the melting range (1723 to 1773 K).

A provisional curve is given for Corning 9753 at a wavelength of 3.8 μm . The provisional values are listed in Table 8-15 and shown in Figure 8-11. The provisional values were obtained by using linear interpolation between the 3.75 μm data (curve number 2 in Tables 8-16 and 8-17) and the 4.0 μm data (curve number 3 in Tables 8-16 and 8-17). Values of transmittance were read for the same values of temperatures and then linear interpolation performed. The uncertainty of the provisional values are no larger than 15%.

TABLE 4-15. PROVISIONAL NORMAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (CONFINING 9753) (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| T | τ |
|-----------------|--------|
| 2MM THICK | |
| $\lambda = 3.0$ | |
| 310. | 0.821 |
| 323. | 0.819 |
| 373. | 0.815 |
| 400. | 0.814 |
| 473. | 0.811 |
| 500. | 0.808 |
| 573. | 0.832 |
| 600. | 0.798 |
| 673. | 0.792 |
| 700. | 0.788 |
| 773. | 0.779 |
| 800. | 0.774 |
| 873. | 0.761 |
| 900. | 0.756 |
| 973. | 0.744 |
| 1000. | 0.739 |
| 1073. | 0.727 |
| 1100. | 0.720 |
| 1173. | 0.701 |

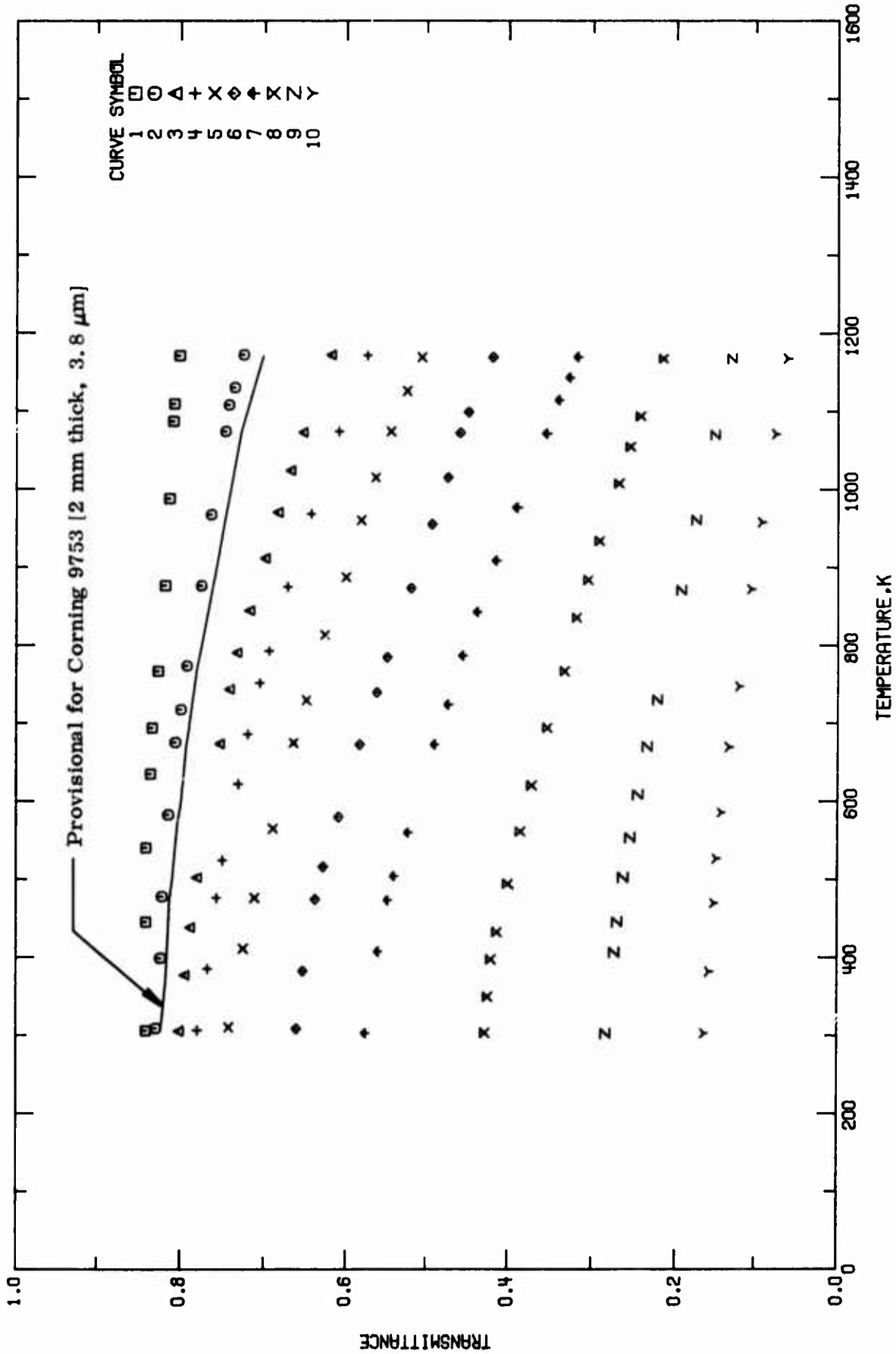


FIGURE 8-11. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE).

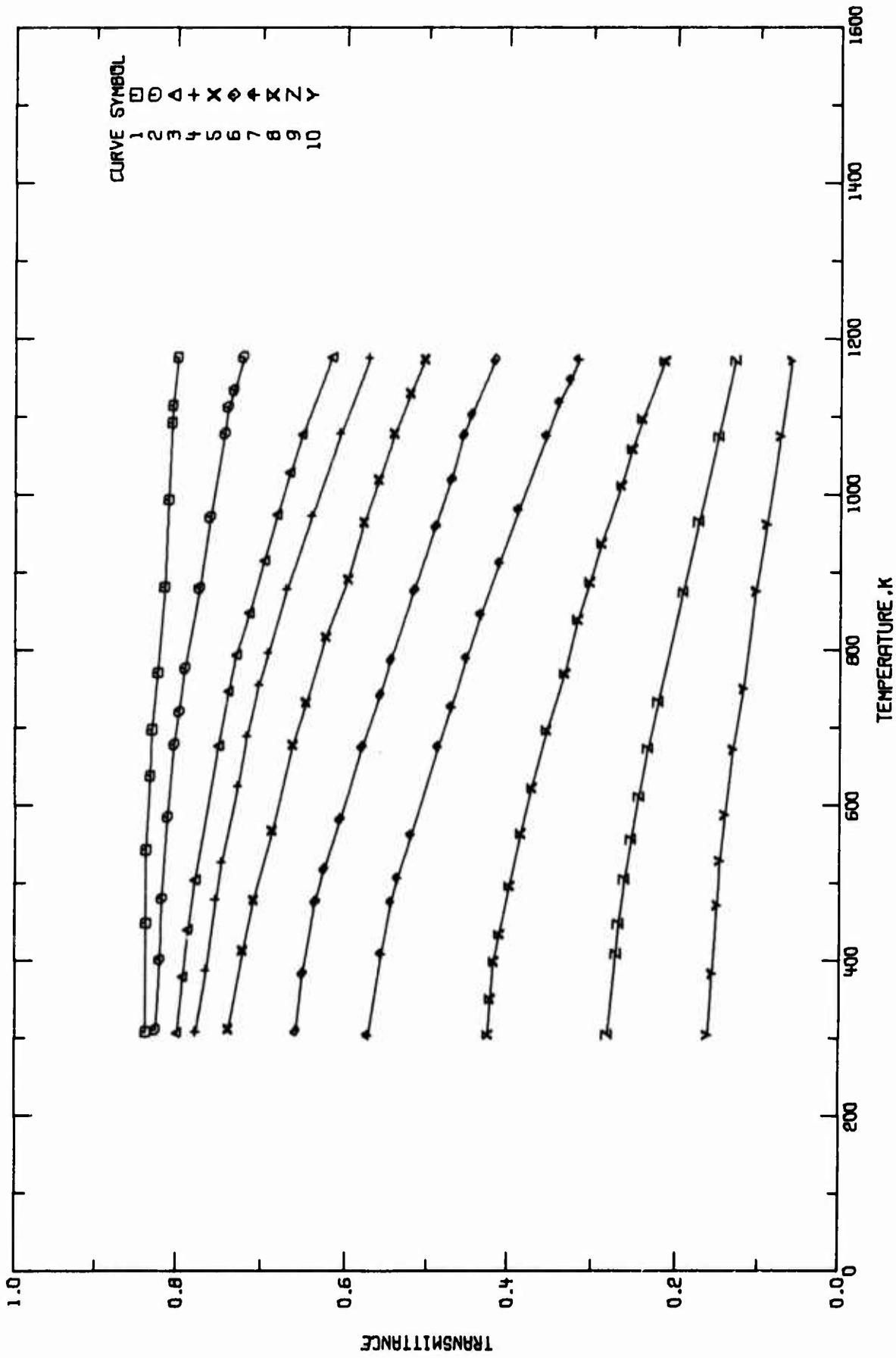


FIGURE 8-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE).

TABLE 8-16. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00009 | Kandrach, G.S. | 1975 | 3.5 | 307-1174 | Code 9753 | Specimen 2 mm thick; smooth values from figure; additional information supplied by Corning Glass Works. |
| 2 A00009 | Kandrach, G.S. | 1975 | 3.75 | 310-1174 | Code 9753 | Similar to the above specimen. |
| 3 A00009 | Kandrach, G.S. | 1975 | 4.0 | 306-1174 | Code 9753 | Similar to the above specimen. |
| 4 A00009 | Kandrach, G.S. | 1975 | 4.1 | 307-1173 | Code 9753 | Similar to the above specimen. |
| 5 A00009 | Kandrach, G.S. | 1975 | 4.2 | 311-1171 | Code 9753 | Similar to the above specimen. |
| 6 A00009 | Kandrach, G.S. | 1975 | 4.3 | 309-1171 | Code 9753 | Similar to the above specimen. |
| 7 A00009 | Kandrach, G.S. | 1975 | 4.4 | 303-1171 | Code 9753 | Similar to the above specimen. |
| 8 A00009 | Kandrach, G.S. | 1975 | 4.5 | 304-1169 | Code 9753 | Similar to the above specimen. |
| 9 A00009 | Kandrach, G.S. | 1975 | 4.6 | 303-1169 | Code 9753 | Similar to the above specimen. |
| 10 A00009 | Kandrach, G.S. | 1975 | 4.7 | 303-1169 | Code 9753 | Similar to the above specimen. |

TABLE 3-17. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF CALCIUM ALUMINUM SILICATE (TEMPERATURE DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| T | T | T | T | T | T | T | T | T | T | T | T | T | T |
|-----------------------------|-------|----------------------------|-------|----------------------------|-------|----------------------------|-------|-----------------------------|-------|----------------------------|-------|----------------------------|-------|
| CURVE 1 $\lambda = 3.5$ | | | | | | | | | | | | | |
| 307. | 0.838 | 846. | 0.716 | 309. | 0.660 | 398. | 0.416 | 742. | 0.119 | | | | |
| 447. | 0.838 | 913. | 0.698 | 383. | 0.652 | 433. | 0.411 | 873. | 0.104 | | | | |
| 542. | 0.838 | 1026. | 0.668 | 475. | 0.637 | 495. | 0.399 | 959. | 0.091 | | | | |
| 637. | 0.833 | 1075. | 0.653 | 517. | 0.627 | 562. | 0.385 | 1072. | 0.074 | | | | |
| 695. | 0.831 | 1174. | 0.618 | 531. | 0.608 | 621. | 0.372 | 1169. | 0.060 | | | | |
| 769. | 0.824 | | | 574. | 0.582 | 695. | 0.354 | | | | | | |
| 879. | 0.816 | CURVE 4 $\lambda = 4.1$ | | | | | | | | | | | |
| 591. | 0.811 | 741. | 0.560 | 780. | 0.547 | 837. | 0.318 | | | | | | |
| 1090. | 0.807 | 875. | 0.518 | 957. | 0.492 | 885. | 0.304 | | | | | | |
| 1112. | 0.806 | 1017. | 0.472 | 1099. | 0.267 | 935. | 0.290 | | | | | | |
| 1174. | 0.800 | 1074. | 0.457 | 1009. | 0.254 | 1056. | 0.267 | | | | | | |
| | | 1101. | 0.447 | 1095. | 0.242 | 1095. | 0.242 | | | | | | |
| | | 1171. | 0.417 | 1171. | 0.447 | 1169. | 0.215 | | | | | | |
| CURVE 2 $\lambda = 3.75$ | | | | | | | | | | | | | |
| 310. | 0.826 | 687. | 0.716 | CURVE 5 $\lambda = 4.2$ | | | | | | | | | |
| 430. | 0.821 | 753. | 0.704 | 311. | 0.740 | CURVE 6 $\lambda = 4.3$ | | | | | | | |
| 479. | 0.819 | 794. | 0.693 | 412. | 0.723 | 303. | 0.574 | CURVE 7 $\lambda = 4.4$ | | | | | |
| 584. | 0.812 | 876. | 0.671 | 477. | 0.710 | 408. | 0.558 | 303. | 0.282 | CURVE 8 $\lambda = 4.6$ | | | |
| 677. | 0.804 | 970. | 0.642 | 566. | 0.688 | 477. | 0.546 | 407. | 0.272 | 303. | 0.269 | CURVE 9 $\lambda = 4.6$ | |
| 719. | 0.798 | 1076. | 0.608 | 676. | 0.664 | 505. | 0.538 | 446. | 0.262 | 303. | 0.254 | 303. | 0.282 |
| 775. | 0.791 | 1173. | 0.573 | 731. | 0.643 | 561. | 0.521 | 533. | 0.262 | 407. | 0.245 | 407. | 0.272 |
| 378. | 0.774 | CURVE 3 $\lambda = 4.0$ | | | | | | | | | | | |
| 959. | 0.762 | 311. | 0.740 | 674. | 0.488 | 674. | 0.488 | 554. | 0.254 | 609. | 0.222 | 609. | 0.245 |
| 1076. | 0.745 | 412. | 0.723 | 725. | 0.471 | 725. | 0.471 | 609. | 0.245 | 671. | 0.234 | 671. | 0.234 |
| 1110. | 0.741 | 477. | 0.710 | 788. | 0.453 | 788. | 0.453 | 731. | 0.222 | 731. | 0.222 | 731. | 0.222 |
| 1132. | 0.734 | 566. | 0.688 | 844. | 0.435 | 844. | 0.435 | 672. | 0.193 | 672. | 0.193 | 672. | 0.193 |
| 1174. | 0.723 | 477. | 0.710 | 910. | 0.412 | 910. | 0.412 | 962. | 0.175 | 962. | 0.175 | 962. | 0.175 |
| | | 566. | 0.688 | 978. | 0.389 | 978. | 0.389 | 1071. | 0.151 | 1071. | 0.151 | 1071. | 0.151 |
| | | 731. | 0.643 | 1073. | 0.355 | 1073. | 0.355 | 1169. | 0.130 | 1169. | 0.130 | 1169. | 0.130 |
| | | 815. | 0.625 | 1116. | 0.340 | 1116. | 0.340 | CURVE 10 $\lambda = 4.7$ | | | | | |
| | | 889. | 0.599 | 1145. | 0.327 | 1145. | 0.327 | 303. | 0.163 | 303. | 0.163 | 303. | 0.163 |
| | | 902. | 0.580 | 1171. | 0.317 | 1171. | 0.317 | 352. | 0.157 | 352. | 0.157 | 352. | 0.157 |
| | | 1017. | 0.562 | CURVE 8 $\lambda = 4.5$ | | | | | | | | | |
| | | 1076. | 0.543 | 304. | 0.425 | 304. | 0.425 | 470. | 0.151 | 470. | 0.151 | 470. | 0.151 |
| | | 1128. | 0.523 | 350. | 0.422 | 350. | 0.422 | 527. | 0.148 | 527. | 0.148 | 527. | 0.148 |
| | | 1171. | 0.505 | | | | | 586. | 0.142 | 586. | 0.142 | 586. | 0.142 |
| | | | | | | | | 670. | 0.132 | 670. | 0.132 | 670. | 0.132 |

4.9. Magnesium Fluoride

Since data evaluation was asked to be carried out on the specific kind of magnesium fluoride known as Irtran 1, the treatment in this section will concentrate on that material.

Irtran 1, produced by the Eastman Kodak Company, is a hot-pressed, polycrystalline solid of magnesium fluoride, MgF_2 . The word "Irtran" is a trademark of the Eastman Kodak Company. Because it is polycrystalline it does not exhibit cleavage. The visual appearance of Irtran 1 is transparent in colors ranging from tan to green [E62600]. According to Kodak [E62600], the long-range infrared cut-off frequency is approximately $7.5 \mu m$ for a 2 mm thick specimen for which the transmittance is 10%. It has a Knoop hardness of 576 and is approximately as hard as soft steel. The density is 3.18 g cm^{-3} at 298 K. Other physical properties include a modulus of rupture of 21,800 psi at 298 K, and an expansion coefficient of $11.0 \times 10^{-6} \text{ C}^{-1}$ between 298 and 473 K. It is insoluble in water and there is no change in transmittance or weight upon both inorganic and organic chemical immersion. It has a melting point of 1528 K [T39947] and a high thermal shock resistance. It is used as windows, domes, prisms, and filter substrates for infrared systems.

a. Normal Spectral Emittance (Wavelength Dependence)

A total of 20 sets of experimental data were located for the wavelength dependence of the normal spectral emittance of Irtran 1. The data are listed in Table 9-3 and shown in Figures 9-1 and 9-2. Specimen characterization and measurement information for the data are given in Table 9-2.

Numerical values of the data are low at $4.5 \mu m$, being less than 0.16 and above $5.5 \mu m$ they increase sharply such that above $10 \mu m$ all the data are above 0.75. There is a conflicting element in the data. Stierwalt, et al. [T33450] presented data for a 2 mm thick specimen at 333 K (curve 17), 393 K (curve 18), and 453 K (curve 19). Above $10 \mu m$ the values of the normal spectral emittance for these curves are between 0.75 and 0.90. Hatch [T76525] presented an argument that the emittance for specimen thicknesses of 1 mm or greater should be greater than 0.99 from 293 to 970 K and between 10 and $15 \mu m$. The argument of Hatch and the data of Stierwalt, et al. are incompatible. As a consequence it was decided to consider evaluated data only within a restricted wavelength range of 3 to $6.4 \mu m$.

Provisional values for a 2 mm thick specimen at a temperature of 293 K for a wavelength region of 3 to $6.4 \mu m$ are listed in Table 9-1 and shown in Figure 9-1. These values were generated by using the Kodak scheme, Eqs. (2.6-13) and (2.6-15), for

calculating emittance from transmittance and refractive index data. The transmittance data used was data from curve 22 in Tables 9-17 and 9-18. The refractive index data used was taken from the data of curve 2 in Tables 9-4 and 9-5. The refractive index data is shown in Figure 9-3. Provisional values for a specimen thickness of 3.8 mm at a temperature of 589 K for a wavelength range of 3 to 6.4 μm are given, as well as a set of provisional values for a thickness of 3.8 mm, a temperature of 970 K, and a wavelength range of 3 to 6.0 μm . The provisional values for 589 K are based on curve 8 while those for 970 K are based on curve 11. The values are listed in Table 9-1 and shown in Figure 9-1. Because of the low value of emittance, the uncertainty for all three provisional curves can be as high as 25%.

TABLE 9-1. PROVISIONAL NORMAL SPECTRAL EMISSANCE OF MAGNESIUM FLUORIDE (IRTRAN 1) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMISSANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ |
|-----------|------------|-------------|------------|-------------|------------|
| 2MM THICK | | 3.0MM THICK | | 3.0MM THICK | |
| T = 293 | | T = 589 | | T = 970 | |
| 3.00 | 0.089 | 3.0 | 0.154 | 3.0 | 0.177 |
| 3.03 | 0.095 | 3.11 | 0.124 | 3.07 | 0.155 |
| 3.10 | 0.073 | 3.24 | 0.102 | 3.31 | 0.109 |
| 3.19 | 0.074 | 3.42 | 0.076 | 3.56 | 0.083 |
| 3.27 | 0.069 | 3.80 | 0.053 | 3.80 | 0.071 |
| 3.30 | 0.065 | 4.0 | 0.048 | 4.0 | 0.070 |
| 3.49 | 0.060 | 4.14 | 0.045 | 4.42 | 0.066 |
| 3.80 | 0.060 | 4.64 | 0.045 | 4.61 | 0.076 |
| 3.98 | 0.059 | 4.97 | 0.052 | 4.98 | 0.081 |
| 4.00 | 0.060 | 5.0 | 0.054 | 5.0 | 0.084 |
| 4.46 | 0.060 | 5.09 | 0.061 | 5.23 | 0.111 |
| 4.68 | 0.060 | 5.25 | 0.078 | 5.47 | 0.094 |
| 4.78 | 0.057 | 5.46 | 0.061 | 5.65 | 0.111 |
| 4.88 | 0.052 | 5.68 | 0.051 | 5.84 | 0.154 |
| 4.95 | 0.058 | 5.79 | 0.077 | 6.00 | 0.187 |
| 5.00 | 0.057 | 6.0 | 0.107 | | |
| 5.01 | 0.058 | 6.01 | 0.108 | | |
| 5.13 | 0.050 | 6.20 | 0.145 | | |
| 5.23 | 0.046 | 6.35 | 0.185 | | |
| 5.32 | 0.044 | 6.4 | 0.197 | | |
| 5.59 | 0.045 | | | | |
| 5.69 | 0.050 | | | | |
| 5.79 | 0.054 | | | | |
| 5.87 | 0.060 | | | | |
| 6.00 | 0.071 | | | | |
| 6.16 | 0.087 | | | | |
| 6.34 | 0.109 | | | | |
| 6.40 | 0.118 | | | | |

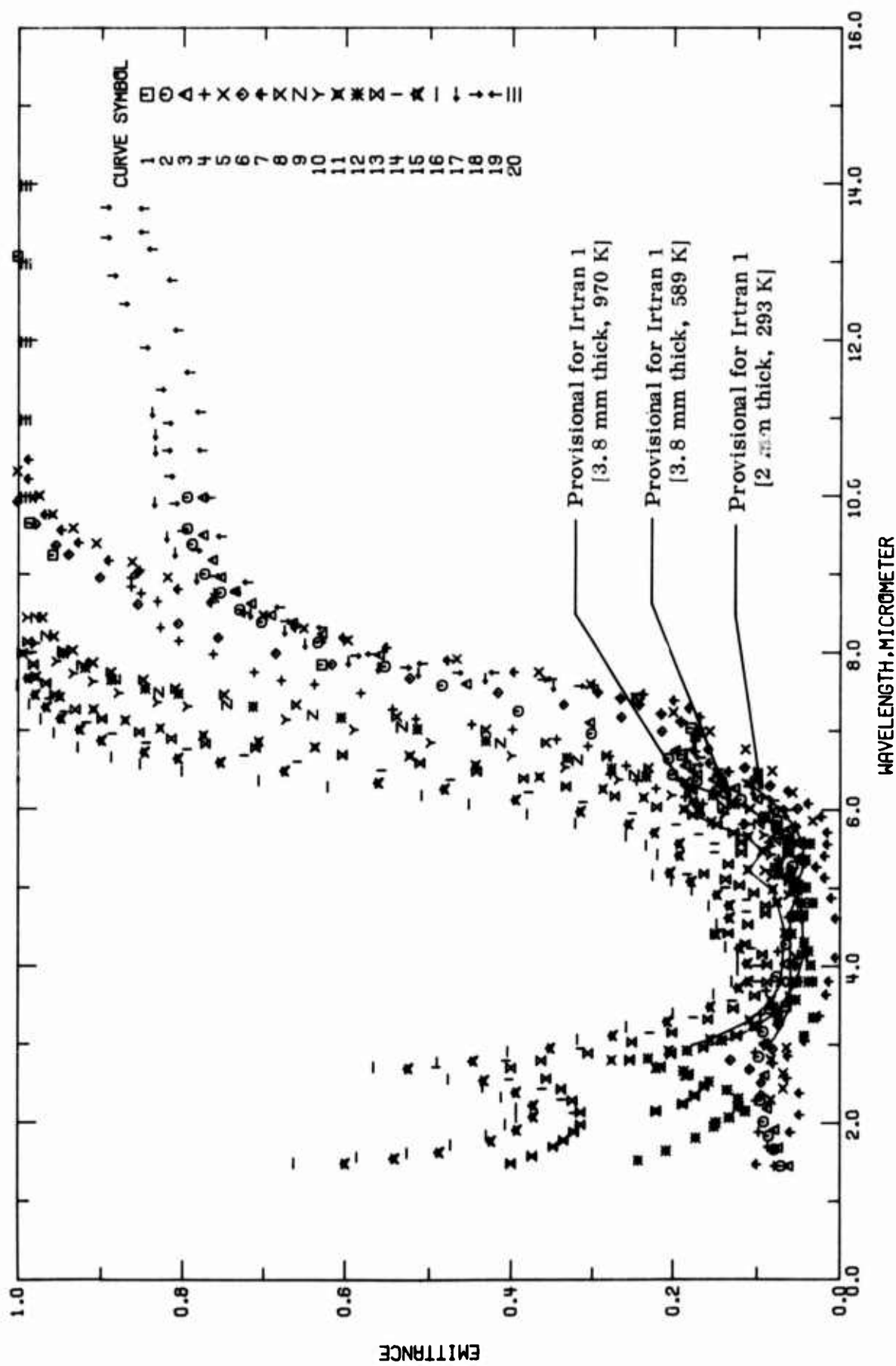


FIGURE 9-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

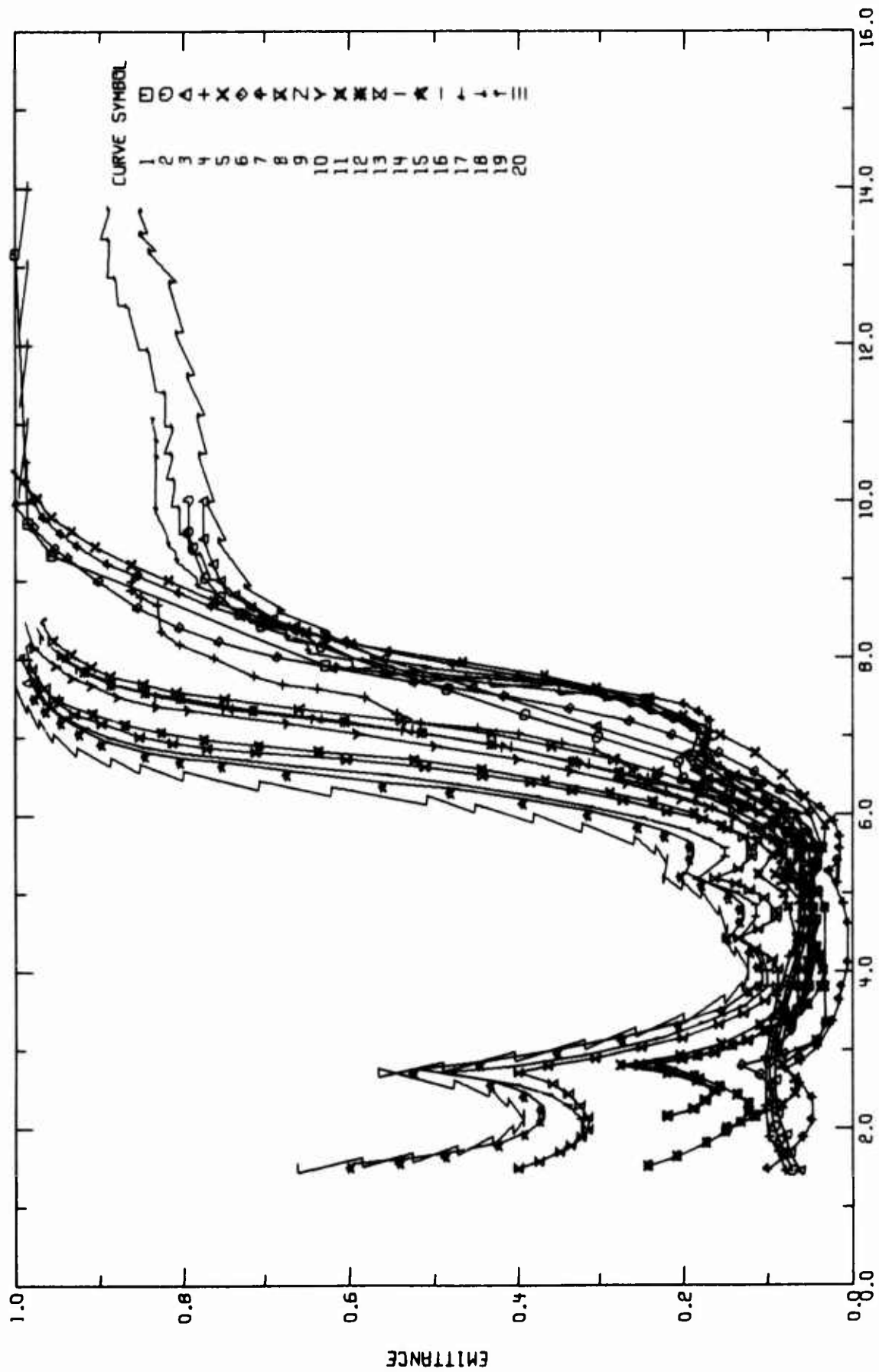


FIGURE 9-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

TABLE 9-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T39952 | Stierwalt, D. L. | 1966 | 3.5-45 | 77 | Irtran 1 | Sample 2.0 mm thick; material from Eastman Kodak Co.; smooth values from figure; $\theta' = 0^\circ$. |
| 2 T17017 | Ballard, S.S., McCarthy, K.A., and Wolfe, W. L. | 1961 | 1.5-10 | 673 | Irtran 1 | Specimen thickness 1.75 mm; emissivity; information in this reference was obtained from Eastman Kodak Co. sales literature dated 15 June 1959 and 23 February 1961; $\theta' = 0^\circ$. |
| 3 T17017 | Ballard, S.S., et al. | 1961 | 1.5-10 | 873 | Irtran 1 | Similar to the above specimen. |
| 4 T17017 | Ballard, S.S., et al. | 1961 | 1.5-9.1 | 1073 | Irtran 1 | Similar to the above specimen. |
| 5 T76525 | Hatch, S.E. | 1962 | 2.0-10 | 647 | Irtran 1 | Specimen 1 mm thick; specimen holder uncoated stainless steel; smooth values from figure. |
| 6 T76525 | Hatch, S.E. | 1962 | 2.0-10 | 865 | Irtran 1 | The above specimen. |
| 7 T76525 | Hatch, S.E. | 1962 | 1.5-10 | 647 | Irtran 1 | The above specimen except specimen holder gold plated. |
| 8 T76525 | Hatch, S.E. | 1962 | 2.2-8.5 | 589 | Irtran 1 | Specimen 3.8 mm thick; specimen holder uncoated stainless steel; smooth values from figure. |
| 9 T76525 | Hatch, S.E. | 1962 | 2.2-8.5 | 647 | Irtran 1 | The above specimen. |
| 10 T76525 | Hatch, S.E. | 1962 | 2.2-8.5 | 865 | Irtran 1 | The above specimen. |
| 11 T76525 | Hatch, S.E. | 1962 | 2.2-8.0 | 970 | Irtran 1 | The above specimen. |
| 12 T76525 | Hatch, S.E. | 1962 | 1.5-8.0 | 647 | Irtran 1 | The above specimen except specimen holder gold plated. |
| 13 T76525 | Hatch, S.E. | 1962 | 1.5-8.2 | 594 | Irtran 1 | Specimen 7.6 mm thick; specimen holder uncoated stainless steel; smooth values from figure. |
| 14 T76525 | Hatch, S.E. | 1962 | 1.5-8.0 | 647 | Irtran 1 | The above specimen. |
| 15 T76525 | Hatch, S.E. | 1962 | 1.5-7.7 | 865 | Irtran 1 | The above specimen. |
| 16 T76525 | Hatch, S.E. | 1962 | 1.5-8.0 | 970 | Irtran 1 | The above specimen. |
| 17 T33450 | Stierwalt, D. L., Kirk, D.D., and Bernstein, J.B. | 1963 | 3.0-11 | 333 | Irtran 1 | Specimen 2 mm thick; smooth values from figure. |
| 18 T33450 | Stierwalt, D. L., et al. | 1963 | 3.0-15 | 393 | Irtran 1 | Similar to the above specimen. |
| 19 T33450 | Stierwalt, D. L., et al. | 1963 | 3.0-15 | 453 | Irtran 1 | Similar to the above specimen. |
| 20 T76525 | Hatch, S.E. | 1962 | 10-15 | 293 | Irtran 1 | Thickness 1 mm or greater; argument given on p. 597 of this reference that emittance between 10 and 15 μ is greater than 0.99 from ambient temperature, 293 K assigned, to 970 K; $\theta' = 0^\circ$. |

TABLE 9-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CURVE 12 (CONT.) | | CURVE 13 (CONT.) | | CURVE 14 (CONT.) | | CURVE 15 | | CURVE 15 (CONT.) | | CURVE 16 (CONT.) | | |
|------------------|------------|------------------|------------|------------------|------------|-----------|------------|------------------|------------|------------------|------------|-------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | |
| 6.18 | 0.152 | 4.42 | 0.134 | 2.12 | 0.322 | 1.49 | 0.600 | 7.16 | 0.947 | 5.94 | 0.381 | |
| 6.26 | 0.180 | 4.53 | 0.111 | 2.29 | 0.338 | 1.55 | 0.541 | 7.31 | 0.365 | 6.07 | 0.452 | |
| 6.42 | 0.233 | 4.67 | 0.090 | 2.43 | 0.362 | 1.63 | 0.488 | 7.47 | 0.978 | 6.18 | 0.509 | |
| 6.52 | 0.276 | 4.77 | 0.090 | 2.55 | 0.401 | 1.77 | 0.425 | 7.58 | 0.987 | 6.29 | 0.521 | |
| 6.66 | 0.332 | 4.93 | 0.104 | 2.71 | 0.491 | 1.91 | 0.393 | CURVE 16 | | | 6.37 | 0.706 |
| 6.88 | 0.432 | 5.03 | 0.121 | 2.79 | 0.406 | 2.08 | 0.373 | T = 970. | | | 6.49 | 0.800 |
| 7.03 | 0.514 | 5.11 | 0.137 | 2.94 | 0.314 | 2.22 | 0.373 | 1.49 | 0.662 | 6.58 | 0.852 | |
| 7.18 | 0.605 | 5.18 | 0.163 | 3.14 | 0.228 | 2.39 | 0.394 | 1.57 | 0.585 | 6.67 | 0.887 | |
| 7.32 | 0.713 | 5.30 | 0.134 | 3.34 | 0.176 | 2.54 | 0.434 | 1.62 | 0.526 | 6.80 | 0.927 | |
| 7.46 | 0.804 | 5.45 | 0.119 | 3.55 | 0.129 | 2.70 | 0.525 | 1.72 | 0.474 | 6.98 | 0.955 | |
| 7.55 | 0.946 | 5.58 | 0.119 | 3.80 | 0.100 | 2.79 | 0.447 | 1.84 | 0.431 | 7.16 | 0.971 | |
| 7.66 | 0.887 | 5.70 | 0.128 | 4.00 | 0.100 | 2.95 | 0.352 | 1.98 | 0.407 | 7.35 | 0.985 | |
| 7.82 | 0.918 | 5.81 | 0.147 | 4.22 | 0.107 | 3.11 | 0.274 | 2.07 | 0.393 | 7.59 | 1.000 | |
| 8.00 | 0.944 | 5.93 | 0.177 | 4.41 | 0.133 | 3.29 | 0.207 | 2.18 | 0.393 | 8.00 | 0.999 | |
| CURVE 13 | | 6.33 | 0.220 | 4.69 | 0.113 | 3.48 | 0.155 | 2.33 | 0.412 | CURVE 17 | | |
| T = 594. | | 6.17 | 0.272 | 4.84 | 0.113 | 3.72 | 0.122 | 2.46 | 0.435 | T = 333. | | |
| 1.49 | 0.400 | 6.30 | 0.333 | 5.00 | 0.137 | 3.80 | 0.111 | 2.56 | 0.477 | 3.00 | 0.091 | |
| 1.58 | 0.374 | 6.40 | 0.305 | 5.17 | 0.184 | 4.03 | 0.112 | 2.71 | 0.565 | 3.25 | 0.074 | |
| 1.70 | 0.348 | 6.60 | 0.511 | 5.45 | 0.150 | 4.22 | 0.121 | 2.91 | 0.490 | 3.54 | 0.061 | |
| 1.78 | 0.335 | 6.70 | 0.603 | 5.68 | 0.170 | 4.40 | 0.148 | 2.78 | 0.404 | 3.80 | 0.052 | |
| 1.89 | 0.322 | 6.79 | 0.710 | 5.86 | 0.197 | 4.61 | 0.133 | 3.06 | 0.318 | 4.01 | 0.054 | |
| 1.95 | 0.314 | 6.84 | 0.771 | 5.95 | 0.250 | 4.77 | 0.133 | 3.22 | 0.257 | 4.61 | 0.046 | |
| 2.14 | 0.314 | 6.91 | 0.813 | 6.09 | 0.312 | 4.91 | 0.147 | 3.39 | 0.200 | 4.82 | 0.050 | |
| 2.29 | 0.324 | 6.99 | 0.853 | 6.22 | 0.379 | 5.03 | 0.179 | 3.64 | 0.151 | 5.07 | 0.050 | |
| 2.44 | 0.339 | 7.16 | 0.898 | 6.38 | 0.475 | 5.19 | 0.204 | 3.80 | 0.130 | 5.32 | 0.043 | |
| 2.57 | 0.357 | 7.28 | 0.930 | 6.50 | 0.556 | 5.41 | 0.193 | 3.94 | 0.123 | 5.58 | 0.043 | |
| 2.71 | 0.400 | 7.47 | 0.954 | 6.61 | 0.658 | 5.56 | 0.193 | 4.09 | 0.123 | 5.78 | 0.054 | |
| 2.80 | 0.363 | 7.62 | 0.965 | 6.69 | 0.724 | 5.70 | 0.223 | 4.24 | 0.137 | 5.94 | 0.065 | |
| 2.89 | 0.305 | 7.86 | 0.980 | 6.77 | 0.794 | 5.81 | 0.255 | 4.41 | 0.154 | 6.07 | 0.065 | |
| 3.03 | 0.250 | 8.15 | 0.987 | 6.85 | 0.845 | 5.97 | 0.315 | 4.53 | 0.147 | 6.23 | 0.105 | |
| 3.15 | 0.201 | CURVE 14 | | 6.97 | 0.886 | 6.12 | 0.395 | 4.77 | 0.157 | 6.36 | 0.141 | |
| 3.32 | 0.158 | T = 647. | | 7.11 | 0.917 | 6.26 | 0.482 | 4.97 | 0.178 | 6.50 | 0.175 | |
| 3.46 | 0.128 | 1.49 | 0.400 | 7.25 | 0.943 | 6.34 | 0.560 | 5.09 | 0.202 | 6.54 | 0.180 | |
| 3.62 | 0.103 | 1.58 | 0.374 | 7.42 | 0.961 | 6.49 | 0.674 | 5.16 | 0.225 | 6.66 | 0.136 | |
| 3.90 | 0.086 | 1.70 | 0.346 | 7.67 | 0.977 | 6.60 | 0.753 | 5.42 | 0.219 | 6.81 | 0.176 | |
| 4.02 | 0.088 | 1.78 | 0.346 | 8.00 | 0.986 | 6.65 | 0.805 | 5.54 | 0.233 | 6.97 | 0.176 | |
| 4.15 | 0.0394 | 1.78 | 0.335 | | | 6.73 | 0.847 | 5.66 | 0.256 | 7.12 | 0.191 | |
| 4.28 | 0.114 | 1.89 | 0.332 | | | 7.02 | 0.899 | 5.82 | 0.321 | 7.22 | 0.215 | |

TABLE 9-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|------------------|------------|-----------|------------|------------------|------------|------------------|------------|
| CURVE 17 (CONT.) | | | | | | | |
| 7.34 | 0.242 | 6.94 | 0.174 | 5.07 | 0.050 | 12. | >0.99 |
| 7.42 | 0.265 | 7.12 | 0.191 | 5.32 | 0.043 | 13. | >0.99 |
| 7.50 | 0.294 | 7.22 | 0.215 | 5.58 | 0.043 | 14. | >0.99 |
| 7.59 | 0.349 | 7.34 | 0.242 | 5.73 | 0.054 | 15. | >0.99 |
| 7.66 | 0.433 | 7.42 | 0.265 | 5.99 | 0.064 | | |
| 7.75 | 0.513 | 7.50 | 0.294 | 6.11 | 0.080 | | |
| 7.82 | 0.560 | 7.58 | 0.316 | 6.34 | 0.109 | | |
| 7.90 | 0.595 | 7.66 | 0.352 | 6.51 | 0.146 | | |
| 8.12 | 0.649 | 7.75 | 0.460 | 5.66 | 0.168 | | |
| 8.29 | 0.674 | 7.82 | 0.525 | 5.93 | 0.153 | | |
| 8.51 | 0.717 | 7.97 | 0.537 | 7.12 | 0.191 | | |
| 8.77 | 0.761 | 8.15 | 0.632 | 7.22 | 0.215 | | |
| 8.96 | 0.783 | 8.41 | 0.673 | 7.34 | 0.242 | | |
| 9.29 | 0.809 | 8.78 | 0.725 | 7.42 | 0.265 | | |
| 9.50 | 0.819 | 8.99 | 0.760 | 7.50 | 0.294 | | |
| 9.94 | 0.835 | 9.32 | 0.783 | 7.57 | 0.351 | | |
| 10.60 | 0.834 | 9.57 | 0.800 | 7.75 | 0.422 | | |
| 10.81 | 0.834 | 9.92 | 0.810 | 7.87 | 0.538 | | |
| 11.09 | 0.838 | 10.27 | 0.818 | 7.99 | 0.569 | | |
| CURVE 18 (CONT.) | | | | | | | |
| | | 10.60 | 0.819 | 8.33 | 0.628 | | |
| | | 10.95 | 0.818 | 8.59 | 0.680 | | |
| | | 11.38 | 0.827 | 8.91 | 0.720 | | |
| | | 11.92 | 0.847 | 9.50 | 0.752 | | |
| | | 12.48 | 0.872 | 9.99 | 0.766 | | |
| | | 12.84 | 0.886 | 10.60 | 0.776 | | |
| | | 13.33 | 0.894 | 11.09 | 0.778 | | |
| | | 13.72 | 0.894 | 11.60 | 0.791 | | |
| | | 14.17 | 0.882 | 12.14 | 0.805 | | |
| | | 14.62 | 0.862 | 12.78 | 0.813 | | |
| | | 13.18 | 0.838 | 13.18 | 0.838 | | |
| | | 13.40 | 0.848 | 13.40 | 0.848 | | |
| | | 13.70 | 0.849 | 13.70 | 0.849 | | |
| | | 14.29 | 0.817 | 14.29 | 0.817 | | |
| | | 15.00 | 0.789 | 15.00 | 0.789 | | |
| | | CURVE 19 | | CURVE 19 (CONT.) | | CURVE 20 (CONT.) | |
| | | T = 453. | | T = 293. | | | |
| 3.00 | 0.091 | 3.00 | 0.091 | | | | |
| 3.25 | 0.074 | 3.25 | 0.074 | | | | |
| 3.54 | 0.061 | 3.54 | 0.061 | | | | |
| 3.80 | 0.052 | 3.80 | 0.052 | | | | |
| 4.01 | 0.054 | 4.01 | 0.054 | | | | |
| 4.51 | 0.046 | 4.51 | 0.046 | | | | |
| 4.82 | 0.050 | | | | | | |
| 5.07 | 0.050 | | | | | | |
| 5.32 | 0.043 | | | | | | |
| 5.58 | 0.043 | | | | | | |
| 5.78 | 0.054 | | | | | | |
| 6.02 | 0.071 | | | | | | |
| 6.14 | 0.089 | | | | | | |
| 6.29 | 0.110 | | | | | | |
| 6.45 | 0.140 | | | | | | |
| 6.67 | 0.171 | | | | | | |
| 6.76 | 0.180 | | | | | | |
| | | | | 10. | >0.99 | | |
| | | | | 11. | >0.99 | | |

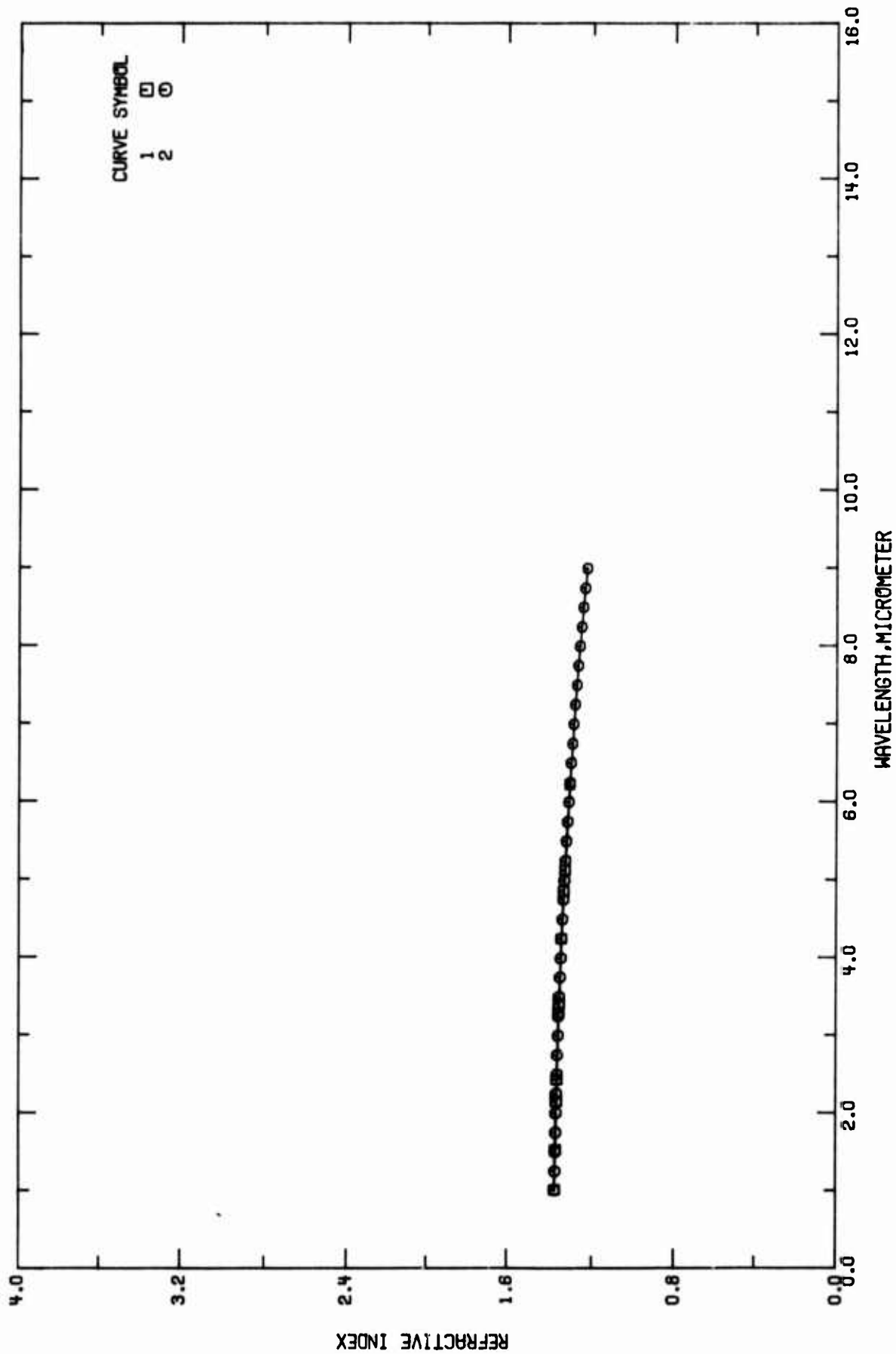


FIGURE 9-3. EXPERIMENTAL REFRACTIVE INDEX OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

TABLE 9-4. MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF MAGNESIUM FLUORIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 TT7017 | Ballard, S. S., McCarthy, K. A., and Wolfe, W. L. | 1965 | 1.0-6.3 | 293 | Irtran 1 | Information in this reference was obtained from Eastman Kodak Co. sales literature dated 15 June 1959 and 23 February 1961; measurement temperature not explicitly given, assumed to be 293 K. |
| 2 E62600 | Eastman Kodak Co. | 1971 | 1.0-9.0 | 293 | Irtran 1 | Measurements taken, constants in Herzberger dispersion equation determined by least squares methods; numerical values quoted here calculated from Herzberger dispersion equation: $n = n_0 + b\lambda + c\lambda^2 + d\lambda^4 + e\lambda^6$, where $L = 1.0 (\lambda^2 - 0.025)$, $n_0 = 1.3776955$, $b = 1.3515529 \times 10^{-3}$, $c = 2.1254394 \times 10^{-6}$, $d = -1.5041172 \times 10^{-9}$, $e = -4.4109708 \times 10^{-6}$, and λ is in micrometers, range of validity 1-9 μ ; measurement temperature not explicitly given, assumed to be 293 K. |

TABLE 9-5. EXPERIMENTAL REFRACTIVE INDEX OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFRACTIVE INDEX, n)

| λ | n | λ | n |
|-----------|--------|-----------|--------|
| CURVE 1 | | | |
| T = 293. | | | |
| 1.0140 | 1.3776 | 7.2500 | 1.2865 |
| 1.5295 | 1.3747 | 7.5000 | 1.2792 |
| 2.1526 | 1.3708 | 7.7500 | 1.2715 |
| 2.4374 | 1.3688 | 8.0000 | 1.2634 |
| 3.3033 | 1.3639 | 9.2500 | 1.2549 |
| 3.4188 | 1.3594 | 8.5000 | 1.2463 |
| 4.253 | 1.3489 | 8.7500 | 1.2367 |
| 4.866 | 1.3402 | 9.0000 | 1.2269 |
| 5.136 | 1.3345 | | |
| 6.238 | 1.3122 | | |
| CURVE 2 | | | |
| T = 293. | | | |
| 1.0000 | 1.3778 | | |
| 1.2500 | 1.3763 | | |
| 1.5000 | 1.3749 | | |
| 1.7500 | 1.3735 | | |
| 2.0000 | 1.3720 | | |
| 2.2500 | 1.3702 | | |
| 2.5000 | 1.3683 | | |
| 2.7500 | 1.3663 | | |
| 3.0000 | 1.3640 | | |
| 3.2500 | 1.3614 | | |
| 3.5000 | 1.3587 | | |
| 3.7500 | 1.3556 | | |
| 4.0000 | 1.3526 | | |
| 4.2500 | 1.3492 | | |
| 4.5000 | 1.3455 | | |
| 4.7500 | 1.3416 | | |
| 5.0000 | 1.3374 | | |
| 5.2500 | 1.3329 | | |
| 5.5000 | 1.3282 | | |
| 5.7500 | 1.3232 | | |
| 6.0000 | 1.3179 | | |
| 6.2500 | 1.3122 | | |
| 6.5000 | 1.3063 | | |
| 6.7500 | 1.3000 | | |
| 7.0000 | 1.2934 | | |

b. Normal Spectral Emittance (Temperature Dependence)

No experimental data was found for the temperature dependence of the normal spectral emittance of Irtran 1. However, using curves 8, 9, 10, and 11 of Tables 9-2 and 9-3, a set of provisional values for a specimen thickness of 3.8 mm and a wavelength of 3.8 μm were generated. The provisional values are listed in Table 9-6 and shown in Figure 9-4. The uncertainty is assigned a value of not more than 25%.

TABLE 9-6. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (IRTRAN 1) (TEMPERATURE DEPENDENCE)
(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ |
|------------------|------------|
| 3.0MM THICK | |
| $\lambda = 3.00$ | |
| 589. | 0.053 |
| 647. | 0.053 |
| 865. | 0.059 |
| 970. | 0.071 |

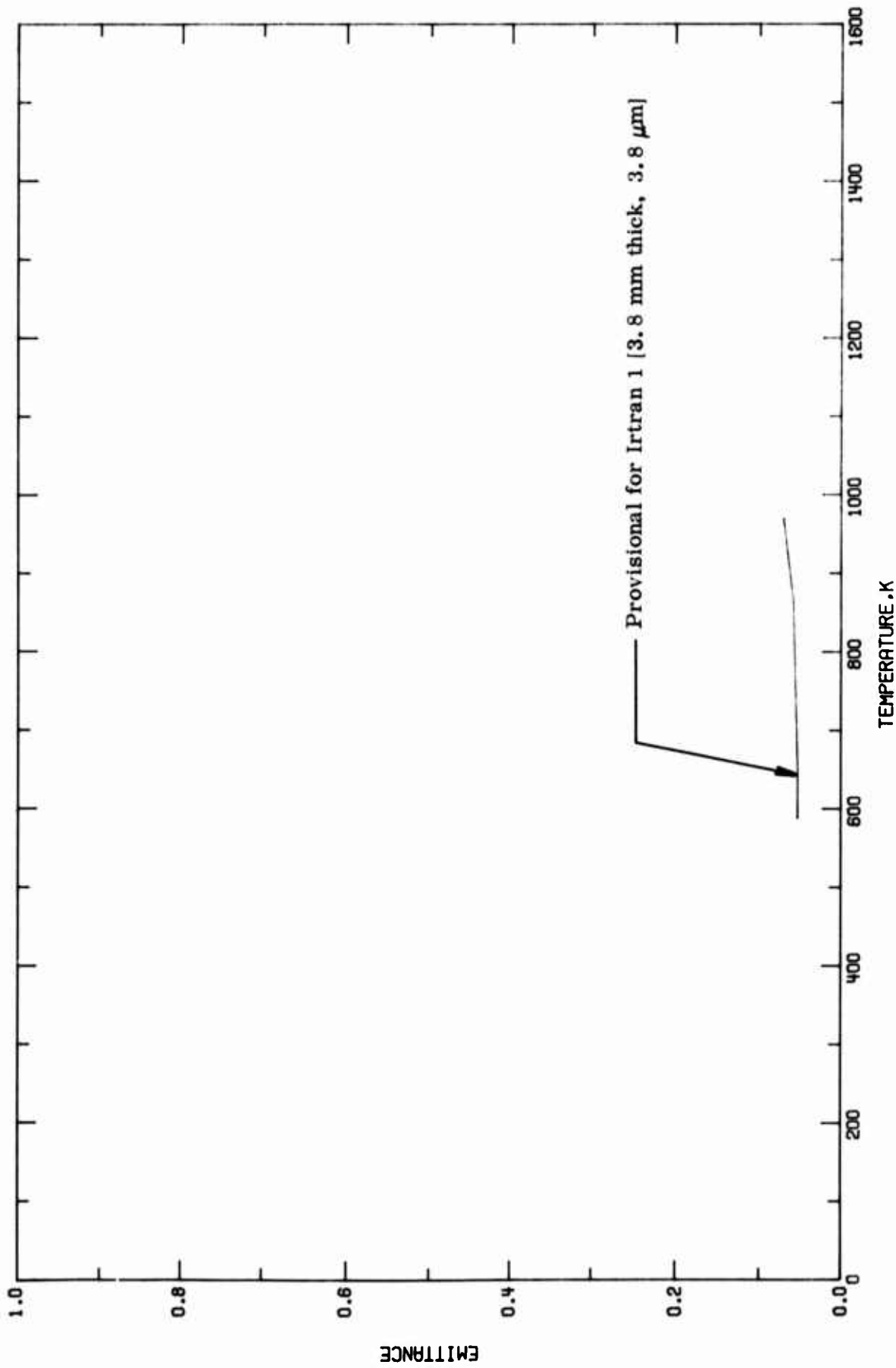


FIGURE 9-4. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF MAGNESIUM FLUORIDE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

Only one set of experimental data was located for the wavelength dependence of the normal spectral reflectance of magnesium fluoride. The data is listed in Table 9-9 and shown in Figures 9-5 and 9-6. Specimen characterization and measurement information for the data are given in Table 9-8.

Calculations were carried out using the Kodak scheme, Eqs. (2.6-13) and (2.6-14), to determine the reflectance at 293 K over a range of thickness from 0.5 mm to 12 mm (curves 2-7). In addition, Hatch[T76525] presented an argument concerning the reflectance from 10 to 15 μm with the conclusion the reflectance is less than 1% (curve 8).

Values for a provisional curve at 293 K for a 2 mm thick specimen are listed in Table 9-7 and shown in Figure 9-5. These values cover a wavelength range of 3 to 6.4 μm to agree with the wavelength range for the provisional curve at 293 K for the wavelength dependence of the normal spectral emittance. The uncertainty is thought to be no more than 25%.

TABLE 9-7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (IRTPAN 1) (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ |
|-----------|--------|
| 2MM THICK | |
| T = 293 | |
| 3.00 | 0.042 |
| 3.03 | 0.043 |
| 3.10 | 0.043 |
| 3.19 | 0.043 |
| 3.27 | 0.043 |
| 3.30 | 0.043 |
| 3.49 | 0.043 |
| 3.80 | 0.042 |
| 3.98 | 0.041 |
| 4.00 | 0.041 |
| 4.46 | 0.040 |
| 4.58 | 0.040 |
| 4.70 | 0.039 |
| 4.88 | 0.039 |
| 4.95 | 0.039 |
| 5.00 | 0.039 |
| 5.01 | 0.039 |
| 5.13 | 0.038 |
| 5.23 | 0.038 |
| 5.32 | 0.038 |
| 5.59 | 0.037 |
| 5.69 | 0.036 |
| 5.79 | 0.036 |
| 5.87 | 0.035 |
| 6.00 | 0.034 |
| 6.16 | 0.033 |
| 6.34 | 0.032 |
| 6.40 | 0.031 |

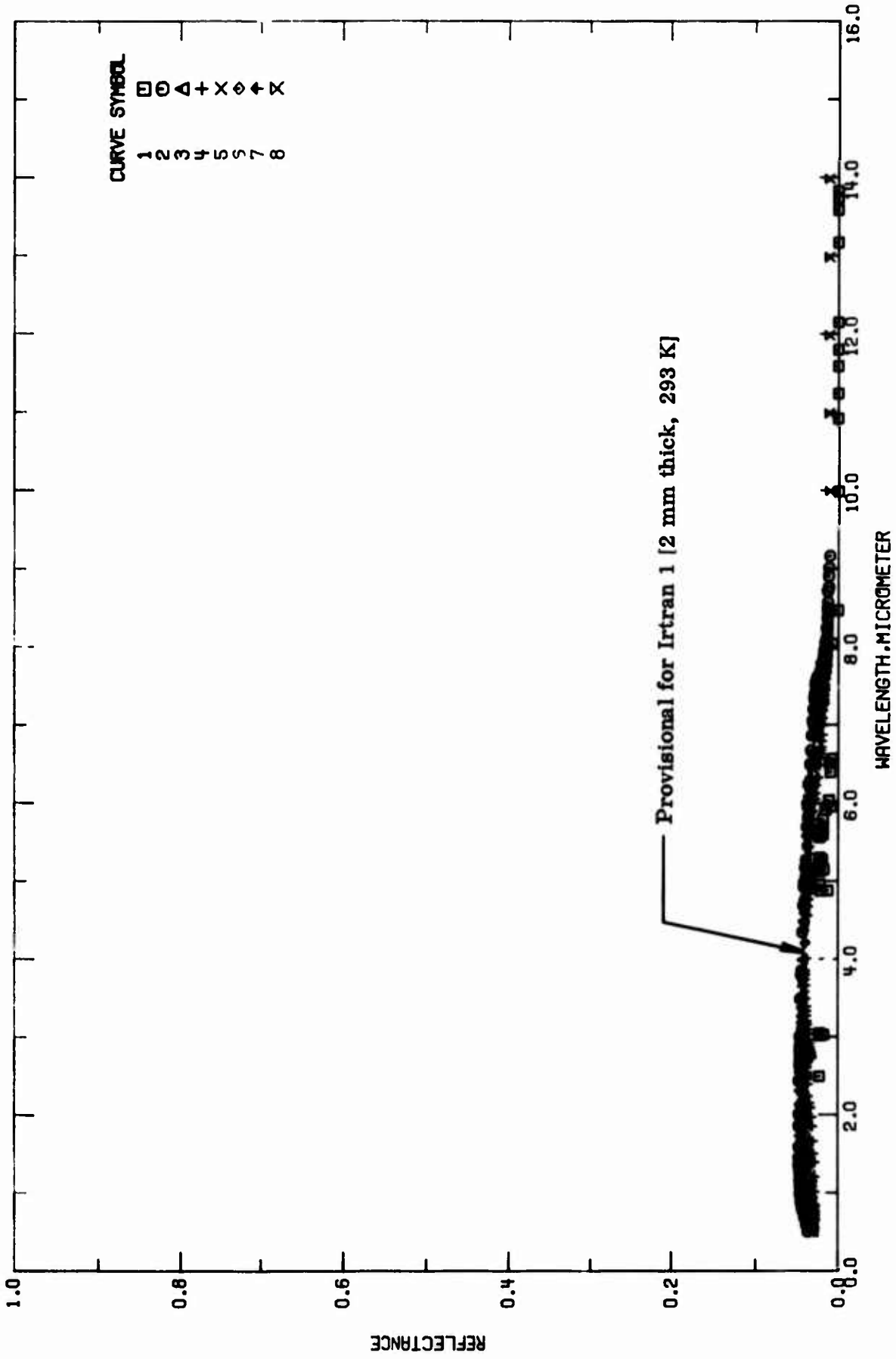


FIGURE 9-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

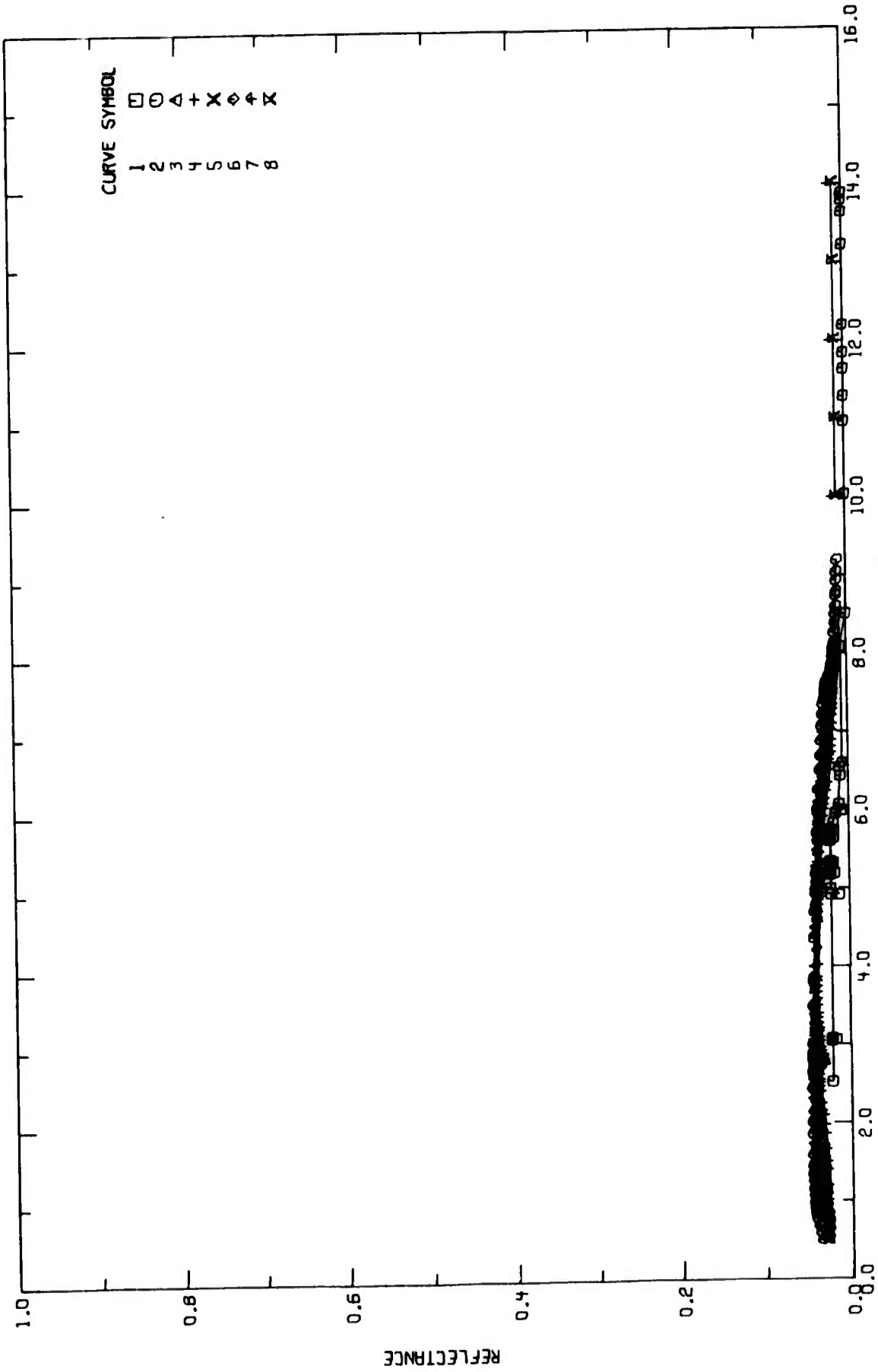


FIGURE 9-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

TABLE 9-S. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 E62501 | Schaefer, J.C. and Hill, E.R. | 1965 | 2.5-35 | 293 | Magnesium Fluoride | Thick crystal; measurement temperature not given explicitly, assumed to be 293 K; $\theta \approx 0^\circ$, $\theta' \approx 0^\circ$. |
| 2 E62500 | | 1971 | 0.5-9.2 | 293 | Irtran 1 | Specimen thickness 0.5 mm; temperature not explicitly given, presumed to be room temperature, 293 K assigned; calculated from transmittance and refractive index; see pp. 16-18 and p. 52. [E62600]. |
| 3 E62500 | | 1971 | 0.5-8.5 | 293 | Irtran 1 | Similar to the above specimen except 1 mm thick. |
| 4 E62500 | | 1971 | 0.5-8.0 | 293 | Irtran 1 | Similar to the above specimen except 2 mm thick. |
| 5 E62500 | | 1971 | 0.5-7.9 | 293 | Irtran 1 | Similar to the above specimen except 3 mm thick. |
| 6 E62600 | | 1971 | 0.65-7.7 | 293 | Irtran 1 | Similar to the above specimen except 5 mm thick. |
| 7 E62500 | | 1971 | 0.84-7.6 | 293 | Irtran 1 | Similar to the above specimen except 12 mm thick. |
| 8 T76525 | Hatch, S.E. | 1962 | 10-15 | 293 | Irtran 1 | Thicknesses of 1 mm or greater; applicable temperature is ambient, 293 K assigned; measurements performed on a Perkin-Elmer Model 221 spectrometer with reflection attachment; reflectance less than 1 percent from 10 to 15 μ ; argument presented on p. 597 of this reference that reflectance not expected to change significantly within the range of 10-15 μ up to 970 K. |

TABLE 9-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 2 | | CURVE 2 (CONT.) | | CURVE 3 | | CURVE 3 (CONT.) | |
|-----------|--------|-----------------|--------|-----------------|--------|-----------|--------|-----------------|--------|-----------|--------|-----------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| T = 293. | | | | | | | | | | | | | |
| 2.50 | 0.022 | 14.83 | 0.032 | 30.58 | 0.021 | 3.49 | 0.044 | 0.50 | 0.030 | 6.50 | 0.032 | | |
| 3.329 | 0.022 | 15.17 | 0.057 | 31.45 | 0.000 | 3.80 | 0.043 | 0.76 | 0.030 | 6.98 | 0.029 | | |
| 3.040 | 0.017 | 15.41 | 0.081 | 32.05 | 0.020 | 3.85 | 0.043 | 0.82 | 0.035 | 7.10 | 0.028 | | |
| 3.054 | 0.022 | 15.60 | 0.121 | 32.57 | 0.402 | 4.35 | 0.042 | 0.89 | 0.037 | 7.20 | 0.027 | | |
| 4.890 | 0.021 | 15.85 | 0.202 | 32.89 | 0.576 | 4.69 | 0.041 | 0.92 | 0.039 | 7.28 | 0.026 | | |
| 4.890 | 0.012 | 15.95 | 0.303 | 33.33 | 0.592 | 4.93 | 0.040 | 1.00 | 0.039 | 7.35 | 0.025 | | |
| 4.558 | 0.022 | 16.16 | 0.380 | 33.56 | 0.652 | 4.99 | 0.040 | 1.10 | 0.040 | 7.43 | 0.025 | | |
| 5.141 | 0.022 | 16.31 | 0.455 | 34.84 | 0.657 | 5.18 | 0.039 | 1.19 | 0.041 | 7.47 | 0.024 | | |
| 5.160 | 0.017 | 16.61 | 0.489 | 35.34 | 0.703 | 5.70 | 0.037 | 1.32 | 0.042 | 7.53 | 0.023 | | |
| 5.173 | 0.022 | 17.01 | 0.532 | 35.34 | 0.900 | 6.00 | 0.036 | 1.42 | 0.043 | 7.56 | 0.022 | | |
| 5.260 | 0.022 | 17.24 | 0.569 | CURVE 2 | | 6.25 | 0.035 | 1.50 | 0.044 | 7.63 | 0.020 | | |
| 5.294 | 0.019 | 18.15 | 0.637 | T = 293. | | 6.50 | 0.033 | 1.50 | 0.044 | 7.70 | 0.018 | | |
| 5.311 | 0.022 | 18.62 | 0.663 | 0.50 | 0.035 | 6.68 | 0.032 | 1.63 | 0.044 | 7.74 | 0.017 | | |
| 5.577 | 0.022 | 18.62 | 0.672 | 0.60 | 0.030 | 6.87 | 0.031 | 1.73 | 0.045 | 7.78 | 0.017 | | |
| 5.609 | 0.015 | 18.90 | 0.679 | 0.65 | 0.029 | 7.06 | 0.030 | 1.84 | 0.045 | 7.81 | 0.016 | | |
| 5.624 | 0.022 | 19.30 | 0.692 | 0.60 | 0.037 | 7.21 | 0.029 | 2.31 | 0.045 | 7.84 | 0.015 | | |
| 5.679 | 0.022 | 19.19 | 0.655 | 0.69 | 0.039 | 7.34 | 0.023 | 2.42 | 0.045 | 7.87 | 0.015 | | |
| 5.706 | 0.018 | 19.65 | 0.709 | 0.77 | 0.041 | 7.50 | 0.027 | 2.55 | 0.045 | 7.90 | 0.015 | | |
| 5.807 | 0.018 | 20.24 | 0.715 | 0.83 | 0.042 | 7.50 | 0.026 | 2.62 | 0.045 | 7.92 | 0.014 | | |
| 5.931 | 0.015 | 20.70 | 0.715 | 0.89 | 0.043 | 7.54 | 0.026 | 2.67 | 0.044 | 7.94 | 0.014 | | |
| 5.970 | 0.008 | 20.73 | 0.694 | 0.94 | 0.043 | 7.59 | 0.025 | 2.70 | 0.043 | 7.98 | 0.014 | | |
| 6.050 | 0.011 | 21.05 | 0.691 | 0.99 | 0.044 | 7.63 | 0.024 | 2.71 | 0.042 | 8.03 | 0.014 | | |
| 6.414 | 0.009 | 21.37 | 0.606 | 1.08 | 0.044 | 7.70 | 0.021 | 2.73 | 0.039 | 8.05 | 0.014 | | |
| 6.523 | 0.010 | 21.88 | 0.553 | 1.16 | 0.045 | 7.79 | 0.019 | 2.73 | 0.041 | 8.11 | 0.014 | | |
| 6.579 | 0.007 | 22.62 | 0.310 | 1.26 | 0.045 | 7.83 | 0.018 | 2.77 | 0.043 | 8.17 | 0.013 | | |
| 6.607 | 0.007 | 23.42 | 0.159 | 1.35 | 0.046 | 7.86 | 0.017 | 2.79 | 0.043 | 8.25 | 0.013 | | |
| 6.658 | 0.007 | 23.64 | 0.361 | 1.45 | 0.046 | 7.89 | 0.016 | 2.86 | 0.044 | 8.35 | 0.013 | | |
| 6.492 | 0.000 | 23.64 | 0.363 | 1.59 | 0.046 | 7.95 | 0.016 | 2.92 | 0.044 | 8.35 | 0.013 | | |
| 10.01 | 0.000 | 24.33 | 0.286 | 1.36 | 0.046 | 8.01 | 0.015 | 3.05 | 0.044 | 8.51 | 0.012 | | |
| 10.94 | 0.000 | 24.45 | 0.258 | 2.01 | 0.046 | 8.06 | 0.015 | 3.49 | 0.043 | | | | |
| 11.26 | 0.000 | 24.61 | 0.251 | 2.44 | 0.046 | 8.12 | 0.014 | 3.80 | 0.043 | | | | |
| 11.61 | 0.000 | 25.19 | 0.200 | 2.83 | 0.045 | 8.25 | 0.014 | 3.99 | 0.043 | | | | |
| 12.17 | 0.000 | 25.77 | 0.157 | 2.65 | 0.045 | 8.38 | 0.013 | 4.49 | 0.041 | | | | |
| 13.19 | 0.000 | 26.53 | 0.140 | 2.71 | 0.044 | 8.49 | 0.013 | 5.07 | 0.040 | | | | |
| 13.61 | 0.000 | 26.88 | 0.120 | 2.72 | 0.041 | 8.58 | 0.012 | 5.27 | 0.039 | | | | |
| 13.76 | 0.000 | 27.93 | 0.105 | 2.72 | 0.044 | 8.72 | 0.012 | 5.68 | 0.039 | | | | |
| 13.85 | 0.000 | 28.57 | 0.076 | 2.75 | 0.044 | 8.77 | 0.011 | 5.93 | 0.037 | | | | |
| 14.31 | 0.006 | 29.41 | 0.061 | 2.81 | 0.045 | 8.91 | 0.011 | 6.09 | 0.036 | | | | |
| 14.84 | 0.019 | 29.41 | 0.048 | 2.88 | 0.045 | 9.02 | 0.011 | 6.26 | 0.035 | | | | |
| | | 30.30 | 0.040 | 3.00 | 0.045 | 9.17 | 0.010 | | 0.034 | | | | |
| CURVE 3 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |
| CURVE 3 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |
| CURVE 3 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |

TABLE 9-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ |
|-----------------|-----------------|-----------------|-----------------|
| CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) |
| 2.69 | 0.036 | 5.44 | 0.033 |
| 2.70 | 0.035 | 5.55 | 0.032 |
| 2.73 | 0.031 | 5.64 | 0.031 |
| 2.74 | 0.030 | 5.71 | 0.031 |
| 2.77 | 0.031 | 5.79 | 0.030 |
| 2.80 | 0.031 | 5.90 | 0.029 |
| 2.83 | 0.032 | 6.00 | 0.028 |
| 2.86 | 0.032 | 6.05 | 0.027 |
| 2.91 | 0.033 | 6.13 | 0.026 |
| 2.95 | 0.034 | 6.23 | 0.025 |
| 3.04 | 0.035 | 6.33 | 0.023 |
| 3.09 | 0.035 | 6.49 | 0.022 |
| 3.16 | 0.036 | 6.58 | 0.021 |
| 3.25 | 0.036 | 6.63 | 0.020 |
| 3.27 | 0.037 | 6.68 | 0.020 |
| 3.33 | 0.037 | 6.72 | 0.019 |
| 3.39 | 0.037 | 6.80 | 0.019 |
| 3.49 | 0.038 | 6.88 | 0.018 |
| 3.59 | 0.038 | 7.00 | 0.018 |
| 3.65 | 0.038 | 7.09 | 0.017 |
| 3.74 | 0.038 | 7.19 | 0.017 |
| 3.83 | 0.038 | 7.28 | 0.016 |
| 3.85 | 0.038 | 7.33 | 0.016 |
| 4.01 | 0.077 | 7.45 | 0.016 |
| 4.56 | 0.030 | 7.59 | 0.015 |
| 4.66 | 0.035 | | |
| 4.77 | 0.035 | | |
| 4.84 | 0.035 | | |
| 4.88 | 0.034 | | |
| 4.92 | 0.034 | | |
| 4.97 | 0.033 | | |
| 5.01 | 0.032 | | |
| 5.03 | 0.033 | | |
| 5.04 | 0.033 | | |
| 5.07 | 0.033 | | |
| 5.11 | 0.034 | | |
| 5.15 | 0.034 | | |
| 5.19 | 0.034 | | |
| 5.23 | 0.034 | | |
| 5.35 | 0.033 | | |
| | | CURVE 3 | |
| | | T = 293. | |
| | | 10. | < 0.01 |
| | | 11. | < 0.01 |
| | | 12. | < 0.01 |
| | | 13. | < 0.01 |
| | | 14. | < 0.01 |
| | | 15. | < 0.01 |

d. Angular Spectral Reflectance (Wavelength Dependence)

One set of experimental data was located for the wavelength dependence of the angular spectral reflectance of Irtran 1. Three sets are for magnesium fluoride. The data are listed in Table 9-11 and shown in Figure 9-7. Specimen characterization and measurement information for the data are given in Table 9-10.

All four sets are for room temperature measurements. The one set for Irtran 1 measured by McCarthy [T30100] is for a polished specimen 2 mm thick with the measurement taken at an angle of incidence, θ , of 30° and an angle of reflection, θ' , of 30° . The data shows a decrease from about 0.04 at $4 \mu\text{m}$ to zero value at $9.5 \mu\text{m}$. Because of the wide range in cut off exemplified by the data for the wavelength dependence of normal spectral reflectance (see the section on the wavelength dependence of the normal spectral transmittance and Figure 9-12), it was decided not to give evaluated data in this angular spectral reflectance section.

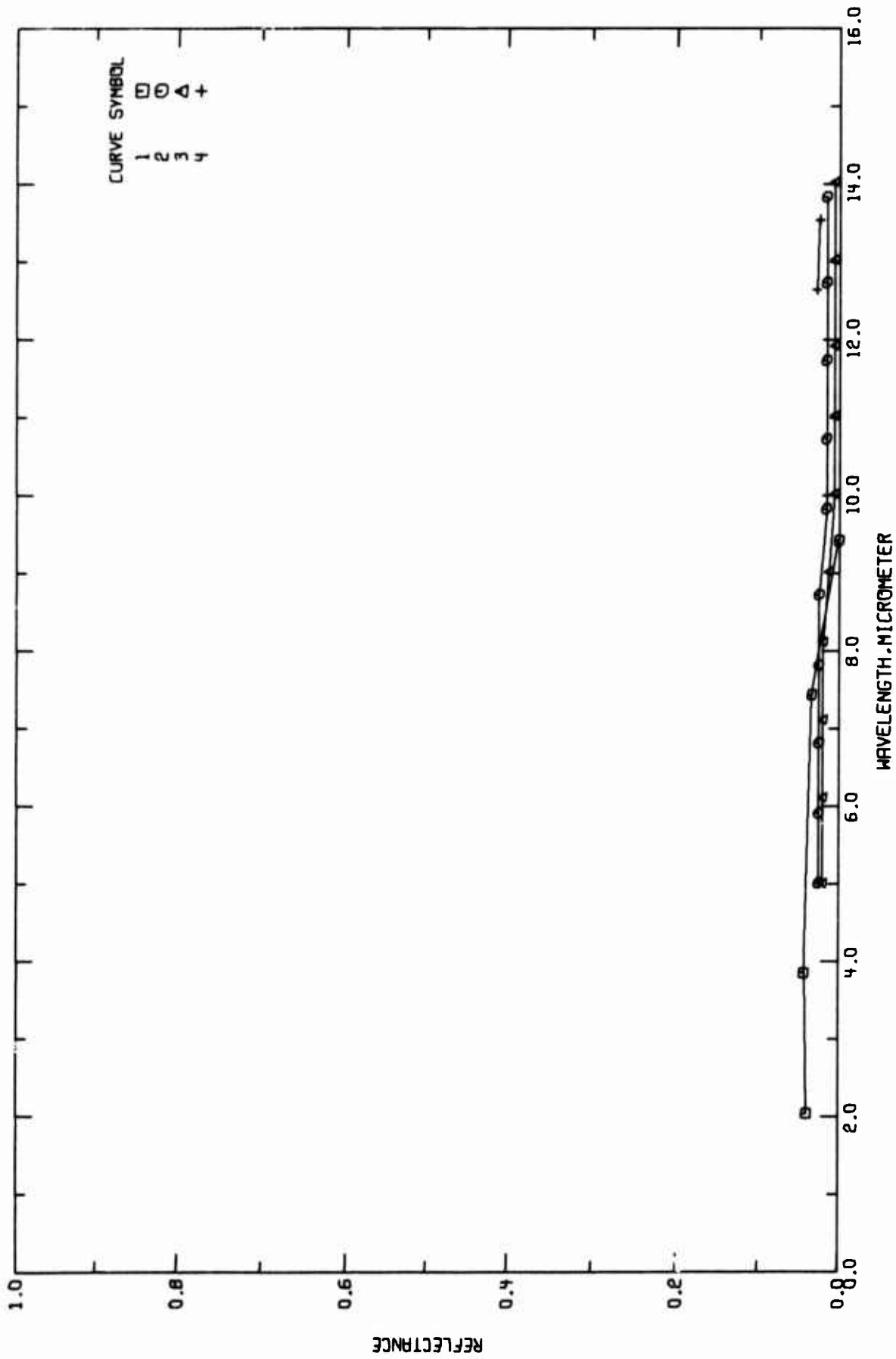


FIGURE 9-7. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

TABLE 9-10. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF MAGNESIUM FLUORIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T30100 | McCarthy, D. E. | 1963 | 2-50 | 293 | Irttran 1 | Specimen 2 mm thick; pressed and sintered; ground and polished to a flatness of seven fringes or better; reference standard was aluminum mirror; smooth values from figure; temperature presumed to be room temperature, 293 K assigned; $\theta = 30^\circ$. |
| 2 T38423 | Barker, A. S., Jr. | 1964 | 5.0-130 | 293 | MgF ₂ | Single crystal; cut and polished; electric vector of infrared beam perpendicular to c-axis; one sample contained 1 Ni and 1 Co and had a pink-orange color; other specimen 0.5 Ni and was optically clear; no feature of spectrum could be associated with Ni and Co doping; angle of incidence was near 15° ; measurement temperature specified as room temperature, 293 K assigned; $\theta \approx 15^\circ$, $\theta' \approx 15^\circ$. |
| 3 T38423 | Barker, A. S., Jr. | 1964 | 5.0-35 | 293 | MgF ₂ | Similar to the above specimen except electric vector is parallel to c-axis. |
| 4 T33043 | Hunt, G. R., Perry, C. H., and Ferguson, J. | 1964 | 13-5000 | 293 | MgF ₂ | Not a single crystal; grown at Bell Telephone Laboratories; smooth values from figure; measurement temperature specified as room temperature, 293 K assigned; $\theta = 15^\circ$, $\theta' = 15^\circ$. |

e. Normal Spectral Absorptance (Wavelength Dependence)

Three sets of experimental data were located for the wavelength dependence of the normal spectral absorptance of Irtran 1. The data are listed in Table 9-14 and shown in Figures 9-8 and 9-9. Specimen characterization and measurement information for the data are given in Table 9-13.

The three sets of data were results of measurements by Stierwalt, et al. [T45698] for a 2 mm thick specimen. The measurement temperatures were 333, 393, and 453 K. The values are between 0.1 and 0.01 within the wavelength range 3 to 6 μm , rise rapidly in the range of 6.5 to 8.5 μm , and are within the range of 0.75 to 0.9 above 10 μm . This data is very similar to the normal spectral emittance data of Stierwalt, et al. [T33450] in Tables 9-2 and 9-3 and Figures 9-1 and 9-2 (curves 17, 18, and 19).

Calculations were carried out to determine the absorptance using transmittance and refractive index data. See the section on the wavelength dependence of the normal spectral emittance for more details. The results of the calculations are curves 4-9 in Table 9-14 and Figures 9-8 and 9-9.

For wavelengths greater than 7 μm , the calculations show the absorptance reaching 0.98 or greater. However, the data of Stierwalt, et al. for the lowest temperature, 333 K, does not reach 0.98. The same type of difficulty manifested itself in the data for the normal spectral emittance.

However, in a lower wavelength region, the calculations for a 2 mm thick specimen (curve 6) and the data for a 2 mm thick specimen at 333 K agree reasonably well. Therefore, between 3 and 6.4 μm , the calculated values are taken as the provisional values for 293 K with an uncertainty of 25%. The provisional values are listed in Table 9-12 and shown in Figure 9-8.

Applying Kirchhoff's law, equating normal spectral absorptance to normal spectral emittance, two more provisional curves are given (see the section on the wavelength dependence of the normal spectral emittance). One applies to a specimen thickness of 3.8 mm, a temperature of 589 K, and a wavelength range of 3 to 6.4 μm ; the other applies to a thickness of 3.8 mm, a temperature of 970 K, and a wavelength range of 3 to 6.0 μm . These values are also listed in Table 9-12 and shown in Figure 9-8. Because of the low value of absorptance, the uncertainty can be as high as 25%.

TABLE 9-12. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (IRTRAN 1) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α |
|-------------|----------|-----------|----------|-----------|----------|
| 2MM THICK | | | | | |
| T = 293 | | | | | |
| 3.00 | 0.069 | 3.0 | 0.154 | 3.0 | 0.177 |
| 3.63 | 0.095 | 3.11 | 0.124 | 3.07 | 0.151 |
| 3.10 | 0.079 | 3.24 | 0.102 | 3.31 | 0.109 |
| 3.19 | 0.074 | 3.42 | 0.076 | 3.56 | 0.083 |
| 3.27 | 0.069 | 3.80 | 0.053 | 3.80 | 0.071 |
| 3.38 | 0.065 | 4.0 | 0.048 | 4.0 | 0.070 |
| 3.49 | 0.060 | 4.14 | 0.045 | 4.42 | 0.066 |
| 3.80 | 0.060 | 4.64 | 0.045 | 4.81 | 0.076 |
| 3.98 | 0.059 | 4.97 | 0.052 | 4.98 | 0.081 |
| 4.00 | 0.060 | 5.0 | 0.054 | 5.6 | 0.084 |
| 4.46 | 0.060 | 5.09 | 0.061 | 5.23 | 0.111 |
| 4.68 | 0.060 | 5.25 | 0.078 | 5.47 | 0.094 |
| 4.70 | 0.057 | 5.46 | 0.061 | 5.65 | 0.111 |
| 4.88 | 0.052 | 5.60 | 0.061 | 5.84 | 0.154 |
| 4.95 | 0.058 | 5.79 | 0.077 | 6.00 | 0.167 |
| 5.00 | 0.057 | 6.0 | 0.107 | | |
| 5.01 | 0.058 | 6.01 | 0.108 | | |
| 5.13 | 0.050 | 6.20 | 0.145 | | |
| 5.23 | 0.046 | 6.35 | 0.185 | | |
| 5.32 | 0.044 | 6.4 | 0.197 | | |
| 5.59 | 0.045 | | | | |
| 5.69 | 0.050 | | | | |
| 5.79 | 0.054 | | | | |
| 5.87 | 0.060 | | | | |
| 6.00 | 0.071 | | | | |
| 6.16 | 0.087 | | | | |
| 6.34 | 0.109 | | | | |
| 6.40 | 0.118 | | | | |
| 3.8MM THICK | | | | | |
| T = 973 | | | | | |
| | | 3.0 | 0.154 | 3.0 | 0.177 |
| | | 3.11 | 0.124 | 3.07 | 0.151 |
| | | 3.24 | 0.102 | 3.31 | 0.109 |
| | | 3.42 | 0.076 | 3.56 | 0.083 |
| | | 3.80 | 0.053 | 3.80 | 0.071 |
| | | 4.0 | 0.048 | 4.0 | 0.070 |
| | | 4.14 | 0.045 | 4.42 | 0.066 |
| | | 4.64 | 0.045 | 4.81 | 0.076 |
| | | 4.97 | 0.052 | 4.98 | 0.081 |
| | | 5.0 | 0.054 | 5.6 | 0.084 |
| | | 5.09 | 0.061 | 5.23 | 0.111 |
| | | 5.25 | 0.078 | 5.47 | 0.094 |
| | | 5.46 | 0.061 | 5.65 | 0.111 |
| | | 5.60 | 0.061 | 5.84 | 0.154 |
| | | 5.79 | 0.077 | 6.00 | 0.167 |
| | | 6.0 | 0.107 | | |
| | | 6.01 | 0.108 | | |
| | | 6.20 | 0.145 | | |
| | | 6.35 | 0.185 | | |
| | | 6.4 | 0.197 | | |

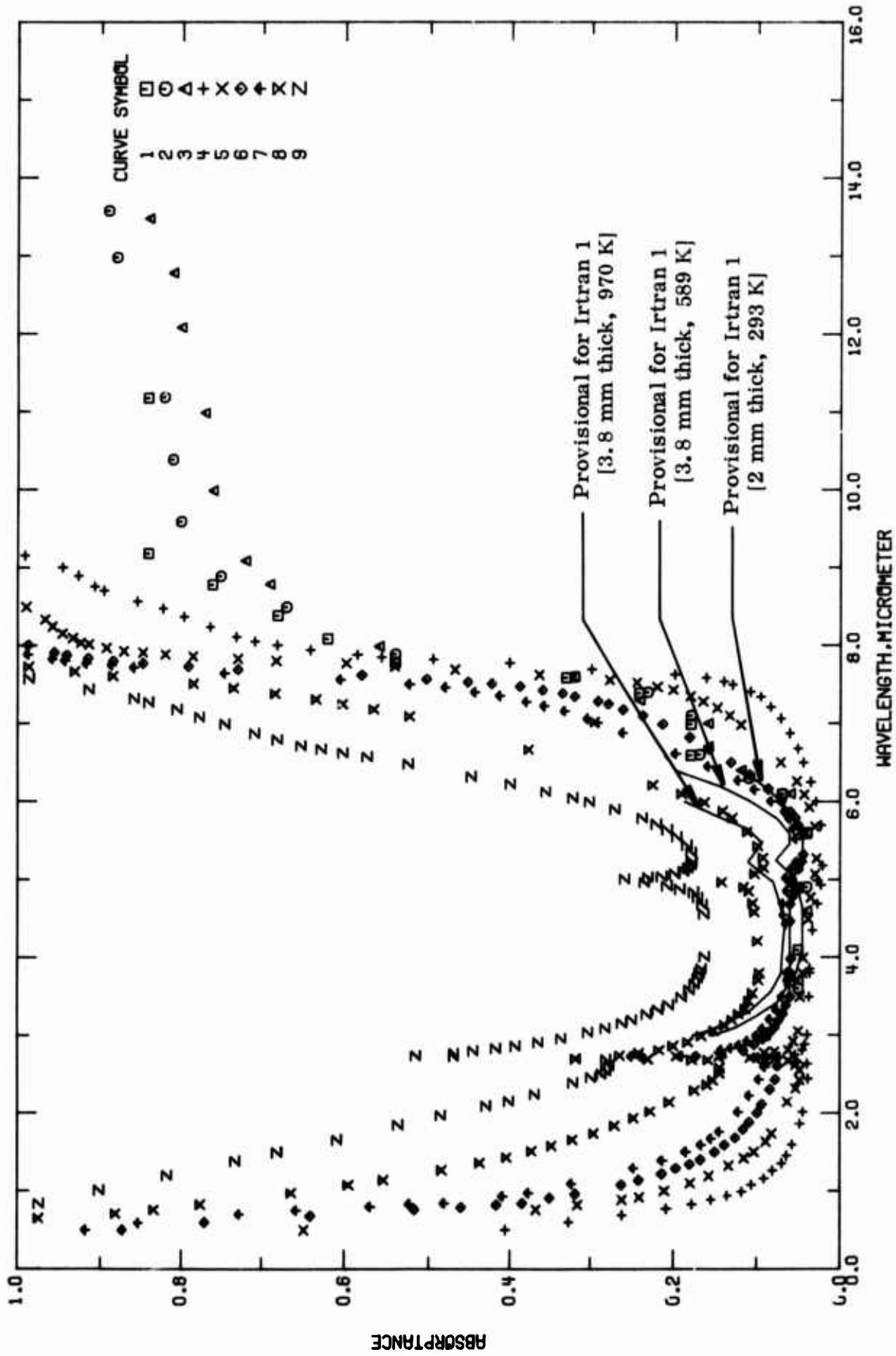


FIGURE 9-8. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

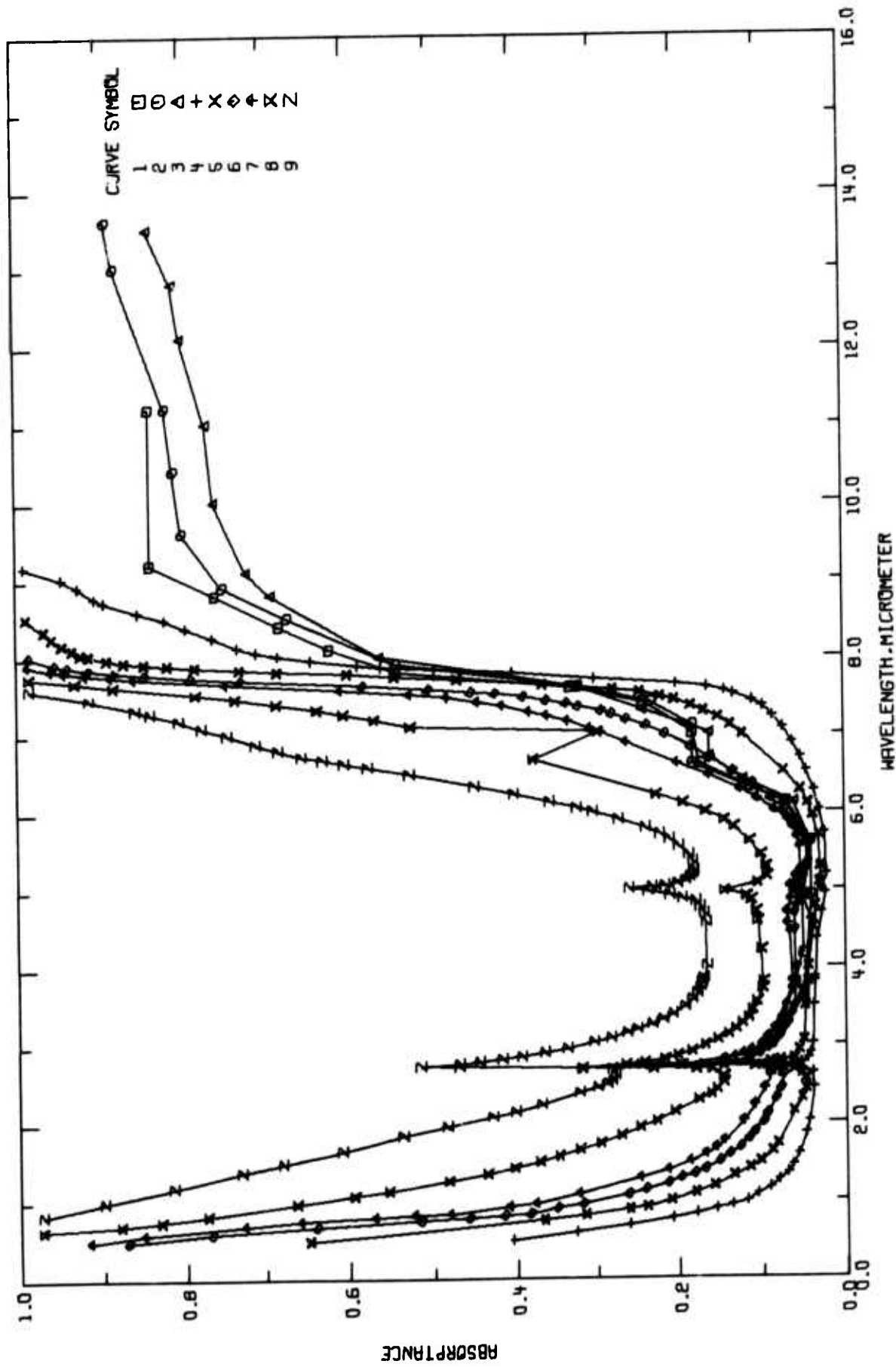


FIGURE 9-9. EXPERIMENTAL NORMAL SPECTRAL ABSORBANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

TABLE 9-13. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T45698 | Sterwalt, D. L., Bernstein, J. B., and Kirk, D. D. | 1963 | 3.0-11 | 333 | Irtran 1 | Specimen 2 mm thick; hot pressed; measured in vacuum; smooth values from figure; $\theta = 0^\circ$. |
| 2 T45698 | Sterwalt, D. L., et al. | 1963 | 3-15 | 393 | Irtran 1 | Similar to the above specimen. |
| 3 T45698 | Sterwalt, D. L., et al. | 1963 | 3-15 | 453 | Irtran 1 | Similar to the above specimen. |
| 4 E62600 | | 1971 | 0.5-9.2 | 293 | Irtran 1 | Specimen thickness 0.5 mm; temperature not explicitly given, presumed to be room temperature, 293 K assigned; calculated from transmittance and refractive index, see pp. 16-15 and p. 52, [E62600]. |
| 5 E62600 | | 1971 | 0.5-8.5 | 293 | Irtran 1 | Similar to the above specimen except 1 mm thick. |
| 6 E62600 | | 1971 | 0.5-8.0 | 293 | Irtran 1 | Similar to the above specimen except 2 mm thick. |
| 7 E62600 | | 1971 | 0.5-7.9 | 293 | Irtran 1 | Similar to the above specimen except 3 mm thick. |
| 8 E62600 | | 1971 | 0.65-7.7 | 293 | Irtran 1 | Similar to the above specimen except 6 mm thick. |
| 9 E62600 | | 1971 | 0.84-7.6 | 292 | Irtran 1 | Similar to the above specimen except 12 mm thick. |

TABLE 9-14. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α | λ | α |
|---------------------|----------|-----------|----------|-----------|----------|---------------------|----------|-----------|----------|---------------------|----------|-----------|----------|
| CURVE 1 T = 333. | | | | | | | | | | | | | |
| 3.00 | 0.09 | 3.00 | 0.09 | 2.01 | 0.044 | 8.06 | 0.708 | 2.81 | 0.062 | 8.35 | 0.966 | 0.50 | 0.672 |
| 3.70 | 0.36 | 3.70 | 0.05 | 2.44 | 0.033 | 8.12 | 0.731 | 2.92 | 0.056 | 8.51 | 0.988 | 0.60 | 0.769 |
| 4.10 | 0.05 | 4.60 | 0.04 | 2.63 | 0.039 | 8.25 | 0.763 | 3.05 | 0.050 | CURVE 6 T = 293. | | | |
| 4.90 | 0.05 | 4.90 | 0.05 | 2.65 | 0.051 | 8.33 | 0.796 | 3.49 | 0.046 | 0.50 | 0.672 | 0.60 | 0.769 |
| 5.50 | 0.07 | 5.50 | 0.04 | 2.71 | 0.076 | 8.49 | 0.822 | 3.80 | 0.045 | 0.68 | 0.640 | 0.68 | 0.640 |
| 5.10 | 0.07 | 6.10 | 0.06 | 2.72 | 0.142 | 8.56 | 0.854 | 3.99 | 0.044 | 0.76 | 0.516 | 0.76 | 0.516 |
| 6.60 | 0.18 | 6.10 | 0.12 | 2.72 | 0.073 | 8.72 | 0.895 | 4.49 | 0.038 | 0.79 | 0.459 | 0.82 | 0.416 |
| 7.00 | 0.18 | 6.70 | 0.16 | 2.75 | 0.054 | 8.77 | 0.906 | 4.77 | 0.035 | 0.84 | 0.384 | 0.84 | 0.384 |
| 7.40 | 0.18 | 6.70 | 0.16 | 2.81 | 0.045 | 8.91 | 0.926 | 5.07 | 0.030 | 0.91 | 0.350 | 0.91 | 0.350 |
| 7.60 | 0.33 | 7.30 | 0.16 | 3.00 | 0.042 | 9.02 | 0.945 | 5.27 | 0.028 | 0.96 | 0.313 | 1.08 | 0.251 |
| 7.60 | 0.33 | 7.30 | 0.24 | 3.00 | 0.039 | 9.17 | 0.990 | 5.63 | 0.030 | 1.14 | 0.240 | 1.22 | 0.213 |
| 7.80 | 0.54 | 7.60 | 0.24 | 3.49 | 0.037 | CURVE 5 T = 293. | | 6.98 | 0.120 | 1.29 | 0.197 | 1.34 | 0.181 |
| 8.10 | 0.62 | 8.00 | 0.56 | 3.80 | 0.036 | 0.50 | 0.648 | 6.98 | 0.134 | 1.40 | 0.158 | 1.40 | 0.158 |
| 8.40 | 0.68 | 8.30 | 0.69 | 3.80 | 0.036 | 0.76 | 0.367 | 7.10 | 0.149 | 1.50 | 0.151 | 1.50 | 0.151 |
| 8.80 | 0.76 | 8.30 | 0.69 | 3.35 | 0.036 | 0.82 | 0.315 | 7.20 | 0.149 | 1.59 | 0.139 | 1.59 | 0.139 |
| 9.20 | 0.84 | 9.10 | 0.72 | 4.35 | 0.033 | 0.89 | 0.260 | 7.28 | 0.166 | 1.68 | 0.126 | 1.68 | 0.126 |
| 11.2 | 0.84 | 11.0 | 0.77 | 4.69 | 0.027 | 0.92 | 0.239 | 7.35 | 0.181 | 1.79 | 0.116 | 1.79 | 0.116 |
| CURVE 2 T = 393. | | | | | | | | | | | | | |
| 3.00 | 0.09 | 3.00 | 0.07 | 6.00 | 0.029 | 1.00 | 0.210 | 7.43 | 0.201 | 1.89 | 0.109 | 1.89 | 0.109 |
| 3.60 | 0.05 | 3.60 | 0.04 | 6.25 | 0.035 | 1.10 | 0.160 | 7.47 | 0.219 | 2.00 | 0.099 | 2.00 | 0.099 |
| 4.90 | 0.04 | 4.90 | 0.04 | 6.50 | 0.044 | 1.19 | 0.153 | 7.53 | 0.243 | 2.11 | 0.094 | 2.11 | 0.094 |
| 5.60 | 0.04 | 5.60 | 0.04 | 6.68 | 0.051 | 1.32 | 0.134 | 7.56 | 0.276 | 2.30 | 0.084 | 2.30 | 0.084 |
| 6.10 | 0.07 | 6.10 | 0.07 | 6.87 | 0.061 | 1.42 | 0.115 | 7.63 | 0.364 | 2.43 | 0.073 | 2.43 | 0.073 |
| 6.30 | 0.11 | 6.30 | 0.11 | 7.06 | 0.072 | 1.50 | 0.103 | 7.70 | 0.468 | 2.60 | 0.075 | 2.60 | 0.075 |
| 6.60 | 0.17 | 6.60 | 0.17 | 7.21 | 0.084 | 1.63 | 0.089 | 7.74 | 0.541 | 2.71 | 0.089 | 2.71 | 0.089 |
| 7.10 | 0.15 | 7.10 | 0.15 | 7.34 | 0.096 | 1.73 | 0.082 | 7.76 | 0.598 | 2.73 | 0.237 | 2.73 | 0.237 |
| 7.40 | 0.23 | 7.40 | 0.23 | 7.41 | 0.108 | 1.73 | 0.082 | 7.81 | 0.682 | 2.76 | 0.174 | 2.76 | 0.174 |
| 7.60 | 0.32 | 7.60 | 0.32 | 7.50 | 0.130 | 2.31 | 0.053 | 7.84 | 0.729 | 2.80 | 0.143 | 2.80 | 0.143 |
| 7.60 | 0.54 | 7.60 | 0.54 | 7.54 | 0.141 | 2.42 | 0.048 | 8.05 | 0.923 | 2.85 | 0.116 | 2.85 | 0.116 |
| 8.50 | 0.67 | 8.50 | 0.67 | 7.59 | 0.162 | 2.55 | 0.048 | 8.05 | 0.923 | 2.95 | 0.103 | 2.95 | 0.103 |
| 8.90 | 0.75 | 8.90 | 0.75 | 7.63 | 0.199 | 2.62 | 0.048 | 8.11 | 0.933 | 3.03 | 0.085 | 3.03 | 0.085 |
| 9.50 | 0.80 | 9.50 | 0.80 | 7.70 | 0.299 | 2.67 | 0.062 | 8.17 | 0.945 | 3.03 | 0.085 | 3.03 | 0.085 |
| 10.4 | 0.81 | 10.4 | 0.81 | 7.73 | 0.401 | 2.70 | 0.062 | 8.17 | 0.945 | 3.10 | 0.079 | 3.10 | 0.079 |
| 11.2 | 0.82 | 11.2 | 0.82 | 7.83 | 0.495 | 2.71 | 0.108 | 7.98 | 0.892 | | | | |
| 13.0 | 0.98 | 13.0 | 0.98 | 7.86 | 0.557 | 2.73 | 0.197 | 8.03 | 0.913 | | | | |
| 13.6 | 0.89 | 13.6 | 0.89 | 7.69 | 0.585 | 2.73 | 0.146 | 8.05 | 0.923 | | | | |
| 14.8 | 0.85 | 14.8 | 0.85 | 7.95 | 0.641 | 2.77 | 0.091 | 8.17 | 0.945 | | | | |
| | | | | 8.01 | 0.681 | 2.79 | 0.079 | 8.26 | 0.957 | | | | |

TABLE 9-14. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| CURVE 5 (CONT.) | | CURVE 6 (CONT.) | | CURVE 7 (CONT.) | | CURVE 8 | | CURVE 8 (CONT.) | | CURVE 9 (CONT.) | |
|-----------------|----------|---------------------|----------|-----------------|----------|---------------------|----------|---------------------|----------|-----------------|----------|
| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α |
| 3.19 | 0.074 | 7.78 | 0.847 | 3.08 | 0.093 | CURVE 8 T = 293. | | 3.54 | 0.105 | 1.66 | 0.608 |
| 3.27 | 0.069 | 7.81 | 0.884 | 3.20 | 0.084 | 0.65 | 0.973 | 3.71 | 0.098 | 1.95 | 0.536 |
| 3.36 | 0.065 | 7.85 | 0.914 | 3.32 | 0.076 | 0.71 | 0.880 | 3.80 | 0.097 | 1.97 | 0.485 |
| 3.49 | 0.060 | 7.89 | 0.944 | 3.49 | 0.070 | 0.76 | 0.832 | 4.21 | 0.099 | 2.09 | 0.429 |
| 3.60 | 0.059 | 7.92 | 0.955 | 3.70 | 0.063 | 0.83 | 0.774 | 4.58 | 0.103 | 2.15 | 0.401 |
| 3.96 | 0.060 | 8.02 | 0.986 | 3.80 | 0.063 | 0.98 | 0.663 | 4.70 | 0.105 | 2.24 | 0.369 |
| 4.46 | 0.060 | | | 4.43 | 0.065 | 1.08 | 0.594 | 4.85 | 0.110 | 2.39 | 0.321 |
| 4.68 | 0.057 | CURVE 7 T = 293. | | 4.54 | 0.068 | 1.14 | 0.553 | 4.90 | 0.116 | 2.46 | 0.299 |
| 4.88 | 0.052 | | | 4.85 | 0.064 | 1.27 | 0.483 | 4.97 | 0.143 | 2.50 | 0.286 |
| 4.95 | 0.058 | | | 5.02 | 0.065 | 1.36 | 0.436 | 5.37 | 0.103 | 2.54 | 0.280 |
| 5.11 | 0.058 | | | 5.14 | 0.058 | 1.43 | 0.403 | 5.15 | 0.092 | 2.61 | 0.276 |
| 5.13 | 0.050 | | | 5.22 | 0.052 | 1.51 | 0.372 | 5.28 | 0.093 | 2.69 | 0.280 |
| 5.23 | 0.046 | | | 5.32 | 0.051 | 1.58 | 0.347 | 5.43 | 0.099 | 2.70 | 0.318 |
| 5.32 | 0.044 | | | 5.52 | 0.056 | 1.66 | 0.321 | 5.61 | 0.112 | 2.73 | 0.459 |
| 5.59 | 0.045 | | | 5.65 | 0.056 | 1.74 | 0.295 | 5.79 | 0.130 | 2.74 | 0.515 |
| 5.69 | 0.050 | | | 5.78 | 0.061 | 1.84 | 0.269 | 5.88 | 0.142 | 2.77 | 0.469 |
| 5.79 | 0.054 | | | 5.87 | 0.067 | 1.94 | 0.246 | 5.99 | 0.164 | 2.80 | 0.445 |
| 5.87 | 0.060 | | | 6.00 | 0.083 | 2.02 | 0.226 | 6.10 | 0.191 | 2.83 | 0.417 |
| 6.00 | 0.071 | | | 6.15 | 0.103 | 2.14 | 0.204 | 6.21 | 0.224 | 2.86 | 0.393 |
| 6.16 | 0.067 | | | 6.27 | 0.123 | 2.29 | 0.175 | 6.57 | 0.377 | 2.91 | 0.365 |
| 6.34 | 0.109 | | | 6.45 | 0.160 | 2.36 | 0.160 | 7.02 | 0.295 | 2.95 | 0.336 |
| 6.50 | 0.132 | | | 6.61 | 0.198 | 2.42 | 0.153 | 7.10 | 0.525 | 3.04 | 0.303 |
| 6.67 | 0.159 | | | 6.88 | 0.260 | 2.51 | 0.145 | 7.19 | 0.566 | 3.09 | 0.281 |
| 6.82 | 0.182 | | | 7.01 | 0.291 | 2.58 | 0.159 | 7.26 | 0.602 | 3.16 | 0.261 |
| 6.99 | 0.213 | | | 7.06 | 0.304 | 2.68 | 0.178 | 7.32 | 0.634 | 3.20 | 0.249 |
| 7.10 | 0.236 | | | 7.16 | 0.332 | 2.69 | 0.178 | 7.39 | 0.683 | 3.27 | 0.231 |
| 7.25 | 0.260 | | | 7.23 | 0.358 | 2.69 | 0.229 | 7.46 | 0.734 | 3.33 | 0.218 |
| 7.29 | 0.291 | | | 7.28 | 0.380 | 2.70 | 0.316 | 7.52 | 0.784 | 3.39 | 0.206 |
| 7.35 | 0.320 | | | 7.36 | 0.413 | 2.74 | 0.263 | 7.62 | 0.994 | 3.43 | 0.191 |
| 7.39 | 0.335 | | | 7.41 | 0.443 | 2.77 | 0.240 | 7.68 | 0.935 | 3.58 | 0.182 |
| 7.43 | 0.360 | | | 7.47 | 0.460 | 2.81 | 0.216 | 7.74 | 0.985 | 3.66 | 0.176 |
| 7.48 | 0.388 | | | 7.51 | 0.523 | 2.86 | 0.200 | CURVE 9 T = 293. | | 3.74 | 0.172 |
| 7.52 | 0.423 | | | 7.57 | 0.605 | 2.91 | 0.183 | 0.64 | 0.973 | 3.80 | 0.170 |
| 7.54 | 0.452 | | | 7.65 | 0.745 | 2.99 | 0.167 | 1.01 | 0.900 | 3.85 | 0.169 |
| 7.56 | 0.503 | | | 7.73 | 0.858 | 3.06 | 0.152 | 1.20 | 0.816 | 4.01 | 0.164 |
| 7.63 | 0.580 | | | 7.76 | 0.886 | 3.13 | 0.139 | 1.39 | 0.731 | 4.50 | 0.165 |
| 7.70 | 0.729 | | | 7.78 | 0.942 | 3.20 | 0.130 | 1.50 | 0.680 | 4.68 | 0.167 |
| 7.74 | 0.791 | | | 7.82 | 0.942 | 3.27 | 0.122 | 1.64 | 0.644 | 4.77 | 0.167 |
| | | | | 7.84 | 0.957 | 3.34 | 0.114 | 1.84 | 0.614 | 4.84 | 0.177 |
| | | | | 7.90 | 0.986 | 3.44 | 0.110 | 1.99 | 0.611 | 4.88 | 0.193 |

TABLE 9-14. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|-----------------|----------|
| CURVE 9 (CONT.) | |
| 4.92 | 0.216 |
| 4.97 | 0.234 |
| 5.01 | 0.258 |
| 5.03 | 0.230 |
| 5.04 | 0.214 |
| 5.07 | 0.199 |
| 5.11 | 0.189 |
| 5.15 | 0.164 |
| 5.19 | 0.190 |
| 5.23 | 0.179 |
| 5.35 | 0.180 |
| 5.44 | 0.185 |
| 5.55 | 0.197 |
| 5.64 | 0.209 |
| 5.71 | 0.225 |
| 5.79 | 0.237 |
| 5.93 | 0.273 |
| 6.00 | 0.302 |
| 6.35 | 0.322 |
| 6.13 | 0.356 |
| 6.23 | 0.400 |
| 6.33 | 0.448 |
| 6.49 | 0.525 |
| 6.56 | 0.577 |
| 6.63 | 0.602 |
| 6.68 | 0.628 |
| 6.72 | 0.653 |
| 6.80 | 0.681 |
| 6.88 | 0.739 |
| 7.00 | 0.745 |
| 7.09 | 0.777 |
| 7.19 | 0.805 |
| 7.28 | 0.845 |
| 7.33 | 0.858 |
| 7.45 | 0.913 |
| 7.59 | 0.985 |

f. Normal Spectral Absorptance (Temperature Dependence)

No experimental data was found for the temperature dependence of the normal spectral absorptance of Irtran 1. However, using curves 8, 9, 10, and 11 of Tables 9-2 and 9-3 together with Kirchhoff's law, Eq. (2.3-7), a set of provisional values for a specimen thickness of 3.8 mm and at a wavelength of 3.8 μm was generated. The provisional values are listed in Table 9-15 and shown in Figure 9-10. The uncertainty is assigned a value of not more than 25%.

TABLE 3-15. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (IRTFAN 1) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α |
|------------------|----------|
| 3.0MM THICK | |
| $\lambda = 3.80$ | |
| 589. | 0.053 |
| 647. | 0.053 |
| 865. | 0.059 |
| 970. | 0.071 |

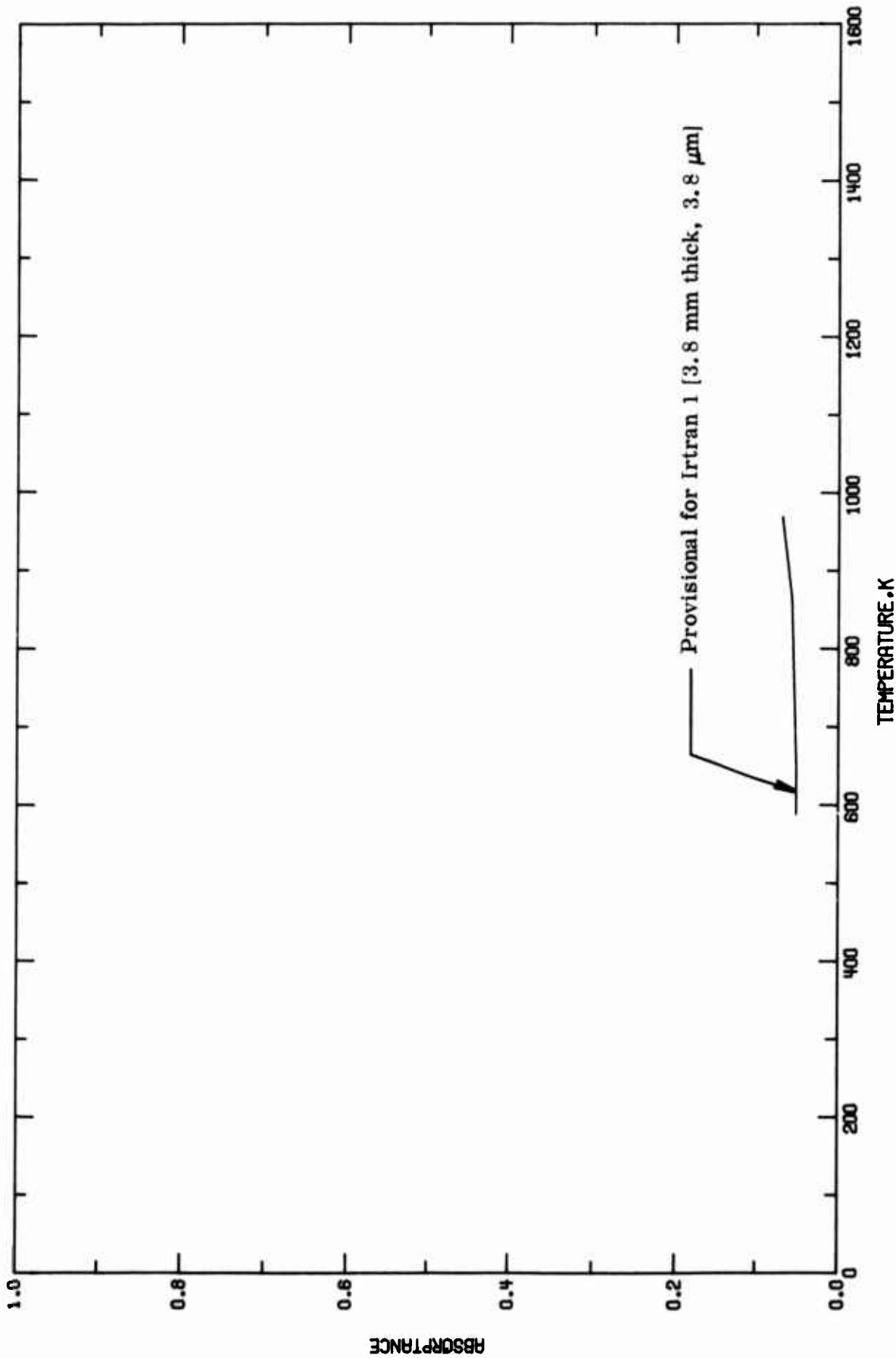


FIGURE 9-10. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF MAGNESIUM FLUORIDE (TEMPERATURE DEPENDENCE).

g. Normal Spectral Transmittance (Wavelength Dependence)

A total of 30 sets of experimental data were found for the wavelength dependence of the normal spectral transmittance of magnesium fluoride. The data are listed in Table 9-18 and shown in Figures 9-11 and 9-12. Specimen characterization and measurement information for the data are given in Table 9-17.

The data reported by Linsteadt [T38121] (curves 8 and 9) was supposedly for a 1.02 mm thick specimen of Irtran 1. However, the shape is so different from curves 15, 21, and 26, all of which apply to an approximately 1 mm thick specimen at room temperature, that the conclusion is reached that the material is not Irtran 1 contrary to what was reported for curves 8 and 9.

A look at curves 15 and 21 shows there is considerable difference in the high wavelength cut-off region. The data of curve 15 applies to a specimen thickness of 1.02 mm at a temperature of 300 K; the data in curve 21 applies to a specimen thickness of 1 mm at 293 K. Above 8 μm , curve 15 is considerably above curve 21. In addition, curve 15 reaches zero transmittance at 9.93 μm while for curve 21 it is 8.51 μm .

A comparison between curve 22, a specimen thickness of 2 mm, a measurement temperature of 293 K, and curve 1, a specimen thickness of 2 mm and a measurement temperature of 293 K shows differences. For most of the wavelength region from 7 to 10 μm , curve 1 is considerably above curve 22. For example, at 8 μm curve 22 is near zero while curve 1 is 0.432. The absorption band in the range 2.7-2.8 μm also shows differences between the two curves. Curve 1 at 2.80 μm is 0.607 while curve 22 is 0.842.

Because of these differences, a provisional curve at 293 K for a specimen thickness of 2 mm is only given for the wavelength range 3 to 7 μm . The uncertainty at 7 μm is 12% and, therefore, this uncertainty is assigned to this curve. These provisional values are based on curve 22 and the values are listed in Table 9-16 and shown in Figure 9-11.

Transmittance data was given by Ballard, et al. [T17017] for a 1.75 mm thick specimen at several high temperatures: curve 17 at 673 K, curve 18 at 873 K, and curve 19 at 1073 K. Curve 16 is at 299 K for the same thickness. The curves are identical up to 5.4 μm but above that wavelength the effect of increasing temperature is to decrease the transmittance and also to decrease the wavelength at which the transmittance reaches zero. Since the shape of curve 16, for 299 K and 1.75 mm thick, is different enough from curve 22 for 293 K and 2 mm thick, it is not thought justified to give evaluated data over a range of wavelengths for the highest temperature, i.e., 1073 K.

However, one fact that will be used in the next section is pertinent to make here. From curves 16 through 19, it is noted the transmittance has the same value for 299, 673, 873, and 1033 K at a wavelength of 3.8 μm .

TABLE 9-16. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (IRTRAN 1) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T |
|-----------|-------|
| 2MM THICK | |
| T = 293 | |
| 3.00 | 0.869 |
| 3.03 | 0.972 |
| 3.10 | 0.975 |
| 3.19 | 0.993 |
| 3.27 | 0.888 |
| 3.38 | 0.892 |
| 3.49 | 0.897 |
| 3.80 | 0.898 |
| 3.98 | 0.899 |
| 4.00 | 0.899 |
| 4.46 | 0.900 |
| 4.68 | 0.900 |
| 4.78 | 0.904 |
| 4.88 | 0.909 |
| 4.95 | 0.903 |
| 5.00 | 0.904 |
| 5.01 | 0.933 |
| 5.13 | 0.912 |
| 5.23 | 0.916 |
| 5.32 | 0.918 |
| 5.59 | 0.918 |
| 5.69 | 0.914 |
| 5.79 | 0.910 |
| 5.87 | 0.905 |
| 6.00 | 0.895 |
| 6.16 | 0.880 |
| 6.34 | 0.859 |
| 6.40 | 0.851 |
| 6.50 | 0.838 |
| 6.67 | 0.812 |
| 6.82 | 0.790 |
| 6.99 | 0.761 |
| 7.00 | 0.756 |

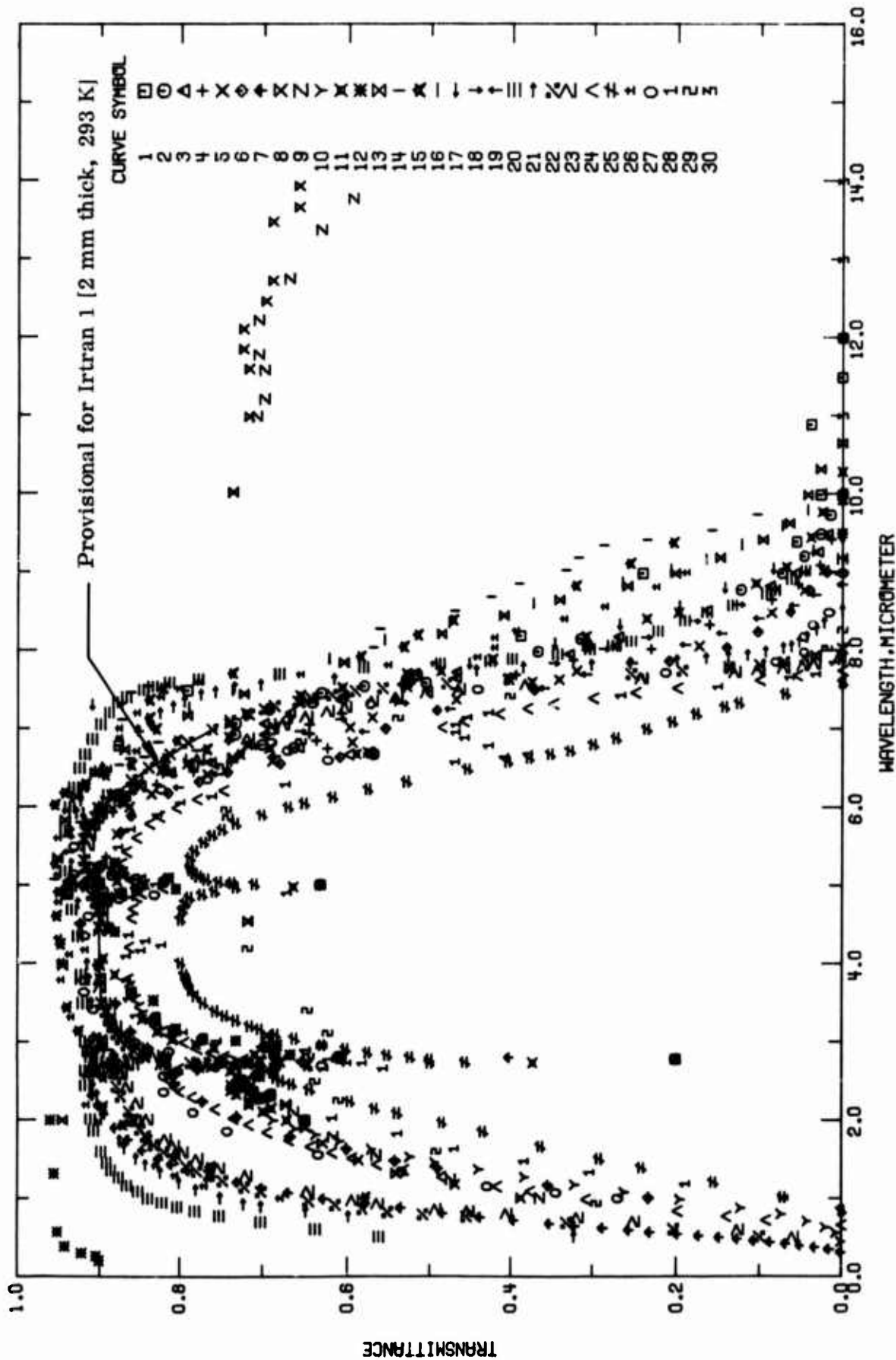


FIGURE 9-11. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

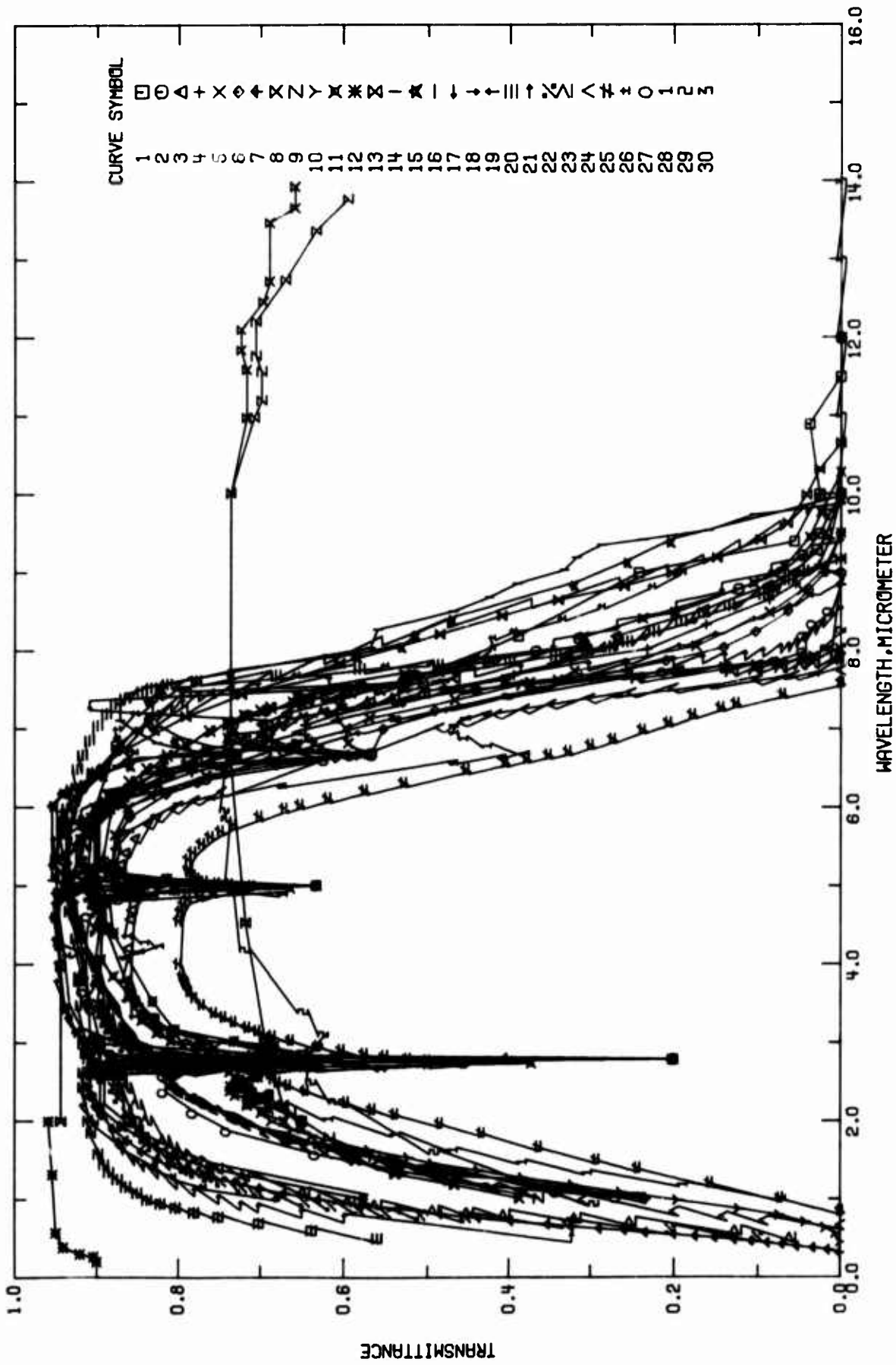


FIGURE 9-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE).

TABLE 9-17. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|--------------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T30100 | McCarthy, D.E. | 1963 | 2-5 ^o | 293 | Irtran 1 | Specimen 2 mm thick; pressed and sintered; ground and polished to a flatness of seven fringes or better; reference standard was aluminum mirror; smooth values from figure; temperature presumed to be room temperature, 293 K assigned; Beckman IR-5A used in 2-16 μ range and Beckman IR-7 with Cal interchange used in 12.5-50 μ range; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 2 T38674 T20810 | Gillespie, D.T., Olsen, A.L., and Nichols, L.W. | 1965 | 2-12 | 298 | Irtran 1 | Specimen 3.150 cm in diameter and 2.80 mm thick; hot-pressed; optically polished flat to within 5 green mercury fringes and a parallelism tolerance of $\pm 2.5 \mu$; smooth values from figure; Perkin-Elmer Model 21 spectrophotometer with sodium chloride optics used; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 3 T38674 T20810 | Gillespie, D.T., et al. | 1965 | 2-12 | 375 | Irtran 1 | The above specimen. |
| 4 T38674 T20810 | Gillespie, D.T., et al. | 1965 | 2-12 | 473 | Irtran 1 | The above specimen. |
| 5 T38674 T20810 | Gillespie, D.T., et al. | 1965 | 2-12 | 573 | Irtran 1 | The above specimen. |
| 6 T38674 T20810 | Gillespie, D.T., et al. | 1965 | 2-12 | 673 | Irtran 1 | The above specimen. |
| 7 T44164 | McCarthy, D.E. | 1967 | 0.31-3.1 | 293 | Irtran 1 | Specimen 2.0 mm thick; specimen flat to within ten fringes or better of mercury green line, surfaces were parallel to within 0.001 mm/mm of length; pressed and sintered; measurements made on commercial double-beam instruments; reported error $\pm 2\%$. |
| 8 T38121 | Linsteadt, G. | 1964 | 1.0-15 | 50 | Irtran 1 | Specimen 1.27 cm in diameter and 1.02 mm thick; measurements made on Perkin-Elmer Model 221 spectrophotometer with NaCl optics; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 9 T38121 | Linsteadt, G. | 1964 | 1.0-15 | 300 | Irtran 1 | The above specimen. |
| 10 T36646 | Olsen, A.L. and McBride, W.R. | 1963 | 0.44-2.0 | 293 | Irtran 1 | Polycrystalline compact; cut, ground, and polished to provide plane parallel samples of thickness 0.110 in. (2.70 mm), values of thickness given in paper; comparative Knoop hardness number under 100 g load was 625; measurements performed with Cary 14 spectrometer; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 11 T36746 | Olsen, A.L. and McBride, W.R. | 1963 | 2.0-10 | 293 | Irtran 1 | The above specimen except measurement performed with a Perkin-Elmer 221 spectrometer. |
| 12 T36646 | Olsen, A.L. and McBride, W.R. | 1963 | 0.20-2.0 | 293 | Magnesium fluoride | 99.95 pure (estimate) prior to growth; single crystal; cut, ground, and polished to provide plane parallel samples of thickness 0.110 in. (2.70 mm), values of thickness given in paper; grown by Stockbarger method and obtained from Semi-Elements, Inc., Saxonburg, Pennsylvania; comparative Knoop hardness number under 100 g load was 415; measurements performed with Cary 14 spectrometer; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 13 T36646 | Olsen, A.L. and McBride, W.R. | 1963 | 2.0-11 | 293 | Magnesium fluoride | The above specimen except measurement performed with a Perkin-Elmer 221 spectrometer. |
| 14 T35848 | Linsteadt, G. | 1965 | 1.0-9.9 | 50 | Irtran 1 | Specimen 1.27 cm in diameter and 1.02 mm thick; measurements made on Perkin-Elmer Model 221 spectrophotometer with NaCl optics; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 15 T35848 | Linsteadt, G. | 1965 | 1.0-9.9 | 300 | Irtran 1 | The above specimen. |

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 16 T17017 | Ballard, S.S., McCarthy, K.A., and Wolfe, W.L. | 1961 | 1.0-10.0 | 299 | Irttran 1 | Specimen 1.75 mm thick; specular transmittance; information in this reference was obtained from Eastman Kodak Co. sales literature dated 15 June 1959 and 23 February 1961. |
| 17 T17017 | Ballard, S.S., et al. | 1961 | 1.0-9.5 | 673 | Irttran 1 | Similar to the above specimen. |
| 18 T17017 | Ballard, S.S., et al. | 1961 | 1.0-9.2 | 873 | Irttran 1 | Similar to the above specimen. |
| 19 T17017 | Ballard, S.S., et al. | 1961 | 1.0-8.8 | 1073 | Irttran 1 | Similar to the above specimen. |
| 20 E62600 | Eastman Kodak Co. | 1971 | 0.50-9.2 | 293 | Irttran 1 | Specimen thickness 0.5 mm; uncoated; spectral transmittance; temperature not explicitly mentioned, presumed to be room temperature, 293 K assigned; smooth values from figure. |
| 21 E62600 | Eastman Kodak Co. | 1971 | 0.5-8.5 | 293 | Irttran 1 | Similar to the above specimen except thickness 1 mm. |
| 22 E62600 | Eastman Kodak Co. | 1971 | 0.5-8.0 | 293 | Irttran 1 | Similar to the above specimen except thickness 2 mm. |
| 23 E62600 | Eastman Kodak Co. | 1971 | 0.5-7.9 | 293 | Irttran 1 | Similar to the above specimen except thickness 3 mm. |
| 24 E62600 | Eastman Kodak Co. | 1971 | 0.65-7.7 | 293 | Irttran 1 | Similar to the above specimen except thickness 6 mm. |
| 25 E62600 | Eastman Kodak Co. | 1971 | 0.84-7.6 | 293 | Irttran 1 | Similar to the above specimen except thickness 12 mm. |
| 26 T76525 | Hatch, S.E. | 1962 | 1.0-9.0 | 293 | Irttran 1 | Specimen thickness 1 mm; smooth values from figure; called "ambient transmittance", presumed room temperature, 293 K assigned; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 27 T76525 | Hatch, S.E. | 1962 | 1.0-9.0 | 293 | Irttran 1 | Similar to the above specimen except thickness 3.4 mm. |
| 28 T76525 | Hatch, S.E. | 1962 | 1.0-9.0 | 293 | Irttran 1 | Similar to the above specimen except thickness 7.6 mm. |
| 29 T53988 | Ballard, S.S. | 1965 | 0.93-8.3 | 293 | Irttran 1 | Specimen 6.2 mm thick; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 30 T76525 | Hatch, S.E. | 1962 | 10-15 | 295 | Irttran 1 | Thicknesses of 1 mm or greater; transmittance essentially zero in this wavelength range (argument presented on p. 597 of this reference that transmittance essentially zero in this wavelength range to 970 K); the applicable temperature is ambient, 293 K assigned; $\theta = 0^\circ$, $\theta' = 0^\circ$. |

TABLE 9-18. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ, μm; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| CURVE 1 | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 | | CURVE 5 (CONT.) | |
|----------|-------|-----------------|-------|-----------------|-------|---------|-------|-----------------|-------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| T = 293. | | | | | | | | | |
| 2.00 | 0.852 | 5.05 | 0.819 | 2.74 | 0.750 | 2.00 | 0.649 | 7.80 | 0.324 |
| 2.50 | 0.975 | 5.08 | 0.853 | 2.78 | 0.201 | 2.28 | 0.704 | 8.02 | 0.231 |
| 3.00 | 0.607 | 5.14 | 0.803 | 2.81 | 0.610 | 2.33 | 0.689 | 8.33 | 0.162 |
| 3.00 | 0.895 | 5.24 | 0.899 | 2.83 | 0.684 | 2.36 | 0.710 | 8.65 | 0.087 |
| 4.50 | 0.937 | 5.98 | 0.898 | 2.94 | 0.696 | 2.43 | 0.725 | 8.85 | 0.054 |
| 6.80 | 0.875 | 6.49 | 0.835 | 3.04 | 0.771 | 2.51 | 0.725 | 9.09 | 0.026 |
| 7.50 | 0.790 | 6.53 | 0.783 | 3.15 | 0.829 | 2.58 | 0.705 | 9.42 | 0.013 |
| 7.60 | 0.529 | 6.68 | 0.567 | 3.31 | 0.829 | 2.58 | 0.705 | 10.0 | 0.000 |
| 8.20 | 0.388 | 6.76 | 0.663 | 3.63 | 0.858 | 2.74 | 0.750 | 12.0 | 0.000 |
| 9.00 | 0.241 | 6.80 | 0.780 | 4.46 | 0.887 | 2.78 | 0.201 | | |
| 9.40 | 0.056 | 6.93 | 0.733 | 4.80 | 0.889 | 2.81 | 0.610 | | |
| 10.0 | 0.025 | 7.07 | 0.732 | 4.90 | 0.871 | 2.83 | 0.684 | | |
| 11.5 | 0.037 | 7.25 | 0.692 | 5.31 | 0.632 | 2.94 | 0.696 | | |
| 50.0 | 0.000 | 7.34 | 0.641 | 5.68 | 0.878 | 3.04 | 0.771 | | |
| | | 7.46 | 0.631 | 5.14 | 0.878 | 3.15 | 0.507 | | |
| | | 7.55 | 0.579 | 5.29 | 0.896 | 3.31 | 0.829 | | |
| | | 7.59 | 0.505 | 5.92 | 0.896 | 3.63 | 0.658 | | |
| | | 7.69 | 0.516 | 6.12 | 0.811 | 4.46 | 0.887 | | |
| | | 7.93 | 0.367 | 6.44 | 0.809 | 4.80 | 0.889 | | |
| | | 8.06 | 0.337 | 6.57 | 0.762 | 4.90 | 0.871 | | |
| | | 8.15 | 0.315 | 6.69 | 0.574 | 5.01 | 0.632 | | |
| | | 8.78 | 0.123 | 6.76 | 0.698 | 5.09 | 0.819 | | |
| | | 9.99 | 0.074 | 6.93 | 0.657 | 5.15 | 0.867 | | |
| | | 9.21 | 0.046 | 7.07 | 0.698 | 5.23 | 0.984 | | |
| | | 9.49 | 0.025 | 7.21 | 0.667 | 5.37 | 0.891 | | |
| | | 10.0 | 0.014 | 7.37 | 0.608 | 5.94 | 0.882 | | |
| | | | 0.000 | 7.42 | 0.605 | 6.10 | 0.869 | | |
| | | | | 7.57 | 0.534 | 6.29 | 0.329 | | |
| | | | | 7.95 | 0.466 | 6.46 | 0.783 | | |
| | | | | 7.73 | 0.466 | 6.58 | 0.738 | | |
| | | | | 7.96 | 0.329 | 6.62 | 0.575 | | |
| | | | | 8.06 | 0.273 | 6.75 | 0.624 | | |
| | | | | 8.18 | 0.270 | 6.85 | 0.637 | | |
| | | | | 8.52 | 0.165 | 6.94 | 0.645 | | |
| | | | | 8.83 | 0.039 | 7.06 | 0.645 | | |
| | | | | 9.39 | 0.058 | 7.20 | 0.607 | | |
| | | | | 9.26 | 0.028 | 7.36 | 0.542 | | |
| | | | | 9.49 | 0.017 | 7.49 | 0.504 | | |
| | | | | 10.0 | 0.000 | 7.64 | 0.403 | | |
| | | | | 12.0 | 0.000 | 4.69 | 0.394 | | |
| CURVE 3 | | | | | | | | | |
| T = 373. | | | | | | | | | |
| 2.00 | 0.649 | 2.00 | 0.649 | 2.00 | 0.649 | 2.00 | 0.649 | 2.00 | 0.649 |
| 2.28 | 0.704 | 2.28 | 0.704 | 2.28 | 0.704 | 2.28 | 0.704 | 2.28 | 0.704 |
| 2.33 | 0.689 | 2.26 | 0.704 | 2.33 | 0.659 | 2.36 | 0.887 | 2.33 | 0.689 |
| 2.36 | 0.713 | 2.33 | 0.669 | 2.33 | 0.669 | 2.36 | 0.887 | 2.36 | 0.725 |
| 2.43 | 0.725 | 2.36 | 0.637 | 2.43 | 0.725 | 2.43 | 0.889 | 2.43 | 0.725 |
| 2.51 | 0.725 | 2.51 | 0.725 | 2.51 | 0.725 | 2.51 | 0.887 | 2.51 | 0.725 |
| 2.58 | 0.750 | 2.43 | 0.725 | 2.58 | 0.725 | 2.58 | 0.889 | 2.58 | 0.725 |
| 2.74 | 0.201 | 2.51 | 0.725 | 2.74 | 0.725 | 2.74 | 0.889 | 2.74 | 0.725 |
| 2.81 | 0.610 | 2.58 | 0.725 | 2.81 | 0.725 | 2.81 | 0.889 | 2.81 | 0.725 |
| 2.93 | 0.634 | 2.74 | 0.610 | 2.93 | 0.634 | 2.93 | 0.889 | 2.93 | 0.634 |
| 2.94 | 0.696 | 2.81 | 0.634 | 2.94 | 0.696 | 2.94 | 0.889 | 2.94 | 0.696 |
| 3.04 | 0.771 | 2.81 | 0.634 | 3.04 | 0.771 | 3.04 | 0.889 | 3.04 | 0.771 |
| 3.15 | 0.829 | 2.94 | 0.634 | 3.15 | 0.829 | 3.15 | 0.889 | 3.15 | 0.829 |
| 3.31 | 0.889 | 3.04 | 0.634 | 3.31 | 0.889 | 3.31 | 0.889 | 3.31 | 0.889 |
| 3.63 | 0.887 | 3.15 | 0.634 | 3.63 | 0.887 | 3.63 | 0.889 | 3.63 | 0.887 |
| 4.46 | 0.887 | 3.31 | 0.634 | 4.46 | 0.887 | 4.46 | 0.889 | 4.46 | 0.887 |
| 4.90 | 0.889 | 3.63 | 0.634 | 4.90 | 0.889 | 4.90 | 0.889 | 4.90 | 0.889 |
| 5.01 | 0.632 | 4.46 | 0.634 | 5.01 | 0.632 | 5.01 | 0.889 | 5.01 | 0.632 |
| 5.17 | 0.889 | 4.90 | 0.634 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 |
| 5.17 | 0.889 | 5.01 | 0.632 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 |
| 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 |
| 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 |
| 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 |
| 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 | 5.17 | 0.889 |

CURVE 6
T = 673.

CURVE 5
T = 573.

CURVE 4
T = 473.

TABLE 9-16. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
|-----------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|------------------|---|
| CURVE 6 (CONT.) | | | | | | | | | | | | | |
| 5.66 | 0.872 | 0.752 | 0.436 | 10.99 | 0.716 | 14.92 | 0.116 | 2.68 | 0.760 | 9.67 | 0.069 | CURVE 11 (CONT.) | |
| 5.83 | 0.859 | 0.837 | 0.482 | 11.60 | 0.716 | 15.00 | 0.116 | 2.73 | 0.372 | 9.45 | 0.037 | | |
| 6.18 | 0.814 | 0.877 | 0.534 | 11.95 | 0.723 | CURVE 10 | | 2.77 | 0.702 | 9.77 | 0.023 | | |
| 6.33 | 0.776 | 0.921 | 0.577 | 12.11 | 0.723 | T = 293. | | 2.84 | 0.706 | 10.28 | 0.000 | | |
| 6.45 | 0.742 | 0.995 | 0.627 | 12.47 | 0.696 | 0.442 | 0.000 | 2.92 | 0.757 | CURVE 12 | | | |
| 6.56 | 0.679 | 1.07 | 0.668 | 12.73 | 0.688 | 0.553 | 0.006 | 2.97 | 0.779 | T = 253. | | | |
| 6.64 | 0.609 | 1.13 | 0.699 | 13.48 | 0.682 | 0.624 | 0.018 | 3.03 | 0.808 | | | | |
| 6.70 | 0.567 | 1.21 | 0.729 | 13.67 | 0.657 | 0.699 | 0.041 | 3.13 | 0.826 | | | | |
| 7.01 | 0.533 | 1.28 | 0.760 | 13.94 | 0.657 | 0.792 | 0.074 | 3.29 | 0.845 | | | | |
| 7.24 | 0.491 | 1.36 | 0.788 | 14.14 | 0.622 | 0.868 | 0.122 | 3.61 | 0.859 | | | | |
| 7.50 | 0.371 | 1.43 | 0.809 | 14.49 | 0.426 | 0.979 | 0.195 | 3.86 | 0.879 | | | | |
| 7.87 | 0.203 | 1.50 | 0.825 | 14.64 | 0.269 | 1.077 | 0.262 | 4.07 | 0.894 | | | | |
| 8.04 | 0.141 | 1.61 | 0.844 | 14.70 | 0.119 | 1.169 | 0.321 | 4.85 | 0.894 | | | | |
| 8.24 | 0.103 | 1.75 | 0.862 | 14.79 | 0.051 | 1.266 | 0.382 | 4.90 | 0.874 | | | | |
| 8.50 | 0.064 | 1.90 | 0.873 | 15.00 | 0.372 | 1.458 | 0.493 | 4.98 | 0.663 | | | | |
| 8.77 | 0.038 | 2.08 | 0.893 | CURVE 9 | | | | 5.02 | 0.842 | | | | |
| 9.00 | 0.018 | 2.19 | 0.905 | T = 300. | | | | 5.06 | 0.876 | | | | |
| 9.50 | 0.000 | 2.32 | 0.937 | 1.50 | 0.363 | 1.532 | 0.523 | 5.15 | 0.902 | | | | |
| 12.0 | 0.000 | 2.62 | 0.907 | 1.59 | 0.472 | 1.629 | 0.569 | 6.00 | 0.902 | | | | |
| CURVE 7 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |
| 0.356 | 0.000 | 2.73 | 0.887 | 1.79 | 0.616 | 1.895 | 0.660 | 6.16 | 0.835 | | | | |
| 0.341 | 0.014 | 2.74 | 0.716 | 2.11 | 0.662 | 2.000 | 0.686 | 6.47 | 0.822 | | | | |
| 0.366 | 0.031 | 2.80 | 0.402 | 2.20 | 0.671 | CURVE 11 | | 6.56 | 0.790 | | | | |
| 0.366 | 0.051 | 2.84 | 0.880 | 3.08 | 0.694 | T = 293. | | 6.56 | 0.718 | | | | |
| 0.414 | 0.059 | 3.06 | 0.898 | 4.54 | 0.717 | 2.00 | 0.670 | 6.75 | 0.691 | | | | |
| 0.433 | 0.087 | CURVE 8 | | 6.83 | 0.736 | 2.11 | 0.698 | 6.80 | 0.718 | | | | |
| 0.452 | 0.156 | T = 50. | | 10.02 | 0.736 | 2.24 | 0.715 | 7.07 | 0.740 | | | | |
| 0.473 | 0.126 | 1.00 | 0.386 | 10.99 | 0.707 | 2.26 | 0.705 | 7.23 | 0.720 | | | | |
| 0.497 | 0.149 | 1.18 | 0.456 | 11.21 | 0.698 | 2.33 | 0.733 | 7.34 | 0.655 | | | | |
| 0.497 | 0.149 | 1.32 | 0.539 | 11.59 | 0.692 | 2.38 | 0.737 | 7.43 | 0.655 | | | | |
| 0.516 | 0.173 | 1.49 | 0.585 | 11.78 | 0.705 | 2.45 | 0.737 | 7.53 | 0.606 | | | | |
| 0.537 | 0.138 | 1.71 | 0.626 | 12.22 | 0.705 | 2.51 | 0.718 | 7.62 | 0.528 | | | | |
| 0.552 | 0.231 | 1.91 | 0.648 | 12.75 | 0.669 | 2.56 | 0.730 | 7.71 | 0.528 | | | | |
| 0.550 | 0.256 | 2.20 | 0.671 | 13.38 | 0.632 | 2.63 | 0.737 | 7.74 | 0.496 | | | | |
| 0.612 | 0.287 | 3.08 | 0.694 | 13.78 | 0.594 | 2.63 | 0.737 | 7.89 | 0.423 | | | | |
| 0.641 | 0.321 | 4.54 | 0.717 | 14.07 | 0.538 | 2.56 | 0.718 | 8.06 | 0.308 | | | | |
| 0.671 | 0.351 | 6.63 | 0.736 | 14.41 | 0.457 | 2.56 | 0.730 | 8.18 | 0.308 | | | | |
| 0.710 | 0.395 | 13.02 | 0.736 | 14.76 | 0.233 | 2.63 | 0.737 | 8.41 | 0.236 | | | | |
| | | | | | | | | 8.49 | 0.198 | | | | |
| | | | | | | | | 8.66 | 0.105 | | | | |
| | | | | | | | | 10.32 | 0.025 | | | | |
| | | | | | | | | 10.65 | 0.000 | | | | |

TABLE 3-16. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T , K; TRANSMITTANCE, T]

| CURVE 13 (CONT.) | | CURVE 14 (CONT.) | | CURVE 15 (CONT.) | | CURVE 16 (CONT.) | | CURVE 17 (CONT.) | | CURVE 18 (CONT.) | |
|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 1.00 | 0.577 | 6.83 | 0.826 | 4.97 | 0.854 | 2.65 | 0.777 | 2.46 | 0.806 | 2.46 | 0.806 |
| 1.40 | 0.762 | 6.97 | 0.850 | 5.03 | 0.916 | 2.75 | 0.652 | 2.59 | 0.806 | 2.58 | 0.806 |
| 1.56 | 0.803 | 7.12 | 0.671 | 5.07 | 0.931 | 2.79 | 0.817 | 2.65 | 0.777 | 2.65 | 0.777 |
| 1.74 | 0.839 | 7.33 | 0.671 | 5.28 | 0.952 | 2.92 | 0.838 | 2.75 | 0.652 | 2.75 | 0.652 |
| 1.94 | 0.869 | 7.47 | 0.659 | 6.03 | 0.953 | 3.13 | 0.859 | 2.79 | 0.817 | 2.79 | 0.817 |
| CURVE 14 | | 7.55 | 0.836 | 6.19 | 0.941 | 3.49 | 0.878 | 2.92 | 0.836 | 2.92 | 0.838 |
| $T = 50.$ | | 8.04 | 0.568 | 6.30 | 0.917 | 3.98 | 0.901 | 3.13 | 0.859 | 3.13 | 0.859 |
| 1.00 | 0.577 | 8.28 | 0.560 | 6.41 | 0.892 | 4.51 | 0.922 | 3.49 | 0.876 | 3.49 | 0.878 |
| 1.40 | 0.762 | 8.51 | 0.468 | 6.54 | 0.859 | 5.05 | 0.936 | 3.98 | 0.901 | 3.98 | 0.901 |
| 1.56 | 0.803 | 8.69 | 0.425 | 6.63 | 0.817 | 5.73 | 0.936 | 4.51 | 0.922 | 4.51 | 0.922 |
| 1.74 | 0.839 | 8.86 | 0.390 | 6.68 | 0.727 | 6.15 | 0.921 | 5.05 | 0.936 | 5.05 | 0.936 |
| 1.94 | 0.869 | 9.03 | 0.333 | 6.74 | 0.767 | 6.46 | 0.905 | 5.73 | 0.936 | 5.63 | 0.936 |
| 2.17 | 0.895 | 9.19 | 0.315 | 6.85 | 0.803 | 6.76 | 0.870 | 5.93 | 0.919 | 5.81 | 0.921 |
| 2.55 | 0.955 | 9.35 | 0.287 | 7.00 | 0.829 | 7.06 | 0.835 | 6.16 | 0.895 | 5.99 | 0.896 |
| 2.68 | 0.908 | 9.42 | 0.236 | 7.14 | 0.837 | 7.27 | 0.789 | 6.37 | 0.846 | 6.19 | 0.859 |
| 2.73 | 0.884 | 9.54 | 0.159 | 7.37 | 0.837 | 7.50 | 0.736 | 6.61 | 0.792 | 6.41 | 0.810 |
| 2.74 | 0.778 | 9.74 | 0.104 | 7.52 | 0.820 | 7.69 | 0.685 | 6.87 | 0.741 | 6.59 | 0.766 |
| 2.79 | 0.854 | 9.87 | 0.000 | 7.71 | 0.736 | 7.90 | 0.622 | 7.06 | 0.685 | 6.77 | 0.711 |
| 2.93 | 0.687 | CURVE 15 | | 7.92 | 0.584 | 8.14 | 0.554 | 7.32 | 0.905 | 6.97 | 0.655 |
| 3.02 | 0.910 | $T = 300.$ | | 8.05 | 0.532 | 8.36 | 0.475 | 7.63 | 0.521 | 7.12 | 0.658 |
| 3.14 | 0.924 | 1.00 | 0.577 | 8.20 | 0.515 | 8.61 | 0.372 | 7.84 | 0.450 | 7.33 | 0.533 |
| 3.44 | 0.933 | 1.40 | 0.762 | 8.39 | 0.470 | 8.88 | 0.265 | 8.09 | 0.346 | 7.51 | 0.467 |
| 4.25 | 0.940 | 1.74 | 0.839 | 8.83 | 0.321 | 9.04 | 0.207 | 8.34 | 0.268 | 7.68 | 0.404 |
| 4.51 | 0.951 | 1.94 | 0.869 | 9.12 | 0.256 | 9.17 | 0.166 | 8.57 | 0.197 | 7.84 | 0.347 |
| 4.92 | 0.946 | 2.17 | 0.695 | 9.38 | 0.204 | 9.35 | 0.122 | 8.81 | 0.143 | 8.02 | 0.287 |
| 5.07 | 0.854 | 2.55 | 0.695 | 9.93 | 0.000 | 9.60 | 0.074 | 9.05 | 0.085 | 8.17 | 0.237 |
| 5.03 | 0.916 | 2.68 | 0.908 | CURVE 16 | | 9.80 | 0.041 | 9.29 | 0.034 | 8.38 | 0.179 |
| 5.08 | 0.953 | 2.73 | 0.884 | $T = 299.$ | | 10.00 | 0.019 | 9.45 | 0.000 | 8.59 | 0.125 |
| 6.03 | 0.953 | 2.74 | 0.876 | 1.00 | 0.233 | CURVE 17 | | CURVE 18 | | CURVE 15 | |
| 6.33 | 0.941 | 2.74 | 0.884 | 1.16 | 0.353 | $T = 673.$ | | $T = 873.$ | | $T = 1073.$ | |
| 6.19 | 0.941 | 2.74 | 0.676 | 1.38 | 0.499 | 1.00 | 0.233 | 1.00 | 0.233 | 0.233 | |
| 6.33 | 0.917 | 2.62 | 0.841 | 1.48 | 0.541 | 1.16 | 0.353 | 1.16 | 0.353 | 0.353 | |
| 6.44 | 0.892 | 3.22 | 0.896 | 1.63 | 0.600 | 1.38 | 0.489 | 1.38 | 0.489 | 0.489 | |
| 6.52 | 0.874 | 3.14 | 0.924 | 1.79 | 0.666 | 1.48 | 0.541 | 1.48 | 0.541 | 0.541 | |
| 6.64 | 0.843 | 3.44 | 0.938 | 2.04 | 0.730 | 1.63 | 0.600 | 1.63 | 0.600 | 0.600 | |
| 6.68 | 0.843 | 4.25 | 0.946 | 2.24 | 0.771 | 1.79 | 0.666 | 1.79 | 0.666 | 0.666 | |
| 6.72 | 0.728 | 4.61 | 0.951 | 2.46 | 0.806 | 2.04 | 0.730 | 2.04 | 0.730 | 0.730 | |
| 6.72 | 0.779 | 4.92 | 0.948 | 2.58 | 0.806 | 2.24 | 0.771 | 2.24 | 0.771 | 0.771 | |

TABLE 9-16. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T | λ | T | λ | T | λ | T | λ | T | | |
|------------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-------|-------|
| CURVE 19 (CONT.) | | | | | | | | | | | |
| 1.79 | 0.066 | 0.63 | 0.780 | 7.50 | 0.844 | 2.31 | 0.902 | 7.84 | 0.256 | | |
| 2.04 | 0.730 | 0.89 | 0.602 | 7.54 | 0.833 | 2.42 | 0.907 | 7.87 | 0.206 | | |
| 2.24 | 0.771 | 0.94 | 0.821 | 7.59 | 0.813 | 2.55 | 0.907 | 7.90 | 0.166 | | |
| 2.46 | 0.806 | 0.99 | 0.638 | 7.63 | 0.777 | 2.62 | 0.912 | 7.92 | 0.139 | | |
| 2.53 | 0.806 | 1.08 | 0.530 | 7.70 | 0.680 | 2.67 | 0.894 | 7.94 | 0.115 | | |
| 2.65 | 0.777 | 1.16 | 0.664 | 7.78 | 0.580 | 2.70 | 0.879 | 7.98 | 0.094 | | |
| 2.75 | 0.652 | 1.26 | 0.674 | 7.83 | 0.487 | 2.71 | 0.850 | 8.03 | 0.073 | | |
| 2.79 | 0.817 | 1.35 | 0.894 | 7.86 | 0.426 | 2.73 | 0.764 | 8.05 | 0.063 | | |
| 2.92 | 0.838 | 1.45 | 0.890 | 7.89 | 0.399 | 2.73 | 0.813 | 8.11 | 0.053 | | |
| 3.13 | 0.859 | 1.59 | 0.697 | 7.95 | 0.343 | 2.77 | 0.856 | 8.17 | 0.042 | | |
| 3.49 | 0.878 | 1.66 | 0.906 | 8.01 | 0.304 | 2.79 | 0.878 | 8.26 | 0.030 | | |
| 3.98 | 0.901 | 2.01 | 0.910 | 8.06 | 0.277 | 2.86 | 0.894 | 8.35 | 0.021 | | |
| 4.51 | 0.922 | 2.44 | 0.916 | 8.12 | 0.255 | 2.92 | 0.900 | 8.51 | 0.000 | | |
| 4.85 | 0.936 | 2.63 | 0.916 | 8.25 | 0.223 | 3.05 | 0.906 | CURVE 22 | | | |
| 5.43 | 0.936 | 2.65 | 0.904 | 8.38 | 0.191 | 3.49 | 0.909 | T = 293. | | | |
| 5.64 | 0.917 | 2.71 | 0.880 | 8.49 | 0.165 | 3.80 | 0.912 | 0.100 | | | |
| 5.81 | 0.901 | 2.72 | 0.817 | 8.58 | 0.134 | 3.99 | 0.914 | 0.50 | 0.203 | | |
| 6.32 | 0.870 | 2.72 | 0.683 | 8.72 | 0.093 | 4.49 | 0.921 | 0.60 | 0.331 | | |
| 6.25 | 0.801 | 2.75 | 0.902 | 8.77 | 0.083 | 4.49 | 0.925 | 0.68 | 0.331 | | |
| 6.42 | 0.754 | 2.81 | 0.910 | 8.91 | 0.053 | 5.07 | 0.931 | 0.76 | 0.468 | | |
| 6.65 | 0.665 | 3.00 | 0.913 | 9.02 | 0.044 | 5.27 | 0.933 | 0.79 | 0.536 | | |
| 6.86 | 0.579 | 3.49 | 0.916 | 9.17 | 0.000 | 5.68 | 0.933 | 0.82 | 0.550 | | |
| 7.25 | 0.474 | 3.80 | 0.919 | CURVE 21 | | | | | | 0.86 | 0.581 |
| 7.52 | 0.359 | 3.80 | 0.921 | T = 293. | | | | | | 0.91 | 0.614 |
| 7.69 | 0.308 | 3.85 | 0.921 | 0.50 | 0.896 | 6.09 | 0.922 | 0.96 | 0.645 | | |
| 7.84 | 0.254 | 4.35 | 0.925 | 6.50 | 0.851 | 6.26 | 0.914 | 1.08 | 0.701 | | |
| 8.57 | 0.190 | 4.69 | 0.932 | 6.98 | 0.822 | 6.98 | 0.896 | 1.14 | 0.721 | | |
| 8.22 | 0.147 | 4.93 | 0.937 | 7.10 | 0.838 | 7.10 | 0.838 | 1.22 | 0.747 | | |
| 8.41 | 0.132 | 4.99 | 0.933 | 7.62 | 0.648 | 7.28 | 0.824 | 1.29 | 0.763 | | |
| 8.58 | 0.059 | 5.18 | 0.940 | 8.89 | 0.701 | 7.35 | 0.803 | 1.34 | 0.778 | | |
| 8.71 | 0.031 | 5.70 | 0.940 | 9.92 | 0.722 | 7.43 | 0.794 | 1.40 | 0.791 | | |
| 8.84 | 0.006 | 6.00 | 0.935 | 1.00 | 0.750 | 7.47 | 0.774 | 1.50 | 0.807 | | |
| CURVE 20 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 0.59 | 0.560 | 6.50 | 0.923 | 1.10 | 0.775 | 7.53 | 0.734 | 1.59 | 0.819 | | |
| 0.60 | 0.637 | 6.50 | 0.917 | 1.32 | 0.823 | 7.56 | 0.702 | 1.68 | 0.831 | | |
| 0.69 | 0.701 | 6.87 | 0.908 | 1.42 | 0.841 | 7.63 | 0.616 | 1.79 | 0.841 | | |
| 0.77 | 0.751 | 7.06 | 0.696 | 1.50 | 0.853 | 7.70 | 0.514 | 1.88 | 0.848 | | |
| 0.89 | 0.761 | 7.21 | 0.867 | 1.53 | 0.867 | 7.74 | 0.442 | 2.00 | 0.857 | | |
| 0.84 | 0.006 | 7.34 | 0.876 | 1.73 | 0.873 | 7.78 | 0.385 | 2.11 | 0.862 | | |
| 0.77 | 0.751 | 7.41 | 0.865 | 2.14 | 0.892 | 7.81 | 0.332 | 2.30 | 0.872 | | |
| 2.43 | 0.678 | | | | | | | | 2.43 | 0.678 | |
| 2.60 | 0.681 | | | | | | | | 2.60 | 0.681 | |
| 2.71 | 0.868 | | | | | | | | 2.71 | 0.868 | |
| 2.73 | 0.726 | | | | | | | | 2.73 | 0.726 | |
| 2.73 | 0.785 | | | | | | | | 2.73 | 0.785 | |
| 2.75 | 0.816 | | | | | | | | 2.75 | 0.816 | |
| 2.80 | 0.842 | | | | | | | | 2.80 | 0.842 | |
| 2.86 | 0.855 | | | | | | | | 2.86 | 0.855 | |
| 2.95 | 0.865 | | | | | | | | 2.95 | 0.865 | |
| 3.03 | 0.872 | | | | | | | | 3.03 | 0.872 | |
| 3.10 | 0.878 | | | | | | | | 3.10 | 0.878 | |
| 3.19 | 0.893 | | | | | | | | 3.19 | 0.893 | |
| 3.27 | 0.838 | | | | | | | | 3.27 | 0.838 | |
| 3.38 | 0.892 | | | | | | | | 3.38 | 0.892 | |
| 3.49 | 0.897 | | | | | | | | 3.49 | 0.897 | |
| 3.60 | 0.899 | | | | | | | | 3.60 | 0.899 | |
| 3.98 | 0.900 | | | | | | | | 3.98 | 0.900 | |
| 4.46 | 0.900 | | | | | | | | 4.46 | 0.900 | |
| 4.78 | 0.904 | | | | | | | | 4.78 | 0.904 | |
| 4.68 | 0.908 | | | | | | | | 4.68 | 0.908 | |
| 4.95 | 0.913 | | | | | | | | 4.95 | 0.913 | |
| 5.01 | 0.903 | | | | | | | | 5.01 | 0.903 | |
| 5.13 | 0.912 | | | | | | | | 5.13 | 0.912 | |
| 5.23 | 0.916 | | | | | | | | 5.23 | 0.916 | |
| 5.32 | 0.918 | | | | | | | | 5.32 | 0.918 | |
| 5.53 | 0.918 | | | | | | | | 5.53 | 0.918 | |
| 5.69 | 0.914 | | | | | | | | 5.69 | 0.914 | |
| 5.79 | 0.910 | | | | | | | | 5.79 | 0.910 | |
| 5.67 | 0.905 | | | | | | | | 5.67 | 0.905 | |
| 6.00 | 0.895 | | | | | | | | 6.00 | 0.895 | |
| 6.16 | 0.880 | | | | | | | | 6.16 | 0.880 | |
| 6.34 | 0.859 | | | | | | | | 6.34 | 0.859 | |
| 6.50 | 0.838 | | | | | | | | 6.50 | 0.838 | |
| 6.67 | 0.812 | | | | | | | | 6.67 | 0.812 | |
| 6.82 | 0.790 | | | | | | | | 6.82 | 0.790 | |
| 6.99 | 0.751 | | | | | | | | 6.99 | 0.751 | |
| 7.10 | 0.739 | | | | | | | | 7.10 | 0.739 | |
| 7.18 | 0.716 | | | | | | | | 7.18 | 0.716 | |
| 7.25 | 0.698 | | | | | | | | 7.25 | 0.698 | |

TABLE 9-18. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | | |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|------------------|--------|-----------|--------|--|--|
| CURVE 25 (CONT.) | | | | | | | | | | | | | | | |
| 6.72 | 0.328 | 5.96 | 0.939 | 3.19 | 0.882 | 1.63 | 0.469 | 6.89 | 0.457 | CURVE 26 (CONT.) | | | | | |
| 6.30 | 0.306 | 6.24 | 0.919 | 3.43 | 0.907 | 1.83 | 0.539 | 6.96 | 0.468 | CURVE 27 (CONT.) | | | | | |
| 6.88 | 0.273 | 6.49 | 0.898 | 3.65 | 0.918 | 2.03 | 0.618 | 7.06 | 0.468 | CURVE 28 (CONT.) | | | | | |
| 7.00 | 0.237 | 6.72 | 0.853 | 3.80 | 0.918 | 2.21 | 0.671 | 7.15 | 0.454 | CURVE 29 | | | | | |
| 7.09 | 0.236 | 6.99 | 0.874 | 4.37 | 0.918 | 2.32 | 0.693 | 7.21 | 0.429 | T = 293. | | | | | |
| 7.19 | 0.173 | 7.01 | 0.874 | 4.62 | 0.913 | 2.45 | 0.715 | 7.43 | 0.268 | | | | | | |
| 7.28 | 0.144 | 7.21 | 0.852 | 4.76 | 0.902 | 2.54 | 0.715 | 7.54 | 0.153 | | | | | | |
| 7.33 | 0.126 | 7.41 | 0.823 | 4.84 | 0.874 | 2.62 | 0.697 | 7.66 | 0.066 | | | | | | |
| 7.45 | 0.071 | 7.52 | 0.801 | 4.69 | 0.831 | 2.66 | 0.629 | 7.70 | 0.332 | | | | | | |
| 7.59 | 0.000 | 7.59 | 0.776 | 4.95 | 0.895 | 2.66 | 0.556 | 7.85 | 0.010 | | | | | | |
| CURVE 26 | | | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | |
| 1.33 | 0.676 | 7.82 | 0.950 | 5.02 | 0.939 | 2.73 | 0.582 | 9.00 | 0.005 | | | | | | |
| 1.16 | 0.709 | 7.84 | 0.795 | 5.16 | 0.930 | 2.73 | 0.601 | CURVE 29 | | | | | | | |
| 1.29 | 0.905 | 7.92 | 0.441 | 5.78 | 0.917 | 2.78 | 0.623 | T = 293. | | | | | | | |
| 1.42 | 0.328 | 8.04 | 0.421 | 5.99 | 0.896 | 2.90 | 0.649 | | | | | | | | |
| 1.70 | 0.371 | 8.26 | 0.394 | 6.13 | 0.866 | 3.01 | 0.700 | | | | | | | | |
| 1.98 | 0.900 | 8.41 | 0.335 | 6.24 | 0.823 | 3.12 | 0.755 | | | | | | | | |
| 2.20 | 0.915 | 8.57 | 0.286 | 6.37 | 0.767 | 3.21 | 0.796 | | | | | | | | |
| 2.57 | 0.915 | 8.82 | 0.225 | 6.73 | 0.671 | 3.55 | 0.856 | | | | | | | | |
| 2.63 | 0.982 | 9.00 | 0.169 | 6.84 | 0.690 | 3.80 | 0.866 | | | | | | | | |
| 2.65 | 0.773 | CURVE 27 | | | | | | | | | | | | | |
| 2.67 | 0.755 | T = 293. | | | | | | | | | | | | | |
| 2.71 | 0.780 | 1.51 | 0.270 | 7.73 | 0.214 | 4.29 | 0.863 | | | | | | | | |
| 2.73 | 0.891 | 1.28 | 0.244 | 7.97 | 0.082 | 4.37 | 0.863 | | | | | | | | |
| 2.81 | 0.312 | 1.15 | 0.429 | 7.99 | 0.047 | 4.42 | 0.863 | | | | | | | | |
| 3.22 | 0.333 | 1.35 | 0.334 | 8.19 | 0.047 | 4.90 | 0.672 | | | | | | | | |
| 3.49 | 0.945 | 1.57 | 0.534 | 8.34 | 0.035 | 5.02 | 0.930 | | | | | | | | |
| 4.12 | 0.935 | 1.67 | 0.742 | 8.50 | 0.016 | 5.14 | 0.976 | | | | | | | | |
| 4.18 | 0.917 | 2.11 | 0.783 | 9.00 | 0.000 | 5.49 | 0.861 | | | | | | | | |
| 4.33 | 0.948 | 2.37 | 0.619 | CURVE 28 | | | | | | | | | | | |
| 4.79 | 0.943 | 2.53 | 0.802 | T = 293. | | | | | | | | | | | |
| 4.86 | 0.935 | 2.64 | 0.802 | 6.06 | 0.802 | 6.06 | 0.802 | | | | | | | | |
| 4.90 | 0.917 | 2.69 | 0.684 | 6.14 | 0.762 | 6.14 | 0.762 | | | | | | | | |
| 5.01 | 0.937 | 2.71 | 0.630 | 6.29 | 0.674 | 6.29 | 0.674 | | | | | | | | |
| 5.14 | 0.949 | 2.79 | 0.739 | 6.58 | 0.469 | 6.58 | 0.469 | | | | | | | | |
| 5.61 | 0.949 | 2.89 | 0.813 | 6.65 | 0.410 | 6.65 | 0.410 | | | | | | | | |
| | | 3.00 | 0.854 | 6.69 | 0.360 | 6.69 | 0.360 | | | | | | | | |
| | | | | 6.79 | 0.429 | 6.79 | 0.429 | | | | | | | | |
| | | | | | | | | CURVE 29 | | | | | | | |
| | | | | | | | | T = 293. | | | | | | | |
| | | | | 3.93 | 0.295 | 3.93 | 0.295 | | | | | | | | |
| | | | | 1.60 | 0.491 | 1.60 | 0.491 | | | | | | | | |
| | | | | 2.25 | 0.610 | 2.25 | 0.610 | | | | | | | | |
| | | | | 2.50 | 0.638 | 2.50 | 0.638 | | | | | | | | |
| | | | | 2.82 | 0.645 | 2.82 | 0.645 | | | | | | | | |
| | | | | 2.96 | 0.630 | 2.96 | 0.630 | | | | | | | | |
| | | | | 3.11 | 0.623 | 3.11 | 0.623 | | | | | | | | |
| | | | | 3.40 | 0.647 | 3.40 | 0.647 | | | | | | | | |
| | | | | 4.19 | 0.716 | 4.19 | 0.716 | | | | | | | | |
| | | | | 5.02 | 0.733 | 5.02 | 0.733 | | | | | | | | |
| | | | | 5.87 | 0.742 | 5.87 | 0.742 | | | | | | | | |
| | | | | 5.97 | 0.744 | 5.97 | 0.744 | | | | | | | | |
| | | | | 5.52 | 0.749 | 5.52 | 0.749 | | | | | | | | |
| | | | | 6.84 | 0.655 | 6.84 | 0.655 | | | | | | | | |
| | | | | 7.14 | 0.539 | 7.14 | 0.539 | | | | | | | | |
| | | | | 7.42 | 0.702 | 7.42 | 0.702 | | | | | | | | |
| | | | | 7.66 | 0.241 | 7.66 | 0.241 | | | | | | | | |
| | | | | 7.79 | 0.138 | 7.79 | 0.138 | | | | | | | | |
| | | | | 7.85 | 0.373 | 7.85 | 0.373 | | | | | | | | |
| | | | | 7.93 | 0.031 | 7.93 | 0.031 | | | | | | | | |
| | | | | 8.03 | 0.018 | 8.03 | 0.018 | | | | | | | | |
| | | | | 8.26 | 0.000 | 8.26 | 0.000 | | | | | | | | |

h. Normal Spectral Transmittance (Temperature Dependence)

No experimental data was found for the temperature dependence of the normal spectral transmittance of Irtran 1. However, a provisional curve at $3.8 \mu\text{m}$, with an uncertainty of 12%, and applying to a specimen thickness of 1.75 mm is listed in Table 9-19 and shown in Figure 9-13. Several considerations were relevant in arriving at this provisional curve. The data of curves 16, 17, 18, and 19 of the previous section show the transmittance as constant at temperatures of 299, 673, 873, and 1073 K. The uncertainty of 12% takes account of the slight variation at $3.8 \mu\text{m}$ by curves 2-6 of the previous section. The constant value selected at $3.8 \mu\text{m}$ was the value from the provisional curve in the preceding section.

TABLE 9-19. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (IRTRAN 1) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| T | T |
|-----------------|-------|
| 1.75MM THICK | |
| $\lambda = 3.6$ | |
| 299. | 0.898 |
| 673. | 0.898 |
| 873. | 0.898 |
| 1073. | 0.898 |

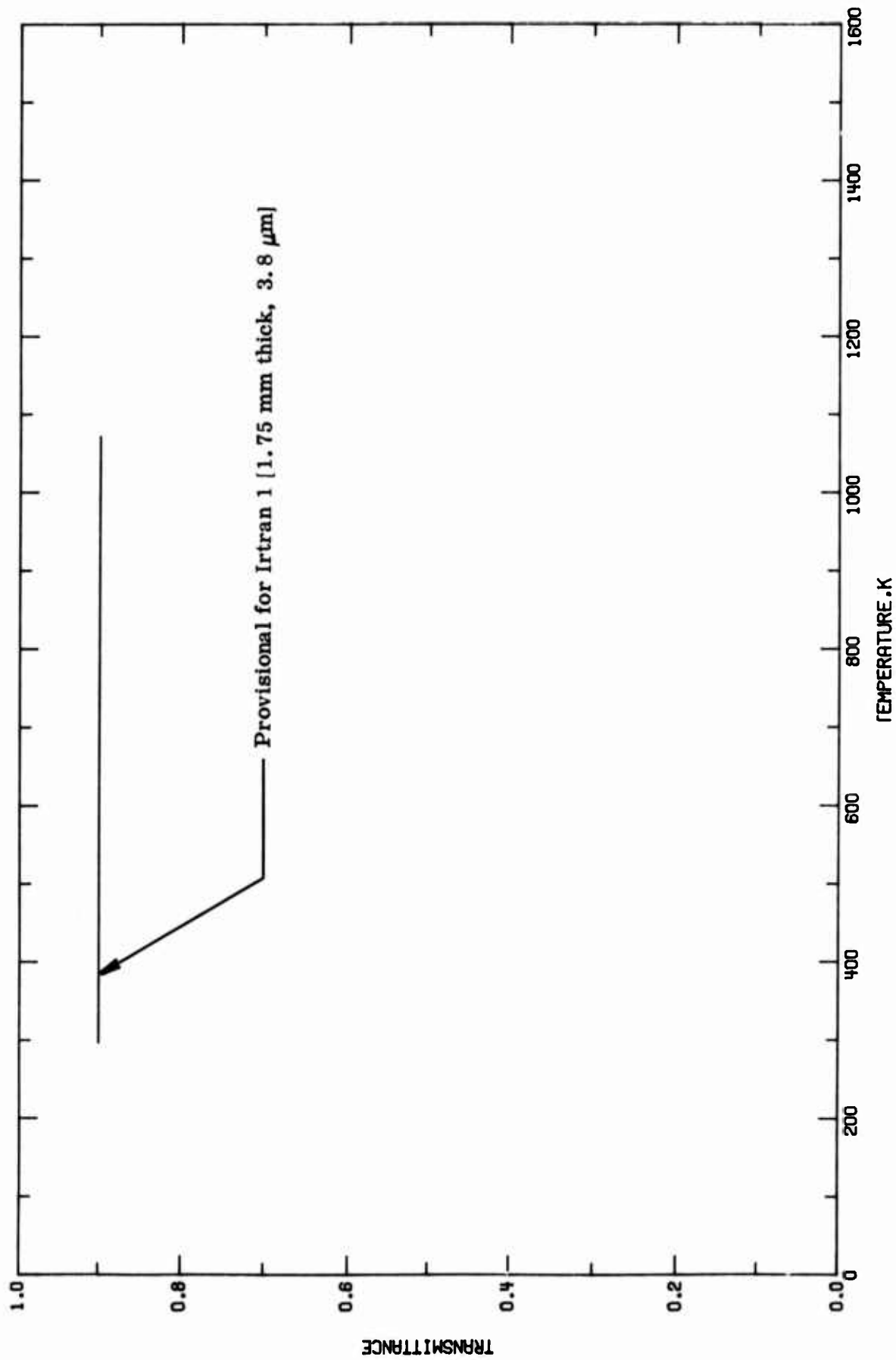


FIGURE 9-13. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF MAGNESIUM FLUORIDE (TEMPERATURE DEPENDENCE).

4.10. Pyroceram

Pyroceram is a generic name for a group of glass-ceramic materials, which were developed by the Corning Glass Works, Corning, New York 14830. The word "Pyroceram" is a trademark of Corning Glass Works and is registered with the United States Patent Office. Pyrocerams are microcrystalline materials formed originally from a noncrystalline glass.

The specific Pyroceram that is of interest for the purposes of this report is Corning Code 9606, therefore, specific properties mentioned in this general section will be for Corning 9606. In addition, in the data sections pertaining to Pyroceram, the aim is to give evaluated data, when appropriate, for Corning 9606. Data was extracted not only for Corning 9606 but also for any other material subsumed under the name of Pyroceram or that was labeled as a Pyroceramic type material. This was done in order to see the similarities and differences of the various Pyrocerams with the purpose of aiding data evaluation.

Corning Code 9606 is a magnesia aluminosilicate glass ceramic (composed of silicon dioxide, aluminum oxide, magnesium oxide, and a small amount of titanium dioxide). The ingredients are melted together at temperatures of the order of 1900 K using special techniques to insure uniform composition, constant density, freedom from bubbles and striations, and uniform electrical properties. Pyroceram 9606 is non-porous, considerably harder than glass, opaque, and gray in color.

Code 9606 is primarily used in military products and specifically as missile radomes since it has uniform electrical properties throughout the material at elevated temperatures and the ability to pass R. F. signals. Other properties which make it good for radome applications are good thermal shock and rain erosion characteristics.

According to 9606 Data Sheets [A00009], its physical properties include a softening point of 1623 K, a density of 2.6 g/cm³, a porosity (void volume) of 0.00%, water absorption of 0.00%, and the property of being impermeable to gas. Mechanical properties of Corning Code 9606 include a strength to weight ratio (modulus of rupture to specific gravity) of 13.5×10^3 psi at 293 K, Young's modulus of 17.4×10^6 psi at 293 K, a shear modulus of 6.9×10^6 psi at 293 K, Poisson's ratio of 0.245 at 293 K, a modulus of rupture of 35×10^3 psi at 293 K, a Knoop hardness of 619 kg/mm² with a 500 gram load, and a Knoop hardness of 698 kg/mm² with a 100 gram load. Thermal properties include a coefficient of linear expansion of $57 \times 10^{-7} \text{ C}^{-1}$ over a temperature range of 293 to 593 K, a mean thermal conductivity of $0.034 \text{ W cm}^{-1} \text{ C}^{-1}$ over a temperature range of 293 to 1093 K, a mean thermal diffusivity of $0.0127 \text{ cm}^2 \text{ s}^{-1}$ over a temperature range of 293 to 1093 K, and a

mean specific heat of $0.233 \text{ cal g}^{-1} \text{ C}^{-1}$ over the temperature range of 298 to 673 K. Electrical properties include a loss factor of 0.8% at 293 K and a dielectric strength of 350 volts rms mil⁻¹ at 293 K and 60 cps.

a. Normal Spectral Emittance (Wavelength Dependence)

There are four sets of experimental data available for the wavelength dependence of the normal spectral emittance of Corning 9606 as listed in Table 10-2 and shown in Figure 10-1. Specimen characterization and measurement information for the data are given in Table 10-1.

The data for Corning 9606 covers a temperature range of 813 to 1403 K. Four sets of experimental also are available for another kind of Pyroceram known as Corning 9608 which shows the same general trend as Corning 9606, but the values are different enough that using data of Corning 9608 to help in generating evaluated data for Corning 9606 is not justified.

It is noted that the data for Corning 9606 are widely separated and, therefore, there is not enough factual evidence to justify giving evaluated values.

The lines in Figure 10-1 connecting the data points are not meant to imply that they represent a smooth curve. The data for all eight curves in Figure 10-1 and Tables 10-1 and 10-2 were extracted from tabular data. A smooth curve should not be drawn through the data points because of the widely spaced nature of the data. In addition, it is not justified to generate values for a plot of normal spectral emittance as a function of temperature for 3.8 and 10.6 μm .

Data for the wavelength dependence of the normal spectral emittance of Corning 9606 below 813 K and above 1403 K were not located.

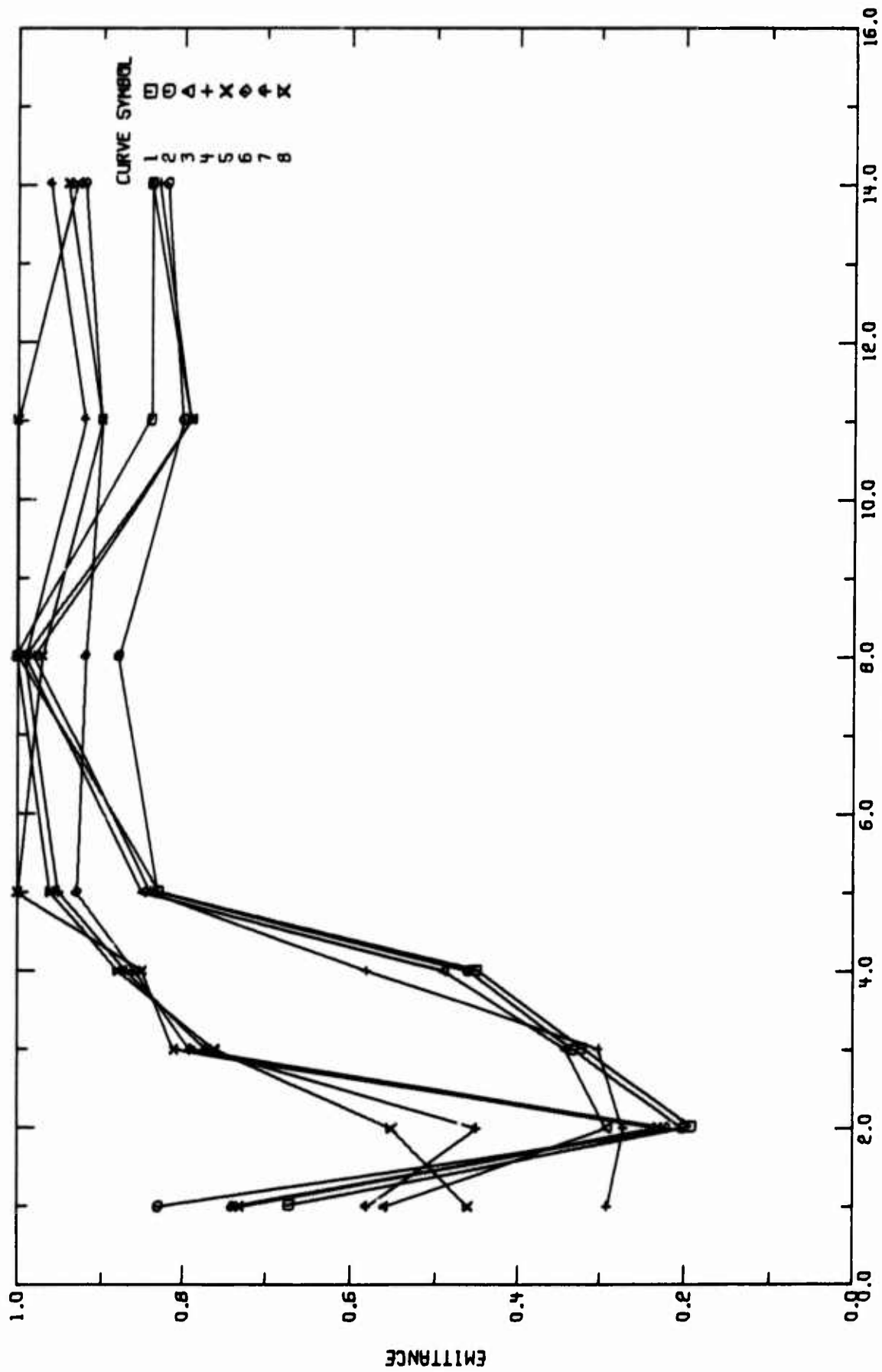


FIGURE 10-1. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE).

TABLE 10-1. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF PYROCERAM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μ m | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------|------|---------------------------|----------------------|-------------------------------|---|
| 1 T29570 | Folweiler, R. C. | 1964 | 1-14 | 813 | Corning 9606 | Method of measurement used was rotating sample method; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance measurement; $\theta \sim 0^\circ$, reported error ± 10 . |
| 2 T29570 | Folweiler, R. C. | 1964 | 1-14 | 1021 | Corning 9606 | The above specimen. |
| 3 T29570 | Folweiler, R. C. | 1964 | 1-14 | 1205 | Corning 9606 | The above specimen. |
| 4 T29570 | Folweiler, R. C. | 1964 | 1-14 | 1403 | Corning 9606 | The above specimen. |
| 5 T29570 | Folweiler, R. C. | 1964 | 1-14 | 813 | Corning 9608 | Method of measurement used was rotating sample method; rotating specimen in furnace used in conjunction with Baird-Atomic infrared spectrometer, model NK-1A, for emittance measurement; value reported at 5μ of 1.04 obviously in error, it cannot be greater than 1.0; $\theta \sim 0^\circ$, reported error ± 10 . |
| 6 T29570 | Folweiler, R. C. | 1964 | 1-14 | 1018 | Corning 9608 | The above specimen. |
| 7 T29570 | Folweiler, R. C. | 1964 | 1-14 | 1205 | Corning 9608 | The above specimen. |
| 8 T29570 | Folweiler, R. C. | 1964 | 1-14 | 1405 | Corning 9608 | The above specimen except value reported at 11μ of 1.04 obviously in error, it cannot be greater than 1.0. |

TABLE 10-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | |
|----------------------|------------|----------------------|------------|----------------------|------------|------|
| CURVE 1 T = 813. | | | | | | |
| 1. | 0.67 | 4. | 0.58 | 14. | 0.96 | |
| 2. | 0.19 | 5. | 0.64 | CURVE 8 T = 1405. | | |
| 3. | 0.32 | 8. | 0.98 | 1. | 0.46 | |
| 4. | 0.45 | 11. | 0.79 | 2. | 0.55 | |
| 5. | 0.83 | 14. | 0.83 | 3. | 0.76 | |
| 8. | 1.00 | CURVE 5 T = 813. | | 4. | 0.88 | |
| 11. | 0.34 | 1. | 0.73 | 5. | 0.96 | |
| 14. | 0.84 | 2. | 0.23 | 8. | 1.00 | |
| CURVE 2 T = 1021. | | | | | | |
| 1. | 0.83 | 3. | 0.81 | 11. | 1.0 | |
| 2. | 0.20 | 4. | 0.85 | 14. | 0.93 | |
| 3. | 0.33 | 5. | 1.0 | CURVE 6 T = 1018. | | |
| 4. | 0.46 | 8. | 0.97 | 1. | 0.74 | |
| 5. | 0.83 | 11. | 0.90 | 2. | 0.22 | |
| 8. | 0.88 | 14. | 0.94 | 3. | 0.79 | |
| 11. | 0.90 | CURVE 3 T = 1205. | | 4. | 0.66 | |
| 14. | 0.82 | 1. | 0.50 | 5. | 0.93 | |
| CURVE 3 T = 1205. | | | | | | |
| 2. | 0.29 | 8. | 0.92 | CURVE 7 T = 1205. | | |
| 3. | 0.34 | 11. | 0.90 | 1. | 0.58 | |
| 4. | 0.49 | 14. | 0.92 | 2. | 0.45 | |
| 5. | 0.85 | CURVE 4 T = 1403. | | 3. | 0.77 | |
| 8. | 0.99 | 1. | 0.29 | 4. | 0.67 | |
| 11. | 0.79 | 2. | 0.27 | 5. | 0.95 | |
| 14. | 0.84 | 3. | 0.30 | 8. | 0.99 | |
| CURVE 4 T = 1403. | | | | | | |
| 1. | 0.29 | 11. | | | | 0.92 |
| 2. | 0.27 | | | | | |
| 3. | 0.30 | | | | | |

b. Normal Spectral Emittance (Temperature Dependence)

There is one set of experimental data available for the temperature dependence of the normal spectral emittance of Corning 9606 as well as three sets for Corning 9608. These data sets are tabulated in Table 10-4 and shown graphically in Figure 10-2. The specimen characterization and measurement information are given in Table 10-3.

The one data set for Corning 9606 covers a temperature range of 1191 to 1456 K and for a wavelength of $0.665 \mu\text{m}$. Because of the lack of data at 3.8 and $10.6 \mu\text{m}$, no evaluated values can be given.

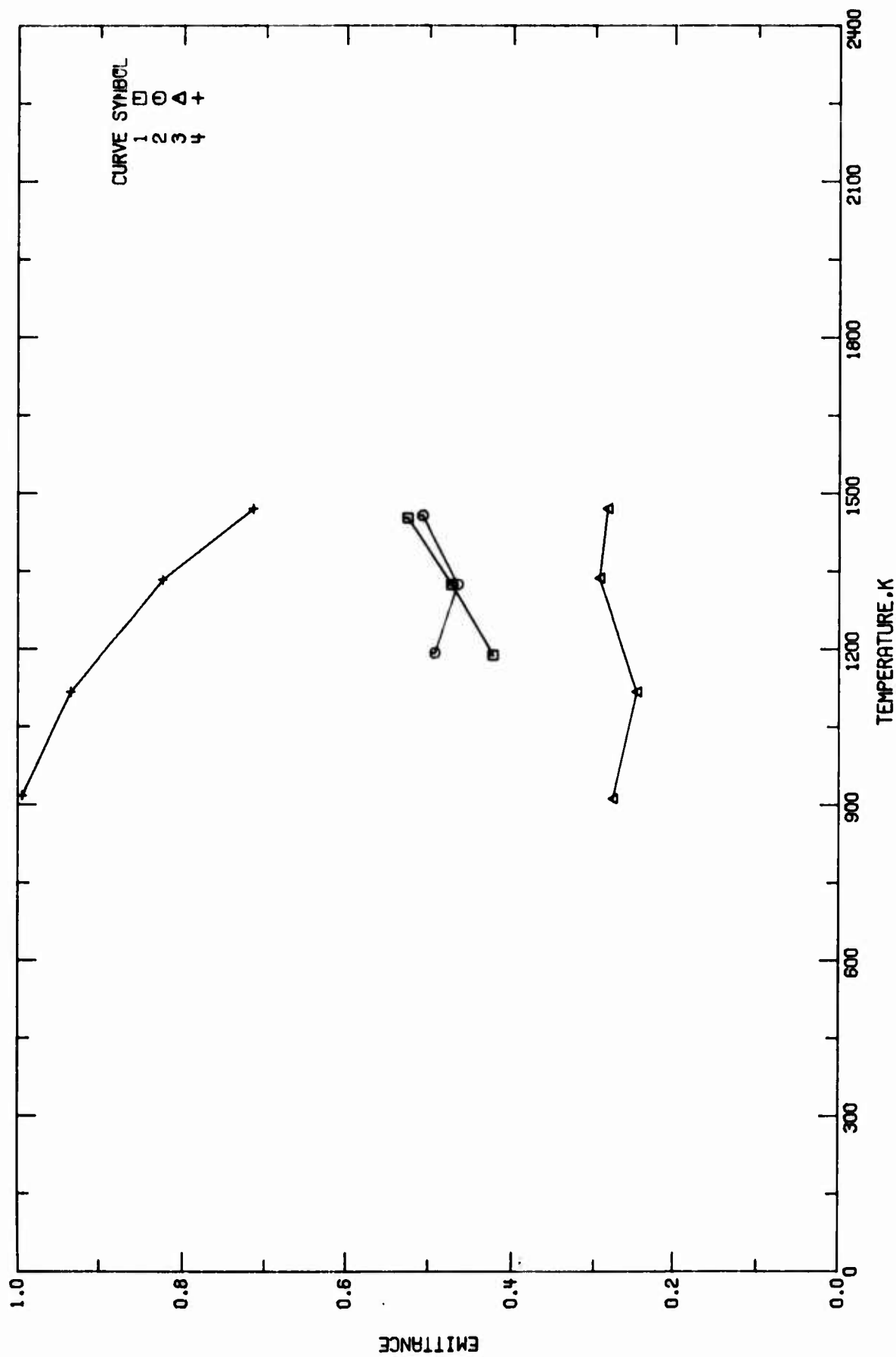


FIGURE 10-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (TEMPERATURE DEPENDENCE).

TABLE 10-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF PYROCERAM (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1191-1456 | Pyroceram 9606 | Data from figure; $\theta'=0^\circ$. |
| 2 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1195-1460 | Pyroceram 9608 | Data from figure; $\theta'=0^\circ$. |
| 3 T18630 | Blair, G.R. | 1960 | 0.640 | | Corning body 9608 | Ground to size, ultrasonically cleaned, surface polished with 1-5 μm diamond polishing compound until normally mat surface began to reflect light, cleaned, polished with cloth charged with a paste of cerium oxide and Kerosene; measured in vacuum; data from figure; emissivity reported; $\theta'=0^\circ$, reported error $\sim 10\%$. |
| 4 T18630 | Blair, G.R. | 1960 | 1 | | Corning body 9608 | The above specimen. |

TABLE 10-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF PYROCERAM (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ |
|-------------------|------------|
| CURVE 1 | |
| $\lambda = 0.665$ | |
| 1191. | 0.423 |
| 1327. | 0.472 |
| 1456. | 0.525 |
| CURVE 2 | |
| $\lambda = 0.665$ | |
| 1195. | 0.492 |
| 1327. | 0.465 |
| 1459. | 0.507 |
| CURVE 3 | |
| $\lambda = 0.640$ | |
| 913. | 0.277 |
| 1119. | 0.247 |
| 1339. | 0.294 |
| 1473. | 0.284 |
| CURVE 4 | |
| $\lambda = 1.$ | |
| 919. | 0.993 |
| 1119. | 0.934 |
| 1336. | 0.824 |
| 1473. | 0.714 |

c. Normal Spectral Reflectance (Wavelength Dependence)

There is one set of experimental data applicable to Corning 9606 and one to Corning 9608 for the wavelength dependence of normal spectral reflectance as listed in Table 10-7 and shown in Figures 10-3 and 10-4. Specimen characterization and measurement information for the data are given in Table 10-6. The data obtained by Olson and Morris [T10060] (curve 1) is applicable only at room temperature and only covers the wavelength range of 0.30 to 2.7 μm . Confirmatory data for Corning 9606 over this wavelength range is lacking and no data has been found in the wavelength range of 2.7 to 15 μm . In addition, no data was located above room temperature for any portion of the wavelength range of interest.

Provisional values for Corning 9606 are listed in Table 10-5 and shown in Figure 10-3. The structure was kept at 1.36 and 1.78 μm because Corning 9608 also shows this structure which indicates the structure is characteristic of the Pyroceram class of materials.

The context within which this set of provisional values is valid is the following: (1) they hold for room temperature, 293 K, (2) the geometrical conditions are that incidence is for near normal, specifically $\theta = 9^\circ$, while the viewed conditions are over a hemisphere, i. e., 2π , and (3) the wavelength range covered is from 0.3 to 2.7 μm . The estimate of the uncertainty is that for wavelengths between 0.35 and 2.7 μm it is thought to be of the order of 10% and for wavelengths less than 0.35 μm it would be larger in percentage value.

TABLE 10-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (CORNING 9606) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|-----------------|--------|-----------|--------|
| T = 293 (CONT.) | | | |
| 0.297 | 0.062 | 2.1 | 0.939 |
| 0.310 | 0.142 | 2.12 | 0.938 |
| 0.339 | 0.224 | 2.2 | 0.933 |
| 0.446 | 0.529 | 2.32 | 0.925 |
| 0.480 | 0.582 | 2.3 | 0.926 |
| 0.5 | 0.588 | 2.39 | 0.919 |
| 0.516 | 0.593 | 2.4 | 0.915 |
| 0.6 | 0.612 | 2.45 | 0.890 |
| 0.639 | 0.619 | 2.5 | 0.862 |
| 0.7 | 0.638 | 2.51 | 0.852 |
| 0.710 | 0.642 | 2.59 | 0.819 |
| 0.795 | 0.706 | 2.6 | 0.817 |
| 0.8 | 0.706 | 2.68 | 0.791 |
| 0.9 | 0.770 | 2.7 | 0.786 |
| 0.952 | 0.800 | 2.72 | 0.780 |
| 1.0 | 0.817 | | |
| 1.05 | 0.835 | | |
| 1.1 | 0.844 | | |
| 1.16 | 0.852 | | |
| 1.2 | 0.854 | | |
| 1.21 | 0.854 | | |
| 1.28 | 0.854 | | |
| 1.3 | 0.853 | | |
| 1.35 | 0.850 | | |
| 1.4 | 0.853 | | |
| 1.41 | 0.855 | | |
| 1.49 | 0.869 | | |
| 1.5 | 0.896 | | |
| 1.58 | 0.919 | | |
| 1.6 | 0.917 | | |
| 1.64 | 0.912 | | |
| 1.7 | 0.899 | | |
| 1.77 | 0.891 | | |
| 1.8 | 0.894 | | |
| 1.83 | 0.900 | | |
| 1.9 | 0.923 | | |
| 1.94 | 0.934 | | |
| 1.99 | 0.944 | | |
| 2.0 | 0.944 | | |

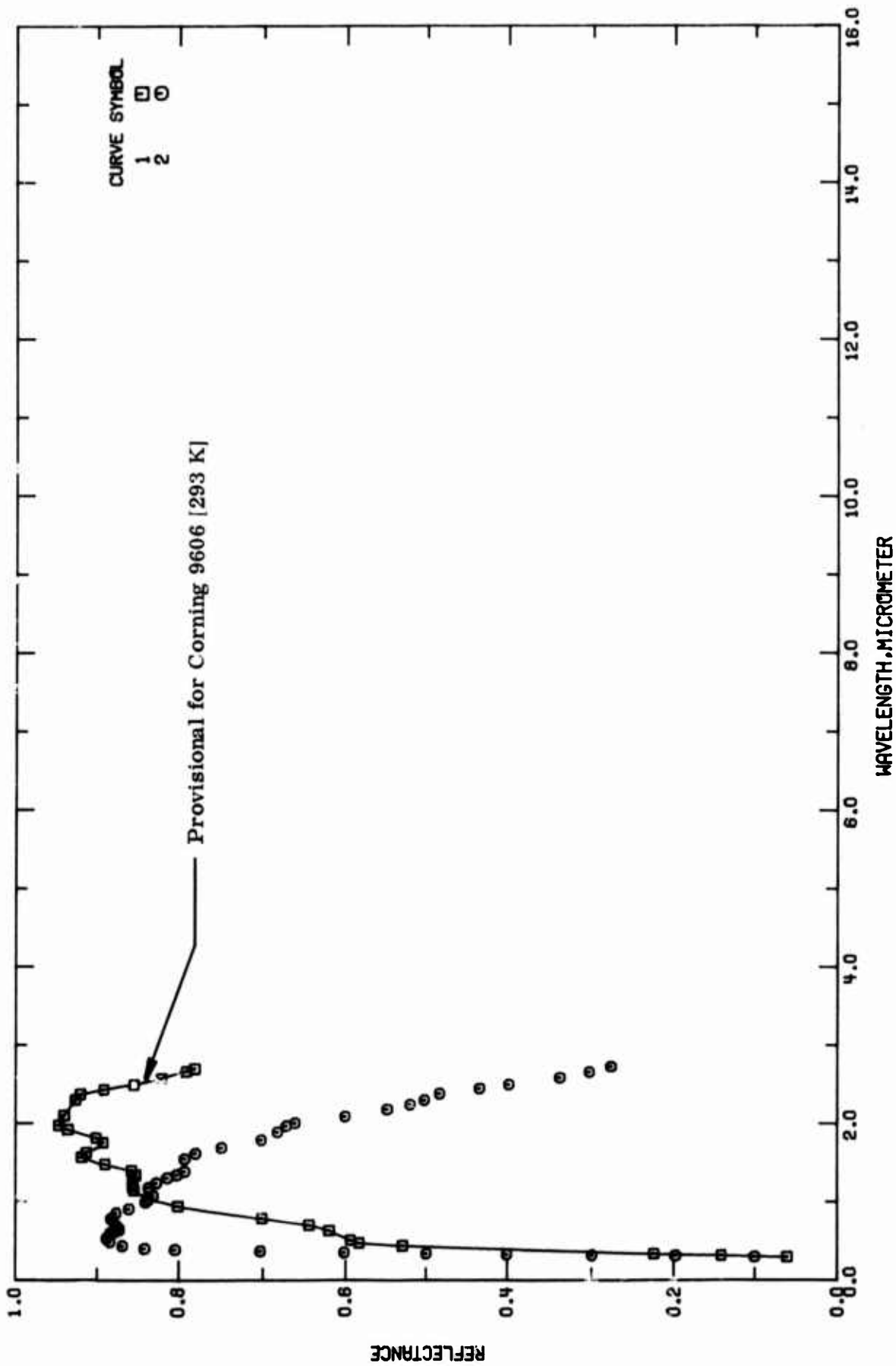


FIGURE 10-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE).

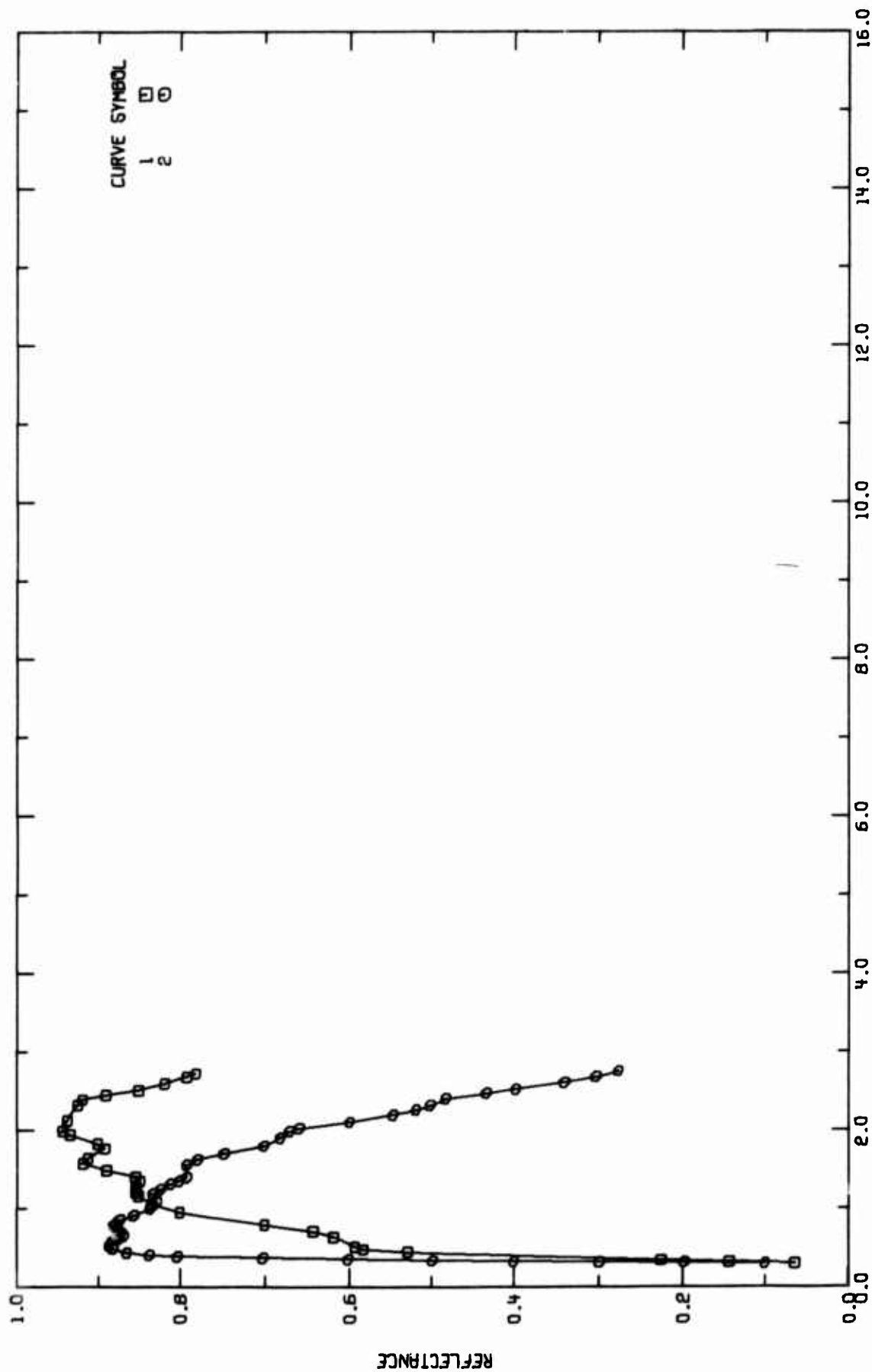


FIGURE 10-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE).

TABLE 10-6. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T110060 | Olson, O.H. and Morris, J.C. | 1959 | 0.30-2.7 | 293 | Pyroceram 9606 | Integrating sphere reflectometer used; reflectance factor measured then values converted to absolute reflectance values; working standard magnesium carbonate surface; smooth values from figure; temperature presumed to be room temperature, 293 K assigned; $\theta=9^\circ$, $\omega'=2\pi$; reported error 4%. |
| 2 T110060 | Olson, O.H. and Morris, J.C. | 1959 | 0.30-2.7 | 293 | Pyroceram 9608 | Integrating sphere reflectometer used; reflectance factor measured then values converted to absolute reflectance values; working standard magnesium carbonate surface; smooth values from figure; temperature presumed to be room temperature, 293 K assigned; $\theta=9^\circ$, $\omega'=2\pi$; reported error 4%. |

TABLE 10-7. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|-----------|--------|-----------|--------|
| CURVE 1 | | | |
| T = 293. | | | |
| 0.297 | 0.062 | 0.338 | 0.499 |
| 0.318 | 0.142 | 0.355 | 0.661 |
| 0.339 | 0.224 | 0.372 | 0.702 |
| 0.446 | 0.529 | 0.391 | 0.693 |
| 0.480 | 0.552 | 0.407 | 0.639 |
| 0.516 | 0.593 | 0.440 | 0.865 |
| 0.639 | 0.619 | 0.493 | 0.652 |
| 0.710 | 0.642 | 0.534 | 0.697 |
| 0.755 | 0.700 | 0.603 | 0.882 |
| 0.952 | 0.800 | 0.628 | 0.875 |
| 1.05 | 0.855 | 0.652 | 0.670 |
| 1.15 | 0.852 | 0.696 | 0.673 |
| 1.21 | 0.854 | 0.755 | 0.678 |
| 1.28 | 0.854 | 0.792 | 0.681 |
| 1.35 | 0.850 | 0.861 | 0.874 |
| 1.41 | 0.855 | 0.915 | 0.658 |
| 1.49 | 0.869 | 1.001 | 0.838 |
| 1.58 | 0.918 | 1.085 | 0.829 |
| 1.64 | 0.912 | 1.139 | 0.934 |
| 1.77 | 0.891 | 1.246 | 0.825 |
| 1.83 | 0.900 | 1.312 | 0.812 |
| 1.94 | 0.934 | 1.352 | 0.601 |
| 1.99 | 0.944 | 1.397 | 0.792 |
| 2.12 | 0.938 | 1.557 | 0.792 |
| 2.32 | 0.925 | 1.625 | 0.779 |
| 2.39 | 0.919 | 1.700 | 0.745 |
| 2.45 | 0.890 | 1.798 | 0.761 |
| 2.51 | 0.852 | 1.900 | 0.681 |
| 2.59 | 0.819 | 1.981 | 0.570 |
| 2.68 | 0.791 | 2.017 | 0.659 |
| 2.72 | 0.780 | 2.099 | 0.600 |
| | | 2.191 | 0.547 |
| | | 2.251 | 0.520 |
| | | 2.309 | 0.502 |
| | | 2.392 | 0.483 |
| | | 2.460 | 0.435 |
| | | 2.509 | 0.398 |
| | | 2.596 | 0.339 |
| | | 2.658 | 0.303 |
| | | 2.738 | 0.276 |
| CURVE 2 | | | |
| T = 293. | | | |
| 0.298 | 0.100 | | |
| 0.312 | 0.198 | | |
| 0.317 | 0.299 | | |
| 0.326 | 0.400 | | |

d. Hemispherical Spectral Transmittance (Wavelength Dependence)

There are four sets of experimental data for the wavelength dependence of the hemispherical spectral transmittance of Pyroceram with two data sets applicable to the specific material of interest here in this report, i.e., Corning 9606, and two data sets to a different Pyroceram, Corning 9608. The data for these four sets are listed in Table 10-9 and shown in Figure 10-5. Specimen characterization and measurement information for the data are given in Table 10-8.

The two sets of measurements of Folweiler [T29570] (curves 1 and 2) for Corning 9606 are both for room temperature. One set (curve 1) is for a specimen 0.005 inches thick and the second set (curve 2) is for a greater thickness of 0.016 in. As expected, the data for the greater thickness (curve 2) is less than the data for curve 1. The data for these two sets was given in tabular form and over widely spaced wavelengths. Because of this fact, no evaluated values are justified. It should further be pointed out that straight lines connecting the data points, as in Figure 10-5, are not meant to imply a smooth curve but are done that way for ease of visual presentation.

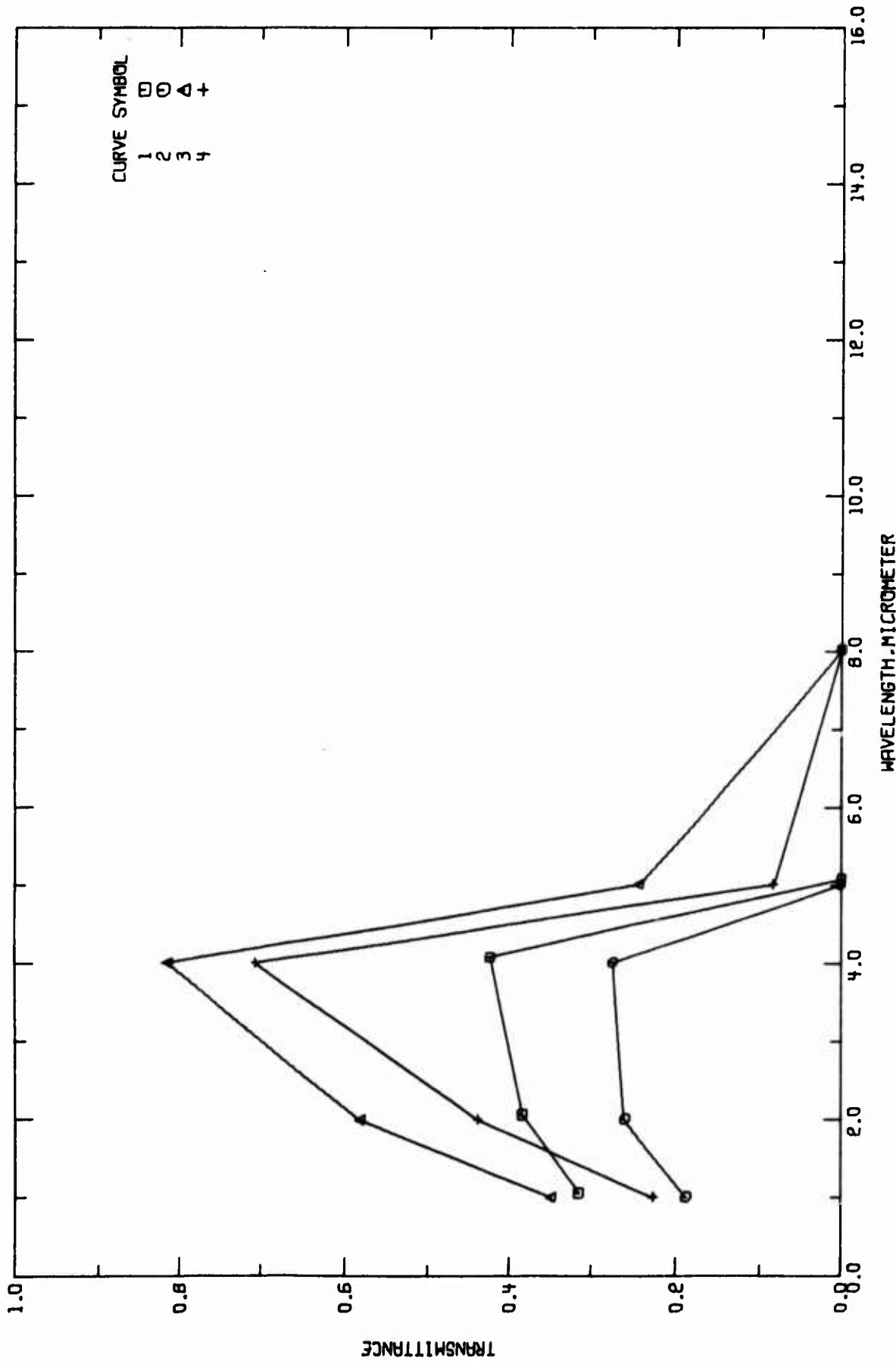


FIGURE 10-5. EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE).

TABLE 10-8. MEASUREMENT INFORMATION ON THE HEMISPHERICAL SPECTRAL TRANSMITTANCE OF PYROCERAM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Corning 9606 | Specimen 0.005 in. thick, cross-sectional dimensions 0.25 by 0.62 in., diffusing screen used in front of specimen; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\omega=2\pi$, reported error $\pm 5\%$. |
| 2 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Corning 9606 | Similar to the above specimen except specimen is 0.010 in. thick. |
| 3 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Corning 9608 | Specimen 0.008 in. thick, cross-sectional dimensions 0.25 by 0.62 in.; diffusing screen used in front of specimen; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\omega=2\pi$, reported error $\pm 5\%$. |
| 4 | T29570 Folweiler, R. C. | 1964 | 1-8 | 293 | Corning 9608 | Similar to the above specimen except specimen is 0.016 in. thick. |

TABLE 10-9. EXPERIMENTAL HEMISPHERICAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ |
|-----------|--------|
| CURVE 1 | |
| T = 293. | |
| 1. | 0.515 |
| 2. | 0.385 |
| 4. | 0.424 |
| 5. | 0.0 |
| 8. | 0.0 |
| CURVE 2 | |
| T = 293. | |
| 1. | 0.188 |
| 2. | 0.259 |
| 4. | 0.274 |
| 5. | 0.0 |
| 8. | 0.0 |
| CURVE 3 | |
| T = 293. | |
| 1. | 0.349 |
| 2. | 0.532 |
| 4. | 0.617 |
| 5. | 0.243 |
| 8. | 0.000 |
| CURVE 4 | |
| T = 293. | |
| 1. | 0.225 |
| 2. | 0.435 |
| 4. | 0.707 |
| 5. | 0.084 |
| 8. | 0.000 |

e. Normal Spectral Transmittance (Wavelength Dependence)

A total of 23 sets of experimental data were located for the wavelength dependence of the normal spectral transmittance of Pyroceram. These data sets are listed in Table 10-12 and shown in Figures 10-6 and 10-7. Specimen characterization and measurement information for the data are given in Table 10-11.

Of the 23 data sets only nine are specifically for Corning 9606 with data of eight reported by Folweiler [T29570] (curves 1-8) and data of the ninth reported by Hobbs and Folweiler [T39365], (curve 17). Data of curves 1 through 4 were given in tabular form and reported for integral wavelengths from 1 to 5 μm . On the other hand, data of curves 5-8 were given in graphical form and hence the shape of the curves is known. Curves 5-8 cover the wavelength range of 1 to 5 μm and data are reported for 293, 770, 900, and 1040 K. Data of curve 17 covers the wavelength region of 1 to 5 μm and is applicable to a temperature of 293 K.

Provisional values for 293 K and 1040 K are listed in Table 10-10 and shown in Figure 10-6 and apply to a specimen 3.18 mm thick. The values for 293 K are based on curve 5 while the values for 1040 K are based on curve 8. These values are called provisional because of the lack of much confirmatory evidence. The data of curve 17 is disregarded because the preponderance of evidence shows the transmittance reaching zero at 5 μm (curves 1 and 5 in Table 10-12 and Figure 10-7 together with curves 1 and 2 in Table 10-9 and Figure 10-5) whereas the data of curve 17 does not show this behavior. It is thought the uncertainty assigned to the two provisional curves is 20%.

TABLE 10-10. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCELFAM(CORNING 9636) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm : TEMPERATURE, T, K; TRANSMITTANCE, T)

| 3.18MM THICK | | 3.19MM THICK | | 3.1944 THICK | | 3.1844 THICK | |
|--------------|-------|--------------|-------|--------------|-------|--------------|-------|
| λ | T | λ | T | λ | T | λ | T |
| T = 293 | | | | | | | |
| 1.00 | 0.681 | 3.15 | 0.227 | 1.03 | 0.600 | 3.50 | 0.219 |
| 1.10 | 0.703 | 3.20 | 0.236 | 1.10 | 0.630 | 3.63 | 0.219 |
| 1.08 | 0.700 | 3.21 | 0.239 | 1.14 | 0.650 | 3.79 | 0.219 |
| 1.20 | 0.723 | 3.30 | 0.269 | 1.20 | 0.656 | 3.80 | 0.219 |
| 1.30 | 0.742 | 3.37 | 0.300 | 1.30 | 0.677 | 3.90 | 0.219 |
| 1.33 | 0.746 | 3.40 | 0.314 | 1.43 | 0.696 | 4.00 | 0.219 |
| 1.40 | 0.761 | 3.48 | 0.350 | 1.42 | 0.700 | 4.10 | 0.216 |
| 1.50 | 0.775 | 3.50 | 0.360 | 1.53 | 0.714 | 4.11 | 0.216 |
| 1.53 | 0.779 | 3.58 | 0.400 | 1.60 | 0.732 | 4.20 | 0.210 |
| 1.60 | 0.788 | 3.60 | 0.420 | 1.68 | 0.743 | 4.30 | 0.202 |
| 1.70 | 0.803 | 3.67 | 0.443 | 1.70 | 0.746 | 4.33 | 0.200 |
| 1.80 | 0.807 | 3.70 | 0.454 | 1.80 | 0.754 | 4.40 | 0.193 |
| 1.82 | 0.809 | 3.74 | 0.467 | 1.84 | 0.757 | 4.42 | 0.191 |
| 1.88 | 0.811 | 3.80 | 0.485 | 1.90 | 0.760 | 4.50 | 0.177 |
| 1.90 | 0.812 | 3.86 | 0.500 | 1.94 | 0.761 | 4.60 | 0.159 |
| 2.00 | 0.813 | 3.90 | 0.507 | 2.00 | 0.757 | 4.62 | 0.154 |
| 2.09 | 0.807 | 3.92 | 0.511 | 2.10 | 0.747 | 4.67 | 0.139 |
| 2.10 | 0.806 | 4.00 | 0.513 | 2.16 | 0.740 | 4.70 | 0.134 |
| 2.20 | 0.796 | 4.10 | 0.514 | 2.20 | 0.730 | 4.73 | 0.125 |
| 2.21 | 0.794 | 4.19 | 0.500 | 2.30 | 0.704 | 4.78 | 0.100 |
| 2.23 | 0.778 | 4.20 | 0.499 | 2.31 | 0.700 | 4.80 | 0.094 |
| 2.30 | 0.774 | 4.30 | 0.481 | 2.40 | 0.656 | 4.86 | 0.080 |
| 2.31 | 0.759 | 4.39 | 0.457 | 2.44 | 0.641 | 4.90 | 0.064 |
| 2.40 | 0.744 | 4.40 | 0.452 | 2.50 | 0.600 | 4.91 | 0.060 |
| 2.43 | 0.734 | 4.46 | 0.423 | 2.55 | 0.546 | 4.95 | 0.040 |
| 2.50 | 0.703 | 4.50 | 0.408 | 2.60 | 0.510 | 4.96 | 0.026 |
| 2.54 | 0.692 | 4.52 | 0.400 | 2.61 | 0.500 | 4.98 | 0.026 |
| 2.60 | 0.638 | 4.60 | 0.355 | 2.66 | 0.444 | 5.00 | 0.000 |
| 2.64 | 0.600 | 4.62 | 0.343 | 2.70 | 0.400 | | |
| 2.70 | 0.538 | 4.69 | 0.300 | 2.80 | 0.300 | | |
| 2.73 | 0.500 | 4.70 | 0.292 | 2.86 | 0.262 | | |
| 2.80 | 0.400 | 4.77 | 0.241 | 2.90 | 0.244 | | |
| 2.90 | 0.266 | 4.80 | 0.214 | 2.93 | 0.236 | | |
| 2.86 | 0.300 | 4.82 | 0.206 | 3.00 | 0.222 | | |
| 2.91 | 0.255 | 4.87 | 0.142 | 3.08 | 0.219 | | |
| 2.95 | 0.236 | 4.90 | 0.116 | 3.10 | 0.219 | | |
| 3.00 | 0.228 | 4.92 | 0.100 | 3.20 | 0.219 | | |
| 3.07 | 0.223 | 4.96 | 0.045 | 3.30 | 0.219 | | |
| 3.10 | 0.224 | 5.00 | 0.000 | 3.40 | 0.219 | | |

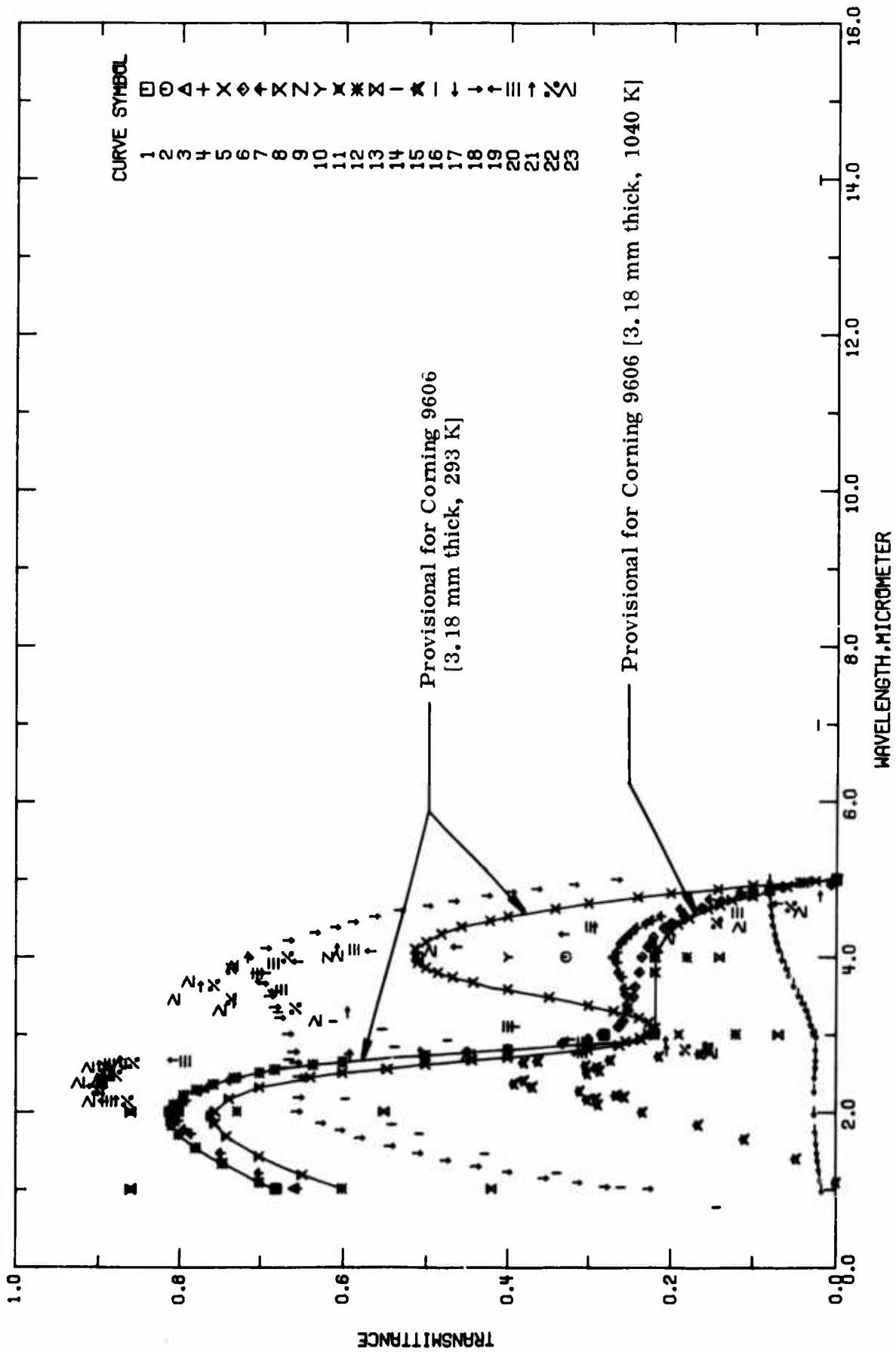


FIGURE 10-6. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE).

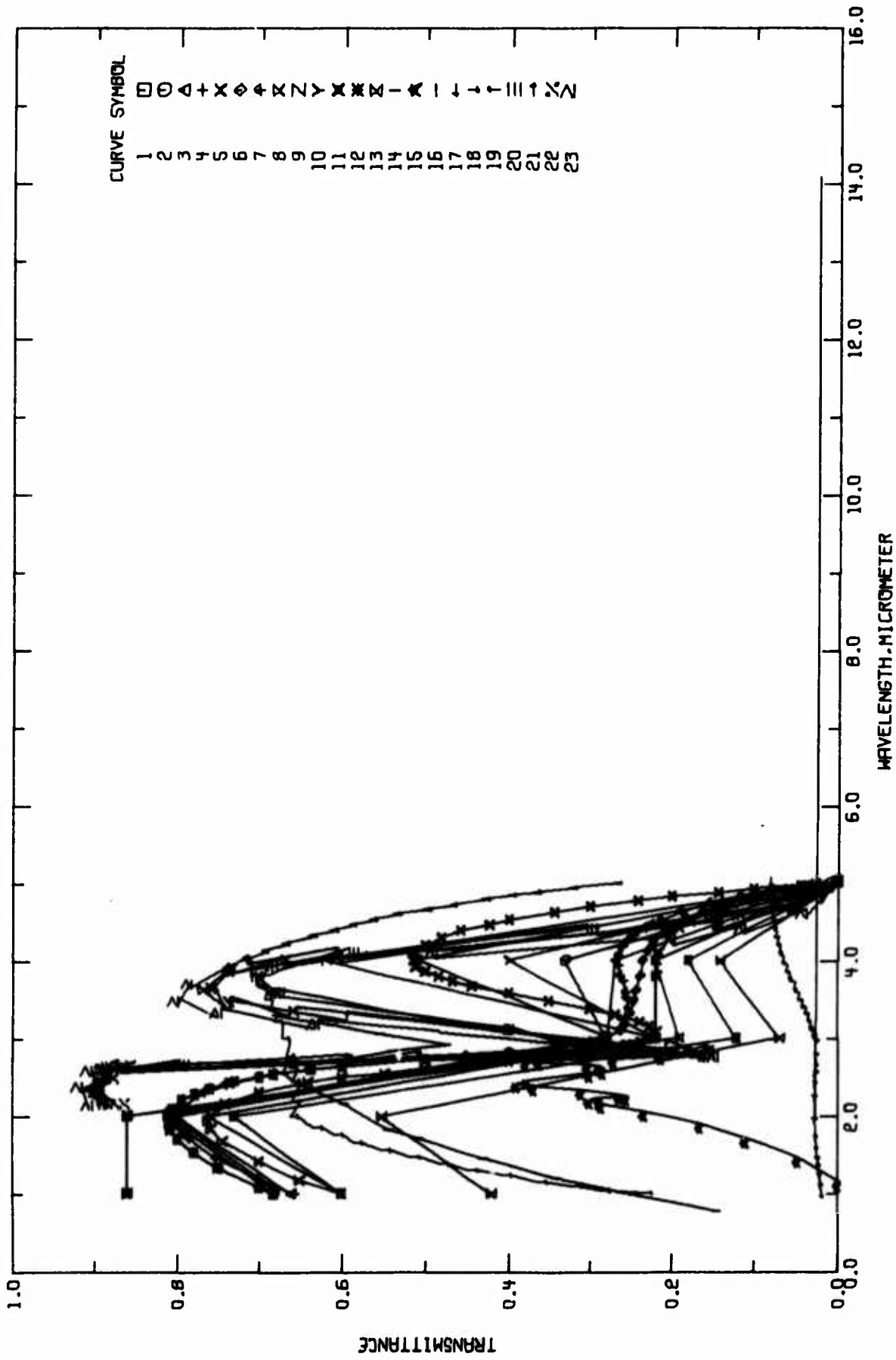


FIGURE 10-7. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE).

TABLE 10-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T29570 | Folweiler, R.C. | 1964 | 1-5 | 293 | Pyroceram Glass 9606 | Specimen dimensions 0.125 by 0.5 by 1.5 in.; $\theta=0^\circ$, $\theta'=0^\circ$; reported error $\pm 5\%$. |
| 2 T29570 | Folweiler, R.C. | 1964 | 1-5 | 770 | Pyroceram Glass 9606 | The above specimen. |
| 3 T29570 | Folweiler, R.C. | 1964 | 1-5 | 900 | Pyroceram Glass 9606 | The above specimen. |
| 4 T29570 | Folweiler, R.C. | 1964 | 1-5 | 1040 | Pyroceram Glass 9606 | The above specimen. |
| 5 T29570 | Folweiler, R.C. | 1964 | 1-5 | 293 | Pyroceram Glass 9606 | Similar to the above specimen except measurement temperature specified as room temperature, 293 K assigned, author reports transmissivity, uncorrected for surface reflectance, and data from figure. |
| 6 T29570 | Folweiler, R.C. | 1964 | 1-5 | 770 | Pyroceram Glass 9606 | The above specimen. |
| 7 T29570 | Folweiler, R.C. | 1964 | 1-5 | 900 | Pyroceram Glass 9606 | The above specimen. |
| 8 T29570 | Folweiler, R.C. | 1964 | 1-5 | 1040 | Pyroceram Glass 9606 | The above specimen. |
| 9 T29570 | Folweiler, R.C. | 1964 | 1-5 | 293 | Corning 9608 | Specimen dimensions 0.125 by 0.5 by 1.5 in.; uncorrected for surface reflectance; measurement temperature specified as room temperature, 293 K assigned; data from figure; $\theta=0^\circ$, $\theta'=0^\circ$; reported error $\pm 5\%$. |
| 10 T29570 | Folweiler, R.C. | 1964 | 1-5 | 784 | Corning 9608 | The above specimen. |
| 11 T29570 | Folweiler, R.C. | 1964 | 1-5 | 919 | Corning 9608 | The above specimen. |
| 12 T29570 | Folweiler, R.C. | 1964 | 1-5 | 1070 | Corning 9608 | The above specimen. |
| 13 T29570 | Folweiler, R.C. | 1964 | 1-5 | 1182 | Corning 9608 | The above specimen. |
| 14 T31344 | Kroeckel, O. | 1964 | 0.77-3.3 | 293 | Pyroceramic Material | Contains crystallites of about 0.5 μm diameter; little change in curve noted at 1173 K; smooth values from figure; reported error 3.5%. |
| 15 T10360 | Ginza, O.H. and Morris, J.C. | 1959 | 1.1-2.8 | 293 | Pyroceram 9608 | Integrating sphere reflectometer adopted for diffuse transmission measurements; smooth values from figure; $\theta=0^\circ$, $\theta'=0^\circ$, $\omega^2=2\alpha$. |
| 16 T20771 | Finkelstein, I.S. | 1958 | 2-16 | 295 | Pyroceram | Smooth values from figure; $\theta=0^\circ$, $\theta'=0^\circ$, $\omega^2=1.5/\omega^2$. |
| 17 T39365 | Hobbs, H.A. and Folweiler, R.C. | 1966 | 1.0-5.0 | 293 | Pyroceram 9606 | Fully dense, no porosity; grain size optically indeterminate; thickness presumably 0.0152 cm (0.006 in.); author reports measured transmissivity; data from figure and smooth curve; $\theta=0^\circ$, $\theta'=0^\circ$, $\omega^2=15/4\pi$. |
| 18 T39365 | Hobbs, H.A. and Folweiler, R.C. | 1966 | 1.0-5.0 | 293 | Pyroceram 9608 | Fully dense, no porosity; grain size optically indeterminate; thickness presumably 0.0152 cm (0.006 in.); author reports measured transmissivity; data from figure and smooth curve; $\theta=0^\circ$, $\theta'=0^\circ$, $\omega^2=15/4\pi$. |
| 19 T39377 | Troitski, O.A. and Shmurak, S.Z. | 1965 | 2.1-5.0 | 293 | Pyroceram | 62 SiO ₂ , 29 Al ₂ O ₃ , 6.5 Li ₂ O, and additives containing TiO ₂ as a catalyst; vitreous structure; specimen 1.5 mm thick and 25 x 25 cm; ground and polished to obtain plane-parallel sides; measurements made on a UR-10 spectrophotometer with a precision of $\pm 10 \text{ cm}^{-1}$; smooth values from figure of infrared absorption spectra; measurement temperature not given explicitly, assumed to be 293 K; data taken to mean normal spectral transmittance; $\theta=0^\circ$. |

TABLE 10-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 20 T40977 | Troitskii, O. A. and Shmurak, S. Z. | 1966 | 2.1-5.0 | 293 | Pyroceram | Similar to the above specimen except heated at 923 K for 10 hr. |
| 21 T40977 | Troitskii, O. A. and Shmurak, S. Z. | 1966 | 2.1-5.0 | 293 | Pyroceram | Similar to the above specimen except heated at 923 K for 10 hr and then heated at 1053 K for 0.5 hr; crystalline structure. |
| 22 T40977 | Troitskii, O. A. and Shmurak, S. Z. | 1966 | 2.1-5.0 | 293 | Pyroceram | Similar to the above specimen except heated at 923 K for 10 hr and then heated at 1053 K for 1 hr; crystalline structure. |
| 23 T40977 | Troitskii, O. A. and Shmurak, S. Z. | 1966 | 2.1-5.0 | 293 | Pyroceram | Similar to the above specimen except heated at 923 K for 10 hr and then heated at 1053 K for 7 hr; crystalline structure. |

TABLE 10-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| CURVE 1 T = 293. | λ | T | CURVE 5 (CONT.) | λ | T | CURVE 6 (CONT.) | λ | T | CURVE 7 (CONT.) | λ | T | CURVE 8 (CONT.) | λ | T | CURVE 9 T = 293. | λ | T | CURVE 10 T = 784. | |
|----------------------|-----------|-------|---------------------|---------------------|-------|-----------------|-----------|-------|-----------------|-----------|----------------------|-----------------|-----------|---|---------------------|-----------|---|----------------------|--|
| | 1.53 | 0.779 | 0.69 | 4.00 | 0.235 | 4.00 | 4.00 | 0.235 | 2.88 | 0.334 | 2.50 | 0.600 | | | | | | | |
| | 1.70 | 0.600 | 0.77 | 4.13 | 0.229 | 4.13 | 4.13 | 0.229 | 2.94 | 0.300 | 2.55 | 0.546 | | | | | | | |
| 1. | 0.55 | | 0.82 | 4.19 | 0.224 | 4.19 | 4.19 | 0.224 | 3.00 | 0.263 | 2.61 | 0.500 | | | | | | | |
| 2. | 0.81 | | 0.87 | 4.25 | 0.222 | 4.25 | 4.25 | 0.222 | 3.10 | 0.263 | 2.66 | 0.444 | | | | | | | |
| 3. | 0.28 | | 0.92 | 4.37 | 0.209 | 4.37 | 4.37 | 0.209 | 3.17 | 0.258 | 2.70 | 0.400 | | | | | | | |
| 4. | 0.51 | | 0.96 | 4.43 | 0.200 | 4.43 | 4.43 | 0.200 | 3.31 | 0.252 | 2.80 | 0.300 | | | | | | | |
| 5. | 0.0 | | 0.000 | 4.54 | 0.184 | 4.54 | 4.54 | 0.184 | 3.38 | 0.253 | 2.86 | 0.262 | | | | | | | |
| | 2.21 | 0.794 | 0.773 | 4.63 | 0.162 | 4.63 | 4.63 | 0.162 | 3.52 | 0.255 | 2.93 | 0.236 | | | | | | | |
| CURVE 2 T = 770. | 2.28 | 0.773 | CURVE 6 T = 770. | | | | | | | | | | | | | | | | |
| | 2.35 | 0.759 | 0.759 | 4.72 | 0.133 | 4.72 | 4.72 | 0.133 | 3.59 | 0.256 | 3.00 | 0.222 | | | | | | | |
| | 2.43 | 0.734 | 0.734 | 4.81 | 0.115 | 4.81 | 4.81 | 0.115 | 3.74 | 0.259 | 3.08 | 0.219 | | | | | | | |
| | 2.50 | 0.700 | 0.700 | 4.85 | 0.100 | 4.85 | 4.85 | 0.100 | 3.80 | 0.253 | 3.80 | 0.219 | | | | | | | |
| 1. | 0.68 | | 0.681 | 4.90 | 0.081 | 4.90 | 4.90 | 0.081 | 3.93 | 0.265 | 4.00 | 0.219 | | | | | | | |
| 2. | 0.81 | | 0.700 | 4.93 | 0.065 | 4.93 | 4.93 | 0.065 | 4.06 | 0.265 | 4.11 | 0.216 | | | | | | | |
| 3. | 0.28 | | 0.638 | 5.00 | 0.000 | 5.00 | 5.00 | 0.000 | 4.24 | 0.255 | 4.33 | 0.200 | | | | | | | |
| 4. | 0.33 | | 0.748 | CURVE 7 T = 900. | | | | | | | | | | | | | | | |
| 5. | 0.0 | | 0.775 | 1.00 | 0.656 | 1.00 | 1.00 | 0.656 | 4.52 | 0.212 | 4.78 | 0.190 | | | | | | | |
| | 2.80 | 0.400 | 0.800 | 1.20 | 0.700 | 1.20 | 1.20 | 0.700 | 4.62 | 0.186 | 4.86 | 0.080 | | | | | | | |
| CURVE 3 T = 900. | 2.86 | 0.300 | 0.809 | 1.46 | 0.750 | 1.46 | 1.46 | 0.750 | 4.74 | 0.152 | 4.91 | 0.060 | | | | | | | |
| | 2.91 | 0.255 | 0.811 | 1.71 | 0.784 | 1.71 | 1.71 | 0.784 | 4.83 | 0.114 | 4.96 | 0.040 | | | | | | | |
| | 2.95 | 0.238 | 0.813 | 1.77 | 0.792 | 1.77 | 1.77 | 0.792 | 4.91 | 0.078 | 4.93 | 0.026 | | | | | | | |
| | 3.00 | 0.228 | 0.807 | 1.89 | 0.800 | 1.89 | 1.89 | 0.800 | 4.93 | 0.067 | 5.00 | 0.000 | | | | | | | |
| 1. | 0.66 | | 0.800 | 1.94 | 0.804 | 1.94 | 1.94 | 0.804 | 5.00 | 0.000 | CURVE 8 T = 1040. | | | | | | | | |
| 2. | 0.80 | | 0.809 | 2.00 | 0.801 | 2.00 | 2.00 | 0.801 | | | | | | | | | | | |
| 3. | 0.28 | | 0.794 | 2.09 | 0.795 | 2.09 | 2.09 | 0.795 | | | | | | | | | | | |
| 4. | 0.27 | | 0.776 | 2.14 | 0.790 | 2.14 | 2.14 | 0.790 | | | | | | | | | | | |
| 5. | 0.0 | | 0.755 | 2.30 | 0.765 | 2.30 | 2.30 | 0.765 | | | | | | | | | | | |
| | 3.30 | 0.269 | 0.734 | 2.40 | 0.739 | 2.40 | 2.40 | 0.739 | 1.00 | 0.600 | 1.18 | 0.66 | | | | | | | |
| CURVE 4 T = 1040. | 3.37 | 0.300 | 0.700 | 2.44 | 0.726 | 2.44 | 2.44 | 0.726 | 1.42 | 0.700 | 1.68 | 0.52 | | | | | | | |
| | 3.48 | 0.350 | 0.692 | 2.50 | 0.700 | 2.50 | 2.50 | 0.700 | 1.68 | 0.743 | 1.84 | 0.0 | | | | | | | |
| | 3.58 | 0.400 | 0.638 | 2.54 | 0.682 | 2.54 | 2.54 | 0.682 | 1.84 | 0.757 | CURVE 9 T = 293. | | | | | | | | |
| | 3.67 | 0.443 | 0.600 | 2.60 | 0.601 | 2.60 | 2.60 | 0.601 | 1.94 | 0.761 | | | | | | | | | |
| | 3.74 | 0.485 | 0.600 | 2.64 | 0.600 | 2.64 | 2.64 | 0.600 | 2.00 | 0.757 | | | | | | | | | |
| 1. | 0.60 | | 0.500 | 2.73 | 0.500 | 2.73 | 2.73 | 0.500 | 2.16 | 0.740 | | | | | | | | | |
| 2. | 0.76 | | 0.450 | 2.77 | 0.450 | 2.77 | 2.77 | 0.450 | 2.31 | 0.641 | | | | | | | | | |
| 3. | 0.22 | | 0.400 | 2.81 | 0.400 | 2.81 | 2.81 | 0.400 | 2.44 | 0.600 | | | | | | | | | |
| 4. | 0.22 | | 0.334 | 2.88 | 0.334 | 2.88 | 2.88 | 0.334 | 2.50 | 0.550 | | | | | | | | | |
| 5. | 0.0 | | 0.300 | 2.94 | 0.300 | 2.94 | 2.94 | 0.300 | 2.54 | 0.562 | | | | | | | | | |
| | 4.00 | 0.514 | 0.283 | 3.00 | 0.283 | 3.00 | 3.00 | 0.283 | 2.58 | 0.639 | | | | | | | | | |
| CURVE 5 T = 293. | 4.19 | 0.514 | 0.263 | 3.10 | 0.263 | 3.10 | 3.10 | 0.263 | 2.64 | 0.600 | | | | | | | | | |
| | 4.30 | 0.481 | 0.258 | 3.17 | 0.258 | 3.17 | 3.17 | 0.258 | 2.73 | 0.550 | | | | | | | | | |
| | 4.39 | 0.457 | 0.252 | 3.31 | 0.252 | 3.31 | 3.31 | 0.252 | 2.77 | 0.450 | | | | | | | | | |
| | 4.46 | 0.423 | 0.246 | 3.48 | 0.246 | 3.48 | 3.48 | 0.246 | 2.81 | 0.400 | | | | | | | | | |
| 1.00 | 0.681 | | 0.244 | 3.61 | 0.244 | 3.61 | 3.61 | 0.244 | 2.86 | 0.343 | | | | | | | | | |
| 1.08 | 0.700 | | 0.239 | 3.80 | 0.239 | 3.80 | 3.80 | 0.239 | 2.94 | 0.300 | | | | | | | | | |
| 1.33 | 0.748 | | 0.239 | 4.62 | 0.239 | 4.62 | 4.62 | 0.239 | 3.00 | 0.239 | | | | | | | | | |

TABLE 10-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | | |
|------------------|-------|-----------|--------|-----------|--------|-----------|-------|-----------|-------|------|-------|
| CURVE 10 (CONT.) | | | | | | | | | | | |
| 3. | 0.22 | 2.16 | 0.597 | 4.57 | 0.0793 | 4.72 | 0.466 | 2.59 | 0.303 | | |
| 4. | 0.40 | 2.40 | 0.649 | 4.70 | 0.0797 | 4.79 | 0.427 | 3.10 | 0.400 | | |
| 5. | 0.0 | 2.56 | 0.671 | 4.84 | 0.0808 | 4.84 | 0.396 | 3.58 | 0.675 | | |
| CURVE 11 | | | | | | | | | | | |
| T = 919. | | 2.67 | 0.665 | 5.00 | 0.0807 | 4.88 | 0.365 | 3.79 | 0.704 | | |
| | | 2.74 | 0.592 | | | 4.93 | 0.320 | 3.92 | 0.684 | | |
| | | 2.83 | 0.538 | CURVE 16 | | | | | | 4.10 | 0.585 |
| | | 2.92 | 0.473 | T = 293. | | | | | | 4.39 | 0.293 |
| 1. | 0.80 | 3.06 | 0.552 | 1.00 | 0.227 | 5.00 | 0.266 | 4.57 | 0.119 | | |
| 2. | 0.85 | 3.17 | 0.613 | 1.03 | 0.279 | CURVE 19 | | | | | |
| 3. | 0.19 | 3.29 | 0.679 | 1.08 | 0.314 | T = 293. | | | | | |
| 4. | 0.22 | | | | | | | | | 2.14 | 0.892 |
| 5. | 0.0 | | | | | | | | | 2.24 | 0.897 |
| CURVE 12 | | | | | | | | | | | |
| T = 1070. | | 1.08 | 0.0182 | 1.14 | 0.400 | 2.33 | 0.907 | CURVE 21 | | | |
| | | 1.39 | 0.049 | 1.29 | 0.439 | 2.46 | 0.892 | T = 293. | | | |
| | | 1.54 | 0.110 | 1.37 | 0.473 | 2.59 | 0.884 | 2.14 | 0.877 | | |
| 1. | 0.50 | 1.50 | 0.0240 | 1.46 | 0.510 | 2.66 | 0.819 | 2.27 | 0.593 | | |
| 2. | 0.73 | 1.62 | 0.0251 | 1.55 | 0.543 | 2.75 | 0.822 | 2.42 | 0.500 | | |
| 3. | 0.12 | 1.99 | 0.0235 | 1.66 | 0.573 | 2.82 | 0.295 | 2.49 | 0.835 | | |
| 4. | 0.18 | 2.09 | 0.288 | 1.76 | 0.603 | 2.93 | 0.325 | 2.59 | 0.872 | | |
| 5. | 0.0 | 2.15 | 0.352 | 1.85 | 0.628 | 3.10 | 0.391 | 2.65 | 0.591 | | |
| CURVE 13 | | | | | | | | | | | |
| T = 1482. | | 2.17 | 0.290 | 2.00 | 0.657 | 3.50 | 0.583 | 2.70 | 0.507 | | |
| | | 2.19 | 0.257 | 2.13 | 0.655 | 3.68 | 0.699 | 2.79 | 0.205 | | |
| | | 2.21 | 0.260 | 2.45 | 0.655 | 3.83 | 0.694 | 2.84 | 0.157 | | |
| | | 2.26 | 0.312 | 2.63 | 0.658 | 3.94 | 0.657 | 2.90 | 0.206 | | |
| 1. | 0.42 | 2.32 | 0.370 | 2.77 | 0.661 | 4.08 | 0.566 | 3.28 | 0.594 | | |
| 2. | 0.55 | 2.36 | 0.392 | 3.00 | 0.667 | 4.13 | 0.463 | 3.42 | 0.735 | | |
| 3. | 0.07 | 2.40 | 0.380 | 3.22 | 0.676 | 4.29 | 0.333 | 3.62 | 0.774 | | |
| 4. | 0.14 | 2.49 | 0.302 | 3.36 | 0.682 | 4.44 | 0.188 | 4.00 | 0.716 | | |
| 5. | 0.0 | 2.53 | 0.260 | 3.50 | 0.688 | 4.69 | 0.071 | 4.10 | 0.605 | | |
| CURVE 14 | | | | | | | | | | | |
| T = 293. | | 2.57 | 0.290 | 3.66 | 0.696 | 5.00 | 0.000 | 4.37 | 0.292 | | |
| | | 2.59 | 0.304 | 3.80 | 0.706 | CURVE 20 | | | | | |
| | | 2.63 | 0.395 | 4.00 | 0.715 | T = 293. | | | | | |
| | | 2.65 | 0.363 | 4.12 | 0.693 | 2.14 | 0.888 | 4.44 | 0.132 | | |
| | | 2.67 | 0.273 | 4.22 | 0.657 | 2.39 | 0.894 | 4.78 | 0.021 | | |
| 0.77 | 0.143 | 2.67 | 0.273 | 4.32 | 0.636 | CURVE 22 | | | | | |
| 1.02 | 0.260 | 2.71 | 0.215 | 4.39 | 0.610 | T = 293. | | | | | |
| 1.20 | 0.340 | 2.75 | 0.164 | 4.46 | 0.587 | 2.47 | 0.885 | 2.14 | 0.864 | | |
| 1.45 | 0.429 | 2.75 | 0.164 | 4.53 | 0.561 | 2.62 | 0.685 | 2.29 | 0.901 | | |
| 1.71 | 0.508 | 4.33 | 0.0743 | 4.60 | 0.532 | 2.65 | 0.792 | 2.38 | 0.694 | | |
| 1.83 | 0.541 | 4.45 | 0.0747 | 4.66 | 0.498 | 2.76 | 0.308 | | | | |

TABLE 10-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF PYROCERAM (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T |
|------------------|-------|
| CURVE 22 (CONT.) | |
| 2.47 | 0.877 |
| 2.56 | 0.990 |
| 2.63 | 0.857 |
| 2.75 | 0.399 |
| 2.80 | 0.162 |
| 2.82 | 0.154 |
| 3.34 | 0.659 |
| 3.46 | 0.738 |
| 3.64 | 0.759 |
| 3.85 | 0.738 |
| 4.00 | 0.668 |
| 4.44 | 0.144 |
| 4.65 | 0.056 |
| 5.00 | 0.000 |
| CURVE 23 | |
| T = 293. | |
| 2.14 | 0.907 |
| 2.38 | 0.920 |
| 2.43 | 0.895 |
| 2.58 | 0.958 |
| 2.62 | 0.859 |
| 2.73 | 0.445 |
| 2.76 | 0.146 |
| 2.80 | 0.152 |
| 3.18 | 0.632 |
| 3.32 | 0.748 |
| 3.46 | 0.803 |
| 3.69 | 0.785 |
| 3.89 | 0.733 |
| 4.02 | 0.604 |
| 4.08 | 0.491 |
| 4.24 | 0.290 |
| 4.39 | 0.113 |
| 4.59 | 0.041 |
| 5.00 | 0.000 |

f. Normal Spectral Transmittance (Temperature Dependence)

No experimental data sets specifically for the temperature dependence of the normal spectral transmittance of Corning 9606 were found. However, from curves 5, 6, 7, and 8 of the previous section (see Tables 10-11 and 10-12), the transmittance value at 3.80 μm is 0.485, 0.239, 0.263, and 0.219 at 293 K, 770 K, 900 K, and 1040 K, respectively.

4.11. Silica(Vitreous)

This material is labeled "Silica(Vitreous)" in the above heading so that in alphabetization this material will fall under "s". However, in this discussion the wording "vitreous silica" will be used for ease in reading.

Vitreous silica is a glass which is composed essentially of SiO_2 . The most general and unambiguous term that refers to the entire range of noncrystalline silica is vitreous silica. It is also known as fused silica, silica glass, and fused quartz. Additional information is available concerning the terminology and naming [T76945, T76946, A00026]. The two general types of vitreous silica are transparent and nontransparent. The latter arises from microscopic bubbles in the material. The emphasis in this section is to give evaluated data for the transparent type of vitreous silica.

Vitreous silica has many interesting physical properties. One source [T34753] gives a range for the melting point of 1950 to 2000 K while another source [A00017] identifies the melting point as 1996 K. It boils at 2500 K. The density is about 2.2 g cm^{-3} . One distinction for vitreous silica is that the coefficient of thermal expansion is among the lowest of all known materials. In the range of 273-573 K, the range for the linear expansion coefficient is between 5.4 and $5.6 \times 10^{-7} \text{ C}^{-1}$. At approximately 293 K, Young's modulus is 730 kbar, the shear modulus 311 kbar, and Poisson's ratio 0.17. The Knoop hardness falls in the range of $545\text{-}575 \text{ kg mm}^{-2}$.

a. Normal Spectral Emittance (Wavelength Dependence)

A total of six sets of experimental data were located for the wavelength dependence of the normal spectral emittance of vitreous silica. The data are listed in Table 11-3 and shown in Figures 11-1 and 11-2. Specimen characterization and measurement information for the data are given in Table 11-2.

Stierwalt [T16961] (curve 1) reported data for a specimen 0.84 mm thick at a temperature of 313 K. Dumbaugh and Schultz [T76945] reported calculations of Parker for a 0.50 in. thick specimen at room temperature (curve 2) and also for a 0.250 in. thick specimen (curve 3). Champetier and Friese [A00012] reported data for Optosil 1 at a temperature of 373 K for parallel polarization of the light emitted (curve 4), for perpendicular polarization (curve 5), and for unpolarized light (curve 6).

Above $5 \mu\text{m}$, all the data show the same general trend. From 5 to $6 \mu\text{m}$ the emittance is greater than 0.9. From that region the values fall, in the wavelength range of 8 to $9 \mu\text{m}$, to a minimum. From the minimum, the values rise and above $11 \mu\text{m}$ the

values are greater than 0.85. In addition, above 5 μm the data of curves 1 and 2 are close together. The value of the wavelength at which the minimum occurs for two groups of data is different. For curves 5 and 6 (Honeywell data), the wavelength at which the minimum occurs is 8.3 μm while for curves 1 and 2 it is 8.9 μm .

Calculations were carried out to determine the emittance for radiation that is polarized perpendicular to the plane of incidence (curves 7-9), the emittance for radiation that is polarized parallel to the plane of incidence (curves 10-12), and the emittance for unpolarized radiation (curves 13-15). The calculation for emittance with radiation polarized perpendicular to the plane of incidence was carried out in the following sequence: First the Fresnel equation for specular reflection for radiation polarized perpendicular to the plane of incidence was used, Eq. (2.4-1). Kirchhoff's law was then applied and Eq. (2.4-6) used to determine the emittance for radiation polarized perpendicular to the plane of incidence. The appropriate equations were used for radiation polarized parallel to the plane of incidence (see Eqs. (2.4-2) and (2.4-7)) and for unpolarized radiation (see Eqs. (2.4-5) and (2.4-8)).

The calculations of the emittance, or absorptance, using Eqs. (2.4-6) through (2.4-8) are based on the fact the material is opaque, i. e., the transmittance is zero. Champetier and Friese [A00012] reported transmittance for a 1 mm thick specimen of Optosil 1 at 293 K from 3.7 to 16 μm and found it to be opaque (see curve 38, Table 11-23). Hence, direct evidence exists for opaqueness to 16 μm and, therefore, calculations were not carried out past 16 μm .

The Fresnel equations are functions of the index of refraction n and the absorption index k as well as the angle of incidence θ . The index of refraction of vitreous silica is shown in Figure 11-3 and listed in Table 11-5. Specimen characterization and measurement information for the data of the index of refraction are given in Table 11-4. The absorption index of vitreous silica is shown in Figure 11-4 and listed in Table 11-7. Specimen characterization and measurement information for the data of absorption index are given in Table 11-6. Table 11-5 lists four places below the decimal point for wavelength values and five places below the decimal point for index of refraction values. If original data was given to more decimal places, the computer program generating Table 11-5 truncated and dropped the additional digits. The original data of curve 2 was given for up to five places below the decimal point for wavelength values and the original data for wavelength values of curves 1, 3-7, and 12 was given for up to six places below the decimal point. The original data for index of refraction of curves 3-7 was given for six places below the decimal point. The index of refraction and the absorption index values

used in the calculations were taken from Champetier and Friese [A00012, p. 61]. The index of refraction from Champetier and Friese is curve 11 in Figure 11-3 and in Tables 11-4 and 11-5; the absorption index is curve 3 in Figure 11-4 and Tables 11-6 and 11-7. The Champetier and Friese data is for a wavelength range of 7 to 26 μm , a temperature of 293 K, and is based on data in the literature. Below 9 μm it is based on the data of Zolotarev [T60820] and above 9 μm it is based on the data of Popova, Tolstykh, and Vorobev [E64849].

The calculations using the Fresnel equations were programmed and carried out for all wavelengths from 7 to 16 μm for which refractive index and absorption index data were given by Champetier and Friese. The calculations are valid for an optically smooth surface of vitreous silica, a temperature of 293 K, and a wavelength range of 7 to 16 μm . The lower range of the calculations were 7 μm since the data of the index of refraction and absorption index needed in the Fresnel equations only started at 7 μm . Optically smooth means the surface is "smooth in comparison with the wavelength of the incident radiation so that specular reflections result" [p. 111, T52053].

Because of the comment made in [A00012] questioning the validity of the data reported as curves 4, 5, and 6, this data was disregarded in developing evaluated values. A set of provisional values for vitreous silica at 293 K is listed in Table 11-1 and shown in Figure 11-1. Below 7 μm the provisional values are based on curve 2 and, therefore, apply to a 0.50 in. thick specimen of Corning 7940 vitreous silica. From 7 to 16 μm , the provisional values were calculated for unpolarized radiation. The calculated provisional values hold for an optically smooth specimen at 293 K that is opaque and has a viewing angle of 0° .

Because of the index of refraction and absorption index data are not themselves fully evaluated, the calculated emittance is called provisional. Below 7 μm the values for Corning 7940 do not have supporting evidence and it is only justified in labeling them provisional. Another reason for calling the calculated values above 7 μm provisional is that these values are close to curve 2 but do differ. An uncertainty of within 30% is therefore assigned to the provisional values. The provisional value at 10.6 μm of the normal spectral emittance at 293 K is 0.89. It is noted that high temperature normal spectral emittance data was not located.

TABLE 11-1. PROVISIONAL NOMINAL SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CORNING 7940 1.27CM THICK T = 293 | | | CORNING 7940 1.27CM THICK T = 293 (CONT.) | | | OPTICALLY SMOOTH T = 293 | | | OPTICALLY SMOOTH T = 293 (CONT.) | | |
|---|------------|-----------|---|-----------|------------|-----------------------------|------------|-----------|-------------------------------------|-----------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 2.14 | 0.026 | 4.49 | 0.970 | 7.00 | 0.999 | 10.4 | 0.955 | | | | |
| 2.32 | 0.042 | 4.55 | 0.976 | 7.10 | 1.000 | 10.6 | 0.887 | | | | |
| 2.42 | 0.062 | 4.66 | 0.974 | 7.20 | 1.000 | 10.8 | 0.889 | | | | |
| 2.50 | 0.083 | 4.81 | 0.973 | 7.30 | 1.000 | 11.0 | 0.897 | | | | |
| 2.52 | 0.131 | 4.99 | 0.973 | 7.40 | 1.000 | 11.2 | 0.902 | | | | |
| 2.52 | 0.252 | 5.00 | 0.974 | 7.50 | 0.999 | 11.4 | 0.909 | | | | |
| 2.50 | 0.408 | 5.27 | 0.979 | 7.60 | 0.997 | 11.6 | 0.915 | | | | |
| 2.51 | 0.439 | 5.56 | 0.986 | 7.70 | 0.990 | 11.8 | 0.923 | | | | |
| 2.54 | 0.473 | 5.77 | 0.986 | 7.80 | 0.980 | 12.0 | 0.923 | | | | |
| 2.58 | 0.568 | 5.88 | 0.986 | 7.90 | 0.949 | 12.2 | 0.917 | | | | |
| 2.58 | 0.643 | 6.00 | 0.986 | 8.00 | 0.865 | 12.4 | 0.907 | | | | |
| 2.58 | 0.692 | 6.18 | 0.989 | 8.10 | 0.732 | 12.6 | 0.894 | | | | |
| 2.58 | 0.762 | 6.40 | 0.993 | 8.20 | 0.686 | 12.8 | 0.881 | | | | |
| 2.63 | 0.914 | 6.62 | 0.994 | 8.30 | 0.694 | 13.0 | 0.890 | | | | |
| 2.62 | 0.957 | 6.76 | 0.993 | 8.40 | 0.664 | 13.2 | 0.898 | | | | |
| 2.66 | 0.970 | 6.90 | 0.993 | 8.50 | 0.632 | 13.4 | 0.903 | | | | |
| 2.76 | 0.957 | | | 8.60 | 0.578 | 13.6 | 0.911 | | | | |
| 2.81 | 0.889 | | | 8.65 | 0.539 | 13.8 | 0.919 | | | | |
| 2.81 | 0.687 | | | 8.70 | 0.475 | 14.0 | 0.923 | | | | |
| 2.85 | 0.623 | | | 8.75 | 0.433 | 14.2 | 0.928 | | | | |
| 2.95 | 0.524 | | | 8.80 | 0.368 | 14.4 | 0.857 | | | | |
| 3.00 | 0.450 | | | 8.85 | 0.321 | 14.6 | 0.935 | | | | |
| 3.03 | 0.395 | | | 8.90 | 0.298 | 14.6 | 0.935 | | | | |
| 3.03 | 0.313 | | | 8.95 | 0.281 | 16.0 | 0.960 | | | | |
| 3.09 | 0.299 | | | 9.00 | 0.330 | | | | | | |
| 3.22 | 0.302 | | | 9.05 | 0.382 | | | | | | |
| 3.39 | 0.315 | | | 9.10 | 0.535 | | | | | | |
| 3.50 | 0.332 | | | 9.15 | 0.470 | | | | | | |
| 3.57 | 0.410 | | | 9.20 | 0.526 | | | | | | |
| 3.61 | 0.471 | | | 9.30 | 0.547 | | | | | | |
| 3.67 | 0.547 | | | 9.35 | 0.584 | | | | | | |
| 3.74 | 0.642 | | | 9.40 | 0.685 | | | | | | |
| 3.80 | 0.699 | | | 9.50 | 0.657 | | | | | | |
| 3.88 | 0.903 | | | 9.60 | 0.687 | | | | | | |
| 3.95 | 0.890 | | | 9.70 | 0.716 | | | | | | |
| 4.00 | 0.907 | | | 9.80 | 0.748 | | | | | | |
| 4.05 | 0.927 | | | 9.90 | 0.771 | | | | | | |
| 4.21 | 0.952 | | | 10.0 | 0.795 | | | | | | |
| 4.37 | 0.965 | | | 10.2 | 0.834 | | | | | | |

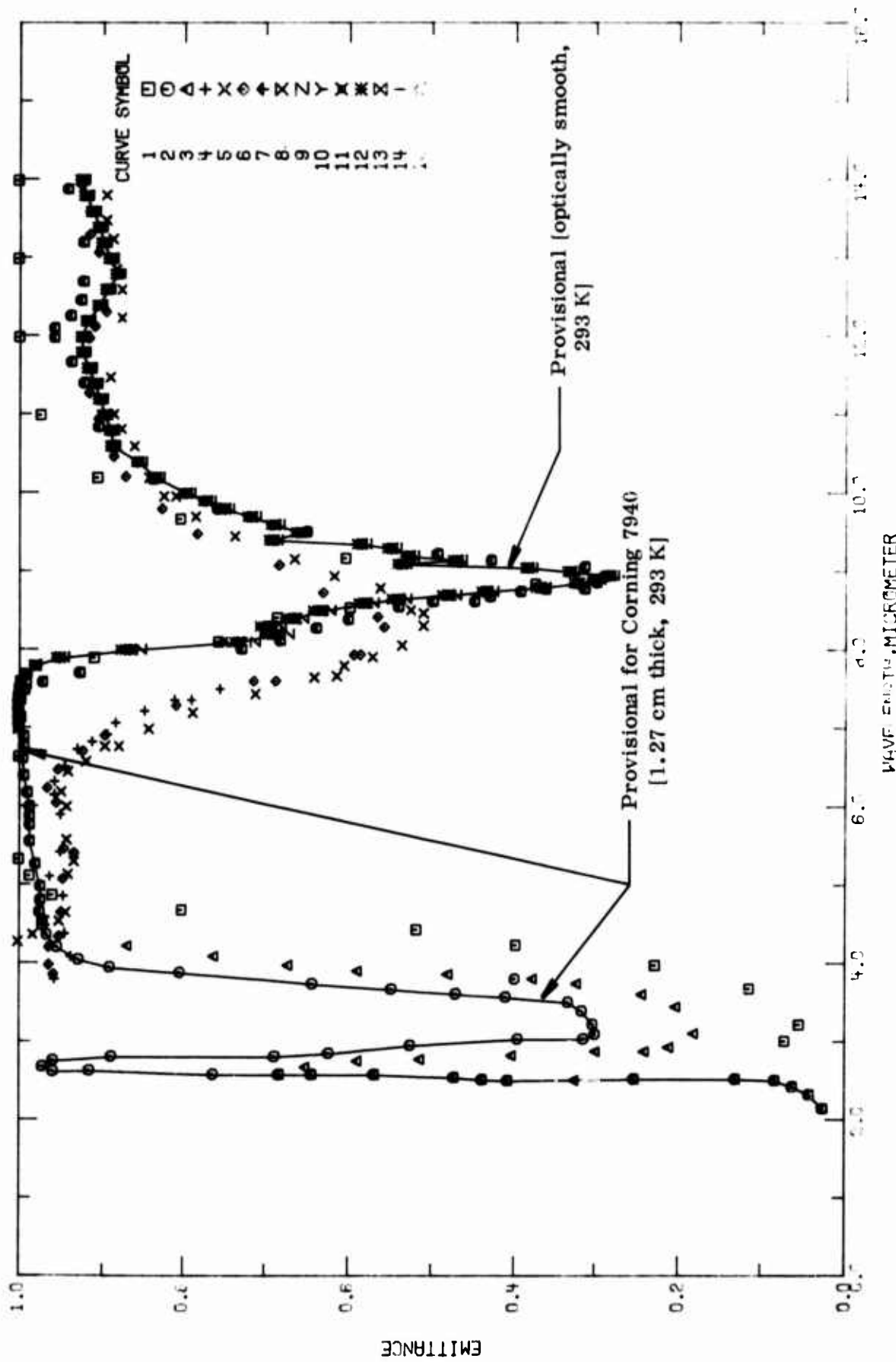


FIGURE 11-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SiO_2 (VITREOUS) (WAVELENGTH DEPENDENCE).

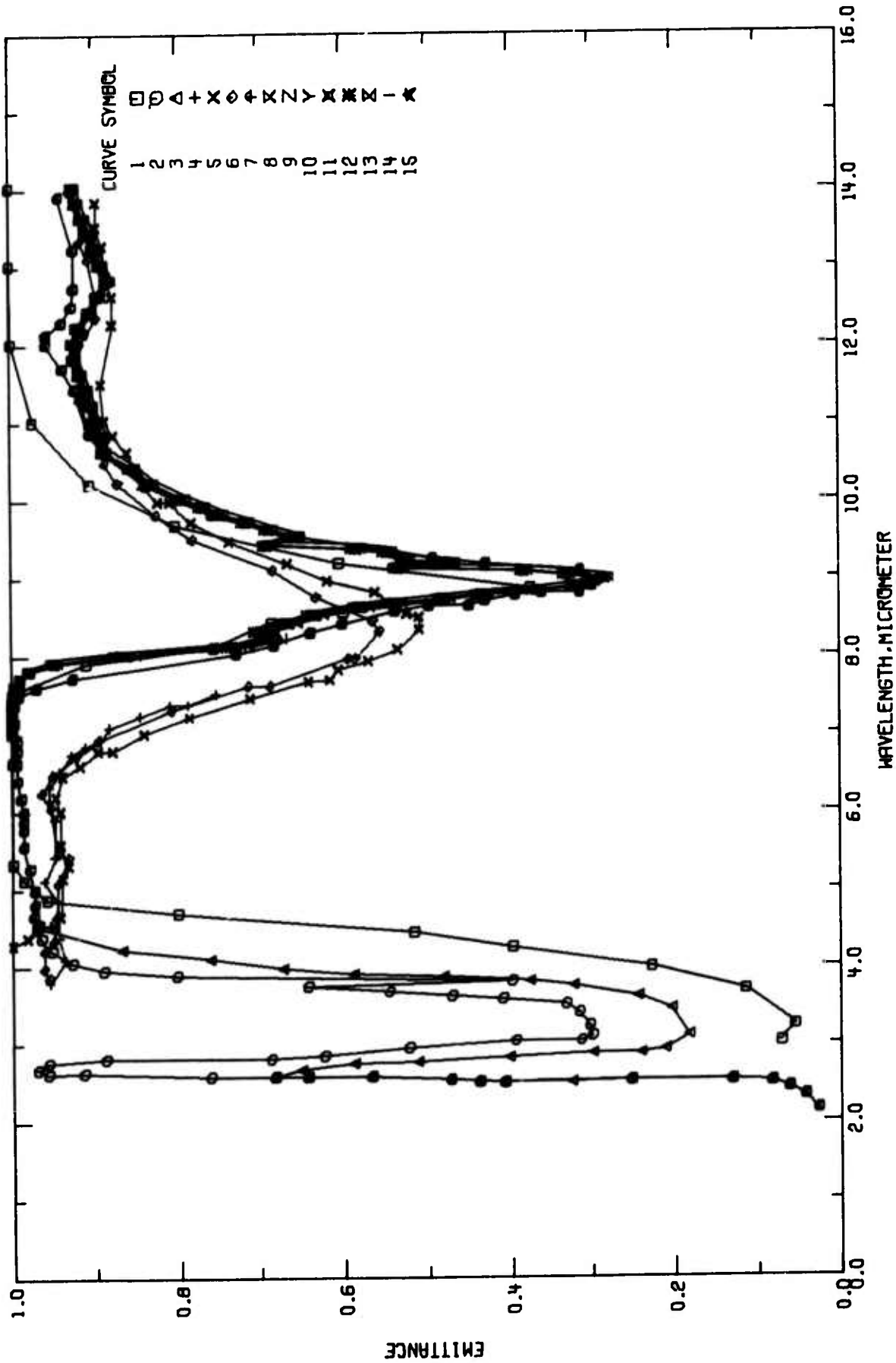


FIGURE 11-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

TABLE 11-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------------|------|---------------------------------|----------------------|-----------------------------------|---|
| 1 T16961 | Stierwalt, D. L. | 1961 | 3.0-14 | 313 | Fused quartz | Plate 0.84 mm thick; measured in vacuum; smooth values from figure; spectral emissivity reported; $\theta' \sim 0^\circ$. |
| 2 T76945 | Dumbaugh, W. H. and Schultz, P. C. | 1969 | 2.1-25 | 293 | Corning Code 7940 vitreous silica | Specimen 0.50 in. thick; emissivity calculated by C. J. Parker from room temperature (293 K assigned) measurements of transmittance and reflectance. |
| 3 T76945 | Dumbaugh, W. H. and Schultz, F. C. | 1969 | 2.1-25 | 293 | Corning Code 7940 vitreous silica | Similar to the above specimen except specimen 0.250 in. thick. |
| 4 A00012 | Champetier, R. J. and Friese, G. J. | 1974 | 3.8-7.5 | 373 | Optosil 1 | Specimen thickness 0.125 in.; polished disk; Honeywell spectral emissometer used which includes a Leiss double prism monochromator with prisms of potassium cesium bromide; computed system band width 0.19 μm ; optics, chopper, and enclosure near 300 K while sample and black body reference are heated to 373 K; polarization of monochromator which is present has not been removed from data; 0° data taken but not reported, the 0° and 12° data were identical; emittance data for parallel polarization; a conclusion in this report [A00012] is that "Honeywell emissometer currently produces incorrect data at angles greater than 40 degrees and previously generated data cannot be used with confidence in their validity."; smooth values from figure; because of overlap of curves, data could not be extracted for full wavelength range for which data reported; $\theta' = 12^\circ$. |
| 5 A00012 | Champetier, R. J. and Friese, G. J. | 1974 | 4.3-24 | 373 | Optosil 1 | Similar to the above specimen except for perpendicular polarization. |
| 6 A00012 | Champetier, R. J. and Friese, G. J. | 1974 | 3.9-20 | 373 | Optosil 1 | Similar to the above specimen except for unpolarized light. |
| 7 A00012 | | 1975 | 7.0-16 | 293 | | Calculations for fused silica performed for a homogeneous, smooth surface and for perpendicular component of radiation, equations (2.4-6), (2.4-1), (2.4-3), and (2.4-4); data for index of refraction, n , and absorption index, k , from [A00012]; $\theta' = 0^\circ$. |
| 8 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta' = 5^\circ$. |
| 9 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta' = 10^\circ$. |
| 10 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for parallel component of radiation, equation (2.4-7) and $\theta' = 0^\circ$. |
| 11 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta' = 5^\circ$. |
| 12 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta' = 10^\circ$. |
| 13 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for unpolarized radiation, equation (2.4-8), and $\theta' = 0^\circ$. |
| 14 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta' = 5^\circ$. |
| 15 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta' = 10^\circ$. |

TABLE 11-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CURVE 1 T = 313. | | CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 3 (CONT.) | |
|---------------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 3.00 | 0.071 | 2.50 | 0.682 | 5.90 | 0.997 | 16.77 | 0.982 | 2.54 | 0.473 |
| 3.21 | 0.054 | 2.58 | 0.762 | 7.14 | 0.997 | 17.24 | 0.987 | 2.58 | 0.562 |
| 3.67 | 0.114 | 2.63 | 0.514 | 7.36 | 0.997 | 17.55 | 0.385 | 2.58 | 0.643 |
| 3.97 | 0.227 | 2.62 | 0.957 | 7.49 | 0.992 | 18.37 | 0.982 | 2.58 | 0.600 |
| 4.23 | 0.398 | 2.68 | 0.970 | 7.59 | 0.970 | 19.56 | 0.990 | 2.67 | 0.651 |
| 4.43 | 0.517 | 2.76 | 0.957 | 7.71 | 0.926 | 18.89 | 0.997 | 2.75 | 0.599 |
| 4.68 | 0.801 | 2.81 | 0.689 | 9.01 | 0.726 | 13.14 | 0.988 | 2.77 | 0.513 |
| 4.87 | 0.959 | 2.81 | 0.687 | 9.12 | 0.681 | 19.29 | 0.965 | 2.82 | 0.430 |
| 5.12 | 0.986 | 2.85 | 0.623 | 9.28 | 0.638 | 19.47 | 0.937 | 2.87 | 0.299 |
| 5.33 | 0.999 | 2.95 | 0.524 | 9.39 | 0.600 | 19.55 | 0.905 | 2.87 | 0.240 |
| 6.64 | 0.999 | 3.03 | 0.395 | 9.55 | 0.539 | 19.63 | 0.870 | 2.92 | 0.211 |
| 7.56 | 0.999 | 3.03 | 0.313 | 9.62 | 0.498 | 19.76 | 0.825 | 3.10 | 0.182 |
| 7.90 | 0.909 | 3.09 | 0.299 | 9.62 | 0.449 | 19.92 | 0.738 | 3.44 | 0.203 |
| 8.10 | 0.756 | 3.22 | 0.302 | 9.68 | 0.430 | 20.48 | 0.485 | 3.60 | 0.243 |
| 8.41 | 0.684 | 3.39 | 0.315 | 9.75 | 0.393 | 20.55 | 0.467 | 3.74 | 0.322 |
| 8.54 | 0.598 | 3.50 | 0.332 | 9.79 | 0.361 | 20.66 | 0.451 | 3.80 | 0.377 |
| 8.84 | 0.374 | 3.57 | 0.410 | 9.78 | 0.313 | 20.80 | 0.444 | 3.86 | 0.481 |
| 9.17 | 0.603 | 3.61 | 0.471 | 9.86 | 0.298 | 21.00 | 0.453 | 3.90 | 0.589 |
| 9.67 | 0.803 | 3.67 | 0.547 | 9.94 | 0.289 | 21.16 | 0.486 | 3.97 | 0.572 |
| 10.2 | 0.995 | 3.74 | 0.642 | 9.06 | 0.313 | 21.74 | 0.586 | 4.09 | 0.762 |
| 11.0 | 0.973 | 3.80 | 0.399 | 9.15 | 0.429 | 21.99 | 0.623 | 4.22 | 0.869 |
| 12.0 | 0.999 | 3.88 | 0.803 | 9.23 | 0.493 | 22.39 | 0.670 | 4.53 | 0.970 |
| 13.8 | 1.80 | 3.95 | 0.890 | 9.31 | 0.645 | 22.79 | 0.784 | 4.66 | 0.974 |
| 14.0 | 1.00 | 4.05 | 0.927 | 9.60 | 0.758 | 23.21 | 0.728 | 4.81 | 0.973 |
| | | 4.21 | 0.952 | 10.18 | 0.838 | 23.74 | 0.751 | 4.99 | 0.973 |
| | | 4.37 | 0.965 | 10.60 | 0.886 | 24.35 | 0.775 | 5.27 | 0.979 |
| | | 4.49 | 0.970 | 11.85 | 0.904 | 24.91 | 0.801 | 5.56 | 0.986 |
| | | 4.55 | 0.970 | 11.41 | 0.921 | CURVE 3 | | 5.77 | 0.986 |
| | | 4.66 | 0.974 | 11.68 | 0.936 | T = 293. | | 5.88 | 0.986 |
| | | 4.81 | 0.973 | 11.99 | 0.956 | | | 6.00 | 0.986 |
| | | 4.99 | 0.973 | 12.11 | 0.956 | | | 6.18 | 0.989 |
| | | 5.27 | 0.979 | 12.27 | 0.937 | 2.14 | 0.026 | 6.40 | 0.993 |
| | | 5.56 | 0.986 | 12.47 | 0.925 | 2.32 | 0.042 | 15.59 | 0.977 |
| | | 5.72 | 0.986 | 12.71 | 0.922 | 2.42 | 0.062 | 16.00 | 0.977 |
| | | 5.88 | 0.986 | 13.21 | 0.922 | 2.50 | 0.063 | 16.49 | 0.977 |
| | | 6.00 | 0.986 | 13.83 | 0.940 | 2.52 | 0.131 | 16.77 | 0.982 |
| | | 6.18 | 0.989 | 14.61 | 0.961 | 2.52 | 0.252 | 17.24 | 0.987 |
| | | 6.40 | 0.993 | 15.59 | 0.974 | 2.50 | 0.325 | 17.55 | 0.985 |
| | | 6.62 | 0.994 | 16.00 | 0.977 | 2.50 | 0.408 | 18.37 | 0.985 |
| | | 6.78 | 0.993 | 16.49 | 0.977 | 2.51 | 0.435 | 18.66 | 0.990 |
| | | | | | | | | 18.89 | 0.997 |

TABLE 11-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|------------|
| CURVE 3 (CONT.) | CURVE 4 (CONT.) | CURVE 5 (CONT.) | CURVE 6 (CONT.) | CURVE 5 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | ϵ |
| 19.14 | 0.988 | 7.36 | 0.810 | 13.60 | 0.850 | 21.71 | 0.477 | 7.94 | 0.585 | 20.00 | 0.656 |
| 19.29 | 0.965 | 7.36 | 0.769 | 13.82 | 0.876 | 21.83 | 0.489 | 8.29 | 0.556 | CURVE 7 | |
| 19.47 | 0.937 | 7.50 | 0.754 | 11.01 | 0.806 | 21.99 | 0.530 | 8.42 | 0.564 | T = 293. | |
| 19.55 | 0.905 | | | 11.48 | 0.890 | 22.35 | 0.534 | 8.73 | 0.630 | | |
| 19.63 | 0.870 | CURVE 5 | | 12.24 | 0.876 | 22.53 | 0.585 | 9.08 | 0.682 | | |
| 19.76 | 0.825 | T = 373. | | 12.00 | 0.876 | 22.60 | 0.593 | 9.48 | 0.782 | | |
| 19.92 | 0.738 | | | 12.86 | 0.883 | 22.76 | 0.593 | 9.80 | 0.826 | 7.00 | 0.99940 |
| 20.48 | 0.483 | 4.28 | 1.000 | 13.25 | 0.887 | 22.88 | 0.604 | 9.80 | 0.826 | 7.10 | 0.99960 |
| 20.55 | 0.467 | 4.37 | 0.982 | 13.49 | 0.895 | 22.88 | 0.615 | 10.21 | 0.871 | 7.20 | 0.99999 |
| 20.66 | 0.451 | 4.54 | 0.967 | 13.81 | 0.895 | 23.00 | 0.623 | 10.47 | 0.886 | 7.30 | 0.99999 |
| 20.80 | 0.444 | 4.65 | 0.950 | 14.36 | 0.903 | 23.15 | 0.656 | 10.60 | 0.889 | 7.40 | 0.99995 |
| 21.00 | 0.453 | 4.85 | 0.942 | 14.58 | 0.916 | 23.28 | 0.661 | 10.95 | 0.904 | 7.50 | 0.99805 |
| 21.16 | 0.486 | 5.14 | 0.939 | 14.85 | 0.926 | 23.28 | 0.668 | 11.28 | 0.915 | 7.60 | 0.99699 |
| 21.74 | 0.586 | 5.30 | 0.932 | 15.31 | 0.923 | 23.44 | 0.575 | 11.98 | 0.915 | 7.70 | 0.99004 |
| 21.99 | 0.623 | 5.58 | 0.941 | 15.60 | 0.928 | 23.51 | 0.659 | 12.32 | 0.908 | 7.80 | 0.9796 |
| 22.38 | 0.670 | 6.00 | 0.941 | 15.72 | 0.922 | 23.55 | 0.682 | 12.61 | 0.895 | 7.90 | 0.9489 |
| 22.79 | 0.704 | 6.19 | 0.947 | 15.91 | 0.930 | 23.79 | 0.674 | 13.08 | 0.895 | 8.00 | 0.8649 |
| 23.21 | 0.728 | 6.45 | 0.939 | 16.37 | 0.928 | 23.93 | 0.668 | 13.31 | 0.914 | 8.10 | 0.7319 |
| 23.74 | 0.751 | 6.58 | 0.918 | 16.54 | 0.932 | 23.93 | 0.668 | 13.60 | 0.914 | 8.20 | 0.6863 |
| 24.35 | 0.775 | 6.77 | 0.896 | 15.91 | 0.932 | 24.00 | 0.689 | 13.94 | 0.924 | 8.30 | 0.6936 |
| 24.91 | 0.801 | 6.99 | 0.879 | 17.10 | 0.936 | | | 14.10 | 0.916 | 8.40 | 0.6640 |
| | | 7.20 | 0.787 | 17.27 | 0.942 | CURVE 6 | | 14.28 | 0.920 | 8.60 | 0.5784 |
| | | 7.44 | 0.711 | 17.43 | 0.935 | T = 373. | | 14.44 | 0.932 | 8.65 | 0.5387 |
| | | 7.65 | 0.640 | 18.06 | 0.937 | | | 14.58 | 0.926 | 8.70 | 0.4793 |
| | | 7.67 | 0.614 | 18.14 | 0.950 | 3.86 | 0.956 | 14.76 | 0.935 | 8.75 | 0.4334 |
| | | 7.80 | 0.605 | 18.35 | 0.956 | 4.21 | 0.962 | 14.95 | 0.931 | 8.80 | 0.3675 |
| | | 7.91 | 0.570 | 18.74 | 0.944 | 4.34 | 0.959 | 15.49 | 0.947 | 8.85 | 0.3206 |
| | | 8.06 | 0.535 | 18.86 | 0.951 | 4.65 | 0.947 | 15.67 | 0.942 | 8.90 | 0.2982 |
| | | 8.31 | 0.509 | 19.03 | 0.945 | 5.08 | 0.945 | 16.85 | 0.955 | 8.95 | 0.2813 |
| | | 8.47 | 0.509 | 19.29 | 0.945 | 5.41 | 0.932 | 17.06 | 0.948 | 9.00 | 0.3296 |
| | | 8.51 | 0.524 | 19.69 | 0.945 | 5.46 | 0.944 | 17.37 | 0.954 | 9.05 | 0.3824 |
| | | 8.79 | 0.561 | 19.83 | 0.869 | 6.05 | 0.953 | 17.65 | 0.954 | 9.10 | 0.5351 |
| | | 8.94 | 0.617 | 20.15 | 0.748 | 6.24 | 0.964 | 18.30 | 0.960 | 9.15 | 0.4699 |
| | | 9.16 | 0.664 | 20.39 | 0.666 | 6.47 | 0.951 | 18.50 | 0.967 | 9.20 | 0.5256 |
| | | 9.45 | 0.736 | 20.66 | 0.540 | 6.71 | 0.922 | 18.85 | 0.967 | 9.30 | 0.5473 |
| | | 9.70 | 0.784 | 20.87 | 0.475 | 6.91 | 0.895 | 18.99 | 0.962 | 9.35 | 0.5836 |
| | | 9.96 | 0.809 | 21.13 | 0.436 | 7.29 | 0.809 | 19.20 | 0.940 | 9.40 | 0.6894 |
| | | 9.96 | 0.824 | 21.32 | 0.418 | 7.60 | 0.713 | 19.58 | 0.931 | 9.50 | 0.6567 |
| | | 10.20 | 0.847 | 21.45 | 0.421 | 7.60 | 0.686 | 19.80 | 0.880 | 9.60 | 0.6871 |
| | | | | | | 7.94 | 0.593 | 19.82 | 0.871 | 9.70 | 0.7159 |

TABLE 11-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CURVE 11 (CONT.) | | | CURVE 12 (CONT.) | | | CURVE 13 (CONT.) | | | CURVE 13 (CONT.) | | | CURVE 14 (CONT.) | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
|------------------|------------|-----------|------------------|-----------|------------|------------------|------------|-----------|------------------|-----------|------------|------------------|------------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|------|--------|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|------|--------|------|--------|--|--|--|--|------|--------|--|--|------|--------|------|--------|--|--|--|--|------|--------|--|--|------|--------|------|--------|--|--|--|--|------|--------|--|--|------|--------|------|--------|--|--|--|--|------|--------|--|--|------|--------|------|--------|--|--|--|--|------|--------|--|--|------|--------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 8.30 | 0.6970 | 13.2 | 0.8990 | 9.15 | 0.4753 | 7.17 | 0.9936 | 10.8 | 0.9986 | 8.50 | 0.6310 | 8.40 | 0.6668 | 13.4 | 0.9038 | 9.20 | 0.5312 | 7.20 | 0.9999 | 11.0 | 0.8971 | 8.60 | 0.5784 | 8.50 | 0.6344 | 13.6 | 0.9120 | 3.30 | 0.5529 | 7.30 | 0.9999 | 11.2 | 0.9023 | 8.65 | 0.5306 | 8.65 | 0.5809 | 13.8 | 0.9197 | 3.35 | 0.5894 | 7.40 | 0.9995 | 11.4 | 0.9085 | 8.70 | 0.4793 | 8.70 | 0.5409 | 14.0 | 0.9241 | 3.40 | 0.6949 | 7.50 | 0.9985 | 11.6 | 0.9152 | 8.75 | 0.4334 | 8.75 | 0.4814 | 14.2 | 0.9283 | 9.50 | 0.6623 | 7.60 | 0.9969 | 11.8 | 0.9225 | 8.80 | 0.3675 | 8.80 | 0.4353 | 14.4 | 0.9353 | 9.50 | 0.6926 | 7.70 | 0.9974 | 12.0 | 0.9229 | 8.85 | 0.3205 | 8.85 | 0.3692 | 14.6 | 0.9577 | 9.60 | 0.7212 | 7.80 | 0.9796 | 12.2 | 0.9172 | 8.90 | 0.2982 | 8.90 | 0.3220 | 14.8 | 0.9354 | 9.70 | 0.7531 | 7.90 | 0.9489 | 12.4 | 0.9034 | 8.95 | 0.2813 | 8.90 | 0.2994 | 15.0 | 0.9606 | 3.90 | 0.7754 | 8.00 | 0.8649 | 12.6 | 0.8937 | 9.00 | 0.3296 | 9.00 | 0.2824 | | | 10.0 | 0.7997 | 8.10 | 0.7319 | 12.8 | 0.8814 | 9.05 | 0.3824 | 9.05 | 0.3307 | | | 10.0 | 0.8374 | 8.20 | 0.6863 | 13.0 | 0.8899 | 9.10 | 0.5351 | 9.05 | 0.3637 | | | 10.4 | 0.8583 | 8.30 | 0.6936 | 13.2 | 0.8982 | 9.15 | 0.4699 | 9.10 | 0.3365 | | | 10.6 | 0.8909 | 8.40 | 0.6640 | 13.4 | 0.9030 | 9.20 | 0.5256 | 9.15 | 0.4713 | | | 10.8 | 0.8920 | 8.50 | 0.6318 | 13.6 | 0.9113 | 9.30 | 0.5473 | 9.20 | 0.5270 | | | 11.0 | 0.9004 | 8.60 | 0.5784 | 13.8 | 0.9190 | 9.35 | 0.5036 | 9.30 | 0.5487 | | | 11.2 | 0.9055 | 8.65 | 0.5387 | 14.0 | 0.9234 | 9.40 | 0.6894 | 9.35 | 0.5851 | | | 11.4 | 0.9115 | 8.70 | 0.4793 | 14.2 | 0.9277 | 9.50 | 0.6567 | 9.40 | 0.6908 | | | 11.6 | 0.9181 | 8.75 | 0.4334 | 14.4 | 0.8567 | 9.60 | 0.6871 | 9.50 | 0.6581 | | | 11.8 | 0.9251 | 8.80 | 0.3675 | 14.6 | 0.9348 | 9.70 | 0.7159 | 9.60 | 0.6805 | | | 12.0 | 0.9256 | 8.85 | 0.3206 | 15.0 | 0.9602 | 9.80 | 0.7479 | 9.70 | 0.7172 | | | 12.2 | 0.9201 | 8.90 | 0.2982 | | | 9.90 | 0.7705 | 9.80 | 0.7492 | | | 12.4 | 0.9066 | 8.95 | 0.2813 | | | 10.0 | 0.7950 | 9.90 | 0.7717 | | | 12.6 | 0.8970 | 9.00 | 0.3296 | | | 10.2 | 0.8335 | 10.0 | 0.7961 | | | 12.8 | 0.8849 | 9.05 | 0.3824 | | | 10.4 | 0.8548 | 10.2 | 0.8346 | | | 13.0 | 0.8933 | 9.10 | 0.5331 | | | 10.6 | 0.8874 | 10.4 | 0.8358 | | | 13.2 | 0.9014 | 9.15 | 0.4699 | | | 10.8 | 0.8886 | 10.6 | 0.8883 | | | 13.4 | 0.9062 | 9.20 | 0.5256 | | | 11.0 | 0.8971 | 10.8 | 0.8895 | | | 13.6 | 0.9142 | 9.30 | 0.5473 | | | 11.2 | 0.9023 | 11.0 | 0.8979 | | | 13.8 | 0.9218 | 9.35 | 0.5836 | | | 11.4 | 0.9085 | 11.2 | 0.9031 | | | 14.0 | 0.9261 | 9.40 | 0.5894 | | | 11.6 | 0.9152 | 11.4 | 0.9092 | | | 14.2 | 0.9302 | 9.50 | 0.6567 | | | 11.8 | 0.9225 | 11.6 | 0.9159 | | | 14.4 | 0.8609 | 9.60 | 0.6871 | | | 12.0 | 0.9229 | 11.8 | 0.9231 | | | 14.6 | 0.9372 | 9.70 | 0.7159 | | | 12.2 | 0.9172 | 12.0 | 0.9235 | | | 15.0 | 0.9618 | 9.80 | 0.7479 | | | 12.4 | 0.9034 | 12.2 | 0.9179 | | | | | 9.90 | 0.7735 | | | 12.6 | 0.8937 | 12.4 | 0.9042 | | | | | 10.0 | 0.7950 | | | 12.8 | 0.8814 | 12.6 | 0.8945 | | | | | 10.2 | 0.8335 | | | 13.0 | 0.8839 | 12.8 | 0.8823 | | | | | 10.4 | 0.8548 | | | 13.2 | 0.8982 | 13.0 | 0.8907 | | | | | 10.6 | 0.8874 | | | 13.4 | 0.9030 |

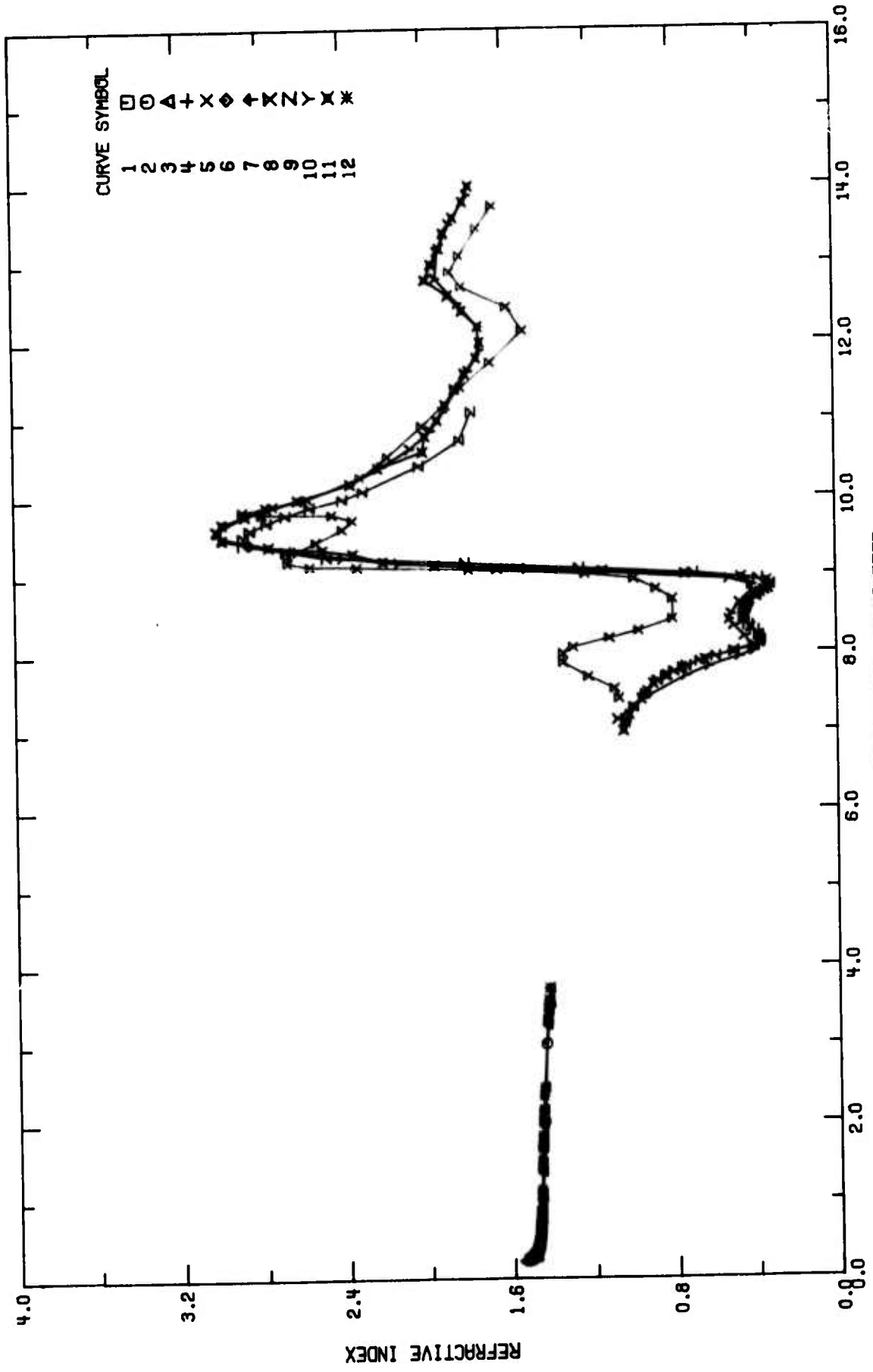
CURVE 14
T = 293.

CURVE 13
T = 293.

7.00 0.9994

TABLE 11-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ |
|------------------|------------|-----------|------------|
| CURVE 14 (CONT.) | | | |
| 13.6 | 0.9113 | 9.30 | 0.5473 |
| 13.8 | 0.9190 | 9.35 | 0.5836 |
| 14.0 | 0.9234 | 9.40 | 0.6894 |
| 14.2 | 0.9277 | 9.50 | 0.6567 |
| 14.4 | 0.8567 | 9.60 | 0.6871 |
| 14.6 | 0.9348 | 9.70 | 0.7159 |
| 16.0 | 0.9602 | 9.80 | 0.7479 |
| | | 9.90 | 0.7704 |
| CURVE 15 | | | |
| T = 293. | | | |
| 7.00 | 0.9994 | 10.0 | 0.7949 |
| 7.10 | 0.9996 | 10.2 | 0.8335 |
| 7.20 | 0.9999 | 10.4 | 0.8548 |
| 7.30 | 0.9999 | 10.6 | 0.8874 |
| 7.40 | 0.9995 | 10.8 | 0.8886 |
| 7.50 | 0.9985 | 11.0 | 0.8971 |
| 7.60 | 0.9969 | 11.2 | 0.9023 |
| 7.70 | 0.9904 | 11.4 | 0.9084 |
| 7.80 | 0.9796 | 11.6 | 0.9152 |
| 7.90 | 0.9488 | 11.8 | 0.9224 |
| 8.00 | 0.9643 | 12.0 | 0.9228 |
| 8.10 | 0.7307 | 12.2 | 0.9172 |
| 8.20 | 0.6856 | 12.4 | 0.9034 |
| 8.30 | 0.6931 | 12.6 | 0.8935 |
| 8.40 | 0.6637 | 12.8 | 0.8813 |
| 8.50 | 0.6316 | 13.0 | 0.8899 |
| 8.60 | 0.5782 | 13.2 | 0.8982 |
| 8.65 | 0.5385 | 13.4 | 0.9030 |
| 8.70 | 0.4792 | 13.6 | 0.9113 |
| 8.75 | 0.4334 | 13.8 | 0.9190 |
| 8.80 | 0.3675 | 14.0 | 0.9234 |
| 8.85 | 0.3206 | 14.2 | 0.9277 |
| 8.90 | 0.2982 | 14.4 | 0.8567 |
| 8.95 | 0.2813 | 14.6 | 0.9348 |
| 9.00 | 0.3296 | 16.0 | 0.9602 |
| 9.05 | 0.3824 | | |
| 9.10 | 0.5351 | | |
| 9.15 | 0.4699 | | |
| 9.20 | 0.5256 | | |



WAVELENGTH, MICROMETER

FIGURE 11-3. EXPERIMENTAL REFRACTIVE INDEX OF SILICA (VITREOUS)
(WAVELENGTH DEPENDENCE).

TABLE 11-4. MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF SILICA (VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|--|--|
| 1 A00010 | Thermal American Fused Quartz Company | 1970 | 0.24-0.77 | 297 | Spectrosil Synthetic Fused Quartz | <0.00001 Ca, <0.00001 Fe, 0.000004 Na, <0.000002 Al, <0.000001 B, <0.0000004 Ca, <0.0000004 K, <0.0000001 P, <0.0000001 Mn, <0.0000002 As, <0.0000002 Cu, and 0.0000001 Sb (see Hetherington, G. and Bell, L.W., "Analysis of High-Purity Synthetic Vitreous Silicas," Physics and Chemistry of Glasses, 8(5), 206-8, 1967, [A00011]). 99.8 \pm SiO ₂ ; measurement temperature not given explicitly, assumed to be 293 K. |
| 2 A00010 | Thermal American Fused Quartz Company | 1970 | 0.41-3.5 | 293 | Vitreosil | Typical analysis 0.0010-0.0100 Cl, 0.00001-0.0001 Ca, 0.00001-0.0010 Ti, 0.00005-0.0005 Al, 0.00005-0.00005 B, 0.00005-0.0005 Zn, 0.00001-0.00001 Bi, 0.00001-0.00005 Cu, 0.00001-0.0005 Fe, 0.00001-0.00001 K, 0.00001-0.00001 Mg, 0.00001-0.0001 Na, 0.00001-0.00001 P, 0.00001-0.00001 V, 0.000001-0.000005 As, 0.000001-0.000003 Cr, 0.000001-0.00001 Mn, and 0.000001-0.000005 Sb; maximum total impurities other than water do not exceed 0.01, water content estimated at 0.1 or less; amorphous; made by flame hydrolysis. |
| 3 T76891 | Corning Glass Works | 1971 | 0.21-3.7 | 293 | Corning Code 7940 Fused Silica | Material submitted for testing was from four different production runs. |
| 4 E21758 | Malitson, I.H. | 1965 | 0.21-3.7 | 293 | Dynasil High-Purity Synthetic Fused Silica | Material submitted for testing was from four different production runs. |
| 5 E21758 | Malitson, I.H. | 1965 | 0.21-3.7 | 293 | General Electric Type 151 | Material submitted for testing was from four different production runs. |
| 6 E21758 | Malitson, I.H. | 1965 | 0.21-3.7 | 293 | Corning Code 7940 Fused Silica | Material submitted for testing was from four different production runs. |
| 7 E21758 | Malitson, I.H. | 1965 | 0.21-3.7 | 293 | Fused Silica | Refractive index for high-purity optical quality fused silica made by three companies determined; materials Corning 7940 fused silica, Dynasil high purity synthetic fused silica, and General Electric type 151; minimum deviation method used; data fitted to three-term Sellmeier dispersion equation $n^2 - 1 = (0.6961663 \lambda^2 / (\lambda^2 - (0.0661043)^2)) + (0.4079426 \lambda^2 / (\lambda^2 - (0.1162414)^2)) + (0.8974794 \lambda^2 / (\lambda^2 - (9.896161)^2))$ with λ in μm ; average of absolute values of residuals = 10.5×10^{-6} ; data reported here calculated from above expression. |
| 8 E64850 | Crozier, D. and Douglas, R.W. | 1965 | 7.4-14.6 | 293 | Fused Silica | 100 SiO ₂ ; blown films prepared, selected areas stuck on copper wire loops and absorption spectra determined on a Grubb Parsons double-beam spectrometer; thin film method of Blain and Douglas used to analyze spectra to give refractive index and absorption index; measurement temperature not given explicitly, assumed to be 293 K. |
| 9 T60820 | Zolotarev, V.M. | 1970 | 7.1-11 | 293 | Fused Quartz | Several overlapping methods used to determine refractive index; measurement temperature not explicitly given, assumed to be 293 K. |
| 10 E64849 | Popova, S.I., Toletykh, T.S., and Vorobev, V.T. | 1972 | 7.1-50 | 293 | Amorphous Quartz | Total impurity content (CaCO ₃ , sodium chloride, and oxides of Al, Mg, Cu, Ca, and Fe) <0.007; SiO ₂ samples of grades KJ and KI used; refractive index n and absorption index k derived from reflectance spectra; measurement temperature not given explicitly, assumed to be 293 K. |
| 11 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 7.0-26 | 293 | Fused Silica | Refractive index values for wavelengths shorter than 9 μm based on data in [T60820] (curve 9 above), for longer wavelengths based on data in [E64849] (curve 10 above). |

TABLE 11-4. MEASUREMENT INFORMATION ON THE REFRACTIVE INDEX OF SILICA(VITREOUS) (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|--|--|
| 12 E19326 | Jerrard, H. G. and Turpin, J. | 1965 | 0.20-0.30 | 291.7 | Optical Quality Fused Silica, Spectrosil A | Specimen supplied by the Thermal Syndicate, Wallaseid, England; light source was copper arc and wavelength values taken from table (44th edition of Handbook of Chemistry and Physics); values reported are mean values for three different experiments conducted in air; most of the deviations found in the fifth decimal place in range 0.00002 to 0.00004. |

TABLE 11-5. EXPERIMENTAL REFRACTIVE INDEX OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ ; μ m; TEMPERATURE, T, K; REFRACTIVE INDEX, n)

| λ | CURVE 10 (CONT.) | | CURVE 11 (CONT.) | | CURVE 11 (CONT.) | | CURVE 11 (CONT.) | | CURVE 12 (CONT.) | | CURVE 12 (CONT.) | |
|-----------|------------------|------|------------------|------|------------------|------|------------------|---------|------------------|---------|------------------|---|
| | λ | n | λ | n | λ | n | λ | n | λ | n | λ | n |
| 23.81 | 2.77 | 2.35 | 9.3 | 2.35 | 23.0 | 2.77 | 0.2590 | 1.50272 | 0.2590 | 1.50272 | | |
| 24.39 | 2.71 | 2.50 | 9.35 | 2.50 | 24.0 | 2.75 | 3.2599 | 1.50231 | 3.2599 | 1.50231 | | |
| 25.00 | 2.62 | 2.76 | 9.4 | 2.76 | 25.0 | 2.80 | 0.2609 | 1.50180 | 0.2609 | 1.50180 | | |
| 28.57 | 2.33 | 2.98 | 9.5 | 2.98 | | | 0.2618 | 1.49139 | 0.2618 | 1.49139 | | |
| 33.33 | 2.19 | 3.00 | 9.6 | 3.00 | | | 0.2666 | 1.49932 | 0.2666 | 1.49932 | | |
| 46.00 | 2.12 | 2.98 | 9.7 | 2.98 | | | 0.2689 | 1.49834 | 0.2689 | 1.49834 | | |
| 50.00 | 2.06 | 2.87 | 9.8 | 2.87 | | | 0.2700 | 1.49781 | 0.2700 | 1.49781 | | |
| | | 2.77 | 9.9 | 2.77 | | | 0.2713 | 1.49735 | 0.2713 | 1.49735 | | |
| | | 2.62 | 10.0 | 2.62 | | | 0.2718 | 1.49714 | 0.2718 | 1.49714 | | |
| | | 2.36 | 10.2 | 2.36 | | | 0.2745 | 1.49610 | 0.2745 | 1.49610 | | |
| | | 2.22 | 10.4 | 2.22 | | | 0.2769 | 1.49516 | 0.2769 | 1.49516 | | |
| | 1.05 | 2.00 | 10.6 | 2.00 | | | 0.2824 | 1.49321 | 0.2824 | 1.49321 | | |
| 7.0 | 1.04 | 1.99 | 10.8 | 1.99 | | | 0.2837 | 1.49274 | 0.2837 | 1.49274 | | |
| 7.1 | 1.02 | 1.93 | 11.0 | 1.93 | | | 0.2877 | 1.49138 | 0.2877 | 1.49138 | | |
| 7.2 | 1.00 | 1.89 | 11.2 | 1.89 | | | 0.2961 | 1.48879 | 0.2961 | 1.48879 | | |
| 7.3 | 0.96 | 1.84 | 11.4 | 1.84 | | | | | | | | |
| 7.4 | 0.93 | 1.79 | 11.6 | 1.79 | | | | | | | | |
| 7.5 | 0.93 | 1.73 | 11.8 | 1.73 | | | | | | | | |
| 7.6 | 0.90 | 1.71 | 12.0 | 1.71 | | | | | | | | |
| 7.7 | 0.83 | 1.72 | 12.2 | 1.72 | | | | | | | | |
| 7.8 | 0.76 | 1.80 | 12.4 | 1.80 | | | | | | | | |
| 7.9 | 0.645 | 1.87 | 12.6 | 1.87 | | | | | | | | |
| 8.0 | 0.50 | 1.98 | 12.8 | 1.98 | | | | | | | | |
| 8.1 | 0.374 | 1.95 | 13.0 | 1.95 | | | | | | | | |
| 8.2 | 0.38 | 1.91 | 13.2 | 1.91 | | | | | | | | |
| 8.3 | 0.417 | 1.89 | 13.4 | 1.89 | | | | | | | | |
| 8.4 | 0.45 | 1.84 | 13.6 | 1.84 | | | | | | | | |
| 8.5 | 0.448 | 1.79 | 13.8 | 1.79 | | | | | | | | |
| 8.6 | 0.433 | 1.76 | 14.0 | 1.76 | | | | | | | | |
| 8.65 | 0.42 | 1.73 | 14.2 | 1.73 | | | | | | | | |
| 8.7 | 0.39 | 1.71 | 14.4 | 1.71 | | | | | | | | |
| 8.75 | 0.37 | 1.69 | 14.6 | 1.69 | | | | | | | | |
| 8.8 | 0.33 | 1.68 | 16.0 | 1.68 | | | | | | | | |
| 8.85 | 0.32 | 1.26 | 18.0 | 1.26 | | | | | | | | |
| 8.9 | 0.336 | 1.02 | 19.0 | 1.02 | | | | | | | | |
| 8.95 | 0.46 | 0.64 | 20.0 | 0.64 | | | | | | | | |
| 9.0 | 0.74 | 0.52 | 20.5 | 0.52 | | | | | | | | |
| 9.05 | 1.14 | 1.30 | 21.0 | 1.30 | | | | | | | | |
| 9.1 | 1.84 | 2.24 | 21.5 | 2.24 | | | | | | | | |
| 9.15 | 1.95 | 2.59 | 22.0 | 2.59 | | | | | | | | |
| 9.2 | 2.20 | | | | | | | | | | | |

CURVE 12
T = 291.7

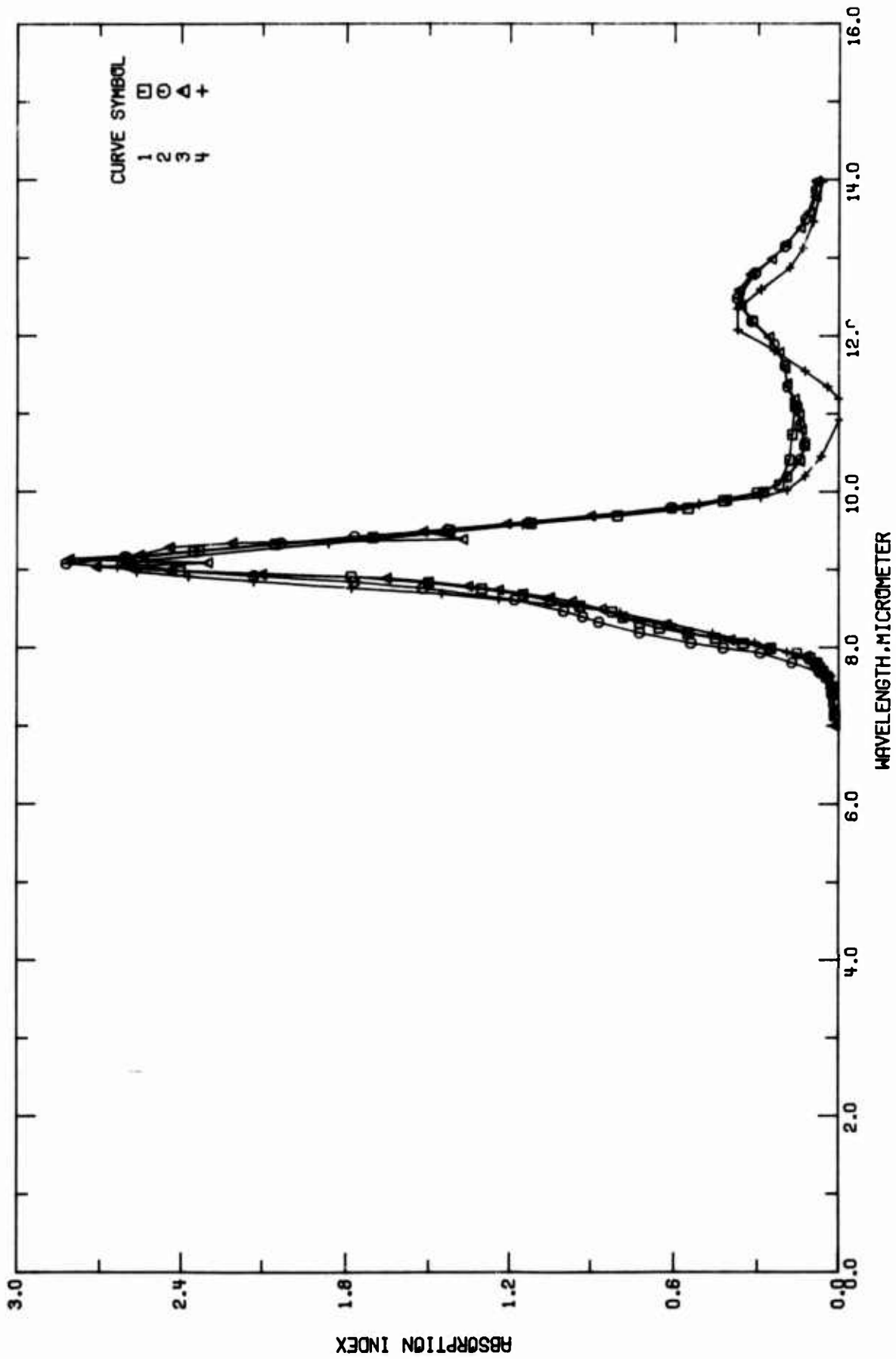


FIGURE 11-4. EXPERIMENTAL ABSORPTION INDEX OF SILICA (VITREOUS)
(WAVELENGTH DEPENDENCE).

TABLE 11-6. MEASUREMENT INFORMATION ON THE ABSORPTION INDEX OF SILICA(VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 E45777 | Zolotarev, V.M. | 1970 | 7.1-11 | ~293 | Fused Quartz | Several overlapping methods used to determine absorption index; measurement temperature not explicitly given, assumed to be 293 K. |
| 2 E64649 | Popova, S.L., Tolstykh, T.S., and Vorobev, V.T. | 1972 | 7.1-50 | 293 | Amorphous Quartz | Total impurity content (CaCO_3 , sodium chloride, and oxides of Al, Mg, Cu, Ca, and Fe) < 0.007; SiO_2 samples of grades KU and KI used; refractive index n and absorption index k derived from reflectance spectra; measurement temperature not given explicitly, assumed to be 293 K. |
| 3 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 7.0-26.0 | 293 | Fused Silica | Absorption index values for wavelengths shorter than 9 μm based on data in [T060820] (curve 1 above), for longer wavelengths based on data in [E64649] (curve 2 above). |
| 4 E64850 | Crozler, D. and Douglas, R.W. | 1965 | 7.5-14 | 293 | Fused Silica | 100 SiO_2 ; blown films prepared, selected areas stuck on copper wire loops and absorption spectra determined on a Grubb Parsons double-beam spectrometer; thin film method of Blain and Douglas used to analyze spectra to give refractive index and absorption index; measurement temperature not given explicitly, assumed to be 293 K. |

b. Angular Spectral Emittance (Wavelength Dependence)

A total of 11 sets of experimental data were located for the wavelength dependence of the angular spectral emittance of vitreous silica. The data are listed in Table 11-10 and shown in Figures 11-5 and 11-6. Specimen characterization and measurement information for the data are given in Table 11-9.

All 11 sets apply to Optosil 1 and were measured at a specimen temperature of 373 K using the Honeywell spectral emissometer. The minima in the curves are closer to 8 μm than 9 μm which was the same phenomenon observed for Honeywell data in the normal spectral emittance section.

A set of provisional values for optically smooth vitreous silica at 293 K, a viewing angle θ' of 40° , and a wavelength range of 7.0 to 16.0 μm is listed in Table 11-8 and shown in Figure 11-5. The values were calculated using Eqs. (2.4-1) to (2.4-5) and Eq. (2.4-8). Equation (2.4-8) includes Kirchhoff's law equating the emittance to the absorptance. The index of refraction and absorption index data were taken from Champetier and Friese [A00012] as mentioned in the section on the wavelength dependence of the normal spectral emittance. Because the index of refraction and absorption index data are themselves not evaluated and because good experimental data has not been located, the values for the angular spectral emittance are called provisional with an uncertainty which is thought to be within 30%.

TABLE 11-3. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, κ ; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ |
|----------------------|------------|-----------|------------|
| OPTICALLY SMOOTH | | | |
| $\theta' = 40^\circ$ | | | |
| T = 293 (CONT.) | | | |
| 7.00 | 0.999 | 10.4 | 0.849 |
| 7.10 | 0.999 | 10.6 | 0.891 |
| 7.20 | 1.000 | 10.8 | 0.882 |
| 7.30 | 1.000 | 11.0 | 0.890 |
| 7.40 | 0.999 | 11.2 | 0.896 |
| 7.50 | 0.998 | 11.4 | 0.902 |
| 7.60 | 0.997 | 11.6 | 0.908 |
| 7.70 | 0.991 | 11.8 | 0.915 |
| 7.80 | 0.950 | 12.0 | 0.916 |
| 7.90 | 0.822 | 12.2 | 0.910 |
| 8.00 | 0.688 | 12.4 | 0.896 |
| 8.10 | 0.577 | 12.6 | 0.887 |
| 8.20 | 0.508 | 12.8 | 0.875 |
| 8.30 | 0.615 | 13.0 | 0.883 |
| 8.40 | 0.609 | 13.2 | 0.891 |
| 8.50 | 0.585 | 13.4 | 0.896 |
| 8.60 | 0.541 | 13.6 | 0.904 |
| 8.65 | 0.507 | 13.8 | 0.912 |
| 8.70 | 0.455 | 14.0 | 0.917 |
| 8.75 | 0.414 | 14.2 | 0.921 |
| 8.80 | 0.354 | 14.4 | 0.848 |
| 8.85 | 0.312 | 14.6 | 0.928 |
| 8.90 | 0.293 | 16.0 | 0.954 |
| 8.95 | 0.280 | | |
| 9.00 | 0.330 | | |
| 9.05 | 0.384 | | |
| 9.10 | 0.534 | | |
| 9.15 | 0.472 | | |
| 9.20 | 0.527 | | |
| 9.30 | 0.548 | | |
| 9.35 | 0.504 | | |
| 9.40 | 0.687 | | |
| 9.50 | 0.656 | | |
| 9.60 | 0.686 | | |
| 9.70 | 0.714 | | |
| 9.80 | 0.745 | | |
| 9.90 | 0.767 | | |
| 10.0 | 0.791 | | |
| 10.2 | 0.828 | | |

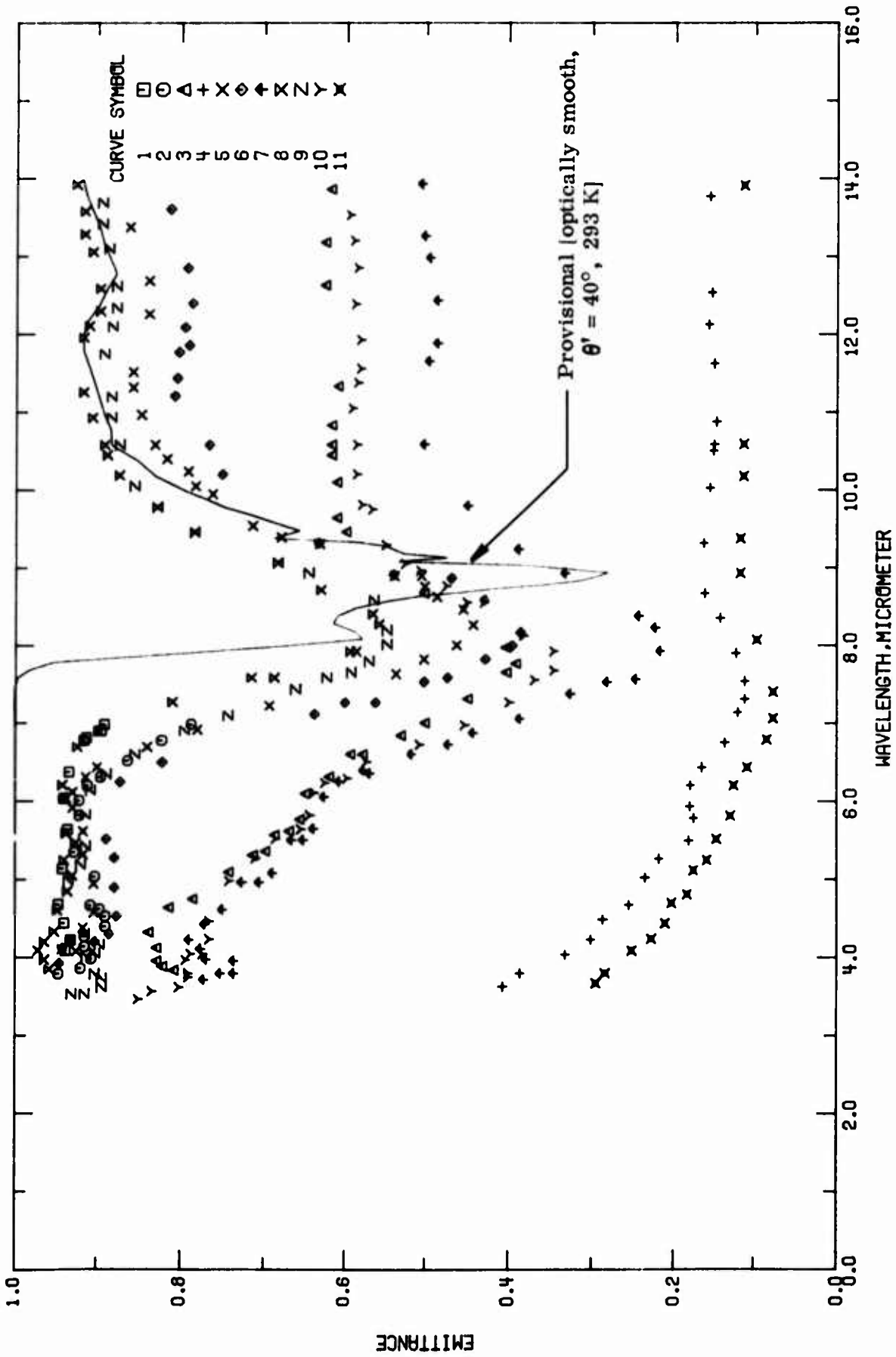


FIGURE 11-5. PROVISIONAL ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

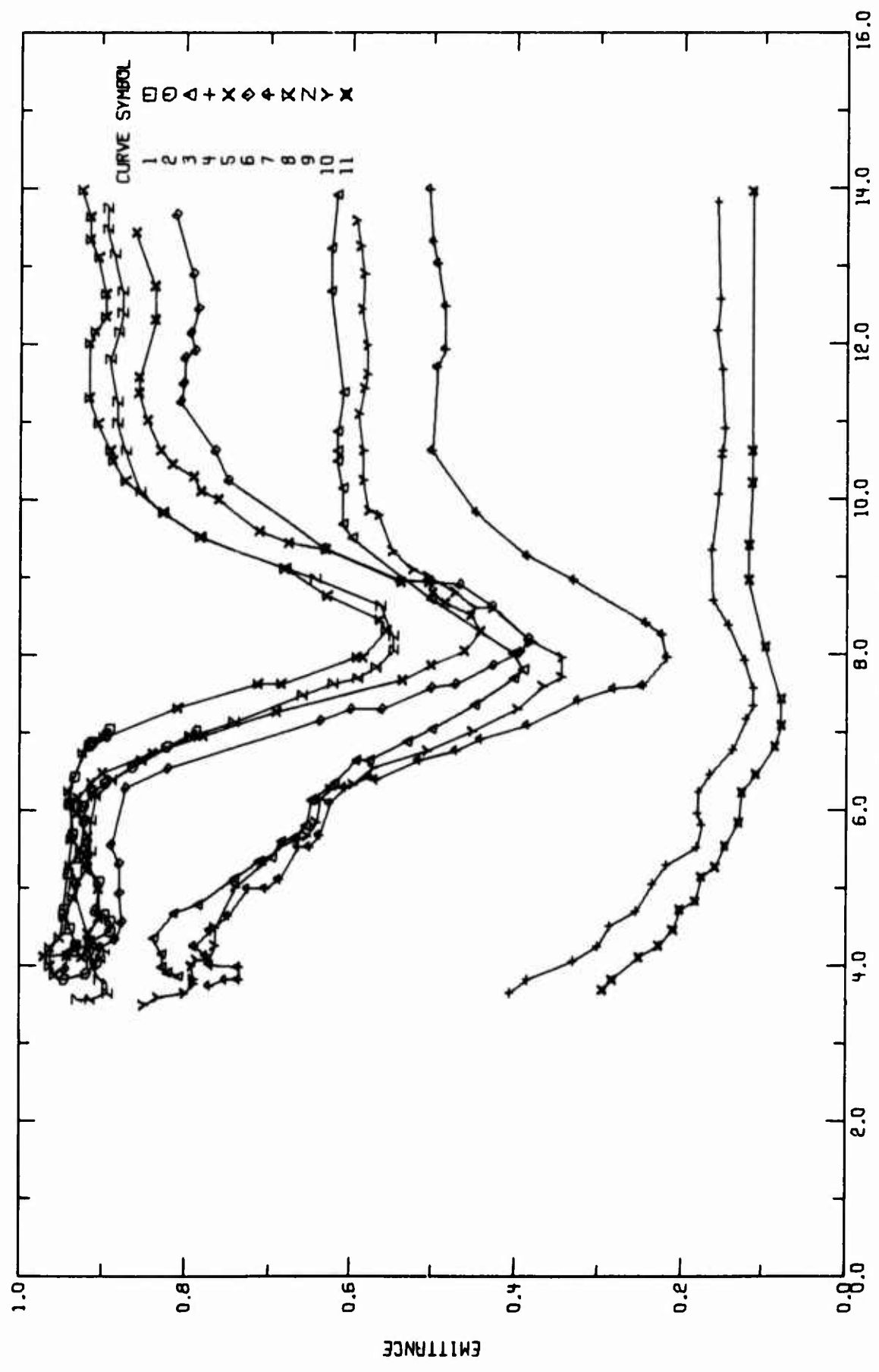


FIGURE 11-6. EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

TABLE 11-9. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 4.1-7.0 | 373 | Optosil 1 | Specimen thickness 0.125 in.; polished disk; Honeywell spectral emissometer used which includes a Leiss double prism monochromator with prisms of potassium or cesium bromide; computed system band width 0.19 μm ; optics, chopper, and enclosure near 300 K while sample and black body reference are heated to 373 K; polarization of monochromator which is present has not been removed from data; 0° data taken but not reported, the 0° and 12° data were identical; emittance data for parallel polarization; a conclusion in this report [A00012] is that "Honeywell emissometer currently produces incorrect data at angles greater than 40 degrees and previously generated data cannot be used with confidence in their validity"; smooth values from figure; because of overlap of curves, data could not be extracted for full wavelength range for which data reported; $\theta' = 30^\circ$. |
| 2 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.8-7.0 | 373 | Optosil 1 | Similar to the above specimen; $\theta' = 40^\circ$. |
| 3 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.8-30 | 373 | Optosil 1 | Similar to the above specimen except data extracted for full wavelength range for which it is reported; $\theta' = 50^\circ$. |
| 4 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.6-30 | 373 | Optosil 1 | Similar to the above specimen except data reported for θ' of 70° and 75°, however, it could not be extracted due to overlap of curves; $\theta' = 60^\circ$. |
| 5 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 4.1-19 | 373 | Optosil 1 | Similar to the above specimen except data reported for perpendicular polarization and because of overlap of curves, data could not be extracted for full wavelength range; $\theta' = 30^\circ$. |
| 6 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.9-19 | 373 | Optosil 1 | Similar to the above specimen; $\theta' = 40^\circ$. |
| 7 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.7-30 | 373 | Optosil 1 | Similar to the above specimen except data extracted for full wavelength range for which it is reported; in addition, data reported for θ' of 60°, 70°, and 75°, however, it could not be extracted due to overlap of curves; $\theta' = 50^\circ$. |
| 8 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.9-20 | 373 | Optosil 1 | Similar to the above specimen except data reported for unpolarized radiation and because of overlap of curves, data could not be extracted for the full wavelength range for which data reported; $\theta' = 30^\circ$. |
| 9 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.5-20 | 373 | Optosil 1 | Similar to the above specimen; $\theta' = 40^\circ$. |
| 10 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.5-30 | 373 | Optosil 1 | Similar to the above specimen except data extracted for full wavelength range for which it is reported; $\theta' = 50^\circ$. |
| 11 A00012 | Champetier, R.J. and Friese, G.J. | 1974 | 3.7-30 | 373 | Optosil 1 | Similar to the above specimen except data reported for θ' of 70° and 75°, however, it could not be extracted due to the overlap of the curves; $\theta' = 60^\circ$. |

TABLE 11-10. EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|
| CURVE 4 (CONT.) | | CURVE 5 (CONT.) | | CURVE 6 (CONT.) | | CURVE 7 (CONT.) | | CURVE 7 (CONT.) | | CURVE 7 (CONT.) | | CURVE 7 (CONT.) | |
| 29.10 | 0.173 | 10.26 | 0.790 | 8.01 | 0.395 | 4.11 | 0.774 | 15.80 | 0.581 | 25.35 | 0.427 | 25.35 | 0.427 |
| 29.32 | 0.173 | 10.42 | 0.815 | 8.10 | 0.385 | 4.23 | 0.780 | 16.37 | 0.581 | 25.66 | 0.401 | 25.66 | 0.401 |
| 29.46 | 0.235 | 10.60 | 0.829 | 8.60 | 0.427 | 4.43 | 0.769 | 16.67 | 0.571 | 25.87 | 0.405 | 25.87 | 0.405 |
| 29.57 | 0.247 | 10.99 | 0.845 | 8.80 | 0.467 | 4.62 | 0.747 | 17.27 | 0.530 | 25.95 | 0.399 | 25.95 | 0.399 |
| 29.73 | 0.229 | 11.34 | 0.855 | 8.93 | 0.539 | 4.97 | 0.724 | 17.59 | 0.522 | 25.95 | 0.380 | 25.95 | 0.380 |
| 29.73 | 0.213 | 11.54 | 0.836 | 9.34 | 0.633 | 4.97 | 0.704 | 18.10 | 0.571 | 26.18 | 0.365 | 26.18 | 0.365 |
| 30.00 | 0.199 | 12.28 | 0.836 | 10.22 | 0.748 | 5.09 | 0.688 | 18.21 | 0.585 | 26.26 | 0.355 | 26.26 | 0.355 |
| CURVE 5 | | 12.71 | 0.836 | 10.60 | 0.764 | 5.51 | 0.665 | 18.38 | 0.592 | 26.26 | 0.343 | 26.26 | 0.343 |
| T = 373. | | 13.40 | 0.859 | 11.23 | 0.806 | 5.51 | 0.651 | 18.59 | 0.577 | 26.42 | 0.343 | 26.42 | 0.343 |
| | | 14.09 | 0.868 | 11.46 | 0.803 | 5.66 | 0.639 | 18.97 | 0.569 | 26.50 | 0.394 | 26.50 | 0.394 |
| | | 14.63 | 0.887 | 11.79 | 0.801 | 6.07 | 0.626 | 19.25 | 0.523 | 26.58 | 0.384 | 26.58 | 0.384 |
| 4.10 | 0.970 | 15.55 | 0.887 | 11.88 | 0.785 | 6.27 | 0.607 | 19.42 | 0.502 | 26.90 | 0.401 | 26.90 | 0.401 |
| 4.11 | 0.941 | 15.93 | 0.899 | 12.11 | 0.794 | 6.41 | 0.576 | 19.55 | 0.468 | 27.04 | 0.424 | 27.04 | 0.424 |
| 4.09 | 0.923 | 16.50 | 0.899 | 12.42 | 0.785 | 6.37 | 0.568 | 19.72 | 0.453 | 27.09 | 0.498 | 27.09 | 0.498 |
| 4.39 | 0.915 | 16.93 | 0.911 | 12.87 | 0.791 | 6.62 | 0.516 | 19.81 | 0.423 | 27.25 | 0.513 | 27.25 | 0.513 |
| 4.59 | 0.902 | 17.54 | 0.911 | 13.83 | 0.811 | 6.74 | 0.471 | 20.18 | 0.384 | 27.34 | 0.502 | 27.34 | 0.502 |
| 4.96 | 0.902 | 18.60 | 0.934 | 14.01 | 0.821 | 6.89 | 0.441 | 20.18 | 0.351 | 27.34 | 0.465 | 27.34 | 0.465 |
| 5.33 | 0.915 | 18.79 | 0.882 | 14.18 | 0.834 | 7.07 | 0.386 | 20.49 | 0.289 | 27.49 | 0.461 | 27.49 | 0.461 |
| 5.63 | 0.915 | 19.00 | 0.874 | 14.53 | 0.838 | 7.39 | 0.325 | 20.72 | 0.249 | 27.49 | 0.445 | 27.49 | 0.445 |
| 5.93 | 0.928 | 15.01 | 0.838 | 15.01 | 0.838 | 7.54 | 0.282 | 20.84 | 0.218 | 27.61 | 0.448 | 27.61 | 0.448 |
| 6.13 | 0.928 | 15.45 | 0.850 | 15.45 | 0.850 | 7.58 | 0.248 | 21.10 | 0.193 | 27.69 | 0.447 | 27.69 | 0.447 |
| 6.32 | 0.912 | 16.09 | 0.862 | 16.09 | 0.862 | 7.94 | 0.218 | 21.34 | 0.193 | 27.73 | 0.470 | 27.73 | 0.470 |
| 6.45 | 0.898 | 16.61 | 0.871 | 16.61 | 0.871 | 8.24 | 0.224 | 21.57 | 0.214 | 27.81 | 0.475 | 27.81 | 0.475 |
| 6.71 | 0.838 | 17.28 | 0.876 | 17.28 | 0.876 | 8.39 | 0.244 | 21.69 | 0.234 | 27.81 | 0.451 | 27.81 | 0.451 |
| 6.93 | 0.778 | 17.46 | 0.869 | 17.46 | 0.869 | 8.94 | 0.331 | 22.01 | 0.245 | 28.06 | 0.445 | 28.06 | 0.445 |
| 7.24 | 0.692 | 17.59 | 0.867 | 17.59 | 0.867 | 9.25 | 0.387 | 22.40 | 0.285 | 28.14 | 0.372 | 28.14 | 0.372 |
| 7.65 | 0.536 | 18.09 | 0.880 | 18.09 | 0.880 | 9.81 | 0.447 | 22.62 | 0.307 | 28.17 | 0.436 | 28.17 | 0.436 |
| 7.84 | 0.501 | 18.39 | 0.888 | 18.39 | 0.888 | 10.60 | 0.501 | 22.78 | 0.317 | 28.27 | 0.456 | 28.27 | 0.456 |
| 8.02 | 0.461 | 18.58 | 0.882 | 18.58 | 0.882 | 11.67 | 0.495 | 22.98 | 0.320 | 28.44 | 0.495 | 28.44 | 0.495 |
| 8.28 | 0.441 | 18.80 | 0.882 | 18.80 | 0.882 | 11.90 | 0.485 | 23.18 | 0.316 | 28.44 | 0.437 | 28.44 | 0.437 |
| 8.48 | 0.453 | 19.00 | 0.874 | 19.00 | 0.874 | 12.45 | 0.485 | 23.49 | 0.341 | 28.63 | 0.410 | 28.63 | 0.410 |
| 8.64 | 0.485 | 19.00 | 0.874 | 19.00 | 0.874 | 13.00 | 0.494 | 23.70 | 0.351 | 28.81 | 0.442 | 28.81 | 0.442 |
| 8.77 | 0.500 | 6.26 | 0.870 | 6.26 | 0.870 | 13.20 | 0.500 | 24.16 | 0.355 | 28.90 | 0.469 | 28.90 | 0.469 |
| 8.91 | 0.504 | 6.51 | 0.820 | 6.51 | 0.820 | 13.20 | 0.504 | 24.35 | 0.373 | 28.92 | 0.512 | 28.92 | 0.512 |
| 9.33 | 0.538 | 7.13 | 0.638 | 7.13 | 0.638 | 14.26 | 0.492 | 24.52 | 0.395 | 29.10 | 0.487 | 29.10 | 0.487 |
| 9.33 | 0.632 | 7.28 | 0.600 | 7.28 | 0.600 | 14.48 | 0.487 | 24.67 | 0.401 | 29.38 | 0.550 | 29.38 | 0.550 |
| 9.41 | 0.678 | 7.28 | 0.561 | 7.28 | 0.561 | 14.77 | 0.487 | 24.89 | 0.391 | 29.46 | 0.638 | 29.46 | 0.638 |
| 9.56 | 0.712 | 7.55 | 0.501 | 7.55 | 0.501 | 15.10 | 0.521 | 25.19 | 0.430 | 29.46 | 0.524 | 29.46 | 0.524 |
| 9.97 | 0.760 | 7.60 | 0.474 | 7.60 | 0.474 | 15.41 | 0.544 | 25.27 | 0.443 | 29.62 | 0.465 | 29.62 | 0.465 |
| 10.07 | 0.781 | 7.84 | 0.426 | 7.84 | 0.426 | 15.68 | 0.571 | 25.35 | 0.437 | 29.69 | 0.491 | 29.69 | 0.491 |

CURVE 7
T = 373.

3.72 0.770

3.80 0.750

3.80 0.734

3.96 0.774

3.98 0.767

TABLE 11-10. EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|------------------|------------|------------------|------------|------------------|------------|
| CURVE 7 (CONT.) | | CURVE 8 (CONT.) | | CURVE 9 (CONT.) | | CURVE 9 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | |
| 30.00 | 0.519 | 13.31 | 0.914 | 5.44 | 0.912 | 19.55 | 0.875 | 9.63 | 0.570 | 21.90 | 0.410 | | |
| | | 13.60 | 0.914 | 5.84 | 0.912 | 19.80 | 0.835 | 10.22 | 0.585 | 22.10 | 0.422 | | |
| CURVE 8 | | 13.94 | 0.924 | 6.15 | 0.906 | 20.00 | 0.812 | 10.60 | 0.585 | 22.35 | 0.450 | | |
| T = 373. | | 14.10 | 0.910 | 6.36 | 0.887 | | | 11.07 | 0.591 | 22.53 | 0.470 | | |
| | | 14.28 | 0.920 | 6.61 | 0.852 | CURVE 10 | | 11.40 | 0.584 | 22.87 | 0.481 | | |
| 3.86 | 0.920 | 14.79 | 0.918 | 6.92 | 0.794 | T = 373. | | 11.50 | 0.580 | 23.25 | 0.480 | | |
| 3.98 | 0.962 | 15.04 | 0.926 | 7.11 | 0.741 | | | 11.95 | 0.580 | 23.52 | 0.500 | | |
| 4.21 | 0.962 | 15.39 | 0.930 | 7.45 | 0.661 | 3.47 | 0.848 | 12.41 | 0.587 | 23.84 | 0.494 | | |
| 4.34 | 0.950 | 15.52 | 0.926 | 7.60 | 0.623 | 3.57 | 0.832 | 12.87 | 0.584 | 24.03 | 0.505 | | |
| 4.61 | 0.946 | 15.95 | 0.936 | 7.67 | 0.592 | 3.62 | 0.800 | 13.22 | 0.589 | 24.19 | 0.527 | | |
| 4.86 | 0.934 | 16.31 | 0.936 | 7.81 | 0.569 | 3.75 | 0.789 | 13.55 | 0.594 | 24.46 | 0.524 | | |
| 5.06 | 0.920 | 16.58 | 0.940 | 8.03 | 0.547 | 3.80 | 0.789 | 14.20 | 0.550 | 24.66 | 0.537 | | |
| 5.26 | 0.938 | 16.71 | 0.940 | 8.21 | 0.547 | 3.97 | 0.792 | 14.37 | 0.550 | 24.70 | 0.561 | | |
| 5.48 | 0.924 | 16.89 | 0.942 | 8.60 | 0.563 | 4.05 | 0.786 | 15.01 | 0.583 | 25.02 | 0.580 | | |
| 5.60 | 0.936 | 17.12 | 0.938 | 8.95 | 0.645 | 4.05 | 0.771 | 15.24 | 0.599 | 25.13 | 0.610 | | |
| 6.05 | 0.936 | 17.49 | 0.945 | 9.08 | 0.682 | 4.24 | 0.763 | 15.33 | 0.608 | 25.22 | 0.616 | | |
| 6.22 | 0.940 | 17.76 | 0.942 | 9.48 | 0.782 | 4.47 | 0.763 | 15.59 | 0.622 | 25.34 | 0.611 | | |
| 6.71 | 0.922 | 18.05 | 0.942 | 9.80 | 0.826 | 4.99 | 0.739 | 16.00 | 0.631 | 25.46 | 0.570 | | |
| 6.91 | 0.890 | 18.46 | 0.949 | 10.07 | 0.853 | 5.28 | 0.708 | 16.16 | 0.628 | 25.87 | 0.562 | | |
| 7.29 | 0.808 | 18.70 | 0.949 | 10.60 | 0.871 | 5.53 | 0.684 | 16.54 | 0.617 | 26.05 | 0.535 | | |
| 7.60 | 0.713 | 18.93 | 0.945 | 10.95 | 0.881 | 5.65 | 0.643 | 16.80 | 0.585 | 26.30 | 0.490 | | |
| 7.60 | 0.686 | 19.12 | 0.933 | 11.22 | 0.881 | 5.83 | 0.643 | 17.28 | 0.561 | 26.50 | 0.469 | | |
| 7.94 | 0.593 | 19.34 | 0.914 | 11.77 | 0.890 | 6.12 | 0.638 | 17.76 | 0.592 | 26.73 | 0.485 | | |
| 7.94 | 0.585 | 19.51 | 0.897 | 12.12 | 0.880 | 6.25 | 0.625 | 18.04 | 0.612 | 26.80 | 0.499 | | |
| 8.29 | 0.550 | 20.00 | 0.842 | 12.36 | 0.875 | 6.31 | 0.597 | 18.47 | 0.612 | 27.02 | 0.572 | | |
| 8.42 | 0.504 | | | 12.64 | 0.875 | 6.52 | 0.572 | 18.89 | 0.596 | 27.08 | 0.610 | | |
| 8.73 | 0.630 | | | 13.12 | 0.885 | 6.74 | 0.506 | 19.30 | 0.572 | 27.16 | 0.620 | | |
| 9.08 | 0.682 | | | 13.44 | 0.893 | 6.99 | 0.451 | 19.61 | 0.547 | 27.25 | 0.616 | | |
| 9.48 | 0.782 | | | 13.71 | 0.893 | 7.20 | 0.398 | 19.96 | 0.512 | 27.41 | 0.560 | | |
| 9.80 | 0.820 | | | 14.05 | 0.889 | 7.57 | 0.368 | 20.22 | 0.461 | 27.97 | 0.549 | | |
| 10.21 | 0.871 | | | 14.45 | 0.896 | 7.69 | 0.345 | 20.31 | 0.431 | 28.25 | 0.578 | | |
| 10.47 | 0.886 | | | 14.93 | 0.897 | 7.94 | 0.345 | 20.44 | 0.415 | 28.52 | 0.539 | | |
| 10.60 | 0.889 | | | 15.33 | 0.907 | 8.14 | 0.381 | 20.68 | 0.362 | 28.85 | 0.522 | | |
| 10.95 | 0.904 | | | 15.20 | 0.906 | 8.57 | 0.427 | 20.90 | 0.339 | 28.85 | 0.519 | | |
| 11.28 | 0.915 | | | 16.73 | 0.920 | 8.78 | 0.473 | 21.22 | 0.323 | 29.17 | 0.545 | | |
| 11.90 | 0.915 | | | 17.55 | 0.916 | 8.98 | 0.524 | 21.54 | 0.360 | 29.36 | 0.559 | | |
| 12.13 | 0.908 | | | 18.00 | 0.916 | 9.07 | 0.548 | 21.72 | 0.376 | 29.57 | 0.548 | | |
| 12.32 | 0.895 | | | 18.81 | 0.925 | 9.31 | 0.548 | | | | | | |
| 12.61 | 0.895 | | | 19.02 | 0.917 | 9.77 | 0.565 | | | | | | |
| 13.00 | 0.904 | | | 19.20 | 0.909 | | | | | | | | |
| | | | | 19.20 | 0.910 | | | | | | | | |

TABLE 11-10. EXPERIMENTAL ANGULAR SPECTRAL EMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ |
|------------------|------------|------------------|------------|------------------|------------|
| CURVE 10 (CONT.) | | CURVE 11 (CONT.) | | CURVE 11 (CONT.) | |
| 29.73 | 0.557 | 19.22 | 0.099 | 30.00 | 0.133 |
| 30.00 | 0.556 | 19.45 | 0.099 | | |
| | | 19.97 | 0.083 | | |
| CURVE 11 | | 20.47 | 0.070 | | |
| T = 373. | | 20.75 | 0.073 | | |
| | | 21.15 | 0.073 | | |
| 3.67 | 0.295 | 21.42 | 0.090 | | |
| 3.80 | 0.284 | 21.55 | 0.097 | | |
| 4.09 | 0.252 | 22.33 | 0.097 | | |
| 4.24 | 0.228 | 22.94 | 0.106 | | |
| 4.44 | 0.211 | 23.52 | 0.101 | | |
| 4.70 | 0.203 | 23.96 | 0.101 | | |
| 4.81 | 0.184 | 24.14 | 0.104 | | |
| 5.12 | 0.176 | 24.28 | 0.111 | | |
| 5.25 | 0.159 | 24.54 | 0.111 | | |
| 5.52 | 0.147 | 24.64 | 0.129 | | |
| 5.82 | 0.130 | 24.75 | 0.146 | | |
| 6.21 | 0.126 | 24.95 | 0.146 | | |
| 6.44 | 0.109 | 25.61 | 0.112 | | |
| 6.80 | 0.085 | 25.80 | 0.114 | | |
| 7.07 | 0.077 | 26.00 | 0.109 | | |
| 7.41 | 0.077 | 26.00 | 0.095 | | |
| 8.08 | 0.097 | 26.26 | 0.086 | | |
| 8.94 | 0.118 | 26.45 | 0.093 | | |
| 9.39 | 0.118 | 26.56 | 0.109 | | |
| 10.19 | 0.114 | 27.07 | 0.133 | | |
| 10.60 | 0.114 | 27.24 | 0.133 | | |
| 13.93 | 0.114 | 27.55 | 0.105 | | |
| 14.13 | 0.106 | 27.87 | 0.121 | | |
| 14.69 | 0.103 | 28.21 | 0.121 | | |
| 14.99 | 0.121 | 28.47 | 0.112 | | |
| 15.57 | 0.130 | 28.47 | 0.102 | | |
| 15.07 | 0.130 | 28.67 | 0.080 | | |
| 16.89 | 0.106 | 28.83 | 0.080 | | |
| 17.47 | 0.106 | 28.91 | 0.106 | | |
| 17.74 | 0.118 | 29.00 | 0.133 | | |
| 18.02 | 0.118 | 29.34 | 0.152 | | |
| 18.39 | 0.106 | 29.43 | 0.143 | | |
| 18.59 | 0.103 | 29.43 | 0.125 | | |
| 18.82 | 0.114 | 29.58 | 0.121 | | |

c. Normal Spectral Reflectance (Wavelength Dependence)

A total of 16 sets of experimental data were located for the wavelength dependence of the normal spectral reflectance of vitreous silica. The data are listed in Table 11-13 and shown in Figures 11-7 and 11-8. Specimen characterization and measurement information for the data are given in Table 11-12. Calculations were carried out using the Fresnel equations for specular reflection, Eqs. (2.4-1), (2.4-2), and (2.4-5). These calculations appear as curves 17 to 25 in Tables 11-12 and 11-13 and in Figures 11-7 and 11-8.

The data above 7 μm shows a general trend. It rises sharply above 7.4 μm to a peak at about 9 μm and then decreases to about 0.1 at 12 μm . All the data is for room temperature, with the exception of Gaskell's [T39543] which were measured at up to 1173 K.

Provisional values are listed in Table 11-11 and shown in Figure 11-7. One curve is based on calculations using the Fresnel equations and is valid with the context of an optically smooth specimen, a temperature of 293 K, unpolarized radiation, a wavelength range of 7 to 16.0 μm , an angle of incidence, θ , of 0° , and a viewing angle, θ' , of 0° . The calculated values and curve 16 differ by about 30% at 12.8 μm and, therefore, the uncertainty for these provisional values are within 30%. A provisional curve for 1173 K is also given with a wavelength range of validity between 7.7 and 14 μm . These values are also listed in Table 11-11 and shown in Figure 11-7. These values are based on curve 10 and an uncertainty of 30% is assigned because of the lack of confirmatory data.

TABLE 11-11. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μ m; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ |
|------------------|-----------------|------------------|----------|-----------|----------|
| OPTICALLY SMOOTH | | OPTICALLY SMOOTH | | T = 1173 | |
| T = 293 | T = 293 (CONT.) | T = 293 (CONT.) | T = 1173 | T = 1173 | T = 1173 |
| 7.00 | 0.001 | 10.4 | 0.145 | 7.05 | 0.000 |
| 7.10 | 0.000 | 10.6 | 0.113 | 7.83 | 0.009 |
| 7.20 | 0.000 | 10.8 | 0.111 | 7.95 | 0.037 |
| 7.30 | 0.000 | 11.0 | 0.103 | 8.0 | 0.057 |
| 7.40 | 0.000 | 11.2 | 0.098 | 8.10 | 0.099 |
| 7.50 | 0.001 | 11.4 | 0.091 | 8.31 | 0.216 |
| 7.60 | 0.003 | 11.6 | 0.085 | 8.63 | 0.309 |
| 7.70 | 0.010 | 11.8 | 0.077 | 8.74 | 0.345 |
| 7.80 | 0.020 | 12.0 | 0.077 | 9.0 | 0.475 |
| 7.90 | 0.051 | 12.2 | 0.083 | 9.06 | 0.505 |
| 8.00 | 0.135 | 12.4 | 0.097 | 9.15 | 0.510 |
| 8.10 | 0.269 | 12.6 | 0.106 | 9.25 | 0.497 |
| 8.20 | 0.314 | 12.8 | 0.119 | 9.59 | 0.368 |
| 8.30 | 0.305 | 13.0 | 0.110 | 9.88 | 0.278 |
| 8.40 | 0.336 | 13.2 | 0.102 | 10.0 | 0.247 |
| 8.50 | 0.368 | 13.4 | 0.097 | 10.1 | 0.220 |
| 8.60 | 0.422 | 13.6 | 0.089 | 10.5 | 0.160 |
| 8.65 | 0.461 | 13.8 | 0.081 | 10.9 | 0.120 |
| 8.70 | 0.521 | 14.0 | 0.077 | 11.0 | 0.116 |
| 8.75 | 0.567 | 14.2 | 0.072 | 11.5 | 0.087 |
| 8.80 | 0.632 | 14.4 | 0.143 | 11.9 | 0.078 |
| 8.85 | 0.679 | 14.6 | 0.065 | 12.0 | 0.077 |
| 8.90 | 0.702 | 14.8 | 0.039 | 12.2 | 0.078 |
| 8.95 | 0.719 | 15.0 | | 12.7 | 0.068 |
| 9.00 | 0.670 | | | 13.0 | 0.088 |
| 9.05 | 0.618 | | | 13.3 | 0.079 |
| 9.10 | 0.465 | | | 13.5 | 0.076 |
| 9.15 | 0.530 | | | | |
| 9.20 | 0.474 | | | | |
| 9.30 | 0.453 | | | | |
| 9.35 | 0.416 | | | | |
| 9.40 | 0.311 | | | | |
| 9.50 | 0.343 | | | | |
| 9.60 | 0.313 | | | | |
| 9.70 | 0.294 | | | | |
| 9.80 | 0.252 | | | | |
| 9.90 | 0.229 | | | | |
| 10.0 | 0.205 | | | | |
| 10.2 | 0.166 | | | | |

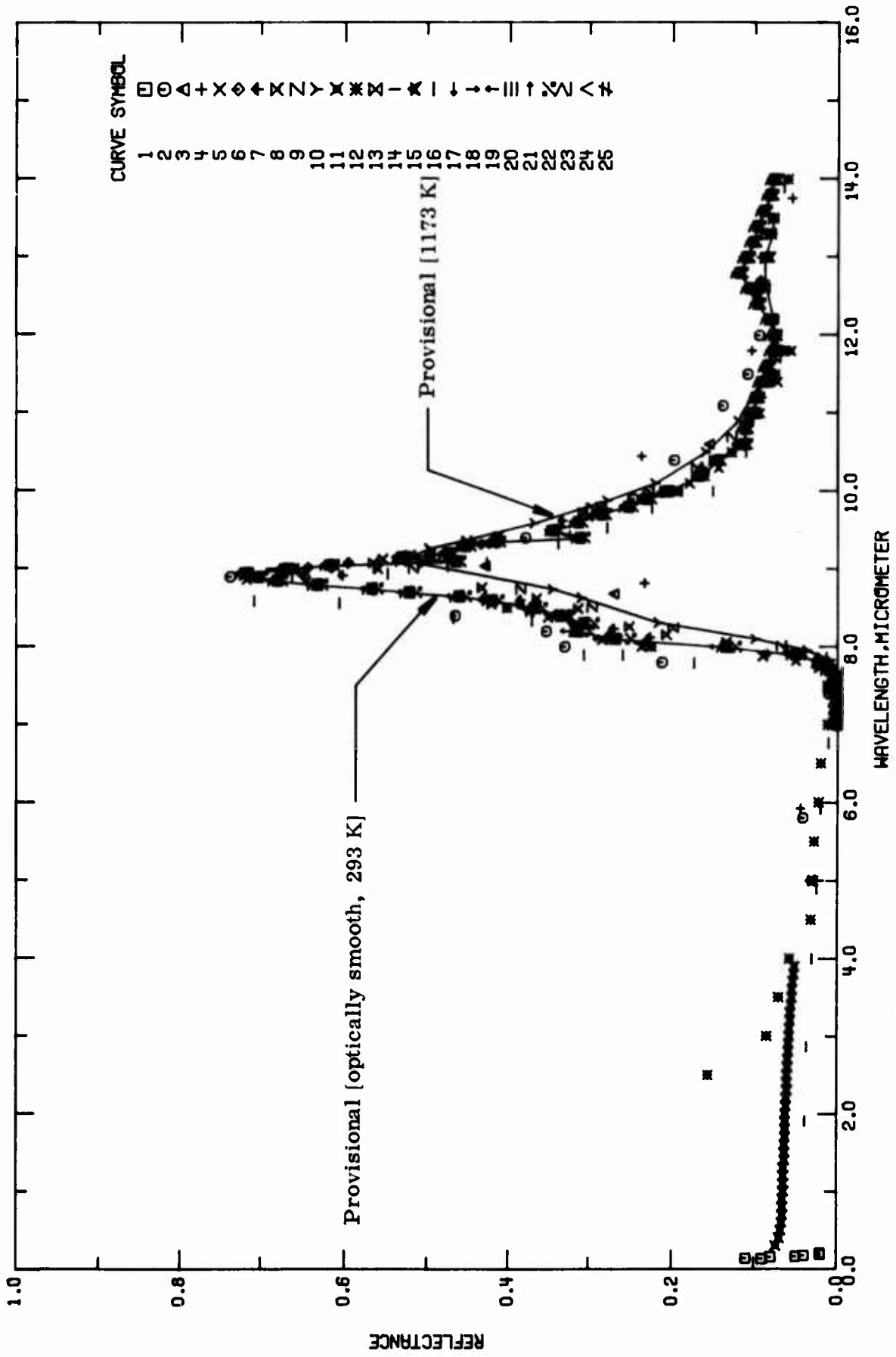


FIGURE 11-7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

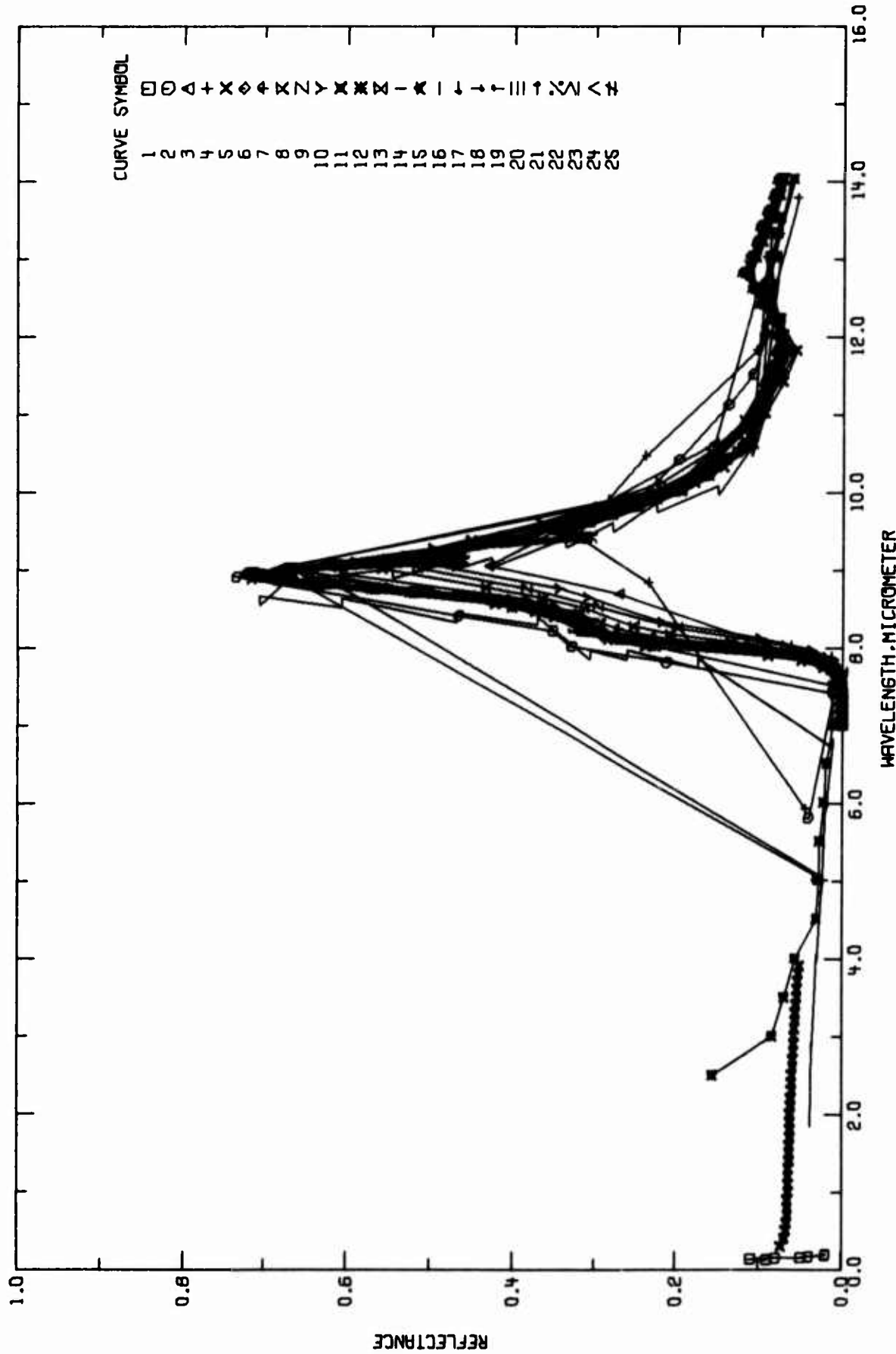


FIGURE 11-8. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

TABLE 11-12. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T31731 | Johnson, B.K. | 1941 | 0.13-0.20 | 293 | Fused quartz | Reflecting surface polished, back surface ground to prevent reflection from it; measured in vacuum (0.001 mm Hg); measurement temperature not given explicitly, assumed to be 293 K; data reported called reflection coefficient; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$. |
| 2 T40528 | Sulzbach, F. and Turner, A.F. | 1966 | 5.8-38 | 293 | Fused quartz | Measurement temperature specified as room temperature, 293 K assigned; data extracted from smooth curve; Perkin Elmer models 21 and 221 spectrophotometers used for reflectance measurements; $\theta \sim 0^\circ$. |
| 3 T40528 | Sulzbach, F. and Turner, A.F. | 1966 | 7.7-38 | 293 | | Clear film; electron beam deposited at normal incidence on glass at 588 K at 2 to 8×10^{-3} mm Hg; rate of deposit one quarterwave min^{-1} at $\lambda = 0.5 \mu\text{m}$; optical film thickness, i.e., index of refraction times thickness equals $10 \lambda/4$ at $2.5 \mu\text{m}$; measurement temperature specified as room temperature, 293 K assigned; data from figure; Perkin Elmer models 21 and 221 spectrophotometers used for reflectance measurements; $\theta \sim 0^\circ$. |
| 4 T40528 | Sulzbach, F. and Turner, A.F. | 1966 | 5.9-34 | 293 | | Unfilmed glass substrate; measurement temperature specified as room temperature, 293 K assigned; data from figure; Perkin Elmer models 21 and 221 spectrophotometers used for reflectance measurement; $\theta \sim 0^\circ$. |
| 5 T39543 | Gaskell, P.H. | 1965 | 7.5-14 | 293 | Vitreous silica | Plate specimen; author reports reflectivity; Perkin Elmer 12c spectrometer used; smooth values from figure; $\theta \sim 7^\circ$, $\theta' \sim 7^\circ$. |
| 6 T39543 | Gaskell, P.H. | 1965 | 7.5-14 | 480 | Vitreous silica | Similar to the above specimen. |
| 7 T39543 | Gaskell, P.H. | 1965 | 7.5-14 | 636 | Vitreous silica | Similar to the above specimen. |
| 8 T39543 | Gaskell, P.H. | 1965 | 7.6-14 | 796 | Vitreous silica | Similar to the above specimen. |
| 9 T39543 | Gaskell, P.H. | 1965 | 7.7-14 | 1036 | Vitreous silica | Similar to the above specimen. |
| 10 T39543 | Gaskell, P.H. | 1965 | 7.7-14 | 1173 | Vitreous silica | Similar to the above specimen. |
| 11 E62600, E21758 | | | 0.30-3.9 | 293 | Fused silica | Normal spectral reflectance calculated from $(n-1)^2/(n^2+1)$ (for polished, uncoated, plane-parallel plate, considering multiple internal reflections, and assuming zero absorption) where refractive index n was calculated using $n^2-1 = 0.6961663 \lambda^2/(\lambda^2 - (0.0684043)^2) + 0.4079426 \lambda^2/(\lambda^2 - (0.1162414)^2) - 0.8974794 \lambda^2/(\lambda^2 - (9.896161)^2)$, with wavelength λ in microns [E21758]; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 12 T76947 | General Dynamics Convair Aerospace Division | 1974 | 2.5-24 | 293 | Optosil 1 | Specimen thickness 0.125 in.; polished disk; specimen provided by Aerospace Corp. who obtained it from Amersil, Inc., Hillside, New Jersey; measurements made using the General Dynamics Convair Aerospace ellipsoidal reflectometer and a Perkin Elmer Model 210 monochromator for dispersion; data gathered without use of polarizers; reflectance obtained by comparison of reflected energy from specimen with that reflected by Convair vacuum-deposited gold sample; data gathered at atmospheric pressure; measurement temperature specified as room temperature, 293 K assigned; five readings taken of the gold standard and five of the specimen, average values used in determination of reflectance; $\theta = 12^\circ$, $\theta' = 12^\circ$. |
| 13 T76947 | General Dynamics Convair Aerospace Division | 1974 | 10-22 | 293 | Optosil 1, Convair Sample F | Specimen thickness 0.125 in.; polished disk; specimen provided by Aerospace Corp. who obtained it from Amersil, Inc., Hillside, New Jersey; measurements made using the General Dynamics Convair Aerospace ellipsoidal reflectometer and a Perkin Elmer Model 210 monochromator for dispersion and Advanced Ballistic Missile Defense Agency wire grid polarizers which were mounted as close as possible to the thermocouple detector; data gathered at atmospheric pressure; measurement temperature specified as room temperature, 293 K assigned; absolute reflectance determined directly; reflectance values reported are for component parallel to plane of incidence; five readings taken and average used in determining reflectance; data from figure; $\theta = 12^\circ$, $\theta' = 12^\circ$. |

TABLE 11-12. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 14 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen except reflectance values reported are for component perpendicular to the plane of incidence. |
| 15 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen except reflectance values reported are for average of the two polarized components. |
| 16 T30490 | Howarth, L. E. and Spitzer, W. G. | 1961 | 1.9-29 | 293 | Vitreous silica | Reflectivity measured by comparison with front surface aluminum mirror; Perkin Elmer single-beam double pass spectrometer used; measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$. |
| 17 A00012 | | 1975 | 7.0-16 | 293 | | Calculations for fused silica performed for a homogeneous, smooth surface and for perpendicular component (eq. 2.4-1) of incident radiation; data for index of refraction, n , and absorption index, k , from [A00012]; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 18 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta = 5^\circ$, $\theta' = 5^\circ$. |
| 19 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta = 10^\circ$, $\theta' = 10^\circ$. |
| 20 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for parallel component (eq. 2.4-2) of incident radiation and $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 21 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta = 5^\circ$, $\theta' = 5^\circ$. |
| 22 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta = 10^\circ$, $\theta' = 10^\circ$. |
| 23 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for unpolarized radiation (eq. 2.4-5) and $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 24 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for $\theta = 5^\circ$, $\theta' = 5^\circ$. |
| 25 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for $\theta = 10^\circ$, $\theta' = 10^\circ$. |

TABLE 11-13. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| CURVE 10 (CONT.) | | | CURVE 11 (CONT.) | | | CURVE 12 (CONT.) | | | CURVE 16 | | | CURVE 16 (CONT.) | | | CURVE 17 (CONT.) | | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|----------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
| CURVE 10 (CONT.) | | | CURVE 11 (CONT.) | | | CURVE 12 (CONT.) | | | CURVE 16 | | | CURVE 16 (CONT.) | | | CURVE 17 (CONT.) | | | |
| 10.9 | 0.120 | 3.10 | 0.658 | 13.0 | 0.631 | 13.0 | 0.239 | 1.90 | 0.239 | 21.4 | 0.475 | 9.10 | 0.4649 | 9.10 | 0.4649 | 9.10 | 0.4649 | |
| 11.5 | 0.087 | 3.20 | 0.657 | 21.0 | 0.257 | 21.0 | 0.037 | 2.06 | 0.037 | 21.9 | 0.405 | 9.15 | 0.5301 | 9.15 | 0.5301 | 9.15 | 0.5301 | |
| 11.9 | 0.078 | 3.30 | 0.657 | 21.0 | 0.553 | 21.0 | 0.031 | 3.99 | 0.031 | 23.5 | 0.264 | 9.20 | 0.4744 | 9.20 | 0.4744 | 9.20 | 0.4744 | |
| 12.2 | 0.078 | 3.40 | 0.656 | 22.0 | 0.306 | 22.0 | 0.025 | 4.89 | 0.025 | 23.9 | 0.236 | 9.30 | 0.4527 | 9.30 | 0.4527 | 9.30 | 0.4527 | |
| 12.7 | 0.088 | 3.50 | 0.655 | 23.0 | 0.206 | 23.0 | 0.021 | 5.92 | 0.021 | 24.4 | 0.222 | 9.35 | 0.4164 | 9.35 | 0.4164 | 9.35 | 0.4164 | |
| 13.0 | 0.088 | 3.60 | 0.654 | 24.0 | 0.227 | 24.0 | 0.011 | 6.75 | 0.011 | 25.9 | 0.191 | 9.40 | 0.3106 | 9.40 | 0.3106 | 9.40 | 0.3106 | |
| 13.3 | 0.0788 | 3.70 | 0.654 | CURVE 13 | | | 7.73 | 0.174 | 7.73 | 0.174 | 27.0 | 0.175 | 9.50 | 0.3433 | 9.50 | 0.3433 | 9.50 | 0.3433 |
| 13.5 | 0.078 | 3.80 | 0.653 | T = 293. | | | 7.89 | 0.259 | 7.89 | 0.259 | 28.4 | 0.169 | 9.60 | 0.3129 | 9.60 | 0.3129 | 9.60 | 0.3129 |
| CURVE 11 | | | CURVE 12 | | | CURVE 13 | | | CURVE 16 | | | CURVE 16 (CONT.) | | | CURVE 17 (CONT.) | | | |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | |
| 0.30 | 0.074 | 2.5 | 0.156 | 13.0 | 0.099 | 13.0 | 0.468 | 8.37 | 0.468 | 7.00 | 0.0006 | 10.6 | 0.1126 | 10.6 | 0.1126 | 10.6 | 0.1126 | |
| 0.50 | 0.068 | 3.0 | 0.085 | 13.0 | 0.088 | 13.0 | 0.077 | 8.56 | 0.077 | 7.10 | 0.0004 | 10.8 | 0.1114 | 10.8 | 0.1114 | 10.8 | 0.1114 | |
| 0.60 | 0.067 | 3.5 | 0.071 | 16.0 | 0.044 | 16.0 | 0.044 | 8.59 | 0.044 | 7.20 | 0.0001 | 11.0 | 0.1029 | 11.0 | 0.1029 | 11.0 | 0.1029 | |
| 0.70 | 0.066 | 4.0 | 0.058 | 22.0 | 0.364 | 22.0 | 0.364 | 8.91 | 0.364 | 7.30 | 0.0001 | 11.2 | 0.0977 | 11.2 | 0.0977 | 11.2 | 0.0977 | |
| 0.80 | 0.066 | 4.5 | 0.032 | CURVE 14 | | | 9.08 | 0.427 | 9.08 | 0.427 | 7.40 | 0.0001 | 11.4 | 0.0915 | 11.4 | 0.0915 | 11.4 | 0.0915 |
| 0.90 | 0.066 | 5.0 | 0.029 | T = 293. | | | 9.33 | 0.338 | 9.33 | 0.338 | 7.50 | 0.0015 | 11.6 | 0.0848 | 11.6 | 0.0848 | 11.6 | 0.0848 |
| 1.00 | 0.065 | 5.5 | 0.028 | 5.0 | 0.022 | 5.0 | 0.022 | 9.53 | 0.022 | 7.60 | 0.0031 | 11.8 | 0.0775 | 11.8 | 0.0775 | 11.8 | 0.0775 | |
| 1.10 | 0.065 | 6.0 | 0.023 | 9.0 | 0.687 | 9.0 | 0.687 | 9.78 | 0.274 | 7.70 | 0.0096 | 12.0 | 0.0771 | 12.0 | 0.0771 | 12.0 | 0.0771 | |
| 1.20 | 0.065 | 6.5 | 0.020 | 13.0 | 0.210 | 13.0 | 0.210 | 10.0 | 0.151 | 7.80 | 0.0024 | 12.2 | 0.0828 | 12.2 | 0.0828 | 12.2 | 0.0828 | |
| 1.30 | 0.065 | 7.0 | 0.012 | 13.0 | 0.108 | 13.0 | 0.108 | 10.5 | 0.111 | 7.90 | 0.0511 | 12.4 | 0.0966 | 12.4 | 0.0966 | 12.4 | 0.0966 | |
| 1.40 | 0.064 | 7.5 | 0.013 | 13.0 | 0.092 | 13.0 | 0.092 | 11.4 | 0.081 | 8.00 | 0.1351 | 12.6 | 0.1063 | 12.6 | 0.1063 | 12.6 | 0.1063 | |
| 1.50 | 0.064 | 8.0 | 0.025 | 16.0 | 0.049 | 16.0 | 0.049 | 12.9 | 0.089 | 8.10 | 0.2681 | 12.8 | 0.1186 | 12.8 | 0.1186 | 12.8 | 0.1186 | |
| 1.60 | 0.064 | 8.5 | 0.402 | 22.0 | 0.398 | 22.0 | 0.398 | 12.9 | 0.089 | 8.20 | 0.3137 | 13.0 | 0.1101 | 13.0 | 0.1101 | 13.0 | 0.1101 | |
| 1.70 | 0.063 | 9.0 | 0.667 | CURVE 15 | | | 13.9 | 0.065 | 13.9 | 0.065 | 8.30 | 0.3064 | 13.2 | 0.1010 | 13.2 | 0.1010 | 13.2 | 0.1010 |
| 1.80 | 0.063 | 9.5 | 0.347 | T = 293. | | | 14.9 | 0.055 | 14.9 | 0.055 | 8.40 | 0.3360 | 13.4 | 0.0970 | 13.4 | 0.0970 | 13.4 | 0.0970 |
| 1.90 | 0.063 | 10.0 | 0.195 | 5.0 | 0.660 | 5.0 | 0.660 | 16.0 | 0.047 | 8.50 | 0.3682 | 13.6 | 0.0887 | 13.6 | 0.0887 | 13.6 | 0.0887 | |
| 2.00 | 0.063 | 10.5 | 0.128 | 3.0 | 0.660 | 3.0 | 0.660 | 16.9 | 0.035 | 8.60 | 0.4216 | 13.8 | 0.0810 | 13.8 | 0.0810 | 13.8 | 0.0810 | |
| 2.10 | 0.062 | 11.0 | 0.100 | 3.0 | 0.660 | 3.0 | 0.660 | 17.9 | 0.025 | 8.70 | 0.4613 | 14.0 | 0.0766 | 14.0 | 0.0766 | 14.0 | 0.0766 | |
| 2.20 | 0.062 | 11.5 | 0.075 | 10.0 | 0.204 | 10.0 | 0.204 | 17.9 | 0.039 | 8.75 | 0.5207 | 14.2 | 0.0723 | 14.2 | 0.0723 | 14.2 | 0.0723 | |
| 2.30 | 0.061 | 12.0 | 0.073 | 11.0 | 0.104 | 11.0 | 0.104 | 18.9 | 0.031 | 8.80 | 0.5666 | 14.4 | 0.1433 | 14.4 | 0.1433 | 14.4 | 0.1433 | |
| 2.40 | 0.061 | 12.5 | 0.098 | 13.0 | 0.082 | 13.0 | 0.082 | 19.6 | 0.075 | 8.85 | 0.6325 | 14.6 | 0.0652 | 14.6 | 0.0652 | 14.6 | 0.0652 | |
| 2.50 | 0.061 | 13.0 | 0.066 | 16.0 | 0.051 | 16.0 | 0.051 | 19.9 | 0.146 | 8.90 | 0.6794 | 14.8 | 0.0610 | 14.8 | 0.0610 | 14.8 | 0.0610 | |
| 2.60 | 0.060 | 14.0 | 0.061 | 22.0 | 0.394 | 22.0 | 0.394 | 20.2 | 0.280 | 8.95 | 0.7018 | 15.0 | 0.0590 | 15.0 | 0.0590 | 15.0 | 0.0590 | |
| 2.70 | 0.060 | 15.0 | 0.049 | CURVE 16 | | | 20.3 | 0.406 | 20.3 | 0.406 | 9.00 | 0.6764 | 15.2 | 0.0552 | 15.2 | 0.0552 | 15.2 | 0.0552 |
| 2.80 | 0.059 | 16.0 | 0.044 | 17.0 | 0.036 | 17.0 | 0.036 | 20.7 | 0.503 | 9.05 | 0.6176 | 15.4 | 0.0510 | 15.4 | 0.0510 | 15.4 | 0.0510 | |
| 2.90 | 0.059 | 17.0 | 0.036 | 18.0 | 0.032 | 18.0 | 0.032 | 21.2 | 0.554 | 9.10 | 0.5616 | 15.6 | 0.0470 | 15.6 | 0.0470 | 15.6 | 0.0470 | |
| 3.00 | 0.058 | 18.0 | 0.032 | CURVE 17 | | | 21.2 | 0.508 | 21.2 | 0.508 | 9.15 | 0.5176 | 15.8 | 0.0430 | 15.8 | 0.0430 | 15.8 | 0.0430 |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | |

TABLE 11-13. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED),
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| CURVE 16 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |
| 7.00 | 0.0006 | 10.4 | 0.1462 | 8.30 | 0.3200 | 13.2 | 0.1050 | 9.15 | 0.5301 | 7.10 | 0.0004 | 9.90 | 0.0500 |
| 7.10 | 0.0004 | 10.6 | 0.1134 | 9.40 | 0.3473 | 13.4 | 0.1001 | 9.20 | 0.4744 | 7.20 | 0.0001 | 9.90 | 0.0500 |
| 7.20 | 0.0002 | 10.9 | 0.1122 | 9.50 | 0.3768 | 13.6 | 0.0917 | 9.30 | 0.4527 | 7.30 | 0.0001 | 10.0 | 0.0500 |
| 7.30 | 0.0001 | 11.0 | 0.1037 | 9.60 | 0.4314 | 13.8 | 0.0838 | 9.35 | 0.4164 | 7.40 | 0.0005 | 10.2 | 0.0500 |
| 7.40 | 0.0005 | 11.2 | 0.0985 | 9.65 | 0.4705 | 14.0 | 0.0793 | 9.40 | 0.3106 | 7.50 | 0.0015 | 10.4 | 0.0500 |
| 7.50 | 0.0015 | 11.4 | 0.0923 | 9.70 | 0.5290 | 14.2 | 0.0749 | 9.50 | 0.3433 | 7.60 | 0.0031 | 10.6 | 0.0500 |
| 7.60 | 0.0032 | 11.6 | 0.0855 | 9.75 | 0.5741 | 14.4 | 0.1475 | 9.60 | 0.3129 | 7.70 | 0.0094 | 10.8 | 0.0500 |
| 7.70 | 0.0097 | 11.8 | 0.0782 | 9.80 | 0.6390 | 14.6 | 0.0676 | 9.70 | 0.2841 | 7.80 | 0.0200 | 11.0 | 0.0500 |
| 7.80 | 0.0208 | 12.0 | 0.0778 | 9.85 | 0.6850 | 16.0 | 0.0414 | 9.80 | 0.2521 | 7.90 | 0.0500 | 11.2 | 0.0500 |
| 7.90 | 0.0523 | 12.2 | 0.0835 | 9.90 | 0.7069 | CURVE 20 | | 9.90 | 0.2295 | 8.00 | 0.1319 | 11.4 | 0.0500 |
| 8.00 | 0.1385 | 12.4 | 0.0974 | 9.95 | 0.7231 | T = 293. | | 10.0 | 0.2050 | 8.10 | 0.2630 | 11.6 | 0.0500 |
| 8.10 | 0.2732 | 12.6 | 0.1072 | 9.00 | 0.6751 | 7.00 | 0.0006 | 10.2 | 0.1665 | 8.20 | 0.3098 | 11.8 | 0.0500 |
| 8.20 | 0.3176 | 12.8 | 0.1195 | 9.05 | 0.6225 | 7.10 | 0.0004 | 10.4 | 0.1452 | 8.30 | 0.3030 | 12.0 | 0.0500 |
| 8.30 | 0.3098 | 13.0 | 0.1109 | 9.10 | 0.4707 | 7.20 | 0.0004 | 10.6 | 0.1126 | 8.40 | 0.3332 | 12.2 | 0.0500 |
| 8.40 | 0.3389 | 13.2 | 0.1026 | 9.15 | 0.5355 | 7.30 | 0.0001 | 10.8 | 0.1114 | 8.50 | 0.3656 | 12.4 | 0.0500 |
| 8.50 | 0.3709 | 13.4 | 0.0977 | 9.20 | 0.4800 | 7.40 | 0.0001 | 11.0 | 0.1029 | 8.60 | 0.4191 | 12.6 | 0.0500 |
| 8.60 | 0.4240 | 13.6 | 0.0895 | 9.30 | 0.4584 | 7.50 | 0.0005 | 11.2 | 0.0977 | 8.65 | 0.4591 | 12.8 | 0.0500 |
| 8.65 | 0.4637 | 13.8 | 0.0817 | 9.35 | 0.4221 | 7.60 | 0.0015 | 11.4 | 0.0915 | 8.70 | 0.5106 | 13.0 | 0.0500 |
| 8.70 | 0.5228 | 14.0 | 0.0773 | 9.40 | 0.3162 | 7.70 | 0.0031 | 11.6 | 0.0848 | 8.75 | 0.5647 | 13.2 | 0.0500 |
| 8.75 | 0.5685 | 14.2 | 0.0729 | 9.50 | 0.3489 | 7.80 | 0.0096 | 11.8 | 0.0775 | 8.80 | 0.6308 | 13.4 | 0.0500 |
| 8.80 | 0.6341 | 14.4 | 0.1443 | 9.60 | 0.3184 | 7.90 | 0.0204 | 12.0 | 0.0771 | 8.85 | 0.6780 | 13.6 | 0.0500 |
| 8.85 | 0.6808 | 14.6 | 0.0659 | 9.70 | 0.2895 | 8.00 | 0.0511 | 12.2 | 0.0828 | 8.90 | 0.7006 | 13.8 | 0.0500 |
| 8.90 | 0.7031 | 16.0 | 0.0402 | 9.80 | 0.2572 | 7.90 | 0.0511 | 12.4 | 0.0966 | 8.95 | 0.7176 | 14.0 | 0.0500 |
| 9.00 | 0.6716 | CURVE 19 | | 9.90 | 0.2345 | 8.00 | 0.1351 | 12.6 | 0.1063 | 9.00 | 0.6693 | 14.2 | 0.0500 |
| 9.05 | 0.6188 | T = 293. | | 10.0 | 0.2098 | 8.10 | 0.2681 | 12.8 | 0.1186 | 9.05 | 0.6163 | 14.4 | 0.0500 |
| 9.10 | 0.4664 | 7.00 | 0.0007 | 10.2 | 0.1704 | 8.20 | 0.3137 | 13.0 | 0.1101 | 9.10 | 0.4635 | 14.6 | 0.0500 |
| 9.15 | 0.5314 | 7.10 | 0.0005 | 10.4 | 0.1492 | 8.30 | 0.3064 | 13.2 | 0.1018 | 9.15 | 0.5287 | 14.8 | 0.0500 |
| 9.20 | 0.4758 | 7.20 | 0.0002 | 10.6 | 0.1160 | 8.40 | 0.3360 | 13.4 | 0.0970 | 9.20 | 0.4730 | 15.0 | 0.0500 |
| 9.30 | 0.4541 | 7.30 | 0.0001 | 10.8 | 0.1148 | 8.50 | 0.3682 | 13.6 | 0.0887 | 9.30 | 0.4513 | 15.2 | 0.0500 |
| 9.35 | 0.4178 | 7.40 | 0.0005 | 11.0 | 0.1062 | 8.60 | 0.4216 | 13.8 | 0.0810 | 9.35 | 0.4149 | 15.4 | 0.0500 |
| 9.40 | 0.3120 | 7.50 | 0.0016 | 11.2 | 0.1008 | 8.65 | 0.4613 | 14.0 | 0.0766 | 9.40 | 0.3092 | 15.6 | 0.0500 |
| 9.50 | 0.3447 | 7.60 | 0.0034 | 11.4 | 0.0946 | 8.70 | 0.5207 | 14.2 | 0.0723 | 9.50 | 0.3419 | 15.8 | 0.0500 |
| 9.60 | 0.3142 | 7.70 | 0.0103 | 11.6 | 0.0877 | 8.75 | 0.5666 | 14.4 | 0.1433 | 9.60 | 0.3115 | 16.0 | 0.0500 |
| 9.70 | 0.2854 | 7.80 | 0.0221 | 11.8 | 0.0803 | 8.80 | 0.6325 | 14.6 | 0.0652 | 9.70 | 0.2828 | 16.2 | 0.0500 |
| 9.80 | 0.2534 | 7.90 | 0.0561 | 12.0 | 0.0799 | 8.85 | 0.6794 | 16.0 | 0.0398 | 9.80 | 0.2508 | 16.4 | 0.0500 |
| 9.90 | 0.2308 | 8.00 | 0.1490 | 12.2 | 0.0856 | 8.90 | 0.7018 | CURVE 21 | | 9.90 | 0.2283 | 16.6 | 0.0500 |
| 10.0 | 0.2052 | 8.10 | 0.2888 | 12.4 | 0.0998 | 8.95 | 0.7187 | T = 293. | | 10.0 | 0.2039 | 16.8 | 0.0500 |
| 10.2 | 0.1676 | 8.20 | 0.3295 | 12.6 | 0.1097 | 9.00 | 0.6704 | 7.00 | 0.0006 | 10.2 | 0.1654 | 17.0 | 0.0500 |
| | | | | 12.8 | 0.1222 | 9.05 | 0.6176 | 7.10 | 0.0006 | 10.4 | 0.1442 | 17.2 | 0.0500 |
| | | | | 13.0 | 0.1135 | 9.10 | 0.4649 | 7.20 | 0.0006 | 10.6 | 0.1117 | 17.4 | 0.0500 |

TABLE 11-13. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T , K ; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|------------------|--------|-----------|--------|
| CURVE 25 (CONT.) | | | |
| 8.65 | 0.4615 | 14.0 | 0.0766 |
| 8.70 | 0.5208 | 14.2 | 0.0723 |
| 8.75 | 0.5666 | 14.4 | 0.1433 |
| 8.80 | 0.5325 | 14.6 | 0.0652 |
| 8.95 | 0.6734 | 16.0 | 0.0391 |
| 8.90 | 0.7018 | | |
| 8.95 | 0.7187 | | |
| 9.00 | 0.6704 | | |
| 9.05 | 0.6175 | | |
| 9.10 | 0.4649 | | |
| 9.15 | 0.5331 | | |
| 9.20 | 0.4744 | | |
| 9.30 | 0.4527 | | |
| 9.35 | 0.4164 | | |
| 9.40 | 0.3106 | | |
| 9.50 | 0.3433 | | |
| 9.60 | 0.3129 | | |
| 9.70 | 0.2841 | | |
| 9.80 | 0.2521 | | |
| 9.90 | 0.2296 | | |
| 10.0 | 0.2051 | | |
| 10.2 | 0.1665 | | |
| 10.4 | 0.1452 | | |
| 10.6 | 0.1126 | | |
| 10.8 | 0.1114 | | |
| 11.0 | 0.1229 | | |
| 11.2 | 0.0977 | | |
| 11.4 | 0.0916 | | |
| 11.6 | 0.0848 | | |
| 11.8 | 0.0776 | | |
| 12.0 | 0.0772 | | |
| 12.2 | 0.0828 | | |
| 12.4 | 0.0956 | | |
| 12.6 | 0.1064 | | |
| 12.8 | 0.1167 | | |
| 13.0 | 0.1101 | | |
| 13.2 | 0.1018 | | |
| 13.4 | 0.0970 | | |
| 13.6 | 0.0887 | | |
| 13.8 | 0.0810 | | |

d. Normal Spectral Reflectance (Temperature Dependence)

No experimental data sets were found for the temperature dependence of the normal spectral reflectance of vitreous silica. However, a provisional curve was generated for 10.6 μm from curves 5-10 of Tables 11-12 and 11-13 together with the provisional values at 293 K for the wavelength dependence of the normal spectral reflectance. The values are listed in Table 11-14 and shown in Figure 11-9. An uncertainty of within 30% is assigned. It is noted that from 293 to 1173 K, there is an increase in the normal spectral reflectance.

TABLE 11-14. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ |
|------------------|--------|
| $\lambda = 10.6$ | |
| 293. | 0.113 |
| 400. | 0.122 |
| 636. | 0.134 |
| 796. | 0.138 |
| 1035. | 0.138 |
| 1173. | 0.150 |

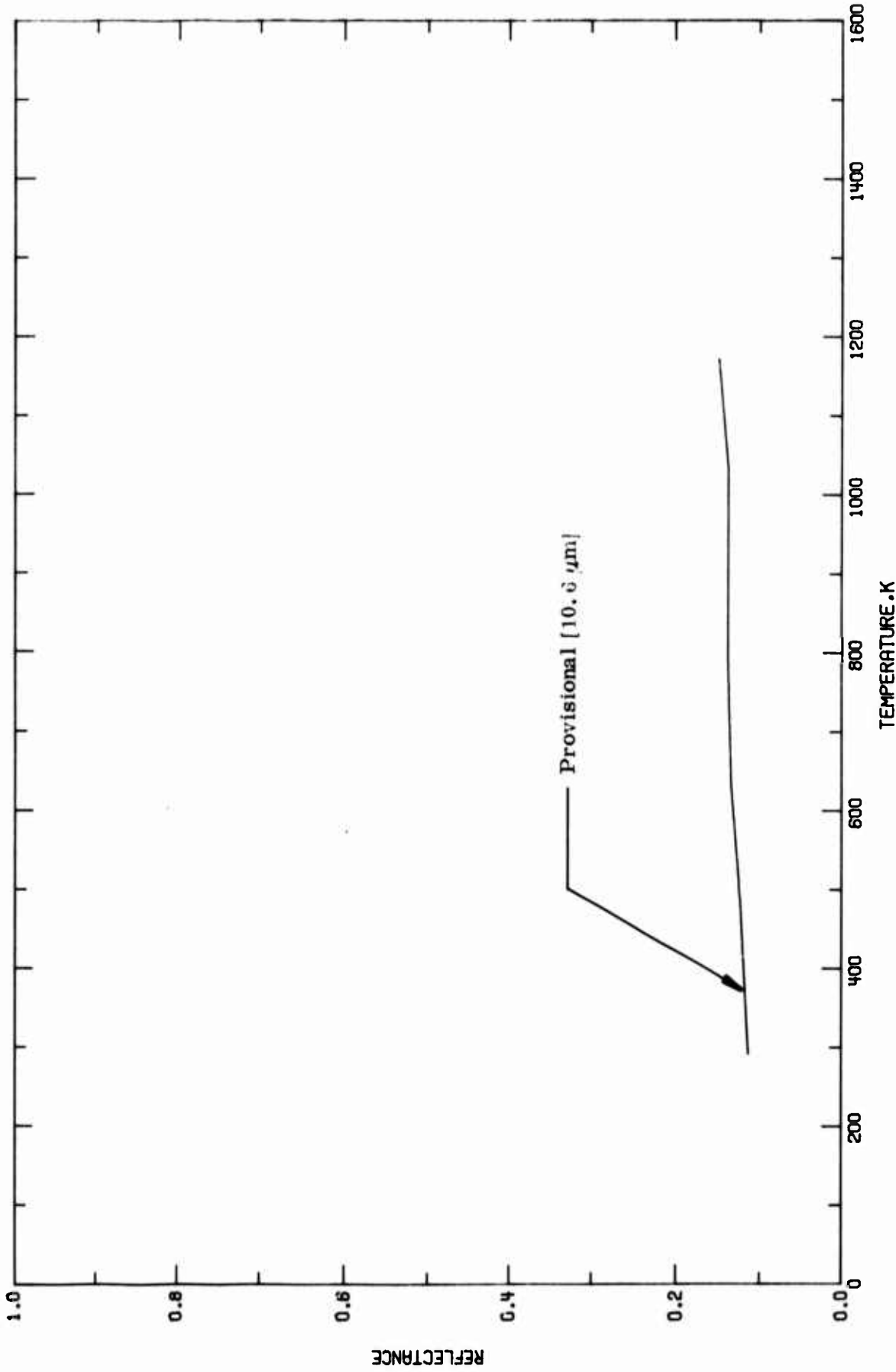


FIGURE 11-9. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (TEMPERATURE DEPENDENCE).

e. Angular Spectral Reflectance (Wavelength Dependence)

A total of 32 sets of experimental data were located for the wavelength dependence of the angular spectral reflectance of vitreous silica. One additional data set for synthetic quartz was located and included. The data are listed in Table 11-17 and shown in Figures 11-10 and 11-11. Specimen characterization and measurement information for the data are given in Table 11-16. Curves 20 and 21 are not shown on Figures 11-10 and 11-11, since the computer plotting routine cannot plot 33 curves.

The data above $1 \mu\text{m}$ are all for 293 K and is widely spaced. Lines connecting such widely spaced points (see Figure 11-11) do not imply a smooth curve connecting the points but are used for ease in visualizing the points belonging to the same curve.

Using the Fresnel equations, a set of provisional values was generated for angular spectral reflectance for unpolarized radiation (see Eqs. (2.4-1)-(2.4-5)). The values are for angles of incidence and reflection of 40° , for a temperature of 293 K, and hold within the wavelength range of $7.0\text{-}16.0 \mu\text{m}$ for an optically smooth specimen. The provisional values are listed in Table 11-15 and shown in Figure 11-10. An uncertainty within 30% is assigned.

TABLE 11-15. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|-------------------------------|--------|-----------|--------|
| OPTICALLY SMOOTH | | | |
| $\theta = \theta' = 40^\circ$ | | | |
| T = 293 (CONT.) | | | |
| 7.00 | 0.001 | 10.4 | 0.151 |
| 7.10 | 0.001 | 10.6 | 0.119 |
| 7.20 | 0.000 | 10.8 | 0.116 |
| 7.30 | 0.000 | 11.0 | 0.110 |
| 7.40 | 0.001 | 11.2 | 0.104 |
| 7.50 | 0.002 | 11.4 | 0.098 |
| 7.60 | 0.005 | 11.6 | 0.092 |
| 7.70 | 0.019 | 11.8 | 0.085 |
| 7.80 | 0.050 | 12.0 | 0.084 |
| 7.90 | 0.178 | 12.2 | 0.090 |
| 8.00 | 0.312 | 12.4 | 0.104 |
| 8.10 | 0.423 | 12.6 | 0.113 |
| 8.20 | 0.412 | 12.8 | 0.125 |
| 8.30 | 0.385 | 13.0 | 0.117 |
| 8.40 | 0.391 | 13.2 | 0.109 |
| 8.50 | 0.415 | 13.4 | 0.104 |
| 8.60 | 0.459 | 13.6 | 0.096 |
| 8.65 | 0.493 | 13.8 | 0.088 |
| 8.70 | 0.545 | 14.0 | 0.083 |
| 8.75 | 0.586 | 14.2 | 0.079 |
| 8.80 | 0.646 | 14.4 | 0.152 |
| 8.85 | 0.688 | 14.6 | 0.072 |
| 8.90 | 0.707 | 16.0 | 0.045 |
| 8.95 | 0.720 | | |
| 9.00 | 0.670 | | |
| 9.05 | 0.614 | | |
| 9.10 | 0.466 | | |
| 9.15 | 0.478 | | |
| 9.20 | 0.473 | | |
| 9.30 | 0.452 | | |
| 9.35 | 0.416 | | |
| 9.40 | 0.313 | | |
| 9.50 | 0.344 | | |
| 9.60 | 0.314 | | |
| 9.70 | 0.286 | | |
| 9.80 | 0.255 | | |
| 9.90 | 0.233 | | |
| 10.0 | 0.209 | | |
| 10.2 | 0.172 | | |

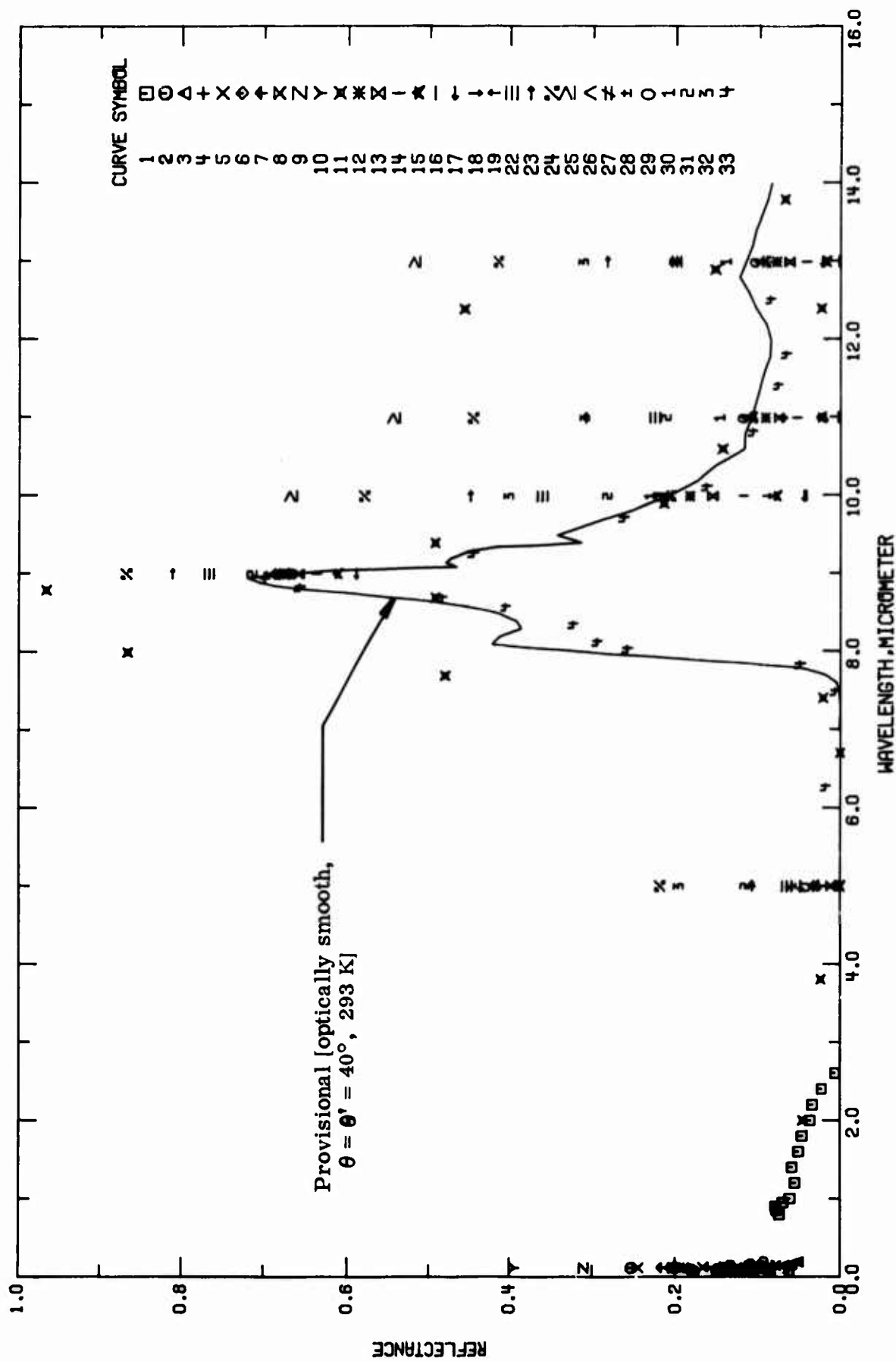


FIGURE 11-10. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE).

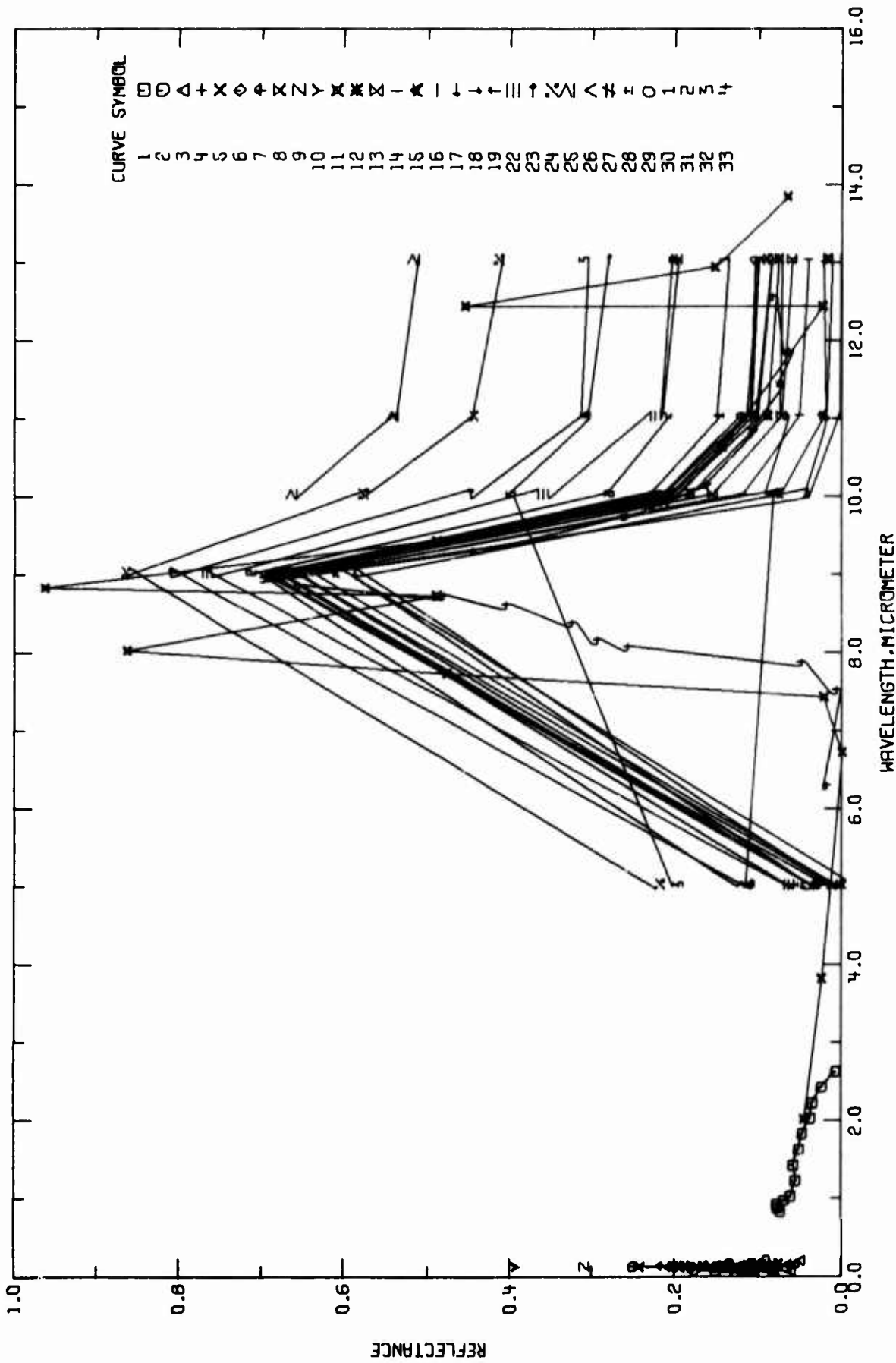


FIGURE 11-11. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE).

TABLE 11-16. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (Wavelength Dependence)

| Cur. No. | Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|----------|----------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 | T27141 | Bogdan, L. | 1964 | 0.80-2.6 | 293 | Fused quartz | Disk specimen 0.375 in. in diameter and 0.0625 in. thick; clear fused quartz blank; aluminum mirror used as reference standard, reported measurements corrected; data from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 45^\circ$, $\theta' = 45^\circ$. |
| 2 | T36689 | Rabinovitch, K., Canfield, L. R., and Madden, R. P. | 1965 | 0.056-0.19 | 293 | Silica | Specimen 6 mm thick; measured in vacuum with the plane of incidence perpendicular to exit slit of the monochromator; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 45^\circ$, $\theta' = 45^\circ$. |
| 3 | T36689 | Rabinovitch, K., et al. | 1965 | 0.058-0.19 | 293 | Silica | The above specimen except measured with the plane of incidence parallel to exit slit of the monochromator. |
| 4 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.057-0.15 | 293 | Fused quartz, type Suprasil | Specimens 1 mm thick; carefully cleaned and outgassed before measurement; samples supplied by Quarzschmelze Heraeus-Hansau; temperature specified as room temperature, 293 K assigned; $\theta = 20^\circ$. |
| 5 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.059-0.15 | 423 | Fused quartz, type Suprasil | Similar to the above specimen except measured at 423 K. |
| 6 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.1216 | 293 | Fused quartz, type Suprasil | Similar to the above specimen except temperature presumed to be room temperature, 293 K assigned; $\theta = 40^\circ$. |
| 7 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.1216 | 293 | Fused quartz, type Suprasil | Similar to the above specimen; $\theta = 50^\circ$. |
| 8 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.1216 | 293 | Fused quartz, type Suprasil | Similar to the above specimen; $\theta = 60^\circ$. |
| 9 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.1216 | 293 | Fused quartz, type Suprasil | Similar to the above specimen; $\theta = 70^\circ$. |
| 10 | T47322 | Platzoder, K. and Steinmann, W. | 1968 | 0.1216 | 293 | Fused quartz, type Suprasil | Similar to the above specimen; $\theta = 76^\circ$. |
| 11 | T30100 | McCarthy, D. E. | 1963 | 2.0-50 | 293 | Quartz | Synthetic; specimen 10 mm thick; ground and polished to a flatness of seven fringes or better; reference standard was aluminum mirror; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; Beckman IR-5A used in 2-16 μm range and Beckman IR-7 with CsI interchange used in 12.5-50 μm range; $\theta = 30^\circ$, $\theta' = 30^\circ$. |
| 12 | T76947 | General Dynamics Convair Aerospace Division | 1974 | 9.0-22 | 293 | Optosil 1, Convair Sample F | Specimen thickness 0.125 in.; polished disk; specimen provided by Aerospace Corp. who obtained it from Amersil, Inc., Hillside, New Jersey; measurements made using the General Dynamics Convair Aerospace ellipsoidal reflectometer and a Perkin Elmer Model 210 monochromator for dispersion and Advanced Ballistic Missile Defense Agency wire grid polarizers which were mounted as close as possible to the thermocouple detector; data gathered at atmospheric pressure; measurement temperature specified as room temperature, 293 K assigned; absolute reflectance determined directly; reflectance values reported are for component parallel to plane of incidence; five readings taken and average used in determining reflectance; data from figure; $\theta = 20^\circ$, $\theta' = 20^\circ$. |
| 13 | T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 30^\circ$, $\theta' = 30^\circ$. |

TABLE 11-16. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 14 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 40^\circ$, $\theta' = 40^\circ$. |
| 15 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 50^\circ$, $\theta' = 50^\circ$. |
| 16 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 60^\circ$, $\theta' = 60^\circ$. |
| 17 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 70^\circ$, $\theta' = 70^\circ$. |
| 18 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 75^\circ$, $\theta' = 75^\circ$. |
| 19 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen except reflectance measurements reported are for the component perpendicular to the plane of incidence; $\theta = 20^\circ$, $\theta' = 20^\circ$. |
| 20 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 30^\circ$, $\theta' = 30^\circ$. |
| 21 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 40^\circ$, $\theta' = 40^\circ$. |
| 22 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 50^\circ$, $\theta' = 50^\circ$. |
| 23 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 60^\circ$, $\theta' = 60^\circ$. |
| 24 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 70^\circ$, $\theta' = 70^\circ$. |
| 25 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 75^\circ$, $\theta' = 75^\circ$. |
| 26 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen except reflectance values reported are for average of polarized components; $\theta = 20^\circ$, $\theta' = 20^\circ$. |
| 27 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 30^\circ$, $\theta' = 30^\circ$. |

TABLE 11-16. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 28 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 40^\circ$, $\theta' = 40^\circ$. |
| 29 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 50^\circ$, $\theta' = 50^\circ$. |
| 30 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 60^\circ$, $\theta' = 60^\circ$. |
| 31 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 70^\circ$, $\theta' = 70^\circ$. |
| 32 T76947 | General Dynamics Convair Aerospace Division | 1974 | 5.0-22 | 293 | Optosil 1, Convair Sample F | The above specimen; $\theta = 75^\circ$, $\theta' = 75^\circ$. |
| 33 T40553 | Perry, C.H. and Whigley, J.D., Jr. | 1967 | 7-32 | 293 | Fused quartz | Two faces polished; smooth values from figure; measurement temperature specified as room temperature, 293 K assigned; $\theta = 15^\circ$, $\theta' = 15^\circ$. |

TABLE 11-17. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | | |
|------------------|--------|------------------|--------|-----------|--------|-----------|--------|-----------|--------|----------|-------|
| CURVE 17 (CONT.) | | | | | | | | | | | |
| 22.0 | 0.230 | CURVE 21 (CONT.) | | | | | | | | | |
| CURVE 18 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 5.0 | 0.111 | 11.0 | 0.171 | CURVE 25 | | | | | | CURVE 33 | |
| 10.0 | 0.089 | 13.0 | 0.149 | 10.0 | 0.662 | 5.0 | 0.043 | 6.25 | 0.019 | | |
| 11.0 | 0.070 | 16.0 | 0.084 | 11.0 | 0.540 | 9.0 | 0.683 | 7.47 | 0.007 | | |
| 13.0 | 0.079 | 22.0 | 0.475 | 13.0 | 0.515 | 10.0 | 0.220 | 7.02 | 0.049 | | |
| 16.0 | 0.108 | CURVE 22 | | | | | | | | 8.02 | 0.257 |
| 22.0 | 0.267 | T = 293. | | | | | | | | 8.11 | 0.294 |
| CURVE 19 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 5.0 | 0.024 | 5.0 | 0.064 | CURVE 26 | | | | | | 8.33 | 0.325 |
| 9.0 | 0.693 | 9.0 | 0.766 | 5.0 | 0.033 | CURVE 29 | | | | 8.56 | 0.485 |
| 10.0 | 0.222 | 10.0 | 0.361 | 9.0 | 0.674 | 5.0 | 0.043 | 8.68 | 0.483 | | |
| 11.0 | 0.117 | 11.0 | 0.225 | 9.0 | 0.206 | T = 293. | | | | 8.81 | 0.656 |
| 13.0 | 0.100 | 13.0 | 0.199 | 10.0 | 0.109 | 5.0 | 0.059 | 8.91 | 0.698 | | |
| 16.0 | 0.053 | 16.0 | 0.122 | 11.0 | 0.091 | 9.0 | 0.682 | 9.25 | 0.747 | | |
| 22.0 | 0.411 | 22.0 | 0.528 | 13.0 | 0.051 | 10.0 | 0.232 | 9.70 | 0.261 | | |
| CURVE 20 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 5.0 | 0.029 | 5.0 | 0.109 | CURVE 27 | | | | | | 10.1 | 0.162 |
| 9.0 | 0.710 | 9.0 | 0.811 | 5.0 | 0.031 | 5.0 | 0.059 | 10.8 | 0.108 | | |
| 10.0 | 0.251 | 10.0 | 0.450 | 9.0 | 0.682 | 9.0 | 0.232 | 11.4 | 0.075 | | |
| 11.0 | 0.138 | 11.0 | 0.308 | 10.0 | 0.207 | 10.0 | 0.141 | 11.8 | 0.065 | | |
| 13.0 | 0.119 | 13.0 | 0.281 | 11.0 | 0.108 | 13.0 | 0.086 | 12.5 | 0.305 | | |
| 16.0 | 0.064 | 16.0 | 0.190 | 13.0 | 0.092 | 16.0 | 0.086 | 15.7 | 0.040 | | |
| 22.0 | 0.436 | 22.0 | 0.603 | 22.0 | 0.393 | 22.0 | 0.409 | 18.9 | 0.015 | | |
| CURVE 21 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 5.0 | 0.029 | 5.0 | 0.219 | CURVE 30 | | | | | | 19.4 | 0.056 |
| 9.0 | 0.710 | 9.0 | 0.867 | 5.0 | 0.034 | CURVE 31 | | | | 19.8 | 0.164 |
| 10.0 | 0.251 | 10.0 | 0.578 | 9.0 | 0.685 | 5.0 | 0.118 | 20.6 | 0.498 | | |
| 11.0 | 0.138 | 11.0 | 0.447 | 9.0 | 0.212 | 9.0 | 0.714 | 20.8 | 0.479 | | |
| 13.0 | 0.119 | 13.0 | 0.415 | 10.0 | 0.113 | 10.0 | 0.281 | 22.5 | 0.298 | | |
| 16.0 | 0.064 | 16.0 | 0.315 | 11.0 | 0.099 | 11.0 | 0.212 | 23.7 | 0.241 | | |
| 22.0 | 0.436 | 22.0 | 0.708 | 13.0 | 0.055 | 13.0 | 0.202 | 26.0 | 0.183 | | |
| CURVE 22 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 5.0 | 0.041 | 5.0 | 0.219 | CURVE 32 | | | | | | 28.9 | 0.148 |
| 9.0 | 0.734 | 9.0 | 0.867 | 5.0 | 0.034 | T = 293. | | | | 31.7 | 0.140 |
| 10.0 | 0.297 | 10.0 | 0.578 | 9.0 | 0.685 | 5.0 | 0.196 | | | | |
| | | 11.0 | 0.447 | 10.0 | 0.212 | 10.0 | 0.401 | | | | |
| | | 13.0 | 0.415 | 11.0 | 0.113 | 11.0 | 0.310 | | | | |
| | | 16.0 | 0.315 | 13.0 | 0.099 | 13.0 | 0.312 | | | | |
| | | 22.0 | 0.708 | 16.0 | 0.055 | 16.0 | 0.264 | | | | |
| | | | | 22.0 | 0.399 | 22.0 | 0.550 | | | | |

f. Normal Spectral Absorptance (Wavelength Dependence)

One set of experimental data was located for the wavelength dependence of the normal spectral absorptance of vitreous silica. In addition, two sets of experimental data for crystalline quartz was located. The data are listed in Table 11-20 and shown in Figures 11-12 and 11-13. Specimen characterization and measurement information for the data are given in Table 11-19.

The data of Bogdan [T27141] (curve 3) is for a temperature of 293 K and covers a wavelength range of 0.8 to 2.60 μm . That data was calculated from reflectance and transmittance data.

Calculations were carried out to determine the wavelength dependence of the normal spectral absorptance for radiation that is polarized perpendicular to the plane of incidence (curves 4-6), the absorptance that is parallel to the plane of incidence (curves 7-9), and the absorptance for unpolarized radiation (curves 10-12). The calculations used the Fresnel equations, Eqs. (2.4-1)-(2.4-5), together with Eq. (2.4-8). For a discussion of the index of refraction and absorption index data that were used in the calculations, see the section on the wavelength dependence of the normal spectral emittance.

Provisional values for the wavelength dependence of the normal spectral absorptance were generated. The values are listed in Table 11-18 and shown in Figure 11-12. The values here were equated to the provisional values for the wavelength dependence of the normal spectral emittance. Below 7 μm the provisional values apply to a 0.50 in. thick specimen of Corning 7940 vitreous silica at 293 K and Kirchhoff's law was used to equate the normal spectral absorptance to the normal spectral emittance. Above 7 μm the provisional values are the calculated values using the Fresnel equations for unpolarized radiation, Eqs. (2.4-1)-(2.4-5) and (2.4-8). The calculated values hold for an optically smooth specimen at 293 K that is opaque and the angle of incidence is 0° . An uncertainty of 30% is assigned. For more details see the section on the wavelength dependence of the normal spectral emittance for vitreous silica. The value of the normal spectral absorptance at 10.6 μm and 293 K is 0.89.

TABLE 11-13. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| CORNING 7940 1.27CM THICK T = 293 | | | CORNING 7946 1.27CM THICK T = 293 (CONT.) | | | OPTICALLY SMOOTH T = 293 | | | OPTICALLY SMOOTH T = 293 (CONT.) | | |
|---|----------|-----------|---|-----------|----------|-----------------------------|----------|-----------|-------------------------------------|-----------|----------|
| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α |
| 2.14 | 0.025 | 4.49 | 0.976 | 7.00 | 0.999 | 10.4 | 0.855 | | | | |
| 2.32 | 0.042 | 4.55 | 0.970 | 7.10 | 1.000 | 10.6 | 0.887 | | | | |
| 2.42 | 0.062 | 4.66 | 0.974 | 7.20 | 1.000 | 10.8 | 0.889 | | | | |
| 2.50 | 0.083 | 4.81 | 0.973 | 7.30 | 1.000 | 11.0 | 0.897 | | | | |
| 2.52 | 0.131 | 4.99 | 0.973 | 7.40 | 1.000 | 11.2 | 0.902 | | | | |
| 2.52 | 0.252 | 5.00 | 0.974 | 7.50 | 0.999 | 11.4 | 0.909 | | | | |
| 2.50 | 0.408 | 5.27 | 0.979 | 7.60 | 0.997 | 11.6 | 0.915 | | | | |
| 2.51 | 0.439 | 5.56 | 0.986 | 7.70 | 0.990 | 11.8 | 0.923 | | | | |
| 2.54 | 0.473 | 5.77 | 0.986 | 7.80 | 0.980 | 12.0 | 0.923 | | | | |
| 2.58 | 0.563 | 5.88 | 0.986 | 7.90 | 0.949 | 12.2 | 0.917 | | | | |
| 2.58 | 0.643 | 6.00 | 0.986 | 8.00 | 0.865 | 12.4 | 0.903 | | | | |
| 2.58 | 0.682 | 6.18 | 0.989 | 8.10 | 0.732 | 12.6 | 0.894 | | | | |
| 2.58 | 0.762 | 6.40 | 0.993 | 8.20 | 0.606 | 12.8 | 0.881 | | | | |
| 2.63 | 0.914 | 6.62 | 0.994 | 8.30 | 0.694 | 13.0 | 0.890 | | | | |
| 2.62 | 0.957 | 6.76 | 0.993 | 8.40 | 0.664 | 13.2 | 0.998 | | | | |
| 2.68 | 0.373 | 6.90 | 0.993 | 8.50 | 0.632 | 13.4 | 0.903 | | | | |
| 2.76 | 0.957 | | | 8.60 | 0.578 | 13.6 | 0.911 | | | | |
| 2.81 | 0.883 | | | 8.85 | 0.539 | 13.8 | 0.919 | | | | |
| 2.81 | 0.687 | | | 8.70 | 0.475 | 14.0 | 0.923 | | | | |
| 2.85 | 0.623 | | | 8.75 | 0.433 | 14.2 | 0.928 | | | | |
| 2.95 | 0.524 | | | 8.80 | 0.368 | 14.4 | 0.857 | | | | |
| 3.00 | 0.450 | | | 8.85 | 0.321 | 14.6 | 0.935 | | | | |
| 3.03 | 0.395 | | | 8.90 | 0.298 | 14.6 | 0.960 | | | | |
| 3.03 | 0.313 | | | 8.95 | 0.281 | | | | | | |
| 3.09 | 0.299 | | | 9.00 | 0.330 | | | | | | |
| 3.22 | 0.302 | | | 9.05 | 0.382 | | | | | | |
| 3.39 | 0.315 | | | 9.10 | 0.535 | | | | | | |
| 3.50 | 0.332 | | | 9.15 | 0.470 | | | | | | |
| 3.57 | 0.410 | | | 9.20 | 0.526 | | | | | | |
| 3.61 | 0.471 | | | 9.30 | 0.547 | | | | | | |
| 3.67 | 0.547 | | | 9.35 | 0.584 | | | | | | |
| 3.74 | 0.642 | | | 9.40 | 0.689 | | | | | | |
| 3.80 | 0.699 | | | 9.50 | 0.657 | | | | | | |
| 3.88 | 0.803 | | | 9.60 | 0.687 | | | | | | |
| 3.95 | 0.890 | | | 9.70 | 0.716 | | | | | | |
| 4.00 | 0.907 | | | 9.80 | 0.748 | | | | | | |
| 4.15 | 0.927 | | | 9.90 | 0.771 | | | | | | |
| 4.21 | 0.952 | | | 10.0 | 0.795 | | | | | | |
| 4.37 | 0.965 | | | 10.2 | 0.834 | | | | | | |

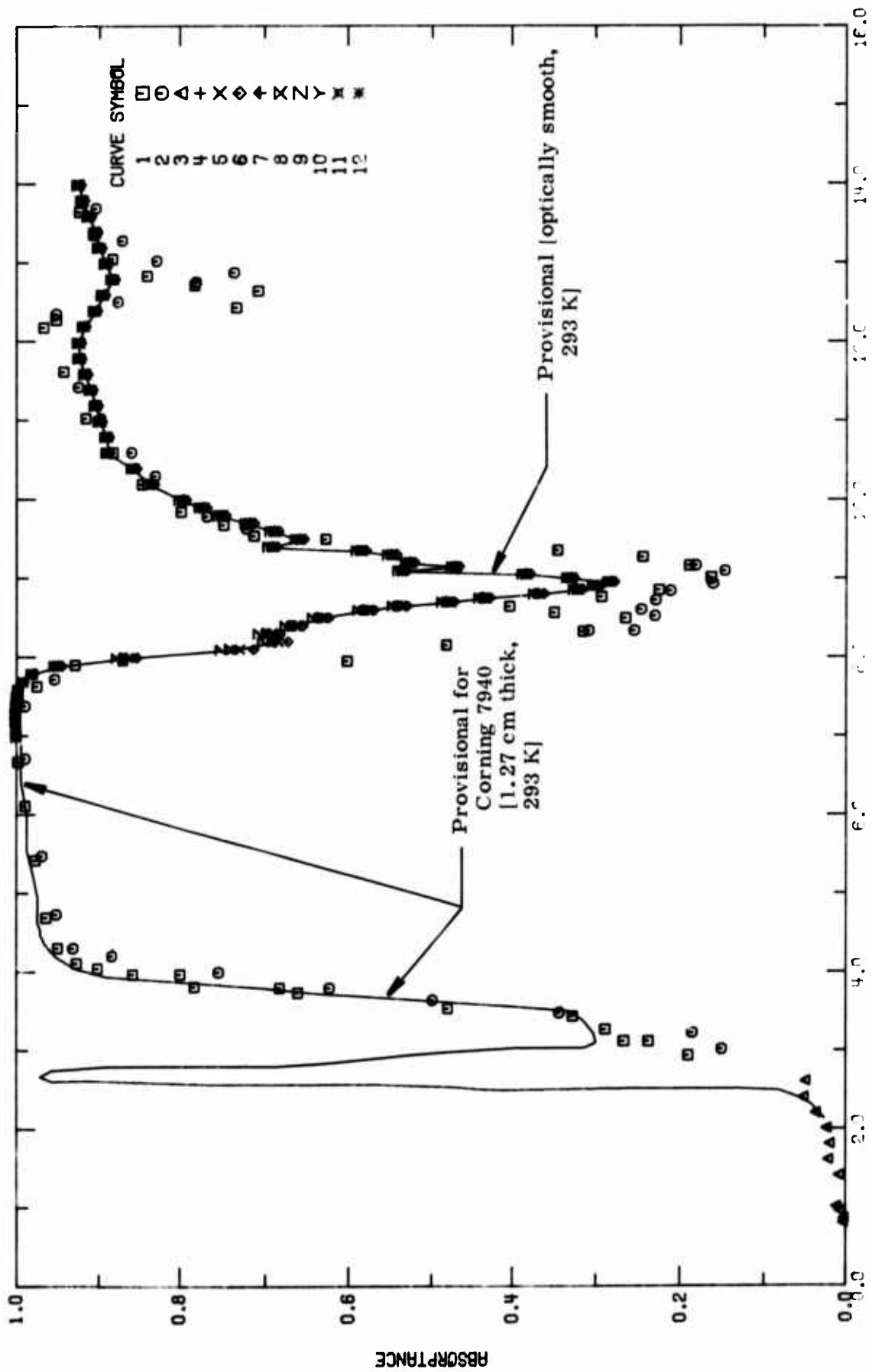


FIGURE 11-12. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

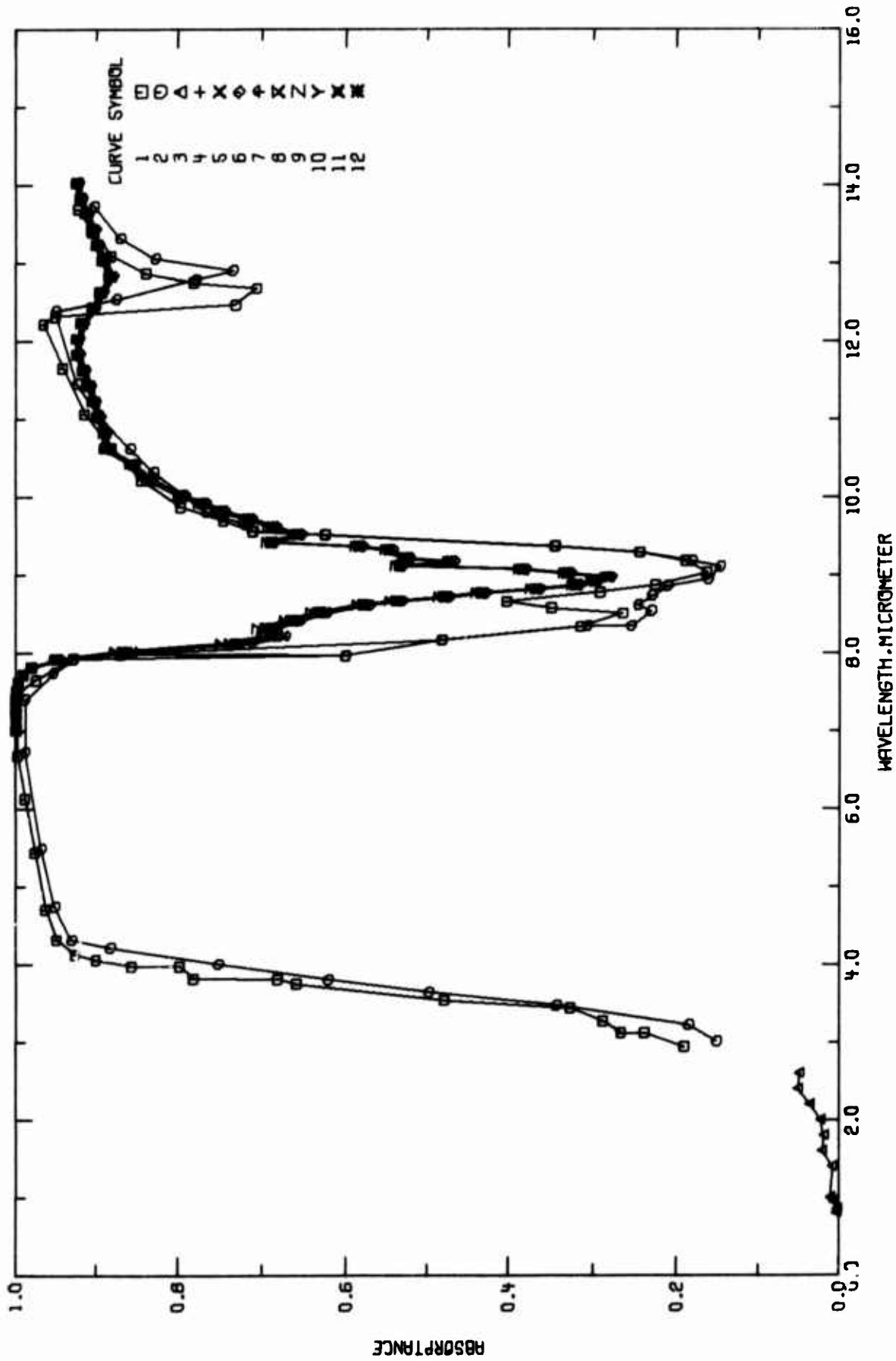


FIGURE 11-13. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

TABLE 11-19. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF SILICA(VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent). Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T45698 | Stierwalt, D. L., Bernstein, J. B., and Kirk, D. D. | 1963 | 2.9-24 | 373 | Crystalline Quartz | Measurement for ordinary ray; a Beckman IR-3 spectrophotometer, modified, used for measurement; this instrument evacuable and its temperature controlled by a water bath system; smooth values from figure; emittance measured, absorptance determined by applying Kirchoff's Law, $\theta=0^\circ$. Similar to the above specimen except measurement made for extraordinary ray. |
| 2 T-5698 | Stierwalt, D. L., et al. | 1963 | 3.0-23 | 373 | Crystalline Quartz | |
| 3 T27141 | Bogdan, L. | 1964 | 0.80-2.60 | 293 | Fused Quartz | Disk specimen 0.375 in. in diameter and 0.0625 in. thick; clear fused quartz blank; data from figure; temperature not given explicitly, assumed to be 293 K; author calculates absorptance (θ) from $1.0-p(45^\circ, 45^\circ) - \tau(\theta^\circ, 0^\circ)$, angle θ presumed to be 0° . |
| 4 A00012 | | 1975 | 7.0-16 | 293 | | Calculations for fused silica performed for a homogeneous; smooth surface and for perpendicular component of radiation, equations (2.4-6), (2.4-1), (2.4-3), and (2.4-4); data for index of refraction, n , and absorption index, k , from [A00012]; $\theta=0^\circ$. |
| 5 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta=5^\circ$. |
| 6 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta=10^\circ$. |
| 7 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for parallel component of radiation; equation (2.4-7) and $\theta=0^\circ$. |
| 8 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta=5^\circ$. |
| 9 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta=10^\circ$. |
| 10 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except for unpolarized radiation, equation (2.4-8) and $\theta=0^\circ$. |
| 11 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta=5^\circ$. |
| 12 A00012 | | 1975 | 7.0-16 | 293 | | Similar to the above specimen except $\theta=10^\circ$. |

TABLE 11-20. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| CURVE 1 T = 373. | | | CURVE 2 T = 473. | | | CURVE 3 T = 293. | | | CURVE 4 T = 293. | | | CURVE 5 T = 293. | | |
|---------------------|----------|-----------|---------------------|-----------|----------|---------------------|----------|-----------|---------------------|-----------|----------|---------------------|----------|--|
| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α | λ | α | |
| 2.93 | 0.190 | 10.60 | 0.661 | 3.01 | 0.151 | 12.68 | 0.734 | 1.40 | 0.068 | 9.30 | 0.5473 | | | |
| 3.11 | 0.230 | 11.04 | 0.915 | 3.22 | 0.185 | 13.63 | 0.827 | 1.60 | 0.021 | 9.35 | 0.5636 | | | |
| 3.26 | 0.266 | 11.63 | 0.942 | 3.47 | 0.347 | 13.29 | 1.871 | 1.80 | 0.019 | 9.40 | 0.6094 | | | |
| 3.43 | 0.280 | 12.19 | 0.966 | 3.64 | 0.498 | 13.70 | 0.903 | 2.00 | 0.023 | 9.50 | 0.6567 | | | |
| 3.53 | 0.327 | 12.44 | 0.951 | 3.80 | 0.731 | 14.13 | 0.923 | 2.20 | 0.036 | 9.60 | 0.6871 | | | |
| 3.74 | 0.479 | 12.65 | 0.706 | 4.00 | 0.621 | 14.89 | 0.939 | 2.40 | 0.051 | 9.70 | 0.7159 | | | |
| 3.80 | 0.659 | 12.72 | 0.781 | 4.21 | 0.882 | 15.73 | 0.959 | 2.60 | 0.049 | 9.80 | 0.7479 | | | |
| 3.81 | 0.681 | 12.84 | 0.839 | 4.31 | 0.930 | 16.96 | 0.907 | CURVE 4 | | | 0.7950 | | | |
| 3.97 | 0.798 | 13.06 | 0.882 | 4.74 | 0.951 | 17.41 | 0.989 | T = 293. | | | 0.8335 | | | |
| 3.97 | 0.798 | 13.37 | 0.906 | 5.48 | 0.968 | 17.71 | 0.965 | | | | 0.8548 | | | |
| 4.05 | 0.856 | 13.66 | 0.923 | 6.72 | 0.988 | 17.97 | 0.896 | | | | 0.8874 | | | |
| 4.12 | 0.900 | 14.16 | 0.934 | 7.39 | 0.988 | 18.22 | 0.668 | | | | 0.8886 | | | |
| 4.31 | 0.949 | 14.39 | 0.893 | 7.73 | 0.955 | 18.35 | 0.558 | | | | 0.8971 | | | |
| 4.70 | 0.963 | 14.60 | 0.916 | 7.91 | 0.928 | 18.43 | 0.524 | | | | 0.9023 | | | |
| 5.43 | 0.976 | 14.99 | 0.924 | 7.95 | 0.600 | 18.75 | 0.478 | | | | 0.9085 | | | |
| 6.12 | 0.988 | 16.28 | 0.958 | 7.97 | 0.869 | 19.12 | 0.472 | | | | 0.9152 | | | |
| 6.68 | 0.997 | 17.72 | 0.986 | 9.15 | 0.481 | 19.41 | 0.502 | | | | 0.9225 | | | |
| 7.46 | 0.997 | 18.39 | 0.996 | 8.33 | 0.307 | 19.54 | 0.586 | | | | 0.9229 | | | |
| 7.64 | 0.974 | 18.47 | 0.996 | 9.33 | 0.254 | 19.89 | 0.383 | | | | 0.9796 | | | |
| 7.91 | 0.928 | 19.16 | 0.947 | 9.52 | 0.230 | 19.98 | 0.322 | | | | 0.9489 | | | |
| 7.97 | 0.869 | 19.36 | 0.947 | 9.60 | 0.246 | 20.13 | 0.302 | | | | 0.8649 | | | |
| 8.15 | 0.600 | 19.48 | 0.861 | 9.72 | 0.229 | 20.36 | 0.355 | | | | 0.7319 | | | |
| 8.32 | 0.314 | 19.52 | 0.651 | 9.84 | 0.211 | 20.50 | 0.448 | | | | 0.6863 | | | |
| 8.49 | 0.264 | 19.87 | 0.395 | 8.93 | 0.161 | 20.65 | 0.518 | | | | 0.6936 | | | |
| 8.56 | 0.349 | 20.06 | 0.249 | 9.09 | 0.147 | 21.08 | 0.554 | | | | 0.6640 | | | |
| 8.64 | 0.402 | 20.37 | 0.196 | 9.16 | 0.181 | 21.64 | 0.590 | | | | 0.6318 | | | |
| 8.76 | 0.292 | 20.71 | 0.165 | 9.27 | 0.244 | 21.95 | 0.618 | | | | 0.5784 | | | |
| 8.85 | 0.225 | 21.06 | 0.155 | 9.35 | 0.345 | 22.24 | 0.659 | | | | 0.5387 | | | |
| 9.01 | 0.163 | 21.55 | 0.173 | 9.50 | 0.625 | 22.53 | 0.699 | | | | 0.4793 | | | |
| 9.16 | 0.189 | 21.84 | 0.202 | 9.54 | 0.711 | 22.76 | 0.725 | | | | 0.4334 | | | |
| 9.27 | 0.244 | 22.15 | 0.294 | 9.63 | 0.719 | 23.45 | 0.779 | | | | 0.3675 | | | |
| 9.35 | 0.345 | 22.38 | 0.448 | 9.79 | 0.766 | CURVE 3 | | | 0.3206 | | | | | |
| 9.50 | 0.625 | 10.30 | 0.829 | 10.30 | 0.829 | T = 293. | | | 0.2982 | | | | | |
| 9.54 | 0.711 | 10.60 | 0.619 | 10.60 | 0.850 | | | | 0.2813 | | | | | |
| 9.60 | 0.746 | 11.03 | 0.672 | 11.03 | 0.897 | | | | 0.3296 | | | | | |
| 9.85 | 0.797 | 11.43 | 0.924 | 11.43 | 0.924 | | | | 0.3824 | | | | | |
| 10.20 | 0.845 | 12.36 | 0.951 | 12.36 | 0.951 | | | | 0.5351 | | | | | |
| | | 12.51 | 0.875 | 12.51 | 0.875 | | | | 0.4699 | | | | | |
| | | 12.76 | 0.779 | 12.76 | 0.779 | | | | 0.5256 | | | | | |
| | | | | | | | | | 7.00 | | | | | |
| | | | | | | | | | 7.10 | | | | | |
| | | | | | | | | | 7.20 | | | | | |

TABLE 11-20. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORBANCE, α)

| CURVE 5 (CONT.) | | CURVE 6 (CONT.) | | CURVE 7 (CONT.) | | CURVE 8 (CONT.) | |
|-----------------|----------|-----------------|----------|-----------------|----------|-----------------|----------|
| λ | α | λ | α | λ | α | λ | α |
| 7.30 | 0.9999 | 11.2 | 0.9015 | 14.0 | 0.9207 | 9.40 | 0.9985 |
| 7.40 | 0.9995 | 11.4 | 0.9077 | 14.2 | 0.9251 | 9.50 | 0.9969 |
| 7.50 | 0.9985 | 11.6 | 0.9145 | 14.4 | 0.9325 | 9.60 | 0.9906 |
| 7.60 | 0.9968 | 11.8 | 0.9218 | 14.6 | 0.9324 | 9.70 | 0.9800 |
| 7.70 | 0.9933 | 12.0 | 0.9222 | 15.0 | 0.9396 | 9.80 | 0.9500 |
| 7.80 | 0.9732 | 12.2 | 0.9165 | | | 9.90 | 0.8681 |
| 7.90 | 0.9477 | 12.4 | 0.9026 | CURVE 7 | | 10.0 | 0.7370 |
| 8.00 | 0.9115 | 12.6 | 0.8924 | T = 293. | | 10.2 | 0.6902 |
| 8.10 | 0.8768 | 12.8 | 0.8855 | | | 10.4 | 0.6970 |
| 8.20 | 0.8424 | 13.0 | 0.8891 | 7.00 | 0.9994 | 10.6 | 0.6668 |
| 8.30 | 0.8092 | 13.2 | 0.8974 | 7.10 | 0.9996 | 10.8 | 0.6344 |
| 8.40 | 0.7711 | 13.4 | 0.9023 | 7.20 | 0.9999 | 11.0 | 0.5809 |
| 8.50 | 0.7291 | 13.6 | 0.9105 | 7.30 | 0.9939 | 11.2 | 0.5409 |
| 8.60 | 0.6850 | 13.8 | 0.9183 | 7.40 | 0.9935 | 11.4 | 0.4814 |
| 8.65 | 0.6363 | 14.0 | 0.9227 | 7.50 | 0.9985 | 11.5 | 0.4353 |
| 8.70 | 0.4772 | 14.2 | 0.9271 | 7.60 | 0.9969 | 11.8 | 0.3692 |
| 8.75 | 0.4315 | 14.4 | 0.8557 | 7.70 | 0.9904 | 12.0 | 0.3220 |
| 8.80 | 0.3659 | 14.6 | 0.9342 | 7.80 | 0.9796 | 12.2 | 0.2994 |
| 8.85 | 0.3192 | 16.0 | 0.9598 | 7.90 | 0.9439 | 12.4 | 0.2824 |
| 8.90 | 0.2969 | | | 8.00 | 0.8649 | 12.6 | 0.3307 |
| 8.95 | 0.2802 | CURVE 6 | | 8.10 | 0.7319 | 12.8 | 0.3837 |
| 9.00 | 0.3284 | T = 293. | | 8.20 | 0.6863 | 13.0 | 0.5365 |
| 9.05 | 0.3812 | 7.00 | 0.9993 | 8.30 | 0.6936 | 13.2 | 0.4713 |
| 9.10 | 0.5336 | 7.10 | 0.9995 | 8.40 | 0.6640 | 13.4 | 0.5270 |
| 9.15 | 0.4686 | 7.20 | 0.9998 | 8.50 | 0.6318 | 13.5 | 0.5487 |
| 9.20 | 0.5242 | 7.30 | 0.9999 | 8.60 | 0.5794 | 13.8 | 0.5851 |
| 9.30 | 0.5459 | 7.40 | 0.9995 | 8.70 | 0.4797 | 14.0 | 0.6908 |
| 9.35 | 0.5822 | 7.50 | 0.9984 | 8.80 | 0.4334 | 14.2 | 0.6581 |
| 9.40 | 0.6880 | 7.60 | 0.9966 | 8.90 | 0.3675 | 14.4 | 0.6885 |
| 9.50 | 0.6553 | 7.70 | 0.9897 | 9.00 | 0.3206 | 14.6 | 0.7172 |
| 9.60 | 0.6858 | 7.80 | 0.9779 | 9.10 | 0.2982 | 16.0 | 0.7492 |
| 9.70 | 0.7146 | 7.90 | 0.9439 | 9.20 | 0.2813 | | |
| 9.80 | 0.7466 | 8.00 | 0.8510 | 9.30 | 0.3296 | CURVE 8 | |
| 9.90 | 0.7692 | 8.10 | 0.7112 | 9.40 | 0.3824 | T = 293. | |
| 10.0 | 0.7938 | 8.20 | 0.6705 | 9.50 | 0.5351 | 7.00 | 0.9994 |
| 10.2 | 0.8324 | 8.30 | 0.6800 | 9.60 | 0.8865 | 7.10 | 0.9996 |
| 10.4 | 0.8538 | 8.40 | 0.6527 | 9.70 | 0.8999 | 7.20 | 0.9999 |
| 10.6 | 0.8166 | 8.50 | 0.6212 | 9.80 | 0.9043 | 7.30 | 0.9999 |
| 10.8 | 0.8878 | 8.60 | 0.5686 | 9.90 | 0.9162 | 7.40 | 0.9995 |
| 11.0 | 0.8363 | | | | | | |

TABLE 11-20. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α | λ | α |
|------------------|----------|------------------|----------|
| CURVE 12 (CONT.) | | CURVE 12 (CONT.) | |
| 8.85 | 0.3206 | 16.0 | 0.9602 |
| 8.90 | 0.2982 | | |
| 8.95 | 0.2813 | | |
| 9.00 | 0.3236 | | |
| 9.05 | 0.3824 | | |
| 9.10 | 0.5351 | | |
| 9.15 | 0.4639 | | |
| 9.20 | 0.5256 | | |
| 9.30 | 0.5473 | | |
| 9.35 | 0.5836 | | |
| 9.40 | 0.6894 | | |
| 9.50 | 0.6567 | | |
| 9.60 | 0.6871 | | |
| 9.70 | 0.7159 | | |
| 9.80 | 0.7479 | | |
| 9.90 | 0.7704 | | |
| 10.0 | 0.7949 | | |
| 10.2 | 0.8335 | | |
| 10.4 | 0.9548 | | |
| 10.6 | 0.8874 | | |
| 10.8 | 0.8886 | | |
| 11.0 | 0.8971 | | |
| 11.2 | 0.9023 | | |
| 11.4 | 0.9084 | | |
| 11.6 | 0.9152 | | |
| 11.8 | 0.9224 | | |
| 12.0 | 0.9228 | | |
| 12.2 | 0.9172 | | |
| 12.4 | 0.9034 | | |
| 12.6 | 0.8936 | | |
| 12.8 | 0.9013 | | |
| 13.0 | 0.8899 | | |
| 13.2 | 0.8982 | | |
| 13.4 | 0.9030 | | |
| 13.6 | 0.9113 | | |
| 13.8 | 0.9190 | | |
| 14.0 | 0.9234 | | |
| 14.2 | 0.9277 | | |
| 14.4 | 0.8567 | | |
| 14.6 | 0.9348 | | |

g. Angular Spectral Absorptance (Wavelength Dependence)

No experimental data sets were found for the wavelength dependence of the angular spectral absorptance of vitreous silica. However, a set of provisional values is listed in Table 11-21 and shown in Figure 11-14. The values were calculated using the Fresnel equations for specular reflection for unpolarized radiation (see Eqs. (2.4-1)-(2.4-5) and (2.4-8)). The context within which the provisional values are valid is a temperature of 293 K, a wavelength range of 7.0 to 16.0 μm , an angle of incidence, θ , of 40° , and an optically smooth specimen. An uncertainty of within 30% is assigned. See the section on the wavelength dependence of the angular spectral emittance for more discussion of the reasoning for the assignment of this uncertainty.

TABLE 11-21. PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|---------------------|----------|-----------|----------|
| OPTICALLY SMOOTH | | | |
| $\theta = 40^\circ$ | | | |
| T = 293 | | | |
| 7.00 | 0.993 | 10.4 | 0.849 |
| 7.10 | 0.999 | 10.6 | 0.881 |
| 7.20 | 1.000 | 10.8 | 0.882 |
| 7.30 | 1.000 | 11.0 | 0.890 |
| 7.40 | 0.999 | 11.2 | 0.896 |
| 7.50 | 0.998 | 11.4 | 0.902 |
| 7.60 | 0.995 | 11.6 | 0.908 |
| 7.70 | 0.991 | 11.8 | 0.915 |
| 7.80 | 0.950 | 12.0 | 0.916 |
| 7.90 | 0.922 | 12.2 | 0.910 |
| 8.00 | 0.688 | 12.4 | 0.896 |
| 8.10 | 0.577 | 12.6 | 0.887 |
| 8.20 | 0.588 | 12.8 | 0.875 |
| 8.30 | 0.615 | 13.0 | 0.883 |
| 8.40 | 0.609 | 13.2 | 0.891 |
| 8.50 | 0.585 | 13.4 | 0.896 |
| 8.60 | 0.541 | 13.6 | 0.904 |
| 8.65 | 0.507 | 13.8 | 0.912 |
| 8.70 | 0.455 | 14.0 | 0.917 |
| 8.75 | 0.414 | 14.2 | 0.921 |
| 8.80 | 0.354 | 14.4 | 0.848 |
| 8.85 | 0.312 | 14.6 | 0.928 |
| 8.90 | 0.293 | 16.0 | 0.954 |
| 8.95 | 0.280 | | |
| 9.00 | 0.330 | | |
| 9.05 | 0.384 | | |
| 9.10 | 0.534 | | |
| 9.15 | 0.472 | | |
| 9.20 | 0.527 | | |
| 9.30 | 0.548 | | |
| 9.35 | 0.584 | | |
| 9.40 | 0.687 | | |
| 9.50 | 0.656 | | |
| 9.60 | 0.586 | | |
| 9.70 | 0.714 | | |
| 9.80 | 0.745 | | |
| 9.90 | 0.767 | | |
| 10.0 | 0.791 | | |
| 10.2 | 0.828 | | |

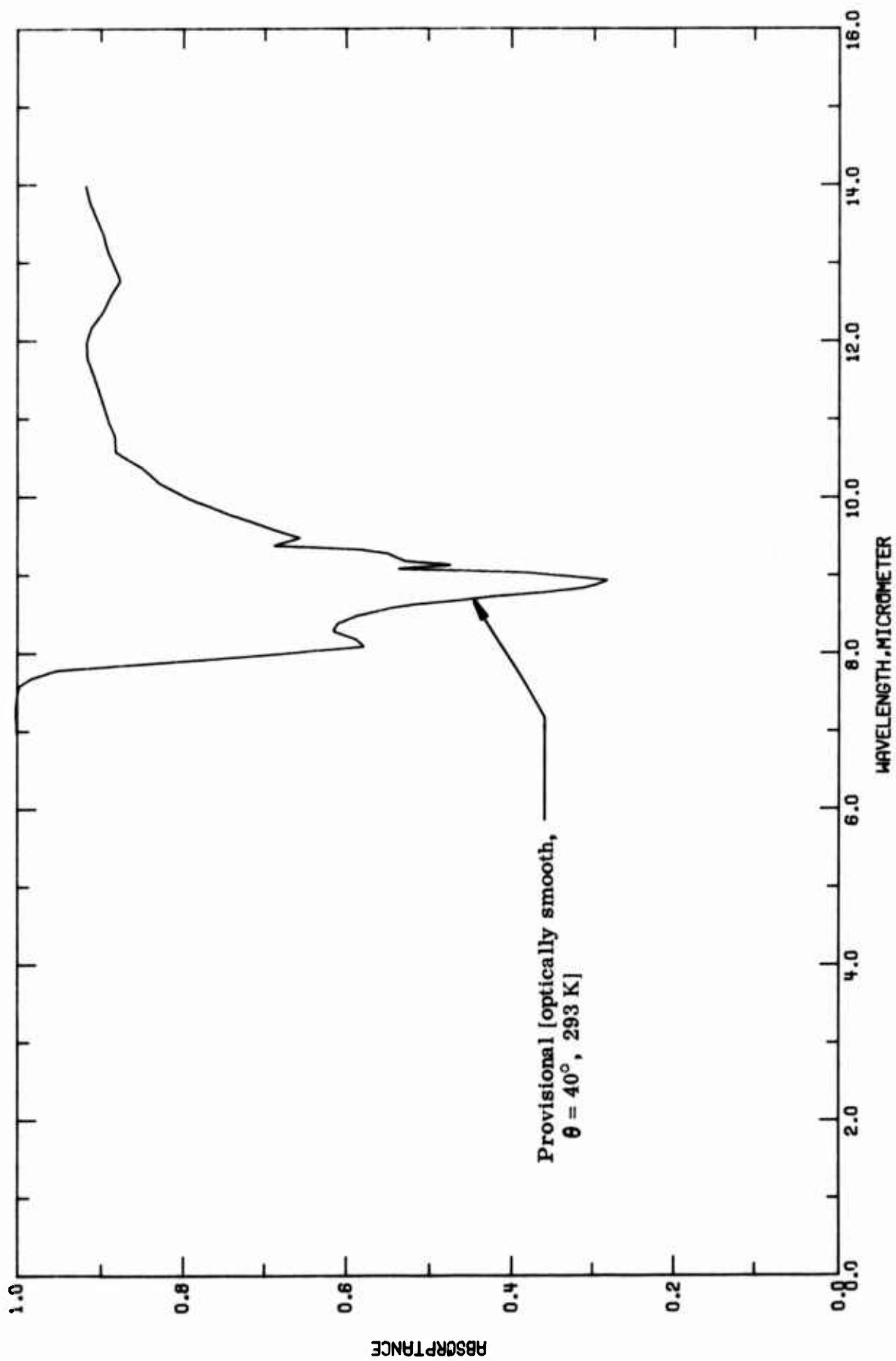


FIGURE 11-14. PROVISIONAL ANGULAR SPECTRAL ABSORPTANCE OF SILICA (VITREOUS)
(WAVELENGTH DEPENDENCE).

h. Normal Spectral Transmittance (Wavelength Dependence)

A total of 38 sets of experimental data were located and processed for the category of the wavelength dependence of the normal spectral transmittance of vitreous silica. The data are listed in Table 11-24 and shown in Figures 11-15 to 11-18. Specimen characterization and measurement information for the data are given in Table 11-23. The plots of the raw data connected by lines is broken up into two figures, Figure 11-17 and 11-18. The reason for this is that the plotting routine can only plot 32 curves without repeating a symbol used to plot a curve. Therefore, it was decided to plot curves 1 through 30 on Figure 11-17 and curves 31 through 38 on Figure 11-18. The same idea was used in showing the provisional values against the background of data points in Figures 11-15 and 11-16.

With the exception of the work of Gillespie, Olsen, and Nichols [T38674] (curves 2-5) and Kroeckel [T31344] (curves 34-36), all the reported data are for room temperature. Most of the room temperature data show the usual behavior - a transmittance over 80% between 1 and 2 μm and a cut off between 4 and 5 μm . The data not showing this behavior are for a specimen 0.022 mm thick (curves 15 and 16), a specimen 6500 Å thick (curve 17), opal (curve 18), silica gel (curve 20), and fused quartz in 2 gm polyethylene binder (curve 21).

A strong word of caution needs to be expressed concerning the absorption band that can exist in the area of 2.8 to 2.9 μm . The decrease in transmittance due to this absorption band can be very large (see curves 22, 24, and 26) or barely exist (see curve 25). This decrease depends on the type of vitreous silica.

Provisional values, for various situations, are listed in Table 11-22 and shown in Figures 11-15 and 11-16. One set of values is for Dynasil 1000 and holds for a 10 mm thick specimen at 293 K with a coverage of wavelength from 0.157 to 4.39 μm . Another is applicable to a 1 mm thick specimen of Optosil 1 at 293 K. The transmittance is less than 0.005 from 5 to 16 μm . The only high temperature data that includes 3.8 μm is the data of Gillespie [T38674] (curves 1-5) for the G. E. type 106 fused quartz kind of vitreous silica. To cover the effect of temperature, two provisional curves for G. E. type 106 fused quartz are given. Both are for a 2.8 mm thick specimen and polished. One curve is for a temperature of 373 K and the other is for 673 K. An uncertainty of within 30% is assigned to all these curves because the transmittance values are low in some places with a consequently high percentage and because there is not confirmatory data for individual data sets.

TABLE 11-22. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| DYNASIL 1000 1CMR THICK T = 293 | | DYNASIL 1000 10MM THICK T = 293 (CONT.) | | DYNASIL 1000 10MM THICK T = 293 (CONT.) | | GE TYPE 106 2.9MM THICK T = 673 | | OPTOSIL 1 1MM THICK T = 293 | |
|---------------------------------------|--------|---|--------|---|--------|---------------------------------------|--------|-----------------------------------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 0.157 | 0.017 | 1.48 | 0.928 | 3.33 | 0.118 | 2.00 | 0.933 | 5.0 | 0.005 |
| 0.160 | 0.249 | 1.55 | 0.930 | 4.00 | 0.098 | 2.30 | 0.528 | 5.5 | 0.005 |
| 0.166 | 0.500 | 1.64 | 0.928 | 4.05 | 0.077 | 2.52 | 0.919 | 6.0 | 0.005 |
| 0.169 | 0.657 | 1.75 | 0.922 | 4.19 | 0.047 | 2.84 | 0.919 | 6.5 | 0.005 |
| 0.171 | 0.746 | 1.84 | 0.914 | 4.39 | 0.030 | 3.00 | 0.899 | 7.0 | 0.005 |
| 0.173 | 0.792 | 1.93 | 0.903 | 3.14 | 0.981 | 3.14 | 0.881 | 7.5 | 0.005 |
| 0.175 | 0.817 | 1.98 | 0.884 | 3.49 | 0.881 | 3.37 | 0.872 | 8.0 | 0.005 |
| 0.178 | 0.832 | 2.00 | 0.832 | 3.61 | 0.799 | 3.52 | 0.852 | 8.5 | 0.005 |
| 0.184 | 0.852 | 2.02 | 0.871 | 3.72 | 0.697 | 3.67 | 0.721 | 9.0 | 0.005 |
| 0.188 | 0.865 | 2.06 | 0.846 | 3.77 | 0.620 | 3.80 | 0.530 | 9.5 | 0.005 |
| 0.197 | 0.880 | 2.08 | 0.816 | 3.83 | 0.060 | 3.83 | 0.490 | 10.0 | 0.005 |
| 0.204 | 0.930 | 2.14 | 0.701 | 3.86 | 0.562 | 3.90 | 0.459 | 10.5 | 0.005 |
| 0.211 | 0.898 | 2.17 | 0.635 | 3.94 | 0.562 | 4.00 | 0.437 | 11.0 | 0.005 |
| 0.215 | 0.900 | 2.20 | 0.600 | 4.00 | 0.552 | 4.11 | 0.352 | 11.5 | 0.005 |
| 0.220 | 0.908 | 2.24 | 0.624 | 4.02 | 0.549 | 4.19 | 0.248 | 12.0 | 0.005 |
| 0.230 | 0.915 | 2.33 | 0.754 | 4.16 | 0.403 | 4.31 | 0.224 | 12.5 | 0.005 |
| 0.236 | 0.918 | 2.40 | 0.841 | 4.22 | 0.319 | 4.35 | 0.136 | 13.0 | 0.005 |
| 0.242 | 0.923 | 2.43 | 0.850 | 4.28 | 0.308 | 4.39 | 0.077 | 13.5 | 0.005 |
| 0.246 | 0.924 | 2.47 | 0.840 | 4.33 | 0.201 | 4.47 | 0.052 | 14.0 | 0.005 |
| 0.252 | 0.927 | 2.53 | 0.703 | 4.37 | 0.130 | 4.71 | 0.031 | 14.5 | 0.005 |
| 0.266 | 0.932 | 2.55 | 0.654 | 4.49 | 0.084 | 4.78 | 0.000 | 15.0 | 0.005 |
| 0.281 | 0.932 | 2.61 | 0.335 | 4.60 | 0.100 | 5.00 | 0.000 | 16.0 | 0.005 |
| 0.299 | 0.932 | 2.64 | 0.144 | 4.71 | 0.060 | 6.00 | 0.000 | | |
| 0.339 | 0.933 | 2.65 | 0.100 | 4.76 | 0.028 | | | | |
| 0.398 | 0.933 | 2.70 | 0.657 | 4.86 | 0.000 | | | | |
| 0.493 | 0.934 | 2.77 | 0.042 | 5.00 | 0.000 | | | | |
| 0.560 | 0.935 | 2.83 | 0.061 | 6.00 | 0.000 | | | | |
| 0.743 | 0.937 | 2.89 | 0.102 | | | | | | |
| 0.805 | 0.937 | 2.92 | 0.415 | | | | | | |
| 1.00 | 0.933 | 2.93 | 0.609 | | | | | | |
| 1.22 | 0.930 | 2.95 | 0.743 | | | | | | |
| 1.27 | 0.921 | 3.00 | 0.776 | | | | | | |
| 1.29 | 0.903 | 3.04 | 0.782 | | | | | | |
| 1.31 | 0.882 | 3.10 | 0.773 | | | | | | |
| 1.32 | 0.869 | 3.38 | 0.529 | | | | | | |
| 1.34 | 0.859 | 3.66 | 0.304 | | | | | | |
| 1.37 | 0.870 | 3.77 | 0.203 | | | | | | |
| 1.41 | 0.898 | 3.80 | 0.182 | | | | | | |
| 1.43 | 0.915 | 3.84 | 0.154 | | | | | | |

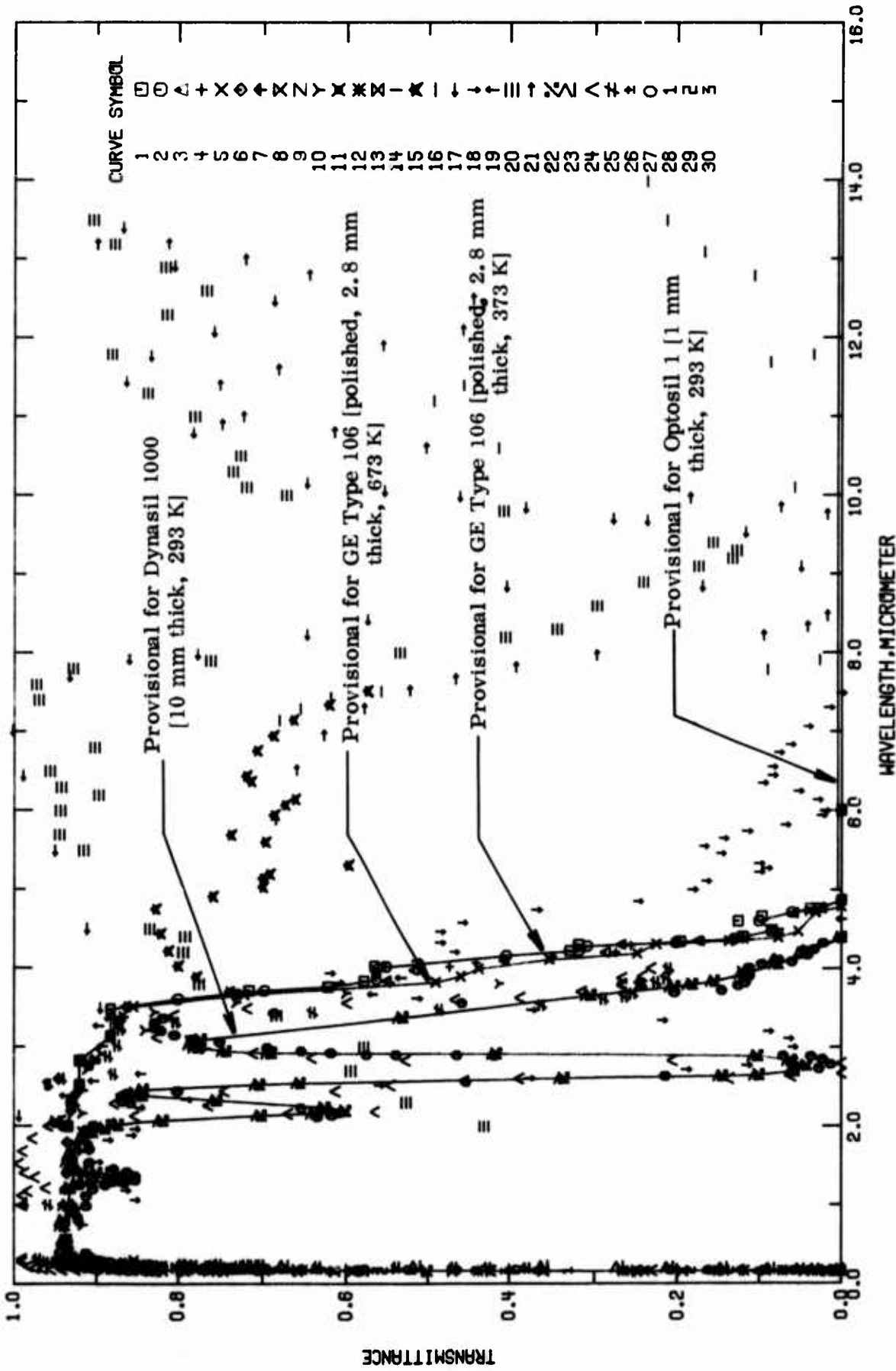


FIGURE 11-15. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

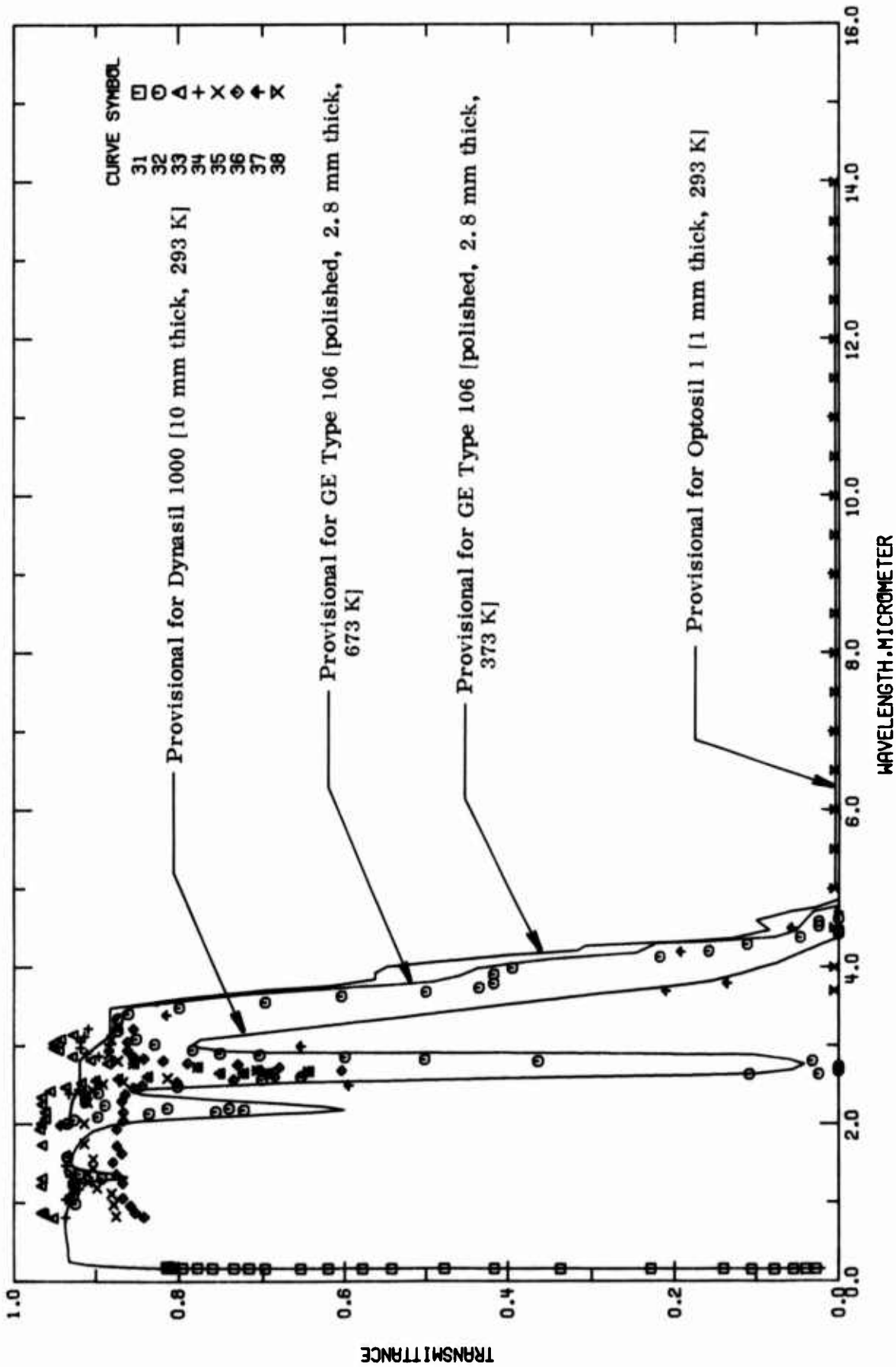


FIGURE 11-16. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE).

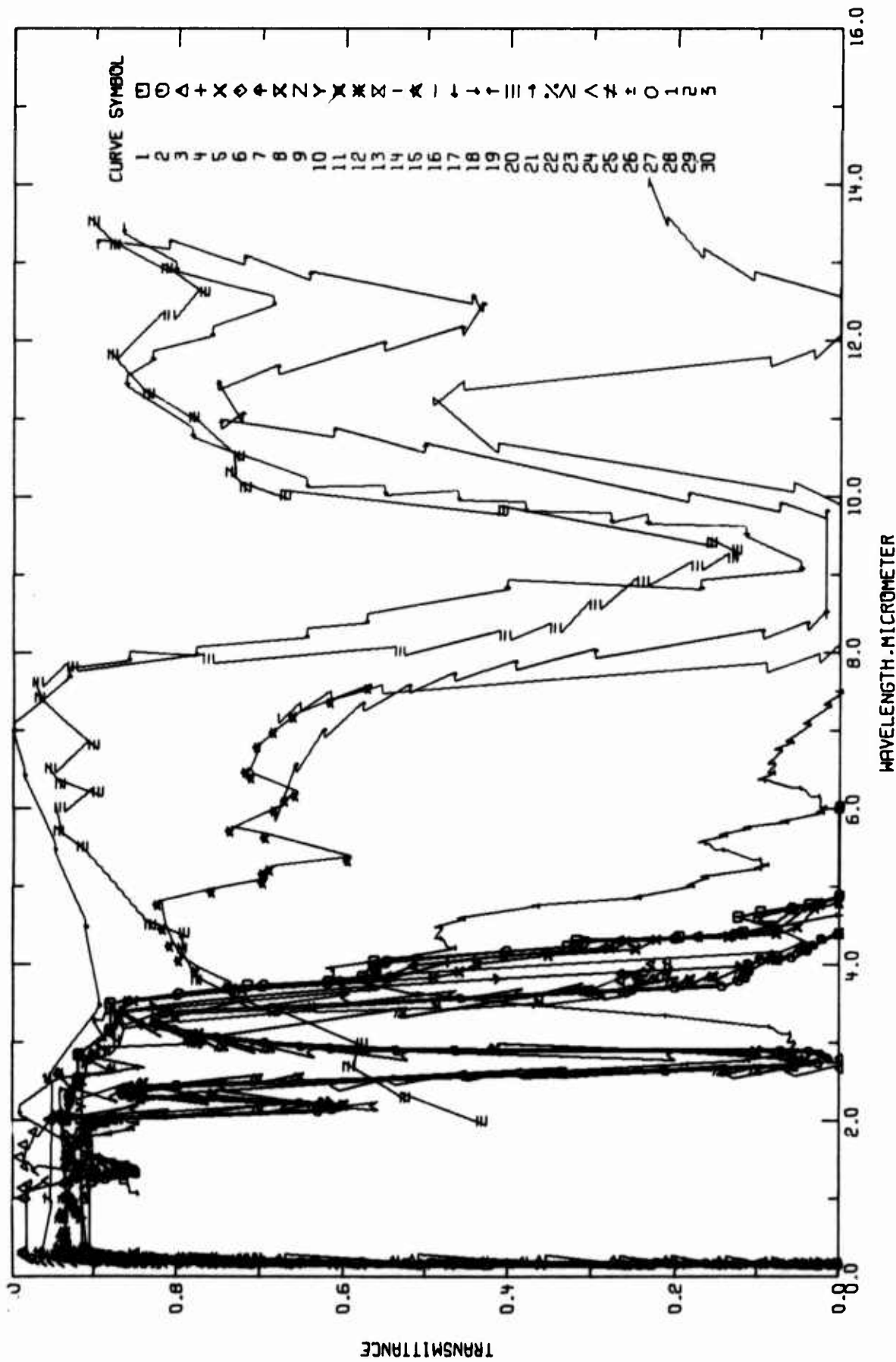


FIGURE 11-17. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE).

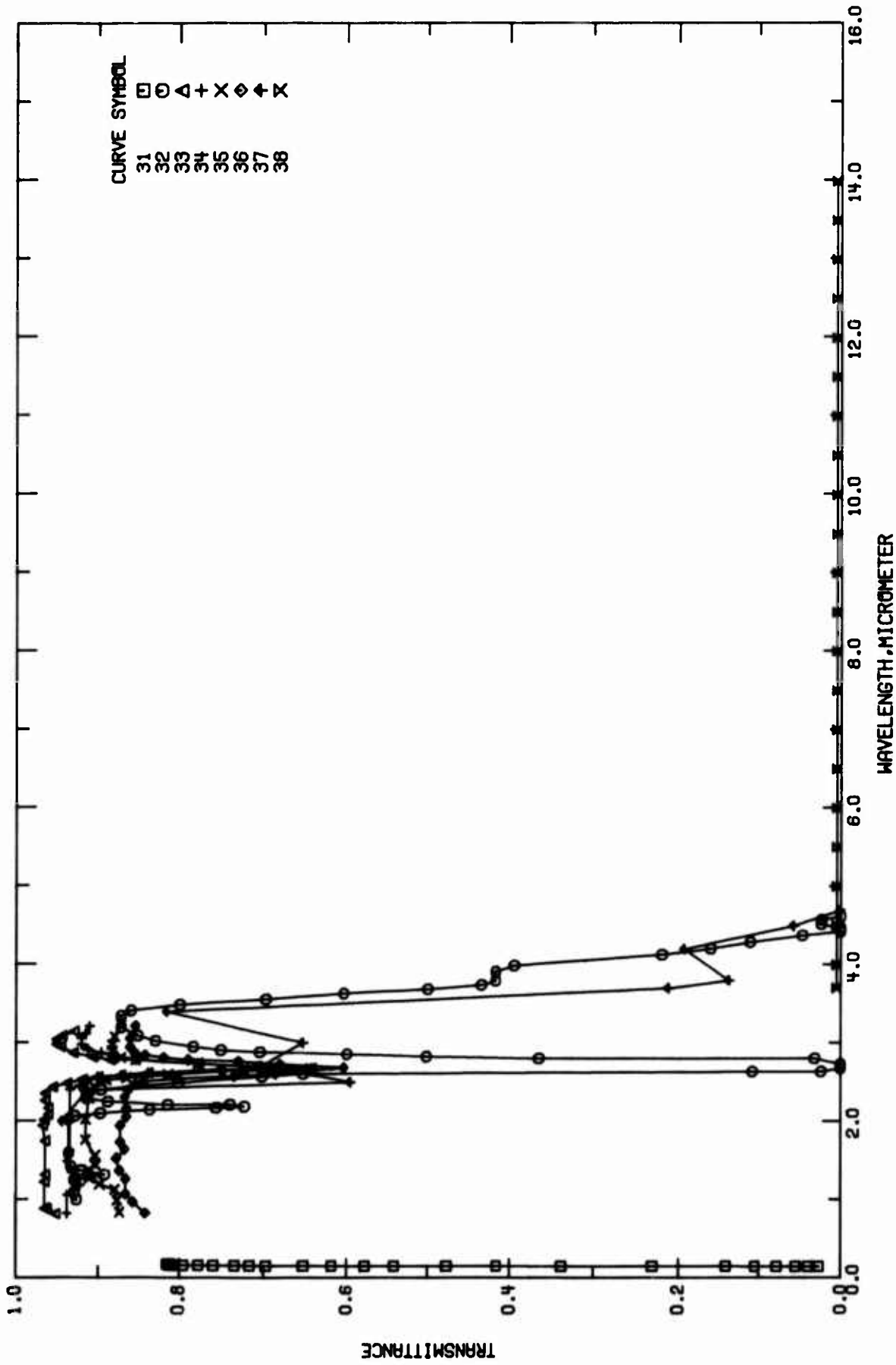


FIGURE 11-18. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS)
(WAVELENGTH DEPENDENCE).

TABLE 11-23. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------------|---|
| 1 T39674 | Gillespie, D. T., Glason, A. L., and Nichols, L. W. | 1965 | 2.0-6.0 | 298 | Fused Quartz; GE Type 106 | Disk specimen 3.150 cm in diameter and 2.8 mm thick; polished optically flat to within five green mercury fringes and a parallelism tolerance of $\pm 2.5 \mu\text{m}$; smooth values from figure; Perkin-Elmer model 21 spectrophotometer used; $\theta=0^\circ$, $\theta'=0^\circ$. The above specimen. |
| 2 T38674 | Gillespie, D. T., et al. | 1965 | 2.0-6.0 | 373 | Fused Quartz; GE Type 106 | The above specimen. |
| 3 T38674 | Gillespie, D. T., et al. | 1965 | 2.0-6.0 | 473 | Fused Quartz; GE Type 106 | The above specimen. |
| 4 T38674 | Gillespie, D. T., et al. | 1965 | 2.0-6.0 | 573 | Fused Quartz; GE Type 106 | The above specimen. |
| 5 T39674 | Gillespie, D. T., et al. | 1965 | 2.0-6.0 | 673 | Fused Quartz; GE Type 106 | The above specimen. |
| 6 T27141 | Bogdan, L. | 1964 | 0.80-2.6 | 293 | Fused Quartz | Disk specimen 0.375 in. in diameter and 0.0625 in. thick; clear fused quartz blank; data from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 7 T33865 | Laulainen, N.S. and McDermott, M.N. | 1966 | 0.19-0.30 | 293 | Fused Silica; Suprasil II | Two 0.0625 in. disks with an air space in between disks; measurements made with Cary model 14 spectrophotometer; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 8 T32965 | Laulainen, N.S. and McDermott, M.N. | 1966 | 0.19-0.30 | 293 | Fused Silica; Suprasil II | Similar to the above specimen except cemented by 0.0002 in. thick d-xylose obtained from Difco Labs, Detroit. |
| 9 T45017 | Sviridova, A.A. and Sukhovskaya, N.V. | 1967 | 0.19-0.42 | 293 | Fused Quartz | Specimen 35 mm in diameter and 2 mm thick; surfaces plane-parallel; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 10 T54563 | Callingaert, G., Herot, S. D., and Stair, R. | 1936 | 0.21-4.0 | 293 | Quartz | Synthetic fused quartz; amorphous; cylindrical specimen approx. 5/8 in. in diameter and 5/16 in. thick; two flat surfaces polished; measurement temperature not given explicitly, assumed to be 293 K; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$. |
| 11 T39011 | Heath, D.F. and Sacher, P.A. | 1966 | 0.16-0.30 | 293 | Fused Silica; Dynasil Optical Grade | High purity; specimen 6.46 mm thick; measured with aid of McPherson Model 225 monochromator; possibly measured in vacuum; data from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 12 T39011 | Heath, D.F. and Sacher, P.A. | 1966 | 0.16-0.30 | 293 | Fused Silica; Dynasil Optical Grade | The above specimen except irradiated with 10^{14} electrons cm^{-2} at 1.0 MeV and then 10^{14} electrons cm^{-2} at 2.0 MeV, irradiation times 30 min at each energy. |
| 13 T39011 | Heath, D.F. and Sacher, P.A. | 1966 | 0.16-0.30 | 293 | Fused Silica; Dynasil 1850 A | Specimen 2.04 mm thick; data from figure; possibly measured in vacuum; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 14 T39011 | Heath, D.F. and Sacher, P.A. | 1966 | 0.16-0.30 | 293 | Fused Silica; Dynasil 1850 A | The above specimen except irradiated with 10^{14} electrons cm^{-2} at 2.0 MeV incident through a sapphire shield, 6.4 mm thick. |
| 15 T38719 | Hanna, R. | 1965 | 3.7-7.5 | 293 | Fused Silica | Specimen $22 \pm 2 \times 10^{-3}$ mm thick; cut and ground but not polished; smooth values from figure; Perkin-Elmer model 130 instrument used below 15 μm and above Perkin-Elmer model 201 spectrophotometer used; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 16 T38719 | Hanna, R. | 1965 | 7.1-20 | 293 | Fused Silica | The above specimen. |
| 17 T30490 | Howarth, L.E. and Spitzer, W.G. | 1961 | 1.0-30 | 293 | Vitreous Silica | Specimen 6500 \AA thick; Perkin-Elmer single-beam double-pass spectrometer used; measurement temperature not given explicitly, assumed to be 293 K; $\theta=0^\circ$, $\theta'=0^\circ$. |

TABLE 11-23. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------------|------|---------------------------------|----------------------|-----------------------------------|---|
| 18 T51607 | Coblentz, M. W. | 1906 | 1.1-7.5 | 293 | Opal | $\text{SiO}_2 + \text{XH}_2\text{O}$ (opal contains varying amount of water from 5 to 30%); massive; transparent; thickness 0.12 mm; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 19 T35036 | Grenis, A. F. and Machovich, M. J. | 1965 | 1.0-4.6 | 293 | Fused Silica | Specimen approx. 5.08 cm in diameter and 3.18 mm thick; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 20 T43741 | Bartlet, R. W. and Gage, P. R. | 1964 | 2.0-15 | 293 | Silica Gel | Smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 21 T34168 | Engelsrath, A. | 1965 | 5.9-39 | 293 | Fused Quartz | 50 mg crushed fused quartz in 2 gm polyethylene binder; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; $\theta = 0^\circ$, $\theta' = 0^\circ$. |
| 22 T77041 | Dynasil Corporation of America | 1975 | 0.16-4.4 | 293 | Dynasil 1000 Fused Silica | Typical analysis has total metallic impurity content approx. 0.0001-0.0002, water content approx. 0.06-0.1, 0.00865 Cl, <0.0001 B, 0.000020 Fe, 0.000020 Li, <0.000008 Cd, <0.000005 Ge, <0.000003 Ti, <0.000004 Bi, <0.000003 Be, <0.000002 Al, <0.000002 Ga, 0.000002 Na, 0.000006 Cr, 0.0000025 Br, 0.000001 Au, 0.000001 Co, 0.0000004 Sb, and the following not detected, As, Cs, Cu, Mn, Rb, Ag, Ti, V, and Zn; specimen thickness 10 mm; smooth values from figure; temperature not given explicitly, presumed to be room temperature, 293 K assigned; reflection losses are included. |
| 23 T77041 | Dynasil Corporation of America | 1973 | 0.18-4.4 | 293 | Dynasil 4000 Fused Silica | Similar to the above specimen. |
| 24 A00010 | Thermal American Fused Quartz Co. | | 0.17-4.0 | 293 | Spectrosil Synthetic Fused Quartz | <0.00001 Ca, <0.00001 Fe, 0.000004 Na, <0.000002 Al, <0.000001 B, <0.0000004 Ga, <0.0000004 K, <0.000001 P, <0.000001 Mn, <0.0000002 As, <0.0000002 Cu, and 0.0000001 Sb (see Hetherington, G. and Bell, L. W., "Analysis of High-Purity Synthetic Vitreous Silicas," Physics and Chemistry of Glasses, 5(5), 206-8, 1967, [A00011]); 10 mm path; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 25 A00010 | Thermal American Fused Quartz Co. | | 0.20-4.0 | 293 | Vitreosil I.R. | 99.8% SiO_2 ; 10 mm path; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 26 T76891 | Corning Glass Works | 1971 | 0.16-4.4 | 293 | Corning Code 7940 Fused Silica | Typical analysis 0.0010-0.0100 Cl, 0.00001-0.0001 Ca, 0.00001-0.0010 Ti, 0.000005-0.0005 Al, 0.000005-0.00005 Be, 0.000003-0.00005 Zn, 0.000001-0.00001 Bi, 0.000001-0.000005 Cu, 0.000001-0.0005 Fe, 0.000001-0.00001 N, 0.000001-0.000001 Mg, 0.000001-0.0001 Na, 0.000001-0.00001 P, 0.000001-0.00001 V, 0.0000001-0.0000005 As, 0.0000001-0.000005 Cr, 0.0000001-0.000001 Mn, and 0.0000001-0.0000005 Sb, maximum total impurities other than water do not exceed 0.01, water content estimated at 0.1 or less; amorphous, made by flame hydrolysis; specimen 10 mm thick; minimum transmittance for U.V. grades; surface reflections included; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 27 T76891 | Corning Glass Works | 1971 | 0.18-4.4 | 293 | Corning Code 7940 Fused Silica | Similar to the above specimen except minimum transmittance values for optical and industrial grades. |
| 28 T76891 | Corning Glass Works | 1971 | 0.16-0.19 | 293 | Corning Code 7940 Fused Silica | Same typical analysis, impurity content, and method of fabrication as above; specimen 10 mm thick; U.V. grade; surface reflections included smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K. |
| 29 T76891 | Corning Glass Works | 1971 | 0.16-0.18 | 293 | Corning Code 7940 Fused Silica | Similar to the above specimen except 5 mm thick. |

TABLE 11-23. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VTREOUS) (Wavelength Dependence) (continued)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent). Specifications, and Remarks |
|-------------------|-----------------------------------|------|---------------------------------|----------------------|--------------------------------|--|
| 30 T76891 | Corning Glass Works | 1971 | 0.15-0.19 | 293 | Corning Code 7940 Fused Silica | Similar to the above specimen except 1 mm thick. |
| 31 T76891 | Corning Glass Works | 1971 | 0.15-0.19 | 293 | Corning Code 7940 Fused Silica | Similar to the above specimen except 0.5 mm thick. |
| 32 T76891 | Corning Glass Works | 1971 | 1.0-4.6 | 298 | Corning Code 7940 Fused Silica | Same typical analysis, impurity content, and method of fabrication as above; specimen 5.0 mm thick. |
| 33 T31344 | Kroedel, O. | 1964 | 0.82-3.2 | 293 | Quartz Glass | Smooth values from figure; relative error in transmission of 3.5%; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 34 T31344 | Kroedel, O. | 1964 | 0.83-3.2 | 773 | Quartz Glass | Similar to the above specimen. |
| 35 T31344 | Kroedel, O. | 1964 | 0.84-3.2 | 973 | Quartz Glass | Similar to the above specimen. |
| 36 T31344 | Kroedel, O. | 1964 | 0.83-3.2 | 1173 | Quartz Glass | Similar to the above specimen. |
| 37 T30100 | McCarthy, D.E. | 1963 | 2.0-50 | 293 | Quartz | Synthetic; specimen 2 mm thick; ground and polished to a flatness of seven fringes or better; reference standard was aluminum mirror; smooth values from figure; measurement temperature not given explicitly, assumed to be 293 K; Beckman IR-5A used in 2-16 μm range and Beckman IR-7 with CsI interchange used in 12.5-50 μm range; $\theta=0^\circ$, $\theta'=0^\circ$. |
| 38 Accov... | Champetier, R.J. and Friese, G.J. | 1974 | 3.7-16 | 293 | Optosil 1 Fused Silica | Specimen 1 mm thick; measured at Aerospace Corporation's Material Sciences Laboratory; measurement temperature not given explicitly, assumed to be 293 K; complete opacity (<0.005 transmittance from 3.7 to at least 16 μm); $\theta=0^\circ$, $\theta'=0^\circ$. |

TABLE 11-2. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | | | | | | |
|----------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|--------|-------|--|--|--|--|--|
| CURVE 1 | | | | | | | | | | | | | | | | | | | |
| T = 290. | | | | | | | | | | | | | | | | | | | |
| 2.00 | 0.933 | 4.33 | 0.201 | 1.52 | 0.863 | 0.800 | 0.920 | 0.243 | 0.921 | 0.1697 | 0.591 | 0.1946 | 0.837 | | | | | | |
| 2.31 | 0.928 | 4.37 | 0.130 | 3.68 | 0.734 | 0.800 | 0.920 | 0.291 | 0.942 | 0.1748 | 0.696 | 0.1997 | 0.846 | | | | | | |
| 2.53 | 0.919 | 4.48 | 0.044 | 3.92 | 0.544 | 0.850 | 0.921 | 0.359 | 0.942 | 0.1795 | 0.769 | 0.2045 | 0.867 | | | | | | |
| 2.84 | 0.919 | 4.60 | 0.100 | 4.02 | 0.472 | 0.900 | 0.926 | 0.418 | 0.939 | 0.1849 | 0.795 | 0.2097 | 0.877 | | | | | | |
| 3.15 | 0.881 | 4.71 | 0.050 | 4.97 | 0.440 | 0.950 | 0.924 | CURVE 10 | | | | | | | | | | | |
| 3.49 | 0.881 | 4.76 | 0.028 | 4.15 | 0.349 | 1.00 | 0.928 | T = 293. | | | | | | | | | | | |
| 3.72 | 0.715 | 4.86 | 0.000 | 4.20 | 0.274 | 1.20 | 0.935 | 0.310 | 0.912 | 0.2148 | 0.886 | 0.2497 | 0.939 | | | | | | |
| 3.77 | 0.620 | 6.00 | 0.000 | 4.29 | 0.256 | 1.40 | 0.934 | 0.750 | 0.914 | 0.2196 | 0.901 | 0.2548 | 0.941 | | | | | | |
| 3.84 | 0.578 | CURVE 3 | | | | | | | | | | | | | | | | | |
| 4.63 | 0.565 | T = 473. | | | | | | | | | | | | | | | | | |
| 4.22 | 0.328 | 2.00 | 0.933 | 4.44 | 0.076 | 1.80 | 0.934 | 2.17 | 0.915 | 0.2298 | 0.924 | 2.98 | 0.767 | | | | | | |
| 4.30 | 0.310 | 2.31 | 0.928 | 4.72 | 0.043 | 2.00 | 0.939 | 2.46 | 0.914 | 0.2400 | 0.929 | 2.98 | 0.767 | | | | | | |
| 4.34 | 0.196 | 2.52 | 0.919 | 4.78 | 0.022 | 2.40 | 0.929 | 2.73 | 0.909 | 0.2497 | 0.933 | 3.09 | 0.785 | | | | | | |
| 4.40 | 0.119 | 3.52 | 0.862 | 4.86 | 0.000 | 2.60 | 0.944 | 2.85 | 0.899 | 0.2550 | 0.941 | 3.22 | 0.838 | | | | | | |
| 4.48 | 0.085 | 3.68 | 0.734 | 6.00 | 0.000 | CURVE 7 | | | | | | | | | | | | | |
| 4.66 | 0.097 | 3.98 | 0.549 | T = 293. | | | | | | | | | | | | | | | |
| 4.76 | 0.039 | 3.98 | 0.549 | 0.190 | 0.695 | 0.190 | 0.739 | 3.09 | 0.785 | 0.2649 | 0.934 | 3.69 | 0.599 | | | | | | |
| 4.86 | 0.000 | 4.10 | 0.406 | 0.200 | 0.768 | 0.200 | 0.831 | 3.22 | 0.838 | 0.2698 | 0.928 | 3.81 | 0.411 | | | | | | |
| 6.00 | 0.000 | 4.20 | 0.267 | 0.210 | 0.831 | 0.210 | 0.864 | 3.39 | 0.864 | 0.2748 | 0.945 | 3.97 | 0.121 | | | | | | |
| CURVE 2 | | | | | | | | | | | | | | | | | | | |
| T = 373. | | | | | | | | | | | | | | | | | | | |
| 2.00 | 0.933 | 4.30 | 0.268 | 2.64 | 0.919 | 0.250 | 0.887 | 3.45 | 0.826 | 0.2798 | 0.936 | 0.1601 | 0.000 | | | | | | |
| 2.30 | 0.929 | 4.35 | 0.176 | 3.14 | 0.881 | 0.300 | 0.909 | 3.57 | 0.730 | 0.2848 | 0.935 | 0.1614 | 0.002 | | | | | | |
| 2.52 | 0.919 | 4.38 | 0.124 | 3.52 | 0.852 | CURVE 8 | | | | | | | | | | | | | |
| 2.84 | 0.919 | 4.48 | 0.084 | 3.67 | 0.721 | T = 293. | | | | | | | | | | | | | |
| 3.14 | 0.881 | 4.70 | 0.058 | 3.83 | 0.459 | 0.190 | 0.739 | 3.69 | 0.599 | 0.2898 | 0.942 | 0.1628 | 0.029 | | | | | | |
| 3.49 | 0.881 | 4.76 | 0.024 | 3.90 | 0.437 | 0.200 | 0.761 | 3.81 | 0.411 | 0.2949 | 0.941 | 0.1641 | 0.071 | | | | | | |
| 3.61 | 0.799 | 4.86 | 0.000 | 4.00 | 0.437 | 0.210 | 0.800 | 3.97 | 0.121 | 0.3000 | 0.942 | 0.1652 | 0.148 | | | | | | |
| 3.72 | 0.697 | 6.00 | 0.000 | 4.11 | 0.352 | 0.220 | 0.817 | CURVE 11 | | | | | 0.1667 | 0.265 | | | | | |
| 3.77 | 0.620 | T = 293. | | | | | | | | | | | | | | | | | |
| 3.86 | 0.562 | 2.00 | 0.933 | 4.31 | 0.224 | 0.250 | 0.840 | 3.22 | 0.838 | 0.2748 | 0.945 | 0.1699 | 0.437 | | | | | | |
| 3.94 | 0.562 | 2.31 | 0.928 | 4.35 | 0.136 | 0.300 | 0.851 | 3.39 | 0.864 | 0.2798 | 0.936 | 0.1748 | 0.650 | | | | | | |
| 4.62 | 0.549 | 2.52 | 0.919 | 4.39 | 0.077 | CURVE 9 | | | | | | | | | | | | | |
| 4.16 | 0.403 | 2.84 | 0.881 | 4.47 | 0.052 | T = 293. | | | | | | | | | | | | | |
| 4.22 | 0.310 | 3.52 | 0.862 | 4.71 | 0.031 | 0.191 | 0.777 | 0.1636 | 0.091 | 0.1652 | 0.148 | 0.1667 | 0.265 | | | | | | |
| 4.28 | 0.308 | 3.68 | 0.734 | 4.78 | 0.000 | 0.216 | 0.809 | 0.1628 | 0.045 | 0.1641 | 0.071 | 0.1699 | 0.437 | | | | | | |
| | | 3.98 | 0.549 | 5.00 | 0.000 | 0.191 | 0.777 | 0.1652 | 0.238 | 0.1748 | 0.584 | 0.1739 | 0.650 | | | | | | |
| | | 4.10 | 0.406 | | | 0.216 | 0.809 | 0.1671 | 0.421 | | | | | | | | | | |

TABLE 11-24. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | |
|------------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-------|
| CURVE 12 (CONT.) | | | | | | | | | | |
| 0.1848 | 0.598 | 0.1952 | 0.861 | 0.2051 | 0.894 | 6.44 | 0.719 | 1.40 | 0.856 | |
| 0.1897 | 0.725 | 0.1999 | 0.872 | 0.2130 | 0.902 | 6.76 | 0.706 | 2.13 | 0.992 | |
| 0.1948 | 0.738 | 0.2053 | 0.875 | 0.2143 | 0.909 | 6.95 | 0.687 | 2.53 | 0.956 | |
| 0.1997 | 0.749 | 0.2102 | 0.886 | 0.2250 | 0.901 | 7.15 | 0.663 | 3.51 | 0.894 | |
| 0.2046 | 0.735 | 0.2150 | 0.899 | 0.2301 | 0.910 | 7.34 | 0.619 | 4.51 | 0.910 | |
| 0.2097 | 0.740 | 0.2200 | 0.905 | 0.2351 | 0.922 | 7.52 | 0.574 | 5.50 | 0.548 | |
| 0.2148 | 0.750 | 0.2249 | 0.903 | 0.2399 | 0.914 | CURVE 16 | | | | |
| 0.2197 | 0.756 | 0.2300 | 0.912 | 0.2450 | 0.921 | T = 293. | | | | |
| 0.2247 | 0.784 | 0.2350 | 0.912 | 0.2498 | 0.919 | 7.14 | 0.680 | 7.71 | 0.931 | |
| 0.2298 | 0.793 | 0.2400 | 0.908 | 0.2550 | 0.927 | 7.29 | 0.654 | 7.93 | 0.858 | |
| 0.2347 | 0.817 | 0.2453 | 0.921 | 0.2599 | 0.923 | 7.43 | 0.617 | 7.99 | 0.777 | |
| 0.2396 | 0.841 | 0.2500 | 0.918 | 0.2648 | 0.923 | 7.51 | 0.556 | 8.23 | 0.646 | |
| 0.2448 | 0.855 | 0.2550 | 0.928 | 0.2701 | 0.927 | 7.79 | 0.090 | 8.42 | 0.574 | |
| 0.2498 | 0.869 | 0.2600 | 0.936 | 0.2752 | 0.924 | 7.91 | 0.026 | 8.85 | 0.403 | |
| 0.2549 | 0.883 | 0.2648 | 0.939 | 0.2799 | 0.927 | 8.04 | 0.000 | 8.85 | 0.170 | |
| 0.2599 | 0.890 | 0.2704 | 0.940 | 0.2853 | 0.929 | 9.10 | 0.049 | 9.10 | 0.049 | |
| 0.2648 | 0.891 | 0.2751 | 0.942 | 0.2902 | 0.929 | 9.54 | 0.116 | 9.54 | 0.116 | |
| 0.2697 | 0.913 | 0.2796 | 0.928 | 0.2948 | 0.926 | 9.69 | 0.236 | 9.69 | 0.236 | |
| 0.2748 | 0.916 | 0.2850 | 0.929 | 0.3000 | 0.907 | 10.1 | 0.057 | 9.71 | 0.278 | |
| 0.2799 | 0.930 | 0.2902 | 0.937 | CURVE 15 | | | | | | 0.380 |
| 0.2848 | 0.928 | 0.2946 | 0.942 | T = 293. | | | | | | 0.461 |
| 0.2899 | 0.929 | 0.3000 | 0.927 | 3.70 | 0.735 | 11.4 | 0.456 | 10.06 | 0.552 | |
| 0.2951 | 0.925 | CURVE 14 | | | | | | | | 0.546 |
| 0.3000 | 0.929 | T = 293. | | | | | | | | 0.782 |
| CURVE 13 | | | | | | | | | | |
| T = 293. | | | | | | | | | | |
| 0.1595 | 0.004 | 0.1599 | 0.011 | 4.03 | 0.779 | 11.7 | 0.087 | 10.16 | 0.546 | |
| 0.1607 | 0.044 | 0.2200 | 0.909 | 4.22 | 0.810 | 11.8 | 0.034 | 10.80 | 0.782 | |
| 0.1631 | 0.193 | 0.1606 | 0.045 | 4.44 | 0.819 | 12.0 | 0.000 | 11.46 | 0.862 | |
| 0.1647 | 0.359 | 0.1631 | 0.193 | 4.75 | 0.825 | 12.6 | 0.000 | 11.78 | 0.831 | |
| 0.1656 | 0.469 | 0.1649 | 0.359 | 4.91 | 0.755 | 12.8 | 0.106 | 12.09 | 0.758 | |
| 0.1667 | 0.578 | 0.1667 | 0.580 | 5.03 | 0.699 | 13.1 | 0.168 | 12.48 | 0.686 | |
| 0.1667 | 0.612 | 0.1667 | 0.612 | 5.14 | 0.699 | 13.5 | 0.212 | 12.92 | 0.803 | |
| 0.1701 | 0.753 | 0.1702 | 0.762 | 5.19 | 0.691 | 14.0 | 0.236 | 13.41 | 0.866 | |
| 0.1749 | 0.924 | 0.1750 | 0.849 | 5.31 | 0.597 | 14.7 | 0.245 | 14.47 | 0.908 | |
| 0.1803 | 0.845 | 0.1799 | 0.869 | 5.60 | 0.696 | 15.5 | 0.229 | 16.37 | 0.911 | |
| 0.1850 | 0.853 | 0.1799 | 0.869 | 5.69 | 0.737 | 16.9 | 0.158 | 17.37 | 0.895 | |
| 0.1901 | 0.855 | 0.1850 | 0.875 | 5.94 | 0.686 | 18.2 | 0.075 | 18.65 | 0.878 | |
| 0.1901 | 0.855 | 0.1904 | 0.861 | 6.07 | 0.673 | 19.5 | 0.000 | 19.61 | 0.853 | |
| 0.1951 | 0.863 | 0.1951 | 0.866 | 6.14 | 0.661 | CURVE 17 | | | | |
| 0.1901 | 0.855 | 0.1999 | 0.890 | 6.37 | 0.713 | T = 293. | | | | |
| CURVE 17 (CONT.) | | | | | | | | | | |
| 21.20 | 0.338 | 1.40 | 0.856 | 6.44 | 0.719 | 7.02 | 1.00 | 7.02 | 0.644 | |
| 21.38 | 0.204 | 2.13 | 0.992 | 6.76 | 0.706 | 7.14 | 0.931 | 7.71 | 0.730 | |
| 21.65 | 0.235 | 2.53 | 0.956 | 6.95 | 0.687 | 7.29 | 0.858 | 7.93 | 0.786 | |
| 22.36 | 0.276 | 3.51 | 0.894 | 7.15 | 0.663 | 7.43 | 0.777 | 7.99 | 0.811 | |
| 22.87 | 0.360 | 4.51 | 0.910 | 7.34 | 0.619 | 7.51 | 0.556 | 8.23 | 0.840 | |
| 23.43 | 0.456 | 5.50 | 0.548 | 7.52 | 0.574 | 7.79 | 0.090 | 8.42 | 0.861 | |
| 24.42 | 0.580 | 6.45 | 0.387 | 7.71 | 0.403 | 7.91 | 0.026 | 8.85 | 0.861 | |
| 25.04 | 0.644 | 7.02 | 1.00 | 7.93 | 0.170 | 8.04 | 0.000 | 9.10 | 0.895 | |
| 25.89 | 0.730 | 7.71 | 0.931 | 8.23 | 0.049 | 9.10 | 0.116 | 9.54 | 0.895 | |
| 26.98 | 0.786 | 7.93 | 0.858 | 8.42 | 0.049 | 9.69 | 0.236 | 10.16 | 0.895 | |
| 27.55 | 0.811 | 7.99 | 0.777 | 8.85 | 0.170 | 10.1 | 0.057 | 9.71 | 0.850 | |
| 28.35 | 0.840 | 8.23 | 0.646 | 9.10 | 0.049 | 10.6 | 0.413 | 9.85 | 0.862 | |
| 29.04 | 0.861 | 8.42 | 0.574 | 9.54 | 0.116 | 11.2 | 0.493 | 9.99 | 0.974 | |
| 30.42 | 0.895 | 8.85 | 0.403 | 9.69 | 0.236 | 11.4 | 0.456 | 10.06 | 0.869 | |
| CURVE 18 | | | | | | | | | | |
| T = 293. | | | | | | | | | | |
| 1.07 | 0.850 | 9.71 | 0.278 | 11.7 | 0.087 | 11.8 | 0.034 | 10.80 | 0.600 | |
| 1.19 | 0.862 | 9.85 | 0.380 | 10.6 | 0.413 | 12.0 | 0.000 | 11.46 | 0.897 | |
| 1.32 | 0.974 | 9.99 | 0.461 | 11.2 | 0.493 | 12.6 | 0.000 | 11.78 | 0.910 | |
| 1.40 | 0.869 | 10.06 | 0.552 | 11.4 | 0.456 | 12.8 | 0.106 | 12.09 | 0.884 | |
| 1.48 | 0.600 | 10.16 | 0.546 | 11.7 | 0.087 | 13.1 | 0.168 | 12.48 | 0.855 | |
| 1.55 | 0.897 | 10.80 | 0.782 | 12.0 | 0.000 | 13.5 | 0.212 | 12.92 | 0.850 | |
| 1.68 | 0.910 | 11.46 | 0.862 | 12.6 | 0.000 | 14.0 | 0.236 | 13.41 | 0.800 | |
| 1.79 | 0.910 | 11.78 | 0.831 | 12.8 | 0.106 | 14.7 | 0.245 | 14.47 | 0.844 | |
| 1.83 | 0.884 | 12.09 | 0.758 | 13.1 | 0.168 | 15.5 | 0.229 | 16.37 | 0.789 | |
| 1.89 | 0.855 | 12.48 | 0.686 | 13.5 | 0.212 | 16.9 | 0.158 | 17.37 | 0.558 | |
| 1.97 | 0.850 | 12.92 | 0.803 | 14.0 | 0.236 | 18.2 | 0.075 | 18.65 | 0.375 | |
| 2.08 | 0.800 | 13.41 | 0.866 | 14.7 | 0.245 | 19.5 | 0.000 | 19.61 | 0.189 | |
| 2.24 | 0.844 | 14.47 | 0.908 | 15.5 | 0.229 | 19.92 | 0.807 | 19.92 | 0.114 | |
| 2.34 | 0.789 | 16.37 | 0.911 | 16.9 | 0.158 | 20.23 | 0.706 | 20.23 | 0.059 | |
| 2.52 | 0.558 | 17.37 | 0.895 | 18.2 | 0.075 | 20.47 | 0.608 | 20.47 | 0.059 | |
| 2.61 | 0.375 | 18.65 | 0.878 | 19.5 | 0.000 | 20.76 | 0.544 | 20.76 | 0.064 | |
| 2.72 | 0.189 | 19.61 | 0.853 | 19.92 | 0.807 | 20.96 | 0.453 | 20.96 | 0.089 | |
| 2.77 | 0.114 | 19.92 | 0.807 | 1.03 | 0.983 | CURVE 17 | | | | |
| 2.86 | 0.059 | 20.23 | 0.706 | T = 293. | | | | | | |
| 3.00 | 0.059 | 20.47 | 0.608 | CURVE 17 | | | | | | |
| 3.11 | 0.064 | 20.76 | 0.544 | T = 293. | | | | | | |
| 3.20 | 0.089 | 20.96 | 0.453 | CURVE 17 | | | | | | |
| T = 293. | | | | | | | | | | |

TABLE 11-24. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 18 (CONT.) | | | CURVE 19 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 21 (CONT.) | | | CURVE 22 (CONT.) | | |
|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|
| λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ |
| 3.34 | 0.217 | 0.936 | 2.39 | 0.936 | 0.297 | 9.97 | 0.165 | 0.632 | 0.170 | 0.632 | 0.170 | 0.632 | 0.632 | 0.946 |
| 3.47 | 0.373 | 0.902 | 2.58 | 0.902 | 0.241 | 10.5 | 0.502 | 0.852 | 0.184 | 0.852 | 0.184 | 0.852 | 0.816 | 0.816 |
| 3.62 | 0.512 | 0.843 | 2.67 | 0.843 | 0.175 | 10.8 | 0.513 | 0.865 | 0.188 | 0.865 | 0.188 | 0.865 | 0.701 | 0.701 |
| 3.82 | 0.608 | 0.900 | 2.81 | 0.900 | 0.132 | 10.9 | 0.748 | 0.880 | 0.197 | 0.880 | 0.197 | 0.880 | 0.635 | 0.635 |
| 3.94 | 0.619 | 0.891 | 3.02 | 0.891 | 0.127 | 11.0 | 0.722 | 0.890 | 0.204 | 0.890 | 0.204 | 0.890 | 0.600 | 0.600 |
| 4.06 | 0.556 | 0.896 | 3.28 | 0.896 | 0.157 | 11.4 | 0.681 | 0.898 | 0.211 | 0.898 | 0.211 | 0.898 | 0.624 | 0.624 |
| 4.10 | 0.512 | 0.862 | 3.37 | 0.862 | 0.457 | 11.6 | 0.554 | 0.900 | 0.215 | 0.900 | 0.215 | 0.900 | 0.754 | 0.754 |
| 4.21 | 0.467 | 0.567 | 3.67 | 0.567 | 0.672 | 11.9 | 0.554 | 0.900 | 0.220 | 0.900 | 0.220 | 0.900 | 0.841 | 0.841 |
| 4.33 | 0.485 | 0.531 | 3.88 | 0.531 | 0.715 | 12.1 | 0.457 | 0.915 | 0.230 | 0.915 | 0.230 | 0.915 | 0.850 | 0.850 |
| 4.47 | 0.435 | 0.479 | 4.15 | 0.479 | 0.735 | 12.4 | 0.444 | 0.923 | 0.236 | 0.923 | 0.236 | 0.923 | 0.840 | 0.840 |
| 4.58 | 0.457 | 0.643 | 4.26 | 0.643 | 0.726 | 12.5 | 0.444 | 0.923 | 0.242 | 0.923 | 0.242 | 0.923 | 0.703 | 0.703 |
| 4.74 | 0.367 | 0.077 | 4.49 | 0.077 | 0.740 | 12.8 | 0.643 | 0.924 | 0.246 | 0.924 | 0.246 | 0.924 | 0.654 | 0.654 |
| 4.85 | 0.247 | 0.000 | 4.62 | 0.000 | 0.835 | 13.0 | 0.720 | 0.927 | 0.252 | 0.927 | 0.252 | 0.927 | 0.335 | 0.335 |
| 5.00 | 0.182 | 0.165 | 5.00 | 0.165 | 0.860 | 13.2 | 0.810 | 0.932 | 0.266 | 0.932 | 0.266 | 0.932 | 0.144 | 0.144 |
| 5.11 | 0.165 | 0.182 | 5.11 | 0.182 | 0.812 | 13.2 | 0.898 | 0.932 | 0.281 | 0.932 | 0.281 | 0.932 | 0.100 | 0.100 |
| 5.22 | 0.100 | 0.100 | 5.22 | 0.100 | 0.767 | 15.1 | 0.800 | 0.932 | 0.299 | 0.932 | 0.299 | 0.932 | 0.057 | 0.057 |
| 5.27 | 0.091 | 0.091 | 5.27 | 0.091 | 0.814 | 17.2 | 0.605 | 0.933 | 0.339 | 0.933 | 0.339 | 0.933 | 0.042 | 0.042 |
| 5.33 | 0.100 | 0.100 | 5.33 | 0.100 | 0.877 | 18.5 | 0.597 | 0.933 | 0.398 | 0.933 | 0.398 | 0.933 | 0.061 | 0.061 |
| 5.46 | 0.146 | 0.146 | 5.46 | 0.146 | 0.902 | 19.5 | 0.467 | 0.934 | 0.493 | 0.934 | 0.493 | 0.934 | 0.102 | 0.102 |
| 5.55 | 0.168 | 0.168 | 5.55 | 0.168 | 0.901 | 19.9 | 0.348 | 0.935 | 0.560 | 0.935 | 0.560 | 0.935 | 0.415 | 0.415 |
| 5.65 | 0.143 | 0.143 | 5.65 | 0.143 | 0.878 | 20.2 | 0.099 | 0.937 | 0.743 | 0.937 | 0.743 | 0.937 | 0.689 | 0.689 |
| 5.74 | 0.114 | 0.114 | 5.74 | 0.114 | 0.827 | 20.4 | 0.013 | 0.933 | 0.805 | 0.933 | 0.805 | 0.933 | 0.743 | 0.743 |
| 5.82 | 0.068 | 0.068 | 5.82 | 0.068 | 0.847 | 21.4 | 0.013 | 0.933 | 1.00 | 0.933 | 1.00 | 0.933 | 0.776 | 0.776 |
| 5.94 | 0.024 | 0.024 | 5.94 | 0.024 | 0.847 | 22.4 | 0.065 | 0.930 | 1.22 | 0.930 | 1.22 | 0.930 | 0.702 | 0.702 |
| 6.00 | 0.020 | 0.020 | 6.00 | 0.020 | 0.791 | 23.0 | 0.202 | 0.921 | 1.27 | 0.921 | 1.27 | 0.921 | 0.773 | 0.773 |
| 6.14 | 0.029 | 0.029 | 6.14 | 0.029 | 0.832 | 28.2 | 0.822 | 0.903 | 1.29 | 0.903 | 1.29 | 0.903 | 0.529 | 0.529 |
| 6.25 | 0.052 | 0.052 | 6.25 | 0.052 | 0.914 | 29.6 | 0.839 | 0.882 | 1.31 | 0.882 | 1.31 | 0.882 | 0.304 | 0.304 |
| 6.35 | 0.096 | 0.096 | 6.35 | 0.096 | 0.943 | 30.5 | 0.963 | 0.869 | 1.32 | 0.869 | 1.32 | 0.869 | 0.203 | 0.203 |
| 6.45 | 0.084 | 0.084 | 6.45 | 0.084 | 0.942 | 30.5 | 0.853 | 0.859 | 1.34 | 0.859 | 1.34 | 0.859 | 0.182 | 0.182 |
| 6.56 | 0.084 | 0.084 | 6.56 | 0.084 | 0.896 | 30.5 | 0.853 | 0.859 | 1.34 | 0.859 | 1.34 | 0.859 | 0.154 | 0.154 |
| 6.74 | 0.076 | 0.076 | 6.74 | 0.076 | 0.941 | 30.5 | 0.853 | 0.859 | 1.37 | 0.859 | 1.37 | 0.859 | 0.154 | 0.154 |
| 6.84 | 0.062 | 0.062 | 6.84 | 0.062 | 0.954 | 30.5 | 0.853 | 0.859 | 1.41 | 0.859 | 1.41 | 0.859 | 0.118 | 0.118 |
| 7.07 | 0.041 | 0.041 | 7.07 | 0.041 | 0.901 | 30.5 | 0.853 | 0.859 | 1.43 | 0.859 | 1.43 | 0.859 | 0.077 | 0.077 |
| 7.31 | 0.015 | 0.015 | 7.31 | 0.015 | 0.960 | 30.5 | 0.853 | 0.859 | 1.48 | 0.859 | 1.48 | 0.859 | 0.047 | 0.047 |
| 7.49 | 0.000 | 0.000 | 7.49 | 0.000 | 0.971 | 30.5 | 0.853 | 0.859 | 1.55 | 0.859 | 1.55 | 0.859 | 0.000 | 0.000 |
| CURVE 19 | | | CURVE 22 | | | CURVE 23 | | | CURVE 24 | | | CURVE 25 | | |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | |
| 1.00 | 0.938 | 0.938 | 0.157 | 0.317 | 0.157 | 0.157 | 0.317 | 0.317 | 0.157 | 0.317 | 0.157 | 0.157 | 0.317 | 0.317 |
| | | | 0.160 | 0.240 | 0.160 | 0.160 | 0.240 | 0.240 | 0.160 | 0.240 | 0.160 | 0.160 | 0.240 | 0.240 |
| | | | 0.159 | 0.657 | 0.159 | 0.159 | 0.657 | 0.657 | 0.159 | 0.657 | 0.159 | 0.159 | 0.657 | 0.657 |
| | | | 0.171 | 0.746 | 0.171 | 0.171 | 0.746 | 0.746 | 0.171 | 0.746 | 0.171 | 0.171 | 0.746 | 0.746 |
| | | | 0.173 | 0.792 | 0.173 | 0.173 | 0.792 | 0.792 | 0.173 | 0.792 | 0.173 | 0.173 | 0.792 | 0.792 |
| | | | 0.175 | 0.817 | 0.175 | 0.175 | 0.817 | 0.817 | 0.175 | 0.817 | 0.175 | 0.175 | 0.817 | 0.817 |
| | | | 0.170 | 0.000 | 0.170 | 0.170 | 0.000 | 0.000 | 0.170 | 0.000 | 0.170 | 0.170 | 0.000 | 0.000 |
| | | | 0.184 | 0.030 | 0.184 | 0.184 | 0.030 | 0.030 | 0.184 | 0.030 | 0.184 | 0.184 | 0.030 | 0.030 |

TABLE 11-24. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 23 (CONT.) | | | CURVE 24 (CONT.) | | | CURVE 24 (CONT.) | | | CURVE 25 (CONT.) | | | CURVE 26 (CONT.) | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|--|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | |
| 0.188 | 0.048 | 2.14 | 0.701 | 0.177 | 0.865 | 2.856 | 0.640 | 0.275 | 0.954 | 0.201 | 0.816 | | | |
| 0.197 | 0.08+ | 2.17 | 0.635 | 0.179 | 0.932 | 2.922 | 0.711 | 0.296 | 0.964 | 0.209 | 0.840 | | | |
| 0.204 | 0.141 | 2.20 | 0.600 | 0.181 | 0.92+ | 3.026 | 0.775 | 0.304 | 0.969 | 0.220 | 0.869 | | | |
| 0.211 | 0.207 | 2.24 | 0.524 | 0.183 | 0.940 | 3.130 | 0.824 | 0.320 | 0.969 | 0.230 | 0.883 | | | |
| 0.216 | 0.269 | 2.33 | 0.754 | 0.189 | 0.953 | 3.263 | 0.868 | 1.000 | 0.957 | 0.240 | 0.895 | | | |
| 0.221 | 0.357 | 2.40 | 0.841 | 0.195 | 0.963 | 3.432 | 0.804 | 2.535 | 0.957 | 0.251 | 0.906 | | | |
| 0.230 | 0.511 | 2.43 | 0.850 | 0.207 | 0.973 | 3.491 | 0.718 | 2.605 | 0.941 | 0.261 | 0.909 | | | |
| 0.236 | 0.672 | 2.47 | 0.840 | 0.227 | 0.981 | 3.563 | 0.599 | 2.666 | 0.878 | 0.330 | 0.911 | | | |
| 0.242 | 0.787 | 2.53 | 0.703 | 0.279 | 0.989 | 3.602 | 0.467 | 2.785 | 0.909 | 0.398 | 0.911 | | | |
| 0.246 | 0.634 | 2.55 | 0.654 | 0.320 | 0.989 | 3.626 | 0.387 | 2.818 | 0.909 | 1.000 | 0.911 | | | |
| 0.252 | 0.971 | 2.61 | 0.335 | 1.000 | 0.989 | 3.699 | 0.315 | 2.892 | 0.885 | 1.128 | 0.911 | | | |
| 0.266 | 0.996 | 2.64 | 0.144 | 1.126 | 0.989 | 3.778 | 0.267 | 3.025 | 0.873 | 1.215 | 0.903 | | | |
| 0.281 | 0.913 | 2.65 | 0.100 | 1.177 | 0.982 | 3.874 | 0.267 | 3.231 | 0.869 | 1.267 | 0.888 | | | |
| 0.296 | 0.522 | 2.70 | 0.057 | 1.217 | 0.960 | 3.897 | 0.242 | 3.318 | 0.802 | 1.300 | 0.864 | | | |
| 0.339 | 0.926 | 2.77 | 0.042 | 1.330 | 0.867 | 4.000 | 0.231 | 3.446 | 0.639 | 1.333 | 0.850 | | | |
| 0.398 | 0.931 | 2.83 | 0.061 | 1.351 | 0.973 | 3.800 | 0.267 | 3.478 | 0.886 | 1.395 | 0.850 | | | |
| 0.493 | 0.93+ | 2.99 | 0.102 | 1.407 | 0.996 | | | 3.531 | 0.362 | 1.437 | 0.860 | | | |
| 0.560 | 0.335 | 2.92 | 0.415 | 1.523 | 0.993 | | | 3.605 | 0.289 | 1.471 | 0.877 | | | |
| 0.743 | 0.937 | 2.93 | 0.689 | 1.682 | 0.988 | | | 3.637 | 0.264 | 1.551 | 0.907 | | | |
| 0.805 | 0.937 | 2.95 | 0.743 | 1.845 | 0.976 | | | 3.679 | 0.254 | 1.727 | 0.907 | | | |
| 1.00 | 0.933 | 3.00 | 0.776 | 2.001 | 0.957 | | | 3.795 | 0.246 | 1.968 | 0.911 | | | |
| 1.22 | 0.930 | 3.04 | 0.782 | 2.372 | 0.942 | | | 3.820 | 0.225 | 2.028 | 0.902 | | | |
| 1.27 | 0.921 | 3.10 | 0.773 | 2.136 | 0.951 | | | 3.873 | 0.213 | 2.134 | 0.633 | | | |
| 1.29 | 0.903 | 3.38 | 0.529 | 2.158 | 0.670 | | | 4.000 | 0.210 | 2.157 | 0.616 | | | |
| 1.31 | 0.882 | 3.66 | 0.304 | 2.184 | 0.564 | | | 3.800 | 0.242 | 2.184 | 0.609 | | | |
| 1.32 | 0.869 | 3.77 | 0.203 | 2.261 | 0.765 | | | | | 2.218 | 0.619 | | | |
| 1.34 | 0.859 | 3.80 | 0.182 | 2.293 | 0.877 | | | | | 2.242 | 0.653 | | | |
| 1.37 | 0.870 | 3.84 | 0.154 | 2.327 | 0.925 | | | | | 2.313 | 0.856 | | | |
| 1.41 | 0.898 | 3.93 | 0.118 | 2.403 | 0.868 | | | | | 2.336 | 0.867 | | | |
| 1.43 | 0.915 | 4.06 | 0.177 | 2.445 | 0.745 | | | | | 2.389 | 0.857 | | | |
| 1.48 | 0.928 | 4.19 | 0.087 | 2.445 | 0.612 | | | | | 2.439 | 0.800 | | | |
| 1.55 | 0.930 | 4.39 | 0.000 | 2.517 | 0.544 | | | | | 2.463 | 0.800 | | | |
| 1.64 | 0.928 | | | 2.575 | 0.455 | | | | | 2.580 | 0.453 | | | |
| 1.75 | 0.922 | | | 2.601 | 0.389 | | | | | 2.652 | 0.214 | | | |
| 1.84 | 0.914 | | | 2.601 | 0.136 | | | | | 2.718 | 0.057 | | | |
| 1.93 | 0.903 | | | 2.629 | 0.061 | | | | | 2.745 | 0.027 | | | |
| 1.98 | 0.888 | 0.165 | 0.123 | 2.661 | 0.008 | | | | | 2.799 | 0.013 | | | |
| 2.02 | 0.871 | 0.165 | 0.229 | 2.789 | 0.000 | | | | | 2.863 | 0.023 | | | |
| 2.06 | 0.946 | 0.168 | 0.423 | 2.831 | 0.206 | | | | | 2.898 | 0.037 | | | |
| 2.08 | 0.915 | 0.174 | 0.711 | 2.931 | 0.526 | | | | | 2.908 | 0.071 | | | |

CURVE 26
 T = 293.

CURVE 25
 T = 293.

CURVE 24
 T = 293.

TABLE 11-24. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA (VITREOUS) (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 26 (CONT.) | | CURVE 27 (CONT.) | | CURVE 27 (CONT.) | | CURVE 28 T = 293. | | CURVE 29 (CONT.) | | CURVE 30 (CONT.) | |
|------------------|--------|------------------|--------|------------------|--------|----------------------|--------|------------------|--------|------------------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 2.512 | 0.416 | 0.196 | 0.522 | 2.580 | 0.453 | 0.1630 | 0.000 | 0.1609 | 0.553 | 0.1900 | 0.782 |
| 2.914 | 0.464 | 0.201 | 0.577 | 2.652 | 0.214 | 0.1614 | 0.015 | 0.1696 | 0.622 | CURVE 31 | |
| 2.916 | 0.537 | 0.205 | 0.632 | 2.718 | 0.057 | 0.1622 | 0.023 | 0.1702 | 0.656 | T = 293. | |
| 2.919 | 0.575 | 0.213 | 0.676 | 2.745 | 0.027 | 0.1630 | 0.034 | 0.1713 | 0.679 | | |
| 2.943 | 0.617 | 0.221 | 0.717 | 2.799 | 0.013 | 0.1635 | 0.044 | 0.1719 | 0.690 | | |
| 2.964 | 0.653 | 0.232 | 0.753 | 2.863 | 0.023 | 0.1643 | 0.071 | 0.1732 | 0.708 | | |
| 3.006 | 0.694 | 0.242 | 0.791 | 2.894 | 0.037 | 0.1648 | 0.103 | 0.1745 | 0.720 | | |
| 3.073 | 0.751 | 0.256 | 0.825 | 2.904 | 0.071 | 0.1678 | 0.103 | 0.1757 | 0.728 | | |
| 3.117 | 0.783 | 0.269 | 0.849 | 2.912 | 0.414 | 0.1686 | 0.246 | 0.1767 | 0.732 | | |
| 3.171 | 0.803 | 0.279 | 0.867 | 2.914 | 0.464 | 0.1695 | 0.331 | 0.1783 | 0.735 | | |
| 3.224 | 0.819 | 0.291 | 0.881 | 2.916 | 0.537 | 0.1696 | 0.399 | 0.1796 | 0.738 | | |
| 3.259 | 0.826 | 0.302 | 0.890 | 2.919 | 0.575 | 0.1704 | 0.469 | CURVE 30 | | | |
| 3.327 | 0.826 | 0.311 | 0.895 | 2.943 | 0.617 | 0.1711 | 0.511 | T = 293. | | | |
| 3.364 | 0.816 | 0.327 | 0.903 | 2.964 | 0.653 | 0.1717 | 0.546 | | | | |
| 3.450 | 0.686 | 0.342 | 0.907 | 3.006 | 0.694 | 0.1717 | 0.571 | | | | |
| 3.577 | 0.458 | 0.363 | 0.907 | 3.078 | 0.751 | 0.1727 | 0.596 | 0.1525 | 0.009 | | |
| 3.709 | 0.203 | 0.398 | 0.911 | 3.117 | 0.783 | 0.1737 | 0.618 | 0.1536 | 0.014 | | |
| 3.734 | 0.145 | 1.000 | 0.911 | 3.171 | 0.803 | 0.1748 | 0.637 | 0.1545 | 0.018 | | |
| 3.800 | 0.125 | 1.128 | 0.911 | 3.228 | 0.819 | 0.1759 | 0.653 | 0.1554 | 0.027 | | |
| 3.833 | 0.117 | 1.215 | 0.903 | 3.259 | 0.826 | 0.1775 | 0.665 | 0.1561 | 0.038 | | |
| 3.918 | 0.112 | 1.267 | 0.888 | 3.327 | 0.826 | 0.1789 | 0.677 | 0.1571 | 0.055 | | |
| 4.019 | 0.112 | 1.300 | 0.864 | 3.384 | 0.816 | 0.1808 | 0.689 | 0.1578 | 0.075 | | |
| 4.071 | 0.097 | 1.333 | 0.850 | 3.450 | 0.686 | 0.1824 | 0.700 | 0.1583 | 0.097 | | |
| 4.097 | 0.082 | 1.385 | 0.850 | 3.577 | 0.458 | 0.1843 | 0.715 | 0.1594 | 0.162 | | |
| 4.097 | 0.060 | 1.437 | 0.860 | 3.709 | 0.203 | 0.1860 | 0.730 | 0.1607 | 0.252 | | |
| 4.182 | 0.041 | 1.471 | 0.877 | 3.734 | 0.145 | 0.1877 | 0.746 | 0.1633 | 0.403 | | |
| 4.256 | 0.033 | 1.551 | 0.907 | 3.800 | 0.125 | 0.1900 | 0.767 | 0.1665 | 0.566 | | |
| 4.335 | 0.022 | 1.727 | 0.907 | 3.833 | 0.117 | CURVE 29 | | 0.1679 | 0.613 | | |
| 4.400 | 0.000 | 1.968 | 0.911 | 3.918 | 0.112 | T = 293. | | 0.1693 | 0.670 | | |
| | | 2.028 | 0.902 | 4.019 | 0.112 | | | 0.1702 | 0.692 | | |
| | | 2.134 | 0.633 | 4.071 | 0.097 | | | 0.1710 | 0.708 | | |
| | | 2.157 | 0.616 | 4.097 | 0.082 | | | 0.1719 | 0.720 | | |
| | | 2.184 | 0.609 | 4.097 | 0.060 | | | 0.1730 | 0.732 | | |
| | | 2.218 | 0.619 | 4.182 | 0.041 | | | 0.1747 | 0.742 | | |
| | | 2.242 | 0.653 | 4.256 | 0.033 | | | 0.1776 | 0.748 | | |
| | | 2.313 | 0.856 | 4.335 | 0.022 | | | 0.1818 | 0.750 | | |
| | | 2.336 | 0.867 | 4.400 | 0.000 | | | 0.1843 | 0.750 | | |
| | | 2.389 | 0.867 | | | | | 0.1854 | 0.762 | | |
| | | 2.439 | 0.857 | | | | | 0.1865 | 0.771 | | |
| | | 2.463 | 0.800 | | | | | 0.1885 | 0.813 | | |
| | | | | | | | | 0.1900 | 0.811 | | |
| | | | | | | | | CURVE 32 | | | |
| | | | | | | | | T = 298. | | | |
| | | | | | | | | 1.000 | 0.924 | | |
| | | | | | | | | 1.097 | 0.927 | | |
| | | | | | | | | 1.254 | 0.927 | | |
| | | | | | | | | 1.323 | 0.891 | | |
| | | | | | | | | 1.379 | 0.919 | | |

i. Normal Spectral Transmittance (Temperature Dependence)

No experimental data sets were found for the temperature dependence of the normal spectral transmittance of vitreous silica. However, a provisional curve was arrived at for the G.E. type 106 fused quartz kind of vitreous silica for $3.8 \mu\text{m}$ by using curves 1-5 from the previous section on the wavelength dependence of the normal spectral transmittance. The values are listed in Table 11-25 and shown in Figure 11-19. The provisional values are valid for a 2.8 mm thick specimen of polished G.E. type 106 fused quartz at 298, 373, 473, 573, and 673 K.

TABLE 11-25. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| T | T |
|-----------------|-------|
| GE TYPE 106 | |
| 2.0MM THICK | |
| $\lambda = 3.0$ | |
| 298. | 0.600 |
| 373. | 0.600 |
| 473. | 0.590 |
| 573. | 0.560 |
| 673. | 0.530 |

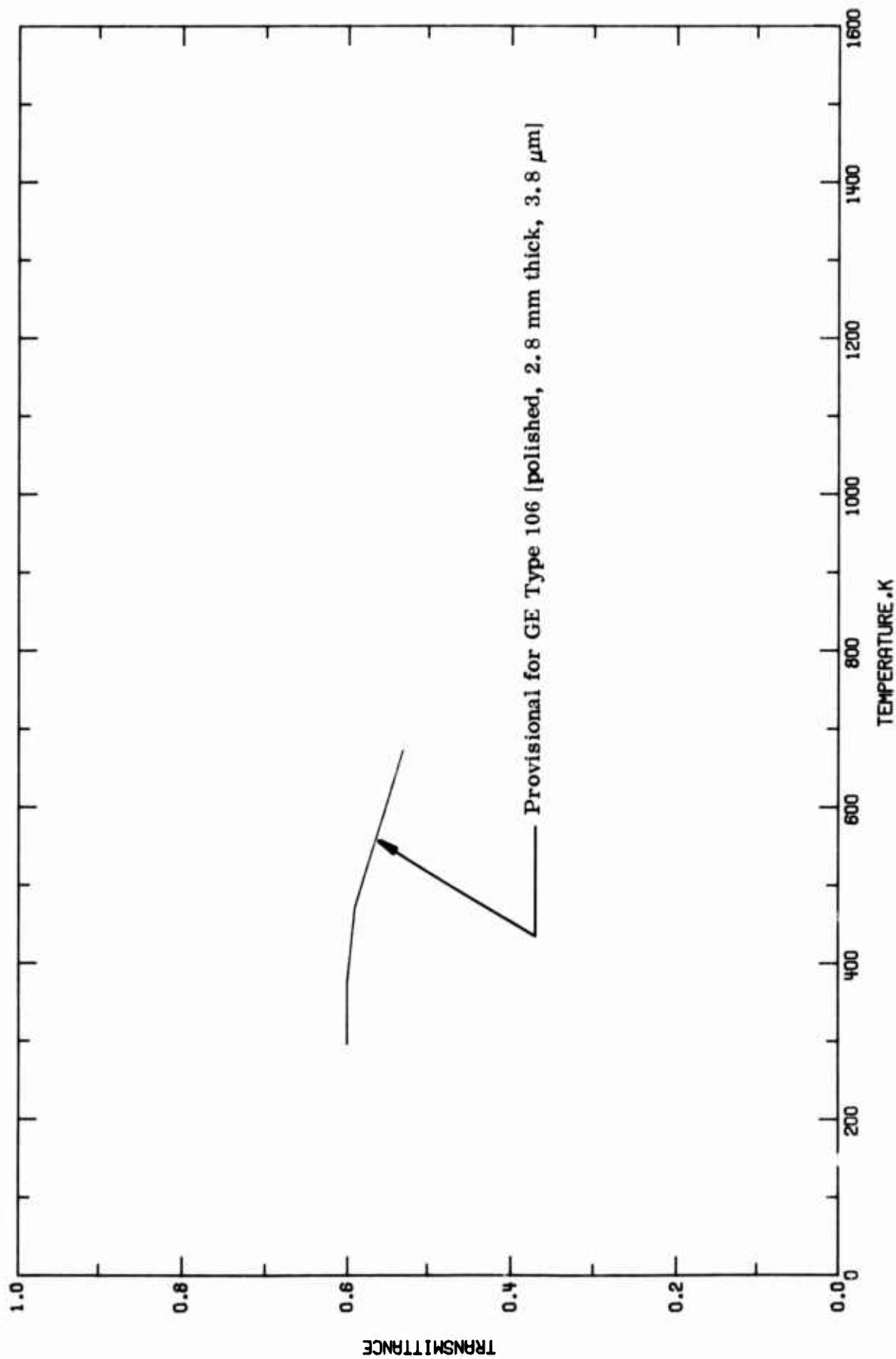


FIGURE 11-19. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICA(VITREOUS) (TEMPERATURE DEPENDENCE).

4.12. Silicon

Silicon crystallizes in a face centered cubic crystal of the A4 diamond type which is very stable from 293-1573 K. The lattice parameter of high purity silicon is 5.43089 Å at 296 K [E30683] and 5.445 Å at 1573 K [A00007]. Its density is 2.42 g cm⁻³ at 293 K. At 300 K, the intrinsic resistivity of very high purity silicon is about 2.5 x 10⁵ ohm-cm. The energy band gap is 1.1 eV. Silicon melts at 1687 K and boils at about 2753 K. Below 1273 K it is a brittle material, but it can be caused to undergo substantial plastic deformation at higher temperatures.

The thermal radiative properties of silicon depend on the method used in producing the crystal, especially in the 9 μm region where the presence of occluded oxygen causes a broad absorption band. In general, the bulk oxygen content is high for crystals grown by the Czochralski method and other methods where there is direct contact between the molten silicon and silica containers, and the 9 μm peak will be correspondingly higher for these crystals. Floating zone or pedestal methods have been developed in order to circumvent the problem of contamination of the crystal by the container. Oxygen is known to be present in Czochralski-grown crystals in concentrations in the range (0.5-2.0) x 10¹⁸ atoms cm⁻³. Crystals grown by float zone and pedestal methods contain essentially no oxygen. Pagot [E65870] and Hu and Patrick [E66704] have discussed various methods of determining the bulk oxygen content of a crystal and have examined the effect of bulk oxygen on the magnitude of the 9 μm absorption band in crystals grown by the different methods.

The thermal radiative properties of silicon may be altered by surface oxidation as well as by bulk oxygen occluded in crystal growth. Silicon oxidizes rapidly at room temperature to form a protective layer of silica about 10 Å thick. More complete oxidation begins at 920 K but is not rapid up to about 1500 K. The oxide layer is amorphous to about 1500 K, crystalline above 1500 K, and is somewhat volatile above 1873 K. Silicon semiconductor devices are generally protected with a silica layer by oxidizing at 1400-1600 K.

Silicon is used as the starting material for silicone resins, oils, and elastomers and as an alloying element to strengthen aluminum, magnesium, copper and other metals. It has a deoxidizing effect on steel and in relatively large concentrations it confers chemical inertness on ferrous alloys. High purity silicon is used in semiconduction devices such as rectifiers and transistors, and in solar batteries. High purity silicon has also been studied for use as an infrared dome material for small air to air missiles [T10703]. For this purpose it can be used in the 1-12 μm range up to about 520 K. Above

this temperature it becomes increasingly opaque due to absorption by free carriers thermally excited to the conduction band. Extremely small amounts of impurities greatly curtail its transmittance. For dome construction, the most feasible fabrication method appears to be a form of shell casting [T48097]. The transmittance of the castings was found to be similar to grown polycrystalline material. Vapor deposited domes have improved transmission characteristics in the 9 μm region due to a lesser bulk oxygen content, but their transmission in the 1-8 μm region was found to be considerably lower than that of cast domes due to scattering by voids in the silicon about 1 μm in diameter [T48097]. In applications as infrared optical components, silicon is normally coated with other materials in order to reduce reflection losses at desired wavelengths.

The electrical and thermal radiative properties of silicon are significantly changed by additions of small amounts of impurities or dopants. Elements of the third group of the periodic table (boron, aluminum, indium, gallium) can be added to pure or intrinsic material to produce p-type silicon which conducts current by migration of electron vacancies or holes. The introduction of Group V elements (arsenic, antimony, phosphorus) produces n-type silicon in which current is carried by migration of extra electrons. The resistivity of silicon is greatly reduced by addition of these impurities, to as low a value as 10^{-4} ohm-cm. Although very pure silicon with a room temperature resistivity of the order of 10^5 ohm-cm and which becomes an intrinsic conductor at as low a temperature as 313 K has been produced, the term "high resistivity silicon" in the following discussion has generally been applied to silicon with a room temperature resistivity of 5 ohm-cm or greater.

The absorption mechanisms responsible for the main thermal radiative characteristics of silicon can be classified into four different types [T48288]: i) intrinsic absorption associated with excitation of electrons from the valence band to the conduction band across the energy gap; ii) absorption associated with impurities or defects in the lattice; iii) absorption due to the presence of free carriers; and iv) absorption due to lattice vibrations. Intrinsic absorption accounts for the sharp increase of the emittance and sharp decrease of the transmittance of silicon at around 1 μm . At longer wavelengths, the radiation has insufficient energy to excite an electron across the energy gap, and the absorption and emittance are low with correspondingly high transmittance. In the 6-15 μm wavelength range, absorption bands associated with lattice vibrations are evident. At room temperature, absorption due to free carriers is not great for silicon of ordinary purity, but as the temperature is raised, the silicon becomes intrinsic as electrons are thermally excited to the conduction band. The free carrier absorption increases rapidly with temperature and finally becomes the dominant absorption mechanism.

It should be noted that the following sections concentrate on pure silicon with relatively low dopant levels. The experimental data for doped silicon samples shown in the following tables and figures by no means represent an exhaustive coverage of the available data for doped samples in the 1-15 μm range.

a. Normal Spectral Emittance (Wavelength Dependence)

Fifty-one experimental data sets for the wavelength dependence (1-14 μm) of the normal spectral emittance of silicon covering the temperature range 77-1075 K are shown in Table 12-3 and Figures 12-2 and 12-3. Of the 51 data sets, 30 sets are for specimens with relatively low dopant levels and high resistivities. Data for relatively pure specimens are shown in Figure 12-2 and for doped, low resistivity specimens in Figure 12-3.

Silicon is a partially transparent material to which the McMahon [T20468] relations (Eq. 2.6-10 to 2.6-12) apply. As the relations indicate, the normal spectral emittance of silicon depends on the thickness of the specimen, unless the specimen is thick enough or at high enough temperatures to be opaque. In this case, the normal spectral emittance is given by Eq. 2.6-1, where $\rho(\lambda, T)$ is the single surface reflectance given by Eq. 2.4-11 and Eq. 2.6-6. For high purity silicon in the 2-15 μm wavelength range, the index of absorption is small compared to the refractive index and can be neglected in Eq. 2.4-11. Both measurements of the refractive index and of the reflectance of opaque specimens indicate that the single surface reflectance of polished, high purity silicon at room temperature has a nearly constant value of 0.30 over the entire 2-15 μm wavelength range. The room temperature emittance of a polished, opaque specimen of relatively pure silicon can therefore be given as 0.70 in the 2-15 μm region. The uncertainty of this value should not be greater than $\pm 5\%$.

The normal spectral emittance of transparent specimens of relatively pure silicon has been extensively investigated by Stierwalt [T16961, T28823] (curves 25-38) Stierwalt and Potter [T32537] (curves 4-9) and Sato [T41640] (curves 39-45). Stierwalt, investigating primarily the emittance due to lattice vibrations, observed emission bands at 5.85, 7.0, 7.8, 9.0, 10.4, 11.3, 12.25, 12.8, and 13.6 μm . Both n-type and p-type silicon show the same emission bands. The 9 μm band is due to bulk oxygen impurities. Stierwalt found that the 9.0 and 11.3 μm bands shift to longer wavelengths as the temperature is increased, the shift being about 0.1 μm when the temperature was raised from 333 to 433 K. Sato and other investigators have observed similar lattice emission bands. Sato found, from measurements on a 15 ohm-cm, n-type specimen, that the lattice emission

increases with temperature from 340 K, reaches a maximum at 493 K, and then decreases with further increasing temperature.

The recommended values for 330 K shown in Table 12-1 and Figure 12-1 are based on Stierwalt's data (curve 25) for a 2.03 mm thick, n-type, 30-60 ohm-cm silicon single crystal. In the 1-3 μm region, the recommended values were generated in a manner consistent with transmittance and reflectance data and with the general trend of Sato's data for higher temperatures. Stierwalt's data were not followed closely in the 9 μm region; rather, an average peak height was chosen for the emission band due to occluded oxygen, because the height of the peak is known to vary greatly according to the method used to grow the crystal. Stierwalt also performed measurements (curves 4-9, 31-34) on two 1.68 mm thick, p-type samples of similar resistivity. In the 7-14 μm region, these samples show a lower emittance than the slightly thicker n-type sample. Thus, the 330 K recommended values may be considered to apply to a 2 mm thick, n-type silicon single crystal of relatively high purity and resistivity. They do not apply to highly doped specimens.

The uncertainties of the values recommended for 330 K vary according to the wavelength. Due to the rapid increase in emittance near the absorption edge (1-1.5 μm), the values in this region must be considered typical only; their uncertainty may be as great as 50%. In the 2-5 μm region, the emittance is very small, varying from about 0.01 to 0.03 for the n-type and p-type specimens with thicknesses of about 2 mm. In the 6-14 μm range, the uncertainty should not be greater than $\pm 15\%$, with the exception of the 9 μm emission peak, where experimental measurements for crystals grown by different methods may differ from the tabulated values by as much as 80-90%.

The recommended values for 1075 K shown in Table 12-1 and Figure 12-1 are based on Sato's data (curve 45) for a 1.77 mm thick, n-type, 15 ohm-cm single crystal. At this high temperature, silicon is opaque in the 2-15 μm range, and absorption due to free carriers dominates the lattice absorption. Sato's data shows that the normal spectral emittance is within $\pm 5\%$ of 0.710 over the entire 2-15 μm range. This value for the emittance, along with Eq. 2.6-1 for opaque materials, gives a single surface reflectance of 0.290 at 1075 K, which compares favorably with the room temperature value of 0.30. Because of the high temperature opacity of silicon, the 1075 recommended values are applicable to relatively pure, high resistivity, single crystal silicon of any thickness. The uncertainty of the recommended values should not exceed $\pm 8\%$.

No recommendations have been made for highly doped p-type or n-type specimens. The normal spectral emittance of silicon specimens which are sufficiently doped to be

opaque can be calculated by use of the free carrier absorption theory. Using this theory, Sato [T41640] performed calculations (curves 50, 51) at 543 and 893 K which show good agreement with experimental data (curves 46, 49) for an n-type specimen. Calculations performed by Liebert [T47262], showed agreement with experimental data to within 14%, for both n-type and p-type specimens for temperatures from 300 to 1075 K and wavelengths from 3.5 to 14.8 μm . The Hagen-Rubens theory is inadequate for doped silicon in the 1-15 μm region [T47262].

TABLE 12-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm : TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|---|---|---|---|--------------------------------------|------------------------------|-----------|------------|
| SINGLE CRYSTAL 2.0 MM THICK T = 330 | SINGLE CRYSTAL 2.0 MM THICK T = 330 (CONT.) | SINGLE CRYSTAL 2.0 MM THICK T = 330 | SINGLE CRYSTAL 2.0 MM THICK T = 330 (CONT.) | SINGLE CRYSTAL OPAQUE T = 1075 | SINGLE CRYSTAL ϵ | | |
| 1.00 | 0.665 | 8.20 | 0.104 | 1.00 | 0.664 | | |
| 1.10 | 0.575 | 8.30 | 0.114 | 1.50 | 0.697 | | |
| 1.20 | 0.2208† | 8.40 | 0.146 | 2.00 | 0.700 | | |
| 1.30 | 0.0248 | 8.50 | 0.1798† | 2.80 | 0.712 | | |
| 1.40 | 0.0178 | 8.60 | 0.2209 | 3.00 | 0.714 | | |
| 1.50 | 0.0148 | 8.70 | 0.2809 | 3.80 | 0.714 | | |
| 1.60 | 0.0138 | 8.80 | 0.3668 | 4.00 | 0.714 | | |
| 1.70 | 0.012A | 8.90 | 0.4358 | 4.50 | 0.715 | | |
| 1.80 | 0.011A | 9.00 | 0.4728 | 5.00 | 0.716 | | |
| 1.90 | 0.011A | 9.10 | 0.4709 | 6.00 | 0.716 | | |
| 2.00 | 0.010A | 9.20 | 0.4208 | 7.00 | 0.716 | | |
| 2.20 | 0.010A | 9.30 | 0.3209 | 9.00 | 0.716 | | |
| 2.40 | 0.010A | 9.40 | 0.1808 | 9.00 | 0.716 | | |
| 2.60 | 0.009A | 9.50 | 0.165 | 10.00 | 0.716 | | |
| 2.80 | 0.009A | 9.60 | 0.158 | 10.60 | 0.716 | | |
| 3.00 | 0.009A | 9.70 | 0.169 | 11.00 | 0.716 | | |
| 3.80 | 0.009A | 9.80 | 0.190 | 12.00 | 0.716 | | |
| 4.00 | 0.009A | 9.90 | 0.210 | 13.00 | 0.716 | | |
| 5.60 | 0.010A | 10.00 | 0.234 | 13.00 | 0.713 | | |
| 5.50 | 0.013A | 10.10 | 0.260 | 14.00 | 0.712 | | |
| 5.85 | 0.024 | 10.20 | 0.284 | 15.00 | 0.710 | | |
| 6.60 | 0.022 | 10.30 | 0.305 | | | | |
| 6.20 | 0.021 | 10.40 | 0.309 | | | | |
| 6.40 | 0.023 | 10.50 | 0.306 | | | | |
| 6.60 | 0.038 | 10.60 | 0.308 | | | | |
| 6.80 | 0.083 | 10.70 | 0.329 | | | | |
| 6.90 | 0.105 | 10.80 | 0.350 | | | | |
| 7.60 | 0.112 | 10.90 | 0.373 | | | | |
| 7.10 | 0.104 | 11.00 | 0.394 | | | | |
| 7.20 | 0.100 | 11.10 | 0.410 | | | | |
| 7.30 | 0.100 | 11.20 | 0.417 | | | | |
| 7.40 | 0.104 | 11.30 | 0.417 | | | | |
| 7.50 | 0.115 | 11.40 | 0.409 | | | | |
| 7.60 | 0.125 | 11.50 | 0.392 | | | | |
| 7.70 | 0.130 | 11.60 | 0.375 | | | | |
| 7.80 | 0.122 | 11.70 | 0.358 | | | | |
| 7.90 | 0.113 | 11.80 | 0.350 | | | | |
| 8.60 | 0.103 | 11.90 | 0.350 | | | | |
| 8.10 | 0.100 | 12.00 | 0.368 | | | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL AND BY A "B" IS TYPICAL.

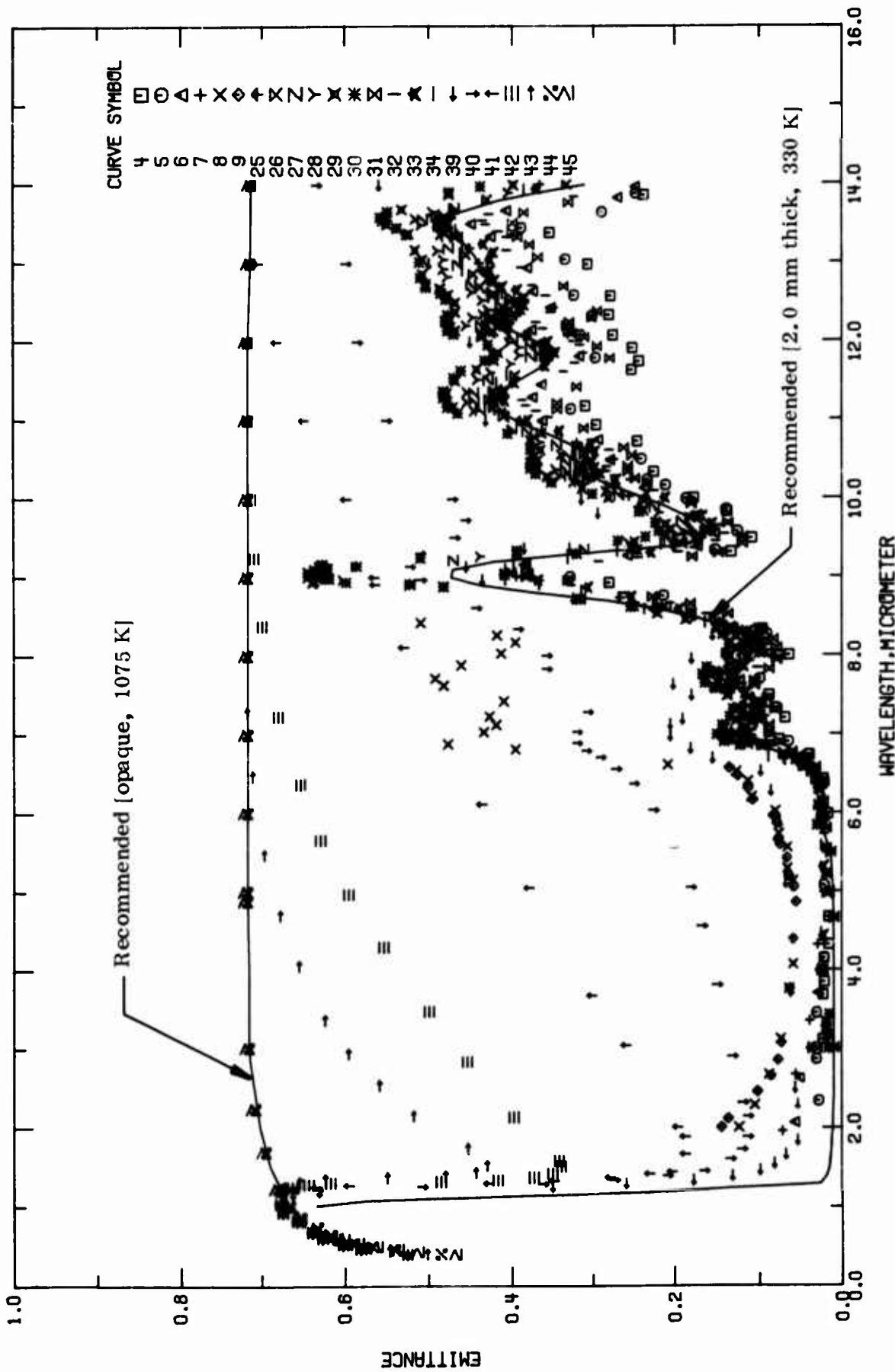


FIGURE 12-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)

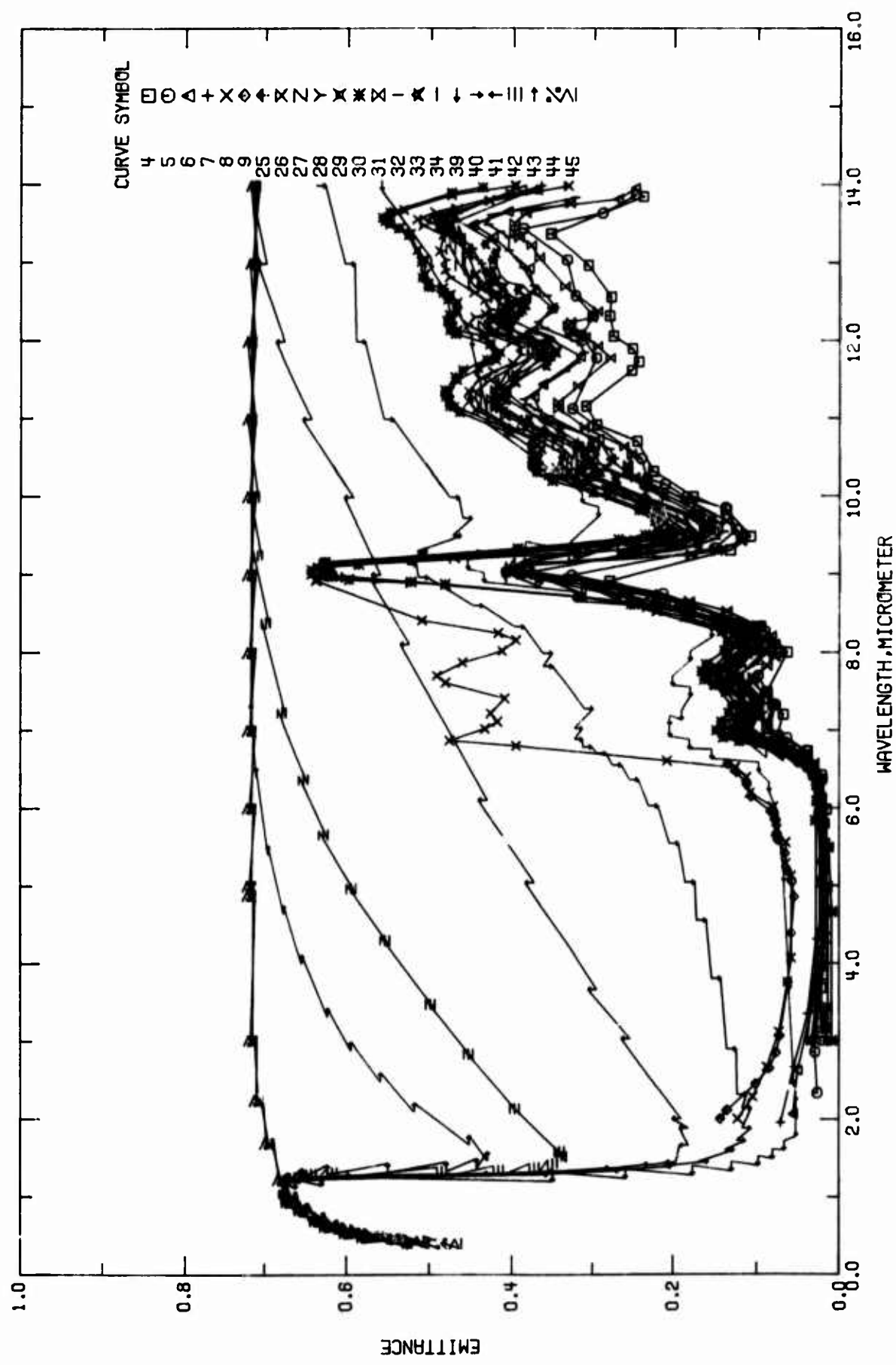


FIGURE 12-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE).

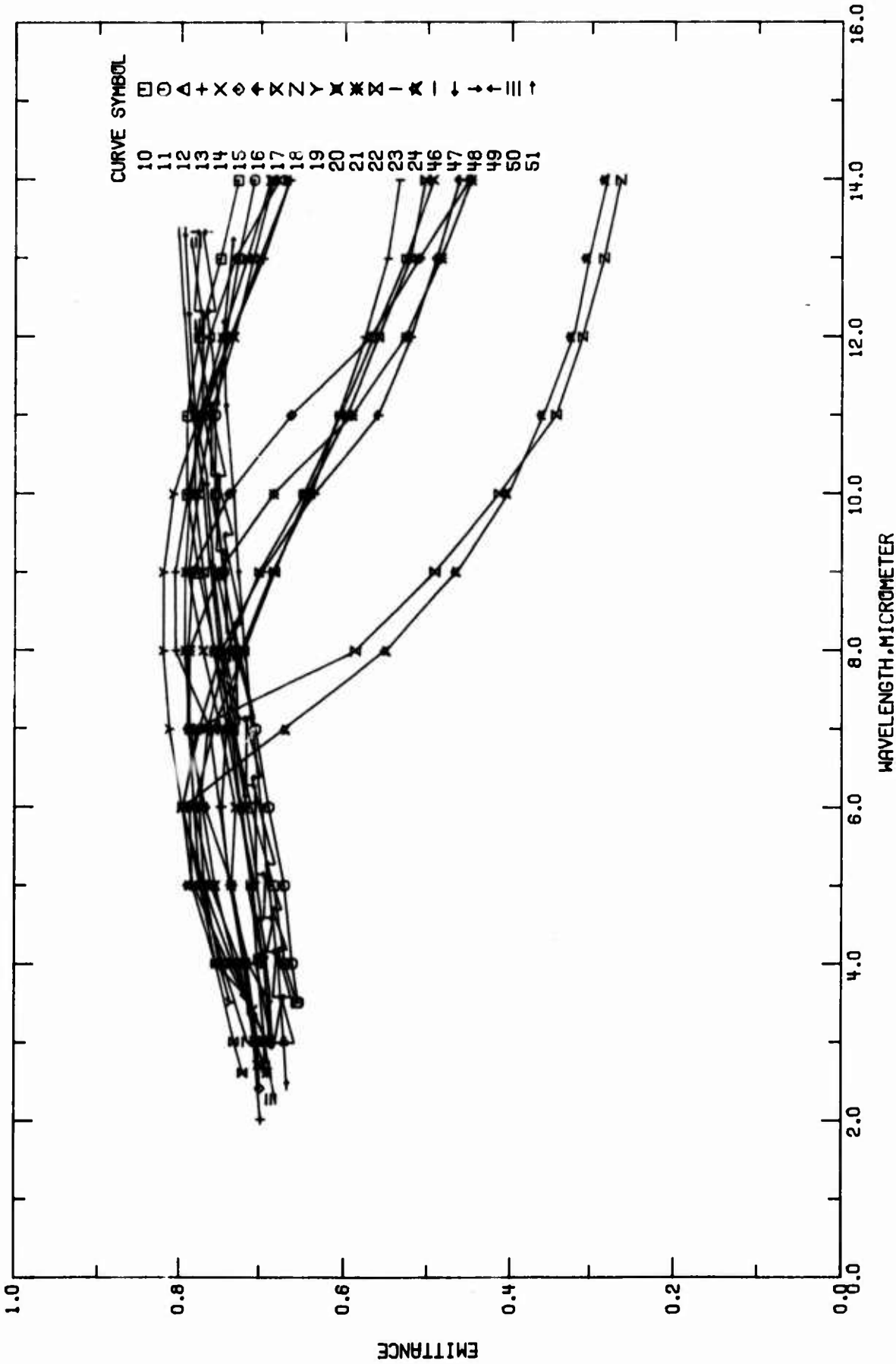


FIGURE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF LOW-RESISTIVITY, DOPED SILICON (WAVELENGTH DEPENDENCE).

TABLE 12-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T32552 | Stierwalt, D.L. | 1966 | 16-42 | 77 | | Single crystal; n-type; 2 mm thick; 10^{-4} torr pressure; smoothed values extracted from figure. |
| 2 T32552 | Stierwalt, D.L. | 1966 | 16-42 | 203 | | Similar to the above specimen. |
| 3 T32552 | Stierwalt, D.L. | 1966 | 16-42 | 373 | | Similar to the above specimen. |
| 4 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2-24 | 323 | | Single crystal; p-type; thickness 1.68 mm; cut to size with ultrasonic tool; optical surfaces prepared using standard lapping and polishing techniques; not etched; resistivity of 30 ohm-cm; data presented in figure. |
| 5 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2-24 | 373 | | The above specimen measured at 373 K. |
| 6 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2-24 | 423 | | The above specimen measured at 423 K. |
| 7 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2-24 | 473 | | The above specimen measured at 473 K. |
| 8 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2-9 | 473 | | Single crystal; p-type; thickness 13.4 mm; cut to size with ultrasonic tool; optical surfaces prepared using standard lapping and polishing techniques; not etched; resistivity of 2000 ohm-cm; data presented in figure. |
| 9 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2-7 | 473 | | The above specimen measured with increased gain. |
| 10 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 882 | | n-type single crystal; doped with arsenic; carrier concentration 2.2×10^{19} electrons cm^{-3} (accurate to $\pm 1\%$); opaque disk 23 mm diameter and 1.6 mm thick cut from doped ingots made by Allegheny Electron Chemicals Co; optically polished and etched; width of ridges produced by polishing about 0.5 μm ; measured in air; hohraum and Perkin Elmer Model 13 spectrophotometer used; data presented in figure; oxidation effects considered to be negligible; resistivity about 0.00644 ohm-cm at 882 K; reported error $\pm 4-7\%$. |
| 11 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 1074 | | The above specimen measured at 1074 K; resistivity about 0.00793 ohm cm at 1074 K. |
| 12 T47262 | Liebert, C.H. | 1967 | 2.5-35 | 300 | | The above specimen; normal spectral emissivity calculated from measurements of near normal (6°) specular reflectivity using hohraum and Perkin Elmer Model 521 spectrophotometer, with aluminum mirror as standard; data reported in figure; resistivity about 0.00329 at 300 K. |
| 13 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 882 | | n-type single crystal doped with arsenic; carrier concentration 3.7×10^{19} electrons cm^{-3} (accurate to $\pm 1\%$); opaque disk 23 mm in diameter and 1.6 mm thick cut from ingots made by Allegheny Electron Chemicals Co; optically polished and etched; width of ridges produced by polishing 0.5 μm ; measured in air using hohraum and Perkin Elmer Model 13 spectrophotometer; oxidation effects considered to be negligible; data presented in figure; resistivity about 0.00429 ohm cm at 882 K; reported error $\pm 4-7\%$. |
| 14 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 1074 | | The above specimen measured at 1074 K; resistivity about 0.00524 ohm-cm at 1074 K. |
| 15 T47262 | Liebert, C.H. | 1967 | 2.5-35 | 300 | | The above specimen; normal spectral emissivity calculated from measurements of near normal (6°) specular reflectivity using hohraum and Perkin Elmer Model 521 spectrophotometer with aluminum mirror as standard; data reported in figure; resistivity about 0.00206 ohm-cm at 300 K. |

TABLE 12-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 16 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 882 | | n-type single crystal doped with arsenic; carrier concentration 8.5×10^{19} electrons cm^{-3} (accurate to $\pm 1\%$); opaque disk 23 mm diameter and 1.6 mm thick cut from ingot made by Allegheny Electron Chemicals Co; optically polished and etched; width of ridges produced by polishing about $0.5 \mu\text{m}$; measured in air using hoblaum and Perkin Elmer Model 13 spectrophotometer; oxidation effects considered to be negligible; data presented in figure; electrical resistivity about 0.00238 ohm-cm at 882 K; reported error $\pm 4-7\%$. |
| 17 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 1074 | | The above specimen measured at 1074 K; resistivity about 0.00292 ohm-cm at 1074 K. |
| 18 T47262 | Liebert, C.H. | 1967 | 2.5-35 | 300 | | The above specimen; normal spectral emissivity calculated from measurements of near normal (6°) specular reflectivity using hoblaum and Perkin Elmer Model 521 spectrophotometer with aluminum mirror as standard; data reported in figure; electrical resistivity about 0.00115 ohm-cm at 300 K. |
| 19 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 882 | | p-type single crystal doped with boron; carrier concentration 6.2×10^{13} holes- cm^{-3} (accurate to $\pm 1\%$); opaque disk 23 mm in diameter and 1.6 mm thick cut from ingot made by Allegheny Electron Chemicals Co; optically polished and etched; width of ridges produced by polishing about $0.5 \mu\text{m}$; measured in air using hoblaum and Perkin Elmer Model 13 spectrophotometer; oxidation effects considered to be negligible; data presented in figure; electrical resistivity about 0.00479 ohm-cm at 882 K; reported error $\pm 4-7\%$. |
| 20 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 1074 | | The above specimen measured at 1074 K; electrical resistivity about 0.00588 ohm-cm at 1074 K. |
| 21 T47262 | Liebert, C.H. | 1967 | 2.5-35 | 300 | | The above specimen; normal spectral emissivity calculated from measurements of near normal (6°) specular reflectivity using hoblaum and Perkin Elmer Model 521 spectrophotometer with aluminum mirror as standard; data presented in figure; electrical resistivity about 0.00218 ohm-cm at 300 K. |
| 22 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 882 | | p-type single crystal doped with boron; carrier concentration 1.4×10^{19} holes- cm^{-3} (accurate to $\pm 1\%$); opaque disk 23 mm in diameter and 1.6 mm thick cut from ingot made by Allegheny Electron Chemicals Co; optically polished and etched; width of ridges produced by polishing about $0.5 \mu\text{m}$; measured in air using hoblaum and Perkin Elmer Model 13 spectrophotometer; oxidation effects considered to be negligible; data presented in figure; electrical resistivity about 0.00281 ohm-cm at 882 K; reported error $\pm 4-7\%$. |
| 23 T47262 | Liebert, C.H. | 1967 | 3.5-14.8 | 1074 | | The above specimen measured at 1074 K; electrical resistivity about 0.00348 ohm-cm at 1074 K. |
| 24 T47262 | Liebert, C.H. | 1967 | 2.5-35 | 300 | | The above specimen; normal spectral emissivity calculated from measurements of near normal (6°) specular reflectivity using hoblaum and Perkin Elmer Model 521 spectrophotometer with aluminum mirror as standard; data presented in figure; electrical resistivity about 0.00124 ohm-cm at 300 K. |
| 25 T16961 | Stierwalt, D.L. | 1961 | 3-15 | 353 | | n-type, single crystal; 2.03 mm thick; ground and polished on top and bottom surfaces; measured in vacuum using modified Beckman IR-3 spectrophotometer; electrical resistivity 30-60 ohm cm; data presented in figure. |
| 26 T16961 | Stierwalt, D.L. | 1961 | 3-15 | 353 | | The above specimen measured at 353 K. |
| 27 T16961 | Stierwalt, D.L. | 1961 | 3-15 | 373 | | The above specimen measured at 373 K. |
| 28 T16961 | Stierwalt, D.L. | 1961 | 3-15 | 393 | | The above specimen measured at 393 K. |

TABLE 12-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 29 T16961 | Stierwalt, D. L. | 1961 | 3-15 | 413 | | The above specimen measured at 413 K. |
| 30 T16961 | Stierwalt, D. L. | 1961 | 3-15 | 433 | | The above specimen measured at 433 K. |
| 31 T16961 | Stierwalt, D. L. | 1961 | 3-15 | 313 | | p-type, single crystal; 1.68 mm thick; ground and polished on top and bottom surfaces; measured in vacuum using modified Beckman IR-3 spectrophotometer; data presented in figure. |
| 32 T16961 | Stierwalt, D. L. | 1961 | 3-15 | 353 | | The above specimen measured at 353 K. |
| 33 T16961 | Stierwalt, D. L. | 1961 | 3-15 | 393 | | The above specimen measured at 393 K. |
| 34 T16961 | Stierwalt, D. L. | 1961 | 3-15 | 433 | | The above specimen measured at 433 K. |
| 35 T28623 | Stierwalt, D. | 1960 | 3-15 | 313 | | 1.65 mm thick sample. |
| 36 T28823 | Stierwalt, D. | 1960 | 3-15 | 353 | | The above specimen. |
| 37 T28823 | Stierwalt, D. | 1960 | 3-15 | 393 | | The above specimen. |
| 38 T28823 | Stierwalt, D. | 1960 | 3-15 | 433 | | The above specimen. |
| 39 T41640 | Sato, T. | 1967 | 0.4-15 | 543 | | n-type, phosphorus doped, single crystal disk with 23 mm diameter and 1.77 mm thickness; resistivity 15 ohm-cm; ground and polished plane parallel using metallographic and then optical techniques; two measurement methods used; direct method compared specimen to V-shaped graphite cavity using Japan Spectroscopic IR-S spectrophotometer with NaCl prism in 2.5-15 μm range and a double pass spectrophotometer with LiF prism below 2.5 μm ; indirect method obtained emissivity from measurements of reflectance and transmittance; measured under 10 ⁻⁴ mm Hg to preclude oxidation; due to difficulties in reading scale of figure, values above 10 μm are uncertain. |
| 40 T41640 | Sato, T. | 1967 | 0.4-15 | 623 | | The above specimen measured at 623 K. |
| 41 T41640 | Sato, T. | 1967 | 0.4-15 | 693 | | The above specimen measured at 693 K. |
| 42 T41640 | Sato, T. | 1967 | 0.4-15 | 743 | | The above specimen measured at 743 K. |
| 43 T41640 | Sato, T. | 1967 | 0.4-15 | 793 | | The above specimen measured at 793 K. |
| 44 T41640 | Sato, T. | 1967 | 0.4-15 | 873 | | The above specimen measured at 873 K. |
| 45 T41640 | Sato, T. | 1967 | 0.4-15 | 1073 | | The above specimen measured at 1073 K. |
| 46 T41640 | Sato, T. | 1967 | 2-15 | 543 | | n-type, phosphorus doped, single crystal disk with 23 mm diameter and 0.2 mm thickness; resistivity 0.007 ohm-cm at 300 K; polished and measured in manner similar to the above specimen; practically opaque even at low temperatures; due to difficulties in reading scale of figure, values above 10 μm are uncertain. |
| 47 T41640 | Sato, T. | 1967 | 2-15 | 693 | | The above specimen measured at 693 K. |
| 48 T41640 | Sato, T. | 1967 | 2-15 | 793 | | The above specimen measured at 793 K. |
| 49 T41640 | Sato, T. | 1967 | 2-15 | 893 | | The above specimen measured at 893 K. |
| 50 T41640 | Sato, T. | 1967 | 2-15 | 543 | | Calculation of the emittance of the above specimen at 543 K. |
| 51 T41640 | Sato, T. | 1967 | 2-15 | 893 | | Calculation of the emittance of the above specimen at 893 K. |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| CURVE 1 T = 77. | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 (CONT.) | | CURVE 5 (CONT.) | | CURVE 6 T = 423. | |
|--------------------|------------|---------------------|------------|---------------------|------------|---------------------|------------|-----------------|------------|---------------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 16.00 | 0.333 | 17.49 | 0.205 | 33.00 | 0.097 | 12.99 | 0.306 | 9.34 | 0.151 | 2.06 | 0.057 |
| 16.32 | 0.466 | 17.80 | 0.291 | 32.00 | 0.091 | 13.39 | 0.353 | 9.58 | 0.125 | 2.62 | 0.051 |
| 16.50 | 0.475 | 18.33 | 0.265 | 34.00 | 0.075 | 13.67 | 1.235 | 9.86 | 0.130 | 3.70 | 0.029 |
| 16.63 | 0.456 | 19.03 | 0.217 | 35.00 | 0.082 | 14.10 | 0.204 | 10.00 | 0.105 | 6.30 | 0.053 |
| 16.79 | 0.344 | 19.48 | 0.227 | 39.00 | 0.083 | 14.34 | 0.166 | 10.17 | 0.210 | 6.70 | 0.118 |
| 16.98 | 0.253 | 20.07 | 0.205 | 40.00 | 0.079 | 15.27 | 0.196 | 10.24 | 0.232 | 6.93 | 0.098 |
| 17.23 | 0.220 | 20.77 | 0.159 | 41.48 | 0.079 | 15.56 | 0.220 | 10.50 | 0.239 | 7.17 | 0.098 |
| 17.52 | 0.230 | 21.44 | 0.120 | | | 15.82 | 0.304 | 11.14 | 0.327 | 7.41 | 0.123 |
| 17.87 | 0.236 | 22.00 | 0.100 | CURVE 4 T = 323. | | 16.29 | 0.591 | 11.79 | 0.296 | 7.68 | 0.091 |
| 18.20 | 0.224 | 24.00 | 0.079 | | | 16.49 | 0.564 | 12.08 | 0.315 | 8.02 | 0.110 |
| 18.92 | 0.176 | 26.00 | 0.073 | | | 16.92 | 0.391 | 12.33 | 0.300 | 9.04 | 0.257 |
| 19.39 | 0.187 | 28.00 | 0.066 | 3.12 | 0.022 | 17.16 | 0.366 | 12.59 | 0.323 | 9.27 | 0.172 |
| 19.87 | 0.166 | 30.00 | 0.063 | 3.69 | 0.022 | 17.36 | 0.349 | 13.05 | 0.334 | 9.55 | 0.152 |
| 20.44 | 0.122 | 32.00 | 0.057 | 3.85 | 0.020 | 17.65 | 0.354 | 13.45 | 0.367 | 9.78 | 0.236 |
| 20.86 | 0.101 | 34.00 | 0.051 | 4.15 | 0.021 | 18.57 | 0.306 | 13.65 | 0.288 | 10.13 | 0.276 |
| 21.33 | 0.086 | 36.00 | 0.048 | 4.33 | 0.015 | 19.01 | 0.291 | 13.89 | 0.246 | 10.49 | 0.293 |
| 21.77 | 0.072 | 38.00 | 0.046 | 4.68 | 0.015 | 19.35 | 0.296 | 14.22 | 0.190 | 10.99 | 0.374 |
| 22.00 | 0.065 | 40.00 | 0.041 | 5.99 | 0.016 | 19.52 | 0.296 | 14.48 | 0.200 | 11.45 | 0.363 |
| 24.00 | 0.045 | 41.91 | 0.041 | 6.43 | 0.022 | 20.00 | 0.259 | 14.74 | 0.216 | 11.81 | 0.317 |
| 26.00 | 0.039 | | | 7.74 | 0.039 | 21.72 | 0.170 | 15.13 | 0.231 | 12.15 | 0.375 |
| 28.00 | 0.032 | CURVE 3 T = 373. | | 8.93 | 0.076 | 22.70 | 0.137 | 15.45 | 0.251 | 12.43 | 0.352 |
| 30.00 | 0.027 | 16.00 | 0.362 | 7.21 | 0.069 | CURVE 5 T = 373. | | 15.63 | 0.309 | 12.64 | 0.373 |
| 32.00 | 0.027 | 16.37 | 0.616 | 7.50 | 0.088 | 16.18 | 0.637 | 16.32 | 0.652 | 12.94 | 0.380 |
| 34.00 | 0.025 | 16.63 | 0.587 | 8.01 | 0.064 | 16.32 | 0.652 | 16.60 | 0.555 | 13.34 | 0.424 |
| 36.00 | 0.026 | 17.25 | 0.409 | 8.93 | 0.075 | 2.33 | 0.027 | 16.92 | 0.424 | 13.50 | 0.406 |
| 38.00 | 0.026 | 17.48 | 0.399 | 9.32 | 0.132 | 2.86 | 0.030 | 17.37 | 0.381 | 13.67 | 0.269 |
| 40.00 | 0.026 | 17.48 | 0.399 | 9.50 | 0.109 | 3.45 | 0.021 | 17.63 | 0.396 | 13.83 | 0.247 |
| 41.66 | 0.026 | 18.33 | 0.399 | 9.84 | 0.137 | 4.15 | 0.021 | 18.15 | 0.373 | 14.27 | 0.233 |
| | | 18.27 | 0.389 | 10.01 | 0.176 | 5.07 | 0.021 | 18.56 | 0.339 | 14.46 | 0.245 |
| | | 18.65 | 0.369 | 10.34 | 0.224 | 6.37 | 0.041 | 19.09 | 0.326 | 14.69 | 0.268 |
| | | 18.93 | 0.336 | 10.73 | 0.244 | 6.74 | 0.041 | 19.41 | 0.326 | 14.99 | 0.294 |
| | | 19.23 | 0.324 | 11.34 | 0.295 | 6.90 | 0.065 | 19.61 | 0.343 | 15.52 | 0.337 |
| | | 19.92 | 0.317 | 11.18 | 0.309 | 6.96 | 0.065 | 20.14 | 0.291 | 15.75 | 0.377 |
| | | 20.67 | 0.268 | 11.64 | 0.251 | 7.33 | 0.079 | 20.61 | 0.264 | | |
| | | 21.40 | 0.230 | 11.75 | 0.242 | 7.70 | 0.099 | 21.60 | 0.200 | | |
| | | 22.00 | 0.207 | 11.92 | 0.250 | 7.99 | 0.076 | 22.61 | 0.152 | | |
| | | 24.00 | 0.160 | 12.09 | 0.274 | 8.27 | 0.091 | 23.21 | 0.136 | | |
| | | 26.00 | 0.125 | 12.34 | 0.279 | 8.76 | 0.213 | 24.00 | 0.125 | | |
| | | 28.00 | 0.096 | 12.58 | 0.277 | 9.00 | 0.328 | | | | |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|------------------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| CURVE 15 (CONT.) | | | | | | | | | | | |
| 16.0 | 0.368 | 11.0 | 0.605 | 5.0 | 0.796 | 11.0 | 0.591 | 5.0 | 0.736 | 3.00 | 0.009 |
| 18.0 | 0.329 | 12.0 | 0.565 | 7.0 | 0.812 | 12.0 | 0.527 | 6.0 | 0.746 | 4.66 | 0.009 |
| 20.0 | 0.304 | 13.0 | 0.526 | 9.0 | 0.820 | 13.0 | 0.484 | 7.0 | 0.741 | 5.49 | 0.013 |
| 22.0 | 0.290 | 14.0 | 0.493 | 9.0 | 0.820 | 14.0 | 0.449 | 8.0 | 0.722 | 5.86 | 0.024 |
| 24.0 | 0.278 | 14.7 | 0.493 | 10.0 | 0.808 | 15.0 | 0.414 | 9.0 | 0.684 | | |
| 26.0 | 0.269 | | | 11.0 | 0.776 | 16.0 | 0.393 | 10.0 | 0.639 | 6.16 | 0.021 |
| 28.0 | 0.260 | CURVE 18 | | 12.0 | 0.737 | 16.0 | 0.356 | 11.0 | 0.607 | 6.39 | 0.023 |
| 30.0 | 0.254 | T = 300. | | 13.0 | 0.700 | 20.0 | 0.324 | 12.0 | 0.575 | 6.54 | 0.031 |
| 32.0 | 0.244 | | | 14.0 | 0.664 | 22.0 | 0.300 | 13.0 | 0.548 | 6.62 | 0.038 |
| 34.0 | 0.238 | 3.0 | 0.713 | 15.0 | 0.623 | 24.0 | 0.278 | 14.0 | 0.534 | 6.70 | 0.056 |
| 34.0 | 0.238 | 4.0 | 0.744 | | | 26.0 | 0.264 | 15.0 | 0.517 | 6.84 | 0.088 |
| | | 5.0 | 0.773 | CURVE 20 | | 28.0 | 0.249 | | | 6.92 | 0.105 |
| | | 6.0 | 0.795 | T = 1074. | | 30.0 | 0.238 | | | 6.98 | 0.112 |
| | | 7.0 | 0.778 | | | 32.0 | 0.229 | CURVE 24 | | 7.15 | 0.103 |
| | | 8.0 | 0.596 | | | 34.0 | 0.225 | T = 300. | | 7.25 | 0.100 |
| | | 9.0 | 0.491 | 3.0 | 0.690 | 35.0 | 0.225 | | | 7.33 | 0.100 |
| | 0.716 | 10.0 | 0.415 | 4.0 | 0.725 | | | | | 7.44 | 0.106 |
| 5.0 | 0.783 | 11.0 | 0.344 | 5.0 | 0.754 | | | | | 7.55 | 0.117 |
| 6.0 | 0.795 | 12.0 | 0.311 | 6.0 | 0.770 | | | | | 7.64 | 0.126 |
| 7.0 | 0.775 | 13.0 | 0.284 | 7.0 | 0.786 | CURVE 22 | | | | 7.72 | 0.130 |
| 8.0 | 0.747 | 14.0 | 0.264 | 8.0 | 0.793 | T = 802. | | | | 7.85 | 0.121 |
| 9.0 | 0.697 | 14.0 | 0.264 | 9.0 | 0.793 | 2.6 | 0.719 | 8.0 | 0.550 | 8.05 | 0.100 |
| 10.0 | 0.635 | 15.0 | 0.253 | 10.0 | 0.797 | 3.0 | 0.730 | 9.0 | 0.467 | 8.17 | 0.100 |
| 11.0 | 0.559 | 16.0 | 0.241 | 11.0 | 0.774 | 4.0 | 0.753 | 10.0 | 0.406 | 8.29 | 0.114 |
| 12.0 | 0.520 | 18.0 | 0.225 | 12.0 | 0.747 | 5.0 | 0.773 | 11.0 | 0.363 | 8.41 | 0.146 |
| 13.0 | 0.489 | 20.0 | 0.214 | 13.0 | 0.716 | 6.0 | 0.781 | 12.0 | 0.327 | 8.53 | 0.179 |
| 14.0 | 0.463 | 22.0 | 0.203 | 14.0 | 0.687 | 7.0 | 0.757 | 13.0 | 0.307 | 8.61 | 0.220 |
| 14.7 | 0.447 | 24.0 | 0.199 | 15.0 | 0.649 | 8.0 | 0.719 | 14.0 | 0.285 | 8.72 | 0.315 |
| | | 26.0 | 0.195 | | | 9.0 | 0.682 | 15.0 | 0.272 | 8.91 | 0.522 |
| | | 28.0 | 0.195 | CURVE 21 | | 10.0 | 0.643 | 16.0 | 0.258 | 8.98 | 0.617 |
| | | 30.0 | 0.194 | T = 300. | | 11.0 | 0.597 | 18.0 | 0.241 | 9.05 | 0.626 |
| | | 32.0 | 0.194 | | | 12.0 | 0.559 | 20.0 | 0.219 | 9.11 | 0.619 |
| | | 34.0 | 0.194 | | | 13.0 | 0.521 | 22.0 | 0.208 | 9.14 | 0.585 |
| | | 35.0 | 0.194 | | | 14.0 | 0.503 | 24.0 | 0.192 | 9.29 | 0.320 |
| | 0.707 | | | 2.6 | 0.689 | 15.0 | 0.492 | 26.0 | 0.179 | 9.34 | 0.245 |
| 4.0 | 0.732 | 3.0 | 0.703 | 3.0 | 0.703 | | | 28.0 | 0.168 | 9.38 | 0.199 |
| 5.0 | 0.758 | 4.0 | 0.723 | 4.0 | 0.723 | CURVE 23 | | 30.0 | 0.157 | 9.42 | 0.185 |
| 6.0 | 0.774 | 5.0 | 0.755 | 5.0 | 0.755 | T = 1074. | | 32.0 | 0.150 | 9.49 | 0.167 |
| 7.0 | 0.764 | 7.0 | 0.781 | 7.0 | 0.781 | | | 34.0 | 0.147 | 9.57 | 0.156 |
| 8.0 | 0.740 | 8.0 | 0.787 | 8.0 | 0.787 | | | | | 9.77 | 0.177 |
| 9.0 | 0.700 | 3.5 | 0.735 | 9.0 | 0.751 | | | | | | |
| 10.0 | 0.647 | 4.0 | 0.748 | 10.0 | 0.751 | | | | | | |
| | | 5.0 | 0.768 | | | | | | | | |
| | | | | | | | | | | | |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIOUS PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T , K; EMITTANCE, ϵ)

| CURVE 25 (CONT.) | | CURVE 26 (CONT.) | | CURVE 27 (CONT.) | | CURVE 28 (CONT.) | |
|------------------|------------|------------------|------------|------------------|------------|------------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 10.00 | 0.234 | 6.53 | 0.045 | 11.05 | 0.024 | 11.13 | 0.437 |
| 10.16 | 0.272 | 6.75 | 0.071 | 11.16 | 0.034 | 11.24 | 0.444 |
| 10.28 | 0.300 | 6.86 | 0.097 | 11.26 | 0.045 | 11.35 | 0.445 |
| 10.31 | 0.606 | 6.91 | 0.113 | 11.37 | 0.071 | 11.51 | 0.427 |
| 10.37 | 0.310 | 6.98 | 0.117 | 11.7 | 0.097 | 11.61 | 0.376 |
| 10.49 | 0.305 | 7.14 | 0.108 | 11.81 | 0.119 | 11.93 | 0.376 |
| 10.59 | 0.305 | 7.34 | 0.103 | 11.99 | 0.127 | 12.03 | 0.398 |
| 10.64 | 0.313 | 7.34 | 0.103 | 11.97 | 0.118 | 12.11 | 0.425 |
| 10.99 | 0.383 | 7.46 | 0.113 | 12.13 | 0.111 | 12.21 | 0.436 |
| 11.09 | 0.407 | 7.59 | 0.127 | 12.21 | 0.111 | 12.34 | 0.425 |
| 11.26 | 0.419 | 7.66 | 0.132 | 12.23 | 0.135 | 12.38 | 0.412 |
| 11.39 | 0.411 | 7.79 | 0.132 | 12.32 | 0.142 | 12.46 | 0.412 |
| 11.76 | 0.354 | 7.88 | 0.126 | 12.41 | 0.142 | 12.57 | 0.421 |
| 11.86 | 0.349 | 7.98 | 0.112 | 12.51 | 0.132 | 12.73 | 0.448 |
| 11.97 | 0.359 | 8.11 | 0.103 | 12.61 | 0.117 | 12.98 | 0.464 |
| 12.07 | 0.380 | 8.22 | 0.112 | 12.70 | 0.114 | 13.19 | 0.475 |
| 12.16 | 0.405 | 8.31 | 0.124 | 12.85 | 0.121 | 13.35 | 0.477 |
| 12.21 | 0.410 | 8.41 | 0.146 | 13.11 | 0.144 | 13.48 | 0.487 |
| 12.25 | 0.405 | 8.53 | 0.179 | 13.33 | 0.180 | 13.56 | 0.506 |
| 12.33 | 0.393 | 8.61 | 0.220 | 13.38 | 0.231 | 13.70 | 0.468 |
| 12.42 | 0.388 | 8.72 | 0.315 | 13.48 | 0.315 | 14.01 | 0.343 |
| 12.50 | 0.391 | 8.91 | 0.522 | 13.50 | 0.522 | 14.19 | 0.246 |
| 12.77 | 0.425 | 8.98 | 0.617 | 13.59 | 0.620 | 14.28 | 0.219 |
| 12.89 | 0.432 | 9.05 | 0.628 | 13.61 | 0.634 | 14.39 | 0.214 |
| 13.19 | 0.449 | 9.11 | 0.619 | 14.00 | 0.626 | 14.48 | 0.218 |
| 13.36 | 0.464 | 9.14 | 0.585 | 14.18 | 0.470 | 15.00 | 0.259 |
| 13.47 | 0.479 | 9.29 | 0.320 | 14.33 | 0.311 | CURVE 28 | |
| 13.50 | 0.482 | 9.34 | 0.245 | 14.60 | 0.230 | T = 393. | |
| | | 9.37 | 0.252 | 14.79 | 0.233 | | |
| | | 9.44 | 0.193 | 15.00 | 0.235 | | |
| | | 9.51 | 0.171 | CURVE 27 | | | |
| | | 9.58 | 0.162 | T = 373. | | | |
| | | 9.75 | 0.181 | | | | |
| | | 9.97 | 0.236 | | | | |
| | | 10.16 | 0.278 | | | | |
| | | 10.26 | 0.307 | | | | |
| | | 5.90 | 0.025 | | | | |
| | | 6.13 | 0.022 | | | | |
| | | 6.35 | 0.024 | | | | |
| | | 6.54 | 0.034 | | | | |
| | | 3.00 | 0.009 | | | | |
| | | 4.66 | 0.009 | | | | |
| | | 5.49 | 0.013 | | | | |
| | | 5.86 | 0.124 | | | | |
| | | 6.13 | 0.025 | | | | |
| | | 6.35 | 0.022 | | | | |
| | | 6.54 | 0.034 | | | | |
| | | 3.00 | 0.015 | | | | |
| | | 3.16 | 0.018 | | | | |
| | | 3.23 | 0.018 | | | | |
| | | 3.33 | 0.018 | | | | |
| | | 3.43 | 0.014 | | | | |
| | | 4.99 | 0.014 | | | | |
| | | 5.22 | 0.018 | | | | |
| | | 5.54 | 0.017 | | | | |
| | | 5.84 | 0.030 | | | | |
| | | 6.09 | 0.028 | | | | |
| | | 3.00 | 0.015 | | | | |
| | | 3.16 | 0.018 | | | | |
| | | 3.23 | 0.018 | | | | |
| | | 3.33 | 0.018 | | | | |
| | | 3.43 | 0.014 | | | | |
| | | 4.99 | 0.014 | | | | |
| | | 5.22 | 0.018 | | | | |
| | | 5.54 | 0.017 | | | | |
| | | 5.84 | 0.030 | | | | |
| | | 6.09 | 0.028 | | | | |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CURVE 28 (CONT.) | | | CURVE 29 (CONT.) | | | CURVE 30 (CONT.) | | | CURVE 31 T = 313. | | | |
|------------------|------------|-----------|------------------|-----------|------------|------------------|------------|-----------|----------------------|-----------|------------|-------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | |
| 11.61 | 0.424 | 6.09 | 0.028 | 11.17 | 0.470 | 3.33 | 0.019 | 10.32 | 0.370 | 3.00 | 0.029 | |
| 11.72 | 0.400 | 6.30 | 0.028 | 11.24 | 0.476 | 3.43 | 0.014 | 10.39 | 0.376 | 3.99 | 0.022 | |
| 11.83 | 0.393 | 6.44 | 0.032 | 11.35 | 0.477 | 4.99 | 0.014 | 10.46 | 0.376 | 4.97 | 0.017 | |
| 11.93 | 0.393 | 6.59 | 0.044 | 11.59 | 0.467 | 5.22 | 0.018 | 10.53 | 0.376 | 5.80 | 0.018 | |
| 11.99 | 0.402 | 6.67 | 0.056 | 11.05 | 0.441 | 5.54 | 0.017 | 10.65 | 0.404 | 5.94 | 0.021 | |
| 12.11 | 0.435 | 6.87 | 0.113 | 11.76 | 0.420 | 5.84 | 0.030 | 10.83 | 0.464 | 6.39 | 0.021 | |
| 12.21 | 0.454 | 6.93 | 0.137 | 11.96 | 0.415 | 6.09 | 0.028 | 11.09 | 0.476 | 6.58 | 0.031 | |
| 12.31 | 0.446 | 6.96 | 0.141 | 12.07 | 0.435 | 6.30 | 0.028 | 11.17 | 0.481 | 6.69 | 0.042 | |
| 12.35 | 0.433 | 7.07 | 0.141 | 12.14 | 0.467 | 6.44 | 0.032 | 11.29 | 0.481 | 6.78 | 0.060 | |
| 12.41 | 0.427 | 7.18 | 0.126 | 12.19 | 0.473 | 6.59 | 0.044 | 11.37 | 0.469 | 6.90 | 0.075 | |
| 12.53 | 0.434 | 7.33 | 0.124 | 12.27 | 0.474 | 6.67 | 0.056 | 11.54 | 0.460 | 7.03 | 0.088 | |
| 12.63 | 0.447 | 7.49 | 0.137 | 12.38 | 0.467 | 6.86 | 0.122 | 11.63 | 0.431 | 7.11 | 0.088 | |
| 12.63 | 0.476 | 7.63 | 0.152 | 12.50 | 0.467 | 6.91 | 0.141 | 11.76 | 0.420 | 7.32 | 0.081 | |
| 12.93 | 0.461 | 7.76 | 0.158 | 12.60 | 0.475 | 7.00 | 0.149 | 11.83 | 0.427 | 7.45 | 0.090 | |
| 13.05 | 0.481 | 7.99 | 0.134 | 12.68 | 0.485 | 7.11 | 0.143 | 11.96 | 0.469 | 7.62 | 0.105 | |
| 13.16 | 0.483 | 8.09 | 0.127 | 12.74 | 0.502 | 7.22 | 0.134 | 12.10 | 0.476 | 7.83 | 0.105 | |
| 13.37 | 0.484 | 8.25 | 0.127 | 12.86 | 0.506 | 7.32 | 0.130 | 12.14 | 0.479 | 7.95 | 0.079 | |
| 13.49 | 0.538 | 8.34 | 0.150 | 13.05 | 0.506 | 7.58 | 0.150 | 12.26 | 0.478 | 8.10 | 0.079 | |
| 13.57 | 0.515 | 8.46 | 0.196 | 13.17 | 0.515 | 7.65 | 0.163 | 12.34 | 0.434 | 8.21 | 0.083 | |
| 13.66 | 0.494 | 8.54 | 0.220 | 13.38 | 0.523 | 7.76 | 0.165 | 12.54 | 0.502 | 8.34 | 0.099 | |
| 13.90 | 0.403 | 8.62 | 0.248 | 13.45 | 0.537 | 7.86 | 0.161 | 12.62 | 0.509 | 8.53 | 0.136 | |
| 14.09 | 0.310 | 8.72 | 0.315 | 13.50 | 0.549 | 8.03 | 0.139 | 12.70 | 0.510 | 8.66 | 0.180 | |
| 14.19 | 0.270 | 8.88 | 0.481 | 13.59 | 0.549 | 8.14 | 0.135 | 12.82 | 0.537 | 8.96 | 0.331 | |
| 14.32 | 0.257 | 8.96 | 0.635 | 13.69 | 0.531 | 8.27 | 0.142 | 13.02 | 0.554 | 9.01 | 0.382 | |
| 14.48 | 0.254 | 9.01 | 0.642 | 13.88 | 0.474 | 8.72 | 0.315 | 13.37 | 0.557 | 9.06 | 0.400 | |
| 14.80 | 0.262 | 9.07 | 0.642 | 14.00 | 0.397 | 8.94 | 0.481 | 13.45 | 0.548 | 9.13 | 0.382 | |
| 15.00 | 0.264 | 9.14 | 0.628 | 14.09 | 0.323 | 8.88 | 0.597 | 13.54 | 0.474 | 9.26 | 0.178 | |
| | | 9.30 | 0.393 | 14.13 | 0.295 | 9.00 | 0.627 | 13.66 | 0.436 | 9.31 | 0.147 | |
| | | 9.45 | 0.248 | 14.23 | 0.274 | 9.09 | 0.634 | 13.98 | 0.349 | 9.43 | 0.119 | |
| | | 9.55 | 0.210 | 14.43 | 0.261 | 9.17 | 0.625 | 14.08 | 0.303 | 9.51 | 0.119 | |
| | | 9.60 | 0.205 | 14.58 | 0.267 | 9.25 | 0.509 | 14.14 | 0.270 | 9.69 | 0.136 | |
| | | 9.67 | 0.210 | 14.86 | 0.270 | 9.34 | 0.268 | 14.26 | 0.269 | 9.94 | 0.179 | |
| | | 9.85 | 0.237 | 15.03 | 0.276 | 9.46 | 0.234 | 14.38 | 0.269 | 10.19 | 0.232 | |
| | | 10.01 | 0.280 | | | 9.51 | 0.219 | 14.46 | 0.279 | 10.26 | 0.247 | |
| | | 10.13 | 0.313 | CURVE 30 | | | 9.58 | 0.222 | 14.60 | 0.287 | 10.35 | 0.256 |
| | | 10.28 | 0.356 | T = 433. | | | 9.69 | 0.242 | 14.74 | 0.296 | 10.41 | 0.256 |
| | | 10.40 | 0.360 | 3.00 | 0.015 | 10.06 | 0.360 | 14.82 | 0.300 | 10.55 | 0.251 | |
| | | 10.49 | 0.368 | 3.16 | 0.015 | 10.21 | 0.351 | 15.00 | 0.300 | | | |
| | | 10.62 | 0.364 | | | | | | | | | |
| | | 10.75 | 0.376 | | | | | | | | | |

CURVE 29
T = 413.

CURVE 30
T = 433.

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIOUS PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T , $^{\circ}\text{K}$; EMITTANCE, ϵ)

| CURVE 31 (CONT.) | | CURVE 32 (CONT.) | | CURVE 32 (CONT.) | | CURVE 33 (CONT.) | | CURVE 33 (CONT.) | | CURVE 34 (CONT.) | |
|------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 10.65 | 0.261 | 6.91 | 0.097 | 11.62 | 0.336 | 7.23 | 0.099 | 12.47 | 0.384 | 7.03 | 0.133 |
| 10.90 | 0.311 | 6.97 | 0.109 | 11.73 | 0.322 | 7.33 | 0.099 | 12.56 | 0.384 | 7.17 | 0.123 |
| 11.14 | 0.344 | 7.05 | 0.109 | 11.96 | 0.312 | 7.53 | 0.116 | 12.66 | 0.393 | 7.31 | 0.110 |
| 11.22 | 0.344 | 7.18 | 0.098 | 11.96 | 0.316 | 7.65 | 0.129 | 12.70 | 0.411 | 7.52 | 0.132 |
| 11.43 | 0.320 | 7.23 | 0.094 | 12.01 | 0.324 | 7.73 | 0.129 | 12.78 | 0.420 | 7.59 | 0.139 |
| 11.79 | 0.275 | 7.34 | 0.093 | 12.17 | 0.361 | 7.95 | 0.118 | 12.91 | 0.425 | 7.73 | 0.144 |
| 11.94 | 0.294 | 7.64 | 0.120 | 12.25 | 0.369 | 8.03 | 0.098 | 13.05 | 0.425 | 7.83 | 0.138 |
| 12.06 | 0.310 | 7.71 | 0.123 | 12.30 | 0.352 | 8.09 | 0.098 | 13.14 | 0.421 | 8.00 | 0.111 |
| 12.11 | 0.326 | 7.85 | 0.102 | 12.44 | 0.348 | 8.19 | 0.106 | 13.14 | 0.421 | 8.15 | 0.113 |
| 12.13 | 0.330 | 8.00 | 0.088 | 12.59 | 0.358 | 8.35 | 0.133 | 13.51 | 0.475 | 8.42 | 0.163 |
| 12.21 | 0.333 | 8.14 | 0.088 | 12.72 | 0.374 | 8.59 | 0.194 | 13.58 | 0.480 | 8.64 | 0.225 |
| 12.25 | 0.329 | 8.20 | 0.095 | 12.95 | 0.387 | 8.75 | 0.202 | 13.63 | 0.471 | 8.74 | 0.267 |
| 12.31 | 0.301 | 8.53 | 0.161 | 13.17 | 0.405 | 8.87 | 0.356 | 13.95 | 0.369 | 8.83 | 0.314 |
| 12.39 | 0.294 | 8.67 | 0.205 | 13.34 | 0.405 | 8.96 | 0.368 | 14.05 | 0.274 | 8.91 | 0.366 |
| 12.71 | 0.335 | 8.80 | 0.266 | 13.41 | 0.415 | 9.04 | 0.408 | 14.14 | 0.239 | 8.97 | 0.487 |
| 13.08 | 0.367 | 8.90 | 0.327 | 13.50 | 0.430 | 9.16 | 0.382 | 14.22 | 0.208 | 9.04 | 0.413 |
| 13.24 | 0.377 | 8.96 | 0.366 | 13.55 | 0.434 | 9.31 | 0.223 | 14.36 | 0.185 | 9.11 | 0.437 |
| 13.34 | 0.392 | 9.00 | 0.365 | 13.63 | 0.426 | 9.46 | 0.172 | 14.42 | 0.185 | 9.16 | 0.397 |
| 13.40 | 0.398 | 9.05 | 0.401 | 13.85 | 0.323 | 9.60 | 0.155 | 14.51 | 0.293 | 9.24 | 0.331 |
| 13.52 | 0.398 | 9.15 | 0.363 | 14.09 | 0.224 | 9.68 | 0.155 | 14.63 | 0.211 | 9.33 | 0.269 |
| 13.65 | 0.384 | 9.20 | 0.292 | 14.22 | 0.212 | 9.77 | 0.167 | 14.77 | 0.217 | 9.35 | 0.244 |
| 14.23 | 0.146 | 9.32 | 0.195 | 14.45 | 0.175 | 10.01 | 0.211 | 14.85 | 0.221 | 9.42 | 0.216 |
| 14.31 | 0.139 | 9.37 | 0.175 | 14.59 | 0.173 | 10.24 | 0.271 | 15.00 | 0.221 | 9.53 | 0.187 |
| 14.48 | 0.139 | 9.46 | 0.150 | 15.00 | 0.185 | 10.39 | 0.298 | | | 9.60 | 0.180 |
| 15.00 | 0.156 | 9.55 | 0.140 | | | 10.47 | 0.301 | CURVE 34 | | 9.69 | 0.183 |
| | | 9.66 | 0.144 | CURVE 33 | | 10.60 | 0.297 | $T = 433.$ | | 10.07 | 0.264 |
| | | 9.82 | 0.169 | $T = 393.$ | | 10.69 | 0.302 | | | 10.25 | 0.305 |
| | | 10.10 | 0.224 | | | 10.86 | 0.342 | 3.00 | 0.040 | 10.34 | 0.316 |
| | | 10.24 | 0.253 | | | 11.00 | 0.380 | 3.99 | 0.028 | 10.39 | 0.322 |
| 3.00 | 0.034 | 10.29 | 0.271 | 3.00 | 0.037 | 11.25 | 0.408 | 4.47 | 0.024 | 10.50 | 0.322 |
| 3.98 | 0.023 | 10.35 | 0.282 | 3.99 | 0.026 | 11.37 | 0.408 | 5.58 | 0.024 | 10.58 | 0.321 |
| 4.37 | 0.022 | 10.41 | 0.282 | 4.43 | 0.022 | 11.48 | 0.396 | 6.14 | 0.028 | 10.66 | 0.325 |
| 4.99 | 0.021 | 10.50 | 0.273 | 5.31 | 0.022 | 11.68 | 0.359 | 6.29 | 0.030 | 10.75 | 0.339 |
| 5.73 | 0.021 | 10.62 | 0.279 | 5.99 | 0.024 | 11.86 | 0.347 | 6.52 | 0.036 | 10.85 | 0.362 |
| 6.80 | 0.024 | 10.75 | 0.301 | 6.36 | 0.028 | 12.00 | 0.356 | 6.59 | 0.042 | 11.05 | 0.403 |
| 6.41 | 0.025 | 11.04 | 0.355 | 6.53 | 0.037 | 12.09 | 0.381 | 6.67 | 0.052 | 11.14 | 0.419 |
| 6.55 | 0.034 | 11.12 | 0.369 | 6.65 | 0.051 | 12.13 | 0.402 | 6.71 | 0.069 | 11.21 | 0.425 |
| 6.66 | 0.043 | 11.19 | 0.382 | 6.85 | 0.097 | 12.29 | 0.406 | 6.87 | 0.089 | 11.35 | 0.425 |
| 6.86 | 0.033 | 11.26 | 0.386 | 7.07 | 0.115 | 12.41 | 0.406 | 6.94 | 0.120 | 11.48 | 0.417 |
| | | | | | 0.115 | | | | 0.129 | | 0.405 |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|------------------|------------|-----------|------------|-----------|------------|-----------|------------|----------------------|------------|
| CURVE 34 (CONT.) | | | | | | | | | |
| 11.82 | 0.369 | 7.08 | 0.091 | 12.19 | 0.338 | 7.71 | 0.124 | 12.25 | 0.369 |
| 11.92 | 0.363 | 7.18 | 0.085 | 12.23 | 0.329 | 7.81 | 0.117 | 12.34 | 0.355 |
| 12.11 | 0.401 | 7.32 | 0.089 | 12.34 | 0.296 | 7.97 | 0.094 | 12.44 | 0.349 |
| 12.21 | 0.412 | 7.50 | 0.094 | 12.49 | 0.311 | 8.03 | 0.089 | 12.77 | 0.376 |
| 12.27 | 0.418 | 7.61 | 0.105 | 12.61 | 0.327 | 8.18 | 0.089 | 12.97 | 0.388 |
| 12.35 | 0.418 | 7.72 | 0.105 | 12.77 | 0.344 | 8.32 | 0.111 | 13.17 | 0.404 |
| 12.53 | 0.405 | 7.82 | 0.090 | 13.13 | 0.357 | 8.50 | 0.114 | 13.32 | 0.406 |
| 12.62 | 0.410 | 8.00 | 0.079 | 13.13 | 0.368 | 8.63 | 0.105 | 13.41 | 0.416 |
| 12.81 | 0.450 | 8.17 | 0.079 | 13.39 | 0.397 | 8.75 | 0.227 | 13.47 | 0.426 |
| 12.91 | 0.458 | 8.35 | 0.093 | 13.52 | 0.397 | 8.85 | 0.208 | 13.52 | 0.433 |
| 13.02 | 0.461 | 8.50 | 0.124 | 13.58 | 0.390 | 8.94 | 0.346 | 13.59 | 0.433 |
| 13.13 | 0.461 | 8.63 | 0.158 | 13.73 | 0.353 | 9.02 | 0.386 | 13.67 | 0.412 |
| 13.23 | 0.458 | 8.74 | 0.218 | 13.97 | 0.243 | 9.09 | 0.398 | 13.90 | 0.288 |
| 13.33 | 0.458 | 8.94 | 0.314 | 14.07 | 0.199 | 9.15 | 0.372 | 14.17 | 0.181 |
| 13.43 | 0.466 | 9.05 | 0.379 | 14.14 | 0.161 | 9.21 | 0.304 | 14.23 | 0.172 |
| 13.54 | 0.486 | 9.09 | 0.398 | 14.17 | 0.157 | 9.25 | 0.258 | 14.40 | 0.172 |
| 13.62 | 0.486 | 9.13 | 0.379 | 14.22 | 0.148 | 9.30 | 0.222 | 14.56 | 0.172 |
| 13.69 | 0.471 | 9.18 | 0.290 | 14.33 | 0.141 | 9.41 | 0.171 | 14.80 | 0.181 |
| 13.95 | 0.384 | 9.27 | 0.176 | 14.45 | 0.141 | 9.50 | 0.146 | 15.00 | 0.186 |
| 14.06 | 0.333 | 9.31 | 0.154 | 15.00 | 0.160 | 9.59 | 0.139 | CURVE 37 T = 393. | |
| 14.15 | 0.284 | 9.38 | 0.129 | CURVE 36 | | 9.69 | 0.146 | 3.00 | 0.039 |
| 14.22 | 0.239 | 9.42 | 0.123 | T = 353. | | 9.95 | 0.192 | 3.93 | 0.030 |
| 14.46 | 0.212 | 9.50 | 0.118 | 3.00 | 0.038 | 10.15 | 0.238 | 4.45 | 0.025 |
| 14.82 | 0.187 | 9.62 | 0.125 | 3.82 | 0.029 | 10.21 | 0.252 | 4.75 | 0.024 |
| 15.00 | 0.194 | 10.05 | 0.198 | 4.39 | 0.025 | 10.35 | 0.283 | 5.42 | 0.025 |
| CURVE 35 | | | | | | | | | |
| T = 313. | | | | | | | | | |
| 3.00 | 0.035 | 10.13 | 0.222 | 4.97 | 0.022 | 10.43 | 0.283 | 5.67 | 0.025 |
| 3.73 | 0.025 | 10.29 | 0.250 | 5.46 | 0.022 | 10.51 | 0.275 | 5.86 | 0.030 |
| 4.03 | 0.018 | 10.36 | 0.258 | 5.74 | 0.026 | 10.60 | 0.275 | 6.24 | 0.030 |
| 4.49 | 0.018 | 10.44 | 0.258 | 5.92 | 0.029 | 10.80 | 0.305 | 6.41 | 0.032 |
| 5.78 | 0.023 | 10.54 | 0.260 | 6.26 | 0.029 | 10.99 | 0.353 | 6.55 | 0.040 |
| 6.37 | 0.023 | 10.55 | 0.260 | 6.43 | 0.032 | 11.14 | 0.367 | 6.83 | 0.089 |
| 6.54 | 0.029 | 10.97 | 0.315 | 6.61 | 0.046 | 11.22 | 0.384 | 6.86 | 0.112 |
| 6.71 | 0.045 | 11.09 | 0.336 | 6.73 | 0.064 | 11.32 | 0.384 | 7.04 | 0.121 |
| 6.87 | 0.066 | 11.21 | 0.342 | 6.95 | 0.099 | 11.71 | 0.329 | 7.21 | 0.105 |
| 6.97 | 0.082 | 11.33 | 0.331 | 7.04 | 0.109 | 11.83 | 0.313 | 7.36 | 0.105 |
| | | 11.60 | 0.280 | 7.25 | 0.095 | 12.07 | 0.328 | 7.65 | 0.131 |
| | | 11.94 | 0.293 | 7.36 | 0.095 | 12.11 | 0.339 | | |
| | | 12.07 | 0.312 | 7.47 | 0.104 | 12.13 | 0.354 | | |
| | | 12.15 | 0.330 | | | | | | |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| CURVE 37 (CONT.) | | | CURVE 38 (CONT.) | | | CURVE 39 (CONT.) | | | CURVE 40 (CONT.) | | | |
|------------------|------------|-----------|------------------|-----------|------------|------------------|------------|-----------|------------------|-----------|------------|-------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | |
| 12.46 | 0.383 | 7.01 | 0.133 | 12.61 | 0.409 | 1.837 | 0.6536 | 0.929 | 0.672 | 13.00 | 0.596 | |
| 12.60 | 0.383 | 7.10 | 0.133 | 12.72 | 0.436 | 2.291 | 0.2530 | 1.804 | 0.675 | 14.00 | 0.631 | |
| 12.68 | 0.396 | 7.26 | 0.113 | 12.60 | 0.451 | 2.500 | 0.0560 | 1.18 | 0.675 | 15.00 | 0.569 | |
| 12.73 | 0.414 | 7.35 | 0.113 | 12.94 | 0.459 | 3.724 | 0.620 | 1.21 | 0.659 | CURVE 41 | | |
| 12.80 | 0.422 | 7.69 | 0.144 | 13.14 | 0.459 | 5.117 | 0.080 | 1.23 | 0.631 | T = 693. | | |
| 12.89 | 0.426 | 7.79 | 0.144 | 13.30 | 0.456 | 5.975 | 0.0750 | 1.26 | 0.506 | 0.398 | 0.525 | |
| 13.14 | 0.423 | 7.98 | 0.126 | 13.36 | 0.460 | 6.291 | 0.0860 | 1.29 | 0.361 | 0.473 | 0.580 | |
| 13.28 | 0.436 | 8.13 | 0.112 | 13.54 | 0.487 | 6.531 | 0.0980 | 1.34 | 0.272 | 0.528 | 0.601 | |
| 13.41 | 0.453 | 8.28 | 0.126 | 13.60 | 0.499 | 6.699 | 0.154 | 1.39 | 0.207 | 0.610 | 0.625 | |
| 13.51 | 0.473 | 8.44 | 0.160 | 13.66 | 0.480 | 6.823 | 0.180 | 1.45 | 0.163 | 0.681 | 0.637 | |
| 13.57 | 0.481 | 8.62 | 0.214 | 13.68 | 0.401 | 6.982 | 0.205 | 1.60 | 0.132 | 0.820 | 0.655 | |
| 13.66 | 0.471 | 8.70 | 0.235 | 14.00 | 0.355 | 7.129 | 0.205 | 1.72 | 0.119 | 0.929 | 0.672 | |
| 13.83 | 0.400 | 8.88 | 0.331 | 14.07 | 0.306 | 7.195 | 0.190 | 1.88 | 0.112 | 1.04 | 0.675 | |
| 13.95 | 0.359 | 8.98 | 0.402 | 14.22 | 0.246 | 7.499 | 0.179 | 2.14 | 0.110 | 1.21 | 0.674 | |
| 14.03 | 0.284 | 9.05 | 0.414 | 14.33 | 0.224 | 7.638 | 0.201 | 2.31 | 0.130 | 1.25 | 0.657 | |
| 14.14 | 0.234 | 9.14 | 0.409 | 14.47 | 0.211 | 7.962 | 0.179 | 2.90 | 0.146 | 1.26 | 0.632 | |
| 14.21 | 0.214 | 9.20 | 0.393 | 14.64 | 0.202 | 8.260 | 0.154 | 3.61 | 0.156 | 1.28 | 0.594 | |
| 14.34 | 0.190 | 9.33 | 0.274 | 14.83 | 0.188 | 8.511 | 0.185 | 4.56 | 0.179 | 1.30 | 0.427 | |
| 14.44 | 0.190 | 9.49 | 0.206 | 15.00 | 0.195 | 8.730 | 0.324 | 5.55 | 0.199 | 1.33 | 0.348 | |
| 14.50 | 0.207 | 9.61 | 0.180 | | | 8.974 | 0.434 | 6.03 | 0.224 | 1.37 | 0.278 | |
| 14.64 | 0.217 | 9.69 | 0.180 | CURVE 39 | | | 9.141 | 0.454 | 6.37 | 0.248 | 1.41 | 0.229 |
| 14.77 | 0.223 | 9.80 | 0.195 | T = 543. | | | 9.376 | 0.384 | 6.56 | 0.270 | 1.44 | 0.202 |
| 15.80 | 0.225 | 10.08 | 0.255 | 0.398 | 0.525 | 9.818 | 0.293 | 6.71 | 0.289 | 1.66 | 0.186 | |
| CURVE 38 | | | 10.24 | 0.296 | 0.473 | 0.580 | 10.00 | 0.314 | 6.79 | 0.307 | 1.88 | 0.195 |
| T = 433. | | | 19.34 | 0.319 | 0.528 | 0.601 | 11.00 | 0.430 | 6.89 | 0.319 | 2.00 | 0.258 |
| 3.00 | 0.041 | 10.70 | 0.332 | 0.619 | 0.625 | 12.00 | 0.449 | 7.03 | 0.319 | 3.04 | 0.300 | |
| 3.52 | 0.035 | 10.81 | 0.348 | 0.681 | 0.637 | 13.00 | 0.498 | 7.28 | 0.305 | 3.67 | 0.378 | |
| 4.32 | 0.029 | 10.95 | 0.379 | 0.820 | 0.655 | 14.00 | 0.558 | 8.00 | 0.356 | 5.05 | 0.435 | |
| 4.55 | 0.025 | 11.04 | 0.400 | 0.929 | 0.672 | 15.00 | 0.460 | 8.34 | 0.391 | 6.11 | 0.529 | |
| 5.42 | 0.025 | 11.23 | 0.425 | 1.127 | 0.672 | CURVE 40 | | | 8.61 | 0.441 | 8.91 | 0.563 |
| 5.86 | 0.031 | 11.32 | 0.425 | 1.175 | 0.660 | T = 623. | | | 8.97 | 0.507 | 9.00 | 0.564 |
| 6.20 | 0.031 | 11.50 | 0.416 | 1.208 | 0.625 | 0.398 | 0.525 | 9.31 | 0.568 | 10.00 | 0.597 | |
| 6.37 | 0.034 | 11.86 | 0.365 | 1.262 | 0.350 | 0.473 | 0.580 | 9.14 | 0.521 | 11.00 | 0.647 | |
| 6.48 | 0.039 | 11.96 | 0.368 | 1.300 | 0.258 | 0.528 | 0.601 | 9.31 | 0.568 | 12.00 | 0.680 | |
| 6.59 | 0.048 | 12.22 | 0.415 | 1.337 | 0.176 | 0.610 | 0.625 | 9.73 | 0.454 | 13.00 | 0.703 | |
| 6.65 | 0.058 | 12.28 | 0.419 | 1.390 | 0.130- | 0.681 | 0.637 | 10.00 | 0.470 | 14.00 | 0.712 | |
| 6.80 | 0.058 | 12.37 | 0.419 | 1.459 | 0.0980 | 0.820 | 0.655 | 11.00 | 0.549 | 15.00 | 0.710 | |
| 6.90 | 0.121 | 12.46 | 0.406 | 1.549 | 0.0810 | 0.820 | 0.655 | 12.00 | 0.583 | | | |
| | | 12.54 | 0.402 | 1.656 | 0.0670 | | | | | | | |

TABLE 12-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF VARIED PURITY SILICCN (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μ m; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CURVE 42 T = 743. | | | CURVE 43 (CONT.) | | | CURVE 44 (CONT.) | | | CURVE 45 (CONT.) | | | CURVE 47 (CONT.) | | | CURVE 49 (CONT.) | | |
|----------------------|------------|-----------|------------------|-----------------------|------------|----------------------|------------|----------------------|------------------|-----------|------------|----------------------|------------|----------------------|------------------|-----------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 0.390 | 0.525 | 0.443 | 0.546 | 0.494 | 0.567 | 3.01 | 0.714 | 6.10 | 0.717 | 10.23 | 0.740 | 2.26 | 0.684 | 2.44 | 0.665 | 2.26 | 0.684 |
| 0.473 | 0.580 | 0.479 | 0.569 | 3.535 | 0.589 | 4.80 | 0.716 | 7.05 | 0.730 | 11.14 | 0.756 | 3.01 | 0.680 | 3.01 | 0.669 | 3.01 | 0.680 |
| 0.520 | 0.601 | 0.530 | 0.591 | 0.601 | 0.600 | 5.00 | 0.716 | 8.11 | 0.747 | 12.33 | 0.761 | 4.06 | 0.699 | 4.06 | 0.677 | 4.06 | 0.699 |
| 0.610 | 0.625 | 0.592 | 0.611 | 0.630 | 0.615 | 6.00 | 0.716 | 9.12 | 0.758 | 13.34 | 0.766 | 5.01 | 0.709 | 5.01 | 0.688 | 5.01 | 0.709 |
| 0.681 | 0.637 | 0.655 | 0.622 | 0.673 | 0.631 | 7.00 | 0.716 | 10.16 | 0.766 | 14.22 | 0.766 | 5.90 | 0.719 | 5.90 | 0.675 | 5.90 | 0.719 |
| 0.820 | 0.655 | 0.813 | 0.647 | 0.855 | 0.650 | 8.00 | 0.716 | 11.14 | 0.782 | 15.00 | 0.782 | 7.11 | 0.730 | 7.11 | 0.697 | 7.11 | 0.730 |
| 0.929 | 0.672 | 0.887 | 0.656 | 1.000 | 0.664 | 9.00 | 0.716 | 12.33 | 0.789 | 15.00 | 0.789 | 7.93 | 0.737 | 7.93 | 0.709 | 7.93 | 0.737 |
| 1.04 | 0.675 | 1.04 | 0.673 | 1.22 | 0.677 | 10.00 | 0.716 | 14.22 | 0.794 | 15.00 | 0.794 | 8.97 | 0.747 | 8.97 | 0.755 | 8.97 | 0.747 |
| 1.21 | 0.674 | 1.20 | 0.676 | 1.69 | 0.693 | 11.00 | 0.716 | 15.00 | 0.790 | 15.00 | 0.790 | 10.00 | 0.755 | 10.00 | 0.755 | 10.00 | 0.755 |
| 1.25 | 0.674 | 1.25 | 0.670 | 2.24 | 0.706 | 12.00 | 0.716 | 2.90 | 0.675 | 10.00 | 0.675 | 11.14 | 0.767 | 11.14 | 0.767 | 11.14 | 0.767 |
| 1.29 | 0.641 | 1.31 | 0.652 | 3.01 | 0.714 | 13.00 | 0.713 | 3.57 | 0.677 | 11.09 | 0.767 | 12.33 | 0.730 | 12.33 | 0.730 | 12.33 | 0.730 |
| 1.32 | 0.616 | 1.35 | 0.622 | 4.80 | 0.716 | 14.00 | 0.712 | 4.50 | 0.684 | 12.16 | 0.776 | 13.34 | 0.747 | 13.34 | 0.747 | 13.34 | 0.747 |
| 1.32 | 0.484 | 1.37 | 0.549 | 5.00 | 0.716 | 15.00 | 0.710 | 5.14 | 0.680 | 13.21 | 0.781 | 14.00 | 0.781 | 14.00 | 0.781 | 14.00 | 0.781 |
| 1.34 | 0.416 | 1.39 | 0.479 | 6.00 | 0.716 | CURVE 46 T = 543. | 0.686 | 6.99 | 0.735 | 14.03 | 0.783 | 15.14 | 0.786 | 15.14 | 0.786 | 15.14 | 0.786 |
| 1.37 | 0.372 | 1.43 | 0.442 | 7.00 | 0.716 | 2.90 | 0.689 | 8.05 | 0.749 | 15.14 | 0.786 | CURVE 48 T = 793. | 0.675 | CURVE 48 T = 793. | 0.675 | 2.90 | 0.684 |
| 1.37 | 0.350 | 1.52 | 0.429 | 8.00 | 0.716 | 3.55 | 0.689 | 9.12 | 0.762 | 2.90 | 0.686 | 3.57 | 0.677 | 3.57 | 0.677 | 3.57 | 0.677 |
| 1.42 | 0.339 | 1.73 | 0.451 | 9.00 | 0.716 | 4.11 | 0.694 | 10.14 | 0.771 | 3.57 | 0.677 | 4.15 | 0.684 | 4.15 | 0.684 | 4.15 | 0.684 |
| 1.51 | 0.339 | 2.15 | 0.517 | 10.00 | 0.716 | 4.56 | 0.702 | 11.14 | 0.786 | 4.50 | 0.680 | 4.50 | 0.680 | 4.50 | 0.680 | 4.50 | 0.680 |
| 1.50 | 0.342 | 2.54 | 0.558 | 11.00 | 0.716 | 5.02 | 0.700 | 12.33 | 0.795 | 5.14 | 0.697 | 5.14 | 0.697 | 5.14 | 0.697 | 5.14 | 0.697 |
| 2.13 | 0.396 | 2.94 | 0.594 | 12.00 | 0.716 | 6.05 | 0.722 | 13.34 | 0.802 | 6.28 | 0.710 | 6.28 | 0.710 | 6.28 | 0.710 | 6.28 | 0.710 |
| 2.04 | 0.452 | 3.37 | 0.622 | 13.00 | 0.713 | 6.99 | 0.735 | 14.22 | 0.805 | 7.13 | 0.721 | 7.13 | 0.721 | 7.13 | 0.721 | 7.13 | 0.721 |
| 3.48 | 0.498 | 4.06 | 0.653 | 14.00 | 0.712 | 8.05 | 0.749 | 15.00 | 0.805 | 8.22 | 0.735 | 8.22 | 0.735 | 8.22 | 0.735 | 8.22 | 0.735 |
| 4.30 | 0.553 | 4.70 | 0.675 | 15.00 | 0.710 | 8.99 | 0.762 | CURVE 47 T = 693. | 0.805 | 9.27 | 0.740 | 9.27 | 0.740 | 9.27 | 0.740 | 9.27 | 0.740 |
| 4.97 | 0.594 | 5.47 | 0.695 | CURVE 45 T = 1073. | 0.710 | 8.05 | 0.749 | 10.14 | 0.771 | 10.23 | 0.755 | 10.23 | 0.755 | 10.23 | 0.755 | 10.23 | 0.755 |
| 5.66 | 0.627 | 6.47 | 0.710 | 0.398 | 0.463 | 9.00 | 0.716 | 11.14 | 0.786 | 11.14 | 0.766 | 11.14 | 0.766 | 11.14 | 0.766 | 11.14 | 0.766 |
| 6.37 | 0.651 | 7.28 | 0.717 | 0.433 | 0.508 | 10.00 | 0.716 | 12.33 | 0.795 | 12.33 | 0.777 | 12.33 | 0.777 | 12.33 | 0.777 | 12.33 | 0.777 |
| 7.23 | 0.679 | 8.00 | 0.716 | 0.463 | 0.533 | 11.00 | 0.716 | 13.34 | 0.802 | 13.34 | 0.781 | 13.34 | 0.781 | 13.34 | 0.781 | 13.34 | 0.781 |
| 8.38 | 0.698 | 9.00 | 0.716 | 0.496 | 0.558 | 12.00 | 0.716 | 14.22 | 0.805 | 14.22 | 0.784 | 14.22 | 0.784 | 14.22 | 0.784 | 14.22 | 0.784 |
| 9.25 | 0.708 | 10.00 | 0.716 | 0.542 | 0.580 | 13.00 | 0.713 | CURVE 49 T = 893. | 0.805 | 2.90 | 0.662 | 2.90 | 0.662 | 2.90 | 0.662 | 2.90 | 0.662 |
| 10.00 | 0.712 | 11.00 | 0.716 | 0.592 | 0.597 | 14.00 | 0.712 | 3.57 | 0.666 | 3.57 | 0.566 | 3.57 | 0.566 | 3.57 | 0.566 | 3.57 | 0.566 |
| 11.00 | 0.716 | 12.00 | 0.716 | 0.638 | 0.615 | 15.00 | 0.710 | 4.10 | 0.671 | 4.10 | 0.671 | 4.10 | 0.671 | 4.10 | 0.671 | 4.10 | 0.671 |
| 12.00 | 0.716 | 13.00 | 0.713 | 0.733 | 0.631 | CURVE 44 T = 873. | 0.631 | 4.69 | 0.670 | 4.69 | 0.670 | 4.69 | 0.670 | 4.69 | 0.670 | 4.69 | 0.670 |
| 13.00 | 0.713 | 14.00 | 0.712 | 1.055 | 0.650 | 0.398 | 0.484 | 5.27 | 0.686 | 5.27 | 0.686 | 5.27 | 0.686 | 5.27 | 0.686 | 5.27 | 0.686 |
| 14.00 | 0.712 | 15.00 | 0.710 | 1.00 | 0.664 | 0.454 | 0.540 | 6.30 | 0.703 | 6.30 | 0.703 | 6.30 | 0.703 | 6.30 | 0.703 | 6.30 | 0.703 |
| 15.00 | 0.710 | 0.398 | 0.484 | 1.22 | 0.677 | 1.69 | 0.693 | 7.13 | 0.711 | 7.13 | 0.711 | 7.13 | 0.711 | 7.13 | 0.711 | 7.13 | 0.711 |
| CURVE 43 T = 793. | 0.500 | 0.398 | 0.484 | 2.24 | 0.706 | 2.24 | 0.706 | 8.34 | 0.727 | 8.34 | 0.727 | 8.34 | 0.727 | 8.34 | 0.727 | 8.34 | 0.727 |
| 0.398 | 0.500 | 0.454 | 0.540 | 5.07 | 0.702 | 5.07 | 0.702 | 9.40 | 0.739 | 9.40 | 0.739 | 9.40 | 0.739 | 9.40 | 0.739 | 9.40 | 0.739 |

b. Normal Spectral Emittance (Temperature Dependence)

Only five papers have reported the normal spectral emittance of high purity silicon at higher than room temperatures. Only three of the five have reported measurements in the 1-15 μm range. The available experimental data, covering a temperature range from 300-1075 K, are shown in Figure 12-5 and Table 12-6. The data of curves 5 through 18 were obtained by reading points from the spectral curves of Section 12.4.a at the selected wavelengths of 2.8, 3.8, 5.0, and 10.6 μm .

The recommended values shown in Table 12-4 and Figure 12-4 are based on the data of Sato [T41640] (curves 11-14) at temperatures above 550 K and on the data of Stierwalt [T16961] (curves 5-10) and Stierwalt and Potter [T32537] (curves 15-18) below 550 K. The samples used by Stierwalt and Stierwalt and Potter were high resistivity, 2.03 mm thick (n-type) and 1.68 mm thick (p-type) single crystals, while Sato's sample was a 1.77 mm thick, n-type single crystal. The tabulated values for the selected wavelengths were obtained by drawing an average curve through the data for the 2.03 and 1.68 mm thick samples in the 300-550 K range and smoothly joining it to the higher temperature data for the 1.77 mm thick sample. Consequently, at the lower temperatures, the tabulated values are applicable only to samples about 2 mm thick. However, at temperatures above about 800 K, silicon of ordinary purity becomes opaque to radiation in the 2-15 μm range and the normal spectral emittance no longer depends on the thickness of the sample. Above about 800 K, therefore, the tabulated values are applicable to polished high resistivity, single crystals of any thickness. In this temperature region, the emittance converges to a value of about 0.710 for all wavelengths in the 2-15 μm region. Sato's measurements show that this value does not vary significantly with increasing temperature in the 900-1100 K range. Assuming that this trend continues, the constant-valued curves have been extended, provisionally, to 1600 K.

The 0.710 value of the emittance for opaque specimens gives a value of 0.290 for the single surface reflectance. As mentioned in the previous section, a variety of experimental evidence confirms a value of 0.30 for the single surface reflectance of polished relatively pure silicon at room temperature for 2-15 μm radiation. This supports the high temperature emittance values, if the single surface reflectance does not vary greatly with temperature. Measurements of the absorption coefficient and refractive index at high temperatures indicate that the single surface reflectance does indeed maintain a value near 0.30 at high temperatures.

The tabulated values for 2.8, 3.8, and 5.0 μm in the 300-700 K range must be considered typical only. Their percentage uncertainty is high (as great as 80-90%) both

because of the method used to generate them and because the emittance is very small in this range. The uncertainty of the values for 10.6 μm radiation should not exceed $\pm 15\%$ in the 300-700 K range. From 800-1100 K, the uncertainty of the values for all wavelengths is believed to be no greater than $\pm 8\%$. From 1100-1600 K, the values are extrapolated, but should be accurate to within 30%.

TABLE 12-4. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)
 [WAVELENGTH, λ , μm : TEMPERATURE, T, K; EMITTANCE, ϵ]

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|----------------------------|------------|-------|------------|-------|------------|-------|------------|
| SINGLE CRYSTAL | | | | | | | |
| 2 MM THICK $\lambda = 2.0$ | | | | | | | |
| 300. | 0.0268† | 300. | 0.0128† | 300. | 0.0118† | 300. | 0.265 |
| 350. | 0.0328 | 350. | 0.0178 | 350. | 0.0153 | 325. | 1.280 |
| 400. | 0.0378 | 400. | 0.0218 | 400. | 0.0198 | 350. | 0.296 |
| 425. | 0.0398 | 425. | 0.0238 | 425. | 0.0218 | 375. | 0.313 |
| 450. | 0.0418 | 450. | 0.0258 | 450. | 0.0248 | 400. | 0.330 |
| 475. | 0.0428 | 475. | 0.0289 | 475. | 0.0279 | 425. | 0.346 |
| 500. | 0.0458 | 500. | 0.0368 | 500. | 0.0378 | 450. | 0.364 |
| 520. | 0.0498 | 520. | 0.0498 | 520. | 0.0498 | 475. | 0.382 |
| 540. | 0.0568 | 540. | 0.0598 | 540. | 0.0659 | 500. | 0.400 |
| 560. | 0.069A | 560. | 0.074A | 560. | 0.085A | 525. | 0.419 |
| 580. | 0.087A | 580. | 0.092A | 590. | 0.109A | 550. | 0.440 |
| 600. | 0.106A | 600. | 0.114A | 600. | 0.138A | 575. | 0.464 |
| 620. | 0.126 | 620. | 0.138 | 620. | 0.173 | 600. | 0.490 |
| 640. | 0.151 | 640. | 0.169 | 640. | 0.217 | 620. | 0.517 |
| 660. | 0.181 | 660. | 0.206 | 660. | 0.270 | 640. | 0.538 |
| 680. | 0.213 | 680. | 0.253 | 680. | 0.333 | 660. | 0.568 |
| 700. | 0.262 | 700. | 0.314 | 700. | 0.404 | 680. | 0.609 |
| 720. | 0.344 | 720. | 0.393 | 720. | 0.490 | 690. | 0.630 |
| 740. | 0.431 | 740. | 0.487 | 740. | 0.581 | 700. | 0.652 |
| 760. | 0.499 | 760. | 0.560 | 760. | 0.634 | 710. | 0.672 |
| 780. | 0.559 | 780. | 0.610 | 780. | 0.664 | 720. | 0.689 |
| 800. | 0.600 | 800. | 0.649 | 800. | 0.685 | 730. | 0.700 |
| 820. | 0.647 | 820. | 0.678 | 820. | 0.699 | 740. | 0.710 |
| 840. | 0.682 | 840. | 0.698 | 840. | 0.705 | 750. | 0.714 |
| 860. | 0.705 | 860. | 0.711 | 860. | 0.715 | 800. | 0.716 |
| 880. | 0.712 | 880. | 0.714 | 880. | 0.716 | 850. | 0.716 |
| 900. | 0.712 | 900. | 0.714 | 900. | 0.716 | 900. | 0.716 |
| 950. | 0.712 | 950. | 0.714 | 950. | 0.716 | 950. | 0.716 |
| 1000. | 0.712 | 1000. | 0.714 | 1000. | 0.716 | 1000. | 0.716 |
| 1050. | 0.712 | 1050. | 0.714 | 1050. | 0.716 | 1050. | 0.716 |
| 1075. | 0.712 | 1075. | 0.714 | 1075. | 0.716 | 1075. | 0.716 |
| 1400. | 0.712A | 1400. | 0.714A | 1400. | 0.716A | 1400. | 0.716A |
| 1600. | 0.712A | 1600. | 0.714A | 1600. | 0.716A | 1600. | 0.716A |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL AND BY A "9" IS TYPICAL.

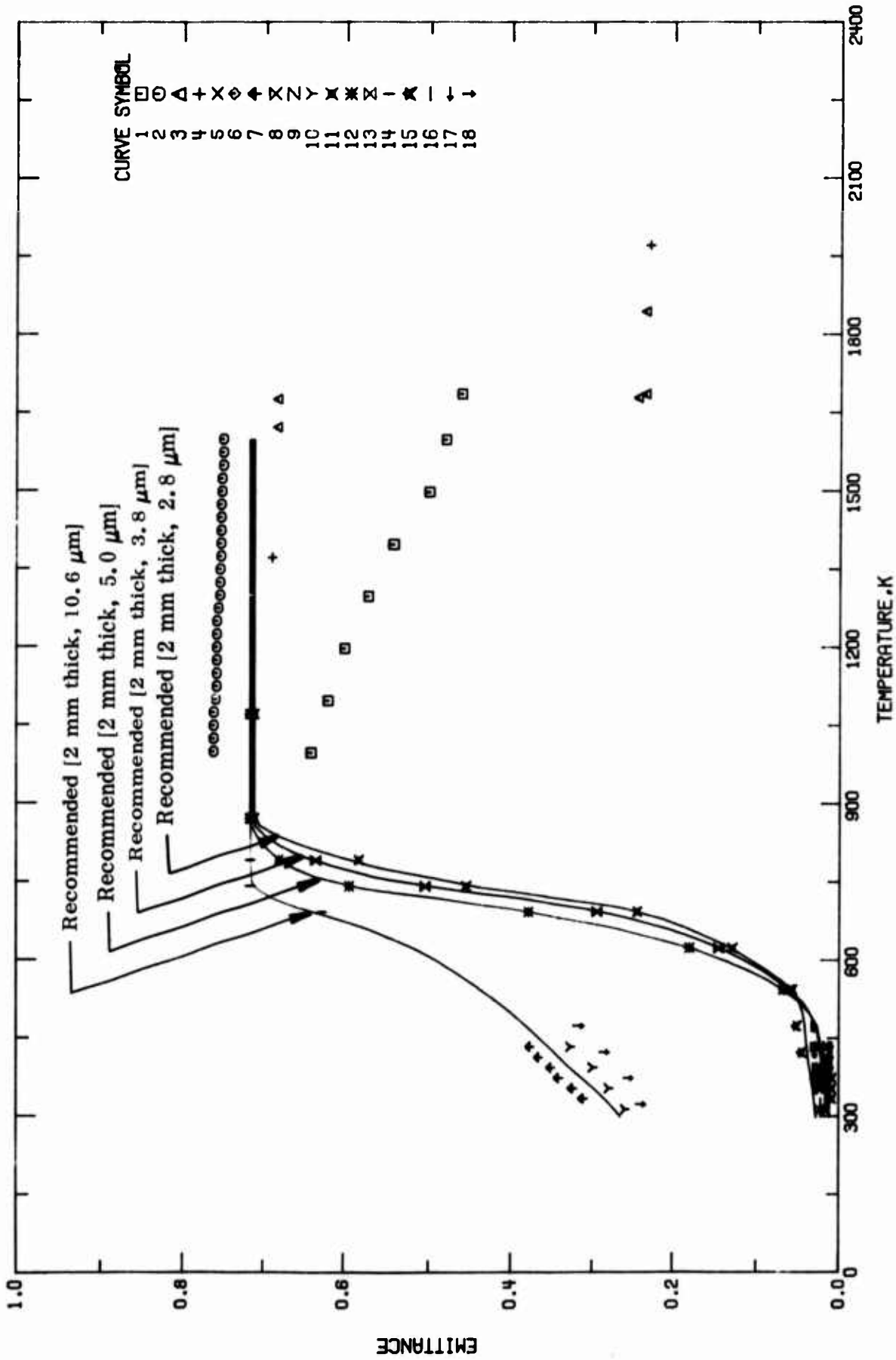


FIGURE 12-4. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF HIGH-RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)

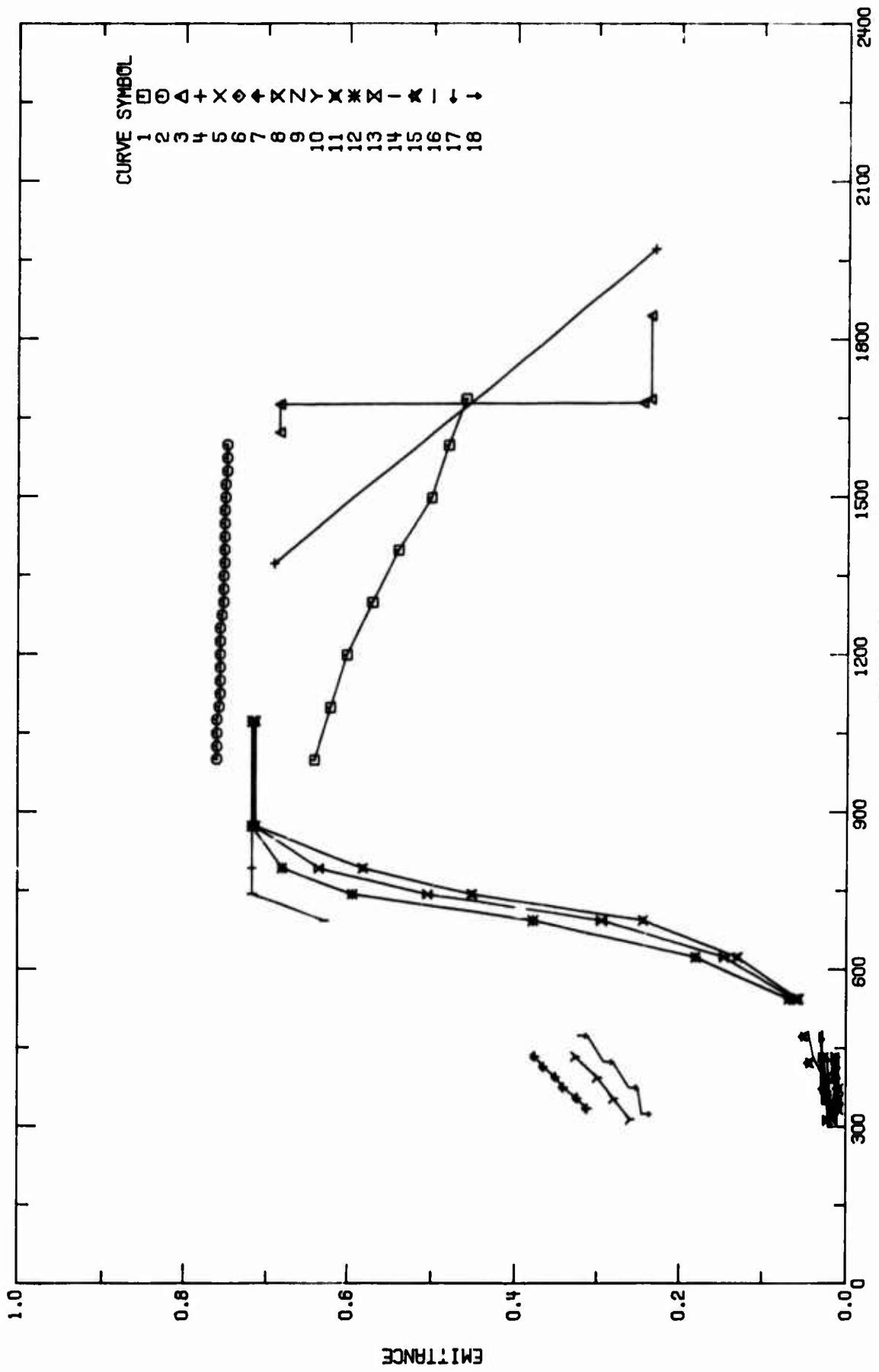


FIGURE 12-5. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON (TEMPERATURE DEPENDENCE)

TABLE 12-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMISSIVITY OF SILICON (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1* T8677 | Allen, F.G. | 1957 | 0.65 | 1000-1688 | | Single crystal; long thin-walled cylinder 1 in. long x 0.5 in. O. D. x 0.020 in. wall; etched; vacuum of 10^{-7} to 10^{-9} mm Hg; Worthing thin-walled cylinder technique; geometry gave as much as 5% less than ideal black body conditions; values may be high, particularly at lower temperatures; reported error $\pm 10\%$. |
| 2* T8677 | Allen, F.C. | 1957 | 0.65 | 1000-1688 | | Similar to the above specimen except specimen sandblasted and measured in open air; rough indication only; extracted from smoothed curve. |
| 3* T74059 | Baum, B.A., Shvarev, K.M., and Gel'd, P.V. | 1971 | 0.72 | | | Values obtained by comparing spectral intensities from the liquid specimen and from simulated graphite black body. |
| 4* T74089 | Baum, B.A., et al. | 1971 | 0.66 | 1973, 1973 | | Similar to the above specimen. |
| 5 T16961 | Stierwalt, D.L. | 1961 | 3.8 | 333-433 | | n-type, single crystal; 2.03 mm thick; both surfaces ground and polished; measured in vacuum using modified Beckman IR-3 spectrophotometer; resistivity 30-60 ohm-cm; data extracted from spectral curves roughly. |
| 6 T16961 | Stierwalt, D.L. | 1961 | 5.0 | 333-433 | | The above specimen. |
| 7 T16961 | Stierwalt, D.L. | 1961 | 10.6 | 333-433 | | The above specimen. |
| 8 T16961 | Stierwalt, D.L. | 1961 | 3.8 | 313-433 | | p-type, single crystal; 1.68 mm thick; ground and polished on both surfaces; measured in vacuum using modified Beckman IR-3 spectrophotometer; data extracted from spectral curves. |
| 9 T16961 | Stierwalt, D.L. | 1961 | 5.0 | 313-433 | | The above specimen. |
| 10 T16961 | Stierwalt, D.L. | 1961 | 10.6 | 313-433 | | The above specimen. |
| 11 T41640 | Sato, T. | 1967 | 2.8 | 543-1073 | | n-type, phosphorous doped, single crystal disk with 28 mm diameter and 1.77 mm thickness; resistivity 15 ohm-cm; ground and polished plane parallel using metallographic and optical techniques; measured under 10^{-4} mm Hg to preclude oxidation; data extracted from spectral curves. |
| 12 T41640 | Sato, T. | 1967 | 5.0 | 543-1073 | | The above specimen. |
| 13 T41640 | Sato, T. | 1967 | 3.8 | 543-1073 | | The above specimen. |
| 14 T41640 | Sato, T. | 1967 | 10.6 | 543-1073 | | The above specimen. |
| 15 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 2.8 | 323-473 | | p-type, single crystal; 1.68 mm thick; resistivity 30 ohm-cm; cut to size with ultrasonic tool; optical surfaces prepared using standard lapping and polishing techniques; not etched; data extracted from spectral curves. |
| 16 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 3.8 | 323-473 | | The above specimen. |
| 17 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 5.0 | 323-473 | | The above specimen. |
| 18 T32537 | Stierwalt, D.L. and Potter, R.F. | 1962 | 10.6 | 323-473 | | The above specimen. |

* Not shown in figure.

TABLE 12-6. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|------------------------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|
| CURVE 1 $\lambda = 0.65$ | | | | | | | | | |
| 1000. | 0.64 | 1623. | 0.684 | 413. | 0.355 | 543. | 0.067 | 373. | 0.026 |
| 1100. | 0.62 | 1677. | 0.684 | 433. | 0.376 | 623. | 0.179 | 423. | 0.028 |
| 1200. | 0.60 | 1680. | 0.245 | CURVE 8 | | 693. | 0.379 | 473. | 0.033 |
| 1300. | 0.57 | 1687. | 0.235 | $\lambda = 3.8$ | | 743. | 0.593 | CURVE 17 | |
| 1400. | 0.54 | 1846. | 0.235 | 313. | 0.023 | 793. | 0.680 | $\lambda = 5.0$ | |
| 1500. | 0.50 | CURVE 4 | | 353. | 0.024 | 873. | 0.716 | 323. | 0.016 |
| 1600. | 0.48 | $\lambda = 0.66$ | | 393. | 0.026 | 1073. | 0.716 | 373. | 0.022 |
| 1688. | 0.46 | 1373. | 0.69 | 433. | 0.028 | CURVE 13 | | 423. | 0.030 |
| CURVE 2 $\lambda = 0.65$ | | | | | | | | | |
| 1000. | 0.759 | 1973. | 0.23 | CURVE 9 | | $\lambda = 3.8$ | | 473. | 0.030 |
| 1025. | 0.759 | CURVE 5 | | 543. | 0.061 | CURVE 10 | | $\lambda = 10.6$ | |
| 1050. | 0.759 | $\lambda = 3.8$ | | 623. | 0.144 | $\lambda = 10.6$ | | | |
| 1075. | 0.759 | 333. | 0.609 | 693. | 0.294 | | | | |
| 1100. | 0.756 | 353. | 0.009 | 743. | 0.504 | | | 0.238 | |
| 1125. | 0.755 | 373. | 0.014 | 793. | 0.634 | | | 0.254 | |
| 1150. | 0.755 | 413. | 0.014 | 873. | 0.714 | | | 0.205 | |
| 1175. | 0.755 | 433. | 0.014 | 1073. | 0.714 | | | 0.315 | |
| 1200. | 0.755 | CURVE 10 | | $\lambda = 10.6$ | | | | | |
| 1225. | 0.755 | 313. | 0.259 | CURVE 14 | | | | | |
| 1250. | 0.755 | 353. | 0.279 | $\lambda = 10.6$ | | | | | |
| 1275. | 0.753 | 393. | 0.298 | 693. | 0.627 | | | | |
| 1300. | 0.751 | 433. | 0.324 | 743. | 0.716 | | | | |
| 1325. | 0.751 | CURVE 11 | | 793. | 0.716 | | | | |
| 1350. | 0.751 | $\lambda = 2.8$ | | 873. | 0.716 | | | | |
| 1375. | 0.750 | | | 1073. | 0.716 | | | | |
| 1400. | 0.750 | 333. | 0.011 | CURVE 15 | | | | | |
| 1425. | 0.750 | 353. | 0.011 | $\lambda = 2.8$ | | | | | |
| 1450. | 0.750 | 373. | 0.011 | 543. | 0.057 | | | | |
| 1475. | 0.750 | 393. | 0.012 | 623. | 0.128 | | | | |
| 1500. | 0.749 | 413. | 0.012 | 693. | 0.243 | | | | |
| 1525. | 0.749 | 433. | 0.012 | 743. | 0.453 | | | | |
| 1550. | 0.747 | CURVE 7 | | 793. | 0.581 | | | | |
| 1575. | 0.747 | $\lambda = 10.6$ | | 873. | 0.712 | | | | |
| 1600. | 0.747 | 333. | 0.310 | 1073. | 0.712 | | | | |
| CURVE 16 (CONT.) | | | | | | | | | |
| 1600. | 0.747 | 353. | 0.322 | CURVE 16 | | | | | |
| | | 373. | 0.333 | $\lambda = 3.8$ | | | | | |
| | | 393. | 0.349 | 323. | 0.022 | | | | |

c. Normal Spectral Reflectance (Wavelength Dependence)

Twenty-four experimental data sets for the wavelength dependence (1-14 μm) of the normal spectral reflectance of silicon are shown in Table 12-9 and Figure 12-7. All of the measurements were made at room temperature for single crystal specimens. Of the 24 data sets, 8 sets are for specimens of relatively high purity.

The recommended values for 330 K shown in Table 12-7 and Figure 12-6 were calculated from the recommended values for the normal spectral emittance at 330 K by use of the McMahon [T20468] relations (Eq. 2.6-10 to 2.6-12). Equation 2.6-12 for the normal spectral emittance, ϵ , can be rearranged to yield

$$ad = \ln \left(\frac{1 - R - R\epsilon}{1 - \epsilon - R} \right) \quad (4.12-1)$$

where a is the absorption coefficient, d is the thickness, and R is the single surface reflectance of a plane-parallel specimen. As discussed in the previous sections, the single surface reflectance (i. e., the reflectance of an opaque specimen) of silicon near room temperature is 0.30 in the 2-15 μm range. Using this value, and the recommended emittance values, ad was calculated from Eq. 4.12-1 and used in the McMahon relation (Eq. 2.6-11) to determine the normal spectral reflectance. The 330 K values are applicable to a 2 mm thick, silicon single crystal of relatively high purity and resistivity.

In the 1.5-8 μm wavelength range, the 330 K recommended values agree with the data of Vasilev, et al. [T49418] (curve 24) and Fray, et al. [T41607] (curves 20, 21) to within 5% and with the data of Sato [T41640] (curve 22) to within 10%. These investigators did not specify the thickness of their samples. In this wavelength range, the normal spectral emittance is quite low and the normal spectral reflectance approaches the 0.46 value predicted by the McMahon relations for negligible absorption and emission. It is worthwhile to note that the 0.46 value is accurate to within 15% for any specimen whose emittance is 0.20 or less. According to measurements by Stierwalt [T32537] (curves 8, 9 of Section 4.12.a), this criteria is satisfied in the 2-6.5 μm range by specimens as thick as 13 mm, so the recommended values are applicable to a rather wide range of thicknesses in the 2-6.5 μm range. In the 1.5-8 μm range, the uncertainty of the 330 K recommended values should not exceed $\pm 10\%$. In the 8-14 μm wavelength range, there is no experimental reflectance data which can be meaningfully compared with the recommended values. However, the uncertainty of the values in this range is believed to be no greater than $\pm 15\%$. The uncertainty may be greater in the 9 μm region due to differences between crystals in the bulk oxygen content.

The 1075 K recommended values were obtained from the normal spectral emittance data of Sato [T41640] (curve 45 of Section 4.12.a). Silicon of ordinary purity is opaque in the 2-15 μm region at this high temperature, because of absorption due to free carriers, and the sum of the normal spectral emittance and the normal spectral reflectance is unity. The values are applicable to plane-parallel, polished, silicon single crystals of relatively high purity and of any thickness. The uncertainty of the 1075 K recommended values is believed to be within $\pm 10\%$ in the 2-15 μm wavelength range.

For applications as infra-red optical components, silicon is often coated with other materials designed to reduce reflection losses in specified wavelength ranges. The thermal radiative properties of these systems of silicon plus anti-reflection coatings may be markedly different from those of silicon alone. Surface oxide layers produced by high temperature atmospheric heating of silicon also alter the reflectance properties, as shown by curves 22 and 23 by Sato [T41640].

The reflectance of silicon may change greatly when it is strongly excited by laser radiation. Bobrova, et al. [T76806] measured the reflectance at 10.6 μm of a high resistivity silicon specimen under excitation by a ruby laser (0.6943 μm). They found that the reflectance first decreased from 0.30 to 0.19, and then increased to 0.50 as the excitation intensity was increased. The minimum reflectance occurred at an excitation intensity of about 10^{24} kW cm⁻² s⁻¹. Birnbaum and Stocker [A000029] found that the reflectance at around 0.5 μm (argon-ion laser) of a silicon specimen under excitation by a ruby laser increased by as much as 60%. Other investigators [A000031, T77096, T36227, T35800, T36304] have observed similar changes in silicon and other semiconductors. Gauster and Bushnell [T37021] and Reintjes and McGroddy [T77510] have observed related increases in the absorption of silicon when excited by laser radiation. These effects have been attributed both to the presence of a thin metallic surface layer produced by melting and to the presence of a high concentration of non-equilibrium charge carriers generated by the laser radiation.

TABLE 12-7. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T , K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|----------------|---------|-----------|---------|-----------|--------|-----------|---------|
| SINGLE CRYSTAL | | | | | | | |
| 2.0 MM THICK | | | | | | | |
| T = 330 | | | | | | | |
| 1.00 | 0.3358† | 8.20 | 0.426 | 12.10 | 0.343 | 1.00 | 0.336A† |
| 1.10 | 0.4208 | 8.30 | 0.422 | 12.20 | 0.339 | 1.50 | 0.313A |
| 1.20 | 0.4468 | 8.40 | 0.412 | 12.30 | 0.341 | 2.00 | 0.307A |
| 1.30 | 0.453 | 8.50 | 0.401A† | 12.40 | 0.343 | 2.80 | 0.288 |
| 1.40 | 0.456 | 8.60 | 0.389A | 12.50 | 0.342 | 3.00 | 0.286 |
| 1.50 | 0.457 | 8.70 | 0.371A | 12.60 | 0.340 | 3.80 | 0.286 |
| 1.60 | 0.457 | 8.80 | 0.348A | 12.70 | 0.336 | 4.00 | 0.286 |
| 1.70 | 0.457 | 8.90 | 0.332A | 12.80 | 0.334 | 4.50 | 0.285 |
| 1.80 | 0.458 | 9.00 | 0.325A | 12.90 | 0.333 | 5.00 | 0.284 |
| 1.90 | 0.458 | 9.10 | 0.325A | 13.00 | 0.332 | 6.00 | 0.284 |
| 2.00 | 0.458 | 9.20 | 0.336A | 13.10 | 0.331 | 7.00 | 0.284 |
| 2.20 | 0.458 | 9.30 | 0.360A | 13.20 | 0.329 | 8.00 | 0.284 |
| 2.40 | 0.458 | 9.40 | 0.339 | 13.30 | 0.327 | 9.00 | 0.284 |
| 2.60 | 0.458 | 9.50 | 0.406 | 13.40 | 0.325 | 10.00 | 0.284 |
| 2.80 | 0.458 | 9.60 | 0.408 | 13.50 | 0.323 | 10.60 | 0.284 |
| 3.00 | 0.458 | 9.70 | 0.405 | 13.60 | 0.324 | 11.00 | 0.284 |
| 3.80 | 0.458 | 9.80 | 0.398 | 13.70 | 0.330 | 12.00 | 0.284 |
| 4.00 | 0.458 | 9.90 | 0.392 | 13.80 | 0.337 | 13.00 | 0.287 |
| 5.00 | 0.458 | 10.00 | 0.385 | 13.90 | 0.348 | 14.00 | 0.288 |
| 5.50 | 0.457 | 10.10 | 0.377 | 14.00 | 0.363 | 15.00 | 0.290 |
| 5.85 | 0.453 | 10.20 | 0.370 | | | | |
| 6.00 | 0.454 | 10.30 | 0.364 | | | | |
| 6.20 | 0.454 | 10.40 | 0.363 | | | | |
| 6.40 | 0.453 | 10.50 | 0.364 | | | | |
| 6.60 | 0.448 | 10.60 | 0.364 | | | | |
| 6.80 | 0.433 | 10.70 | 0.358 | | | | |
| 6.90 | 0.425 | 10.80 | 0.353 | | | | |
| 7.00 | 0.423 | 10.90 | 0.347 | | | | |
| 7.10 | 0.426 | 11.00 | 0.342 | | | | |
| 7.20 | 0.427 | 11.10 | 0.338 | | | | |
| 7.30 | 0.427 | 11.20 | 0.336 | | | | |
| 7.40 | 0.426 | 11.30 | 0.336 | | | | |
| 7.50 | 0.422 | 11.40 | 0.338 | | | | |
| 7.60 | 0.419 | 11.50 | 0.342 | | | | |
| 7.70 | 0.417 | 11.60 | 0.346 | | | | |
| 7.80 | 0.420 | 11.70 | 0.350 | | | | |
| 7.90 | 0.423 | 11.80 | 0.352 | | | | |
| 8.00 | 0.426 | 11.90 | 0.352 | | | | |
| 8.10 | 0.427 | 12.00 | 0.348 | | | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL AND BY A "B" IS TYPICAL.

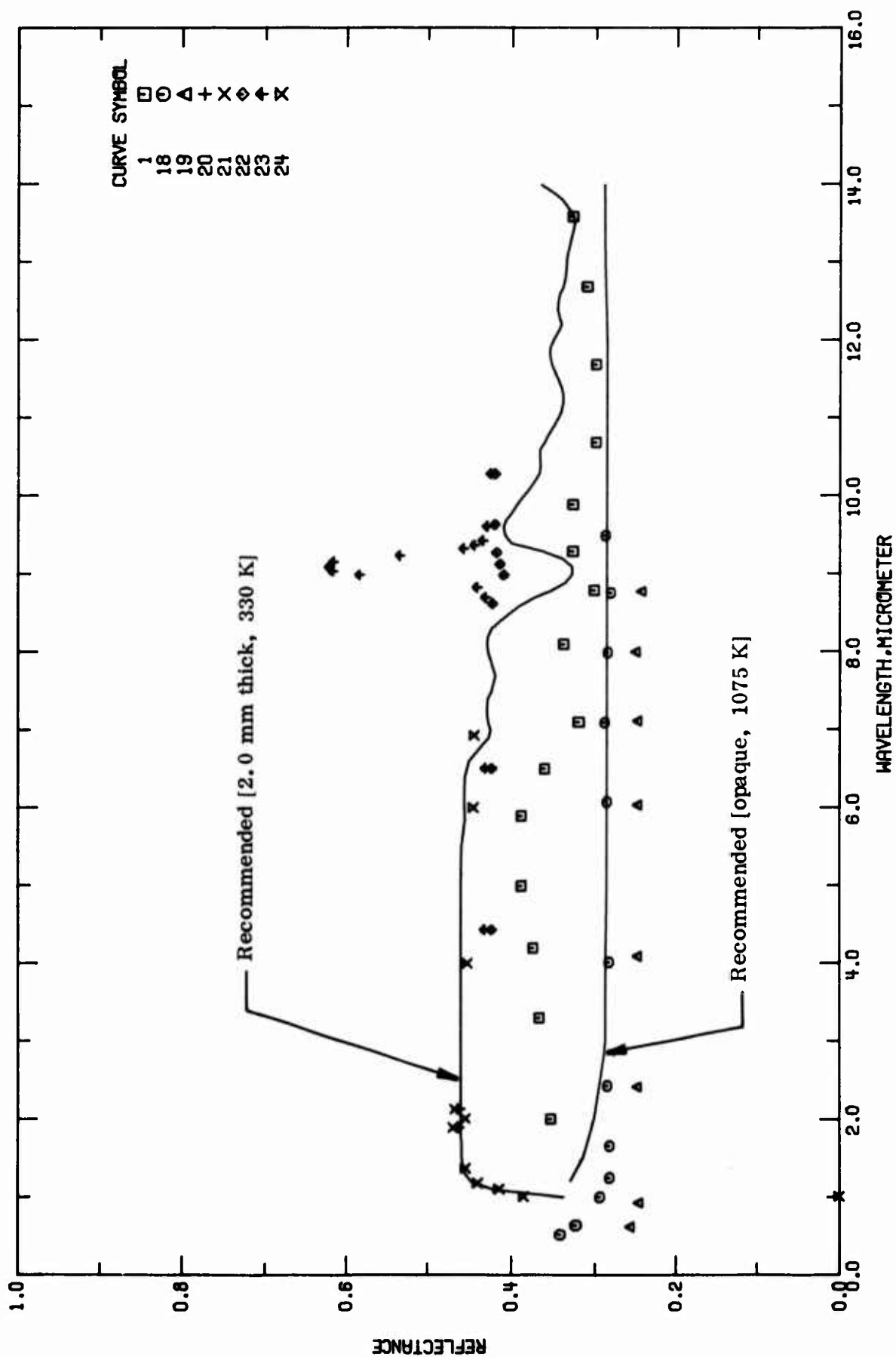


FIGURE 12-6. RECOMMENDED NORMAL SPECTRAL REFLECTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)

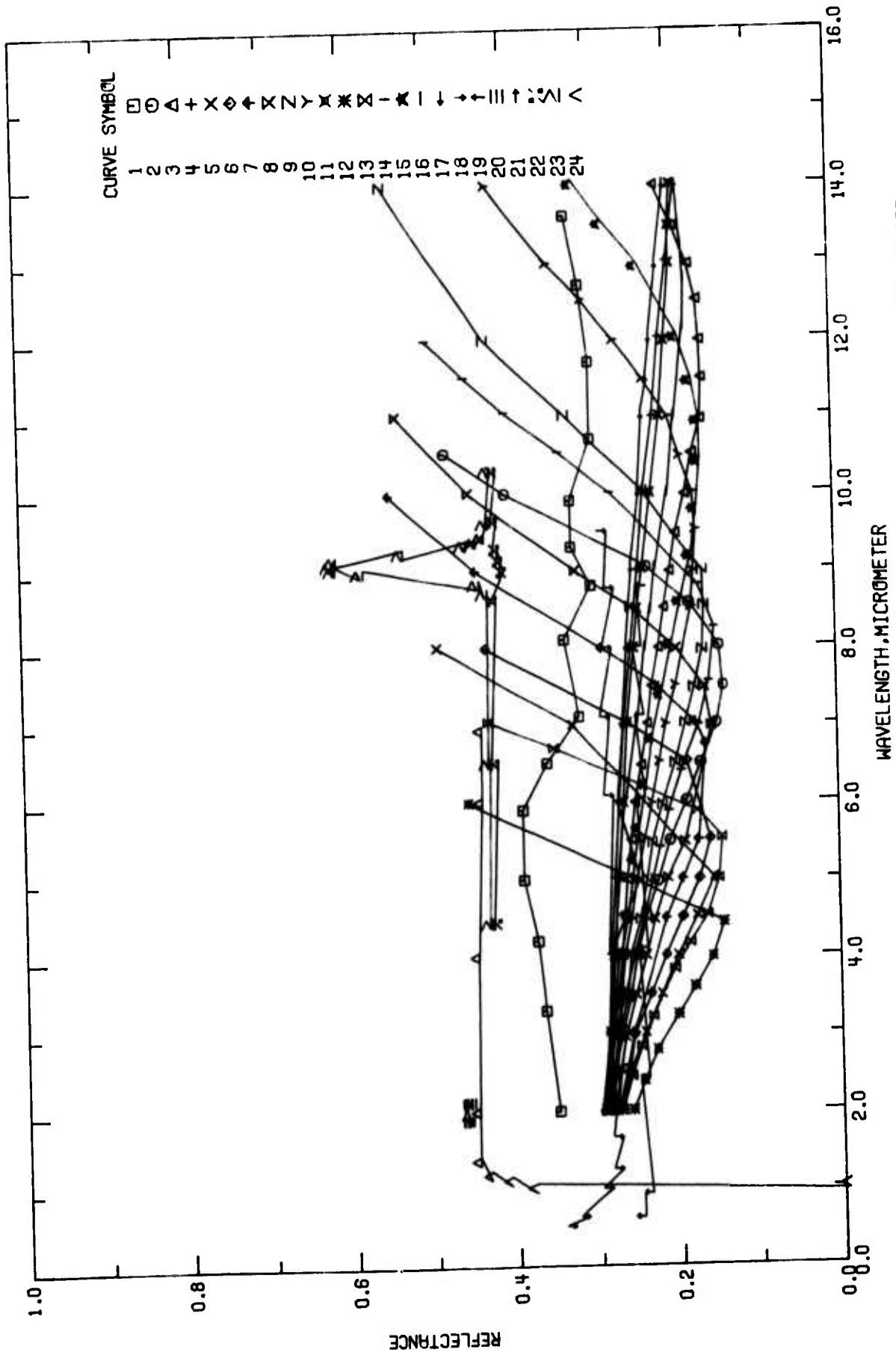


FIGURE 12-7. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON OF VARIOUS PURITY (WAVELENGTH DEPENDENCE).

TABLE 12-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T20100 | McCarthy, D.E. | 1963 | 2-50 | 293 | | 1 cm thick; both surfaces ground and polished to flatness of one fringe; measured with Beckman specular reflectance attachment with Beckman IR-5A in the 2-16 μm region and with Beckman IR-7 in the 12.5-50 μm region; compared to aluminum mirror; measurement temperature not stated explicitly, assumed to be 293 K; data extracted from smooth curve. |
| 2 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-10.5 | 293 | | Doped with antimony; carrier concentration $4.47 \times 10^{19} \text{ cm}^{-3}$; measured with a Perkin-Elmer Model 112 spectrometer; comparative standard a front surfaced aluminum mirror; data corrected for the reference mirror; measurement temperature not stated explicitly; assumed to be 293 K; data presented in figure; reproducibility: 0.5%. |
| 3 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-15 | 293 | | Similar to the above specimen except doped with antimony to a carrier concentration of $1.66 \times 10^{19} \text{ cm}^{-3}$. |
| 4 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-20 | 293 | | Similar to the above specimen except doped with antimony to a carrier concentration of $0.832 \times 10^{19} \text{ cm}^{-3}$. |
| 5 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-8 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $9.03 \times 10^{19} \text{ cm}^{-3}$. |
| 6 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-8 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $7.92 \times 10^{19} \text{ cm}^{-3}$. |
| 7 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-10 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $6.37 \times 10^{19} \text{ cm}^{-3}$. |
| 8 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-11 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $5.05 \times 10^{19} \text{ cm}^{-3}$. |
| 9 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-14 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $3.48 \times 10^{19} \text{ cm}^{-3}$. |
| 10 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-14 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $2.84 \times 10^{19} \text{ cm}^{-3}$. |
| 11 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-14 | 293 | | Similar to the above specimen except doped with arsenic to a carrier concentration of $0.877 \times 10^{19} \text{ cm}^{-3}$. |
| 12 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-20 | 293 | | Similar to the above specimen except doped with phosphorus to a carrier concentration of $16.7 \times 10^{19} \text{ cm}^{-3}$. |
| 13 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-7 | 293 | | Similar to the above specimen except doped with phosphorus to a carrier concentration of $10.22 \times 10^{19} \text{ cm}^{-3}$. |
| 14 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-12 | 293 | | Similar to the above specimen except doped with phosphorus to a carrier concentration of $4.38 \times 10^{19} \text{ cm}^{-3}$. |
| 15 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-15 | 293 | | Similar to the above specimen except doped with phosphorus to a carrier concentration of $2.03 \times 10^{19} \text{ cm}^{-3}$. |
| 16 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-20 | 293 | | Similar to the above specimen except doped with phosphorus to a carrier concentration of $1.37 \times 10^{19} \text{ cm}^{-3}$. |
| 17 T29605 | Howarth, L.E. and Gilbert, J.F. | 1963 | 2-20 | 293 | | Similar to the above specimen except doped with phosphorus to a carrier concentration of $0.74 \times 10^{19} \text{ cm}^{-3}$. |

TABLE 12-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 18 T22741 | Coblentz, W. W. | 1911 | 0.5-9.5 | 293 | b | Specimen from Kahlbaum; quite homogeneous; polished using fine grade of emery paper covered with mixture of tin oxide and graphite; measured using fluorite prism, mirror spectrometer, and vacuum bolometer; compared with silvered glass mirror; crystal of a bluish color; data presented in figure; measurement temperature not stated explicitly, assumed to be 293 K; reported error 1-3%. |
| 19 T22741 | Coblentz, W. W. | 1911 | 0.6-8.8 | 293 | a | Specimen from Carborundum Co.; less homogeneous, more porous, poorer polish, harder than the above specimen; polishing and measurement techniques similar to those of the above specimen. |
| 20 T41607 | Fray, S. J., Goodwin, A. R., Johnson, F. A., and Quarrington, J. E. | 1963 | 1.886, 2.119 | 293 | | Pure, plane parallel specimen; special apparatus measured reflectance and transmittance simultaneously; absorption negligible; optical constants calculated; precision better than 1%; each point represents separate measurement. |
| 21 T41607 | Fray, S. J., et al. | 1963 | 1.886, 2.119 | 293 | | Calculated from known refractive index data. |
| 22 T41640 | Sato, T. | 1966 | 4.4-10.3 | 293 | | n-type, phosphor doped single crystal; optically polished and plane parallel; source radiation split into reference and test beams; aluminumized mirror of known reflectivity used as standard; incident beam chopped at 10 cycle per sec; measured under 10^{-4} mm Hg to prevent oxidation; measurement temperature not stated explicitly, assumed to be 293 K; $\theta = 4^\circ$. |
| 23 T41640 | Sato, T. | 1966 | 4.4-10.3 | 293 | | The above specimen measured after heating in atmosphere, oxidation shown by Reststrahlen of Si-O at $9 \mu\text{m}$. |
| 24 T45418 | Vasil'ev, A. M., Golovner, T. M., Landsman, A. P., and Lidorenko, N. S. | 1967 | | 293 | | Undoped disc specimen cut from rod with free carrier concentration of 10^{17}cm^{-3} ; polished on both sides; measured with IKS-14 spectrometer with reflection attachment; measurement temperature not stated explicitly, assumed to be 293 K. |

TABLE 12-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μM ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 11 (CONT.) | | | CURVE 14 (CONT.) | | | CURVE 17 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 23 (CONT.) | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|----------|-----------|------------------|-----------|----------|------------------|--------|--|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
| CURVE 11 (CONT.) | | | CURVE 14 (CONT.) | | | CURVE 17 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 23 (CONT.) | | |
| 10.00 | 0.235 | 5.67 | 0.203 | 2.00 | 0.297 | 15.72 | 0.195 | 1.006 | 0.4605 | 10.29 | 0.423 | CURVE 24 | | |
| 20.00 | 0.293 | 6.33 | 0.193 | 3.03 | 0.267 | 16.15 | 0.195 | 1.006 | 0.4619 | T = 293. | | T = 293. | | |
| CURVE 12 | | | CURVE 15 | | | CURVE 18 | | | CURVE 21 | | | CURVE 22 | | |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | |
| 2.00 | 0.250 | 10.00 | 0.275 | 10.00 | 0.249 | 16.74 | 0.202 | 1.006 | 0.4674 | 1.00 | 0.384 | CURVE 24 | | |
| 2.38 | 0.245 | 10.53 | 0.335 | 10.99 | 0.194 | 17.00 | 0.222 | 1.006 | 0.4654 | 1.10 | 0.413 | T = 293. | | |
| 2.70 | 0.224 | 11.05 | 0.401 | 12.75 | 0.178 | 18.00 | 0.222 | 2.119 | 0.4622 | 1.17 | 0.438 | T = 293. | | |
| 3.23 | 0.201 | 11.51 | 0.451 | 13.20 | 0.190 | 20.00 | 0.239 | 2.119 | 0.4581 | 2.00 | 0.452 | T = 293. | | |
| 3.59 | 0.181 | 12.00 | 0.497 | 14.50 | 0.186 | CURVE 19 | | | 4.00 | 0.450 | T = 293. | | | |
| 3.94 | 0.159 | CURVE 15 | | | 15.00 | 0.194 | T = 293. | | | 6.00 | 0.443 | T = 293. | | |
| 4.42 | 0.144 | 2.00 | 0.294 | 2.00 | 0.277 | 0.51 | 0.339 | 4.43 | 0.422 | 6.93 | 0.442 | T = 293. | | |
| 6.00 | 0.455 | 3.05 | 0.242 | 3.05 | 0.272 | 0.63 | 0.321 | 6.50 | 0.422 | CURVE 23 | | | | |
| CURVE 13 | | | 4.32 | 0.277 | 4.32 | 0.269 | 0.99 | 0.293 | 8.99 | 0.408 | T = 293. | | | |
| T = 293. | | | 4.51 | 0.265 | 4.51 | 0.259 | 1.24 | 0.280 | 10.29 | 0.416 | T = 293. | | | |
| 2.00 | 0.274 | 5.64 | 0.253 | 5.64 | 0.243 | 2.42 | 0.283 | 4.43 | 0.422 | T = 293. | | | | |
| 2.44 | 0.262 | 6.23 | 0.243 | 6.23 | 0.234 | 4.01 | 0.284 | 6.50 | 0.422 | T = 293. | | | | |
| 2.92 | 0.249 | 6.90 | 0.234 | 6.90 | 0.221 | 6.07 | 0.284 | 8.99 | 0.422 | T = 293. | | | | |
| 3.21 | 0.233 | 7.37 | 0.221 | 7.37 | 0.207 | 7.09 | 0.287 | 9.13 | 0.412 | T = 293. | | | | |
| 3.92 | 0.215 | 8.01 | 0.207 | 8.01 | 0.195 | 7.99 | 0.283 | 9.20 | 0.416 | T = 293. | | | | |
| 4.16 | 0.196 | 8.57 | 0.195 | 8.57 | 0.182 | 8.76 | 0.279 | 9.64 | 0.416 | T = 293. | | | | |
| 4.52 | 0.165 | 9.16 | 0.142 | 9.16 | 0.175 | 9.59 | 0.286 | 10.29 | 0.416 | T = 293. | | | | |
| 4.99 | 0.153 | 9.77 | 0.175 | 9.77 | 0.170 | 9.61 | 0.254 | 4.43 | 0.430 | T = 293. | | | | |
| 5.52 | 0.145 | 10.34 | 0.170 | 10.34 | 0.170 | 0.61 | 0.243 | 6.50 | 0.429 | T = 293. | | | | |
| 5.97 | 0.175 | 11.43 | 0.170 | 11.43 | 0.170 | 0.92 | 0.245 | 8.70 | 0.429 | T = 293. | | | | |
| 6.70 | 0.353 | 12.00 | 0.244 | 12.00 | 0.194 | 2.41 | 0.245 | 8.03 | 0.439 | T = 293. | | | | |
| 7.05 | 0.428 | 13.48 | 0.285 | 13.48 | 0.285 | 4.09 | 0.245 | 8.99 | 0.503 | T = 293. | | | | |
| CURVE 14 | | | 14.00 | 0.320 | 14.00 | 0.242 | 7.11 | 0.245 | 9.64 | 0.615 | T = 293. | | | |
| T = 293. | | | 14.97 | 0.397 | 14.97 | 0.236 | 8.00 | 0.247 | 9.64 | 0.619 | T = 293. | | | |
| 2.00 | 0.293 | 11.49 | 0.229 | 11.49 | 0.229 | 8.00 | 0.247 | 9.16 | 0.614 | T = 293. | | | | |
| 2.99 | 0.282 | 12.00 | 0.224 | 12.00 | 0.224 | 8.70 | 0.240 | 9.24 | 0.532 | T = 293. | | | | |
| 3.50 | 0.268 | 12.96 | 0.214 | 12.96 | 0.214 | 9.33 | 0.245 | 9.33 | 0.455 | T = 293. | | | | |
| 4.02 | 0.256 | 14.00 | 0.202 | 14.00 | 0.202 | 9.37 | 0.242 | 9.37 | 0.442 | T = 293. | | | | |
| 4.59 | 0.241 | 14.94 | 0.197 | 14.94 | 0.197 | 9.43 | 0.240 | 9.43 | 0.432 | T = 293. | | | | |
| 5.40 | 0.221 | CURVE 19 | | | 14.94 | 0.197 | 9.61 | 0.240 | 9.61 | 0.427 | T = 293. | | | |
| CURVE 19 | | | T = 293. | | | CURVE 19 | | | T = 293. | | | T = 293. | | |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | |

d. Normal Spectral Absorptance (Wavelength Dependence)

No experimental data for the normal spectral absorptance of silicon have been reported as such. However, Kirchhoff's law, stating that the absorptance of a specimen is equal to its emittance, is valid for normal spectral properties. Consequently, the values recommended for the normal spectral emittance of silicon in Section 4.12.a are repeated in Table 12-10 and Figure 12-8. The 330 K recommended values apply to a 2 mm thick, n-type single crystal of relatively high purity and resistivity. The 1075 K recommended values are applicable to relatively pure, high resistivity, single crystal silicon of any thickness. The uncertainties of the tabulated values were discussed in Section 4.12.a.

TABLE 12-10. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α | λ | α |
|---|---|---|--|----------------|----------|-----------|----------|
| SINGLE CRYSTAL 2.0 MM THICK T = 330 | SINGLE CRYSTAL 2.0 MM THICK T = 330 (CONT.) | SINGLE CRYSTAL 2.0 MM THICK T = 330 (CONT.) | SINGLE CRYSTAL 2.0 MM THICK T = 1075 | SINGLE CRYSTAL | | | |
| 1.00 | 0.565 | 6.20 | 0.104 | 12.10 | 0.390 | 1.00 | 0.664 |
| 1.10 | 0.575 | 6.30 | 0.114 | 12.20 | 0.410 | 1.50 | 0.687 |
| 1.20 | 0.2208† | 6.40 | 0.146 | 12.30 | 0.397 | 2.00 | 0.703 |
| 1.30 | 0.0248 | 6.50 | 0.1799† | 12.40 | 0.369 | 2.50 | 0.712 |
| 1.40 | 0.0178 | 6.60 | 0.2207 | 12.50 | 0.391 | 3.00 | 0.714 |
| 1.50 | 0.0148 | 6.70 | 0.2608 | 12.60 | 0.403 | 3.80 | 0.714 |
| 1.60 | 0.0138 | 6.80 | 0.3669 | 12.70 | 0.417 | 4.00 | 0.714 |
| 1.70 | 0.012A | 6.90 | 0.4358 | 12.80 | 0.427 | 4.50 | 0.715 |
| 1.80 | 0.011A | 9.00 | 0.4728 | 12.90 | 0.433 | 5.00 | 0.716 |
| 1.90 | 0.011A | 9.10 | 0.4708 | 13.00 | 0.439 | 6.00 | 0.716 |
| 2.00 | 0.010A | 9.20 | 0.4208 | 13.10 | 0.443 | 7.00 | 0.716 |
| 2.20 | 0.010A | 9.30 | 0.3208 | 13.20 | 0.451 | 8.00 | 0.716 |
| 2.40 | 0.009A | 9.40 | 0.1888 | 13.30 | 0.460 | 9.00 | 0.716 |
| 2.60 | 0.009A | 9.50 | 0.155 | 13.40 | 0.470 | 10.00 | 0.716 |
| 2.80 | 0.009A | 9.60 | 0.158 | 13.50 | 0.482 | 10.60 | 0.716 |
| 3.00 | 0.009A | 9.70 | 0.169 | 13.60 | 0.478 | 11.00 | 0.716 |
| 3.80 | 0.009A | 9.80 | 0.190 | 13.70 | 0.446 | 12.00 | 0.716 |
| 4.00 | 0.009A | 9.90 | 0.210 | 13.80 | 0.414 | 13.00 | 0.713 |
| 5.00 | 0.019A | 10.00 | 0.234 | 13.90 | 0.367 | 14.00 | 0.712 |
| 5.50 | 0.013A | 10.10 | 0.260 | 14.00 | 0.310 | 15.00 | 0.710 |
| 5.85 | 0.024 | 10.20 | 0.284 | | | | |
| 6.00 | 0.022 | 10.30 | 0.305 | | | | |
| 6.20 | 0.021 | 10.40 | 0.309 | | | | |
| 6.40 | 0.023 | 10.50 | 0.306 | | | | |
| 6.60 | 0.038 | 10.60 | 0.308 | | | | |
| 6.80 | 0.083 | 10.70 | 0.329 | | | | |
| 6.90 | 0.105 | 10.80 | 0.350 | | | | |
| 7.00 | 0.112 | 10.90 | 0.373 | | | | |
| 7.10 | 0.104 | 11.00 | 0.394 | | | | |
| 7.20 | 0.100 | 11.10 | 0.410 | | | | |
| 7.30 | 0.100 | 11.20 | 0.417 | | | | |
| 7.40 | 0.104 | 11.30 | 0.417 | | | | |
| 7.50 | 0.116 | 11.40 | 0.409 | | | | |
| 7.60 | 0.125 | 11.50 | 0.392 | | | | |
| 7.70 | 0.130 | 11.60 | 0.375 | | | | |
| 7.80 | 0.122 | 11.70 | 0.358 | | | | |
| 7.90 | 0.113 | 11.80 | 0.350 | | | | |
| 8.00 | 0.103 | 11.90 | 0.350 | | | | |
| 8.10 | 0.100 | 12.00 | 0.368 | | | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL AND BY A "B" IS TYPICAL.

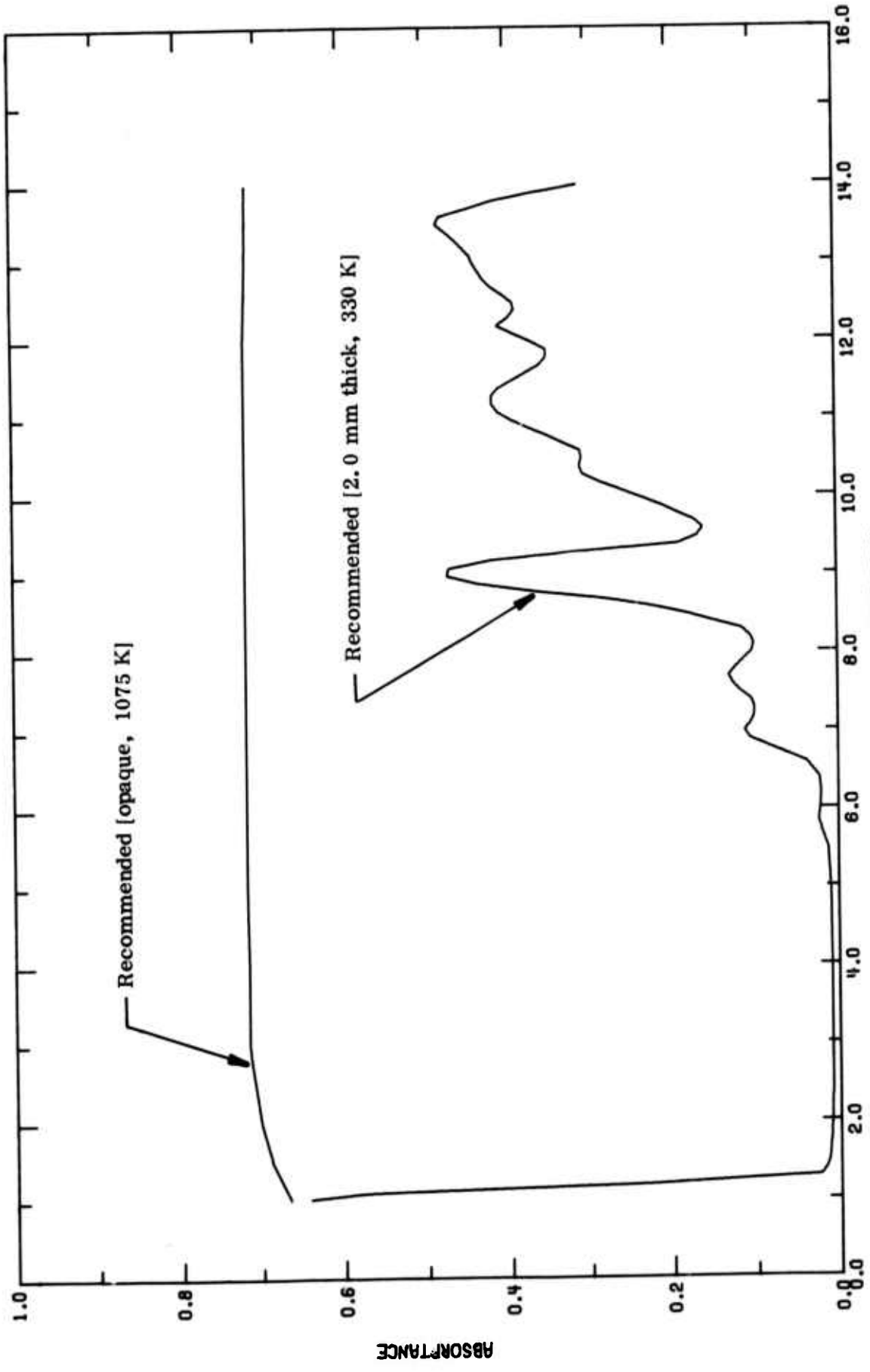


FIGURE 12-8. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)

e. Normal Spectral Absorptance (Temperature Dependence)

No experimental data for the temperature dependence of the normal spectral absorptance of silicon have been reported as such. However Kirchhoff's law, stating that the absorptance of a specimen is equal to its emittance, is valid for normal spectral properties. Consequently, the values recommended for the normal spectral emittance of silicon in Section 4.12.b are repeated in Table 12-11 and Figure 12-9. As discussed in Section 4.12.b, the tabulated values are applicable only to samples about 2 mm thick, at the lower temperatures. Above about 800 K, however, the values are applicable to polished, high resistivity, single crystals of any thickness because of silicon's high temperature opacity. The values above 1100 K are extrapolated. The uncertainties of the tabulated values were discussed in Section 4.12.b.

TABLE 12-11. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| T | α | T | α | T | α | T | α |
|-----------------|----------|-------|----------|-------|----------|-------|----------|
| SINGLE CRYSTAL | | | | | | | |
| 2 MM THICK | | | | | | | |
| $\lambda = 2.0$ | | | | | | | |
| 300. | 0.0288† | 300. | 0.0128† | 300. | 0.0110† | 300. | 0.265 |
| 350. | 0.0328 | 350. | 0.0178 | 350. | 0.0158 | 325. | 0.280 |
| 400. | 0.0378 | 400. | 0.0218 | 400. | 0.0198 | 350. | 0.296 |
| 425. | 0.0398 | 425. | 0.0239 | 425. | 0.0219 | 375. | 0.313 |
| 450. | 0.0418 | 450. | 0.0258 | 450. | 0.0248 | 400. | 0.330 |
| 475. | 0.0428 | 475. | 0.0268 | 475. | 0.0278 | 425. | 0.346 |
| 500. | 0.0458 | 500. | 0.0368 | 500. | 0.0378 | 450. | 0.364 |
| 520. | 0.0498 | 520. | 0.0458 | 520. | 0.0498 | 475. | 0.382 |
| 540. | 0.0568 | 540. | 0.0598 | 540. | 0.0658 | 500. | 0.400 |
| 560. | 0.0698 | 560. | 0.0748 | 560. | 0.0858 | 525. | 0.419 |
| 580. | 0.0878 | 580. | 0.0928 | 580. | 0.1098 | 550. | 0.440 |
| 600. | 0.1068 | 600. | 0.1148 | 600. | 0.1308 | 575. | 0.464 |
| 620. | 0.126 | 620. | 0.138 | 620. | 0.173 | 600. | 0.490 |
| 640. | 0.151 | 640. | 0.169 | 640. | 0.217 | 620. | 0.513 |
| 660. | 0.181 | 660. | 0.206 | 660. | 0.273 | 640. | 0.538 |
| 680. | 0.213 | 680. | 0.253 | 680. | 0.333 | 660. | 0.568 |
| 700. | 0.262 | 700. | 0.314 | 700. | 0.404 | 690. | 0.609 |
| 720. | 0.344 | 720. | 0.393 | 720. | 0.490 | 690. | 0.630 |
| 740. | 0.431 | 740. | 0.487 | 740. | 0.581 | 700. | 0.652 |
| 760. | 0.499 | 760. | 0.560 | 760. | 0.634 | 710. | 0.672 |
| 780. | 0.559 | 780. | 0.610 | 780. | 0.664 | 720. | 0.689 |
| 800. | 0.600 | 800. | 0.649 | 800. | 0.685 | 730. | 0.700 |
| 820. | 0.647 | 820. | 0.678 | 820. | 0.699 | 740. | 0.710 |
| 840. | 0.682 | 840. | 0.698 | 840. | 0.705 | 750. | 0.714 |
| 860. | 0.705 | 860. | 0.711 | 860. | 0.715 | 800. | 0.716 |
| 880. | 0.712 | 880. | 0.714 | 880. | 0.716 | 850. | 0.716 |
| 900. | 0.712 | 900. | 0.714 | 900. | 0.716 | 900. | 0.716 |
| 950. | 0.712 | 950. | 0.714 | 950. | 0.716 | 950. | 0.716 |
| 1000. | 0.712 | 1000. | 0.714 | 1000. | 0.716 | 1000. | 0.716 |
| 1050. | 0.712 | 1050. | 0.714 | 1050. | 0.716 | 1050. | 0.716 |
| 1075. | 0.712 | 1075. | 0.714 | 1075. | 0.716 | 1075. | 0.716 |
| 1400. | 0.712A | 1400. | 0.714A | 1400. | 0.716A | 1400. | 0.716A |
| 1600. | 0.712A | 1600. | 0.714A | 1600. | 0.716A | 1600. | 0.716A |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL AND BY A "B" IS TYPICAL.

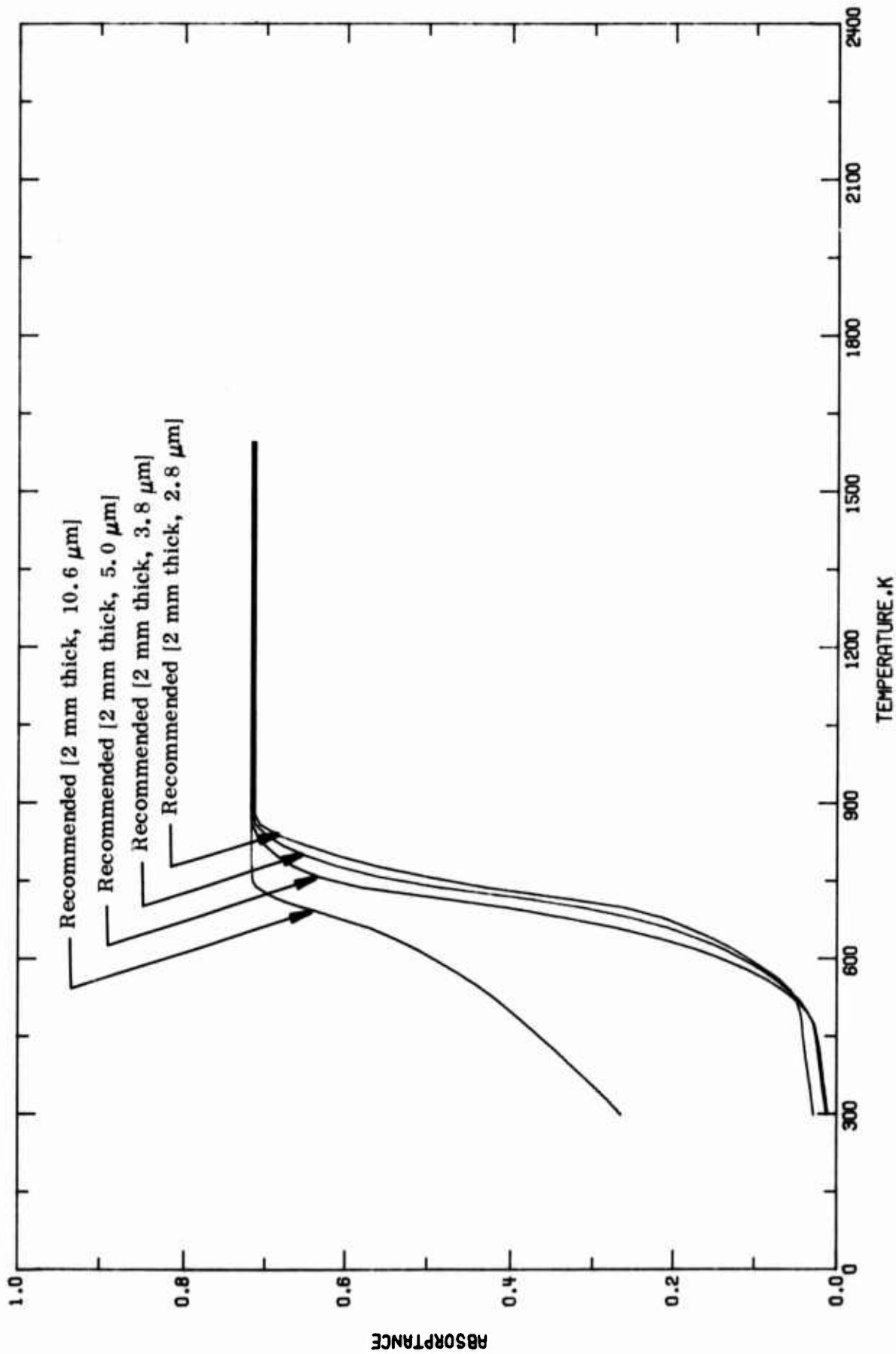


FIGURE 12-9. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF HIGH-RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)

f. Normal Spectral Transmittance (Wavelength Dependence)

Thirty-one experimental data sets for the wavelength dependence of the normal spectral transmittance of silicon covering the temperature range 20-673 K are shown in Table 12-14 and Figure 12-11. Of the 31 data sets, 27 sets are for specimens of relatively high purity.

The recommended values for 330 K shown in Table 12-12 and Figure 12-10 were calculated from the recommended values for the normal spectral emittance at 330 K by use of the McMahon [T20468] relations (Eq. 2.6-10 to 2.6-12). Equation 2.6-12 for the normal spectral emittance, ϵ , can be rearranged to yield

$$ad = \ln \left(\frac{1 - R - R\epsilon}{1 - \epsilon - R} \right) \quad (4.12-1)$$

where a is the absorption coefficient, d is the thickness, and R is the single surface reflectance of a plane-parallel specimen. As discussed in previous sections, the single surface reflectance of silicon is 0.30 in the 2-15 μm range. Using this value, and the recommended emittance values, the product ad was calculated from Eq. 4.12-1 and used in the McMahon relation (Eq. 2.6-10) to determine the normal spectral transmittance. The recommended values are applicable to a 2 mm thick, silicon single crystal of relatively high purity and resistivity.

In the 1.5-6.5 μm wavelength range, the normal spectral emittance of a 2 mm thick sample is quite low, and the normal spectral transmittance approaches the 0.54 value predicted by the McMahon relations for negligible absorption and emission and a single surface reflectance of 0.30. It is worthwhile to note that the 0.54 value is accurate to within 15% for any specimen whose emittance is 0.13 or less. According to measurements by Stierwalt [T32537] (curves 8, 9 of Section 4.12.a), this criteria is satisfied in the 2-6.5 μm range by specimens as thick as 13 mm, so the recommended values are applicable to a rather wide range of thicknesses in the 2-6.5 μm range. In the 1.5-6.5 μm range, the recommended values agree to within $\pm 5\%$ with the data of Labaw, et al. [T27345] (curve 7) for a 6.4 mm thick specimen; Cox, et al. [T46843] (curve 9) for a 1.5 mm specimen; Kraushaar [T10703] (curve 11) for a 4.16 mm specimen; Fray, et al. [T41607] (curves 15, 16); Sherman and Coleman [T64446] (curve 28); and Vasilev, et al. [T49418] (curve 30). They agree to within $\pm 10\%$ with the data of Gillespie, et al. [T20810] (curves 2, 3) for a 2.79 mm thick specimen; Kraushaar [T10703] (curve 10) for a 0.66 mm specimen; DeWaard and Weiner [T36371] (curve 19) for an 11 mm specimen; Meyer [E58966] (curve 29); and Beam, et al. [T28949] (curve 31). The uncertainty of the 330 K recommended values is believed to be within $\pm 10\%$ in the 1.5-6.5 μm wavelength range.

In the 6.5-15 μm range, absorption is no longer negligible, and the transmittance depends more strongly on the thickness of the specimen. In this region, the data of Gillespie, et al. [T20810] (curve 2) for a 2.79 mm thick specimen agrees with the recommended values to within $\pm 10\%$, as does the data of Salzberg and Villa [E3900] (curve 32). The uncertainties of the 330 K recommended values should be within $\pm 15\%$ in the 6.5-15 μm range. As mentioned previously, the values reported in the 9 μm region should be considered typical only because of large differences in the amount of oxygen occluded in the process of growing single crystals by different techniques.

TABLE 12-12. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T |
|-----------------|--------|-----------|---------|-----------|-------|
| SINGLE CRYSTAL | | | | | |
| 2.0 MM THICK | | | | | |
| T = 330 (CONT.) | | | | | |
| 1.00 | 0.008† | 6.20 | 0.470 | 12.10 | 0.267 |
| 1.10 | 0.0058 | 6.30 | 0.464 | 12.20 | 0.252 |
| 1.20 | 0.3348 | 6.40 | 0.442 | 12.30 | 0.262 |
| 1.30 | 0.523 | 6.50 | 0.420 | 12.40 | 0.268 |
| 1.40 | 0.527 | 6.60 | 0.3918† | 12.50 | 0.267 |
| 1.50 | 0.529 | 6.70 | 0.3498 | 12.60 | 0.257 |
| 1.60 | 0.530 | 6.80 | 0.2963 | 12.70 | 0.247 |
| 1.70 | 0.531 | 6.90 | 0.2339 | 12.80 | 0.239 |
| 1.80 | 0.531 | 9.00 | 0.2039 | 12.90 | 0.234 |
| 1.90 | 0.531 | 9.10 | 0.2058 | 13.00 | 0.229 |
| 2.00 | 0.532 | 9.20 | 0.2448 | 13.10 | 0.226 |
| 2.20 | 0.532 | 9.30 | 0.3209 | 13.20 | 0.220 |
| 2.40 | 0.533 | 9.40 | 0.4139 | 13.30 | 0.213 |
| 2.60 | 0.533 | 9.50 | 0.429 | 13.40 | 0.205 |
| 2.80 | 0.533 | 9.60 | 0.434 | 13.50 | 0.195 |
| 3.00 | 0.533 | 9.70 | 0.426 | 13.60 | 0.190 |
| 3.80 | 0.533 | 9.80 | 0.412 | 13.70 | 0.224 |
| 4.00 | 0.533 | 9.90 | 0.398 | 13.80 | 0.249 |
| 5.00 | 0.532 | 10.00 | 0.381 | 13.90 | 0.285 |
| 5.50 | 0.530 | 10.10 | 0.363 | 14.00 | 0.327 |
| 5.85 | 0.523 | 10.20 | 0.346 | | |
| 6.00 | 0.524 | 10.30 | 0.331 | | |
| 6.20 | 0.525 | 10.40 | 0.320 | | |
| 6.40 | 0.523 | 10.50 | 0.330 | | |
| 6.60 | 0.514 | 10.60 | 0.320 | | |
| 6.80 | 0.484 | 10.70 | 0.313 | | |
| 6.90 | 0.470 | 10.80 | 0.298 | | |
| 7.00 | 0.465 | 10.90 | 0.280 | | |
| 7.10 | 0.470 | 11.00 | 0.264 | | |
| 7.20 | 0.473 | 11.10 | 0.252 | | |
| 7.30 | 0.473 | 11.20 | 0.247 | | |
| 7.40 | 0.470 | 11.30 | 0.247 | | |
| 7.50 | 0.462 | 11.40 | 0.253 | | |
| 7.60 | 0.456 | 11.50 | 0.266 | | |
| 7.70 | 0.453 | 11.60 | 0.279 | | |
| 7.80 | 0.450 | 11.70 | 0.292 | | |
| 7.90 | 0.464 | 11.80 | 0.298 | | |
| 8.00 | 0.471 | 11.90 | 0.298 | | |
| 8.10 | 0.473 | 12.00 | 0.284 | | |

† VALUE FOLLOWED BY A "8" IS TYPICAL.

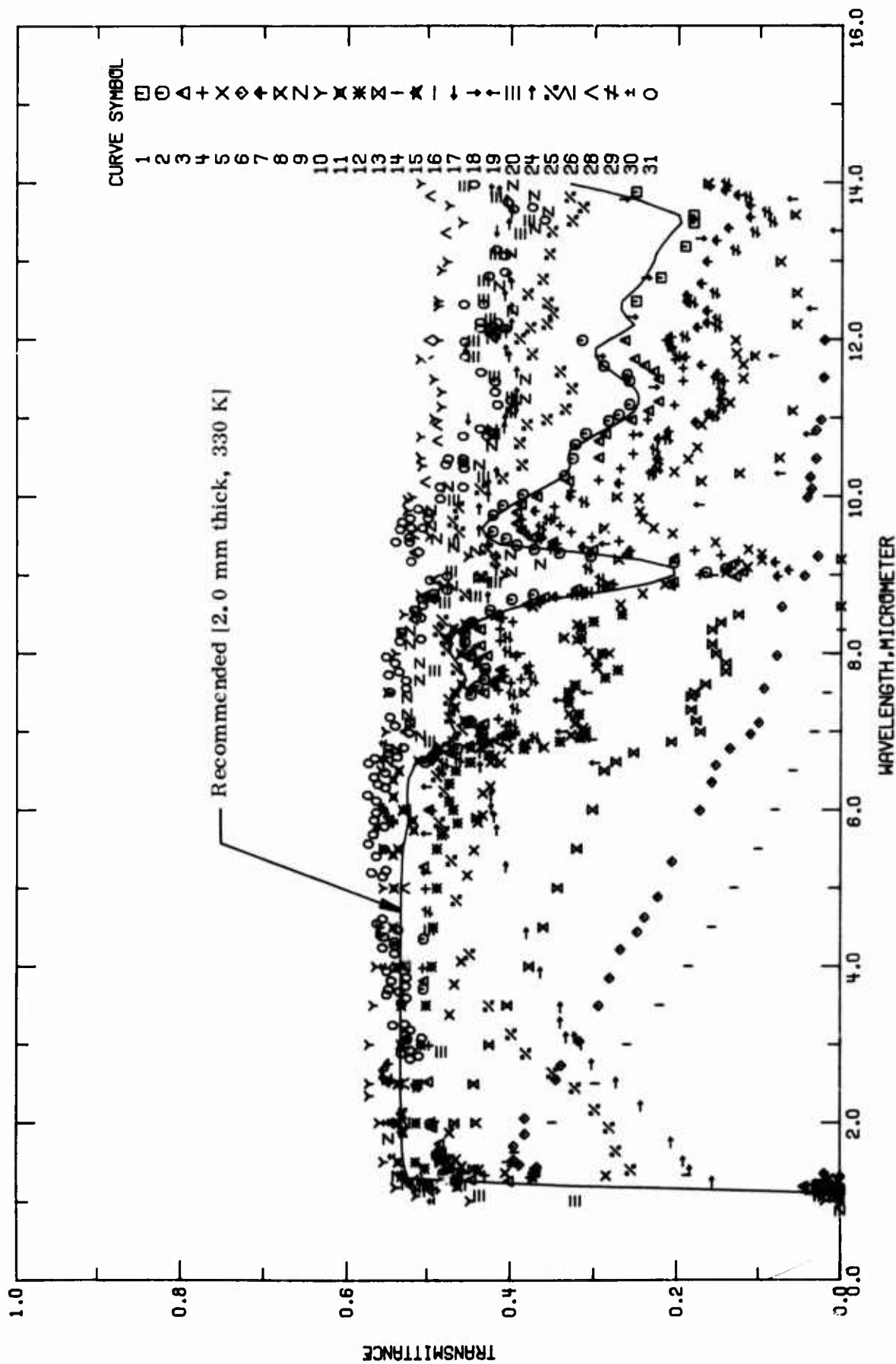


FIGURE 12-10. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH-RESISTIVITY SILICON (WAVELENGTH DEPENDENCE)

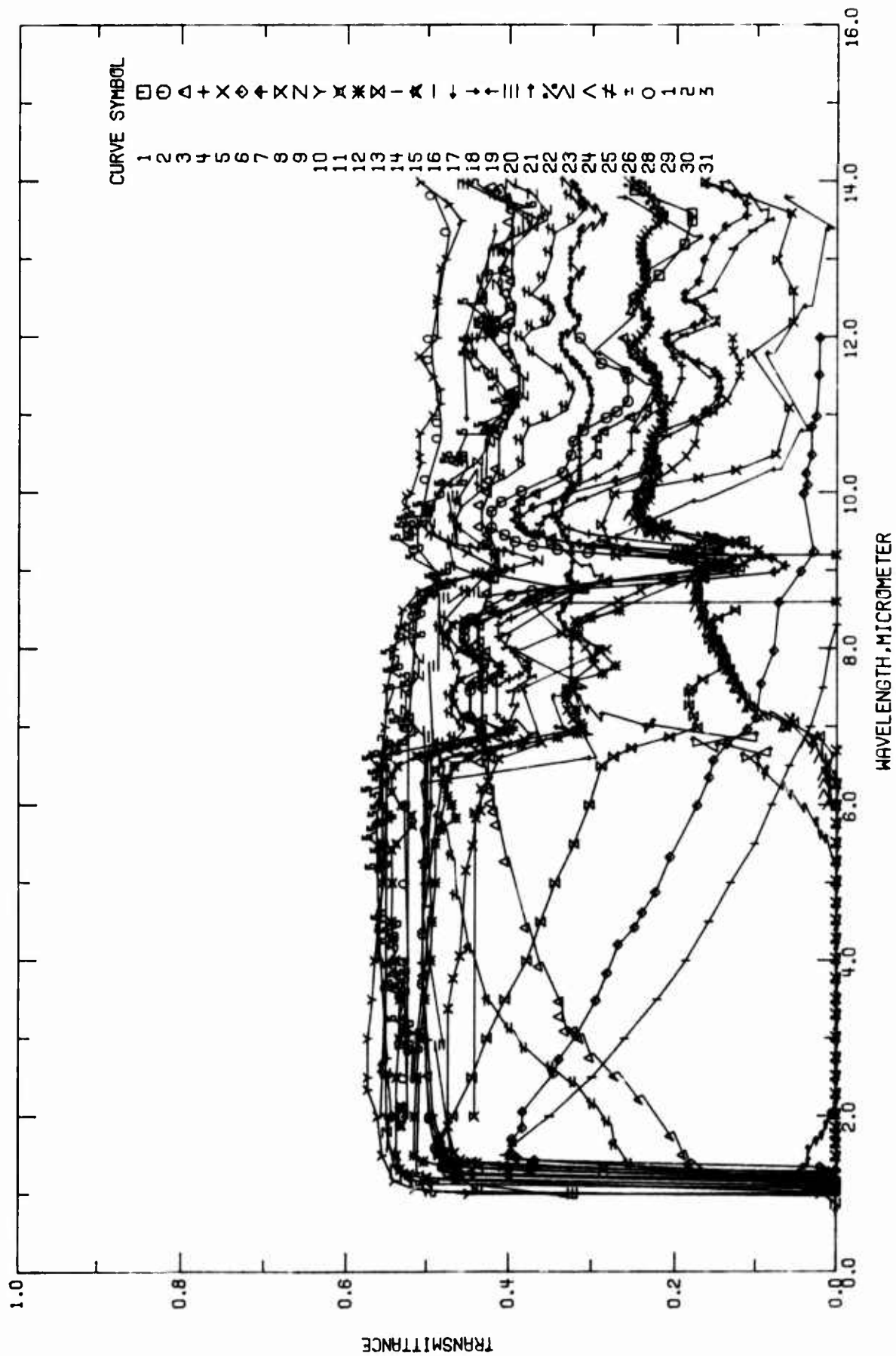


FIGURE 12-11. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON OF VARIOUS PURITIES (WAVELENGTH DEPENDENCE).

TABLE 12-13. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent) | Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|------------------------------|--|
| 1 T33154 | Lord, R.C. | 1952 | 12-40 | 293 | | | 2 mm thick; optically polished; uncorrected for reflection losses; measurement temperature not stated explicitly; assumed to be 293 K. |
| 2 T20810 | Gillespie, D.T., Lisen, A.L., and Nichols, L.W. | 1964 | 1-12 | 298 | | | N-type single crystal; 6 ppb boron and 20 ppb phosphorus; resistivity 5 ohm-cm; disk 1.240 in. diameter by 0.110 in. thick; parallelism tolerance of $\pm 2.5 \mu\text{m}$; polished faces with flatness tolerance of ± 0.0001 in.; provided by Knapp Electro-Physics, Inc.; measured using Perkin-Elmer Model 21 spectrophotometer; not corrected for reflection losses; data extracted from smoothed curve. |
| 3 T20810 | Gillespie, D.T., et al. | 1964 | 1-12 | 373 | | | The above specimen measured at 100 C; edge of sample disk about 1 C hotter than the center. |
| 4 T20810 | Gillespie, D.T., et al. | 1964 | 1-12 | 473 | | | The above specimen measured at 200 C. |
| 5 T20810 | Gillespie, D.T., et al. | 1964 | 1.3-12 | 573 | | | The above specimen measured at 300 C. |
| 6 T20810 | Gillespie, D.T., et al. | 1964 | 1.3-12 | 673 | | | The above specimen measured at 400 C; edge of sample disk about 6 C hotter than the center. |
| 7 T27345 | Labaw, K.B., Lisen, A.L., and Nichols, L.W. | 1963 | 2-15 | 293 | | | Single crystal; approx. 6 ppb boron and 20 ppb phosphorus; disk about 0.25 in. thick and 1 in. diameter; crystal supplied by Knapp Electro-Physics, Inc. and prepared by John H. Ransom Laboratories; faces polished optically flat within 5 green mercury fringes; plane parallel, with wedge angle of 0.00028 radians; measurement temperature not stated explicitly, assumed to be 293 K; data presented in figure. |
| 8 T30100 | McCarthy, D.E. | 1963 | 2-50 | 293 | | | 1 cm thick; both surfaces ground and polished to flatness of one fringe; measured with Beckman IR-5A in 2-16 μm range; measurement temperature not stated explicitly, assumed to be 293 K; data extracted from smooth curve. |
| 9 T46843 | Cox, J.T., Uass, G., and Jaccbus, G.F. | 1961 | 1-14 | 293 | | | High purity plate of 1.5 mm thickness; measured at room temperature; data extracted from smooth curve. |
| 10 T10703 | Kraushaar, R. | 1958 | 1-15 | 293 | | | Single crystal; 0.66 mm thick; data extracted from smooth curve; measurement temperature not stated explicitly, assumed to be 293 K. |
| 11 T10703 | Kraushaar, R. | 1958 | 1-8.5 | 298 | | | Single crystal silicon; 4.16 mm thick; data extracted from smooth curve. |
| 12 T10703 | Kraushaar, R. | 1958 | 1-8.5 | 573 | | | The above specimen measured at 300 C. |
| 13 T10703 | Kraushaar, R. | 1958 | 1-8.5 | 623 | | | The above specimen measured at 350 C. |
| 14 T10703 | Kraushaar, R. | 1958 | 1-8.3 | 673 | | | The above specimen measured at 400 C. |
| 15 T41607 | Frey, S.J., Goodwin, A.R., Johnson, F.A., and Quarrington, J.E. | 1963 | 1.886, 2.119 | 293 | | | Pure, plane parallel specimen; special apparatus measured reflectance and transmittance simultaneously; absorption negligible; $\tau + \rho \approx 0.99$; optical constants calculated; precision better than 1%; each point represents separate measurement. |
| 16 T41607 | Frey, S.J., et al. | 1963 | 1.886, 2.119 | 293 | | | Values calculated from known refractive index data. |
| 17 T36371 | DeVaard, R. and Weiner, S. | 1967 | 5-35 | 293 | | | Uncoated, high purity; 1 mm thick. |
| 18 T36371 | DeVaard, R. and Weiner, S. | 1967 | 5-35 | 293 | | | Uncoated, high purity; 5 mm thick. |

TABLE 12-13. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Designation of Specimen | Composition (weight per cent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|----------------------------------|---|
| 19 T36371 | DeWaard, R. and Weiner, S. | 1967 | 5-35 | 293 | | Uncoated, high purity; 11 mm thick. |
| 20 T35846 | Linsteadt, G.F. | 1965 | 1-15 | 50 | | 1.02 mm thick and 1.27 cm in diameter; Perkin-Elmer Model 221 spectrophotometer with NaCl optics used; measurement temperature is approximate. |
| 21 T71403 | Morgan, H.T. | 1972 | 1-14 | 20 | Sample L-1 | Be doped, p-type, single crystal specimen from Langley Research Center, NASA; resistivity 0.46 $\Omega\text{-cm}$; 0.5 to 4 mm thick and 2.2 to 2.6 cm in diameter; plane-parallel and polished to mirror finish using yellow rouge compound; measured with dual beam Perkin-Elmer Model 13 spectrometer; measurement temperature approximate. |
| 22 T71403 | Morgan, H.T. | 1972 | 1.2-14.2 | 20 | Sample 858-33-2 | Similar to the above specimen but with a resistivity of 0.35 $\Omega\text{-cm}$. |
| 23 T71403 | Morgan, H.T. | 1972 | 1.2-14.2 | 20 | Sample 855-22 | Similar to the above specimen but with a resistivity of 0.40 $\Omega\text{-cm}$. |
| 24 T71403 | Morgan, H.T. | 1972 | 1-15 | 290 | Sample HT-1 | Single crystal, slightly p-type; resistivity 10,000 $\Omega\text{-cm}$; 0.5 to 4 mm thick and 2.2 to 2.6 cm in diameter; boules produced by float zone technique obtained from Monsanto Co.; plane parallel and polished to mirror finish with yellow rouge compound; measured with dual beam Perkin-Elmer Model 13 spectrometer; measurement temperature approximate. |
| 25 T71403 | Morgan, H.T. | 1972 | 2-32 | 290 | Sample M-500-P-7 | Similar to the above specimen but p-type with a resistivity of 500 $\Omega\text{-cm}$. |
| 26 T23974 | Cox, J.I. | 1961 | 2-6 | 293 | | Uncoated silicon plate. |
| 27 T23974 | Cox, J.I. | 1961 | 2-6 | 293 | | Silicon plate vacuum coated with $\text{MgF}_2 + \text{ZnS}$ on both sides with the ZnS layer on the outside. |
| 28 T64446 | Sherman, G.H. and Coeman, P.D. | 1971 | 2.5-50 | 293 | | Optically polished specimen 10 mil thick; resistivity 3 ohm-cm; Beckman IR-12 spectrometer in double beam mode used; measurement temperature not stated explicitly, assumed to be 293 K. |
| 29 E56966 | Meyer, M.D. | 1965 | 1-14 | 293 | | n-type, und-formed, annealed specimen; 1 ohm-cm resistivity; optically polished and plane parallel; measured in air at room temperature using Beckman IR-IV spectrophotometer. |
| 30 T49418 | Vasiliev, A.M., Colovner, T.M., Landsman, A.F., and Lidorenko, N.S. | 1967 | | 293 | | Undoped, disc specimen cut from rod with free carrier concentration of 10^{16} cm^{-3} ; polished on both sides; measured with an IKS-14 spectrometer; measurement temperature not stated explicitly, assumed to be 293 K. |
| 31 T29549 | Baum, K.E., Fahrig, R.H., Medcal, W.E., Powderly, J.E., and Roderique, J.S. | 1962 | 2.5-15 | 293 | | Uncoated silicon; measurement temperature not stated explicitly, assumed to be 293 K. |

TABLE 12-14. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF VARIED PURITY SILICON (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 1 | | | CURVE 2 (CONT.) | | | CURVE 3 (CONT.) | | | CURVE 4 (CONT.) | | | CURVE 5 | | |
|-----------|-------|--------|-----------------|-------|----------|-----------------|-------|--------|-----------------|----------|--------|-----------|------|--------|
| λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ |
| T = 293. | | | | | | | | | | | | | | |
| 12.5 | 0.25 | 0.038 | 10.61 | 0.310 | 6.45 | 0.414 | 1.41 | 0.458 | 10.55 | 0.254 | | | | |
| 12.8 | 0.22 | 0.463 | 11.37 | 0.293 | 8.62 | 0.380 | 1.54 | 0.475 | 10.79 | 0.254 | | | | |
| 13.2 | 0.19 | 0.472 | 11.05 | 0.271 | 8.72 | 0.359 | 2.01 | 0.490 | 10.98 | 0.236 | | | | |
| 13.5 | 0.18 | 0.479 | 11.18 | 0.259 | 8.82 | 0.321 | 2.98 | 0.497 | 11.17 | 0.204 | | | | |
| 13.6 | 0.14 | 0.487 | 11.48 | 0.258 | 8.87 | 0.283 | 3.97 | 0.505 | 11.48 | 0.193 | | | | |
| 13.9 | 0.25 | 0.495 | 11.56 | 0.261 | 8.91 | 0.283 | 4.99 | 0.502 | 11.64 | 0.193 | | | | |
| 14.3 | 0.36 | 0.504 | 11.67 | 0.289 | 8.98 | 0.129 | 5.99 | 0.494 | 11.75 | 0.203 | | | | |
| 14.7 | 0.32 | 0.504 | 12.00 | 0.314 | 9.04 | 0.121 | 6.63 | 0.494 | 12.00 | 0.214 | | | | |
| 15.2 | 0.30 | 0.502 | CURVE 3 | | | 9.13 | 0.135 | 6.73 | 0.468 | CURVE 5 | | | | |
| 15.6 | 0.27 | 0.492 | T = 373. | | | 9.21 | 0.204 | 6.85 | 0.474 | T = 573. | | | | |
| 16.1 | 0.05 | 0.463 | 1.12 | 0.003 | 9.27 | 0.261 | 6.92 | 0.490 | | | | | | |
| 16.4 | 0.03 | 0.433 | 1.16 | 0.011 | 9.32 | 0.302 | 6.96 | 0.394 | | | | | | |
| 16.7 | 0.05 | 0.447 | 1.19 | 0.044 | 9.42 | 0.349 | 7.00 | 0.394 | | | | | | |
| 17.2 | 0.18 | 0.447 | 1.25 | 0.401 | 9.49 | 0.374 | 7.07 | 0.405 | | | | | | |
| 17.9 | 0.17 | 0.439 | 1.27 | 0.44E | 9.57 | 0.387 | 7.16 | 0.414 | | | | | | |
| 18.5 | 0.20 | 0.431 | 1.31 | 0.462 | 9.66 | 0.393 | 7.53 | 0.414 | | | | | | |
| 19.2 | 0.20 | 0.430 | 1.42 | 0.462 | 9.80 | 0.393 | 7.62 | 0.399 | | | | | | |
| 19.4 | 0.14 | 0.447 | 1.52 | 0.472 | 9.90 | 0.387 | 7.67 | 0.387 | | | | | | |
| 20.0 | 0.25 | 0.454 | 1.73 | 0.484 | 10.00 | 0.369 | 7.72 | 0.377 | | | | | | |
| 20.8 | 0.28 | 0.454 | 1.94 | 0.484 | 10.20 | 0.330 | 7.84 | 0.377 | | | | | | |
| 21.7 | 0.37 | 0.446 | 1.96 | 0.493 | 10.50 | 0.295 | 7.96 | 0.393 | | | | | | |
| 22.7 | 0.36 | 0.424 | 2.52 | 0.498 | 10.71 | 0.295 | 8.16 | 0.412 | | | | | | |
| 23.8 | 0.36 | 0.390 | 3.81 | 0.504 | 10.80 | 0.287 | 8.31 | 0.412 | | | | | | |
| 25.0 | 0.36 | 0.372 | 5.27 | 0.504 | 10.98 | 0.256 | 8.40 | 0.397 | | | | | | |
| 26.3 | 0.37 | 0.165 | 6.00 | 0.498 | 11.10 | 0.235 | 8.75 | 0.326 | | | | | | |
| 27.8 | 0.37 | 0.141 | 6.64 | 0.499 | 11.22 | 0.223 | 8.88 | 0.277 | | | | | | |
| 29.4 | 0.37 | 0.203 | 7.73 | 0.474 | 11.50 | 0.223 | 9.00 | 0.173 | | | | | | |
| 31.3 | 0.37 | 0.304 | 8.39 | 0.474 | 11.60 | 0.229 | 9.09 | 0.135 | | | | | | |
| 33.3 | 0.38 | 0.341 | 8.85 | 0.450 | 11.69 | 0.240 | 9.19 | 0.126 | | | | | | |
| 34.5 | 0.39 | 0.371 | 8.88 | 0.434 | 11.76 | 0.252 | 9.25 | 0.147 | | | | | | |
| 35.7 | 0.39 | 0.392 | 9.95 | 0.410 | 12.00 | 0.264 | 9.31 | 0.179 | | | | | | |
| 37.8 | 0.37 | 0.405 | 7.10 | 0.432 | CURVE 4 | | | 9.43 | 0.271 | | | | | |
| 38.5 | 0.36 | 0.421 | 7.49 | 0.432 | T = 473. | | | 9.46 | 0.402 | | | | | |
| | | | | | | | | | | | | | | |
| CURVE 2 | | | CURVE 3 | | | CURVE 4 | | | CURVE 5 | | | CURVE 6 | | |
| T = 298. | | | | | | | | | | | | | | |
| 1.09 | 0.000 | 0.322 | 9.30 | 0.43E | 1.29 | 0.000 | 10.21 | 0.295 | 7.04 | 0.313 | 7.04 | 0.322 | 7.04 | 0.322 |
| 1.13 | 0.010 | 0.335 | 7.97 | 0.428 | 1.22 | 0.015 | 10.37 | 0.327 | 7.22 | 0.329 | 7.22 | 0.329 | 7.22 | 0.329 |
| | | 0.385 | 7.69 | 0.412 | 1.33 | 0.330 | 10.47 | 0.327 | 7.46 | 0.329 | 7.46 | 0.329 | 7.46 | 0.329 |
| | | 0.409 | 7.69 | 0.412 | 1.36 | 0.456 | 10.21 | 0.295 | 7.59 | 0.322 | 7.59 | 0.322 | 7.59 | 0.322 |
| | | 10.03 | 7.97 | 0.412 | | | 10.36 | 0.269 | 7.81 | 0.297 | 7.81 | 0.297 | 7.81 | 0.297 |
| | | 10.27 | 7.97 | 0.335 | | | | | | | | | | |
| | | 10.49 | 9.10 | 0.428 | | | | | | | | | | |
| | | 13.57 | 9.30 | 0.322 | | | | | | | | | | |

TABLE 12-14. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF VARIOUS PURITY SILICON (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| CURVE 22 (CONT.) | | CURVE 22 (CONT.) | | CURVE 22 (CONT.) | | CURVE 23 | | CURVE 23 (CONT.) | | CURVE 24 (CONT.) | |
|------------------|-------|------------------|-------|------------------|-------|---------------------|-------|------------------|-------|------------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 1.85 | 0.000 | 9.93 | 0.172 | 11.61 | 0.231 | CURVE 23 T = 20. | | 9.55 | 0.236 | 6.92 | 0.433 |
| 2.02 | 0.000 | 8.91 | 0.167 | 11.64 | 0.235 | 6.00 | 9.005 | 9.60 | 0.210 | 7.04 | 0.437 |
| 2.28 | 0.000 | 8.90 | 0.167 | 11.72 | 0.241 | 6.14 | 5.010 | 9.66 | 0.245 | 7.90 | 0.443 |
| 2.51 | 0.000 | 9.06 | 0.146 | 11.81 | 0.241 | 6.29 | 0.910 | 9.73 | 0.251 | 8.04 | 0.443 |
| 2.75 | 0.000 | 9.13 | 0.156 | 11.87 | 0.253 | 6.39 | 0.911 | 9.79 | 0.246 | 8.39 | 0.443 |
| 3.01 | 0.000 | 9.16 | 0.189 | 11.93 | 0.253 | 6.60 | 0.516 | 9.85 | 0.240 | 8.72 | 0.427 |
| 3.30 | 0.000 | 9.23 | 0.183 | 11.98 | 0.247 | 6.72 | 0.021 | 9.93 | 0.240 | 8.91 | 0.427 |
| 3.50 | 0.000 | 9.28 | 0.190 | 12.03 | 0.241 | 6.80 | 0.033 | 10.02 | 0.240 | 9.07 | 0.417 |
| 3.77 | 0.000 | 9.33 | 0.146 | 12.08 | 0.236 | 6.88 | 0.018 | 10.09 | 0.231 | 9.24 | 0.417 |
| 4.02 | 0.000 | 9.37 | 0.125 | 12.20 | 0.232 | 7.00 | 0.061 | 10.16 | 0.231 | 9.37 | 0.427 |
| 4.28 | 0.000 | 9.44 | 0.167 | 12.24 | 0.232 | 7.05 | 0.050 | 10.26 | 0.231 | 9.47 | 0.427 |
| 4.52 | 0.000 | 9.46 | 0.211 | 12.33 | 0.236 | 7.14 | 0.085 | 10.30 | 0.231 | 9.57 | 0.438 |
| 4.74 | 0.000 | 9.51 | 0.232 | 12.41 | 0.246 | 7.25 | 0.106 | 10.38 | 0.231 | 9.85 | 0.438 |
| 5.02 | 0.000 | 9.59 | 0.211 | 12.47 | 0.251 | 7.37 | 0.111 | CURVE 24 | | | 0.427 |
| 5.28 | 0.000 | 9.65 | 0.236 | 12.52 | 0.246 | 7.52 | 0.121 | T = 290. | | | 0.427 |
| 5.51 | 0.000 | 9.72 | 0.242 | 12.55 | 0.242 | 7.62 | 0.076 | 1.05 | 0.012 | 10.01 | 0.400 |
| 5.76 | 0.000 | 9.80 | 0.241 | 12.64 | 0.242 | 7.74 | 0.131 | 1.24 | 0.156 | 10.16 | 0.407 |
| 5.99 | 0.000 | 9.85 | 0.237 | 12.71 | 0.236 | 7.87 | 0.136 | 1.38 | 0.183 | 10.31 | 0.417 |
| 6.27 | 0.000 | 9.92 | 0.231 | 12.80 | 0.237 | 7.96 | 0.140 | 1.50 | 0.191 | 10.75 | 0.417 |
| 6.37 | 0.007 | 10.00 | 0.231 | 12.90 | 0.237 | 8.10 | 0.146 | 1.74 | 0.206 | 11.60 | 0.406 |
| 6.51 | 0.012 | 10.08 | 0.231 | 12.94 | 0.237 | 8.23 | 0.155 | 2.21 | 0.243 | 11.79 | 0.402 |
| 6.69 | 0.000 | 10.16 | 0.226 | 13.01 | 0.241 | 8.32 | 0.160 | 2.51 | 0.273 | 11.87 | 0.406 |
| 6.82 | 0.029 | 10.21 | 0.222 | 13.09 | 0.242 | 8.40 | 0.165 | 3.00 | 0.314 | 12.10 | 0.406 |
| 7.00 | 0.063 | 10.33 | 0.222 | 13.17 | 0.242 | 8.55 | 0.170 | 3.09 | 0.322 | 12.21 | 0.399 |
| 7.10 | 0.058 | 10.38 | 0.226 | 13.25 | 0.241 | 8.65 | 0.170 | 3.20 | 0.339 | 12.41 | 0.399 |
| 7.13 | 0.096 | 10.44 | 0.232 | 13.32 | 0.237 | 8.76 | 0.176 | 3.47 | 0.339 | 12.72 | 0.399 |
| 7.25 | 0.108 | 10.52 | 0.232 | 13.37 | 0.233 | 8.85 | 0.162 | 3.92 | 0.363 | 12.82 | 0.402 |
| 7.38 | 0.118 | 10.60 | 0.232 | 13.46 | 0.223 | 8.91 | 0.166 | 4.42 | 0.380 | 13.48 | 0.402 |
| 7.50 | 0.124 | 10.68 | 0.227 | 13.51 | 0.216 | 8.99 | 0.168 | 5.27 | 0.405 | 13.63 | 0.399 |
| 7.62 | 0.129 | 10.76 | 0.227 | 13.56 | 0.216 | 9.03 | 0.168 | 5.74 | 0.416 | 13.79 | 0.405 |
| 7.73 | 0.133 | 10.81 | 0.222 | 13.61 | 0.221 | 9.08 | 0.134 | 5.91 | 0.419 | 13.91 | 0.414 |
| 7.87 | 0.139 | 10.89 | 0.216 | 13.71 | 0.225 | 9.11 | 0.146 | 6.02 | 0.423 | 13.93 | 0.424 |
| 8.00 | 0.145 | 10.97 | 0.216 | 13.78 | 0.231 | 9.14 | 0.176 | 6.10 | 0.423 | 14.05 | 0.431 |
| 8.11 | 0.150 | 11.07 | 0.216 | 13.88 | 0.236 | 9.20 | 0.196 | 6.55 | 0.436 | 14.09 | 0.444 |
| 8.23 | 0.155 | 11.11 | 0.211 | 13.94 | 0.242 | 9.24 | 0.180 | 6.73 | 0.437 | 14.16 | 0.453 |
| 8.33 | 0.159 | 11.20 | 0.216 | 13.96 | 0.248 | 9.30 | 0.195 | 6.81 | 0.433 | 14.33 | 0.467 |
| 8.43 | 0.166 | 11.25 | 0.222 | 14.00 | 0.257 | 9.32 | 0.167 | 6.81 | 0.423 | 14.65 | 0.431 |
| 8.55 | 0.166 | 11.33 | 0.222 | 14.07 | 0.265 | 9.38 | 0.112 | 6.55 | 0.436 | 14.09 | 0.444 |
| 8.67 | 0.172 | 11.44 | 0.222 | 14.16 | 0.265 | 9.42 | 0.157 | 6.73 | 0.437 | 14.16 | 0.453 |
| 8.72 | 0.172 | 11.50 | 0.226 | 14.16 | 0.265 | 9.48 | 0.216 | 6.81 | 0.433 | 14.33 | 0.467 |

g. Normal Spectral Transmittance (Temperature Dependence)

The available experimental data for the temperature dependence of the normal spectral transmittance of silicon are shown in Table 12-17 and Figure 12-13. Only Gillespie, et al. [T20810] (curves 1-4) and Kraushaar [T10703] (curves 5-7) have reported the normal spectral transmittance above room temperature. The data of these curves were obtained by reading points from the spectral curves of Section 12.4.f at selected wavelengths of 2.8, 3.8, 5.0, and 10.6 μm .

In the 300-700 K temperature range, the recommended values shown in Table 12-15 and Figure 12-12 were calculated from the recommended values for the normal spectral emittance given in Section 4.12.b by use of Eq. 4.12-1 and the McMahon relation (Eq. 2.6-10), in a manner similar to that described in the preceding section. Refractive index and absorption coefficient measurements indicate that the single surface reflectance does not vary greatly with temperature, and the room temperature value of 0.30 was assumed to hold at higher temperatures. The recommended values are subject to the same restrictions as discussed in Section 4.12.b; they apply only to polished, plane-parallel, relatively pure single crystals which are about 2 mm thick.

Both the experimental data and the calculations from emittance data show that the transmittance of relatively pure silicon drops rapidly toward zero above about 600 K, for the wavelengths of interest. Above about 800 K, the 2 mm thick specimens are completely opaque. This rapid drop in transmittance with increasing temperature is the result of the thermal excitation of electrons to the conduction band, with consequent absorption due to free carriers. The experimental data exhibit a sharper drop to zero transmittance than do the calculations from emittance recommendations. The more rapid drop of the experimental data was followed in generating recommended values in the 600-800 K range.

In the 300-600 K temperature range, the uncertainty of the recommended values is believed to lie within $\pm 15\%$. At greater temperatures, the high slope of the curves as the transmittance drops rapidly to zero results in larger uncertainties.

Above 600 K, the general trend of the transmittance to zero can be accepted without reservation, but the tabulated values should be considered typical only.

TABLE 12-15. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| T | T | T | T | T | T | T | T |
|------------------|---------|------|---------|------|---------|------|---------|
| SINGLE CRYSTAL | | | | | | | |
| 2 MM THICK | | | | | | | |
| $\lambda = 10.6$ | | | | | | | |
| 300. | 0.359 | 300. | 0.531 | 300. | 0.531 | 300. | 0.520 |
| 350. | 0.337 | 350. | 0.529 | 350. | 0.527 | 350. | 0.518 |
| 400. | 0.312 | 400. | 0.526 | 400. | 0.525 | 400. | 0.514 |
| 425. | 0.300 | 425. | 0.525 | 425. | 0.524 | 425. | 0.513 |
| 450. | 0.287 | 450. | 0.523 | 450. | 0.522 | 450. | 0.512 |
| 475. | 0.273 | 475. | 0.521 | 475. | 0.520 | 475. | 0.511 |
| 500. | 0.260 | 500. | 0.514 | 500. | 0.515 | 500. | 0.509 |
| 525. | 0.245 | 520. | 0.507 | 520. | 0.509 | 520. | 0.507 |
| 550. | 0.229 | 540. | 0.496 | 540. | 0.500 | 540. | 0.502 |
| 575. | 0.210 | 560. | 0.483 | 560. | 0.490 | 560. | 0.493 |
| 600. | 0.189 | 580. | 0.467 | 580. | 0.479 | 580. | 0.482 |
| 620. | 0.170 | 600. | 0.447 | 600. | 0.464 | 600. | 0.469 |
| 640. | 0.149 | 620. | 0.424 | 620. | 0.447 | 620. | 0.456 |
| 660. | 0.123 | 640. | 0.393 | 640. | 0.426 | 640. | 0.439 |
| 680. | 0.0868† | 660. | 0.356 | 660. | 0.401 | 660. | 0.4198† |
| 690. | 0.0608 | 680. | 0.3108† | 680. | 0.3693† | 680. | 0.3968 |
| 700. | 0.0308 | 700. | 0.2578 | 700. | 0.3248 | 700. | 0.3628 |
| 706. | 0.0008 | 720. | 0.1538 | 720. | 0.2658 | 720. | 0.3028 |
| | | 740. | 0.0008 | 740. | 0.1508 | 740. | 0.2368 |
| | | 756. | | 756. | 0.0008 | 760. | 0.1208 |
| | | | | | | 775. | 0.0008 |

† VALUE FOLLOWED BY A "9" IS TYPICAL.

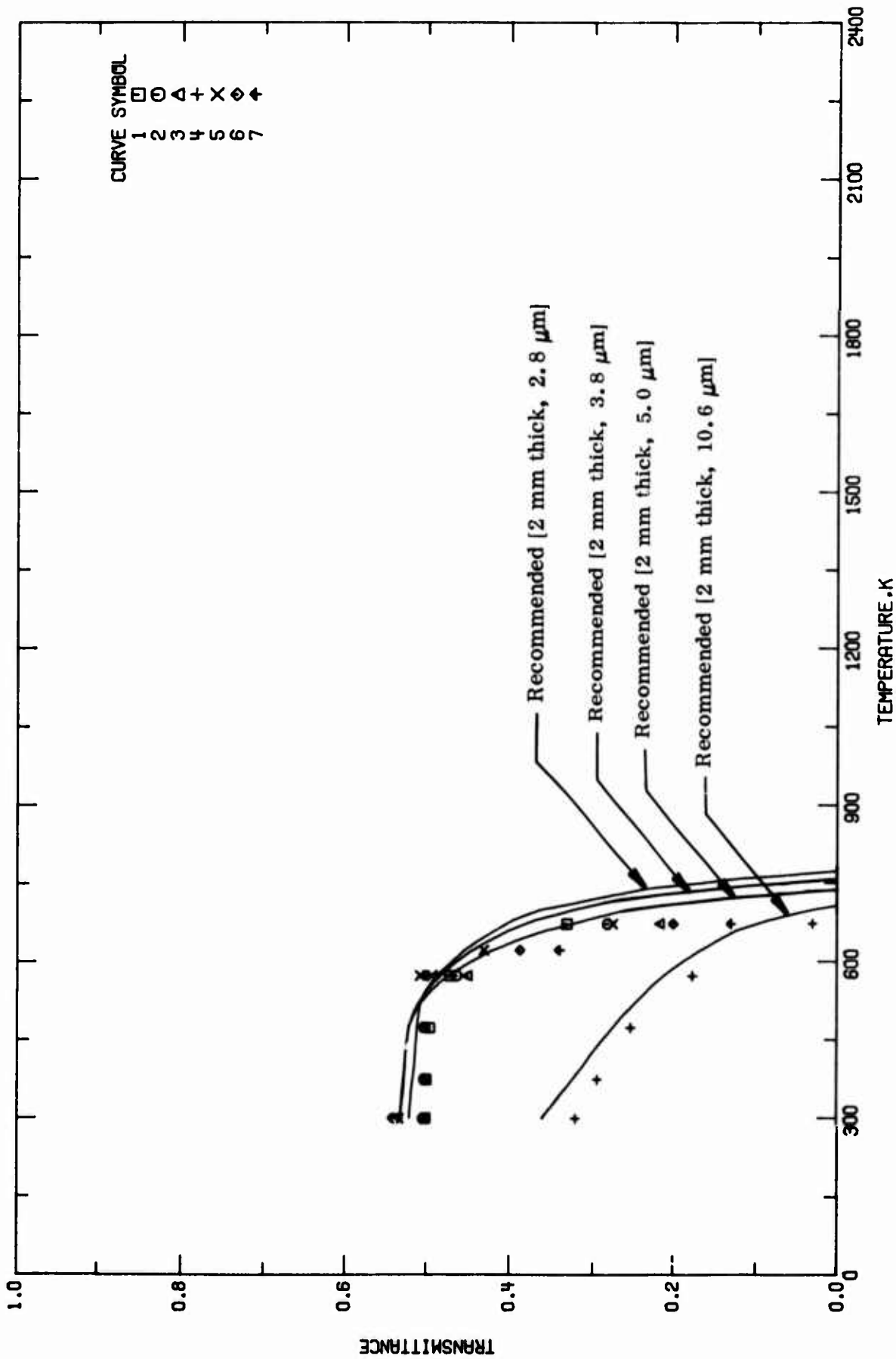


FIGURE 12-12. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF HIGH-RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)

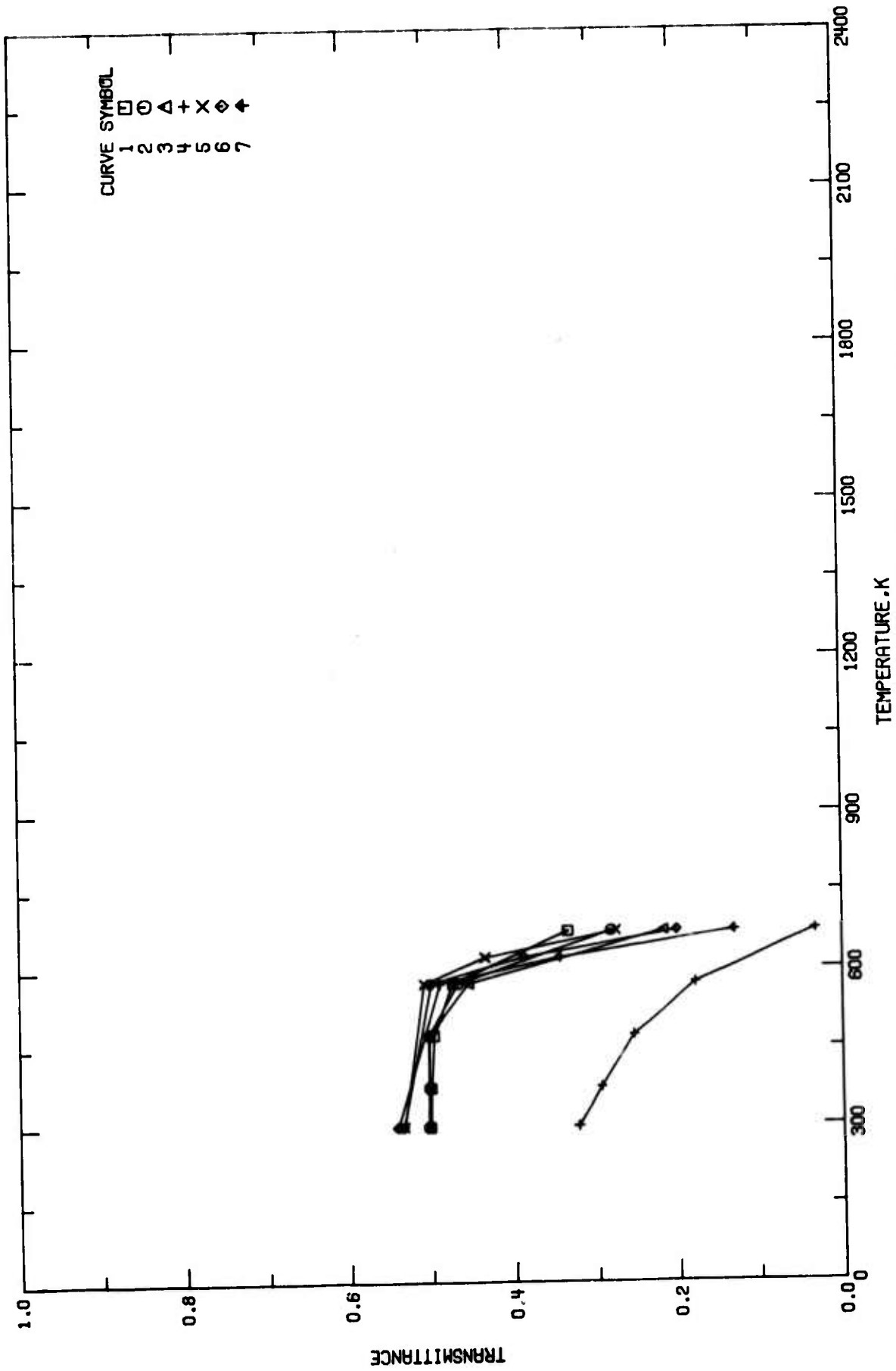


FIGURE 12-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON
(TEMPERATURE DEPENDENCE)

TABLE 12-16. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON (Temperature Dependence)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T20810 | Gillespie, D. T., Olsen, A. L., and Nichols, L. W. | 1964 | 2.8 | 298-673 | | n-type single crystal; 6 ppb boron and 20 ppb phosphorous; resistivity 5 ohm-cm; disk 0.110 in. thick and 1.240 in. in diameter; parallelism tolerance of $\pm 2.3 \mu\text{m}$; polished faces; provided by Knapp Electro-Physics, Inc.; measured using Perkin-Elmer 21 spectrophotometer; not corrected for reflection losses; data extracted from spectral curves. |
| 2 T20810 | Gillespie, D. T., et al. | 1964 | 3.8 | 298-673 | | The above specimen. |
| 3 T20810 | Gillespie, D. T., et al. | 1964 | 5.0 | 298-673 | | The above specimen. |
| 4 T20810 | Gillespie, D. T., et al. | 1964 | 10.6 | 298-673 | | The above specimen. |
| 5 T10703 | Kraushaar, R. | 1958 | 2.8 | 293-673 | | Single crystal silicon; 4.16 mm thick; data extracted from spectral curves. |
| 6 T10703 | Kraushaar, R. | 1958 | 3.8 | 293-673 | | The above specimen. |
| 7 T10703 | Kraushaar, R. | 1958 | 5.0 | 293-673 | | The above specimen. |

TABLE 12-17. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF HIGH RESISTIVITY SILICON (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| T | T | T | T |
|------------------|-------|---|---|
| CURVE 1 | | | |
| $\lambda = 2.0$ | | | |
| 290. | 0.500 | | |
| 373. | 0.499 | | |
| 473. | 0.495 | | |
| 573. | 0.471 | | |
| 673. | 0.332 | | |
| CURVE 2 | | | |
| $\lambda = 3.0$ | | | |
| 290. | 0.503 | | |
| 373. | 0.502 | | |
| 473. | 0.502 | | |
| 573. | 0.464 | | |
| 673. | 0.201 | | |
| CURVE 3 | | | |
| $\lambda = 5.0$ | | | |
| 290. | 0.503 | | |
| 373. | 0.502 | | |
| 473. | 0.502 | | |
| 573. | 0.464 | | |
| 673. | 0.201 | | |
| CURVE 4 | | | |
| $\lambda = 10.6$ | | | |
| 290. | 0.322 | | |
| 373. | 0.294 | | |
| 473. | 0.253 | | |
| 573. | 0.177 | | |
| 673. | 0.030 | | |
| CURVE 5 | | | |
| $\lambda = 2.0$ | | | |
| 290. | 0.533 | | |
| 373. | 0.507 | | |
| 473. | 0.431 | | |
| 573. | 0.533 | | |
| 673. | 0.507 | | |
| CURVE 5 (CONT.) | | | |
| 673. | 0.274 | | |
| CURVE 6 | | | |
| $\lambda = 3.0$ | | | |
| 290. | 0.534 | | |
| 373. | 0.490 | | |
| 473. | 0.386 | | |
| 573. | 0.200 | | |
| CURVE 7 | | | |
| $\lambda = 5.0$ | | | |
| 290. | 0.541 | | |
| 373. | 0.487 | | |
| 473. | 0.341 | | |
| 573. | 0.130 | | |

4.13. Silicon Carbide

Silicon carbide is usually fabricated by heating carbon and silica sand in an oven. The material is a bluish-black iridescent crystal with hexagonal or cubic structure. The molecular weight is 40.10. The theoretical density is 3.217 g cm^{-3} . It sublimates by decomposition at $>2400 \text{ K}$. It is one of the hardest substances in existence, measuring about 9 on Mohs scale hardness. Its fiber has a tensile strength of 3,000,000 psi. The thermal conductivity of a very pure and very dense silicon carbide specimen is comparable to that of metals in the neighborhood of room temperature. The coefficient of linear thermal expansion is about $4 \times 10^{-6} \text{ K}^{-1}$. This substance is soluble in fused alkalis, but is insoluble in water or alcohol.

Silicon carbide is widely used as high refractory material. Its high purity single crystals are used as semiconductors, especially at high temperature applications. Its fibers are used as reinforcement material with plastics.

Industries manufacture various forms of silicon carbide. One of them is carborundum. Optically, carborundum crystallites in various sizes appear from transparent to opaque, and from colorless to deep blue-black. The density ranges from 3.06 to 3.20 g cm^{-3} . It oxidizes slowly above 1273 K . It is commonly used for grinding and polishing. Globar is another form of silicon carbide which is widely used as a source of infrared energy. Its working temperature is up to 1783 K , and may be extended to 1922 K for a short period of time. The coefficient of thermal expansion is low. The structure is not affected by quick heating or abrupt cooling. Its electrical resistivity remains almost constant at above 755 K . It is an excellent material for resistors and heating elements.

a. Normal Spectral Emittance (Wavelength Dependence)

A total of 23 sets of data are available. Most of them were measured in the range of about $1 \mu\text{m}$ to $15 \mu\text{m}$. Measuring temperature ranges from 755 K to 2500 K .

All the data sets show a deep minimum at about $12.6 \mu\text{m}$, and all except the data of Blau and Jasperse [T32045] (Figure 13-2, curves 3-6) have a shallow minimum at about $9.2 \mu\text{m}$. A rather small peak is located around $10.4 \mu\text{m}$. No obvious reason is conceived to account for this difference. For many data sets the values tapered off below $3 \mu\text{m}$. This behavior was probably caused by the oxidation of the specimens and by the error in matching the temperature of the specimen and the blackbody standard [T20946]. The specimen was as thin as $100 \mu\text{m}$ (Figure 13-2, curves 16-18), but the data show no apparent differences compared to that of the thick specimens.

One curve is recommended for the Globar from Carborundum Company. The curve conforms to the data of Mitchell [T25673] (Figure 13-2, curve 9), except between 2 and 6 μm , where the curve follows the shape of Silverman's data [T00758] (Figure 13-2, curve 1) corrected by Morris [T20946]. A shallow minimum around 4 μm is interpreted as caused by a slight oxidation of the specimen in normal circumstances, i. e., the specimen has never been heated in air at elevated temperature over an extended period. The values are recommended for the specimen temperature of 1400 K. Two parallel curves were generated for room temperature and 2400 K. The values at 1400 K are believed to be accurate to within 5% of the true values. For other temperatures, the same set of values are believed to have an uncertainty of 5 to 10% above 700 K, and 10 to 15% below 700 K.

One more curve is presented as provisional for a roughly polished bulk specimen. The curve follows the data of Stewart and Richman [T08277, T40798] (Figure 13-2, curves 11-14 and 19-22). Since the specimens are not well-defined, the values cannot be applied accurately to any polished specimen. The provisional values are applicable to averagely polished specimens at 1000 K, and two parallel curves were generated for room temperature and 2400 K. The uncertainty of these values may be up to 20 to 30% for some specimens.

For thin films with thickness in the order of 10^{-1} μm or thinner, they have very low emittance values between 1 and 15 μm . No recommendation is made due to lack of data.

The recommended and the provisional curves are shown in Figure 13-1 and the experimental curves are shown in Figure 13-2. The recommended values, the experimental measurement information, and the experimental data are tabulated in Tables 13-1, 13-2, and 13-3, respectively.

TABLE 13-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| GLOBAR, BULK OXIDIZED T = 293 | | | GLOBAR, BULK OXIDIZED T = 1400 | | | GLOBAR, BULK OXIDIZED T = 2400 | | | GLOBAR, BULK OXIDIZED T = 2400 (CONT.) | | |
|-------------------------------|------------|-----------|--------------------------------|-----------|------------|--------------------------------|------------|-----------|--|-----------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 1.0 | 0.901 | 10.6 | 0.872 | 1.0 | 0.920 | 10.6 | 0.899 | 1.0 | 0.951 | 10.6 | 0.922 |
| 1.2 | 0.898 | 10.8 | 0.869 | 1.2 | 0.925 | 10.8 | 0.896 | 1.2 | 0.940 | 10.8 | 0.919 |
| 1.5 | 0.893 | 11.0 | 0.862 | 1.5 | 0.920 | 11.0 | 0.889 | 1.5 | 0.943 | 11.0 | 0.912 |
| 1.8 | 0.887 | 11.2 | 0.855 | 1.8 | 0.914 | 11.2 | 0.882 | 1.8 | 0.937 | 11.2 | 0.905 |
| 2.0 | 0.882 | 11.5 | 0.841 | 2.0 | 0.909 | 11.5 | 0.860 | 2.0 | 0.932 | 11.5 | 0.891 |
| 2.2 | 0.876 | 11.8 | 0.826 | 2.2 | 0.903 | 11.8 | 0.853 | 2.2 | 0.926 | 11.8 | 0.876 |
| 2.5 | 0.860 | 12.0 | 0.815 | 2.5 | 0.895 | 12.0 | 0.842 | 2.5 | 0.910 | 12.0 | 0.865 |
| 2.8 | 0.862 | 12.2 | 0.806 | 2.8 | 0.889 | 12.2 | 0.833 | 2.8 | 0.912 | 12.2 | 0.856 |
| 3.0 | 0.859 | 12.5 | 0.795 | 3.0 | 0.886 | 12.5 | 0.822 | 3.0 | 0.909 | 12.5 | 0.845 |
| 3.2 | 0.856 | 12.8 | 0.793 | 3.2 | 0.883 | 12.8 | 0.820 | 3.2 | 0.906 | 12.8 | 0.843 |
| 3.5 | 0.855 | 13.0 | 0.790 | 3.5 | 0.882 | 13.0 | 0.825 | 3.5 | 0.905 | 13.0 | 0.840 |
| 3.8 | 0.855 | 13.2 | 0.804 | 3.8 | 0.882 | 13.2 | 0.831 | 3.8 | 0.905 | 13.2 | 0.854 |
| 4.0 | 0.859 | 13.5 | 0.813 | 4.0 | 0.886 | 13.5 | 0.840 | 4.0 | 0.909 | 13.5 | 0.863 |
| 4.2 | 0.863 | 13.8 | 0.821 | 4.2 | 0.890 | 13.8 | 0.848 | 4.2 | 0.913 | 13.8 | 0.871 |
| 4.5 | 0.870 | 14.0 | 0.825 | 4.5 | 0.897 | 14.0 | 0.852 | 4.5 | 0.920 | 14.0 | 0.875 |
| 4.8 | 0.876 | 14.2 | 0.829 | 4.8 | 0.903 | 14.2 | 0.856 | 4.8 | 0.926 | 14.2 | 0.879 |
| 5.0 | 0.879 | 14.5 | 0.831 | 5.0 | 0.906 | 14.5 | 0.850 | 5.0 | 0.929 | 14.5 | 0.881 |
| 5.5 | 0.881 | 14.8 | 0.833 | 5.5 | 0.908 | 14.8 | 0.860 | 5.5 | 0.931 | 14.8 | 0.883 |
| 5.8 | 0.880 | 15.0 | 0.833 | 5.8 | 0.907 | 15.0 | 0.860 | 5.8 | 0.930 | 15.0 | 0.883 |
| 6.0 | 0.879 | | | 6.0 | 0.906 | | | 6.0 | 0.929 | | |
| 6.2 | 0.878 | | | 6.2 | 0.905 | | | 6.2 | 0.928 | | |
| 6.5 | 0.877 | | | 6.5 | 0.904 | | | 6.5 | 0.927 | | |
| 6.8 | 0.878 | | | 6.8 | 0.905 | | | 6.8 | 0.928 | | |
| 7.0 | 0.878 | | | 7.0 | 0.905 | | | 7.0 | 0.928 | | |
| 7.2 | 0.879 | | | 7.2 | 0.905 | | | 7.2 | 0.928 | | |
| 7.5 | 0.877 | | | 7.5 | 0.904 | | | 7.5 | 0.927 | | |
| 7.8 | 0.876 | | | 7.8 | 0.903 | | | 7.8 | 0.926 | | |
| 8.0 | 0.875 | | | 8.0 | 0.902 | | | 8.0 | 0.925 | | |
| 8.2 | 0.873 | | | 8.2 | 0.900 | | | 8.2 | 0.923 | | |
| 8.5 | 0.871 | | | 8.5 | 0.898 | | | 8.5 | 0.921 | | |
| 8.8 | 0.869 | | | 8.8 | 0.896 | | | 8.8 | 0.919 | | |
| 9.0 | 0.867 | | | 9.0 | 0.894 | | | 9.0 | 0.917 | | |
| 9.2 | 0.865 | | | 9.2 | 0.892 | | | 9.2 | 0.915 | | |
| 9.5 | 0.864 | | | 9.5 | 0.891 | | | 9.5 | 0.914 | | |
| 9.8 | 0.866 | | | 9.8 | 0.893 | | | 9.8 | 0.916 | | |
| 10.0 | 0.869 | | | 10.0 | 0.896 | | | 10.0 | 0.919 | | |
| 10.2 | 0.871 | | | 10.2 | 0.898 | | | 10.2 | 0.921 | | |
| 10.5 | 0.873 | | | 10.5 | 0.900 | | | 10.5 | 0.923 | | |

TABLE 13-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| BULK POLISHED T = 293 | | BULK POLISHED T = 293 (CONT.) | | BULK POLISHED T = 1000 | | BULK POLISHED T = 1000 (CONT.) | | BULK POLISHED T = 2400 | | BULK POLISHED T = 2400 (CONT.) | |
|--------------------------|------------|----------------------------------|------------|---------------------------|------------|-----------------------------------|------------|---------------------------|------------|-----------------------------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 1.0 | 0.597A† | 10.6 | 0.791A† | 1.0 | 0.614A† | 10.6 | 0.798A† | 1.0 | 0.647A† | 10.6 | 0.831A† |
| 1.2 | 0.613A | 10.8 | 0.776A | 1.2 | 0.630A | 10.8 | 0.793A | 1.2 | 0.663A | 10.8 | 0.826A |
| 1.5 | 0.636A | 11.0 | 0.765A | 1.5 | 0.653A | 11.0 | 0.782A | 1.5 | 0.686A | 11.0 | 0.815A |
| 1.8 | 0.658A | 11.2 | 0.749A | 1.8 | 0.675A | 11.2 | 0.766A | 1.8 | 0.708A | 11.2 | 0.799A |
| 2.0 | 0.672A | 11.5 | 0.721A | 2.0 | 0.685A | 11.5 | 0.738A | 2.0 | 0.722A | 11.5 | 0.771A |
| 2.2 | 0.686A | 11.8 | 0.693A | 2.2 | 0.703A | 11.8 | 0.710A | 2.2 | 0.736A | 11.8 | 0.743A |
| 2.5 | 0.705A | 12.0 | 0.675A | 2.5 | 0.722A | 12.0 | 0.692A | 2.5 | 0.755A | 12.0 | 0.725A |
| 2.8 | 0.721A | 12.2 | 0.657A | 2.8 | 0.738A | 12.2 | 0.674A | 2.8 | 0.771A | 12.2 | 0.707A |
| 3.0 | 0.731A | 12.5 | 0.638A | 3.0 | 0.748A | 12.5 | 0.655A | 3.0 | 0.781A | 12.5 | 0.688A |
| 3.2 | 0.738A | 12.6 | 0.637A | 3.2 | 0.755A | 12.6 | 0.654A | 3.2 | 0.788A | 12.6 | 0.687A |
| 3.5 | 0.748A | 12.8 | 0.645A | 3.5 | 0.765A | 12.8 | 0.662A | 3.5 | 0.798A | 12.8 | 0.695A |
| 3.8 | 0.754A | 13.0 | 0.662A | 3.8 | 0.771A | 13.0 | 0.679A | 3.8 | 0.804A | 13.0 | 0.712A |
| 4.0 | 0.756A | 13.2 | 0.682A | 4.0 | 0.773A | 13.2 | 0.699A | 4.0 | 0.806A | 13.2 | 0.732A |
| 4.2 | 0.758A | 13.3 | 0.690A | 4.2 | 0.775A | 13.3 | 0.707A | 4.2 | 0.808A | 13.3 | 0.740A |
| 4.5 | 0.759A | 13.5 | 0.698A | 4.5 | 0.776A | 13.5 | 0.715A | 4.5 | 0.809A | 13.5 | 0.748A |
| 4.8 | 0.759A | 13.8 | 0.700A | 4.8 | 0.776A | 13.8 | 0.717A | 4.8 | 0.809A | 13.8 | 0.750A |
| 5.0 | 0.759A | 14.0 | 0.701A | 5.0 | 0.776A | 14.0 | 0.718A | 5.0 | 0.809A | 14.0 | 0.751A |
| 5.2 | 0.759A | 14.2 | 0.701A | 5.2 | 0.776A | 14.2 | 0.718A | 5.2 | 0.809A | 14.2 | 0.751A |
| 5.5 | 0.758A | 14.5 | 0.700A | 5.5 | 0.775A | 14.5 | 0.717A | 5.5 | 0.808A | 14.5 | 0.750A |
| 5.8 | 0.757A | 14.8 | 0.699A | 5.8 | 0.774A | 14.8 | 0.716A | 5.8 | 0.807A | 14.8 | 0.749A |
| 6.0 | 0.756A | 15.0 | 0.698A | 6.0 | 0.773A | 15.0 | 0.715A | 6.0 | 0.806A | 15.0 | 0.748A |
| 6.2 | 0.754A | | | 6.2 | 0.771A | | | 6.2 | 0.804A | | |
| 6.5 | 0.752A | | | 6.5 | 0.769A | | | 6.5 | 0.802A | | |
| 6.8 | 0.750A | | | 6.8 | 0.767A | | | 6.8 | 0.800A | | |
| 7.0 | 0.748A | | | 7.0 | 0.765A | | | 7.0 | 0.798A | | |
| 7.2 | 0.747A | | | 7.2 | 0.764A | | | 7.2 | 0.797A | | |
| 7.5 | 0.745A | | | 7.5 | 0.762A | | | 7.5 | 0.795A | | |
| 7.8 | 0.743A | | | 7.8 | 0.757A | | | 7.8 | 0.790A | | |
| 8.0 | 0.737A | | | 8.0 | 0.754A | | | 8.0 | 0.787A | | |
| 8.2 | 0.734A | | | 8.2 | 0.751A | | | 8.2 | 0.784A | | |
| 8.5 | 0.728A | | | 8.5 | 0.743A | | | 8.5 | 0.776A | | |
| 8.8 | 0.716A | | | 8.8 | 0.733A | | | 8.8 | 0.766A | | |
| 9.0 | 0.708A | | | 9.0 | 0.725A | | | 9.0 | 0.758A | | |
| 9.2 | 0.706A | | | 9.2 | 0.723A | | | 9.2 | 0.756A | | |
| 9.5 | 0.718A | | | 9.5 | 0.735A | | | 9.5 | 0.768A | | |
| 9.8 | 0.741A | | | 9.8 | 0.758A | | | 9.8 | 0.791A | | |
| 10.0 | 0.760A | | | 10.0 | 0.777A | | | 10.0 | 0.810A | | |
| 10.2 | 0.774A | | | 10.2 | 0.791A | | | 10.2 | 0.824A | | |
| 10.5 | 0.782A | | | 10.5 | 0.799A | | | 10.5 | 0.832A | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

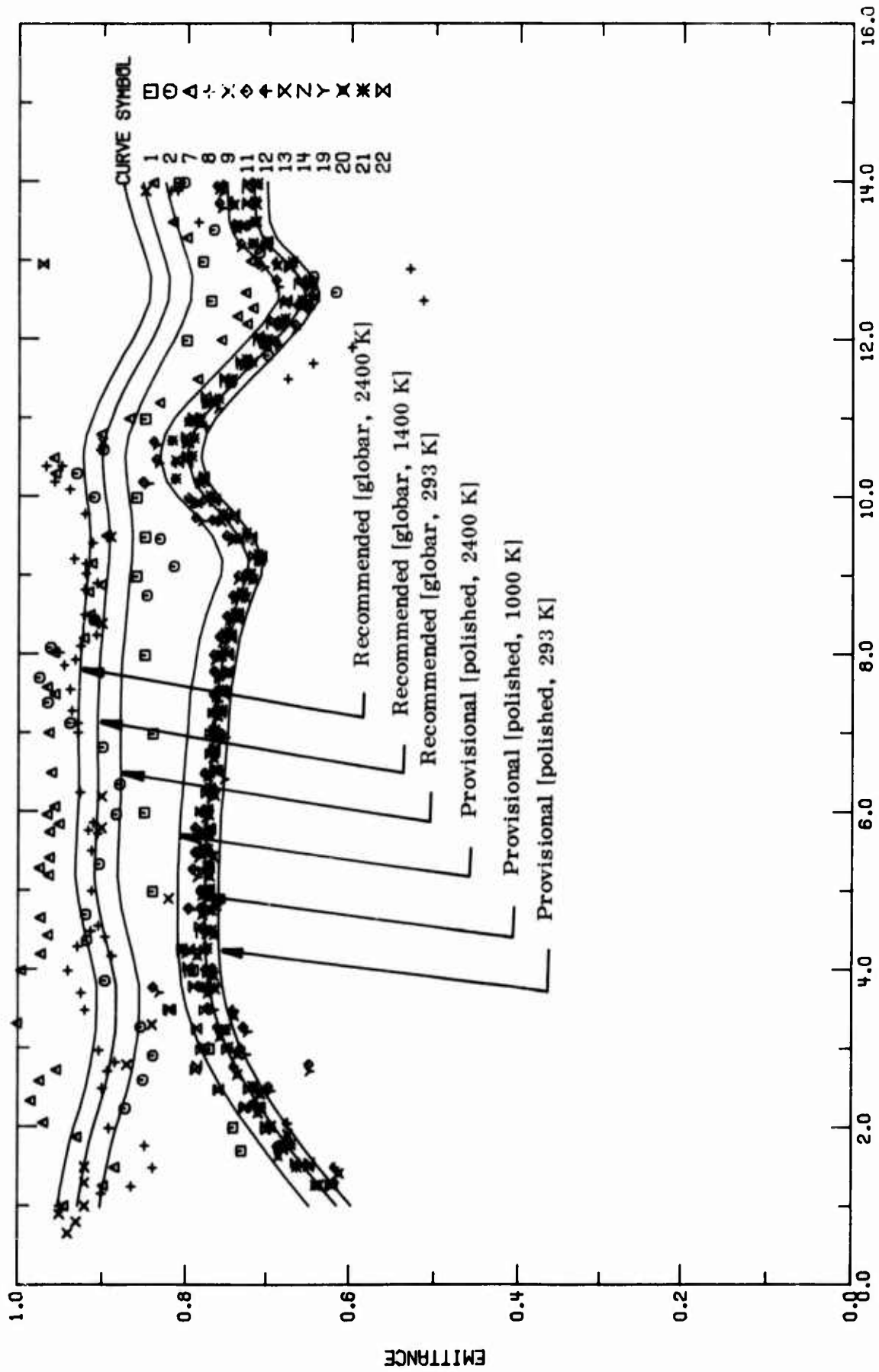


FIGURE 13-1. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

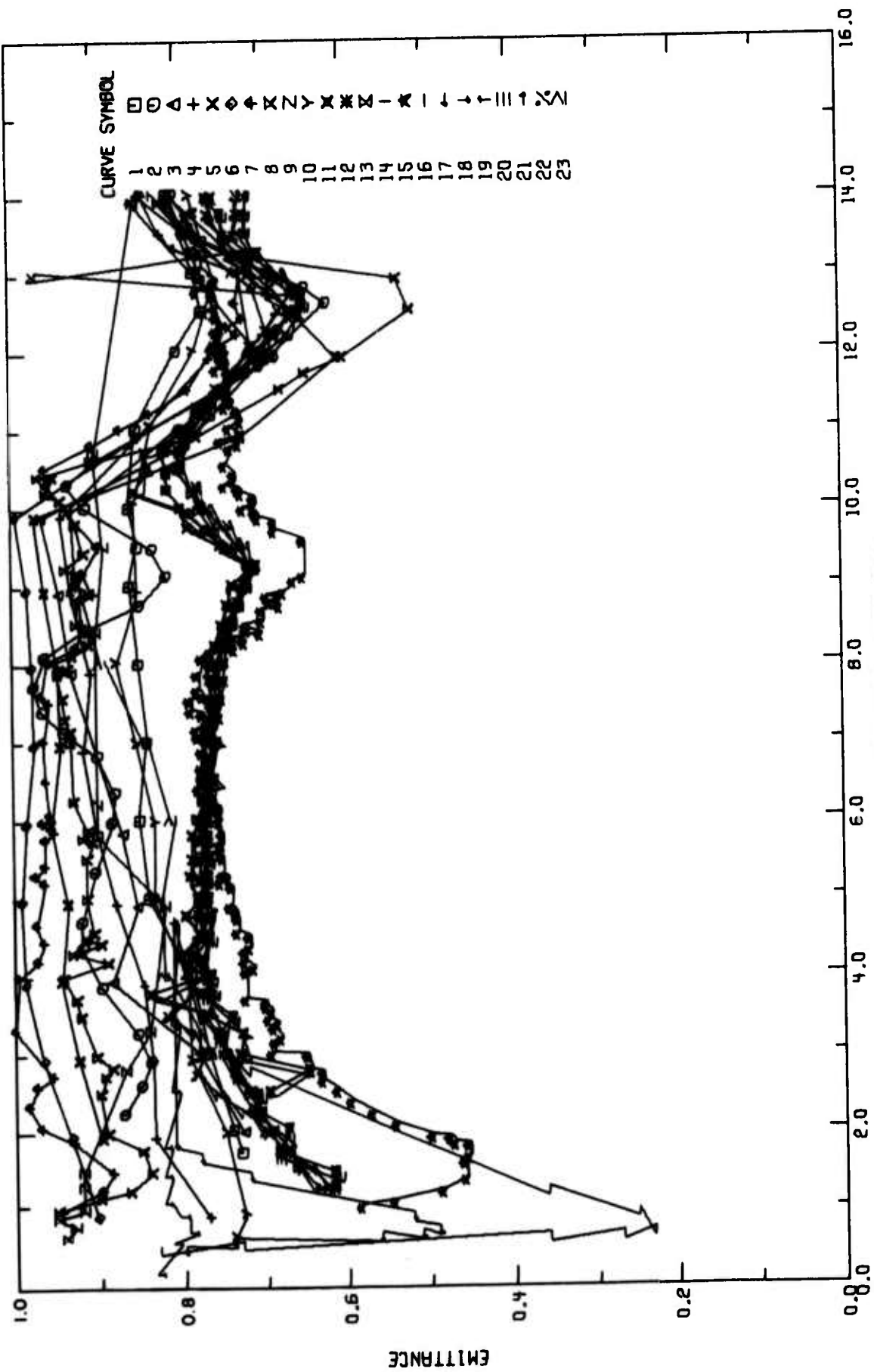


FIGURE 13-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

TABLE 13-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON MONOCARBIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|------|----------------------|--|---|
| | | | | | | | |
| 1 T00758 | Silverman, S. | 1948 | 1.7-15.0 | 1375 | | Globar from the Carborundum Co.; data extracted from smooth curve; $\theta' = \sim 0^\circ$. | |
| 2 T10461 | Blau, H.H., Jr., Chaffee, E., and Jasperse, J.R. | 1960 | 2.24-13.9 | 1296 | | Norton Co. Crystalon-R; flat and smooth surface obtained by diamond wheel cutting; oxidized by heating in air at 1400 K for 1 hr; measured in argon-hydrogen atm; data extracted from smooth curve; $\theta' = \sim 0^\circ$. | |
| 3 T32045 | Blau, H.H., Jr. and Jasperse, J.R. | 1964 | 2.00-13.9 | 873 | | Bonded Norton RC 4237; 80 pure SiC, nitride bonded; ultrasonically machined; measured in air; $\theta' = 0^\circ$; reported error 54%. | |
| 4 T32045 | Blau, H.H., Jr. and Jasperse, J.R. | 1964 | 0.91-13.9 | 1293 | | Above specimen and conditions. | |
| 5 T32045 | Blau, H.H., Jr. and Jasperse, J.R. | 1964 | 1.92-13.9 | 873 | | Norton Crystalon R; 99 pure; ultrasonically machined; measured in air; $\theta' = 0^\circ$; reported error 54%. | |
| 6 T32045 | Blau, H.H., Jr. and Jasperse, J.R. | 1964 | 0.92-13.9 | 1298 | | Above specimen and conditions. | |
| 7 T22272 | Schatz, E.A., Goldberg, D.M., Pearson, E.G., and Burks, T.L. | 1963 | 1.00-15.0 | 1023 | Sample No. 102 | Density 2.32 g cm ⁻³ ; theoretical density 3.21 g cm ⁻³ ; data extracted from smooth curve; $\theta' = \sim 0^\circ$. | |
| 8 T22272 | Schatz, E.A., et al. | 1963 | 1.00-15.0 | 1023 | Sample No. 103 | Sintered at 2173 K for 1 hr (setter material SiC); density 1.49 g cm ⁻³ ; theoretical density 3.21 g cm ⁻³ ; data extracted from smooth curve; $\theta' = \sim 0^\circ$. | |
| 9 T25673 | Mitchell, C.A. | 1962 | 0.65-14.9 | 1358 | | Globar from Carborundum Co; $\theta' = \sim 0^\circ$. | |
| 10 T02147 | Brügel, W. | 1950 | 0.66-15 | 1243 | | Rod specimen electrically heated. | |
| 11 T40798 | Stewart, J.E. and Richman, J.C. | 1957 | 2.5-15 | 755 | Globar | Recrystallized; measured with a Perkin-Elmer spectrophotometer. | |
| 12 T40798 | Stewart, J.E. and Richman, J.C. | 1957 | 1.3-15 | 922 | Globar | The above specimen. | |
| 13 T40798 | Stewart, J.E. and Richman, J.C. | 1957 | 1.3-15 | 1089 | Globar | The above specimen. | |
| 14 T40798 | Stewart, J.E. and Richman, J.C. | 1957 | 1.3-15 | 1255 | Globar | The above specimen. | |
| 15 T36117 | Schatz, E.A. | 1962 | 1.0-15 | 1273 | | Supplied by Carborundum Co.; sintered; density 2.32 g cm ⁻³ . | |
| 16 T62013 | Dubrovskii, G.B. | 1969 | 0.49-4.7 | 2000 | | α -phase 6H type single crystal; 100 μ thick plate specimen with surface perpendicular to c_2 -axis; values calculated from absorption coefficient measurement; data taken from smooth curve. | |
| 17 T62013 | Dubrovskii, G.B. | 1969 | 0.49-4.7 | 2200 | | The above specimen. | |
| 18 T62013 | Dubrovskii, G.B. | 1969 | 0.19-4.7 | 2500 | | The above specimen. | |
| 19 T08277 | Richmond, J.C. and Stewart, J.E. | 1959 | 2.5-15 | 755 | | Recrystallized rod specimen. | |
| 20 T08277 | Richmond, J.C. and Stewart, J.E. | 1959 | 1.3-15 | 922 | | The above specimen. | |
| 21 T08277 | Richmond, J.C. and Stewart, J.E. | 1959 | 1.3-15 | 1089 | | The above specimen. | |

TABLE 13-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON MONOCARBIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 22 T08277 | Richmond, J.C. and Stewart, J.E. | 1959 | 1.3-15 | 1255 | | The above specimen. |
| 23 T16606 | Blau, H.H., Jr., March, J.B., Martin, W.S., Jasperse, J.R., and Chaffee, E. | 1960 | 2.0-14 | 1073 | | The same specimen as for curve No. 5. |

TABLE 13-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | |
|----------------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-------|
| CURVE 1 | | | | | | | | | | | | | | |
| T = 1375. | | | | | | | | | | | | | | |
| 1.7 | 0.73 | 9.47 | 0.832 | 10.9 | 0.848 | 1.00 | 0.945 | 12.3 | 0.738 | 7.56 | 0.938 | 12.3 | 0.738 | |
| 2.0 | 0.74 | 10.0 | 0.910 | 11.9 | 0.761 | 1.26 | 0.698 | 12.4 | 0.719 | 7.87 | 0.945 | 12.4 | 0.719 | |
| 3.0 | 0.77 | 10.3 | 0.931 | 12.3 | 0.744 | 1.49 | 0.885 | 12.6 | 0.728 | 7.94 | 0.932 | 12.6 | 0.728 | |
| 4.0 | 0.79 | 10.6 | 0.899 | 14.0 | 0.806 | 1.88 | 0.930 | 13.0 | 0.722 | 8.03 | 0.951 | 13.0 | 0.722 | |
| 5.0 | 0.84 | 11.8 | 0.700 | CURVE 5 | | 2.06 | 0.969 | 13.3 | 0.800 | 8.11 | 0.926 | 13.3 | 0.800 | |
| 6.0 | 0.84 | 12.6 | 0.617 | T = 873. | | 2.34 | 0.984 | 13.5 | 0.817 | 8.25 | 0.907 | 13.5 | 0.817 | |
| 7.0 | 0.84 | 12.8 | 0.644 | 1.92 | 0.897 | 2.59 | 0.974 | 14.0 | 0.841 | 8.42 | 0.907 | 14.0 | 0.841 | |
| 8.0 | 0.85 | 13.1 | 0.711 | 2.93 | 0.923 | 2.73 | 0.954 | 14.5 | 0.852 | 8.51 | 0.921 | 14.5 | 0.852 | |
| 9.0 | 0.85 | 13.4 | 0.767 | 3.32 | 1.000 | 3.99 | 0.995 | 15.0 | 0.880 | 8.63 | 0.921 | 15.0 | 0.880 | |
| 9.5 | 0.85 | 14.0 | 0.803 | 3.95 | 0.943 | 4.20 | 0.972 | CURVE 8 | | | | | 8.91 | 0.906 |
| 10.0 | 0.86 | CURVE 3 | | 4.94 | 0.934 | 4.44 | 0.964 | T = 1023. | | 9.03 | 0.920 | 9.03 | 0.920 | |
| 11.0 | 0.85 | T = 873. | | 5.95 | 0.954 | 4.66 | 0.973 | | | 9.16 | 0.920 | 9.16 | 0.920 | |
| 12.0 | 0.80 | | | 6.95 | 0.942 | 5.20 | 0.963 | 1.00 | 0.950 | 9.22 | 0.934 | 9.22 | 0.934 | |
| 12.5 | 0.77 | 2.00 | 0.727 | 7.91 | 0.944 | 5.29 | 0.974 | 1.16 | 0.900 | 9.42 | 0.912 | 9.42 | 0.912 | |
| 13.0 | 0.78 | 3.02 | 0.781 | 8.93 | 0.960 | 5.42 | 0.962 | 1.25 | 0.865 | 9.79 | 0.921 | 9.79 | 0.921 | |
| 14.0 | 0.81 | 3.93 | 0.884 | 9.88 | 0.971 | 5.75 | 0.962 | 1.49 | 0.839 | 10.1 | 0.939 | 10.1 | 0.939 | |
| 15.0 | 0.79 | 4.90 | 0.853 | 10.9 | 0.723 | 5.85 | 0.951 | 1.77 | 0.849 | 10.2 | 0.957 | 10.2 | 0.957 | |
| CURVE 2 | | | | | | | | | | | | | | |
| T = 1296. | | | | | | | | | | | | | | |
| 2.24 | 0.872 | 5.83 | 0.870 | 11.9 | 0.604 | 6.07 | 0.956 | 1.99 | 0.891 | 10.4 | 0.948 | 1.99 | 0.891 | |
| 2.60 | 0.851 | 7.88 | 0.928 | 12.8 | 0.685 | 6.50 | 0.960 | 2.50 | 0.899 | 10.4 | 0.967 | 2.50 | 0.899 | |
| 2.91 | 0.839 | 8.90 | 0.942 | 14.0 | 0.807 | 7.01 | 0.963 | 2.72 | 0.893 | 10.6 | 0.903 | 2.72 | 0.893 | |
| 3.27 | 0.854 | 9.88 | 0.963 | CURVE 6 | | 8.03 | 0.958 | 2.83 | 0.884 | 10.9 | 0.777 | 2.83 | 0.884 | |
| 3.86 | 0.896 | 10.8 | 0.791 | T = 1298. | | 8.21 | 0.922 | 2.98 | 0.903 | 11.5 | 0.644 | 2.98 | 0.903 | |
| 4.37 | 0.918 | 11.9 | 0.694 | 1.94 | 0.932 | 8.51 | 0.915 | 3.49 | 0.920 | 11.7 | 0.644 | 3.49 | 0.920 | |
| 4.70 | 0.919 | 12.9 | 0.771 | 2.93 | 0.965 | 8.80 | 0.917 | 3.71 | 0.925 | 11.9 | 0.598 | 3.71 | 0.925 | |
| 5.34 | 0.903 | 13.9 | 0.852 | 3.91 | 0.986 | 8.89 | 0.902 | 3.99 | 0.940 | 12.5 | 0.514 | 3.99 | 0.940 | |
| 5.97 | 0.883 | CURVE 4 | | 4.96 | 0.990 | 9.16 | 0.913 | 4.18 | 0.888 | 12.9 | 0.530 | 4.18 | 0.888 | |
| 6.35 | 0.879 | T = 1293. | | 5.95 | 0.984 | 9.51 | 0.896 | 4.30 | 0.929 | 13.2 | 0.714 | 4.30 | 0.929 | |
| 6.82 | 0.899 | 0.910 | 0.770 | 6.96 | 0.974 | 10.3 | 0.896 | 4.42 | 0.896 | 13.5 | 0.786 | 4.42 | 0.896 | |
| 7.13 | 0.938 | 1.93 | 0.834 | 7.95 | 0.976 | 10.5 | 0.956 | 4.56 | 0.904 | 13.9 | 0.819 | 4.56 | 0.904 | |
| 7.39 | 0.964 | 2.93 | 0.836 | 8.94 | 0.981 | 10.8 | 0.950 | 5.00 | 0.912 | 14.1 | 0.826 | 5.00 | 0.912 | |
| 7.71 | 0.974 | 3.89 | 0.846 | 9.89 | 0.994 | 11.2 | 0.833 | 5.51 | 0.912 | 14.4 | 0.826 | 5.51 | 0.912 | |
| 8.09 | 0.961 | 4.92 | 0.878 | 10.9 | 0.849 | 11.5 | 0.787 | 5.73 | 0.905 | 14.5 | 0.843 | 5.73 | 0.905 | |
| 8.44 | 0.910 | 5.86 | 0.900 | 11.9 | 0.680 | 12.0 | 0.758 | 5.77 | 0.916 | 14.6 | 0.834 | 5.77 | 0.916 | |
| 8.75 | 0.848 | 6.88 | 0.915 | 12.8 | 0.706 | 12.2 | 0.726 | 6.25 | 0.926 | 15.0 | 0.870 | 6.25 | 0.926 | |
| 9.12 | 0.815 | 8.90 | 0.927 | 14.0 | 0.844 | | | 7.01 | 0.929 | CURVE 9 | | 7.01 | 0.929 | |
| T = 1358. | | | | | | | | | | | | | | |
| 0.65 0.94 | | | | | | | | | | | | | | |

TABLE 13-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | | |
|------------------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|------|-------|
| CURVE 9 (CONT.) | | | | | | | | | | | |
| 0.80 | 0.93 | 2.80 | 0.647 | 12.76 | 0.690 | 7.77 | 0.762 | 2.26 | 0.708 | | |
| 0.90 | 0.95 | 3.00 | 0.731 | 12.97 | 0.712 | 7.99 | 0.756 | 2.48 | 0.721 | | |
| 1.00 | 0.92 | 3.27 | 0.728 | 13.22 | 0.734 | 8.23 | 0.747 | 2.99 | 0.748 | | |
| 1.30 | 0.92 | 3.52 | 0.772 | 13.47 | 0.742 | 8.48 | 0.737 | 3.23 | 0.753 | | |
| 1.50 | 0.92 | 3.78 | 0.839 | 13.74 | 0.761 | 8.74 | 0.728 | 3.49 | 0.776 | | |
| 2.80 | 0.87 | 4.01 | 0.775 | 13.97 | 0.756 | 8.96 | 0.718 | 3.75 | 0.762 | | |
| 3.3 | 0.84 | 4.27 | 0.804 | 14.23 | 0.760 | 9.23 | 0.708 | 3.96 | 0.772 | | |
| 4.9 | 0.82 | 4.50 | 0.775 | 14.43 | 0.766 | 9.47 | 0.744 | 4.25 | 0.776 | | |
| 5.8 | 0.90 | 4.78 | 0.796 | 14.69 | 0.759 | 9.71 | 0.768 | 4.47 | 0.771 | | |
| 6.2 | 0.90 | 4.99 | 0.781 | 14.97 | 0.740 | 9.93 | 0.789 | 4.75 | 0.767 | | |
| 8.4 | 0.90 | 5.28 | 0.791 | 15.22 | 0.740 | 10.23 | 0.813 | 5.00 | 0.772 | | |
| 9.5 | 0.89 | 5.49 | 0.788 | CURVE 12 | | | | | | 5.24 | 0.778 |
| 10.7 | 0.90 | 5.80 | 0.788 | T = 922. | | | | | | 5.50 | 0.778 |
| 13.9 | 0.85 | 6.00 | 0.780 | 1.30 | 0.616 | 11.21 | 0.776 | 6.01 | 0.782 | | |
| 14.9 | 0.86 | 6.29 | 0.774 | 1.49 | 0.616 | 11.49 | 0.749 | 6.24 | 0.775 | | |
| CURVE 10 | | | | | | | | | | | |
| T = 1243. | | | | | | | | | | | |
| 0.66 | 0.739 | 7.53 | 0.763 | 1.76 | 0.686 | 11.72 | 0.720 | 6.49 | 0.770 | | |
| 0.95 | 0.726 | 7.79 | 0.766 | 2.05 | 0.673 | 11.96 | 0.707 | 6.74 | 0.770 | | |
| 2.00 | 0.749 | 8.00 | 0.766 | 2.29 | 0.715 | 12.20 | 0.686 | 7.00 | 0.770 | | |
| 2.93 | 0.790 | 8.23 | 0.759 | 2.49 | 0.711 | 12.57 | 0.645 | 7.26 | 0.767 | | |
| 3.97 | 0.793 | 8.49 | 0.750 | 2.77 | 0.739 | 12.70 | 0.653 | 7.53 | 0.758 | | |
| 4.97 | 0.833 | 8.75 | 0.743 | 3.27 | 0.760 | 12.98 | 0.690 | 7.76 | 0.758 | | |
| 5.99 | 0.831 | 9.00 | 0.736 | 3.49 | 0.740 | 13.22 | 0.719 | 7.99 | 0.756 | | |
| 6.99 | 0.853 | 9.25 | 0.710 | 3.78 | 0.778 | 13.43 | 0.741 | 8.27 | 0.751 | | |
| 8.02 | 0.876 | 9.51 | 0.751 | 4.02 | 0.766 | 13.76 | 0.745 | 8.47 | 0.744 | | |
| 8.93 | 0.850 | 9.74 | 0.789 | 4.26 | 0.789 | 13.96 | 0.763 | 8.73 | 0.734 | | |
| 10.06 | 0.854 | 9.99 | 0.798 | 4.50 | 0.768 | 14.20 | 0.754 | 8.97 | 0.725 | | |
| 11.05 | 0.832 | 10.20 | 0.853 | 4.78 | 0.781 | 14.45 | 0.760 | 9.25 | 0.717 | | |
| 12.00 | 0.780 | 10.48 | 0.837 | 5.01 | 0.781 | 14.75 | 0.745 | 9.47 | 0.734 | | |
| 12.93 | 0.754 | 10.71 | 0.840 | 5.28 | 0.774 | 14.98 | 0.745 | 9.69 | 0.757 | | |
| 14.00 | 0.783 | 10.97 | 0.788 | 5.49 | 0.765 | 15.21 | 0.737 | 9.96 | 0.775 | | |
| 15.00 | 0.767 | 11.23 | 0.764 | 5.75 | 0.774 | CURVE 13 | | | | | |
| T = 1069. | | | | | | | | | | | |
| CURVE 11 | | | | | | | | | | | |
| T = 755. | | | | | | | | | | | |
| 2.52 | 0.697 | 11.49 | 0.749 | 6.01 | 0.774 | 1.27 | 0.634 | 11.22 | 0.765 | | |
| | | 11.71 | 0.726 | 6.49 | 0.777 | 1.54 | 0.663 | 11.46 | 0.746 | | |
| | | 11.98 | 0.691 | 7.03 | 0.762 | 1.79 | 0.673 | 11.68 | 0.728 | | |
| | | 12.19 | 0.666 | 7.26 | 0.766 | 2.02 | 0.693 | 11.94 | 0.702 | | |
| | | 12.45 | 0.650 | 7.49 | 0.766 | | | 12.22 | 0.681 | | |
| CURVE 13 (CONT.) | | | | | | | | | | | |
| 12.46 | 0.708 | 2.26 | 0.762 | 7.77 | 0.762 | 1.26 | 0.620 | 12.46 | 0.658 | | |
| 12.69 | 0.721 | 2.48 | 0.756 | 7.99 | 0.756 | 1.54 | 0.646 | 12.69 | 0.647 | | |
| 12.94 | 0.748 | 2.99 | 0.747 | 8.23 | 0.747 | 1.77 | 0.678 | 12.94 | 0.672 | | |
| 13.19 | 0.753 | 3.23 | 0.737 | 8.48 | 0.737 | 2.01 | 0.700 | 13.19 | 0.703 | | |
| 13.50 | 0.776 | 3.49 | 0.728 | 8.74 | 0.728 | 2.26 | 0.725 | 13.50 | 0.714 | | |
| 13.72 | 0.714 | 3.75 | 0.718 | 8.96 | 0.718 | 2.48 | 0.758 | 13.72 | 0.714 | | |
| 13.97 | 0.714 | 3.96 | 0.708 | 9.23 | 0.708 | 2.78 | 0.758 | 13.97 | 0.714 | | |
| 14.21 | 0.776 | 4.25 | 0.744 | 9.47 | 0.744 | 3.01 | 0.776 | 14.21 | 0.714 | | |
| 14.47 | 0.771 | 4.47 | 0.768 | 9.71 | 0.768 | 3.25 | 0.785 | 14.47 | 0.725 | | |
| 14.69 | 0.767 | 4.75 | 0.789 | 9.93 | 0.789 | 3.49 | 0.817 | 14.69 | 0.725 | | |
| 14.93 | 0.772 | 5.00 | 0.813 | 10.23 | 0.813 | 3.78 | 0.788 | 14.93 | 0.722 | | |
| CURVE 14 | | | | | | | | | | | |
| T = 1255. | | | | | | | | | | | |
| 1.26 | 0.620 | 8.27 | 0.719 | 11.49 | 0.749 | 1.26 | 0.620 | 1.26 | 0.620 | | |
| 1.54 | 0.646 | 8.47 | 0.741 | 11.72 | 0.720 | 1.54 | 0.646 | 1.54 | 0.646 | | |
| 1.77 | 0.678 | 8.67 | 0.744 | 11.96 | 0.707 | 1.77 | 0.678 | 1.77 | 0.678 | | |
| 2.01 | 0.700 | 8.73 | 0.734 | 12.20 | 0.686 | 2.01 | 0.700 | 2.01 | 0.700 | | |
| 2.26 | 0.725 | 8.97 | 0.725 | 12.44 | 0.663 | 2.26 | 0.725 | 2.26 | 0.725 | | |
| 2.48 | 0.758 | 9.25 | 0.754 | 12.57 | 0.645 | 2.48 | 0.758 | 2.48 | 0.758 | | |
| 2.78 | 0.758 | 9.47 | 0.754 | 12.70 | 0.653 | 2.78 | 0.758 | 2.78 | 0.758 | | |
| 3.01 | 0.776 | 9.69 | 0.760 | 12.98 | 0.690 | 3.01 | 0.776 | 3.01 | 0.776 | | |
| 3.25 | 0.785 | 9.96 | 0.745 | 13.22 | 0.719 | 3.25 | 0.785 | 3.25 | 0.785 | | |
| 3.49 | 0.817 | 10.18 | 0.745 | 13.43 | 0.741 | 3.49 | 0.817 | 3.49 | 0.817 | | |
| 3.78 | 0.788 | 10.49 | 0.745 | 13.76 | 0.745 | 3.78 | 0.788 | 3.78 | 0.788 | | |
| 3.97 | 0.794 | 10.70 | 0.737 | 13.96 | 0.763 | 3.97 | 0.794 | 3.97 | 0.794 | | |
| 4.23 | 0.803 | 10.98 | 0.784 | 14.20 | 0.754 | 4.23 | 0.803 | 4.23 | 0.803 | | |
| 4.47 | 0.780 | 11.22 | 0.765 | 14.45 | 0.760 | 4.47 | 0.780 | 4.47 | 0.780 | | |
| 4.75 | 0.771 | 11.46 | 0.746 | 14.75 | 0.745 | 4.75 | 0.771 | 4.75 | 0.771 | | |
| 5.00 | 0.771 | 11.68 | 0.728 | 14.98 | 0.745 | 5.00 | 0.771 | 5.00 | 0.771 | | |
| 5.28 | 0.771 | 11.94 | 0.702 | 15.21 | 0.737 | 5.28 | 0.771 | 5.28 | 0.771 | | |
| 5.48 | 0.775 | 12.22 | 0.681 | CURVE 13 | | | | | | | |
| 5.77 | 0.769 | | | T = 1069. | | | | | | | |
| 6.00 | 0.774 | | | 1.27 | 0.634 | 6.00 | 0.774 | 6.00 | 0.774 | | |
| 6.26 | 0.768 | | | 1.54 | 0.663 | 6.26 | 0.768 | 6.26 | 0.768 | | |
| 6.52 | 0.761 | | | 1.79 | 0.673 | 6.52 | 0.761 | 6.52 | 0.761 | | |
| 6.79 | 0.764 | | | 2.02 | 0.693 | 6.79 | 0.764 | 6.79 | 0.764 | | |
| 6.96 | 0.764 | | | | | 6.96 | 0.764 | 6.96 | 0.764 | | |
| 7.25 | 0.764 | | | | | 7.25 | 0.764 | 7.25 | 0.764 | | |
| 7.52 | 0.764 | | | | | 7.52 | 0.764 | 7.52 | 0.764 | | |

TABLE 13-3. EXPERIMENTAL NORMAL SPECTRAL EMISSION OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMISSION, ϵ]

| CURVE 14 (CONT.) | | CURVE 15 (CONT.) | | CURVE 15 (CONT.) | | CURVE 15 (CONT.) | | CURVE 15 (CONT.) | | CURVE 15 (CONT.) | | CURVE 15 (CONT.) | | CURVE 16 (CONT.) | |
|------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|------------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| CURVE 14 (CONT.) | | | | | | | | | | | | | | | |
| 7.49 | 0.753 | 1.63 | 0.459 | 5.62 | 0.771 | 6.79 | 0.682 | 12.40 | 0.754 | 12.40 | 0.754 | 4.69 | 0.81 | CURVE 16 (CONT.) | |
| 7.78 | 0.747 | 1.78 | 0.459 | 5.66 | 0.754 | 6.82 | 0.697 | 12.47 | 0.767 | 12.47 | 0.767 | CURVE 17 | | | |
| 7.98 | 0.747 | 1.80 | 0.475 | 5.79 | 0.754 | 6.87 | 0.676 | 12.53 | 0.753 | 12.53 | 0.753 | T = 2200. | | | |
| 8.20 | 0.744 | 1.88 | 0.481 | 5.90 | 0.774 | 6.92 | 0.663 | 12.69 | 0.758 | 12.69 | 0.758 | 0.490 | 0.80 | | |
| 8.44 | 0.736 | 1.90 | 0.501 | 5.96 | 0.756 | 6.98 | 0.651 | 12.73 | 0.777 | 12.73 | 0.777 | 0.490 | 0.80 | | |
| 8.72 | 0.733 | 2.05 | 0.543 | 6.03 | 0.777 | 7.03 | 0.651 | 12.85 | 0.753 | 12.85 | 0.753 | 0.576 | 0.74 | | |
| 8.99 | 0.725 | 2.20 | 0.572 | 6.05 | 0.757 | 7.09 | 0.687 | 13.02 | 0.773 | 13.02 | 0.773 | 0.643 | 0.56 | | |
| 9.19 | 0.710 | 2.35 | 0.598 | 6.12 | 0.767 | 7.11 | 0.709 | 13.22 | 0.773 | 13.22 | 0.773 | 0.674 | 0.51 | | |
| 9.45 | 0.724 | 2.49 | 0.615 | 6.16 | 0.767 | 7.11 | 0.709 | 13.27 | 0.782 | 13.27 | 0.782 | 0.719 | 0.49 | | |
| 9.72 | 0.742 | 2.62 | 0.633 | 6.31 | 0.773 | 7.14 | 0.724 | 13.44 | 0.777 | 13.44 | 0.777 | 0.902 | 0.52 | | |
| 9.95 | 0.766 | 2.73 | 0.633 | 6.34 | 0.767 | 7.19 | 0.724 | 13.50 | 0.793 | 13.50 | 0.793 | 1.43 | 0.72 | | |
| 10.20 | 0.779 | 2.75 | 0.647 | 6.37 | 0.782 | 7.29 | 0.711 | 13.57 | 0.783 | 13.57 | 0.783 | 1.67 | 0.78 | | |
| 10.44 | 0.799 | 2.95 | 0.652 | 6.43 | 0.764 | 7.33 | 0.711 | 13.62 | 0.793 | 13.62 | 0.793 | 1.87 | 0.81 | | |
| 10.69 | 0.799 | 2.97 | 0.696 | 6.49 | 0.772 | 7.33 | 0.726 | 13.73 | 0.767 | 13.73 | 0.767 | 3.38 | 0.81 | | |
| 10.97 | 0.791 | 3.12 | 0.693 | 6.63 | 0.779 | 7.37 | 0.729 | 13.77 | 0.779 | 13.77 | 0.779 | 4.69 | 0.81 | | |
| 11.20 | 0.775 | 3.17 | 0.684 | 6.68 | 0.771 | 7.46 | 0.746 | 14.05 | 0.788 | 14.05 | 0.788 | CURVE 18 | | | |
| 11.46 | 0.753 | 3.30 | 0.694 | 6.84 | 0.778 | 7.51 | 0.746 | 14.35 | 0.786 | 14.35 | 0.786 | T = 2500. | | | |
| 11.69 | 0.732 | 3.36 | 0.688 | 7.03 | 0.782 | 7.52 | 0.734 | 14.41 | 0.761 | 14.41 | 0.761 | 0.190 | 0.83 | | |
| 11.99 | 0.712 | 3.41 | 0.700 | 7.06 | 0.774 | 7.55 | 0.734 | 14.47 | 0.793 | 14.47 | 0.793 | 0.508 | 0.81 | | |
| 12.20 | 0.696 | 3.52 | 0.696 | 7.12 | 0.784 | 7.55 | 0.739 | 14.55 | 0.785 | 14.55 | 0.785 | 0.716 | 0.79 | | |
| 12.46 | 0.679 | 3.58 | 0.703 | 7.18 | 0.773 | 7.55 | 0.728 | 14.72 | 0.797 | 14.72 | 0.797 | 0.927 | 0.80 | | |
| 12.71 | 0.662 | 3.63 | 0.703 | 7.32 | 0.777 | 7.55 | 0.751 | 14.83 | 0.800 | 14.83 | 0.800 | 1.09 | 0.82 | | |
| 12.93 | 0.674 | 3.67 | 0.727 | 7.36 | 0.790 | 7.55 | 0.724 | 14.87 | 0.789 | 14.87 | 0.789 | 1.44 | 0.82 | | |
| 13.19 | 0.702 | 4.02 | 0.717 | 7.50 | 0.792 | 7.55 | 0.740 | 14.93 | 0.801 | 14.93 | 0.801 | 1.81 | 0.82 | | |
| 13.44 | 0.732 | 4.07 | 0.728 | 7.63 | 0.782 | 7.55 | 0.725 | 14.96 | 0.819 | 14.96 | 0.819 | 2.52 | 0.81 | | |
| 13.72 | 0.726 | 4.15 | 0.728 | 7.83 | 0.782 | 7.55 | 0.729 | 15.00 | 0.827 | 15.00 | 0.827 | 3.38 | 0.81 | | |
| 13.93 | 0.726 | 4.28 | 0.728 | 7.83 | 0.782 | 7.55 | 0.744 | CURVE 16 | | | | | | | |
| 14.21 | 0.721 | 4.33 | 0.722 | 8.04 | 0.777 | 7.55 | 0.735 | T = 2000. | | | | | | | |
| 14.46 | 0.721 | 4.47 | 0.736 | 8.12 | 0.767 | 7.55 | 0.740 | CURVE 19 | | | | | | | |
| 14.67 | 0.721 | 4.53 | 0.736 | 8.15 | 0.736 | 7.55 | 0.755 | T = 755. | | | | | | | |
| 14.95 | 0.724 | 4.71 | 0.736 | 8.20 | 0.750 | 7.55 | 0.755 | 0.490 | 0.83 | 0.490 | 0.83 | 2.46 | 0.694 | | |
| CURVE 15 (CONT.) | | | | | | | | | | | | | | | |
| 4.01 | 0.739 | 4.06 | 0.745 | 8.24 | 0.724 | 8.29 | 0.737 | 0.546 | 0.73 | 0.546 | 0.73 | 2.71 | 0.646 | | |
| 4.86 | 0.745 | 5.11 | 0.743 | 8.29 | 0.737 | 8.35 | 0.741 | 0.614 | 0.36 | 0.614 | 0.36 | 2.92 | 0.724 | | |
| 5.11 | 0.743 | 5.17 | 0.757 | 8.35 | 0.705 | 8.40 | 0.741 | 0.630 | 0.27 | 0.630 | 0.27 | 3.21 | 0.722 | | |
| 5.17 | 0.757 | 5.23 | 0.746 | 8.40 | 0.721 | 8.46 | 0.752 | 0.674 | 0.23 | 0.674 | 0.23 | 3.49 | 0.764 | | |
| 5.23 | 0.746 | 5.27 | 0.754 | 8.46 | 0.721 | 8.51 | 0.744 | 0.923 | 0.36 | 0.923 | 0.36 | 3.71 | 0.831 | | |
| 5.27 | 0.754 | 5.49 | 0.754 | 8.51 | 0.703 | 8.65 | 0.756 | 1.21 | 0.72 | 1.21 | 0.72 | | | | |
| 5.49 | 0.754 | 5.54 | 0.754 | 8.65 | 0.703 | 8.70 | 0.749 | 2.77 | 0.72 | 2.77 | 0.72 | | | | |
| 5.54 | 0.462 | 5.58 | 0.766 | 8.70 | 0.681 | 8.75 | 0.755 | 3.44 | 0.78 | 3.44 | 0.78 | | | | |
| 5.58 | 0.464 | 8.75 | 0.756 | 8.75 | 0.693 | 12.27 | 0.747 | 3.71 | 0.831 | 3.71 | 0.831 | | | | |

TABLE 13-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| 3.96 | 0.773 | 13.88 | 0.755 | 0.72 | 0.727 | 3.78 | 0.774 | 13.50 | 0.716 | 8.52 | 0.736 |
| 4.21 | 0.798 | 14.23 | 0.757 | 8.95 | 0.718 | 3.77 | 0.764 | 13.75 | 0.716 | 8.78 | 0.731 |
| 4.45 | 0.774 | 14.39 | 0.761 | 9.19 | 0.709 | 3.99 | 0.769 | 13.98 | 0.713 | 9.01 | 0.723 |
| 4.76 | 0.792 | 14.73 | 0.755 | 9.47 | 0.740 | 4.27 | 0.773 | 14.23 | 0.711 | 9.25 | 0.708 |
| 4.88 | 0.775 | 14.90 | 0.754 | 9.70 | 0.764 | 4.49 | 0.768 | 14.51 | 0.724 | 9.49 | 0.720 |
| 5.17 | 0.785 | 15.21 | 0.737 | 9.92 | 0.787 | 4.81 | 0.762 | 14.73 | 0.715 | 9.77 | 0.741 |
| 5.42 | 0.783 | | | 10.23 | 0.813 | 5.02 | 0.770 | 14.98 | 0.722 | 9.97 | 0.765 |
| 5.69 | 0.781 | | | 10.46 | 0.813 | 5.30 | 0.773 | | | 10.26 | 0.779 |
| 5.92 | 0.768 | | | 10.72 | 0.817 | 5.52 | 0.773 | CURVE 22 | | 10.52 | 0.800 |
| 6.18 | 0.768 | | | 10.95 | 0.798 | 5.76 | 0.771 | T = 1255. | | 10.76 | 0.801 |
| 6.41 | 0.752 | | | 11.19 | 0.775 | 6.01 | 0.775 | | | 11.01 | 0.793 |
| 6.68 | 0.766 | 1.26 | 0.619 | 11.48 | 0.746 | 6.30 | 0.770 | 1.26 | 0.619 | 11.27 | 0.777 |
| 6.94 | 0.751 | 1.41 | 0.611 | 11.71 | 0.719 | 6.52 | 0.765 | 1.50 | 0.647 | 11.51 | 0.754 |
| 7.18 | 0.762 | 1.63 | 0.684 | 11.91 | 0.719 | 6.72 | 0.764 | 1.72 | 0.679 | 11.72 | 0.734 |
| 7.40 | 0.760 | 1.91 | 0.673 | 12.17 | 0.706 | 7.04 | 0.764 | 1.97 | 0.700 | 12.04 | 0.712 |
| 7.69 | 0.760 | 2.18 | 0.710 | 12.42 | 0.685 | 7.29 | 0.761 | 2.24 | 0.727 | 12.24 | 0.693 |
| 7.92 | 0.764 | 2.42 | 0.707 | 12.54 | 0.642 | 7.55 | 0.755 | 2.47 | 0.759 | 12.50 | 0.677 |
| 8.15 | 0.755 | 2.67 | 0.735 | 12.70 | 0.650 | 7.76 | 0.752 | 2.73 | 0.787 | 12.76 | 0.659 |
| 8.43 | 0.746 | 2.93 | 0.735 | 12.94 | 0.689 | 8.04 | 0.753 | 2.98 | 0.781 | 12.97 | 0.670 |
| 8.70 | 0.739 | 3.15 | 0.757 | 13.22 | 0.719 | 8.29 | 0.748 | 3.26 | 0.786 | 13.25 | 0.701 |
| 8.95 | 0.736 | 3.41 | 0.739 | 13.42 | 0.739 | 8.52 | 0.740 | 3.49 | 0.820 | 13.46 | 0.729 |
| 9.18 | 0.707 | 3.70 | 0.772 | 13.71 | 0.742 | 8.77 | 0.731 | 3.79 | 0.790 | 13.74 | 0.726 |
| 9.44 | 0.744 | 3.92 | 0.765 | 13.92 | 0.760 | 9.02 | 0.721 | 4.03 | 0.797 | 13.99 | 0.726 |
| 9.69 | 0.780 | 4.18 | 0.785 | 14.21 | 0.754 | 9.27 | 0.712 | 4.26 | 0.804 | 14.25 | 0.723 |
| 9.91 | 0.792 | 4.44 | 0.765 | 14.45 | 0.757 | 9.54 | 0.726 | 4.54 | 0.783 | 14.48 | 0.723 |
| 10.17 | 0.846 | 4.70 | 0.779 | 14.72 | 0.743 | 9.78 | 0.755 | 4.76 | 0.773 | 14.72 | 0.720 |
| 10.43 | 0.833 | 4.94 | 0.779 | 14.99 | 0.745 | 10.01 | 0.771 | 5.00 | 0.771 | 14.99 | 0.723 |
| 10.66 | 0.835 | 5.18 | 0.770 | 15.19 | 0.737 | 10.22 | 0.781 | 5.29 | 0.771 | 15.26 | 0.723 |
| 10.90 | 0.786 | 5.43 | 0.766 | | | 10.52 | 0.794 | 5.53 | 0.777 | | |
| 11.12 | 0.761 | 5.71 | 0.771 | | | 10.75 | 0.791 | 5.79 | 0.771 | CURVE 23 | |
| 11.40 | 0.747 | 6.20 | 0.764 | | | 11.00 | 0.784 | 6.03 | 0.773 | T = 1073. | |
| 11.65 | 0.724 | 6.44 | 0.773 | | | 11.25 | 0.761 | 6.27 | 0.770 | | |
| 11.93 | 0.686 | 6.68 | 0.766 | 1.26 | 0.639 | 11.49 | 0.744 | 6.52 | 0.765 | 2.00 | 0.699 |
| 12.13 | 0.665 | 6.95 | 0.760 | 1.50 | 0.662 | 11.75 | 0.727 | 6.79 | 0.766 | 3.00 | 0.761 |
| 12.39 | 0.648 | 7.21 | 0.761 | 1.78 | 0.665 | 12.00 | 0.700 | 7.02 | 0.766 | 4.00 | 0.821 |
| 12.67 | 0.686 | 7.45 | 0.763 | 2.00 | 0.694 | 12.26 | 0.679 | 7.29 | 0.756 | 5.00 | 0.825 |
| 12.92 | 0.704 | 7.72 | 0.760 | 2.25 | 0.706 | 12.50 | 0.658 | 7.53 | 0.753 | 6.00 | 0.610 |
| 13.18 | 0.733 | 7.98 | 0.756 | 2.52 | 0.716 | 12.73 | 0.645 | 7.77 | 0.749 | 7.00 | 0.842 |
| 13.40 | 0.738 | 8.23 | 0.754 | 3.01 | 0.746 | 12.98 | 0.670 | 8.01 | 0.748 | 8.00 | 0.892 |
| 13.67 | 0.757 | 8.49 | 0.735 | 3.24 | 0.750 | 13.24 | 0.702 | 8.25 | 0.745 | 9.00 | 0.921 |

TABLE 13-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ |
|------------------|------------|
| CURVE 23 (CONT.) | |
| 10.00 | 0.929 |
| 11.00 | 0.796 |
| 12.00 | 0.708 |
| 13.00 | 0.726 |
| 14.00 | 0.833 |

b. Normal Spectral Emittance (Temperature Dependence)

A total of 11 sets of data are available. Five sets of the data were measured below 1 μm . The remaining data were measured between 2 and 12 μm at temperatures ranging from 1000 to 1800 K.

The data measured between 2 and 12 μm show a positive but weak dependence on temperature. This fact is supported by Dubrovskii's measurements [T62013] (Figure 13-2, curves 16-18) at higher temperatures for a single crystal and by Morris' values [T20946] at 395 K for Globar. The temperature dependence is assumed linear for simplicity. The slope is determined by the data of Brügel [T02147] (Figure 13-4, curves 3-6 and 9) and Dubrovskii. Using this slope value, four curves were generated as recommended for Globar at 2.8, 3.8, 5.0, and 10.6 μm from room temperature to 2400 K. The uncertainty is believed to be 5 to 10% below 800 K, 5% from 800 to 1800 K, and 10% above 1800 K. For polished bulk material, four similar curves were generated as provisional. The uncertainty is believed to be as high as 30% for some specimens.

The recommended curves are shown in Figure 13-3 and the experimental curves are shown in Figure 13-4. The recommended values, the experimental measurement information, and the experimental data are tabulated in Tables 13-4, 13-5, and 13-6, respectively.

TABLE 13-4. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| GLOBAR, BULK OXIDIZED $\lambda = 2.0$ | | GLOBAR, BULK OXIDIZED $\lambda = 3.0$ | | GLOBAR, BULK OXIDIZED $\lambda = 5.0$ | | GLOBAR, BULK OXIDIZED $\lambda = 10.6$ | | BULK POLISHED $\lambda = 2.0$ | | BULK POLISHED $\lambda = 3.0$ | |
|---------------------------------------|------------|---------------------------------------|------------|---------------------------------------|------------|--|------------|-------------------------------|------------|-------------------------------|------------|
| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
| 293. | 0.862 | 293. | 0.855 | 293. | 0.879 | 293. | 0.872 | 293. | 0.711A† | 293. | 0.744A† |
| 300. | 0.862 | 300. | 0.855 | 300. | 0.879 | 300. | 0.872 | 300. | 0.711A | 300. | 0.744A |
| 400. | 0.864 | 400. | 0.857 | 400. | 0.881 | 400. | 0.874 | 400. | 0.713A | 400. | 0.746A |
| 500. | 0.867 | 500. | 0.860 | 500. | 0.884 | 500. | 0.877 | 500. | 0.716A | 500. | 0.749A |
| 600. | 0.870 | 600. | 0.863 | 600. | 0.887 | 600. | 0.880 | 600. | 0.719A | 600. | 0.752A |
| 700. | 0.872 | 700. | 0.865 | 700. | 0.889 | 700. | 0.882 | 700. | 0.721A | 700. | 0.754A |
| 800. | 0.874 | 800. | 0.867 | 800. | 0.891 | 800. | 0.884 | 800. | 0.723A | 800. | 0.756A |
| 900. | 0.877 | 900. | 0.870 | 900. | 0.894 | 900. | 0.887 | 900. | 0.726A | 900. | 0.759A |
| 1000. | 0.879 | 1000. | 0.872 | 1000. | 0.896 | 1000. | 0.889 | 1000. | 0.728A | 1000. | 0.761A |
| 1100. | 0.882 | 1100. | 0.875 | 1100. | 0.899 | 1100. | 0.892 | 1100. | 0.731A | 1100. | 0.764A |
| 1200. | 0.884 | 1200. | 0.877 | 1200. | 0.901 | 1200. | 0.894 | 1200. | 0.733A | 1200. | 0.766A |
| 1300. | 0.886 | 1300. | 0.879 | 1300. | 0.903 | 1300. | 0.896 | 1300. | 0.735A | 1300. | 0.768A |
| 1400. | 0.889 | 1400. | 0.882 | 1400. | 0.906 | 1400. | 0.899 | 1400. | 0.738A | 1400. | 0.771A |
| 1500. | 0.891 | 1500. | 0.884 | 1500. | 0.908 | 1500. | 0.901 | 1500. | 0.740A | 1500. | 0.773A |
| 1600. | 0.894 | 1600. | 0.887 | 1600. | 0.911 | 1600. | 0.904 | 1600. | 0.743A | 1600. | 0.776A |
| 1700. | 0.896 | 1700. | 0.889 | 1700. | 0.913 | 1700. | 0.906 | 1700. | 0.745A | 1700. | 0.778A |
| 1800. | 0.898 | 1800. | 0.891 | 1800. | 0.915 | 1800. | 0.908 | 1800. | 0.747A | 1800. | 0.780A |
| 1900. | 0.900 | 1900. | 0.893 | 1900. | 0.917 | 1900. | 0.910 | 1900. | 0.749A | 1900. | 0.782A |
| 2000. | 0.903 | 2000. | 0.896 | 2000. | 0.920 | 2000. | 0.913 | 2000. | 0.752A | 2000. | 0.785A |
| 2100. | 0.906 | 2100. | 0.899 | 2100. | 0.923 | 2100. | 0.916 | 2100. | 0.755A | 2100. | 0.788A |
| 2200. | 0.908 | 2200. | 0.901 | 2200. | 0.925 | 2200. | 0.918 | 2200. | 0.757A | 2200. | 0.790A |
| 2300. | 0.910 | 2300. | 0.903 | 2300. | 0.927 | 2300. | 0.920 | 2300. | 0.759A | 2300. | 0.792A |
| 2400. | 0.912 | 2400. | 0.905 | 2400. | 0.929 | 2400. | 0.922 | 2400. | 0.761A | 2400. | 0.794A |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

TABLE 13-4. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ |
|----------------------------------|------------|-----------------------------------|------------|
| BULK POLISHED $\lambda = 5.0$ | | BULK POLISHED $\lambda = 10.6$ | |
| 293. | 0.749A † | 293. | 0.771A † |
| 300. | 0.749A | 300. | 0.771A |
| 400. | 0.751A | 400. | 0.773A |
| 500. | 0.754A | 500. | 0.776A |
| 600. | 0.757A | 600. | 0.779A |
| 700. | 0.759A | 700. | 0.781A |
| 800. | 0.761A | 800. | 0.783A |
| 900. | 0.764A | 900. | 0.786A |
| 1000. | 0.766A | 1000. | 0.788A |
| 1100. | 0.769A | 1100. | 0.791A |
| 1200. | 0.771A | 1200. | 0.793A |
| 1300. | 0.773A | 1300. | 0.795A |
| 1400. | 0.776A | 1400. | 0.798A |
| 1500. | 0.778A | 1500. | 0.800A |
| 1600. | 0.781A | 1600. | 0.803A |
| 1700. | 0.783A | 1700. | 0.805A |
| 1800. | 0.785A | 1800. | 0.807A |
| 1900. | 0.787A | 1900. | 0.809A |
| 2000. | 0.790A | 2000. | 0.812A |
| 2100. | 0.793A | 2100. | 0.815A |
| 2200. | 0.795A | 2200. | 0.817A |
| 2300. | 0.797A | 2300. | 0.819A |
| 2400. | 0.799A | 2400. | 0.821A |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

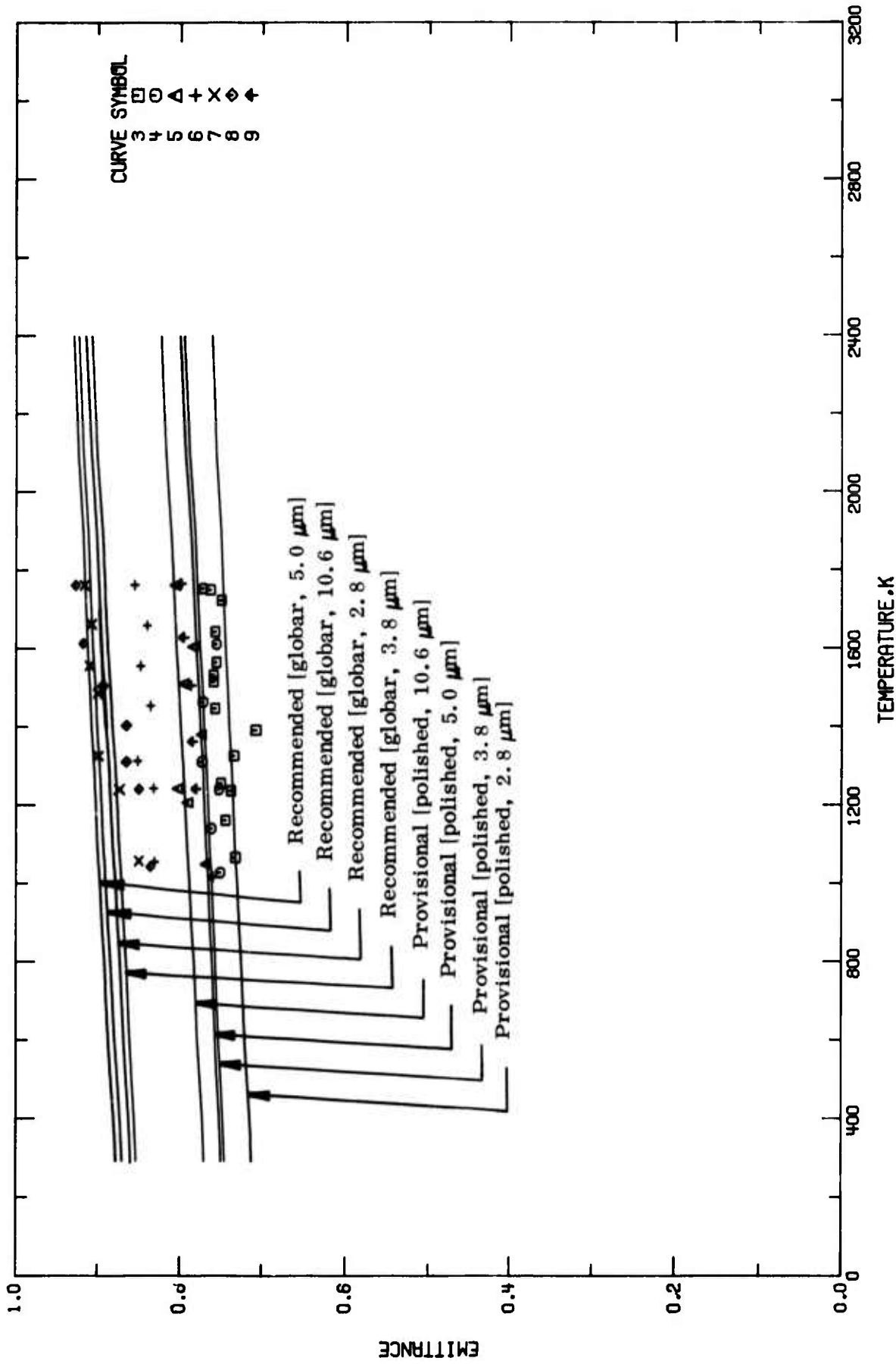


FIGURE 13-3. RECOMMENDED NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE).

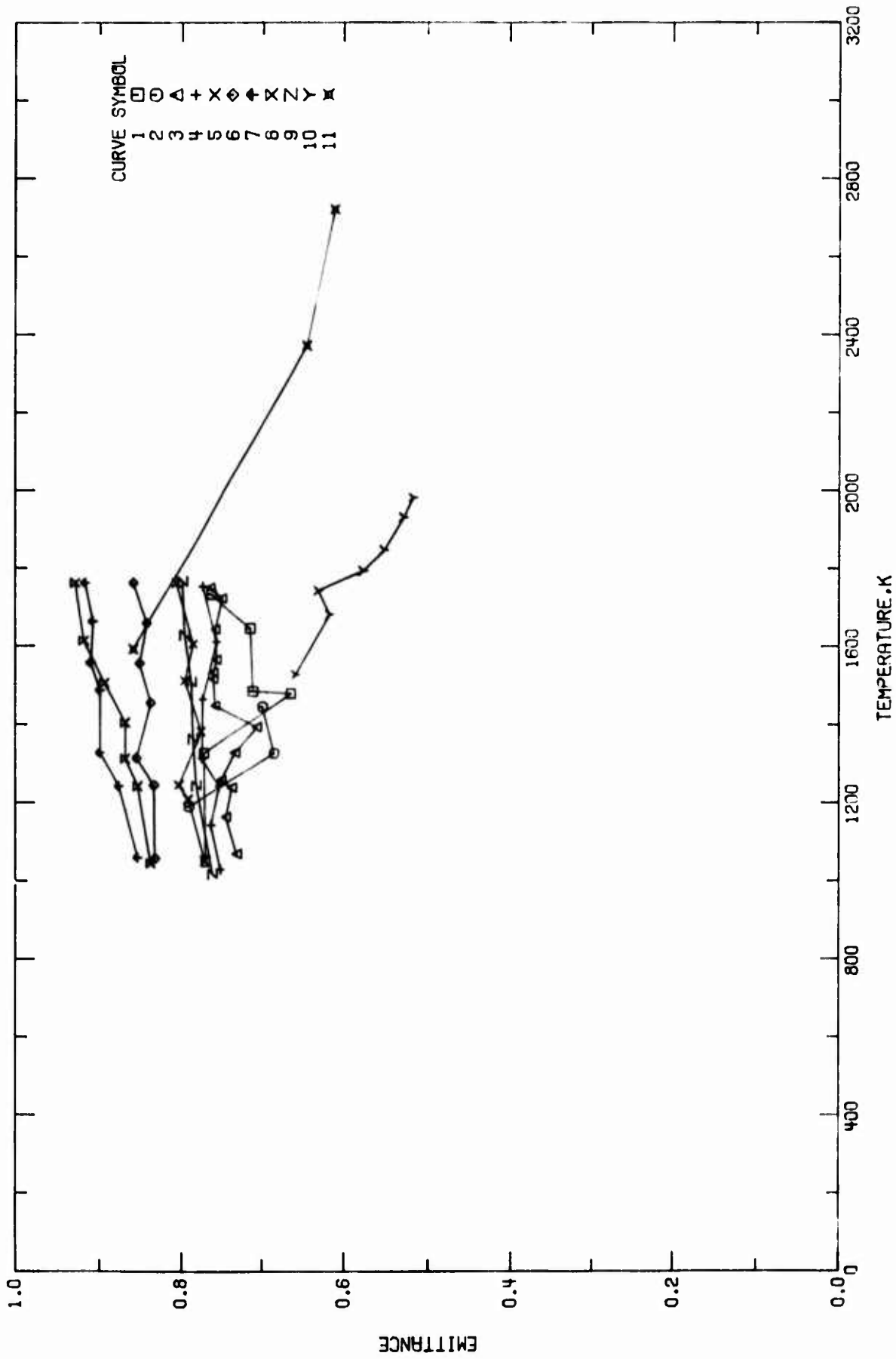


FIGURE 13-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE).

TABLE 13-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON MONOCARBIDE (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1050-1736 | | Cycle 1; $\theta' = \sim 0^\circ$. |
| 2 T10060 | Olson, O.H. and Morris, J.C. | 1959 | 0.665 | 1189-1446 | | Above specimen and conditions; cycle 2. |
| 3 T02147 | Brügel, W. | 1950 | 0.665 | 1068-1752 | | Rod specimen electrically heated. |
| 4 T02147 | Brügel, W. | 1950 | 2 | 1028-1755 | | The above specimen. |
| 5 T02147 | Brügel, W. | 1950 | 4 | 1051-1764 | | The above specimen. |
| 6 T02147 | Brügel, W. | 1950 | 6 | 1057-1764 | | The above specimen. |
| 7 T02147 | Brügel, W. | 1950 | 8 | 1059-1764 | | The above specimen. |
| 8 T02147 | Brügel, W. | 1950 | 10 | 1045-1764 | | The above specimen. |
| 9 T02147 | Brügel, W. | 1950 | 12 | 1017-1768 | | The above specimen. |
| 10 T61239 | Ko, Y.C. | 1969 | 0.665 | 1528-1983 | | Cylindrical specimen 0.25 in. in diameter and 0.5 in. long with a hole 1/16 in. in diameter and 0.25 in. deep in one end; hot-pressed; density 3.1405 g cm ⁻³ . |
| 11 T74177 | Frantsevich, I.N., Gresin, G.G., Dyban, Yu. P., Gaiduchenko, A. K., Osovitski, E. L., and Ostrovkhor, V. I. | 1972 | 0.65 | 1593-2723 | | Polycrystalline; sintered; density 3 to 3.05 g cm ⁻³ ; electrical resistivity 0.1 to 0.4 Ω cm at 293 K and 0.03 to 0.05 Ω cm at 1273 K. |

TABLE 13-6. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON CARBIDE (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ |
|------------------------------|------------|----------------|------------|-------------------|------------|
| CURVE 1 $\lambda = 0.665$ | | | | | |
| 1050. | 0.769 | 1612. | 0.755 | 1242. | 0.851 |
| 1326. | 0.771 | 1755. | 0.773 | 1313. | 0.867 |
| 1480. | 0.664 | CURVE 5 | | | |
| 1485. | 0.711 | $\lambda = 4.$ | | | |
| 1648. | 0.714 | 1051. | 0.770 | 1507. | 0.893 |
| 1736. | 0.762 | 1208. | 0.791 | 1616. | 0.917 |
| CURVE 2 | | | | | |
| $\lambda = 0.665$ | | | | | |
| 1189. | 0.790 | 1244. | 0.802 | CURVE 9 | |
| 1326. | 0.685 | 1302. | 0.775 | $\lambda = 12.$ | |
| 1446. | 0.699 | 1512. | 0.795 | 1017. | 0.760 |
| CURVE 3 | | | | | |
| $\lambda = 0.665$ | | | | | |
| 1060. | 0.730 | 1607. | 0.785 | 1243. | 0.781 |
| 1163. | 0.743 | 1764. | 0.805 | 1364. | 0.785 |
| 1238. | 0.736 | CURVE 6 | | | |
| 1257. | 0.749 | $\lambda = 6.$ | | | |
| 1328. | 0.732 | 1057. | 0.830 | 1508. | 0.767 |
| 1393. | 0.706 | 1244. | 0.831 | 1630. | 0.795 |
| 1448. | 0.757 | 1314. | 0.853 | 1768. | 0.798 |
| 1517. | 0.759 | 1456. | 0.635 | CURVE 10 | |
| 1534. | 0.759 | 1557. | 0.849 | $\lambda = 0.665$ | |
| 1566. | 0.755 | 1661. | 0.840 | 1528. | 0.658 |
| 1645. | 0.757 | 1764. | 0.857 | 1683. | 0.616 |
| 1725. | 0.748 | CURVE 7 | | | |
| 1752. | 0.763 | $\lambda = 8.$ | | | |
| CURVE 4 | | | | | |
| $\lambda = 2.$ | | | | | |
| 1028. | 0.750 | 1059. | 0.851 | CURVE 11 | |
| 1141. | 0.762 | 1242. | 0.875 | $\lambda = 0.65$ | |
| 1241. | 0.752 | 1328. | 0.898 | 1593. | 0.857 |
| 1312. | 0.774 | 1486. | 0.898 | 2373. | 0.644 |
| 1465. | 0.773 | 1559. | 0.909 | 2723. | 0.610 |
| CURVE 8 | | | | | |
| $\lambda = 10.$ | | | | | |
| 1045. | 0.835 | 1665. | 0.906 | | |
| | | 1764. | 0.915 | | |

c. Normal Spectral Reflectance (Wavelength Dependence)

A total of 38 sets of data are available. Fourteen sets were measured on single crystals, two on thin films, and seventeen on compact powder specimens.

Only three sets of data were measured for polycrystalline specimens, and two of them were measured at below $2.7 \mu\text{m}$ (Figure 13-6, curves 2 and 3). Chang's data [T42979] (Figure 13-6, curve 7) were measured at room temperature from 2 to $30 \mu\text{m}$. The specimen was supplied by Carborundum Company, but without any detailed description. The behavior of this set of data is not consistent with any of the emittance data. Thus no recommendation was generated based on the experimental reflectance data. Provisional values were derived from the recommended curves of emittance, assuming the transmittance is negligible, for polished bluk material at 293 K and 2400 K. The error is estimated to be 20 to 30%. A pair of curves were generated the same way for Globar. Since the absolute values of the derived reflectance of Globar are small, they can only be considered as typical.

Provisional values at 293 K were generated in accordance with the data of Spitzer, et al. [T32822] (Figure 13-6, curve 25) for a thin film $0.06 \mu\text{m}$ thick. The uncertainty is estimated to be 15 to 30%.

The provisional and typical curves are shown in Figure 13-5 and the experimental curves are shown in Figure 13-6. The provisional and typical values, the experimental measurement information, and the experimental data are tabulated in Tables 13-7, 13-8, and 13-9, respectively.

TABLE 13-7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| BULK POLISHED T = 293 | | | BULK POLISHED T = 293 (CONT.) | | | BULK POLISHED T = 2400 | | | BULK POLISHED T = 2400 (CONT.) | | | GLOBAL, BULK OXIDIZED T = 293 | | | GLOBAL, BULK OXIDIZED T = 293 (CONT.) | | |
|-----------------------|--------|-----------|-------------------------------|-----------|--------|------------------------|--------|-----------|--------------------------------|-----------|---------|-------------------------------|---------|-----------|---------------------------------------|-----------|---------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 1.0 | 0.403 | 10.6 | 0.219 | 1.0 | 0.353 | 10.6 | 0.169 | 1.0 | 0.0998† | 10.6 | 0.1288† | 10.6 | 0.1288† | 10.6 | 0.1288† | 10.6 | 0.1288† |
| 1.2 | 0.387 | 10.8 | 0.224 | 1.2 | 0.337 | 10.8 | 0.174 | 1.2 | 0.1028 | 10.8 | 0.1318 | 10.8 | 0.1318 | 10.8 | 0.1318 | 10.8 | 0.1318 |
| 1.5 | 0.364 | 11.0 | 0.235 | 1.5 | 0.314 | 11.0 | 0.185 | 1.5 | 0.1078 | 11.0 | 0.1388 | 11.0 | 0.1388 | 11.0 | 0.1388 | 11.0 | 0.1388 |
| 1.8 | 0.342 | 11.2 | 0.251 | 1.8 | 0.292 | 11.2 | 0.201 | 1.8 | 0.1138 | 11.2 | 0.1458 | 11.2 | 0.1458 | 11.2 | 0.1458 | 11.2 | 0.1458 |
| 2.0 | 0.328 | 11.5 | 0.279 | 2.0 | 0.278 | 11.5 | 0.229 | 2.0 | 0.1188 | 11.5 | 0.1598 | 11.5 | 0.1598 | 11.5 | 0.1598 | 11.5 | 0.1598 |
| 2.2 | 0.314 | 11.8 | 0.307 | 2.2 | 0.264 | 11.8 | 0.257 | 2.2 | 0.1248 | 11.8 | 0.1748 | 11.8 | 0.1748 | 11.8 | 0.1748 | 11.8 | 0.1748 |
| 2.5 | 0.295 | 12.0 | 0.325 | 2.5 | 0.245 | 12.0 | 0.275 | 2.5 | 0.1328 | 12.0 | 0.1858 | 12.0 | 0.1858 | 12.0 | 0.1858 | 12.0 | 0.1858 |
| 2.8 | 0.279 | 12.2 | 0.343 | 2.8 | 0.229 | 12.2 | 0.293 | 2.8 | 0.1418 | 12.2 | 0.1948 | 12.2 | 0.1948 | 12.2 | 0.1948 | 12.2 | 0.1948 |
| 3.0 | 0.269 | 12.5 | 0.362 | 3.0 | 0.219 | 12.5 | 0.312 | 3.0 | 0.1488 | 12.5 | 0.2058 | 12.5 | 0.2058 | 12.5 | 0.2058 | 12.5 | 0.2058 |
| 3.2 | 0.262 | 12.6 | 0.363 | 3.2 | 0.212 | 12.6 | 0.313 | 3.2 | 0.1448 | 12.6 | 0.2078 | 12.6 | 0.2078 | 12.6 | 0.2078 | 12.6 | 0.2078 |
| 3.5 | 0.252 | 12.8 | 0.355 | 3.5 | 0.202 | 12.8 | 0.305 | 3.5 | 0.1458 | 12.8 | 0.2028 | 12.8 | 0.2028 | 12.8 | 0.2028 | 12.8 | 0.2028 |
| 3.8 | 0.246 | 13.0 | 0.338 | 3.8 | 0.196 | 13.0 | 0.288 | 3.8 | 0.1458 | 13.0 | 0.1968 | 13.0 | 0.1968 | 13.0 | 0.1968 | 13.0 | 0.1968 |
| 4.0 | 0.244 | 13.2 | 0.318 | 4.0 | 0.194 | 13.2 | 0.268 | 4.0 | 0.1418 | 13.2 | 0.1878 | 13.2 | 0.1878 | 13.2 | 0.1878 | 13.2 | 0.1878 |
| 4.2 | 0.242 | 13.3 | 0.310 | 4.2 | 0.192 | 13.3 | 0.260 | 4.2 | 0.1378 | 13.3 | 0.1798 | 13.3 | 0.1798 | 13.3 | 0.1798 | 13.3 | 0.1798 |
| 4.5 | 0.241 | 13.5 | 0.302 | 4.5 | 0.191 | 13.5 | 0.252 | 4.5 | 0.1308 | 13.5 | 0.1758 | 13.5 | 0.1758 | 13.5 | 0.1758 | 13.5 | 0.1758 |
| 4.8 | 0.241 | 13.8 | 0.300 | 4.8 | 0.191 | 13.8 | 0.250 | 4.8 | 0.1248 | 13.8 | 0.1718 | 13.8 | 0.1718 | 13.8 | 0.1718 | 13.8 | 0.1718 |
| 5.0 | 0.241 | 14.0 | 0.299 | 5.0 | 0.191 | 14.0 | 0.249 | 5.0 | 0.1218 | 14.0 | 0.1698 | 14.0 | 0.1698 | 14.0 | 0.1698 | 14.0 | 0.1698 |
| 5.2 | 0.241 | 14.2 | 0.299 | 5.2 | 0.191 | 14.2 | 0.249 | 5.2 | 0.1198 | 14.2 | 0.1678 | 14.2 | 0.1678 | 14.2 | 0.1678 | 14.2 | 0.1678 |
| 5.5 | 0.242 | 14.5 | 0.300 | 5.5 | 0.192 | 14.5 | 0.250 | 5.5 | 0.1208 | 14.5 | 0.1678 | 14.5 | 0.1678 | 14.5 | 0.1678 | 14.5 | 0.1678 |
| 5.8 | 0.243 | 14.8 | 0.301 | 5.8 | 0.193 | 14.8 | 0.251 | 5.8 | 0.1218 | 14.8 | 0.1678 | 14.8 | 0.1678 | 14.8 | 0.1678 | 14.8 | 0.1678 |
| 6.0 | 0.244 | 15.0 | 0.302 | 6.0 | 0.194 | 15.0 | 0.252 | 6.0 | 0.1228 | 15.0 | 0.1678 | 15.0 | 0.1678 | 15.0 | 0.1678 | 15.0 | 0.1678 |
| 6.2 | 0.246 | | | 6.2 | 0.196 | | | 6.2 | 0.1238 | | | | | | | | |
| 6.5 | 0.248 | | | 6.5 | 0.198 | | | 6.5 | 0.1238 | | | | | | | | |
| 6.8 | 0.250 | | | 6.8 | 0.200 | | | 6.8 | 0.1228 | | | | | | | | |
| 7.0 | 0.252 | | | 7.0 | 0.202 | | | 7.0 | 0.1228 | | | | | | | | |
| 7.2 | 0.253 | | | 7.2 | 0.203 | | | 7.2 | 0.1228 | | | | | | | | |
| 7.5 | 0.255 | | | 7.5 | 0.205 | | | 7.5 | 0.1238 | | | | | | | | |
| 7.8 | 0.260 | | | 7.8 | 0.210 | | | 7.8 | 0.1248 | | | | | | | | |
| 8.0 | 0.263 | | | 8.0 | 0.213 | | | 8.0 | 0.1258 | | | | | | | | |
| 8.2 | 0.266 | | | 8.2 | 0.216 | | | 8.2 | 0.1278 | | | | | | | | |
| 8.5 | 0.274 | | | 8.5 | 0.224 | | | 8.5 | 0.1298 | | | | | | | | |
| 8.8 | 0.284 | | | 8.8 | 0.234 | | | 8.8 | 0.1318 | | | | | | | | |
| 9.0 | 0.292 | | | 9.0 | 0.242 | | | 9.0 | 0.1338 | | | | | | | | |
| 9.2 | 0.294 | | | 9.2 | 0.244 | | | 9.2 | 0.1358 | | | | | | | | |
| 9.5 | 0.282 | | | 9.5 | 0.232 | | | 9.5 | 0.1368 | | | | | | | | |
| 9.8 | 0.259 | | | 9.8 | 0.209 | | | 9.8 | 0.1348 | | | | | | | | |
| 10.0 | 0.240 | | | 10.0 | 0.190 | | | 10.0 | 0.1318 | | | | | | | | |
| 10.2 | 0.226 | | | 10.2 | 0.176 | | | 10.2 | 0.1298 | | | | | | | | |
| 10.5 | 0.218 | | | 10.5 | 0.168 | | | 10.5 | 0.1278 | | | | | | | | |

† VALUE FOLLOWED BY A "8" IS TYPICAL.

TABLE 13-7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

| [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ] | | | |
|--|---------|-----------|---------|
| λ | ρ | λ | ρ |
| GLOBAR, BULK OXIDIZED T = 2400 (CONT.) | | | |
| 1.0 | 0.0498† | 10.6 | 0.6788† |
| 1.2 | 0.0528 | 10.8 | 0.0818 |
| 1.5 | 0.0578 | 11.0 | 0.0888 |
| 1.8 | 0.0638 | 11.2 | 0.0958 |
| 2.0 | 0.0688 | 11.5 | 0.1098 |
| 2.2 | 0.0748 | 11.8 | 0.1248 |
| 2.5 | 0.0828 | 12.0 | 0.1358 |
| 2.8 | 0.0888 | 12.2 | 0.1448 |
| 3.0 | 0.0918 | 12.5 | 0.1558 |
| 3.2 | 0.0948 | 12.8 | 0.1578 |
| 3.5 | 0.0958 | 13.0 | 0.1528 |
| 3.8 | 0.0958 | 13.2 | 0.1468 |
| 4.0 | 0.0918 | 13.5 | 0.1378 |
| 4.2 | 0.0878 | 13.8 | 0.1298 |
| 4.5 | 0.0808 | 14.0 | 0.1258 |
| 4.8 | 0.0748 | 14.2 | 0.1218 |
| 5.0 | 0.0718 | 14.5 | 0.1198 |
| 5.2 | 0.0698 | 14.8 | 0.1178 |
| 5.5 | 0.0708 | 15.0 | 0.1178 |
| 5.8 | 0.0718 | | |
| 6.0 | 0.0728 | | |
| 6.2 | 0.0738 | | |
| 6.5 | 0.0738 | | |
| 6.8 | 0.0728 | | |
| 7.0 | 0.0728 | | |
| 7.2 | 0.0728 | | |
| 7.5 | 0.0738 | | |
| 7.8 | 0.0748 | | |
| 8.0 | 0.0758 | | |
| 8.2 | 0.0778 | | |
| 8.5 | 0.0798 | | |
| 8.8 | 0.0818 | | |
| 9.0 | 0.0838 | | |
| 9.2 | 0.0858 | | |
| 9.5 | 0.0868 | | |
| 9.8 | 0.0848 | | |
| 10.0 | 0.0818 | | |
| 10.2 | 0.0798 | | |
| 10.5 | 0.0778 | | |
| GLOBAR, BULK OXIDIZED T = 2400 (CONT.) | | | |
| 1.0 | 0.447 | 1.0 | 0.447 |
| 1.1 | 0.415 | 1.1 | 0.415 |
| 1.2 | 0.387 | 1.2 | 0.387 |
| 1.3 | 0.361 | 1.3 | 0.361 |
| 1.4 | 0.336 | 1.4 | 0.336 |
| 1.5 | 0.316 | 1.5 | 0.316 |
| 1.6 | 0.298 | 1.6 | 0.298 |
| 1.8 | 0.262 | 1.8 | 0.262 |
| 2.0 | 0.232 | 2.0 | 0.232 |
| 2.2 | 0.206 | 2.2 | 0.206 |
| 2.5 | 0.174 | 2.5 | 0.174 |
| 2.8 | 0.149 | 2.8 | 0.149 |
| 3.0 | 0.136 | 3.0 | 0.136 |
| 3.2 | 0.125 | 3.2 | 0.125 |
| 3.5 | 0.111 | 3.5 | 0.111 |
| 3.8 | 0.099 | 3.8 | 0.099 |
| 4.0 | 0.092 | 4.0 | 0.092 |
| 4.2 | 0.086 | 4.2 | 0.086 |
| 4.5 | 0.078 | 4.5 | 0.078 |
| 4.8 | 0.072 | 4.8 | 0.072 |
| 5.0 | 0.068 | 5.0 | 0.068 |
| 5.2 | 0.065 | 5.2 | 0.065 |
| 5.5 | 0.061 | 5.5 | 0.061 |
| 5.8 | 0.057 | 5.8 | 0.057 |
| 6.0 | 0.055 | 6.0 | 0.055 |
| 6.2 | 0.053 | 6.2 | 0.053 |
| 6.5 | 0.051 | 6.5 | 0.051 |
| 6.8 | 0.049 | 6.8 | 0.049 |
| 7.0 | 0.048 | 7.0 | 0.048 |
| 7.2 | 0.047 | 7.2 | 0.047 |
| 7.5 | 0.046 | 7.5 | 0.046 |
| 7.8 | 0.044 | 7.8 | 0.044 |
| 8.0 | 0.044 | 8.0 | 0.044 |
| 8.2 | 0.043 | 8.2 | 0.043 |
| 8.5 | 0.038 | 8.5 | 0.038 |
| 8.8 | 0.032 | 8.8 | 0.032 |
| 9.0 | 0.027 | 9.0 | 0.027 |
| 9.2 | 0.023 | 9.2 | 0.023 |
| 9.5 | 0.017 | 9.5 | 0.017 |
| THIN FILM THICKNESS 0.06 T = 293 (CONT.) | | | |
| 9.8 | 0.016 | 9.8 | 0.016 |
| 10.0 | 0.016 | 10.0 | 0.016 |
| 10.2 | 0.016 | 10.2 | 0.016 |
| 10.5 | 0.017 | 10.5 | 0.017 |
| 10.6 | 0.018 | 10.6 | 0.018 |
| 11.0 | 0.019 | 11.0 | 0.019 |
| 11.2 | 0.022 | 11.2 | 0.022 |
| 11.4 | 0.028 | 11.4 | 0.028 |
| 11.5 | 0.040 | 11.5 | 0.040 |
| 11.6 | 0.059 | 11.6 | 0.059 |
| 11.7 | 0.073 | 11.7 | 0.073 |
| 11.8 | 0.091 | 11.8 | 0.091 |
| 11.9 | 0.122 | 11.9 | 0.122 |
| 12.0 | 0.190 | 12.0 | 0.190 |
| 12.1 | 0.298 | 12.1 | 0.298 |
| 12.2 | 0.427 | 12.2 | 0.427 |
| 12.3 | 0.578 | 12.3 | 0.578 |
| 12.3E | 0.653 | 12.3E | 0.653 |
| 12.38 | 0.667 | 12.38 | 0.667 |
| 12.40 | 0.675 | 12.40 | 0.675 |
| 12.42 | 0.678 | 12.42 | 0.678 |
| 12.46 | 0.680 | 12.46 | 0.680 |
| 12.5 | 0.682 | 12.5 | 0.682 |
| 12.54 | 0.681 | 12.54 | 0.681 |
| 12.6 | 0.676 | 12.6 | 0.676 |
| 12.64 | 0.661 | 12.64 | 0.661 |
| 12.7 | 0.620 | 12.7 | 0.620 |
| 12.8 | 0.524 | 12.8 | 0.524 |
| 12.9 | 0.435 | 12.9 | 0.435 |
| 13.0 | 0.360 | 13.0 | 0.360 |
| 13.1 | 0.289 | 13.1 | 0.289 |
| 13.2 | 0.227 | 13.2 | 0.227 |
| 13.3 | 0.189 | 13.3 | 0.189 |
| 13.5 | 0.147 | 13.5 | 0.147 |
| 13.7 | 0.121 | 13.7 | 0.121 |
| 13.8 | 0.112 | 13.8 | 0.112 |
| 14.0 | 0.100 | 14.0 | 0.100 |
| 14.2 | 0.092 | 14.2 | 0.092 |

† VALUE FOLLOWED BY A "8" IS TYPICAL.

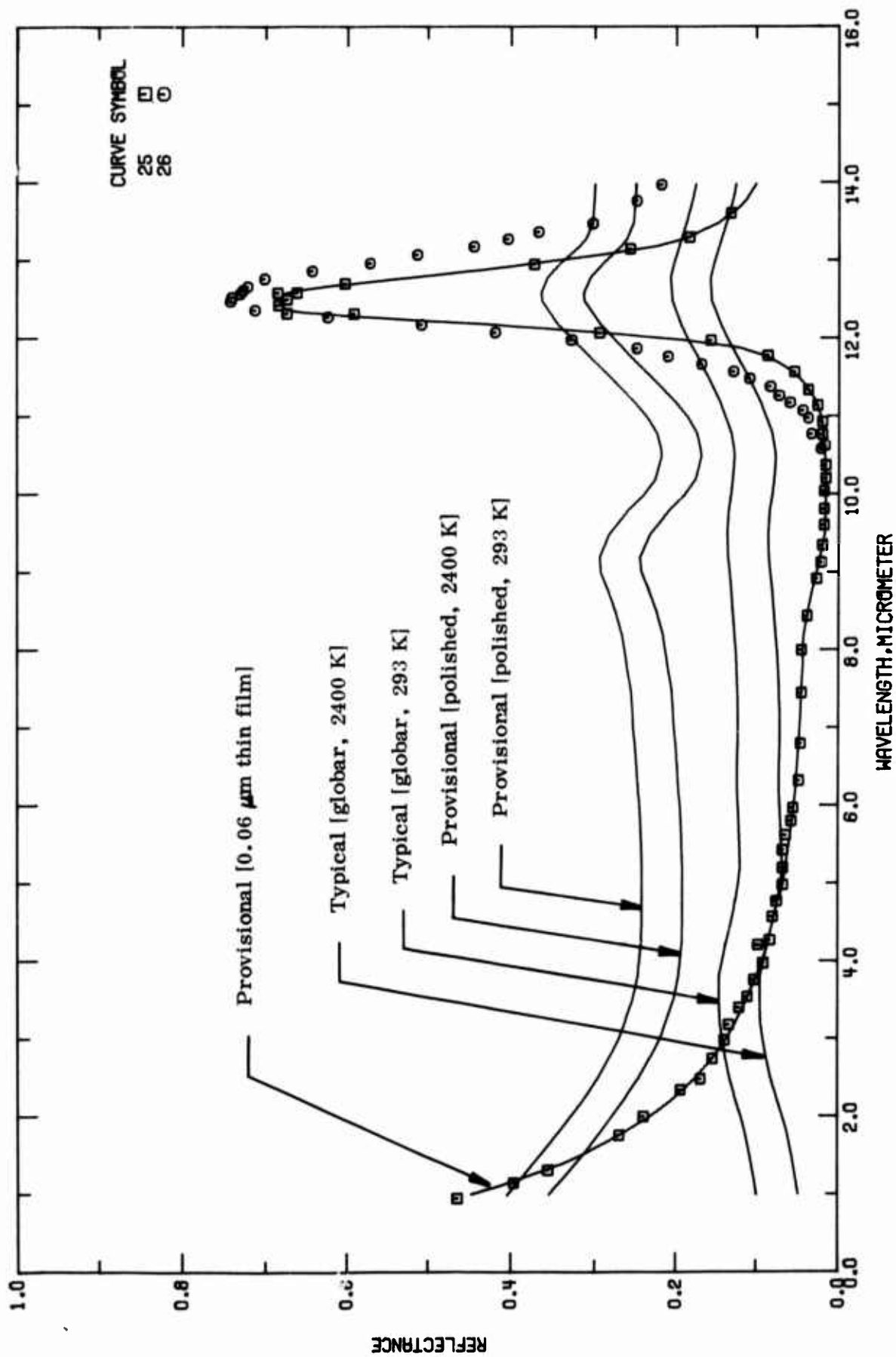


FIGURE 13-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

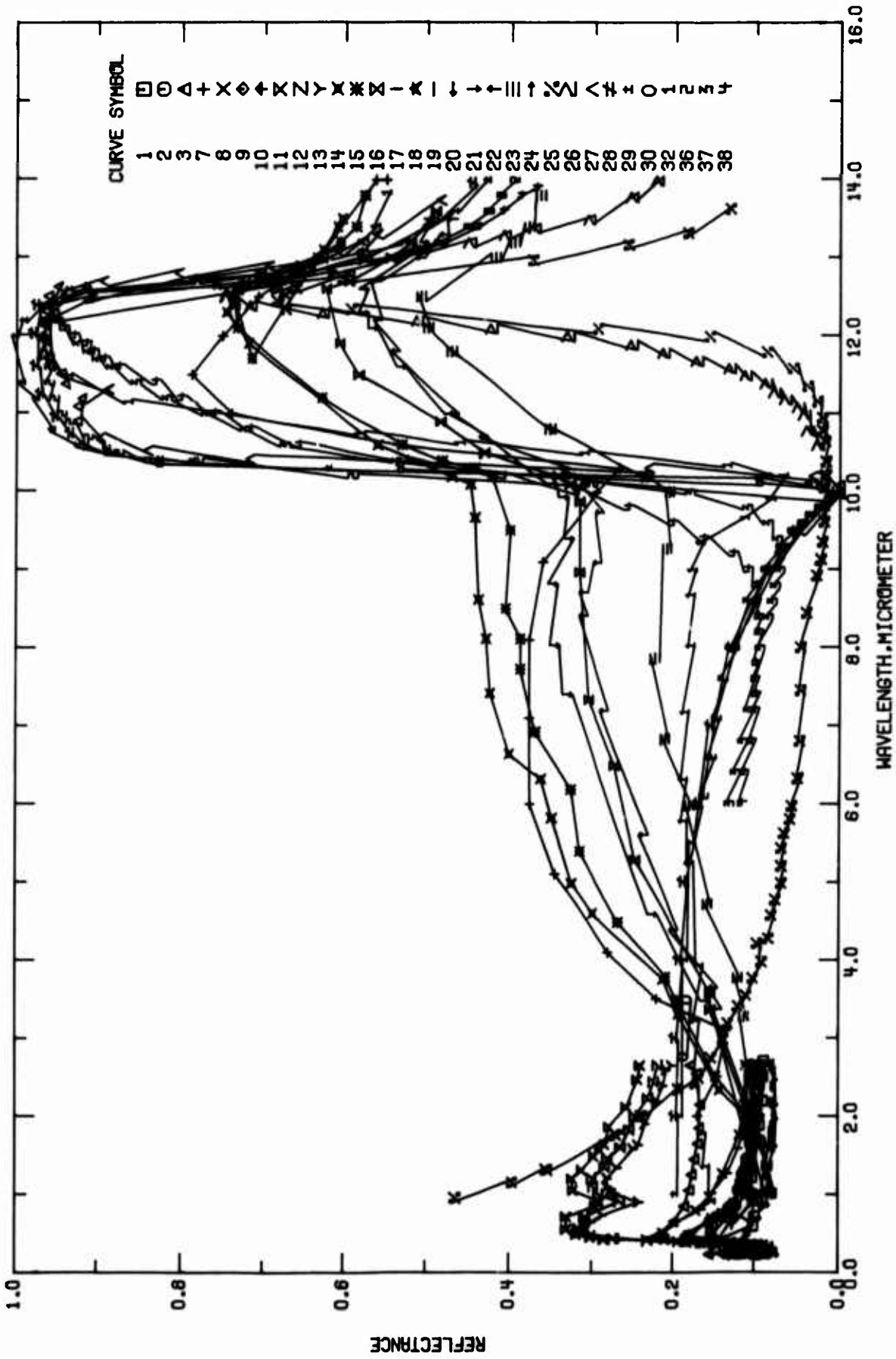


FIGURE 13-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

TABLE 13-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON MONOCARBIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | T10060 Olson, O. H. and Morris, J. C. | 1959 | 0.316-2.70 | 298 | | Magnesium carbonate reference standard; $\theta = 9^\circ$, $\omega' = 2\pi$; reported error 4%. |
| 2 | T22272 Schatz, E. A., Goldberg, D. M., Pearson, E. G., and Burks, T. L. | 1963 | 0.230-2.64 | 298 | Sample No. 102 | Commercially sintered sample from Carborundum; density 2.32 g cm ⁻³ ; theoretical density 3.21 g cm ⁻³ ; MgO reference standard; data extracted from smooth curve; $\theta = \sim 0^\circ$, $\omega' = 2\pi$. |
| 3 | T22272 Schatz, E. A., et al. | 1963 | 0.230-2.65 | 298 | Sample No. 103 | Sintered at 2173 K for 1 hr (setter material SiC); density 1.49 g cm ⁻³ ; theoretical density 3.21 g cm ⁻³ ; MgO reference standard; data extracted from smooth curve; $\theta = \sim 0^\circ$, $\omega' = 2\pi$. |
| 4 | T40808 Imai, A. | 1966 | 15.1-30.1 | 300 | B-106 | a-type; single crystal of hexagonal plate; grown in a Lely's type furnace from commercial grade or purified SiC; carrier density at 300 K 1.4 x 10 ¹⁹ cm ⁻² ; measured in argon-nitrogen; incident beam perpendicular to the c-plane; $\theta = \sim 0^\circ$, $\theta' = \sim 0^\circ$. |
| 5 | T40808 Imai, A. | 1966 | 14.5-32.5 | 300 | B-93 | Similar to the above specimen and conditions except carrier density at 300 K 3.9 x 10 ¹⁷ cm ⁻² . |
| 6 | T40908 Imai, A. | 1966 | 14.0-31.1 | 300 | B-97 | Similar to the above specimen and conditions except 15 μm thick; carrier density at 300 K 1.2 x 10 ¹⁸ cm ⁻² . |
| 7 | T42979 Chang, L. | 1965 | 2.00-29.9 | ~ 298 | | Polycrystalline (Carborundum Co.); $\theta = \sim 0^\circ$, $\theta' = \sim 0^\circ$. |
| 8 | T35840 Schatz, E. A., Alvarez, G. H., Counts, C. R., and Hoppe, M. A. | 1965 | 0.230-2.65 | ~ 298 | | Black powder from Norton Co.; 98 pure; compacted at 70,500 psi; data extracted from smooth curve; MgO reference standard; $\theta = 0^\circ$, $\omega' = 2\pi$. |
| 9 | T35840 Schatz, E. A., et al. | 1965 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except compacted at 35,250 psi. |
| 10 | T35840 Schatz, E. A., et al. | 1965 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except compacted at 11,750 psi. |
| 11 | T35840 Schatz, E. A., et al. | 1965 | 0.230-2.65 | ~ 298 | | Green powder from Norton Co.; 99.4 pure; compacted at 70,500 psi; data extracted from smooth curve; MgO reference standard; $\theta = 0^\circ$, $\omega' = 2\pi$. |
| 12 | T35840 Schatz, E. A., et al. | 1965 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except compacted at 35,250 psi. |
| 13 | T35840 Schatz, E. A., et al. | 1965 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except compacted at 11,750 psi. |
| 14 | T37398 Schatz, E. A., Counts, C. R., III, and Burks, T. L. | 1964 | 1.00-15.0 | ~ 298 | | 98.1 pure powder from Fisher Scientific Co.; mesh size 320; compacted at 1400 psi with highly polished stainless steel ram; data extracted from smooth curve; converted from reflectance factor; $\theta = 0^\circ$, $\omega' = 2\pi$. |
| 15 | T37398 Schatz, E. A., et al. | 1964 | 1.00-15.0 | ~ 298 | | Similar to the above specimen and conditions except compacted at 7000 psi; $\theta = \sim 0^\circ$. |
| 16 | T37398 Schatz, E. A., et al. | 1964 | 1.00-15.0 | ~ 298 | | Similar to the above specimen and conditions except compacted at 28,000 psi. |
| 17 | T37398 Schatz, E. A., et al. | 1964 | 0.230-2.65 | ~ 298 | | 98.1 pure powder (regular crystalline, Norton Co.); particle size 7 μm ; compacted at 23,500 psi with highly polished stainless steel ram; data extracted from smooth curve; MgO reference standard; $\theta = 0^\circ$, $\omega' = 2\pi$. |
| 18 | T37398 Schatz, E. A., et al. | 1964 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except particle size 30 μm ; $\theta = \sim 0^\circ$. |
| 19 | T37398 Schatz, E. A., et al. | 1964 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except particle size 70 μm . |
| 20 | T37398 Schatz, E. A., et al. | 1964 | 0.230-2.65 | ~ 298 | | Similar to the above specimen and conditions except particle size 160 μm . |
| 21 | T37398 Schatz, E. A., et al. | 1964 | 1.00-15.0 | ~ 298 | | 98.1 pure powder (regular crystalline, Norton Co.); particle size 7 μm ; compacted at 42,000 psi with highly polished stainless steel ram; data extracted from smooth curve; converted from reflectance factor; $\theta = 0^\circ$, $\omega' = 2\pi$. |

TABLE 13-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON MONOCARBIDE (Wavelength Dependence) (continued)

| Cur. No. | Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|----------|------------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 22 | T37398 | Schatz, E. A., Counts, C. R., III, and Barks, T. L. | 1964 | 1.00-15.0 | ~298 | | Similar to the above specimen and conditions except particle size 30 μm ; $\theta \approx 0^\circ$. |
| 23 | T37398 | Schatz, E. A., et al. | 1964 | 1.00-15.0 | ~298 | | Similar to the above specimen and conditions except particle size 70 μm . |
| 24 | T37398 | Schatz, E. A., et al. | 1964 | 0.230-2.65 | ~298 | | 98.1 pure powder, Norton Co.; mesh size 400; compacted with highly polished stainless steel ram; data extracted from smooth curve; MgO reference standard; $\theta = 0^\circ$, $\omega' = 2^\circ$. |
| 25 | T32822 E17420 | Spitzer, W. G., Kleinman, D. A., and Frosch, C. J. | 1959 | 0.95-14 | 293 | | β -phase polycrystalline cubic SiC film 0.06 μm thick; measured by comparing reflected energy from the specimen with that from a good-quality front-surface aluminum mirror; $\theta = 0^\circ$. |
| 26 | T32822 E17420 | Spitzer, W. G., et al. | 1959 | 11-14 | 293 | | Similar to the above except specimen thickness 0.12 μm . |
| 27 | T25821 E17420 | Spitzer, W. G., Kleinman, D., and Walsh, D. | 1959 | 8.0-15 | 293 | | α -II hexagonal; about 3 mm high and larger than 25 mm ² in basal area; supplied by Exolon Corp.; surface polished, oxidized at 1273 K for 2 hr, then washed by HF; measured for extraordinary ray with electric vector polarized parallel to optic axis (lying in surface); $\theta \approx 0^\circ$. |
| 28 | T32821 E17420 | Spitzer, W. G., et al. | 1959 | 2.0-22 | 293 | | The above specimen measured for ordinary ray with electric vector polarized perpendicular to optic axis. |
| 29 | E3607 | Lely, J. A. and Kröger, F. A. | 1958 | 1.0-15 | 293 | | Hexagonal; colorless; single crystal; measured with unpolarized light normal to a plane perpendicular to c-axis; data taken from smooth curve; $\theta = 0^\circ$. |
| 30 | E17415 | Lipson, H. G. | 1960 | 2.77, 3.5 | 293 | | α -II hexagonal; values calculated from measured transmittance. |
| 31 | E17419 | Philipp, H. R. and Taft, E. A. | 1960 | 0.11-1.2 | 300 | | Type 6H hexagonal; data measured by using a vacuum grating monochromator. |
| 32 | T22517 | Coblenz, W. W. | 1906 | 0.90-14 | 293 | Carborundum | No details reported. |
| 33 | T43162 | Wheeler, B. E. | 1966 | 0.096-0.41 | 293 | | 6H hexagonal single crystal; data taken from smooth curve |
| 34 | T43162 | Wheeler, B. E. | 1966 | 0.096-0.41 | 293 | | β -phase cubic single crystal; data taken from smooth curve. |
| 35 | T72608 | Purtseladze, I. M. and Khavtasi, L. G. | 1971 | 0.18-2.5 | 300 | | Type 27R; α -phase; nitrogen doped; 150 to 200 μ thick; mechanically ground and polished; difference between donor and acceptor concentrations $N_D - N_A = 2 \times 10^{17} \text{ cm}^{-3}$. |
| 36 | T64949 | Il'in, M. A., Kulkharidi, A. A., Rashevskaya, E. P., and Subashiev, V. K. | 1971 | 6.1-44 | 293 | 1 | 6H hexagonal single crystal; prepared by recrystallization; electrical conductivity 20 to 25 $\Omega^{-1} \text{ cm}^{-1}$; carrier concentration $1.1 \times 10^{17} \text{ cm}^{-3}$. |
| 37 | T64949 | Il'in, M. A., et al. | 1971 | 6.0-44 | 293 | 4 | Similar to the above specimen except electrical conductivity 66 to 71 $\Omega^{-1} \text{ cm}^{-1}$ and carrier concentration $6.8 \times 10^{17} \text{ cm}^{-3}$. |
| 38 | T64949 | Il'in, M. A., et al. | 1971 | 6.0-44 | 293 | 6 | Similar to the above specimen except electrical conductivity 103 to 105 $\Omega^{-1} \text{ cm}^{-1}$ and carrier concentration $1.36 \times 10^{18} \text{ cm}^{-3}$. |

TABLE 13-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|--|
| CURVE 1 | | | | | | | | | | | | | | |
| T = 298. | | | | | | | | | | | | | | |
| 0.316 | 0.147 | 2.45 | 0.100 | 22.0 | 0.405 | 28.0 | 0.304 | 3.10 | 0.134 | 0.796 | 0.171 | | | |
| 0.397 | 0.149 | 2.55 | 0.103 | 23.0 | 0.412 | 28.5 | 0.300 | 3.50 | 0.221 | 0.964 | 0.154 | | | |
| 0.600 | 0.130 | 2.65 | 0.103 | 24.0 | 0.431 | 29.0 | 0.293 | 4.0 | 0.279 | 1.25 | 0.138 | | | |
| 0.921 | 0.100 | CURVE 3 | | | | | | | | | | | | |
| 1.00 | 0.102 | T = 298. | | | | | | | | | | | | |
| 1.22 | 0.102 | 0.230 | 0.155 | 27.0 | 0.443 | 30.5 | 0.291 | 5.10 | 0.345 | 1.76 | 0.118 | | | |
| 1.35 | 0.108 | 0.240 | 0.140 | 29.0 | 0.466 | 31.5 | 0.291 | 6.00 | 0.374 | 2.14 | 0.111 | | | |
| 1.70 | 0.097 | 0.250 | 0.130 | 29.1 | 0.466 | 31.5 | 0.291 | 7.10 | 0.375 | 2.65 | 0.110 | | | |
| 1.89 | 0.093 | 0.270 | 0.117 | 30.1 | 0.466 | 32.5 | 0.291 | 8.10 | 0.375 | CURVE 9 | | | | |
| 2.20 | 0.085 | T = 298. | | | | | | | | | | | | |
| 2.41 | 0.093 | CURVE 5* | | | | | | | | | | | | |
| 2.51 | 0.089 | T = 300. | | | | | | | | | | | | |
| 2.71 | 0.068 | 14.5 | 0.400 | 14.0 | 0.440 | 14.0 | 0.440 | 12.5 | 0.706 | 0.230 | 0.104 | | | |
| CURVE 2 | | | | | | | | | | | | | | |
| T = 298. | | | | | | | | | | | | | | |
| 0.230 | 0.095 | 15.0 | 0.380 | 15.0 | 0.375 | 15.0 | 0.390 | 13.0 | 0.631 | 0.252 | 0.090 | | | |
| 0.240 | 0.090 | 15.5 | 0.350 | 16.0 | 0.347 | 15.0 | 0.375 | 14.0 | 0.552 | 0.284 | 0.086 | | | |
| 0.250 | 0.088 | 16.0 | 0.320 | 16.5 | 0.342 | 15.5 | 0.375 | 14.0 | 0.550 | 0.330 | 0.091 | | | |
| 0.260 | 0.089 | 16.5 | 0.290 | 17.0 | 0.332 | 16.0 | 0.361 | 15.0 | 0.530 | 0.347 | 0.096 | | | |
| 0.280 | 0.090 | 17.0 | 0.220 | 17.6 | 0.326 | 17.0 | 0.338 | 16.0 | 0.520 | 0.427 | 0.181 | | | |
| 0.290 | 0.093 | 18.0 | 0.185 | 18.0 | 0.320 | 18.0 | 0.333 | 18.0 | 0.497 | 0.466 | 0.181 | | | |
| 0.320 | 0.099 | 18.5 | 0.179 | 18.5 | 0.317 | 19.0 | 0.327 | 19.9 | 0.488 | 0.701 | 0.147 | | | |
| 0.330 | 0.104 | 19.0 | 0.176 | 19.0 | 0.313 | 20.0 | 0.332 | 22.0 | 0.488 | 0.840 | 0.131 | | | |
| 0.340 | 0.105 | 19.4 | 0.173 | 19.4 | 0.311 | 21.0 | 0.332 | 24.0 | 0.488 | 1.04 | 0.117 | | | |
| 0.350 | 0.111 | 1.65 | 0.169 | 20.0 | 0.310 | 22.0 | 0.327 | 26.0 | 0.488 | 1.28 | 0.110 | | | |
| 0.410 | 0.148 | 1.85 | 0.167 | 20.5 | 0.306 | 23.0 | 0.327 | 27.9 | 0.489 | 1.46 | 0.102 | | | |
| 0.493 | 0.152 | 2.15 | 0.166 | 21.0 | 0.303 | 24.0 | 0.327 | 29.9 | 0.491 | 2.00 | 0.092 | | | |
| 0.510 | 0.150 | 2.55 | 0.170 | 21.5 | 0.300 | 25.0 | 0.329 | 29.9 | 0.491 | 2.65 | 0.090 | | | |
| 0.751 | 0.134 | 2.65 | 0.178 | 22.0 | 0.295 | 26.0 | 0.329 | CURVE 10 | | | | | | |
| 0.850 | 0.121 | T = 298. | | | | | | | | | | | | |
| 1.05 | 0.119 | 22.5 | 0.294 | 27.0 | 0.294 | 28.0 | 0.342 | 0.230 | 0.107 | 0.230 | 0.101 | | | |
| 1.15 | 0.115 | 23.0 | 0.292 | 28.0 | 0.292 | 28.0 | 0.336 | 0.261 | 0.086 | 0.261 | 0.086 | | | |
| 1.25 | 0.114 | 23.5 | 0.292 | 30.0 | 0.292 | 30.0 | 0.336 | 0.280 | 0.083 | 0.280 | 0.083 | | | |
| 1.45 | 0.108 | 24.0 | 0.295 | 31.1 | 0.295 | 31.1 | 0.334 | 0.328 | 0.064 | 0.328 | 0.064 | | | |
| 1.65 | 0.104 | 24.5 | 0.294 | CURVE 7 | | | | | 0.340 | 0.089 | 0.340 | 0.089 | | |
| 1.85 | 0.102 | 25.0 | 0.293 | T = 298. | | | | | 0.348 | 0.093 | 0.348 | 0.093 | | |
| 2.15 | 0.100 | 25.5 | 0.293 | 2.00 | 0.169 | 2.50 | 0.145 | 0.350 | 0.115 | 0.350 | 0.105 | | | |
| | | 26.0 | 0.291 | 2.00 | 0.169 | 2.50 | 0.145 | 0.395 | 0.209 | 0.401 | 0.157 | | | |
| | | 27.0 | 0.293 | 2.50 | 0.145 | 2.50 | 0.145 | 0.425 | 0.212 | 0.608 | 0.133 | | | |
| | | 27.5 | 0.290 | 27.5 | 0.290 | 27.5 | 0.290 | 0.443 | 0.212 | 0.805 | 0.121 | | | |

NOT SHOWN IN FIGURE.

TABLE 13-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T , K; REFLECTANCE, ρ)

| CURVE 10 (CONT.) | | | CURVE 12 (CONT.) | | | CURVE 13 (CONT.) | | | CURVE 14 (CONT.) | | | CURVE 15 (CONT.) | | | CURVE 17 (CONT.) | | | | | |
|------------------|--------|------------|------------------|------------|--------|------------------|--------|------------|------------------|-----------|------------|------------------|--------|-----------|------------------|-----------|--------|-------|-------|-------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | | | |
| 1.03 | 0.108 | 0.240 | 0.115 | 0.356 | 0.122 | 0.356 | 0.122 | 9.67 | 0.442 | 13.4 | 0.585 | 0.230 | 0.109 | 0.230 | 0.127 | 0.327 | 0.109 | | | |
| 1.31 | 0.100 | 0.249 | 0.105 | 0.380 | 0.141 | 0.380 | 0.141 | 10.1 | 0.447 | 13.8 | 0.575 | 0.239 | 0.113 | 0.249 | 0.103 | 0.336 | 0.113 | | | |
| 1.74 | 0.093 | 0.268 | 0.099 | 0.416 | 0.232 | 0.416 | 0.232 | 10.2 | 0.460 | 14.5 | 0.569 | 0.260 | 0.119 | 0.268 | 0.119 | 0.338 | 0.119 | | | |
| 2.65 | 0.086 | 0.294 | 0.097 | 0.438 | 0.263 | 0.438 | 0.263 | 10.6 | 0.560 | 15.0 | 0.565 | 0.311 | 0.119 | 0.294 | 0.119 | 0.349 | 0.119 | | | |
| CURVE 11 | | | 0.319 | 0.101 | 0.495 | 0.300 | 0.495 | 0.300 | 11.9 | 0.718 | CURVE 16 | | | 0.350 | 0.154 | 0.350 | 0.154 | 0.350 | 0.154 | |
| $T = 298.$ | | | 0.337 | 0.110 | 0.532 | 0.309 | 0.532 | 0.309 | 12.3 | 0.745 | $T = 298.$ | | | 0.391 | 0.202 | 0.391 | 0.202 | 0.391 | 0.202 | |
| 0.230 | 0.131 | 0.353 | 0.130 | 0.649 | 0.299 | 0.649 | 0.299 | 12.5 | 0.738 | 0.444 | 0.228 | 0.248 | 0.119 | 0.248 | 0.119 | 0.444 | 0.228 | 0.248 | 0.119 | |
| 0.239 | 0.120 | 0.378 | 0.160 | 0.733 | 0.285 | 0.733 | 0.285 | 12.7 | 0.700 | 0.482 | 0.164 | 0.346 | 0.118 | 0.346 | 0.118 | 0.806 | 0.164 | 0.806 | 0.164 | |
| 0.248 | 0.111 | 0.408 | 0.231 | 0.899 | 0.241 | 0.899 | 0.241 | 12.9 | 0.655 | 1.00 | 0.079 | 0.378 | 0.117 | 0.378 | 0.117 | 0.806 | 0.164 | 0.806 | 0.164 | |
| 0.260 | 0.103 | 0.432 | 0.271 | 1.01 | 0.270 | 1.01 | 0.270 | 13.1 | 0.627 | 1.36 | 0.003 | 0.408 | 0.110 | 0.408 | 0.110 | 0.912 | 0.164 | 0.912 | 0.164 | |
| 0.311 | 0.100 | 0.471 | 0.300 | 1.04 | 0.274 | 1.04 | 0.274 | 13.4 | 0.608 | 3.36 | 0.154 | 0.248 | 0.119 | 0.248 | 0.119 | 1.01 | 0.154 | 1.01 | 0.154 | |
| 0.331 | 0.106 | 0.515 | 0.314 | 1.07 | 0.274 | 1.07 | 0.274 | 13.5 | 0.602 | 3.57 | 0.154 | 0.311 | 0.106 | 0.311 | 0.106 | 1.26 | 0.154 | 1.26 | 0.154 | |
| 0.346 | 0.118 | 0.561 | 0.317 | 1.10 | 0.279 | 1.10 | 0.279 | 15.0 | 0.597 | 5.28 | 0.247 | 0.349 | 0.119 | 0.349 | 0.119 | 1.58 | 0.119 | 1.58 | 0.119 | |
| 0.349 | 0.123 | 0.643 | 0.307 | 1.21 | 0.279 | 1.21 | 0.279 | CURVE 15 | | | 6.49 | 0.272 | 6.49 | 0.272 | 1.81 | 0.111 | 1.81 | 0.111 | | |
| 0.378 | 0.165 | 0.716 | 0.309 | 1.34 | 0.267 | 1.34 | 0.267 | $T = 298.$ | | | 7.33 | 0.305 | 7.33 | 0.305 | 2.18 | 0.107 | 2.18 | 0.107 | | |
| 0.428 | 0.283 | 0.910 | 0.264 | 1.58 | 0.248 | 1.58 | 0.248 | CURVE 15 | | | 8.97 | 0.317 | 8.97 | 0.317 | 2.65 | 0.107 | 2.65 | 0.107 | | |
| 0.450 | 0.301 | 1.00 | 0.290 | 1.63 | 0.242 | 1.63 | 0.242 | $T = 298.$ | | | 9.88 | 0.317 | 9.88 | 0.317 | CURVE 18 | | | | | |
| 0.491 | 0.319 | 1.10 | 0.297 | 1.90 | 0.234 | 1.90 | 0.234 | 1.00 | 0.104 | 10.1 | 0.323 | 0.450 | 0.301 | 0.450 | 0.301 | T = 298. | | | | |
| 0.548 | 0.331 | 1.21 | 0.299 | 2.19 | 0.220 | 2.19 | 0.220 | 1.57 | 0.104 | 10.2 | 0.342 | 0.491 | 0.319 | 0.491 | 0.319 | 0.230 | 0.127 | 0.230 | 0.127 | |
| 0.710 | 0.331 | 1.35 | 0.282 | 2.39 | 0.212 | 2.39 | 0.212 | 2.50 | 0.147 | 10.5 | 0.431 | 0.548 | 0.331 | 0.548 | 0.331 | 0.249 | 0.103 | 0.249 | 0.103 | |
| 0.850 | 0.295 | 1.46 | 0.279 | 2.59 | 0.208 | 2.59 | 0.208 | 3.48 | 0.195 | 10.9 | 0.482 | 0.710 | 0.331 | 0.710 | 0.331 | 0.298 | 0.101 | 0.298 | 0.101 | |
| 0.883 | 0.289 | 1.60 | 0.263 | 2.65 | 0.201 | 2.65 | 0.201 | 3.78 | 0.209 | 11.5 | 0.502 | 0.850 | 0.295 | 0.850 | 0.295 | 0.330 | 0.103 | 0.330 | 0.103 | |
| 0.915 | 0.289 | 1.83 | 0.253 | CURVE 14 | | | 4.48 | 0.267 | 0.267 | 11.9 | 0.605 | 0.883 | 0.289 | 0.883 | 0.289 | 0.332 | 0.108 | 0.332 | 0.108 | |
| 1.05 | 0.323 | 2.00 | 0.246 | $T = 298.$ | | | 5.39 | 0.316 | 0.316 | 12.6 | 0.623 | 0.915 | 0.289 | 0.915 | 0.289 | 0.350 | 0.112 | 0.350 | 0.112 | |
| 1.20 | 0.324 | 2.23 | 0.231 | 1.00 | 0.107 | 1.00 | 0.107 | 6.18 | 0.327 | 12.7 | 0.593 | 1.20 | 0.324 | 1.20 | 0.324 | 0.350 | 0.112 | 0.350 | 0.112 | |
| 1.31 | 0.312 | 2.44 | 0.224 | 6.92 | 0.368 | 6.92 | 0.368 | 7.73 | 0.386 | 13.0 | 0.545 | 1.31 | 0.312 | 1.31 | 0.312 | 0.395 | 0.182 | 0.395 | 0.182 | |
| 1.49 | 0.296 | 2.65 | 0.219 | 8.12 | 0.386 | 8.12 | 0.386 | 8.50 | 0.405 | 13.6 | 0.488 | 1.49 | 0.296 | 1.49 | 0.296 | 0.424 | 0.185 | 0.424 | 0.185 | |
| 1.571 | 0.288 | CURVE 13 | | | 9.51 | 0.399 | 9.51 | 0.399 | 10.2 | 0.422 | CURVE 17 | | | 0.472 | 0.182 | 0.472 | 0.182 | 0.472 | 0.182 | |
| 1.64 | 0.282 | $T = 298.$ | | | 10.2 | 0.422 | 10.2 | 0.422 | 10.3 | 0.443 | $T = 298.$ | | | 0.624 | 0.155 | 0.624 | 0.155 | 0.624 | 0.155 | |
| 1.87 | 0.277 | 0.230 | 0.114 | 10.3 | 0.443 | 10.3 | 0.443 | 10.4 | 0.480 | 0.480 | 0.141 | 1.87 | 0.277 | 1.87 | 0.277 | 0.687 | 0.153 | 0.687 | 0.153 | |
| 2.12 | 0.256 | 0.240 | 0.103 | 10.4 | 0.480 | 10.4 | 0.480 | 10.6 | 0.530 | 0.530 | 0.147 | 2.12 | 0.256 | 2.12 | 0.256 | 0.750 | 0.141 | 0.750 | 0.141 | |
| 2.47 | 0.243 | 0.249 | 0.103 | 11.2 | 0.628 | 11.2 | 0.628 | 11.2 | 0.628 | 0.628 | 0.147 | 2.47 | 0.243 | 2.47 | 0.243 | 0.881 | 0.126 | 0.881 | 0.126 | |
| 2.65 | 0.249 | 0.251 | 0.095 | 12.1 | 0.732 | 12.1 | 0.732 | 12.1 | 0.732 | 0.732 | 0.122 | 2.65 | 0.249 | 2.65 | 0.249 | 1.04 | 0.126 | 1.04 | 0.126 | |
| CURVE 12 | | | 0.288 | 0.092 | 6.32 | 0.361 | 6.32 | 0.361 | 12.4 | 0.735 | 0.270 | 0.110 | 0.288 | 0.092 | 0.288 | 0.092 | 1.17 | 0.116 | 1.17 | 0.116 |
| $T = 298.$ | | | 0.313 | 0.096 | 7.42 | 0.424 | 7.42 | 0.424 | 12.7 | 0.714 | 0.276 | 0.107 | 0.313 | 0.096 | 0.313 | 0.096 | 1.25 | 0.111 | 1.25 | 0.111 |
| 0.230 | 0.125 | 0.331 | 0.102 | 8.12 | 0.429 | 8.12 | 0.429 | 13.0 | 0.635 | 0.298 | 0.103 | 0.230 | 0.125 | 0.230 | 0.125 | 1.33 | 0.111 | 1.33 | 0.111 | |
| | | 0.348 | 0.112 | 8.62 | 0.438 | 8.62 | 0.438 | 13.2 | 0.604 | 0.319 | 0.103 | 0.230 | 0.125 | 0.230 | 0.125 | 1.40 | 0.107 | 1.40 | 0.107 | |
| | | | | | | | | | | | | | | | | 1.65 | 0.102 | 1.65 | 0.102 | |

TABLE 13-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED).
 (WAVELENGTH, λ , μm ; TEMPERATURE, T , K ; REFLECTANCE, ρ)

| λ | | ρ | | λ | | ρ | | λ | | ρ | | λ | | ρ | |
|------------|-------|------------------|-------|------------------|-------|------------------|-------|-------------------|-------|-------------------|-------|-------------------|-------|------------|-------|
| CURVE 26 | | CURVE 27 (CONT.) | | CURVE 28 (CONT.) | | CURVE 29 (CONT.) | | CURVE 31 (CONT.)* | | CURVE 31 (CONT.)* | | CURVE 31 (CONT.)* | | CURVE 32 | |
| $T = 293.$ | | $T = 293.$ | | $T = 293.$ | | $T = 293.$ | | $T = 293.$ | | $T = 293.$ | | $T = 293.$ | | $T = 293.$ | |
| 10.59 | 0.022 | 9.96 | 0.0 | 8.98 | 0.086 | 10.1 | 0.037 | 0.121 | 0.393 | 0.413 | 0.219 | 0.153 | 0.153 | 0.153 | 0.153 |
| 10.78 | 0.034 | 10.07 | 0.0 | 9.49 | 0.053 | 10.2 | 0.085 | 0.123 | 0.393 | 0.443 | 0.215 | 0.160 | 0.160 | 0.160 | 0.160 |
| 10.98 | 0.038 | 10.19 | 0.031 | 9.99 | 0.011 | 10.3 | 0.619 | 0.126 | 0.399 | 0.475 | 0.213 | 0.164 | 0.164 | 0.164 | 0.164 |
| 11.08 | 0.045 | 10.30 | 0.231 | 10.09 | 0.024 | 10.4 | 0.786 | 0.129 | 0.404 | 0.514 | 0.209 | 0.173 | 0.173 | 0.173 | 0.173 |
| 11.18 | 0.060 | 10.41 | 0.716 | 10.14 | 0.095 | 10.5 | 0.886 | 0.131 | 0.409 | 0.564 | 0.207 | 0.181 | 0.181 | 0.181 | 0.181 |
| 11.27 | 0.073 | 10.52 | 0.839 | 10.31 | 0.533 | 10.6 | 0.925 | 0.134 | 0.415 | 0.620 | 0.202 | 0.189 | 0.189 | 0.189 | 0.189 |
| 11.39 | 0.083 | 10.69 | 0.925 | 10.38 | 0.825 | 10.8 | 0.956 | 0.138 | 0.422 | 0.713 | 0.202 | 0.199 | 0.199 | 0.199 | 0.199 |
| 11.49 | 0.108 | 10.90 | 0.925 | 10.53 | 0.887 | 11.2 | 0.975 | 0.140 | 0.432 | 0.838 | 0.199 | 0.199 | 0.199 | 0.199 | 0.199 |
| 11.58 | 0.128 | 11.09 | 0.919 | 10.60 | 0.914 | 11.4 | 0.991 | 0.144 | 0.450 | 0.984 | 0.199 | 0.199 | 0.199 | 0.199 | 0.199 |
| 11.68 | 0.168 | 11.19 | 0.919 | 10.75 | 0.934 | 12.0 | 1.000 | 0.147 | 0.473 | 1.24 | 0.199 | 0.199 | 0.199 | 0.199 | 0.199 |
| 11.78 | 0.210 | 11.31 | 0.885 | 10.97 | 0.953 | 12.0 | 0.989 | 0.149 | 0.493 | | | | | | |
| 11.88 | 0.248 | 11.38 | 0.940 | 11.26 | 0.970 | 12.4 | 0.966 | 0.150 | 0.505 | | | | | | |
| 11.99 | 0.327 | 11.51 | 0.946 | 11.62 | 0.976 | 12.6 | 0.936 | 0.152 | 0.522 | | | | | | |
| 12.09 | 0.419 | 11.61 | 0.959 | 12.04 | 0.978 | 12.7 | 0.781 | 0.154 | 0.531 | | | | | | |
| 12.19 | 0.507 | 11.72 | 0.961 | 12.40 | 0.975 | 12.8 | 0.706 | 0.156 | 0.536 | | | | | | |
| 12.29 | 0.623 | 11.93 | 0.964 | 12.62 | 0.912 | 12.9 | 0.651 | 0.158 | 0.540 | | | | | | |
| 12.38 | 0.712 | 12.13 | 0.964 | 12.66 | 0.758 | 13.0 | 0.619 | 0.160 | 0.541 | | | | | | |
| 12.49 | 0.742 | 12.32 | 0.964 | 12.82 | 0.664 | 13.1 | 0.576 | 0.162 | 0.541 | | | | | | |
| 12.54 | 0.741 | 12.51 | 0.961 | 13.04 | 0.580 | 13.2 | 0.529 | 0.166 | 0.535 | | | | | | |
| 12.59 | 0.730 | 12.63 | 0.949 | 13.51 | 0.489 | 13.4 | 0.500 | 0.172 | 0.526 | | | | | | |
| 12.63 | 0.727 | 12.70 | 0.891 | 13.96 | 0.446 | 13.6 | 0.466 | 0.176 | 0.515 | | | | | | |
| 12.68 | 0.721 | 12.80 | 0.802 | 14.48 | 0.415 | 14.0 | 0.428 | 0.181 | 0.495 | | | | | | |
| 12.78 | 0.700 | 12.89 | 0.692 | 16.00 | 0.358 | 14.3 | 0.386 | 0.187 | 0.470 | | | | | | |
| 12.88 | 0.642 | 13.08 | 0.607 | 19.01 | 0.324 | 15.0 | 0.322 | 0.193 | 0.442 | | | | | | |
| 13.09 | 0.512 | 13.21 | 0.578 | 22.00 | 0.303 | 15.4 | 0.271 | 0.199 | 0.417 | | | | | | |
| 13.19 | 0.445 | 13.30 | 0.561 | | | | | 0.207 | 0.389 | | | | | | |
| 13.29 | 0.403 | 13.74 | 0.482 | | | | | 0.213 | 0.360 | | | | | | |
| 13.38 | 0.366 | 14.47 | 0.401 | | | | | 0.219 | 0.336 | | | | | | |
| 13.49 | 0.302 | 15.00 | 0.379 | | | | | 0.229 | 0.316 | | | | | | |
| 13.78 | 0.248 | | | | | | | 0.238 | 0.299 | | | | | | |
| 13.99 | 0.218 | | | | | | | 0.257 | 0.276 | | | | | | |
| | | | | | | | | 0.268 | 0.257 | | | | | | |
| | | | | | | | | 0.281 | 0.259 | | | | | | |
| | | | | | | | | 0.294 | 0.253 | | | | | | |
| | | | | | | | | 0.310 | 0.245 | | | | | | |
| | | | | | | | | 0.325 | 0.240 | | | | | | |
| | | | | | | | | 0.345 | 0.235 | | | | | | |
| | | | | | | | | 0.363 | 0.229 | | | | | | |
| | | | | | | | | 0.389 | 0.224 | | | | | | |
| | | | | | | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 13-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μ M; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 32 (CONT.) | | | CURVE 33 (CONT.)* | | | CURVE 34 (CONT.)* | | | CURVE 35 (CONT.)* | | | CURVE 36 (CONT.) | | |
|------------------|--------|--|-------------------|--------|-----------|-------------------|----------|-------|-------------------|--------|----------|------------------|--------|--|
| λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | | λ | ρ | |
| 12.45 | 0.912 | | 0.182 | 0.722 | 0.142 | 0.392 | 0.40 | 0.200 | 9.5 | 0.056 | 36.0 | 0.259 | | |
| 12.75 | 0.786 | | 0.185 | 0.722 | 0.147 | 0.461 | 0.49 | 0.186 | 9.6 | 0.044 | 40.1 | 0.260 | | |
| 12.96 | 0.629 | | 0.190 | 0.716 | 0.148 | 0.482 | 0.58 | 0.171 | 9.7 | 0.035 | 42.1 | 0.260 | | |
| 13.23 | 0.578 | | 0.197 | 0.684 | 0.149 | 0.510 | 0.69 | 0.148 | 9.8 | 0.024 | 44.1 | 0.260 | | |
| 13.41 | 0.564 | | 0.206 | 0.640 | 0.152 | 0.536 | 0.80 | 0.133 | 9.9 | 0.012 | | | | |
| 13.84 | 0.551 | | 0.215 | 0.609 | 0.155 | 0.553 | 0.91 | 0.113 | 10.1 | 0.003 | CURVE 37 | | | |
| 14.34 | 0.534 | | 0.223 | 0.597 | 0.158 | 0.572 | 0.99 | 0.065 | 10.2 | 0.589 | T = 293. | | | |
| | | | 0.225 | 0.589 | 0.160 | 0.589 | 0.99 | 0.192 | 10.4 | 0.779 | | | | |
| | | | 0.231 | 0.577 | 0.162 | 0.583 | 1.02 | 0.440 | 10.4 | 0.637 | 6.0 | 0.132 | | |
| | | | 0.236 | 0.557 | 0.163 | 0.563 | 1.03 | 0.702 | 10.5 | 0.873 | 6.4 | 0.125 | | |
| | | | 0.243 | 0.543 | 0.165 | 0.553 | 1.06 | 0.821 | 10.7 | 0.911 | 6.8 | 0.116 | | |
| | | | 0.252 | 0.532 | 0.168 | 0.542 | 1.06 | 0.883 | 10.9 | 0.935 | 7.2 | 0.139 | | |
| | | | 0.261 | 0.526 | 0.172 | 0.537 | 1.10 | 0.914 | 11.0 | 0.945 | 8.0 | 0.095 | | |
| | | | 0.270 | 0.520 | 0.175 | 0.533 | 1.14 | 0.914 | 11.2 | 0.954 | 8.4 | 0.085 | | |
| | | | 0.276 | 0.520 | 0.178 | 0.525 | 1.19 | 0.825 | 11.4 | 0.960 | 8.6 | 0.080 | | |
| | | | 0.284 | 0.508 | 0.186 | 0.496 | 1.19 | 0.714 | 11.6 | 0.960 | 8.8 | 0.076 | | |
| | | | 0.301 | 0.501 | 0.198 | 0.457 | 1.23 | 0.619 | 11.8 | 0.964 | 9.0 | 0.071 | | |
| | | | 0.319 | 0.488 | 0.204 | 0.448 | 1.29 | 0.529 | 12.0 | 0.964 | 9.2 | 0.071 | | |
| | | | 0.369 | 0.478 | 0.209 | 0.451 | 1.45 | 0.411 | 12.2 | 0.964 | 9.4 | 0.074 | | |
| | | | 0.413 | 0.469 | 0.213 | 0.439 | 1.56 | 0.360 | 12.5 | 0.940 | 9.6 | 0.085 | | |
| | | | | | 0.217 | 0.417 | 1.66 | 0.329 | 12.6 | 0.914 | 9.8 | 0.110 | | |
| | | | | | 0.220 | 0.400 | 1.93 | 0.308 | 12.8 | 0.663 | 10.0 | 0.180 | | |
| | | | | | 0.225 | 0.380 | 2.06 | 0.308 | 13.0 | 0.542 | 10.2 | 0.329 | | |
| | | | | | 0.232 | 0.361 | 2.14 | 0.308 | 13.2 | 0.485 | 10.4 | 0.538 | | |
| | | | | | 0.240 | 0.338 | 2.22 | 0.308 | 13.4 | 0.450 | 10.6 | 0.673 | | |
| | | | | | 0.248 | 0.324 | 2.28 | 0.316 | 13.6 | 0.427 | 10.8 | 0.723 | | |
| | | | | | 0.257 | 0.313 | 2.45 | 0.316 | 13.8 | 0.412 | 11.0 | 0.769 | | |
| | | | | | 0.270 | 0.313 | 2.52 | 0.304 | 14.0 | 0.395 | 11.2 | 0.817 | | |
| | | | | | 0.282 | 0.305 | CURVE 36 | | 15.0 | 0.350 | 11.4 | 0.853 | | |
| | | | | | 0.302 | 0.294 | T = 293. | | 15.9 | 0.315 | 11.6 | 0.882 | | |
| | | | | | 0.343 | 0.284 | 6.1 | 0.163 | 16.0 | 0.305 | 11.7 | 0.900 | | |
| | | | | | 0.413 | 0.267 | 6.6 | 0.154 | 20.0 | 0.296 | 11.8 | 0.912 | | |
| | | | | | CURVE 35* | | 7.1 | 0.148 | 21.9 | 0.289 | 11.9 | 0.925 | | |
| | | | | | T = 300. | | 7.6 | 0.140 | 24.1 | 0.276 | 12.2 | 0.950 | | |
| | | | | | 0.18 | 0.219 | 8.0 | 0.126 | 26.0 | 0.274 | 12.7 | 0.979 | | |
| | | | | | 0.26 | 0.213 | 8.6 | 0.110 | 28.2 | 0.267 | 12.8 | 0.594 | | |
| | | | | | 0.34 | 0.213 | 9.0 | 0.088 | 30.1 | 0.262 | 15.0 | 0.328 | | |
| | | | | | | | 9.3 | 0.070 | 32.0 | 0.261 | 16.0 | 0.303 | | |
| | | | | | | | | | 34.2 | 0.259 | 17.0 | 0.286 | | |
| | | | | | | | | | 36.2 | 0.260 | 18.1 | 0.286 | | |

*NOT SHOWN IN FIGURE.

TABLE 13-9. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| CURVE 37 (CONT.) | | CURVE 38 (CONT.) | |
|------------------|--------|------------------|--------|
| λ | ρ | λ | ρ |
| 18.9 | 0.286 | 11.2 | 0.799 |
| 20.1 | 0.288 | 11.4 | 0.830 |
| 22.0 | 0.298 | 11.6 | 0.872 |
| 23.9 | 0.303 | 11.7 | 0.890 |
| 26.1 | 0.316 | 11.8 | 0.904 |
| 28.0 | 0.327 | 11.9 | 0.913 |
| 30.2 | 0.346 | 12.0 | 0.929 |
| 32.1 | 0.363 | 12.1 | 0.942 |
| 34.1 | 0.380 | 12.3 | 0.955 |
| 36.2 | 0.398 | 12.4 | 0.960 |
| 38.0 | 0.419 | 12.5 | 0.906 |
| 40.1 | 0.441 | 12.7 | 0.693 |
| 42.0 | 0.460 | 12.8 | 0.616 |
| 43.9 | 0.475 | 13.0 | 0.530 |
| | | 13.2 | 0.476 |
| | | 13.4 | 0.438 |
| | | 13.6 | 0.409 |
| | | 13.8 | 0.386 |
| | | 13.9 | 0.367 |
| 6.0 | 0.116 | 15.0 | 0.345 |
| 6.4 | 0.113 | 15.9 | 0.327 |
| 6.8 | 0.104 | 17.0 | 0.300 |
| 7.2 | 0.100 | 18.1 | 0.297 |
| 7.4 | 0.099 | 20.0 | 0.322 |
| 7.6 | 0.100 | 22.1 | 0.352 |
| 7.8 | 0.099 | 24.1 | 0.377 |
| 8.2 | 0.096 | 26.1 | 0.408 |
| 8.4 | 0.096 | 28.1 | 0.432 |
| 8.6 | 0.099 | 30.1 | 0.457 |
| 8.8 | 0.099 | 32.1 | 0.473 |
| 9.0 | 0.109 | 34.1 | 0.496 |
| 9.2 | 0.127 | 36.0 | 0.513 |
| 9.4 | 0.163 | 38.1 | 0.529 |
| 9.6 | 0.201 | 40.0 | 0.550 |
| 9.8 | 0.255 | 41.9 | 0.562 |
| 10.0 | 0.319 | 44.1 | 0.579 |
| 10.2 | 0.406 | | |
| 10.4 | 0.523 | | |
| 10.6 | 0.656 | | |
| 10.8 | 0.715 | | |
| 11.0 | 0.759 | | |

CURVE 38
T = 293.

d. Normal Spectral Absorptance (Wavelength Dependence)

Only four sets of data are available. Three of them were measured below 1 μm . The remaining one [T32388] was measured between 0.4 and 2.6 μm for Globar without any detailed description about the specimen.

It is impossible to generate recommended curves from the meager experimental data. However, it is adequate to apply Kirchhoff's law on the Globar and the averagely polished silicon carbide. Hence, the recommended values presented in subsection (a) are repeated here as recommended values for the normal spectral absorptance. The uncertainty of each curve is believed to be the same as that of the emittance.

The recommended and the provisional curves are shown in Figure 13-7 and the experimental curves are shown in Figure 13-8. The recommended and the provisional values, the experimental measurement information, and the experimental data are tabulated in Tables 13-10, 13-11, and 13-12, respectively.

TABLE 13-10. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | | α | | λ | | α | | λ | | α | | λ | | α | |
|-------------------------------------|-------|---|-------|--------------------------------------|-------|--|-------|--------------------------------------|-------|--|-------|--------------------------------------|--|--|--|
| GLOBAL, BULK OXIDIZED T = 293 | | GLOBAL, BULK OXIDIZED T = 293 (CONT.) | | GLOBAL, BULK OXIDIZED T = 1400 | | GLOBAL, BULK OXIDIZED T = 1400 (CONT.) | | GLOBAL, BULK OXIDIZED T = 2400 | | GLOBAL, BULK OXIDIZED T = 2400 (CONT.) | | GLOBAL, BULK OXIDIZED T = 2400 | | GLOBAL, BULK OXIDIZED T = 2400 (CONT.) | |
| 1.0 | 0.901 | 10.6 | 0.872 | 1.0 | 0.928 | 10.6 | 0.899 | 1.0 | 0.951 | 10.6 | 0.922 | | | | |
| 1.2 | 0.899 | 10.6 | 0.869 | 1.2 | 0.925 | 10.6 | 0.896 | 1.2 | 0.948 | 10.6 | 0.919 | | | | |
| 1.5 | 0.893 | 11.0 | 0.862 | 1.5 | 0.920 | 11.0 | 0.889 | 1.5 | 0.943 | 11.0 | 0.912 | | | | |
| 1.8 | 0.887 | 11.2 | 0.855 | 1.8 | 0.914 | 11.2 | 0.882 | 1.8 | 0.937 | 11.2 | 0.905 | | | | |
| 2.0 | 0.882 | 11.5 | 0.841 | 2.0 | 0.909 | 11.5 | 0.868 | 2.0 | 0.932 | 11.5 | 0.891 | | | | |
| 2.2 | 0.876 | 11.8 | 0.826 | 2.2 | 0.903 | 11.8 | 0.853 | 2.2 | 0.926 | 11.8 | 0.876 | | | | |
| 2.5 | 0.868 | 12.0 | 0.815 | 2.5 | 0.895 | 12.0 | 0.842 | 2.5 | 0.918 | 12.0 | 0.865 | | | | |
| 2.8 | 0.862 | 12.2 | 0.806 | 2.8 | 0.889 | 12.2 | 0.833 | 2.8 | 0.912 | 12.2 | 0.856 | | | | |
| 3.0 | 0.859 | 12.5 | 0.795 | 3.0 | 0.886 | 12.5 | 0.822 | 3.0 | 0.909 | 12.5 | 0.845 | | | | |
| 3.2 | 0.856 | 12.8 | 0.793 | 3.2 | 0.883 | 12.8 | 0.820 | 3.2 | 0.906 | 12.8 | 0.843 | | | | |
| 3.5 | 0.853 | 13.0 | 0.790 | 3.5 | 0.882 | 13.0 | 0.821 | 3.5 | 0.905 | 13.0 | 0.848 | | | | |
| 3.8 | 0.855 | 13.2 | 0.804 | 3.8 | 0.882 | 13.2 | 0.831 | 3.8 | 0.905 | 13.2 | 0.854 | | | | |
| 4.0 | 0.859 | 13.5 | 0.813 | 4.0 | 0.886 | 13.5 | 0.840 | 4.0 | 0.909 | 13.5 | 0.863 | | | | |
| 4.2 | 0.863 | 13.8 | 0.821 | 4.2 | 0.890 | 13.8 | 0.848 | 4.2 | 0.913 | 13.8 | 0.871 | | | | |
| 4.5 | 0.870 | 14.0 | 0.825 | 4.5 | 0.897 | 14.0 | 0.852 | 4.5 | 0.920 | 14.0 | 0.875 | | | | |
| 4.8 | 0.876 | 14.2 | 0.829 | 4.8 | 0.903 | 14.2 | 0.856 | 4.8 | 0.926 | 14.2 | 0.879 | | | | |
| 5.0 | 0.879 | 14.5 | 0.831 | 5.0 | 0.906 | 14.5 | 0.858 | 5.0 | 0.929 | 14.5 | 0.881 | | | | |
| 5.2 | 0.881 | 14.8 | 0.833 | 5.2 | 0.908 | 14.8 | 0.860 | 5.2 | 0.931 | 14.8 | 0.883 | | | | |
| 5.5 | 0.880 | 15.0 | 0.833 | 5.5 | 0.907 | 15.0 | 0.860 | 5.5 | 0.930 | 15.0 | 0.883 | | | | |
| 5.8 | 0.879 | | | 5.8 | 0.906 | | | 5.8 | 0.929 | | | | | | |
| 6.0 | 0.878 | | | 6.0 | 0.905 | | | 6.0 | 0.928 | | | | | | |
| 6.2 | 0.877 | | | 6.2 | 0.904 | | | 6.2 | 0.927 | | | | | | |
| 6.5 | 0.877 | | | 6.5 | 0.904 | | | 6.5 | 0.927 | | | | | | |
| 6.8 | 0.878 | | | 6.8 | 0.905 | | | 6.8 | 0.928 | | | | | | |
| 7.0 | 0.878 | | | 7.0 | 0.905 | | | 7.0 | 0.928 | | | | | | |
| 7.2 | 0.878 | | | 7.2 | 0.905 | | | 7.2 | 0.928 | | | | | | |
| 7.5 | 0.877 | | | 7.5 | 0.904 | | | 7.5 | 0.927 | | | | | | |
| 7.8 | 0.876 | | | 7.8 | 0.903 | | | 7.8 | 0.926 | | | | | | |
| 8.0 | 0.875 | | | 8.0 | 0.902 | | | 8.0 | 0.925 | | | | | | |
| 8.2 | 0.873 | | | 8.2 | 0.900 | | | 8.2 | 0.923 | | | | | | |
| 8.5 | 0.871 | | | 8.5 | 0.898 | | | 8.5 | 0.921 | | | | | | |
| 8.8 | 0.869 | | | 8.8 | 0.896 | | | 8.8 | 0.919 | | | | | | |
| 9.0 | 0.867 | | | 9.0 | 0.894 | | | 9.0 | 0.917 | | | | | | |
| 9.2 | 0.865 | | | 9.2 | 0.892 | | | 9.2 | 0.915 | | | | | | |
| 9.5 | 0.864 | | | 9.5 | 0.891 | | | 9.5 | 0.914 | | | | | | |
| 9.8 | 0.866 | | | 9.8 | 0.893 | | | 9.8 | 0.916 | | | | | | |
| 10.0 | 0.869 | | | 10.0 | 0.896 | | | 10.0 | 0.919 | | | | | | |
| 10.2 | 0.871 | | | 10.2 | 0.898 | | | 10.2 | 0.921 | | | | | | |
| 10.5 | 0.873 | | | 10.5 | 0.900 | | | 10.5 | 0.923 | | | | | | |

TABLE 13-10. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α | λ | α |
|--------------------------|----------|----------------------------------|----------|---------------------------|----------|-----------------------------------|----------|---------------------------|----------|-----------------------------------|----------|---------------------------|----------|
| BULK POLISHED T = 293 | | BULK POLISHED T = 293 (CONT.) | | BULK POLISHED T = 1000 | | BULK POLISHED T = 1000 (CONT.) | | BULK POLISHED T = 2400 | | BULK POLISHED T = 2400 (CONT.) | | BULK POLISHED T = 2400 | |
| 1.0 | 0.597A† | 10.6 | 0.781A† | 1.0 | 0.614A† | 10.6 | 0.798A† | 1.0 | 0.647A† | 10.6 | 0.831A† | 10.6 | 0.826A |
| 1.2 | 0.613A | 10.8 | 0.776A | 1.2 | 0.630A | 10.8 | 0.793A | 1.2 | 0.663A | 10.8 | 0.826A | 10.8 | 0.815A |
| 1.5 | 0.636A | 11.0 | 0.765A | 1.5 | 0.653A | 11.0 | 0.782A | 1.5 | 0.586A | 11.0 | 0.799A | 11.0 | 0.771A |
| 1.8 | 0.658A | 11.2 | 0.749A | 1.8 | 0.675A | 11.2 | 0.766A | 1.8 | 0.708A | 11.2 | 0.743A | 11.2 | 0.725A |
| 2.0 | 0.672A | 11.5 | 0.721A | 2.0 | 0.689A | 11.5 | 0.738A | 2.0 | 0.722A | 11.5 | 0.743A | 11.5 | 0.707A |
| 2.2 | 0.685A | 11.8 | 0.693A | 2.2 | 0.703A | 11.8 | 0.710A | 2.2 | 0.736A | 11.8 | 0.743A | 11.8 | 0.688A |
| 2.5 | 0.705A | 12.0 | 0.675A | 2.5 | 0.722A | 12.0 | 0.692A | 2.5 | 0.755A | 12.0 | 0.743A | 12.0 | 0.687A |
| 2.8 | 0.721A | 12.2 | 0.657A | 2.8 | 0.738A | 12.2 | 0.674A | 2.8 | 0.771A | 12.2 | 0.743A | 12.2 | 0.687A |
| 3.0 | 0.731A | 12.5 | 0.638A | 3.0 | 0.748A | 12.5 | 0.655A | 3.0 | 0.781A | 12.5 | 0.743A | 12.5 | 0.687A |
| 3.2 | 0.738A | 12.6 | 0.637A | 3.2 | 0.755A | 12.6 | 0.654A | 3.2 | 0.788A | 12.6 | 0.743A | 12.6 | 0.695A |
| 3.5 | 0.748A | 12.8 | 0.645A | 3.5 | 0.765A | 12.8 | 0.662A | 3.5 | 0.798A | 12.8 | 0.743A | 12.8 | 0.712A |
| 3.8 | 0.754A | 13.0 | 0.662A | 3.8 | 0.771A | 13.0 | 0.679A | 3.8 | 0.804A | 13.0 | 0.743A | 13.0 | 0.732A |
| 4.0 | 0.756A | 13.2 | 0.682A | 4.0 | 0.773A | 13.2 | 0.699A | 4.0 | 0.806A | 13.2 | 0.743A | 13.2 | 0.748A |
| 4.2 | 0.758A | 13.3 | 0.690A | 4.2 | 0.775A | 13.3 | 0.707A | 4.2 | 0.808A | 13.3 | 0.743A | 13.3 | 0.750A |
| 4.5 | 0.759A | 13.5 | 0.698A | 4.5 | 0.776A | 13.5 | 0.715A | 4.5 | 0.809A | 13.5 | 0.743A | 13.5 | 0.751A |
| 4.8 | 0.759A | 13.8 | 0.700A | 4.8 | 0.776A | 13.8 | 0.717A | 4.8 | 0.809A | 13.8 | 0.743A | 13.8 | 0.751A |
| 5.0 | 0.759A | 14.0 | 0.701A | 5.0 | 0.776A | 14.0 | 0.718A | 5.0 | 0.809A | 14.0 | 0.743A | 14.0 | 0.751A |
| 5.2 | 0.759A | 14.2 | 0.701A | 5.2 | 0.776A | 14.2 | 0.718A | 5.2 | 0.809A | 14.2 | 0.743A | 14.2 | 0.751A |
| 5.5 | 0.758A | 14.5 | 0.700A | 5.5 | 0.775A | 14.5 | 0.717A | 5.5 | 0.808A | 14.5 | 0.743A | 14.5 | 0.750A |
| 5.8 | 0.757A | 14.8 | 0.699A | 5.8 | 0.774A | 14.8 | 0.716A | 5.8 | 0.807A | 14.8 | 0.743A | 14.8 | 0.748A |
| 6.0 | 0.756A | 15.0 | 0.698A | 6.0 | 0.773A | 15.0 | 0.715A | 6.0 | 0.806A | 15.0 | 0.743A | 15.0 | 0.748A |
| 6.2 | 0.754A | | | 6.2 | 0.771A | | | 6.2 | 0.804A | | | | |
| 6.5 | 0.752A | | | 6.5 | 0.769A | | | 6.5 | 0.802A | | | | |
| 6.8 | 0.750A | | | 6.8 | 0.767A | | | 6.8 | 0.800A | | | | |
| 7.0 | 0.748A | | | 7.0 | 0.765A | | | 7.0 | 0.798A | | | | |
| 7.2 | 0.747A | | | 7.2 | 0.764A | | | 7.2 | 0.797A | | | | |
| 7.5 | 0.745A | | | 7.5 | 0.762A | | | 7.5 | 0.795A | | | | |
| 7.8 | 0.740A | | | 7.8 | 0.757A | | | 7.8 | 0.790A | | | | |
| 8.0 | 0.737A | | | 8.0 | 0.754A | | | 8.0 | 0.787A | | | | |
| 8.2 | 0.734A | | | 8.2 | 0.751A | | | 8.2 | 0.784A | | | | |
| 8.5 | 0.726A | | | 8.5 | 0.743A | | | 8.5 | 0.776A | | | | |
| 8.8 | 0.716A | | | 8.8 | 0.733A | | | 8.8 | 0.766A | | | | |
| 9.0 | 0.709A | | | 9.0 | 0.725A | | | 9.0 | 0.758A | | | | |
| 9.2 | 0.706A | | | 9.2 | 0.723A | | | 9.2 | 0.756A | | | | |
| 9.5 | 0.718A | | | 9.5 | 0.735A | | | 9.5 | 0.768A | | | | |
| 9.8 | 0.741A | | | 9.8 | 0.758A | | | 9.8 | 0.791A | | | | |
| 10.0 | 0.760A | | | 10.0 | 0.777A | | | 10.0 | 0.810A | | | | |
| 10.2 | 0.774A | | | 10.2 | 0.791A | | | 10.2 | 0.824A | | | | |
| 10.5 | 0.782A | | | 10.5 | 0.799A | | | 10.5 | 0.832A | | | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL.

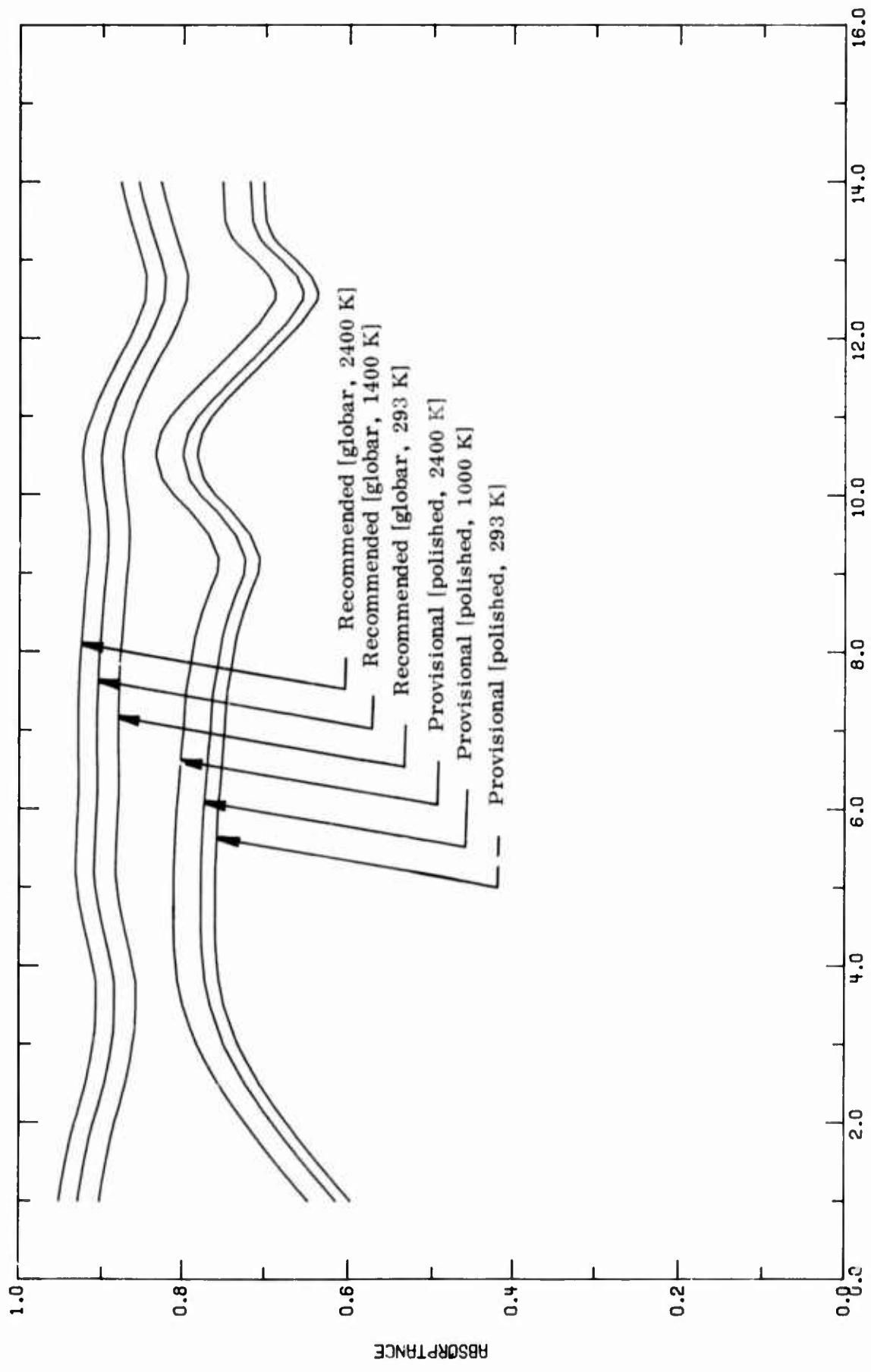


FIGURE 13-7. RECOMMENDED NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

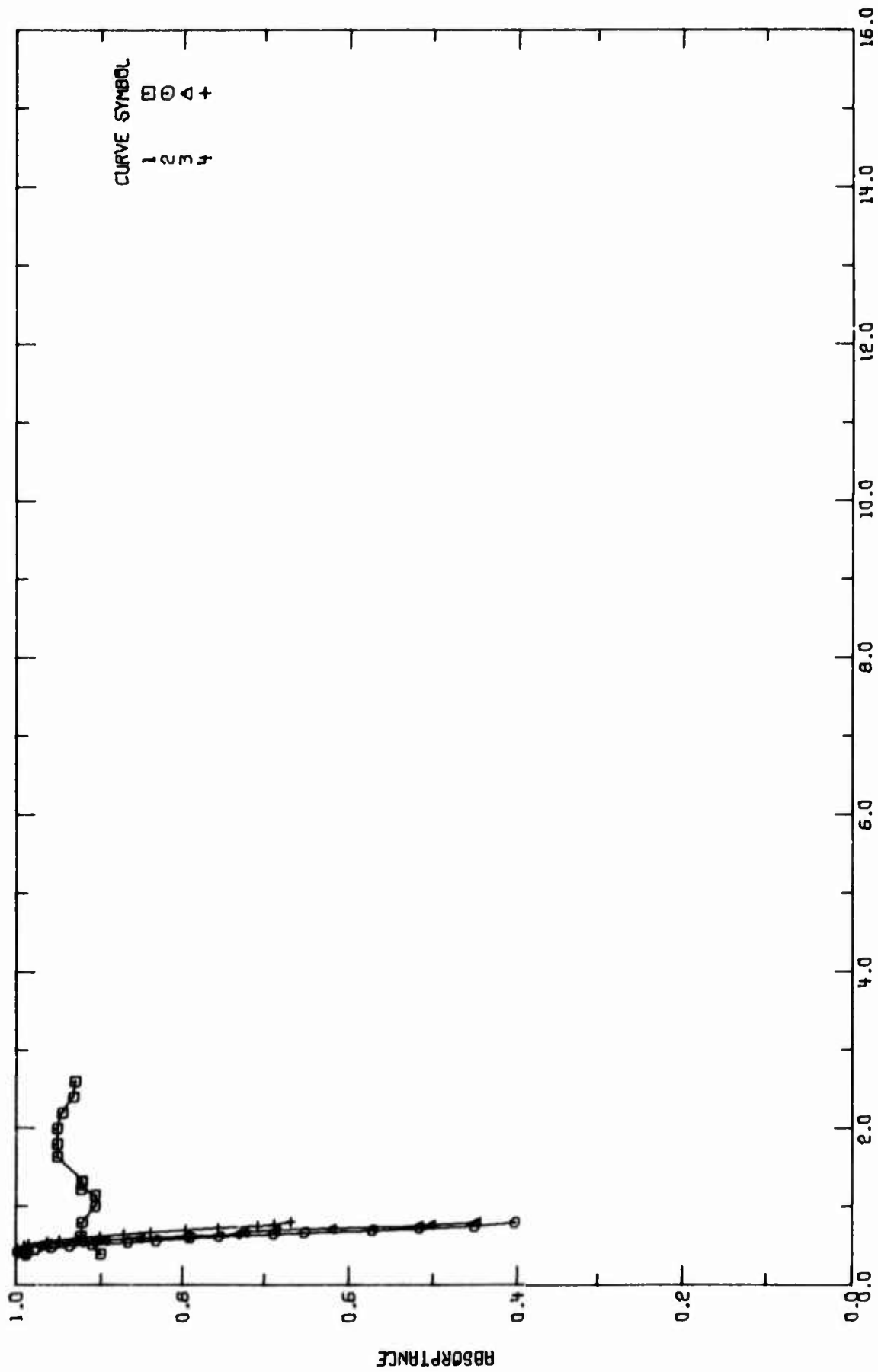


FIGURE 13-8. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

TABLE 13-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTION OF SILICON MONOCARBIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T32388 | Byrne, R. F. and Mancinelli, L. N. | 1954 | 0.40-2.60 | ≈ 298 | | Globar; data extracted from smooth curve; $\theta \approx 0^\circ$. |
| 2 T57246 | Bumton, G. V. | 1970 | 0.39-0.80 | 293 | A | Film specimen 0.3 μm thick; deposited on glass at 300 K; electrical resistivity 446, 378, 357, 312, 292, 269, 237, 202, 179, and 163 $\Omega \text{ cm}$ at 295, 303, 308, 315, 322, 328, 337, 346, and 353 K, respectively. |
| 3 T57246 | Bumton, G. V. | 1970 | 0.39-0.80 | 293 | B | Film specimen 0.3 μm thick; deposited on glass at 315 K; electrical resistivity 115, 100, 91.2, 83.9, 74.3, 66.7, 63.3, 55.3, 51.3, 42.9, 43.7, 40.5, 37.6, 34.4, 32.6, and 30.8 $\Omega \text{ cm}$ at 294, 300, 303, 310, 314, 320, 323, 328, 333, 338, 342, 349, 354, 358, 362, and 367 K, respectively. |
| 4 T57246 | Bumton, G. V. | 1970 | 0.39-0.80 | 293 | C | Film specimen 0.5 μm thick; deposited on glass at 550 K; electrical resistivity 2800, 2180, 1880, 1730, 1570, 1380, 1250, 1150, 1040, 938, 857, 794, 736, 698, 638, and 601 $\Omega \text{ cm}$ at 294, 308, 314, 319, 324, 328, 334, 338, 343, 349, 353, 359, 362, 365, 371, and 376 K, respectively. |

TABLE 13-12. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|----------------|----------|----------------|----------|
| CURVE 1 | | | |
| T = 298. | | | |
| 0.400 | 0.900 | 0.404 | 0.994 |
| 0.630 | 0.923 | 0.422 | 0.994 |
| 0.803 | 0.921 | 0.452 | 0.993 |
| 1.01 | 0.906 | 0.471 | 0.988 |
| 1.15 | 0.906 | 0.502 | 0.973 |
| 1.23 | 0.922 | 0.523 | 0.963 |
| 1.33 | 0.921 | 0.554 | 0.924 |
| 1.64 | 0.950 | 0.572 | 0.896 |
| 1.80 | 0.950 | 0.603 | 0.853 |
| 2.00 | 0.950 | 0.624 | 0.796 |
| 2.20 | 0.944 | 0.651 | 0.733 |
| 2.40 | 0.931 | 0.674 | 0.724 |
| 2.60 | 0.929 | 0.702 | 0.686 |
| | | 0.721 | 0.620 |
| | | 0.755 | 0.518 |
| | | 0.772 | 0.503 |
| | | 0.804 | 0.450 |
| CURVE 2 | | | |
| T = 293. | | | |
| 0.386 | 0.987 | CURVE 4 | |
| 0.404 | 0.987 | T = 293. | |
| 0.422 | 0.987 | 0.386 | 0.998 |
| 0.452 | 0.976 | 0.404 | 0.998 |
| 0.481 | 0.957 | 0.422 | 0.998 |
| 0.504 | 0.935 | 0.452 | 0.998 |
| 0.524 | 0.909 | 0.471 | 0.998 |
| 0.550 | 0.867 | 0.502 | 0.990 |
| 0.571 | 0.833 | 0.523 | 0.985 |
| 0.604 | 0.790 | 0.554 | 0.963 |
| 0.622 | 0.754 | 0.572 | 0.948 |
| 0.651 | 0.688 | 0.603 | 0.922 |
| 0.671 | 0.652 | 0.624 | 0.901 |
| 0.701 | 0.572 | 0.653 | 0.872 |
| 0.724 | 0.515 | 0.673 | 0.840 |
| 0.752 | 0.451 | 0.707 | 0.796 |
| 0.798 | 0.403 | 0.730 | 0.756 |
| | | 0.755 | 0.708 |
| | | 0.776 | 0.688 |
| | | 0.805 | 0.668 |
| CURVE 3 | | | |
| T = 293. | | | |
| 0.386 | 0.994 | | |

e. Normal Spectral Transmittance (Wavelength Dependence)

A total of 61 sets of data are available at room temperature. Thirty-one sets were measured below 1 μm and six sets above 15 μm .

Most of the data measured between 1 and 15 μm were for thin specimens with thickness ranging from several μm to over 300 μm and colored from colorless to dark green. A recommended curve applicable to colorless specimen with thickness ranging from 100 to 200 μm is generated following the data of Lipson [E17415] (Figure 13-10, curve 30). The values are typical above 5 μm where a series of peaks and valleys occur. Below 5 μm , the uncertainty is believed to be 10%.

Four sets of data were measured for thin films about 0.1 μm thick or thinner. One curve was generated following the data of Schatz, et al. [T22272] (Figure 13-10, curve 2) for a specimen 0.06 μm thick. The recommended values below 10 μm have an uncertainty of 5%. The values above 10 μm are typical.

The recommended and the typical curves are shown in Figure 13-9 and the experimental curves are shown in Figure 13-10. The recommended and the typical values, the experimental measurement information, and the experimental data are tabulated in Tables 13-13, 13-14, and 13-15, respectively.

TABLE 13-13. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|-----------|---------|-----------|---------|-----------|---------|-----------|---------|-----------|---------|------------------------------|--------|
| 1.0 | 0.641 | 6.82 | 0.4928† | 10.0 | 0.000A† | 1.0 | 0.548 | 11.5 | 0.9148† | THIN FILM | |
| 1.2 | 0.643 | 6.86 | 0.5328 | | | 1.2 | 0.604 | 11.6 | 0.8938 | THICKNESS 0.05 μm | |
| 1.5 | 0.647 | 6.95 | 0.4008 | | | 1.5 | 0.675 | 11.8 | 0.8258 | T = 293 (CONT.) | |
| 1.9 | 0.650 | 7.0 | 0.1408 | | | 1.8 | 0.734 | 11.9 | 0.7628 | | |
| 2.0 | 0.653 | 7.04 | 0.1018 | | | 2.0 | 0.765 | 12.0 | 0.6838 | | |
| 2.2 | 0.655 | 7.1 | 0.0808 | | | 2.2 | 0.791 | 12.1 | 0.5728 | | |
| 2.5 | 0.658 | 7.2 | 0.0598 | | | 2.5 | 0.822 | 12.2 | 0.4458 | | |
| 2.8 | 0.660 | 7.4 | 0.0298 | | | 2.8 | 0.846 | 12.3 | 0.2728 | | |
| 3.0 | 0.661 | 7.5 | 0.0178 | | | 3.0 | 0.859 | 12.4 | 0.1208 | | |
| 3.2 | 0.662 | 7.64 | 0.000A | | | 3.2 | 0.871 | 12.45 | 0.0658 | | |
| 3.5 | 0.662 | 7.76 | 0.000A | | | 3.5 | 0.888 | 12.5 | 0.0398 | | |
| 3.8 | 0.660 | 7.8 | 0.0148 | | | 3.8 | 0.902 | 12.55 | 0.0268 | | |
| 4.0 | 0.658 | 7.9 | 0.0678 | | | 4.0 | 0.909 | 12.6 | 0.0428 | | |
| 4.2 | 0.655A† | 8.0 | 0.0968 | | | 4.2 | 0.915 | 12.65 | 0.0888 | | |
| 4.5 | 0.646A | 8.05 | 0.1038 | | | 4.5 | 0.923 | 12.7 | 0.1788 | | |
| 4.8 | 0.631A | 8.1 | 0.1058 | | | 4.8 | 0.929 | 12.75 | 0.2988 | | |
| 5.0 | 0.6158 | 8.2 | 0.1038 | | | 5.0 | 0.932 | 12.8 | 0.3768 | | |
| 5.2 | 0.5928 | 8.3 | 0.0928 | | | 5.2 | 0.934 | 12.9 | 0.4908 | | |
| 5.4 | 0.5558 | 8.5 | 0.0808 | | | 5.5 | 0.938 | 13.0 | 0.5768 | | |
| 5.5 | 0.5288 | 8.8 | 0.0618 | | | 5.8 | 0.940 | 13.1 | 0.6358 | | |
| 5.6 | 0.4828 | 8.9 | 0.0588 | | | 6.0 | 0.942 | 13.3 | 0.7188 | | |
| 5.65 | 0.4388 | 9.0 | 0.0578 | | | 6.2 | 0.942 | 13.5 | 0.7748 | | |
| 5.68 | 0.3838 | 9.1 | 0.0568 | | | 6.5 | 0.944 | 13.8 | 0.8338 | | |
| 5.7 | 0.3428 | 9.2 | 0.0568 | | | 6.8 | 0.944 | 14.0 | 0.862A | | |
| 5.75 | 0.2368 | 9.3 | 0.0578 | | | 7.0 | 0.945 | 14.2 | 0.881A | | |
| 5.8 | 0.1308 | 9.4 | 0.0608 | | | 7.5 | 0.945 | 14.4 | 0.893A | | |
| 5.82 | 0.1058 | 9.5 | 0.0658 | | | 8.0 | 0.945 | 14.5 | 0.897A | | |
| 5.86 | 0.0708 | 9.58 | 0.0708 | | | 8.5 | 0.945 | 14.6 | 0.899A | | |
| 5.9 | 0.0498 | 9.62 | 0.0718 | | | 8.8 | 0.944 | 14.8 | 0.903A | | |
| 6.0 | 0.0148 | 9.64 | 0.0718 | | | 9.0 | 0.944 | 15.0 | 0.902A | | |
| 6.2 | 0.000A | 9.68 | 0.0698 | | | 9.5 | 0.944 | | | | |
| 6.26 | 0.0708 | 9.75 | 0.0618 | | | 9.8 | 0.945 | | | | |
| 6.32 | 0.1408 | 9.8 | 0.0518 | | | 10.0 | 0.945 | | | | |
| 6.39 | 0.000A | 9.86 | 0.0408 | | | 10.5 | 0.945A† | | | | |
| 6.52 | 0.000A | 9.9 | 0.0328 | | | 10.6 | 0.945A | | | | |
| 6.6 | 0.1758 | 10.0 | 0.0258 | | | 10.8 | 0.944A | | | | |
| 6.7 | 0.3408 | 10.1 | 0.0118 | | | 11.0 | 0.943A | | | | |
| 6.75 | 0.4118 | 10.2 | 0.0058 | | | 11.2 | 0.938A | | | | |
| 6.8 | 0.4688 | 10.6 | 0.0028 | | | 11.4 | 0.9278 | | | | |

† VALUE FOLLOWED BY AN "A" IS PROVISIONAL AND BY A "B" IS TYPICAL.

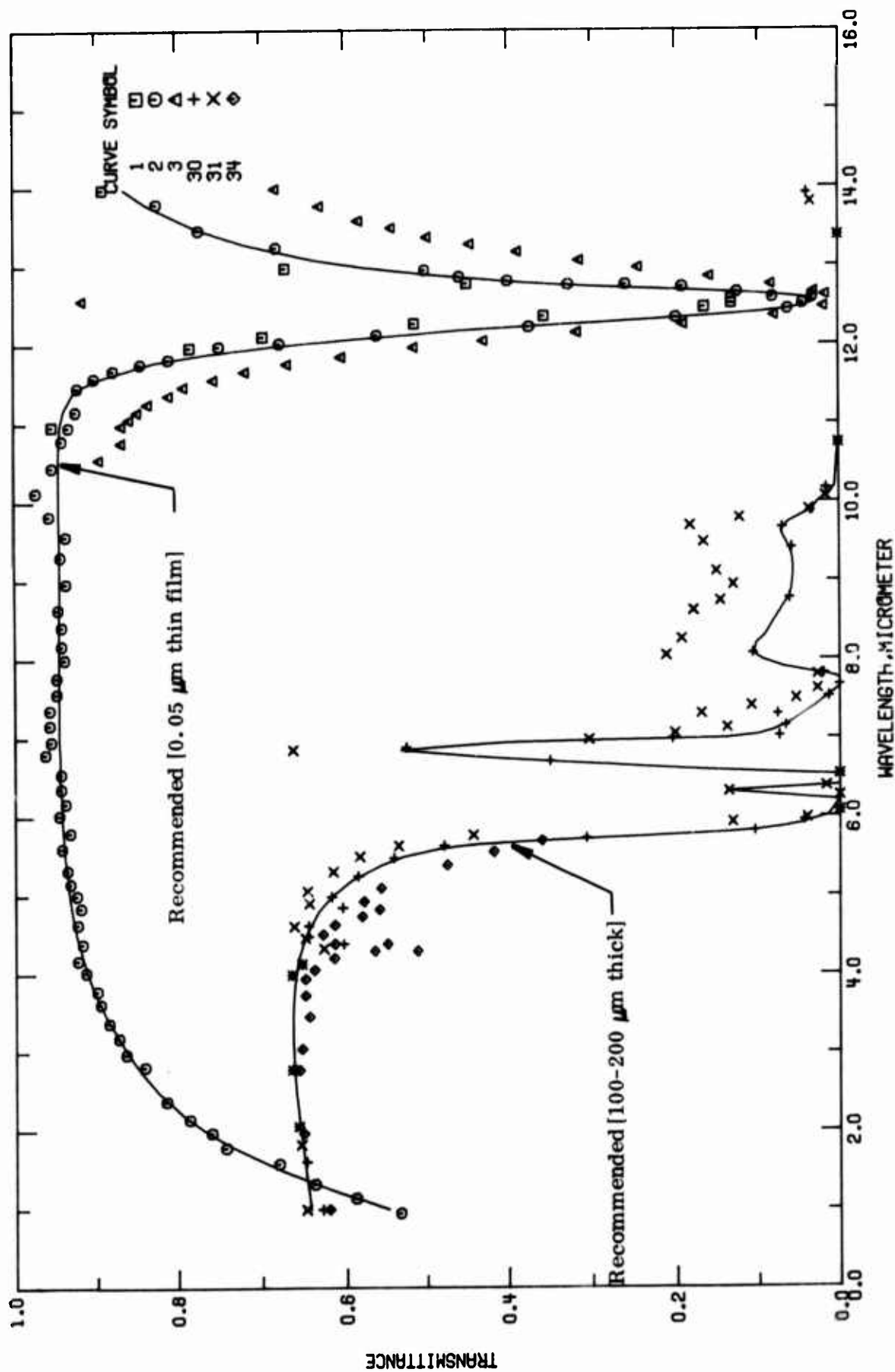


FIGURE 13-9. RECOMMENDED NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

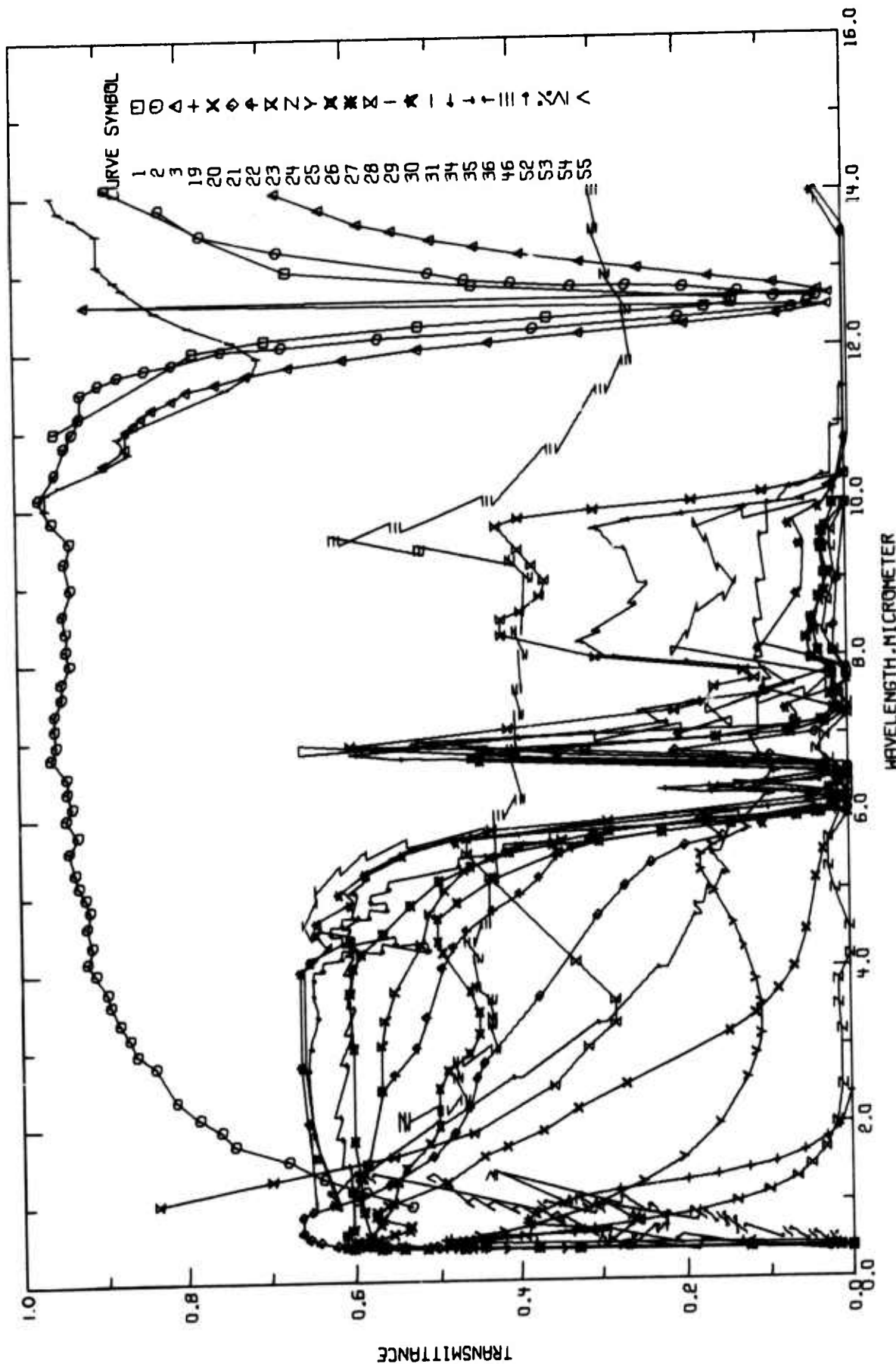


FIGURE 13-10. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE).

TABLE 13-14. MEASUREMENT INFORMATION ON THE SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|--------------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T32822 E17420 | Spitzer, W. G., Kleinman, D. A., and Froesch, C. J. et al. | 1959 | 11-14 | 293 | | β -phase polycrystalline cubic SiC film 0.04 μm thick; measured by a conventional sample in-sample out technique with a double-pass Perkin Elmer spectrometer; $\theta = 0^\circ$. |
| 2 T32822 E17420 | Spitzer, W. G., et al. | 1959 | 0.95-15 | 293 | | Similar to the above except specimen thickness 0.06 μm . |
| 3 T32822 E17420 | Spitzer, W. G., et al. | 1959 | 11-14 | 293 | | Similar to the above except specimen thickness 0.12 μm . |
| 4 E02863 | Namba, M. | 1957 | 0.3-1.0 | 293 | | p-type colorless single crystal; electrical resistivity $10^4 \Omega \text{ cm}$. |
| 5 E02863 | Namba, M. | 1957 | 0.4-1.0 | 293 | | n-type green single crystal; electrical resistivity $10^3 \Omega \text{ cm}$. |
| 6 E02863 | Namba, M. | 1957 | 0.4-1.0 | 293 | | p-type black single crystal; electrical resistivity 0.1 $\Omega \text{ cm}$. |
| 7 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.38-0.57 | 293 | 1.61 | Hexagonal colorless crystal; 200 μm in thickness; prepared by sublimation at $\sim 2773 \text{ K}$ in a stream of pure argon; data taken from smooth curve. |
| 8 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.42-0.62 | 293 | | From the same batch as the above specimen except surface covered by a thin layer of yellow cubic SiC. |
| 9 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.39-0.43 | 77 | | Hexagonal; prepared by sublimation in argon; data taken from smooth curve. |
| 10 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.40-0.45 | 292.5 | | The above specimen. |
| 11 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.40-0.45 | 394 | | The above specimen. |
| 12 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.41-0.46 | 461 | | The above specimen. |
| 13 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.41-0.47 | 5.4 | | The above specimen. |
| 14 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.42-0.47 | 585 | | The above specimen. |
| 15 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.43-0.48 | 744 | | The above specimen. |
| 16 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.44-0.49 | 800 | | The above specimen. |
| 17 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.45-0.50 | 948 | | The above specimen. |
| 18 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.46-0.51 | 1036 | | The above specimen. |
| 19 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.40-2.4 | 293 | 101 | 1.5 x 10^{18} N ; hexagonal; dark green; 135 μm in thickness; prepared by sublimation at $\sim 2773 \text{ K}$ in an Ar + 10% N_2 atm; data taken from smooth curve. |
| 20 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.39-6.0 | 293 | 103 | 2.7 x 10^{18} N ; hexagonal; green; 97 μm in thickness; prepared by sublimation at $\sim 2773 \text{ K}$ in an Ar + 0.1% N_2 atm; data taken from smooth curve. |
| 21 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.39-9.9 | 293 | 131 | Hexagonal; colorless; $\sim 270 \mu\text{m}$ in thickness; prepared by sublimation at $\sim 2773 \text{ K}$ in an Ar + 0.01% N_2 atm; data taken from smooth curve. |

TABLE 13-14. MEASUREMENT INFORMATION ON THE SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 22 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.39-9.9 | 293 | 130 | Hexagonal; colorless; 230 μm in thickness; prepared by sublimation at ~ 2773 K in an Ar + 0.001% N ₂ atm; data taken from smooth curve. |
| 23 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.39-9.9 | 293 | 132 | Hexagonal; colorless; 215 μm in thickness; prepared by sublimation at ~ 2773 K in pure argon; data taken from smooth curve. |
| 24 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.38-9.9 | 293 | 96 | 10 ¹⁸ Al; hexagonal; blue; 107 μm in thickness; prepared by sublimation at ~ 2773 K in an Ar + 0.51% AlCl ₃ atm; data taken from smooth curve. |
| 25 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.37-5.8 | 293 | 201 | 5.7 x 10 ¹⁸ Al; hexagonal; blue; 66 μm in thickness; prepared by sublimation at ~ 2773 K in an Ar + 0.51% AlCl ₃ atm; data taken from smooth curve. |
| 26 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.38-9.9 | 293 | 98 | $\sim 10^{18}$ Al; hexagonal; light blue; 200 μm in thickness; prepared by sublimation at ~ 2773 K in an Ar + 0.0085% AlCl ₃ atm; data taken from smooth curve. |
| 27 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 0.38-9.9 | 293 | 115 | Hexagonal; colorless; prepared by sublimation at ~ 2773 K in pure argon; data taken from smooth curve. |
| 28 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 1.0-10 | 293 | 188 | $\sim 2 \times 10^{18}$ Al; hexagonal; light blue; 155 μm in thickness; prepared by sublimation at ~ 2773 K in an Ar + 0.076% AlCl ₃ atm; data taken from smooth curve. |
| 29 E03607 | Lely, J. A. and Kröger, F. A. | 1958 | 10-14 | 293 | | Cubic; yellow; data taken from smooth curve. |
| 30 E17415 | Lipson, H. G. | 1960 | 1.0-25 | 293 | S-25 | α -II hexagonal crystal 0.155 mm thick; obtained from General Electric Co.; as grown; measured by the conventional in-out technique; data taken from smooth curve. |
| 31 E17415 | Lipson, H. G. | 1960 | 1.0-24 | 293 | S-25 | Similar to the above except specimen 0.11 mm thick. |
| 32 E17415 | Lipson, H. G. | 1960 | 14-24 | 293 | S-25 | Similar to the above except specimen 0.105 mm thick and surface polished. |
| 33 E17415 | Lipson, H. G. | 1960 | 14-24 | 293 | S-25 | Similar to the above except specimen 0.145 mm thick. |
| 34 E17415 | Lipson, H. G. | 1960 | 1.0-5.7 | 293 | R-256 | α -II hexagonal crystal 0.27 mm thick; obtained from Westinghouse Research Lab.; measured by the conventional in-out technique; data taken from smooth curve. |
| 35 E17415 | Lipson, H. G. | 1960 | 1.0-10 | 293 | R-278 | Similar to the above except specimen 0.07 mm thick. |
| 36 E17415 | Lipson, H. G. | 1960 | 1.0-11 | 293 | | α -II hexagonal; light green crystal 0.007 mm thick; obtained from Norton Co.; measured by the conventional in-out technique; data taken from smooth curve. |
| 37 T35131 | Dalven, R. | 1965 | 0.44-0.76 | 295 | | β -phase n-type cubic single crystal; $< 10^{17}$ cm ⁻³ each of Al, B, Ca, Fe, and Mg; about 2 mm in diameter and 0.114 mm thick; grown an extension of Kendall's method; polished; measured by the conventional in-out technique with unpolarized light normal to the polished surface 17° to a $< 111 \rangle$ direction. |
| 38 T35131 | Dalven, R. | 1965 | 0.44-0.76 | 351 | | The above specimen. |
| 39 T35131 | Dalven, R. | 1965 | 0.45-0.76 | 400 | | The above specimen. |
| 40 T35131 | Dalven, R. | 1965 | 0.46-0.76 | 450 | | The above specimen. |
| 41 T35131 | Dalven, R. | 1965 | 0.46-0.76 | 499 | | The above specimen. |
| 42 T35131 | Dalven, R. | 1965 | 0.47-0.76 | 550 | | The above specimen. |
| 43 T35131 | Dalven, R. | 1965 | 0.47-0.76 | 601 | | The above specimen. |
| 44 T35131 | Dalven, R. | 1965 | 0.48-0.76 | 652 | | The above specimen. |
| 45 T35131 | Dalven, R. | 1965 | 0.48-0.76 | 700 | | The above specimen. |

TABLE 13-14. MEASUREMENT INFORMATION ON THE SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (Wavelength Dependence) (continued)

| Cat. No. | Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|----------|----------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 46 | T60470 | Brame, E. G., Jr., Margrave, J. L., and Meloche, V. W. | 1957 | 2.0-16 | 293 | | High-purity; 12 mm diameter x 1 mm thick; measured by KBr disk method; data taken from smooth curve. |
| 47 | T32121 | Pichugin, I. G. and Pikhin, A. N. | 1966 | 0.14-0.19 | 293 | 171 | 6H single crystal; pure; grown at 2723 K; data taken from smooth curve. |
| 48 | T32121 | Pichugin, I. G. and Pikhin, A. N. | 1966 | 0.14-0.19 | 293 | 171 | Similar to the above specimen except 0.0025 B-doped; acceptor concentration $N_A = 2.70 \times 10^{18} \text{ cm}^{-3}$; donor concentration $N_D = 8.1 \times 10^{17} \text{ cm}^{-3}$. |
| 49 | T32121 | Pichugin, I. G. and Pikhin, A. N. | 1966 | 0.14-0.19 | 293 | 172 | Similar to the above specimen except 0.0033 B-doped; N_A and N_D not given. |
| 50 | T32121 | Pichugin, I. G. and Pikhin, A. N. | 1966 | 0.14-0.19 | 293 | 173 | Similar to the above specimen except 0.0037 B-doped; $N_A = 4.40 \times 10^{18} \text{ cm}^{-3}$; $N_D = 4.4 \times 10^{17} \text{ cm}^{-3}$. |
| 51 | T32121 | Pichugin, I. G. and Pikhin, A. N. | 1966 | 0.14-0.18 | 293 | 175 | Similar to the above specimen except 0.091 B-doped; N_A and N_D not given. |
| 52 | T65652 | Il'in, M. A., Kosyganova, M. G., Solomatina, V. N., Barinov, Yu. V., and Bulgakov, Yu. V. | 1971 | 0.40-1.4 | 293 | D-2-353 P1 | 6H α -phase p-type single crystal; B-doped; 460 μm thick; obtained by evaporating β -SiC; electrical resistivity 625 $\Omega \text{ cm}$; carrier concentration $2.1 \times 10^{14} \text{ cm}^{-3}$. |
| 53 | T65652 | Il'in, M. A., et al. | 1971 | 0.46-1.3 | 293 | | The above specimen neutron-irradiated by a dose of $3.9 \times 10^{15} \text{ cm}^{-2}$; electrical resistivity $10^7 \Omega \text{ cm}$. |
| 54 | T65652 | Il'in, M. A., et al. | 1971 | 0.43-1.4 | 293 | D-2-336 P2 | 6H α -phase p-type single crystal; B-doped; 310 μm thick; obtained by evaporating β -SiC; electrical resistivity 362 $\Omega \text{ cm}$; carrier concentration $5.2 \times 10^{14} \text{ cm}^{-3}$. |
| 55 | T65652 | Il'in, M. A., et al. | 1971 | 0.45-1.3 | 293 | | The above specimen neutron-irradiated by a dose of $2.3 \times 10^{15} \text{ cm}^{-2}$; electrical resistivity $1.2 \times 10^4 \Omega \text{ cm}$; carrier concentration $0.7 \times 10^{14} \text{ cm}^{-3}$. |
| 56 | T65652 | Il'in, M. A., et al. | 1971 | 0.40-1.0 | 293 | S-3-273 PA4 | 6H α -phase p-type single crystal; B-doped; 400 μm thick; obtained by evaporating pure silicon and graphite; electrical resistivity 200 $\Omega \text{ cm}$; carrier concentration $4 \times 10^{14} \text{ cm}^{-3}$; data taken from smooth curve. |
| 57 | T65652 | Il'in, M. A., et al. | 1971 | 0.40-1.0 | 293 | | The above specimen α -irradiated by a dose of $3.6 \times 10^{15} \text{ cm}^{-2}$; electrical resistivity 642 $\Omega \text{ cm}$; carrier concentration $2.56 \times 10^{14} \text{ cm}^{-3}$. |
| 58 | T63770 | Il'in, M. A., Rashevskaya, E. P., and Buras, E. M. | 1971 | 15-21 | 293 | | 6H α -phase n-type single crystal; light polarized parallel to c-axis; data taken from smooth curve. |
| 59 | T63770 | Il'in, M. A., et al. | 1971 | 15-21 | 293 | | Similar to the above specimen except light polarized perpendicular to c-axis. |
| 60 | T63770 | Il'in, M. A., et al. | 1971 | 15-21 | 293 | | 6H α -phase p-type single crystal; light polarized parallel to c-axis. |
| 61 | T63770 | Il'in, M. A., et al. | 1971 | 15-21 | 293 | | Similar to the above specimen except light polarized perpendicular to c-axis. |

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ, μm; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 1 T = 293. | | | | CURVE 2 (CONT.) | | | | CURVE 2 (CONT.) | | | | CURVE 3 (CONT.) | | | | CURVE 6* T = 293. | | | | CURVE 8 (CONT.)* | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| 10.98 | 0.953 | 6.03 | 0.945 | 12.77 | 0.325 | 13.19 | 0.367 | 0.400 | 0.0 | 0.467 | 0.176 | 10.98 | 0.782 | 6.18 | 0.937 | 12.82 | 0.398 | 13.29 | 0.444 | 0.400 | 0.0 | 0.499 | 0.478 | 11.98 | 0.695 | 6.37 | 0.943 | 12.87 | 0.456 | 13.38 | 0.498 | 0.500 | 0.0 | 0.508 | 0.534 | 12.12 | 0.513 | 6.56 | 0.943 | 12.96 | 0.500 | 13.50 | 0.543 | 0.600 | 0.0 | 0.512 | 0.555 | 12.28 | 0.354 | 6.81 | 0.962 | 13.25 | 0.679 | 13.59 | 0.583 | 0.700 | 0.0 | 0.518 | 0.567 | 12.48 | 0.165 | 6.97 | 0.955 | 13.47 | 0.771 | 13.78 | 0.628 | 0.750 | 0.014 | 0.526 | 0.572 | 12.58 | 0.132 | 7.18 | 0.957 | 13.81 | 0.822 | 14.00 | 0.661 | 0.777 | 0.057 | 0.537 | 0.571 | 12.79 | 0.447 | 7.37 | 0.957 | 14.13 | 0.890 | | | 0.800 | 0.107 | 0.548 | 0.569 | 12.99 | 0.668 | 7.58 | 0.948 | 14.33 | 0.878 | | | 0.820 | 0.156 | 0.568 | 0.557 | 14.00 | 0.869 | 7.78 | 0.948 | 14.53 | 0.898 | | | 0.843 | 0.197 | 0.515 | 0.521 | | | 8.01 | 0.938 | 14.97 | 0.897 | | | 0.900 | 0.199 | | | | | 8.19 | 0.942 | | | | | | | | | | | | | | | | | | | | | | 8.43 | 0.942 | | | | | | | | | | | | | | | | | | | | | | 8.65 | 0.946 | | | | | | | | | | | | | | | | | | | | | | 8.98 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.32 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 8.19 | 0.942 | | | | | | | | | | | | | | | | | | | | | | 8.43 | 0.942 | | | | | | | | | | | | | | | | | | | | | | 8.65 | 0.946 | | | | | | | | | | | | | | | | | | | | | | 8.98 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.32 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 8.43 | 0.942 | | | | | | | | | | | | | | | | | | | | | | 8.65 | 0.946 | | | | | | | | | | | | | | | | | | | | | | 8.98 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.32 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 8.65 | 0.946 | | | | | | | | | | | | | | | | | | | | | | 8.98 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.32 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 8.98 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.32 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 9.32 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 9.58 | 0.936 | | | | | | | | | | | | | | | | | | | | | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 9.84 | 0.957 | | | | | | | | | | | | | | | | | | | | | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 10.14 | 0.973 | | | | | | | | | | | | | | | | | | | | | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 1.58 | 0.679 | 10.46 | 0.953 | 11.07 | 0.857 | 10.56 | 0.895 | 10.99 | 0.867 | 0.398 | 0.055 | 0.389 | 0.012 | 0.393 | 0.118 | 0.391 | 0.0 | 0.397 | 0.0 | | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 1.79 | 0.742 | 10.80 | 0.941 | 11.16 | 0.834 | 10.77 | 0.867 | 10.99 | 0.867 | 0.406 | 0.200 | 0.394 | 0.030 | 0.395 | 0.118 | 0.395 | 0.055 | 0.400 | 0.055 | | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 1.98 | 0.759 | 10.97 | 0.932 | 11.26 | 0.809 | 10.99 | 0.867 | 11.07 | 0.857 | 0.417 | 0.308 | 0.402 | 0.052 | 0.398 | 0.310 | 0.398 | 0.310 | 0.407 | 0.299 | | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 2.15 | 0.785 | 11.17 | 0.923 | 11.48 | 0.791 | 11.07 | 0.857 | 11.16 | 0.834 | 0.452 | 0.372 | 0.403 | 0.030 | 0.402 | 0.554 | 0.402 | 0.554 | 0.412 | 0.484 | | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 2.38 | 0.813 | 11.47 | 0.921 | 11.57 | 0.755 | 11.26 | 0.809 | 11.37 | 0.809 | 0.500 | 0.476 | 0.406 | 0.051 | 0.403 | 0.627 | 0.403 | 0.627 | 0.415 | 0.814 | | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 2.82 | 0.839 | 11.59 | 0.900 | 11.67 | 0.712 | 11.48 | 0.791 | 11.57 | 0.755 | 0.700 | 0.476 | 0.409 | 0.052 | 0.409 | 0.704 | 0.406 | 0.704 | 0.432 | 0.912 | | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 2.98 | 0.862 | 11.69 | 0.876 | 11.77 | 0.667 | 11.67 | 0.712 | 11.77 | 0.667 | 0.800 | 0.508 | 0.415 | 0.814 | 0.412 | 0.509 | 0.415 | 0.814 | 0.432 | 0.912 | | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 3.19 | 0.871 | 11.77 | 0.842 | 11.86 | 0.603 | 11.77 | 0.667 | 11.86 | 0.603 | 1.000 | 0.527 | 0.418 | 0.539 | 0.418 | 0.539 | 0.418 | 0.539 | | | | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 3.38 | 0.883 | 11.83 | 0.808 | 11.98 | 0.515 | 11.86 | 0.603 | 11.98 | 0.515 | | | 0.422 | 0.561 | 0.422 | 0.561 | 0.422 | 0.561 | | | | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 3.62 | 0.894 | 11.99 | 0.747 | 12.06 | 0.428 | 11.98 | 0.515 | 12.06 | 0.428 | | | 0.430 | 0.593 | 0.430 | 0.593 | 0.430 | 0.593 | | | | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 3.79 | 0.898 | 12.03 | 0.675 | 12.16 | 0.316 | 12.06 | 0.428 | 12.16 | 0.316 | | | 0.438 | 0.602 | 0.438 | 0.602 | 0.438 | 0.602 | | | | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 4.03 | 0.912 | 12.13 | 0.560 | 12.26 | 0.191 | 12.16 | 0.316 | 12.26 | 0.191 | | | 0.511 | 0.605 | 0.511 | 0.605 | 0.511 | 0.605 | | | | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 4.18 | 0.922 | 12.23 | 0.372 | 12.37 | 0.080 | 12.26 | 0.191 | 12.37 | 0.080 | | | 0.569 | 0.604 | 0.569 | 0.604 | 0.569 | 0.604 | | | | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 4.39 | 0.916 | 12.35 | 0.198 | 12.48 | 0.019 | 12.37 | 0.080 | 12.48 | 0.019 | | | | | | | | | | | | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 4.64 | 0.922 | 12.45 | 0.062 | 12.58 | 0.009 | 12.48 | 0.019 | 12.58 | 0.009 | | | | | | | | | | | | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 4.85 | 0.918 | 12.52 | 0.043 | 12.63 | 0.016 | 12.58 | 0.009 | 12.63 | 0.016 | | | | | | | | | | | | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 5.01 | 0.923 | 12.60 | 0.031 | 12.67 | 0.031 | 12.63 | 0.016 | 12.67 | 0.031 | | | | | | | | | | | | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 5.16 | 0.931 | 12.60 | 0.081 | 12.77 | 0.084 | 12.67 | 0.031 | 12.77 | 0.084 | | | | | | | | | | | | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 5.33 | 0.935 | 12.67 | 0.125 | 12.87 | 0.160 | 12.77 | 0.084 | 12.87 | 0.160 | | | | | | | | | | | | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 5.61 | 0.942 | 12.74 | 0.191 | 12.99 | 0.244 | 12.87 | 0.160 | 12.99 | 0.244 | | | | | | | | | | | | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
| | | 5.81 | 0.931 | 12.77 | 0.258 | 13.08 | 0.313 | 12.99 | 0.244 | 13.08 | 0.313 | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | | |
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* NOT SHOWN IN FIGURE.

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T |
|------------------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| CURVE 11* T = 394. | | | | | | | | | |
| 0.402 | 0.0 | 0.417 | 0.0 | 0.447 | 0.0 | 0.593 | 0.336 | 1.26 | 0.491 |
| 0.406 | 0.062 | 0.422 | 0.046 | 0.451 | 0.030 | 0.603 | 0.302 | 1.59 | 0.445 |
| 0.410 | 0.149 | 0.430 | 0.130 | 0.456 | 0.072 | 0.624 | 0.291 | 1.71 | 0.416 |
| 0.417 | 0.374 | 0.437 | 0.226 | 0.461 | 0.163 | 0.641 | 0.310 | 1.91 | 0.371 |
| 0.425 | 0.625 | 0.438 | 0.560 | 0.477 | 0.628 | 0.705 | 0.384 | 2.20 | 0.326 |
| 0.429 | 0.721 | 0.442 | 0.677 | 0.477 | 0.754 | 0.726 | 0.393 | 2.51 | 0.269 |
| 0.432 | 0.762 | 0.447 | 0.742 | 0.483 | 0.816 | 0.771 | 0.393 | 3.17 | 0.146 |
| 0.437 | 0.809 | 0.452 | 0.794 | 0.487 | 0.862 | 0.865 | 0.379 | 3.40 | 0.115 |
| 0.442 | 0.843 | 0.452 | 0.794 | 0.491 | 0.862 | 0.973 | 0.353 | 3.71 | 0.088 |
| 0.450 | 0.878 | 0.460 | 0.843 | 0.494 | 0.890 | 1.05 | 0.326 | 4.00 | 0.069 |
| | | 0.471 | 0.891 | 0.498 | 0.914 | 1.14 | 0.279 | 4.48 | 0.054 |
| CURVE 12* T = 461. | | | | | | | | | |
| 0.406 | 0.0 | | | | | | | | |
| 0.409 | 0.045 | | | | | | | | |
| 0.414 | 0.099 | | | | | | | | |
| 0.417 | 0.181 | | | | | | | | |
| 0.426 | 0.469 | | | | | | | | |
| 0.433 | 0.667 | | | | | | | | |
| 0.437 | 0.747 | | | | | | | | |
| 0.441 | 0.791 | | | | | | | | |
| 0.451 | 0.861 | | | | | | | | |
| 0.460 | 0.892 | | | | | | | | |
| CURVE 13* T = 514. | | | | | | | | | |
| 0.410 | 0.0 | | | | | | | | |
| 0.414 | 0.042 | | | | | | | | |
| 0.418 | 0.104 | | | | | | | | |
| 0.423 | 0.204 | | | | | | | | |
| 0.431 | 0.496 | | | | | | | | |
| 0.437 | 0.651 | | | | | | | | |
| 0.441 | 0.739 | | | | | | | | |
| 0.449 | 0.806 | | | | | | | | |
| 0.457 | 0.854 | | | | | | | | |
| 0.467 | 0.896 | | | | | | | | |
| CURVE 14* T = 585. | | | | | | | | | |
| 0.417 | 0.0 | 0.447 | 0.0 | 0.498 | 0.914 | | | | |
| 0.422 | 0.046 | 0.451 | 0.030 | 0.494 | 0.890 | | | | |
| 0.430 | 0.130 | 0.456 | 0.072 | 0.491 | 0.862 | | | | |
| 0.437 | 0.226 | 0.461 | 0.163 | 0.483 | 0.816 | | | | |
| 0.438 | 0.560 | 0.477 | 0.628 | 0.487 | 0.862 | | | | |
| 0.442 | 0.677 | 0.477 | 0.754 | 0.483 | 0.816 | | | | |
| 0.447 | 0.742 | 0.483 | 0.816 | 0.487 | 0.862 | | | | |
| 0.452 | 0.794 | 0.491 | 0.862 | 0.491 | 0.862 | | | | |
| 0.460 | 0.843 | 0.494 | 0.890 | 0.494 | 0.890 | | | | |
| 0.471 | 0.891 | 0.498 | 0.914 | 0.498 | 0.914 | | | | |
| CURVE 15* T = 744. | | | | | | | | | |
| 0.429 | 0.0 | | | | | | | | |
| 0.433 | 0.036 | | | | | | | | |
| 0.438 | 0.096 | | | | | | | | |
| 0.443 | 0.240 | | | | | | | | |
| 0.454 | 0.607 | | | | | | | | |
| 0.460 | 0.737 | | | | | | | | |
| 0.465 | 0.807 | | | | | | | | |
| 0.470 | 0.857 | | | | | | | | |
| 0.475 | 0.884 | | | | | | | | |
| 0.481 | 0.911 | | | | | | | | |
| CURVE 16* T = 800. | | | | | | | | | |
| 0.435 | 0.0 | | | | | | | | |
| 0.440 | 0.032 | | | | | | | | |
| 0.444 | 0.085 | | | | | | | | |
| 0.449 | 0.191 | | | | | | | | |
| 0.464 | 0.659 | | | | | | | | |
| 0.469 | 0.777 | | | | | | | | |
| 0.473 | 0.822 | | | | | | | | |
| 0.477 | 0.856 | | | | | | | | |
| 0.481 | 0.879 | | | | | | | | |
| 0.486 | 0.903 | | | | | | | | |
| CURVE 17* T = 948. | | | | | | | | | |
| 0.447 | 0.0 | | | | | | | | |
| 0.451 | 0.030 | | | | | | | | |
| 0.456 | 0.072 | | | | | | | | |
| 0.461 | 0.163 | | | | | | | | |
| 0.477 | 0.628 | | | | | | | | |
| 0.483 | 0.754 | | | | | | | | |
| 0.487 | 0.816 | | | | | | | | |
| 0.491 | 0.862 | | | | | | | | |
| 0.494 | 0.890 | | | | | | | | |
| 0.498 | 0.914 | | | | | | | | |
| CURVE 18* T = 1036. | | | | | | | | | |
| 0.457 | 0.0 | | | | | | | | |
| 0.463 | 0.038 | | | | | | | | |
| 0.466 | 0.085 | | | | | | | | |
| 0.471 | 0.157 | | | | | | | | |
| 0.489 | 0.644 | | | | | | | | |
| 0.492 | 0.717 | | | | | | | | |
| 0.496 | 0.785 | | | | | | | | |
| 0.500 | 0.844 | | | | | | | | |
| 0.512 | 0.921 | | | | | | | | |
| CURVE 19 T = 293. | | | | | | | | | |
| 0.397 | 0.0 | | | | | | | | |
| 0.420 | 0.017 | | | | | | | | |
| 0.437 | 0.033 | | | | | | | | |
| 0.450 | 0.134 | | | | | | | | |
| 0.461 | 0.297 | | | | | | | | |
| 0.472 | 0.382 | | | | | | | | |
| 0.484 | 0.440 | | | | | | | | |
| 0.500 | 0.478 | | | | | | | | |
| 0.518 | 0.495 | | | | | | | | |
| 0.529 | 0.489 | | | | | | | | |
| 0.551 | 0.435 | | | | | | | | |
| 0.566 | 0.419 | | | | | | | | |
| CURVE 20 T = 293. | | | | | | | | | |
| 0.389 | 0.0 | | | | | | | | |
| 0.396 | 0.123 | | | | | | | | |
| 0.407 | 0.378 | | | | | | | | |
| 0.413 | 0.461 | | | | | | | | |
| 0.422 | 0.498 | | | | | | | | |
| 0.438 | 0.510 | | | | | | | | |
| 0.450 | 0.547 | | | | | | | | |
| 0.470 | 0.568 | | | | | | | | |
| 0.489 | 0.574 | | | | | | | | |
| 0.536 | 0.555 | | | | | | | | |
| 0.599 | 0.555 | | | | | | | | |
| 0.646 | 0.537 | | | | | | | | |
| 0.702 | 0.535 | | | | | | | | |
| 0.795 | 0.568 | | | | | | | | |
| 0.836 | 0.575 | | | | | | | | |
| 0.887 | 0.575 | | | | | | | | |
| 0.973 | 0.562 | | | | | | | | |
| CURVE 21 T = 293. | | | | | | | | | |
| 0.389 | 0.0 | | | | | | | | |
| 0.396 | 0.123 | | | | | | | | |
| 0.407 | 0.378 | | | | | | | | |
| 0.418 | 0.568 | | | | | | | | |
| 0.428 | 0.603 | | | | | | | | |
| 0.465 | 0.622 | | | | | | | | |
| 0.510 | 0.642 | | | | | | | | |
| 0.554 | 0.654 | | | | | | | | |
| 0.633 | 0.663 | | | | | | | | |
| 0.836 | 0.663 | | | | | | | | |
| 0.904 | 0.651 | | | | | | | | |
| 1.08 | 0.594 | | | | | | | | |
| 1.24 | 0.560 | | | | | | | | |
| 1.60 | 0.508 | | | | | | | | |
| 1.91 | 0.481 | | | | | | | | |
| 2.24 | 0.463 | | | | | | | | |
| 2.62 | 0.453 | | | | | | | | |
| 2.81 | 0.444 | | | | | | | | |
| 3.66 | 0.374 | | | | | | | | |
| 4.69 | 0.302 | | | | | | | | |
| 5.07 | 0.269 | | | | | | | | |
| 5.36 | 0.237 | | | | | | | | |
| CURVE 22 T = 293. | | | | | | | | | |
| 0.389 | 0.0 | | | | | | | | |
| 0.396 | 0.123 | | | | | | | | |
| 0.407 | 0.378 | | | | | | | | |
| 0.421 | 0.569 | | | | | | | | |
| 0.429 | 0.601 | | | | | | | | |
| 0.448 | 0.610 | | | | | | | | |
| 0.597 | 0.610 | | | | | | | | |
| 0.668 | 0.603 | | | | | | | | |
| 1.16 | 0.603 | | | | | | | | |
| 1.36 | 0.592 | | | | | | | | |
| 1.52 | 0.585 | | | | | | | | |
| 2.47 | 0.567 | | | | | | | | |
| 2.66 | 0.552 | | | | | | | | |
| 3.01 | 0.526 | | | | | | | | |
| 3.40 | 0.514 | | | | | | | | |
| 4.03 | 0.495 | | | | | | | | |
| 4.30 | 0.481 | | | | | | | | |
| 4.51 | 0.464 | | | | | | | | |
| 4.77 | 0.431 | | | | | | | | |
| 4.98 | 0.397 | | | | | | | | |
| 5.19 | 0.373 | | | | | | | | |
| 5.46 | 0.352 | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| CURVE 22 (CONT.) | | CURVE 23 (CONT.) | | CURVE 24 (CONT.) | | CURVE 24 (CONT.) | | CURVE 25 | | CURVE 26 (CONT.) | | CURVE 26 (CONT.) | |
|------------------|--------|------------------|--------|------------------|--------|------------------|--------|-----------|--------|------------------|--------|------------------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 5.56 | 0.332 | 2.47 | 0.567 | 0.400 | 0.328 | 9.02 | 0.013 | 0.374 | 0.0 | 0.381 | 0.0 | 6.78 | 0.444 |
| 5.66 | 0.310 | 3.05 | 0.567 | 0.409 | 0.471 | 9.36 | 0.019 | 0.379 | 0.024 | 0.391 | 0.016 | 7.00 | 0.070 |
| 5.76 | 0.286 | 3.37 | 0.563 | 0.419 | 0.488 | 9.57 | 0.019 | 0.392 | 0.345 | 0.409 | 0.328 | 7.13 | 0.028 |
| 5.89 | 0.171 | 3.74 | 0.551 | 0.431 | 0.500 | 9.93 | 0.0 | 0.402 | 0.416 | 0.414 | 0.471 | 7.28 | 0.012 |
| 5.95 | 0.034 | 4.34 | 0.520 | 0.447 | 0.488 | | | 0.408 | 0.440 | 0.419 | 0.516 | 7.48 | 0.021 |
| 6.08 | 0.020 | 4.74 | 0.510 | 0.469 | 0.474 | | | 0.421 | 0.446 | 0.430 | 0.543 | 7.73 | 0.018 |
| 6.27 | 0.023 | 5.04 | 0.491 | 0.501 | 0.466 | | | 0.430 | 0.480 | 0.452 | 0.589 | 8.04 | 0.035 |
| 6.43 | 0.0 | 5.29 | 0.466 | 0.556 | 0.396 | | | 0.442 | 0.460 | 0.480 | 0.597 | 8.34 | 0.042 |
| 6.58 | 0.027 | 5.45 | 0.434 | 0.628 | 0.329 | | | 0.469 | 0.470 | 0.460 | 0.589 | 8.73 | 0.034 |
| 6.73 | 0.402 | 5.59 | 0.397 | 0.725 | 0.259 | | | 0.515 | 0.457 | 0.512 | 0.598 | 9.04 | 0.023 |
| 6.83 | 0.440 | 5.66 | 0.345 | 0.846 | 0.192 | | | 0.574 | 0.453 | 0.570 | 0.584 | 9.36 | 0.031 |
| 6.95 | 0.158 | 5.76 | 0.286 | 0.978 | 0.140 | | | 0.622 | 0.421 | 0.570 | 0.584 | 9.57 | 0.031 |
| 7.10 | 0.064 | 5.89 | 0.171 | 1.11 | 0.102 | | | 0.702 | 0.385 | 0.733 | 0.571 | 9.93 | 0.0 |
| 7.15 | 0.033 | 5.96 | 0.034 | 1.28 | 0.069 | | | 0.900 | 0.319 | 1.00 | 0.556 | | |
| 7.31 | 0.016 | 6.08 | 0.020 | 1.44 | 0.052 | | | 1.24 | 0.250 | 1.27 | 0.550 | | |
| 7.55 | 0.001 | 6.27 | 0.023 | 1.65 | 0.033 | | | 1.55 | 0.203 | 1.45 | 0.540 | | |
| 7.81 | 0.019 | 6.43 | 0.0 | 1.99 | 0.019 | | | 1.99 | 0.159 | 1.77 | 0.512 | | |
| 7.95 | 0.044 | 6.57 | 0.027 | 2.46 | 0.011 | | | 2.46 | 0.125 | 1.99 | 0.500 | | |
| 8.21 | 0.049 | 6.73 | 0.402 | 3.17 | 0.011 | | | 3.17 | 0.114 | 2.48 | 0.500 | | |
| 8.47 | 0.043 | 6.83 | 0.441 | 3.50 | 0.015 | | | 3.50 | 0.108 | 2.71 | 0.489 | | |
| 8.81 | 0.027 | 6.95 | 0.158 | 3.81 | 0.015 | | | 4.14 | 0.100 | 2.93 | 0.462 | | |
| 9.03 | 0.027 | 7.10 | 0.064 | 4.14 | 0.0 | | | 4.49 | 0.08 | 3.18 | 0.449 | | |
| 9.40 | 0.032 | 7.15 | 0.033 | 4.49 | 0.0 | | | 4.98 | 0.018 | 3.46 | 0.449 | | |
| 9.64 | 0.025 | 7.31 | 0.016 | 4.98 | 0.018 | | | 5.27 | 0.026 | 3.73 | 0.460 | | |
| 9.93 | 0.015 | 7.55 | 0.011 | 5.27 | 0.026 | | | 5.64 | 0.026 | 4.23 | 0.494 | | |
| | | 7.81 | 0.019 | 5.64 | 0.026 | | | 6.22 | 0.011 | 4.37 | 0.500 | | |
| | | 7.95 | 0.044 | 5.98 | 0.011 | | | 6.53 | 0.011 | 4.67 | 0.500 | | |
| | | 8.21 | 0.049 | 6.13 | 0.011 | | | 6.84 | 0.0 | 4.87 | 0.476 | | |
| | | 8.47 | 0.043 | 6.34 | 0.0 | | | 7.22 | 0.0 | 5.10 | 0.429 | | |
| | | 8.81 | 0.027 | 6.53 | 0.011 | | | 7.36 | 0.0 | 5.50 | 0.349 | | |
| | | 9.03 | 0.027 | 6.78 | 0.024 | | | 7.47 | 0.011 | 5.64 | 0.299 | | |
| | | 9.40 | 0.032 | 6.78 | 0.040 | | | 7.73 | 0.0 | 5.74 | 0.224 | | |
| | | 9.64 | 0.025 | 6.95 | 0.029 | | | 8.04 | 0.016 | 5.84 | 0.141 | | |
| | | 9.93 | 0.015 | 7.22 | 0.0 | | | 8.49 | 0.039 | 6.15 | 0.048 | | |
| | | | | 7.36 | 0.0 | | | 8.73 | 0.179 | 6.34 | 0.048 | | |
| | | | | 7.47 | 0.011 | | | 8.93 | 0.165 | 6.44 | 0.048 | | |
| | | | | 7.73 | 0.0 | | | 9.03 | 0.122 | 6.44 | 0.011 | | |
| | | | | 8.04 | 0.016 | | | | | 6.50 | 0.034 | | |
| | | | | 8.30 | 0.030 | | | | | 6.69 | 0.445 | | |
| | | | | 8.67 | 0.024 | | | | | 6.73 | 0.455 | | |
| | | | | 0.389 | 0.0 | | | | | | | | |
| | | | | 0.396 | 0.123 | | | | | | | | |
| | | | | 0.407 | 0.378 | | | | | | | | |
| | | | | 0.420 | 0.569 | | | | | | | | |
| | | | | 0.429 | 0.601 | | | | | | | | |
| | | | | 0.447 | 0.610 | | | | | | | | |
| | | | | 0.597 | 0.610 | | | | | | | | |
| | | | | 1.668 | 0.603 | | | | | | | | |
| | | | | 1.16 | 0.603 | | | | | | | | |
| | | | | 1.35 | 0.592 | | | | | | | | |
| | | | | 1.52 | 0.585 | | | | | | | | |
| | | | | | | | | | | | | | |

CURVE 27
T = 293.

CURVE 23
T = 293.

CURVE 24
T = 293.

CURVE 25
T = 293.

CURVE 26
T = 293.

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| CURVE 27 (CONT.) | | | CURVE 28 (CONT.) | | | CURVE 29 (CONT.) | | | CURVE 30 (CONT.) | | | CURVE 31 (CONT.) | | | CURVE 31 (CONT.) | | | CURVE 32* | | | CURVE 33* | | | | | | | |
|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|-----------|-------|--------|-----------|-------|--------|----------|-------|--|-------|-------|
| λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | | | | | |
| 5.74 | 0.224 | 0.268 | 5.9 | 0.703 | 0.013 | 7.52 | 0.013 | 0.614 | 17.55 | 0.395 | 0.614 | 5.31 | 0.614 | 0.614 | 17.55 | 0.395 | 0.614 | 17.55 | 0.395 | 0.614 | 17.55 | 0.395 | 0.614 | 0.395 | | | | |
| 5.84 | 0.141 | 0.000 | 6.2 | 0.734 | 0.0 | 7.67 | 0.0 | 0.503 | 18.18 | 0.421 | 0.503 | 5.50 | 0.503 | 0.503 | 18.18 | 0.421 | 0.503 | 18.18 | 0.421 | 0.503 | 18.18 | 0.421 | 0.503 | 0.421 | | | | |
| 5.92 | 0.064 | 0.162 | 6.3 | 0.786 | 0.019 | 7.81 | 0.019 | 0.535 | 18.91 | 0.435 | 0.535 | 5.64 | 0.535 | 0.535 | 18.91 | 0.435 | 0.535 | 18.91 | 0.435 | 0.535 | 18.91 | 0.435 | 0.535 | 0.435 | | | | |
| 5.99 | 0.339 | 0.000 | 6.5 | 0.828 | 0.107 | 8.07 | 0.107 | 0.441 | 19.78 | 0.450 | 0.441 | 5.77 | 0.441 | 0.441 | 19.78 | 0.450 | 0.441 | 19.78 | 0.450 | 0.441 | 19.78 | 0.450 | 0.441 | 0.450 | | | | |
| 6.15 | 0.348 | 0.153 | 6.7 | 0.869 | 0.061 | 8.77 | 0.061 | 0.598 | 21.04 | 0.462 | 0.598 | 5.93 | 0.598 | 0.598 | 21.04 | 0.462 | 0.598 | 21.04 | 0.462 | 0.598 | 21.04 | 0.462 | 0.598 | 0.462 | | | | |
| 6.34 | 0.011 | 0.314 | 6.8 | 0.878 | 0.058 | 9.41 | 0.058 | 0.039 | 22.58 | 0.474 | 0.039 | 6.07 | 0.039 | 0.039 | 22.58 | 0.474 | 0.039 | 22.58 | 0.474 | 0.039 | 22.58 | 0.474 | 0.039 | 0.474 | | | | |
| 6.44 | 0.011 | 0.600 | 6.9 | 0.899 | 0.070 | 9.67 | 0.070 | 0.0 | 24.33 | 0.480 | 0.0 | 6.26 | 0.0 | 0.0 | 24.33 | 0.480 | 0.0 | 24.33 | 0.480 | 0.0 | 24.33 | 0.480 | 0.0 | 0.480 | | | | |
| 6.50 | 0.034 | 0.410 | 7.1 | 0.899 | 0.034 | 9.88 | 0.034 | 0.015 | CURVE 32* | | | 6.32 | 0.015 | 0.015 | CURVE 32* | | | 6.32 | 0.015 | 0.015 | CURVE 32* | | | 6.32 | 0.015 | | | |
| 6.69 | 0.445 | 0.208 | 7.3 | 0.927 | 0.0 | 10.17 | 0.0 | 0.0 | CURVE 32* | | | 6.38 | 0.0 | 0.0 | CURVE 32* | | | 6.38 | 0.0 | 0.0 | CURVE 32* | | | 6.38 | 0.0 | | | |
| 6.73 | 0.455 | 0.172 | 7.4 | 0.944 | 0.038 | 10.75 | 0.038 | 0.0 | CURVE 32* | | | 6.53 | 0.038 | 0.038 | CURVE 32* | | | 6.53 | 0.038 | 0.038 | CURVE 32* | | | 6.53 | 0.038 | | | |
| 6.78 | 0.444 | 0.160 | 7.6 | 0.953 | 0.078 | 13.39 | 0.078 | 0.0 | CURVE 32* | | | 6.86 | 0.078 | 0.078 | CURVE 32* | | | 6.86 | 0.078 | 0.078 | CURVE 32* | | | 6.86 | 0.078 | | | |
| 7.00 | 0.070 | 0.111 | 7.7 | 0.111 | 0.038 | 13.93 | 0.038 | 0.0 | CURVE 32* | | | 7.06 | 0.038 | 0.038 | CURVE 32* | | | 7.06 | 0.038 | 0.038 | CURVE 32* | | | 7.06 | 0.038 | | | |
| 7.00 | 0.070 | 0.124 | 7.7 | 0.124 | 0.078 | 14.38 | 0.078 | 0.0 | CURVE 32* | | | 7.13 | 0.078 | 0.078 | CURVE 32* | | | 7.13 | 0.078 | 0.078 | CURVE 32* | | | 7.13 | 0.078 | | | |
| 7.13 | 0.029 | 0.300 | 7.8 | 0.300 | 0.139 | 14.84 | 0.139 | 0.0 | CURVE 32* | | | 7.31 | 0.139 | 0.139 | CURVE 32* | | | 7.31 | 0.139 | 0.139 | CURVE 32* | | | 7.31 | 0.139 | | | |
| 7.28 | 0.012 | 0.417 | 8.0 | 0.417 | 0.255 | 15.23 | 0.255 | 0.0 | CURVE 32* | | | 7.41 | 0.255 | 0.255 | CURVE 32* | | | 7.41 | 0.255 | 0.255 | CURVE 32* | | | 7.41 | 0.255 | | | |
| 7.48 | 0.021 | 0.417 | 8.3 | 0.417 | 0.294 | 16.00 | 0.294 | 0.0 | CURVE 32* | | | 7.50 | 0.294 | 0.294 | CURVE 32* | | | 7.50 | 0.294 | 0.294 | CURVE 32* | | | 7.50 | 0.294 | | | |
| 7.73 | 0.018 | 0.417 | 8.5 | 0.417 | 0.323 | 17.25 | 0.323 | 0.0 | CURVE 32* | | | 7.62 | 0.323 | 0.323 | CURVE 32* | | | 7.62 | 0.323 | 0.323 | CURVE 32* | | | 7.62 | 0.323 | | | |
| 8.04 | 0.035 | 0.395 | 8.6 | 0.395 | 0.344 | 17.83 | 0.344 | 0.0 | CURVE 32* | | | 7.80 | 0.344 | 0.344 | CURVE 32* | | | 7.80 | 0.344 | 0.344 | CURVE 32* | | | 7.80 | 0.344 | | | |
| 8.34 | 0.042 | 0.368 | 8.8 | 0.368 | 0.358 | 18.22 | 0.358 | 0.0 | CURVE 32* | | | 8.05 | 0.358 | 0.358 | CURVE 32* | | | 8.05 | 0.358 | 0.358 | CURVE 32* | | | 8.05 | 0.358 | | | |
| 8.73 | 0.034 | 0.362 | 9.0 | 0.362 | 0.368 | 19.02 | 0.368 | 0.0 | CURVE 32* | | | 8.26 | 0.368 | 0.368 | CURVE 32* | | | 8.26 | 0.368 | 0.368 | CURVE 32* | | | 8.26 | 0.368 | | | |
| 9.04 | 0.023 | 0.378 | 9.2 | 0.378 | 0.374 | 20.18 | 0.374 | 0.0 | CURVE 32* | | | 8.62 | 0.374 | 0.374 | CURVE 32* | | | 8.62 | 0.374 | 0.374 | CURVE 32* | | | 8.62 | 0.374 | | | |
| 9.36 | 0.031 | 0.395 | 9.4 | 0.395 | 0.384 | 22.09 | 0.384 | 0.0 | CURVE 32* | | | 8.74 | 0.384 | 0.384 | CURVE 32* | | | 8.74 | 0.384 | 0.384 | CURVE 32* | | | 8.74 | 0.384 | | | |
| 9.57 | 0.031 | 0.422 | 9.7 | 0.422 | 0.397 | 24.62 | 0.397 | 0.0 | CURVE 32* | | | 8.95 | 0.397 | 0.397 | CURVE 32* | | | 8.95 | 0.397 | 0.397 | CURVE 32* | | | 8.95 | 0.397 | | | |
| 9.93 | 0.0 | 0.301 | 9.8 | 0.301 | 0.466 | CURVE 31 | | | 9.49 | 0.466 | 0.466 | CURVE 31 | | | 9.49 | 0.466 | 0.466 | CURVE 31 | | | 9.49 | 0.466 | 0.466 | CURVE 31 | | | 9.49 | 0.466 |
| 10.0 | 0.185 | 0.100 | 10.0 | 0.185 | 0.167 | T = 293. | | | 9.70 | 0.167 | 0.167 | T = 293. | | | 9.70 | 0.167 | 0.167 | T = 293. | | | 9.70 | 0.167 | 0.167 | T = 293. | | | 9.70 | 0.167 |
| 10.1 | 0.100 | 0.000 | 10.1 | 0.100 | 0.183 | T = 293. | | | 9.80 | 0.183 | 0.183 | T = 293. | | | 9.80 | 0.183 | 0.183 | T = 293. | | | 9.80 | 0.183 | 0.183 | T = 293. | | | 9.80 | 0.183 |
| 10.3 | 0.000 | 0.000 | 10.3 | 0.000 | 0.211 | T = 293. | | | 9.90 | 0.211 | 0.211 | T = 293. | | | 9.90 | 0.211 | 0.211 | T = 293. | | | 9.90 | 0.211 | 0.211 | T = 293. | | | 9.90 | 0.211 |
| 10.3 | 0.837 | 0.699 | 10.3 | 0.837 | 0.226 | T = 293. | | | 10.07 | 0.226 | 0.226 | T = 293. | | | 10.07 | 0.226 | 0.226 | T = 293. | | | 10.07 | 0.226 | 0.226 | T = 293. | | | 10.07 | 0.226 |
| 1.3 | 0.699 | 0.554 | 1.6 | 0.554 | 0.016 | T = 293. | | | 10.75 | 0.016 | 0.016 | T = 293. | | | 10.75 | 0.016 | 0.016 | T = 293. | | | 10.75 | 0.016 | 0.016 | T = 293. | | | 10.75 | 0.016 |
| 1.6 | 0.458 | 0.357 | 1.9 | 0.357 | 0.0 | T = 293. | | | 13.39 | 0.0 | 0.0 | T = 293. | | | 13.39 | 0.0 | 0.0 | T = 293. | | | 13.39 | 0.0 | 0.0 | T = 293. | | | 13.39 | 0.0 |
| 2.5 | 0.314 | 0.281 | 3.0 | 0.281 | 0.033 | T = 293. | | | 13.82 | 0.033 | 0.033 | T = 293. | | | 13.82 | 0.033 | 0.033 | T = 293. | | | 13.82 | 0.033 | 0.033 | T = 293. | | | 13.82 | 0.033 |
| 3.0 | 0.314 | 0.281 | 3.3 | 0.281 | 0.122 | T = 293. | | | 14.29 | 0.122 | 0.122 | T = 293. | | | 14.29 | 0.122 | 0.122 | T = 293. | | | 14.29 | 0.122 | 0.122 | T = 293. | | | 14.29 | 0.122 |
| 3.6 | 0.281 | 0.329 | 3.6 | 0.281 | 0.191 | T = 293. | | | 14.73 | 0.191 | 0.191 | T = 293. | | | 14.73 | 0.191 | 0.191 | T = 293. | | | 14.73 | 0.191 | 0.191 | T = 293. | | | 14.73 | 0.191 |
| 4.1 | 0.434 | 0.434 | 4.1 | 0.434 | 0.250 | T = 293. | | | 15.19 | 0.250 | 0.250 | T = 293. | | | 15.19 | 0.250 | 0.250 | T = 293. | | | 15.19 | 0.250 | 0.250 | T = 293. | | | 15.19 | 0.250 |
| 5.2 | 0.463 | 0.463 | 5.2 | 0.463 | 0.291 | T = 293. | | | 15.57 | 0.291 | 0.291 | T = 293. | | | 15.57 | 0.291 | 0.291 | T = 293. | | | 15.57 | 0.291 | 0.291 | T = 293. | | | 15.57 | 0.291 |
| 5.7 | 0.463 | 0.463 | 5.7 | 0.463 | 0.333 | T = 293. | | | 16.22 | 0.333 | 0.333 | T = 293. | | | 16.22 | 0.333 | 0.333 | T = 293. | | | 16.22 | 0.333 | 0.333 | T = 293. | | | 16.22 | 0.333 |
| 5.8 | 0.432 | 0.432 | 5.8 | 0.432 | 0.350 | T = 293. | | | 16.73 | 0.350 | 0.350 | T = 293. | | | 16.73 | 0.350 | 0.350 | T = 293. | | | 16.73 | 0.350 | 0.350 | T = 293. | | | 16.73 | 0.350 |

*NOT SHOWN IN FIGURE.

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|-------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| CURVE 33 (CONT.)* | | | | | | | | | | | |
| 19.39 | 0.414 | 2.81 | 0.612 | 6.00 | 0.281 | 8.94 | 0.182 | 0.456 | 0.037 | 0.642 | 0.577 |
| 19.98 | 0.420 | 3.19 | 0.607 | 8.20 | 0.320 | 9.54 | 0.099 | 0.463 | 0.050 | 0.664 | 0.581 |
| 20.52 | 0.429 | 3.54 | 0.603 | 8.33 | 0.299 | 9.95 | 0.089 | 0.476 | 0.096 | 0.690 | 0.592 |
| 21.97 | 0.439 | 3.96 | 0.607 | 8.68 | 0.255 | 10.15 | 0.063 | 0.470 | 0.148 | 0.721 | 0.592 |
| 22.97 | 0.446 | 4.21 | 0.604 | 8.94 | 0.241 | 10.30 | 0.024 | 0.486 | 0.217 | 0.758 | 0.585 |
| 24.05 | 0.453 | 4.29 | 0.599 | 9.39 | 0.268 | 10.92 | 0.012 | 0.495 | 0.311 | CURVE 40* | |
| CURVE 34 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 1.00 | 0.619 | 4.43 | 0.603 | 9.65 | 0.301 | 11.43 | 0.0 | 0.515 | 0.420 | T = 450. | |
| 1.97 | 0.649 | 4.56 | 0.607 | 9.75 | 0.262 | CURVE 37* | | 0.528 | 0.497 | 0.456 | |
| 2.78 | 0.654 | 4.70 | 0.599 | 9.82 | 0.199 | T = 295. | | 0.543 | 0.533 | 0.463 | |
| 3.05 | 0.651 | 5.01 | 0.584 | 9.90 | 0.124 | 0.438 | 0.006 | 0.555 | 0.558 | 0.470 | |
| 3.46 | 0.642 | 5.21 | 0.550 | 9.99 | 0.055 | 0.444 | 0.015 | 0.570 | 0.570 | 0.478 | |
| 3.73 | 0.647 | 5.45 | 0.499 | 10.15 | 0.022 | 0.450 | 0.031 | 0.602 | 0.581 | 0.486 | |
| 3.94 | 0.647 | 5.65 | 0.499 | 10.34 | 0.0 | 0.456 | 0.052 | 0.620 | 0.580 | 0.495 | |
| 4.06 | 0.636 | 5.88 | 0.302 | CURVE 36 | | 0.463 | 0.086 | 0.642 | 0.595 | 0.505 | |
| 4.21 | 0.613 | 5.96 | 0.224 | T = 293. | | 0.470 | 0.131 | 0.664 | 0.608 | 0.515 | |
| 4.30 | 0.565 | 6.03 | 0.101 | 1.00 | 0.621 | 0.478 | 0.191 | 0.631 | 0.618 | 0.527 | |
| 4.39 | 0.549 | 6.15 | 0.046 | 1.16 | 0.628 | 0.486 | 0.274 | 0.642 | 0.618 | 0.543 | |
| 4.39 | 0.612 | 6.23 | 0.072 | 1.39 | 0.596 | 0.496 | 0.371 | 0.722 | 0.630 | 0.564 | |
| 4.51 | 0.626 | 6.24 | 0.168 | 2.04 | 0.499 | 0.505 | 0.469 | 0.757 | 0.666 | 0.691 | |
| 4.63 | 0.612 | 6.29 | 0.223 | 2.61 | 0.404 | 0.515 | 0.517 | CURVE 39* | | 0.722 | |
| 4.74 | 0.580 | 6.33 | 0.132 | 3.30 | 0.299 | 0.527 | 0.540 | T = 600. | | 0.757 | |
| 4.83 | 0.559 | 6.37 | 0.039 | 4.00 | 0.226 | 0.544 | 0.551 | 0.450 | 0.010 | 0.559 | |
| 4.93 | 0.578 | 6.45 | 0.019 | 4.67 | 0.182 | 0.556 | 0.556 | 0.456 | 0.021 | 0.559 | |
| 5.10 | 0.557 | 6.56 | 0.037 | 4.81 | 0.182 | 0.570 | 0.567 | 0.463 | 0.042 | 0.559 | |
| 5.39 | 0.473 | 6.62 | 0.192 | 5.01 | 0.167 | 0.585 | 0.573 | 0.470 | 0.073 | 0.559 | |
| 5.56 | 0.417 | 6.70 | 0.394 | 5.20 | 0.148 | 0.602 | 0.589 | 0.478 | 0.114 | 0.559 | |
| 5.70 | 0.359 | 6.73 | 0.543 | 5.48 | 0.161 | 0.621 | 0.592 | 0.486 | 0.170 | 0.559 | |
| CURVE 35 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 1.00 | 0.597 | 6.79 | 0.596 | 5.84 | 0.137 | 0.642 | 0.607 | 0.495 | 0.259 | 0.559 | |
| 1.50 | 0.611 | 6.88 | 0.510 | 6.20 | 0.094 | 0.664 | 0.607 | 0.504 | 0.365 | 0.559 | |
| 1.85 | 0.618 | 7.03 | 0.291 | 6.24 | 0.109 | 0.691 | 0.610 | 0.515 | 0.454 | 0.559 | |
| 2.14 | 0.620 | 7.15 | 0.220 | 6.34 | 0.109 | 0.721 | 0.618 | 0.527 | 0.497 | 0.559 | |
| CURVE 36 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 1.00 | 0.597 | 7.29 | 0.247 | 6.49 | 0.088 | 0.757 | 0.627 | 0.543 | 0.528 | 0.559 | |
| 1.50 | 0.611 | 7.40 | 0.188 | 6.68 | 0.109 | CURVE 38* | | 0.556 | 0.543 | 0.559 | |
| 1.85 | 0.618 | 7.51 | 0.099 | 6.96 | 0.113 | T = 351. | | 0.570 | 0.548 | 0.559 | |
| 2.14 | 0.620 | 7.63 | 0.069 | 7.47 | 0.102 | 0.444 | 0.007 | 0.602 | 0.567 | 0.559 | |
| CURVE 37 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 1.00 | 0.619 | 7.81 | 0.103 | 7.95 | 0.106 | 0.450 | 0.018 | 0.621 | 0.570 | 0.559 | |
| 1.97 | 0.649 | 7.92 | 0.196 | 8.43 | 0.106 | CURVE 39* | | 0.602 | 0.567 | 0.559 | |
| 2.78 | 0.654 | | | | | | | | | | |
| 3.05 | 0.651 | | | | | | | | | | |
| 3.46 | 0.642 | | | | | | | | | | |
| 3.73 | 0.647 | | | | | | | | | | |
| 3.94 | 0.647 | | | | | | | | | | |
| 4.06 | 0.636 | | | | | | | | | | |
| 4.21 | 0.613 | | | | | | | | | | |
| 4.30 | 0.565 | | | | | | | | | | |
| 4.39 | 0.549 | | | | | | | | | | |
| 4.39 | 0.612 | | | | | | | | | | |
| 4.51 | 0.626 | | | | | | | | | | |
| 4.63 | 0.612 | | | | | | | | | | |
| 4.74 | 0.580 | | | | | | | | | | |
| 4.83 | 0.559 | | | | | | | | | | |
| 4.93 | 0.578 | | | | | | | | | | |
| 5.10 | 0.557 | | | | | | | | | | |
| 5.39 | 0.473 | | | | | | | | | | |
| 5.56 | 0.417 | | | | | | | | | | |
| 5.70 | 0.359 | | | | | | | | | | |
| CURVE 41* | | | | | | | | | | | |
| T = 499. | | | | | | | | | | | |
| 0.463 | 0.011 | | | | | | | | | | |
| 0.470 | 0.030 | | | | | | | | | | |
| 0.478 | 0.056 | | | | | | | | | | |
| 0.486 | 0.094 | | | | | | | | | | |
| 0.495 | 0.159 | | | | | | | | | | |
| 0.504 | 0.248 | | | | | | | | | | |
| 0.515 | 0.354 | | | | | | | | | | |
| 0.527 | 0.439 | | | | | | | | | | |
| 0.544 | 0.489 | | | | | | | | | | |
| 0.555 | 0.513 | | | | | | | | | | |
| 0.570 | 0.528 | | | | | | | | | | |
| 0.585 | 0.530 | | | | | | | | | | |
| 0.570 | 0.548 | | | | | | | | | | |
| 0.585 | 0.555 | | | | | | | | | | |
| 0.602 | 0.520 | | | | | | | | | | |
| 0.585 | 0.530 | | | | | | | | | | |
| 0.602 | 0.536 | | | | | | | | | | |
| 0.621 | 0.536 | | | | | | | | | | |

*NOT SHOWN IN FIGURE.

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
|-------------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| CURVE 41 (CONT.)* | | | | | | | | | | | | | |
| 0.621 | 0.534 | 0.570 | 0.502 | 0.570 | 0.483 | 10.03 | 0.431 | 0.142 | 0.0 | 0.399 | 0.026 | 0.427 | 0.271 |
| 0.641 | 0.535 | 0.602 | 0.533 | 0.585 | 0.500 | 10.60 | 0.351 | 0.149 | 3.043 | 0.417 | 0.104 | 0.495 | 0.264 |
| 0.664 | 0.541 | 0.621 | 0.532 | 0.602 | 0.533 | 11.43 | 0.289 | 0.157 | 0.090 | 0.626 | 0.237 | 0.800 | 0.226 |
| 0.692 | 0.546 | 0.641 | 0.529 | 0.621 | 0.540 | 11.80 | 0.257 | 0.166 | 0.077 | 0.898 | 0.244 | 1.013 | 0.277 |
| 0.721 | 0.541 | 0.663 | 0.529 | 0.641 | 0.545 | 12.45 | 0.257 | 0.171 | 0.120 | 1.357 | 0.434 | | |
| 0.750 | 0.459 | 0.692 | 0.522 | 0.664 | 0.547 | 12.91 | 0.281 | 0.180 | 0.172 | | | | |
| CURVE 42* | | | | | | | | | | | | | |
| T = 499. | | | | | | | | | | | | | |
| 0.470 | 0.020 | 0.723 | 0.517 | 0.692 | 0.552 | 13.49 | 0.295 | 0.184 | 0.208 | | | | |
| 0.478 | 0.035 | 0.759 | 0.498 | 0.722 | 0.548 | 13.99 | 0.296 | 0.188 | 0.226 | | | | |
| 0.486 | 0.064 | CURVE 46 | | | | | | | | | | | |
| 0.495 | 0.120 | T = 293. | | | | | | | | | | | |
| 0.504 | 0.192 | 2.00 | 0.542 | 14.68 | 0.319 | 15.34 | 0.350 | | | | | | |
| 0.515 | 0.295 | 2.12 | 0.542 | 15.70 | 0.395 | 16.00 | 0.409 | | | | | | |
| 0.527 | 0.397 | 2.20 | 0.497 | CURVE 47* | | | | | | | | | |
| 0.544 | 0.455 | 2.33 | 0.468 | T = 293. | | | | | | | | | |
| 0.555 | 0.493 | 2.61 | 0.477 | 0.141 | 0.026 | 0.147 | 0.057 | 0.148 | 0.059 | 0.483 | 0.026 | 0.510 | 0.053 |
| 0.570 | 0.514 | 2.83 | 0.477 | 0.153 | 0.079 | 0.157 | 0.112 | 0.155 | 0.114 | 0.554 | 0.083 | 0.603 | 0.136 |
| 0.602 | 0.528 | 2.98 | 0.429 | 0.157 | 0.112 | 0.160 | 0.164 | 0.160 | 0.137 | 0.699 | 0.148 | 0.755 | 0.161 |
| 0.621 | 0.532 | 3.30 | 0.433 | 0.167 | 0.164 | 0.167 | 0.164 | 0.169 | 0.195 | 0.798 | 0.184 | 0.898 | 0.305 |
| 0.641 | 0.532 | 3.39 | 0.433 | 0.174 | 0.215 | 0.178 | 0.238 | 0.178 | 0.223 | 0.951 | 0.376 | 1.345 | 0.584 |
| 0.663 | 0.531 | 3.62 | 0.453 | 0.183 | 0.258 | 0.183 | 0.258 | 0.188 | 0.249 | | | | |
| 0.692 | 0.532 | 3.78 | 0.450 | 0.188 | 0.268 | CURVE 51* | | | | | | | |
| 0.722 | 0.528 | 4.15 | 0.461 | T = 293. | | | | | | | | | |
| 0.750 | 0.507 | 4.36 | 0.461 | 0.141 | 0.153 | 0.150 | 0.215 | 0.141 | 0.153 | 0.427 | 0.271 | 0.506 | 0.297 |
| CURVE 43* | | | | | | | | | | | | | |
| T = 601. | | | | | | | | | | | | | |
| 0.470 | 0.009 | 5.17 | 0.429 | 0.147 | 0.063 | 5.99 | 0.423 | 0.155 | 0.202 | 0.746 | 0.254 | 0.800 | 0.260 |
| 0.478 | 0.021 | 6.19 | 0.395 | 0.158 | 0.152 | 6.83 | 0.405 | 0.159 | 0.215 | 0.953 | 0.304 | 1.024 | 0.337 |
| 0.486 | 0.038 | 7.27 | 0.395 | 0.160 | 0.138 | 7.60 | 0.397 | 0.166 | 0.245 | 1.357 | 0.434 | | |
| 0.495 | 0.077 | 8.04 | 0.389 | 0.165 | 0.206 | 8.35 | 0.397 | 0.169 | 0.320 | | | | |
| 0.505 | 0.141 | 9.03 | 0.381 | 0.171 | 0.236 | 9.26 | 0.404 | 0.172 | 0.342 | | | | |
| 0.515 | 0.229 | 9.41 | 0.404 | 0.175 | 0.263 | 9.55 | 0.515 | 0.177 | 0.351 | | | | |
| 0.527 | 0.337 | 9.71 | 0.615 | 0.188 | 0.283 | 9.71 | 0.615 | | | | | | |
| 0.544 | 0.419 | | | | | | | | | | | | |
| 0.555 | 0.471 | | | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 13-15. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON CARBIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm); TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | τ | λ | τ | λ | τ | λ | τ |
|----------------------|--------|----------------------|--------|----------------------|--------|-----------|--------|
| CURVE 55 T = 293. | | | | | | | |
| 0.452 | 0.123 | 0.449 | 0.167 | 19.9 | 0.093 | 19.7 | 0.257 |
| 0.499 | 0.210 | 0.508 | 0.167 | 20.0 | 0.382 | 19.8 | 0.246 |
| 0.606 | 0.311 | 0.556 | 0.160 | 20.2 | 0.399 | 19.9 | 0.267 |
| 0.741 | 0.351 | 0.616 | 0.156 | 20.5 | 0.413 | 20.2 | 0.402 |
| 0.803 | 0.360 | 0.722 | 0.152 | 20.8 | 0.421 | 20.3 | 0.429 |
| 0.849 | 0.382 | 0.808 | 0.152 | 21.3 | 0.425 | 20.5 | 0.439 |
| 0.933 | 0.407 | 0.859 | 0.157 | CURVE 59 T = 293. | | | |
| 0.956 | 0.439 | 0.906 | 0.169 | 14.0 | 0.201 | 15.1 | 0.341 |
| 1.014 | 0.465 | 0.936 | 0.181 | 15.3 | 0.212 | 15.8 | 0.376 |
| 1.345 | 0.513 | 0.965 | 0.195 | 15.8 | 0.240 | 16.3 | 0.406 |
| CURVE 56* | | | | | | | |
| T = 293. | | | | | | | |
| 0.400 | 0.0 | 0.984 | 0.206 | 16.1 | 0.249 | 16.7 | 0.419 |
| 0.400 | 0.144 | 0.999 | 0.219 | 17.0 | 0.260 | 17.0 | 0.433 |
| 0.408 | 0.170 | 1.014 | 0.237 | 18.0 | 0.269 | 17.7 | 0.442 |
| 0.418 | 0.186 | CURVE 58 T = 293. | | | | | |
| 0.430 | 0.194 | 15.1 | 0.219 | 18.8 | 0.274 | 18.3 | 0.448 |
| 0.449 | 0.194 | 15.2 | 0.236 | 19.5 | 0.278 | 19.0 | 0.458 |
| 0.479 | 0.189 | 15.4 | 0.278 | 20.0 | 0.285 | 20.0 | 0.461 |
| 0.528 | 0.165 | 15.6 | 0.319 | 20.6 | 0.295 | 21.0 | 0.466 |
| 0.580 | 0.154 | 15.7 | 0.329 | CURVE 60 T = 293. | | | |
| 0.645 | 0.141 | 15.8 | 0.326 | 15.4 | 0.307 | 15.5 | 0.323 |
| 0.703 | 0.131 | 15.9 | 0.322 | 15.5 | 0.323 | 15.6 | 0.344 |
| 0.756 | 0.125 | 16.4 | 0.349 | 15.6 | 0.344 | 15.7 | 0.344 |
| 0.833 | 0.125 | 16.6 | 0.366 | 15.7 | 0.339 | 15.8 | 0.339 |
| 0.880 | 0.132 | 16.7 | 0.366 | 16.0 | 0.339 | 16.0 | 0.339 |
| 0.929 | 0.142 | 16.9 | 0.381 | 16.2 | 0.347 | 16.2 | 0.347 |
| 0.973 | 0.150 | 17.2 | 0.395 | 16.3 | 0.365 | 16.3 | 0.365 |
| 0.996 | 0.161 | 17.8 | 0.408 | 16.5 | 0.386 | 16.5 | 0.386 |
| 1.022 | 0.177 | 18.1 | 0.414 | 16.7 | 0.389 | 16.7 | 0.389 |
| CURVE 57* | | | | | | | |
| T = 293. | | | | | | | |
| 0.399 | 0.0 | 18.5 | 0.414 | 17.0 | 0.408 | 17.0 | 0.408 |
| 0.399 | 0.138 | 18.8 | 0.406 | 17.4 | 0.424 | 17.4 | 0.424 |
| 0.414 | 0.153 | 19.0 | 0.397 | 17.9 | 0.436 | 17.9 | 0.436 |
| | | 19.2 | 0.384 | 18.4 | 0.445 | 18.4 | 0.445 |
| | | 19.4 | 0.359 | 19.1 | 0.449 | 19.1 | 0.449 |
| | | 19.5 | 0.306 | 19.2 | 0.444 | 19.2 | 0.444 |
| | | 19.6 | 0.245 | | | | |
| | | 19.7 | 0.095 | | | | |
| | | 19.8 | 0.072 | | | | |

*NOT SHOWN IN FIGURE.

4.14. Silicon Nitride

Bulk silicon nitride is manufactured by standard metallurgical techniques based on reacting silicon powder with nitrogen at elevated temperatures (above 1573 K). It is used as a hard refractory material in high temperature ceramic applications with a useful service temperature of about 1500 K. It dissociates at about 2200 K. It has been reported that there are two types of crystal structure of silicon nitride, α - Si_3N_4 and β - Si_3N_4 , both of which are hexagonal but with different lattice constants in the c-axis [T52257]. Four types of crystal structure of Si_3N_4 have also been reported [T29667]. Silicon nitride is a good electrical insulator with reported resistivity of 10^{12} ohm-cm at room temperature and 10^6 ohm-cm at 1300 K. Its thermal expansion coefficient is $2.5 \times 10^{-6} \text{ K}^{-1}$ over the range of 300-1300 K. As a result of this low thermal expansion, its thermal shock resistance is very good so that this bulk material can be used as a high temperature radome material.

Dense silicon nitride is produced by hot pressing and sintering silicon powder compact in a nitrogen atmosphere at high pressure and at a temperature near the melting point of silicon (1687 K). Using this technique, laboratory preparations have resulted in samples of 98% purity.

There is a considerable increase of interest in silicon nitride thin films for microelectronic applications in the recent years. Silicon nitride films can be prepared by several different deposition techniques:

- a) Direct nitridation
- b) Evaporation
- c) Glow discharge (dc and rf)
- d) Sputtering (dc, rf, and reactive)
- e) Pyrolytic (chemical vapor deposition)

The reactive sputtering and pyrolysis methods have been most frequently utilized. In each of these deposition methods, several parameters can be varied: temperature, flow rate, plasma density, pressure or degree of vacuum, ratio of reactants, or electric field. Prior to deposition, the substrates are usually given a mechanical lap followed by a mechanical or chemical polish. Heat treatment of the film is also utilized.

a. Normal Spectral Emittance (Wavelength Dependence)

There is only one set of data on the normal spectral emittance of Si_3N_4 available. Schatz, Goldberg, Pearson, and Burks [T22272] have measured the emittance for the

sintered specimen with density 1.82 g cm^{-3} at 1023 K. Compared with the theoretical density of 3.43 g cm^{-3} , their specimen has very high porosity. Therefore, based on this measurement only provisional values of normal spectral emittance were reported here which are listed in Table 14-1 and shown in Figure 14-1, and they are slightly lower than the experimental results. The estimated uncertainty of the normal spectral emittance is about $\pm 30\%$.

TABLE 14-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ |
|-----------|------------|-----------|------------|
| SINTERED | | | |
| T = 1023 | | | |
| 1.00 | 0.740 | 11.5 | 0.604 |
| 1.25 | 0.692 | 11.8 | 0.804 |
| 1.39 | 0.687 | 12.0 | 0.815 |
| 1.81 | 0.721 | 12.2 | 0.633 |
| 2.00 | 0.776 | 12.5 | 0.833 |
| 2.25 | 0.789 | 12.6 | 0.836 |
| 3.00 | 0.309 | 12.9 | 0.632 |
| 3.46 | 0.839 | 13.0 | 0.633 |
| 3.60 | 0.835 | 13.5 | 0.641 |
| 3.80 | 0.847 | 14.0 | 0.841 |
| 4.10 | 0.850 | 14.3 | 0.847 |
| 4.16 | 0.851 | 14.5 | 0.841 |
| 4.25 | 0.820 | 14.8 | 0.844 |
| 4.50 | 0.335 | 15.0 | 0.864 |
| 5.00 | 0.355 | | |
| 5.32 | 0.966 | | |
| 5.91 | 0.868 | | |
| 6.00 | 0.358 | | |
| 6.21 | 0.855 | | |
| 6.34 | 0.855 | | |
| 6.50 | 0.872 | | |
| 7.00 | 0.868 | | |
| 7.50 | 0.890 | | |
| 7.68 | 0.896 | | |
| 8.00 | 0.896 | | |
| 8.17 | 0.854 | | |
| 8.55 | 0.873 | | |
| 8.71 | 0.363 | | |
| 9.00 | 0.343 | | |
| 9.25 | 0.825 | | |
| 9.50 | 0.808 | | |
| 9.76 | 0.805 | | |
| 10.0 | 0.914 | | |
| 10.3 | 0.809 | | |
| 10.5 | 0.799 | | |
| 10.6 | 0.810 | | |
| 10.9 | 0.797 | | |
| 11.0 | 0.799 | | |
| 11.3 | 0.798 | | |

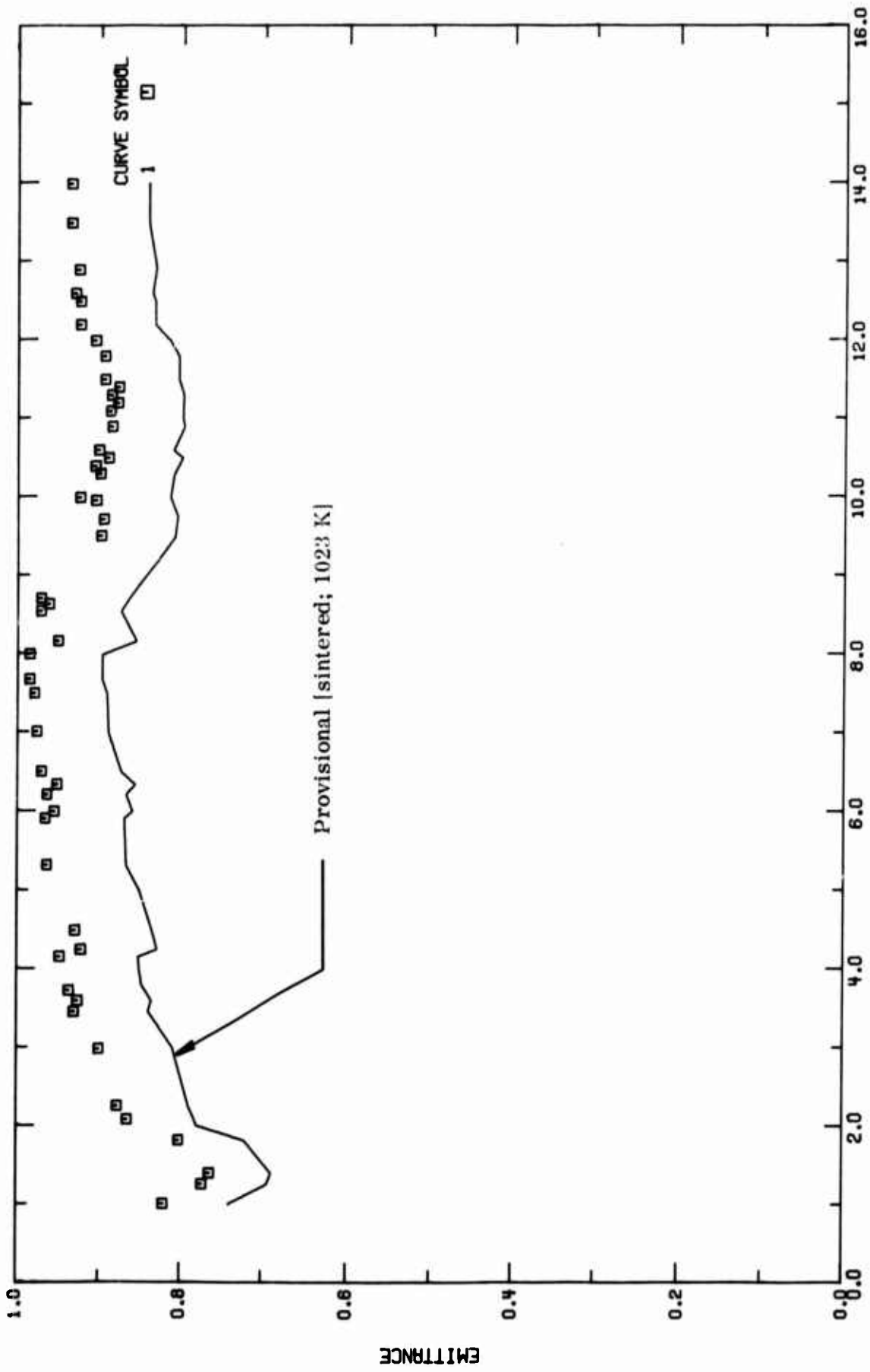


FIGURE 14-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE).

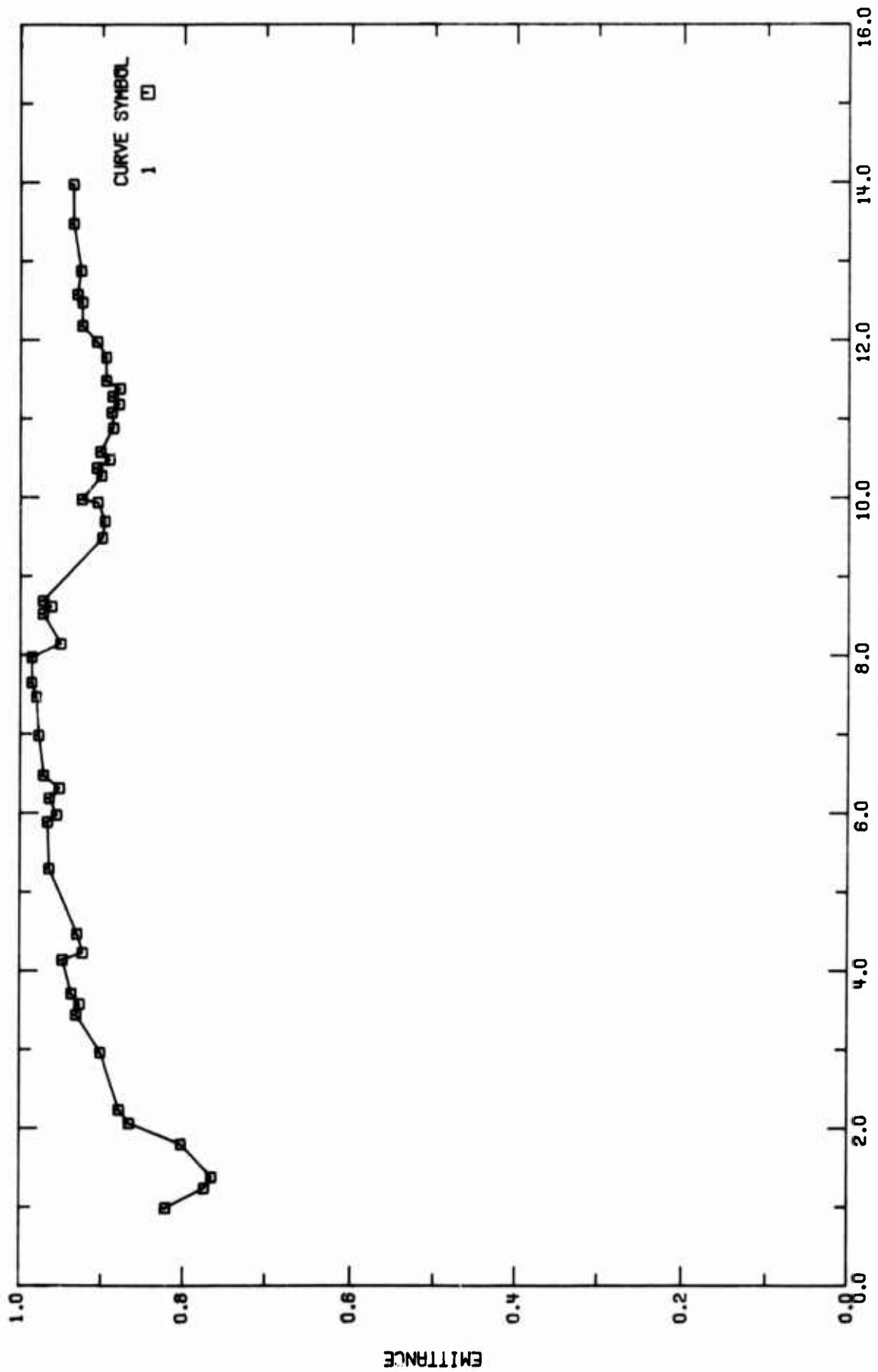


FIGURE 14-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 14-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T22272 | Schatz, E. A., Goldberg, D.M., Pearson, E.A., and Burks, T.L. | 1963 | 1-15 | 1023 | | Sintered at 1673 K for 2 hr (settle material Si_3N_4); density 1.82 g cm^{-3} ; $\theta' = 0^\circ$. |

TABLE 14-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ |
|-----------|------------|-----------------|------------|
| CURVE 1 | | CURVE 1 (CONT.) | |
| T = 1323. | | | |
| 1.00 | 0.820 | 11.4 | 0.877 |
| 1.25 | 0.772 | 11.5 | 0.894 |
| 1.39 | 0.763 | 11.8 | 0.894 |
| 1.81 | 0.801 | 12.0 | 0.905 |
| 2.08 | 0.864 | 12.2 | 0.923 |
| 2.25 | 0.876 | 12.5 | 0.923 |
| 2.98 | 0.899 | 12.6 | 0.929 |
| 3.46 | 0.929 | 12.9 | 0.925 |
| 3.60 | 0.925 | 13.5 | 0.934 |
| 3.73 | 0.935 | 14.0 | 0.934 |
| 4.16 | 0.946 | 14.3 | 0.941 |
| 4.25 | 0.921 | 14.5 | 0.934 |
| 4.49 | 0.928 | 14.8 | 0.938 |
| 5.32 | 0.962 | 15.0 | 0.960 |
| 5.91 | 0.964 | | |
| 6.60 | 0.953 | | |
| 6.21 | 0.962 | | |
| 6.34 | 0.950 | | |
| 6.50 | 0.969 | | |
| 7.01 | 0.975 | | |
| 7.50 | 0.978 | | |
| 7.68 | 0.984 | | |
| 8.00 | 0.984 | | |
| 8.17 | 0.949 | | |
| 8.55 | 0.970 | | |
| 8.64 | 0.960 | | |
| 8.71 | 0.970 | | |
| 9.51 | 0.898 | | |
| 9.72 | 0.895 | | |
| 9.96 | 0.904 | | |
| 10.0 | 0.923 | | |
| 10.3 | 0.899 | | |
| 10.4 | 0.905 | | |
| 10.5 | 0.885 | | |
| 10.6 | 0.901 | | |
| 10.9 | 0.885 | | |
| 11.1 | 0.887 | | |
| 11.2 | 0.878 | | |
| 11.3 | 0.886 | | |

b. Normal Spectral Reflectance (Wavelength Dependence)

There are ten sets of experimental data available for the wavelength dependence of the normal spectral reflectance of silicon nitride as listed in Table 14-6 and shown in Figure 14-4. Specimen characterization and measurement information for the data are given in Table 14-5. Schatz, Goldberg, Pearson, and Burks [T22272] measured the normal spectral reflectance for sintered samples in the 0.23-2.65 μm wavelength region while Schatz [T34908] and Schatz, Alvarez, Counts, and Hepplu [T35840] measured the normal spectral reflectance of compacted powder specimen with compaction pressure from 2350 psi to 70 500 psi in the 0.23-2.65 μm region. Schatz, Alvarez, Burkes, Counts, and Dunkerley [T33974] measured the reflectance for the specimen pressed at 21 000 psi in the 1.0-15 μm wavelength region at 373 K. It is observed that for the sintered specimen, the reflectance data values were lower than those of the pressed samples. One possible explanation is that it has lower density (1.82 g cm^{-3}), hence a lower reflectance value. Since all the measurements were made by the same research group, only one set of data is available for the longer wavelength region. As a consequence, only provisional values are justified. The provisional values are for the pressed specimen at 373 K which are listed in Table 14-4 and shown in Figure 14-3. The estimated uncertainty for the provisional values is within $\pm 30\%$.

TABLE 14-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|--------------------------|--------|-----------|--------|
| COMPACTED POWDER T = 373 | | | |
| 0.23 | 0.225 | 13.50 | 0.301 |
| 0.30 | 0.324 | 14.00 | 0.301 |
| 0.40 | 0.353 | 14.50 | 0.301 |
| 0.50 | 0.368 | 15.00 | 0.296 |
| 0.60 | 0.393 | | |
| 0.75 | 0.418 | | |
| 0.80 | 0.425 | | |
| 0.97 | 0.441 | | |
| 1.00 | 0.429 | | |
| 1.25 | 0.405 | | |
| 1.50 | 0.379 | | |
| 1.75 | 0.347 | | |
| 2.00 | 0.315 | | |
| 2.50 | 0.290 | | |
| 2.65 | 0.270 | | |
| 2.80 | 0.240 | | |
| 3.00 | 0.241 | | |
| 3.25 | 0.241 | | |
| 3.50 | 0.237 | | |
| 3.80 | 0.233 | | |
| 4.00 | 0.231 | | |
| 4.50 | 0.225 | | |
| 5.00 | 0.200 | | |
| 5.50 | 0.183 | | |
| 6.00 | 0.192 | | |
| 6.50 | 0.195 | | |
| 7.00 | 0.200 | | |
| 7.50 | 0.200 | | |
| 8.00 | 0.195 | | |
| 8.50 | 0.204 | | |
| 9.00 | 0.254 | | |
| 9.50 | 0.279 | | |
| 10.00 | 0.297 | | |
| 10.50 | 0.310 | | |
| 11.00 | 0.309 | | |
| 11.50 | 0.303 | | |
| 12.00 | 0.307 | | |
| 12.50 | 0.302 | | |
| 13.00 | 0.306 | | |

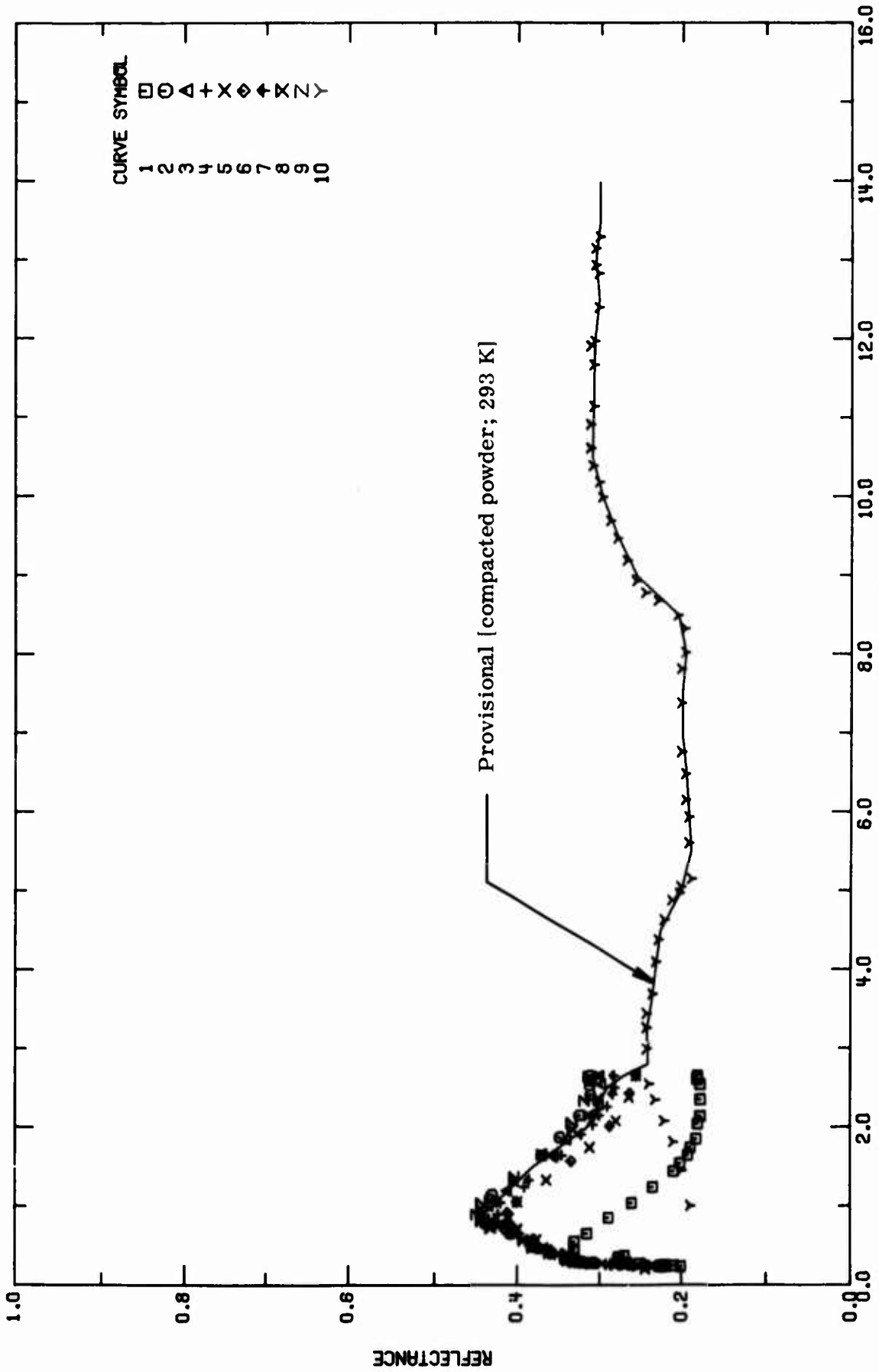


FIGURE 14-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE).

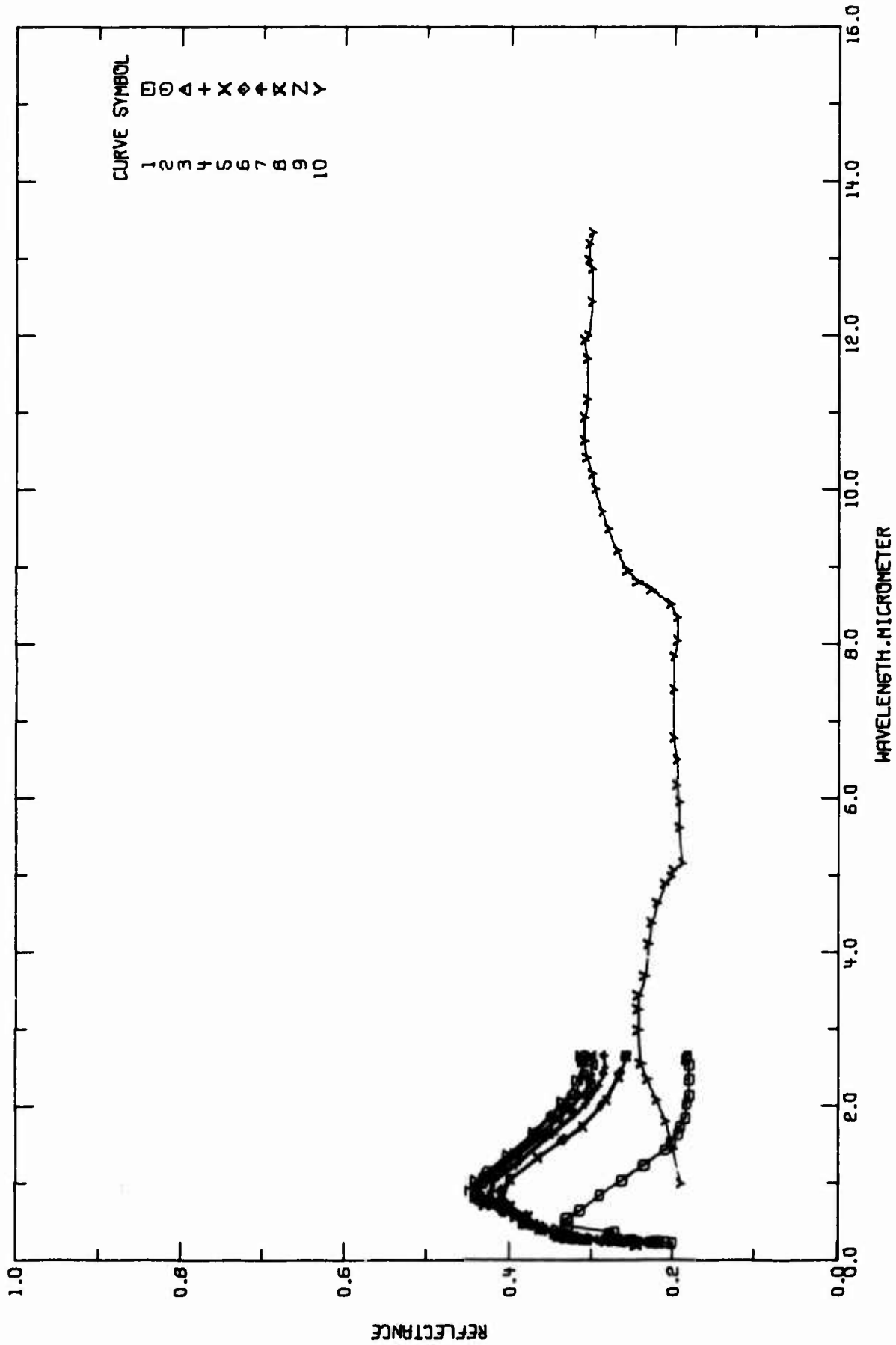


FIGURE 14-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 14-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T22272 | Schatz, E.A., Goldberg, D.M., Pearson, E.G., and Burks, T.L. | 1963 | 0.23-2.65 | 293 | No. 106 | Sintered at 1673 K for 2 hr; density 1.82 g cm^{-3} ; MgO reference standard; data extracted from smooth curve; $\theta=0^\circ$, $\omega'=2\pi$. |
| 2 T34908 | Schatz, E.A. | 1966 | 0.23-2.65 | 293 | | Compacted Si_3N_4 powder; compaction pressure 2350 psi; measurements will be performed on a Beckman DK-2A Spectroreflectometer U.S. MgO standards; $\theta=0^\circ$, $\omega'=2\pi$. |
| 3 T34906 | Schatz, E.A. | 1966 | 0.23-2.65 | 293 | | Similar to the above specimen except compaction pressure 11800 psi. |
| 4 T34908 | Schatz, E.A. | 1966 | 0.23-2.65 | 293 | | Similar to the above specimen except compaction pressure 35300 psi. |
| 5 T34906 | Schatz, E.A. | 1966 | 0.23-2.65 | 293 | | Similar to the above specimen except compaction pressure 70500 psi. |
| 6 T35840 | Schatz, E.A., Alvarez, G.H., Courts, C.H., III, and Hoppe, M.A. | 1965 | 0.23-2.65 | 298 | | Specimen was Si_3N_4 powders compacted into stainless steel circular sample holder under compacting pressure 2350 psi; measurements U.S. MgO standard; $\theta=0^\circ$, $\omega'=2\pi$. |
| 7 T35840 | Schatz, E.A., et al. | 1965 | 0.23-2.65 | 298 | | Similar to the above specimen except compacting pressure 11750 psi. |
| 8 T35840 | Schatz, E.A., et al. | 1965 | 0.23-2.65 | 298 | | Similar to the above specimen except compacting pressure 35350 psi. |
| 9 T35840 | Schatz, E.A., et al. | 1965 | 0.23-2.65 | 298 | | Similar to the above specimen except compacting pressure 70500 psi. |
| 10 T35974 | Schatz, E.A., Alvarez, G.H., Burks, T.L., Courts, C.R., III, and Dunckerley, F.J. | 1964 | 1-15 | 373 | | Pressed Si_3N_4 powder specimen; pressed at 21000 psi; the absolute spectral reflectance are measured by using a blackbody reflectometer apparatus; $\theta=0^\circ$, $\omega'=2\pi$. |

TABLE 14-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|------------------|--------|
| CURVE 10 (CONT.) | |
| 5.61 | 0.191 |
| 5.94 | 0.191 |
| 6.16 | 0.195 |
| 6.49 | 0.195 |
| 6.77 | 0.200 |
| 7.39 | 0.200 |
| 7.82 | 0.200 |
| 8.03 | 0.195 |
| 8.33 | 0.195 |
| 8.50 | 0.204 |
| 8.69 | 0.228 |
| 8.79 | 0.243 |
| 8.94 | 0.254 |
| 9.20 | 0.266 |
| 9.48 | 0.278 |
| 9.70 | 0.287 |
| 10.00 | 0.297 |
| 10.19 | 0.301 |
| 10.40 | 0.309 |
| 10.62 | 0.312 |
| 10.92 | 0.312 |
| 11.15 | 0.308 |
| 11.68 | 0.308 |
| 11.92 | 0.312 |
| 11.98 | 0.307 |
| 12.41 | 0.302 |
| 12.84 | 0.302 |
| 12.95 | 0.306 |
| 13.16 | 0.306 |
| 13.31 | 0.301 |
| 14.15 | 0.301 |
| 14.38 | 0.304 |
| 14.51 | 0.301 |
| 14.87 | 0.302 |
| 15.00 | 0.296 |

c. Normal Spectral Absorptance (Wavelength Dependence)

There are four sets of experimental data available for the wavelength dependence of the normal spectral absorptance of silicon nitride as listed in Table 14-9 and shown in Figure 14-5. Specimen characterization and measurement information for the data are given in Table 14-8. Three sets of data are for the thin film specimen coating on silicon substrate and one set of data is for the powder specimen. All the measurements were performed at room temperature. They all show a broad peak of absorption with the maximum near the 10-12 μm region. However, there is no information on the thickness of the sample and substrate which is essentially for the absorptance value. Therefore, we cannot make any recommended values for the absorptance on coating specimens. According to Kirchhoff's law, the absorptance is equal to the emittance, $\alpha = \epsilon$. Therefore, the provisional values on the normal spectral absorptance for sintered specimens at 1023 K were obtained which are listed in Table 14-7 and shown in Figure 14-6. The estimated uncertainty is about $\pm 30\%$.

TABLE 14-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|-----------|----------|------------------|----------|
| SINTERED | | SINTERED | |
| T = 1623 | | T = 1023 (CONT.) | |
| 1.00 | 0.740 | 11.5 | 0.854 |
| 1.25 | 0.592 | 11.3 | 0.604 |
| 1.39 | 0.687 | 12.0 | 0.815 |
| 1.81 | 0.721 | 12.2 | 0.833 |
| 2.00 | 0.778 | 12.5 | 0.833 |
| 2.25 | 0.789 | 12.6 | 0.836 |
| 3.00 | 0.809 | 12.9 | 0.832 |
| 3.46 | 0.839 | 13.0 | 0.833 |
| 3.60 | 0.835 | 13.5 | 0.641 |
| 3.80 | 0.847 | 14.0 | 0.841 |
| 4.00 | 0.850 | 14.3 | 0.847 |
| 4.16 | 0.851 | 14.5 | 0.841 |
| 4.25 | 0.829 | 14.8 | 0.844 |
| 4.50 | 0.835 | 15.0 | 0.664 |
| 5.00 | 0.858 | | |
| 5.32 | 0.866 | | |
| 5.91 | 0.856 | | |
| 6.00 | 0.853 | | |
| 6.21 | 0.856 | | |
| 6.34 | 0.855 | | |
| 6.50 | 0.872 | | |
| 7.00 | 0.888 | | |
| 7.50 | 0.890 | | |
| 7.68 | 0.896 | | |
| 8.00 | 0.896 | | |
| 8.17 | 0.854 | | |
| 8.55 | 0.873 | | |
| 8.71 | 0.863 | | |
| 9.00 | 0.843 | | |
| 9.25 | 0.825 | | |
| 9.50 | 0.808 | | |
| 9.76 | 0.805 | | |
| 10.0 | 0.814 | | |
| 10.3 | 0.809 | | |
| 10.5 | 0.793 | | |
| 10.6 | 0.810 | | |
| 10.9 | 0.797 | | |
| 11.0 | 0.799 | | |
| 11.3 | 0.798 | | |

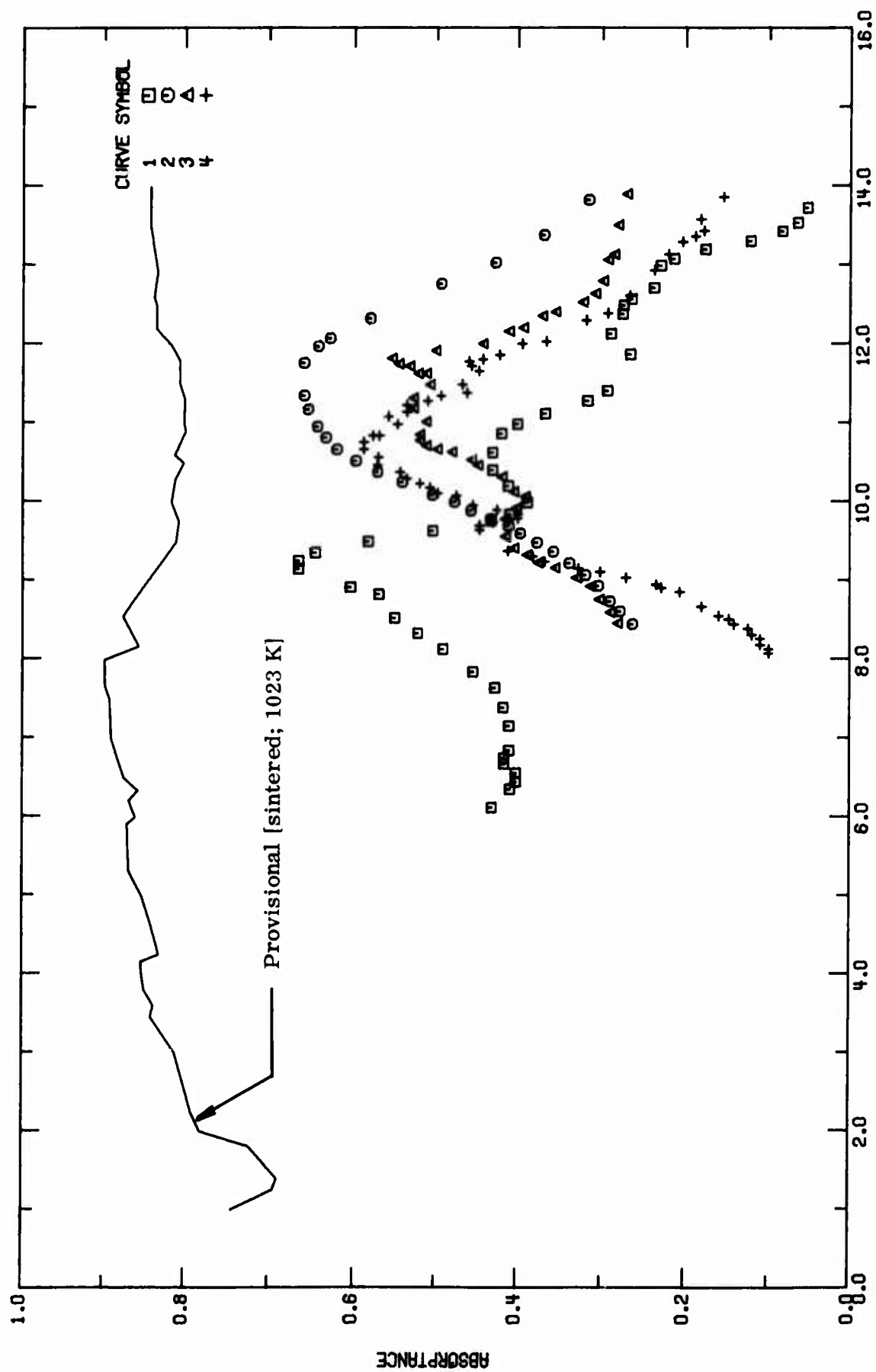


FIGURE 14-5. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE).

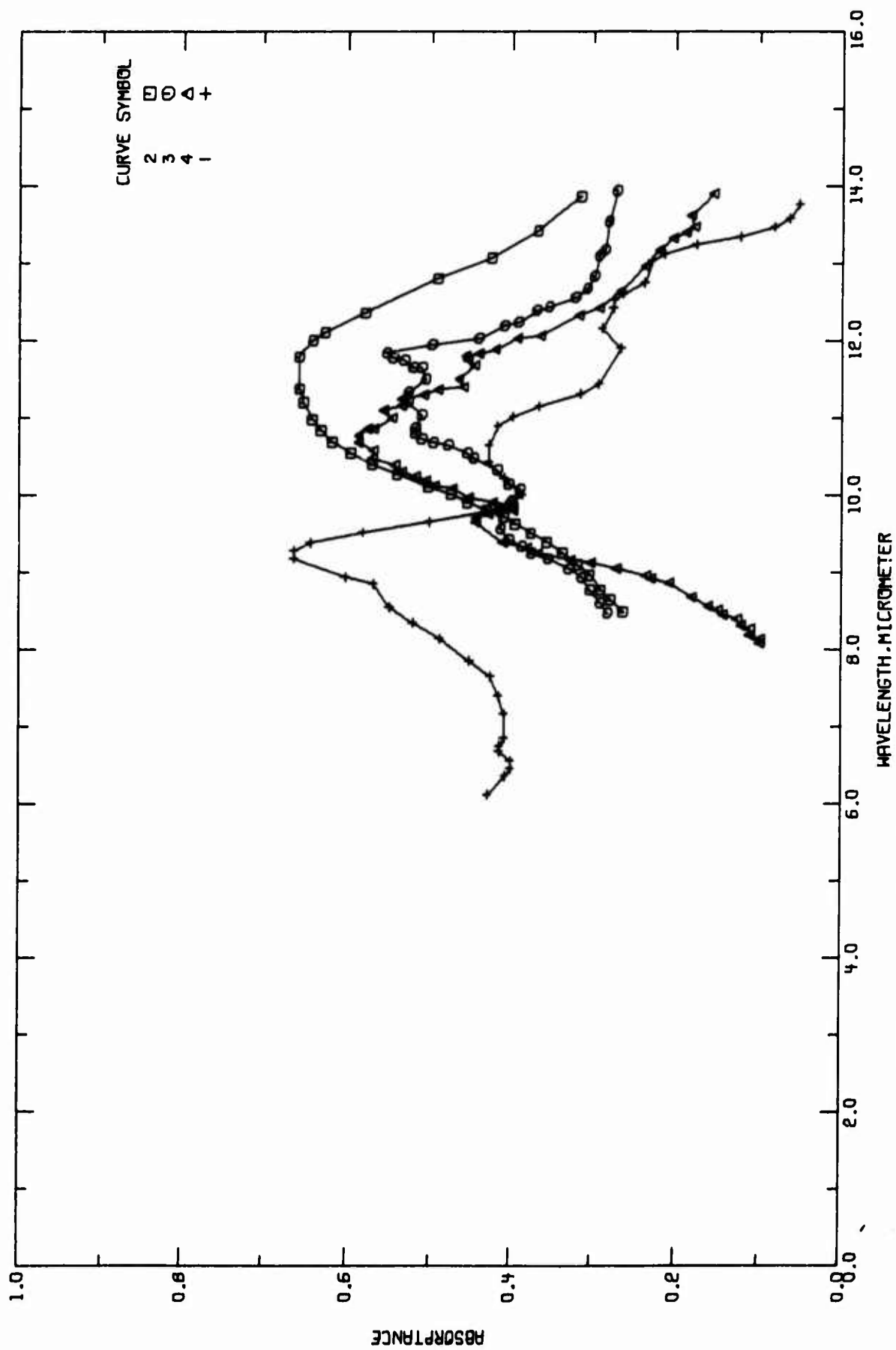


FIGURE 14-6. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE).

TABLE 14-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 E46853 | Bartnitski, I.N., Ayunoo, B.M., and Kuryalva, R.G. | 1970 | 6-25 | ~293 | Si_3N_4 on Si | Silicon nitride film was deposited on silicon by electrolysis in liquid ammonia with a constant voltage applied to the cell; the film resistivity was of the order of $10^3 \Omega\text{-cm}$; a UR-10 spectrograph was used to obtain the absorption spectra. |
| 2 E3-318 | Badcock, F.R., Lamb, D.R., and Wood, S.S. | 1967 | 8.5-14.5 | ~293 | | Silicon nitride film was deposited on silicon substrate by reacting together ammonia and silane or trichlorosilane vapor; data were extracted from the smooth curve; $9\text{-}0^\circ$. |
| 3 E24316 | Badcock, F.R., et al. | 1967 | 8.5-14.5 | ~293 | | Silicon nitride crystalline film was grown thermally at 1300 C in ammonia at atm pressure; data were extracted from the smooth curve; $9\text{-}0^\circ$. |
| 4 E34318 | Badcock, F.R., et al. | 1967 | 8.5-14.5 | ~293 | | Silicon nitride powder; data were extracted from the smooth curve; $9\text{-}0^\circ$. |

TABLE 14-9. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| CURVE 1 T = 293. | | CURVE 1 (CONT.) | | CURVE 2 T = 293. | | CURVE 3 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 T = 293. | | CURVE 4 (CONT.) | |
|---------------------|----------|-----------------|----------|---------------------|----------|-----------------|----------|-----------------|----------|---------------------|----------|-----------------|----------|
| λ | α | λ | α | λ | α | λ | α | λ | α | λ | α | λ | α |
| 6.11 | 0.429 | 13.09 | 0.213 | 8.45 | 0.262 | 9.16 | 0.353 | 14.12 | 0.257 | 8.07 | 0.899 | 10.46 | 0.570 |
| 6.35 | 0.407 | 13.21 | 0.176 | 6.61 | 0.277 | 9.23 | 0.374 | 14.37 | 0.255 | 8.12 | 0.099 | 10.56 | 0.569 |
| 6.64 | 0.400 | 13.32 | 0.122 | 8.73 | 0.289 | 9.32 | 0.387 | 14.58 | 0.255 | 8.18 | 0.110 | 10.66 | 0.587 |
| 5.55 | 0.480 | 13.44 | 0.083 | 8.93 | 0.303 | 9.41 | 0.403 | 14.77 | 0.252 | 8.26 | 0.120 | 10.75 | 0.587 |
| 6.67 | 0.414 | 13.55 | 0.064 | 9.07 | 0.303 | 9.55 | 0.413 | | | 8.31 | 0.120 | 10.83 | 0.576 |
| 6.74 | 0.414 | 13.74 | 0.052 | 9.22 | 0.336 | 9.78 | 0.413 | | | 8.38 | 0.125 | 10.83 | 0.568 |
| 6.84 | 0.408 | 14.10 | 0.052 | 9.36 | 0.355 | 9.91 | 0.400 | | | 8.44 | 0.142 | 10.98 | 0.546 |
| 7.15 | 0.408 | 14.31 | 0.035 | 9.48 | 0.375 | 10.06 | 0.389 | | | 8.50 | 0.160 | 11.07 | 0.557 |
| 7.39 | 0.415 | 14.60 | 0.020 | 9.60 | 0.395 | 10.12 | 0.403 | | | 8.55 | 0.140 | 11.14 | 0.535 |
| 7.64 | 0.425 | 14.84 | 0.030 | 9.69 | 0.409 | 10.31 | 0.417 | | | 8.67 | 0.160 | 11.22 | 0.535 |
| 7.84 | 0.452 | 15.04 | 0.065 | 9.88 | 0.431 | 10.46 | 0.447 | | | 8.85 | 0.206 | 11.27 | 0.509 |
| 8.13 | 0.489 | 15.20 | 0.225 | 9.99 | 0.455 | 10.53 | 0.455 | | | 8.90 | 0.228 | 11.34 | 0.492 |
| 8.33 | 0.521 | 15.31 | 0.265 | 10.08 | 0.475 | 10.66 | 0.497 | | | 9.03 | 0.234 | 11.38 | 0.460 |
| 8.53 | 0.549 | 15.41 | 0.303 | 10.88 | 0.503 | 10.66 | 0.497 | | | 9.11 | 0.301 | 11.46 | 0.466 |
| 8.83 | 0.568 | 15.60 | 0.405 | 10.37 | 0.540 | 10.78 | 0.511 | | | 9.15 | 0.326 | 11.66 | 0.446 |
| 8.92 | 0.602 | 15.75 | 0.442 | 10.52 | 0.570 | 10.85 | 0.519 | | | 9.23 | 0.366 | 11.72 | 0.455 |
| 9.16 | 0.663 | 16.00 | 0.468 | 10.66 | 0.596 | 10.85 | 0.519 | | | 9.30 | 0.380 | 11.81 | 0.458 |
| 9.26 | 0.663 | 16.16 | 0.323 | 11.17 | 0.618 | 11.01 | 0.511 | | | 9.37 | 0.410 | 11.86 | 0.420 |
| 9.36 | 0.543 | 16.31 | 0.157 | 11.17 | 0.631 | 11.19 | 0.527 | | | 9.44 | 0.445 | 12.00 | 0.393 |
| 9.50 | 0.581 | 16.45 | 0.114 | 11.35 | 0.641 | 11.31 | 0.527 | | | 9.69 | 0.445 | 12.03 | 0.364 |
| 9.63 | 0.502 | 16.61 | 0.082 | 11.76 | 0.652 | 11.48 | 0.506 | | | 9.74 | 0.428 | 12.30 | 0.317 |
| 9.77 | 0.439 | 16.92 | 0.064 | 13.04 | 0.657 | 11.63 | 0.511 | | | 9.78 | 0.398 | 12.39 | 0.292 |
| 9.84 | 0.407 | 17.36 | 0.064 | 13.39 | 0.657 | 11.63 | 0.521 | | | 9.85 | 0.423 | 12.61 | 0.266 |
| 9.99 | 0.396 | 17.86 | 0.032 | 13.83 | 0.640 | 11.72 | 0.532 | | | 9.89 | 0.453 | 12.94 | 0.237 |
| 10.20 | 0.409 | 18.49 | 0.006 | 13.83 | 0.626 | 11.75 | 0.545 | | | 9.95 | 0.423 | 13.14 | 0.220 |
| 10.41 | 0.428 | 19.16 | 0.011 | 12.33 | 0.575 | 11.82 | 0.553 | | | 10.07 | 0.473 | 13.30 | 0.203 |
| 10.63 | 0.428 | 20.28 | 0.045 | 12.77 | 0.592 | 11.92 | 0.499 | | | 10.10 | 0.496 | 13.37 | 0.188 |
| 10.87 | 0.417 | 21.65 | 0.109 | 13.04 | 0.425 | 12.00 | 0.441 | | | 10.17 | 0.506 | 13.44 | 0.178 |
| 10.99 | 0.398 | 22.62 | 0.109 | 13.39 | 0.367 | 12.17 | 0.409 | | | 10.29 | 0.519 | 13.59 | 0.162 |
| 11.12 | 0.365 | 23.31 | 0.095 | 13.83 | 0.314 | 12.21 | 0.392 | | | 10.29 | 0.535 | 13.67 | 0.155 |
| 11.29 | 0.315 | 23.81 | 0.060 | | | 12.36 | 0.369 | | | 10.29 | 0.535 | 14.18 | 0.134 |
| 11.42 | 0.292 | 24.27 | 0.026 | | | 12.41 | 0.353 | | | 10.29 | 0.535 | 14.49 | 0.121 |
| 11.68 | 0.285 | 24.81 | 0.012 | | | 12.53 | 0.321 | | | 10.29 | 0.535 | 14.64 | 0.113 |
| 12.14 | 0.285 | 25.38 | 0.051 | | | 12.64 | 0.307 | | | | | | |
| 12.39 | 0.274 | 25.77 | 0.104 | 8.45 | 0.280 | 12.80 | 0.298 | | | | | | |
| 12.50 | 0.273 | 25.97 | 0.161 | 8.59 | 0.289 | 13.07 | 0.292 | | | | | | |
| 12.58 | 0.263 | | | 8.76 | 0.302 | 13.14 | 0.285 | | | | | | |
| 12.72 | 0.237 | | | 8.92 | 0.312 | 13.51 | 0.280 | | | | | | |
| 13.00 | 0.229 | | | 9.03 | 0.328 | 13.91 | 0.270 | | | | | | |

d. Normal Spectral Transmittance (Wavelength Dependence)

There are 33 sets of experimental data available for the wavelength dependence of the normal spectral transmittance of silicon nitride as listed in Table 14-12 and shown in Figure 14-8 for the thin film coatings and Figure 14-9 for the powder specimens. Specimen characterization and measurement information are given in Table 14-11. All the measurements were performed at room temperature (~ 293 K) and a broad absorption peak due to Si-N has a maximum near $11.4 \mu\text{m}$.

Silicon, germanium, molybdenum, graphite, gallium arsenide, graphite, and potassium chloride were used as the coating substrate. Fifteen sets of experimental data were measured for the transmittance of thin Si_3N_4 film coating on silicon substrates. However, few authors have reported the thickness of the film and substrate. The various deposition techniques for preparation of the thin films also affect the transmittance. The silicon nitride film was also used as an antireflection coating for silicon and the maximum of transmission was dependent on the thickness of the coating by the well-known square-root condition for quarter-wave films as follows:

$$4n_1 d\lambda_0^{-1} = 2m + 1; m = 0, 1, 2, 3, \dots \quad (14-1)$$

$$R_{\min} \approx \left(\frac{n_2 - n_1}{n_2 + n_1} \right)^2 \ll 1 \text{ for } n_1^2 \approx n_2 \quad (14-2)$$

where d is the coating thickness, λ_0 the free space wavelength, R_{\min} the minimum intensity reflectance, and n_1 and n_2 are the refractive indices of the coating and substrate, respectively. Therefore, as a consequence of these difficulties, only the provisional values for a $0.5 \mu\text{m}$ thick silicon nitride film deposited on both sides of a $250 \mu\text{m}$ thick silicon substrate by the reactive sputtering technique at room temperature are presented. The estimated uncertainty is within $\pm 30\%$.

TABLE 14--10. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T |
|--------------|-------|-----------------|-------|
| COATING | | COATING | |
| SI SUBSTRATE | | SI SUBSTRATE | |
| T = 293 | | T = 293 (CONT.) | |
| 1.00 | 0.059 | 7.50 | 0.592 |
| 1.08 | 0.446 | 8.00 | 0.557 |
| 1.16 | 0.780 | 8.50 | 0.413 |
| 1.19 | 0.854 | 9.00 | 0.282 |
| 1.24 | 0.950 | 9.70 | 0.241 |
| 1.26 | 0.976 | 10.00 | 0.172 |
| 1.30 | 0.999 | 10.50 | 0.128 |
| 1.34 | 0.973 | 11.00 | 0.110 |
| 1.40 | 0.925 | 11.40 | 0.097 |
| 1.44 | 0.945 | 11.60 | 0.098 |
| 1.50 | 0.757 | 12.00 | 0.098 |
| 1.57 | 0.563 | 12.35 | 0.109 |
| 1.62 | 0.625 | 13.03 | 0.118 |
| 1.66 | 0.594 | 13.50 | 0.133 |
| 1.73 | 0.565 | 14.00 | 0.180 |
| 1.78 | 0.546 | 14.50 | 0.210 |
| 1.87 | 0.535 | 15.00 | 0.243 |
| 1.93 | 0.535 | | |
| 2.00 | 0.542 | | |
| 2.10 | 0.562 | | |
| 2.29 | 0.611 | | |
| 2.39 | 0.645 | | |
| 2.57 | 0.723 | | |
| 2.80 | 0.835 | | |
| 3.00 | 0.897 | | |
| 3.20 | 0.928 | | |
| 3.50 | 0.980 | | |
| 3.65 | 0.994 | | |
| 3.80 | 0.993 | | |
| 4.00 | 0.981 | | |
| 4.25 | 0.962 | | |
| 4.50 | 0.939 | | |
| 4.75 | 0.895 | | |
| 5.00 | 0.856 | | |
| 5.25 | 0.823 | | |
| 5.50 | 0.771 | | |
| 5.80 | 0.722 | | |
| 6.40 | 0.665 | | |
| 7.00 | 0.612 | | |

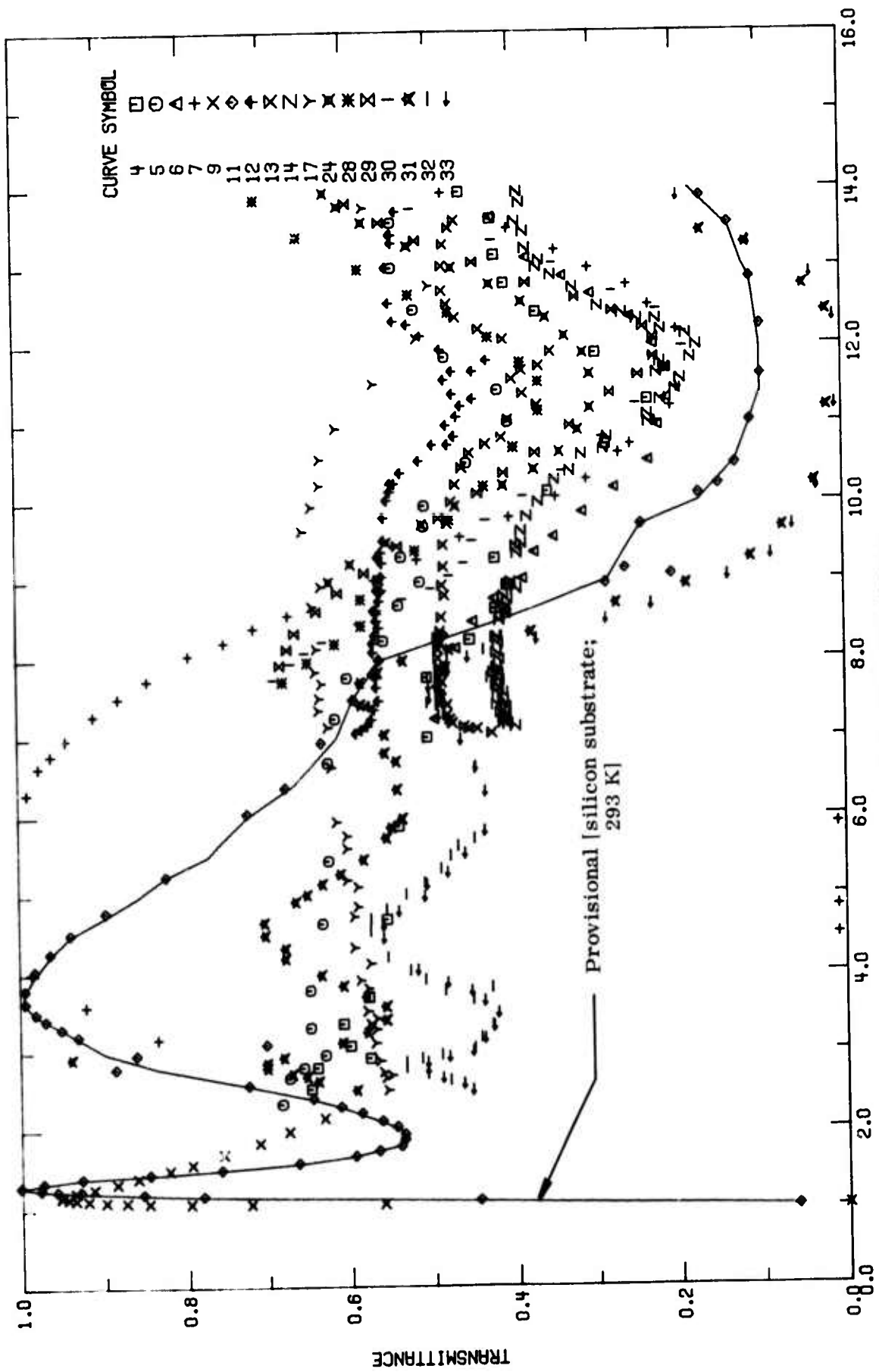


FIGURE 14-7. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE COATINGS (WAVELENGTH DEPENDENCE).

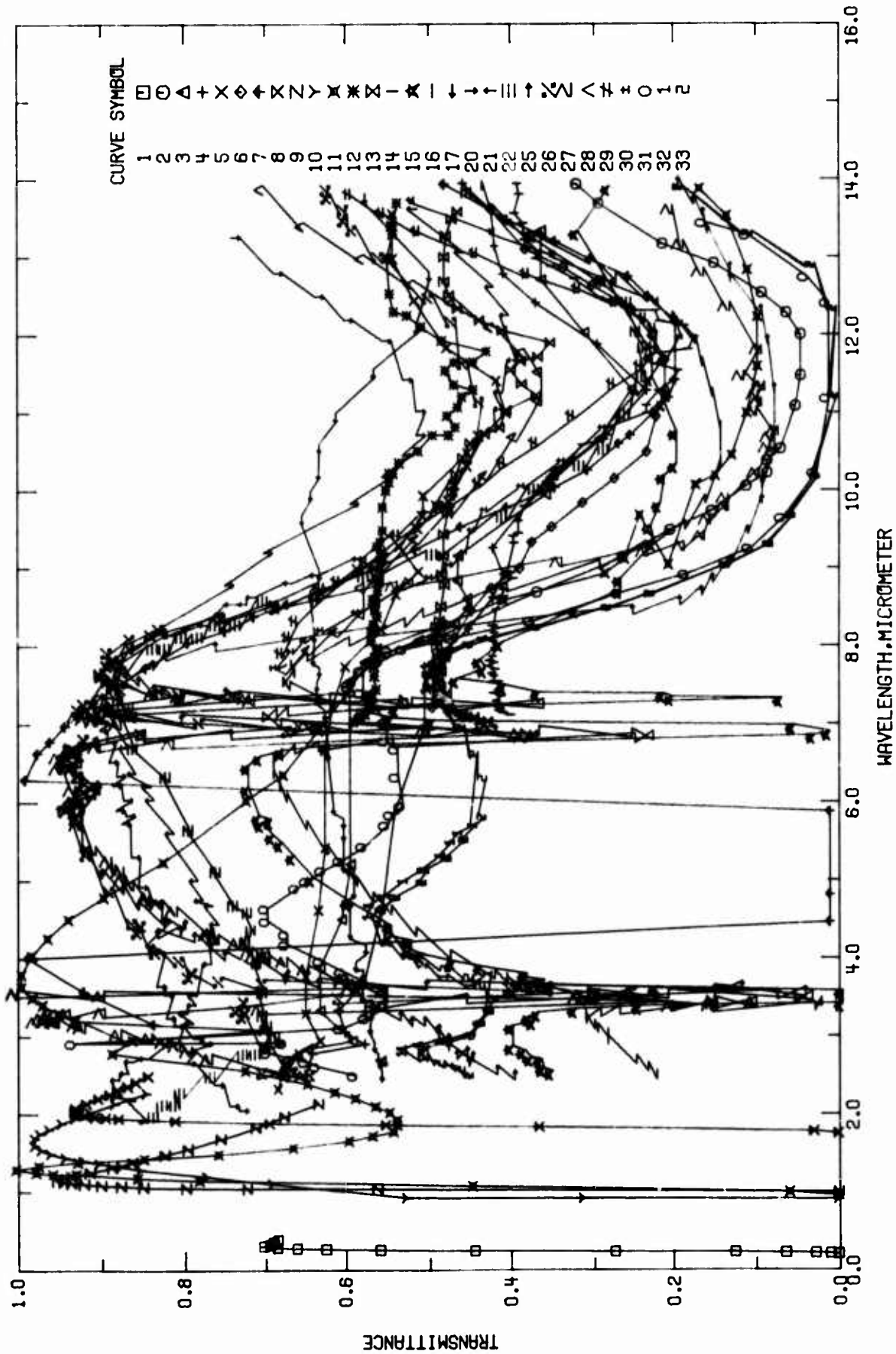


FIGURE 14-8. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE COATINGS (WAVELENGTH DEPENDENCE).

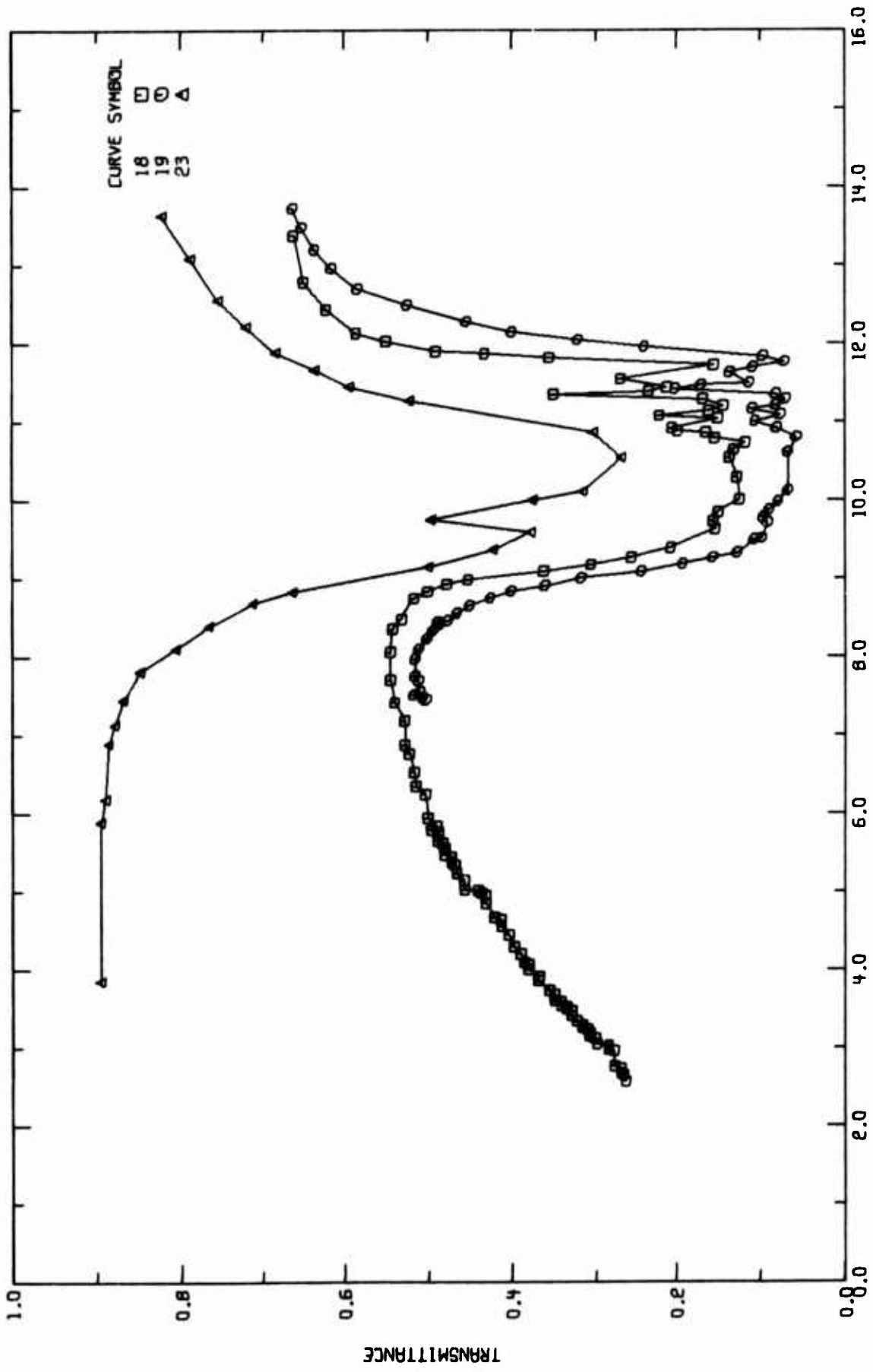


FIGURE 14-9. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE POWDERS (WAVELENGTH DEPENDENCE).

TABLE 14-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|------------------------------------|---|
| 1 T45177 | Dean, K.E., Klein, P.S., Yeakly, R.L., and Runyan, W.R. | 1967 | 0.2-0.4 | 293 | | Si_3N_4 film was deposited on fused silica substrate; index of refraction 2.0; no absorption band between 0.4 and 8 μ ; θ - 0° . |
| 2 T45177 | Bean, K.E., et al. | 1967 | 8-24 | 293 | | Similar to the above specimen. |
| 3 T45954 | Saki, H. and Moriyama, K. | 1967 | 2.5-16 | 293 | | Si_3N_4 film was deposited on GaAs substrate by reacting SiCl_4 and NH_3 in N_2 atm at 823 K; θ - 0° . |
| 4 T45954 | Seki, H. and Moriyama, K. | 1967 | 2.5-16 | 293 | | Similar to the above specimen except deposited on Si substrate by reacting SiCl_4 and NH_3 in N_2 atm at 823 K. |
| 5 T45954 | Seki, H. and Moriyama, K. | 1967 | 2.5-16 | 293 | | Similar to the above specimen except at 723 K. |
| 6 T48136 | Sugano, T., Hirai, K., Kuroiwa, K., and Itoh, K. | 1968 | 7-12 | 293 | | Si_3N_4 film was deposited on Si substrate by gas phase reaction of SiH_4 and NH_3 , using N_2 as carrier gas at 1123 K; θ - 0° . |
| 7 T-2872 | Nuttall, P., Rowbottom, C., and Eastwood, E. | 1967 | 3-15 | 293 | | 1 μm thickness Si_3N_4 films were deposited on 10 Ω cm N-type Si substrate at 1273 K by thermal reaction of NH_3 with SiH_4 , SiCl_4 , or SiBr_4 ; θ - 0° . |
| 8 T61411 | Laff, R.A. | 1971 | 1.8-2.6 | 293 | | 0.245 μm film of silicon nitride was coated on both sides of Ge window (3840 μm thickness) by rf-diode reactive sputtering technique; θ - 0° . |
| 9 T61411 | Laff, R.A. | 1971 | 1.0-2.2 | 293 | | Similar to the above specimen except 0.140 μm film of silicon nitride was coated on both side of Si window (750 μm thickness). |
| 10 T61411 | Laff, R.A. | 1971 | 0.9-2.3 | 293 | | Similar to the above specimen except 0.220 μm film of silicon nitride was coated on both side of GaAs window (100 μm thickness). |
| 11 T61411 | Laff, R.A. | 1971 | 1-15 | 293 | | Similar to the above specimen except 0.505 μm film of silicon nitride was coated on both side of Si window (250 μm thickness). |
| 12 T65344 | Kamchaska, M.I., and Ormont, B.F. | 1971 | 6.67-20 | 293 | | Polycrystalline Si_3N_4 was coated on p-type Si single crystal substrate by reaction of ammonia with the silicon substrate at 1623 K for 18 min; θ - 0° . |
| 13 T65344 | Kamchaska, M.I., and Ormont, B.F. | 1971 | 6.67-20 | 293 | | Similar to the above specimen except it was prepared for 60 min. |
| 14 T65344 | Kamchaska, M.I., and Ormont, B.F. | 1971 | 6.67-20 | 293 | | Similar to the above specimen except it was prepared for 180 min. |
| 15 T44942 | Berg, D., Lewis, D.W., Dakin, T.W., Estrich, D.E., and Epposito, J.N. | 1966 | 2.5-50 | 293 | | Si_3N_4 film was deposited on graphite substrate by pyrolysis of SiF_4 and 2NH_3 ; θ - 0° . |
| 16 T44942 | Berg, D., et al. | 1966 | 2.5-50 | 293 | | Similar to the above specimen except amorphous Si_3N_4 film was deposited on graphite substrate by pyrolysis of SiH_4 and NH_3 . |
| 17 T70779 | Kijima, K., Setaka, N., Ishii, M., and Tanaka, H. | 1973 | 2.5-25 | 293 | α - Si_3N_4 | Polycrystalline Si_3N_4 film was deposited on Si substrate in 15 min at 1473 K; θ - 0° . |

TABLE 14-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (Wavelength Dependence) (continued)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|--|------|---------------------------------|----------------------|------------------------------------|---|
| 18 T70731 | Mazdiyasi, K.S. and Cooke, C.M. | 1973 | 2.5-50 | 293 | α - Si_3N_4 | Si_3N_4 powder prepared by amonolysis of SiCl_4 and calcined at 1573 K for 2 hr in vacuum; a 1 mg of the nitride was dispersed in 400 mg of anhydrous spectrographic grade Cel Powder and pressed into disks for infrared studies; $\theta \sim 0^\circ$. Similar to the above specimen except it was calcined at 1563 K for 2 hr in vacuum. |
| 19 T70731 | Mazdiyasi, K.S. and Cooke, C.M. | 1973 | 7.4-50 | 293 | α - Si_3N_4 | |
| 20 T71498 | Buck, J. | 1973 | 2-15 | 293 | | Si_3N_4 film was sputtering on KCl substrate by pyrolysis of SiH_4 and NH_3 at 823 K. Similar to the above specimen. |
| 21 T71498 | Buck, J. | 1973 | 2-15 | 293 | | Similar to the above specimen. |
| 22 T71498 | Buck, J. | 1973 | 2-15 | 293 | | Similar to the above specimen. |
| 23 E5770 | Kaiser, W. and Tharmond, C.D. | 1959 | 3.5-15 | ~ 293 | | Si_3N_4 powder was contained in KBr pellet; data were extracted from the smooth figure. |
| 24 E42663 | Fränz, I. and Langschiech, W. | 1966 | 9-14 | ~ 293 | | Amorphous silicon nitride film was applied to the mechanically polished p-type silicon wafer by means of reaction between silane and ammonia at 1000 C, and then was tempered in dry nitrogen for 10 min at 1200 C; data were extracted from the smooth curve; $\theta \sim 0^\circ$. |
| 25 E27965 | Lewis, D.W., Esposito, J.N., Dakin, T.W., and Berg, D. | 1966 | 2.5-15 | ~ 293 | Sample 104-114 | Silicon nitride coating was deposited on Mo substrate by pyrolysis of silane and ammonia at reduced pressure; infrared spectra (Nujol) was extracted from the figure; $\theta \sim 0^\circ$. |
| 26 F27955 | Lewis, D.W., et al. | 1966 | 2.5-15 | ~ 293 | Sample 104-112 | Similar to the above specimen. |
| 27 E47985 | Lewis, D.W., et al. | 1966 | 2.5-4.0 | ~ 293 | Sample 118-140 | Similar to the above specimen except large area of well crystallized α - Si_3N_4 plus some amorphous were formed. |
| 28 E32764 | Kuwano, Yukinov' | 1968 | 7.7-15 | ~ 293 | | Silicon nitride film was deposited on 10 Ω -cm N-type silicon wafer by the glow discharge reaction of SiH_4 and NH_3 ; data were extracted from the smooth curve; $\theta \sim 0^\circ$. |
| 29 E32764 | Kuwano, Yukinov' | 1968 | 7.7-15 | ~ 293 | | Silicon nitride film was deposited on 10 Ω -cm N-type silicon wafer by the glow discharge reaction of SiH_4 and N_2 ; data were extracted from the smooth curve; $\theta \sim 0^\circ$. |
| 30 E32764 | Kuwano, Yukinov' | 1968 | 7.7-15 | ~ 293 | | Silicon nitride film was deposited on 10 Ω -cm N-type silicon by the reactive sputtering; data were extracted from the smooth curve; $\theta \sim 0^\circ$. |
| 31 E27192 | Doo, V.Y., Nichols, D.R., and Slivey, G.A. | 1966 | 2.5-30 | ~ 293 | | Silicon nitride film was deposited on silicon substrate by pyrolytic process by react silane and ammonia in the pressure of excess hydrogen; data were extracted from the smooth curve; $\theta \sim 0^\circ$. |
| 32 E27192 | Doo, V.Y., et al. | 1966 | 2.5-30 | ~ 293 | | Similar to the above specimen except it was annealed at 1160 C for 3 hr in N_2 atm. |
| 33 E27192 | Doo, V.Y., et al. | 1966 | 2.5-30 | ~ 293 | | Similar to the above specimen. |

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE)
(WAVELENGTH, λ, μm; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 1 | | | CURVE 2 (CONT.) | | | CURVE 3 (CONT.) | | | CURVE 4 (CONT.) | | | CURVE 5 | | | CURVE 6 (CONT.) | | | CURVE 7 (CONT.) | | | |
|---------------------|-------|-------|-----------------|-------|-------|-----------------|-------|-------|-----------------|-------|-------|---------------------|-------|-------|-----------------|-------|-------|-----------------|-------|-------|-------|
| λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | |
| CURVE 1 T = 293. | | | CURVE 2 (CONT.) | | | CURVE 3 (CONT.) | | | CURVE 4 (CONT.) | | | CURVE 5 T = 293. | | | CURVE 6 (CONT.) | | | CURVE 7 (CONT.) | | | |
| 0.220 | 0.000 | 0.352 | 14.16 | 0.352 | 0.454 | 9.18 | 0.454 | 0.475 | 14.70 | 0.475 | 0.13 | 8.13 | 0.468 | 0.712 | 8.40 | 0.712 | 0.568 | 9.00 | 0.568 | 0.346 | 0.346 |
| 0.225 | 0.010 | 0.361 | 14.31 | 0.361 | 0.357 | 9.97 | 0.357 | 0.475 | 15.93 | 0.475 | 6.47 | 6.47 | 0.448 | 0.670 | 8.56 | 0.670 | 0.423 | 9.00 | 0.423 | 0.267 | 0.267 |
| 0.230 | 0.028 | 0.363 | 14.64 | 0.363 | 0.348 | 10.21 | 0.348 | 0.475 | | | 8.76 | 8.76 | 0.308 | 0.565 | 9.00 | 0.565 | 0.374 | 9.26 | 0.374 | 0.253 | 0.253 |
| 0.235 | 0.064 | 0.385 | 14.96 | 0.385 | 0.292 | 10.68 | 0.292 | 0.475 | | | 9.02 | 9.02 | 0.350 | 0.514 | 9.55 | 0.514 | 0.350 | 9.55 | 0.350 | 0.403 | 0.403 |
| 0.240 | 0.124 | 0.387 | 15.94 | 0.387 | 0.251 | 11.32 | 0.251 | 0.475 | | | 9.35 | 9.35 | 0.313 | 0.461 | 9.60 | 0.461 | 0.313 | 9.60 | 0.313 | 0.307 | 0.307 |
| 0.250 | 0.272 | 0.340 | 16.57 | 0.340 | 0.311 | 12.05 | 0.311 | 0.475 | | | 9.55 | 9.55 | 0.273 | 0.461 | 9.60 | 0.461 | 0.273 | 9.60 | 0.273 | 0.346 | 0.346 |
| 0.300 | 0.443 | 0.388 | 17.12 | 0.388 | 0.362 | 12.73 | 0.362 | 0.475 | | | 9.86 | 9.86 | 0.233 | 0.461 | 9.60 | 0.461 | 0.233 | 9.60 | 0.233 | 0.307 | 0.307 |
| 0.350 | 0.557 | 0.380 | 17.96 | 0.380 | 0.362 | 13.36 | 0.362 | 0.475 | | | 10.17 | 10.17 | 0.232 | 0.461 | 9.60 | 0.461 | 0.232 | 9.60 | 0.232 | 0.267 | 0.267 |
| 0.400 | 0.658 | 0.362 | 18.37 | 0.362 | 0.362 | 13.36 | 0.362 | 0.475 | | | 10.52 | 10.52 | 0.220 | 0.461 | 9.60 | 0.461 | 0.220 | 9.60 | 0.220 | 0.253 | 0.253 |
| 0.450 | 0.770 | 0.362 | 18.73 | 0.362 | 0.375 | 14.67 | 0.375 | 0.475 | | | 10.96 | 10.96 | 0.209 | 0.461 | 9.60 | 0.461 | 0.209 | 9.60 | 0.209 | 0.223 | 0.223 |
| 0.500 | 0.843 | 0.362 | 18.90 | 0.362 | 0.364 | 14.92 | 0.364 | 0.475 | | | 11.31 | 11.31 | 0.209 | 0.461 | 9.60 | 0.461 | 0.209 | 9.60 | 0.209 | 0.234 | 0.234 |
| 0.550 | 0.888 | 0.304 | 19.27 | 0.304 | 0.368 | 15.32 | 0.368 | 0.475 | | | 11.70 | 11.70 | 0.225 | 0.461 | 9.60 | 0.461 | 0.225 | 9.60 | 0.225 | 0.196 | 0.196 |
| 0.600 | 0.922 | 0.302 | 19.84 | 0.302 | 0.355 | 15.67 | 0.355 | 0.475 | | | 12.00 | 12.00 | 0.252 | 0.461 | 9.60 | 0.461 | 0.252 | 9.60 | 0.252 | 0.230 | 0.230 |
| 0.650 | 0.968 | 0.314 | 21.41 | 0.314 | 0.314 | 15.87 | 0.314 | 0.475 | | | 12.36 | 12.36 | 0.301 | 0.461 | 9.60 | 0.461 | 0.301 | 9.60 | 0.301 | 0.255 | 0.255 |
| 0.700 | 0.988 | 0.320 | 21.72 | 0.320 | 0.320 | | | 0.475 | | | 12.66 | 12.66 | 0.336 | 0.461 | 9.60 | 0.461 | 0.336 | 9.60 | 0.336 | 0.303 | 0.303 |
| 0.750 | 0.997 | 0.360 | 22.09 | 0.360 | 0.360 | | | 0.475 | | | 13.12 | 13.12 | 0.381 | 0.461 | 9.60 | 0.461 | 0.381 | 9.60 | 0.381 | 0.345 | 0.345 |
| 0.800 | 0.999 | 0.369 | 22.55 | 0.369 | 0.369 | | | 0.475 | | | 13.64 | 13.64 | 0.423 | 0.461 | 9.60 | 0.461 | 0.423 | 9.60 | 0.423 | 0.402 | 0.402 |
| 0.850 | 0.999 | 0.387 | 22.79 | 0.387 | 0.387 | 2.52 | 0.647 | 0.475 | | | 14.03 | 14.03 | 0.464 | 0.461 | 9.60 | 0.461 | 0.464 | 9.60 | 0.464 | 0.480 | 0.480 |
| 0.900 | 0.999 | 0.432 | 23.40 | 0.432 | 0.432 | 2.79 | 0.639 | 0.475 | | | 14.51 | 14.51 | 0.533 | 0.461 | 9.60 | 0.461 | 0.533 | 9.60 | 0.533 | 0.528 | 0.528 |
| 0.950 | 0.999 | 0.439 | 24.15 | 0.439 | 0.439 | 2.91 | 0.575 | 0.475 | | | 15.38 | 15.38 | 0.506 | 0.461 | 9.60 | 0.461 | 0.506 | 9.60 | 0.506 | 0.551 | 0.551 |
| 1.000 | 0.999 | 0.439 | 25.00 | 0.439 | 0.439 | 3.07 | 0.599 | 0.475 | | | 16.70 | 16.70 | 0.453 | 0.461 | 9.60 | 0.461 | 0.453 | 9.60 | 0.453 | 0.579 | 0.579 |
| CURVE 2 | | | CURVE 3 | | | CURVE 4 | | | CURVE 5 | | | CURVE 6 | | | CURVE 7 | | | CURVE 8 | | | |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | |
| 7.50 | 0.597 | 0.675 | 2.49 | 0.675 | 0.504 | 7.00 | 0.504 | 0.416 | 3.17 | 0.834 | 3.17 | 0.834 | 0.000 | 0.000 | 1.759 | 0.000 | 1.759 | 0.030 | 0.030 | 1.871 | 0.550 |
| 7.94 | 0.520 | 0.658 | 2.77 | 0.658 | 0.504 | 7.76 | 0.504 | 0.478 | 3.59 | 0.919 | 3.59 | 0.919 | 0.030 | 0.030 | 1.785 | 0.030 | 1.785 | 0.365 | 0.365 | 1.871 | 0.550 |
| 8.11 | 0.494 | 0.644 | 2.85 | 0.644 | 0.421 | 8.24 | 0.421 | 0.511 | 4.02 | 0.985 | 4.02 | 0.985 | 0.365 | 0.365 | 1.846 | 0.365 | 1.846 | 0.480 | 0.480 | 1.974 | 0.906 |
| 8.71 | 0.368 | 0.590 | 2.95 | 0.590 | 0.421 | 8.64 | 0.421 | 0.541 | 4.47 | 1.010 | 4.47 | 1.010 | 0.480 | 0.480 | 1.871 | 0.480 | 1.871 | 0.579 | 0.579 | 2.001 | 0.919 |
| 9.16 | 0.263 | 0.629 | 3.34 | 0.629 | 0.421 | 8.94 | 0.421 | 0.541 | 4.82 | 1.010 | 4.82 | 1.010 | 0.550 | 0.550 | 1.909 | 0.550 | 1.909 | 0.809 | 0.809 | 2.081 | 0.925 |
| 9.51 | 0.203 | 0.629 | 3.90 | 0.629 | 0.421 | 9.28 | 0.421 | 0.571 | 5.88 | 0.810 | 5.88 | 0.810 | 0.809 | 0.809 | 1.959 | 0.809 | 1.959 | 0.809 | 0.809 | 2.174 | 0.906 |
| 9.75 | 0.153 | 0.603 | 4.51 | 0.603 | 0.356 | 10.13 | 0.356 | 0.574 | 6.65 | 0.974 | 6.65 | 0.974 | 0.893 | 0.893 | 1.968 | 0.893 | 1.968 | 0.893 | 0.893 | 2.281 | 0.925 |
| 10.07 | 0.111 | 0.592 | 5.22 | 0.592 | 0.283 | 10.73 | 0.283 | 0.581 | 7.00 | 0.959 | 7.00 | 0.959 | 0.893 | 0.893 | 1.974 | 0.893 | 1.974 | 0.893 | 0.893 | 2.374 | 0.925 |
| 10.24 | 0.086 | 0.593 | 7.57 | 0.593 | 0.232 | 11.30 | 0.232 | 0.581 | 7.52 | 0.941 | 7.52 | 0.941 | 0.893 | 0.893 | 1.979 | 0.893 | 1.979 | 0.893 | 0.893 | 2.467 | 0.925 |
| 10.40 | 0.086 | 0.593 | 7.81 | 0.593 | 0.232 | 11.90 | 0.232 | 0.581 | 7.74 | 0.941 | 7.74 | 0.941 | 0.893 | 0.893 | 1.981 | 0.893 | 1.981 | 0.893 | 0.893 | 2.560 | 0.925 |
| 10.55 | 0.070 | 0.511 | 8.09 | 0.511 | 0.269 | 12.43 | 0.269 | 0.581 | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 1.984 | 0.893 | 1.984 | 0.893 | 0.893 | 2.653 | 0.925 |
| 11.10 | 0.052 | 0.468 | 8.32 | 0.468 | 0.407 | 12.73 | 0.407 | 0.422 | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 1.987 | 0.893 | 1.987 | 0.893 | 0.893 | 2.746 | 0.925 |
| 11.49 | 0.046 | 0.453 | 8.50 | 0.453 | 0.418 | 13.16 | 0.418 | 0.422 | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 1.990 | 0.893 | 1.990 | 0.893 | 0.893 | 2.839 | 0.925 |
| 12.02 | 0.046 | 0.453 | 8.63 | 0.453 | 0.458 | 13.63 | 0.458 | 0.422 | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 1.993 | 0.893 | 1.993 | 0.893 | 0.893 | 2.932 | 0.925 |
| 12.30 | 0.063 | 0.465 | 8.86 | 0.465 | 0.465 | 13.97 | 0.465 | 0.458 | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 1.996 | 0.893 | 1.996 | 0.893 | 0.893 | 3.025 | 0.925 |
| 12.56 | 0.092 | 0.468 | | | | | | | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 1.999 | 0.893 | 1.999 | 0.893 | 0.893 | 3.118 | 0.925 |
| 12.94 | 0.150 | 0.468 | | | | | | | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 2.002 | 0.893 | 2.002 | 0.893 | 0.893 | 3.211 | 0.925 |
| 13.19 | 0.212 | 0.453 | | | | | | | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 2.005 | 0.893 | 2.005 | 0.893 | 0.893 | 3.304 | 0.925 |
| 13.71 | 0.293 | 0.453 | | | | | | | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 2.008 | 0.893 | 2.008 | 0.893 | 0.893 | 3.397 | 0.925 |
| 13.96 | 0.322 | 0.465 | | | | | | | 8.06 | 0.922 | 8.06 | 0.922 | 0.893 | 0.893 | 2.011 | 0.893 | 2.011 | 0.893 | 0.893 | 3.490 | 0.925 |

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| CURVE 13 (CONT.) | | | CURVE 14 (CONT.) | | | CURVE 14 (CONT.) | | | CURVE 14 (CONT.) | | | CURVE 15 (CONT.) | | | CURVE 15 (CONT.) | | | CURVE 15 (CONT.) | | | CURVE 16 | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|----------|--|--|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | | |
| 11.74 | 0.366 | 6.08 | 0.420 | 12.74 | 0.322 | 3.60 | 0.354 | 7.79 | 0.441 | 7.79 | 0.441 | 7.79 | 0.441 | 2.50 | 0.210 | 2.50 | 0.210 | 2.50 | 0.210 | 2.50 | 0.210 | | |
| 11.92 | 0.351 | 8.19 | 0.418 | 12.90 | 0.350 | 3.62 | 0.377 | 8.01 | 0.414 | 8.01 | 0.414 | 8.01 | 0.414 | 2.61 | 0.229 | 2.61 | 0.229 | 2.61 | 0.229 | 2.61 | 0.229 | | |
| 12.08 | 0.408 | 8.28 | 0.421 | 13.00 | 0.368 | 3.64 | 0.390 | 8.44 | 0.325 | 8.44 | 0.325 | 8.44 | 0.325 | 2.70 | 0.244 | 2.70 | 0.244 | 2.70 | 0.244 | 2.70 | 0.244 | | |
| 12.21 | 0.437 | 8.28 | 0.419 | 13.09 | 0.364 | 3.67 | 0.363 | 8.68 | 0.270 | 8.68 | 0.270 | 8.68 | 0.270 | 2.85 | 0.280 | 2.85 | 0.280 | 2.85 | 0.280 | 2.85 | 0.280 | | |
| 12.36 | 0.464 | 8.49 | 0.416 | 13.25 | 0.381 | 3.70 | 0.385 | 9.29 | 0.227 | 9.29 | 0.227 | 9.29 | 0.227 | 3.05 | 0.293 | 3.05 | 0.293 | 3.05 | 0.293 | 3.05 | 0.293 | | |
| 12.53 | 0.474 | 8.58 | 0.408 | 13.46 | 0.363 | 3.75 | 0.385 | 9.51 | 0.232 | 9.51 | 0.232 | 9.51 | 0.232 | 3.11 | 0.307 | 3.11 | 0.307 | 3.11 | 0.307 | 3.11 | 0.307 | | |
| 12.71 | 0.480 | 8.63 | 0.414 | 13.59 | 0.393 | 3.85 | 0.440 | 9.79 | 0.220 | 9.79 | 0.220 | 9.79 | 0.220 | 3.22 | 0.330 | 3.22 | 0.330 | 3.22 | 0.330 | 3.22 | 0.330 | | |
| 13.02 | 0.489 | 8.66 | 0.409 | 13.83 | 0.387 | 3.92 | 0.474 | 10.15 | 0.215 | 10.15 | 0.215 | 10.15 | 0.215 | 3.31 | 0.354 | 3.31 | 0.354 | 3.31 | 0.354 | 3.31 | 0.354 | | |
| 13.30 | 0.478 | 8.75 | 0.406 | 13.97 | 0.390 | 4.01 | 0.511 | 10.30 | 0.200 | 10.30 | 0.200 | 10.30 | 0.200 | 3.37 | 0.387 | 3.37 | 0.387 | 3.37 | 0.387 | 3.37 | 0.387 | | |
| 13.51 | 0.471 | 8.80 | 0.411 | 14.10 | 0.383 | 4.07 | 0.525 | 10.72 | 0.200 | 10.72 | 0.200 | 10.72 | 0.200 | 3.44 | 0.417 | 3.44 | 0.417 | 3.44 | 0.417 | 3.44 | 0.417 | | |
| 13.61 | 0.464 | 8.89 | 0.395 | 14.18 | 0.394 | 4.19 | 0.525 | 11.10 | 0.215 | 11.10 | 0.215 | 11.10 | 0.215 | 3.52 | 0.450 | 3.52 | 0.450 | 3.52 | 0.450 | 3.52 | 0.450 | | |
| 14.08 | 0.460 | 8.94 | 0.404 | 14.18 | 0.367 | 4.24 | 0.548 | 11.42 | 0.230 | 11.42 | 0.230 | 11.42 | 0.230 | 3.58 | 0.483 | 3.58 | 0.483 | 3.58 | 0.483 | 3.58 | 0.483 | | |
| 14.16 | 0.450 | 8.98 | 0.402 | 14.45 | 0.390 | 4.37 | 0.548 | 11.71 | 0.230 | 11.71 | 0.230 | 11.71 | 0.230 | 3.62 | 0.517 | 3.62 | 0.517 | 3.62 | 0.517 | 3.62 | 0.517 | | |
| 14.33 | 0.446 | 9.35 | 0.394 | 14.58 | 0.372 | 4.69 | 0.599 | 12.72 | 0.290 | 12.72 | 0.290 | 12.72 | 0.290 | 3.65 | 0.542 | 3.65 | 0.542 | 3.65 | 0.542 | 3.65 | 0.542 | | |
| 14.41 | 0.434 | 9.43 | 0.395 | 14.71 | 0.360 | 5.00 | 0.642 | 13.30 | 0.323 | 13.30 | 0.323 | 13.30 | 0.323 | 3.69 | 0.577 | 3.69 | 0.577 | 3.69 | 0.577 | 3.69 | 0.577 | | |
| 14.66 | 0.424 | 9.47 | 0.389 | 14.79 | 0.356 | 5.28 | 0.667 | 13.87 | 0.284 | 13.87 | 0.284 | 13.87 | 0.284 | 3.72 | 0.602 | 3.72 | 0.602 | 3.72 | 0.602 | 3.72 | 0.602 | | |
| | | 9.62 | 0.389 | 14.90 | 0.342 | 5.44 | 0.682 | 14.04 | 0.368 | 14.04 | 0.368 | 14.04 | 0.368 | 3.76 | 0.637 | 3.76 | 0.637 | 3.76 | 0.637 | 3.76 | 0.637 | | |
| | | 9.81 | 0.382 | 15.06 | 0.338 | 5.54 | 0.693 | 14.20 | 0.426 | 14.20 | 0.426 | 14.20 | 0.426 | 3.80 | 0.662 | 3.80 | 0.662 | 3.80 | 0.662 | 3.80 | 0.662 | | |
| | | 10.00 | 0.368 | 15.22 | 0.340 | 5.74 | 0.706 | 14.95 | 0.480 | 14.95 | 0.480 | 14.95 | 0.480 | 3.84 | 0.687 | 3.84 | 0.687 | 3.84 | 0.687 | 3.84 | 0.687 | | |
| | | 10.20 | 0.347 | 15.38 | 0.337 | 5.79 | 0.695 | 15.27 | 0.480 | 15.27 | 0.480 | 15.27 | 0.480 | 3.88 | 0.712 | 3.88 | 0.712 | 3.88 | 0.712 | 3.88 | 0.712 | | |
| | | 10.40 | 0.328 | | | 6.15 | 0.724 | 16.26 | 0.529 | 16.26 | 0.529 | 16.26 | 0.529 | 3.92 | 0.737 | 3.92 | 0.737 | 3.92 | 0.737 | 3.92 | 0.737 | | |
| | | 10.60 | 0.313 | | | 6.44 | 0.724 | 16.26 | 0.548 | 16.26 | 0.548 | 16.26 | 0.548 | 3.96 | 0.762 | 3.96 | 0.762 | 3.96 | 0.762 | 3.96 | 0.762 | | |
| | | 10.67 | 0.286 | | | 6.55 | 0.708 | 16.56 | 0.541 | 16.56 | 0.541 | 16.56 | 0.541 | 4.00 | 0.787 | 4.00 | 0.787 | 4.00 | 0.787 | 4.00 | 0.787 | | |
| | | 10.82 | 0.281 | | | 6.63 | 0.681 | 17.48 | 0.579 | 17.48 | 0.579 | 17.48 | 0.579 | 4.04 | 0.812 | 4.04 | 0.812 | 4.04 | 0.812 | 4.04 | 0.812 | | |
| | | 11.11 | 0.232 | | | 6.80 | 0.624 | 18.59 | 0.579 | 18.59 | 0.579 | 18.59 | 0.579 | 4.08 | 0.837 | 4.08 | 0.837 | 4.08 | 0.837 | 4.08 | 0.837 | | |
| | | 11.30 | 0.216 | | | 6.85 | 0.615 | 19.01 | 0.548 | 19.01 | 0.548 | 19.01 | 0.548 | 4.12 | 0.862 | 4.12 | 0.862 | 4.12 | 0.862 | 4.12 | 0.862 | | |
| | | 11.43 | 0.198 | | | 6.85 | 0.615 | 19.96 | 0.455 | 19.96 | 0.455 | 19.96 | 0.455 | 4.16 | 0.887 | 4.16 | 0.887 | 4.16 | 0.887 | 4.16 | 0.887 | | |
| | | 11.56 | 0.192 | | | 6.93 | 0.058 | 21.36 | 0.434 | 21.36 | 0.434 | 21.36 | 0.434 | 4.20 | 0.912 | 4.20 | 0.912 | 4.20 | 0.912 | 4.20 | 0.912 | | |
| | | 11.64 | 0.220 | | | 7.01 | 0.498 | 23.36 | 0.487 | 23.36 | 0.487 | 23.36 | 0.487 | 4.24 | 0.937 | 4.24 | 0.937 | 4.24 | 0.937 | 4.24 | 0.937 | | |
| | | 11.70 | 0.211 | | | 7.04 | 0.547 | 26.18 | 0.536 | 26.18 | 0.536 | 26.18 | 0.536 | 4.28 | 0.962 | 4.28 | 0.962 | 4.28 | 0.962 | 4.28 | 0.962 | | |
| | | 11.78 | 0.216 | | | 7.12 | 0.581 | 27.03 | 0.563 | 27.03 | 0.563 | 27.03 | 0.563 | 4.32 | 0.987 | 4.32 | 0.987 | 4.32 | 0.987 | 4.32 | 0.987 | | |
| | | 11.83 | 0.180 | | | 7.17 | 0.540 | 28.90 | 0.601 | 28.90 | 0.601 | 28.90 | 0.601 | 4.36 | 1.012 | 4.36 | 1.012 | 4.36 | 1.012 | 4.36 | 1.012 | | |
| | | 11.99 | 0.173 | | | 7.28 | 0.073 | 31.95 | 0.640 | 31.95 | 0.640 | 31.95 | 0.640 | 4.40 | 1.037 | 4.40 | 1.037 | 4.40 | 1.037 | 4.40 | 1.037 | | |
| | | 12.14 | 0.185 | | | 7.30 | 0.205 | 34.36 | 0.640 | 34.36 | 0.640 | 34.36 | 0.640 | 4.44 | 1.062 | 4.44 | 1.062 | 4.44 | 1.062 | 4.44 | 1.062 | | |
| | | 12.20 | 0.215 | | | 7.34 | 0.215 | 35.71 | 0.618 | 35.71 | 0.618 | 35.71 | 0.618 | 4.48 | 1.087 | 4.48 | 1.087 | 4.48 | 1.087 | 4.48 | 1.087 | | |
| | | 12.33 | 0.221 | | | 7.36 | 0.370 | 40.00 | 0.544 | 40.00 | 0.544 | 40.00 | 0.544 | 4.52 | 1.112 | 4.52 | 1.112 | 4.52 | 1.112 | 4.52 | 1.112 | | |
| | | 12.33 | 0.243 | | | 7.46 | 0.410 | | | | | | | 4.56 | 1.137 | 4.56 | 1.137 | 4.56 | 1.137 | 4.56 | 1.137 | | |
| | | 12.33 | 0.261 | | | 7.55 | 0.000 | | | | | | | 4.60 | 1.162 | 4.60 | 1.162 | 4.60 | 1.162 | 4.60 | 1.162 | | |
| | | 12.41 | 0.261 | | | 7.68 | 0.470 | | | | | | | 4.64 | 1.187 | 4.64 | 1.187 | 4.64 | 1.187 | 4.64 | 1.187 | | |
| | | 12.50 | 0.291 | | | 7.68 | 0.435 | | | | | | | 4.68 | 1.212 | 4.68 | 1.212 | 4.68 | 1.212 | 4.68 | 1.212 | | |

CURVE 14
T = 293.CURVE 15
T = 293.CURVE 16
T = 293.

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | | |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|--|--|
| CURVE 16 (CONT.) | | | | | | | | | | | |
| 6.65 | 0.676 | 13.30 | 0.377 | 3.11 | 0.568 | 19.96 | 0.651 | 4.28 | 0.398 | | |
| 6.70 | 0.660 | 13.64 | 0.420 | 3.20 | 0.567 | 20.75 | 0.642 | 4.43 | 0.404 | | |
| 6.73 | 0.630 | 13.95 | 0.433 | 3.36 | 0.574 | 21.74 | 0.638 | 4.54 | 0.413 | | |
| 6.78 | 0.543 | 14.06 | 0.484 | 3.42 | 0.566 | 23.70 | 0.603 | 4.62 | 0.413 | | |
| 6.83 | 0.246 | 14.35 | 0.524 | 3.51 | 0.577 | 25.00 | 0.613 | 4.65 | 0.421 | | |
| 6.86 | 0.223 | 14.66 | 0.533 | 3.81 | 0.576 | CURVE 18 | | | | | |
| 6.90 | 0.250 | 14.66 | 0.546 | 3.91 | 0.585 | T = 293. | | | | | |
| 6.93 | 0.364 | 15.90 | 0.590 | 4.12 | 0.573 | 2.50 | 0.264 | 4.94 | 0.432 | | |
| 6.99 | 0.591 | 17.06 | 0.621 | 4.33 | 0.592 | 2.59 | 0.266 | 4.97 | 0.437 | | |
| 7.03 | 0.677 | 18.12 | 0.621 | 4.72 | 0.592 | 2.60 | 0.270 | 5.00 | 0.441 | | |
| 7.12 | 0.700 | 18.73 | 0.606 | 4.85 | 0.587 | 2.67 | 0.270 | 5.01 | 0.450 | | |
| 7.16 | 0.693 | 19.38 | 0.579 | 5.10 | 0.587 | 2.70 | 0.279 | 5.13 | 0.450 | | |
| 7.19 | 0.669 | 20.12 | 0.545 | 5.19 | 0.600 | 2.89 | 0.279 | 5.22 | 0.467 | | |
| 7.24 | 0.479 | 20.53 | 0.545 | 5.59 | 0.600 | 2.91 | 0.286 | 5.34 | 0.469 | | |
| 7.28 | 0.359 | 21.23 | 0.561 | 5.75 | 0.600 | 2.96 | 0.286 | 5.37 | 0.473 | | |
| 7.30 | 0.518 | 22.37 | 0.606 | 5.93 | 0.612 | 2.98 | 0.300 | 5.44 | 0.473 | | |
| 7.34 | 0.532 | 23.58 | 0.647 | 6.62 | 0.618 | 3.06 | 0.302 | 5.46 | 0.481 | | |
| 7.36 | 0.616 | 24.75 | 0.681 | 7.13 | 0.622 | 3.08 | 0.309 | 5.55 | 0.481 | | |
| 7.51 | 0.666 | 25.45 | 0.695 | 7.35 | 0.633 | 3.16 | 0.312 | 5.61 | 0.484 | | |
| 7.57 | 0.675 | 26.04 | 0.675 | 7.50 | 0.632 | 3.19 | 0.318 | 5.64 | 0.489 | | |
| 7.68 | 0.660 | 26.67 | 0.679 | 7.69 | 0.629 | 3.23 | 0.325 | 5.76 | 0.489 | | |
| 7.79 | 0.665 | 26.95 | 0.688 | 7.84 | 0.637 | 3.35 | 0.331 | 5.76 | 0.497 | | |
| 7.89 | 0.644 | 26.95 | 0.729 | 8.14 | 0.635 | 3.41 | 0.331 | 5.83 | 0.491 | | |
| 8.08 | 0.593 | 28.25 | 0.751 | 8.67 | 0.640 | 3.47 | 0.337 | 5.93 | 0.501 | | |
| 8.32 | 0.526 | 29.33 | 0.757 | 8.93 | 0.629 | 3.49 | 0.344 | 6.24 | 0.504 | | |
| 8.45 | 0.505 | 31.85 | 0.757 | 9.64 | 0.651 | 3.54 | 0.344 | 6.34 | 0.515 | | |
| 8.78 | 0.402 | 33.56 | 0.745 | 9.95 | 0.640 | 3.56 | 0.351 | 6.52 | 0.517 | | |
| 9.07 | 0.291 | 35.09 | 0.717 | 10.22 | 0.630 | 3.65 | 0.351 | 6.76 | 0.523 | | |
| 9.31 | 0.232 | 36.36 | 0.693 | 10.56 | 0.629 | 3.71 | 0.357 | 6.86 | 0.528 | | |
| 9.57 | 0.184 | 38.31 | 0.597 | 10.95 | 0.609 | 3.84 | 0.370 | 7.17 | 0.528 | | |
| 9.90 | 0.160 | 40.00 | 0.590 | 11.52 | 0.563 | 3.89 | 0.369 | 7.41 | 0.540 | | |
| 10.35 | 0.141 | CURVE 17 | | | | | | | | | |
| 10.65 | 0.141 | T = 293. | | | | | | | | | |
| 11.27 | 0.151 | 2.50 | 0.554 | 15.13 | 0.657 | 3.99 | 0.381 | 7.69 | 0.545 | | |
| 11.67 | 0.163 | 2.59 | 0.561 | 15.67 | 0.654 | 4.05 | 0.381 | 8.05 | 0.545 | | |
| 11.96 | 0.171 | 2.66 | 0.556 | 16.08 | 0.661 | 4.28 | 0.386 | 8.34 | 0.542 | | |
| 12.25 | 0.199 | 2.69 | 0.550 | 17.36 | 0.661 | 4.41 | 0.386 | 8.47 | 0.532 | | |
| 12.50 | 0.230 | 2.73 | 0.559 | 18.02 | 0.673 | 4.07 | 0.386 | 8.73 | 0.517 | | |
| 12.77 | 0.270 | 2.88 | 0.563 | 18.55 | 0.662 | 4.19 | 0.390 | 8.82 | 0.501 | | |
| 12.99 | 0.303 | | | | | | | 9.05 | 0.479 | | |
| | | | | | | | | 9.16 | 0.453 | | |
| | | | | | | | | 9.27 | 0.363 | | |
| | | | | | | | | 9.42 | 0.306 | | |
| | | | | | | | | 9.52 | 0.270 | | |
| | | | | | | | | 9.70 | 0.155 | | |
| | | | | | | | | 10.01 | 0.433 | | |
| | | | | | | | | 10.88 | 0.492 | | |
| | | | | | | | | 12.00 | 0.550 | | |
| | | | | | | | | 12.11 | 0.586 | | |
| | | | | | | | | 12.76 | 0.622 | | |
| | | | | | | | | 13.35 | 0.650 | | |
| | | | | | | | | 14.33 | 0.662 | | |
| | | | | | | | | 14.43 | 0.674 | | |
| | | | | | | | | 14.47 | 0.635 | | |
| | | | | | | | | 14.51 | 0.612 | | |
| | | | | | | | | 14.60 | 0.603 | | |
| | | | | | | | | 14.66 | 0.634 | | |
| | | | | | | | | 14.77 | 0.610 | | |
| | | | | | | | | 14.93 | 0.672 | | |
| | | | | | | | | 14.93 | 0.676 | | |

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| CURVE 20 (CONT.) | | | | | | | | | | | |
| 7.24 | 0.693 | 3.18 | 0.792 | 14.79 | 0.612 | 6.91 | 0.576 | 10.09 | 0.317 | 15.22 | 0.664 |
| 7.39 | 0.899 | 3.31 | 0.799 | 14.90 | 0.629 | 9.19 | 0.495 | 10.52 | 0.269 | 15.72 | 0.664 |
| 7.59 | 0.899 | 3.42 | 0.789 | 15.02 | 0.622 | 9.67 | 0.409 | 10.84 | 0.304 | CURVE 25 | |
| 7.79 | 0.890 | 3.54 | 0.788 | 15.17 | 0.629 | 10.03 | 0.371 | 11.25 | 0.523 | T = 293. | |
| 8.21 | 0.828 | 3.94 | 0.770 | CURVE 22 | | 10.33 | 0.317 | 11.43 | 0.594 | | |
| 8.31 | 0.743 | 4.20 | 0.761 | T = 293. | | 10.54 | 0.267 | 11.64 | 0.636 | | |
| 9.22 | 0.694 | 4.45 | 0.761 | 1.98 | 0.835 | 10.99 | 0.260 | 11.86 | 0.684 | | |
| 9.85 | 0.586 | 4.69 | 0.768 | 2.13 | 0.825 | 11.48 | 0.238 | 12.19 | 0.721 | | |
| 10.19 | 0.548 | 4.76 | 0.780 | 2.13 | 0.825 | 11.85 | 0.237 | 12.53 | 0.756 | | |
| 10.47 | 0.523 | 5.01 | 0.786 | 2.13 | 0.809 | 12.06 | 0.246 | 13.06 | 0.789 | | |
| 10.73 | 0.507 | 5.62 | 0.815 | 2.29 | 0.804 | 12.43 | 0.257 | 13.61 | 0.822 | | |
| 11.04 | 0.507 | 6.05 | 0.838 | 2.49 | 0.767 | 12.70 | 0.290 | 14.42 | 0.854 | | |
| 11.44 | 0.522 | 6.22 | 0.842 | 2.78 | 0.727 | 13.05 | 0.375 | CURVE 24 | | | |
| 11.94 | 0.547 | 6.39 | 0.860 | 2.78 | 0.711 | 13.85 | 0.453 | T = 293. | | | |
| 12.21 | 0.593 | 6.72 | 0.870 | 3.00 | 0.686 | 14.14 | 0.499 | | | | |
| 12.51 | 0.628 | 7.14 | 0.881 | 3.14 | 0.696 | 14.51 | 0.544 | | | | |
| 12.81 | 0.680 | 7.36 | 0.888 | 3.27 | 0.702 | 14.90 | 0.583 | | | | |
| 13.28 | 0.724 | 7.58 | 0.888 | 3.57 | 0.702 | 14.90 | 0.572 | | | | |
| 14.01 | 0.790 | 7.75 | 0.874 | 3.95 | 0.709 | 15.06 | 0.584 | | | | |
| 14.26 | 0.816 | 7.84 | 0.874 | 4.23 | 0.723 | CURVE 23 | | | | | |
| 14.69 | 0.823 | 8.16 | 0.815 | 4.37 | 0.716 | T = 293. | | | | | |
| 14.85 | 0.847 | 8.29 | 0.774 | 4.60 | 0.721 | | | | | | |
| 14.93 | 0.832 | 8.56 | 0.743 | 4.69 | 0.739 | | | | | | |
| 15.04 | 0.849 | 8.56 | 0.26 | 5.12 | 0.760 | | | | | | |
| 15.38 | 0.854 | 8.65 | 0.716 | 5.66 | 0.793 | | | | | | |
| 15.44 | 0.848 | 8.83 | 0.669 | 6.34 | 0.820 | | | | | | |
| 15.55 | 0.843 | 8.93 | 0.635 | 6.71 | 0.859 | | | | | | |
| CURVE 21 | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | |
| 1.92 | 0.846 | 9.44 | 0.539 | 7.13 | 0.869 | | | | | | |
| 3.11 | 0.852 | 9.74 | 0.501 | 7.21 | 0.864 | | | | | | |
| 2.19 | 0.861 | 10.13 | 0.469 | 7.32 | 0.877 | | | | | | |
| 2.25 | 0.881 | 10.79 | 0.422 | 7.69 | 0.875 | | | | | | |
| 2.46 | 0.861 | 11.06 | 0.413 | 7.99 | 0.835 | | | | | | |
| 2.54 | 0.870 | 11.28 | 0.413 | 7.99 | 0.821 | | | | | | |
| 2.69 | 0.864 | 11.69 | 0.396 | 8.15 | 0.801 | | | | | | |
| 2.73 | 0.845 | 12.27 | 0.405 | 8.13 | 0.762 | | | | | | |
| 2.94 | 0.810 | 12.63 | 0.424 | 8.29 | 0.760 | | | | | | |
| | | 13.08 | 0.462 | 8.29 | 0.736 | | | | | | |
| | | 13.64 | 0.517 | 8.60 | 0.701 | | | | | | |
| | | 14.27 | 0.575 | 8.76 | 0.630 | | | | | | |
| | | | | 8.81 | 0.664 | | | | | | |
| | | | | 8.81 | 0.664 | | | | | | |
| | | | | 9.13 | 0.501 | | | | | | |
| | | | | 9.35 | 0.423 | | | | | | |
| | | | | 9.57 | 0.379 | | | | | | |
| | | | | 9.73 | 0.498 | | | | | | |
| | | | | 9.73 | 0.498 | | | | | | |
| | | | | 14.16 | 0.636 | | | | | | |
| | | | | 14.45 | 0.650 | | | | | | |
| | | | | 14.77 | 0.659 | | | | | | |

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 25 (CONT.) | | | CURVE 25 (CONT.) | | | CURVE 26 (CONT.) | | | CURVE 26 (CONT.) | | | CURVE 27 (CONT.) | | | CURVE 27 (CONT.) | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 5.41 | 0.919 | 7.47 | 0.833 | 3.33 | 0.737 | 7.93 | 0.891 | 2.99 | 0.839 | 4.31 | 0.769 | 2.99 | 0.839 | 4.31 | 0.769 | 2.99 | 0.839 |
| 5.80 | 0.934 | 7.58 | 0.851 | 3.44 | 0.726 | 8.10 | 0.863 | 3.05 | 0.876 | 4.34 | 0.765 | 3.05 | 0.876 | 4.34 | 0.765 | 3.05 | 0.876 |
| 5.89 | 0.920 | 7.64 | 0.866 | 3.49 | 0.602 | 8.16 | 0.838 | 3.12 | 0.920 | 4.62 | 0.809 | 3.12 | 0.920 | 4.62 | 0.809 | 3.12 | 0.920 |
| 5.92 | 0.948 | 7.78 | 0.834 | 3.51 | 0.298 | 8.23 | 0.828 | 3.16 | 0.927 | 4.72 | 0.826 | 3.16 | 0.927 | 4.72 | 0.826 | 3.16 | 0.927 |
| 5.95 | 0.918 | 7.90 | 0.819 | 3.56 | 0.251 | 8.37 | 0.754 | 3.19 | 0.951 | 4.75 | 0.841 | 3.19 | 0.951 | 4.75 | 0.841 | 3.19 | 0.951 |
| 6.03 | 0.936 | 8.02 | 0.759 | 3.61 | 0.401 | 8.50 | 0.686 | 3.20 | 0.976 | 4.81 | 0.841 | 3.20 | 0.976 | 4.81 | 0.841 | 3.20 | 0.976 |
| 6.06 | 0.914 | 8.21 | 0.560 | 3.63 | 0.355 | 8.71 | 0.628 | 3.22 | 0.954 | 4.96 | 0.861 | 3.22 | 0.954 | 4.96 | 0.861 | 3.22 | 0.954 |
| 6.12 | 0.904 | 8.48 | 0.249 | 3.68 | 0.703 | 9.00 | 0.583 | 3.25 | 0.963 | 5.03 | 0.871 | 3.25 | 0.963 | 5.03 | 0.871 | 3.25 | 0.963 |
| 6.15 | 0.927 | 8.59 | 0.190 | 3.71 | 0.757 | 9.15 | 0.552 | 3.29 | 0.969 | 5.14 | 0.873 | 3.29 | 0.969 | 5.14 | 0.873 | 3.29 | 0.969 |
| 6.19 | 0.890 | 8.72 | 0.164 | 3.76 | 0.794 | 9.53 | 0.512 | 3.31 | 0.961 | 5.16 | 0.883 | 3.31 | 0.961 | 5.16 | 0.883 | 3.31 | 0.961 |
| 6.21 | 0.921 | 8.88 | 0.151 | 3.82 | 0.789 | 9.81 | 0.488 | 3.32 | 0.938 | 5.27 | 0.888 | 3.32 | 0.938 | 5.27 | 0.888 | 3.32 | 0.938 |
| 6.24 | 0.901 | 9.11 | 0.129 | 3.97 | 0.805 | 9.87 | 0.474 | 3.35 | 0.896 | 5.41 | 0.907 | 3.35 | 0.896 | 5.41 | 0.907 | 3.35 | 0.896 |
| 6.30 | 0.919 | 9.50 | 0.108 | 4.08 | 0.833 | 10.09 | 0.468 | 3.38 | 0.704 | 5.73 | 0.924 | 3.38 | 0.704 | 5.73 | 0.924 | 3.38 | 0.704 |
| 6.42 | 0.930 | 9.89 | 0.091 | 4.34 | 0.855 | 10.33 | 0.453 | 3.39 | 0.201 | 5.80 | 0.935 | 3.39 | 0.201 | 5.80 | 0.935 | 3.39 | 0.201 |
| 6.46 | 0.939 | 10.10 | 0.091 | 4.43 | 0.850 | 10.71 | 0.438 | 3.40 | 0.153 | 5.90 | 0.935 | 3.40 | 0.153 | 5.90 | 0.935 | 3.40 | 0.153 |
| 6.48 | 0.932 | 10.52 | 0.076 | 4.46 | 0.861 | 11.15 | 0.430 | 3.48 | 0.148 | 5.97 | 0.936 | 3.48 | 0.148 | 5.97 | 0.936 | 3.48 | 0.148 |
| 6.50 | 0.949 | 11.33 | 0.076 | 4.87 | 0.889 | 11.64 | 0.458 | 3.43 | 0.101 | 6.03 | 0.931 | 3.43 | 0.101 | 6.03 | 0.931 | 3.43 | 0.101 |
| 6.53 | 0.921 | 11.95 | 0.084 | 5.34 | 0.917 | 12.18 | 0.472 | 3.45 | 0.152 | 6.18 | 0.931 | 3.45 | 0.152 | 6.18 | 0.931 | 3.45 | 0.152 |
| 6.57 | 0.948 | 12.34 | 0.092 | 6.01 | 0.926 | 12.48 | 0.499 | 3.47 | 0.299 | 6.45 | 0.948 | 3.47 | 0.299 | 6.45 | 0.948 | 3.47 | 0.299 |
| 6.61 | 0.923 | 12.74 | 0.129 | 6.35 | 0.926 | 13.01 | 0.558 | 3.48 | 0.319 | 6.60 | 0.948 | 3.48 | 0.319 | 6.60 | 0.948 | 3.48 | 0.319 |
| 6.65 | 0.941 | 12.89 | 0.129 | 6.69 | 0.930 | 13.36 | 0.590 | 3.49 | 0.256 | 6.69 | 0.932 | 3.49 | 0.256 | 6.69 | 0.932 | 3.49 | 0.256 |
| 6.69 | 0.925 | 13.35 | 0.157 | 6.82 | 0.919 | 13.48 | 0.600 | 3.51 | 0.221 | 6.73 | 0.902 | 3.51 | 0.221 | 6.73 | 0.902 | 3.51 | 0.221 |
| 6.72 | 0.940 | 13.59 | 0.162 | 6.89 | 0.849 | 13.63 | 0.600 | 3.54 | 0.897 | 6.77 | 0.813 | 3.54 | 0.897 | 6.77 | 0.813 | 3.54 | 0.897 |
| 6.74 | 0.901 | 13.74 | 0.173 | 6.92 | 0.671 | 13.77 | 0.620 | 3.55 | 1.000 | 6.84 | 0.383 | 3.55 | 1.000 | 6.84 | 0.383 | 3.55 | 1.000 |
| 6.76 | 0.922 | 13.99 | 0.192 | 6.96 | 0.634 | 13.88 | 0.621 | 3.58 | 1.000 | 6.86 | 0.370 | 3.58 | 1.000 | 6.86 | 0.370 | 3.58 | 1.000 |
| 6.81 | 0.904 | 14.16 | 0.228 | 6.99 | 0.656 | 14.24 | 0.684 | 3.58 | 0.551 | 6.89 | 0.389 | 3.58 | 0.551 | 6.89 | 0.389 | 3.58 | 0.551 |
| 6.85 | 0.845 | 14.42 | 0.248 | 7.03 | 0.780 | 14.41 | 0.697 | 3.60 | 0.580 | 6.92 | 0.503 | 3.60 | 0.580 | 6.92 | 0.503 | 3.60 | 0.580 |
| 6.89 | 0.740 | 14.62 | 0.261 | 7.11 | 0.897 | 14.71 | 0.721 | 3.63 | 0.591 | 7.02 | 0.876 | 3.63 | 0.591 | 7.02 | 0.876 | 3.63 | 0.591 |
| 6.92 | 0.498 | 14.84 | 0.262 | 7.20 | 0.926 | 14.83 | 0.736 | 3.68 | 0.584 | 7.06 | 0.905 | 3.68 | 0.584 | 7.06 | 0.905 | 3.68 | 0.584 |
| 6.94 | 0.416 | 15.00 | 0.268 | 7.27 | 0.919 | 15.00 | 0.754 | 3.71 | 0.600 | 7.09 | 0.916 | 3.71 | 0.600 | 7.09 | 0.916 | 3.71 | 0.600 |
| 6.99 | 0.448 | | | 7.33 | 0.803 | | | 3.76 | 0.600 | 7.13 | 0.926 | 3.76 | 0.600 | 7.13 | 0.926 | 3.76 | 0.600 |
| 7.09 | 0.600 | | | 7.37 | 0.740 | | | 3.87 | 0.646 | 7.16 | 0.918 | 3.87 | 0.646 | 7.16 | 0.918 | 3.87 | 0.646 |
| 7.11 | 0.855 | | | 7.39 | 0.804 | | | 3.97 | 0.673 | 7.19 | 0.890 | 3.97 | 0.673 | 7.19 | 0.890 | 3.97 | 0.673 |
| 7.13 | 0.883 | | | 7.43 | 0.827 | | | 4.00 | 0.695 | 7.28 | 0.876 | 4.00 | 0.695 | 7.28 | 0.876 | 4.00 | 0.695 |
| 7.16 | 0.676 | 2.50 | 0.642 | 7.46 | 0.874 | | | 4.04 | 0.695 | 7.32 | 0.876 | 4.04 | 0.695 | 7.32 | 0.876 | 4.04 | 0.695 |
| 7.21 | 0.900 | 2.53 | 0.703 | 7.51 | 0.885 | | | 4.06 | 0.711 | 7.35 | 0.883 | 4.06 | 0.711 | 7.35 | 0.883 | 4.06 | 0.711 |
| 7.26 | 0.890 | 2.54 | 0.664 | 7.59 | 0.805 | | | 4.10 | 0.696 | 7.37 | 0.802 | 4.10 | 0.696 | 7.37 | 0.802 | 4.10 | 0.696 |
| 7.36 | 0.598 | 2.86 | 0.698 | 7.63 | 0.900 | | | 4.21 | 0.717 | 7.41 | 0.833 | 4.21 | 0.717 | 7.41 | 0.833 | 4.21 | 0.717 |
| 7.39 | 0.731 | 3.25 | 0.729 | 7.67 | 0.901 | | | 4.26 | 0.806 | 7.47 | 0.884 | 4.26 | 0.806 | 7.47 | 0.884 | 4.26 | 0.806 |
| 7.43 | 0.747 | 3.31 | 0.724 | 7.76 | 0.891 | | | | 0.821 | 7.70 | 0.870 | | 0.821 | 7.70 | 0.870 | | 0.821 |

CURVE 27
T = 293.

CURVE 26
T = 293.

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| CURVE 27 (CONT.) | | | | | | | | | | | | | |
| 7.78 | 0.874 | 16.84 | 0.124 | 8.42 | 0.581 | 12.22 | 0.236 | 11.98 | 0.190 | 6.34 | 0.541 | 11.98 | 0.190 |
| 7.84 | 0.874 | 17.79 | 0.297 | 8.76 | 0.581 | 12.44 | 0.273 | 12.17 | 0.190 | 6.69 | 0.542 | 12.17 | 0.190 |
| 7.99 | 0.362 | 18.69 | 0.502 | 9.02 | 0.559 | 12.61 | 0.319 | 12.45 | 0.220 | 6.80 | 0.555 | 12.45 | 0.220 |
| 8.19 | 0.822 | 19.01 | 0.550 | 9.38 | 0.516 | 12.80 | 0.380 | 12.69 | 0.273 | 7.03 | 0.555 | 12.69 | 0.273 |
| 8.40 | 0.753 | 19.34 | 0.564 | 9.78 | 0.474 | 13.07 | 0.443 | 13.05 | 0.348 | 7.42 | 0.583 | 13.05 | 0.348 |
| 8.55 | 0.686 | 19.57 | 0.536 | 10.20 | 0.433 | 13.35 | 0.512 | 13.35 | 0.421 | 7.70 | 0.583 | 13.35 | 0.421 |
| 8.79 | 0.538 | 19.80 | 0.358 | 10.70 | 0.397 | 13.59 | 0.554 | 13.76 | 0.518 | 7.82 | 0.562 | 13.76 | 0.518 |
| 8.84 | 0.520 | 20.08 | 0.351 | 11.16 | 0.367 | 13.83 | 0.594 | 14.01 | 0.558 | 7.97 | 0.533 | 14.01 | 0.558 |
| 9.09 | 0.340 | 20.62 | 0.152 | 11.53 | 0.367 | 14.08 | 0.624 | 14.37 | 0.591 | 8.12 | 0.476 | 14.37 | 0.591 |
| 9.23 | 0.234 | 21.14 | 0.286 | 11.78 | 0.388 | 14.41 | 0.661 | CURVE 31 | | | | | |
| 9.29 | 0.188 | 21.55 | 0.230 | 12.11 | 0.426 | 14.66 | 0.682 | T = 293. | | | | | |
| 9.43 | 0.164 | 21.98 | 0.141 | 12.42 | 0.473 | 14.99 | 0.705 | 2.50 | 0.592 | 8.70 | 0.272 | 2.50 | 0.592 |
| 9.63 | 0.157 | 22.57 | 0.199 | 12.66 | 0.521 | 15.41 | 0.720 | 2.62 | 0.638 | 8.94 | 0.188 | 2.62 | 0.638 |
| 9.80 | 0.135 | 24.27 | 0.445 | 12.99 | 0.580 | 15.80 | 0.720 | 2.68 | 0.652 | 9.27 | 0.111 | 2.68 | 0.652 |
| 9.91 | 0.135 | 24.63 | 0.316 | 13.40 | 0.654 | 16.10 | 0.706 | 2.72 | 0.670 | 9.66 | 0.072 | 2.72 | 0.670 |
| 10.24 | 0.098 | 25.13 | 0.381 | 13.89 | 0.705 | 16.37 | 0.665 | 2.79 | 0.700 | 10.24 | 0.033 | 2.79 | 0.700 |
| 10.56 | 0.084 | 25.58 | 0.573 | 14.25 | 0.735 | 16.56 | 0.630 | 2.85 | 0.680 | 11.20 | 0.018 | 2.85 | 0.680 |
| 10.70 | 0.082 | 25.97 | 0.619 | 14.68 | 0.765 | 16.84 | 0.607 | 2.92 | 0.700 | 12.42 | 0.018 | 2.92 | 0.700 |
| 11.03 | 0.101 | 27.03 | 0.305 | 14.95 | 0.776 | 17.09 | 0.619 | 3.11 | 0.609 | 12.76 | 0.044 | 3.11 | 0.609 |
| 11.15 | 0.095 | 28.17 | 0.727 | 15.43 | 0.791 | 17.36 | 0.637 | 3.24 | 0.578 | 13.30 | 0.114 | 3.24 | 0.578 |
| 11.24 | 0.099 | 28.65 | 0.634 | CURVE 29 | | | | CURVE 30 | | | | | |
| 11.35 | 0.091 | 28.99 | 0.755 | T = 293. | | | | T = 293. | | | | | |
| 11.40 | 0.116 | 29.76 | 0.834 | 7.75 | 0.680 | 7.75 | 0.683 | 3.40 | 0.556 | 14.45 | 0.286 | 3.40 | 0.556 |
| 11.82 | 0.133 | 30.58 | 0.860 | 7.95 | 0.671 | 7.95 | 0.667 | 3.57 | 0.556 | 15.75 | 0.321 | 3.57 | 0.556 |
| 12.38 | 0.165 | 32.68 | 0.892 | 8.08 | 0.662 | 8.08 | 0.650 | 3.70 | 0.579 | 16.16 | 0.310 | 3.70 | 0.579 |
| 12.82 | 0.165 | 34.13 | 0.806 | 8.22 | 0.635 | 8.22 | 0.620 | 3.84 | 0.607 | 16.58 | 0.301 | 3.84 | 0.607 |
| 13.18 | 0.189 | 34.72 | 0.860 | 8.45 | 0.609 | 8.45 | 0.585 | 3.98 | 0.633 | 16.78 | 0.333 | 3.98 | 0.633 |
| 13.62 | 0.202 | 35.59 | 0.881 | 8.85 | 0.609 | 8.85 | 0.585 | 4.19 | 0.677 | 17.12 | 0.346 | 4.19 | 0.677 |
| 14.37 | 0.292 | 36.50 | 0.881 | 9.10 | 0.576 | 9.10 | 0.532 | 4.32 | 0.677 | 17.06 | 0.346 | 4.32 | 0.677 |
| 14.56 | 0.197 | 36.90 | 0.906 | 9.44 | 0.537 | 9.44 | 0.498 | 4.49 | 0.701 | 18.28 | 0.311 | 4.49 | 0.701 |
| 14.73 | 0.165 | 39.06 | 0.927 | 9.79 | 0.487 | 9.79 | 0.475 | 4.65 | 0.702 | 19.34 | 0.263 | 4.65 | 0.702 |
| 14.95 | 0.165 | 39.06 | 1.000 | 10.11 | 0.440 | 9.23 | 0.457 | 4.91 | 0.664 | 20.49 | 0.241 | 4.91 | 0.664 |
| 15.15 | 0.168 | 10.37 | 0.409 | 10.37 | 0.409 | 9.51 | 0.447 | 5.00 | 0.650 | 21.88 | 0.285 | 5.00 | 0.650 |
| 15.65 | 0.152 | 10.63 | 0.371 | 9.77 | 0.431 | 9.77 | 0.431 | 5.13 | 0.631 | 23.70 | 0.338 | 5.13 | 0.631 |
| 16.00 | 0.134 | 10.98 | 0.327 | 10.07 | 0.386 | 10.07 | 0.386 | 5.26 | 0.609 | 25.84 | 0.374 | 5.26 | 0.609 |
| 16.00 | 0.152 | 11.39 | 0.277 | 10.40 | 0.338 | 10.40 | 0.338 | 5.44 | 0.581 | 27.40 | 0.399 | 5.44 | 0.581 |
| 16.00 | 0.152 | 11.61 | 0.242 | 10.82 | 0.288 | 10.82 | 0.288 | 5.72 | 0.554 | 29.85 | 0.425 | 5.72 | 0.554 |
| 16.45 | 0.131 | 11.85 | 0.224 | 11.25 | 0.246 | 11.25 | 0.246 | 5.85 | 0.548 | | | 5.85 | 0.548 |
| 16.69 | 0.134 | 12.09 | 0.224 | 11.64 | 0.214 | 11.64 | 0.214 | 5.96 | 0.535 | | | 5.96 | 0.535 |

TABLE 14-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON NITRIDE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T |
|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| CURVE 32 | | | | | | | |
| T = 293. | | | | | | | |
| 2.50 | 0.453 | 10.18 | 0.030 | 4.61 | 0.550 | 10.18 | 0.030 |
| 2.63 | 0.479 | 11.22 | 0.008 | 4.79 | 0.540 | 11.22 | 0.008 |
| 2.71 | 0.507 | 12.35 | 0.009 | 4.96 | 0.509 | 12.35 | 0.009 |
| 2.79 | 0.533 | 12.90 | 0.035 | 5.13 | 0.506 | 12.90 | 0.035 |
| 2.86 | 0.533 | 13.32 | 0.110 | 5.29 | 0.480 | 13.32 | 0.110 |
| 2.91 | 0.514 | 13.91 | 0.194 | 5.53 | 0.459 | 13.91 | 0.194 |
| 2.95 | 0.489 | 14.62 | 0.266 | 5.81 | 0.436 | 14.62 | 0.266 |
| 3.04 | 0.450 | 14.99 | 0.279 | 6.31 | 0.435 | 14.99 | 0.279 |
| 3.17 | 0.442 | 15.62 | 0.297 | 6.63 | 0.446 | 15.62 | 0.297 |
| 3.33 | 0.429 | 16.05 | 0.309 | 6.97 | 0.463 | 16.05 | 0.309 |
| 3.61 | 0.429 | 16.67 | 0.296 | 7.28 | 0.489 | 16.67 | 0.296 |
| 3.65 | 0.451 | 17.36 | 0.333 | 7.50 | 0.501 | 17.36 | 0.333 |
| 3.77 | 0.484 | 18.42 | 0.321 | 7.65 | 0.502 | 18.42 | 0.321 |
| 3.91 | 0.509 | 18.55 | 0.309 | 7.89 | 0.480 | 18.55 | 0.309 |
| 4.03 | 0.527 | 20.08 | 0.230 | 8.03 | 0.454 | 20.08 | 0.230 |
| 4.20 | 0.553 | 20.70 | 0.223 | 8.25 | 0.372 | 20.70 | 0.223 |
| 4.54 | 0.573 | 21.83 | 0.258 | 8.50 | 0.285 | 21.83 | 0.258 |
| 4.69 | 0.572 | 23.98 | 0.323 | 8.68 | 0.230 | 23.98 | 0.323 |
| 4.81 | 0.554 | 25.84 | 0.369 | 9.04 | 0.130 | 25.84 | 0.369 |
| 5.00 | 0.531 | 27.62 | 0.399 | 9.31 | 0.086 | 27.62 | 0.399 |
| 5.15 | 0.509 | 32.79 | 0.417 | 9.68 | 0.059 | 32.79 | 0.417 |
| 5.33 | 0.488 | CURVE 33 | | | | | |
| 5.50 | 0.476 | T = 293. | | | | | |
| 5.62 | 0.467 | 2.50 | 0.453 | 13.32 | 0.110 | 12.90 | 0.035 |
| 5.71 | 0.448 | 2.58 | 0.463 | 13.91 | 0.194 | 13.32 | 0.110 |
| 6.61 | 0.463 | 2.66 | 0.488 | 14.62 | 0.266 | 13.91 | 0.194 |
| 6.97 | 0.489 | 2.77 | 0.507 | 15.95 | 0.296 | 14.62 | 0.266 |
| 7.50 | 0.501 | 2.86 | 0.507 | 16.58 | 0.287 | 15.95 | 0.296 |
| 7.44 | 0.504 | 2.93 | 0.480 | 17.33 | 0.324 | 16.58 | 0.287 |
| 7.76 | 0.503 | 3.00 | 0.452 | 18.55 | 0.309 | 17.33 | 0.324 |
| 7.97 | 0.478 | 3.16 | 0.438 | 20.70 | 0.214 | 18.55 | 0.309 |
| 8.12 | 0.435 | 3.32 | 0.427 | 23.20 | 0.293 | 20.70 | 0.214 |
| 8.25 | 0.372 | 3.49 | 0.422 | 25.91 | 0.363 | 23.20 | 0.293 |
| 8.50 | 0.285 | 3.64 | 0.438 | 29.05 | 0.363 | 25.91 | 0.363 |
| 8.68 | 0.230 | 3.77 | 0.453 | | | | |
| 9.04 | 0.138 | 3.87 | 0.481 | | | | |
| 9.31 | 0.086 | 4.04 | 0.518 | | | | |
| 9.68 | 0.059 | 4.45 | 0.558 | | | | |

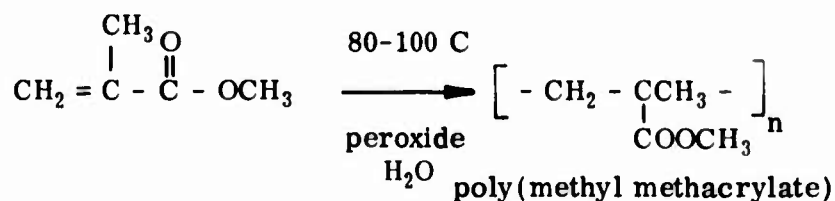
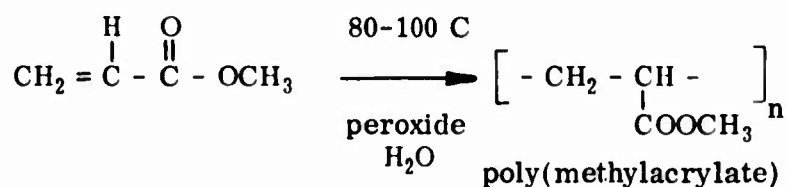
4.15. Acrylic Resins

The four major categories of acrylic resins include polymethacrylate, polyacrylate, poly(methyl methacrylate), and copolymer of acrylonitrile. The list of esters range from methyl to lauryl, C₁-C₁₂. Because of the many combinations possible, there are at least 40 varieties of acrylic resins commercially available. Lucite is a trade name of DuPont for poly(methyl methacrylate) which will be described in the next subsection. Other trade names for the various acrylic resins include Acryloid, Acrysol, Acryrin, Hycar PA, Acrilan, Creslan, Dynel, Orlon, Plexiglass, Vernonite, etc. These materials are manufactured in a wide range of colors and are in demand where aesthetic considerations predominate. They possess low specific gravity, low water absorption, good weather ability, and tensile strengths but only moderate heat resistance and low hardness. They soften from 250 to 400 K and are more easily scratched than glass.

According to the Reference [A00025], the softening points of acrylics are as follows:

| <u>Acrylics</u> | <u>Softening Point (K)</u> |
|----------------------------------|----------------------------|
| Polymethylacrylate (PMA) | 277 |
| Polyethylacrylate (PEA) | 248 |
| Polymethylmethacrylate (PMMA) | 397 |
| Polyethylmethacrylate (PEMA) | 339 |
| Poly n-butyl methacrylate (PBMA) | 303 |
| Polyacrylonitrile | 511 |

The polymerization of acrylate and methacrylate esters is carried out in water suspension with peroxide catalyst. The resulting polymer is washed, dried, and blended with plasticizers and colorants before pelletizing for use as molding powders.



Acrylic resins are soluble in aromatic and most chlorinated hydrocarbons (toluene, ethylene dichloride, chloroform), esters (ethyl acetate), ketones, tetrahydrofuran; 80/20 toluene/methanol gives low-viscosity solutions. Polymers of butyl and higher esters are

soluble in aliphatic hydrocarbons (e.g., white spirit, also in molten waxes). Cross-linked polymers are insoluble but swell in chlorinated hydrocarbons. Acrylic resins can also be swollen by alcohols, phenols, ether, and carbon tetrachloride. They are decomposable by conc. oxidizing acids (HNO_3 , H_2SO_4 , H_2CrO_4), alcoholic alkalis.

Acrylic resins have a density of about $1.02\text{-}1.22\text{ g cm}^{-3}$. Their refractive index is about $1.47\text{-}1.49$. The ultraviolet cut off is below 2800 \AA , it transmits about 85% in the visible region, and the infrared cut off is about 23000 \AA ($2.3\text{ }\mu\text{m}$).

a. Normal Spectral Emittance (Wavelength Dependence)

There are four sets of experimental data available for the wavelength dependence of the normal spectral emittance of acrylic resins as listed in Table 15-3 and shown in Figure 15-2. Specimen characterization and measurement information for the data are given in Table 15-2. All the data are for the paint coatings with green, blue/black, or white color. In the wavelength region above $\lambda = 6\text{ }\mu\text{m}$, there are small differences among the values of emittance for the different paints. In the shorter wavelength region the white paint has lowest emittance value. Since the data are limited, as a consequence, only provisional values were reported here. The provisional values listed in Table 15-1 and shown in Figure 15-1 are for the "white acrylic paint" on stainless steel substrate. The estimated uncertainty is within $\pm 30\%$.

TABLE 15-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ |
|-----------|------------|-----------|------------|
| 0.32 | 0.953 | 11.00 | 0.934 |
| 0.36 | 0.935 | 11.50 | 0.944 |
| 0.37 | 0.799 | 12.00 | 0.952 |
| 0.40 | 0.503 | 12.50 | 0.958 |
| 0.45 | 0.372 | 13.00 | 0.962 |
| 0.50 | 0.264 | 13.50 | 0.956 |
| 0.65 | 0.275 | 14.00 | 0.944 |
| 0.80 | 0.320 | 14.50 | 0.928 |
| 1.00 | 0.465 | 15.00 | 0.900 |
| 1.50 | 0.555 | | |
| 2.00 | 0.643 | | |
| 2.50 | 0.795 | | |
| 3.00 | 0.880 | | |
| 3.20 | 0.795 | | |
| 3.50 | 0.930 | | |
| 3.60 | 0.943 | | |
| 3.70 | 0.940 | | |
| 3.80 | 0.880 | | |
| 4.00 | 0.795 | | |
| 4.40 | 0.686 | | |
| 4.80 | 0.665 | | |
| 5.00 | 0.665 | | |
| 5.50 | 0.688 | | |
| 5.70 | 0.760 | | |
| 5.80 | 0.914 | | |
| 5.90 | 0.926 | | |
| 6.00 | 0.862 | | |
| 6.50 | 0.808 | | |
| 6.75 | 0.765 | | |
| 6.80 | 0.876 | | |
| 7.00 | 0.890 | | |
| 7.50 | 0.921 | | |
| 8.50 | 0.942 | | |
| 8.50 | 0.923 | | |
| 9.00 | 0.930 | | |
| 9.50 | 0.925 | | |
| 9.80 | 0.884 | | |
| 10.00 | 0.880 | | |
| 10.60 | 0.925 | | |

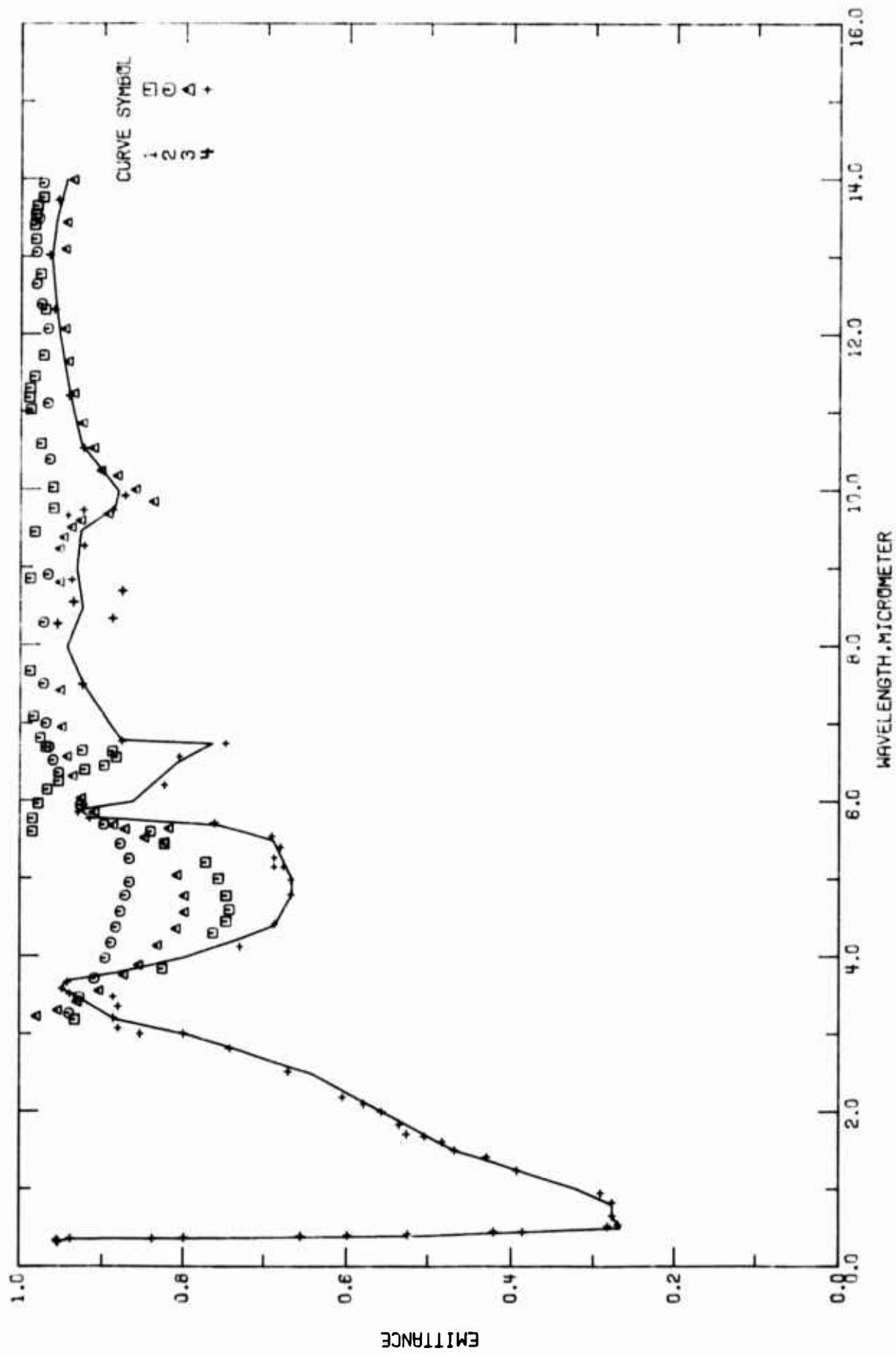


FIGURE 15-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE).

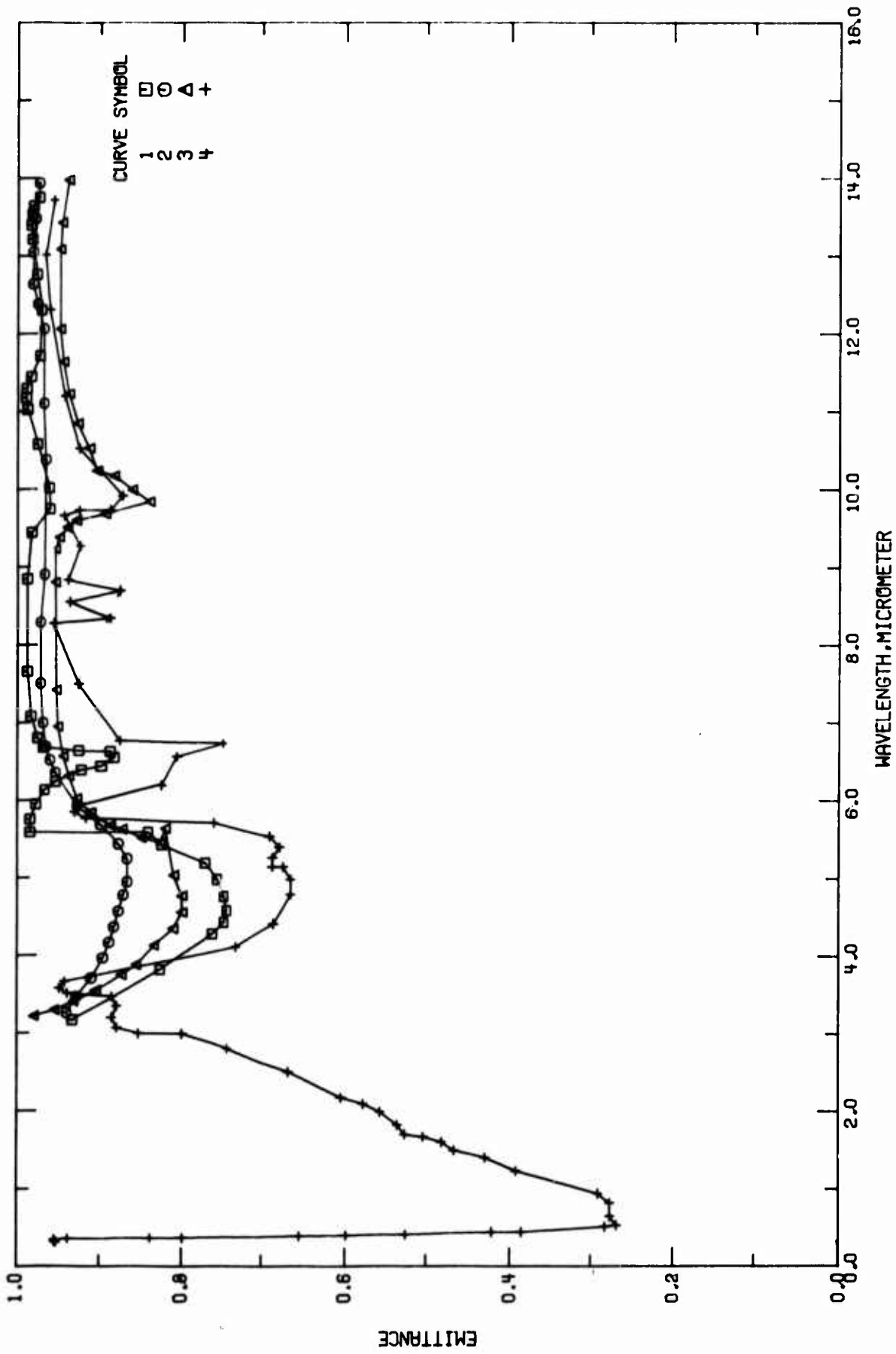


FIGURE 15-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE).

TABLE 15-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN COATING (Wavelength Dependence)

| Cur. Ref. No. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|-------------------|--|------|---------------------------------|----------------------|---|---|
| 1 T63130 | Faulkner, D., Horvath, R., Ulrich, J. P., and Work, E. | 1971 | 3.3-14 | 293 | MIL-L-19538B Paint (Field Green ANA-627) | Aluminum substrate, MIL-C-5541 surface preparation, MIL-C-8514 wash primer, MIL-P-7962 primer; Field Infrared Spectro-Radiometer was used; data were extracted from the figure; $\theta' \sim 9^\circ$. |
| 2 T63130 | Faulkner, D., et al. | 1971 | 3.3-14 | 293 | MIL-L-19538B Blue/Black (15042) Glossy Acrylic | Similar to the above specimen. |
| 3 T63130 | Faulkner, D., et al. | 1971 | 3.3-14 | 293 | O. D. (X34087) Lusterless Acrylic | Similar to the above specimen. |
| 4 T52784 | Shizkle, F. J. | 1961 | 0.3-40 | ~300 | Flat White Acrylic Paint | 7/16 in. disc stainless steel No. 301 substrate; the paint was obtained from Sherwin Williams; one coat over one coat pre-treatment wash coating; formula No. E90CC22, MIL-C-153284; $\theta' \sim 0^\circ$. |

TABLE 15-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| CURVE 1 T = 293. | | CURVE 2 T = 293. | | CURVE 3 (CONT.) | | CURVE 4 T = 300. | | CURVE 4 (CONT.) | | CURVE 4 (CONT.) | |
|---------------------|------------|---------------------|------------|-----------------|------------|---------------------|------------|-----------------|------------|-----------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 3.19 | 0.931 | 3.27 | 0.938 | 3.42 | 0.929 | 0.316 | 0.951 | 4.797 | 0.666 | 17.219 | 0.880 |
| 3.84 | 0.825 | 3.48 | 0.926 | 3.56 | 0.903 | 0.329 | 0.953 | 4.989 | 0.666 | 17.906 | 0.671 |
| 4.30 | 0.764 | 3.72 | 0.908 | 3.76 | 0.873 | 0.348 | 0.953 | 5.152 | 0.675 | 20.941 | 0.607 |
| 4.45 | 0.749 | 3.98 | 0.895 | 3.89 | 0.855 | 0.352 | 0.936 | 5.272 | 0.687 | 21.281 | 0.759 |
| 4.60 | 0.745 | 4.13 | 0.888 | 4.14 | 0.832 | 0.365 | 0.837 | 5.408 | 0.679 | 21.281 | 0.719 |
| 4.78 | 0.749 | 4.33 | 0.882 | 4.36 | 0.809 | 0.373 | 0.798 | 5.546 | 0.690 | 21.678 | 0.710 |
| 5.00 | 0.773 | 4.58 | 0.877 | 4.57 | 0.799 | 0.402 | 0.655 | 5.720 | 0.762 | 22.439 | 0.757 |
| 5.21 | 0.823 | 4.79 | 0.871 | 5.05 | 0.808 | 0.414 | 0.596 | 5.781 | 0.914 | 23.388 | 0.777 |
| 5.45 | 0.843 | 4.96 | 0.866 | 5.65 | 0.618 | 0.443 | 0.524 | 5.861 | 0.928 | 24.322 | 0.791 |
| 5.61 | 0.934 | 5.26 | 0.866 | 5.47 | 0.824 | 0.443 | 0.421 | 5.957 | 0.922 | 25.644 | 0.762 |
| 5.78 | 0.984 | 5.45 | 0.877 | 5.53 | 0.848 | 0.516 | 0.385 | 5.957 | 0.869 | 25.122 | 0.706 |
| 5.97 | 0.977 | 5.70 | 0.897 | 5.64 | 0.872 | 0.532 | 0.281 | 6.209 | 0.823 | 27.164 | 0.635 |
| 6.15 | 0.965 | 5.95 | 0.856 | 5.69 | 0.886 | 0.652 | 0.275 | 6.577 | 0.805 | 28.104 | 0.793 |
| 6.26 | 0.920 | 6.37 | 0.866 | 5.85 | 0.909 | 0.819 | 0.275 | 6.776 | 0.750 | 29.242 | 0.772 |
| 6.41 | 0.897 | 6.53 | 0.877 | 6.04 | 0.925 | 0.940 | 0.290 | 7.516 | 0.923 | 33.729 | 0.781 |
| 6.45 | 0.882 | 6.70 | 0.897 | 6.33 | 0.935 | 1.233 | 0.392 | 8.291 | 0.954 | 34.356 | 0.765 |
| 6.55 | 0.867 | 7.01 | 0.925 | 6.58 | 0.949 | 1.407 | 0.429 | 8.356 | 0.867 | 35.156 | 0.759 |
| 6.66 | 0.923 | 7.52 | 0.952 | 7.43 | 0.942 | 1.500 | 0.466 | 8.570 | 0.934 | 37.053 | 0.770 |
| 6.70 | 0.968 | 8.30 | 0.959 | 8.82 | 0.952 | 1.637 | 0.481 | 8.710 | 0.875 | 37.497 | 0.769 |
| 6.82 | 0.975 | 8.52 | 0.964 | 9.25 | 0.952 | 1.706 | 0.503 | 7.516 | 0.923 | 37.497 | 0.742 |
| 7.10 | 0.983 | 9.40 | 0.968 | 9.40 | 0.947 | 1.828 | 0.526 | 8.291 | 0.954 | 38.194 | 0.734 |
| 7.68 | 0.937 | 10.40 | 0.971 | 9.62 | 0.926 | 2.000 | 0.557 | 8.356 | 0.887 | 39.719 | 0.731 |
| 8.37 | 0.937 | 10.40 | 0.966 | 9.70 | 0.893 | 2.099 | 0.578 | 8.570 | 0.934 | 97.959 | 0.727 |
| 9.47 | 0.982 | 11.12 | 0.964 | 9.86 | 0.838 | 2.183 | 0.604 | 8.710 | 0.875 | | |
| 9.77 | 0.959 | 12.38 | 0.967 | 10.01 | 0.860 | 2.512 | 0.669 | 9.290 | 0.921 | | |
| 10.04 | 0.965 | 12.40 | 0.967 | 10.19 | 0.882 | 2.812 | 0.744 | 9.683 | 0.941 | | |
| 10.60 | 0.975 | 12.56 | 0.975 | 10.26 | 0.902 | 3.026 | 0.799 | 9.750 | 0.922 | | |
| 11.05 | 0.987 | 13.07 | 0.981 | 10.55 | 0.914 | 3.076 | 0.852 | 9.750 | 0.887 | | |
| 11.20 | 0.989 | 13.50 | 0.981 | 10.67 | 0.924 | 3.076 | 0.879 | 9.931 | 0.872 | | |
| 11.32 | 0.982 | 13.94 | 0.978 | 11.25 | 0.935 | 3.216 | 0.885 | 10.544 | 0.922 | | |
| 11.47 | 0.983 | 13.94 | 0.973 | 11.66 | 0.942 | 3.257 | 0.879 | 11.220 | 0.953 | | |
| 11.74 | 0.972 | | | 12.08 | 0.946 | 3.483 | 0.885 | 12.331 | 0.959 | | |
| 12.33 | 0.970 | | | 13.11 | 0.946 | 3.524 | 0.937 | 13.032 | 0.965 | | |
| 12.79 | 0.976 | | | 13.45 | 0.944 | 3.589 | 0.947 | 13.740 | 0.954 | | |
| 13.24 | 0.982 | | | 14.00 | 0.936 | 3.673 | 0.940 | 14.825 | 0.920 | | |
| 13.42 | 0.983 | 3.23 | 0.979 | | | 4.122 | 0.732 | 15.066 | 0.893 | | |
| 13.56 | 0.982 | 3.31 | 0.953 | | | 4.416 | 0.586 | 15.922 | 0.884 | | |

b. Normal Spectral Reflectance (Wavelength Dependence)

There are thirteen sets of experimental data available for the wavelength dependence of the normal spectral reflectance of acrylic resin coatings as listed in Table 15-6 and shown in Figure 15-4. Specimen characterization and measurement information for the data are given in Table 15-5. There are seven different kinds of acrylic resins used for measurements. The normal spectral reflectance values for flat black acrylic were the lowest. White paint (Sherwin Williams) has the highest reflectance value. Only Brandenburg [T52153] and Afonaseva, et al. [T56239] measured the normal spectral reflectance in the wavelength region above 2.6 μm . Because the range of reflectance for acrylic was wide, only provisional values were reported here which are listed in Table 15-4 and shown in Figure 15-3. The provisional values are for the flat white acrylic paint (Sherwin Williams) coatings at 310 K. The estimated uncertainty is within $\pm 30\%$.

TABLE 15-7. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|---------------|---------------|---------------|---------------|
| ACRYLIC PAINT | ACRYLIC PAINT | ACRYLIC PAINT | ACRYLIC PAINT |
| WHITE | WHITE | WHITE | WHITE |
| T = 310 | T = 310 | T = 310 | T = 310 |
| 0.35 | 0.14 | 12.50 | 0.06 |
| 0.40 | 0.40 | 13.00 | 0.06 |
| 0.50 | 0.90 | 13.50 | 0.06 |
| 1.50 | 0.89 | 14.00 | 0.09 |
| 1.00 | 0.26 | 14.50 | 0.10 |
| 1.50 | 0.77 | 15.00 | 0.11 |
| 2.00 | 0.60 | | |
| 2.50 | 0.45 | | |
| 2.75 | 0.29 | | |
| 3.00 | 0.13 | | |
| 3.30 | 0.12 | | |
| 3.50 | 0.09 | | |
| 3.75 | 0.23 | | |
| 3.80 | 0.24 | | |
| 4.00 | 0.28 | | |
| 4.40 | 0.33 | | |
| 4.84 | 0.35 | | |
| 5.30 | 0.34 | | |
| 5.50 | 0.29 | | |
| 5.70 | 0.12 | | |
| 5.80 | 0.07 | | |
| 6.00 | 0.09 | | |
| 6.10 | 0.20 | | |
| 6.30 | 0.25 | | |
| 6.40 | 0.23 | | |
| 6.50 | 0.33 | | |
| 6.90 | 0.08 | | |
| 7.20 | 0.09 | | |
| 7.20 | 0.10 | | |
| 7.30 | 0.10 | | |
| 7.67 | 0.05 | | |
| 8.00 | 0.07 | | |
| 8.20 | 0.17 | | |
| 9.00 | 0.07 | | |
| 9.30 | 0.08 | | |
| 10.00 | 0.10 | | |
| 10.60 | 0.16 | | |
| 11.70 | 0.09 | | |
| 12.00 | 0.07 | | |

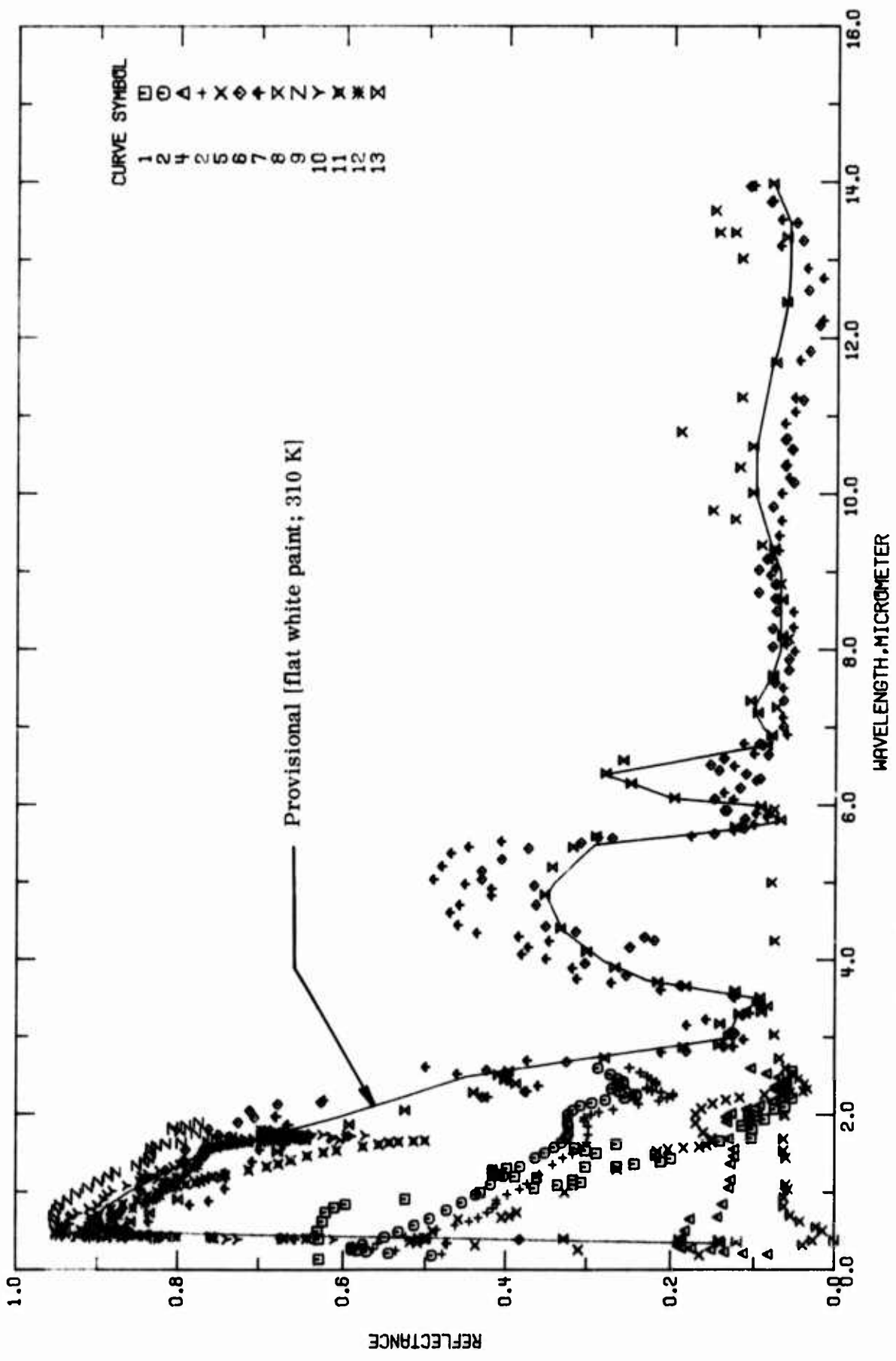


FIGURE 15-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE).

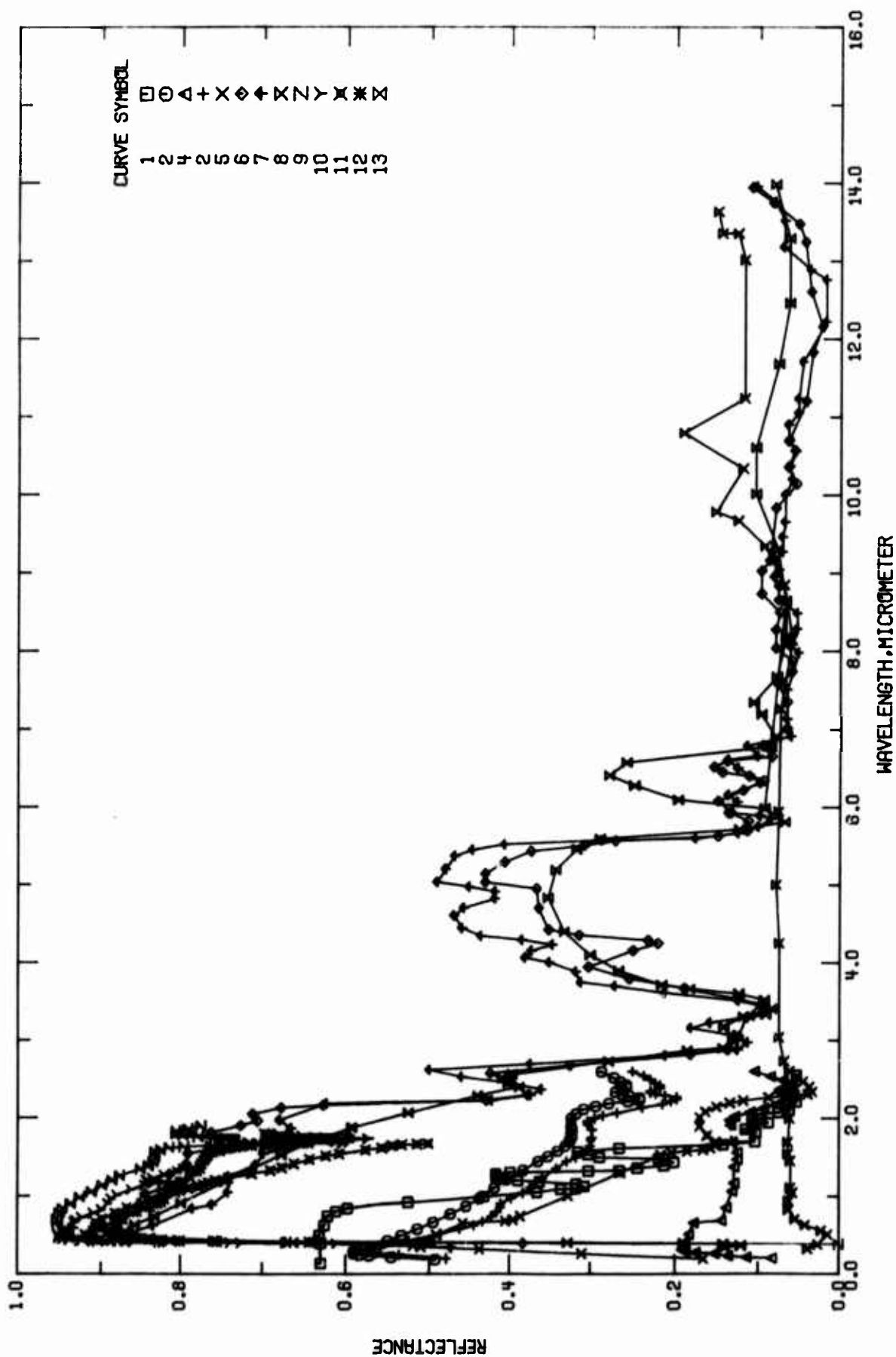


FIGURE 15-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE).

TABLE 15-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN COATING (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|--|--|
| 1 T64206 | Pennington, C.W. and Moore, G.L. | 1971 | 0.4-2.6 | ~293 | Acrylic Panel | Reflective type acrylic panel; reflectance spectra was measured by using a DK-2 spectrophotometer; data were extracted from figure; $\theta \sim 0^\circ$. |
| 2 T62587 | Gilligan, J.E. and Brzuszkiewicz, | 1971 | 0.2-2.6 | ~293 | DuPont Elvacite 6011 (methyl-methacrylate) | 0.015 in. thick sprayed film; Beckman DK-2 spectrometer was used; data were extracted from figure; $\theta \sim 0^\circ$. |
| 3 T62387 | Gilligan, J.E. and Brzuszkiewicz, | 1971 | 0.2-2.6 | ~293 | DuPont Elvacite 6011 (methyl-methacrylate) | Similar to the above specimen except 0.032 in. thick. |
| 4 T62587 | Gilligan, J.E. and Brzuszkiewicz, | 1971 | 0.2-2.6 | ~293 | DuPont Elvacite 6011 (methyl-methacrylate) | Similar to the above specimen except 0.054 in. thick. |
| 5 T62587 | Gilligan, J.E. and Brzuszkiewicz, | 1971 | 0.2-2.6 | ~293 | DuPont Elvacite 6011 (methyl-methacrylate) | Similar to the above specimen except 0.035 in. thick film by a doctor's blade technique. |
| 6 T56229 | Afanaseva, G.O., Vinogradova, L.M., Il'yasov, S.G., Fridzon, M.B., and Tyuria, B.F. | 1969 | 0.25-15 | ~293 | AS-81 | Acrylic white enamals; data were extracted from figure; $\theta \sim 0^\circ$. |
| 7 T56229 | Afanaseva, G.O., et al. | 1969 | 0.25-15 | ~293 | AS-2Cp (R) | Similar to the above specimen. |
| 8 T53498 | Shinkle, F.J. | 1961 | 0.38-38 | 338 | Flat Black Acrylic Paint | A heavy coat of paint had been sprayed on 5/16 in. diameter disc of 0.012 in. thick stainless steel; a Perkin-Elmer Model 13 double beam spectrometer was used; data were extracted from figure; $\theta \sim 0^\circ$. |
| 9 T39754 | Anderson, R.B. | 1965 | 0.38-1.9 | ~293 | (Sherwin Williams) White Paint | 3 mil spray coating of W. P. Fuller Co. 171W-560 Acrylic Vehicle glass white paint on a white substrate; a Gier-Dunkel reflectometer and a Cary reflectometer were used; data were extracted from figure; $\theta \sim 0^\circ$. |
| 10 T39754 | Anderson, R.B. | 1965 | 0.38-1.9 | ~293 | White Paint (DMS 1765) | 2.6 mil spray coating of DMS 1765 white paint on aluminum; other specifications similar to above. |
| 11 T39754 | Anderson, R.B. | 1965 | 0.38-1.9 | ~293 | White Paint (NASA-S-13) | 8.5 mil spray coating of NASA-S-13 white paint on aluminum; other specifications similar to above. |
| 12 T39754 | Anderson, R.B. | 1965 | 0.38-1.9 | ~293 | White Paint (MIL-C22750) | 2.2 mil spray coating of MIL-C22750 white paint on aluminum; other specifications similar to above. |
| 13 T52153 | Bradenberg, W.M. | 1961 | 0.3-25 | 310.8 | Flat White Acrylic Paint | Two coats of Sherwin Williams Flat White acrylic paint over one coat of Sherwin Williams Pre-treatment Wash coating were coated on vehicle; Perkin-Elmer Model 13 double beam meter was used; data were extracted from figure; $\theta \sim 0^\circ$. |

TABLE 15-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| 0.400 | 0.628 | 1.996 | 0.106 | 2.220 | 0.254 | 2.218 | 0.069 | 1.919 | 0.302 | 1.615 | 0.156 | 0.39 | 0.382 | 0.41 | 0.672 |
| 0.140 | 0.628 | 2.056 | 0.099 | 2.242 | 0.241 | 2.260 | 0.063 | 1.961 | 0.302 | 1.653 | 0.150 | 0.47 | 0.976 | 0.51 | 0.867 |
| 0.500 | 0.630 | 2.080 | 0.075 | 2.266 | 0.241 | 2.293 | 0.063 | 2.002 | 0.294 | 1.695 | 0.150 | 0.59 | 0.895 | 0.59 | 0.895 |
| 0.530 | 0.624 | 2.109 | 0.062 | 2.293 | 0.253 | 2.335 | 0.074 | 2.038 | 0.284 | 1.776 | 0.160 | 0.76 | 0.868 | 0.76 | 0.868 |
| 0.750 | 0.620 | 2.219 | 0.053 | 2.310 | 0.261 | 2.367 | 0.074 | 2.071 | 0.267 | 1.898 | 0.169 | 1.02 | 0.843 | 1.02 | 0.843 |
| 0.811 | 0.610 | 2.559 | 0.053 | 2.342 | 0.269 | 2.408 | 0.060 | 2.142 | 0.238 | 2.016 | 0.169 | 1.41 | 0.813 | 1.41 | 0.791 |
| 0.847 | 0.596 | | | 2.378 | 0.261 | 2.452 | 0.060 | 2.185 | 0.214 | 2.086 | 0.162 | 1.55 | 0.789 | 1.55 | 0.789 |
| 3.871 | 0.566 | | | 2.405 | 0.256 | 2.490 | 0.070 | 2.222 | 0.204 | 2.151 | 0.149 | 1.62 | 0.769 | 1.62 | 0.769 |
| 0.919 | 0.524 | | | 2.428 | 0.256 | 2.538 | 0.085 | 2.247 | 0.197 | 2.1976 | 0.133 | 1.72 | 0.734 | 1.72 | 0.734 |
| 0.996 | 0.431 | 0.186 | 0.491 | 2.470 | 0.263 | 2.600 | 0.104 | 2.273 | 0.197 | 2.227 | 0.117 | 1.82 | 0.760 | 1.82 | 0.760 |
| 1.055 | 0.364 | 0.215 | 0.544 | 2.526 | 0.271 | | | 2.295 | 0.211 | 2.267 | 0.087 | 1.91 | 0.724 | 1.91 | 0.724 |
| 1.0941 | 0.335 | 0.236 | 0.570 | 2.600 | 0.286 | | | 2.317 | 0.222 | 2.227 | 0.117 | 2.01 | 0.701 | 2.01 | 0.701 |
| 1.104 | 0.316 | 0.250 | 0.592 | | | | | 2.333 | 0.228 | 2.298 | 0.055 | 2.05 | 0.687 | 2.05 | 0.687 |
| 1.159 | 0.306 | 0.269 | 0.589 | | | | | 2.352 | 0.228 | 2.312 | 0.039 | 2.09 | 0.669 | 2.09 | 0.669 |
| 1.189 | 0.361 | 0.289 | 0.589 | | | | | 2.393 | 0.217 | 2.338 | 0.033 | 2.14 | 0.652 | 2.14 | 0.652 |
| 1.205 | 0.388 | 0.426 | 0.549 | | | | | 2.427 | 0.217 | 2.405 | 0.037 | 2.18 | 0.635 | 2.18 | 0.635 |
| 1.228 | 0.407 | 0.575 | 0.532 | | | | | 2.459 | 0.223 | 2.470 | 0.045 | 2.22 | 0.618 | 2.22 | 0.618 |
| 1.253 | 0.416 | 0.663 | 0.494 | | | | | 2.500 | 0.228 | 2.531 | 0.053 | 2.26 | 0.601 | 2.26 | 0.601 |
| 1.288 | 0.416 | 0.771 | 0.473 | | | | | 2.550 | 0.236 | 2.600 | 0.062 | 2.30 | 0.584 | 2.30 | 0.584 |
| 1.309 | 0.398 | 0.671 | 0.454 | | | | | 2.600 | 0.249 | | | 2.34 | 0.567 | 2.34 | 0.567 |
| 1.328 | 0.301 | 0.973 | 0.437 | | | | | | | | | 2.38 | 0.550 | 2.38 | 0.550 |
| 1.334 | 0.264 | 1.103 | 0.418 | | | | | | | | | 2.42 | 0.533 | 2.42 | 0.533 |
| 1.365 | 0.243 | 1.214 | 0.402 | | | | | | | | | 2.46 | 0.516 | 2.46 | 0.516 |
| 1.397 | 0.212 | 1.331 | 0.382 | | | | | | | | | 2.50 | 0.499 | 2.50 | 0.499 |
| 1.439 | 0.200 | 1.447 | 0.363 | | | | | | | | | 2.54 | 0.482 | 2.54 | 0.482 |
| 1.486 | 0.218 | 1.511 | 0.351 | | | | | | | | | 2.58 | 0.465 | 2.58 | 0.465 |
| 1.507 | 0.268 | 1.581 | 0.339 | | | | | | | | | 2.62 | 0.448 | 2.62 | 0.448 |
| 1.538 | 0.301 | 1.641 | 0.330 | | | | | | | | | 2.66 | 0.431 | 2.66 | 0.431 |
| 1.574 | 0.314 | 1.707 | 0.324 | | | | | | | | | 2.70 | 0.414 | 2.70 | 0.414 |
| 1.622 | 0.264 | 1.755 | 0.321 | | | | | | | | | 2.74 | 0.397 | 2.74 | 0.397 |
| 1.654 | 0.144 | 1.856 | 0.321 | | | | | | | | | 2.78 | 0.380 | 2.78 | 0.380 |
| 1.702 | 0.103 | 1.902 | 0.322 | | | | | | | | | 2.82 | 0.363 | 2.82 | 0.363 |
| 1.787 | 0.900 | 2.002 | 0.322 | | | | | | | | | 2.86 | 0.346 | 2.86 | 0.346 |
| 1.820 | 0.102 | 2.060 | 0.322 | | | | | | | | | 2.90 | 0.329 | 2.90 | 0.329 |
| 1.852 | 0.114 | 2.118 | 0.316 | | | | | | | | | 2.94 | 0.312 | 2.94 | 0.312 |
| 1.919 | 0.105 | 2.158 | 0.307 | | | | | | | | | 2.98 | 0.295 | 2.98 | 0.295 |
| 1.947 | 0.087 | 2.194 | 0.293 | | | | | | | | | 3.02 | 0.278 | 3.02 | 0.278 |
| 1.986 | 0.096 | | 0.277 | | | | | | | | | 3.06 | 0.261 | 3.06 | 0.261 |
| | | | | | | | | | | | | 3.10 | 0.244 | 3.10 | 0.244 |
| | | | | | | | | | | | | 3.14 | 0.227 | 3.14 | 0.227 |
| | | | | | | | | | | | | 3.18 | 0.210 | 3.18 | 0.210 |
| | | | | | | | | | | | | 3.22 | 0.193 | 3.22 | 0.193 |
| | | | | | | | | | | | | 3.26 | 0.176 | 3.26 | 0.176 |
| | | | | | | | | | | | | 3.30 | 0.159 | 3.30 | 0.159 |
| | | | | | | | | | | | | 3.34 | 0.142 | 3.34 | 0.142 |
| | | | | | | | | | | | | 3.38 | 0.125 | 3.38 | 0.125 |
| | | | | | | | | | | | | 3.42 | 0.108 | 3.42 | 0.108 |
| | | | | | | | | | | | | 3.46 | 0.091 | 3.46 | 0.091 |
| | | | | | | | | | | | | 3.50 | 0.074 | 3.50 | 0.074 |
| | | | | | | | | | | | | 3.54 | 0.057 | 3.54 | 0.057 |
| | | | | | | | | | | | | 3.58 | 0.040 | 3.58 | 0.040 |
| | | | | | | | | | | | | 3.62 | 0.023 | 3.62 | 0.023 |
| | | | | | | | | | | | | 3.66 | 0.006 | 3.66 | 0.006 |
| | | | | | | | | | | | | 3.70 | | 3.70 | |
| | | | | | | | | | | | | 3.74 | | 3.74 | |
| | | | | | | | | | | | | 3.78 | | 3.78 | |
| | | | | | | | | | | | | 3.82 | | 3.82 | |
| | | | | | | | | | | | | 3.86 | | 3.86 | |
| | | | | | | | | | | | | 3.90 | | 3.90 | |
| | | | | | | | | | | | | 3.94 | | 3.94 | |
| | | | | | | | | | | | | 3.98 | | 3.98 | |
| | | | | | | | | | | | | 4.02 | | 4.02 | |
| | | | | | | | | | | | | 4.06 | | 4.06 | |
| | | | | | | | | | | | | 4.10 | | 4.10 | |
| | | | | | | | | | | | | 4.14 | | 4.14 | |
| | | | | | | | | | | | | 4.18 | | 4.18 | |
| | | | | | | | | | | | | 4.22 | | 4.22 | |
| | | | | | | | | | | | | 4.26 | | 4.26 | |
| | | | | | | | | | | | | 4.30 | | 4.30 | |
| | | | | | | | | | | | | 4.34 | | 4.34 | |
| | | | | | | | | | | | | 4.38 | | 4.38 | |
| | | | | | | | | | | | | 4.42 | | 4.42 | |
| | | | | | | | | | | | | 4.46 | | 4.46 | |
| | | | | | | | | | | | | 4.50 | | 4.50 | |
| | | | | | | | | | | | | 4.54 | | 4.54 | |
| | | | | | | | | | | | | 4.58 | | 4.58 | |
| | | | | | | | | | | | | 4.62 | | 4.62 | |
| | | | | | | | | | | | | 4.66 | | 4.66 | |
| | | | | | | | | | | | | 4.70 | | 4.70 | |
| | | | | | | | | | | | | 4.74 | | 4.74 | |
| | | | | | | | | | | | | 4.78 | | 4.78 | |
| | | | | | | | | | | | | 4.82 | | 4.82 | |
| | | | | | | | | | | | | 4.86 | | 4.86 | |
| | | | | | | | | | | | | 4.90 | | 4.90 | |
| | | | | | | | | | | | | 4.94 | | 4.94 | |
| | | | | | | | | | | | | 4.98 | | 4.98 | |
| | | | | | | | | | | | | 5.02 | | 5.02 | |
| | | | | | | | | | | | | 5.06 | | 5.06 | |
| | | | | | | | | | | | | 5.10 | | 5.10 | |
| | | | | | | | | | | | | 5.14 | | 5.14 | |
| | | | | | | | | | | | | 5.18 | | 5.18 | |
| | | | | | | | | | | | | 5.22 | | 5.22 | |
| | | | | | | | | | | | | 5.26 | | 5.26 | |
| | | | | | | | | | | | | 5.30 | | 5.30 | |
| | | | | | | | | | | | | 5.34 | | 5.34 | |
| | | | | | | | | | | | | 5.38 | | 5.38 | |
| | | | | | | | | | | | | 5.42 | | 5.42 | |
| | | | | | | | | | | | | 5.46 | | 5.46 | |
| | | | | | | | | | | | | 5.50 | | 5.50 | |
| | | | | | | | | | | | | 5.54 | | 5.54 | |
| | | | | | | | | | | | | 5.58 | | 5.58 | |
| </ | | | | | | | | | | | | | | | |

TABLE 15-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|-----------------|
| CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 6 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) | CURVE 7 (CONT.) |
| 2.06 | 0.716 | 6.60 | 0.137 | 0.45 | 0.831 | 4.35 | 0.436 | 9.47 | 0.072 | 0.819 | 0.063 | 0.819 | 0.063 |
| 2.14 | 0.676 | 6.65 | 0.084 | 0.53 | 0.859 | 4.45 | 0.460 | 9.66 | 0.069 | 0.935 | 0.063 | 0.935 | 0.063 |
| 2.17 | 0.626 | 6.79 | 0.095 | 0.62 | 0.833 | 4.45 | 0.470 | 10.01 | 0.069 | 1.042 | 0.058 | 1.042 | 0.058 |
| 2.23 | 0.429 | 7.01 | 0.066 | 0.84 | 0.783 | 4.71 | 0.453 | 10.01 | 0.060 | 1.104 | 0.051 | 1.104 | 0.051 |
| 2.30 | 0.376 | 7.35 | 0.066 | 0.89 | 0.759 | 4.83 | 0.418 | 10.34 | 0.063 | 1.449 | 0.061 | 1.449 | 0.061 |
| 2.47 | 0.393 | 7.58 | 0.077 | 1.05 | 0.739 | 4.92 | 0.418 | 10.57 | 0.056 | 1.538 | 0.064 | 1.538 | 0.064 |
| 2.58 | 0.424 | 7.74 | 0.060 | 1.25 | 0.739 | 4.98 | 0.451 | 10.70 | 0.065 | 1.693 | 0.064 | 1.693 | 0.064 |
| 2.68 | 0.324 | 7.88 | 0.060 | 1.40 | 0.706 | 5.04 | 0.490 | 10.91 | 0.065 | 1.995 | 0.062 | 1.995 | 0.062 |
| 2.82 | 0.191 | 8.04 | 0.080 | 1.55 | 0.697 | 5.21 | 0.480 | 11.06 | 0.053 | 2.366 | 0.065 | 2.366 | 0.065 |
| 2.88 | 0.136 | 8.28 | 0.080 | 1.62 | 0.668 | 5.38 | 0.469 | 11.24 | 0.053 | 2.730 | 0.069 | 2.730 | 0.069 |
| 3.05 | 0.123 | 8.50 | 0.075 | 1.69 | 0.644 | 5.46 | 0.447 | 11.72 | 0.047 | 3.034 | 0.075 | 3.034 | 0.075 |
| 3.29 | 0.114 | 8.74 | 0.097 | 1.78 | 0.664 | 5.53 | 0.406 | 12.23 | 0.018 | 4.246 | 0.075 | 4.246 | 0.075 |
| 3.46 | 0.097 | 9.03 | 0.097 | 1.87 | 0.664 | 5.58 | 0.287 | 12.77 | 0.018 | 5.000 | 0.079 | 5.000 | 0.079 |
| 3.53 | 0.125 | 9.17 | 0.087 | 1.98 | 0.622 | 5.60 | 0.175 | 12.90 | 0.038 | 5.943 | 0.076 | 5.943 | 0.076 |
| 3.67 | 0.189 | 9.84 | 0.090 | 2.19 | 0.622 | 5.67 | 0.124 | 13.19 | 0.071 | 7.261 | 0.074 | 7.261 | 0.074 |
| 3.80 | 0.253 | 10.15 | 0.055 | 2.23 | 0.422 | 5.75 | 0.100 | 13.53 | 0.070 | 8.140 | 0.060 | 8.140 | 0.060 |
| 3.95 | 0.302 | 10.37 | 0.065 | 2.30 | 0.373 | 5.85 | 0.085 | 13.77 | 0.081 | 8.851 | 0.070 | 8.851 | 0.070 |
| 4.16 | 0.249 | 10.58 | 0.064 | 2.37 | 0.359 | 5.89 | 0.098 | 13.97 | 0.103 | 9.351 | 0.093 | 9.351 | 0.093 |
| 4.25 | 0.220 | 10.72 | 0.064 | 2.45 | 0.398 | 5.93 | 0.135 | 14.07 | 0.096 | 9.683 | 0.124 | 9.683 | 0.124 |
| 4.29 | 0.232 | 11.21 | 0.043 | 2.53 | 0.460 | 6.07 | 0.125 | 14.11 | 0.116 | 9.795 | 0.151 | 9.795 | 0.151 |
| 4.36 | 0.313 | 11.84 | 0.035 | 2.62 | 0.499 | 6.16 | 0.136 | 14.18 | 0.127 | 10.35 | 0.119 | 10.35 | 0.119 |
| 4.43 | 0.351 | 12.17 | 0.033 | 2.70 | 0.373 | 6.31 | 0.098 | 14.35 | 0.127 | 10.61 | 0.190 | 10.61 | 0.190 |
| 4.71 | 0.363 | 12.62 | 0.037 | 2.81 | 0.211 | 6.50 | 0.124 | 14.41 | 0.156 | 11.25 | 0.117 | 11.25 | 0.117 |
| 4.96 | 0.366 | 13.26 | 0.044 | 2.88 | 0.124 | 6.61 | 0.136 | 14.49 | 0.192 | 13.03 | 0.117 | 13.03 | 0.117 |
| 5.04 | 0.431 | 13.49 | 0.052 | 2.97 | 0.112 | 6.66 | 0.101 | 14.54 | 0.192 | 13.37 | 0.125 | 13.37 | 0.125 |
| 5.15 | 0.431 | 13.76 | 0.083 | 3.06 | 0.128 | 6.79 | 0.113 | 14.64 | 0.182 | 13.65 | 0.144 | 13.65 | 0.144 |
| 5.30 | 0.406 | 13.96 | 0.108 | 3.16 | 0.180 | 6.91 | 0.061 | 14.79 | 0.220 | 14.16 | 0.149 | 14.16 | 0.149 |
| 5.44 | 0.373 | 14.11 | 0.091 | 3.23 | 0.157 | 7.13 | 0.066 | 14.89 | 0.253 | 14.52 | 0.089 | 14.52 | 0.089 |
| 5.51 | 0.307 | 14.31 | 0.082 | 3.31 | 0.105 | 7.51 | 0.066 | 14.97 | 0.198 | 14.79 | 0.080 | 14.79 | 0.080 |
| 5.57 | 0.270 | 14.44 | 0.093 | 3.43 | 0.093 | 7.98 | 0.052 | 15.06 | 0.170 | 14.93 | 0.091 | 14.93 | 0.091 |
| 5.63 | 0.149 | 14.51 | 0.093 | 3.51 | 0.123 | 8.07 | 0.063 | CURVE 8 | | 15.32 | 0.124 | 15.32 | 0.124 |
| 5.70 | 0.113 | 14.79 | 0.125 | 3.61 | 0.212 | 8.16 | 0.063 | T = 338. | | 16.00 | 0.117 | 16.00 | 0.117 |
| 5.82 | 0.112 | 14.91 | 0.148 | 3.70 | 0.270 | 8.29 | 0.054 | 0.321 | 0.039 | 16.79 | 0.127 | 16.79 | 0.127 |
| 5.93 | 0.133 | 15.05 | 0.179 | 3.75 | 0.311 | 8.49 | 0.054 | 0.376 | 0.026 | 17.06 | 0.177 | 17.06 | 0.177 |
| 6.08 | 0.148 | CURVE 7 | | 3.89 | 0.317 | 8.66 | 0.077 | 0.504 | 0.014 | 18.75 | 0.213 | 18.75 | 0.213 |
| 6.22 | 0.118 | T = 293. | | 4.01 | 0.350 | 8.84 | 0.077 | 0.552 | 0.022 | 19.23 | 0.221 | 19.23 | 0.221 |
| 6.34 | 0.094 | | | 4.07 | 0.380 | 8.96 | 0.082 | 0.625 | 0.042 | 20.14 | 0.221 | 20.14 | 0.221 |
| 6.40 | 0.111 | | | 4.16 | 0.372 | 9.05 | 0.076 | 0.702 | 0.055 | 22.44 | 0.170 | 22.44 | 0.170 |
| 6.45 | 0.111 | 0.34 | 0.472 | 4.24 | 0.346 | 9.17 | 0.081 | | | | | | |
| 6.52 | 0.153 | 0.40 | 0.656 | 4.30 | 0.384 | 9.28 | 0.072 | | | | | | |

TABLE 15-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ |
|------------------|------------------|------------------|------------------|------------------|------------------|
| CURVE 13 (CONT.) | CURVE 13 (CONT.) | CURVE 13 (CONT.) | CURVE 13 (CONT.) | CURVE 13 (CONT.) | CURVE 13 (CONT.) |
| 0.401 | 0.327 | 5.715 | 0.123 | 19.634 | 0.143 |
| 0.406 | 0.507 | 5.806 | 0.069 | 19.953 | 0.183 |
| 0.427 | 0.757 | 5.984 | 0.093 | 20.701 | 0.215 |
| 0.433 | 0.812 | 6.095 | 0.197 | 21.528 | 0.236 |
| 0.444 | 0.839 | 6.280 | 0.248 | 22.856 | 0.248 |
| 0.460 | 0.859 | 6.412 | 0.279 | 24.210 | 0.235 |
| 0.493 | 0.863 | 6.577 | 0.257 | 25.941 | 0.200 |
| 0.542 | 0.868 | 6.776 | 0.086 | 100.00 | 0.200 |
| 0.624 | 0.856 | 6.902 | 0.080 | | |
| 0.738 | 0.832 | 7.195 | 0.097 | | |
| 0.912 | 0.798 | 7.345 | 0.106 | | |
| 1.189 | 0.743 | 7.674 | 0.079 | | |
| 1.531 | 0.676 | 8.1846 | 0.068 | | |
| 1.683 | 0.644 | 8.650 | 0.068 | | |
| 1.879 | 0.592 | 5.984 | 0.093 | | |
| 2.055 | 0.525 | 6.095 | 0.197 | | |
| 2.291 | 0.440 | 6.281 | 0.248 | | |
| 2.404 | 0.387 | 6.412 | 0.278 | | |
| 2.455 | 0.401 | 6.577 | 0.257 | | |
| 2.518 | 0.409 | 6.776 | 0.086 | | |
| 2.565 | 0.396 | 6.9024 | 0.080 | | |
| 2.735 | 0.278 | 7.195 | 0.097 | | |
| 2.871 | 0.185 | 7.345 | 0.106 | | |
| 2.904 | 0.142 | 7.674 | 0.079 | | |
| 3.013 | 0.130 | 8.185 | 0.068 | | |
| 3.177 | 0.141 | 8.650 | 0.068 | | |
| 3.304 | 0.118 | 9.311 | 0.078 | | |
| 3.327 | 0.091 | 10.023 | 0.104 | | |
| 3.404 | 0.084 | 10.617 | 0.104 | | |
| 3.516 | 0.093 | 11.695 | 0.077 | | |
| 3.598 | 0.123 | 12.473 | 0.064 | | |
| 3.664 | 0.182 | 13.305 | 0.064 | | |
| 3.715 | 0.216 | 13.996 | 0.081 | | |
| 3.899 | 0.266 | 14.555 | 0.105 | | |
| 4.102 | 0.300 | 15.066 | 0.116 | | |
| 4.406 | 0.332 | 15.922 | 0.105 | | |
| 4.842 | 0.352 | 16.673 | 0.095 | | |
| 5.200 | 0.343 | 17.418 | 0.095 | | |
| 5.458 | 0.317 | 18.535 | 0.107 | | |
| 5.598 | 0.269 | 19.187 | 0.127 | | |

c. Normal Spectral Absorptance (Wavelength Dependence)

There are five sets of experimental data available for the wavelength dependence of the normal spectral absorptance of acrylic resin coatings as listed in Table 15-9 and shown in Figure 15-6. Specimen characterization and measurement information for the data are given in Table 15-8. Four of the data sets each contains a single point (10.6 μm). Therefore, as a consequence of the limited data, only provisional values of normal spectral emittance are presented here as listed in Table 15-7 and shown in Figure 15-5. The provisional values are for the "white acrylic paint" on stainless steel substrate. The estimated uncertainty is within $\pm 30\%$.

TABLE 15-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|------------------|----------|-----------|----------|
| WHITE PAINT | | | |
| S. STEEL SUBSTRA | | | |
| T = 293 | | | |
| 0.32 | 0.953 | 11.00 | 0.934 |
| 0.36 | 0.936 | 11.50 | 0.944 |
| 0.37 | 0.793 | 12.00 | 0.952 |
| 0.40 | 0.508 | 12.50 | 0.958 |
| 0.45 | 0.372 | 13.00 | 0.962 |
| 0.50 | 0.264 | 13.50 | 0.956 |
| 0.55 | 0.275 | 14.00 | 0.944 |
| 1.00 | 0.320 | 14.50 | 0.928 |
| 1.50 | 0.465 | 15.00 | 0.900 |
| 2.00 | 0.555 | | |
| 2.50 | 0.643 | | |
| 3.00 | 0.795 | | |
| 3.20 | 0.863 | | |
| 3.50 | 0.930 | | |
| 3.60 | 0.948 | | |
| 3.70 | 0.940 | | |
| 3.80 | 0.930 | | |
| 4.00 | 0.795 | | |
| 4.40 | 0.686 | | |
| 4.80 | 0.665 | | |
| 5.00 | 0.665 | | |
| 5.50 | 0.689 | | |
| 5.70 | 0.760 | | |
| 5.80 | 0.914 | | |
| 5.90 | 0.926 | | |
| 6.00 | 0.362 | | |
| 6.50 | 0.808 | | |
| 6.75 | 0.765 | | |
| 6.80 | 0.876 | | |
| 7.00 | 0.890 | | |
| 7.50 | 0.921 | | |
| 8.00 | 0.942 | | |
| 8.50 | 0.923 | | |
| 9.00 | 0.930 | | |
| 9.50 | 0.925 | | |
| 9.80 | 0.984 | | |
| 10.00 | 0.880 | | |
| 10.60 | 0.925 | | |

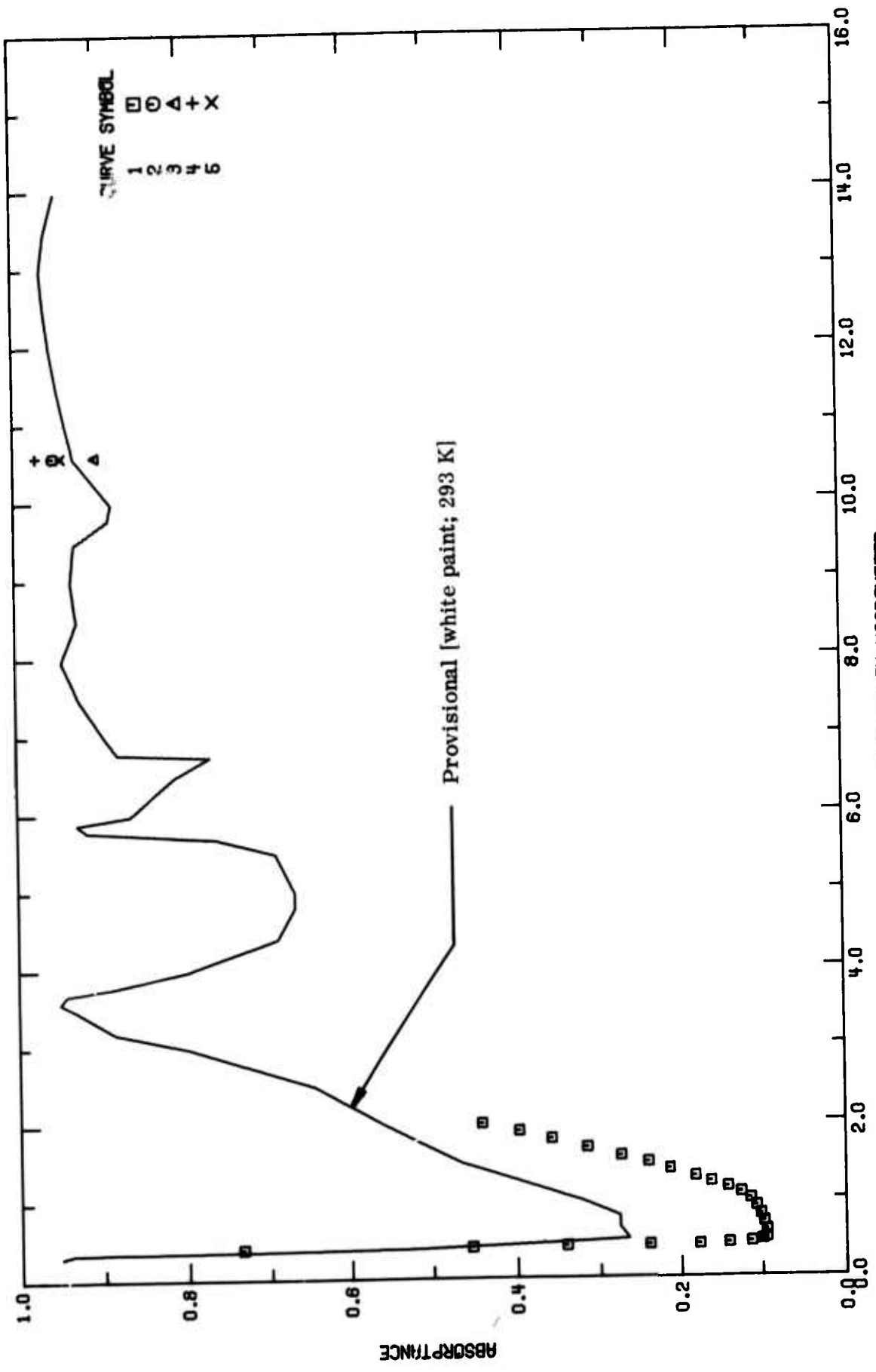


FIGURE 15-5. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE).

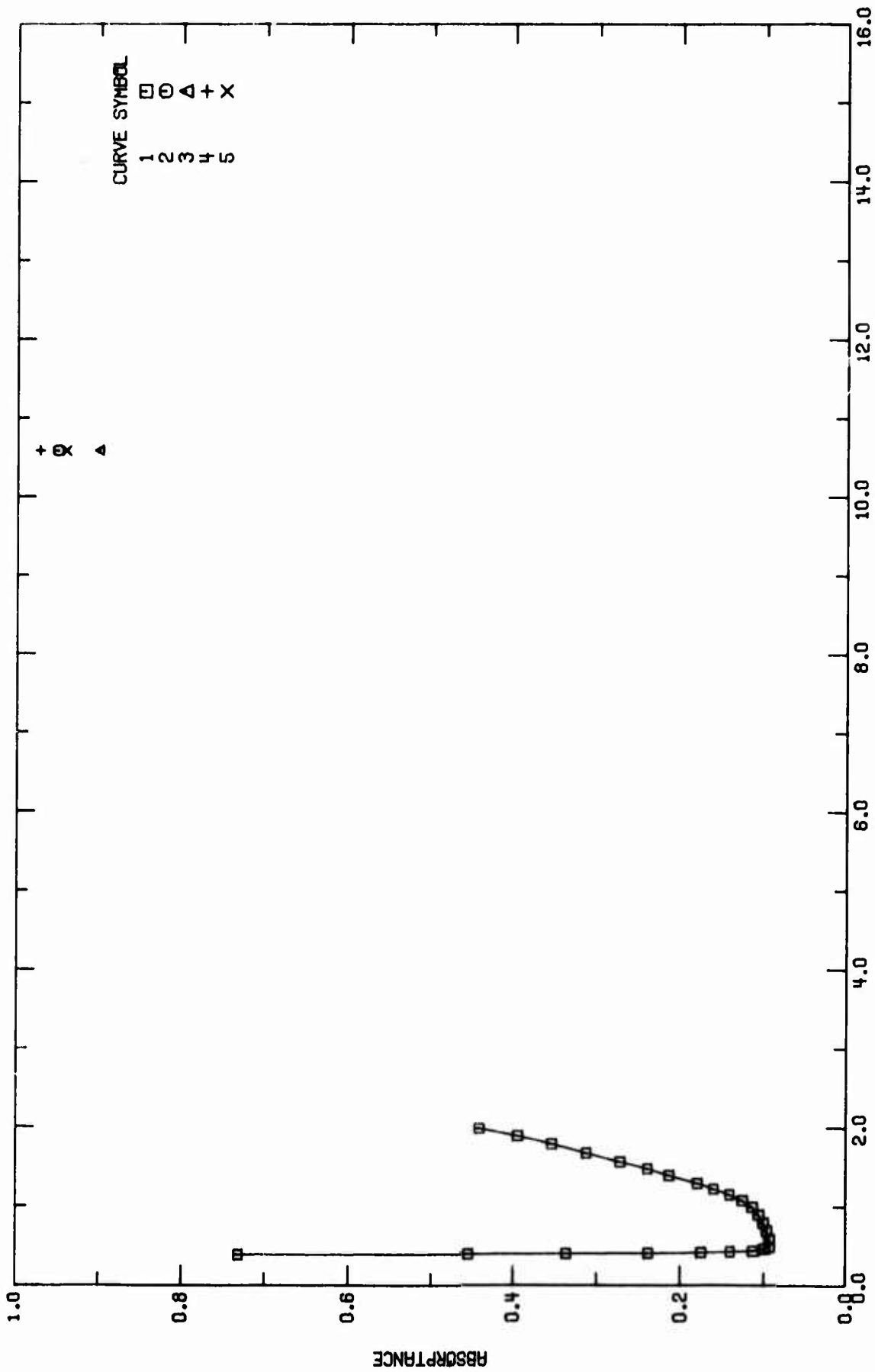


FIGURE 15-6. EXPERIMENTAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATINGS (WAVELENGTH DEPENDENCE).

TABLE 15-8. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATING (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T29754 | Anderson, R. B. | 1965 | 0.38-2.0 | ~293 | White Paint | 3 mil spray coating of W. P. Fuller Co. 171W-560 Acrylic Vehicle gloss white paint on a white substrate; data were extracted from figure; $\theta \sim 0^\circ$. |
| 2 A00004 | Firsdon, R. | 1968 | 10.6 | 300 | Acrylic (black) | Acrylic-Mil-L-1953SB-black; Mil-P-7968 0.7 mil thick primer; 3.0 mil thick top coat; an IR-9 Beckman spectrometer was used for measurements. |
| 3 A00004 | Firsdon, R. | 1968 | 10.6 | 300 | Acrylic (black) | The above specimen; a calorimeter was used for measurements. |
| 4 A00004 | Firsdon, R. | 1968 | 10.6 | 300 | Acrylic (white) | Acrylic-Mil-C-81352-white; Mil-P-23377-0.5 mil thick primer; 1.7 mil thick top coat; an IR-9 Beckman spectrometer was used. |
| 5 A00004 | Firsdon, R. | 1968 | 10.6 | 300 | Acrylic (white) | The above specimen; a calorimeter was used for measurements. |

TABLE 15-9. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|---------------------|----------|---------------------|----------|
| CURVE 1 T = 293. | | | |
| 0.400 | 0.732 | CURVE 4 T = 300. | |
| 0.404 | 0.453 | 10.6 | 0.97 |
| 0.409 | 0.339 | CURVE 5 T = 300. | |
| 0.415 | 0.239 | | |
| 0.420 | 0.176 | | |
| 0.432 | 0.139 | 10.6 | 0.94 |
| 0.446 | 0.112 | | |
| 0.459 | 0.099 | | |
| 0.495 | 0.094 | | |
| 0.592 | 0.094 | | |
| 0.701 | 0.037 | | |
| 0.800 | 0.101 | | |
| 0.903 | 0.106 | | |
| 1.000 | 0.113 | | |
| 1.086 | 0.124 | | |
| 1.155 | 0.140 | | |
| 1.229 | 0.161 | | |
| 1.298 | 0.181 | | |
| 1.399 | 0.213 | | |
| 1.482 | 0.240 | | |
| 1.571 | 0.273 | | |
| 1.684 | 0.313 | | |
| 1.801 | 0.356 | | |
| 1.902 | 0.395 | | |
| 2.000 | 0.440 | | |
| CURVE 2 T = 300. | | | |
| 10.6 | 0.95 | | |
| CURVE 3 T = 300. | | | |
| 10.5 | 0.90 | | |

d. Normal Spectral Absorptance (Temperature Dependence)

There is no experimental data available for the temperature dependence of the normal spectral absorptance of acrylic resins. However, Frisdon [A00004] measured the absorptance of acrylic paints as a function of the incident power of CO₂ laser. His results show that there is very small decreasing or no change in the absorptance value for the incident power of CO₂ laser up to 130 watts. As the incident power equals to 60 watts or higher, there is instantaneous surface charring happening at the point of incidence. Probably this charring occurs at the decomposing temperature. Therefore, we can roughly say that the absorptance of acrylic paints at wavelength 10.6 μm is independent of temperature in the temperature region from 293 K to 400 K (decomposing temperature). Figure 15-7 shows the provisional value for the normal spectral absorptance of acrylic white and black paints as a function of temperature.

The absorptance is 0.97 for white paint and 0.95 for black paint. The estimated uncertainty is within $\pm 20\%$.

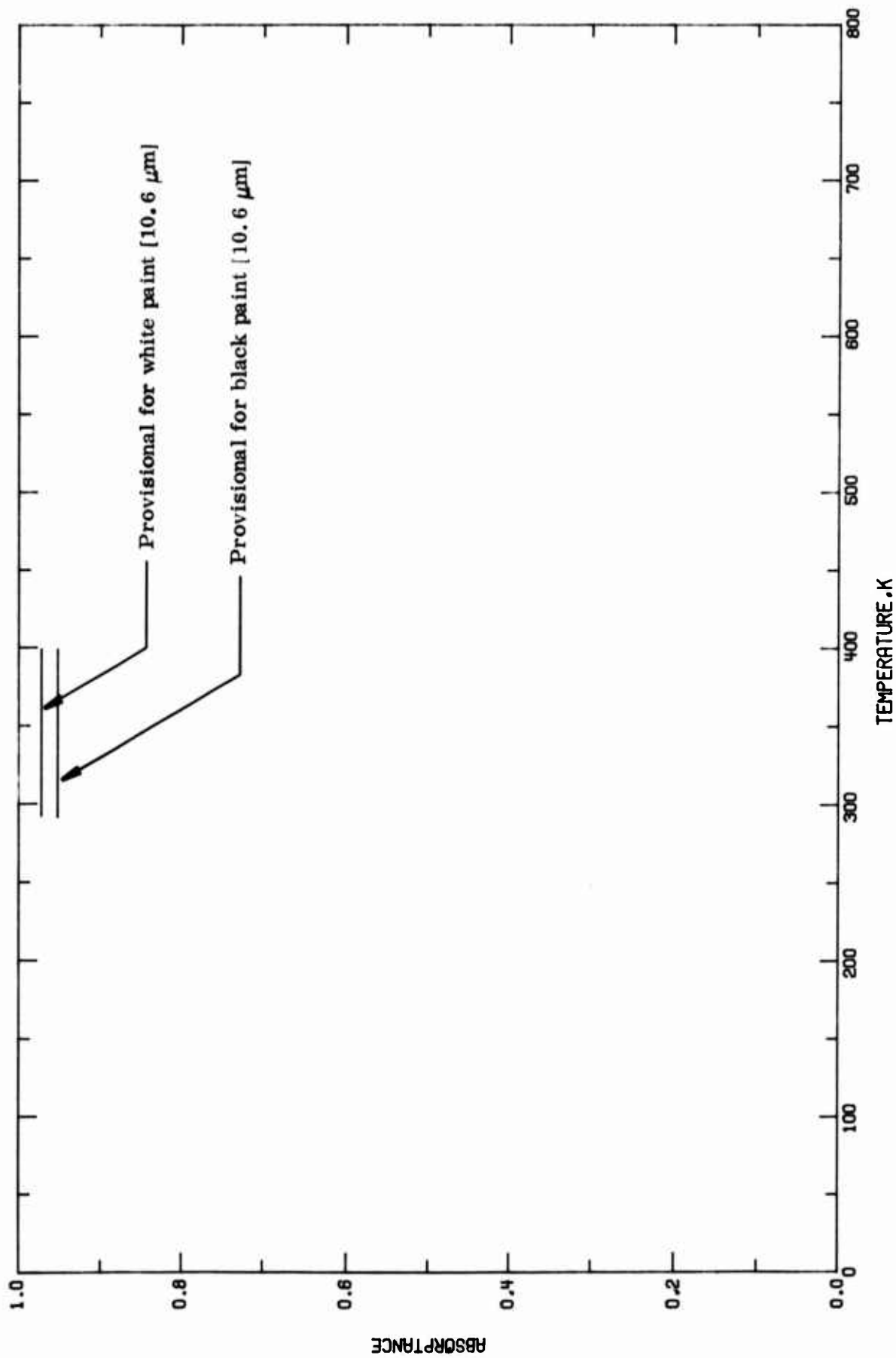


FIGURE 15-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ACRYLIC RESIN COATING
(TEMPERATURE DEPENDENCE)

e. Normal Spectral Transmittance (Wavelength Dependence)

There are 30 sets of experimental data available for the wavelength dependence of the normal spectral transmittance of acrylic resins as listed in Table 15-12 and shown in Figure 15-8 (bulk materials) and Figure 15-9 (thin films). Specimen characterization and measurement information for the data are given in Table 15-11. There were 20 different kinds of acrylic resins used for measurement; their transmittance values were quite different. Therefore, only provisional values are reported here as listed in Table 15-10 and shown in Figure 15-7. The provisional values are for the acrylic sheet with thickness 6.3 mm at 293 K. The estimated uncertainty is within $\pm 30\%$.

708

TABLE 15-10. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ |
|---------------|--------|-----------|--------|
| ACRYLIC SHEET | | | |
| 6.3MM THICK | | | |
| T = 293 | | | |
| 0.42 | 0.82 | 1.50 | 0.61 |
| 0.43 | 0.81 | 1.54 | 0.61 |
| 0.45 | 0.81 | 1.59 | 0.60 |
| 0.47 | 0.80 | 1.62 | 0.59 |
| 0.49 | 0.81 | 1.64 | 0.59 |
| 0.50 | 0.83 | 1.70 | 0.54 |
| 0.51 | 0.83 | 1.74 | 0.50 |
| 0.62 | 0.83 | 1.76 | 0.48 |
| 0.64 | 0.84 | 1.79 | 0.46 |
| 0.64 | 0.85 | 1.81 | 0.45 |
| 0.66 | 0.86 | 1.84 | 0.45 |
| 0.68 | 0.88 | 1.85 | 0.49 |
| 0.69 | 0.90 | 1.87 | 0.47 |
| 0.71 | 0.92 | 1.89 | 0.49 |
| 0.72 | 0.92 | 1.91 | 0.51 |
| 0.75 | 0.92 | 1.91 | 0.53 |
| 0.77 | 0.92 | 1.92 | 0.57 |
| 0.81 | 0.91 | 1.94 | 0.63 |
| 0.84 | 0.90 | 1.95 | 0.68 |
| 0.88 | 0.89 | 1.96 | 0.71 |
| 0.91 | 0.88 | 1.97 | 0.73 |
| 0.94 | 0.88 | 1.98 | 0.76 |
| 0.99 | 0.89 | 2.00 | 0.77 |
| 1.05 | 0.89 | 2.01 | 0.79 |
| 1.07 | 0.90 | 2.03 | 0.80 |
| 1.10 | 0.90 | 2.05 | 0.80 |
| 1.13 | 0.89 | 2.09 | 0.81 |
| 1.17 | 0.89 | 2.16 | 0.82 |
| 1.20 | 0.88 | 2.31 | 0.82 |
| 1.22 | 0.87 | 2.51 | 0.83 |
| 1.24 | 0.86 | | |
| 1.26 | 0.84 | | |
| 1.29 | 0.82 | | |
| 1.32 | 0.75 | | |
| 1.35 | 0.71 | | |
| 1.39 | 0.66 | | |
| 1.41 | 0.64 | | |
| 1.43 | 0.63 | | |
| 1.46 | 0.62 | | |

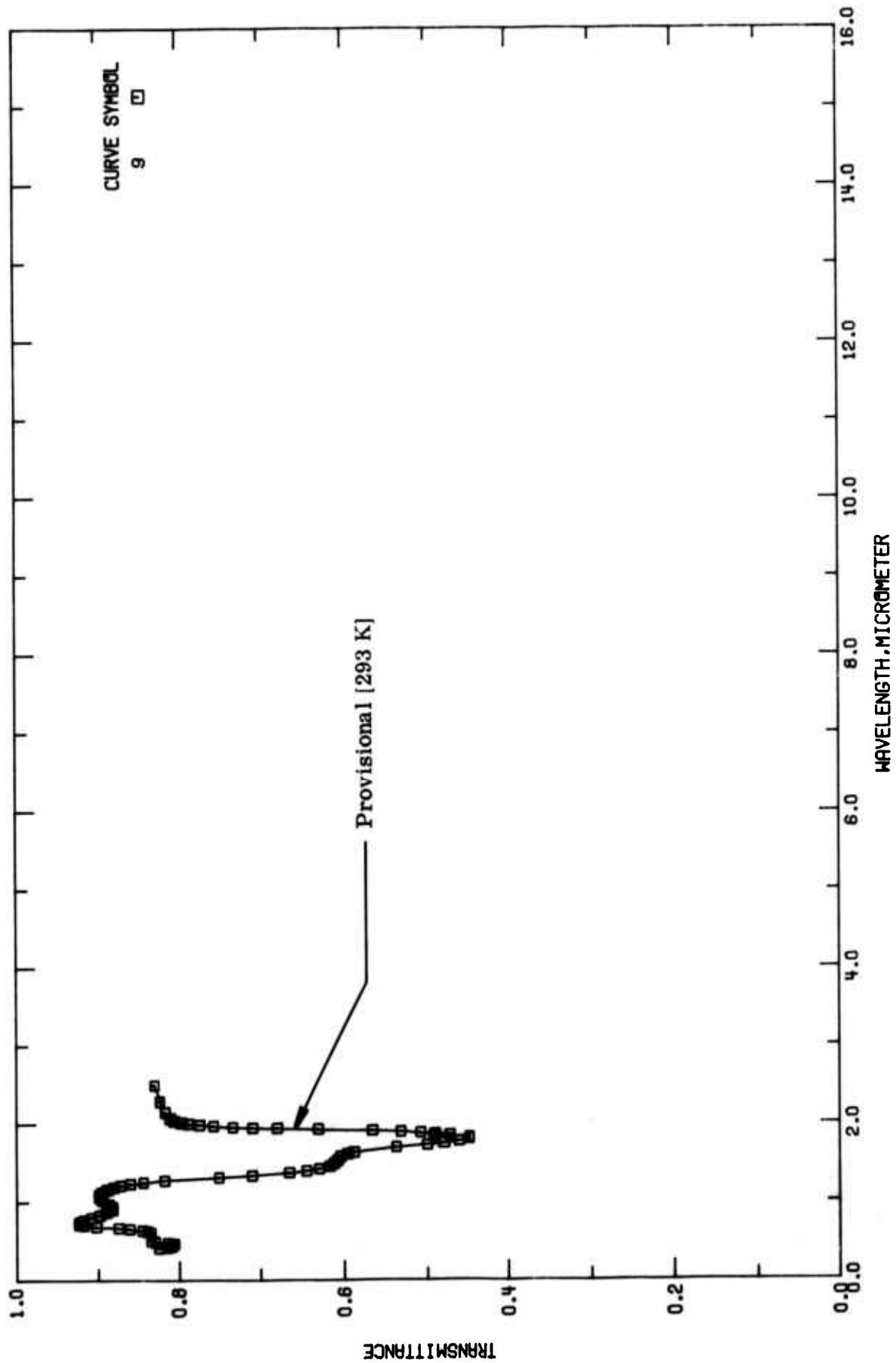


FIGURE 15-8. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE).

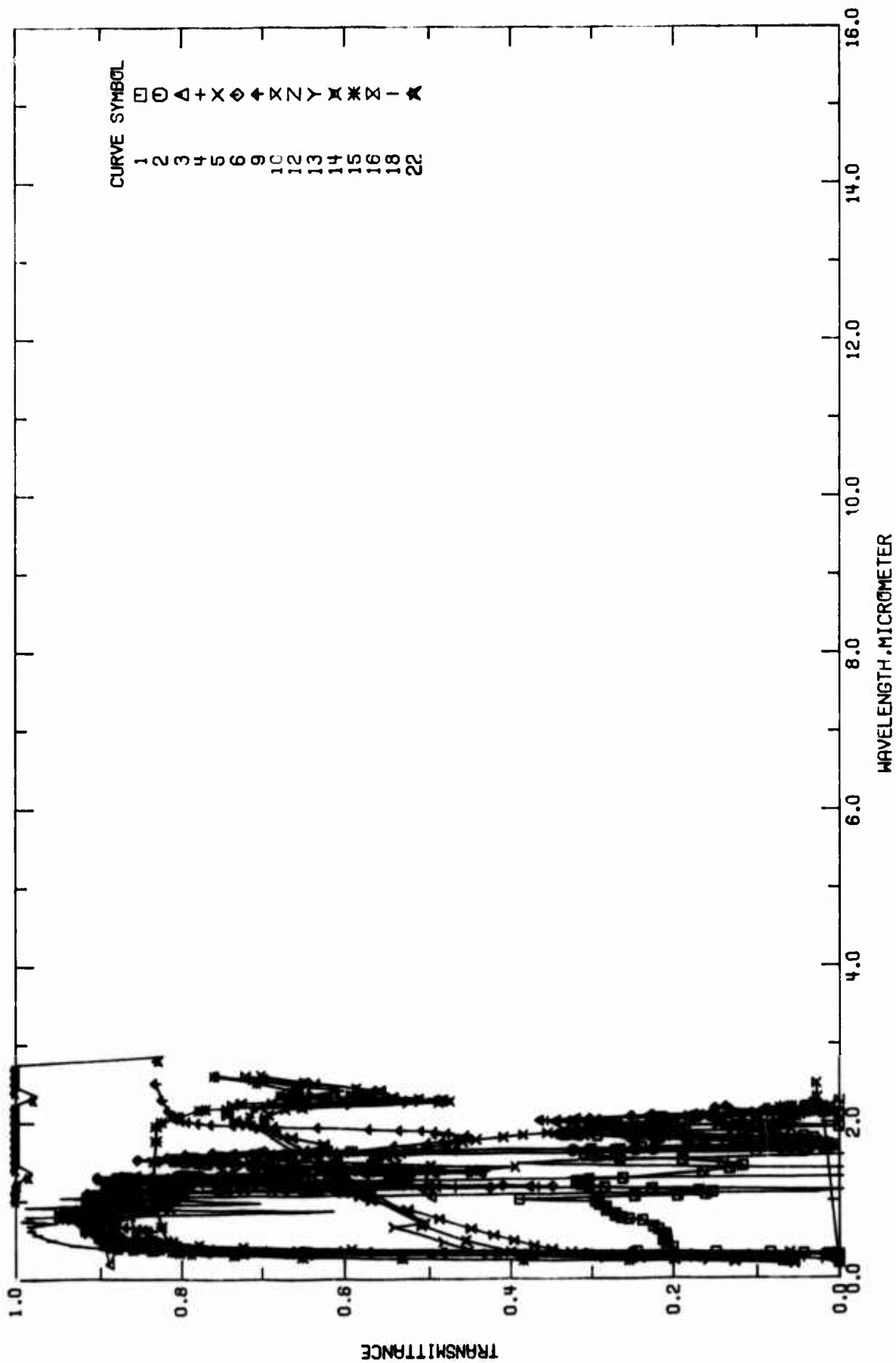


FIGURE 15-9. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE).

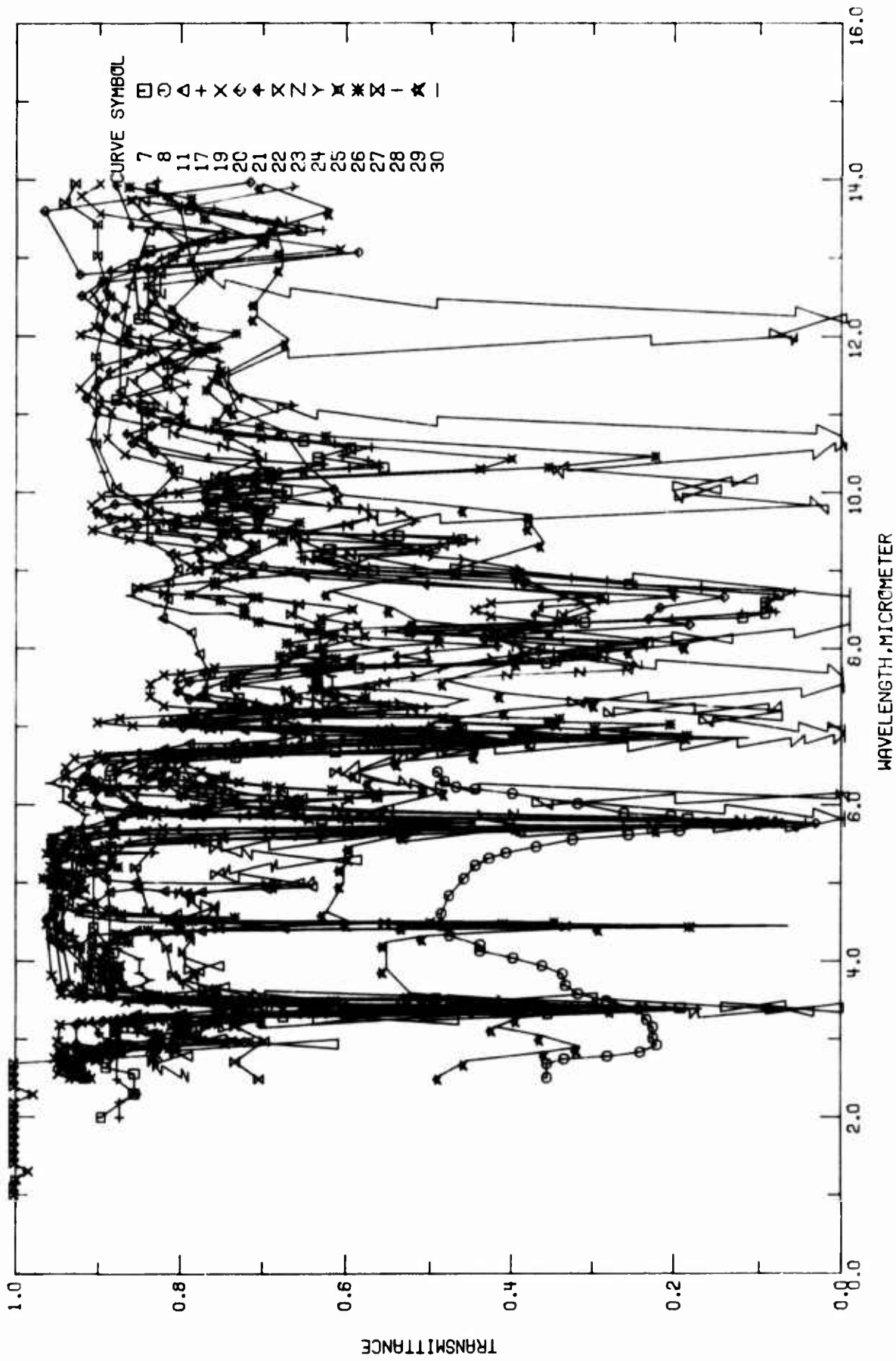


FIGURE 15-10. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC THIN FILMS (WAVELENGTH DEPENDENCE).

TABLE 15-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESINS (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|---|--|
| 1 T40338 | Acitelli, M.A., Cumbby, W.L., and Naujokas, A.A. | 1966 | 0.2-2.2 | 298 | Poly (Allyl-methacrylate) | 7.13 mm thickness; measurements were determined by Cary Spectrophotometer Model 14; the sample used was disc approx. 50 mm in diameter. |
| 2 T40338 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 298 | Poly (Allyl-methacrylate) | The above specimen; after 100 standard fade hours of solarization. |
| 3 T40338 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 298 | Poly (isobutyl methacrylate) | 6.67 mm thickness; measurements were determined by Cary Spectrophotometer Model 14; the sample used was disc approx. 50 mm in diameter. |
| 4 T40338 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 298 | Poly (isobutyl methacrylate) | The above specimen; after 100 standard fade hours of solarization. |
| 5 T40338 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 298 | Poly (ethylene glycol dimethacrylate) | 6.95 mm thick disc approx. 50 mm in diameter; Cary Spectrophotometer Model 14 was employed. |
| 6 T40338 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 298 | Poly (cyclohexyl methacrylate) | 6.75 mm thick disc specimen approx. 50 mm in diameter; Cary Spectrophotometer was employed. |
| 7 T19914 | Moore, L.E., Prasteln, M., Tompkins, E.H., and Van Ostenburg, D.O. | 1958 | 2-15.0 | 293 | Poly-n-butyl methacrylate | Refractive index 1.48 at $\lambda = 5893 \text{ \AA}$; unknown thickness. |
| 8 T34840 | Boyer-Kawenoki, F. | 1966 | 2.5-6.5 | 293 | Polyacrylic Acid | Specimen was obtained by making pellets with KBr and measured by Perkin-Elmer spectrometer; unfractionated polymer with molecular weight 25000 determined by viscosymetric technique. |
| 9 T47094 | Holland, W.R. | 1967 | 0.2-2.6 | 293 | Acrylic Sheets | 0.25 in. thick sheets; Perkin-Elmer Model 99 monochromometer was used. |
| 10 T47094 | Holland, W.R. | 1967 | 0.2-2.6 | 293 | Acrylic Sheets | Similar to the above specimen. |
| 11 T49135 | Hirai, T. and Nakada, O. | 1968 | 2.5-16 | ~293 | Polyacrylonitrile (PAN) | Thin film was formed on a rock salt crystal plate (30 mm diameter and 2 mm thick); infrared spectra was measured by using a Hitachi E.P-2 infrared spectrometer; data were extracted from figure; $\theta \sim 0^\circ$. |
| 12 T64206 | Pemington, C.W. and Moore, G.L. | 1971 | 0.4-2.6 | ~293 | Acrylic Panel | Reflective type acrylic panel; transmittance spectra was obtained by using a DK-2 spectrometer; data were extracted from figure; $\theta \sim 0^\circ$. |
| 13 T62397 | Gilligan, J.E. and Brzuskiwicz, J. | 1971 | 0.2-2.6 | ~293 | DuPont Evacite 6011 (methyl-methacrylate) | 0.015 in. thick sprayed film; Beckman DK-2 spectrometer was used; data were extracted from figure |
| 14 T62397 | Gilligan, J.E. and Brzuskiwicz, J. | 1971 | 0.2-2.6 | ~293 | DuPont Evacite 6011 (methyl-methacrylate) | Similar to the above specimen except 0.032 in. thick. |
| 15 T62397 | Gilligan, J.E. and Brzuskiwicz, J. | 1971 | 0.2-2.6 | ~293 | DuPont Evacite 6011 (methyl-methacrylate) | Similar to the above specimen except 0.054 in. thick. |
| 16 T62397 | Gilligan, J.E. and Brzuskiwicz, J. | 1971 | 0.2-2.6 | ~293 | DuPont Evacite 6011 (methyl-methacrylate) | 0.035 in. thick film was obtained by a doctor blade technique; Beckman DK-2 spectrometer was used; data were extracted from figure. |
| 17 T76312 | Kagarise, R.E. and Wetzelger, L.A. | 1954 | 2-15 | ~293 | Hypalon P-4 | The specimen was obtained from DuPont Co.; dissolved in C_6H_6 and the resulting viscous solution was spread uniformly over a rock salt on KBr plate; the solvent was removed by heating in vacuum on normal evaporation at room temperature; a Perkin-Elmer Model 21 double beam spectrophotometer was used; data were extracted from figure. |

TABLE 15-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESINS (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|---|--|
| 18 T39490 | Cobble, M. H., Fang, P. C., and Lumsdaine, E. | 1966 | 0.3-1.6 | ~293 | Methyl Methacrylate | The transmission spectra of the 2.5 in. slab of methyl methacrylate plastic is determined using a Beckman spectrometer; data were corrected for surface reflectance; data were extracted from figure; $\theta \sim 0^\circ$. |
| 19 T76795 | Skimler, S. S. and Kagarise, R. E. | 1966 | 2.5-25 | ~293 | Zerlon-150 (Methyl methacrylate- α - styrene copolymer) | Film specimen was obtained from Dow Chemical; a Beckman IR-12 spectrophotometer was used to obtain spectra; data were extracted from figure; $\theta \sim 0^\circ$. |
| 20 T76795 | Skimler, S. S. and Kagarise, R. E. | 1966 | 2.5-25 | ~293 | Davick 11-X-1 (Methyl methacrylate- α - methylstyrene copolymer) | Film specimen was obtained from J. T. Baker Chemical Co.; other specifications similar to the above. |
| 21 T76795 | Skimler, S. S. and Kagarise, R. E. | 1966 | 2.5-25 | ~293 | Implax | Film specimen was obtained from Rohm and Haas Co.; other specifications similar to the above. |
| 22 T68740 | Janardhanan, K. K., Ramakrishnan, P. K., Rao, H. N. V., Subramanian, V., and Suryanarayana, C. V. | 1972 | 1.0-2.8 | ~293 | Perspex in methyl methacrylate | The transmission was studied by using a Carl Zeiss SPM-2 monochromator; $\theta \sim 0^\circ$. |
| 23 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~293 | Acrylic, Lacquer Erolite MIL-L-61352 (Andrew Brown Co.) | The specimen was condensed pyrolyzite on potassium bromide on sodium chloride; a Beckman IR-9 double beam, prism-grating infrared spectrophotometer was used to obtain the spectra; data were extracted from figure; $\theta \sim 0^\circ$. |
| 24 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~293 | Acrylic LATEX Spred House Paint (The Glidden Co.) | Similar to the above specimen. |
| 25 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~293 | Orlon (Polyacrylonitrile) | Similar to the above specimen. |
| 26 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~293 | Orlon (Polyacrylonitrile) | Similar to the above specimen. |
| 27 T77043 | Baetonu, P. | 1969 | 2.5-15 | ~293 | Orlon 42 | No details given; data were extracted from figure; $\theta \sim 0^\circ$. |
| 28 T77043 | Baetonu, P. | 1969 | 2.5-15 | ~293 | (Polyacrylonitrile) | Similar to the above specimen. |
| 29 T77043 | Baetonu, P. | 1969 | 2.5-15 | ~293 | Creolan | Similar to the above specimen. |
| 30 E26638 | Carbajal, B. G. III | 1966 | 2.5-25 | ~293 | MMA | Methylmethacrylate; data were extracted from the figure; $\theta \sim 0^\circ$. |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| CURVE 1 | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 2 (CONT.) | |
|-----------|-------|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 0.394 | 0.200 | 1.567 | 0.292 | 0.695 | 0.912 | 1.329 | 0.797 | 1.870 | 0.332 | 0.366 | 0.721 |
| 0.400 | 0.207 | 1.596 | 0.308 | 0.803 | 0.928 | 1.352 | 0.610 | 1.631 | 0.303 | 0.378 | 0.770 |
| 0.470 | 0.207 | 1.641 | 0.364 | 0.842 | 0.928 | 1.351 | 0.602 | 1.694 | 0.197 | 0.387 | 0.805 |
| 0.490 | 0.211 | 1.678 | 0.238 | 0.869 | 0.899 | 1.366 | 0.545 | 1.902 | 0.165 | 0.395 | 0.827 |
| 0.515 | 0.211 | 1.702 | 0.122 | 0.887 | 0.899 | 1.387 | 0.544 | 1.919 | 0.214 | 0.410 | 0.842 |
| 0.537 | 0.208 | 1.738 | 0.069 | 0.901 | 0.891 | 1.399 | 0.528 | 1.925 | 0.257 | 0.435 | 0.853 |
| 0.570 | 0.203 | 1.765 | 0.041 | 0.919 | 0.901 | 1.405 | 0.569 | 1.932 | 0.267 | 0.474 | 0.855 |
| 0.627 | 0.217 | 1.793 | 0.032 | 0.936 | 0.911 | 1.416 | 0.553 | 1.944 | 0.257 | 0.534 | 0.880 |
| 0.665 | 0.223 | 1.820 | 0.045 | 0.963 | 0.915 | 1.426 | 0.583 | 1.954 | 0.212 | 0.557 | 0.870 |
| 0.745 | 0.236 | 1.842 | 0.079 | 1.004 | 0.895 | 1.435 | 0.583 | 1.963 | 0.217 | 0.557 | 0.886 |
| 0.766 | 0.253 | 1.871 | 0.100 | 1.036 | 0.895 | 1.435 | 0.583 | 1.963 | 0.267 | 0.649 | 0.895 |
| 0.780 | 0.262 | 1.901 | 0.117 | 1.058 | 0.907 | 1.457 | 0.660 | 1.972 | 0.288 | 0.745 | 0.906 |
| 0.804 | 0.270 | 1.928 | 0.109 | 1.080 | 0.907 | 1.467 | 0.712 | 1.978 | 0.302 | 0.797 | 0.915 |
| 0.830 | 0.269 | 1.941 | 0.000 | 1.091 | 0.883 | 1.486 | 0.764 | 1.988 | 0.289 | 0.841 | 0.915 |
| 0.873 | 0.281 | 1.991 | 0.100 | 1.100 | 0.886 | 1.509 | 0.793 | 1.995 | 0.237 | 0.857 | 0.911 |
| 0.914 | 0.281 | 1.991 | 0.135 | 1.110 | 0.795 | 1.524 | 0.808 | 2.001 | 0.211 | 0.865 | 0.889 |
| 0.949 | 0.290 | 2.051 | 0.145 | 1.118 | 0.818 | 1.540 | 0.808 | 2.014 | 0.223 | 0.880 | 0.891 |
| 0.986 | 0.295 | 2.175 | 0.123 | 1.136 | 0.603 | 1.559 | 0.784 | 2.022 | 0.204 | 0.895 | 0.881 |
| 1.021 | 0.338 | 2.143 | 0.039 | 1.140 | 0.594 | 1.568 | 0.745 | 2.032 | 0.191 | 0.909 | 0.881 |
| 1.045 | 0.293 | 2.188 | 0.020 | 1.148 | 0.594 | 1.577 | 0.751 | 2.047 | 0.215 | 0.926 | 0.898 |
| 1.059 | 0.245 | 0.200 | 0.000 | 1.153 | 0.532 | 1.594 | 0.705 | 2.056 | 0.219 | 0.959 | 0.901 |
| 1.059 | 0.194 | 0.292 | 0.000 | 1.159 | 0.646 | 1.601 | 0.652 | 2.069 | 0.172 | 0.965 | 0.894 |
| 1.079 | 0.161 | 0.304 | 0.014 | 1.171 | 0.598 | 1.621 | 0.669 | 2.081 | 0.151 | 0.979 | 0.894 |
| 1.109 | 0.153 | 0.316 | 0.044 | 1.176 | 0.590 | 1.626 | 0.645 | 2.098 | 0.000 | 0.998 | 0.883 |
| 1.127 | 0.169 | 0.326 | 0.084 | 1.186 | 0.614 | 1.629 | 0.665 | 2.114 | 0.000 | 1.016 | 0.883 |
| 1.148 | 0.225 | 0.336 | 0.149 | 1.197 | 0.674 | 1.640 | 0.270 | 2.124 | 0.019 | 1.059 | 0.897 |
| 1.167 | 0.263 | 0.346 | 0.243 | 1.214 | 0.795 | 1.648 | 0.300 | 2.140 | 0.315 | 1.075 | 0.897 |
| 1.189 | 0.303 | 0.346 | 0.644 | 1.223 | 0.840 | 1.665 | 0.040 | 2.150 | 0.022 | 1.080 | 0.894 |
| 1.205 | 0.312 | 0.350 | 0.726 | 1.236 | 0.866 | 1.674 | 0.015 | 2.165 | 0.017 | 1.055 | 0.876 |
| 1.225 | 0.318 | 0.357 | 0.307 | 1.255 | 0.875 | 1.699 | 0.208 | 2.180 | 0.043 | 1.096 | 0.875 |
| 1.250 | 0.318 | 0.377 | 0.832 | 1.263 | 0.892 | 1.712 | 0.051 | 2.180 | 0.043 | 1.137 | 0.835 |
| 1.263 | 0.303 | 0.390 | 0.854 | 1.267 | 0.869 | 1.720 | 0.051 | 2.200 | 0.042 | 1.137 | 0.835 |
| 1.283 | 0.260 | 0.403 | 0.874 | 1.274 | 0.869 | 1.728 | 0.041 | CURVE 2 | | 1.114 | 0.817 |
| 1.365 | 0.164 | 0.418 | 0.884 | 1.279 | 0.849 | 1.744 | 0.049 | T = 296. | | 1.124 | 0.722 |
| 1.410 | 0.132 | 0.444 | 0.694 | 1.284 | 0.857 | 1.755 | 0.116 | 0.200 | 0.000 | 1.133 | 0.635 |
| 1.446 | 0.117 | 0.539 | 0.901 | 1.288 | 0.877 | 1.771 | 0.170 | 0.291 | 0.000 | 1.147 | 0.605 |
| 1.446 | 0.140 | 0.549 | 0.894 | 1.304 | 0.877 | 1.790 | 0.220 | 0.302 | 0.017 | 1.155 | 0.642 |
| 1.521 | 0.188 | 0.558 | 0.901 | 1.311 | 0.865 | 1.807 | 0.245 | 0.322 | 0.017 | 1.163 | 0.608 |
| 1.542 | 0.264 | 0.617 | 0.901 | 1.325 | 0.784 | 1.831 | 0.292 | 0.356 | 0.249 | 1.170 | 0.583 |
| | | | | | | 1.846 | 0.332 | 0.356 | 0.649 | 1.184 | 0.603 |
| | | | | | | | | | | 1.203 | 0.735 |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 3 (CONT.) | | CURVE 3 (CONT.) | | CURVE 4 | |
|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 1.210 | 0.793 | 1.644 | 0.245 | 2.096 | 0.600 | 0.932 | 0.884 | 1.602 | 0.737 | 2.140 | 0.055 | | | | | | |
| 1.220 | 0.931 | 1.650 | 0.223 | 2.110 | 0.000 | 0.951 | 0.888 | 1.611 | 0.707 | 2.151 | 0.075 | | | | | | |
| 1.229 | 0.853 | 1.661 | 0.043 | 2.122 | 0.021 | 0.970 | 0.869 | 1.624 | 0.640 | 2.158 | 0.061 | | | | | | |
| 1.252 | 0.853 | 1.670 | 0.021 | 2.137 | 0.013 | 0.970 | 0.886 | 1.641 | 0.620 | 2.173 | 0.091 | | | | | | |
| 1.259 | 0.324 | 1.680 | 0.017 | 2.148 | 0.021 | 1.003 | 0.857 | 1.664 | 0.185 | 2.200 | 0.064 | | | | | | |
| 1.262 | 0.362 | 1.689 | 0.012 | 2.158 | 0.015 | 1.052 | 0.670 | 1.672 | 0.109 | | | | | | | | |
| 1.269 | 0.355 | 1.697 | 0.022 | 2.167 | 0.029 | 1.082 | 0.883 | 1.678 | 0.036 | | | | | | | | |
| 1.277 | 0.843 | 1.705 | 0.050 | 2.173 | 0.039 | 1.106 | 0.883 | 1.686 | 0.011 | | | | | | | | |
| 1.285 | 0.868 | 1.714 | 0.050 | 2.192 | 0.041 | 1.121 | 0.850 | 1.701 | 0.011 | | | | | | | | |
| 1.299 | 0.358 | 1.726 | 0.042 | | | 1.138 | 0.755 | 1.711 | 0.026 | | | | | | | | |
| 1.303 | 0.853 | 1.738 | 0.053 | | | 1.144 | 0.671 | 1.722 | 0.026 | | | | | | | | |
| 1.313 | 0.805 | 1.756 | 0.135 | | | 1.155 | 0.650 | 1.729 | 0.021 | | | | | | | | |
| 1.319 | 0.773 | 1.772 | 0.183 | | | 1.183 | 0.376 | 1.748 | 0.059 | | | | | | | | |
| 1.325 | 0.793 | 1.787 | 0.215 | | | 1.209 | 0.691 | 1.763 | 0.054 | | | | | | | | |
| 1.347 | 0.508 | 1.807 | 0.250 | | | 1.218 | 0.787 | 1.774 | 0.162 | | | | | | | | |
| 1.356 | 0.593 | 1.826 | 0.292 | | | 1.223 | 0.787 | 1.781 | 0.183 | | | | | | | | |
| 1.362 | 0.536 | 1.835 | 0.314 | | | 1.241 | 0.829 | 1.796 | 0.169 | | | | | | | | |
| 1.368 | 0.521 | 1.848 | 0.324 | | | 1.258 | 0.548 | 1.828 | 0.233 | | | | | | | | |
| 1.379 | 0.533 | 1.853 | 0.324 | | | 1.266 | 0.843 | 1.837 | 0.309 | | | | | | | | |
| 1.390 | 0.532 | 1.871 | 0.313 | | | 1.269 | 0.870 | 1.855 | 0.343 | | | | | | | | |
| 1.401 | 0.555 | 1.889 | 0.211 | | | 1.292 | 0.863 | 1.882 | 0.314 | | | | | | | | |
| 1.409 | 0.548 | 1.897 | 0.198 | | | 1.299 | 0.862 | 1.894 | 0.260 | | | | | | | | |
| 1.416 | 0.570 | 1.905 | 0.216 | | | 1.320 | 0.851 | 1.903 | 0.247 | | | | | | | | |
| 1.427 | 0.533 | 1.914 | 0.247 | | | 1.341 | 0.749 | 1.914 | 0.259 | | | | | | | | |
| 1.448 | 0.658 | 1.918 | 0.255 | | | 1.352 | 0.574 | 1.922 | 0.291 | | | | | | | | |
| 1.456 | 0.693 | 1.925 | 0.243 | | | 1.358 | 0.435 | 1.930 | 0.300 | | | | | | | | |
| 1.471 | 0.731 | 1.934 | 0.213 | | | 1.375 | 0.450 | 1.936 | 0.288 | | | | | | | | |
| 1.486 | 0.765 | 1.943 | 0.206 | | | 1.387 | 0.440 | 1.942 | 0.243 | | | | | | | | |
| 1.511 | 0.792 | 1.946 | 0.222 | | | 1.397 | 0.506 | 1.949 | 0.230 | | | | | | | | |
| 1.535 | 0.792 | 1.951 | 0.279 | | | 1.409 | 0.496 | 1.956 | 0.253 | | | | | | | | |
| 1.550 | 0.780 | 1.968 | 0.294 | | | 1.439 | 0.555 | 1.961 | 0.276 | | | | | | | | |
| 1.560 | 0.739 | 1.978 | 0.294 | | | 1.445 | 0.572 | 1.971 | 0.292 | | | | | | | | |
| 1.568 | 0.748 | 1.998 | 0.223 | | | 1.425 | 0.563 | 1.985 | 0.292 | | | | | | | | |
| 1.582 | 0.714 | 2.011 | 0.223 | | | 1.436 | 0.603 | 2.013 | 0.344 | | | | | | | | |
| 1.595 | 0.652 | 2.028 | 0.199 | | | 1.454 | 0.658 | 2.028 | 0.363 | | | | | | | | |
| 1.602 | 0.558 | 2.043 | 0.219 | | | 1.469 | 0.697 | 2.045 | 0.319 | | | | | | | | |
| 1.618 | 0.101 | 2.054 | 0.211 | | | 1.490 | 0.713 | 2.068 | 0.252 | | | | | | | | |
| 1.622 | 0.653 | 2.065 | 0.176 | | | 1.510 | 0.783 | 2.086 | 0.226 | | | | | | | | |
| 1.633 | 0.303 | 2.075 | 0.155 | | | 1.519 | 0.802 | 2.106 | 0.161 | | | | | | | | |
| 1.640 | 0.322 | 2.088 | 0.056 | | | 1.534 | 0.811 | 2.127 | 0.044 | | | | | | | | |

CURVE 3
T = 296.

CURVE 4
T = 296.

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| CURVE 4 (CONT.) | | CURVE 5 | | CURVE 5 (CONT.) | | CURVE 5 (CONT.) | | CURVE 6 | | CURVE 6 (CONT.) | |
|-----------------|-------|-----------|-------|-----------------|-------|-----------------|-------|-----------|-------|-----------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 0.923 | 0.854 | 1.527 | 0.789 | 1.369 | 0.497 | 2.200 | 0.059 | 1.209 | 0.708 | 1.216 | 0.754 |
| 0.946 | 0.864 | 1.538 | 0.789 | 1.386 | 0.000 | CURVE 6 | | 1.228 | 0.812 | 1.228 | 0.812 |
| 0.959 | 0.847 | 1.552 | 0.776 | 1.394 | 0.445 | T = 296. | | 1.243 | 0.859 | 1.243 | 0.859 |
| 0.976 | 0.860 | 1.572 | 0.745 | 1.425 | 0.011 | | | 1.265 | 0.891 | 1.265 | 0.891 |
| 0.991 | 0.845 | 1.599 | 0.712 | 1.451 | 0.497 | | | 1.282 | 0.903 | 1.282 | 0.903 |
| 1.015 | 0.834 | 1.617 | 0.609 | 1.470 | 0.538 | | | 1.309 | 0.933 | 1.309 | 0.933 |
| 1.026 | 0.845 | 1.644 | 0.597 | 1.528 | 0.692 | | | 1.324 | 0.970 | 1.324 | 0.970 |
| 1.056 | 0.847 | 1.667 | 0.156 | 1.577 | 0.677 | | | 1.347 | 0.736 | 1.347 | 0.736 |
| 1.071 | 0.858 | 1.683 | 0.022 | 1.598 | 0.677 | | | 1.358 | 0.616 | 1.358 | 0.616 |
| 1.099 | 0.859 | 1.696 | 0.014 | 1.610 | 0.664 | | | 1.370 | 0.488 | 1.370 | 0.488 |
| 1.114 | 0.846 | 1.708 | 0.029 | 1.620 | 0.613 | | | 1.394 | 0.510 | 1.394 | 0.510 |
| 1.125 | 0.807 | 1.722 | 0.028 | 1.631 | 0.623 | | | 1.429 | 0.525 | 1.429 | 0.525 |
| 1.144 | 0.852 | 1.731 | 0.024 | 1.643 | 0.623 | | | 1.443 | 0.703 | 1.443 | 0.703 |
| 1.154 | 0.815 | 1.750 | 0.059 | 1.647 | 0.588 | | | 1.470 | 0.748 | 1.470 | 0.748 |
| 1.164 | 0.804 | 1.759 | 0.059 | 1.658 | 0.476 | | | 1.475 | 0.775 | 1.475 | 0.775 |
| 1.175 | 0.465 | 1.771 | 0.119 | 1.673 | 0.388 | | | 1.512 | 0.781 | 1.512 | 0.781 |
| 1.180 | 0.363 | 1.790 | 0.179 | 1.683 | 0.388 | | | 1.536 | 0.849 | 1.536 | 0.849 |
| 1.192 | 0.465 | 1.798 | 0.169 | 1.694 | 0.073 | | | 1.595 | 0.817 | 1.595 | 0.817 |
| 1.205 | 0.653 | 1.829 | 0.249 | 1.696 | 0.042 | | | 1.610 | 0.700 | 1.610 | 0.700 |
| 1.222 | 0.770 | 1.837 | 0.319 | 1.723 | 0.014 | | | 1.637 | 0.695 | 1.637 | 0.695 |
| 1.253 | 0.323 | 1.850 | 0.441 | 1.744 | 0.035 | | | 1.648 | 0.464 | 1.648 | 0.464 |
| 1.266 | 0.347 | 1.876 | 0.329 | 1.768 | 0.075 | | | 1.652 | 0.246 | 1.652 | 0.246 |
| 1.286 | 0.835 | 1.899 | 0.258 | 1.798 | 0.065 | | | 1.681 | 0.054 | 1.681 | 0.054 |
| 1.312 | 0.833 | 1.905 | 0.258 | 1.855 | 0.205 | | | 1.693 | 0.013 | 1.693 | 0.013 |
| 1.325 | 0.804 | 1.922 | 0.296 | 1.868 | 0.221 | | | 1.712 | 0.013 | 1.712 | 0.013 |
| 1.347 | 0.667 | 1.947 | 0.235 | 1.885 | 0.189 | | | 1.723 | 0.122 | 1.723 | 0.122 |
| 1.352 | 0.577 | 1.967 | 0.290 | 1.902 | 0.032 | | | 1.735 | 0.014 | 1.735 | 0.014 |
| 1.359 | 0.450 | 1.983 | 0.250 | 1.911 | 0.060 | | | 1.749 | 0.024 | 1.749 | 0.024 |
| 1.366 | 0.433 | 2.015 | 0.337 | 1.931 | 0.125 | | | 1.762 | 0.077 | 1.762 | 0.077 |
| 1.375 | 0.448 | 2.026 | 0.352 | 1.949 | 0.120 | | | 1.768 | 0.366 | 1.768 | 0.366 |
| 1.384 | 0.430 | 2.038 | 0.337 | 1.980 | 0.213 | | | 1.793 | 0.091 | 1.793 | 0.091 |
| 1.390 | 0.480 | 2.067 | 0.249 | 1.994 | 0.225 | | | 1.815 | 0.132 | 1.815 | 0.132 |
| 1.394 | 0.494 | 2.083 | 0.226 | 2.012 | 0.225 | | | | | | |
| 1.401 | 0.486 | 2.100 | 0.130 | 2.050 | 0.120 | | | | | | |
| 1.414 | 0.553 | 2.130 | 0.046 | 2.077 | 0.125 | | | | | | |
| 1.422 | 0.536 | 2.151 | 0.073 | 2.093 | 0.159 | | | | | | |
| 1.467 | 0.596 | 2.163 | 0.037 | 2.111 | 0.069 | | | | | | |
| 1.484 | 0.691 | 2.175 | 0.091 | 2.139 | 0.036 | | | | | | |
| 1.510 | 0.770 | 2.200 | 0.073 | 2.162 | 0.070 | | | | | | |
| | | | | 2.186 | 0.073 | | | | | | |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
(WAVELENGTH, λ, μm; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | CURVE 6 (CONT.) | | CURVE 7 (CONT.) | | CURVE 7 (CONT.) | | CURVE 8 | | CURVE 9 | | CURVE 9 (CONT.) | | |
|-------|-----------------|-------|-----------------|-------|-----------------|-------|---------|-------|---------|-------|-----------------|-------|--|
| | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | |
| 1.823 | 0.204 | 4.11 | 0.679 | 0.632 | 9.19 | 0.632 | 2.50 | 0.354 | 0.417 | 0.824 | 1.498 | 0.611 | |
| 1.834 | 0.235 | 4.43 | 0.905 | 0.619 | 9.28 | 0.619 | 2.68 | 0.354 | 0.429 | 0.813 | 1.541 | 0.607 | |
| 1.845 | 0.259 | 5.30 | 0.505 | 0.517 | 9.28 | 0.517 | 2.68 | 0.333 | 0.446 | 0.808 | 1.589 | 0.603 | |
| 1.861 | 0.259 | 5.47 | 0.882 | 0.459 | 9.40 | 0.459 | 2.74 | 0.291 | 0.475 | 0.305 | 1.622 | 0.595 | |
| 1.885 | 0.221 | 5.56 | 0.767 | 0.536 | 9.45 | 0.536 | 2.73 | 0.240 | 0.487 | 0.312 | 1.642 | 0.588 | |
| 1.902 | 0.234 | 5.67 | 0.388 | 0.732 | 9.50 | 0.732 | 2.83 | 0.219 | 0.499 | 0.828 | 1.704 | 0.533 | |
| 1.922 | 0.234 | 5.77 | 0.099 | 0.808 | 9.60 | 0.808 | 2.92 | 0.224 | 0.513 | 0.834 | 1.737 | 0.499 | |
| 1.949 | 0.206 | 5.94 | 0.194 | 0.780 | 9.65 | 0.780 | 3.01 | 0.224 | 0.513 | 0.834 | 1.759 | 0.430 | |
| 1.992 | 0.296 | 5.82 | 0.627 | 0.703 | 9.71 | 0.703 | 3.15 | 0.224 | 0.619 | 0.834 | 1.786 | 0.462 | |
| 1.996 | 0.318 | 5.90 | 0.782 | 0.691 | 9.79 | 0.691 | 3.25 | 0.232 | 0.635 | 0.839 | 1.815 | 0.443 | |
| 2.013 | 0.326 | 5.98 | 0.852 | 0.759 | 9.84 | 0.759 | 3.39 | 0.242 | 0.645 | 0.846 | 1.835 | 0.449 | |
| 2.029 | 0.290 | 5.19 | 0.884 | 0.759 | 9.93 | 0.759 | 3.49 | 0.292 | 0.661 | 0.862 | 1.851 | 0.491 | |
| 2.045 | 0.302 | 6.39 | 0.834 | 0.669 | 10.03 | 0.669 | 3.58 | 0.316 | 0.675 | 0.875 | 1.865 | 0.473 | |
| 2.063 | 0.250 | 6.54 | 0.845 | 0.747 | 10.12 | 0.747 | 3.69 | 0.331 | 0.694 | 0.901 | 1.879 | 0.490 | |
| 2.085 | 0.171 | 6.62 | 0.731 | 0.747 | 10.20 | 0.747 | 3.84 | 0.335 | 0.710 | 0.916 | 1.892 | 0.507 | |
| 2.119 | 0.105 | 6.69 | 0.611 | 0.690 | 10.27 | 0.690 | 3.94 | 0.350 | 0.724 | 0.923 | 1.905 | 0.532 | |
| 2.131 | 0.055 | 6.79 | 0.376 | 0.553 | 10.33 | 0.553 | 4.04 | 0.397 | 0.754 | 0.923 | 1.920 | 0.567 | |
| 2.163 | 0.132 | 6.87 | 0.449 | 0.632 | 10.46 | 0.632 | 4.13 | 0.435 | 0.774 | 0.917 | 1.943 | 0.630 | |
| 2.185 | 0.150 | 6.90 | 0.632 | 0.593 | 10.58 | 0.593 | 4.21 | 0.436 | 0.807 | 0.907 | 1.954 | 0.679 | |
| 2.200 | 0.137 | 7.02 | 0.760 | 0.649 | 10.67 | 0.649 | 4.33 | 0.474 | 0.841 | 0.897 | 1.962 | 0.709 | |
| | | 7.20 | 0.606 | 0.740 | 10.75 | 0.740 | 4.46 | 0.485 | 0.878 | 0.889 | 1.970 | 0.733 | |
| | | 7.22 | 0.667 | 0.818 | 10.91 | 0.818 | 4.51 | 0.485 | 0.912 | 0.883 | 1.985 | 0.758 | |
| | | 7.37 | 0.727 | 0.646 | 11.10 | 0.646 | 4.84 | 0.475 | 0.941 | 0.833 | 2.000 | 0.775 | |
| | | 7.53 | 0.743 | 0.877 | 11.20 | 0.877 | 5.06 | 0.442 | 0.980 | 0.887 | 2.014 | 0.736 | |
| | | 7.76 | 0.583 | 0.816 | 11.41 | 0.816 | 5.23 | 0.426 | 1.034 | 0.894 | 2.029 | 0.795 | |
| | | 8.03 | 0.353 | 0.816 | 11.66 | 0.816 | 5.32 | 0.406 | 1.070 | 0.897 | 2.051 | 0.854 | |
| | 0.895 | 8.37 | 0.760 | 0.760 | 11.87 | 0.760 | 5.39 | 0.406 | 1.105 | 0.997 | 2.086 | 0.809 | |
| 2.30 | 0.955 | 12.24 | 0.850 | 0.850 | 12.24 | 0.850 | 5.47 | 0.356 | 1.133 | 0.894 | 2.086 | 0.809 | |
| 2.55 | 0.855 | 12.93 | 0.856 | 0.856 | 12.93 | 0.856 | 5.56 | 0.323 | 1.169 | 0.883 | 2.163 | 0.815 | |
| 2.64 | 0.869 | 13.11 | 0.938 | 0.938 | 13.11 | 0.938 | 5.62 | 0.255 | 1.195 | 0.863 | 2.305 | 0.822 | |
| 2.92 | 0.864 | 13.27 | 0.836 | 0.836 | 13.27 | 0.836 | 5.67 | 0.193 | 1.219 | 0.873 | 2.510 | 0.829 | |
| 3.05 | 0.878 | 13.37 | 0.749 | 0.749 | 13.37 | 0.749 | 5.77 | 0.162 | 1.242 | 0.861 | | | |
| 3.14 | 0.878 | 13.64 | 0.309 | 0.652 | 13.64 | 0.652 | 5.86 | 0.203 | 1.262 | 0.844 | | | |
| 3.23 | 0.863 | 13.91 | 0.788 | 0.788 | 13.91 | 0.788 | 5.90 | 0.261 | 1.286 | 0.816 | | | |
| 3.29 | 0.799 | 14.16 | 0.836 | 0.836 | 14.16 | 0.836 | 6.02 | 0.317 | 1.322 | 0.751 | | | |
| 3.29 | 0.673 | 14.50 | 0.812 | 0.812 | 14.50 | 0.812 | 6.15 | 0.398 | 1.349 | 0.709 | | | |
| 3.40 | 0.192 | 14.63 | 0.819 | 0.819 | 14.63 | 0.819 | 6.21 | 0.442 | 1.361 | 0.665 | | | |
| 3.45 | 0.407 | 14.79 | 0.802 | 0.802 | 14.79 | 0.802 | 6.24 | 0.466 | 1.406 | 0.644 | | | |
| 3.52 | 0.491 | 15.00 | 0.824 | 0.824 | 15.00 | 0.824 | 6.31 | 0.481 | 1.430 | 0.629 | | | |
| 3.52 | 0.837 | | 0.467 | | | 0.467 | 6.43 | 0.490 | 1.463 | 0.616 | | | |
| 3.78 | 0.879 | | 0.566 | | | 0.566 | | | | | | | |
| | | | | | | | | | | | | | |

CURVE 10
T = 293.
0.412 0.830
0.429 0.840
0.455 0.856
0.471 0.870
0.482 0.882
0.498 0.891

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 11 (CONT.) | | CURVE 11 (CONT.) | | CURVE 11 (CONT.) | | CURVE 12 | | CURVE 12 (CONT.) | |
|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|-----------|-------|------------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 0.516 | 0.898 | 1.350 | 0.606 | 2.88 | 0.903 | 5.95 | 0.769 | 0.394 | 0.200 | 1.596 | 0.306 | 1.596 | 0.306 | 1.596 | 0.306 |
| 0.554 | 0.898 | 1.385 | 0.590 | 2.95 | 0.876 | 6.01 | 0.730 | 0.400 | 0.207 | 1.641 | 0.310 | 1.641 | 0.310 | 1.641 | 0.310 |
| 0.566 | 0.901 | 1.404 | 0.582 | 2.98 | 0.834 | 6.11 | 0.695 | 0.470 | 0.207 | 1.675 | 0.264 | 1.675 | 0.264 | 1.675 | 0.264 |
| 0.593 | 0.913 | 1.422 | 0.577 | 3.07 | 0.834 | 6.25 | 0.760 | 0.490 | 0.211 | 1.702 | 0.236 | 1.702 | 0.236 | 1.702 | 0.236 |
| 0.614 | 0.917 | 1.446 | 0.570 | 3.11 | 0.878 | 6.34 | 0.785 | 0.515 | 0.211 | 1.738 | 0.222 | 1.738 | 0.222 | 1.738 | 0.222 |
| 0.629 | 0.917 | 1.476 | 0.565 | 3.22 | 0.878 | 6.60 | 0.799 | 0.537 | 0.208 | 1.756 | 0.069 | 1.756 | 0.069 | 1.756 | 0.069 |
| 0.645 | 0.912 | 1.511 | 0.562 | 3.32 | 0.853 | 6.65 | 0.919 | 0.515 | 0.208 | 1.756 | 0.041 | 1.756 | 0.041 | 1.756 | 0.041 |
| 0.672 | 0.910 | 1.573 | 0.549 | 3.33 | 0.796 | 6.72 | 0.820 | 0.570 | 0.239 | 1.795 | 0.032 | 1.795 | 0.032 | 1.795 | 0.032 |
| 0.696 | 0.851 | 1.595 | 0.541 | 3.38 | 0.751 | 6.80 | 0.787 | 0.627 | 0.217 | 1.820 | 0.045 | 1.820 | 0.045 | 1.820 | 0.045 |
| 0.707 | 0.879 | 1.614 | 0.533 | 3.42 | 0.698 | 6.80 | 0.733 | 0.665 | 0.223 | 1.845 | 0.079 | 1.845 | 0.079 | 1.845 | 0.079 |
| 0.726 | 0.879 | 1.645 | 0.521 | 3.42 | 0.755 | 6.84 | 0.676 | 0.745 | 0.236 | 1.871 | 0.100 | 1.871 | 0.100 | 1.871 | 0.100 |
| 0.737 | 0.883 | 1.682 | 0.532 | 3.47 | 0.815 | 6.90 | 0.552 | 0.766 | 0.253 | 1.901 | 0.117 | 1.901 | 0.117 | 1.901 | 0.117 |
| 0.748 | 0.889 | 1.722 | 0.478 | 3.54 | 0.886 | 6.94 | 0.675 | 0.760 | 0.262 | 1.928 | 0.109 | 1.928 | 0.109 | 1.928 | 0.109 |
| 0.757 | 0.889 | 1.758 | 0.456 | 3.62 | 0.901 | 6.97 | 0.721 | 0.804 | 0.270 | 1.941 | 0.080 | 1.941 | 0.080 | 1.941 | 0.080 |
| 0.765 | 0.924 | 1.783 | 0.456 | 3.82 | 0.909 | 7.05 | 0.752 | 0.830 | 0.269 | 1.991 | 0.100 | 1.991 | 0.100 | 1.991 | 0.100 |
| 0.775 | 0.931 | 1.816 | 0.458 | 3.94 | 0.914 | 7.17 | 0.766 | 0.873 | 0.281 | 1.991 | 0.135 | 1.991 | 0.135 | 1.991 | 0.135 |
| 0.783 | 0.937 | 1.841 | 0.393 | 4.18 | 0.926 | 7.28 | 0.747 | 0.914 | 0.281 | 2.051 | 0.145 | 2.051 | 0.145 | 2.051 | 0.145 |
| 0.796 | 0.942 | 1.867 | 0.352 | 4.33 | 0.908 | 7.42 | 0.773 | 0.949 | 0.290 | 2.075 | 0.123 | 2.075 | 0.123 | 2.075 | 0.123 |
| 0.807 | 0.945 | 1.901 | 0.299 | 4.40 | 0.853 | 7.59 | 0.762 | 0.986 | 0.295 | 2.143 | 0.039 | 2.143 | 0.039 | 2.143 | 0.039 |
| 0.833 | 0.945 | 1.932 | 0.233 | 4.40 | 0.772 | 7.94 | 0.775 | 1.043 | 0.293 | 2.189 | 0.020 | 2.189 | 0.020 | 2.189 | 0.020 |
| 0.851 | 0.945 | 1.969 | 0.146 | 4.43 | 0.772 | 8.22 | 0.735 | 1.059 | 0.246 | 2.275 | 0.000 | 2.275 | 0.000 | 2.275 | 0.000 |
| 0.870 | 0.931 | 1.986 | 0.109 | 4.52 | 0.762 | 8.40 | 0.822 | 1.079 | 0.194 | | | | | | |
| 0.884 | 0.932 | 1.996 | 0.092 | 4.53 | 0.807 | 8.54 | 0.815 | 1.079 | 0.161 | | | | | | |
| 0.905 | 0.937 | 2.010 | 0.077 | 4.64 | 0.830 | 8.67 | 0.814 | 1.109 | 0.153 | | | | | | |
| 0.922 | 0.940 | 2.023 | 0.066 | 4.74 | 0.805 | 9.03 | 0.802 | 1.127 | 0.169 | | | | | | |
| 0.942 | 0.943 | 2.043 | 0.060 | 4.90 | 0.884 | 9.23 | 0.812 | 1.148 | 0.225 | | | | | | |
| 0.969 | 0.945 | 2.066 | 0.054 | 4.94 | 0.884 | 9.39 | 0.840 | 1.170 | 0.283 | | | | | | |
| 0.997 | 0.885 | 2.097 | 0.049 | 4.90 | 0.819 | 9.88 | 0.840 | 1.199 | 0.303 | | | | | | |
| 1.030 | 0.875 | 2.130 | 0.043 | 4.88 | 0.790 | 10.31 | 0.822 | 1.205 | 0.312 | | | | | | |
| 1.087 | 0.869 | 2.172 | 0.037 | 4.90 | 0.772 | 10.73 | 0.847 | 1.225 | 0.318 | | | | | | |
| 1.131 | 0.859 | 2.245 | 0.031 | 4.94 | 0.693 | 11.35 | 0.847 | 1.250 | 0.316 | | | | | | |
| 1.212 | 0.854 | 2.322 | 0.027 | 4.96 | 0.638 | 11.31 | 0.872 | 1.268 | 0.303 | | | | | | |
| 1.232 | 0.859 | 2.500 | 0.028 | 5.00 | 0.682 | 11.95 | 0.872 | 1.283 | 0.260 | | | | | | |
| 1.245 | 0.851 | | | 5.02 | 0.689 | 12.66 | 0.861 | 1.365 | 0.164 | | | | | | |
| 1.254 | 0.839 | | | 5.05 | 0.689 | 13.37 | 0.839 | 1.410 | 0.132 | | | | | | |
| 1.276 | 0.700 | | | 5.14 | 0.607 | 14.41 | 0.846 | 1.446 | 0.117 | | | | | | |
| 1.290 | 0.671 | | | 5.27 | 0.507 | 15.60 | 0.821 | 1.466 | 0.140 | | | | | | |
| 1.311 | 0.670 | | | 5.71 | 0.523 | | | 1.486 | 0.188 | | | | | | |
| 1.333 | 0.638 | | | 5.87 | 0.671 | | | 1.542 | 0.264 | | | | | | |
| 1.345 | 0.618 | | | 5.94 | 0.831 | | | 1.567 | 0.292 | | | | | | |

CURVE 13
T = 293.

0.213 0.053
0.231 0.158
0.264 0.283
0.259 0.363
0.306 0.415
0.317 0.427
0.472 0.481
0.668 0.540
0.706 0.509
0.575 0.575
1.362 0.646
1.968 0.709
2.611 0.714
2.077 0.714
2.148 0.710

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 19 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 20 (CONT.) | | | CURVE 21 (CONT.) | | | CURVE 21 (CONT.) | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 23.58 | 0.935 | 5.37 | 0.951 | 8.01 | 0.280 | 14.31 | 0.947 | 3.61 | 0.921 | 7.78 | 0.677 | 7.78 | 0.677 | 7.78 | 0.677 | 7.78 | 0.677 |
| 24.21 | 0.811 | 5.55 | 0.915 | 8.13 | 0.431 | 14.64 | 0.980 | 3.74 | 0.935 | 7.81 | 0.536 | 7.81 | 0.536 | 7.81 | 0.536 | 7.81 | 0.536 |
| 25.00 | 0.776 | 5.63 | 0.683 | 8.19 | 0.412 | 15.65 | 0.975 | 4.18 | 0.943 | 7.65 | 0.499 | 7.65 | 0.499 | 7.65 | 0.499 | 7.65 | 0.499 |
| | | 5.73 | 0.394 | 8.31 | 0.192 | 19.21 | 0.963 | 5.00 | 0.945 | 7.91 | 0.536 | 7.91 | 0.536 | 7.91 | 0.536 | 7.91 | 0.536 |
| | | 5.72 | 0.553 | 8.39 | 0.210 | 19.53 | 0.906 | 5.13 | 0.945 | 7.97 | 0.501 | 7.97 | 0.501 | 7.97 | 0.501 | 7.97 | 0.501 |
| | | 5.77 | 0.029 | 8.53 | 0.216 | 19.92 | 0.906 | 5.26 | 0.952 | 8.04 | 0.415 | 8.04 | 0.415 | 8.04 | 0.415 | 8.04 | 0.415 |
| | | 5.84 | 0.595 | 8.67 | 0.142 | 20.53 | 0.872 | 5.38 | 0.952 | 8.20 | 0.642 | 8.20 | 0.642 | 8.20 | 0.642 | 8.20 | 0.642 |
| | | 5.83 | 0.769 | 8.75 | 0.201 | 20.88 | 0.925 | 5.48 | 0.940 | 8.26 | 0.597 | 8.26 | 0.597 | 8.26 | 0.597 | 8.26 | 0.597 |
| | | 5.95 | 0.662 | 8.98 | 0.594 | 22.03 | 0.930 | 5.59 | 0.917 | 8.35 | 0.318 | 8.35 | 0.318 | 8.35 | 0.318 | 8.35 | 0.318 |
| | | 6.22 | 0.902 | 9.07 | 0.697 | 23.31 | 0.911 | 5.65 | 0.896 | 8.44 | 0.369 | 8.44 | 0.369 | 8.44 | 0.369 | 8.44 | 0.369 |
| | | 6.18 | 0.902 | 9.14 | 0.737 | 23.31 | 0.879 | 5.73 | 0.798 | 8.54 | 0.350 | 8.54 | 0.350 | 8.54 | 0.350 | 8.54 | 0.350 |
| | | 6.21 | 0.686 | 9.32 | 0.748 | 23.92 | 0.872 | 5.72 | 0.405 | 8.67 | 0.198 | 8.67 | 0.198 | 8.67 | 0.198 | 8.67 | 0.198 |
| | | 6.24 | 0.823 | 9.43 | 0.775 | 25.00 | 0.828 | 5.75 | 0.098 | 8.83 | 0.502 | 8.83 | 0.502 | 8.83 | 0.502 | 8.83 | 0.502 |
| | | 6.27 | 0.907 | 9.53 | 0.876 | | | 5.76 | 0.071 | 8.92 | 0.642 | 8.92 | 0.642 | 8.92 | 0.642 | 8.92 | 0.642 |
| | | 6.32 | 0.897 | 9.59 | 0.952 | | | 5.79 | 0.103 | 9.14 | 0.771 | 9.14 | 0.771 | 9.14 | 0.771 | 9.14 | 0.771 |
| | | 6.37 | 0.918 | 9.65 | 0.603 | | | 5.88 | 0.713 | 9.26 | 0.776 | 9.26 | 0.776 | 9.26 | 0.776 | 9.26 | 0.776 |
| | | 6.52 | 0.911 | 9.69 | 0.885 | | | 5.93 | 0.090 | 9.43 | 0.749 | 9.43 | 0.749 | 9.43 | 0.749 | 9.43 | 0.749 |
| | | 6.58 | 0.691 | 9.77 | 0.902 | | | 6.11 | 0.796 | 9.52 | 0.625 | 9.52 | 0.625 | 9.52 | 0.625 | 9.52 | 0.625 |
| | | 6.60 | 0.793 | 9.86 | 0.878 | | | 6.14 | 0.851 | 9.71 | 0.639 | 9.71 | 0.639 | 9.71 | 0.639 | 9.71 | 0.639 |
| | | 6.64 | 0.784 | 9.95 | 0.672 | | | 6.24 | 0.871 | 9.86 | 0.850 | 9.86 | 0.850 | 9.86 | 0.850 | 9.86 | 0.850 |
| | | 6.68 | 0.515 | 10.05 | 0.613 | | | 6.29 | 0.963 | 10.00 | 0.647 | 10.00 | 0.647 | 10.00 | 0.647 | 10.00 | 0.647 |
| | | 6.72 | 0.481 | 10.17 | 0.721 | | | 6.37 | 0.910 | 10.24 | 0.703 | 10.24 | 0.703 | 10.24 | 0.703 | 10.24 | 0.703 |
| | | 6.80 | 0.472 | 10.28 | 0.676 | | | 6.51 | 0.910 | 10.37 | 0.624 | 10.37 | 0.624 | 10.37 | 0.624 | 10.37 | 0.624 |
| | | 6.83 | 0.394 | 10.53 | 0.332 | | | 6.62 | 0.889 | 10.46 | 0.753 | 10.46 | 0.753 | 10.46 | 0.753 | 10.46 | 0.753 |
| | | 6.86 | 0.329 | 10.65 | 0.957 | | | 6.68 | 0.843 | 10.60 | 0.835 | 10.60 | 0.835 | 10.60 | 0.835 | 10.60 | 0.835 |
| | | 6.90 | 0.597 | 10.87 | 0.835 | | | 6.70 | 0.598 | 10.76 | 0.863 | 10.76 | 0.863 | 10.76 | 0.863 | 10.76 | 0.863 |
| | | 6.94 | 0.387 | 11.03 | 0.902 | | | 6.73 | 0.625 | 10.95 | 0.797 | 10.95 | 0.797 | 10.95 | 0.797 | 10.95 | 0.797 |
| | | 7.01 | 0.795 | 11.22 | 0.916 | | | 6.79 | 0.651 | 11.15 | 0.859 | 11.15 | 0.859 | 11.15 | 0.859 | 11.15 | 0.859 |
| | | 7.06 | 0.821 | 11.44 | 0.899 | | | 6.84 | 0.600 | 11.19 | 0.894 | 11.19 | 0.894 | 11.19 | 0.894 | 11.19 | 0.894 |
| | | 7.11 | 0.796 | 11.81 | 0.773 | | | 6.88 | 0.479 | 11.35 | 0.903 | 11.35 | 0.903 | 11.35 | 0.903 | 11.35 | 0.903 |
| | | 7.12 | 0.694 | 11.92 | 0.861 | | | 6.91 | 0.507 | 11.56 | 0.884 | 11.56 | 0.884 | 11.56 | 0.884 | 11.56 | 0.884 |
| | | 7.19 | 0.556 | 12.11 | 0.697 | | | 6.96 | 0.494 | 11.67 | 0.863 | 11.67 | 0.863 | 11.67 | 0.863 | 11.67 | 0.863 |
| | | 7.23 | 0.709 | 12.30 | 0.651 | | | 7.03 | 0.768 | 11.79 | 0.647 | 11.79 | 0.647 | 11.79 | 0.647 | 11.79 | 0.647 |
| | | 7.30 | 0.723 | 12.53 | 0.922 | | | 7.07 | 0.782 | 11.92 | 0.500 | 11.92 | 0.500 | 11.92 | 0.500 | 11.92 | 0.500 |
| | | 7.37 | 0.787 | 12.71 | 0.696 | | | 7.12 | 0.765 | 12.62 | 0.854 | 12.62 | 0.854 | 12.62 | 0.854 | 12.62 | 0.854 |
| | | 7.47 | 0.801 | 13.09 | 0.584 | | | 7.22 | 0.637 | 12.11 | 0.859 | 12.11 | 0.859 | 12.11 | 0.859 | 12.11 | 0.859 |
| | | 7.59 | 0.787 | 12.80 | 0.924 | | | 7.27 | 0.736 | 12.25 | 0.878 | 12.25 | 0.878 | 12.25 | 0.878 | 12.25 | 0.878 |
| | | 7.68 | 0.724 | 13.62 | 0.955 | | | 7.46 | 0.802 | 12.39 | 0.665 | 12.39 | 0.665 | 12.39 | 0.665 | 12.39 | 0.665 |
| | | 7.86 | 0.596 | 13.99 | 0.714 | | | 7.59 | 0.802 | 12.59 | 0.889 | 12.59 | 0.889 | 12.59 | 0.889 | 12.59 | 0.889 |
| | | 7.93 | 0.386 | 14.12 | 0.534 | | | 7.70 | 0.768 | 12.85 | 0.883 | 12.85 | 0.883 | 12.85 | 0.883 | 12.85 | 0.883 |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μ ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
|-----------|-------|----------------------|-------|-----------|-------|-----------|-------|----------------------|-------|-----------|-------|-----------|-------|-----------|-------|
| 12.59 | 0.889 | 2.699 | 0.810 | 4.17 | 0.923 | 6.81 | 0.500 | 11.11 | 0.822 | 2.76 | 0.953 | 11.11 | 0.822 | 2.76 | 0.953 |
| 12.85 | 0.883 | 2.800 | 0.827 | 4.23 | 0.954 | 6.87 | 0.462 | 11.44 | 0.858 | 2.80 | 0.925 | 11.44 | 0.858 | 2.80 | 0.925 |
| 13.07 | 0.840 | | | 4.35 | 0.937 | 6.96 | 0.505 | 11.71 | 0.819 | 2.85 | 0.865 | 11.71 | 0.819 | 2.85 | 0.865 |
| 13.35 | 0.745 | CURVE 23 T = 293. | | 4.47 | 0.948 | 7.03 | 0.692 | 11.98 | 0.842 | 2.91 | 0.824 | 11.98 | 0.842 | 2.91 | 0.824 |
| 13.42 | 0.857 | | | 4.75 | 0.937 | 7.13 | 0.683 | 12.18 | 0.797 | 2.95 | 0.830 | 12.18 | 0.797 | 2.95 | 0.830 |
| 13.95 | 0.876 | 2.50 | 0.928 | 5.00 | 0.934 | 7.23 | 0.520 | 12.35 | 0.845 | 3.06 | 0.830 | 12.35 | 0.845 | 3.06 | 0.830 |
| 14.14 | 0.863 | 2.51 | 0.926 | 5.13 | 0.927 | 7.29 | 0.552 | 12.55 | 0.825 | 3.16 | 0.850 | 12.55 | 0.825 | 3.16 | 0.850 |
| 14.29 | 0.732 | 2.53 | 0.915 | 5.28 | 0.927 | 7.34 | 0.632 | 12.80 | 0.825 | 3.22 | 0.850 | 12.80 | 0.825 | 3.22 | 0.850 |
| 14.49 | 0.880 | 2.54 | 0.932 | 5.41 | 0.906 | 7.41 | 0.666 | 13.02 | 0.809 | 3.29 | 0.797 | 13.02 | 0.809 | 3.29 | 0.797 |
| 15.87 | 0.689 | 2.57 | 0.932 | 5.47 | 0.889 | 7.47 | 0.632 | 13.19 | 0.699 | 3.32 | 0.725 | 13.19 | 0.699 | 3.32 | 0.725 |
| 17.64 | 0.662 | 2.59 | 0.922 | 5.53 | 0.774 | 7.52 | 0.569 | 13.48 | 0.676 | 3.37 | 0.417 | 13.48 | 0.676 | 3.37 | 0.417 |
| 18.80 | 0.853 | 2.68 | 0.925 | 5.68 | 0.524 | 7.58 | 0.552 | 13.74 | 0.844 | 3.40 | 0.326 | 13.74 | 0.844 | 3.40 | 0.326 |
| 19.80 | 0.632 | 2.66 | 0.935 | 5.64 | 0.594 | 7.67 | 0.484 | 14.06 | 0.808 | 3.41 | 0.230 | 14.06 | 0.808 | 3.41 | 0.230 |
| 20.49 | 0.924 | 2.68 | 0.925 | 5.68 | 0.524 | 7.70 | 0.314 | 14.29 | 0.750 | 3.43 | 0.266 | 14.29 | 0.750 | 3.43 | 0.266 |
| 20.92 | 0.796 | 2.70 | 0.936 | 5.72 | 0.225 | 7.73 | 0.256 | 14.43 | 0.685 | 3.47 | 0.475 | 14.43 | 0.685 | 3.47 | 0.475 |
| 21.51 | 0.816 | 2.73 | 0.902 | 5.74 | 0.186 | 7.79 | 0.244 | 14.97 | 0.920 | 3.51 | 0.411 | 14.97 | 0.920 | 3.51 | 0.411 |
| 22.62 | 0.888 | 2.76 | 0.887 | 5.78 | 0.087 | 7.90 | 0.287 | 15.29 | 0.899 | 3.53 | 0.711 | 15.29 | 0.899 | 3.53 | 0.711 |
| 23.64 | 0.794 | 2.79 | 0.899 | 5.80 | 0.122 | 8.04 | 0.392 | 15.43 | 0.917 | 3.56 | 0.812 | 15.43 | 0.917 | 3.56 | 0.812 |
| 25.00 | 0.737 | 2.83 | 0.873 | 5.88 | 0.396 | 8.14 | 0.424 | 15.65 | 0.930 | 3.61 | 0.876 | 15.65 | 0.930 | 3.61 | 0.876 |
| | | 2.86 | 0.873 | 5.93 | 0.547 | 8.36 | 0.336 | 16.45 | 0.986 | 3.66 | 0.877 | 16.45 | 0.986 | 3.66 | 0.877 |
| | | 2.93 | 0.838 | 5.96 | 0.606 | 8.45 | 0.336 | 17.42 | 0.914 | 3.77 | 0.910 | 17.42 | 0.914 | 3.77 | 0.910 |
| | | 2.99 | 0.824 | 6.00 | 0.657 | 8.63 | 0.286 | 17.70 | 0.898 | 3.87 | 0.910 | 17.70 | 0.898 | 3.87 | 0.910 |
| | | 3.10 | 0.846 | 6.05 | 0.664 | 8.83 | 0.386 | 18.12 | 0.909 | 4.18 | 0.940 | 18.12 | 0.909 | 4.18 | 0.940 |
| | | 3.17 | 0.857 | 6.08 | 0.650 | 8.90 | 0.390 | 18.45 | 0.891 | 4.23 | 0.924 | 18.45 | 0.891 | 4.23 | 0.924 |
| | | 3.23 | 0.825 | 6.12 | 0.673 | 9.02 | 0.591 | 19.31 | 0.907 | 4.27 | 0.937 | 19.31 | 0.907 | 4.27 | 0.937 |
| | | 3.28 | 0.790 | 6.16 | 0.771 | 9.15 | 0.642 | 19.72 | 0.889 | 4.32 | 0.930 | 19.72 | 0.889 | 4.32 | 0.930 |
| | | 3.31 | 0.753 | 6.21 | 0.794 | 9.21 | 0.593 | 20.33 | 0.888 | 4.38 | 0.946 | 20.33 | 0.888 | 4.38 | 0.946 |
| | | 3.33 | 0.598 | 6.24 | 0.772 | 9.25 | 0.585 | 20.53 | 0.869 | 4.62 | 0.954 | 20.53 | 0.869 | 4.62 | 0.954 |
| | | 3.34 | 0.507 | 6.27 | 0.820 | 9.32 | 0.482 | 21.46 | 0.869 | 5.00 | 0.954 | 21.46 | 0.869 | 5.00 | 0.954 |
| | | 3.38 | 0.456 | 6.31 | 0.807 | 9.41 | 0.649 | 22.57 | 0.823 | 5.13 | 0.956 | 22.57 | 0.823 | 5.13 | 0.956 |
| | | 3.41 | 0.531 | 6.36 | 0.842 | 9.49 | 0.664 | 23.53 | 0.789 | 5.27 | 0.953 | 23.53 | 0.789 | 5.27 | 0.953 |
| | | 3.43 | 0.624 | 6.40 | 0.824 | 9.59 | 0.596 | 24.33 | 0.718 | 5.28 | 0.944 | 24.33 | 0.718 | 5.28 | 0.944 |
| | | 3.45 | 0.681 | 6.44 | 0.824 | 9.70 | 0.566 | 25.00 | 0.718 | 5.32 | 0.953 | 25.00 | 0.718 | 5.32 | 0.953 |
| | | 3.48 | 0.681 | 6.49 | 0.811 | 9.80 | 0.577 | | | 5.37 | 0.942 | | | 5.37 | 0.942 |
| | | 3.52 | 0.827 | 6.56 | 0.822 | 9.92 | 0.723 | CURVE 24 T = 293. | | 5.39 | 0.831 | | | 5.39 | 0.831 |
| | | 3.56 | 0.881 | 6.61 | 0.792 | 10.21 | 0.755 | | | 5.42 | 0.910 | | | 5.42 | 0.910 |
| | | 3.57 | 0.919 | 6.65 | 0.737 | 10.46 | 0.700 | | | 5.45 | 0.928 | | | 5.45 | 0.928 |
| | | 3.76 | 0.913 | 6.68 | 0.744 | 10.60 | 0.746 | | | 5.49 | 0.884 | | | 5.49 | 0.884 |
| | | 3.87 | 0.913 | 6.73 | 0.697 | 10.76 | 0.808 | | | 5.56 | 0.782 | | | 5.56 | 0.782 |
| | | 3.93 | 0.923 | 6.78 | 0.577 | 10.89 | 0.793 | | | 5.58 | 0.626 | | | 5.58 | 0.626 |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|------------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| 5.61 | 0.654 | 7.47 | 0.628 | 16.10 | 0.919 | 3.52 | 0.787 | 6.30 | 0.727 | 12.17 | 0.811 | 12.17 | 0.811 |
| 5.63 | 0.521 | 7.65 | 0.516 | 16.89 | 0.902 | 3.57 | 0.849 | 6.44 | 0.773 | 12.66 | 0.841 | 12.66 | 0.841 |
| 5.65 | 0.551 | 7.75 | 0.484 | 18.28 | 0.902 | 3.68 | 0.869 | 6.54 | 0.793 | 12.74 | 0.776 | 12.74 | 0.776 |
| 5.68 | 0.511 | 7.88 | 0.423 | 18.76 | 0.854 | 3.87 | 0.874 | 6.68 | 0.768 | 12.95 | 0.787 | 12.95 | 0.787 |
| 5.71 | 0.257 | 7.96 | 0.350 | 19.08 | 0.884 | 3.90 | 0.896 | 6.76 | 0.699 | 13.21 | 0.773 | 13.21 | 0.773 |
| 5.75 | 0.128 | 8.14 | 0.419 | 19.96 | 0.892 | 3.96 | 0.871 | 6.87 | 0.303 | 13.42 | 0.828 | 13.42 | 0.828 |
| 5.81 | 0.211 | 8.29 | 0.362 | 21.51 | 0.892 | 4.05 | 0.895 | 6.96 | 0.391 | 13.76 | 0.859 | 13.76 | 0.859 |
| 5.88 | 0.434 | 8.48 | 0.300 | 23.09 | 0.849 | 4.10 | 0.888 | 7.01 | 0.343 | 14.03 | 0.896 | 14.03 | 0.896 |
| 5.92 | 0.604 | 8.61 | 0.314 | 23.53 | 0.806 | 4.16 | 0.888 | 7.06 | 0.466 | 14.27 | 0.885 | 14.27 | 0.885 |
| 5.97 | 0.696 | 8.67 | 0.335 | 24.27 | 0.788 | 4.21 | 0.906 | 7.12 | 0.483 | 14.51 | 0.897 | 14.51 | 0.897 |
| 6.02 | 0.744 | 8.98 | 0.383 | 25.00 | 0.769 | 4.28 | 0.875 | 7.12 | 0.634 | 15.36 | 0.871 | 15.36 | 0.871 |
| 6.08 | 0.744 | 9.03 | 0.389 | 25.00 | 0.769 | 4.35 | 0.875 | 7.12 | 0.634 | 16.04 | 0.858 | 16.04 | 0.858 |
| 6.11 | 0.733 | 9.15 | 0.457 | 25.00 | 0.769 | 4.39 | 0.798 | 7.49 | 0.639 | 16.64 | 0.882 | 16.64 | 0.882 |
| 6.17 | 0.753 | 9.18 | 0.497 | 25.00 | 0.769 | 4.44 | 0.331 | 7.69 | 0.639 | 17.36 | 0.809 | 17.36 | 0.809 |
| 6.22 | 0.741 | 9.31 | 0.529 | 25.00 | 0.769 | 4.46 | 0.534 | 7.85 | 0.590 | 17.92 | 0.835 | 17.92 | 0.835 |
| 6.25 | 0.757 | 9.46 | 0.561 | 25.00 | 0.769 | 4.50 | 0.499 | 7.92 | 0.626 | 18.42 | 0.798 | 18.42 | 0.798 |
| 6.27 | 0.723 | 9.63 | 0.516 | 25.00 | 0.769 | 4.52 | 0.812 | 8.03 | 0.626 | 19.12 | 0.844 | 19.12 | 0.844 |
| 6.32 | 0.790 | 9.76 | 0.534 | 25.00 | 0.769 | 4.56 | 0.768 | 8.17 | 0.576 | 21.28 | 0.917 | 21.28 | 0.917 |
| 6.37 | 0.848 | 9.82 | 0.615 | 25.00 | 0.769 | 4.60 | 0.894 | 8.31 | 0.585 | 22.99 | 0.876 | 22.99 | 0.876 |
| 6.41 | 0.856 | 9.97 | 0.684 | 25.00 | 0.769 | 4.66 | 0.922 | 8.40 | 0.629 | 23.53 | 0.837 | 23.53 | 0.837 |
| 6.44 | 0.869 | 10.19 | 0.719 | 25.00 | 0.769 | 4.76 | 0.909 | 8.51 | 0.591 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.53 | 0.884 | 10.33 | 0.707 | 25.00 | 0.769 | 4.87 | 0.926 | 8.67 | 0.704 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.57 | 0.864 | 10.54 | 0.707 | 25.00 | 0.769 | 4.93 | 0.916 | 8.83 | 0.756 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.61 | 0.903 | 10.81 | 0.757 | 25.00 | 0.769 | 5.00 | 0.922 | 8.92 | 0.734 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.67 | 0.825 | 11.12 | 0.660 | 25.00 | 0.769 | 5.07 | 0.921 | 9.03 | 0.754 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.72 | 0.757 | 11.25 | 0.727 | 25.00 | 0.769 | 5.15 | 0.894 | 9.16 | 0.734 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.76 | 0.693 | 11.44 | 0.760 | 25.00 | 0.769 | 5.26 | 0.861 | 9.31 | 0.712 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.80 | 0.504 | 11.68 | 0.750 | 25.00 | 0.769 | 5.35 | 0.917 | 9.45 | 0.728 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.81 | 0.451 | 11.83 | 0.783 | 25.00 | 0.769 | 5.55 | 0.914 | 9.58 | 0.704 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.85 | 0.437 | 12.24 | 0.881 | 25.00 | 0.769 | 5.63 | 0.877 | 9.67 | 0.741 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.89 | 0.458 | 12.42 | 0.833 | 25.00 | 0.769 | 5.68 | 0.842 | 9.72 | 0.768 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.89 | 0.486 | 12.87 | 0.886 | 25.00 | 0.769 | 5.74 | 0.538 | 10.05 | 0.768 | 25.00 | 0.837 | 25.00 | 0.837 |
| 6.98 | 0.539 | 13.02 | 0.805 | 25.00 | 0.769 | 5.77 | 0.446 | 10.16 | 0.738 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.02 | 0.651 | 13.18 | 0.795 | 25.00 | 0.769 | 5.82 | 0.642 | 10.31 | 0.637 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.09 | 0.674 | 13.57 | 0.843 | 25.00 | 0.769 | 5.88 | 0.689 | 10.44 | 0.399 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.15 | 0.656 | 13.93 | 0.659 | 25.00 | 0.769 | 5.96 | 0.659 | 10.71 | 0.701 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.25 | 0.501 | 14.16 | 0.851 | 25.00 | 0.769 | 6.03 | 0.685 | 10.89 | 0.795 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.31 | 0.535 | 14.60 | 0.895 | 25.00 | 0.769 | 6.08 | 0.595 | 11.19 | 0.795 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.34 | 0.592 | 15.04 | 0.919 | 25.00 | 0.769 | 6.15 | 0.562 | 11.61 | 0.837 | 25.00 | 0.837 | 25.00 | 0.837 |
| 7.41 | 0.684 | 15.62 | 0.911 | 25.00 | 0.769 | 6.23 | 0.677 | 11.98 | 0.784 | 25.00 | 0.837 | 25.00 | 0.837 |
| CURVE 25 (CONT.) | | | | | | | | | | | | | |
| CURVE 26 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |
| CURVE 25 | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μ m; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | CURVE 26 (CONT.) | | CURVE 26 (CONT.) | | CURVE 26 (CONT.) | | CURVE 26 (CONT.) | | λ | CURVE 27 (CONT.) | | CURVE 27 (CONT.) | |
|-----------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|-----------|------------------|-------|------------------|---|
| | T | T | T | T | T | T | T | T | | T | T | T | T |
| 3.20 | 0.769 | 0.911 | 7.97 | 0.511 | 14.16 | 0.897 | 4.65 | 0.839 | 19.64 | 0.903 | 0.839 | 0.839 | |
| 3.22 | 0.750 | 0.937 | 7.92 | 0.672 | 14.41 | 0.866 | 5.21 | 0.854 | 11.75 | 0.904 | 0.854 | 0.854 | |
| 3.25 | 0.767 | 0.957 | 8.01 | 0.659 | 14.79 | 0.875 | 5.57 | 0.824 | 12.52 | 0.898 | 0.875 | 0.875 | |
| 3.29 | 0.795 | 0.957 | 8.03 | 0.670 | 15.22 | 0.853 | 5.68 | 0.690 | 13.65 | 0.932 | 0.690 | 0.690 | |
| 3.32 | 0.735 | 0.935 | 8.16 | 0.514 | 15.72 | 0.825 | 5.70 | 0.575 | 13.45 | 0.932 | 0.575 | 0.575 | |
| 3.35 | 0.551 | 0.950 | 8.27 | 0.654 | 16.31 | 0.827 | 5.75 | 0.478 | 13.73 | 0.943 | 0.478 | 0.478 | |
| 3.38 | 0.413 | 0.938 | 8.35 | 0.704 | 16.64 | 0.859 | 5.82 | 0.596 | 13.97 | 0.930 | 0.596 | 0.596 | |
| 3.40 | 0.349 | 0.879 | 8.45 | 0.721 | 17.21 | 0.774 | 5.87 | 0.654 | 14.15 | 0.930 | 0.654 | 0.654 | |
| 3.44 | 0.529 | 0.886 | 8.54 | 0.721 | 17.67 | 0.736 | 5.89 | 0.792 | 14.50 | 0.930 | 0.792 | 0.792 | |
| 3.46 | 0.522 | 0.846 | 8.63 | 0.750 | 18.21 | 0.764 | 6.02 | 0.661 | 15.00 | 0.895 | 0.661 | 0.661 | |
| 3.49 | 0.513 | 0.781 | 8.70 | 0.798 | 18.69 | 0.699 | 6.14 | 0.798 | | | | | |
| 3.55 | 0.754 | 0.759 | 8.87 | 0.757 | 18.99 | 0.713 | 6.30 | 0.829 | | | | | |
| 3.57 | 0.823 | 0.654 | 8.93 | 0.711 | 19.42 | 0.639 | 6.38 | 0.839 | | | | | |
| 3.64 | 0.884 | 0.561 | 9.15 | 0.722 | 19.60 | 0.805 | 6.60 | 0.809 | | | | | |
| 3.72 | 0.894 | 0.561 | 9.39 | 0.674 | 20.12 | 0.861 | 6.77 | 0.704 | | | | | |
| 3.77 | 0.895 | 0.508 | 9.49 | 0.587 | 20.83 | 0.948 | 6.81 | 0.548 | | | | | |
| 3.83 | 0.873 | 0.615 | 9.52 | 0.654 | 21.55 | 0.899 | 7.00 | 0.459 | | | | | |
| 3.87 | 0.894 | 0.693 | 9.72 | 0.705 | 22.27 | 0.858 | 7.00 | 0.762 | | | | | |
| 3.91 | 0.894 | 0.761 | 9.81 | 0.735 | 23.20 | 0.693 | 7.09 | 0.817 | | | | | |
| 3.94 | 0.911 | 0.744 | 9.87 | 0.716 | 23.20 | 0.854 | 7.18 | 0.781 | | | | | |
| 3.99 | 0.890 | 0.804 | 10.03 | 0.739 | 24.04 | 0.831 | 7.26 | 0.677 | | | | | |
| 4.05 | 0.903 | 0.846 | 10.17 | 0.687 | 24.51 | 0.756 | 7.36 | 0.559 | | | | | |
| 4.19 | 0.908 | 0.801 | 10.33 | 0.353 | 25.00 | 0.769 | 7.48 | 0.670 | | | | | |
| 4.25 | 0.852 | 0.771 | 10.47 | 0.222 | | | 7.55 | 0.733 | | | | | |
| 4.35 | 0.876 | 0.721 | 10.73 | 0.623 | | | 7.67 | 0.733 | | | | | |
| 4.40 | 0.839 | 0.706 | 10.85 | 0.703 | | | 7.84 | 0.672 | | | | | |
| 4.44 | 0.162 | 0.550 | 10.92 | 0.755 | | | 8.01 | 0.630 | | | | | |
| 4.48 | 0.410 | 0.435 | 11.09 | 0.742 | 2.49 | 0.703 | 8.31 | 0.630 | | | | | |
| 4.50 | 0.345 | 0.260 | 11.33 | 0.767 | 2.71 | 0.732 | 8.45 | 0.664 | | | | | |
| 4.52 | 0.784 | 0.297 | 11.56 | 0.750 | 2.98 | 0.696 | 8.58 | 0.655 | | | | | |
| 4.57 | 0.732 | 0.254 | 11.82 | 0.804 | 3.17 | 0.732 | 8.67 | 0.708 | | | | | |
| 4.51 | 0.971 | 0.353 | 11.82 | 0.779 | 3.28 | 0.706 | 8.72 | 0.820 | | | | | |
| 4.64 | 0.924 | 0.339 | 12.05 | 0.731 | 3.45 | 0.611 | 8.80 | 0.852 | | | | | |
| 4.71 | 0.948 | 0.642 | 12.14 | 0.783 | 3.58 | 0.771 | 9.01 | 0.777 | | | | | |
| 4.83 | 0.954 | 0.575 | 12.36 | 0.811 | 3.83 | 0.809 | 9.28 | 0.708 | | | | | |
| 4.88 | 0.929 | 0.619 | 12.84 | 0.764 | 4.18 | 0.816 | 9.35 | 0.708 | | | | | |
| 5.00 | 0.957 | 0.632 | 13.21 | 0.692 | 4.33 | 0.630 | 9.47 | 0.523 | | | | | |
| 5.07 | 0.966 | 0.632 | 13.51 | 0.770 | 4.43 | 0.751 | 9.63 | 0.569 | | | | | |
| 5.14 | 0.937 | 0.647 | 13.77 | 0.786 | 4.50 | 0.552 | 9.77 | 0.828 | | | | | |
| 5.22 | 0.874 | 0.627 | 13.93 | 0.862 | 4.59 | 0.801 | 10.08 | 0.877 | | | | | |

CURVE 28
T = 293.

3.12 0.300
 3.19 0.800
 3.26 0.758
 3.34 0.685
 3.41 0.277
 3.44 0.435
 3.54 0.499
 3.66 0.630
 3.79 0.624
 3.51 0.716
 3.51 0.814
 3.62 0.839
 3.69 0.850
 3.76 0.837
 3.85 0.850
 4.03 0.849
 4.16 0.875
 4.29 0.875
 4.34 0.858
 4.39 0.821
 4.42 0.613
 4.42 0.823
 4.45 0.669
 4.49 0.528
 4.49 0.782
 4.51 0.862

CURVE 27
T = 293.

2.49 0.703
 2.71 0.732
 2.98 0.696
 3.17 0.732
 3.28 0.706
 3.45 0.611
 3.58 0.771
 3.83 0.809
 4.18 0.816
 4.33 0.630
 4.43 0.751
 4.50 0.552
 4.59 0.801

10.08

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 23 (CONT.) | | | CURVE 28 (CONT.) | | | CURVE 29 (CONT.) | | | CURVE 30 (CONT.) | | | CURVE 30 (CONT.) | | |
|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|------------------|-------|--------|
| λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ | λ | T | τ |
| 4.59 | 0.915 | 0.558 | 9.38 | 0.558 | 0.573 | 2.52 | 0.788 | 0.738 | 3.68 | 0.738 | 0.738 | 5.41 | 0.723 | 0.723 |
| 4.69 | 0.944 | 0.695 | 9.60 | 0.695 | 0.591 | 2.57 | 0.796 | 0.794 | 3.71 | 0.794 | 0.794 | 5.45 | 0.762 | 0.762 |
| 4.99 | 0.954 | 0.750 | 9.60 | 0.750 | 0.539 | 2.57 | 0.796 | 0.794 | 3.78 | 0.800 | 0.800 | 5.48 | 0.748 | 0.748 |
| 5.63 | 0.954 | 0.817 | 9.76 | 0.817 | 0.445 | 2.66 | 0.822 | 0.822 | 3.81 | 0.776 | 0.776 | 5.50 | 0.690 | 0.690 |
| 5.73 | 0.922 | 0.885 | 10.02 | 0.885 | 0.445 | 2.66 | 0.822 | 0.822 | 3.84 | 0.785 | 0.785 | 5.59 | 0.537 | 0.537 |
| 5.88 | 0.916 | 0.894 | 10.23 | 0.894 | 0.187 | 2.70 | 0.827 | 0.827 | 3.88 | 0.769 | 0.769 | 5.66 | 0.338 | 0.338 |
| 6.35 | 0.944 | 0.911 | 10.70 | 0.911 | 0.499 | 2.72 | 0.839 | 0.839 | 3.91 | 0.793 | 0.793 | 5.71 | 0.154 | 0.154 |
| 6.24 | 0.944 | 0.698 | 11.11 | 0.698 | 0.409 | 2.75 | 0.831 | 0.831 | 3.95 | 0.745 | 0.745 | 5.72 | 0.067 | 0.067 |
| 6.29 | 0.959 | | | | 0.299 | 2.79 | 0.783 | 0.783 | 4.00 | 0.792 | 0.792 | 5.77 | 0.064 | 0.064 |
| 6.54 | 0.917 | | | | 0.415 | 2.82 | 0.911 | 0.911 | 4.09 | 0.792 | 0.792 | 5.87 | 0.054 | 0.054 |
| 6.67 | 0.987 | | | | 0.485 | 2.86 | 0.799 | 0.799 | 4.13 | 0.800 | 0.800 | 5.90 | 0.032 | 0.032 |
| 6.73 | 0.755 | | | | 0.394 | 2.89 | 0.813 | 0.813 | 4.28 | 0.800 | 0.800 | 5.95 | 0.141 | 0.141 |
| 6.79 | 0.471 | 0.490 | 7.94 | 0.490 | 0.256 | 2.92 | 0.803 | 0.803 | 4.33 | 0.791 | 0.791 | 6.01 | 0.347 | 0.347 |
| 6.85 | 0.118 | 0.457 | 8.00 | 0.457 | 0.189 | 2.94 | 0.607 | 0.607 | 4.38 | 0.732 | 0.732 | 6.05 | 0.373 | 0.373 |
| 6.92 | 0.429 | 0.358 | 8.18 | 0.358 | 0.351 | 2.98 | 0.795 | 0.795 | 4.41 | 0.802 | 0.802 | 6.08 | 0.198 | 0.198 |
| 6.97 | 0.653 | 0.319 | 8.20 | 0.319 | 0.419 | 3.01 | 0.742 | 0.742 | 4.53 | 0.810 | 0.810 | 6.10 | 0.509 | 0.509 |
| 7.01 | 0.773 | 0.364 | 8.31 | 0.364 | 0.522 | 3.03 | 0.792 | 0.792 | 4.55 | 0.823 | 0.823 | 6.11 | 0.300 | 0.300 |
| 7.07 | 0.809 | 0.424 | 8.47 | 0.424 | 0.548 | 3.06 | 0.801 | 0.801 | 4.59 | 0.823 | 0.823 | 6.14 | 0.025 | 0.025 |
| 7.17 | 0.710 | 0.394 | 8.69 | 0.394 | 0.623 | 3.13 | 0.792 | 0.792 | 4.62 | 0.752 | 0.752 | 6.22 | 0.438 | 0.438 |
| 7.26 | 0.579 | 0.279 | 8.98 | 0.279 | 0.469 | 3.15 | 0.778 | 0.778 | 4.66 | 0.752 | 0.752 | 6.24 | 0.492 | 0.492 |
| 7.27 | 0.482 | 0.423 | 9.31 | 0.423 | 0.364 | 3.16 | 0.751 | 0.751 | 4.70 | 0.761 | 0.761 | 6.28 | 0.322 | 0.322 |
| 7.35 | 0.455 | 0.529 | 9.53 | 0.529 | 0.380 | 3.21 | 0.702 | 0.702 | 4.73 | 0.751 | 0.751 | 6.32 | 0.535 | 0.535 |
| 7.46 | 0.526 | 0.555 | 9.66 | 0.555 | 0.380 | 3.25 | 0.462 | 0.462 | 4.74 | 0.773 | 0.773 | 6.35 | 0.532 | 0.532 |
| 7.51 | 0.615 | 0.555 | 9.76 | 0.555 | 0.459 | 3.26 | 0.537 | 0.537 | 4.77 | 0.789 | 0.789 | 6.42 | 0.617 | 0.617 |
| 7.55 | 0.615 | 0.510 | 9.92 | 0.510 | 0.625 | 3.30 | 0.511 | 0.511 | 4.81 | 0.761 | 0.761 | 6.44 | 0.505 | 0.505 |
| 7.66 | 0.641 | 0.293 | 10.29 | 0.293 | 0.650 | 3.32 | 0.161 | 0.161 | 4.88 | 0.805 | 0.805 | 6.52 | 0.583 | 0.583 |
| 7.76 | 0.585 | 0.534 | 10.74 | 0.534 | 0.679 | 3.34 | 0.171 | 0.171 | 4.91 | 0.796 | 0.796 | 6.56 | 0.544 | 0.544 |
| 7.93 | 0.546 | 0.599 | 11.01 | 0.599 | 0.735 | 3.35 | 0.331 | 0.331 | 4.95 | 0.682 | 0.682 | 6.60 | 0.541 | 0.541 |
| 8.05 | 0.585 | 0.627 | 11.46 | 0.627 | 0.753 | 3.39 | 0.391 | 0.391 | 4.99 | 0.698 | 0.698 | 6.65 | 0.527 | 0.527 |
| 8.21 | 0.617 | 0.607 | 11.91 | 0.607 | 0.573 | 3.40 | 0.003 | 0.003 | 5.01 | 0.684 | 0.684 | 6.68 | 0.493 | 0.493 |
| 8.37 | 0.702 | 0.607 | 12.21 | 0.712 | 0.712 | 3.41 | 0.145 | 0.145 | 5.01 | 0.643 | 0.643 | 6.72 | 0.416 | 0.416 |
| 8.46 | 0.740 | 0.597 | 12.40 | 0.712 | 0.712 | 3.43 | 0.066 | 0.066 | 5.04 | 0.636 | 0.636 | 6.75 | 0.256 | 0.256 |
| 8.46 | 0.782 | 0.597 | 12.64 | 0.681 | 0.681 | 3.46 | 0.288 | 0.288 | 5.07 | 0.727 | 0.727 | 6.76 | 0.192 | 0.192 |
| 8.46 | 0.829 | 0.532 | 13.06 | 0.681 | 0.681 | 3.47 | 0.298 | 0.298 | 5.12 | 0.761 | 0.761 | 6.80 | 0.126 | 0.126 |
| 8.69 | 0.860 | 0.222 | 13.35 | 0.690 | 0.690 | 3.51 | 0.478 | 0.478 | 5.15 | 0.745 | 0.745 | 6.80 | 0.061 | 0.061 |
| 6.79 | 0.849 | 0.396 | 13.57 | 0.621 | 0.621 | 3.53 | 0.293 | 0.293 | 5.19 | 0.738 | 0.738 | 6.84 | 0.043 | 0.043 |
| 9.03 | 0.772 | 0.447 | 13.90 | 0.704 | 0.704 | 3.57 | 0.695 | 0.695 | 5.21 | 0.657 | 0.657 | 6.84 | 0.038 | 0.038 |
| 9.18 | 0.515 | 0.545 | 14.08 | 0.545 | 0.704 | 3.59 | 0.715 | 0.715 | 5.26 | 0.661 | 0.661 | 6.86 | 0.034 | 0.034 |
| 9.18 | 0.568 | 0.583 | 14.48 | 0.583 | 0.693 | 3.61 | 0.751 | 0.751 | 5.31 | 0.579 | 0.579 | 6.93 | 0.004 | 0.004 |
| 9.23 | 0.495 | 0.483 | 15.00 | 0.567 | 0.567 | 3.65 | 0.775 | 0.775 | 5.37 | 0.711 | 0.711 | 7.00 | 0.015 | 0.015 |

TABLE 15-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF ACRYLIC RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T | λ | T | λ | T | λ | T |
|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| 7.00 | 0.051 | 10.05 | 0.146 | 15.39 | 0.165 | 21.07 | 0.678 |
| 7.36 | 0.155 | 10.09 | 0.201 | 15.64 | 0.531 | 22.11 | 0.673 |
| 7.10 | 0.171 | 10.15 | 0.133 | 15.75 | 0.673 | 22.28 | 0.667 |
| 7.14 | 0.072 | 10.13 | 0.103 | 15.84 | 0.704 | 22.41 | 0.652 |
| 7.19 | 0.274 | 10.25 | 0.335 | 15.94 | 0.725 | 23.06 | 0.624 |
| 7.20 | 0.285 | 10.30 | 0.347 | 16.03 | 0.750 | 23.19 | 0.604 |
| 7.24 | 0.176 | 10.35 | 0.329 | 16.31 | 0.755 | 23.48 | 0.596 |
| 7.24 | 0.033 | 10.49 | 0.033 | 16.44 | 0.718 | 23.98 | 0.586 |
| 7.27 | 0.073 | 10.59 | 0.007 | 16.55 | 0.464 | 24.08 | 0.560 |
| 7.31 | 0.309 | 10.59 | 0.006 | 16.61 | 0.359 | 24.39 | 0.532 |
| 7.33 | 0.329 | 10.66 | 0.000 | 16.66 | 0.347 | 24.56 | 0.516 |
| 7.39 | 0.231 | 10.79 | 0.000 | 16.72 | 0.359 | 24.56 | 0.495 |
| 7.44 | 0.346 | 10.82 | 0.029 | 16.78 | 0.476 | 24.65 | 0.480 |
| 7.49 | 0.003 | 10.92 | 0.091 | 16.85 | 0.419 | 24.81 | 0.468 |
| 7.71 | 0.001 | 11.01 | 0.633 | 16.90 | 0.402 | | |
| 7.75 | 0.115 | 11.09 | 0.681 | 16.96 | 0.421 | | |
| 7.80 | 0.221 | 11.22 | 0.725 | 16.96 | 0.545 | | |
| 7.85 | 0.333 | 11.38 | 0.741 | 17.05 | 0.625 | | |
| 7.87 | 0.389 | 11.57 | 0.741 | 17.21 | 0.755 | | |
| 7.90 | 0.402 | 11.80 | 0.668 | 17.33 | 0.780 | | |
| 7.93 | 0.402 | 11.99 | 0.228 | 17.55 | 0.783 | | |
| 8.01 | 0.333 | 11.95 | 0.001 | 17.70 | 0.789 | | |
| 8.10 | 0.231 | 12.00 | 0.054 | 18.09 | 0.788 | | |
| 8.13 | 0.132 | 12.03 | 0.086 | 18.45 | 0.788 | | |
| 8.16 | 0.202 | 12.24 | 0.006 | 18.68 | 0.780 | | |
| 8.23 | 0.357 | 12.33 | 0.056 | 18.91 | 0.765 | | |
| 8.26 | 0.210 | 12.43 | 0.492 | 19.13 | 0.736 | | |
| 8.73 | 0.210 | 12.57 | 0.666 | 19.31 | 0.696 | | |
| 8.91 | 0.280 | 12.68 | 0.745 | 19.50 | 0.583 | | |
| 9.03 | 0.474 | 12.78 | 0.769 | 19.65 | 0.484 | | |
| 9.15 | 0.533 | 12.84 | 0.704 | 19.74 | 0.443 | | |
| 9.34 | 0.653 | 13.55 | 0.801 | 19.82 | 0.425 | | |
| 9.45 | 0.665 | 13.75 | 0.812 | 19.97 | 0.456 | | |
| 9.54 | 0.653 | 14.25 | 0.812 | 20.01 | 0.500 | | |
| 9.55 | 0.551 | 14.43 | 0.801 | 20.08 | 0.529 | | |
| 9.63 | 0.487 | 14.60 | 0.761 | 20.19 | 0.594 | | |
| 9.79 | 0.315 | 14.77 | 0.666 | 20.34 | 0.632 | | |
| 9.90 | 0.335 | 14.95 | 0.468 | 20.47 | 0.655 | | |
| 9.93 | 0.300 | 15.08 | 0.219 | 20.67 | 0.671 | | |
| 9.96 | 0.199 | 15.32 | 0.156 | 20.97 | 0.671 | | |

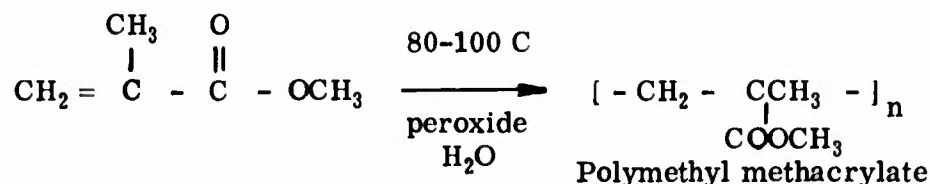
4.16 Lucite

Lucite is a propriatory acrylic resin, poly(methyl methacrylate), manufactured by DuPont Co. "Plexiglas" and "Perspex" are essentially the same material manufactured by Rohm and Haas Co. and Imperial Chemical Industrial Chemicals Ltd. respectively.

Lucite is a rigid, crystal-clear thermoplastic material with excellent mechanical and chemical properties. It has the best resistance to the effects of sunlight and outdoor weathering among all the transparent plastics. Industrial uses include optical applications such as in TV screens, automobile taillights, and lenses for cameras and slide viewers.

Lucite acrylic resins can be easily processed by all fabricating techniques currently practiced in the industry. They can be injection molded, blow molded, compression molded, and extruded. It also can be machined, drilled, threaded, and routed with standard wood and metal-working equipment.

The polymerization of Lucite is carried out in water suspension with peroxide catalyst. The resulting polymer is washed, dried and blended with plasticizer and colorants before pelletizing for use as molding powders.



The molecular weight of Lucite is of the order of 5×10^5 to over 10^6 (degree of polymerisation approximately 5000-10000). According to x-ray data, Lucite is substantially amorphous materials. It is soluble in aromatic and most chlorinated hydrocarbons (toulene, ethylene, dichloride, chloroform), esters (ethyl acetate), leetones, tetrahydrofurar. It will be swollen by alchols, phenols, ether and carbon tetrachloride. It can be decomposed by conc. oxidizing acids (HNO_3 , H_2SO_4 , H_2CrO_4) and alcoholic alkalis.

Lucite has density 1.18-1.19 gm cm⁻³, has the second order (glass) transition temperature at about 378 K, softens above 397 K and decomposes around 520 K. The maximum service temperature is 350 K. Its dielectric constants are 2.7-3.9 over the range 50-10⁵ Hz. Its resistivity is about 10¹⁴-10¹⁵ ohm-cm. Its dielectric strength is about 16 KV/mm for 3 mm sheet.

Lucite has specific heat 0.35, thermal conductivity 0.00188 W cm⁻¹ K⁻¹, and thermal expansion coefficient 0.75 x 10⁻⁴ K⁻¹ at 293 K (1.05 x 10⁻⁴/K at 350 K). It shrinks 0.2-0.7% when molding.

a. Normal Spectral Emittance (Wavelength Dependence)

There is no data on the normal spectral emittance of Lucite available. However, Pregelhof, Francy, and Haas [T77125] used a one-dimensional model, assuming uniform properties, and gave the emittance $\epsilon(\lambda)$, the absorptance $\alpha(\lambda)$, the transmittance $\tau(\lambda)$, and the reflectance $\rho(\lambda)$ of a polymer sheet in the following expressions:

$$\epsilon(\lambda) = \alpha(\lambda) = \frac{(1-R) [(1+R) \sinh ad + (1-R) (\cosh ad - 1)]}{(1+R^2) \sinh ad + (1-R^2) \cosh ad} \quad (4.16-1)$$

$$\tau(\lambda) = \frac{(1-R)^2}{(1+R^2) \sinh ad + (1-R^2) \cosh ad} \quad (4.16-2)$$

$$\rho(\lambda) = \frac{2R [R \sinh ad + (1-R) \cosh ad]}{(1+R^2) \sinh ad + (1-R^2) \cosh ad} \quad (4.16-3)$$

where $R = (n - 1/n + 1)^2$ and n is the refractive index, d is the thickness of the sample, and a is the absorption coefficient.

For the Lucite bulk material, it can be assumed that

$$e^{ad} \gg R e^{-ad} \quad (4.16-4)$$

which enables eqs. (4.16-1, 4.16-2, and 4.16-3) to become the following:

$$\epsilon(\lambda) = \alpha(\lambda) \cong (1-R) [1 - (1-R) e^{-ad} - R e^{-2ad}] \quad (4.16-5)$$

$$\tau(\lambda) \cong (1-R)^2 e^{-ad} \quad (4.16-6)$$

$$\rho(\lambda) \cong R [1 + (1-2R) e^{-2ad}] \quad (4.16-7)$$

By using these equations together with the experimental data of transmittance and reflectance, the emittance can be calculated. Here we used $d = 3.2$ mm for calculation. The calculated results of the normal spectral emittance for Lucite sample with thickness 3.2 mm at 293 K are shown in Table 16-1 and Fig. 16-1 with an estimated uncertainty of about $\pm 20\%$.

TABLE 16-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ |
|-----------------|------------|-----------|------------|-----------|------------|
| THICKNESS 3.2MM | | | | | |
| T = 293 | | | | | |
| 5.240 | 0.919 | 1.92 | 0.430 | 9.00 | 0.564 |
| 6.259 | 0.901 | 1.95 | 0.430 | 9.50 | 0.967 |
| 6.290 | 0.910 | 2.00 | 0.371 | 10.00 | 0.957 |
| 6.350 | 0.910 | 2.09 | 0.699 | 10.50 | 0.959 |
| 6.364 | 0.902 | 2.13 | 0.611 | 11.00 | 0.567 |
| 6.390 | 0.890 | 2.20 | 0.950 | 11.60 | 0.971 |
| 6.374 | 0.850 | 2.43 | 0.964 | 12.00 | 0.958 |
| 6.376 | 0.772 | 2.53 | 0.951 | 12.70 | 0.977 |
| 6.391 | 0.745 | 2.58 | 0.926 | 13.00 | 0.958 |
| 6.395 | 0.705 | 2.63 | 0.927 | 13.50 | 0.970 |
| 6.403 | 0.690 | 2.66 | 0.922 | 14.00 | 0.967 |
| 6.420 | 0.610 | 3.00 | 0.565 | 14.50 | 0.963 |
| 6.510 | 0.512 | 3.00 | 0.564 | 15.00 | 0.963 |
| 6.700 | 0.312 | 3.07 | 0.974 | | |
| 6.741 | 0.009 | 3.12 | 0.563 | | |
| 6.765 | 0.007 | 3.20 | 0.666 | | |
| 6.790 | 0.007 | 3.25 | 0.970 | | |
| 6.825 | 0.005 | 3.41 | 0.950 | | |
| 6.854 | 0.020 | 3.54 | 0.562 | | |
| 6.890 | 0.005 | 3.58 | 0.564 | | |
| 6.900 | 0.004 | 3.60 | 0.970 | | |
| 6.981 | 0.263 | 3.64 | 0.971 | | |
| 7.014 | 0.111 | 3.95 | 0.957 | | |
| 7.270 | 0.009 | 4.22 | 0.963 | | |
| 7.310 | 0.074 | 4.10 | 0.567 | | |
| 7.347 | 0.250 | 4.60 | 0.568 | | |
| 7.367 | 0.311 | 4.70 | 0.972 | | |
| 7.400 | 0.250 | 5.00 | 0.971 | | |
| 7.500 | 0.201 | 5.20 | 0.974 | | |
| 7.607 | 0.145 | 5.62 | 0.975 | | |
| 7.662 | 0.600 | 5.78 | 0.961 | | |
| 7.677 | 0.160 | 6.00 | 0.958 | | |
| 7.700 | 0.070 | 6.50 | 0.973 | | |
| 7.727 | 0.732 | 6.75 | 0.972 | | |
| 7.750 | 0.510 | 7.00 | 0.970 | | |
| 7.825 | 0.341 | 7.50 | 0.977 | | |
| 7.877 | 0.365 | 8.00 | 0.973 | | |
| 7.890 | 0.617 | 8.50 | 0.962 | | |
| 7.900 | 0.700 | 8.75 | 0.957 | | |

THICKNESS 3.2MM

T = 293

THICKNESS 3.2MM

T = 293 (CONT.)

THICKNESS 3.2MM

T = 293 (CONT.)

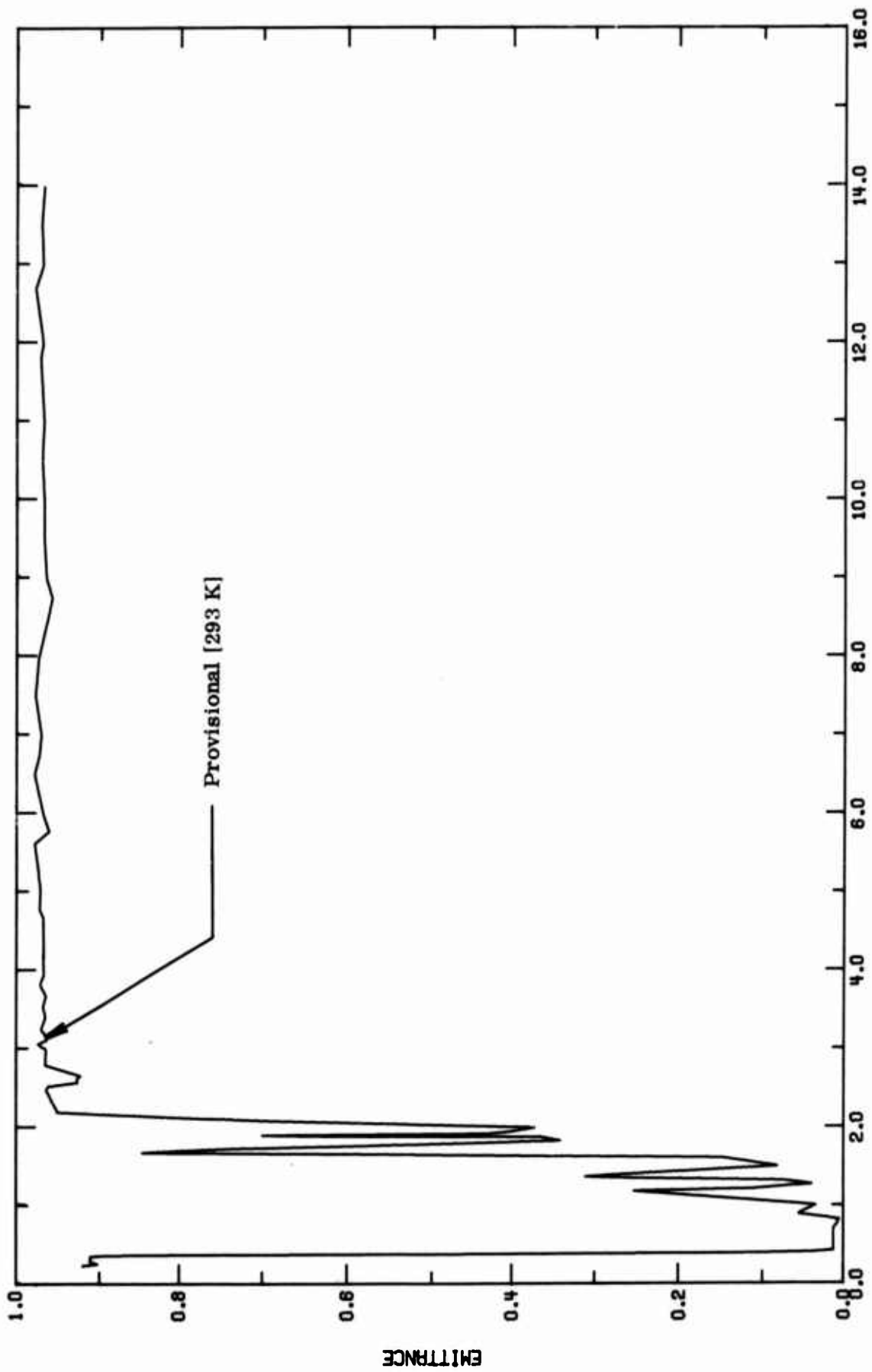


FIGURE 16-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF LUCITE
(WAVELENGTH DEPENDENCE).

b. Normal Spectral Reflectance (Wavelength Dependence)

Only Byrne and Mancinilli [T32388] have measured the normal spectral reflectance for a 3.2 mm thick specimen in the 0.24 to 2.6 μm region. Grim, Linford, Dillow, Spinak, and Mills [A00001] measured the angular spectral reflectance for a 290 mil thick disk of Plexiglas in the 2-15 μm region with the incident angle of 15° and 45° . The reflectance value increases slightly with the increase of the incident angle.

Pregelhof, Francy, and Haas [T77125] calculated the absorption coefficient $a = 20 \text{ cm}^{-1}$ or larger in the wavelength region $\lambda > 4 \mu\text{m}$. Then, Eq. (4.16-7) becomes

$$\rho(\lambda) \approx R = (n - 1)^2 / (n + 1)^2 \quad (4.16-8)$$

which is independent of the thickness of the sample and depends only on index of refraction. However, the data of index of refraction is not available in the wavelength region above 1 μm . Thus, Eq. (4.16-8) is not applicable in this case.

Based on the three sets of experimental data and Eq. (4.16-7), the provisional values of normal spectral reflectance are presented in Table 16-2 and Figure 16-2 with an estimated uncertainty of about $\pm 30\%$.

TABLE 16-2. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ |
|-----------|--------|-----------|--------|-----------|--------|
| PLEXIGLAS | | | | | |
| T = 293 | | | | | |
| 0.24 | 0.081 | 3.25 | 0.030 | 14.3 | 0.037 |
| 0.39 | 0.092 | 3.41 | 0.035 | 15.0 | 0.037 |
| 0.51 | 0.079 | 3.54 | 0.032 | | |
| 0.80 | 0.072 | 3.68 | 0.036 | | |
| 0.94 | 0.070 | 3.80 | 0.030 | | |
| 1.08 | 0.070 | 3.84 | 0.029 | | |
| 1.19 | 0.063 | 3.95 | 0.033 | | |
| 1.27 | 0.069 | 4.00 | 0.032 | | |
| 1.33 | 0.060 | 4.16 | 0.033 | | |
| 1.46 | 0.067 | 4.68 | 0.032 | | |
| 1.54 | 0.073 | 4.78 | 0.025 | | |
| 1.60 | 0.069 | 5.00 | 0.025 | | |
| 1.65 | 0.077 | 5.29 | 0.026 | | |
| 1.79 | 0.061 | 5.62 | 0.022 | | |
| 1.82 | 0.060 | 5.78 | 0.039 | | |
| 1.89 | 0.049 | 6.00 | 0.032 | | |
| 1.96 | 0.060 | 6.50 | 0.022 | | |
| 2.09 | 0.047 | 6.75 | 0.028 | | |
| 2.15 | 0.046 | 7.00 | 0.030 | | |
| 2.21 | 0.050 | 7.30 | 0.027 | | |
| 2.40 | 0.036 | 7.50 | 0.023 | | |
| 2.53 | 0.035 | 7.75 | 0.025 | | |
| 2.58 | 0.024 | 8.00 | 0.027 | | |
| 2.63 | 0.022 | 8.50 | 0.038 | | |
| 2.66 | 0.036 | 8.75 | 0.043 | | |
| 2.69 | 0.030 | 9.00 | 0.036 | | |
| 2.70 | 0.026 | 9.50 | 0.033 | | |
| 2.73 | 0.029 | 9.73 | 0.031 | | |
| 2.76 | 0.025 | 10.00 | 0.033 | | |
| 2.80 | 0.035 | 10.50 | 0.031 | | |
| 2.84 | 0.029 | 11.0 | 0.033 | | |
| 2.90 | 0.038 | 11.8 | 0.029 | | |
| 2.96 | 0.026 | 12.0 | 0.032 | | |
| 3.00 | 0.035 | 12.4 | 0.035 | | |
| 3.07 | 0.025 | 12.7 | 0.033 | | |
| 3.12 | 0.037 | 13.0 | 0.032 | | |
| 3.17 | 0.030 | 13.5 | 0.030 | | |
| 3.20 | 0.034 | 13.8 | 0.030 | | |
| | | 14.0 | 0.033 | | |

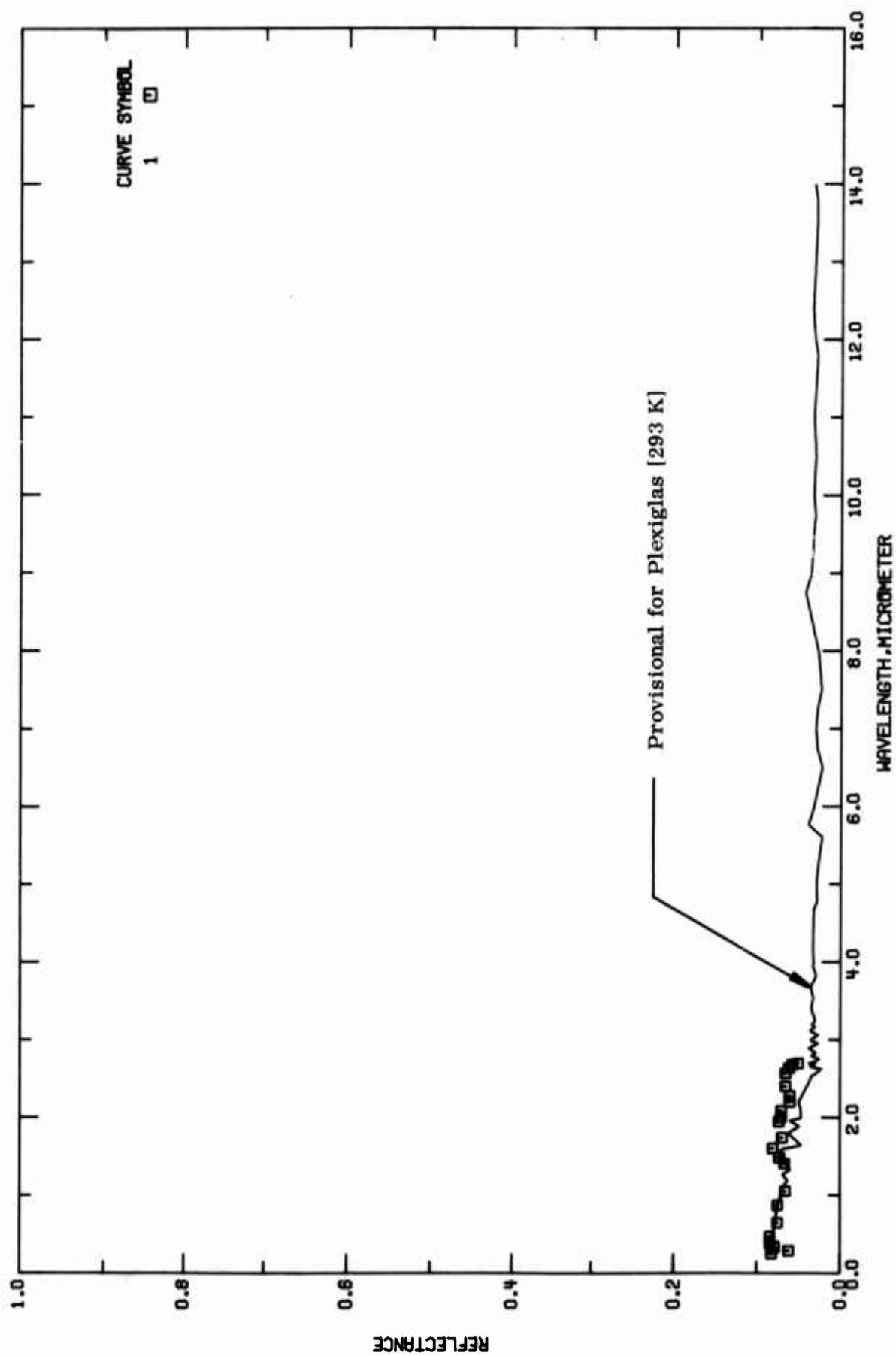
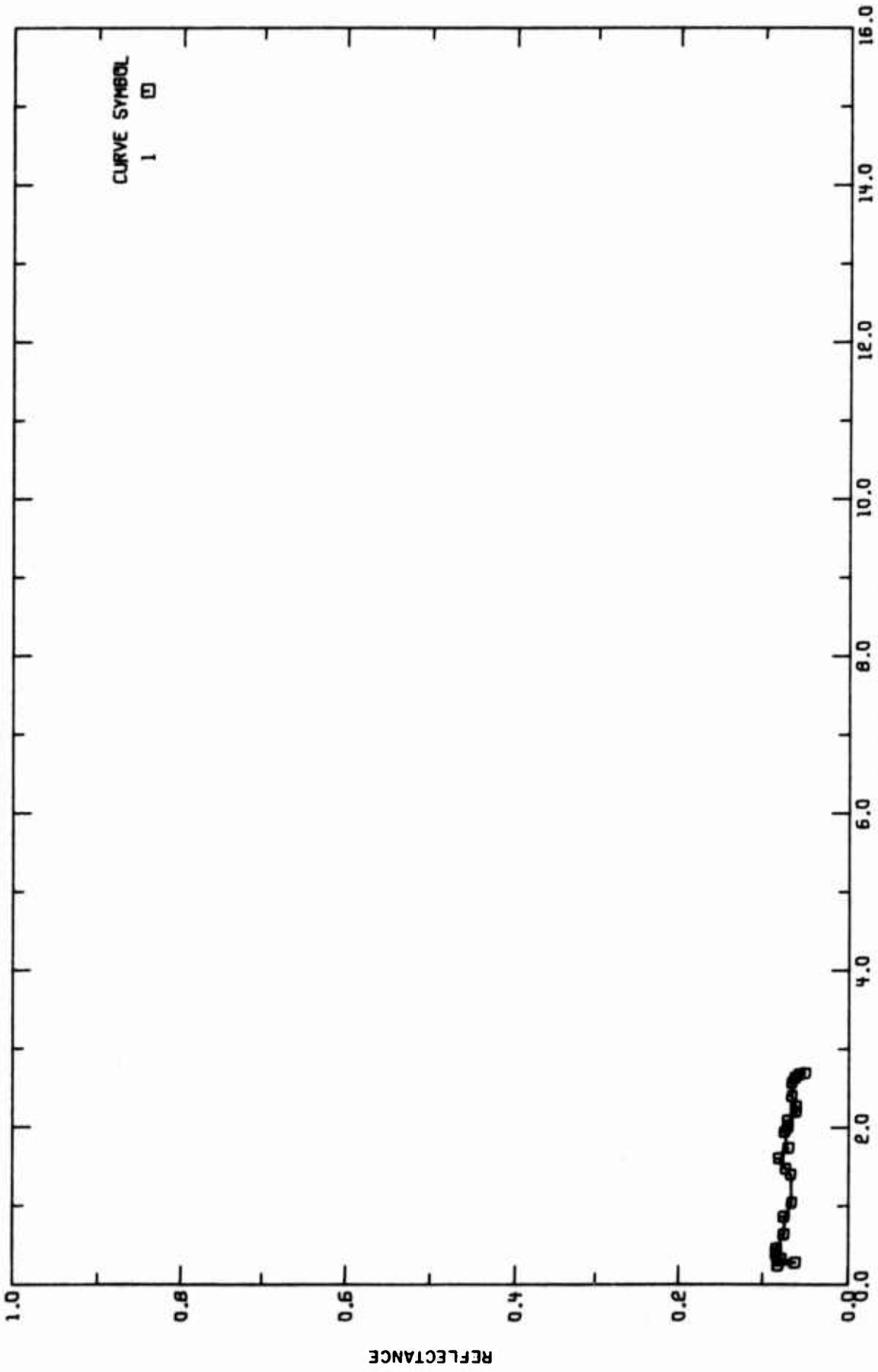


FIGURE 16-2. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE).



WAVELENGTH, MICROMETER

FIGURE 16-3. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF LUCITE
(WAVELENGTH DEPENDENCE).

TABLE 16-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF LUCITE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|------------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T32398 | Byrne, R. F. and Mancinelli, L. N. | 1954 | 0.24-2.6 | 293 | Lucite | Approx. 1/8 in. thick; General Electric Spectrometer, Beckman Spectrometer and Perkin-Elmer Spectrometer were used; data extracted from the smooth curve; $\theta=0^\circ$, $\omega'=2\pi$; reported error $\leq 5\%$. |

TABLE 16-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------|--------|
| CURVE 1 | |
| T = 293. | |
| 0.241 | 0.382 |
| 0.279 | 0.062 |
| 0.326 | 0.079 |
| 0.326 | 0.079 |
| 0.376 | 0.084 |
| 0.461 | 0.084 |
| 0.636 | 0.075 |
| 0.861 | 0.075 |
| 1.043 | 0.065 |
| 1.399 | 0.067 |
| 1.476 | 0.073 |
| 1.601 | 0.081 |
| 1.734 | 0.070 |
| 1.538 | 0.074 |
| 1.956 | 0.071 |
| 2.082 | 0.071 |
| 2.193 | 0.061 |
| 2.259 | 0.061 |
| 2.395 | 0.065 |
| 2.561 | 0.066 |
| 2.628 | 0.062 |
| 2.672 | 0.058 |
| 2.689 | 0.051 |

c. Angular Spectral Reflectance (Wavelength Dependence)

Only Grim, Linford, Dillow, Spinak, and Mills [A00001] have measured the angular spectral reflectance for a 290 mil thick disk of Plexiglas in the 2-15 μm region with the incident angle of 15° and 45° , as shown in Table 16-6 and Figure 16-5. The reflectance values increase slightly with the increasing of incident angle. The provisional values are for Plexiglas at 293 K and are listed in Table 16-5 and shown in Figure 16-4. The estimated uncertainty is about $\pm 30\%$.

TABLE 16-5. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ |
|---------------------|--------|-----------|--------|-----------|--------|
| PLEXIGLAS | | | | | |
| $\theta = 15^\circ$ | | | | | |
| T = 293 (CONT.) | | | | | |
| 0.24 | 0.081 | 3.25 | 0.030 | 14.3 | 0.037 |
| 0.39 | 0.082 | 3.41 | 0.035 | 15.0 | 0.037 |
| 0.51 | 0.079 | 3.54 | 0.032 | | |
| 0.80 | 0.075 | 3.68 | 0.036 | | |
| 0.94 | 0.072 | 3.80 | 0.030 | | |
| 1.00 | 0.070 | 3.94 | 0.029 | | |
| 1.02 | 0.072 | 3.95 | 0.033 | | |
| 1.19 | 0.063 | 4.00 | 0.032 | | |
| 1.27 | 0.059 | 4.16 | 0.033 | | |
| 1.33 | 0.050 | 4.68 | 0.032 | | |
| 1.46 | 0.067 | 4.78 | 0.029 | | |
| 1.54 | 0.073 | 5.00 | 0.029 | | |
| 1.60 | 0.069 | 5.29 | 0.026 | | |
| 1.65 | 0.047 | 5.62 | 0.022 | | |
| 1.79 | 0.061 | 5.79 | 0.029 | | |
| 1.82 | 0.060 | 6.00 | 0.032 | | |
| 1.89 | 0.049 | 6.50 | 0.022 | | |
| 1.96 | 0.060 | 6.75 | 0.026 | | |
| 2.00 | 0.047 | 7.00 | 0.030 | | |
| 2.13 | 0.048 | 7.30 | 0.027 | | |
| 2.20 | 0.050 | 7.50 | 0.023 | | |
| 2.48 | 0.036 | 7.75 | 0.025 | | |
| 2.53 | 0.035 | 8.50 | 0.027 | | |
| 2.58 | 0.028 | 8.75 | 0.038 | | |
| 2.63 | 0.022 | 9.00 | 0.043 | | |
| 2.55 | 0.036 | 9.25 | 0.036 | | |
| 2.59 | 0.030 | 9.50 | 0.033 | | |
| 2.70 | 0.038 | 9.73 | 0.031 | | |
| 2.73 | 0.029 | 10.00 | 0.033 | | |
| 2.76 | 0.025 | 10.50 | 0.031 | | |
| 2.80 | 0.035 | 11.0 | 0.033 | | |
| 2.84 | 0.029 | 11.8 | 0.029 | | |
| 2.90 | 0.038 | 12.0 | 0.032 | | |
| 2.96 | 0.026 | 12.4 | 0.035 | | |
| 3.00 | 0.036 | 12.7 | 0.033 | | |
| 3.07 | 0.026 | 13.0 | 0.032 | | |
| 3.12 | 0.037 | 13.5 | 0.030 | | |
| 3.17 | 0.033 | 13.8 | 0.030 | | |
| 3.20 | 0.034 | 14.0 | 0.033 | | |

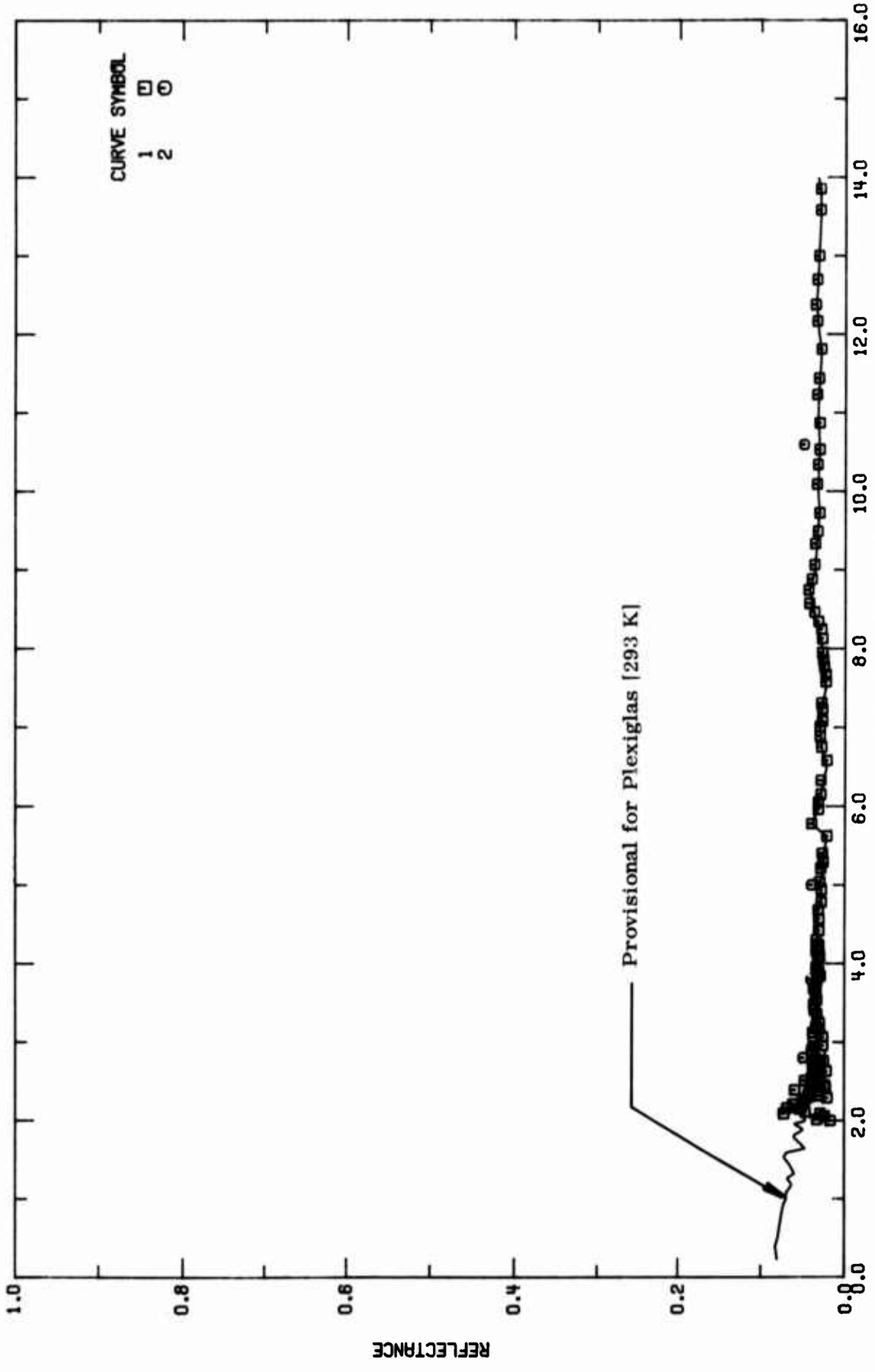


FIGURE 16-4. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE).

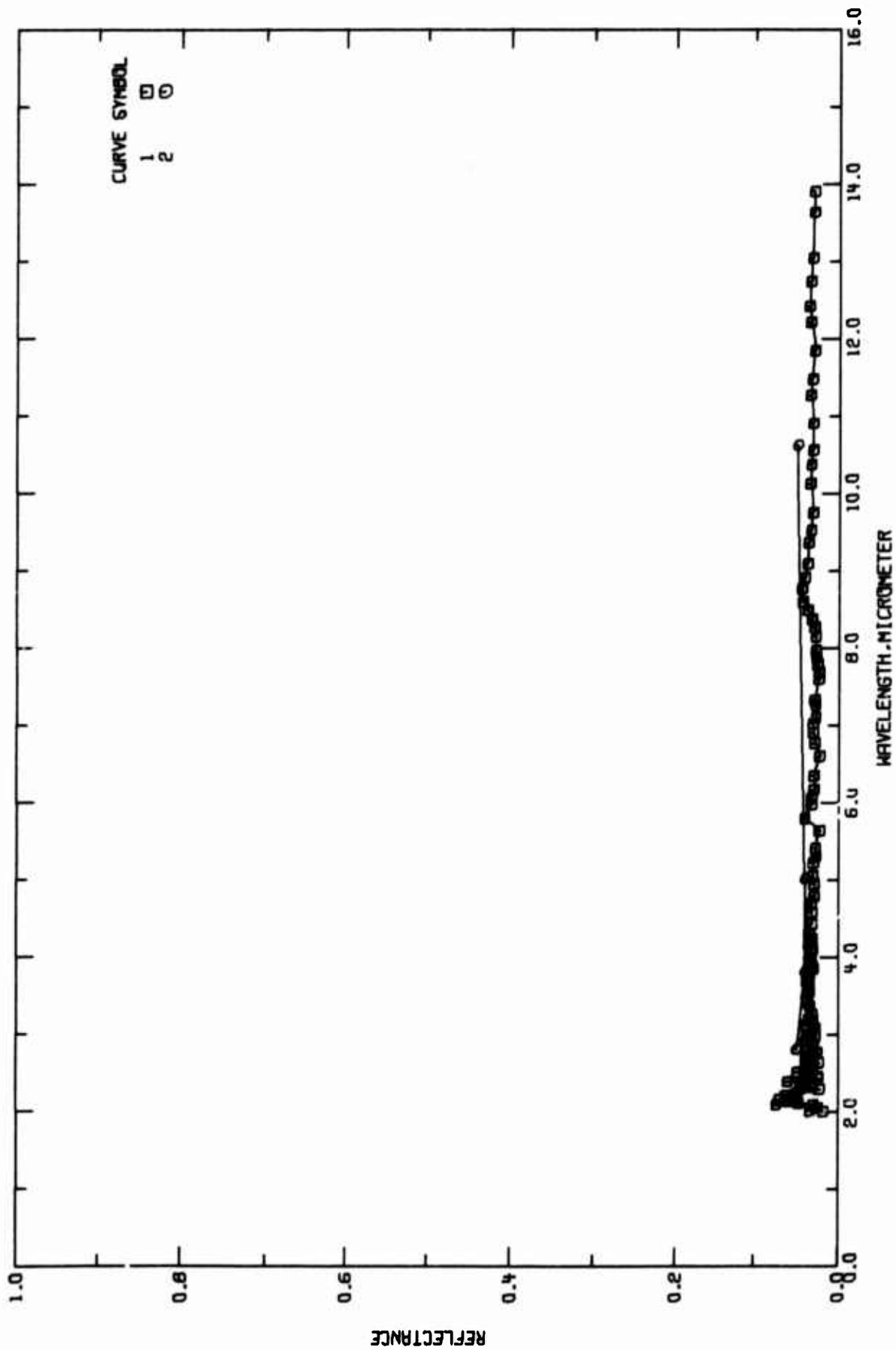


FIGURE 16-5. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE).

TABLE 16-a. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF LUCITE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | Grimm, T. C., Linford, K. M. F., Dillow, C. F., Spinak, S., and Mills, J. P. | 1972 | 2-15 | 293 | Plexiglas 55 Sample M-1 | Spectral hemispherical reflectance was measured by utilizing a Dune Associate ellipsoidal-mirror reflectometer; one in. diameter disc sample was used; data were extracted from the smooth curve; $\theta=15^\circ$, $\omega'=2\pi$. |
| 2 | Grimm, T. C., et al. | 1972 | 2-15 | 293 | Plexiglas 55 Sample M-1 | The above specimen except the incident angle $\theta=45^\circ$ and data were extracted from the table. |

TABLE 16-7. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF LUCITE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 T = 293. | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 2 (CONT.) | |
|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 2.00 | 0.017 | 3.12 | 0.030 | 7.00 | 0.027 | 3.0 | 0.04 |
| 2.01 | 0.033 | 3.17 | 0.030 | 7.24 | 0.027 | 5.0 | 0.04 |
| 2.05 | 0.024 | 3.20 | 0.034 | 7.31 | 0.028 | 10.6 | 0.05 |
| 2.09 | 0.073 | 3.25 | 0.030 | 7.58 | 0.023 | | |
| 2.09 | 0.029 | 3.36 | 0.033 | 7.67 | 0.023 | | |
| 2.11 | 0.047 | 3.41 | 0.036 | 7.77 | 0.025 | | |
| 2.15 | 0.054 | 3.48 | 0.037 | 7.86 | 0.026 | | |
| 2.16 | 0.059 | 3.54 | 0.033 | 7.95 | 0.027 | | |
| 2.19 | 0.051 | 3.63 | 0.034 | 8.13 | 0.027 | | |
| 2.21 | 0.062 | 3.68 | 0.037 | 8.25 | 0.028 | | |
| 2.24 | 0.050 | 3.73 | 0.034 | 8.35 | 0.032 | | |
| 2.27 | 0.047 | 3.78 | 0.033 | 8.47 | 0.037 | | |
| 2.29 | 0.021 | 3.84 | 0.029 | 8.59 | 0.043 | | |
| 2.30 | 0.043 | 3.88 | 0.031 | 8.75 | 0.044 | | |
| 2.32 | 0.030 | 3.95 | 0.034 | 8.89 | 0.040 | | |
| 2.34 | 0.043 | 3.98 | 0.032 | 9.07 | 0.037 | | |
| 2.37 | 0.031 | 4.04 | 0.030 | 9.34 | 0.036 | | |
| 2.39 | 0.060 | 4.09 | 0.030 | 9.50 | 0.033 | | |
| 2.43 | 0.023 | 4.16 | 0.034 | 9.73 | 0.031 | | |
| 2.45 | 0.039 | 4.23 | 0.031 | 10.10 | 0.034 | | |
| 2.45 | 0.024 | 4.30 | 0.034 | 10.35 | 0.033 | | |
| 2.47 | 0.040 | 4.42 | 0.031 | 10.54 | 0.031 | | |
| 2.49 | 0.035 | 4.57 | 0.031 | 10.88 | 0.031 | | |
| 2.51 | 0.048 | 4.68 | 0.032 | 11.24 | 0.034 | | |
| 2.53 | 0.036 | 4.78 | 0.028 | 11.45 | 0.032 | | |
| 2.55 | 0.039 | 4.94 | 0.028 | 11.82 | 0.029 | | |
| 2.57 | 0.029 | 5.04 | 0.030 | 12.18 | 0.034 | | |
| 2.63 | 0.022 | 5.21 | 0.029 | 12.39 | 0.036 | | |
| 2.66 | 0.037 | 5.29 | 0.026 | 12.71 | 0.034 | | |
| 2.69 | 0.030 | 5.40 | 0.027 | 13.01 | 0.032 | | |
| 2.70 | 0.038 | 5.62 | 0.022 | 13.60 | 0.030 | | |
| 2.73 | 0.029 | 5.78 | 0.040 | 13.87 | 0.030 | | |
| 2.76 | 0.025 | 5.96 | 0.032 | 14.02 | 0.033 | | |
| 2.79 | 0.036 | 6.05 | 0.032 | 14.29 | 0.037 | | |
| 2.84 | 0.029 | 6.15 | 0.029 | 14.67 | 0.037 | | |
| 2.90 | 0.039 | 6.33 | 0.029 | | | | |
| 2.96 | 0.026 | 6.50 | 0.022 | CURVE 2 | | | |
| 3.00 | 0.037 | 6.75 | 0.028 | T = 293. | | | |
| 3.07 | 0.026 | 6.89 | 0.030 | 2.6 | 0.05 | | |
| | | 7.01 | 0.030 | | | | |

d. Normal Spectral Absorptance (Wavelength Dependence)

Byrne and Mancinelli [T32388] measured the absorptance of a 3.2 mm thick specimen in the 0.2 to 2.7 μm region. Pilipetskii, Raizer, and Upadyshov [E37991] used a ruby laser $\lambda = 0.69 \mu\text{m}$ with incident power of 0.5-1.1 joules to obtain the absorptance for specimens 43 mm long. According to Eq. (4.16-5), $\alpha(\lambda) \cong (1-R) [1 - (1-R)e^{-ad} - Re^{-2ad}]$ which is strongly dependent on the thickness of thin films. However, for the bulk materials in the wavelength region $\lambda > 3 \mu\text{m}$

$$\alpha(\lambda) \approx (1-R) \quad (4.16-9)$$

which is independent of the thickness, and the material becomes opaque. From Kirchhoff's law $\alpha(\lambda) = \epsilon(\lambda)$, the absorptance is equal to emittance. The calculated values are shown in Table 16-8 and in Figure 16-6 together with the experimental results.

The estimated uncertainty is about $\pm 20\%$.

TABLE 16-8. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α | λ | α |
|-----------------|----------|-----------|----------|-----------|----------|
| THICKNESS 3.2MM | | | | | |
| T = 293 | | | | | |
| 0.240 | 0.919 | 1.92 | 0.430 | 9.33 | 0.964 |
| 0.259 | 0.981 | 1.95 | 0.400 | 9.50 | 0.967 |
| 0.290 | 0.910 | 2.00 | 0.371 | 10.00 | 0.957 |
| 0.350 | 0.910 | 2.09 | 0.699 | 10.50 | 0.969 |
| 0.364 | 0.902 | 2.13 | 0.811 | 11.00 | 0.967 |
| 0.369 | 0.890 | 2.20 | 0.950 | 11.80 | 0.971 |
| 0.374 | 0.855 | 2.28 | 0.984 | 12.00 | 0.968 |
| 0.376 | 0.772 | 2.33 | 0.961 | 12.70 | 0.977 |
| 0.389 | 0.745 | 2.39 | 0.920 | 13.00 | 0.968 |
| 0.396 | 0.700 | 2.63 | 0.927 | 13.50 | 0.970 |
| 0.403 | 0.640 | 2.66 | 0.922 | 14.00 | 0.967 |
| 0.422 | 0.612 | 2.80 | 0.985 | 14.50 | 0.963 |
| 0.510 | 0.612 | 3.00 | 0.964 | 15.00 | 0.963 |
| 0.700 | 0.612 | 3.07 | 0.974 | | |
| 0.741 | 0.639 | 3.12 | 0.963 | | |
| 0.763 | 0.637 | 3.20 | 0.966 | | |
| 0.788 | 0.607 | 3.25 | 0.970 | | |
| 0.815 | 0.635 | 3.41 | 0.965 | | |
| 0.844 | 0.620 | 3.54 | 0.968 | | |
| 0.890 | 0.656 | 3.69 | 0.984 | | |
| 1.000 | 0.654 | 3.80 | 0.970 | | |
| 1.181 | 0.653 | 3.84 | 0.971 | | |
| 1.214 | 0.611 | 3.92 | 0.967 | | |
| 1.270 | 0.639 | 4.22 | 0.966 | | |
| 1.318 | 0.674 | 4.16 | 0.957 | | |
| 1.347 | 0.650 | 4.68 | 0.968 | | |
| 1.367 | 0.611 | 4.78 | 0.972 | | |
| 1.400 | 0.658 | 5.00 | 0.971 | | |
| 1.500 | 0.681 | 5.29 | 0.974 | | |
| 1.607 | 0.648 | 5.62 | 0.978 | | |
| 1.662 | 0.600 | 5.78 | 0.961 | | |
| 1.677 | 0.645 | 6.00 | 0.968 | | |
| 1.759 | 0.778 | 6.50 | 0.978 | | |
| 1.727 | 0.732 | 6.75 | 0.972 | | |
| 1.764 | 0.510 | 7.05 | 0.970 | | |
| 1.826 | 0.640 | 7.50 | 0.977 | | |
| 1.877 | 0.655 | 8.00 | 0.973 | | |
| 1.890 | 0.637 | 8.50 | 0.952 | | |
| 1.900 | 0.700 | 8.75 | 0.957 | | |
| THICKNESS 3.2MM | | | | | |
| T = 293 (CONT.) | | | | | |

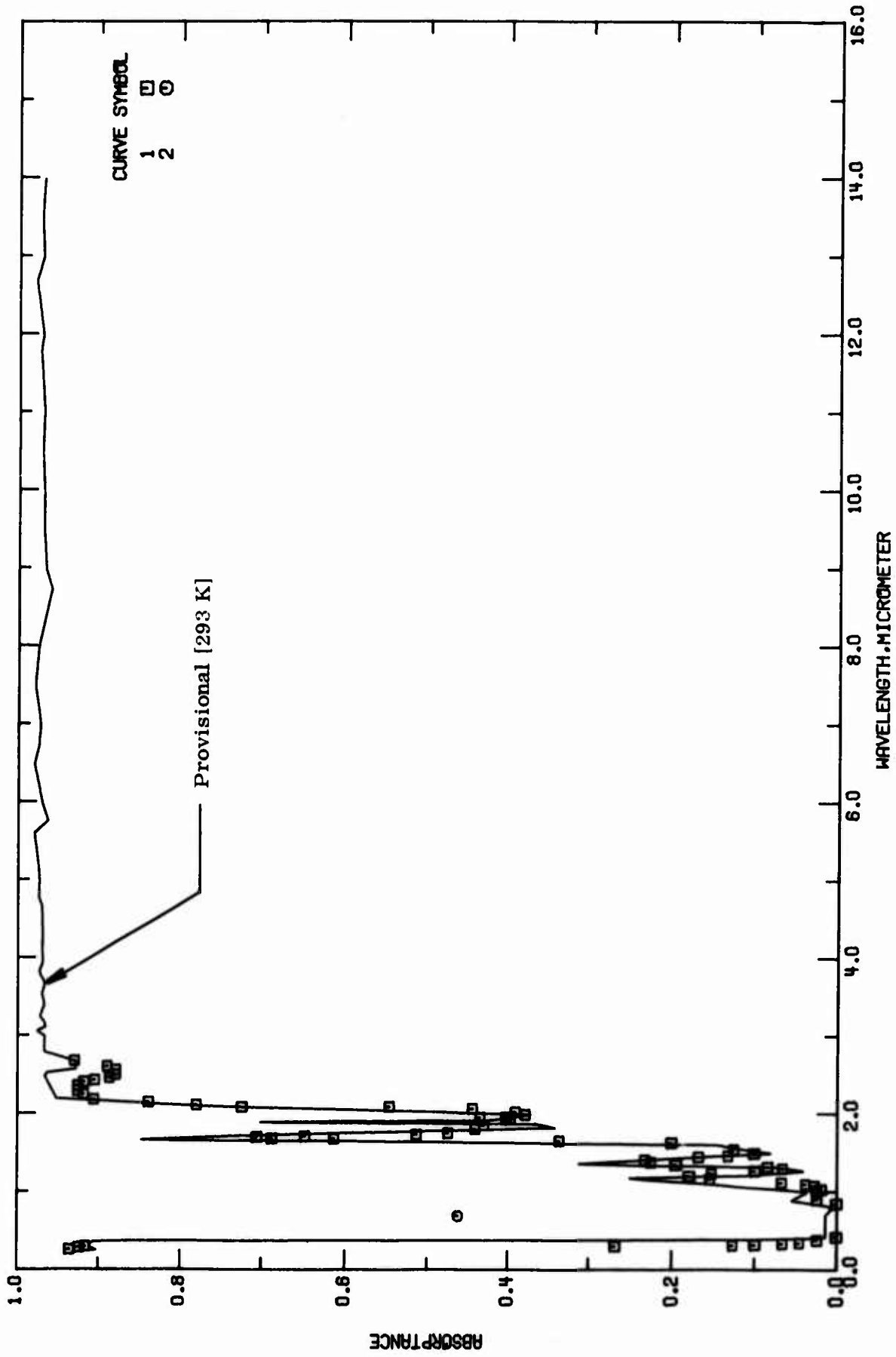


FIGURE 16-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE).

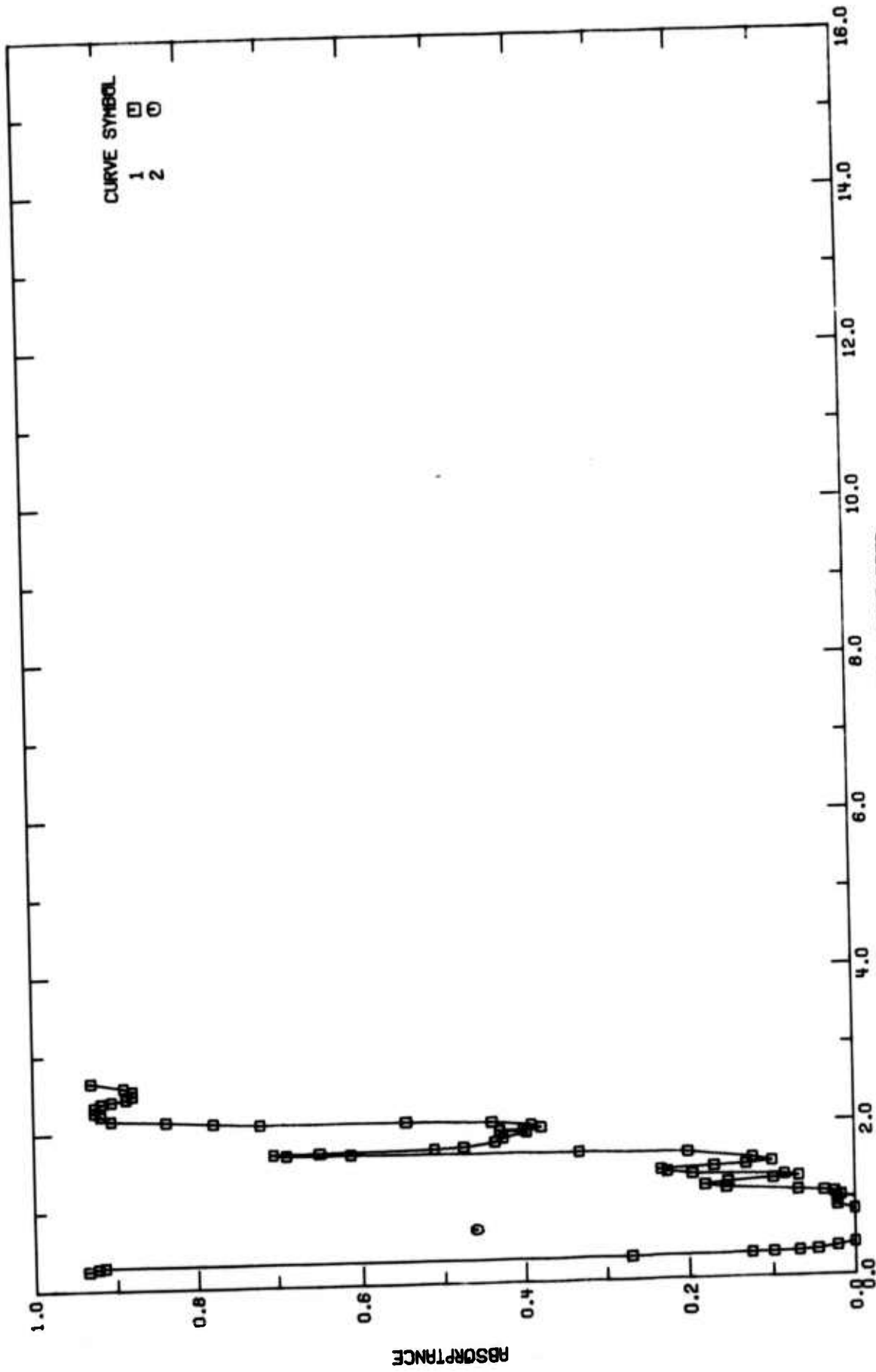


FIGURE 16-7. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE).

TABLE 16-9. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF LUCITE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T32389 | Byrne, R. T. and Mancinelli, L. N. | 1954 | 0.2-2.7 | ~293 | Lucite | Approx. 1/8 in. thick specimen; Beckman Spectrometer, General Electric Spectrometer and Perkin-Elmer Spectrometer were employed; data were extracted from the smooth curve; $9 \sim 0^\circ$, reported error 5%. |
| 2 E37991 | Philipetsidi, N. F., Raizer, Yu. P., and Upadyshev, V. A. | 1968 | 0.69 | ~293 | PMA | Polymethylmeth acrylate sample of dimension $43 \times 9 \times 9$ mm; ruby laser with incident power about 0.5-1.1 Joules was used; $9 \sim 0^\circ$, reported error 9%. |

TABLE 16-10. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|-----------|----------|-----------|----------|
| CURVE 1 | | | |
| T = 293. | | | |
| 0.260 | 0.934 | 1.860 | 0.428 |
| 0.285 | 0.922 | 1.930 | 0.396 |
| 0.296 | 0.914 | 1.956 | 0.433 |
| 0.298 | 0.270 | 1.956 | 0.401 |
| 0.309 | 0.126 | 1.992 | 0.378 |
| 0.316 | 0.099 | 2.024 | 0.390 |
| 3.326 | 0.067 | 2.069 | 0.442 |
| 0.337 | 0.045 | 2.094 | 0.545 |
| 0.375 | 0.022 | 2.094 | 0.721 |
| 0.410 | 0.000 | 2.123 | 0.777 |
| 0.843 | 0.000 | 2.157 | 0.837 |
| 0.899 | 0.022 | 2.182 | 0.904 |
| 0.999 | 0.022 | 2.252 | 0.917 |
| 1.027 | 0.017 | 2.298 | 0.924 |
| 1.073 | 0.025 | 2.362 | 0.924 |
| 1.098 | 0.937 | 2.408 | 0.916 |
| 1.112 | 0.068 | 2.431 | 0.903 |
| 1.156 | 0.156 | 2.464 | 0.884 |
| 1.196 | 0.181 | 2.504 | 0.876 |
| 1.230 | 0.154 | 2.564 | 0.876 |
| 1.264 | 0.399 | 2.608 | 0.887 |
| 1.290 | 0.067 | 2.682 | 0.928 |
| 1.315 | 0.085 | CURVE 2 | |
| 1.345 | 0.195 | T = 293. | |
| 1.378 | 0.225 | 0.69 | 0.46 |
| 1.408 | 0.233 | | |
| 1.441 | 0.170 | | |
| 1.456 | 0.132 | | |
| 1.491 | 0.100 | | |
| 1.539 | 0.124 | | |
| 1.628 | 0.200 | | |
| 1.657 | 0.335 | | |
| 1.682 | 0.612 | | |
| 1.688 | 0.687 | | |
| 1.705 | 0.704 | | |
| 1.712 | 0.648 | | |
| 1.737 | 0.512 | | |
| 1.755 | 0.473 | | |
| 1.811 | 0.439 | | |

e. Normal Spectral Transmittance (Wavelength Dependence)

There are 20 sets of experimental data available for the transmittance of Lucite as listed in Table 16-13. Of these, 12 sets measured on thin film samples are shown in Figure 16-10. They represent reasonably consistent results with each other. Major absorption peaks near $\lambda = 3.4, 5.8, 6.9, 7.2, 8.0, 8.7,$ and $13.4 \mu\text{m}$ are observed.

As we have mentioned in d., the bulk Lucite materials become opaque above $\lambda = 3 \mu\text{m}$. At the visible and near infrared region it transmits about 90%. According to Eq. (4.16-6), $\tau(\lambda) = (1-R)^2 e^{-ad}$, the transmittance becomes very strongly dependent on the thickness of the sample where absorption coefficient a is not small. Therefore, the provisional values of transmittance for a sample with thickness of 3.2 mm at 293 K are derived, based on the works of Byrne and Mancinelli [T32388], Acitelli, Gumby, and Naujobas [T40338], Turner and Keller [T77381], and duPont Co. [E62601]. The values are shown in Table 16-11 and in Figure 16-8 with the experimental data.

The provisional values are estimated with an uncertainty of about $\pm 30\%$.

TABLE 16-11. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T |
|-----------------|-------|-----------|-------|-----------|------|
| THICKNESS 3.2MM | | | | | |
| T = 293 | | | | | |
| 0.250 | 0.300 | 1.828 | 0.600 | 11.50 | 0.00 |
| 0.259 | 0.013 | 1.877 | 0.585 | 12.00 | 0.00 |
| 0.261 | 0.041 | 1.886 | 0.333 | 12.50 | 0.00 |
| 0.262 | 0.018 | 1.899 | 0.253 | 13.00 | 0.00 |
| 0.264 | 0.013 | 1.909 | 0.271 | 13.50 | 0.00 |
| 0.268 | 0.000 | 1.909 | 0.319 | 14.00 | 0.00 |
| 0.357 | 0.030 | 1.914 | 0.339 | 14.50 | 0.00 |
| 0.364 | 0.015 | 1.916 | 0.456 | 15.00 | 0.00 |
| 0.369 | 0.030 | 1.924 | 0.470 | | |
| 0.374 | 0.069 | 1.928 | 0.502 | | |
| 0.376 | 0.146 | 1.950 | 0.444 | | |
| 0.389 | 0.775 | 2.00 | 0.582 | | |
| 0.398 | 0.917 | 2.09 | 0.251 | | |
| 0.403 | 0.680 | 2.13 | 0.141 | | |
| 0.422 | 0.903 | 2.20 | 0.000 | | |
| 0.510 | 0.908 | 2.48 | 0.000 | | |
| 0.700 | 0.912 | 2.53 | 0.003 | | |
| 0.741 | 0.916 | 2.58 | 0.046 | | |
| 0.765 | 0.513 | 2.61 | 0.060 | | |
| 0.788 | 0.918 | 2.63 | 0.051 | | |
| 0.815 | 0.923 | 2.65 | 0.042 | | |
| 0.844 | 0.922 | 2.80 | 0.000 | | |
| 0.890 | 0.874 | 3.00 | 0.003 | | |
| 1.000 | 0.356 | 3.80 | 0.001 | | |
| 1.181 | 0.694 | 4.00 | 0.005 | | |
| 1.214 | 0.325 | 4.50 | 0.004 | | |
| 1.259 | 0.392 | 5.00 | 0.00 | | |
| 1.318 | 0.866 | 5.50 | 0.00 | | |
| 1.347 | 0.692 | 6.00 | 0.00 | | |
| 1.367 | 0.629 | 6.50 | 0.00 | | |
| 1.400 | 0.679 | 7.00 | 0.00 | | |
| 1.500 | 0.849 | 7.50 | 0.00 | | |
| 1.607 | 0.763 | 8.00 | 0.00 | | |
| 1.662 | 0.355 | 8.50 | 0.00 | | |
| 1.670 | 0.134 | 9.00 | 0.00 | | |
| 1.677 | 0.104 | 9.50 | 0.00 | | |
| 1.709 | 0.170 | 10.00 | 0.00 | | |
| 1.727 | 0.209 | 10.50 | 0.00 | | |
| 1.784 | 0.429 | 11.00 | 0.00 | | |
| THICKNESS 3.2MM | | | | | |
| T = 293 (CONT.) | | | | | |
| | | | | | |

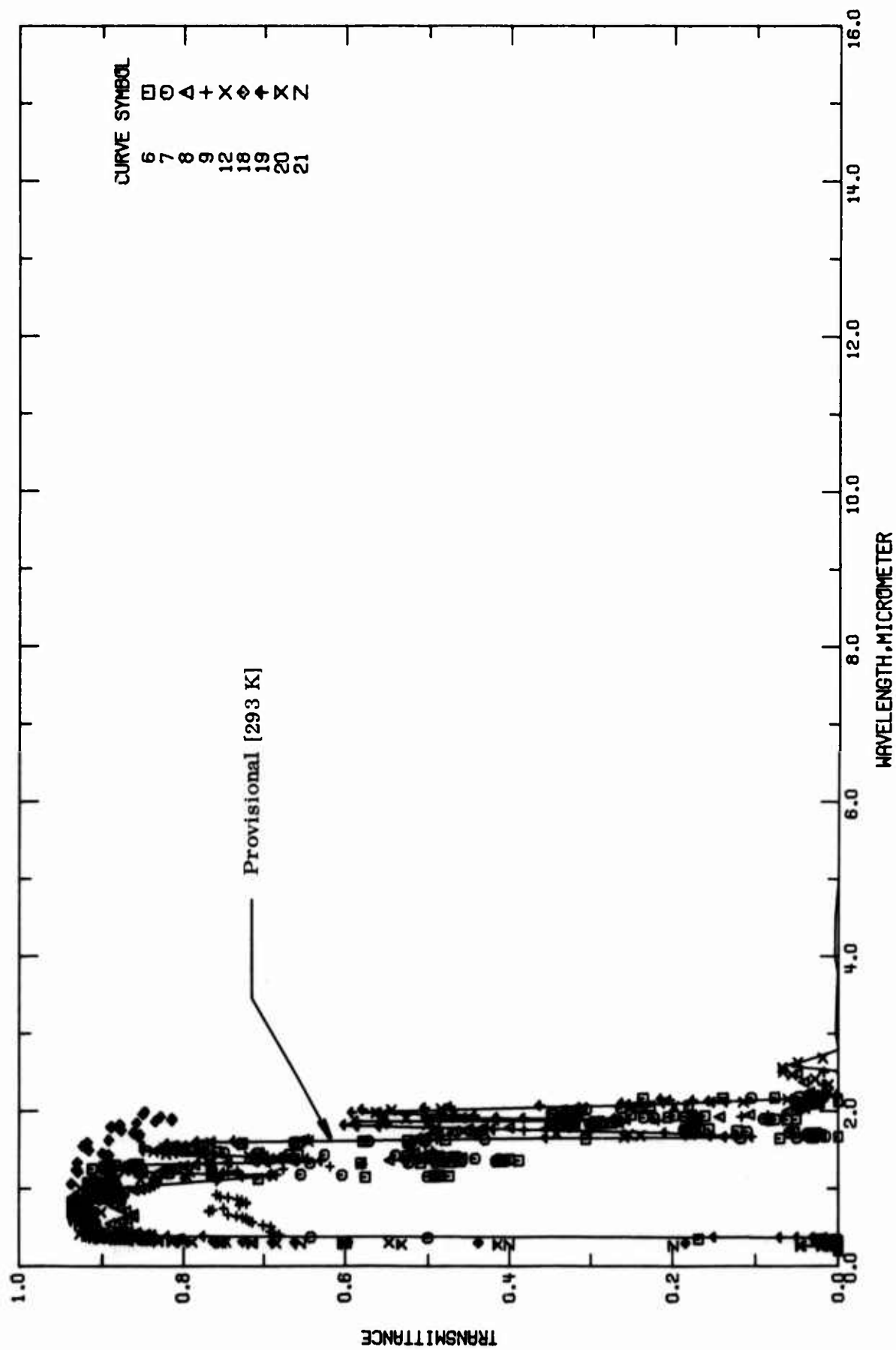


FIGURE 16-8. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE).

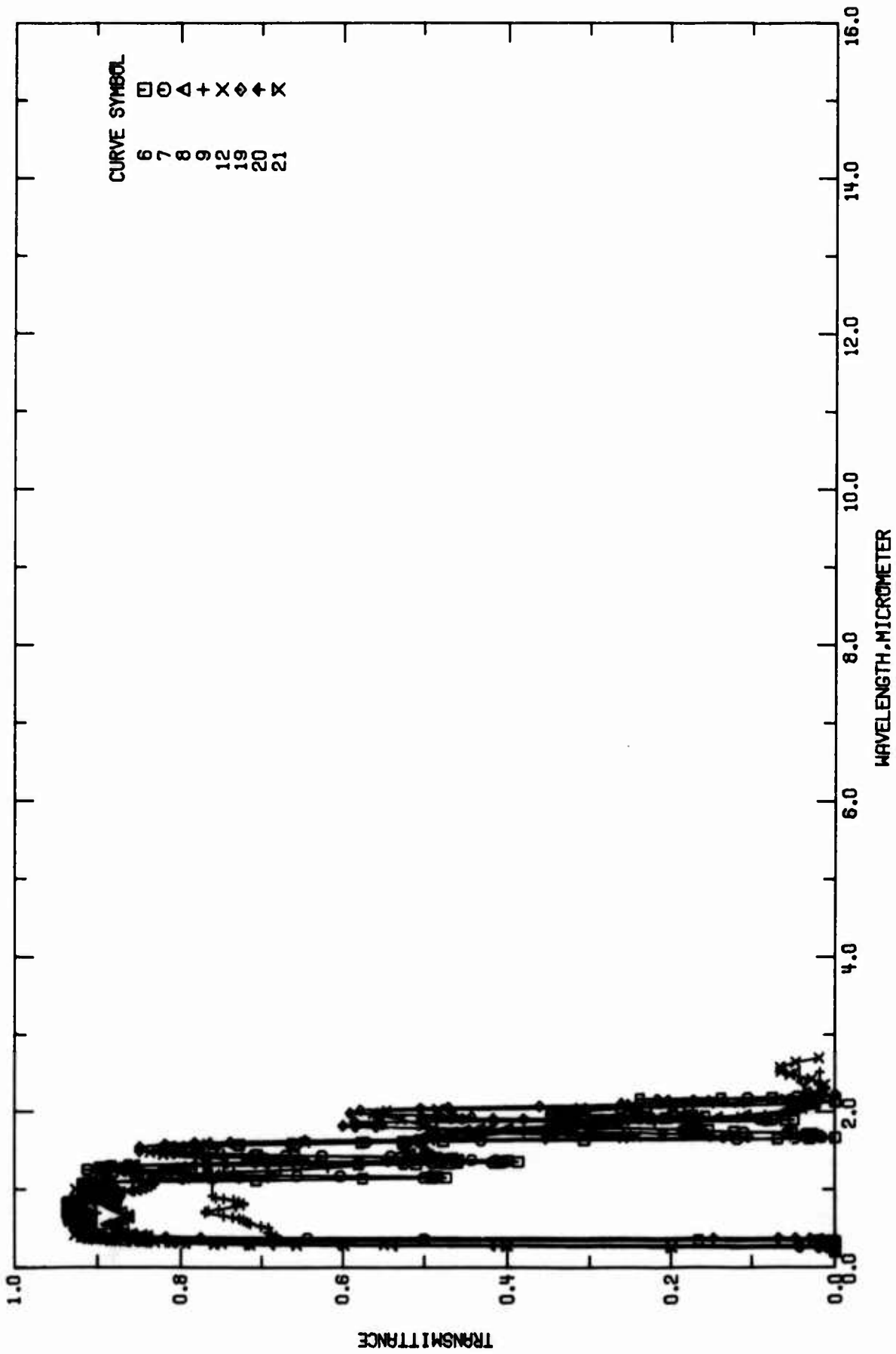


FIGURE 16-9. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE).

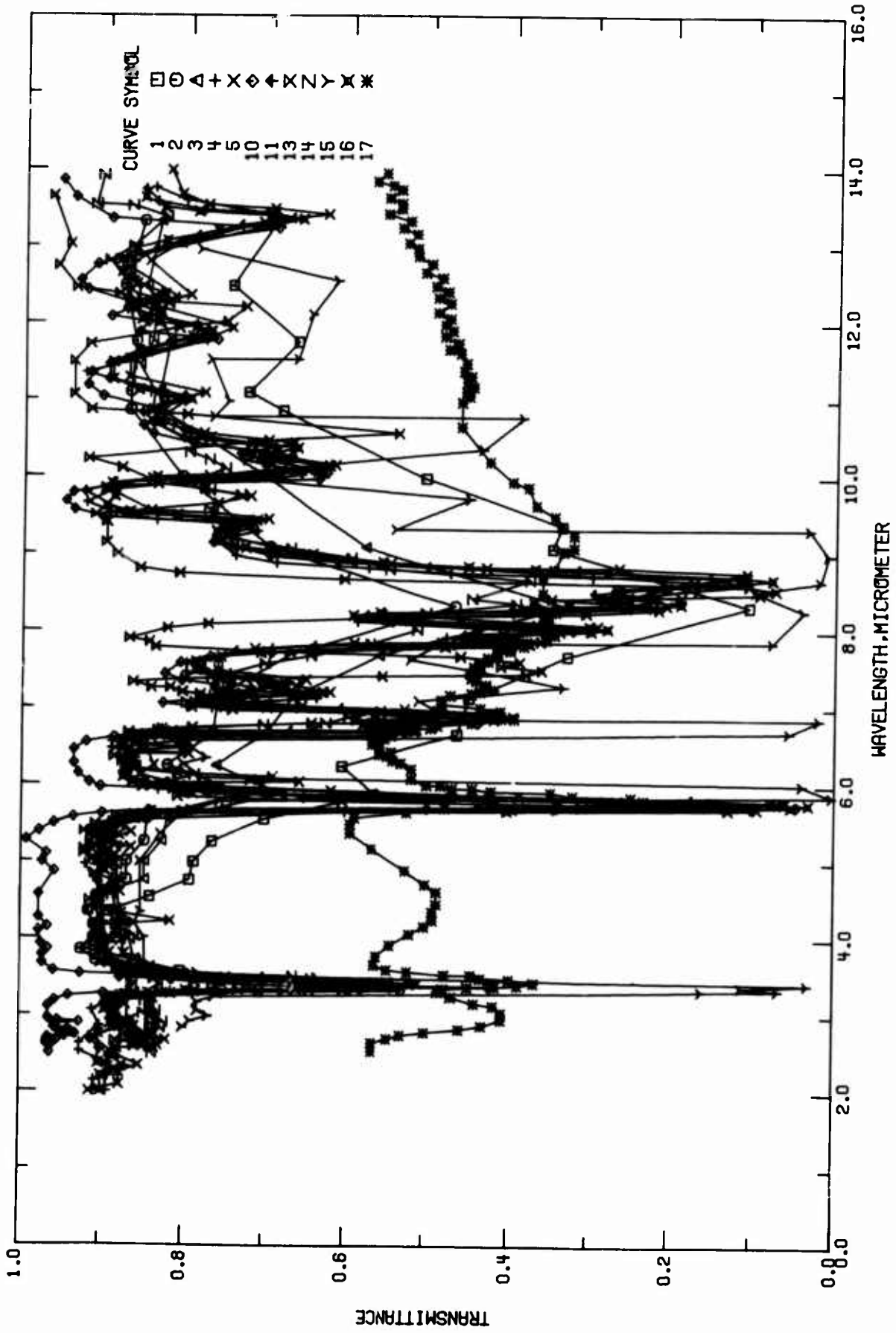


FIGURE 16-10. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE THIN FILMS (WAVELENGTH DEPENDENCE).

TABLE 16-12. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|------------------------------------|--|
| 1 T40581 | Wells, A.J. | 1940 | 3.3-25 | 293 | Lucite | Films were made from the powder of DuPont Co. by mercury and dip method; film thickness 25 μ ; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 2 T40581 | Wells, A.J. | 1940 | 3.3-25 | 293 | Plexiglas | 5 μ thickness sheet was obtained from the Röme and Haas Co.; films were made by mercury method; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 3 T40581 | Wells, A.J. | 1940 | 3.3-25 | 293 | Plexiglas | The above specimen except 7 μ thickness. |
| 4 T24947 | Armour Research Foundation | 1961 | 2-15 | 293 | Lucite | 0.01 in. thickness sample was deposited on the surface of sodium chloride discs, it transmit well in the 2-6 μ and 9.5-15 μ spectral region; in the visible region, its refractive index is 1.49; curing temperature = 54 C; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 5 T19814 | Moore, L.E., Trampkin, M., Tompkins, E.H., and VanOsterburg, D.O. | 1958 | 2-15 | 293 | Lucite | Refractive index = 1.49 at $\lambda = 5893 \text{ \AA}$; unknown thickness; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 6 T40328 | Acitelli, M.A., Gurnby, W.L., and Naujokas, A.A. | 1966 | 0.3-2.2 | 296 | Poly(methyl methacrylate) | 7.46 mm thickness disc about 50 mm in diameter; Cary Spectrophotometer model 14 was employed; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 7 T40338 | Acitelli, M.A., et al. | 1966 | 0.3-2.2 | 296 | Poly(methyl methacrylate) | The above specimen after 100 standard fade hr in solarization. |
| 8 T47094 | Holland, W.R. | 1967 | 0.2-2.6 | 296 | Cross linked methacrylate | 1/4 in. thick; the transmittance was measured by using a Perkin-Elmer model 99 mono-chrometer; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 9 T47094 | Holland, W.R. | 1967 | 0.2-2.6 | 296 | Cross linked methacrylate | The above specimen except it was indicated by simulated sunlight for 14 days, 30 days, 60 days and 90 days respectively. |
| 10 T76795 | Simler, S.S. and Kaganise, R.E. | 1966 | 2.5-25 | ~293 | Lucite 763497 | A Beckman model IR-12 spectrophotometer was used to obtain the spectra of film sample; specimen was obtained from DuPont; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 11 T31594 | Story, J.G. | 1961 | 2-15 | 296 | Polymethyl methacrylate | No thickness has been given; the absorption peak at 3.37 μ indicating absence of long chains of CH_2 groups; strong absorption at 5.77 μ due to the C-O bond and strong absorption at 8 to 9 μ region, probably due to C-O-C stretching made; data were extracted from the figure. |
| 12 T32238 | Byrne, R.F. and Maddicelli, L.N. | 1954 | 0.2-2.7 | 293 | Lucite | Approx. 1/8 in. thick; for the ultraviolet region Beckman Model DC Spectrometer was used; for the visible and near infrared region a General Electric Recording Spectrometer was used; for the measurement above 1 μm , a Perkin-Elmer Infrared Spectrometer was employed; data were extracted from the figure. |
| 13 T76798 | Lara, M.O. | 1967 | 2.5-25 | ~293 | Lucite | The specimen was condensed pyrolyzate on potassium bromide or sodium chloride; a Beckman IR-9 double beam, prism-grating infrared spectrophotometer was used to obtain the spectra; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 14 T76798 | Lara, M.O. | 1967 | 2.5-25 | ~293 | Plexiglass | Similar to the above specimen. |
| 15 T35117 | Hass, M. and O'Hara, M. | 1965 | 2.86-100 | ~293 | DP Polymethyl methacrylate grating | 0.051 μm thickness specimen was obtained from diffraction products; a Perkin-Elmer model and a Cary Spectrometer were used for measurements; data were extracted from the figure; $\theta \sim 0^\circ$. |

TABLE 16-12. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μ m | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------------------------------|------|---------------------------|----------------------|--------------------------------|--|
| 16 T76812 | Kagarise, R. E. and Weinberger, L. A. | 1954 | 2-15 | ~293 | Plexiglas B | The specimen was obtained from Rohm and Haas Co.; the specimen was dissolved in methylethyl ketone and the resulting viscous solution spread uniformly over a rock salt or KBr plate, the solvent was removed by heating under vacuum or normal evaporation at room temperature; a Perkin-Elmer model 21 spectrometer was used; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 17 E26638 | Carbajal, B. G., III. | 1966 | 2.5-25 | ~293 | GDP MMA | Glow discharge polymerized methymethacrylate; data were extracted from the smooth curve. |
| 18 T77381 | Turner, H. C. and Keller, E. E. | 1959 | 0.185-2.0 | ~293 | Plexiglas | Beckman DK-2 spectrorflectometer was used for measurement; data were extracted from the figure; $\theta \sim 0^\circ$. |
| 19 E62501 | du Pont Co. | 1968 | 0.20-2.30 | ~293 | Lucite 129, 130, 140, 147, 148 | 3.2 mm thickness; index of refraction = 1.491; dispersion = 54; data were extracted from the figure. |
| 20 E62601 | du Pont Co. | 1968 | 0.2-0.7 | ~293 | Lucite 140 T | 3.2 mm thickness; data were extracted from the figure. |
| 21 E16981 | Imperial Chemical Industries, Ltd. | 1962 | 0.25-0.7 | ~293 | "Daikon" MG | 0.125 in. thickness; disc specimen; data were extracted from the figure. |

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| CURVE 1 | | | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | |
| 3.35 | 0.762 | 3.45 | 0.862 | 3.55 | 0.896 | 3.66 | 0.906 | 7.46 | 0.799 | 12.74 | 0.878 | 12.85 | 0.878 | 13.36 | 0.665 |
| 3.45 | 0.751 | 3.70 | 0.904 | 4.00 | 0.907 | 3.21 | 0.878 | 7.57 | 0.799 | 13.61 | 0.805 | 13.77 | 0.843 | 14.10 | 0.810 |
| 3.57 | 0.802 | 3.85 | 0.923 | 4.35 | 0.914 | 3.33 | 0.680 | 7.78 | 0.693 | 14.24 | 0.810 | 14.65 | 0.810 | 14.77 | 0.797 |
| 3.70 | 0.857 | 4.00 | 0.907 | 4.55 | 0.904 | 3.36 | 0.532 | 7.84 | 0.403 | 14.96 | 0.810 | | | | |
| 3.85 | 0.914 | 4.17 | 0.907 | 4.76 | 0.849 | 3.47 | 0.622 | 7.93 | 0.478 | | | | | | |
| 4.00 | 0.880 | 4.35 | 0.914 | 5.26 | 0.827 | 3.53 | 0.806 | 8.02 | 0.349 | | | | | | |
| 4.17 | 0.880 | 4.55 | 0.904 | 5.56 | 0.820 | 3.60 | 0.868 | 8.13 | 0.500 | | | | | | |
| 4.35 | 0.889 | 4.76 | 0.870 | 5.88 | 0.680 | 3.78 | 0.895 | 8.25 | 0.398 | | | | | | |
| 4.55 | 0.841 | 5.00 | 0.870 | 6.25 | 0.762 | 4.20 | 0.895 | 8.33 | 0.228 | | | | | | |
| 4.76 | 0.792 | 5.26 | 0.846 | 6.67 | 0.700 | 4.41 | 0.907 | 8.43 | 0.289 | | | | | | |
| 5.00 | 0.787 | 5.56 | 0.728 | 7.14 | 0.667 | 4.58 | 0.898 | 8.56 | 0.172 | | | | | | |
| 5.26 | 0.765 | 5.88 | 0.821 | 7.69 | 0.560 | 4.96 | 0.918 | 8.62 | 0.111 | | | | | | |
| 5.56 | 0.700 | 6.25 | 0.766 | 8.33 | 0.332 | 5.07 | 0.918 | 8.73 | 0.153 | | | | | | |
| 5.88 | 0.564 | 6.67 | 0.760 | 9.09 | 0.579 | 5.43 | 0.889 | 8.77 | 0.474 | | | | | | |
| 6.25 | 0.605 | 7.14 | 0.671 | 10.00 | 0.702 | 5.54 | 0.847 | 8.83 | 0.575 | | | | | | |
| 6.67 | 0.464 | 7.63 | 0.468 | 10.87 | 0.835 | 5.65 | 0.602 | 8.98 | 0.689 | | | | | | |
| 7.14 | 0.450 | 8.09 | 0.697 | 11.11 | 0.835 | 5.70 | 0.346 | 9.08 | 0.739 | | | | | | |
| 7.69 | 0.328 | 9.09 | 0.806 | 11.76 | 0.823 | 5.74 | 0.097 | 9.17 | 0.765 | | | | | | |
| 8.33 | 0.185 | 10.00 | 0.871 | 12.50 | 0.853 | 5.81 | 0.286 | 9.30 | 0.713 | | | | | | |
| 9.09 | 0.346 | 10.87 | 0.871 | 13.33 | 0.835 | 5.83 | 0.651 | 9.42 | 0.743 | | | | | | |
| 9.38 | 0.336 | 11.11 | 0.865 | 14.29 | 0.840 | 5.93 | 0.703 | 9.44 | 0.838 | | | | | | |
| 10.00 | 0.503 | 11.76 | 0.879 | 15.38 | 0.863 | 5.93 | 0.832 | 9.52 | 0.888 | | | | | | |
| 10.87 | 0.682 | 12.50 | 0.85E | 16.67 | 0.863 | 6.08 | 0.868 | 9.66 | 0.921 | | | | | | |
| 11.11 | 0.724 | 13.33 | 0.851 | 18.18 | 0.861 | 6.29 | 0.860 | 9.83 | 0.890 | | | | | | |
| 11.76 | 0.653 | 14.29 | 0.890 | 20.00 | 0.835 | 6.42 | 0.868 | 9.95 | 0.783 | | | | | | |
| 12.50 | 0.745 | 15.38 | 0.879 | 22.22 | 0.891 | 6.42 | 0.888 | 10.00 | 0.683 | | | | | | |
| 13.33 | 0.692 | 16.67 | 0.879 | 25.00 | 0.871 | 6.56 | 0.888 | 10.04 | 0.658 | | | | | | |
| 14.29 | 0.606 | 18.18 | 0.879 | | | 6.61 | 0.817 | 10.12 | 0.581 | | | | | | |
| 15.38 | 0.835 | 20.00 | 0.870 | | | 6.64 | 0.572 | 10.22 | 0.731 | | | | | | |
| 16.67 | 0.844 | 22.22 | 0.922 | | | 6.74 | 0.572 | 10.32 | 0.690 | | | | | | |
| 18.18 | 0.835 | 25.00 | 0.916 | | | 6.86 | 0.446 | 10.43 | 0.792 | | | | | | |
| 20.00 | 0.799 | | | | | 6.94 | 0.520 | 10.70 | 0.843 | | | | | | |
| 22.22 | 0.858 | | | | | 6.97 | 0.747 | 10.98 | 0.805 | | | | | | |
| 25.00 | 0.848 | | | | | 7.02 | 0.793 | 11.36 | 0.923 | | | | | | |
| CURVE 2 | | | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | |
| 3.35 | 0.830 | 3.35 | 0.830 | 3.35 | 0.830 | 3.35 | 0.830 | 3.35 | 0.830 | 3.35 | 0.830 | 3.35 | 0.830 | 3.35 | 0.830 |
| 3.45 | 0.830 | 3.45 | 0.830 | 3.45 | 0.830 | 3.45 | 0.830 | 3.45 | 0.830 | 3.45 | 0.830 | 3.45 | 0.830 | 3.45 | 0.830 |
| 3.57 | 0.844 | 3.57 | 0.844 | 3.57 | 0.844 | 3.57 | 0.844 | 3.57 | 0.844 | 3.57 | 0.844 | 3.57 | 0.844 | 3.57 | 0.844 |
| 3.70 | 0.888 | 3.70 | 0.888 | 3.70 | 0.888 | 3.70 | 0.888 | 3.70 | 0.888 | 3.70 | 0.888 | 3.70 | 0.888 | 3.70 | 0.888 |
| CURVE 3 | | | | | | | | | | | | | | | |
| T = 293. | | | | | | | | | | | | | | | |
| 2.00 | 0.911 | 2.00 | 0.876 | 2.24 | 0.876 | 2.34 | 0.854 | 2.47 | 0.881 | 2.70 | 0.906 | 2.86 | 0.867 | 3.25 | 0.784 |
| 2.09 | 0.876 | 2.24 | 0.876 | 2.34 | 0.854 | 2.47 | 0.881 | 2.70 | 0.906 | 2.86 | 0.867 | 3.25 | 0.784 | 3.32 | 0.587 |
| 2.24 | 0.876 | 2.34 | 0.854 | 2.47 | 0.881 | 2.70 | 0.906 | 2.86 | 0.867 | 3.25 | 0.784 | 3.32 | 0.587 | 3.42 | 0.508 |
| 2.34 | 0.854 | 2.47 | 0.881 | 2.70 | 0.906 | 2.86 | 0.867 | 3.25 | 0.784 | 3.32 | 0.587 | 3.42 | 0.508 | 3.48 | 0.640 |
| 2.47 | 0.881 | 2.70 | 0.906 | 2.86 | 0.867 | 3.25 | 0.784 | 3.32 | 0.587 | 3.42 | 0.508 | 3.48 | 0.640 | 3.53 | 0.798 |
| 2.70 | 0.906 | 2.86 | 0.867 | 3.25 | 0.784 | 3.32 | 0.587 | 3.42 | 0.508 | 3.48 | 0.640 | 3.53 | 0.798 | 3.79 | 0.872 |
| 2.86 | 0.867 | 3.25 | 0.784 | 3.32 | 0.587 | 3.42 | 0.508 | 3.48 | 0.640 | 3.53 | 0.798 | 3.79 | 0.872 | 4.96 | 0.883 |
| 3.25 | 0.784 | 3.32 | 0.587 | 3.42 | 0.508 | 3.48 | 0.640 | 3.53 | 0.798 | 3.79 | 0.872 | 4.96 | 0.883 | 5.18 | 0.865 |
| 3.32 | 0.587 | 3.42 | 0.508 | 3.48 | 0.640 | 3.53 | 0.798 | 3.79 | 0.872 | 4.96 | 0.883 | 5.18 | 0.865 | 5.26 | 0.889 |
| 3.42 | 0.508 | 3.48 | 0.640 | 3.53 | 0.798 | 3.79 | 0.872 | 4.96 | 0.883 | 5.18 | 0.865 | 5.26 | 0.889 | 5.38 | 0.865 |
| 3.48 | 0.640 | 3.53 | 0.798 | 3.79 | 0.872 | 4.96 | 0.883 | 5.18 | 0.865 | 5.26 | 0.889 | 5.38 | 0.865 | 5.46 | 0.877 |
| 3.53 | 0.798 | 3.79 | 0.872 | 4.96 | 0.883 | 5.18 | 0.865 | 5.26 | 0.889 | 5.38 | 0.865 | 5.46 | 0.877 | 5.57 | 0.848 |
| 3.79 | 0.872 | 4.96 | 0.883 | 5.18 | 0.865 | 5.26 | 0.889 | 5.38 | 0.865 | 5.46 | 0.877 | 5.57 | 0.848 | 5.65 | 0.801 |
| 4.96 | 0.883 | 5.18 | 0.865 | 5.26 | 0.889 | 5.38 | 0.865 | 5.46 | 0.877 | 5.57 | 0.848 | 5.65 | 0.801 | 5.71 | 0.400 |
| 5.18 | 0.865 | 5.26 | 0.889 | 5.38 | 0.865 | 5.46 | 0.877 | 5.57 | 0.848 | 5.65 | 0.801 | 5.71 | 0.400 | 5.80 | 0.064 |
| 5.26 | 0.889 | 5.38 | 0.865 | 5.46 | 0.877 | 5.57 | 0.848 | 5.65 | 0.801 | 5.71 | 0.400 | 5.80 | 0.064 | 5.86 | 0.389 |
| 5.38 | 0.865 | 5.46 | 0.877 | 5.57 | 0.848 | 5.65 | 0.801 | 5.71 | 0.400 | 5.80 | 0.064 | 5.86 | 0.389 | 5.93 | 0.618 |
| 5.46 | 0.877 | 5.57 | 0.848 | 5.65 | 0.801 | 5.71 | 0.400 | 5.80 | 0.064 | 5.86 | 0.389 | 5.93 | 0.618 | | |

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ, μm; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 5 (CONT.) | | CURVE 5 (CONT.) | | CURVE 6 (CONT.) | | CURVE 6 (CONT.) | | CURVE 6 (CONT.) | | CURVE 7 | |
|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|-----------------|-------|----------|-------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 5.97 | 0.755 | 9.21 | 0.742 | 0.349 | 0.841 | 1.202 | 0.766 | 1.696 | 0.022 | 2.177 | 0.137 |
| 6.02 | 0.815 | 9.32 | 0.742 | 0.355 | 0.868 | 1.207 | 0.817 | 1.705 | 0.027 | 2.165 | 0.076 |
| 6.12 | 0.855 | 9.46 | 0.699 | 0.368 | 0.885 | 1.216 | 0.850 | 1.717 | 0.027 | 2.200 | 0.019 |
| 6.25 | 0.838 | 9.53 | 0.768 | 0.384 | 0.899 | 1.234 | 0.861 | 1.733 | 0.052 | CURVE 7 | |
| 6.47 | 0.848 | 9.56 | 0.845 | 0.415 | 0.909 | 1.251 | 0.895 | 1.749 | 0.121 | T = 296. | |
| 6.54 | 0.863 | 9.65 | 0.899 | 0.537 | 0.911 | 1.261 | 0.911 | 1.759 | 0.170 | 0.200 | 0.000 |
| 6.69 | 0.815 | 10.00 | 0.838 | 0.544 | 0.908 | 1.268 | 0.889 | 1.766 | 0.170 | 0.336 | 0.000 |
| 6.71 | 0.639 | 10.00 | 0.665 | 0.554 | 0.911 | 1.277 | 0.896 | 1.775 | 0.153 | 0.345 | 0.018 |
| 6.71 | 0.515 | 10.17 | 0.617 | 0.628 | 0.911 | 1.291 | 0.896 | 1.782 | 0.169 | 0.364 | 0.500 |
| 6.84 | 0.529 | 10.33 | 0.722 | 0.696 | 0.919 | 1.308 | 0.883 | 1.810 | 0.320 | 0.399 | 0.854 |
| 6.94 | 0.426 | 10.45 | 0.668 | 0.734 | 0.919 | 1.318 | 0.855 | 1.819 | 0.330 | 0.426 | 0.894 |
| 6.99 | 0.527 | 10.57 | 0.781 | 0.772 | 0.925 | 1.335 | 0.580 | 1.831 | 0.330 | 0.456 | 0.905 |
| 7.02 | 0.654 | 10.77 | 0.830 | 0.772 | 0.925 | 1.338 | 0.509 | 1.840 | 0.321 | 0.538 | 0.909 |
| 7.10 | 0.757 | 10.96 | 0.830 | 0.793 | 0.933 | 1.348 | 0.474 | 1.847 | 0.280 | 0.549 | 0.907 |
| 7.16 | 0.738 | 11.10 | 0.780 | 0.832 | 0.935 | 1.354 | 0.462 | 1.856 | 0.274 | 0.558 | 0.915 |
| 7.16 | 0.856 | 11.30 | 0.851 | 0.851 | 0.927 | 1.359 | 0.408 | 1.866 | 0.295 | 0.685 | 0.919 |
| 7.21 | 0.620 | 11.54 | 0.873 | 0.864 | 0.917 | 1.366 | 0.388 | 1.876 | 0.267 | 0.768 | 0.926 |
| 7.29 | 0.663 | 11.62 | 0.775 | 0.876 | 0.899 | 1.374 | 0.405 | 1.893 | 0.061 | 0.813 | 0.933 |
| 7.37 | 0.649 | 11.95 | 0.746 | 0.886 | 0.877 | 1.383 | 0.400 | 1.899 | 0.050 | 0.859 | 0.926 |
| 7.48 | 0.760 | 12.23 | 0.846 | 0.893 | 0.877 | 1.393 | 0.468 | 1.908 | 0.083 | 0.873 | 0.912 |
| 7.64 | 0.760 | 12.37 | 0.799 | 0.904 | 0.895 | 1.401 | 0.475 | 1.918 | 0.167 | 0.883 | 0.893 |
| 7.77 | 0.714 | 12.61 | 0.650 | 0.925 | 0.916 | 1.412 | 0.468 | 1.927 | 0.206 | 0.898 | 0.880 |
| 7.85 | 0.592 | 13.05 | 0.811 | 0.940 | 0.916 | 1.420 | 0.487 | 1.934 | 0.184 | 0.911 | 0.905 |
| 7.88 | 0.363 | 13.32 | 0.710 | 0.948 | 0.913 | 1.449 | 0.658 | 1.942 | 0.158 | 0.924 | 0.916 |
| 7.98 | 0.841 | 13.43 | 0.629 | 0.962 | 0.913 | 1.462 | 0.705 | 1.950 | 0.174 | 0.964 | 0.916 |
| 8.01 | 0.338 | 13.50 | 0.696 | 0.970 | 0.899 | 1.481 | 0.760 | 1.957 | 0.251 | 0.974 | 0.901 |
| 8.03 | 0.293 | 13.55 | 0.778 | 0.986 | 0.895 | 1.496 | 0.790 | 1.968 | 0.317 | 0.984 | 0.880 |
| 8.23 | 0.557 | 13.69 | 0.810 | 0.999 | 0.882 | 1.514 | 0.816 | 1.982 | 0.330 | 0.993 | 0.888 |
| 8.30 | 0.381 | 14.00 | 0.823 | 1.012 | 0.895 | 1.533 | 0.816 | 1.992 | 0.330 | 1.004 | 0.880 |
| 8.35 | 0.327 | 14.47 | 0.603 | 1.026 | 0.895 | 1.562 | 0.781 | 1.992 | 0.318 | 1.015 | 0.895 |
| 8.35 | 0.226 | 15.00 | 0.766 | 1.050 | 0.911 | 1.587 | 0.726 | 2.004 | 0.314 | 1.029 | 0.895 |
| 8.45 | 0.188 | | | 1.063 | 0.916 | 1.601 | 0.658 | 2.020 | 0.314 | 1.053 | 0.915 |
| 8.51 | 0.271 | | | 1.094 | 0.916 | 1.614 | 0.577 | 2.051 | 0.244 | 1.074 | 0.901 |
| 8.57 | 0.271 | | | 1.094 | 0.909 | 1.625 | 0.524 | 2.065 | 0.228 | 1.093 | 0.901 |
| 8.65 | 0.173 | | | 1.104 | 0.889 | 1.635 | 0.479 | 2.077 | 0.179 | 1.093 | 0.888 |
| 8.77 | 0.109 | | | 1.130 | 0.706 | 1.645 | 0.306 | 2.110 | 0.024 | 1.084 | 0.888 |
| 8.84 | 0.267 | | | 1.151 | 0.575 | 1.653 | 0.070 | 2.132 | 0.000 | 1.015 | 0.895 |
| 8.84 | 0.431 | | | 1.160 | 0.490 | 1.660 | 0.031 | 2.152 | 0.000 | 1.029 | 0.895 |
| 8.89 | 0.546 | | | 1.165 | 0.475 | 1.673 | 0.030 | 2.152 | 0.024 | 1.053 | 0.915 |
| 9.01 | 0.659 | | | 1.173 | 0.486 | 1.685 | 0.026 | 2.171 | 0.023 | 1.074 | 0.915 |
| | | | | | | | | 2.171 | 0.237 | 1.090 | 0.905 |

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T , $^{\circ}\text{K}$; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | | |
|-----------------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-------|-------|
| CURVE 7 (CONT.) | | | | | | | | | | | | | |
| 1.102 | 0.884 | 1.559 | 0.781 | 1.978 | 0.349 | 0.942 | 0.861 | 0.409 | 9.681 | 1.605 | 0.503 | | |
| 1.114 | 0.833 | 1.582 | 0.729 | 2.006 | 0.332 | 0.999 | 0.853 | 0.428 | 0.688 | 1.623 | 0.500 | | |
| 1.160 | 0.500 | 1.600 | 0.663 | 2.026 | 0.305 | 1.019 | 0.846 | 0.451 | 0.691 | 1.641 | 0.489 | | |
| 1.166 | 0.485 | 1.614 | 0.571 | 2.046 | 0.263 | 1.046 | 0.840 | 0.517 | 0.691 | 1.691 | 0.443 | | |
| 1.173 | 0.492 | 1.627 | 0.503 | 2.064 | 0.240 | 1.082 | 0.835 | 0.536 | 0.700 | 1.758 | 0.382 | | |
| 1.181 | 0.603 | 1.636 | 0.432 | 2.096 | 0.048 | 1.125 | 0.832 | 0.568 | 0.713 | 1.782 | 0.356 | | |
| 1.186 | 0.655 | 1.651 | 0.117 | 2.102 | 0.032 | 1.213 | 0.830 | 0.587 | 0.717 | 1.827 | 0.302 | | |
| 1.205 | 0.816 | 1.657 | 0.049 | 2.116 | 0.032 | 1.239 | 0.824 | 0.587 | 0.721 | 1.858 | 0.261 | | |
| 1.215 | 0.856 | 1.671 | 0.016 | 2.129 | 0.000 | 1.260 | 0.816 | 0.615 | 0.721 | 1.883 | 0.218 | | |
| 1.238 | 0.889 | 1.685 | 0.037 | 2.141 | 0.028 | 1.279 | 0.808 | 0.633 | 0.726 | 1.905 | 0.176 | | |
| 1.259 | 0.911 | 1.693 | 0.027 | 2.148 | 0.034 | 1.295 | 0.799 | 0.648 | 0.734 | 1.936 | 0.116 | | |
| 1.265 | 0.890 | 1.701 | 0.036 | 2.164 | 0.034 | 1.313 | 0.786 | 0.666 | 0.745 | 1.949 | 0.085 | | |
| 1.274 | 0.896 | 1.713 | 0.036 | 2.179 | 0.020 | 1.326 | 0.771 | 0.707 | 0.769 | 1.963 | 0.064 | | |
| 1.236 | 0.895 | 1.727 | 0.058 | 2.181 | 0.105 | 1.341 | 0.746 | 0.719 | 0.769 | 1.994 | 0.045 | | |
| 1.305 | 0.823 | 1.741 | 0.110 | 2.190 | 0.047 | 1.355 | 0.712 | 0.730 | 0.765 | 2.038 | 0.035 | | |
| 1.313 | 0.861 | 1.756 | 0.177 | 2.200 | 0.027 | 1.362 | 0.665 | 0.750 | 0.751 | 2.104 | 0.029 | | |
| 1.333 | 0.643 | 1.762 | 0.186 | | | 1.369 | 0.547 | 0.789 | 0.730 | 2.188 | 0.023 | | |
| 1.338 | 0.523 | 1.772 | 0.164 | CURVE 8 | | | | | | | | 2.348 | 0.019 |
| 1.343 | 0.498 | 1.779 | 0.181 | T = 296. | | | | | | | | 2.506 | 0.018 |
| 1.355 | 0.481 | 1.804 | 0.326 | 0.405 | 0.839 | 1.406 | 0.511 | 0.851 | 0.727 | CURVE 10 | | | |
| 1.357 | 0.416 | 1.811 | 0.342 | 0.413 | 0.846 | 1.469 | 0.516 | 0.869 | 0.733 | T = 293. | | | |
| 1.364 | 0.405 | 1.821 | 0.347 | 0.434 | 0.858 | 1.539 | 0.523 | 0.887 | 0.745 | 2.50 | 0.961 | | |
| 1.373 | 0.414 | 1.832 | 0.340 | 0.452 | 0.868 | 1.592 | 0.523 | 0.901 | 0.755 | 2.61 | 0.964 | | |
| 1.383 | 0.414 | 1.837 | 0.323 | 0.474 | 0.875 | 1.620 | 0.520 | 0.923 | 0.760 | 2.62 | 0.957 | | |
| 1.388 | 0.444 | 1.843 | 0.301 | 0.474 | 0.875 | 1.644 | 0.514 | 1.103 | 0.760 | 2.65 | 0.964 | | |
| 1.394 | 0.490 | 1.849 | 0.293 | 0.493 | 0.876 | 1.679 | 0.502 | 1.142 | 0.758 | 2.66 | 0.952 | | |
| 1.402 | 0.499 | 1.862 | 0.320 | 0.551 | 0.889 | 1.706 | 0.488 | 1.182 | 0.754 | 2.68 | 0.963 | | |
| 1.413 | 0.490 | 1.871 | 0.287 | 0.587 | 0.878 | 1.730 | 0.471 | 1.211 | 0.751 | 2.70 | 0.963 | | |
| 1.419 | 0.499 | 1.890 | 0.083 | 0.605 | 0.869 | 1.750 | 0.456 | 1.223 | 0.745 | 2.74 | 0.929 | | |
| 1.424 | 0.527 | 1.898 | 0.075 | 0.639 | 0.862 | 1.765 | 0.439 | 1.233 | 0.733 | 2.76 | 0.934 | | |
| 1.434 | 0.539 | 1.906 | 0.090 | 0.670 | 0.862 | 1.791 | 0.400 | 1.259 | 0.676 | 2.78 | 0.949 | | |
| 1.441 | 0.625 | 1.911 | 0.172 | 0.714 | 0.871 | 1.932 | 0.141 | 1.293 | 0.618 | 2.80 | 0.938 | | |
| 1.447 | 0.670 | 1.917 | 0.223 | 0.747 | 0.878 | 1.959 | 0.107 | 1.320 | 0.578 | 2.83 | 0.955 | | |
| 1.457 | 0.708 | 1.921 | 0.236 | 0.783 | 0.886 | 2.004 | 0.061 | 1.361 | 0.528 | 2.87 | 0.955 | | |
| 1.457 | 0.750 | 1.927 | 0.224 | 0.831 | 0.892 | 2.028 | 0.049 | 1.375 | 0.513 | 2.90 | 0.924 | | |
| 1.478 | 0.775 | 1.935 | 0.186 | 0.876 | 0.897 | 2.061 | 0.041 | 1.390 | 0.504 | 2.92 | 0.951 | | |
| 1.493 | 0.799 | 1.940 | 0.174 | 0.918 | 0.897 | 2.111 | 0.035 | 1.414 | 0.491 | 2.95 | 0.963 | | |
| 1.509 | 0.821 | 1.947 | 0.198 | 0.940 | 0.892 | 2.247 | 0.035 | 1.456 | 0.491 | | | | |
| 1.529 | 0.821 | 1.958 | 0.324 | 0.953 | 0.885 | 2.383 | 0.041 | 1.489 | 0.495 | | | | |
| 1.544 | 0.813 | 1.969 | 0.347 | 0.966 | 0.873 | 2.494 | 0.049 | 1.567 | 0.503 | | | | |

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|---|
| 3.11 | 0.963 | 6.14 | 0.928 | 9.15 | 0.768 | 17.79 | 0.951 | 5.74 | 0.197 | 8.42 | 0.210 | | |
| 3.16 | 0.955 | 6.27 | 0.934 | 9.26 | 0.750 | 18.59 | 0.951 | 5.70 | 0.072 | 8.45 | 0.267 | | |
| 3.25 | 0.939 | 6.45 | 0.934 | 9.35 | 0.718 | 19.06 | 0.915 | 5.83 | 0.174 | 8.51 | 0.296 | | |
| 3.28 | 0.895 | 6.55 | 0.918 | 9.40 | 0.754 | 19.84 | 0.908 | 5.85 | 0.429 | 8.60 | 0.211 | | |
| 3.33 | 0.528 | 6.61 | 0.886 | 9.47 | 0.897 | 20.45 | 0.857 | 5.89 | 0.563 | 8.72 | 0.119 | | |
| 3.35 | 0.667 | 6.64 | 0.854 | 9.57 | 0.936 | 20.83 | 0.893 | 5.94 | 0.703 | 8.81 | 0.315 | | |
| 3.38 | 0.424 | 6.69 | 0.527 | 9.69 | 0.947 | 21.74 | 0.906 | 5.98 | 0.800 | 8.84 | 0.498 | | |
| 3.40 | 0.608 | 6.72 | 0.516 | 9.79 | 0.938 | 22.78 | 0.893 | 6.02 | 0.846 | 8.90 | 0.611 | | |
| 3.43 | 0.659 | 6.78 | 0.559 | 9.87 | 0.892 | 23.81 | 0.836 | 6.12 | 0.574 | 8.97 | 0.696 | | |
| 3.46 | 0.813 | 6.80 | 0.523 | 9.98 | 0.636 | 25.00 | 0.776 | 6.25 | 0.850 | 9.09 | 0.737 | | |
| 3.48 | 0.876 | 6.81 | 0.440 | 10.06 | 0.827 | | | 6.50 | 0.877 | 9.18 | 0.761 | | |
| 3.52 | 0.833 | 6.87 | 0.416 | 10.15 | 0.703 | | | 6.62 | 0.857 | 9.28 | 0.761 | | |
| 3.53 | 0.923 | 6.90 | 0.442 | 10.28 | 0.671 | | | 6.66 | 0.818 | 9.43 | 0.723 | | |
| 3.57 | 0.957 | 6.95 | 0.433 | 10.44 | 0.793 | | | 6.70 | 0.658 | 9.52 | 0.877 | | |
| 3.68 | 0.971 | 7.02 | 0.796 | 10.56 | 0.843 | | | 6.70 | 0.567 | 9.80 | 0.922 | | |
| 3.78 | 0.971 | 7.06 | 0.827 | 10.67 | 0.856 | | | 6.73 | 0.539 | 9.92 | 0.889 | | |
| 3.86 | 0.964 | 7.11 | 0.778 | 10.86 | 0.832 | | | 6.82 | 0.552 | 10.00 | 0.717 | | |
| 3.92 | 0.973 | 7.13 | 0.714 | 11.05 | 0.903 | | | 6.93 | 0.439 | 10.11 | 0.645 | | |
| 4.09 | 0.976 | 7.18 | 0.641 | 11.20 | 0.921 | | | 7.00 | 0.606 | 10.23 | 0.706 | | |
| 4.15 | 0.965 | 7.23 | 0.749 | 11.36 | 0.917 | | | 7.00 | 0.562 | 10.31 | 0.734 | | |
| 4.27 | 0.976 | 7.26 | 0.764 | 11.63 | 0.848 | | | 7.08 | 0.779 | 10.39 | 0.691 | | |
| 4.57 | 0.976 | 7.30 | 0.764 | 11.79 | 0.765 | | | 7.14 | 0.755 | 10.51 | 0.804 | | |
| 4.87 | 0.957 | 7.35 | 0.804 | 11.89 | 0.862 | | | 7.18 | 0.648 | 10.71 | 0.844 | | |
| 5.00 | 0.972 | 7.44 | 0.825 | 12.02 | 0.851 | | | 7.26 | 0.685 | 10.84 | 0.856 | | |
| 5.10 | 0.967 | 7.58 | 0.806 | 12.09 | 0.895 | | | 7.33 | 0.674 | 11.05 | 0.804 | | |
| 5.28 | 0.992 | 7.66 | 0.770 | 12.24 | 0.864 | | | 7.39 | 0.721 | 11.27 | 0.895 | | |
| 5.40 | 0.976 | 7.72 | 0.694 | 12.44 | 0.922 | | | 7.44 | 0.760 | 11.47 | 0.896 | | |
| 5.50 | 0.958 | 7.82 | 0.396 | 12.56 | 0.931 | | | 7.50 | 0.777 | 11.64 | 0.857 | | |
| 5.58 | 0.934 | 7.93 | 0.425 | 12.77 | 0.911 | | | 7.61 | 0.777 | 11.85 | 0.779 | | |
| 5.62 | 0.699 | 8.03 | 0.322 | 13.05 | 0.811 | | | 7.74 | 0.736 | 11.98 | 0.791 | | |
| 5.67 | 0.844 | 8.14 | 0.543 | 13.25 | 0.691 | | | 7.84 | 0.638 | 12.10 | 0.648 | | |
| 5.70 | 0.499 | 8.19 | 0.574 | 13.37 | 0.895 | | | 7.84 | 0.469 | 12.19 | 0.871 | | |
| 5.72 | 0.102 | 8.29 | 0.399 | 13.64 | 0.938 | | | 7.88 | 0.393 | 12.33 | 0.840 | | |
| 5.75 | 0.046 | 8.35 | 0.230 | 13.87 | 0.954 | | | 7.96 | 0.456 | 12.60 | 0.670 | | |
| 5.80 | 0.079 | 8.45 | 0.290 | 14.12 | 0.941 | | | 8.04 | 0.323 | 12.80 | 0.869 | | |
| 5.84 | 0.591 | 8.55 | 0.263 | 14.43 | 0.965 | | | 8.09 | 0.372 | 12.98 | 0.640 | | |
| 5.88 | 0.771 | 8.65 | 0.143 | 15.08 | 0.974 | | | 8.15 | 0.527 | 13.15 | 0.789 | | |
| 5.93 | 0.805 | 8.91 | 0.593 | 15.43 | 0.966 | | | 8.21 | 0.575 | 13.29 | 0.735 | | |
| 5.97 | 0.901 | 9.01 | 0.695 | 16.18 | 0.973 | | | 8.31 | 0.366 | 13.38 | 0.671 | | |
| 6.03 | 0.914 | 9.08 | 0.745 | 17.18 | 0.965 | | | 8.35 | 0.264 | 13.45 | 0.704 | | |

CURVE 11
T = 296.CURVE 10 (CONT.)
CURVE 11 (CONT.)

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| CURVE 11 (CONT.) | | CURVE 12 (CONT.) | | CURVE 13 (CONT.) | | CURVE 13 (CONT.) | | CURVE 13 (CONT.) | | CURVE 13 (CONT.) | |
|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 13.43 | 0.783 | 1.558 | 0.801 | 2.67 | 0.819 | 4.32 | 0.875 | 6.20 | 0.872 | 8.09 | 0.773 |
| 13.59 | 0.840 | 1.591 | 0.767 | 2.71 | 0.862 | 4.41 | 0.900 | 6.36 | 0.886 | 8.18 | 0.550 |
| 13.75 | 0.855 | 1.617 | 0.645 | 2.74 | 0.868 | 4.46 | 0.900 | 6.40 | 0.862 | 8.24 | 0.306 |
| 14.08 | 0.855 | 1.670 | 0.259 | 2.74 | 0.833 | 4.49 | 0.912 | 6.40 | 0.795 | 8.30 | 0.216 |
| 14.99 | 0.816 | 1.685 | 0.240 | 2.78 | 0.860 | 4.60 | 0.877 | 6.43 | 0.868 | 8.37 | 0.255 |
| | | 1.700 | 0.254 | 2.82 | 0.860 | 4.65 | 0.895 | 6.48 | 0.800 | 8.43 | 0.349 |
| | | 1.714 | 0.342 | 2.83 | 0.880 | 4.73 | 0.883 | 6.51 | 0.852 | 8.50 | 0.092 |
| | | 1.747 | 0.456 | 2.87 | 0.880 | 4.84 | 0.906 | 6.57 | 0.798 | 8.55 | 0.072 |
| | | 1.793 | 0.490 | 2.89 | 0.867 | 4.93 | 0.890 | 6.61 | 0.842 | 8.61 | 0.106 |
| | | 1.834 | 0.501 | 2.92 | 0.880 | 5.00 | 0.901 | 6.63 | 0.793 | 8.68 | 0.604 |
| | | 1.912 | 0.526 | 3.02 | 0.880 | 5.04 | 0.908 | 6.68 | 0.869 | 8.75 | 0.888 |
| | | 1.968 | 0.554 | 3.06 | 0.880 | 5.11 | 0.920 | 6.72 | 0.828 | 8.82 | 0.857 |
| | | 1.989 | 0.562 | 3.08 | 0.888 | 5.14 | 0.909 | 6.74 | 0.791 | 9.00 | 0.884 |
| | | 2.021 | 0.544 | 3.13 | 0.865 | 5.17 | 0.929 | 6.80 | 0.642 | 9.15 | 0.897 |
| 0.275 | 0.000 | 2.038 | 0.484 | 3.16 | 0.883 | 5.20 | 0.897 | 6.80 | 0.569 | 9.42 | 0.897 |
| 0.303 | 0.547 | 2.050 | 0.310 | 3.18 | 0.874 | 5.24 | 0.912 | 6.84 | 0.589 | 9.51 | 0.910 |
| 0.313 | 0.747 | 2.066 | 0.198 | 3.21 | 0.835 | 5.29 | 0.888 | 6.88 | 0.500 | 9.66 | 0.762 |
| 0.327 | 0.812 | 2.122 | 0.114 | 3.25 | 0.868 | 5.32 | 0.897 | 6.93 | 0.564 | 9.76 | 0.721 |
| 0.336 | 0.845 | 2.156 | 0.060 | 3.28 | 0.813 | 5.35 | 0.879 | 6.98 | 0.741 | 9.84 | 0.779 |
| 0.351 | 0.878 | 2.195 | 0.023 | 3.29 | 0.750 | 5.36 | 0.911 | 7.01 | 0.792 | 9.91 | 0.836 |
| 0.369 | 0.904 | 2.259 | 0.012 | 3.31 | 0.704 | 5.40 | 0.920 | 7.03 | 0.770 | 10.12 | 0.888 |
| 0.419 | 0.926 | 2.350 | 0.012 | 3.34 | 0.641 | 5.42 | 0.906 | 7.07 | 0.770 | 10.24 | 0.919 |
| 0.567 | 0.926 | 2.418 | 0.028 | 3.35 | 0.652 | 5.49 | 0.860 | 7.11 | 0.758 | 10.48 | 0.700 |
| 0.609 | 0.933 | 2.476 | 0.055 | 3.36 | 0.536 | 5.56 | 0.860 | 7.17 | 0.782 | 10.58 | 0.537 |
| 0.838 | 0.933 | 2.516 | 0.066 | 3.40 | 0.718 | 5.59 | 0.882 | 7.20 | 0.803 | 10.81 | 0.801 |
| 0.900 | 0.914 | 2.572 | 0.067 | 3.43 | 0.784 | 5.61 | 0.862 | 7.26 | 0.818 | 10.88 | 0.916 |
| 0.943 | 0.914 | 2.635 | 0.048 | 3.47 | 0.835 | 5.67 | 0.403 | 7.26 | 0.842 | 11.07 | 0.938 |
| 1.002 | 0.925 | 2.688 | 0.019 | 3.51 | 0.806 | 5.69 | 0.130 | 7.34 | 0.864 | 11.51 | 0.918 |
| 1.068 | 0.904 | | | 3.54 | 0.865 | 5.71 | 0.094 | 7.37 | 0.800 | 11.74 | 0.918 |
| 1.119 | 0.853 | | | 3.60 | 0.879 | 5.75 | 0.145 | 7.42 | 0.555 | 11.95 | 0.812 |
| 1.155 | 0.795 | | | 3.67 | 0.888 | 5.79 | 0.605 | 7.45 | 0.381 | 12.03 | 0.753 |
| 1.197 | 0.765 | | | 3.81 | 0.888 | 5.84 | 0.808 | 7.50 | 0.361 | 12.22 | 0.729 |
| 1.226 | 0.792 | | | 3.83 | 0.898 | 5.88 | 0.790 | 7.56 | 0.412 | 12.30 | 0.868 |
| 1.271 | 0.859 | | | 3.93 | 0.898 | 5.93 | 0.814 | 7.61 | 0.389 | 12.39 | 0.886 |
| 1.289 | 0.867 | | | 3.96 | 0.885 | 5.97 | 0.852 | 7.68 | 0.461 | 12.47 | 0.936 |
| 1.312 | 0.857 | | | 4.01 | 0.902 | 6.02 | 0.827 | 7.73 | 0.699 | 12.76 | 0.959 |
| 1.344 | 0.766 | | | 4.06 | 0.902 | 6.04 | 0.657 | 7.79 | 0.837 | 13.04 | 0.944 |
| 1.364 | 0.701 | | | 4.16 | 0.902 | 6.06 | 8.718 | 7.86 | 0.845 | 13.66 | 0.966 |
| 1.391 | 0.633 | | | 4.19 | 0.870 | 6.11 | 0.691 | 7.91 | 0.869 | 14.39 | 0.942 |
| 1.422 | 0.718 | | | 4.23 | 0.815 | 6.14 | 0.808 | 8.03 | 0.822 | 15.08 | 0.874 |
| 1.437 | 0.778 | | | | | | | | | | |
| 1.457 | 0.820 | | | | | | | | | | |
| 1.488 | 0.836 | | | | | | | | | | |
| 1.526 | 0.823 | | | | | | | | | | |

CURVE 13
T = 293.

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μ m; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 16 (CONT.) | | CURVE 16 (CONT.) | | CURVE 16 (CONT.) | | CURVE 16 (CONT.) | | CURVE 16 (CONT.) | | CURVE 16 (CONT.) | | CURVE 17 (CONT.) | | CURVE 17 (CONT.) | | |
|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | |
| 3.28 | 0.842 | 6.77 | 0.559 | 8.46 | 0.256 | 11.27 | 0.892 | 3.04 | 0.408 | 5.91 | 0.349 | 5.91 | 0.408 | 5.91 | 0.349 | |
| 3.32 | 0.795 | 6.79 | 0.581 | 8.53 | 0.229 | 11.49 | 0.892 | 3.13 | 0.418 | 5.93 | 0.423 | 5.93 | 0.418 | 5.93 | 0.423 | |
| 3.34 | 0.671 | 6.82 | 0.559 | 8.59 | 0.206 | 11.64 | 0.863 | 3.16 | 0.441 | 5.96 | 0.446 | 5.96 | 0.441 | 5.96 | 0.446 | |
| 3.34 | 0.601 | 6.87 | 0.420 | 8.65 | 0.115 | 11.82 | 0.796 | 3.24 | 0.469 | 5.96 | 0.470 | 5.96 | 0.469 | 5.96 | 0.470 | |
| 3.38 | 0.591 | 6.90 | 0.397 | 8.69 | 0.077 | 11.90 | 0.772 | 3.31 | 0.484 | 6.00 | 0.403 | 6.00 | 0.484 | 6.00 | 0.403 | |
| 3.38 | 0.543 | 6.95 | 0.420 | 8.72 | 0.109 | 11.95 | 0.792 | 3.35 | 0.478 | 6.00 | 0.499 | 6.00 | 0.478 | 6.00 | 0.499 | |
| 3.41 | 0.518 | 6.98 | 0.487 | 8.78 | 0.282 | 12.01 | 0.838 | 3.37 | 0.449 | 6.08 | 0.518 | 6.08 | 0.449 | 6.08 | 0.518 | |
| 3.43 | 0.564 | 7.01 | 0.699 | 8.82 | 0.371 | 12.05 | 0.859 | 3.38 | 0.416 | 6.21 | 0.518 | 6.21 | 0.416 | 6.21 | 0.518 | |
| 3.45 | 0.700 | 7.04 | 0.749 | 8.85 | 0.453 | 12.13 | 0.834 | 3.40 | 0.388 | 6.29 | 0.531 | 6.29 | 0.388 | 6.29 | 0.531 | |
| 3.48 | 0.782 | 7.10 | 0.769 | 8.90 | 0.557 | 12.26 | 0.876 | 3.43 | 0.368 | 6.32 | 0.542 | 6.32 | 0.368 | 6.32 | 0.542 | |
| 3.55 | 0.852 | 7.14 | 0.731 | 9.00 | 0.643 | 12.38 | 0.830 | 3.47 | 0.399 | 6.38 | 0.549 | 6.38 | 0.399 | 6.38 | 0.549 | |
| 3.59 | 0.879 | 7.21 | 0.629 | 9.04 | 0.690 | 12.51 | 0.866 | 3.49 | 0.434 | 6.40 | 0.559 | 6.40 | 0.434 | 6.40 | 0.559 | |
| 3.67 | 0.898 | 7.24 | 0.680 | 9.08 | 0.727 | 12.67 | 0.883 | 3.53 | 0.446 | 6.43 | 0.559 | 6.43 | 0.446 | 6.43 | 0.559 | |
| 4.01 | 0.902 | 7.27 | 0.706 | 9.18 | 0.765 | 12.83 | 0.883 | 3.53 | 0.477 | 6.43 | 0.559 | 6.43 | 0.477 | 6.43 | 0.559 | |
| 4.78 | 0.925 | 7.31 | 0.677 | 9.29 | 0.765 | 12.98 | 0.866 | 3.57 | 0.521 | 6.51 | 0.559 | 6.51 | 0.521 | 6.51 | 0.559 | |
| 4.83 | 0.895 | 7.34 | 0.699 | 9.37 | 0.740 | 13.08 | 0.828 | 3.59 | 0.547 | 6.53 | 0.569 | 6.53 | 0.547 | 6.53 | 0.569 | |
| 5.00 | 0.904 | 7.39 | 0.744 | 9.44 | 0.714 | 13.21 | 0.766 | 3.65 | 0.564 | 6.56 | 0.559 | 6.56 | 0.564 | 6.56 | 0.559 | |
| 5.13 | 0.890 | 7.43 | 0.770 | 9.50 | 0.812 | 13.31 | 0.689 | 3.77 | 0.561 | 6.61 | 0.552 | 6.61 | 0.561 | 6.61 | 0.552 | |
| 5.22 | 0.901 | 7.49 | 0.788 | 9.54 | 0.871 | 13.36 | 0.659 | 3.91 | 0.544 | 6.64 | 0.557 | 6.64 | 0.544 | 6.64 | 0.557 | |
| 5.34 | 0.901 | 7.60 | 0.788 | 9.62 | 0.888 | 13.46 | 0.699 | 4.06 | 0.519 | 6.65 | 0.544 | 6.65 | 0.519 | 6.65 | 0.544 | |
| 5.50 | 0.880 | 7.67 | 0.757 | 9.74 | 0.889 | 13.46 | 0.790 | 4.16 | 0.501 | 6.67 | 0.560 | 6.67 | 0.501 | 6.67 | 0.560 | |
| 5.59 | 0.867 | 7.72 | 0.707 | 9.85 | 0.899 | 13.51 | 0.831 | 4.24 | 0.491 | 6.73 | 0.528 | 6.73 | 0.491 | 6.73 | 0.528 | |
| 5.65 | 0.841 | 7.77 | 0.639 | 9.91 | 0.892 | 13.64 | 0.856 | 4.35 | 0.491 | 6.75 | 0.495 | 6.75 | 0.491 | 6.75 | 0.495 | |
| 5.67 | 0.791 | 7.81 | 0.480 | 9.97 | 0.844 | 14.01 | 0.854 | 4.45 | 0.467 | 6.78 | 0.488 | 6.78 | 0.467 | 6.78 | 0.488 | |
| 5.70 | 0.397 | 7.83 | 0.414 | 10.05 | 0.687 | 14.19 | 0.854 | 4.61 | 0.487 | 6.82 | 0.447 | 6.82 | 0.487 | 6.82 | 0.447 | |
| 5.74 | 0.052 | 7.85 | 0.377 | 10.08 | 0.638 | 14.34 | 0.835 | 4.71 | 0.500 | 6.87 | 0.395 | 6.87 | 0.500 | 6.87 | 0.395 | |
| 5.77 | 0.031 | 7.88 | 0.397 | 10.15 | 0.624 | 14.60 | 0.830 | 4.89 | 0.525 | 6.88 | 0.411 | 6.88 | 0.525 | 6.88 | 0.411 | |
| 5.78 | 0.060 | 7.90 | 0.432 | 10.21 | 0.675 | 15.00 | 0.830 | 5.17 | 0.568 | 6.91 | 0.415 | 6.91 | 0.568 | 6.91 | 0.415 | |
| 5.85 | 0.586 | 7.93 | 0.453 | 10.24 | 0.693 | | 0.807 | 5.37 | 0.595 | 6.94 | 0.423 | 6.94 | 0.595 | 6.94 | 0.423 | |
| 5.89 | 0.724 | 7.97 | 0.410 | 10.27 | 0.710 | CURVE 17 | | | | | 6.97 | 0.412 | 6.97 | 0.412 | 6.97 | 0.412 |
| 5.96 | 0.771 | 8.02 | 0.301 | 10.32 | 0.691 | T = 293. | | | | | 7.01 | 0.437 | 7.01 | 0.437 | 7.01 | 0.437 |
| 5.99 | 0.840 | 8.05 | 0.281 | 10.38 | 0.663 | | | 5.65 | 0.523 | 7.06 | 0.483 | 7.06 | 0.523 | 7.06 | 0.483 | |
| 6.04 | 0.864 | 8.08 | 0.303 | 10.44 | 0.721 | 2.53 | 0.566 | 5.71 | 0.478 | 7.11 | 0.483 | 7.11 | 0.478 | 7.11 | 0.483 | |
| 6.10 | 0.875 | 8.13 | 0.462 | 10.51 | 0.773 | 2.64 | 0.566 | 5.72 | 0.438 | 7.17 | 0.473 | 7.17 | 0.438 | 7.17 | 0.473 | |
| 6.30 | 0.870 | 8.16 | 0.551 | 10.59 | 0.802 | 2.69 | 0.546 | 5.74 | 0.419 | 7.20 | 0.448 | 7.20 | 0.419 | 7.20 | 0.448 | |
| 6.57 | 0.876 | 8.21 | 0.594 | 10.73 | 0.836 | 2.74 | 0.529 | 5.75 | 0.339 | 7.23 | 0.438 | 7.23 | 0.339 | 7.23 | 0.438 | |
| 6.60 | 0.859 | 8.25 | 0.560 | 10.87 | 0.844 | 2.78 | 0.499 | 5.79 | 0.248 | 7.25 | 0.420 | 7.25 | 0.248 | 7.25 | 0.420 | |
| 5.64 | 0.831 | 8.29 | 0.386 | 11.01 | 0.797 | 2.82 | 0.459 | 5.81 | 0.234 | 7.28 | 0.431 | 7.28 | 0.234 | 7.28 | 0.431 | |
| 6.71 | 0.533 | 8.33 | 0.258 | 11.06 | 0.831 | 2.87 | 0.432 | 5.85 | 0.258 | 7.31 | 0.431 | 7.31 | 0.258 | 7.31 | 0.431 | |
| 6.73 | 0.512 | 8.37 | 0.189 | 11.13 | 0.862 | 2.95 | 0.408 | 5.87 | 0.321 | 7.37 | 0.442 | 7.37 | 0.321 | 7.37 | 0.442 | |

TABLE 16-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF LUCITE (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

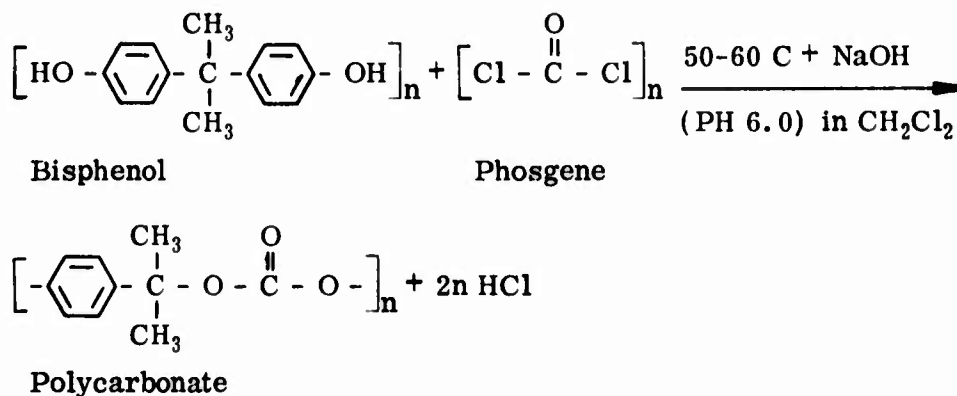
| λ | T | λ | T | λ | T | λ | T |
|------------------|-------|-----------|-------|-----------|-------|-----------|-------|
| CURVE 19 (CONT.) | | | | | | | |
| 1.191 | 0.730 | 1.877 | 0.585 | 0.250 | 0.000 | 0.552 | 0.926 |
| 1.214 | 0.825 | 1.879 | 0.554 | 0.254 | 0.009 | 0.600 | 0.931 |
| 1.236 | 0.367 | 1.886 | 0.415 | 0.257 | 0.020 | 0.647 | 0.933 |
| 1.259 | 0.892 | 1.886 | 0.333 | 0.259 | 0.044 | 0.668 | 0.933 |
| 1.273 | 0.873 | 1.891 | 0.268 | 0.279 | 0.415 | 0.700 | 0.935 |
| 1.288 | 0.283 | 1.899 | 0.253 | 0.284 | 0.531 | | |
| 1.318 | 0.866 | 1.909 | 0.271 | 0.290 | 0.602 | | |
| 1.347 | 0.692 | 1.909 | 0.319 | 0.297 | 0.684 | | |
| 1.367 | 0.629 | 1.914 | 0.339 | 0.302 | 0.714 | | |
| 1.377 | 0.657 | 1.914 | 0.382 | 0.308 | 0.753 | | |
| 1.388 | 0.646 | 1.916 | 0.417 | 0.316 | 0.789 | | |
| 1.388 | 0.566 | 1.916 | 0.456 | 0.323 | 0.813 | | |
| 1.401 | 0.679 | 1.924 | 0.470 | 0.333 | 0.840 | | |
| 1.401 | 0.695 | 1.928 | 0.502 | 0.344 | 0.860 | | |
| 1.421 | 0.695 | 1.946 | 0.444 | 0.353 | 0.873 | | |
| 1.470 | 0.807 | 1.953 | 0.467 | 0.361 | 0.881 | | |
| 1.500 | 0.849 | 1.963 | 0.483 | 0.369 | 0.889 | | |
| 1.550 | 0.449 | 1.976 | 0.559 | 0.375 | 0.893 | | |
| 1.584 | 0.818 | 1.991 | 0.591 | 0.389 | 0.900 | | |
| 1.607 | 0.783 | 2.028 | 0.578 | 0.700 | 0.900 | | |
| 1.608 | 0.763 | 2.051 | 0.504 | | | | |
| 1.618 | 0.737 | 2.064 | 0.473 | CURVE 21 | | | |
| 1.643 | 0.645 | 2.079 | 0.363 | T = 293. | | | |
| 1.654 | 0.508 | 2.093 | 0.253 | 0.250 | 0.000 | | |
| 1.662 | 0.355 | 2.108 | 0.262 | 0.265 | 0.199 | | |
| 1.670 | 0.134 | 2.116 | 0.211 | 0.277 | 0.400 | | |
| 1.677 | 0.104 | 2.120 | 0.147 | 0.289 | 0.598 | | |
| 1.688 | 0.123 | 2.127 | 0.133 | 0.294 | 0.655 | | |
| 1.688 | 0.151 | 2.139 | 0.153 | 0.303 | 0.713 | | |
| 1.696 | 0.163 | 2.148 | 0.173 | 0.310 | 0.757 | | |
| 1.709 | 0.170 | 2.148 | 0.203 | 0.320 | 0.800 | | |
| 1.727 | 0.209 | 2.165 | 0.215 | 0.327 | 0.830 | | |
| 1.741 | 0.390 | 2.181 | 0.031 | 0.339 | 0.857 | | |
| 1.769 | 0.420 | 2.198 | 0.000 | 0.351 | 0.883 | | |
| 1.769 | 0.447 | 2.226 | 0.000 | 0.366 | 0.900 | | |
| 1.784 | 0.429 | | | 0.378 | 0.909 | | |
| 1.809 | 0.558 | CURVE 20 | | | | | |
| 1.815 | 0.584 | T = 293. | | | | | |
| 1.828 | 0.600 | 0.200 | 0.000 | 0.400 | 0.913 | | |
| 1.850 | 0.550 | | | 0.450 | 0.913 | | |
| | | | | 0.500 | 0.920 | | |

4.17. Polycarbonate Plastics

Polycarbonates are transparent, faintly amber-colored, thermoplastic materials showing good dimensional stability, thermal resistance, and electrical properties, as well as good tensile and impact strength. Their unique hardness properties allow polycarbonates to substitute for metals in some applications, as in plastic rivets and bolts.

Trade names of polycarbonates are "Lexan" for General Electric, "Merlon" for Mobay, "Lexel" (fibre), "Makrolon", and "Panlite". The softening point of Lexan is 428 K and that of Merlon is 410 K. The heat distortion temperature and mold temperature is 406-411 K and 561-589 K, respectively.

Polycarbonates are formed by the condensation of polyphenols (usually Bis-phenol-A) with phosgene. The resulting thermoplastic polymer can be considered an ester of carbonic acid and bisphenol A.



The molecular weight of commercial polycarbonate plastics is up to 30000 (degree of polymerization c. 120), beyond which increasing viscosity limits practical processing. The commonest polycarbonate unit cell contains 4 chains and 8 fundamental units; identity period 21.5 Å. It can be dissolved by certain chlorinated hydrocarbons (dichloroform, methylene chloride, di-, tri-, and tetrachloroethane, hot chlorobenzene), pyridine, dioxan, cyclohexanone, and hot phenols. It will be swollen by acetone, benzene, and carbon tetrachloride. It can be decomposed by hot alcoholic alkalis, amines, and other organic bases, and its surface attack by aq. alkalis.

Polycarbonate has density 1.20 g cm⁻³, has the second order (glass) transition temperature at about 420 K, softens above 430 K, decomposes around 580 K, and is serviceable up to 410 K. Its tensile strength halves at 400 K. Its dielectric constants are 2.7-3.1 over the range 50-10¹⁰ Hz. Its resistivity is about 10¹⁶ Ω cm at room temperature and 10¹⁴ Ω cm at 400 K. Dielectric strength of very thin films is 120 KV/mm and 109 KV/mm for 0.05-0.125 mm films. Its electrical properties show little dependence

on frequency, and are not greatly changed by heating to 410 K or by long immersion in water.

Polycarbonate has specific heat 0.28-0.30, thermal conductivity $0.00192 \text{ W cm}^{-1} \text{ K}^{-1}$, and thermal expansion coefficient $0.6-0.7 \times 10^{-4} \text{ K}^{-1}$ ($0.76 \times 10^{-8} \text{ K}^{-1}$ at 30-410 K). It shrinks 0.5 ~ 0.7% when molding and it is self-extinguishing by the ASTM D-635 test.

a. Normal Spectral Emittance (Wavelength Dependence)

There is no data on emittance of polycarbonate plastics available. However, Pregelhof, Franey, and Haas [T77125] used a one-dimensional model, assuming uniform properties, and gave the emittance $\epsilon(\lambda)$, the absorptance $\alpha(\lambda)$, the transmittance $\tau(\lambda)$, and the reflectance $\rho(\lambda)$ of a polymer sheet in the following expressions:

$$\epsilon(\lambda) = \alpha(\lambda) = \frac{(1-R) [(1+R) \sinh ad + (1-R) (\cosh ad - 1)]}{(1+R^2) \sinh ad + (1-R^2) \cosh ad} \quad (4.17-1)$$

$$\tau(\lambda) = \frac{(1-R)^2}{(1+R^2) \sinh ad + (1-R^2) \cosh ad} \quad (4.17-2)$$

$$\rho(\lambda) = \frac{2R [R \sinh ad + (1-R) \cosh ad]}{(1+R^2) \sinh ad + (1-R^2) \cosh ad} \quad (4.17-3)$$

where $R = (n - 1/n + 1)^2$ and n is the refractive index, d is the thickness of the sample, and a is the absorption coefficient. Therefore, the absorptance can be calculated from the above equations.

For the polycarbonate plastic bulk materials, it can be assumed that

$$e^{ad} \gg R e^{-ad} \quad (4.17-4)$$

which enables Eqs. (4.17-1, 4.17-2, and 4.17-3) to become the following:

$$\epsilon(\lambda) = \alpha(\lambda) \cong (1-R) [1 - (1-R) e^{-ad} - R e^{-2ad}] \quad (4.17-5)$$

$$\tau(\lambda) \cong (1-R)^2 e^{-ad} \quad (4.17-6)$$

$$\rho(\lambda) \cong R [1 + (1-R) e^{-2ad}] \quad (4.17-7)$$

By using these equations together with the experimental data of transmittance and reflectance, the emittance can be calculated. Here we used $d = 4 \text{ mm}$ for the

calculation. The calculated results of emittance for bulk polycarbonate plastic samples with thickness 4 mm at 293K are shown in Table 17-1 and Figure 17-1 with an estimated uncertainty of about $\pm 20\%$.

TABLE 17-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ |
|---------------|------------|-----------|------------|
| THICKNESS 4MM | | | |
| T = 293 | | | |
| 6.61 | 0.12 | 12.50 | 0.940 |
| 6.75 | 0.05 | 13.00 | 0.931 |
| 6.92 | 0.05 | 13.50 | 0.940 |
| 7.00 | 0.05 | 14.00 | 0.949 |
| 7.19 | 0.05 | 14.50 | 0.969 |
| 7.34 | 0.10 | 15.00 | 0.943 |
| 7.59 | 0.16 | | |
| 7.77 | 0.07 | | |
| 7.83 | 0.60 | | |
| 7.95 | 0.77 | | |
| 8.09 | 0.72 | | |
| 8.25 | 0.33 | | |
| 8.43 | 0.37 | | |
| 8.63 | 0.43 | | |
| 8.87 | 0.46 | | |
| 9.08 | 0.52 | | |
| 9.30 | 0.41 | | |
| 9.54 | 0.34 | | |
| 9.80 | 0.35 | | |
| 10.00 | 0.92 | | |
| 10.20 | 0.953 | | |
| 10.40 | 0.961 | | |
| 10.50 | 0.960 | | |
| 10.60 | 0.962 | | |
| 10.70 | 0.955 | | |
| 10.80 | 0.959 | | |
| 10.90 | 0.957 | | |
| 11.00 | 0.953 | | |
| 11.10 | 0.972 | | |
| 11.20 | 0.962 | | |
| 11.30 | 0.914 | | |
| 11.40 | 0.935 | | |
| 11.50 | 0.944 | | |
| 11.60 | 0.939 | | |
| 11.70 | 0.945 | | |
| 11.80 | 0.953 | | |
| 11.90 | 0.947 | | |
| 12.00 | 0.951 | | |
| 12.10 | 0.951 | | |
| 12.20 | 0.951 | | |
| 12.30 | 0.951 | | |
| 12.40 | 0.951 | | |
| 12.50 | 0.951 | | |

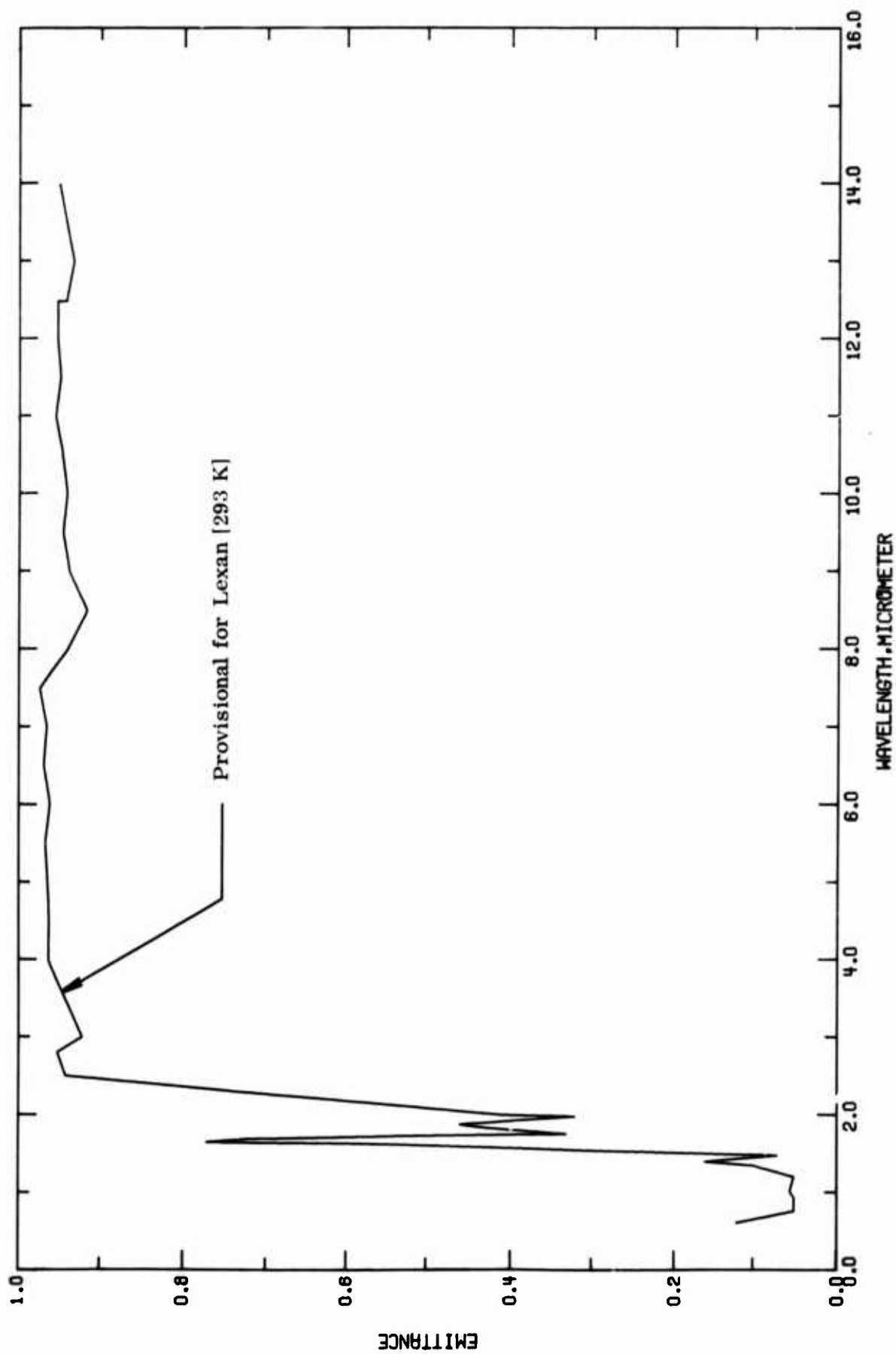


FIGURE 17-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

b. Normal Spectral Reflectance (Wavelength Dependence)

Only Vinokanov, Cherkusov, and Kisilitsu [T71819] have measured the normal spectral reflectance in the 0.05-0.25 μm wavelength region. We can only roughly estimate the normal spectral reflectance by the results of angular reflectance. The provisional normal spectral reflectance values are slightly lower than that of the angular reflectance and are shown in Table 17-2 and Figure 17-2 with an uncertainty of about $\pm 30\%$.

TABLE 17-2. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|-----------|--------|-----------------|--------|
| LEXAN | | LEXAN | |
| T = 293 | | T = 293 (CONT.) | |
| 0.06 | 0.07 | 11.00 | 0.047 |
| 0.10 | 0.11 | 11.50 | 0.053 |
| 0.25 | 0.13 | 12.00 | 0.049 |
| 0.60 | 0.11 | 12.50 | 0.057 |
| 0.75 | 0.17 | 13.00 | 0.061 |
| 0.92 | 0.148 | 13.50 | 0.060 |
| 1.00 | 0.150 | 14.00 | 0.051 |
| 1.19 | 0.190 | 14.50 | 0.051 |
| 1.34 | 0.170 | 15.00 | 0.057 |
| 1.39 | 0.165 | | |
| 1.47 | 0.155 | | |
| 1.53 | 0.128 | | |
| 1.65 | 0.170 | | |
| 1.75 | 0.200 | | |
| 1.78 | 0.364 | | |
| 1.83 | 0.055 | | |
| 1.87 | 0.330 | | |
| 1.98 | 0.030 | | |
| 2.00 | 0.330 | | |
| 2.30 | 0.058 | | |
| 2.50 | 0.050 | | |
| 2.80 | 0.047 | | |
| 2.92 | 0.031 | | |
| 3.00 | 0.034 | | |
| 3.30 | 0.340 | | |
| 4.00 | 0.039 | | |
| 4.50 | 0.040 | | |
| 5.00 | 0.033 | | |
| 5.50 | 0.035 | | |
| 6.00 | 0.041 | | |
| 6.50 | 0.033 | | |
| 7.00 | 0.027 | | |
| 7.50 | 0.120 | | |
| 8.00 | 0.062 | | |
| 8.50 | 0.086 | | |
| 9.00 | 0.054 | | |
| 9.50 | 0.050 | | |
| 10.00 | 0.051 | | |
| 10.60 | 0.054 | | |

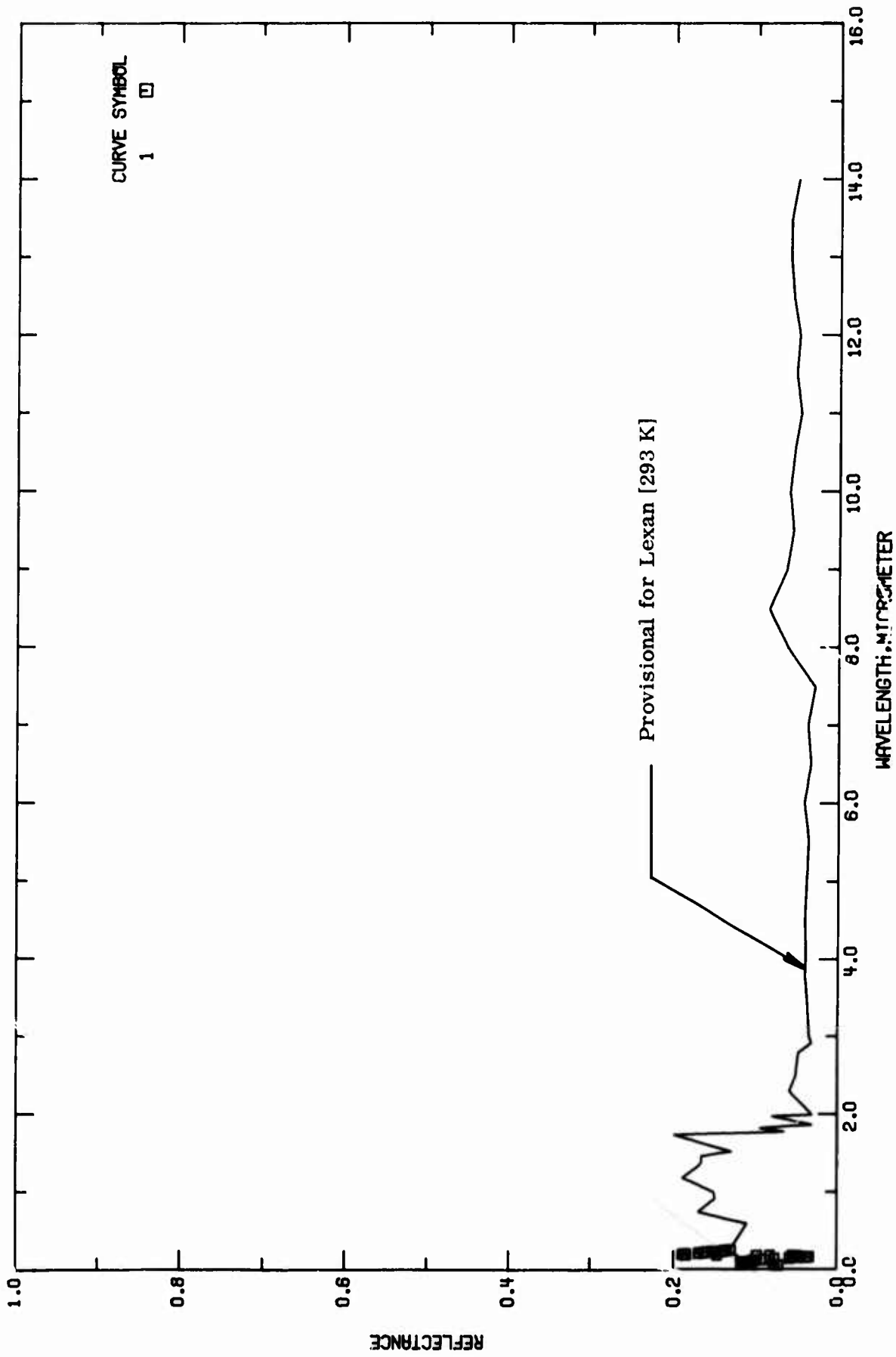


FIGURE 17-2. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

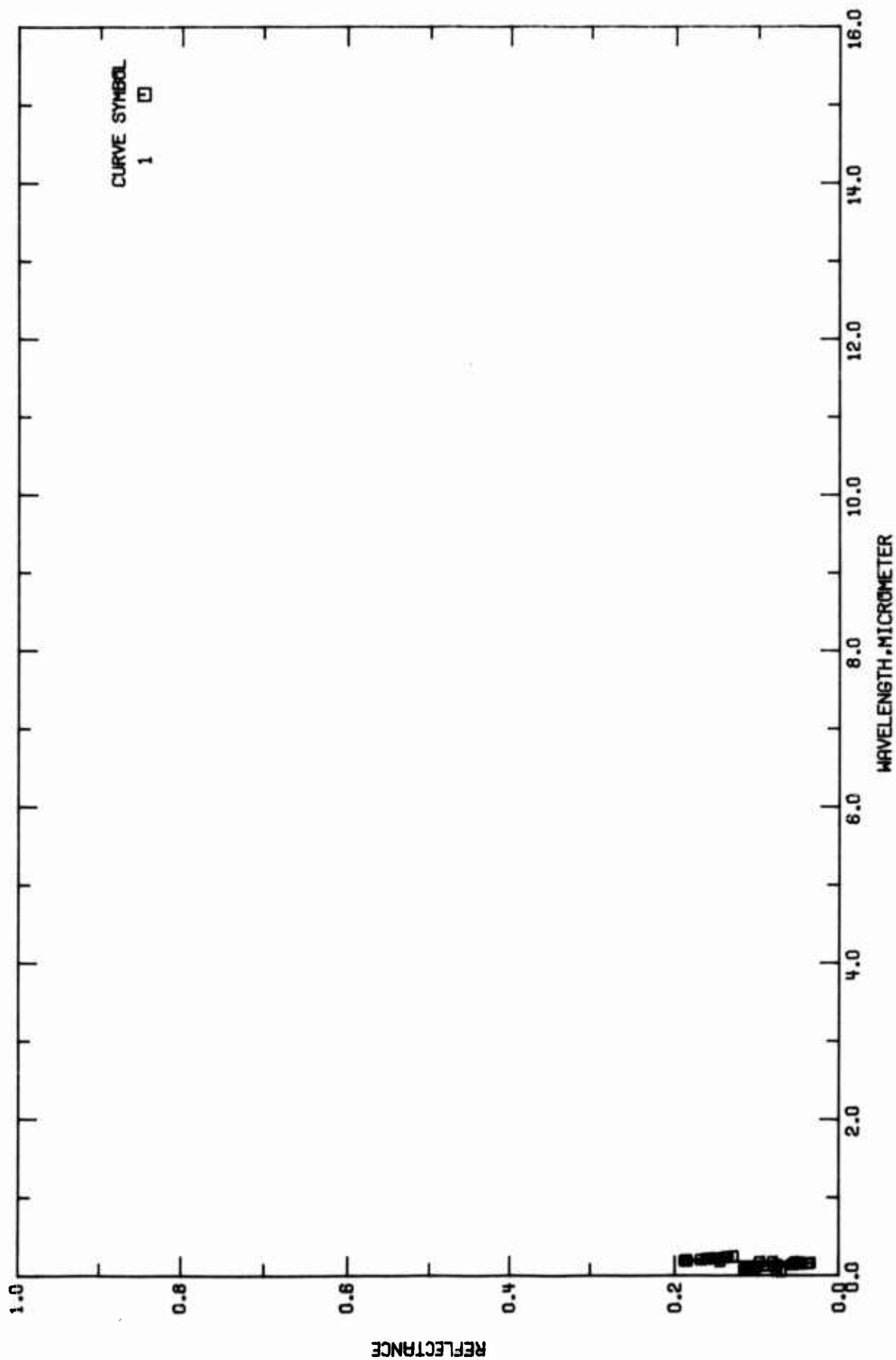


FIGURE 17-3. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

TABLE 17-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|------------------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T71813, T72331 | Vinokurova, L.N., Cherkasov, Yu. A., and Kisilitsa, P. P. | 1973 | 0.05-0.25 | 293 | Polycarbonate | Polymer film with thickness about several μm was deposited from solution on a polished glass face plate; a VMR-2 vacuum monochromator at a resolution of 1.6 mm was used and a glow discharge in hydrogen and technical helium was used as radiation source; data were extracted from figure; $\theta \sim 0^\circ$. |

TABLE 17-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------|--------|
| CURVE 1 | |
| T = 293. | |
| 0.0554 | 0.071 |
| 0.0592 | 0.077 |
| 0.0833 | 0.112 |
| 0.0996 | 0.116 |
| 0.0977 | 0.111 |
| 0.1064 | 0.105 |
| 0.1154 | 0.102 |
| 0.1219 | 0.101 |
| 0.1296 | 0.093 |
| 0.1408 | 0.076 |
| 0.1485 | 0.057 |
| 0.1566 | 0.044 |
| 0.1605 | 0.037 |
| 0.1662 | 0.034 |
| 0.1730 | 0.048 |
| 0.1756 | 0.054 |
| 0.1797 | 0.082 |
| 0.1798 | 0.098 |
| 0.1879 | 0.145 |
| 0.1933 | 0.185 |
| 0.1985 | 0.189 |
| 0.2040 | 0.186 |
| 0.2119 | 0.169 |
| 0.2176 | 0.162 |
| 0.2242 | 0.158 |
| 0.2315 | 0.151 |
| 0.2356 | 0.139 |
| 0.2454 | 0.136 |
| 0.2511 | 0.129 |

c. Angular Spectral Reflectance (Wavelength Dependence)

Only Grimm, Linford, Dillow, Spinak, and Mills [A00001] have measured the angular spectral reflectance for a 290 mm thick disk of Lexan in the 2-15 μm region with the incident angle of 15° and 45° , respectively for curves 1 and 2. The reflectance values increase slightly with the increasing of incident angle.

Pregelhof, Francy, and Haas [T77125] calculated the absorption coefficient $a = 50 \text{ cm}^{-1}$ or larger in the wavelength region $\lambda > 4 \mu\text{m}$. Therefore, Eq. (4.17-7) becomes

$$\rho(\lambda) \cong R = (n - 1/n + 1)^2 \quad (4.17-8)$$

which is independent of the thickness of the sample and depends only on index of refraction. However, the data of index of refraction are not available in the wavelength region above $1 \mu\text{m}$. Thus, Eq. (4.17-8) is not applicable here.

For the wavelength region below $2 \mu\text{m}$, with the aid of the transmittance data, the reflectance can be calculated. Together with the experimental data of Grimm, et al., which is shown in Table 17-3, the provisional values of angular reflectance are shown in Table 17-2 and Figure 17-4 with an estimated uncertainty of about $\pm 30\%$.

TABLE 17-5. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ |
|---------------------|--------|-----------|--------|
| LEXAN | | | |
| $\theta = 15^\circ$ | | | |
| T = 293 (CONT.) | | | |
| 0.06 | 0.071 | 11.00 | 0.048 |
| 0.10 | 0.115 | 11.50 | 0.054 |
| 0.25 | 0.135 | 12.00 | 0.050 |
| 0.60 | 0.115 | 12.50 | 0.058 |
| 0.74 | 0.170 | 13.00 | 0.061 |
| 0.75 | 0.173 | 13.50 | 0.061 |
| 1.00 | 0.149 | 14.00 | 0.052 |
| 1.19 | 0.150 | 14.50 | 0.052 |
| 1.34 | 0.195 | 15.00 | 0.050 |
| 1.39 | 0.174 | | |
| 1.47 | 0.168 | | |
| 1.53 | 0.169 | | |
| 1.53 | 0.130 | | |
| 1.65 | 0.174 | | |
| 1.75 | 0.208 | | |
| 1.79 | 0.265 | | |
| 1.83 | 0.297 | | |
| 1.97 | 0.232 | | |
| 1.98 | 0.242 | | |
| 2.00 | 0.281 | | |
| 2.30 | 0.251 | | |
| 2.50 | 0.251 | | |
| 2.92 | 0.232 | | |
| 3.00 | 0.235 | | |
| 3.30 | 0.241 | | |
| 4.00 | 0.240 | | |
| 4.50 | 0.241 | | |
| 5.00 | 0.239 | | |
| 5.50 | 0.236 | | |
| 6.00 | 0.242 | | |
| 6.50 | 0.234 | | |
| 7.00 | 0.238 | | |
| 7.50 | 0.229 | | |
| 8.00 | 0.263 | | |
| 8.50 | 0.287 | | |
| 9.00 | 0.265 | | |
| 9.50 | 0.257 | | |
| 10.00 | 0.262 | | |
| 10.50 | 0.255 | | |

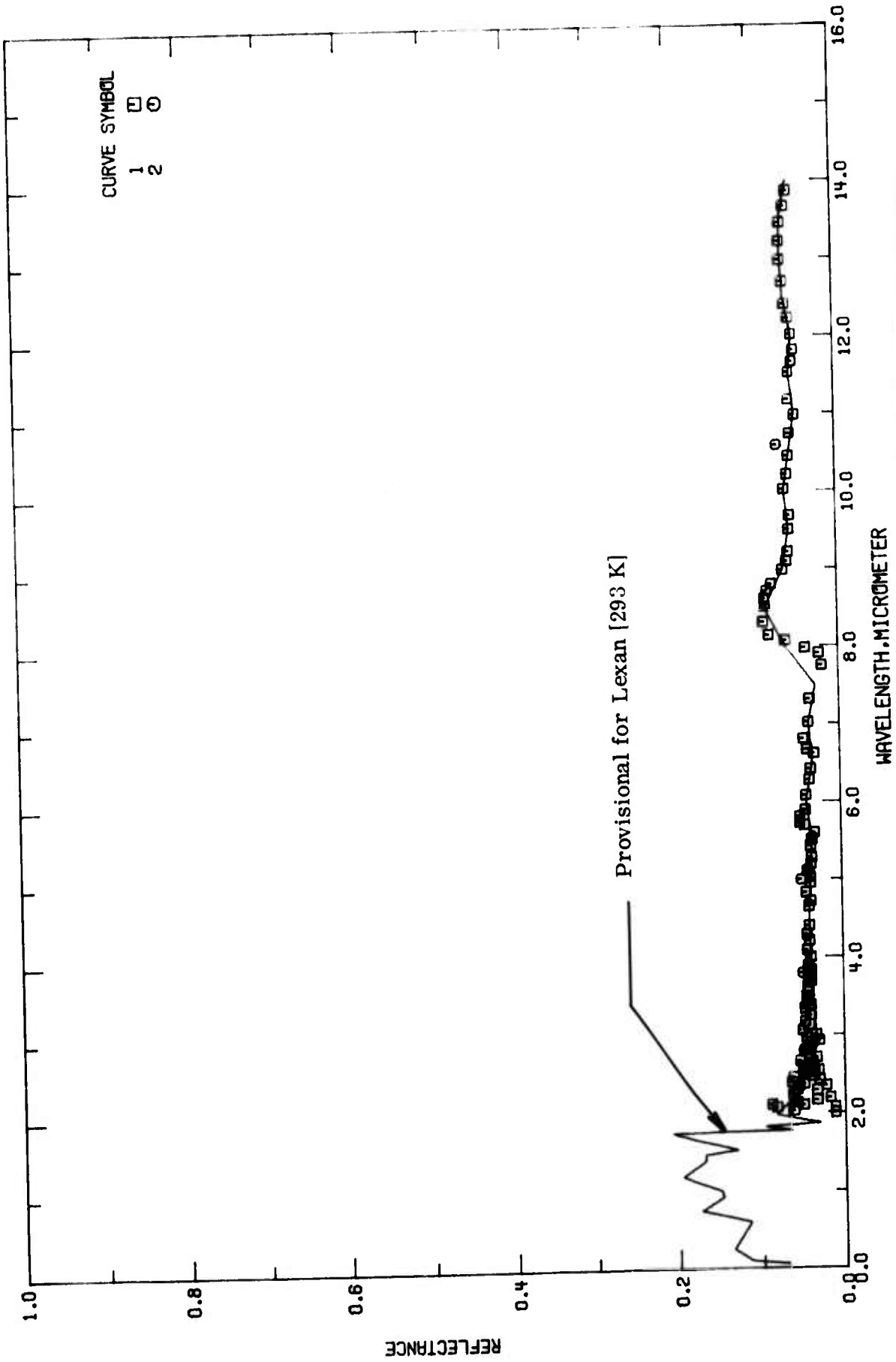


FIGURE 17-4. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

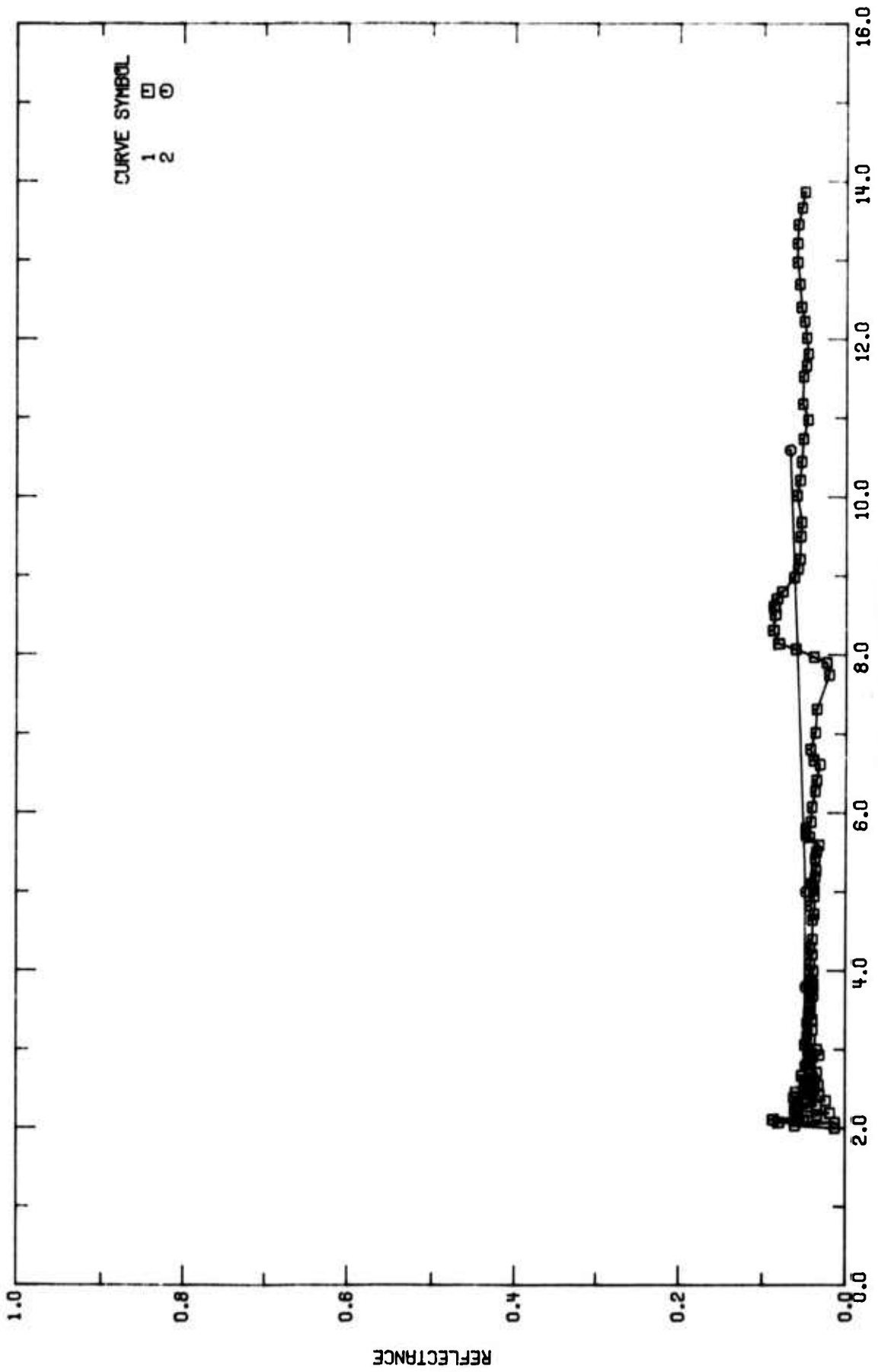


FIGURE 17-5. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

TABLE 17-6. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (Wavelength Dependent)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | Grimm, T.C., Linford, R.M.F., Dillow, C.F., Spinak, S., and Mills, J.P. | 1972 | 2-15 | 293 | Lexan Sample N-1 | One in. diameter disc sample with thickness 290 mil.; reflectance was measured by utilizing a Dune Associate ellipsoidal-mirror reflectometer; $\theta=15^\circ$. |
| 2 | Grimm, T.C., et al. | 1972 | 2-15 | 293 | Lexan Sample N-1 | The above specimen except $\theta=45^\circ$. |

TABLE 17-7. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 T = 293. | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 2 (CONT.) | |
|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 2.00 | 0.013 | 3.38 | 0.041 | 7.98 | 0.040 | 10.6 | 0.07 |
| 2.03 | 0.063 | 3.44 | 0.046 | 8.08 | 0.063 | | |
| 2.07 | 0.013 | 3.46 | 0.044 | 8.15 | 0.083 | | |
| 2.10 | 0.082 | 3.49 | 0.046 | 8.32 | 0.089 | | |
| 2.11 | 0.088 | 3.55 | 0.043 | 8.52 | 0.087 | | |
| 2.13 | 0.059 | 3.61 | 0.044 | 8.62 | 0.088 | | |
| 2.16 | 0.035 | 3.69 | 0.040 | 8.72 | 0.085 | | |
| 2.19 | 0.019 | 3.75 | 0.043 | 8.81 | 0.079 | | |
| 2.23 | 0.063 | 3.83 | 0.040 | 8.99 | 0.065 | | |
| 2.29 | 0.035 | 3.89 | 0.043 | 9.10 | 0.060 | | |
| 2.30 | 0.059 | 4.00 | 0.040 | 9.22 | 0.058 | | |
| 2.35 | 0.024 | 4.09 | 0.044 | 9.51 | 0.057 | | |
| 2.37 | 0.050 | 4.21 | 0.041 | 9.69 | 0.056 | | |
| 2.39 | 0.064 | 4.29 | 0.044 | 10.03 | 0.062 | | |
| 2.42 | 0.032 | 4.40 | 0.041 | 10.22 | 0.058 | | |
| 2.46 | 0.062 | 4.55 | 0.039 | 10.46 | 0.056 | | |
| 2.47 | 0.040 | 4.72 | 0.039 | 10.75 | 0.054 | | |
| 2.50 | 0.051 | 4.83 | 0.044 | 10.99 | 0.048 | | |
| 2.52 | 0.038 | 4.95 | 0.039 | 11.19 | 0.055 | | |
| 2.55 | 0.033 | 5.03 | 0.039 | 11.54 | 0.054 | | |
| 2.59 | 0.051 | 5.11 | 0.042 | 11.68 | 0.050 | | |
| 2.62 | 0.040 | 5.19 | 0.038 | 11.83 | 0.048 | | |
| 2.67 | 0.055 | 5.28 | 0.037 | 12.03 | 0.050 | | |
| 2.68 | 0.043 | 5.43 | 0.036 | 12.24 | 0.053 | | |
| 2.71 | 0.035 | 5.51 | 0.036 | 12.42 | 0.057 | | |
| 2.75 | 0.043 | 5.60 | 0.033 | 12.71 | 0.059 | | |
| 2.81 | 0.046 | 5.70 | 0.045 | 12.99 | 0.062 | | |
| 2.83 | 0.044 | 5.73 | 0.050 | 13.23 | 0.062 | | |
| 2.90 | 0.041 | 5.81 | 0.043 | 13.47 | 0.061 | | |
| 2.93 | 0.032 | 6.08 | 0.042 | 13.68 | 0.056 | | |
| 2.97 | 0.047 | 6.28 | 0.038 | 13.88 | 0.052 | | |
| 3.00 | 0.035 | 6.42 | 0.036 | 14.56 | 0.052 | | |
| 3.06 | 0.051 | 6.62 | 0.032 | 14.68 | 0.054 | | |
| 3.13 | 0.043 | 6.67 | 0.040 | CURVE 2 | | | |
| 3.17 | 0.048 | 6.81 | 0.044 | T = 293. | | | |
| 3.25 | 0.041 | 7.02 | 0.038 | 2.8 | 0.05 | | |
| 3.34 | 0.046 | 7.32 | 0.036 | 3.8 | 0.05 | | |
| | | 7.75 | 0.021 | 5.0 | 0.05 | | |
| | | 7.91 | 0.024 | | | | |

d. Normal Spectral Absorptance (Wavelength Dependence)

There is no data of absorptance available for bulk polycarbonate plastics. Only Fujikura and Ishikawa [T77102] have measured the absorptive power of thin films with thickness of 18 μm and 118 μm at 300 K. The absorptance data was obtained by dividing the absorptive power with the black body radiation power. According to Eq. (4.17-5), the absorptance is strongly dependent on the thickness of the sample for thin films. However, for the bulk materials, in the wavelength region $\lambda > 4 \mu\text{m}$,

$$\alpha(\lambda) \cong (1-R) \quad (4.17-9)$$

which is independent of the thickness, and the material becomes opaque. By using Eqs. (4.17-5, 4.17-6, and 4.17-7), the absorptance can be calculated as equal to the emittance. The calculated results are for a sample with thickness 4 mm at 293 K which are shown in Table 17-8 and Figure 17-6 together with the experimental data of thin films. The estimated uncertainty is about $\pm 20\%$.

TABLE 17-8. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α | λ | α |
|--------------------------|--------------------------|--------------------------|--------------------------|
| THICKNESS μMM | THICKNESS μMM | THICKNESS μMM | THICKNESS μMM |
| T = 293 | T = 293 | T = 293 | T = 293 |
| 0.60 | 0.12 | 12.50 | 0.940 |
| 0.75 | 0.05 | 13.00 | 0.931 |
| 0.92 | 0.05 | 13.50 | 0.940 |
| 1.20 | 0.05 | 14.00 | 0.949 |
| 1.19 | 0.35 | 14.50 | 0.969 |
| 1.34 | 0.10 | 15.00 | 0.943 |
| 1.39 | 0.16 | | |
| 1.47 | 0.07 | | |
| 1.53 | 0.60 | | |
| 1.55 | 0.77 | | |
| 1.69 | 0.72 | | |
| 1.75 | 0.33 | | |
| 1.78 | 0.37 | | |
| 1.83 | 0.43 | | |
| 1.87 | 0.46 | | |
| 1.98 | 0.32 | | |
| 2.00 | 0.41 | | |
| 2.50 | 0.94 | | |
| 2.80 | 0.95 | | |
| 3.00 | 0.92 | | |
| 3.20 | 0.953 | | |
| 4.00 | 0.951 | | |
| 4.50 | 0.960 | | |
| 5.00 | 0.962 | | |
| 5.50 | 0.965 | | |
| 6.00 | 0.959 | | |
| 6.50 | 0.967 | | |
| 7.00 | 0.953 | | |
| 7.50 | 0.972 | | |
| 8.00 | 0.933 | | |
| 8.50 | 0.914 | | |
| 9.00 | 0.936 | | |
| 9.50 | 0.944 | | |
| 10.00 | 0.939 | | |
| 10.60 | 0.946 | | |
| 11.00 | 0.953 | | |
| 11.50 | 0.947 | | |
| 12.00 | 0.951 | | |
| 12.50 | 0.951 | | |

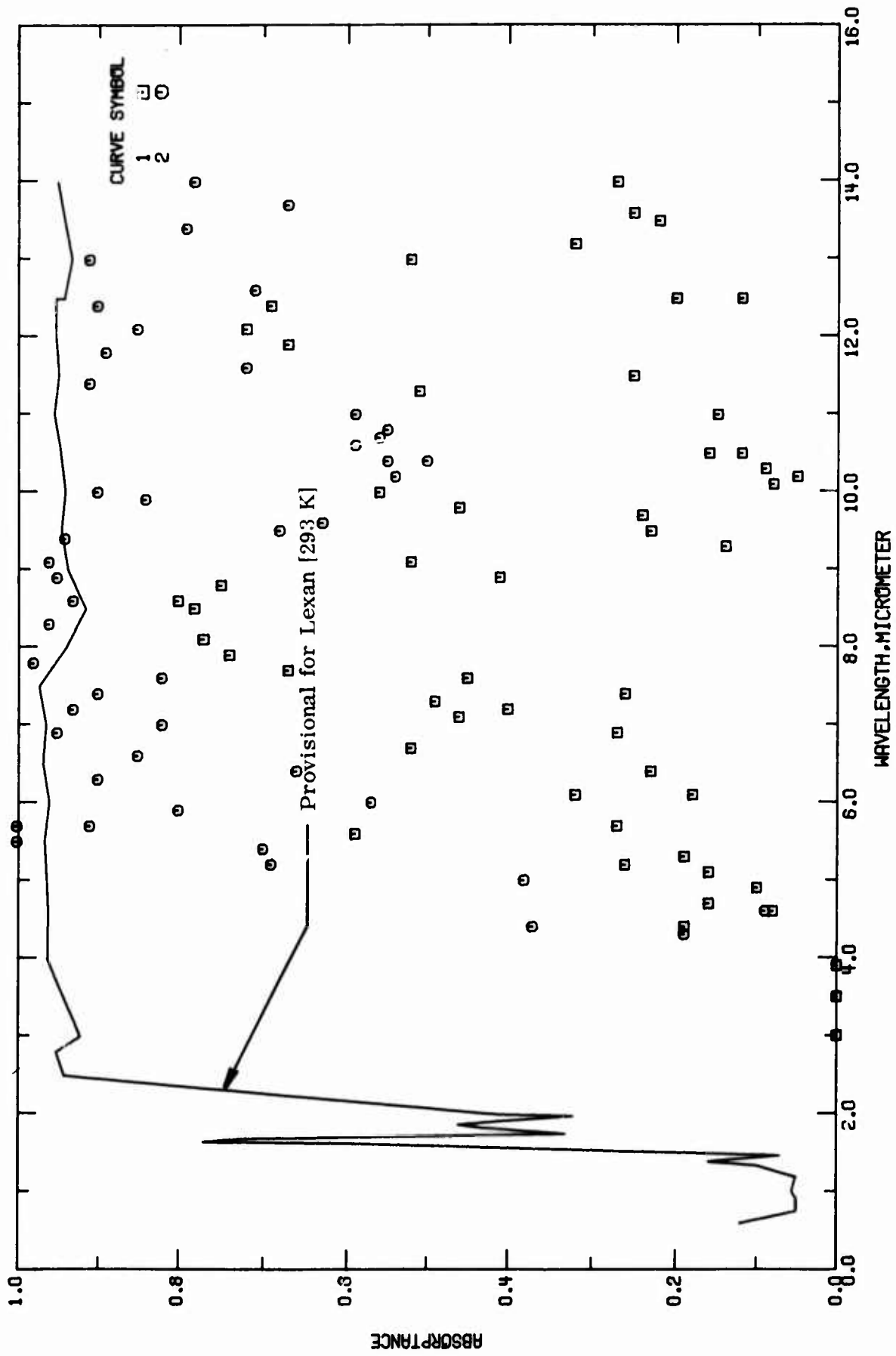


FIGURE 17-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

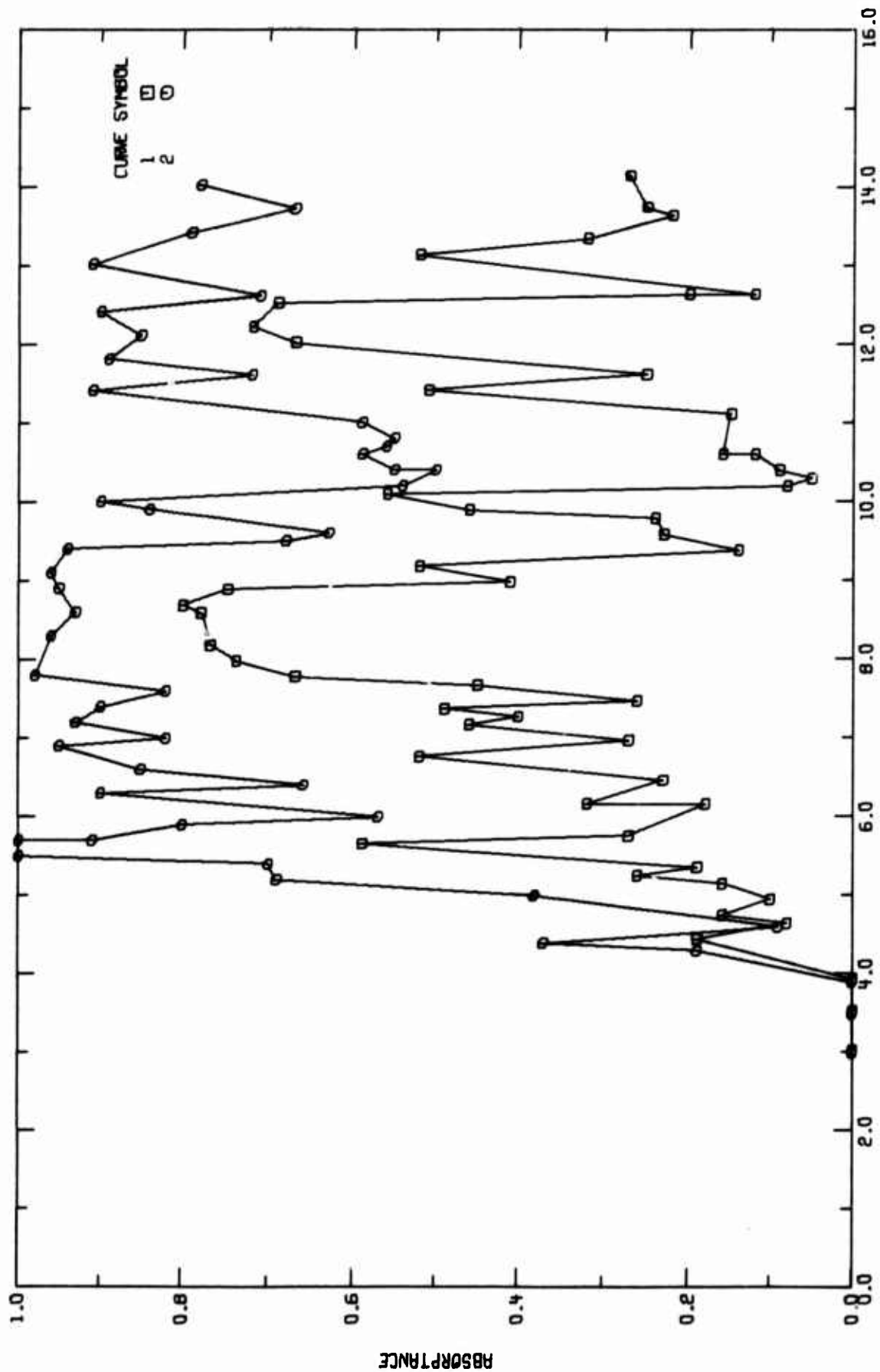


FIGURE 17-7. EXPERIMENTAL NORMAL SPECTRAL ABSORBANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

TABLE 17-9. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T77102 | Fujikura, Y. and Ishikawa, K. | 1968 | 2.5-50 | 300 | | Polycarbonate film; thickness 16 μm ; absorptive power data were extracted from the figure; $\theta=0^\circ$. |
| 2 T77102 | Fujikura, Y. and Ishikawa, K. | 1968 | 2.5-50 | 300 | | Polycarbonate film; thickness 118 μm ; absorptive power data were extracted from the figure; $\theta=0^\circ$. |

TABLE 17-10. EXPERIMENTAL SPECTRAL ABSORPTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| CURVE 1 T = 300. | | CURVE 1 (CONT.) | | CURVE 2 T = 300. | | CURVE 2 (CONT.) | |
|---------------------|----------|-----------------|----------|---------------------|----------|-----------------|----------|
| λ | α | λ | α | λ | α | λ | α |
| 3.00 | 0.00 | 10.50 | 0.16 | 3.00 | 0.000 | 11.40 | 0.91 |
| 3.50 | 0.00 | 11.00 | 0.15 | 3.50 | 0.00 | 11.60 | 0.72 |
| 3.90 | 0.03 | 11.30 | 0.51 | 3.90 | 0.00 | 11.80 | 0.89 |
| 4.40 | 0.19 | 11.50 | 0.25 | 4.30 | 0.00 | 12.10 | 0.85 |
| 4.60 | 0.08 | 11.90 | 0.67 | 4.40 | 0.19 | 12.40 | 0.90 |
| 4.70 | 0.16 | 12.10 | 0.72 | 4.40 | 0.37 | 12.60 | 0.71 |
| 4.90 | 0.10 | 12.40 | 0.69 | 4.50 | 0.09 | 13.00 | 0.91 |
| 5.10 | 0.16 | 12.50 | 0.20 | 5.00 | 0.38 | 13.40 | 0.79 |
| 5.20 | 0.26 | 13.00 | 0.12 | 5.20 | 0.69 | 13.70 | 0.67 |
| 5.30 | 0.19 | 13.20 | 0.52 | 5.40 | 0.70 | 14.00 | 0.78 |
| 5.60 | 0.59 | 13.50 | 0.32 | 5.50 | 1.00 | 14.70 | 0.31 |
| 5.70 | 0.27 | 13.60 | 0.22 | 5.70 | 1.00 | 15.30 | 0.20 |
| 6.10 | 0.18 | 14.00 | 0.25 | 5.70 | 0.91 | 15.70 | 0.37 |
| 6.10 | 0.32 | 14.00 | 0.27 | 5.90 | 0.80 | 16.00 | 0.25 |
| 6.40 | 0.23 | 14.40 | 0.09 | 6.00 | 0.57 | 16.50 | 0.44 |
| 6.70 | 0.52 | 14.90 | 0.07 | 6.30 | 0.90 | 16.90 | 0.67 |
| 6.90 | 0.27 | 15.20 | 0.07 | 6.40 | 0.66 | 17.50 | 0.91 |
| 7.10 | 0.46 | 15.40 | 0.05 | 6.60 | 0.85 | 18.20 | 0.94 |
| 7.20 | 0.40 | 15.60 | 0.05 | 6.90 | 0.95 | 18.60 | 0.81 |
| 7.30 | 0.49 | 16.00 | 0.00 | 7.00 | 0.82 | 18.90 | 0.55 |
| 7.45 | 0.26 | 16.40 | 0.00 | 7.20 | 0.93 | 19.40 | 0.52 |
| 7.60 | 0.45 | 16.80 | 0.10 | 7.40 | 0.90 | 20.50 | 0.51 |
| 7.70 | 0.67 | 17.10 | 0.24 | 7.60 | 0.82 | 21.10 | 0.37 |
| 7.90 | 0.74 | 17.50 | 0.36 | 7.80 | 0.98 | 21.90 | 0.24 |
| 8.10 | 0.77 | 17.80 | 0.60 | 8.30 | 0.96 | 22.40 | 0.25 |
| 8.50 | 0.78 | 18.10 | 0.65 | 8.60 | 0.93 | 23.00 | 0.40 |
| 8.80 | 0.75 | 18.50 | 0.35 | 8.90 | 0.95 | 23.40 | 0.49 |
| 8.90 | 0.41 | 19.30 | 0.15 | 9.10 | 0.96 | 24.00 | 0.55 |
| 9.10 | 0.52 | 19.80 | 0.12 | 9.40 | 0.94 | 24.50 | 0.70 |
| 9.30 | 0.14 | 20.00 | 0.04 | 9.50 | 0.68 | 25.00 | 0.74 |
| 9.50 | 0.23 | 21.00 | 0.05 | 9.60 | 0.63 | 26.70 | 0.65 |
| 9.70 | 0.24 | 22.40 | 0.10 | 9.90 | 0.84 | 28.30 | 0.56 |
| 9.80 | 0.46 | 23.40 | 0.11 | 10.00 | 0.90 | 29.50 | 0.48 |
| 10.00 | 0.56 | 24.30 | 0.16 | 10.20 | 0.54 | 31.00 | 0.41 |
| 10.10 | 0.08 | 24.90 | 0.24 | 10.40 | 0.50 | 32.00 | 0.45 |
| 10.20 | 0.05 | 28.00 | 0.33 | 10.40 | 0.55 | 32.80 | 0.34 |
| 10.30 | 0.09 | 29.10 | 0.33 | 10.60 | 0.59 | 35.00 | 0.39 |
| 10.50 | 0.12 | | | 10.70 | 0.56 | 36.60 | 0.25 |
| | | | | 10.60 | 0.55 | 37.40 | 0.27 |
| | | | | 11.00 | 0.59 | 39.30 | 0.38 |
| | | | | | | 41.00 | 0.23 |
| | | | | | | 45.20 | 0.35 |
| | | | | | | 50.00 | 0.00 |

e. Normal Spectral Transmittance (Wavelength Dependence)

There are 16 sets of experimental data available for the transmittance of polycarbonate plastics as listed in Table 17-13. Of these, 5 sets were measured on thin film samples which are shown in Figure 17-5. They represent reasonably consistent results with each other. The major absorption peaks near $\lambda = 3.4, 5.6, 6.6, 8.1, 8.2, 8.6, 9.8,$ and $12 \mu\text{m}$ are observed.

As we have mentioned in d., the bulk polycarbonate materials become opaque above $\lambda = 4 \mu\text{m}$. At the visible and near infrared region it transmits about 80-90%. Above $1.7 \mu\text{m}$ the transmittance becomes very strongly dependent on the thickness of the sample. Therefore, the recommended values of transmittance for a sample with thickness of 4 mm at 293 K were derived based on the works of Cloud [T54891, curve 4], Acitelli [T40338, curve 7], and Progelhof, et al. [T77125, curve 16]. The values are shown in Table 17-11 and in Figure 17-8 with the experimental data.

The recommended values which are for polished samples are estimated with an uncertainty of about $\pm 20\%$.

TABLE 17-11. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | T | λ | T |
|---------------|---------------|---------------|---------------|
| THICKNESS 4MM | THICKNESS 4MM | THICKNESS 4MM | THICKNESS 4MM |
| T = 293 | T = 293 | T = 293 | (CONT.) |
| 0.35 | 0.35 | 2.60 | 0.07 |
| 0.37 | 0.57 | 2.52 | 0.08 |
| 0.36 | 0.57 | 2.65 | 0.06 |
| 0.40 | 0.66 | 2.70 | 0.00 |
| 0.50 | 0.76 | 2.80 | 0.00 |
| 0.60 | 0.77 | 2.84 | 0.00 |
| 0.70 | 0.84 | 2.90 | 0.05 |
| 0.80 | 0.78 | 2.92 | 0.06 |
| 0.90 | 0.89 | 3.00 | 0.04 |
| 0.92 | 0.37 | 3.22 | 0.00 |
| 1.00 | 0.80 | 3.80 | 0.007 |
| 1.19 | 0.84 | 3.62 | 0.030 |
| 1.30 | 0.76 | 3.92 | 0.002 |
| 1.34 | 0.81 | 3.93 | 0.013 |
| 1.37 | 0.73 | 4.00 | 0.015 |
| 1.39 | 0.66 | 4.12 | 0.013 |
| 1.46 | 0.57 | 4.10 | 0.0 |
| 1.47 | 0.72 | 5.0 | 0.0 |
| 1.50 | 0.76 | 6.0 | 0.0 |
| 1.53 | 0.80 | 7.0 | 0.0 |
| 1.55 | 0.80 | 8.0 | 0.0 |
| 1.59 | 0.79 | 9.0 | 0.0 |
| 1.62 | 0.56 | 10.0 | 0.0 |
| 1.65 | 0.06 | 10.6 | 0.0 |
| 1.69 | 0.11 | 11.0 | 0.0 |
| 1.74 | 0.38 | 12.0 | 0.0 |
| 1.75 | 0.43 | 13.0 | 0.0 |
| 1.83 | 0.57 | 14.0 | 0.0 |
| 1.87 | 0.56 | 15.0 | 0.0 |
| 1.90 | 0.54 | | |
| 1.95 | 0.48 | | |
| 1.98 | 0.50 | | |
| 2.00 | 0.60 | | |
| 2.18 | 0.56 | | |
| 2.21 | 0.07 | | |
| 2.30 | 0.17 | | |
| 2.30 | 0.11 | | |
| 2.50 | 0.01 | | |

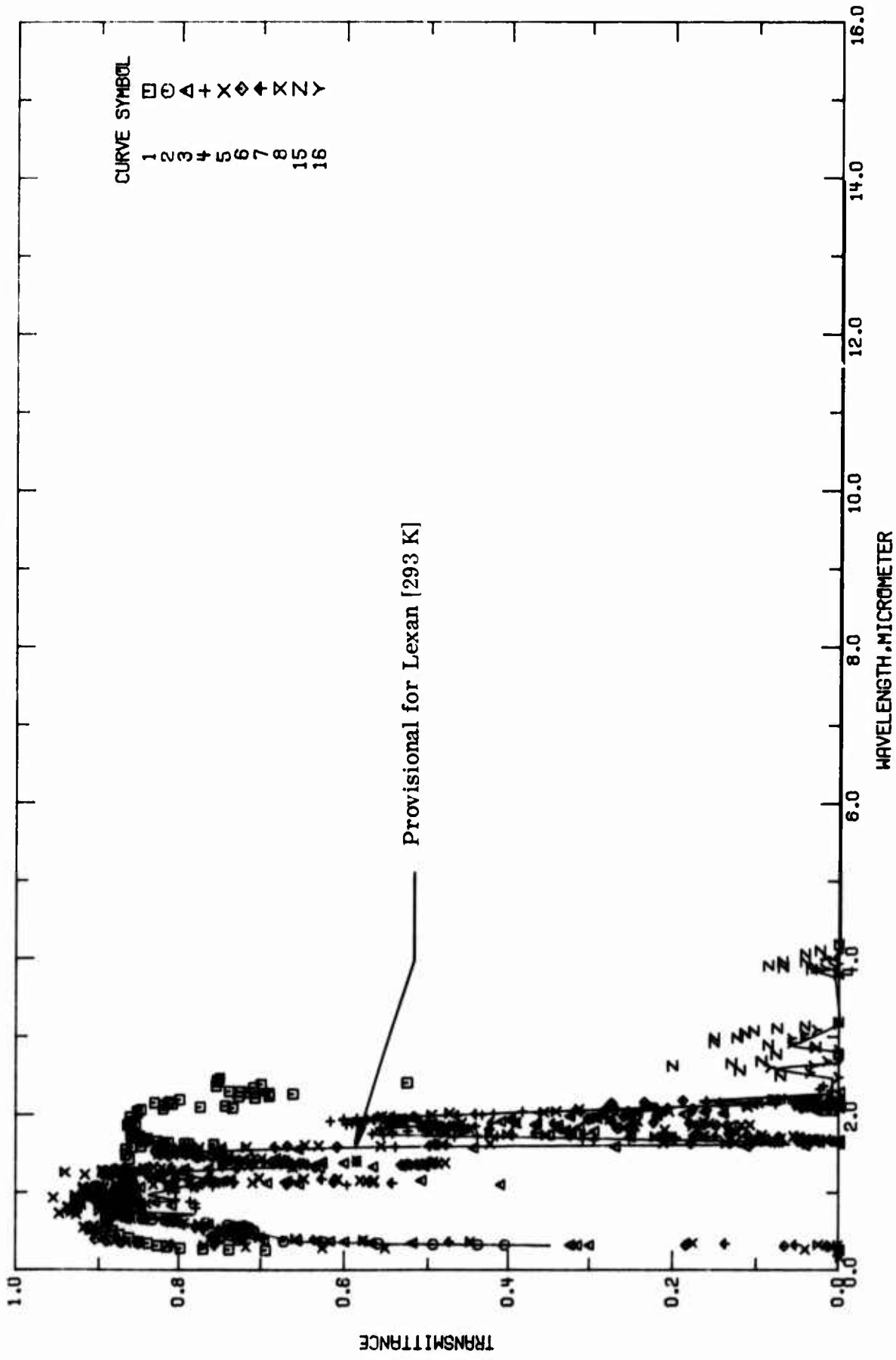


FIGURE 17-8. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

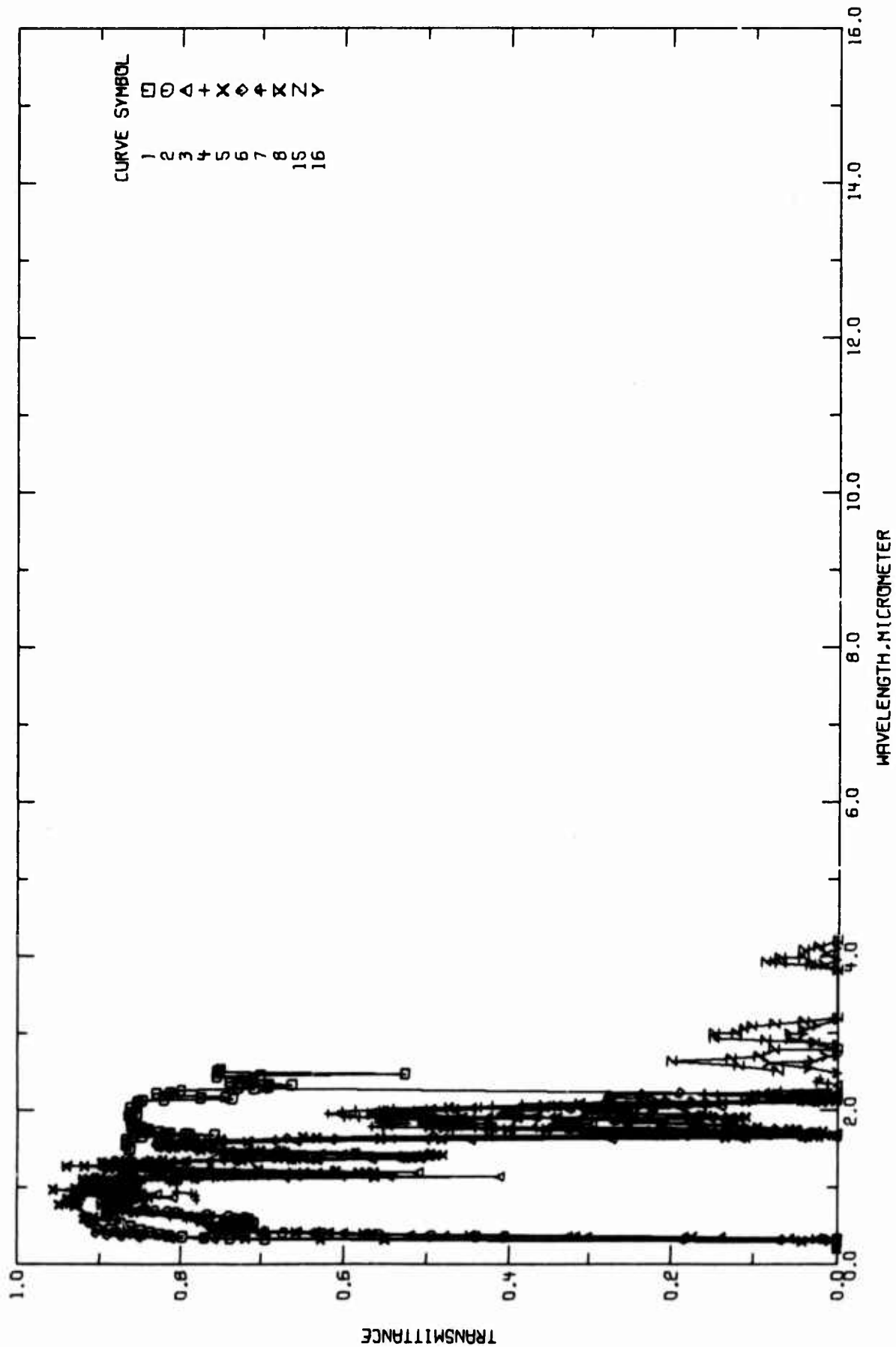


FIGURE 17-9. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE).

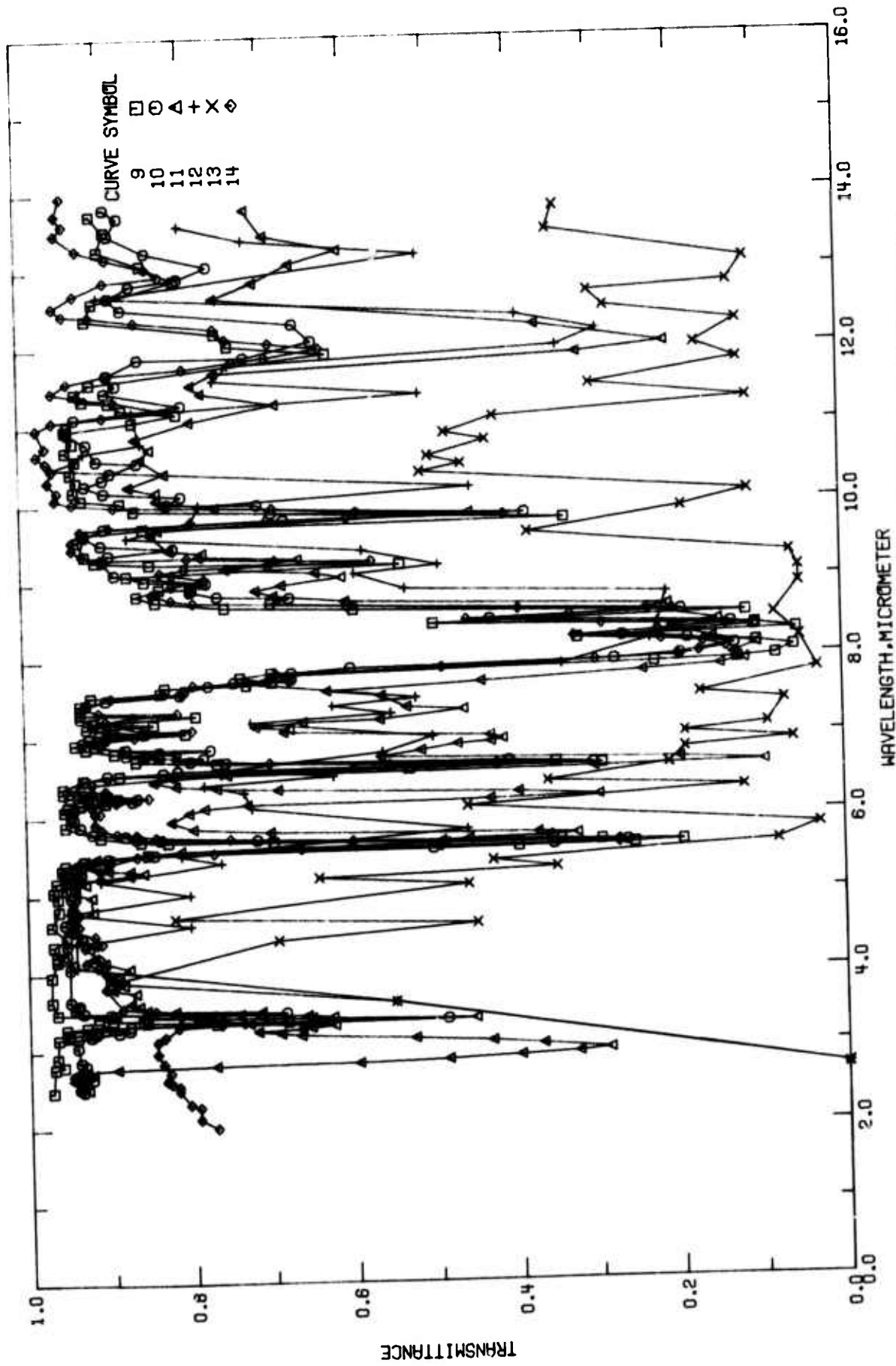


FIGURE 17-10. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS THIN FILMS (WAVELENGTH DEPENDENCE).

TABLE 17-12. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|--------------------------------|--|
| 1 T29-24 | Mobay Chemical Co. | 1962 | 0.2-2.5 | 293 | "Merlon" 100 ASTM D1003-59T | 5 mil. thickness film; refractive index 1.5947; it absorbs essentially all light in the ultraviolet region (up to 2750 Å), it transmits between 80-90% in the visible region (4000 to 7500 Å) and 90% in the infrared wavelength range (8500-1100 Å); the slight absorption of light in 3600 to 5000 Å range gives natural Merlon the light straw-colored hue. |
| 2 T57841 | Cloud, G. | 1970 | 0.3-2.3 | 293 | Merlon | 9.5 mm thickness unannealed sample; Perkin-Elmer model 137-BT spectrometer and Bausch and Lomb Petronic is colorimeter was utilized to measure the transmission spectra; reported error 5%. |
| 3 T57841 | Cloud, G. | 1970 | 0.3-0.9 | 293 | Merlon | 9.4 mm thickness annealed sample (at 154 C for 100 hr); Perkin-Elmer model 137-BT spectrometer and Bausch and Lomb Petronic is colorimeter was utilized to measure the transmission spectra; reported error 5%. |
| 4 T57841 | Cloud, G. | 1970 | 0.8-2.3 | 293 | Lexan | 4.27 mm thickness sample; Perkin-Elmer model 137-BT spectrometer and Bausch and Lomb Petronic is colorimeter was utilized to measure the transmission spectra; reported error 5%. |
| 5 T40338 | Acitelli, M.A., Gumby, W. L., and Nujkas, A.A. | 1966 | 0.2-2.2 | 296 | Poly(allyl diglycol carbonate) | 7.2 mm thickness disc, approx. 50 mm in diameter; Cary Spectrophotometer model 14 was used in measurements. |
| 6 T40333 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 296 | Poly(allyl diglycol carbonate) | The above specimen after 100 standard fade hr in solarization. |
| 7 T40338 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 296 | Polycarbonate "Lexan" | 6.15 mm thickness disc approximately 50 mm in diameter; Cary Spectrophotometer was used in measurements. |
| 8 T40336 | Acitelli, M.A., et al. | 1966 | 0.2-2.2 | 296 | Polycarbonate "Lexan" | The above specimen after 100 standard fade hr in solarization. |
| 9 T76795 | Stimler, S.S. and Kagarise, R.E. | 1966 | 2.5-25 | ~293 | K-1 Resin | Film specimen was obtained from Eastman Chemical Products; a Beckman IR-12 model spectrophotometer was used to obtain the spectra; data were extracted from the figure; $\theta=0^\circ$. |
| 10 T76795 | Stimler, S.S. and Kagarise, R.E. | 1966 | 2.5-25 | ~293 | Merlon M-50 | Film specimen was obtained from Mobay Chemical Co.; other specifications similar to the above specimen. |
| 11 T76798 | Lara, M.O. | 1967 | 2.5-25 | ~293 | Lexan | The specimen was condensed pyrolyzate on potassium bromide or sodium chloride; a Beckman IR-9 double beamed, prism-grating infrared spectrophotometer was used to obtain the spectra; data were extracted from the figures; $\theta=0^\circ$. |
| 12 T77102 | Fujikura, Y. and Isikawa, K. | 1968 | 3-35 | 300 | | Polycarbonate film; thickness 18 μm ; penetrating power data were extracted from the figure. |
| 13 T77102 | Fujikura, Y. and Isikawa, K. | 1968 | 3-35 | 300 | | Polycarbonate film; thickness 118 μm ; penetrating power data were extracted from the figure. |
| 14 T77125 | Frogelhof, R.C., Froney, J., and Haas, T.W. | 1971 | 2-15 | ~293 | | Polycarbonate film was obtained from General Electrical Co.; thickness, 40 μm ; data were extracted from the figure. |
| 15 T77125 | Frogelhof, R.C., et al. | 1971 | 2.5-4.19 | ~293 | | Cast sheet, thickness 0.0825 in.; data were extracted from the figure; $\theta=0^\circ$. |
| 16 T77125 | Frogelhof, R.C., et al. | 1971 | 2.48-4.09 | ~293 | | Cast sheet, thickness 0.1288 in.; data were extracted from the figure; $\theta=0^\circ$. |

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ , %)

| CURVE 1 T = 293. | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | | CURVE 2 T = 293. | | CURVE 2 (CONT.) | | CURVE 3 (CONT.) | | CURVE 3 (CONT.) | |
|---------------------|--------|-----------------|--------|-----------------|--------|---------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 0.286 | 0.000 | 1.662 | 0.819 | 2.778 | 0.754 | 0.353 | 0.406 | 0.842 | 0.874 | 0.651 | 0.804 | 1.346 | 0.631 |
| 0.286 | 0.595 | 1.673 | 0.814 | 2.500 | 0.751 | 0.356 | 0.440 | 0.655 | 0.857 | 0.662 | 0.814 | 1.358 | 0.566 |
| 0.292 | 0.739 | 1.686 | 0.828 | | | 0.363 | 0.495 | 0.864 | 0.857 | 0.683 | 0.846 | 1.369 | 0.506 |
| 0.302 | 0.771 | 1.692 | 0.844 | | | 0.373 | 0.555 | 0.872 | 0.866 | 0.694 | 0.846 | 1.398 | 0.513 |
| 0.314 | 0.799 | 1.710 | 0.846 | | | 0.390 | 0.626 | 0.884 | 0.874 | 0.708 | 0.868 | 1.408 | 0.602 |
| 0.330 | 0.816 | 1.719 | 0.841 | | | 0.402 | 0.673 | 0.891 | 0.868 | 0.719 | 0.872 | 1.413 | 0.628 |
| 0.348 | 0.826 | 1.737 | 0.857 | | | 0.422 | 0.728 | 0.898 | 0.873 | 0.747 | 0.873 | 1.421 | 0.628 |
| 0.375 | 0.840 | 1.751 | 0.851 | | | 0.436 | 0.750 | 0.904 | 0.868 | 0.756 | 0.883 | 1.441 | 0.672 |
| 0.400 | 0.852 | 1.768 | 0.862 | | | 0.458 | 0.759 | 0.914 | 0.868 | 0.784 | 0.884 | 1.464 | 0.683 |
| 0.444 | 0.864 | 1.871 | 0.862 | | | 0.493 | 0.737 | 0.925 | 0.869 | 0.796 | 0.872 | 1.474 | 0.716 |
| 0.455 | 0.876 | 1.888 | 0.856 | | | 0.497 | 0.721 | 0.949 | 0.901 | 0.802 | 0.869 | 1.492 | 0.765 |
| 0.535 | 0.884 | 1.902 | 0.866 | | | 0.536 | 0.705 | 0.957 | 0.893 | 0.812 | 0.882 | 1.517 | 0.797 |
| 0.583 | 0.892 | 1.913 | 0.856 | | | 0.548 | 0.720 | | | 0.830 | 0.849 | 1.535 | 0.797 |
| 0.636 | 0.892 | 1.926 | 0.863 | | | 0.577 | 0.715 | | | 0.843 | 0.849 | 1.554 | 0.778 |
| 0.665 | 0.890 | 2.000 | 0.863 | | | 0.584 | 0.721 | | | 0.868 | 0.810 | 1.572 | 0.749 |
| 0.743 | 0.892 | 2.052 | 0.854 | | | 0.593 | 0.721 | | | 0.877 | 0.850 | 1.591 | 0.656 |
| 0.759 | 0.877 | 2.075 | 0.854 | | | 0.614 | 0.741 | | | 0.888 | 0.850 | 1.605 | 0.446 |
| 0.844 | 0.877 | 2.092 | 0.849 | | | 0.640 | 0.762 | | | 0.902 | 0.831 | 1.615 | 0.271 |
| 0.844 | 0.877 | 2.104 | 0.821 | | | 0.664 | 0.807 | | | 0.927 | 0.866 | 1.628 | 0.114 |
| 0.944 | 0.866 | 2.119 | 0.735 | | | 0.678 | 0.818 | | | 0.988 | 0.866 | 1.633 | 0.042 |
| 0.964 | 0.872 | 2.132 | 0.775 | | | 0.684 | 0.834 | | | 1.010 | 0.856 | 1.654 | 0.000 |
| 1.038 | 0.872 | 2.146 | 0.744 | | | 0.697 | 0.847 | | | 1.029 | 0.868 | 1.694 | 0.000 |
| 1.097 | 0.868 | 2.155 | 0.821 | | | 0.706 | 0.848 | | | 1.073 | 0.868 | 1.702 | 0.075 |
| 1.125 | 0.861 | 2.169 | 0.809 | | | 0.722 | 0.868 | | | 1.094 | 0.850 | 1.715 | 0.092 |
| 1.141 | 0.866 | 2.185 | 0.832 | | | 0.741 | 0.871 | | | 1.104 | 0.783 | 1.726 | 0.049 |
| 1.173 | 0.862 | 2.196 | 0.814 | | | 0.762 | 0.871 | | | 1.130 | 0.412 | 1.735 | 0.212 |
| 1.198 | 0.865 | 2.226 | 0.800 | | | 0.778 | 0.818 | | | 1.142 | 0.655 | 1.743 | 0.253 |
| 1.237 | 0.866 | 2.249 | 0.708 | | | 0.784 | 0.848 | | | 1.152 | 0.694 | 1.754 | 0.177 |
| 1.251 | 0.861 | 2.265 | 0.728 | | | 0.791 | 0.866 | | | 1.162 | 0.672 | 1.771 | 0.351 |
| 1.286 | 0.863 | 2.274 | 0.691 | | | 0.834 | 0.834 | | | 1.182 | 0.510 | 1.792 | 0.324 |
| 1.452 | 0.863 | 2.300 | 0.662 | | | 0.847 | 0.847 | | | 1.191 | 0.738 | 1.802 | 0.325 |
| 1.517 | 0.868 | 2.306 | 0.691 | | | 0.856 | 0.856 | | | 1.197 | 0.790 | 1.816 | 0.296 |
| 1.586 | 0.868 | 2.318 | 0.716 | | | 0.866 | 0.866 | | | 1.204 | 0.624 | 1.830 | 0.331 |
| 1.610 | 0.868 | 2.330 | 0.726 | | | 0.866 | 0.866 | | | 1.241 | 0.869 | 1.847 | 0.340 |
| 1.624 | 0.861 | 2.335 | 0.710 | | | 0.866 | 0.866 | | | 1.263 | 0.869 | 1.868 | 0.314 |
| 1.639 | 0.849 | 2.342 | 0.739 | | | 0.875 | 0.875 | | | 1.293 | 0.869 | 1.887 | 0.131 |
| 1.650 | 0.823 | 2.382 | 0.710 | | | 0.875 | 0.875 | | | 1.293 | 0.869 | 1.896 | 0.340 |
| 1.650 | 0.758 | 2.403 | 0.755 | | | 0.872 | 0.872 | | | 1.308 | 0.812 | 1.896 | 0.369 |
| 1.656 | 0.758 | 2.424 | 0.701 | | | 0.882 | 0.882 | | | 1.322 | 0.796 | 1.919 | 0.366 |
| 1.662 | 0.794 | 2.442 | 0.526 | | | 0.882 | 0.882 | | | 1.335 | 0.765 | 1.928 | 0.393 |
| | | 2.463 | 0.753 | | | 0.828 | 0.828 | | | | | | |

CURVE 3
T = 293.

0.349 0.302
0.351 0.317
0.354 0.326
0.377 0.520
0.382 0.568
0.395 0.601
0.406 0.634
0.412 0.657
0.412 0.697
0.422 0.725
0.430 0.725
0.441 0.751
0.460 0.761
0.469 0.761
0.502 0.719
0.523 0.719
0.537 0.730
0.560 0.730
0.566 0.724
0.578 0.737
0.588 0.733
0.600 0.730
0.622 0.764

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)

| [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ] | |
|--|--------|
| λ | τ |
| 1.943 | 0.411 |
| 1.958 | 0.399 |
| 1.975 | 0.399 |
| 2.012 | 0.326 |
| 2.022 | 0.221 |
| 2.036 | 0.169 |
| 2.048 | 0.141 |
| 2.066 | 0.164 |
| 2.098 | 0.032 |
| 2.118 | 0.000 |
| 2.176 | 0.000 |
| 2.195 | 0.031 |
| 2.212 | 0.031 |
| 2.225 | 0.000 |
| 2.325 | 0.000 |
| CURVE 3 (CONT.) | |
| 1.367 | 0.662 |
| 1.391 | 0.666 |
| 1.415 | 0.726 |
| 1.421 | 0.723 |
| 1.437 | 0.742 |
| 1.463 | 0.746 |
| 1.484 | 0.778 |
| 1.512 | 0.803 |
| 1.547 | 0.603 |
| 1.596 | 0.751 |
| 1.602 | 0.683 |
| 1.618 | 0.539 |
| 1.652 | 0.045 |
| 1.662 | 0.000 |
| 1.670 | 0.080 |
| 1.678 | 0.071 |
| 1.686 | 0.096 |
| 1.705 | 0.296 |
| 1.715 | 0.310 |
| 1.726 | 0.254 |
| 1.747 | 0.469 |
| 1.754 | 0.416 |
| 1.760 | 0.441 |
| 1.768 | 0.553 |
| 1.779 | 0.567 |
| 1.792 | 0.543 |
| 1.808 | 0.543 |
| 1.818 | 0.525 |
| 1.834 | 0.557 |
| 1.861 | 0.557 |
| 1.875 | 0.543 |
| 1.884 | 0.443 |
| 1.891 | 0.475 |
| 1.898 | 0.582 |
| 1.907 | 0.589 |
| 1.921 | 0.592 |
| 1.949 | 0.616 |
| 1.962 | 0.602 |
| 1.975 | 0.602 |
| 1.987 | 0.586 |
| CURVE 4 | |
| T = 293. | |
| 0.830 | 0.786 |
| 0.889 | 0.781 |
| 0.912 | 0.787 |
| 0.934 | 0.805 |
| 1.035 | 0.605 |
| 1.058 | 0.814 |
| 1.091 | 0.814 |
| 1.161 | 0.786 |
| 1.112 | 0.759 |
| 1.131 | 0.598 |
| 1.147 | 0.735 |
| 1.151 | 0.751 |
| 1.165 | 0.732 |
| 1.178 | 0.664 |
| 1.189 | 0.764 |
| 1.200 | 0.602 |
| 1.248 | 0.819 |
| 1.285 | 0.819 |
| 1.314 | 0.737 |
| 1.325 | 0.769 |
| 1.344 | 0.731 |
| CURVE 4 (CONT.) | |
| 1.996 | 0.553 |
| 2.014 | 0.541 |
| 2.031 | 0.435 |
| 2.044 | 0.421 |
| 2.053 | 0.363 |
| 2.069 | 0.384 |
| 2.090 | 0.268 |
| 2.109 | 0.047 |
| 2.125 | 0.011 |
| 2.151 | 0.020 |
| 2.165 | 0.079 |
| 2.178 | 0.058 |
| 2.187 | 0.145 |
| 2.190 | 0.162 |
| 2.207 | 0.161 |
| 2.221 | 0.082 |
| 2.237 | 0.068 |
| 2.258 | 0.011 |
| 2.339 | 0.011 |
| 2.360 | 0.025 |
| 2.400 | 0.021 |
| CURVE 5 | |
| T = 296. | |
| 0.200 | 0.000 |
| 0.284 | 0.000 |
| 0.296 | 0.042 |
| 0.313 | 0.551 |
| 0.318 | 0.627 |
| 0.333 | 0.719 |
| 0.346 | 0.770 |
| 0.357 | 0.814 |
| 0.376 | 0.849 |
| 0.393 | 0.867 |
| 0.413 | 0.881 |
| 0.455 | 0.896 |
| 0.539 | 0.904 |
| 0.554 | 0.912 |
| 0.561 | 0.908 |
| CURVE 5 (CONT.) | |
| 0.569 | 0.908 |
| 0.584 | 0.919 |
| 0.598 | 0.907 |
| 0.754 | 0.928 |
| 0.765 | 0.948 |
| 0.784 | 0.934 |
| 0.817 | 0.934 |
| 0.827 | 0.938 |
| 0.845 | 0.938 |
| 0.878 | 0.922 |
| 0.901 | 0.893 |
| 0.952 | 0.925 |
| 0.963 | 0.955 |
| 0.973 | 0.928 |
| 0.998 | 0.508 |
| 1.027 | 0.898 |
| 1.069 | 0.920 |
| 1.100 | 0.920 |
| 1.118 | 0.899 |
| 1.134 | 0.833 |
| 1.155 | 0.711 |
| 1.173 | 0.573 |
| 1.181 | 0.564 |
| 1.186 | 0.582 |
| 1.199 | 0.609 |
| 1.217 | 0.703 |
| 1.238 | 0.831 |
| 1.258 | 0.879 |
| 1.266 | 0.918 |
| 1.273 | 0.893 |
| 1.296 | 0.897 |
| 1.314 | 0.897 |
| 1.331 | 0.876 |
| 1.341 | 0.823 |
| 1.359 | 0.662 |
| 1.381 | 0.517 |
| 1.392 | 0.520 |
| 1.402 | 0.489 |
| 1.411 | 0.480 |
| 1.421 | 0.495 |
| CURVE 5 (CONT.) | |
| 1.436 | 0.586 |
| 1.466 | 0.700 |
| 1.494 | 0.775 |
| 1.524 | 0.827 |
| 1.581 | 0.829 |
| 1.596 | 0.817 |
| 1.604 | 0.790 |
| 1.611 | 0.749 |
| 1.627 | 0.556 |
| 1.634 | 0.632 |
| 1.642 | 0.648 |
| 1.661 | 0.425 |
| 1.666 | 0.213 |
| 1.674 | 0.126 |
| 1.684 | 0.080 |
| 1.701 | 0.031 |
| 1.714 | 0.017 |
| 1.738 | 0.050 |
| 1.751 | 0.057 |
| 1.764 | 0.095 |
| 1.796 | 0.124 |
| 1.834 | 0.211 |
| 1.854 | 0.251 |
| 1.865 | 0.260 |
| 1.877 | 0.247 |
| 1.891 | 0.178 |
| 1.894 | 0.119 |
| 1.901 | 0.109 |
| 1.918 | 0.158 |
| 1.930 | 0.164 |
| 1.949 | 0.244 |
| 1.970 | 0.277 |
| 1.984 | 0.292 |
| 1.995 | 0.292 |
| 2.007 | 0.284 |
| 2.017 | 0.253 |
| 2.048 | 0.245 |
| 2.075 | 0.206 |
| 2.087 | 0.139 |
| 2.103 | 0.019 |
| CURVE 6 | |
| T = 296. | |
| 0.200 | 0.060 |
| 0.294 | 0.000 |
| 0.306 | 0.012 |
| 0.313 | 0.066 |
| 0.322 | 0.164 |
| 0.328 | 0.755 |
| 0.335 | 0.809 |
| 0.346 | 0.850 |
| 0.360 | 0.873 |
| 0.375 | 0.890 |
| 0.402 | 0.904 |
| 0.533 | 0.912 |
| 0.543 | 0.908 |
| 0.556 | 0.914 |
| 0.764 | 0.925 |
| 0.782 | 0.932 |
| 0.809 | 0.934 |
| 0.848 | 0.934 |
| 0.872 | 0.923 |
| 0.896 | 0.899 |
| 0.914 | 0.899 |
| 0.934 | 0.906 |
| 0.957 | 0.921 |
| 0.967 | 0.910 |
| 0.985 | 0.914 |
| 1.005 | 0.899 |
| 1.025 | 0.899 |
| 1.065 | 0.917 |
| 1.089 | 0.917 |

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| CURVE 6 (CONT.) | | | CURVE 7 (CONT.) | | | CURVE 7 (CONT.) | | | CURVE 7 (CONT.) | | | CURVE 8 | | |
|-----------------|--------|-----------|-----------------|-----------|--------|-----------------|--------|-----------|-----------------|-----------|--------|-----------|--------|--|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | |
| 1.108 | 0.908 | 1.744 | 0.075 | 0.378 | 0.573 | 1.258 | 0.855 | 1.764 | 0.366 | 0.320 | 0.000 | 0.320 | 0.000 | |
| 1.119 | 0.877 | 1.750 | 0.098 | 0.394 | 0.635 | 1.264 | 0.892 | 1.777 | 0.484 | 0.330 | 0.024 | 0.330 | 0.024 | |
| 1.141 | 0.773 | 1.766 | 0.112 | 0.415 | 0.695 | 1.264 | 0.868 | 1.788 | 0.458 | 0.350 | 0.175 | 0.350 | 0.175 | |
| 1.165 | 0.614 | 1.790 | 0.134 | 0.438 | 0.728 | 1.282 | 0.849 | 1.808 | 0.456 | 0.373 | 0.447 | 0.373 | 0.447 | |
| 1.176 | 0.570 | 1.840 | 0.251 | 0.456 | 0.751 | 1.328 | 0.808 | 1.816 | 0.424 | 0.388 | 0.575 | 0.388 | 0.575 | |
| 1.196 | 0.612 | 1.857 | 0.268 | 0.471 | 0.751 | 1.340 | 0.745 | 1.825 | 0.450 | 0.410 | 0.656 | 0.410 | 0.656 | |
| 1.223 | 0.754 | 1.875 | 0.250 | 0.492 | 0.738 | 1.343 | 0.710 | 1.830 | 0.476 | 0.430 | 0.700 | 0.430 | 0.700 | |
| 1.237 | 0.829 | 1.884 | 0.172 | 0.510 | 0.744 | 1.359 | 0.643 | 1.840 | 0.466 | 0.452 | 0.728 | 0.452 | 0.728 | |
| 1.259 | 0.890 | 1.893 | 0.136 | 0.522 | 0.762 | 1.370 | 0.662 | 1.850 | 0.481 | 0.468 | 0.737 | 0.468 | 0.737 | |
| 1.265 | 0.877 | 1.898 | 0.149 | 0.555 | 0.772 | 1.380 | 0.647 | 1.859 | 0.468 | 0.486 | 0.738 | 0.486 | 0.738 | |
| 1.285 | 0.896 | 1.904 | 0.165 | 0.592 | 0.792 | 1.385 | 0.668 | 1.875 | 0.461 | 0.501 | 0.728 | 0.501 | 0.728 | |
| 1.306 | 0.896 | 1.924 | 0.162 | 0.620 | 0.813 | 1.396 | 0.677 | 1.889 | 0.343 | 0.529 | 0.745 | 0.529 | 0.745 | |
| 1.323 | 0.884 | 1.933 | 0.225 | 0.663 | 0.860 | 1.405 | 0.715 | 1.897 | 0.421 | 0.556 | 0.774 | 0.556 | 0.774 | |
| 1.334 | 0.843 | 1.954 | 0.275 | 0.711 | 0.877 | 1.416 | 0.705 | 1.908 | 0.508 | 0.595 | 0.774 | 0.595 | 0.774 | |
| 1.346 | 0.730 | 1.969 | 0.303 | 0.755 | 0.887 | 1.434 | 0.734 | 1.925 | 0.497 | 0.618 | 0.792 | 0.618 | 0.792 | |
| 1.353 | 0.636 | 1.986 | 0.303 | 0.774 | 0.875 | 1.456 | 0.734 | 1.938 | 0.524 | 0.671 | 0.859 | 0.671 | 0.859 | |
| 1.376 | 0.528 | 1.998 | 0.291 | 0.836 | 0.845 | 1.486 | 0.803 | 1.945 | 0.532 | 0.692 | 0.876 | 0.692 | 0.876 | |
| 1.387 | 0.532 | 2.005 | 0.261 | 0.853 | 0.865 | 1.512 | 0.803 | 1.952 | 0.513 | 0.716 | 0.885 | 0.716 | 0.885 | |
| 1.396 | 0.503 | 2.023 | 0.252 | 0.866 | 0.866 | 1.558 | 0.788 | 1.958 | 0.516 | 0.757 | 0.885 | 0.757 | 0.885 | |
| 1.404 | 0.492 | 2.064 | 0.216 | 0.879 | 0.866 | 1.575 | 0.756 | 1.977 | 0.463 | 0.768 | 0.898 | 0.768 | 0.898 | |
| 1.415 | 0.498 | 2.077 | 0.179 | 0.869 | 0.851 | 1.593 | 0.682 | 1.997 | 0.441 | 0.784 | 0.869 | 0.784 | 0.869 | |
| 1.431 | 0.586 | 2.090 | 0.161 | 0.905 | 0.870 | 1.607 | 0.497 | 2.016 | 0.441 | 0.847 | 0.863 | 0.847 | 0.863 | |
| 1.451 | 0.672 | 2.103 | 0.178 | 0.918 | 0.874 | 1.614 | 0.477 | 2.031 | 0.319 | 0.862 | 0.863 | 0.862 | 0.863 | |
| 1.486 | 0.777 | 2.111 | 0.208 | 0.949 | 0.874 | 1.634 | 0.105 | 2.044 | 0.310 | 0.883 | 0.863 | 0.883 | 0.863 | |
| 1.504 | 0.814 | 2.122 | 0.224 | 0.959 | 0.889 | 1.646 | 0.018 | 2.048 | 0.253 | 0.907 | 0.851 | 0.907 | 0.851 | |
| 1.517 | 0.925 | 2.142 | 0.231 | 0.976 | 0.870 | 1.653 | 0.000 | 2.055 | 0.237 | 0.927 | 0.868 | 0.927 | 0.868 | |
| 1.543 | 0.825 | 2.160 | 0.275 | 0.997 | 0.857 | 1.659 | 0.009 | 2.069 | 0.218 | 0.954 | 0.881 | 0.954 | 0.881 | |
| 1.551 | 0.831 | 2.180 | 0.275 | 1.015 | 0.865 | 1.662 | 0.035 | 2.084 | 0.042 | 0.966 | 0.927 | 0.966 | 0.927 | |
| 1.572 | 0.831 | 2.196 | 0.236 | 1.069 | 0.865 | 1.673 | 0.023 | 2.102 | 0.000 | 0.985 | 0.888 | 0.985 | 0.888 | |
| 1.585 | 0.816 | 2.213 | 0.190 | 1.085 | 0.852 | 1.677 | 0.036 | 2.116 | 0.003 | 1.010 | 0.879 | 1.010 | 0.879 | |
| 1.599 | 0.781 | | | 1.100 | 0.812 | 1.687 | 0.047 | 2.155 | 0.003 | 1.058 | 0.893 | 1.058 | 0.893 | |
| 1.617 | 0.610 | | | 1.110 | 0.667 | 1.697 | 0.197 | 2.160 | 0.025 | 1.075 | 0.893 | 1.075 | 0.893 | |
| 1.629 | 0.669 | | | 1.121 | 0.541 | 1.708 | 0.196 | 2.174 | 0.013 | 1.101 | 0.877 | 1.101 | 0.877 | |
| 1.649 | 0.493 | | | 1.132 | 0.665 | 1.714 | 0.209 | 2.184 | 0.055 | 1.110 | 0.803 | 1.110 | 0.803 | |
| 1.662 | 0.180 | | | 1.142 | 0.755 | 1.718 | 0.159 | 2.190 | 0.075 | 1.129 | 0.563 | 1.129 | 0.563 | |
| 1.667 | 0.133 | | | 1.156 | 0.739 | 1.724 | 0.147 | 2.200 | 0.043 | 1.146 | 0.748 | 1.146 | 0.748 | |
| 1.676 | 0.106 | | | 1.174 | 0.626 | 1.728 | 0.175 | | | 1.150 | 0.784 | 1.150 | 0.784 | |
| 1.691 | 0.051 | | | 1.188 | 0.803 | 1.734 | 0.323 | | | 1.181 | 0.647 | 1.181 | 0.647 | |
| 1.704 | 0.031 | | | 1.201 | 0.837 | 1.742 | 0.394 | | | | | | | |
| 1.723 | 0.053 | | | 1.247 | 0.863 | 1.753 | 0.306 | | | | | | | |

CURVE 7
 T = 296.

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | | τ | | λ | | τ | | λ | | τ | | λ | | τ | |
|-----------------|-------|-----------|-------|-----------------|-------|--------|-------|-----------------|-------|-----------|-------|-----------------|-------|-----------|-------|
| CURVE 8 (CONT.) | | 8 (CONT.) | | CURVE 8 (CONT.) | | 9 | | CURVE 9 (CONT.) | | 9 (CONT.) | | CURVE 9 (CONT.) | | 9 (CONT.) | |
| 1.192 | 0.823 | 1.771 | 0.423 | 5.62 | 0.193 | 7.67 | 0.827 | 10.83 | 0.933 | 10.83 | 0.933 | 10.83 | 0.933 | 10.83 | 0.933 |
| 1.207 | 0.865 | 1.774 | 0.479 | 5.64 | 0.293 | 7.69 | 0.724 | 10.99 | 0.942 | 10.99 | 0.942 | 10.99 | 0.942 | 10.99 | 0.942 |
| 1.238 | 0.889 | 1.781 | 0.497 | 5.68 | 0.694 | 7.72 | 0.692 | 11.09 | 0.860 | 11.09 | 0.860 | 11.09 | 0.860 | 11.09 | 0.860 |
| 1.261 | 0.889 | 1.794 | 0.478 | 5.69 | 0.958 | 7.78 | 0.732 | 11.19 | 0.806 | 11.19 | 0.806 | 11.19 | 0.806 | 11.19 | 0.806 |
| 1.266 | 0.939 | 1.812 | 0.478 | 5.71 | 0.859 | 7.84 | 0.693 | 11.25 | 0.873 | 11.25 | 0.873 | 11.25 | 0.873 | 11.25 | 0.873 |
| 1.274 | 0.893 | 1.823 | 0.449 | 5.78 | 0.908 | 7.91 | 0.225 | 11.35 | 0.888 | 11.35 | 0.888 | 11.35 | 0.888 | 11.35 | 0.888 |
| 1.285 | 0.871 | 1.830 | 0.471 | 5.92 | 0.951 | 7.94 | 0.125 | 11.38 | 0.920 | 11.38 | 0.920 | 11.38 | 0.920 | 11.38 | 0.920 |
| 1.295 | 0.871 | 1.837 | 0.501 | 6.05 | 0.944 | 7.97 | 0.079 | 11.47 | 0.929 | 11.47 | 0.929 | 11.47 | 0.929 | 11.47 | 0.929 |
| 1.313 | 0.843 | 1.847 | 0.489 | 6.12 | 0.925 | 8.08 | 0.057 | 11.59 | 0.911 | 11.59 | 0.911 | 11.59 | 0.911 | 11.59 | 0.911 |
| 1.333 | 0.831 | 1.857 | 0.505 | 6.17 | 0.948 | 8.14 | 0.102 | 11.93 | 0.620 | 11.93 | 0.620 | 11.93 | 0.620 | 11.93 | 0.620 |
| 1.349 | 0.723 | 1.865 | 0.490 | 6.20 | 0.932 | 8.23 | 0.320 | 12.05 | 0.740 | 12.05 | 0.740 | 12.05 | 0.740 | 12.05 | 0.740 |
| 1.367 | 0.656 | 1.875 | 0.494 | 6.22 | 0.902 | 8.31 | 0.054 | 12.21 | 0.756 | 12.21 | 0.756 | 12.21 | 0.756 | 12.21 | 0.756 |
| 1.375 | 0.579 | 1.893 | 0.389 | 6.27 | 0.892 | 8.37 | 0.103 | 12.41 | 0.915 | 12.41 | 0.915 | 12.41 | 0.915 | 12.41 | 0.915 |
| 1.385 | 0.657 | 1.902 | 0.458 | 6.30 | 0.922 | 8.45 | 0.497 | 12.63 | 0.906 | 12.63 | 0.906 | 12.63 | 0.906 | 12.63 | 0.906 |
| 1.390 | 0.680 | 1.907 | 0.527 | 6.30 | 0.945 | 8.54 | 0.114 | 12.90 | 0.806 | 12.90 | 0.806 | 12.90 | 0.806 | 12.90 | 0.806 |
| 1.402 | 0.691 | 1.913 | 0.542 | 6.35 | 0.953 | 8.64 | 0.592 | 13.11 | 0.847 | 13.11 | 0.847 | 13.11 | 0.847 | 13.11 | 0.847 |
| 1.411 | 0.731 | 1.922 | 0.532 | 6.41 | 0.953 | 8.68 | 0.750 | 13.30 | 0.896 | 13.30 | 0.896 | 13.30 | 0.896 | 13.30 | 0.896 |
| 1.424 | 0.720 | 1.932 | 0.544 | 6.51 | 0.928 | 8.77 | 0.836 | 13.55 | 0.890 | 13.55 | 0.890 | 13.55 | 0.890 | 13.55 | 0.890 |
| 1.438 | 0.745 | 1.942 | 0.567 | 6.55 | 0.884 | 8.85 | 0.859 | 13.76 | 0.907 | 13.76 | 0.907 | 13.76 | 0.907 | 13.76 | 0.907 |
| 1.465 | 0.751 | 1.952 | 0.567 | 6.60 | 0.929 | 8.94 | 0.831 | 14.12 | 0.885 | 14.12 | 0.885 | 14.12 | 0.885 | 14.12 | 0.885 |
| 1.477 | 0.774 | 1.967 | 0.547 | 6.62 | 0.291 | 8.94 | 0.791 | 14.27 | 0.915 | 14.27 | 0.915 | 14.27 | 0.915 | 14.27 | 0.915 |
| 1.513 | 0.811 | 1.950 | 0.553 | 6.65 | 0.349 | 9.02 | 0.776 | 14.47 | 0.927 | 14.47 | 0.927 | 14.47 | 0.927 | 14.47 | 0.927 |
| 1.540 | 0.811 | 2.001 | 0.495 | 6.69 | 0.763 | 9.04 | 0.849 | 15.38 | 0.932 | 15.38 | 0.932 | 15.38 | 0.932 | 15.38 | 0.932 |
| 1.561 | 0.799 | 2.026 | 0.473 | 6.73 | 0.864 | 9.12 | 0.871 | 15.58 | 0.923 | 15.58 | 0.923 | 15.58 | 0.923 | 15.58 | 0.923 |
| 1.576 | 0.774 | 2.037 | 0.355 | 6.81 | 0.835 | 9.22 | 0.535 | 16.05 | 0.931 | 16.05 | 0.931 | 16.05 | 0.931 | 16.05 | 0.931 |
| 1.590 | 0.716 | 2.048 | 0.340 | 6.84 | 0.890 | 9.26 | 0.842 | 16.72 | 0.919 | 16.72 | 0.919 | 16.72 | 0.919 | 16.72 | 0.919 |
| 1.620 | 0.482 | 2.058 | 0.274 | 6.91 | 0.924 | 9.30 | 0.909 | 17.27 | 0.885 | 17.27 | 0.885 | 17.27 | 0.885 | 17.27 | 0.885 |
| 1.641 | 0.135 | 2.076 | 0.312 | 6.96 | 0.937 | 9.36 | 0.921 | 17.54 | 0.763 | 17.54 | 0.763 | 17.54 | 0.763 | 17.54 | 0.763 |
| 1.654 | 0.028 | 2.108 | 0.110 | 7.03 | 0.920 | 9.57 | 0.929 | 17.83 | 0.732 | 17.83 | 0.732 | 17.83 | 0.732 | 17.83 | 0.732 |
| 1.665 | 0.000 | 2.118 | 0.031 | 7.08 | 0.802 | 9.66 | 0.922 | 18.21 | 0.837 | 18.21 | 0.837 | 18.21 | 0.837 | 18.21 | 0.837 |
| 1.674 | 0.041 | 2.131 | 0.000 | 7.11 | 0.892 | 9.72 | 0.849 | 18.48 | 0.870 | 18.48 | 0.870 | 18.48 | 0.870 | 18.48 | 0.870 |
| 1.686 | 0.030 | 2.162 | 0.000 | 7.14 | 0.907 | 9.78 | 0.334 | 19.01 | 0.890 | 19.01 | 0.890 | 19.01 | 0.890 | 19.01 | 0.890 |
| 1.698 | 0.070 | 2.172 | 0.042 | 7.18 | 0.890 | 9.95 | 0.860 | 20.04 | 0.889 | 20.04 | 0.889 | 20.04 | 0.889 | 20.04 | 0.889 |
| 1.704 | 0.204 | 2.185 | 0.025 | 7.20 | 0.841 | 10.05 | 0.877 | 20.37 | 0.886 | 20.37 | 0.886 | 20.37 | 0.886 | 20.37 | 0.886 |
| 1.714 | 0.206 | 2.190 | 0.037 | 7.24 | 0.915 | 10.10 | 0.923 | 21.83 | 0.886 | 21.83 | 0.886 | 21.83 | 0.886 | 21.83 | 0.886 |
| 1.720 | 0.221 | 2.192 | 0.077 | 7.30 | 0.789 | 10.20 | 0.933 | 22.57 | 0.861 | 22.57 | 0.861 | 22.57 | 0.861 | 22.57 | 0.861 |
| 1.730 | 0.161 | 2.200 | 0.080 | 7.35 | 0.930 | 10.33 | 0.929 | 23.58 | 0.808 | 23.58 | 0.808 | 23.58 | 0.808 | 23.58 | 0.808 |
| 1.744 | 0.353 | 2.281 | 0.698 | 7.46 | 0.930 | 10.44 | 0.936 | 25.00 | 0.749 | 25.00 | 0.749 | 25.00 | 0.749 | 25.00 | 0.749 |
| 1.749 | 0.401 | 5.54 | 0.397 | 7.56 | 0.917 | 10.60 | 0.930 | 10.60 | 0.930 | 10.60 | 0.930 | 10.60 | 0.930 | 10.60 | 0.930 |
| 1.762 | 0.323 | 5.59 | 0.253 | 7.60 | 0.832 | 10.72 | 0.942 | 10.72 | 0.942 | 10.72 | 0.942 | 10.72 | 0.942 | 10.72 | 0.942 |

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 10 (CONT.) | | CURVE 11 (CONT.) | |
|------------------|--------|------------------|--------|------------------|--------|------------------|--------|------------------|--------|------------------|--------|------------------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 2.50 | 0.934 | 5.49 | 0.900 | 7.06 | 0.998 | 10.00 | 0.766 | 17.57 | 0.803 | 3.31 | 0.624 | | |
| 2.65 | 0.932 | 5.52 | 0.843 | 7.08 | 0.852 | 10.02 | 0.820 | 17.89 | 0.817 | 3.33 | 0.728 | | |
| 2.66 | 0.923 | 5.56 | 0.502 | 7.15 | 0.923 | 10.12 | 0.802 | 18.28 | 0.868 | 3.37 | 0.454 | | |
| 2.68 | 0.930 | 5.59 | 0.353 | 7.23 | 0.913 | 10.18 | 0.896 | 18.59 | 0.782 | 3.40 | 0.652 | | |
| 2.82 | 0.931 | 5.61 | 0.262 | 7.29 | 0.930 | 10.28 | 0.919 | 19.12 | 0.815 | 3.41 | 0.626 | | |
| 2.87 | 0.937 | 5.65 | 0.344 | 7.46 | 0.923 | 10.35 | 0.897 | 19.69 | 0.893 | 3.43 | 0.657 | | |
| 3.06 | 0.942 | 5.69 | 0.714 | 7.52 | 0.899 | 10.44 | 0.888 | 20.24 | 0.911 | 3.44 | 0.715 | | |
| 3.18 | 0.941 | 5.71 | 0.835 | 7.57 | 0.808 | 10.56 | 0.855 | 20.79 | 0.902 | 3.46 | 0.740 | | |
| 3.20 | 0.924 | 5.74 | 0.865 | 7.62 | 0.803 | 10.59 | 0.904 | 21.32 | 0.910 | 3.49 | 0.713 | | |
| 3.24 | 0.919 | 5.77 | 0.879 | 7.68 | 0.773 | 10.81 | 0.916 | 22.68 | 0.894 | 3.51 | 0.822 | | |
| 3.25 | 0.991 | 5.81 | 0.918 | 7.72 | 0.740 | 10.95 | 0.939 | 23.53 | 0.864 | 3.53 | 0.857 | | |
| 3.28 | 0.878 | 5.90 | 0.933 | 7.75 | 0.668 | 11.05 | 0.939 | 25.00 | 0.772 | 3.59 | 0.866 | | |
| 3.30 | 0.878 | 6.00 | 0.940 | 7.83 | 0.668 | 11.14 | 0.930 | | | 3.62 | 0.876 | | |
| 3.33 | 0.877 | 6.12 | 0.940 | 7.89 | 0.597 | 11.29 | 0.800 | | | 3.75 | 0.870 | | |
| 3.37 | 0.869 | 6.19 | 0.932 | 7.94 | 0.274 | 11.47 | 0.893 | | | 3.81 | 0.899 | | |
| 3.40 | 0.704 | 6.21 | 0.917 | 7.99 | 0.194 | 11.56 | 0.880 | | | 3.86 | 0.884 | | |
| 3.44 | 0.857 | 6.22 | 0.869 | 8.10 | 0.128 | 11.70 | 0.890 | | | 3.93 | 0.890 | | |
| 3.47 | 0.682 | 6.25 | 0.863 | 8.19 | 0.184 | 11.89 | 0.852 | | | 3.96 | 0.500 | | |
| 3.49 | 0.901 | 6.25 | 0.886 | 8.24 | 0.264 | 11.89 | 0.720 | | | 4.07 | 0.877 | | |
| 3.51 | 0.933 | 6.31 | 0.901 | 8.34 | 0.105 | 12.09 | 0.637 | | | 4.16 | 0.907 | | |
| 3.56 | 0.944 | 6.32 | 0.928 | 8.39 | 0.132 | 12.32 | 0.659 | | | 4.22 | 0.920 | | |
| 3.58 | 0.939 | 6.39 | 0.939 | 8.48 | 0.428 | 12.53 | 0.872 | | | 4.39 | 0.920 | | |
| 3.61 | 0.938 | 6.49 | 0.926 | 8.56 | 0.192 | 12.69 | 0.887 | | | 4.47 | 0.934 | | |
| 3.66 | 0.949 | 6.55 | 0.899 | 8.59 | 0.598 | 12.84 | 0.861 | | | 4.56 | 0.950 | | |
| 4.07 | 0.949 | 6.57 | 0.831 | 8.73 | 0.692 | 12.92 | 0.802 | | | 4.72 | 0.943 | | |
| 4.13 | 0.944 | 6.59 | 0.813 | 8.80 | 0.669 | 13.07 | 0.765 | | | 4.81 | 0.920 | | |
| 4.26 | 0.952 | 6.61 | 0.503 | 8.83 | 0.755 | 13.26 | 0.841 | | | 5.00 | 0.921 | | |
| 4.38 | 0.952 | 6.62 | 0.303 | 8.90 | 0.793 | 13.50 | 0.886 | | | 5.06 | 0.941 | | |
| 4.47 | 0.933 | 6.67 | 0.408 | 8.94 | 0.793 | 13.72 | 0.874 | | | 5.14 | 0.941 | | |
| 4.66 | 0.954 | 6.69 | 0.752 | 9.00 | 0.772 | 13.83 | 0.890 | | | 5.17 | 0.928 | | |
| 4.84 | 0.945 | 6.71 | 0.797 | 9.12 | 0.886 | 14.34 | 0.897 | | | 5.21 | 0.935 | | |
| 5.00 | 0.946 | 6.75 | 0.780 | 9.30 | 0.899 | 14.35 | 0.889 | | | 5.27 | 0.875 | | |
| 5.10 | 0.952 | 6.78 | 0.854 | 9.38 | 0.892 | 14.56 | 0.910 | | | 5.29 | 0.857 | | |
| 5.20 | 0.952 | 6.81 | 0.876 | 9.45 | 0.813 | 15.06 | 0.927 | | | 5.32 | 0.874 | | |
| 5.29 | 0.933 | 6.84 | 0.835 | 9.51 | 0.901 | 15.58 | 0.927 | | | 5.34 | 0.901 | | |
| 5.34 | 0.939 | 6.86 | 0.771 | 9.62 | 0.921 | 15.87 | 0.916 | | | 5.40 | 0.922 | | |
| 5.38 | 0.933 | 6.88 | 0.876 | 9.73 | 0.897 | 16.18 | 0.931 | | | 5.47 | 0.899 | | |
| 5.40 | 0.938 | 6.93 | 0.914 | 9.79 | 0.674 | 16.86 | 0.908 | | | 5.49 | 0.915 | | |
| 5.46 | 0.931 | 6.98 | 0.928 | 9.85 | 0.383 | 17.09 | 0.923 | | | 5.56 | 0.811 | | |
| | | 7.03 | 0.951 | 9.89 | 0.689 | 17.30 | 0.913 | | | 5.60 | 0.600 | | |

CURVE 11
T = 293.

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T , K ; TRANSMITTANCE, τ]

| CURVE 11 (CONT.) | | CURVE 11 (CONT.) | | CURVE 11 (CONT.) | | CURVE 12 (CONT.) | | CURVE 12 (CONT.) | | CURVE 13 (CONT.) | |
|------------------|--------|------------------|--------|------------------|--------|------------------|--------|------------------|--------|------------------|--------|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
| 5.63 | 0.489 | 7.79 | 0.240 | 12.66 | 0.759 | 5.00 | 0.80 | 12.40 | 0.39 | 3.90 | 0.90 |
| 5.66 | 0.492 | 7.85 | 0.146 | 12.85 | 0.702 | 5.20 | 0.91 | 12.70 | 0.90 | 4.40 | 0.69 |
| 5.68 | 0.459 | 7.91 | 0.117 | 13.09 | 0.663 | 5.40 | 0.76 | 13.20 | 0.51 | 4.60 | 0.45 |
| 5.69 | 0.360 | 7.99 | 0.130 | 13.26 | 0.605 | 5.50 | 0.81 | 13.40 | 0.72 | 4.70 | 0.82 |
| 5.72 | 0.324 | 8.11 | 0.102 | 13.46 | 0.694 | 5.80 | 0.46 | 13.60 | 0.80 | 5.10 | 0.46 |
| 5.74 | 0.373 | 8.20 | 0.155 | 13.79 | 0.717 | 6.10 | 0.72 | 14.20 | 0.76 | 5.20 | 0.64 |
| 5.79 | 0.698 | 8.34 | 0.203 | 14.10 | 0.744 | 6.30 | 0.73 | 14.70 | 0.94 | 5.30 | 0.35 |
| 5.84 | 0.795 | 8.42 | 0.148 | 14.25 | 0.692 | 6.40 | 0.78 | 15.40 | 0.96 | 5.40 | 0.43 |
| 5.94 | 0.823 | 8.58 | 0.236 | 14.43 | 0.698 | 6.50 | 0.62 | 15.70 | 0.99 | 5.60 | 0.08 |
| 6.05 | 0.800 | 8.64 | 0.209 | 14.62 | 0.674 | 6.60 | 0.75 | 15.90 | 0.99 | 5.80 | 0.03 |
| 6.10 | 0.780 | 8.75 | 0.602 | 14.84 | 0.733 | 6.80 | 0.56 | 16.20 | 1.00 | 6.10 | 0.46 |
| 6.14 | 0.726 | 8.83 | 0.689 | 15.08 | 0.747 | 7.00 | 0.50 | 16.70 | 1.00 | 6.30 | 0.12 |
| 6.19 | 0.432 | 8.90 | 0.711 | 15.87 | 0.703 | 7.20 | 0.72 | 17.60 | 0.65 | 6.40 | 0.36 |
| 6.21 | 0.296 | 8.96 | 0.679 | 16.13 | 0.730 | 7.30 | 0.55 | 17.80 | 0.43 | 6.60 | 0.21 |
| 6.27 | 0.397 | 9.06 | 0.606 | 16.39 | 0.699 | 7.40 | 0.62 | 18.10 | 0.38 | 6.80 | 0.19 |
| 6.33 | 0.688 | 9.12 | 0.638 | 16.75 | 0.709 | 7.50 | 0.52 | 18.40 | 0.50 | 6.90 | 0.06 |
| 6.36 | 0.764 | 9.17 | 0.749 | 17.27 | 0.669 | 7.70 | 0.72 | 18.60 | 0.68 | 7.00 | 0.19 |
| 6.40 | 0.816 | 9.29 | 0.658 | 17.57 | 0.606 | 7.80 | 0.69 | 19.50 | 0.88 | 7.10 | 0.09 |
| 6.45 | 0.843 | 9.35 | 0.782 | 17.73 | 0.494 | 7.90 | 0.34 | 19.80 | 0.91 | 7.40 | 0.07 |
| 6.50 | 0.819 | 9.39 | 0.777 | 18.35 | 0.484 | 8.20 | 0.23 | 20.10 | 0.99 | 7.50 | 0.17 |
| 6.53 | 0.751 | 9.43 | 0.818 | 18.45 | 0.527 | 8.40 | 0.22 | 21.10 | 1.00 | 7.80 | 0.03 |
| 6.57 | 0.302 | 9.63 | 0.840 | 18.73 | 0.600 | 8.60 | 0.21 | 21.60 | 1.00 | 8.20 | 0.05 |
| 6.61 | 0.895 | 9.70 | 0.832 | 19.31 | 0.700 | 8.90 | 0.53 | 22.10 | 0.97 | 8.50 | 0.08 |
| 6.67 | 0.196 | 9.86 | 0.452 | 19.88 | 0.631 | 9.10 | 0.59 | 23.50 | 0.94 | 8.90 | 0.05 |
| 6.74 | 0.563 | 9.97 | 0.760 | 20.24 | 0.686 | 9.20 | 0.49 | 25.00 | 0.83 | 9.10 | 0.05 |
| 6.82 | 0.515 | 10.07 | 0.833 | 20.66 | 0.703 | 9.40 | 0.58 | 26.90 | 0.79 | 9.30 | 0.06 |
| 6.90 | 0.471 | 10.17 | 0.833 | 20.92 | 0.740 | 9.60 | 0.87 | 28.90 | 0.77 | 9.60 | 0.38 |
| 6.92 | 0.430 | 10.26 | 0.867 | 21.83 | 0.755 | 9.80 | 0.79 | 33.80 | 1.00 | 9.90 | 0.19 |
| 6.95 | 0.415 | 10.42 | 0.823 | 24.04 | 0.720 | 10.00 | 0.78 | 35.00 | 1.00 | 10.10 | 0.11 |
| 7.00 | 0.431 | 10.60 | 0.851 | 25.00 | 0.755 | 10.20 | 0.45 | 37.10 | 1.00 | 10.40 | 0.51 |
| 7.07 | 0.680 | 10.73 | 0.851 | | | 10.50 | 0.96 | 39.60 | 0.99 | 10.50 | 0.46 |
| 7.11 | 0.672 | 10.87 | 0.858 | CURVE 12 | | 10.60 | 0.93 | 42.20 | 0.97 | 10.60 | 0.50 |
| 7.14 | 0.714 | 11.07 | 0.791 | T = 300. | | 10.70 | 0.92 | 46.00 | 1.00 | 10.80 | 0.43 |
| 7.20 | 0.656 | 11.29 | 0.653 | | | 10.80 | 0.85 | 48.00 | 1.00 | 10.90 | 0.48 |
| 7.22 | 0.563 | 11.44 | 0.776 | | | 11.20 | 0.66 | 50.00 | 1.00 | 11.10 | 0.42 |
| 7.34 | 0.463 | 11.55 | 0.789 | 2.70 | 0.00 | 11.40 | 0.51 | | | 11.30 | 0.11 |
| 7.38 | 0.531 | 11.70 | 0.759 | 3.60 | 0.55 | 11.60 | 0.76 | CURVE 13 | | 11.50 | 0.30 |
| 7.53 | 0.561 | 11.90 | 0.316 | 4.10 | 0.94 | 11.80 | 0.74 | T = 300. | | 11.80 | 0.12 |
| 7.59 | 0.627 | 12.02 | 0.208 | 4.40 | 0.80 | 12.00 | 0.34 | | | 12.00 | 0.17 |
| 7.59 | 0.441 | 12.27 | 0.367 | 4.60 | 0.95 | 12.20 | 0.29 | 3.60 | 0.55 | 12.30 | 0.12 |

TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | CURVE 13 (CONT.) | | CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 15 | | |
|-----------|------------------|----------------------|------------------|--------|------------------|--------|------------------|--------|-----------|--------|-------|
| | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | |
| 12.50 | 6.28 | | 4.72 | 0.943 | 6.81 | 0.814 | 9.19 | 0.800 | 12.13 | 0.743 | |
| 12.70 | 0.30 | 47.90 | 4.79 | 0.937 | 6.86 | 0.881 | 9.22 | 0.694 | 12.27 | 0.758 | |
| 12.80 | 0.13 | 50.00 | 4.86 | 0.943 | 6.93 | 0.906 | 9.26 | 0.569 | 12.37 | 0.856 | |
| 13.10 | 0.11 | CURVE 14 T = 293. | | 4.97 | 0.940 | 7.00 | 0.914 | 9.28 | 0.686 | 12.45 | 0.911 |
| 13.50 | 0.35 | | 5.17 | 0.940 | 7.04 | 0.865 | 9.33 | 0.796 | 12.47 | 0.943 | |
| 13.80 | 0.34 | | 5.22 | 0.933 | 7.11 | 0.794 | 9.33 | 0.902 | 12.57 | 0.955 | |
| 14.10 | 0.25 | 2.00 | 5.24 | 0.910 | 7.11 | 0.856 | 9.38 | 0.924 | 12.73 | 0.929 | |
| 14.50 | 0.51 | 2.12 | 5.34 | 0.910 | 7.25 | 0.900 | 9.46 | 0.937 | 12.89 | 0.892 | |
| 14.80 | 0.71 | 2.27 | 5.51 | 0.900 | 7.30 | 0.867 | 9.56 | 0.937 | 12.95 | 0.825 | |
| 15.40 | 0.84 | 2.31 | 5.52 | 0.865 | 7.34 | 0.812 | 9.70 | 0.926 | 13.06 | 0.841 | |
| 15.70 | 0.79 | 2.49 | 5.53 | 0.854 | 7.36 | 0.908 | 9.74 | 0.891 | 13.19 | 0.889 | |
| 15.90 | 0.56 | 2.54 | 5.53 | 0.765 | 7.44 | 0.926 | 9.77 | 0.792 | 13.31 | 0.925 | |
| 16.20 | 0.78 | 2.58 | 5.57 | 0.660 | 7.55 | 0.893 | 9.80 | 0.695 | 13.51 | 0.951 | |
| 16.40 | 0.70 | 2.62 | 5.59 | 0.493 | 7.59 | 0.807 | 9.82 | 0.598 | 13.63 | 0.941 | |
| 16.90 | 0.41 | 2.72 | 5.59 | 0.829 | 7.69 | 0.792 | 9.83 | 0.409 | 13.76 | 0.950 | |
| 17.30 | 0.22 | 2.84 | 5.63 | 0.272 | 7.73 | 0.671 | 9.89 | 0.586 | 13.99 | 0.943 | |
| 17.60 | 0.11 | 2.97 | 5.63 | 0.493 | 7.82 | 0.683 | 9.95 | 0.688 | 14.12 | 0.919 | |
| 18.00 | 0.08 | 3.12 | 5.67 | 0.598 | 7.88 | 0.488 | 10.00 | 0.885 | 14.26 | 0.936 | |
| 18.40 | 0.12 | 3.18 | 5.71 | 0.748 | 7.94 | 0.298 | 10.05 | 0.935 | 14.39 | 0.947 | |
| 19.10 | 0.50 | 3.30 | 5.75 | 0.841 | 7.97 | 0.196 | 10.10 | 0.956 | 14.61 | 0.941 | |
| 20.50 | 0.53 | 3.33 | 5.79 | 0.865 | 8.02 | 0.170 | 10.20 | 0.953 | 14.74 | 0.915 | |
| 21.00 | 0.66 | 3.33 | 5.81 | 0.889 | 8.07 | 0.138 | 10.33 | 0.964 | 15.00 | 0.912 | |
| 21.70 | 0.74 | 3.35 | 5.86 | 0.907 | 8.14 | 0.165 | 10.48 | 0.959 | CURVE 15 | | |
| 22.10 | 0.81 | 3.35 | 5.93 | 0.915 | 8.18 | 0.216 | 10.58 | 0.966 | T = 293. | | |
| 22.60 | 0.80 | 3.39 | 6.07 | 0.915 | 8.25 | 0.325 | 10.67 | 0.977 | 2.50 | 0.071 | |
| 23.00 | 0.57 | 3.41 | 6.07 | 0.909 | 8.30 | 0.220 | 10.77 | 0.967 | 2.57 | 0.119 | |
| 23.60 | 0.54 | 3.45 | 6.16 | 0.919 | 8.36 | 0.138 | 11.00 | 0.977 | 2.63 | 0.200 | |
| 24.10 | 0.51 | 3.45 | 6.21 | 0.889 | 8.40 | 0.289 | 11.10 | 0.958 | 2.66 | 0.129 | |
| 24.50 | 0.36 | 3.52 | 6.26 | 0.849 | 8.49 | 0.457 | 11.16 | 0.896 | 2.69 | 0.094 | |
| 25.10 | 0.31 | 3.56 | 6.30 | 0.896 | 8.52 | 0.329 | 11.22 | 0.816 | 2.78 | 0.000 | |
| 26.30 | 0.51 | 3.82 | 6.36 | 0.902 | 8.57 | 0.203 | 11.36 | 0.883 | 2.87 | 0.028 | |
| 29.30 | 0.60 | 4.03 | 6.35 | 0.918 | 8.61 | 0.393 | 11.41 | 0.924 | 2.90 | 0.066 | |
| 30.60 | 0.68 | 4.10 | 6.45 | 0.918 | 8.69 | 0.592 | 11.48 | 0.958 | 2.93 | 0.150 | |
| 31.90 | 0.73 | 4.16 | 6.55 | 0.756 | 8.75 | 0.790 | 11.60 | 0.939 | 2.99 | 0.150 | |
| 33.00 | 0.81 | 4.21 | 6.60 | 0.595 | 8.79 | 0.817 | 11.70 | 0.890 | 3.05 | 0.113 | |
| 35.00 | 0.92 | 4.36 | 6.61 | 0.423 | 8.87 | 0.840 | 11.76 | 0.798 | 3.08 | | |
| 37.10 | 0.82 | 4.40 | 6.64 | 0.423 | 8.97 | 0.816 | 11.84 | 0.735 | | | |
| 39.50 | 0.76 | 4.50 | 6.64 | 0.552 | 9.05 | 0.775 | 11.89 | 0.694 | | | |
| 41.60 | 0.91 | 4.57 | 6.68 | 0.697 | 9.12 | 0.815 | 12.00 | 0.628 | | | |
| 45.80 | 0.75 | 4.63 | 6.74 | 0.814 | 9.14 | 0.830 | 12.07 | 0.689 | | | |

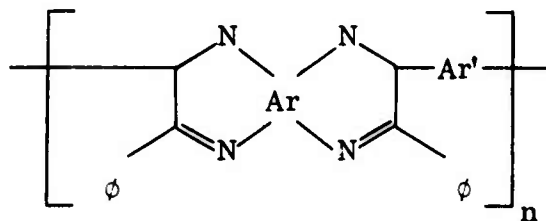
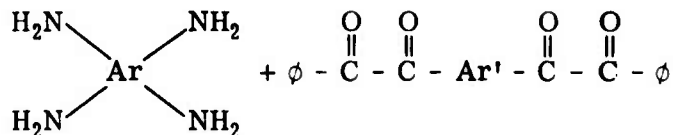
TABLE 17-13. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF POLYCARBONATE PLASTICS (WAVELENGTH DEPENDENCE) (CONTINUED)
[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

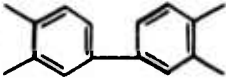

| λ | T |
|------------------|-------|
| CURVE 15 (CONT.) | |
| 3.11 | 0.075 |
| 3.14 | 0.041 |
| 3.19 | 0.000 |
| 3.81 | 0.000 |
| 3.87 | 0.033 |
| 3.90 | 0.068 |
| 3.92 | 0.046 |
| 3.97 | 0.069 |
| 3.97 | 0.041 |
| 4.07 | 0.041 |
| 4.11 | 0.023 |
| 4.19 | 0.000 |

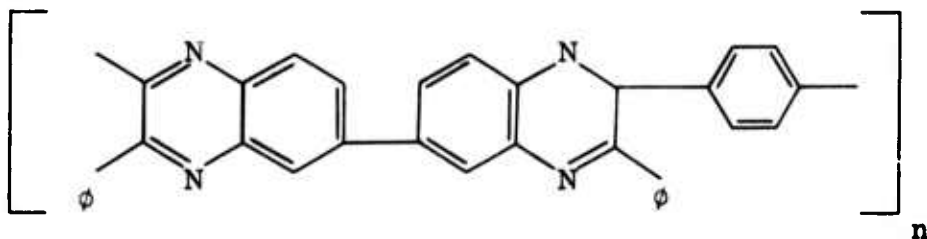
| | |
|----------|-------|
| CURVE 16 | |
| T = 293. | |
| 2.48 | 0.000 |
| 2.48 | 0.060 |
| 2.54 | 0.034 |
| 2.61 | 0.083 |
| 2.63 | 0.030 |
| 2.69 | 0.014 |
| 2.70 | 0.000 |
| 2.84 | 0.000 |
| 2.87 | 0.027 |
| 2.92 | 0.057 |
| 2.98 | 0.057 |
| 2.98 | 0.041 |
| 3.04 | 0.041 |
| 3.59 | 0.026 |
| 3.17 | 0.000 |
| 3.62 | 0.000 |
| 3.84 | 0.024 |
| 3.88 | 0.017 |
| 3.94 | 0.000 |
| 4.03 | 0.016 |
| 4.09 | 0.000 |

4.18. Poly(phenylquinoxaline), PPQ

The preparation of soluble high molecular weight poly(phenylquinoxalines), PPQ, by the condensation of aromatic bis(o-diamines) with aromatic bisbenzils was first reported in 1967.

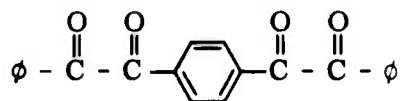


where $\phi = \text{C}_6\text{H}_5$ and Ar, Ar' = aromatic typically, for PPQI Ar =  and Ar' = , hence PPQI is described by the formula:



UV data for homo- and copolymers exhibit a λ_{max} in the case of PPQI at 292 μm . Apparently the p-phenylene moiety and the phenyl group are forced out of the plane due to steric interaction, and therefore, are unable to participate significantly in resonance, for λ_{max} to appear at shorter wavelength.

The current interest in PPQ's is due to the high thermal stability and unusual ease of formation of these polymers. Formation is a one stage quantitative process at room temperature which yields completely cyclized, soluble polymers. Reaction of 1,4-di(phenylglyoxal) benzene



in excess in air yields a crosslinked polymer compared with the usual linear polymer when the reagents are used in stoichiometric amounts.

PPQ's are faintly yellow fibrous amorphous substances readily soluble in most organic solvents. Typical molecular weights are of the order of 330,000. PPQ polymers were shown to exhibit good solubility and processability as well as excellent thermal oxidative stability. However, IR spectra of PPQ demonstrates the ease of oxidation of the methylene bridges in those polymers containing this structural feature. It starts decomposition at 780 to 830 K.

The potential of PPQ for use as functional and structural resin in high temperature environment has been demonstrated.

PPQ specimens may be cured at 644 K and 1000 psi for four hours. The thermal linear expansion of the cured material increases gradually to the instability temperature of 578 K with the expansion at this point being 1.3% [T77908]. Above the instability temperature, PPQ first contracts, then expands slightly, then finally contracts severely above 756 K where degradation occurs.

The thermal conductivity of PPQ exhibits increasing values from $0.00293 \text{ W cm}^{-1} \text{ K}^{-1}$ at 340 K to $0.00317 \text{ W cm}^{-1} \text{ K}^{-1}$ at 533 K. Typical densities fall in the range $1.196 - 1.205 \text{ g cm}^{-3}$.

PPQ carbon fiber composites have been studied as potential re-entry vehicle (REV) materials.

No information on the thermal radiative properties of this material was uncovered from the search of literature. Consequently, no tabulation or recommendation of the thermal radiative properties of this material is possible at this time.

4.19. Silicone Resin

These organo-silicon oxide polymers may be resins, rubbers, or liquids. They are characterized by resistance to heat, oxidation, and weathering; water repellency; near independence of physical properties with temperature; and resistance to electrical breakdown. Their thermal degradation temperature is about 473 to 873 K.

Industrial uses include silicone release agents, lubricants, adhesives, laminating resins, electrical insulation, molding compounds, and additives. Trade names include Silastic, Polysil, Versilube, Dow Corning Silicone, etc.

In the United States, major companies producing silicones for industrial use include Dow Corning Corporation, General Electric Company, and Union Carbide Corporation.

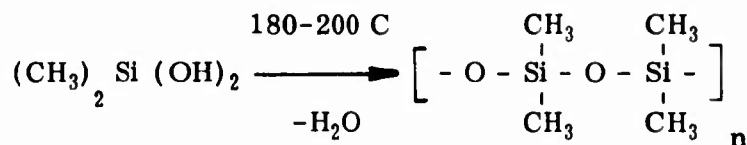
For the purpose of aircraft design, the application of silicone resins may be classified in the following three ways:

- (1) **Silicone laminating resins** - These are used primarily in bonding glass cloth to produce structural and electrical laminates. They are also used to bond asbestos paper and cloth. Silicone-glass laminates have excellent resistance to heat and heat aging.
- (2) **Interlayer for laminates glass** - Silastic Type K Interlayer serves as the center layer in safety glass windshield for supersonic aircraft.
- (3) **Silicone molding compounds** - These are thermosetting materials that can be formed by either compression or transfer molding techniques. For high-impact, glass fiber-filled silicone molding compounds, the heat distortion temperature is about 755 K. Parts molded from silicone molding compounds find use as both structural and dielectric materials in aircraft and missiles.

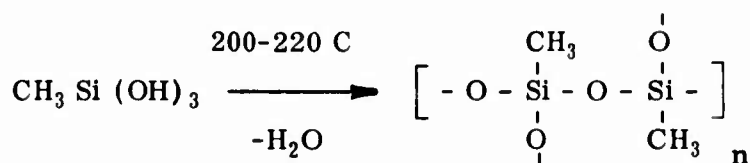
Several silicone resins have been considered for application in aerospace construction. Poly(dimethylsilanediol) with a melting point of 740 K has been considered for use as a matrix material for flexible windows and domes in manned spacecraft, although it has been suggested that it has insufficient tear resistance for this purpose. Polyphenyl silicone has been considered for use as a paint-like organic coating for spacecraft, designed to control emission and absorption of radiant energy. Silicone DC 808 has been considered for similar uses. Silicone XRG-2044 has been considered for use as a coating for solar cells. Owens-Illinois "Glass Resin 100" has been studied for possible use as a lightweight optical material for aerospace reconnaissance. Some elastomers

are used for oxygen hoses, space suits, and cabin seals. Silicone resins are also used as ablation shields for space ships.

Silicones consist of chains of alternate Si and O atoms. The chains are modified by various organic groups attached to Si, or by crosslinking. Silicone polymers are prepared by condensation of di- or trihydroxymethylsilanes.



Silicone rubber



Silicone resin

Uncured silicone resins are soluble in some organic liquids such as toluene, xylene, petroleum spirit, and n-butyl acetate. Cured silicone resins can be swollen by toluene and some other hydrocarbons, carbon tetrachloride, methyl chloride, acetone, methyl ethyl ketone, liquid ammonia, liquid sulphur dioxide, and glacial acetic acid. They may be decomposed by the attack of concentrated hydrochloric and sulphuric acids.

Silicone resins have density about 1.0-1.2 g cm⁻³. Its refractive index is about 1.405-1.49, specific heat 0.36-0.37, thermal conductivity 0.00146 W cm⁻¹ K⁻¹. Silicone resins that are flexible at room temperature have a brittleness temperature of 200 K or lower. The resins soften at temperatures from 300 K to above 470 K according to the degree of cure (cross-linkage). Prolonged heating causes gradual loss of weight by breakdown of volatile products, e. g., benzene and cyclic siloxanes from methylsiloxanes at 400-500 K. Its electrical resistivity at room temperature is about 3.10¹³ - 5.10¹⁵ Ω cm and dielectric constant is 2.75-2.85 from 60-10⁶ HZ. Its dielectric strength is about 20-120 kV/mm at room temperature, 50% lower at 370 K, and 20-30% lower for wet film. The arc resistance of silicone resins is greater than that of the organic resins.

a. Normal Spectral Emittance (Wavelength Dependence)

There are six sets of experimental data available for the wavelength dependence of the normal spectral emittance of silicone resins as listed in Table 19-3 and shown in Fig. 19-2. Specimen characterization and measurement information for the data are

given in Table 19-2. Two data sets each are for "Pyrosin" heat resistant paint on aluminum plate at 473 and 673 K with brown, green, and beige color, respectively. In the wavelength region above $\lambda = 8 \mu\text{m}$, there are very small differences among the values of emittance for different paint. However, in the shorter wavelength region, i. e., $\lambda < 8 \mu\text{m}$, brown paint has the highest emittance value and beige paint has the lowest emittance value. Since the data are limited, as a consequence, only provisional values were reported here. The provisional values are listed in Table 19-1 and shown in Figure 19-1 for the green "Pyrosin" paint on aluminum plate at 473 K. The estimated uncertainty is within $\pm 30\%$.

TABLE 19-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ |
|-----------|------------|
| PYROSIN | |
| GREEN | |
| T = 473 | |
| 2.70 | 0.67 |
| 2.90 | 0.74 |
| 3.00 | 0.81 |
| 3.20 | 0.84 |
| 3.40 | 0.82 |
| 3.80 | 0.74 |
| 4.00 | 0.73 |
| 4.60 | 0.76 |
| 5.00 | 0.86 |
| 5.20 | 0.90 |
| 5.80 | 0.91 |
| 6.00 | 0.82 |
| 6.50 | 0.93 |
| 7.00 | 0.93 |
| 7.50 | 0.94 |
| 8.80 | 0.84 |
| 8.50 | 0.85 |
| 9.00 | 0.86 |
| 9.60 | 0.94 |
| 10.00 | 0.94 |
| 10.20 | 0.94 |
| 10.50 | 0.94 |
| 11.00 | 0.96 |
| 11.80 | 0.96 |
| 12.00 | 0.96 |
| 12.50 | 0.97 |
| 13.00 | 0.97 |
| 13.50 | 0.97 |
| 14.00 | 0.98 |
| 14.50 | 0.98 |
| 15.00 | 0.98 |

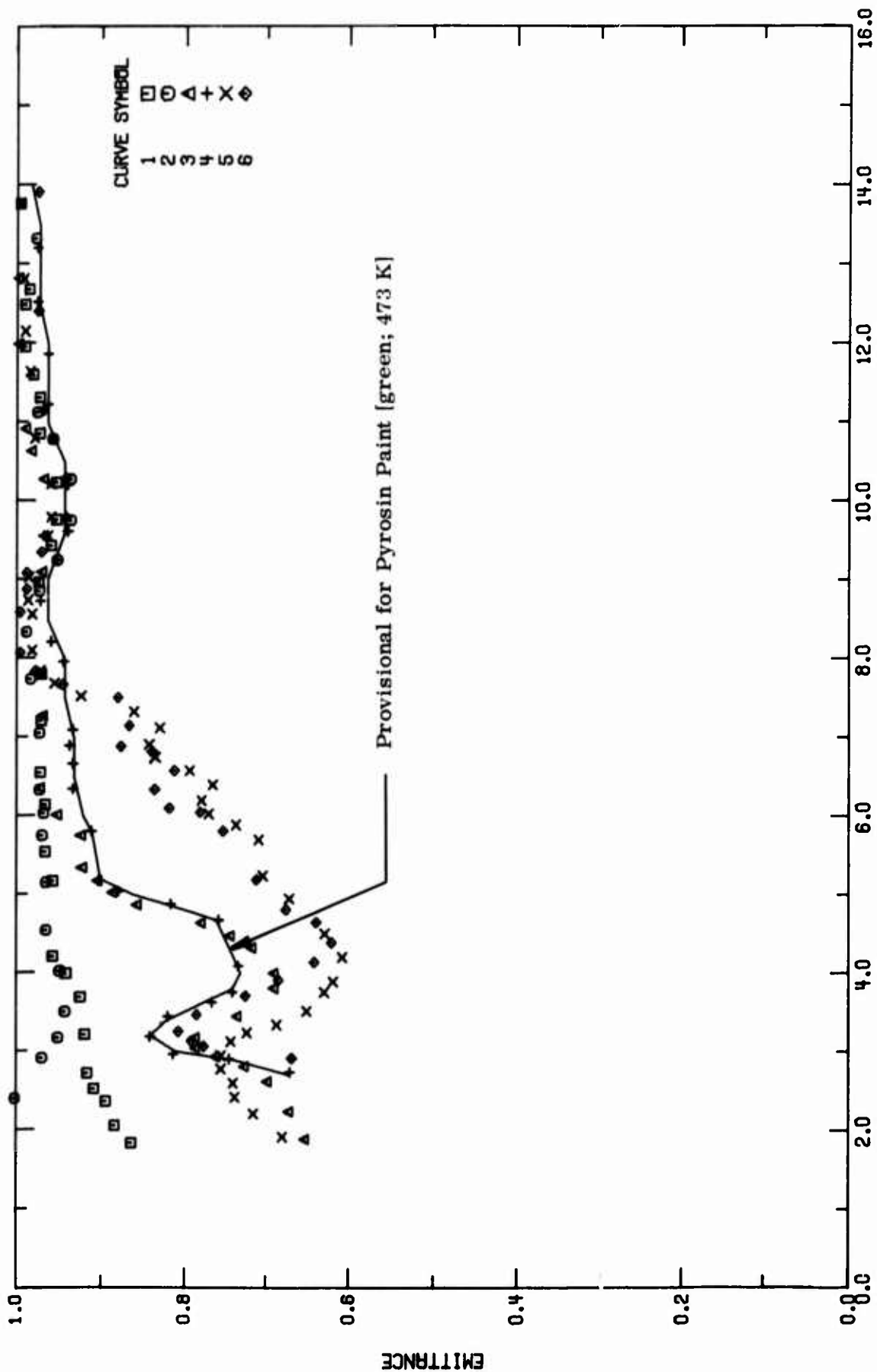


FIGURE 19-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN COATING (WAVELENGTH DEPENDENCE).

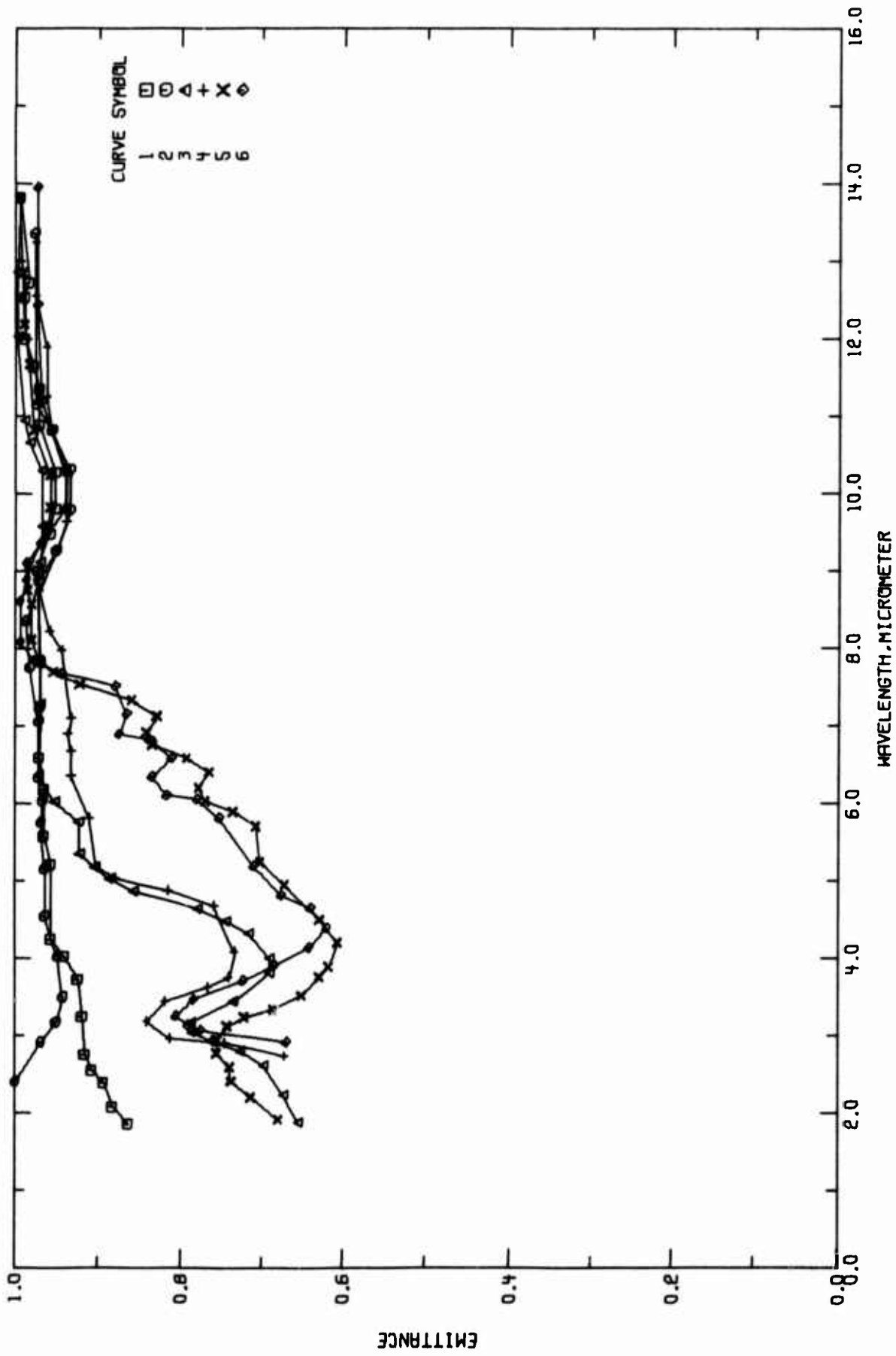


FIGURE 19-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE).

TABLE 19-2. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF SILICONE RESIN COATING (Wavelength Dependence).

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 T71893 | Kamayama, K. | 1972 | 1-25 | 673 | "Pyrosin" | Heat resisting paint with brown color was coated on aluminum plate; data were extracted from figure; $\theta \sim 0^\circ$. |
| 2 T71903 | Kamayama, K. | 1972 | 1-25 | 473 | "Pyrosin" | Similar to the above specimen. |
| 3 T71893 | Kamayama, K. | 1972 | 1-25 | 673 | "Pyrosin" | Similar to the above specimen except paint with green color. |
| 4 T71893 | Kamayama, K. | 1972 | 1-25 | 473 | "Pyrosin" | Similar to the above specimen. |
| 5 T71893 | Kamayama, K. | 1972 | 1-25 | 673 | "Pyrosin" | Similar to the above specimen except paint with beige color. |
| 6 T71893 | Kamayama, K. | 1972 | 1-25 | 473 | "Pyrosin" | Similar to the above specimen. |

TABLE 19-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| CURVE 1 T = 673. | | CURVE 2 T = 473. | | CURVE 3 (CONT.) | | CURVE 4 T = 473. | | CURVE 4 (CONT.) | | CURVE 5 (CONT.) | |
|---------------------|------------|---------------------|------------|-----------------|------------|---------------------|------------|-----------------|------------|-----------------|------------|
| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
| 1.83 | 0.862 | 2.40 | 1.000 | 2.80 | 0.726 | 2.73 | 0.670 | 22.79 | 0.962 | 8.56 | 0.979 |
| 2.05 | 0.882 | 2.91 | 0.967 | 2.93 | 0.761 | 2.90 | 0.744 | 23.27 | 0.973 | 8.74 | 0.984 |
| 2.36 | 0.893 | 3.17 | 0.948 | 3.04 | 0.786 | 2.96 | 0.813 | 23.67 | 0.988 | 9.037 | 0.983 |
| 2.52 | 0.907 | 3.50 | 0.940 | 3.17 | 0.786 | 3.18 | 0.840 | 24.39 | 0.988 | 9.56 | 0.960 |
| 2.72 | 0.915 | 4.02 | 0.946 | 3.44 | 0.735 | 3.44 | 0.819 | 24.74 | 0.982 | 9.80 | 0.956 |
| 3.21 | 0.918 | 4.54 | 0.962 | 3.80 | 0.690 | 3.62 | 0.765 | 25.00 | 0.987 | 10.22 | 0.956 |
| 3.69 | 0.923 | 5.15 | 0.962 | 3.99 | 0.690 | 3.75 | 0.740 | CURVE 5 | | | 0.976 |
| 3.99 | 0.939 | 5.75 | 0.967 | 4.31 | 0.717 | 4.08 | 0.733 | T = 673. | | | 0.982 |
| 4.21 | 0.954 | 6.03 | 0.965 | 4.47 | 0.744 | 4.67 | 0.757 | 1.91 | 0.679 | 12.82 | 0.990 |
| 4.54 | 0.954 | 6.33 | 0.970 | 4.63 | 0.779 | 4.87 | 0.757 | 2.20 | 0.714 | 13.78 | 0.994 |
| 5.17 | 0.954 | 7.05 | 0.970 | 4.86 | 0.856 | 5.03 | 0.816 | 2.41 | 0.737 | 15.40 | 0.994 |
| 5.54 | 0.963 | 7.74 | 0.981 | 5.02 | 0.866 | 5.17 | 0.878 | 2.59 | 0.739 | 18.01 | 0.989 |
| 6.14 | 0.963 | 8.34 | 0.986 | 5.17 | 0.904 | 5.80 | 0.910 | 2.77 | 0.754 | 18.42 | 0.993 |
| 6.55 | 0.969 | 8.86 | 0.986 | 5.34 | 0.922 | 6.34 | 0.931 | 2.94 | 0.754 | 19.09 | 0.990 |
| 7.21 | 0.968 | 9.25 | 0.949 | 5.75 | 0.923 | 6.66 | 0.931 | 3.12 | 0.742 | 19.99 | 0.990 |
| 7.80 | 0.968 | 9.75 | 0.934 | 6.01 | 0.950 | 6.89 | 0.935 | 3.23 | 0.722 | 20.71 | 0.975 |
| 8.97 | 0.971 | 10.26 | 0.934 | 6.35 | 0.970 | 7.09 | 0.931 | 3.33 | 0.686 | 22.32 | 0.975 |
| 9.44 | 0.956 | 10.79 | 0.954 | 7.27 | 0.967 | 7.96 | 0.942 | 3.51 | 0.650 | 22.86 | 0.969 |
| 9.77 | 0.950 | 11.13 | 0.973 | 7.80 | 0.968 | 8.21 | 0.956 | 3.75 | 0.629 | 23.44 | 0.965 |
| 10.24 | 0.950 | 13.33 | 0.975 | 8.97 | 0.971 | 9.25 | 0.949 | 3.88 | 0.618 | 24.48 | 0.962 |
| 10.36 | 0.970 | 14.39 | 0.981 | 9.10 | 0.968 | 9.62 | 0.937 | 4.19 | 0.607 | 25.15 | 0.962 |
| 11.32 | 0.970 | 15.00 | 0.981 | 9.56 | 0.966 | 10.21 | 0.937 | 4.49 | 0.628 | CURVE 6 | |
| 11.61 | 0.978 | 15.72 | 0.977 | 10.28 | 0.966 | 10.79 | 0.954 | 4.94 | 0.671 | T = 473. | |
| 11.97 | 0.988 | 16.27 | 0.982 | 10.64 | 0.981 | 11.23 | 0.960 | 5.23 | 0.703 | 2.91 | 0.668 |
| 12.50 | 0.988 | 17.32 | 0.964 | 10.92 | 0.988 | 11.87 | 0.960 | 5.69 | 0.700 | 3.06 | 0.775 |
| 12.69 | 0.983 | 18.25 | 0.964 | 12.00 | 0.997 | 12.53 | 0.973 | 6.08 | 0.736 | 3.13 | 0.791 |
| 13.78 | 0.994 | 19.47 | 0.978 | 12.83 | 0.997 | 13.21 | 0.973 | 6.19 | 0.770 | 3.25 | 0.807 |
| 15.40 | 0.994 | 23.25 | 0.969 | 13.78 | 0.994 | 14.11 | 0.981 | 6.39 | 0.764 | 3.46 | 0.784 |
| 16.39 | 0.989 | 25.00 | 0.969 | 15.40 | 0.994 | 14.96 | 0.984 | 6.57 | 0.793 | 3.70 | 0.724 |
| 19.09 | 0.975 | 21.91 | 0.969 | 18.39 | 0.989 | 15.29 | 0.977 | 6.74 | 0.834 | 3.90 | 0.684 |
| 19.91 | 0.975 | 22.29 | 0.974 | 19.09 | 0.975 | 15.99 | 0.977 | 6.90 | 0.841 | 4.13 | 0.641 |
| 20.52 | 0.965 | 22.99 | 0.987 | 20.32 | 0.975 | 17.08 | 0.970 | 7.11 | 0.829 | 4.38 | 0.620 |
| 21.35 | 0.960 | 25.00 | 0.987 | 21.18 | 0.959 | 18.16 | 0.977 | 7.32 | 0.859 | 4.54 | 0.639 |
| 21.94 | 0.946 | CURVE 3 | | 21.90 | 0.969 | 18.70 | 0.968 | 7.52 | 0.922 | 4.80 | 0.675 |
| 23.33 | 0.948 | T = 673. | | 22.41 | 0.961 | 19.22 | 0.968 | 7.68 | 0.952 | 5.18 | 0.711 |
| 23.87 | 0.958 | 1.88 | 0.653 | 22.69 | 0.967 | 19.79 | 0.967 | 7.84 | 0.969 | 5.80 | 0.752 |
| 24.45 | 0.977 | 2.23 | 0.672 | 23.24 | 0.967 | 24.48 | 0.961 | 8.10 | 0.979 | | |
| 25.15 | 0.984 | 2.61 | 0.698 | 23.81 | 0.979 | 25.11 | 0.989 | | | | |
| | | | | 24.48 | 0.981 | | | | | | |
| | | | | 25.11 | 0.989 | | | | | | |

TABLE 19-3. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ |
|-----------|------------|
| CURVE | 6 (CONT.) |
| 6.04 | 0.720 |
| 6.09 | 0.810 |
| 6.33 | 0.835 |
| 6.57 | 0.812 |
| 6.81 | 0.838 |
| 6.88 | 0.875 |
| 7.14 | 0.865 |
| 7.50 | 0.679 |
| 7.66 | 0.943 |
| 7.83 | 0.976 |
| 8.07 | 0.994 |
| 8.59 | 0.994 |
| 8.88 | 0.985 |
| 9.09 | 0.986 |
| 9.35 | 0.928 |
| 9.79 | 0.939 |
| 10.29 | 0.939 |
| 10.79 | 0.954 |
| 11.15 | 0.966 |
| 12.41 | 0.972 |
| 13.92 | 0.972 |
| 14.60 | 0.959 |
| 15.22 | 0.949 |
| 15.86 | 0.949 |
| 17.09 | 0.954 |
| 18.09 | 0.959 |
| 18.67 | 0.957 |
| 19.79 | 0.951 |
| 21.82 | 0.959 |
| 23.19 | 0.959 |
| 23.60 | 0.967 |
| 23.98 | 0.978 |
| 24.91 | 0.978 |

b. Normal Spectral Reflectance (Wavelength Dependence)

There are 21 sets of experimental data available for the wavelength dependence of the normal spectral reflectance of silicone resin coating as listed in Table 19-6 and shown in Figure 19-4. Specimen characterization and measurement information for the data are given in Table 19-5. There were 10 different kinds of silicone used for measurements. The normal spectral reflectance values for silicone black paint (Pyrolac 7G 800) were the lowest. RTV-602 silicone on aluminum substrate has the highest reflectance values. Only Wilburn and Renius [T47062] and Wetmore [T40420] measured the normal spectral reflectance in the wavelength region above 2.6 μm . Because the range of reflectance for silicone is so wide, only provisional values are reported here which are listed in Table 19-4 and shown in Figure 19-3. The provisional values are for a 0.43 mm thick Dow Corning 6510 silicone on aluminum substrate at 400 K. The estimated uncertainty is within $\pm 30\%$.

TABLE 19-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------|--------|
| DC 5510 | |
| T = 403 | |
| 1.75 | 0.52 |
| 2.00 | 0.50 |
| 2.10 | 0.59 |
| 2.15 | 0.21 |
| 2.22 | 0.17 |
| 2.40 | 0.18 |
| 2.50 | 0.21 |
| 2.56 | 0.21 |
| 2.72 | 0.07 |
| 2.80 | 0.22 |
| 3.00 | 0.24 |
| 3.10 | 0.04 |
| 3.30 | 0.03 |
| 3.50 | 0.04 |
| 3.60 | 0.29 |
| 3.84 | 0.42 |
| 4.00 | 0.29 |
| 4.25 | 0.47 |
| 4.45 | 0.44 |
| 4.50 | 0.18 |
| 4.80 | 0.07 |
| 5.00 | 0.05 |
| 5.30 | 0.05 |
| 7.00 | 0.09 |
| 7.50 | 0.10 |
| 8.00 | 0.13 |
| 8.50 | 0.16 |
| 9.00 | 0.19 |
| 9.30 | 0.23 |
| 10.00 | 0.22 |
| 10.50 | 0.21 |
| 11.00 | 0.21 |
| 11.50 | 0.21 |
| 12.00 | 0.21 |
| 12.50 | 0.22 |
| 13.00 | 0.22 |
| 13.50 | 0.23 |
| 14.00 | 0.23 |

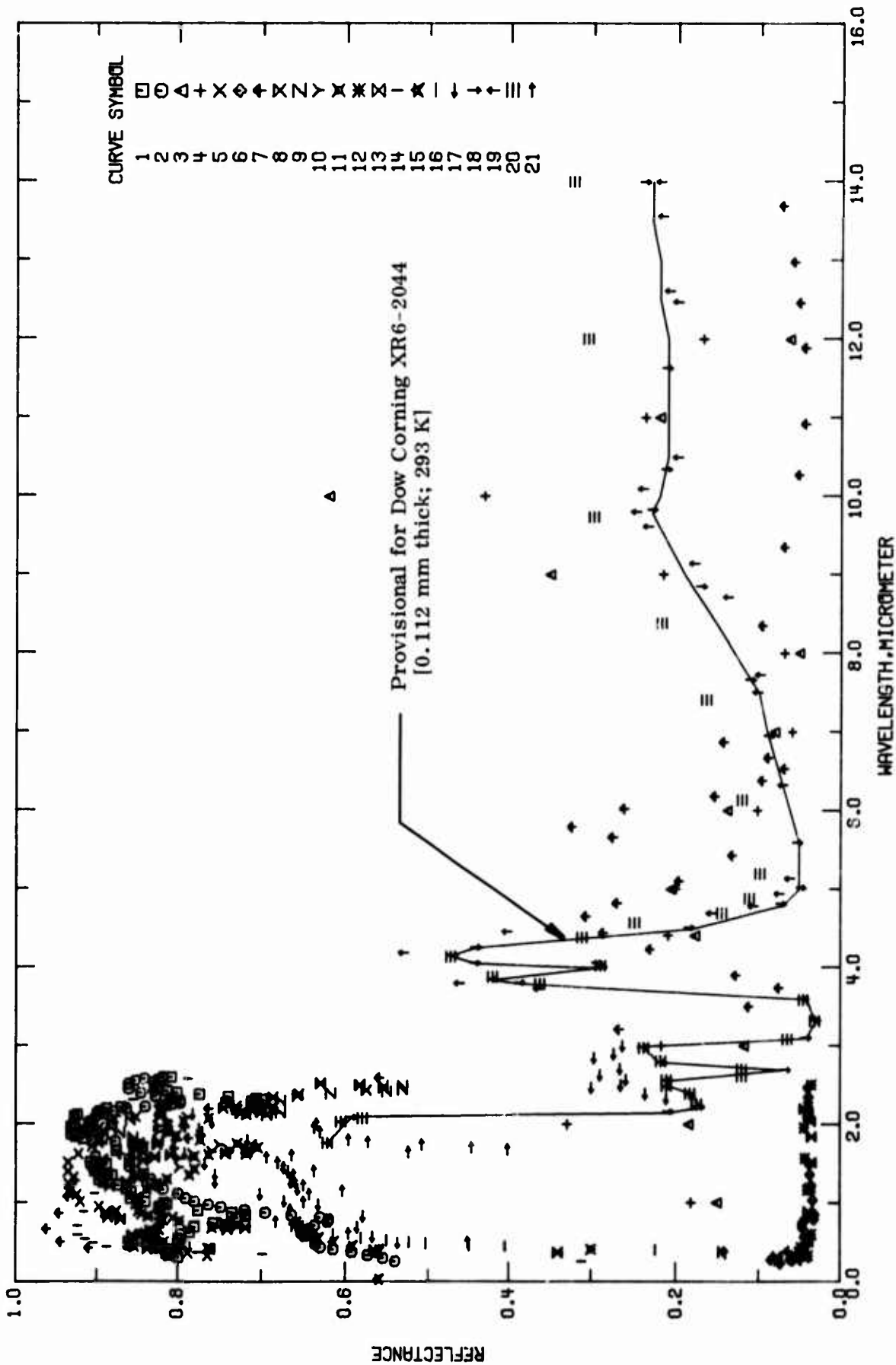


FIGURE 19-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (WAVELENGTH DEPENDENCE).

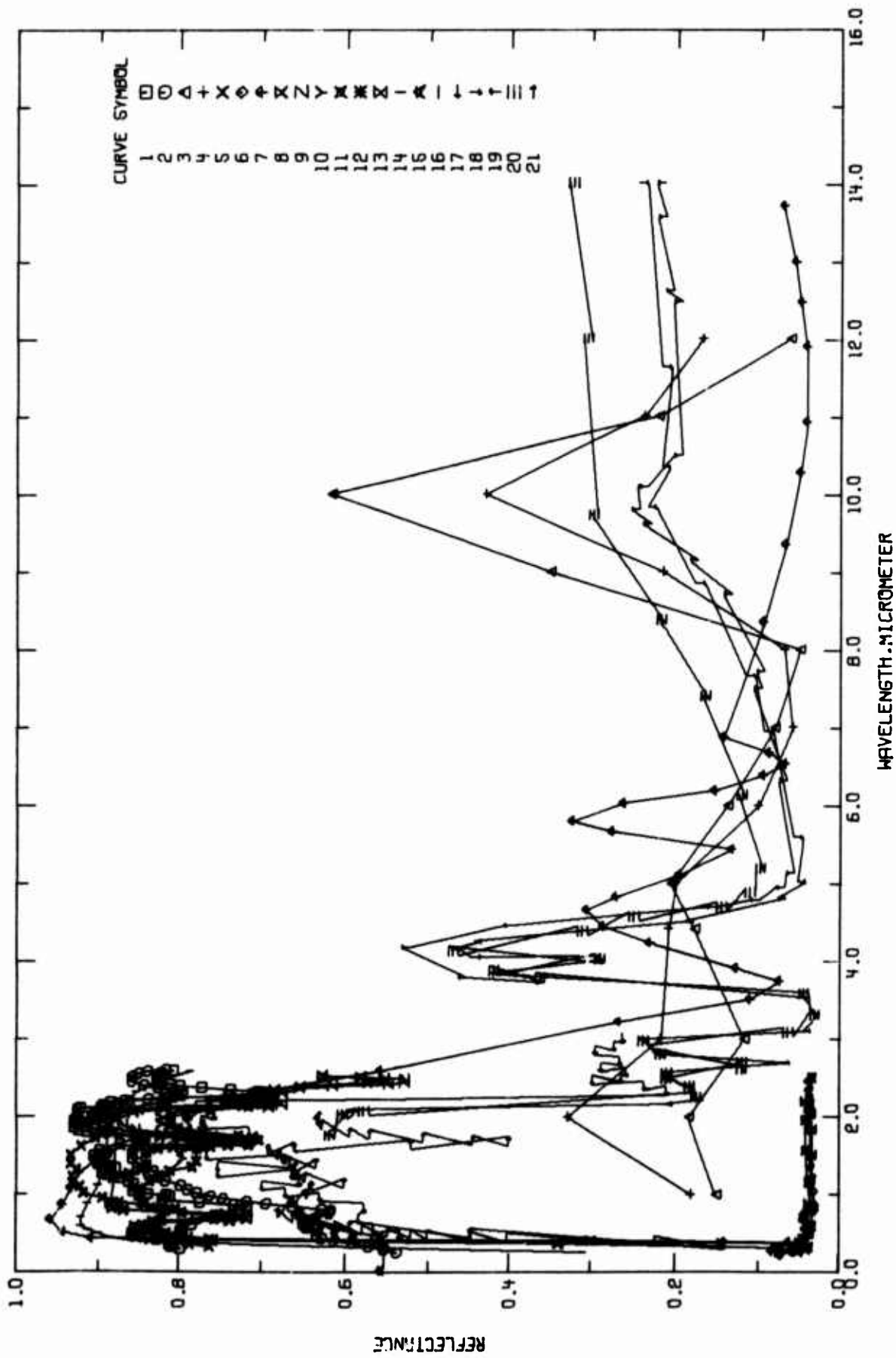


FIGURE 19-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE).

TABLE 19-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------------------------|------|---------------------------------|----------------------|---|---|
| 1 T41945 | Caldwell, C.R. and Nelsen, P.A. | 1969 | 0.25-2.6 | ~293 | RTV-602 | 3.8 mil RTV-602 silicone over aluminum foil; data were extracted from figure; $\theta \sim 0^\circ$. |
| 2 T41945 | Caldwell, C.R. and Nelsen, P.A. | 1969 | 0.25-2.6 | ~293 | RTV-602 | Similar to the above specimen except 2.6 mil. |
| 3 T47062 | Wilburn, D.K. and Reius, O. | 1955 | 1-12 | ~293 | Silicone coated on cotton fabric | Silicone coated on cotton fabric; magnesium oxide was chosen as a standard for diffuse reflector; data were extracted from figure; $\theta \sim 0^\circ$. |
| 4 T47062 | Wilburn, D.K. and Reius, O. | 1955 | 1-12 | ~293 | Silicone coated on cotton fabric | Similar to the above specimen. |
| 5 T41421 | Griffin, R.N. and Linder, B. | 1969 | 0.3-2.3 | ~293 | Silicone PJ 113 on Aluminum | General Electric experimental silicone resin 301-15-170 (PJ 113) was on aluminum substrate; data were extracted from figure; $\theta \sim 0^\circ$. |
| 6 T35934 | Faugers, J.F. | 1965 | 0.3-2.6 | ~293 | Pyroloc 7G800 | Silicone black paint; a DK 2A spectrometer was used to measure the reflectance; $\theta \sim 0^\circ$. |
| 7 T53491 | Marshall, K.N. and Branch, R.A. | 1968 | 0.3-25 | 295 | Silicone coating | White silicone coating on optical solar reflector; the spectral reflectance data were obtained using a Gier-Dunkle integrating sphere and a Gier Dunkle heated cavity directional reflectometer; data were extracted from figure; $\theta \sim 0^\circ$. |
| 8 T34045 | Porter, J. and Butler, E.A.W. | 1965 | 0.3-2.6 | ~293 | White Silicone Paint F663-2020-1/001/35 | Air dried on MKI integrating sphere; a Beckman DK 2A spectrometer was used; data were extracted from figure; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 9 T34045 | Porter, J. and Butler, E.A.W. | 1965 | 0.3-2.6 | ~293 | White Silicone Paint F663-2020-1/001/35 | Similar to the above specimen except cured at 250 C. |
| 10 T34045 | Porter, J. and Butler, E.A.W. | 1965 | 0.3-2.6 | ~293 | White Silicone Paint F663-2020-1/001/35 | Similar to the above specimen except air dried on MKII sphere. |
| 11 T34045 | Porter, J. and Butler, E.A.W. | 1965 | 0.3-2.6 | ~293 | White Silicone Paint F663-2020-1/001/35 | Similar to the above specimen except cured at 250 C. |
| 12 T34045 | Porter, J. and Butler, E.A.W. | 1965 | 0.3-2.6 | ~293 | Gloss Black Silicone Paint F663-2021-1/001/35 | Similar to the above specimen except air dried on MKI sphere. |
| 13 T34045 | Porter, J. and Butler, E.A.W. | 1965 | 0.3-2.6 | ~293 | Gloss Black Silicone Paint F663-2021-1/001/35 | Similar to the above specimen except air dried on MKII sphere. |
| 14 T41934 | Slomp, W.S. and Hamkinson, T.W.E. | 1969 | 0.3-2.6 | ~293 | H-10 | Calcined (Mons 90) clay-methyl silicone (RTV-602) specimen was obtained from Hughes Aircraft Co.; data were extracted from figure; $\theta \sim 0^\circ$. |
| 15 T29599 | Carroll, W.F. | 1962 | 0.021-0.751 | 298 | | DC 808 silicone 3 parts by wt. TBT 2 parts by wt.; polished aluminum substrate; data were extracted from figure; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 16 T29599 | Carroll, W.F. | 1962 | 0.372-0.751 | 298 | | The above specimen except it was exposed to UV at about 10 runs for 22.75 hr; data were extracted from smooth curve. |
| 17 T40420 | Wetmore, R.A. | 1963 | 0.49-3.00 | 300 | Sample 29R | Dow Corning 6510 silicone (0.432 mm thick); aluminum substrate; data were extracted from smooth curve; $\theta = 5^\circ$, $\omega' = 2\pi$. |
| 18 T40420 | Wetmore, R.A. | 1963 | 1.76-14.0 | 389 | Sample 31Ra | Similar to the above specimen. |
| 19 T40420 | Wetmore, R.A. | 1963 | 3.72-14.0 | 422 | Sample 30Ra | Similar to the above specimen. |
| 20 T40420 | Wetmore, R.A. | 1963 | 1.76-14.0 | 450 | Sample 31Rb | Similar to the above specimen. |

TABLE 19-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 21 T77391 | Turner, H.C. and Keller, E.E. | 1959 | 0.25-2.0 | ~293 | X5G-138 | Silicone/"5" glass; a Beckman DK-2 spectrorreflectometer was used in measurements; data were extracted from smooth curve. |

TABLE 19-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE)
(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 T = 293. | | | CURVE 2 (CONT.) | | | CURVE 2 (CONT.) | | | CURVE 3 T = 293. | | | CURVE 4 T = 293. | | | CURVE 5 T = 293. | | | CURVE 6 (CONT.) | | | |
|---------------------|--------|---------------------|-----------------|-----------|--------|---------------------|--------|-----------|---------------------|---------------------|--------|---------------------|--------|-----------|---------------------|-----------|--------|-----------------|--------|-----------|--------|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
| 0.313 | 0.798 | 1.748 | 0.652 | 0.620 | 0.651 | 2.362 | 0.825 | 2.402 | 0.843 | 0.333 | 0.762 | 0.40 | 0.0432 | | | | | | | | |
| 0.344 | 0.209 | 1.817 | 0.915 | 0.663 | 0.646 | 2.455 | 0.858 | 2.455 | 0.858 | 0.364 | 0.786 | 0.44 | 0.0423 | | | | | | | | |
| 0.368 | 0.812 | 1.875 | 0.930 | 0.760 | 0.619 | 2.520 | 0.850 | 2.520 | 0.850 | 0.391 | 0.798 | 0.57 | 0.0423 | | | | | | | | |
| 0.406 | 0.826 | 1.966 | 0.930 | 0.812 | 0.618 | 2.555 | 0.839 | 2.555 | 0.839 | 0.418 | 0.809 | 0.69 | 0.0451 | | | | | | | | |
| 0.540 | 0.798 | 2.005 | 0.926 | 0.845 | 0.663 | 2.583 | 0.817 | 2.583 | 0.817 | 0.444 | 0.820 | 0.74 | 0.0451 | | | | | | | | |
| 0.608 | 0.794 | 2.105 | 0.926 | 0.879 | 0.694 | 2.600 | 0.817 | 2.600 | 0.817 | 0.477 | 0.827 | 0.77 | 0.0424 | | | | | | | | |
| 0.626 | 0.784 | 2.122 | 0.922 | 0.910 | 0.718 | CURVE 3 T = 293. | | | 0.535 | 0.838 | 0.0311 | 0.0357 | | | | | | | | | |
| 0.693 | 0.778 | 2.135 | 0.897 | 0.950 | 0.746 | 1.00 | 0.151 | 2.00 | 0.184 | 0.607 | 0.838 | 1.03 | 0.0323 | | | | | | | | |
| 0.744 | 0.755 | 2.165 | 0.694 | 0.978 | 0.761 | 2.00 | 0.118 | 3.00 | 0.118 | 0.663 | 0.821 | 1.22 | 0.0344 | | | | | | | | |
| 0.812 | 0.727 | 2.201 | 0.885 | 1.020 | 0.778 | 4.41 | 0.177 | 4.41 | 0.177 | 0.750 | 0.821 | 1.36 | 0.0357 | | | | | | | | |
| 0.833 | 0.717 | 2.219 | 0.867 | 1.062 | 0.785 | 5.00 | 0.206 | 5.00 | 0.206 | 0.787 | 0.816 | 1.50 | 0.0364 | | | | | | | | |
| 0.856 | 0.717 | 2.244 | 0.867 | 1.117 | 0.799 | 6.00 | 0.139 | 6.00 | 0.139 | 0.817 | 0.804 | 2.09 | 0.0364 | | | | | | | | |
| 0.880 | 0.733 | 2.282 | 0.740 | 1.174 | 0.816 | 7.00 | 0.081 | 7.00 | 0.081 | 0.862 | 0.842 | 2.19 | 0.0371 | | | | | | | | |
| 0.907 | 0.774 | 2.298 | 0.710 | 1.218 | 0.823 | 8.00 | 0.050 | 8.00 | 0.050 | 0.904 | 0.873 | 2.35 | 0.0377 | | | | | | | | |
| 0.930 | 0.820 | 2.319 | 0.698 | 1.297 | 0.831 | 9.00 | 0.350 | 9.00 | 0.350 | 1.020 | 0.919 | 2.47 | 0.0385 | | | | | | | | |
| 0.949 | 0.820 | 2.332 | 0.705 | 1.357 | 0.840 | 10.00 | 0.619 | 10.00 | 0.619 | 1.109 | 0.923 | CURVE 7 T = 295. | | | | | | | | | |
| 0.983 | 0.811 | 2.356 | 0.737 | 1.402 | 0.850 | 11.00 | 0.221 | 11.00 | 0.221 | 1.156 | 0.933 | 0.27 | 0.084 | | | | | | | | |
| 0.999 | 0.815 | 2.385 | 0.772 | 1.464 | 0.857 | 12.00 | 0.063 | 12.00 | 0.063 | 1.240 | 0.933 | 0.38 | 0.063 | | | | | | | | |
| 1.016 | 0.838 | 2.404 | 0.799 | 1.550 | 0.857 | CURVE 4 T = 293. | | | 1.325 | 0.927 | 0.67 | 0.0960 | | | | | | | | | |
| 1.032 | 0.847 | 2.428 | 0.611 | 1.626 | 0.851 | 1.00 | 0.181 | 2.00 | 0.328 | 1.514 | 0.934 | 0.38 | 0.142 | | | | | | | | |
| 1.057 | 0.855 | 2.456 | 0.623 | 1.679 | 0.841 | 3.00 | 0.217 | 3.00 | 0.217 | 1.624 | 0.921 | 0.43 | 0.0808 | | | | | | | | |
| 1.142 | 0.855 | 2.484 | 0.827 | 1.679 | 0.841 | 4.41 | 0.209 | 4.41 | 0.209 | 1.726 | 0.904 | 0.51 | 0.0943 | | | | | | | | |
| 1.183 | 0.861 | 2.539 | 0.827 | 1.730 | 0.853 | 5.00 | 0.200 | 5.00 | 0.200 | 1.769 | 0.895 | 0.67 | 0.0960 | | | | | | | | |
| 1.227 | 0.871 | 2.569 | 0.821 | 1.781 | 0.874 | 6.00 | 0.102 | 6.00 | 0.102 | 1.811 | 0.895 | 0.87 | 0.0945 | | | | | | | | |
| 1.260 | 0.889 | 2.600 | 0.806 | 1.836 | 0.889 | 7.00 | 0.059 | 7.00 | 0.059 | 1.867 | 0.916 | 0.87 | 0.0945 | | | | | | | | |
| 1.295 | 0.895 | CURVE 2 T = 293. | | | 1.900 | 0.903 | 8.00 | 0.069 | 8.00 | 0.069 | 1.956 | 0.916 | 1.08 | 0.0934 | | | | | | | |
| 1.347 | 0.884 | 0.255 | 0.539 | 1.960 | 0.908 | 9.00 | 0.216 | 9.00 | 0.216 | 1.998 | 0.904 | 1.28 | 0.0924 | | | | | | | | |
| 1.350 | 0.878 | 0.296 | 0.554 | 2.028 | 0.908 | 10.00 | 0.430 | 10.00 | 0.430 | 2.075 | 0.876 | 1.43 | 0.0934 | | | | | | | | |
| 1.369 | 0.884 | 0.335 | 0.572 | 2.085 | 0.900 | 11.00 | 0.805 | 11.00 | 0.805 | 2.180 | 0.821 | 1.55 | 0.0934 | | | | | | | | |
| 1.407 | 0.900 | 0.376 | 0.591 | 2.135 | 0.889 | 12.00 | 0.795 | 12.00 | 0.795 | CURVE 6 T = 293. | | | 1.62 | 0.0968 | | | | | | | |
| 1.432 | 0.901 | 0.411 | 0.613 | 2.166 | 0.877 | 0.23 | 0.073 | 0.23 | 0.073 | 1.64 | 0.737 | 1.69 | 0.0802 | | | | | | | | |
| 1.462 | 0.894 | 0.434 | 0.628 | 2.199 | 0.861 | 0.28 | 0.0604 | 0.28 | 0.0604 | 1.69 | 0.705 | 1.74 | 0.0705 | | | | | | | | |
| 1.489 | 0.865 | 0.479 | 0.634 | 2.225 | 0.838 | 0.31 | 0.0529 | 0.31 | 0.0529 | 1.76 | 0.839 | 1.82 | 0.0785 | | | | | | | | |
| 1.515 | 0.906 | 0.560 | 0.635 | 2.254 | 0.818 | 0.35 | 0.0456 | 0.35 | 0.0456 | 1.82 | 0.785 | 1.96 | 0.0769 | | | | | | | | |
| 1.560 | 0.899 | 0.581 | 0.647 | 2.275 | 0.795 | | | | | | | 2.20 | 0.761 | | | | | | | | |
| 1.666 | 0.873 | 0.647 | 0.647 | 2.275 | 0.795 | | | | | | | 2.59 | 0.559 | | | | | | | | |
| 1.728 | 0.848 | 0.647 | 0.647 | 2.303 | 0.795 | | | | | | | | | | | | | | | | |
| | | 0.647 | 0.647 | 2.331 | 0.807 | | | | | | | | | | | | | | | | |

TABLE 13-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | | |
|-----------------------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------------|--------|-----------|--------|-------|-------|
| CURVE 14 T = 293. | | | | | | | | | | | | | |
| 0.253 | 0.310 | 0.372 | 0.149 | 2.50 | 0.265 | 10.34 | 0.213 | 2.70 | 0.121 | 1.506 | 0.680 | | |
| 0.351 | 0.657 | 0.399 | 0.224 | 2.57 | 0.259 | 11.63 | 0.212 | 2.80 | 0.210 | 1.575 | 0.693 | | |
| 0.374 | 0.775 | 0.449 | 0.403 | 2.63 | 0.289 | 14.00 | 0.240 | 2.97 | 0.239 | 1.601 | 0.663 | | |
| 0.385 | 0.822 | 0.466 | 0.447 | 2.71 | 0.266 | CURVE 19 | | | | | 1.641 | 0.523 | |
| 0.405 | 0.857 | 0.487 | 0.502 | 2.85 | 0.296 | T = 422. | | | | | 1.678 | 0.401 | |
| 0.443 | 0.885 | 0.500 | 0.522 | 2.90 | 0.273 | 3.72 | 0.363 | 3.58 | 0.045 | 1.701 | 0.445 | | |
| 0.495 | 0.902 | 0.518 | 0.550 | 3.00 | 0.263 | 3.79 | 0.460 | 3.78 | 0.362 | 1.739 | 0.507 | | |
| 0.542 | 0.913 | 0.549 | 0.580 | CURVE 18 | | | | | | | | 1.775 | 0.572 |
| 0.593 | 0.922 | 0.600 | 0.613 | T = 389. | | | | | | | | 1.798 | 0.595 |
| 0.709 | 0.922 | 0.649 | 0.637 | 1.76 | 0.620 | 4.18 | 0.529 | 4.02 | 0.289 | 1.898 | 0.629 | | |
| 0.689 | 0.914 | 0.702 | 0.654 | 2.03 | 0.604 | 4.45 | 0.402 | 4.38 | 0.311 | 1.951 | 0.636 | | |
| 1.123 | 0.901 | 0.751 | 0.658 | 2.09 | 0.592 | 4.69 | 0.158 | 4.57 | 0.250 | 2.000 | 0.633 | | |
| 1.381 | 0.895 | CURVE 17 | | | | | | | | | 2.000 | 0.633 | |
| 1.743 | 0.889 | T = 300. | | | | | | | | | | | |
| 1.940 | 0.883 | 1.49 | 0.536 | 2.16 | 0.209 | 4.94 | 0.075 | 4.69 | 0.146 | | | | |
| 2.100 | 0.873 | 2.03 | 0.567 | 2.22 | 0.172 | 5.13 | 0.062 | 4.80 | 0.112 | | | | |
| 2.209 | 0.862 | 2.38 | 0.183 | 2.38 | 0.183 | 6.32 | 0.071 | 4.99 | 0.099 | | | | |
| 2.312 | 0.853 | 2.48 | 0.211 | 2.48 | 0.211 | 7.50 | 0.102 | 5.19 | 0.121 | | | | |
| 2.406 | 0.834 | 2.56 | 0.211 | 2.56 | 0.211 | 7.72 | 0.099 | 6.13 | 0.165 | | | | |
| 2.491 | 0.815 | 2.69 | 0.585 | 2.69 | 0.067 | 8.71 | 0.139 | 7.40 | 0.218 | | | | |
| 2.580 | 0.786 | 2.79 | 0.578 | 2.79 | 0.217 | 9.14 | 0.179 | 8.38 | 0.298 | | | | |
| | | 0.97 | 0.631 | 2.98 | 0.240 | 9.80 | 0.235 | 9.73 | 0.305 | | | | |
| | | 1.02 | 0.672 | 3.10 | 0.041 | 10.09 | 0.241 | 12.00 | 0.323 | | | | |
| | | 1.11 | 0.700 | 3.32 | 0.030 | 10.49 | 0.199 | CURVE 21 | | | | | |
| | | 1.17 | 0.656 | 3.60 | 0.044 | 12.47 | 0.199 | T = 293. | | | | | |
| | | 1.26 | 0.664 | 3.84 | 0.386 | 12.61 | 0.209 | 0.350 | 0.141 | 0.350 | 0.141 | | |
| | | 1.27 | 0.753 | 3.84 | 0.420 | 13.56 | 0.218 | 0.502 | 0.449 | 0.502 | 0.449 | | |
| | | 1.36 | 0.753 | 4.01 | 0.288 | 14.00 | 0.220 | 0.602 | 0.595 | 0.602 | 0.595 | | |
| | | 1.40 | 0.667 | 4.06 | 0.293 | CURVE 20 | | | | | 0.702 | 0.663 | |
| | | 1.45 | 0.673 | 4.05 | 0.441 | T = 450. | | | | | 0.757 | 0.682 | |
| | | 1.50 | 0.766 | 4.15 | 0.468 | 1.76 | 0.620 | 0.903 | 0.665 | 0.903 | 0.665 | | |
| | | 1.63 | 0.790 | 4.25 | 0.440 | 2.03 | 0.604 | 1.002 | 0.649 | 1.002 | 0.649 | | |
| | | 1.80 | 0.715 | 4.51 | 0.184 | 2.63 | 0.620 | 1.103 | 0.642 | 1.103 | 0.642 | | |
| | | 1.90 | 0.769 | 4.81 | 0.073 | 2.07 | 0.579 | 1.147 | 0.602 | 1.147 | 0.602 | | |
| | | 1.94 | 0.773 | 5.02 | 0.048 | 2.25 | 0.175 | 1.217 | 0.649 | 1.217 | 0.649 | | |
| | | 2.02 | 0.757 | 5.59 | 0.052 | 2.39 | 0.183 | 1.250 | 0.659 | 1.250 | 0.659 | | |
| | | 2.13 | 0.780 | 6.95 | 0.088 | 2.49 | 0.211 | 1.301 | 0.665 | 1.301 | 0.665 | | |
| | | 2.33 | 0.211 | 7.06 | 0.111 | 2.56 | 0.211 | 1.350 | 0.661 | 1.350 | 0.661 | | |
| | | 2.39 | 0.237 | 8.85 | 0.171 | 2.61 | 0.121 | 1.399 | 0.636 | 1.399 | 0.636 | | |
| | | 2.47 | 0.299 | 9.53 | 0.230 | | | 1.450 | 0.673 | 1.450 | 0.673 | | |

c. Angular Spectral Reflectance (Wavelength Dependence)

There are seven sets of experimental data available for the wavelength dependence of the angular spectral reflectance of silicone resin coatings as listed in Table 19-9 and shown in Figure 19-6. Specimen characterization and measurement information for the data are given in Table 19-8. Only specular reflectance data were measured. All the specimens were coated over silver thin films and there is no information on the thickness of the silicone coating and silver thin film. As a consequence of these difficulties, only provisional values are reported here which are listed in Table 19-7 and shown in Figure 19-5 with the experimental data as background. The estimated uncertainty is about $\pm 30\%$.

TABLE 19-7. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE)
[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ |
|--------------------------|--------|
| COATING | |
| $\theta' = 0 - 45^\circ$ | |
| T = 293 | |
| 1.00 | 0.45 |
| 1.50 | 0.62 |
| 2.00 | 0.73 |
| 2.50 | 0.75 |
| 3.00 | 0.77 |
| 3.50 | 0.79 |
| 4.00 | 0.81 |
| 4.50 | 0.84 |
| 5.00 | 0.85 |
| 5.50 | 0.86 |
| 6.00 | 0.87 |
| 6.50 | 0.87 |
| 7.00 | 0.87 |
| 7.50 | 0.87 |
| 8.00 | 0.87 |
| 8.50 | 0.88 |
| 9.00 | 0.89 |
| 9.50 | 0.89 |
| 10.00 | 0.89 |
| 10.50 | 0.89 |
| 11.00 | 0.89 |
| 11.50 | 0.91 |
| 12.00 | 0.91 |
| 12.50 | 0.91 |
| 13.00 | 0.91 |
| 13.50 | 0.91 |
| 14.00 | 0.91 |
| 14.50 | 0.91 |
| 15.00 | 0.91 |

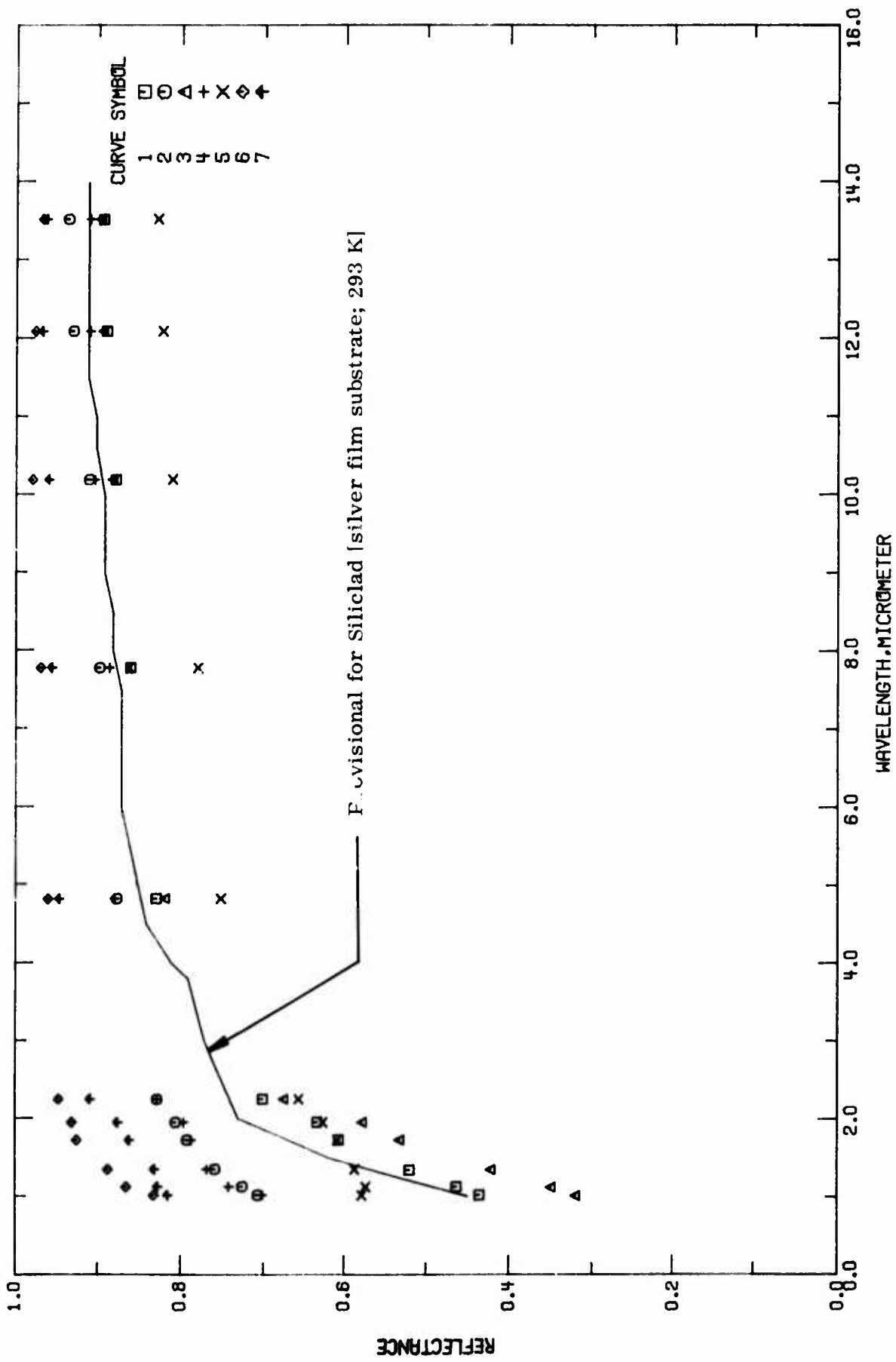


FIGURE 19-5. PROVISIONAL ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (WAVELENGTH DEPENDENCE).

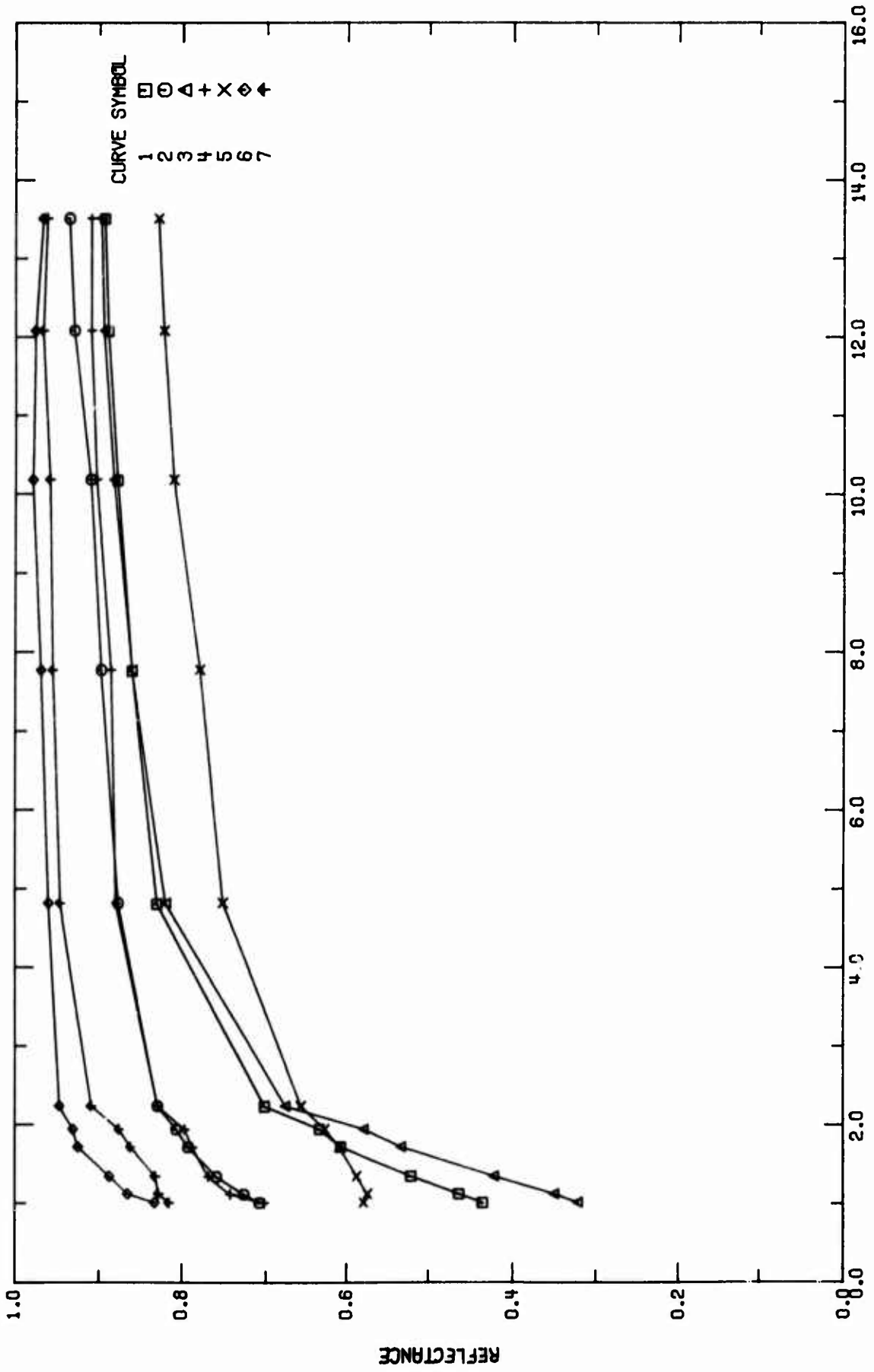


FIGURE 19-6. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE).

TABLE 19-8. MEASUREMENT INFORMATION ON THE ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN COATING (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | T33388 Belser, R. B., Carithers, M. D., Britt, F. L., Menders, J. C., Elston, L. W., Koralek, A. S., Cooke, J. C., and Frahm, C. P. | 1962 | 1-14.4 | ~293 | Ag 87 CS | Siliclad; silicone resin over coating on a silver film which is deposited on silicone resin coated 316 stainless steel substrate; silver film was applied by Brashear method; specular reflectance; data were extracted from the table; $\theta = 45^\circ$, $\theta' = 45^\circ$. |
| 2 | T33388 Belser, R. B., et al. | 1962 | 1-14.4 | ~293 | Ag 88 CS | Similar to the above specimen. |
| 3 | T33388 Belser, R. B., et al. | 1962 | 1-14.4 | ~293 | Ag 89 CS | Similar to the above specimen. |
| 4 | T33388 Belser, R. B., et al. | 1962 | 1-14.4 | ~293 | Ag 90 CS | Similar to the above specimen except silver film was deposited on SY627-119 polyurethane (Febert Shorndorfer Co.), and 316 stainless steel substrates. |
| 5 | T33388 Belser, R. B., et al. | 1962 | 1-14.4 | ~293 | Ag 91 CS | Similar to the above specimen. |
| 6 | T33388 Belser, R. B., et al. | 1962 | 1-14.4 | ~293 | Ag 92 CS | Similar to the above specimen except silver film was deposited on Maraset 617-C epoxy resin (Marblett Co.), and 316 stainless steel substrate. |
| 7 | T33388 Belser, R. B., et al. | 1962 | 1-14.4 | ~293 | Ag 93 CS | Similar to the above specimen. |

TABLE 19-9. EXPERIMENTAL ANGULAR SPECTRAL REFLECTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|---------------------|--------|-----------|--------|-----------|--------|-----------|--------|
| CURVE 1 T = 293. | | | | | | | |
| 1.009 | 0.435 | 7.780 | 0.859 | 1.009 | 0.831 | 10.198 | 0.661 |
| 1.120 | 0.463 | 10.198 | 0.661 | 1.120 | 0.864 | 12.099 | 0.893 |
| 1.345 | 0.519 | 12.099 | 0.893 | 1.345 | 0.886 | 13.530 | 0.896 |
| 1.720 | 0.606 | 13.530 | 0.896 | 1.720 | 0.923 | 14.375 | 0.892 |
| 1.945 | 0.633 | 14.375 | 0.892 | 1.945 | 0.929 | | |
| 2.240 | 0.700 | | | 2.240 | 0.945 | | |
| 4.824 | 0.828 | | | 4.824 | 0.958 | | |
| 7.780 | 0.859 | | | 7.780 | 0.967 | | |
| 10.198 | 0.877 | | | 10.198 | 0.977 | | |
| 12.099 | 0.888 | | | 12.099 | 0.974 | | |
| 13.530 | 0.892 | | | 13.530 | 0.965 | | |
| 14.375 | 0.889 | | | 14.375 | 0.953 | | |
| CURVE 2 T = 293. | | | | | | | |
| 1.009 | 0.706 | 10.198 | 0.700 | 1.009 | 0.614 | 1.120 | 0.826 |
| 1.120 | 0.725 | 1.120 | 0.741 | 1.120 | 0.826 | 1.345 | 0.630 |
| 1.345 | 0.757 | 1.345 | 0.767 | 1.345 | 0.630 | 1.720 | 0.860 |
| 1.720 | 0.791 | 1.720 | 0.786 | 1.720 | 0.860 | 1.945 | 0.874 |
| 1.945 | 0.805 | 1.945 | 0.795 | 1.945 | 0.874 | 2.240 | 0.907 |
| 2.240 | 0.827 | 2.240 | 0.827 | 2.240 | 0.907 | 4.824 | 0.944 |
| 4.824 | 0.875 | 4.824 | 0.878 | 4.824 | 0.944 | 7.780 | 0.953 |
| 7.780 | 0.896 | 7.780 | 0.884 | 7.780 | 0.953 | 10.198 | 0.957 |
| 10.198 | 0.909 | 10.198 | 0.902 | 10.198 | 0.957 | 12.099 | 0.965 |
| 12.099 | 0.928 | 12.099 | 0.908 | 12.099 | 0.965 | 13.530 | 0.960 |
| 13.530 | 0.934 | 13.530 | 0.908 | 13.530 | 0.960 | 14.375 | 0.962 |
| 14.375 | 0.932 | 14.375 | 0.917 | 14.375 | 0.962 | | |
| 1.945 | 0.605 | | | | | | |
| 2.240 | 0.827 | | | | | | |
| 4.824 | 0.875 | | | | | | |
| 7.780 | 0.896 | | | | | | |
| 10.198 | 0.909 | | | | | | |
| 12.099 | 0.928 | | | | | | |
| 13.530 | 0.934 | | | | | | |
| 14.375 | 0.932 | | | | | | |
| CURVE 3 T = 293. | | | | | | | |
| 1.009 | 0.320 | 1.009 | 0.577 | 1.009 | 0.577 | 1.120 | 0.572 |
| 1.120 | 0.349 | 1.120 | 0.572 | 1.120 | 0.572 | 1.345 | 0.586 |
| 1.345 | 0.422 | 1.345 | 0.586 | 1.345 | 0.586 | 1.720 | 0.508 |
| 1.720 | 0.531 | 1.720 | 0.508 | 1.720 | 0.508 | 1.945 | 0.626 |
| 1.945 | 0.577 | 1.945 | 0.626 | 1.945 | 0.626 | 2.240 | 0.656 |
| 2.240 | 0.675 | 2.240 | 0.656 | 2.240 | 0.656 | 4.824 | 0.750 |
| 4.824 | 0.818 | 4.824 | 0.750 | 4.824 | 0.750 | 7.780 | 0.778 |
| 7.780 | 0.818 | 7.780 | 0.778 | 7.780 | 0.778 | 10.198 | 0.809 |
| 10.198 | 0.832 | 10.198 | 0.809 | 10.198 | 0.809 | 12.099 | 0.821 |
| 12.099 | 0.842 | 12.099 | 0.821 | 12.099 | 0.821 | 13.530 | 0.827 |
| 13.530 | 0.842 | 13.530 | 0.827 | 13.530 | 0.827 | 14.375 | 0.842 |
| 14.375 | 0.842 | 14.375 | 0.842 | 14.375 | 0.842 | | |
| CURVE 4 T = 293. | | | | | | | |
| 1.009 | 0.700 | 1.009 | 0.700 | 1.009 | 0.700 | 1.120 | 0.741 |
| 1.120 | 0.741 | 1.120 | 0.741 | 1.120 | 0.741 | 1.345 | 0.767 |
| 1.345 | 0.767 | 1.345 | 0.767 | 1.345 | 0.767 | 1.720 | 0.786 |
| 1.720 | 0.786 | 1.720 | 0.786 | 1.720 | 0.786 | 1.945 | 0.795 |
| 1.945 | 0.795 | 1.945 | 0.795 | 1.945 | 0.795 | 2.240 | 0.827 |
| 2.240 | 0.827 | 2.240 | 0.827 | 2.240 | 0.827 | 4.824 | 0.878 |
| 4.824 | 0.878 | 4.824 | 0.878 | 4.824 | 0.878 | 7.780 | 0.884 |
| 7.780 | 0.884 | 7.780 | 0.884 | 7.780 | 0.884 | 10.198 | 0.902 |
| 10.198 | 0.902 | 10.198 | 0.902 | 10.198 | 0.902 | 12.099 | 0.908 |
| 12.099 | 0.908 | 12.099 | 0.908 | 12.099 | 0.908 | 13.530 | 0.908 |
| 13.530 | 0.908 | 13.530 | 0.908 | 13.530 | 0.908 | 14.375 | 0.917 |
| 14.375 | 0.917 | 14.375 | 0.917 | 14.375 | 0.917 | | |
| CURVE 5 T = 293. | | | | | | | |
| 1.009 | 0.577 | 1.009 | 0.577 | 1.009 | 0.577 | 1.120 | 0.572 |
| 1.120 | 0.572 | 1.120 | 0.572 | 1.120 | 0.572 | 1.345 | 0.586 |
| 1.345 | 0.586 | 1.345 | 0.586 | 1.345 | 0.586 | 1.720 | 0.508 |
| 1.720 | 0.508 | 1.720 | 0.508 | 1.720 | 0.508 | 1.945 | 0.626 |
| 1.945 | 0.626 | 1.945 | 0.626 | 1.945 | 0.626 | 2.240 | 0.656 |
| 2.240 | 0.656 | 2.240 | 0.656 | 2.240 | 0.656 | 4.824 | 0.750 |
| 4.824 | 0.750 | 4.824 | 0.750 | 4.824 | 0.750 | 7.780 | 0.778 |
| 7.780 | 0.778 | 7.780 | 0.778 | 7.780 | 0.778 | 10.198 | 0.809 |
| 10.198 | 0.809 | 10.198 | 0.809 | 10.198 | 0.809 | 12.099 | 0.821 |
| 12.099 | 0.821 | 12.099 | 0.821 | 12.099 | 0.821 | 13.530 | 0.827 |
| 13.530 | 0.827 | 13.530 | 0.827 | 13.530 | 0.827 | 14.375 | 0.842 |
| 14.375 | 0.842 | 14.375 | 0.842 | 14.375 | 0.842 | | |
| CURVE 6 T = 293. | | | | | | | |
| 1.009 | 0.831 | 1.009 | 0.831 | 1.009 | 0.831 | 1.120 | 0.864 |
| 1.120 | 0.864 | 1.120 | 0.864 | 1.120 | 0.864 | 1.345 | 0.886 |
| 1.345 | 0.886 | 1.345 | 0.886 | 1.345 | 0.886 | 1.720 | 0.923 |
| 1.720 | 0.923 | 1.720 | 0.923 | 1.720 | 0.923 | 1.945 | 0.929 |
| 1.945 | 0.929 | 1.945 | 0.929 | 1.945 | 0.929 | 2.240 | 0.945 |
| 2.240 | 0.945 | 2.240 | 0.945 | 2.240 | 0.945 | 4.824 | 0.958 |
| 4.824 | 0.958 | 4.824 | 0.958 | 4.824 | 0.958 | 7.780 | 0.967 |
| 7.780 | 0.967 | 7.780 | 0.967 | 7.780 | 0.967 | 10.198 | 0.977 |
| 10.198 | 0.977 | 10.198 | 0.977 | 10.198 | 0.977 | 12.099 | 0.974 |
| 12.099 | 0.974 | 12.099 | 0.974 | 12.099 | 0.974 | 13.530 | 0.965 |
| 13.530 | 0.965 | 13.530 | 0.965 | 13.530 | 0.965 | 14.375 | 0.953 |
| 14.375 | 0.953 | 14.375 | 0.953 | 14.375 | 0.953 | | |
| CURVE 7 T = 293. | | | | | | | |
| 1.009 | 0.614 | 1.009 | 0.614 | 1.009 | 0.614 | 1.120 | 0.826 |
| 1.120 | 0.826 | 1.120 | 0.826 | 1.120 | 0.826 | 1.345 | 0.630 |
| 1.345 | 0.630 | 1.345 | 0.630 | 1.345 | 0.630 | 1.720 | 0.860 |
| 1.720 | 0.860 | 1.720 | 0.860 | 1.720 | 0.860 | 1.945 | 0.874 |
| 1.945 | 0.874 | 1.945 | 0.874 | 1.945 | 0.874 | 2.240 | 0.907 |
| 2.240 | 0.907 | 2.240 | 0.907 | 2.240 | 0.907 | 4.824 | 0.944 |
| 4.824 | 0.944 | 4.824 | 0.944 | 4.824 | 0.944 | 7.780 | 0.953 |
| 7.780 | 0.953 | 7.780 | 0.953 | 7.780 | 0.953 | 10.198 | 0.957 |
| 10.198 | 0.957 | 10.198 | 0.957 | 10.198 | 0.957 | 12.099 | 0.965 |
| 12.099 | 0.965 | 12.099 | 0.965 | 12.099 | 0.965 | 13.530 | 0.960 |
| 13.530 | 0.960 | 13.530 | 0.960 | 13.530 | 0.960 | 14.375 | 0.962 |
| 14.375 | 0.962 | 14.375 | 0.962 | 14.375 | 0.962 | | |

d. Normal Spectral Transmittance (Wavelength Dependence)

There are 26 sets of experimental data available for the wavelength dependence of the normal spectral reflectance of silicone resin as listed in Table 19-9 and shown in Figure 19-6 (bulk materials) and Figure 19-7 (thin films). Specimen characterization and measurement information for the data are given in Table 19-8. There were 22 different kinds of silicone resins used for measurement; their transmittance values were quite different. Therefore, only provisional values are reported here which are listed in Table 19-7 and shown in Figure 19-5. The provisional values are for Dow Corning XR6-2044 silicone resin with thickness 0.112 mm at 293 K. The estimated uncertainty is about $\pm 30\%$.

TABLE 19-10. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T |
|----------------|------|
| DC XR6-2044 | |
| 0.112 MM THICK | |
| T = 293 | |
| 0.30 | 0.34 |
| 0.40 | 0.86 |
| 0.50 | 0.58 |
| 0.70 | 0.89 |
| 1.00 | 0.90 |
| 1.25 | 0.93 |
| 1.35 | 0.89 |
| 1.40 | 0.87 |
| 1.45 | 0.88 |
| 1.50 | 0.89 |
| 1.60 | 0.89 |
| 1.62 | 0.88 |
| 1.64 | 0.71 |
| 1.65 | 0.58 |
| 1.68 | 0.40 |
| 1.70 | 0.35 |
| 1.71 | 0.33 |
| 1.74 | 0.66 |
| 1.76 | 0.63 |
| 1.78 | 0.75 |
| 1.80 | 0.77 |
| 1.83 | 0.80 |
| 1.85 | 0.84 |
| 1.90 | 0.85 |
| 2.00 | 0.86 |
| 2.15 | 0.86 |

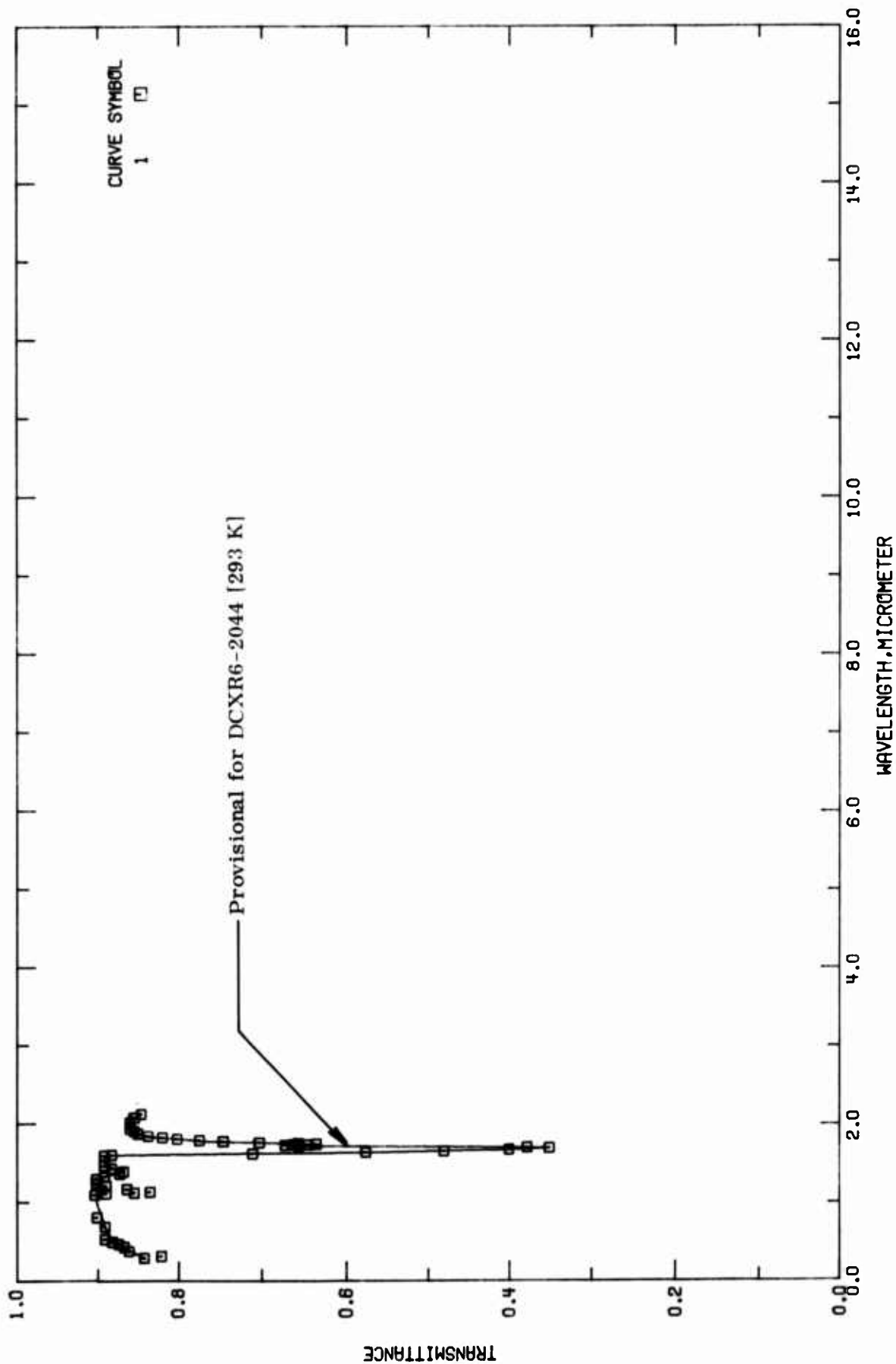


FIGURE 19-7. PROVISIONAL NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE).

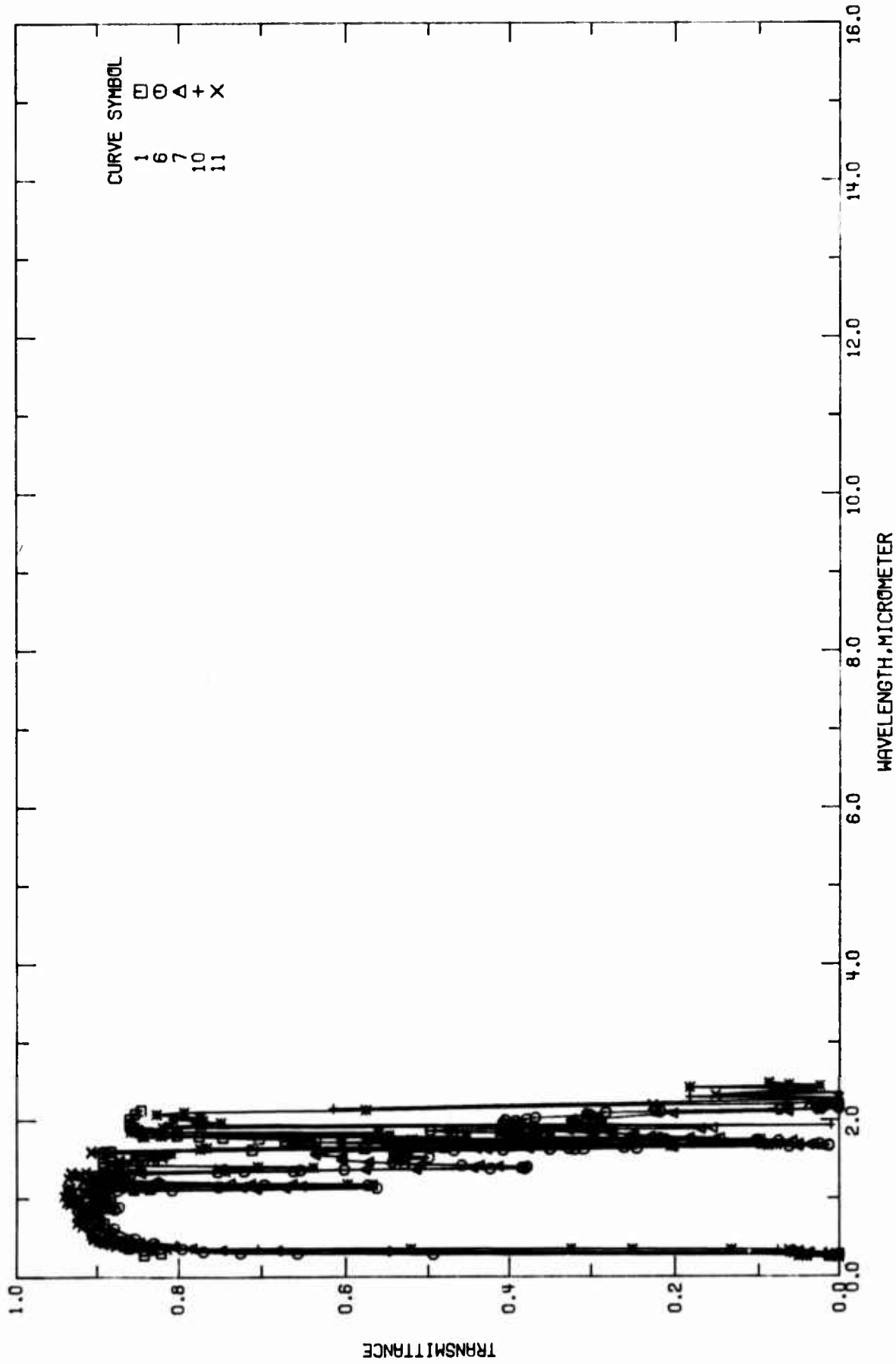


FIGURE 19-8. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESIN (WAVELENGTH DEPENDENCE).

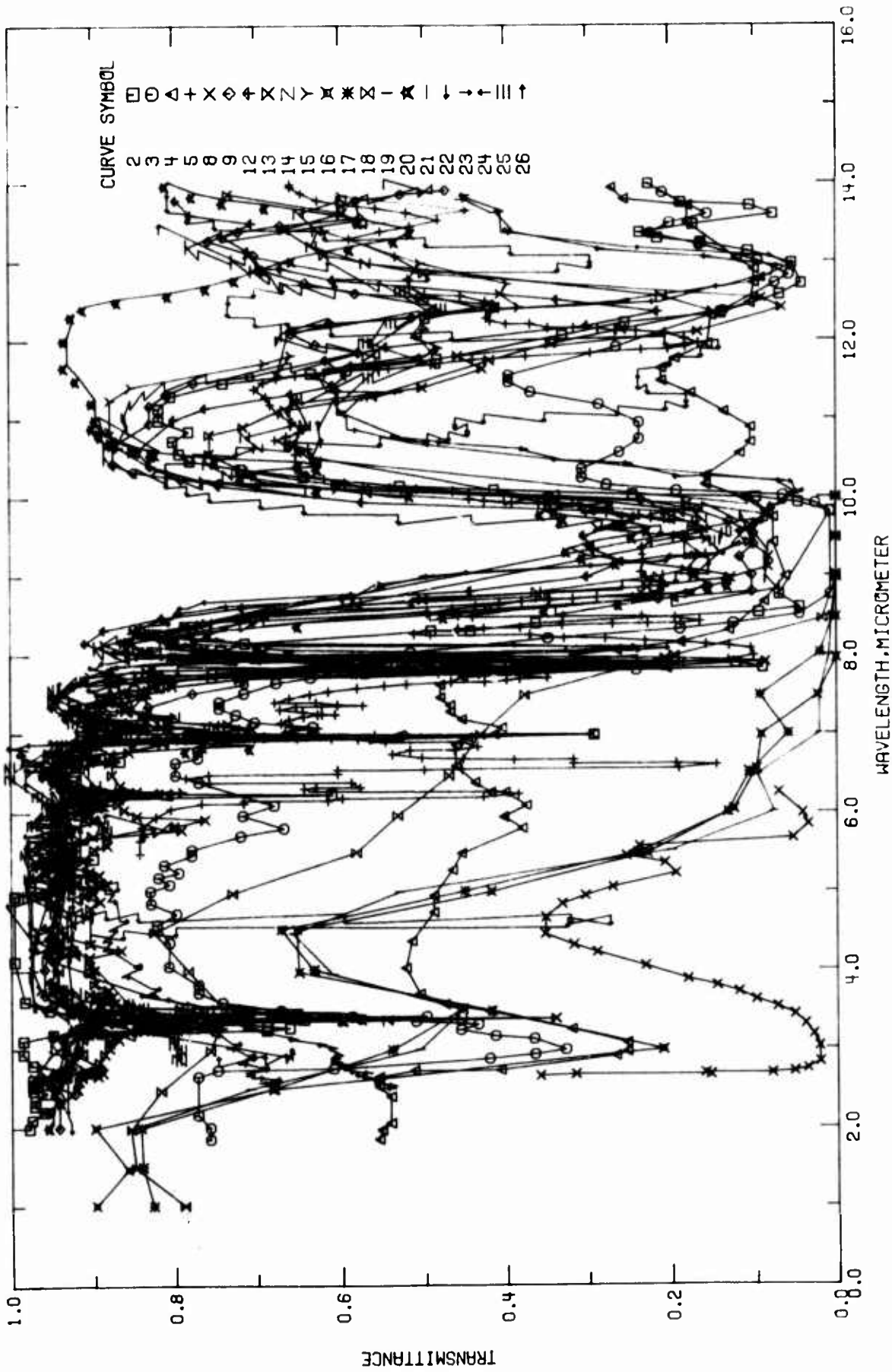


FIGURE 19-9. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESIN COATINGS (WAVELENGTH DEPENDENCE).

TABLE 19-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESINS (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent). Specifications, and Remarks |
|--------------------|---|------|---------------------------------|----------------------|--|--|
| 1 T19818 | Wituchi, R. M. and Lewis, A. E. | 1961 | 0.3-2.1 | 293 | XR6-2044 Resin (Dow Corning) | 0.046 in. thick with no substrate, curve not corrected for reflection losses; measurements on Dow Corning 805 and Dow Corning 4000 resins showed all to be very similar; $\theta \sim 0^\circ$. |
| 2 T24833 | Cowling, J. E., Alexander, A. V., Noonan, F., Kagariase, H., and Stokes, S. | 1960 | 2-15 | 293 | Phenyl Silicone Resin Film | Film-forming polymers in a vacuum of approx. 10^{-4} mm pressure; $\theta \sim 0^\circ$. |
| 3 T24833 | Cowling, J. E., et al. | 1960 | 2-15 | 293 | Phenyl Silicone Resin Film | Similar to the above specimen except film was exposed to mercury vapor lamp 80 hr (11.3 mW/cm^2 at 10 cm). |
| 4 T24833 | Cowling, J. E., et al. | 1960 | 2-15 | 293 | Phenyl Silicone Resin Film | Similar to the above specimen except film was exposed to mercury vapor lamp 250 hr. |
| 5 T36546 | Zerlaut, G. A. | 1960 | 5.5-14 | 293 | Dow Corning 808 | No thickness or details given; $\theta \sim 0^\circ$. |
| 6 T40338 | Acitelli, M. A., Gandy, W. L., and Nujokas, A. A. | 1966 | 0.2-2.2 | 296 | Glass Resin 100 | 6.67 mm thick disc approx. 50 mm in diameter; specimen was obtained from Owen-Illinois; Cary spectrophotometer was used for measurements; $\theta \sim 0^\circ$. |
| 7 T40338 | Acitelli, M. A., et al. | 1966 | 0.2-2.2 | 296 | Glass Resin 100 "CR 39" | Similar to the above specimen except 6.75 mm thick. |
| 8 T51317 T51318 | Chuiko, A. A., Pavlik, G. E., Tertykh, V. A., Chuiko, E. A., Artenov, V. A., Neimark, I. E., and Tsipenyuk, E. V. | 1966 | 2.7-5.5 | 295 | Carboxyorganosilica | Powder specimen; $\theta \sim 0^\circ$. |
| 9 T51594 | Stoy, J. G. | 1961 | 2-15 | 296 | Silicone | No thickness was given; $\theta \sim 0^\circ$. |
| 10 T61459 | Williams, J. G. and Judd, J. H. | 1971 | 0.23-2.5 | 293 | Silicone 1 | 3.064 mm thick; 100 dimethyl silicone rubber RTV 615 part A and 10 RTV 615 part B; the specimen was cast, cured 2 hr at 71 C; $\theta \sim 0^\circ$. |
| 11 T61459 | Williams, J. G. and Judd, J. H. | 1971 | 0.23-2.5 | 293 | Silicone 2 | 2.976 mm thick; 100 dimethyl silicone rubber Sygard 184 part A and 10 Sygard 184 part B; the specimen was cast, cured 2 hr at 71 C; $\theta \sim 0^\circ$. |
| 12 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~ 293 | Silastic 916 (Dow Corning Co.) | The specimen was condensed pyrolyzate on potassium bromide or sodium chloride; a Beckman IR-9 double beam, prism-grating infrared spectrophotometer was used to obtain the spectra; data were extracted from figure; $\theta \sim 0^\circ$. |
| 13 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~ 293 | Silastic 6526 (Dow Corning Co.) | Similar to the above specimen. |
| 14 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~ 293 | Silicone Rubber Heat Shrinkable (Dow Corning Co.) | Similar to the above specimen. |
| 15 T76798 | Lara, M. O. | 1967 | 2.5-25 | ~ 293 | 5542 Silicone Finish Aluminum Silicone (Dutch Boy) | Similar to the above specimen. |
| 16 T45212 | Schmidt, R. N. | 1967 | 1-10 | ~ 293 | Dow Corning Silicone 991 | 0.014 in. thick (356 μ); not baked; data were extracted from figure; $\theta \sim 0^\circ$. |

TABLE 19-11. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL TRANSMITTANCE OF SILICONE RESINS (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|--|
| 17 T45212 | Schmidt, R. N. | 1967 | 1-10 | ~293 | Dow Corning Silicone 991 | Similar to the above specimen except it was baked at 600 F. |
| 18 T45212 | Schmidt, R. N. | 1967 | 1-10 | ~293 | General Electric Silicone PT | 0.003 in. thick specimen after 600 F bake; data were extracted from figure; $\theta \sim 0^\circ$. |
| 19 T45212 | Schmidt, R. N. | 1967 | 1-10 | ~293 | General Electric Silicone 120 | 0.0175 in. thick specimen after 600 F bake; data were extracted from figure; $\theta \sim 0^\circ$. |
| 20 T76812 | Kagarise, R. E. and Weinberger, L. A. | 1954 | 2-15 | ~293 | Silicone Resin 4746-26A | The specimen was obtained from Lindie Air Products; it was dissolved in C_2H_4 and the resulting viscous solution was spread uniformly on rock salt or KBr plate; the solvent was removed by heating in vacuum or normal evaporation at room temperature; a Perkin-Elmer spectrophotometer was used in measurement; data were extracted from figure; $\theta \sim 0^\circ$. |
| 21 T76812 | Kagarise, R. E. and Weinberger, L. A. | 1954 | 2-15 | ~293 | Silicone Resin 173-8-211 | Similar to the above specimen except obtained from General Electric Co. |
| 22 T76812 | Kagarise, R. E. and Weinberger, L. A. | 1954 | 2-15 | ~293 | Dow Corning 1107 | Similar to the above specimen except obtained from Dow Corning Co. |
| 23 T68915 | Jayne, G. and Trazer, G. | 1972 | 2.5-25 | ~293 | Silicone Resin | The transmittance spectra was obtained by using FMIR technique (multiple reflection); data were extracted from figure; $\theta \sim 0^\circ$. |
| 24 T68915 | Jayne, G. and Trazer, G. | 1972 | 2.5-25 | ~293 | Silicone coated paper | Similar to the above specimens. |
| 25 T77141 | Tkachuk, B. V., Perova, L. V., and Kololyskina, V. M. | 1971 | 3-12 | ~293 | HMDS film | Hexamethyldisiloxane film about 0.5-2 μm thick was prepared in a silence discharge; $\theta \sim 0^\circ$. |
| 26 T77141 | Tkachuk, B. V., et al. | 1971 | 3-12 | ~293 | HMDS film | Similar to the above specimen except it was irradiated by 400 Mrad dose γ -ray. |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| CURVE 1 | | | CURVE 2 (CONT.) | | | CURVE 2 (CONT.) | | | CURVE 2 (CONT.) | | | CURVE 3 (CONT.) | | |
|-----------|--------|-----------|-----------------|-----------|--------|-----------------|--------|-----------|-----------------|-----------|--------|-----------------|--------|--|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | |
| T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | | T = 293. | | |
| 0.300 | 0.841 | 1.827 | 0.801 | 5.16 | 0.975 | 8.17 | 0.712 | 14.07 | 0.278 | 5.10 | 0.805 | | | |
| 0.324 | 0.820 | 1.843 | 0.819 | 5.23 | 0.902 | 8.32 | 0.490 | 14.24 | 0.114 | 5.19 | 0.818 | | | |
| 0.367 | 0.860 | 1.864 | 0.836 | 5.28 | 0.940 | 8.32 | 0.442 | 14.28 | 0.082 | 5.25 | 0.793 | | | |
| 0.442 | 0.666 | 1.893 | 0.849 | 5.34 | 0.955 | 8.41 | 0.361 | 14.33 | 0.072 | 5.35 | 0.811 | | | |
| 0.480 | 0.873 | 1.926 | 0.854 | 5.44 | 0.898 | 8.54 | 0.095 | 14.41 | 0.107 | 5.47 | 0.777 | | | |
| 0.506 | 0.881 | 1.957 | 0.859 | 5.48 | 0.932 | 8.60 | 0.045 | 14.52 | 0.501 | 5.54 | 0.777 | | | |
| 0.537 | 0.890 | 2.034 | 0.859 | 5.55 | 0.945 | 8.76 | 0.07 | 14.60 | 0.568 | 5.71 | 0.718 | | | |
| 0.659 | 0.890 | 2.101 | 0.853 | 5.61 | 0.920 | 9.82 | 0.007 | 14.66 | 0.583 | 5.81 | 0.665 | | | |
| 0.819 | 0.900 | 2.147 | 0.845 | 5.73 | 0.945 | 9.93 | 0.047 | 14.80 | 0.601 | 5.97 | 0.715 | | | |
| 1.112 | 0.903 | | | 5.86 | 0.945 | 10.00 | 0.098 | 15.00 | 0.678 | 6.10 | 0.677 | | | |
| 1.126 | 0.889 | CURVE 2 | | | 6.01 | 0.916 | 10.04 | 0.243 | 6.40 | 0.768 | | | | |
| 1.136 | 0.854 | T = 293. | | | 6.09 | 0.937 | 10.11 | 0.412 | 6.49 | 0.797 | | | | |
| 1.147 | 0.834 | 2.00 | 0.977 | 6.20 | 0.900 | 10.16 | 0.527 | 6.65 | 0.737 | | | | | |
| 1.182 | 0.863 | 2.11 | 0.974 | 6.24 | 0.605 | 10.28 | 0.640 | 6.71 | 0.769 | | | | | |
| 1.225 | 0.889 | 2.21 | 0.959 | 6.27 | 0.668 | 10.38 | 0.716 | 6.80 | 0.769 | | | | | |
| 1.263 | 0.901 | 2.29 | 0.970 | 6.31 | 0.897 | 10.49 | 0.778 | 6.92 | 0.743 | | | | | |
| 1.309 | 0.901 | 2.36 | 0.970 | 6.44 | 0.923 | 10.58 | 0.791 | 6.99 | 0.291 | | | | | |
| 1.342 | 0.891 | 2.45 | 0.956 | 6.49 | 0.940 | 10.74 | 0.799 | 7.00 | 0.630 | | | | | |
| 1.378 | 0.872 | 2.53 | 0.973 | 6.60 | 0.943 | 10.86 | 0.779 | 7.10 | 0.631 | | | | | |
| 1.409 | 0.867 | 2.62 | 0.973 | 6.68 | 0.865 | 11.00 | 0.816 | 7.16 | 0.780 | | | | | |
| 1.446 | 0.882 | 2.74 | 0.933 | 6.71 | 0.917 | 11.15 | 0.816 | 7.26 | 0.723 | | | | | |
| 1.479 | 0.891 | 2.81 | 0.973 | 6.76 | 0.936 | 11.31 | 0.801 | 7.34 | 0.743 | | | | | |
| 1.610 | 0.891 | 2.95 | 0.984 | 6.89 | 0.906 | 11.47 | 0.737 | 7.42 | 0.743 | | | | | |
| 1.617 | 0.882 | 3.12 | 0.994 | 6.94 | 0.820 | 11.59 | 0.631 | 7.53 | 0.713 | | | | | |
| 1.637 | 0.710 | 3.20 | 0.949 | 6.99 | 0.291 | 11.77 | 0.482 | 7.66 | 0.674 | | | | | |
| 1.653 | 0.577 | 3.24 | 0.687 | 7.01 | 0.767 | 12.07 | 0.328 | 7.73 | 0.633 | | | | | |
| 1.665 | 0.480 | 3.27 | 0.659 | 7.08 | 0.755 | 12.23 | 0.252 | 7.81 | 0.239 | | | | | |
| 1.682 | 0.400 | 3.29 | 0.686 | 7.15 | 0.869 | 12.35 | 0.138 | 7.84 | 0.090 | | | | | |
| 1.703 | 0.350 | 3.32 | 0.710 | 7.22 | 0.899 | 12.58 | 0.069 | 7.90 | 0.121 | | | | | |
| 1.711 | 0.377 | 3.32 | 0.753 | 7.33 | 0.922 | 12.72 | 0.042 | 7.97 | 0.498 | | | | | |
| 1.739 | 0.656 | 3.32 | 0.753 | 7.40 | 0.922 | 12.93 | 0.054 | 8.05 | 0.515 | | | | | |
| 1.745 | 0.672 | 3.38 | 0.711 | 7.53 | 0.637 | 13.14 | 0.106 | 8.22 | 0.346 | | | | | |
| 1.753 | 0.663 | 3.38 | 0.844 | 7.59 | 0.847 | 13.25 | 0.162 | 8.33 | 0.187 | | | | | |
| 1.755 | 0.645 | 3.43 | 0.900 | 7.62 | 0.816 | 13.31 | 0.212 | 8.40 | 0.124 | | | | | |
| 1.762 | 0.635 | 3.51 | 0.953 | 7.70 | 0.824 | 13.38 | 0.234 | 8.51 | 0.045 | | | | | |
| 1.770 | 0.657 | 3.62 | 0.982 | 7.75 | 0.714 | 13.48 | 0.171 | 8.76 | 0.007 | | | | | |
| 1.770 | 0.702 | 4.13 | 0.994 | 7.84 | 0.090 | 13.61 | 0.677 | 9.82 | 0.007 | | | | | |
| 1.796 | 0.745 | 4.97 | 0.994 | 7.90 | 0.121 | 13.72 | 0.104 | 9.92 | 0.025 | | | | | |
| 1.809 | 0.774 | 5.05 | 0.944 | 7.99 | 0.708 | 13.76 | 0.185 | 10.02 | 0.065 | | | | | |
| | | 5.10 | 0.975 | 8.08 | 0.741 | 14.00 | 0.223 | 10.09 | 0.828 | | | | | |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ)

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| 8.98 | 0.227 | 10.97 | 0.653 | 13.39 | 0.549 | 1.192 | 0.822 | 1.692 | 0.024 | 2.163 | 0.019 | 1.702 | 0.099 |
| 9.05 | 0.233 | 11.08 | 0.670 | 13.45 | 0.514 | 1.232 | 0.822 | 1.702 | 0.099 | 2.177 | 0.038 | 1.713 | 0.178 |
| 9.18 | 0.231 | 11.19 | 0.680 | 13.53 | 0.480 | 1.211 | 0.858 | 1.713 | 0.178 | 2.187 | 0.017 | 1.726 | 0.099 |
| 9.27 | 0.231 | 11.29 | 0.685 | 13.63 | 0.518 | 1.224 | 0.876 | 1.726 | 0.099 | 2.200 | 0.013 | 1.735 | 0.375 |
| 9.36 | 0.232 | 11.39 | 0.699 | 13.69 | 0.554 | 1.254 | 0.876 | 1.735 | 0.375 | CURVE 7 | | | |
| 9.43 | 0.220 | 11.47 | 0.688 | 13.73 | 0.592 | 1.262 | 0.867 | 1.741 | 0.103 | T = 296. | | | |
| 9.49 | 0.184 | 11.52 | 0.672 | 13.79 | 0.623 | 1.271 | 0.889 | 1.753 | 0.212 | 0.286 | 0.000 | 1.776 | 0.297 |
| 9.55 | 0.155 | 11.56 | 0.649 | 13.88 | 0.642 | 1.285 | 0.875 | 1.758 | 0.254 | 0.300 | 0.038 | 1.776 | 0.365 |
| 9.59 | 0.155 | 11.58 | 0.615 | 13.96 | 0.655 | 1.306 | 0.858 | 1.776 | 0.297 | 0.320 | 0.551 | 1.793 | 0.401 |
| 9.67 | 0.172 | 11.63 | 0.584 | 13.99 | 0.655 | 1.324 | 0.858 | 1.776 | 0.297 | 0.340 | 0.681 | 1.801 | 0.396 |
| 9.70 | 0.193 | 11.65 | 0.539 | CURVE 6 | | | | 1.347 | 0.751 | 1.776 | 0.410 | 1.808 | 0.410 |
| 9.74 | 0.221 | 11.70 | 0.489 | T = 296. | | | | 1.356 | 0.719 | 1.793 | 0.401 | 1.815 | 0.397 |
| 9.77 | 0.235 | 11.76 | 0.438 | 0.278 | 0.000 | 1.368 | 0.654 | 1.808 | 0.410 | 0.352 | 0.746 | 1.808 | 0.410 |
| 9.75 | 0.256 | 11.80 | 0.372 | 0.291 | 0.493 | 1.374 | 0.601 | 1.815 | 0.397 | 0.372 | 0.782 | 1.822 | 0.359 |
| 9.80 | 0.275 | 11.84 | 0.294 | 0.302 | 0.657 | 1.382 | 0.423 | 1.822 | 0.359 | 0.392 | 0.829 | 1.832 | 0.392 |
| 9.80 | 0.306 | 11.88 | 0.232 | 0.310 | 0.723 | 1.387 | 0.380 | 1.832 | 0.392 | 0.456 | 0.847 | 1.832 | 0.392 |
| 9.91 | 0.308 | 11.89 | 0.200 | 0.329 | 0.768 | 1.397 | 0.377 | 1.837 | 0.355 | 0.552 | 0.881 | 1.837 | 0.355 |
| 9.92 | 0.308 | 11.92 | 0.180 | 0.366 | 0.794 | 1.408 | 0.377 | 1.847 | 0.469 | 0.640 | 0.897 | 1.847 | 0.469 |
| 9.92 | 0.357 | 11.96 | 0.165 | 0.440 | 0.830 | 1.426 | 0.458 | 1.869 | 0.497 | 0.737 | 0.910 | 1.869 | 0.497 |
| 9.93 | 0.390 | 12.02 | 0.181 | 0.498 | 0.852 | 1.442 | 0.528 | 1.880 | 0.473 | 0.773 | 0.919 | 1.880 | 0.473 |
| 9.96 | 0.424 | 12.09 | 0.203 | 0.629 | 0.878 | 1.470 | 0.543 | 1.889 | 0.390 | 0.843 | 0.919 | 1.889 | 0.390 |
| 9.99 | 0.443 | 12.12 | 0.238 | 0.735 | 0.895 | 1.504 | 0.528 | 1.897 | 0.304 | 0.868 | 0.897 | 1.897 | 0.304 |
| 10.09 | 0.463 | 12.15 | 0.285 | 0.843 | 0.901 | 1.525 | 0.498 | 1.904 | 0.286 | 0.886 | 0.900 | 1.904 | 0.286 |
| 10.12 | 0.507 | 12.16 | 0.314 | 0.874 | 0.877 | 1.546 | 0.527 | 1.919 | 0.370 | 0.902 | 0.884 | 1.919 | 0.370 |
| 10.14 | 0.538 | 12.16 | 0.345 | 0.901 | 0.872 | 1.562 | 0.541 | 1.935 | 0.385 | 0.924 | 0.902 | 1.935 | 0.385 |
| 10.15 | 0.570 | 12.21 | 0.367 | 0.919 | 0.894 | 1.575 | 0.541 | 1.951 | 0.389 | 0.946 | 0.904 | 1.951 | 0.389 |
| 10.20 | 0.592 | 12.21 | 0.396 | 0.938 | 0.894 | 1.586 | 0.532 | 1.961 | 0.408 | 0.961 | 0.888 | 1.961 | 0.408 |
| 10.25 | 0.616 | 12.25 | 0.416 | 0.965 | 0.882 | 1.601 | 0.525 | 1.991 | 0.392 | 1.005 | 0.895 | 1.991 | 0.392 |
| 10.30 | 0.637 | 12.29 | 0.421 | 1.016 | 0.882 | 1.614 | 0.467 | 2.003 | 0.405 | 1.025 | 0.895 | 2.003 | 0.405 |
| 10.38 | 0.649 | 12.36 | 0.415 | 1.036 | 0.893 | 1.617 | 0.407 | 2.015 | 0.378 | 1.066 | 0.912 | 2.015 | 0.378 |
| 10.56 | 0.649 | 12.41 | 0.406 | 1.109 | 0.874 | 1.615 | 0.349 | 2.034 | 0.367 | 1.096 | 0.912 | 2.034 | 0.367 |
| 10.59 | 0.643 | 12.50 | 0.422 | 1.138 | 0.862 | 1.625 | 0.319 | 2.058 | 0.300 | 1.122 | 0.856 | 2.058 | 0.300 |
| 10.63 | 0.634 | 12.57 | 0.453 | 1.158 | 0.750 | 1.632 | 0.308 | 2.078 | 0.304 | 1.139 | 0.705 | 2.078 | 0.304 |
| 10.66 | 0.648 | 12.58 | 0.496 | 1.173 | 0.573 | 1.638 | 0.326 | 2.101 | 0.282 | 1.167 | 0.653 | 2.101 | 0.282 |
| 10.70 | 0.660 | 12.68 | 0.514 | 1.182 | 0.696 | 1.642 | 0.246 | 2.109 | 0.217 | 1.182 | 0.653 | 2.109 | 0.217 |
| 10.74 | 0.674 | 12.79 | 0.515 | 1.182 | 0.696 | 1.651 | 0.261 | 2.115 | 0.223 | 1.139 | 0.672 | 2.115 | 0.223 |
| 10.79 | 0.660 | 12.91 | 0.506 | 1.173 | 0.573 | 1.662 | 0.062 | 2.136 | 0.074 | 1.153 | 0.672 | 2.136 | 0.074 |
| 10.84 | 0.645 | 13.07 | 0.531 | 1.182 | 0.696 | 1.668 | 0.012 | 2.139 | 0.026 | 1.167 | 0.653 | 2.139 | 0.026 |
| 10.88 | 0.640 | 13.30 | 0.586 | | | 1.679 | 0.012 | 2.153 | 0.000 | | | 2.153 | 0.000 |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T]

| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | |
|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|--|
| 1.177 | 0.568 | 1.793 | 0.230 | 3.52 | 0.073 | 4.86 | 0.946 | 9.83 | 0.168 | 14.87 | 0.861 | 14.98 | 0.888 | |
| 1.198 | 0.664 | 1.811 | 0.253 | 3.62 | 0.099 | 4.97 | 0.965 | 9.96 | 0.233 | CURVE 10 | | | | |
| 1.193 | 0.712 | 1.821 | 0.250 | 3.71 | 0.119 | 5.08 | 0.928 | 10.02 | 0.344 | T = 293. | | | | |
| 1.204 | 0.736 | 1.827 | 0.275 | 3.80 | 0.145 | 5.16 | 0.942 | 10.11 | 0.565 | | | | | |
| 1.229 | 0.828 | 1.837 | 0.275 | 3.88 | 0.179 | 5.25 | 0.928 | 10.20 | 0.742 | | | | | |
| 1.243 | 0.865 | 1.839 | 0.298 | 4.05 | 0.229 | 5.45 | 0.940 | 10.25 | 0.789 | | | | | |
| 1.260 | 0.882 | 1.864 | 0.350 | 4.22 | 0.288 | 5.60 | 0.940 | 10.35 | 0.848 | | | | | |
| 1.278 | 0.893 | 1.875 | 0.327 | 4.31 | 0.316 | 5.77 | 0.927 | 10.45 | 0.673 | | | | | |
| 1.297 | 0.893 | 1.887 | 0.275 | 4.45 | 0.351 | 5.97 | 0.943 | 10.69 | 0.873 | | | | | |
| 1.321 | 0.881 | 1.893 | 0.170 | 4.67 | 0.350 | 6.09 | 0.943 | 10.96 | 0.827 | | | | | |
| 1.334 | 0.845 | 1.901 | 0.156 | 4.84 | 0.330 | 6.17 | 0.924 | 11.18 | 0.827 | | | | | |
| 1.374 | 0.576 | 1.952 | 0.268 | 4.94 | 0.302 | 6.26 | 0.820 | 11.33 | 0.807 | | | | | |
| 1.375 | 0.514 | 1.979 | 0.323 | 5.05 | 0.269 | 6.33 | 0.912 | 11.47 | 0.773 | | | | | |
| 1.395 | 0.444 | 2.005 | 0.323 | 5.22 | 0.193 | 6.41 | 0.935 | 11.55 | 0.704 | | | | | |
| 1.414 | 0.413 | 2.018 | 0.293 | 5.36 | 0.206 | 6.58 | 0.945 | 11.85 | 0.576 | | | | | |
| 1.424 | 0.436 | 2.067 | 0.202 | 5.45 | 0.252 | 6.68 | 0.925 | 11.95 | 0.626 | | | | | |
| 1.440 | 0.509 | 2.108 | 0.063 | 5.57 | 0.236 | 6.79 | 0.944 | 12.09 | 0.654 | | | | | |
| 1.469 | 0.572 | 2.131 | 0.063 | 5.67 | 0.054 | 6.89 | 0.898 | 12.22 | 0.609 | | | | | |
| 1.496 | 0.604 | 2.131 | 0.024 | 5.95 | 0.035 | 6.97 | 0.797 | 12.29 | 0.512 | | | | | |
| 1.536 | 0.627 | 2.143 | 0.003 | 5.98 | 0.042 | 7.25 | 0.830 | 12.45 | 0.413 | | | | | |
| 1.566 | 0.636 | 2.157 | 0.026 | 6.25 | 0.071 | 7.36 | 0.830 | 12.55 | 0.504 | | | | | |
| 1.581 | 0.636 | 2.167 | 0.007 | | | 7.53 | 0.776 | 12.60 | 0.579 | | | | | |
| 1.605 | 0.627 | 2.185 | 0.027 | CURVE 9 | | | | 7.64 | 0.713 | 0.638 | | | | |
| 1.620 | 0.529 | 2.200 | 0.000 | T = 296. | | | | 7.75 | 0.713 | 0.689 | | | | |
| 1.631 | 0.427 | | | 2.00 | 0.942 | 7.83 | 0.639 | 13.09 | 0.699 | | | | | |
| 1.641 | 0.440 | CURVE 8 | | | | 7.95 | 0.501 | 13.28 | 0.754 | | | | | |
| 1.643 | 0.376 | 2.33 | 0.942 | 2.33 | 0.942 | 7.97 | 0.589 | 13.39 | 0.718 | | | | | |
| 1.653 | 0.262 | 2.44 | 0.922 | 2.44 | 0.922 | 7.97 | 0.788 | 13.47 | 0.667 | | | | | |
| 1.662 | 0.050 | 2.56 | 0.953 | 2.56 | 0.953 | 8.07 | 0.858 | 13.56 | 0.573 | | | | | |
| 1.672 | 0.022 | 2.66 | 0.314 | 2.67 | 0.933 | 8.17 | 0.858 | 13.78 | 0.578 | | | | | |
| 1.683 | 0.037 | 2.66 | 0.153 | 2.78 | 0.891 | 8.31 | 0.776 | 13.86 | 0.525 | | | | | |
| 1.691 | 0.032 | 2.68 | 0.159 | 3.01 | 0.934 | 8.45 | 0.702 | 13.91 | 0.471 | | | | | |
| 1.694 | 0.050 | 2.68 | 0.080 | 3.20 | 0.915 | 8.58 | 0.420 | 14.06 | 0.583 | | | | | |
| 1.704 | 0.063 | 2.70 | 0.053 | 3.25 | 0.832 | 8.70 | 0.212 | 14.15 | 0.601 | | | | | |
| 1.719 | 0.058 | 2.74 | 0.036 | 3.17 | 0.949 | 8.79 | 0.103 | 14.22 | 0.521 | | | | | |
| 1.735 | 0.058 | 2.82 | 0.021 | 3.38 | 0.894 | 9.00 | 0.103 | 14.34 | 0.339 | | | | | |
| 1.742 | 0.105 | 3.02 | 0.022 | 3.49 | 0.928 | 9.23 | 0.117 | 14.41 | 0.509 | | | | | |
| 1.759 | 0.153 | 3.17 | 0.029 | 3.70 | 0.959 | 9.39 | 0.101 | 14.47 | 0.608 | | | | | |
| 1.772 | 0.147 | 3.30 | 0.039 | 4.03 | 0.959 | 9.53 | 0.101 | 14.52 | 0.784 | | | | | |
| 1.776 | 0.183 | 3.42 | 0.052 | 4.42 | 0.954 | 9.68 | 0.130 | 14.75 | 0.861 | | | | | |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T , K; TRANSMITTANCE, τ]

| CURVE 10 (CONT.) | | | CURVE 11 (CONT.) | | | CURVE 11 (CONT.) | | | CURVE 11 (CONT.) | | | CURVE 12 (CONT.) | | |
|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|-----------|------------------|-----------|--------|------------------|--------|--|
| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | |
| 0.689 | 0.915 | 1.552 | 0.764 | 0.240 | 0.000 | 1.040 | 0.940 | 1.712 | 0.604 | 2.64 | 0.932 | 0.689 | 0.915 | |
| 0.735 | 0.910 | 1.683 | 0.205 | 0.245 | 0.013 | 1.086 | 0.935 | 1.750 | 0.098 | 2.70 | 0.932 | 0.735 | 0.910 | |
| 0.776 | 0.916 | 1.675 | 0.088 | 0.256 | 0.040 | 1.132 | 0.937 | 1.750 | 0.519 | 2.78 | 0.926 | 0.776 | 0.916 | |
| 0.822 | 0.916 | 1.687 | 0.078 | 0.256 | 0.050 | 1.146 | 0.932 | 1.762 | 0.574 | 2.93 | 0.922 | 0.822 | 0.916 | |
| 0.857 | 0.920 | 1.694 | 0.096 | 0.260 | 0.043 | 1.153 | 0.848 | 1.786 | 0.452 | 2.95 | 0.934 | 0.857 | 0.920 | |
| 0.893 | 0.921 | 1.694 | 0.551 | 0.264 | 0.043 | 1.161 | 0.860 | 1.795 | 0.841 | 2.97 | 0.916 | 0.893 | 0.921 | |
| 0.910 | 0.897 | 1.706 | 0.543 | 0.268 | 0.010 | 1.180 | 0.567 | 1.811 | 0.546 | 3.00 | 0.913 | 0.910 | 0.897 | |
| 0.920 | 0.911 | 1.714 | 0.604 | 0.275 | 0.000 | 1.191 | 0.597 | 1.811 | 0.821 | 3.03 | 0.918 | 0.920 | 0.911 | |
| 0.940 | 0.922 | 1.750 | 0.519 | 0.287 | 0.013 | 1.205 | 0.880 | 1.841 | 0.560 | 3.17 | 0.918 | 0.940 | 0.922 | |
| 0.991 | 0.928 | 1.750 | 0.098 | 0.296 | 0.039 | 1.222 | 0.890 | 1.858 | 0.858 | 3.20 | 0.908 | 0.991 | 0.928 | |
| 1.030 | 0.916 | 1.762 | 0.574 | 0.303 | 0.056 | 1.227 | 0.917 | 1.888 | 0.848 | 3.25 | 0.908 | 1.030 | 0.916 | |
| 1.054 | 0.926 | 1.786 | 0.452 | 0.310 | 0.060 | 1.247 | 0.914 | 1.914 | 0.818 | 3.27 | 0.890 | 1.054 | 0.926 | |
| 1.081 | 0.933 | 1.795 | 0.841 | 0.324 | 0.050 | 1.274 | 0.935 | 1.932 | 0.810 | 3.30 | 0.900 | 1.081 | 0.933 | |
| 1.114 | 0.933 | 1.811 | 0.821 | 0.332 | 0.050 | 1.306 | 0.918 | 1.945 | 0.771 | 3.34 | 0.877 | 1.114 | 0.933 | |
| 1.140 | 0.920 | 1.811 | 0.546 | 0.338 | 0.062 | 1.324 | 0.931 | 1.972 | 0.747 | 3.36 | 0.740 | 1.140 | 0.920 | |
| 1.146 | 0.866 | 1.841 | 0.560 | 0.347 | 0.133 | 1.340 | 0.931 | 1.986 | 0.778 | 3.37 | 0.578 | 1.146 | 0.866 | |
| 1.153 | 0.848 | 1.858 | 0.858 | 0.354 | 0.251 | 1.349 | 0.913 | 2.004 | 0.768 | 3.39 | 0.735 | 1.153 | 0.848 | |
| 1.16 | 0.860 | 1.888 | 0.848 | 0.358 | 0.323 | 1.355 | 0.870 | 2.023 | 0.806 | 3.41 | 0.850 | 1.16 | 0.860 | |
| 1.180 | 0.567 | 1.914 | 0.818 | 0.360 | 0.520 | 1.358 | 0.749 | 2.037 | 0.772 | 3.45 | 0.850 | 1.180 | 0.567 | |
| 1.191 | 0.597 | 1.932 | 0.810 | 0.360 | 0.813 | 1.390 | 0.638 | 2.084 | 0.826 | 3.45 | 0.850 | 1.191 | 0.597 | |
| 1.205 | 0.880 | 1.945 | 0.771 | 0.370 | 0.841 | 1.403 | 0.703 | 2.109 | 0.792 | 3.51 | 0.910 | 1.205 | 0.880 | |
| 1.222 | 0.890 | 1.972 | 0.747 | 0.382 | 0.855 | 1.416 | 0.703 | 2.133 | 0.575 | 3.55 | 0.926 | 1.222 | 0.890 | |
| 1.247 | 0.938 | 1.986 | 0.778 | 0.391 | 0.864 | 1.435 | 0.847 | 2.193 | 0.226 | 3.58 | 0.917 | 1.247 | 0.938 | |
| 1.262 | 0.903 | 2.004 | 0.768 | 0.404 | 0.876 | 1.449 | 0.880 | 2.208 | 0.064 | 3.61 | 0.938 | 1.262 | 0.903 | |
| 1.285 | 0.882 | 2.023 | 0.806 | 0.417 | 0.882 | 1.476 | 0.872 | 2.223 | 0.837 | 3.74 | 0.949 | 1.285 | 0.882 | |
| 1.312 | 0.891 | 2.037 | 0.772 | 0.435 | 0.890 | 1.500 | 0.672 | 2.223 | 0.014 | 3.77 | 0.933 | 1.312 | 0.891 | |
| 1.355 | 0.870 | 2.084 | 0.826 | 0.459 | 0.897 | 1.517 | 0.833 | 2.275 | 0.000 | 3.87 | 0.952 | 1.355 | 0.870 | |
| 1.358 | 0.742 | 2.105 | 0.792 | 0.484 | 0.903 | 1.542 | 0.820 | 2.323 | 0.152 | 4.02 | 0.945 | 1.358 | 0.742 | |
| 1.390 | 0.741 | 2.133 | 0.575 | 0.512 | 0.904 | 1.563 | 0.652 | 2.366 | 0.082 | 4.17 | 0.952 | 1.390 | 0.741 | |
| 1.403 | 0.630 | 2.153 | 0.614 | 0.548 | 0.906 | 1.585 | 0.808 | 2.399 | 0.034 | 4.22 | 0.939 | 1.403 | 0.630 | |
| 1.416 | 0.703 | 2.265 | 0.000 | 0.600 | 0.906 | 1.596 | 0.906 | 2.421 | 0.182 | 4.27 | 0.955 | 1.416 | 0.703 | |
| 1.435 | 0.847 | 2.296 | 0.182 | 0.647 | 0.918 | 1.611 | 0.906 | 2.438 | 0.023 | 4.32 | 0.938 | 1.435 | 0.847 | |
| 1.459 | 0.871 | 2.344 | 0.000 | 0.690 | 0.924 | 1.618 | 0.827 | 2.455 | 0.062 | 4.38 | 0.950 | 1.459 | 0.871 | |
| 1.500 | 0.957 | 2.355 | 0.082 | 0.782 | 0.924 | 1.637 | 0.772 | 2.472 | 0.087 | 4.51 | 0.950 | 1.500 | 0.957 | |
| 1.510 | 0.824 | 2.399 | 0.034 | 0.826 | 0.919 | 1.652 | 0.764 | | | 4.55 | 0.958 | 1.510 | 0.824 | |
| 1.531 | 0.814 | 2.421 | 0.182 | 0.904 | 0.925 | 1.663 | 0.205 | | | 4.63 | 0.945 | 1.531 | 0.814 | |
| 1.563 | 0.852 | 2.436 | 0.023 | 0.912 | 0.908 | 1.675 | 0.088 | | | 4.81 | 0.945 | 1.563 | 0.852 | |
| 1.585 | 0.808 | 2.455 | 0.062 | 0.938 | 0.933 | 1.687 | 0.078 | | | 5.00 | 0.954 | 1.585 | 0.808 | |
| 1.618 | 0.837 | 2.472 | 0.087 | 0.959 | 0.937 | 1.694 | 0.096 | | | 5.10 | 0.950 | 1.618 | 0.837 | |
| 1.637 | 0.772 | 1.007 | | 1.007 | 0.921 | 1.706 | 0.543 | | | 5.19 | 0.945 | 1.637 | 0.772 | |

CURVE 12
 $T = 293.$

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
[WAVELENGTH, λ, μm; TEMPERATURE, T, K; TRANSMITTANCE, T]

| CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 14 (CONT.) | | CURVE 15 (CONT.) | | CURVE 15 (CONT.) | |
|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|------------------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 3.38 | 0.455 | 5.92 | 0.908 | 9.72 | 0.162 | 22.73 | 0.748 | 4.57 | 0.973 | 8.30 | 0.838 | 4.57 | 0.973 | 8.30 | 0.838 |
| 3.40 | 0.758 | 6.05 | 0.908 | 9.80 | 0.188 | 23.42 | 0.666 | 5.00 | 0.974 | 8.41 | 0.765 | 5.00 | 0.974 | 8.41 | 0.765 |
| 3.42 | 0.704 | 6.17 | 0.888 | 10.07 | 0.567 | 23.70 | 0.599 | 5.11 | 0.945 | 8.58 | 0.708 | 5.11 | 0.945 | 8.58 | 0.708 |
| 3.45 | 0.770 | 6.20 | 0.868 | 10.31 | 0.732 | 24.21 | 0.589 | 5.19 | 0.973 | 8.70 | 0.342 | 5.19 | 0.973 | 8.70 | 0.342 |
| 3.46 | 0.834 | 6.26 | 0.809 | 10.45 | 0.756 | 25.00 | 0.595 | 5.32 | 0.950 | 8.77 | 0.232 | 5.32 | 0.950 | 8.77 | 0.232 |
| 3.47 | 0.868 | 6.29 | 0.867 | 10.65 | 0.695 | | | 5.36 | 0.970 | 8.77 | 0.176 | 5.36 | 0.970 | 8.77 | 0.176 |
| 3.50 | 0.882 | 6.37 | 0.896 | 10.79 | 0.711 | | | 5.42 | 0.970 | 8.90 | 0.156 | 5.42 | 0.970 | 8.90 | 0.156 |
| 3.54 | 0.909 | 6.52 | 0.910 | 10.94 | 0.650 | | | 5.51 | 0.939 | 8.99 | 0.171 | 5.51 | 0.939 | 8.99 | 0.171 |
| 3.57 | 0.909 | 6.63 | 0.910 | 11.12 | 0.662 | | | 5.59 | 0.963 | 9.29 | 0.140 | 5.59 | 0.963 | 9.29 | 0.140 |
| 3.61 | 0.940 | 6.67 | 0.879 | 11.30 | 0.560 | | | 5.65 | 0.944 | 9.46 | 0.156 | 5.65 | 0.944 | 9.46 | 0.156 |
| 3.65 | 0.940 | 6.76 | 0.879 | 11.75 | 0.418 | 2.49 | 0.972 | 5.69 | 0.956 | 9.61 | 0.287 | 5.69 | 0.956 | 9.61 | 0.287 |
| 3.66 | 0.931 | 6.90 | 0.812 | 11.96 | 0.342 | 2.50 | 0.972 | 5.87 | 0.971 | 9.82 | 0.203 | 5.87 | 0.971 | 9.82 | 0.203 |
| 3.71 | 0.941 | 6.93 | 0.812 | 12.14 | 0.257 | 2.79 | 0.962 | 5.93 | 0.948 | 9.96 | 0.228 | 5.93 | 0.948 | 9.96 | 0.228 |
| 3.74 | 0.921 | 6.97 | 0.695 | 12.36 | 0.148 | 2.96 | 0.950 | 6.06 | 0.938 | 10.13 | 0.601 | 6.06 | 0.938 | 10.13 | 0.601 |
| 3.78 | 0.943 | 7.01 | 0.761 | 12.56 | 0.208 | 3.06 | 0.937 | 6.13 | 0.951 | 10.24 | 0.761 | 6.13 | 0.951 | 10.24 | 0.761 |
| 4.02 | 0.943 | 7.06 | 0.715 | 12.99 | 0.567 | 3.17 | 0.921 | 6.23 | 0.926 | 10.37 | 0.819 | 6.23 | 0.926 | 10.37 | 0.819 |
| 4.16 | 0.956 | 7.13 | 0.750 | 13.21 | 0.630 | 3.19 | 0.900 | 6.28 | 0.788 | 10.66 | 0.866 | 6.28 | 0.788 | 10.66 | 0.866 |
| 4.22 | 0.922 | 7.19 | 0.813 | 13.40 | 0.623 | 3.22 | 0.915 | 6.31 | 0.910 | 10.87 | 0.877 | 6.31 | 0.910 | 10.87 | 0.877 |
| 4.24 | 0.935 | 7.24 | 0.798 | 13.62 | 0.645 | 3.25 | 0.887 | 6.39 | 0.947 | 11.26 | 0.877 | 6.39 | 0.947 | 11.26 | 0.877 |
| 4.28 | 0.925 | 7.26 | 0.837 | 13.79 | 0.595 | 3.27 | 0.741 | 6.53 | 0.957 | 11.43 | 0.851 | 6.53 | 0.957 | 11.43 | 0.851 |
| 4.33 | 0.947 | 7.43 | 0.680 | 14.01 | 0.595 | 3.28 | 0.813 | 6.70 | 0.946 | 11.72 | 0.687 | 6.70 | 0.946 | 11.72 | 0.687 |
| 4.42 | 0.942 | 7.55 | 0.651 | 14.22 | 0.500 | 3.29 | 0.762 | 6.73 | 0.697 | 11.82 | 0.655 | 6.73 | 0.697 | 11.82 | 0.655 |
| 4.46 | 0.930 | 7.68 | 0.806 | 14.45 | 0.691 | 3.30 | 0.643 | 6.73 | 0.923 | 11.57 | 0.672 | 6.73 | 0.923 | 11.57 | 0.672 |
| 4.55 | 0.944 | 7.76 | 0.752 | 14.66 | 0.734 | 3.33 | 0.810 | 6.78 | 0.933 | 12.18 | 0.656 | 6.78 | 0.933 | 12.18 | 0.656 |
| 4.59 | 0.906 | 7.84 | 0.483 | 14.97 | 0.701 | 3.36 | 0.865 | 6.86 | 0.896 | 12.42 | 0.388 | 6.86 | 0.896 | 12.42 | 0.388 |
| 4.74 | 0.935 | 7.91 | 0.195 | 15.11 | 0.758 | 3.39 | 0.700 | 6.92 | 0.911 | 12.59 | 0.404 | 6.92 | 0.911 | 12.59 | 0.404 |
| 4.98 | 0.946 | 7.99 | 0.580 | 15.36 | 0.785 | 3.41 | 0.814 | 6.96 | 0.902 | 12.72 | 0.395 | 6.96 | 0.902 | 12.72 | 0.395 |
| 5.00 | 0.947 | 8.05 | 0.768 | 15.53 | 0.751 | 3.43 | 0.747 | 7.03 | 0.518 | 12.99 | 0.502 | 7.03 | 0.518 | 12.99 | 0.502 |
| 5.07 | 0.942 | 8.17 | 0.810 | 15.65 | 0.795 | 3.47 | 0.897 | 7.03 | 0.840 | 13.40 | 0.616 | 7.03 | 0.840 | 13.40 | 0.616 |
| 5.13 | 0.920 | 8.30 | 0.810 | 16.05 | 0.803 | 3.50 | 0.887 | 7.06 | 0.861 | 13.66 | 0.444 | 7.06 | 0.861 | 13.66 | 0.444 |
| 5.26 | 0.938 | 8.42 | 0.758 | 16.29 | 0.833 | 3.51 | 0.839 | 7.14 | 0.831 | 13.85 | 0.596 | 7.14 | 0.831 | 13.85 | 0.596 |
| 5.29 | 0.928 | 8.49 | 0.717 | 16.95 | 0.816 | 3.51 | 0.836 | 7.19 | 0.883 | 14.03 | 0.662 | 7.19 | 0.883 | 14.03 | 0.662 |
| 5.32 | 0.948 | 8.66 | 0.580 | 17.33 | 0.794 | 3.53 | 0.928 | 7.33 | 0.936 | 14.35 | 0.403 | 7.33 | 0.936 | 14.35 | 0.403 |
| 5.36 | 0.955 | 8.74 | 0.356 | 17.45 | 0.911 | 3.62 | 0.951 | 7.43 | 0.946 | 14.58 | 0.822 | 7.43 | 0.946 | 14.58 | 0.822 |
| 5.42 | 0.944 | 8.80 | 0.361 | 18.94 | 0.572 | 3.78 | 0.963 | 7.76 | 0.902 | 14.99 | 0.859 | 7.76 | 0.902 | 14.99 | 0.859 |
| 5.46 | 0.926 | 8.99 | 0.213 | 19.42 | 0.602 | 4.02 | 0.972 | 7.83 | 0.833 | 15.34 | 0.897 | 7.83 | 0.833 | 15.34 | 0.897 |
| 5.62 | 0.926 | 9.07 | 0.180 | 19.96 | 0.776 | 4.25 | 0.972 | 7.87 | 0.868 | 15.67 | 0.869 | 7.87 | 0.868 | 15.67 | 0.869 |
| 5.73 | 0.900 | 9.27 | 0.163 | 20.62 | 0.767 | 4.30 | 0.950 | 7.94 | 0.885 | 16.42 | 0.887 | 7.94 | 0.885 | 16.42 | 0.887 |
| 5.80 | 0.883 | 9.50 | 0.190 | 21.01 | 0.740 | 4.40 | 0.966 | 8.05 | 0.854 | 16.98 | 0.671 | 8.05 | 0.854 | 16.98 | 0.671 |
| 5.87 | 0.887 | 9.59 | 0.173 | 21.98 | 0.797 | 4.50 | 0.966 | 8.16 | 0.884 | 17.51 | 0.890 | 8.16 | 0.884 | 17.51 | 0.890 |

CURVE 15
T = 293.

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T | λ | T | λ | T | λ | T | λ | T |
|-------------------------|-------|-----------|-------|-----------|-------|-----------|-------|-----------|-------|
| CURVE 15 (CONT.) | | | | | | | | | |
| 18.45 | 0.857 | 2.50 | 0.678 | 3.60 | 0.936 | 8.26 | 0.757 | 11.22 | 0.899 |
| 18.94 | 0.835 | 2.99 | 0.538 | 3.80 | 0.950 | 8.37 | 0.649 | 11.50 | 0.919 |
| 20.16 | 0.785 | 3.51 | 0.452 | 4.40 | 0.950 | 8.47 | 0.476 | 11.67 | 0.934 |
| 20.62 | 0.511 | 4.01 | 0.631 | 4.97 | 0.940 | 8.54 | 0.351 | 12.01 | 0.934 |
| 21.23 | 0.584 | 4.52 | 0.669 | 5.12 | 0.948 | 8.62 | 0.262 | 12.31 | 0.925 |
| 21.46 | 0.696 | 5.01 | 0.450 | 5.24 | 0.932 | 8.72 | 0.194 | 12.41 | 0.910 |
| 22.03 | 0.721 | 5.49 | 0.238 | 5.43 | 0.932 | 8.81 | 0.154 | 12.50 | 0.868 |
| 23.20 | 0.592 | 6.00 | 0.131 | 5.50 | 0.924 | 8.86 | 0.132 | 12.57 | 0.805 |
| 24.33 | 0.644 | 6.51 | 0.106 | 5.74 | 0.937 | 8.93 | 0.132 | 12.66 | 0.758 |
| 25.00 | 0.670 | 6.99 | 0.059 | 6.13 | 0.937 | 9.01 | 0.173 | 12.76 | 0.723 |
| | | 7.48 | 0.094 | 6.35 | 0.930 | 9.14 | 0.265 | 12.89 | 0.687 |
| CURVE 16 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 1.01 | 0.895 | 8.02 | 0.020 | 6.41 | 0.943 | 9.21 | 0.306 | 13.01 | 0.654 |
| 1.47 | 0.857 | 8.48 | 0.004 | 6.57 | 0.943 | 9.30 | 0.325 | 13.15 | 0.586 |
| 2.00 | 0.897 | 9.01 | 0.000 | 6.66 | 0.932 | 9.38 | 0.296 | 13.25 | 0.533 |
| 2.49 | 0.679 | 9.49 | 0.030 | 6.72 | 0.893 | 9.47 | 0.245 | 13.35 | 0.514 |
| 2.98 | 0.208 | 10.00 | 0.000 | 6.78 | 0.785 | 9.56 | 0.227 | 13.49 | 0.576 |
| 3.48 | 0.416 | | | 6.81 | 0.707 | 9.62 | 0.255 | 13.68 | 0.686 |
| 3.98 | 0.648 | | | 6.84 | 0.764 | 9.71 | 0.328 | 13.75 | 0.737 |
| 4.52 | 0.650 | | | 6.86 | 0.849 | 9.77 | 0.356 | 13.83 | 0.775 |
| 5.00 | 0.417 | | | 6.88 | 0.892 | 9.81 | 0.339 | 13.97 | 0.808 |
| 5.48 | 0.226 | | | 6.92 | 0.909 | 9.87 | 0.272 | 14.05 | 0.783 |
| 6.04 | 0.124 | | | 6.99 | 0.876 | 9.93 | 0.347 | 14.12 | 0.742 |
| 6.55 | 0.098 | | | 7.04 | 0.781 | 10.02 | 0.517 | 14.18 | 0.698 |
| 6.98 | 0.092 | | | 7.08 | 0.868 | 10.07 | 0.625 | 14.25 | 0.600 |
| 7.48 | 0.023 | | | 7.12 | 0.907 | 10.15 | 0.695 | 14.32 | 0.514 |
| 7.96 | 0.000 | | | 7.19 | 0.907 | 10.24 | 0.716 | 14.39 | 0.487 |
| 8.47 | 0.000 | | | 7.23 | 0.900 | 10.30 | 0.700 | 14.47 | 0.524 |
| 9.01 | 0.000 | | | 7.29 | 0.931 | 10.36 | 0.625 | 14.55 | 0.605 |
| 9.49 | 0.000 | | | 7.54 | 0.938 | 10.41 | 0.647 | 14.62 | 0.681 |
| 10.00 | 0.000 | | | 7.71 | 0.907 | 10.46 | 0.747 | 14.68 | 0.725 |
| | | | | 7.81 | 0.878 | 10.55 | 0.826 | 14.74 | 0.755 |
| | | | | 7.86 | 0.924 | 10.60 | 0.845 | 14.79 | 0.771 |
| | | | | 7.93 | 0.492 | 10.72 | 0.877 | 14.91 | 0.762 |
| | | | | 7.96 | 0.465 | 10.84 | 0.891 | 15.00 | 0.815 |
| | | | | 7.99 | 0.500 | 11.00 | 0.895 | | |
| | | | | 8.02 | 0.658 | 10.56 | 0.821 | CURVE 21 | |
| | | | | 8.04 | 0.693 | 10.60 | 0.851 | T = 293. | |
| | | | | 8.10 | 0.697 | 10.69 | 0.875 | | |
| | | | | 8.15 | 0.774 | 10.79 | 0.889 | 2.00 | 0.953 |
| | | | | 8.19 | 0.799 | 10.90 | 0.899 | 2.46 | 0.944 |
| | | | | | | | | | |
| CURVE 17 | | | | | | | | | |
| T = 293. | | | | | | | | | |
| 1.00 | 0.825 | 1.00 | 0.787 | 2.00 | 0.955 | 2.00 | 0.955 | | |
| 1.50 | 0.838 | 1.49 | 0.847 | 2.22 | 0.941 | 2.22 | 0.941 | | |
| 2.50 | 0.840 | 1.98 | 0.853 | 2.43 | 0.947 | 2.43 | 0.947 | | |
| | | 2.47 | 0.816 | 2.72 | 0.947 | 2.72 | 0.947 | | |
| | | 2.98 | 0.755 | 3.15 | 0.936 | 3.15 | 0.936 | | |
| | | 3.49 | 0.736 | 3.27 | 0.925 | 3.27 | 0.925 | | |
| | | 4.00 | 0.782 | 3.30 | 0.904 | 3.30 | 0.904 | | |
| | | 4.49 | 0.824 | 3.35 | 0.598 | 3.35 | 0.598 | | |
| | | 4.98 | 0.728 | 3.37 | 0.575 | 3.37 | 0.575 | | |
| | | 5.50 | 0.581 | 3.40 | 0.606 | 3.40 | 0.606 | | |
| | | 5.97 | 0.531 | 3.41 | 0.654 | 3.41 | 0.654 | | |
| | | 6.47 | 0.469 | 3.45 | 0.650 | 3.45 | 0.650 | | |
| | | 6.99 | 0.430 | 3.48 | 0.863 | 3.48 | 0.863 | | |
| | | 7.49 | 0.375 | 3.53 | 0.892 | 3.53 | 0.892 | | |
| | | 7.99 | 0.194 | 3.58 | 0.918 | 3.58 | 0.918 | | |
| | | 8.45 | 0.017 | | | | | | |
| | | 8.97 | 0.000 | | | | | | |
| | | 9.48 | 0.000 | | | | | | |
| | | 10.00 | 0.000 | | | | | | |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ | λ | τ |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| 2.54 | 0.962 | 6.28 | 0.905 | 9.53 | 0.104 | 13.05 | 0.726 | 4.42 | 0.903 | 8.19 | 0.849 | 10.02 | 0.754 |
| 2.63 | 0.962 | 6.47 | 0.960 | 9.74 | 0.116 | 13.11 | 0.766 | 4.47 | 0.863 | 8.29 | 0.831 | 10.11 | 0.782 |
| 2.68 | 0.951 | 6.62 | 0.960 | 9.86 | 0.161 | 13.17 | 0.782 | 4.50 | 0.798 | 8.38 | 0.791 | 10.21 | 0.808 |
| 2.74 | 0.898 | 6.70 | 0.927 | 9.93 | 0.315 | 13.25 | 0.782 | 4.59 | 0.324 | 8.52 | 0.686 | 10.40 | 0.808 |
| 2.84 | 0.931 | 6.78 | 0.959 | 9.97 | 0.400 | 13.33 | 0.738 | 4.61 | 0.272 | 8.67 | 0.514 | 10.52 | 0.774 |
| 2.96 | 0.938 | 6.89 | 0.943 | 10.03 | 0.332 | 13.49 | 0.738 | 4.63 | 0.320 | 8.88 | 0.256 | 10.60 | 0.721 |
| 3.04 | 0.952 | 6.93 | 0.918 | 10.07 | 0.525 | 13.61 | 0.599 | 4.66 | 0.595 | 8.96 | 0.192 | 10.72 | 0.657 |
| 3.18 | 0.952 | 6.95 | 0.564 | 10.10 | 0.638 | 13.75 | 0.599 | 4.69 | 0.844 | 9.07 | 0.154 | 10.84 | 0.468 |
| 3.21 | 0.896 | 6.98 | 0.525 | 10.19 | 0.762 | 13.81 | 0.563 | 4.72 | 0.884 | 9.17 | 0.154 | 10.88 | 0.445 |
| 3.26 | 0.820 | 6.99 | 0.787 | 10.26 | 0.806 | 13.89 | 0.503 | 4.76 | 0.913 | 9.27 | 0.182 | 10.92 | 0.460 |
| 3.29 | 0.841 | 7.02 | 0.806 | 10.34 | 0.844 | 13.93 | 0.486 | 4.80 | 0.925 | 9.49 | 0.182 | 10.96 | 0.460 |
| 3.33 | 0.901 | 7.12 | 0.819 | 10.44 | 0.872 | 14.00 | 0.544 | 4.87 | 0.925 | 9.57 | 0.209 | 11.00 | 0.424 |
| 3.37 | 0.859 | 6.66 | 0.838 | 10.50 | 0.884 | 14.06 | 0.616 | 4.92 | 0.915 | 9.64 | 0.201 | 11.02 | 0.350 |
| 3.40 | 0.930 | 7.30 | 0.851 | 10.70 | 0.884 | 14.11 | 0.630 | 4.98 | 0.930 | 9.67 | 0.334 | 11.09 | 0.260 |
| 3.45 | 0.933 | 7.40 | 0.851 | 10.75 | 0.869 | 14.16 | 0.606 | 5.05 | 0.924 | 9.72 | 0.440 | 11.15 | 0.203 |
| 3.50 | 0.957 | 7.48 | 0.832 | 10.90 | 0.855 | 14.29 | 0.385 | 5.09 | 0.870 | 9.73 | 0.529 | 11.18 | 0.179 |
| 3.55 | 0.969 | 7.58 | 0.835 | 11.00 | 0.859 | 14.34 | 0.337 | 5.11 | 0.917 | 9.86 | 0.640 | 11.24 | 0.179 |
| 3.92 | 0.977 | 7.65 | 0.819 | 11.05 | 0.862 | 14.38 | 0.389 | 5.15 | 0.930 | 9.93 | 0.692 | 11.37 | 0.225 |
| 4.48 | 0.969 | 7.72 | 0.830 | 11.21 | 0.851 | 14.45 | 0.690 | 5.28 | 0.930 | 10.02 | 0.754 | 11.42 | 0.236 |
| 4.85 | 0.955 | 7.76 | 0.812 | 11.33 | 0.833 | 14.49 | 0.760 | 5.49 | 0.915 | 10.11 | 0.782 | | |
| 4.99 | 0.961 | 7.86 | 0.551 | 11.44 | 0.808 | 14.55 | 0.820 | 5.82 | 0.915 | 10.21 | 0.808 | | |
| 5.06 | 0.935 | 7.90 | 0.510 | 11.53 | 0.757 | 14.65 | 0.853 | 6.07 | 0.900 | 10.40 | 0.808 | | |
| 5.11 | 0.935 | 7.93 | 0.537 | 11.67 | 0.654 | 14.81 | 0.887 | 6.24 | 0.914 | 10.52 | 0.774 | | |
| 5.15 | 0.952 | 7.96 | 0.722 | 11.80 | 0.570 | 15.00 | 0.907 | 6.70 | 0.914 | 10.60 | 0.721 | | |
| 5.21 | 0.953 | 7.98 | 0.854 | 11.84 | 0.550 | | | 6.92 | 0.902 | 10.66 | 0.657 | | |
| 5.27 | 0.925 | 8.03 | 0.886 | 11.91 | 0.612 | | | 7.02 | 0.874 | 10.72 | 0.550 | | |
| 5.33 | 0.950 | 8.07 | 0.897 | 12.00 | 0.673 | | | 7.09 | 0.834 | 10.76 | 0.494 | | |
| 5.39 | 0.950 | 8.15 | 0.897 | 12.05 | 0.666 | | | 7.21 | 0.891 | 10.78 | 0.468 | | |
| 5.45 | 0.925 | 8.23 | 0.869 | 12.16 | 0.666 | | | 7.48 | 0.868 | 10.84 | 0.445 | | |
| 5.51 | 0.950 | 8.30 | 0.826 | 12.23 | 0.610 | | | 7.61 | 0.878 | 10.88 | 0.445 | | |
| 5.54 | 0.950 | 8.35 | 0.753 | 12.32 | 0.502 | | | 7.75 | 0.846 | 10.92 | 0.460 | | |
| 5.61 | 0.933 | 8.38 | 0.718 | 12.42 | 0.405 | | | 7.82 | 0.794 | 10.96 | 0.460 | | |
| 5.68 | 0.951 | 8.45 | 0.689 | 12.51 | 0.492 | | | 7.87 | 0.515 | 11.00 | 0.424 | | |
| 5.91 | 0.951 | 8.51 | 0.492 | 12.60 | 0.602 | | | 7.98 | 0.368 | 11.02 | 0.350 | | |
| 6.00 | 0.936 | 8.57 | 0.337 | 12.65 | 0.641 | | | 7.92 | 0.238 | 11.09 | 0.260 | | |
| 6.04 | 0.953 | 8.66 | 0.197 | 12.70 | 0.667 | | | 7.94 | 0.392 | 11.15 | 0.203 | | |
| 6.14 | 0.947 | 8.77 | 0.070 | 12.79 | 0.680 | | | 7.98 | 0.784 | 11.18 | 0.179 | | |
| 6.20 | 0.924 | 8.86 | 0.070 | 12.86 | 0.703 | | | 8.00 | 0.766 | 11.24 | 0.179 | | |
| 6.22 | 0.896 | 8.95 | 0.088 | 12.92 | 0.703 | | | 8.03 | 0.815 | 11.37 | 0.225 | | |
| 6.24 | 0.801 | 9.36 | 0.083 | 12.98 | 0.726 | | | 8.09 | 0.849 | 11.42 | 0.236 | | |

CURVE 22
 T = 293.

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| CURVE 22 (CONT.) | | | CURVE 23 (CONT.) | | | CURVE 23 (CONT.) | | | CURVE 23 (CONT.) | | | CURVE 23 (CONT.) | | | CURVE 24 (CONT.) | | |
|------------------|-------|-----------|------------------|-----------|-------|------------------|-------|-----------|------------------|-----------|-------|------------------|----------|-----------|------------------|-----------|-------|
| λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T | λ | T |
| 11.93 | 0.162 | 2.77 | 0.691 | 5.80 | 0.929 | 8.64 | 0.738 | 15.43 | 0.314 | 3.70 | 0.837 | 15.43 | 0.314 | 3.70 | 0.837 | 15.43 | 0.314 |
| 11.93 | 0.141 | 2.81 | 0.713 | 5.92 | 0.897 | 8.69 | 0.6+3 | 15.62 | 0.257 | 3.97 | 0.906 | 15.62 | 0.257 | 3.97 | 0.906 | 15.62 | 0.257 |
| 11.98 | 0.283 | 2.84 | 0.713 | 5.97 | 0.897 | 8.73 | 0.620 | 15.82 | 0.245 | 4.15 | 0.947 | 15.82 | 0.245 | 4.15 | 0.947 | 15.82 | 0.245 |
| 12.05 | 0.453 | 2.88 | 0.767 | 6.14 | 0.919 | 8.73 | 0.587 | 16.10 | 0.271 | 4.24 | 0.955 | 16.10 | 0.271 | 4.24 | 0.955 | 16.10 | 0.271 |
| 12.12 | 0.607 | 2.93 | 0.707 | 6.11 | 0.919 | 8.87 | 0.552 | 16.58 | 0.240 | 4.30 | 0.973 | 16.58 | 0.240 | 4.30 | 0.973 | 16.58 | 0.240 |
| 12.17 | 0.656 | 3.01 | 0.732 | 6.22 | 0.900 | 9.01 | 0.500 | 16.95 | 0.207 | 4.86 | 1.000 | 16.95 | 0.207 | 4.86 | 1.000 | 16.95 | 0.207 |
| 12.24 | 0.698 | 3.07 | 0.724 | 6.29 | 0.907 | 9.12 | 0.298 | 18.55 | 0.172 | 5.06 | 0.927 | 18.55 | 0.172 | 5.06 | 0.927 | 18.55 | 0.172 |
| 12.37 | 0.731 | 3.18 | 0.749 | 6.34 | 0.924 | 9.18 | 0.207 | 18.94 | 0.140 | 5.14 | 0.933 | 18.94 | 0.140 | 5.14 | 0.933 | 18.94 | 0.140 |
| 12.52 | 0.730 | 3.23 | 0.755 | 6.40 | 0.937 | 9.27 | 0.177 | 22.32 | 0.139 | 5.17 | 0.927 | 22.32 | 0.139 | 5.17 | 0.927 | 22.32 | 0.139 |
| 12.62 | 0.690 | 3.28 | 0.755 | 6.48 | 0.937 | 9.27 | 0.140 | 22.63 | 0.132 | 5.27 | 0.939 | 22.63 | 0.132 | 5.27 | 0.939 | 22.63 | 0.132 |
| 12.67 | 0.664 | 3.32 | 0.746 | 6.57 | 0.922 | 9.40 | 0.121 | 25.00 | 0.126 | 5.24 | 0.946 | 25.00 | 0.126 | 5.24 | 0.946 | 25.00 | 0.126 |
| 12.73 | 0.682 | 3.36 | 0.684 | 6.65 | 0.902 | 9.55 | 0.118 | CURVE 24 | | | 5.38 | 1.883 | CURVE 24 | | | | |
| 12.81 | 0.492 | 3.39 | 0.568 | 6.71 | 0.902 | 9.67 | 0.095 | T = 293. | | | 5.41 | 0.843 | T = 293. | | | | |
| 12.92 | 0.333 | 3.40 | 0.652 | 6.79 | 0.911 | 9.81 | 0.088 | | | | 5.44 | 0.959 | | | | | |
| 12.97 | 0.294 | 3.43 | 0.641 | 6.85 | 0.911 | 9.92 | 0.067 | | | | 5.52 | 0.856 | | | | | |
| 13.02 | 0.294 | 3.45 | 0.690 | 6.96 | 0.899 | 10.07 | 0.045 | | | | 5.58 | 0.978 | | | | | |
| 13.14 | 0.390 | 3.47 | 0.715 | 7.08 | 0.876 | 10.18 | 0.060 | | | | 5.64 | 0.961 | | | | | |
| 13.25 | 0.495 | 3.51 | 0.706 | 7.16 | 0.885 | 10.45 | 0.309 | | | | 5.67 | 0.975 | | | | | |
| 13.34 | 0.614 | 3.53 | 0.735 | 7.25 | 0.903 | 10.67 | 0.499 | | | | 5.71 | 0.947 | | | | | |
| 13.48 | 0.746 | 3.59 | 0.787 | 7.32 | 0.873 | 10.87 | 0.584 | | | | 5.74 | 0.979 | | | | | |
| 13.57 | 0.804 | 3.65 | 0.811 | 7.40 | 0.897 | 11.06 | 0.596 | | | | 5.76 | 0.952 | | | | | |
| 13.71 | 0.804 | 3.70 | 0.828 | 7.46 | 0.876 | 11.35 | 0.600 | | | | 5.83 | 0.919 | | | | | |
| 13.89 | 0.804 | 3.78 | 0.822 | 7.53 | 0.876 | 11.53 | 0.627 | | | | 5.86 | 0.971 | | | | | |
| 14.04 | 0.902 | 3.9+ | 0.860 | 7.58 | 0.863 | 11.64 | 0.614 | | | | 5.88 | 0.944 | | | | | |
| 14.49 | 0.974 | 4.36 | 0.645 | 7.66 | 0.872 | 11.75 | 0.505 | | | | 5.91 | 0.971 | | | | | |
| 14.86 | 0.932 | 4.03 | 0.645 | 7.72 | 0.863 | 11.88 | 0.436 | | | | 5.95 | 0.954 | | | | | |
| 15.00 | 0.946 | 4.27 | 0.833 | 7.82 | 0.860 | 12.03 | 0.509 | | | | 5.97 | 0.954 | | | | | |
| CURVE 23 | | | 4.39 | 0.833 | 7.88 | 0.873 | 0.496 | | | | 6.00 | 0.963 | | | | | |
| T = 293. | | | 4.53 | 0.276 | 7.97 | 0.623 | 0.252 | | | | 6.02 | 0.916 | | | | | |
| | | | 4.65 | 0.862 | 7.99 | 0.552 | 3.06 | | | | 6.03 | 0.930 | | | | | |
| | | | 5.00 | 0.877 | 8.05 | 0.241 | 3.13 | | | | 6.05 | 0.856 | | | | | |
| | | | 5.17 | 0.680 | 8.08 | 0.206 | 3.26 | | | | 6.11 | 0.939 | | | | | |
| 2.50 | 0.673 | 5.17 | 0.890 | 8.10 | 0.247 | 13.07 | 0.085 | | | | 6.12 | 0.882 | | | | | |
| 2.54 | 0.532 | 5.31 | 0.637 | 8.14 | 0.637 | 13.18 | 0.240 | | | | 6.15 | 0.910 | | | | | |
| 2.57 | 0.593 | 5.44 | 0.768 | 8.16 | 0.768 | 13.37 | 0.396 | | | | 6.18 | 0.895 | | | | | |
| 2.60 | 0.677 | 5.50 | 0.938 | 8.24 | 0.835 | 13.62 | 0.409 | | | | 6.22 | 0.913 | | | | | |
| 2.62 | 0.677 | 5.50 | 0.938 | 8.24 | 0.835 | 13.79 | 0.453 | | | | 6.22 | 0.895 | | | | | |
| 2.63 | 0.698 | 5.54 | 0.938 | 8.31 | 0.852 | 14.03 | 0.470 | | | | 6.22 | 0.895 | | | | | |
| 2.66 | 0.703 | 5.65 | 0.911 | 8.39 | 0.842 | 14.35 | 0.446 | | | | 6.24 | 0.919 | | | | | |
| 2.69 | 0.709 | 5.69 | 0.911 | 8.42 | 0.809 | 14.66 | 0.365 | | | | 6.24 | 0.892 | | | | | |
| 2.74 | 0.691 | 5.73 | 0.929 | 8.55 | 0.795 | 15.04 | 0.338 | | | | 6.26 | 0.921 | | | | | |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, τ]

| λ | τ | λ | τ | λ | τ | λ | τ |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| 6.34 | 0.921 | 7.81 | 0.684 | 11.90 | 0.481 | 7.60 | 0.948 |
| 6.36 | 0.940 | 7.87 | 0.699 | 12.05 | 0.506 | 7.70 | 0.914 |
| 6.41 | 0.949 | 7.93 | 0.885 | 12.14 | 0.497 | 7.78 | 0.990 |
| 6.44 | 0.926 | 7.99 | 0.842 | 12.22 | 0.497 | 7.84 | 0.442 |
| 6.45 | 0.950 | 8.06 | 0.322 | 12.36 | 0.486 | 7.89 | 0.527 |
| 6.49 | 0.940 | 8.08 | 0.250 | 12.48 | 0.216 | 7.99 | 0.802 |
| 6.51 | 0.960 | 8.13 | 0.385 | 12.67 | 0.141 | 8.07 | 0.837 |
| 6.54 | 0.929 | 8.17 | 0.719 | 12.82 | 0.085 | 8.18 | 0.860 |
| 6.56 | 0.974 | 8.22 | 0.743 | 12.94 | 0.070 | 8.33 | 0.840 |
| 6.60 | 0.939 | 8.28 | 0.822 | 13.05 | 0.155 | 8.58 | 0.670 |
| 6.64 | 0.981 | 8.35 | 0.570 | 13.16 | 0.282 | 9.43 | 0.147 |
| 6.67 | 0.957 | 8.48 | 0.605 | 13.40 | 0.394 | 9.54 | 0.133 |
| 6.69 | 0.980 | 8.62 | 0.785 | 13.64 | 0.404 | 9.73 | 0.200 |
| 6.76 | 0.986 | 8.70 | 0.758 | 13.85 | 0.448 | 10.47 | 0.526 |
| 6.82 | 0.983 | 8.79 | 0.583 | 14.03 | 0.463 | 10.68 | 0.657 |
| 6.85 | 0.993 | 8.92 | 0.550 | 14.27 | 0.444 | 10.93 | 0.638 |
| 6.89 | 0.974 | 9.06 | 0.444 | 14.60 | 0.360 | 11.26 | 0.648 |
| 6.91 | 0.923 | 9.12 | 0.292 | 14.90 | 0.324 | 11.53 | 0.454 |
| 6.93 | 0.942 | 9.25 | 0.196 | 15.29 | 0.306 | 11.71 | 0.484 |
| 6.93 | 0.918 | 9.25 | 0.156 | 15.60 | 0.242 | 11.98 | 0.570 |
| 6.99 | 0.896 | 9.40 | 0.115 | 15.97 | 0.263 | 12.22 | 0.537 |
| 7.01 | 0.915 | 9.56 | 0.115 | 16.26 | 0.251 | 12.41 | 0.477 |
| 7.04 | 0.997 | 9.68 | 0.090 | 17.12 | 0.186 | 12.64 | 0.526 |
| 7.07 | 0.916 | 9.89 | 0.078 | 18.02 | 0.170 | 14.10 | 0.973 |
| 7.08 | 0.880 | 10.03 | 0.053 | 18.45 | 0.152 | CURVE 26 | |
| 7.13 | 0.903 | 10.19 | 0.068 | 18.90 | 0.124 | T = 293. | |
| 7.19 | 0.950 | 10.27 | 0.151 | 19.34 | 0.136 | 2.84 | 0.746 |
| 7.23 | 0.985 | 10.26 | 0.190 | 19.88 | 0.129 | 2.87 | 0.690 |
| 7.27 | 0.876 | 10.43 | 0.249 | 20.49 | 0.137 | 2.89 | 0.655 |
| 7.31 | 0.915 | 10.49 | 0.336 | 21.19 | 0.131 | 2.91 | 0.657 |
| 7.39 | 0.956 | 10.62 | 0.376 | 21.55 | 0.138 | 2.96 | 0.558 |
| 7.41 | 0.964 | 10.71 | 0.477 | 22.08 | 0.139 | 3.15 | 0.849 |
| 7.44 | 0.676 | 10.79 | 0.532 | 22.88 | 0.118 | 3.30 | 0.528 |
| 7.45 | 0.890 | 11.11 | 0.596 | 23.87 | 0.090 | 3.35 | 0.906 |
| 7.50 | 0.874 | 11.27 | 0.569 | 23.67 | 0.075 | 3.36 | 0.880 |
| 7.52 | 0.891 | 11.35 | 0.529 | 25.00 | 0.072 | 3.39 | 0.823 |
| 7.59 | 0.901 | 11.56 | 0.601 | | | 3.40 | 0.858 |
| 7.63 | 0.875 | 11.57 | 0.622 | | | | |
| 7.69 | 0.979 | 11.71 | 0.582 | | | | |
| 7.73 | 0.963 | 11.81 | 0.501 | | | | |

TABLE 19-12. EXPERIMENTAL NORMAL SPECTRAL TRANSMITTANCE OF SILICON RESIN (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; TRANSMITTANCE, T)

| λ | T |
|------------------|-------|
| CURVE 26 (CONT.) | |
| 12.95 | 0.611 |
| 13.04 | 0.710 |
| 13.44 | 0.815 |
| 14.20 | 1.000 |

4.20. Aluminized Grafoil

Aluminized grafoil is made by applying thin coatings of aluminum on grafoil, a pure flexible, insulating graphite tape with highly directional properties similar to those of pyrolytic graphite.

The grafoil adds the advantage of flexibility to the thermal-insulating properties of pyrolytic graphite from the cryogenic range up to about 4000 K. Preliminary values of the ratio of the thermal conductivity perpendicular to the surface plane to that along the surface range between 0.001 to 0.006, depending upon the type of grafoil tape measured. There is no increase in thermal conductivity at high temperatures as found in conventional insulation materials. Grafoil tape and foil are normally produced in the 1.0 to 1.3 g cm⁻³ density range. It can be embossed, wrapped, rolled, pressed or otherwise formed.

Aluminized grafoil was made primarily for the purpose of providing a high-reflectivity, low thermal-conductivity material for cryogenic applications. However, advantages of this material made it a favorable material in the area of aircraft design and space vehicle construction where heat insulation plays an important role.

Experimental data on the thermal radiative properties of aluminized grafoil were not found in our literature search. This discouraging fact does not prevent us from making a reasonable estimation for the radiative properties because the thin coatings of aluminum are usually thick enough to be opaque to the radiation and are therefore considered as the sole material interacting with the incident radiation. Therefore, the generation of the most probable values on the thermal radiative properties of aluminized grafoil is based on the available data of aluminum.

Literature survey for aluminum revealed an adequate amount of data on the normal spectral emittance, reflectance and absorptance. Measurement information and experimental results obtained in this survey are given in Tables 20-1 to 20-10 and Figures 20-1 to 20-5. By careful review of the tables and figures, one will see that the magnitudes of the thermal radiative properties are very much affected by the surface conditions of the specimens. The literature abounds with examples of test surfaces shown to be very sensitive to methods of preparation, thermal history, and environmental conditions. Despite this awareness, descriptions of test surfaces are generally inadequate because of our modest understanding of the mechanisms or real surface effects and how to properly characterize a surface.

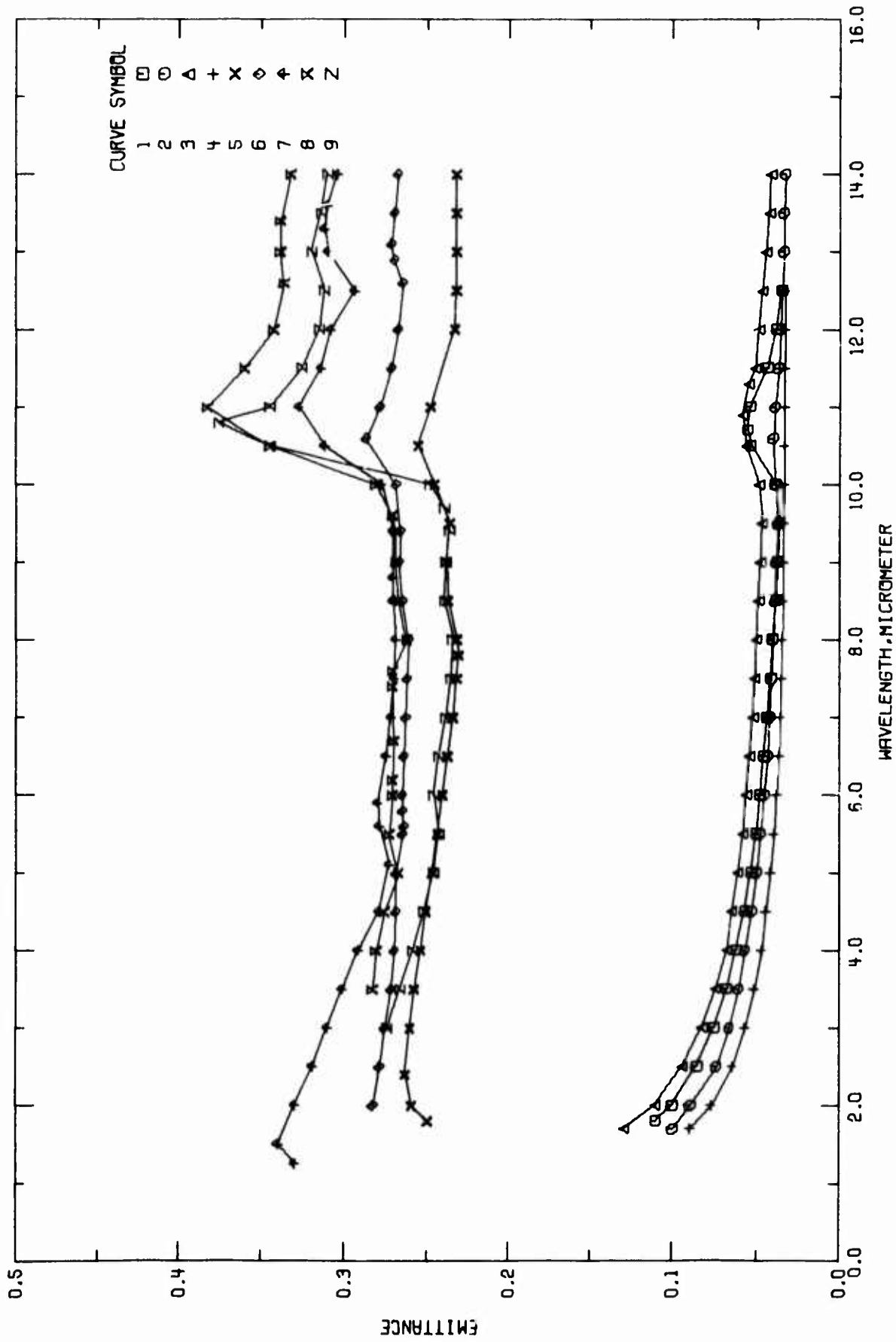


FIGURE 20-1. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE).

TABLE 20-1. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-----------------------|------|---------------------------------|----------------------|-------------------------------|--|
| 1 | T11723 Reynolds, P.M. | 1961 | 1.8-12.5 | 599 | | 99.7 Al, 0.11 Fe, 0.11 Si, 0.01 Cu, 0.01 Mg, <0.01 Mn, Ni and Zn; cylindrical tube; heated at 467 K for 15 hr; polished with Carumi on Selvylt cloth; surface roughness 0.076 μm (center line average); data extracted from smooth curve; reported error $\pm 20\%$. The above specimen and conditions except heated at 697 K for 20 hr before measurement. |
| 2 | T11723 Reynolds, P.M. | 1961 | 1.7-14.0 | 697 | | |
| 3 | T11723 Reynolds, P.M. | 1961 | 1.7-14.0 | 805 | | The above specimen and conditions except heated at 805 K for 15 hr before measurement. |
| 4 | T11723 Reynolds, P.M. | 1961 | 1.7-12.5 | 599 | | The above specimen and conditions. |
| 5 | T11723 Reynolds, P.M. | 1961 | 1.8-14.5 | 462 | | 99.7 Al, 0.11 Fe, 0.11 Si, 0.01 Cu, 0.01 Mg, <0.01 Mn, Ni and Zn; tube; heated for 25 hr at 462 K; roughened and knurled with grade 180 silicon carbide paper; surface roughness 2.92 μm (center line average); data extracted from a smooth curve; error given over the wavelength range 2 to 10 μm , reported error $\pm 10\%$. The above specimen and conditions except heated at 598 K for 22 hr before measurement. |
| 6 | T11723 Reynolds, P.M. | 1961 | 2.0-14.0 | 599 | | |
| 7 | T11723 Reynolds, P.M. | 1961 | 1.25-14.5 | 715 | | The above specimen and conditions except heated at 715 K for 27 hr before measurement. |
| 8 | T11723 Reynolds, P.M. | 1961 | 3.5-14.5 | 803 | | The above specimen and conditions except heated at 787 K for 17 hr before measurement. |
| 9 | T11723 Reynolds, P.M. | 1961 | 3.0-14.0 | 461 | | The above specimen and conditions. |

TABLE 20-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|----------------|------------|-----------|------------|----------------|------------|-----------|------------|----------------|------------|----------------|------------|-----------|------------|
| CURVE 1 | | | | | | | | | | | | | |
| T = 599. | | | | | | | | | | | | | |
| 1.8 | 0.110 | 7.0 | 0.043 | 11.5 | 0.051 | 3.0 | 0.261 | 7.0 | 0.264 | 11.0 | 0.324 | 11.0 | 0.324 |
| 2.0 | 0.100 | 7.5 | 0.042 | 12.0 | 0.049 | 3.5 | 0.258 | 7.0 | 0.263 | 11.5 | 0.314 | 11.5 | 0.314 |
| 2.5 | 0.089 | 8.0 | 0.041 | 12.5 | 0.047 | 4.0 | 0.254 | 7.5 | 0.258 | 12.0 | 0.308 | 12.0 | 0.308 |
| 3.0 | 0.078 | 8.5 | 0.040 | 13.0 | 0.045 | 4.5 | 0.251 | 8.0 | 0.262 | 12.5 | 0.294 | 12.5 | 0.294 |
| 3.5 | 0.068 | 9.0 | 0.039 | 13.5 | 0.043 | 5.0 | 0.247 | 8.5 | 0.263 | 13.0 | 0.280 | 13.0 | 0.280 |
| 4.0 | 0.058 | 9.5 | 0.038 | 14.0 | 0.042 | 5.5 | 0.244 | 9.0 | 0.267 | 13.5 | 0.270 | 13.5 | 0.270 |
| 4.5 | 0.057 | 10.0 | 0.039 | CURVE 4 | | | | | | | | | |
| 5.0 | 0.053 | 10.5 | 0.041 | T = 599. | | | | | | | | | |
| 5.5 | 0.050 | 11.0 | 0.040 | 1.7 | 0.090 | 7.8 | 0.233 | 11.5 | 0.273 | 14.5 | 0.301 | 14.5 | 0.301 |
| 6.0 | 0.048 | 11.5 | 0.038 | 2.0 | 0.076 | 8.0 | 0.233 | 12.0 | 0.269 | CURVE 8 | | | |
| 6.5 | 0.045 | 12.0 | 0.037 | 2.5 | 0.063 | 8.5 | 0.233 | 12.5 | 0.258 | T = 803. | | | |
| 7.0 | 0.044 | 12.5 | 0.035 | 3.0 | 0.050 | 9.0 | 0.234 | 13.0 | 0.271 | 3.5 | 0.264 | 3.5 | 0.264 |
| 7.5 | 0.042 | 13.0 | 0.035 | 3.5 | 0.038 | 9.5 | 0.237 | 13.5 | 0.273 | 4.0 | 0.267 | 4.0 | 0.267 |
| 8.0 | 0.041 | 13.5 | 0.034 | 4.0 | 0.025 | 10.0 | 0.246 | 14.0 | 0.269 | 4.5 | 0.271 | 4.5 | 0.271 |
| 8.5 | 0.039 | 14.0 | 0.034 | 4.5 | 0.046 | 10.5 | 0.256 | CURVE 7 | | | | | |
| 9.0 | 0.038 | T = 805. | | | | | | | | | | | |
| 9.5 | 0.037 | 1.7 | 0.130 | 12.0 | 0.248 | 10.5 | 0.256 | T = 715. | | | | | |
| 10.0 | 0.036 | 2.0 | 0.110 | 12.5 | 0.234 | 11.0 | 0.234 | 1.2E | 0.330 | 9.4 | 0.270 | 9.4 | 0.270 |
| 10.5 | 0.034 | 2.5 | 0.094 | 13.0 | 0.232 | 11.5 | 0.233 | 1.5 | 0.340 | 9.6 | 0.260 | 9.6 | 0.260 |
| 11.0 | 0.034 | 3.0 | 0.083 | 13.5 | 0.233 | 12.0 | 0.233 | 2.0 | 0.333 | 10.0 | 0.274 | 10.0 | 0.274 |
| 11.5 | 0.034 | 3.5 | 0.075 | 14.0 | 0.233 | 12.5 | 0.233 | 2.5 | 0.319 | 10.5 | 0.280 | 10.5 | 0.280 |
| 12.0 | 0.033 | 4.0 | 0.068 | 14.5 | 0.231 | 13.0 | 0.233 | 3.0 | 0.310 | 11.0 | 0.261 | 11.0 | 0.261 |
| 12.5 | 0.030 | 4.5 | 0.065 | CURVE 6 | | | | | | | | | |
| T = 697. | | | | | | | | | | | | | |
| 1.7 | 0.100 | 5.0 | 0.051 | 2.0 | 0.284 | 13.5 | 0.233 | 4.0 | 0.292 | 11.5 | 0.276 | 11.5 | 0.276 |
| 2.0 | 0.090 | 5.5 | 0.058 | 2.5 | 0.280 | 14.0 | 0.231 | 4.5 | 0.280 | 12.0 | 0.273 | 12.0 | 0.273 |
| 2.5 | 0.075 | 6.0 | 0.052 | 3.0 | 0.277 | 14.5 | 0.265 | 5.0 | 0.274 | 12.5 | 0.271 | 12.5 | 0.271 |
| 3.0 | 0.067 | 6.5 | 0.054 | 3.5 | 0.273 | 15.0 | 0.266 | 5.5 | 0.270 | 13.0 | 0.270 | 13.0 | 0.270 |
| 3.5 | 0.061 | 7.0 | 0.051 | 4.0 | 0.271 | 15.5 | 0.266 | 6.0 | 0.270 | 13.5 | 0.272 | 13.5 | 0.272 |
| 4.0 | 0.057 | 7.5 | 0.050 | 4.5 | 0.270 | 16.0 | 0.266 | 6.5 | 0.270 | 14.0 | 0.272 | 14.0 | 0.272 |
| 4.5 | 0.057 | 8.0 | 0.048 | 5.0 | 0.270 | 16.5 | 0.265 | 7.0 | 0.273 | 14.5 | 0.272 | 14.5 | 0.272 |
| 5.0 | 0.057 | 8.5 | 0.048 | 5.5 | 0.270 | 17.0 | 0.265 | 7.5 | 0.271 | 15.0 | 0.272 | 15.0 | 0.272 |
| 5.5 | 0.057 | 9.0 | 0.047 | 6.0 | 0.270 | 17.5 | 0.265 | 8.0 | 0.271 | 15.5 | 0.272 | 15.5 | 0.272 |
| 6.0 | 0.057 | 9.5 | 0.049 | 6.5 | 0.270 | 18.0 | 0.265 | 8.5 | 0.271 | 16.0 | 0.272 | 16.0 | 0.272 |
| 6.5 | 0.057 | 10.0 | 0.049 | 7.0 | 0.270 | 18.5 | 0.265 | 9.0 | 0.271 | 16.5 | 0.272 | 16.5 | 0.272 |
| 7.0 | 0.053 | 10.5 | 0.057 | 7.5 | 0.270 | 19.0 | 0.265 | 9.5 | 0.271 | 17.0 | 0.272 | 17.0 | 0.272 |
| 7.5 | 0.053 | 11.0 | 0.059 | 8.0 | 0.270 | 19.5 | 0.265 | 10.0 | 0.271 | 17.5 | 0.272 | 17.5 | 0.272 |
| 8.0 | 0.050 | 11.5 | 0.059 | 8.5 | 0.270 | 20.0 | 0.265 | 10.5 | 0.271 | 18.0 | 0.272 | 18.0 | 0.272 |
| 8.5 | 0.048 | 12.0 | 0.059 | 9.0 | 0.270 | 20.5 | 0.265 | 11.0 | 0.271 | 18.5 | 0.272 | 18.5 | 0.272 |
| 9.0 | 0.047 | 12.5 | 0.055 | 9.5 | 0.270 | 21.0 | 0.265 | 11.5 | 0.271 | 19.0 | 0.272 | 19.0 | 0.272 |
| 9.5 | 0.046 | 13.0 | 0.055 | 10.0 | 0.270 | 21.5 | 0.265 | 12.0 | 0.271 | 19.5 | 0.272 | 19.5 | 0.272 |
| 10.0 | 0.046 | 13.5 | 0.055 | 10.5 | 0.270 | 22.0 | 0.265 | 12.5 | 0.271 | 20.0 | 0.272 | 20.0 | 0.272 |
| 10.5 | 0.046 | 14.0 | 0.055 | 11.0 | 0.270 | 22.5 | 0.265 | 13.0 | 0.271 | 20.5 | 0.272 | 20.5 | 0.272 |
| 11.0 | 0.046 | 14.5 | 0.055 | 11.5 | 0.270 | 23.0 | 0.265 | 13.5 | 0.271 | 21.0 | 0.272 | 21.0 | 0.272 |
| 11.5 | 0.046 | 15.0 | 0.055 | 12.0 | 0.270 | 23.5 | 0.265 | 14.0 | 0.271 | 21.5 | 0.272 | 21.5 | 0.272 |
| 12.0 | 0.046 | 15.5 | 0.055 | 12.5 | 0.270 | 24.0 | 0.265 | 14.5 | 0.271 | 22.0 | 0.272 | 22.0 | 0.272 |
| 12.5 | 0.046 | 16.0 | 0.055 | 13.0 | 0.270 | 24.5 | 0.265 | 15.0 | 0.271 | 22.5 | 0.272 | 22.5 | 0.272 |
| 13.0 | 0.046 | 16.5 | 0.055 | 13.5 | 0.270 | 25.0 | 0.265 | 15.5 | 0.271 | 23.0 | 0.272 | 23.0 | 0.272 |
| 13.5 | 0.046 | 17.0 | 0.055 | 14.0 | 0.270 | 25.5 | 0.265 | 16.0 | 0.271 | 23.5 | 0.272 | 23.5 | 0.272 |
| 14.0 | 0.046 | 17.5 | 0.055 | 14.5 | 0.270 | 26.0 | 0.265 | 16.5 | 0.271 | 24.0 | 0.272 | 24.0 | 0.272 |
| 14.5 | 0.046 | 18.0 | 0.055 | 15.0 | 0.270 | 26.5 | 0.265 | 17.0 | 0.271 | 24.5 | 0.272 | 24.5 | 0.272 |
| 15.0 | 0.046 | 18.5 | 0.055 | 15.5 | 0.270 | 27.0 | 0.265 | 17.5 | 0.271 | 25.0 | 0.272 | 25.0 | 0.272 |
| 15.5 | 0.046 | 19.0 | 0.055 | 16.0 | 0.270 | 27.5 | 0.265 | 18.0 | 0.271 | 25.5 | 0.272 | 25.5 | 0.272 |
| 16.0 | 0.046 | 19.5 | 0.055 | 16.5 | 0.270 | 28.0 | 0.265 | 18.5 | 0.271 | 26.0 | 0.272 | 26.0 | 0.272 |
| 16.5 | 0.046 | 20.0 | 0.055 | 17.0 | 0.270 | 28.5 | 0.265 | 19.0 | 0.271 | 26.5 | 0.272 | 26.5 | 0.272 |
| 17.0 | 0.046 | 20.5 | 0.055 | 17.5 | 0.270 | 29.0 | 0.265 | 19.5 | 0.271 | 27.0 | 0.272 | 27.0 | 0.272 |
| 17.5 | 0.046 | 21.0 | 0.055 | 18.0 | 0.270 | 29.5 | 0.265 | 20.0 | 0.271 | 27.5 | 0.272 | 27.5 | 0.272 |
| 18.0 | 0.046 | 21.5 | 0.055 | 18.5 | 0.270 | 30.0 | 0.265 | 20.5 | 0.271 | 28.0 | 0.272 | 28.0 | 0.272 |
| 18.5 | 0.046 | 22.0 | 0.055 | 19.0 | 0.270 | 30.5 | 0.265 | 21.0 | 0.271 | 28.5 | 0.272 | 28.5 | 0.272 |
| 19.0 | 0.046 | 22.5 | 0.055 | 19.5 | 0.270 | 31.0 | 0.265 | 21.5 | 0.271 | 29.0 | 0.272 | 29.0 | 0.272 |
| 19.5 | 0.046 | 23.0 | 0.055 | 20.0 | 0.270 | 31.5 | 0.265 | 22.0 | 0.271 | 29.5 | 0.272 | 29.5 | 0.272 |
| 20.0 | 0.046 | 23.5 | 0.055 | 20.5 | 0.270 | 32.0 | 0.265 | 22.5 | 0.271 | 30.0 | 0.272 | 30.0 | 0.272 |
| 20.5 | 0.046 | 24.0 | 0.055 | 21.0 | 0.270 | 32.5 | 0.265 | 23.0 | 0.271 | 30.5 | 0.272 | 30.5 | 0.272 |
| 21.0 | 0.046 | 24.5 | 0.055 | 21.5 | 0.270 | 33.0 | 0.265 | 23.5 | 0.271 | 31.0 | 0.272 | 31.0 | 0.272 |
| 21.5 | 0.046 | 25.0 | 0.055 | 22.0 | 0.270 | 33.5 | 0.265 | 24.0 | 0.271 | 31.5 | 0.272 | 31.5 | 0.272 |
| 22.0 | 0.046 | 25.5 | 0.055 | 22.5 | 0.270 | 34.0 | 0.265 | 24.5 | 0.271 | 32.0 | 0.272 | 32.0 | 0.272 |
| 22.5 | 0.046 | 26.0 | 0.055 | 23.0 | 0.270 | 34.5 | 0.265 | 25.0 | 0.271 | 32.5 | 0.272 | 32.5 | 0.272 |
| 23.0 | 0.046 | 26.5 | 0.055 | 23.5 | 0.270 | 35.0 | 0.265 | 25.5 | 0.271 | 33.0 | 0.272 | 33.0 | 0.272 |
| 23.5 | 0.046 | 27.0 | 0.055 | 24.0 | 0.270 | 35.5 | 0.265 | 26.0 | 0.271 | 33.5 | 0.272 | 33.5 | 0.272 |
| 24.0 | 0.046 | 27.5 | 0.055 | 24.5 | 0.270 | 36.0 | 0.265 | 26.5 | 0.271 | 34.0 | 0.272 | 34.0 | 0.272 |
| 24.5 | 0.046 | 28.0 | 0.055 | 25.0 | 0.270 | 36.5 | 0.265 | 27.0 | 0.271 | 34.5 | 0.272 | 34.5 | 0.272 |
| 25.0 | 0.046 | 28.5 | 0.055 | 25.5 | 0.270 | 37.0 | 0.265 | 27.5 | 0.271 | 35.0 | 0.272 | 35.0 | 0.272 |
| 25.5 | 0.046 | 29.0 | 0.055 | 26.0 | 0.270 | 37.5 | 0.265 | 28.0 | 0.271 | 35.5 | 0.272 | 35.5 | 0.272 |
| 26.0 | 0.046 | 29.5 | 0.055 | 26.5 | 0.270 | 38.0 | 0.265 | 28.5 | 0.271 | 36.0 | 0.272 | 36.0 | 0.272 |
| 26.5 | 0.046 | 30.0 | 0.055 | 27.0 | 0.270 | 38.5 | 0.265 | 29.0 | 0.271 | 36.5 | 0.272 | 36.5 | 0.272 |
| 27.0 | 0.046 | 30.5 | 0.055 | 27.5 | 0.270 | 39.0 | 0.265 | 29.5 | 0.271 | 37.0 | 0.272 | 37.0 | 0.272 |
| 27.5 | 0.046 | 31.0 | 0.055 | 28.0 | 0.270 | 39.5 | 0.265 | 30.0 | 0.271 | 37.5 | 0.272 | 37.5 | 0.272 |
| 28.0 | 0.046 | 31.5 | 0.055 | 28.5 | 0.270 | 40.0 | 0.265 | 30.5 | 0.271 | 38.0 | 0.272 | 38.0 | 0.272 |
| 28.5 | 0.046 | 32.0 | 0.055 | 29.0 | 0.270 | 40.5 | 0.265 | 31.0 | 0.271 | 38.5 | 0.272 | 38.5 | 0.272 |
| 29.0 | 0.046 | 32.5 | 0.055 | 29.5 | 0.270 | 41.0 | 0.265 | 31.5 | 0.271 | 39.0 | 0.272 | 39.0 | 0.272 |
| 29.5 | 0.046 | 33.0 | 0.055 | 30.0 | 0.270 | 41.5 | 0.265 | 32.0 | 0.271 | 39.5 | 0.272 | 39.5 | 0.272 |
| 30.0 | 0.046 | 33.5 | 0.055 | 30.5 | 0.270 | 42.0 | 0.265 | 32.5 | 0.271 | 40.0 | 0.272 | 40.0 | 0.272 |
| 30.5 | 0.046 | 34.0 | 0.055 | 31.0 | 0.270 | 42.5 | 0.265 | 33.0 | 0.271 | 40.5 | 0.272 | 40.5 | 0.272 |
| 31.0 | 0.046 | 34.5 | 0.055 | 31.5 | 0.270 | 43.0 | 0.265 | 33.5 | 0.271 | 41.0 | 0.272 | 41.0 | 0.272 |
| 31.5 | 0.046 | 35.0 | 0.055 | 32.0 | 0.270 | 43.5 | 0.265 | 34.0 | 0.271 | 41.5 | 0.272 | 41.5 | 0.272 |
| 32.0 | 0.046 | 35.5 | 0.055 | 32.5 | 0.270 | 44.0 | 0.265 | 34.5 | 0.271 | 42.0 | 0.272 | 42.0 | 0.272 |
| 32.5 | 0.046 | 36.0 | 0.055 | 33.0 | 0.270 | 44.5 | 0.265 | 35.0 | 0.271 | 42.5 | 0.272 | 42.5 | 0.272 |
| 33.0 | 0.046 | 36.5 | 0.055 | 33.5 | 0.270 | 45.0 | 0.265 | 35.5 | 0.271 | 43.0 | 0.272 | 43.0 | 0.272 |
| 33.5 | 0.046 | 37.0 | 0.055 | 34.0 | 0.270 | 45.5 | 0.265 | 36.0 | 0.271 | 43.5 | 0.272 | 43.5 | 0.272 |
| 34.0 | 0.046 | 37.5 | 0.055 | 34.5 | 0.270 | 46.0 | 0.265 | 36.5 | 0.271 | 44.0 | | | |

TABLE 20-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) (CONTINUED)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ |
|-----------|------------|
| CURVE 9 | |
| T = 465. | |
| 3.0 | 0.275 |
| 3.5 | 0.267 |
| 4.0 | 0.255 |
| 4.5 | 0.252 |
| 5.0 | 0.246 |
| 5.5 | 0.243 |
| 6.0 | 0.246 |
| 6.5 | 0.253 |
| 7.0 | 0.259 |
| 7.5 | 0.236 |
| 8.0 | 0.235 |
| 8.5 | 0.243 |
| 9.0 | 0.239 |
| 9.4 | 0.237 |
| 9.7 | 0.243 |
| 10.0 | 0.249 |
| 10.5 | 0.345 |
| 10.8 | 0.377 |
| 11.0 | 0.345 |
| 11.5 | 0.320 |
| 12.0 | 0.313 |
| 12.5 | 0.312 |
| 13.0 | 0.322 |
| 13.5 | 0.314 |
| 14.0 | 0.316 |

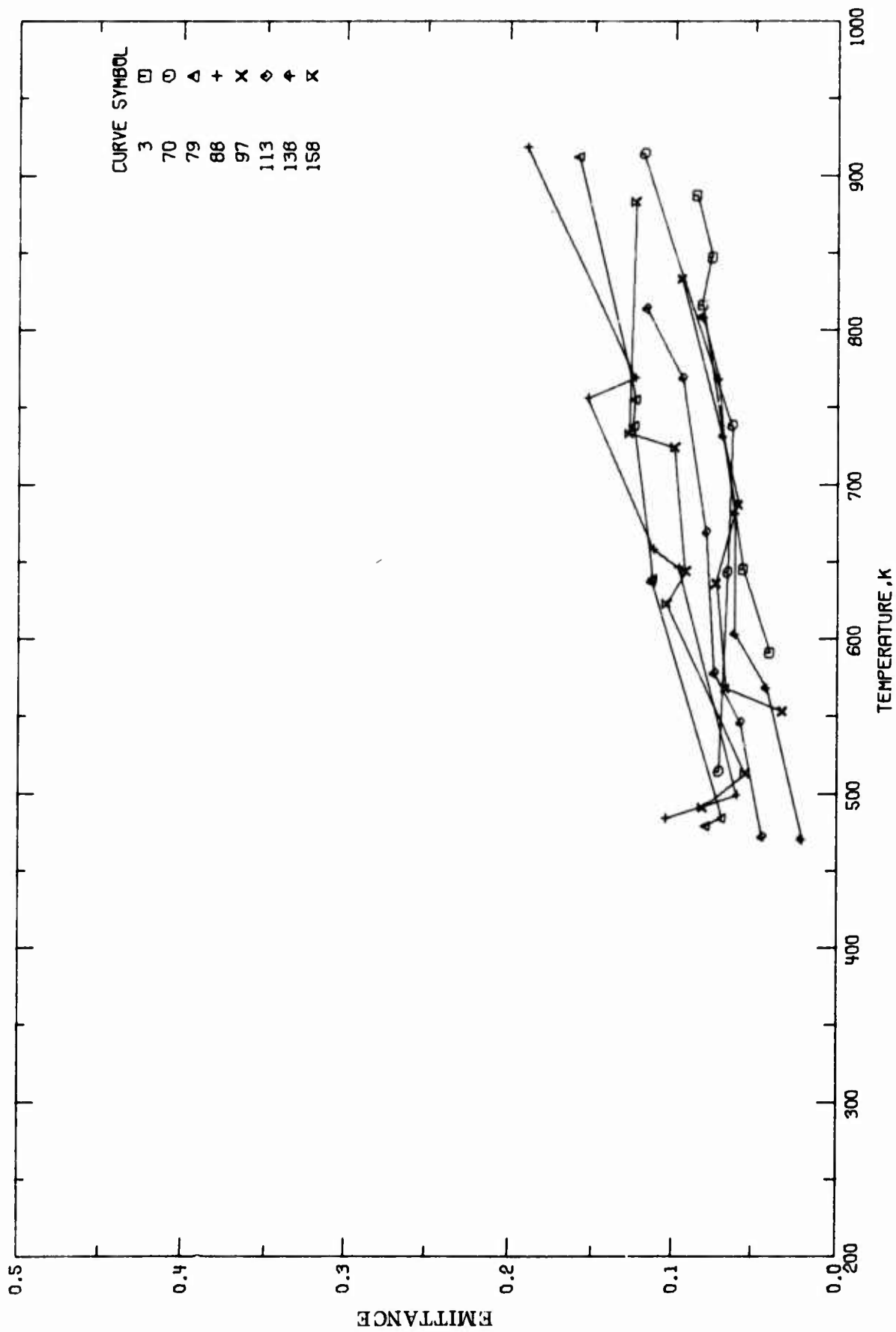


FIGURE 20-2. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM
(TEMPERATURE DEPENDENCE).

TABLE 20-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T53964 | Curcio, J. V. | 1968 | 2.0 | 591-887 | No. 1 | 99.992 Al, 0.005 Cu, 0.002 Fe, and 0.001 Si; supplied by Alcoa, made from a semi-circular disk about 1.25 in. in diameter and 0.375 in. thick; polished with various grades of emery paper, abraded with 400 aluminum for 30 min. and with 600 aluminum for 40 min, then oxidized in air at 811 K; reported error 3-6%. |
| 2 T53964 | Curcio, J. V. | 1968 | 2.5 | 591-887 | No. 1 | The above specimen. |
| 3 T53964 | Curcio, J. V. | 1965 | 3.0 | 591-887 | No. 1 | The above specimen. |
| 4 T53964 | Curcio, J. V. | 1968 | 3.5 | 591-887 | No. 1 | The above specimen. |
| 5 T53964 | Curcio, J. V. | 1968 | 4.0 | 591-887 | No. 1 | The above specimen. |
| 6 T53964 | Curcio, J. V. | 1968 | 4.5 | 591-887 | No. 1 | The above specimen. |
| 7 T53964 | Curcio, J. V. | 1968 | 5.0 | 591-887 | No. 1 | The above specimen. |
| 8 T53964 | Curcio, J. V. | 1968 | 5.5 | 591-887 | No. 1 | The above specimen. |
| 9 T53964 | Curcio, J. V. | 1968 | 6.0 | 591-887 | No. 1 | The above specimen. |
| 10 T53964 | Curcio, J. V. | 1968 | 6.5 | 591-887 | No. 1 | The above specimen. |
| 11 T53964 | Curcio, J. V. | 1968 | 7.0 | 645-887 | No. 1 | The above specimen. |
| 12 T53964 | Curcio, J. V. | 1968 | 7.5 | 645-887 | No. 1 | The above specimen. |
| 13 T53964 | Curcio, J. V. | 1968 | 8.0 | 645-887 | No. 1 | The above specimen. |
| 14 T53964 | Curcio, J. V. | 1968 | 8.5 | 645-887 | No. 1 | The above specimen. |
| 15 T53964 | Curcio, J. V. | 1968 | 9.0 | 645-887 | No. 1 | The above specimen. |
| 16 T53964 | Curcio, J. V. | 1968 | 9.5 | 316-887 | No. 1 | The above specimen. |
| 17 T53964 | Curcio, J. V. | 1968 | 10.0 | 816-887 | No. 1 | The above specimen. |
| 18 T53964 | Curcio, J. V. | 1968 | 10.5 | 816-887 | No. 1 | The above specimen. |
| 19 T53964 | Curcio, J. V. | 1968 | 11.0 | 816-887 | No. 1 | The above specimen. |
| 20 T53964 | Curcio, J. V. | 1968 | 11.5 | 816-887 | No. 1 | The above specimen. |
| 21 T53964 | Curcio, J. V. | 1968 | 12.0 | 816-887 | No. 1 | The above specimen. |
| 22 T53964 | Curcio, J. V. | 1968 | 12.5 | 815-887 | No. 1 | The above specimen. |
| 23 T53964 | Curcio, J. V. | 1968 | 13.0 | 816-887 | No. 1 | The above specimen. |
| 24 T53964 | Curcio, J. V. | 1968 | 13.5 | 816-887 | No. 1 | The above specimen. |
| 25 T53964 | Curcio, J. V. | 1968 | 14.0 | 816, 887 | No. 1 | The above specimen. |
| 26 T53964 | Curcio, J. V. | 1968 | 2.0 | 502-888 | No. 2 | Cut from a disk of the same batch as the above specimen; as received; reported error 3-5%. |
| 27 T53964 | Curcio, J. V. | 1968 | 2.5 | 502-888 | No. 2 | The above specimen. |
| 28 T53964 | Curcio, J. V. | 1968 | 3.0 | 502-888 | No. 2 | The above specimen. |
| 29 T53964 | Curcio, J. V. | 1968 | 3.5 | 502-888 | No. 2 | The above specimen. |
| 30 T53964 | Curcio, J. V. | 1968 | 4.0 | 502-888 | No. 2 | The above specimen. |
| 31 T53964 | Curcio, J. V. | 1968 | 4.5 | 502-888 | No. 2 | The above specimen. |

TABLE 20-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Temperature Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks | |
|---------------|-----------|---------------|---------------------------------|----------------------|-------------------------------|---|--|
| 32 | T53964 | Curcio, J. V. | 1968 | 5.0 | 502-888 | No. 2 | The above specimen. |
| 33 | T53964 | Curcio, J. V. | 1968 | 5.5 | 502-888 | No. 2 | The above specimen. |
| 34 | T53964 | Curcio, J. V. | 1968 | 6.0 | 502-888 | No. 2 | The above specimen. |
| 35 | T53964 | Curcio, J. V. | 1968 | 6.5 | 502-888 | No. 2 | The above specimen. |
| 36 | T53964 | Curcio, J. V. | 1968 | 7.0 | 502-888 | No. 2 | The above specimen. |
| 37 | T53964 | Curcio, J. V. | 1968 | 7.5 | 502-888 | No. 2 | The above specimen. |
| 38 | T53964 | Curcio, J. V. | 1968 | 8.0 | 502-888 | No. 2 | The above specimen. |
| 39 | T53964 | Curcio, J. V. | 1968 | 8.5 | 502-888 | No. 2 | The above specimen. |
| 40 | T53964 | Curcio, J. V. | 1968 | 9.0 | 502-888 | No. 2 | The above specimen. |
| 41 | T53964 | Curcio, J. V. | 1968 | 9.5 | 502-888 | No. 2 | The above specimen. |
| 42 | T53964 | Curcio, J. V. | 1968 | 10.0 | 502-888 | No. 2 | The above specimen. |
| 43 | T53964 | Curcio, J. V. | 1968 | 2.0 | 617-877 | No. 3 | Similar to the above specimen; polished with various grades of emery paper; reported error 3-5%. |
| 44 | T53964 | Curcio, J. V. | 1968 | 2.5 | 483-877 | No. 3 | The above specimen. |
| 45 | T53964 | Curcio, J. V. | 1968 | 3.0 | 399-877 | No. 3 | The above specimen. |
| 46 | T53964 | Curcio, J. V. | 1968 | 3.5 | 399-877 | No. 3 | The above specimen. |
| 47 | T53964 | Curcio, J. V. | 1968 | 4.0 | 399-877 | No. 3 | The above specimen. |
| 48 | T53964 | Curcio, J. V. | 1968 | 4.5 | 399-877 | No. 3 | The above specimen. |
| 49 | T53964 | Curcio, J. V. | 1968 | 5.0 | 399-877 | No. 3 | The above specimen. |
| 50 | T53964 | Curcio, J. V. | 1968 | 5.5 | 399-877 | No. 3 | The above specimen. |
| 51 | T53964 | Curcio, J. V. | 1968 | 6.0 | 399-877 | No. 3 | The above specimen. |
| 52 | T53964 | Curcio, J. V. | 1968 | 6.5 | 399-877 | No. 3 | The above specimen. |
| 53 | T53964 | Curcio, J. V. | 1968 | 7.0 | 399-877 | No. 3 | The above specimen. |
| 54 | T53964 | Curcio, J. V. | 1968 | 7.5 | 399-877 | No. 3 | The above specimen. |
| 55 | T53964 | Curcio, J. V. | 1968 | 8.0 | 399-877 | No. 3 | The above specimen. |
| 56 | T53964 | Curcio, J. V. | 1968 | 8.5 | 399-877 | No. 3 | The above specimen. |
| 57 | T53964 | Curcio, J. V. | 1968 | 9.0 | 399-877 | No. 3 | The above specimen. |
| 58 | T53964 | Curcio, J. V. | 1968 | 9.5 | 399-877 | No. 3 | The above specimen. |
| 59 | T53964 | Curcio, J. V. | 1968 | 10.0 | 399-877 | No. 3 | The above specimen. |
| 60 | T53964 | Curcio, J. V. | 1968 | 10.5 | 399-877 | No. 3 | The above specimen. |
| 61 | T53964 | Curcio, J. V. | 1968 | 11.0 | 399-877 | No. 3 | The above specimen. |
| 62 | T53964 | Curcio, J. V. | 1968 | 11.5 | 399-877 | No. 3 | The above specimen. |
| 63 | T53964 | Curcio, J. V. | 1968 | 12.0 | 399-877 | No. 3 | The above specimen. |
| 64 | T53964 | Curcio, J. V. | 1968 | 12.5 | 399-877 | No. 3 | The above specimen. |

TABLE 20-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Temperature Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 65 | T53964 Curcio, J. V. | 1968 | 13.0 | 399-877 | No. 3 | The above specimen. |
| 66 | T53964 Curcio, J. V. | 1968 | 13.5 | 399-877 | No. 3 | The above specimen. |
| 67 | T53964 Curcio, J. V. | 1968 | 14.0 | 399-877 | No. 3 | The above specimen. |
| 68 | T53964 Curcio, J. V. | 1968 | 2.0 | 643-914 | No. 4 | Similar to the above specimen; polished with various grades of emery paper and abraded with 400 aluminum for 5 min; reported error 3-8%. |
| 69 | T53964 Curcio, J. V. | 1968 | 2.5 | 514-914 | No. 4 | The above specimen. |
| 70 | T53964 Curcio, J. V. | 1968 | 3.0 | 514-914 | No. 4 | The above specimen. |
| 71 | T53964 Curcio, J. V. | 1968 | 3.5 | 514-914 | No. 4 | The above specimen. |
| 72 | T53964 Curcio, J. V. | 1968 | 4.0 | 514-914 | No. 4 | The above specimen. |
| 73 | T53964 Curcio, J. V. | 1968 | 4.5 | 514-914 | No. 4 | The above specimen. |
| 74 | T53964 Curcio, J. V. | 1968 | 5.0 | 514-914 | No. 4 | The above specimen. |
| 75 | T53964 Curcio, J. V. | 1968 | 5.5 | 643-914 | No. 4 | The above specimen. |
| 76 | T53964 Curcio, J. V. | 1968 | 6.0 | 643-914 | No. 4 | The above specimen. |
| 77 | T53964 Curcio, J. V. | 1968 | 2.0 | 637-912 | No. 5 | Similar to the above specimen; polished with various grades of emery paper and abraded with 400 aluminum for 1 hr; reported error 3-8%. |
| 78 | T53964 Curcio, J. V. | 1968 | 2.5 | 484-912 | No. 5 | The above specimen. |
| 79 | T53964 Curcio, J. V. | 1968 | 3.0 | 479-912 | No. 5 | The above specimen. |
| 80 | T53964 Curcio, J. V. | 1968 | 3.5 | 479-912 | No. 5 | The above specimen. |
| 81 | T53964 Curcio, J. V. | 1968 | 4.0 | 479-912 | No. 5 | The above specimen. |
| 82 | T53964 Curcio, J. V. | 1968 | 4.5 | 479-912 | No. 5 | The above specimen. |
| 83 | T53964 Curcio, J. V. | 1968 | 5.0 | 479-912 | No. 5 | The above specimen. |
| 84 | T53964 Curcio, J. V. | 1968 | 5.5 | 479-912 | No. 5 | The above specimen. |
| 85 | T53964 Curcio, J. V. | 1968 | 6.0 | 479-912 | No. 5 | The above specimen. |
| 86 | T53964 Curcio, J. V. | 1968 | 2.0 | 646-918 | No. 6 | Similar to the above specimen; polished with various grades of emery paper, abraded with 400 aluminum for 1 hr and with 600 aluminum for 5 min; reported error 3-8%. |
| 87 | T53964 Curcio, J. V. | 1968 | 2.5 | 484-918 | No. 6 | The above specimen. |
| 88 | T53964 Curcio, J. V. | 1968 | 3.0 | 484-918 | No. 6 | The above specimen. |
| 89 | T53964 Curcio, J. V. | 1968 | 3.5 | 484-918 | No. 6 | The above specimen. |
| 90 | T53964 Curcio, J. V. | 1968 | 4.0 | 484-918 | No. 6 | The above specimen. |
| 91 | T53964 Curcio, J. V. | 1968 | 4.5 | 484-918 | No. 6 | The above specimen. |
| 92 | T53964 Curcio, J. V. | 1968 | 5.0 | 646-918 | No. 6 | The above specimen. |
| 93 | T53964 Curcio, J. V. | 1968 | 5.5 | 646-918 | No. 6 | The above specimen. |
| 94 | T53964 Curcio, J. V. | 1968 | 6.0 | 646-918 | No. 6 | The above specimen. |
| 95 | T53964 Curcio, J. V. | 1968 | 2.0 | 568-833 | No. 7 | Similar to the above specimen; polished with various grades of emery paper, abraded with 400 aluminum for 30 min and with 600 aluminum for 15 min; reported error 3-8%. |

TABLE 20-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Temperature Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|----------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 96 | T53964 Curcio, J. V. | 1968 | 2.5 | 568-833 | No. 7 | The above specimen. |
| 97 | T53964 Curcio, J. V. | 1968 | 3.0 | 553-833 | No. 7 | The above specimen. |
| 98 | T53964 Curcio, J. V. | 1968 | 3.5 | 553-833 | No. 7 | The above specimen. |
| 99 | T53964 Curcio, J. V. | 1968 | 4.0 | 553-833 | No. 7 | The above specimen. |
| 100 | T53964 Curcio, J. V. | 1968 | 4.5 | 553-833 | No. 7 | The above specimen. |
| 101 | T53964 Curcio, J. V. | 1968 | 5.0 | 553-833 | No. 7 | The above specimen. |
| 102 | T53964 Curcio, J. V. | 1968 | 5.5 | 553-833 | No. 7 | The above specimen. |
| 103 | T53964 Curcio, J. V. | 1968 | 6.0 | 553-833 | No. 7 | The above specimen. |
| 104 | T53964 Curcio, J. V. | 1968 | 6.5 | 636-833 | No. 7 | The above specimen. |
| 105 | T53964 Curcio, J. V. | 1968 | 7.0 | 687, 833 | No. 7 | The above specimen. |
| 106 | T53964 Curcio, J. V. | 1968 | 7.5 | 687, 833 | No. 7 | The above specimen. |
| 107 | T53964 Curcio, J. V. | 1968 | 8.0 | 687, 833 | No. 7 | The above specimen. |
| 108 | T53964 Curcio, J. V. | 1968 | 8.5 | 687, 833 | No. 7 | The above specimen. |
| 109 | T53964 Curcio, J. V. | 1968 | 9.0 | 687, 833 | No. 7 | The above specimen. |
| 110 | T53964 Curcio, J. V. | 1968 | 9.5 | 833 | No. 7 | The above specimen. |
| 111 | T53964 Curcio, J. V. | 1968 | 2.0 | 546-814 | No. 8 | Similar to the above specimen; polished with various grades of emery paper, abraded with 400 aluminum for 30 min and with 600 aluminum for 30 min; reported error 3-6%. |
| 112 | T53964 Curcio, J. V. | 1968 | 2.5 | 472-814 | No. 8 | The above specimen. |
| 113 | T53964 Curcio, J. V. | 1968 | 3.0 | 472-814 | No. 8 | The above specimen. |
| 114 | T53964 Curcio, J. V. | 1968 | 3.5 | 472-814 | No. 8 | The above specimen. |
| 115 | T53964 Curcio, J. V. | 1968 | 4.0 | 472-814 | No. 8 | The above specimen. |
| 116 | T53964 Curcio, J. V. | 1968 | 4.5 | 472-814 | No. 8 | The above specimen. |
| 117 | T53964 Curcio, J. V. | 1968 | 5.0 | 472-814 | No. 8 | The above specimen. |
| 118 | T53964 Curcio, J. V. | 1968 | 5.5 | 472-814 | No. 8 | The above specimen. |
| 119 | T53964 Curcio, J. V. | 1968 | 6.0 | 472-814 | No. 8 | The above specimen. |
| 120 | T53964 Curcio, J. V. | 1968 | 6.5 | 472-814 | No. 8 | The above specimen. |
| 121 | T53964 Curcio, J. V. | 1968 | 7.0 | 546-814 | No. 8 | The above specimen. |
| 122 | T53964 Curcio, J. V. | 1968 | 7.5 | 546-814 | No. 8 | The above specimen. |
| 123 | T53964 Curcio, J. V. | 1968 | 8.0 | 578-814 | No. 8 | The above specimen. |
| 124 | T53964 Curcio, J. V. | 1968 | 8.5 | 578-814 | No. 8 | The above specimen. |
| 125 | T53964 Curcio, J. V. | 1968 | 9.0 | 669-814 | No. 8 | The above specimen. |
| 126 | T53964 Curcio, J. V. | 1968 | 9.5 | 669-814 | No. 8 | The above specimen. |
| 127 | T53964 Curcio, J. V. | 1968 | 10.0 | 769, 814 | No. 8 | The above specimen. |
| 128 | T53964 Curcio, J. V. | 1968 | 10.5 | 769, 814 | No. 8 | The above specimen. |

TABLE 20-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Temperature Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------|------|---------------------------------|----------------------|-------------------------------|---|
| 129 T53964 | Curcio, J. V. | 1968 | 11.0 | 769, 814 | No. 8 | The above specimen. |
| 130 T53964 | Curcio, J. V. | 1968 | 11.5 | 769, 814 | No. 8 | The above specimen. |
| 131 T53964 | Curcio, J. V. | 1968 | 12.0 | 769, 814 | No. 8 | The above specimen. |
| 132 T53964 | Curcio, J. V. | 1968 | 12.5 | 769, 814 | No. 8 | The above specimen. |
| 133 T53964 | Curcio, J. V. | 1968 | 13.0 | 769, 814 | No. 8 | The above specimen. |
| 134 T53964 | Curcio, J. V. | 1968 | 13.5 | 769, 814 | No. 8 | The above specimen. |
| 135 T53964 | Curcio, J. V. | 1968 | 14.0 | 769, 814 | No. 8 | The above specimen. |
| 136 T53964 | Curcio, J. V. | 1968 | 2.0 | 603-808 | No. 9 | Similar to the above specimen; polished with various grades of emery paper, abraded with 400 aluminum for 30 min and with 600 aluminum for 30 min; reported error 3-8%. |
| 137 T53964 | Curcio, J. V. | 1968 | 2.5 | 568-808 | No. 9 | The above specimen. |
| 138 T53964 | Curcio, J. V. | 1968 | 3.0 | 470-808 | No. 9 | The above specimen. |
| 139 T53964 | Curcio, J. V. | 1968 | 3.5 | 470-808 | No. 9 | The above specimen. |
| 140 T53964 | Curcio, J. V. | 1968 | 4.0 | 470-808 | No. 9 | The above specimen. |
| 141 T53964 | Curcio, J. V. | 1968 | 4.5 | 470-808 | No. 9 | The above specimen. |
| 142 T53964 | Curcio, J. V. | 1968 | 5.0 | 470-808 | No. 9 | The above specimen. |
| 143 T53964 | Curcio, J. V. | 1968 | 5.5 | 470-808 | No. 9 | The above specimen. |
| 144 T53964 | Curcio, J. V. | 1968 | 6.0 | 568-808 | No. 9 | The above specimen. |
| 145 T53964 | Curcio, J. V. | 1968 | 6.5 | 568-808 | No. 9 | The above specimen. |
| 146 T53964 | Curcio, J. V. | 1968 | 7.0 | 568-808 | No. 9 | The above specimen. |
| 147 T53964 | Curcio, J. V. | 1968 | 7.5 | 568-808 | No. 9 | The above specimen. |
| 148 T53964 | Curcio, J. V. | 1968 | 8.0 | 603-808 | No. 9 | The above specimen. |
| 149 T53964 | Curcio, J. V. | 1968 | 8.5 | 603-808 | No. 9 | The above specimen. |
| 150 T53964 | Curcio, J. V. | 1968 | 9.0 | 681-808 | No. 9 | The above specimen. |
| 151 T53964 | Curcio, J. V. | 1968 | 9.5 | 681-768 | No. 9 | The above specimen. |
| 152 T53964 | Curcio, J. V. | 1968 | 10.0 | 681-768 | No. 9 | The above specimen. |
| 153 T53964 | Curcio, J. V. | 1968 | 10.5 | 581, 768 | No. 9 | The above specimen. |
| 154 T53964 | Curcio, J. V. | 1968 | 11.0 | 681, 768 | No. 9 | The above specimen. |
| 155 T53964 | Curcio, J. V. | 1968 | 11.5 | 681, 768 | No. 9 | The above specimen. |
| 156 T53964 | Curcio, J. V. | 1968 | 2.0 | 623-883 | No. 10 | Similar to the above specimen; polished with various grades of emery paper, and abraded with 400 aluminum for 1 hr and with 600 aluminum for 1 hr; reported error 3-8%. |
| 157 T53964 | Curcio, J. V. | 1968 | 2.5 | 491-883 | No. 10 | The above specimen. |
| 158 T53964 | Curcio, J. V. | 1968 | 3.0 | 491-883 | No. 10 | The above specimen. |
| 159 T53964 | Curcio, J. V. | 1968 | 3.5 | 491-883 | No. 10 | The above specimen. |
| 160 T53964 | Curcio, J. V. | 1968 | 4.0 | 491-883 | No. 10 | The above specimen. |

TABLE 20-3. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL EMITTANCE OF ALUMINUM (Temperature Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------|------|---------------------------------|----------------------|-------------------------------|---|
| 161 T53964 | Curcio, J. V. | 1968 | 4.5 | 513-883 | No. 10 | The above specimen. |
| 162 T53964 | Curcio, J. V. | 1968 | 5.0 | 513-883 | No. 10 | The above specimen. |
| 163 T53964 | Curcio, J. V. | 1968 | 5.5 | 623-883 | No. 10 | The above specimen. |
| 164 T53964 | Curcio, J. V. | 1968 | 6.0 | 623-883 | No. 10 | The above specimen. |
| 165 T53964 | Curcio, J. V. | 1968 | 6.5 | 644, 883 | No. 10 | The above specimen. |
| 166 T53964 | Curcio, J. V. | 1968 | 7.0 | 644, 883 | No. 10 | The above specimen. |
| 167 T53964 | Curcio, J. V. | 1968 | 7.5 | 644, 883 | No. 10 | The above specimen. |
| 168 T53964 | Curcio, J. V. | 1968 | 8.0 | 644, 883 | No. 10 | The above specimen. |

TABLE 20-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|-----------------------------|------------|------------------------------|------------|-------------------------------|------------|------|------------|-------------------------------|------------|-------------------------------|------------|------------------------------|------------|
| CURVE 1* $\lambda = 2.0$ | | | | | | | | | | | | | |
| 591. | 0.050 | 847. | 0.070 | CURVE 10* $\lambda = 6.5$ | | 591. | 0.005 | 645. | 0.037 | CURVE 21* $\lambda = 12.0$ | | 744. | 0.535 |
| 645. | 0.059 | 857. | 0.057 | | | 645. | 0.025 | 816. | 0.100 | | | 828. | 0.597 |
| 816. | 0.100 | CURVE 6* $\lambda = 4.5$ | | | | 816. | 0.080 | 847. | 0.040 | | | CURVE 27* $\lambda = 2.5$ | |
| 847. | 0.090 | 591. | 0.049 | | | 847. | 0.107 | 887. | 0.115 | | | 502. | 0.535 |
| 887. | 0.086 | 887. | 0.097 | CURVE 16* $\lambda = 9.5$ | | 887. | 0.097 | CURVE 22* $\lambda = 12.5$ | | 502. | 0.535 | 581. | 0.540 |
| CURVE 2* $\lambda = 2.5$ | | | | | | | | | | | | | |
| 591. | 0.047 | CURVE 11* $\lambda = 7.0$ | | | | 591. | 0.023 | 816. | 0.093 | 581. | 0.561 | 596. | 0.555 |
| 645. | 0.050 | 645. | 0.057 | | | 645. | 0.087 | 847. | 0.036 | 596. | 0.555 | 700. | 0.547 |
| 816. | 0.067 | 847. | 0.068 | | | 847. | 0.107 | CURVE 23* $\lambda = 13.0$ | | 744. | 0.522 | 886. | 0.602 |
| 847. | 0.097 | CURVE 7* $\lambda = 5.0$ | | | | 887. | 0.046 | 816. | 0.100 | CURVE 28* $\lambda = 3.0$ | | 502. | 0.535 |
| 887. | 0.085 | 591. | 0.099 | | | 816. | 0.093 | 847. | 0.020 | 502. | 0.535 | 511. | 0.521 |
| CURVE 3 $\lambda = 3.0$ | | | | | | | | | | | | | |
| 591. | 0.043 | CURVE 12* $\lambda = 7.5$ | | | | 591. | 0.020 | 816. | 0.093 | 511. | 0.521 | 531. | 0.550 |
| 645. | 0.054 | 645. | 0.054 | | | 645. | 0.090 | 847. | 0.035 | 531. | 0.550 | 596. | 0.460 |
| 816. | 0.091 | 847. | 0.070 | | | 847. | 0.045 | 887. | 0.110 | 596. | 0.460 | 700. | 0.517 |
| 847. | 0.077 | 887. | 0.090 | CURVE 18* $\lambda = 10.5$ | | 887. | 0.100 | 816. | 0.094 | 744. | 0.553 | 888. | 0.669 |
| 887. | 0.087 | CURVE 8* $\lambda = 5.5$ | | | | 816. | 0.100 | 847. | 0.036 | CURVE 29* $\lambda = 3.5$ | | 502. | 0.520 |
| 591. | 0.033 | 591. | 0.033 | | | 847. | 0.047 | 887. | 0.112 | 502. | 0.520 | 511. | 0.516 |
| 645. | 0.047 | 645. | 0.047 | | | 887. | 0.033 | CURVE 25* $\lambda = 14.0$ | | 511. | 0.516 | 531. | 0.530 |
| 816. | 0.092 | 816. | 0.092 | | | 816. | 0.015 | 316. | 0.093 | 531. | 0.530 | 596. | 0.458 |
| 847. | 0.062 | 847. | 0.062 | CURVE 19* $\lambda = 11.0$ | | 847. | 0.096 | 887. | 0.102 | 596. | 0.458 | 744. | 0.502 |
| 887. | 0.090 | 645. | 0.042 | | | 887. | 0.101 | CURVE 26* $\lambda = 2.0$ | | 744. | 0.502 | 888. | 0.663 |
| 591. | 0.040 | 887. | 0.101 | | | 645. | 0.034 | 502. | 0.500 | CURVE 30* $\lambda = 4.0$ | | 502. | 0.495 |
| 645. | 0.055 | CURVE 14* $\lambda = 8.5$ | | | | 847. | 0.034 | 511. | 0.514 | 511. | 0.514 | 531. | 0.522 |
| 816. | 0.085 | 645. | 0.020 | | | 887. | 0.105 | 596. | 0.492 | 596. | 0.492 | 700. | 0.570 |
| 847. | 0.075 | 816. | 0.034 | CURVE 20* $\lambda = 11.5$ | | 887. | 0.116 | 502. | 0.500 | 502. | 0.500 | 581. | 0.540 |
| 887. | 0.090 | 816. | 0.093 | | | 816. | 0.100 | 511. | 0.514 | 511. | 0.514 | 596. | 0.492 |
| CURVE 5 (CONT.)* | | | | | | | | | | | | | |
| 847. | 0.050 | 847. | 0.057 | | | 847. | 0.032 | 596. | 0.492 | 596. | 0.492 | 700. | 0.570 |
| 887. | 0.057 | CURVE 9* $\lambda = 6.0$ | | | | 887. | 0.090 | 700. | 0.570 | 700. | 0.570 | 888. | 0.663 |
| 591. | 0.020 | 591. | 0.020 | | | 591. | 0.020 | 888. | 0.663 | 888. | 0.663 | 888. | 0.663 |
| 645. | 0.034 | 645. | 0.034 | | | 645. | 0.034 | 888. | 0.663 | 888. | 0.663 | 888. | 0.663 |
| 816. | 0.085 | 816. | 0.085 | | | 816. | 0.085 | 888. | 0.663 | 888. | 0.663 | 888. | 0.663 |
| 847. | 0.075 | 847. | 0.075 | | | 847. | 0.075 | 888. | 0.663 | 888. | 0.663 | 888. | 0.663 |
| 887. | 0.090 | 887. | 0.090 | | | 887. | 0.090 | 888. | 0.663 | 888. | 0.663 | 888. | 0.663 |

* NOT SHOWN IN FIGURE.

TABLE 20--4. EXPERIMENTAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|-------------------|------------|-----------------|------------|------------------|------------|-----------------|------------|-----------------|------------|-----------------|------------|
| CURVE 30 (CONT.)* | | | | | | | | | | | |
| CURVE 34* | | | | | | | | | | | |
| $\lambda = 6.0$ | | | | | | | | | | | |
| 511. | 0.510 | 865. | 0.490 | 700. | 0.470 | 399. | 0.652 | 399. | 0.652 | 399. | 0.672 |
| 561. | 0.520 | CURVE 38* | | 744. | 0.451 | 483. | 0.795 | 483. | 0.795 | 483. | 0.755 |
| 596. | 0.455 | $\lambda = 8.0$ | | 866. | 0.477 | 617. | 0.798 | 617. | 0.798 | 617. | 0.767 |
| 700. | 0.492 | | | CURVE 42* | | 758. | 0.790 | 758. | 0.790 | 758. | 0.774 |
| 744. | 0.467 | | | $\lambda = 10.0$ | | 844. | 0.872 | 844. | 0.872 | 844. | 0.811 |
| 868. | 0.614 | | | 502. | 0.433 | 877. | 0.895 | 877. | 0.895 | 877. | 0.794 |
| CURVE 31* | | | | | | | | | | | |
| $\lambda = 4.5$ | | | | | | | | | | | |
| 502. | 0.510 | 502. | 0.385 | 502. | 0.385 | CURVE 47* | | CURVE 51* | | $\lambda = 6.0$ | |
| 511. | 0.510 | 511. | 0.462 | 511. | 0.395 | $\lambda = 4.0$ | | $\lambda = 6.0$ | | | |
| 561. | 0.518 | 561. | 0.428 | 531. | 0.424 | | | | | | |
| 596. | 0.455 | 596. | 0.464 | 700. | 0.465 | | | | | | |
| 700. | 0.497 | 744. | 0.471 | 744. | 0.445 | | | | | | |
| 744. | 0.494 | 838. | 0.490 | 868. | 0.477 | | | | | | |
| 868. | 0.586 | CURVE 39* | | CURVE 43* | | | | | | | |
| $\lambda = 6.5$ | | | | | | | | | | | |
| 502. | 0.486 | 502. | 0.420 | $\lambda = 2.0$ | | | | | | | |
| 511. | 0.465 | 511. | 0.440 | 617. | 0.792 | | | | | | |
| 561. | 0.476 | 561. | 0.459 | 758. | 0.770 | | | | | | |
| 596. | 0.437 | 596. | 0.422 | 844. | 0.830 | | | | | | |
| 700. | 0.484 | 744. | 0.468 | 877. | 0.796 | | | | | | |
| 744. | 0.484 | 868. | 0.490 | CURVE 44* | | | | | | | |
| 868. | 0.503 | 868. | 0.490 | $\lambda = 2.5$ | | | | | | | |
| CURVE 32* | | | | | | | | | | | |
| $\lambda = 5.0$ | | | | | | | | | | | |
| 502. | 0.490 | CURVE 40* | | CURVE 48* | | | | | | | |
| 511. | 0.505 | $\lambda = 9.0$ | | $\lambda = 4.5$ | | | | | | | |
| 561. | 0.512 | | | CURVE 49* | | | | | | | |
| 596. | 0.452 | | | $\lambda = 5.0$ | | | | | | | |
| 700. | 0.497 | | | | | | | | | | |
| 744. | 0.490 | | | | | | | | | | |
| 868. | 0.554 | | | | | | | | | | |
| CURVE 33* | | | | | | | | | | | |
| $\lambda = 5.5$ | | | | | | | | | | | |
| 502. | 0.465 | CURVE 45* | | CURVE 53* | | | | | | | |
| 511. | 0.491 | $\lambda = 3.0$ | | $\lambda = 7.0$ | | | | | | | |
| 561. | 0.508 | | | CURVE 46* | | | | | | | |
| 596. | 0.445 | | | $\lambda = 3.5$ | | | | | | | |
| 700. | 0.491 | | | | | | | | | | |
| 744. | 0.495 | | | | | | | | | | |
| 868. | 0.510 | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 20-- EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|-------------------------------|------------|------|------------|------|------------|------|------------|------|------------|------------------------------|------------|
| CURVE 54* $\lambda = 7.5$ | | | | | | | | | | | |
| 399. | 0.630 | 399. | 0.535 | 399. | 0.495 | 399. | 0.310 | 514. | 0.065 | 543. | 0.520 |
| 403. | 0.705 | 403. | 0.634 | 403. | 0.594 | 403. | 0.473 | 643. | 0.059 | 738. | 0.835 |
| 617. | 0.722 | 617. | 0.659 | 617. | 0.617 | 617. | 0.577 | 738. | 0.056 | 914. | 0.057 |
| 756. | 0.743 | 756. | 0.694 | 756. | 0.625 | 756. | 0.592 | 914. | 0.103 | | |
| 844. | 0.773 | 844. | 0.720 | 844. | 0.650 | 844. | 0.620 | | | CURVE 77* $\lambda = 2.0$ | |
| 877. | 0.765 | 877. | 0.706 | 877. | 0.632 | 877. | 0.603 | | | | |
| CURVE 55* $\lambda = 8.0$ | | | | | | | | | | | |
| CURVE 58* $\lambda = 9.5$ | | | | | | | | | | | |
| 399. | 0.621 | 399. | 0.520 | 399. | 0.480 | 399. | 0.447 | 514. | 0.034 | 514. | 0.152 |
| 403. | 0.657 | 403. | 0.616 | 403. | 0.553 | 403. | 0.525 | 643. | 0.044 | 637. | 0.156 |
| 617. | 0.715 | 617. | 0.653 | 617. | 0.593 | 617. | 0.572 | 738. | 0.053 | 738. | 0.175 |
| 756. | 0.730 | 756. | 0.674 | 756. | 0.620 | 756. | 0.592 | 914. | 0.050 | 755. | 0.175 |
| 844. | 0.761 | 844. | 0.701 | 844. | 0.643 | 844. | 0.616 | | | 912. | 0.202 |
| 877. | 0.741 | 877. | 0.685 | 877. | 0.624 | 877. | 0.588 | | | CURVE 78* $\lambda = 2.5$ | |
| CURVE 56* $\lambda = 8.5$ | | | | | | | | | | | |
| 399. | 0.600 | 399. | 0.520 | 399. | 0.430 | 399. | 0.109 | 514. | 0.034 | 514. | 0.024 |
| 403. | 0.670 | 403. | 0.600 | 403. | 0.530 | 403. | 0.481 | 643. | 0.041 | 637. | 0.131 |
| 617. | 0.700 | 617. | 0.642 | 617. | 0.574 | 617. | 0.560 | 738. | 0.048 | 639. | 0.126 |
| 756. | 0.721 | 756. | 0.660 | 756. | 0.606 | 756. | 0.581 | 914. | 0.076 | 738. | 0.146 |
| 844. | 0.752 | 844. | 0.680 | 844. | 0.634 | 844. | 0.604 | | | 755. | 0.147 |
| 877. | 0.732 | 877. | 0.665 | 877. | 0.623 | 877. | 0.595 | | | 912. | 0.174 |
| CURVE 57* $\lambda = 9.0$ | | | | | | | | | | | |
| 399. | 0.598 | 399. | 0.510 | 399. | 0.350 | 399. | 0.135 | 514. | 0.019 | 514. | 0.080 |
| 403. | 0.653 | 403. | 0.194 | 403. | 0.504 | 403. | 0.484 | 643. | 0.035 | 464. | 0.070 |
| 617. | 0.681 | 617. | 0.632 | 617. | 0.557 | 617. | 0.570 | 738. | 0.045 | 637. | 0.115 |
| 756. | 0.698 | 756. | 0.641 | 756. | 0.603 | 756. | 0.584 | 914. | 0.070 | 639. | 0.114 |
| 844. | 0.739 | 844. | 0.657 | 844. | 0.630 | 844. | 0.607 | | | 738. | 0.125 |
| 877. | 0.719 | 877. | 0.640 | 877. | 0.615 | 877. | 0.584 | | | 755. | 0.135 |
| CURVE 59* $\lambda = 10.0$ | | | | | | | | | | | |
| CURVE 60* $\lambda = 10.5$ | | | | | | | | | | | |
| CURVE 61* $\lambda = 11.0$ | | | | | | | | | | | |
| CURVE 62* $\lambda = 11.5$ | | | | | | | | | | | |
| CURVE 63* $\lambda = 12.0$ | | | | | | | | | | | |
| CURVE 64* $\lambda = 12.5$ | | | | | | | | | | | |
| CURVE 65* $\lambda = 13.5$ | | | | | | | | | | | |
| CURVE 66* $\lambda = 14.0$ | | | | | | | | | | | |
| CURVE 67* $\lambda = 14.0$ | | | | | | | | | | | |
| CURVE 68* $\lambda = 14.5$ | | | | | | | | | | | |
| CURVE 69* $\lambda = 2.5$ | | | | | | | | | | | |
| CURVE 70 $\lambda = 3.0$ | | | | | | | | | | | |
| CURVE 71* $\lambda = 3.5$ | | | | | | | | | | | |
| CURVE 72* $\lambda = 4.0$ | | | | | | | | | | | |
| CURVE 73* $\lambda = 4.5$ | | | | | | | | | | | |
| CURVE 74* $\lambda = 5.0$ | | | | | | | | | | | |
| CURVE 75* $\lambda = 5.5$ | | | | | | | | | | | |
| CURVE 76* $\lambda = 6.0$ | | | | | | | | | | | |
| CURVE 79 $\lambda = 3.0$ | | | | | | | | | | | |
| CURVE 80* $\lambda = 3.5$ | | | | | | | | | | | |
| 479. | 0.075 | 479. | 0.064 | 479. | 0.120 | 479. | 0.072 | 479. | 0.029 | 479. | 0.080 |
| 484. | 0.072 | 484. | 0.064 | 484. | 0.120 | 484. | 0.072 | 484. | 0.042 | 484. | 0.070 |
| 484. | 0.072 | 484. | 0.064 | 484. | 0.120 | 484. | 0.072 | 484. | 0.062 | 484. | 0.070 |

* NOT SHOWN IN FIGURE.

TABLE 20-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | |
|-------------------|------------|-----------------|------------|-----------|------------|------------|------------|-----------------|------------|--------------------|-----------------|-----------------|------------|-------|
| CURVE 80 (CONT.)* | | | | | | | | | | | | | | |
| 637. | 0.106 | CURVE 84* | | 646. | 0.066 | CURVE 92* | | 636. | 0.032 | CURVE 101 (CONT.)* | | 627. | 0.094 | |
| 535. | 0.106 | 479. | 0.026 | 653. | 0.060 | 553. | 0.032 | 833. | 0.032 | 568. | 0.040 | 833. | 0.090 | |
| 735. | 0.117 | 484. | 0.014 | 658. | 0.094 | 568. | 0.094 | CURVE 97 | | CURVE 102* | | CURVE 103* | | |
| 755. | 0.116 | 637. | 0.082 | 755. | 0.037 | 636. | 0.116 | $\lambda = 3.0$ | 636. | 0.074 | $\lambda = 5.5$ | $\lambda = 6.0$ | | |
| 912. | 0.153 | 639. | 0.039 | 769. | 0.113 | 687. | 0.094 | | 687. | 0.060 | | | | |
| CURVE 81* | | | | | | | | | | | | | | |
| $\lambda = 4.0$ | | 733. | 0.099 | 918. | 0.122 | 833. | 0.096 | CURVE 93* | | CURVE 98* | | CURVE 104* | | |
| 479. | 0.051 | 755. | 0.092 | 918. | 0.125 | 833. | 0.099 | $\lambda = 5.5$ | 553. | 0.051 | 553. | 0.020 | 553. | 0.004 |
| 637. | 0.057 | 912. | 0.110 | CURVE 89* | | 646. | 0.040 | $\lambda = 3.5$ | 568. | 0.040 | 636. | 0.055 | 636. | 0.033 |
| 639. | 0.100 | CURVE 85* | | 653. | 0.057 | 755. | 0.057 | | 687. | 0.056 | 833. | 0.057 | 833. | 0.075 |
| 735. | 0.103 | 473. | 0.011 | 769. | 0.045 | 918. | 0.105 | | 833. | 0.073 | CURVE 105* | | | |
| 912. | 0.130 | 637. | 0.079 | 918. | 0.089 | CURVE 94* | | $\lambda = 4.0$ | 553. | 0.105 | CURVE 106* | | | |
| CURVE 82* | | | | | | | | | | | | | | |
| $\lambda = 4.5$ | | 737. | 0.091 | 646. | 0.019 | 553. | 0.019 | | 568. | 0.058 | CURVE 107* | | | |
| 479. | 0.061 | 639. | 0.087 | 653. | 0.034 | 568. | 0.034 | | 636. | 0.073 | CURVE 108* | | | |
| 637. | 0.099 | 733. | 0.104 | 755. | 0.060 | 636. | 0.060 | | 687. | 0.085 | CURVE 109* | | | |
| 639. | 0.097 | 755. | 0.085 | 769. | 0.063 | 833. | 0.090 | | 833. | 0.100 | CURVE 110* | | | |
| 735. | 0.107 | CURVE 86* | | 646. | 0.057 | 553. | 0.057 | | 568. | 0.055 | CURVE 111* | | | |
| 912. | 0.125 | $\lambda = 2.0$ | 0.159 | 653. | 0.210 | 568. | 0.210 | | 636. | 0.073 | CURVE 112* | | | |
| CURVE 83* | | | | | | | | | | | | | | |
| $\lambda = 5.0$ | | 646. | 0.235 | 653. | 0.047 | 646. | 0.047 | | 687. | 0.067 | CURVE 113* | | | |
| 479. | 0.053 | 484. | 0.240 | 755. | 0.130 | 687. | 0.114 | | 833. | 0.099 | CURVE 114* | | | |
| 637. | 0.095 | 639. | 0.178 | 769. | 0.108 | 833. | 0.114 | | 553. | 0.145 | CURVE 115* | | | |
| 735. | 0.104 | 918. | 0.277 | 918. | 0.145 | 553. | 0.145 | | 568. | 0.052 | CURVE 116* | | | |
| 912. | 0.125 | CURVE 87* | | 646. | 0.007 | 568. | 0.036 | | 636. | 0.067 | CURVE 117* | | | |
| $\lambda = 5.0$ | | 484. | 0.128 | 653. | 0.075 | 687. | 0.036 | | 687. | 0.067 | CURVE 118* | | | |
| 479. | 0.053 | 484. | 0.102 | 755. | 0.093 | 833. | 0.114 | | 833. | 0.099 | CURVE 119* | | | |
| 637. | 0.095 | 639. | 0.119 | 918. | 0.124 | 553. | 0.095 | | 568. | 0.055 | CURVE 120* | | | |
| 639. | 0.095 | 733. | 0.194 | 918. | 0.103 | 568. | 0.079 | | 636. | 0.055 | CURVE 121* | | | |
| 735. | 0.104 | 755. | 0.147 | 918. | 0.129 | 636. | 0.079 | | 687. | 0.053 | CURVE 122* | | | |
| 912. | 0.120 | 918. | 0.240 | 918. | 0.129 | 833. | 0.114 | | 833. | 0.070 | CURVE 123* | | | |
| CURVE 88* | | | | | | | | | | | | | | |
| $\lambda = 3.0$ | | 484. | 0.135 | 646. | 0.066 | 553. | 0.066 | | 568. | 0.052 | CURVE 124* | | | |
| 479. | 0.026 | 493. | 0.060 | 653. | 0.094 | 568. | 0.094 | | 636. | 0.067 | CURVE 125* | | | |
| 637. | 0.082 | 645. | 0.037 | 755. | 0.116 | 636. | 0.116 | | 687. | 0.083 | CURVE 126* | | | |
| 639. | 0.039 | 658. | 0.113 | 769. | 0.094 | 687. | 0.094 | | 833. | 0.083 | CURVE 127* | | | |
| 733. | 0.099 | 756. | 0.154 | 918. | 0.122 | 833. | 0.099 | | 553. | 0.061 | CURVE 128* | | | |
| 755. | 0.092 | 918. | 0.125 | CURVE 89* | | 553. | 0.061 | | 568. | 0.055 | CURVE 129* | | | |
| 912. | 0.110 | $\lambda = 3.5$ | 0.190 | 646. | 0.040 | 568. | 0.040 | | 636. | 0.055 | CURVE 130* | | | |
| CURVE 89* | | | | | | | | | | | | | | |
| $\lambda = 3.5$ | | 493. | 0.030 | 653. | 0.057 | 568. | 0.057 | | 687. | 0.056 | CURVE 131* | | | |
| 479. | 0.011 | 645. | 0.045 | 755. | 0.099 | 636. | 0.099 | | 687. | 0.073 | CURVE 132* | | | |
| 637. | 0.079 | 658. | 0.089 | 769. | 0.073 | 687. | 0.073 | | 833. | 0.105 | CURVE 133* | | | |
| 639. | 0.035 | 756. | 0.106 | 918. | 0.105 | CURVE 94* | | $\lambda = 4.0$ | 553. | 0.010 | CURVE 134* | | | |
| 733. | 0.091 | 756. | 0.134 | 646. | 0.019 | 553. | 0.019 | | 568. | 0.058 | CURVE 135* | | | |
| 755. | 0.087 | 769. | 0.114 | 653. | 0.034 | 568. | 0.034 | | 636. | 0.073 | CURVE 136* | | | |
| 912. | 0.104 | 918. | 0.152 | 755. | 0.060 | 636. | 0.060 | | 687. | 0.085 | CURVE 137* | | | |
| CURVE 90* | | | | | | | | | | | | | | |
| $\lambda = 4.0$ | | 484. | 0.057 | 646. | 0.019 | 553. | 0.019 | | 568. | 0.055 | CURVE 138* | | | |
| 479. | 0.159 | 493. | 0.210 | 653. | 0.034 | 568. | 0.034 | | 636. | 0.073 | CURVE 139* | | | |
| 637. | 0.235 | 646. | 0.047 | 755. | 0.063 | 636. | 0.063 | | 687. | 0.085 | CURVE 140* | | | |
| 639. | 0.240 | 756. | 0.090 | 769. | 0.090 | 833. | 0.090 | | 833. | 0.100 | CURVE 141* | | | |
| 735. | 0.178 | CURVE 95* | | 646. | 0.145 | 553. | 0.145 | | 568. | 0.052 | CURVE 142* | | | |
| 918. | 0.277 | $\lambda = 2.0$ | 0.130 | 653. | 0.094 | 636. | 0.094 | | 687. | 0.067 | CURVE 143* | | | |
| CURVE 91* | | | | | | | | | | | | | | |
| $\lambda = 4.5$ | | 484. | 0.007 | 646. | 0.036 | 687. | 0.036 | | 833. | 0.083 | CURVE 144* | | | |
| 479. | 0.128 | 484. | 0.075 | 755. | 0.114 | 833. | 0.114 | | 553. | 0.099 | CURVE 145* | | | |
| 637. | 0.102 | 646. | 0.093 | 918. | 0.124 | 553. | 0.095 | | 568. | 0.055 | CURVE 146* | | | |
| 639. | 0.119 | 756. | 0.124 | 918. | 0.103 | 568. | 0.079 | | 636. | 0.055 | CURVE 147* | | | |
| 639. | 0.095 | 756. | 0.147 | 918. | 0.129 | 636. | 0.079 | | 687. | 0.053 | CURVE 148* | | | |
| 735. | 0.104 | 918. | 0.240 | 918. | 0.129 | 833. | 0.114 | | 833. | 0.070 | CURVE 149* | | | |
| 912. | 0.120 | CURVE 96* | | 646. | 0.066 | 553. | 0.066 | | 568. | 0.052 | CURVE 150* | | | |
| $\lambda = 2.5$ | | 484. | 0.007 | 653. | 0.094 | 636. | 0.094 | | 687. | 0.067 | CURVE 151* | | | |
| 479. | 0.128 | 484. | 0.075 | 755. | 0.116 | 636. | 0.116 | | 687. | 0.083 | CURVE 152* | | | |
| 637. | 0.102 | 646. | 0.093 | 769. | 0.094 | 833. | 0.099 | | 553. | 0.061 | CURVE 153* | | | |
| 639. | 0.095 | 756. | 0.124 | 918. | 0.103 | 568. | 0.079 | | 568. | 0.055 | CURVE 154* | | | |
| 735. | 0.104 | 918. | 0.240 | 918. | 0.129 | 636. | 0.079 | | 636. | 0.055 | CURVE 155* | | | |
| 912. | 0.120 | CURVE 97 | | 646. | 0.040 | 687. | 0.040 | | 687. | 0.053 | CURVE 156* | | | |
| $\lambda = 3.0$ | | 484. | 0.135 | 653. | 0.057 | 833. | 0.114 | | 833. | 0.070 | CURVE 157* | | | |
| 479. | 0.026 | 493. | 0.060 | 755. | 0.099 | 833. | 0.099 | | 553. | 0.061 | CURVE 158* | | | |
| 637. | 0.082 | 645. | 0.037 | 769. | 0.073 | 833. | 0.099 | | 568. | 0.055 | CURVE 159* | | | |
| 639. | 0.039 | 658. | 0.113 | 918. | 0.105 | CURVE 99* | | $\lambda = 4.0$ | 636. | 0.055 | CURVE 160* | | | |
| 733. | 0.099 | 756. | 0.154 | 646. | 0.019 | 553. | 0.019 | | 636. | 0.020 | CURVE 161* | | | |
| 755. | 0.092 | 763. | 0.125 | 653. | 0.034 | 568. | 0.034 | | 637. | 0.070 | CURVE 162* | | | |
| 912. | 0.110 | 918. | 0.190 | 755. | 0.060 | 636. | 0.060 | | 637. | 0.070 | CURVE 163* | | | |
| CURVE 92* | | | | | | | | | | | | | | |
| $\lambda = 5.0$ | | 484. | 0.007 | 646. | 0.036 | 687. | 0.036 | | 687. | 0.083 | CURVE 164* | | | |
| 479. | 0.128 | 484. | 0.075 | 755. | 0.114 | 833. | 0.114 | | 553. | 0.099 | CURVE 165* | | | |
| 637. | 0.102 | 646. | 0.093 | 918. | 0.124 | 553. | 0.095 | | 568. | 0.055 | CURVE 166* | | | |
| 639. | 0.095 | 756. | 0.124 | 918. | 0.103 | 568. | 0.079 | | 636. | 0.055 | CURVE 167* | | | |
| 735. | 0.104 | 918. | 0.240 | 918. | 0.129 | 636. | 0.079 | | 687. | 0.053 | CURVE 168* | | | |
| 912. | 0.120 | CURVE 98* | | 646. | 0.066 | 687. | 0.066 | | 833. | 0.070 | CURVE 169* | | | |
| $\lambda = 3.5$ | | 484. | 0.007 | 653. | 0.094 | 833. | 0.099 | | 553. | 0.061 | CURVE 170* | | | |
| 479. | 0.128 | 484. | 0.075 | 755. | 0.116 | 833. | 0.099 | | 568. | 0.055 | CURVE 171* | | | |
| 637. | 0.102 | 646. | 0.093 | 769. | 0.094 | 833. | 0.099 | | 636. | 0.055 | CURVE 172* | | | |
| 639. | 0.095 | 756. | 0.124 | 918. | 0.103 | CURVE 100* | | $\lambda = 4.5$ | 636. | 0.055 | CURVE 173* | | | |
| 735. | 0.104 | 918. | 0.240 | 646. | 0.019 | 553. | 0.019 | | 637. | 0.070 | CURVE 174* | | | |
| 912. | 0.120 | CURVE 99* | | 653. | 0.034 | 568. | 0.034 | | 637. | 0.070 | CURVE 175* | | | |
| $\lambda = 4.5$ | | 484. | 0.007 | 653. | 0.063 | 636. | 0.063 | | 687. | 0.085 | CURVE 176* | | | |
| 479. | 0.128 | 484. | 0.075 | 755. | 0.116 | 636. | 0.116 | | 833. | 0.072 | CURVE 177* | | | |
| 637. | 0.102 | 646. | 0.093 | 769. | 0.094 | CURVE 100* | | $\lambda = 4.5$ | 553. | 0.061 | CURVE 178* | | | |
| 639. | 0.095 | 756. | 0.124 | 918. | 0.103 | 553. | 0.061 | | 568. | 0.055 | CURVE 179* | | | |
| 735. | 0.104 | 918. | 0.240 | 646. | 0.019 | 568. | 0.034 | | 636. | 0.055 | CURVE 180* | | | |
| 912. | 0.120 | CURVE 101* | | 653. | 0.034 | 636. | 0.034 | | 687. | 0.085 | CURVE 181* | | | |
| $\lambda = 5.0$ | | 484. | 0.007 | | | | | | | | | | | |

TABLE 20-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) (CONTINUED)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|-----------------|------------|------------|------------|------------|------------|------------------|------------|------------------|------------|------------------|------------|
| CURVE 107* | | | | | | | | | | | |
| $\lambda = 8.0$ | | | | | | | | | | | |
| 687. | 0.042 | 472. | 0.044 | 546. | 0.059 | 546. | 0.015 | 669. | 0.012 | 769. | 0.054 |
| 833. | 0.035 | 546. | 0.058 | 578. | 0.057 | 578. | 0.029 | 765. | 0.069 | 814. | 0.055 |
| CURVE 108* | | | | | | | | | | | |
| $\lambda = 9.5$ | | | | | | | | | | | |
| 687. | 0.034 | 578. | 0.072 | 669. | 0.077 | 769. | 0.067 | 814. | 0.078 | CURVE 134* | |
| 833. | 0.020 | 669. | 0.080 | 769. | 0.077 | 814. | 0.097 | $\lambda = 10.0$ | | $\lambda = 13.5$ | |
| CURVE 109* | | | | | | | | | | | |
| $\lambda = 9.0$ | | | | | | | | | | | |
| 687. | 0.034 | 814. | 0.110 | 814. | 0.120 | CURVE 122* | | 769. | 0.075 | 769. | 0.041 |
| 833. | 0.034 | CURVE 114* | | CURVE 118* | | $\lambda = 7.5$ | | 814. | 0.080 | 814. | 0.043 |
| $\lambda = 3.5$ | | | | | | | | | | | |
| 472. | 0.061 | 472. | 0.061 | 472. | 0.060 | 546. | 0.012 | CURVE 128* | | CURVE 135* | |
| 546. | 0.056 | 546. | 0.061 | 546. | 0.061 | 578. | 0.023 | $\lambda = 10.5$ | | $\lambda = 14.0$ | |
| 578. | 0.056 | 578. | 0.066 | 578. | 0.066 | 669. | 0.069 | 765. | 0.075 | 769. | 0.019 |
| 669. | 0.020 | 669. | 0.074 | 669. | 0.074 | 814. | 0.085 | 814. | 0.079 | 814. | 0.023 |
| 769. | 0.096 | 769. | 0.096 | 769. | 0.099 | CURVE 123* | | CURVE 129* | | CURVE 136* | |
| 814. | 0.116 | 814. | 0.116 | 814. | 0.108 | $\lambda = 8.0$ | | $\lambda = 11.0$ | | $\lambda = 2.0$ | |
| CURVE 115* | | | | | | | | | | | |
| $\lambda = 4.0$ | | | | | | | | | | | |
| 633. | 0.003 | CURVE 119* | | CURVE 125* | | 578. | 0.009 | 765. | 0.075 | 603. | 0.079 |
| $\lambda = 6.0$ | | | | | | | | | | | |
| 472. | 0.059 | 472. | 0.038 | 472. | 0.038 | 669. | 0.020 | 814. | 0.078 | 681. | 0.067 |
| 546. | 0.055 | 546. | 0.039 | 546. | 0.039 | 769. | 0.062 | CURVE 130* | | 731. | 0.034 |
| 578. | 0.066 | 578. | 0.048 | 578. | 0.048 | 814. | 0.061 | $\lambda = 11.5$ | | 768. | 0.087 |
| 559. | 0.074 | 669. | 0.062 | 669. | 0.062 | CURVE 124* | | $\lambda = 2.5$ | | 800. | 0.100 |
| 769. | 0.101 | 769. | 0.090 | 769. | 0.090 | 578. | 0.005 | 765. | 0.076 | CURVE 137* | |
| 814. | 0.115 | 814. | 0.090 | 814. | 0.090 | 669. | 0.019 | 814. | 0.069 | $\lambda = 2.5$ | |
| CURVE 116* | | | | | | | | | | | |
| $\lambda = 4.5$ | | | | | | | | | | | |
| 472. | 0.064 | 472. | 0.064 | 472. | 0.005 | 669. | 0.019 | 569. | 0.069 | 569. | 0.031 |
| 546. | 0.050 | 546. | 0.017 | 546. | 0.017 | 769. | 0.055 | 603. | 0.059 | 603. | 0.059 |
| 578. | 0.072 | 578. | 0.037 | 578. | 0.037 | 814. | 0.071 | 631. | 0.056 | 631. | 0.056 |
| 669. | 0.076 | 669. | 0.039 | 669. | 0.039 | CURVE 125* | | 731. | 0.077 | 731. | 0.077 |
| 769. | 0.116 | 769. | 0.075 | 769. | 0.075 | $\lambda = 9.0$ | | 769. | 0.054 | 769. | 0.089 |
| 814. | 0.118 | 814. | 0.093 | 814. | 0.093 | 669. | 0.020 | 814. | 0.054 | 800. | 0.090 |
| CURVE 112* | | | | | | | | | | | |
| $\lambda = 2.5$ | | | | | | | | | | | |
| 472. | 0.031 | 669. | 0.068 | 669. | 0.068 | CURVE 132* | | CURVE 138 | | $\lambda = 3.0$ | |
| 546. | 0.059 | 769. | 0.076 | 769. | 0.076 | $\lambda = 12.5$ | | $\lambda = 3.0$ | | 470. | |
| 578. | 0.082 | 814. | 0.076 | 814. | 0.076 | 765. | 0.061 | 765. | 0.061 | 560. | 0.020 |
| 669. | 0.112 | 814. | 0.093 | 814. | 0.093 | 814. | 0.055 | 814. | 0.055 | 560. | 0.042 |
| 769. | 0.131 | | | | | | | | | | |
| 814. | 0.140 | | | | | | | | | | |

* NOT SHOWN IN FIGURE.

TABLE 20-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) (CONTINUED)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|--------------------|------------|------|-----------------|------------------|------------|-----------------|------------|--------------------|-----------------|------|------------|
| CURVE 133 (CONT.)* | | | | | | | | | | | |
| CURVE 142* | | | CURVE 143* | | | CURVE 144* | | | CURVE 145* | | |
| $\lambda = 5.0$ | | | $\lambda = 5.5$ | | | $\lambda = 6.0$ | | | $\lambda = 6.5$ | | |
| 603. | 0.062 | 470. | 0.018 | 568. | 0.035 | 603. | 0.012 | 603. | 0.006 | 491. | 0.092 |
| 631. | 0.052 | 568. | 0.043 | 603. | 0.037 | 681. | 0.044 | 681. | 0.042 | 513. | 0.025 |
| 731. | 0.070 | 603. | 0.054 | 681. | 0.046 | 731. | 0.053 | 731. | 0.052 | 623. | 0.105 |
| 768. | 0.073 | 681. | 0.061 | 731. | 0.053 | 768. | 0.056 | 768. | 0.067 | 644. | 0.093 |
| 808. | 0.083 | 731. | 0.067 | 808. | 0.056 | 808. | 0.074 | 808. | 0.074 | 724. | 0.100 |
| CURVE 139* | | | CURVE 147* | | | CURVE 148* | | | CURVE 149* | | |
| $\lambda = 3.5$ | | | $\lambda = 7.5$ | | | $\lambda = 8.0$ | | | $\lambda = 8.5$ | | |
| 470. | 0.031 | 568. | 0.035 | 603. | 0.073 | 603. | 0.077 | 603. | 0.006 | 681. | 0.014 |
| 568. | 0.045 | 603. | 0.037 | 681. | 0.073 | 731. | 0.073 | 731. | 0.042 | 768. | 0.048 |
| 603. | 0.061 | 681. | 0.042 | 731. | 0.073 | 768. | 0.073 | 808. | 0.042 | 808. | 0.048 |
| 631. | 0.059 | 731. | 0.043 | 768. | 0.060 | 808. | 0.073 | CURVE 155* | | | |
| 731. | 0.074 | 808. | 0.086 | CURVE 152* | | | | $\lambda = 11.5$ | | | |
| CURVE 140* | | | | | | | | | | | |
| $\lambda = 4.0$ | | | | | | | | | | | |
| 470. | 0.023 | 470. | 0.002 | 568. | 0.035 | 568. | 0.035 | 568. | 0.035 | 568. | 0.035 |
| 568. | 0.034 | 568. | 0.034 | 603. | 0.046 | 603. | 0.046 | 603. | 0.046 | 603. | 0.046 |
| 603. | 0.059 | 603. | 0.043 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 |
| 681. | 0.051 | 681. | 0.055 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 |
| 731. | 0.057 | 731. | 0.054 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 |
| 768. | 0.073 | 768. | 0.073 | CURVE 153* | | | | CURVE 156 (CONT.)* | | | |
| 808. | 0.091 | 808. | 0.077 | $\lambda = 10.0$ | | | | $\lambda = 2.5$ | | | |
| CURVE 141* | | | | | | | | | | | |
| $\lambda = 4.5$ | | | | | | | | | | | |
| 470. | 0.022 | 470. | 0.018 | 568. | 0.035 | 568. | 0.035 | 568. | 0.035 | 568. | 0.035 |
| 568. | 0.043 | 568. | 0.043 | 603. | 0.046 | 603. | 0.046 | 603. | 0.046 | 603. | 0.046 |
| 603. | 0.057 | 603. | 0.047 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 |
| 681. | 0.052 | 681. | 0.051 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 |
| 731. | 0.053 | 731. | 0.056 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 |
| 768. | 0.074 | 768. | 0.056 | CURVE 154* | | | | CURVE 157* | | | |
| 809. | 0.090 | 808. | 0.077 | $\lambda = 11.0$ | | | | $\lambda = 2.5$ | | | |
| CURVE 146* | | | | | | | | | | | |
| $\lambda = 7.0$ | | | | | | | | | | | |
| 731. | 0.043 | 731. | 0.010 | 768. | 0.060 | 768. | 0.060 | 768. | 0.060 | 768. | 0.060 |
| 808. | 0.070 | 808. | 0.047 | 808. | 0.075 | 808. | 0.075 | 808. | 0.075 | 808. | 0.075 |
| CURVE 147* | | | | | | | | | | | |
| $\lambda = 7.5$ | | | | | | | | | | | |
| 681. | 0.033 | 681. | 0.010 | 731. | 0.035 | 731. | 0.035 | 731. | 0.035 | 731. | 0.035 |
| 731. | 0.035 | 731. | 0.035 | 768. | 0.056 | 768. | 0.056 | 768. | 0.056 | 768. | 0.056 |
| CURVE 148* | | | | | | | | | | | |
| $\lambda = 8.0$ | | | | | | | | | | | |
| 568. | 0.035 | 568. | 0.035 | 603. | 0.046 | 603. | 0.046 | 603. | 0.046 | 603. | 0.046 |
| 603. | 0.046 | 603. | 0.046 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 |
| 681. | 0.053 | 681. | 0.053 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 |
| 731. | 0.056 | 731. | 0.056 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 |
| 768. | 0.073 | 768. | 0.073 | CURVE 151* | | | | CURVE 158* | | | |
| 808. | 0.091 | 808. | 0.077 | $\lambda = 9.5$ | | | | $\lambda = 3.0$ | | | |
| CURVE 149* | | | | | | | | | | | |
| $\lambda = 8.5$ | | | | | | | | | | | |
| 681. | 0.014 | 681. | 0.006 | 731. | 0.035 | 731. | 0.035 | 731. | 0.035 | 731. | 0.035 |
| 731. | 0.035 | 731. | 0.035 | 768. | 0.056 | 768. | 0.056 | 768. | 0.056 | 768. | 0.056 |
| 768. | 0.056 | 768. | 0.056 | 808. | 0.073 | 808. | 0.073 | 808. | 0.073 | 808. | 0.073 |
| 808. | 0.073 | 808. | 0.073 | CURVE 152* | | | | CURVE 159* | | | |
| CURVE 150* | | | | | | | | | | | |
| $\lambda = 2.0$ | | | | | | | | | | | |
| 623. | 0.095 | 623. | 0.042 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 | 681. | 0.053 |
| 644. | 0.065 | 644. | 0.052 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 | 731. | 0.056 |
| 724. | 0.072 | 724. | 0.052 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 | 768. | 0.073 |
| 733. | 0.100 | 733. | 0.056 | CURVE 153* | | | | CURVE 160* | | | |
| 883. | 0.113 | 883. | 0.067 | $\lambda = 2.0$ | | | | $\lambda = 4.0$ | | | |
| CURVE 151* | | | | | | | | | | | |
| $\lambda = 2.5$ | | | | | | | | | | | |
| 491. | 0.102 | 491. | 0.010 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 |
| 513. | 0.025 | 513. | 0.025 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 |
| 623. | 0.046 | 623. | 0.046 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 |
| 644. | 0.053 | 644. | 0.053 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 |
| 724. | 0.056 | 724. | 0.056 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 |
| 733. | 0.073 | 733. | 0.073 | CURVE 154* | | | | CURVE 161* | | | |
| 883. | 0.113 | 883. | 0.067 | $\lambda = 3.0$ | | | | $\lambda = 4.5$ | | | |
| CURVE 152* | | | | | | | | | | | |
| $\lambda = 3.0$ | | | | | | | | | | | |
| 491. | 0.092 | 491. | 0.014 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 |
| 513. | 0.025 | 513. | 0.025 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 |
| 623. | 0.046 | 623. | 0.046 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 |
| 644. | 0.053 | 644. | 0.053 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 |
| 724. | 0.056 | 724. | 0.056 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 |
| 733. | 0.073 | 733. | 0.073 | CURVE 155* | | | | CURVE 162* | | | |
| 883. | 0.113 | 883. | 0.067 | $\lambda = 3.5$ | | | | $\lambda = 5.0$ | | | |
| CURVE 153* | | | | | | | | | | | |
| $\lambda = 3.5$ | | | | | | | | | | | |
| 491. | 0.092 | 491. | 0.014 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 |
| 513. | 0.025 | 513. | 0.025 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 |
| 623. | 0.046 | 623. | 0.046 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 |
| 644. | 0.053 | 644. | 0.053 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 |
| 724. | 0.056 | 724. | 0.056 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 |
| 733. | 0.073 | 733. | 0.073 | CURVE 156* | | | | CURVE 163* | | | |
| 883. | 0.113 | 883. | 0.067 | $\lambda = 3.5$ | | | | $\lambda = 5.5$ | | | |
| CURVE 154* | | | | | | | | | | | |
| $\lambda = 3.5$ | | | | | | | | | | | |
| 491. | 0.092 | 491. | 0.014 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 | 513. | 0.025 |
| 513. | 0.025 | 513. | 0.025 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 | 623. | 0.046 |
| 623. | 0.046 | 623. | 0.046 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 | 644. | 0.053 |
| 644. | 0.053 | 644. | 0.053 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 | 724. | 0.056 |
| 724. | 0.056 | 724. | 0.056 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 | 733. | 0.073 |
| 733. | 0.073 | 733. | 0.073 | CURVE 157* | | | | CURVE 164* | | | |
| 883. | 0.113 | 883. | 0.067 | $\lambda = 3.5$ | | | | $\lambda = 5.5$ | | | |

* NOT SHOWN IN FIGURE.

TABLE 20-4. EXPERIMENTAL NORMAL SPECTRAL EMITTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ |
|-----------------|------------|
| CURVE 164* | |
| $\lambda = 6.0$ | |
| 623. | 0.034 |
| 644. | 0.058 |
| 724. | 0.065 |
| 733. | 0.093 |
| 883. | 0.107 |
| CURVE 165* | |
| $\lambda = 6.5$ | |
| 644. | 0.026 |
| 883. | 0.097 |
| CURVE 166* | |
| $\lambda = 7.0$ | |
| 644. | 0.028 |
| 883. | 0.107 |
| CURVE 167* | |
| $\lambda = 7.5$ | |
| 644. | 0.020 |
| 883. | 0.105 |
| CURVE 168* | |
| $\lambda = 8.0$ | |
| 644. | 0.016 |
| 883. | 0.107 |

* NOT SHOWN IN FIGURE.

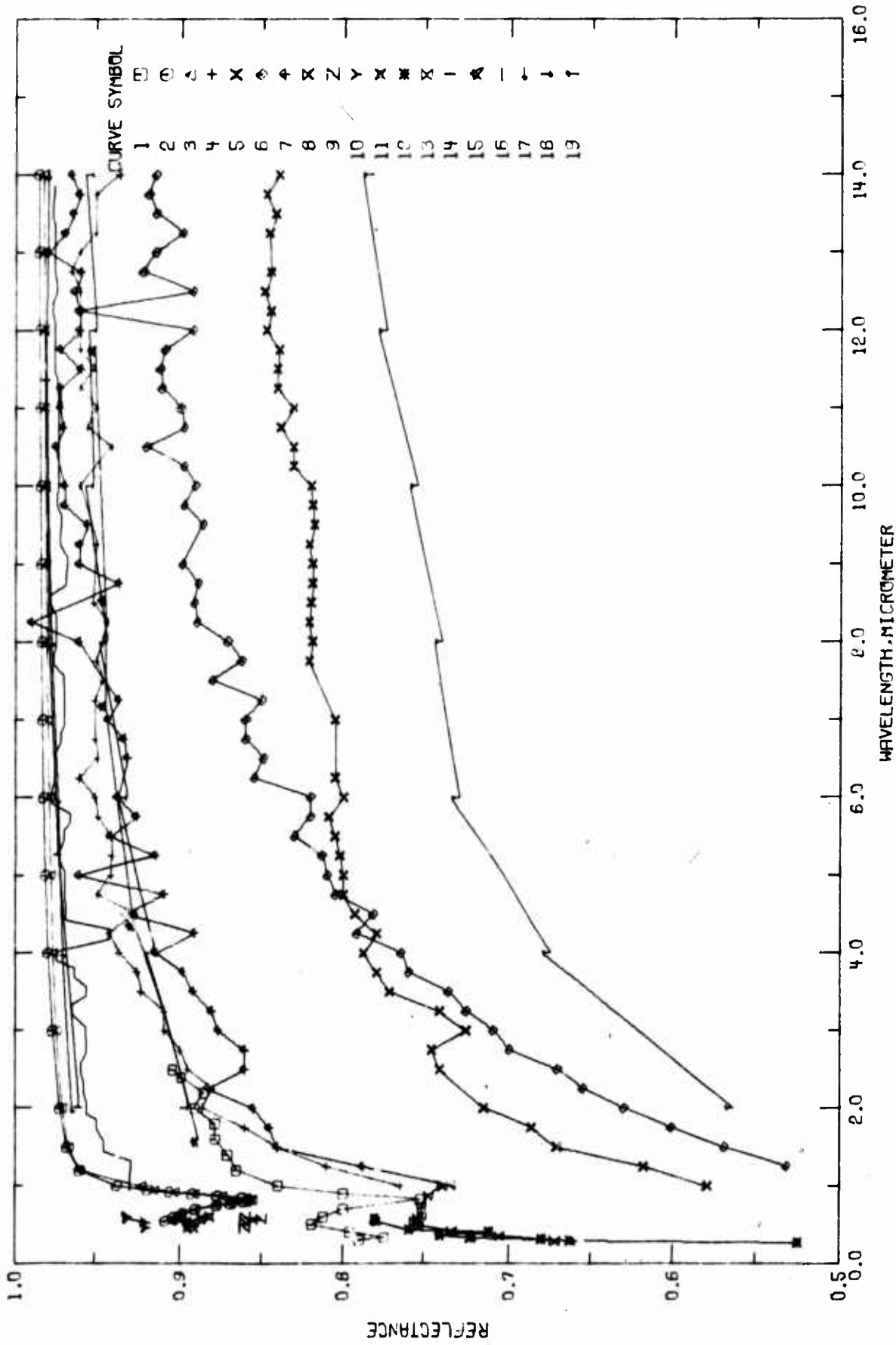


FIGURE 20-3. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE).

TABLE 20-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T27253 | Walsh, D.R. | 1960 | 0.30-2.50 | 298 | | Foil; cemented on fiberglass laminate; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 2 T27424 | Bennett, H.E., Bennett, J.M., and Ashley, E.J. | 1962 | 0.550-32 | 298 | | 99.998 pure; Al film (0.065 to 0.11 μm thick), evaporated at 1×10^{-5} mm Hg, super-smooth fused quartz optical flats as substrate, no watermarks or other blemishes on the substrate surface, no shadows or streaks in the evaporated Al film; freshly prepared; measured in dry nitrogen; $\theta = 5^\circ$, $\theta' = 5^\circ$, reported error $\pm 0.1\%$. |
| 3 T27424 | Bennett, H.E., et al. | 1962 | 0.550-32 | 298 | | 99.998 pure; Al film (0.065 to 0.11 μm thick), evaporated at 1×10^{-5} mm Hg, super-smooth fused quartz optical flats as substrate, no watermarks or other blemishes on the substrate surfaces, no shadows or streaks in the evaporated Al film; aged in air for several weeks; measured in dry nitrogen; $\theta = 5^\circ$, $\theta' = 5^\circ$, reported error $\pm 0.1\%$. |
| 4 T28940 | Dunkle, R.V. and Gier, J.T. | 1953 | 1.00-15.00 | 300 | | Foil; data extracted from smooth curve; converted from $R(2\pi, 5^\circ)$; $\theta = 5^\circ$, $\omega' = 2\pi$, reported error $\pm 2.6\%$. |
| 5 T28940 | Dunkle, R.V. and Gier, J.T. | 1953 | 1.00-15.00 | 300 | | Disc; polished, roughened (roughness approx. 1.27 μm); data extracted from smooth curve; converted from $R(2\pi, 5^\circ)$; $\theta = 5^\circ$, $\omega' = 2\pi$, reported error $\pm 2.6\%$. |
| 6 T28940 | Dunkle, R.V. and Gier, J.T. | 1953 | 1.00-15.00 | 300 | | Disc; commercial finish; data extracted from smooth curve; converted from $R(2\pi, 5^\circ)$; $\theta = 5^\circ$, $\omega' = 2\pi$, reported error $\pm 4.3\%$. |
| 7 T28940 | Dunkle, R.V. and Gier, J.T. | 1953 | 1.00-15.00 | 300 | | Disc; polished; data extracted from smooth curve; converted from $R(2\pi, 5^\circ)$; $\theta = 5^\circ$, $\omega' = 2\pi$, reported error $\pm 2.7\%$. |
| 8 T28906 | Hollatz, L. and Williams, B.J. | 1955 | 0.46-0.60 | 298 | | 99 pure; vacuum deposited on glass; measured immediately after removed from vacuum chamber; calculated by authors from $p = 1 - \alpha$ using an incandescent tungsten lamp as source; $\theta = 10^\circ$, $\omega' = 2\pi$, reported error $\pm 0.5\%$. |
| 9 T25606 | Holland, L. and Williams, B.J. | 1955 | 0.46-0.60 | 298 | | The above specimen and conditions except exposed to the atmosphere for 8 days. |
| 10 T25606 | Holland, L. and Williams, B.J. | 1955 | 0.46-0.60 | 298 | | 99.99 pure; vacuum deposited on glass; measured immediately after removed from vacuum chamber; calculated by authors from $p = 1 - \alpha$ using an incandescent tungsten lamp as source; $\theta = 10^\circ$, $\omega' = 2\pi$, reported error $\pm 0.5\%$. |
| 11 T25606 | Holland, L. and Williams, B.J. | 1955 | 0.46-0.60 | 298 | | The above specimen and conditions except exposed to atmosphere for 8 days. |
| 12 T7159 | Wulff, J. | 1934 | 0.235-0.578 | 298 | | Disc; cold worked, annealed, etch tested, polished, stored in a solution of NaOH + NaF, washed and dried; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$, reported error 2%. |
| 13 T36320 | Davies, J.M. and Zagieboylo, W. | 1965 | 0.300-1.000 | 298 | | Sand blasted; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 14 T33512 | Leigh, C.H. | 1962 | 2.01-25.96 | 298 | | Polished; converted from $R(2\pi, 0^\circ)$; $\theta \sim 0^\circ$, $\omega' = 2\pi$. |
| 15 T33512 | Leigh, C.H. | 1962 | 1.57-25.94 | 298 | | The above specimen and conditions except after particle impact. |
| 16 T29648 | Geir, J.T., Possner, L., Test, A.J., Dunkle, R.V., and Bevans, J.T. | 1949 | 1.01-15.00 | ~298 | | Foil; data extracted from smooth curve; $\theta = 0^\circ$, $\omega' = 2\pi$, reported error 5%. |
| 17 T40413 | Schocken, K. and Fountain, J.A. | 1964 | 2.00-23.99 | 298 | | Polished; $\theta \sim 0^\circ$, $\theta' \sim 0^\circ$. |

TABLE 20-5. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (Wavelength Dependence) (continued)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---------------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 18 T40413 | Schocken, K. and Fountain, J.A. | 1964 | 2.00-23.99 | 298 | | The above specimen and conditions except cratered with spherical particles (100 μm diameter) of Zircalloy at 1.5 km sec ⁻¹ ; average crater diameter 123 μm ; average crater depth 289 μm ; Knoop hardness 22 (100 g load). |
| 19 T40413 | Schocken, K. and Fountain, J.A. | 1964 | 2.00-22.00 | 298 | | Different sample, the above specimen and conditions except cratered with spherical particles (100 μm diameter) of tungsten at 7 km sec ⁻¹ ; average crater diameter 54 μm ; average crater depth 183 μm . |

TABLE 20-6. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE) (CONTINUED)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|------------------|--------|
| CURVE 17 (CONT.) | |
| 10.00 | 0.980 |
| 12.00 | 0.981 |
| 14.00 | 0.980 |
| 16.00 | 0.980 |
| 18.00 | 0.980 |
| 20.00 | 0.979 |
| 22.00 | 0.979 |
| 23.99 | 0.973 |
| CURVE 18 | |
| T = 296. | |
| 2.00 | 0.897 |
| 4.00 | 0.912 |
| 5.99 | 0.933 |
| 5.00 | 0.945 |
| 10.00 | 0.954 |
| 12.00 | 0.952 |
| 14.00 | 0.954 |
| 16.00 | 0.955 |
| 18.00 | 0.955 |
| 20.00 | 0.955 |
| 22.00 | 0.946 |
| 23.99 | 0.946 |
| CURVE 19 | |
| T = 293. | |
| 2.00 | 0.569 |
| 4.00 | 0.576 |
| 5.99 | 0.731 |
| 6.00 | 0.741 |
| 10.00 | 0.757 |
| 12.00 | 0.777 |
| 14.00 | 0.786 |
| 16.00 | 0.789 |
| 18.00 | 0.793 |
| 20.00 | 0.792 |
| 22.00 | 0.792 |

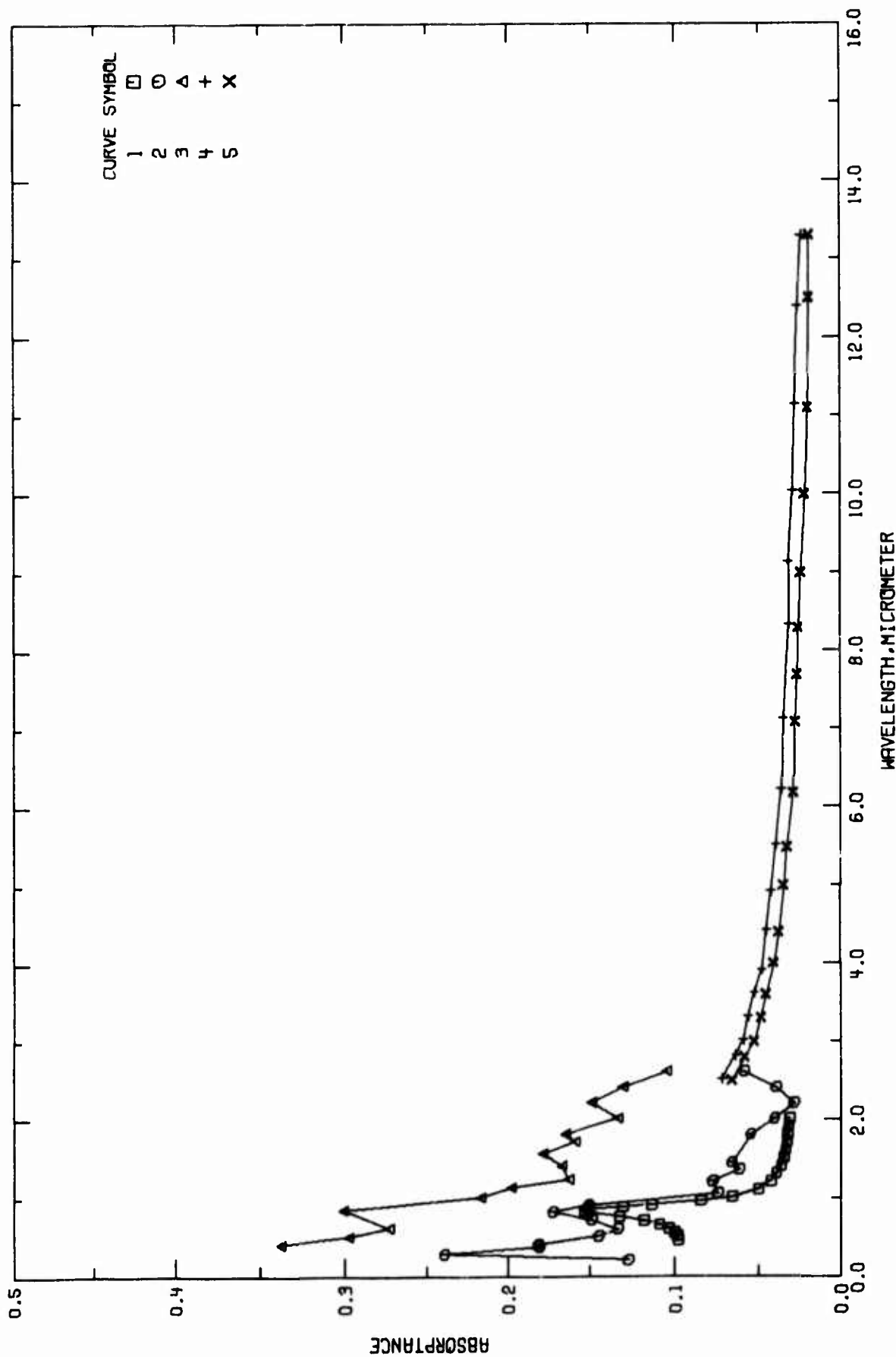


FIGURE 20-4. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE).

TABLE 20-7. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|---|------|---------------------------------|----------------------|-------------------------------|---|
| 1 T34454 | Brandenberg, W. M., Clausen, O. W., and McKeown, D. | 1966 | 0.45-2.00 | 298 | | Evaporated film; evaporation rate 300 \AA sec^{-1} at 2×10^{-1} mm Hg; measured in vacuum; aged 8 days before measurement; $\theta \sim 10^\circ$, reported error $\pm 1.4\%$. |
| 2 T32388 | Byrne, R. F. and Mancinelli, L. N. | 1954 | 0.204-2.600 | ~ 298 | | Data extracted from smooth curve; $\theta \sim 0^\circ$. |
| 3 T32388 | Byrne, R. F. and Mancinelli, L. N. | 1954 | 0.402-2.600 | ~ 298 | | Polished; data extracted from smooth curve; $\theta \sim 0^\circ$. |
| 4 A00003 | Harmon, N. F. (editor) | 1974 | 2.5-20.0 | 573 | | Bulk sample; mechanically polished. |
| 5 A00003 | Harmon, N. F. (editor) | 1974 | 2.5-20.0 | 293 | | The above specimen except at 293 K. |

TABLE 20-8. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α | λ | α | λ | α | λ | α |
|----------------|----------|----------------|----------|-----------|----------|-----------|----------|
| CURVE 1 | | | | | | | |
| T = 298. | | | | | | | |
| 0.45 | 0.0962 | 1.352 | 0.062 | 7.1 | 0.0344 | 19.9 | 0.0157 |
| 0.50 | 0.0567 | 1.449 | 0.067 | 6.3 | 0.0307 | | |
| 0.55 | 0.0301 | 1.798 | 0.055 | 9.1 | 0.0314 | | |
| 0.60 | 0.0107 | 2.000 | 0.040 | 10.0 | 0.0285 | | |
| 0.65 | 0.0096 | 2.200 | 0.029 | 11.1 | 0.0272 | | |
| 0.70 | 0.0129 | 2.400 | 0.039 | 12.7 | 0.0213 | | |
| 0.75 | 0.01331 | 2.600 | 0.059 | 13.3 | 0.0232 | | |
| 0.80 | 0.0111 | CURVE 3 | | | | | |
| 0.85 | 0.01233 | T = 298. | | | | | |
| 0.90 | 0.01501 | 0.402 | 0.038 | | | | |
| 0.975 | 0.01322 | 0.496 | 0.0298 | | | | |
| 1.00 | 0.01142 | 0.627 | 0.0273 | | | | |
| 1.05 | 0.00653 | 0.841 | 0.031 | | | | |
| 1.10 | 0.00498 | 0.997 | 0.0217 | | | | |
| 1.20 | 0.00420 | 1.119 | 0.0198 | | | | |
| 1.30 | 0.0037 | 1.220 | 0.0163 | | | | |
| 1.40 | 0.00357 | 1.397 | 0.0167 | | | | |
| 1.50 | 0.00311 | 1.553 | 0.0179 | | | | |
| 1.60 | 0.00321 | 1.704 | 0.0159 | | | | |
| 1.70 | 0.0022 | 1.800 | 0.0165 | | | | |
| 1.80 | 0.00319 | 2.000 | 0.0134 | | | | |
| 1.95 | 0.00213 | 2.200 | 0.0149 | | | | |
| 2.00 | 0.00358 | 2.400 | 0.0131 | | | | |
| | | 2.600 | 0.0125 | | | | |
| CURVE 2 | | | | | | | |
| T = 295. | | | | | | | |
| 0.204 | 0.0128 | 2.5 | 0.0721 | 2.5 | 0.0243 | 7.1 | 0.0277 |
| 0.231 | 0.0239 | 2.8 | 0.0642 | 3.0 | 0.0216 | 7.7 | 0.0255 |
| 0.307 | 0.0161 | 3.0 | 0.0593 | 3.3 | 0.0243 | 8.3 | 0.0257 |
| 0.401 | 0.0132 | 3.3 | 0.0503 | 3.6 | 0.0209 | 9.0 | 0.0243 |
| 0.500 | 0.0143 | 3.6 | 0.0562 | 4.0 | 0.0187 | 10.0 | 0.0216 |
| 0.597 | 0.0134 | 3.9 | 0.0522 | 4.0 | 0.0166 | 11.1 | 0.0209 |
| 0.709 | 0.0149 | 4.4 | 0.0474 | 4.4 | 0.0179 | 12.5 | 0.0187 |
| 0.815 | 0.0173 | 4.9 | 0.0445 | 4.9 | 0.0175 | 13.3 | 0.0166 |
| 0.895 | 0.0151 | 5.5 | 0.0359 | 5.5 | 0.0176 | 14.2 | 0.0179 |
| 1.078 | 0.0075 | 6.0 | 0.0354 | 6.0 | 0.0165 | 15.3 | 0.0175 |
| 1.200 | 0.0076 | | | | | 16.6 | 0.0176 |
| | | | | | | 17.3 | 0.0165 |
| | | | | | | 19.0 | 0.0159 |
| CURVE 4 | | | | | | | |
| T = 573. | | | | | | | |
| 2.5 | 0.0721 | 2.5 | 0.0243 | 2.5 | 0.0243 | 7.1 | 0.0277 |
| 2.8 | 0.0642 | 3.0 | 0.0216 | 3.0 | 0.0216 | 7.7 | 0.0255 |
| 3.0 | 0.0593 | 3.3 | 0.0243 | 3.3 | 0.0243 | 8.3 | 0.0257 |
| 3.3 | 0.0503 | 3.6 | 0.0209 | 3.6 | 0.0209 | 9.0 | 0.0243 |
| 3.6 | 0.0562 | 4.0 | 0.0187 | 4.0 | 0.0187 | 10.0 | 0.0216 |
| 3.9 | 0.0522 | 4.4 | 0.0179 | 4.4 | 0.0179 | 11.1 | 0.0209 |
| 4.4 | 0.0474 | 4.9 | 0.0175 | 4.9 | 0.0175 | 12.5 | 0.0187 |
| 4.9 | 0.0445 | 5.5 | 0.0176 | 5.5 | 0.0176 | 13.3 | 0.0166 |
| 5.5 | 0.0359 | 6.0 | 0.0165 | 6.0 | 0.0165 | 14.2 | 0.0179 |
| 6.0 | 0.0354 | | | | | 15.3 | 0.0175 |
| | | | | | | 16.6 | 0.0176 |
| | | | | | | 17.3 | 0.0165 |
| | | | | | | 19.0 | 0.0159 |

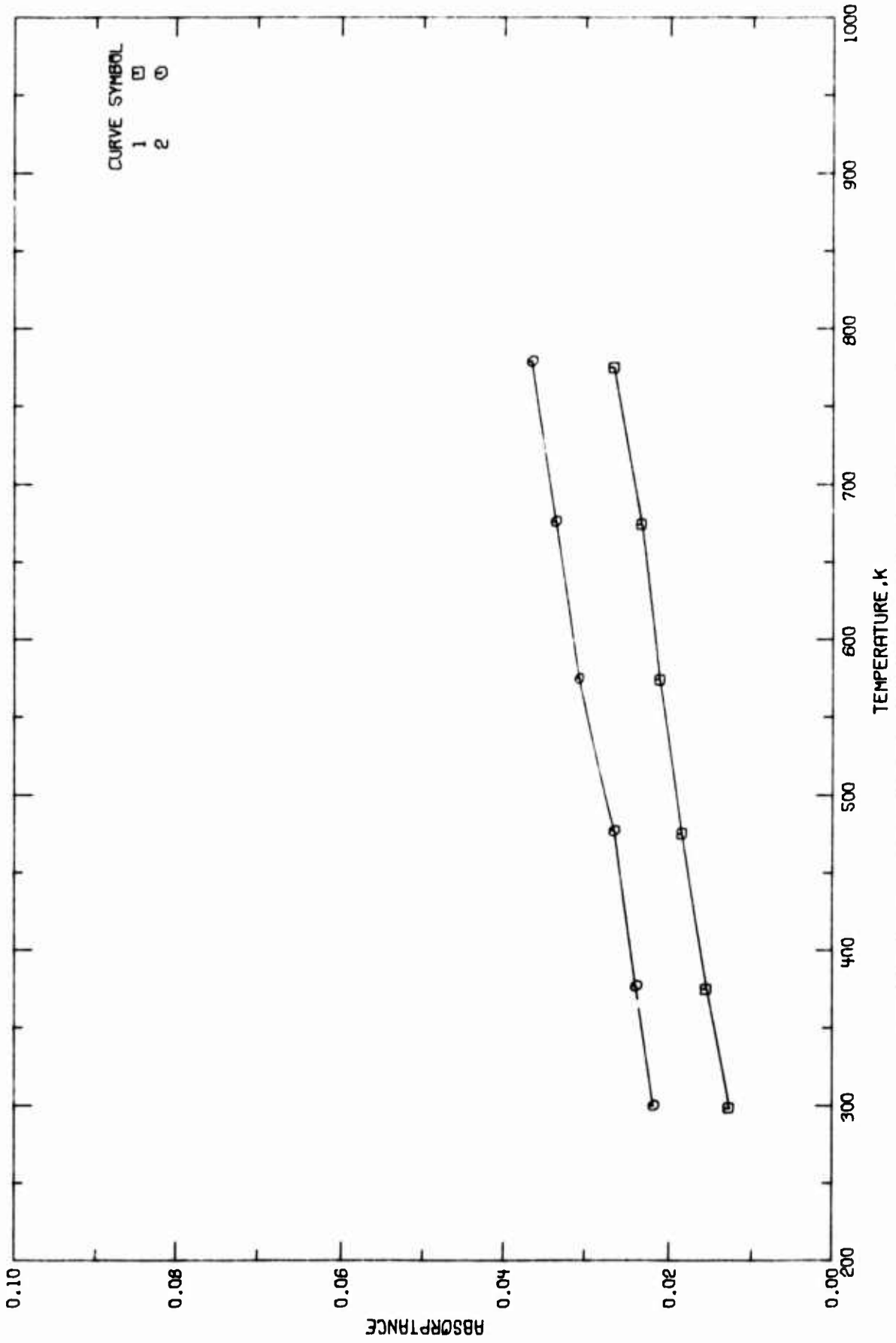


FIGURE 20-5. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE).

TABLE 20-9. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (Temperature Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|--------------------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00003 | Harmon, N.F. (editor) | 1974 | 5.0 | 300-779 | | Film; fast-evaporated; absorptance obtained for wavelength 5.0 μm at various temperatures. |
| 2 A00003 | Harmon, N.F. (editor) | 1974 | 10.0 | 298-775 | | The above specimen except wavelength 10.0 μm . |

TABLE 20-10. EXPERIMENTAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINUM (TEMPERATURE DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| T | α |
|------------------|----------|
| CURVE 1 | |
| $\lambda = 10.0$ | |
| 295. | 0.0129 |
| 375. | 0.0155 |
| 475. | 0.0185 |
| 574. | 0.0213 |
| 674. | 0.0234 |
| 775. | 0.0265 |
| CURVE 2 | |
| $\lambda = 5.0$ | |
| 300. | 0.0219 |
| 377. | 0.0239 |
| 477. | 0.0264 |
| 575. | 0.0328 |
| 676. | 0.0337 |
| 779. | 0.0356 |

To isolate the individual surface characteristics is a difficult task. For most materials it is not practical to alter one characteristic without causing an influence on another. The control of the many variables required to study surface characterization in a logical manner is a complex problem. As a result only the simplest of surface profiles or compositional effects have been studied or are understood. One of the most important influences on the radiative properties of metals arises from surface roughness.

Because of the difficulties mentioned above, data analysis and evaluation is not a straight forward task; some logical but not exact means should be used in the generation of the most probable values for the properties of our interest. Although the radiative properties could be strongly dependent upon the process of applying the metallized thin films, we considered them as mechanically polished surface as a first approximation and decided to use the classical model of Hagen and Rubens with some modification in the interpretation of the selected emittance data for mechanically polished surfaces. Details of such modification are discussed in Section 2 and Eq. (2.5-5) is the resulted expression.

Reliable and accurate available data on the normal spectral emittance of mechanically polished aluminum surface were obtained by converting the data sets, curves 4 and 5 of Figure 20-4, from absorptance to emittance using Kirchhoff's law. Data for curves 4 and 5 were measured at temperatures of 573 K and 293 K respectively. By a least squares calculation the following equation was found to fit the selected data with uncertainties of less than $\pm 10\%$ for wavelength range 2.5 to 20 μm .

$$\begin{aligned} \epsilon(0, \lambda) = & 0.0007 + 0.0644 \left[\frac{1 + 0.00429 (T-293)}{\lambda - 2.279} \right]^{1/2} \\ & - 0.0206 \left[\frac{1 + 0.00429 (T-293)}{\lambda - 2.279} \right] \\ & + 0.00234 \left[\frac{1 + 0.00429 (T-293)}{\lambda - 2.279} \right]^{3/2}, \end{aligned} \quad (4.20-1)$$

$$\alpha(0, \lambda) = \epsilon(0, \lambda), \quad (4.20-2)$$

and

$$\rho(0, 2\pi, \lambda) = 1 - \alpha(0, \lambda), \quad (4.20-3)$$

where λ is in units of μm and T in K. These three equations are used to generate the most probable values on the normal spectral radiative properties for the aluminized grafoil.

a. Normal Spectral Emittance (Wavelength Dependence)

Normal spectral emittance of aluminized grafoil is calculated from Eq. (4.20-1) and listed in Table 20-11 and plotted in Figure 20-6. The values generated are considered as provisional (about $\pm 25\%$ uncertainty) since they are estimated based on the aluminum data. Provisional values are presented at five temperatures, 293, 450, 600, 750, and 850 K. Note that the provisional values are for the mechanically polished surface only. Values of true surfaces are expected to deviate from those listed. However, the tabulated values are believed to be reasonable for those surfaces of roughness less than $0.5 \mu\text{m}$.

TABLE 20-11. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | | | | | |
|-----------|------------|-------------------------------------|------------|-----------|-------------------------------------|-----------|------------|-------------------------------------|------------|-------|-------------------------------------|------|-------|-------------------------------------|
| 2.5 | 0.067 | MECHANICALLY POLISHED T = 293 | 2.5 | 0.071 | MECHANICALLY POLISHED T = 450 | 2.5 | 0.073 | MECHANICALLY POLISHED T = 600 | 2.5 | 0.075 | MECHANICALLY POLISHED T = 750 | 2.5 | 0.076 | MECHANICALLY POLISHED T = 850 |
| 2.8 | 0.057 | | 2.8 | 0.063 | | 2.8 | 0.067 | | 2.8 | 0.059 | | 2.8 | 0.070 | |
| 3.0 | 0.052 | | 3.0 | 0.059 | | 3.0 | 0.063 | | 3.0 | 0.066 | | 3.0 | 0.067 | |
| 3.5 | 0.044 | | 3.5 | 0.052 | | 3.5 | 0.056 | | 3.5 | 0.060 | | 3.5 | 0.062 | |
| 3.8 | 0.041 | | 3.8 | 0.046 | | 3.8 | 0.053 | | 3.8 | 0.057 | | 3.8 | 0.059 | |
| 4.0 | 0.035 | | 4.0 | 0.045 | | 4.0 | 0.051 | | 4.0 | 0.055 | | 4.0 | 0.057 | |
| 4.5 | 0.033 | | 4.5 | 0.043 | | 4.5 | 0.047 | | 4.5 | 0.051 | | 4.5 | 0.053 | |
| 5.0 | 0.031 | | 5.0 | 0.040 | | 5.0 | 0.044 | | 5.0 | 0.048 | | 5.0 | 0.050 | |
| 5.5 | 0.029 | | 5.5 | 0.037 | | 5.5 | 0.042 | | 5.5 | 0.046 | | 5.5 | 0.048 | |
| 6.0 | 0.027 | | 6.0 | 0.035 | | 6.0 | 0.040 | | 6.0 | 0.043 | | 6.0 | 0.045 | |
| 6.5 | 0.026 | | 6.5 | 0.034 | | 6.5 | 0.038 | | 6.5 | 0.042 | | 6.5 | 0.044 | |
| 7.0 | 0.025 | | 7.0 | 0.032 | | 7.0 | 0.037 | | 7.0 | 0.040 | | 7.0 | 0.042 | |
| 7.5 | 0.024 | | 7.5 | 0.031 | | 7.5 | 0.035 | | 7.5 | 0.039 | | 7.5 | 0.041 | |
| 8.0 | 0.023 | | 8.0 | 0.030 | | 8.0 | 0.034 | | 8.0 | 0.037 | | 8.0 | 0.039 | |
| 8.5 | 0.023 | | 8.5 | 0.029 | | 8.5 | 0.033 | | 8.5 | 0.036 | | 8.5 | 0.038 | |
| 9.0 | 0.022 | | 9.0 | 0.028 | | 9.0 | 0.032 | | 9.0 | 0.035 | | 9.0 | 0.037 | |
| 9.5 | 0.021 | | 9.5 | 0.027 | | 9.5 | 0.031 | | 9.5 | 0.034 | | 9.5 | 0.036 | |
| 10.0 | 0.021 | | 10.0 | 0.026 | | 10.0 | 0.030 | | 10.0 | 0.033 | | 10.0 | 0.035 | |
| 10.5 | 0.020 | | 10.5 | 0.025 | | 10.5 | 0.029 | | 10.5 | 0.032 | | 10.5 | 0.034 | |
| 11.0 | 0.020 | | 11.0 | 0.025 | | 11.0 | 0.028 | | 11.0 | 0.031 | | 11.0 | 0.033 | |
| 11.5 | 0.019 | | 11.5 | 0.024 | | 11.5 | 0.028 | | 11.5 | 0.031 | | 11.5 | 0.033 | |
| 12.0 | 0.019 | | 12.0 | 0.024 | | 12.0 | 0.026 | | 12.0 | 0.030 | | 12.0 | 0.032 | |
| 12.5 | 0.018 | | 12.5 | 0.023 | | 12.5 | 0.026 | | 12.5 | 0.029 | | 12.5 | 0.031 | |
| 13.0 | 0.018 | | 13.0 | 0.023 | | 13.0 | 0.026 | | 13.0 | 0.029 | | 13.0 | 0.031 | |
| 13.5 | 0.017 | | 13.5 | 0.022 | | 13.5 | 0.025 | | 13.5 | 0.028 | | 13.5 | 0.030 | |
| 14.0 | 0.017 | | 14.0 | 0.022 | | 14.0 | 0.025 | | 14.0 | 0.028 | | 14.0 | 0.030 | |
| 14.5 | 0.017 | | 14.5 | 0.022 | | 14.5 | 0.025 | | 14.5 | 0.028 | | 14.5 | 0.029 | |
| 15.0 | 0.017 | | 15.0 | 0.021 | | 15.0 | 0.025 | | 15.0 | 0.028 | | 15.0 | 0.029 | |

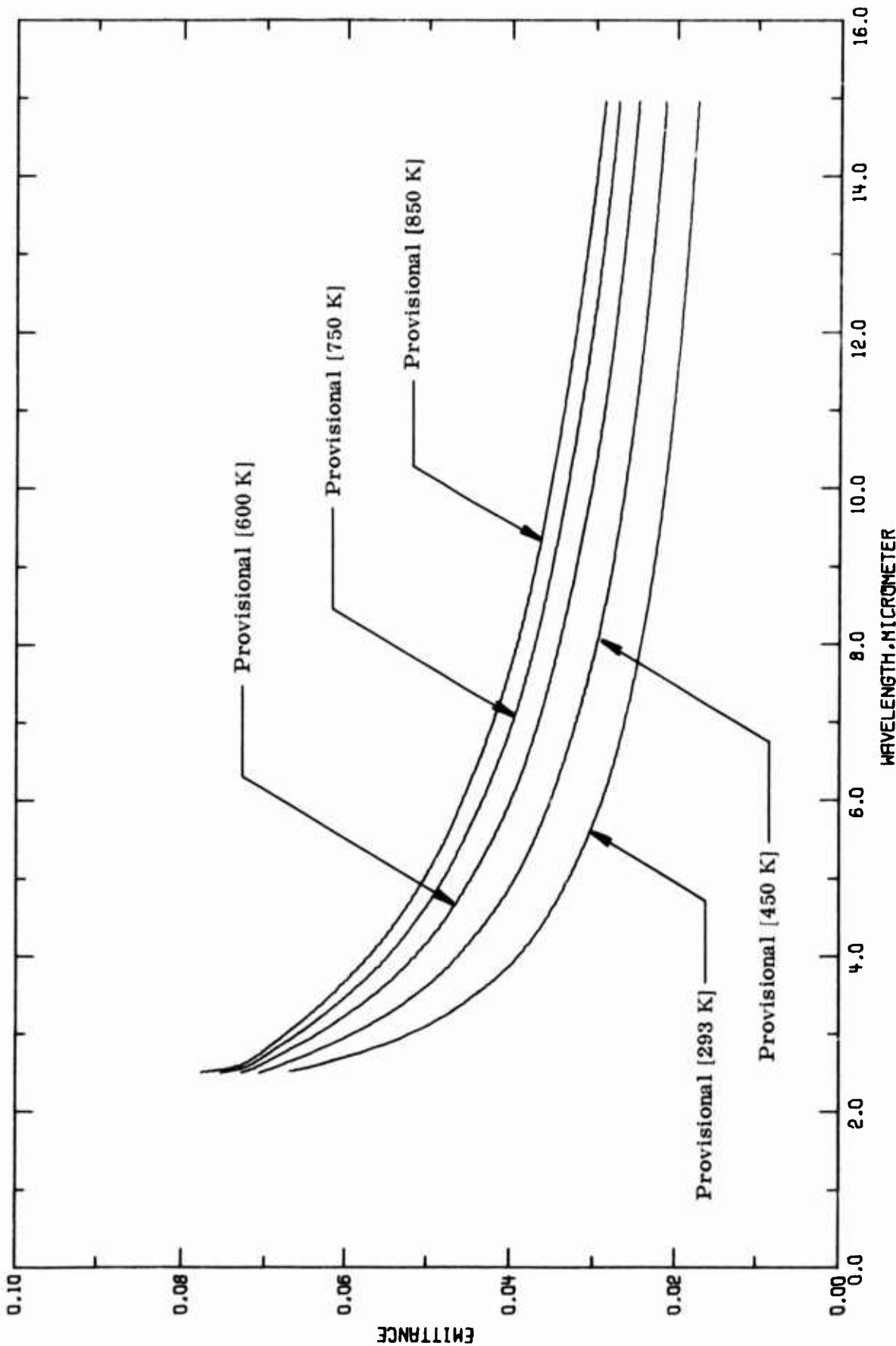


FIGURE 20-6. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE).

b. Normal Spectral Emittance (Temperature Dependence)

The normal spectral emittance as a function of temperature is given in Table 20-12 and Figure 20-7. The generated values are considered as provisional (uncertainty $\pm 25\%$). The plot clearly shows that emittance for a given wavelength does not vary appreciably for a wide temperature range. Note that the melting point of aluminum at about 930 K is not far from the ending point (about 880 K) of each curve. It seems that the curves can be extrapolated to or beyond the melting point. However, there is no definite evidence to support this attempt.

TABLE 26-12. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|---------------------------------------|------------|-------|------------|-------|------------|-------|------------|
| MECHANICALLY POLISHED $\lambda = 2.8$ | | | | | | | |
| 250.0 | 0.054 | 250.0 | 0.038 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.057 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.061 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.062 | 400.0 | 0.046 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.063 | 450.0 | 0.048 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.066 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.067 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.068 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 700.0 | 0.068 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| 800.0 | 0.069 | 800.0 | 0.058 | 800.0 | 0.049 | 800.0 | 0.033 |
| 850.0 | 0.070 | 850.0 | 0.059 | 850.0 | 0.050 | 850.0 | 0.034 |
| 880.0 | 0.070 | 880.0 | 0.059 | 880.0 | 0.051 | 880.0 | 0.035 |
| MECHANICALLY POLISHED $\lambda = 5.0$ | | | | | | | |
| 250.0 | 0.030 | 250.0 | 0.030 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.033 | 293.0 | 0.033 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.033 | 300.0 | 0.033 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.036 | 350.0 | 0.036 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.038 | 400.0 | 0.038 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.040 | 450.0 | 0.040 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.041 | 500.0 | 0.041 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.043 | 550.0 | 0.043 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.044 | 600.0 | 0.044 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.046 | 650.0 | 0.046 | 650.0 | 0.046 | 650.0 | 0.030 |
| 700.0 | 0.047 | 700.0 | 0.047 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.048 | 750.0 | 0.048 | 750.0 | 0.048 | 750.0 | 0.032 |
| 800.0 | 0.049 | 800.0 | 0.049 | 800.0 | 0.049 | 800.0 | 0.033 |
| 850.0 | 0.050 | 850.0 | 0.050 | 850.0 | 0.050 | 850.0 | 0.034 |
| 880.0 | 0.051 | 880.0 | 0.051 | 880.0 | 0.051 | 880.0 | 0.035 |

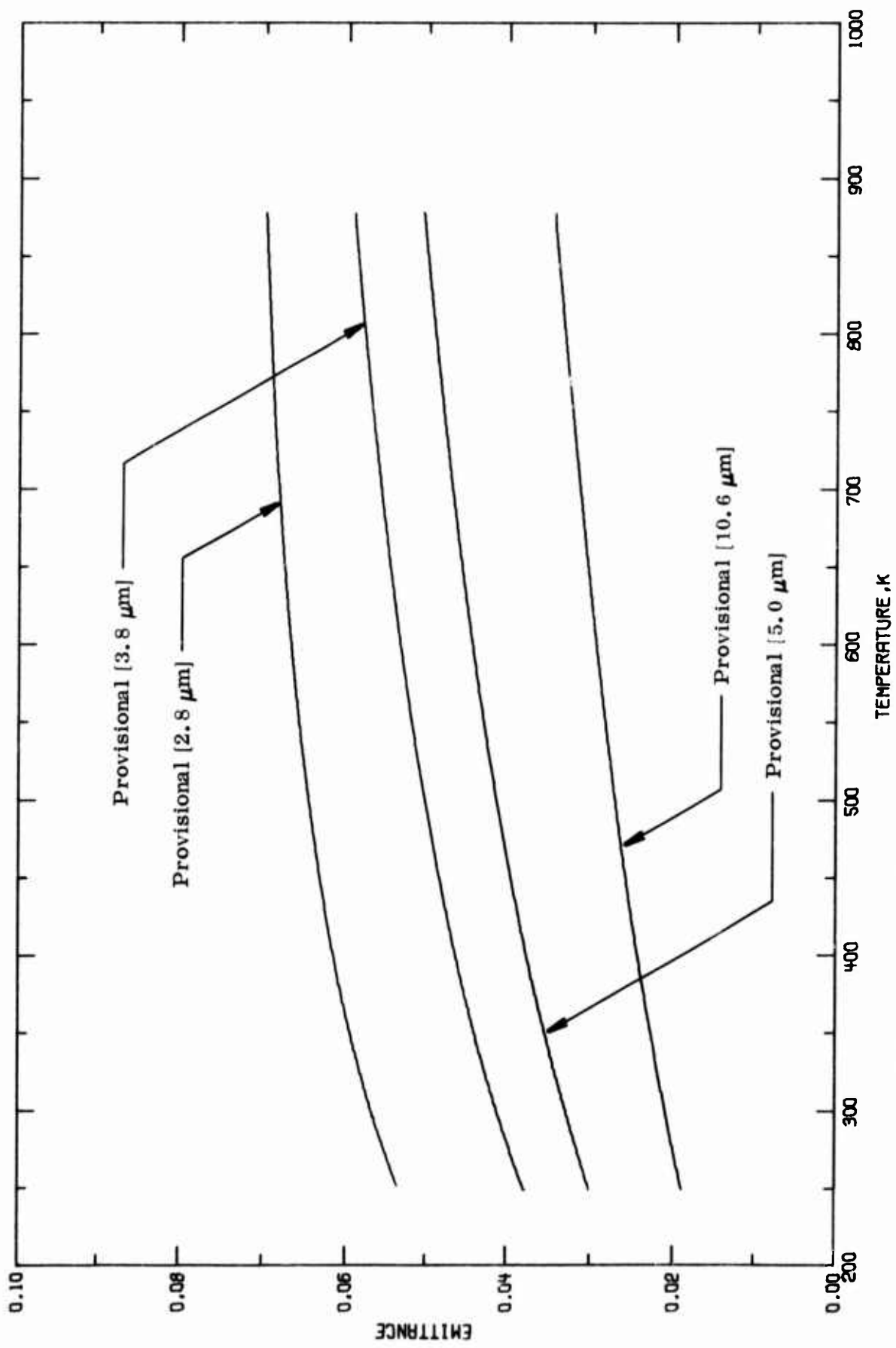


FIGURE 20-7. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

As given in Table 20-13 and plotted in Figure 20-8 the normal spectral reflectance of aluminized grafoil is calculated by assuming that energy loss of the impinging radiation is entirely due to absorption. The result is remarkably good as one can see by comparing Figures 20-3 and 20-8. Since the data analysis is totally based on the available data of aluminum, allowance is given in the estimation of the predicted values. An estimated uncertainty of $\pm 20\%$ is given to the calculated values so that the estimated values can be used for most of the true surfaces.

TABLE 20-13. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | | ρ | | λ | | ρ | | λ | | ρ | | λ | | ρ | |
|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|
| MECHANICALLY POLISHED T = 233 | | MECHANICALLY POLISHED T = 450 | | MECHANICALLY POLISHED T = 500 | | MECHANICALLY POLISHED T = 750 | | MECHANICALLY POLISHED T = 850 | | MECHANICALLY POLISHED T = 850 | | MECHANICALLY POLISHED T = 850 | | MECHANICALLY POLISHED T = 850 | |
| 2.5 | 0.933 | 2.5 | 0.929 | 2.5 | 0.927 | 2.5 | 0.925 | 2.5 | 0.925 | 2.5 | 0.925 | 2.5 | 0.925 | 2.5 | 0.922 |
| 2.8 | 0.943 | 2.8 | 0.937 | 2.8 | 0.933 | 2.8 | 0.931 | 2.8 | 0.931 | 2.8 | 0.931 | 2.8 | 0.931 | 2.8 | 0.930 |
| 3.0 | 0.948 | 3.0 | 0.941 | 3.0 | 0.937 | 3.0 | 0.934 | 3.0 | 0.934 | 3.0 | 0.934 | 3.0 | 0.934 | 3.0 | 0.933 |
| 3.5 | 0.956 | 3.5 | 0.948 | 3.5 | 0.944 | 3.5 | 0.940 | 3.5 | 0.940 | 3.5 | 0.940 | 3.5 | 0.940 | 3.5 | 0.938 |
| 3.8 | 0.959 | 3.8 | 0.952 | 3.8 | 0.947 | 3.8 | 0.943 | 3.8 | 0.943 | 3.8 | 0.943 | 3.8 | 0.943 | 3.8 | 0.941 |
| 4.0 | 0.951 | 4.0 | 0.954 | 4.0 | 0.949 | 4.0 | 0.945 | 4.0 | 0.945 | 4.0 | 0.945 | 4.0 | 0.945 | 4.0 | 0.943 |
| 4.5 | 0.955 | 4.5 | 0.957 | 4.5 | 0.953 | 4.5 | 0.949 | 4.5 | 0.949 | 4.5 | 0.949 | 4.5 | 0.949 | 4.5 | 0.947 |
| 5.0 | 0.957 | 5.0 | 0.959 | 5.0 | 0.956 | 5.0 | 0.952 | 5.0 | 0.952 | 5.0 | 0.952 | 5.0 | 0.952 | 5.0 | 0.950 |
| 5.5 | 0.959 | 5.5 | 0.963 | 5.5 | 0.958 | 5.5 | 0.954 | 5.5 | 0.954 | 5.5 | 0.954 | 5.5 | 0.954 | 5.5 | 0.952 |
| 6.0 | 0.971 | 6.0 | 0.955 | 6.0 | 0.950 | 6.0 | 0.947 | 6.0 | 0.947 | 6.0 | 0.947 | 6.0 | 0.947 | 6.0 | 0.945 |
| 6.5 | 0.973 | 6.5 | 0.969 | 6.5 | 0.963 | 6.5 | 0.959 | 6.5 | 0.959 | 6.5 | 0.959 | 6.5 | 0.959 | 6.5 | 0.955 |
| 7.0 | 0.974 | 7.0 | 0.966 | 7.0 | 0.963 | 7.0 | 0.960 | 7.0 | 0.960 | 7.0 | 0.960 | 7.0 | 0.960 | 7.0 | 0.958 |
| 7.5 | 0.975 | 7.5 | 0.969 | 7.5 | 0.966 | 7.5 | 0.963 | 7.5 | 0.963 | 7.5 | 0.963 | 7.5 | 0.963 | 7.5 | 0.960 |
| 8.0 | 0.976 | 8.0 | 0.976 | 8.0 | 0.966 | 8.0 | 0.964 | 8.0 | 0.964 | 8.0 | 0.964 | 8.0 | 0.964 | 8.0 | 0.961 |
| 8.5 | 0.977 | 8.5 | 0.971 | 8.5 | 0.967 | 8.5 | 0.964 | 8.5 | 0.964 | 8.5 | 0.964 | 8.5 | 0.964 | 8.5 | 0.962 |
| 9.0 | 0.977 | 9.0 | 0.972 | 9.0 | 0.968 | 9.0 | 0.965 | 9.0 | 0.965 | 9.0 | 0.965 | 9.0 | 0.965 | 9.0 | 0.963 |
| 9.5 | 0.978 | 9.5 | 0.973 | 9.5 | 0.969 | 9.5 | 0.966 | 9.5 | 0.966 | 9.5 | 0.966 | 9.5 | 0.966 | 9.5 | 0.964 |
| 10.0 | 0.979 | 10.0 | 0.974 | 10.0 | 0.970 | 10.0 | 0.967 | 10.0 | 0.967 | 10.0 | 0.967 | 10.0 | 0.967 | 10.0 | 0.965 |
| 10.5 | 0.979 | 10.5 | 0.974 | 10.5 | 0.971 | 10.5 | 0.968 | 10.5 | 0.968 | 10.5 | 0.968 | 10.5 | 0.968 | 10.5 | 0.966 |
| 11.0 | 0.980 | 11.0 | 0.975 | 11.0 | 0.971 | 11.0 | 0.968 | 11.0 | 0.968 | 11.0 | 0.968 | 11.0 | 0.968 | 11.0 | 0.967 |
| 11.5 | 0.980 | 11.5 | 0.975 | 11.5 | 0.972 | 11.5 | 0.969 | 11.5 | 0.969 | 11.5 | 0.969 | 11.5 | 0.969 | 11.5 | 0.967 |
| 12.0 | 0.981 | 12.0 | 0.976 | 12.0 | 0.972 | 12.0 | 0.970 | 12.0 | 0.970 | 12.0 | 0.970 | 12.0 | 0.970 | 12.0 | 0.968 |
| 12.5 | 0.981 | 12.5 | 0.976 | 12.5 | 0.973 | 12.5 | 0.971 | 12.5 | 0.971 | 12.5 | 0.971 | 12.5 | 0.971 | 12.5 | 0.969 |
| 13.0 | 0.981 | 13.0 | 0.977 | 13.0 | 0.974 | 13.0 | 0.971 | 13.0 | 0.971 | 13.0 | 0.971 | 13.0 | 0.971 | 13.0 | 0.969 |
| 13.5 | 0.982 | 13.5 | 0.977 | 13.5 | 0.974 | 13.5 | 0.971 | 13.5 | 0.971 | 13.5 | 0.971 | 13.5 | 0.971 | 13.5 | 0.970 |
| 14.0 | 0.982 | 14.0 | 0.976 | 14.0 | 0.975 | 14.0 | 0.972 | 14.0 | 0.972 | 14.0 | 0.972 | 14.0 | 0.972 | 14.0 | 0.970 |
| 14.5 | 0.983 | 14.5 | 0.978 | 14.5 | 0.975 | 14.5 | 0.972 | 14.5 | 0.972 | 14.5 | 0.972 | 14.5 | 0.972 | 14.5 | 0.971 |
| 15.0 | 0.983 | 15.0 | 0.979 | 15.0 | 0.975 | 15.0 | 0.973 | 15.0 | 0.973 | 15.0 | 0.973 | 15.0 | 0.973 | 15.0 | 0.971 |

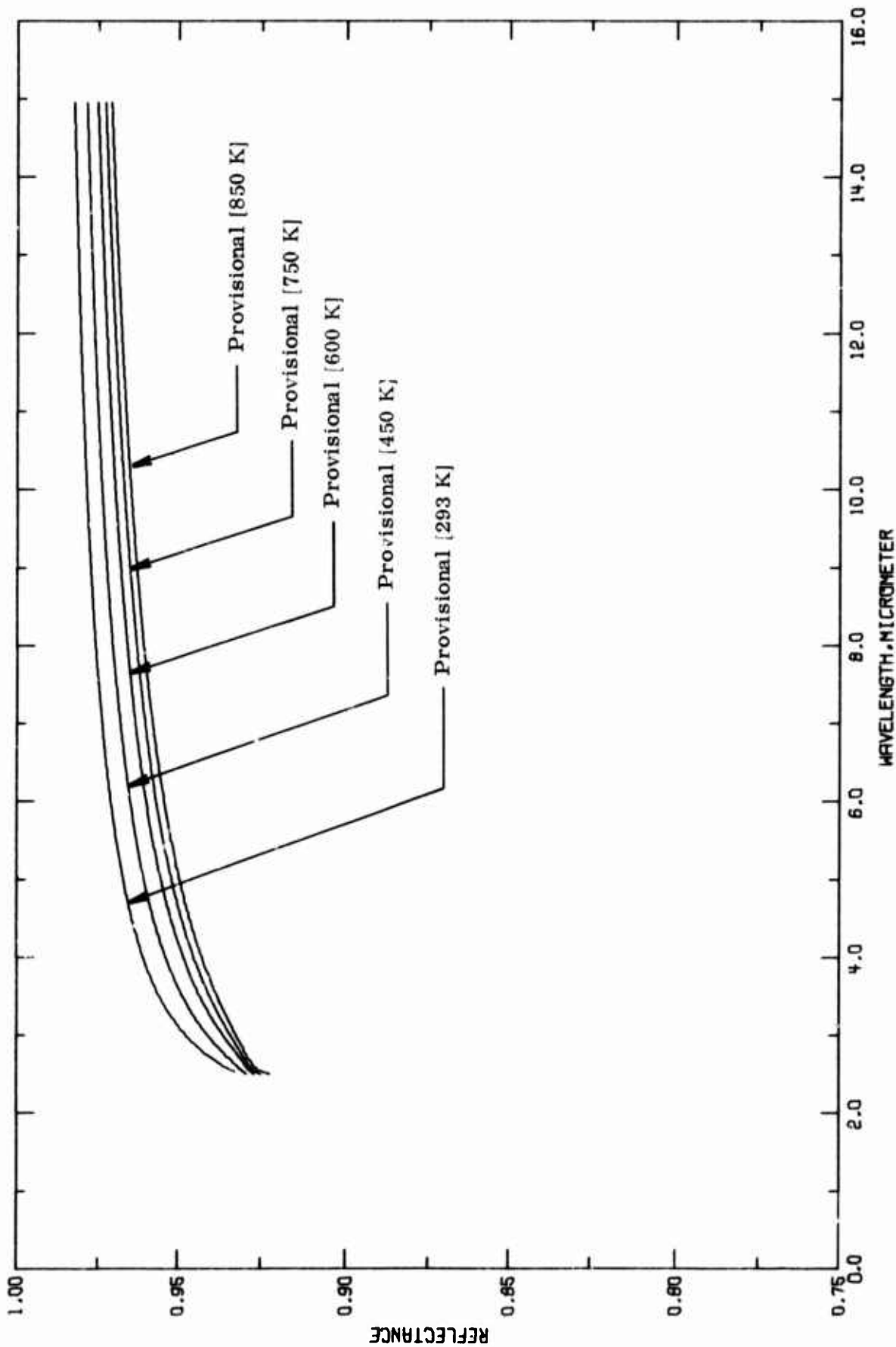


FIGURE 20-8. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE).

d. Normal Spectral Reflectance (Temperature Dependence)

In Table 20-14, the provisional values of the normal spectral reflectance are given with an estimated uncertainty of $\pm 20\%$. The variation of the property as a function of temperature is demonstrated in Figure 20-9. For a given wavelength, the normal spectral reflectance remains as a constant from room temperature up to near the melting point of the material. At higher temperatures our knowledge on this property is lacking. However, it seems that a linear extrapolation of the curve to and above the melting point can be used with uncertainty of no more than $\pm 35\%$.

TABLE 20-1*. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| $\lambda = 2.8$ | | $\lambda = 3.8$ | | $\lambda = 5.0$ | | $\lambda = 10.6$ | |
|-----------------------|--------|-----------------------|--------|-----------------------|--------|-----------------------|--------|
| T | ρ | T | ρ | T | ρ | T | ρ |
| MECHANICALLY POLISHED | | MECHANICALLY POLISHED | | MECHANICALLY POLISHED | | MECHANICALLY POLISHED | |
| 250.0 | 0.946 | 250.0 | 0.962 | 250.0 | 0.970 | 250.0 | 0.981 |
| 300.0 | 0.945 | 293.0 | 0.959 | 293.0 | 0.967 | 293.0 | 0.979 |
| 350.0 | 0.943 | 300.0 | 0.959 | 300.0 | 0.967 | 300.0 | 0.979 |
| 400.0 | 0.940 | 350.0 | 0.956 | 350.0 | 0.964 | 350.0 | 0.977 |
| 450.0 | 0.938 | 400.0 | 0.954 | 400.0 | 0.962 | 400.0 | 0.976 |
| 500.0 | 0.937 | 450.0 | 0.952 | 450.0 | 0.960 | 450.0 | 0.974 |
| 550.0 | 0.935 | 500.0 | 0.950 | 500.0 | 0.959 | 500.0 | 0.973 |
| 600.0 | 0.934 | 550.0 | 0.948 | 550.0 | 0.957 | 550.0 | 0.972 |
| 650.0 | 0.933 | 600.0 | 0.947 | 600.0 | 0.956 | 600.0 | 0.971 |
| 700.0 | 0.932 | 650.0 | 0.945 | 650.0 | 0.954 | 650.0 | 0.970 |
| 750.0 | 0.931 | 700.0 | 0.944 | 700.0 | 0.953 | 700.0 | 0.969 |
| 800.0 | 0.931 | 750.0 | 0.943 | 750.0 | 0.952 | 750.0 | 0.968 |
| 850.0 | 0.930 | 800.0 | 0.942 | 800.0 | 0.951 | 800.0 | 0.967 |
| 900.0 | 0.930 | 850.0 | 0.941 | 850.0 | 0.950 | 850.0 | 0.966 |
| 950.0 | 0.930 | 900.0 | 0.941 | 900.0 | 0.949 | 900.0 | 0.965 |

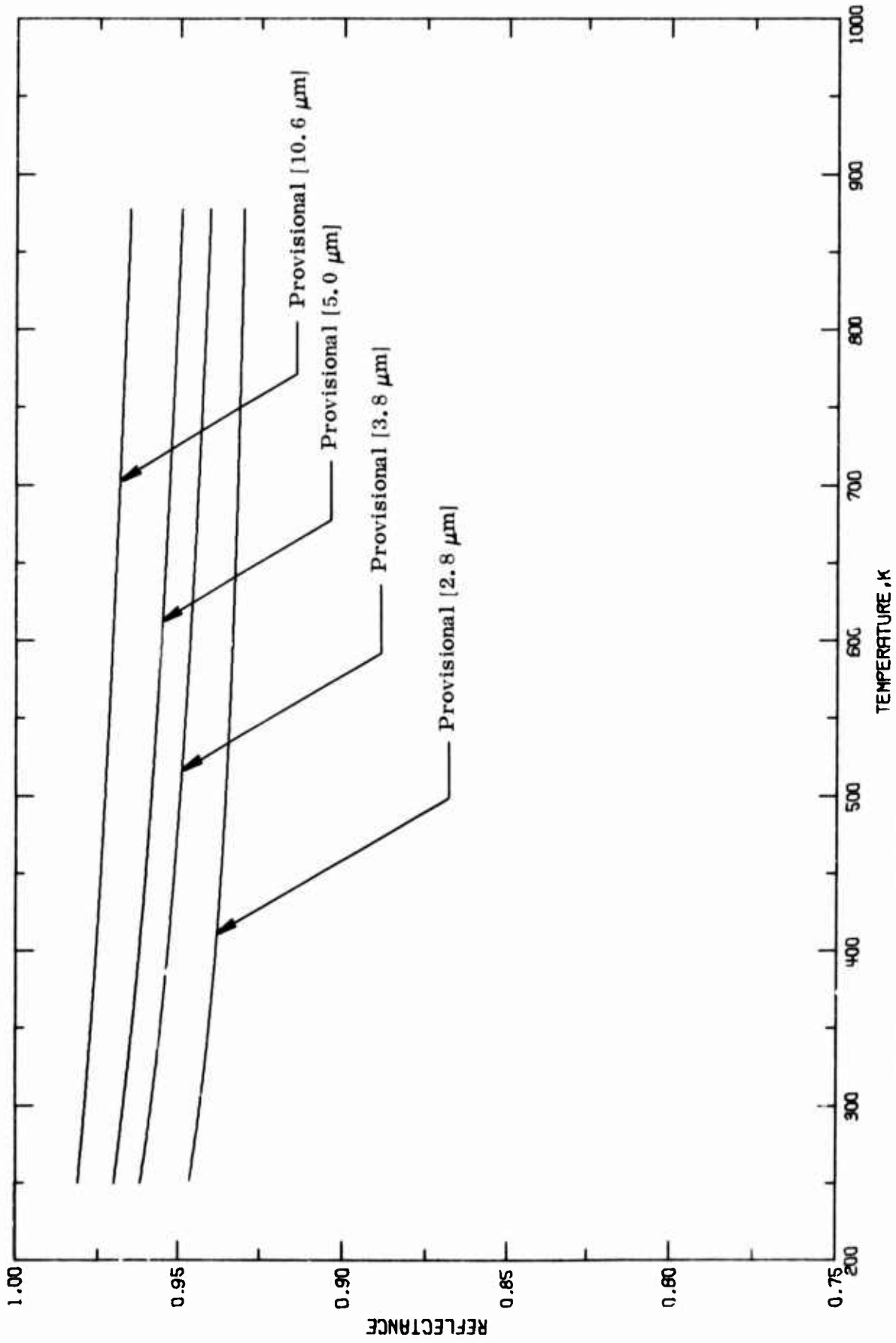


FIGURE 20-9. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

The normal spectral absorptance is obtained from reflectance according to the Kirchhoff's law, and is numerically equal to the emittance. The absorptance varies appreciably for wavelengths lower than $4.0 \mu\text{m}$ and remains practically unchanged for longer wavelengths. The generated provisional values with $\pm 25\%$ uncertainty are given in Table 20-15 and plotted in Figure 20-10.

TABLE 23-15. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α | λ | α | λ | α | λ | α | λ | α |
|-------------------------------------|----------|-------------------------------------|----------|-------------------------------------|----------|-------------------------------------|----------|-------------------------------------|----------|
| MECHANICALLY POLISHED T = 293 | | MECHANICALLY POLISHED T = 450 | | MECHANICALLY POLISHED T = 600 | | MECHANICALLY POLISHED T = 750 | | MECHANICALLY POLISHED T = 850 | |
| 2.5 | 0.057 | 2.5 | 0.071 | 2.5 | 0.073 | 2.5 | 0.075 | 2.5 | 0.076 |
| 2.8 | 0.057 | 2.8 | 0.063 | 2.8 | 0.067 | 2.8 | 0.069 | 2.8 | 0.070 |
| 3.0 | 0.052 | 3.0 | 0.059 | 3.0 | 0.063 | 3.0 | 0.065 | 3.0 | 0.067 |
| 3.5 | 0.044 | 3.5 | 0.052 | 3.5 | 0.055 | 3.5 | 0.060 | 3.5 | 0.062 |
| 3.8 | 0.041 | 3.8 | 0.049 | 3.8 | 0.053 | 3.8 | 0.057 | 3.8 | 0.059 |
| 4.0 | 0.039 | 4.0 | 0.046 | 4.0 | 0.051 | 4.0 | 0.055 | 4.0 | 0.057 |
| 4.5 | 0.033 | 4.5 | 0.043 | 4.5 | 0.047 | 4.5 | 0.051 | 4.5 | 0.053 |
| 5.0 | 0.031 | 5.0 | 0.040 | 5.0 | 0.044 | 5.0 | 0.048 | 5.0 | 0.050 |
| 5.5 | 0.029 | 5.5 | 0.037 | 5.5 | 0.042 | 5.5 | 0.046 | 5.5 | 0.048 |
| 6.0 | 0.027 | 6.0 | 0.035 | 6.0 | 0.040 | 6.0 | 0.044 | 6.0 | 0.046 |
| 6.5 | 0.027 | 6.5 | 0.034 | 6.5 | 0.039 | 6.5 | 0.042 | 6.5 | 0.044 |
| 7.0 | 0.026 | 7.0 | 0.032 | 7.0 | 0.037 | 7.0 | 0.040 | 7.0 | 0.042 |
| 7.5 | 0.025 | 7.5 | 0.031 | 7.5 | 0.035 | 7.5 | 0.039 | 7.5 | 0.040 |
| 8.0 | 0.024 | 8.0 | 0.030 | 8.0 | 0.034 | 8.0 | 0.037 | 8.0 | 0.039 |
| 8.5 | 0.023 | 8.5 | 0.029 | 8.5 | 0.033 | 8.5 | 0.036 | 8.5 | 0.038 |
| 9.0 | 0.023 | 9.0 | 0.028 | 9.0 | 0.032 | 9.0 | 0.035 | 9.0 | 0.037 |
| 9.5 | 0.022 | 9.5 | 0.027 | 9.5 | 0.031 | 9.5 | 0.034 | 9.5 | 0.036 |
| 10.0 | 0.021 | 10.0 | 0.026 | 10.0 | 0.030 | 10.0 | 0.033 | 10.0 | 0.035 |
| 10.5 | 0.021 | 10.5 | 0.026 | 10.5 | 0.029 | 10.5 | 0.032 | 10.5 | 0.034 |
| 11.0 | 0.021 | 11.0 | 0.025 | 11.0 | 0.028 | 11.0 | 0.031 | 11.0 | 0.033 |
| 11.5 | 0.020 | 11.5 | 0.025 | 11.5 | 0.028 | 11.5 | 0.031 | 11.5 | 0.033 |
| 12.0 | 0.019 | 12.0 | 0.024 | 12.0 | 0.028 | 12.0 | 0.031 | 12.0 | 0.032 |
| 12.5 | 0.019 | 12.5 | 0.024 | 12.5 | 0.027 | 12.5 | 0.030 | 12.5 | 0.032 |
| 13.0 | 0.019 | 13.0 | 0.023 | 13.0 | 0.026 | 13.0 | 0.029 | 13.0 | 0.031 |
| 13.5 | 0.018 | 13.5 | 0.023 | 13.5 | 0.026 | 13.5 | 0.029 | 13.5 | 0.030 |
| 14.0 | 0.018 | 14.0 | 0.022 | 14.0 | 0.025 | 14.0 | 0.028 | 14.0 | 0.030 |
| 14.5 | 0.017 | 14.5 | 0.022 | 14.5 | 0.025 | 14.5 | 0.028 | 14.5 | 0.029 |
| 15.0 | 0.017 | 15.0 | 0.021 | 15.0 | 0.025 | 15.0 | 0.027 | 15.0 | 0.029 |

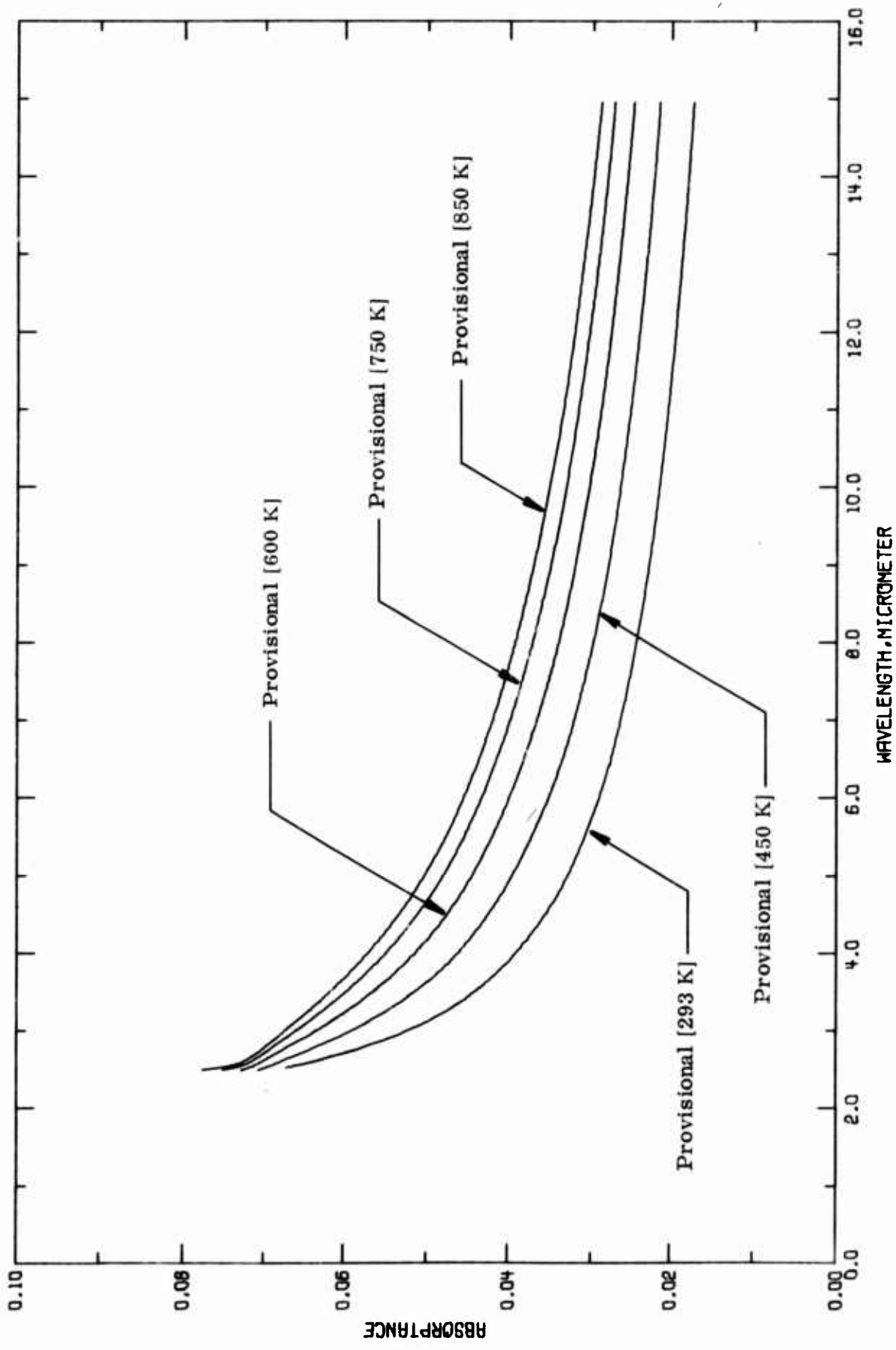


FIGURE 20-10. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (WAVELENGTH DEPENDENCE).

f. Normal Spectral Absorptance (Temperature Dependence)

The provisional values of the normal spectral absorptance of aluminized grafoil is given in Table 20-16 and plotted in Figure 20-11. They are numerically equal to the normal spectral emittance. Comparing our predicted curves for 5.0 μm and 10.0 μm with the available data in Figure 20-5, it appears that our predicted values are higher than experimental values. By a careful examination of the measurement information, one sees that the experimental points in Figure 20-5 are for thin films. The absorptance of bulk material is in general higher than that of thin film. An uncertainty of 25% is incooperated to the provisional values so that they can be used for most of the real surfaces.

TABLE 20-16. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| T | α | T | α | T | α | T | α |
|---------------------------------------|----------|---------------------------------------|----------|---------------------------------------|----------|--|----------|
| MECHANICALLY POLISHED $\lambda = 2.8$ | | MECHANICALLY POLISHED $\lambda = 3.8$ | | MECHANICALLY POLISHED $\lambda = 5.0$ | | MECHANICALLY POLISHED $\lambda = 13.6$ | |
| 250.0 | 0.054 | 250.0 | 0.039 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 350.0 | 0.057 | 350.0 | 0.041 | 350.0 | 0.033 | 350.0 | 0.021 |
| 350.0 | 0.050 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.052 | 400.0 | 0.045 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.063 | 450.0 | 0.048 | 450.0 | 0.040 | 450.0 | 0.025 |
| 500.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.065 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.067 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.068 | 650.0 | 0.055 | 650.0 | 0.045 | 650.0 | 0.030 |
| 700.0 | 0.069 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| 800.0 | 0.070 | 800.0 | 0.058 | 800.0 | 0.049 | 800.0 | 0.033 |
| 850.0 | 0.070 | 850.0 | 0.059 | 850.0 | 0.050 | 850.0 | 0.034 |
| 860.0 | 0.070 | 880.0 | 0.059 | 930.0 | 0.051 | 890.0 | 0.035 |

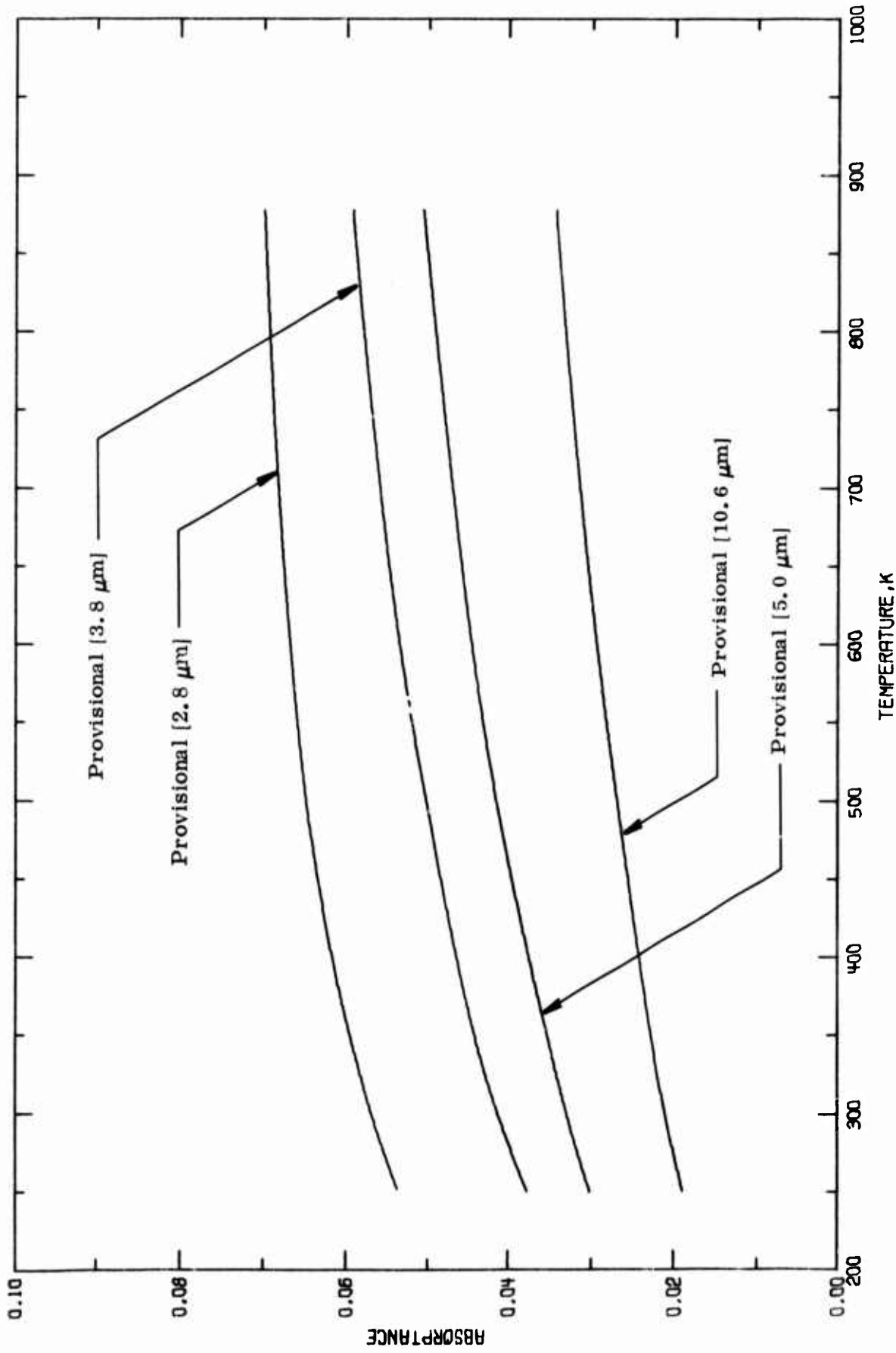


FIGURE 20-11. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF ALUMINIZED GRAFOIL (TEMPERATURE DEPENDENCE).

g. Transmittance

Although it is true that metals in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms. Consequently, composites with a metal layer are opaque to visible and infrared radiation because in general applications they are not used as extremely thin films. This leads to the conclusion that as an aircraft/spacecraft structural material, this composite is opaque and its transmittance is zero.

4.21. Boron Fiber Aluminum Matrix Composite

Boron fiber aluminum matrix composite is made in the form of sheet or tape. The sheets are made by diffusion bonding boron fibers between two sheets of aluminum or aluminum alloys. The tape is made by plasma spraying the 713 braze alloys. The tape is then diffusion or braze bonded into any desired configuration.

Boron filaments are formed by the vapor deposition of boron on a fine tungsten wire substrate within a reactor. Exposure of the tungsten substrate to the high temperature boron trichloride reactor environment results in a filament consisting of a boron sheath on a tungsten boride core. Boron fibers have higher tensile strength and modulus of elasticity than the graphite fibers commonly used in composite materials. Their melting point is higher than that of aluminum generally used in conjunction with them. The boron filaments are currently produced by two principal sources, Hamilton Standard and Avco. It might be noted that composites using Borsic filaments are also available commercially. These are boron filaments coated with silicon carbide in order to adapt boron filaments to high temperature usage in composite.

In the area of metal matrix, aluminum or aluminum alloys are currently commercially available.

The advantage of the boron fiber aluminum matrix composite is that along with its light weight it has a high temperature and heat resistance. Although the fiber material stands very high temperatures, its aluminum composite is not recommended for continuous service above 590 K, but the intermittent service to 645 K is possible. The products are available commercially in a wide range of laminate thickness including monolayer sheets in finished form. Virtually all of the actual hardware items built to date have been fabricated using standard fiber volume fractions of fifty percent.

The composite materials are fabricated primarily for aircraft constructions because of their advantages. Much of their mechanical and thermal properties are extensively as well as intensively measured. As a result, numerous publications in those areas are available at users' disposal.

With regard to the thermal radiative properties of these composites, it is unfortunate to find that there is nothing available, a very discouraging fact to workers in laser research. However, in view of the facts that the fiber materials are diffusion bonded between sheets of aluminum and the thickness of aluminum sheet is far more than enough to be opaque to the radiation, the thermal radiative properties of composite materials can be fully described by considering them as aluminum alone. Although aluminum alloys

2024-T851 and 6061-T6 are also commonly used as the matrix materials, the final products of the composites are usually clad for corrosion resistance. Therefore, the generation of the most probable values on the thermal radiative properties of boron fiber aluminum matrix composite is based on the available data of aluminum.

Literature survey for aluminum revealed an adequate amount of data on the normal spectral emittance, reflectance, and absorptance. Measurement information and experimental results obtained in this survey are given in Tables 20-1 to 20-10 and Figures 20-1 to 20-5. By careful review of the tables and figures, one will see that the magnitudes of the thermal radiative properties are very much affected by the surface conditions of the specimens. The literature abounds with examples of test surfaces shown to be very sensitive to methods of preparation, thermal history, and environmental conditions. Despite this awareness, descriptions of test surfaces are generally inadequate because of our modest understanding of the mechanisms or real surface effects and how to properly characterize a surface.

To isolate the individual surface characteristics is a difficult task. For most materials it is not practical to alter one characteristic without causing an influence on another. The control of the many variables required to study surface characterization in a logical manner is a complex problem. As a result only the simplest of surface profiles or compositional effects have been studied or are understood. One of the most important influences on the radiative properties of metals arises from surface roughness.

Because of the difficulties mentioned above, data analysis and evaluation is not a straightforward task; some logical but not exact means should be used in the generation of the most probable values for the properties of our interest. It is decided that the classical model of Hagen and Rubens with some modification is used to interpret the selected emittance data for mechanically polished surfaces, which is chosen as a good approximation to the real surfaces. Details of modifying the Hagen and Rubens equation are discussed in Section 2 and Eq. (2.5-5) is used for data analysis.

Reliable and accurate available data on the normal spectral emittance of mechanically polished aluminum surface were obtained by converting the data sets, curves 4 and 5 of Figure 20-4, from absorptance to emittance using Kirchhoff's law. Data for curves 4 and 5 were obtained at temperatures of 573 K and 293 K respectively. By a least squares calculation Eq. (4.20-1) was found to fit the selected data with uncertainties of less than $\pm 10\%$. Absorptance and reflectance can be calculated by using Eqs. (4.20-2) and (4.20-3).

By a quick scanning review of the details on the available data and information given in Tables 20-1 to 20-10 and Figures 20-1 to 20-5, it appears that the surface roughness

can be incorporated into Eq. (4.20-1). However, no attempt was made because there was not a single systematic information on the roughness dependence of the radiative properties available for data analysis. As a result, only the radiative properties of mechanically polished surface are presented here. Note that in the following tables more decimal places are reported than warranted merely for the purpose of tabular smoothness and internal comparison. Readers are advised to use the appropriate uncertainties given in each case.

a. Normal Spectral Emittance (Wavelength Dependence)

Normal spectral emittance of mechanically polished boron fiber aluminum matrix composite is calculated from Eq. (4.20-1) and listed in Table 21-1 and plotted in Figure 21-1. The values generated are considered as provisional (about $\pm 25\%$ uncertainty) since they are estimated based on the aluminum data. Provisional values are presented at five temperatures, 293, 450, 600, 750, and 850 K. Note that the emittance is usually quite low and remains practically constant for wavelengths longer than $6 \mu\text{m}$.

TABLE 21-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-------------------------------------|------------|-------------------------------------|------------|-------------------------------------|------------|-------------------------------------|------------|-------------------------------------|------------|
| MECHANICALLY POLISHED T = 293 | | MECHANICALLY POLISHED T = 450 | | MECHANICALLY POLISHED T = 600 | | MECHANICALLY POLISHED T = 750 | | MECHANICALLY POLISHED T = 850 | |
| 2.5 | 0.067 | 2.5 | 0.071 | 2.5 | 0.075 | 2.5 | 0.075 | 2.5 | 0.078 |
| 2.8 | 0.057 | 2.8 | 0.063 | 2.8 | 0.067 | 2.8 | 0.069 | 2.8 | 0.070 |
| 3.0 | 0.052 | 3.0 | 0.059 | 3.0 | 0.063 | 3.0 | 0.066 | 3.0 | 0.067 |
| 3.5 | 0.044 | 3.5 | 0.052 | 3.5 | 0.056 | 3.5 | 0.060 | 3.5 | 0.062 |
| 3.8 | 0.041 | 3.8 | 0.048 | 3.8 | 0.052 | 3.8 | 0.057 | 3.8 | 0.059 |
| 4.0 | 0.039 | 4.0 | 0.046 | 4.0 | 0.051 | 4.0 | 0.055 | 4.0 | 0.057 |
| 4.5 | 0.035 | 4.5 | 0.043 | 4.5 | 0.047 | 4.5 | 0.051 | 4.5 | 0.053 |
| 5.0 | 0.033 | 5.0 | 0.040 | 5.0 | 0.044 | 5.0 | 0.048 | 5.0 | 0.050 |
| 5.5 | 0.031 | 5.5 | 0.037 | 5.5 | 0.042 | 5.5 | 0.046 | 5.5 | 0.048 |
| 6.0 | 0.029 | 6.0 | 0.035 | 6.0 | 0.040 | 6.0 | 0.043 | 6.0 | 0.045 |
| 6.5 | 0.027 | 6.5 | 0.034 | 6.5 | 0.038 | 6.5 | 0.042 | 6.5 | 0.044 |
| 7.0 | 0.025 | 7.0 | 0.032 | 7.0 | 0.037 | 7.0 | 0.040 | 7.0 | 0.042 |
| 7.5 | 0.023 | 7.5 | 0.031 | 7.5 | 0.035 | 7.5 | 0.039 | 7.5 | 0.040 |
| 8.0 | 0.022 | 8.0 | 0.030 | 8.0 | 0.034 | 8.0 | 0.037 | 8.0 | 0.039 |
| 8.5 | 0.022 | 8.5 | 0.029 | 8.5 | 0.033 | 8.5 | 0.036 | 8.5 | 0.038 |
| 9.0 | 0.023 | 9.0 | 0.028 | 9.0 | 0.032 | 9.0 | 0.035 | 9.0 | 0.037 |
| 9.5 | 0.022 | 9.5 | 0.027 | 9.5 | 0.031 | 9.5 | 0.034 | 9.5 | 0.036 |
| 10.0 | 0.021 | 10.0 | 0.026 | 10.0 | 0.030 | 10.0 | 0.033 | 10.0 | 0.035 |
| 10.5 | 0.020 | 10.5 | 0.025 | 10.5 | 0.029 | 10.5 | 0.032 | 10.5 | 0.034 |
| 11.0 | 0.020 | 11.0 | 0.025 | 11.0 | 0.029 | 11.0 | 0.032 | 11.0 | 0.033 |
| 11.5 | 0.020 | 11.5 | 0.025 | 11.5 | 0.028 | 11.5 | 0.031 | 11.5 | 0.033 |
| 12.0 | 0.019 | 12.0 | 0.024 | 12.0 | 0.028 | 12.0 | 0.030 | 12.0 | 0.032 |
| 12.5 | 0.019 | 12.5 | 0.024 | 12.5 | 0.027 | 12.5 | 0.030 | 12.5 | 0.031 |
| 13.0 | 0.019 | 13.0 | 0.023 | 13.0 | 0.026 | 13.0 | 0.029 | 13.0 | 0.031 |
| 13.5 | 0.018 | 13.5 | 0.023 | 13.5 | 0.026 | 13.5 | 0.029 | 13.5 | 0.030 |
| 14.0 | 0.018 | 14.0 | 0.022 | 14.0 | 0.025 | 14.0 | 0.028 | 14.0 | 0.030 |
| 14.5 | 0.017 | 14.5 | 0.022 | 14.5 | 0.025 | 14.5 | 0.028 | 14.5 | 0.029 |
| 15.0 | 0.017 | 15.0 | 0.021 | 15.0 | 0.025 | 15.0 | 0.027 | 15.0 | 0.029 |

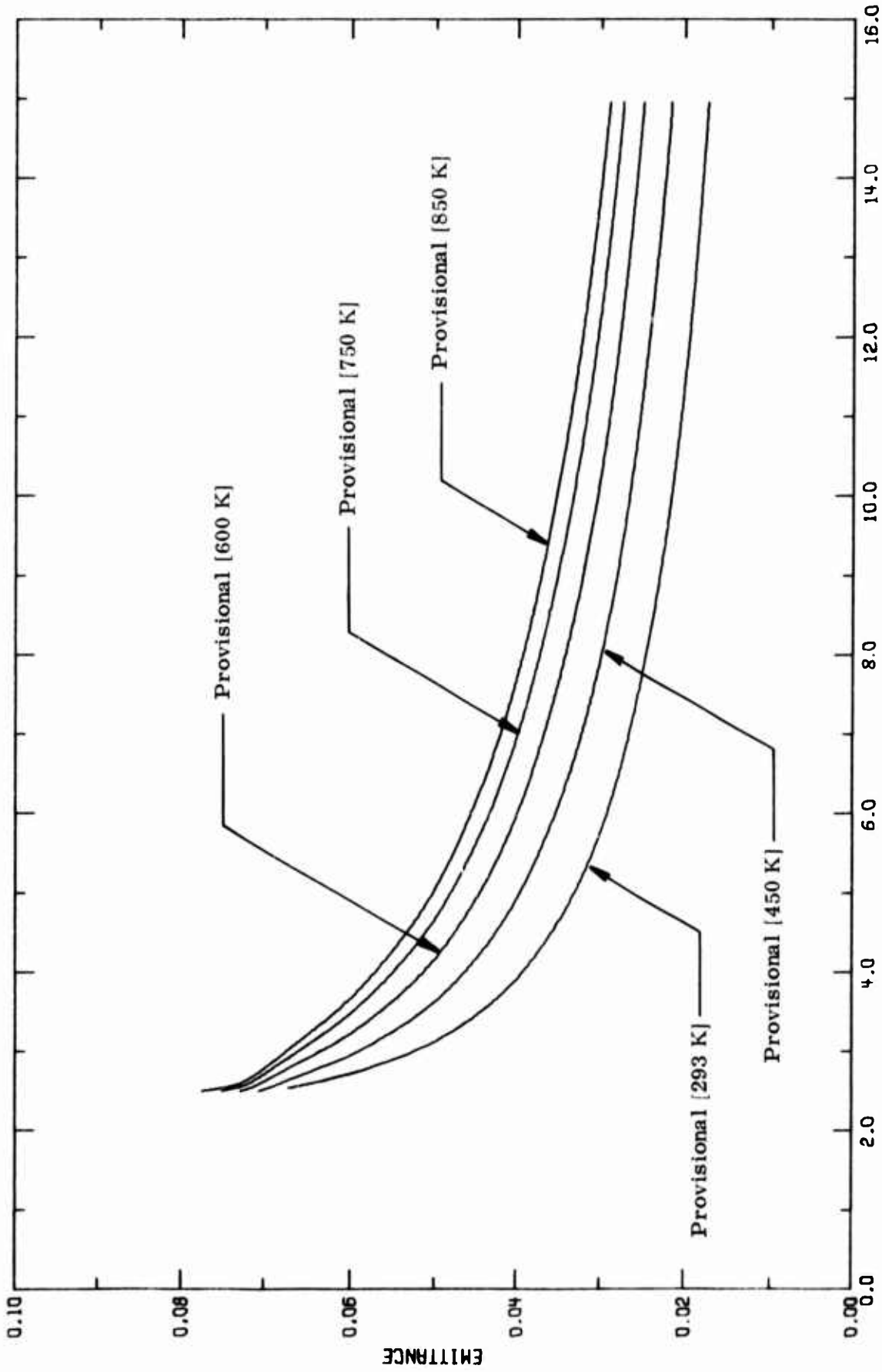


FIGURE 21-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE).

b. Normal Spectral Emittance (Temperature Dependence)

The normal spectral emittance as a function of temperature is given in Table 21-2 and Figure 21-2. The generated values are considered as provisional with uncertainty $\pm 25\%$. The plot clearly shows that emittance for a given wavelength does not vary appreciably for a wide temperature range. Note that the melting point of aluminum at about 930 K is not far from the endpoint (about 880 K) of each curve. It seems that the curves can be extrapolated to or beyond the melting point.

TABLE 21-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINIUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|--|------------|-------|------------|-------|------------|-------|------------|
| MECHANICALLY POLISHED $\lambda = 2.8$ | | | | | | | |
| 250.0 | 0.057 | 250.0 | 0.036 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 350.0 | 0.060 | 350.0 | 0.041 | 350.0 | 0.033 | 350.0 | 0.021 |
| 400.0 | 0.062 | 400.0 | 0.044 | 400.0 | 0.036 | 400.0 | 0.023 |
| 450.0 | 0.063 | 450.0 | 0.046 | 450.0 | 0.038 | 450.0 | 0.024 |
| 500.0 | 0.065 | 500.0 | 0.048 | 500.0 | 0.040 | 500.0 | 0.026 |
| 550.0 | 0.066 | 550.0 | 0.050 | 550.0 | 0.041 | 550.0 | 0.027 |
| 600.0 | 0.067 | 600.0 | 0.052 | 600.0 | 0.043 | 600.0 | 0.028 |
| 650.0 | 0.068 | 650.0 | 0.053 | 650.0 | 0.044 | 650.0 | 0.029 |
| 700.0 | 0.069 | 700.0 | 0.055 | 700.0 | 0.046 | 700.0 | 0.030 |
| 750.0 | 0.069 | 750.0 | 0.056 | 750.0 | 0.047 | 750.0 | 0.031 |
| 800.0 | 0.069 | 800.0 | 0.057 | 800.0 | 0.048 | 800.0 | 0.032 |
| 850.0 | 0.070 | 850.0 | 0.058 | 850.0 | 0.049 | 850.0 | 0.033 |
| 880.0 | 0.070 | 880.0 | 0.059 | 880.0 | 0.050 | 880.0 | 0.034 |
| MECHANICALLY POLISHED $\lambda = 5.0$ | | | | | | | |
| 250.0 | 0.057 | 250.0 | 0.036 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 350.0 | 0.060 | 350.0 | 0.041 | 350.0 | 0.033 | 350.0 | 0.021 |
| 400.0 | 0.062 | 400.0 | 0.044 | 400.0 | 0.036 | 400.0 | 0.023 |
| 450.0 | 0.063 | 450.0 | 0.046 | 450.0 | 0.038 | 450.0 | 0.024 |
| 500.0 | 0.065 | 500.0 | 0.048 | 500.0 | 0.040 | 500.0 | 0.026 |
| 550.0 | 0.066 | 550.0 | 0.050 | 550.0 | 0.041 | 550.0 | 0.027 |
| 600.0 | 0.067 | 600.0 | 0.052 | 600.0 | 0.043 | 600.0 | 0.028 |
| 650.0 | 0.068 | 650.0 | 0.053 | 650.0 | 0.044 | 650.0 | 0.029 |
| 700.0 | 0.069 | 700.0 | 0.055 | 700.0 | 0.046 | 700.0 | 0.030 |
| 750.0 | 0.069 | 750.0 | 0.056 | 750.0 | 0.047 | 750.0 | 0.031 |
| 800.0 | 0.069 | 800.0 | 0.057 | 800.0 | 0.048 | 800.0 | 0.032 |
| 850.0 | 0.070 | 850.0 | 0.058 | 850.0 | 0.049 | 850.0 | 0.033 |
| 880.0 | 0.070 | 880.0 | 0.059 | 880.0 | 0.050 | 880.0 | 0.034 |
| MECHANICALLY POLISHED $\lambda = 10.6$ | | | | | | | |
| 250.0 | 0.057 | 250.0 | 0.036 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 350.0 | 0.060 | 350.0 | 0.041 | 350.0 | 0.033 | 350.0 | 0.021 |
| 400.0 | 0.062 | 400.0 | 0.044 | 400.0 | 0.036 | 400.0 | 0.023 |
| 450.0 | 0.063 | 450.0 | 0.046 | 450.0 | 0.038 | 450.0 | 0.024 |
| 500.0 | 0.065 | 500.0 | 0.048 | 500.0 | 0.040 | 500.0 | 0.026 |
| 550.0 | 0.066 | 550.0 | 0.050 | 550.0 | 0.041 | 550.0 | 0.027 |
| 600.0 | 0.067 | 600.0 | 0.052 | 600.0 | 0.043 | 600.0 | 0.028 |
| 650.0 | 0.068 | 650.0 | 0.053 | 650.0 | 0.044 | 650.0 | 0.029 |
| 700.0 | 0.069 | 700.0 | 0.055 | 700.0 | 0.046 | 700.0 | 0.030 |
| 750.0 | 0.069 | 750.0 | 0.056 | 750.0 | 0.047 | 750.0 | 0.031 |
| 800.0 | 0.069 | 800.0 | 0.057 | 800.0 | 0.048 | 800.0 | 0.032 |
| 850.0 | 0.070 | 850.0 | 0.058 | 850.0 | 0.049 | 850.0 | 0.033 |
| 880.0 | 0.070 | 880.0 | 0.059 | 880.0 | 0.050 | 880.0 | 0.034 |

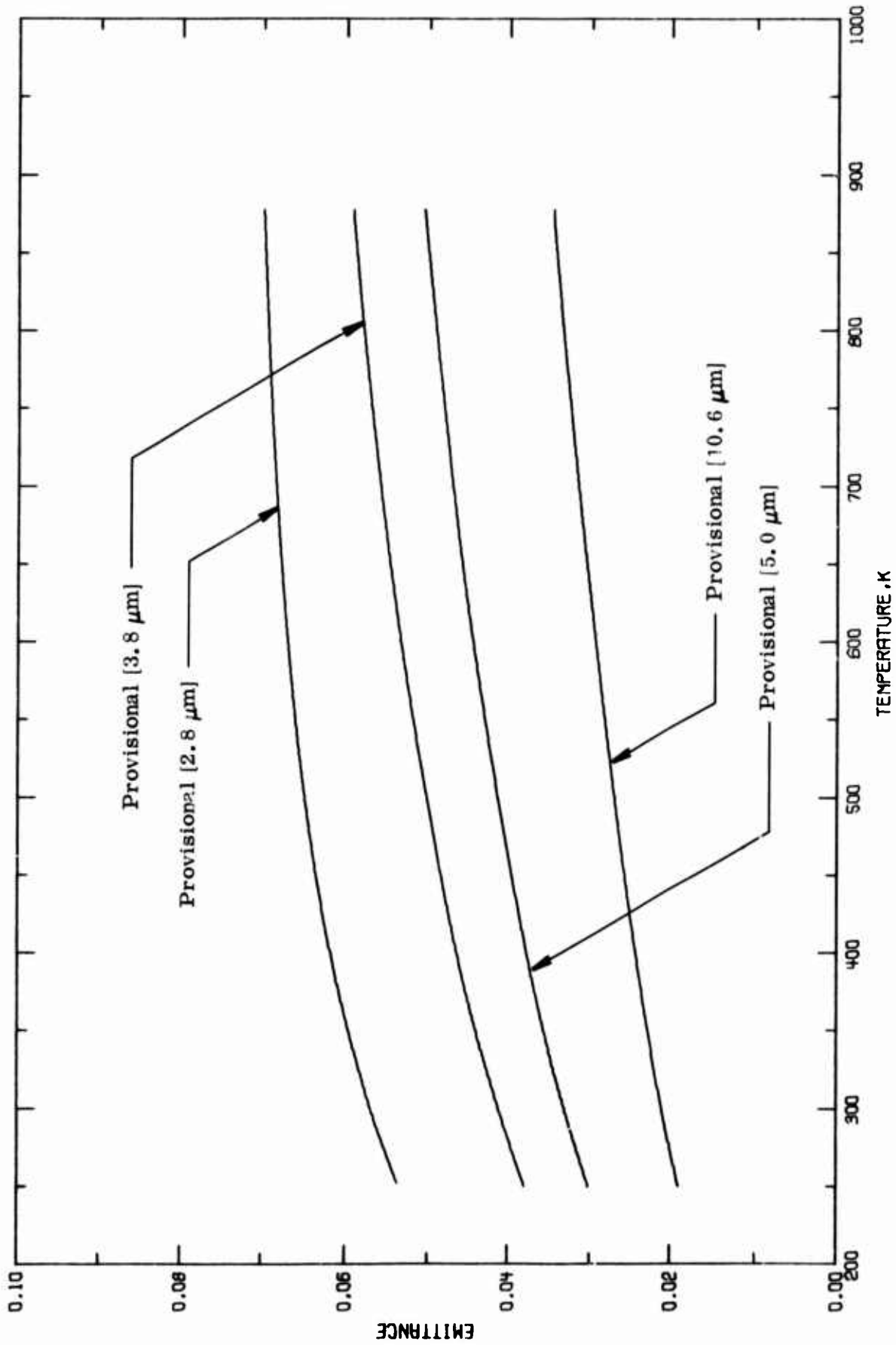


FIGURE 21-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

As given in Table 21-3 and plotted in Figure 21-3, the normal spectral reflectance of boron fiber aluminum composite is calculated by assuming that energy loss of the impinging radiation is entirely due to absorption. The result is remarkably good as one can see by comparing Figure 20-3 and Figure 21-3. Since the data analysis is totally based on the available data of aluminum, allowance is given in the estimation of the predicted values. An estimated uncertainty of $\pm 20\%$ is given to the calculated values.

TABLE 21-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ]

| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ |
|-----------|--------|-----------|--------|-----------|--------|-----------|--------|-----------|--------|
| 2.5 | 0.933 | 2.5 | 0.929 | 2.5 | 0.927 | 2.5 | 0.925 | 2.5 | 0.922 |
| 2.8 | 0.943 | 2.8 | 0.937 | 2.8 | 0.933 | 2.8 | 0.931 | 2.8 | 0.930 |
| 3.0 | 0.948 | 3.0 | 0.941 | 3.0 | 0.937 | 3.0 | 0.934 | 3.0 | 0.933 |
| 3.5 | 0.956 | 3.5 | 0.949 | 3.5 | 0.944 | 3.5 | 0.940 | 3.5 | 0.938 |
| 3.8 | 0.959 | 3.8 | 0.952 | 3.8 | 0.947 | 3.8 | 0.943 | 3.8 | 0.941 |
| 4.0 | 0.961 | 4.0 | 0.954 | 4.0 | 0.949 | 4.0 | 0.945 | 4.0 | 0.943 |
| 4.5 | 0.965 | 4.5 | 0.957 | 4.5 | 0.953 | 4.5 | 0.949 | 4.5 | 0.947 |
| 5.0 | 0.967 | 5.0 | 0.960 | 5.0 | 0.956 | 5.0 | 0.952 | 5.0 | 0.950 |
| 5.5 | 0.969 | 5.5 | 0.963 | 5.5 | 0.958 | 5.5 | 0.954 | 5.5 | 0.952 |
| 6.0 | 0.971 | 6.0 | 0.965 | 6.0 | 0.960 | 6.0 | 0.957 | 6.0 | 0.955 |
| 6.5 | 0.973 | 6.5 | 0.967 | 6.5 | 0.962 | 6.5 | 0.958 | 6.5 | 0.956 |
| 7.0 | 0.974 | 7.0 | 0.968 | 7.0 | 0.963 | 7.0 | 0.960 | 7.0 | 0.958 |
| 7.5 | 0.975 | 7.5 | 0.969 | 7.5 | 0.965 | 7.5 | 0.962 | 7.5 | 0.960 |
| 8.0 | 0.976 | 8.0 | 0.970 | 8.0 | 0.966 | 8.0 | 0.963 | 8.0 | 0.961 |
| 8.5 | 0.977 | 8.5 | 0.971 | 8.5 | 0.967 | 8.5 | 0.964 | 8.5 | 0.962 |
| 9.0 | 0.977 | 9.0 | 0.972 | 9.0 | 0.968 | 9.0 | 0.965 | 9.0 | 0.963 |
| 9.5 | 0.978 | 9.5 | 0.973 | 9.5 | 0.969 | 9.5 | 0.966 | 9.5 | 0.964 |
| 10.0 | 0.979 | 10.0 | 0.974 | 10.0 | 0.970 | 10.0 | 0.967 | 10.0 | 0.965 |
| 10.5 | 0.980 | 10.5 | 0.974 | 10.5 | 0.971 | 10.5 | 0.968 | 10.5 | 0.966 |
| 11.0 | 0.980 | 11.0 | 0.975 | 11.0 | 0.971 | 11.0 | 0.969 | 11.0 | 0.967 |
| 11.5 | 0.980 | 11.5 | 0.975 | 11.5 | 0.972 | 11.5 | 0.969 | 11.5 | 0.967 |
| 12.0 | 0.981 | 12.0 | 0.976 | 12.0 | 0.972 | 12.0 | 0.970 | 12.0 | 0.968 |
| 12.5 | 0.981 | 12.5 | 0.976 | 12.5 | 0.973 | 12.5 | 0.970 | 12.5 | 0.968 |
| 13.0 | 0.981 | 13.0 | 0.977 | 13.0 | 0.974 | 13.0 | 0.971 | 13.0 | 0.969 |
| 13.5 | 0.982 | 13.5 | 0.977 | 13.5 | 0.974 | 13.5 | 0.971 | 13.5 | 0.969 |
| 14.0 | 0.982 | 14.0 | 0.978 | 14.0 | 0.975 | 14.0 | 0.972 | 14.0 | 0.970 |
| 14.5 | 0.983 | 14.5 | 0.978 | 14.5 | 0.975 | 14.5 | 0.972 | 14.5 | 0.971 |
| 15.0 | 0.983 | 15.0 | 0.979 | 15.0 | 0.975 | 15.0 | 0.973 | 15.0 | 0.971 |

MECHANICALLY
POLISHED
T = 850MECHANICALLY
POLISHED
T = 750MECHANICALLY
POLISHED
T = 600MECHANICALLY
POLISHED
T = 450

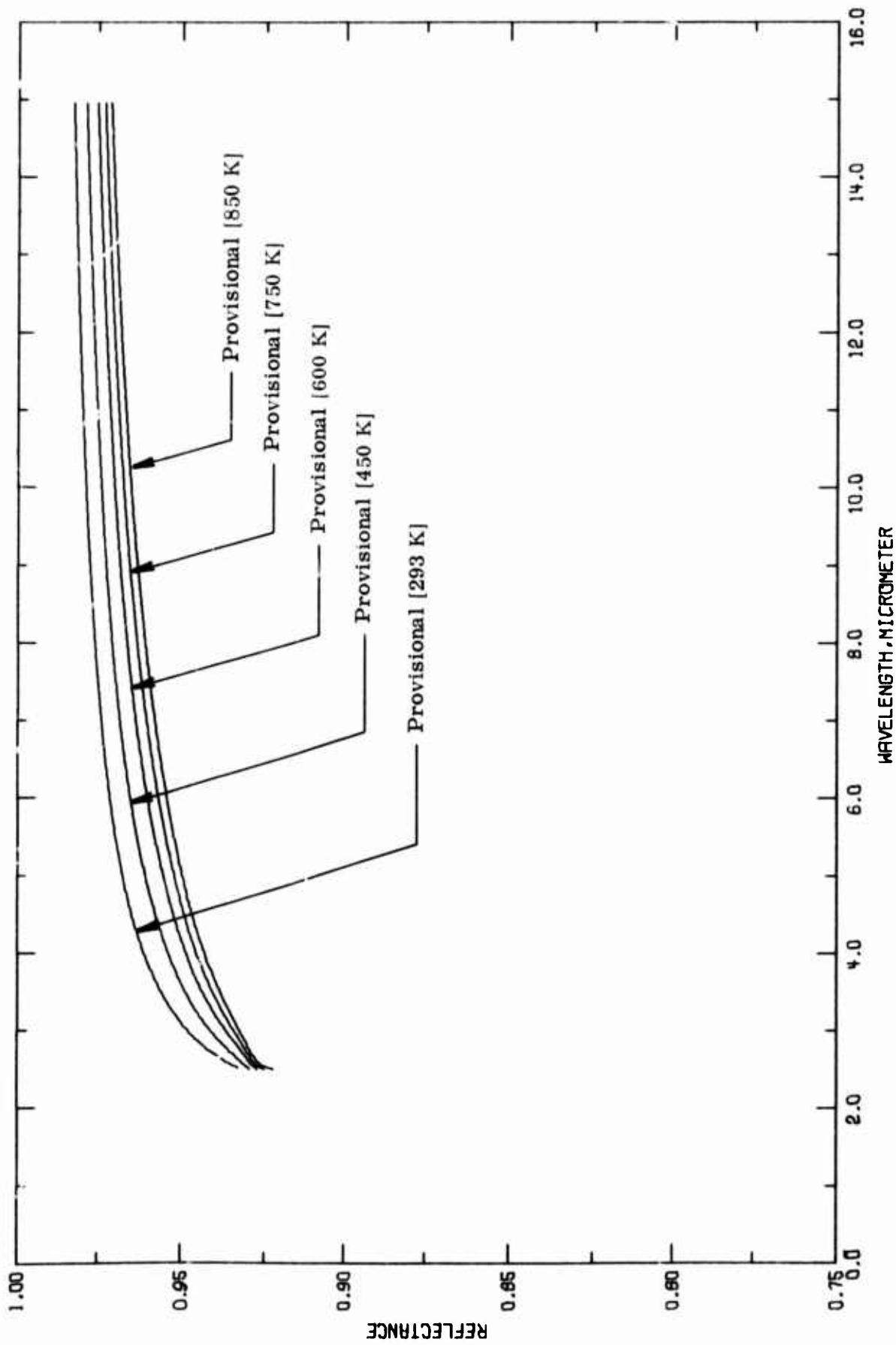


FIGURE 21-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE).

d. Normal Spectral Reflectance (Temperature Dependence)

In Table 21-4, the provisional values of the normal spectral reflectance are given with estimated uncertainties of $\pm 20\%$. The variation of the property as a function of temperature is demonstrated in Figure 21-4. For a given wavelength, the normal spectral reflectance remains as a constant from room temperature up to near the melting point of the material. At higher temperatures our knowledge on this property is lacking. However, it seems that a linear extrapolation of the curve to and above the melting point can be used with uncertainty of no more than $\pm 35\%$.

TABLE 21-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINIUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ | T | ρ | T | ρ | T | ρ |
|--|--------|-------|--------|-------|--------|-------|--------|
| MECHANICALLY POLISHED $\lambda = 2.0$ | | | | | | | |
| 250.0 | 0.976 | 250.0 | 0.952 | 250.0 | 0.970 | 250.0 | 0.981 |
| 293.0 | 0.973 | 293.0 | 0.959 | 293.0 | 0.967 | 293.0 | 0.979 |
| 300.0 | 0.973 | 300.0 | 0.959 | 300.0 | 0.967 | 300.0 | 0.979 |
| 350.0 | 0.940 | 350.0 | 0.950 | 350.0 | 0.964 | 350.0 | 0.977 |
| 400.0 | 0.939 | 400.0 | 0.954 | 400.0 | 0.962 | 400.0 | 0.976 |
| 450.0 | 0.937 | 450.0 | 0.952 | 450.0 | 0.950 | 450.0 | 0.974 |
| 500.0 | 0.935 | 500.0 | 0.950 | 500.0 | 0.959 | 500.0 | 0.973 |
| 550.0 | 0.934 | 550.0 | 0.948 | 550.0 | 0.957 | 550.0 | 0.972 |
| 600.0 | 0.933 | 600.0 | 0.947 | 600.0 | 0.956 | 600.0 | 0.971 |
| 650.0 | 0.932 | 650.0 | 0.945 | 650.0 | 0.954 | 650.0 | 0.970 |
| 700.0 | 0.932 | 700.0 | 0.944 | 700.0 | 0.953 | 700.0 | 0.969 |
| 750.0 | 0.931 | 750.0 | 0.943 | 750.0 | 0.952 | 750.0 | 0.968 |
| 800.0 | 0.931 | 800.0 | 0.942 | 800.0 | 0.951 | 800.0 | 0.967 |
| 850.0 | 0.930 | 850.0 | 0.941 | 850.0 | 0.950 | 850.0 | 0.966 |
| 900.0 | 0.930 | 900.0 | 0.941 | 900.0 | 0.949 | 900.0 | 0.965 |
| MECHANICALLY POLISHED $\lambda = 3.0$ | | | | | | | |
| 250.0 | 0.976 | 250.0 | 0.952 | 250.0 | 0.970 | 250.0 | 0.981 |
| 293.0 | 0.973 | 293.0 | 0.959 | 293.0 | 0.967 | 293.0 | 0.979 |
| 300.0 | 0.973 | 300.0 | 0.959 | 300.0 | 0.967 | 300.0 | 0.979 |
| 350.0 | 0.940 | 350.0 | 0.950 | 350.0 | 0.964 | 350.0 | 0.977 |
| 400.0 | 0.939 | 400.0 | 0.954 | 400.0 | 0.962 | 400.0 | 0.976 |
| 450.0 | 0.937 | 450.0 | 0.952 | 450.0 | 0.950 | 450.0 | 0.974 |
| 500.0 | 0.935 | 500.0 | 0.950 | 500.0 | 0.959 | 500.0 | 0.973 |
| 550.0 | 0.934 | 550.0 | 0.948 | 550.0 | 0.957 | 550.0 | 0.972 |
| 600.0 | 0.933 | 600.0 | 0.947 | 600.0 | 0.956 | 600.0 | 0.971 |
| 650.0 | 0.932 | 650.0 | 0.945 | 650.0 | 0.954 | 650.0 | 0.970 |
| 700.0 | 0.932 | 700.0 | 0.944 | 700.0 | 0.953 | 700.0 | 0.969 |
| 750.0 | 0.931 | 750.0 | 0.943 | 750.0 | 0.952 | 750.0 | 0.968 |
| 800.0 | 0.931 | 800.0 | 0.942 | 800.0 | 0.951 | 800.0 | 0.967 |
| 850.0 | 0.930 | 850.0 | 0.941 | 850.0 | 0.950 | 850.0 | 0.966 |
| 900.0 | 0.930 | 900.0 | 0.941 | 900.0 | 0.949 | 900.0 | 0.965 |
| MECHANICALLY POLISHED $\lambda = 10.6$ | | | | | | | |
| 250.0 | 0.976 | 250.0 | 0.952 | 250.0 | 0.970 | 250.0 | 0.981 |
| 293.0 | 0.973 | 293.0 | 0.959 | 293.0 | 0.967 | 293.0 | 0.979 |
| 300.0 | 0.973 | 300.0 | 0.959 | 300.0 | 0.967 | 300.0 | 0.979 |
| 350.0 | 0.940 | 350.0 | 0.950 | 350.0 | 0.964 | 350.0 | 0.977 |
| 400.0 | 0.939 | 400.0 | 0.954 | 400.0 | 0.962 | 400.0 | 0.976 |
| 450.0 | 0.937 | 450.0 | 0.952 | 450.0 | 0.950 | 450.0 | 0.974 |
| 500.0 | 0.935 | 500.0 | 0.950 | 500.0 | 0.959 | 500.0 | 0.973 |
| 550.0 | 0.934 | 550.0 | 0.948 | 550.0 | 0.957 | 550.0 | 0.972 |
| 600.0 | 0.933 | 600.0 | 0.947 | 600.0 | 0.956 | 600.0 | 0.971 |
| 650.0 | 0.932 | 650.0 | 0.945 | 650.0 | 0.954 | 650.0 | 0.970 |
| 700.0 | 0.932 | 700.0 | 0.944 | 700.0 | 0.953 | 700.0 | 0.969 |
| 750.0 | 0.931 | 750.0 | 0.943 | 750.0 | 0.952 | 750.0 | 0.968 |
| 800.0 | 0.931 | 800.0 | 0.942 | 800.0 | 0.951 | 800.0 | 0.967 |
| 850.0 | 0.930 | 850.0 | 0.941 | 850.0 | 0.950 | 850.0 | 0.966 |
| 900.0 | 0.930 | 900.0 | 0.941 | 900.0 | 0.949 | 900.0 | 0.965 |

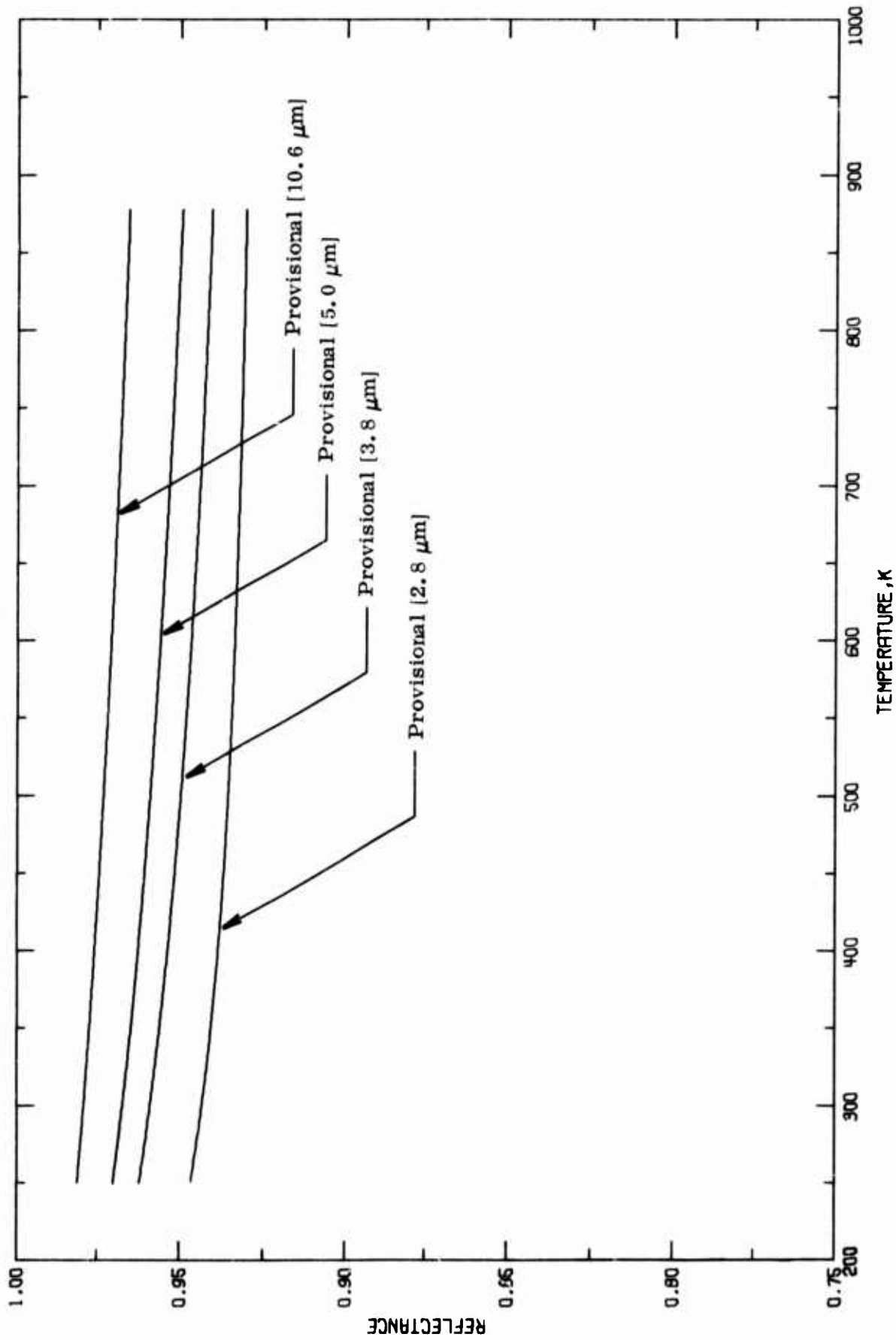


FIGURE 21-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

The normal spectral absorptance is obtained according to the Kirchhoff's law, i. e., numerically the absorptance is equal to the emittance. As a result, Table 21-5 and Figure 21-5 appear the same as Table 21-1 and Figure 21-1, as well as the uncertainties ($\pm 25\%$). The absorptance varies appreciably for wavelengths lower than $4.0 \mu\text{m}$ and remains practically unchanged for longer wavelengths as shown in Figure 21-5.

TABLE 21-5. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| MECHANICALLY POLISHED T = 293 | | MECHANICALLY POLISHED T = 450 | | MECHANICALLY POLISHED T = 600 | | MECHANICALLY POLISHED T = 750 | | MECHANICALLY POLISHED T = 850 | |
|-------------------------------------|----------|-------------------------------------|----------|-------------------------------------|----------|-------------------------------------|----------|-------------------------------------|----------|
| λ | α | λ | α | λ | α | λ | α | λ | α |
| 2.5 | 0.067 | 2.5 | 0.071 | 2.5 | 0.073 | 2.5 | 0.075 | 2.5 | 0.078 |
| 2.8 | 0.057 | 2.8 | 0.053 | 2.8 | 0.067 | 2.8 | 0.069 | 2.8 | 0.070 |
| 3.0 | 0.052 | 3.0 | 0.059 | 3.0 | 0.063 | 3.0 | 0.066 | 3.0 | 0.067 |
| 3.5 | 0.044 | 3.5 | 0.052 | 3.5 | 0.056 | 3.5 | 0.059 | 3.5 | 0.062 |
| 3.8 | 0.041 | 3.8 | 0.048 | 3.8 | 0.052 | 3.6 | 0.055 | 3.8 | 0.059 |
| 4.0 | 0.039 | 4.0 | 0.046 | 4.0 | 0.051 | 4.0 | 0.055 | 4.0 | 0.057 |
| 4.5 | 0.035 | 4.5 | 0.043 | 4.5 | 0.047 | 4.5 | 0.051 | 4.5 | 0.053 |
| 5.0 | 0.033 | 5.0 | 0.040 | 5.0 | 0.044 | 5.0 | 0.048 | 5.0 | 0.050 |
| 5.5 | 0.029 | 5.5 | 0.037 | 5.5 | 0.042 | 5.5 | 0.046 | 5.5 | 0.048 |
| 6.0 | 0.029 | 6.0 | 0.035 | 6.0 | 0.040 | 6.0 | 0.043 | 6.0 | 0.045 |
| 6.5 | 0.026 | 6.5 | 0.032 | 6.5 | 0.035 | 6.5 | 0.042 | 6.5 | 0.044 |
| 7.0 | 0.025 | 7.0 | 0.032 | 7.0 | 0.037 | 7.0 | 0.040 | 7.0 | 0.042 |
| 7.5 | 0.025 | 7.5 | 0.031 | 7.5 | 0.035 | 7.5 | 0.039 | 7.5 | 0.040 |
| 8.0 | 0.023 | 8.0 | 0.029 | 8.0 | 0.034 | 8.0 | 0.037 | 8.0 | 0.039 |
| 8.5 | 0.023 | 8.5 | 0.029 | 8.5 | 0.033 | 8.5 | 0.036 | 8.5 | 0.039 |
| 9.0 | 0.022 | 9.0 | 0.027 | 9.0 | 0.032 | 9.0 | 0.035 | 9.0 | 0.037 |
| 9.5 | 0.021 | 9.5 | 0.026 | 9.5 | 0.031 | 9.5 | 0.034 | 9.5 | 0.036 |
| 10.0 | 0.021 | 10.0 | 0.026 | 10.0 | 0.030 | 10.0 | 0.033 | 10.0 | 0.035 |
| 10.5 | 0.021 | 10.5 | 0.026 | 10.5 | 0.029 | 10.5 | 0.032 | 10.5 | 0.034 |
| 11.0 | 0.020 | 11.0 | 0.025 | 11.0 | 0.029 | 11.0 | 0.032 | 11.0 | 0.033 |
| 11.5 | 0.020 | 11.5 | 0.025 | 11.5 | 0.028 | 11.5 | 0.031 | 11.5 | 0.033 |
| 12.0 | 0.019 | 12.0 | 0.024 | 12.0 | 0.028 | 12.0 | 0.030 | 12.0 | 0.032 |
| 12.5 | 0.019 | 12.5 | 0.024 | 12.5 | 0.027 | 12.5 | 0.030 | 12.5 | 0.032 |
| 13.0 | 0.019 | 13.0 | 0.023 | 13.0 | 0.026 | 13.0 | 0.029 | 13.0 | 0.031 |
| 13.5 | 0.018 | 13.5 | 0.023 | 13.5 | 0.026 | 13.5 | 0.029 | 13.5 | 0.030 |
| 14.0 | 0.018 | 14.0 | 0.022 | 14.0 | 0.025 | 14.0 | 0.028 | 14.0 | 0.030 |
| 14.5 | 0.017 | 14.5 | 0.022 | 14.5 | 0.025 | 14.5 | 0.028 | 14.5 | 0.029 |
| 15.0 | 0.017 | 15.0 | 0.021 | 15.0 | 0.025 | 15.0 | 0.027 | 15.0 | 0.029 |

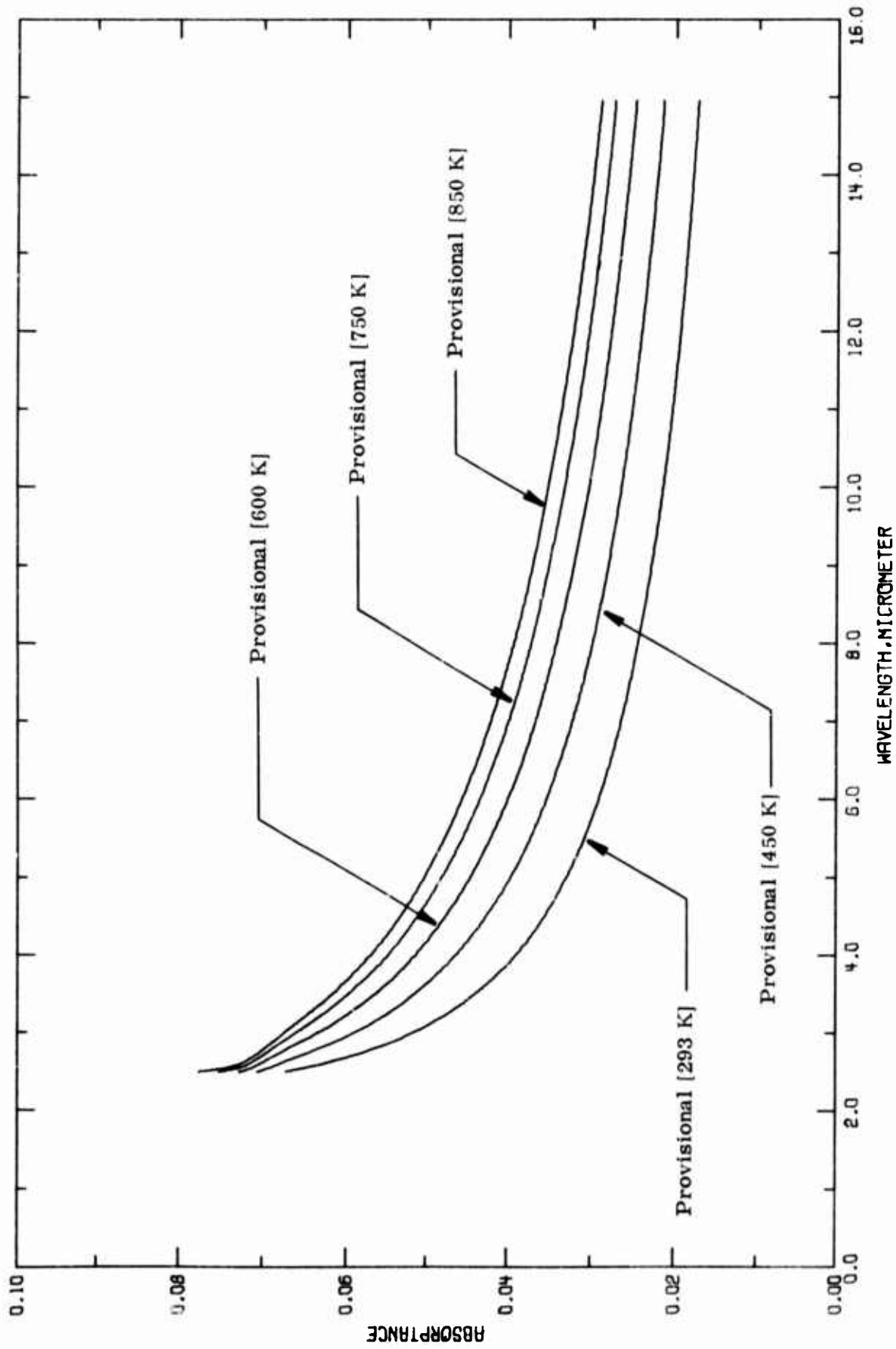


FIGURE 21-5. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE).

f. Normal Spectral Absorptance (Temperature Dependence)

The provisional values of the normal spectral absorptance of boron fiber aluminum matrix composite is given in Table 21-6 and plotted in Figure 21-6. They are numerically equal to the normal spectral emittance. In Figure 21-6, our predicted curves for 5.0 μm and 10.0 μm are higher than experimental values plotted in Figure 20-5. By a careful examination of the measurement information, one sees that the experimental points in Figure 20-5 are for thin films. The absorptance of bulk material is in general higher than that of thin film. An uncertainty of 25% is given to the provisional values so that they can be used for most of the real surfaces.

TABLE 21-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α | T | α | T | α | T | α |
|---------------------------------------|----------|-------|----------|-------|----------|-------|----------|
| MECHANICALLY POLISHED $\lambda = 2.8$ | | | | | | | |
| 250.0 | 0.0354 | 250.0 | 0.038 | 250.0 | 0.0330 | 250.0 | 0.019 |
| 300.0 | 0.037 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 350.0 | 0.037 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 400.0 | 0.050 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 450.0 | 0.052 | 400.0 | 0.046 | 400.0 | 0.033 | 400.0 | 0.024 |
| 500.0 | 0.063 | 450.0 | 0.048 | 450.0 | 0.040 | 450.0 | 0.026 |
| 550.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 600.0 | 0.067 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 650.0 | 0.068 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 700.0 | 0.069 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 750.0 | 0.069 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 800.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| 850.0 | 0.070 | 800.0 | 0.058 | 800.0 | 0.049 | 800.0 | 0.033 |
| 900.0 | 0.070 | 850.0 | 0.059 | 850.0 | 0.050 | 850.0 | 0.034 |
| 950.0 | 0.070 | 900.0 | 0.059 | 900.0 | 0.051 | 900.0 | 0.035 |
| MECHANICALLY POLISHED $\lambda = 5.0$ | | | | | | | |
| 250.0 | 0.0354 | 250.0 | 0.038 | 250.0 | 0.0330 | 250.0 | 0.019 |
| 300.0 | 0.037 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 350.0 | 0.037 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 400.0 | 0.050 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 450.0 | 0.052 | 400.0 | 0.046 | 400.0 | 0.033 | 400.0 | 0.024 |
| 500.0 | 0.063 | 450.0 | 0.048 | 450.0 | 0.040 | 450.0 | 0.026 |
| 550.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 600.0 | 0.067 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 650.0 | 0.068 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 700.0 | 0.069 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 750.0 | 0.069 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 800.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| 850.0 | 0.070 | 800.0 | 0.058 | 800.0 | 0.049 | 800.0 | 0.033 |
| 900.0 | 0.070 | 850.0 | 0.059 | 850.0 | 0.050 | 850.0 | 0.034 |
| 950.0 | 0.070 | 900.0 | 0.059 | 900.0 | 0.051 | 900.0 | 0.035 |

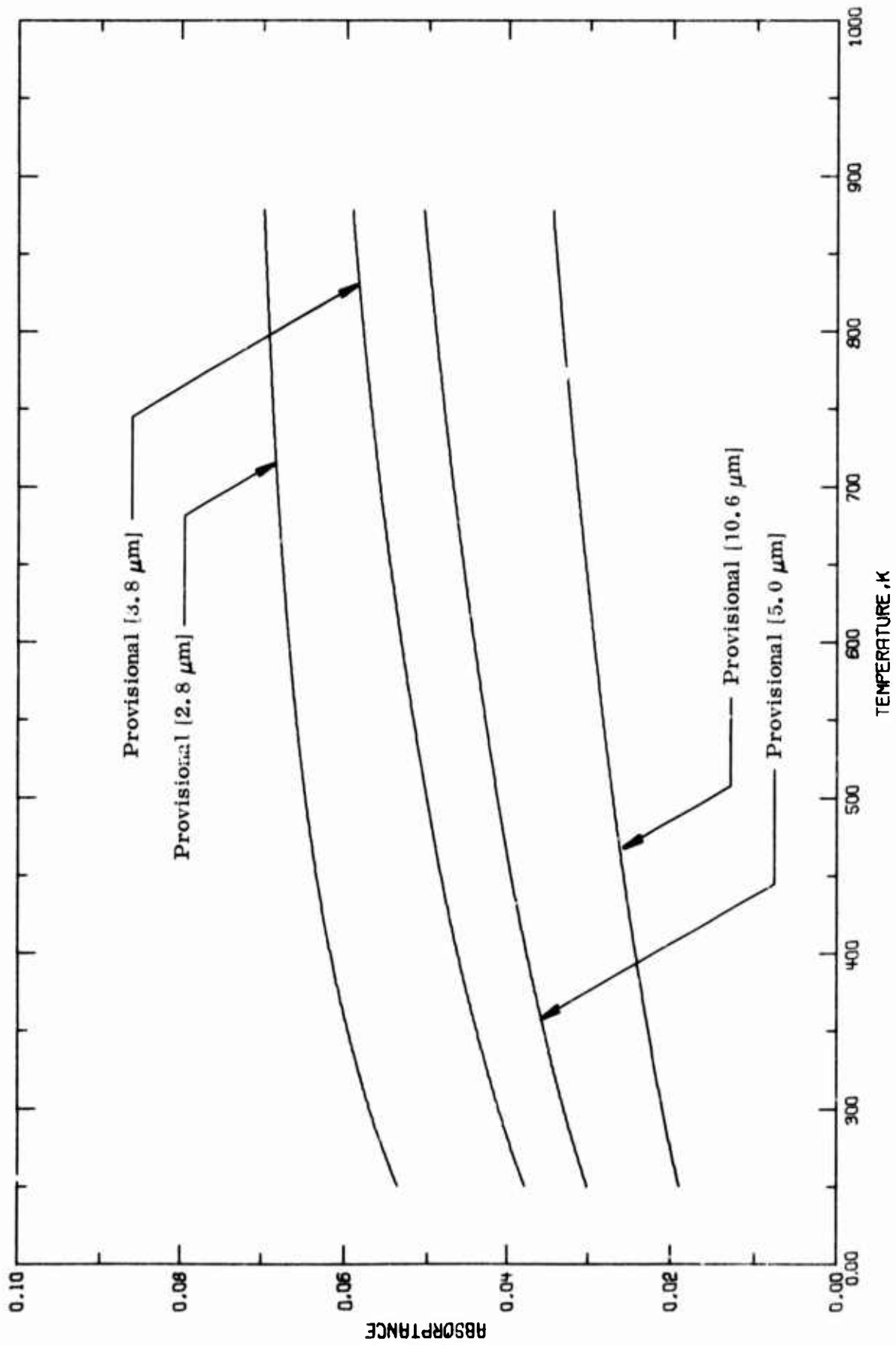


FIGURE 21-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE).

g. Transmittance

Although it is true that metals in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms. Consequently, composites with metal matrix are opaque to visible and infrared radiation because in general applications they are not used as extremely thin films. This leads to the conclusion that as an aircraft/spacecraft structural material, this composite is opaque and its transmittance is zero.

4.22. Graphite Fiber Aluminum Matrix Composite

Graphite fiber aluminum matrix composite is made in the form of sheet or tape. The sheets are made by diffusion bonding graphite fibers between two sheets of aluminum or aluminum alloys. The tape is made by plasma spraying the 713 braze alloys. The tape is then diffusion or braze bonded into any desired configuration.

There are three types of graphite fibers currently in large-scale production. These filaments have varied tensile strengths, moduli of elasticity, and densities. Graphite fibers for use in composite materials are made by the carbonization of organic fibers. Polyacrylonitrile (PAN) is most commonly used today, but acrylic and rayon fibers have been used to some extent in the past. The mechanical properties of the fibers depend on the temperatures used in the carbonization process. Temperatures of 2800-3300 K yield fibers with high moduli of elasticity but with relatively low tensile strength while temperatures of 1800-2300 K result in fibers of the highest tensile strength but only moderate elasticity. The melting point of the graphite fibers is much higher than the aluminum matrix components generally used. The fibers are available in short lengths (about 48 inches) and continuous lengths up to 3000 feet. The mechanical properties of these two forms are somewhat different.

In the area of metal matrix, aluminum or aluminum alloys are currently commercially available.

The advantage of the graphite fiber aluminum matrix composite is that along with its light weight it has a high temperature and heat resistance. Although the fiber material stands very high temperatures, its aluminum composite is not recommended for continuous service above 590 K, but the intermittent service to 645 K is possible. The products are available commercially in a wide range of laminate thickness including monolayer sheets in finished form. Virtually all of the actual hardware items built to date have been fabricated using standard fiber volume fractions of fifty percent.

The composite materials are fabricated primarily for aircraft constructions because of their advantages. Much of their mechanical and thermal properties are extensively as well as intensively measured. As a result, numerous publications in those areas are available at users' disposal.

With regard to the thermal radiative properties of these composites, it is unfortunate to find that there is nothing available, a very discouraging fact to workers in laser research. However, in view of the facts that the fiber materials are diffusion bonded between sheets of aluminum and the thickness of aluminum sheet is far more than

enough to be opaque to the radiation, the thermal radiative properties of composite materials can be fully described by considering them as aluminum alone. Although aluminum alloys 2024-T851 and 6061-T6 are also commonly used as the matrix materials, the final products of the composites are usually clad for corrosion resistance. Therefore, the generation of the most probable values on the thermal radiative properties of graphite fiber aluminum matrix composite is based on the available data of aluminum.

Literature survey for aluminum revealed an adequate amount of data on the normal spectral emittance, reflectance, and absorptance. Measurement information and experimental results obtained in this survey are given in Tables 20-1 to 20-10 and Figures 20-1 to 20-5. By careful review of the tables and figures, one will see that the magnitudes of the thermal radiative properties are very much affected by the surface conditions of the specimens. The literature abounds with examples of test surfaces shown to be very sensitive to methods of preparation, thermal history, and environmental conditions. Despite this awareness, descriptions of test surfaces are generally inadequate because of our modest understanding of the mechanisms or real surface effects and how to properly characterize a surface.

To isolate the individual surface characteristics is a difficult task. For most materials it is not practical to alter one characteristic without causing an influence on another. The control of the many variables required to study surface characterization in a logical manner is a complex problem. As a result only the simplest of surface profiles or compositional effects have been studied or are understood. One of the most important influences on the radiative properties of metals arises from surface roughness.

Because of the difficulties mentioned above, data analysis and evaluation is not a straightforward task; some logical but not exact means should be used in the generation of the most probable values for the properties of our interest. It is decided that the classical model of Hagen and Rubens with some modification is used to interpret the selected emittance data for mechanically polished surfaces, which is chosen as a good approximation to the real surfaces. Details of modifying the Hagen and Rubens equation are discussed in Section 2 and Eq. (2.5-5) is used for data analysis.

Reliable and accurate available data on the normal spectral emittance of mechanically polished aluminum surface were obtained by converting the data sets, curves 4 and 5 of Figure 20-4, from absorptance to emittance using Kirchhoff's law. Data for curves 4 and 5 were obtained at temperatures of 573 K and 293 K respectively. By a least squares calculation Eq. (4.20-1) was found to fit the selected data with uncertainties of less than $\pm 10\%$. Absorptance and reflectance can be calculated by using Eqs. (4.20-2) and (4.20-3).

By a quick scanning review of the details on the available data and information given in Tables 20-1 to 20-10 and Figures 20-1 to 20-5, it appears that the surface roughness can be incorporated into Eq. (4.20-1). However, no attempt was made because there was not a single systematic information on the roughness dependence of the radiative properties available for data analysis. As a result, only the radiative properties of mechanically polished surface are presented here. Note that in the following tables more decimal places are reported than warranted merely for the purpose of tabular smoothness and internal comparison. Readers are advised to use the appropriate uncertainties given in each case.

a. Normal Spectral Emittance (Wavelength Dependence)

Normal spectral emittance of mechanically polished graphite fiber aluminum matrix composite is calculated from Eq. (4.20-1) and listed in Table 22-1 and plotted in Figure 22-1. The values generated are considered as provisional (about $\pm 25\%$ uncertainty) since they are estimated based on the aluminum data. Provisional values are presented at five temperatures, 293, 450, 600, 750, and 850 K. Note that the emittance is usually quite low and remains practically constant for wavelengths longer than $6 \mu\text{m}$.

TABLE 22-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE)

[WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| λ | ϵ | λ | ϵ | λ | ϵ | λ | ϵ |
|-----------|------------|-----------|------------|-----------|------------|-----------|------------|
| 2.5 | 0.057 | 2.5 | 0.073 | 2.5 | 0.075 | 2.5 | 0.076 |
| 2.8 | 0.057 | 2.8 | 0.067 | 2.8 | 0.069 | 2.8 | 0.070 |
| 3.0 | 0.052 | 3.0 | 0.063 | 3.0 | 0.065 | 3.0 | 0.067 |
| 3.5 | 0.044 | 3.5 | 0.055 | 3.5 | 0.056 | 3.5 | 0.062 |
| 3.8 | 0.041 | 3.8 | 0.053 | 3.8 | 0.057 | 3.8 | 0.059 |
| 4.0 | 0.039 | 4.0 | 0.046 | 4.0 | 0.051 | 4.0 | 0.057 |
| 4.5 | 0.039 | 4.5 | 0.043 | 4.5 | 0.047 | 4.5 | 0.053 |
| 5.0 | 0.033 | 5.0 | 0.040 | 5.0 | 0.044 | 5.0 | 0.050 |
| 5.5 | 0.031 | 5.5 | 0.037 | 5.5 | 0.042 | 5.5 | 0.048 |
| 6.0 | 0.029 | 6.0 | 0.035 | 6.0 | 0.040 | 6.0 | 0.045 |
| 6.5 | 0.027 | 6.5 | 0.034 | 6.5 | 0.039 | 6.5 | 0.044 |
| 7.0 | 0.026 | 7.0 | 0.032 | 7.0 | 0.037 | 7.0 | 0.042 |
| 7.5 | 0.025 | 7.5 | 0.031 | 7.5 | 0.035 | 7.5 | 0.040 |
| 8.0 | 0.024 | 8.0 | 0.030 | 8.0 | 0.034 | 8.0 | 0.039 |
| 8.5 | 0.023 | 8.5 | 0.029 | 8.5 | 0.033 | 8.5 | 0.038 |
| 9.0 | 0.023 | 9.0 | 0.028 | 9.0 | 0.032 | 9.0 | 0.037 |
| 9.5 | 0.022 | 9.5 | 0.027 | 9.5 | 0.031 | 9.5 | 0.036 |
| 10.0 | 0.021 | 10.0 | 0.026 | 10.0 | 0.030 | 10.0 | 0.035 |
| 10.5 | 0.021 | 10.5 | 0.025 | 10.5 | 0.029 | 10.5 | 0.034 |
| 11.0 | 0.020 | 11.0 | 0.025 | 11.0 | 0.029 | 11.0 | 0.033 |
| 11.5 | 0.020 | 11.5 | 0.025 | 11.5 | 0.028 | 11.5 | 0.033 |
| 12.0 | 0.019 | 12.0 | 0.024 | 12.0 | 0.028 | 12.0 | 0.032 |
| 12.5 | 0.019 | 12.5 | 0.024 | 12.5 | 0.027 | 12.5 | 0.031 |
| 13.0 | 0.019 | 13.0 | 0.023 | 13.0 | 0.026 | 13.0 | 0.031 |
| 13.5 | 0.018 | 13.5 | 0.023 | 13.5 | 0.026 | 13.5 | 0.030 |
| 14.0 | 0.018 | 14.0 | 0.022 | 14.0 | 0.025 | 14.0 | 0.030 |
| 14.5 | 0.017 | 14.5 | 0.022 | 14.5 | 0.025 | 14.5 | 0.029 |
| 15.0 | 0.017 | 15.0 | 0.021 | 15.0 | 0.025 | 15.0 | 0.029 |

MECHANICALLY
POLISHED
T = 293MECHANICALLY
POLISHED
T = 450MECHANICALLY
POLISHED
T = 600MECHANICALLY
POLISHED
T = 750MECHANICALLY
POLISHED
T = 850

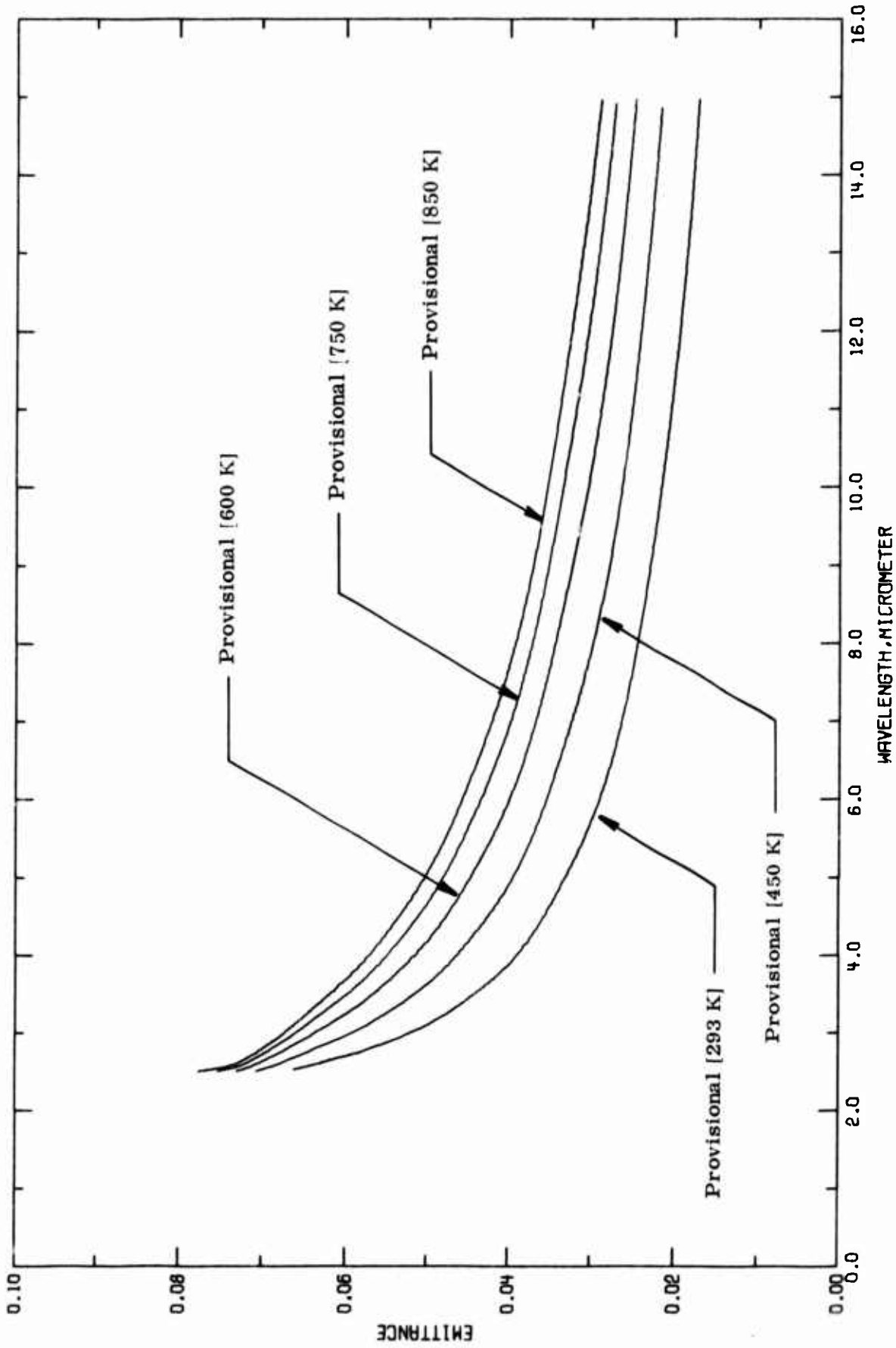


FIGURE 22-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE).

b. Normal Spectral Emittance (Temperature Dependence)

The normal spectral emittance as a function of temperature is given in Table 22-2 and Figure 22-2. The generated values are considered as provisional with $\pm 25\%$ uncertainty. The plot clearly shows that emittance for a given wavelength does not vary appreciably for a wide temperature range. Note that the melting point of aluminum at about 930 K is not far from the ending point (about 880 K) of each curve. It seems that the curves can be extrapolated to or beyond the melting point.

TABLE 22-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ]

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|---|------------|---|------------|---|------------|--|------------|
| MECHANICALLY POLISHED $\lambda = 2.6$ | | MECHANICALLY POLISHED $\lambda = 3.8$ | | MECHANICALLY POLISHED $\lambda = 5.0$ | | MECHANICALLY POLISHED $\lambda = 10.6$ | |
| 250.0 | 0.054 | 250.0 | 0.038 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.057 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.052 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.052 | 400.0 | 0.045 | 400.0 | 0.035 | 400.0 | 0.024 |
| 450.0 | 0.053 | 450.0 | 0.046 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.055 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.056 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.026 |
| 600.0 | 0.057 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.058 | 650.0 | 0.055 | 650.0 | 0.045 | 650.0 | 0.030 |
| 700.0 | 0.059 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.059 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| 800.0 | 0.059 | 800.0 | 0.058 | 800.0 | 0.049 | 800.0 | 0.033 |
| 850.0 | 0.070 | 850.0 | 0.059 | 850.0 | 0.050 | 850.0 | 0.034 |
| 880.0 | 0.070 | 880.0 | 0.059 | 880.0 | 0.051 | 880.0 | 0.035 |

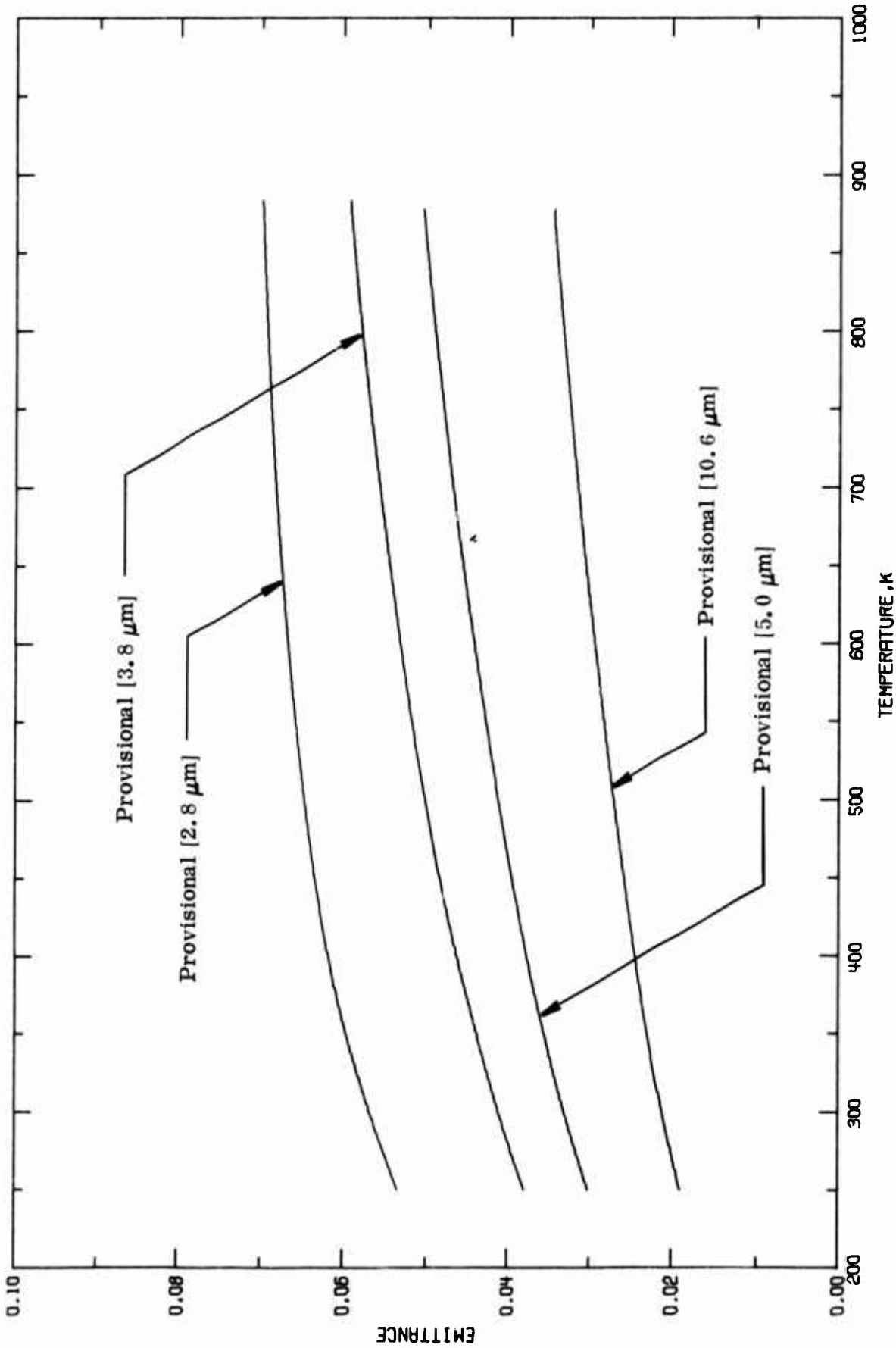


FIGURE 22-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

As given in Table 22-3 and plotted in Figure 22-3 the normal spectral reflectance of graphite fiber aluminum matrix composite is calculated by assuming that energy loss of the impinging radiation is entirely due to absorption. Since the data analysis is totally based on the available data of aluminum, allowance is given in the estimation of the predicted values. An estimated uncertainty of $\pm 20\%$ is given to the calculated values.

TABLE 22-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| MECHANICALLY POLISHED T = 293 | | | MECHANICALLY POLISHED T = 450 | | | MECHANICALLY POLISHED T = 603 | | | MECHANICALLY POLISHED T = 750 | | | MECHANICALLY POLISHED T = 850 | | |
|----------------------------------|--------|-----------|----------------------------------|-----------|--------|----------------------------------|--------|-----------|----------------------------------|-----------|--------|----------------------------------|--------|--|
| λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | λ | ρ | |
| 2.5 | 0.933 | 2.5 | 0.929 | 2.5 | 0.927 | 2.5 | 0.925 | 2.5 | 0.925 | 2.5 | 0.922 | 2.5 | 0.922 | |
| 2.6 | 0.943 | 2.6 | 0.937 | 2.6 | 0.933 | 2.6 | 0.931 | 2.6 | 0.931 | 2.6 | 0.930 | 2.6 | 0.930 | |
| 3.0 | 0.948 | 3.0 | 0.941 | 3.0 | 0.937 | 3.0 | 0.934 | 3.0 | 0.934 | 3.0 | 0.933 | 3.0 | 0.933 | |
| 3.5 | 0.956 | 3.5 | 0.948 | 3.5 | 0.944 | 3.5 | 0.940 | 3.5 | 0.940 | 3.5 | 0.938 | 3.5 | 0.938 | |
| 3.8 | 0.959 | 3.8 | 0.952 | 3.8 | 0.947 | 3.8 | 0.943 | 3.8 | 0.943 | 3.8 | 0.941 | 3.8 | 0.941 | |
| 4.0 | 0.961 | 4.0 | 0.954 | 4.0 | 0.949 | 4.0 | 0.945 | 4.0 | 0.945 | 4.0 | 0.943 | 4.0 | 0.943 | |
| 4.5 | 0.965 | 4.5 | 0.957 | 4.5 | 0.952 | 4.5 | 0.949 | 4.5 | 0.949 | 4.5 | 0.947 | 4.5 | 0.947 | |
| 5.0 | 0.967 | 5.0 | 0.959 | 5.0 | 0.956 | 5.0 | 0.952 | 5.0 | 0.952 | 5.0 | 0.950 | 5.0 | 0.950 | |
| 5.5 | 0.969 | 5.5 | 0.963 | 5.5 | 0.958 | 5.5 | 0.954 | 5.5 | 0.954 | 5.5 | 0.952 | 5.5 | 0.952 | |
| 6.0 | 0.971 | 6.0 | 0.965 | 6.0 | 0.960 | 6.0 | 0.957 | 6.0 | 0.957 | 6.0 | 0.955 | 6.0 | 0.955 | |
| 6.5 | 0.973 | 6.5 | 0.967 | 6.5 | 0.962 | 6.5 | 0.958 | 6.5 | 0.958 | 6.5 | 0.956 | 6.5 | 0.956 | |
| 7.0 | 0.974 | 7.0 | 0.968 | 7.0 | 0.963 | 7.0 | 0.959 | 7.0 | 0.959 | 7.0 | 0.957 | 7.0 | 0.957 | |
| 7.5 | 0.975 | 7.5 | 0.969 | 7.5 | 0.964 | 7.5 | 0.961 | 7.5 | 0.961 | 7.5 | 0.959 | 7.5 | 0.959 | |
| 8.0 | 0.976 | 8.0 | 0.970 | 8.0 | 0.965 | 8.0 | 0.962 | 8.0 | 0.962 | 8.0 | 0.960 | 8.0 | 0.960 | |
| 8.5 | 0.977 | 8.5 | 0.971 | 8.5 | 0.966 | 8.5 | 0.963 | 8.5 | 0.963 | 8.5 | 0.961 | 8.5 | 0.961 | |
| 9.0 | 0.977 | 9.0 | 0.972 | 9.0 | 0.967 | 9.0 | 0.964 | 9.0 | 0.964 | 9.0 | 0.962 | 9.0 | 0.962 | |
| 9.5 | 0.978 | 9.5 | 0.973 | 9.5 | 0.968 | 9.5 | 0.965 | 9.5 | 0.965 | 9.5 | 0.963 | 9.5 | 0.963 | |
| 10.0 | 0.979 | 10.0 | 0.974 | 10.0 | 0.970 | 10.0 | 0.967 | 10.0 | 0.967 | 10.0 | 0.965 | 10.0 | 0.965 | |
| 10.5 | 0.980 | 10.5 | 0.975 | 10.5 | 0.971 | 10.5 | 0.968 | 10.5 | 0.968 | 10.5 | 0.966 | 10.5 | 0.966 | |
| 11.0 | 0.981 | 11.0 | 0.976 | 11.0 | 0.972 | 11.0 | 0.969 | 11.0 | 0.969 | 11.0 | 0.967 | 11.0 | 0.967 | |
| 11.5 | 0.982 | 11.5 | 0.977 | 11.5 | 0.973 | 11.5 | 0.970 | 11.5 | 0.970 | 11.5 | 0.968 | 11.5 | 0.968 | |
| 12.0 | 0.983 | 12.0 | 0.978 | 12.0 | 0.974 | 12.0 | 0.971 | 12.0 | 0.971 | 12.0 | 0.969 | 12.0 | 0.969 | |
| 12.5 | 0.984 | 12.5 | 0.979 | 12.5 | 0.975 | 12.5 | 0.972 | 12.5 | 0.972 | 12.5 | 0.970 | 12.5 | 0.970 | |
| 13.0 | 0.985 | 13.0 | 0.980 | 13.0 | 0.976 | 13.0 | 0.973 | 13.0 | 0.973 | 13.0 | 0.971 | 13.0 | 0.971 | |
| 13.5 | 0.986 | 13.5 | 0.981 | 13.5 | 0.977 | 13.5 | 0.974 | 13.5 | 0.974 | 13.5 | 0.972 | 13.5 | 0.972 | |
| 14.0 | 0.987 | 14.0 | 0.982 | 14.0 | 0.978 | 14.0 | 0.975 | 14.0 | 0.975 | 14.0 | 0.973 | 14.0 | 0.973 | |
| 14.5 | 0.988 | 14.5 | 0.983 | 14.5 | 0.979 | 14.5 | 0.976 | 14.5 | 0.976 | 14.5 | 0.974 | 14.5 | 0.974 | |
| 15.0 | 0.989 | 15.0 | 0.984 | 15.0 | 0.980 | 15.0 | 0.977 | 15.0 | 0.977 | 15.0 | 0.975 | 15.0 | 0.975 | |

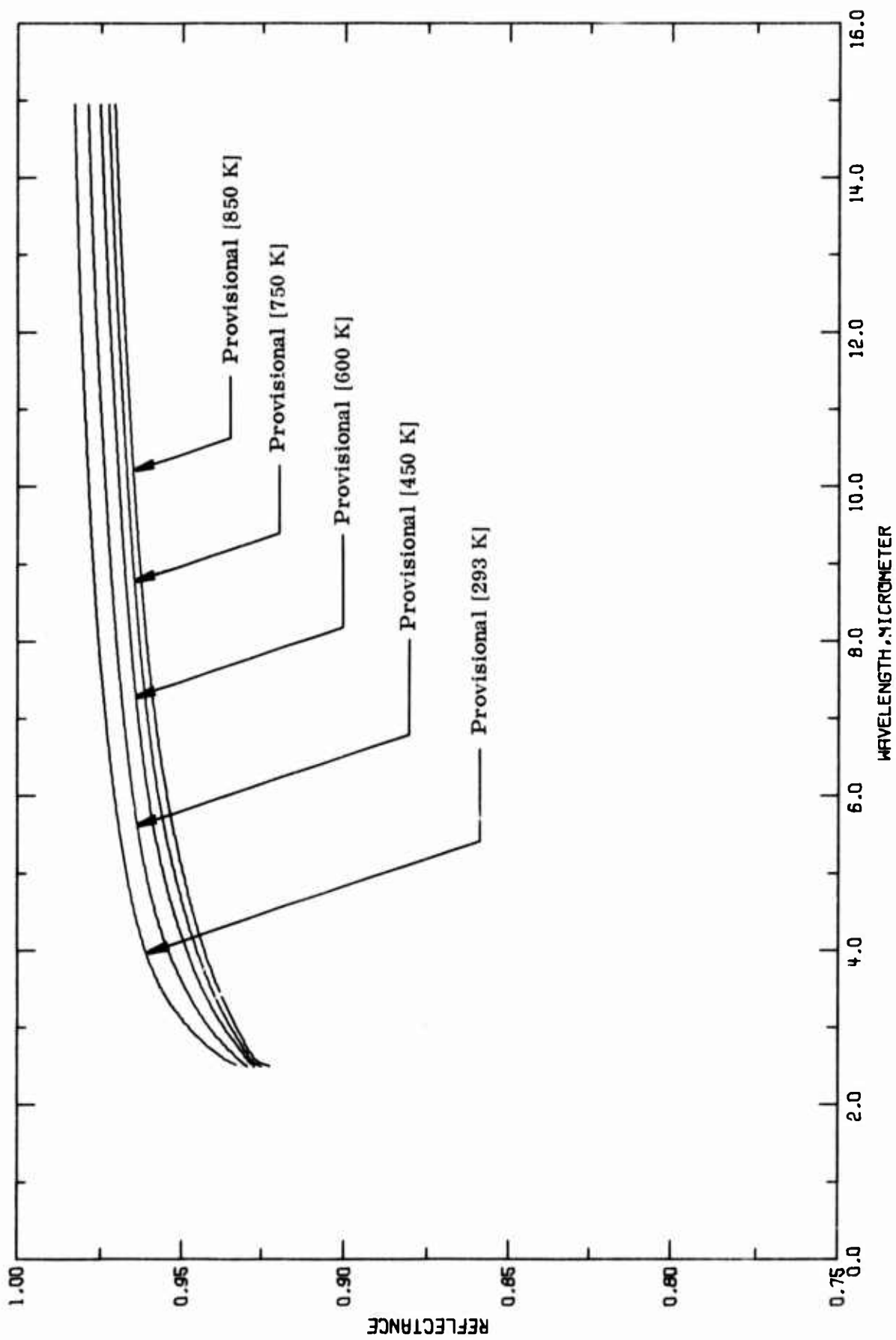


FIGURE 22-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE).

d. Normal Spectral Reflectance (Temperature Dependence)

In Table 22-4, the provisional values of the normal spectral reflectance are given with an estimated uncertainty of $\pm 20\%$. The variation of the property as a function of temperature is demonstrated in Figure 22-4. For a given wavelength, the normal spectral reflectance remains as a constant from room temperature up to near the melting point of the material. At higher temperatures our knowledge on this property is lacking. However, it seems that a linear extrapolation of the curve to and above the melting point can be used with uncertainty of no more than $\pm 35\%$.

TABLE 22-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | $\lambda = 2.8$ | | $\lambda = 3.8$ | | $\lambda = 5.0$ | | $\lambda = 10.6$ | |
|-------|--------------------------|--------|--------------------------|--------|--------------------------|--------|--------------------------|--------|
| | MECHANICALLY POLISHED | ρ | MECHANICALLY POLISHED | ρ | MECHANICALLY POLISHED | ρ | MECHANICALLY POLISHED | ρ |
| 250.0 | 0.946 | 0.962 | 250.0 | 0.962 | 250.0 | 0.970 | 250.0 | 0.951 |
| 293.0 | 0.943 | 0.959 | 293.0 | 0.959 | 293.0 | 0.967 | 293.0 | 0.979 |
| 300.0 | 0.943 | 0.959 | 300.0 | 0.959 | 300.0 | 0.967 | 300.0 | 0.979 |
| 350.0 | 0.940 | 0.956 | 350.0 | 0.956 | 350.0 | 0.964 | 350.0 | 0.977 |
| 400.0 | 0.936 | 0.954 | 400.0 | 0.954 | 400.0 | 0.962 | 400.0 | 0.976 |
| 450.0 | 0.937 | 0.952 | 450.0 | 0.952 | 450.0 | 0.960 | 450.0 | 0.974 |
| 500.0 | 0.935 | 0.951 | 500.0 | 0.951 | 500.0 | 0.959 | 500.0 | 0.973 |
| 550.0 | 0.934 | 0.949 | 550.0 | 0.949 | 550.0 | 0.957 | 550.0 | 0.972 |
| 600.0 | 0.933 | 0.947 | 600.0 | 0.947 | 600.0 | 0.956 | 600.0 | 0.971 |
| 650.0 | 0.932 | 0.945 | 650.0 | 0.945 | 650.0 | 0.954 | 650.0 | 0.970 |
| 700.0 | 0.932 | 0.944 | 700.0 | 0.944 | 700.0 | 0.953 | 700.0 | 0.969 |
| 750.0 | 0.931 | 0.943 | 750.0 | 0.943 | 750.0 | 0.952 | 750.0 | 0.968 |
| 800.0 | 0.931 | 0.942 | 800.0 | 0.942 | 800.0 | 0.951 | 800.0 | 0.967 |
| 850.0 | 0.930 | 0.941 | 850.0 | 0.941 | 850.0 | 0.950 | 850.0 | 0.966 |
| 900.0 | 0.930 | 0.941 | 900.0 | 0.941 | 900.0 | 0.949 | 900.0 | 0.965 |

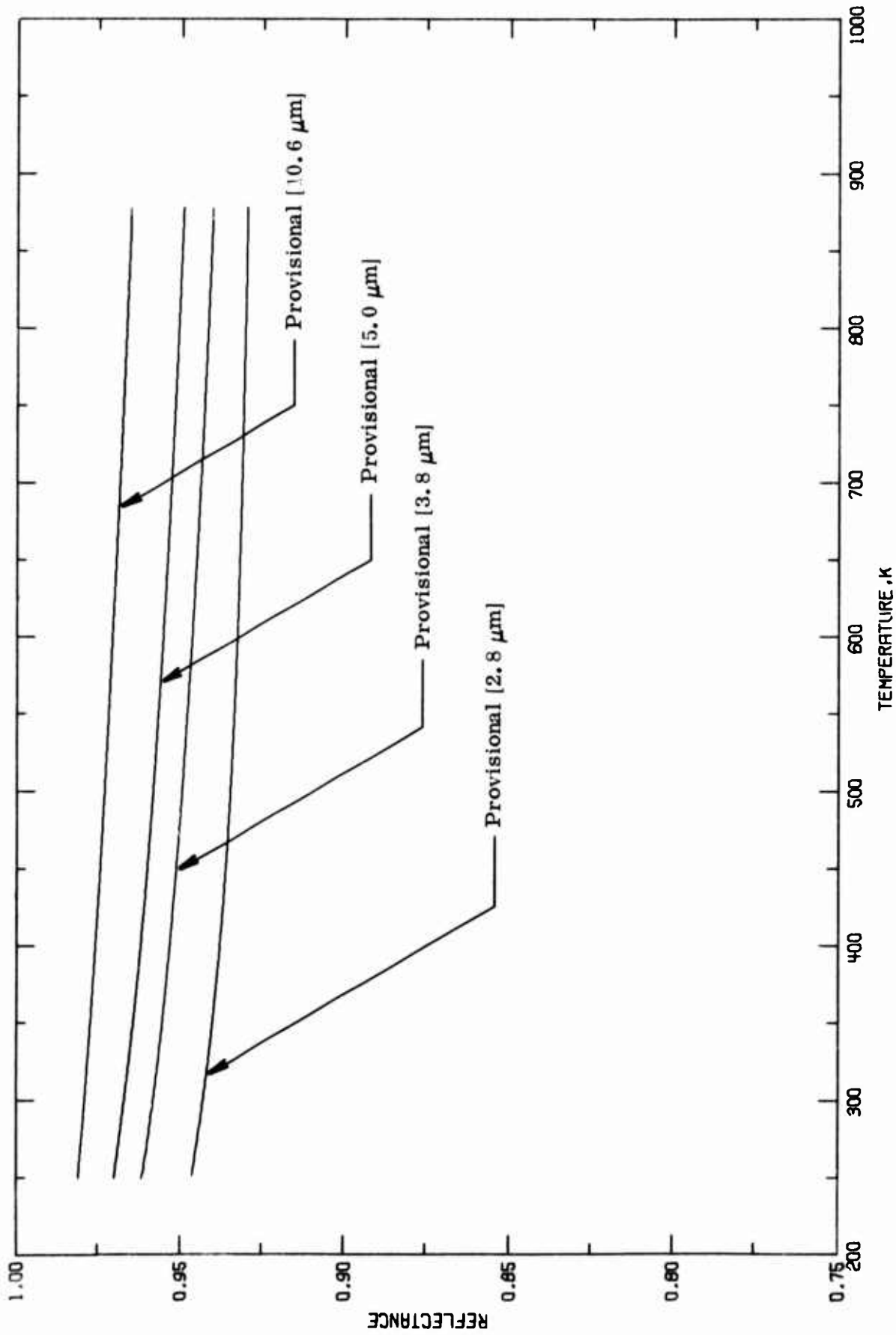


FIGURE 22-4. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

The normal spectral absorptance is obtained according to the Kirchhoff's law, i. e., numerically the absorptance is equal to the emittance. The absorptance varies appreciably for wavelengths lower than $4.0 \mu\text{m}$ and remains practically unchanged for longer wavelengths. The generated provisional values with $\pm 25\%$ uncertainty are given in Table 22-5 and plotted in Figure 22-5.

TABLE 22-5. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | | α | | λ | | α | | λ | | α | | λ | | α | |
|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|-------------------------------------|-------|
| MECHANICALLY POLISHED T = 293 | | MECHANICALLY POLISHED T = 450 | | MECHANICALLY POLISHED T = 600 | | MECHANICALLY POLISHED T = 750 | | MECHANICALLY POLISHED T = 850 | | MECHANICALLY POLISHED T = 850 | | MECHANICALLY POLISHED T = 850 | | MECHANICALLY POLISHED T = 850 | |
| 2.5 | 0.057 | 2.5 | 0.071 | 2.5 | 0.073 | 2.5 | 0.075 | 2.5 | 0.078 | 2.5 | 0.078 | 2.5 | 0.078 | 2.5 | 0.078 |
| 2.8 | 0.057 | 2.8 | 0.063 | 2.8 | 0.067 | 2.8 | 0.069 | 2.8 | 0.070 | 2.8 | 0.070 | 2.8 | 0.070 | 2.8 | 0.070 |
| 3.0 | 0.052 | 3.0 | 0.059 | 3.0 | 0.063 | 3.0 | 0.066 | 3.0 | 0.067 | 3.0 | 0.067 | 3.0 | 0.067 | 3.0 | 0.067 |
| 3.5 | 0.044 | 3.5 | 0.052 | 3.5 | 0.058 | 3.5 | 0.058 | 3.5 | 0.062 | 3.5 | 0.062 | 3.5 | 0.062 | 3.5 | 0.062 |
| 3.8 | 0.041 | 3.8 | 0.048 | 3.8 | 0.053 | 3.8 | 0.053 | 3.8 | 0.057 | 3.8 | 0.057 | 3.8 | 0.057 | 3.8 | 0.057 |
| 4.0 | 0.039 | 4.0 | 0.040 | 4.0 | 0.051 | 4.0 | 0.055 | 4.0 | 0.057 | 4.0 | 0.057 | 4.0 | 0.057 | 4.0 | 0.057 |
| 4.5 | 0.035 | 4.5 | 0.045 | 4.5 | 0.047 | 4.5 | 0.051 | 4.5 | 0.055 | 4.5 | 0.055 | 4.5 | 0.055 | 4.5 | 0.055 |
| 5.0 | 0.033 | 5.0 | 0.040 | 5.0 | 0.044 | 5.0 | 0.048 | 5.0 | 0.051 | 5.0 | 0.051 | 5.0 | 0.051 | 5.0 | 0.051 |
| 5.5 | 0.031 | 5.5 | 0.037 | 5.5 | 0.042 | 5.5 | 0.046 | 5.5 | 0.051 | 5.5 | 0.051 | 5.5 | 0.051 | 5.5 | 0.051 |
| 6.0 | 0.029 | 6.0 | 0.035 | 6.0 | 0.040 | 6.0 | 0.044 | 6.0 | 0.048 | 6.0 | 0.048 | 6.0 | 0.048 | 6.0 | 0.048 |
| 6.5 | 0.027 | 6.5 | 0.033 | 6.5 | 0.038 | 6.5 | 0.042 | 6.5 | 0.046 | 6.5 | 0.046 | 6.5 | 0.046 | 6.5 | 0.046 |
| 7.0 | 0.026 | 7.0 | 0.032 | 7.0 | 0.037 | 7.0 | 0.042 | 7.0 | 0.046 | 7.0 | 0.046 | 7.0 | 0.046 | 7.0 | 0.046 |
| 7.5 | 0.025 | 7.5 | 0.031 | 7.5 | 0.035 | 7.5 | 0.039 | 7.5 | 0.043 | 7.5 | 0.043 | 7.5 | 0.043 | 7.5 | 0.043 |
| 8.0 | 0.024 | 8.0 | 0.030 | 8.0 | 0.034 | 8.0 | 0.037 | 8.0 | 0.041 | 8.0 | 0.041 | 8.0 | 0.041 | 8.0 | 0.041 |
| 8.5 | 0.023 | 8.5 | 0.029 | 8.5 | 0.033 | 8.5 | 0.036 | 8.5 | 0.040 | 8.5 | 0.040 | 8.5 | 0.040 | 8.5 | 0.040 |
| 9.0 | 0.023 | 9.0 | 0.028 | 9.0 | 0.032 | 9.0 | 0.035 | 9.0 | 0.039 | 9.0 | 0.039 | 9.0 | 0.039 | 9.0 | 0.039 |
| 9.5 | 0.022 | 9.5 | 0.027 | 9.5 | 0.031 | 9.5 | 0.034 | 9.5 | 0.038 | 9.5 | 0.038 | 9.5 | 0.038 | 9.5 | 0.038 |
| 10.0 | 0.021 | 10.0 | 0.026 | 10.0 | 0.030 | 10.0 | 0.033 | 10.0 | 0.037 | 10.0 | 0.037 | 10.0 | 0.037 | 10.0 | 0.037 |
| 10.5 | 0.021 | 10.5 | 0.026 | 10.5 | 0.029 | 10.5 | 0.032 | 10.5 | 0.036 | 10.5 | 0.036 | 10.5 | 0.036 | 10.5 | 0.036 |
| 11.0 | 0.020 | 11.0 | 0.025 | 11.0 | 0.029 | 11.0 | 0.032 | 11.0 | 0.036 | 11.0 | 0.036 | 11.0 | 0.036 | 11.0 | 0.036 |
| 11.5 | 0.020 | 11.5 | 0.025 | 11.5 | 0.028 | 11.5 | 0.031 | 11.5 | 0.035 | 11.5 | 0.035 | 11.5 | 0.035 | 11.5 | 0.035 |
| 12.0 | 0.019 | 12.0 | 0.024 | 12.0 | 0.028 | 12.0 | 0.031 | 12.0 | 0.035 | 12.0 | 0.035 | 12.0 | 0.035 | 12.0 | 0.035 |
| 12.5 | 0.019 | 12.5 | 0.024 | 12.5 | 0.027 | 12.5 | 0.030 | 12.5 | 0.034 | 12.5 | 0.034 | 12.5 | 0.034 | 12.5 | 0.034 |
| 13.0 | 0.019 | 13.0 | 0.023 | 13.0 | 0.026 | 13.0 | 0.029 | 13.0 | 0.033 | 13.0 | 0.033 | 13.0 | 0.033 | 13.0 | 0.033 |
| 13.5 | 0.018 | 13.5 | 0.023 | 13.5 | 0.026 | 13.5 | 0.029 | 13.5 | 0.033 | 13.5 | 0.033 | 13.5 | 0.033 | 13.5 | 0.033 |
| 14.0 | 0.018 | 14.0 | 0.022 | 14.0 | 0.025 | 14.0 | 0.028 | 14.0 | 0.032 | 14.0 | 0.032 | 14.0 | 0.032 | 14.0 | 0.032 |
| 14.5 | 0.017 | 14.5 | 0.022 | 14.5 | 0.025 | 14.5 | 0.028 | 14.5 | 0.032 | 14.5 | 0.032 | 14.5 | 0.032 | 14.5 | 0.032 |
| 15.0 | 0.017 | 15.0 | 0.021 | 15.0 | 0.025 | 15.0 | 0.028 | 15.0 | 0.032 | 15.0 | 0.032 | 15.0 | 0.032 | 15.0 | 0.032 |

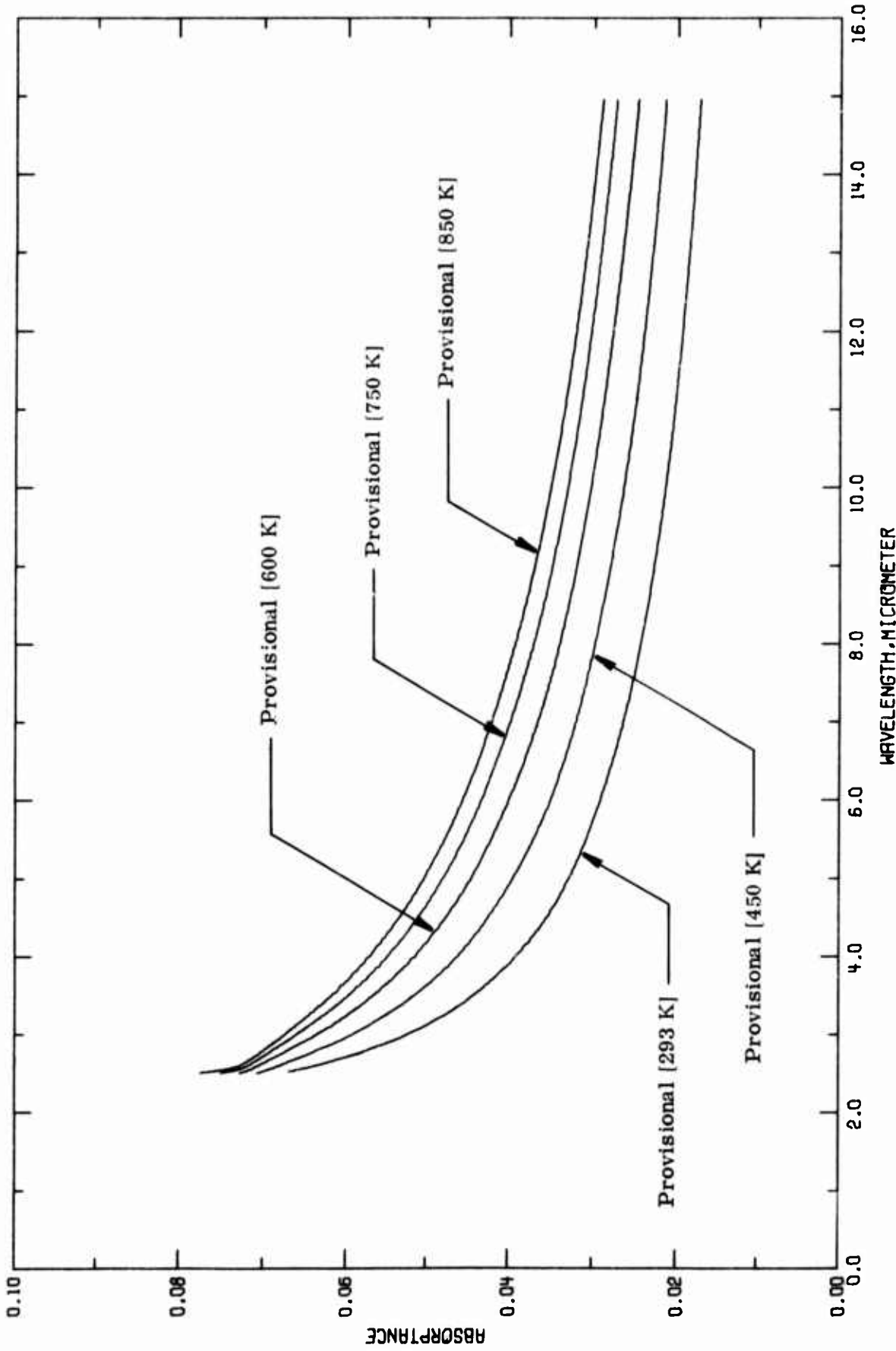


FIGURE 22-5. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (WAVELENGTH DEPENDENCE).

f. Normal Spectral Absorptance (Temperature Dependence)

The provisional values of the normal spectral absorptance of graphite fiber aluminum matrix composite is given in Table 22-6 and plotted in Figure 22-6. They are numerically equal to the normal spectral emittance. In Figure 22-6, our predicted curves for $5.0\ \mu\text{m}$ and $10.0\ \mu\text{m}$ are higher than experimental values plotted in Figure 20-5. By a careful examination of the measurement information, one sees that the experimental points in Figure 20-5 are for thin films. The absorptance of bulk material is in general higher than that of thin film. An uncertainty of 25% is incorporated to the provisional values so that they can be used for most of the real surfaces.

TABLE 22-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE)

WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α :

| T | α | T | α | T | α | T | α |
|---|----------|---|----------|---|----------|--|----------|
| MECHANICALLY POLISHED $\lambda = 2.0$ | | MECHANICALLY POLISHED $\lambda = 3.8$ | | MECHANICALLY POLISHED $\lambda = 5.0$ | | MECHANICALLY POLISHED $\lambda = 10.6$ | |
| 250.0 | 0.054 | 250.0 | 0.038 | 250.0 | 0.030 | 250.0 | 0.019 |
| 293.0 | 0.057 | 293.0 | 0.041 | 293.0 | 0.033 | 293.0 | 0.021 |
| 300.0 | 0.057 | 300.0 | 0.041 | 300.0 | 0.033 | 300.0 | 0.021 |
| 350.0 | 0.060 | 350.0 | 0.044 | 350.0 | 0.036 | 350.0 | 0.023 |
| 400.0 | 0.062 | 400.0 | 0.046 | 400.0 | 0.038 | 400.0 | 0.024 |
| 450.0 | 0.063 | 450.0 | 0.048 | 450.0 | 0.040 | 450.0 | 0.026 |
| 500.0 | 0.065 | 500.0 | 0.050 | 500.0 | 0.041 | 500.0 | 0.027 |
| 550.0 | 0.066 | 550.0 | 0.052 | 550.0 | 0.043 | 550.0 | 0.028 |
| 600.0 | 0.067 | 600.0 | 0.053 | 600.0 | 0.044 | 600.0 | 0.029 |
| 650.0 | 0.068 | 650.0 | 0.055 | 650.0 | 0.046 | 650.0 | 0.030 |
| 700.0 | 0.069 | 700.0 | 0.056 | 700.0 | 0.047 | 700.0 | 0.031 |
| 750.0 | 0.069 | 750.0 | 0.057 | 750.0 | 0.048 | 750.0 | 0.032 |
| 800.0 | 0.069 | 800.0 | 0.058 | 800.0 | 0.049 | 800.0 | 0.033 |
| 850.0 | 0.070 | 850.0 | 0.059 | 850.0 | 0.050 | 850.0 | 0.034 |
| 900.0 | 0.070 | 900.0 | 0.059 | 900.0 | 0.051 | 900.0 | 0.035 |

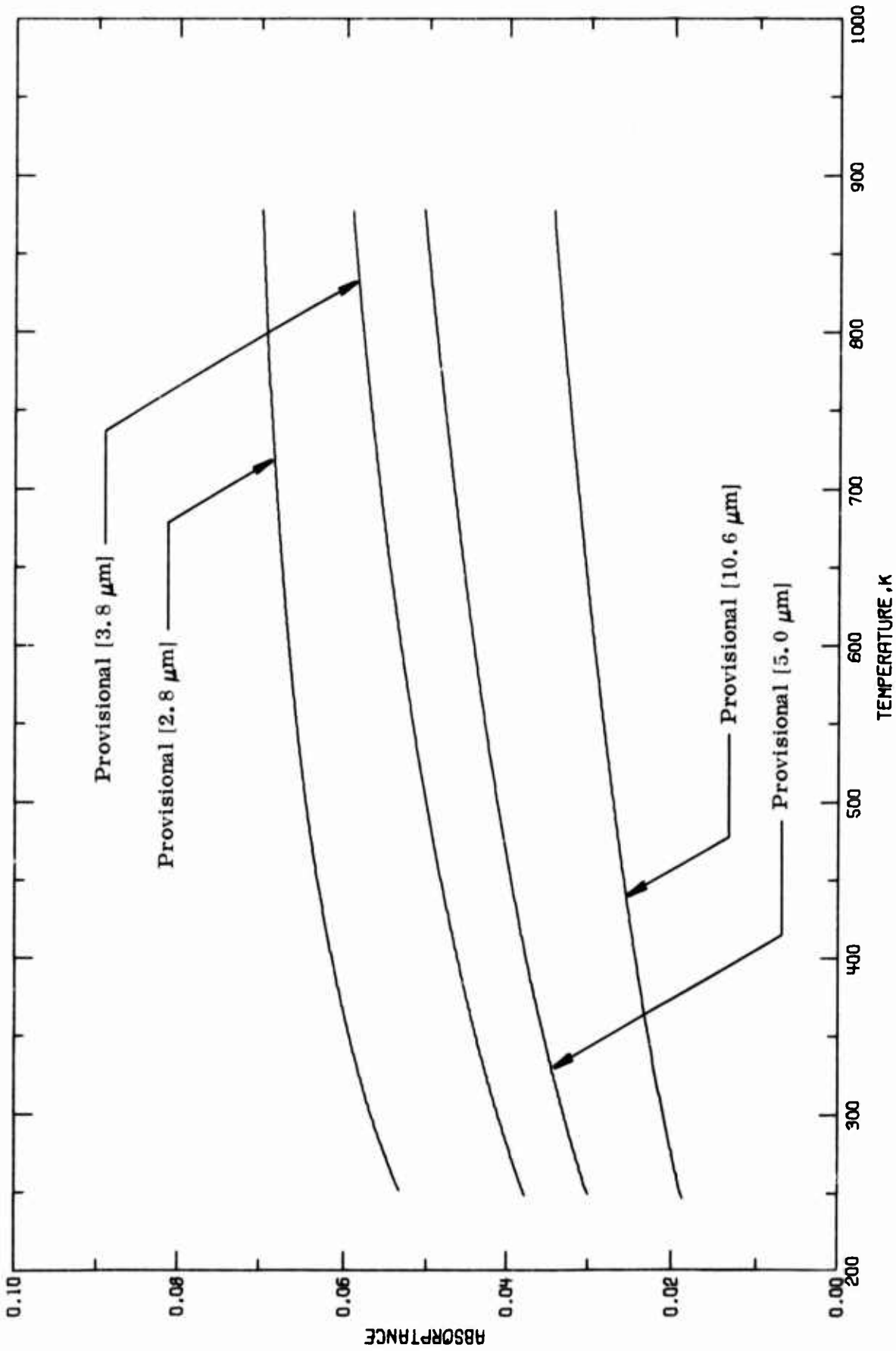


FIGURE 22-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER ALUMINUM MATRIX COMPOSITE (TEMPERATURE DEPENDENCE).

g. Transmittance

Although it is true that metals in the form of extremely thin films may be transparent for a wide wavelength range, they are opaque if the thickness is greater than several hundred angstroms. Consequently, composites with metal matrix are opaque to visible and infrared radiation because in general applications they are not used as extremely thin films. This leads to the conclusion that as an aircraft/spacecraft structural material, this composite is opaque and its transmittance is zero.

4.23. Boron Fiber Epoxy Composite

This composite material consists usually of continuous boron filaments surrounded by a matrix of epoxy resin. It is usually produced in tape form so it can be used in further fabrication of specialized materials.

The boron filaments, as currently produced, are formed by vapor deposition of boron on a fine tungsten wire substrate within a reactor. Exposure of the tungsten substrate to the high-temperature boron trichloride reactor environment results in a filament consisting of a boron sheath on a tungsten boride core. Other means of producing boron filaments are currently being investigated which would eliminate the tungsten substrate.

The organic matrix resins most commonly used with boron filaments are modified epoxy resins available as commercial formulations developed specifically for this purpose. Other organic resins used include polyamides and phenolics. However, the state of the art with these resins is less advanced than for the epoxy materials.

The normal service temperature range of the boron fiber epoxy composite is dependent on the type of epoxy resin being used as a matrix. This range is nominally 220 K, where the epoxy becomes very brittle, to 450 K. Epoxy resin decomposes around 590 K.

The boron fiber epoxy is fabricated primarily for aircraft constructions, much of its mechanical and thermal properties are studied. As a result, a large amount of experimental data are made available. However, with regard to the thermal radiative properties of the composite, it is quite discouraging. Only one set of systematic experimentally determined data on the normal spectral reflectance is all that can be uncovered by our open literature search. This leaves us no choice but to use it as the basis for the estimation of the most probable values of the radiative properties for boron fiber epoxy composite.

The fact that the composite material is made by bonding boron fibers in a matrix of epoxy resin implies that epoxy is the material which predominately contributes to the thermal radiative properties of the composite material. The other component, the boron fiber, plays minor role. Indeed, by comparing the shapes of the normal spectral reflectance curves (Figure 23-4 in this subsection and Figures 24-4 and 25-4 in subsections 4.24 and 4.25 respectively) we can see the spectral band patterns of the three epoxy composite materials (boron fiber epoxy composite, glass fiber epoxy composite and graphite fiber epoxy composite) are similar.

Reflectance of epoxy is generally fairly low, about 10%, for wavelengths longer than 2.5 μm . Also, it does not change appreciably as the material is heated up and goes decomposition phase and into the char region [A00004]. In other words, the radiative properties of epoxy are independent of temperature.

For epoxy composite materials, the following two relations are commonly used as good approximations:

$$\alpha(0, \lambda) = 1 - \rho(0, 2\pi, \lambda);$$

$$\epsilon(0, \lambda) = \alpha(0, \lambda),$$

because of opaqueness of the materials.

According to the facts discussed above, we are in a position to estimate the following six subproperties for boron fiber epoxy composite based on the single available set of reflectance data:

- Normal spectral emittance (wavelength dependence)
- Normal spectral emittance (temperature dependence)
- Normal spectral reflectance (wavelength dependence)
- Normal spectral reflectance (temperature dependence)
- Normal spectral absorptance (wavelength dependence)
- Normal spectral absorptance (temperature dependence)

a. Normal Spectral Emittance (Wavelength Dependence)

Provisional values of the normal spectral emittance of slightly grit-blasted boron fiber epoxy composite are obtained from the analyzed result of reflectance by using the relation $\alpha(0, \lambda) = 1 - \rho(0, 2\pi, \lambda)$ and Kirchhoff's law. Such conversion is frequently used for the materials whose reflectance is known [A00004]. The provisional values, listed in Table 23-1 and plotted in Figure 23-1, are in general very close to unity. For rough uses, a value of 0.95 can be safely used because the uncertainty of the provisional values is $\pm 20\%$.

TABLE 23-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ |
|--------------|------------|
| LIGHTLY | |
| GRIT-BLASTED | |
| T = 293 | |
| 2.5 | 0.934 |
| 2.8 | 0.955 |
| 3.0 | 0.962 |
| 3.5 | 0.955 |
| 3.8 | 0.944 |
| 4.0 | 0.942 |
| 4.5 | 0.940 |
| 5.0 | 0.940 |
| 5.5 | 0.940 |
| 6.0 | 0.965 |
| 6.5 | 0.967 |
| 7.0 | 0.967 |
| 7.5 | 0.967 |
| 8.0 | 0.966 |
| 8.5 | 0.962 |
| 9.0 | 0.959 |
| 9.5 | 0.958 |
| 10.0 | 0.956 |
| 10.5 | 0.956 |
| 10.6 | 0.956 |
| 11.0 | 0.956 |
| 11.5 | 0.956 |
| 12.0 | 0.956 |
| 12.5 | 0.956 |
| 13.0 | 0.956 |
| 13.5 | 0.956 |
| 14.0 | 0.957 |
| 14.5 | 0.961 |
| 15.0 | 0.973 |

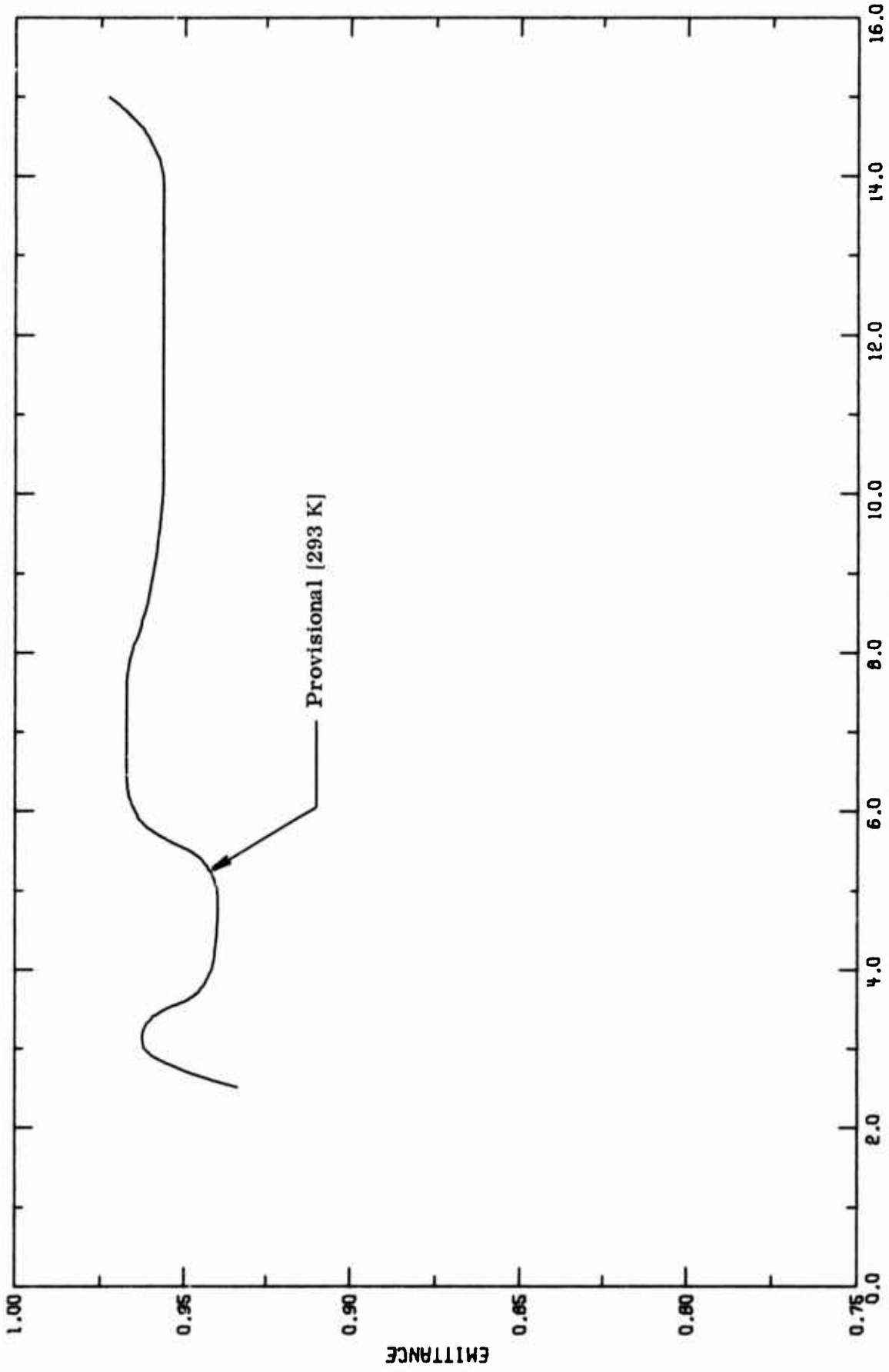


FIGURE 23-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

b. Normal Spectral Emittance (Temperature Dependence)

The normal spectral emittance as a function of temperature is given in Table 23-2 and plotted in Figure 23-2. The generated values are considered as provisional with 20% uncertainty. Here, we present the property values as a constant for a given wavelength because it has been observed in epoxy composites that the radiative properties do not change appreciably with temperature [A00002]. With 20% uncertainty, the provisional values can be safely used for most of the true surfaces.

TABLE 23-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIRED EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|---|------------|---|------------|---|------------|--|------------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 3.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | |
| 250.0 | 0.955 | 250.0 | 0.944 | 250.0 | 0.940 | 250.0 | 0.956 |
| 300.0 | 0.955 | 300.0 | 0.944 | 300.0 | 0.940 | 300.0 | 0.956 |
| 350.0 | 0.955 | 350.0 | 0.944 | 350.0 | 0.940 | 350.0 | 0.956 |
| 400.0 | 0.955 | 400.0 | 0.944 | 400.0 | 0.940 | 400.0 | 0.956 |
| 450.0 | 0.955 | 450.0 | 0.944 | 450.0 | 0.940 | 450.0 | 0.956 |
| 500.0 | 0.955 | 500.0 | 0.944 | 500.0 | 0.940 | 500.0 | 0.956 |

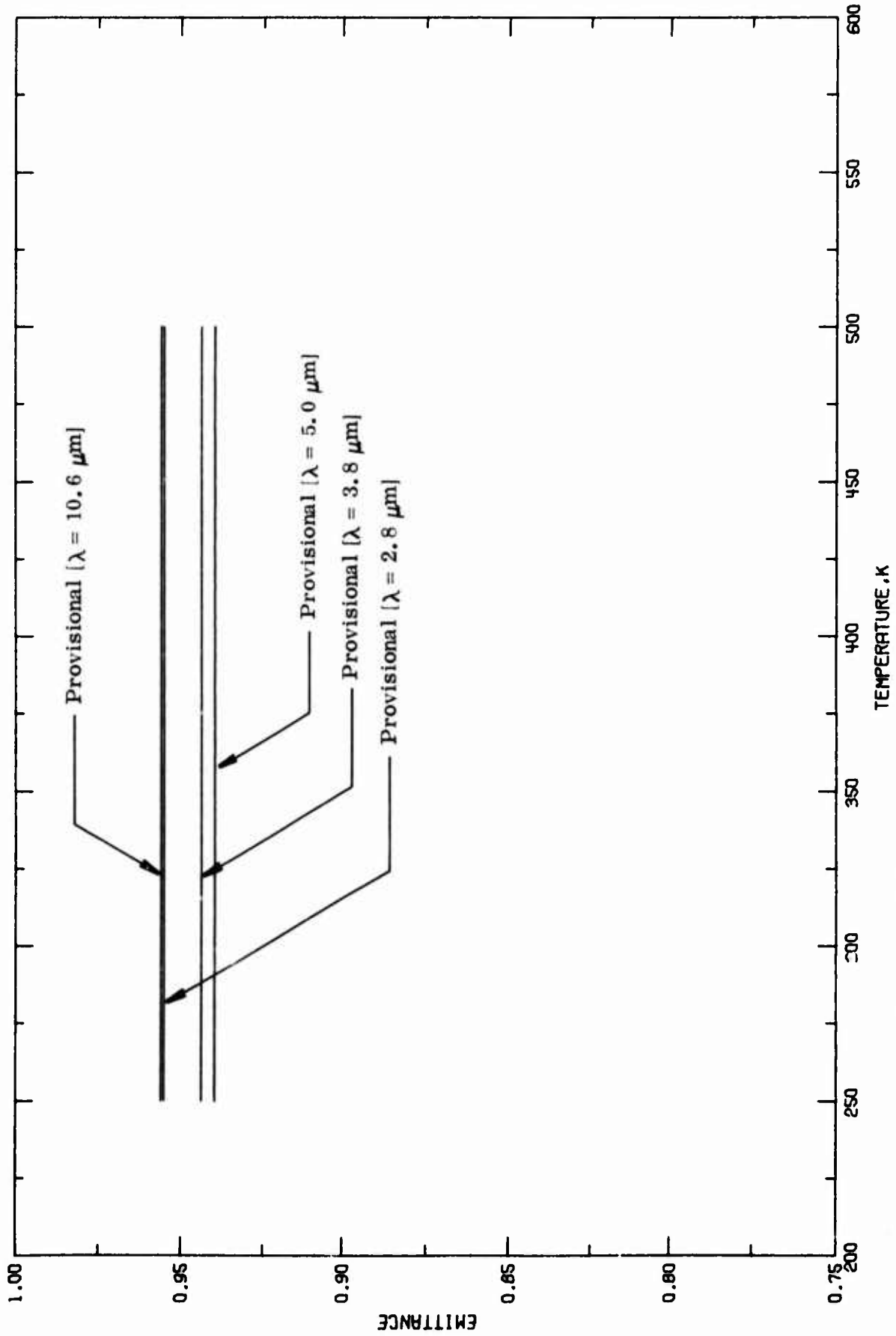


FIGURE 23-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

As given in Table 23-3 and plotted in Figure 23-3, the provisional values of boron fiber epoxy composite are obtained by reading off from a curve smoothed out from the only available set of data shown in Figure 23-4. It shows a quite complex spectral distribution of energy reflected from the composite material. Because of scantiness of the available data and spectral complexity, no attempt was made to carry out analytical calculations but the smoothing technique. An estimated uncertainty of 25% is given to the provisional values which are believed to be reasonable for most of the real surfaces.

TABLE 23-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|--------------|--------|
| LIGHTLY | |
| GRIT-BLASTED | |
| $T = 293$ | |
| 2.5 | 0.066 |
| 2.8 | 0.045 |
| 3.0 | 0.038 |
| 3.5 | 0.045 |
| 3.8 | 0.056 |
| 4.0 | 0.058 |
| 4.5 | 0.060 |
| 5.0 | 0.060 |
| 5.5 | 0.052 |
| 6.0 | 0.035 |
| 6.5 | 0.033 |
| 7.0 | 0.033 |
| 7.5 | 0.033 |
| 8.0 | 0.034 |
| 8.5 | 0.038 |
| 9.0 | 0.041 |
| 9.5 | 0.042 |
| 10.0 | 0.044 |
| 10.5 | 0.044 |
| 10.6 | 0.044 |
| 11.0 | 0.044 |
| 11.5 | 0.044 |
| 12.0 | 0.044 |
| 12.5 | 0.044 |
| 13.0 | 0.044 |
| 13.5 | 0.044 |
| 14.0 | 0.043 |
| 14.5 | 0.039 |
| 15.0 | 0.027 |

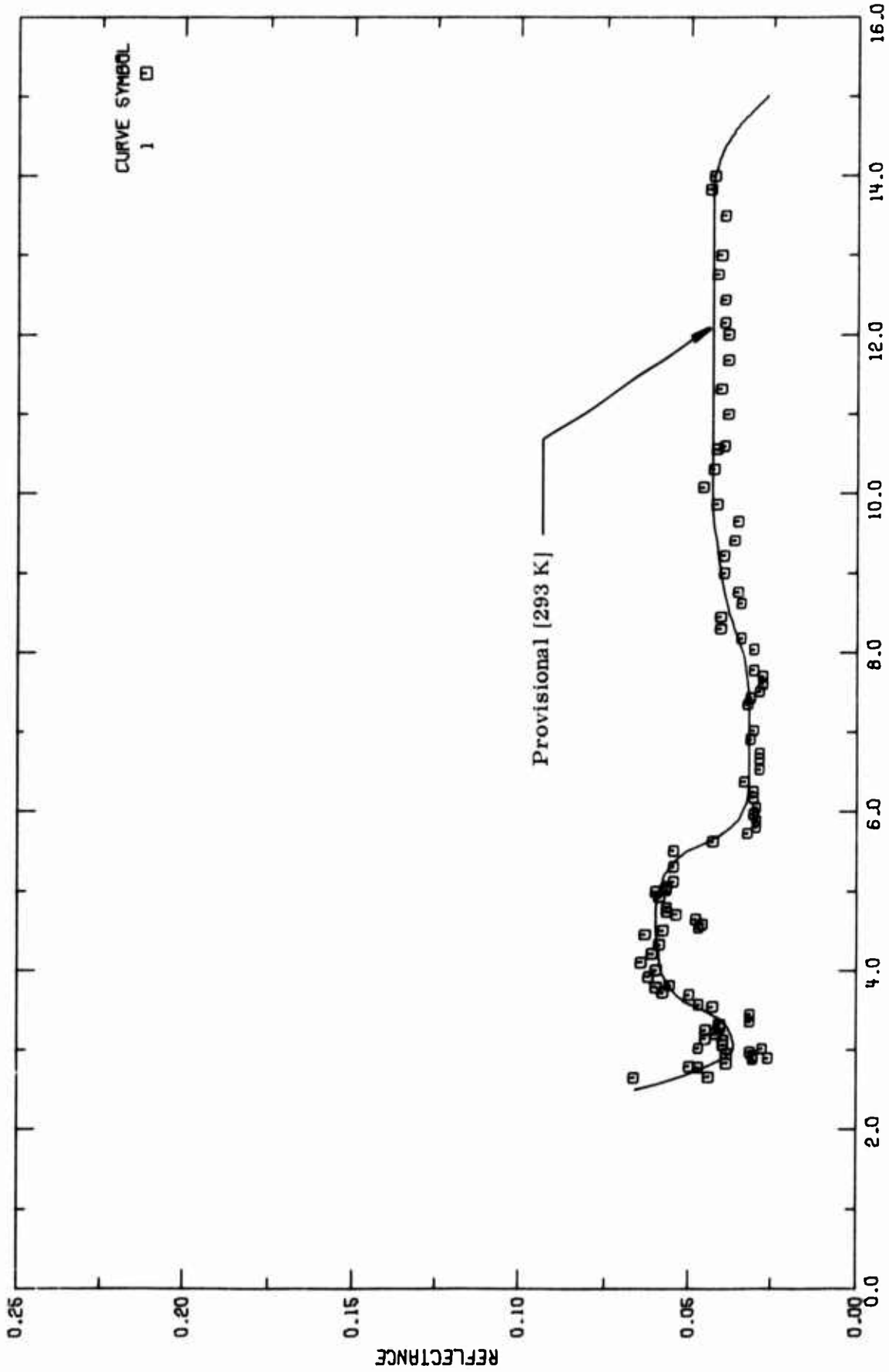


FIGURE 23-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

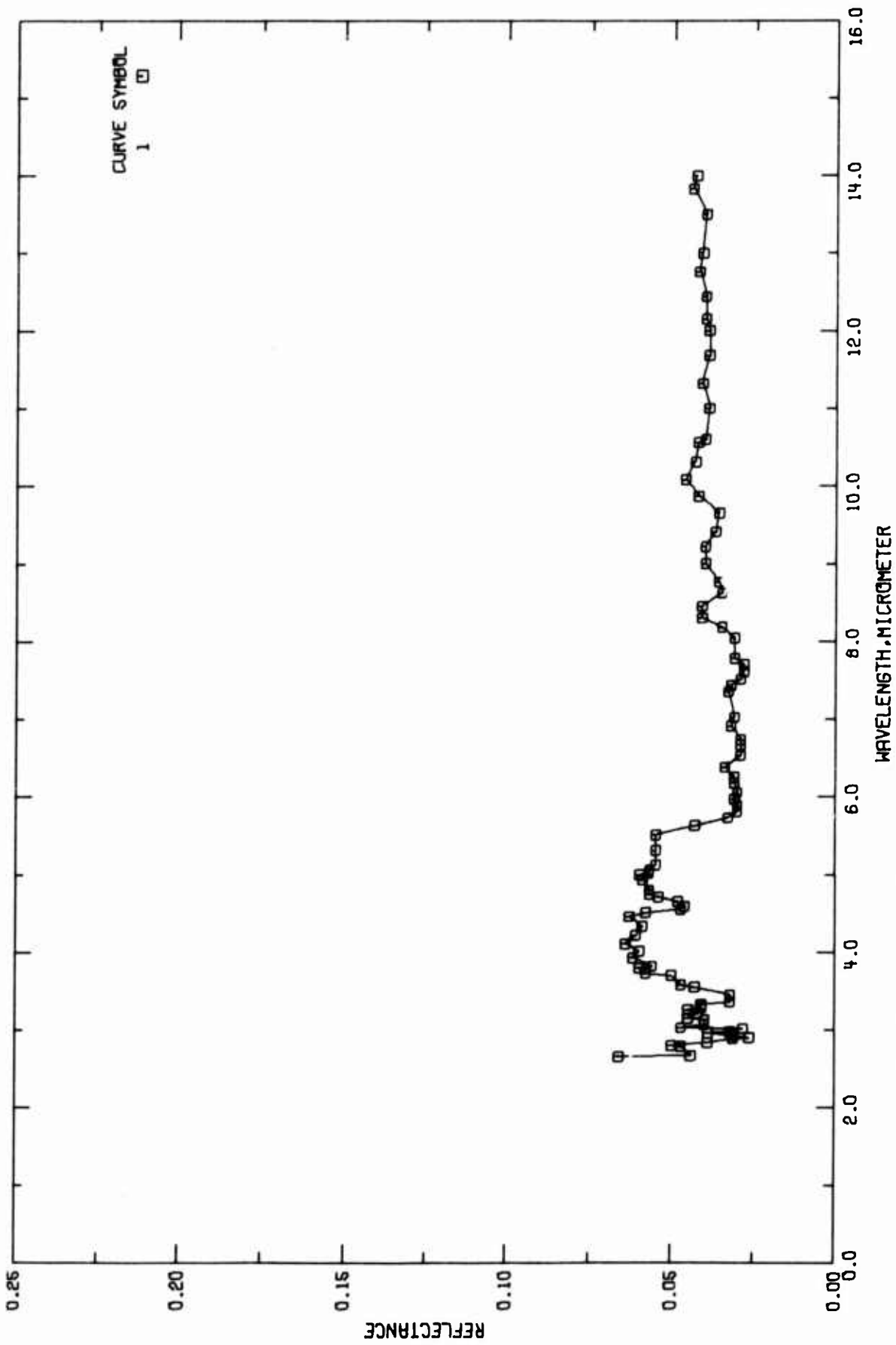


FIGURE 23-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

TABLE 23-4 MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00001 | Grimm, T.C. | 1972 | 2.0-14.7 | 293 | | Bare surface specimen; 2.54 cm square; lightly grit-blasted; prepared by the Organic Chemistry Laboratory in the company where the author worked; measurements made with a Dunn Associates ellipsoidal mirror reflectometer; data extracted from a figure; relative reflectance reported; multiplied by 0.95 to convert to absolute values (gold reference mirror used); $\theta = 15^\circ$, $\omega' = 2\pi$. |

TABLE 23-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF RANDOM FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | |
|-----------|--------|-----------------|--------|-----------------|--------|
| λ | ρ | λ | ρ | λ | ρ |
| 2.66 | 0.066 | 4.80 | 0.057 | 10.31 | 0.043 |
| 2.67 | 0.044 | 4.93 | 0.059 | 10.56 | 0.042 |
| 2.79 | 0.047 | 5.00 | 0.060 | 10.60 | 0.043 |
| 2.80 | 0.050 | 5.02 | 0.057 | 11.00 | 0.039 |
| 2.84 | 0.039 | 5.05 | 0.057 | 11.32 | 0.041 |
| 2.89 | 0.031 | 5.12 | 0.055 | 11.69 | 0.039 |
| 2.90 | 0.026 | 5.31 | 0.055 | 12.00 | 0.039 |
| 2.93 | 0.031 | 5.51 | 0.055 | 12.15 | 0.040 |
| 2.96 | 0.039 | 5.63 | 0.043 | 12.44 | 0.040 |
| 2.98 | 0.032 | 5.73 | 0.033 | 12.76 | 0.042 |
| 3.02 | 0.020 | 5.81 | 0.030 | 13.00 | 0.041 |
| 3.03 | 0.047 | 5.89 | 0.030 | 13.50 | 0.040 |
| 3.07 | 0.040 | 5.97 | 0.031 | 13.63 | 0.044 |
| 3.13 | 0.040 | 6.05 | 0.030 | 14.00 | 0.042 |
| 3.15 | 0.045 | 6.18 | 0.031 | 14.26 | 0.040 |
| 3.21 | 0.042 | 6.25 | 0.031 | 14.51 | 0.033 |
| 3.26 | 0.045 | 6.38 | 0.034 | 14.69 | 0.030 |
| 3.29 | 0.041 | 6.53 | 0.029 | | |
| 3.33 | 0.041 | 6.67 | 0.029 | | |
| 3.36 | 0.032 | 6.73 | 0.029 | | |
| 3.45 | 0.032 | 6.91 | 0.032 | | |
| 3.55 | 0.043 | 7.02 | 0.031 | | |
| 3.58 | 0.047 | 7.35 | 0.033 | | |
| 3.70 | 0.050 | 7.43 | 0.032 | | |
| 3.73 | 0.050 | 7.51 | 0.029 | | |
| 3.80 | 0.060 | 7.61 | 0.028 | | |
| 3.82 | 0.056 | 7.70 | 0.029 | | |
| 3.93 | 0.062 | 7.78 | 0.031 | | |
| 4.01 | 0.060 | 8.04 | 0.031 | | |
| 4.11 | 0.064 | 8.18 | 0.035 | | |
| 4.22 | 0.061 | 8.30 | 0.041 | | |
| 4.33 | 0.059 | 8.45 | 0.041 | | |
| 4.46 | 0.063 | 8.62 | 0.035 | | |
| 4.51 | 0.058 | 8.76 | 0.036 | | |
| 4.55 | 0.047 | 9.00 | 0.040 | | |
| 4.59 | 0.046 | 9.22 | 0.040 | | |
| 4.65 | 0.048 | 9.41 | 0.037 | | |
| 4.71 | 0.054 | 9.65 | 0.036 | | |
| 4.75 | 0.057 | 9.87 | 0.042 | | |
| | | 10.08 | 0.046 | | |

d. Normal Spectral Reflectance (Temperature Dependence)

In Table 23-6, the provisional values of the normal spectral reflectance are given with estimated uncertainties of $\pm 25\%$. The variation of the property as a function of temperature is demonstrated in Figure 23-5. For a given wavelength, the normal spectral reflectance remains as a constant from room temperature up to the char region of epoxy. The independency of the reflectance of epoxy composite with temperature has been observed experimentally [A00002]. The reported provisional values are believed to be reasonable in most of the real situation.

TABLE 23-6. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ | T | ρ | T | ρ | T | ρ |
|---------------------------------------|--------|-------|--------|-------|--------|-------|--------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.8$ | | | | | | | |
| 250.0 | 0.045 | 250.0 | 0.056 | 250.0 | 0.060 | 250.0 | 0.044 |
| 300.0 | 0.045 | 300.0 | 0.056 | 300.0 | 0.060 | 300.0 | 0.044 |
| 350.0 | 0.045 | 350.0 | 0.056 | 350.0 | 0.060 | 350.0 | 0.044 |
| 400.0 | 0.045 | 400.0 | 0.056 | 400.0 | 0.060 | 400.0 | 0.044 |
| 450.0 | 0.045 | 450.0 | 0.056 | 450.0 | 0.060 | 450.0 | 0.044 |
| 500.0 | 0.045 | 500.0 | 0.056 | 500.0 | 0.060 | 500.0 | 0.044 |
| LIGHTLY GRIT-BLASTED $\lambda = 3.0$ | | | | | | | |
| 250.0 | 0.045 | 250.0 | 0.056 | 250.0 | 0.060 | 250.0 | 0.044 |
| 300.0 | 0.045 | 300.0 | 0.056 | 300.0 | 0.060 | 300.0 | 0.044 |
| 350.0 | 0.045 | 350.0 | 0.056 | 350.0 | 0.060 | 350.0 | 0.044 |
| 400.0 | 0.045 | 400.0 | 0.056 | 400.0 | 0.060 | 400.0 | 0.044 |
| 450.0 | 0.045 | 450.0 | 0.056 | 450.0 | 0.060 | 450.0 | 0.044 |
| 500.0 | 0.045 | 500.0 | 0.056 | 500.0 | 0.060 | 500.0 | 0.044 |
| LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | | | | | | | |
| 250.0 | 0.045 | 250.0 | 0.056 | 250.0 | 0.060 | 250.0 | 0.044 |
| 300.0 | 0.045 | 300.0 | 0.056 | 300.0 | 0.060 | 300.0 | 0.044 |
| 350.0 | 0.045 | 350.0 | 0.056 | 350.0 | 0.060 | 350.0 | 0.044 |
| 400.0 | 0.045 | 400.0 | 0.056 | 400.0 | 0.060 | 400.0 | 0.044 |
| 450.0 | 0.045 | 450.0 | 0.056 | 450.0 | 0.060 | 450.0 | 0.044 |
| 500.0 | 0.045 | 500.0 | 0.056 | 500.0 | 0.060 | 500.0 | 0.044 |
| LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | | | | | | | |
| 250.0 | 0.045 | 250.0 | 0.056 | 250.0 | 0.060 | 250.0 | 0.044 |
| 300.0 | 0.045 | 300.0 | 0.056 | 300.0 | 0.060 | 300.0 | 0.044 |
| 350.0 | 0.045 | 350.0 | 0.056 | 350.0 | 0.060 | 350.0 | 0.044 |
| 400.0 | 0.045 | 400.0 | 0.056 | 400.0 | 0.060 | 400.0 | 0.044 |
| 450.0 | 0.045 | 450.0 | 0.056 | 450.0 | 0.060 | 450.0 | 0.044 |
| 500.0 | 0.045 | 500.0 | 0.056 | 500.0 | 0.060 | 500.0 | 0.044 |

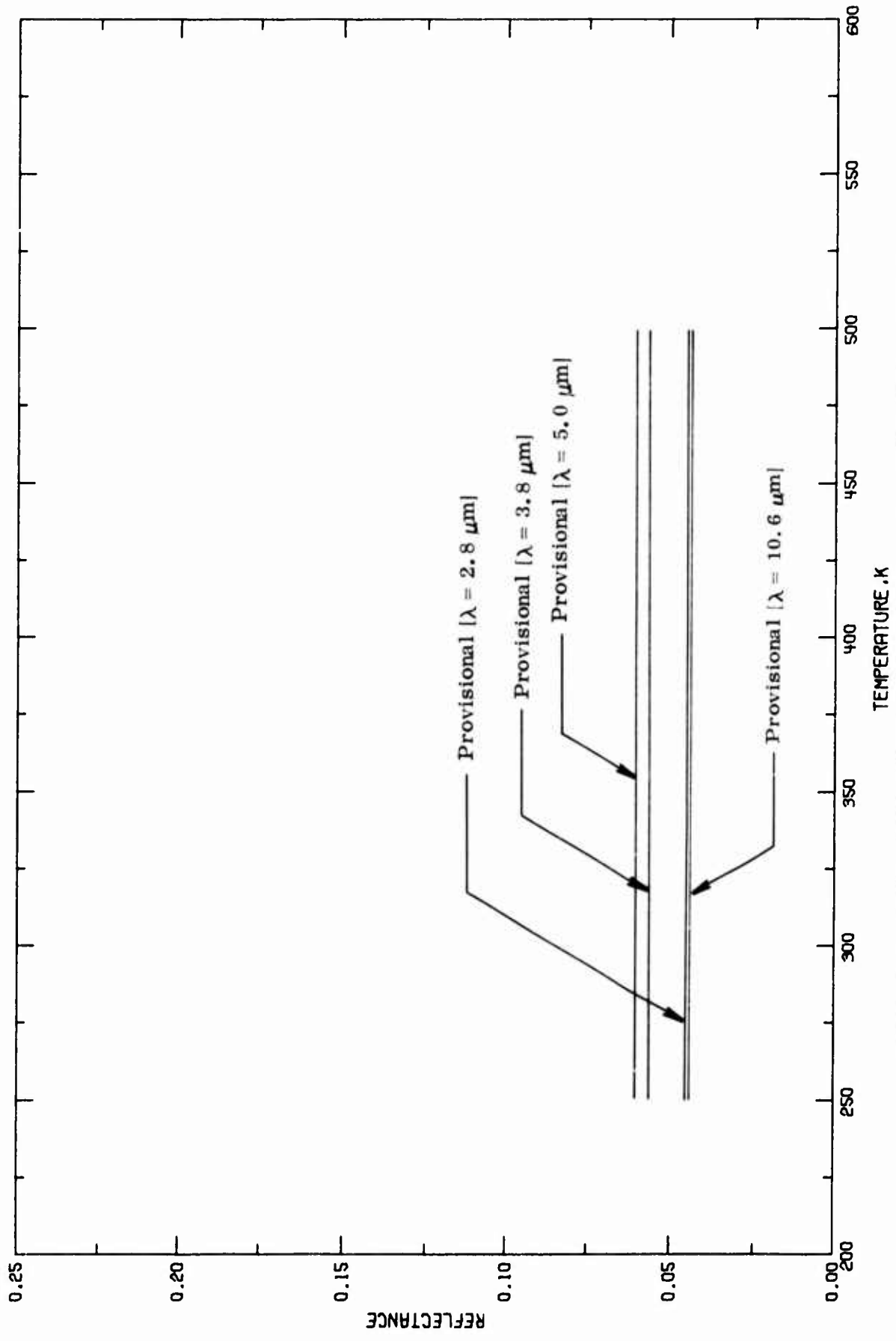


FIGURE 23-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

The normal spectral absorptance is obtained according to the Kirchhoff's law, i. e., numerically the absorptance is equal to the emittance. As a result, Table 23-7 and Figure 23-6 appear the same as Table 23-1 and Figure 23-1, as well as the estimated uncertainties ($\pm 20\%$).

TABLE 23-7. PROVISIONAL NORMAL SPECTRAL ABSORPTIANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|------------------------------------|----------|
| LIGHTLY GRIT-BLASTED T = 293 | |
| 2.5 | 0.934 |
| 2.8 | 0.955 |
| 3.0 | 0.962 |
| 3.5 | 0.955 |
| 3.8 | 0.944 |
| 4.0 | 0.942 |
| 4.5 | 0.940 |
| 5.0 | 0.940 |
| 5.5 | 0.955 |
| 6.0 | 0.967 |
| 6.5 | 0.967 |
| 7.0 | 0.967 |
| 7.5 | 0.967 |
| 8.0 | 0.966 |
| 8.5 | 0.962 |
| 9.0 | 0.959 |
| 9.5 | 0.958 |
| 10.0 | 0.956 |
| 10.5 | 0.956 |
| 10.6 | 0.956 |
| 11.0 | 0.956 |
| 11.5 | 0.956 |
| 12.0 | 0.956 |
| 12.5 | 0.956 |
| 13.0 | 0.956 |
| 13.5 | 0.956 |
| 14.0 | 0.957 |
| 14.5 | 0.961 |
| 15.0 | 0.973 |

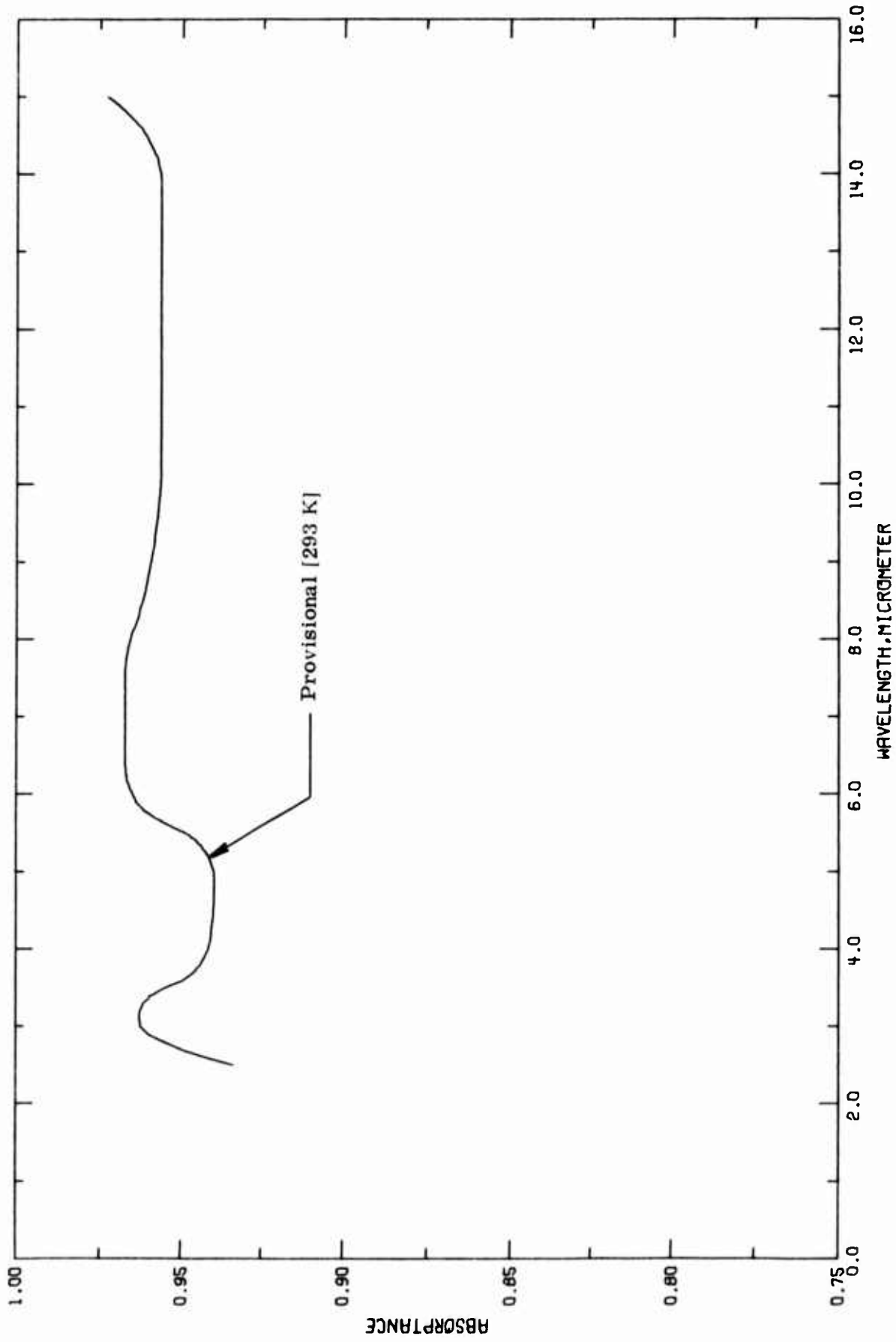


FIGURE 23-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

f. Normal Spectral Absorptance (Temperature Dependence)

The normal spectral absorptance as a function of temperature is given in Table 23-8 and plotted in Figure 23-7. The generated values are considered as provisional with 20% uncertainty. Here, we present the property values as constant for a given wavelength because it has been observed in epoxy composites that the radiative properties do not change appreciably with temperature [A00002]. With 20% uncertainty, the provisional values can be safely used for most of the true surfaces.

TABLE 23-8. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF UDOPON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α | T | α | T | α | T | α |
|--|----------|--|----------|--|----------|---|----------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.0$ | 0.955 | LIGHTLY GRIT-BLASTED $\lambda = 3.0$ | 0.944 | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | 0.940 | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | 0.956 |
| 250.0 | 0.955 | 250.0 | 0.944 | 250.0 | 0.940 | 250.0 | 0.956 |
| 300.0 | 0.955 | 300.0 | 0.944 | 300.0 | 0.940 | 300.0 | 0.956 |
| 350.0 | 0.955 | 350.0 | 0.944 | 350.0 | 0.940 | 350.0 | 0.956 |
| 400.0 | 0.955 | 400.0 | 0.944 | 400.0 | 0.940 | 400.0 | 0.956 |
| 450.0 | 0.955 | 450.0 | 0.944 | 450.0 | 0.940 | 450.0 | 0.956 |
| 500.0 | 0.955 | 500.0 | 0.944 | 500.0 | 0.940 | 500.0 | 0.956 |

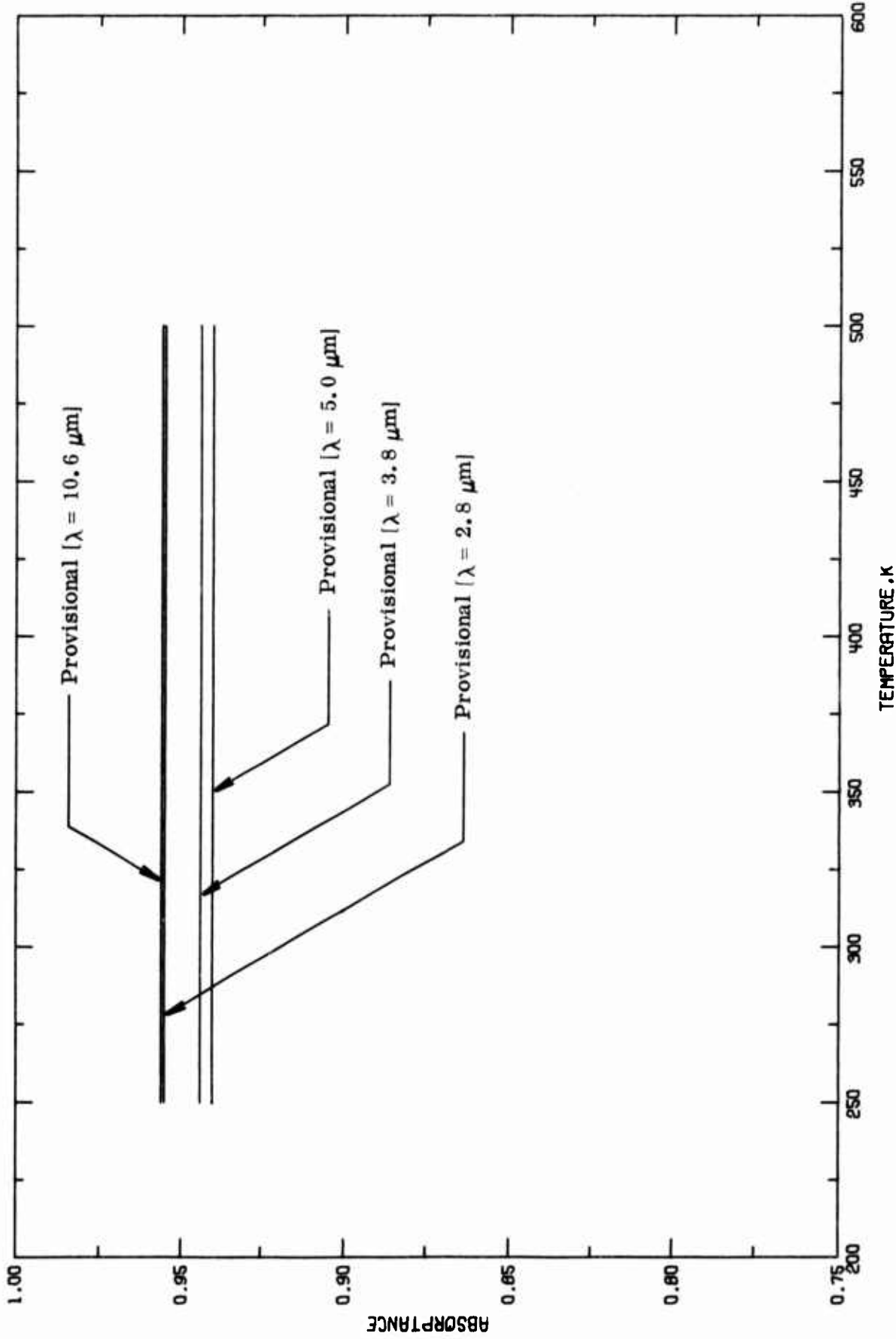


FIGURE 23-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF BORON FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

4.24. Glass Fiber Epoxy Composite

A small amount of the exterior area of the aircraft is composed of nonmetallics. These nonmetallics consist chiefly various glass fiber reinforced plastics, and epoxy composites, etc.

Composite materials have received great interest in the last decade because they provide unusual combinations of properties which cannot be obtained with any single, homogeneous substance. In aircraft and missile design, they have provided structural materials of very high strength and elastic modulus which also have low densities.

Among nonmetallic composites, the glass/epoxy composites are the most commonly used. The glass fiber epoxy composite consists usually of fine glass fibers surrounded by a matrix of epoxy resin. The other alternative form commonly used is the glass fabric reinforced plastics with epoxy surfacer.

Modified epoxy resins developed specifically for use in composites with glass fiber are available commercially. These are thermosetting resins used for low pressure laminating which normally cannot be used in continuous service above about 450 K although intermittent service at temperature up to 490 K is possible. Many of the various epoxy resins used as matrix constituents of composites are proprietary formulations whose exact chemical compositions are not available.

Although the mechanical and thermal properties of glass/epoxy composites are well studied, the thermal radiative properties are unattended. As a result, only one set of experimentally determined data on the normal spectral reflectance is all that can be found by our open literature search. This leaves us no choice but to use it as the basis for the estimation of the most probable values of the radiative properties for glass fiber epoxy composite.

The fact that the composite material is made by bonding the fibers in a matrix of epoxy resin implies that epoxy is the material which predominately contributes to the thermal radiative properties of the composite material. The other component, the fiber material, plays a minor role. Indeed, by comparing the shapes of the normal spectral reflectance curves (Figure 24-4 in this subsection and Figures 23-4 and 25-4 in subsections 4.23 and 4.25 respectively) we can see the spectral band patterns of the three epoxy composite materials (boron fiber epoxy composite, glass fiber epoxy composite and graphite fiber epoxy composite) are similar.

Reflectance of epoxy is generally fairly low, about 10%, for wavelengths longer than 2.5 μm . Also, it does not change appreciably as the material is heated up and goes

decomposition phase and into the char region [A00004]. In other words, the radiative properties of epoxy are independent of temperature.

For epoxy composite materials, the following two relations are commonly used [A00004] as good approximations:

$$\alpha(0, \lambda) = 1 - \rho(0, 2\pi, \lambda);$$

$$\epsilon(0, \lambda) = \alpha(0, \lambda),$$

because of opaqueness of the materials.

According to the facts discussed above, we are in a position to estimate the following six subproperties for glass fiber epoxy composite based on the single available set of reflectance data:

- Normal spectral emittance (wavelength dependence)
- Normal spectral emittance (temperature dependence)
- Normal spectral reflectance (wavelength dependence)
- Normal spectral reflectance (temperature dependence)
- Normal spectral absorptance (wavelength dependence)
- Normal spectral absorptance (temperature dependence)

a. Normal Spectral Emittance (Wavelength Dependence)

Provisional values of the normal spectral emittance of slightly grit-blasted glass fiber epoxy composite are obtained from the analyzed result of reflectance by using the relation $\alpha(0, \lambda) = 1 - \rho(0, 2\pi, \lambda)$ and Kirchhoff's law. Such conversion is frequently used for the materials whose reflectance is known [A00004]. The provisional values, listed in Table 24-1 and plotted in Figure 24-1, are in general very close to unity. For rough uses, a value of 0.95 can be safely used because the uncertainty of the provisional values is $\pm 20\%$.

TABLE 24-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)

WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ

| λ | ϵ |
|--------------|------------|
| LIGHTLY | |
| GRIT-BLASTED | |
| T = 293 | |
| 2.0 | 0.926 |
| 3.0 | 0.943 |
| 3.5 | 0.954 |
| 3.8 | 0.943 |
| 4.0 | 0.939 |
| 4.5 | 0.937 |
| 5.0 | 0.940 |
| 5.5 | 0.954 |
| 6.0 | 0.971 |
| 6.5 | 0.976 |
| 7.0 | 0.976 |
| 7.5 | 0.976 |
| 8.0 | 0.976 |
| 8.5 | 0.976 |
| 9.0 | 0.975 |
| 9.5 | 0.964 |
| 10.0 | 0.957 |
| 10.5 | 0.964 |
| 10.6 | 0.966 |
| 11.0 | 0.970 |
| 11.5 | 0.974 |
| 12.0 | 0.977 |
| 12.5 | 0.980 |
| 13.0 | 0.980 |
| 13.5 | 0.975 |
| 14.0 | 0.970 |
| 14.5 | 0.966 |
| 15.0 | 0.963 |

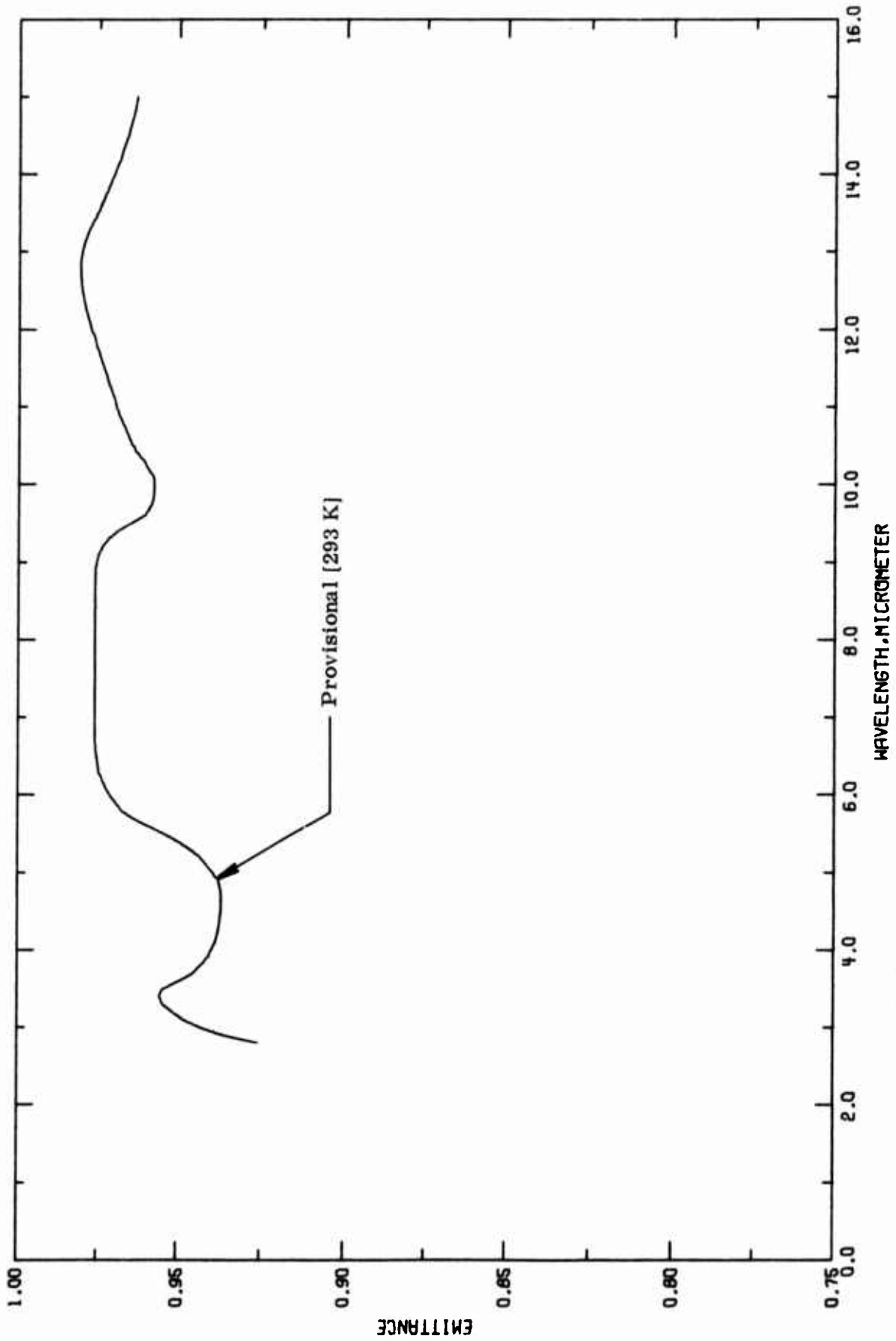


FIGURE 24-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

b. Normal Spectral Emittance (Temperature Dependence)

The normal spectral emittance as a function of temperature is given in Table 24-2 and plotted in Figure 24-2. The generated values are considered as provisional with 20% uncertainty. Here, we present the property values as a constant for a given wavelength because it has been observed in epoxy composites that the radiative properties do not change appreciably with temperature [A00002]. With 20% uncertainty, the provisional values can be safely used for most of the true surfaces.

TABLE 2-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|---------------------------------------|------------|-------|------------|-------|------------|-------|------------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.8$ | | | | | | | |
| 250.0 | 0.926 | 250.0 | 0.943 | 250.0 | 0.940 | 250.0 | 0.966 |
| 300.0 | 0.926 | 300.0 | 0.943 | 300.0 | 0.940 | 300.0 | 0.966 |
| 350.0 | 0.926 | 350.0 | 0.943 | 350.0 | 0.940 | 350.0 | 0.966 |
| 400.0 | 0.926 | 400.0 | 0.943 | 400.0 | 0.940 | 400.0 | 0.966 |
| 450.0 | 0.926 | 450.0 | 0.943 | 450.0 | 0.940 | 450.0 | 0.966 |
| 500.0 | 0.926 | 500.0 | 0.943 | 500.0 | 0.940 | 500.0 | 0.966 |
| LIGHTLY GRIT-BLASTED $\lambda = 3.8$ | | | | | | | |
| 250.0 | 0.926 | 250.0 | 0.943 | 250.0 | 0.940 | 250.0 | 0.966 |
| 300.0 | 0.926 | 300.0 | 0.943 | 300.0 | 0.940 | 300.0 | 0.966 |
| 350.0 | 0.926 | 350.0 | 0.943 | 350.0 | 0.940 | 350.0 | 0.966 |
| 400.0 | 0.926 | 400.0 | 0.943 | 400.0 | 0.940 | 400.0 | 0.966 |
| 450.0 | 0.926 | 450.0 | 0.943 | 450.0 | 0.940 | 450.0 | 0.966 |
| 500.0 | 0.926 | 500.0 | 0.943 | 500.0 | 0.940 | 500.0 | 0.966 |
| LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | | | | | | | |
| 250.0 | 0.926 | 250.0 | 0.943 | 250.0 | 0.940 | 250.0 | 0.966 |
| 300.0 | 0.926 | 300.0 | 0.943 | 300.0 | 0.940 | 300.0 | 0.966 |
| 350.0 | 0.926 | 350.0 | 0.943 | 350.0 | 0.940 | 350.0 | 0.966 |
| 400.0 | 0.926 | 400.0 | 0.943 | 400.0 | 0.940 | 400.0 | 0.966 |
| 450.0 | 0.926 | 450.0 | 0.943 | 450.0 | 0.940 | 450.0 | 0.966 |
| 500.0 | 0.926 | 500.0 | 0.943 | 500.0 | 0.940 | 500.0 | 0.966 |
| LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | | | | | | | |
| 250.0 | 0.926 | 250.0 | 0.943 | 250.0 | 0.940 | 250.0 | 0.966 |
| 300.0 | 0.926 | 300.0 | 0.943 | 300.0 | 0.940 | 300.0 | 0.966 |
| 350.0 | 0.926 | 350.0 | 0.943 | 350.0 | 0.940 | 350.0 | 0.966 |
| 400.0 | 0.926 | 400.0 | 0.943 | 400.0 | 0.940 | 400.0 | 0.966 |
| 450.0 | 0.926 | 450.0 | 0.943 | 450.0 | 0.940 | 450.0 | 0.966 |
| 500.0 | 0.926 | 500.0 | 0.943 | 500.0 | 0.940 | 500.0 | 0.966 |

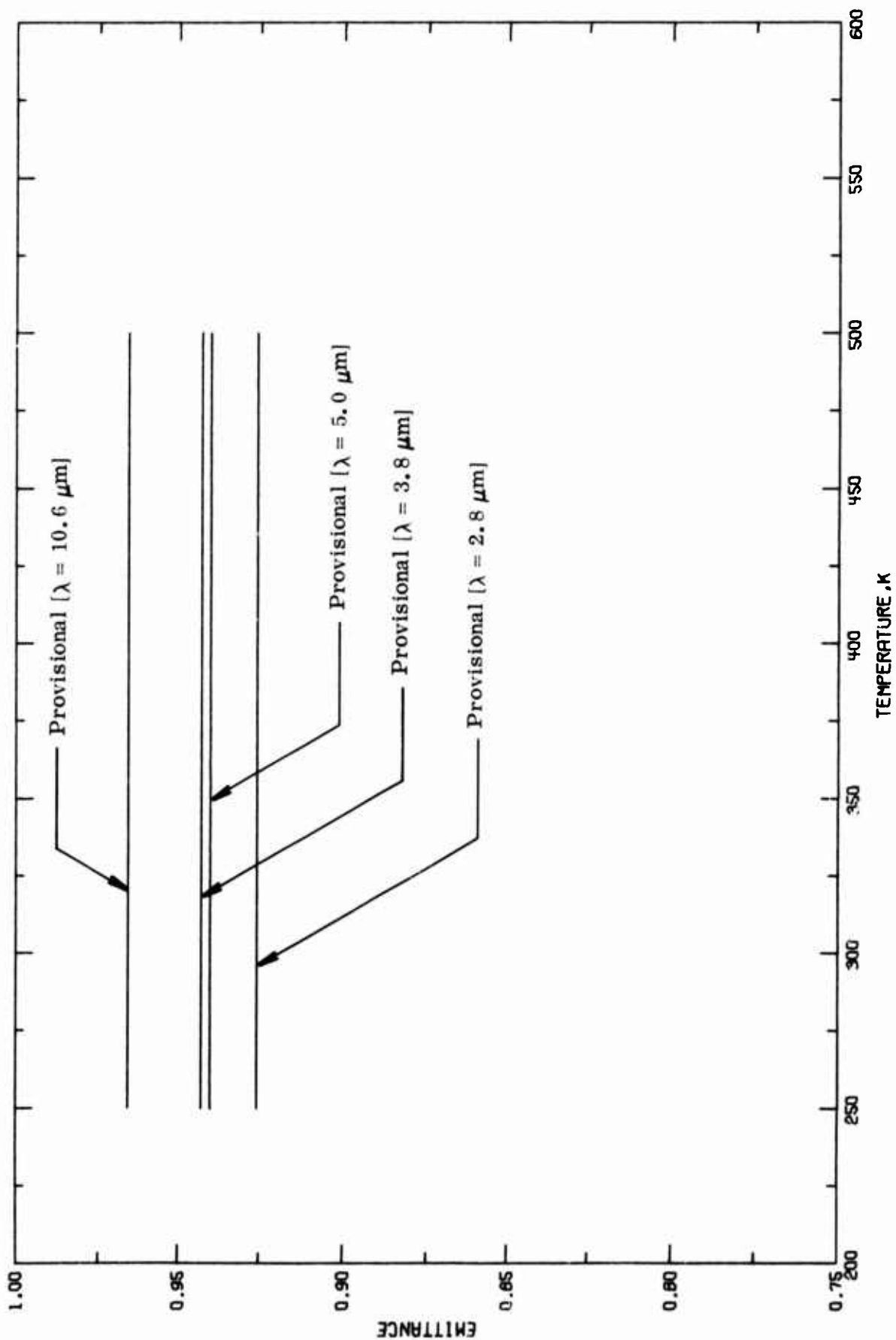


FIGURE 24-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

As given in Table 24-3 and plotted in Figure 24-3, the provisional values of glass fiber epoxy composite are obtained by reading off from a curve smoothed out from the only available set of data shown in Figure 24-4. It shows a quite complex spectral distribution of energy reflected from the composite material. Because of scantiness of the available data and spectral complexity, no attempt was made to carry out analytical calculations but the smoothing technique. An estimated uncertainty of 25% is given to the provisional values which are believed to be reasonable for most of the real surfaces.

TABLE 24-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|--------------|--------|
| LIGHTLY | |
| GRIT-BLASTED | |
| T = 293 | |
| 2.0 | 0.074 |
| 3.0 | 0.057 |
| 3.5 | 0.045 |
| 3.8 | 0.057 |
| 4.0 | 0.061 |
| 4.5 | 0.063 |
| 5.0 | 0.060 |
| 5.5 | 0.046 |
| 6.0 | 0.029 |
| 6.5 | 0.024 |
| 7.0 | 0.024 |
| 7.5 | 0.024 |
| 8.0 | 0.024 |
| 8.5 | 0.024 |
| 9.0 | 0.025 |
| 9.5 | 0.036 |
| 10.0 | 0.043 |
| 10.5 | 0.036 |
| 10.6 | 0.034 |
| 11.0 | 0.030 |
| 11.5 | 0.026 |
| 12.0 | 0.023 |
| 12.5 | 0.020 |
| 13.0 | 0.020 |
| 13.5 | 0.025 |
| 14.0 | 0.030 |
| 14.5 | 0.034 |
| 15.0 | 0.037 |

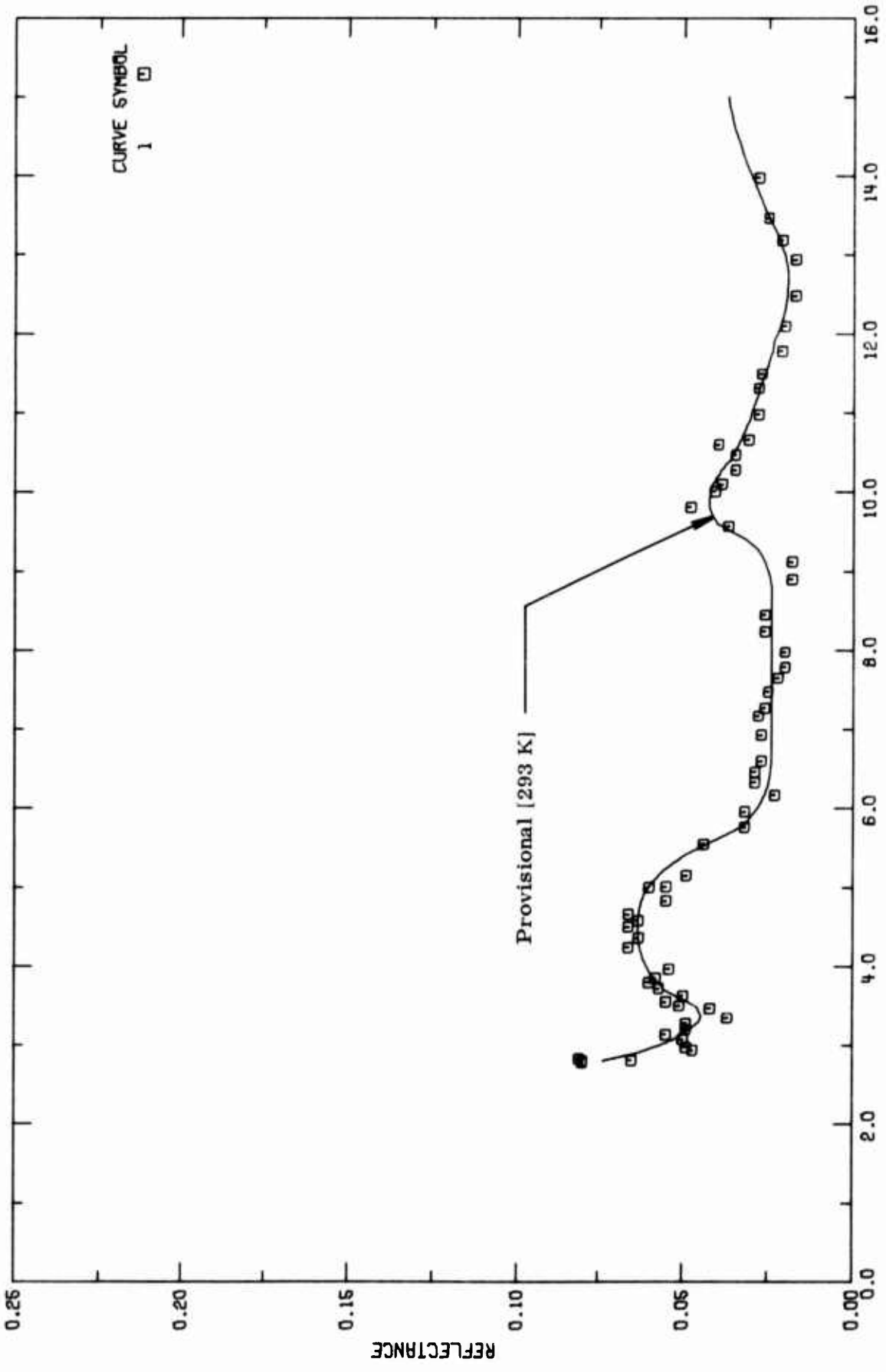


FIGURE 24-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

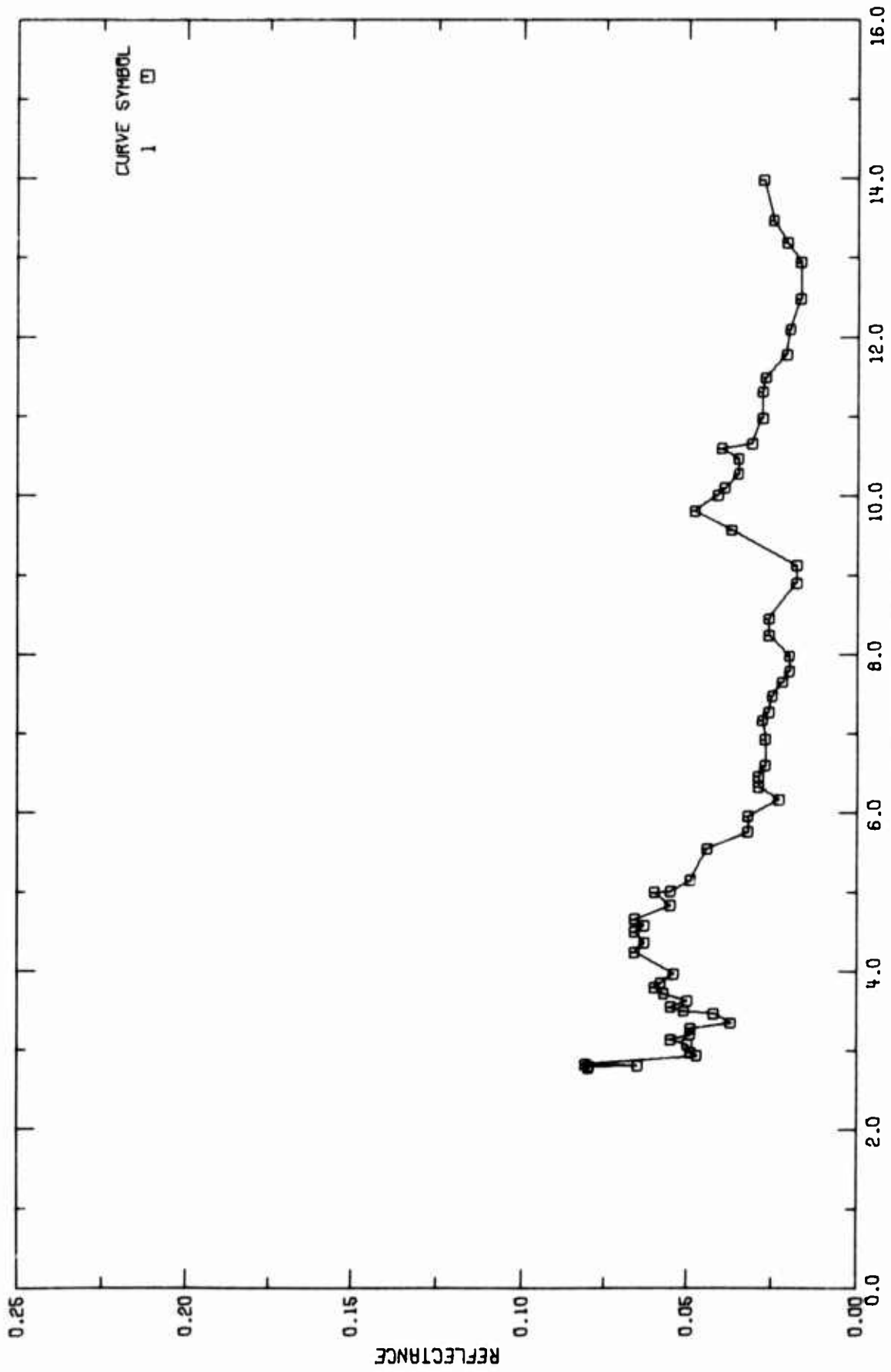


FIGURE 24-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

TABLE 24-4. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00001 | Grimm, T.C. | 1972 | 2.0-14.7 | 293 | | Bare surface specimen; 2.54 cm square; lightly grit-blasted; prepared by the Organic Chemistry Laboratory in the company where the author worked; measurements made with a Dunn Associates ellipsoidal mirror reflectometer; data extracted from a figure; relative reflectance reported; multiplied by 0.95 to convert to absolute values (gold reference mirror used); $\theta = 15^\circ$, $\omega' = 2\pi$. |

TABLE 24-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| CURVE 1 | λ | ρ | CURVE 1 (CONT.) | λ | ρ |
|----------|-----------|--------|-----------------|-----------|--------|
| T = 293. | | | | | |
| 2.50 | 0.262 | | 6.93 | 0.027 | |
| 2.66 | 0.196 | | 7.17 | 0.028 | |
| 2.70 | 0.138 | | 7.27 | 0.026 | |
| 2.74 | 0.103 | | 7.48 | 0.025 | |
| 2.78 | 0.080 | | 7.65 | 0.022 | |
| 2.80 | 0.080 | | 7.79 | 0.020 | |
| 2.81 | 0.065 | | 7.98 | 0.020 | |
| 2.83 | 0.081 | | 8.24 | 0.026 | |
| 2.94 | 0.047 | | 8.45 | 0.026 | |
| 2.98 | 0.049 | | 8.90 | 0.018 | |
| 3.08 | 0.050 | | 9.12 | 0.018 | |
| 3.14 | 0.055 | | 9.57 | 0.037 | |
| 3.20 | 0.049 | | 9.81 | 0.048 | |
| 3.28 | 0.049 | | 10.01 | 0.041 | |
| 3.35 | 0.037 | | 10.10 | 0.039 | |
| 3.47 | 0.042 | | 10.28 | 0.035 | |
| 3.50 | 0.051 | | 10.47 | 0.035 | |
| 3.55 | 0.055 | | 10.60 | 0.040 | |
| 3.63 | 0.050 | | 10.66 | 0.031 | |
| 3.72 | 0.057 | | 10.98 | 0.028 | |
| 3.80 | 0.060 | | 11.31 | 0.028 | |
| 3.85 | 0.054 | | 11.49 | 0.027 | |
| 3.97 | 0.054 | | 11.78 | 0.021 | |
| 4.24 | 0.066 | | 12.10 | 0.020 | |
| 4.36 | 0.063 | | 12.48 | 0.017 | |
| 4.50 | 0.066 | | 12.94 | 0.017 | |
| 4.58 | 0.063 | | 13.19 | 0.021 | |
| 4.66 | 0.066 | | 13.47 | 0.025 | |
| 4.83 | 0.055 | | 13.98 | 0.028 | |
| 5.00 | 0.060 | | 14.13 | 0.028 | |
| 5.01 | 0.055 | | 14.23 | 0.032 | |
| 5.15 | 0.049 | | 14.64 | 0.033 | |
| 5.55 | 0.044 | | | | |
| 5.76 | 0.032 | | | | |
| 5.96 | 0.032 | | | | |
| 6.17 | 0.023 | | | | |
| 6.33 | 0.029 | | | | |
| 6.46 | 0.029 | | | | |
| 6.60 | 0.027 | | | | |

d. Normal Spectral Reflectance (Temperature Dependence)

In Table 24-6, the provisional values of the normal spectral reflectance are given with an estimated uncertainty of $\pm 25\%$. The variation of the property as a function of temperature is demonstrated in Figure 24-5. For a given wavelength, the normal spectral reflectance remains as a constant from room temperature up to the char region of epoxy. The independency of the reflectance of epoxy composite with temperature has been observed experimentally [A00002]. The reported provisional values are believed to be reasonable in most of the real situation.

TABLE 24-6. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| T | ρ | T | ρ | T | ρ | T | ρ |
|--|--------|--|--------|--|--------|---|--------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.8$ | | LIGHTLY GRIT-BLASTED $\lambda = 3.6$ | | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | |
| 250.0 | 0.074 | 250.0 | 0.057 | 250.0 | 0.060 | 250.0 | 0.034 |
| 300.0 | 0.074 | 300.0 | 0.057 | 300.0 | 0.060 | 300.0 | 0.034 |
| 350.0 | 0.074 | 350.0 | 0.057 | 350.0 | 0.060 | 350.0 | 0.034 |
| 400.0 | 0.074 | 400.0 | 0.057 | 400.0 | 0.060 | 400.0 | 0.034 |
| 450.0 | 0.074 | 450.0 | 0.057 | 450.0 | 0.060 | 450.0 | 0.034 |
| 500.0 | 0.074 | 500.0 | 0.057 | 500.0 | 0.060 | 500.0 | 0.034 |

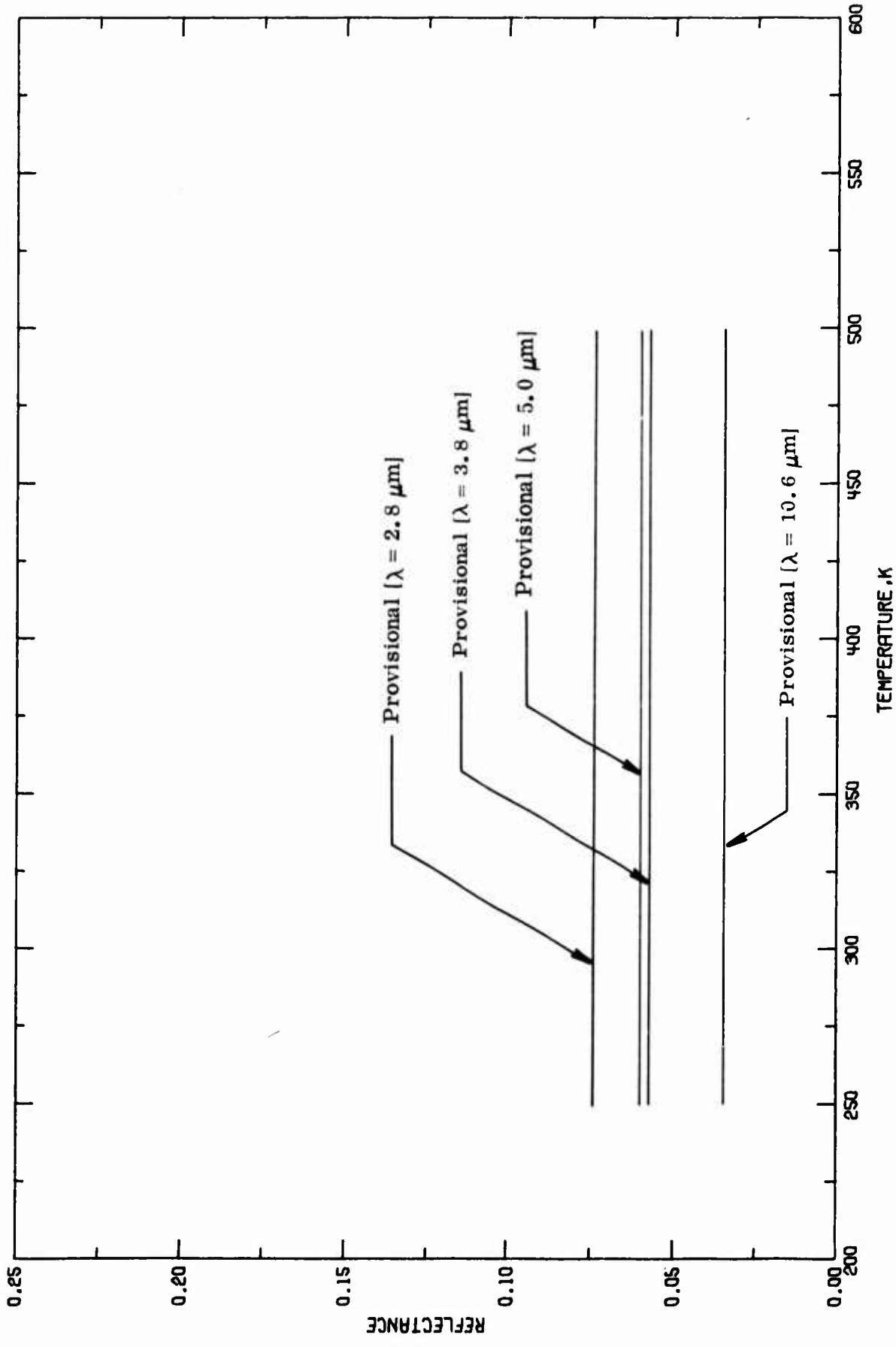


FIGURE 24-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

The normal spectral absorptance is obtained according to the Kirchhoff's law, i.e., numerically the absorptance is equal to the emittance. As a result, Table 24-7 and Figure 24-6 appear the same as Table 24-1 and Figure 24-1, as well as the estimated uncertainties ($\pm 20\%$).

TABLE 24-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 [WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α]

| λ | α |
|------------------------------------|----------|
| LIGHTLY GRIT-BLASTED T = 293 | |
| 2.8 | 0.326 |
| 3.0 | 0.943 |
| 3.5 | 0.354 |
| 3.8 | 0.343 |
| 4.0 | 0.339 |
| 4.5 | 0.937 |
| 5.0 | 0.340 |
| 5.5 | 0.354 |
| 6.0 | 0.371 |
| 6.5 | 0.976 |
| 7.0 | 0.976 |
| 7.5 | 0.976 |
| 8.0 | 0.976 |
| 8.5 | 0.976 |
| 9.0 | 0.975 |
| 9.5 | 0.364 |
| 10.0 | 0.957 |
| 10.5 | 0.964 |
| 10.6 | 0.966 |
| 11.0 | 0.970 |
| 11.5 | 0.374 |
| 12.0 | 0.977 |
| 12.5 | 0.980 |
| 13.0 | 0.380 |
| 13.5 | 0.975 |
| 14.0 | 0.970 |
| 14.5 | 0.966 |
| 15.0 | 0.963 |

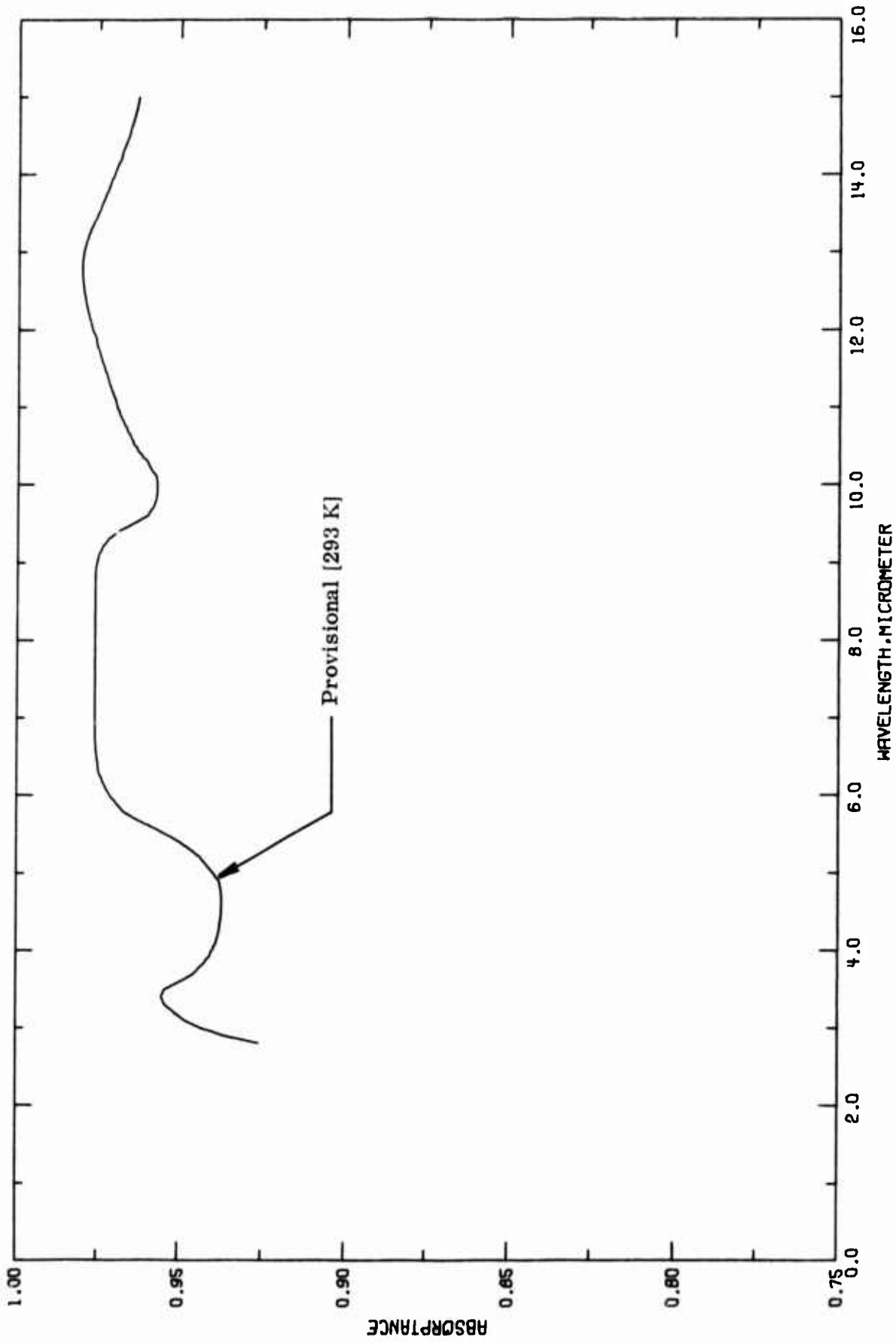


FIGURE 24-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

f. Normal Spectral Absorptance (Temperature Dependence)

The normal spectral absorptance as a function of temperature is given in Table 24-8 and plotted in Figure 24-7. The generated values are considered as provisional with 20% uncertainty. Here, we present the property values as constant for a given wavelength because it has been observed in epoxy composites that the radiative properties do not change appreciably with temperature [A00002]. With 20% uncertainty, the provisional values can be safely used for most of the true surfaces.

TABLE 24-1. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ - μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α | T | α | T | α | T | α |
|--|----------|--|----------|--|----------|---|----------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 3.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | |
| 250.0 | 0.926 | 250.0 | 0.943 | 250.0 | 0.940 | 250.0 | 0.966 |
| 300.0 | 0.926 | 300.0 | 0.943 | 300.0 | 0.940 | 300.0 | 0.966 |
| 350.0 | 0.926 | 350.0 | 0.943 | 350.0 | 0.940 | 350.0 | 0.966 |
| 400.0 | 0.926 | 400.0 | 0.943 | 400.0 | 0.940 | 400.0 | 0.966 |
| 450.0 | 0.926 | 450.0 | 0.943 | 450.0 | 0.940 | 450.0 | 0.966 |
| 500.0 | 0.926 | 500.0 | 0.943 | 500.0 | 0.940 | 500.0 | 0.966 |

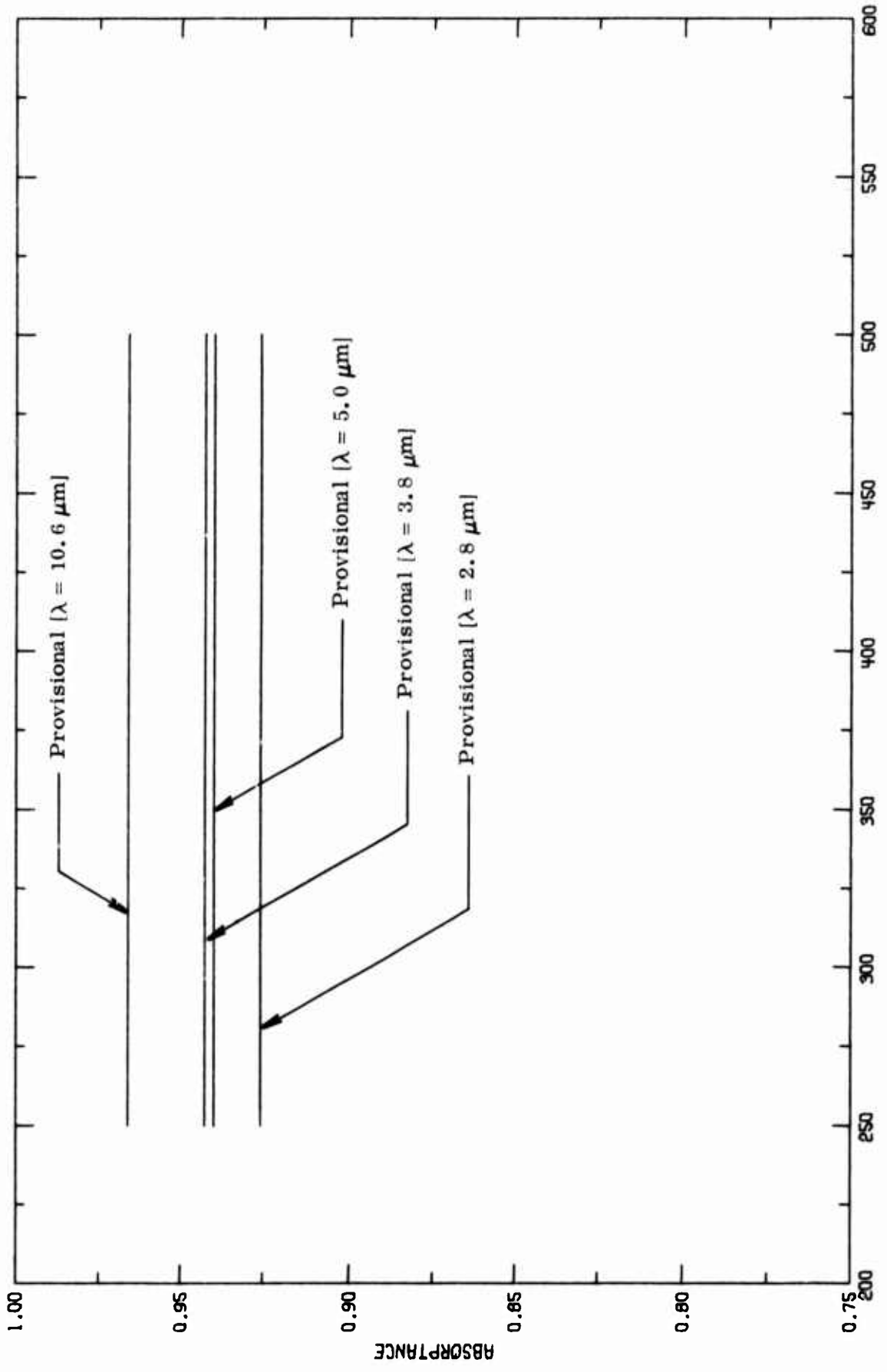


FIGURE 24-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GLASS FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

4.25. Graphite Fiber Epoxy Composite

Composite materials have received great interest in the last decade because they provide unusual combinations of properties which cannot be obtained with any single, homogeneous substance. In aircraft and missile design, they have provided structural materials of very high strength and elastic modulus which also have low densities.

The graphite fibers used in composites are made by the carbonization of organic filaments. The filaments most often used today are made from polyacrylonitrile (PAN) although rayon and acrylic fibers have been used to a limited extent. The mechanical properties of graphite fiber depend on the temperatures used in the carbonization process. Temperatures of 2800–3300 K result in fibers with high elastic modulus but relatively low tensile strength. Temperatures of 1800–2300 K yield fibers of the greatest tensile strength but only moderate modulus of elasticity. The density of the fibers varies from 1.74–1.94 g cm⁻³ depending on the carbonization temperatures used. The filaments are normally produced in untwisted, loose bundles, or tows, consisting of ten thousand fibers.

Modified epoxy resins developed specifically for use in composites with graphite fiber are available commercially. These are thermosetting resins used for low pressure laminating which normally cannot be used in continuous service above about 450 K although intermittent service at temperature up to 490 K is possible. Many of the various epoxy resins used as matrix constituents of composites are proprietary formulations whose exact chemical compositions are not available.

For aerospace design, graphite fiber-epoxy composites are generally supplied by the manufacturer as prepregs. These are tapes or broadgoods consisting of the graphite fibers impregnated with the epoxy resin matrix which have been only partially cured and consequently have a limited shelf life and require special storage facilities. The prepregs are used in the fabrication of laminates whose layer orientations are tailored to match individual design requirements. Consequently, large numbers of individually different crossplied laminates are likely to be encountered, each of which has distinctive properties and characteristics, and hence must be distinctly identified whenever it is to be associated with specific quantitative data.

The graphite fiber epoxy is fabricated primarily for aircraft constructions because of its advantages. Much of its mechanical and thermal properties are studied. As a result, sizable amount of data are made available at users disposal.

With regard to the thermal radiative properties of the composite, it is unfortunate to find that there is only one set of experimental data on the normal spectral reflectance

uncovered by our search. This leaves us no choice but to use it as the basis in the estimation of the most probable values of the radiative properties for graphite fiber epoxy composite.

The fact that the composite material is made by bonding graphite fibers in a matrix of epoxy resin implies that epoxy is the material which predominately contributes to the thermal radiative properties of the composite material. The other component, the graphite fiber, plays a minor role. Indeed, by comparing the shapes of the normal spectral reflectance curves (Figure 25-4 in this subsection and Figures 23-4 and 24-4 in subsections 4.23 and 4.24 respectively) we can see the spectral band patterns of the three epoxy composite materials (boron fiber epoxy composite, glass fiber epoxy composite and graphite fiber epoxy composite) are similar.

Reflectance of epoxy is generally fairly low, about 10%, for wavelengths longer than 2.5 μm . Also, it does not change appreciably as the material is heated up and goes decomposition phase and into the char region [A00004]. In other words, the radiative properties of epoxy are independent of temperature.

For epoxy composite materials, the following two relations are commonly used as good approximations:

$$\alpha(0, \lambda) = 1 - \rho(0, 2\pi, \lambda);$$

$$\epsilon(0, \lambda) = \alpha(0, \lambda),$$

because of opaqueness of the materials.

According to the facts discussed above, we are in a position to make reasonable estimation of the following six subproperties for graphite fiber epoxy composite based on the single available set of reflectance data:

- Normal spectral emittance (wavelength dependence)
- Normal spectral emittance (temperature dependence)
- Normal spectral reflectance (wavelength dependence)
- Normal spectral reflectance (temperature dependence)
- Normal spectral absorptance (wavelength dependence)
- Normal spectral absorptance (temperature dependence)

a. Normal Spectral Emittance (Wavelength Dependence)

Provisional values of the thermal spectral emittance of slightly grit-blasted boron fiber epoxy composite are obtained from the analyzed result of reflectance by using

the relation $\alpha(0, \lambda) = 1 - \rho(0, 2\pi, \lambda)$ and Kirchhoff's law. Such conversion is frequently used for the materials whose reflectance is known [A00004]. The provisional values, listed in Table 25-1 and plotted in Figure 25-1, are in general very close to unity. For rough uses, a value of 0.95 can be safely used because the uncertainty of the provisional values is $\pm 20\%$.

TABLE 20-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| λ | ϵ |
|------------------------------------|------------|
| LIGHTLY GRIT-BLASTED T = 293 | |
| 2.5 | 0.903 |
| 2.8 | 0.921 |
| 3.0 | 0.927 |
| 3.5 | 0.928 |
| 3.8 | 0.900 |
| 4.0 | 0.894 |
| 4.5 | 0.888 |
| 5.0 | 0.888 |
| 5.5 | 0.893 |
| 6.0 | 0.914 |
| 6.5 | 0.938 |
| 7.0 | 0.945 |
| 7.5 | 0.947 |
| 8.0 | 0.947 |
| 8.5 | 0.946 |
| 9.0 | 0.944 |
| 9.5 | 0.939 |
| 10.0 | 0.931 |
| 10.5 | 0.925 |
| 10.6 | 0.925 |
| 11.0 | 0.925 |
| 11.5 | 0.930 |
| 12.0 | 0.937 |
| 12.5 | 0.935 |
| 13.0 | 0.928 |
| 13.5 | 0.914 |
| 14.0 | 0.904 |
| 14.5 | 0.898 |
| 15.0 | 0.894 |

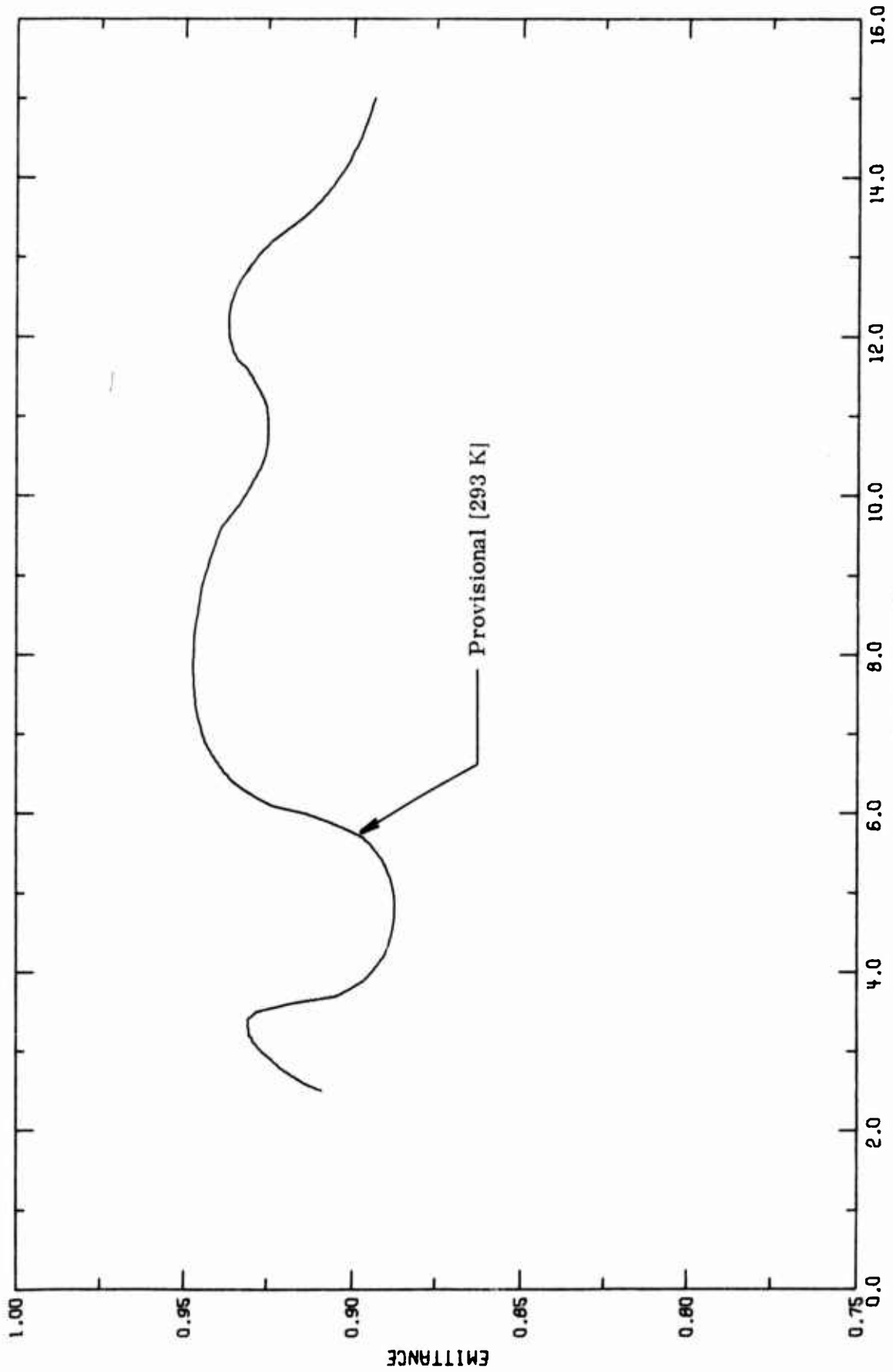


FIGURE 25-1. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

b. Normal Spectral Emittance (Temperature Dependence)

The normal spectral emittance as a function of temperature is given in Table 25-2 and plotted in Figure 25-2. The generated values are considered as provisional with 20% uncertainty. Here, we present the property values as a constant for a given wavelength because it has been observed in epoxy composites that the radiative properties do not change appreciably with temperature [A00002]. With 20% uncertainty, the provisional values can be safely used for most of the true surfaces.

TABLE 25-2. PROVISIONAL NORMAL SPECTRAL RADIANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)

(WAVELENGTH, λ , μm ; TEMPERATURE, T, K; EMITTANCE, ϵ)

| T | ϵ | T | ϵ | T | ϵ | T | ϵ |
|---|------------|---|------------|---|------------|--|------------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.8$ | | LIGHTLY GRIT-BLASTED $\lambda = 3.8$ | | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | |
| 250.0 | 0.921 | 250.0 | 0.900 | 250.0 | 0.888 | 250.0 | 0.925 |
| 300.0 | 0.921 | 300.0 | 0.900 | 300.0 | 0.888 | 300.0 | 0.925 |
| 350.0 | 0.921 | 350.0 | 0.900 | 350.0 | 0.888 | 350.0 | 0.925 |
| 400.0 | 0.921 | 400.0 | 0.900 | 400.0 | 0.888 | 400.0 | 0.925 |
| 450.0 | 0.921 | 450.0 | 0.900 | 450.0 | 0.888 | 450.0 | 0.925 |
| 500.0 | 0.921 | 500.0 | 0.900 | 500.0 | 0.888 | 500.0 | 0.925 |

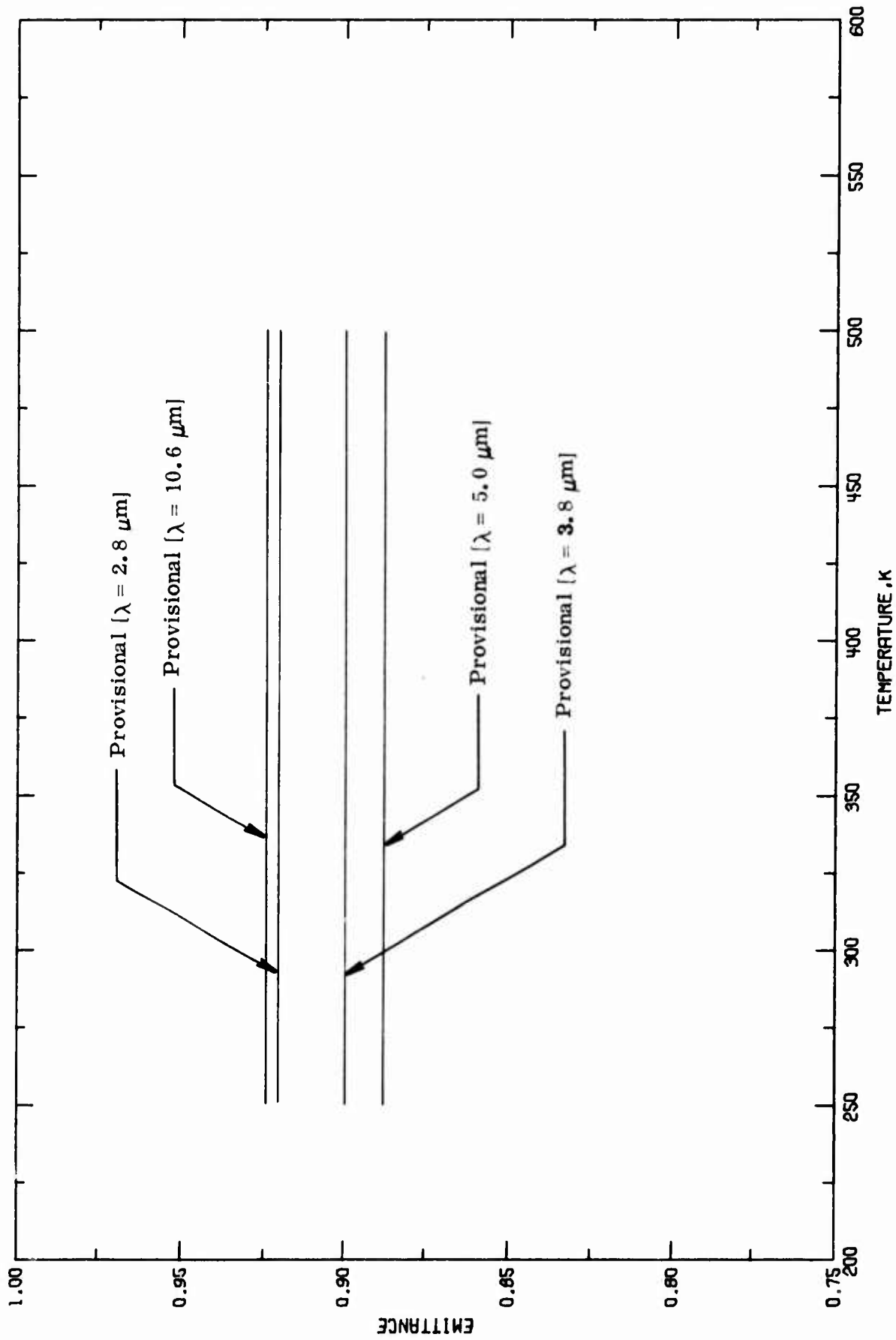


FIGURE 25-2. PROVISIONAL NORMAL SPECTRAL EMITTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

c. Normal Spectral Reflectance (Wavelength Dependence)

As given in Table 25-3 and plotted in Figure 25-3, the provisional values of graphite fiber epoxy composite are obtained by reading off from a curve smoothed out from the only available set of data shown in Figure 25-4. It shows a quite complex spectral distribution of energy reflected from the composite material. Because of scantiness of the available data and spectral complexity, no attempt was made to carry out analytical calculations but the smoothing technique. An estimated uncertainty of 25% is given to the provisional values which are believed to be reasonable for most of the real surfaces.

TABLE 25-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | ρ |
|-----------------------|--------|
| LIGHTLY GRIT-BLASTED. | |
| T = 293 | |
| 2.5 | 0.091 |
| 2.8 | 0.079 |
| 3.0 | 0.073 |
| 3.5 | 0.072 |
| 3.8 | 0.100 |
| 4.0 | 0.106 |
| 4.5 | 0.112 |
| 5.0 | 0.112 |
| 5.5 | 0.107 |
| 6.0 | 0.086 |
| 6.5 | 0.062 |
| 7.0 | 0.055 |
| 7.5 | 0.053 |
| 8.0 | 0.053 |
| 8.5 | 0.054 |
| 9.0 | 0.056 |
| 9.5 | 0.061 |
| 10.0 | 0.069 |
| 10.5 | 0.074 |
| 10.6 | 0.075 |
| 11.0 | 0.075 |
| 11.5 | 0.070 |
| 12.0 | 0.063 |
| 12.5 | 0.065 |
| 13.0 | 0.072 |
| 13.5 | 0.086 |
| 14.0 | 0.096 |
| 14.5 | 0.102 |
| 15.0 | 0.106 |

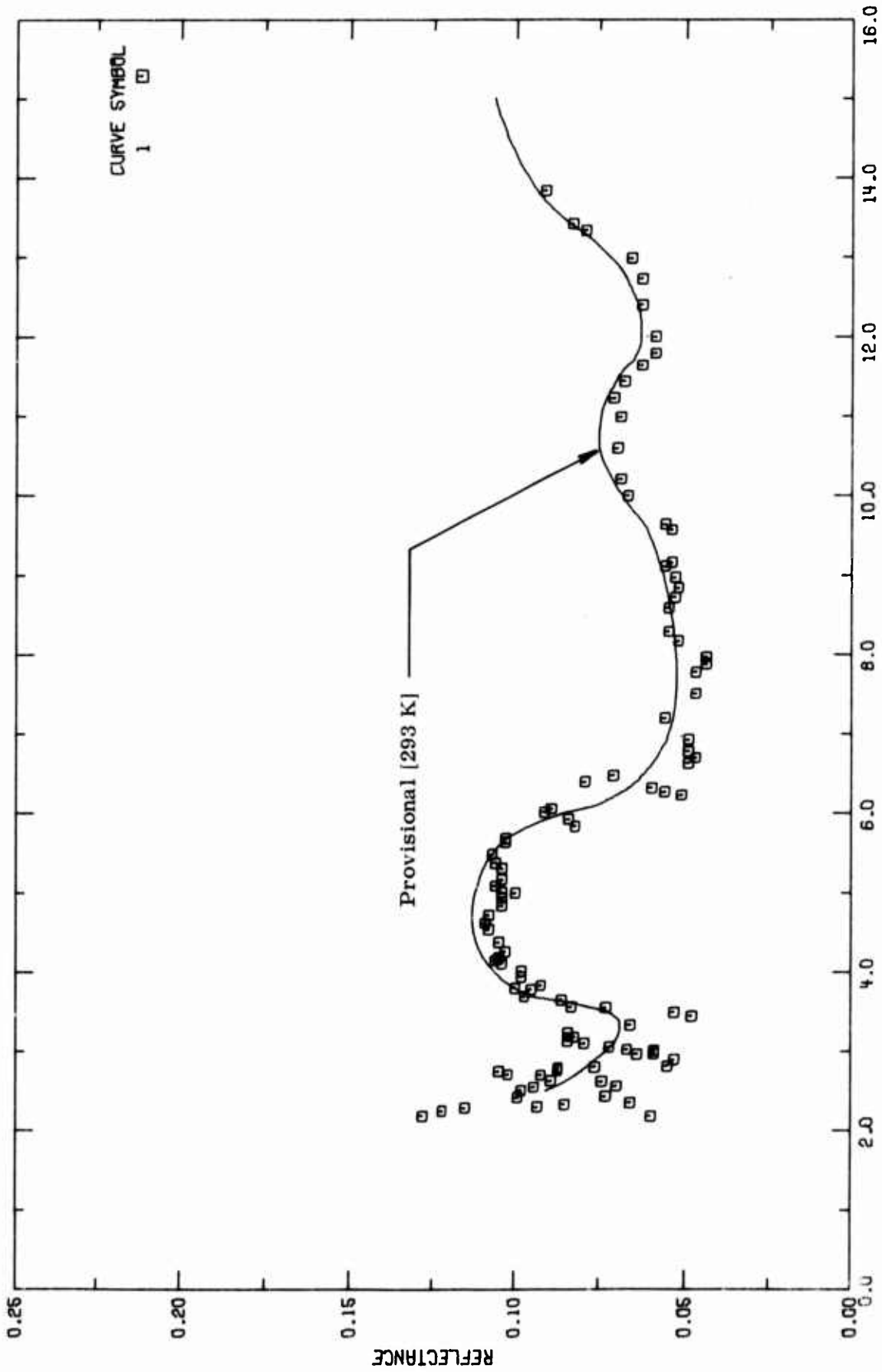


FIGURE 25-3. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

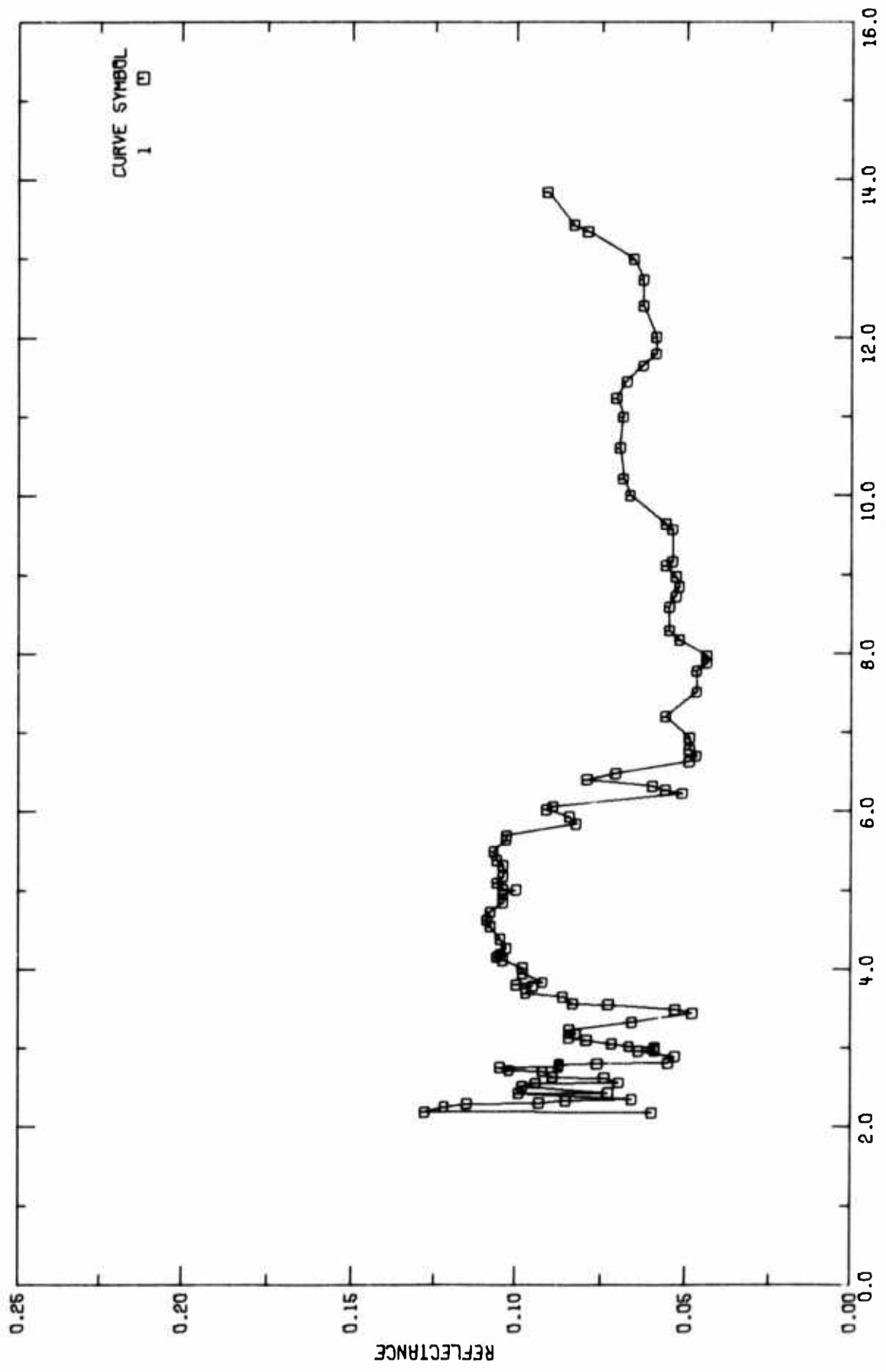


FIGURE 25-4. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

TABLE 25-4. MEASUREMENT INFORMATION ON THE NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE. (Wavelength Dependence)

| Cur. Ref. No. | Author(s) | Year | Wavelength Range, μm | Temperature Range, K | Name and Specimen Designation | Composition (weight percent), Specifications, and Remarks |
|---------------|-------------|------|---------------------------------|----------------------|-------------------------------|---|
| 1 A00001 | Grimm, T.C. | 1972 | 2.0-14.7 | 293 | | Bare surface specimen; 2.54 cm square; lightly grit-blasted; prepared by the Organic Chemistry Laboratory in the company where the author worked; measurements made with a Dunn Associates ellipsoidal mirror reflectometer; data extracted from a figure; relative reflectance reported; multiplied by 0.95 to convert to absolute values (gold reference mirror used); $\theta = 15^\circ$, $\omega' = 2\pi$. |

TABLE 25-5. EXPERIMENTAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, ρ)

| λ | CURVE 1 | | CURVE 1 (CONT.) | | CURVE 1 (CONT.) | |
|-----------|-----------|--------|-----------------|--------|-----------------|--------|
| | λ | ρ | λ | ρ | λ | ρ |
| 2.10 | 0.064 | 3.80 | 0.100 | 7.97 | 0.044 | |
| 2.19 | 0.124 | 3.93 | 0.092 | 8.17 | 0.052 | |
| 2.25 | 0.122 | 3.94 | 0.098 | 8.29 | 0.055 | |
| 2.29 | 0.115 | 4.01 | 0.098 | 8.53 | 0.055 | |
| 2.30 | 0.093 | 4.11 | 0.104 | 8.72 | 0.053 | |
| 2.33 | 0.085 | 4.15 | 0.106 | 8.84 | 0.052 | |
| 2.35 | 0.065 | 4.18 | 0.105 | 8.97 | 0.053 | |
| 2.42 | 0.093 | 4.26 | 0.103 | 9.11 | 0.056 | |
| 2.43 | 0.073 | 4.38 | 0.105 | 9.16 | 0.054 | |
| 2.51 | 0.098 | 4.54 | 0.108 | 9.57 | 0.054 | |
| 2.55 | 0.094 | 4.62 | 0.109 | 9.64 | 0.056 | |
| 2.56 | 0.070 | 4.72 | 0.108 | 10.00 | 0.067 | |
| 2.62 | 0.074 | 4.84 | 0.104 | 10.21 | 0.069 | |
| 2.63 | 0.069 | 4.94 | 0.104 | 10.50 | 0.070 | |
| 2.70 | 0.092 | 5.00 | 0.100 | 10.99 | 0.069 | |
| 2.71 | 0.102 | 5.01 | 0.104 | 11.23 | 0.071 | |
| 2.75 | 0.105 | 5.09 | 0.106 | 11.44 | 0.068 | |
| 2.76 | 0.087 | 5.17 | 0.104 | 11.64 | 0.063 | |
| 2.79 | 0.087 | 5.31 | 0.104 | 11.79 | 0.059 | |
| 2.80 | 0.075 | 5.38 | 0.106 | 12.00 | 0.059 | |
| 2.81 | 0.055 | 5.49 | 0.107 | 12.40 | 0.063 | |
| 2.89 | 0.053 | 5.64 | 0.103 | 12.73 | 0.063 | |
| 2.96 | 0.064 | 5.69 | 0.103 | 12.99 | 0.066 | |
| 2.97 | 0.059 | 5.84 | 0.082 | 13.34 | 0.079 | |
| 3.01 | 0.059 | 5.93 | 0.084 | 13.42 | 0.083 | |
| 3.02 | 0.067 | 6.02 | 0.091 | 13.84 | 0.091 | |
| 3.05 | 0.072 | 6.06 | 0.089 | 14.18 | 0.095 | |
| 3.10 | 0.079 | 6.23 | 0.051 | 14.44 | 0.095 | |
| 3.13 | 0.084 | 6.27 | 0.056 | 14.69 | 0.100 | |
| 3.16 | 0.082 | 6.32 | 0.060 | | | |
| 3.23 | 0.084 | 6.40 | 0.079 | | | |
| 3.33 | 0.066 | 6.48 | 0.071 | | | |
| 3.44 | 0.048 | 6.63 | 0.049 | | | |
| 3.49 | 0.053 | 6.70 | 0.047 | | | |
| 3.55 | 0.073 | 6.78 | 0.049 | | | |
| 3.56 | 0.063 | 6.93 | 0.049 | | | |
| 3.65 | 0.086 | 7.20 | 0.056 | | | |
| 3.69 | 0.097 | 7.51 | 0.047 | | | |
| 3.78 | 0.095 | 7.78 | 0.047 | | | |
| | | 7.88 | 0.044 | | | |

d. Normal Spectral Reflectance (Temperature Dependence)

In Table 25-6, the provisional values of the normal spectral reflectance are given with an estimated uncertainty of $\pm 25\%$. The variation of the property as a function of temperature is demonstrated in Figure 25-5. For a given wavelength, the normal spectral reflectance remains as a constant from room temperature up to the char region of epoxy. The independency of the reflectance of epoxy composite with temperature has been observed experimentally [A00002]. The reported provisional values are believed to be reasonable in most of the real situation.

TABLE 25-6. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRIT-BLASTED WHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; REFLECTANCE, R)

| LIGHTLY GRIT-BLASTED $\lambda = 2.0$ | LIGHTLY GRIT-BLASTED $\lambda = 3.0$ | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ |
|--|--|--|---|
| 250.0 | 250.0 | 250.0 | 250.0 |
| 300.0 | 300.0 | 300.0 | 300.0 |
| 350.0 | 350.0 | 350.0 | 350.0 |
| 400.0 | 400.0 | 400.0 | 400.0 |
| 450.0 | 450.0 | 450.0 | 450.0 |
| 500.0 | 500.0 | 500.0 | 500.0 |
| 0.079 | 0.100 | 0.112 | 0.075 |
| 0.079 | 0.100 | 0.112 | 0.075 |
| 0.079 | 0.100 | 0.112 | 0.075 |
| 0.079 | 0.100 | 0.112 | 0.075 |
| 0.079 | 0.100 | 0.112 | 0.075 |

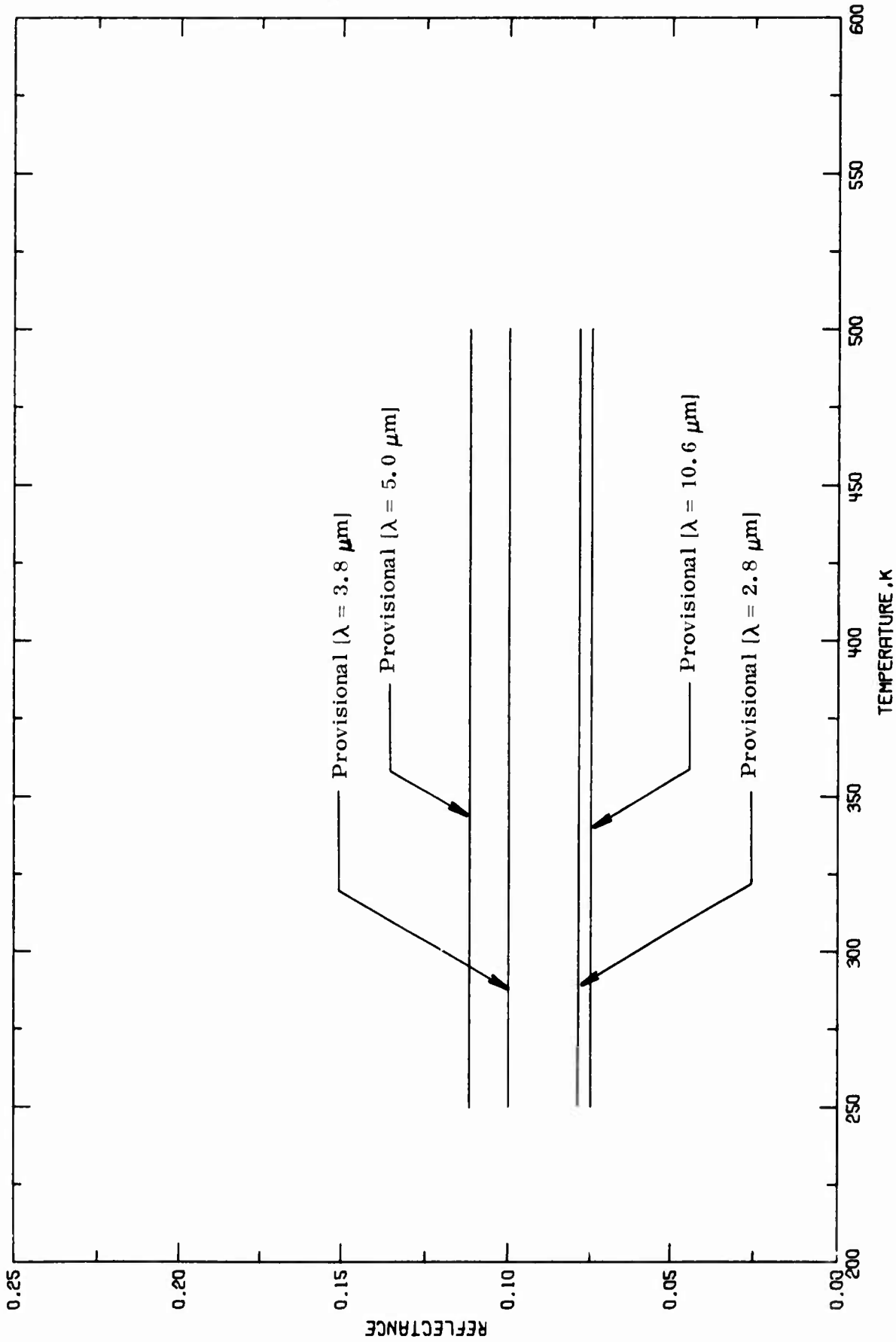


FIGURE 25-5. PROVISIONAL NORMAL SPECTRAL REFLECTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

e. Normal Spectral Absorptance (Wavelength Dependence)

The normal spectral absorptance is obtained according to the Kirchhoff's law, i. e., numerically the absorptance is equal to the emittance. As a result, Table 25-7 and Figure 25-6 appear the same as Table 25-1 and Figure 25-1, as well as the estimated uncertainties ($\pm 20\%$).

TABLE 25-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| λ | α |
|---------------------------------|----------|
| LIGHTLY GRIT-BLASTED T = 293 | |
| 2.5 | 0.903 |
| 2.8 | 0.921 |
| 3.0 | 0.927 |
| 3.5 | 0.928 |
| 3.8 | 0.900 |
| 4.0 | 0.894 |
| 4.5 | 0.889 |
| 5.0 | 0.888 |
| 5.5 | 0.893 |
| 6.0 | 0.914 |
| 6.5 | 0.938 |
| 7.0 | 0.945 |
| 7.5 | 0.947 |
| 8.0 | 0.947 |
| 8.5 | 0.946 |
| 9.0 | 0.944 |
| 9.5 | 0.939 |
| 10.0 | 0.931 |
| 10.5 | 0.926 |
| 10.6 | 0.925 |
| 11.0 | 0.925 |
| 11.5 | 0.930 |
| 12.0 | 0.937 |
| 12.5 | 0.935 |
| 13.0 | 0.925 |
| 13.5 | 0.914 |
| 14.0 | 0.904 |
| 14.5 | 0.899 |
| 15.0 | 0.894 |

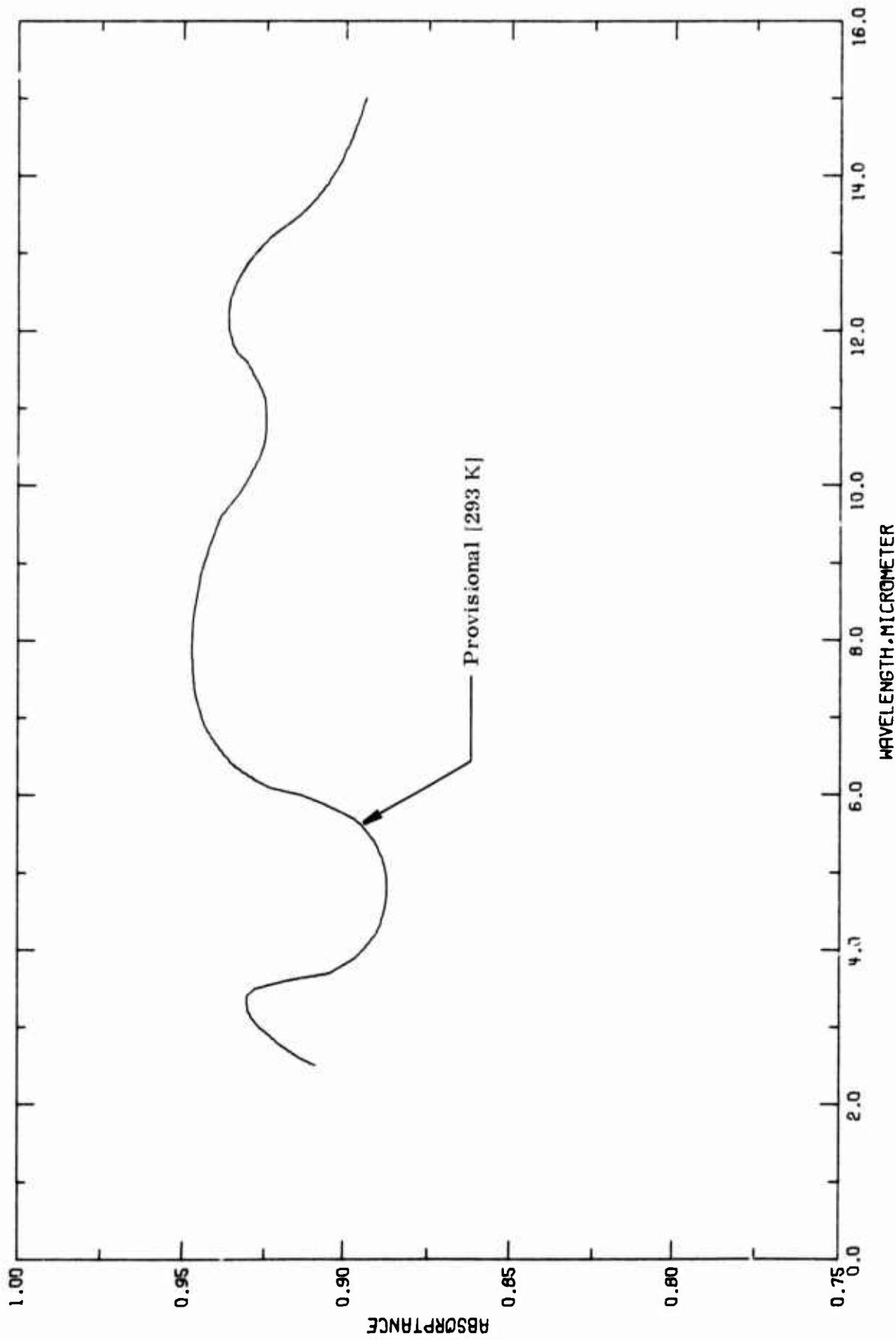


FIGURE 25-6. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (WAVELENGTH DEPENDENCE).

f. Normal Spectral Absorptance (Temperature Dependence)

The normal spectral absorptance as a function of temperature is given in Table 25-8 and plotted in Figure 25-7. The generated values are considered as provisional with 20% uncertainty. Here, we present the property values as constant for a given wavelength because it has been observed in epoxy composites that the radiative properties do not change appreciably with temperature [A00002]. With 20% uncertainty, the provisional values can be safely used for most of the true surfaces.

TABLE 25-8. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE)
 (WAVELENGTH, λ , μm ; TEMPERATURE, T, K; ABSORPTANCE, α)

| T | α | T | α | T | α | T | α |
|--|----------|--|----------|--|----------|---|----------|
| LIGHTLY GRIT-BLASTED $\lambda = 2.8$ | 0.921 | LIGHTLY GRIT-BLASTED $\lambda = 3.6$ | 0.900 | LIGHTLY GRIT-BLASTED $\lambda = 5.0$ | 0.888 | LIGHTLY GRIT-BLASTED $\lambda = 10.6$ | 0.925 |
| 250.0 | 0.921 | 250.0 | 0.900 | 250.0 | 0.888 | 250.0 | 0.925 |
| 300.0 | 0.921 | 300.0 | 0.900 | 300.0 | 0.888 | 300.0 | 0.925 |
| 350.0 | 0.921 | 350.0 | 0.900 | 350.0 | 0.888 | 350.0 | 0.925 |
| 400.0 | 0.921 | 400.0 | 0.900 | 400.0 | 0.888 | 400.0 | 0.925 |
| 450.0 | 0.921 | 450.0 | 0.900 | 450.0 | 0.888 | 450.0 | 0.925 |
| 500.0 | 0.921 | 500.0 | 0.900 | 500.0 | 0.888 | 500.0 | 0.925 |

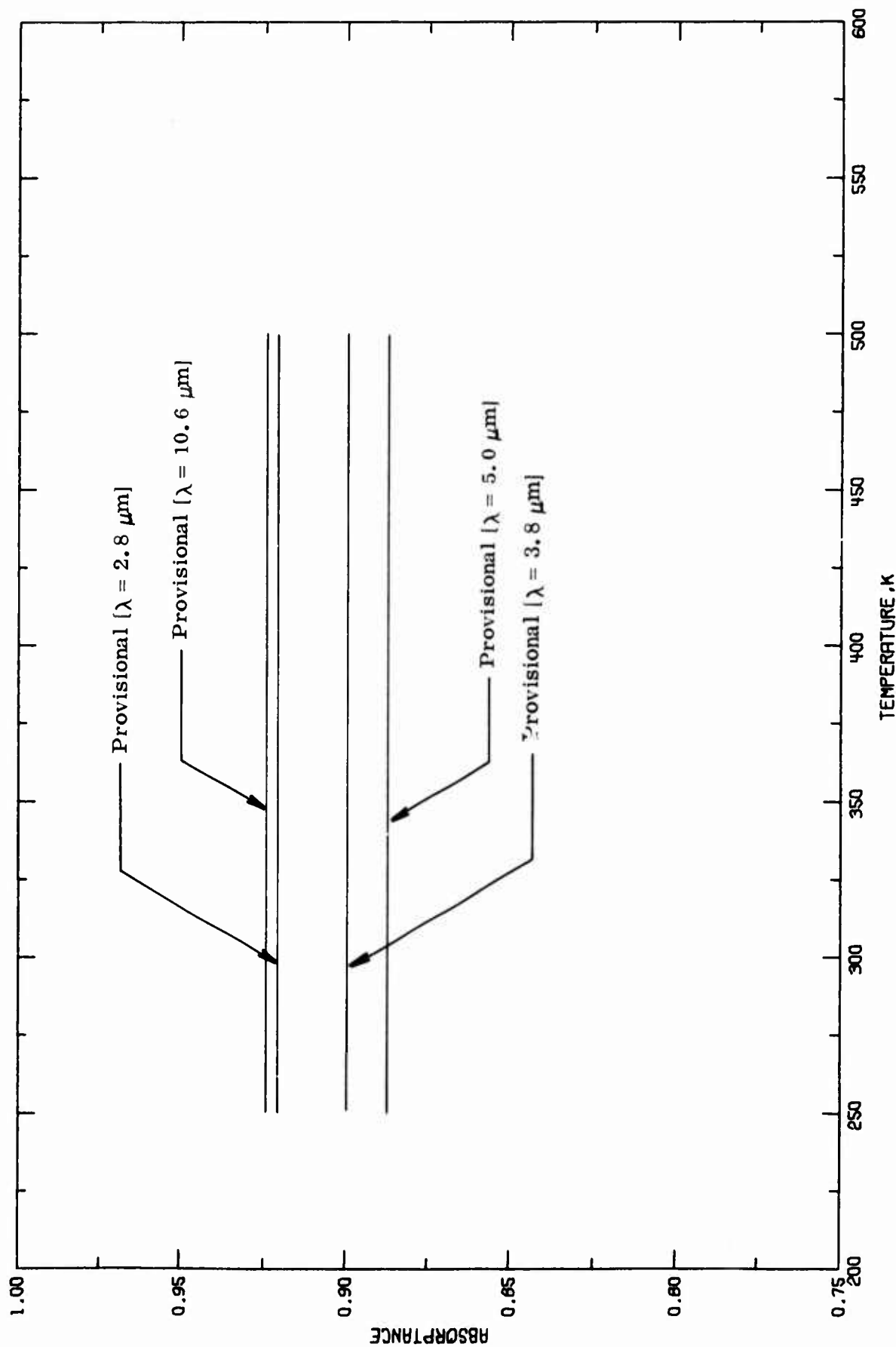


FIGURE 25-7. PROVISIONAL NORMAL SPECTRAL ABSORPTANCE OF GRAPHITE FIBER EPOXY COMPOSITE (TEMPERATURE DEPENDENCE).

4.26. Silicon Nitride with Chopped Graphite Fiber

No information on the thermal radiative properties of this composite material was uncovered from the search of literature. Consequently, no tabulation or recommendation of the thermal radiative properties of this material is possible at this time.

However, it is reasonable to assume that this material in its bulk form is opaque; that is, the transmittance is zero.

4.27. Silicon Nitride with Vitreous Silica

No information on the thermal radiative properties of this composite material was uncovered from the search of literature. Consequently, no tabulation or recommendation of the thermal radiative properties of this material is possible at this time.

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