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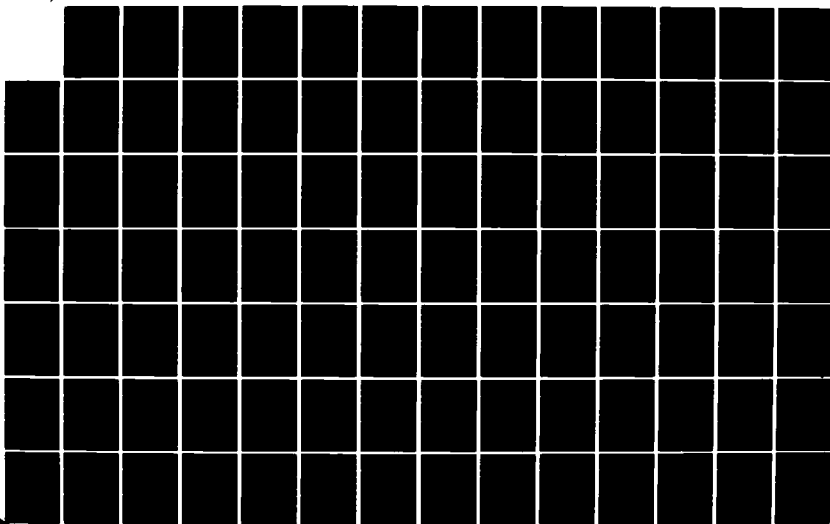
AN INVESTIGATION INTO THE CONTROL LIMITATIONS OF A BANK
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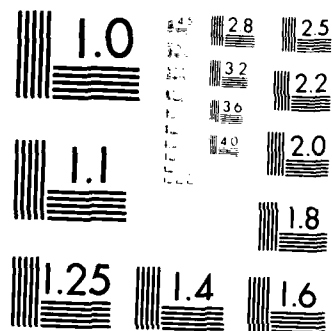
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THESIS

AN INVESTIGATION INTO THE CONTROL
LIMITATIONS OF A BANK TO TURN MISSILE
IN THE TERMINAL HOMING PHASE

by

Barton P. Anderson

September 1984

Thesis Advisor:

M. D. Hewett

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simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 35 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popup maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested however the missile was unable to produce the necessary sideforce needed to track a passive target and produced undesirable coupling in the flight controls. An attempt to use the altitude command channel to fly a ballistic profile was unsuccessful due to instabilities created in the control system. It is recommended that a popup maneuver be included in the terminal guidance of a BTT cruise missile and that further tests be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a BTT missile.

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An Investigation into the Control
Limitations of a Bank to Turn Missile
in the Terminal Homing Phase

by

Barton P. Anderson
Commander, United States Navy
P.S., Wheaton College, 1970

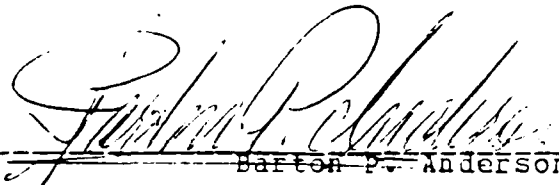
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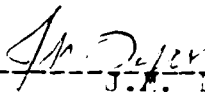
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ABSTRACT

The purpose of this thesis was to examine guidance and control deficiencies in a bank to turn (BT) cruise missile with limited roll authority in the terminal homing phase of its mission. A six degree of freedom simulation of a typical BT missile was translated into FORTRAN H from the Continuous System Modelling Program (CSMP) simulation language and run on the IBM System 370 computer. Tests were conducted with the revised simulation program to examine the effects of electronic countermeasures (ECM) blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. In addition to the standard attack profile involving a popout attack, several other attack profiles were tested including skid-to-turn (STT) control laws and a ballistic trajectory. Miss distances varied from 3.7 feet without ECM or glint to 85 feet with ECM operating. Susceptibility of the missile to ECM blinking varied with the blinking frequency. The largest miss distances occurred with ECM frequencies below 0.2 Hz and near 6.0 Hz. Analysis of the data showed that errors at the low frequencies were primarily caused by the bank command loop of the autopilot. Those at the higher frequency were due to the roll rate command loop. Variation of the geometry of the missile's flight profile had no significant impact upon missile accuracy except that, without a popup maneuver, the roll rate channel demonstrated a marked decrease in effectiveness. Variation of the autopilot gain in the roll rate control loop changed the frequency at which degradation occurred but actually increased its effects. Skid to turn control laws were tested

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I. INTRODUCTION

A. BACKGROUND

Bank-To-Turn (BTT) control is utilized extensively on missiles which must cruise for long ranges within the atmosphere. These missiles utilize a primary lifting surface (wing) and smaller controlling surfaces as on a conventional airplane. This method has two primary advantages. First, the wing provides lift to support the missile's weight at a relatively high efficiency thereby permitting longer ranges for a given size engine and fuel load. Second, the lift vector can be positioned by banking the missile to provide large lateral accelerations resulting in excellent turn performance. Certain BTT cruise missile configurations, however, use differential tail for roll control as opposed to ailerons and suffer from poor roll rate and acceleration performance. It is the investigation into the control limitations of a BTT cruise missile configured this way in the terminal homing phase which is the subject of this thesis.

B. STATEMENT OF THE PROBLEM

In order to provide compact storage of a BTT missile, the main wings are usually folded back and designed to snap into position as the missile emerges from its canister at launch. Because of this feature, it is generally not feasible to install roll control devices at the extremities of the wings. Roll control is normally provided by differential actuation of the tail fins of the missile. Because of their short moment arm and small area and because the main wing has a relatively large degree of roll damping, BTT missiles are limited in their ability to roll rapidly.

Because of the need to bank the missile in order to align its lift vector in the desired direction it has been suggested that the requirement for rapid roll maneuvering in the terminal phase of flight would limit the accuracy of the missile. In addition, natural fluctuations in the position of the radar target, known as glint, and artificial fluctuations due to the presence of electronic countermeasures (ECM) might further degrade the performance of a BT missile.

C. MISSION SCENARIO

1. Control Configuration

The missile simulated in this thesis is a hypothetical bank to turn cruise missile with limited roll control authority. Its design incorporates characteristics typical of many similar designs. The missile is equipped with a standard rudder for yaw control and stabilators for both roll and pitch control. Inner loop closures for stabilization and command are included in the simulation. Command loop closures consist of normal acceleration, bank angle, and lateral acceleration. The lateral acceleration command system can be used as a turn coordinator in the bank-to-turn mode (normal) mode or as a lateral load factor (NY) command system in a skid-to-turn mode. Outer loop closures are provided for altitude and flight path angle. The autopilot control loop design is presented in detail in [Ref. 1].

2. Target

The target is assumed to be a surface combatant ship located initially 24,000 feet due North from the missile and moving East at a constant speed of 20 knots. It is assumed that the missile seeker tracks an aim point perfectly. The aim point is located nominally 10 feet above the ship's

waterline and amidships. This aim point continually shifts as a function of ECM blinking and a random glint simulation.

3. ECM Simulation

The ECM blinker simulation shifts the radar target seen by the missile's seeker forward and aft from the true target aim point by ± 75 feet along the ships longitudinal axis at a specified frequency. The aim point is simultaneously shifted vertically ± 10 feet at the same frequency.

4. Attack Profiles

The attack profile used as a baseline for this simulation began at 50 feet of altitude at a speed of Mach 0.75. The missile tracked toward the target using proportional navigation in azimuth and altitude hold at 50 feet. At a range of 18000 feet the missile rolled to 60 degrees of bank and turned away from the target to the right until the target line of sight was offset by 10 degrees. When the offset was reached, the missile climbed to an altitude of approximately 250 feet and then dove toward the target using proportional navigation in both azimuth and elevation. This mission profile is often referred to as a popout attack.

Variations of this mission included eliminating the 10 degree offset turn and/or the climb to altitude and substituting skid-to-turn control laws for some phase of the mission. A ballistic altitude profile was also attempted.

D. EXISTING WORK

In order to examine the existence of such problems and to test several proposed solutions, a six degree of freedom simulation of a typical BTT cruise missile was produced by LCDR Kent Watterson and published in [Ref. 1]. This simulation was produced using the IBM Continuous System Modelling

Program (CSMP III) simulation language. A detailed description of this language and its constructions is presented in [Ref. 2] and [Ref. 3]. The simulation included dynamics, autopilot, guidance and mission profiles. It did not represent any specific missile but, rather, included characteristics typical of missiles configured in this way. In order to overcome limitations imposed upon the simulation program by the available computer installation, this CSMP program was rewritten in extended FORTRAN H. This allowed greater flexibility and full utilization of the DISPLA graphics programming package available at NPS. A complete copy of the program listing is presented in Appendix D.

E. SCOPE OF TESTS

The tests conducted with the revised simulation program were limited to examining the effects of ECM blinking and glint upon the missile's control system and accuracy against a simulated medium sized combatant vessel traveling at 20 knots perpendicular to the missile's track over the earth. Alternate attack profiles using modified flight geometry and, in some cases, skid-to-turn control laws were also tested. A listing of the different flight profiles examined is presented in table I.

For all flight tests of the missile, certain parameters were held constant. A list of these values is presented in table II.

TABLE I
Missile Attack Profile Test Configurations

	OFFSET BURN	POP-UP	REOLIF	TOPN
BASLINE	X	X	0.5	BTT
II		X	0.5	BTT
III			0.5	BTT
IV		X	0.1	BTT
V		X	0.5	STT
VI		X	0.5	*

* 90 degree bank on ballistic terminal trajectory

TABLE II
Simulation Variables Held Constant

Variable Name	Value
*****	*****
Radar Burn-Through Range	500 ft
EC* Blinker Shifts:	
Longitudinal	± 75 ft
Lateral	± 00 ft
Vertical	± 10 ft
Baseline guidance scheme:	
Offset	10 deg
Popup Altitude	100 ft
Popup Range	13000 ft
Roll rate limit	7°/s
*****	*****

II. PROGRAM DESCRIPTION

A. INTEGRATION OF THE EQUATIONS OF MOTION

This simulation uses the linear, six degree of freedom equations of flight developed by Boskam in [Ref. 5:vol 1] and modified by Hewett in [Ref. 4]. The CSMP program developed by Watterson [Ref. 1] used a variable step Runge-Kutta integration method. The FORTRAN translation program uses a

$$\text{INTEGRAL}(\text{YDOT DT}) = \text{Y} + (\text{YDOT}) * \text{DT} \quad (\text{eqn 2.1})$$

simple Eulerian integration which is given by equation 2.1. The incremental time element, DT, is fixed at 0.01 seconds and the integration period lasts for less than 30 seconds.

B. PROGRAM NOMENCLATURE

A detailed description of the nomenclature used throughout the simulation program is presented in Appendix C. The variable names used in the FORTRAN translation are, with few exceptions, the same as those used in the the CSMP simulation.

C. AXIS SYSTEM

The simulation uses a right handed earth reference frame where the x-axis points North, the y-axis points East and the z-axis points down. However, altitude and vertical velocity are always given as positive upwards (i.e. ALTITUDE = -Z). For plotting the geographical track in the output routines, the axes are transformed so that the X,Y, and Z axes point East, North and upward, respectively.

D. PROGRAM ARCHITECTURE

The FORTRAN simulation program consists of an executive program which calls seven major subroutines which are briefly described as follows.

1. Executive Program

The main calling program is short and handles only three tasks. It increments the TIME variable for each integration cycle. It calls the output data storage routine, PREPAP, at the specified output interval and it controls the execution of multiple flights within a single program run changing one or more key variables between the runs.

2. Subroutine INIT

This subroutine contains a small section of executable statements which resets variables to their initial value when more than one flight is flown during a program run. Included with this subroutine is the BLOCK DATA subroutine which must be used to initialize all variables in named common areas. The majority of the BLOCK DATA subprogram is taken up with arrays listed in table form which contain the aerodynamic coefficient data for the missile. Static coefficients which are functions of one variable are shown in figures A.2 through A.9 Static coefficients which are functions of two parameters are presented in figures A.10 through A.13 Dynamic coefficients are assumed to be constant and are not presented graphically.

3. Subroutine MISSION

This subroutine dictates the mission profile. It is divided into sections which activate in sequence as the mission progresses. Each section takes the flight dynamics data for the missile, compares it with the target

acquisition data (generated in subroutine TGTNAV) and outputs vertical and horizontal acceleration commands in the geographic earth reference frame. These in turn are translated into commanded bank angle and normal load factor for the missile according to equations 2.2 and 2.3. A diagram

$$PHIC = \text{ARCTAN}(AYC/AZC) \quad (\text{eqn 2.2})$$

$$NCC = AZC \cos(PHI) + AYC \sin(PHI) \quad (\text{eqn 2.3})$$

of these vectors is given in figure A.1. Different terminal attack profiles are implemented using variations of this subroutine, MISSN1 and MISSN2, which are presented in Appendices E and F.

4. Subroutine ABPILOT

This subroutine takes the commanded normal load factor and bank angle and applies them to the missile autopilot system. A detailed description of the design of the missile's autopilot is presented in reference [Ref. 1]. The output of the control system is delivered in terms of conventional airplane elevator, aileron and rudder control positions. These are mixed to obtain the commanded missile fin positions. The control limits of ± 15 degrees are applied to the fins and these controls are then unmixed to obtain the limited conventional control positions. The dynamics of the servo actuators that move the tail surfaces are modelled as a first order real pole. Although CSM2-III provides macros that perform the simulation of many types of transfer functions within the control system only the first order real pole transfer function was necessary for this program. It is modelled in the FORTRAN translation using subroutine REALPI, presented in the program listing in Appendix C.

5. Subroutine AEFC

Subroutine AEFC uses two table lookup routines to retrieve the aerodynamic coefficients from the data presented in figures A.2 through A.18. Linear interpolations are used to obtain values between given parameters. Error messages are printed when the input parameters are outside the bounds of the data in the lookup table and these are suppressed after about 5 successive integration cycles. AEFC completes the buildup process, uses these data to compute the forces and moments on the aircraft and then integrates the equations of motion to update all of the aircraft's flight parameters and position information.

6. Subroutine TGTNAV

The TGTNAV subroutine navigates the target vessel on a course of East at a steady speed of 20 knots. It shifts the position of the radar target relative to its real position according to the ECM and GLINT parameters. The GLINT offset is produced by multiplying the GLINT shift in each axis by a random number between -1 and 1. The GLINT offset is calculated every output interval rather than 100 times per second. The ECM offset is switched according to the sign of a sine wave which runs at the ECM blinking frequency, FFEQ. These offsets are then added to the actual target position to produce the radar target position. Line of sight angles and rates are calculated from this information with the assumption that the seeker has perfect pointing capability.

7. Subroutine PFERAE

At intervals specified by the output counter, this subroutine is called and stores up to 20 variables in a large array call PTS. The output interval used for all tests

was 0.20 sec. The PTS array is passed to the output routines when the simulation run is completed. This subroutine also converts output variables from radian to degree format and, in the final attack phase, calculates four error functions. These error functions are time averaged differences between commanded variables (e.g. BANK or ROLL RATE) and their actual counterparts. These are later used to analyse the performance of the control system under various conditions.

8. Subroutine OUTPUT

OUTPUT produces 3 forms of output information. The primary data output lists the value of MISDST (the distance at which the missile passed the target at its closest approach), the value of the error functions at the end of the mission, and the ranges of all the variables stored. These data are also printed to another file followed by the full contents of the PTS array in tabular form. This gives a numerical history of all the output variables from the start to the finish of the mission. (Normally, to save disk space, this file was routed to a dummy variable. It was needed only when detailed data histories of a portion of the mission were required.)

OUTPUT also calls the necessary DISPLA routines to print graphs of the output variables. The independent variable in six graphs is TIME. In the seventh graph the positions of the missile and the target ship are plotted in three dimensional space for each output interval. Each of the graphs in this subroutine are controlled by the setting of 7 flags in the first column of the data statement at the beginning of the routine (0 to pass over and 1 to plot).

III. BASELINE ATTACK CONFIGURATION

A. AUTOPILCT ROLL RATE COMMAND LOOP ADJUSTMENT

Initial testing of the simulation was conducted on the CSMP version of the program. The frequency of the ECM blinker was varied from 0.2 Hz to a maximum of 2.0 Hz and the roll performance of the missile was graphed. Figure A.19 shows the commanded roll rate and actual roll rate plotted against time for the duration of a thirty second flight straight toward the target at a constant altitude of 50 feet. The target's radar position was blinked at a rate of 0.4 Hz and roll rate command was limited to 75 degrees per sec. In the figure, the command oscillations increased in magnitude as the target range decreased and, after 24 seconds, the autopilot commanded the maximum rate with every shift of the target's apparent position. While the commanded roll rate remained at 75 degrees per second, the actual roll rate never exceeded 35 degrees per second. Figure A.20, which plots the fin positions as a function of time, shows that the fin servos never used more than 3 degrees (of the maximum 15) of travel in either direction. To remedy this problem, the missile autopilot roll rate command loop gain (KROLLPT in the program) was increased from 0.1 to 0.5. The value of this gain had been set by Watterson [Ref. 1] using root locus based upon the perturbation equations of motion [Ref. 4] in steady state level flight. Figures A.21 and A.22 show the results of a subsequent run with the revised guidance loop. Steady state error in roll rate was significantly reduced and the full range of available flight controls (± 15 deg.) was used. This difference in the autopilot was incorporated into the baseline program and remained throughout all subsequent tests.

E. BASELINE PROGRAM

In order to provide a baseline performance record against which to examine the effects of ECM and glint and/or alternate attack profiles on the accuracy of the missile and the performance of its control system, a standard, pop-out attack with an offset turn was selected and flown and is used as a standard for comparison. The parameters which apply to this baseline are listed in table II. Figures A.23 through A.28 are a complete record of the baseline program run without any ECM or glint offsets applied to the target. Figures A.29 through A.35 are a complete record of the baseline program run with the ECM blinker operating at 0.2 Hz and the glint feature operating. The complete tabular data output from this latter run is presented in Appendix F.

IV. FREQUENCY SCAN TESTS

A. ERROR FUNCTIONS

For testing the effects of glint and ECM at various blinking frequencies against the control system of the missile, a quantitative measure of the system's effectiveness was needed. Four error functions were developed for this purpose. The time weighted difference between the commanded value and the actual value of a variable was computed according to equation 4.1. This time weighted error was summed over all of the time intervals and divided by the

$$EFE = DT * ABS(COMMAND - VARIABLE) \quad (\text{eqn 4.1})$$

total time to produce the error function for the variable. The variables for which these functions were computed are

TABLE III
Error Function Variables

VARIABLE	COMMAND VARIABLE
*****	*****
1. BANK	BANK
2. ROLL RATE	ROLLST
3. AZIMUTH LOS RATE	0.0
4. ELEVATION LOS RATE	0.0
*****	*****

listed in Table III. In the terminal phase where proportional guidance is used in both the azimuth and elevation channels, the commanded azimuth and elevation angle rates are zero to produce a constant bearing intercept.

B. ECM PHASING

At low frequency blinking rates, the phase of the ECM blinker at the start of the mission had a very large effect on the miss distance. To minimize the distortion of the data due to this effect, a phase variable was added to the ECM generator to change the phase of the blinker at the start of each run. Four runs were conducted at each frequency using values of 0.0, $\pi/2$, π , $(3/2)\pi$ for the phase variable. The data for each frequency were averaged to get mean values for the miss distance and each error function.

C. BASELINE TEST RESULTS

1. ECM Frequency Scans

Four simulated flights were conducted at each frequency from 0.0 to 30 Hz. Glint was disabled for the course of these tests. The attack profile flown was the baseline popout attack mission. A graph of the mean value of the miss distance (MISDST) versus frequency is presented in figure A.36. The data show that maximum miss distance occurs in the very low frequency range of the order of 0.2 Hz and again to a lesser degree in the vicinity of 6 Hz. Figures A.40 and A.44 are plots of the error function means against frequency for the autopilot command errors and the tracking errors respectively. These data show that the bank angle command loop is susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop is primarily responsible for the errors that occur at the higher frequencies in the range of 5 to 10 Hz. Figure A.44 also demonstrates that the time averaged tracking errors follow the same basic pattern.

Figures A.48 through A.53 demonstrate these effects in flight. Figures A.48 and A.51 show the bank angle and

roll rate performance of the baseline missile without ECM. Both variables track closely to their commanded values with the exception of a small, steady state error in the rate channel which is most evident at large commanded rates. Figures A.49 and A.50 show the effects of ECM at 0.4 and 6.0 Hz upon the bank channel. In figure A.49 significant errors exist in bank as the system cannot keep up with the large, sudden changes in commanded bank caused by the ECM shift of the target. The bracket in figure A.49 is drawn between two corresponding points to emphasize the large lag present in the channel. Roll rate tracks close to its commanded level at this frequency.

At 6.0 Hz, figures A.52 and A.53 show the opposite effect. In figure A.53 the bracket emphasizes the large lag that exists in the aircraft roll response to the rapid changes in rate command. The bank command loop at this frequency has effectively filtered out most of the high frequency input.

The results of the frequency scan tests showed that the baseline BTT cruise missile simulated by the program was more susceptible to ECM frequencies in the vicinity of 0.2 and 6.0 Hz due to the excitation of the bank and roll rate command loops respectively. If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

2. Effects of Glint

In order to isolate the effects of glint, the baseline configuration was flown without ECM or glint and again with glint only. Figure A.33 shows a trace of the random glint

displacement applied to the target's position as a function of time. Figures A.23 through A.28, which trace the missile's load factor, bank angle, roll rate and flight controls without glint, may be compared with figures A.54 through A.57 which show the same traces for the mission with glint.

The miss distance recorded without glint and an ECM phase of 0 was 3.7 feet. The distance measured with glint was 9.4 feet. Although these distances are very small compared with the miss distances achieved with ECM, the degradation induced by glint was large (154 percent) compared to the best obtainable value. Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Since the miss distances without ECM and glint were very small compared to those obtained with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

D. ALTERNATE CONFIGURATION FREQUENCY SCAN RESULTS

1. Mission Profile

Similar frequency scan profiles were flown using the MISSN1 (Appendix E) subroutine to generate the guidance commands for configurations II, III and IV. These attack profiles committed the offset turn and proceeded straight toward the target using proportional navigation in azimuth from start to finish. The popup maneuver was commenced at 15000 feet from the target. Of ranges from 20,000 to 5,000

feet which were tested, 15,000 feet produced the most consistent hits with a 200 foot popup altitude command. All subsequent tests of these missile attack configurations used 15,000 ft. popup range and a 200 ft. altitude command when the maneuver was performed.

An algorithm was added to the baseline proportional guidance scheme for the terminal phase which ensured that the missile rolled to place the nearest of the positive or negative Z-axis vectors on the direction commanded by the guidance system. This ensured that the missile would command negative load factor rather than trying to roll the missile upside down as it reached the apex of its climb. Azimuthal accelerations commanded by the guidance were still achieved by banking the missile except for configuration V.

A complete set of mission profile graphs for configurations II, III, and IV against a target with glint and ECM blinking at 0.2 Hz are presented in figures A.58 through A.75

2. Frequency Scan Results

a. Miss Distances

Each configuration was flown against the target four times per test frequency. The tests covered a range of blinker frequencies from 0.05 through 30.0 Hz. The mean miss distances recorded are graphically presented as a function of frequency in figures A.37 through A.39. The results obtained were very similar to those obtained from the baseline configuration. There were two areas of higher than normal errors, one at low frequency below 0.2 Hz and another at a higher frequency near 6.0 Hz. Table IV compares the miss distances for each of the configurations.

The maximum values that occurred for all configurations appeared at the same frequencies with one

TABLE IV
Maximum Miss Distances

CONFIGURATION	FREQ. RANGE (Hz)	LOCATION (ft)	MAGNITUDE
BASLINE	0.20 - 20.0	≤ 0.20 6.00	≥ 45 22
II	0.05 - 21.0	≤ 0.05 6.00	≥ 75 17
III	0.10 - 30.0	≤ 0.10 5.50	≥ 75 17
IV	0.10 - 30.0	≤ 0.10 N/A	≥ 75 N/A

exception: changing the roll rate gain from 0.5 to 0.1 eliminated the maximum at the higher frequency. In addition, the magnitude of the errors did not differ significantly. (The baseline shows a smaller magnitude because the data do not extend below 0.2 Hz. while the other configurations were tested down to 0.1 and 0.05 Hz). Changing the attack geometry of the missile did not significantly alter its susceptibility to ECM jamming within the scope of these tests. Altering the gain of the roll rate command channel in the missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies. Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

1. Autopilot Errors

Figures A.40 through A.43 graphically present the error functions for both the bank angle and roll rate command loops within the autopilot. These functions are representative of the ability of the missile to follow the

commands given it by the autopilot (the higher the function, the poorer the performance). As with the baseline configuration these figures demonstrate that the bank angle loop contributed most to the errors at low frequency and the roll rate loop contributed most at the higher frequency. Table V

TABLE V
Autopilot Errors

CONFIGURATION	BANK ERROR		RATE ERROR	
	FREQ (HZ)	MAGNI- TUDE	FREQ (HZ)	MAGNI- TUDE
BASELINE	0.4	0.22	7.0	0.19
II	0.6	0.17	8.0	0.18
III	0.5	0.18	8.0	0.27
IV	0.6	0.21	2.0	0.37

is a summary of these graphs.

Magnitude of the bank error function and the frequency at which it occurred were not significantly altered in any one of the tested configurations. Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but

increased the magnitude of the errors by more than 100 percent. This effect is reflected in the miss distance graphs (figures A.36 through A.39) in the disappearance of the distinct maximum at 6 Hz and a widening of the lower maximum (figure A.39). Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect.

c. Tracking System Errors

Errors in the tracking loops are charted in figures A.44 through A.47. These errors follow the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

3. Skid To Turn Guidance Results

The MISSN1 subroutine was further modified to allow the lateral load factor command variable, NYC, to be set according to guidance commands rather than being kept at zero for turn coordination purposes. The commanded bank angle was set to zero in the terminal phase in order to examine the effectiveness of lateral G command. No changes to the basic dynamics of the autopilot were made. The missile was flown in this configuration against a passive target. Figures A.76 through A.81 present the full data set from this test. The missile splashed into the water 99 feet left and short of the target. Once the missile came within 5 seconds of impact, cross coupling between the rudder channel and normal load factor, roll rate and bank can be seen in the figures. Although the rudder commands were never saturated, neither could the lateral load factor control loop create enough sideforce to follow the ship's lateral drift to the right. The addition of ECM and/or glint would have

only worsened the performance of the missile in this configuration. No further tests of this configuration were conducted. The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

4. Ballistic Trajectory

Because the majority of the apparent target shift with ECM blinking occurs in the horizontal plane, an attempt was made to place the missile on a ballistic trajectory and then roll the aircraft to 90 degrees angle of bank until impact using the primary load factor to follow the ECM target and lateral load factor to maintain the ballistic trajectory. In order to fly the ballistic trajectory, the altitude hold system was driven by a commanded altitude slaved to a parabolic trajectory derived from the missile's vertical speed and range to the target according to equation

$$ALT = HMDOT * RANGE / V_H + (G/2) * (RANGE / V_T)^2 + 10 \quad (\text{eqn 4.2})$$

4.2. where HMDOT, V_H and V_T are the vertical, horizontal and total speeds of the missile. The controlling subroutine used for this mission was MISSN2 and is presented in Appendix F.

Figures A.82 through A.85 show that the addition of the dynamics of the altitude command loop made the missile's control system unstable. Oscillations to the limits occurred in normal load factor and in roll rate. Considerable cross coupling occurred between the lateral-directional and longitudinal dynamics of the missile. The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

V. CONCLUSIONS

The conclusions listed below were derived from analysis of the results of simulated flights conducted using the baseline popout attack profile configuration, three variations of the baseline attack, a skid-to-turn control configuration and a ballistic altitude trajectory.

A. BASELINE CONFIGURATION TESTS

At low frequency blinking rates, the phase of the ECM blinker had a very large effect on the miss distance.

The best obtainable performance for the baseline mission without ECM or glint was a miss distance of 3.7 feet. The addition of GLINT produced a miss distance of 9.7 feet, a degradation of 154 percent.

The bank angle command loop of the missile autopilot in the baseline configuration was especially susceptible to ECM frequencies of the order of 0.2 Hz while the roll rate command loop was primarily affected at the higher frequencies in the range of 5 to 10 Hz. The time averaged tracking errors also followed the same basic pattern.

If distances greater than 20 ft from the center of the target are considered likely misses, then the excitation of the roll rate command loop did not produce enough error to cause a likely miss. The best results, from the target's point of view, will be obtained with low blinking frequencies in the vicinity of 0.2 Hz.

B. ALTERNATE ATTACK PROFILE CONFIGURATIONS

In terms of the average miss distances measured, changing the flight geometry of the missile did not signifi-

cantly alter its susceptibility to ECM jamming within the scope of these tests.

Altering the gain of the roll rate command channel in the baseline missile autopilot significantly decreased its susceptibility to ECM blinking at higher frequencies.

Changing the geometry of the attack had no effect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the roll rate gain from 0.5 to 0.1 had no noticeable affect on the magnitude of the bank error function and the frequency at which its maximum occurred.

Changing the geometry of the attack had no effect on the frequency at which ECM was most effective against the roll rate control system, however the magnitude of the errors were increased by approximately 50 percent when the popup maneuver was eliminated (configuration III).

Decreasing the roll rate autopilot gain from 0.5 to 0.1 (configuration IV) moved the resonant frequency for the roll rate command system to a lower frequency but increased the magnitude of the errors by more than 100 percent. This effect was reflected in the miss distance data by the disappearance of the distinct maximum at 6 HZ and a widening of the lower maximum. Altering the autopilot gain was effective at moving the resonant frequency to a different region but could not eliminate its effect and, in this case enlarged it.

Errors in the azimuth and elevation tracking loops closely followed the trends of the autopilot and miss distance errors. At the lower frequencies, azimuth performance was dominant while at higher frequencies the elevation tracking loop experienced the largest degradation.

C. SKID TO TURN CONTROL

The use of skid-to-turn control laws could not produce sufficient sideforce to adequately follow a passive crossing target and produced excessive coupling into the longitudinal and lateral flight controls of the missile.

D. BALLISTIC ATTACK PROFILE

The attempt to fly a ballistic trajectory using the existing altitude control system was unsuccessful. In order to fly the attempted profile, a major redesign of the missile's autopilot would be necessary.

VI. RECOMMENDATIONS

Ways of minimizing the effect of random perturbations in the target position due to radar glint will make a significant improvement in the missile's accuracy in the absence of ECM and should be developed.

Further testing should be conducted to determine the extent to which autopilot modifications and gain adjustments can decrease the effectiveness of an ECM blinker against a bank to turn missile.

Since the elimination of a popup increased roll rate errors by 50 percent, a popup profile is recommended for the terminal phase of a BTT cruise missile. Further testing should be conducted to determine the effects of different popup profiles on the susceptibility of the roll rate command system to ECM blinking.

Since the miss distances without ECM and glint were very small compared to those with very slow blinking frequencies (0.05 to 0.2 Hz), further tests should be run concentrating on ECM in the very low frequency range. These tests should obtain a much larger sample of ECM phases in order to best define the shape of the miss distance curve below 0.2 Hz.

APPENDIX A
FIGURES

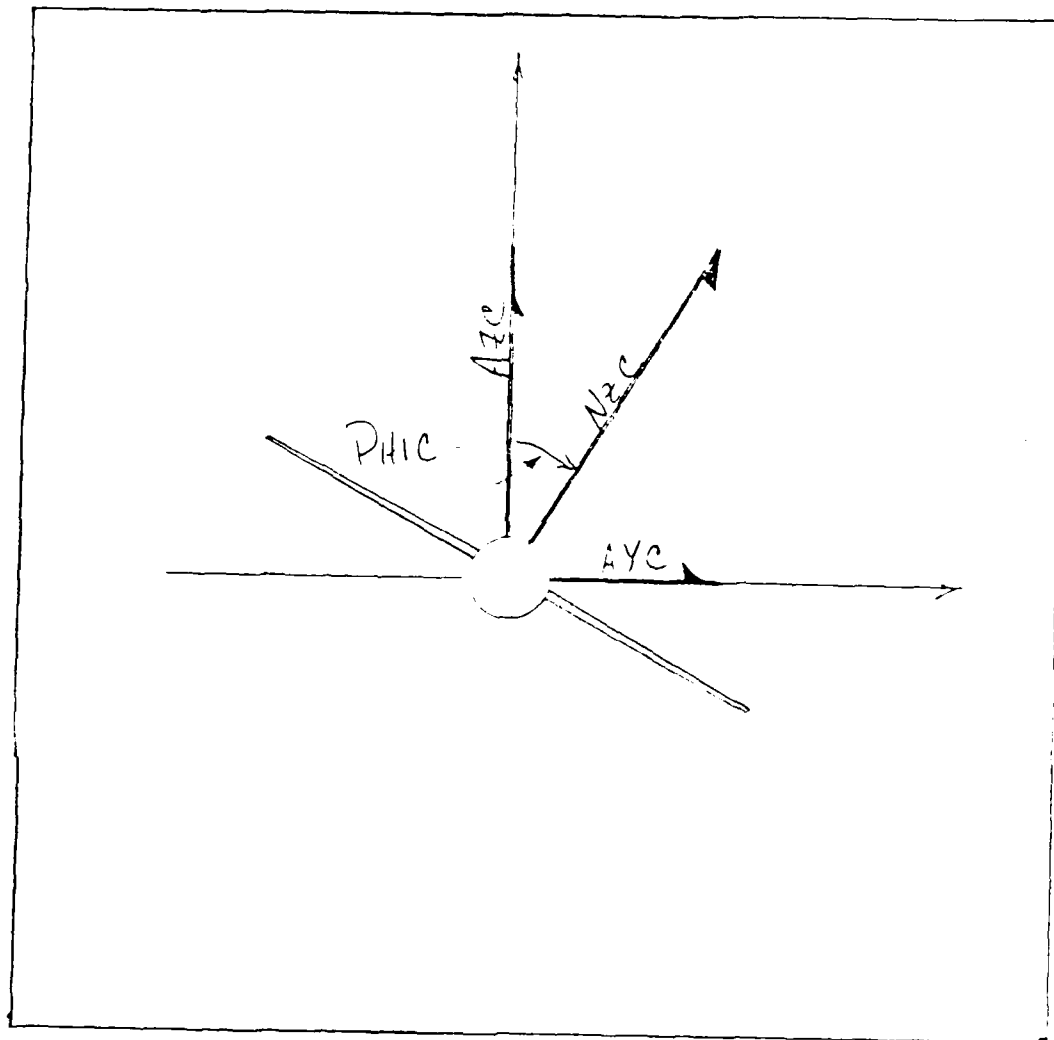


Figure A.1 Load Factor Commands.

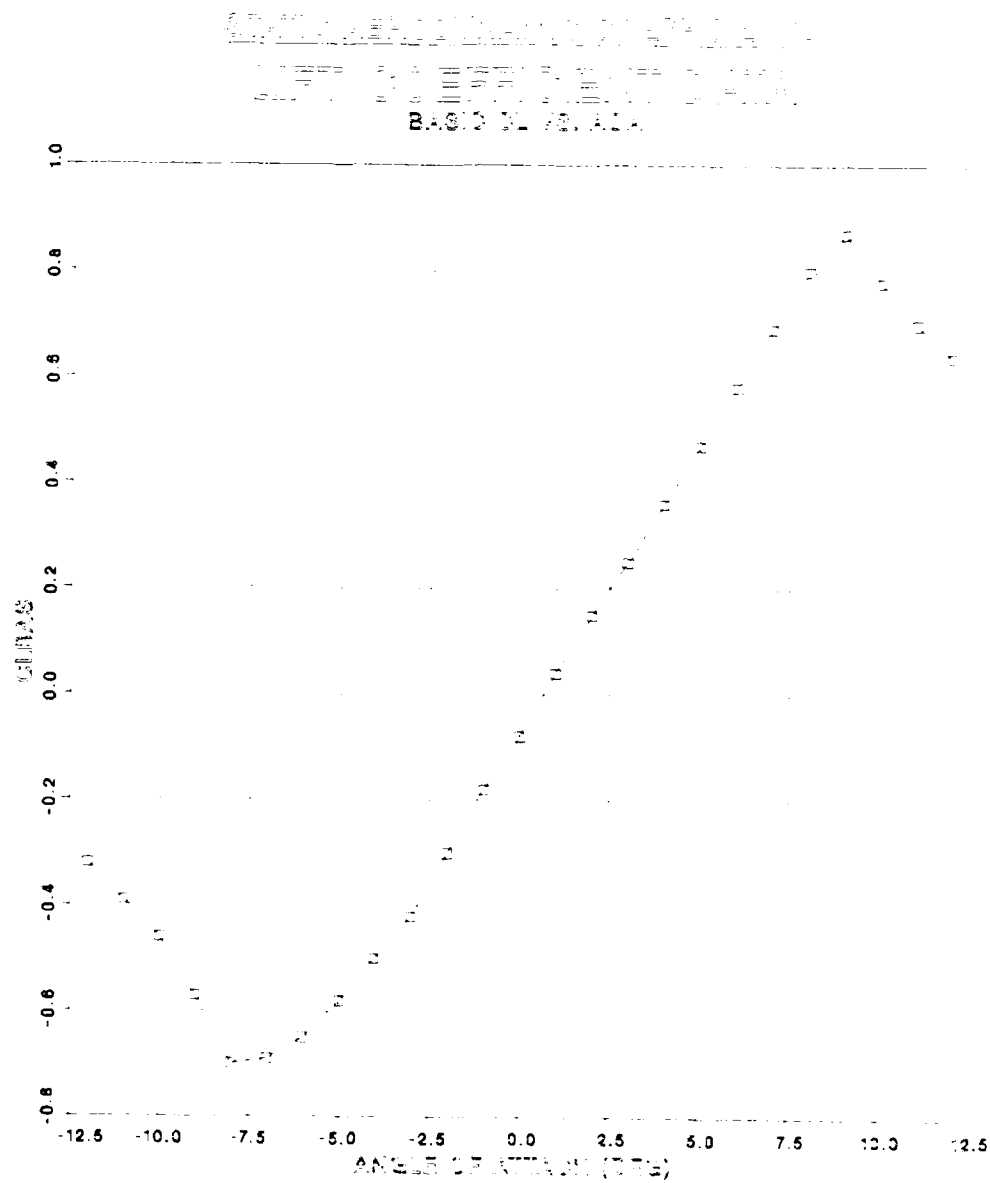


Figure A.2 Data Array LFT1.

BANK OF AMERICA

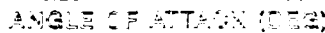


Figure A.4 Data Array DRG1.

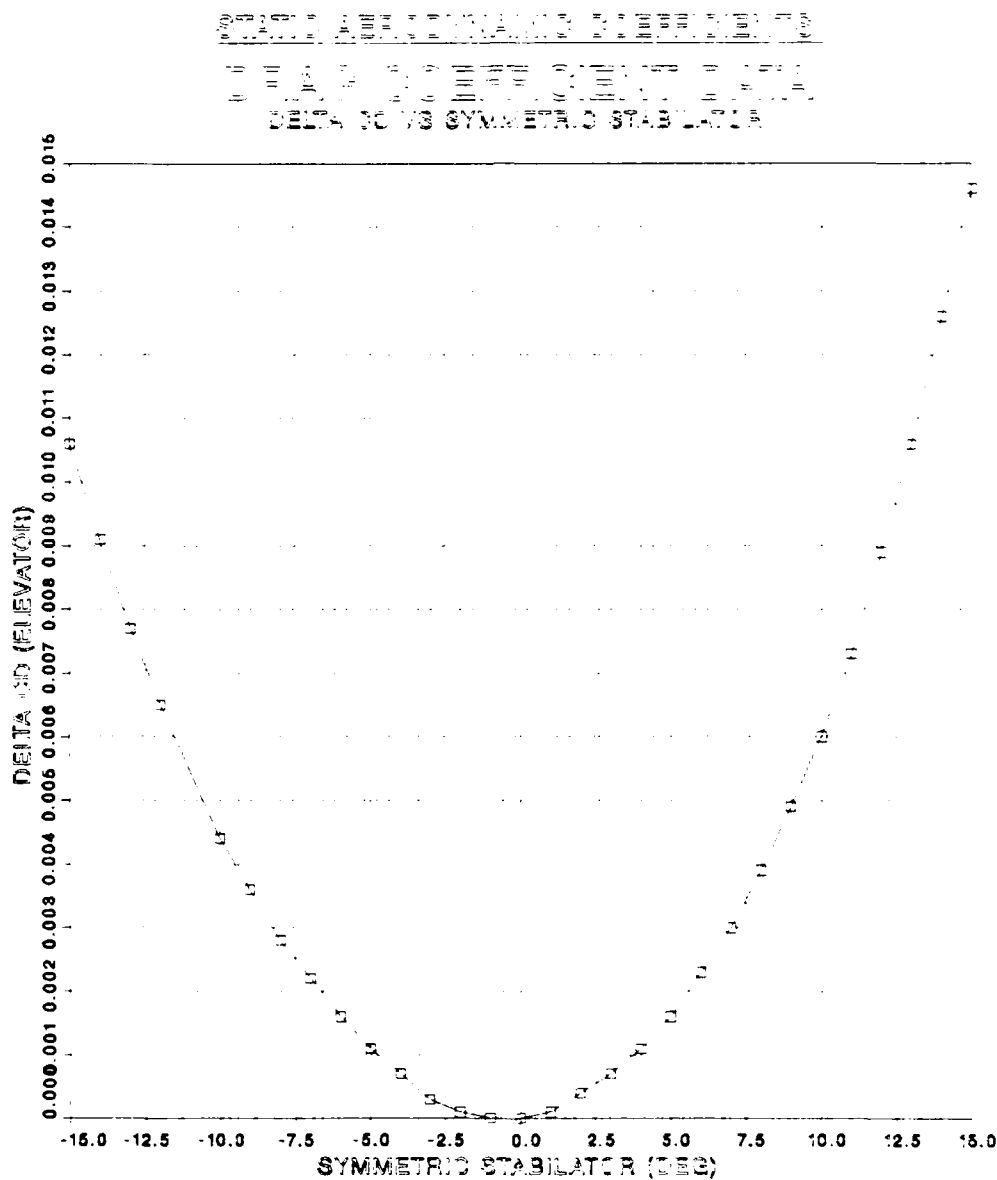


Figure A.5 Data Array DRG2.

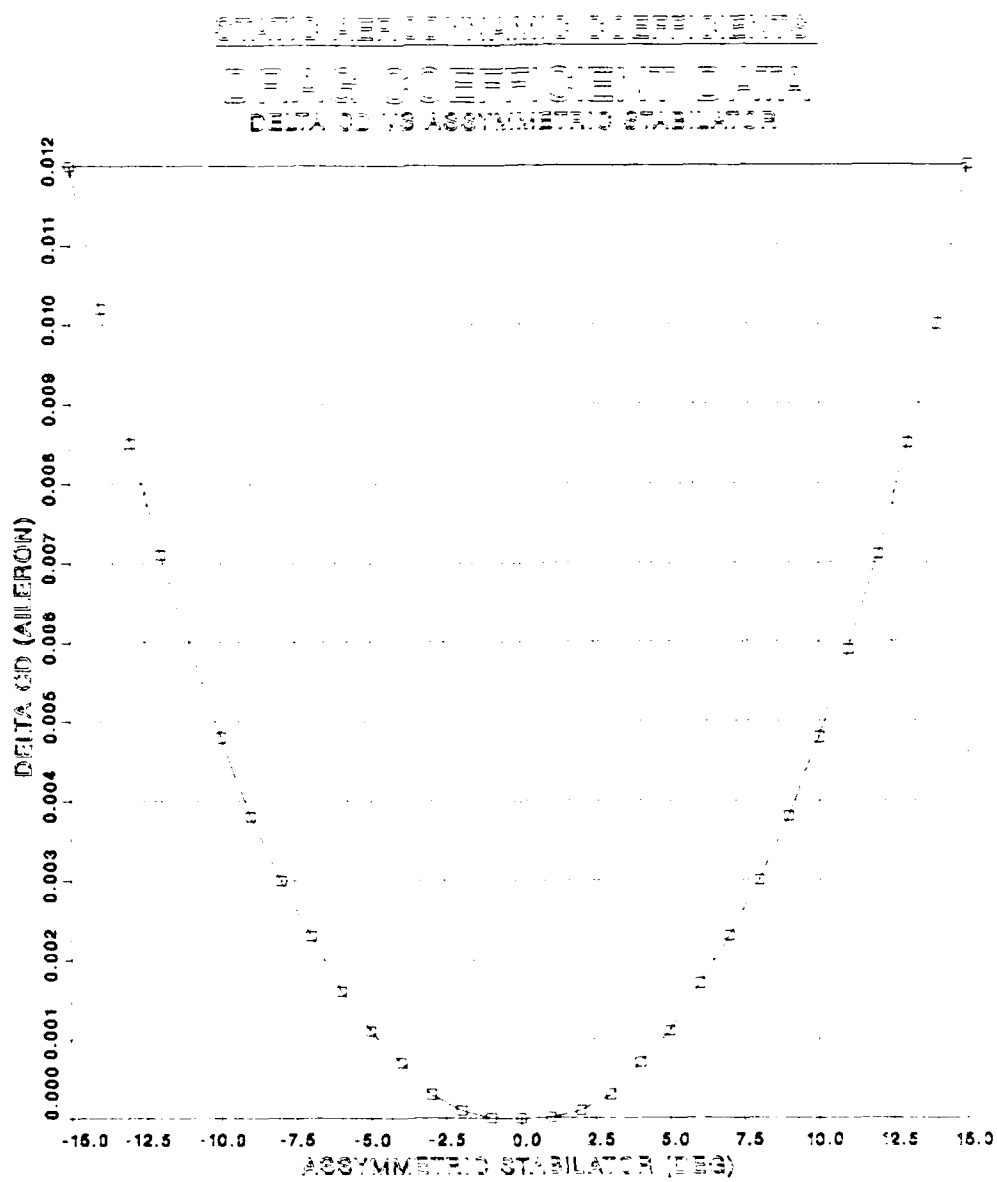


Figure A.6 Data Array DRG3.

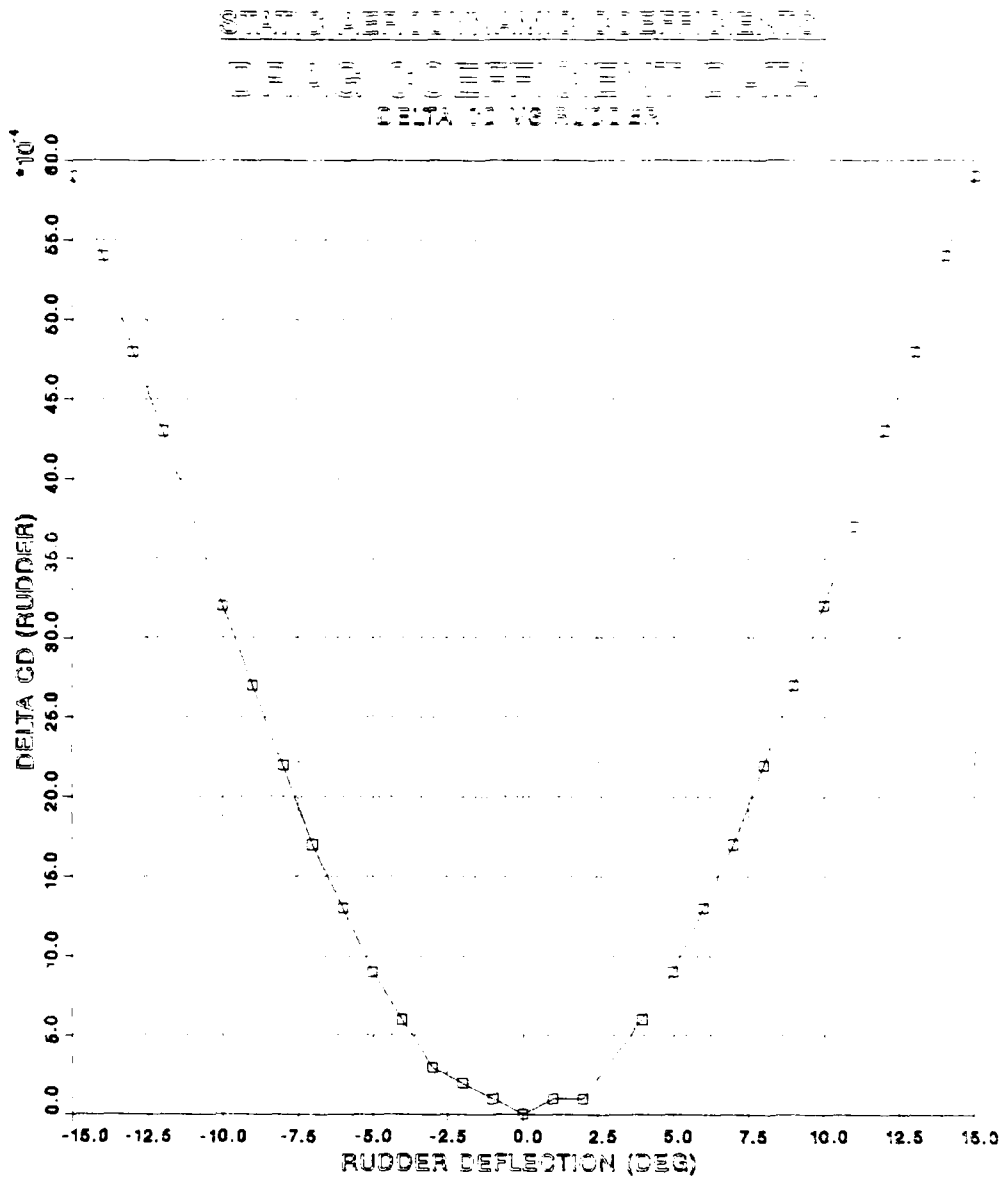


Figure A.7 Data Array DPG4.

BIOGRAPHICAL

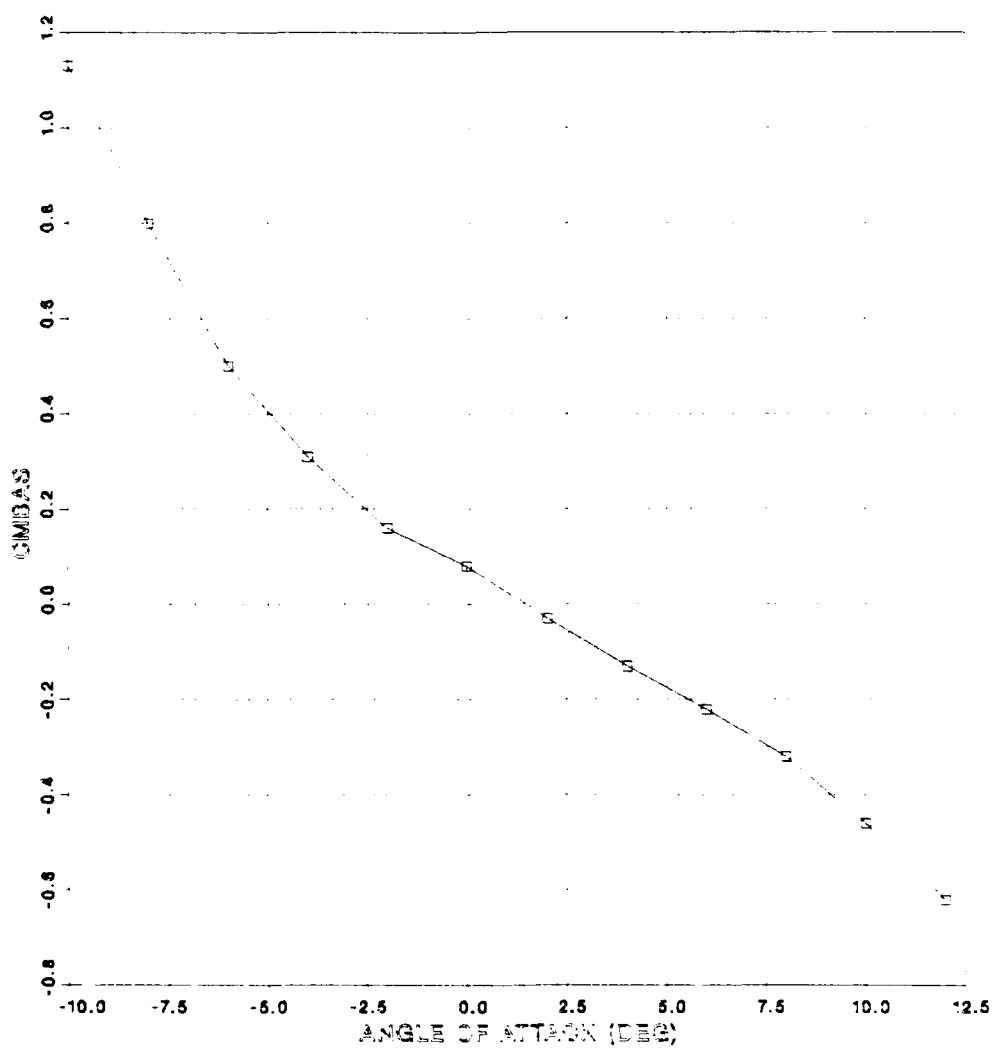


Figure A.8 Data Array PTCH1.

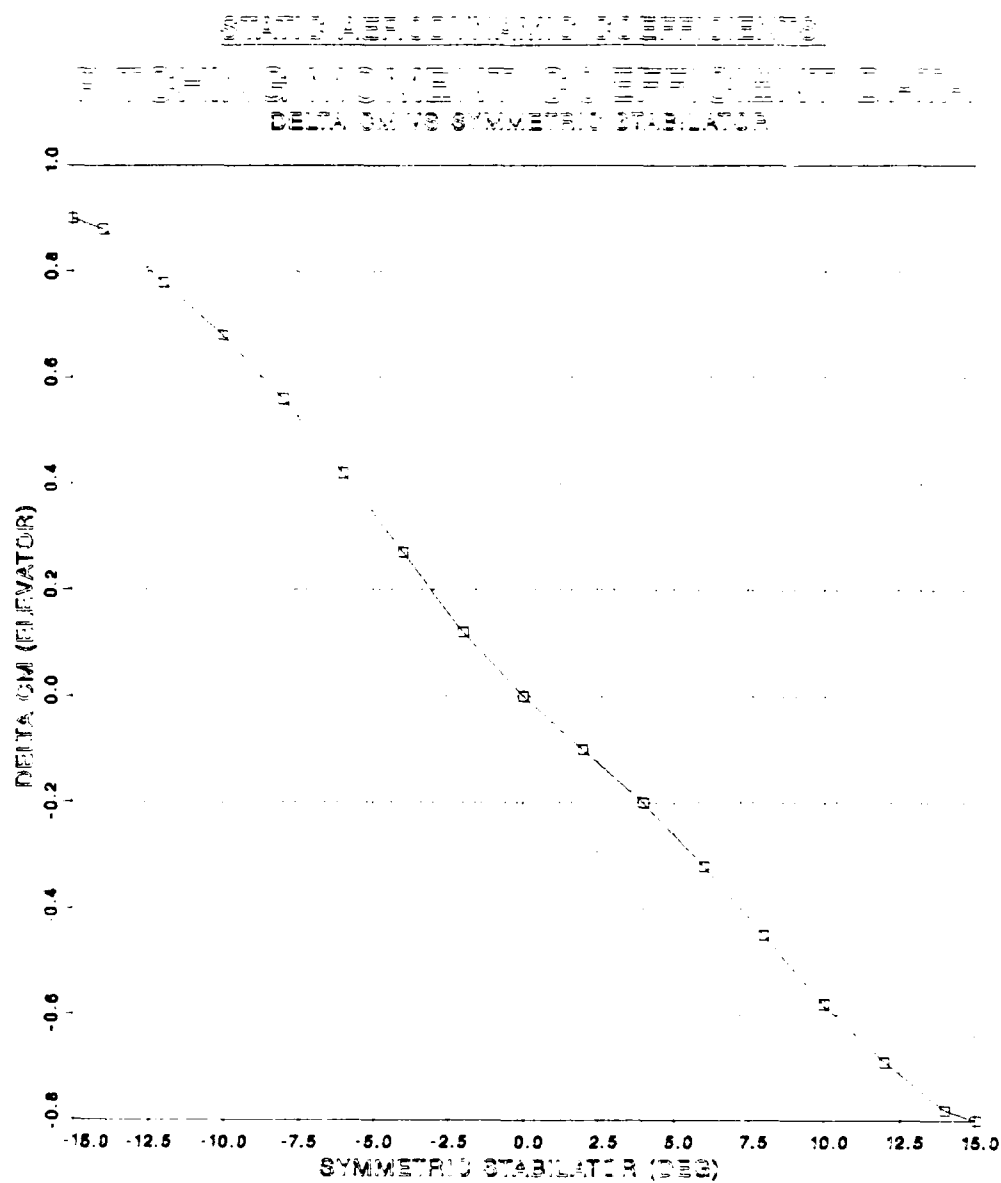


Figure A.9 Data Array PTCH2.

COEFFICIENTS OF THE
COEFFICIENT DATA
 BASED ON α , β

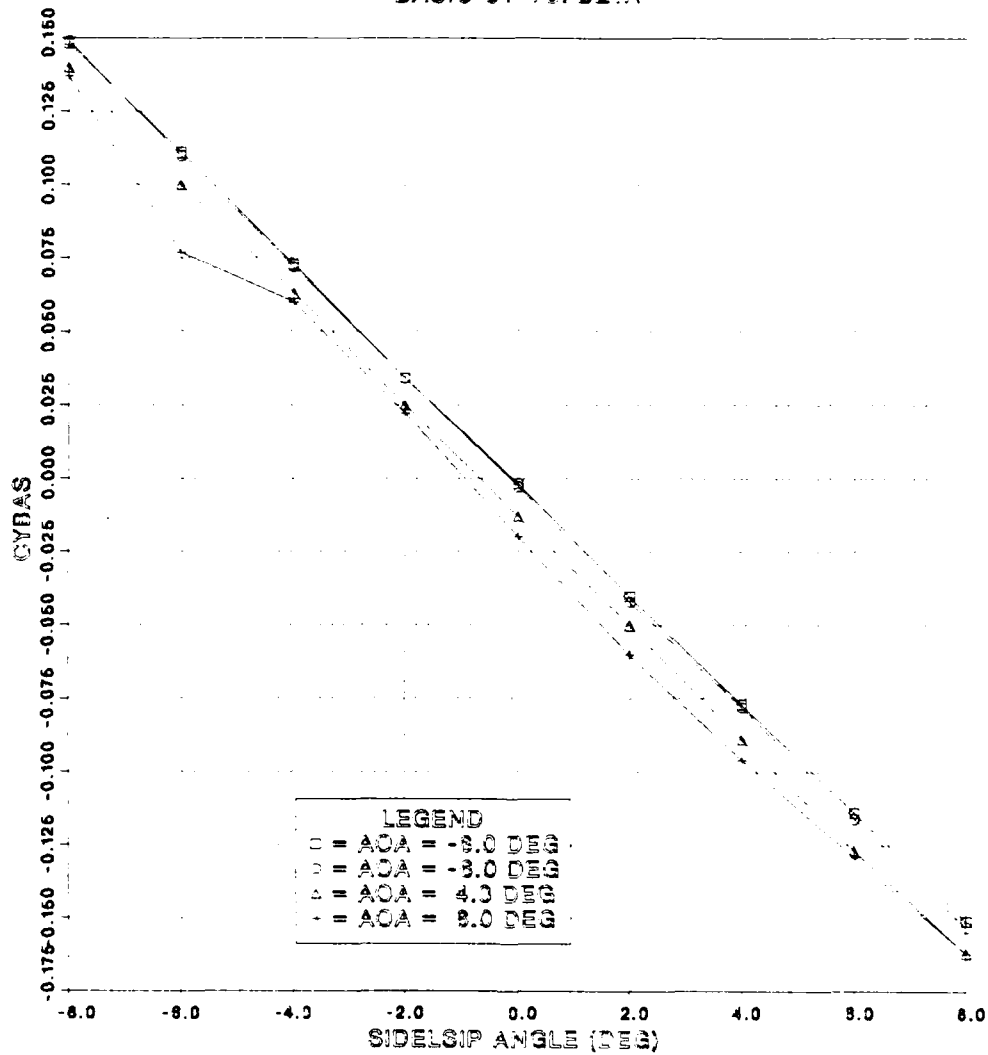


Figure A.10 Data Array SID1.

DATE: 11-2-78

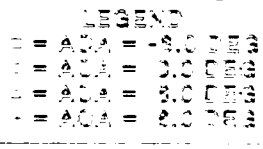


Figure A.12 Data Array SID3.

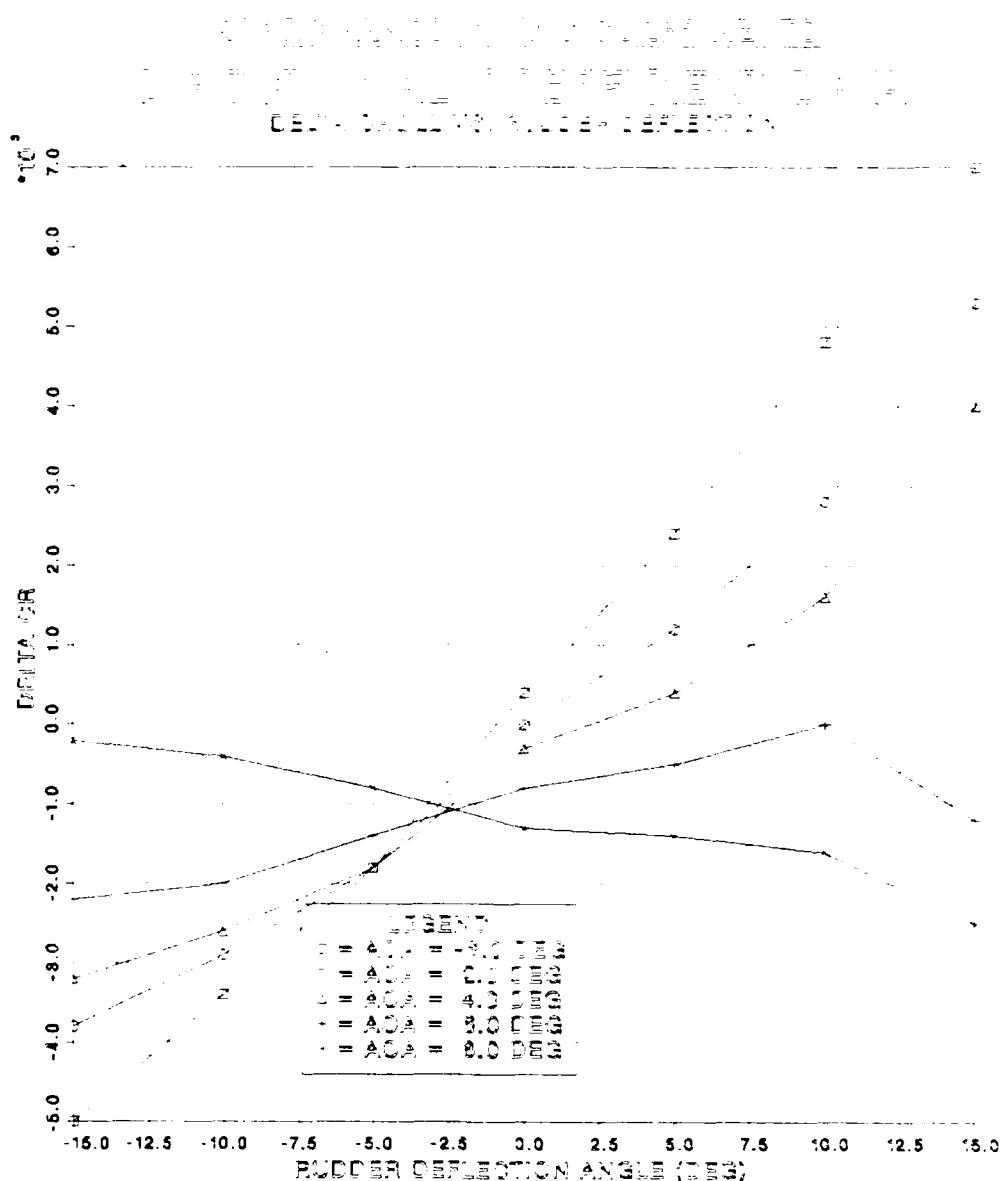


Figure A.15 Data Array DR3C3.

Figure 1 is a graph showing the effect of the concentration of the monomer on the rate of polymerization. The Y-axis is labeled "RATE OF POLYMERIZATION" and ranges from 0.000 to 0.020. The X-axis is labeled "MONOMER CONCENTRATION (M)" and ranges from -0.040 to 0.040. Five linear data series are plotted, labeled 1 through 5, all showing a positive linear relationship. A legend is provided in the bottom right corner.

Series	Symbol	Equation
1	□	$y = 0.49x + 0.001$
2	△	$y = 0.49x + 0.001$
3	○	$y = 0.49x + 0.001$
4	×	$y = 0.49x + 0.001$
5	•	$y = 0.49x + 0.001$

52

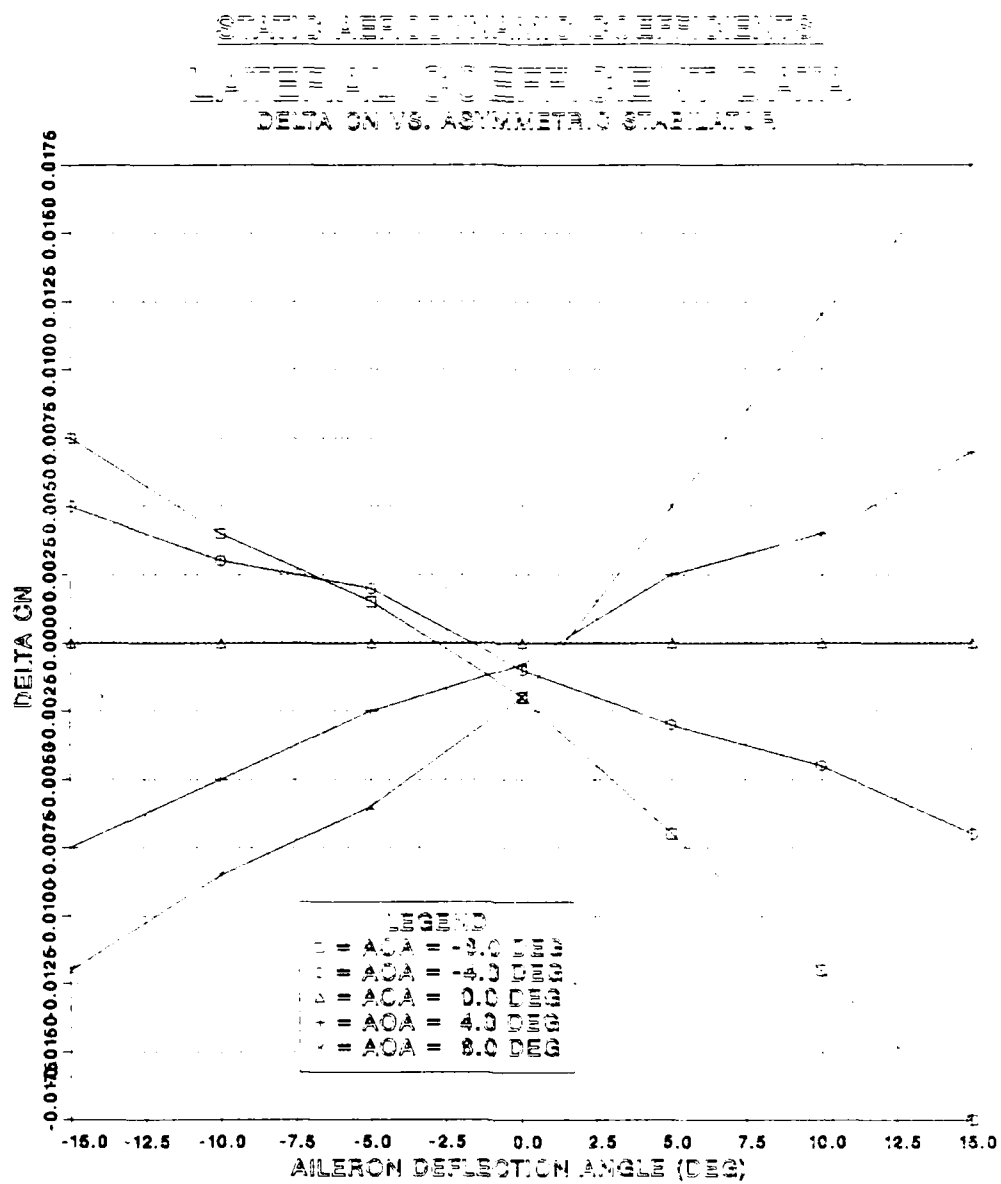


Figure A.17 Data Array LTFL2.

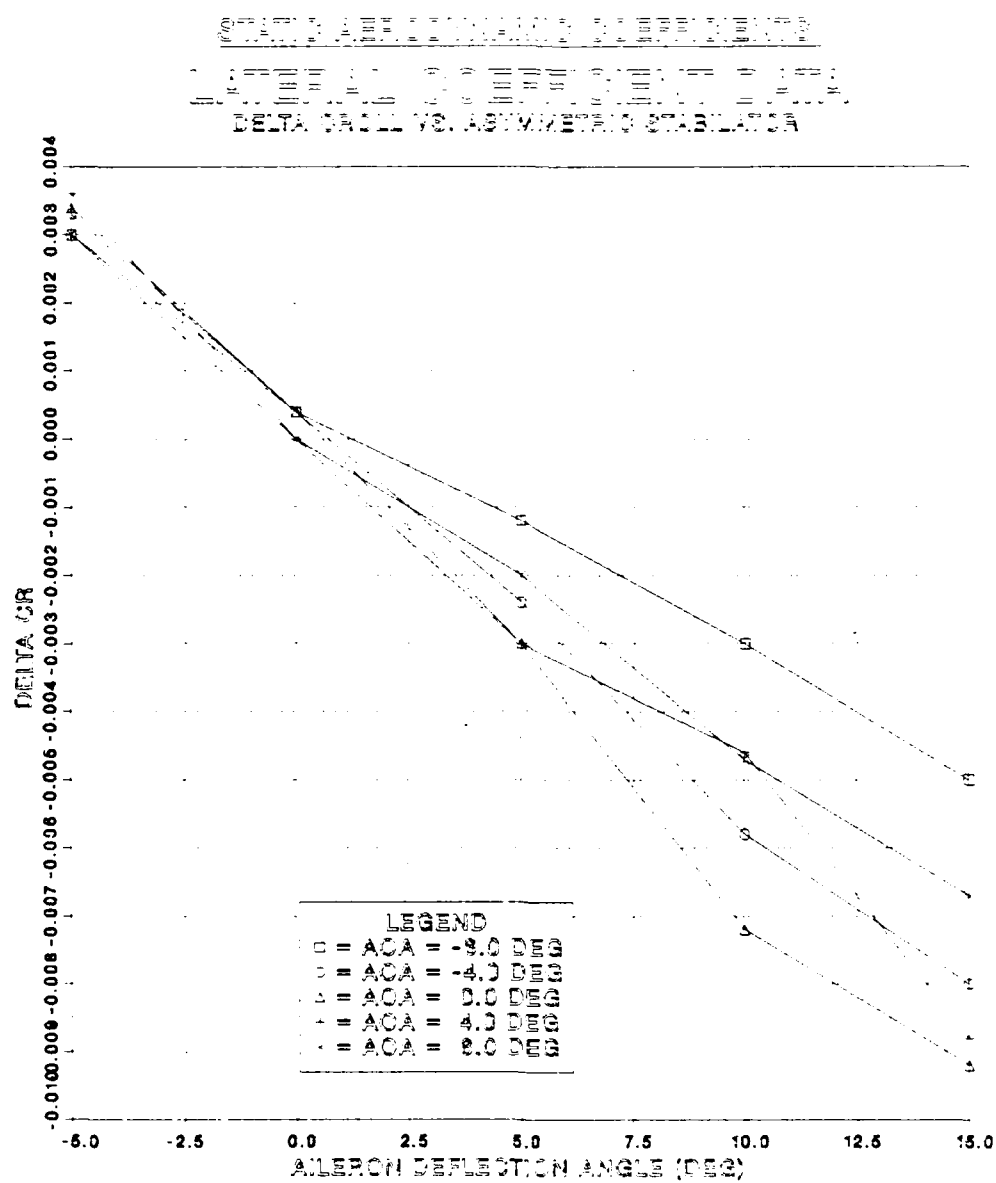


Figure A.18 Data Array LTFL3.

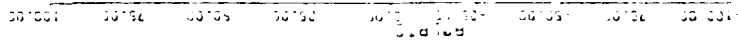


Figure A.19 CSMP Data (Roll Rate) - KROLLR = 0.1.

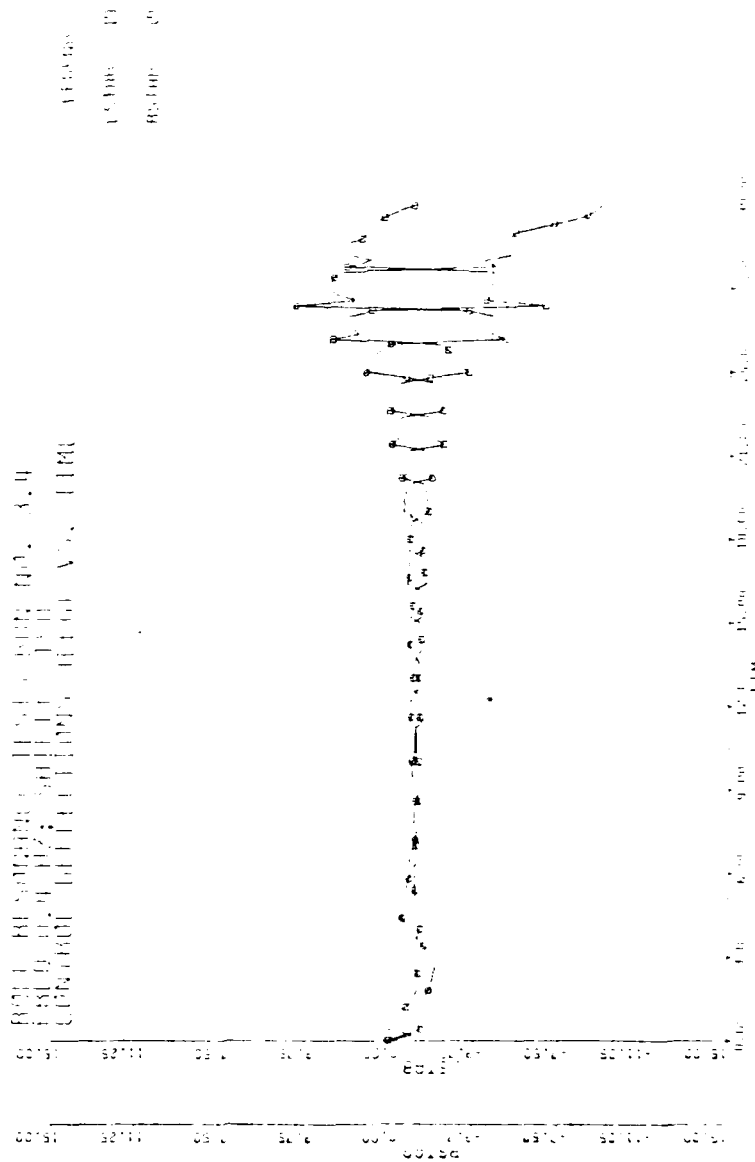


Figure A.20 CSMP Data (Controls) - KROLLF = 0.1.

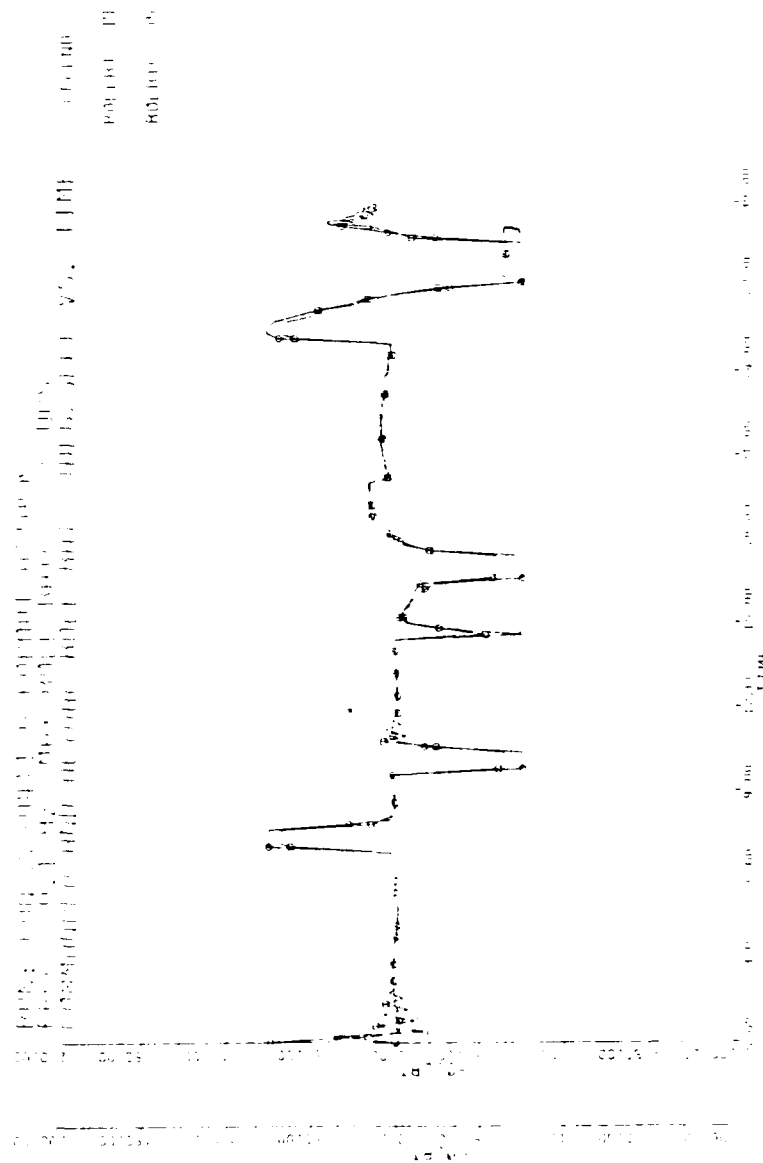


Figure A.21 CSMP Data (Roll Rate) - KROLLP = 0.5.

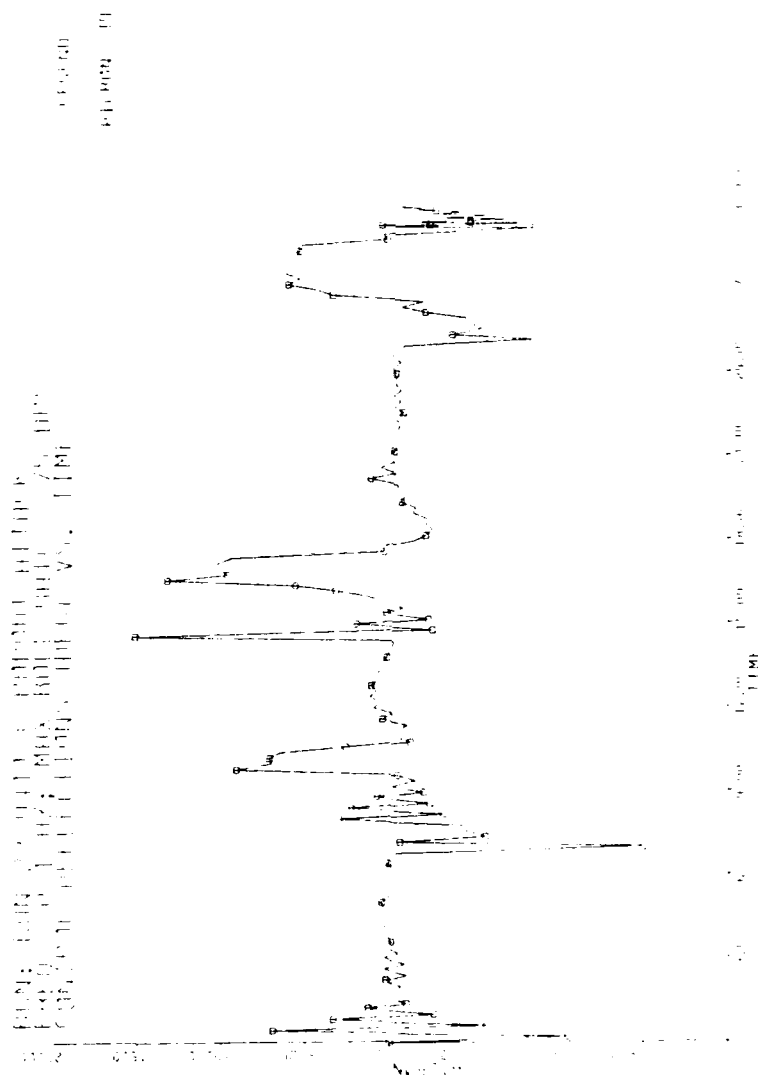


Figure A.22 CSMP Data (Controls) - Krollr = 0.5.

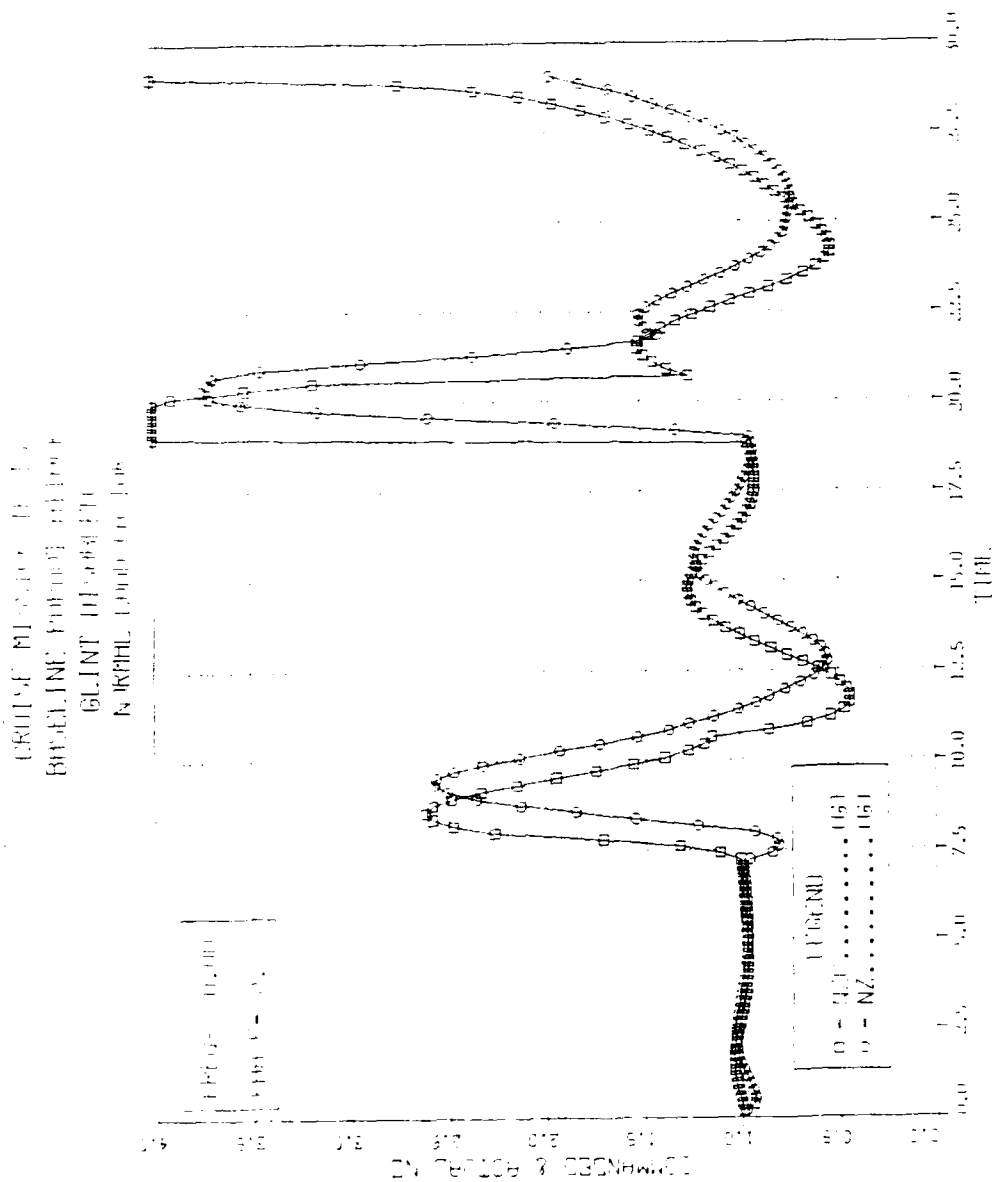


Figure A.23 Baseline - no FCM or GLINT - Load Factor.

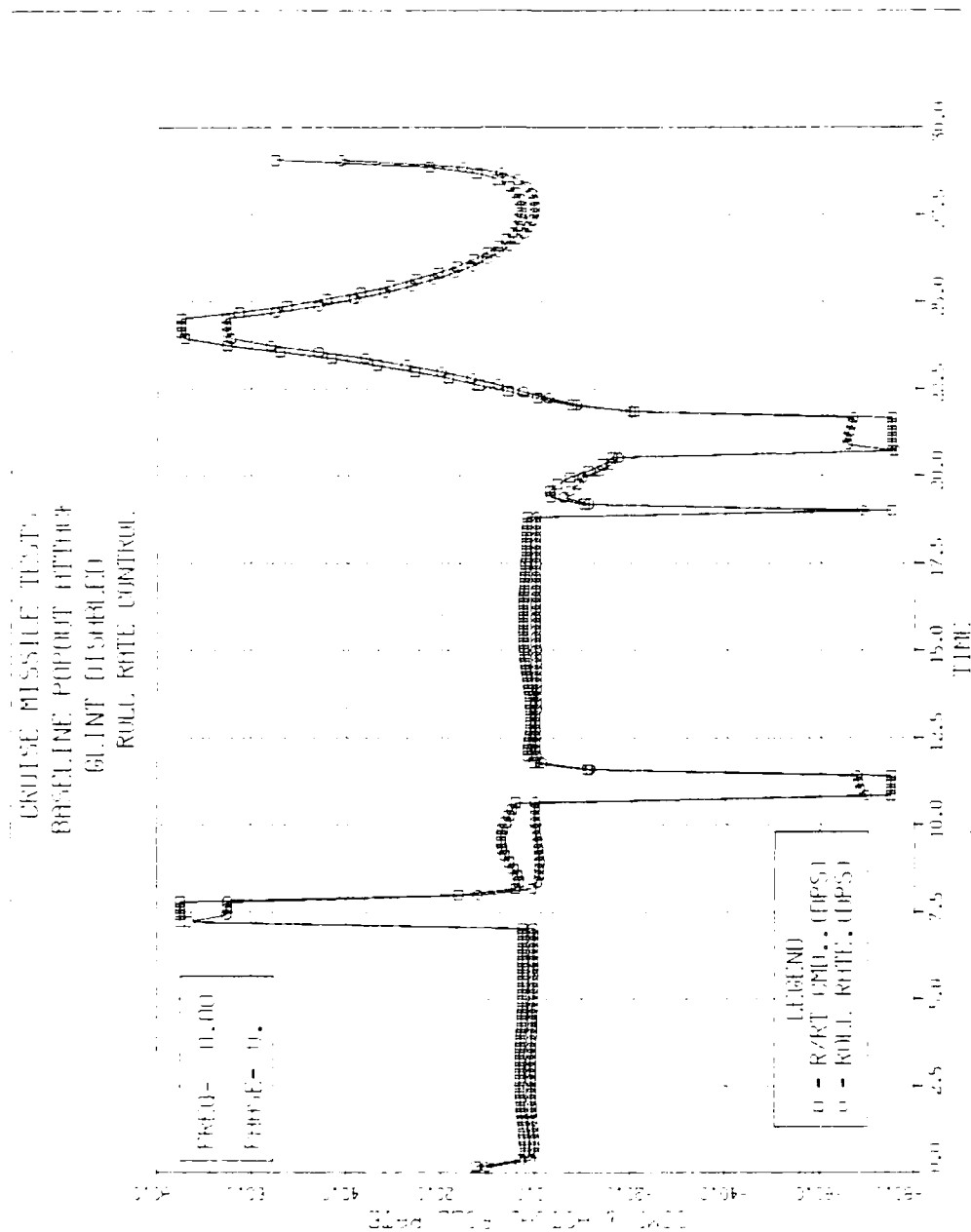


Figure A.24 Baseline - no ECM or GLINT - Roll Rate.

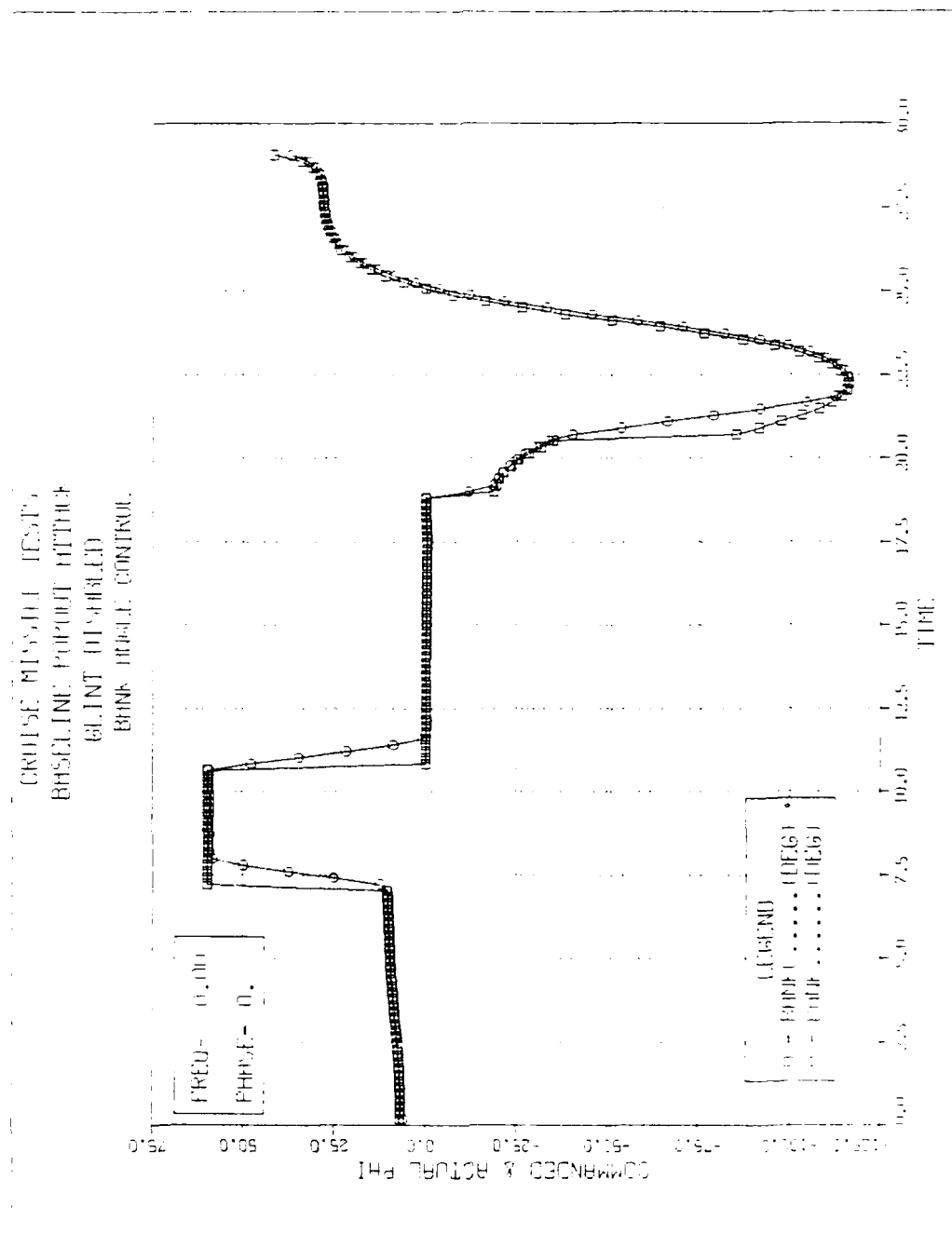


Figure A.25 Baseline - no ECM or GLINT - Bank.

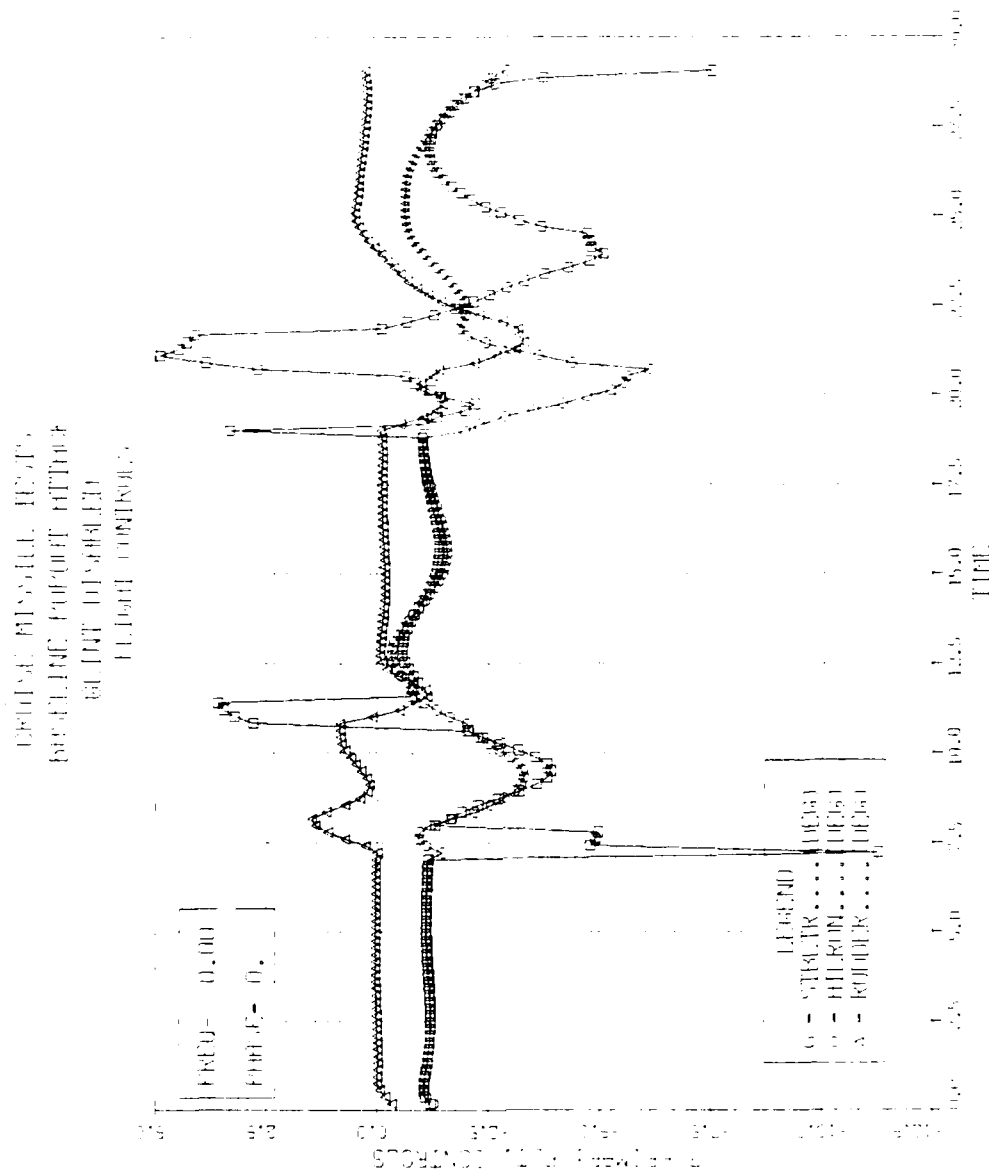


Figure A.26 Baseline - no ECM or GLINT - Controls.

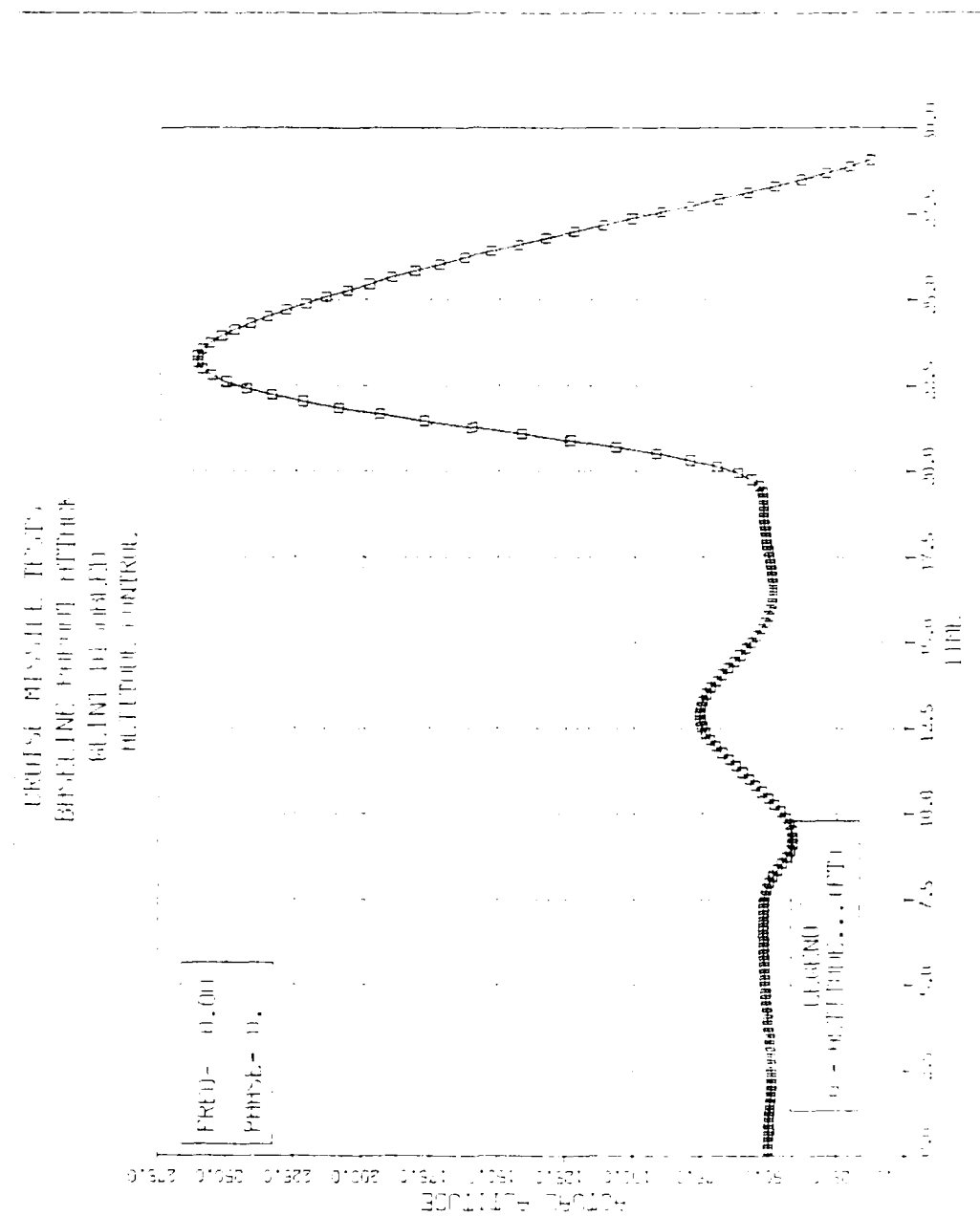
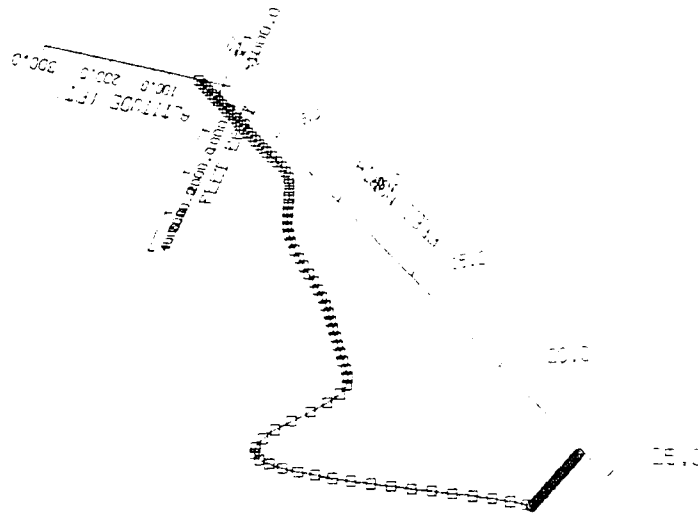


Figure A.27 Baseline - no ECM or GLINT - Altitude.

0-00000

0-00000



65

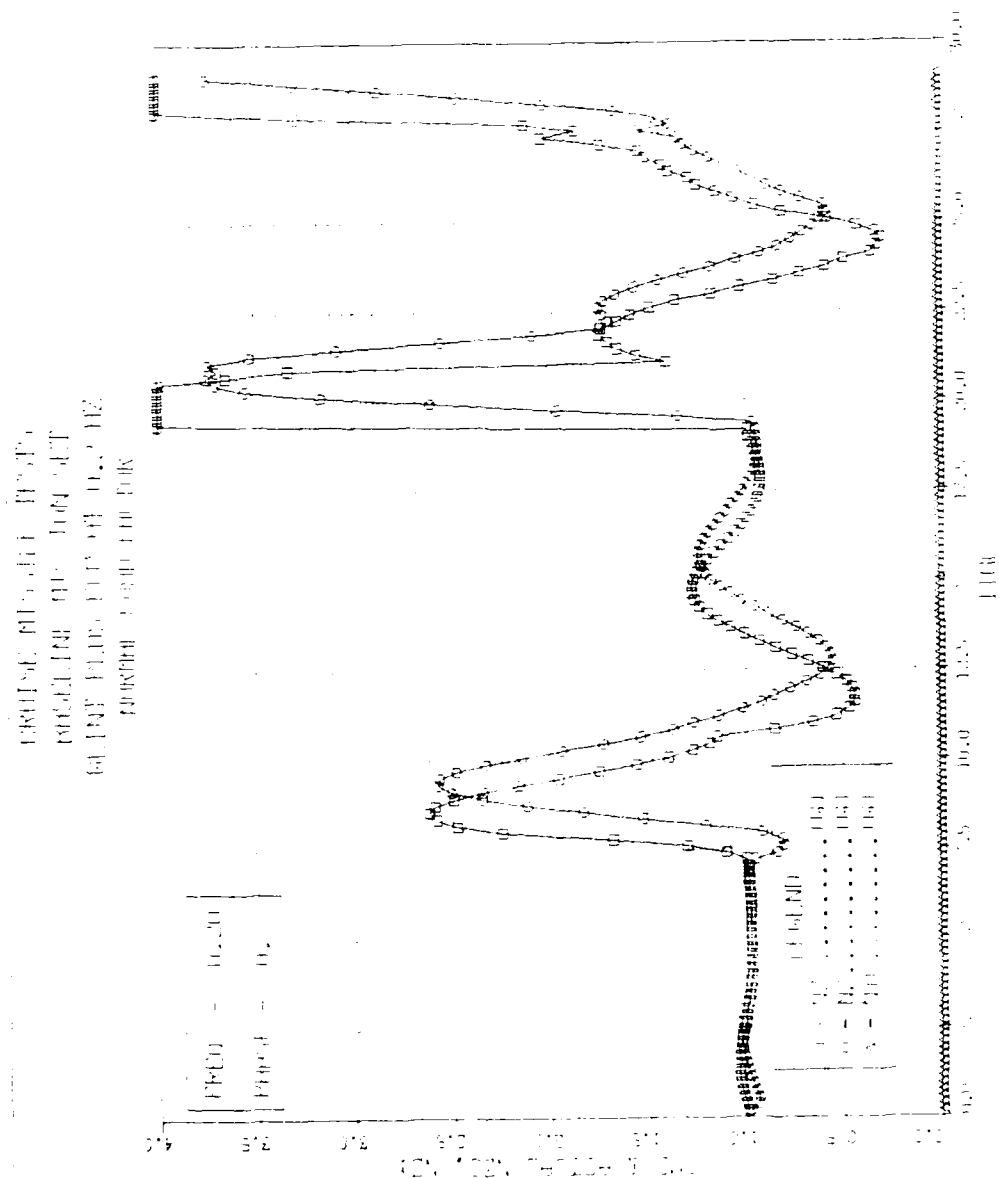


Figure A.29 Baseline with GLINT & ECM - Load Factor.

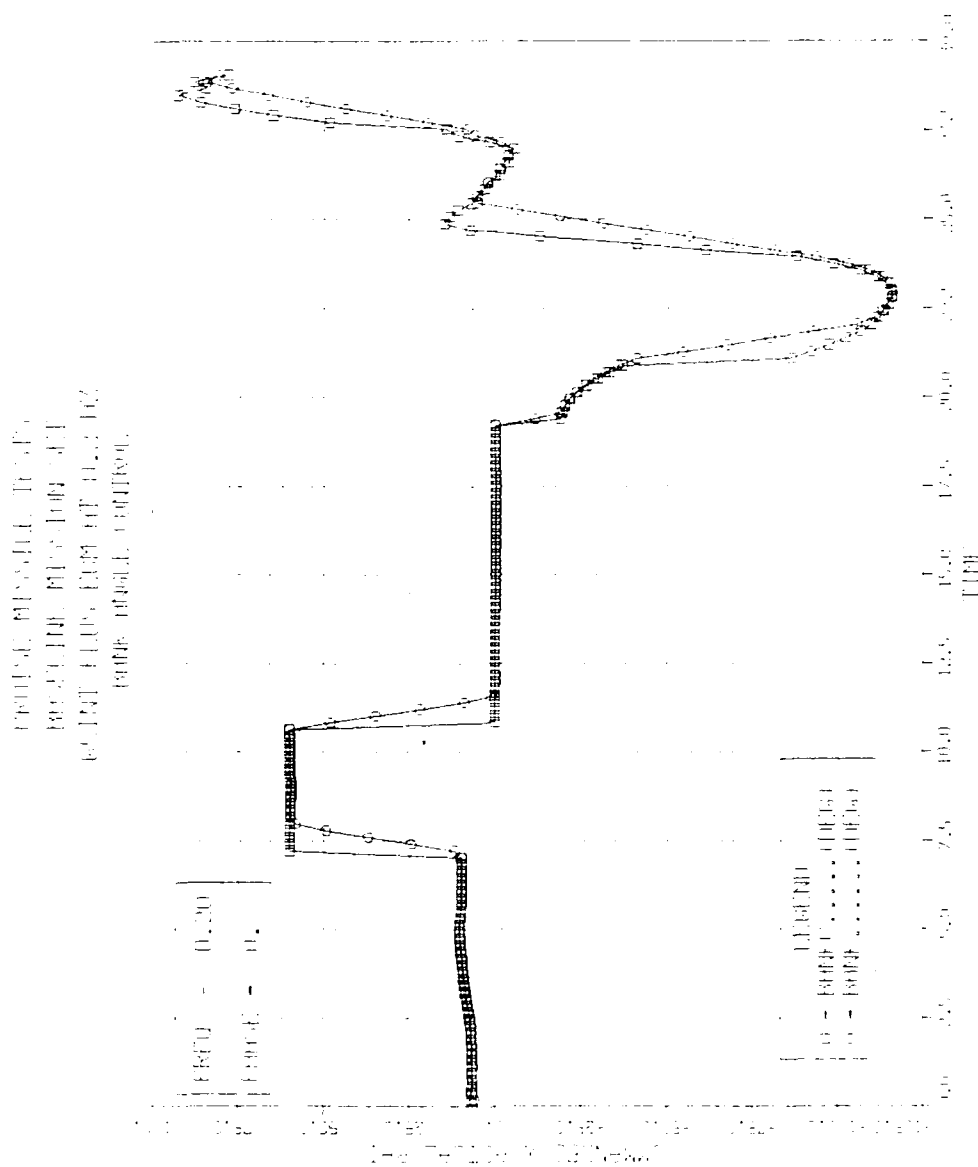


Figure A.30 Baseline with GLINT & ECM - Bank.

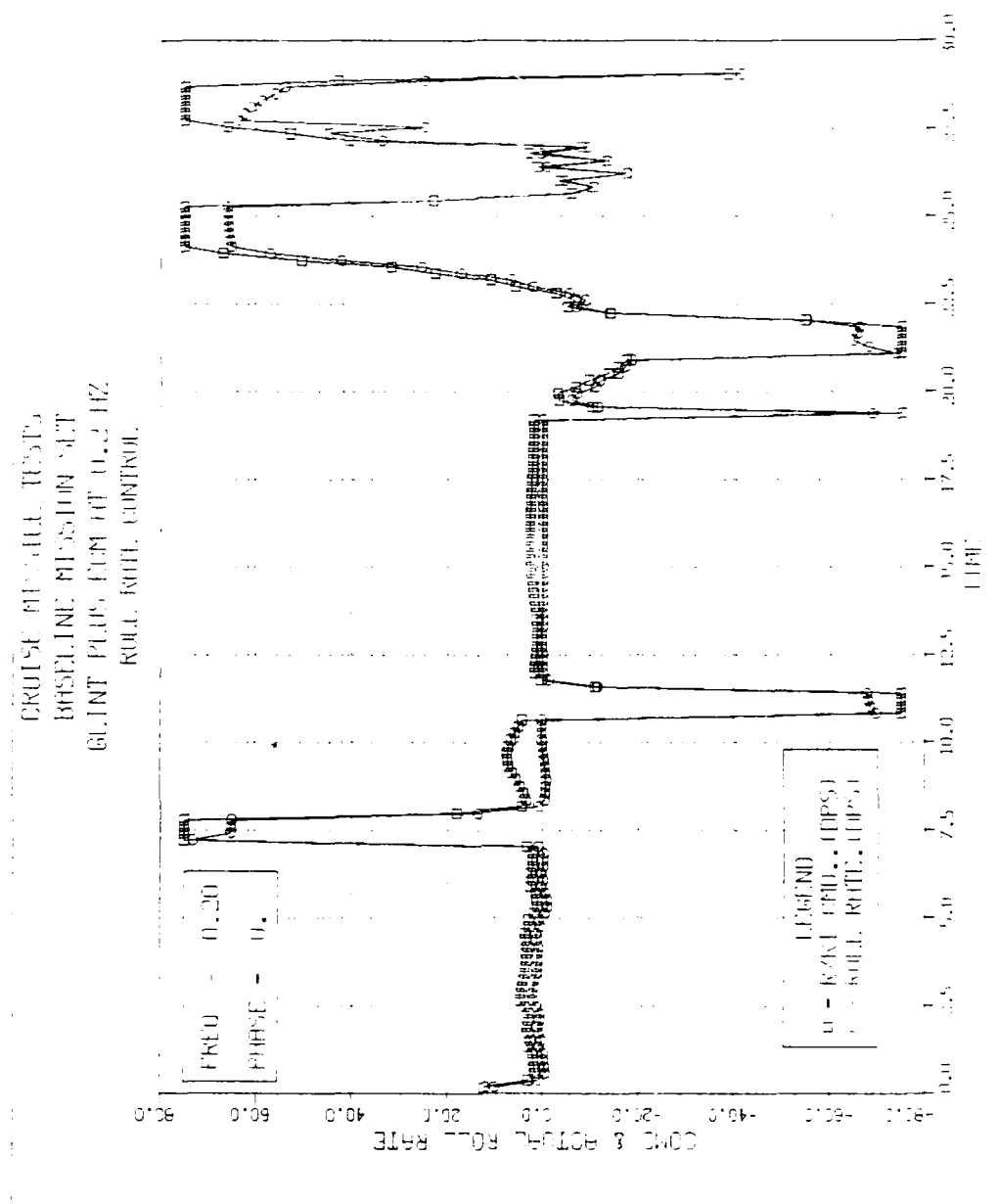


Figure A.31 Baseline with GLINT & ECM - Roll Rate.

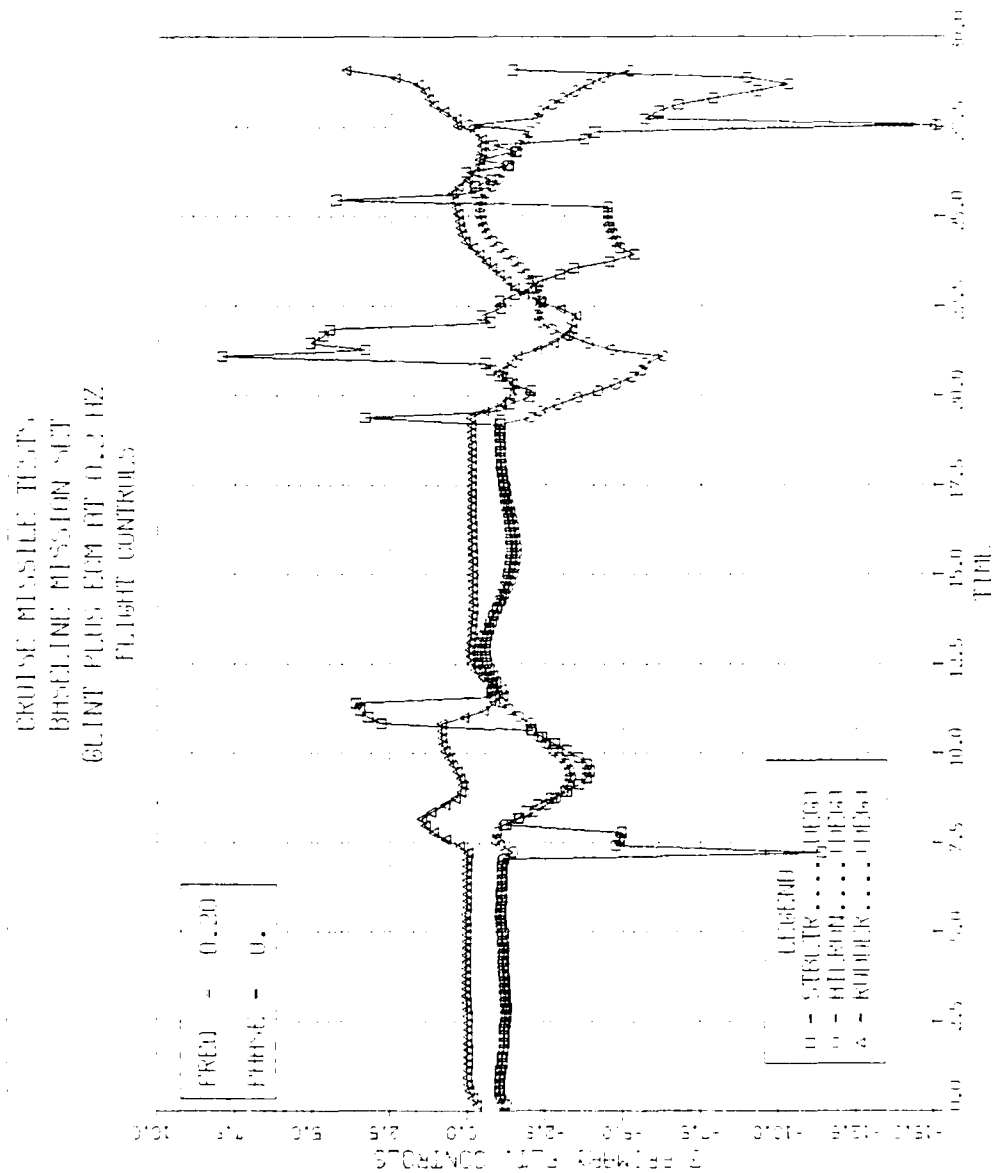


Figure A.32 Baseline with GLINT & ECM - Controls.

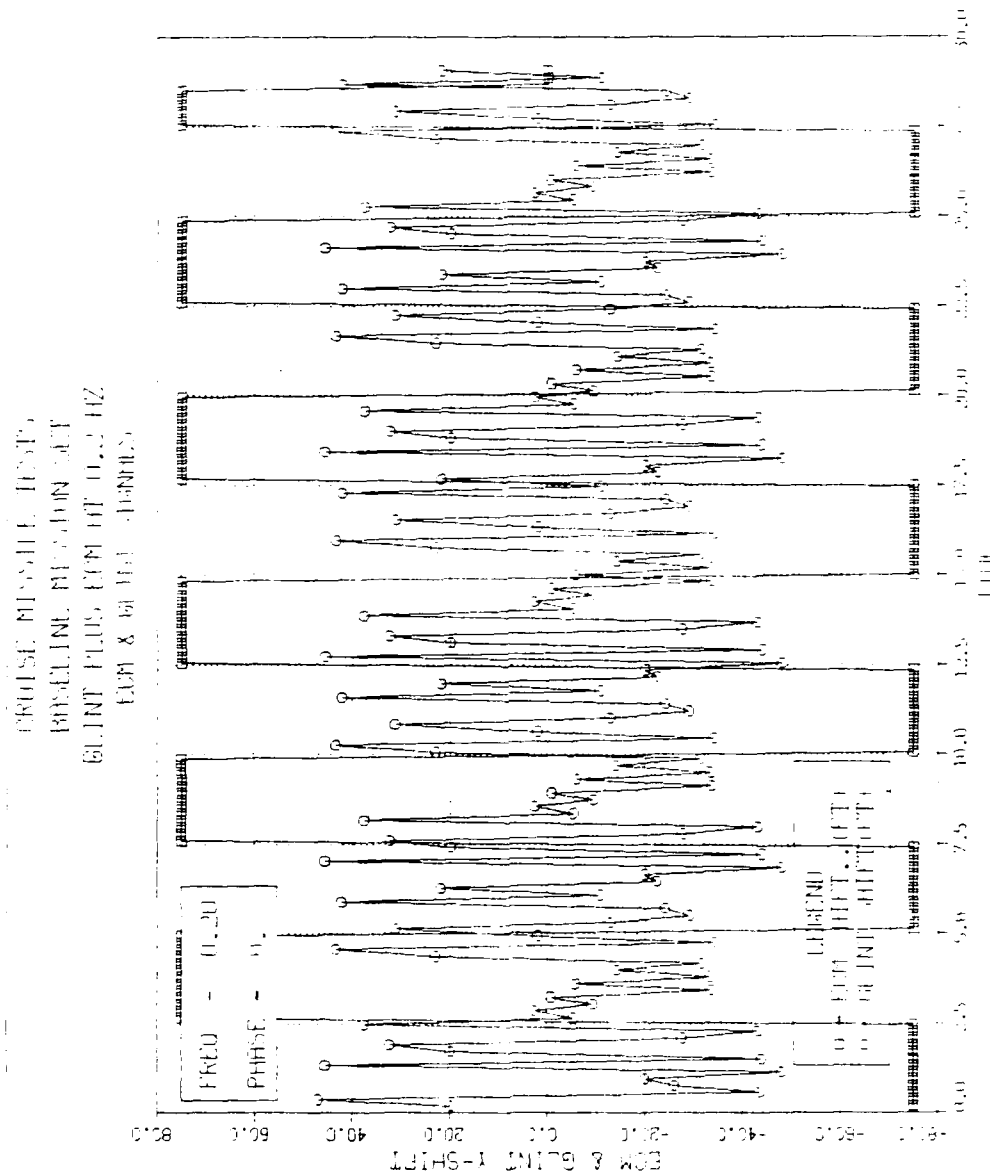


Figure A.33 Baseline with GLINT & ECM - ECM & GLINT.

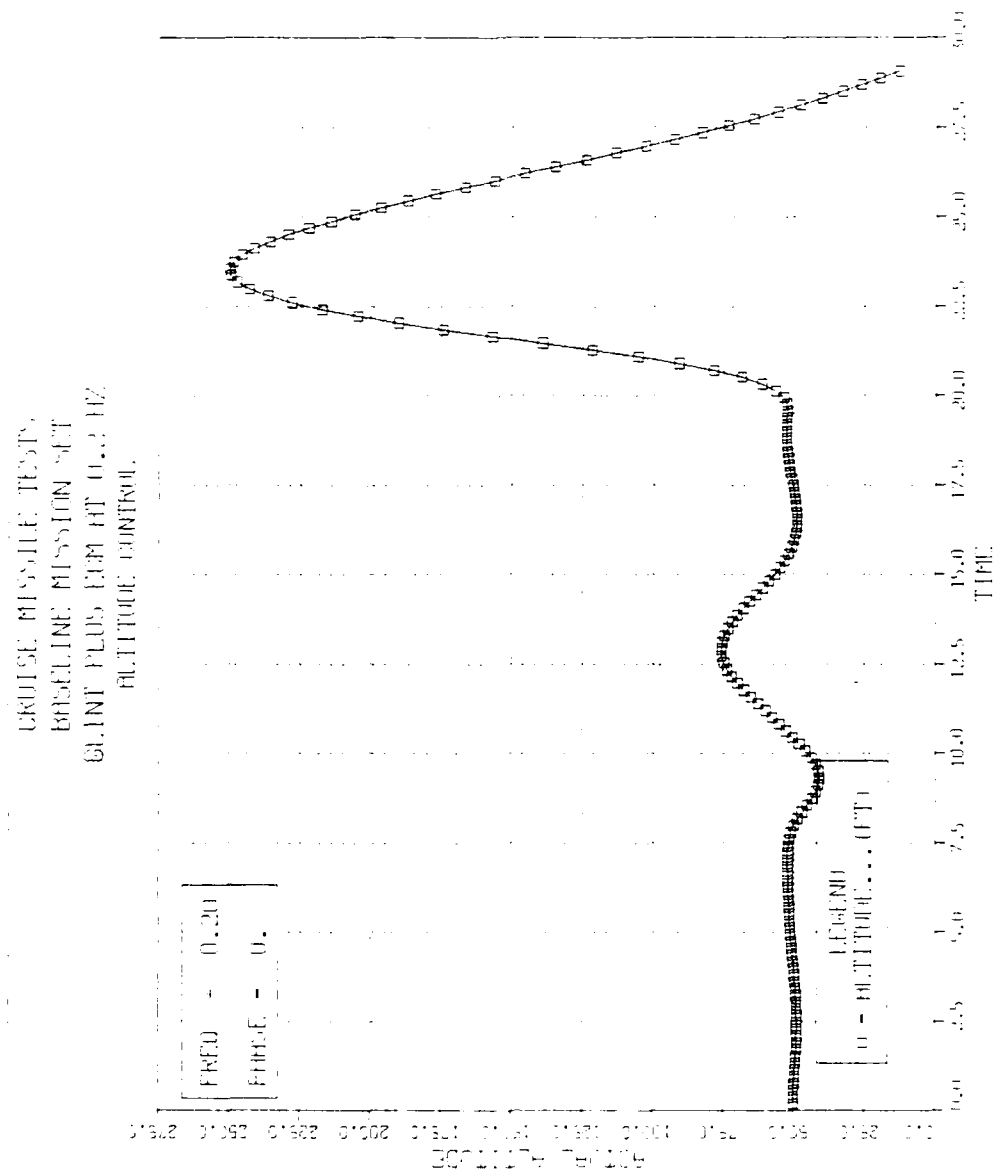


Figure A.34 Baseline with GLINT & ECM - Altitude.

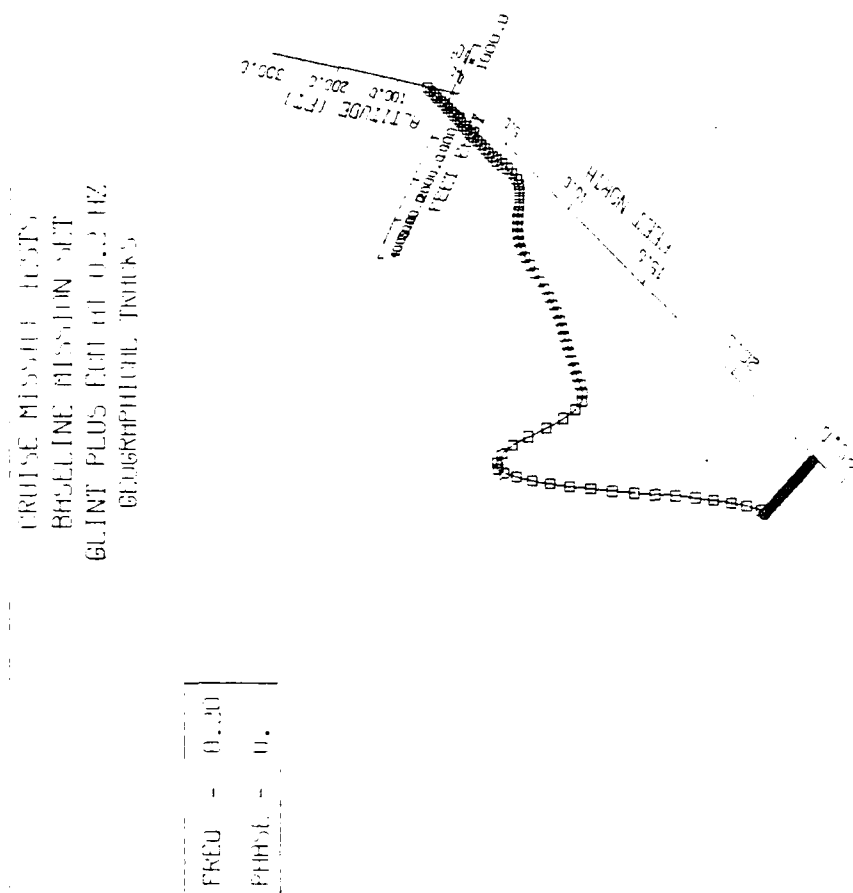


Figure A.35 Baseline with GLINT & ECM - Geo Plot.

BASELINE SCAN RESULTS

MISS DISTANCES

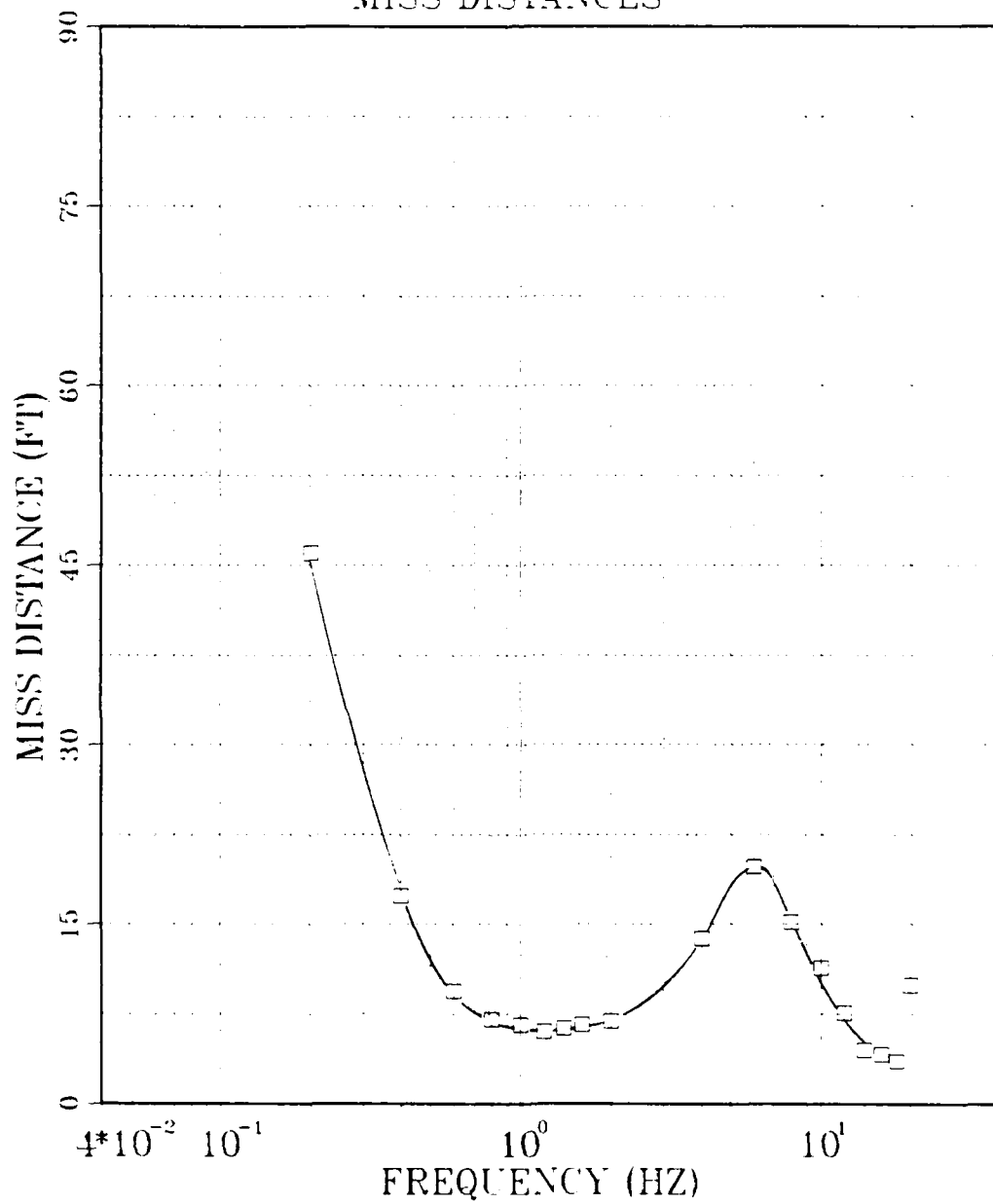


Figure A.36 Mean Miss Distances - Baseline.

CONFIGURATION II SCANS

MISS DISTANCES

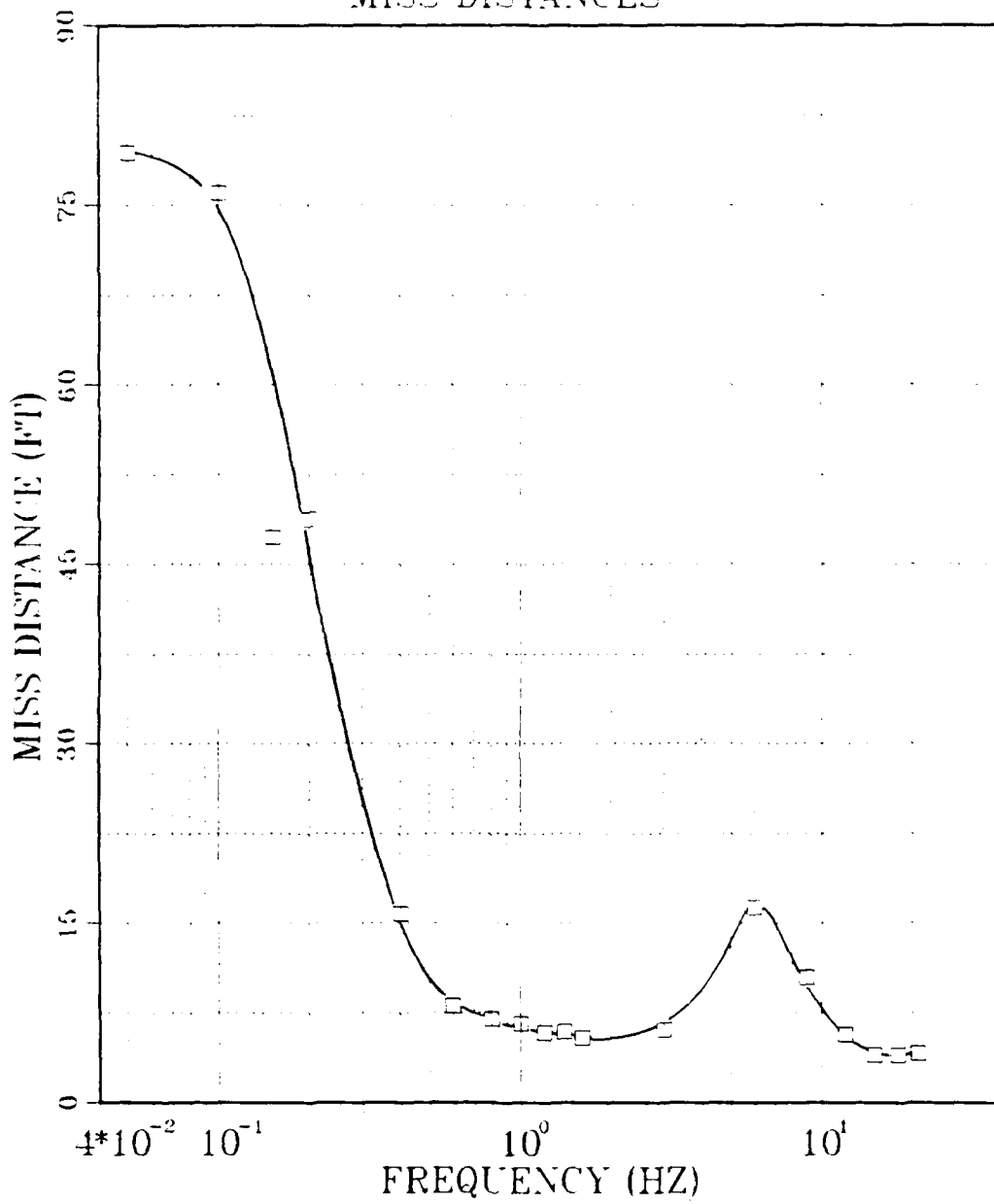


Figure A.37 Mean Miss Distances - Configuration II.

CONFIGURATION III SCANS

MISS DISTANCES

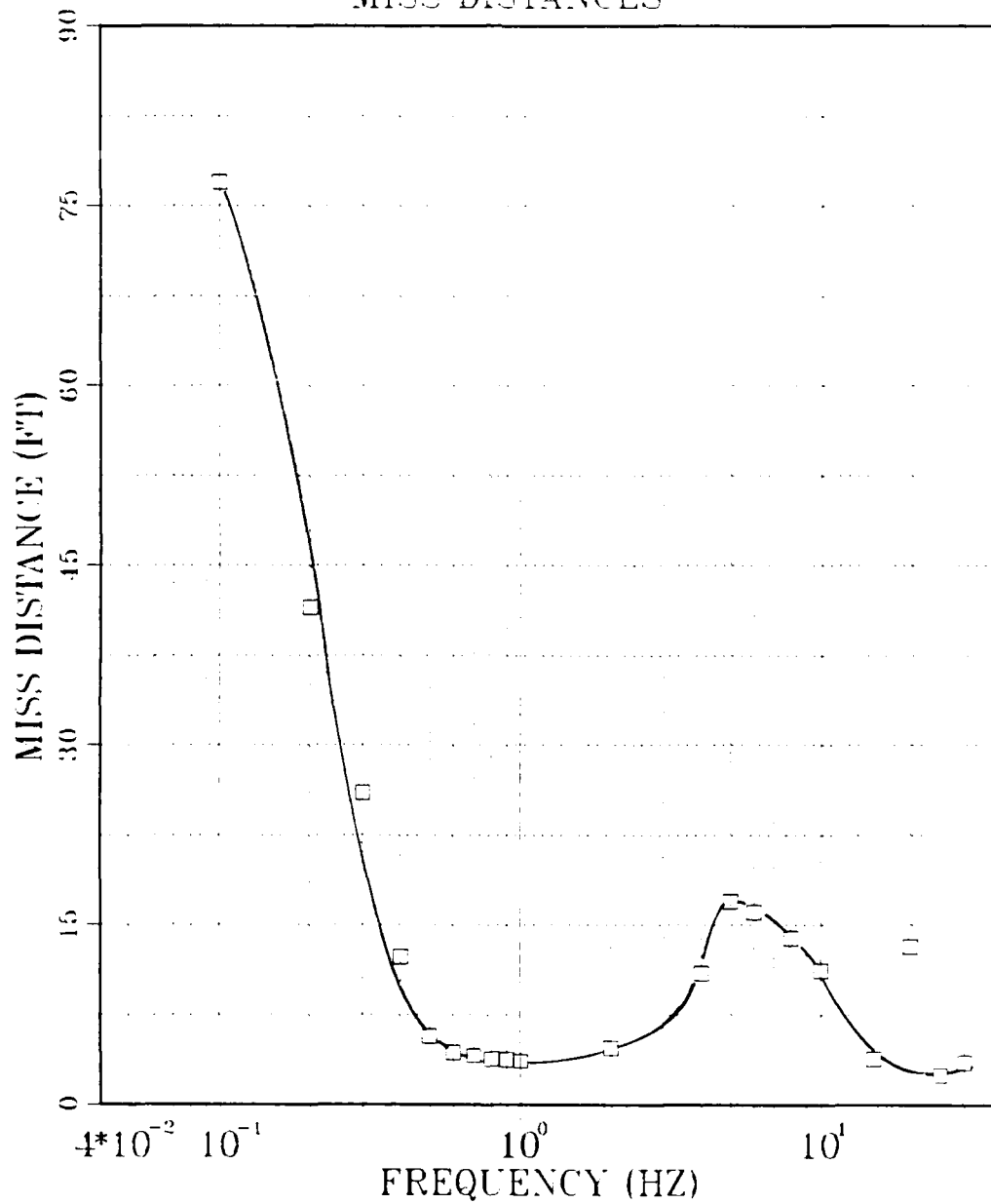


Figure A.38 Mean Miss Distances - Configuration III.

CONFIGURATION IV SCANS

MISS DISTANCES

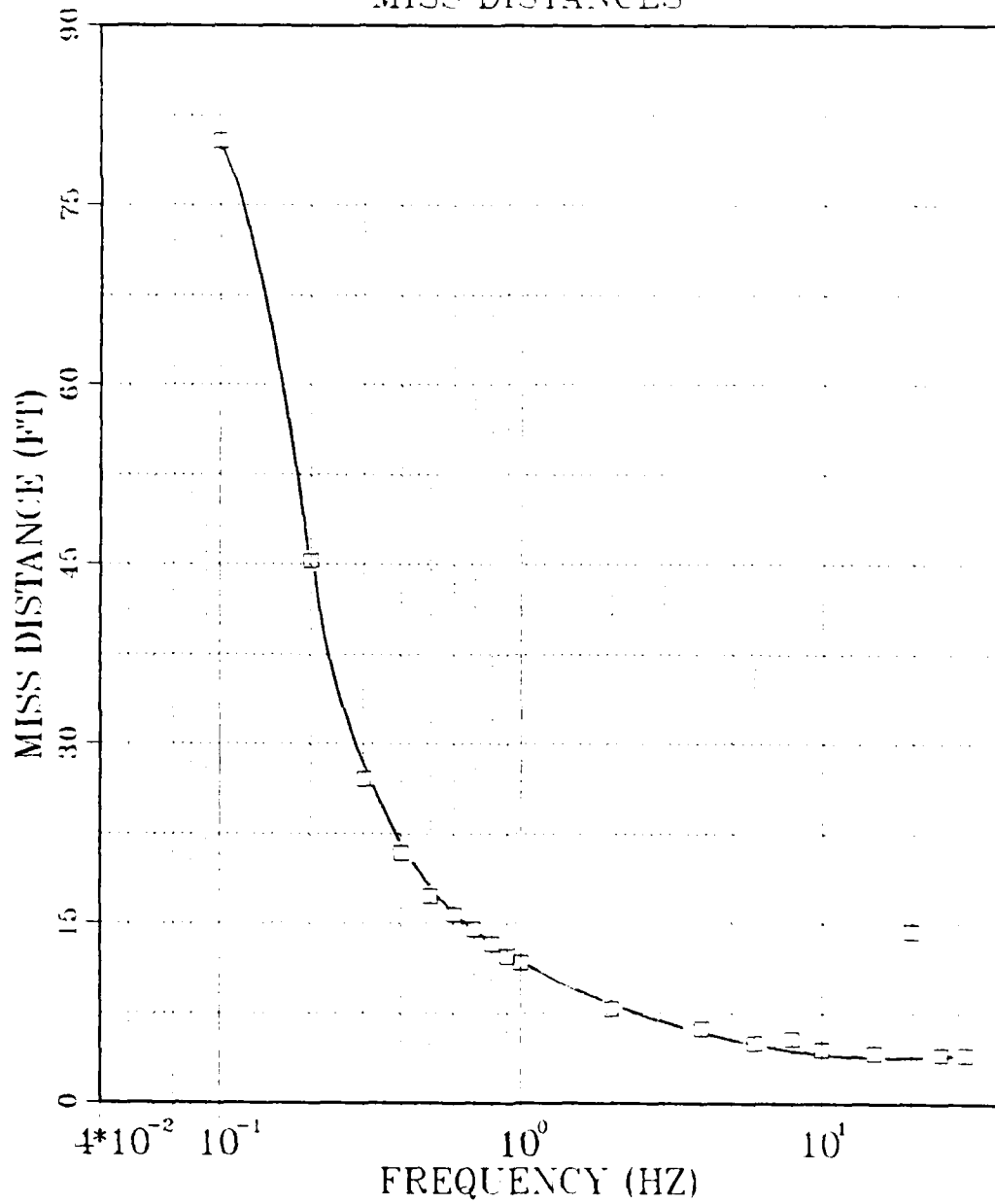


Figure A.39 Mean Miss Distances - Configuration IV.

BASELINE SCAN RESULTS

AUTOPILOT ERRORS

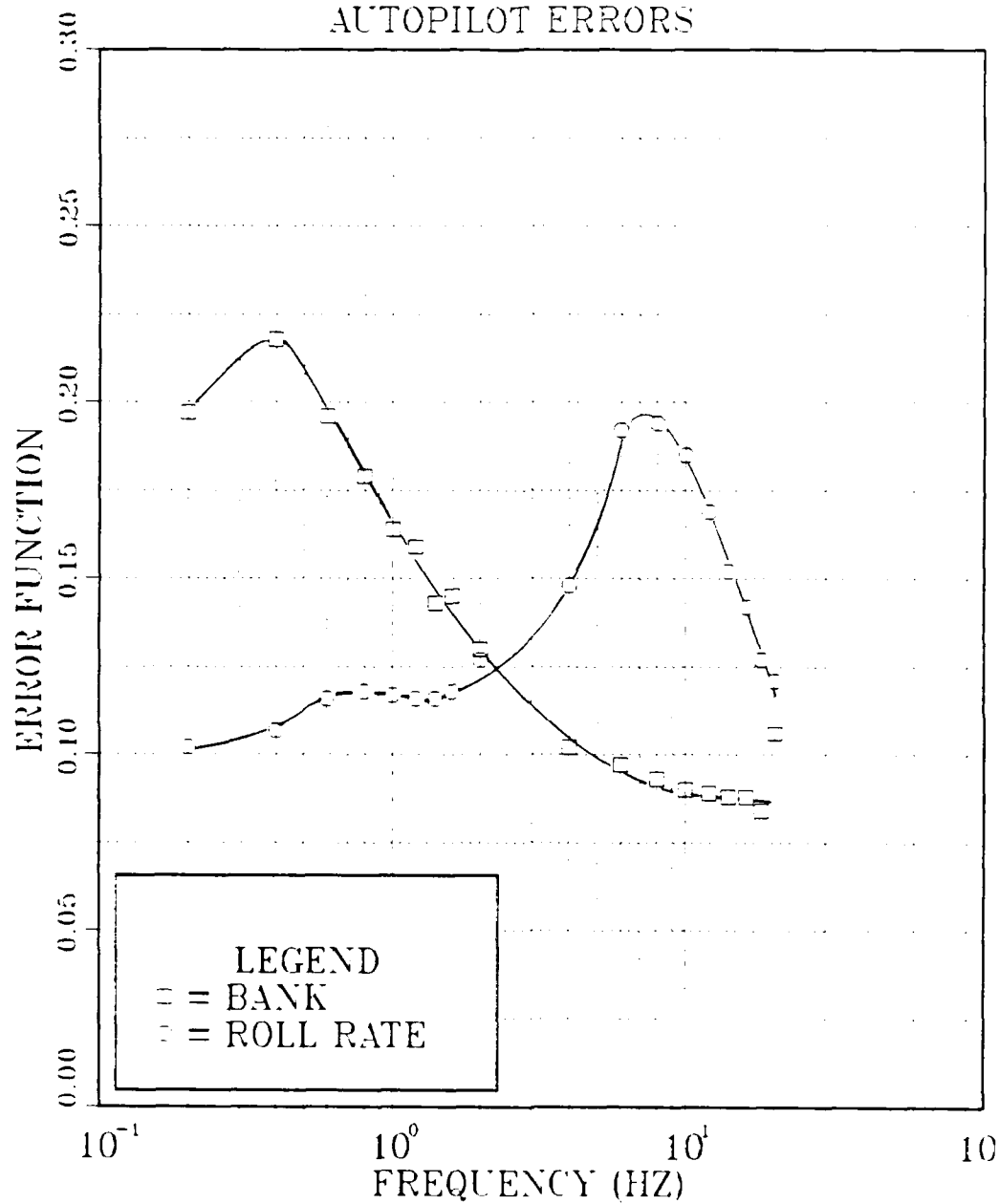


Figure A.40 Autopilot Errors - Paseline.

CONFIGURATION II SCANS

AUTOPILOT ERRORS

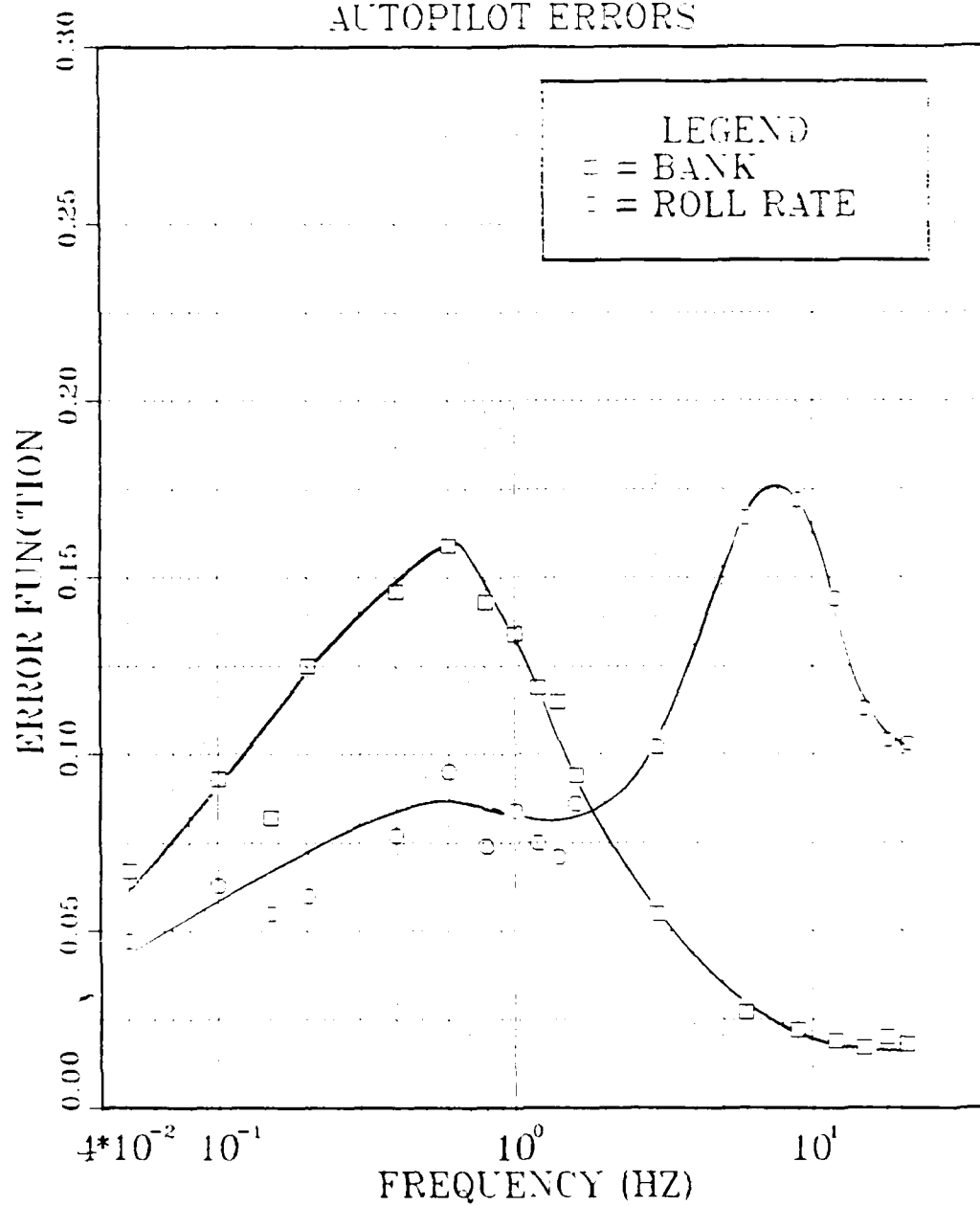


Figure A.41 Autopilot Errors - Configuration II.

CONFIGURATION III SCANS

AUTOPILOT ERRORS

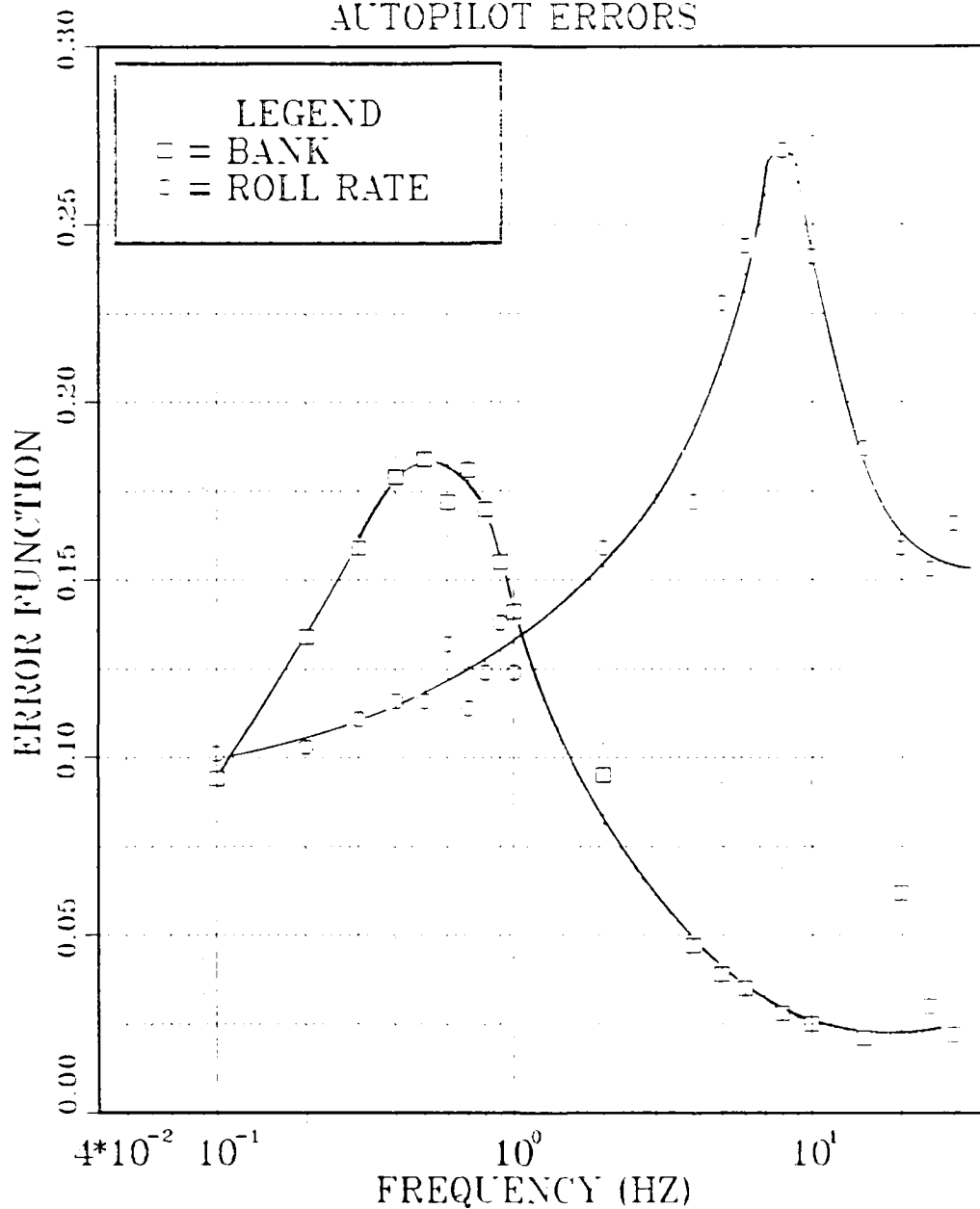


Figure A.42 Autopilot Errors - Configuration III.

CONFIGURATION IV SCANS

AUTOPILOT ERRORS

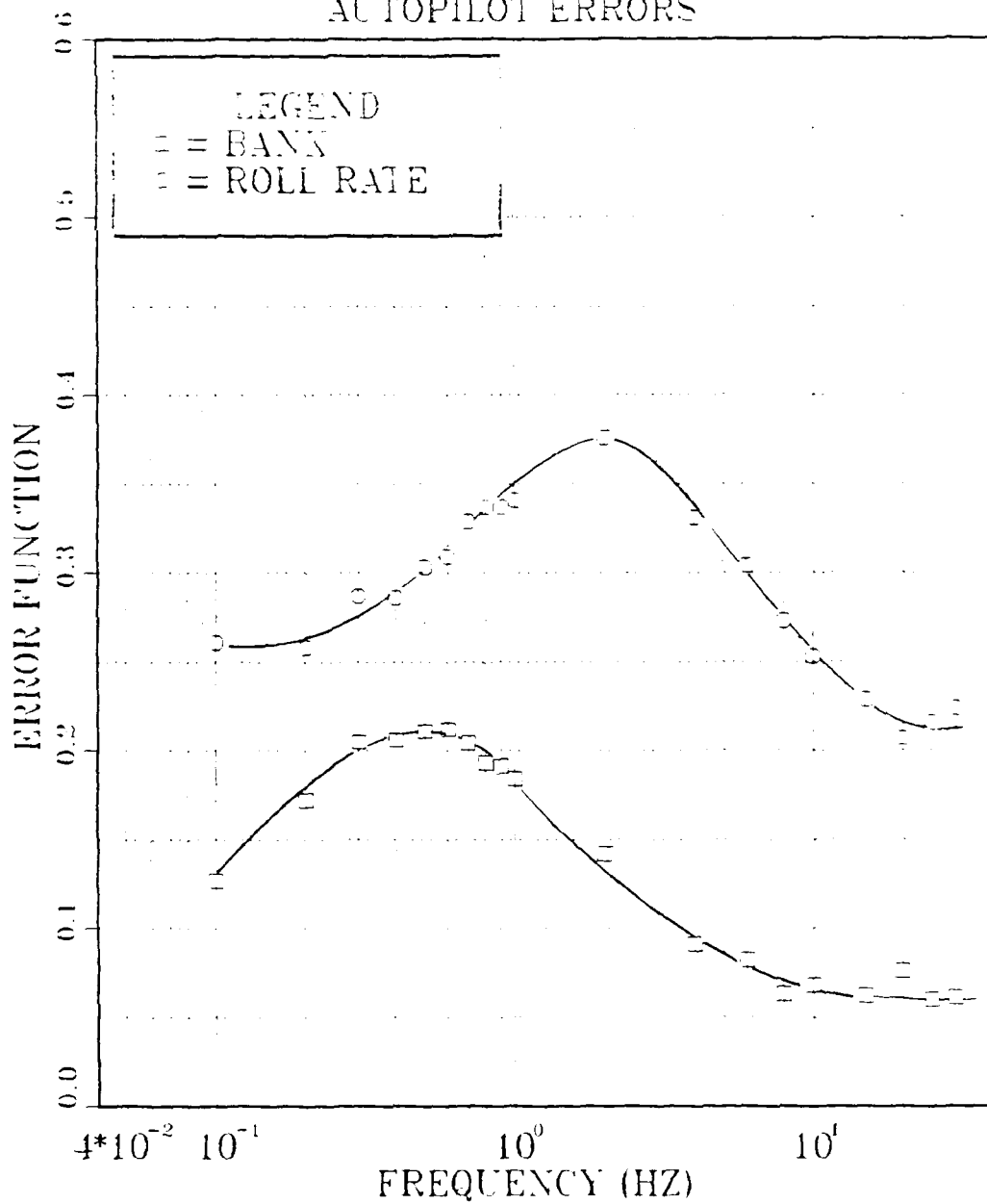


Figure A.43 Autopilot Errors - Configuration IV.

BASELINE SCAN RESULTS

TRACKING ERRORS

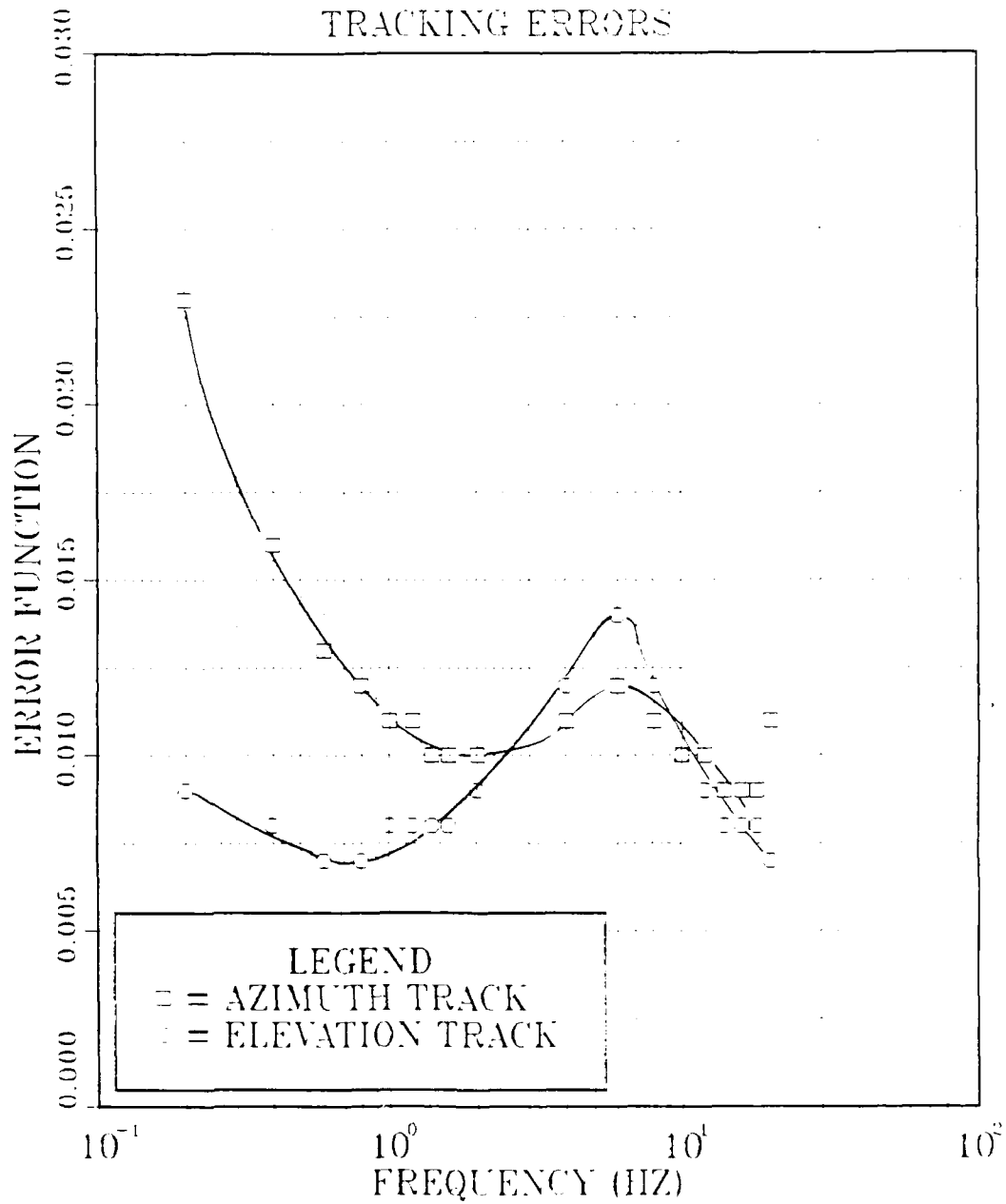


Figure A.44 Tracking Errors - Baseline.

CONFIGURATION II SCANS

TRACKING ERRORS

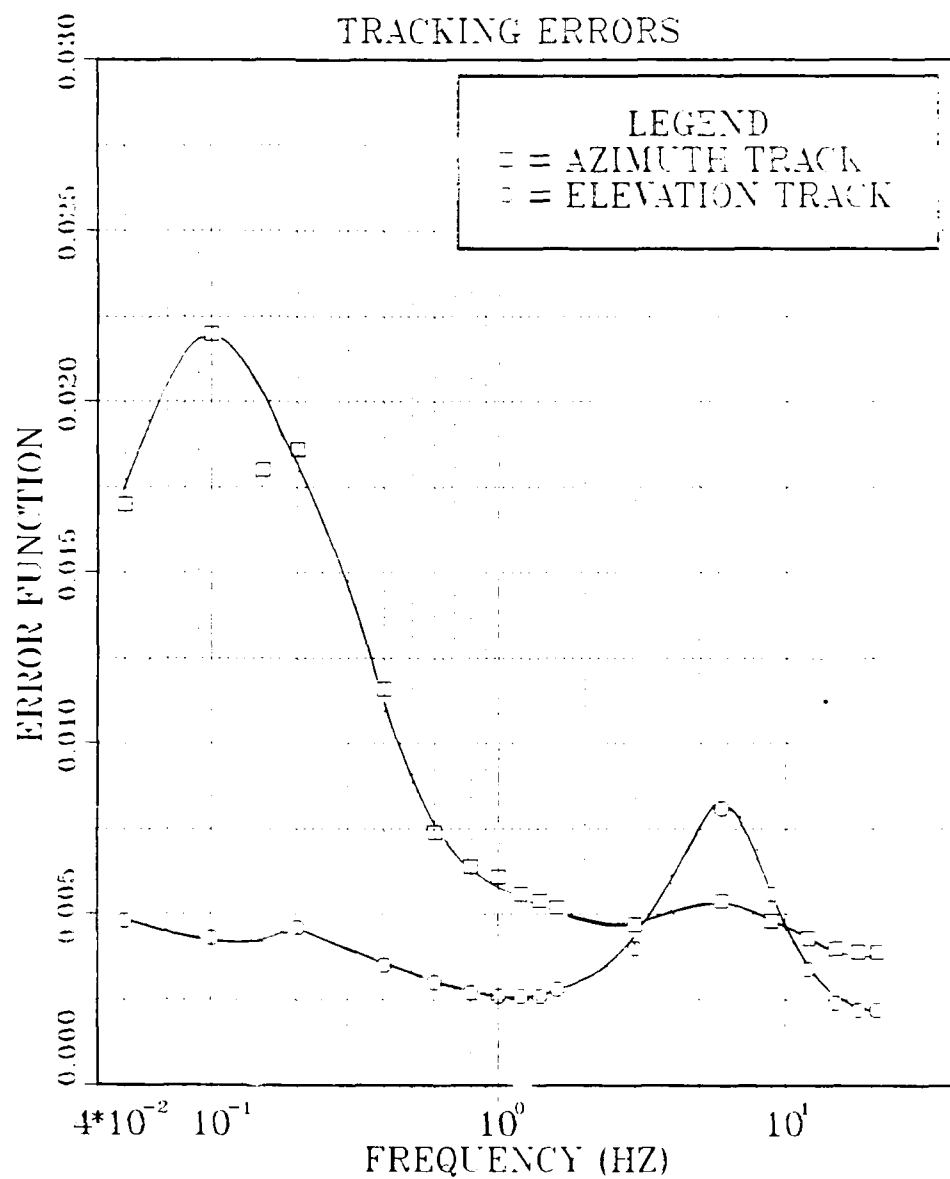


Figure A.45 Tracking Errors - Configuration II.

CONFIGURATION III SCANS

TRACKING ERRORS

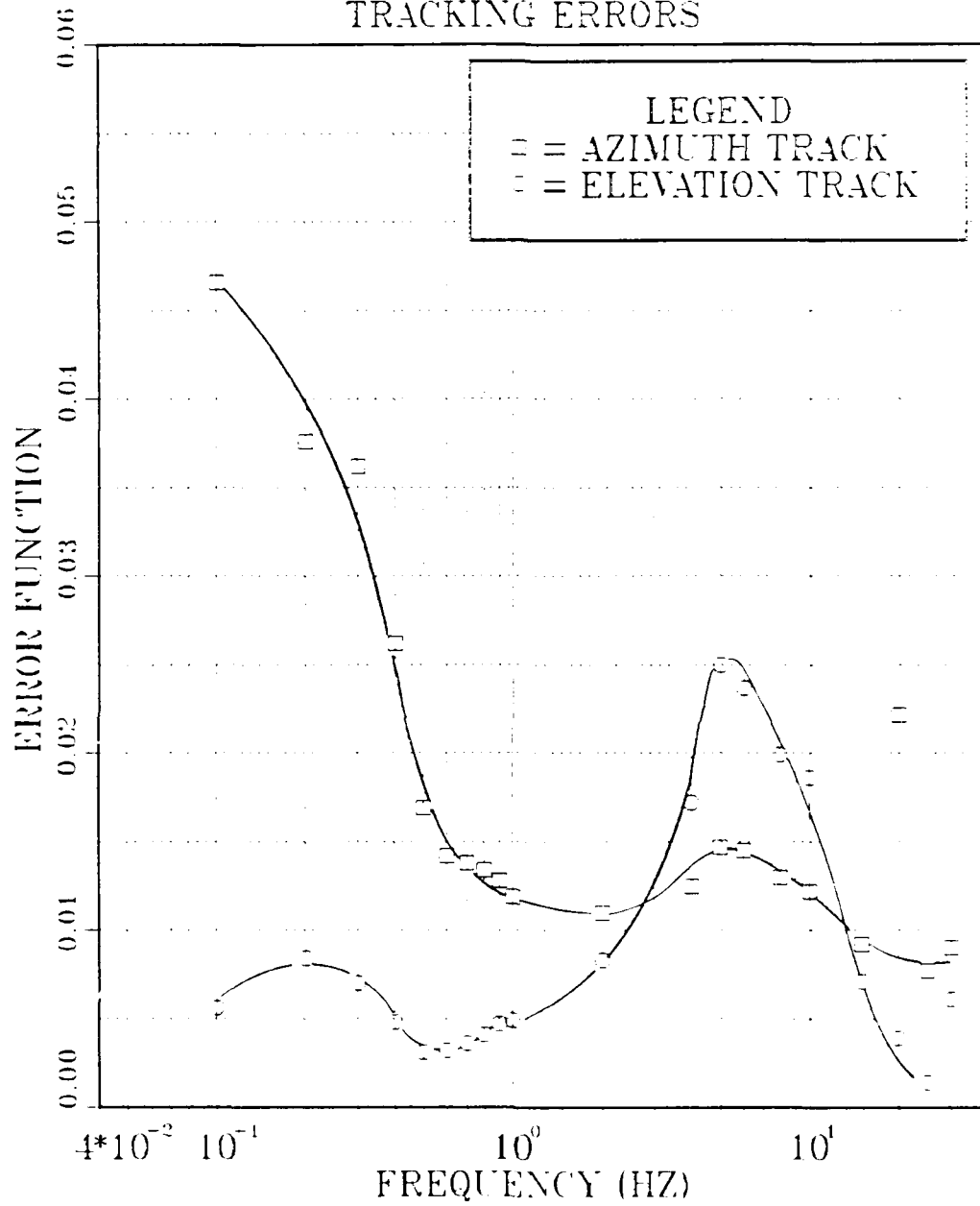


Figure A.46 Tracking Errors - Configuration III.

CONFIGURATION IV SCANS

TRACKING ERRORS

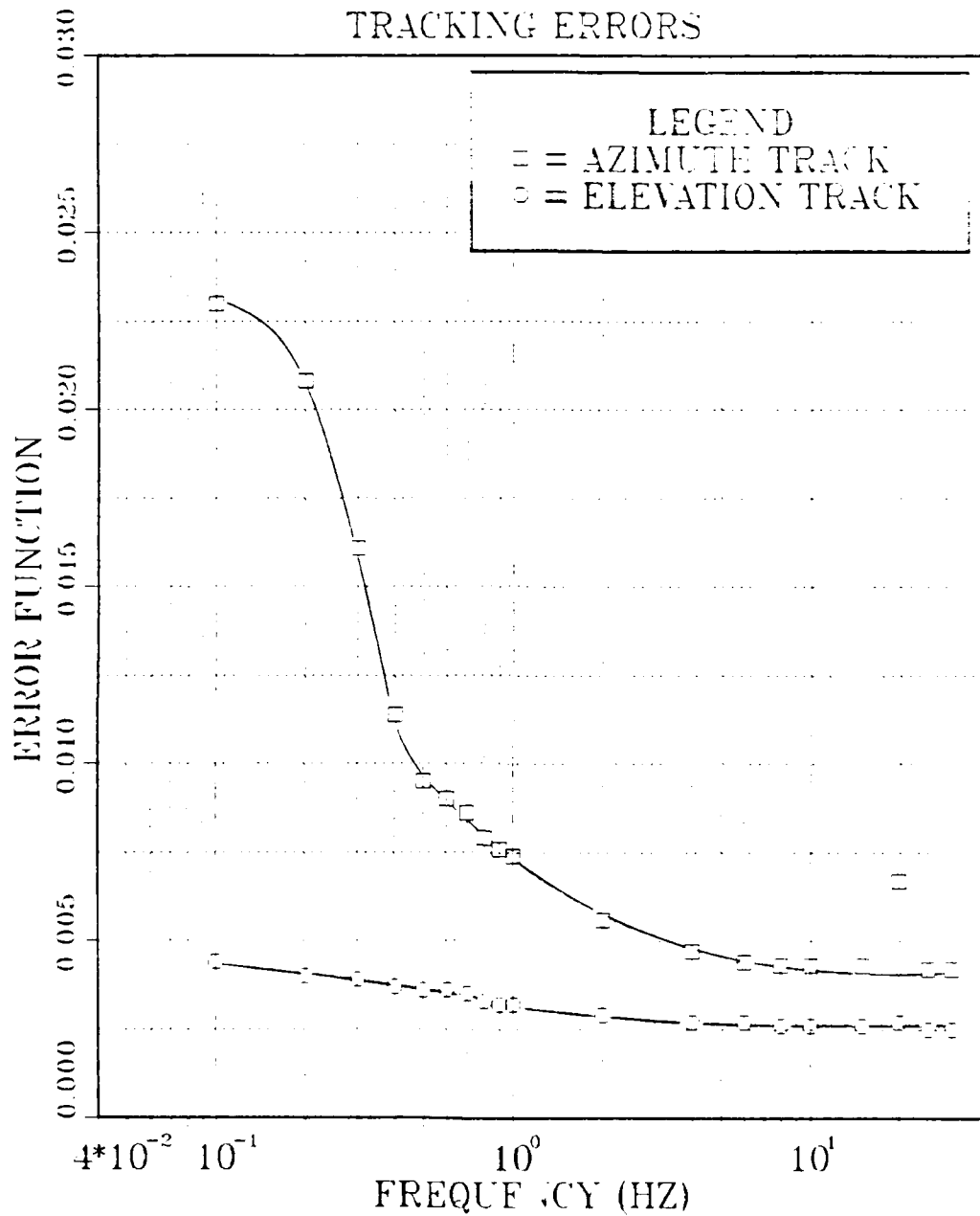


Figure A.47 Tracking Errors - Configuration IV.

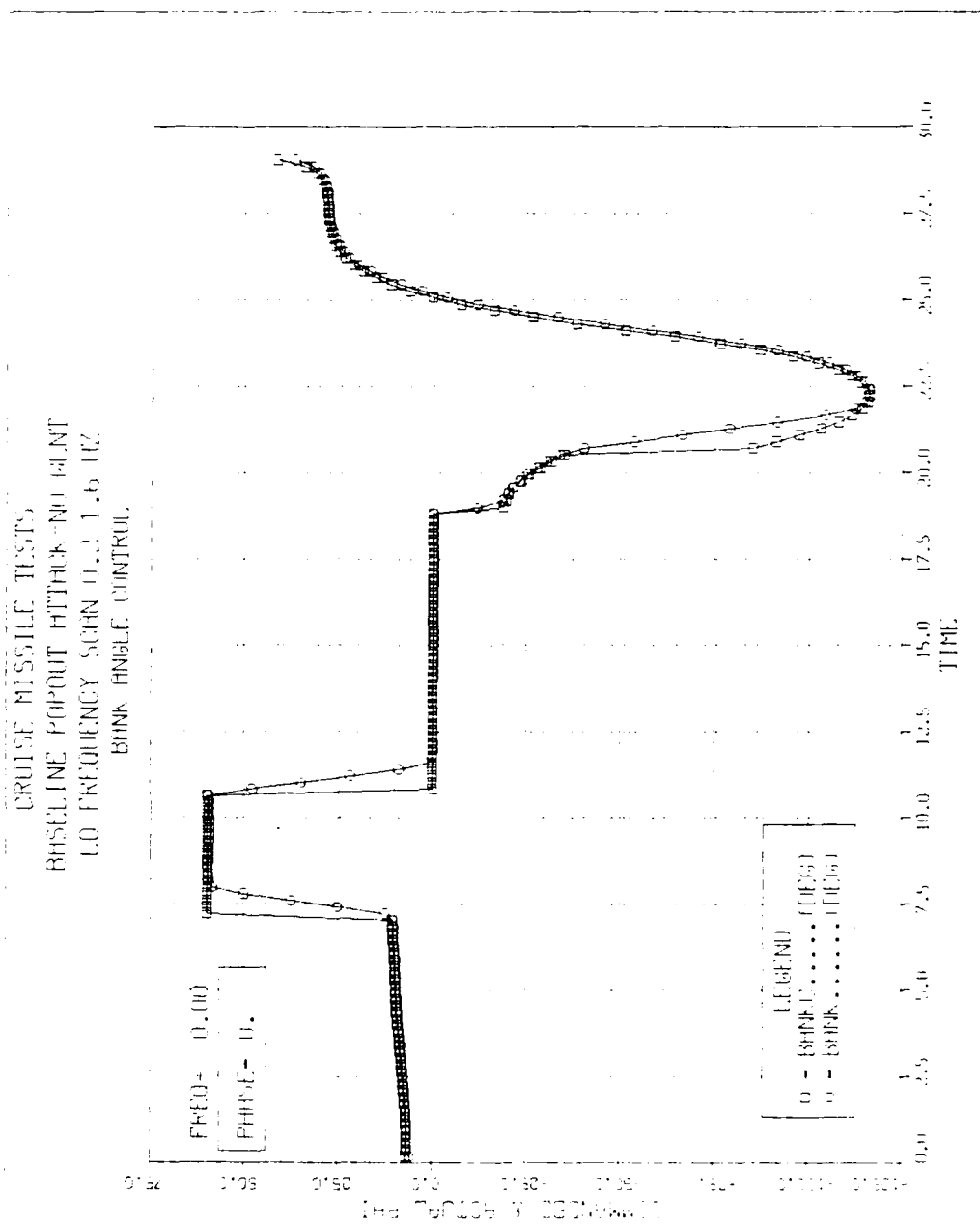


Figure A.48 Baseline/ECM Preq = 0.0 Hz - Bank.

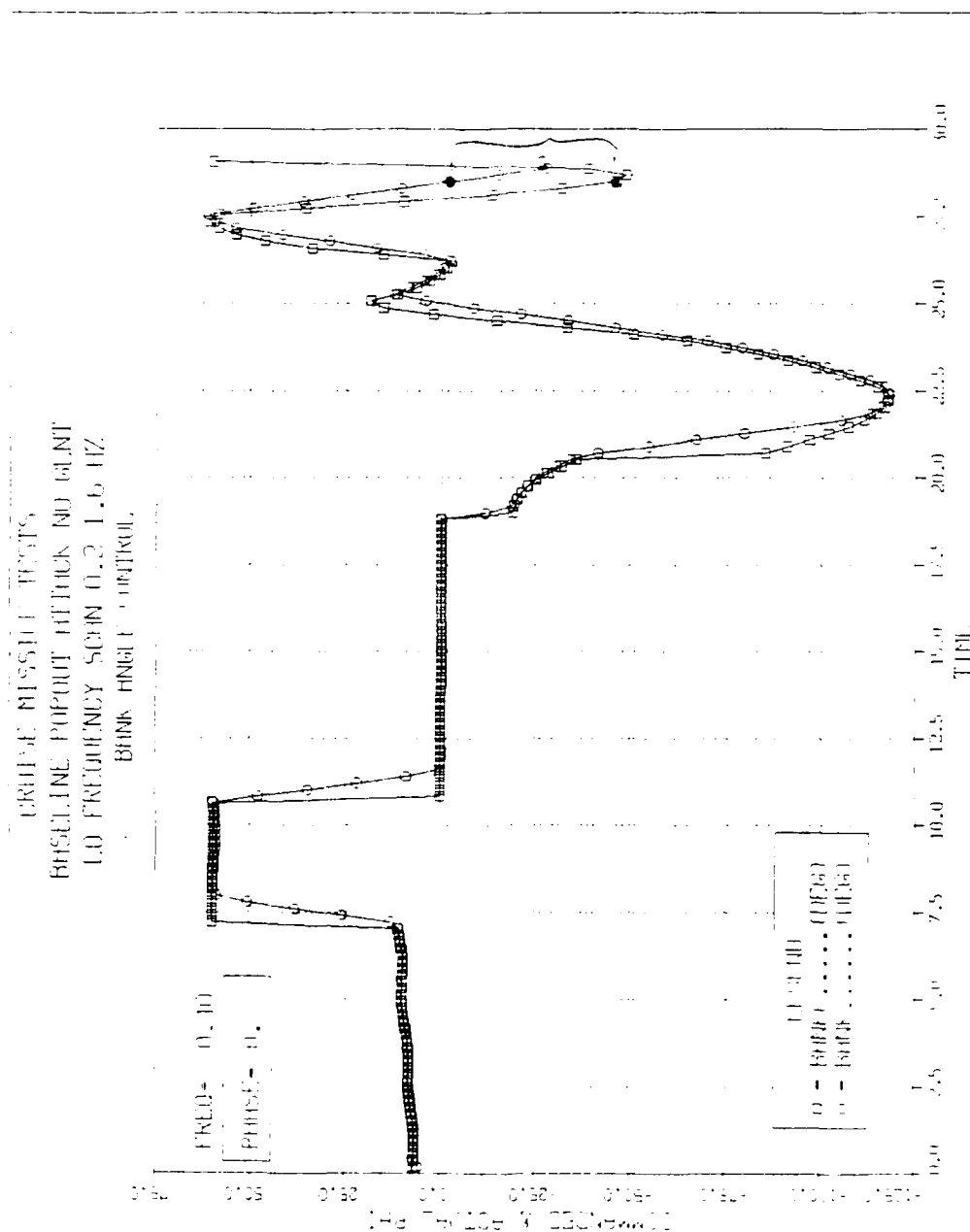


Figure A.49 Baseline/ECM Freq = 0.4 Hz - Bank.

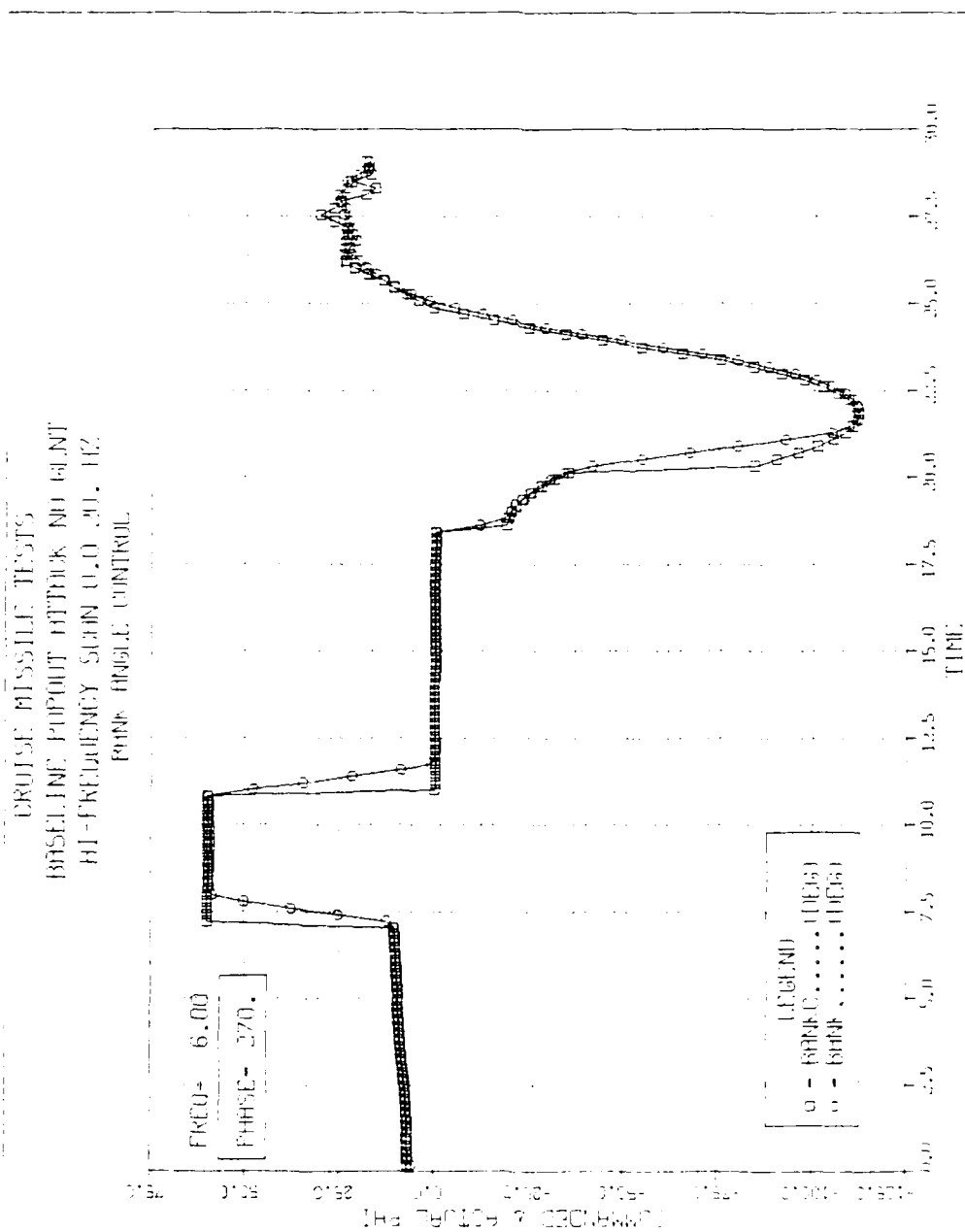


Figure A.50 Baseline/ECM Freq = 6.0 Hz - Bank.

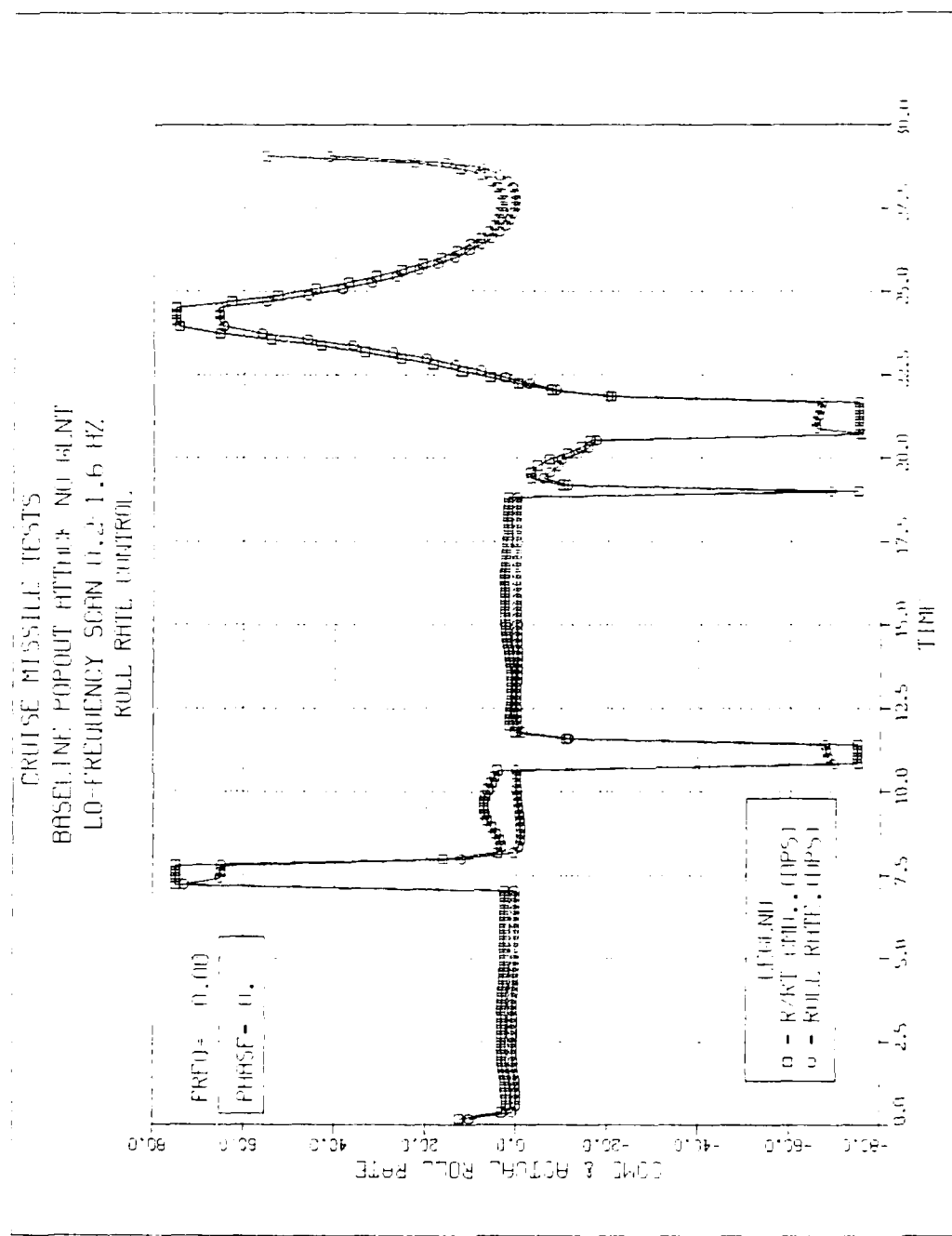


Figure A.51 Baseline/ECM Freq = 0.0 Hz - Roll Rate.

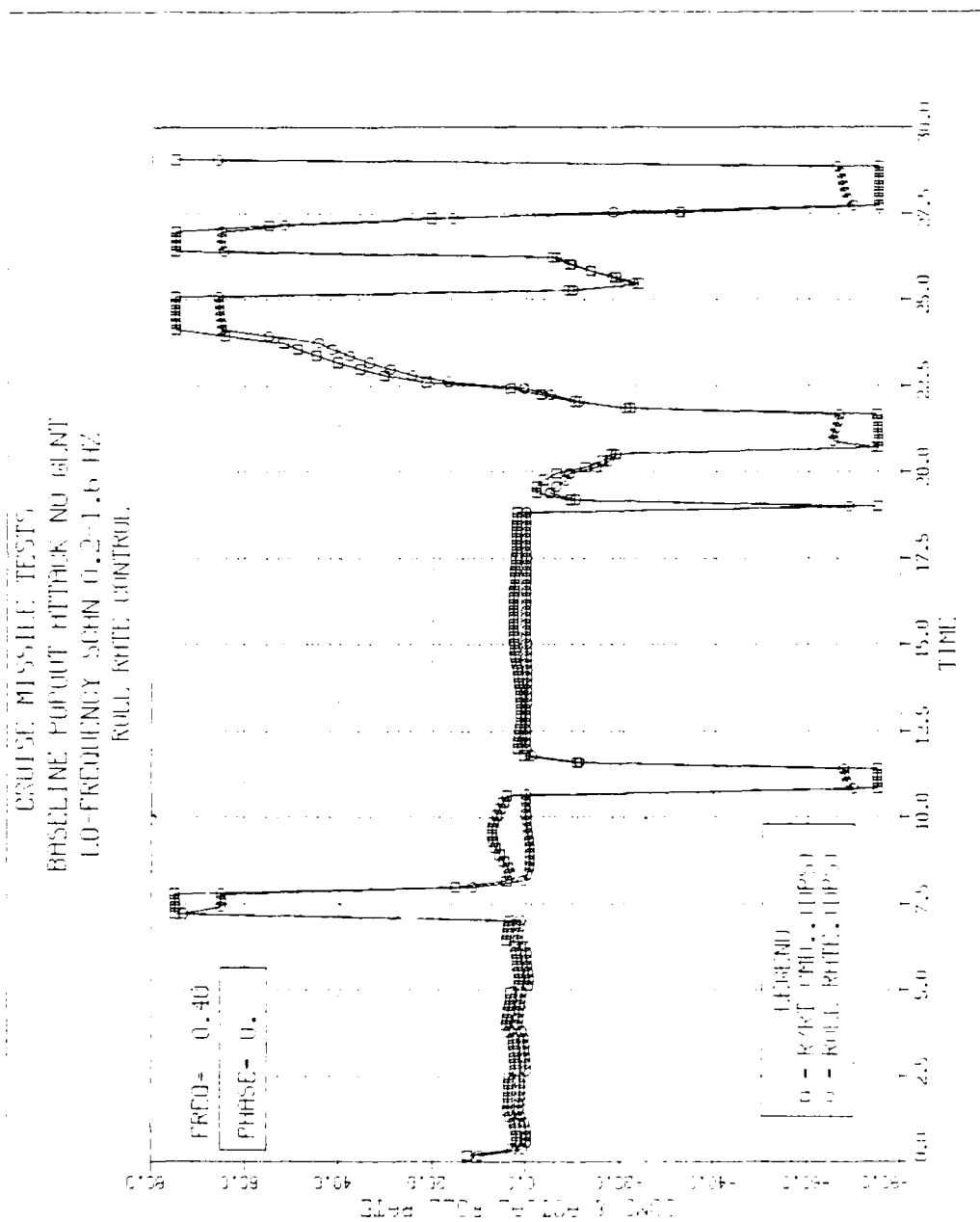


Figure A.52 Baseline/ECM Freq = 0.4 Hz - Roll Rate.

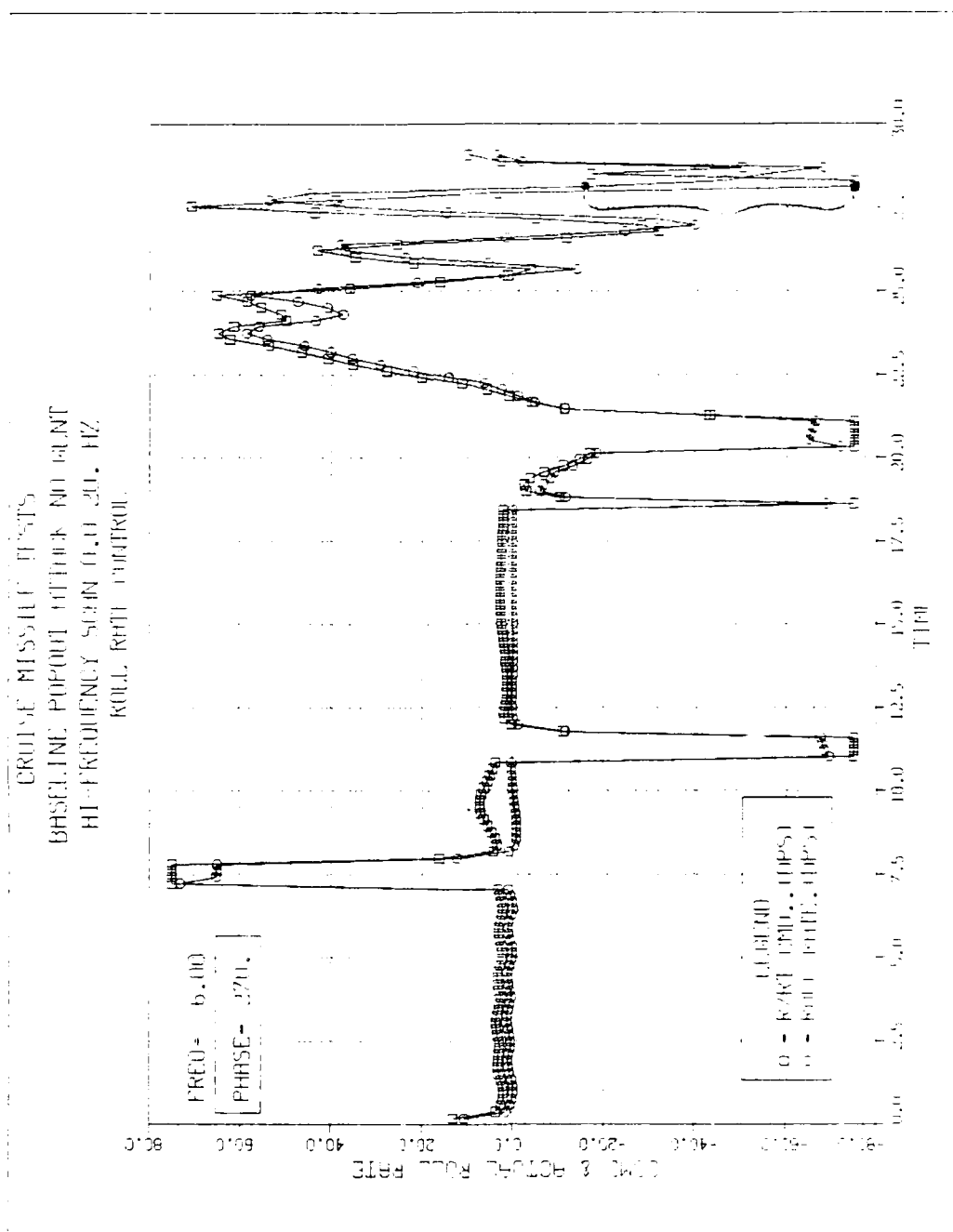


Figure A.53 Baseline/ECM Freq = 6.0 Hz - Roll Rate.

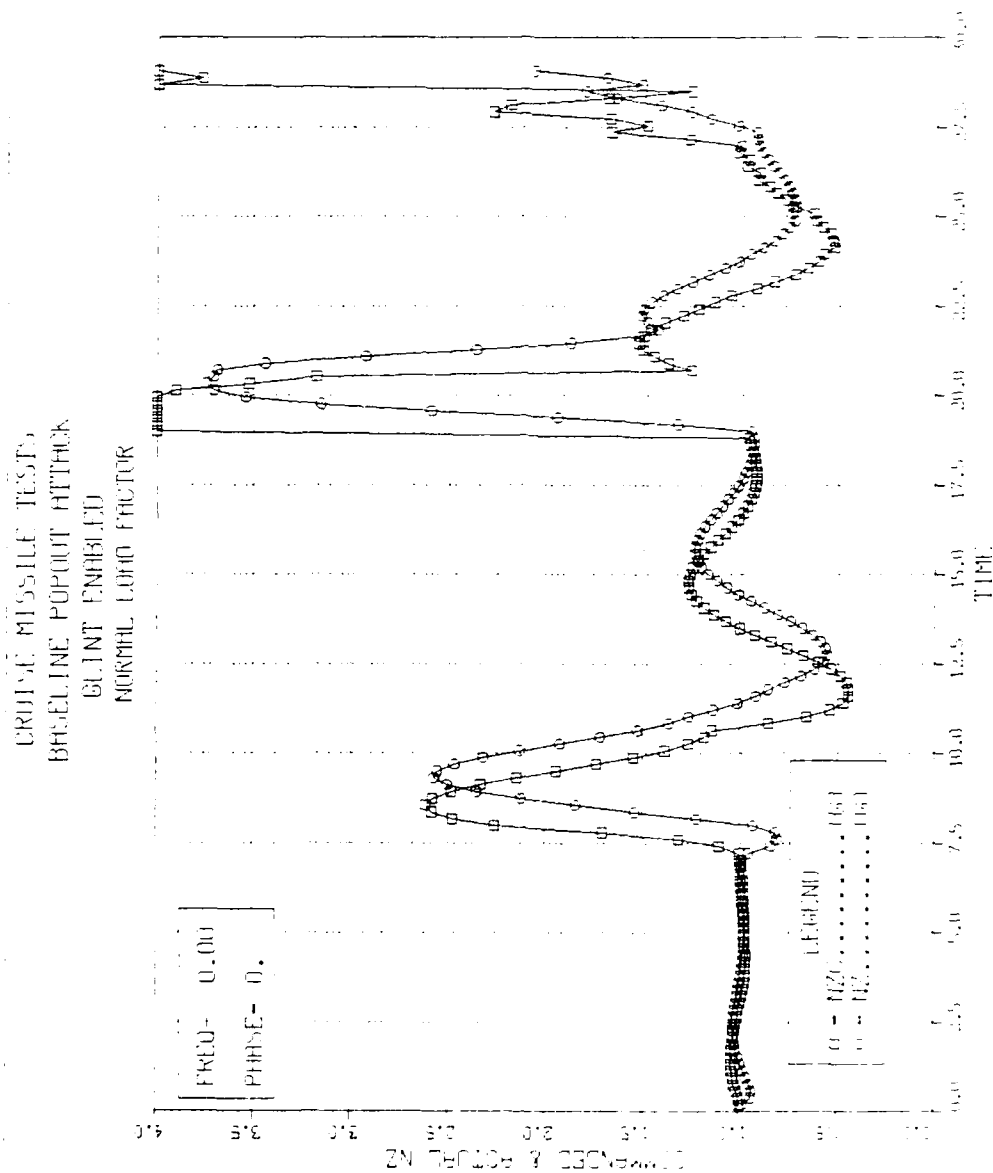


Figure A.54 Baseline with GLINT only - Load Factor.

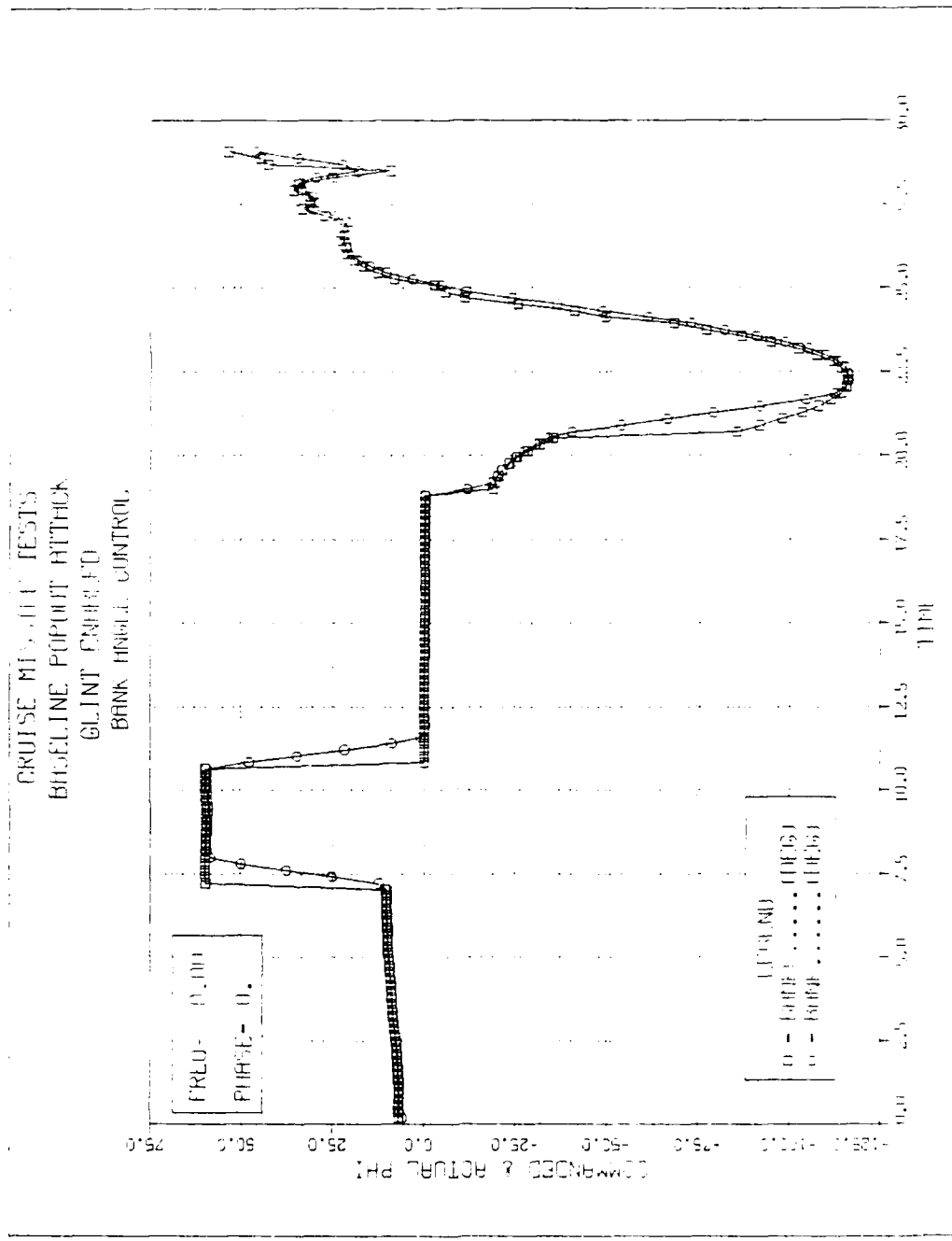


Figure A.55 Easeline with GLINT only - Bank.

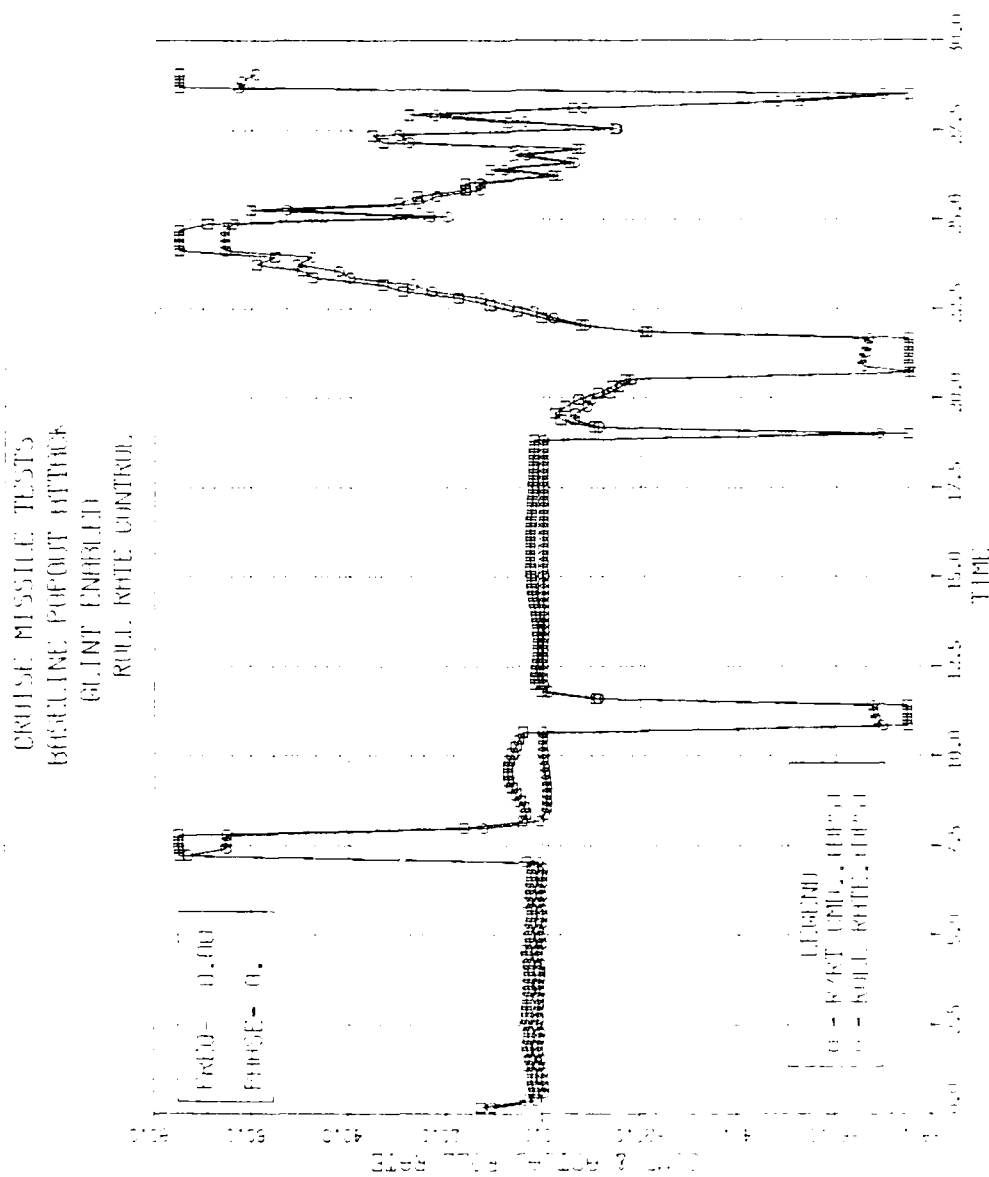


Figure A.56 Baseline with GLINT only - Roll Rate.

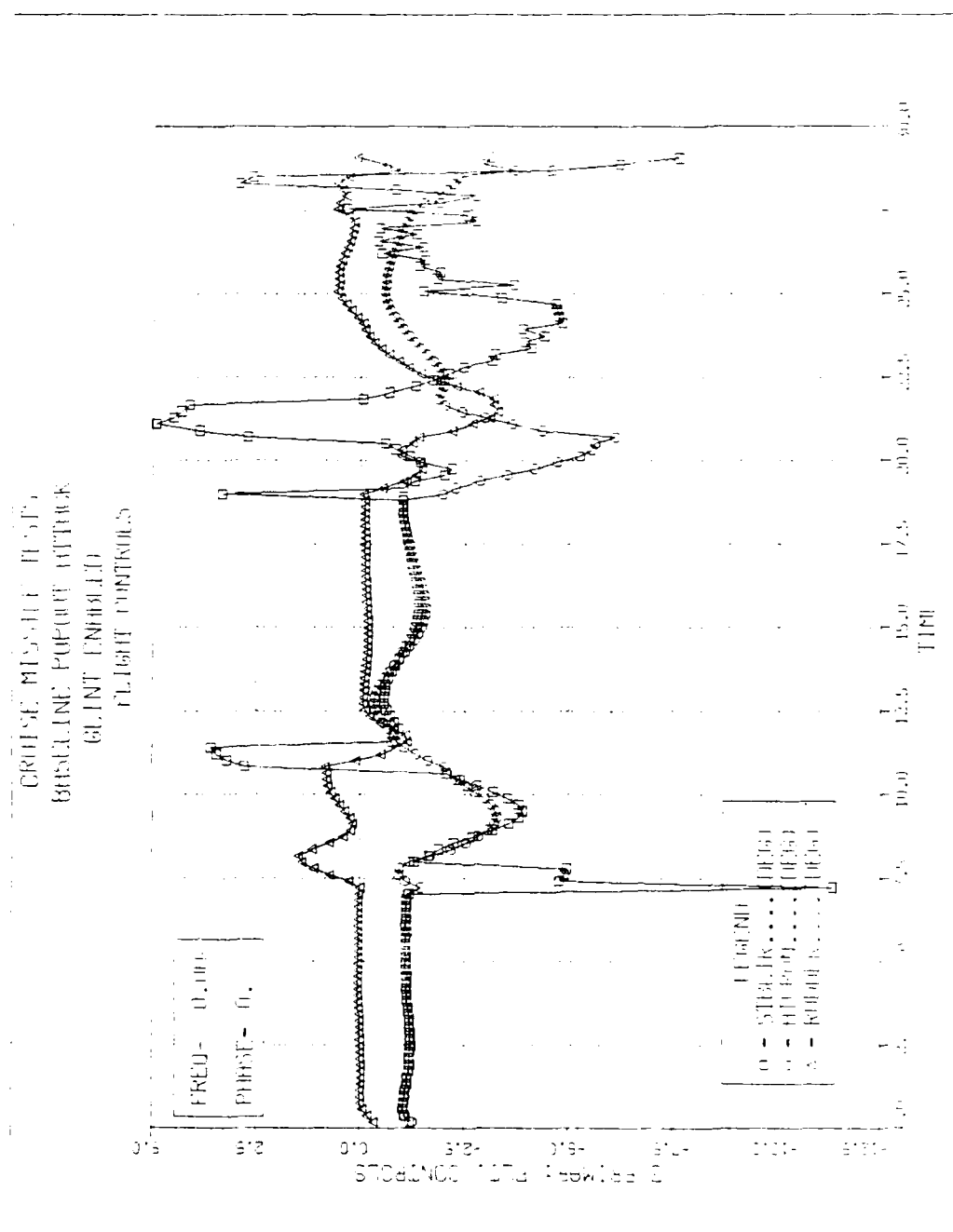


Figure A.57 Baseline with GLINT only - Controls.

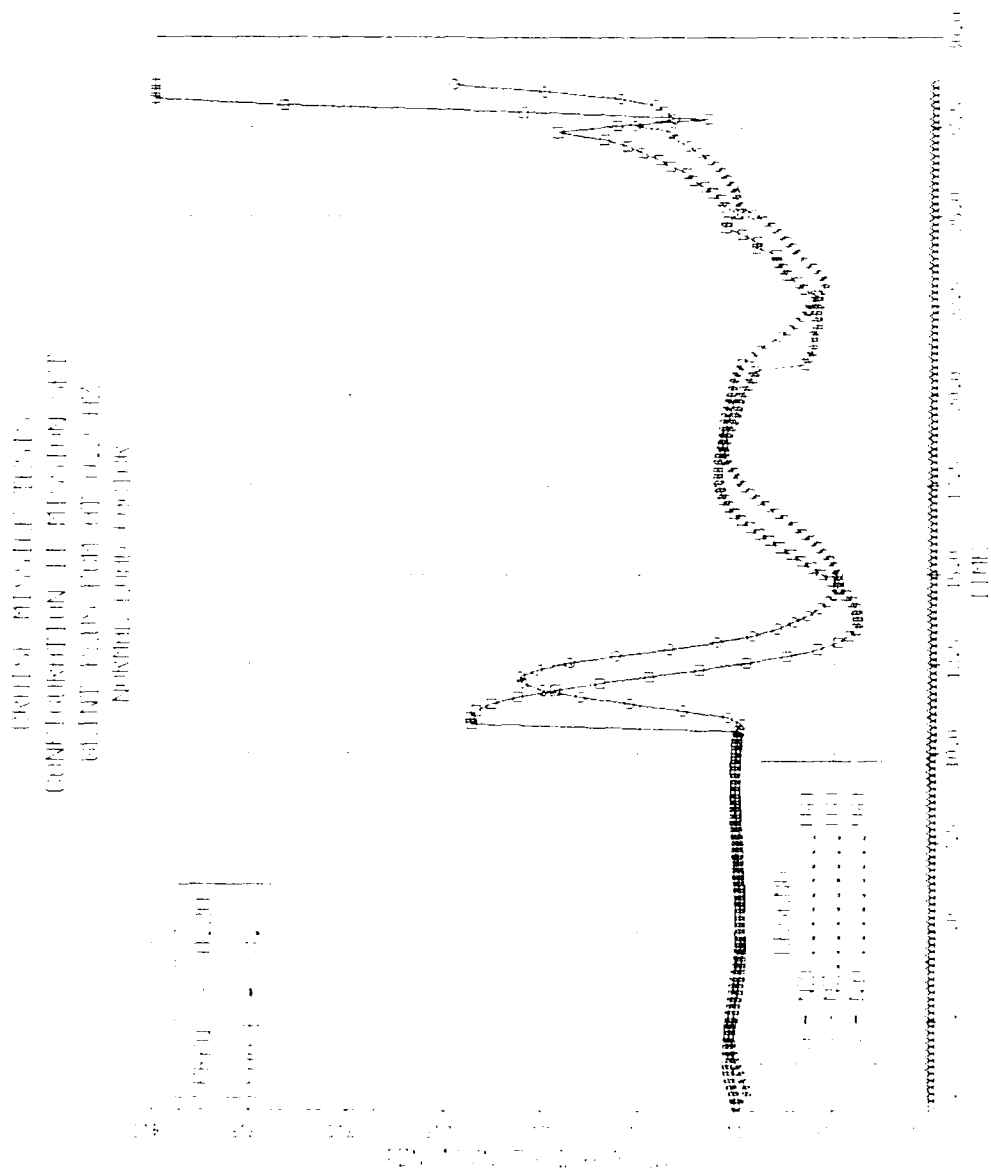


Figure A.58 Conf. II Mission Set - Load Factor.

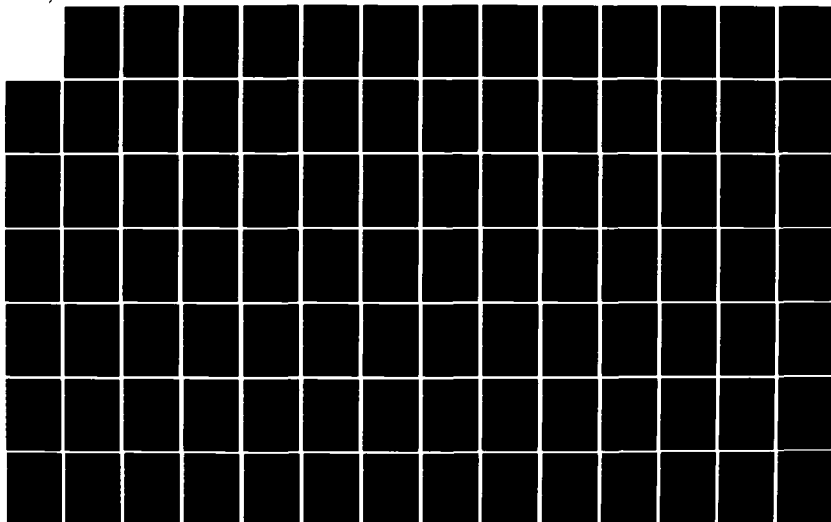
AD-A152 193

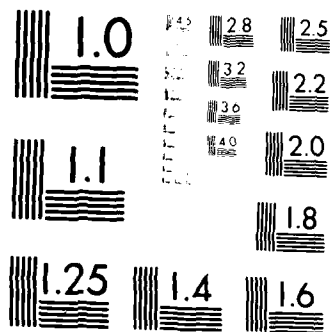
AN INVESTIGATION INTO THE CONTROL LIMITATIONS OF A BANK 2/3
TO TURN MISSILE IN THE TERMINAL HOMING PHASE(U) NAVAL
POSTGRADUATE SCHOOL MONTEREY CA 8 P ANDERSON SEP 84

UNCLASSIFIED

F/G 17/7

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

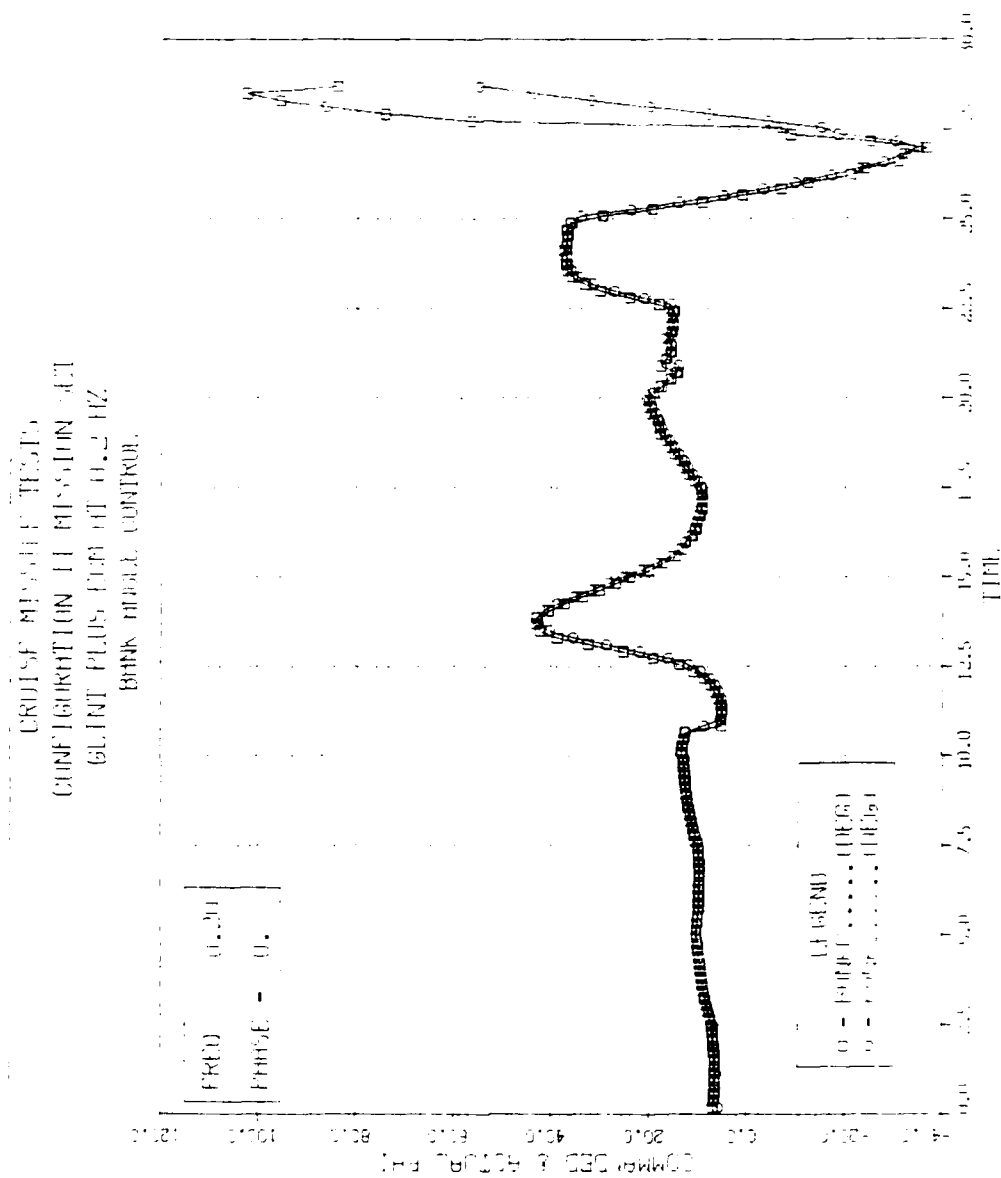


Figure A.59 Conf. II Mission Set - Bank.

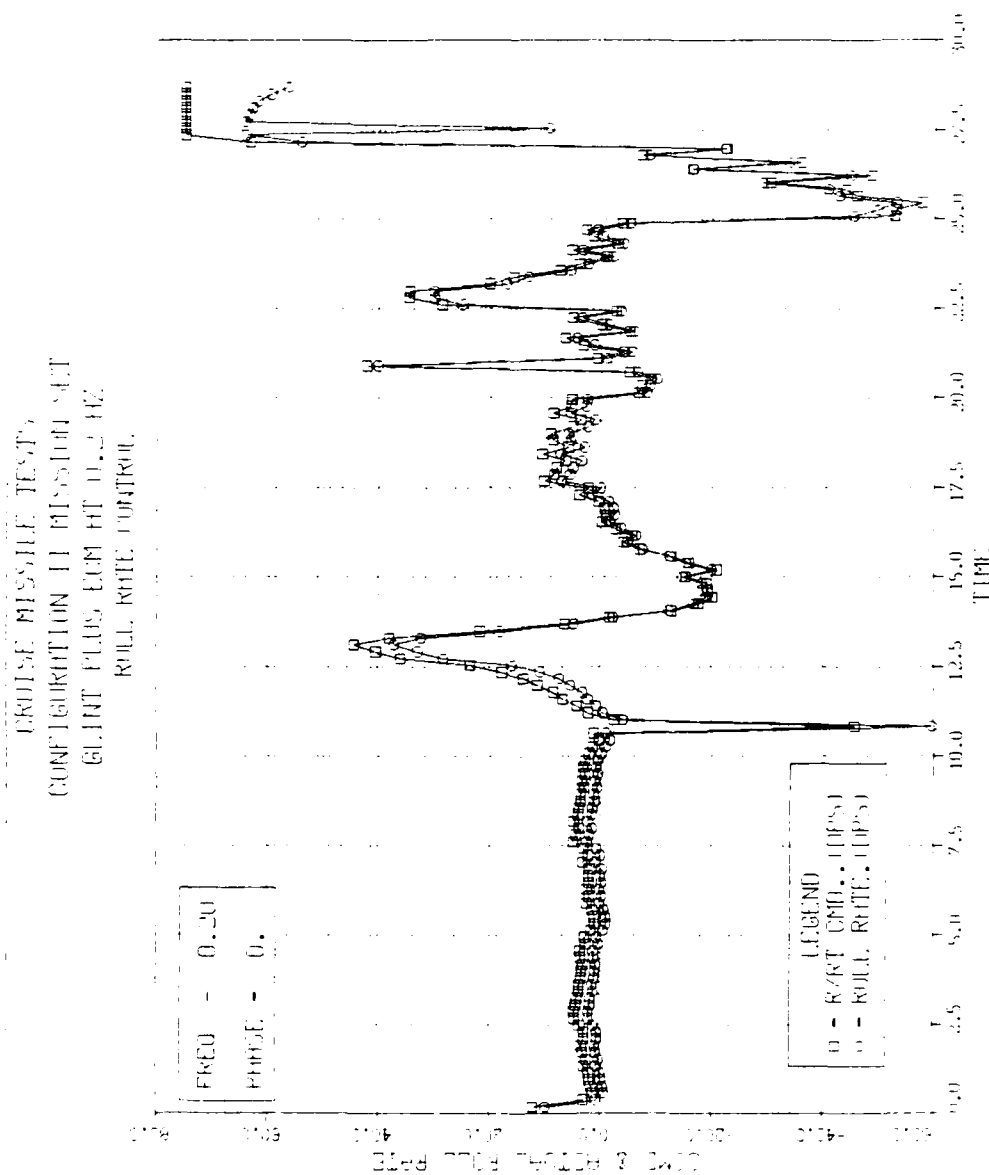


Figure A.60 Conf. II Mission Set - Roll Rate.

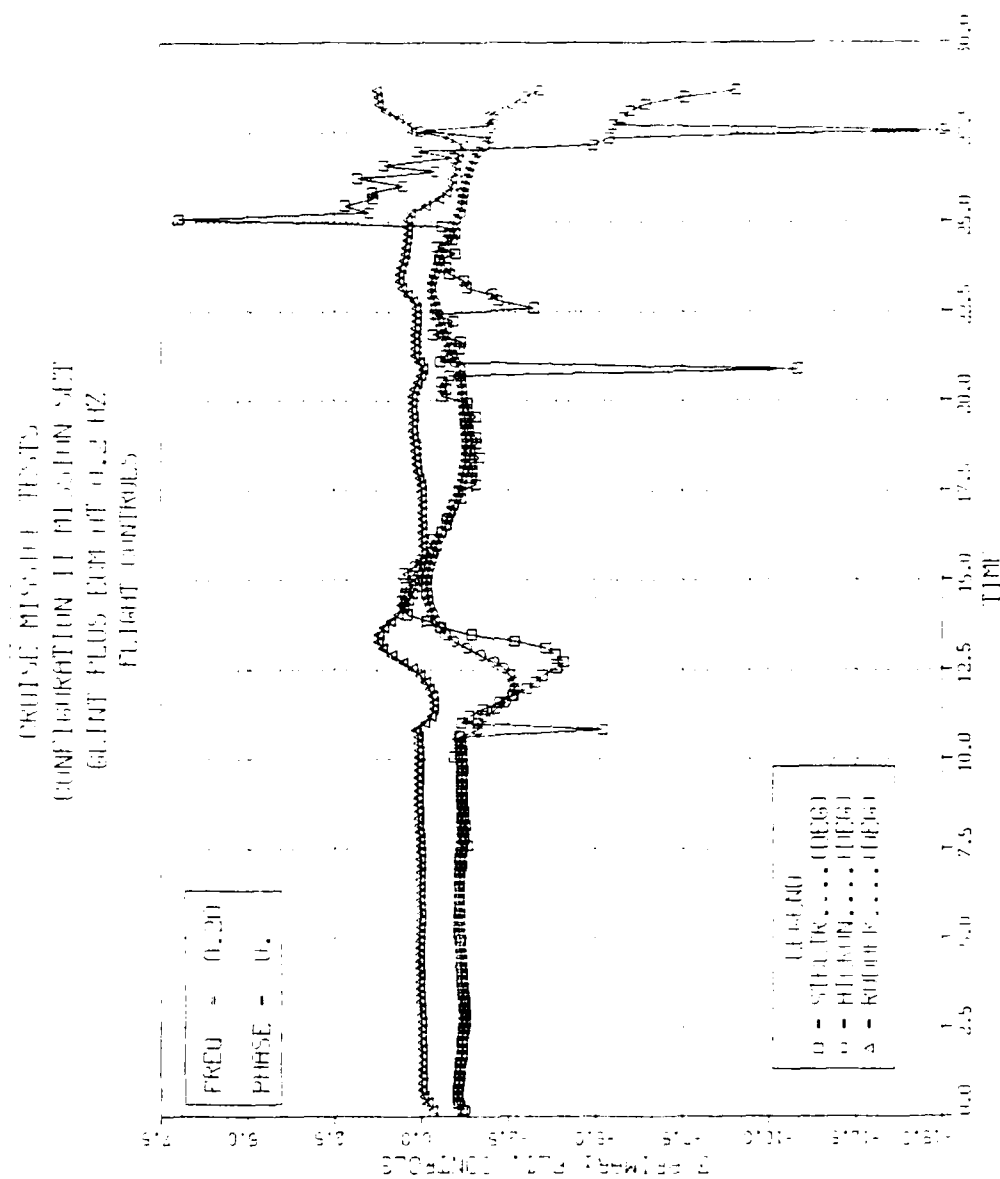


Figure A.61 Conf. II Mission Set - Controls.

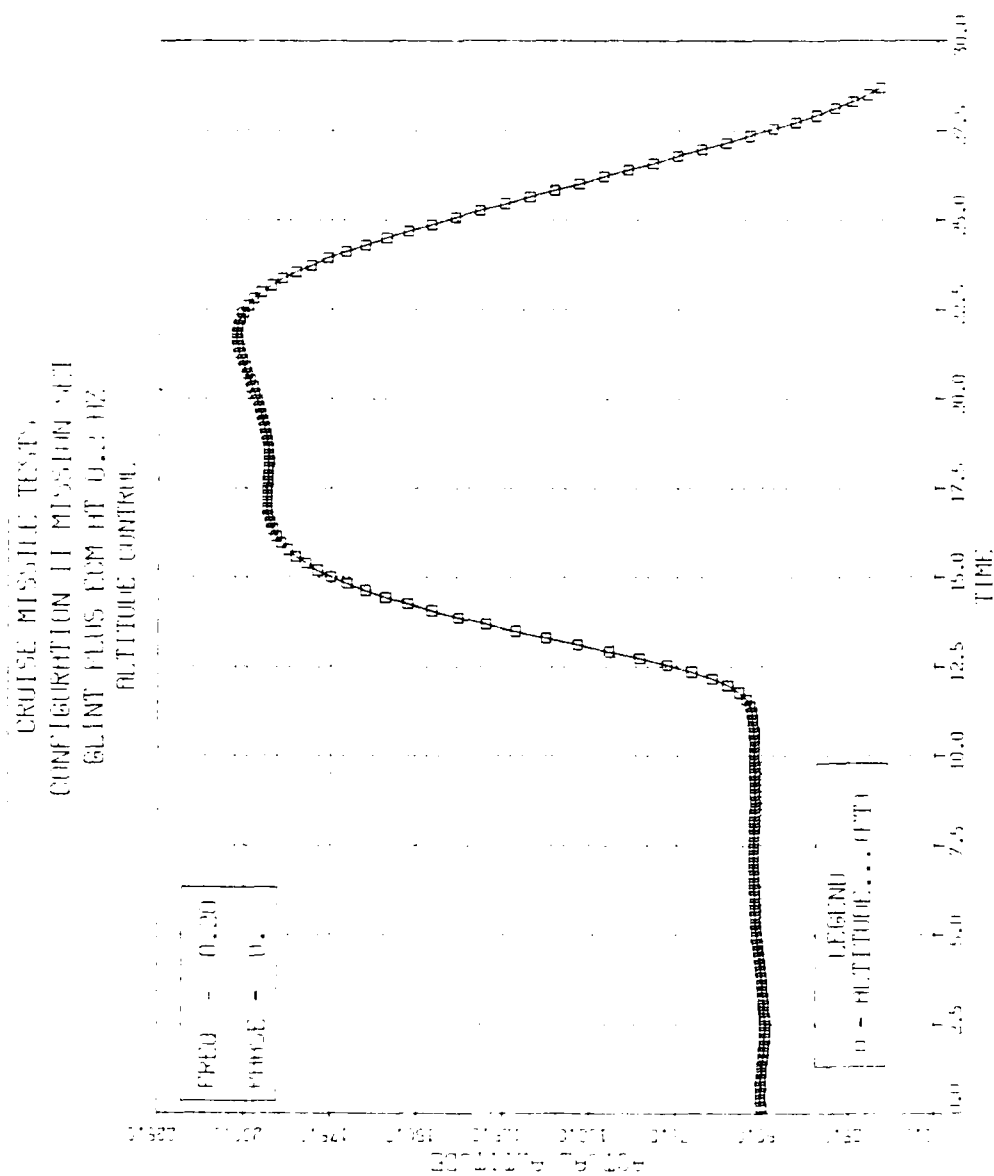


Figure A.62 Conf. II Mission Set - Altitude.

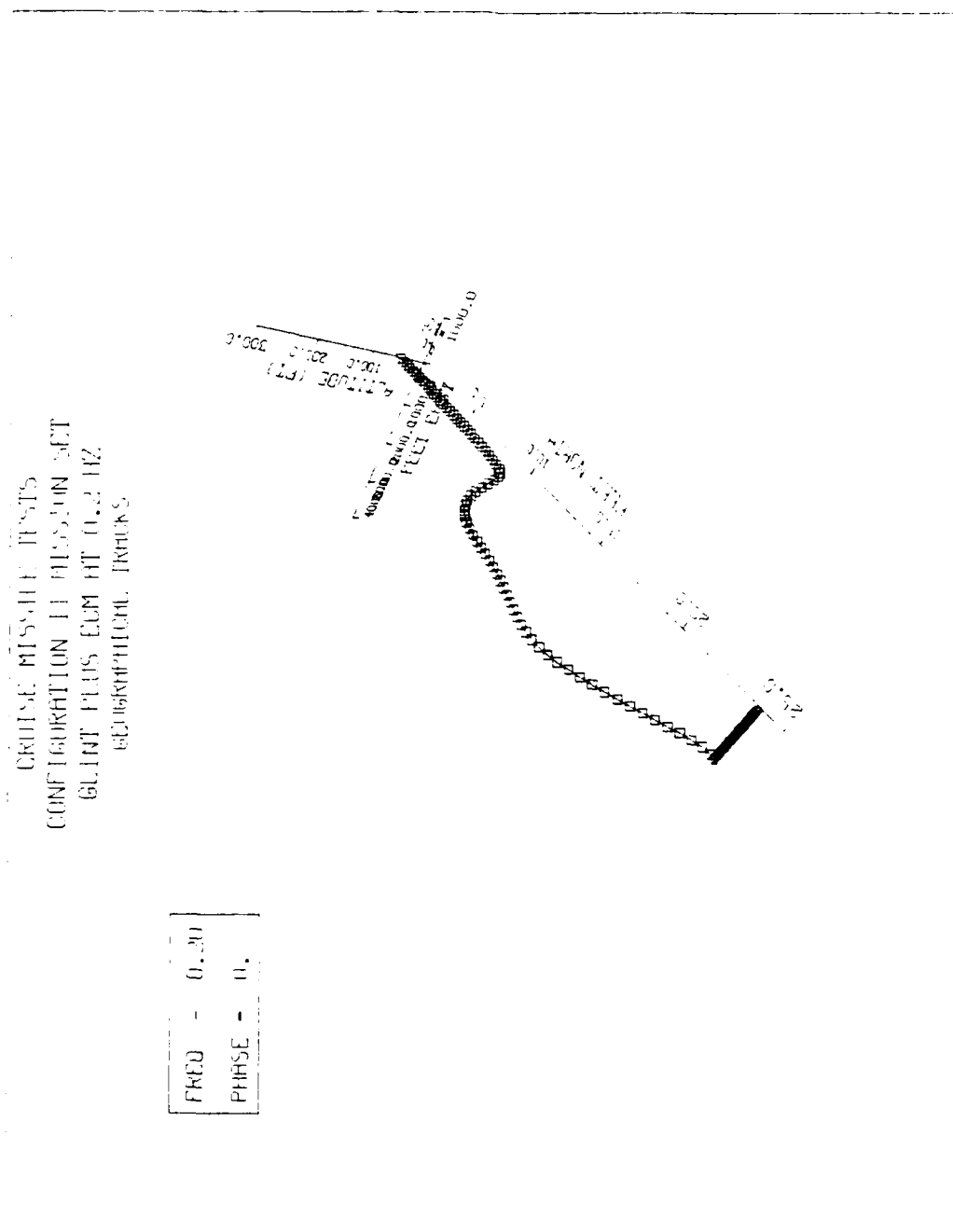


Figure A.63 Conf. II Mission Set - Geo Plot.

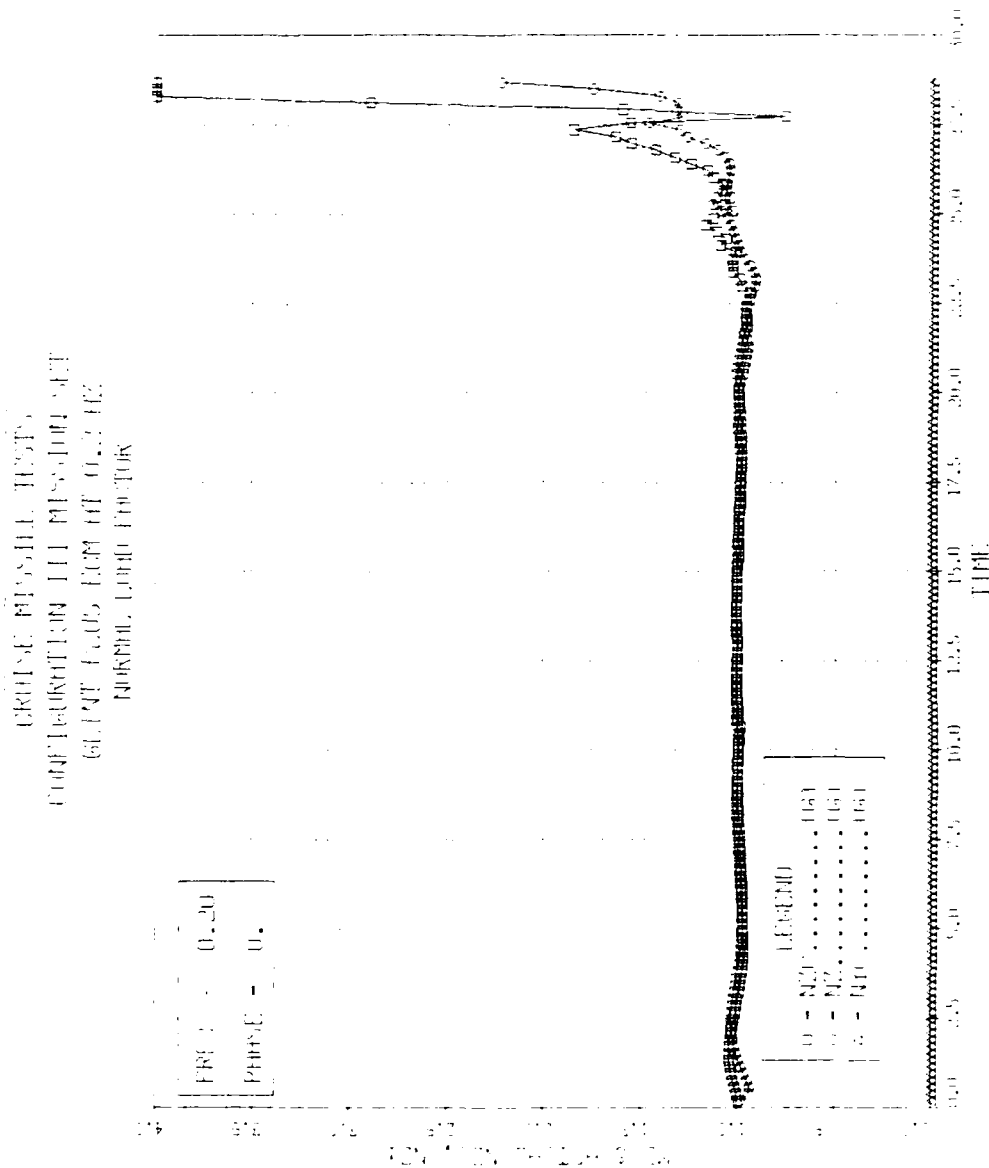


Figure A.64 Conf. III Mission Set - Load Factor.

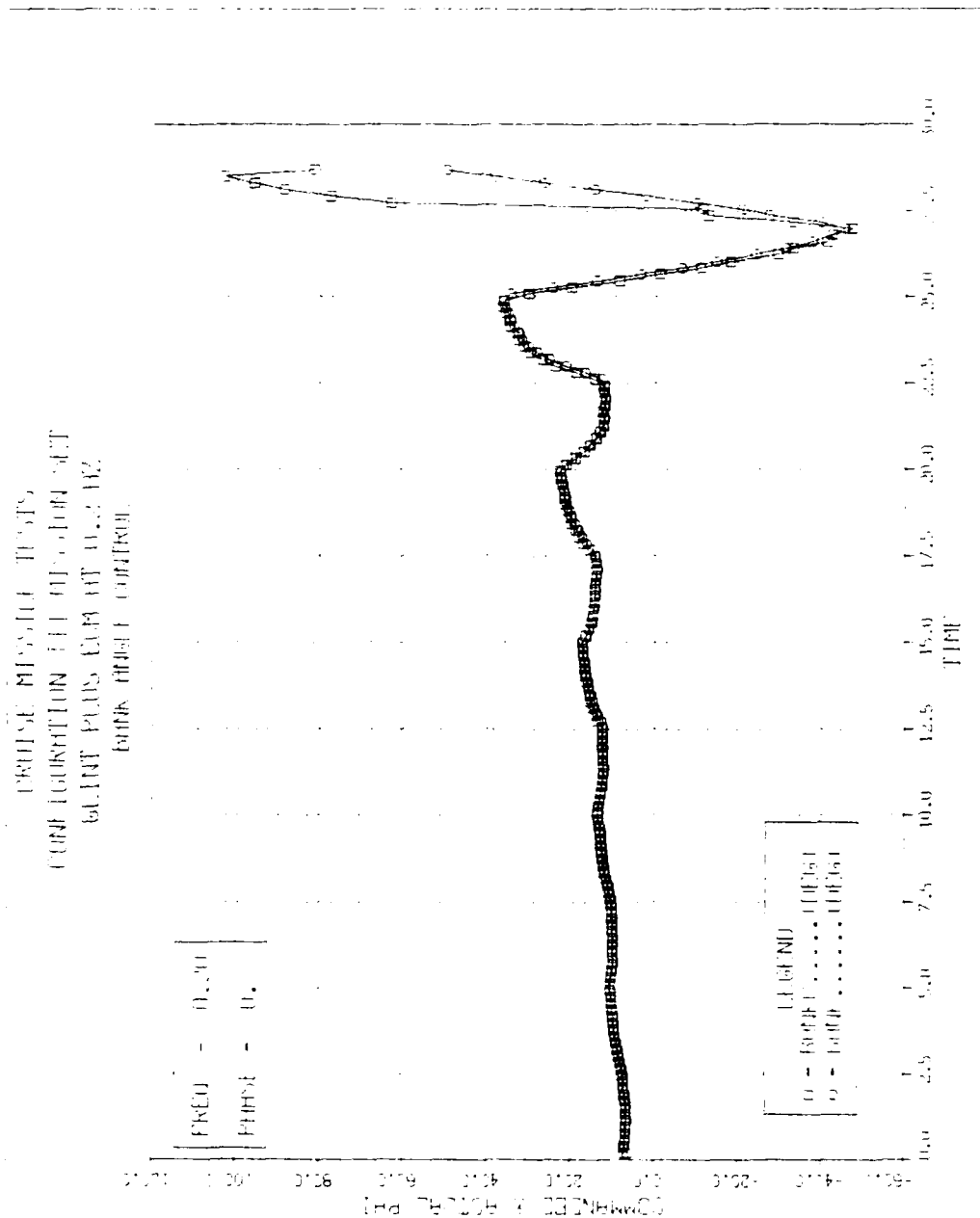


Figure A.65 Conf. III Mission Set - Bank.

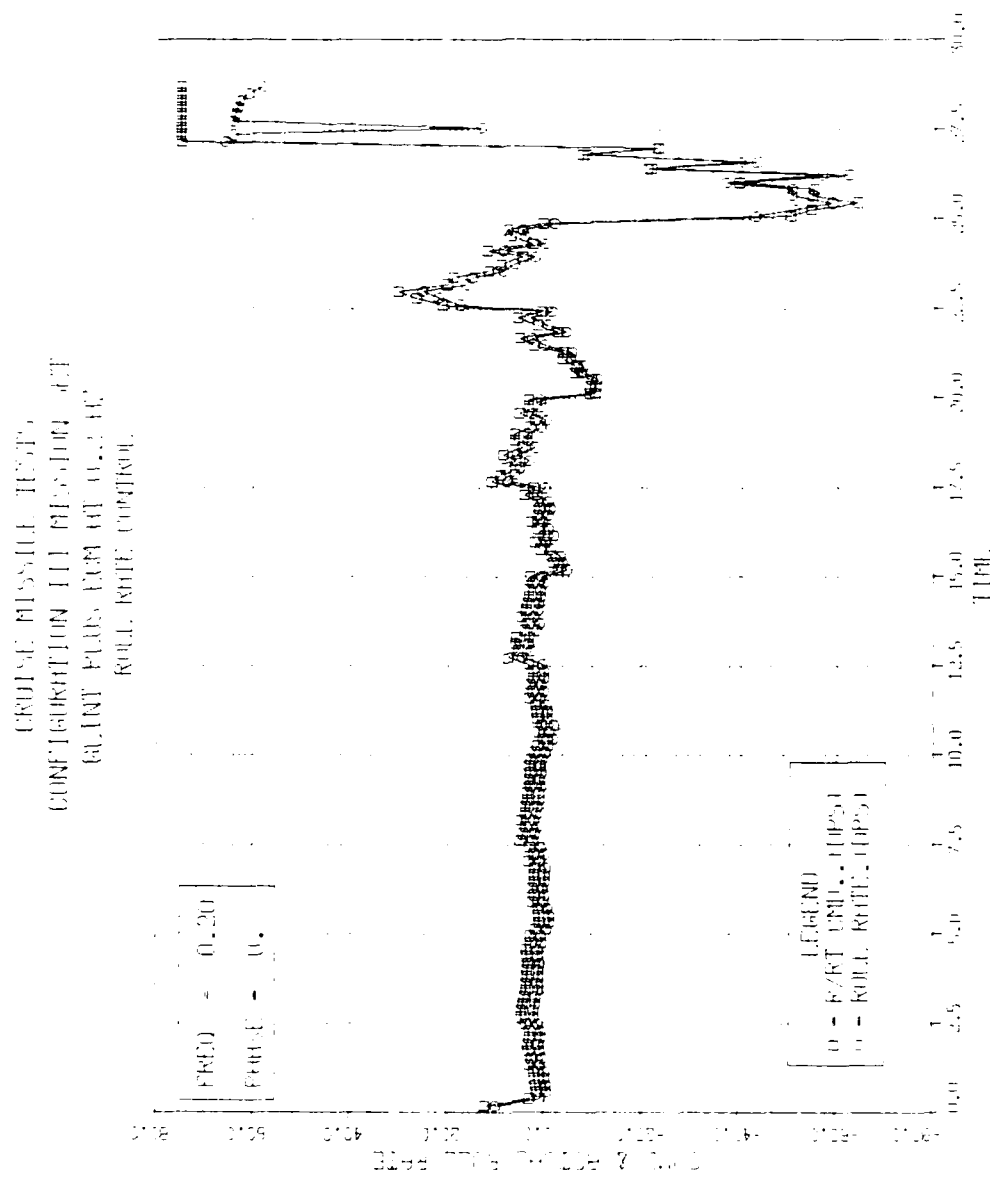


Figure A.66 Conf. III Mission Set - Roll Rate.

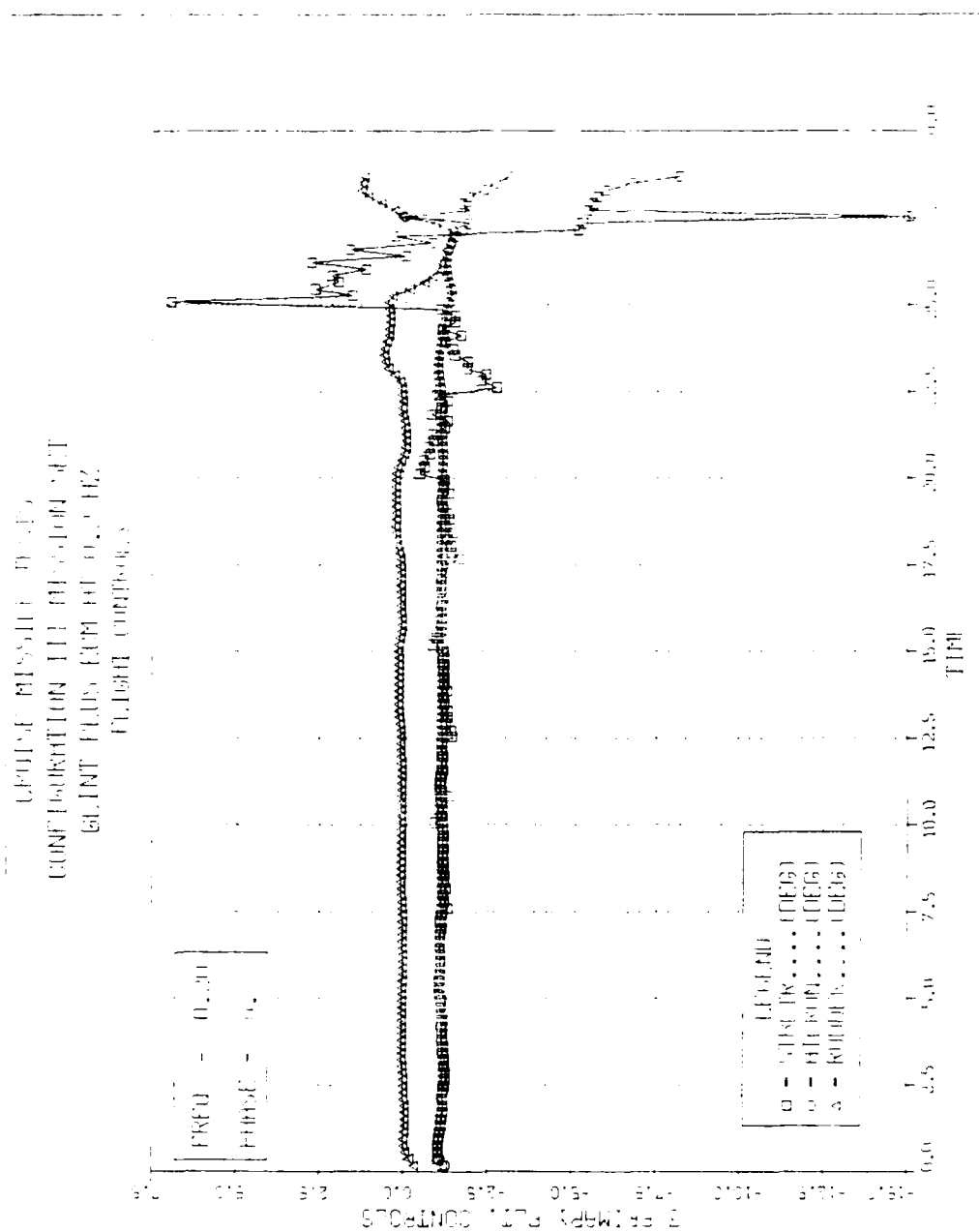


Figure A.67 Conf. III Mission Set - Controls.

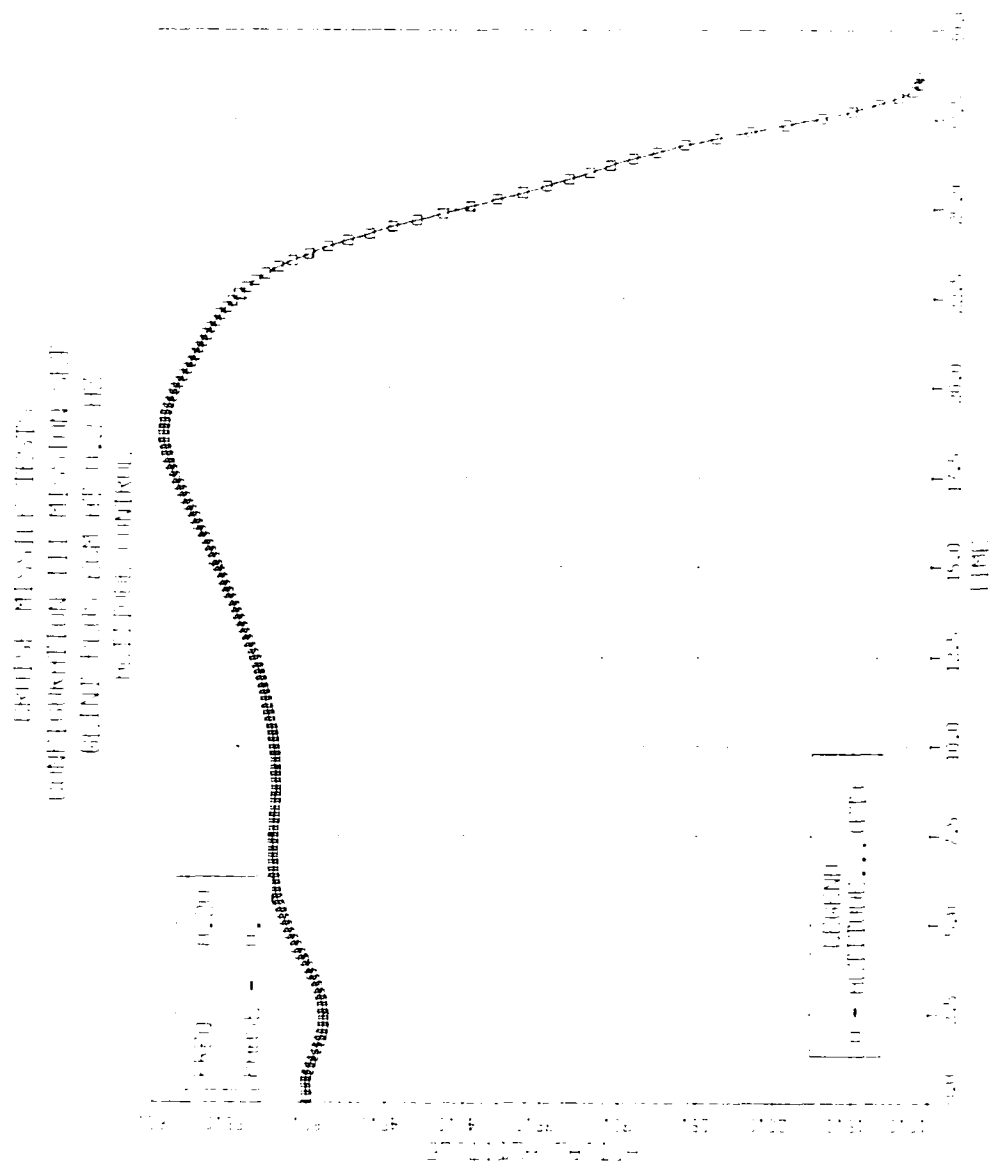


Figure A.68 Conf. III Mission Set - Altitude.

CRUISE RESULTS PLOTS
 CONFIGURATION III MISSION SET
 COUNT PLUS ALTITUDE TRACK

TIME	11.20
ALTITUDE	0.

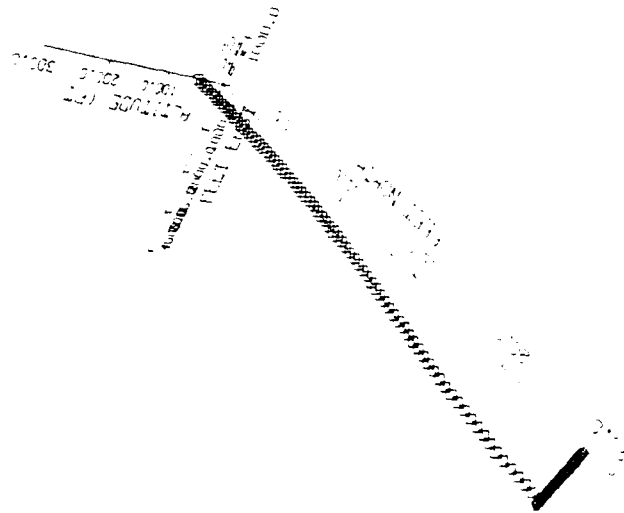
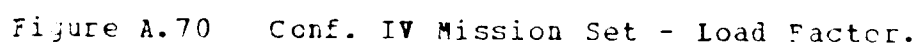


Figure A.69 Conf. III Mission Set - Geo Plot.



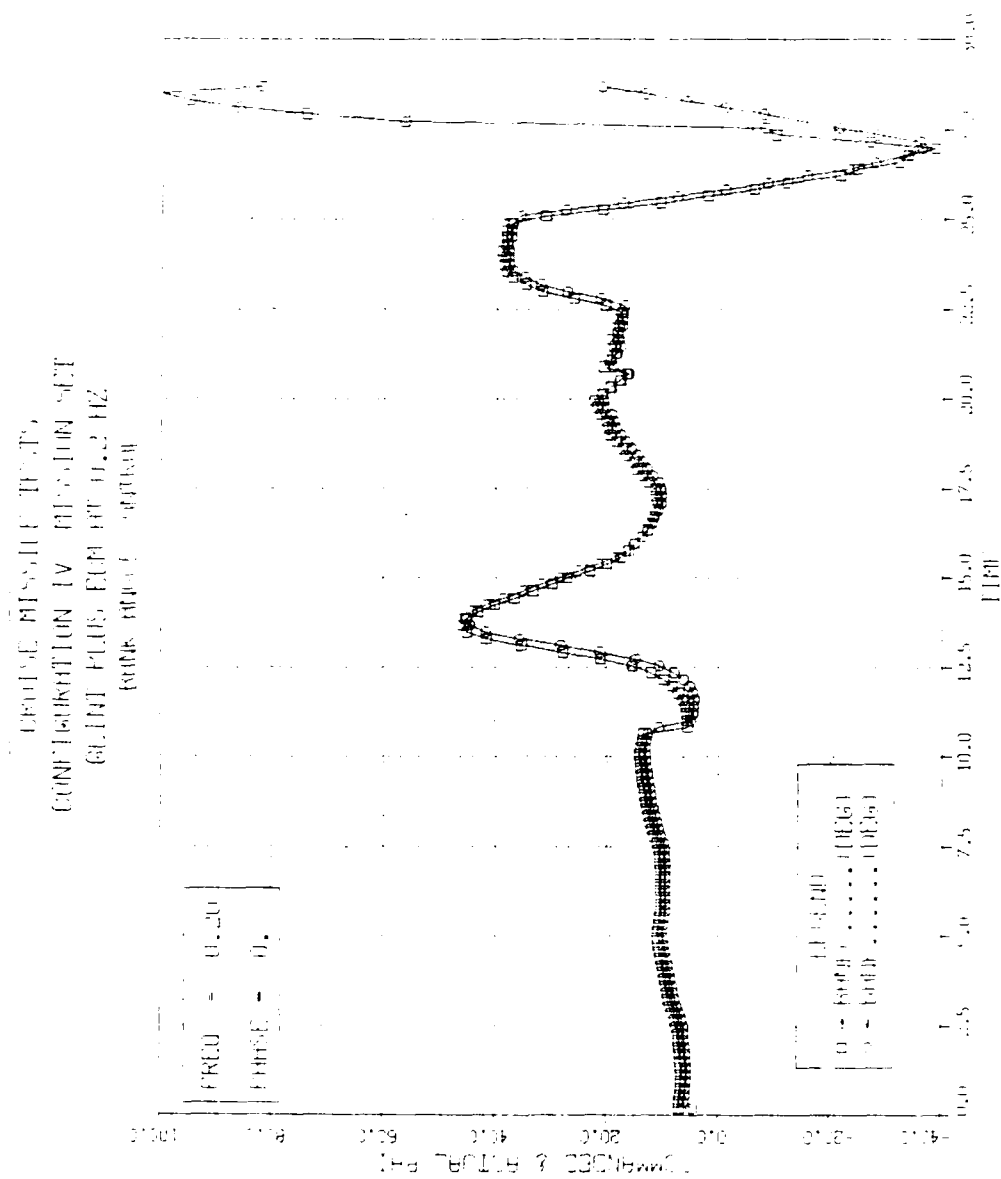


Figure A.71 Conf. IV Mission Set - Bank.

CRUISE MISSILE TESTS
 CONFIGURATION IV MISSION SET
 GLIDE FLIPS EUM HT 0.2 HZ
 ROLL RATE CONTROL

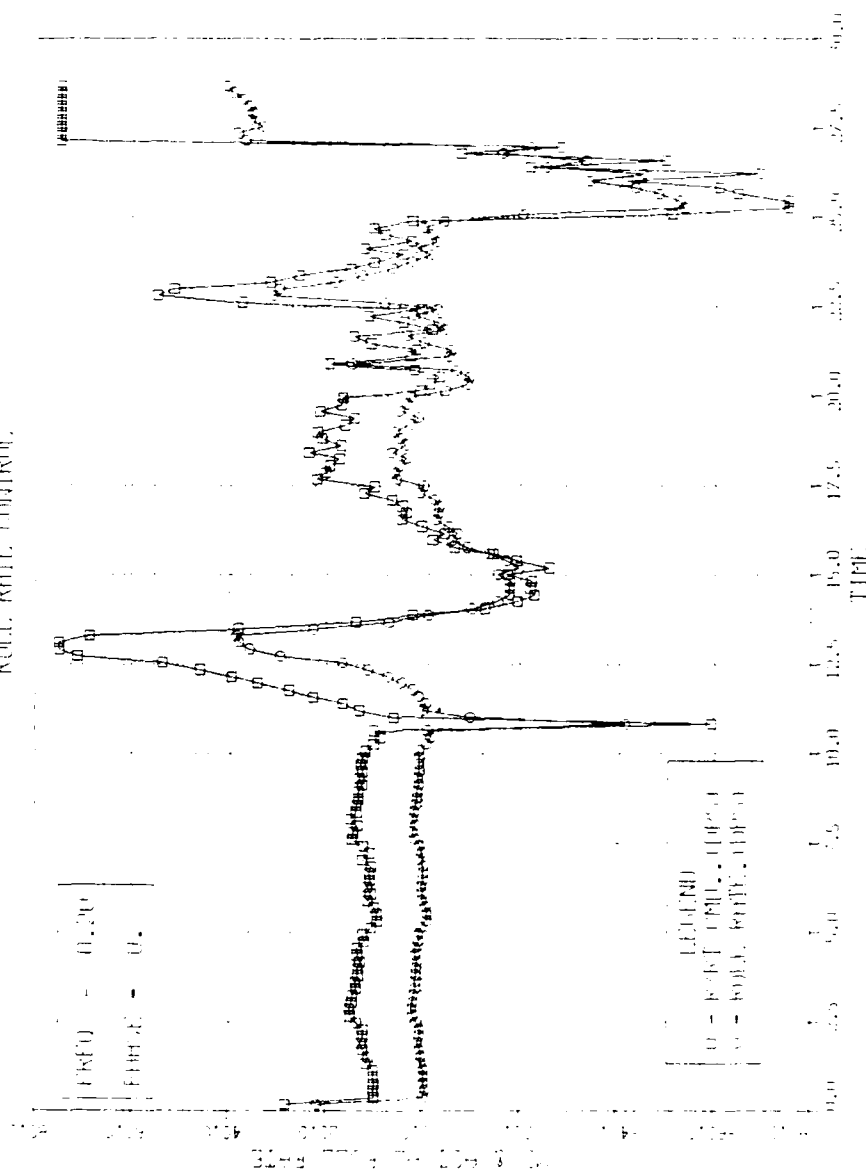


Figure A.72 Ccnf. IV Mission Set - Roll Rate.

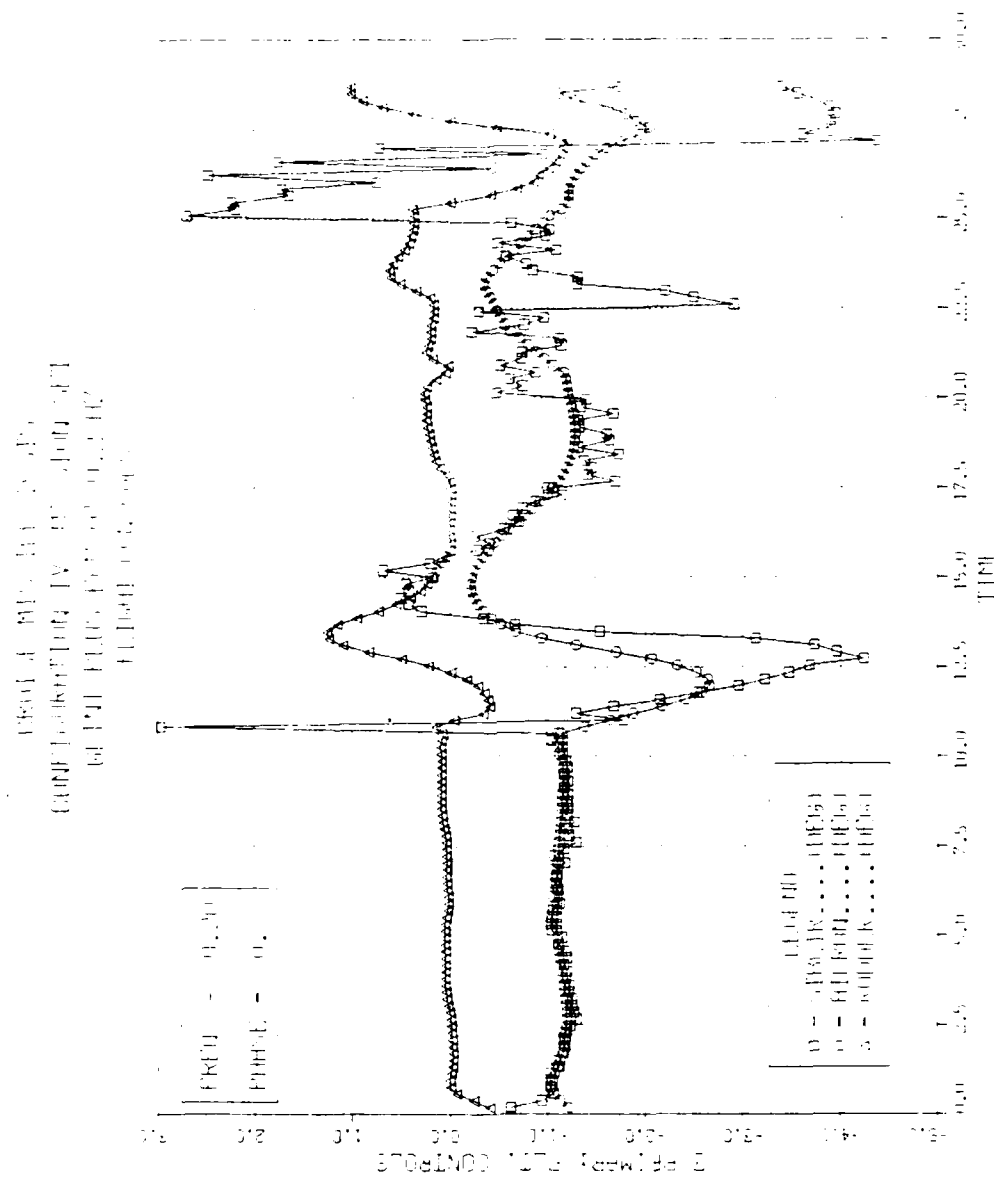


Figure A.73 Conf. IV Mission Set - Controls.

GROUND MISSILE TESTS
 CONFIRMATION IV MISSION SET
 GLINT PLUS CCM OF 0.2 HZ
 ALTITUDE CONTROL

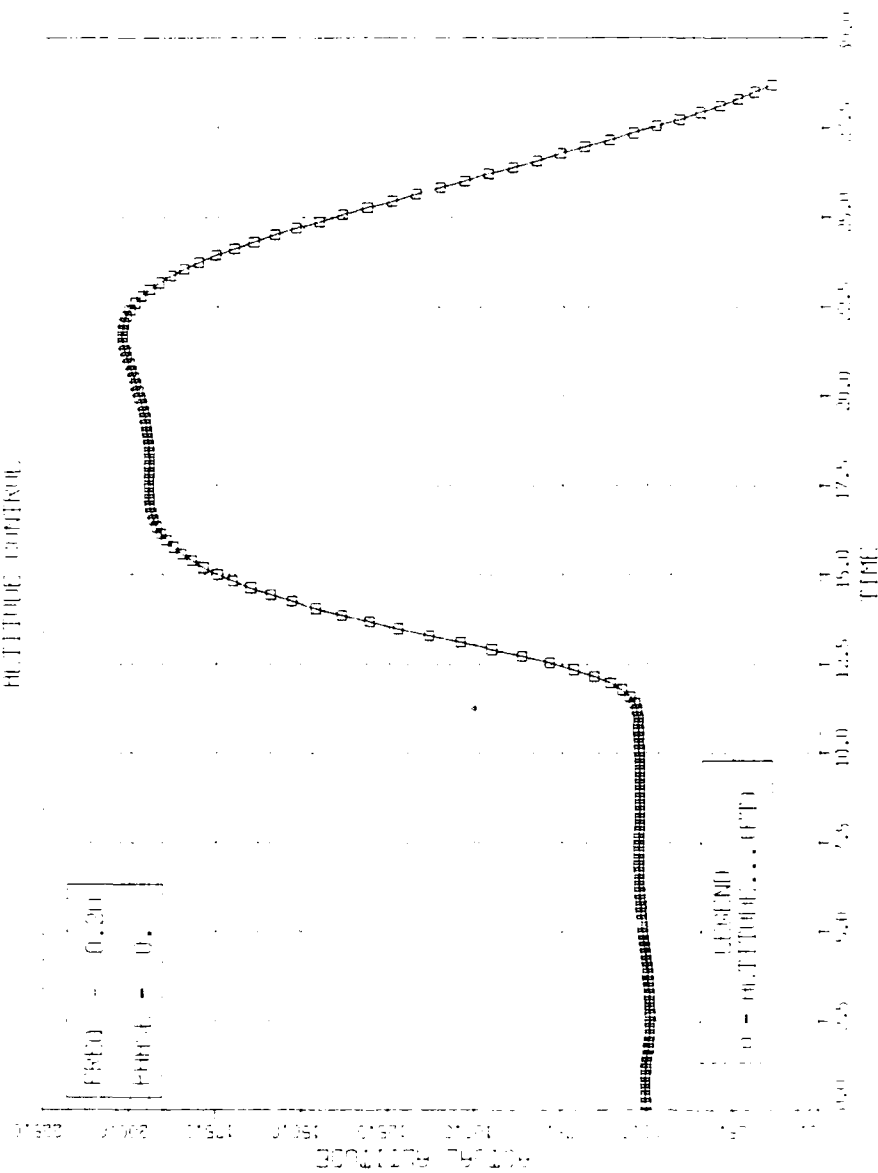


Figure A.74 Conf. IV Mission Set - Altitude.

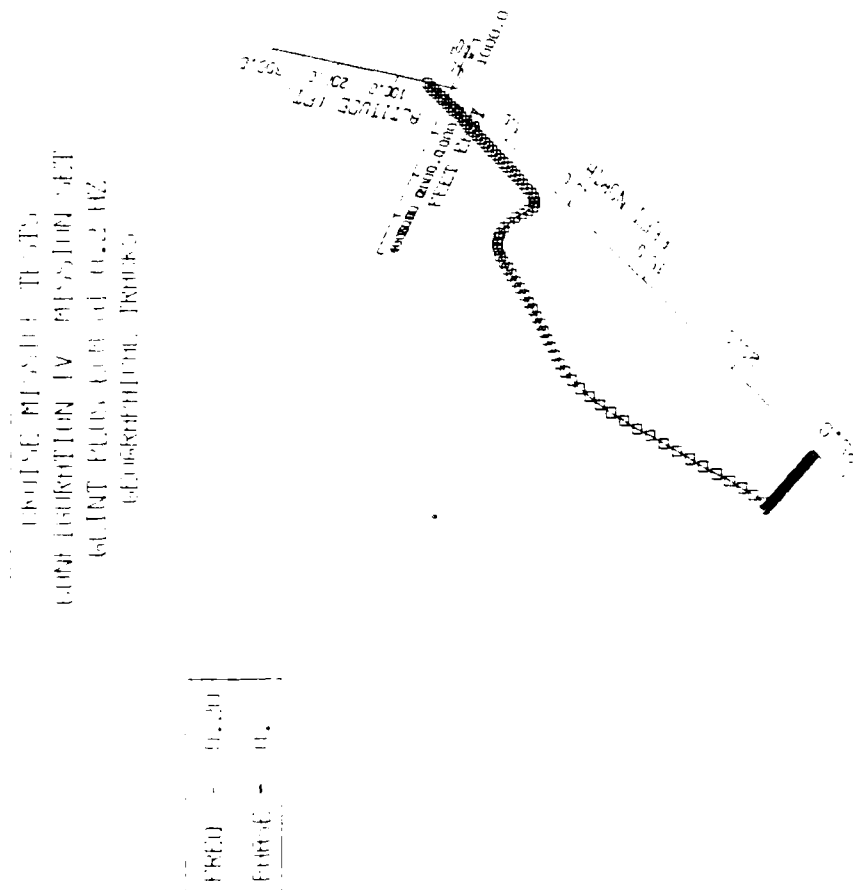


Figure A.75 Conf. IV Mission Set - Geo Plot.

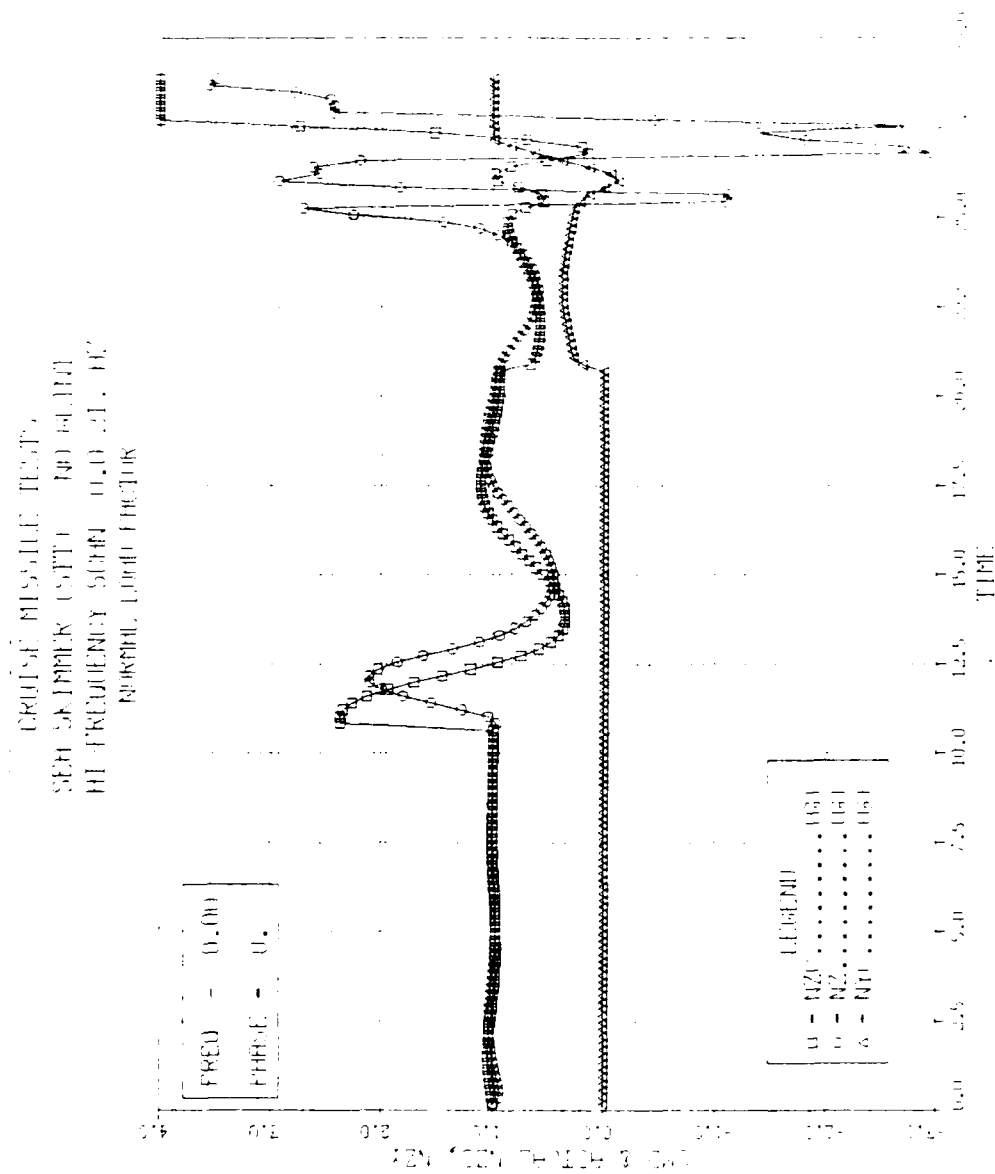


Figure A.76 Ccnf. V Mission Set - Load Factor.

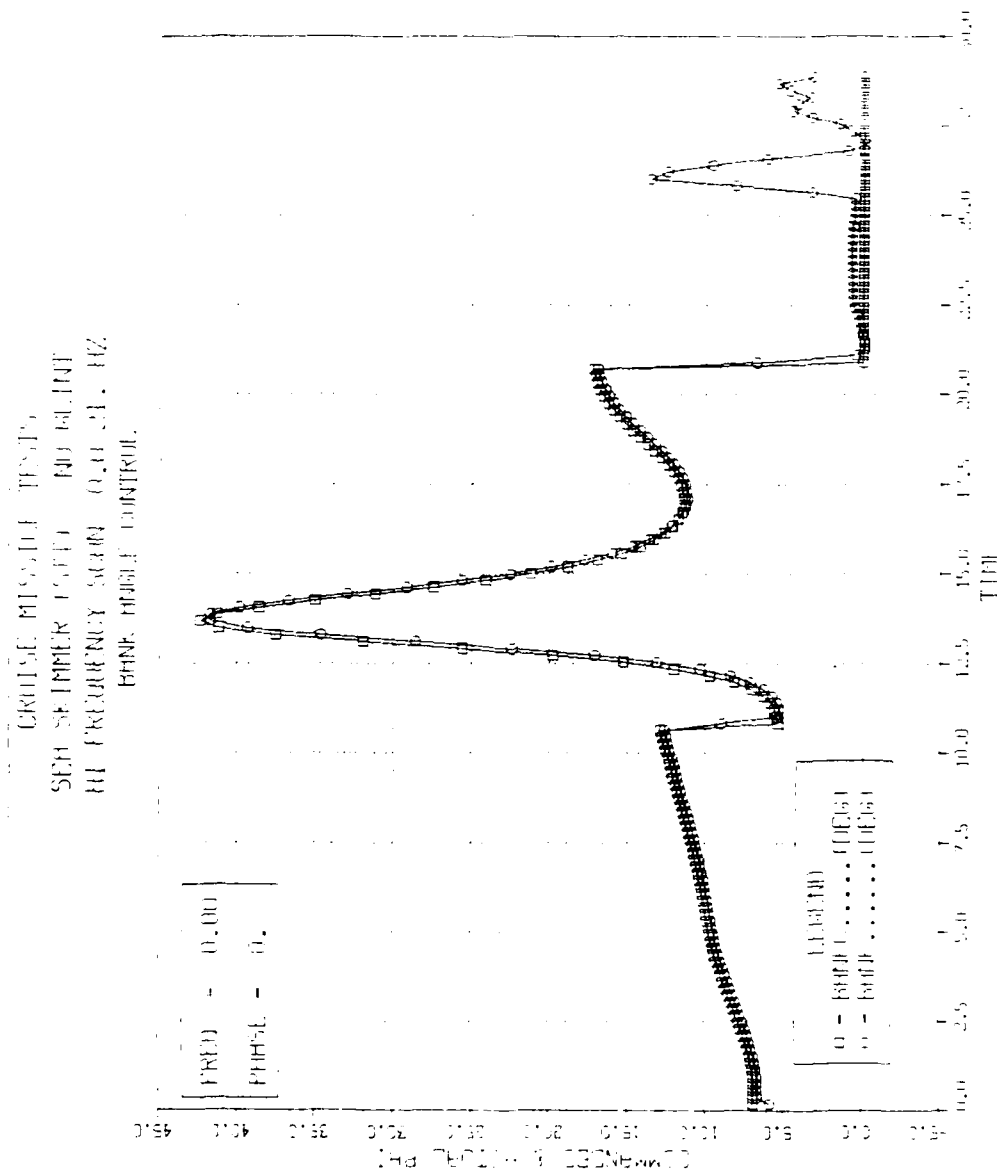


Figure A.77 Conf. V Mission Set - Bank.

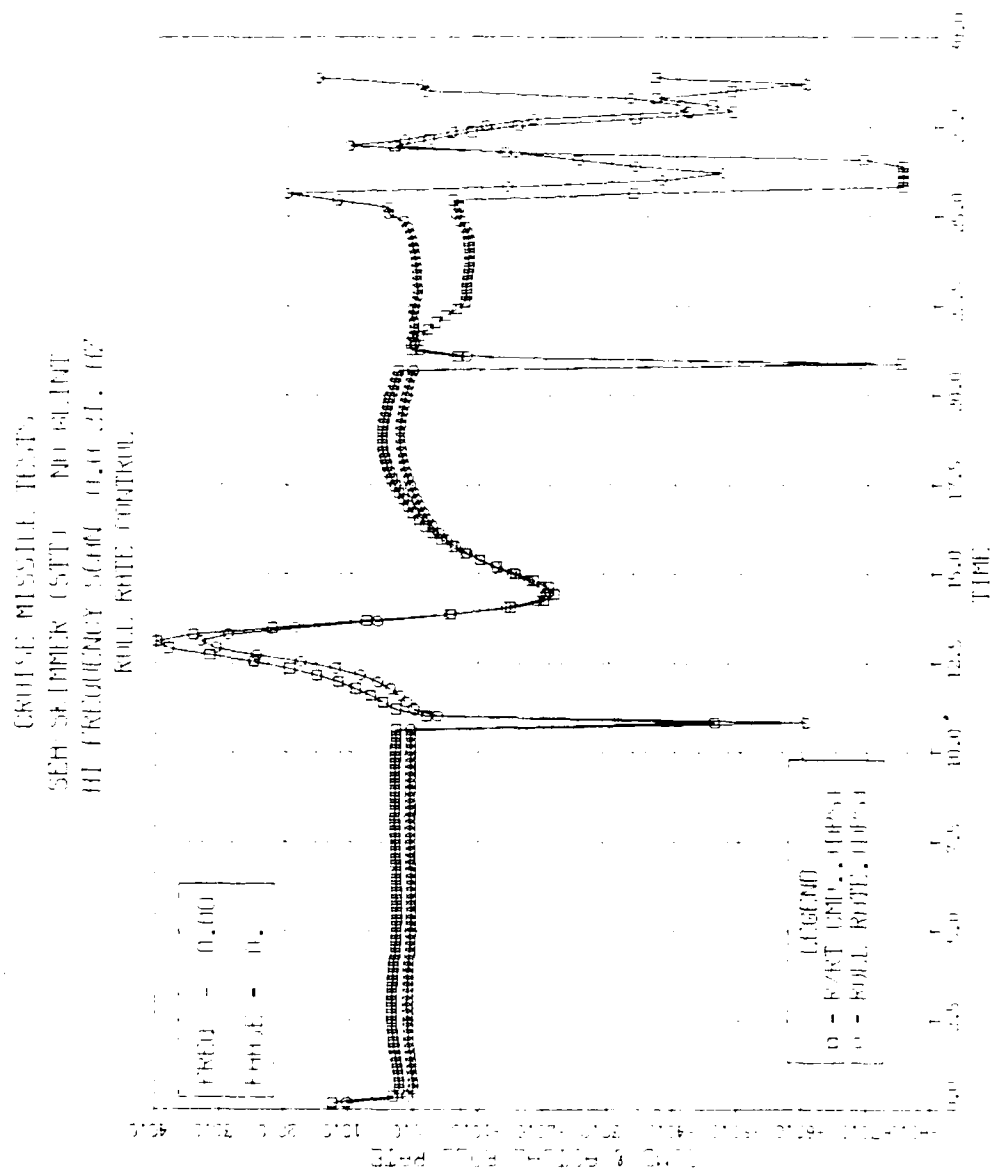


Figure A.78 Conf. V Mission Set - Roll Rate.

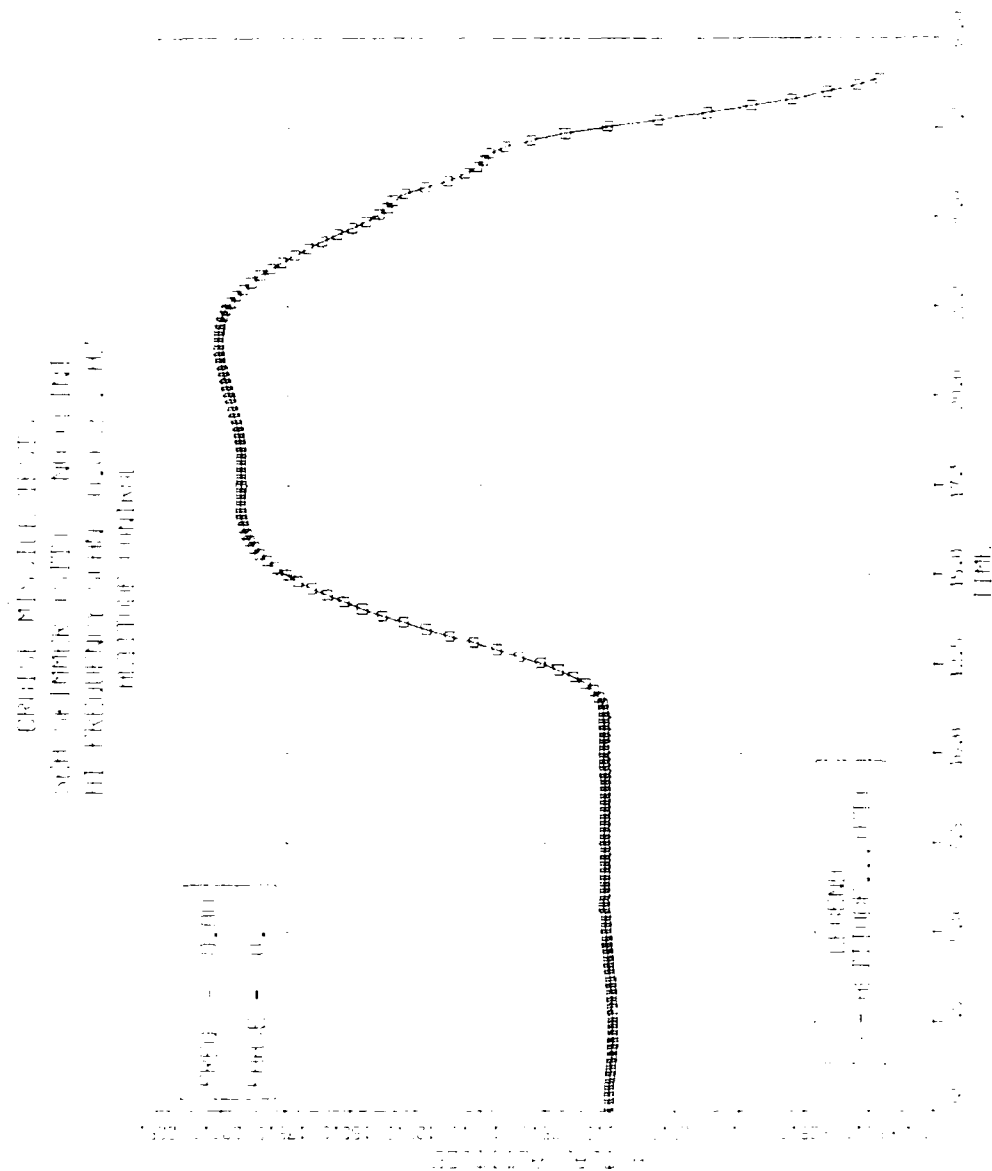


Figure A.80 Conf. V Mission Set - Altitude.

CONFIDENTIAL
 SET OF LINES - 1000
 HI FREQUENCY - 1000
 GEOMETRIC TRUCKS

1000	0.100
1000	0.

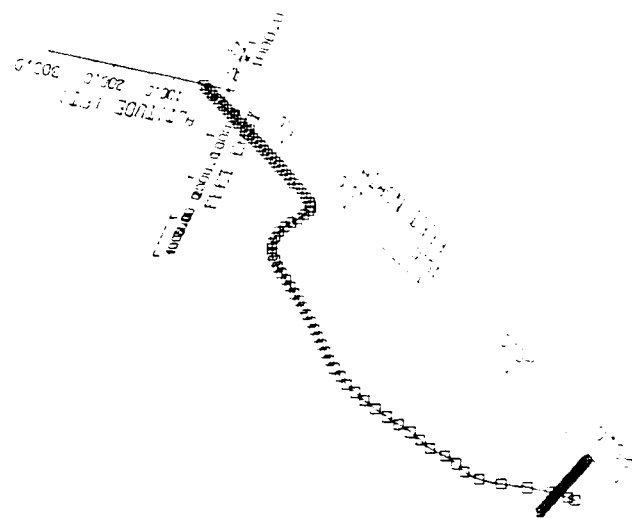


Figure A.81 Conf. V Mission Set - Geo Plot.

CONF. VI, 11, 12, 13, 14, 15, 16, 17, 18, 19, 20, 21, 22, 23, 24, 25, 26, 27, 28, 29, 30, 31, 32, 33, 34, 35, 36, 37, 38, 39, 40, 41, 42, 43, 44, 45, 46, 47, 48, 49, 50, 51, 52, 53, 54, 55, 56, 57, 58, 59, 60, 61, 62, 63, 64, 65, 66, 67, 68, 69, 70, 71, 72, 73, 74, 75, 76, 77, 78, 79, 80, 81, 82, 83, 84, 85, 86, 87, 88, 89, 90, 91, 92, 93, 94, 95, 96, 97, 98, 99, 100, 101, 102, 103, 104, 105, 106, 107, 108, 109, 110, 111, 112, 113, 114, 115, 116, 117, 118, 119, 120, 121, 122, 123, 124, 125, 126, 127, 128, 129, 130, 131, 132, 133, 134, 135, 136, 137, 138, 139, 140, 141, 142, 143, 144, 145, 146, 147, 148, 149, 150, 151, 152, 153, 154, 155, 156, 157, 158, 159, 160, 161, 162, 163, 164, 165, 166, 167, 168, 169, 170, 171, 172, 173, 174, 175, 176, 177, 178, 179, 180, 181, 182, 183, 184, 185, 186, 187, 188, 189, 190, 191, 192, 193, 194, 195, 196, 197, 198, 199, 200, 201, 202, 203, 204, 205, 206, 207, 208, 209, 210, 211, 212, 213, 214, 215, 216, 217, 218, 219, 220, 221, 222, 223, 224, 225, 226, 227, 228, 229, 230, 231, 232, 233, 234, 235, 236, 237, 238, 239, 240, 241, 242, 243, 244, 245, 246, 247, 248, 249, 250, 251, 252, 253, 254, 255, 256, 257, 258, 259, 260, 261, 262, 263, 264, 265, 266, 267, 268, 269, 270, 271, 272, 273, 274, 275, 276, 277, 278, 279, 280, 281, 282, 283, 284, 285, 286, 287, 288, 289, 290, 291, 292, 293, 294, 295, 296, 297, 298, 299, 300, 301, 302, 303, 304, 305, 306, 307, 308, 309, 310, 311, 312, 313, 314, 315, 316, 317, 318, 319, 320, 321, 322, 323, 324, 325, 326, 327, 328, 329, 330, 331, 332, 333, 334, 335, 336, 337, 338, 339, 340, 341, 342, 343, 344, 345, 346, 347, 348, 349, 350, 351, 352, 353, 354, 355, 356, 357, 358, 359, 360, 361, 362, 363, 364, 365, 366, 367, 368, 369, 370, 371, 372, 373, 374, 375, 376, 377, 378, 379, 380, 381, 382, 383, 384, 385, 386, 387, 388, 389, 390, 391, 392, 393, 394, 395, 396, 397, 398, 399, 400, 401, 402, 403, 404, 405, 406, 407, 408, 409, 410, 411, 412, 413, 414, 415, 416, 417, 418, 419, 420, 421, 422, 423, 424, 425, 426, 427, 428, 429, 430, 431, 432, 433, 434, 435, 436, 437, 438, 439, 440, 441, 442, 443, 444, 445, 446, 447, 448, 449, 450, 451, 452, 453, 454, 455, 456, 457, 458, 459, 460, 461, 462, 463, 464, 465, 466, 467, 468, 469, 470, 471, 472, 473, 474, 475, 476, 477, 478, 479, 480, 481, 482, 483, 484, 485, 486, 487, 488, 489, 490, 491, 492, 493, 494, 495, 496, 497, 498, 499, 500, 501, 502, 503, 504, 505, 506, 507, 508, 509, 510, 511, 512, 513, 514, 515, 516, 517, 518, 519, 520, 521, 522, 523, 524, 525, 526, 527, 528, 529, 530, 531, 532, 533, 534, 535, 536, 537, 538, 539, 540, 541, 542, 543, 544, 545, 546, 547, 548, 549, 550, 551, 552, 553, 554, 555, 556, 557, 558, 559, 560, 561, 562, 563, 564, 565, 566, 567, 568, 569, 570, 571, 572, 573, 574, 575, 576, 577, 578, 579, 580, 581, 582, 583, 584, 585, 586, 587, 588, 589, 590, 591, 592, 593, 594, 595, 596, 597, 598, 599, 600, 601, 602, 603, 604, 605, 606, 607, 608, 609, 610, 611, 612, 613, 614, 615, 616, 617, 618, 619, 620, 621, 622, 623, 624, 625, 626, 627, 628, 629, 630, 631, 632, 633, 634, 635, 636, 637, 638, 639, 640, 641, 642, 643, 644, 645, 646, 647, 648, 649, 650, 651, 652, 653, 654, 655, 656, 657, 658, 659, 660, 661, 662, 663, 664, 665, 666, 667, 668, 669, 670, 671, 672, 673, 674, 675, 676, 677, 678, 679, 680, 681, 682, 683, 684, 685, 686, 687, 688, 689, 690, 691, 692, 693, 694, 695, 696, 697, 698, 699, 700, 701, 702, 703, 704, 705, 706, 707, 708, 709, 710, 711, 712, 713, 714, 715, 716, 717, 718, 719, 720, 721, 722, 723, 724, 725, 726, 727, 728, 729, 730, 731, 732, 733, 734, 735, 736, 737, 738, 739, 740, 741, 742, 743, 744, 745, 746, 747, 748, 749, 750, 751, 752, 753, 754, 755, 756, 757, 758, 759, 760, 761, 762, 763, 764, 765, 766, 767, 768, 769, 770, 771, 772, 773, 774, 775, 776, 777, 778, 779, 780, 781, 782, 783, 784, 785, 786, 787, 788, 789, 790, 791, 792, 793, 794, 795, 796, 797, 798, 799, 800, 801, 802, 803, 804, 805, 806, 807, 808, 809, 810, 811, 812, 813, 814, 815, 816, 817, 818, 819, 820, 821, 822, 823, 824, 825, 826, 827, 828, 829, 830, 831, 832, 833, 834, 835, 836, 837, 838, 839, 840, 841, 842, 843, 844, 845, 846, 847, 848, 849, 850, 851, 852, 853, 854, 855, 856, 857, 858, 859, 860, 861, 862, 863, 864, 865, 866, 867, 868, 869, 870, 871, 872, 873, 874, 875, 876, 877, 878, 879, 880, 881, 882, 883, 884, 885, 886, 887, 888, 889, 890, 891, 892, 893, 894, 895, 896, 897, 898, 899, 900, 901, 902, 903, 904, 905, 906, 907, 908, 909, 910, 911, 912, 913, 914, 915, 916, 917, 918, 919, 920, 921, 922, 923, 924, 925, 926, 927, 928, 929, 930, 931, 932, 933, 934, 935, 936, 937, 938, 939, 940, 941, 942, 943, 944, 945, 946, 947, 948, 949, 950, 951, 952, 953, 954, 955, 956, 957, 958, 959, 960, 961, 962, 963, 964, 965, 966, 967, 968, 969, 970, 971, 972, 973, 974, 975, 976, 977, 978, 979, 980, 981, 982, 983, 984, 985, 986, 987, 988, 989, 990, 991, 992, 993, 994, 995, 996, 997, 998, 999, 1000

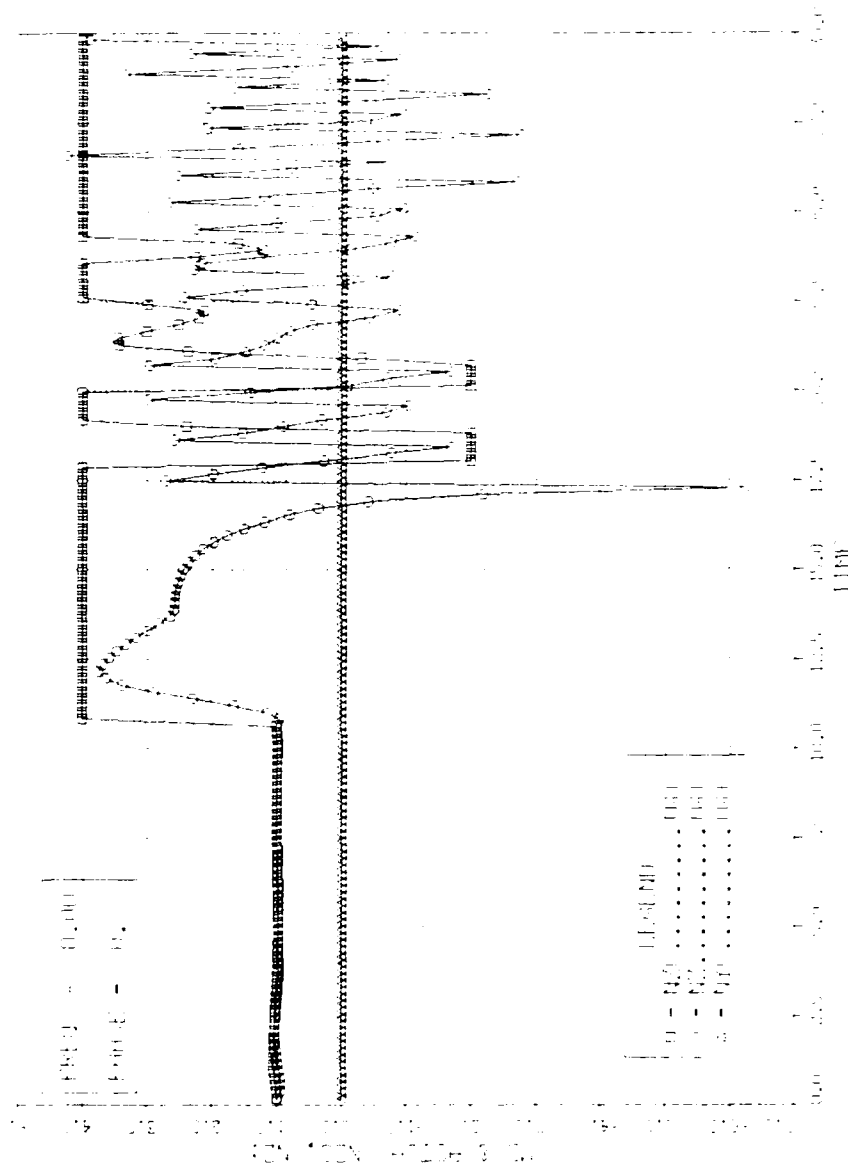


Figure A.82 Conf. VI Mission Set - Load Factor.

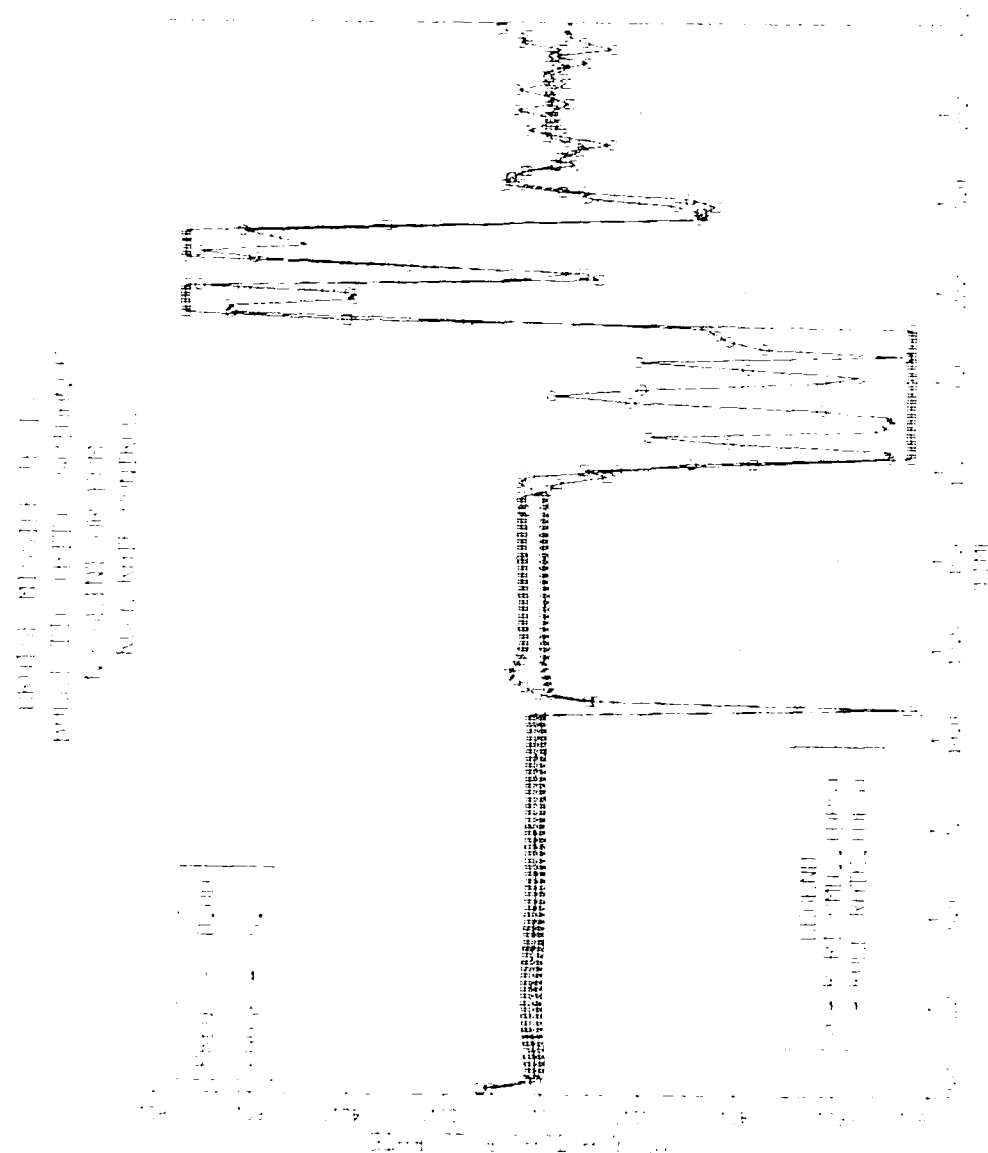


Figure A.84 Conf. VI Mission Set - Roll Rate.

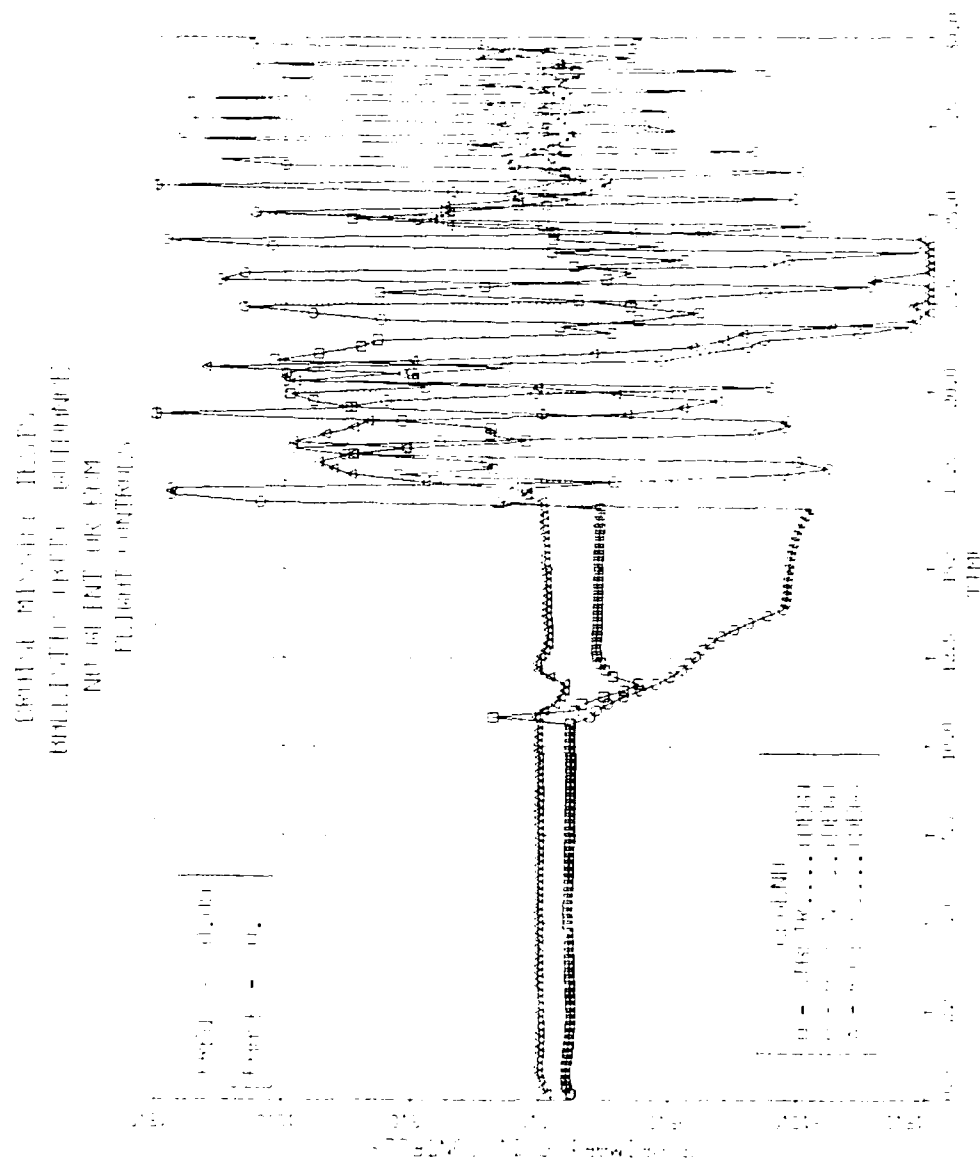


Figure A.85 Conf. VI Mission Set - Controls.

APPENDIX B

SIMULATION PROGRAM TABULAR DATA OUTPUT

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

SIMULATION TERMINATED DUE TO CPA
 *** BLINKER FREQUENCY = 0.20
 *** BLINKER PHASE

MISS	DISTANCE	BANK	ROLLRATE	ERROR	FUNCTIONS	AZIMUTH	ELEVATION
42.87372	*	0.20466	*	0.11202	*	0.03046	*
							0.00866

***** RANGES FOR ALL SAVED VARIABLES *****

	MINIMUM	MAXIMUM
TIME..... (SEC)	0.190000	29.061737
NZC..... (G)	0.289882	4.000000
NZ..... (G)	0.551692	3.750864
BANK..... (DEG)	-115.634293	92.840149
BANK..... (DEG)	-115.765106	84.187943
R/RT CMG..... (DPS)	-74.999985	74.999985
ROLL RATE..... (DPS)	-73.526184	73.167145
ECM SHIFT..... (FT)	-75.000000	75.000000
GLINT SHIF..... (FT)	-47.524835	47.070313
STBLTR..... (DLS)	-15.000000	7.934396
AIRLN..... (DEG)	-6.261881	0.000000

RUDDER.....(DEG)
 ALTITUDE.....(FT)
 XM.....(FT NORTH)
 YM.....(FT EAST)
 XT.....(FT NORTH)
 XM.....(FT EAST)
 RANGE.....(FT)
 PHASE MARKER

-3.440085
 13.361130
 159.440155
 -3.520452
 24000.000000
 6.649955
 110.888184
 0.000000

2.952714
 250.106537
 23887.324200
 1771.405030
 24000.000000
 1017.160640
 23840.589800
 4.000000

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 Hz
 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 1 OF 4

TIME.....(SEC)	NZC.....(G)	NZ.....(G)	BANK.....(DEG)	BANK.....(DEG)
0.190070	*	0.996454	*	0.838765
0.380000	*	1.002067	*	6.808969
0.570000	*	1.012286	*	6.645293
0.759999	*	1.022474	*	6.546911
0.949999	*	1.030748	*	6.503017
1.139989	*	1.036386	*	6.458877
1.329975	*	1.039639	*	6.585023
1.519961	*	1.040093	*	6.806047
1.709948	*	1.038448	*	6.744779
1.899934	*	1.034911	*	6.918423
2.089920	*	1.029593	*	7.007813
2.279906	*	1.023017	*	7.091106
2.469893	*	1.015957	*	7.323308
2.659879	*	1.008910	*	7.690206
2.849865	*	1.002075	*	8.092773
3.039851	*	0.995503	*	8.427508
3.229837	*	0.989945	*	8.742263
3.419824	*	0.983682	*	8.969087
3.609810	*	0.975212	*	9.224430
3.799796	*	0.972487	*	9.405898
3.989782	*	0.970403	*	9.605278
4.179769	*	0.970192	*	9.752930
4.369755	*	0.969642	*	9.988862
5.825313	*	0.984984	*	0.838765
6.542444	*	0.939250	*	6.808969
6.510144	*	0.935853	*	6.645293
6.556442	*	0.946945	*	6.546911
6.527555	*	0.962120	*	6.503017
6.279075	*	0.977738	*	6.458877
6.320140	*	0.951862	*	6.585023
6.580812	*	1.004217	*	6.806047
6.470833	*	1.014323	*	6.744779
6.623720	*	1.021769	*	6.918423
6.747380	*	1.027047	*	7.007813
6.834517	*	1.030146	*	7.091106
7.001084	*	1.030580	*	7.323308
7.254130	*	1.028598	*	7.690206
7.688922	*	1.024992	*	8.092773
8.050653	*	1.020577	*	8.427508
8.517364	*	1.015759	*	8.742263
8.645078	*	1.010625	*	8.969087
8.392548	*	1.005136	*	9.224430
9.108009	*	0.995566	*	9.405898
9.502847	*	0.994111	*	9.605278
9.474053	*	0.988990	*	9.752930
9.074053	*	0.984181	*	9.988862

4.555741	0.969938	0.979871	10.235960	9.915122
4.745727	0.970555	0.976926	10.229715	10.058768
4.935713	0.972024	0.974900	10.223241	10.101740
5.129700	0.973334	0.973648	10.338453	10.226965
5.319686	0.974787	0.973969	10.169158	10.063795
5.509672	0.976223	0.977441	9.974529	9.865085
5.699658	0.977961	0.974676	9.844348	9.706358
5.889645	0.980385	0.974635	9.897495	9.076970
6.079631	0.982658	0.975111	9.851146	9.668716
6.269617	0.985226	0.976146	9.896841	9.074454
6.459603	0.987471	0.977097	9.856885	9.069850
6.649590	0.989611	0.977964	9.846107	9.047773
6.839576	0.991370	0.981773	9.794549	9.013314
7.029562	0.993606	0.983401	9.991575	9.700086
7.219548	0.995817	0.985411	59.999954	11.834124
7.409534	1.097366	0.984173	59.999954	24.587097
7.599521	1.299035	0.803401	59.999954	37.007508
7.789507	1.677993	0.811473	59.999954	45.419754
7.979493	2.247480	0.916378	59.999954	58.482132
8.169479	2.473261	1.204178	59.999954	59.001837
8.359466	2.579926	1.523088	59.999954	55.080084
8.549452	2.618698	1.830282	59.999954	59.036536
8.739438	2.585437	1.115276	59.999954	55.560257
8.929424	2.495302	2.347334	59.999954	59.475677
9.119411	2.347077	2.504561	59.999954	59.397644
9.309397	2.161033	2.576695	59.999954	59.342728
9.499383	1.955719	2.563868	59.999954	55.316010
9.689369	1.749104	2.477899	59.999954	55.314651
9.879355	1.557662	2.332685	59.999954	55.346558
10.069342	1.354344	2.146254	59.999954	59.401413
10.259328	1.268420	1.938939	59.999954	55.469284
10.449314	1.184954	1.730132	59.999954	55.540421
10.639300	1.144872	1.536979	59.999954	59.066598
10.829287	1.050376	1.371496	0.000000	47.870846
11.019273	0.654307	1.266437	0.000000	34.769897
11.209255	0.533505	1.138158	0.000000	21.753655
11.399245	0.404801	1.010703	0.000000	8.865244
11.589231	0.440540	0.917152	0.000000	0.877188
11.779218	0.437432	0.851973	0.000000	-0.043441

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 1 OF 4

TIME.....(SEC) NZC.....(G) NZ.....(G) BANK.....(DEG)

11.969204	0.450394	0.768242	0.000000	0.000000	0.161884
12.159190	0.482046	0.685690	0.000000	0.000000	-0.162543
12.349176	0.5131986	0.614517	0.000000	0.000000	-0.135814
12.539163	0.557679	0.565422	0.000000	0.000000	-0.120245
12.729145	0.674333	0.551692	0.000000	0.000000	-0.108407
12.919135	0.757205	0.557850	0.000000	0.000000	-0.104236
13.109121	0.844995	0.584029	0.000000	0.000000	-0.105790
13.299108	0.924948	0.626355	0.000000	0.000000	-0.111587
13.489094	1.002845	0.679794	0.000000	0.000000	-0.119782
13.679080	1.073686	0.738611	0.000000	0.000000	-0.132744
13.869066	1.135511	0.804878	0.000000	0.000000	-0.148205
14.059052	1.186506	0.874575	0.000000	0.000000	-0.164887
14.249035	1.225576	0.943393	0.000000	0.000000	-0.181834
14.439025	1.252302	1.009762	0.000000	0.000000	-0.198240
14.629011	1.269858	1.065501	0.000000	0.000000	-0.213442
14.818997	1.261632	1.123638	0.000000	0.000000	-0.226920
15.008984	1.243847	1.165641	0.000000	0.000000	-0.238204
15.198970	1.218340	1.203627	0.000000	0.000000	-0.246988
15.388956	1.187195	1.235422	0.000000	0.000000	-0.253153
15.578942	1.152465	1.234756	0.000000	0.000000	-0.256717
15.768925	1.116103	1.224596	0.000000	0.000000	-0.253706
15.958915	1.079892	1.182526	0.000000	0.000000	-0.245153
16.148834	1.045580	1.154176	0.000000	0.000000	-0.243445
16.338730	1.013837	1.123310	0.000000	0.000000	-0.239110
16.528625	0.986244	1.092164	0.000000	0.000000	-0.233170
16.718521	0.963268	1.063370	0.000000	0.000000	-0.226391
16.908417	0.944965	1.036421	0.000000	0.000000	-0.219006
17.098312	0.931297	1.011223	0.000000	0.000000	-0.213910
17.288208	0.922266	0.988825	0.000000	0.000000	-0.209162
17.478104	0.917679	0.965775	0.000000	0.000000	-0.204973
17.667995	0.917206	0.944433	0.000000	0.000000	-0.201571
17.857891	0.920379	0.932518	0.000000	0.000000	-0.199403
18.047791	0.923043	0.935418	0.000000	0.000000	-0.198026
18.237686	0.935383	0.931596	0.000000	0.000000	-0.197525
18.427582	0.945946	0.931231	0.000000	0.000000	-0.197027
18.617477	0.957685	0.933928	0.000000	0.000000	-0.196614
18.807373	0.969778	0.933921	0.000000	0.000000	-0.196215
18.997265	0.982247	0.935664	0.000000	0.000000	-0.195815
19.187164	4.000000		-19.212936		

TIME.....(SEC)	NZC.....(G)	NZ.....(G)	DATA SET NUMBER	1 OF 4	BANK.....(DEG)	LEG
19.56956	*	*	1.336203	*	-19.645432	*
19.56851	*	*	1.903647	*	-20.514221	*
19.946747	*	*	2.603067	*	-21.803818	*
20.136642	*	*	3.165137	*	-23.917558	*
20.326538	*	*	3.547853	*	-26.628387	*
20.516434	*	*	3.707685	*	-29.875137	*
20.706325	*	*	3.750864	*	-33.380920	*
20.896225	*	*	3.655785	*	-37.201050	*
21.086121	*	*	3.743388	*	-46.270721	*
21.276016	*	*	3.527078	*	-91.988892	*
21.465912	*	*	3.080334	*	-97.266113	*
21.655807	*	*	2.546545	*	-102.053802	*
21.845703	*	*	2.077121	*	-106.587250	*
22.035595	*	*	2.733549	*	-109.825348	*
22.225494	*	*	1.687409	*	-111.873642	*
22.415350	*	*	1.724775	*	-113.150738	*
22.605286	*	*	1.736968	*	-114.502014	*
22.795181	*	*	1.709265	*	-115.634293	*
22.985077	*	*	1.647637	*	-115.255144	*
23.174973	*	*	1.550969	*	-114.066710	*
23.364868	*	*	1.428517	*	-110.889008	*
23.554764	*	*	1.257051	*	-106.212891	*
23.744655	*	*	1.162587	*	-98.385605	*
23.934555	*	*	1.033371	*	-87.793304	*
24.124451	*	*	0.913162	*	-61.075912	*

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 HZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

TIME.....(SEC) NZC.....(G) NZ.....(G) EANKC.....(DEG) BANK.....(LEG)

24.314346	*	*	0.312690	*	-41.207794	*
24.504242	*	*	0.289882	*	-12.722109	*
24.694138	*	*	0.323168	*	7.391577	*
24.884033	*	*	0.411515	*	14.987059	*
25.073925	*	*	0.560545	*	13.566058	*
25.263824	*	*	0.793154	*	11.106000	*
25.453720	*	*	1.025800	*	-68.765150	*
25.643616	*	*	1.258446	*	-56.286392	*
25.833512	*	*	1.491092	*	-43.769882	*
26.023408	*	*	1.723738	*	-31.229416	*
26.213304	*	*	1.956384	*	-18.679732	*
26.403200	*	*	2.189030	*	-6.130111	*

TIME.....(SEC)	R/RT CMD..(DPS)	ROLL RATE..(DPS)	ECM SHIFT..(FT)	GLINT SHIFT(FT)
25.453720	0.933357	0.581695	7.270296	5.453405
25.833616	1.042595	0.699352	5.325726	5.767002
25.833611	1.131395	0.796295	3.147260	3.985222
26.023407	1.231064	0.873536	2.354088	2.606244
26.213303	1.275287	0.949175	-1.190448	0.250407
26.403158	1.373239	1.020734	-1.089107	-1.234868
26.593094	1.474258	1.053145	-3.873116	-2.833504
26.782990	1.498616	1.170446	-3.584943	-3.880577
26.972885	1.534853	1.246133	-5.245676	-4.724376
27.162781	1.728691	1.302967	-1.781992	-1.055412
27.352676	2.026227	1.332957	10.870007	6.405855
27.542572	1.853992	1.533800	14.333593	8.333620
27.732468	2.105669	1.368543	48.266494	15.853433
27.922363	3.284542	1.460158	64.898895	31.915710
28.112259	4.000000	1.654933	70.102646	43.756592
28.302155	4.000000	2.015216	85.941116	55.250161
28.492050	4.000000	2.458335	92.840149	66.378754
28.681946	4.000000	2.864714	84.516556	77.037064
28.871841	4.000000	3.297837	87.914276	84.187943
29.061737	4.000000	3.747063	78.001495	81.152344

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 Hz
 9-19-84

*** BLINKER FREQUENCY= 0.20 DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CMD..(DPS) ROLL RATE..(DPS) ECM SHIFT..(FT) GLINT SHIFT(FT)

0.150000	12.067198	9.865781	-75.000000	19.921875
0.380000	2.970557	0.744763	-75.000000	47.070313
0.570000	1.389124	-0.660753	-75.000000	-43.310547
0.759995	1.571068	-0.488012	-75.000000	-25.952148
0.949999	1.868235	-0.235456	-75.000000	-15.886760
1.139985	1.916773	-0.222514	-75.000000	-47.524805
1.329975	2.881227	0.608558	-75.000000	45.671082
1.519961	2.381867	0.131125	-75.000000	-43.750000
1.709948	3.031882	0.885417	-75.000000	15.897461
1.899934	3.278272	0.850394	-75.000000	32.354405
2.089920	2.867801	0.508725	-75.000000	-27.555065

*	11.399245	*	-74.995985	*	-67.782478	*	-75.000000	*	-24.087524
*	11.589231	*	-10.854013	*	-11.366899	*	-75.000000	*	42.173767
*	11.779218	*	0.305608	*	-1.175964	*	-75.000000	*	-10.717773

CRUISE MISSILE TESTS
 BASELINE MISSION SET
 GLINT PLUS ECM AT 0.2 FZ
 9-19-84

*** BLINKER FREQUENCY= 0.20

DATA SET NUMBER 2 UF 4

TIME.....(SEC) R/RT CMD..(DPS) ROLL RATE..(DPS) ECM SHIFT..(FT) GLINT SHIFT(FT)

*	11.969204	*	1.725770	*	-0.077368	*	-75.000000	*	21.820172
*	12.159190	*	1.766047	*	0.153380	*	-75.000000	*	-22.363281
*	12.345176	*	1.522800	*	0.138551	*	-75.000000	*	-15.866780
*	12.535163	*	1.307845	*	0.090493	*	75.000000	*	-47.924805
*	12.729145	*	1.175968	*	0.044148	*	75.000000	*	45.671082
*	12.919135	*	1.126412	*	0.008935	*	75.000000	*	-43.750000
*	13.109121	*	1.140405	*	-0.015377	*	75.000000	*	15.857401
*	13.299108	*	1.198962	*	-0.031489	*	75.000000	*	32.354405
*	13.485094	*	1.287829	*	-0.049077	*	75.000000	*	-27.339063
*	13.679080	*	1.425424	*	-0.068103	*	75.000000	*	-42.953164
*	13.869099	*	1.591445	*	-0.075865	*	75.000000	*	37.622070
*	14.055052	*	1.771146	*	-0.078154	*	75.000000	*	-5.271912
*	14.245039	*	1.954254	*	-0.075742	*	75.000000	*	2.807017
*	14.435025	*	2.131940	*	-0.069467	*	75.000000	*	-5.204102
*	14.625011	*	2.256958	*	-0.060213	*	75.000000	*	-0.720215
*	14.818997	*	2.436211	*	-0.048663	*	75.000000	*	-3.415748
*	15.008984	*	2.568422	*	-0.035191	*	-75.000000	*	-5.082373
*	15.198970	*	2.63178	*	-0.021065	*	-75.000000	*	-3.227535
*	15.388956	*	2.731251	*	-0.007072	*	-75.000000	*	-14.042664
*	15.578942	*	2.771195	*	0.006111	*	-75.000000	*	-31.372070
*	15.768925	*	2.784501	*	0.017965	*	-75.000000	*	22.955322
*	15.958915	*	2.773720	*	0.028139	*	-75.000000	*	43.412781
*	16.148834	*	2.742187	*	0.036394	*	-75.000000	*	-14.065247
*	16.338730	*	2.653789	*	0.042625	*	-75.000000	*	2.099605
*	16.528625	*	2.63655	*	0.046833	*	-75.000000	*	31.255770
*	16.718521	*	2.565117	*	0.045088	*	-75.000000	*	-12.055313
*	16.908417	*	2.489133	*	0.049557	*	-75.000000	*	-26.857422
*	17.098312	*	2.414101	*	0.048846	*	-75.000000	*	-24.087524

17.288208	2.340792	0.046959	75.000000	42.173707
17.478104	2.271522	0.044037	75.000000	-10.717773
17.667999	2.208578	0.040282	75.000000	-21.826172
17.857895	2.153597	0.035907	75.000000	-22.363281
18.047791	2.107845	0.031138	75.000000	-15.886780
18.237686	2.072085	0.026206	75.000000	-47.524605
18.427582	2.046605	0.021321	75.000000	45.071082
18.617477	2.031211	0.016687	75.000000	-43.750000
18.807373	2.025372	0.012457	75.000000	19.857461
18.997265	2.028170	0.008771	75.000000	32.354405
19.187164	2.038470	0.005110	75.000000	-27.539005
19.377060	2.049985	0.001975	75.000000	-42.553104
19.566956	2.061747	0.000510	75.000000	37.622370
19.756851	2.073731	0.000000	75.000000	-5.271912
19.946747	2.085915	0.000000	75.000000	2.807617
20.136642	2.098255	0.000000	75.000000	-5.204102
20.326538	2.110734	0.000000	75.000000	-0.720215
20.516434	2.123255	0.000000	75.000000	-33.416748
20.706329	2.135855	0.000000	75.000000	-5.682375
20.896225	2.148455	0.000000	75.000000	-33.227555
21.086121	2.161055	0.000000	75.000000	-14.042604
21.276016	2.173655	0.000000	75.000000	-31.572070
21.465912	2.186255	0.000000	75.000000	22.955222
21.655807	2.198855	0.000000	75.000000	43.412781
21.845703	2.211455	0.000000	75.000000	-34.065247
22.035599	2.224055	0.000000	75.000000	2.059605
22.225494	2.236655	0.000000	75.000000	31.255776
22.415390	2.249255	0.000000	75.000000	-12.655515
22.605286	2.261855	0.000000	75.000000	-28.857422
22.795181	2.274455	0.000000	75.000000	-24.087524
22.985077	2.287055	0.000000	75.000000	42.173707
23.174973	2.300000	0.000000	75.000000	-10.717773
23.364868	2.312955	0.000000	75.000000	-21.826172
23.554764	2.325900	0.000000	75.000000	-22.363281
23.744659	2.338855	0.000000	75.000000	-15.886780
23.934555	2.351800	0.000000	75.000000	-47.524605
24.124451	2.364755	0.000000	75.000000	45.071082

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 HZ
9-19-84

*** BLINKER FREQUENCY= 0.20 DATA SET NUMBER 2 OF 4

TIME.....(SEC) R/RT CME...(CPS) ROLL RATE...(CPS) ECM SHIFT...(FT) GLINT SHIFT(FT)

24.314346	*	74.955985	*	65.262851	*	75.000000	*	-43.700000
24.504242	*	74.955985	*	65.786815	*	75.000000	*	15.997401
24.654138	*	74.955985	*	65.964462	*	75.000000	*	32.354405
24.884033	*	74.955985	*	66.055204	*	75.000000	*	-27.535065
25.073925	*	74.955985	*	66.085938	*	-75.000000	*	-42.953164
25.263824	*	74.955985	*	66.059158	*	-75.000000	*	37.622070
25.453720	*	22.935425	*	22.956116	*	-75.000000	*	-5.271912
25.643616	*	-5.669250	*	-6.440586	*	-75.000000	*	2.807617
25.833511	*	-10.200815	*	-10.561381	*	-75.000000	*	-9.204102
26.023407	*	-3.224416	*	-4.481498	*	-75.000000	*	-0.720215
26.213303	*	-17.724454	*	-17.331482	*	-75.000000	*	-35.416748
26.403198	*	-1.460428	*	-0.733393	*	-75.000000	*	-5.682373
26.593094	*	-12.043291	*	-13.444024	*	-75.000000	*	-33.227355
26.782990	*	3.221104	*	0.505555	*	-75.000000	*	-14.042664
26.972885	*	-7.714266	*	33.777487	*	-75.000000	*	-31.372070
27.162781	*	40.710358	*	33.784058	*	-75.000000	*	4.955322
27.352676	*	53.080215	*	44.755210	*	75.000000	*	45.412781
27.542572	*	66.124893	*	25.035751	*	75.000000	*	-34.065247
27.732468	*	74.955985	*	63.833176	*	75.000000	*	2.099605
27.922363	*	74.955985	*	62.675156	*	75.000000	*	31.255776
28.112255	*	74.955985	*	61.318130	*	75.000000	*	-12.655313
28.302155	*	74.955985	*	58.976955	*	75.000000	*	-28.857422
28.492050	*	74.955985	*	56.136641	*	75.000000	*	-24.087524
28.681946	*	74.955985	*	54.246460	*	0.000000	*	42.173707
28.871841	*	43.046890	*	24.955106	*	0.000000	*	-10.717773
29.061737	*	-38.403168	*	-41.171707	*	0.000000	*	21.060172

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 HZ
9-19-84

*** BLINKER FREQUENCY= 0.20 DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AIRLN.....(DEG) RUDDER.....(DEG) ALTITUDE....(FT)

50.04715C
50.089844
50.075516
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TIME.....(SEC)	STBLTR.....(DEG)	AILRON.....(DEG)	KODDER.....(DEG)	ALTITUDE....(FT)
9.115411	-3.565754	-3.222716	0.192114	41.088508
9.309397	-3.802303	-3.288725	0.248152	41.537570
9.459383	-3.889286	-3.262568	0.364863	41.000983
9.689365	-3.815103	-3.148677	0.485630	42.413740
9.879355	-3.543250	-2.976035	0.613060	43.850743
10.069342	-3.206109	-2.761302	0.718114	45.777054
10.259328	-2.801994	-2.526126	0.790657	47.981018
10.449314	-2.403330	-2.252121	0.826747	50.565045
10.639300	-2.053359	-2.077678	0.831056	52.159927
10.829287	2.765983	-2.031552	0.837751	53.158740
11.019273	3.203503	-1.638245	0.10612	57.002005
11.209255	3.445302	-1.337570	-0.511520	60.055918
11.399245	3.550609	-1.067041	-0.603214	62.670740
11.589231	-0.761381	-0.860477	-1.135111	65.250515
11.779218	-0.606800	-0.768152	-1.088782	67.755087

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 Hz
9-19-84

*** BLINKER FREQUENCY= 0.20 DATA SET NUMBER 3 OF 4

TIME.....(SEC) STBLTR.....(DEG) AILRON.....(DEG) KODDER.....(DEG) ALTITUDE....(FT)

11.969204	-0.915540	-0.655329	-0.792145	70.043457
12.159190	-0.818488	-0.529124	-0.461040	72.077484
12.349176	-0.699540	-0.417514	-0.218915	73.742950
12.539163	-0.612691	-0.335986	-0.095435	74.960114
12.729149	-0.56952	-0.305905	-0.054520	75.678207
12.919135	-0.557567	-0.324278	-0.055930	75.877514
13.109121	-0.575181	-0.376057	-0.073167	75.967385
13.299108	-0.611483	-0.457703	-0.095069	74.777695
13.489094	-0.661711	-0.561647	-0.110690	73.928517
13.679080	-0.739960	-0.676090	-0.125492	71.971645
13.869066	-0.826459	-0.795570	-0.138116	70.006105
14.059052	-0.917433	-0.928560	-0.148669	67.978912
14.249039	-1.006072	-1.056622	-0.156873	65.750785
14.439025	-1.094344	-1.177841	-0.162444	63.421967
14.629011	-1.177998	-1.287473	-0.165773	61.128918
14.818997	-1.264513	-1.381750	-0.165945	58.915155

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-1. 68654
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-1. 71774
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-1. 76454
-1. 76714
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-1. 77494
-1. 77754
-1. 78014
-1. 78274
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-1. 79054
-1. 79314
-1. 79574
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-1. 82174
-1. 82434
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-1. 89714
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-1. 90754
-1. 91014
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-1. 94654
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-1. 95954
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-1. 17154
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-1. 17274
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-1. 17394
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-1. 18534
-1. 18594
-1. 18654
-1. 18714
-1. 18774
-1. 18834
-1. 18894
-1. 18954
-1. 19014
-1

* 24.124451	* -4.849390	* -0.962144	* -0.114661	* 241.416747
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CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 FZ
9-19-84

*** PLINKER FREQUENCY= 0.20

CATA SET NUMBER 3 UF 4

TIME... (SEC) STBLTR... (CEG) AILRN... (DEG) RUDDER... (DEG) ALTITUDE... (FT)

[illegible]

CRUISE MISSILE TESTS
BASELINE MISSION SET

GLINT PLUS ELM AT 0.2 FZ 9-19-84

*** BLINKER FREQUENCY=

0.20

DATA SET NUMBER 4 LF 4

TIME.....(SEC) XM....(FT NORTH) YM....(FT EAST) XT....(FT NORTH) XM....(FT EAST)

0.190000	*	159.440155	*	-0.009810	*	24000.000000	*	6.049995
0.380000	*	318.873291	*	-0.049694	*	24000.000000	*	13.259989
0.570000	*	478.301758	*	-0.113570	*	24000.000000	*	15.949982
0.759995	*	637.728271	*	-0.201762	*	24000.000000	*	26.559976
0.949995	*	797.151011	*	-0.313580	*	24000.000000	*	33.249965
1.139989	*	956.573486	*	-0.448021	*	24000.000000	*	35.859977
1.329975	*	1115.991400	*	-0.603947	*	24000.000000	*	46.545118
1.519961	*	1275.407716	*	-0.779674	*	24000.000000	*	55.158655
1.709948	*	1434.820310	*	-0.973391	*	24000.000000	*	55.848160
1.899934	*	1594.228760	*	-1.182685	*	24000.000000	*	66.457681
2.089920	*	1753.632810	*	-1.404678	*	24000.000000	*	73.147202
2.279906	*	1913.032470	*	-1.636795	*	24000.000000	*	75.756707
2.469893	*	2072.426510	*	-1.876554	*	24000.000000	*	86.446228
2.659879	*	2231.814940	*	-2.120413	*	24000.000000	*	93.055745
2.849865	*	2391.157750	*	-2.362842	*	24000.000000	*	95.745270
3.039851	*	2550.574710	*	-2.557082	*	24000.000000	*	106.354791
3.229837	*	2709.944090	*	-2.816305	*	24000.000000	*	113.044296
3.419824	*	2869.307860	*	-3.014300	*	24000.000000	*	119.053817
3.609810	*	3028.665530	*	-3.185804	*	24000.000000	*	126.343338
3.799796	*	3188.016300	*	-3.326302	*	24000.000000	*	132.952855
3.989782	*	3347.361530	*	-3.432030	*	24000.000000	*	135.042380
4.179765	*	3506.700200	*	-3.459740	*	24000.000000	*	140.251885
4.369755	*	3666.032710	*	-3.526452	*	24000.000000	*	152.941406
4.559741	*	3825.359620	*	-3.508787	*	24000.000000	*	155.550927
4.749727	*	3984.681400	*	-3.443329	*	24000.000000	*	166.240448
4.939713	*	4143.984370	*	-3.327466	*	24000.000000	*	172.859305
5.129700	*	4303.257810	*	-3.155135	*	24000.000000	*	175.539490
5.319686	*	4462.531250	*	-2.938205	*	24000.000000	*	180.188955
5.509672	*	4621.804690	*	-2.666635	*	24000.000000	*	192.838516
5.699658	*	4781.078120	*	-2.347534	*	24000.000000	*	199.488037
5.889645	*	4940.351560	*	-1.983534	*	24000.000000	*	206.137558
6.079631	*	5099.825000	*	-1.525941	*	24000.000000	*	212.787075
6.269617	*	5258.898440	*	-1.125271	*	24000.000000	*	219.436584
6.459603	*	5418.171870	*	-0.631455	*	24000.000000	*	226.086105
6.649590	*	5577.444510	*	-0.054406	*	24000.000000	*	232.735026

TIME.....(SEC)	XM....(FT NORTH)	YM....(FT EAST)	XI....(FT NORTH)	XM....(FT EAST)
6.839576	5736.703120	0.485856	24000.000000	255.385147
7.029562	5895.902340	1.109634	*24000.000000	246.034608
7.219548	6055.101560	1.785213	*24000.000000	252.684174
7.409534	6214.300780	2.594645	*24000.000000	259.333496
7.599521	6373.500300	3.660096	*24000.000000	265.583154
7.789507	6532.699220	5.144712	*24000.000000	272.632568
7.979493	6691.898440	7.223592	*24000.000000	279.282227
8.169479	6851.023440	10.115357	*24000.000000	285.931641
8.359466	7010.148440	14.135207	*24000.000000	292.581055
8.549452	7169.210940	19.605545	*24000.000000	299.230713
8.739438	7328.160160	26.823135	*24000.000000	305.880147
8.929424	7486.953120	36.051483	*24000.000000	312.529785
9.119411	7645.527340	47.457543	*24000.000000	319.179195
9.309397	7803.820310	61.294495	*24000.000000	325.828857
9.499383	7961.785160	77.454766	*24000.000000	332.478271
9.689369	8119.371090	96.073334	*24000.000000	339.127086
9.879355	8276.554690	116.038950	*24000.000000	345.777344
10.069342	8433.333590	139.948761	*24000.000000	352.426758
10.259328	8589.730470	164.924744	*24000.000000	359.076418
10.449314	8745.746090	191.672058	*24000.000000	365.725830
10.639300	8901.429690	219.956425	*24000.000000	372.375488
10.829287	9056.800780	249.667542	*24000.000000	379.024502
11.019273	9211.929690	280.360840	*24000.000000	385.674316
11.209259	9366.850620	311.764160	*24000.000000	392.323975
11.399245	9521.742190	343.555176	*24000.000000	398.973385
11.589231	9676.562500	375.463623	*24000.000000	405.623047
11.779218	9831.382810	407.341797	*24000.000000	412.272401

CRUISE MISSILE TESTS
BASELINE MISSION SET
GLINT PLUS ECM AT 0.2 Hz
9-19-84

*** BLINKER FREQUENCY=	0.20	DATA SET NUMBER	4	OF	4
11.965204	* 9986.203120	* 435.127930	* 24000.000000	* 418.522115	
12.159190	* 10141.523420	* 470.755654	* 24000.000000	* 425.571553	
12.349176	* 10295.845700	* 502.336670	* 24000.000000	* 432.220947	
12.539163	* 10450.663600	* 533.751709	* 24000.000000	* 438.670005	

* * *	27.732468	*22811.261700	*1137.262230	*24000.000000	* * *	970.856230
* * *	27.922363	*22964.343700	*1110.862550	*24000.000000	* * *	977.282715
* * *	28.112255	*23117.585900	*1085.108890	*24000.000000	* * *	983.528955
* * *	28.302155	*23271.027300	*1060.465970	*24000.000000	* * *	990.575195
* * *	28.452050	*23424.718700	*1037.558840	*24000.000000	* * *	997.271680
* * *	28.681946	*23578.683600	*1017.097500	*24000.000000	* * *	1005.897920
* * *	28.871841	*23732.902300	*999.782715	*24000.000000	* * *	1010.514400
* * *	29.061737	*23887.324200	*986.245850	*24000.000000	* * *	1017.160640

APPENDIX C

TASM SIMULATION PROGRAM NOMENCLATURE

CONFCL

TIME IN SECONDS
INTEGRATION INTERVAL
OUTPUT INTERVAL
NUMBER OF OUTPUT SETS SAVED
FLAG SET TO INDICATE TERMINATION & REASON
ARRAY CONTAINING ALL SAVED DATA
SETS THE PHASE APPLIED TO ECM BLINKER
SETS THE RANGE AT WHICH CLIMB IS COMMENCED

MISSILE DYNAMICS

U,V,W, VDOT, WDOT
P,Q,R, PTCHRT, YAWRT
PCCT, QDOT, RDOT
X,Y,Z
LA, MA, NA
PFI, THETA, SY
BANK, PITCH, HEADING
PHICCT, THETAD, SYDOT
ALFA, BETA
ACA, SIDESL
ALFADT, BETADT
GAMMA
FLTPTH
NY, NZ
XM, YM, ALTUDE
XPCT, YMDOT, HMDOT
VT
CFLRD, SPAN
CFLRD2, SPAN2
BODY AXIS LINEAR VELOCITIES (FT/SEC)
BODY AXIS LINEAR ACCELERATIONS (RAD/SEC)
BODY AXIS ANGULAR VELOCITIES (DEG/SEC)
BODY AXIS ANGULAR ACCELERATIONS (DEG/SEC)
BODY AXIS AERODYNAMIC FORCES (LBS)
LIFT, DRAG, AERODYNAMIC FORCES (LBS)
BODY AXIS AERODYNAMIC MOMENTS (FT-LBS)
EULER ANGLES (RAD)
" " RATE OF CHANGE OF (DEG)
ANGLE OF ATTACK, SLIP (RAD)
RATE OF CHANGE OF ALFA, BETA (DEG)
FLIGHT PATH ANGLE (RAD)
" " (DEG)
LATERAL ACCELERATION, LOAD FACTOR (G'S)
EARTH COORDINATES OF MISSILE (FT)
(AM-NORTH, YM-EAST)
RATES OF CHANGE OF XM, YM, ALTITUDE (FT/SEC)
TOTAL MISSILE VELOCITY (FT/SEC)
MEAN AERODYNAMIC CHORD, SPAN (FT)
HALF CHORD, HALF SPAN

WT,M,G
T,S
RFC
US
C--
DC--
IAX,IYV,IZZ,IXZ
IA- IK
ELE,AII,RUD
STBLTR,AII,IRON,RUDDER
RSTAB1,LSSTAB1
RSTAB,LSSTAB
---I
GROSS WEIGHT, MASS, ACCEL DUE TO GRAVITY
THRUST, WING AREA
AIR DENSITY
DYNAMIC PRESSURE X WING AREA
AERODYNAMIC COEFFICIENTS
INCREMENTS IN
MOMENTS AND PRODUCTS OF INERTIA
FUNCTIONS OF
STANDARD CONTROL DEFLECTIONS (DEG)
CONTROL DEFLECTIONS WITH LIMITS
APPLIED (DEG)
TASM UNLIMITED CONTROL DEFLECTIONS (DEG)
TASM LIMITED CONTROL DEFLECTIONS (DEG)
INITIAL CONCITION

AUTCPILLOT

K---
CGARM-
E---
---LIM
---SERI
---SERC
---C
---F,---FF,---FFF
FACCF-,FDCOF-
AUTCPILLOT GAINS
ACCELEROMETER LOCATION WRT CG
COMPARATOR ERRORS
LIMITED VALUES
SERVO INPUTS
SERVO OUTPUTS
COMMANDED VALUES
FILTERED SENSOR VARIABLE
NOTCH FILTER COEFFICIENTS

GUIDANCE

AZC,AYC
XI,YT,HT
XR,YR,HR
XREC,M,YREC,M,HREC,M
XDCTR,YDCTR,HDOCTR
XECM,YECM,HECM
XGLNT,YGLNT,HGLNT
RANGE
RNGECM,RGECMT
TSPEED
SYT,THETAT
HEAUT,ELEV
VTANAZ,VTANEL
TRAKAZ,TRAKEL
COMMANDED VERTICAL AND HORIZONTAL
ACCELERATIONS IN EARTH AXES (G,S)
EARTH COORDINATES OF TARGET (FT)
POSITION OF THE TARGET WRT MISSILE IN
EARTH COORDINATES (FT)
POSITION OF RADAR TARGET (XR,YR,HR WITH ECM
AND GLINT ADDED WRT MISSILE (FT)
RATES OF CHANGE OF XREC,M,YREC,M,HREC,M (FT/S)
(RELATIVE VELOCITY OF TGT WRT MISSILE)
INCR. IN TARGET RADAR POSITION DUE TO ECM
INCR. IN TARGET RADAR POSITION DUE TO GLINT
RANGE TO TARGET (FT)
RANGE TO RADAR TARGET (TGT WITH ECM+GLINT)
TARGET SPEED (FT/SEC)
HEADING, ELEV. TC TARGET FROM MISSILE (RAD)
HEADING, ELEV. TC TARGET FROM MISSILE (DEG)
COMPONENT OF RELATIVE VEL. PERPENDICULAR
TO LOS IN AZIMUTH AND ELEVATION (FT/SEC)
COMPONENT OF MISSILE VELOCITY VECTOR IN

AZIMUTH AND ELEVATION (FT/SEC)
 EARTH AZIMUTH, ELEVATION LOS ANGLES (RAD)
 EARTH AZIMUTH, ELEVATION LOS ANGLES (DEG)
 RATES OF CHANGE OF EARTH REFERENCED LOS
 (RAD/SEC)
 SAME AS ABOVE (DEG/SEC)
 FILTERED SIGDAI, SIGDET (RAD/SEC)
 FILTERED DSGCAI, CSGDET (DEG/SEC)
 PROPORTIONAL NAVIGATION CONSTANTS
 FREQUENCY OF ECM BLINKING
 DISTANCE OF ECM BLINKER FROM TARGET AIM
 POINT (FT)
 BURN-THROUGH RANGE
 AZIMUTH AND ELEVATION NAVIGATION FILTER
 CONSTANTS

SIGAZ, SIGEL
 DSGAZ, DSGEL
 SIGDAZ, SIGDEL
 DSGCAZ, DSGDEL
 SICCAF, SIGDEF
 DSGCAF, DSGDEF
 LAMCAZ, LAMDEL
 FREQ
 SFIFTY, SHIFTH
 BRNTHR
 KNFAZ, KNFEL

APPENDIX D
MAIN PROGRAM LISTING
FOR
TACTICAL CRUISE MISSILE SIMULATION

TRANSLATED BY
CDR BARTEN P. ANDERSON, USN

NAVY POSTGRADUATE SCHOOL
DEPARTMENT OF AERONAUTICAL ENGINEERING
MCNTEREY, CA 95943

TRANSLATED FROM CSMP PROGRAM BY
DR. MARLE HEWETT
LCDR KENT WATTERSON, USN

PROGRAM TCMC

CONTROLS THE OVERALL EXECUTION OF THE SIMULATION. CALLS THE
NECESSARY SUBROUTINES, DETERMINES WHEN THE DATA MUST BE STORED
FOR OUTPUT AND WHEN THE RUN HAS COMPLETED DUE TO CPA OR FINTIM.

9-10-84

IMPLICIT REAL (A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE

COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS

COMMON /A/ TIME , FINTIM, DT , CPUT , NUT , NPTS , CPA , PCOUNT,
IXX , IYY , RHO , PI , PII , MASS , WT , S ,
ID , IE , IZ , IXZ , IA , IB , IC ,
CHORD2, CHORD , SPAN2, SPAN , NFAZE , II , IJ , IK ,

COMMON BLOCK /H/: ECM/GLINT PARAMETERS

[illegible]

```

C      CALL MISSN1
C
C      *** GENERATE CONTROL MOVEMENTS: STBLTR, AILKON, RUDDER
C      CALL APILOT
C
C      *** GENERATE MISSILE MOTION AND POSITION
C      CALL AERO
C
C      *** GENERATE APPARENT RADAR TARGET POSITION & MOTION
C      CALL TGTNAV
C
C      *** STORE REQUIRED PLOT DATA IN THE PTS ARRAY.
C      IF (PCOUNT.LT.NCUT) GO TO 50
C      CALL PREPAR
C      PCOUNT = 0.0
C      5C CONTINUE
C      GC TO 10
C      10C CONTINUE
C      *** END DYNAMIC SIMULATION *****
C      *** INVOKE DISSPLA AND TABULAR OUTPUT ROUTINES
C      CALL CLTPUT(NPTS,CPA)
C      ***** TESTPATCH TO BYPASS ITERATIONS (KTEST = 1)
C      KTEST = 0
C      IF (KTEST.EQ.1) GC TO 150
C      ***** ENDTEST
C      *** ITERATE THE PHASE VARIABLE IN THE ECM PACKAGE
C      NFAZE = NFAZE + 1
C      IF (NFAZE.LE.4) GO TO 1
C      NFAZE = 1

```

```

C *** ITERATE THE BLINKER FREQUENCY
C
C   FREQ = FREQ +5.0
C   IF (FREQ-LE-30.0) GC IC 1
C   CALL CCNEPL
C
C   STOP
C   END
C
C ***** 9-07-84 *****
C ***** SUBROUTINE INIT *****
C ***** BLCCCK DATA *****
C ***** CONTAINS DATA STATEMENTS AND ASSIGNMENT STATEMENTS FOR *****
C ***** VARIABLES NOT INITIALIZED IN THE BLCCCK DATA SUBPROGRAM *****
C ***** ALSO REINITIALIZES INITIAL CONDITIONS FOR MORE THAN ONE RUN *****
C *****
C ***** IMPLICIT REAL(A-Z) *****
C ***** INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE *****
C
C ***** COMMON /A/ TIME , FLWTIM,DT , CPDT , NULT , NPTS , CPA , PCOUNT, *****
C ***** IXX , IYY , IZZ , IXXZ , IIA , IIB , IIC , IIS , IJK , *****
C ***** ID , IIF , IIG , IIAZ , IIBZ , IICZ , IISZ , IJKZ , *****
C ***** CHUR02,CHURC , SPAN2,SPAN ,NFAZE *****
C
C ***** COMMON /C/ KPTCHR , KROLLR , KYAWRT , CGARML , KBANK , *****
C ***** KRTLLM , PLIM , KNY , KNYRUDCLR , CGARML , CUARMN , *****
C ***** ATLRON , STBLTR , RUDCLR , NYSEK , KNY , KNYRUDCLR , *****
C ***** BSEK , NZSEK , NYSEK , NYSEK , *****
C
C ***** COMMON /G/ ALFA , BETA , VT , W , THETA , SY , CK , *****
C ***** U , P , PDOT , ALTUDE , *****
C ***** PHI , GAMMA , CL , P , BETA , NZ , XMDLT , *****
C ***** CU , CM , CN , ALFADT , RDLT , *****
C ***** R , QOUT , YM , *****
C ***** X4 , *****
C
C ***** COMMON /E/ XMI , PITCHI , YMI , BANKI , *****
C ***** *****

```

```

C
* *
* *      AJA1      PITCHK1      ROLLK1      YAWK1
* *      XT1       VTI        HT1       JSPEED
*
* *      COMMON /F/  PH1 OFF SET      PH3      PH4
* *      LAMDAZ      LAMTATT      SGCZPU      MISUST
* *      NZC          LAMUEL      KNFAZ      KNFEL
* *      PC           PHIC        GAMMAC      PLLIM
* *      SIGAZ       SIGEL        RC          RANGE
* *      SYT         THETAT      SIGDEF      ST
* *      HT          NYC          PUPRNG      YI
*
C
* *      COMMON /H/  FREQ      SHIFTY      SHIFTH      DRNTHK
* *      XECM        YECM       HGLNT       HECM        XGLNT
* *      HTECM      HGLNT       XT ECM      YTECM
*
C
* *      COMMON /I/  PTS(300,20)
*
C
EXECUTABLE STMTS *****
C
** COMPUTEL CONSTANTS
C
PII= 1EC.0/PI
IA = IXX*IZZ-IXZ**2
IB = IZZ/IA
IC = IXZ/IA
ID = IXZ*(IYY-IXX-IZZ)/IA
IE = (IZZ**2-IYY*IZZ+IXZ**2)/IA
IF = I/IVY
IG = (IXX-IZZ)/IVY
IH = IXZ/IVY
II = IXX/IA
IJ = (IXX*IYY-IXX**2-IXZ**2)/IA
IK = (IXX+IZZ-IVY)*IXZ/IA
C
PLIM = RRLIM/PII
C
*****
PARAMETERS TO BE INITIALIZED FOR EACH RUN FOLLOW.
*****
C
TIME = C.0
CPA = C
PCOUNT = 0
NOUT = INT(CPUT/DT)
IF (AMLC(CPUT,DT).GE.0.5) NOUT=NOUT+1
*****

```

```

C      NPTS = C
DU 100 I=1,300
DC 50 J=1,20
      PTS(I,J) = 0.0
5C      CCNTINLE
10C CONTINUE
C
U = LI
W = LI*TAN(AOAL/PII)
V = SRT(U**2+W**2)*TAN(SIDESL/PII)
VT = SRT(U**2+V**2)
QS = 12.0*RH0*(VT**2)/2.0
C
P = FCLRL/PII
Q = FTCHRL/PII
R = VAWRL/PII
C
PDCT = 0.0
QDCT = 0.0
RDOT = 0.0
C
THETA = PITCH1/PII
PHI = BANK1/PII
SY = HEDNG1/PII
GAMMA = 0.0
NZ = 1.0
C
XM = XM1
YM = YM1
ALTUDE = ALTUD1
C
AOA = ACAI
ALFA = ACAI/PII
ALFADT = 0.0
C
SICESL = SIDESI
BETA = SIDESI/PII
BETAUT = 3.0
C
XT = XTI
YT = YTI
HT = HTI
KANGE = SRT((XT-XM)**2+(YT-YM)**2+(HT-ALTUDE)**2)
C
PH1 = 0
PH2 = C

```

```

PH3 = C
PH4 = C
C *** INITIAL CONTROL POSITIONS
C
ELEI = -1.0
AII I = 0.0
RUDI = 0.0
C
NZ SERC = -ELEI/PII
BSERO = -AII I/PII
NY SERO = -RUDI/PII
C *** INITIAL ACCELERATIONS & COMMANDED RATES
C
NZ = 1.0
NY = 0.0
C
PC = C.0
QC = -ELEI/PII
RC = 0.0
C *** PARAMETERS TO BE CHANGED FROM BASELINE VALUES
C
FINTIM = 30.0
KRCLLK = 0.5
ALTATT = 0.0
BRNTHR= 500
C
SIGDAF = TSPEED/XTI
SIGDEF = (HTI-ALTCU1)*UI/XTI**2
C
RETURN
END
CCCCC
9-07-84
*****
BLCK DATA SUBPROGRAM TO INITIALIZE COMMON BLOCKS OF MEMORY.
*****
BLOCK DATA
*****
C
C
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,NPTS,CPA,NULT,PCOUNT,TITLE,PLIN,LECU,XIN,

```

C	*	COMMON	/A/	TIME	FINTIM,DT	OPDT	NCUT	NPTS	CPA	PCOUNT
	*		G	T	RHO	PI	PII	MASS	WT	S
	*		IXX	IYY	IZZ	IXZ	IA	IB	IC	QS
	*		ID	IE	IF	IG	IF	II	IJ	IK
	*		CHORD2	CHORD	SPAN2	SPAN	HAFAZ			
C	*	COMMON	/B/	LFT1(2,36)	LFT2(2,36)	DRG1(2,36)	DRG2(2,36)			
	*		DRG3(2,36)	DRG4(2,36)	SID2(6,10)	SID3(6,10)	PITCH2(2,36)			
	*		SID1(6,10)	SID2(6,10)	DKEC3(6,10)	LTRL1(6,10)	DRECI(6,10)			
	*		DRREC2(6,10)	CLADT	COACT	CMADT	LTRL2(6,10)			
	*		LTRL3(6,10)	CUQ	CMC	CRBLT				
	*		CLQ	CNBUT	CCR	CYP				
	*		CYR	CRP	CYBCT	CNP				
	*		CNR							
C	*	COMMON	/C/	KPTCHR	KROLLR	KYAWRT	KBAN			
	*		KGAMMA	KALT	CGARML	CGARML	CGARML			
	*		RRTLLIM	PLIM	KNY	KNZ				
	*		AILLRON	STBLTR	RUDDER					
	*		BSERO	NZSERU	NYSERU					
C	*	COMMON	/D/	ALFA	BETA	VT	HMDUT			
	*		U	V	W					
	*		PHI	GAMMA	THETA	SY				
	*		CD	CY	CL	CR				
	*		C4	CN	P	Q				
	*		R	ALFADT	BETADT	PDOT				
	*		WDUT	RDCT	NZ	ALTUDE				
	*		X4	YM	XMDCT	YMDUT				
C	*	COMMON	/E/	XMI	YMI	ALTUD1	UI			
	*		PITCH1	BANK1	HECAG1	SI DESI	SI DESI			
	*		AOA1	PITCHR1	RULLK1	YAWRI	YAWRI			
	*		XT1	YTI	HT1	TSPEED	TSPEED			
C	*	COMMON	/F/	PH1	PH2	PH3	PH4			
	*		CHFFSET	ALTATT	SGDPU	MI SUST	MI SUST			
	*		LAMDZ	LAMDZ	KNFAZ	KNFEL	KNFEL			
	*		NZC	PHIC	GAMMAC	PULLIM	PULLIM			
	*		PC	QC	RC	RANGE	RANGE			
	*		SIGAZ	SIGEL	SI GDAF	SI GULF	SI GULF			
	*		SYT	THETAT	XT	YI	YI			
	*		FT	NYC	PUPKNG					
C	*	COMMON	/H/	FREQ	SHIFTY	SHIFTH	BRNTHK			
	*		XECM	YECM	HECM	XULNT	XULNT			

```

**          YGLNT      HGLNT      XTECM      YTECM      .
**          PTECM
*****
COMMON BLOCK /1/: OUTPUT ARRAY
*****
COMMON /1/ PIS(300,20),PLIN(6,7),XN(6,7),YN(6,7),TITLE(8,4),
LEG(4,20)
*

*** INITIALIZE THE DATA
*****
COMMON ELCCCK /A/: MISCELLANEOUS CONSTANTS
*****
DATA      TIME      FINTIM      DT      GPDIT      CPA      /
/C.0      /30.0      /0.01      /0.20      /0
*
DATA      G      T      RHU      PI      WT      MASS      /
/32.17      /242.3      /0.002377      /3.141593      /2200.      /68.38
*
DATA      IXX      IYY      IZZ      IXZ      S      /
/27.8      /1507.0      /1512.0      /11.7      /12.0
*
DATA      CHURD2,CHORD      SPAN2      SPAN      NFAZE      /
/0.707      /1.414      /4.2425      /8.485      /1
*

*****
COMMON ELCCCK /8/: AERODYNAMIC COEFFICIENT TABLES
*****

** STATIC AERODYNAMIC COEFFICIENTS
* 1. LIFT COEFFICIENT DATA
A. CLBAS VS. AOA (BASIC LIFT COEFFICIENT AS A FUNCTION
OF ANGLE OF ATTACK)
DATA LFT1/ -12.0,-0.32, -11.0,-0.29, -10.0,-0.46, -9.0,-0.57,
-8.0,-0.70, -7.0,-0.69, -6.0,-0.65, -5.0,-0.56,

```

```

*      -4.0, -0.50,      -3.0, -0.42,      -2.0, -0.30,      -1.0, -0.18,
*      0.0,  0.08,      1.0,  0.04,      2.0,  0.15,      3.0,  0.25,
*      4.0,  0.38,      5.0,  0.47,      6.0,  0.58,      7.0,  0.69,
*      8.0,  0.80,      9.0,  0.87,      10.0,  0.98,      11.0,  0.99,
*      12.0,  0.94,      22*9999.0/

```

CCCCC

B. DCLSTIE VS. SIBLTR (INCREMENT IN LIFT COEFFICIENT DUE TO SYMMETRIC STABILATOR DEFLECTION)

```

DATA LFT2/ -15.0, -100,      -14.0, -0.97,      -13.0, -0.94,      -12.0, -0.90,
*      -11.0, -0.84,      -10.0, -0.76,      -9.0, -0.71,      -8.0, -0.69,
*      -7.0, -0.59,      -6.0, -0.48,      -5.0, -0.40,      -4.0, -0.32,
*      -3.0, -0.24,      -2.0, -0.16,      -1.0, -0.08,      0.0,  0.00,
*      1.0,  0.08,      2.0,  0.16,      3.0,  0.24,      4.0,  0.33,
*      5.0,  0.41,      6.0,  0.49,      7.0,  0.57,      8.0,  0.65,
*      9.0,  0.73,      10.0,  0.80,      11.0,  0.86,      12.0,  0.92,
*      13.0,  0.96,      14.0,  0.98,      15.0,  1.00,      10*9999. /

```

CCCCCCCC

* 2. DRAG COEFFICIENT DATA

A. CCBAS VS. CLBAS (BASIC DRAG COEFFICIENT AS A FUNCTION OF BASIC LIFT COEFFICIENT)

```

DATA DRG1/ -9,  0.80,      -8,  0.61,      -7,  0.50,      -6,  0.42,
*      -5,  0.35,      -4,  0.31,      -3,  0.28,      -2,  0.23,
*      -1,  0.22,      0,  0.20,      1,  0.18,      2,  0.16,
*      3,  0.14,      4,  0.12,      5,  0.10,      6,  0.08,
*      7,  0.07,      8,  0.06,      9,  0.05,      10,  0.04,
*      11,  0.03,      12,  0.02,      13,  0.01,      14,  0.00,
*      15,  0.00,      16,  0.00,      17,  0.00,      18,  0.00,
*      19,  0.00,      20,  0.00,      21,  0.00,      22,  0.00,
*      23,  0.00,      24,  0.00,      25,  0.00,      26,  0.00,
*      27,  0.00,      28,  0.00,      29,  0.00,      30,  0.00,
*      31,  0.00,      32,  0.00,      33,  0.00,      34,  0.00,
*      35,  0.00,      36,  0.00,      37,  0.00,      38,  0.00,
*      39,  0.00,      40,  0.00,      41,  0.00,      42,  0.00,
*      43,  0.00,      44,  0.00,      45,  0.00,      46,  0.00,
*      47,  0.00,      48,  0.00,      49,  0.00,      50,  0.00,
*      51,  0.00,      52,  0.00,      53,  0.00,      54,  0.00,
*      55,  0.00,      56,  0.00,      57,  0.00,      58,  0.00,
*      59,  0.00,      60,  0.00,      61,  0.00,      62,  0.00,
*      63,  0.00,      64,  0.00,      65,  0.00,      66,  0.00,
*      67,  0.00,      68,  0.00,      69,  0.00,      70,  0.00,
*      71,  0.00,      72,  0.00,      73,  0.00,      74,  0.00,
*      75,  0.00,      76,  0.00,      77,  0.00,      78,  0.00,
*      79,  0.00,      80,  0.00,      81,  0.00,      82,  0.00,
*      83,  0.00,      84,  0.00,      85,  0.00,      86,  0.00,
*      87,  0.00,      88,  0.00,      89,  0.00,      90,  0.00,
*      91,  0.00,      92,  0.00,      93,  0.00,      94,  0.00,
*      95,  0.00,      96,  0.00,      97,  0.00,      98,  0.00,
*      99,  0.00,      100,  0.00,      101,  0.00,      102,  0.00,
*      103,  0.00,      104,  0.00,      105,  0.00,      106,  0.00,
*      107,  0.00,      108,  0.00,      109,  0.00,      110,  0.00,
*      111,  0.00,      112,  0.00,      113,  0.00,      114,  0.00,
*      115,  0.00,      116,  0.00,      117,  0.00,      118,  0.00,
*      119,  0.00,      120,  0.00,      121,  0.00,      122,  0.00,
*      123,  0.00,      124,  0.00,      125,  0.00,      126,  0.00,
*      127,  0.00,      128,  0.00,      129,  0.00,      130,  0.00,
*      131,  0.00,      132,  0.00,      133,  0.00,      134,  0.00,
*      135,  0.00,      136,  0.00,      137,  0.00,      138,  0.00,
*      139,  0.00,      140,  0.00,      141,  0.00,      142,  0.00,
*      143,  0.00,      144,  0.00,      145,  0.00,      146,  0.00,
*      147,  0.00,      148,  0.00,      149,  0.00,      150,  0.00,
*      151,  0.00,      152,  0.00,      153,  0.00,      154,  0.00,
*      155,  0.00,      156,  0.00,      157,  0.00,      158,  0.00,
*      159,  0.00,      160,  0.00,      161,  0.00,      162,  0.00,
*      163,  0.00,      164,  0.00,      165,  0.00,      166,  0.00,
*      167,  0.00,      168,  0.00,      169,  0.00,      170,  0.00,
*      171,  0.00,      172,  0.00,      173,  0.00,      174,  0.00,
*      175,  0.00,      176,  0.00,      177,  0.00,      178,  0.00,
*      179,  0.00,      180,  0.00,      181,  0.00,      182,  0.00,
*      183,  0.00,      184,  0.00,      185,  0.00,      186,  0.00,
*      187,  0.00,      188,  0.00,      189,  0.00,      190,  0.00,
*      191,  0.00,      192,  0.00,      193,  0.00,      194,  0.00,
*      195,  0.00,      196,  0.00,      197,  0.00,      198,  0.00,
*      199,  0.00,      200,  0.00,      201,  0.00,      202,  0.00,
*      203,  0.00,      204,  0.00,      205,  0.00,      206,  0.00,
*      207,  0.00,      208,  0.00,      209,  0.00,      210,  0.00,
*      211,  0.00,      212,  0.00,      213,  0.00,      214,  0.00,
*      215,  0.00,      216,  0.00,      217,  0.00,      218,  0.00,
*      219,  0.00,      220,  0.00,      221,  0.00,      222,  0.00,
*      223,  0.00,      224,  0.00,      225,  0.00,      226,  0.00,
*      227,  0.00,      228,  0.00,      229,  0.00,      230,  0.00,
*      231,  0.00,      232,  0.00,      233,  0.00,      234,  0.00,
*      235,  0.00,      236,  0.00,      237,  0.00,      238,  0.00,
*      239,  0.00,      240,  0.00,      241,  0.00,      242,  0.00,
*      243,  0.00,      244,  0.00,      245,  0.00,      246,  0.00,
*      247,  0.00,      248,  0.00,      249,  0.00,      250,  0.00,
*      251,  0.00,      252,  0.00,      253,  0.00,      254,  0.00,
*      255,  0.00,      256,  0.00,      257,  0.00,      258,  0.00,
*      259,  0.00,      260,  0.00,      261,  0.00,      262,  0.00,
*      263,  0.00,      264,  0.00,      265,  0.00,      266,  0.00,
*      267,  0.00,      268,  0.00,      269,  0.00,      270,  0.00,
*      271,  0.00,      272,  0.00,      273,  0.00,      274,  0.00,
*      275,  0.00,      276,  0.00,      277,  0.00,      278,  0.00,
*      279,  0.00,      280,  0.00,      281,  0.00,      282,  0.00,
*      283,  0.00,      284,  0.00,      285,  0.00,      286,  0.00,
*      287,  0.00,      288,  0.00,      289,  0.00,      290,  0.00,
*      291,  0.00,      292,  0.00,      293,  0.00,      294,  0.00,
*      295,  0.00,      296,  0.00,      297,  0.00,      298,  0.00,
*      299,  0.00,      300,  0.00,      301,  0.00,      302,  0.00,
*      303,  0.00,      304,  0.00,      305,  0.00,      306,  0.00,
*      307,  0.00,      308,  0.00,      309,  0.00,      310,  0.00,
*      311,  0.00,      312,  0.00,      313,  0.00,      314,  0.00,
*      315,  0.00,      316,  0.00,      317,  0.00,      318,  0.00,
*      319,  0.00,      320,  0.00,      321,  0.00,      322,  0.00,
*      323,  0.00,      324,  0.00,      325,  0.00,      326,  0.00,
*      327,  0.00,      328,  0.00,      329,  0.00,      330,  0.00,
*      331,  0.00,      332,  0.00,      333,  0.00,      334,  0.00,
*      335,  0.00,      336,  0.00,      337,  0.00,      338,  0.00,
*      339,  0.00,      340,  0.00,      341,  0.00,      342,  0.00,
*      343,  0.00,      344,  0.00,      345,  0.00,      346,  0.00,
*      347,  0.00,      348,  0.00,      349,  0.00,      350,  0.00,
*      351,  0.00,      352,  0.00,      353,  0.00,      354,  0.00,
*      355,  0.00,      356,  0.00,      357,  0.00,      358,  0.00,
*      359,  0.00,      360,  0.00,      361,  0.00,      362,  0.00,
*      363,  0.00,      364,  0.00,      365,  0.00,      366,  0.00,
*      367,  0.00,      368,  0.00,      369,  0.00,      370,  0.00,
*      371,  0.00,      372,  0.00,      373,  0.00,      374,  0.00,
*      375,  0.00,      376,  0.00,      377,  0.00,      378,  0.00,
*      379,  0.00,      380,  0.00,      381,  0.00,      382,  0.00,
*      383,  0.00,      384,  0.00,      385,  0.00,      386,  0.00,
*      387,  0.00,      388,  0.00,      389,  0.00,      390,  0.00,
*      391,  0.00,      392,  0.00,      393,  0.00,      394,  0.00,
*      395,  0.00,      396,  0.00,      397,  0.00,      398,  0.00,
*      399,  0.00,      400,  0.00,      401,  0.00,      402,  0.00,
*      403,  0.00,      404,  0.00,      405,  0.00,      406,  0.00,
*      407,  0.00,      408,  0.00,      409,  0.00,      410,  0.00,
*      411,  0.00,      412,  0.00,      413,  0.00,      414,  0.00,
*      415,  0.00,      416,  0.00,      417,  0.00,      418,  0.00,
*      419,  0.00,      420,  0.00,      421,  0.00,      422,  0.00,
*      423,  0.00,      424,  0.00,      425,  0.00,      426,  0.00,
*      427,  0.00,      428,  0.00,      429,  0.00,      430,  0.00,
*      431,  0.00,      432,  0.00,      433,  0.00,      434,  0.00,
*      435,  0.00,      436,  0.00,      437,  0.00,      438,  0.00,
*      439,  0.00,      440,  0.00,      441,  0.00,      442,  0.00,
*      443,  0.00,      444,  0.00,      445,  0.00,      446,  0.00,
*      447,  0.00,      448,  0.00,      449,  0.00,      450,  0.00,
*      451,  0.00,      452,  0.00,      453,  0.00,      454,  0.00,
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*      467,  0.00,      468,  0.00,      469,  0.00,      470,  0.00,
*      471,  0.00,      472,  0.00,      473,  0.00,      474,  0.00,
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*      483,  0.00,      484,  0.00,      485,  0.00,      486,  0.00,
*      487,  0.00,      488,  0.00,      489,  0.00,      490,  0.00,
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*      495,  0.00,      496,  0.00,      497,  0.00,      498,  0.00,
*      499,  0.00,      500,  0.00,      501,  0.00,      502,  0.00,
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*      535,  0.00,      536,  0.00,      537,  0.00,      538,  0.00,
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*      543,  0.00,      544,  0.00,      545,  0.00,      546,  0.00,
*      547,  0.00,      548,  0.00,      549,  0.00,      550,  0.00,
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*      555,  0.00,      556,  0.00,      557,  0.00,      558,  0.00,
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*      579,  0.00,      580,  0.00,      581,  0.00,      582,  0.00,
*      583,  0.00,      584,  0.00,      585,  0.00,      586,  0.00,
*      587,  0.00,      588,  0.00,      589,  0.00,      590,  0.00,
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*      595,  0.00,      596,  0.00,      597,  0.00,      598,  0.00,
*      599,  0.00,      600,  0.00,      601,  0.00,      602,  0.00,
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*      615,  0.00,      616,  0.00,      617,  0.00,      618,  0.00,
*      619,  0.00,      620,  0.00,      621,  0.00,      622,  0.00,
*      623,  0.00,      624,  0.00,      625,  0.00,      626,  0.00,
*      627,  0.00,      628,  0.00,      629,  0.00,      630,  0.00,
*      631,  0.00,      632,  0.00,      633,  0.00,      634,  0.00,
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*      643,  0.00,      644,  0.00,      645,  0.00,      646,  0.00,
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*      655,  0.00,      656,  0.00,      657,  0.00,      658,  0.00,
*      659,  0.00,      660,  0.00,      661,  0.00,      662,  0.00,
*      663,  0.00,      664,  0.00,      665,  0.00,      666,  0.00,
*      667,  0.00,      668,  0.00,      669,  0.00,      670,  0.00,
*      671,  0.00,      672,  0.00,      673,  0.00,      674,  0.00,
*      675,  0.00,      676,  0.00,      677,  0.00,      678,  0.00,
*      679,  0.00,      680,  0.00,      681,  0.00,      682,  0.00,
*      683,  0.00,      684,  0.00,      685,  0.00,      686,  0.00,
*      687,  0.00,      688,  0.00,      689,  0.00,      690,  0.00,
*      691,  0.00,      692,  0.00,      693,  0.00,      694,  0.00,
*      695,  0.00,      696,  0.00,      697,  0.00,      698,  0.00,
*      699,  0.00,      700,  0.00,      701,  0.00,      702,  0.00,
*      703,  0.00,      704,  0.00,      705,  0.00,      706,  0.00,
*      707,  0.00,      708,  0.00,      709,  0.00,      710,  0.00,
*      711,  0.00,      712,  0.00,      713,  0.00,      714,  0.00,
*      715,  0.00,      716,  0.00,      717,  0.00,      718,  0.00,
*      719,  0.00,      720,  0.00,      721,  0.00,      722,  0.00,
*      723,  0.00,      724,  0.00,      725,  0.00,      726,  0.00,
*      727,  0.00,      728,  0.00,      729,  0.00,      730,  0.00,
*      731,  0.00,      732,  0.00,      733,  0.00,      734,  0.00,
*      735,  0.00,      736,  0.00,      737,  0.00,      738,  0.00,
*      739,  0.00,      740,  0.00,      741,  0.00,      742,  0.00,
*      743,  0.00,      744,  0.00,      745,  0.00,      746,  0.00,
*      747,  0.00,      748,  0.00,      749,  0.00,      750,  0.00,
*      751,  0.00,      752,  0.00,      753,  0.00,      754,  0.00,
*      755,  0.00,      756,  0.00,      757,  0.00,      758,  0.00,
*      759,  0.00,      760,  0.00,      761,  0.00,      762,  0.00,
*      763,  0.00,      764,  0.00,      765,  0.00,      766,  0.00,
*      767,  0.00,      768,  0.00,      769,  0.00,      770,  0.00,
*      771,  0.00,      772,  0.00,      773,  0.00,      774,  0.00,
*      775,  0.00,      776,  0.00,      777,  0.00,      778,  0.00,
*      779,  0.00,      780,  0.00,      781,  0.00,      782,  0.00,
*      783,  0.00,      784,  0.00,      785,  0.00,      786,  0.00,
*      787,  0.00,      788,  0.00,      789,  0.00,      790,  0.00,
*      791,  0.00,      792,  0.00,      793,  0.00,      794,  0.00,
*      795,  0.00,      796,  0.00,      797,  0.00,      798,  0.00,
*      799,  0.00,      800,  0.00,      801,  0.00,      802,  0.00,
*      803,  0.00,      804,  0.00,      805,  0.00,      806,  0.00,
*      807,  0.00,      808,  0.00,      809,  0.00,      810,  0.00,
*      811,  0.00,      812,  0.00,      813,  0.00,      814,  0.00,
*      815,  0.00,      816,  0.00,      817,  0.00,      818,  0.00,
*      819,  0.00,      820,  0.00,      821,  0.00,      822,  0.00,
*      823,  0.00,      824,  0.00,      825,  0.00,      826,  0.00,
*      827,  0.00,      828,  0.00,      829,  0.00,      830,  0.00,
*      831,  0.00,      832,  0.00,      833,  0.00,      834,  0.00,
*      835,  0.00,      836,  0.00,      837,  0.00,      838, 
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DATA DRG3/ -15., .0120, -14., .0102, -13., .0085, -12., .0071,
 * -10., .0048, -9., .0036, -8., .0030, -7., .0023,
 * -6., .0016, -5., .0011, -4., .0007, -3., .0003,
 * -2., .0001, -1., .0000, 0., .0000, 1., .0000,
 * 2., .0017, 3., .0003, 4., .0007, 5., .0011,
 * 6., .0017, 7., .0003, 8., .0007, 9., .0011,
 * 10., .0048, 11., .0055, 12., .0030, 13., .0038,
 * 14., .0100, 15., .0120, 12*9999, 13., .0085,
 * 14., .0100, 15., .0120, 12*9999, 13., .0085,

D. DCDSTR VS. RUDDER (INCREMENT IN DRAG COEFFICIENT
 DUE TO RUDDER DEFLECTION)

DATA DRG4/ -15., .0059, -14., .0054, -13., .0048, -12., .0043,
 * -10., .0032, -9., .0027, -8., .0022, -7., .0017,
 * -6., .0013, -5., .0005, -4., .0006, -3., .0003,
 * -2., .0002, -1., .0001, 0., .0000, 1., .0001,
 * 2., .0001, 3., .0006, 4., .0009, 5., .0013,
 * 6., .0017, 7., .0022, 8., .0027, 9., .0032,
 * 10., .0037, 11., .0043, 12., .0048, 13., .0054,
 * 14., .0059, 15., .0064, 12*9999, 13., .0054,

3. PITCHING MOMENT COEFFICIENT DATA

A. CMBAS VS. ACA (BASIC PITCHING MOMENT COEFFICIENT
 AS A FUNCTION OF ANGLE OF ATTACK)

DATA PTC1/ -10., 1.13, -8., 0.80, -6., 0.50, -4., 0.31,
 * -2., 0.16, 0., 0.08, 2., -0.03, 4., -0.13,
 * 6., -0.22, 8., -0.32, 10., -0.40, 12., -0.62,
 * 14., -0.95, 16., -1.13, 18., -1.31, 20., -1.51,
 * 22., -1.71, 24., -1.91, 26., -2.11, 28., -2.31,
 * 30., -2.51, 32., -2.71, 34., -2.91, 36., -3.11,
 * 38., -3.31, 40., -3.51, 42., -3.71, 44., -3.91,
 * 46., -4.11, 48., -4.31, 50., -4.51, 52., -4.71,
 * 54., -4.91, 56., -5.11, 58., -5.31, 60., -5.51,
 * 62., -5.71, 64., -5.91, 66., -6.11, 68., -6.31,
 * 70., -6.51, 72., -6.71, 74., -6.91, 76., -7.11,
 * 78., -7.31, 80., -7.51, 82., -7.71, 84., -7.91,
 * 86., -8.11, 88., -8.31, 90., -8.51, 92., -8.71,
 * 94., -8.91, 96., -9.11, 98., -9.31, 100., -9.51,
 * 102., -9.71, 104., -9.91, 106., -10.11, 108., -10.31,
 * 110., -10.51, 112., -10.71, 114., -10.91, 116., -11.11,
 * 118., -11.31, 120., -11.51, 122., -11.71, 124., -11.91,
 * 126., -12.11, 128., -12.31, 130., -12.51, 132., -12.71,
 * 134., -12.91, 136., -13.11, 138., -13.31, 140., -13.51,
 * 142., -13.71, 144., -13.91, 146., -14.11, 148., -14.31,
 * 150., -14.51, 152., -14.71, 154., -14.91, 156., -15.11,
 * 158., -15.31, 160., -15.51, 162., -15.71, 164., -15.91,
 * 166., -16.11, 168., -16.31, 170., -16.51, 172., -16.71,
 * 174., -16.91, 176., -17.11, 178., -17.31, 180., -17.51,
 * 182., -17.71, 184., -17.91, 186., -18.11, 188., -18.31,
 * 190., -18.51, 192., -18.71, 194., -18.91, 196., -19.11,
 * 198., -19.31, 200., -19.51, 202., -19.71, 204., -19.91,
 * 206., -20.11, 208., -20.31, 210., -20.51, 212., -20.71,
 * 214., -20.91, 216., -21.11, 218., -21.31, 220., -21.51,
 * 222., -21.71, 224., -21.91, 226., -22.11, 228., -22.31,
 * 230., -22.51, 232., -22.71, 234., -22.91, 236., -23.11,
 * 238., -23.31, 240., -23.51, 242., -23.71, 244., -23.91,
 * 246., -24.11, 248., -24.31, 250., -24.51, 252., -24.71,
 * 254., -24.91, 256., -25.11, 258., -25.31, 260., -25.51,
 * 262., -25.71, 264., -25.91, 266., -26.11, 268., -26.31,
 * 270., -26.51, 272., -26.71, 274., -26.91, 276., -27.11,
 * 278., -27.31, 280., -27.51, 282., -27.71, 284., -27.91,
 * 286., -28.11, 288., -28.31, 290., -28.51, 292., -28.71,
 * 294., -28.91, 296., -29.11, 298., -29.31, 300., -29.51,
 * 302., -29.71, 304., -29.91, 306., -30.11, 308., -30.31,
 * 310., -30.51, 312., -30.71, 314., -30.91, 316., -31.11,
 * 318., -31.31, 320., -31.51, 322., -31.71, 324., -31.91,
 * 326., -32.11, 328., -32.31, 330., -32.51, 332., -32.71,
 * 334., -32.91, 336., -33.11, 338., -33.31, 340., -33.51,
 * 342., -33.71, 344., -33.91, 346., -34.11, 348., -34.31,
 * 350., -34.51, 352., -34.71, 354., -34.91, 356., -35.11,
 * 358., -35.31, 360., -35.51, 362., -35.71, 364., -35.91,
 * 366., -36.11, 368., -36.31, 370., -36.51, 372., -36.71,
 * 374., -36.91, 376., -37.11, 378., -37.31, 380., -37.51,
 * 382., -37.71, 384., -37.91, 386., -38.11, 388., -38.31,
 * 390., -38.51, 392., -38.71, 394., -38.91, 396., -39.11,
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 * 566., -56.11, 568., -56.31, 570., -56.51, 572., -56.71,
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 * 638., -63.31, 640., -63.51, 642., -63.71, 644., -63.91,
 * 646., -64.11, 648., -64.31, 650., -64.51, 652., -64.71,
 * 654., -64.91, 656., -65.11, 658., -65.31, 660., -65.51,
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 * 702., -69.71, 704., -69.91, 706., -70.11, 708., -70.31,
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 * 718., -71.31, 720., -71.51, 722., -71.71, 724., -71.91,
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 * 734., -72.91, 736., -73.11, 738., -73.31, 740., -73.51,
 * 742., -73.71, 744., -73.91, 746., -74.11, 748., -74.31,
 * 750., -74.51, 752., -74.71, 754., -74.91, 756., -75.11,
 * 758., -75.31, 760., -75.51, 762., -75.71, 764., -75.91,
 * 766., -76.11, 768., -76.31, 770., -76.51, 772., -76.71,
 * 774., -76.91, 776., -77.11, 778., -77.31, 780., -77.51,
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 * 998., -99.31, 1000., -99.51, 1002., -99.71, 1004., -99.91,
 * 1006., -100.11, 1008., -100.31, 1010., -100.51, 1012., -100.71,
 * 1014., -100.91, 1016., -101.11, 1018., -101.31, 1020., -101.51,
 * 1022., -101.71, 1024., -101.91, 1026., -102.11, 1028., -102.31,
 * 1030., -102.51, 1032., -102.71, 1034., -102.91, 1036., -103.11,
 * 1038., -103.31, 1040., -103.51, 1042., -103.71, 1044., -103.91,
 * 1046., -104.11, 1048., -104.31, 1050., -104.51, 1052., -104.71,
 * 1054., -104.91, 1056., -105.11, 1058., -105.31, 1060., -105.51,
 * 1062., -105.71, 1064., -105.91, 1066., -106.11, 1068., -106.31,
 * 1070., -106.51, 1072., -106.71, 1074., -106.91, 1076., -107.11,
 * 1078., -107.31, 1080., -107.51, 1082., -107.71, 1084., -107.91,
 * 1086., -108.11, 1088., -108.31, 1090., -108.51, 1092., -108.71,
 * 1094., -108.91, 1096., -109.11, 1098., -109.31, 1100., -109.51,
 * 1102., -109.71, 1104., -109.91, 1106., -110.11, 1108., -110.31,
 * 1110., -110.51, 1112., -110.71, 1114., -110.91, 1116., -111.11,
 * 1118., -111.31, 1120., -111.51, 1122., -111.71, 1124., -111.91,
 * 1126., -112.11, 1128., -112.31, 1130., -112.51, 1132., -112.71,
 * 1134., -112.91, 1136., -113.11, 1138., -113.31, 1140., -113.51,
 * 1142., -113.71, 1144., -113.91, 1146., -114.11, 1148., -114.31,
 * 1150., -114.51, 1152., -114.71, 1154., -114.91, 1156., -115.11,
 * 1158., -115.31, 1160., -115.51, 1162., -115.71, 1164., -115.91,
 * 1166., -116.11, 1168., -116.31, 1170., -116.51, 1172., -116.71,
 * 1174., -116.91, 1176., -117.11, 1178., -117.31, 1180., -117.51,
 * 1182., -117.71, 1184., -117.91, 1186., -118.11, 1188., -118.31,
 * 1190., -118.51, 1192., -118.71, 1194., -118.91, 1196., -119.11,
 * 1198., -119.31, 1200., -119.51, 1202., -119.71, 1204., -119.91,
 * 1206., -120.11, 1208., -120.31, 1210., -120.51, 1212., -120.71,
 * 1214., -120.91, 1216., -121.11, 1218., -121.31, 1220., -121.51,
 * 1222., -121.71, 1224., -121.91, 1226., -122.11, 1228., -122.31,
 * 1230., -122.51, 1232., -122.71, 1234., -122.91, 1236., -123.11,
 * 1238., -123.31, 1240., -123.51, 1242., -123.71, 1244., -123.91,
 * 1246., -124.11, 1248., -124.31, 1250., -124.51, 1252., -124.71,
 * 1254., -124.91, 1256., -125.11, 1258., -125.31, 1260., -125.51,
 * 1262., -125.71, 1264., -125.91, 1266., -126.11, 1268., -126.31,
 * 1270., -126.51, 1272., -126.71, 1274., -126.91, 1276., -127.11,
 * 1278., -127.31, 1280., -127.51, 1282., -127.71, 1284., -127.91,
 * 1286., -128.11, 1288., -128.31, 1290., -128.51, 1292., -128.71,
 * 1294., -128.91, 1296., -129.11, 1298., -129.31, 1300., -129.51,
 * 1302., -129.71, 1304., -129.91, 1306., -130.11, 1308., -130.31,
 * 1310., -130.51, 1312., -130.71, 1314., -130.91, 1316., -131.11,
 * 1318., -131.31, 1320., -131.51, 1322., -131.71, 1324., -131.91,
 * 1326., -132.11, 1328., -132.31, 1330., -132.51, 1332., -132.71,
 * 1334., -132.91, 1336., -133.11, 1338., -133.31, 1340., -133.51,
 * 1342., -133.71, 1344., -133.91, 1346., -134.11, 1348., -134.31,
 * 1350., -134.51, 1352., -134.71, 1354., -134.91, 1356., -135.11,
 * 1358., -135.31, 1360., -135.51, 1362., -135.71, 1364., -135.91,
 * 1366., -136.11, 1368., -136.31, 1370., -136.51, 1372., -136.71,
 * 1374., -136.91, 1376., -137.11, 1378., -137.31, 1380., -137.51,
 * 1382., -137.71, 1384., -137.91, 1386., -138.11, 1388., -138.31,
 * 1390., -138.51, 1392., -138.71, 1394., -138.91, 1396., -139.11,
 * 1398., -139.31, 1400., -139.51, 1402., -139.71, 1404., -139.91,
 * 1406., -140.11, 1408., -140.31, 1410., -140.51, 1412., -140.71,
 * 1414., -140.91, 1416., -141.11, 1418., -141.31, 1420., -141.51,
 * 1422., -141.71, 1424., -141.91, 1426., -142.11, 1428., -142.31,
 * 1430., -142.51, 1432., -142.71, 1434., -142.91, 1436., -143.11,
 * 1438., -143.31, 1440., -143.51, 1442., -143.71, 1444., -143.91,
 * 1446., -144.11, 1448., -144.31, 1450., -144.51, 1452., -144.71,
 * 1454., -144.91, 1456., -145.11, 1458., -145.31, 1460., -145.51,
 * 1462., -145.71, 1464., -145.91, 1466., -146.11, 1468., -146.31,
 * 1470., -146.51, 1472., -146.71, 1474., -146.91, 1476., -147.11,
 * 1478., -147.31, 1480., -147.51, 1482., -147.71, 1484., -147.91,
 * 1486., -148.11, 1488., -148.31, 1490., -148.51, 1492., -148.71,
 * 1494., -148.91, 1496., -149.11, 1498., -149.31, 1500., -149.51,
 * 1502., -149.71, 1504., -149.91, 1506., -150.11, 1508., -150.31,
 * 1510., -150.51, 1512., -150.71, 1514., -150.91, 1516., -151.11,
 * 1518., -151.31, 1520., -151.51, 1522., -151.71, 1524., -151.91,
 * 1526., -152.11, 1528., -152.31, 1530., -152.51, 1532., -152.71,
 * 1534., -152.91, 1536., -153.11, 1538., -153.31, 1540., -153.51,
 * 1542., -153.71, 1544., -153.91, 1546., -154.11, 1548., -154.31,
 * 1550., -154.51, 1552., -154.71, 1554., -154.91, 1556., -155.11,
 * 1558., -155.31, 1560., -155.51, 1562., -155.71, 1564., -155.91,
 * 1566., -156.11, 1568., -156.31, 1570., -156.51, 1572., -156.71,
 * 1574., -156.91, 1576., -157.11, 1578., -157.31, 1580., -157.51,
 * 1582., -157.71, 1584., -157.91, 1586., -158.11, 1588., -158.31,
 * 1590., -158.51, 1592., -158.71, 1594., -158.91, 1596., -159.11,
 * 1598., -159.31, 1600., -159.51, 1602., -159.71, 1604., -159.91,
 * 1606., -160.11, 1608., -160.31, 1610., -160.51, 1612., -160.71,
 * 1614., -160.91, 1616., -161.11, 1618., -161.31, 1620., -161.51,
 * 1622., -161.71, 1624., -161.91, 1626., -162.11, 1628., -162.31,

C

DATA	SIC1/	0.0,	-8.0,	-6.0,	4.0,	8.0	9999.7
*	-8.0,	0.148,	0.149,	0.140,	0.137,	9999.7	
*	-6.0,	0.111,	0.110,	0.100,	0.077,	9999.7	
*	-4.0,	0.073,	0.072,	0.063,	0.060,	9999.7	
*	-2.0,	0.034,	0.034,	0.025,	0.022,	9999.7	
*	0.0,	-0.002,	-0.003,	-0.013,	-0.020,	9999.7	
*	2.0,	-0.040,	-0.042,	-0.050,	-0.060,	9999.7	
*	4.0,	-0.077,	-0.078,	-0.085,	-0.096,	9999.7	
*	6.0,	-0.114,	-0.116,	-0.127,	-0.129,	9999.7	
*	8.0,	-0.151,	-0.153,	-0.162,	-0.162,	5599.7	

B. CRBAS VS. SIDESLIP AND AGA (BASIC ROLL COEFFICIENT AS A FUNCTION OF SIDESLIP AND PARAMETER ANGLE OF ATTACK)

CCCCC

DATA	SIC2/	0.0,	-8.0,	2.0,	6.0,	10.0	9999.7
*	-8.0,	0.048,	0.046,	0.040,	0.044,	9999.7	
*	-6.0,	0.038,	0.036,	0.028,	0.030,	9999.7	
*	-4.0,	0.026,	0.022,	0.015,	0.020,	9999.7	
*	-2.0,	0.014,	0.010,	0.004,	0.008,	9999.7	
*	0.0,	-0.004,	-0.004,	-0.006,	-0.002,	9999.7	
*	2.0,	-0.005,	-0.014,	-0.020,	-0.014,	9999.7	
*	4.0,	-0.016,	-0.026,	-0.032,	-0.025,	9999.7	
*	6.0,	-0.030,	-0.038,	-0.042,	-0.036,	9999.7	
*	8.0,	-0.044,	-0.052,	-0.057,	-0.048,	5599.7	

C. CNBAS VS. SIDESLIP AND AGA (BASIC YAW COEFFICIENT AS A FUNCTION OF SIDESLIP AND PARAMETER ANGLE OF ATTACK)

CCCCC

DATA	SIC3/	0.0,	-8.0,	0.0,	6.0,	8.0	9999.7
*	-8.0,	0.034,	0.037,	0.042,	0.042,	9999.7	
*	-6.0,	0.025,	0.028,	0.033,	0.033,	9999.7	
*	-4.0,	0.016,	0.019,	0.022,	0.023,	9999.7	
*	-2.0,	0.007,	0.009,	0.012,	0.014,	9999.7	
*	0.0,	-0.001,	-0.001,	-0.004,	-0.004,	9999.7	
*	2.0,	0.010,	0.009,	0.007,	0.007,	9999.7	
*	4.0,	0.019,	0.018,	0.016,	0.016,	9999.7	
*	6.0,	0.028,	0.026,	0.024,	0.024,	9999.7	
*	8.0,	0.036,	0.034,	0.032,	0.032,	5599.7	

* 5. DIRECTIONAL CONTROL COEFFICIENT DATA

CCCCC

A. CYSTR VS. RUDDER AND AGA (INCREMENT IN SIDE FORCE COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER ANGLE OF ATTACK)

C

```

DATA DREC1/ 0.0, -8.0, 2.0, 5.0, 8.0, 9999.
-15.0, -0.90, -.097, -.095, -.102, 9999.
-10.0, -.060, -.062, -.062, -.069, 9999.
-5.0, -.332, -.036, -.037, -.042, 9999.
0.0, -.004, -.003, -.003, -.003, 9999.
5.0, -.040, -.042, -.038, -.034, 9999.
10.0, -.070, -.066, -.062, -.060, 9999.
15.0, -.100, -.098, -.092, -.096, 9999.
* 12*99999.

```

C C C C C C

B. DCNSTR VS. RUDDER AND AGA (INCREMENT IN YAWING MOMENT
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

```

DATA DREC2/ 0.0, -8.0, 2.0, 6.0, 8.0, 9999.
-15.0, -.070, -.068, -.062, -.065, 9999.
-10.0, -.050, -.049, -.048, -.048, 9999.
-5.0, -.026, -.024, -.022, -.018, 9999.
0.0, -.000, -.000, -.000, -.000, 9999.
5.0, -.022, -.023, -.018, -.014, 9999.
10.0, -.052, -.048, -.047, -.046, 9999.
15.0, -.080, -.079, -.074, -.075, 9999.
* 12*99999.

```

C C C C C C

C. DCRSTR VS. RUDDER AND AGA (INCREMENT IN ROLLING MOMENT
COEFFICIENT DUE TO RUDDER DEFLECTION AND PARAMETER
ANGLE OF ATTACK)

```

DATA DREC3/ 0.0, -8.0, 2.0, 4.0, 6.0, 9999.
-15.0, -.050, -.038, -.032, -.032, 8.0
-10.0, -.034, -.029, -.026, -.022, -.0032
-5.0, -.018, -.018, -.018, -.014, -.0004
0.0, -.004, -.000, -.000, -.000, -.0008
5.0, -.024, -.012, -.004, -.005, -.0013
10.0, -.048, -.028, -.018, -.005, -.0016
15.0, -.070, -.053, -.040, -.012, -.0025
* 12*99999.

```

C C C C C C C C

* 6. LATERAL CONTROL COEFFICIENT DATA

A. CCYSTA VS. ALLRGN AND AGA (INCREMENT IN SIDE FORCE
COEFFICIENT DUE TO ASYMMETRIC STABILATOR DEFLECTION AND
PARAMETER ANGLE OF ATTACK)


```

* /0.0 /0.4 /0.15 /,
* C/P /0.1 /CNR /-0.2 /,
* C/P /0.2 /CNP /-0.01 /,
* /-0.4 /-0.1 /-0.01 /

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CCCCCCCC

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*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

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*** CONTROL SYSTEM PARAMETERS

```

DATA KPTCHR /0.28 /KROLLR /KVAWRT /KPAWK /
* KGAMMA /1.0 /KALT /0.10 /0.40 /10.8 /,
* /KRT LIM /75.0 /0.3 /CGARML /0.0 /CGARMIN /,
* /KNY /0.35 /KNZ /0.05 /0.0 /,

```

CCCCCCCC

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

*** MISSILE INITIAL CONDITIONS

```

DATA XMI /0.0 /YMI /50.0 /ALTUD1 /838.1 /
* PITCH1 /3.00 /BANK1 /0.0 /HEDNG1 /3.0 /,
* AUA1 /3.00 /PTCHR1 /0.0 /ROLLR1 /0.0 /YAWK1 /,

```

CCCCC

*** TARGET INITIAL CONDITIONS

```

DATA XTI /24000.0 /YTI /0.0 /HT1 /10.0 /
* /TSPEED /35.0 /

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CCCCC

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*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

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*****
*** PROPORTIONAL NAVIGATION & NAV FILTER CONSTANTS (AZIMUTH & ELEV.)
DATA      LAMDAZ      ,LAMDEL      ,KNFAZ      ,KNFEL
*          /3.15      ,/3.85      ,/0.8        ,/0.50 /

*** MISSION PHASE FLAGS & DECISION PARAMETERS
DATA      PH1      ,PH2      ,PH3      ,PH4
*          /0       ,/0       ,/0       ,/0
DATA      CFFSET    ,ALIAIT    ,SGCZPU    ,MISDST
*          /10.0    ,/200.0   ,/1.12   ,/0.0 /

*****
COMMON ELCCCK /H/: ECM/GLINT PARAMETERS
*****

DATA      FREQ      ,SHIFT      ,SHIFTH      ,BRNTHR
*          /0.00     ,/75.0    ,/10.0     ,/250.0 /

END

*****
SUBROUTINE MISSN
*****
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTRCL LOOPS. NYC IS ASSUMED TO ALWAYS BE ZERO EXCEPT DURING
ATTACK. NZC IS LIMITED TO *4.0 AND -2.0 G'S.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCJUNT,NFAZE

*****
COMMON ELCCCK /A/: MISCELLANEOUS CONSTANTS
*****

COMMON /A/ TIME ,FINTIM,DT ,CPUT ,NCUT ,NPTS ,CPA ,PCJUNT,
, I ,PHO ,PI ,PII ,PASS ,INT ,S ,

```

```

* * *
      IXX      ,IYY      ,IZZ      ,IXZ      ,IA      ,IB      ,JS      ,
      ID       ,IE      ,IF      ,IG      ,IH      ,II      ,IK      ,
      CHORD2,CHORD ,SPAN2,SPAN ,NFAZE

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*****
COMMON BLOCK /C/: CONTROL SYSTEM PARAMETERS
*****

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* * * * *
COMMON /C/ KPITCHR      ,KROLLR      ,KYART      ,KBANK      ,
      KGAMMA      ,KALT      ,CGARML      ,CGARM      ,
      RRTLLIM      ,PLIM      ,KNY      ,KNZ      ,
      AILRON      ,STBLTR      ,RUCCER      ,
      BSERO      ,NZSERO      ,NYSERO

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*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

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* * * * *
COMMON /D/ ALFA      ,BETA      ,VT      ,HMDUT      ,
      U      ,V      ,W      ,THETA      ,
      PHI      ,GAMMA      ,CL      ,SY      ,
      CD      ,CY      ,CN      ,CR      ,
      CM      ,CA      ,ALFAUT      ,PDUT      ,
      R      ,RDOT      ,NZ      ,ALTUDE      ,
      CUOT      ,YM      ,XMDCT      ,YMDCT

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*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****

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* * * * *
COMMON /F/ PH1      ,PH2      ,PH3      ,PH4      ,
      CFFSET      ,ALTATT      ,SGDZPU      ,MISDST      ,
      LAMDZ      ,LAMDDEL      ,KNFAPZ      ,KNFEL      ,
      NZC      ,PHIC      ,GAMMAC      ,PCLIM      ,
      PC      ,QC      ,RC      ,KANGE      ,
      SIGAZ      ,SIGEL      ,SIGUAF      ,SIGDEF      ,
      SYT      ,THEAT      ,XT      ,YI      ,
      FT      ,NYC      ,PUPRNG

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*****
COMMON BLOCK /G/: CLTPUT PARAMETERS
*****

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* * * * *
COMMON /G/ AJA      ,SIDESL      ,BANK      ,FLTPHC      ,
      EANKC      ,PITCH      ,KULLKT      ,KULLTC      ,
      PTCHRT      ,YAWRT      ,HEALNG      ,FLTPH

```

```
* * *
** *****
C C C      ,ELEV   ,DSIGAZ  ,DSIGEL  ,
C C C      ,DSGOAZ  ,ERFEK   ,ERGDEL  ,
C C C      ,ERFAZ   ,ERFEL   ,ERFR    ,
C C C      *****
C C C      MISSION PHASE LOGIC AND GUIDANCE COMMANDS
C C C
1 IF (PH4.EC.1) GO TO 40
  IF (PH3.EC.1) GO TO 30
  IF (PH2.EC.1) GO TO 20
  IF (PH1.EC.1) GO TO 10
*** INGRESS FROM INITIAL CONDITION TO OFFSET MANEUVER
    IF (RANGE.LT.18000.0) GO TO 9
        ALTITUDE HOLD
            ALTC = 50.0
            ALTUOF = ALTUC
            GAMMAC = KALT#(ALTC-ALTUDF)/VT
            GAMMAF = GAMMA
            AZC = COS(GAMMAF)*KGAMMA*VT*(GAMMAL-GAMMAF)/G
                PROPORTIONAL NAVIGATION IN AZIMUTH
                    AYC = LANCAL*VT*SIGDAF/G
                    FFIC = ATAN2(AYC,AZC)
                    NZC = AZC*CUS(PHI)+AYC*SIN(PHI)
                    GC TO 100
                    FFI = 1
5 *** OFFSET TURN (60 DEG BANK) TO OFFSET HEADING
  IC ABSCSZ = ABS(DSIGAZ)
    IF (AESDSZ.GT.OFFSET) GO TO 19
        ALTITUDE HOLD
            ALTC = 50.0
            ALTUDF = ALTUCE
            GAMMAC = KALT#(ALTC-ALTUDF)/VT
            GAMMAF = GAMMA
            AZC = COS(GAMMAF)*KGAMMA*VT*(GAMMAL-GAMMAF)/G
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```

C      C      BANK ANGLE HCLD (60 DEG)
C      C      AYC = 0.0
C      C      PFIC = 60.0/PII
C      C      NZC = AZC/COS(PHI)
C      C      GC TO 100
C      C      PF2 = 1
C      C      15
C      C      ***
C      C      COURSE HCLD UN OFFSET HEADING TO PUPUP
C      C      20
C      C      ABDSC2 = ABS(DSGCAZ)
C      C      IF(AEDSD2.GT.SGDZPU) GU TO 29
C      C      C
C      C      ALTITUDE HCLD
C      C      C
C      C      ALTC = 50.0
C      C      ALTUDF = ALTUCE
C      C      GAMMAC = KALT*(ALTC-ALTUDF)/VT
C      C      GAMMAF = GAMMA
C      C      AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C      C      C
C      C      BANK ANGLE HCLD (0 DEG)
C      C      C
C      C      AYC = 0.0
C      C      PFIC = 0.0
C      C      NZC = AZC/COS(PHI)
C      C      GC TO 100
C      C      PF3 = 1
C      C      25
C      C      ***
C      C      PULLUP TO ATTACK ALTITUDE
C      C      PROPORTIONAL NAVIGATION IN AZIMUTH
C      C      C
C      C      30
C      C      IF(ALTUDE.GT.ALTATT) GU TO 39
C      C      C
C      C      VERTICAL FLIGHT PATH ANGLE HCLD (8.5 DEG)
C      C      C
C      C      ALTC = 0.0
C      C      GAMMAC = 8.5/PII
C      C      GAMMAF = GAMMA
C      C      AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C      C      C
C      C      PROPORTIONAL NAVIGATION IN AZIMUTH
C      C      C
C      C      AYC = LAMDAZ*VT*SIGDAF/G
C      C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      C      PFIC = ATAN2(AYC,AZC)
C      C      GC TO 100
C      C      PF4 = 1
C      C      35

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```

C ***
C      ATTACK
C      PROFCRTICNAL NAVIGATION IN AZIMUTH AND ELEVATION
C
C      4 C
C      ALTIC = 0.0
C      GAMMAC = 0.0
C      GAMMAF = GAMMA
C      AYC = LAMCAZ*VI*SIGDAF/G
C      AZC = LAMDEL*VI*SIGDEF/G+COS(GAMMAF)
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C      NYC = 0.0
C
C      BANK ANGLE CCMAND ROUTINE INSURES ROLL
C      IN SHORTEST DIRECTION
C
C      PFIC = ATAN2(AYC,AZC)
C      CELPHI = PHIC-PHI
C      LPHIAB = ABS(CELPHI)
C      IF(OPHIAB.LT.PI) GO TO 100
C      IF(PFIC.GE.0.0) GC TC 90
C      PFIC = PHIC+2.0*PI
C      GC TO 100
C      PFIC = PHIC-2.0*PI
C
C      9C CONTINUE
C      10C *****
C      ** NZ COMMAND LIMITED TO -2 & +4 G'S
C      NZC = LIMIT(-2.0,4.0,NZC)
C
C      RETURN
C      END
C
C      *****
C      SUBROUTINE APILOT
C      *****
C      LIMIT, FEALPL
C      *****
C      MODELS THE INNER LOOP AUTOPILOT AND CONTROL MIXER. CALCULATES
C      REQUIRED ELEVATOR,AILERON & RUDDER REQURES THESE TO GET
C      THE FIN STABILATOR COMMANDS, APPLIES THE FIN LIMITS UP +-15 DEG.
C      AND ADJUSTS THE THREE CONTROL OUTPUTS TO ACCOUNT FOR THE LIMITS.
C      *****
C      IMPLICIT REAL(A-Z)
C      INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CFA,ROLL,PLUNTI,NFAZE

```

9-07-84


```

* HT ,NYC ,PU PRNG
EXECUTABLE SIMTS *****
INNER LCCF AUTOPILOT

NORMAL ACCELERATION COMMAND SYSTEM

NZCLIM = LIMIT(-2.0,4.0,NZC)
NZZ = NZ+CGARM*(DOT/G
ENZ = NZCLIM-NZZ
ENZKNZ = ENZ*KNZ
QC = QC + ENZKNZ*DT
NZSERI = QC-KPTCHR*G
NZSEFC = REALPL(NZSERO,0.025,NZSERI,DT)

ELE = -PII*NZSERO

BANK ANGLE COMMAND SYSTEM

EPHI = PHIC-PHI
PC = KBANK*EPI
PCLIM = LIMIT(-PLIM,PLIM,PC)
EP = PCLIM-P
BSERI = EP*KROLLR
BSERC = REALPL(BSERO,0.025,BSERI,DT)

AIL = -PII*BSERO

TURN COORDINATOR

IF(PT4,EC.1) GO TO 30
NYC = 0.0
CONTINUE
NYV = NY+CGARM*L*RDOT/G
ENY = NYC-NYV
RC = ENY*KNY*DT
NYSEFI = RC-KYAWRT*R
NYSEFC = REALPL(NYSERO,0.025,NYSERI,DT)

RUD = -PII*NYSERC
CONTROLS MIXER AND LIMITS

LSTABI = ELE-AIL
RSTABI = ELE+AIL
LSTAB = LIMIT(-15.0,15.0,LSTABI)

```



```

* *      AILRON      STBLTR      RUDDER      ,
      BSERO      NZSERO      NYSERO      ,

*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

COMMON /C/ ALFA      BETA      VT      HMDOT
      U      V      W      ,
      PHI      GAMMA      THETA      ,
      CO      CY      CL      ,
      CM      CN      P      ,
      R      ALFADT      BETADT      ,
      QUOT      RDCT      NZ      ,
      XM      YM      XMDCT      YMDCT

*****
SIDESL = PII*BETA
AOA = FII*ALFA

CLEAS = TABLE1(LFT1,ACA)
DCLSTE = TABLE1(LFT2,STBLTR)
CDBAS = TABLE1(DRG1,CLBAS)
DCDSTE = TABLE1(DRG2,STBLTR)
DCCSTA = TABLE1(DRG3,AILRON)
DCLSTR = TABLE1(DRG4,RUDDER)
CMBAS = TABLE1(PTCH1,ACA)
DCMSTE = TABLE1(PTCH2,STBLTR)
CYBAS = TABLE2(SID1,ACA,SIDESL)
CRBAS = TABLE2(SID2,ACA,SIDESL)
CNBAS = TABLE2(SID3,ACA,SIDESL)
DCVSTR = TABLE2(DREC1,ACA,RUDDER)
DCNSTR = TABLE2(DREC2,ACA,RUDDER)
DCVSTA = TABLE2(LTRL1,ACA,AILRCN)
DCNSTA = TABLE2(LTRL2,ACA,AILRCN)
DCRSTA = TABLE2(LTRL3,ACA,AILRCN)

AERCDYNAMIC COEFFICIENTS

CL = CLEAS+DCLSTE+CHORD2*(CLAUT*ALFADT+CLQ*CY)/VT
CD = CLEAS+DCLSTE+DCCSTA+DCDSTR+CHORD2*(CDACT*ALFADT+CDQ*Q)/VT
CY = CLEAS+DCVSTR+DCYSTA+SPAN2*(CYR*R+CYP*P+CYBUT*BETADT)/VT
CM = CMEAS+DCMSTE+CHORD2*(CMADI*ALFADT+CMQ*Q)/VT
CN = CNEAS+DCNSTR+DCNSTA+SPAN2*(CNBDT*BETADT+CNRR*R+CNPP*P)/VT
CK = CREAS+DCRSTA+DCRSTR+SPAN2*(CKRLT*BETADT+CKRR*R+CKPP*P)/VT

```

```

C C C C
AERODYNAMIC FORCES AND MOMENTS
L = CL*CS
D = CD*CS
LA = SPAN*CR*QS
MA = CFCR*CM*QS
NA = SPAN*CN*QS
X = L*SIN(ALFA)-D*COS(ALFA)
Y = CY*QS
Z = -L*COS(ALFA)-D*SIN(ALFA)

C C C
NORMAL & LATERAL ACCELERATIONS
NZ = -Z/(MASS*G)
NY = Y/(MASS*G)

C C C C
*** COMMENCE INTEGRATION OF EQUATIONS OF MOTION
EULER ANGLES
PHIDOT = P*TAN(THETA)*(Q*SIN(PHI)+R*COS(PHI))
THETAD = Q*COS(PHI)-R*SIN(PHI)
SYDOT = (Q*SIN(PHI)+R*COS(PHI))/COS(THETA)
PHI = PHI + PHIDOT*DT
THETA = THETA + THETAD*DT
SY = SY + SYDOT*DT

C C C
LINEAR ACCELERATIONS AND VELOCITIES
UDOT = -G*SIN(THETA)+V*R-W*Q+X/MASS+T/MASS
VDOT = G*SIN(PHI)+C*(THETA)-U*R+W*P+Y/MASS
WDOT = G*COS(PHI)+C*(THETA)+U*Q-V*P+Z/MASS
U = U + UDOT*DT
V = V + VDOT*DT
W = W + WDOT*DT
VT = SQR(U**2+V**2+W**2)
VTCOT = SQR(UDOT**2+VDOT**2+WDOT**2)

C C C
ANGULAR ACCELERATIONS AND VELOCITIES
PDCT = IY*LA+IG*NA-ID*P*Q-IE*R*Q
QDOT = IF*MA-IG*P*R-IH*(P**2-R**2)
RDCT = IC*LA+II*NA-IJ*P*Q-IK*K*Q
P = P + PDCT*DT
Q = Q + QDOT*DT

```

```

CC C
K = R + RDOT*DT
ANGLES OF ATTACK, SIDESLIP, AND FLIGHT PATH
ALFADT = (ATAN(W/U)-ALFA)/DT
BETADT = (ASIN(V/VT))-BETA)/DT
ALFA = ATAN(W/U)
BETA = ASIN(V/VT)
GAMMA = ASIN(HMDOT/VT)
MISSILE POSITION IN INERTIAL SPACE
XMDOT = U*CCS(SY)*CCS(THETA)+V*(CCS(SY)*SIN(THETA)*SIN(PHI)
      -SIN(SY)*CCS(PHI))+W*(CCS(SY)*SIN(THETA)*CCS(PHI)+
      *YMDOY = U*SIN(SY)*CCS(THETA)+V*(SIN(SY)*SIN(THETA)*SIN(PHI)
      +CCS(SY)*CCS(PHI))+W*(SIN(SY)*SIN(THETA)*CCS(PHI)-
      *CGS(SY)*SIN(PHI))
HMDOT = U*SIN(THETA)-V*CCS(THETA)*SIN(PHI)-W*CCS(THETA)*CCS(PHI)
HURDOT = SCRT(XMDOT**2+YMDOT**2)
XM = XM + XMDOT*DT
YM = YM + YMDOT*DT
ALTUDE = ALTUDE + HMDOT*DT
RETURN
END
9-07-84
FUNCTION TABLE1 (ARRAY,IP)
TABLE LOOKUP WITH LINEAR INTERPOLATION FOR A FUNCTION
OF ONE VARIABLE, Y=F(X). MAXIMUM NUMBER OF POINTS IS
LIMITED TO 20 BY THE DIMENSION STATEMENT. NOTE: THE ALL
FIRST ARRAY ENTRY (ARRAY(1,1)) CANNOT BE 9959.0 AND ALL
UNUSED ARRAY ELEMENTS MUST BE EXACTLY 9999. THE INDEPENDENT
VARIABLE DATA IS STORED IN ROW 1, THE DEPENDENT IN ROW 2.
WARNINGS ARE SUPPRESSED AFTER 20 CONSECUTIVE CALLS (ABOUT 5 DT'S)
*****
REAL ARRAY(2,30),IP,C,TABLE1
INTEGER I,J,K,N,SUPRES
DATA J,K,N/3*0/
K = K+1
IF (.NOT.(IP.LT.ARRAY(1,1)) GO TO 10
TABLE1=ARRAY(2,1)

```

```

C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,101) IF, TABLE1
C      RETURN
C      ENC IF
C
10 DO 90 I=1,30
    IF(.NOT.ARRAY(1,1).EQ.9995.0) GO TO 20
    TABLE1=ARRAY(2,1-1)
    IF(SUPRES(J,K,N).EQ.1) WRITE(6,102) IP, TABLE1
    RETURN
20  IF(.NOT.IP.GT.ARRAY(1,1)) GO TO 30
    GO TO 90
30  IF(.NOT.IP.EQ.ARRAY(1,1)) GO TO 40
    TABLE1 = ARRAY(2,1)
    RETURN
40  IF(.NOT.IP.LT.ARRAY(1,1)) GO TO 90
    C= (IP-ARRAY(1,1-1))/(ARRAY(1,1)-ARRAY(1,1-1))
    TABLE1= ARRAY(2,1-1) +C*(ARRAY(2,1)-ARRAY(2,1-1))
    RETURN
C      ENC IF
C      CONTINUE
C      WRITE(6,103)
C      RETURN
C
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE1*****
101  FORMAT('0','SUBROUTINE TABLE1: INPUT BELOW INDEPENDENT VARIABLE DA
*TA.//:
*      USED LOWEST DATA AVAILABLE = ',F10.2,
102  FORMAT('0','SUBROUTINE TABLE1: INPUT ABOVE INDEPENDENT VARIABLE DA
*TA.//:
*      USED HIGHEST DATA AVAILABLE = ',F10.2,
103  FORMAT('0','SUBROUTINE TABLE1: ERROR. SUBROUTINE DID NOT END )
END
C
C
C      9-07-84*****
C      FUNCTION TABLE2(A,IP,IV)*****
C      TABLE2*****
C      TABLE LOOKUP WITH LINEAR INTERPOLATION FOR A FUNCTION
C      OF TWO VARIABLES, Z=F(X,Y). MAXIMUM NUMBER OF INPUT PARAMETERS IS
C      LIMITED TO 5, INDEPENDENT VARIABLE DATA POINTS TO 9 BY THE
C      DIMENSION OF THE ARRAY. A(1,1) IS NOT USED. THE PARAMETER VALUES
C      ARE STORED IN COL 1, INDEP. VAR. VALUES IN ROW 1. THE COEFFICIENT
C      DATA ARE STORED IN THE GRID CREATED BY ROW AND COL 1.
C      TABLE2 WARNINGS ARE SUPPRESSED AFTER 5 CONSECUTIVE OCCURRENCES.***

```

```

C      REAL A(6,10),IP,IV,CP,CV,LFI,RGT, TABLE 2
C      INTEGER I,LI,UI,J,K,N,SUPRES
C      DATA J,K,N /3#0/

C      K = K+1
C      IF(.NOT.IP.LT.A(2,1)) GO TO 10
C      CP = 0.
C      LI = 2
C      UI = 2
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1001) IP,A(2,1)
C      GO TO 55

C      10      DC 50 I=2,6
C      IF(.NOT.A(I,1).EQ.9999.0) GO TO 20
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1002) IP,A(I-1,1)
C      CP = 0.
C      LI = I-1
C      UI = I-1
C      GO TO 55

C      20      IF(IP-A(I,1)) 30,40,50
C      IP < A(I,1)
C      30      CP = (IP-A(I-1,1))/(A(I,1)-A(I-1,1))
C      LI = I-1
C      UI = I
C      GO TO 55

C      40      IF = A(I,1)
C      CP = 0
C      LI = I
C      UI = I
C      GO TO 55

C      50      END IF
C      CONTINUE
C      END IF

C      55      IF(.NOT.IV.LT.A(1,2)) GO TO 60
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1003) IV,A(1,2)
C      TABLE2=A(LI,2)+CP*(A(UI,2)-A(LI,2))
C      RETURN

C      60      DC 100 I=2,10
C      IF(.NOT.A(1,I).EQ.9999.0) GO TO 70
C      IF(SUPRES(J,K,N).EQ.1) WRITE(6,1004) IV,A(1,I-1)
C      TABLE2=A(LI,I-1)+CP*(A(UI,I-1)-A(LI,I-1))
C      RETURN

```

```

7C      IF (IV-A(L,I)) 80,90,100
C      IV < A(L,I)
80      CV = (IV-A(L,I-1))/(A(L,I)-A(L,I-1))
      LFT = A(L,I-1)+CP*(A(L,I)-A(L,I-1))
      RGT = A(L,I)+CP*(A(L,I)-A(L,I-1))
      TABLE2 = LFT+CV*(RGT-LFT)
      RETURN
C      IV = A(L,I)
90      TABLE2 = A(L,I)+CP*(A(L,I)-A(L,I-1))
      RETURN
C      END IF
100      CONTINUE
C      END IF
C      WRITE(6,1005)
C      RETURN
C
C      FORMAT STATEMENTS FOR SUBROUTINE TABLE2*****
1001  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER, BELOW DATA.',
*      'INPUT PARAMETER',
*      'USEC LOWEST PARAMETER',
1002  FORMAT('0','SUBROUTINE TABLE2: INPUT PARAMETER, ABOVE DATA.',
*      'INPUT PARAMETER',
*      'USEC HIGHEST PARAMETER',
1003  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. BELOW DATA.',
*      'INPUT INDEP. VAR.',
*      'USEC LOWEST INDEP. VAR.',
1004  FORMAT('0','SUBROUTINE TABLE2: INPUT INDEP. VAR. ABOVE DATA.',
*      'INPUT INDEP. VAR.',
*      'USEC HIGHEST INDEP. VAR.',
1005  FORMAT('0','SUBROUTINE TABLE2: ERRCK. SUBROUTINE DID NOT END.')
C      END
C
C      *****
C      FUNCTION SUPRES(J,K,N) *****
C      *****
C      DETERMINES TO SUPPRESS WARNINGS FROM TABLE1 OR TABLE2 AFTER THEY
C      HAVE BEEN CALLED ABOUT 20 TIMES IN A ROW. (ABOUT 5 UT INTERVALS.)
C      *****
C      INTEGER J,K,N, SUPRES
C
C      IF (K-J.EQ.1) GO TO 10
C      N = 0
C      K = 0
C      J = 0
C      GO TO 10

```

9-05-84

```

10 CONTINUE = N+1
15 CONTINUE = K
C
IF (N-EC-20) WRITE(6,105)
105 FORMAT('0',TABLE LCOKUP WARNINGS SUPPRESSED')
C
IF (N-GE-20) SUPRES = 1
IF (N-LT-20) SUPRES = 0
RETURN
END
C
SUBROUTINE TGINAV
C
C   RNG, SCV
C
C   NAVIGATES THE TARGET AND COMPUTES RELATIVE RANGE, RANGE RATES,
C   INCRPCRTES ECM AND GLINT MODELS TO GIVE APPARENT TARGET
C   POSITIONS. ALSO CALCULATES LINE OF SIGHT ANGLES AND RATES.
C
C   IMPLICIT REAL(A-Z)
C   INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,C,FA,NOLIT,PCOUNT,NFAZE
C
C   COMMON BLOCK /A/: MISCELLANEOUS CONSTANTS
C
C   COMMON /A/ TIME , FINTIM,DT , CPDT , NCLT , NPTS , CPA , PCOUNT,
C   G , IXX , IYY , IZZ , PI , PII , IA , IB , IC , IS ,
C   ID , IE , IF , IH , II , IJ , IK ,
C   CHORD, CHORD2, CHORD , SPAN2 , SPAN , NFAZE
C
C   COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
C
C   COMMON /D/ ALFA , BETA , VT , HMDUT
C   U , V , W , SY
C   CU , GAMMA , CL , CK
C   CM , CN , CP , CW

```

```

** *
** *
** *

```

```

R      QUOT      ALFADT      BETADT      PDUT      ,
XM      XM      ,RUOT      ,NZ      ,ALTUDE      ,
      ,YM      ,XMDCT      ,VMDCT      ,

```

```

*****
COMMON BLOCK /E/: INITIAL CONDITIONS
*****

```

```

** *
** *
** *

```

```

COMMON /E/  XM1  PITCH1  AL TUD1
      AQAI  ,BANK1  ,HE LNS1
      XTI   ,PCHRI  ,KULLRI
      ,YTI   ,HT I

```

```

,UI DES1
,YAWRI
,TSPEED

```

```

*****
COMMON ELCCCK /F/: GUIDANCE PARAMETERS
*****

```

```

** *
** *
** *

```

```

COMMON /F/  PH1  CFF SET  PH2  ALTATT  PH3  SG DZPU
      LAMDZ  ,LMDAZ  ,LMDL  ,KNFAZ
      NZC    ,PC    ,PHIC  ,GAMMAC
      PC     ,WC     ,KC    ,RANGE
      SIGAZ  ,SIGEL  ,SI GDAF
      SYT    ,THETAT
      FI     ,NYC    ,PJ PRNG

```

```

,PH4
,MISDST
,KNFEL
,PC LIM
,RANGE
,SI GDEF
,YT

```

```

*****
COMMON ELCCCK /H/: ECM/GLINT PARAMETERS
*****

```

```

** *
** *
** *

```

```

COMMON /H/  FREQ  XECM  SHIFT  SHIFTH
      XECM    ,YGLNT  ,YECM  ,HECM
      HTECM   ,HGLNT  ,XTECM

```

```

,BKNTHK
,XGLNT
,YTECM

```

```

C EXECUTABLE STATEMENTS:
C *****

```

```

C ** TARGET ACTION
C *****

```

```

XI = XTI
YT = YTI+TSPEED*TIME
HT = HTI

```

```

RELATIVE RANGE TO TARGET

```

```

C      XR = XT-XM
C      YR = YT-YM
C      HR = HT-ALTDE
C
C      ** RANGE & MISS DISTANCE
C
C      RMIGE = SQRT(XR**2+YR**2+HR**2)
C      IF (RNGE.GT.2000.)GC TO 25
C      IF (RNGE.LT.RANGE)GO TC 25
C      CPA = 1
C      MISDST = RANGE
C
C      25 CONTINUE
C      RANGE = RNGE
C
C      ** GLINT MODEL (SUPPRESSED AT A RANGE OF 100 FT)
C      ***** TESTPATCH TO SUPPRESS GLINT (KTEST = 1)
C      KTEST = 1
C      IF (KTEST.EQ.1) GO TC 50
C      ***** ENDTEST
C      CALL RNG(RAND)
C
C      IF (PCCLNT.NE.1) GO TO 100
C      IF (RANGE.LT.100.0) GO TO 50
C      XGLNT = 20*RAND
C      YGLNT = 50*RAND
C      HGLNT = 20*RAND
C      GC TO 100
C
C      50      CCNTINUE
C              XGLNT = 0.0
C              YGLNT = 0.0
C              HGLNT = 0.0
C
C      100 CONTINUE
C
C      ** ECM BLINKING MODEL (SUPPRESSED AT BURN-THROUGH RANGE)
C
C      * SELECT THE PHASE APPLIED TO THE ECM SIGNAL
C
C      GO TO(1C1,1C2,103,104),NFAZE
C      101      PFAZE = 0.0
C              GC TC 105
C      102      PFAZE = PI*0.5
C              GC TC 105
C      103      PFAZE = PI
C              GC TC 105
C      104      PFAZE = PI*1.5

```

```

C 105 CONTINUE
C POPRNG = PHASE*PII
C IF (RANGE.LT.BRNTHR) GO TO 350
C XECMH = SIN(2*PI*FREQ*TIME+PHASE)
C XECM = SQWV(XECMH,SHIFTX)
C
C YECMH = SIN(2*PI*FREQ*TIME+PHASE)
C YECM = SQWV(YECMH,SHIFLY)
C
C HECMH = SIN(2*PI*FREQ*TIME+PHASE)
C HECM = SQWV(HECMH,SHIFTH)
C GO TO 400
C 35C CONTINUE
C XECM = 0.0
C YECM = 0.0
C HECM = 0.0
C 400 CUNTINUE
C
C XTECM = XI+XECM+XGLNT
C YTECM = YI+YECM+YGLNT
C HTECM = HI+HECM+HGLNT
C
C *** RELATIVE RANGE AND RANGE RATE TO RADAR TARGET
C
C XTECM = XTECM-XM
C YTECM = YTECM-YM
C HTECM = HTECM-ALTUDE
C RNTECM = SQRT(XTECM**2+YTECM**2)
C RGECHT = SQRT(XTECM**2+YTECM**2+HTECM**2)
C
C XDCTR = -XMDOT
C YDCTR = TSPEED-YMCDT
C HDCTR = -HMDOT
C HURDTR = SQRT(XDCTR**2+YDCTR**2)
C
C *** SEEKER LCS AND LCS RATE CALCULATIONS
C
C SYT = ATAN2(YTECM,XTECM)
C TRAKAZ = ATAN2(YMDCT,XMDUT)
C SIGAZ = SYT-TRAKAZ
C
C VTANAZ = -XDCTR*SIN(SYT)+YDCTR*COS(SYT)
C SIGDAZ = VTANAZ/RNTECM
C SIGDAF = REALPL(SIGDAF,KNFAZ,SIGDAZ,DT)

```



```

SUBROUTINE PREPAR
*****
DESIGNATES UP TO 20 PARAMETERS TO BE STORED FOR OUTPUT AND
ASSIGNS THEM TO THE NEXT ROW OF THE PITS ARRAY. EACH PARAM. IS
STORED IN A COLUMN OF THE ARRAY FROM ROW 3 UNTIL THE END OF THE
ARRAY IS REACHED OR CPA OCCURS. ROWS 1 & 2 CONTAIN MINIMUM AND
MAXIMUM VALUES OF EACH VARIABLE RESPECTIVELY. COL. 1 CONTAINS
THE VALUES OF TIME FOR EACH POINT. NPTS IS COMMON TO BLOCK A
AND INDICATES THE NUMBER OF POINTS STORED.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NUCT,PCOUNT,NFAZE
DIMENSION KEEP(20)
*****
COMMON /A/ TIME , FINTIM,DT , CPDT , NUCT , NPTS , CPA , PCOUNT,
, IXX , IYY , IZZ , IXZ , IA , IB , IC , IS ,
, ID , IE , IF , IG , IH , II , IJ , IK ,
, CHORD2,CHURC , SPAN2,SPAN ,NFAZE
*****
C' "MON /C/ KPTCHR ,KYAWRT ,CGARML ,KBANK ,
,KGAMMA ,KALT ,CGARML ,CGARML ,
,RRTLIM ,PLIM ,KNY ,KNZ ,
,AILRON ,STBLTR ,RUDDER ,
,BSERO ,NZSERU ,NYSERU
*****
COMMON /C/ ALFA ,BETA ,VT ,HMDOT ,
, U , V , W , THETA ,
, CU , CY , CL , P ,
, CM , CN , ALFADT , BEIADT ,
, R , RDOT , NZ , ALTUDE ,
, XM , YM , XMDCT , YMDOT
*****
COMMON /E/ XM1 ,ALTLU1 ,
, PITCH1 ,HEDNCL ,
, AQAI ,ROLLR1 ,
, XT1 ,VT1 ,HT1
*****
COMMON /F/ PH1 ,PH2 ,PH3 ,PH4 ,
, OFFSET ,ALTATT ,SGDZPU ,
, LAMDAZ ,LAMDCL ,KNFAZ ,
, NZC ,PHIC ,GAMMAC ,
, PC ,QC ,RC ,RANGE
*****

```

```

* * * SIGAZ SIGDEF
* * * SYT ,YI
* * * FT ,POPRNG

COMMON /G/ AOA ,FLTPHC
BANKC ,ROLKTC
PTCHRT ,FLTPTH
HEADT ,DSIGEL
DSGDAZ ,ERFRK
ERFAZ

COMMON /H/ FREQ ,BRNTHK
XECM ,XULNT
VGLNT ,YTECM
HTECM

COMMON /I/ PTS(300,20),PLTN(6,7),XN(6,7),YN(6,7),TITLE(6),
LEG(4,20)

EXECUTABLE STMTS *****
RACIAN TC DEGREE CONVERSIONS FOR ULPUT

AOA = ALFA*PII
SIDESL = BETA*PII
BANK = PHI*PII
FLTPHC = GAMMA*PII
BANKC = PHIC*PII
PTCH = THETA*PII
ROLLRT = P*PII
ROLKTC = PCLIM*PII
PTCHRT = C*PII
YAWRT = R*PII
HEADNG = SY*PII
FLTPTH = GAMMA*PII
ELEV = SYT*PII
DSIGAZ = THETA*PII
DSIGEL = SIGAZ*PII
DSGDAZ = SIGEL*PII
DSGLEL = SIGDAF*PII

*** CREATE THE MISSION PHASE MARKER (MARK)
MARK = C.0
IF (PH1.EC.1)MARK = 1.0
IF (PH2.EC.1)MARK = 2.0

```

```

C      IF (PH3.EQ.1)MARK = 3.0
C      IF (PH4.EQ.1)MARK = 4.0
C      NPTS = NPTS+1
C      K = NPTS+2
C      *** COMPUTE THE ERROR FUNCTIONS
C
C      IF (MARK.EQ.4) GO TO 50
C      ERBK = 0.0
C      ERRRR = 0.0
C      ERRRAZ = 0.0
C      ERREL = 0.0
C      GC TC 100
C      50 CONTINUE
C      ERBK = ERRBK + ABS(BANKC-BANK) *DI
C      ERRRR = ERRRR + ABS(ROLLRTC-ROLLKT) *DI
C      ERRRAZ = ERRRAZ + ABS(DSQUAZ) *DI
C      ERREL = ERREL + ABS(DSGUEL) *DI
C      100 CONTINUE
C
C      ERFBK = ERRBK/TIME
C      ERFRK = ERRRR/TIME
C      EKFEZ = ERRRAZ/TIME
C      *** SELECT THE VARIABLES TO BE STORED
C      KEEP(1) = TIME
C
C      GRAPH 1 = NZC
C      KEEP(2) = NZC
C      KEEP(3) = NZ
C
C      GRAPH 2 = BANKC
C      KEEP(4) = BANKC
C      KEEP(5) = BANK
C
C      GRAPH 3 = ROLLRTC
C      KEEP(6) = ROLLRTC
C      KEEP(7) = ROLLRT
C
C      GRAPH 4 = YECM
C      KEEP(8) = YECM
C      KEEP(9) = YCLNT
C
C      GRAPH 5 = AILRCN
C      KEEP(10) = AILRCN

```

```

C      KEEP(11) = STBLTR
C      KEEP(12) = RUDDER
C
C      GRAPH 6
C      KEEP(13) = ALTUDE
C
C      GRAPH 7
C      KEEP(14) = XM
C      KEEP(15) = YM
C      KEEP(16) = XT
C      KEEP(17) = YT
C
C      SPARES
C      KEEP(18) = RANGE
C      KEEP(19) = MARK
C      KEEP(20) = NYC
C
C      *** STORE MINIMUM AND MAXIMUM VALUES OF EACH VARIABLE
C
C      DO 20 I=1,20
C      IF (NPTS.GT.1) GO TO 10
C      P1S(1,I) = KEEP(1)
C      P1S(2,I) = KEEP(1)
C
C      10      CCNTINUE
C      P1S(1,I) = AMIN1(P1S(1,I),KEEP(1))
C      P1S(2,I) = AMAX1(P1S(2,I),KEEP(1))
C      20 CONTINUE
C
C      *** STORE VALUES OF EACH VARIABLE WITH THE TIME
C
C      DO 30 I=1,20
C      P1S(K,I) = KEEP(1)
C      30 CONTINUE
C
C      *** CHECK FOR ARRAY OVERFLOW AND TERMINATE AT 255 POINTS
C      IF (NPTS.GE.295) CPA = 3.0
C
C      RETURN
C      END
C
C      *****
C      SUBROUTINE CUIPUT(NPTS,CPA)
C      *****
C      HEACER, PLOT1, PLOT2, PLOT3, PLOT21, PLOT13
C      *****
C      *****

```

9-07-84


```

C      FLAG = 1.0
C      18 CONTINUE
C
C      ***** WRITE PRIMARY DATA OUTPUT *****
C      ***** TO FILE 6 (TERMINAL) AND THEN FILE 9 (TCMC DATA) *****
C
C      DO 100 K=1,2
C      IF(K.EQ.1)KFILE=0
C      IF(K.EQ.2)KFILE=5
C
C      ***** TITLES *****
C      *****
C      20 WRITE(KFILE,20)((TITLE(I,J),I=1,8),J=1,4)
C      FCFRMT('1',4(20X,8A47))//)
C
C      ***** INDICATE HOW THE SIMULATION TERMINATED *****
C      ***** GC TC(30,40,50),CPA *****
C      30 WRITE(KFILE,35)
C      35 FCFRMT(1X,'SIMULATION TERMINATED DUE TO CPA')
C      GC TO 60
C
C      40 WRITE(KFILE,45)
C      45 FCFRMT(1X,'SIMULATION TERMINATED DUE TO FINTIME')
C      GC TO 60
C
C      50 WRITE(KFILE,55)
C      55 FCFRMT(1X,'SIMULATION TERMINATED DUE TO FULL ARRAY')
C
C      60 CCNTINUE
C      ***** VALUE OF THE ITERATED PARAMETER *****
C      *****
C      65 WRITE(KFILE,65) FREQ
C      FCFRMT(1X,'*** BLINKER FREQUENCY= ',F8.2)
C
C      67 WRITE(KFILE,67) PCPKNG
C      FCFRMT(1X,'*** BLINKER PHASE = ',F6.0//)
C
C      ***** LIST THE PRIMARY DATA OUTPUTS *****
C      *****
C      75 WRITE(KFILE,75) MISDST,ERFBK,ERFKR,ERFAZ,ERFEL
C      FCFRMT(1X,'MISS ***** / ***** ERROR ***** BANK *****')
C
C      ***** DISTANCE *****

```

```

* * ROLLRATE * AZIMUTH * ELEVATION *//
5(3X,F10.5,2X,*,*////////)

C **
C LIST THE VARIABLE RANGES
C
80 *
C WRITE(KFILE,80)
FCFMAT(18X,*,* RANGES FOR ALL SAVED VARIABLES *****
//30X,*,* MINIMUM
WRITE(KFILE,90)((LEG(I,J),I=1,4),PTS(1,J),PTS(2,J),J=1,20)
FCFMAT(11X,4A4,4X,F12.6,3X,F12.6)

C 100 CONTINUE
C
C ***** TABULAR DATA OUTPUT *****
C
DU 200 I=1,4
J=(I-1)*4+2
K=J+3
WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
WRITE(5,65) FREQ
WRITE(9,125) I
FCFMAT(50X,*,* DATA SET NUMBER *,I1,*,* (F 4,////)
WRITE(9,135)((LEG(L,1),L=1,4),((LEG(L,M),L=1,4),M=J,K)
FCFMAT(2X,20A4,////)

C
C NN=APTS+2
DC 150 N=3,NN
START NEW PAGE EVERY 65 LINES
L = MOD(N,65)
IF(L.NE.0) GC TO 140
WRITE(9,20)((TITLE(L,M),L=1,8),M=1,4)
WRITE(9,65) FREQ
WRITE(9,125) I
WRITE(9,135)((LEG(L,1),L=1,4),((LEG(L,M),L=1,4),M=J,K)

C
C COUNTINUE
WRITE(9,145) PTS(N,1),PTS(N,L),L=J,K)
FCFMAT(1X,5(*,*,F12.6,3X))

C
C COUNTINUE
C 200 CONTINUE
C
C ***** PRCLUCE GRAPHIC OUTPUT USING DISSPLA SUEROUTINES *****
C

```

[illegible]

```

DO 50 J=1,3
  DC 30 I=1,8
    HC(I) = TITLE(I,J)
  30 CONTINUE
  CALL HEADIN(HC ,32 , 1-1 ,4)
  50 CONTINUE
  DO 60 I=1,6
    HC(I) = PLTN(I,KP)
    XNM(I) = XN(I,KP)
    YNM(I) = YN(I,KP)
  60 CONTINUE
  CALL HEADIN(HD ,24 , 1-0 ,4)
  CALL XNAME( XNM ,24)
  CALL YNAME( YNM ,24)
  RETURN
END
*** FILE: FLCT1 ***
*** CONTAINS ALL S/R'S THAT INTERFACE WITH CISSPLA EXCEPT HEADER ***
*** 9-10-84 ***
*** SUBROUTINE PLOT1(MESS1,MESS2,VARI,VAR2) ***
*** INITIALIZES DISSPLA FGR A NEW PAGE AND GRAPT ***
*** IMPLICIT REAL(A-H,C-Z),INTEGER(I-N) ***
*** DIMENSION MESS1(2),MESS2(2) ***
  CALL NCCHEK
  CALL GRACE(0.)
  CALL BLCAUP(3.,647)
  CALL PACE(11.,8.5)
  CALL HWFLCT('AUTO')
  CALL HNSCAL('SCREEN')
  CALL NCERDR
  CALL PHYSQR(1.,.75)
  CALL AREA2C(9.,6.5)
  CALL SWISSM
  *** PUT THE MESSAGES INTO THE GRAPHS ***
  CALL MESSAGE(MESS1,8,0.2,0.0)

```

```

CALL SUBROUTINE PLOT2(P1S,LEG,DV,IV,NPTS)
RETURN
END
SUBROUTINE PLOT2(P1S,LEG,DV,IV,NPTS)
LOADS THE LEGEND ARRAY WITH CURVE LABELS: P1S THE POINTS FOR
EACH CURVE, DEP ENDS THE VARIABLE: INDEXES. IV,DV ARE IN-
DEPENDENT, DEP ENDS WHERE THEIR VALUES ARE F. LEG IS THE COLUMN IN
THE P1S ARRAY CONTAINING THE LABELS FOR EACH VARIABLE. DV IS A
ARRAY CONTAINING THE INDEXES FOR UP TO 4 DEP VAR'S.
ELEMENT ARRAY CONTAINING THE INDEXES FOR UP TO 4 DEP VAR'S.

```

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```
*****  
LOADS THE LEGEND ARRAY WITH CURVE LABELS; GETS THE POINTS FOR  
EACH CURVE FROM THE PIS ARRAY; PLOTS EACH CURVE. I,V,UV ARE IN-  
DEPENDENT, DEPENDENT VARIABLE; INDEXES. THEY GIVE THE COLUMN IN  
THE PIS ARRAY WHERE THEIR VALUES ARE FOUND. LEG IS THE PACKED  
ARRAY CONTAINING LEGEND LABELS FOR EACH VARIABLE. DV IS A  
ELEMENT ARRAY CONTAINING THE INDICES FCUR UP TO 4 DEP VAR'S.  
*****
```

DATA MCNEY /' \$ ' /

III

GC IC 5
1C CONTINUE

```
*** NEXT PACK THE LEGEND ARRAY AND RANGE THE Y-AXIS
```

```

15      CONTINUE
      YMIN = AMIN1(YMIN,PTS(1,K))
      YMAX = AMAX1(YMAX,PTS(2,K))

```

[illegible]

AD-A152 193

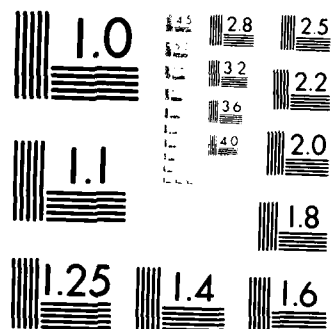
AN INVESTIGATION INTO THE CONTROL LIMITATIONS OF A BANK 3/3
TO TURN MISSILE IN THE TERMINAL HOMING PHASE(U) NAVAL
POSTGRADUATE SCHOOL MONTEREY CA B P ANDERSON SEP 84

UNCLASSIFIED

F/G 17/7

NL





MICROCOPY RESOLUTION TEST CHART
NATIONAL BUREAU OF STANDARDS-1963-A

```

C C C      END
C C C      SUBROUTINE PLOT3(NPTS,PTS,TITLE)
C C C      *CREATES A 3-D GEOGRAPHICAL PLOT OF MISSILE AND TARGET TRACKS. BY CHANGING THE VIEWPOINT YCU CAN GET DIFFERENT PORTIONS OF THE MISSION FROM VARIOUS PERSPECTIVES.*
C C C      IMPLICIT REAL(A-H,C-Z), INTEGER(I-N)
C C C      DIMENSION PTS(300,20),XP(300),YP(300),ZP(300),IPACK(100)
C C C      CALL BLCWUP(1.0)
C C C      *** CREATE THE TITLES
C C C      DO 40 J=1,3
C C C          DC 30 I=1,8
C C C              HC(I) = TITLE(I,J)
C C C          CONTINUE
C C C          CALL HEADIN(HC ,32 , 1.1 ,4)
C C C          CONTINUE
C C C          CALL HEADIN('GEOGRAPHICAL TRACKS',15,1.0,4)
C C C          *** DEFINE THE WORKBOX
C C C          CALL VCLM3D(10,20,7.5)
C C C          ** LABEL THE AXES
C C C          CALL XNAME('FEET EAST',9)
C C C          CALL YNAME('FEET NCRTH',10)
C C C          CALL ZNAME('ALTITUDE (FT)',13)
C C C          ** DEFINE THE VIEWPCINT
C C C          CALL VLANGL(130,40,26)
C C C          ** SET UP THE AXIS SYSTEM
C C C          CALL CRCSX
C C C          CALL GRAF3D(-1000.,1000.,4000., 0.0,5000.,25000,

```


APPENDIX E

LISTING FOR SUBROUTINE MISSN1

```

*****9-07-84*****
SUBROUTINE MISSN1
*****
SEA SKIMMER GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE
WITH NC OFFSET TURN. AFTER POPUP, GUIDANCE IS STANDARD PRO-
PORTIONAL. POPUP USES ONLY ALTITUDE COMMAND VICE GAMMAC.
*****
MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES
OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT
CONTROL LOOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED
TO +4.C AND -2.0 G.S.
*****
IMPLICIT REAL(A-Z)
INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE
*****
COMMON ELCK /A/: MISCELLANEOUS CONSTANTS
*****
COMMON /A/ TIME , FINTIM,DT , CPDT , NCLT , APTS , CPA , PCOUNT,
IXX , IYY , RHU , PI , PII , MASS , WT , S ,
ID , IE , IZZ , IXZ , IA , IB , IC , US ,
CHORD2,CHORD , SPAN2,SPAN , NFAZE , IH , II , IJ , IK ,
*****
COMMON /C/: CONTROL SYSTEM PARAMETERS
*****
COMMON /C/ KPTCHR , KRCCLR , KYAKNT , KQANK ,
KGAMMA , KALT , CGARML , CGARML ,
RRTLIM , PLIM , KNY , KNYZ ,
AILRON , STBLTR , RUDDER ,
BSERO , NZSERO , NYSEK
*****
COMMON BLOCK /D/: MISSILE FLIGHT DYNAMICS PARAMETERS
*****

```

```

C C
*****
COMMON /G/ ALFA
* U
* PHI
* CD
* CM
* R
* CDOOT
* XM
*
* BETA
* V
* GAMMA
* CY
* CN
* ALFADT
* RDOOT
* YM
*
* VT
* M
* THETA
* CL
* P
* BEIADT
* NZ
* XMDCT
*
*****
COMMON BLOCK /F/: GUIDANCE PARAMETERS
*****
C C C C C
COMMON /F/ PH1 OFFSET
* LAMDAZ
* NZC
* PL
* SIGAZ
* SYT
* FT
*
* PH2
* ALTATT
* LAMDEL
* PHIC
* QC
* SIGEL
* THETAT
* NYC
*
* PH3
* SGDZPU
* KNFAZ
* GAMMAC
* RC
* SIGDAF
* XT
* POPRNG
*
*****
COMMON ELGCK /G/: OUTPUT PARAMETERS
*****
C C C C C
COMMON /G/ ADA
* BANK
* PTCHRT
* HEADT
* DSGDAZ
* ERFAZ
*
* SIDESL
* PITCH
* YAWRT
* ELEVT
* DSGDEL
* ERFEL
*
* BANK
* RULLRT
* HEACNG
* USICAZ
* ERFBK
*
* FLTPHC
* RULRTC
* FLTPTH
* USIGEL
* ERFRR
*
*****
C C EXECUTABLE STMTS:
C C *****
C C SET POPUP RANGE AND ALTITUDE
C C POPRNG = 15000.
C C
C C MISSION PHASE LOGIC AND GUIDANCE COMMANDS
C C 1 IF (PH4.EC.1) GO TO 40
C C IF (PH1.EC.1) GO TO 30
C C ***** INGRESS FROM INITIAL CONDITION TO POPUP MANEUVER

```

```

C
C
C
IF(RANGE.LT.POPRNG) GO TO 9
  ALTITUDE HOLD
  ALTC = 50.0
  ALTUDF = ALTUDE
  GAMMAC = KALT*(ALTC-ALTUDF)/VT
  GAMMAF = GAMMA
  AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMA(-GAMMAF))/G
  PROPORTIONAL NAVIGATION IN AZIMUTH
  AYC = LAMDAZ*VT*SIGDAF/G
  PFIC = ATAN2(AYC,AZC)
  NZC = AZC*COS(PHI)+AYC*SIN(PHI)
  GC TO 100
  PF4 = 1
  S
  ***
  C
  C
  C
  PULLF TO ATTACK ALTITUDE
  PROPORTIONAL NAVIGATION IN AZIMUTH
  3C
  IF(ALTUDE.GE.ALTAIT) GO TO 39
  COMMAND ATTACK ALTITUDE
  C
  C
  C
  ALTC = ALTAIT
  ALTUDF = ALTUDE
  GAMMAC = KALT*(ALTC-ALTUDF)/VT
  GAMMAF = GAMMA
  AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMA(-GAMMAF))/G
  PROPORTIONAL NAVIGATION IN AZIMUTH
  AYC = LAMCAZ*VT*SIGDAF/G
  NZC = AZC*COS(PHI)+AYC*SIN(PHI)
  PFIC = ATAN2(AYC,AZC)
  GC TO 100
  PF4 = 1
  3S
  ***
  C
  C
  C
  ATTACK - BANK-TC-TURN OR SKID-TC-TURN OR BOTH
  PROPORTIONAL NAVIGATION IN AZIMUTH AND ELEVATION
  ALTC = 0.0
  GAMMAC = 0.0
  GAMMAF = GAMMA
  AYC = LAMDAZ*VT*SIGDAF/G
  AZC = LAMDEL*VT*SIGDEF/G+CLS(GAMMAF)
  40

```


APPENDIX F

LISTING FOR SUBROUTINE MISSA2

9-07-84

***** SUBROUTINE MISSA2 *****

***** BALLISTIC GUIDANCE SCHEME. ALLOWS VARIABLE POPUP IN CLOSE *****
 WITH NC OFFSET TURN. AFTER POPUP, MISSILE RCLLS TO 50 DEGREES
 ANGLE OF BANK AND USES LATERAL AND VERTICAL PROPORTIONAL NAV. *****

***** MAKES MISSION PHASE DECISIONS AND INVOKES THE DIFFERENT MODES *****
 OF GUIDANCE AS REQUIRED. DELIVERS NZC AND PHIC TO THE AUTOPILOT *****
 CONTRL LGOPS. NYC IS ASSUMED TO ALWAYS BE ZERO. NZC IS LIMITED *****
 TO +4.C AND -2.0 G.S. *****

***** IMPLICIT REAL(A-Z) *****

***** INTEGER PH1,PH2,PH3,PH4,I,J,K,N,NPTS,CPA,NULT,PCOUNT,NFAZE *****

***** COMMON /A/ TIME , FINIM,DT , CPUT ,NULT ,NPTS ,CPA ,PCOUNT, *****
 IXX , IY , RHO , PI ,PII ,MASS ,MI ,S , *****
 ID , IY , IZZ , IIA ,IB ,IC ,CS , *****
 CHORD2,CHORD ,SPAN2,SPAN ,NFAZE ,IH ,IJ ,IK , *****

***** COMMON /C/ KPTCHR ,KRULLR ,KYAWRT ,KBANK , *****
 KGAMMA ,KALT ,CGARML ,CGARMN , *****
 RRTLLM ,PLIM ,KNY ,CGARMN , *****
 AILRUN ,STBLTR ,RUDDER ,KNZ , *****
 RSERO ,NZSERO ,NYSERU , *****

***** COMMON /C/ ALFA ,BETA ,VT ,HMDUT , *****
 L ,V ,THETA ,SY , *****
 PHI ,GAMMA ,CL ,CR , *****
 CD ,CY ,CL ,P , *****
 CM ,CN ,BETAUT ,POUT , *****
 R ,ALFADT ,NZ ,ALTUJE , *****
 QUOT ,RDGT ,XMDCT ,YMDCT , *****
 XM ,YM , *****

***** COMMON /F/ PH1 ,PH2 ,PH3 ,PH4 , *****
 OFFSET ,ALFATT ,SGDZPU ,MI SUST , *****

```
C      *      LAMDAZ    ,LAMDEL    ,KNFAZ    ,KNFEL  
C      *      NZC       ,PHIC     ,GAMPAC   ,PC LIM  
C      *      PC        ,QC        ,RC         ,RANGE  
C      *      SIGAZ     ,SIGEL    ,SIGDZF   ,SIGDEF  
C      *      SVT       ,THETAT   ,XT         ,VT  
C      *      HT        ,NYC      ,POPRNG   ,YI  
  
C      COMMON /G/ AOA          SIDESL    BANK      FLTPHC  
C      *      BANKC      PITCH     KOLLRT    ROLTRIC  
C      *      PCHRT      YAWRT     HEADING    FLTPIH  
C      *      HEADT      ELEVT      USIGAZ     DSIGEL  
C      *      CSGDAZ     DSGDEL    ERFK       ERFR  
C      *      ERFZ      ERFEL  
  
C      EXECUTABLE SIMTS:  
C      *****  
C      SET POCLF RANGE AND A PARABOLIC ALTITUDE TRACK  
C  
C      POPRG = 15000  
C      VH = SCHR(XMDOOT**2+YMDOOT**2)  
C      ALTT = HMDOT*RANGE/VH + (G/2.)*(RANGE/VT)**2 + 10.  
  
C      MISSION PHASE LOGIC AND GUIDANCE CMDS  
  
C      1 IF(Phi.EC.I) GO TO 40  
C      IF(PHI.EC.I) GO TO 39  
  
C      *** INGRESS FROM INITIAL CONDITION TO FCPU MANEUVER  
C  
C      IF(RANGE.LT.POPRG) GO TO 9  
  
C      ALTITUDE HOLD  
  
C      ALTIC = 50.C  
C      ALTUDF = ALTUDE  
C      GAMMAC = KALT*(ALTC-ALTUDF)/VT  
C      GAMMAF = GAMMA  
C      AZC = COS(GAMMAF)*KGAMMA*VT*((GAMMAC-GAMMAF)/J  
  
C      FCCPCTIONAL NAVIGATION IN AZIMUTH  
  
C      AYC = LAMDZ*VT*SIGDAF/G  
C      PFIC = ATAN2(AYC,AZC)  
C      NZC = AZC*COS(PHI)+AYC*SIN(PHI)  
C      GC TC 100  
C      PHI = 1
```

```

C ** PULLF TC ATTACK ALTITUDE
C ** PROFCRTIONAL NAVIGATION IN AZIMUTH
C ** ***** PATCH TC RETAIN BIT GUIDANCE TO IMPACT (KTEST=1)
C ** KTEST = 1
C ** IF (KTEST.EQ.1) GO TO 32
C ** ***** ENDPATCH
C 3C IF (ALTITUDE.GE.ALTAIT) GO TO 39
C 32 CONTINUE
C ** COMMAND BALLISTIC ATTACK ALTITUDE
C **
C ** ALTC = ALTAIT
C ** ALTUDF = ALTUDE
C ** GAMMAC = KALT*(ALTC-ALTUDF)/VT
C ** GAMMAF = GAMMA
C ** AZC = COS(GAMMAF)+KGAMMA*VT*(GAMMAC-GAMMAF)/G
C **
C ** PROPORTIONAL NAVIGATION IN AZIMUTH
C **
C ** AYC = LAMCAZ*VT*SIGDAF/G
C ** NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C ** PFIC = ATAN2(AYC,AZC)
C ** GC TO 100
C ** PF4 = 1
C 35
C **
C ** ATTACK
C ** PROFCRTIONAL NAVIGATION IN AZIMUTH AND ELEVATION
C **
C ** COMMAND ATTACK ALTITUDE & ROLL TC 90 DEG BANK.
C **
C 4C PFIC = PI/2.
C ** ALTC = ALTAIT
C ** ALTUDF = ALTUDE
C ** GAMMAC = KALT*(ALTC-ALTUDF)/VT
C ** GAMMAF = GAMMA
C ** AZC = KGAMMA*VT*(GAMMAC-GAMMAF)/G
C **
C ** PROFCRTIONAL NAVIGATION IN AZIMUTH
C **
C ** AYC = LAMDAZ*VT*SIGDAF/G
C ** NZC = AZC*COS(PHI)+AYC*SIN(PHI)
C ** NYC = AYC*COS(PHI)-AZC*SIN(PHI)
C ** NYC = 0.0
C 10C CONTINUE
C ** *****

```

C
 C NZ COMPAND LIMITED TO -2 & +4 G'S; NYC TO +/- 0.5 G.
 NZC= LIMIT(-2,0; 4,0,NZC)
 NYC= LIMIT(-0.5; 0.5,NYC)
 C
 RETURN
 END

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