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INTERACTION OF MOVING SHOCK WITH THIN STATIONARY

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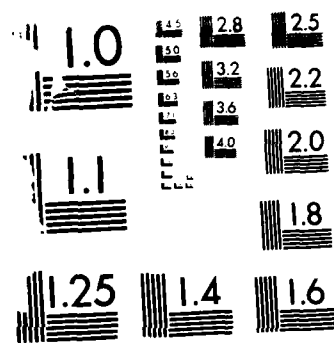
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Interaction of Moving Shock
with Thin Stationary Thermal Layer

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20 February 1986

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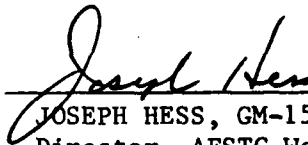
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location. Good agreement with Schneyer and Wilkins is obtained subject to appropriate choice of an arbitrary constant k introduced into the analytical model. Further validation of the model is needed. *found*

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I. INTRODUCTION

It is well known that radiation from a nuclear explosion can generate a thin layer of heated air adjacent to the ground.¹ The interaction of the nuclear blast wave with this thermal layer results in a precursor wave system, which affects dust cloud generation and the aerodynamic load on ground structures.¹ A general discussion of this interaction has been provided by Hess.² Experimental studies of the interaction of weak ($\bar{M}_s < 1.14$) moving shocks with thin thermal layers have been reported in Refs. 3 and 4.

Detailed numerical code calculations of the inviscid interaction between an incident shock and a thin thermal layer of semi-infinite streamwise extent have recently been reported.⁵ The present study is an attempt to deduce properties of the latter interaction by simple analytic methods and to compare with the numerical results of Ref. 5.

II. THEORY

Consider a normal shock wave moving over a thin thermal layer of semi-infinite extent and assume ideal gases. The initial flow field, in laboratory stationary coordinates, is illustrated in Fig. 1. For generality, the ratio of specific heats γ is allowed to differ in the thermal layer and in the external flow. After the initial transient, the interaction can be characterized as either unseparated or separated. These flows are steady and unsteady, respectively, in incident shock stationary coordinates. Both cases are considered herein. Flow velocity and Mach number are denoted by $\bar{u}$ and $\bar{M}$, respectively, in the laboratory coordinate system (Fig. 1), and by u and M in the incident shock stationary coordinate system (Fig. 2). Note that $\bar{M}_s \equiv \bar{u}_s/a_1 = u_1/a_1 = M_1$.

A. UNSEPARATED FLOW REGIME

We consider unseparated steady flow in a shock stationary coordinate system (Fig. 2). The static pressure downstream of the incident shock is⁵

$$\frac{p_2}{p_1} = \frac{2\gamma_1 M_1^2 - (\gamma_1 - 1)}{\gamma_1 + 1} \quad (1)$$

The stagnation pressure in the downstream portion of the thermal layer is⁶

$$\frac{p_{5,t}}{p_4} = \left[1 + \left(\frac{\gamma_4 - 1}{2} \right) M_4^2 \right]^{\gamma_4/(\gamma_4 - 1)} \quad M_4 < 1 \quad (2a)$$

$$= \left[\left(\frac{\gamma_4 + 1}{2} \right) M_4^2 \right]^{\gamma_4/(\gamma_4 - 1)} \left[\frac{\gamma_4 + 1}{2\gamma_4 M_4^2 - (\gamma_4 - 1)} \right]^{1/(\gamma_4 - 1)} \quad M_4 > 1 \quad (2b)$$

As noted in Ref. 2, the interaction between the shock and thermal layer will remain unseparated and steady (in shock fixed coordinates) provided

$p_{5,t}/p_4 > p_2/p_1$. The flow becomes separated and unsteady when $p_{5,t}/p_4 <$

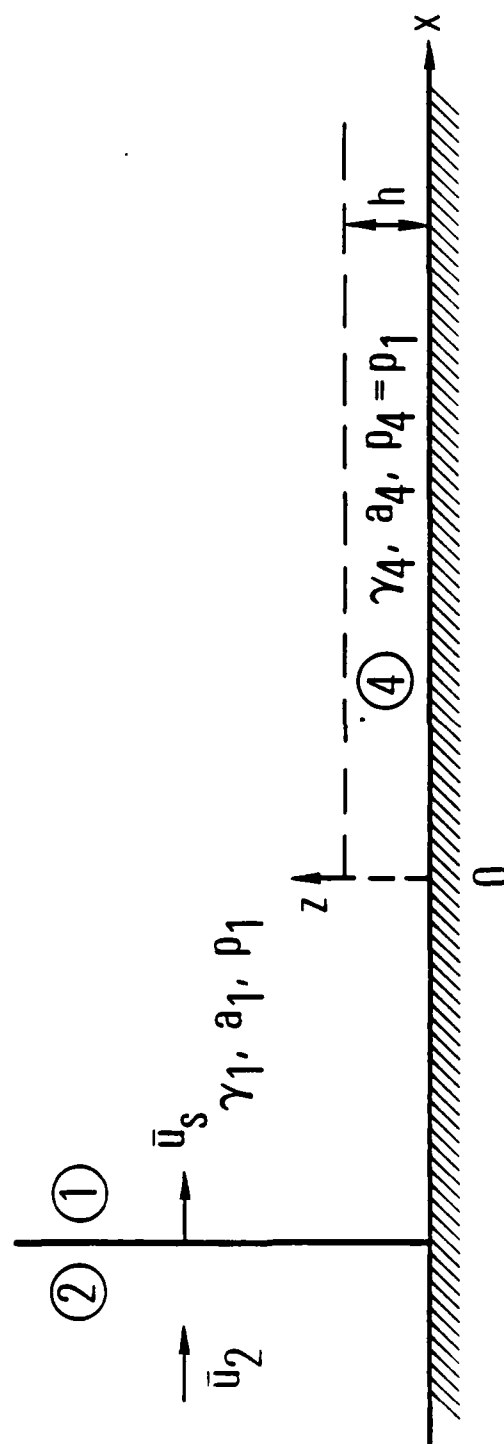


Fig. 1. Initial Conditions in Laboratory Stationary Coordinate System

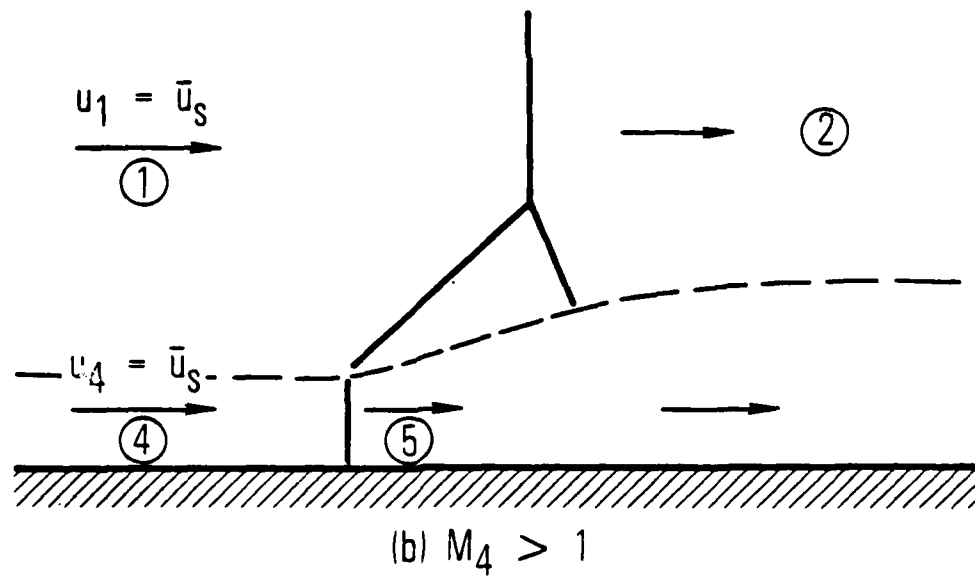
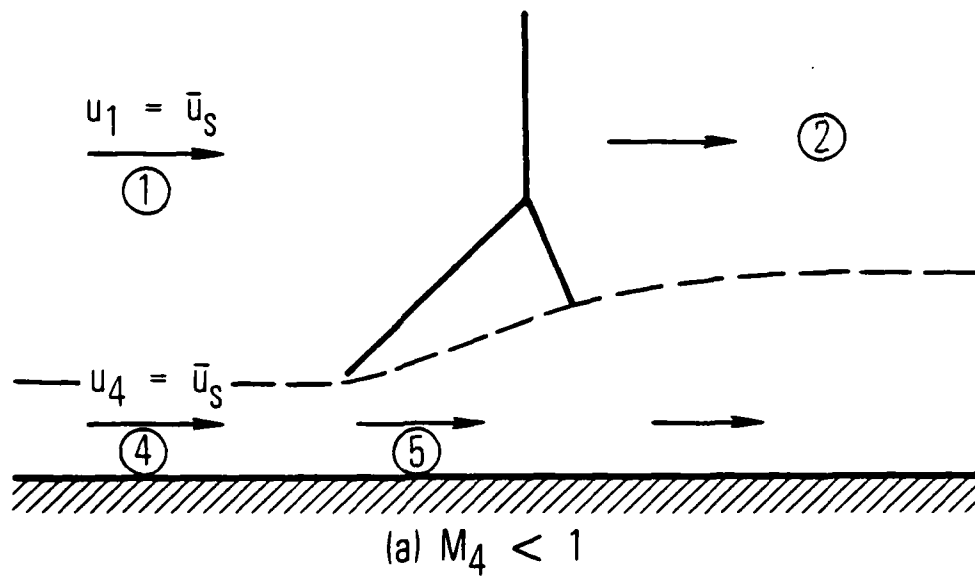


Fig. 2. Unseparated Steady Flow in Incident Shock Stationary Coordinate System

p_2/p_1 . The boundary between the separated and unseparated flow regimes is obtained by equating Eqs. 1 and 2 and noting $M_4 = (a_1/a_4)M_1$. The results are given in Fig. 3 and agree with similar results in Ref. 2. The unseparated flow regime occurs for values of a_4/a_1 and M_1 near one. Increased values of a_4/a_1 and/or M_1 lead to a separated flow, which is discussed in the next section.

B. SEPARATED FLOW REGIME

Numerical results from Ref. 5 and an analytic model are presented herein.

1. NUMERICAL RESULTS

Detailed numerical calculations of the interaction between an incident shock and a thermal layer have been presented in Ref. 5 for various incident shock Mach numbers $\bar{M}_s$ and speed of sound ratios a_4/a_1 . Specific heat ratio values $\gamma_1 = 1.4$ and $\gamma_4 = 5/3$ (approximately) were assumed so that the interface between the fluid in regions 1 and 4 was well defined. Viscous effects were neglected.

Results from Ref. 5 are given in Table 1 and Fig. 4. Figs. 4(a) and 4(b) provide density contours at a fixed instant of time ($x_s = 20.1$ cm), and Fig. 4(c) provides the corresponding pressure distribution at three heights above the ground. Initial conditions were $\bar{M}_s = 2.61$ and $a_4/a_1 = 2.26$. The latter was termed Case II in Ref. 5. A schematic representation of the flow field, inferred from Fig. 4, is given in Fig. 5(a) using coordinates wherein the incident shock is stationary. Shock-heated gas originally from region 1 moves forward of the incident shock and separates the thermal layer gas flow from the wall. The interface between gas from region 1 and gas from region 4 is indicated by a dashed line in Fig. 5(a). The interface location at the wall is denoted x_i . The quantities x_{sp} , x_s , and x_{st} , in Fig. 5(a), denote the streamwise location of a stagnation point, the incident shock, and the leading edge of the normal shock in the thermal layer, respectively. The corresponding locations of these stations are included in Fig. 4. The variation of these locations, with time, deduced from the data reported in Ref. 5, are given in Fig. 6. The local slope of the curves in Fig. 6 define local velocity. These results indicate that, after an initial transient, the

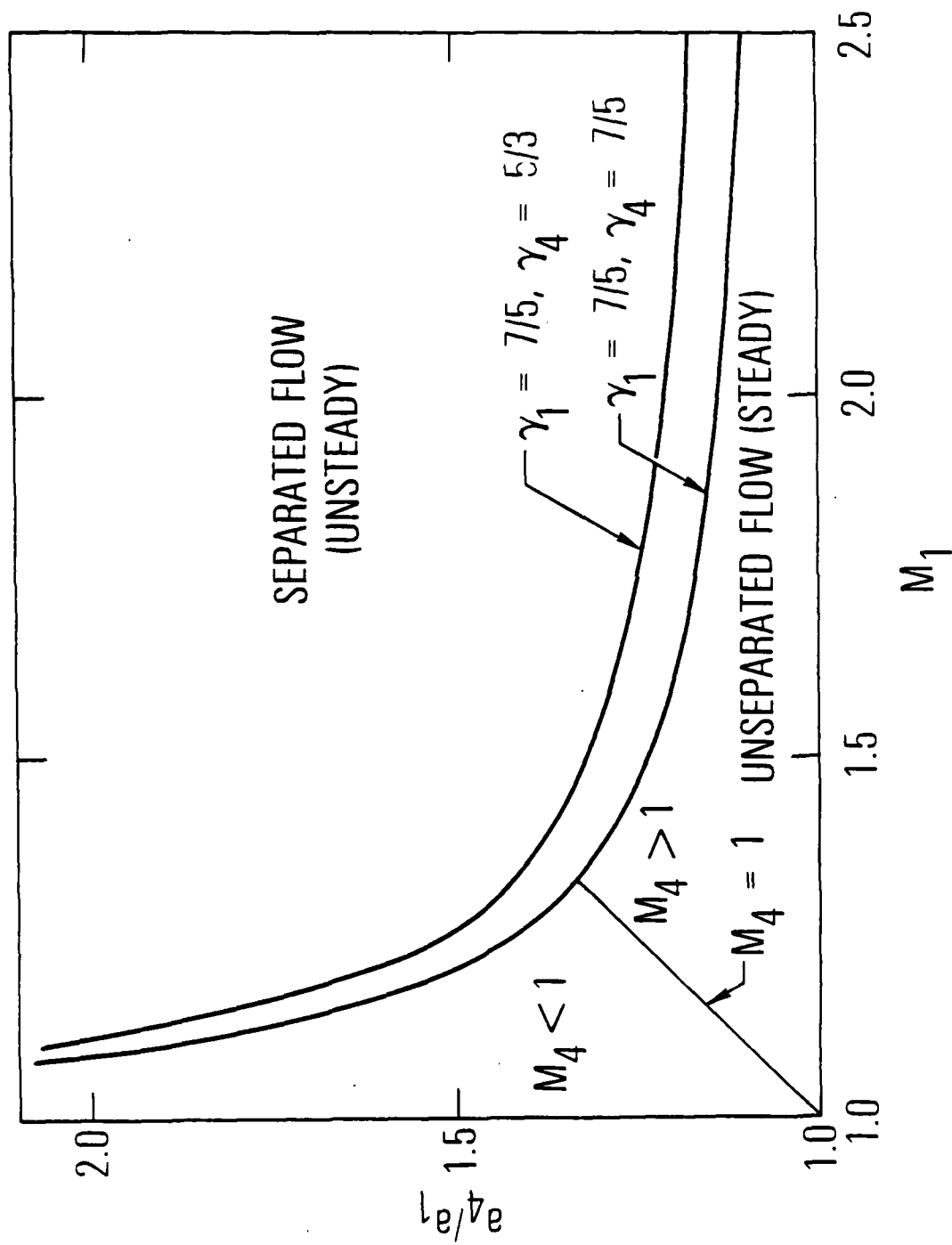


Fig. 3. Boundary Between Separated and Unseparated Flow Regimes

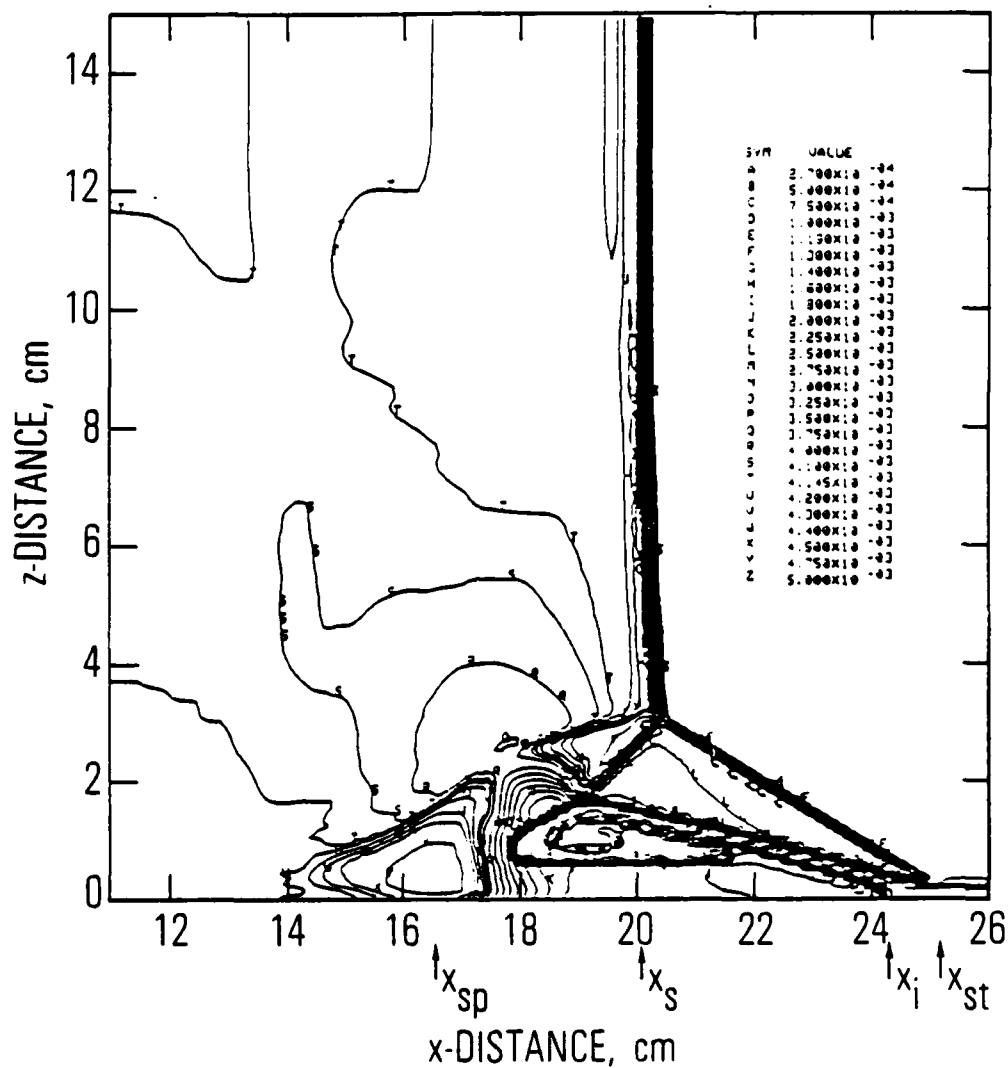


Fig. 4a. Numerical Results of Ref. 5 for Shock-Thermal Layer Interaction. Case II, $x_s = 20.1$ cm. Initial conditions noted in Table 1. (Contours of constant density, overall).

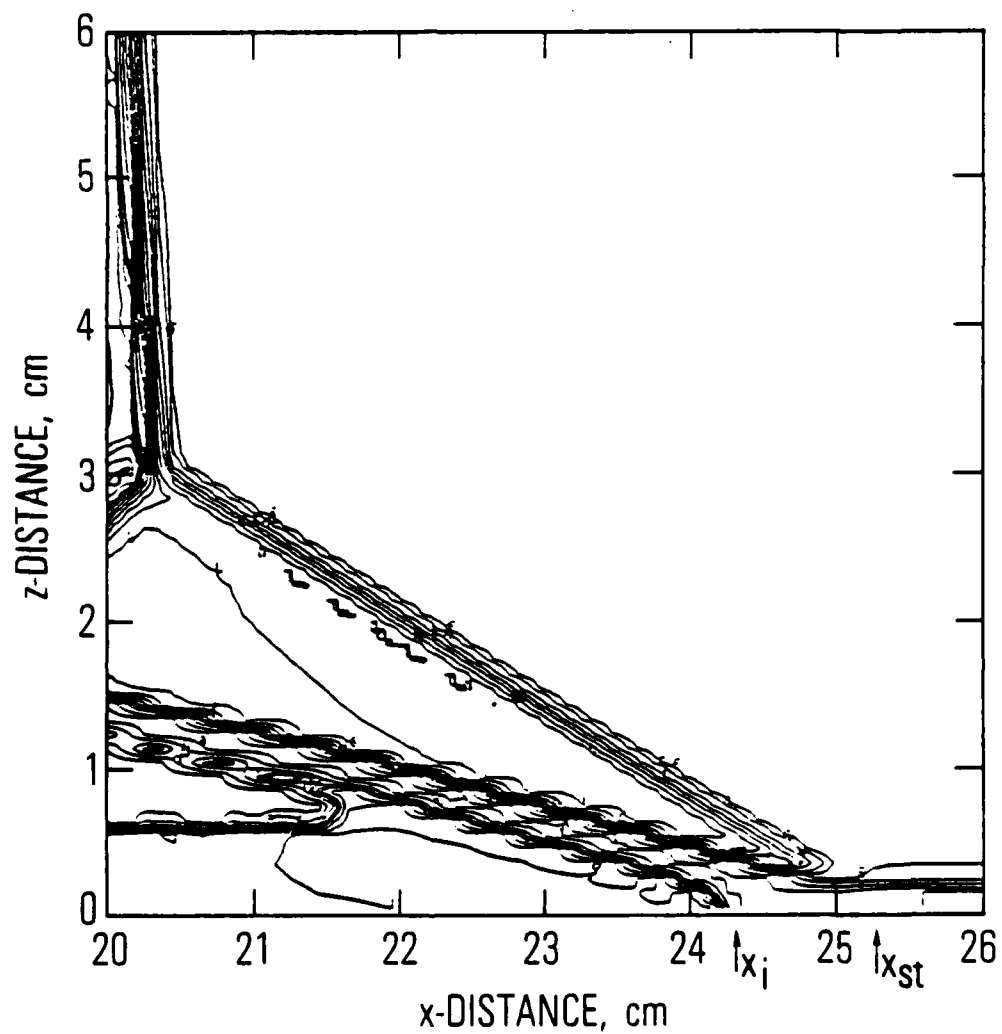


Fig. 4b. Numerical Results of Ref. 5 for Shock-Thermal Layer Interaction. Case II, $x_s = 20.1$ cm. Initial conditions noted in Table 1. (Contours of constant density, detail).

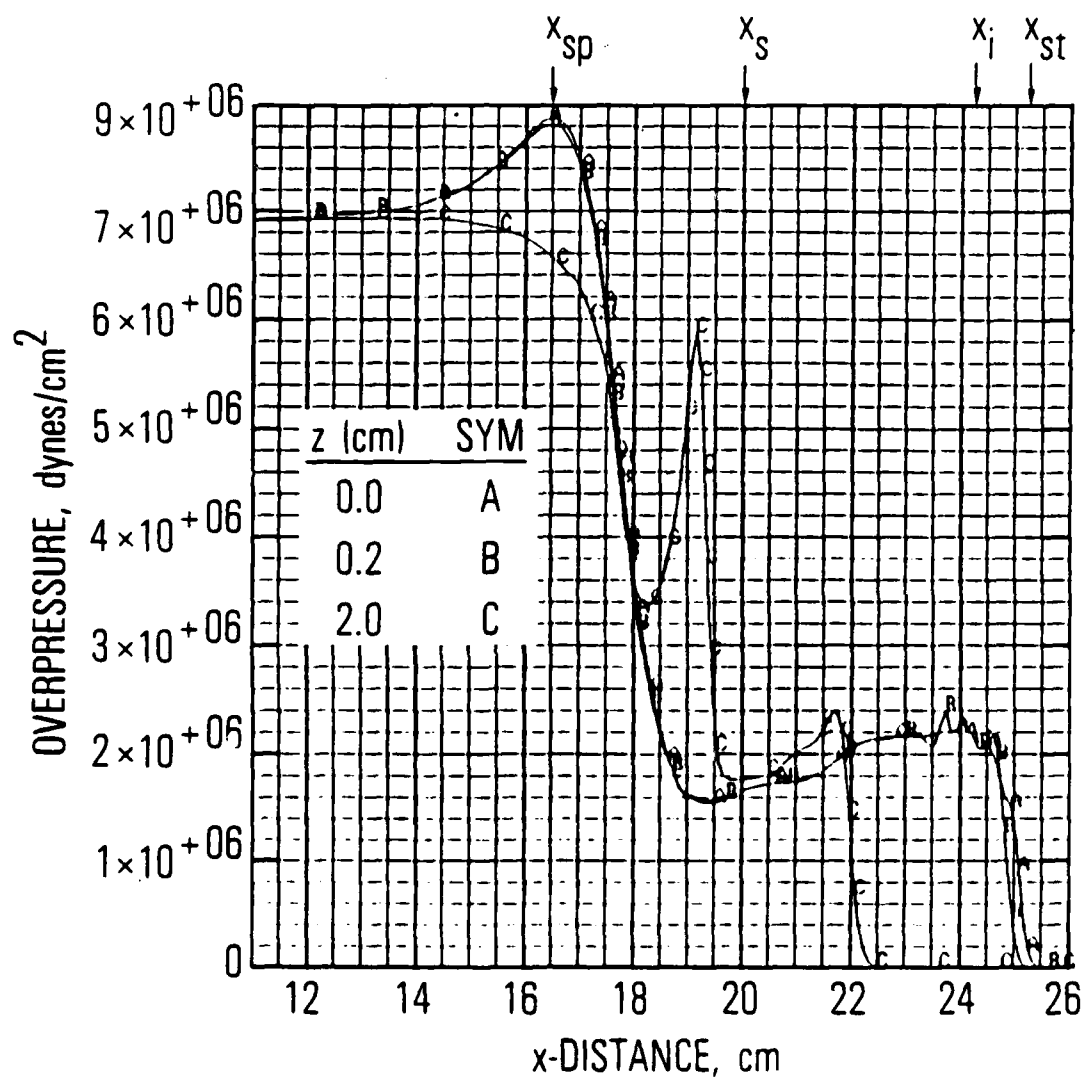


Fig. 4c. Numerical Results of Ref. 5 for Shock-Thermal Layer Interaction. Case II, $x_s = 20.1$ cm. Initial conditions noted in Table 1. (Overpressure at three heights ($p_1 = 1.013 \times 10^6$ dynes/cm²)).

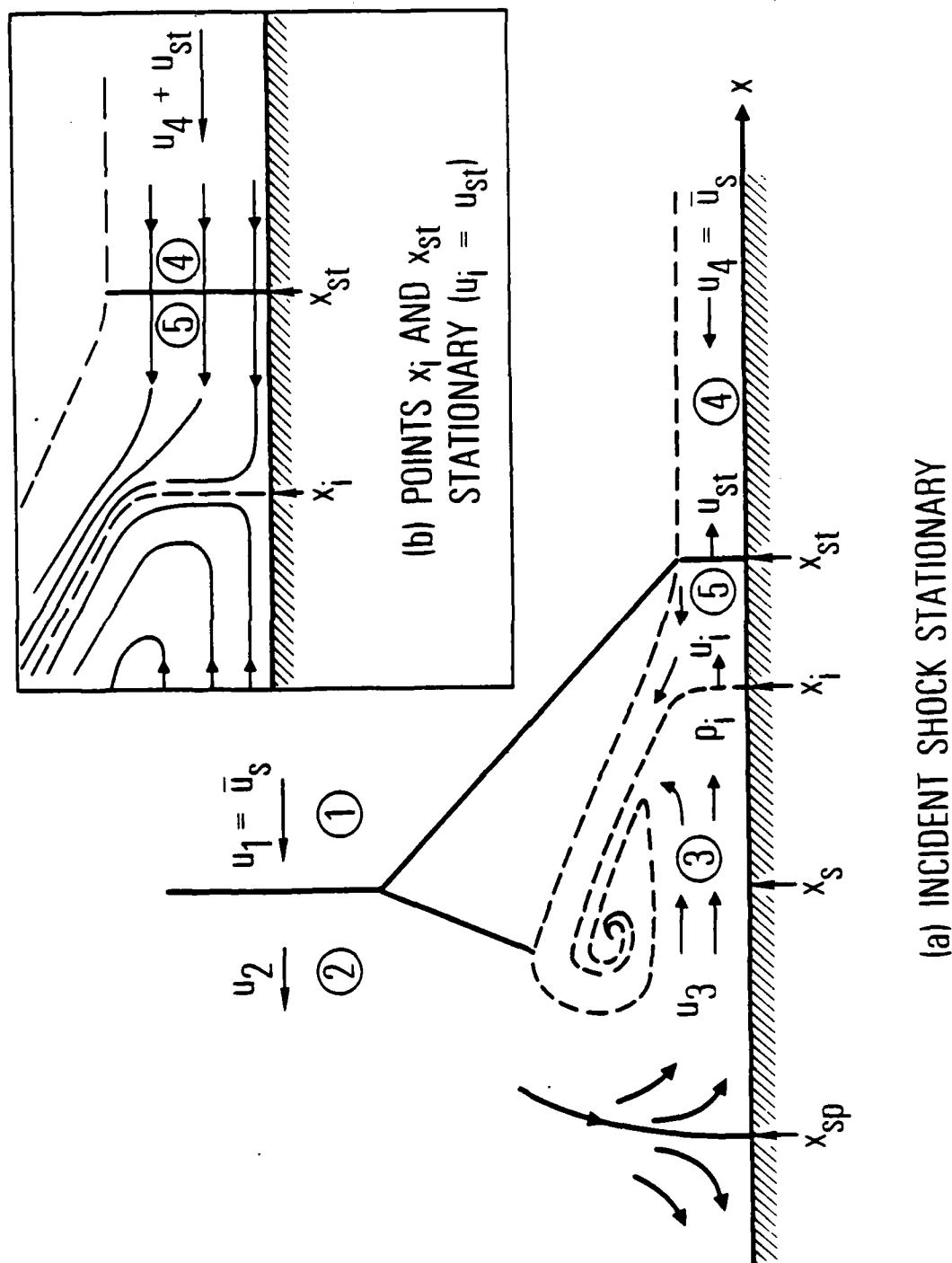


Fig. 5. Schematic Representation of Shock-Thermal Layer Interaction for Case of Separated Flow

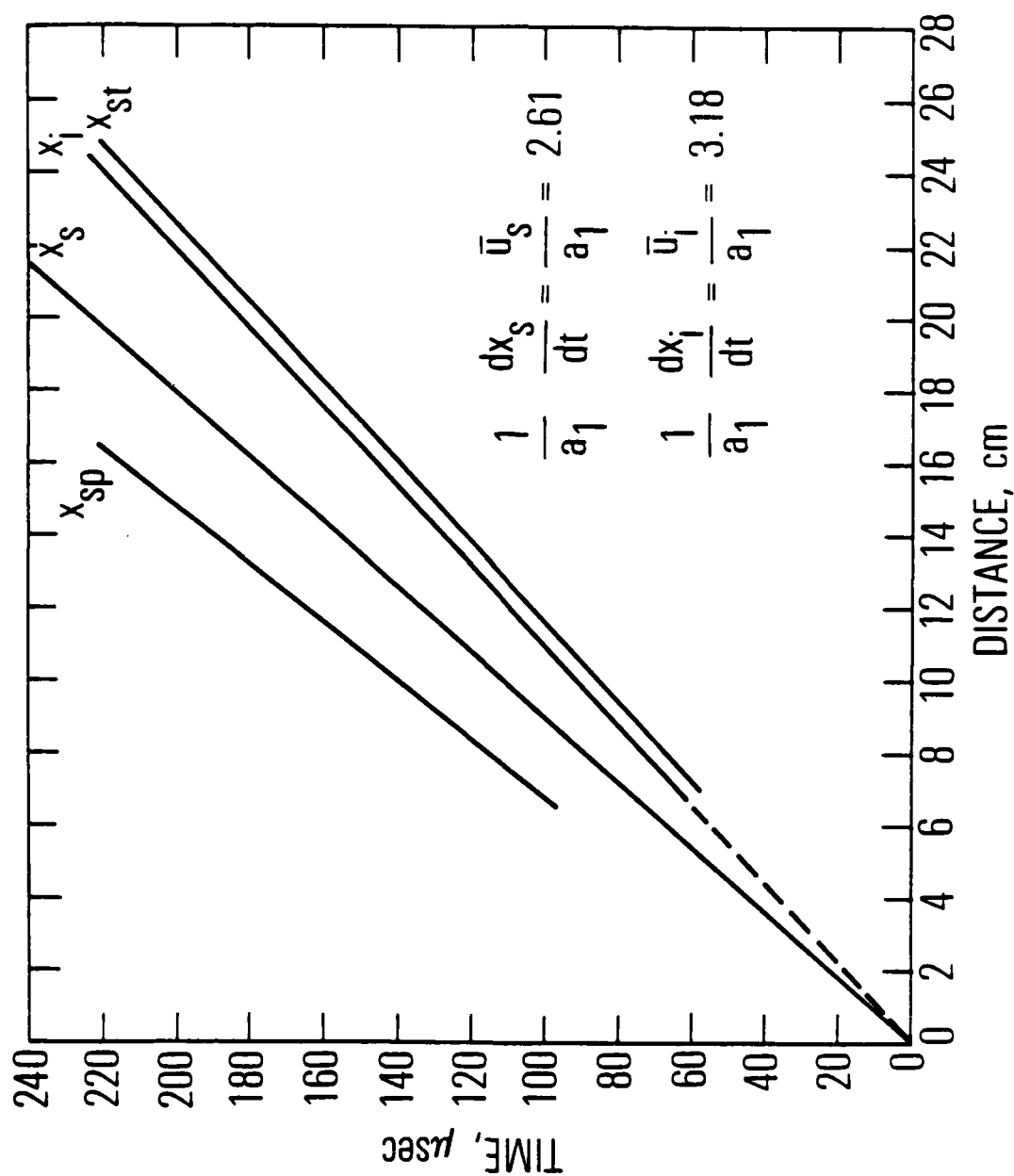


Fig. 6a. Interface Trajectories Based on Numerical Solution of Ref. 5. Initial conditions noted in Table 1. (Case II ($a_4/a_1 = 2.26$, $\bar{M}_8 = 2.61$)).

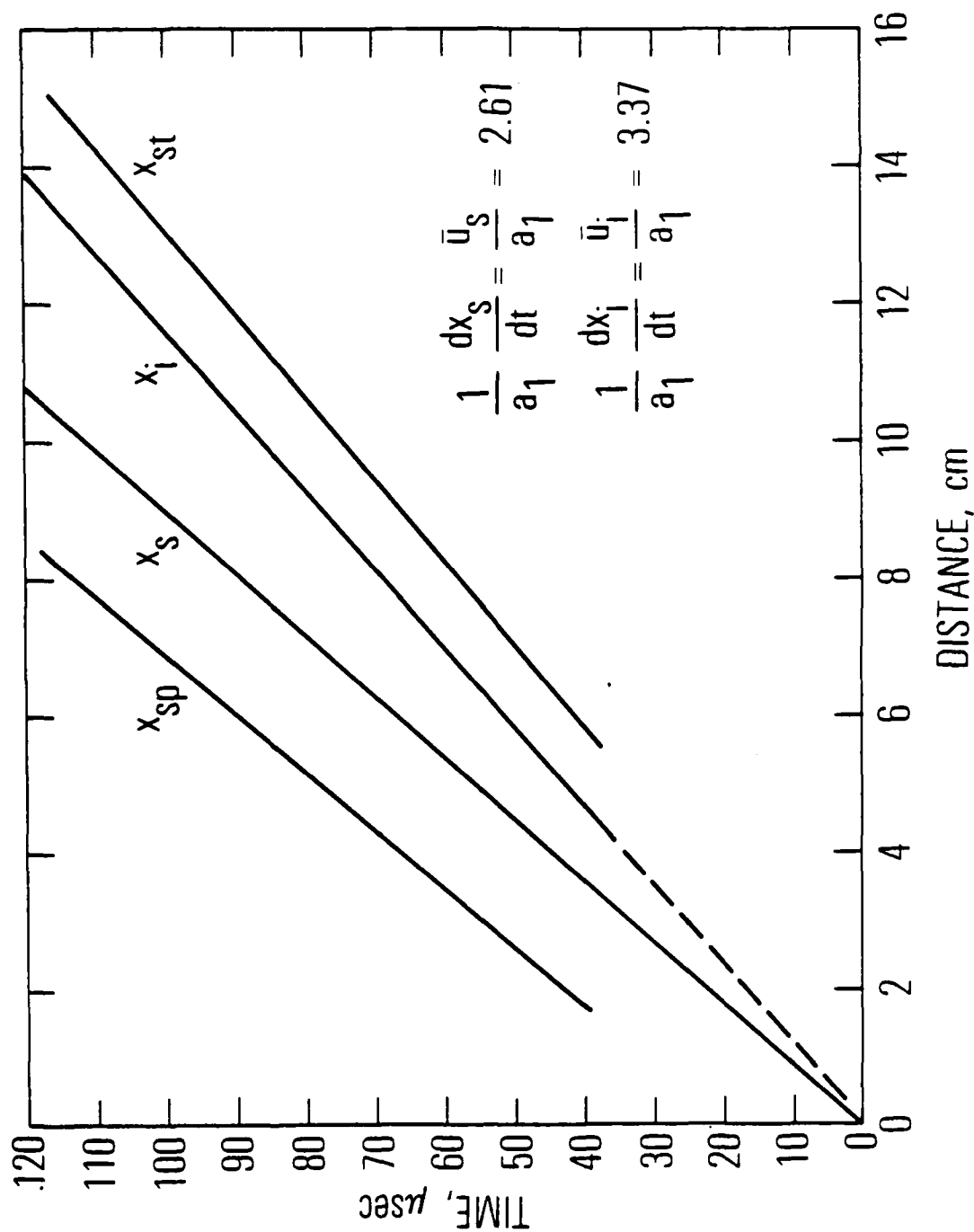


Fig. 6b. Interface Trajectories Based on Numerical Solution of Ref. 5. Initial conditions noted in Table I. (Case VII ($a_4 a_1 = 2.92$, $\bar{M}_s = 2.61$)).

Table 1. Comparison of Numerical Results of Ref. 5 with Present Analytic Model. Initial

conditions are $\gamma_1 = 1.4$, $\gamma_4 = 5/3$, $T_1 = 293$ K, $a_1 = 3.46 \times 10^4$ cm/sec,
 $p_1 = 1.013 \times 10^6$ dynes/cm², $h = 0.2$ cm, $p_2/p_1 = 7.80$, $\bar{M}_s = 2.61$.

Case	$\bar{M}_s$	a_4/a_1	x_s , cm	u_1/a_1	$\bar{M}_{st}$	p_{sp}/p_1	p_1/p_1	$(p_1/p_1)\bar{M}_{st}^b$
II (Ref. 5)	2.61	2.26	8.8	0.57	1.41	8.0	3.2	3.4
			13.7	0.57	1.41	8.3	3.2	3.4
			20.1	0.57	1.41	8.7	3.2	3.4
$k = 0.27^a$				0.47	1.36	9.2	3.2	
$k = 1.00^a$				1.37	1.76	9.2	5.0	
VII (Ref. 5)	2.61	2.92	3.4	0.76	1.15	7.7	2.6	2.5
			7.0	0.76	1.15	7.9	2.6	2.5
			10.5	0.76	1.15	8.3	2.6	2.5
$k = 0.27^a$				0.53	1.08	9.2	2.3	
$k = 1.00^a$				1.66	1.41	9.2	3.7	

^aAnalytic model

^b p_1/p_1 computed from $\bar{M}_{st}$ and Eq. 6(a)

interface location x_i moves with constant speed. The wall stagnation point location x_{sp} moves with a velocity approximately equal to that of the incident shock x_g and, hence, is stationary in incident shock coordinates. Similarly, the leading edge of the normal shock in the thermal layer x_{st} moves with approximately the same velocity as x_i . Thus, the separation distance $x_{st} - x_i$ remains constant. The flow in a coordinate system wherein x_{st} and x_i are stationary is illustrated in Fig. 5(b). The flow in region 5 is steady in this coordinate system. These results suggest an analytic model described in the next section.

2. ANALYTIC MODEL

We consider the flow in an incident shock stationary coordinate system as shown in Fig. 5(a). The stagnation point x_{sp} is assumed to be stationary, and the separation distance $x_{st} - x_i$ is assumed to remain constant for cases when a shock develops in the thermal layer. Flow conditions in each of the regions noted in Fig. 5 are obtained from the following expressions.

a. Region 2

Region 2 is the uniform region downstream of the incident shock. Normal shock relations indicate⁶

$$\frac{p_2}{p_1} = \frac{2\gamma_1 M_1^2 - (\gamma_1 - 1)}{\gamma_1 + 1} \quad (3a)$$

$$\frac{p_{2,t}}{p_1} = \left[\frac{(\gamma_1 + 1)M_1^2}{2} \right]^{\gamma_1/(\gamma_1 - 1)} \left[\frac{\gamma_1 + 1}{2\gamma_1 M_1^2 - (\gamma_1 - 1)} \right]^{1/(\gamma_1 - 1)} \quad (3b)$$

where $p_{2,t}$ is the stagnation pressure in region 2. Since x_{sp} is stationary in the present coordinate system,

$$p_{sp}/p_1 = p_{2,t}/p_1 \quad (3c)$$

The possibility that the flow at p_{sp} was processed by the oblique-normal shock structure at the base of the incident shock is ignored in Eq. 3(c). However, the effect on p_{sp} should not be large.

b. Region 3

Conditions in region 3 are assumed to result from a steady isentropic expansion from conditions in region 2. Expressions of interest are

$$\frac{p_3}{p_1} \equiv \frac{p_3}{p_{3,t}} \frac{p_{2,t}}{p_1} = \left[1 + \frac{(\gamma_1 - 1)M_3^2}{2} \right]^{-\gamma_1/(\gamma_1 - 1)} \frac{p_{2,t}}{p_1} \quad (4a)$$

$$\frac{u_3}{a_1} \equiv \frac{u_3}{a_3} \frac{a_3/a_{3,t}}{a_1/a_{1,t}} = M_3 \left[\frac{2 + (\gamma_1 - 1)M_3^2}{2 + (\gamma_1 - 1)M_1^2} \right]^{-1/2} \quad (4b)$$

$$\begin{aligned} \frac{\bar{Q}_3}{\bar{Q}_2} &\equiv \frac{\rho_3(\bar{u}_3)^2}{\rho_2(\bar{u}_2)^2} \\ &= \left[\frac{2 + (\gamma_1 - 1)M_3^2}{2 + (\gamma_1 - 1)M_2^2} \right]^{-1/(\gamma_1 - 1)} \left[\frac{(u_3/a_1) + M_1}{2(\gamma_1 + 1)^{-1}(M_1 - M_1^{-1})} \right]^2 \end{aligned} \quad (4c)$$

where $\bar{Q}$ denotes dynamic pressure in laboratory coordinates.

c. Region 5

For cases in which a shock develops in the thermal layer, the separation distance $x_{st} - x_i$ is assumed to remain constant (Fig. 6). The flow in region 5 is then equivalent to steady supersonic flow with Mach number

$$\bar{M}_{st} \equiv \frac{\bar{u}_{st}}{a_4} = \frac{\bar{u}_i}{a_4} = \frac{M_1 + (u_i/a_1)}{a_4/a_1} \quad (5)$$

over a blunt body defined by the interface at x_i . For cases in which a shock does not develop, the flow in region 5 is equivalent to subsonic flow at Mach number $\bar{u}_1/a_4$ over a blunt body defined by the interface. The pressure p_1 corresponds to the stagnation pressure at the nose of the equivalent body and is found from

$$\frac{p_1}{p_1} = \left[\frac{(\gamma_4 + 1) \bar{M}_{st}^2}{2} \right]^{\gamma_4/(\gamma_4 - 1)} \left[\frac{\gamma_4 + 1}{2\gamma_4 \bar{M}_{st}^2 - (\gamma_4 - 1)} \right]^{1/(\gamma_4 - 1)} \quad \bar{M}_{st} > 1 \quad (6a)$$

$$= \left[1 + \frac{\gamma_4 - 1}{2} \left(\frac{\bar{u}_1}{a_4} \right)^2 \right]^{\gamma_4/(\gamma_4 - 1)} \quad \bar{u}_1/a_4 < 1 \quad (6b)$$

where $\bar{M}_{st}$ and $\bar{u}_1/a_4$ can be used interchangeably (Eq. 5).

d. Method of Solution

The interaction is uniquely determined by specification of the initial conditions $\bar{M}_s$, γ_1 , γ_4 , a_4/a_1 , and h . (The quantity h is not needed, however, for the present model.) Estimates for flow properties can be obtained from the previous equations if the boundary conditions at the interface location x_i are specified. In the present model, we assume that conditions in regions 3 and 5, at x_i , are related by

$$p_1 = p_3 \quad (7a)$$

$$u_1 = k u_3 \quad (7b)$$

The arbitrary constant k is introduced to permit matching of the analytic model with numerical code calculations. A value of $k < 1$ can be interpreted as indicating a transverse velocity in region 3 at the interface (Fig. 7). A simple procedure for evaluating the previous equations is to specify γ_1 , γ_4 , $M_1 \equiv \bar{M}_s$, and M_3 . $\bar{M}_{st}$ (or, equivalent, $\bar{u}_1/a_4$) is found, by iteration, by

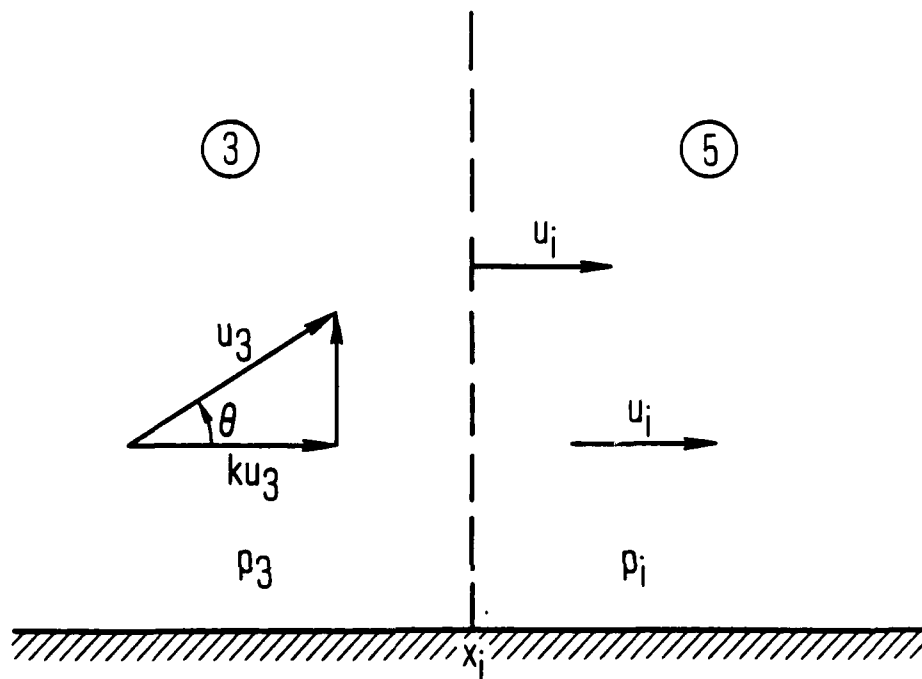


Fig. 7. Boundary Conditions Near Interface x_i in Incident Shock Stationary Coordinate System, $k \equiv \cos \theta$.

equating Eqs. 6 and 4(a). The corresponding values of a_4/a_1 and $\bar{u}_1/a_1$ are obtained from Eqs. 5 and 7(b), namely

$$a_4/a_1 = [(M_1 + (ku_3/a_1))/\bar{M}_{st}] \quad (8a)$$

$$\bar{u}_1/a_1 = (\bar{u}_1/a_4)(a_4/a_1) \quad (8b)$$

Using the present procedure, a_4/a_1 and $\bar{u}_1/a_1$ are the only quantities that depend on the value of k . Numerical results are given in Table 2 for the case $k = 1$. For a given incident shock $\bar{M}_s$, the dynamic pressure ratio $\bar{Q}_3/\bar{Q}_2$ has a maximum at a particular value of a_4/a_1 . The maximum is characteristic of the isentropic expansion to M_3 . Values of $\bar{M}_{st}$ in the range $\bar{M}_{st} < 1$ indicate that a shock is not formed in the thermal layer.

Table 2. Results of Analytical Model for $k = 1$, $\gamma_1 = 1.4$, and $\gamma_4 = 1.4$, $5/3$

$\bar{M}_s$	M_3	u_3/a_1	p_3/p_1	a_4/a_1	$\bar{M}_{st}$	Q_3/Q_2	a_4/a_1	$\bar{M}_{st}$	Q_3/Q_2
1.100	1.300	1.017	1.127	5.005	.416	164.943	5.529	.383	164.943
1.100	1.300	1.017	1.127	2.733	.710	148.668	3.957	.657	148.668
1.100	1.300	1.017	1.127	1.963	.880	148.668	3.103	.859	148.668
1.500	1.400	1.017	1.127	1.406	1.402	9.442	1.501	1.316	9.442
1.500	1.400	1.017	1.127	1.111	1.288	10.642	1.318	1.209	10.642
1.500	1.400	1.017	1.127	1.072	1.194	11.239	1.252	1.109	11.239
1.500	1.400	1.017	1.127	1.021	1.168	12.836	1.102	1.063	12.836
2.000	2.000	1.017	1.127	1.151	1.965	3.790	1.235	1.791	3.790
2.000	2.000	1.017	1.127	1.091	1.881	4.476	1.169	1.737	4.476
2.000	2.000	1.017	1.127	1.037	1.745	5.048	1.097	1.637	5.048
2.000	2.000	1.017	1.127	1.000	1.630	5.568	1.043	1.595	5.568
2.000	2.000	1.017	1.127	1.000	1.572	6.045	1.012	1.589	6.045
3.000	3.000	1.017	1.127	1.131	2.63	2.57	1.20	3.0	2.57
3.000	3.000	1.017	1.127	1.053	2.35	3.42	1.03	2.1	3.42
3.000	3.000	1.017	1.127	1.037	2.19	4.29	1.03	2.1	4.29
3.000	3.000	1.017	1.127	1.017	2.06	5.02	1.03	2.1	5.02
3.000	3.000	1.017	1.127	1.000	1.927	5.76	1.03	2.1	5.76
4.000	4.000	1.017	1.127	1.202	3.52	2.65	1.20	4.0	2.65
4.000	4.000	1.017	1.127	1.093	3.04	3.53	1.03	3.5	3.53
4.000	4.000	1.017	1.127	1.037	2.64	4.29	1.03	3.5	4.29
4.000	4.000	1.017	1.127	1.017	2.36	5.02	1.03	3.5	5.02
4.000	4.000	1.017	1.127	1.000	2.11	5.76	1.03	3.5	5.76
5.000	5.000	1.017	1.127	1.302	4.52	2.65	1.30	5.0	2.65
5.000	5.000	1.017	1.127	1.111	3.83	3.53	1.10	4.5	3.53
5.000	5.000	1.017	1.127	1.037	3.24	4.29	1.03	4.5	4.29
5.000	5.000	1.017	1.127	1.017	2.85	5.02	1.03	4.5	5.02
5.000	5.000	1.017	1.127	1.000	2.56	5.76	1.03	4.5	5.76
6.000	6.000	1.017	1.127	1.402	5.52	2.65	1.40	6.0	2.65
6.000	6.000	1.017	1.127	1.111	4.63	3.53	1.10	5.5	3.53
6.000	6.000	1.017	1.127	1.037	3.94	4.29	1.03	5.5	4.29
6.000	6.000	1.017	1.127	1.017	3.45	5.02	1.03	5.5	5.02
6.000	6.000	1.017	1.127	1.000	3.16	5.76	1.03	5.5	5.76
7.000	7.000	1.017	1.127	1.502	6.52	2.65	1.50	7.0	2.65
7.000	7.000	1.017	1.127	1.111	5.43	3.53	1.10	6.5	3.53
7.000	7.000	1.017	1.127	1.037	4.64	4.29	1.03	6.5	4.29
7.000	7.000	1.017	1.127	1.017	4.15	5.02	1.03	6.5	5.02
7.000	7.000	1.017	1.127	1.000	3.86	5.76	1.03	6.5	5.76
8.000	8.000	1.017	1.127	1.602	7.52	2.65	1.60	8.0	2.65
8.000	8.000	1.017	1.127	1.111	6.43	3.53	1.10	7.5	3.53
8.000	8.000	1.017	1.127	1.037	5.64	4.29	1.03	7.5	4.29
8.000	8.000	1.017	1.127	1.017	5.15	5.02	1.03	7.5	5.02
8.000	8.000	1.017	1.127	1.000	4.86	5.76	1.03	7.5	5.76

Table 2. Results of Analytical Model for $k = 1$, $Y_1 = 1.4$, and $Y_4 = 5/3$ (Continued)

$\bar{M}_s$	M_3	u_3/a_1	p_3/p_1	$Y_4 = 1.4$				$Y_4 = 5/3$			
				a_4/a_1	$\bar{M}_{st}$	Q_3/Q_2	a_4/a_1	$\bar{M}_{st}$	Q_3/Q_2	a_4/a_1	Q_3/Q_2
4.0000	2.330	1.207	23.163	1.128	3.967	2.140	1.193	3.941	2.140	1.193	2.140
4.0000	2.400	1.108	18.517	1.129	3.530	2.150	1.156	3.507	2.150	1.156	2.150
4.0000	2.500	1.054	16.923	1.172	3.220	2.155	1.137	3.197	2.155	1.137	2.155
4.0000	1.0000	1.0000	1.0000	1.204	2.525	2.163	1.170	2.500	2.163	1.170	2.163
4.0000	1.230	1.162	6.062	2.294	2.182	2.163	2.203	2.167	2.163	2.203	2.163
4.0000	2.000	1.473	25.358	1.126	4.327	2.163	1.191	4.285	2.163	1.191	2.163
4.0000	2.600	1.302	22.406	1.246	4.275	2.162	1.359	4.173	2.162	1.359	2.162
4.0000	3.000	1.095	17.121	1.722	3.621	2.158	1.826	3.389	2.158	1.826	2.158
4.0000	1.230	1.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
4.0000	1.400	2.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
5.0000	2.000	1.473	25.358	1.126	4.327	2.163	1.191	4.285	2.163	1.191	2.163
5.0000	2.600	1.302	22.406	1.246	4.275	2.162	1.359	4.173	2.162	1.359	2.162
5.0000	3.000	1.095	17.121	1.722	3.621	2.158	1.826	3.389	2.158	1.826	2.158
5.0000	1.230	1.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
5.0000	1.400	2.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
6.0000	2.000	1.473	25.358	1.126	4.327	2.163	1.191	4.285	2.163	1.191	2.163
6.0000	2.600	1.302	22.406	1.246	4.275	2.162	1.359	4.173	2.162	1.359	2.162
6.0000	3.000	1.095	17.121	1.722	3.621	2.158	1.826	3.389	2.158	1.826	2.158
6.0000	1.230	1.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
6.0000	1.400	2.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
6.0000	2.000	1.473	25.358	1.126	4.327	2.163	1.191	4.285	2.163	1.191	2.163
6.0000	2.600	1.302	22.406	1.246	4.275	2.162	1.359	4.173	2.162	1.359	2.162
6.0000	3.000	1.095	17.121	1.722	3.621	2.158	1.826	3.389	2.158	1.826	2.158
6.0000	1.230	1.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
6.0000	1.400	2.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
8.0000	2.000	1.473	25.358	1.126	4.327	2.163	1.191	4.285	2.163	1.191	2.163
8.0000	2.600	1.302	22.406	1.246	4.275	2.162	1.359	4.173	2.162	1.359	2.162
8.0000	3.000	1.095	17.121	1.722	3.621	2.158	1.826	3.389	2.158	1.826	2.158
8.0000	1.230	1.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
8.0000	1.400	2.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
10.0000	2.000	1.473	25.358	1.126	4.327	2.163	1.191	4.285	2.163	1.191	2.163
10.0000	2.600	1.302	22.406	1.246	4.275	2.162	1.359	4.173	2.162	1.359	2.162
10.0000	3.000	1.095	17.121	1.722	3.621	2.158	1.826	3.389	2.158	1.826	2.158
10.0000	1.230	1.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131
10.0000	1.400	2.061	10.340	2.241	2.471	2.131	2.209	2.472	2.131	2.209	2.131

III. DISCUSSION

The present analytic model is compared in Table 1 with numerical data from Ref. 5. Values of u_1/a_1 , $\bar{M}_{st}$, p_{sp}/p_1 , and p_i/p_1 , from Ref. 5, are given as a function of incident shock location x_s for two initial conditions (Cases II and VII). Analytic estimates for these quantities, based on $k = 1.00$ and $k = 0.27$, are included in Table 1. The values of p_{sp}/p_1 in Ref. 5 increase with x_s and appear to approach the analytic estimate. Hence, the assumption $p_{sp}/p_1 = p_{2,t}/p_1$ [Eq. 3(c)] appears reasonable. Other analytic estimates in Table 1 depend on the choice for k . The initial choice, $k = 1.00$, led to an overestimate of u_1/a_1 , $\bar{M}_{st}$, and p_i/p_1 . However, the variation of these quantities with a_4/a_1 had the proper trend. The second value, $k = 0.27$, was chosen so that the analytic estimate for p_i/p_1 would agree with the numerical result in Ref. 5 for Case II. This led to improved correlations between the analytic model and the Cases II and VII data from Ref. 5. However, the usefulness of the approximation $k = 0.27$ for other initial conditions is uncertain and requires further study.

The interface pressure p_i/p_1 was also computed from Eq. 6(a) using the value of $\bar{M}_{st}$ deduced from the data in Ref. 5. The resulting pressure is denoted $(p_i/p_1)_{\bar{M}_{st}}$ in Table 1 and agrees with the value of p_i/p_1 reported in Ref. 5. This calculation confirms the analytic model assumption that the pressure p_i/p_1 equals the stagnation pressure associated with $\bar{M}_{st}$ (Eq. 6).

IV. CONCLUSION

Numerical solutions⁵ for the inviscid interaction between a moving shock and a thermal layer have been reviewed. The streamwise locations x_{sp} , x_s , x_i , and x_{st} were of particular interest. It was determined that after an initial transient $dx_{sp}/dt \doteq dx_s/dt \equiv \bar{u}_s$. This led to the assumption, in the analytic model, that the pressure at x_{sp} can be equated to the stagnation pressure behind the incident shock in incident shock stationary coordinates ($p_{sp} = p_{2,t}$). Similarly, it was concluded that after an initial transient $dx_{st}/dt \doteq dx_i/dt \equiv \bar{u}_i$. Hence, the pressure p_i at x_i was assumed, in the analytic model, to be equivalent to the stagnation pressure on a blunt body in a Mach number $\bar{M}_{st} = \bar{u}_i/a_4$ flow. The analytic model was only partly successful in predicting x_i and p_i . The introduction of a free constant $k = u_3/u_1$ was required. This constant is related to the angularity of the flow in region 3. The choice $k = 0.27$ led to good agreement between the analytic model and data from cases II and VII. However, the large departure of k , from one, makes the physical interpretation questionable. Further comparisons with numerical solutions are needed to validate the analytic model.

In the present inviscid model, the scale of the disturbed flow grows linearly and without limit. It is expected that viscous effects will cause the flow to approach an asymptotic limit. The scale and nature of the flow, in this limit, also requires further study.

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SYMBOLS

a	speed of sound
h	initial height of thermal layer
k	arbitrary constant, $k < 1$
M	Mach number in incident shock stationary coordinate system, u/a
$\bar{M}$	Mach number in laboratory coordinates, $\bar{u}/a$
p	pressure
$\bar{Q}$	dynamic pressure in laboratory coordinates, $\rho(\bar{u})^2/2$
t	time
$u, \bar{u}$	velocity
x, z	streamwise and vertical directions, respectively
γ	ratio of specific heats

SUBSCRIPTS

$1, 2, 3, 4, 5$	flow regions
i	interface value
s	incident shock
st	shock in thermal layer
sp	stagnation point at foot of incident shock
t	stagnation value

SUPERSCRIPTS

$(\bar{\quad})$	superscript bar denotes laboratory coordinates
$(\quad)$	absence of superscript bar denotes incident shock stationary coordinates

LABORATORY OPERATIONS

The Aerospace Corporation functions as an "architect-engineer" for national security projects, specializing in advanced military space systems. Providing research support, the corporation's Laboratory Operations conducts experimental and theoretical investigations that focus on the application of scientific and technical advances to such systems. Vital to the success of these investigations is the technical staff's wide-ranging expertise and its ability to stay current with new developments. This expertise is enhanced by a research program aimed at dealing with the many problems associated with rapidly evolving space systems. Contributing their capabilities to the research effort are these individual laboratories:

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