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An Electron Ring Extraction Scheme from The Modified Betatron Accelerator

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AN ELECTRON RING EXTRACTION SCHEME FROM THE MODIFIED BETATRON ACCELERATOR

INTRODUCTION

The modified betatron accelerator^{1,2} is one among the several compact¹⁻⁵ high current accelerator concepts currently under development in various laboratories. In this device a strong toroidal magnetic field B_θ has been added to the conventional betatron⁶ magnetic field configuration. Although B_θ substantially improves the stability of the conventional betatron, the beam injection and capture and the electron ring extraction after the completion of acceleration are substantially more involved as a result of the toroidal field.

In this report, we describe an extraction scheme that is easily realizable and has the potential to lead to very high extraction efficiency. Briefly, the proposed extraction scheme is based on the transformation of the circulating electron ring into a stationary helix, in the toroidal direction, by exciting the resonance that naturally exists for some specific values of the ratio of the vertical to toroidal magnetic field. Transformation of the ring into a helix is achieved with a localized vertical magnetic field disturbance that is generated by an agitator coil. As the minor radius of the helix increases with each passage through the gap of the agitator coil, the electrons eventually reach the extractor, which has the property that all the magnetic field components transverse to its axis are equal to zero. Thus, the electron ring unwinds into a straight beam.

Description of the Extraction Scheme

After the completion of acceleration, i.e., when the desired electron beam energy has been achieved, the electron ring centroid is displaced radially by intentionally mismatching the magnetic flux and the betatron magnetic field. In the results that

will be shown in the next Section, this mismatch has been achieved by superimposing a low amplitude vertical magnetic field that varies exponentially with time on the betatron field. It has been shown theoretically and verified by extensive numerical results that during the radial displacement of the ring centroid the amplitude of the slow mode¹ remains very small, i.e., a few mm, provided the mismatching field varies slowly with respect to the ring bounce (poloidal) period. Furthermore, computer simulations with the NRL MOBE particle-in-cell computer code have shown that during the radial displacement, that lasts several microseconds, the minor cross section of the ring preserves its integrity and the ring emittance remains constant.

As the major radius of the ring centroid increases slowly with time, the gyrating electrons reach the localized magnetic disturbance generated by the agitator coil. At this radial position the ratio of the vertical magnetic field B_z to the toroidal magnetic field B_θ has been selected to satisfy the condition

$$B_z/B_\theta = 2 l / (2 l^2 - 1), \quad (1)$$

where $l = 1, 2, 3, \dots$

Equation (1) implies that the frequency of the fast mode¹ is l times the frequency of gyration around the major axis. When $B_\theta \gg B_z$, Eq. (1) is reduced to $\Omega_\theta = l\Omega_z$, where $\Omega_\theta = eB_\theta/m$ and $\Omega_z = eB_z/m$.

The purpose of the magnetic disturbance is to excite the resonance^{7,8}. As an electron enters the lower magnetic field region of the disturbance, its velocity vector that initially is directed in the toroidal direction, rotates slightly in the radial direction, i.e., the electron obtains a radial velocity component. It can be

shown from the equations of motion that this radial velocity is given by

$$\Delta v_r \approx -2(\Delta \Omega_z^a / \gamma) r_a \Delta \theta, \quad (2)$$

where $\Delta \Omega_z^a$ is the cyclotron frequency that corresponds to the field of the disturbance generated by the agitator coil, γ is the relativistic factor, r_a is the radial distance of the agitator coil and $\Delta \theta$ is the toroidal half width of the magnetic disturbance.

As a result of the acquired radial velocity, the electrons start to gyrate in the toroidal magnetic field with a radius

$$\rho = 2(N/l)(\Delta \Omega_z^a / \Omega_z) r_a \Delta \theta, \quad (3)$$

where N is the number of passes through the disturbance. If condition (1) is not satisfied, ρ grows as $N^{1/2}$ instead of proportionally to N .

Since γ is very large, self fields can be ignored. However, because of the gradient of B_z the slow mode¹ (bounce motion) is still excited and the orbits of electrons in the transverse (r, z) plane precess very slowly. Therefore, for times short in comparison with the bounce period, i.e., for a few revolutions around the major axis, all the electrons of the ring perform coherent motion and a stationary helix, in the toroidal direction, is formed. A top view of the helix is shown in Fig. 1, for $l = 3$.

Ideally, the radial gradient of the magnetic disturbance should be extremely high, because otherwise the fast mode¹ is excited before the ring reaches the disturbance. In the computer runs of the next Section a disturbance with a

satisfactorily sharp radial gradient is obtained by the single turn agitator coil shown in Fig. 2. The radial gradient of the disturbance is further improved with two single turn loops that are located at the edges of the gap. The radial profile of the B_z field is shown schematically in Fig. 3. In the computer runs, the magnetic field of the disturbance has been obtained from exact analytical expressions that are given in the Appendix.

With successive passes through the disturbance of the agitator the radial excursion of the orbit increases until the gyrating electrons reach the extractor, which is located at $\theta=0$ and at a slightly greater radial distance than the agitator coil. The results of the next section were obtained with a simple extractor consisting of two parallel plates with current flowing in opposite directions. These two plates have infinite extent in the z and semi-infinite extent in the y direction. The linear current density of the plates is adjusted to make the total B_z between the plates at $\theta=0$ equal to zero. The side of the extractor at $\theta=0$ is completely enclosed by the thin conducting foil. As a result the fringing fields are absent. The electrons enter the extractor through this foil without any substantial energy loss. At the entrance of the extractor the vertical displacement of the electrons and their radial velocity are almost zero. However, they have a small vertical velocity.

In practice, this extractor can be realized by bending the two plates to form a torus. In order for the field to be uniform over a finite vertical distance, the cross section of each plate, after bending, should be D-shaped. In the results of the next Section, the orbit of the extracted beam is terminated after it propagates tens of cm inside the extractor. The reason is that the disturbance of the extractor ΔB_z^e is independent of y while the betatron field decreases with y . Thus,

cancellation of the fields is not achieved over the entire length of the extractor. In practice exact cancellation of the two fields can be obtained by increasing the separation of the two plates as y increases.

In the previous discussions, we have assumed that the magnetic disturbance generated by the agitator coil is static. An alternate mode of operation is to expand the ring until it reaches the gap of the agitator coil and then to rapidly pulse the coil. Since the inductance of the agitator is typically only a few nH, short rise times, of the order of 1 nsec can be achieved with modest voltages. In the pulsed mode of operation the fraction of the ring that will be lost is approximately equal to the ratio: coil rise time/ period of gyration around the major axis.

Finally, it should be noticed that an ion channel⁹ formed by a laser beam along the axis of the extractor may improve the extraction process and eliminate the need for an additional coil to cancel the component of B_θ that is transverse to the axis of the extractor or the need to completely cancel the B_z inside the extractor.

RESULTS

We have studied the proposed extraction scheme in both the static and pulsed mode for a range of parameters that are compatible with the NRL modified betatron accelerator. In this report we will present results from five runs, one in the pulsed mode and four in the static mode. The various parameters of the runs for $\gamma=40$ are listed in Table I and the parameters of the runs for $\gamma=400$ are listed in Table II. Since $\gamma \gg 1$, self and image field have been ignored and therefore the ring current is not a relevant parameter. Also at this high γ the beam minor diameter is expected to be only a few mm.

In the run 267, the pulsed agitator was turned-on after the ring's major radius became 121 cm. Figure 4a shows the radial excursion of a typical electron that was located at $\theta=0$ at the turn-on of agitator. After a single pass through the agitator the electron obtains enough radial excursion to enter the extractor and is extracted. Figure 4b shows that the electron at the disturbance obtains a transverse velocity approximately $2.8 \times 10^{-2} c$. Equation (2) predicts a $\Delta v_r = 2.7 \times 10^{-2} c$. In addition, the numerical results show that the electron gyrates around B_θ with a 1 cm radius, which is also the radius predicted by Eq. (3).

In the run 268, the electron started at $r=110$ cm and was moved radially by the mismatching field. The elapsed time from the minor axis to the agitator is ~ 4.5 μsec , that corresponds to an average radial velocity of $\sim 2.2 \times 10^6$ cm/sec. The amplitude of the slow mode is less than 2 mm. Figure 5a shows the radial excursions of a typical electron in the r, θ plane and Fig. 5b shows a top view of its orbit. The electrons reach the extractor with a vertical displacement from the midplane that is only a few mm. For the reason given in the previous section, the run was terminated after the electron propagated ~ 30 cm inside the extractor.

In the runs 268, 270, and 272 the γ was increased to 400 with a corresponding increase in the value of magnetic fields. Results from run 268 are shown in Fig. 6. Figure 6a shows the radial excursions of the electron and Fig. 6b is a top view of its orbit, when the resonance condition is satisfied at $r=120$ cm. The coherence of the radial excursions is remarkable. We have found that this coherence is preserved even when Eq. (1) is not satisfied exactly, i.e., when the value of B_θ field is off a few percent. In run 270 the value of B_θ was reduced by 2% from its corresponding value in run 268. The results are shown in Fig. 7. Finally, by operating at $l=1$ or $l=2$ instead of at $l=3$, the value of B_θ can be substantially reduced. The results for $l=2$ are shown in Fig. 8.

In conclusion, we have developed a new extraction scheme that is practical and has the potential, since all the electrons of the ring perform coherent motion, to lead to a very high extraction efficiency.

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TABLE I

List of various parameters for the runs shown in Figs. 4 and 5

RUN #	267	266
Agitator's mode	Pulsed	Static
Relativistic factor γ	40	40
Major radius r_0 (cm)	100	100
Vertical field at r_0 (G)	649.9	649.9
Toroidal field at r_0 (G)	-1921	-1971
Field index n	0.5	0.5
Resonance integer l	3	3
Amplitude of mismatching field (G)	---	60
Time constant of mismatching field (μsec)	---	10
Agitator's toroidal position	1.3π	1.26π
Agitator's toroidal width $2\Delta\theta$ (rad)	0.05	0.066
Agitator's inner radius (cm)	120	120
Agitator's outer radius (cm)	122	124
Agitator's opening (cm)	1.0	2
Agitator's linear current density (kA/cm)	0.25	0.375
Agitator's field ΔB_z^a (G)	-300	-450
Extractor's opening toroidal position	0	0
Extractor's minimum inner radius (cm)	121.5	120.5
Extractor's minimum outer radius (cm)	125.5	124.5
Extractor's field ΔB_z^e (G)	-590.0	-590

TABLE II
List of various parameters for the runs shown in Figs. 6, 7, and 8

RUN #	268	270	272
Agitator's mode	Static	Static	Static
Relativistic factor γ	400	400	400
Major radius r_0 (cm)	100	100	100
Vertical field at r_0 (G)	6501	6501	6501
Toroidal field at r_0 (G)	-19710	-19310	-11940
Field index n	0.5	0.5	0.5
Resonance integer l	3	3	2
Amplitude of mismatching field (G)	600	600	600
Time constant of mismatching field (μ sec)	10	10	10
Agitator's toroidal position	1.26π	1.26π	0.94π
Agitator's toroidal width $2\Delta\theta$ (rad)	0.066	0.066	0.066
Agitator's inner radius (cm)	120	120	120
Agitator's outer radius (cm)	124	124	124
Agitator's opening (cm)	2	2.0	2
Agitator's linear current density (kA/cm)	3.75	3.75	3.75
Agitator's field ΔB_z^a (G)	-4500	-4500	-4500
Extractor's opening toroidal position	0	0	0
Extractor's minimum inner radius (cm)	120.5	120.5	120.5
Extractor's minimum outer radius (cm)	124.5	124.5	124.5
Extractor's field ΔB_z^e (G)	-5900	-5900	-5900

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APPENDIX

The Applied Fields

The purpose of this Appendix is to describe the various magnetic fields that were used in the numerical integration of the ring orbits.

Let the global cylindrical coordinates be (r, θ, z) and the global cartesian coordinates be (x, y, z) , so that

$$x = r \cos \theta, \quad (1a)$$

$$y = r \sin \theta. \quad (1b)$$

The two cylindrical components of the applied betatron field, that were used in the code are:

$$B_z = B_{z0} \left(\frac{r_0}{r} \right)^n, \quad (2a)$$

$$B_r = -B_{z0} n \frac{z}{r}, \quad (2b)$$

where r_0 is the major radius and n is the field index.

In addition to the betatron field, a time dependent homogeneous magnetic field, the mismatching field, is applied to shift the electron ring radially outward. The mismatching field is given by

$$B_z^{\text{mis}} = B_{z0}^{\text{mis}} (1 - e^{-t/\tau}), \quad (3)$$

where τ is the time constant.

The applied toroidal magnetic field varies inverse proportionally to the radial distance, i.e.,

$$B_\theta = B_{\theta 0} \frac{r_0}{r}. \quad (4)$$

The extractor consists of two parallel plates with current flowing in opposite directions. These plates have infinite extent in the z and semi-infinite extent in the y -direction. A thin conducting foil completely encloses the extractor at $\theta=0$. The magnetic field inside the extractor is given by

$$B_z^{\text{ext}} = \frac{4\pi}{c} I_1^{\text{ext}}, \quad (4)$$

where I_1^{ext} is the linear current density of the extractor.

Outside the extractor, the linear current density I_1^{ext} does not produce any field. The current of the extractor is adjusted to make the vertical field zero near $\theta=0$.

The agitator field is more complicated. Let the agitator be located symmetrically at some toroidal angle θ_0 , and let (x', y', z) be the local coordinate system of the agitator. Then

$$x' = x \cos \theta_0 + y \sin \theta_0 - r_1, \quad (5a)$$

$$y' = -x \sin \theta_0 + y \cos \theta_0, \quad (5b)$$

where r_1 is the radial distance of the minor axis of the agitator from the origin of the global coordinate system. In addition, let a be the radial width of the agitator, b its toroidal width and h the height of its gap. For simplicity, the toroidal correction will be omitted. In this case, the magnetic field of the agitator is that of a solenoid of rectangular cross section and infinite length minus the contribution of the missing piece of the solenoid of height h , radial length a , width b and linear current density I_1 .

As a representative case, consider the contribution of one section of the missing piece of the solenoid, namely, the one which is perpendicular to the x' -axis and

located at $x'=a/2$ in the local coordinate system of the agitator. The vector potential due to this section is equal to

$$A_{y'} = \frac{I_1}{c} \int_{-b/2}^{b/2} dy'' \int_{-h/2}^{h/2} dz'' \frac{1}{\left[\left(\frac{a}{2} - x' \right)^2 + (y'' - y')^2 + (z'' - z)^2 \right]^{1/2}}, \quad (6)$$

or, after performing the integral with respect to y'' ,

$$A_{y'} = \frac{I_1}{c} \int_{-h/2}^{(h/2)} dz'' \ln \frac{\frac{b}{2} - y' + \left[\left(\frac{a}{2} - x' \right)^2 + \left(\frac{b}{2} - y' \right)^2 + (z'' - z)^2 \right]^{1/2}}{-\left(\frac{b}{2} + y' \right) + \left[\left(\frac{a}{2} - x' \right)^2 + \left(\frac{b}{2} + y' \right)^2 + (z'' - z)^2 \right]^{1/2}} \quad (7)$$

where Gaussian units are being used everywhere. The magnetic field is computed from the expressions

$$B_{x'} = - \frac{\partial A_{y'}}{\partial z}, \quad (8a)$$

$$B_z = \frac{\partial A_{y'}}{\partial x'}. \quad (8b)$$

The $B_{x'}$ - component is easily computed since $A_{y'}$ depends on $z'' - z$, the $\partial/\partial z$ can be replaced by $-\partial/\partial z''$ inside the integral, and the integration with respect to z'' becomes trivial. Therefore, we have

$$B_{x'} = \frac{I_1}{c} \left[\ln \frac{\frac{b}{2} - y' + \left[\left(\frac{a}{2} - x' \right)^2 + \left(\frac{b}{2} - y' \right)^2 + \left(\frac{h}{2} - z \right)^2 \right]^{1/2}}{-\left(\frac{b}{2} + y' \right) + \left[\left(\frac{a}{2} - x' \right)^2 + \left(\frac{b}{2} + y' \right)^2 + \left(\frac{h}{2} - z \right)^2 \right]^{1/2}} \right]$$

$$- \ln \frac{\frac{b}{2} - y' + \left[\left(\frac{a}{2} - x' \right)^2 + \left(\frac{b}{2} - y' \right)^2 + \left(\frac{h}{2} + z \right)^2 \right]^{1/2}}{- \left(\frac{b}{2} + y' \right) + \left[\left(\frac{a}{2} - x' \right)^2 + \left(\frac{b}{2} + y' \right)^2 + \left(\frac{h}{2} + z \right)^2 \right]^{1/2}} \quad (9)$$

In order to write the fields in compact form, we introduce the following functions:

$$h_p = \frac{h}{2} - z \quad , \quad (10a)$$

$$h_m = - \frac{h}{2} - z \quad , \quad (10b)$$

$$f_p^2 = u^2 + v_p^2 \quad , \quad (11a)$$

$$f_m^2 = u^2 + v_m^2 \quad , \quad (11b)$$

$$f_{pp}^2 = f_p^2 + h_p^2 \quad , \quad (12a)$$

$$f_{pm}^2 = f_p^2 + h_m^2 \quad , \quad (12b)$$

$$f_{mp}^2 = f_m^2 + h_p^2 \quad , \quad (12c)$$

$$f_{mm}^2 = f_m^2 + h_m^2 \quad , \quad (12d)$$

$$g_{pp} = v_p + f_{pp} \quad , \quad (13a)$$

$$g_{pm} = v_p + f_{pm} \quad , \quad (13b)$$

$$g_{mp} = v_m + f_{mp} \quad , \quad (13c)$$

$$g_{mm} = v_m + f_{mm} \quad . \quad (13d)$$

where the variables u , v_p , and v_m will be defined later on.

Furthermore, by defining the following two qualities

$$\hat{A}(u, v_p, v_m, z, h) = \ln \left(\frac{g_{pp} g_{mm}}{g_{pm} g_{mp}} \right), \quad (14a)$$

$$\begin{aligned} \hat{B}(u, v_p, v_m, z, h) = \text{sign}(u) * \\ \left\{ \text{sign}(h_p) * \text{Arcsin} \left(\frac{f_p^2 + v_p f_{pp}}{f_p g_{pp}} \right) \right. \\ - \text{sign}(h_p) * \text{Arcsin} \left(\frac{f_m^2 + v_m f_{mp}}{f_m g_{mp}} \right) \\ - \text{sign}(h_m) * \text{Arcsin} \left(\frac{f_p^2 + v_p f_{pm}}{f_p g_{pm}} \right) \\ \left. + \text{sign}(h_m) * \text{Arcsin} \left(\frac{f_m^2 + v_m f_{mm}}{f_m g_{mm}} \right) \right\}, \quad (14b) \end{aligned}$$

the B_x component can be written as

$$B_x(x', y', z) = \frac{I_1}{c} \hat{A} \left(\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right). \quad (15)$$

The B_z component is obtained from Eqs. (8b) and (7) and is equal to

$$\begin{aligned} B_z = - \frac{I_1}{c} \int_{-h/2}^{h/2} dz'' \left[\frac{\frac{a}{2} - x'}{(z''-z)^2 + \left(\frac{a}{2} - x'\right)^2 + \left(\frac{b}{2} - y'\right)^2 + \left(\frac{b}{2} - y'\right)^2 \left[(z''-z)^2 + \left(\frac{a}{2} - x'\right)^2 + \left(\frac{b}{2} - y'\right)^2 \right]^{1/2}} \right. \\ \left. - \frac{\frac{a}{2} - x'}{(z''-z)^2 + \left(\frac{a}{2} - x'\right)^2 + \left(\frac{b}{2} + y'\right)^2 + \left(\frac{b}{2} + y'\right)^2 \left[(z''-z)^2 + \left(\frac{a}{2} - x'\right)^2 + \left(\frac{b}{2} + y'\right)^2 \right]^{1/2}} \right] \quad (16) \end{aligned}$$

These are integrable functions and the B_z component can be expressed in terms of $\hat{B}$ as follows:

$$B_z(x', y', z) = \frac{I_1}{c} \hat{B} \left(\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) . \quad (17)$$

In a similar fashion, the contribution of the other three sections can be computed and the total contribution of all four sections of the missing piece is:

$$B_{x'}(x', y', z) = \frac{I_1}{c} \left[\hat{A} \left(\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) - \hat{A} \left(-\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) \right], \quad (18a)$$

$$B_{y'}(x', y', z) = \frac{I_1}{c} \left[\hat{A} \left(\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) - \hat{A} \left(-\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) \right], \quad (18b)$$

$$B_z(x', y', z) = \frac{I_1}{c} \left[\hat{B} \left(\frac{a}{2} - x', \frac{b}{2} - y', \frac{b}{2} - y', z, h \right) - \hat{B} \left(-\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) + \hat{B} \left(\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) - \hat{B} \left(-\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) \right]. \quad (18c)$$

As mentioned above, these fields should be subtracted from the magnetic field of the solenoid, which is equal to

$$B_z = \begin{cases} \frac{4\pi}{c} I_1 & \text{inside the solenoid} \\ 0 & \text{outside the solenoid.} \end{cases} \quad (19)$$

In the order to make the fields drop sharper in the radial direction, two rectangular loops at $z = h/2$ and $z = -h/2$ were added to the agitator, to compensate for the missing current of the gap. The radial and the toroidal width of the loops were the same as those of the rectangular solenoid, while the current in each loop was chosen equal to

$$I_w = - \frac{I_1 h}{2} \quad (20)$$

The computation of the magnetic fields of these two loops is straight forward.

It is convenient to define the following two functions:

$$\begin{aligned} \hat{A}_w(u, v_p, v_m, z, h) &= \\ &= h_p \left(\frac{1}{f_{pp} g_{pp}} - \frac{1}{f_{mp} g_{mp}} \right) \\ &- h_m \left(\frac{1}{f_{pm} g_{pm}} - \frac{1}{f_{mm} g_{mm}} \right) \end{aligned} \quad (21a)$$

$$\begin{aligned} \hat{B}_w(u, v_p, v_m, z, h) &= \\ &= -u \left(\frac{1}{f_{pp} g_{pp}} - \frac{1}{f_{mp} g_{mp}} + \frac{1}{f_{pm} g_{pm}} - \frac{1}{f_{mm} g_{mm}} \right) \end{aligned} \quad (21b)$$

where all quantities have already been defined in Eqs. (10) - (13). Then the magnetic field components of both loops are:

$$B_{x'}^{(w)}(x', y', z) = \frac{I_w}{c} \left[\hat{A}_w \left(\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) - \hat{A}_w \left(-\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) \right] \quad (22a)$$

$$B_{y'}^{(w)}(x', y', z) = \frac{I_w}{c} \left[\hat{A}_w \left(\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) - \hat{A}_w \left(-\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) \right], \quad (22b)$$

$$B_z^{(w)}(x', y', z) = \frac{I_w}{c} \left[\hat{B}_w \left(\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) - \hat{B}_w \left(-\frac{a}{2} - x', \frac{b}{2} - y', -\frac{b}{2} - y', z, h \right) + \hat{B}_w \left(\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) - \hat{B}_w \left(-\frac{b}{2} - y', \frac{a}{2} - x', -\frac{a}{2} - x', z, h \right) \right]. \quad (22c)$$

These components are easily transformed from the local coordinate system of the agitator to the global coordinate system.

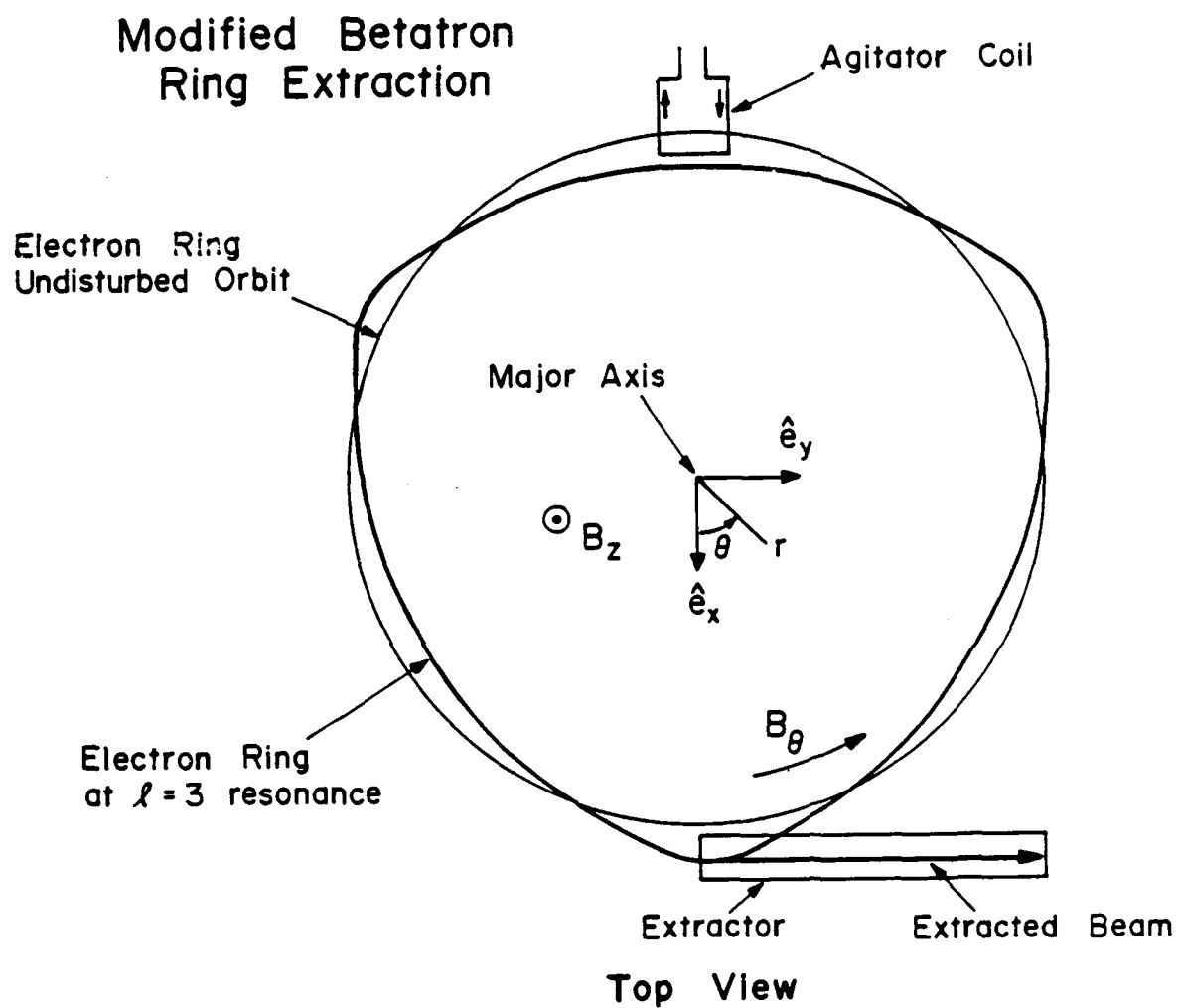
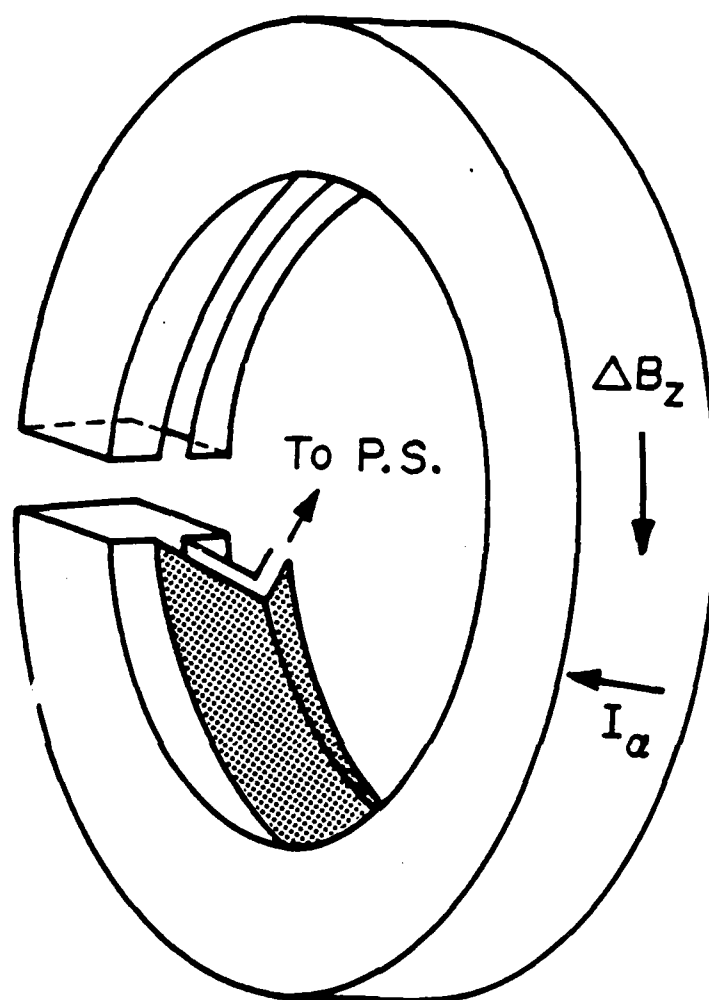


Fig. 1. Schematic of the proposed extraction scheme.



Agitator Coil

Fig. 2. Agitator coil that generates the localized disturbance.
It is powered by a coaxial transmission line.

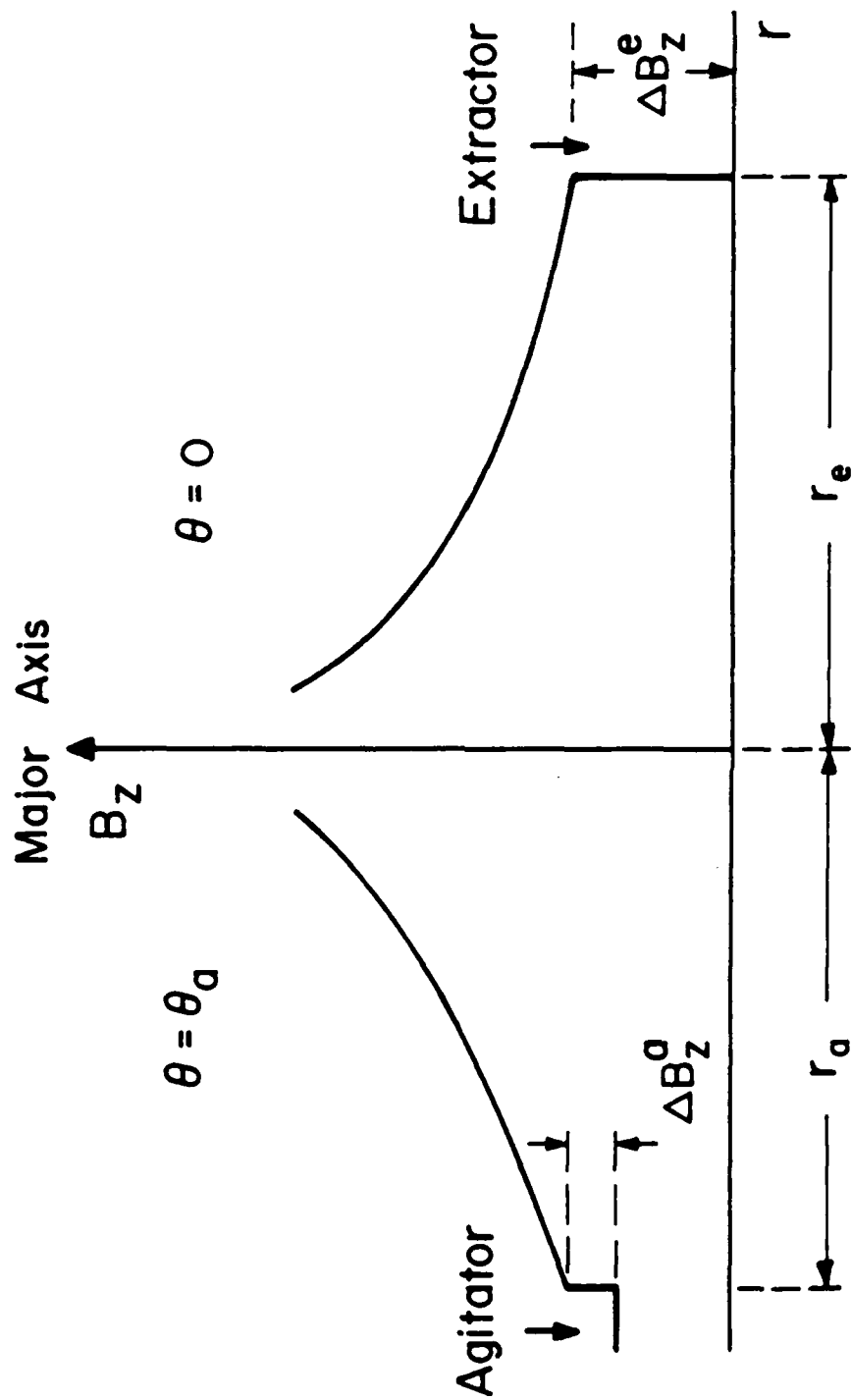


Fig. 3. Radial profile of the vertical magnetic field.

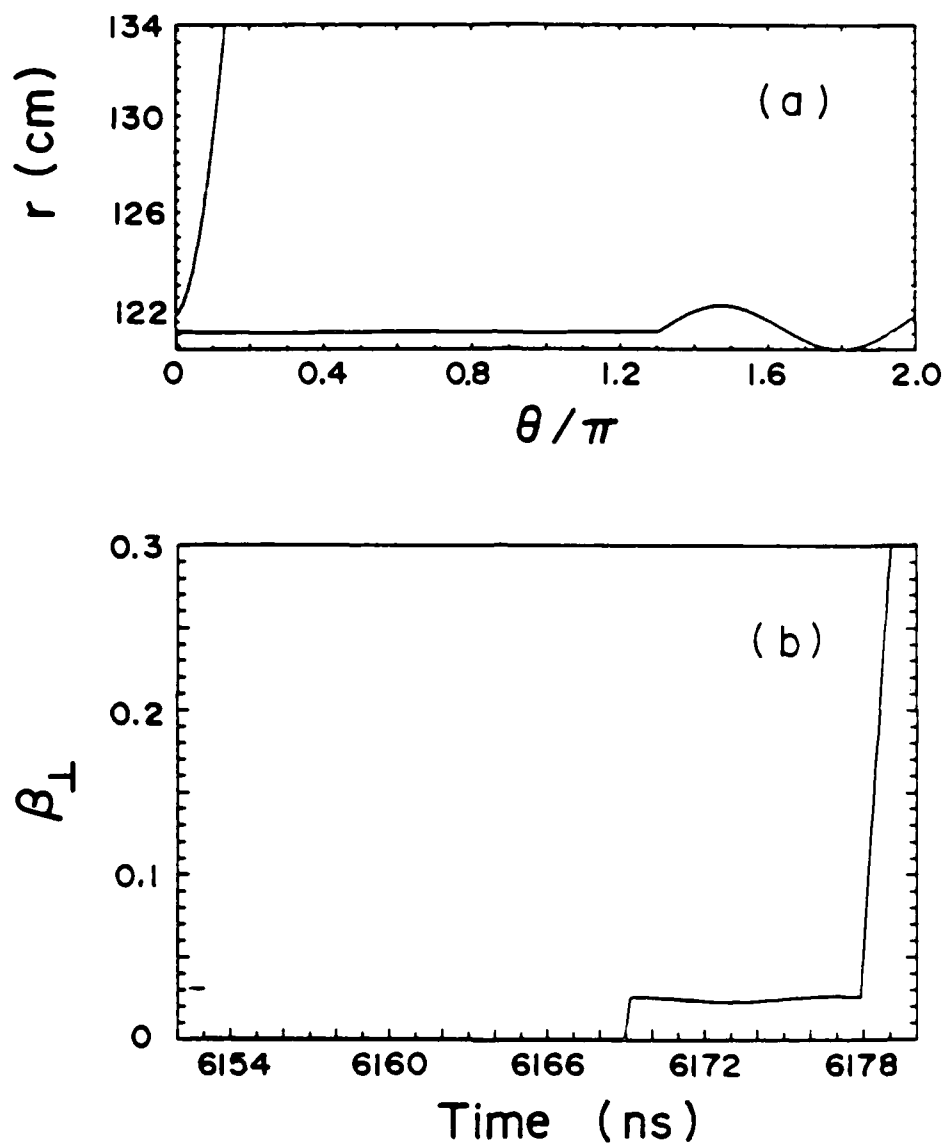


Fig. 4. Radial excursions of a typical electron (1) and its corresponding normalized transverse velocity (b) for the run 267.

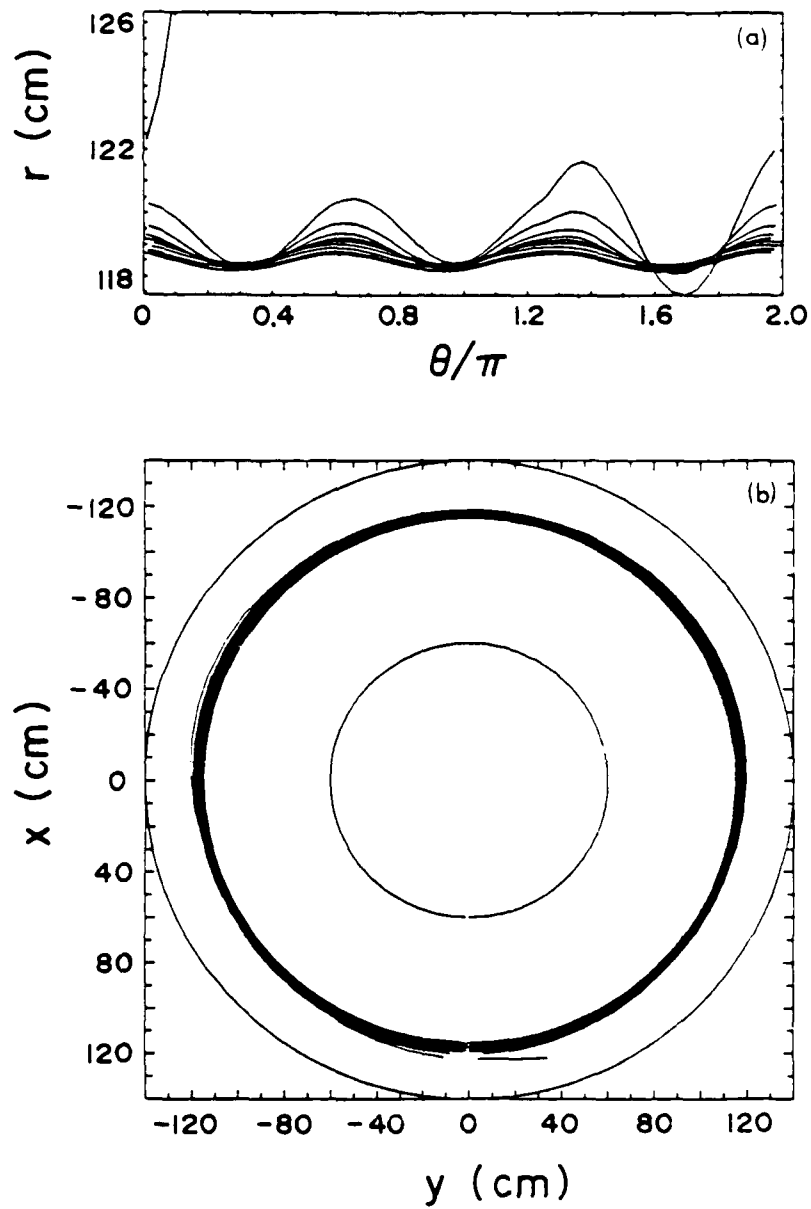


Fig. 5. Radial excursions of a typical electron (a) and top view of its trajectory in the x, y plane for the run 266.

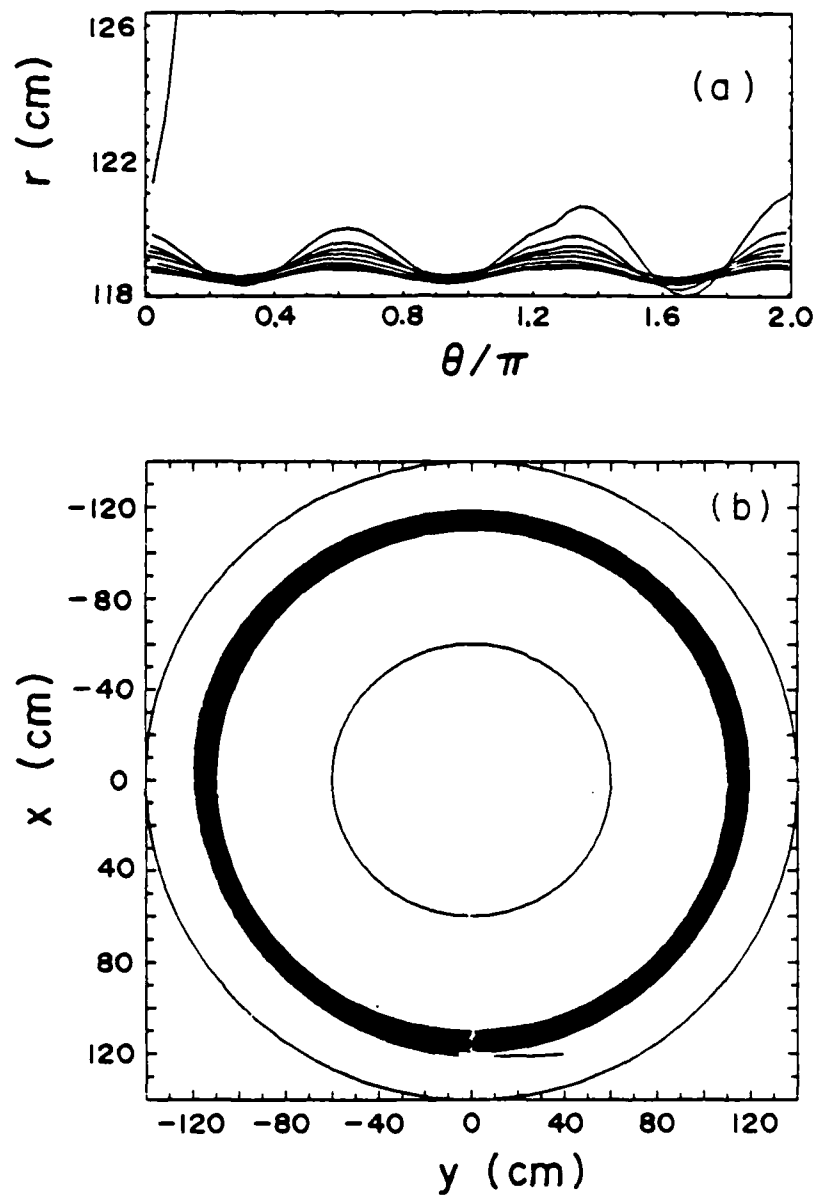


Fig. 6. Radial excursion of a typical electron (a) and top view of its trajectory in the x, y plane for the run 268.

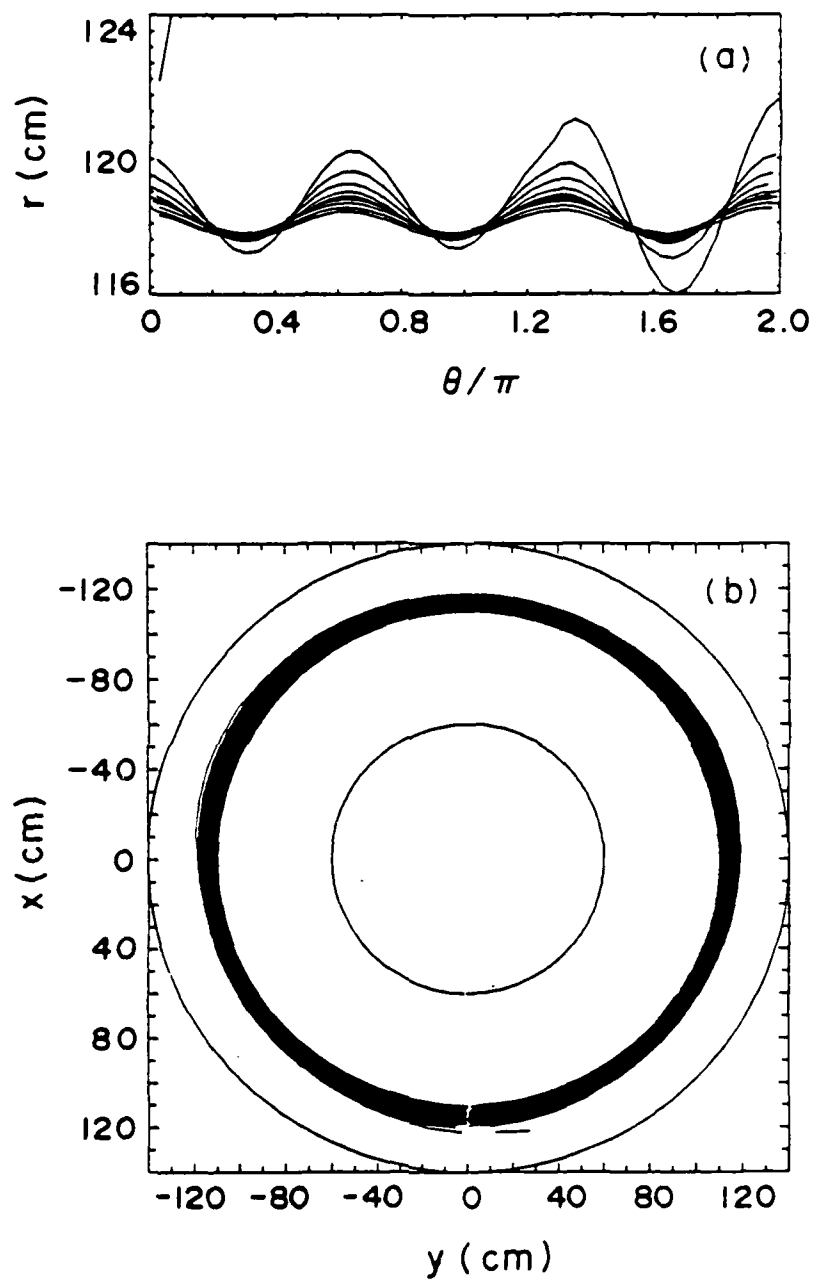


Fig. 7. Radial excursion of a typical electron (a) and top view of its trajectory in the x, y plane for the run 270.

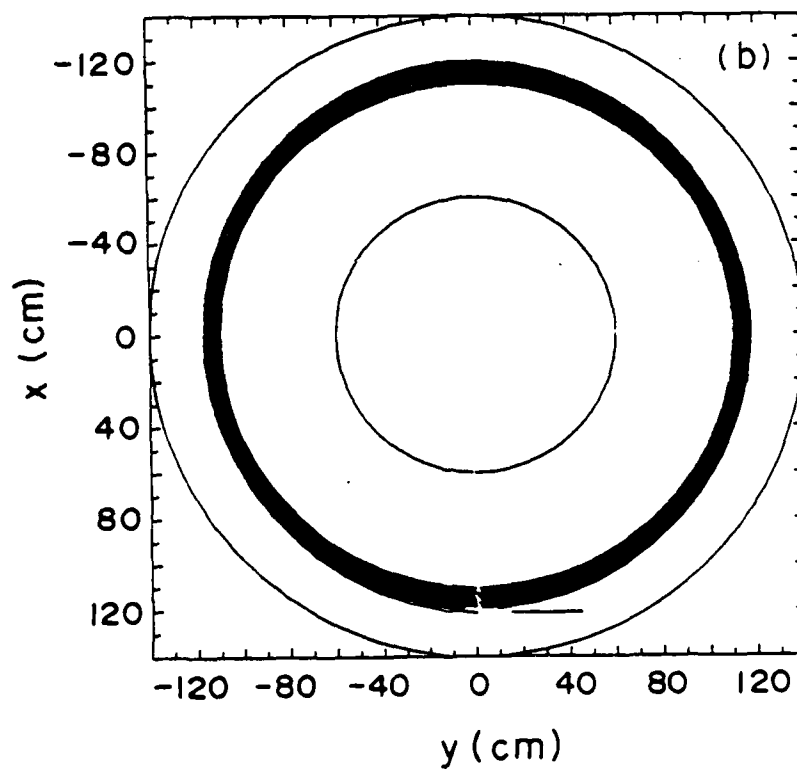
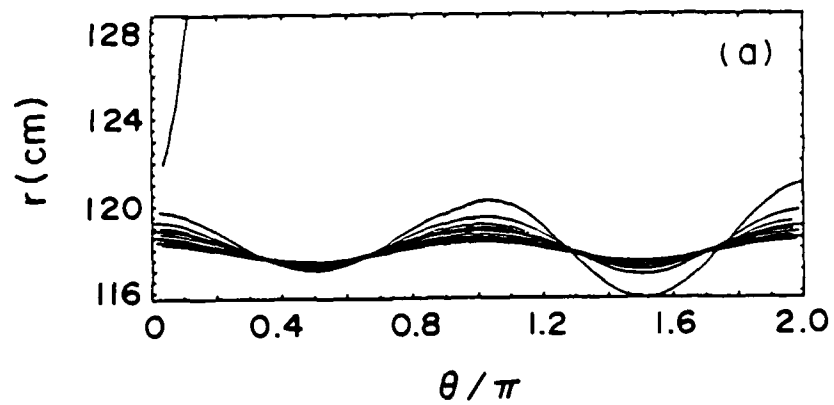


Fig. 8. Radial excursion of a typical electron (a) and top view of its trajectory in the x, y plane for the run 272.

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