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**FINAL TECHNICAL REPORT
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**True Asymptotic Plasma - Sheath Matching with an
Asymptotically Correct Collisional Presheath**

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TABLE OF CONTENTS

INTRODUCTION	p.
BASIC THEMIONIC CONVERTOR THEORY	p.
ASYMPTOTIC SHEATH THEORY.....	p.
TEC PROGRAM RESULTS.....	p.
PAPERS AND PUBLICATIONS	p.
APPENDIX A - Fokker Planck Collisions Presheath.....	p.
APPENDIX B - The TEC program	p.

INTRODUCTION

The work under this grant on plasma presheaths, which form a transition region between the collisionless electrode sheaths and the plasma, is directed toward the problems of the Thermionic Energy Converter (TEC). Figure 1 shows a schematic of a TEC in a reactor core for space power applications and the basic physics. Cesium is put the gap between the emitter and collector for two purposes: first, to ionize and neutralize the space charge so that a useful electron current density can pass (10 - 100 amps/square cm), and second to reduce the electrode work functions by adsorption of cesium. Of the plasma physics of the the cesium filled gap of the TEC, the plasma-electrode interactions are the most significant part because these regions form boundary conditions which control the plasma density and temperatures of the entire gap. Thus the research under this grant has been directed toward the study of collisional presheaths which form the layer adjacent to an electrode on the order of one ion mean free path thick. However, the research pursued under this grant is not limited in applicabilty to TECs but is of interest to plasma-surface interactions in general. Other applications include electric propulsion where electrode erosion is a problem and not fully understood and more generally any plasma-surface interaction.

This report includes the asymptotic presheath theory developed, and is preceded by the basic theory of the Thermionic Energy Converter (TEC) and is followed by the application of the theory to a time dependent model of the TEC in the program called TEC. As shown in the TEC results, the agreement with experiment is good except in the low current regime of the TEC where an unexplained disagreement remains. This is still a puzzle.

BASIC TEC THEORY

The basic theory of the TEC is set forth in the following paper published under this grant.

Effects of Emitter Sheath Ion Reflection and Trapped Ions on Thermionic Converter Performance Using an Isothermal Electron Model

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Effects of Emitter Sheath Ion Reflection and Trapped Ions on Thermionic Converter Performance Using an Isothermal Electron Model

GEOFFREY L. MAIN AND S. H. LAM

Abstract—This paper couples exact collisionless sheath calculations to an isothermal electron model of a thermionic converter. The emitter sheath structure takes into account reflected ions, trapped ions, and surface emission ions. It is shown that lessening the net loss of ions at the emitter in the ignited mode by these phenomena degrades performance. In addition, it is shown that when the emitter returns too many of the ions, the arc is extinguished because there is insufficient resistive heating to maintain the necessary plasma electron temperature for ionization. These results suggest that the ignited mode cannot be improved much. However, nonignited modes in which the electron temperature remains low, such as the pulsed mode, do not suffer from this adverse behavior.

I. INTRODUCTION

EMITTER sheath phenomena are important in thermionic energy converters because the emitter sheath forms the emitter boundary condition for the plasma in the gap by controlling both the ion loss rate and the loss rate of hot (3000 K) plasma electrons to the emitter. This paper examines two expected emitter sheath phenomena and their effects on converter performance: reflection of ions coming from the plasma by a double emitter sheath, and ions trapped in the double emitter sheath. The authors have previously suggested that ion reflection might improve thermionic energy converter performance [1] and have subsequently shown that ion reflection at the emitter is likely to degrade the performance in the ignited mode and, in addition, that trapped ions in a double emitter sheath are also likely to degrade performance in the ignited mode [2]. Lundgren [3], [4] has also shown this with simplified ion and electron dynamics. In the present paper the effects of emitter ion reflection and ion trapping in the ignited mode are calculated using exact electron and ion dynamics in the collisionless (except for ion trapping) sheaths. The electrons entering the sheaths from the plasma are assumed to have a Maxwellian distribution, but no assumptions are made about the returning electrons, and the electron density in the sheath is calculated exactly. The ions entering the sheaths from the plasma are

not assumed cold, but are given the correct ion temperature and shifted in velocity according to a generalization of the Bohm criterion [5], [6].

Both ion reflection and trapped ions in the emitter sheath reduce the normalized (by plasma density) net ion loss rate to the emitter. Also, both of these phenomena raise the normalized plasma density adjacent to the emitter. The higher plasma density at the emitter causes a greater increase in the loss of hot plasma electron energy to the emitter than the corresponding decrease in the loss of ionization energy (carried by the ions) to the emitter. Therefore, these emitter sheath phenomena increase arc-drop. Within the limitations of the present isothermal thermionic converter formulation, all three of these phenomena (which become significant at low currents) steepen the current-voltage characteristic. At low current densities, the present theory shows that the collector sheath height decreases, resulting in a larger electron diffusion velocity than can be justified for the continuum model used in the plasma region. The result of lower performance at lower current is in agreement with experimental studies. At some current density which depends strongly on the emitter sheath conditions, the ignited mode is no longer self-sustaining and the arc is extinguished.

Fig. 1 is a schematic diagram of the cesium diode converter. The emitter is heated externally to temperature T_A which is typically 1750 K or higher, and the collector is cooled to temperature T_C which is typically 900–1100 K. The gap space d , or converter length, which is typically 0.25 mm, separates the emitter from the collector. The cesium reservoir, which is sometimes imbedded in the collector, is kept at temperature T_R to maintain the desired cesium pressure (typically 1 to 2 torr) in the gap. The electrical load is connected across the emitter and collector to produce power.

II. THE ISOTHERMAL ELECTRON FORMULATION

In this section the isothermal thermionic converter formulation is developed. The formulation is similar to that of Lam [7] but is generalized to eliminate the assumption of high sheaths which has previously been used to simplify the electron dynamics. Since both low-emitter and low-collector sheath heights are encountered as a consequence of ion reflection and trapped ions, the assumption

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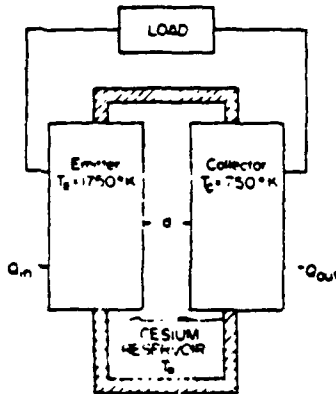


Fig. 1. The cesium diode converter.

of Boltzmann plasma electron distributions at the plasma-sheath interface must be abandoned. At both the emitter and collector, the low sheaths return few plasma electrons, leaving the distributions largely one sided. Furthermore, at the emitter sheath emitted electrons must be taken into account. Thus the ratio of electrons moving toward the sheath to the total density of electrons at the sheath edge is not $1/2$, as in the Boltzmann assumption.

In Fig. 2 we define the potentials in the converter. All of the potentials are nondimensionalized by emitter temperature as follows:

$$\chi = \frac{q\phi}{kT_E} \quad (1)$$

where

- χ nondimensional potential.
- ϕ potential.
- q electron charge.
- k Boltzmann constant, and
- T_E emitter temperature.

We also use the following terminology for various potentials in the converter:

- ϕ_E emitter work function.
- $\Delta\chi$ back sheath height.
- $\Delta\chi_r$ reflective potential.
- χ_E emitter sheath height.
- $\Delta\chi_p$ plasma potential drop.
- V_d arc-drop.
- χ_C collector sheath height.
- ϕ_C collector work function, and
- V_{out} converter output voltage.

Inspection of Fig. 2 immediately yields the following relations:

$$V_d = V_{out} - (\phi_E - \phi_C) - \Delta\chi \quad (2)$$

$$V_d = (\chi_C - \chi_E) - \Delta\chi_p. \quad (3)$$

The Richardson current density of electrons from the emitter is

$$J_R \left(\frac{A}{cm^2} \right) = 120 T_E^2 (K^2) \exp(-\phi_E). \quad (4)$$

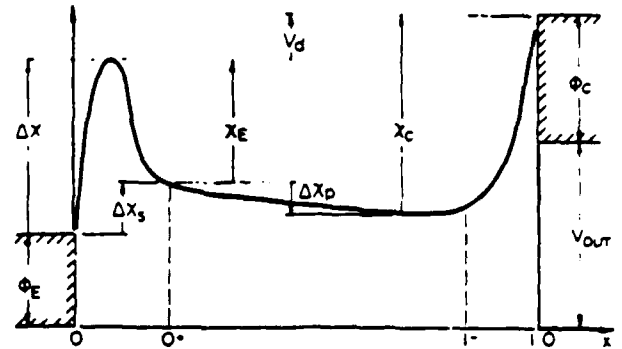


Fig. 2. The potential distribution in the converter.

The emitted current density which crosses the emitter sheath potential peak into the converter plasma region is

$$J_E = J_R \exp(-\Delta\chi), \quad \Delta\chi > 0$$

$$J_E = J_R, \quad \Delta\chi \leq 0. \quad (5)$$

We also define the net current density through the converter J and the normalized current density

$$j = \frac{J}{J_E}. \quad (6)$$

We have assumed for convenience that the ion contribution to net current is negligible because the cesium-ion-to-electron-mass ratio is enormous. Ions will typically contribute no more than 1 percent of the net current. Electron temperature is nondimensionalized as

$$\tau = \frac{T_e}{T_E} \quad (7)$$

where T_e is the plasma electron temperature which, in this section, is constant by the isothermal assumption. Finally, we have the thermal speeds:

$$a_e = \sqrt{\frac{8kT_e}{\pi m}} \quad (8)$$

$$a_E = \sqrt{\frac{8kT_E}{\pi m}}. \quad (9)$$

The isothermal formulation is developed from here in the same way as the general formulation except that we take full advantage of the isothermal assumption by looking only at the global conservation equations instead of the local ones used in the general formulation. We then assume that the transport properties, collision frequencies, and the ionization source coefficient are constant across the converter because of the isothermal assumption. Also, we find only the steady-state solution. We carry out this development by deriving the global conservation equations for the isothermal case (current, momentum, and electron energy) and then reducing these to a set of three simultaneous equations in the variables τ , χ_E , and χ_C . In some cases the actual calculations are carried out

using different variables when χ_E or χ_C are small or zero. In the case, for instance, of a single ion-repelling emitter sheath we use j because χ_E is zero. These equations are nonlinear and solved numerically using a positive definite Newton's method.

First, we consider conservation of current. The collector is assumed to emit nothing; therefore, at the plasma-collector sheath interface we have

$$J = \frac{a_r \alpha_1 n(1)}{2} e^{-\chi_C/\tau} \quad (10)$$

where α_1 is the fraction of the total plasma density at the collector sheath which is moving toward the collector and $n(1)$ is the total plasma density at the plasma-collector sheath interface. Because we continue to assume that the part of the plasma electron distribution coming into the collector sheath is Maxwellian, we can write α_1 as

$$\alpha_1 = \frac{1}{1 + \frac{2}{\sqrt{\pi}} \int_0^{\chi_C/\tau} e^{-u^2} du} \quad (11)$$

which takes into account the plasma electrons reflected by the collector sheath. We still assume that the plasma electron distribution coming into the collector sheath is Maxwellian and that it does not have any velocity shift because the sheath is expected to be electron repelling. In the limit of a high collector sheath, $\alpha_1 = 1/2$ and we have a fully Boltzmann distribution of electrons at the collector sheath edge. The situation at the emitter is more complex because the emitted electrons must be taken into account. We have the backscattered current density J_{BS} which is the plasma electron current density moving into the emitter:

$$J_{BS} = \frac{n(0)a_r\alpha_0}{2} \exp\left(-\frac{\chi_E}{\tau}\right) \quad (12)$$

where $n(0)$ is the total plasma density at the emitter sheath-plasma interface and α_0 is the fraction of total plasma density at the interface moving toward the emitter.

Continuity of electron current demands

$$J_E = J_{BS} + J \quad (13)$$

which can be written as

$$J_E = J \left(1 + \frac{n(0)\alpha_0}{n(1)\alpha_1} \exp\left(\frac{\chi_C - \chi_E}{\tau}\right) \right) \quad (14)$$

This can be rewritten using (3) and (6) as

$$j = \frac{1}{1 + \frac{n(0)\alpha_0}{n(1)\alpha_1} \exp\left(\frac{V_d + \Delta\chi_r}{\tau}\right)} \quad (15)$$

The quantity α_0 can be written as

$$\alpha_0 = \sqrt{\frac{\pi}{2}} Q \left(\frac{1}{j} - 1 \right) \exp\left(\frac{\chi_E}{\tau}\right) \quad (16)$$

where

$$Q = \frac{(u_r)_0}{\sqrt{\frac{kT_e}{m}}}$$

is the electron Mach number at the emitter. This is just an application of (13).

Electron energy conservation is developed by considering energy exchange with the emitter and collector and energy lost to ionization. Power carried into the plasma by emitted electrons is

$$P_E = J_E (2 + \Phi_E + \Delta\chi) \frac{kT_e}{q} \quad (17)$$

Power returned to the emitter is

$$P_{BS} = (J_E - J)(2\tau + \Phi_E + \Delta\chi) \frac{kT_e}{q} \quad (18)$$

Power flowing into the collector is

$$P_C = J(2\tau + \Phi_E + V_d + \Delta\chi) \frac{kT_e}{q} \quad (19)$$

Ionization power loss is

$$P_{un} = J_{un} V_{fi} \frac{kT_e}{q} \quad (20)$$

where J_{un} is the total ion current into both the emitter and collector, and V_{fi} is the first ionization energy. Conservation of electron energy is

$$P_E = P_{BS} + P_C + P_{un} \quad (21)$$

which can be reduced to

$$\tau = 1 - \frac{1}{2} j V_d - \frac{1}{2} j_i V_{fi} \quad (22)$$

where $j_i = J_{un}/J_E$. In the ignited mode τ is generally about 2 ($T_e = 1750$ K and $T_r = 3000$ K), consequently the arc-drop V_d is negative. In other words, the high plasma electron temperature is generated by resistance heating.

Finally, we consider electron and ion momentum. From electron momentum conservation, we find the potential drop in the plasma region. By adding the electron and ion momentum equations as in the general case, we find our diffusion equation and boundary conditions to which the sheaths contribute flux terms. When we introduce the ionization source term into this, we have the complete formulation. Electron momentum conservation is

$$0 = -\frac{dp_e}{dx} - qn \frac{d\psi}{dx} - \frac{a_r m n u_r}{\lambda_r} \quad (23)$$

where λ_r is electron mean-free path. Using $p_e = nkT_e$ and $J = qn u_r$, we can rearrange (23) into

$$J = -\frac{q\lambda_r}{ma_r} \left(kT_e \frac{dn}{dx} + nq \frac{d\psi}{dx} \right) \quad (24)$$

This can be further reduced by dividing by J_e and using $\xi = x/d$ where d is the converter gap thickness:

$$j = -\frac{\pi \lambda_e}{4 d} \frac{1}{\sqrt{\tau} n_e} \left(\tau \frac{dn}{d\xi} + n \frac{d\tau}{d\xi} \right). \quad (25)$$

Integration of this equation from the emitter sheath interface to the collector sheath interface yields

$$\Delta \lambda_e = \tau \ln \left(\frac{n(1)}{n(0)} \right) + jR \quad (26)$$

where

$$R = \frac{4}{\pi} \frac{d}{\lambda_e} \sqrt{\tau} \int_0^1 \frac{n_e}{n(\xi)} d\xi. \quad (27)$$

The quantity R is the normalized plasma resistance.

The ion and electron momentum equations can be written

$$kT_e \frac{dn}{dx} = -qn \frac{d\psi}{dx} - \frac{mnu_e a_e}{\lambda_e} \quad (28a)$$

$$kT_i \frac{dn}{dx} = qn \frac{d\psi}{dx} - \frac{Mnu_i a_i}{\lambda_i} \quad (28b)$$

where λ_i is ion mean-free path and a_i is ion thermal speed:

$$a_i = \sqrt{\frac{8kT_i}{\pi M}}.$$

Addition of (28a) and (28b) yields

$$(kT_e + kT_i) \frac{dn}{dx} = - \left(\frac{a_e m}{\lambda_e} n_e + \frac{a_i M}{\lambda_i} n_i \right) n \quad (29)$$

which is ambipolar diffusion. Equation (29) is differentiated to become

$$(kT_e + kT_i) \frac{d^2 n}{dx^2} + \frac{a_e m}{\lambda_e} \frac{d}{dx} (nu_e) + \frac{a_i M}{\lambda_i} \frac{d}{dx} (nu_i) = 0. \quad (30)$$

We assume recombination is negligible and the ionization source term is

$$\frac{d}{dx} (u, n) = \frac{d}{dx} (u, n) = Sn. \quad (31)$$

Using (31) in (30) yields

$$\frac{d^2 n}{d\xi^2} + \left(\frac{a_e m}{\lambda_e} + \frac{a_i M}{\lambda_i} \right) S d^2 \left| n = 0. \quad (32) \right.$$

Equation (29) taken at the boundaries of the plasma (at the emitter and collector sheath interfaces) forms the plasma boundary conditions

$$\left(\frac{dn}{d\xi} \right)_0 = \beta_0 n_0$$

$$\left(\frac{dn}{d\xi} \right)_1 = \beta_1 n_1 \quad (33)$$

where

$$\beta_0 = \frac{-d}{kT_e + kT_i} \left(\frac{a_e m}{\lambda_e} u_{e0} + \frac{a_i M}{\lambda_i} u_{i0} \right)$$

$$\beta_1 = \frac{d}{kT_e + kT_i} \left(\frac{a_e m}{\lambda_e} u_{e1} + \frac{a_i M}{\lambda_i} u_{i1} \right). \quad (34)$$

Equation (32) is written as

$$\frac{d^2 n}{d\xi^2} + A^2(\tau) n = 0 \quad (35)$$

where

$$A^2(\tau) = d^2 S \left(\frac{a_e m}{\lambda_e} + \frac{a_i M}{\lambda_i} \right) \quad (36)$$

where $A(\tau)$ is the ionization coefficient and is found from consideration of ionization kinetics of the cesium according to Lawless [8]. Its solution for n is

$$n(\xi) = B \sin(A\xi + C) \quad (37)$$

where B and C are constants of integration and $A = A(\tau)$. The quantities β_0 and β_1 , which are the boundary conditions for (37), can be written as functions of τ , χ_e , χ_i , and $\Delta \chi_i$:

$$\beta_0 = \beta_0(\tau, \chi_e, \chi_i, \Delta \chi_i)$$

$$\beta_1 = \beta_1(\tau, \chi_e, \chi_i, \Delta \chi_i). \quad (38)$$

When there is no reflection, β_0 and β_1 are both large, i.e.:

$$\beta_0 = O\left(\frac{d}{\lambda_i}\right), \quad \beta_1 = O\left(\frac{d}{\lambda_i}\right).$$

Significant reflection on the emitter side reduces β_0 and it may indeed attain negative values for sufficiently strong reflection.

The density equation (35) with the boundary conditions β_0 and β_1 is a linear eigenvalue problem; its solution yields A and C as functions of β_0 and β_1 . The calculated results are shown in Fig. 3. Since $A(\tau)$ is a function of τ from the ionization kinetics, the value of τ is thus determined by a function of β_0 and β_1 . The plasma resistance R also can be expressed in terms of functions of β_0 and β_1 through A and C using (27):

$$R = \frac{4}{\sqrt{2\pi}} \frac{d}{\lambda_i} \tau \frac{\sin C}{A} \ln \left(\frac{\tan \left(\frac{A+C}{2} \right)}{\tan \left(\frac{C}{2} \right)} \right). \quad (39)$$

The sheath results which provide j , Q , β_0 , and β_1 , complete the isothermal formulation. The sheath theory used is an exact solution to the Poisson equation and collisionless Boltzmann equation for warm plasma ion distribution with a 10 percent of Bohm speed cutoff velocity to approximate the effect of the collisional presheath [6]. The results are summarized below. The quantities β_0 , β_1 , Q ,

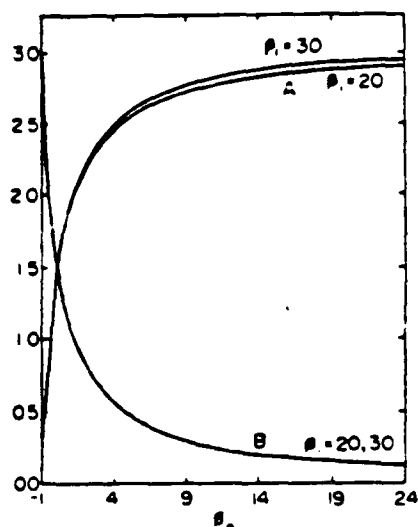


Fig. 3. The eigenvalue problem.

and j are found from the sheath calculations as functions of τ , χ_F , χ_C , and $\Delta\chi$, i.e.:

$$\beta_0 = \beta_0(\tau, \chi_F, \chi_C, \Delta\chi)$$

$$\beta_1 = \beta_1(\tau, \chi_F, \chi_C, \Delta\chi)$$

$$Q = Q(\tau, \chi_F, \chi_C, \Delta\chi)$$

$$j = j(\tau, \chi_F, \chi_C, \Delta\chi).$$

From the eigenvalue problem for the plasma density we then find

$$A(\tau) = A(\beta_0, \beta_1). \quad (40)$$

From the continuity equation for current we find

$$\chi_C - \chi_F = \tau \ln \left(\frac{\sin(A + C)}{\sin(C)} \right) + \tau \ln \frac{\alpha_1}{\alpha_0} + \tau \ln \left(\frac{1}{j} - 1 \right) \quad (41)$$

and from the electron momentum equation we find

$$\chi_C - \chi_F = \tau \ln \left(\frac{\sin(A + C)}{\sin(C)} \right) + jR + \frac{2(\tau - 1)}{j} - \frac{j}{j} V_R. \quad (42)$$

These three previous equations determine χ_F , χ_C , and τ when $\Delta\chi$ is given. This set of equations is valid for all $\Delta\chi$. Even in the case of $\Delta\chi \leq 0$ when there is no reflection, the calculations differ from previous isothermal calculations because the Boltzmann assumption on the electrons is not used as indicated by the presence of α_0 and α_1 .

III. CALCULATED RESULTS FOR ION REFLECTION AND TRAPPED IONS

In this section we develop isothermal solutions for the thermionic converter with the emitter sheath phenomena

TABLE I
ISOTHERMAL SOLUTION CONDITIONS

CASE 1	CASE 2
$T_C = 1750$ K	$T_E = 1750$ K
$T_C = 750$ K	$T_C = 750$ K
$p_{cs} = 1$ torr	$p_{cs} = 1$ torr
$d = 10$ mil	$d = 10$ mil
$\phi_E = 2.12$ eV	$\phi_E = 2.67$ eV
$\phi_C = 1.60$ eV	$\phi_C = 1.60$ eV
$J_R = 20$ amp/cm ²	$J_R = 7.57$ amp/cm ²
$J_{\text{loss}} = 1.80 \times 10^{-3}$ amp/cm ²	$J_{\text{loss}} = 2.10 \times 10^{-3}$ amp/cm ²

of ion reflection, trapped ions, and surface emission ions included. Emitter sheath effects on thermionic converter performance can be divided into two categories: 1) changes in net ion flux rate into the sheath which affect plasma density directly; and 2) changes in sheath potential distribution which affect the exchange of "hot" plasma electrons for "cold" emitter ions directly. A decreased influx of ions into the sheath, which occurs for all three emitter sheath phenomena, increases the plasma density at the neutral plasma emitter sheath interface. Theoretical intuition suggests that an increased plasma density at the emitter would benefit performance by reducing resistance through the plasma and therefore reducing arc-drop. However, this is not the case. While the plasma density at the emitter increases slightly, plasma density at the collector decreases. Consequently, total resistance increases.

All three of these phenomena increase in significance as net current density through the converter is reduced. Each of these reduces the net ion loss rate to the emitter and consequently increases arc-drop (therefore, degrading performance at low current densities). This increase in arc-drop is in agreement with the same tendency in the experimental results. However, the experimental results also show a plateau (of low arc-drop) at low current density. This plateau occurs at a current density corresponding to significant surface ion emission and is therefore thought to occur as surface emission replaces volume ionization as the dominant source of plasma ions. Unfortunately, the theoretical calculations cannot be carried into this region because the collisionless collector sheath matching (to the neutral plasma) fails.

To provide a realistic framework for presenting the results, we consider the converter conditions shown as case 1 in Table I. Case 2 is shown because it has the largest surface emission of any typical thermionic converter operating condition (because the work function is high and the temperature is also high). Instead of presenting case 2 separately, we demonstrate the effects of surface emis-

sion in case 1 by increasing the surface emission by a factor of 100 thereby bringing it up to the level in case 2. The net current density at which surface emission becomes significant can be estimated by multiplying J_{R1} by the square root of the ion to electron mass ratio (approximately 500). In case 1, this means that surface emission becomes significant at $J = 0.01 \text{ A/cm}^2$ while in case 2 significant surface emission begins at $J = 1.0 \text{ A/cm}^2$.

IV. EFFECTS OF ION REFLECTION

In this section we discuss the isothermal results for case 1 with ion reflection, but without trapped ions and with the small amount of surface emission ions of case 1. Fig. 4 is the CV diagram for this case.

The dotted line extending upward from point A is the single electron-repelling emitter sheath solution. However, we have not taken recombination or the Schottky effect into account in this isothermal formulation which are expected to become important at current densities near J_R . The interest of this paper begins at point A, where the single sheath doubles over. Between points A and B, where the back sheath height $\Delta\chi$ is less than the sheath height χ_E , the emitter sheath is nonreflecting. In this region the sheath heights χ_E and χ_C remain constant while the plasma density is proportional to net current J (the normalized plasma density nc/J is constant). Only the back sheath height $\Delta\chi$ changes and the CV curve in this region is Boltzmann (the arc-drop is constant). Beginning at point B and continuing to point C, the double emitter sheath reflects plasma ions because the back sheath is larger than the front sheath; in other words, the reflective potential $\Delta\chi_r = \Delta\chi - \chi_E$ is positive. The result is that net ion loss rate into the sheath $\bar{u}$ decreases and that arc-drop increases. The quantity $\bar{u}$ is defined as the mean ion velocity into the sheath normalized by the Bohm speed, $\sqrt{kT_e/M}$. The dotted curve BD is the same double sheath except that it assumes no ions are reflected; therefore, $\bar{u}$ is constant and arc-drop is constant. The two curves BC and BD are almost indistinguishable because the increase in arc-drop is small until the net current density is extremely small. The reason for this is that the shift speed is approximately $u_s = 2$, and, therefore, a large increase in reflective potential is required to change $\bar{u}$ significantly (the half-reflection point is $\Delta\chi_r = 4.0$ or approximately $J = J_R \exp(-4) = 0.4 \text{ A/cm}^2$). The shift speed u_s is defined as the velocity at the peak of the incoming ion distribution again normalized by the Bohm speed.

The curve EF is the single electron-repelling emitter sheath case. It is the limiting case for large amounts of trapped ions in which the double sheath peak has been completely suppressed by the trapped ions. For this case, the emitter sheath solutions gives $u_s = 0$. This curve is not topologically connected to the curve ABC; it will be shown in Section V that trapped ions move ABC toward the single ion-repelling sheath case. The curve is much steeper (a faster increase in arc-drop) in this case because $u_s = 0$ (the half-point in ion reflection is approximately J

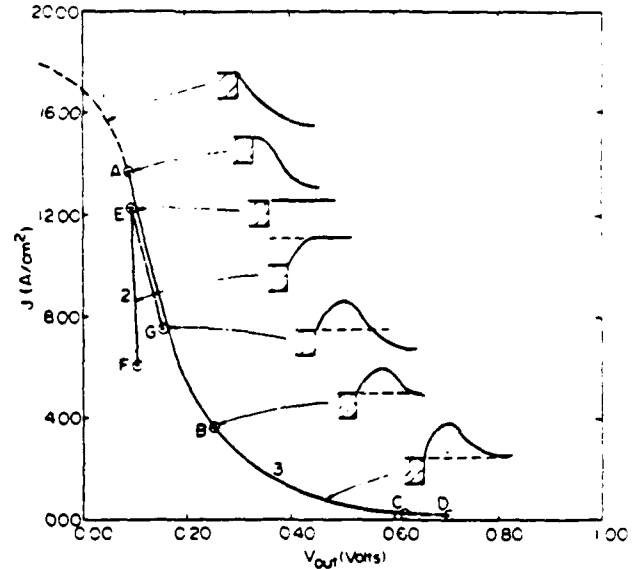


Fig. 4. CV diagram with ion reflection for case 1.

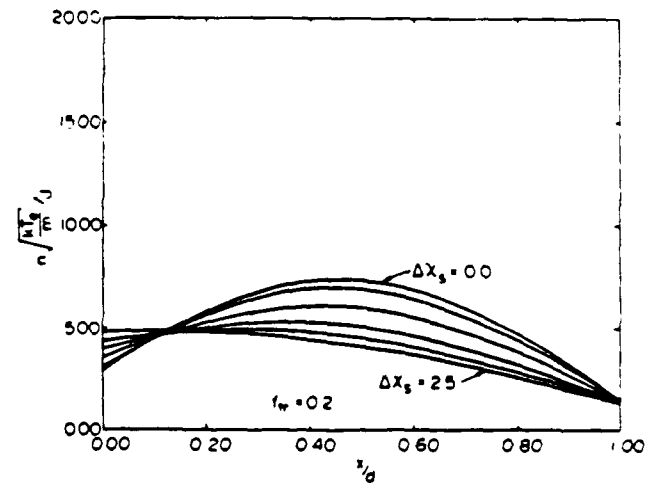


Fig. 5. Normalized plasma density with reflection.

$= 8 \text{ A/cm}^2$). Curve EG is the single ion-repelling case assuming no reflection and is therefore a Boltzmann line with constant arc-drop.

At points F and C the solutions fail at the collector. The explanation for this failure is best given by examining Figs. 5-8.

Fig. 5 is the normalized plasma density through the converter gap. The highest curve with no reflection $\Delta\chi_r = 0$ has the largest plasma density at the collector but the lowest plasma density at the emitter. Ion reflection, which decreases the ion loss rate to the emitter, raises the plasma density at the emitter but lowers the plasma density at the collector. The lower plasma density at the collector forces a smaller collector sheath height to pass the net current density. This can be seen from (10). Fig. 6 is the potential through the converter under the same reflection conditions as in Fig. 5. In Fig. 6 the first two spaces on the left make up the double emitter sheath, and the last space on the

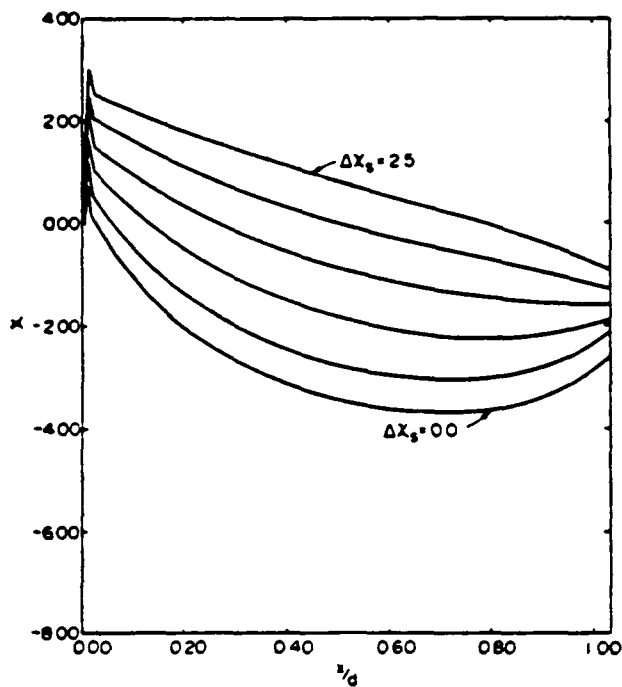


Fig. 6. Potential distribution in the converter.

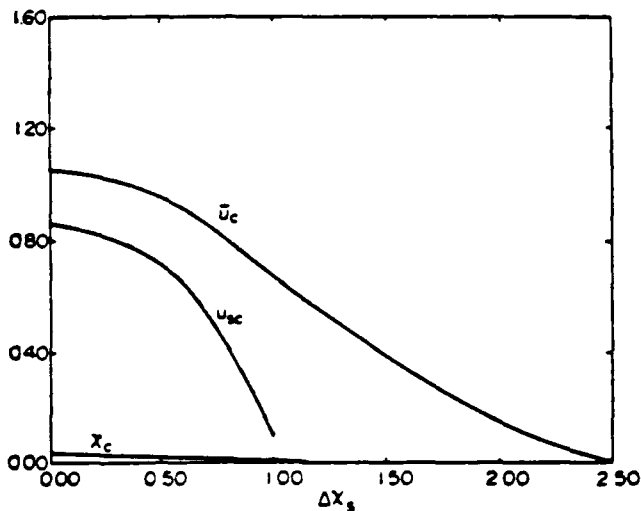


Fig. 7. Collector sheath failure.

right is the collector sheath. The region between the two sheaths is the neutral plasma region. In the no-reflection case, it can be seen that the potential has a pronounced well in the middle. This is the result of the large plasma density in the middle. As reflection increases, this well disappears on the collector side of the plasma because resistive drop there (due to low plasma density) increases to the degree that it is greater than the ambipolar rise (due to decreasing density toward the collector). Simultaneously with plasma potential gradient at the collector becoming negative, the collector sheath goes toward zero height. Fig. 7 shows the critical collector sheath quantities as the collector sheath failure occurs. Collector sheath height X_c goes toward zero, the shift speed u_{sc} goes

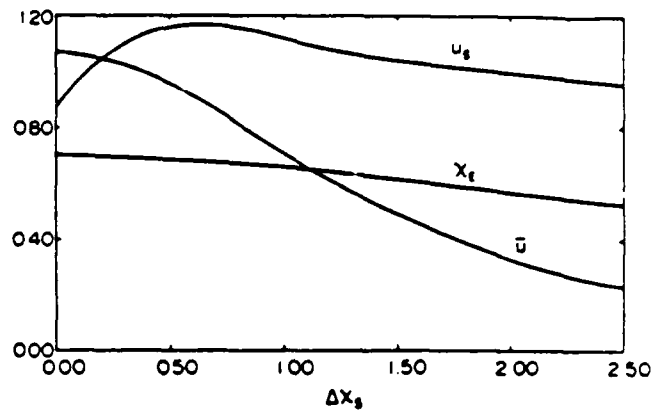


Fig. 8. Emitter sheath during reflection.

toward negative infinity, and the ion loss rate to the collector $\bar{u}_c$ is driven to zero. The two preceding quantities $\bar{u}_c$ and u_{sc} are defined at the collector sheath as $\bar{u}$ and u , were at the emitter sheath. Fig. 8 shows the changes in the emitter sheath height, ion shift speed and ion loss rate. When the collector sheath failure occurs, the ion loss rate to the collector is zero ($\bar{u}_c = 0$) and the corresponding plasma ion distribution at the collector is bunched at zero velocity ($u_{sc} = -\infty$). While the mathematics hold self-consistently until $\bar{u}_c = 0$, the physics is clearly poor at this point because $\bar{u}_c = 0$ demands that the plasma ions at the collector have zero energy (zero temperature and zero mean velocity). An estimate of when the physics becomes poor is $u_{sc} = 0$. At this point the net ion loss rate is close to the thermal speed. A second physical difficulty that occurs with collector sheath failure is that the electron Mach number there Q_c (from (10)) becomes

$$Q_c = \sqrt{\frac{2}{\pi}}$$

because the collector sheath height approaches zero (actually about 0.001). In the present continuum formulation of the plasma region, it was assumed in (13) that Q_c is small so that the electron momentum term $u_e du_e / dx$ can be neglected.

One could take the solution below the collector sheath failure point if $\bar{u}_c$ could attain negative values or if Q_c could attain values larger than $\sqrt{2/\pi}$. There is no physical basis for assuming that $\bar{u}_c$ can become negative since the collector emits nothing. However, there is a physical basis for allowing Q_c to be larger than $\sqrt{2/\pi}$ (an electron distribution shift) as can be seen in Fig. 6: the potential drop nearing the collector becomes progressively more electron accelerating as the collector sheath fails, and, therefore, the electron distribution should be shifted as the ion distribution is in an electron-repelling sheath. However, this would clearly invalidate the assumption that the electron momentum term is negligible. Therefore, the momentum term must be added to explore further in this direction and this has not been done because of the resulting complexity in the equations.

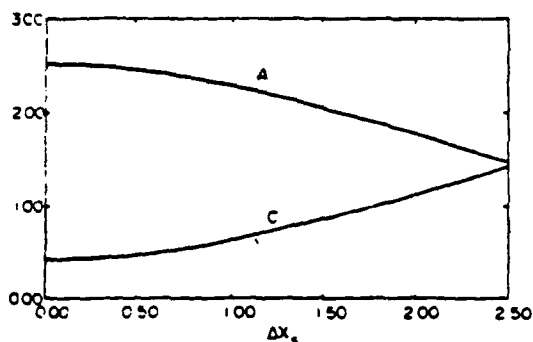


Fig. 9. Ionization coefficient A and C.

Comparison of Fig. 7 to Fig. 8 at the collector sheath failure point ($\Delta x_s = 2.5$, $u_c = 0$) shows that the ion loss rate to the emitter is positive. At this point the plasma is still ignited and generating ions as can be seen from Figs. 9 and 10. The ionization coefficient A has dropped by 50 percent, but the plasma electron temperature has dropped by only 5 percent. Finally, we note in Fig. 11 that the normalized plasma resistance R has risen by almost 100 percent. This is responsible for the increase in arc-drop and the decrease in performance. Plasma resistance increases in response to reflection because the loss of plasma electron energy to the emitter is more important than the loss of ionization energy to the emitter. Ion reflection at the emitter increases the normalized plasma density there, and consequently increases the normalized loss of plasma electron energy there. The basis of this can be seen from conservation of electron energy (22):

$$\tau = 1 - \frac{1}{2}jV_d - \frac{1}{2}j_iV_{fi}. \quad (43)$$

The ion energy loss term is generally small compared to the electron energy loss term:

$$\frac{\frac{1}{2}j_iV_{fi}}{\frac{1}{2}jV_d} = \frac{j_iV_{fi}}{jV_d} = O(0.02). \quad (44)$$

Therefore, we take the electron energy equation as

$$\tau = 1 - \frac{1}{2}jV_d. \quad (45)$$

Since τ is nearly constant (because of the ionization kinetics), the product jV_d is nearly constant. Ion reflection decreases j (because the normalized plasma density increases) and therefore increases arc-drop V_d (makes V_d a more negative number).

If the equations are reformulated in such a way as to be valid past the collector sheath failure point, then we can eventually expect to see a decrease in arc-drop and a low-current plateau as the electron temperature approaches 1 (the ignited plasma is extinguished and the ionization source is surface emission). This can be seen from (43). However, as we see, the collector failure occurs before τ has dropped more than 5 percent. Consequently, we do

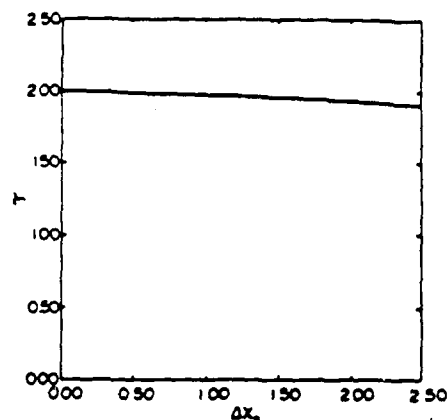


Fig. 10. Plasma electron temperature.

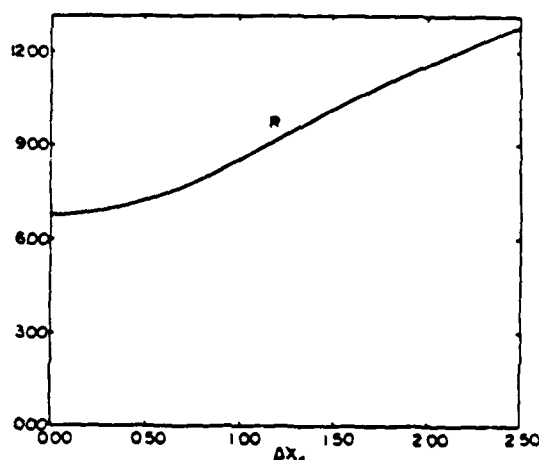


Fig. 11. Normalized plasma resistance.

not see any plateau or decrease in arc-drop as net current density is decreased in the present calculations.

V. EFFECTS OF TRAPPED IONS

Fig. 12 shows the effect of trapped ions on the CV characteristics. In this section the trapped ion distribution is assumed to have the temperature of plasma ion distribution, and 100-percent trapped ions ($f_{tr} = 1.0$) is defined to complete the ion distribution at the double emitter sheath peak such that one has a Maxwellian distribution there. Based on physical reasoning about the trapping mechanism, one expects on the order of 10. Also, some trapping calculations have been done for approximate sheath formulations [9], [10] which support this.

Curve AHJ is the CV characteristic for $f_{tr} = 0.10$. At point A there cannot be any trapped ions since the back sheath height Δx is zero. Therefore, the trapped CV merges into the nontrapped curve there. The actual amount of trapped ions on the $f_{tr} = 0.10$ curve increases from zero at point A to the full 10 percent of a thermal distribution at point H where the back sheath height Δx is equal to the sheath height x_E . The shift speed increases on AH from 1.95 to 3.00. This corresponds to what is seen in Fig. 12 where $\Delta x < x_E$.

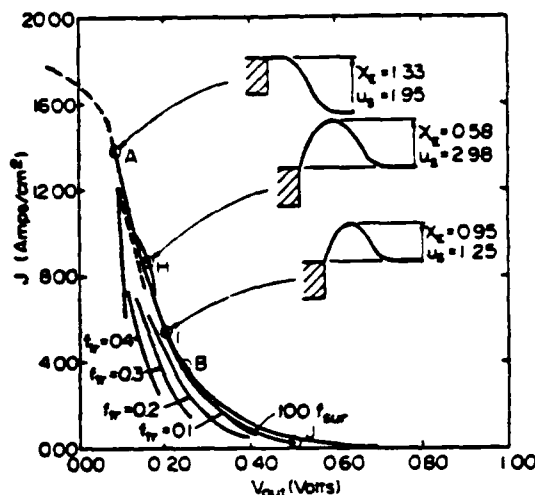


Fig. 12. CV diagram with trapped ions and surface emission.

The rise in shift speed has been limited to 3.00. This limit is placed on the shift speed because a sheath with height of about 1.0 should not have a presheath region capable of shifting the entire distribution so far. In fact, limiting the shift speed is equivalent to increasing the cut-off speed for the ion distribution function.

The arc-drop decreases as a result of the increase in u , and the consequent increase in the net ion loss rate to the emitter. A "hump" can be seen on AH where the shift speed hits 3.00. The arc-drop is lowest on this "hump" because the shift speed is at its maximum of 3.00. Between points H and I the back sheath height remains equal to the sheath height. $\Delta\chi - \chi_E = \chi_s = 0$. On this segment, u decreases to 1.25, therefore increasing arc-drop.

From point I to point J , the shift speed remains constant at 1.25 and the ion loss rate decreases because of reflection. The other trapped cases $f_{tr} = 0.2, 0.3$, and 0.4 have not been connected because they hit the 3.00 maximum shift speed much sooner than in the $f_{tr} = 0.1$ case.

Point J is the collector sheath failure point. Each of the $f_{tr} = 0.2, 0.3$, and 0.4 curves begins at $\Delta\chi_s = 0$ and ends at the collector sheath failure point. It should be noted that each of the trapped ion curves fails at a higher current than the last because the shift speed is lower.

VI. EFFECTS OF EMITTER SURFACE EMISSION

Fig. 12 shows the effect of surface emission on the $f_{tr} = 0.10$ curve: surface emission is added by multiplying the actual small amount of surface emission in case 1 by a factor of 100. This brings the surface emission up to the level in case 2, making it significant at $J = 1.0 \text{ A/cm}^2$. It can be seen that surface emission increases arc-drop: it does so in exactly the same way as reflection or trapped ions do—it decreases the net loss rate of ions to the emitter.

VII. COMPARISON WITH EXPERIMENTAL RESULTS AND CONCLUSIONS

Fig. 13 superimposes the isothermal results of Fig. 12 on the experimental results for a cesium reservoir temperature of 551 K which produces a 1-torr neutral cesium

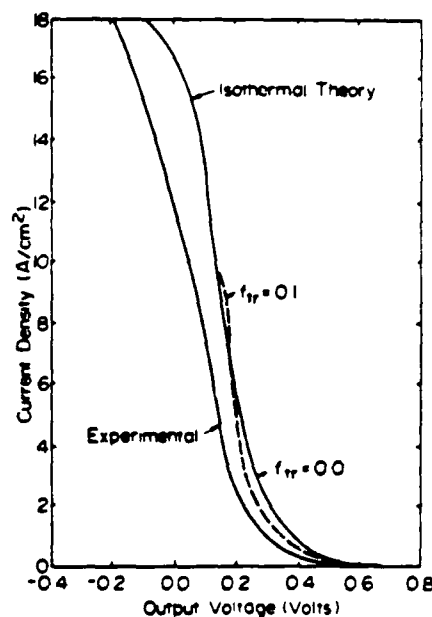


Fig. 13. Isothermal and experimental CV diagrams.

pressure. The experimental results are from [11]. The point of this comparison is that the steepness of the CV characteristic in the experimental converters can be explained by a decreasing ion loss rate to the emitter. We have shown that all three of the expected emitter sheath phenomena decrease the ion loss rate to the emitter. We cannot calculate the amount of trapped ions in a collisionless sheath without knowledge of the collisional processes. However, the experimental CV suggests that if the amount of trapped ions (f_{tr}) increases from 0 percent at $J = 14 \text{ A/cm}^2$ (the double sheath formation point) to 10 percent at $J = 2 \text{ A/cm}^2$, then the steepness could result from trapped ions reducing the ion loss rate to the emitter. Since these percentages are based on a thermal distribution of ions, they seem physically reasonable. Unfortunately, the collector sheath failure prevents us from going to the point in the calculations where τ drops enough to make surface emission the source of ions.

The experimental curve is nearly a constant 0.05 V below the isothermal result ($f_{tr} = 0.10$) except at high current densities and at the "hump." Comparison of the curves at high current density is not valid since neither the Schottky effect nor recombination has been included. The Schottky effect is important above 12 A/cm^2 in this case because the emitter sheath is single electron repelling (to the plasma) and therefore puts a strong electric field against the emitter with the appropriate sign. Recombination is also potentially important because the plasma density scales with current density, and at high current densities the plasma density in the middle of the converter approaches the Saha density. The 0.05-V difference may or may not be explained by a discrepancy in the assumed collector work function. At 750 K the collector emits essentially nothing and therefore any change in the collector work function directly affects output voltage. If the collector work function were in fact 1.65 instead of 1.60 V, then the isothermal result would lie nearly on top of the

experimental result. We have not adjusted the assumed collector work function so as to illustrate the importance of it and therefore the importance of the surface physics of the adsorbed cesium layer. The "hump" should not be taken as an expected experimental result since it results from the interaction of the trapped ions with the plasma-emitter sheath interface. Instead it should be taken as a second reason (in addition to the cutoff of the ion distribution) for further study of the matching region between the collisionless sheath and the neutral plasma.

REFERENCES

- [1] G. L. Main and S. H. Lam, in *Proc. 1982 Int. IEEE Conf. Plasma Sci.* (Ottawa, Canada), May 1982, p. 118.
- [2] G. L. Main and S. H. Lam, in *Proc. Int. Energy Conversion Eng. Conf.* (Orlando, FL), Aug. 1983, p. 215.
- [3] L. Lundgren, *J. Appl. Phys.*, vol. 58, p. 142, 1985.
- [4] L. Lundgren, *J. Appl. Phys.*, vol. 58, p. 4032, 1985.
- [5] E. R. Harrison and W. B. Thompson, *Proc. Phys. Soc. London*, vol. 74, p. 145, 1959.
- [6] G. L. Main, Ph.D. dissertation, Princeton Univ., Princeton, NJ, 1984.
- [7] S. H. Lam, "Preliminary report on plasma arc-drop in thermionic converters," Princeton Univ., Princeton, NJ, 1976.
- [8] J. L. Lawless, Ph.D. dissertation, Princeton Univ., Princeton, NJ, 1980.
- [9] C. Warner and L. K. Hansen, Tech. Summary Rep. AI-69-112 Contract NONR-3192(00), Dec. 1969.
- [10] D. R. Wilkins and D. J. Rush, presented at Electrostatic Sheath Phenomena in Thermionic Converters, IEEE Thermionic Converter Specialist Conf., 1970.
- [11] Thermo-Electron Corp., Waltham, MA, DOE Advanced Thermionic Tech. Program, Progress Rep. 48, Sept. 1981.

ASYMPTOTIC SHEATH THEORY

The Asymptotic Sheath Theory developed under this grant is set forth in the following paper.

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Asymptotically correct collisional presheaths

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Asymptotically correct collisional presheaths

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Few exact solutions for collisional presheaths exist because of the difficulty of simultaneously satisfying both the collisional Boltzmann equation and the Poisson equation. The exact solutions that do exist are for very specialized collision terms such as constant cross-section charge exchange with cold neutrals. The present paper presents an asymptotic method which is applicable to a variety of collision terms and is applied in particular to constant collision frequency charge exchange with noncold neutrals. Constant collision frequency and constant cross-section collision with cold neutral results are also presented. The first-order terms for the presheath potential rise and ion distribution functions are calculated and it is shown that second- and higher-order terms can be calculated using a multiexponential expansion for presheath potential rise. The first-order cold neutral constant cross-section results correspond well to the exact solution. The calculated presheath potential rises are of the order expected from the Bohm criterion, and in some of the specialized cold neutral cases, exactly $kT_e/2$. The presheath potential rise is reduced by a neutral plasma potential gradient which accelerates ions toward the presheath. In all cases the collisional presheath is asymptotically matched to both the neutral plasma and the collisionless sheath.

I. INTRODUCTION

The majority of plasma-surface interaction work matches a neutral plasma to a collisionless sheath without detailed consideration of a collisional presheath. However, the collisional presheath structure is of great interest. Sheath theory, beginning with Bohm,¹ tends to assume that the plasma ion distribution is cold so that a minimum presheath potential rise may be calculated, which makes the collisionless sheath self-consistent. Harrison and Thompson² generalize the Bohm criterion to noncold ion distributions; however, the result is sensitive to the density of the low energy tail of the ion distribution, which in turn is strongly affected by the collisional presheath. And, a second difficulty in the absence of a collisional presheath is that the collisionless sheath and the surface beyond it may return no ions or a nonthermal distribution of ions which the collisional presheath must match to the neutral plasma region.

Some exact solutions exist for presheaths; notable is the work of Ecker and Kanne³ and Riemann,⁴ who derive exact solutions for collision terms based on charge exchange with cold neutrals and Emmert *et al.*,⁵ who derive an exact collisionless solution in which there is an ionization source. In the present paper an asymptotically correct collisional presheath theory is developed which can be applied to a less restrictive range of collision terms. Potential in the presheath is expanded as a multiexponential series and the distribution functions are expanded in terms of presheath potential rise. First-order approximations are calculated for both constant collision frequency and constant cross-section charge exchange collisions.

II. FIRST-ORDER ASYMPTOTIC POTENTIAL FORMULATION

In this section it is assumed that the potential in the collisional presheath is of the form

$$U = U_0 + \Delta U = \alpha x + e^{\beta x}, \quad (1)$$

where $U_0 = \alpha x$ is the assumed linear potential in the neutral plasma and $\Delta U = e^{\beta x}$ is the additional potential rise in the collisional presheath, as shown in Fig. 1. In this paper the convention used is that $U = q\phi$, where q is the electron charge and ϕ is potential in electron volts so that U has units of energy. In addition, potential is defined in the reverse of the usual sign convention so that increasing potential repels electrons. With these conventions, the Boltzmann equation can be written as

$$\frac{dU}{dx} \left(v \frac{\partial f}{\partial U} \pm \frac{1}{m} \frac{\partial f}{\partial v} \right) = \left(\frac{\partial f}{\partial t} \right)_c. \quad (2)$$

In Eq. (2) and those following, the $\pm$ denotes the sign of the charged species in question; the upper sign refers to positively charged ions and the lower sign to electrons. The Boltzmann equation is expressed in terms of ΔU , which will be the expansion variable in the presheath:

$$v\beta\Delta U \frac{\partial f}{\partial \Delta U} \pm \frac{1}{m} (\beta\Delta U + \alpha) \frac{\partial f}{\partial v} = \left(\frac{\partial f}{\partial t} \right)_c. \quad (3)$$

The distribution function is then expanded as

$$f = f_0(v) + \Delta U f_1(v) + \Delta^2 U f_2(v) + \dots, \quad (4)$$

so that the derivatives are

$$\frac{\partial f}{\partial \Delta U} = f_1(v) + 2\Delta U f_2(v) + 3\Delta^2 U f_3(v) + \dots \quad (5)$$

and

$$\frac{\partial f}{\partial v} = \frac{\partial f_0}{\partial v}(v) + \Delta U \frac{\partial f_1}{\partial v}(v) + \Delta^2 U \frac{\partial f_2}{\partial v}(v) + \dots \quad (6)$$

Substitution of (5) and (6) into the Boltzmann equation (3) yields the terms

$$1: \pm \frac{\alpha}{m} \frac{\partial f_0}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_1, \quad (7a)$$

$$\Delta U: \alpha \beta f_1(v) \pm \frac{\beta}{m} \frac{\partial f_0}{\partial v}(v) \pm \frac{\alpha}{m} \frac{\partial f_1}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_{\Delta U}, \quad (7b)$$

$$\Delta U^2: 2\alpha \beta f_2(v) \pm \frac{\beta}{m} \frac{\partial f_1}{\partial v}(v) \pm \frac{\alpha}{m} \frac{\partial f_2}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_{\Delta U^2}, \quad (7c)$$

⋮

$$\Delta U^n: \alpha \beta f_n(v) \pm \frac{\beta}{m} \frac{\partial f_{n-1}}{\partial v}(v) \pm \frac{\alpha}{m} \frac{\partial f_n}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_{\Delta U^n}. \quad (7d)$$

The quantity β , representing the presheath potential rise, is determined from the Poisson equation

$$\frac{d^2 U}{dx^2} = 4\pi q^2 \left(\int_{-\infty}^{\infty} f_i(v, \Delta U) dv - \int_{-\infty}^{\infty} f_e(v, \Delta U) dv \right), \quad (8)$$

where q is the electron charge. It is assumed that the ions are singly ionized for simplicity. The Poisson equation (8) is expanded as

$$\beta^2 \Delta U = 4\pi q^2 \left[\left(\int_{-\infty}^{\infty} f_{i1}(v) dv - \int_{-\infty}^{\infty} f_{e1}(v) dv \right) \Delta U + \left(\int_{-\infty}^{\infty} f_{i2}(v) dv - \int_{-\infty}^{\infty} f_{e2}(v) dv \right) \Delta U^2 + \dots \right], \quad (9)$$

where charge neutrality at $\Delta U = 0$ has eliminated the terms containing f_{i0} and f_{e0} :

$$n_0 = \int_{-\infty}^{\infty} f_{i0}(v) dv = \int_{-\infty}^{\infty} f_{e0}(v) dv.$$

The quantity n_0 is the neutral plasma density of the asymptotic presheath, not of the neutral plasma.

III. FIRST-ORDER SOLUTION WITH A CONSTANT COLLISION FREQUENCY CHARGE EXCHANGE COLLISION TERM

The constant collision frequency charge exchange collision term is modeled as

$$\left(\frac{\partial f_i}{\partial t} \right)_c = \frac{1}{\tau n_n} \left(f_n(v) \int_{-\infty}^{\infty} f_i(u) du - f_i(v) \int_{-\infty}^{\infty} f_n(u) du \right), \quad (10)$$

where $f_n(v)$ is the neutral distribution and τ is the collision time. Previous work has assumed cold neutrals and results in an integral equation which is solvable only for constant collision cross section.⁴

A. Zero plasma potential gradient ($\alpha = 0$)

In this case Eqs. (7) become

$$1: 0 = \frac{1}{\tau n_n} \left(f_n(v) \int_{-\infty}^{\infty} f_{i0}(u) du - f_{i0}(v) \int_{-\infty}^{\infty} f_n(u) du \right),$$

$$\Delta U: \alpha \beta f_{i1}(v) + \frac{\beta}{m} \frac{\partial f_{i0}}{\partial v}(v) = \frac{1}{\tau n_n} \left(f_{i1}(v) \int_{-\infty}^{\infty} f_n(u) du - f_{i1}(v) \int_{-\infty}^{\infty} f_n(u) du \right), \quad (11)$$

⋮

$$\Delta U^n: \alpha \beta f_{in}(v) + \frac{\beta}{m} \frac{\partial f_{i(n-1)}}{\partial v}(v) = \frac{1}{\tau n_n} \left(f_{in}(v) \int_{-\infty}^{\infty} f_n(u) du - f_{in}(v) \int_{-\infty}^{\infty} f_n(u) du \right).$$

Under the assumption that the neutral distribution is Maxwellian $f_n(v) = n_n \sqrt{m/2\pi kT} \exp(-mv^2/2kT)$, the solution to (11) is

$$f_{i0} = C f_n(v),$$

$$f_{i1}(v) = (1/kT) f_{i0}(v), \quad (12)$$

⋮

$$f_{in}(v) = (1/nkT) f_{i(n-1)}(v).$$

Thus

$$f_i(v, \Delta U) = C e^{(\Delta U/kT)} f_n(v), \quad (13)$$

which is the expected result. In this case the mean ion velocity is zero throughout the collisional presheath since charge exchange collisions conserve ions and the mean ion velocity in the neutral plasma is zero. Thus, if $\alpha = 0$, constant collision frequency charge exchange collisions do not shift the ion distribution upward in velocity. This presheath can be matched to a collisionless sheath only if the collisionless sheath returns all the ions entering it from the collisional presheath.

With electron density assumed to follow

$$n_e(\Delta U) = n_0 e^{(-\Delta U/kT_e)},$$

the Poisson equation (9) yields, to first order,

$$\beta^2 = 4\pi q^2 n_0 (1/kT + 1/kT_e),$$

which is the length scale of the Debye length. Thus for $\alpha = 0$ the collisional presheath is not distinct from the collisionless sheath since there is no separate collisional presheath length scale.

B. Nonzero plasma potential gradient ($\alpha \neq 0$)

Under this condition there is a net flux of ions from the plasma into the sheath, which allows the construction of a collisional presheath that accelerates the ions and depopulates the ion distribution of returning ions. Thus the collisional presheath may be correctly matched to the collisionless sheath which returns no ions. In this case (7a) and (7b) can be written as

$$\frac{\alpha}{m} \frac{\partial f_0}{\partial v}(v) = \frac{1}{\tau n_e} [f_n(v) n_0 - n_e f_0(v)], \quad (14a)$$

$$v \beta f_1(v) + \frac{\beta}{m} \frac{\partial f_0}{\partial v} + \frac{\alpha}{m} \frac{\partial f_1}{\partial v}(v) = \frac{1}{\tau n_e} [f_n(v) n_1 - n_e f_1(v)]. \quad (14b)$$

The solution to Eqs. (14) are

$$f_0(v) = n_0 \exp\left(\frac{-mv}{\alpha\tau}\right) \frac{m}{\alpha\tau} \sqrt{\frac{m}{2\pi kT}} \int_{-\infty}^v \exp\left(-\frac{mu^2}{2kT} + \frac{mu}{\alpha\tau}\right) du \quad (15)$$

and

$$f_1(v) = \exp\left(-\frac{\beta mv^2}{2\alpha} - \frac{mv}{\alpha\tau}\right) \left[\int_0^v \exp\left(\frac{\beta mu^2}{2\alpha} + \frac{mu}{\alpha\tau}\right) \left[\frac{n_1 m}{\alpha\tau} \sqrt{\frac{m}{\alpha\pi kT}} \exp\left(\frac{mu^2}{2kT}\right) - \frac{\beta}{\alpha} \frac{\partial f_0}{\partial v}(u) \right] du + C \right], \quad (16)$$

where

$$n_0 = \int_{-\infty}^{\infty} f_0(v) dv \quad (17)$$

and

$$n_1 = \int_{-\infty}^{\infty} f_1(v) dv. \quad (18)$$

The constant of integration in (15) has been set so that f_0 goes to zero at $-\infty$; f_0 goes to zero at ∞ regardless of the constant of integration. Equation (17) is immediately satisfied by (15). The constant of integration C in (16) must be set so that (18), which represents self-consistency, is satisfied. It can be seen from (16) that f_1 goes to zero at $-\infty$ and ∞ regardless of the constant C . From (18), then

$$\begin{aligned} C = n_1 & \left[1 - \int_{-\infty}^{\infty} \exp\left(-\frac{\beta mv^2}{2\alpha} - \frac{mv}{\alpha\tau}\right) \int_0^v \exp\left(\frac{\beta mu^2}{2\alpha} + \frac{mu}{\alpha\tau}\right) \frac{m}{\alpha\tau} \sqrt{\frac{m}{2\pi kT}} \exp\left(-\frac{mu^2}{2kT}\right) du dv \right] \\ & \times \left[\sqrt{\frac{2\pi\alpha}{m\beta}} \exp\left(\frac{m}{2\alpha\beta\tau^2}\right) \right]^{-1} + \left[\int_{-\infty}^{\infty} \exp\left(-\frac{\beta mv^2}{2\alpha} - \frac{mv}{\alpha\tau}\right) \int_0^v \frac{\beta}{\alpha} \exp\left(\frac{\beta mu^2}{2\alpha} + \frac{mu}{\alpha\tau}\right) \frac{\partial f_0}{\partial v}(u) du dv \right] \\ & \times \left[\sqrt{\frac{2\pi\alpha}{m\beta}} \exp\left(\frac{m}{2\alpha\beta\tau^2}\right) \right]^{-1}. \end{aligned} \quad (19)$$

The exponential sheath rise β is determined from the Poisson equation under the simplifying assumption that

$$n_e = \int_{-\infty}^{\infty} f_e(v) dv = n_0 \exp\left(-\frac{\Delta U}{kT_e}\right). \quad (20)$$

One might expect that the approximation should be $n_e = n_0 \exp(-U/kT_e)$; however, this cannot be true in the asymptotic presheath because n_e must approach n_0 as U approaches negative infinity. With (20) the Poisson equation (9) to first order becomes

$$\beta^2 = 4\pi q^2 (n_1 + n_0/kT_e). \quad (21)$$

Since the ion density is only calculated to first order, the same will be done for the electron density in (20).

To obtain a particular solution it is assumed here that the collisionless sheath to which the collisional presheath is joined at $\Delta U = \Delta U^*$ returns no ions. In particular,

$$\int_{-\infty}^0 f(v, \Delta U^*) dv = 0, \quad (22)$$

or

$$\int_{-\infty}^{\infty} f_0(v) dv + \Delta U^* \int_{-\infty}^{\infty} f_1(v) dv = 0 \quad (23)$$

and

$$\int_{-\infty}^{\infty} v f(v, \Delta U^*) dv = 0, \quad (24)$$

or

$$\int_{-\infty}^{\infty} v f_0(v) dv + \Delta U^* \int_{-\infty}^{\infty} v f_1(v) dv = 0. \quad (25)$$

Because the approximation is only first order, it is not possible to impose the condition that $f(v)$ is uniformly zero for returning ions. Equations (23) and (25) represent zero returning ion density and zero returning ion flux. When higher-order terms are included, the conditions of zero returning ion momentum flux, zero returning ion energy flux, etc., can be applied in succession. Equations (21), (23), and (25) are solved for n_1 , β , and ΔU^* , with all other quantities assumed constant. Equation (21) immediately satisfies the Bohm criterion at $\Delta U = \Delta U^*$ for the first-order approximation

$$n_1 + n_0/kT_e > 0. \quad (26)$$

The Poisson equation (21) can be written as

$$\beta^2 \lambda_D^2 = 1 + kT_e (n_1/n_0), \quad (27)$$

where

$$\lambda_D = \sqrt{kT_e/4\pi q^2 n_0} \quad (28)$$

is the Debye length. It is expected that the length scale of the presheath should be of the order $\beta = 1/\lambda_i$, where λ_i is the ion mean free path. In the circumstance that the Debye length is small compared to the ion mean free path, the product $\beta^2 \lambda_D^2$ is small and

$$n_1 = -n_0/kT_e. \quad (29)$$

The neutral plasma region is matched to the collisional presheath also at $\Delta U = \Delta U^*$, as shown in Fig. 1, to produce a three-scale uniform asymptotic solution. In particular, assuming constant collision frequencies, the momentum equations become

$$\left(kT_i - \frac{m_i \Gamma_i^2}{n^2} \right) \frac{dn}{dx} = n \frac{dU}{dx} - \frac{m_i \Gamma_i}{\tau} \quad (30)$$

and

$$\left(kT_e - \frac{m_e \Gamma_e^2}{n^2} \right) \frac{dn}{dx} = -n \frac{dU}{dx} - \frac{m_e \Gamma_e}{\tau_e}, \quad (31)$$

where

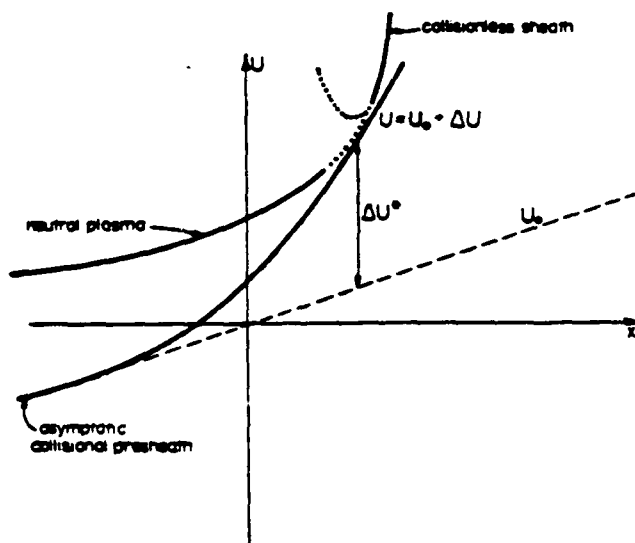


FIG. 1. Asymptotically correct potential in the collisional presheath.

$$n = n_0(1 - \Delta U^*/kT_e), \quad (32)$$

$$\frac{dn}{dx} = -n_0\beta \frac{\Delta U^*}{kT_e}, \quad (33)$$

and

$$\frac{dU}{dx} = \alpha + \beta\Delta U^*. \quad (34)$$

The quantity n is the plasma density at the matching point ΔU^* and Γ , and Γ_e are, respectively, the ion and electron net fluxes. Nondimensionalization results in

$$A = (\alpha\tau/m)\sqrt{m/2kT}, \quad (35)$$

$$B = \beta kT/\alpha, \quad (36)$$

$$R_e = T_e/T, \quad (37)$$

$$\omega = \sqrt{m/2kT} v, \quad (38)$$

where A and R_e are the parameters and B is a function of A and R_e . The quantity A represents the nondimensional asymptotic presheath potential gradient, B represents the nondimensional exponential presheath rise, R_e is the electron to neutral temperature ratio, and ω is the nondimensional velocity. The distribution functions can then be written as

$$F_0(\omega, A) = \frac{f_0(v)}{n_0\sqrt{m/2kT}} = \frac{\exp(-\omega/A)}{\sqrt{\pi} A} \int_{-\infty}^{\omega} \exp\left(-\xi^2 + \frac{\xi}{A}\right) d\xi \quad (39)$$

and

$$\begin{aligned} F_1(\omega, A, B) &= \frac{f_1(v)}{(n_0/kT_e)\sqrt{m/2kT}} \\ &= \frac{\exp(-B\omega^2 - \omega/A)}{\sqrt{\pi}} \left(\int_0^{\omega} \exp\left(B\xi^2 + \frac{\xi}{A}\right) \left[-\frac{1}{A} \exp(-\xi^2) \right. \right. \\ &\quad \left. \left. - R_e B \left[\frac{1}{A} \exp(-\xi^2) - \frac{1}{A^2} \exp\left(-\frac{\xi}{A}\right) \int_{-\infty}^{\xi} \exp\left(-\eta^2 + \frac{\eta}{A}\right) d\eta \right] \right] d\xi + C \right), \end{aligned} \quad (40)$$

where

$$\begin{aligned} C &= - \left[1 - \frac{1}{\sqrt{\pi} A} \int_{-\infty}^{\omega} \exp\left(-B\omega^2 - \frac{\omega}{A}\right) \int_0^{\omega} \exp\left(B\xi^2 + \frac{\xi}{A} - \xi^2\right) d\xi d\omega \right] \left[\sqrt{\frac{1}{B}} \exp\left(\frac{1}{4BA^2}\right) \right]^{-1} \\ &\quad + \frac{R_e B}{\sqrt{\pi}} \int_{-\infty}^{\omega} \exp\left(-B\omega^2 - \frac{\omega}{A}\right) \int_0^{\omega} \exp\left(B\xi^2 + \frac{\xi}{A}\right) \\ &\quad \times \left[\frac{1}{A} \exp(-\xi^2) - \frac{1}{A^2} \exp\left(-\frac{\xi}{A}\right) \int_{-\infty}^{\xi} \exp\left(-\eta^2 + \frac{\eta}{A}\right) d\eta \right] d\xi d\omega \left[\sqrt{\frac{1}{B}} \exp\left(\frac{1}{4BA^2}\right) \right]^{-1}. \end{aligned} \quad (41)$$

Thus (23) and (25) become

$$\int_{-\infty}^0 F_0(\omega, A) d\omega + \frac{\Delta U^*}{kT_e} \int_{-\infty}^0 F_1(\omega, A, B) d\omega = 0 \quad (42)$$

and

$$\int_{-\infty}^0 \omega F_0(\omega, A) d\omega + \frac{\Delta U^*}{kT_e} \int_{-\infty}^0 \omega F_1(\omega, A, B) d\omega = 0. \quad (43)$$

Figure 2 presents the presheath potential rise $\Delta U^*/kT_e$ and the nondimensional exponential rise B as a function of the nondimensional asymptotic presheath potential gradient A for a range of electron to neutral temperature ratios R_e . As would be intuitively expected, the presheath potential rise decreases with increasing A . Figure 3 presents the ion distribution functions at the neutral plasma-collisional presheath interface $F_0(\omega)$, the first-order correction to the distribution function $F_1(\omega)$, and the resulting distribution function at the collisional presheath-collisionless sheath interface $F_0(\omega) + \Delta U^* F_1(\omega)$. Although the resulting distribution is not uniformly zero for $\omega < 0$, its net returning density and flux are zero by (42) and (43). It is expected that higher-order corrections to the distribution function and potential with the corresponding application of higher-order moment conditions of zero returning momentum, energy, etc., will converge the returning distribution function toward a uniform zero.

In the limit of cold neutrals, the constant collision frequency charge exchange solution is considerably simplified. Equations (14a) and (14b) become

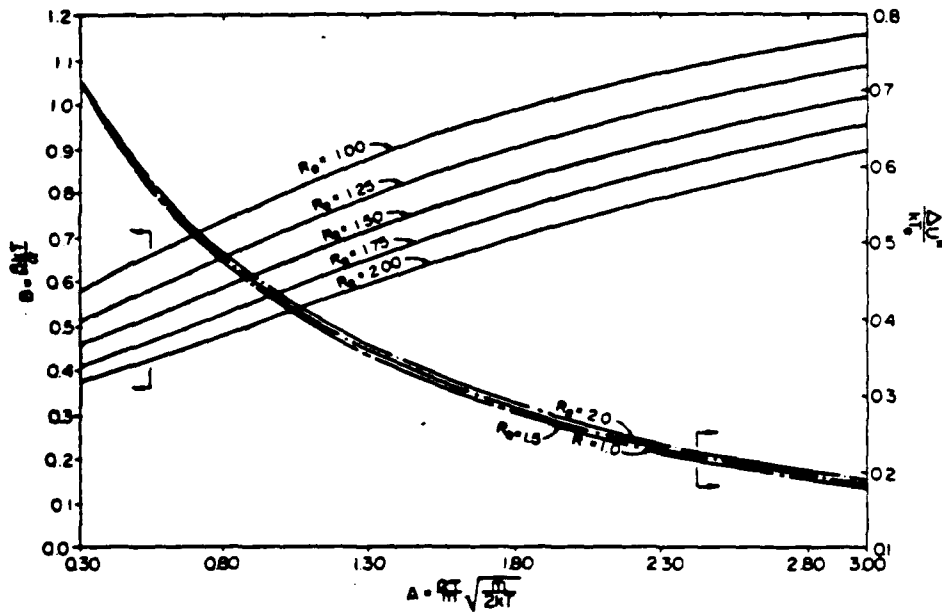


FIG. 2. Constant collision frequency presheath potential rise.

$$\frac{\alpha}{m} \frac{\partial f_0}{\partial v}(v) = \frac{1}{\tau n_n} [n_n \delta_n(v) n_0 - n_n f_0(v)] \quad (44)$$

and

$$v \beta f_1(v) + \frac{\beta}{m} \frac{\partial f_0}{\partial v} + \frac{\alpha}{m} \frac{\partial f_1}{\partial v}(v) = \frac{1}{\tau n_n} [n_n \delta_n(v) n_1 - n_n f_1(v)]. \quad (45)$$

The solutions to (44) and (45) are

$$f_0(v) = \begin{cases} n_0 (m/\alpha \tau) \exp(-mv/\alpha \tau), & v > 0, \\ 0, & v < 0, \end{cases} \quad (46)$$

and

$$f_1(v) = \begin{cases} \exp\left(-\frac{\beta m v^2}{2\alpha} - \frac{mv}{\alpha \tau}\right) \left[C^+ + \frac{\beta}{\alpha} n_0 \left(\frac{m}{\alpha \tau}\right)^2 \int_0^v \exp\left(\frac{\beta m u^2}{2\alpha}\right) du \right], & v > 0, \\ \exp\left(-\frac{\beta m v^2}{2\alpha} - \frac{mv}{\alpha \tau}\right) (C^-), & v < 0, \end{cases} \quad (47)$$

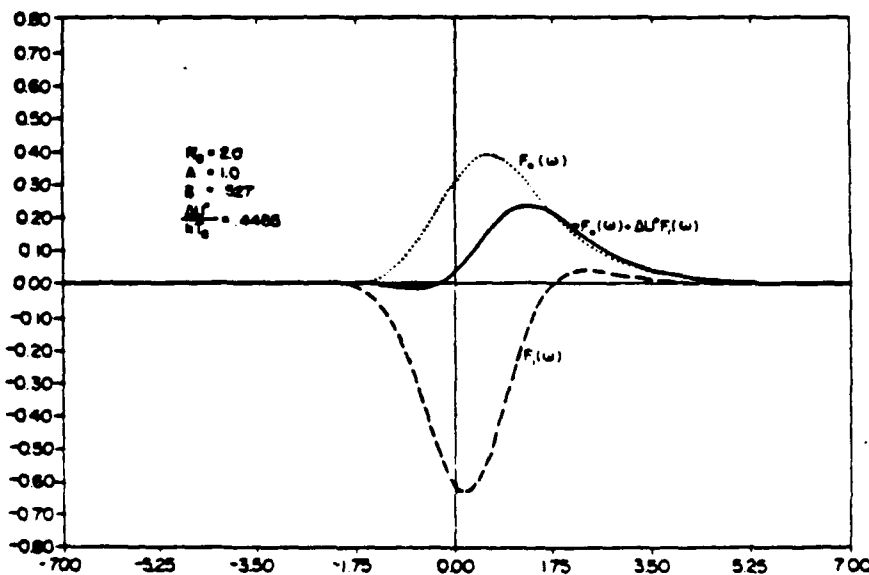


FIG. 3. Constant collision frequency ion distributions in the neutral plasma and at the presheath-sheath boundary.

such that

$$C^+ - C^- = (m/\alpha\tau)[n_1 - (\beta/\alpha)n_0]. \quad (48)$$

Equation (46) immediately satisfies $n_0 = \int_{-\infty}^{\infty} f_0(v)dv$. No returning ions implies that

$$C^- = 0 \quad (49)$$

and

$$C^+ = (m/\alpha\tau)[n_1 - (\beta/\alpha)n_0] \quad (50)$$

since f_0 on $v < 0$ is already zero. The final condition is then that $n_1 = \int_0^{\infty} f_1(v)dv$, or

$$n_1 = \int_0^{\infty} \exp\left(-\frac{\beta mv^2}{2\alpha} - \frac{mv}{\alpha\tau}\right) \left[\frac{n_1 m}{\alpha\tau} - \frac{\beta n_0}{\alpha} \frac{m}{\alpha\tau} + \frac{\beta n_0}{\alpha} \left(\frac{m}{\alpha\tau}\right)^2 \int_0^v \exp\left(\frac{\beta mu^2}{2\alpha}\right) du \right] dv. \quad (51)$$

The application of $n_1 = -n_0/kT_e$ yields

$$\frac{\beta kT_e}{\alpha} = \left\{ 1 - \int_0^{\infty} \exp\left(-\frac{\beta \alpha \tau^2}{2m} \xi^2 - \xi\right) d\xi \right\} \left\{ \int_0^{\infty} \exp\left(-\frac{\beta \alpha \tau^2}{2m} \xi^2 - \xi\right) \left[1 - \int_0^{\xi} \exp\left(\frac{\beta \alpha \tau^2}{2m} \eta^2\right) d\eta \right] d\xi \right\}^{-1}. \quad (52)$$

In this case, ΔU^* is defined by

$$f_0(0^+) + \Delta U^* f_1(0^+) = 0, \quad (53)$$

which yields

$$\Delta U^*/kT_e = 1/(\beta kT_e/\alpha + 1), \quad (54)$$

as expected. In the limit of $\beta \alpha \tau^2/2m \rightarrow 0$ we have

$$\beta kT_e/\alpha = 1 \quad (55)$$

and

$$\Delta U^* = kT_e/2, \quad (56)$$

which corresponds to the Bohm criterion. Figure 4 presents the variation of $B = \beta kT_e/\alpha$, with $\beta \alpha \tau^2/2m$ for the cold neutral case. A particular β for the parameters can be conveniently found by drawing a line from the origin, with slope $2mkT_e/\tau^2\alpha^2$, so that the intersection is the solution. Figure 5 presents an example cold neutral ion distribution. Examination of the ion distribution function at $v = 0$ shows that the slope is discontinuous. This is because the neutral source is a delta function at $v = 0$. It appears that the Bohm criterion cannot be satisfied at ΔU^* because the integral $\int_0^{\infty} [f(v)/v^2]dv$ is singular; however, the use of this integral in the Bohm criterion assumes that the ions accelerated are not replaced. In this case the ions accelerated from $v = 0$ are replaced by ions from the cold neutral distribution which, of course, is a delta function at $v = 0$.

IV. FIRST-ORDER SOLUTION WITH A QUASICONSTANT CROSS-SECTION COLLISION TERM

First-order asymptotic solutions can also be developed for a quasiconstant cross-section collision term

$$\left(\frac{\partial f}{\partial t}\right)_c = \sigma \left(\int_{-\infty}^{\infty} f_n(v)f(u)|v-u|du - \int_{-\infty}^{\infty} f(v)f_n(u)|v-u|du \right). \quad (57)$$

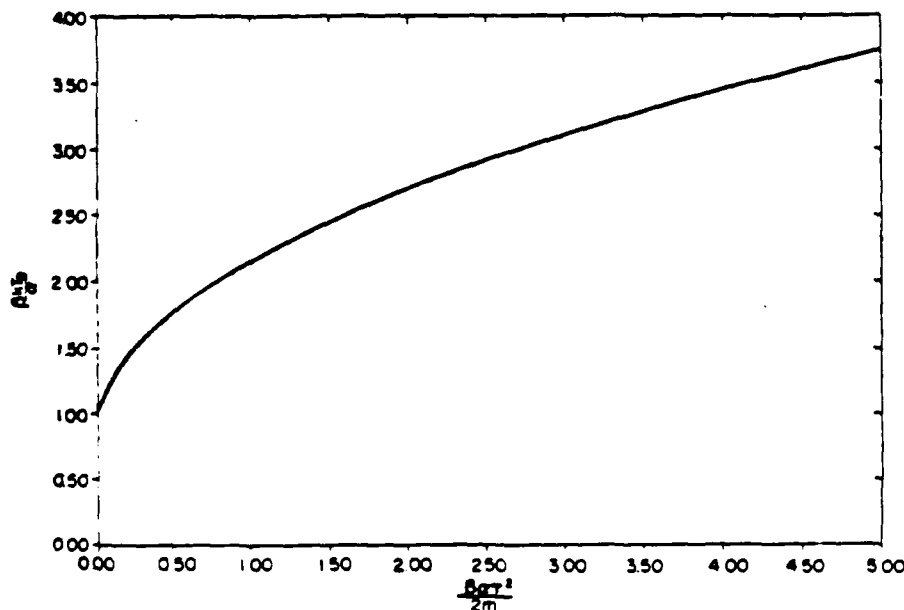


FIG. 4. Constant collision frequency presheath rise with cold neutrals.

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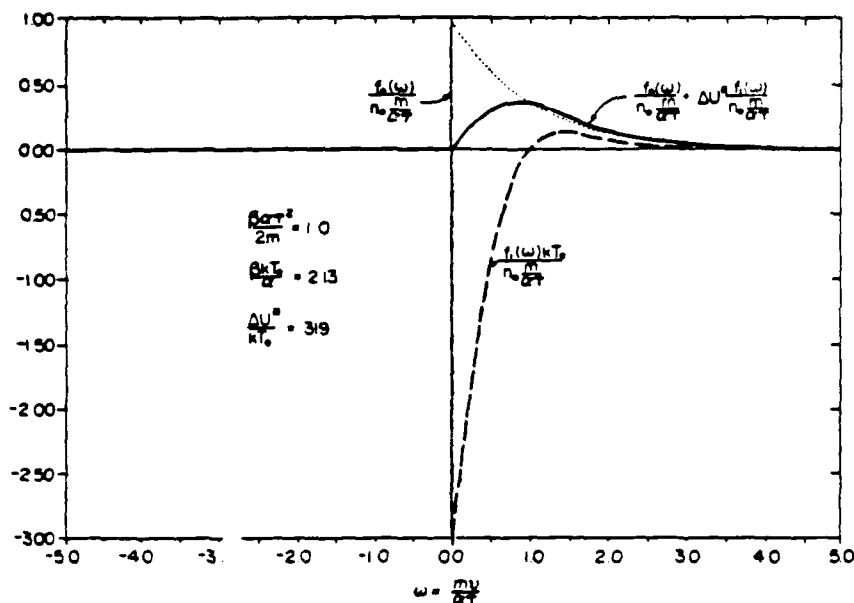


FIG. 5. Constant collision frequency ion distribution with cold neutrals.

This collision term is not really constant cross section because it is a one-dimensional representation which does not take into account average velocities in the other two dimensions. However, this collision term corresponds to that commonly called constant cross section. The application of this term leads to a set of integro-differential equations which can be at least approximately solved, and in the cold neutral case it leads to readily soluble first-order differential equations. The cold neutral case presented here corresponds to that which can be solved exactly (Riemann⁴). Unfortunately, though, the exact solution method is not extensible to noncold neutrals. The cold neutral collision term is

$$\left(\frac{\partial f}{\partial t}\right)_c = \sigma n_n \delta(v) \int_{-\infty}^{\infty} f(u) |u| du - \sigma f(v) n_n |v| \quad (58)$$

and the zero-order Boltzmann equation term (7a) becomes

$$\frac{\alpha}{m} \frac{\partial f_0}{\partial v}(v) = \sigma n_n \delta(v) \int_{-\infty}^{\infty} f_0(u) |u| du - \sigma n_n |v| f_0(v), \quad (59)$$

for which the solution is

$$f_0(v) = \begin{cases} n_0 \sqrt{\frac{2}{\pi}} \sqrt{\frac{\sigma m n_n}{\alpha}} \exp\left(-\frac{\sigma m n_n}{2\alpha} v^2\right), & v > 0, \\ 0, & v < 0. \end{cases} \quad (60)$$

The first-order Boltzmann term is

$$v \beta f_1(v) + \frac{\beta}{m} \frac{\partial f_0}{\partial v}(v) + \frac{\alpha}{m} \frac{\partial f_1}{\partial v}(v) = \sigma n_n \delta(v) \int_{-\infty}^{\infty} f_1(u) |u| du - \sigma n_n |v| f_1(v), \quad (61)$$

for which the solution is

$$f_1(v) = \begin{cases} \exp\left[-\frac{1}{2}\left(\frac{\beta m}{\alpha} + \frac{\sigma m n_n}{\alpha}\right)v^2\right] \left[\frac{n_0}{m} \sqrt{\frac{2}{\pi}} \left(\sqrt{\frac{\sigma m n_n}{\alpha}}\right)^3 \left[\exp\left(\frac{\beta m v^2}{2\alpha}\right) - 1\right] + C^+\right], & v > 0, \\ \exp\left[-\frac{1}{2}\left(\frac{\beta m}{\alpha} - \frac{\sigma m n_n}{\alpha}\right)v^2\right] (C^-), & v < 0. \end{cases} \quad (62)$$

The jump condition at $v = 0$ must be satisfied in (61):

$$C^+ - C^- = \frac{\sigma m n_n}{\alpha} \int_{-\infty}^{\infty} f_1(u) |u| du - \frac{\beta}{\alpha} n_0 \sqrt{\frac{2}{\pi}} \sqrt{\frac{\sigma m n_n}{\alpha}}. \quad (63)$$

No returning ions, $C^- = 0$, and the application of (63) to (62) yields

$$C^+ = -n_0 (\beta/\alpha) \sqrt{2/\pi} \sqrt{\sigma m n_n / \alpha}. \quad (64)$$

The collisional presheath-collisionless sheath boundary ΔU^* is again

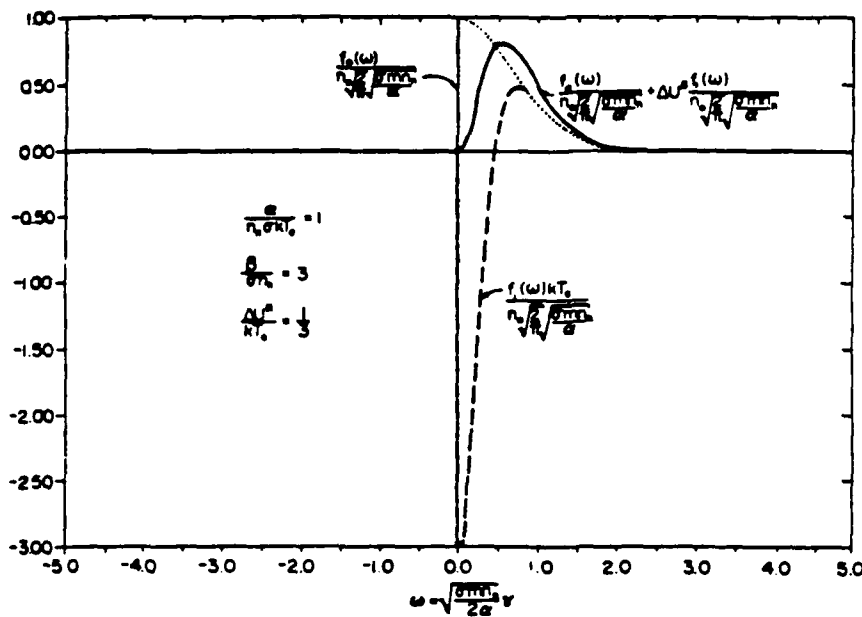


FIG. 6. Constant cross section ion distribution with cold neutrals.

$$0 = f(0^+) = f_0(0^+) + \Delta U^* f_1(0^+), \quad (65)$$

which yields

$$\Delta U^* / k T_e = \alpha / \beta k T_e. \quad (66)$$

Equation (62) is integrated to

$$n_1 = \int_{-\infty}^{\infty} f_1(v) dv = \frac{n_0 n_n \sigma}{\alpha} \left(1 - \sqrt{1 + \frac{\beta}{\sigma n_n}} \right) \quad (67)$$

and applied to the Poisson equation (8) to produce

$$\left(\frac{\beta}{\sigma n_n} \right)^2 = \left(\frac{4\pi q^2 n_0}{k T_e} \right)^2 \left(\frac{1}{\sigma n_n} \right)^2 \left[\frac{n_n \sigma k T_e}{\alpha} \left(1 - \sqrt{1 + \frac{\beta}{\sigma n_n}} \right) + 1 \right]. \quad (68)$$

Under the assumption that the Debye length is short compared to the ion mean free path,

$$(4\pi q^2 n_0 / k T_e)^2 (1 / \sigma n_n)^2 \gg 1,$$

Eq. (68) results in

$$\beta / \sigma n_n = \alpha / n_n \sigma k T_e (2 + \alpha / n_n \sigma k T_e) \quad (69)$$

and

$$\Delta U^* / k T_e = 1 / (2 + \alpha / n_n \sigma k T_e). \quad (70)$$

The Bohm criterion is satisfied at ΔU^* to the first order by virtue of (68). And interestingly, the presheath potential rise for $\alpha = 0$ is exactly that required by the cold ion Bohm criterion. Figure 6 presents the results for cold neutrals with $\alpha / n_n \sigma k T_e = 1$. From the ion distribution at ΔU^* , the mean ion velocity into the sheath can be determined to be $\bar{v} = 1.06 \sqrt{k T_e / m_i}$, while the exact solution of Riemann gives $\bar{v} = 1.27 \sqrt{k T_e / m_i}$; thus the first-order asymptotic result appears close.

V. CONCLUSIONS

It has been shown that approximate collisional presheath solutions can be obtained for a variety of collision terms. In particular the constant collision frequency case has been solved approximately, whereas previous attempts at exact solutions have found this case intractable. In addition, it has been shown that higher-order corrections can be made a regular and tractable fashion. Also the return of ions from the collisionless sheath can be treated.

ACKNOWLEDGMENTS

Thanks are due to Gregory Ridderbusch who produced the numerical results. This work was supported by the Air Force Office of Scientific Research Grant No. 85-0375.

APPENDIX: MULTIEXPONENTIAL FORMULATION

In the previous sections we have calculated only the first-order terms in the ion distribution and presheath potential rise. Also, we have implicitly made the same first-order approximation for electrons:

$$n_e = n_0(1 - \Delta U/kT_e). \quad (\text{A1})$$

A complete multiexponential expansion can also be constructed that correctly calculates the second- and higher-order terms. Potential in the presheath is

$$U = U_0 + \Delta U + a_2 \Delta U^2 + a_3 \Delta U^3 + \dots, \quad (\text{A2})$$

where $U_0 = \alpha x$ and $\Delta U = \exp(\beta x)$. Thus

$$\frac{dU}{dx} = \alpha + \beta \Delta U + 2\beta a_2 \Delta U^2 + 3\beta a_3 \Delta U^3 + \dots \quad (\text{A3})$$

and

$$\frac{d(\Delta U)}{dU} = \frac{\beta \Delta U}{\alpha + \beta \Delta U + 2\beta a_2 \Delta U^2 + 3\beta a_3 \Delta U^3 + \dots}, \quad (\text{A4})$$

which transforms the Boltzmann equation

$$\frac{dU}{dx} \left(v \frac{\partial f}{\partial \Delta U}(v) \frac{\partial \Delta U}{\partial U} \pm \frac{1}{m} \frac{\partial f}{\partial v}(v) \right) = \left(\frac{\partial f}{\partial t} \right)_c \quad (\text{A5})$$

into

$$v \beta \Delta U \frac{\partial f}{\partial \Delta U}(v) \pm \frac{1}{m} (\alpha + \beta \Delta U + 2\beta a_2 \Delta U^2 + \dots) \frac{\partial f}{\partial v}(v) = \left(\frac{\partial f}{\partial t} \right)_c, \quad (\text{A6})$$

or

$$1: \pm \frac{\alpha}{m} \frac{\partial f_0}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_1, \quad (\text{A7a})$$

$$\Delta U: v \beta f_1(v) \pm \frac{\beta}{m} \frac{\partial f_0}{\partial v}(v) \pm \frac{\alpha}{m} \frac{\partial f_1}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_{\Delta U}, \quad (\text{A7b})$$

$$\Delta U^2: 2v \beta f_2(v) \pm \frac{2\beta a_2}{m} \frac{\partial f_0}{\partial v}(v) \pm \frac{\beta}{m} \frac{\partial f_1}{\partial v}(v) \pm \frac{\alpha}{m} \frac{\partial f_2}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_{\Delta U^2}, \quad (\text{A7c})$$

:

$$\Delta U^n: n v \beta f_n(v) \pm \frac{n \beta a_n}{m} \frac{\partial f_0}{\partial v}(v) \pm \frac{(n-1) \beta a_{n-1}}{m} \frac{\partial f_1}{\partial v}(v) \pm \dots \pm \frac{\beta}{m} \frac{\partial f_{n-1}}{\partial v}(v) \pm \frac{\alpha}{m} \frac{\partial f_n}{\partial v}(v) = \left[\left(\frac{\partial f}{\partial t} \right)_c \right]_{\Delta U^n}. \quad (\text{A7d})$$

The Poisson equation (8) becomes

$$\begin{aligned} & \beta^2 \Delta U + (2\beta)^2 a_2 \Delta U^2 + (3\beta)^2 a_3 \Delta U^3 + \dots \\ &= 4\pi q^2 \left[\Delta U \left(\int_{-\infty}^{\infty} f_{e1}(v) dv - \int_{-\infty}^{\infty} f_{e1}(v) dv \right) \right. \\ & \quad \left. + \Delta U^2 \left(\int_{-\infty}^{\infty} f_{e2}(v) dv - \int_{-\infty}^{\infty} f_{e2}(v) dv \right) + \dots \right]. \end{aligned} \quad (\text{A8})$$

¹D. Bohm, in *Characteristics of Electrical Discharges in Magnetic Fields*, edited by A. Guthrie and R. Wakering (McGraw-Hill, New York, 1949), p. 77.

²E. R. Harrison and W. B. Thompson, *Proc. Phys. Soc. London* 74, 145 (1959).

³G. Ecker and H. Kanne, *Z. Naturforsch. Teil A* 21, 2027 (1966).

⁴K. U. Riemann, *Phys. Fluids* 24, 2163 (1981).

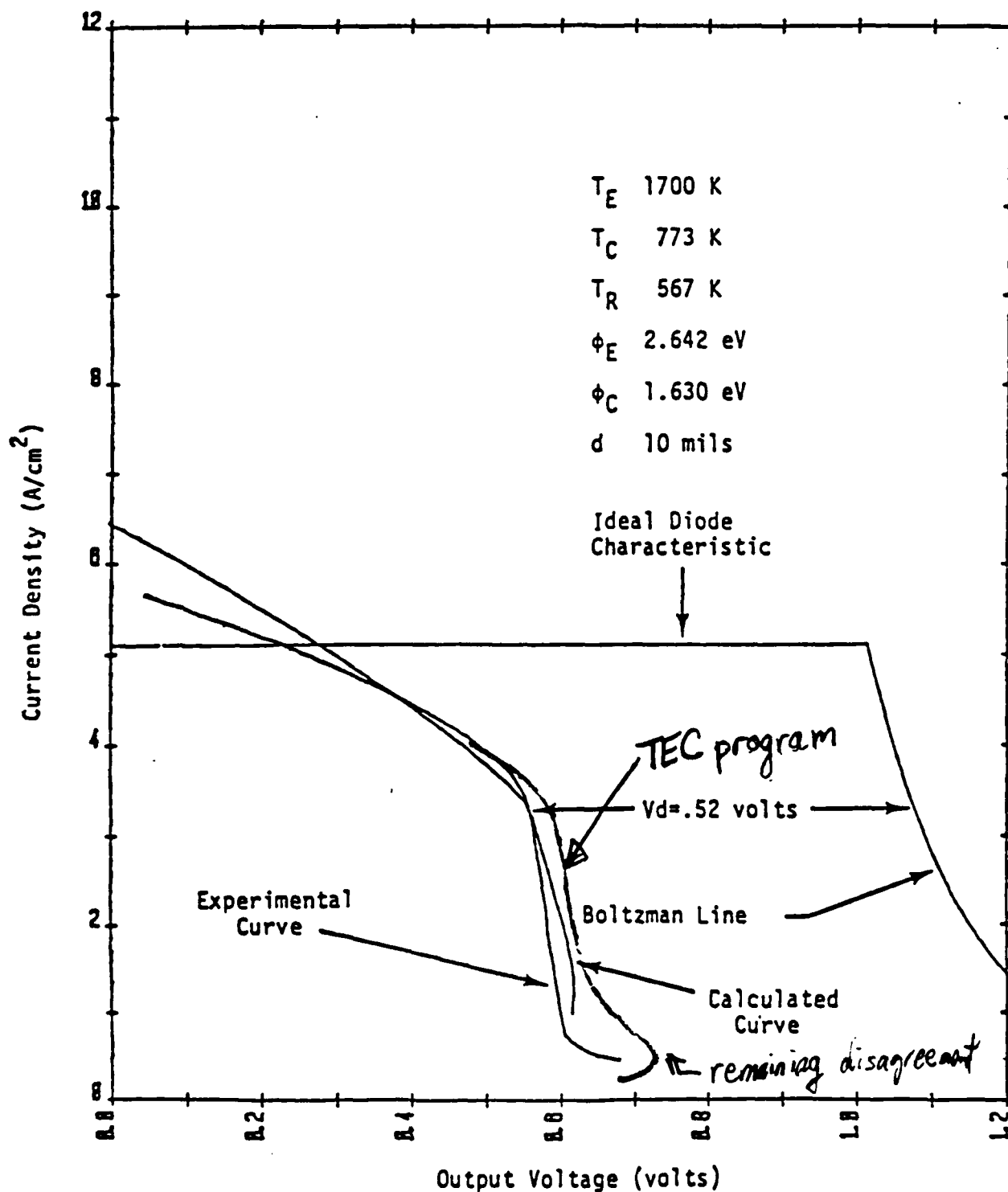
⁵G. A. Emmert, R. M. Wieland, A. T. Mense, and J. N. Davidson, *Phys. Fluids* 23, 803 (1980).

THE TEC PROGRAM RESULTS

The TEC program results shown here incorporate the asymptotic presheath work and give good agreement except at low current density. This disagreement is still not understood.

Comparison of TEC Program Results to Experimental Data

Reference: Advanced Thermionic Technology Program, Vol. 4, Oct. 1984. Thermo Electron Corporation, DOE/ET/11292-2



TEC INITIAL DATA SUMMARY

PHYSICAL OPERATING CONDITIONS-----

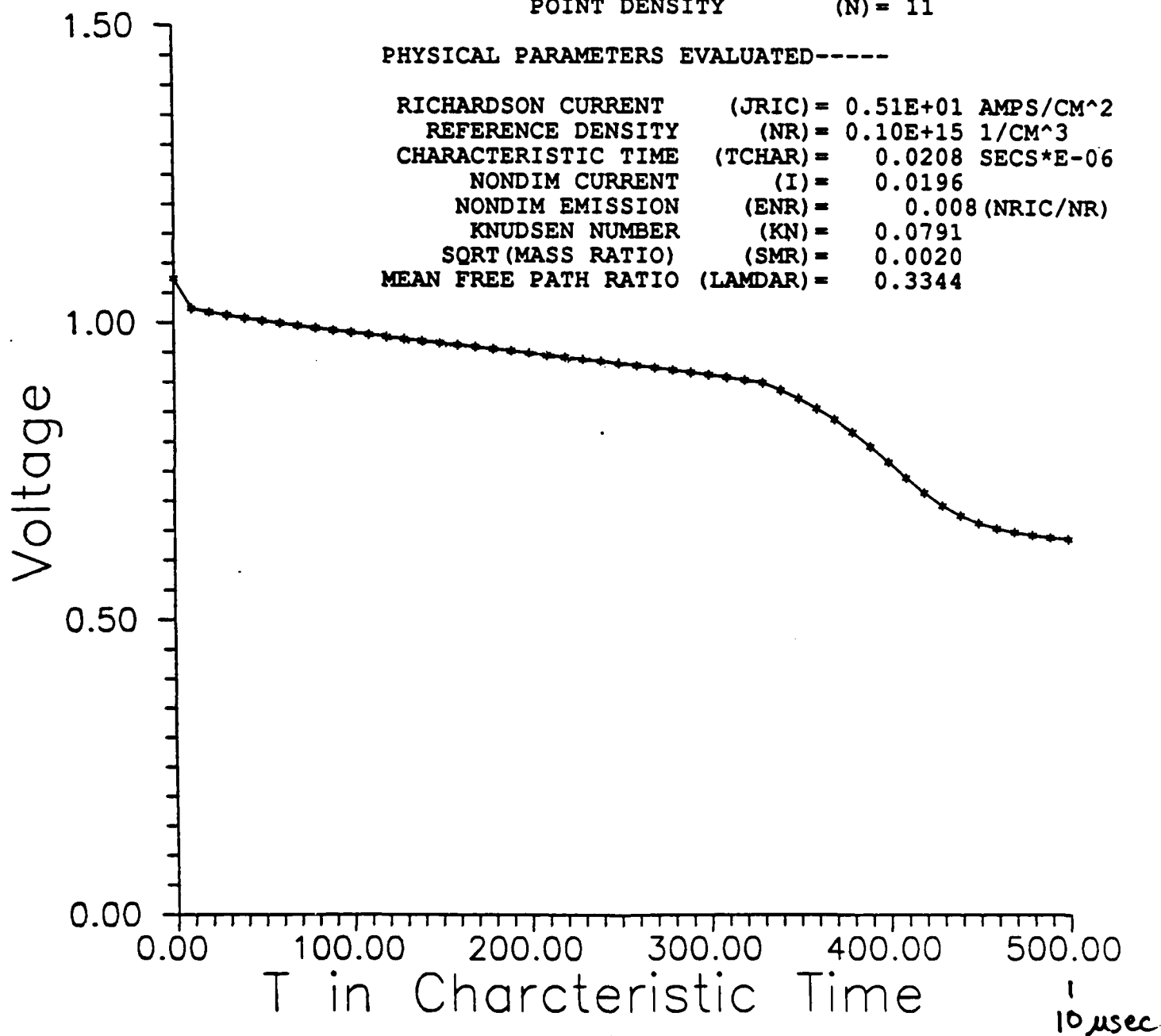
EMITTER TEMPERATURE (TE) = 1700.0 KELVIN
 COLLECTOR TEMPERATURE (TC) = 773.0 KELVIN
 EMITTER WORK FUNCTION (EWF) = 2.642 EV
 COLLECTOR WORK FUNCTION (CWF) = 1.630 EV
 CONVERTOR PRESSURE (PN) = 1.541 TORR
 GAP THICKNESS (D) = 0.254 MM
 OPERATING CURRENT (J) = 2.000 AMPS/CM²

TEC FUNCTION SETTINGS-----

DIAGNOSTIC LEVEL (CHKDOT) = 1
 RESTART SEQUENCE (OFILE) = 0
 POINT DENSITY (N) = 11

PHYSICAL PARAMETERS EVALUATED-----

RICHARDSON CURRENT (JRIC) = 0.51E+01 AMPS/CM²
 REFERENCE DENSITY (NR) = 0.10E+15 1/CM³
 CHARACTERISTIC TIME (TCHAR) = 0.0208 SECS*E-06
 NONDIM CURRENT (I) = 0.0196
 NONDIM EMISSION (ENR) = 0.008 (NRIC/NR)
 KNUDSEN NUMBER (KN) = 0.0791
 SQRT(MASS RATIO) (SMR) = 0.0020
 MEAN FREE PATH RATIO (LAMDAR) = 0.3344



TEC INITIAL DATA SUMMARY

PHYSICAL OPERATING CONDITIONS-----

EMITTER TEMPERATURE (TE)= 1700.0 KELVIN
 COLLECTOR TEMPERATURE (TC)= 773.0 KELVIN
 EMITTER WORK FUNCTION (EWF)= 2.642 EV
 COLLECTOR WORK FUNCTION (CWF)= 1.630 EV
 CONVERTOR PRESSURE (PN)= 1.541 TORR
 GAP THICKNESS (D)= 0.254 MM
 OPERATING CURRENT (J)= 2.000 AMPS/CM^2

TEC FUNCTION SETTINGS-----

DIAGNOSTIC LEVEL (CHKDOT)= 1
 RESTART SEQUENCE (OFILE)= 0
 POINT DENSITY (N)= 11

PHYSICAL PARAMETERS EVALUATED-----

RICHARDSON CURRENT (JRIC)= 0.51E+01 AMPS/CM^2
 REFERENCE DENSITY (NR)= 0.10E+15 1/CM^3
 CHARACTERISTIC TIME (TCHAR)= 0.0208 SECS*E-06
 NONDIM CURRENT (I)= 0.0196
 NONDIM EMISSION (ENR)= 0.008 (NRIC/NR)
 KNUDSEN NUMBER (KN)= 0.0791
 SQRT(MASS RATIO) (SMR)= 0.0020
 MEAN FREE PATH RATIO (LAMDAR)= 0.3344

TIME SETTINGS-----

NSTEPS= 1
 T2= 500.0
 DELTAT= 1.000
 DTP= 1.000
 LSF= 10

RESULTS AT TIME = 0.00 OPERATING VOLTAGE= 1.074

ENE = 0.027 ECHI= 6.241 EALPHA= 0.460
 CNE = 0.000 CCHI= 6.734 CALPHA= 0.482
 PHIB= 0.000 VD = 0.422 EMISS =.268E-01

#	NDOT (#)	NEB (#)	TDOT (#)	TAU (#)
0	0.0015	-0.154	-0.0526	1.52
1	-0.0151	0.298	-0.0537	1.52
2	-0.0158	0.661	-0.0555	1.51
3	-0.0141	0.943	-0.0569	1.51
4	-0.0122	1.145	-0.0582	1.50
5	-0.0104	1.267	-0.0594	1.50
6	-0.0088	1.309	-0.0608	1.50
7	-0.0072	1.271	-0.0623	1.49
8	-0.0058	1.153	-0.0641	1.49
9	-0.0050	0.953	-0.0665	1.48
10	-0.0083	0.670	-0.0698	1.47
11	-0.0340	0.270	-0.0768	1.45

12 -0.0704 -0.551 -0.0807 1.43

RESULTS AT TIME = 100.00 OPERATING VOLTAGE= 0.982

ENE = 0.098 ECHI= 3.183 EALPHA= 0.617
CNE = 0.000 CCHI= 3.069 CALPHA= 0.719
PHIB= 0.000 VD = -0.203 EMISS =.981E-01

#	NDOT (#)	NEB (#)	TDOT (#)	TAU (#)
0	0.0003	-0.035	0.0001	1.14
1	-0.0007	0.081	0.0001	1.13
2	-0.0018	0.200	0.0000	1.11
3	-0.0028	0.316	-0.0001	1.10
4	-0.0037	0.419	-0.0001	1.09
5	-0.0043	0.501	-0.0002	1.08
6	-0.0047	0.552	-0.0003	1.07
7	-0.0046	0.562	-0.0003	1.06
8	-0.0043	0.524	-0.0004	1.05
9	-0.0035	0.431	-0.0005	1.03
10	-0.0022	0.281	-0.0006	1.01
11	-0.0006	0.074	-0.0008	0.97
12	0.0013	-0.170	-0.0009	0.95

RESULTS AT TIME = 200.00 OPERATING VOLTAGE= 0.946

ENE = 0.232 ECHI= 2.324 EALPHA= 0.587
CNE = 0.000 CCHI= 2.167 CALPHA= 0.750
PHIB= 0.000 VD = -0.448 EMISS =.232E+00

#	NDOT (#)	NEB (#)	TDOT (#)	TAU (#)
0	0.0001	-0.014	0.0006	1.19
1	-0.0003	0.034	0.0008	1.19
2	-0.0007	0.084	0.0008	1.17
3	-0.0011	0.134	0.0008	1.15
4	-0.0015	0.179	0.0007	1.13
5	-0.0018	0.216	0.0006	1.11
6	-0.0020	0.240	0.0005	1.09
7	-0.0020	0.247	0.0005	1.08
8	-0.0019	0.232	0.0004	1.06
9	-0.0016	0.193	0.0002	1.03
10	-0.0010	0.127	0.0001	1.00
11	-0.0003	0.033	-0.0002	0.93
12	0.0006	-0.081	-0.0003	0.90

RESULTS AT TIME = 300.00 OPERATING VOLTAGE= 0.910

ENE = 0.526 ECHI= 1.440 EALPHA= 0.551
CNE = 0.000 CCHI= 1.374 CALPHA= 0.754
PHIB= 0.000 VD = -0.698 EMISS =.526E+00

#	NDOT (#)	NEB (#)	TDOT (#)	TAU (#)
0	0.0001	-0.006	-0.0001	1.23
1	-0.0001	0.015	0.0007	1.27
2	-0.0003	0.036	0.0012	1.27

3	-0.0005	0.057	0.0013	1.25
4	-0.0007	0.077	0.0013	1.22
5	-0.0008	0.093	0.0012	1.20
6	-0.0009	0.104	0.0012	1.17
7	-0.0009	0.107	0.0011	1.15
8	-0.0009	0.101	0.0009	1.11
9	-0.0007	0.085	0.0008	1.07
10	-0.0005	0.056	0.0006	1.02
11	-0.0001	0.014	0.0003	0.93
12	0.0003	-0.038	0.0006	0.90

RESULTS AT TIME = 400.00 OPERATING VOLTAGE= 0.763

ENE =	0.879	ECHI=	1.392	EALPHA=	0.420
CNE =	0.000	CCHI=	0.914	CALPHA=	0.541
PHIB=	0.264	VD =	-1.960	EMISS =	.114E+01

#	NDOT (#)	NEB (#)	TDOT (#)	TAU (#)
0	0.0000	-0.002	0.0037	1.46
1	0.0000	0.007	0.0061	1.66
2	-0.0001	0.015	0.0077	1.76
3	-0.0002	0.024	0.0081	1.77
4	-0.0003	0.032	0.0082	1.75
5	-0.0003	0.038	0.0082	1.72
6	-0.0004	0.042	0.0081	1.68
7	-0.0004	0.043	0.0079	1.63
8	-0.0004	0.041	0.0076	1.58
9	-0.0003	0.034	0.0072	1.51
10	-0.0002	0.022	0.0068	1.42
11	-0.0001	0.006	0.0066	1.29
12	0.0002	-0.015	0.0086	1.35

RESULTS AT TIME = 500.00 OPERATING VOLTAGE= 0.632

ENE =	1.001	ECHI=	1.516	EALPHA=	0.371
CNE =	0.000	CCHI=	0.348	CALPHA=	0.433
PHIB=	0.352	VD =	-2.945	EMISS =	.142E+01

#	NDOT (#)	NEB (#)	TDOT (#)	TAU (#)
0	0.0000	-0.002	0.0001	1.59
1	0.0000	0.006	0.0002	1.88
2	0.0000	0.012	0.0003	2.04
3	0.0000	0.019	0.0003	2.06
4	0.0000	0.024	0.0003	2.05
5	0.0000	0.029	0.0003	2.02
6	0.0000	0.031	0.0003	1.98
7	0.0000	0.030	0.0003	1.93
8	0.0000	0.027	0.0003	1.87
9	0.0000	0.021	0.0004	1.79
10	0.0000	0.013	0.0004	1.69
11	0.0000	0.003	0.0008	1.61
12	0.0000	-0.007	0.0019	1.90

PAPERS AND PUBLICATIONS

1. The paper entitled "Asymptotically Correct Collisional Presheaths," by G L. Main, Phys. Fluids, June 1987, has been produced under this grant.
- 2 "Effects of Emitter Sheath Ion Reflection and Trapped Ions on Thermionic Converter Performance Using an Isothermal Electron Model" by G. L. Main and S. H. Lam, IEEE Transactions on Plasma Science, June 1987.
- 3 "A Uniform Three Scale Asymptotic Solution for a Collisional Presheath and Collisionless Sheath with Ion Reflection," by G. L. Main and G. L. Ridderbusch is to appear in IEEE Trans. on Plasma Science, and has been produced under this grant.

APPENDIX A - Fokker Planck Collisions Presheath

This theory has been developed under this grant and is found to be applicable to fully ionized plasmas but was not incorporated into the Thermionic Converter work due to its computational complexity.

**AN ANALYTIC - NUMERICAL SCHEME FOR A COLLISIONAL
FOKKER - PLANCK TIME DEPENDENT SHEATH - PRESHEATH
STRUCTURE**

**A THESIS
Presented to
The Faculty of the Division of Graduate Studies
By
Jeffrey Paul Dansereau**

**In Partial Fulfillment
of the Requirements for the Degree
Master of Science in Mechanical Engineering**

**Georgia Institute of Technology
September, 1987**

AN ANALYTIC - NUMERICAL SCHEME FOR A COLLISIONAL
FOKKER - PLANCK TIME DEPENDENT SHEATH - PRESHEATH
STRUCTURE

Approved:

Geoffrey L. Main, Chairman

J. Narl Davidson

Thomas L. Eddy

Date approved by chairman _____

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TABLE OF CONTENTS

Title Page	i
Thesis Approval Page	ii
Acknowledgments	iii
Table of Contents	iv
List of Figures	v
Nomenclature	vi
Summary	viii
1. Introduction	1
2. Background	3
3. Model Formulation	5
3.1 Concepts	5
3.2 Wall Region Model	7
3.3 Presheath Model	9
3.3.1 Equations Describing the Collective Behavior of a Plasma	9
3.3.2 Solution Conditions	11
3.3.3 Expansion of the Boltzmann Equation	12
3.3.4 Expansion of the Poisson Equation	15
3.3.5 Expansion of the Fokker - Planck Term	16
3.3.6 Solution Approach	19
4. Numerical Technique	21
4.1 Problem Approach	21
4.2 Numerical Integration, Differentiation, and Matrix Inversion	24
4.2.1 Numerical Integration	25
4.2.2 Numerical Differentiation	25
4.2.3 Matrix Inversion	26
4.3 Obtaining a Solution	27
4.3.1 Initial Distribution	27
4.3.2 Instability Damping	27
4.4 Program Structure	28
5. Results	31
6. Conclusions	35
References	37
Figures	38
Appendix: Program Listing	55

LIST OF FIGURES

3.1 Debye Shielding	38
3.2 Wall Potential	38
3.3 Wall Region Model	39
3.4 Coordinate System in Velocity Space	40
3.5 Radial, Symmetric, and No Returning Ions Conditions	41
4.1 Program Diagram	42
5.1 Zero Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-4}$	43
5.2 First Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-4}$	44
5.3 Total Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-4}$	45
5.4 Zero Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-3}$	46
5.5 First Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-3}$	47
5.6 Total Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-3}$	48
5.7 Zero Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-5}$	49
5.8 First Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-5}$	50
5.9 Total Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-5}$	51
5.10 Time Dependent Position of the Potential	52
5.11 Potential Structure of the Presheath	53
5.12 Time Dependent Structure of the Sheath Height	54

NOMENCLATURE

- a - Inverse square of the particle thermal velocity
- $a_1, a_2, \dots$ - Coefficients of the potential structure
- a, b - Integral limits
- A - First derived Fokker Planck collision function
- B - Second derived Fokker Planck collision function
- $d_i(r)$ - An $m \times 1$ matrix
- $D(r)$ - An $m \times 1$ solution matrix
- e - Electron charge
- E - Electric field strength
- f - Particle distribution function in velocity space
- F - Nondimensional particle distribution function in velocity space
- g - Collision function
- h - Grid spacing width
- k - Boltzmann's constant
- L - System dimension
- m - Number of points in velocity space
- m - Particle mass
- M - Reduced mass
- n - Plasma density
- n_R - Reference density
- q - Elementary charge
- R - Radial velocity component
- t - Time
- T_i - Ion temperature
- T_e - Electron temperature
- $T(r)$ - An $m \times m$ matrix
- U - Potential
- $\mathbf{v}$ - Velocity vector

$u_i(r)$ - An $m \times 1$ matrix
 $V(r)$ - An $m \times 1$ solution matrix
 x - Position vector
 x - Axial position component
 z - Axial velocity component
 Z - Ionization level
 Z - Nondimensional axial velocity component
 α - Potential gradient across the plasma
 β - Exponential coefficient of the presheath rise
 Γ - Fokker - Planck coefficient
 ΔU - Potential expansion parameter
 ϵ_0 - Permittivity of free space
 ζ, η, ξ - Variables of integration
 θ - Velocity rotation angle in cylindrical coordinates
 λ_D - Debye length
 λ_i - Mean free path
 Λ - Coulomb logarithm
 τ - Nondimensional time
 Φ - Electric potential
 φ - Nondimensional coefficients of the potential structure

Subscripts:

c - Collision term
 e - Electron
 i - Ion
 n - Order of expansion

Superscripts:

i - Particle species with which collisions occur
 $\bullet$ - Nondimensional

SUMMARY

The Maxwellian sources and charge exchange terms used to model particle interactions in current presheath models do not represent the Coulomb collisions taking place in fully ionized plasmas. These models approximate the collisional effects in the presheaths of partially ionized plasmas but are used to implicitly extrapolate the interesting case of fully ionized plasmas. The present study uses a Fokker - Planck collision term which models the limit of the small angle Coulomb collisions that occur in fully ionized plasmas. Normally these small angle collisions dominate the particle interactions of fully ionized plasmas. The Boltzmann equation coupled with the Fokker - Planck term, and the Poisson equation have been expanded using an exponential asymptotic technique. These equations have been solved numerically to determine the time dependent evolution of the presheath. The results presented show the presheath potential structure and particle distribution in velocity space. The model produces a self-consistent and accurate potential structure. The particle velocity distribution in the presheath has the correct acceleration of ions toward the wall but because the Fokker - Planck collision term only models the limit of small angle collisions it is unable to clear the particle distribution of returning ions. The collisional processes become dominated by the effects of the large angle collisions as the Debye sheath edge is approached. This study has found that a presheath model which describes the Coulomb collisions occurring in a fully ionized plasma must account for both the small angle and the large angle particle collisions to explain the clearing out of returning ions that must exist for the transition to an absorbing wall.

CHAPTER I

INTRODUCTION

The interaction of man and plasma, in some form, exists at almost all levels of society. A plasma is an ionized gas that has a collective behavior in an electromagnetic field. Plasmas exist in everyday devices like fluorescent lights, neon signs, and electric arc welders. An understanding of the basic behavior and interaction of plasmas is essential to the advancement of all current plasma applications and to the discovery of new applications. This thesis involves the study of how a plasma interacts with the walls and surfaces with which it comes in contact.

Why is it important to understand plasma - wall interactions? Two basic reasons answer this question. First, a plasma has a strong effect on any surfaces it comes in contact with. The high temperature plasma can erode or destroy any surface quickly pitting and changing a wall which may need to maintain a particular profile or surface condition. Secondly, the wall affects the characteristics of the plasma. A surface can have a profound effect on the plasma depending on the amount and rate at which it can absorb energy. Examples of situations in which plasma - wall interactions are of importance include:

- Diverter plates in magnetic confinement fusion reactors.
- The rails in a plasma rail gun.
- Any body (like the space shuttle) upon reentry to the atmosphere.
- Plasma switches.
- Plasma etching.

- Almost every other use or occurrence of plasmas.

This study is primarily applicable to fully ionized plasmas. The hot temperatures necessary to produce fully ionized plasmas occur only in situations like on the surfaces of diverter plates in Tokamak fusion reactors.

The development of a mathematical model to represent the plasma - wall interaction region, or sheath, and a numerical solution to this model is the focus of this thesis. An understanding of the interaction between the plasma and the wall is achieved with a time dependent solution to the sheath region. If the potential structure and the particle velocity distributions are known for every location in the sheath then the energy going into the surface can be determined. In this way the results of this study can be used as a boundary condition for problems involving plasma characteristics and for problems involving the surface physics of plasma devices.

CHAPTER II

BACKGROUND

A plasma will naturally maintain itself in a neutral and field free state. Application of forces and processes that try to alter the equilibrium are resisted by the plasma. A surface within a plasma that is not at the same potential as the plasma will be shielded from the remainder of the plasma by a sheath. The outer edge of this sheath is nearly at the plasma potential. Bohm^[1] first came up with a criterion to determine the extent of the sheath. Bohm modeled the sheath region as completely collisionless. He also considered that the transition region from this collisionless sheath to the plasma was too small to be important.

More recent work has been done to describe this transition, or presheath, region. Self^[2] has an exact solution to the sheath equation and has shown that the collisionless sheath makes a transition directly to the neutral plasma in the limit as $\frac{\lambda_D}{L} \rightarrow 0$, where λ_D is the Debye length and L is the plasma dimension. Emmert et al.^[3] has determined a presheath structure based on the assumption of a Maxwellian source of ions to model the particle collisions. The solution to this model shows that the transition point from the sheath to the presheath has a finite electric field strength. Bissell and Johnson^[4] have performed a similar solution using a Maxwellian source of ions. In contrast to Emmert et al., Bissell and Johnson have found that the electric field strength becomes infinite at the sheath edge. This solution agrees with the fluid and cold ion models. In a recent paper Bissell^[5] shows that Emmert obtained a finite electric field strength because the Maxwellian source term used produced no ions at the point of zero velocity. Bissell and Johnson used a more realistic

Maxwellian source that produced ions at the zero point in velocity space for their solution.

Another approach to the problem involves the use of a charge exchange term to model the particle collisions. Riemann^[6] has produced results using this technique. In a recent paper by Main^[7] a charge exchange model is used to obtain a solution to the presheath potential structure and particle distribution. This model involves an asymptotic approximation of the plasma equations. The Boltzmann and Poisson equations are asymptotically expanded and then solved analytically when combined with a charge exchange model of the particle collisions.

All of these sheath and presheath solutions have modeled particle collisions by large instantaneous changes in particle velocity. These models do not represent the Coulomb collisions occurring in the presheath of a fully ionized plasma.

The current study extends the asymptotic solution presented by Main^[7] to include a Fokker - Planck collision term instead of the charge exchange term. Unlike the previous collision terms used, the Fokker - Planck term describes the Coulomb collisions that exist within a fully ionized plasma. The addition of the Fokker - Planck term necessitates the use of numerical techniques, rather than analytical techniques, to obtain a solution. In using the Fokker - Planck term the collision processes are being modeled directly. The model developed obtains the time dependent evolution of the presheath for a fully ionized plasma.

CHAPTER III

MODEL FORMULATION

3.1 Concepts

In order to have a complete understanding of the problem at hand certain concepts need to be presented which will help in understanding the overall structure of the model.

1) Debye Length (λ_D) - The shielding distance beyond which the particle charge effect is weak. This is the natural charge separation distance. Negatively charged particles become surrounded by positively charged particles and vice versa, thus, balancing the overall charge at any point (see figure 3.1). There is a point beyond which a particle is not effected by the specific charge but responds to the influence of the entire plasma. The thermal effects in the plasma become dominant over the electric field strength.

2) Mean Free Path (λ_i) - The average distance a particle travels before its trajectory has been altered by ninety degrees. The mean free path is a function of the density of the plasma. The denser the plasma the shorter the mean free path. For the plasma under consideration in this study $\lambda_i \gg \lambda_D$.

3) The coordinate system used to describe the plasma - The coordinate system used in the model is known phase space. In this system any point is described using three position coordinates and three velocity coordinates. Any orthogonal coordinate system, cartesian, cylindrical, spherical, can be used to describe both the position and the velocity components.

4) Distributions and Distribution Functions - Plasmas are studied in a collective sense. The motion of the entire plasma and not individual particles is described by the model. Therefore, the velocity of the plasma at any given location must be described by a distribution. The distribution function describes the overall particle velocity distribution.

5) Potential - In a plasma the wall potential is greater than the neutral plasma potential. The lighter, thus, faster electrons are absorbed by the wall faster than the heavier and slower ions. A net positive charge exists near the wall, increasing the potential (see figure 3.2). The potential at the physical interface between the wall and the plasma is dependent on the rate at which ions are absorbed by the surface. In this study $U = -e\Phi$ where e is the electron charge and Φ is electric potential in electron volts so that U has units of energy. The addition of the negative sign defines potential in the reverse of the usual sign convention so that increasing potential repels electrons.

6) Collision Possibilities using the Fokker - Planck Collision term - To describe the overall structure of the sheath the various collision possibilities must be included in a comprehensive model. The Fokker - Planck term describes the four major collision possibilities.

- 1) Ion - Ion
- 2) Ion - Electron
- 3) Electron - Ion
- 4) Electron - Electron

The collision model does not take into account three body collisions. Three body collisions are very rare, as such, the model is not hampered by the lack of

terms to describe these collisions.

3.2 Wall Region Model

The model of the Plasma - Wall region can be broken into three areas.

1) Neutral Plasma Region ($O(L)$) - The neutral plasma region represents the majority of the system and can be considered to have a physical width that is on the order of the overall dimension of the system, L . This region is considered to be fully collisional. The velocity distribution is near Maxwellian and as such can be modeled by fluid type equations (see figure 3.3).

2) Debye Sheath Region ($O(\lambda_D)$) - This region is a very thin area directly adjacent to the wall. Its width is considered to be on the order of a Debye length and since $\lambda_i \gg \lambda_D$ no collisions are expected in this region. This collisionless sheath was first modeled by Langmuir^[8] and Bohm^[1] and is considered very well known and understood.

3) Collisional Presheath Region ($O(\lambda_i)$) - This is a transition region between the collisional neutral plasma and the collisionless Debye sheath region. It is considered to have a physical width on the order of a mean free path. Therefore, collisions are expected but at the same time the region cannot be considered fully collisional.

The potential must transition from a lower level in the neutral plasma to a higher level at the wall. The goal of this study has been to obtain a time dependent model of the evolution of the presheath region which asymptotically approaches the known potential in both the neutral plasma and in the Debye sheath region.

In order to show the validity of the three region model an example of Debye sheath width in relation to the overall wall region is appropriate. For this example

average hydrogen fusion plasma characteristics have been assumed:

$$T_i = 10^5 K$$

$$n_0 = 10^{20} m^{-3}$$

If the Debye length within this plasma is calculated an order of magnitude value for the Debye sheath width is determined. An appropriate equation for the Debye length in meters is:^[9]

$$\lambda_D = 69 \left(\frac{T_i}{n_0} \right)^{\frac{1}{2}} \quad (3.1)$$

From this equation:

$$\lambda_D = 2.18 \times 10^{-6} m$$

The overall sheath width is on the order of a mean free path. An appropriate equation for the mean free path in meters is:^[10]

$$\lambda_i = 1.2 \times 10^{-4} \frac{1}{Z^2} \left(\frac{T_i}{e} \right)^2 \left(\frac{n_i}{10^{20}} \right)^{-1} \quad (3.2)$$

For a singly ionized plasma $Z = 1$. Using this equation and the above example plasma characteristics the mean free path can be calculated.

$$\lambda_i = 1.14 \times 10^{-2} m$$

This is an order of magnitude estimate value for the width of the entire sheath region. Since the Debye sheath width is on the order of a Debye length it can be seen that the collisionless sheath is very thin in comparison with the entire wall region.

In order to obtain an idea of the importance of the electric field in the wall region an order of magnitude analysis is useful. The magnitude of the electric field is proportional to the thermal energy per length scale.

$$E \sim \frac{kT_i}{x} \quad (3.3)$$

In the sheath region the length scale is the Debye length.

$$E \sim \frac{kT_i}{\lambda_D} \quad (3.4)$$

Therefore, in this region the electric field is very significant since λ_D is very small. The collisional effects are small in comparison, and can be neglected.

In the presheath region the length scale is the mean free path.

$$E \sim \frac{kT_i}{\lambda_i} \quad (3.5)$$

Therefore, the electric field strength is on the order of the collisional effects making both important factors within this region.

In the neutral plasma region the length scale is the overall system dimension.

$$E \sim \frac{kT_i}{L} \quad (3.6)$$

Therefore, the electric field is very weak and can be neglected in comparison with the collisional effects.

3.3 Presheath Model

3.3.1 Equations Describing the Collective Behavior of a Plasma

The primary equation used to describe the behavior of a plasma is the Boltzmann equation. The Boltzmann equation represents the collective motion of many charged particles moving in an electromagnetic field^[11].

$$\frac{\partial f}{\partial t} + v \frac{\partial f}{\partial x} \pm \frac{1}{m} \frac{\partial U}{\partial x} \frac{\partial f}{\partial v} = \left\{ \frac{\partial f}{\partial t} \right\}_c \quad (3.7)$$

Where the + sign is for ion particles and the - sign is for electrons. In the Boltzmann equation f is the particle distribution function, and is defined such that $n = \int_{-\infty}^{\infty} f dv$.

The quantity t is time, v is a velocity vector, x is a position vector, m is the particle mass, and U is the potential. The term on the right hand side represents particle collisions and can take on various forms depending on the model being used.

Another important equation in describing the behavior of a plasma is the Poisson equation. The Poisson equation is the elementary definition of potential as the collective effect of charged particles on a point^[7].

$$\frac{d^2 U}{dx^2} = 4\pi q^2 \left[\int_{-\infty}^{\infty} f_i(v, \Delta U) dv - \int_{-\infty}^{\infty} f_e(v, \Delta U) dv \right] \quad (3.8)$$

Where q is the elementary charge, the subscript i refers to ions and the subscript e refers to electrons. The term in brackets is the ion - electron density difference. The potential is the driving force in the Boltzmann equation. The Poisson equation relates the potential to the particle distribution.

To complete the set of equations necessary for a full description of the presheath a collision term must be chosen to model the particle interactions. This study uses the Fokker - Planck collision term to model the particle collisions. The Fokker - Planck term represents the right hand side of the Boltzmann equation^[11].

$$\left\{ \frac{\partial f}{\partial t} \right\}_e = \Gamma \left[- \frac{\partial}{\partial v_i} \left(f \frac{m}{2M} \frac{\partial}{\partial v_i} \nabla^2 g \right) + \frac{1}{2} \frac{\partial^2}{\partial v_i \partial v_k} \left(f \frac{\partial^2 g}{\partial v_i \partial v_k} \right) \right] \quad (3.9)$$

Where,

$$\Gamma = \frac{q^2 q'^2 \ln \Lambda}{4\pi \epsilon_0^2 m^2} \quad (3.10)$$

$$g(v) = \int f(v') |v - v'| dv' \quad (3.11)$$

$$M = \frac{mm'}{m + m'} \quad (3.12)$$

Where M is called the reduced mass. No superscript refers to the particle species undergoing the collisions and the superscript i refers to the particle species with which the collision occurs.

The Fokker - Planck equation describes the Coulomb collision between two charged particles. Certain restrictions and assumptions are made when using the Fokker - Planck collision term. First, it best describes fully ionized plasmas. The collision term models charged particle interaction and is most accurate for plasmas with few neutrals. This situation occurs only on the hottest of plasma surfaces like the diverter plates in Tokamak fusion reactors.

The second restriction involves the type of collisions that the Fokker - Planck term models. The overwhelming majority of particle collisions lead to only small deflections in the particle trajectories. The Fokker - Planck term describes the limit of these small angle deflections. Finally, the model does not take into account three body, and higher order, collisions.

3.3.2 Solution Conditions

The three equations presented in the previous section in conjunction with the asymptotic forms of potential and velocity distribution provide the necessary information to determine the presheath structure if two additional conditions are met.

First, if the equations are written in cylindrical coordinates the particle velocity distribution is axially symmetric. There is no θ , dependence of the velocity distribution. Cylindrical coordinates are used for both the velocity and the position. The 'z' direction is perpendicular to the wall (see Figure 3.4) with the positive direction being defined into the wall. The coordinates R, θ, z have been used in velocity space for convenience.

The second condition for a solution to these equations involves an assumption of the particle velocity distribution parallel to the surface. For this model the radial velocity distribution has been assumed to take the form of a Maxwellian distribution. In addition, the temperature in the radial direction has been assumed

to be uniform and constant at all ' x ' locations. Thus, the radial velocity distribution is constant for any position. Figure 3.5 is a schematic of these conditions. Note that at any ' x ' location and rotation angle, θ , the radial velocity distribution is constant and follows a Maxwellian distribution. This represents the conditions of uniform temperature and axial symmetry, throughout the wall region. Figure 3.5 also shows a representation of the point of no returning ions. This is the point where the presheath transitions to the collisionless sheath.

The conditions of uniform temperature and radial Maxwellian distribution although good approximations are not exact models of the real situation.

The overall problem reduces to one dimension, the z direction, with the above conditions. The θ dependence having been removed by the axial symmetry and the radial dependence having been removed by the Maxwellian assumption. This one dimensional problem can be solved by straight forward numerical techniques.

3.3.3 Expansion of the Boltzmann Equation

The presheath model involves the expansion of the potential and velocity into asymptotic approximations. The potential is assumed to follow an exponential asymptotic form.

$$U = U_0 + a_1 \Delta U + a_2 \Delta U^2 + \dots \quad (3.13)$$

where

$$U_0 = \alpha z \quad \text{and} \quad \Delta U = e^{\beta z} \quad (3.14)$$

$a_1, a_2, \dots$ are parameters which describe the potential structure. Alpha, α , is non-zero for a non-zero potential gradient in the neutral plasma. ΔU is called the potential expansion parameter.

The particle distribution in velocity space is a function of potential and can be

similarly expanded.

$$f(v, \Delta U) = f_0(v) + \Delta U f_1(v) + \Delta U^2 f_2(v) + \dots \quad (3.15)$$

The Boltzmann equation can be written as

$$\frac{\partial f}{\partial t} + v \frac{\partial f}{\partial(\Delta U)} \frac{\partial(\Delta U)}{\partial x} \pm \frac{1}{m} \frac{\partial U}{\partial x} \frac{\partial f}{\partial v} = \left\{ \frac{\partial f}{\partial t} \right\}_c \quad (3.16)$$

where $\pm$ sign is respectively positive for ion particles and negative for electrons. The potential U has units of energy and is defined as shown in figure 3.3 such that $U = -e\Phi$ where Φ is electric potential. The Boltzmann equation can be expanded using equations 3.13 and 3.14. In addition since the solution is one dimensional in velocity space the velocity derivatives reflect only the 'x' direction. The following expansions are used.

$$\frac{\partial f}{\partial t} = \frac{\partial f_0}{\partial t} + \Delta U \frac{\partial f_1}{\partial t} + \Delta U^2 \frac{\partial f_2}{\partial t} + \dots \quad (3.17)$$

$$\frac{\partial f}{\partial(\Delta U)} = f_1 + 2\Delta U f_2 + 3\Delta U^2 f_3 + \dots \quad (3.18)$$

$$\frac{\partial(\Delta U)}{\partial x} = \beta \Delta U \quad (3.19)$$

$$\frac{\partial U}{\partial x} = \alpha + \beta a_1 \Delta U + 2\beta a_2 \Delta U^2 + 3\beta a_3 \Delta U^3 + \dots \quad (3.20)$$

$$\frac{\partial f}{\partial x} = \frac{\partial f_0}{\partial x} + \Delta U \frac{\partial f_1}{\partial x} + \Delta U^2 \frac{\partial f_2}{\partial x} + \dots \quad (3.21)$$

Using these expansions the Boltzmann equation can be broken down by order in ΔU assuming the collision term can be likewise broken down:

$$1: \frac{\partial f_0}{\partial t} \pm \frac{\alpha}{m} \frac{\partial f_0}{\partial x} = \left[\left\{ \frac{\partial f}{\partial t} \right\}_c \right]_1 \quad (3.22a)$$

$$\Delta U: \frac{\partial f_1}{\partial t} + \beta x f_1 \pm \frac{\alpha}{m} \frac{\partial f_1}{\partial x} \pm \frac{\beta a_1}{m} \frac{\partial f_0}{\partial x} = \left[\left\{ \frac{\partial f}{\partial t} \right\}_c \right]_{\Delta U} \quad (3.22b)$$

$$\Delta U^2: \frac{\partial f_2}{\partial t} + 2\beta x f_2 \pm \frac{\alpha}{m} \frac{\partial f_2}{\partial x} \pm \frac{\beta a_1}{m} \frac{\partial f_1}{\partial x} \pm \frac{2\beta a_2}{m} \frac{\partial f_0}{\partial x} = \left[\left\{ \frac{\partial f}{\partial t} \right\}_c \right]_{\Delta U^2} \quad (3.22c)$$

⋮

$$\begin{aligned} \Delta U^n: & \frac{\partial f_n}{\partial t} + n\beta x f_n \pm \frac{\alpha}{m} \frac{\partial f_n}{\partial x} \pm \frac{\beta a_1}{m} \frac{\partial f_{n-1}}{\partial x} \pm \frac{2\beta a_2}{m} \frac{\partial f_{n-2}}{\partial x} \pm \\ & \dots \pm \frac{(n-1)\beta a_{n-1}}{m} \frac{\partial f_1}{\partial x} \pm \frac{n\beta a_n}{m} \frac{\partial f_0}{\partial x} = \left[\left\{ \frac{\partial f}{\partial t} \right\}_c \right]_{\Delta U^n} \end{aligned} \quad (3.22d)$$

The above exponential expansion is the only known way to break apart the Boltzmann equation. To complete the expansion the Poisson and Fokker - Planck terms must be similarly broken down.

At this point it is appropriate to nondimensionalize the expansion of the Boltzmann equation. The following nondimensional quantities have been used.

$$F_i = \frac{f_i}{n_R a^{3/2}} \quad \text{for } 0 \leq i \leq n \quad (3.23a)$$

$$\tau = \frac{n_R \Gamma}{a^{1/2}} t \quad (3.23b)$$

$$Z = \sqrt{a'} z \quad (3.23c)$$

$$\varphi_{-1} = \frac{\alpha a}{m n_R \Gamma} \quad (3.23d)$$

$$\varphi_0 = \frac{\beta}{n_R \Gamma} \quad (3.23e)$$

$$\varphi_i = \frac{\beta a_i a}{m n_R \Gamma} \quad \text{for } 1 \leq i \leq n \quad (3.23f)$$

Where n_R is a reference density, a and a' are the inverse square of the thermal velocities of the colliding particles, $a = \frac{m}{2kT}$ and $a' = \frac{m'}{2kT'}$. The quantities φ_{-1} through φ_n represent the potential structure of the presheath. F_i is nondimensionalized such that $1 = \int_{-\infty}^{\infty} F dZ$. Using these nondimensionalizations, the expansion of the Boltzmann equations becomes

$$1: \frac{\partial F_0}{\partial \tau} \pm \varphi_{-1} \frac{\partial F_0}{\partial Z} = \left[\left\{ \frac{\partial F}{\partial \tau} \right\}_e \right]_1 \quad (3.24a)$$

$$\Delta U: \frac{\partial F_1}{\partial \tau} + \varphi_0 Z F_1 \pm \varphi_{-1} \frac{\partial F_1}{\partial Z} \pm \varphi_1 \frac{\partial F_0}{\partial Z} = \left[\left\{ \frac{\partial F}{\partial \tau} \right\}_e \right]_{\Delta U} \quad (3.24b)$$

$$\Delta U^2: \frac{\partial F_2}{\partial \tau} + 2\varphi_0 Z F_2 \pm \varphi_{-1} \frac{\partial F_2}{\partial Z} \pm \varphi_1 \frac{\partial F_1}{\partial Z} \pm 2\varphi_2 \frac{\partial F_0}{\partial Z} = \left[\left\{ \frac{\partial F}{\partial \tau} \right\}_e \right]_{\Delta U^2} \quad (3.24c)$$

⋮

$$\begin{aligned} \Delta U^n: & \frac{\partial F_n}{\partial \tau} + n\varphi_0 Z F_n \pm \varphi_{-1} \frac{\partial F_n}{\partial Z} \pm \varphi_1 \frac{\partial F_{n-1}}{\partial Z} \pm 2\varphi_2 \frac{\partial F_{n-2}}{\partial Z} \pm \\ & \dots \pm (n-1)\varphi_{n-1} \frac{\partial F_1}{\partial Z} \pm n\varphi_n \frac{\partial F_0}{\partial Z} = \left[\left\{ \frac{\partial F}{\partial \tau} \right\}_e \right]_{\Delta U^n} \end{aligned} \quad (3.24d)$$

3.3.4 Expansion of the Poisson Equation

The Poisson equation,

$$\frac{d^2 U}{dx^2} = 4\pi q^2 \left[\int_{-\infty}^{\infty} f_i(v, \Delta U) dv - \int_{-\infty}^{\infty} f_e(v, \Delta U) dv \right] \quad (3.8)$$

is broken down using the same technique as the Boltzmann equation. Since:

$$\frac{\partial^2 U}{\partial x^2} = \beta^2 a_1 \Delta U + 4\beta^2 a_2 \Delta U^2 + 9\beta^2 a_3 \Delta U^3 + \dots \quad (3.25)$$

$$\int_{-\infty}^{\infty} f(v, \Delta U) dv = \int_{-\infty}^{\infty} f_0(v) dv + \Delta U \int_{-\infty}^{\infty} f_1(v) dv + \Delta U^2 \int_{-\infty}^{\infty} f_2(v) dv + \dots \quad (3.26)$$

Using these expansions the Poisson equation can be broken down by order in ΔU .

$$1: 0 = 4\pi q^2 \left[\int_{-\infty}^{\infty} f_{i0} dv - \int_{-\infty}^{\infty} f_{e0}(v) dv \right] \quad (3.27a)$$

$$\Delta U: \beta^2 a_1 = 4\pi q^2 \left[\int_{-\infty}^{\infty} f_{i1}(v) dv - \int_{-\infty}^{\infty} f_{e1}(v) dv \right] \quad (3.27b)$$

$$\Delta U^2: 4\beta^2 a_2 = 4\pi q^2 \left[\int_{-\infty}^{\infty} f_{i2}(v) dv - \int_{-\infty}^{\infty} f_{e2}(v) dv \right] \quad (3.27c)$$

⋮

$$\Delta U^n: n^2 \beta^2 a_n = 4\pi q^2 \left[\int_{-\infty}^{\infty} f_{in}(v) dv - \int_{-\infty}^{\infty} f_{en}(v) dv \right] \quad (3.27d)$$

The assumption of Boltzmann electrons is made to enable the numerical calculations to proceed with time steps on the order of an ion characteristic time. In the asymptotic presheath the Boltzmann electron assumption becomes

$$n_e = n_0 e^{-[a_1 \Delta U + a_2 \Delta U^2 + \dots + a_n \Delta U^n] / T_e} \quad (3.28)$$

where n_e is the electron density, T_e is the electron temperature, and n_0 is the electron density in the asymptotic presheath at $\Delta U = 0$. Expansion of (3.28) in terms of ΔU yields

$$\begin{aligned} n_e = & \left[n_0 \right] + \Delta U \left[-\frac{a_1}{kT_e} n_0 \right] + \Delta U^2 \left[\left(-\frac{a_2}{kT_e} + \frac{1}{2} \frac{a_1^2}{(kT_e)^2} \right) n_0 \right] \\ & + \Delta U^3 \left[\left(-\frac{a_3}{kT_e} + \frac{a_1 a_2}{(kT_e)^2} - \frac{1}{6} \frac{a_1^3}{(kT_e)^3} \right) n_0 \right] + \dots \end{aligned} \quad (3.29)$$

With the assumption that $\lambda_D \ll \lambda_i$ the Poisson equation reduces to equating electron and ion densities in order of ΔU . The Poisson and Boltzmann electron equations are nondimensionalized in the same manner as the Boltzmann equation. The nondimensionalized Poisson equation (3.27a-d) is combined with the Boltzmann electron equation (3.28) to become

$$\int_{-\infty}^{\infty} F_0 dZ = \eta e^{(\varphi_1 + \dots + \varphi_n) \frac{1}{\varphi_0} \left(\frac{2T_i}{T_e} \right)} \quad (3.30a)$$

$$\int_{-\infty}^{\infty} F_1 dZ = \eta e^{(\varphi_1 + \dots + \varphi_n) \frac{1}{\varphi_0} \left(\frac{2T_i}{T_e} \right)} \left[-\frac{\varphi_1}{\varphi_0} \left(\frac{2T_i}{T_e} \right) \right] \quad (3.30b)$$

$$\int_{-\infty}^{\infty} F_2 dZ = \eta e^{(\varphi_1 + \dots + \varphi_n) \frac{1}{\varphi_0} \left(\frac{2T_i}{T_e} \right)} \left[-\frac{\varphi_2}{\varphi_0} \left(\frac{2T_i}{T_e} \right) + \frac{1}{2} \left(\frac{\varphi_1}{\varphi_0} \right)^2 \left(\frac{2T_i}{T_e} \right)^2 \right] \quad (3.30c)$$

$$\int_{-\infty}^{\infty} F_3 dZ = \eta e^{(\varphi_1 + \dots + \varphi_n) \frac{1}{\varphi_0} \left(\frac{2T_i}{T_e} \right)} \left[-\frac{\varphi_3}{\varphi_0} \left(\frac{2T_i}{T_e} \right) + \frac{\varphi_1 \varphi_2}{\varphi_0 \varphi_0} \left(\frac{2T_i}{T_e} \right)^2 - \frac{1}{6} \left(\frac{\varphi_1}{\varphi_0} \right)^3 \left(\frac{2T_i}{T_e} \right)^3 \right] \quad (3.30d)$$

⋮

where $\eta = \frac{n}{n_A}$ and may be specified as a function of time. This equation can be used to solve for the potential structure at each time step. T_i is the ion temperature and T_e is the electron temperature.

3.3.5 Expansion of the Fokker - Planck Term

The Fokker - Planck term must also be expanded in order of ΔU but first must be put into cylindrical coordinates. In addition, the assumption of axial symmetry must be accounted for in the term. This can be accomplished by expanding each term in the general Fokker - Planck term.

$$\left\{ \frac{\partial f}{\partial t} \right\}_e = \Gamma \left[-\frac{\partial}{\partial u_i} \left(f \frac{m}{2M} \frac{\partial}{\partial u_i} \nabla^2 g \right) + \frac{1}{2} \frac{\partial^2}{\partial u_i \partial u_k} \left(f \frac{\partial^2 g}{\partial u_i \partial u_k} \right) \right] \quad (3.9)$$

The first term can be rewritten:

$$-\frac{m}{2M} (\nabla \cdot f \nabla (\nabla^2 g)) \quad (3.31)$$

$$\nabla^2 g = \frac{1}{R} \frac{\partial}{\partial R} \left(R \frac{\partial g}{\partial R} \right) + \frac{1}{R^2} \frac{\partial^2 g}{\partial \theta^2} + \frac{\partial^2 g}{\partial z^2} \quad (3.32)$$

Axial symmetry eliminates all θ dependence, eliminating the middle term. In addition, with the assumption of a Maxwellian radial velocity distribution the problem has been reduced to one dimension. Thus,

$$\nabla(\nabla^2 g) = \frac{\partial^3 g}{\partial x^3} \quad (3.33)$$

and the first term reduces to:

$$-\frac{\partial}{\partial x} \left(f \frac{m}{2M} \frac{\partial^3 g}{\partial x^3} \right) \quad (3.34)$$

The second term in the Fokker - Planck equation,

$$\frac{1}{2} \frac{\partial^2}{\partial v_i \partial v_k} \left(f \frac{\partial^2 g}{\partial v_i \partial v_k} \right),$$

can be reduced directly to the one dimensional case.

$$\frac{1}{2} \frac{\partial^2}{\partial x^2} \left(f \frac{\partial^2 g}{\partial x^2} \right) \quad (3.35)$$

Therefore, the Fokker - Planck term in one dimensional cylindrical coordinates is:

$$\frac{1}{\Gamma} \left\{ \frac{\partial f}{\partial t} \right\}_e = \frac{1}{2} \frac{\partial^2}{\partial x^2} \left(f \frac{\partial^2 g}{\partial x^2} \right) - \frac{\partial}{\partial x} \left(f \frac{m}{2M} \frac{\partial^3 g}{\partial x^3} \right) \quad (3.36)$$

In order to get a complete collision model the function g must also be converted to the appropriate coordinate system.

$$g(v) = \int_{-\infty}^{\infty} f(v') |v - v'| dv'$$

This definition can be reduced for the one dimensional case.

$$g(x) = \int_{-\infty}^{\infty} f(\eta) |x - \eta| d\eta \quad (3.37)$$

or, written another way

$$g(x) = \int_{-\infty}^{\infty} f(x + \xi) |\xi| d\xi \quad (3.38)$$

With this definition the Fokker - Planck term becomes:

$$\frac{1}{\Gamma} \left\{ \frac{\partial f}{\partial t} \right\}_e = \frac{1}{2} \frac{\partial^2}{\partial z^2} \left(f \int_{-\infty}^{\infty} \frac{\partial^2}{\partial z^2} (f(z+\xi)) |\xi| d\xi \right) - \frac{\partial}{\partial z} \left(f \frac{m}{2M} \int_{-\infty}^{\infty} \frac{\partial^3}{\partial z^3} (f(z+\xi)) |\xi| d\xi \right) \quad (3.39)$$

For brevity let / denote a derivative with respect to z . Using this notation the Fokker - Planck term becomes:

$$\frac{1}{\Gamma} \left\{ \frac{\partial f}{\partial t} \right\}_e = \frac{1}{2} \frac{\partial^2}{\partial z^2} \left(f \int_{-\infty}^{\infty} f''(z+\xi) |\xi| d\xi \right) - \frac{\partial}{\partial z} \left(f \frac{m}{2M} \int_{-\infty}^{\infty} f'''(z+\xi) |\xi| d\xi \right) \quad (3.40)$$

The Fokker - Planck term is nondimensionalized using the same variables as the Boltzmann equation.

$$\left\{ \frac{\partial F}{\partial \tau} \right\}_e = \frac{\partial^2}{\partial Z^2} \left(F \frac{1}{2} \frac{a}{a'} \int_{-\infty}^{\infty} F''(Z+\zeta) |\zeta| d\zeta \right) + \frac{\partial}{\partial Z} \left(F \frac{-m}{2M} \frac{a}{a'} \int_{-\infty}^{\infty} F'''(Z+\zeta) |\zeta| d\zeta \right) \quad (3.41)$$

Let:

$$A(F) = \frac{1}{2} \frac{a}{a'} \int_{-\infty}^{\infty} F''(Z+\zeta) |\zeta| d\zeta \quad (3.42)$$

$$B(F) = \frac{-m}{2M} \frac{a}{a'} \int_{-\infty}^{\infty} F'''(Z+\zeta) |\zeta| d\zeta \quad (3.43)$$

The Fokker - Planck term can be written in a compact form using these defined functions.

$$\left\{ \frac{\partial F}{\partial \tau} \right\}_e = \frac{\partial^2}{\partial Z^2} (FA(F)) + \frac{\partial}{\partial Z} (FB(F)) \quad (3.44)$$

The Fokker - Planck term can be expanded by order in ΔU using the same technique as the Boltzmann equation.

$$\begin{aligned} \left\{ \frac{\partial F}{\partial \tau} \right\}_e = & \left[\frac{\partial^2}{\partial Z^2} (F_0 A(F_0)) + \frac{\partial}{\partial Z} (F_0 B(F_0)) \right] \\ & + \Delta U \left[\frac{\partial^2}{\partial Z^2} (F_1 A(F_0)) + \frac{\partial}{\partial Z} (F_1 B(F_0)) + \frac{\partial^2}{\partial Z^2} (F_0 A(F_1)) + \frac{\partial}{\partial Z} (F_0 B(F_1)) \right] \\ & + \dots \\ & + \Delta U^n \left[\sum_{m=0}^n \left(\frac{\partial^2}{\partial Z^2} (F_{n-m} A(F_m)) + \frac{\partial}{\partial Z} (F_{n-m} B(F_m)) \right) \right] \end{aligned} \quad (3.45)$$

This expansion can be combined directly with the expansion of the Boltzmann equation.

3.3.6 Solution Approach

To obtain a time dependent solution to the Boltzmann equation with the Fokker - Planck collision term a numerical technique is necessary. The solution presented has been limited to ion - ion collisions because these collisions represent the majority of the collisional energy and momentum transfer within the presheath. The positive signs in the Boltzmann equation must be applied for ion - ion collisions. The ratio of particle mass to reduced mass, $\frac{m}{M}$, must be equal to two for like particles. The ratio of the inverse squares of the particle thermal velocities, $\frac{q_i}{q_e}$, must be one for like particle collisions. The nondimensional Boltzmann equation reduces to the following form.

$$\begin{aligned} \frac{\partial F_i}{\partial \tau} - \frac{\partial^2}{\partial Z^2} (F_i A(F_0)) - \frac{\partial}{\partial Z} (F_i B(F_0)) + \varphi_0 i Z F_i + \varphi_{-1} \frac{\partial F_i}{\partial Z} \\ = - \sum_{m=1}^i \varphi_m m \frac{\partial F_{i-m}}{\partial Z} + \sum_{m=1}^i \left(\frac{\partial^2}{\partial Z^2} (F_{i-m} A(F_m)) + \frac{\partial}{\partial Z} (F_{i-m} B(F_m)) \right) \end{aligned} \quad (3.46)$$

where the summations are taken to be zero if $i = 0$. The functions $A(F_m)$ and $B(F_m)$ can be written:

$$A(F) = \frac{1}{2} \int_{-\infty}^{\infty} F''(Z + \varsigma) |\varsigma| d\varsigma \quad (3.47)$$

$$B(F) = - \int_{-\infty}^{\infty} F'''(Z + \varsigma) |\varsigma| d\varsigma \quad (3.48)$$

The 'i' equations in the expansion are solved to obtain the time dependent particle velocity distribution. The Poisson equation is employed at each time step to obtain the potential structure. The ratio of the higher order equations with respect to the first order equation eliminates the $\eta e^{(\varphi_1 + \dots + \varphi_{-1}) \frac{1}{\varphi_0} (\frac{2F_i}{F_0})}$ term from the Poisson equation. Using this technique each successive component of the potential

structure can be determined from the previous components.

$$\frac{\int_{-\infty}^{\infty} F_1 dZ}{\int_{-\infty}^{\infty} F_0 dZ} = -\frac{\varphi_1}{\varphi_0} \left(\frac{2T_i}{T_e} \right) \quad (3.49a)$$

$$\frac{\int_{-\infty}^{\infty} F_2 dZ}{\int_{-\infty}^{\infty} F_0 dZ} = -\frac{\varphi_2}{\varphi_0} \left(\frac{2T_i}{T_e} \right) + \frac{1}{2} \left(\frac{\varphi_1}{\varphi_0} \right)^2 \left(\frac{2T_i}{T_e} \right)^2 \quad (3.49b)$$

$$\frac{\int_{-\infty}^{\infty} F_3 dZ}{\int_{-\infty}^{\infty} F_0 dZ} = -\frac{\varphi_3}{\varphi_0} \left(\frac{2T_i}{T_e} \right) + \frac{\varphi_1 \varphi_2}{\varphi_0 \varphi_0} \left(\frac{2T_i}{T_e} \right)^2 - \frac{1}{6} \left(\frac{\varphi_1}{\varphi_0} \right)^3 \left(\frac{2T_i}{T_e} \right)^3 \quad (3.49c)$$

⋮

Using these equations the particle velocity distribution and the potential structure of the presheath are determined as a function of time.

Of interest in this study is the point at which there are no returning ions. This is the presheath - sheath interface. This occurs when the net ion flux away from the wall is zero. To calculate this point in the presheath it is necessary to obtain a value for the potential expansion parameter ΔU such that when the overall particle distribution is reconstructed from the various terms in the expansion no returning ions are present. Thus, at the critical point of no returning ions the model determines the total particle velocity distribution, the potential structure, and a value for the potential expansion parameter. From the potential structure and the potential expansion parameter the presheath height at the point of no returning ions can be determined (see figure 3.5).

CHAPTER IV

NUMERICAL TECHNIQUE

4.1 Problem Approach

The solution of the Boltzmann equation, as written in equation 3.46, coupled with the Poisson equation (3.49) is the goal of the numerical procedure.

The general approach is to solve the Boltzmann equation for the particle velocity distribution using a partially implicit, partially explicit scheme. Each step in time the Boltzmann equation is solved using some results from the previous time step. In equation 3.46 the left hand side is solved implicitly while the right hand side is solved explicitly.

$$\begin{aligned} & \frac{\partial F_i}{\partial \tau} - \frac{\partial^2}{\partial Z^2} (F_i A(F_0)) - \frac{\partial}{\partial Z} (F_i B(F_0)) + \varphi_0 i Z F_i + \varphi_{-1} \frac{\partial F_i}{\partial Z} \\ & = - \sum_{m=1}^i \varphi_m m \frac{\partial F_{i-m}}{\partial Z} + \sum_{m=1}^i \left(\frac{\partial^2}{\partial Z^2} (F_{i-m} A(F_m)) + \frac{\partial}{\partial Z} (F_{i-m} B(F_m)) \right) \end{aligned} \quad (3.46)$$

The left hand side of this equation can be put in a matrix form.

$$\begin{bmatrix} T(\tau) \end{bmatrix} \begin{bmatrix} F_i(\tau + \Delta \tau) \end{bmatrix} \quad (4.1)$$

In this form the matrix $T(\tau)$ is an $m \times m$ matrix created from the left hand side of the Boltzmann equation. The quantity m is the number of divisions in the velocity space Z chosen for the numerical scheme. The matrix $T(\tau)$ is computed from $A(F_0(\tau))$ and $B(F_0(\tau))$. The values of these derived functions are taken from the solution to the particle velocity distribution at the previous time step, τ . Numerical derivatives are used to represent the partial derivatives in the equation. This procedure produces a diagonal matrix where all elements except those on an odd number of centered

diagonals are zero. The number of diagonals reflects the order of accuracy in the solution. Diagonal matrices of this form are easily and quickly inverted. The $F_i(\tau + \Delta\tau)$ matrix is an $m \times 1$ matrix of unknowns that represents the particle velocity distribution at the current time step. 'i' equations of this form can be written corresponding to the number of terms in the expansion.

The right hand side of the Boltzmann equation can also be put in a matrix form.

$$\varphi_1 \begin{bmatrix} v_i^1(\tau) \end{bmatrix} + \dots + \varphi_n \begin{bmatrix} v_i^n(\tau) \end{bmatrix} + \begin{bmatrix} d_i(\tau) \end{bmatrix} \quad (4.2)$$

The scalar φ_n values are unknowns and represent the nondimensional coefficients in the asymptotic potential structure of the presheath.

The $v_i^n(\tau)$ matrices are $m \times 1$ matrices which are comprised of the partial derivatives of the velocity distribution at the previous time step, τ . They represent the first summation on the right hand side of the Boltzmann equation.

$$\sum_{m=1}^i \varphi_m \left(-m \frac{\partial F_{i-m}}{\partial Z} \right)$$

The d_i matrix is an $m \times 1$ matrix comprised of the second summation on the right hand side of the Boltzmann equation.

$$\sum_{m=1}^i \left(\frac{\partial^2}{\partial Z^2} (F_{i-m} A(F_m)) + \frac{\partial}{\partial Z} (F_{i-m} B(F_m)) \right)$$

All values of the distribution and the functions $A(F_m)$ and $B(F_m)$ are taken at the previous time step, τ .

Putting together equations 4.1 and 4.2 a matrix form of the Boltzmann equation is created that can be solved for the particle velocity distribution.

$$\begin{bmatrix} T(\tau) \end{bmatrix} \begin{bmatrix} F_i(\tau + \Delta\tau) \end{bmatrix} = \varphi_1 \begin{bmatrix} v_i^1(\tau) \end{bmatrix} + \dots + \varphi_n \begin{bmatrix} v_i^n(\tau) \end{bmatrix} + \begin{bmatrix} d_i(\tau) \end{bmatrix} \quad (4.3)$$

'i' equations of this form can be written corresponding to the number of terms in the asymptotic expansion being used.

These equations are quickly inverted to obtain the particle velocity distribution at the current time step.

$$\begin{bmatrix} F_i(r + \Delta r) \end{bmatrix} = \varphi_1 \begin{bmatrix} V_i^1(r) \end{bmatrix} + \dots + \varphi_n \begin{bmatrix} V_i^n(r) \end{bmatrix} + \begin{bmatrix} D_i(r) \end{bmatrix} \quad (4.4)$$

Where the V_n and D matrices represent the $m \times 1$ solution matrix to the inversion of the $T(r)$ matrix with the corresponding v_n or d matrix.

The particle velocity distribution is obtained from this equation using the φ_n values from the previous time step.

Equation 3.49 is employed to obtain the φ_n values at the current time step.

$$\frac{\int_{-\infty}^{\infty} F_1 dZ}{\int_{-\infty}^{\infty} F_0 dZ} = -\frac{\varphi_1}{\varphi_0} \left(\frac{2T_i}{T_e} \right) \quad (3.49a)$$

$$\frac{\int_{-\infty}^{\infty} F_2 dZ}{\int_{-\infty}^{\infty} F_0 dZ} = -\frac{\varphi_2}{\varphi_0} \left(\frac{2T_i}{T_e} \right) + \frac{1}{2} \left(\frac{\varphi_1}{\varphi_0} \right)^2 \left(\frac{2T_i}{T_e} \right)^2 \quad (3.49b)$$

$$\frac{\int_{-\infty}^{\infty} F_3 dZ}{\int_{-\infty}^{\infty} F_0 dZ} = -\frac{\varphi_3}{\varphi_0} \left(\frac{2T_i}{T_e} \right) + \frac{\varphi_1 \varphi_2}{\varphi_0 \varphi_0} \left(\frac{2T_i}{T_e} \right)^2 - \frac{1}{6} \left(\frac{\varphi_1}{\varphi_0} \right)^3 \left(\frac{2T_i}{T_e} \right)^3 \quad (3.49c)$$

⋮

The new distributions are integrated numerically and the φ_1 through φ_n scalars are determined consecutively. The value of φ_0 is input and is a nondimensional representation of the coefficient β in the potential expansion parameter, ΔU .

For each time step, the overall particle velocity distribution can be determined at any location from the original expansion once it has been nondimensionalized.

$$F(Z, \Delta U^*) = F_0(Z) + \Delta U^* F_1(Z) + \Delta U^{*2} F_2(Z) + \dots \quad (4.5)$$

since,

$$\Delta U^* = e^{\varphi_0 z^2} \quad (4.6)$$

Where the * quantities are nondimensional. z has been nondimensionalized with respect to an ion mean free path.

$$z^* = \frac{z}{n_R \Gamma}$$

The potential structure of the presheath is determined from the nondimensional form of the original expansion of potential.

$$U^* = U_0^* + \varphi_1 \Delta U^* + \varphi_2 \Delta U^{*2} + \dots \quad (4.7)$$

Using this procedure the time dependent evolution of the presheath is obtained.

The point of no returning ions occurs where the integral of the left half plane of the total particle velocity distribution is zero.

$$0 = \int_{-\infty}^0 F(Z) dZ \quad (4.8)$$

This equation can be rewritten using the expansion of the particle distribution.

$$0 = \int_{-\infty}^0 F_0(Z) dZ + \Delta U^* \int_{-\infty}^0 F_1(Z) dZ + \Delta U^{*2} \int_{-\infty}^0 F_2(Z) dZ + \dots \quad (4.9)$$

Equation 4.9 can be solved for ΔU^* . Since the particle distributions are now known as a function of time and velocity. The entire solution at the point of no returning ions is known with this last piece of information.

4.2 Numerical Integration, Differentiation, and Matrix Inversion

In order to obtain a solution to the potential structure and particle distribution in the presheath it is necessary to develop the applicable mathematical tools. The primary techniques needed are integration, differentiation, and matrix inversion.

4.2.1 Numerical Integration

Throughout the solution integration is computed using a Simpson's $\frac{1}{3}$ rule technique^[12].

$$\int_a^b f(x)dx = \frac{h}{3} (f_1 + 4f_2 + 2f_3 + 4f_4 + 2f_5 + \dots + 2f_{n-1} + 4f_n + f_{n+1}) \quad (4.10)$$

Where h is the spacing between the points and f_1 through f_{n+1} represent the function values at each point. This procedure has a global error of $O(h^4)$. If the step size is chosen appropriately this procedure is very accurate.

4.2.2 Numerical Differentiation

The technique for determining numerical differentiation is a second order accurate scheme. This reduces the number of computations while maintaining high accuracy. Second order accurate numerical differentiation requires that only three points be known. Thus, the ' $T(r)$ ' matrix contains only three diagonals. If third order accuracy was used the ' $T(r)$ ' matrix would require five diagonals to represent the five points needed for the differentiation. In addition, to maintain uniformity a central difference technique is desirable on as many points as possible. The greater the number of points needed for each derivative the more points that require forward or backward difference techniques (rather than the central difference technique). Below is a list of the techniques used to obtain derivatives^[12].

Central Difference

$$\frac{\partial F}{\partial x} = \frac{F(x+1) - F(x-1)}{2h} \quad (4.11a)$$

$$\frac{\partial^2 F}{\partial x^2} = \frac{F(x+1) - 2F(x) + F(x-1)}{h^2} \quad (4.11b)$$

$$\frac{\partial^3 F}{\partial x^3} = \frac{F(x+2) - 2F(x+1) + 2F(x-1) - F(x-2)}{2h^3} \quad (4.11c)$$

Forward Difference

$$\frac{\partial F}{\partial x} = \frac{-F(x+2) + 4F(x+1) - 3F(x)}{2h} \quad (4.12a)$$

$$\frac{\partial^2 F}{\partial x^2} = \frac{F(x+2) - 2F(x+1) + F(x)}{h^2} \quad (4.12b)$$

$$\frac{\partial^3 F}{\partial x^3} = \frac{F(x+3) - 3F(x+2) + 3F(x+1) - F(x)}{h^3} \quad (4.12c)$$

Backward Difference

$$\frac{\partial F}{\partial x} = \frac{3F(x) - 4F(x-1) + F(x-2)}{2h} \quad (4.13a)$$

$$\frac{\partial^2 F}{\partial x^2} = \frac{F(x) - 2F(x-1) + F(x-2)}{h^2} \quad (4.13b)$$

$$\frac{\partial^3 F}{\partial x^3} = \frac{F(x) - 3F(x-1) + 3F(x-2) - F(x-3)}{h^3} \quad (4.13c)$$

Where h is the grid spacing. The derivatives are being taken about point x .

It is worth noting that the third derivative equations require up to five points. There is no second order accurate numerical third derivative representation. These equations are third order accurate. This does not effect the ' $T(r)$ ' matrix in that it contains no third derivatives. The solution procedure requires third derivatives only in the determination of the function $B(F_i(r))$.

These equations are used throughout the solution for derivatives with respect to velocity, Z , and time, τ .

4.2.3 Matrix Inversion

In order to obtain a solution a procedure for inverting a diagonal matrix is necessary. The procedure used will invert any centered diagonal matrix. For the second order accurate case the matrix in question is tridiagonal. The procedure uses Gaussian elimination on all terms below the center diagonal and then through back substitution determines the solution vector. This technique can quickly invert a 200×200 tridiagonal matrix.

4.3 Obtaining a Solution

As in any numerical model certain restraints and conditions must be met to obtain an accurate solution. This model requires some form of input distribution function and in order to obtain higher order terms must also have a perturbation applied to the potential structure. In addition, certain numerical techniques have been used to remove instabilities in the model.

4.3.1 Initial Distribution

To model the presheath region an initial particle velocity distribution that conforms to a Maxwellian profile has been used. This profile represents the distribution that naturally occurs in the neutral plasma region. The idea is that the time dependent evolution of the distribution will change from a Maxwellian at time zero to a shifted new form as the presheath is entered. The Maxwellian profile is initially given to the zero order term having set the initial conditions of all higher order terms to zero.

If the potential structure of the presheath is not perturbed in some manner then the model represents the neutral plasma region and the particle velocity distribution remains Maxwellian (as it should). If, however, a small perturbation in the potential structure is added (ie. a nonzero $a_1, a_2 \dots$) then the model readjusts to describe the presheath region. In this manner the model is used to give the time dependent evolution of the presheath.

4.3.2 Instability Damping

By the nature of the implicit - explicit technique being employed certain numerical problems are expected to appear. This model is no exception. Two techniques have been used to remove these instabilities.

The most important thing to do to avoid numerical problems in a scheme of this nature is to ensure that as much as possible of the solution is computed implicitly. In addition, once some new data has been calculated it should be applied to any new calculations immediately.

In this model each term in the expansion of the particle distribution function uses the new data already determined in calculating all of the lower order terms. Once F_0 is determined that information is used in calculating F_1 . This idea is repeated for the higher order terms.

A second method applied to the model to eliminate oscillatory instabilities that start on a very small scale and grow is the application of a very weak averaging scheme to the particle distribution functions. Each point in the distribution is weakly averaged with the points on either side.

$$F(Z) = \frac{0.025F(Z+1) + F(Z) + 0.025F(Z-1)}{1.05} \quad (4.14)$$

This technique, although necessary, has the negative effect of falsely increasing the energy in the system by spreading the distribution slightly (see figure 5.1). The change is very small and can be considered insignificant with respect to the overall solution.

4.4 Program Structure

The entire program has been written in FORTRAN and can be run on either an IBM PC AT or on the CYBER mainframe. The code has been written in a segmented manner that easily allows one section to be altered without having to alter other sections. The overall structure of the program consists of three initialization programs, three input data files, the main program, and three output data files. The main program contains a driver and seventeen subroutines. Several of the sub-

routines perform operations that are used throughout the main code. Figure 4.1 is a diagram of the structure of the program. The flexibility of the code is derived from the generalized subroutine structure and the ability to enter a variety of input variables. The driver keeps track of time and maintains the overall operating structure of the solution while the subroutines perform the necessary manipulations. Below is a list of the function of each program, data file and subroutine.

AVE - Subroutine to smooth distributions by averaging.

CONSERV - Subroutine to determine conservation of energy, momentum, and particles.

CONSOUT - Conservation output data file.

CRF - Particle distribution initialization program.

CRPHI - Potential structure initialization program.

DENSITY - Subroutine to solve for a new presheath structure.

FDATA - Initial particle distribution data file.

FD1 - Subroutine to find first derivatives.

FD2 - Subroutine to find second derivatives.

FD3 - Subroutine to find third derivatives.

FINDA - Subroutine to determine 'A' function.

FINDB - Subroutine to determine 'B' function.

FPINIT - Primary initialization program.

FPOUT - Output particle distribution data file.

FPSHETH - Main program driver.

GETAB - Subroutine to make A and B function vectors.

INITDAT - Initialization data file.

MAKED - Subroutine to make d matrix.

MAKEF - Subroutine to read initial particle distribution.

MAKEPHI - Subroutine to read initial potential structure.

MAKET - Subroutine to make T matrix.

MAKEV - Subroutine to make v matrix.

MODLAG - Subroutine to invert diagonal matrices.

PHIDAT - Initial potential structure data file.

PHIDOUT - Output potential structure data file.

SIMPS - Subroutine to perform Simpson's rule integration.

TOT - Subroutine to obtain total distribution at point of no returning ions.

CHAPTER V

RESULTS

The ratio of ion temperature to electron temperature, T_i/T_e , has been set to one half throughout these results. There is little effect on the particle distribution or potential structure if the temperature ratio is changed to other values. The electron temperature is expected to be higher than the ion temperature in the presheath since electrons absorb energy from electric and magnetic fields faster than ions and other large particles.

Through repeated test runs of the model it was found that fifty-one points in velocity space were enough to provide high accuracy and produce good results. The range of points in velocity space has been truncated to ± 5 nondimensional units. The results show that at ± 5 the distribution is near zero, substantiating the truncation.

A time step of 0.2 nondimensional times was found to keep the solution accurate. Three nondimensional units in time were sufficient to produce stable results.

It was found that the magnitude of the higher order terms in the particle velocity distribution drop off very rapidly. Thus, the higher order terms have very little impact on the shape of the potential or of the particle distribution.

To understand the effects of a quiescent plasma interacting with a surface the potential gradient in the neutral plasma has been set to zero. To accomplish this the α term in the expansion of potential has been set to zero.

$$U = U_0 + a_1 \Delta U + a_2 \Delta U^2 + \dots \quad (3.13)$$

where

$$U_0 = \alpha x \quad \text{and} \quad \Delta U = e^{\beta x} \quad (3.14)$$

A stable solution exists only for a specific critical value of the exponential coefficient, β , which represents the scale of the presheath. The quantity β is nondimensionalized as $\varphi_0 = \frac{\beta}{n_R \Gamma}$, where $n_R \Gamma$ is an ion mean free path. It is expected, as shown in section 3.2, that the critical value should be on the order of a mean free path. It was found that $\frac{\beta}{n_R \Gamma} = 0.4$ produces the most nearly stable results. The distributions become unstable for values greater or less than 0.4. The small remaining instability at $\frac{\beta}{n_R \Gamma} = 0.4$ can be attributed to the inexact nature of the numerical solution.

The results presented here are first order and produce a complete picture of the structure of the presheath because the higher order terms collective contribution is more than an order of magnitude smaller. Figures 5.1 and 5.2 are plots of the zeroth and first order expansions of the particle distribution in velocity space. The zero order term remains Maxwellian because the potential gradient in the neutral plasma is zero. The first order term of the distribution obtains a profile that has roughly the shape (but not magnitude) of the negative first derivative of the zeroth order solution. The potential expansion parameter at the point of no returning ions is determined for each time step. Using the particle distribution functions and the known potential expansion parameter together produce the overall particle velocity distribution at the point of no returning ions, the presheath - sheath interface. Figure 5.3 shows this distribution.

The positive shift in the total distribution is as expected for the presheath. The ions are being pulled into the wall. The particle distribution for velocities away from the wall is zero for the case of no returning ions. The point of no returning ions exists where the particle distribution for velocities away from the wall integrates

to zero. Figure 5.3 shows that the ion distribution becomes negative for velocities away from the wall. A negative particle distribution cannot exist physically. The addition of higher order terms does not correct the problem because the expansion drops off so quickly that any higher order terms have no impact on the shape of the distribution. The problem is fundamental to the type of collision term being applied in the model. The Fokker - Planck term only models the limit of small angle collisions. However, large angle collisions become important in the presheath.

The first term of the nondimensionalized potential structure, ϕ_1 , has been initially perturbed to 1.0×10^{-4} to obtain the results presented in figures 5.1, 5.2 and 5.3. Perturbing the potential structure provides the model with the nonequilibrium condition necessary to initiate the time dependent development of the presheath. The strength of the initial perturbation is not significant to obtaining an accurate particle distribution and potential structure of the presheath. Figures 5.4, 5.5, and 5.6 are the result of an initial perturbation of 1.0×10^{-3} and figures 5.7, 5.8 and 5.9 are the result of an initial perturbation of 1.0×10^{-5} . Comparing these results show that the magnitude of the initial perturbation only affects the scale of the first order term and has no effect on the overall particle distribution in velocity space.

Figure 5.10 is a plot of the position of the point of no returning ions, the presheath - sheath interface, as a function of time for the three solutions. Since no source of ions exists in the model the relative position of the plasma with respect to the surface changes as a function of time. The wall is moving into the plasma, or the plasma is moving into the wall, at the rate at which the wall is absorbing ions. The three solutions have different magnitudes but follow the same profile. The strength of the perturbation controls the relative position of the zero point.

Figure 5.11 is a plot of the potential structure of the presheath obtained from

the three solutions as a function of position. The data for the potential structure has been taken from the solution at a nondimensional time of two. Note that the affect of the different initial perturbation values is to cause a shift in the relative position of the potential but has no effect on the shape of the potential or on the strength of the potential at the point of no returning ions. Changing the perturbation strength alters the location of the zero point but not its shape. The stronger the perturbation the further the zero point is moved from the surface. The horizontal line in the plot depicts the presheath height at the point of no returning ions. The vertical lines show the position of the point of no returning ions.

A time dependent plot of the presheath height at the point of no returning ions is presented in figure 5.12. This plot shows that the time evolution of the sheath height approaches smoothly to a nearly constant value of 0.16. All three solutions fall on the same curve. This shows that the strength of the perturbation does not affect the results obtained.

CHAPTER VI

CONCLUSIONS

The solution obtained is an accurate representation of the time dependent development of the Fokker - Planck presheath. The model produces a precise potential structure, however, the distribution of returning ions breaks down in the presheath. An oscillation develops in the negative tail of the distribution, as seen in figures 5.3, 5.6, and 5.9. This oscillation cannot be removed by including additional terms to the expansion. In addition, the sheath height of 0.16 determined at the point of no returning ions is roughly an order of magnitude smaller than expected. Both of these conditions lead to the conclusion that the Fokker - Planck collision term does not represent the type of collisions that remove the returning ions in the presheath. This breakdown is due to the failure of the Fokker - Planck collision term to model the large angle collisions that take place within the presheath. The Fokker - Planck term is effective at modeling the collisions present in the center of the plasma but breaks down in the presheath. The primary mechanism behind clearing out the returning ions from within the presheath is not particle diffusion as represented by small angle deflections but rather the large velocity changes caused by large angle collisions. Since the Fokker - Planck term models particle collisions that represent the limit of small angle collisions it is inadequate at describing the mechanisms controlling the ion velocity distribution moving away from the wall. The solutions obtained using a Maxwellian distribution by Bissell and Johnson^[4] and Emmert et al.^[3] and those obtained using a charge exchange collision model by Riemann^[6] and Main^[7] effectively include the large angle collisions since they model the collisions

by instantaneous changes in particle velocity and position. These collision models do not represent the Coulomb collisions taking place in a fully ionized plasma. They do not represent the collision processes but only approximate the collisional effects.

This Fokker - Planck presheath model produces a self-consistent and precise potential structure. The particle velocity distribution in the presheath has the correct acceleration of ions toward the wall but because the Fokker - Planck collision term only models the limit of small angle collisions it is unable to clear the particle distribution of returning ions. The effect of not modeling the large angle collisions is that the particle distribution for returning ions is accurate only in the initial section of the presheath where the collisional processes are dominated by particle diffusion. The collisional processes become dominated by the effects of the large angle collisions as the interface between the presheath and the Debye sheath is approached. Only by including a collision term which accounts for these large angle collisions can a presheath model produce a particle velocity distribution that accurately models the condition of no returning ions. This study has found that a presheath model which describes the Coulomb collisions occurring in a fully ionized plasma must account for both the small angle collisions and the large angle collisions.

REFERENCES

- [1] D. Bohm, in Characteristics of Electrical Discharges in Magnetic Fields, edited by A. Guthrie and R. Wakering, McGraw - Hill, New York, 1949, p. 77
- [2] S. A. Self, "Exact Solution of the Collisionless Plasma - Sheath Equation", The Physics of Fluids, Vol. 6, No. 12, Dec. 1963
- [3] G. A. Emmert, R. M. Wieland, A. T. Mense, and J. N. Davidson, "Electric Sheath and Presheath in a Collisionless Finite Ion Temperature Plasma", The Physics of Fluids, Vol. 23, No. 4, April 1980
- [4] R. C. Bissell and P. C. Johnson, "The Solution of the Plasma Equation in a Plane Parallel Geometry with a Maxwellian Source", The Physics of Fluids, Vol. 30, No. 3, March 1987
- [5] R. C. Bissell, "The Application of the Generalized Bohm Criterion to Emmert's Solution of the warm ion Collisionless Plasma Equation", The Physics of Fluids, Vol. 30, No. 7, July 1987
- [6] K. -U. Riemann, "Kinetic Theory of the Plasma Sheath Transition in a Weakly Ionized Plasma", The Physics of Fluids, Vol. 24, No. 12, March 1987
- [7] G. L. Main, "Asymptotically Correct Collisional Presheaths", The Physics of Fluids, Vol. 30, No. 6, June 1987
- [8] I. Langmuir, Phys. Rev., 34: 876 (1929)
- [9] F. F. Chen, Introduction to Plasma Physics and Controlled Fusion, vol. 1, Plenum, New York, 1984, p. 10
- [10] K. Miyamoto, Plasma Physics for Nuclear Fusion, The MIT Press, Cambridge, Mass., 1980, p. 602
- [11] G. Schmidt, Physics of High Temperature Plasmas, Academic Press, New York, 1979
- [12] C. F. Gerald and P. O. Wheatley, Applied Numerical Analysis, Addison - Wesley, Reading, Mass., 1984
- [13] C. M. Bender and S. A. Orszag, Advanced Mathematical Methods for Scientists and Engineers, McGraw - Hill, New York, 1978

FIGURES

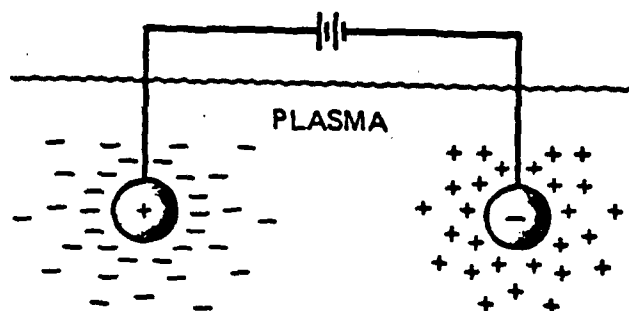


Figure 3.1 Debye Shielding

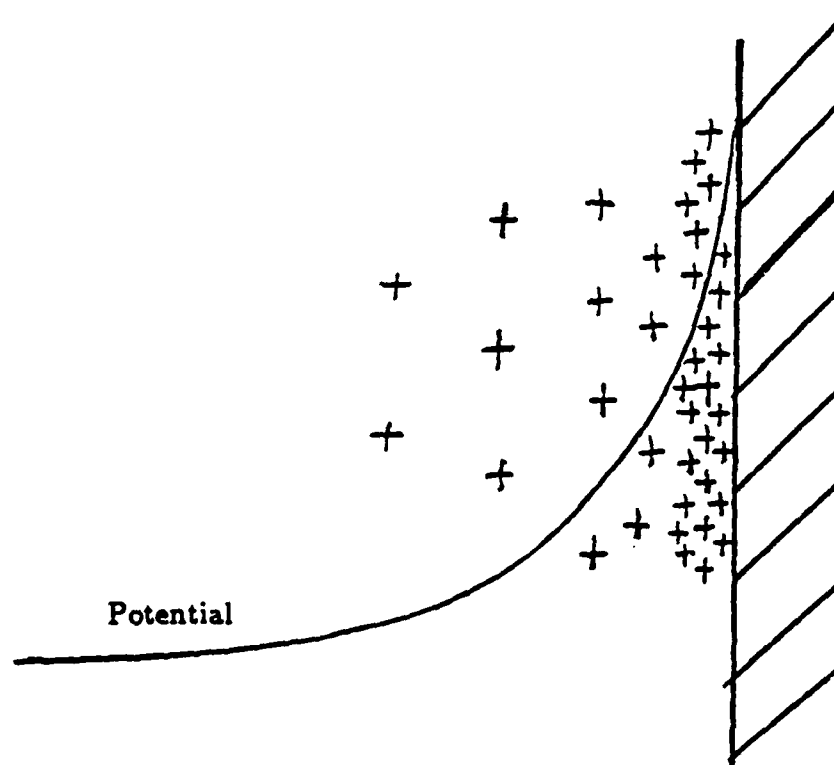


Figure 3.2 Wall Potential

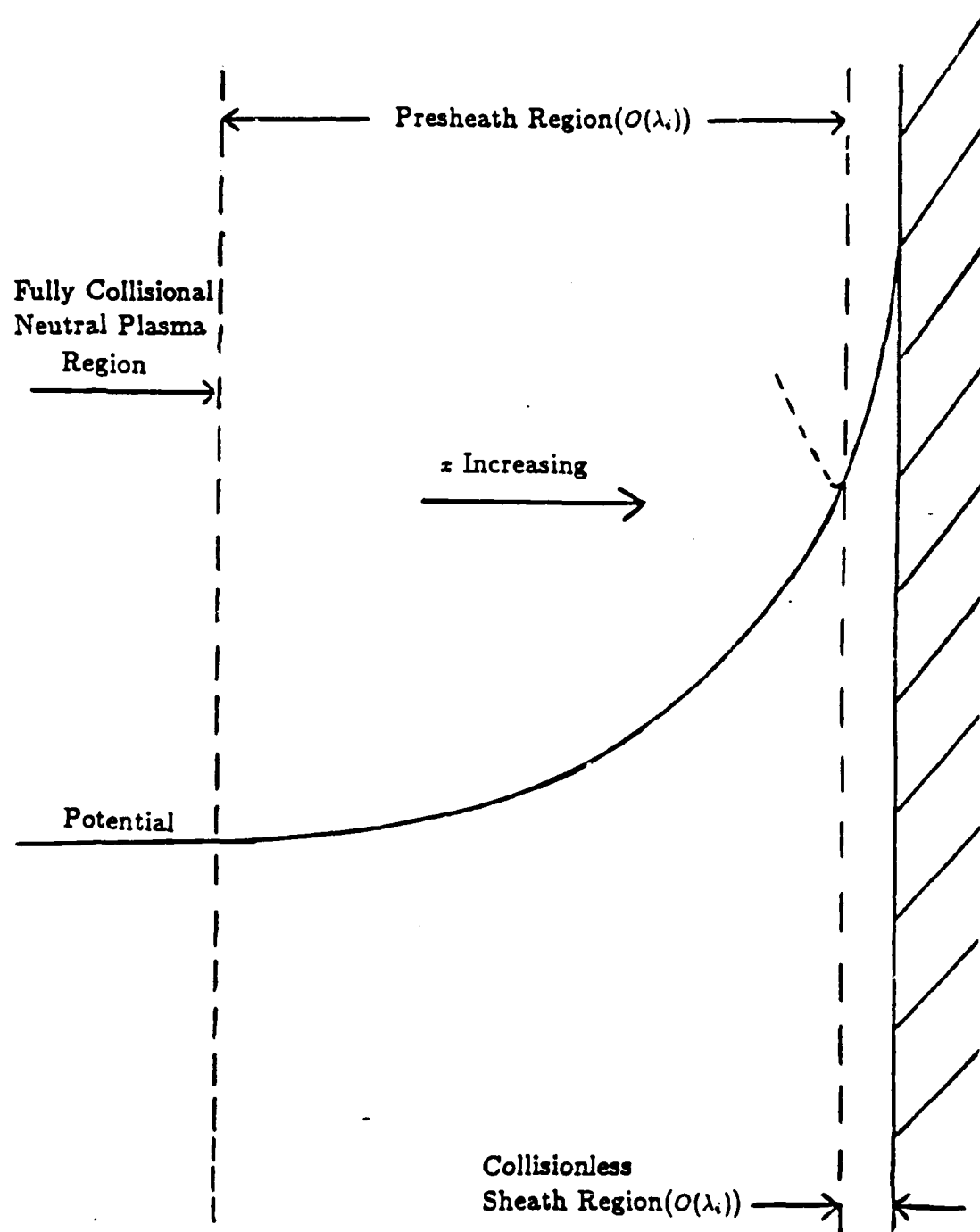


Figure 3.3 Wall Region Model

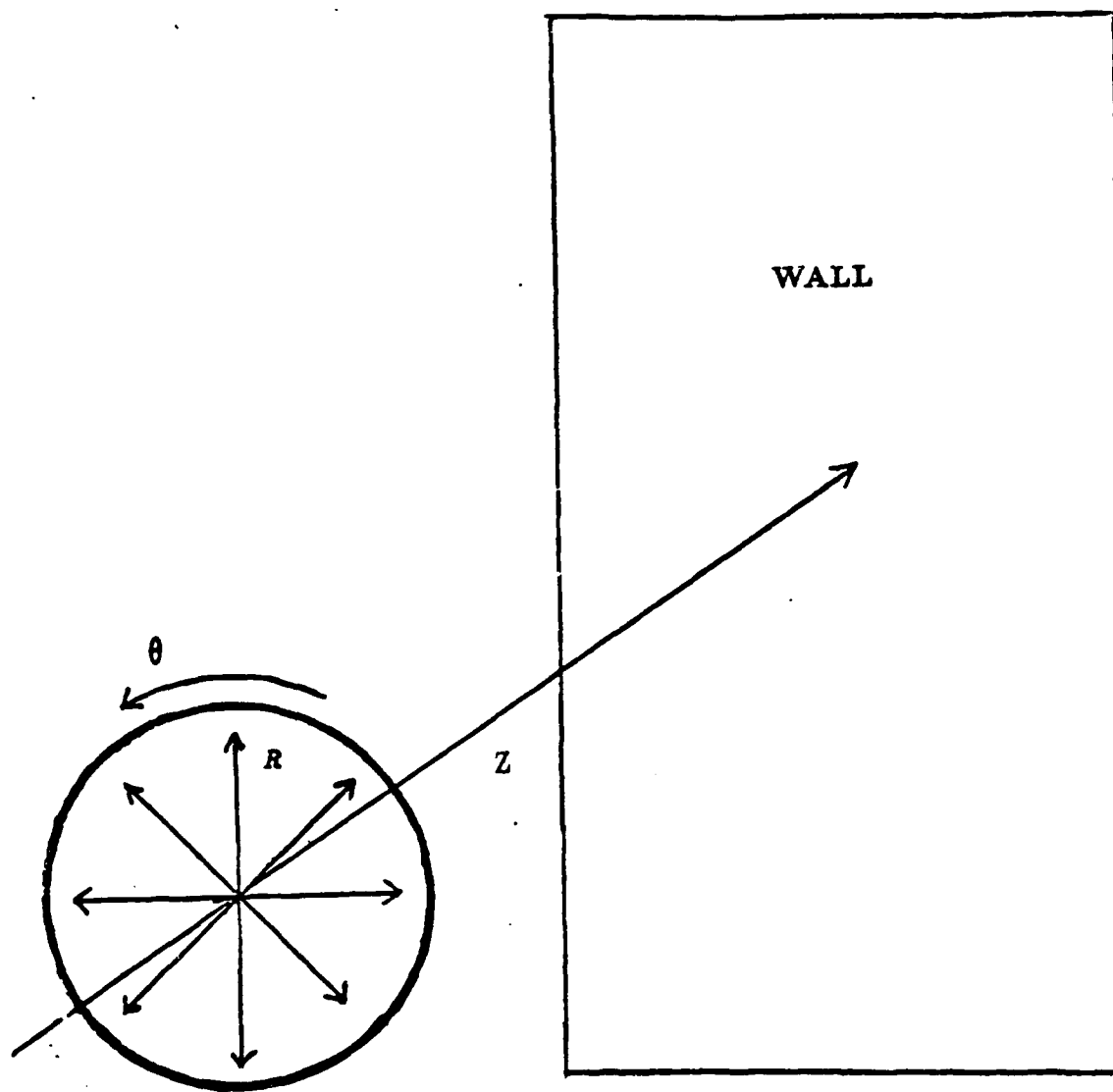


Figure 3.4 Coordinate System in Velocity Space

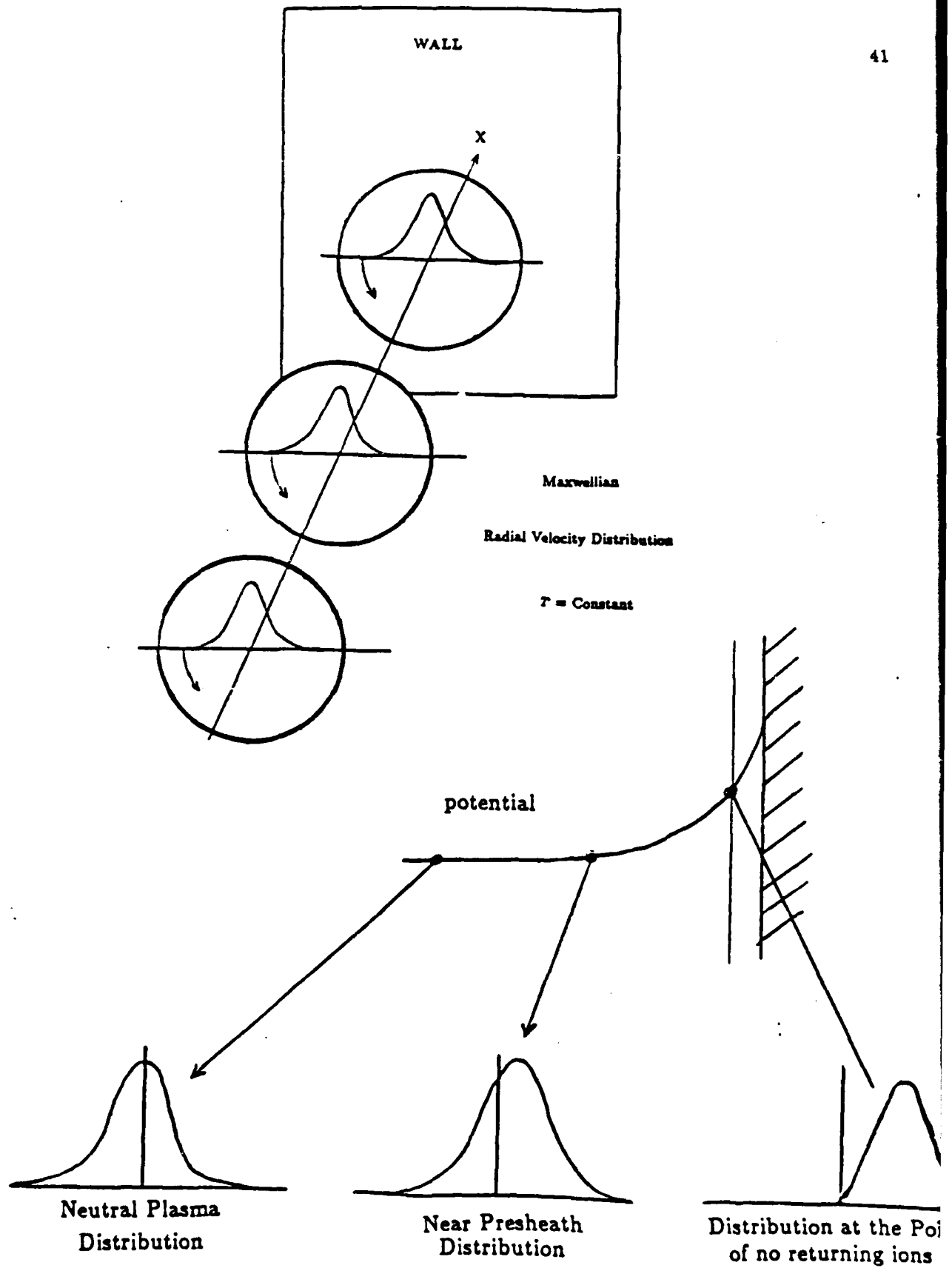


Figure 3.5 Radial, Symmetric, and No Returning Ions Conditions

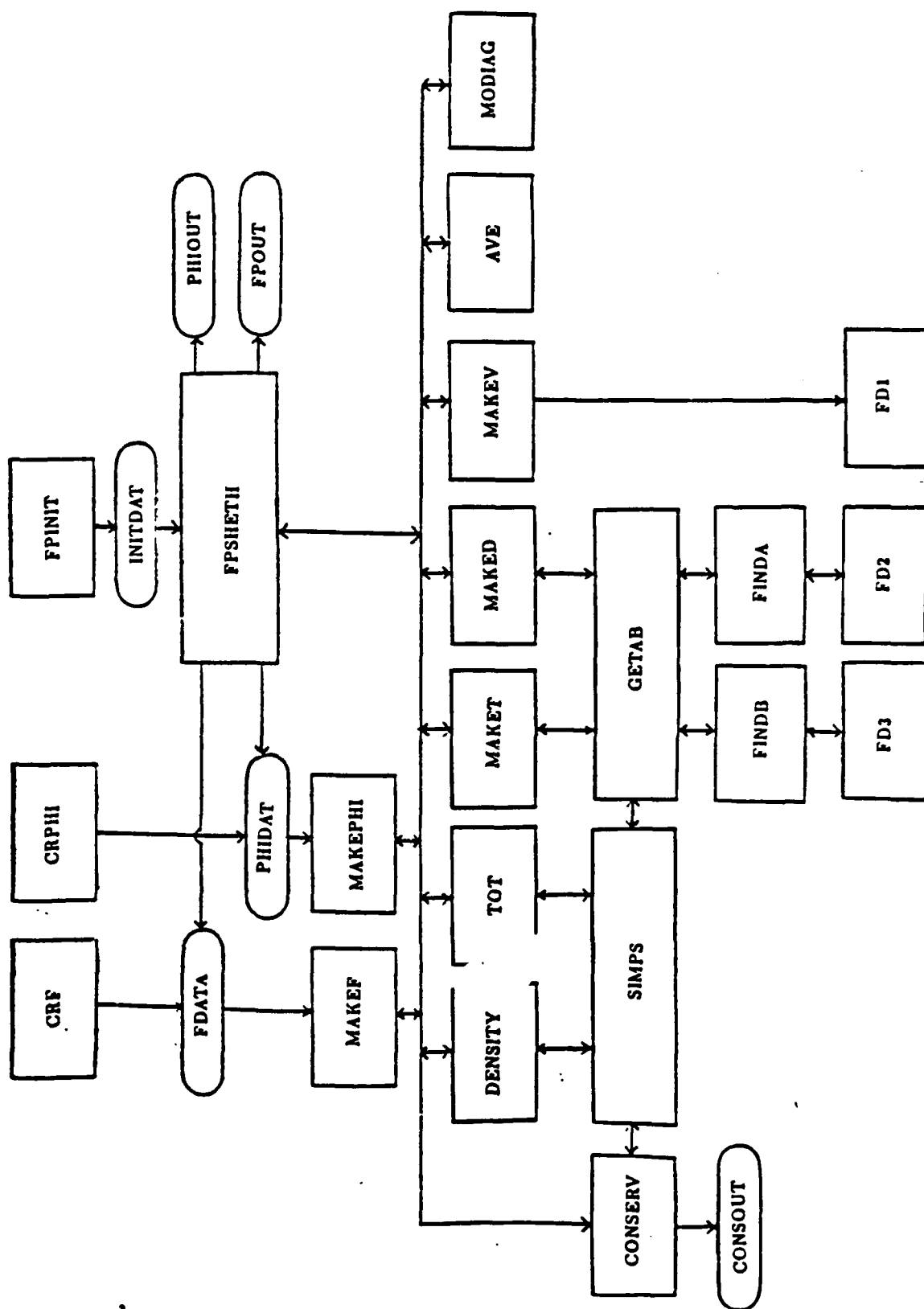
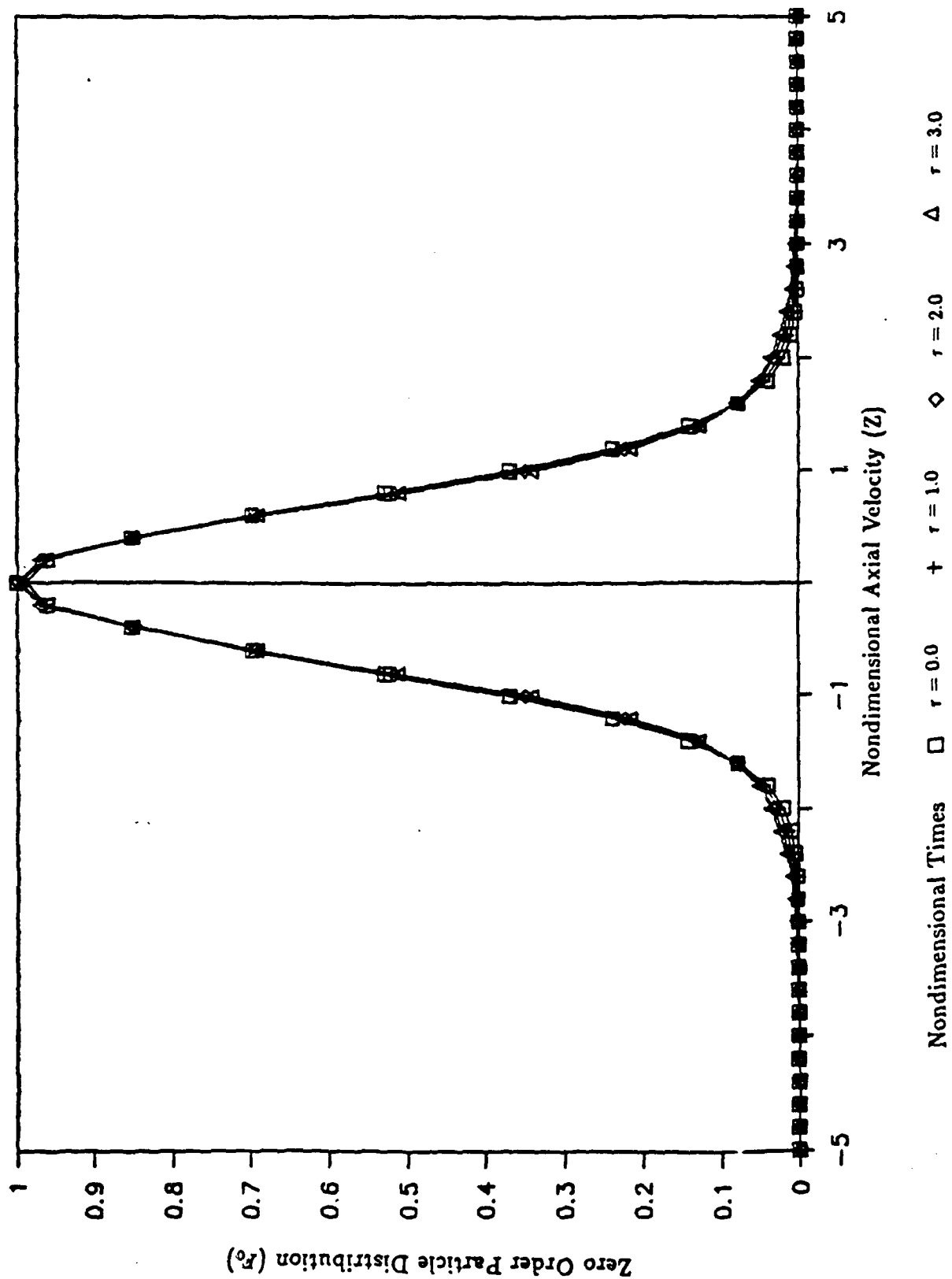
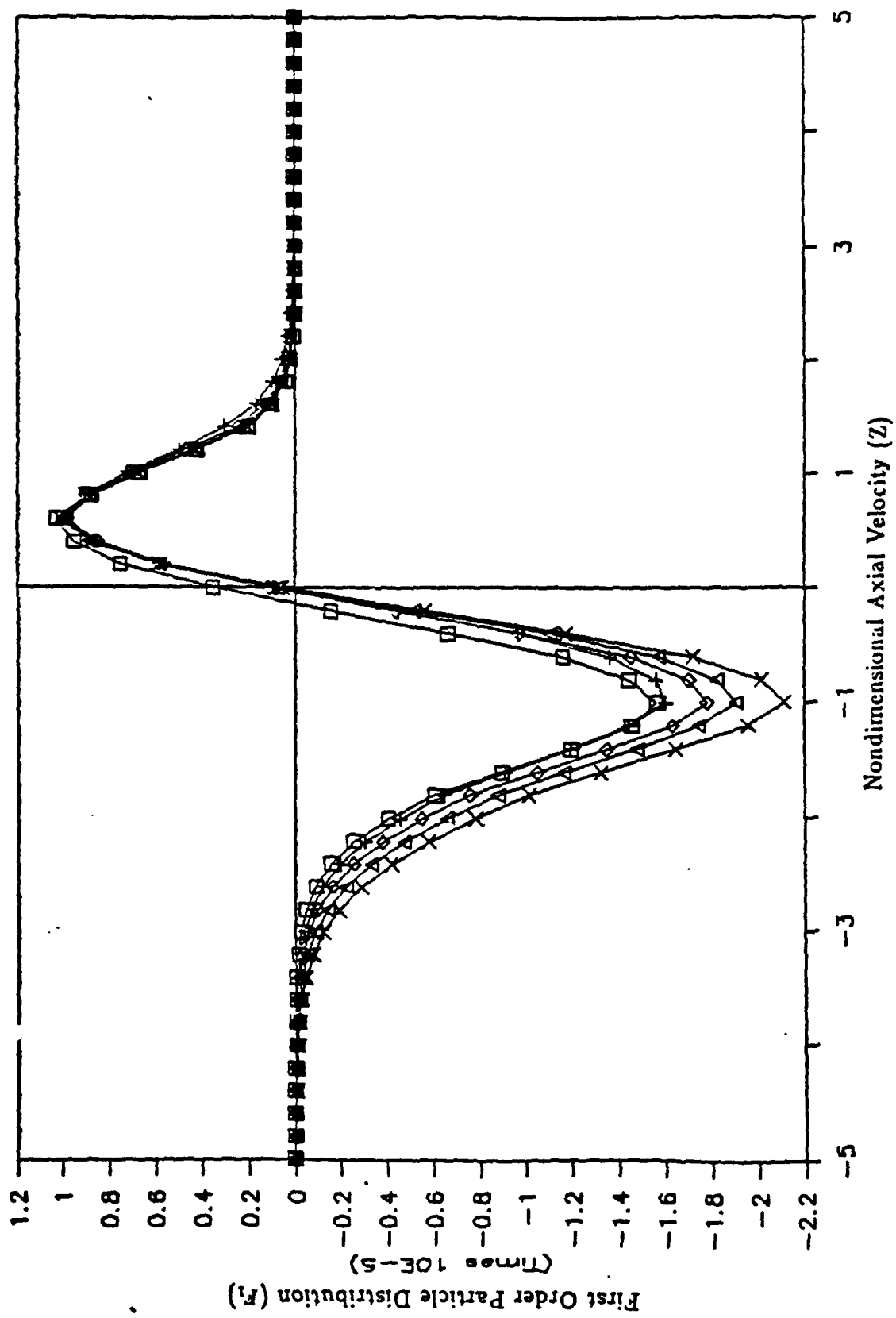


Figure 4.1 Program Diagram





Nondimensional Times $\square$ $r = 0.8$ $+$ $r = 1.0$ $\diamond$ $r = 1.2$ Δ $r = 1.4$ $\times$ $r = 1.6$

Figure 5.2 First Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-4}$

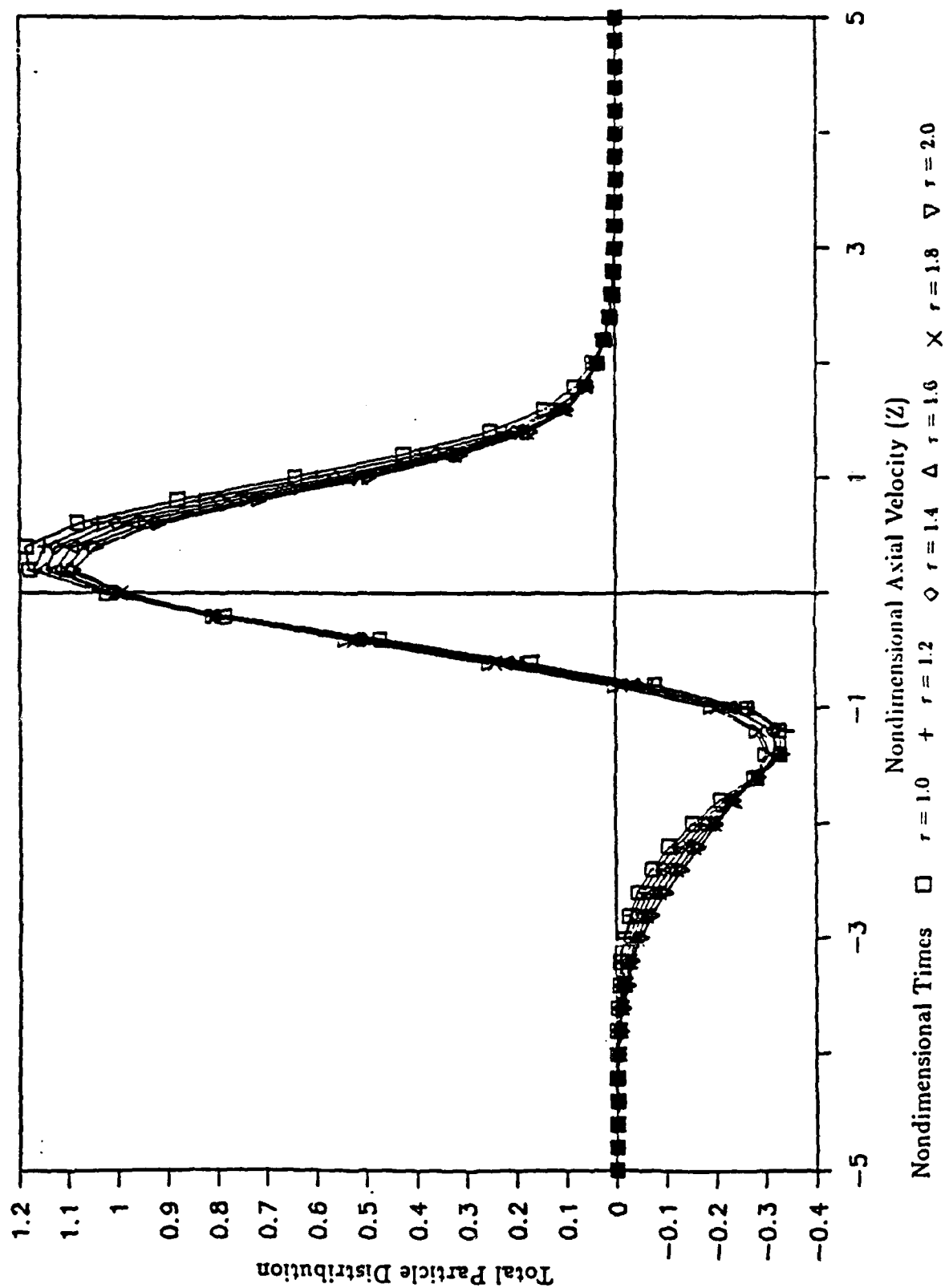


Figure 5.3 Total Particle Velocity Distribution

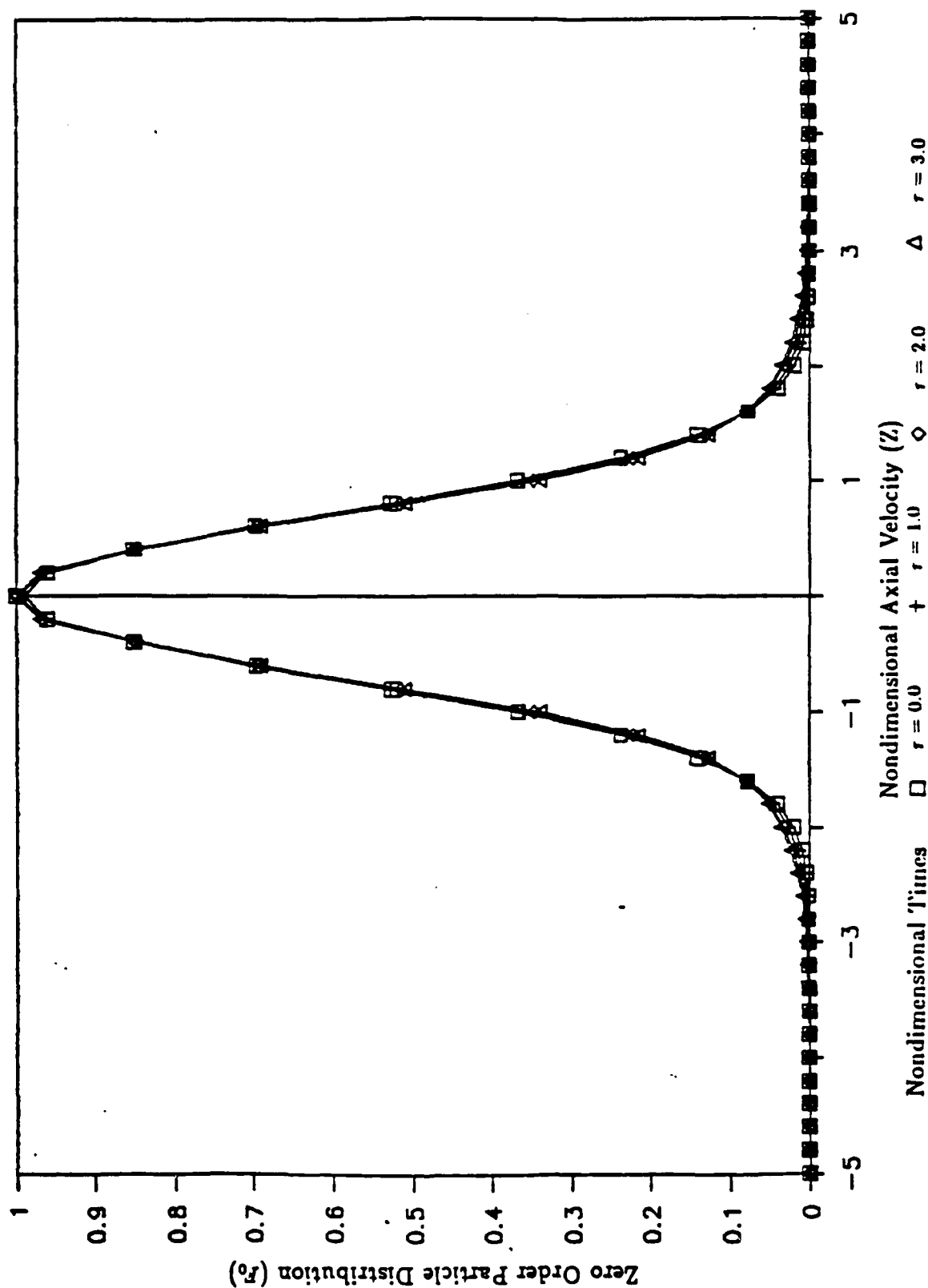


Figure 5.4 Zero Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-3}$

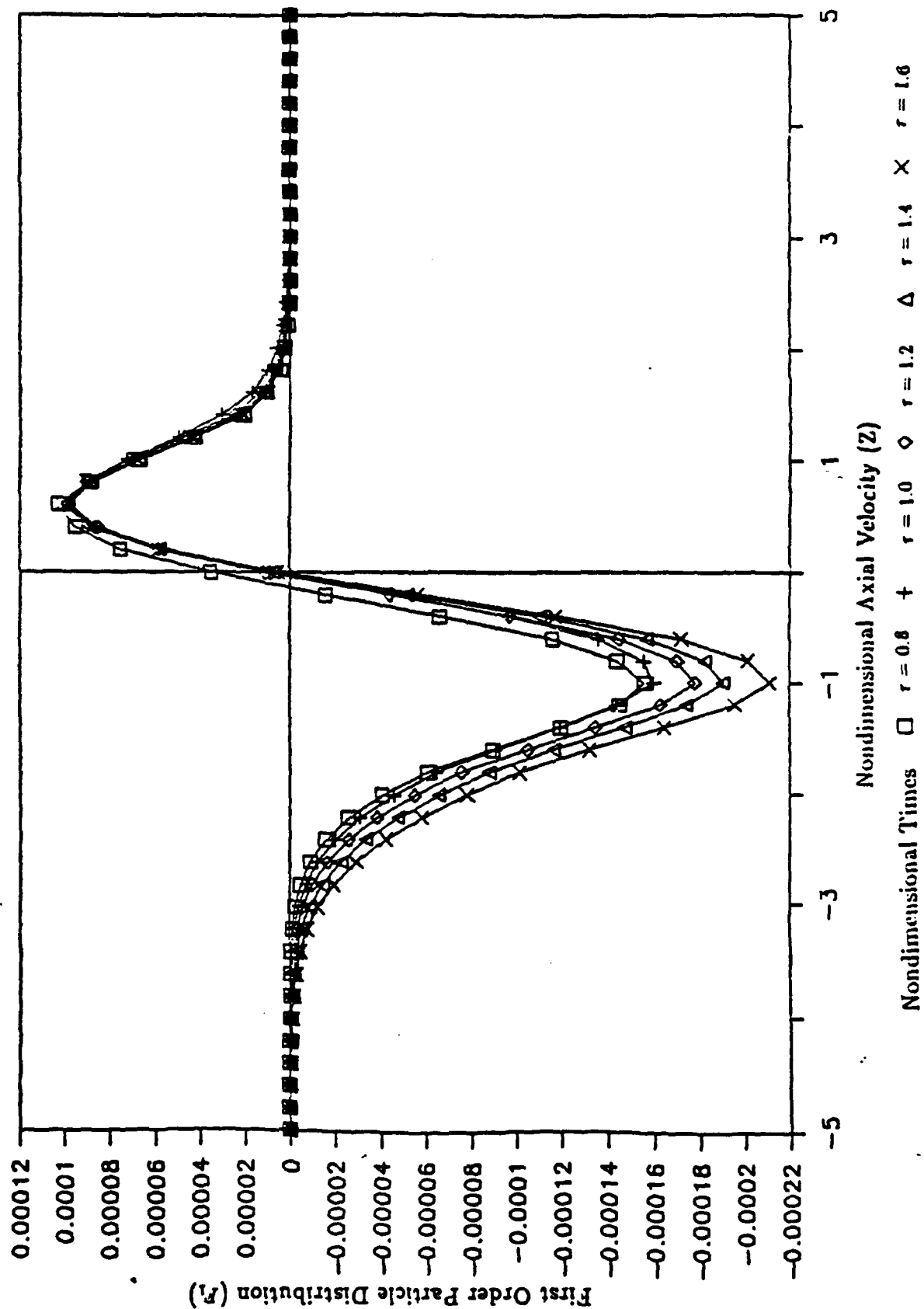


Figure 5.5 First Order Particle Velocity Distribution

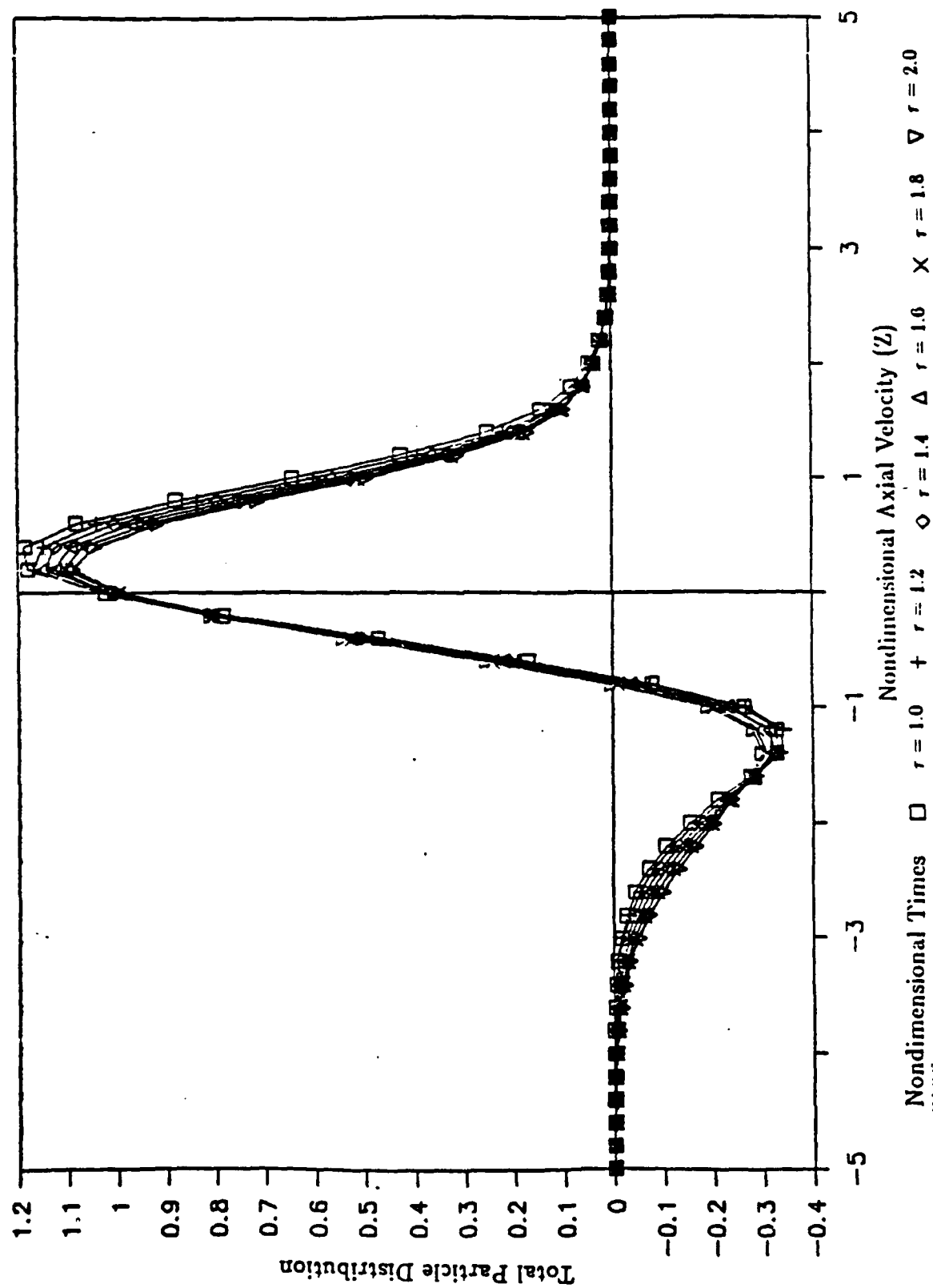


Figure 5.6 Total Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-3}$

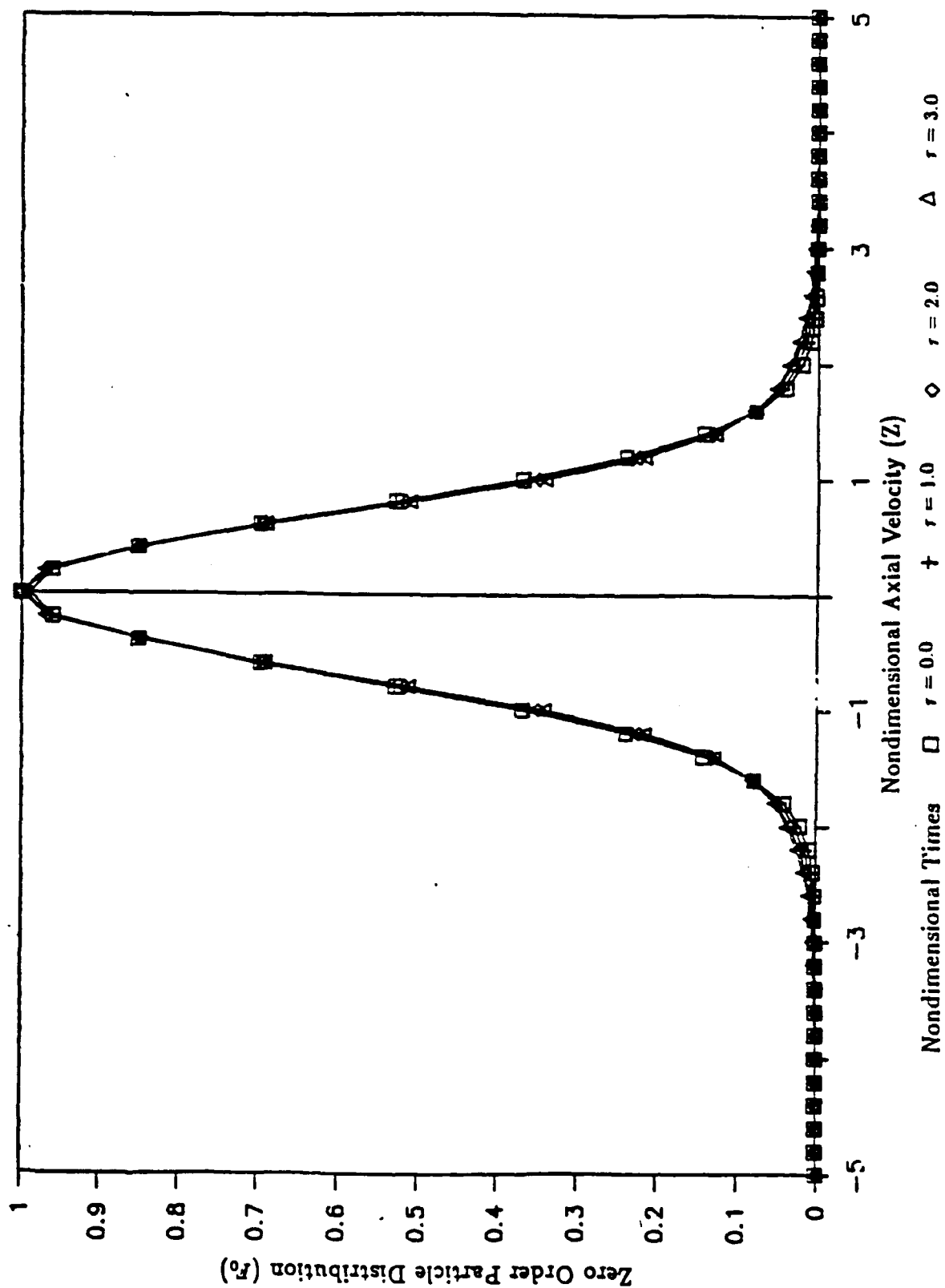


Figure 5.7 Zero Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-5}$

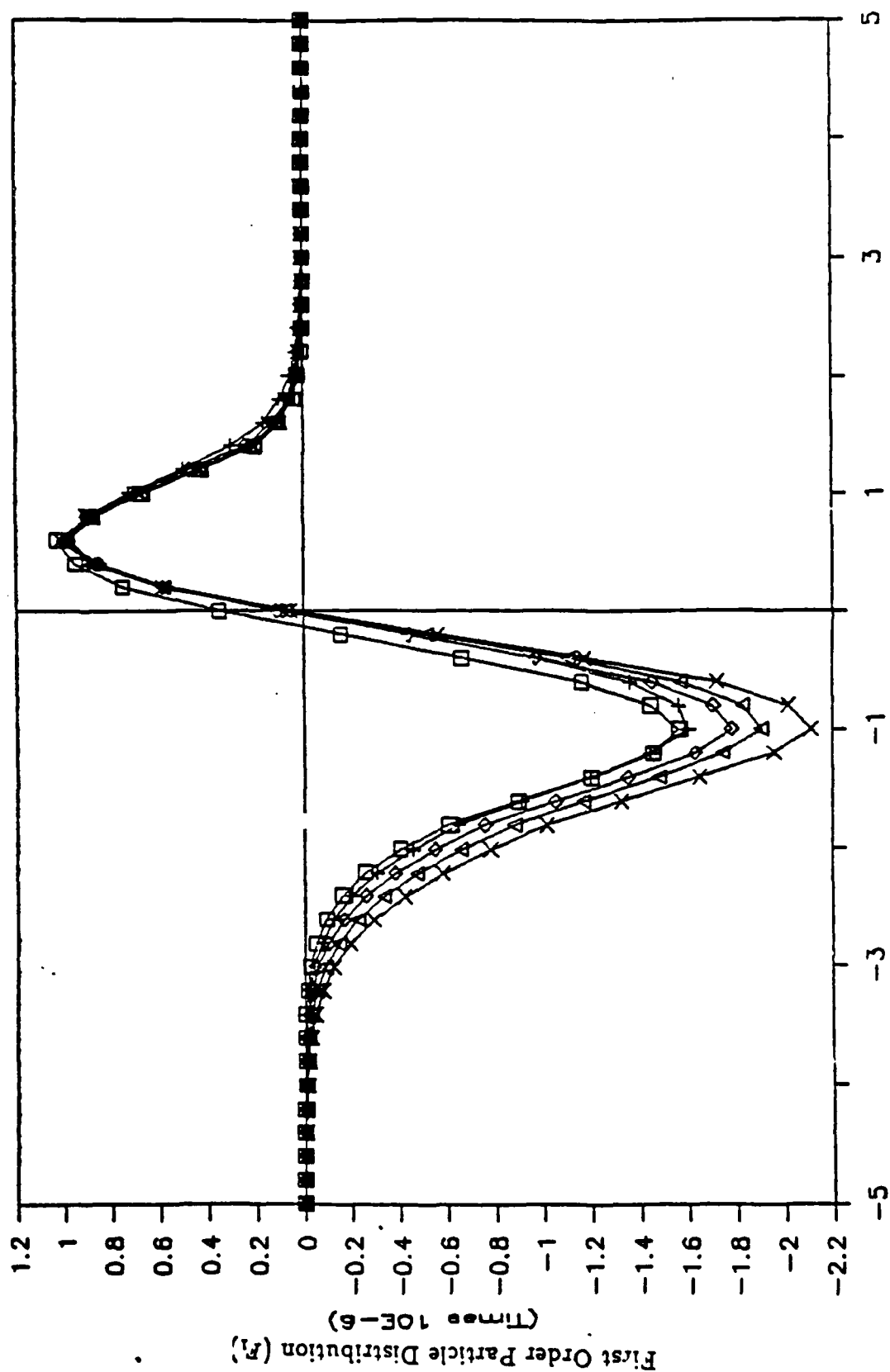


Figure 5.8 First Order Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-6}$

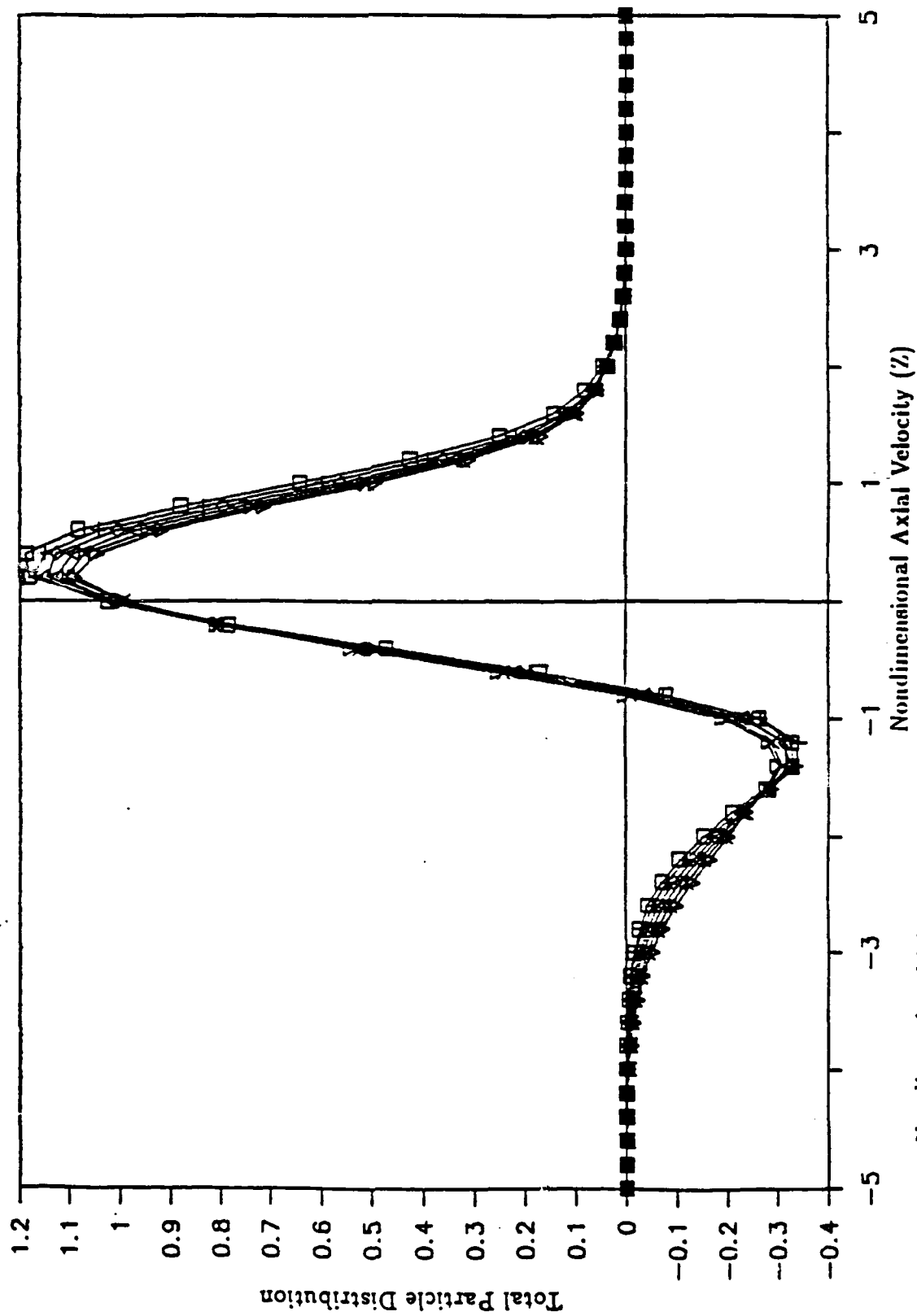


Figure 5.9 Total Particle Velocity Distribution, $\varphi_1 = 1.0 \times 10^{-5}$

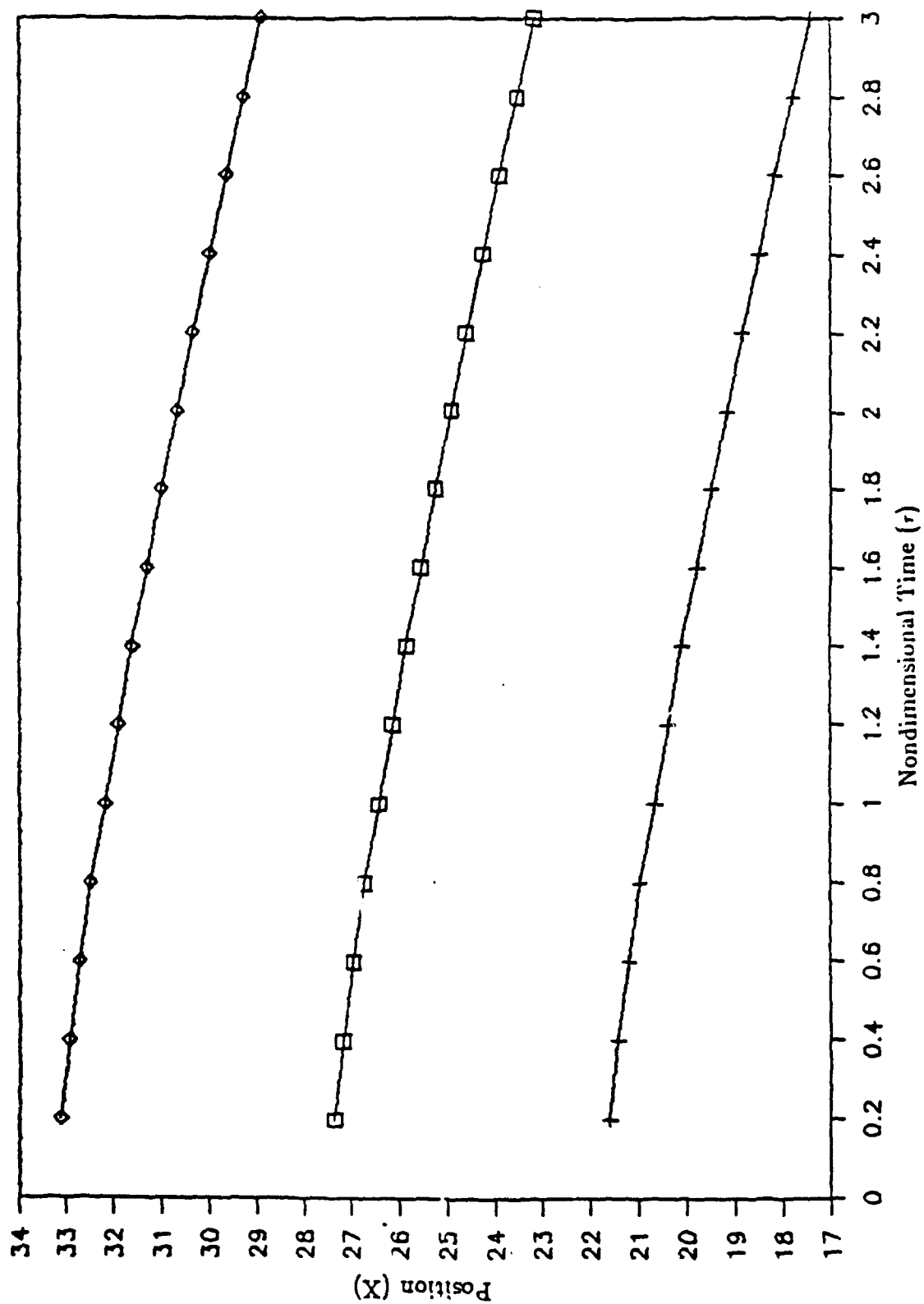


Figure 5.10 Time Dependent Position of the Potential

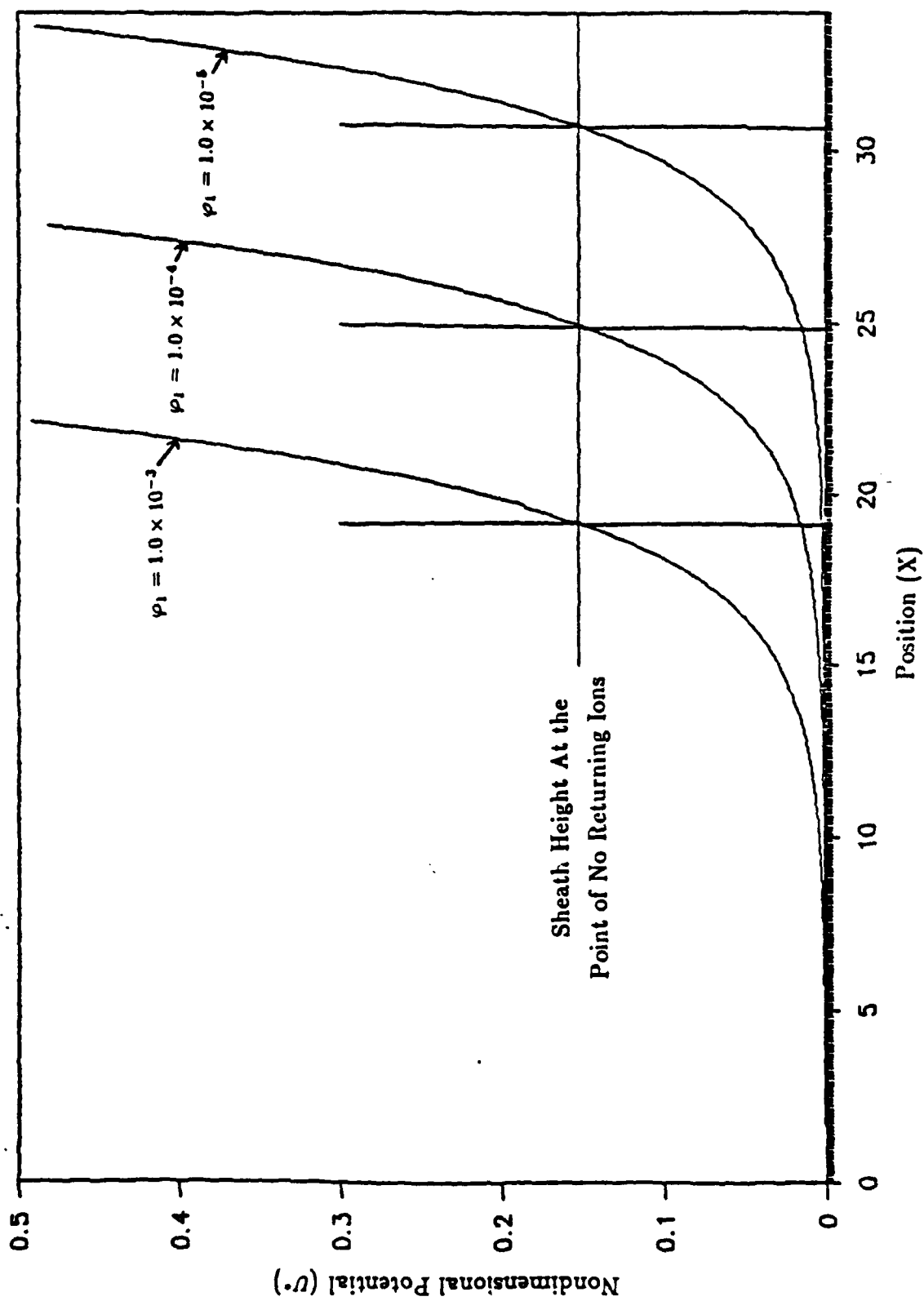


Figure 5.11 Potential Structure of the Presheath

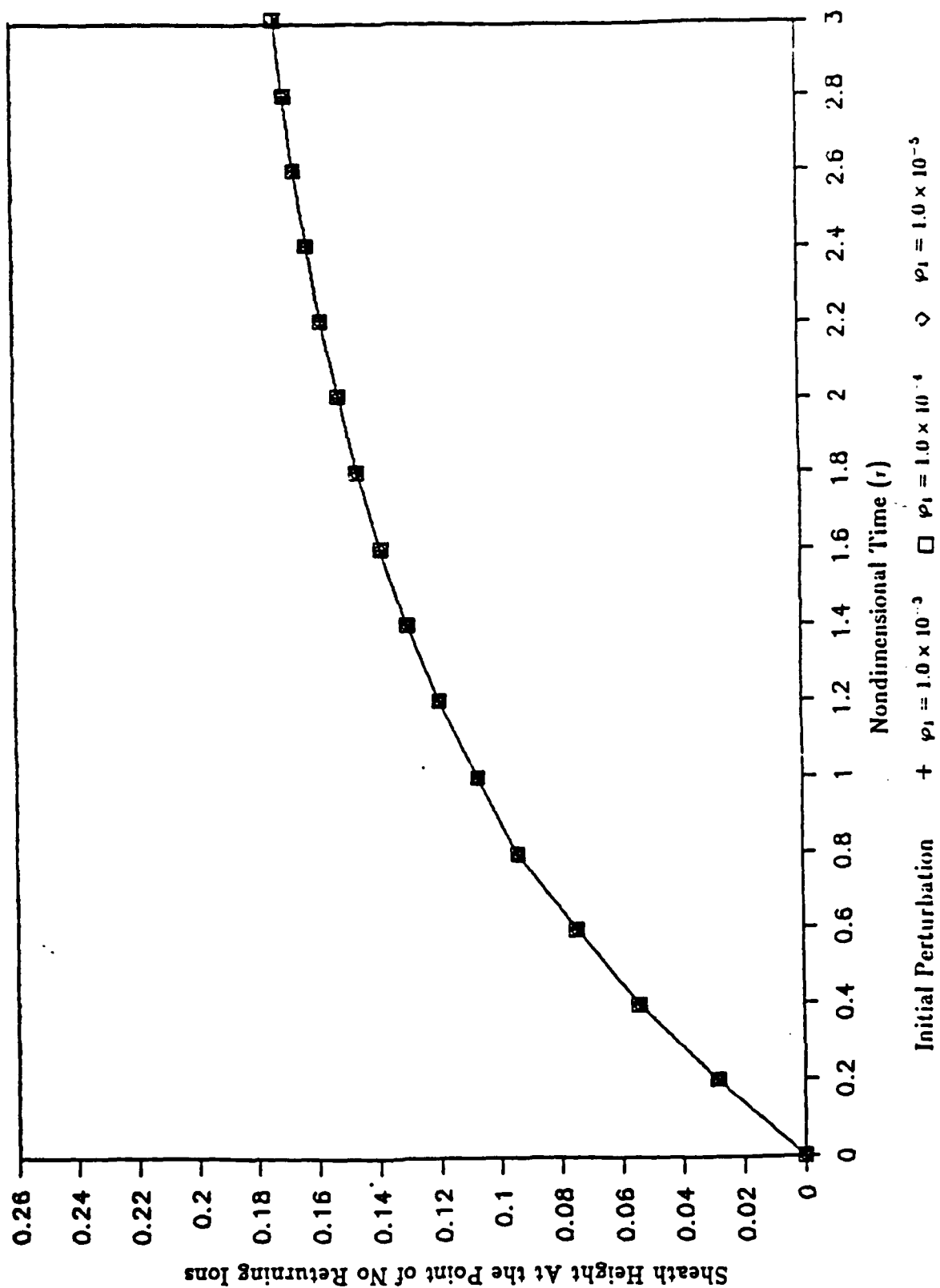


Figure 5.12 Time Dependent Structure of the Sheath Height

APPENDIX: PROGRAM LISTING

.....

* THIS PROGRAM WAS WRITTEN BY JEFFREY P. DANSEREAU

*

* THIS VERSION WAS LAST UPDATED ON 7/17/87

.....

C

C THIS PROGRAM IS A TIME DEPENDENT MODEL OF THE SHEATH -
C PRESHEATH OF A PLASMA. IT USES A FOKKER-PLANCK COLLISION
C TERM WITH ONLY COULOMB COLLISIONS. BELOW IS A LIST OF
C THE VARIABLES AND THEIR MEANING

C

C T - DIAGONAL REPRESENTATION OF T MATRIX. 1ST IS DIAGONALS.
C 2ND IS M VEL POS.

C V - 3-D MATRIX OF V COMPONENTS. 1ST POS. IS F'S, 2ND IS
C N PHI POS., 3RD IS M VEL. POS.

C VV - 3-D MATRIX OF V VALUES AFTER INVERSION WITH T MATRIX.
C POS. ARE SAME AS V MATRIX WITH ADDITIONAL ROW FOR BC'S.

C D - 2-D MATRIX OF D VALUES. 1ST POS. IS F'S, 2ND IS M VEL POS.

C DD - 2-D MATRIX OF D VALUES AFTER INVERSION WITH T MATRIX
C PHI- VECTOR OF PHI VALUES

C F - 2-D MATRIX OF DENSITY FUNCTIONS, 1ST POS. IS THE n F'S
C THAT ARE BEING USED. ($n=N-1$). $F(1,X)=F_0$ ECT... THE
C 2ND POS IS THE M VEL POS.

C TSTEP - VALUE OF DELTA T AS TIME IS STEPPED THROUGH

C VSTEP - VALUE OF DELTA V AS VEL. SPACE IS STEPPED THROUGH

C RTIME - CURRENT VALUE OF NON-DIM. TIME

C ETA - CURRENT VEL.

C NETA - ETA PARAMETER IN POISSON EQN

C TOTE - RATIO OF T TO T_0 (T OVER T_0)

C SM - SMALL M(m) IN F-P EQN

C BM - BIG M(M) IN F-P EQN

C AA - a IN F-P EQN

C AP - a' IN F-P EQN

C M - NUMBER OF DIV. IN VEL. SPACE

C N - NUMBER OF PHI VALUES

C ND - NUMBER OF DIAGONALS IN T MATRIX

```

C      TIME - INTEGER VALUE IN TIME LOOP
C      TEND - RTIME TO FINISH SIMULATION
C      L   - INTEGER TIME VALUE TO END SIMULATION
C      FLAG1 - FLAG TO PRINT OR NOT PRINT MATRICES(99 TO PRINT)
C      FLAG2 - FLAG TO PRINT OR NOT PRINT INTERMEDIATE MATRICES
C              (99 TO PRINT)
C      TRBLE - FLAG TO PRINT TROUBLE STATEMENT IF MATRIX IS NOT
C              INVERTABLE
C      B,SOLN - INTERMEDIATE VALUES OF VARIOUS FUNCTIONS
C      X,Y,Z - INTEGER COUNTERS
C
C      THIS PROGRAM STEPS THROUGH TIME SOLVING THE BOLTZMANN EQN FOR
C      VALUES OF THE EXPANDED DENSITY FUNCTION
C
      REAL T(6,8,202),V(6,6,202),B(202),SOLN(202),TEND
      REAL VV(6,6,202),D(6,202),DD(6,202),PHI(6),L
      REAL F(6,202),TSTEP,RTIME,SM,BM,AA,AP,VSTEP,ETA,NETA,TOTE
      REAL FTOTAL(202),S0,DU,DUPHI1
      INTEGER X,Y,Z,M,N,ND,TIME,TRBLE,FLAG1,FLAG2,FLAG3,P,PSTEP,SKIP
C
C      READ IN PARAMETERS AND PRINT THEM
C
      OPEN(UNIT=2,FILE='INITDAT.DAT',STATUS='OLD')
      READ(2,705) M,NETA,TOTE,AA,AP,SM,FLAG3,SKIP,S0
      READ(2,707) BM,VSTEP,N,ND,TEND,TSTEP,FLAG1,FLAG2
      CLOSE(UNIT=2)
705  FORMAT(I4,1X,F6.4,1X,F6.4,1X,F6.4,1X,F6.4,1X,F6.4,1X,I3,1X,
+        I3,1X,F9.4,/)
707  FORMAT(1X,F6.4,1X,F6.4,1X,I4,1X,I4,1X,F8.5,1X,F7.5,1X,I3,1X,I3)
      OPEN(UNIT=1,FILE='PHI.OUT',STATUS='UNKNOWN')
      OPEN(UNIT=3,FILE='FPSHETH.OUT',STATUS='UNKNOWN')
      WRITE(3,717) '.....'
      +      ,.....
717  FORMAT(A,A)
      WRITE(3,711) 'FOKKER - PLANCK SIMULATION OUTPUT'
      WRITE(3,717) '.....'
      +      ,.....
      WRITE(3,710) 'INPUT PARAMETERS'
      WRITE(3,715) 'NUMBER OF VEL. STEPS - M',M
      WRITE(3,715) 'NUMBER OF PHI VALUES - N',N

```

```

WRITE(3,715) 'NUMBER OF DIAGONALS IN T MATRIX - ND',ND
WRITE(3,720) 'VALUE OF ETA IN POISSON EQN - NETA',NETA
WRITE(3,720) 'VALUE OF T OVER TE - TOTE',TOTE
WRITE(3,720) 'SIZE OF EACH VEL. STEP - VSTEP',VSTEP
WRITE(3,720) 'SIZE OF EACH TIME STEP - TSTEP',TSTEP
WRITE(3,720) 'VALUE OF ENDING TIME FOR SIMULATION',TEND
WRITE(3,720) 'VALUE OF A PARAMETER IN F-P EQN - AA',AA
WRITE(3,720) 'VALUE OF A PRIME PARAMETER IN F-P EQN - AP',AP
WRITE(3,720) 'VALUE OF SMALL M IN F-P EQN - SM',SM
WRITE(3,720) 'VALUE OF BIG M IN F-P EQN - BM',BM
WRITE(3,716) 'FLAG TO PRINT PRIMARY MATRICES(99 TO PRINT)',
+      ' - FLAG1',FLAG1
WRITE(3,716) 'FLAG MAKE FDATA AND PHIDAT NEW FINAL VALUES',
+      '(99 = YES) - FLAG3',FLAG3
WRITE(3,715) 'TIME SKIP FOR PRINT OF F FILE - SKIP',SKIP
716 FORMAT(5X,A,A,2X,I3)
WRITE(3,710) ' '
710 FORMAT(15X,A,/)
711 FORMAT(8X,A,/)
715 FORMAT(5X,A,2X,I3)
720 FORMAT(5X,A,2X,F9.5)
C
C  MAKE NON TIME DEPENDENT QUANTITIES AND INITIAL APPROXIMATIONS
C  TO F'S, PHI'S, AN THE BC
C
DU=0.0
DUPHI1=0.0
CALL MAKEF(M,F)
CALL MAKEPHI(N,RTIME,PHI)
CALL TOT(F,FTOTAL,PHI,N,M,VSTEP,DU,DUPHI1)
TT=0.0
CALL CONSERV(F,VSTEP,TT,M)
C
C  *****
C
C  START MAIN TIME LOOP
C
C  *****
C
C

```

```

C   COMPUTE END LOOP TIME L
C
L=TEND/TSTEP
PSTEP=0
C
DO 40 TIME=1,INT(L)+1
C   PRINT RESULTS OF CURRENT TIME STEP
C
PSTEP=PSTEP+1
IF (TIME.LE.3) GOTO 1000
IF (PSTEP.GE.SKIP) THEN
PSTEP=0
GOTO 1000
ENDIF
GOTO 1001
1000 WRITE(3,350) 'TIME = ',RTIME,'TSTEP = ',TIME-1
DO 210 Z=1,N
WRITE(3,250) 'PHI(',Z-2,') = ',PHI(Z)
210 CONTINUE
WRITE(3,351) 'DU = ',DU,'DU*PHI(1) = ',DUPHI1
WRITE(3,711) ' '
WRITE(3,275) 'M','ETA','F0','F1','F2','F3','FTOTAL'
ETA=-5.0
DO 220 X=1,M
WRITE(3,300) X,ETA,F(1,X),F(2,X),F(3,X),FTOTAL(X)
ETA=ETA+VSTEP
220 CONTINUE
1001 WRITE(3,710) ' '
WRITE(1,813) TIME,RTIME,PHI(1),PHI(2),PHI(3),DU,DUPHI1
813 FORMAT(I3,1X,F7.4,1X,E13.6,1X,E13.6,1X,E13.6,1X,E13.6,
+ 1X,E13.6)
IF (TIME.GT.INT(L)) GOTO 40
WRITE(*,946) 'CURRENTLY IN TIME STEP',TIME,'OF',INT(L)
946 FORMAT(5X,A,I4,2X,A,I4)
C
C   MAKE TIME DEPENDENT QUANTITIES T MATRIX, V MATRIX, D MATRIX
C
DO 445 JJ=1,2
CALL MAKET(ND,M,F,VSTEP,SM,BM,AA,AP,TSTEP,S0,PHI,N,T)
CALL MAKEV(N,M,F,VSTEP,V)

```

```

CALL MAKED(M,F,VSTEP,TSTEP,SM,BM,AA,AP,N,PHI,D)
C
C   INVERT T MATRIX WITH V VECTORS, MAKING VV MATRIX
C
      DO 50 X=1,N-1
        DO 60 Y=3,N
          DO 70 Z=1,M
            B(Z)=V(X,Y,Z)
70      CONTINUE
          CALL MODIAG(M,ND,T,B,SOLN,TRBLE,X)
          IF (TRBLE.EQ.999) THEN
            WRITE(3,*) 'MATRIX HAS NO SOLUTION'
            TRBLE=0
          ENDIF
          DO 80 Z=1,M
            VV(X,Y,Z)=SOLN(Z)
80      CONTINUE
60      CONTINUE
50      CONTINUE
C
C   INVERT T MATRIX WITH D VECTORS, MAKING DD MATRIX
C
      DO 90 X=1,N-1
        DO 100 Y=1,M
          B(Y)=D(X,Y)
100     CONTINUE
          CALL MODIAG(M,ND,T,B,SOLN,TRBLE,X)
          IF (TRBLE.EQ.999) THEN
            WRITE(3,*) 'MATRIX HAS NO SOLUTION'
            TRBLE=0
          ENDIF
          DO 110 Y=1,M
            DD(X,Y)=SOLN(Y)
110     CONTINUE
90      CONTINUE
C
C   GET NEW F VALUES FROM NEW PHI VALUES
C
      DO 160 X=1,N-1
        IF ((JJ.EQ.1).AND.(X.EQ.2)) GOTO 160

```

```

      IF ((JJ.EQ.2).AND.(X.EQ.1)) GOTO 160
      DO 165 Z=1,M
        F(X,Z)=0.0
165    CONTINUE
      DO 170 Y=3,N
        DO 180 Z=1,M
          F(X,Z)=F(X,Z)+PHI(Y)*VV(X,Y,Z)
180    CONTINUE
170    CONTINUE
      DO 190 Z=1,M
        F(X,Z)=F(X,Z)+DD(X,Z)
190    CONTINUE
180    CONTINUE
      CALL AVE(F,M,N,JJ)
C
445    CONTINUE
C
C    GET NEW PHI VALUES
C
      CALL DENSITY(N,M,PHI,F,TOTE,VSTEP)
C
C    MAKE TOTAL DENSITY
C
      CALL TOT(F,FTOTAL,PHI,N,M,VSTEP,DU,DUPHI1)
C
      TT=RTIME+TSTEP
      CALL CONSERV(F,VSTEP,TT,M)
C
C    INCREASE REAL TIME TO NEXT POSITION
C
      RTIME=RTIME+TSTEP
C
C    CONTINUE TIME LOOP
C
40    CONTINUE
C    .....
C
C    END TIME LOOP
C
C    .....

```

```

C
C   FORMAT STATEMENTS FOR PRINTS
C
250  FORMAT(5X,A,I4,A,1X,E13.6)
275  FORMAT(2X,A,2X,A,9X,A,12X,A,12X,A,12X,A,10X,A)
300  FORMAT(I3,1X,F5.2,1X,E13.6,1X,E13.6,1X,E13.6,1X,E13.6,1X,E12.5)
350  FORMAT(5X,A,F7.4,10X,A,I5,/)
351  FORMAT(5X,A,E13.6,5X,A,E13.6)
      CLOSE(UNIT=3)
      IF (FLAG3.EQ.99) THEN
          OPEN(UNIT=4,FILE='FDATA.DAT',STATUS='UNKNOWN')
          DO 265 X=1,M
              WRITE(4,266) F(1,X),F(2,X),F(3,X),F(4,X)
266          FORMAT(E13.6,1X,E13.6,1X,E13.6,1X,E13.6)
265      CONTINUE
          CLOSE(UNIT=1)
          OPEN(UNIT=8,FILE='PHIDAT.DAT',STATUS='UNKNOWN')
          DO 267 X=1,N
              WRITE(8,268) RTIME
              WRITE(8,268) PHI(X)
268          FORMAT(E13.6)
267      CONTINUE
      ENDIF
      STOP
      END

```

```

REAL F(6,202),ETA,VSTEP,NETA,TOTE,B,PI,C
INTEGER X,M,Z
OPEN(UNIT=3,FILE='FDATA.DAT',STATUS='UNKNOWN')
ETA=-5.0
PRINT*,'INPUT M,VSTEP'
READ(*,*) M,VSTEP
N=M-(M-1)/2
DO 10 X=1,N
    F(1,X)=EXP(-(ETA**2))
    F(2,X)=0.0
    F(3,X)=0.0
    F(4,X)=0.0
    ETA=ETA+VSTEP

```

```

10  CONTINUE
    Z=1
    DO 30 X=M,N+1,-1
        DO 40 Y=1,4
            F(1,X)=F(1,Z)
40  CONTINUE
        Z=Z+1
30  CONTINUE
    DO 20 X=1,M
        WRITE(3,100) F(1,X),F(2,X),F(3,X),F(4,X)
100  FORMAT(E13.6,1X,E13.6,1X,E13.6,1X,E13.6)
20  CONTINUE
    STOP
    END

```

```

REAL PHI(6),RTIME
INTEGER N,X
N=5
RTIME=0.0
WRITE(*,*) 'INPUT PHI(-1)'
READ(*,200) PHI(1)
WRITE(*,*) 'INPUT PHI(0)'
READ(*,200) PHI(2)
200  FORMAT(F10.5)
WRITE(*,*) 'INPUT PHI(1)'
READ(*,200) PHI(3)
DO 10 X=4,N
    PHI(X)=0.0
10  CONTINUE
    OPEN(UNIT=9,FILE='PHIDAT.DAT',STATUS='UNKNOWN')
    WRITE(9,120) RTIME
    DO 20 X=1,N
        WRITE(9,120) PHI(X)
120  FORMAT(E13.6)
20  CONTINUE
    RETURN
    END

```

```

SUBROUTINE CONSERV(F,VSTEP,T,M)
REAL F(6,202),F0(202),VSTEP,ZF(202),Z2F(202),ENER,MOM,DEN,T,ETA
INTEGER X,M
ETA=-5.0
DO 10 X=1,M
    F0(X)=F(1,X)
    ZF(X)=F(1,X)*ETA
    Z2F(X)=ZF(X)*ETA
    ETA=ETA+VSTEP
10  CONTINUE
CALL SIMPS(F0,M,VSTEP,DEN)
CALL SIMPS(ZF,M,VSTEP,MOM)
CALL SIMPS(Z2F,M,VSTEP,ENER)
OPEN(UNIT=9,FILE='CONSERV.OUT',STATUS='UNKNOWN')
WRITE(9,100) T,DEN,MOM,ENER
100 FORMAT(2X,F8.5,1X,E13.6,1X,E13.6,1X,E13.6)
RETURN
END

```

```

SUBROUTINE DENSITY(N,M,PHI,F,TOTE,VSTEP)
REAL F(6,202),PHI(6),TOTE,VSTEP,G(202),R(4),NO(6)
INTEGER M,N,X,Y
DO 10 X=1,N-1
    DO 20 Y=1,M
        G(Y)=F(X,Y)
20  CONTINUE
    CALL SIMPS(G,M,VSTEP,NO(X))
10  CONTINUE
R(1)=NO(2)/NO(1)
R(2)=NO(3)/NO(1)
R(3)=NO(4)/NO(1)
PHI(3)=-PHI(2)*R(1)/(2.0*TOTE)
PHI(4)=PHI(2)*(((PHI(3)/PHI(2))**2)*((2.0*TOTE)**2)/2.0)-R(2)
+      /(2.0*TOTE)
PHI(5)=PHI(2)*(((2.0*TOTE)**2)*PHI(3)*PHI(4)/(PHI(2)**2))
+      -(((2.0*TOTE)**3)*((PHI(3)/PHI(2))**3)/6.0)-R(3))/(2.0*TOTE)
RETURN
END

```

```

SUBROUTINE MAKEF(M,F)
REAL F(6,202)
INTEGER X,M
OPEN(UNIT=8,FILE='FDATA.DAT',STATUS='UNKNOWN')
DO 10 X=1,M
    READ(8,100) F(1,X),F(2,X),F(3,X),F(4,X)
100    FORMAT(E13.6,1X,E13.6,1X,E13.6,1X,E13.6)
10    CONTINUE
RETURN
END

```

```

SUBROUTINE MAKEPHI(N,RTIME,PHI)
REAL PHI(6),RTIME
INTEGER N,X
OPEN(UNIT=9,FILE='PHIDAT.DAT',STATUS='UNKNOWN')
READ(9,120) RTIME
DO 20 X=1,N
    READ(9,120) PHI(X)
120    FORMAT(E13.6)
20    CONTINUE
RETURN
END

```

```

SUBROUTINE MAKEV(N,M,F,VSTEP,V)
REAL F(6,202),V(6,6,202),VSTEP,FD1(6),Z,ETA
INTEGER N,M,X,Y,R,S
ETA=-5.0
DO 10 X=1,M
    CALL FD1(F,N,M,X,VSTEP,FD1)
    IF ((X.EQ.1).OR.(X.EQ.M)) THEN
        DO 15 Y=1,N-1
            DO 17 R=3,N
                V(Y,R,X)=0.0
17            CONTINUE
15        CONTINUE
    ELSE
        DO 20 Y=1,N-1

```

```

      Z=1.0
      S=1
      DO 30 R=3,N
        IF (S.GT.(Y-1)) THEN
          V(Y,R,X)=0.0
        ELSE
          V(Y,R,X)=-Z*FD1(Y-R+2)
        ENDIF
        S=S+1
        Z=Z+1.0
30      CONTINUE
20      CONTINUE
      ENDIF
      ETA=ETA+VSTEP
10     CONTINUE
      RETURN
      END

```

```

SUBROUTINE MAKED(M,F,VSTEP,TSTEP,SM,BM,AA,AP,N,PHI,D)
REAL VSTEP,TSTEP,SM,BM,AA,AP,F(6,202),D(6,202),A(6,202),PHI(6)
REAL FD1(6),FD2(6),AH(202),BH(202),B(6,202)
REAL ETA,GD1,GD2
INTEGER N,M,X,Y,Z
DO 10 X=1,N-1
  CALL GETAB(F,VSTEP,M,SM,BM,AA,AP,AH,BH,X)
  DO 15 Y=1,M
    A(X,Y)=AH(Y)
    B(X,Y)=BH(Y)
15  CONTINUE
10  CONTINUE
  DO 17 Y=1,N-1
    D(Y,M)=0.0
    D(Y,1)=0.0
17  CONTINUE
  ETA=-5.0+VSTEP
  DO 20 X=2,M-1
    DO 19 Z=1,N-1
      D(X,Z)=0.0
    DO 20 Z=1,Y

```

```

        IF (Z.LE.Y-1) THEN
            GD2=(A(Z+1,X+1)*F(Y-Z,X+1)-2.0*
+           A(Z+1,X)*F(Y-Z,X)+A(Z+1,X-1)*F(Y-Z,X-1))/(VSTEP**2)
            GD1=(B(Z+1,X+1)*F(Y-Z,X+1)-B(Z+1
+           ,X-1)*F(Y-Z,X-1))/(2.0*VSTEP)
            D(Y,X)=D(Y,X)+GD2+GD1
        ENDIF
40      CONTINUE
        D(Y,X)=D(Y,X)+F(Y,X)/TSTEP
30      CONTINUE
        ETA=ETA+VSTEP
20      CONTINUE
        RETURN
    END

```

```

SUBROUTINE FD1(F,N,M,X,VSTEP,FD1)
REAL F(6,202),FD1(6),VSTEP
INTEGER Y,X,N,M
DO 10 Y=1,N-1
    IF (X.LE.2) THEN
        FD1(Y)=(-F(Y,X+2)+4.0*F(Y,X+1)-3.0*F(Y,X))/(2.0*VSTEP)
    ELSE IF (X.GE.M-1) THEN
        FD1(Y)=(3.0*F(Y,X)-4.0*F(Y,X-1)+F(Y,X-2))/(2.0*VSTEP)
    ELSE
        FD1(Y)=(F(Y,X+1)-F(Y,X-1))/(2.0*VSTEP)
    ENDIF
10  CONTINUE
    RETURN
END

```

```

SUBROUTINE MAKET(ND,M,F,VSTEP,SM,BM,AA,AP,TSTEP,S0,PHI,N,T)
REAL VSTEP,TSTEP,SM,BM,AA,AP,F(6,202),T(6,8,202),A(202)
REAL ETA,B(202),PHI(6),P
INTEGER ND,M,X,Y,N,Z
CALL GETAB(F,VSTEP,M,SM,BM,AA,AP,A,B,1)
P=0.0
DO 5 Z=1,N-1

```

```

ETA=-5.0
DO 10 X=1,M
  IF ((X.EQ.M).OR.(X.EQ.1)) THEN
    T(Z,2,X)=0.0
    T(Z,3,X)=1.0
    T(Z,4,X)=0.0
  ELSE
    T(Z,2,X)=((-A(X-1)/VSTEP)+B(X-1)/2.0)/VSTEP
    T(Z,2,X)=T(Z,2,X)-PHI(1)/(2.0*VSTEP)
    T(Z,3,X)=1.0/TSTEP+(2.0*A(X)/(VSTEP**2))
    T(Z,3,X)=T(Z,3,X)+PHI(2)*P*ETA
    T(Z,4,X)=((-A(X+1)/VSTEP-B(X+1)/2.0)/VSTEP)
    T(Z,4,X)=T(Z,4,X)+PHI(1)/(2.0*VSTEP)
  ENDIF
  ETA=ETA+VSTEP
10  CONTINUE
    P=P+1.0
5   CONTINUE
RETURN
END

```

```

SUBROUTINE GETAB(F,VSTEP,M,SM,BM,AA,AP,A,B,Y)
REAL A(202),B(202),AA,AP,F(6,202),VSTEP,Z,SM,BM,E(202)
REAL P(202),H(202),G(202),K(202),DB,DA,S1,S2,S3,S4,S5
INTEGER M,X,Y,N
Z=-5.0
DO 10 X=1,M
  CALL FINDA(F,Z,VSTEP,AA,AP,M,A(X),Y)
  CALL FINDB(F,Z,VSTEP,AA,AP,SM,BM,M,B(X),Y)
  Z=Z+VSTEP
10  CONTINUE
ETA=-5.0
DO 20 X=1,M
  H(X)=B(X)*F(Y,X)
  G(X)=A(X)*F(Y,X)
  K(X)=ETA*B(X)*F(Y,X)
  P(X)=ETA*A(X)*F(Y,X)
  E(X)=F(Y,X)
  ETA=ETA+VSTEP
20  CONTINUE

```

```

20  CONTINUE
    CALL SIMPS(H,M,VSTEP,S1)
    CALL SIMPS(G,M,VSTEP,S2)
    CALL SIMPS(K,M,VSTEP,S3)
    CALL SIMPS(P,M,VSTEP,S4)
    CALL SIMPS(E,M,VSTEP,S5)
    IF (S5.EQ.0.0) RETURN
    DB=-S1/S5
    DA=-(S2-S3-DB*S4)/S5
    DO 30 X=1,M
        B(X)=B(X)+DB
        A(X)=A(X)+DA
30  CONTINUE
    RETURN
    END

SUBROUTINE FINDA(F,Z,VSTEP,AA,AP,M,A,Y)
REAL F(6,202),Z,VSTEP,AA,AP,A,ETA,SOLN,H(202),FD2
INTEGER X,M,Y
ETA=-5.0
DO 10 X=1,M
    CALL FD2(F,M,X,VSTEP,FD2,Y)
    H(X)=FD2*ABS(ETA-Z)
    ETA=ETA+VSTEP
10  CONTINUE
    CALL SIMPS(H,M,VSTEP,SOLN)
    A=(SOLN*AA)/(2.0*AP)
    RETURN
    END

```

```

SUBROUTINE FINDB(F,Z,VSTEP,AA,AP,SM,BM,M,B,Y)
REAL F(6,202),Z,VSTEP,AA,AP,B,ETA,G2,SOLN
REAL J(202),FD3,SM,BM
INTEGER X,M,Y
ETA=-5.0
DO 10 X=1,M
    CALL FD3(F,M,X,VSTEP,FD3,Y)

```

```

      J(X)=FD3*ABS(ETA-Z)
      ETA=ETA+VSTEP
10  CONTINUE
      CALL SIMPS(J,M,VSTEP,SOLN)
      B=-(AA/AP)*(SM/(2.0*BM))*SOLN
      RETURN
      END

```

```

SUBROUTINE SIMPS(F,N,H,RESULT)
REAL F(202),H,RESULT
INTEGER N,NPANEL,NHALF,NBEGIN,NEND
NPANEL=N-1
NHALF=NPANEL/2
NBEGIN=1
RESULT=0.0
IF ((NPANEL-2*NHALF).NE.0) THEN
      RESULT=3.0*H/8.0*(F(1)+3.0*F(2)+3.0*F(3)+F(4))
      NBEGIN=4
      IF (N.EQ.4) RETURN
ENDIF
RESULT=RESULT+H/3.0*(F(NBEGIN)+4.0*F(NBEGIN+1)+F(N))
NBEGIN=NBEGIN+2
IF (NBEGIN.EQ.4) RETURN
NEND=N-2
DO 10 I=NBEGIN,NEND,2
      RESULT=RESULT+H/3.0*(2.0*F(I)+4.0*F(I+1))
10  CONTINUE
RETURN
END

```

```

SUBROUTINE FD2(F,M,X,VSTEP,FD2,Y)
REAL F(6,202),FD2,VSTEP
INTEGER X,M,Y
IF (X.LE.1) THEN
      FD2=(F(Y,X+2)-2.0*F(Y,X+1)+F(Y,X))/(VSTEP**2)
ELSE IF (X.GE.M) THEN
      FD2=(F(Y,X)-2.0*F(Y,X-1)+F(Y,X-2))/(VSTEP**2)

```

ELSE

FD2=(F(Y,X+1)-2.0*F(Y,X)+F(Y,X-1))/(VSTEP**2)

ENDIF

RETURN

END

SUBROUTINE FD3(F,M,X,VSTEP,FD3,Y)

REAL F(6,202),FD3,VSTEP

INTEGER X,M,Y

IF (X.LE.2) THEN

FD3=(F(Y,X+3)-3.0*F(Y,X+2)+3.0*F(Y,X+1)-F(Y,X))/(VSTEP**3)

ELSE IF (X.GE.M-1) THEN

FD3=(F(Y,X)-3.0*F(Y,X-1)+3.0*F(Y,X-2)-F(Y,X-3))/(VSTEP**3)

ELSE

FD3=(F(Y,X+2)-2.0*F(Y,X+1)+2.0*F(Y,X-1)-F(Y,X-2))/
+ (2.0*(VSTEP**3))

ENDIF

RETURN

END

SUBROUTINE MODIAG(M,D,MATRIX,C,SOLN,TRBLE,N)

REAL A(8,202),B,SOLN(202),MATRIX(6,8,202),C(202)

INTEGER M,D,W,X,Y,Z,TRBLE,N,I,MN1

TRBLE=0

DO 10 X=1,D+2

DO 20 Y=1,M

IF (X.EQ.D+2) THEN

A(X,Y)=C(Y)

ELSE

A(X,Y)=MATRIX(N,X,Y)

ENDIF

20 CONTINUE

10 CONTINUE

DO 30 I=2,M

A(2,I)=A(2,I)/A(3,I-1)

A(3,I)=A(3,I)-A(2,I)*A(4,I-1)

A(5,I)=A(5,I)-A(2,I)*A(5,I-1)

```

30  CONTINUE
    DO 80 X=1,M
      IF (A(3,X).EQ.0) THEN
        PRINT*, 'MATRX HAS NO SOLUTION'
        TRBLE=999
        GOTO 999
      ENDIF
80  CONTINUE
    MN1=M-1
    A(5,M)=A(5,M)/A(3,M)
    DO 40 I=MN1,1,-1
      A(5,I)=(A(5,I)-A(4,I)*A(5,I+1))/A(3,I)
40  CONTINUE
    DO 50 X=1,M
      SOLN(X)=A(5,X)
50  CONTINUE
999  RETURN
    END

```

```

SUBROUTINE AVE(F,M,N,JJ)
REAL F(6,202)
INTEGER X,N,M,Z,JJ
DO 443 Z=1,N-1
  IF ((JJ.EQ.1).AND.(Z.EQ.2)) GOTO 443
  IF ((JJ.EQ.2).AND.(Z.EQ.1)) GOTO 443
  DO 444 X=2,M-1
    F(Z,X)=(.025*F(Z,X-1)+F(Z,X)+.025*F(Z,X+1))/1.05
444  CONTINUE
443  CONTINUE
    RETURN
    END

```

```

SUBROUTINE TOT(F,FTOTAL,PHI,N,M,VSTEP,DU,DUPHI1)
REAL F(6,202),FTOTAL(202),PHI(6),VSTEP,G(202),NO(6),DU
REAL X1,X2,TOL,F1,F2,XERR
INTEGER M,N,X,Y,NLIM
L=(M+1)/2

```

```

DO 10 X=1,N-1
    DO 20 Y=1,L
        G(Y)=F(X,Y)
20    CONTINUE
        CALL SIMPS(G,L,VSTEP,NO(X))
10    CONTINUE
    X1=0.0
    X2=1.0E6
    TOL=.0001
    NLIM=50
30    CALL FCN(NO,X1,N,F1)
    CALL FCN(NO,X2,N,F2)
    IF (F1*F2.GT.0.0) THEN
        X2=X2*10.0
        IF (X2.GT.1.0E15) THEN
            WRITE(*,*) 'NO SIGN CHANGE UP TO 1E15'
            RETURN
        ENDIF
        GOTO 30
    ENDIF
    DO 40 J=1,NLIM
        DU=(X1+X2)/2.0
        CALL FCN(NO,DU,N,FR)
        XERR=ABS(X1-X2)/2.0
        IF (XERR.LE. TOL) GOTO 1000
        IF (ABS(FR).LE.TOL) GOTO 1000
        IF (FR*X1.GT.0.0) THEN
            X1=DU
            F1=FR
        ELSE
            X2=DU
            F2=FR
        ENDIF
40    CONTINUE
    WRITE(*,*) 'NLIM EXCEEDED'
    RETURN
1000 DO 50 X=1,M
        FTOTAL(X)=0.0
        DO 60 Y=1,N-1
            FTOTAL(X)=FTOTAL(X)+DU**(Y-1)*F(Y,X)

```

APPENDIX B - The TEC program

```

C                                     DOS FILE TECINIT.FOR
C*****
C      TEC DATA INITIALIZATION ACCESS CODE
C      WRITTEN BY GREGORY L RIDDERBUSCH
C      AUGUST 1986
C*****
      REAL ARRAY(9)
      INTEGER IPARAM(5)
      WRITE(*,103)
      OPEN(UNIT=2,FILE='PINDATA.DAT',STATUS='OLD')
      READ(2,101) (ARRAY(I),I=1,9)
      READ(2,102) (IPARAM(I),I=1,5)
10  WRITE(*,104) (ARRAY(I),I=1,7)
      WRITE(*,105)
      READ(*,*) IVALUE
      IF (IVALUE .EQ. 0) THEN
          GOTO 20
      ELSE
          WRITE(*,106)
          READ(*,*) VALUE
          ARRAY(IVALUE)=VALUE
          GOTO 10
      ENDIF
20  WRITE(*,107) (IPARAM(I),I=1,5)
      WRITE(*,110) ARRAY(8),ARRAY(9)
      WRITE(*,105)
      READ(*,*) IVALUE
      IF (IVALUE .EQ. 0) THEN
          GOTO 30
      ELSE
          WRITE(*,108)
          IF (IVALUE .EQ. 6 .OR. IVALUE .EQ. 7) THEN
              READ(*,*) VALUE
              ARRAY(IVALUE+2)=VALUE
              GOTO 20
          ELSE
              READ(*,*) INEW
              IPARAM(IVALUE)=INEW
              GOTO 20
          ENDIF
      ENDIF
30  REWIND(2)
      WRITE(2,101) (ARRAY(I),I=1,9)
      WRITE(2,102) (IPARAM(I),I=1,5)
      CLOSE(2)
      WRITE(*,109)
      STOP

C
101  FORMAT(F8.1/F8.1/F6.3/F6.3/F6.3/F6.3/F7.2/F5.2/F6.1)
102  FORMAT(I1/I1/I3/I3/I3)
103  FORMAT(1X,'*****'/
&'      TEC OPERATING CONDITIONS'/
&1X,'*****')
104  FORMAT(//4X,'CURRENT CONVERTOR OPERATING SETTINGS:'//
&7X,'1.      EMITTER TEMPERATURE: ',F8.1,' KELVIN',/
&7X,'2.      COLLECTOR TEMPERATURE: ',F8.1,' KELVIN',/
&7X,'3.      EMITTER WORK FUNCTION: ',F6.2,' EV'/
&7X,'4.      COLLECTOR WORK FUNCTION: ',F6.2,' EV'/
&7X,'5.      CONVERTOR PRESSURE: ',F6.2,' TORR'/
&7X,'6.      GAP THICKNESS: ',F6.2,' MM'/

```

```

&7X,'7.      OPERATING CURRENT: ',F7.2,' AMPS/CM^2')
105 FORMAT(/4X,'ENTER ID NUMBER OF VALUE TO BE CHANGED, 0=NONE: ')
106 FORMAT(4X,'ENTER NEW OPERATING SETTING: ')
107 FORMAT(/4X,'CURRENT TEC FUNCTION SETTINGS:'//
&7X,'1. DIAGNOSTIC LEVEL: ',I3,'      (0-RESTRICTED OUTPUT)'/
&7X,'      (1-FULL OUTPUT)'/
&7X,'      (2-ENABLE SHEATH DIAGNOSTICS)'/
&7X,'      (3-ENABLE DOT DIAGNOSTICS)'/
&7X,'2. RESTART SEQUENCE: ',I3,'      (0-DEFAULT STARTUP VALUES)'/
&7X,'      (1-RESTART WITH PREVIOUS VALUES)'/
&7X,'3. STEPS BETWEEN PRINTS: ',I3/
&7X,'4.      POINT DENSITY: ',I3,'      (11,21,31,...151)'/
&7X,'5. LOTUS SKIP FACTOR: ',I3,'      (1..99)')
108 FORMAT(4X,'ENTER NEW FUNCTIONAL SETTING: ')
109 FORMAT(1X,'*****'/
&'      '/
&1X,'*****')
110 FORMAT(7X,'6.      TIME STEP: ',F5.2,
&'      (0.1,0.2,0.3,0.4,0.5)'/7X,'7.      END TIME: ',
&F6.1,'      (1.0,2.0,...,10.0)')
END

```

```

C                                                     DOS FILE PRED1.FOR
C*****
C    PROGRAM TEC
C*****
    REAL CNE,ENE,ECHI,CCHI,EALPHA,CALPHA,LAMNEB,LAMTAU
    REAL DTP,T2,AN,AT,CN,CT,BN,BT,RE,KN,TCHAR,PN,DT
    REAL SMR,LAMDAR,NR,TE,TC,ENR,I,ARECN,EGNDB,ELOSSB,NNR
    REAL TAU(0:150),NEB(0:150),DELTAT,SN,ST,PI,CA,CSAHA,DZ
    REAL DTAUNDZ,MUI(0:150),RMUR,TAUN(0:150),EMISS,TIME2,LCCHI
    REAL NDOT1(0:150),TDOT1(0:150),NNB(0:150),TIME1,JNET,CV(0:150)
    REAL FYEN,IVD,IKN,EGRADA,PHIB,EWFCWF,D,ESOURCE(0:150)
    INTEGER N,IDEN,EFIX,CFIX,CHKDOT,ICOUNT,NSTEPS,C,PC,LS,LC,EO,EC

C
COMMON /PRED/ CA,CSAHA,DT,DTAUNDZ,DZ,EGNDB,ELOSSB,ENR,I,IDEN,KN
COMMON /PRED/ LAMDAR,LAMNEB,LAMTAU,MUI,N,NNB,NNR,NR,PI,RE,RMUR
COMMON /PRED/ TAUN,EFIX,CFIX,CHKDOT,FYEN,ENE,ECHI,CCHI,CNE
COMMON /PRED/ EALPHA,CALPHA,CV,ESOURCE,LCCHI

C
data nsteps /1/

C
OPEN (UNIT=2,FILE='PINDATA.DAT',STATUS='OLD')
OPEN (UNIT=4,FILE='EXOUT.DAT',STATUS='UNKNOWN')
OPEN (UNIT=7,FILE='LOTUS1.DAT',STATUS='UNKNOWN')
OPEN (UNIT=8,FILE='PREDRES.DAT',STATUS='OLD')
OPEN (UNIT=9,FILE='PRNTOUT.DAT',STATUS='UNKNOWN')
C....SET ABBREVIATED PRNTDAT SAMPLING POINTS WITH PC
C...SET LOTUS SKIP COUNTER WITH LC
C
    CALL INITIAL(TE,TC,EWFCWF,PN,NSTEPS,DTP,T2,AN,AT,
&CN,CT,BN,BT,TCHAR,SMR,ARECN,DELTAT,SN,ST,TAU,NEB,LS,pc)
    C=PC
    LC=LS
    EO=100*LS
    EC=EO

C
    IF (CHKDOT .EQ. 3)
& OPEN (UNIT=9,FILE='D:PDOTDIAG.DAT',STATUS='UNKNOWN')
    IF (CHKDOT .GT. 1)
& OPEN (UNIT=11,FILE='D:PSTHDIAG.DAT',STATUS='UNKNOWN')

C
C-----
    EGRADA=0.0
    ICALCS=INT(T2/DTP+0.001)
    WRITE(*,76)
    DO 30 ICOUNT=0,ICALCS
        WRITE(*,77) (icount),100*(icount)/ICALCS
        TIME1=(icount)*DTP
        TIME2=(icount+1)*DTP
        CALL PREDCOR(TIME1,TIME2,TAU,NEB,NSTEPS,TE,TC,TDOT1,NDOT1,
& PN,ARECN,TCHAR,AN,AT,BN,BT,CN,CT,IVD,SMR,EGRADA,PHIB,JNET)
        VOUT=EWFCWF + (PHIB + IVD/I + LCCHI)*TE/11600 - CWF
        IF (C .EQ. PC) THEN
            WRITE (9,67) TIME1,VOUT
            IF (CHKDOT .EQ. 0) THEN
                WRITE (9,70)
                WRITE (9,71) (I1,NEB(I1),TAU(I1),I1=1,N)
            ELSE
                EMISS=ENR/NEB(1)
                WRITE(9,72) ENE,ECHI,EALPHA,CNE,LCCHI+CCHI,CALPHA,PHIB,

```

```

&          IVD/I,EMISS
      WRITE(9,73) (I1,NDOT1(I1),NEB(I1),
&          TDOT1(I1),TAU(I1),I1=0,N+1)
      ENDIF
      IF (EFIX .EQ. 1) WRITE(9,74)
      IF (CFIX .EQ. 1) WRITE(9,75)
      C=0
    ENDIF
    C=C+1
    IF (LC .EQ. LS) THEN
      WRITE(7,78) TIME1,VOUT,ENE,JNET,ECHI,CCHI,EALPHA,CALPHA,
&      PHIB,IVD/I,EMISS,NEB(1),NEB(11),TAU(1),TAU(11)
      LC=0
    ENDIF
    LC=LC+1
    IF (EC .EQ. EO) THEN
      WRITE(4,*) TIME1
      WRITE(4,71) (I1,NEB(I1),TAU(I1),I1=1,N)
      EC=0
    ENDIF
    EC=EC+1
30    CONTINUE

```

```

C-----
C*****OUTPUT STARTUP VALUES TO PREDRES.DAT
      WRITE(8,69) ENE,CNE,ECHI,CCHI,EALPHA,CALPHA,N
      WRITE(8,68) (NEB(I1),TAU(I1),I1=0,N+1)
      REWIND(8)
      CLOSE(8)
      STOP

```

```

C
67  FORMAT(//,'RESULTS AT TIME = ',F8.2,4X,'OPERATING VOLTAGE=',F6.3)
68  FORMAT(2F8.3)
69  FORMAT(F9.4/F9.4/F8.3/F8.3/F9.4/F9.4/I3)
70  FORMAT(/3X,' #      NEB(#)      TAU(#)' /
&3X,'-----')
71  FORMAT(3X,I3,4X,F6.3,7X,F5.2)
72  FORMAT(/3X,'ENE =',F8.3,4X,'ECHI=',F8.3,4X,'EALPHA=',F8.3/
&3X,'CNE =',F8.3,4X,'CCHI=',F8.3,4X,'CALPHA=',F8.3/
&3X,'PHIB=',F8.3,4X,'VD =',F8.3,4X,'EMISS =',E8.3/
&/3X,' #      NDOT(#)      NEB(#)      TDOT(#)      TAU(#)',
&/3X,'-----')
73  FORMAT(3X,I3,4X,F7.4,4X,F6.3,7X,F7.4,4X,F5.2)
74  FORMAT('****AT LEAST ONE UNPHYSICAL EMITTER BC WAS INVOKED.')
75  FORMAT('****AT LEAST ONE UNPHYSICAL COLLECTOR BC WAS INVOKED.')
76  FORMAT(/1X,'      TEC CALCULATIONS BEGIN...(WAIT)...')
77  FORMAT(4X,'ITERATION #',I3,'      COMPLETION--',I3,' %')
78  FORMAT(16E13.6)
      END

```

```

C*****
      SUBROUTINE PREDCOR(T1,T2,TAU,NEB,NSTEPS,TE,TC,TDOT1,NDOT1,
+      PN,ARECN,TCHAR,AN,AT,BN,BT,CN,CT,IVD,SMR,EGRADA,PHIB,JNET)
C*****
      REAL T1,T2,DT,AN,AT,BN,BT,CN,CT,IVD,LAMTAU,LAMNEB,CNE
      REAL TAU(0:150),NEB(0:150),TDOT1(0:150),NDOT1(0:150),ENE
      REAL ECHI,CCHI,EALPHA,CALPHA,MUI(0:150),I,DZ,TCHAR,LCCHI
      REAL TE,TC,DTAUNDZ,PN,ENR,NR,EGNDB,ELOSSB,RE,SMR,LAMDAR
      REAL RMUR,KN,NNR,ARECN,PI,CA,CSAHA,NNB(0:150),TAUN(0:150)
      REAL MSOURCE(0:150),ESOURCE(0:150),CV(0:150),MUEA(0:150)
      REAL NDOT2(0:150),TDOT2(0:150),TTILDA(0:150),NTILDA(0:150)
      REAL J,IIVD,AVD,FYEN,EGRADA,PHIB,JNET

```

INTEGER N,CFIX,EFIX,IDEN,CHKDOT,NSTEPS

C

COMMON /PRED/ CA,CSAHA,DT,DTAUNDZ,DZ,EGNDB,ELOSSB,ENR,I,IDEN,KN
COMMON /PRED/ LAMDA, LAMNEB, LAMTAU, MUI, N, NNB, NNR, NR, PI, RE, RMUR
COMMON /PRED/ TAUN, EFIX, CFIX, CHKDOT, FYEN, ENE, ECHI, CCHI, CNE
COMMON /PRED/ EALPHA, CALPHA, CV, ESOURCE, LCCHI

C

C*****HANDLE EXCEPTIONAL CONDITIONS

DZ=1.0/(N-1)
DT=(T2-T1)/NSTEPS
CFIX=0
EFIX=0

C*****SET NEUTRAL TEMPERATURE AND DENSITY

IF (TE.EQ.TC) THEN
DO 10 I1=0,N+1
TAUN(I1)=1.0
10 CONTINUE
ELSE
DO 20 I1=0,N+1
TAUN(I1)=1.0+(TC/TE-1.0)*(I1-1.0)/(N-1)
20 CONTINUE

ENDIF
NNR=965.5E16*PN/TE
DO 30 I1=0,N+1
NNB(I1)=1.0/TAUN(I1)

30 CONTINUE
DTAUNDZ=TAUN(N)-TAUN(1)

C*****SET TRANSPORT PARAMETERS

RMUR=LAMDA*SMR
DO 40 I1=0,N+1
MUI(I1)=SQRT(TAUN(I1))

40 CONTINUE

C*****SET IONIZATION AND SAHA PARAMETERS

CA=0.41283*ARECN*TCHAR*(NR/1.0E14)**2*(TE/1500)**(-4.5)
CSAHA=LOG((1.4027E20*NNR/NR/NR)*(TE/1500)**1.5)

C-----

DO 70 ICOUNT=0,NSTEPS-1

C-----PREDICTOR STEP

IF (CHKDOT.EQ.3) WRITE(9,81)
CALL DOT(NDOT1,TDOT1,NEB,TAU,EGRADA,PHIB,JNET)
DO 45 I1=0,N+1
NTILDA(I1)=NEB(I1)+AN*DT*NDOT1(I1)
TTILDA(I1)=TAU(I1)+AT*DT*TDOT1(I1)

45 CONTINUE

C-----CORRECTOR STEP

IF (AN.EQ.0.0.AND.AT.EQ.0.0) THEN
DO 50 I1=0,N+1
NDOT2(I1)=0.0
TDOT2(I1)=0.0

50 CONTINUE
GOTO 55

ELSE

IF (CHKDOT.EQ.3) WRITE(9,82)
CALL DOT(NDOT2,TDOT2,NTILDA,TTILDA,EGRADA,PHIB,JNET)

ENDIF

55 DO 60 I1=0,N+1
NEB(I1)=NEB(I1)+DT*(BN*NDOT1(I1)+CN*NDOT2(I1))
TAU(I1)=TAU(I1)+DT*(BT*TDOT1(I1)+CT*TDOT2(I1))

60 CONTINUE

70 CONTINUE

```

C-----
C*****UPDATE TIME DERIV.S, IMAGE POINTS, AND FIND PLASMA POWER GAIN
  CV(0)=0.0
  CV(N+1)=0.0
  ESOURCE(0)=0.0
  ESOURCE(N+1)=0.0
  IF (CHKDOT.EQ.3) WRITE(9,83)
  CALL DOT(NDOT1,TDOT1,NEB,TAU,EGRADA,PHIB,JNET)
  IIVD=0.0
  DO 75 I1=2,(N-1)
    IIVD=IIVD+(ESOURCE(I1)-CV(I1)*TDOT1(I1))
75  CONTINUE
  AVD=0.5*(ESOURCE(1)-CV(1)*TDOT1(1))+0.5*(ESOURCE(N)-CV(N)
+    *TDOT1(N))
  IVD=(AVD+IIVD)*DZ+2.0*I*(TAU(1)-TAU(N))-(NEB(1)*ENE/KN)
+    *(TAU(1)-1)
  RETURN
C
81  FORMAT(//,'CALL DOT FOR FIRST TIME.',//)
82  FORMAT(//,'CALL DOT FOR SECOND TIME.',//)
83  FORMAT(//,'CALL DOT FOR LAST TIME.',//)
  END
C

```

```

C
C*****DOS FILE PRED2.FOR*****
SUBROUTINE DOT (NEBDOT, TAUDOT, NEB, TAU, EGRADA, PHIB, JNET)
C*****
REAL A, ALPHA(0:150), BETA(0:150), CA, CALPHA, CCHI, CDETA, CNE, SIGMA
REAL CTETA, CTZ, CV(0:150), CONVECT, D21B, D32B, DT, DZ, DGDU, DELU
REAL DETAP, DTAUNDZ, ESOURCE(0:150), ELOSSB, EGNDB, ETZ, ETETA, DELTAU
REAL ENE, ECHI, ENR, F(15), FYEN, GAMMAP, GAMMAM, GU, I, IB, K(0:150)
REAL LAMTAU, LAMDAR, LAMNEB, MUI(0:150), MSOURCE(0:150), MUISOLD
REAL MURSOLD, MUIS, MURS, MUEA(0:150), NR, NNR, NEB(0:150), NBCOA
REAL NBC1A, NBC1B, NBC1C, NES2, NNB(0:150), NUE, NA(0:150), NB(0:150)
REAL NEBU(0:150), ND(0:150), NS(0:150), NEBDOT(0:150), NEBA(0:150)
REAL NEBV(0:150), PC(0:150), PI, PB, PBP, POHMIC, PO, QKP, QKM, RE, RMUR
REAL TAU(0:150), TAUN(0:150), TAUDOT(0:150), TA(0:150), TB(0:150)
REAL TS(0:150), TUAU(0:150), TAUB(0:150), TAUC(0:150), TAUU(0:150)
REAL TBCOB, TBCOC, TBC1A, TBC1B, TBC1C, U, CSAHA, DETA, EALPHA, KN, KDE
REAL NEBB(0:150), TAUU(0:150), NEBC(0:150), NC(0:150), NBCOB, LCCHI
REAL NBCOC, TC(0:150), TBCOA, JNET, SMR, EGRADA, PHIB, BIGU, JRC, CGRADA
INTEGER CFIX, EFIX, CHKDOT, CFLAG

C
COMMON /PRED/ CA, CSAHA, DT, DTAUNDZ, DZ, EGNDB, ELOSSB, ENR, I, IDEN, KN
COMMON /PRED/ LAMDAR, LAMNEB, LAMTAU, MUI, N, NNB, NNR, NR, PI, RE, RMUR
COMMON /PRED/ TAUN, EFIX, CFIX, CHKDOT, FYEN, ENE, ECHI, CCHI, CNE
COMMON /PRED/ EALPHA, CALPHA, CV, ESOURCE, LCCHI

C
F(1)=5.74E-3
F(2)=1.40E-3
F(3)=2.3
F(4)=0.2
F(5)=2.70E-2
F(6)=5.74E-3
F(7)=4.24E-2
F(8)=2.82
F(9)=0.0
F(10)=11.607
F(11)=0.0
F(12)=27.04

C*****SET THERMAL & ELECTRICAL CONDUCTIVITIES AT 0+ (E) & 1- (C)
IF (TAU(1).LT.0.1) THEN
    TAU(1)=0.1
    EFIX=1
ENDIF
IF (TAU(N).LT.0.1) THEN
    TAU(N)=0.1
    CFIX=1
ENDIF
IF (RE.EQ.0.5) THEN
    DO 10 I1=0, N+1
        MUEA(I1)=TAUN(I1)
    CONTINUE
    10 ENDIF
IF (RE.EQ.0.0) THEN
    DO 20 I1=0, N+1
        MUEA(I1)=TAUN(I1)/SQRT(TAU(I1))
    CONTINUE
    20 ENDIF
IF (RE.EQ.-0.5) THEN
    DO 30 I1=0, N+1
        MUEA(I1)=TAUN(I1)/TAU(I1)

```

```

30     CONTINUE
      ELSE
        DO 40 I1=0,N+1
          MUEA(I1)=TAUN(I1)*(TAU(I1)**(RE-0.5))
40     CONTINUE
      ENDIF
      DO 50 I1=0,N+1
        K(I1)=(RE+2.0)/FYEN*MUEA(I1)*NEB(I1)*TAU(I1)
        PC(I1)=NEB(I1)*(TAU(I1)+TAUN(I1))
50     CONTINUE
      DETA=ALOG(K(2)/K(1))*DZ/(K(2)-K(1))
      DETAP=ALOG(K(2)/K(1))*DZ/(K(2)-K(1))
C*****DETERMINE EMITTER SHEATH*****
      JNET=(I*KN*1.595769)/(SQRT(TAU(1))*NEB(1))
      CALL SHEATH(JNET,ENR/NEB(1),TAU(1),ECHI,PHIB,EALPHA,ENE)
C-----FIND EMITTER (0+) DERIVATIVES FROM B.C.
      IF(ECHI.LE.1E-5.OR.ECHI.GE.20) EFIX=1
      ETETA=(TAU(1)-1)*ENE*NEB(1)/KN-I*(ECHI-TAU(1)/2)
      ETZ=ETETA/K(1)
      EPCZ=(SQRT(PI/8/EALPHA)/LAMDA/KN)*NEB(1)/MUI(1)-I/MUEA(1)
      ENZ=(EPCZ-NEB(1)*(ETZ+DTAUNDZ))/(TAU(1)+TAUN(1))
C*****SOLVE COLLECTOR SHEATH
      CFLAG=0
      CNE=0.0
      U=1.0
      GU=G(U,NEB(N),TAU(N),I,KN)
      DELU=0.05
      DO 80 I1=1,50
        DGDU=(G(U+DELU,NEB(N),TAU(N),I,KN)-GU)/DELU
        DELTAU=-GU/DGDU
        U=U+DELTAU
        GU=G(U,NEB(N),TAU(N),I,KN)
        IF (ABS(GU).LE.0.001) THEN
          CCHI=U*TAU(N)
          GOTO 85
        ENDIF
80     CONTINUE
      CCHI = 0.0
      WRITE(*,205)
      IF (CHKDOT.GT. 1) WRITE(11,205)
C*****DETERMINE DERIVATIVES AT COLLECTOR (1-) FROM B.C.
85    IF (CHKDOT.GT. 1)
      &WRITE(11,206) EGRADA,ALPHA2,TAU(1),ENR/NEB(1),
      &JNET,ECHI,PHIB,ENE,EALPHA,CCHI,CALPHA,IFLAG,RCODE
      DPH = -CCHI/TAU(N)
      IF(DPH.LT.0.0000001) DPH = 0.0000001
      CALPHA=(1.0/TAU(N))*(3.14159265/2)*((1.0 + ERF(SQRT(DPH)))
+ - (1./2.)*(1.0 + ERF(SQRT(4.0*DPH)))**2 / (EXP(-DPH)
+ - (1./4.)*EXP(-4.0*DPH))**2
      LCCHI = 0.0
      IF(CCHI.LT.0.0) THEN
        LCCHI = CCHI
        CCHI = 0.0
      ENDIF
      CTETA=-I*(CCHI-TAU(N)/2.0)
      CTZ=CTETA/K(N)
      CDETA=ALOG(K(N)/K(N-1))*DZ/(K(N)-K(N-1))
      NBC0A=TAU(1)+TAUN(1)
      NBC0B=SQRT(PI/EALPHA/8.0)/LAMDA/KN/MUI(1)-ENE*NEB(1)/K(1)*
+      (TAU(1)-1.0)-DTAUNDZ

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NBC0C=I*NEB(1)/K(1)*(ECHI-TAU(1)/2.0)-I/MUEA(1)
NBC1A=TAU(N)+TAUN(N)
NBC1B=-SQRT(PI/CALPHA/8.0)/LAMDA/KN/MUI(N)-CNE*NEB(N)/K(N)*
+ (TAU(N)-1.0)+DTAUNDZ
NBC1C=-I*NEB(N)/K(N)*(CCHI-TAU(N)/2.0)-I/MUEA(N)
TBC0A=1.0
TBC0B=ENE*NEB(1)/KN+I/2.0
TBC0C=-ENE*NEB(1)/KN-I*ECHI
TBC1A=-1.0
TBC1B=CNE*NEB(N)/KN-I/2.0
TBC1C=-CNE*NEB(N)/KN+I*CCHI
NEBA(0)=(NBC0A*LAMNEB)/(2.0*DZ)
NEBB(0)=-LAMNEB*NBC0B
NEBC(0)=-NBC0A*LAMNEB/(2.0*DZ)
NEBV(0)=NBC0B*(1.0-LAMNEB)*NEB(1)+NBC0C-(1.0-LAMNEB)*
+ NBC0A*(NEB(2)-NEB(0))/(2.0*DZ)
TAUA(0)=TBC0A*LAMTAU/(2.0*DETAP)
TAUB(0)=-LAMTAU*TBC0B
TAUC(0)=-TBC0A*LAMTAU/(2.0*DETAP)
TAUV(0)=TBC0B*(1.0-LAMTAU)*TAU(1)+TBC0C-(1.0-LAMTAU)*
+ TBC0A*(TAU(2)-TAU(0))/(2.0*DETAP)
NEBA(N+1)=(NBC1A*LAMNEB)/(2.0*DZ)
NEBB(N+1)=-LAMNEB*NBC1B
NEBC(N+1)=-NBC1A*LAMNEB/(2.0*DZ)
NEBV(N+1)=NBC1B*(1.0-LAMNEB)*NEB(N)+NBC1C-(1.0-LAMNEB)*
+ NBC1A*(NEB(N+1)-NEB(N-1))/(2.0*DZ)
TAUA(N+1)=TBC1A*LAMTAU/(2.0*CDETA)
TAUB(N+1)=-LAMTAU*TBC1B
TAUC(N+1)=-TBC1A*LAMTAU/(2.0*CDETA)
TAUV(N+1)=TBC1B*(1.0-LAMTAU)*TAU(N)+TBC1C-(1.0-LAMTAU)*
+ TBC1A*(TAU(N+1)-TAU(N-1))/(2.0*CDETA)
C*****INITIALIZE GAMMAP & QKP FOR LOOP
MURS=MUI(2)/MUEA(2)+MUI(1)/MUEA(1)*(1-2*DZ*
+ (0.5-RE)*ETZ/TAU(1)-0.5*DTAUNDZ/TAUN(1))
GAMMAP=0.5*((MUI(1)+MUI(2))*(PC(1)-PC(0))
+ )/DZ+I*MURS)
QKP=(TAU(1)-TAU(0))/DETA
MUIS=MUI(1)+MUI(2)
C-----
DO 100 J=1,N
C-----UPDATE FOR NEW J
GAMMAP=GAMMAP
QKM=QKP
DETA=DETAP
MUISOLD=MUIS
MURSOLD=MURS
IF (J.NE.N) THEN
    DETAP=ALOG(K(J+1)/K(J))*DZ/(K(J+1)-K(J))
    MUIS=MUI(J)+MUI(J+1)
    MURS=MUI(J)/MUEA(J)+MUI(J+1)/MUEA(J+1)
ELSE
    MURS=MURS+2*DZ*(MUI(N)/MUEA(N))*((0.5-RE)*CTZ/TAU(N)
+ -0.5*DTAUNDZ/TAUN(N))
ENDIF
C-----FIND AMBIPOLAR FLUX AT J+1/2
GAMMAP=0.5*((MUIS*(PC(J+1)-PC(J)))/DZ+I*MURS)
C-----FIND MASS SOURCE AT J
A=CA/TAU(J)**4.5
NES2=NNB(J)*TAU(J)**1.5*EXP(CSAHA-EGNDB/TAU(J))
D21B=F(7)*(1+F(8)/TAU(J))

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D32B=F(2)*EXP(F(3)/TAU(J))
IB=A*NES2*(1+F(1)/NEB(J))/(1+D21B*(1+D32B/NEB(J))/NEB(J))
P0=1+(F(4)/NEB(J))*(1+F(5)/NEB(J))/(1+F(6)/NEB(J))
NUE=NEB(J)*NEB(J)/NES2
MSOURCE(J)=NEB(J)*IB*(1-P0*NUE)
  IF (IDEN.EQ.1) MSOURCE(J)=NEB(J)*A*NES2
NEBDOT(J)=RMUR*(GAMMAP-GAMMAM)/DZ+MSOURCE(J)
NA(J)=RMUR*MUIS*(TAU(J+1)+TAUN(J+1))/2.0/DZ**2
NB(J)=RMUR*(MUIS+MUISOLD)*(TAU(J)+TAUN(J))/2.0/DZ**2
NC(J)=RMUR*MUISOLD*(TAU(J-1)+TAUN(J-1))/2.0/DZ**2
ND(J)=I*(MURS-MURSOLD)*RMUR/DZ/2.0
+   +NEB(J)*IB*(1.0+SQRT(P0/NES2)*NEB(J))
C NS(J)=IB*(1.0-P0*NUE)
NS(J)=-NEB(J)*IB*(1.0+SQRT(P0/NES2)*NEB(J))*SQRT(P0/NES2)
  IF (IDEN.EQ.1) NS(J)=A*NES2
NEBA(J)=-DT*NA(J)*LAMNEB
NEBB(J)=1.0+DT*NB(J)*LAMNEB-DT*NS(J)*LAMNEB
NEBC(J)=-DT*NC(J)*LAMNEB
NEBV(J)=NEB(J)+DT*NA(J)*(1.0-LAMNEB)*NEB(J+1)-DT*NB(J)*
+   (1.0-LAMNEB)*NEB(J)+DT*NC(J)*(1.0-LAMNEB)*NEB(J-1)+
+   DT*ND(J)+DT*NS(J)*(1.0-LAMNEB)*NEB(J)
KDE=K(J)*(DETA+DETAP)/2
QKP=(TAU(J+1)-TAU(J))/DETAP
CONVECT=-(1.5)*I*(DETA*QKP+DETAP*QKM)/(2*KDE)
SIGMA=NEB(J)*MUEA(J)
POHMIC=I*(I/SIGMA+TAU(J)*(NEB(J+1)-NEB(J-1))
+   /(2*DZ*NEB(J)))
PBP=(F(9)*NNR/NR)*EXP(-F(10)/TAU(J))
PB=(F(11)*NNR/NR)*EXP(-F(12)/TAU(J))
CV(J)=1.5*NEB(J)+NNB(J)*(F(10)*PBP+F(12)*PB*NUE)
+   /(TAU(J)*TAU(J))
ESOURCE(J)=-ELOSSB*MSOURCE(J)
+   -NNB(J)*PB*(2*NUE*NEBDOT(J)/NEB(J))
TAUDOT(J)=(QKP-QKM)/KDE+CONVECT+POHMIC+ESOURCE(J)
+   /CV(J)
TA(J)=1.0/(DETAP*KDE*CV(J))
TB(J)=(1.0/DETAP+1.0/DETA)/KDE/CV(J)
TC(J)=1.0/DETA/KDE/CV(J)
TS(J)=(CONVECT+POHMIC+ESOURCE(J))/CV(J)
TAUA(J)=-DT*LAMTAU*TA(J)
TAUB(J)=1.0+DT*LAMTAU*TB(J)
TAUC(J)=-DT*LAMTAU*TC(J)
TAUV(J)=TAU(J)+DT*(1.0-LAMTAU)*TA(J)*TAU(J+1)
+   -DT*(1.0-LAMTAU)*TB(J)*TAU(J)
+   +DT*(1.0-LAMTAU)*TC(J)*TAU(J-1)
+   +TS(J)*DT
  IF (CHKDOT.EQ.3) WRITE(9,201) J,NEB(J),J,TAU(J),
+   J,MSOURCE(J),J,PB,PBP,A,D21B,D32B,P0,IB,
+   NUE,NES2,QKP,GAMMAP,DETAP,MURS

```

100 CONTINUE

```

C-----
NEBC(0)=NEBC(0)-NEBC(1)*NEBA(0)/NEBA(1)
NEBB(0)=NEBB(0)-NEBB(1)*NEBA(0)/NEBA(1)
NEBV(0)=NEBV(0)-NEBV(1)*NEBA(0)/NEBA(1)
NEBA(0)=NEBB(0)
NEBB(0)=NEBC(0)
NEBA(N+1)=NEBA(N+1)-NEBA(N)*NEBC(N+1)/NEBC(N)
NEBB(N+1)=NEBB(N+1)-NEBB(N)*NEBC(N+1)/NEBC(N)
NEBV(N+1)=NEBV(N+1)-NEBV(N)*NEBC(N+1)/NEBC(N)
NEBC(N+1)=NEBB(N+1)

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NEBB(N+1)=NEBA(N+1)
TAUC(0)=TAUC(0)-TAUC(1)*TAUA(0)/TAUA(1)
TAUB(0)=TAUB(0)-TAUB(1)*TAUA(0)/TAUA(1)
TAUV(0)=TAUV(0)-TAUV(1)*TAUA(0)/TAUA(1)
TAUA(0)=TAUB(0)
TAUB(0)=TAUC(0)
TAUA(N+1)=TAUA(N+1)-TAUA(N)*TAUC(N+1)/TAUC(N)
TAUB(N+1)=TAUB(N+1)-TAUB(N)*TAUC(N+1)/TAUC(N)
TAUV(N+1)=TAUV(N+1)-TAUV(N)*TAUC(N+1)/TAUC(N)
TAUC(N+1)=TAUB(N+1)
TAUB(N+1)=TAUA(N+1)
ALPHA(0)=-NEBA(0)/NEBB(0)
DO 110 I1=1,N
    ALPHA(I1)=-NEBA(I1)/(NEBC(I1)*ALPHA(I1-1)+NEBB(I1))
110 CONTINUE
    ALPHA(N+1)=0.0
    BETA(0)=NEBV(0)/NEBB(0)
    DO 120 I1=1,N+1
        BETA(I1)=(NEBV(I1)-NEBC(I1)*BETA(I1-1))/(NEBC(I1)
+           *ALPHA(I1-1)+NEBB(I1))
120 CONTINUE
    NEBU(N+1)=BETA(N+1)
    DO 130 I1=N,0,-1
        NEBU(I1)=ALPHA(I1)*NEBU(I1+1)+BETA(I1)
130 CONTINUE
    ALPHA(0)=-TAUA(0)/TAUB(0)
    DO 140 I1=1,N
        ALPHA(I1)=-TAUA(I1)/(TAUC(I1)*ALPHA(I1-1)+TAUB(I1))
140 CONTINUE
    ALPHA(N+1)=0.0
    BETA(0)=TAUV(0)/TAUB(0)
    DO 150 I1=1,(N+1)
        BETA(I1)=(TAUV(I1)-TAUC(I1)*BETA(I1-1))/(TAUC(I1)
+           *ALPHA(I1-1)+TAUB(I1))
150 CONTINUE
    TAUU(N+1)=BETA(N+1)
    DO 160 I1=N,0,-1
        TAUU(I1)=ALPHA(I1)*TAUU(I1+1)+BETA(I1)
160 CONTINUE
    DO 170 I1=0,N+1
        TAUDOT(I1)=(TAUU(I1)-TAU(I1))/DT
        NEBDOT(I1)=(NEBU(I1)-NEB(I1))/DT
170 CONTINUE
    IF (CHKDOT.EQ.3) THEN
        WRITE(9,202) (I1,NEBDOT(I1),I1,TAUDOT(I1),I1=0,N+1)
        WRITE(9,203) (I1,ALPHA(I1),I1,BETA(I1),I1=0,N+1)
        WRITE(9,204) (I1,NEBU(I1),I1,TAUU(I1),I1=0,N+1)
    ENDIF
RETURN
C
201 FORMAT('NEB(',I2,')=',F8.3,' TAU(',I2,')=',F8.3,
&' MSOURCE(',I2,')=',F8.3/'J=',I2,' PB=',F8.3,
&' PBP=',F8.3/'A=',F8.3,' D21B=',F8.3,' D32B=',F8.3/
&' P0=',F8.3,' IB=',F8.3/'NUE=',F8.3,' NES2=',F8.3/
&' QKP=',F8.3,' GAMMAP=',F8.3/'DETAP=',F8.3,' MURS=',F8.3)
202 FORMAT('NEBDOT(',I2,')=',F8.3,' TAUDOT(',I2,')=',F8.3)
203 FORMAT('ALPHA(',I2,')=',F8.3,' BETA(',I2,')=',F8.3)
204 FORMAT('NEBU(',I2,')=',F8.3,' TAUU(',I2,')=',F8.3)
205 FORMAT('//2X,'COLLECTOR SHEATH FAILED TO CONVERGE',/)
206 FORMAT(/1X,'EGRADA=',F7.3,3X,'ALPHA2=',F7.3/

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&1X,'RLE=',F5.2,3X,'EMISS=',F9.1,3X,'JNET=',F7.4/
&1X,'ECHI=',F7.3,3X,'PHIB=',F7.3,1X,'ENE=',F10.3,3X,
&'EALPHA=',F7.4/1X,'CCHI=',F7.3,3X,'CALPHA=',F7.4/1X,
&'IFLAG=',I1,3X,'RCODE=',A1)

```

END

C*****

FUNCTION G(UX,NEB,TAU,I,KN)

C*****

REAL UX,NEB,TAU,I,KN,SQX,GX

DOUBLE PRECISION ERF

IF (UX.LE.0.0) THEN

SQX=0.0

ELSE

SQX=SQRT(UX)

ENDIF

C G=UX*LOG(1.0+ERF(SQX)) - LOG(NEB*SQRT(TAU)/I/KN/2.0)

G=UX - LOG(NEB*SQRT(TAU)/I/KN/2.0)

RETURN

END

C*****

FUNCTION ERF(X)

C*****

DOUBLE PRECISION X1,SUM,ERF,ERFX,P(3,6),Q(3,6),PI,TSUM1,TSUM2

INTEGER IPOWER(3)

DATA IPOWER/2,1,-2/

PI=3.1415926535898

TSUM1=0.0

TSUM2=0.0

X1=X

IF (X1.LT. 0.0) X1=-X1

IF (X1.GT. 5.93) THEN

ERFX=1.0

GOTO 1240

END IF

IF (X1.EQ. 0.0) THEN

ERF=0.0

GOTO 1245

ELSE

IFLAG=1

END IF

IF (X1.LE. 4.0 .AND. X1.GE. 0.47) IFLAG=2

IF (X1.GT. 4.0) IFLAG=3

DO 1205 J=1,6

TSUM1=TSUM1 + P(IFLAG,J) * (X1**(IPOWER(IFLAG)*(J-1)))

TSUM2=TSUM2 + Q(IFLAG,J) * (X1**(IPOWER(IFLAG)*(J-1)))

1205 CONTINUE

SUM=TSUM1/TSUM2

GOTO (1210,1220,1230),IFLAG

1210 ERF=X1*SUM

GOTO 1240

1220 ERF=1.0 - DEXP(-X1*X1)*SUM

GOTO 1240

1230 ERF=1.0 - DEXP(-X1*X1)/X1*(1.0/DSQRT(PI) + (1.0/(X1*X1)*SUM))

1240 ERF=ERFX

IF (X.LT. 0.0) ERF=-ERFX

1245 RETURN

C*****P(IFLAG,J)*****Q(IFLAG,J)*****

DATA P(1,1)/3.20937758913847D+03/,P(1,2)/3.774852376853D+02/

DATA P(1,3)/1.1386415415105D+02/,P(1,4)/3.16112374387057/

DATA P(1,5)/1.85777706184603D-01/,P(1,6)/0.0/

DATA Q(1,1)/2.84423683343917D+03/,Q(1,2)/1.2826165077372D+03/
DATA Q(1,3)/2.44024637934444D+02/,Q(1,4)/2.36012909523441D+01/
DATA Q(1,5)/1.0/,Q(1,6)/0.0/,P(2,1)/2.2898992851659D+01/
DATA P(2,2)/2.6094746956075D+01/,P(2,3)/1.4571898596926D+01/
DATA P(2,4)/4.2677201070898/,P(2,5)/5.6437160686381D-01/
DATA P(2,6)/-6.0858151959688D-06/,Q(2,1)/2.2898985749891D+01/
DATA Q(2,2)/5.1933570687552D+01/,Q(2,3)/5.0273202863803D+01/
DATA Q(2,4)/2.6288795758761D+01/,Q(2,5)/7.5688482293618/
DATA Q(2,6)/1.0/,P(3,1)/-6.58749161529838D-04/
DATA P(3,2)/-1.60837851487423D-02/,P(3,3)/-1.2578172611123D-01/
DATA P(3,4)/-3.60344899949804D-01/,P(3,5)/-3.05326634961232D-01/
DATA P(3,6)/-1.63153871373021D-02/,Q(3,1)/2.3352049762687D-03/
DATA Q(3,2)/6.05183413124413D-02/,Q(3,3)/5.27905102951428D-01/
DATA Q(3,4)/1.87295284992346/,Q(3,5)/2.56852019228982/,Q(3,6)/1/
END

```

      CALPHA=0.5
      DO 10 I1=0,N+1
        NEB(I1)=I1
        NEBCAL(I1)=(NEB(I1)-1)/(N-1)
        NEB(I1)=4.0*(KN+NEBCAL(I1)*(1-NEBCAL(I1)))
        TAU(I1)=2700/TE
10    CONTINUE
      ENDIF
C*****MISCELLANEOUS DEFAULTS
      ARECN=0.31
      EGNDB=3.896/8.609E-05/TE
      ELOSSB=EGNDB
      SN=DELTAT*(N-1)**2*3*LAMDAR*SMR*(BN+CN)
      ST=DELTAT*(N-1)**2*0.667*(RE+2)*2*(RE+0.5)*(BT+CT)/FYEN
C*****NONDIMENSIONALIZE CURRENT AND CALCULATE RICHARDSON EMISSION
      VALUE=EXP(-11600.0*EWF/TE)
      ENR=(7.676E+14*(TE)**1.5*VALUE)/NR
      I=J / (KN*NR*(3.1265322E-13)*SQRT(TE))
      JRIC=120.0*TE*TE*(EXP(-11600.0*EWF/TE))
C*****OUTPUT INITIALIZATION DATA TO PRNTOUT.DAT
      WRITE(9,155) TE,TC,EWF,CWF,PN,D,J,CHKDOT,OFIL,N,
&                JRIC,NR,TCHAR,I,ENR,KN,SMR,LAMDAR,
&                NSTEPS,T2,DELTAT,DTP,LS
      IF (CHKDOT.GT.1) THEN
        WRITE(9,160) ECHI,ENE,EALPHA,CCHI,CNE,CALPHA,AN,AT,
&                BN,BT,CN,CT,SN,ST,LAMNEB,LAMTAU,ELOSSB,
&                ARECN,EGNDB,IDEN,FYEN,RE
        WRITE(9,159) (I1,NEB(I1),I1,TAU(I1),I1=1,N)
      ENDIF
      WRITE(9,161)
C*****CHECK FOR UNREAL CURRENT CONDITION  J/JR > 1.0
      IF (2*KN*I/ENR .GE. 1.0) THEN
        WRITE(*,153)
        STOP
      ENDIF
      RETURN

```

```

C
C-----
150 FORMAT(1X,'*****'/
&1X,'*****'
&1X,'*****'          TEC      START          *****'/
&1X,'*****'          *****'/
&1X,'*****'          *****'/
&1X,'*****'          *****'///)
151 FORMAT(F8.1/F8.1/F6.3/F6.3/F6.3/F6.3/F7.2/F5.2/F6.1/
&I1/I1/I3/I3/I3)
152 FORMAT(F9.4/F9.4/F8.3/F8.3/F9.4/F9.4/I3)
153 FORMAT(1X,'***SMALL J IS TOO LARGE...CASE TERMINATED***'//)
154 FORMAT(2F8.3)
155 FORMAT(12X,'      TEC INITIAL DATA SUMMARY'//
&1X,'-----'//
&1X,'PHYSICAL OPERATING CONDITIONS-----'//
&1X,'      EMITTER TEMPERATURE      (TE)='F8.1,' KELVIN'/
&1X,'      COLLECTOR TEMPERATURE     (TC)='F8.1,' KELVIN'/
&1X,'      EMITTER WORK FUNCTION      (EWF)='F6.3,' EV'/
&1X,'      COLLECTOR WORK FUNCTION     (CWF)='F6.3,' EV'/
&1X,'      CONVERTOR PRESSURE         (PN)='F6.3,' TORR'/
&1X,'      GAP THICKNESS              (D)='F6.3,' MM'/
&1X,'      OPERATING CURRENT          (J)='F7.3,' AMPS/CM^2'//
&1X,'      TEC FUNCTION SETTINGS-----'//
&1X,'      DIAGNOSTIC LEVEL (CHKDOT)='I1/

```

```

C                                                    DOS FILE PRED3.FOR
C*****
      SUBROUTINE INITIAL (TE, TC, EWF, CWF, PN, NSTEPS, DTP, T2, AN, AT,
&CN, CT, BN, BT, TCHAR, SMR, ARECN, DELTAT, SN, ST, TAU, NEB, LS, pc)
C*****
      REAL CA, CSAHA, CNE, ENE, ECHI, CCHI, EALPHA, CALPHA, LAMNEB, LAMTAU
      REAL DT, DTAUNDZ, DTP, T2, AN, AT, CN, CT, BN, BT, RE, KN, TCHAR, PN
      REAL SMR, LAMDAR, NR, TE, TC, ENR, I, ARECN, EGNDB, ELOSSB, MUI (0:150)
      REAL TAU (0:150), NEB (0:150), DELTAT, SN, ST, PI, TAUN (0:150), NNB (0:150)
      REAL NEBCAL (0:150), FYEN, LAMDAE, LAMDAI, EWF, CWF, J, RMUR, LCCHI
      REAL ESOURCE (0:150), CV, JRIC, VALUE, PHISDAT (154, 6), PHIBDAT (21, 6)
      INTEGER N, IDEN, CHKDOT, OFILE, EFIX, CFIX, NSTEPS, LS, pc

C
      COMMON /PRED/ CA, CSAHA, DT, DTAUNDZ, DZ, EGNDB, ELOSSB, ENR, I, IDEN, KN
      COMMON /PRED/ LAMDAR, LAMNEB, LAMTAU, MUI, N, NNB, NNR, NR, PI, RE, RMUR
      COMMON /PRED/ TAUN, EFIX, CFIX, CHKDOT, FYEN, ENE, ECHI, CCHI, CNE
      COMMON /PRED/ EALPHA, CALPHA, CV, ESOURCE, LCCHI
      COMMON /XSHEATH/ PHISDAT, PHIBDAT

C
      WRITE (*, 150)
C*****READ FILE INDATA.DAT
      READ (2, 151) TE, TC, EWF, CWF, PN, D, J, DTP, T2, CHKDOT, OFILE, pc, N, LS
      REWIND (2)
      CLOSE (2)
C*****READ FILE PRECOR.DAT
C      CALL DATAINT
C*****SET NUMERICAL PARAMETERS, RECOMPILATION REQUIRED TO CHANGE
      AN=0.5
      AT=0.5
      CN=0.5
      CT=0.5
      BN=1.0-CN
      BT=1.0-CN
      PI=3.1415926
      IDEN=0
      RE=0.0
      FYEN=1.0
      NR=1.0E14
      DELTAT=DTP/NSTEPS
      LAMNEB=1.0
      LAMTAU=1.0
C*****SET TRANSPORT PROPERTIES
      LAMDAE=1.0/32.3/PN
      LAMDAI=1.0/96.6/PN
      LAMDAR=LAMDAI/LAMDAE
      KN=LAMDAE/D
      TCHAR=D/(KN*3.75*(TE**.5))
      SMR=1.0/492.2
C*****EXECUTE OFILE SELECTION SETTING
      IF (OFILE .EQ. 1) THEN
        READ (8, 152) ENE, CNE, ECHI, CCHI, EALPHA, CALPHA, N
        READ (8, 154) (NEB (I1), TAU (I1), I1=0, N+1)
        REWIND (8)
      ELSE
        ENE=0.8
        CNE=0.8
        ECHI=3.0
        CCHI=3.0
        EALPHA=0.5

```

```

&1X,'          RESTART SEQUENCE      (OFILE)= ',I1/
&1X,'          POINT DENSITY          (N)= ',I3//
&1X,' PHYSICAL PARAMETERS EVALUATED-----'//
&1X,' RICHARDSON CURRENT      (JRIC)= ',E9.2,' AMPS/CM^2' /
&1X,' REFERENCE DENSITY      (NR)= ',E9.2,' 1/CM^3' /
&1X,' CHARACTERISTIC TIME    (TCHAR)= ',F7.4,' SECS*E-06' /
&1X,' NONDIM CURRENT          (I)= ',F7.4/
&1X,' NONDIM EMISSION        (ENR)= ',F8.3,' (NRIC/NR)' /
&1X,' KNUDSEN NUMBER          (KN)= ',F7.4/
&1X,' SQRT(MASS RATIO)        (SMR)= ',F7.4/
&1X,' MEAN FREE PATH RATIO    (LAMDAR)= ',F7.4//
&1X,' TIME SETTINGS-----' /4X,' NSTEPS=',I3/
&4X,'      T2=',F6.1/4X,' DELTAT=',F6.3/4X,'      DTP=',F6.3/
&4X,'      LSF=',I3)
159 FORMAT(4X,'NEB(',I2,')=',F8.3,'      TAU(',I2,')=',F8.3)
160 FORMAT(/1X,'ADVANCED DIAGNOSTIC OUTPUT-----'//
&4X,' ECHI=',F5.1,' ENE=',F7.4,' EALPHA=',F7.4/
&4X,' CCHI=',F5.1,' CNE=',F7.4,' CALPHA=',F7.4/
&4X,' AN=',F7.4,' AT=',F7.4/4X,' BN=',F7.4,' BT=',F7.4/
&4X,' CN=',F7.4,' CT=',F7.4/4X,' SN=',F7.4,' ST=',F7.4/
&4X,' LAMNEB= ',F5.2/4X,' LAMTAU=',F5.2/4X,' ELOSSB= ',F6.3/
&4X,' ARECN= ',F6.3/4X,' EGNDDB= ',F6.3,/4X,' IDEN=',I1/
&4X,' FYEN= ',F5.2/4X,' RE= ',F5.2//
&1X,' STARTUP DENSITY AND TEMPERATURE RATIOS-----')
161 FORMAT(/1X,'-----',
&'-----')
      END

```

C

DOS FILE PRED4.FOR

```

SUBROUTINE SHEATH(JNET,ENR,TAU,ECHI,PHIB,EALPHA,ENE)
REAL ENE,ECHI,ENR,TAU,PHIB,EALPHA,JNET,A,S,B,DPH
A=1.1485
B=1.169
S=.1
ECHI=((JNET-A)+SQRT((JNET-A)**2+4*S*B))/(2*S)**2
IF(ECHI.LT.0.0) ECHI = 0.0
ENE=(SQRT(3.14159265/2)*JNET*SQRT(TAU)) +
+ (1/EXP(ECHI/TAU))
PHIB=ALOG(ABS(ENR/ENE))
IF(PHIB.LE.0.0) THEN
    PHIB = 0.0
    ENE = ENR
    ECHI = -TAU*ALOG(ENE - (SQRT(3.14159265/2)*JNET*SQRT(TAU)))
ENDIF
DPH = (PHIB - ECHI)/TAU
IF(DPH.LT.0.0000001) DPH = 0.0000001
EALPHA=(1.0/TAU)*(3.14159265/2)*(1.0 + ERF(SQRT(DPH)))
+ - (1./2.)*(1.0 + ERF(SQRT(4.0*DPH)))**2 / (EXP(-DPH)
+ - (1./4.)*EXP(-4.0*DPH))**2
RETURN
END

```