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Miniature Imaging Photometer
Phase II

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15 July, 1990

Scientific Report No. 1

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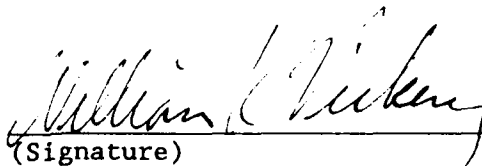
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1. Contract Objectives:

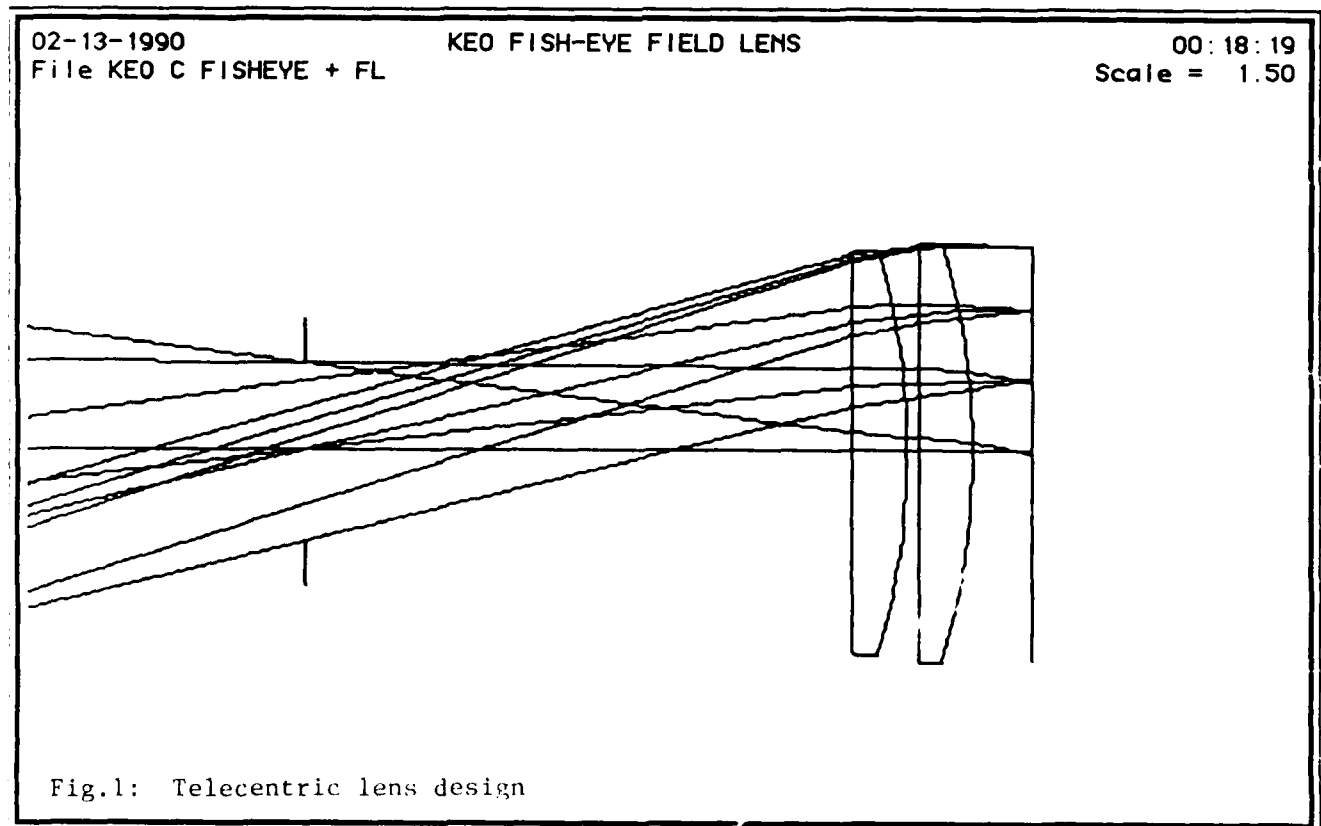
Design, fabricate, test and deliver one Miniature Imaging Photometer (MIP), in accordance with Keo Consultants Technical Proposal entitled *Miniature Imaging Photometer for Aurora and Airglow*, dated 89JAN31, as amended 89APR19.

2. Description of Progress:

(a) Optical:

Quarterly Reports KEO-1 to KEO-4 described design decisions made during the first quarter and progress in implementing those designs during the second through 4th quarters. Current status of design and fabrication of various optical components of the system are summarized in the following:

(i) All-sky Lens: See Figure 1 for optical schematic of the telecentric design. The telecentric elements have been procured (two plano-convex lenses, with anti-reflection coatings all surfaces). This part of the design has been bench tested and performs as expected.



02-13-1990
File KEO SYSTEM L

KEO FISH-EYE FIELD LENS

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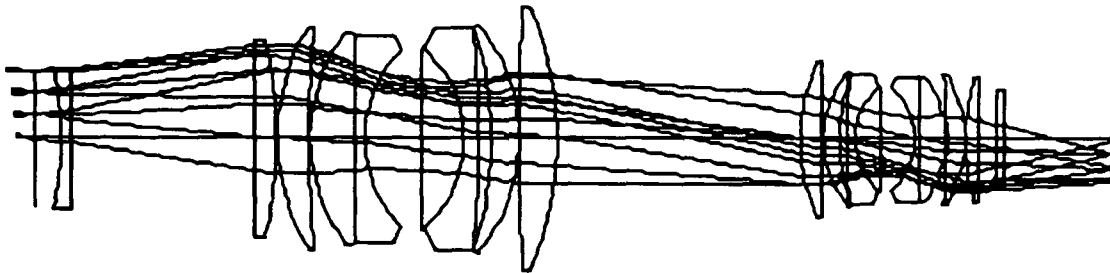


Fig. 2: Reimaging Optics (with spacings for mirror and Fabry Perot)

02-13-1990
File KEO SYSTEM L1

KEO FISH-EYE FIELD LENS

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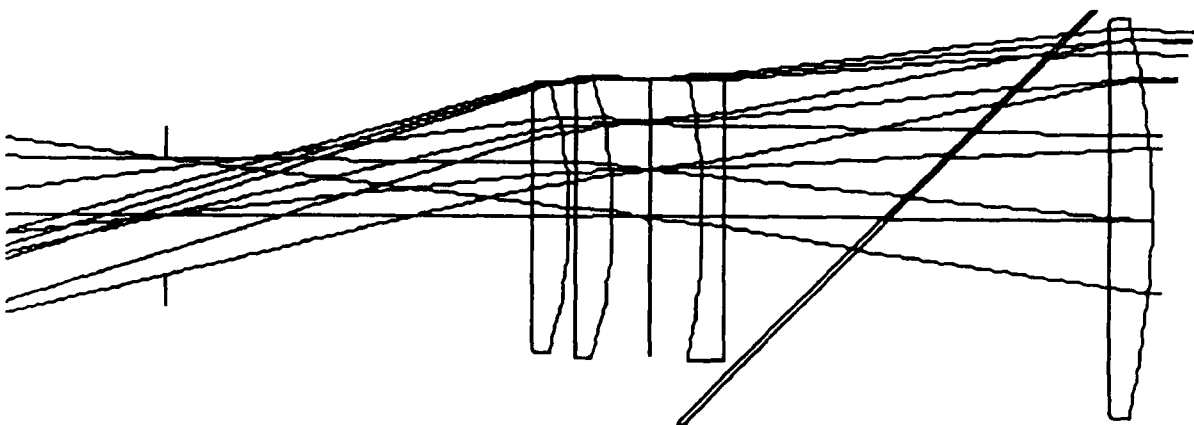


Fig. 3: Provision for 45° mirror (partial)

(ii) Filters and Filter Wheel: Five-position, 1.75" dia. filters. The filter wheel has been fabricated and successfully tested.

A set of five filters has been ordered, at the following wavelengths:

427.8 nm

455.4 nm

555.7 nm

630.0 nm

777.4 nm

(iii) Re-imaging Optics: The assembly as designed by Kidger Optics uses two standard (Canon) camera lenses and one plano-convex lens (see Figure 2). Optical bench testing of the Kidger Optics design revealed a vignetting problem with the Canon 85mm lens. This was traced to the fact that the commercial Canon 85mm/F1.2 lens measures to be only about F1.3, and this difference is sufficient to cause the problem. Kidger is reconsidering the design in light of this problem, but to date has not been able to come up with a solution that still uses commercially available camera lenses. In the meantime, a scaled down version of a previous larger-format design developed by Keo is being considered as an alternative. Bench testing indicates good performance (no vignetting) but there is significant curvature of the image field. A range of plano concave lenses (to act as a field flattener) were procured and bench tested; curvature can be considerably corrected, but additional astigmatism is introduced. The design is currently being further investigated using computer design software.

(iv) Calibration Capability: A (permanent) 45 deg. partially reflecting mirror (90%/10%) will be used to direct calibration charts into the optics train (after the filter plane), see Figure 3. Options (manually switchable) will include resolution chart, gray scale chart, series of relative calibration targets, etc. This mirror has been included in the design, but as yet has not been procured. (These elements will be ordered only after satisfactory testing of the reimaging optics.)

(v) Shutter: A large (2.5") aperture shutter, positioned near an aperture plane (so that shutter open/close characteristics do not affect relative exposure over the image area) is for sky exposure control. The shutter has been procured, modified and mechanically tested. Low-force microswitches were installed to confirm shutter open status, and a photocell also installed to allow premonitoring of input light intensities. This latter feature will be used both as protection and as a means of judging optimum exposure and high voltage setting.

(vi) Fabry-Perot Option: Provision for insertion of a Queensgate Fabry-Perot interferometer cell has been included in the design. This option however will not be included in this instrument under this Contract.

(vii) Image Intensifier Lens: Has been defined to be a Canon 50mm/F1.2 (and has been procured).

(viii) Image Intensifier: Design is to allow interchangeability of 25mm types. Intensifiers with near uv sensitivity (1st Gen + Proximity hybrid), visible (normal Gen II) or infrared sensitive (Gen III) may be used. To minimize thermal noise (especially important if Gen III type used), the image intensifier cathode is to be cooled to approximately 0°C. The phosphor is kept at ambient, as cooling increases decay/lag times appreciably. We discovered recently that a 25mm Gen III tube is not available in inverter form; an 18mm version is available, but is of different mechanical configuration. A 25mm Gen III proximity tube can be obtained from ITT (expensive), and so could be integrated with a Gen I tube to form an IR-hybrid, if future research plans call for near-IR imaging.

(ix) Image Intensifier Cooler: A prototype thermoelectric cooler was built in the first quarter (by Products for Research), and testing indicated satisfactory performance. A final version was designed by Keo, which included provision for dry nitrogen flushing, larger area heat dissipation fins, RTD temperature readout, and appropriate mounting provisions. This cooler has now been procured, and testing indicates performance to specifications. The cooler next has to be mounted in a fan-cooled housing.

(x) Relay Optics: A fast, high-resolution relay lens pair consisting of Rodenstock 100mm.F1.4 + 42mm/F0.7 will be used, reducing the image diameter to the 10mm required to fit on the CCD. These lens components have been procured, and a design has been completed for mounting a large aperture shutter between the lenses (see xi. below).

(xi) CCD Shutter: A second large aperture shutter (see (v) above) between the relay lenses will ensure the CCD is kept dark (from image intensifier dark noise or phosphor lag) during filter changes or between any two exposures.

(xii) Image Intensifier Output Monitor: Part of the beam between relay lenses will be sampled with a photoconductive cell. This will be used to adjust image intensifier gain under computer control so that the image intensifier is kept in its linear gain region (before AGC switches in), and to assist in setting CCD exposure time. This has been incorporated into the shutter, and will be tested next quarter.

(b) Detector - CCD and Housing:

The first quarter of this contract involved an in-depth review of present CCD technology to decide which CCD we should choose for the MIP. After much consideration, we decided that we wanted to take advantage of the new MPP technology. Multi-Pin-Phased (MPP) CCD's have a boron implant that when driven with the proper phasing, have a dark noise of 1/20th of a similar CCD without the boron implant. This technology was developed jointly by Photometrics and Ford Aerospace.

Photometrics developed a 512x512 chip with an 18 um pixel size. SAIC subsequently developed a 1024x1024 chip with the same properties as the Photometrics chip. Both chips were carefully evaluated for our application and an analysis is included in **Appendix 1** of this report. It was determined that the Photometrics chip best suited our needs for the MIP in terms of matching resolution, dynamic range, and cost. The significantly reduced thermal noise will allow long exposures and better S/N in low intensity situations (eg. heater experiments, Fabry-Perot applications).

Initial design for the camera housing considered using standard Photometrics circuit boards, and investigating how they could be miniaturized for our application. Their air-cooled CH200 system was selected, and a repackaging scheme for their camera electronics was developed.

From the Photometrics schematics we re-designed their interface boards to physically fit into our mechanical camera configuration. An analysis of the benefits of a surface-mount implementation was performed and it was found that while saving about 30% in physical size, both the cost and serviceability made it impractical. Finally a two board set was decided upon that would fit into the MIP camera head configuration.

Photometrics subsequently formed a splinter company called Advanced Technologies headed by Dr. Gary Simms. Advanced Technologies (AT) was developing a small camera head, and interface board set for Marine Imaging Systems that closely met our needs. In October 89 we met with Dr. Simms and agreed on a product specification and in December 89 he supplied us with a cost estimate. We decided to use this camera head/electronics implemented with the Photometrics MPP CCD and a generalized 12 bit parallel interface that could either be interfaced to the MacIntosh computer or to one of the available IBM PC based Image Processing boards.

A specially designed head to accommodate our fast relay lens, and with enhanced cooling fins and connector configuration to suit our mechanical requirements, has now been designed by Photometrics.

A firm quote was finally received from AT in May 90 for the cost of the system excluding the custom interface board that we are designing to control all our camera electronics. Progress has been very slow with AT as they had to finish up their product with Marine Imaging Systems first. Complete interface specifications were sent to Doug Donahue (contact engineer at AT) along with a set of circuit schematics designed specifically for our camera system, functional diagrams for all the MIP components, and the planned physical layout of the system.

Advanced Technologies has finally started work on our project the last week of June; they plan to finalize the design by the end of July and present it for our final review, and delivery is slated for the first week in October. While this is much later than we would like (AT first estimated delivery at March 90), this should give us sufficient time to integrate the camera head and electronics into the MIP before late winter (Feb.-Mar., 1991) for field testing (probably in Alaska).

(c) MIP Electronics and Control System:

The MIP control system consists mainly of the filter wheel housing/electronics, shutter controls, intensifier cooler/electronics, temperature measurement/control, and manual control panel. It was decided to develop a set of electronics for the MIP that was compact and fully implemented in the actual MIP unit. In addition, it was decided that for both compactness and convenience all manual controls would actually be located in the camera itself rather than the traditional rackmount unit with the computer. This has the advantage that work done to control the camera manually is usually done when the computer is down, or is not conveniently located (as all aspects of the MIP can be controlled from the computer as well). In addition, have all these components located in the camera housing provides less cabling, connectors, and packaging. These will improve the reliability and portability of the instrument.

(i) Filter Wheel Control:

The filter wheel has been built and the interface electronics has been prototyped and a lab version of the electronics is presently working. The circuit uses an intelligent stepper motor controller that runs self-contained with a memory chip. This has the advantage of small, intelligent and extremely flexible control system that can be easily modified to meet the needs of any changes in the future. Small, powerful

electronics components such as single-package 1.5A Stepper Motor Drivers, and TO-220 package high Wattage resistors have been selected to minimize space for the camera.

This control system has been found to work very well and is a marked improvement on the two previous control systems, as the acceleration and deceleration of the filter wheel is controlled by a mathematical algorithm to ensure smooth operation and a minimum chance of losing steps. An automatic homing function automatically sets the final filter destination every move to ensure consistent filter placement. Final stepper motor voltages, dropping resistors, and acceleration algorithms have to be determined once the filter wheel is anodized, and filters are added to the system.

(ii) Shutter Control:

Large aperture Uniblitz shutters were chosen for the MIP to mount in an aperture plane so as to eliminate the effect of vignetting due to a finite shutter velocity. Because these large shutters require a higher power control circuitry, much effort has gone into the design of a powerful but compact shutter driver circuit. First, the drivers supplied by Uniblitz were evaluated and found to be adequate, but not very cost or size effective.

The Advanced Technologies shutter circuits were finally supplied to us in May, 1990 for evaluation and they proved to be inadequate. Modifications have been made to the circuit so that they could drive our shutters, however they involve large capacitors to provide discharging current to open the shutters. A design was developed by KEO to use advanced supply drivers and a CMOS solenoid driver that provides ample starting current, and is minimized for space. A dual shutter driver has been built for a lab prototype and has been found to work well with our modified Uniblitz shutters. Final testing will be done, when the shutters are anodized and assembled. Limit switches are included in the shutter design to provide a TTL output to the interface electronics indicating that the shutter is completely open. This will be a very useful feature in the field for diagnostics.

(iii) Photoconductive Cell:

A Clairox PL709L Photoconductive cell was evaluated to measure the overall brightness of the image intensifier. It was determined that this will be the easiest way to measure the image intensifier and check for saturation. The photoconductive cell will be interfaced through the camera head into the ADC port E of the 68HC11 MPU on the Advanced Technologies Controller Board. A smaller, lower resistance version of the

709 has been on order from Senisys for evaluation to be located in the Shutter housing. We expect to receive this during the middle of July for final evaluation.

(iv) Intensifier Electronics/Housing:

The Image Intensifier Cooler has been built and tested. It will require approximately 6 Volts unregulated DC to operate. A final power supply will be chosen once we get the final specifications of the TEC for the CCD camera head. The image intensifier power supply and gain control has been designed and is a modified version of KEO's last control circuit. It has not yet been prototyped as we have a high degree of confidence that the circuit will work. A prototype will be built late July or early August.

(v) Temperature Measurement and Control:

A somewhat complicated temperature measurement scheme was developed to allow measurement of all temperatures both at the manual control panel, and at the computer simultaneously, using only one RTD for each temperature. Two Omega Temperature Readout/Controller Panel Meters have been purchased to be mounted in the control panel of the MIP. These are very small packages and are ideal for our application. A four position 4PDT interlocked switching scheme will switch excitation current for the RTD's between the Omega supply and the supply located on the KEO interface board. RTD instrumentation amplifiers will then amplify the RTD signal and calibrate the signal within the temperature range of -50C to 78C. These signals will be inputted into Port E (ADC) of the 68HC11 and digitized to eight bits giving us a resolution of 1/2 degree. This temperature range should adequately cover the ranges of temperature encountered in the MIP. The RTD interface has been designed based on the Advanced Technologies design for Marine Imaging Systems to ensure compatibility with the AT interface.

(vi) Interfacing to the 68HC11 MPU:

A simple but flexible interface to the MPU has been designed to implement the KEO control system into the Advanced Technologies board set. This is presently going under design review at AT. This will provide us with all the signals necessary to implement the present control design. A controller board will be sent to us from AT in August for evaluation of the design.

(d) Image Acquisition Storage and Display:

A detailed study of the current technology and trends in computers and image processing was undertaken to determine the best scheme for implementation in the MIP. This analysis of the present image processing and computational needs and anticipated needs in the near future is presented in **Appendix 2**.

To maximize the benefit of the MIP in the field, the scientist will require a large degree of flexibility in use, and as much processing power as possible. It was decided that to spend a great deal of effort to make a truly small instrument at the sacrifice of the power that is available today packaged in the standard personal computer was counter-productive.

The MIP as presently envisioned will have one monitor for use in the field that will display both control information and image information with the option of using two (possibly higher resolution) monitors in the lab for subsequent detailed analysis of data. The package will be a standard PC desktop unit that will contain all the necessary circuitry to interface directly to the camera body. This will provide a compact and extremely powerful system that will many times outperform capabilities of the present ASIP systems, as well as outperform the data processing capabilities of the computers GL currently uses to analyze the data.

The envisioned MIP would no longer be just a field instrument, but rather a small, powerful image processing work station set up to either take automated ASIP images, and to additionally have the capability to analyze the images and develop new ways to configure the instrument and data taking routine while in the field.

To do this, three different approaches have been looked into in detail. These would be implemented on either the Mac IIci using a custom interface board being developed by Advanced Technologies, or the IBM PC compatibles using either the MATROX Image Series Board Set, or the Image Technology Advanced Frame Grabber board set. Both companies have been visited in the last two months. Complete sets of documentation from the manufacturers were evaluated and several reports were written to help choose which of the systems best meets our needs (see **Appendix 3**).

A final decision will be made in July after an engineering analysis of the ITI board has been completed at the factory, and after final consultations with Air Force scientists. Once this decision is made, the boards and the computer will be acquired to start development of the computer system.

Some thought has gone into whether the MIP should be packaged as an industrial rack mount system or just as a normal desktop computer. It was decided that it would be best to use the standard desktop computer, as they are about the third the

cost, have been proven to work reliably in the field, and provide a much more flexible and portable working system for cramped field sites. In addition, replacement boards are readily available and inexpensive. Also, using standard PC products ensures that we will easily be able to upgrade to take advantage of quickly evolving technologies.

(e) Software Development:

Early work in 1990 focussed on becoming proficient in C and programming in an event-oriented structure using the Macintosh toolbox routines. No further software development has been pursued as the final operating system has yet to be determined. However, operating systems for the IBM AT environment were investigated and the Windows 3.0 operating system was chosen as the first operating system (using DOS 4.0) for the IBM environment. This would prove compatible with existing operating systems at the Geophysics Laboratories, and would provide upward compatibility into true 32-bit operating systems (OS/2) and true 32-bit code (WATCOM 8.0/386). Recently we have been familiarizing with the capabilities of the Windows software.

Appendix 1

Discussion of CCD Selection

KEO Consultants 8/1/89

An in-depth summary of the different characteristics of the CCD's we are considering is necessary at this point in order to make a decision for the design of the Miniature Imaging Photometer. We have made a commitment to trying to use CCD's with multi-pinned phased (MPP) capability. For our purposes, this restricts us to 3 phase boron implanted CCD's made by FORD Aerospace. There are three sizes presently made by FORD -- 512x512, 1024x1024, and 2048x2048. The two sizes applicable here are the 512 and the 1024 chips.

The 512x512 chip is a Photometrics propriety chip and using this chip restricts us to using Photometrics hardware and camera heads. This is not necessarily a drawback as Photometrics makes good products. The 1024x1024 chip is made for S.A.I.C., but FORD will run lots for other customers. It may be possible to attain a 1024 chip through Lockheed as they have ordered a lot. There are some advantages and drawbacks to both chips that will be discussed in detail.

(a) CCD Physical Characteristics

Using these CCD's in MPP mode reduces dark noise by a factor of 30, thus substantially increasing integration times allowed on the CCD (which increases sensitivity of the camera) and/or decreases the cooling requirements of the camera head thus allowing for a smaller head design. It is these characteristic of MPP operation that makes these CCDs ideal for us.

The FORD CCD masks have a pixel size of 18um, thus the physical size of each CCD image area is:

512x512:	$512 \times 18\mu\text{m} = 9.2\text{mm}$
1024x1024:	$1024 \times 18\mu\text{m} = 18.4\text{mm}$

[The Tektronics chip we used in the ASIPII system (TEK512) had a pixel size of 27um, and thus an image area of:

512x512:	$512 \times 27\mu\text{m} = 13.7\text{mm}$]
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The physical size is an important parameter to consider as it determines what kind of optical demagnification is necessary to image the intensifier (24mm) down to the CCD. This coupling ratio influences the efficiency of the coupling optics (because of the limited choice of suitable lenses) and thus the sensitivity of the CCD to the image intensifier image. The importance of this efficiency will be discussed in a later section.

To couple the CCD to the intensifier, commercially available relay lenses (a collimator and camera lens in tandem, with focal lengths f_1 and f_2 , and F numbers F_1 and F_2 respectively) will be used. The efficiency of coupling is given by:

$$(1/(1+4 \cdot F_1^2)) \quad \text{if } f_1 F_1 = f_2 F_2$$

or $(1/(1+4 \cdot F_1^2)) \cdot ((f_1 F_1)/(f_2 F_2))^2 \quad \text{if } f_1 F_1 \neq f_2 F_2$

Coupling ratios for the CCDs are:

TEK512:	13.7mm/24mm	= 0.57
PM512:	9.2mm/24mm	= 0.38
1024:	18.4mm/24mm	= 0.77

In the ASIPII, we used a 100mm F1.4 collimating lens coupled to a 50mm F0.7 lens which imaged the intensifier down onto the CCD. Because we are limiting ourselves to commercially available lenses with good vignetting characteristics, efficiencies are determined by lens speeds that we can buy off the shelf. For the 512 and 1024 MPP chips we would use:

<u>Chip Size</u>	<u>Collimating Lens</u>	<u>CCD Lens</u>	<u>Efficiency</u>
512x512:	100mm F1.4	42mm F0.7	0.08
1024x1024:	75mm F1.1	50mm F0.7	0.17

(Note in the first case the CCD lens limits efficiency, whereas in the second case the collimating lens limits efficiency.)

Thus, in coupling to the larger CCD we gain a factor of two in efficiency. (This is not because of any optical reason, but results from limiting lens selection to commercially available lenses designed for relay application.)

The other important physical characteristic to consider between the two CCD's is the full well depths. The 18um pixel has a normal well depth of 250Kelectrons (Ke), but when used in the MPP mode the well depth decreases by a factor of two. Thus, in MPP mode, a pixel's full well capacity is only 125Ke. Compared to the 700Ke of the TEK512 chip which was chosen for large dynamic range, this is very small. The horizontal pixel size (where each pixel is shifted into during a read) is twice the normal size, and the final summation well is 4 times as big. In addition, these areas on the CCD are not operated in MPP mode as they are cleared directly before reading and thus dark noise is not a problem.

The full well capacity of the horizontal pixels is 500Ke, and the summation amplifier is 1000Ke. Thus, the dynamic range of the chip can be greatly increased using binning. The greatest amount of dynamic range available to the chip would be adding 9 pixels together into the summation well giving 1000Ke. This requires 3x3 binning and 3 pixels would be added to each horizontal well ($3 \times 125\text{Ke} = 375\text{Ke}$) which is within the capacity of a horizontal well. 2x2 binning would give us a summation well of 500Ke. These results are summarized below:

512x512 Chip:

<u>Binning</u>	<u>Resolution</u>	<u>Full Well Capacity</u>
1x1 binning:	512x512	125Ke
2x2 binning:	256x256	500Ke
3x3 binning:	170x170	1000Ke

1024x1024 Chip:

<u>Binning</u>	<u>Resolution</u>	<u>Full Well Capacity</u>
1x1 binning:	1024x1024	125Ke
2x2 binning:	512x512	500Ke
3x3 binning:	340x340	1000Ke

We can see that both chips are capable of the same dynamic range except that if we want to set up a system to utilize the maximum dynamic range of the CCD, the 1024 chip would have twice the resolution. In practice, we have found that 3x3 binning on a 512x512 chip is useful for storing data in minimum space, but the spatial resolution is not very good. 512x512 images are very beautiful but take a long time to read/write and take up a great deal of data space. We have been using 256x256 images in the ASIPII, which have been a good compromise for dynamic range, resolution, speed of image acquisition and display, and data storage capabilities.

The 1024 chip's physical characteristics give it an advantage over the 512 chip in that the coupling from the intensifier is more efficient and that for the same dynamic range (1000Ke), the resolution of the chip would be 340x340 pixels which might be a nice compromise between the 256 and the 512 modes. These differences also have to be looked at in terms of read time and data storage. Briefly, a typical read rate would be 500KHz and a typical optical disk system would be 650Mb per disk (with each 16 bit pixel value requiring 2 bytes of 8 bit storage):

<u>Resolution</u>	<u>Read Time</u>	<u>Images/Disk</u>	<u>Time (@ 4 im/min)</u>
1024x1024	2.0 sec	325 images	1 hr 21 min
512x512	0.5 sec	1300 images	5 hr 25 min
340x340	0.2 sec	3250 images	13 hr 32 min
256x256	0.13 sec	5200 images	21 hr 40 min

The time parameter is an indication of how long an optical disk would take to be filled with a normal data acquisition rate of 4 images/minute. Since it takes about .25 to .5 seconds for the filter to change to its next position, either the 340x340 (1024x1024 at 3x3 binning) or the 256x256 (512x512 at 2x2 binning) options are reasonable operating parameters for us to use. The 1024x1024 chip would double our full well capacity and give us better picture resolution than the 512x512 chip, but the 512x512 chip would enable us to store 1.77x more data on a disk.

(b) CCD Resolution vs. Intensifier Resolution

When deciding between resolutions of 256x256 and 340x340, it is important to see if there is any gain between the two in terms of system resolution. The intensifier has a resolution of 15 lp/mm at a Modulation Transfer Function of 25%, which for a 24mm image gives us 360 line pairs. Thus, if the CCD columns are lined up perfectly with the resolution pattern lines, a minimum of 720 pixels would be needed to get this maximum resolution thus a 512x512 image probably matches fairly well with intensifier resolution. At higher binning (lower resolution), the resolution is limited by the CCD, so resolution of the 340x340 image is better than the 256x256 image by a factor of 340/256 or 1.33. At an MTF of 60%, the image intensifier resolution is only 7.5 lp/mm which gives 180 line pairs, matching closely with a 340x340 image.

From experience, 256x256 is adequate resolution for auroral work to resolve the spatial phenomenon being observed. Any upgrade of resolution increases the quality of the image, but it should be noted there is probably little real increase in scientific information for auroral phenomenon, so both formats would give adequate resolution.

(c) Dynamic Range and Read Electronics

We previously discussed utilizing the full dynamic range of the CCD by optimizing the binning. Now we consider converting the electrons in the summation well to Analogue Digital Units (ADU's) to read into the computer memory. To achieve fast read rates, 12 bits of digitization are typically used. The higher the resolution, the lower the read rates. Read rate also determines to large extent the read noise associated with the conversion.

At 500KHz, one can expect a read noise of around 50 electrons. If we set the minimum ADU to be twice this read noise, we get an ADU of 100 electrons. With 12 bit resolution, our dynamic range will be limited to 4000:1. Thus, if one ADU is 100 electrons, the A/D converter will saturate at 400Ke regardless of when the CCD will saturate. This matches well with a full well capacity of 500Ke (i.e. the PM512 at 2x2 binning).

To achieve a full well capacity of 1000Ke (i.e. the 1024 chip at 3x3 binning) with a 12 bit A/D converter, one would have to set 1 ADU to equal 250 electrons. The dynamic range would still be 4000:1 though, so as far as the data is concerned, there is no increase in dynamic range of the system. Another gain could be included in the electronics ($G=x2.5$) to set 1 ADU = 100 electrons if higher sensitivity was also needed.

If one was to use the 1024 chip at 3x3 binning and fully utilize the dynamic range of the CCD (ratio of read noise to full well depth), one would have to use a 14 bit A/D converter setting the maximum dynamic range at 16,000:1. 1 ADU would be equal to 60 electrons and the A/D converter would saturate at 1000Ke.

Summary of Dynamic Range

<u>Full Well Capacity</u>	<u>Bits</u>	<u>Dynamic Range</u>	<u>ADU (min)</u>	<u>(max)</u>
500Ke	12	4000:1	100e	400Ke
1000Ke	12	4000:1	250e	1000Ke
1000Ke	14	16000:1	60e	1000Ke

In physical terms, a 12 bit dynamic range is probably fully adequate for an instrument for measuring auroral and airglow. For instance, on one sensitivity setting, one could look at airglow/aurora ranging from 25 Rayleighs to 100,000 Rayleighs. Dynamic range is also determined by the image intensifier gain which determines the size of a photon event at the CCD. Before deciding which CCD is better for us, it is necessary to discuss this aspect of the design.

(d) Photon Limited Operation

The first thing to look at in the system is to see whether each photon detected at the image intensifier gives us a detectable signal at the CCD. Intensifier gain is quoted from VARO as 50,000, however corrected for green light this reduces to about 10,000. This gives us the average gain for a stream of photons coming into the intensifier versus the output signal. Since the quantum efficiency for the cathode is of the order of 10%, the gain for an individual photon that gets detected by the cathode must be on the order of 100,000.

Assuming photon statistics, we define a usable picture as one with a signal to noise ratio of 2:1, thus a minimum detectable picture is 4 photoelectron events. This would give us 400,000 electrons out of the intensifier. For a relay optics of 10% efficiency (i.e. PM512), 40,000 photons would reach the CCD spread over an average of four pixels with a quantum efficiency of 30%. Thus, one detectable event at the image intensifier gives us nearly 3000 electrons/pixel in the CCD. For the relay lens coupling for a 1024x1024 chip, this number would be around 5000 electrons/pixel.

This points to a problem in dynamic range. If each event is on the order of 3000 electrons, and our maximum full well is 500Ke, then we only have a dynamic range of 166:1 (8 bits) for a 512x512 chip, and 333:1 (9) bits for a 1024x1024 chip. This means that read noise and dark current noise sources are negligible and that the image intensifier gain is restricting our dynamic range. Using the lowest gain on the image intensifier reduces gain by a factor of 10, thus a minimum event would be on the order of 300 to 500 electrons. This enables us to have a dynamic range of only 11 bits.

It may be that we will have to decrease the coupling efficiency of the relay optics by putting in an aperture or by using relay lenses with smaller apertures (which could decrease the size and cost of the system). It seems that ideally we would want to design a system with a minimum detectable event at 2-4 times the read noise/dark noise. With a read noise of 50 electrons, a good minimal detectable event would be 100 to 200 electrons. This would give us a dynamic range on the order of 12 bits.

It should be noted that there is no disadvantage of using the intensifier at a low gain, in fact it decreases the intensifier noise and thus gives a longer integration capability. The dynamic range of the intensifier is determined by how much light is entering the photocathode. Reducing gain at the intensifier would enable us to increase the dynamic range at the camera for very bright aurora by decreasing the number of electrons in the CCD per photon event at the cathode. Let's take a specific design example:

Relay lens coupling at F4.0: Efficiency is 0.015

4 photoelectrons gives:

450 electrons/pixel at CCD for Max gain
225 electrons/pixel at CCD for Max/2
45 electrons/pixel at CCD for Max/10

and we require 2x read noise, i.e. 100 electrons/pixel for a detectable event.
Hence:

<u>CCD Size</u>	<u>Int. Gain</u>	<u>Min. event</u>	<u>Max. event</u>
512	Max	4pe -- 450e	1000pe--500Ke
512	Max/2	4pe -- 225e	2000pe--500Ke
512	Max/10	10pe --100e	10000pe--500Ke
1024	Max	4pe -- 450e	2000pe--1Me
1024	Max/2	4pe -- 225e	4000pe--1Me
1024	Max/10	10pe --100e	20000pe--1Me

Here, a 512x512 CCD is assumed to be 2x2 binned giving a dynamic range of 500Ke, and a 1024x1024 CCD is 3x3 binned giving it a dynamic range of 1 Million electrons (Me). For instance, using a 512x512 CCD with the intensifier on Maximum/4 in 2x2 binning mode, would give us a minimum photoelectron event of 100 electrons and a maximum of 500Ke with a dynamic range of about 5000:1 matching a 12 bit ADC fairly well. Using a 1024x1024 chip in 3x3 binning mode, we could use the intensifier at Max/2 giving a minimum event 225 electrons and a dynamic range of 4000:1.

(e) System Sensitivity

The final thing to check is whether the system sensitivity is affected by choosing either the 1024x1024 or the 512x512 CCDs. If we require a usable image as in the last section to be 4 photoelectrons, then we need at least 4 photoelectrons/pixel. This gives us our minimum sensitivity since we have already shown that for each 4 photoelectron event the CCD generates more than enough electrons to exceed CCD noise sources. For a 1 Rayleigh source, filter transmission 0.6, image cone at intensifier F2.0, Q.E. of intensifier of 10%, and 512x512 resolution elements, it can be shown that there are 0.02 photoelectron/pixel from the image intensifier cathode. Thus, for a 512x512 image, a minimum image of 4 photoelectron/pixel requires 200 R sec. A 1024x1024 image requires 800 R sec.

Thus: PM512 2x2 binned 256x256: 50 R sec
 1024 3x3 binned..... 340x340: 80 R sec

Thus, a 1024x1024 chip operated in 3x3 binning is less sensitive than the 512x512 chip operated in 2x2 binning.

(f) Conclusion

Thus the 512 supplied by Photometrics is the CCD that is best for our application. At 256x256 resolution, it offers the highest sensitivity, and is comparable in most parameters at 4000:1 dynamic range. It is also less expensive than the 1024 and supplied by Photometrics with whom we have a good working relationship.

There are two reasons for using the 1024x1024 chip. The first is if we wanted to achieve a higher dynamic range on the order of 16000:1. The second is that we could increase the noise headroom of the system by using this chip at 340x340 mode, and defining the least significant event as 250 electrons and matching the relay optics to this. This would give a higher resolution image more immune to system noise than the 512x512 chip with the same dynamic range. It would also take longer to read, write and display images and take up more data storage space. Our experience has been that the higher resolution is not really quantitatively significant, but rather just makes the image prettier and that system noise is not a problem (especially with the new cathode cooler for the image intensifier). The main 'noise' source in practice is the sky background continuum.

Appendix 2

Image Processing Overview for MIP Camera

Keo Consultants 7/7/90

The following description gives an overview of the Image Processing needs for the MIP camera as presently conceived. These needs may be thought of as a basic set of operations that we wish to be able to implement quickly and easily from our hardware/software environment. As the camera is used in a research environment, we want to have a system that can be expanded and improved with minimum effort.

(a) MIP Data Set and Acquisition Cycle

The MIP will be used in long term observations. A typical data set will contain four images and repeat every 30 seconds to a minute depending on the phenomenon being observed. Sometimes the data set will be only one image, and sometimes there may be up to 5 images being recorded at once. However, we consider the normal set to be four images per cycle.

The camera is a slow scan camera with a 512x512 CCD clocked at between 500KHz to 1.1MHz. The final clock rate is to be determined by the read noise of the summing amplifiers. An exposure can be anywhere from 1/4 second to 20 seconds, but typically this will be about one to four seconds. At full resolution, the read time of the CCD will be about 1/4 of a second. However, typical resolution will be 2x2 binned, or 256x256, thus, the read time of the CCD will be about 1/16th of a second.

The CCD output will have 12 bit resolution.

(b) KEO Image Processing Environment

There are two major options for image processing environments. The first is the MacIntosh IIci using a custom designed board to interface the camera to the MacIntosh and using commercial/custom software to control the camera and images. The drawbacks are that both the hardware components (the Mac and the interface board) are costly, and that all image processing has to be done in the computer's CPU. Accelerator boards could be added to speed up processing, but this increases costs. In addition, considerable programming effort would be needed.

The second option is to use an IBM clone platform running a powerful 386 at 25MHz with 4 Mbytes of RAM, and couple this with commercially available image processing hardware (Figure 1). Any IBM solution requires the capability of migrating from 16 bit operating systems (MS-DOS/Windows 3.0) to a true 32 bit OS.

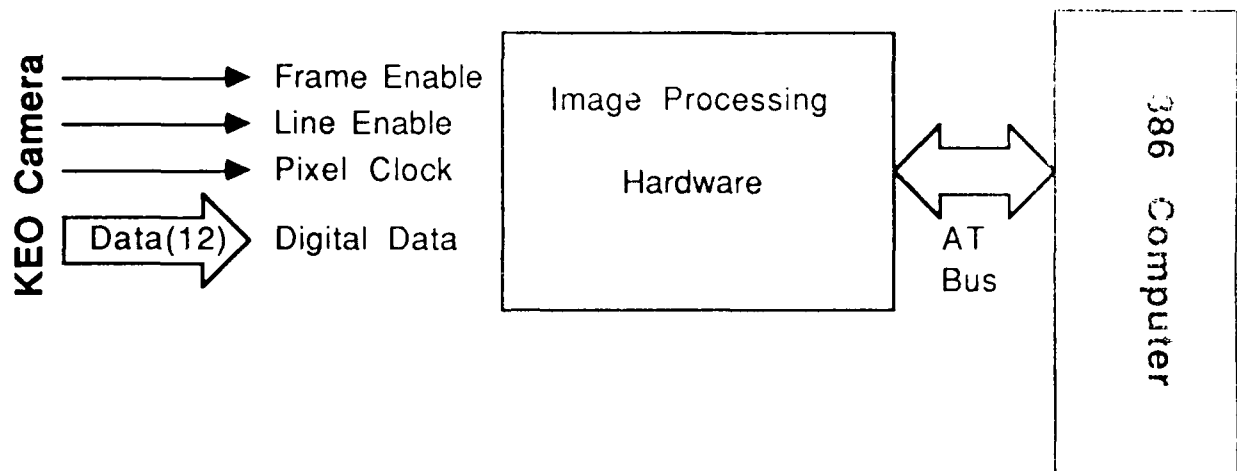


Figure 1: KEO System Overview

Image Processing hardware availability is mainly restricted by the need to have a 12 bit digital input port. There are three companies that presently make board sets with this function available: MATROX, Image Technology Inc., and CORECO (although their product is not yet to market). This report attempts to define our needs in image processing in order to fully investigate which environment will be most suited to this application.

Because this instrument is being designed as a small field instrument, we have restricted the field configuration to have only one monitor. Another monitor could be added back in the lab to facilitate data analysis. It would be preferable to have a monitor that fits in a 19 inch rack, so resolution might be a factor (i.e. are there 1280x1024 monitors that are small enough to be rack mounted?).

This design aspect requires the ability to have either some sort of VGA mixing scheme (i.e. Image Technology), or VGA switching (MATROX). A quick, efficient user interface to control all the controls of the camera will have to be developed. A final analysis of how our design could be implemented on each of the above systems will be the subject of another report (see **Appendix 3**).

(c) MIP Data Sets and Basic Image Processing Sequence

As stated above, the images will normally be acquired as 256x256 images clocked in at 1.1 MHz. Sometimes high resolution images will be desired at 512x512 resolution (Figure 2).

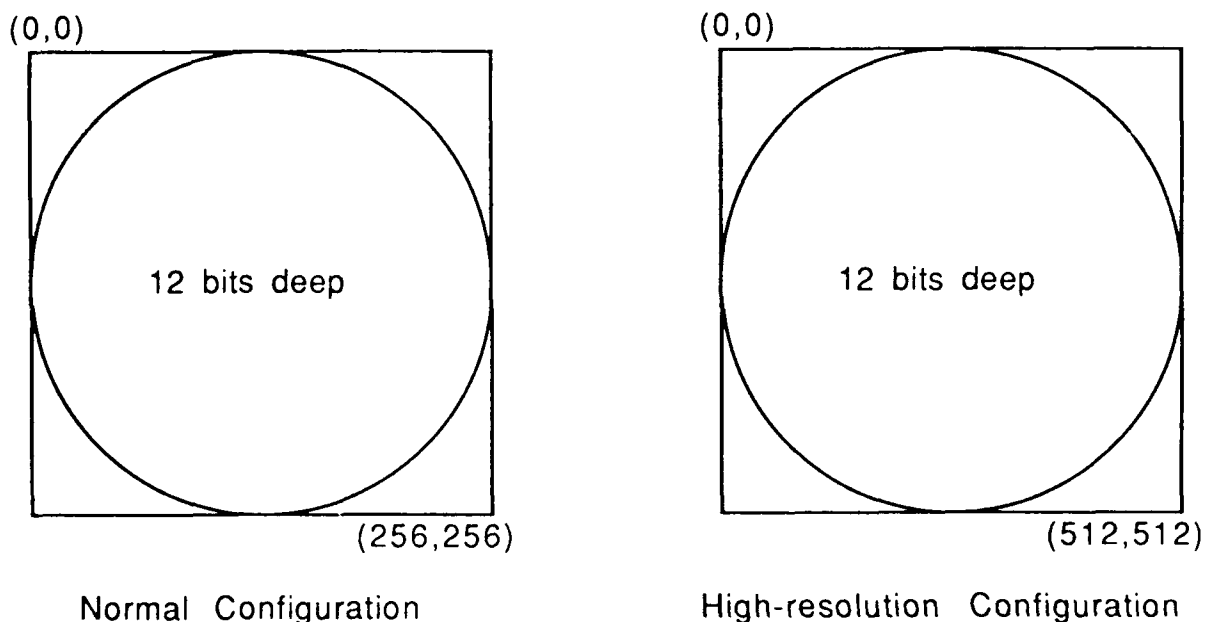


Figure 2: Image Format

Table 1 shows the capabilities of both the MATROX and the ITI IP board sets:

<u>Company</u>	<u>Memory</u>	<u>Frame Format</u>	<u>256x256</u>	<u>512x512</u>
MATROX	4 Mbytes	2Kx1Kx16 bits	32	8
ITI, Inc.	2 Mbytes	1Kx1Kx16 bits	16	4

Table 1: Number of Images stored in a Frame Buffer

Each data set can be considered as one block of memory to further divide up the total frame buffer. For instance, to view a data set of four images (the normal mode of operation), we would have four images contiguous in the frame buffer and display this section of memory. (Figure 3) For normal resolution, this would give us a 512x512 area of the frame buffer and for high resolution, this will give us a 1024x1024 area.

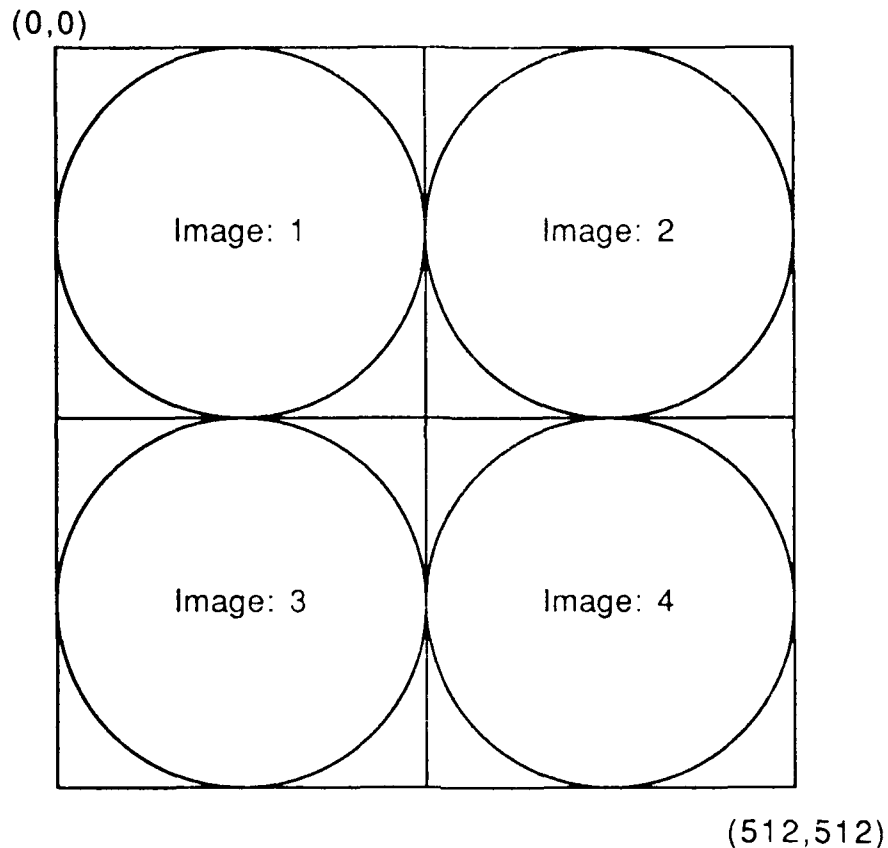


Figure 3: Typical Data Set

For each image we will discuss the typical image processing needs that might be implemented during data acquisition. Keep in mind that these operations have to be carried out for each image in the data set. (Figure 4)

The raw data would be acquired and stored in the Raw data area. Subsequent operations would be subtracting a noise image, multiplying the image by a flat-field correction (different for the four images because of the different filters used), taking a histogram of the data (not necessarily every cycle), and rescaling the image based on the results, and finally outputting this result to the display area so that four images can be displayed on the screen, each maximized for contrast based on its own characteristics. (See Figures 6,7,8.)

Using image processing hardware with a set Frame Buffer, one would then divide the buffer into four regions so that the data could be quickly used for analysis (Figure 5). [Background and Flat-Field images would be read in before the data acquisition process.]

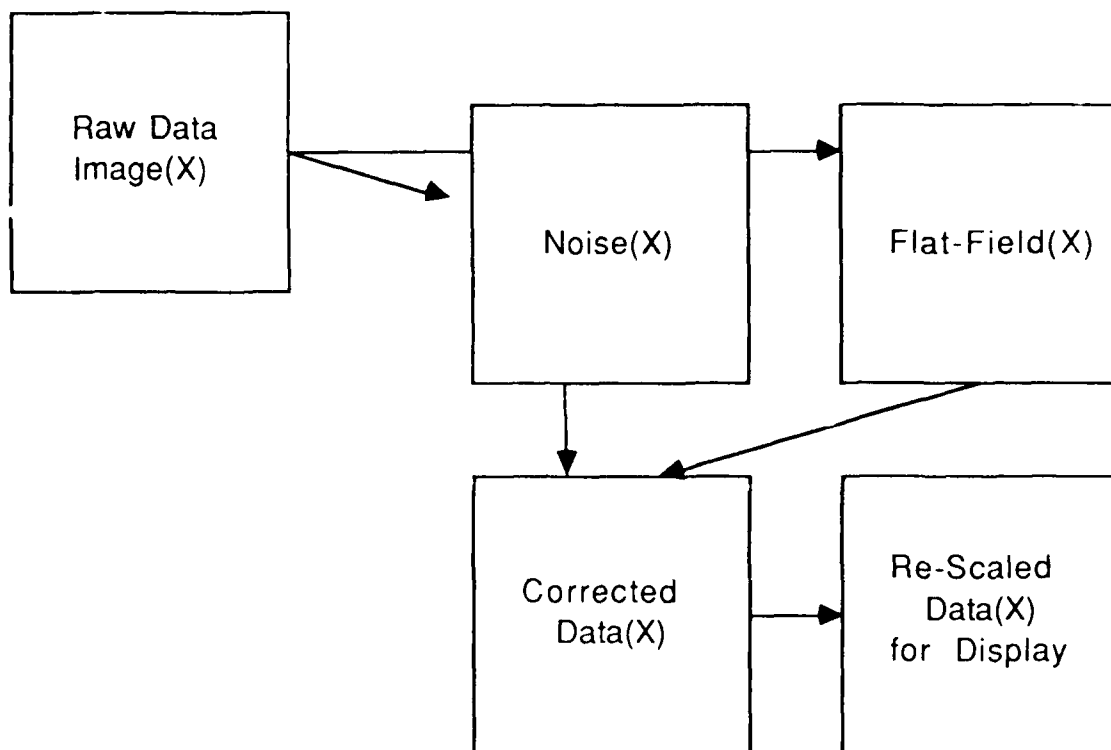


Figure 4: Data Process and Associated Frames Needed

(i) $\boxed{\text{Corrected Image}} = \boxed{\text{Raw Data}} - \boxed{\text{Background Noise}}$

(ii) $\boxed{\text{Corrected Image}} = \boxed{\text{Corrected Image}} * \boxed{\text{Flat-Field}}$

Figure 6: Mathematical Corrections for Data

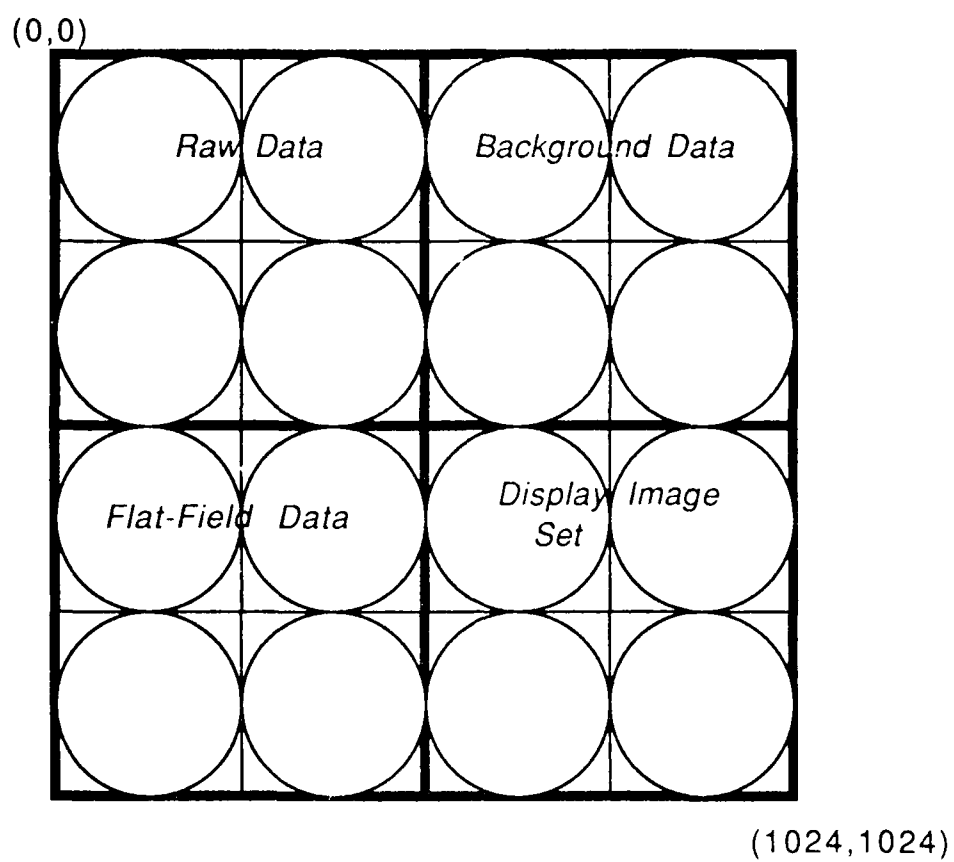


Figure 5: Representation of Frame Buffer

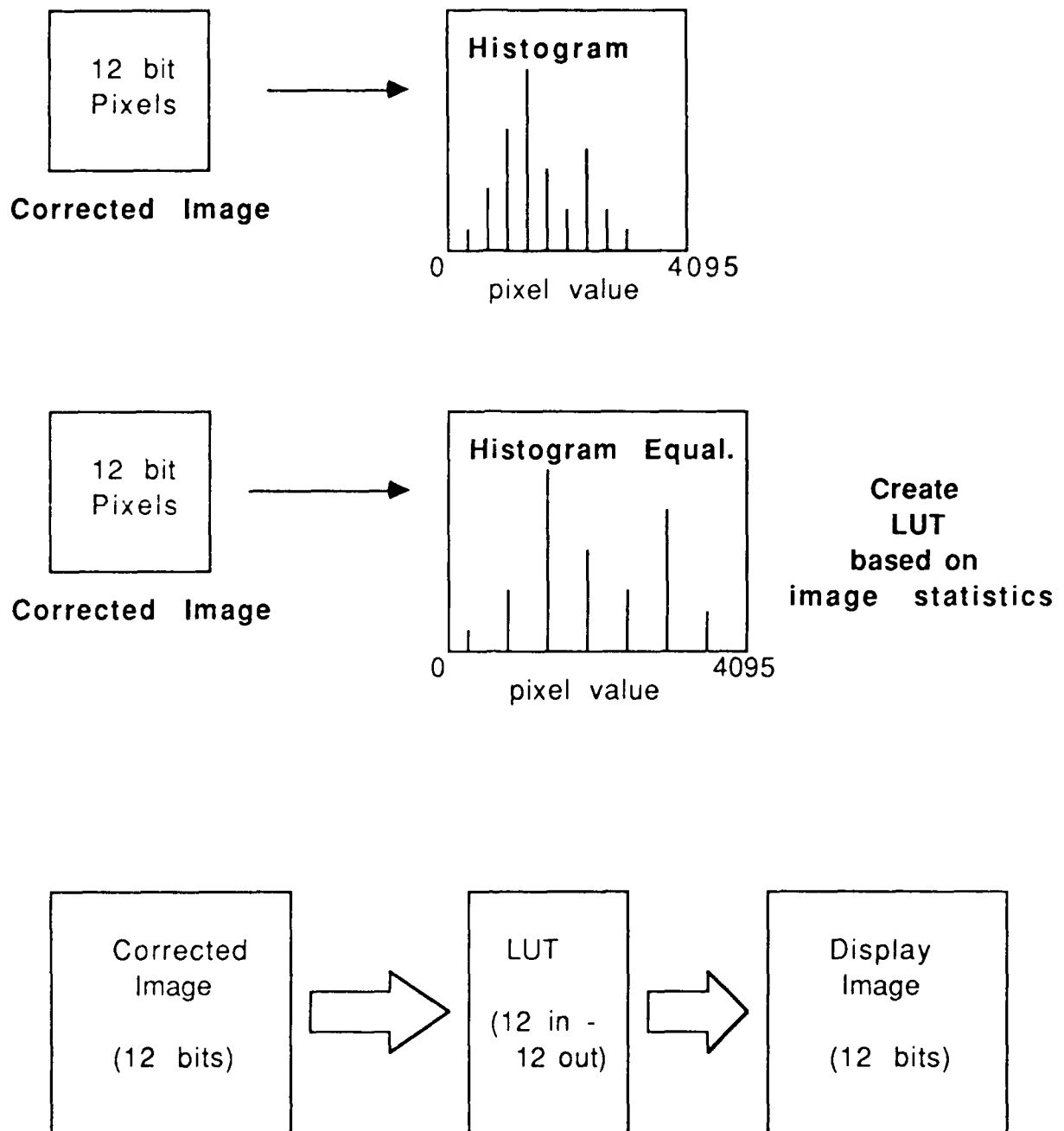
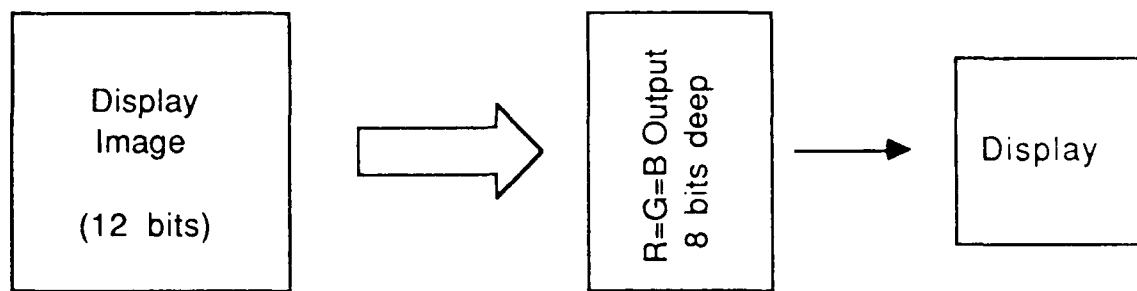
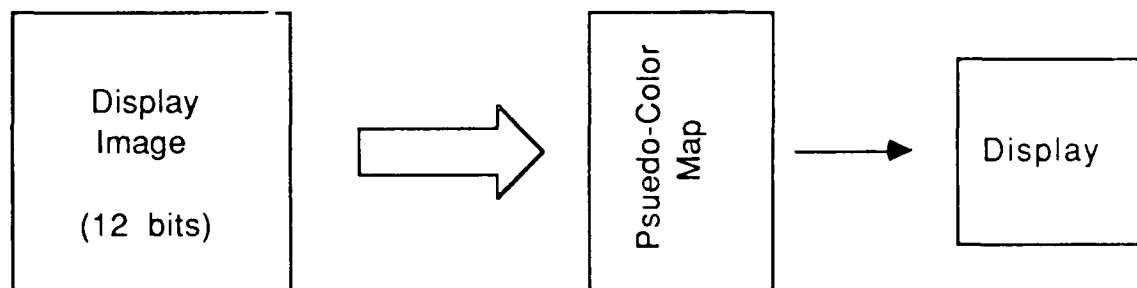


Figure 7: Create Display Image based on image statistics



(a) 12 bits Mapped to 8 bits Monochrome Output



(b) 12 bit Psuedo-Color Map to Color Output

Figure 8: Output Display Image in either Monochrome or Psuedo-Color

Most of these operations do not require real-time computations. In reality, if we collect four images every minute with a 2 second exposure. We will have typically 40 seconds of processing time for each data set. Most of the aspects of the image processing system that concern us in this process are the fact that the image is 12 bits deep rather than the typical 8 bits, and how the image processing hardware handles this. In software, this is not an issue (i.e. on the MAC) but on the image processing boards where you are limited to a finite number of functional operations, this has to be considered.

Two areas of concern are flat-fielding, and display. Flat-fielding is used to correct for known optical effects and CCD inconsistencies that are functions of the camera. Such corrections would certainly never approach a factor of 16, and expected maxima are 3 -5. To implement a high resolution flat-field, one needs to multiply the data by a correction factor and then subsequently normalize the pixel field. An example for 16 bit correction normalization to 16 would be:

- (i) Pixel x 16 bit flat-field Pixel
- (ii) Result = Result/16

If you wanted a flat-field of 3.5, the 16 bit flat-field Pixel would be:

$$3.5 \times (2^{16})/16$$

Normalizing to 16 gives us the advantage that to normalize the result requires only an Arithmetic Shift, rather than a divide. Another factor in using 16 is that final result from a 12 bit image will always fit inside a 16 bit data buffer.

The problem is that a 16 bit by 12 bit multiplication requires 28 bits for storing the result, and most boards do not have appropriate hardware capability. An alternate scheme has been developed using multiple 8 bit divides to get around this problem and is discussed in **Appendix 4**.

Displaying the results of a data set requires some thought only in that the output DAC's are set up for 8 bit resolution, and the data is typically 12 bit. Data could be scaled down so that the display buffer is only 8 bits deep, or perhaps the output hardware supports a 12 in, 8 out LUT. This would be ideal for psuedo-color implementation, where we could define a color spectrum that spans a full 4096 color range (Figure 9).

This describes the basic "automatic" mode of the MIP camera in terms of image processing needs. To summarize: Each data cycle contains four images, and repeats every 30 - 60 seconds. For each image collected:

- (i) Acquire image into Raw data buffer
- (ii) Subtract Noise from Noise buffer
- (iii) Do a flat-field with data from Flat-field buffer
- (iv) Every Nth image, do a histogram
- (v) Create LUT based on histogram results
- (vi) Create a transform image in display buffer through LUT
- (vii) Set display characteristics and display this buffer

Neither the MATROX board, nor the ITI board would be taxed by this application in terms of execution speed. In fact, the boards would be greatly under-utilized. However having the powerful capability of these boards would allow us to develop a field instrument with the power of some of the processing computers used in the lab, and would allow the scientist in the field many more options than an instrument purely targeted for data acquisition. Images could be analyzed during the off periods (daytime, bad weather, etc.). Tasks could be multi-tasked (since the IP hardware takes care of most of the work), and one could envision updating an "observation notes" file while collecting data.

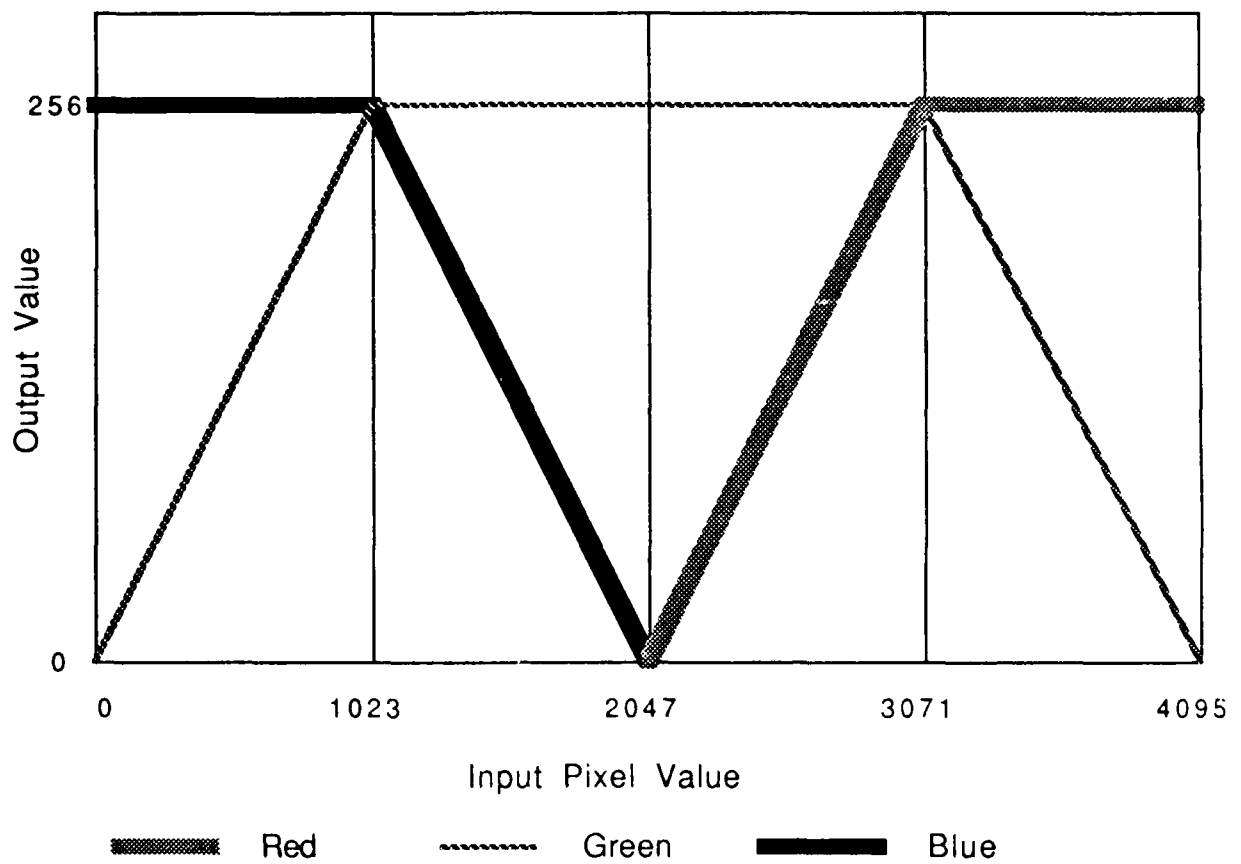


Figure 9: 12 bit in, 8 out Psuedo-color

In the largest view, perhaps some of the processing that was before restricted to non-"real time" applications could be implemented. A few operations will be discussed in brief in the next Section.

(d) Future Applications

The easiest applications that one envisions implementing are graphics and representation of data from other instruments in spatial coordinates relating to the MIP data. Such applications include representing radar data, position of magnetic coordinates, position of the sun with respect to the auroral oval, etc.

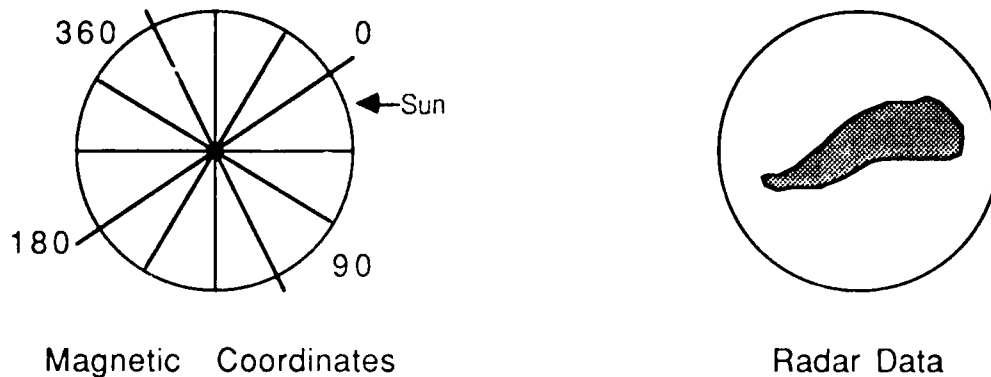


Figure 10: Example Graphics Applications

Another application to implement on the IP hardware could be the geometrical transformations that change the fish-eye coordinate system of the MIP to a real longitude/latitude coordinate system (NorthWest Transformation). This is currently being done on a 286 system and takes an unacceptable time. Implementing this algorithm on the MIP would make this instrument a very powerful lab analysis tool as well as the possibility of having a fast enough system, that this analysis could be done in real time.

There is a question as to whether this transformation can be implemented with the finite number of hardware tools provided either by MATROX or by ITI. Further research needs to be done to see whether this will have any effect on the Image Processing hardware choice.

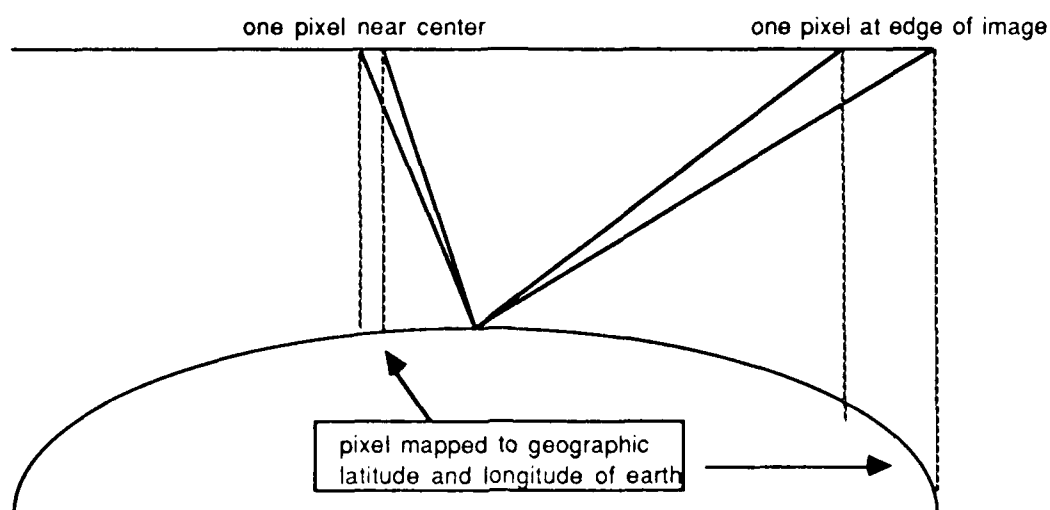


Figure 11: Representation of NorthWest Transformation

Finally, if we add a Fabry-Perot to the front end of the MIP, it would create a camera that requires a great deal of processing power to acquire data. The basic scheme would be to take 10 images (256x256) in succession each with a different Fabry-Perot spacing. For each pixel, there would be a 10 point curve which would be Least Square Fitted and a maximum determined for the curve which corresponds to a velocity. This velocity would then be displayed on an overlay of an image as vectors, much the same way the radar data is overlaid on the data.

These are just a few of the more complicated applications that one may want to implement on the new MIP. Obviously many more will be identified as the instrument is used. Thus, in conceiving of a final design, we plan to have a hardware/software system that matches our present needs well and provides a good path for future development.

Appendix 3

Imaging Processing Analysis

Keo Consultants 6/6/90

1. MacIntosh Solution:

The MacIIci is a very powerful computer housed in a small package. From this point of view it makes a very convenient field package, especially because of the graphical user features. Images and menus would all be displayed on the same screen which has a resolution of 640x480. This could be upgraded with additional hardware to include larger, higher resolution screens, multiple screen applications, and accelerator boards for graphics operations. In practice though, this would not really be necessary. One drawback of using the MacIIci is that you are limited to MacIntosh hardware. At present, the prices are much higher than for the IBM market, and there is a very limited amount of add-on boards that are useful for our image processing needs. This is changing, though, and many companies are bringing out more products for the Mac II series.

Another drawback is that GL uses primarily PC's, and so do most of the other labs working in the atmospheric community. Thus a MacIntosh Instrument, while small and powerful, might cause some transportability of data problems down the line.

Using the NuBus200 board for instrument control has the advantage of using the Photometrics hardware. We know this will work well with our camera head, because it has been specifically designed for the system. It has not yet been modified for our camera though, so delivery could be quite long (6 months would not be unreasonable). The Photometrics software package is very well written for scientific data acquisition, and is well proven in the old ASIPII. In addition, it will be incorporated in with the IPLab software package, which provides a large library of menu-driven image processing functions. Using the NuBus 200 Source code in MPW C++, and the IPLab User Customization Code in MPW C, we can easily incorporate a KEO user's system into the MacIntosh and have it operating as any other Mac application would run.

Experience has shown that Mac applications and system software are very memory intensive, and thus we would need to put at least 4 Mbytes of RAM, but would be safer with 8Mbytes for ultimate flexibility. All images would be stored in the computer RAM, and thus there is as much flexibility for display and manipulation as any other data array, or window. Using the standard QuickDraw routines, images will be able to be dragged, re-sized, and manipulated as any other window on the screen. Thus, this software implementation would allow us maximum flexibility in how many images are displayed, how big they are, etc. In addition, the QuickDraw routines, allow for easy creation of pallets and all the necessary graphics systems.

Writing the software as a MacIntosh application would be straight forward, and would mostly involve developing on the existing structure of the Nu200 Software and IPLab, rather than writing our own user system. There would be the initial effort of

learning MPW which is a complicated programming environment, and in addition, we would have to learn C++ which is an extensive Object-Oriented Language. This would provide very advanced code, but would take a great deal of effort for another person to pick up and learn.

The NuBus200 card has the drawback of not being able to take images from any other camera device, unless it was in strict accordance with the polled I/O Photometrics method. Thus, with this board in the computer, no other camera could be used. In addition, the processing power of the work station is limited by the processing power of the computer since all the work is done inside of the MacIIci. There are more image processing accelerator boards and other hardware peripherals becoming available, but they will add costs to an already expensive system.

Memory for the number of images desired is completely flexible, and the MacIIci does not have addressing problems associated with systems running under DOS. True multi-tasking while theoretically possible on the 68030, is very difficult on the Mac because of the operating system. A psuedo-multi-tasking system running under MultiFinder can be implemented. Software will require extensive use and knowledge of the intricacies of the Mac Toolbox, rather than a small set of image processing related commands. However, this will be minimized by the amount of software already written by Photometrics, and by IPLab.

Drawbacks are the incompatibility of the Mac with IBM systems which are the standard at GL, and a de-facto standard right now in the scientific community. Hardware upgrades are expensive and limited by the Macintosh Market. The plus of having the user friendly system, is reduced by the advent of Windows 3.0 which is very similiar (in some ways even better) than the Mac Operating System. The plus of the Mac in terms of this is that the Windows 3.0 developer's kit is not yet available, and there will be a large development effort needed to write all the menu drivers for the KEO system and the image processing system, that has already been written for the MAC (i.e. example IPLab).

A present software benchmark for the NuBus200 system, is that it can read a 1Kx1K image, scale it, and display it on the monitor in about 7 seconds with a MacII ci. For a 512x512 image, this translates to 2 seconds, and for a 256x256: 1/2 second. This is fast enough for our applications unless we desired to do real-time adding/subtracting, flatfielding, etc.

2. IBM Solution:

With today's computer technology developing so rapidly, it makes sense to buy a computer with state-of-the-art power now, so that it will not become obsolete over the next few years. Unlike the ASIPII, we envision that the new MIP will not only serve as a powerful field instrument but be a compact, powerful workstation back in the lab for processing the data. Thus, we would buy a 386 based machine running at 25MHz with 4 Mbytes of memory and a large disk drive (65-110 Mbytes). These are very affordable right now, and are available with high resolution graphics display drivers

and monitors preparing us for a true 32-bit workstation that can be migrated up into 32 bit operating systems such as OS/2 as it becomes more established.

An example computer would be the GATEWAYS package:

25MHz 386 IBM Compatible with:
4 Mbytes RAM
1.2M 5.25" Drive
1.44M 3.5" Drive
110M ESDI Drive
ESDI Cache Controller
16 Bit VGA with 512K
14" 1024 x 768 Color Monitor
1 Parallel and 2 Serial Ports
101 Key Keyboard
MS DOS 4.01
MS Windows 3.0
Floating Point Coprocessor

Software:
Microsoft C
Microsoft SDK 3.0

There are quite a few advantages with going with the IBM environment. The major advantage is that it is an open architecture, and there are a very large number of products available for any IBM compatible. This gives us the greatest flexibility in what the computer will configure, what hardware we want to use, and how we would want to upgrade the system (i.e. smaller configurations, ruggedized systems, portables, more powerful platforms such as the i486, etc.). And the total cost is about half of a comparable MAC Ilci system.

Another distinct advantage is that GL currently is only allowed to procure IBM compatibles, and the Macintosh is not supported through the Air Force. Therefore, almost all hardware/software environments already existing at the lab are IBM related systems. This means that another system designed around the IBM would remain compatible with existing systems, where there is already a large amount of expertise at the lab.

Another important advantage of the IBM is that the present NorthWest system resides on a 286 at the lab. This would be easy to port over to a new IBM based system whereas as Dave Lucas (who wrote the NorthWest software) feels that it would be totally impractical to port the system over to the Macintosh. The IBM system hardware is generally the least expensive choice and the most innovative as the market is so large. An example is that there are no applicable Image Processing boards available to use on the Macintosh as there are on the IBM series (three different companies to date). This results in available hardware solutions, data portability, and less new systems overhead.

In addition, the IBM is pretty standard in the research community (Steve Mende, et. al.) The IBM provides us with an inexpensive, very powerful, and flexible computing platform that will provide us with a good migrating path upwards in the next decade as the technology continues to develop.

One aspect of the MacIntosh that first attracted us to that platform, was the easy to use graphics interface. Now that Windows 3.0 has come out for the DOS operating system, we can write an almost identical application for the IBM as we can for the Mac, so this is no longer a concern. Windows 3.0 running on a 386 allows real multi-tasking, so we could shrink the KEO application down to an icon, have it taking images, and have a word processing window open, taking notes into a "logbook" file, or be graphing an old image, etc. This is a great tool to have in a field instrument.

Many applications are increasingly being written in object-oriented programs such as C++. While this is somewhat attractive for us, the Image Technology board is directly supported in Microsoft C. Therefore, to save the cost of a new language, and the cost of learning how to program in it, we think that development should start with Microsoft C.

There are also C implementations that utilize the true 32-bit nature of the the 386 processor. WATCOM 8.0/386 is a very good system. If we needed to upgrade to a true 32-bit language, WATCOM is 100% Microsoft compatible, so there is an easy upgrade path.

3.The Image Processing Hardware:

There are three companies that presently make image processing boards for IBM computers: MATROX, ITI, and CORECO. We have looked in depth at MATROX and ITI as these most closely meet our requirements. Both have their advantages and drawbacks, which we will discuss. First we should outline how these boards would be used and how this approach is fundamentally different than image processing on the MacIntosh.

In the MacIntosh solution, we have a board manufactured by Advanced Technologies that reads the camera data coming from the camera head, directly into computer memory. The board commands all the basic camera commands for image acquisition as well as our commands for the KEO interface through a serial interface. Once the image is in the computer, all processing is done through software and images are displayed up on the computer monitor as windows. This gives a great deal of flexibility in displays and processing, but has the disadvantage of taking up a great deal of computer memory, and requiring a lot of software development of image analysis.

The approach on the IBM platform is quite different. The two image processing boards we looked at have digital input ports. The images are read out of the camera as fast as the camera produces the data, directly into an image frame buffer which is on the image processing board. The image processing board has a very powerful graphics processor (the 34010 or the 34020 chip), an arithmetic logic processor for real-time math functions, an output video driver, and a large library of image

processing routines to control the board. Thus, the images are never put onto the computer, and the computer's main task is to tell the image processing board what it's next task is.

This is advantageous because the image processing board has hardware that is designed specifically for these types of operations and is very fast and efficient at it. In addition, this is the board's sole responsibility, and the CPU can be used for other processing applications that could be implemented in multi-tasking mode or whatever. Some disadvantages are that the image buffer on the image processing board is not as flexible as memory in the computer so you limit what you can do, by the image processing board you buy. Also the output display is not as flexible. There will be applications that you want to develop that are not capable of being implemented with the standard set of software routines provided, and thus might have to be implemented within the computer CPU. This involves an extra step of reading the image from the image processing board over to the computer, doing the calculation, and then back into the image processing board again.

A big advantage to the IBM boards are that they are compatible with many imaging products, from RS-170 cameras to Slow-Scan cameras. With these boards, the MIP Image Processing workstation could take data from many different sources all set up at the same time. One could envision having more than one instrument hooked up at the same time such as the MIP CCD camera head and an RS-170 camera input coming from another experimenter's camera. This degree of flexibility will prove to be very valuable when one considers that amount of different auroral cameras that the GL operates alone (film, video, CCD). The MacIntosh solution requires a very expensive board designed to specifically take the MIP camera. Other sources could be included but additional hardware and software would have to be purchased.

Windows 3.0 is nearly identical in use as the MacIntosh operating system, so anything that can be done on the MacIntosh could be done on the IBM now. However, the idea of buying image processing boards is that you won't have to use the main processor for most tasks.

3.1 Matrox Image Series Boards for MIP Application:

Using an IBM 386/25MHz PC, we could implement the MIP project using the MATROX Image Series board set. This is an extremely powerful 3 board set that includes an advanced display/frame buffer board, a digitizing board that has 16 bit digital input port capabilities, and an advanced Real-Time Processing board to do extremely fast mathematical calculations. In addition, a parallel Floating Point Processor will become available in the near future, allowing certain extremely fast computational tools that would give the MIP main frame capabilities.

An advantage that the MATROX does have is that it is completely system independent. The Image Series supports operating systems such as UNIX, XENIX, OS/2, DOS, and many types of languages. We consider a system with MS-DOS 4.01 and Windows 3.0 using MicroSoft C6.0 is used as this is parallel to the requirements of the Image Technology board set.

Discussion of Features:

The MATROX solution would give us the most powerful solution for the MIP and indeed a great number of its real strong points would be drastically under-utilized. The main reasons for choosing this system would be two-fold: the first is the ease and speed of implementing our application; the second is that with the extreme power available for image processing, new ways of displaying and analyzing data might be developed that were previously never thought of due to lack of available tools.

Large Capacity Frame Buffer

The Image Series features a very large frame buffer. The MATROX standard configuration has 4 Mbytes of memory. This can be expanded on board to 8 Mbytes.

<u>Image Size</u>	<u># with 4 MB</u>	<u># with 8MB</u>
512x512	8	16
256x256	32	64

At first glance this may not seem so important. Why would we want to be able to display 32 256x256 images at once in our frame buffer? The answer is that we can store all sorts of different types of information for the same image: raw data, noise, flat-fielding, radar-mapping, sobel-edge detection, warping images, etc. In the field, we would have the power to calculate all these functions and display them side by side.

Considering our own data set: if we were running in 256x256 resolution and were collecting 4 images/cycle, then we could have:

4	Raw Images
4	Noise
4	Flat-fields
4	Scratch area images
<u>4</u>	<u>Display images</u>
= 20	256x256 images

One can already see that to do these types of corrections at 512x512 resolution would require reading images on and off disk for each image, each cycle. This would greatly reduce our ability to do many of these calculations in real-time in the field.

Asynchronous Digitizer

Another feature that is very important to us is the digital input port. The ASD board allows either TTL or RS-422 information be acquired up to 16 bits wide. In addition, four separate video sources can be multiplexed into the frame buffer. This board gives us the greatest flexibility of input sources as any board available today. We require 12 bits, but there may be a point where we want to expand this to 14 bits, or there may be another instrument that requires 16 bits of information (i.e. radar information could be read in as 16 bit data and stored in the frame buffer).

The frame buffer is the only one available that can be configured as 32 bits deep, thus giving the capability of very high precision image arithmetic and true color but neither of these are particularly applicable to the MIP.

Another feature of the Image Series which has potential use is that up to 16 ASD boards can be hooked up to one Baseboard. This would give any PC the power to have many different sources hooked up to the same camera. This could be useful for us if we were to build more than one camera and wanted to sometimes incorporate a system with two cameras (i.e. more filters, one camera with background filters, different types of cameras, different field-of-views, etc.)

Advanced Graphics System Processor (GSP)

The Image Series uses a 40MHz TMS34020 GSP chip which is the most advanced available. This means that the graphics capabilities of this board are outstanding. This is applicable to us mainly in terms of data analysis. The Image Series board set is ideal for data analysis where graphics are overlayed on top of the images for analysis. We do a lot of this type of work, and it seems that our applications in the future will require more and more of this ability. The 34020 has been maximized for this kind of task.

Overlay Frame Buffer

The Image Series board set has a separate overlay frame buffer that is 2Kx1Kx4 bits. This means that the overlay has no effect on the data (even if we were using 16 bit data). There is twice as much overlay as the frame buffer resolution allowing you to create complicated graphics applications off-screen and then pop them instantly up on the screen. This overlay buffer gives you the ability to create a very flexible and pleasant looking user interface using menus, graphics, and bit-maps with 16 color resolution. The Image Shell comes with a very extensive set of tools to create these interfaces including multiple fonts and text formats. An X-Windows driver is presently available that makes the overlay look just like an X-Windows application, and a Windows 3.0 driver is expected to be developed.

VGA Switching

A drawback is that there is no VGA mixing available. In software, one can switch back from VGA to the Image display board, so that if the operator wanted access to the computer system, or change parameters under Windows 3.0, etc., you would just select the VGA screen from software and then switch back when finished. An application written for this board would not be implemented this way, but the capability is there for use in multi-tasking applications and perhaps very complicated set up procedures.

Real Time Processing (RTP) Features

The RTP board is specifically designed to execute image processing functions in real time. Perhaps this is the real selling point of this board, and for people in the

image processing field who want a small, affordable, but extremely powerful processing workstation, the Image Series board is clearly unmatched in this regard.

There are seven custom gate-array chips on board the RTP that have been especially designed to maximize the image processing functions. This is achieved by having the processors run in pipelined parallel processing. The RTP board can add, subtract, multiply, etc. pixels at rates of 15MHz. Thus, all mathematical processes can be done in one pass through the image, giving the ability to implement these functions at video rates. Of course this is complete overkill for us considering it takes us at least a second to acquire an image. What is more important though for this board is that in addition to the math capabilities, there is a Statistical Processor, and a Neighborhood processor implemented in hardware. There is also an arbitrary region-of-interest (OOI) hardware implementation which would allow us to only process an arbitrarily-shaped subset of the image thus saving processing time.

Statistical Processor

The Statistical Processor allows you to do histograms in 1/50th second, and all the statistical calculations that go along with it, such as equalizing an image based on the histogram values. One way the RTP does this is that it has a 64 Kbyte by 24 bit Look-Up Table (LUT) that is used for real-time calculations. Math functions such as multiply, divide, sine, cosine, quadratic equations, etc. can be mapped into the LUT and an image can be processed at 15 MHz using this method.

Again, for us, this is complete overkill. We do not need histograms at 1/50th of a second. But the 64K Statistical LUT has many applications that are directly applicable to us that make this an important feature to consider. One immediate application would be in the way we acquire and display data. One would like to set up a system where the computer automatically sets the displays for the images, so if the auroral activity greatly increases, the display scale is automatically adjusted. Since we want to display four images typically at once we need to separately scale each image to the output image. Every ten or so images we could compute a histogram and set up a new display for each image based on the results. This requires 4 different 12 bit LUT's for every cycle. Since a 64Kbyte LUT can hold 16 12 bit LUT's, many different transforms (i.e. four display LUT's, four Multiplication tables for flat-fielding, etc) could be kept at all times. This means that we could acquire and display corrected data as quickly as we could collect it.

Neighborhood Processor

The Neighborhood Processor would allow us to do real-time neighborhood processes that involve convolutions and kernals. These sort of things include sharpening, softening, noise removal, Sobel edge detections, Laplacian edge detections, grey-scale erosion and dilations, etc. While we have never really used these functions before, there may be cases when we would. For instance, if we are interested in studying the plasma flow along the edge of the aurora and correlating this with radar data, it might be useful to be able to display an auroral arc with a Sobel edge detection on it.

These are things that one would only develop through experimentation. There are not really any applications for the neighborhood processor in the MIP as we presently envision it. However, it might pay off in the long run to have such tools available to the scientist should an application arise.

Floating Point Processor Option (FPU)

The Image Series will have the option of adding a floating point processor. The FPU is the companion chip to the TMS34020 and thus is fully implemented into the system architecture. Its true power lies in the fact that it can run as an independent processor and thus, give very high processing speeds. Software for the FPU option is just becoming available. Ideally, we would want to be able to program our own algorithms using this processor, but this will not be practical as the programming would need to be implemented in micro-code and would be too time consuming to develop. Instead, the FPU, much like the rest of the board, will be supplied with a set of routines with optimized routines for the FPU.

The set of routines will be image processing oriented such as transformations, and FFT's. Some high-precision math functions will also be available. An important question for us to ask is: can we replace the NorthWest Transformation and implement it on the MATROX board in hardware? If we could, it would be a big selling point for the board. Presently, the FPU routines will supply an arbitrary 2nd order geometric warping function that will implement in 2 seconds. Dave Lucas seems to think that this may be able to approximate the NorthWest transform. If this is the case, the MIP with this capability would be able to transform the MIP images to geographical coordinates in 2 seconds per image, whether the image was stationary or moving. This is an incredibly powerful tool not only as a field instrument but also for speeding of the process of data analysis in the lab.

The drawbacks of the FPU are that it is not really feasible to program our own algorithms into it, and that the 2nd order warping function is not really the NorthWest Transformation. So we would have to investigate whether the investment required for this feature is justified.

Frame Buffer Memory Mapping

A final architectural point of the Image Series board that should be noted is that the frame buffer can be fully mapped into the PC's high map. This means that the 4Mbytes of memory could be mapped into the PC, say at memory locations 4MB to 8Mbytes. This is a powerful feature for implementation of custom developed algorithms that run in software. With this feature, we could automatically access the data in the frame buffer without having to read back and forth between the frame buffer and the computer's memory.

Of course, we again have to decide if this is really an important feature to us. At 8MHz bus speed, a 512x512 image would take approximately 1/4 second at the most to read into the computer's memory. A 256x256 image would only take a fourth of that.

MATROX Support

MATROX is a quickly expanding company with a long history of producing image products. Their company headquarters in Dorval is very impressive and their sales engineers and application engineers have been extremely knowledgeable, helpful and additionally always prompt and professional in returning calls and filling requests for information. The Image Series is in production mode with boards at REV 2.0, and there are about 60 companies with about 400 boards in the field. MATROX is always working on developing new products both for image processing in general and in addition to further expand the capabilities of the Image Series using the 30MHz Image Bus. I believe that MATROX would supply superb technical support especially now that we have visited the company.

Drawbacks and Thoughts

The first immediate drawback is that this is definitely the most expensive solution. One would really have to decide if the features of the Image Series are worth the investment. However, comparing the options, the MAC IIci option would have a similar and not give nearly as much power as the MATROX board. The costs of the MAC computer, and the customized Photometrics board reduce the cost benefit of this option greatly when compared to the MATROX.

Another drawback to the MATROX is that the output resolution is 1280x1024. This means that the smallest screen we could use would be a 16" monitor (although smaller ones might become available). High resolution is very nice, but limits our choices in monitors. The VGA switching scheme is adequate but a mixing scheme such as developed by Image Technology seems better.

The MATROX board is definitely a three board set. It is possible to use it as a two-board set without the RTP, but then the real power of the board is lost. A three board set limits your ability to miniaturize the system, where as a one (ITI VS-100-AT) or two board (ITI AFG) implementation might give more flexibility of packaging. For example there is a portable available that has a built-in 8" 1024x768 color monitor.

When investing in such expensive hardware, we have to look at how much of what we do is applicable to that hardware and how much we would have to invest in software. Software has the advantage that it can be easily modified, ported over to different systems, and its performance can be steadily increased as hardware improvements are made. An example of this is the NorthWest transformation being implemented on the 12 MHz 286, verses on a 25MHz 386, and even on a 33MHz i486. We could spend the extra dollars on a high performance i486 rather than on hardware that will always be the same. (The advantage of course of the hardware is that it has already been maximized for the specific application.)

Thus, a strategy needs to be developed. Do we want to invest a great deal now in hardware, or slowly migrate up with the evolving technology. The point should be made that the MATROX hardware does not limit you to migrating up as well, as we can still implement our applications in software as noted in the above discussion

In the final analysis, we have to decide how much of our application we want to develop in hardware and how much in software. We also have to remember that a particular piece of hardware does not restrict us from developing software, but makes the investment in the hardware less worthwhile if it is underutilized. In terms of a flexible system that immediately meets our needs without extensive new programming, etc., the MATROX is clearly our best solution, one that also clears the best path for the future of the MIP in terms of choices of operating systems, powerful tools, and flexibility. We must decide how much we want to have such a system, versus a cheaper system that is not such a powerful image processor.

3.2 Image Technology Boards

Image Technology, Inc. (ITI) offers a 3 board set called the Advanced Frame Grabber Series for the IBM. Two of the boards are currently available, and these are the base boards that we would need to control the MIP. The two board set includes a 1K x 1K x 16 frame buffer a 16 MHz TMS34010, an 16 bit ALU with 8 bit Multiplier/Comparator, 12 bit digital input port, 3 RS-170 inputs, all the appropriate LUT's, and a VGA mixing option:

Advanced Frame Grabber Kit with VGA Option:

VP1510-KIT-512-U-C2-M3-AT

ITEX-AFG Subroutine Library:

ITEXVP1500-A-S

Options:

TMS 42010 Graphics Development Software Kit:

GDK-VP1500-A-S

Image Processing Accelerator (2Mbyte):

VP5102-KIT-AT

With 4 Mbytes:

VP5104-KIT-AT

ITEX-IPA Subroutine Library:

ITEXVP5100-A-S

TMS 320C30 Program Development Kit

From the above list, one can see there are many configurations of this system. This is one of the advantages to the ITI board set. We could start with the minimum configuration which in most cases is probably more than enough power for our application, but as we want to expand the use of the MIP, additional boards or software can be added. Additional needs might be: higher resolution data runs (processing at 512x512), complicated processing algorithms such as geometric transformations at acquisition rates, complicated image processing to unfold Fabry-Perot data.

Let's step through all the configurations and briefly discuss what the options offer:

- . Minimum configurations:
A powerful platform for the KEO camera using 12 bit 256x256 images
- . Adding the TMS Software KIT:
Allows us to add on-board routines utilizing the power of the TMS34010 tailored to our specific image processing needs, getting past the obstacle of having to write data into the computer over the comparatively slow bus. (Not that much of an issue with 256x256 images.)
- . Adding the Image Processing Accelerator:
(This does no longer include the TMS kit, is priced for a 2 MByte configuration, and includes the IPA software)
This allows us to process images in real-time, increase the memory capacity of the board-set by two and would allow us the capability to do histograms, geometric transformations, convolutions, and such at real-time speeds. In addition, this board has two serial ports, and a generalized parallel I/O port. This is particularly applicable if we were to add a Fabry-Perot instrument to the camera that would need a great deal of processing power, and additional instrument control.
- . Upgrading the IPA to 4 Mbytes of memory:
Would allow us to process more images; most likely not necessary unless we wanted to do a great deal of image to image processing on 512x512 images.
- . Using the IPA with the Software Kit: (2MB)
Would allow us to write custom code for the IPA that was located on the board itself (similar to the TMS Kit).
- . Rolls-Royce: AFG with IPA, and both Software Development Kits:
With 2 Mbytes
With 4 Mbytes

It should be kept in mind that neither the TMS kit or any of the IPA products are available yet. The TMS Kit is completed, but not packaged for the public yet. The IPA hardware is completed, but the software is not yet complete.

Thus, using the ITI board set, we have a large range of Image Processing platforms we can use. Most of the research has been completed, and this is the lowest cost system.

Hardware Description

The following outlines the functionality of the Image Technology AFG Board Set from the input to the output stages. Figure 1 is the AFG Block Diagram taken from the AFG User's Manual. It gives a detailed hardware description and shows the bit resolution of all the functions on the board.

The frame buffer is 16 bits deep, so theoretically we can use images up to 16 bits of resolution on this board. In practice, though, there is really only 12 bits of resolution because none of the inputs support 16 bits, except the VISIONbus. Theoretically, if we need to get higher resolution, we could build a camera interface that would directly interface to this bus.

The AFG has five different inputs. Four are regular RS-170 camera inputs, except that variable scan video inputs are also supported with the many synch signals

that come into the board. All video signals are converted to 8 bit deep images, and depending on the board, are converted to 512x480, or 640x480. We would use the 512x480 mode so that we could fit four images into the frame buffer.

The most important input port to us is the Digital Input Port which supports images of any size (depending on the incoming clock signals) and has a maximum resolution of 12 bits. This is perfect for our MIP design and the camera electronics have been made to be compatible with this board. At this point, the data can go directly into the Frame Buffer along a 16 bit data path.

The display memory is 1Kx1Kx16 bits. The upper four bits of display memory are typically used for graphics overlays, but there will be cases where we will want to use all 16 bits as real data (i.e. image arithmetic).

There is an ALU section (Arithmetic Logic Unit) on the board that can do 16 bit addition/subtraction, barrel shifting and logic operations at the full speed of the board (16MHz for an image and a constant, and 8MHz for two images). This means that images can be processed as fast as the clock cycle of the board. A typical application would be to subtract a background image from the data. For a 256x256 image, there are:

$$\begin{aligned} 256 \times 256 \text{ pixels} &= 65536 \text{ pixels} / 8 \text{M pixels/sec} \\ &= 8.2 \text{ msec/image} \end{aligned}$$

For a 512x512 image, the benchmark is 38 msec/image. This shows that for a lot of the image arithmetic we want to do can be done in real time. This gives us a capability we have never had before.

The Processing section also has a 12 bit LUT. This will be very useful to process images in real time to create an output buffer. Our application would be something like this: We have 1/4 of the frame buffer reserved for the four 256x256 images from the camera, but to display them, we would want to display them all with different intensity scales. So for each image, we do a quick statistical analysis, set up the LUT table and write the image into the 1/4 of the frame buffer that is output to the monitor.

The only drawback to this processing section is that the multiplier only allows 8 bit inputs (which makes sense since the maximum output can only be 16 bits). One thing we would like to do in the field is to correct the image for optical aberrations (i.e. a flat-field). This would require us to multiply the image, by its appropriate flat-field correction. Ideally, this would just multiply one high resolution number by another. While we could read the image into the computer and do it there, or with the TMS software development kit, you could write some code for the 34010 (a 32-bit processor) to do it quicker, we can also overcome the processor limitation and do a higher resolution multiplication using a multi-step method described in Appendix A. If we were to use an 8 bit flat-field, a 256x256 multiplication would finish in:

$$\begin{aligned} 256 \times 256: & \quad 1/20\text{th second} \\ 512 \times 512: & \quad 1/5\text{th second} \end{aligned}$$

For a 16 bit flat-field:

256x256:	1/8th second
512x512:	1/2 second

It may be seen from these results that we could do basic image processing functions at data acquisition rates. This would also allow us to expand tools for image processing in the field.

The frame buffer is 1Kx1Kx16. This would allow us to hold:

4	512x512 images
16	256x256 images

While this seems sufficient, there are a few limitations that we have to consider. First of all, the new MIP filter wheel will have provisions for five filters. If one of these is going to be a background filter, then there are only four images of interest. If we wanted to take in five 512x512 images, we couldn't fit these images into the frame buffer without writing one of these images into the computer's memory. In addition, to really display these images together on one screen, we will need to display them at different intensity scales. To do this in 256x256 mode, we would create an area in the frame buffer for the output images to sit, but in 512x512 mode, there isn't any room.

With this problem in mind, one has to evaluate how important it is to have 512x512 capability. If the board set were upgraded with an IPA board as well, then there would be ample memory available:

IPA with 2 Mbytes:	8	512x512 images
	32	256x256 images
IPA with 4 Mbytes:	12	512x512 images
	48	256x256 images

Let's discuss how one could set up the frame buffer using 256x256 images and assuming that only 4 filters are ultimately used. The frame buffer could be set up into 4 distinct areas each holding four images. The first would be the raw data. The second would hold the flat-fielding or background data. The third would be an area for scratch arithmetic. The fourth would be the screen buffer, containing the final images that would appear on the display monitor. This would allow us a very flexible image processing system. If one wanted to use five filters and display five images on one monitor, there are many ways to do this, but we would have to think about the best way to implement this.

The TMS34010 is the main processor on the image board and it is a true 32-bit CPU designed specifically for graphics operations. It controls all communications with the host computer (our 386) and all the graphics operations.

The display interface has a 12 bit in 8 bit out LUT which is exactly what we need for our images. With this LUT, we can do instantaneous pseudo-color renditions of

images, scaling, etc. There are three color LUT's which provide the color palette and finally the tri-DAC video output to a high-resolution multi-synching monitor. The TMS34010 can program images to any monitor, so that we can have as many different resolutions on the output as we have monitors. This is helpful if we wanted a small, low resolution monitor for use out in the field, but a large, high resolution for use in the lab. We could simply just switch monitors and set the board up for the new resolution.

The final piece of hardware that we would use would be the VGA mixing board. This would allow us to use only one monitor for our image processing workstation. In traditional image processing, you typically have one monitor displaying the images and one acting as your computer terminal (much like the ASIP and NorthWest System operate). To reduce size, we want to be able to operate using only one monitor (at least in the field). The VGA board allows us to operate in both modes. When in the lab, if two monitors was desired, we could take out the VGA board and use two monitors. In the field, we could insert the VGA board and use only one monitor for display.

The VGA board allows us to have menus, and windows over the images, or vice-versa. This would be very useful to us, as we could make the application run from one terminal using all the graphics interface techniques of the Windows 3.0 system, and have the images on the same screen. While the software is running automatically, the application icon could be shrunk in the corner. When the operator wants to change a parameter, they would simply click the mouse on the icon, and the user menus would pop-up just like a normal Mac application. This would give us a consistent and easy user interface, that wouldn't have to be different depending on whether you used a one monitor or two monitor system.

The output resolution with the VGA mixing board is programmable to either 640x480, or 800x600. This provides us with good resolution for small monitors for use in the field, and provides comparable resolution to that of the MacIntosh.

Software Description

The AFG board set has a set of routines called the ITEX-AFG. This forms a fairly complete set of image processing routines from graphics functions, image arithmetic, and LUT management to geometrical warping functions, convolutions, and morphological functions. The software has been very carefully evaluated for this application, and has been found to be very suitable.

There are some tasks that would require more manipulation, such as the multiplication for flat-fielding but this is hardware limited and the same manipulation would have to be implemented on the MATROX system.

Another area of concern is transforming 12 bit Corrected data into re-scaled, displayable formats -- either grey-scale, or pseudo-color. This would be implemented by writing LUT transforms into and out of the INPUT LUT which is 12 bits in/12 bits out. The problem is that for every image, every cycle, an LUT would have to be read in and out of the INPUT LUT, taking up a considerable amount of time. We have yet to obtain timing parameters from Image Technology so this may not be a concern. It is an

unfortunate restriction of the hardware. The solution is to overcome this by having a 64Kbyte x 24 bit LUT, so that 16 LUT's could be stored if necessary.

Functions such as histograms take about .325 seconds for a 512x512 image (although this has to be confirmed). So for a 256x256 image, the histogram would be about .325 seconds which is much faster than we realistically need.

All the image processing functions that we need are available under the ITEX-AFG package. The routines are not as flexible, powerful, or as quick as the MATROX board set, but that seem to match our needs well.

Summary

The AFG Series provides us with the least expensive solution for an MIP workstation. It has the advantage of having several different paths of upgrading it both through new ITI hardware such as the IFA board, and through upgrading the computer system such as to a 33MHz 486, and implementing a lot of the functions in the computer.

There are some limitations however. The biggest one would be the fact that the buffer size is limited. This is a problem we will run into immediately and we have to decide if the capability of more than four 512x512 images is important to us. Other limitations will be in speed. It seems that the benchmarks of the AFG will be a little faster than the MacIntosh solution, but can not be improved by upgrading the computer. However, a final analysis of performance verses our needs will be completed in the near future to see if these are real issues to us.

The ITEX routines will give us a capability of experimenting with different image-processing techniques such as Sobel Edge detection if we ever wanted to do such things. The AFG is an excellent compromise between performance and price.

Appendix 4

Flat-fielding Scheme with 8-Bit Arithmetic and an alternative 16-Bit Scheme

Keo Consultants 6/15/90

With 8 Bit Arithmetic, we can still achieve a flat-field with our data in real-time using the following method. We limit ourselves to an 8 bit flat-field correction, giving us a resolution of 255. We could further increase this correction to 4095, if we wanted to extend this algorithm to a 16 bit flat-field.

First, let's define a flat field. If we assume the center pixel value to be the normalized pixel, then everything is related to this. This is not necessary for the algorithm, but it makes it easier to picture. Suppose we exaggerate and consider we could lose 1/8th of the signal, due to vignetting and other optical losses. We could then, for the sake of the algorithm, define our 8 bit flat-field to map to a 0 to 8 correction. This gives us:

$$8/256 = 0.03125 \text{ resolution.}$$

Thus, if a pixel towards the edge of an image needs a correction of 4.5 due to vignetting, image intensifier effect, etc., the flat field value would be:

$$4.5/0.03125 = 144$$

To achieve maximum flat-fielding resolution, we could normalize the 8 bit flat-field value to the actual flat-field data:

$$\begin{aligned} \text{minimum pixel} &= 0.57/\text{center pixel} \\ \text{maximum pixel} &= 5.60/\text{center pixel} \\ (5.60-0.57)/256 &= 0.0196 \text{ resolution.} \end{aligned}$$

Thus, a pixel which needs a correction of 4.5, would have a flat-field value of:

$$4.5/0.019 = 229.$$

While this would give us the most accurate flat-fielding result, we would have to do a divide to renormalize the data, and this would take quite a while. If we limit our flat-field normalization to 8 or 16 (a resolution of 0.0625), then to re-normalize the data, we can just do an arithmetic shift to the right of 3 or 4. This can be achieved at the clock rate of the ITI AFG board.

The following algorithm uses all the standard AFG routines, and each take one pass through the ALU on board, thus we will calculate the flat-field time next:

The flat field will be called FF and is 8 bits deep: FF(8).
 The data will be called D and is 12 bits deep: D(12).
 The high byte of D is called D(H), and the low byte D(L).
 Resultant mathematical fields are labeled F1(16), F2(16).

The following is a step by step algorithm:

- (i) $FF \times D(L) = F1$
- (ii) $FF \times D(H) = F2$
- (iii) $F1 = ASR(5) \rightarrow F1$
- (iv) $F2 = ASL(3) \rightarrow F2$
- (v) $F1 = F1 + F2$

Result is stored in F1 and has 16 bits of real data.

Here is an example:

Normalize to 8: Resolution is 0.03125

Take a pixel whose flat field is 2: $2 / (0.03125) = 64$

FF(8) = 64 01000000

Take a pixel data value of 2730:

D(12) = 2730 0000101010101010

Result should be: $2730 \times 2 = 5460$.

(i) $FF \times D(L) = 10,880 = F1$
0010101010000000

(ii) $FF \times D(H) = 640 = F2$
0000001010000000

(iii) $F1 = ASR(5) \rightarrow F1 = 340$
0000000101010100

(iv) $F2 = ASL(3) \rightarrow F2 = 5120$
0001010000000000

(v) $F1 = F1 + F2 = 5460$
0001010101010100

Each pass takes 38 msec for a 512x512 image. Thus, for the above flat-field, the process took:

$$5 \times 38 \text{ msec} = 190 \text{ msec (or 1/5th second).}$$

This corresponds to roughly a 7MHz pixel rate. Normally, our images will be 256x256 (which will also give us plenty of scrap room in the memory of the AFG), and thus our pixel time will be reduced by 4, so a flat-field this way would be achieved in about:

$$\text{Flat Field for 256x256: } 50 \text{ msec (or 1/20th second).}$$

A 16 bit flat field would have a much higher resolution, and would take probably about 4 times as long.

Note that we know as long as our flat-field ratio is under 16, we will never have a data overflow, because our data is 12 bits, and the pixel depth is 16.

The 16-Bit Alternative:

Increasing the resolution to 16 bits, would mean needing a 32 bit result for the data and thus increase the mathematics greatly. The following is a simplified scheme using a 16 bit flat-field, and normalizing the flat field to 16:

$$16/65536 = 0.00024$$

The solution is:

- (i) $FF(L) \times D(L) = F1$
- (ii) $FF(H) \times D(L) = F2$
- (iii) $FF(L) \times D(H) = F3$
- (iv) $FF(H) \times D(H) = F4$
- (v) $F1 + \text{ASR}(8)[F2] = F1' + \text{CARRY FLAG1}$
- (vi) $F1' + \text{ASR}(8)[F3] = F2'' + \text{CARRY FLAG2}$
- (vii) $F4 + \text{ASL}(8)[F2] + \text{CARRY FLAG1} + \text{CARRY FLAG2} = F4'$
- (viii) $F4' + \text{ASL}(8)[F3] = F4''$
- (ix) $\text{ASR}(12)[F1''] = F1^*$
- (x) $\text{ASL}(4)[F4''] = F4^*$
- (xi) $F1^* + F4^* = F1^{**} = \text{RESULT}$

Time for each for this process adds up to 15 passes through the processor. For a 512x512 image:

$$15 \times 38 \text{ msec} = 570 \text{ msec (just over 1/2 second)}$$

For a 256x256 image:

$$15 \times 9 \text{ msec} = 135 \text{ msec (about 1/8th second)}$$

Let's take an example:

Flat field = 5.35 --> $FF = 5.35 \times (65536/16) = 21913.6$
Data = 1736,

Result = 9287.6

	FF:	0101010110011010
	D:	0000011011001000
(i)	F1:	0111100001010000
(ii)	F2:	0100001001101000
(iii)	F3:	0000001110011100
(iv)	F4:	0000000111111110
(v)	F1':	1110000001010000 + no-carry
(vi)	F1'':	0111110001010000 + carry
(vii)	F4':	0000010010000001
(viii)	F4'':	0000001001000100
(ix)	F1*:	0000000000000111
(x)	F4*:	0010010001000000
(x)	RESULT:	0010010001000111
		= 9283

Error is: $(9287.6 - 9283)/9287.6 = .0005$ (or .05%)

Doing the same calculation with the 8-bit scheme gives 9276, which gives about 1 1/2 times as much error, which is still negligible.