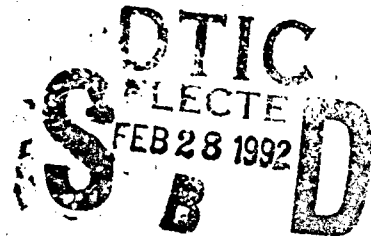


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# NAVAL POSTGRADUATE SCHOOL Monterey, California

AD-A246 505



## THESIS

ACCURACY ASSESSMENT FOR THE  
AUXILIARY TRACKING SYSTEM

by  
Michael P. Taylor

September, 1991

Thesis Advisor: Robert R. Read

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Accuracy Assessment for the  
Auxillary Tracking System

by

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Submitted in partial fulfillment  
of the requirements for the degree of

MASTER OF SCIENCE IN APPLIED SCIENCE

from the

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September 1991

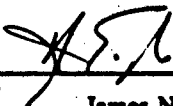
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### ABSTRACT

The Auxiliary Tracking System (ATS) is being developed to allow for an accurate underwater tracking capability that can be deployed anywhere in the world. A simulation was created to determine the impact upon the relative accuracy of the system due to a normally distributed noise. The simulation was used to look at the impact of range between targets and the depth spacing of the suspended transducers on the relative tracking accuracy.

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## I. INTRODUCTION

Within the last several years, the Navy has seen a tightening of the purse strings from congress, and as a result, must find more cost effective ways to perform the various missions that are still required. One area that has long been a concern is the limited number of underwater tracking ranges. Alternatives to the development of another fixed range must be considered because of the financial impact.

On the west coast, there are currently three areas where underwater tracking ranges are available. Washington, San Clemente, California, and Hawaii. With the limited number of sites and the other demands on range time for research and development, fleet ASW training opportunities are limited. Added to this is the fact that for many exercises, the units must transit to Hawaii simply because that is the only range available. The portable Auxiliary Tracking System (ATS) was conceived for these reasons.

The ATS has been designed as a truly portable underwater tracking range. This thesis will look at the theoretical tracking accuracy of the system currently under engineering development and testing at the Naval Undersea Warfare Engineering Station (NUWES).

## II. ATS CONCEPT

### A. GENERAL DESCRIPTION

With the recent improvements made in electronics and the Global Positioning Satellite System (GPSS), the dream of a portable tracking range now seems possible with current technology. The engineering development model consists of four underwater tracking buoys and a portable computer site. The buoys are deployed either from a ship or helicopter and are recoverable. For the four buoy system, deployment will be similar to that shown in Figure 1. The final system will consist of nine buoys to be deployed in various patterns based upon the needs of the system being tested.

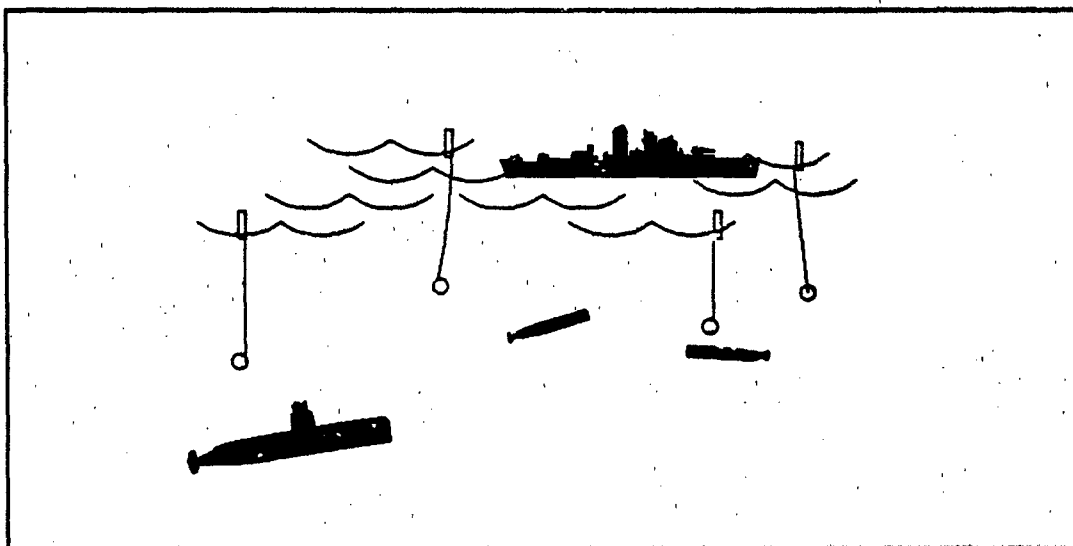


Figure 1. ATS Deployment Configuration

## **1. Buoy System**

The buoys used in the ATS will be free floating, self contained buoys. They will have a transducer suspended below at a predetermined depth (between 50 and 300 meters) used both for tracking the targets and locating the other units in the tracking range. The acoustic signal processor contained in each buoy will provide for the detection of the acoustic pings emitted by the other sources. The GPSS receiver in the buoy will provide the Latitude/Longitude and a very accurate time standard for the system. The on-board computer will control the GPSS receiver and acoustic signal processor, monitor the status of the buoy, perform a system up/down self test, time stamp and format the position data collected by the GPSS receiver and acoustic signal processor and send the data to the computer site via an RF data link.

## **2. Computer Site**

The control station for the ATS range will be the computer site, which will be positioned on a ship located off the range, or on land if the range is set up in coastal waters. The computer site will be contained in a portable van allowing transport anywhere in the world either by ship or by cargo aircraft. The only support needed will be AC power, as the computer site will be self contained. The computer site will contain the RF data link receivers, RF voice

communications equipment, a GPSS receiver, the range tracking computers and peripherals, and other equipment as needed.

#### B. SYSTEM OPERATION

The concept embodied by the ATS is a "sing-around" self calibrating tracking range. This means that the buoys will locate each other. Each buoy has an acoustic pinger on the floating buoy and a transducer suspended below. In a two minute cycle, each buoy pinger will transmit an acoustic signal followed by each suspended transducer also transmitting an acoustic signal. The acoustic processor within each buoy will control the pinging cycle; a coded pulse will be used to identify the signal. The transit time of the signal will be known as each buoy will transmit a pulse at a specific time, and the reception time of the signal will be sent to the computer site via the RF link from the buoy that received the signal. From this, the transit time of the signal is known, and the range between the source and receiver is calculated by using the Sound Velocity Profile of the water mass. The signal from the buoy pinger to the transducer suspended below is used to calculate the depth of each transducer. The transit times from transducer to transducer are then used to calculate the slant ranges when the depth of each transducer has been determined. From this data, a range grid is set up as shown in Figure 2. The location of each transducer and the range grid will be updated every two minutes by this method.

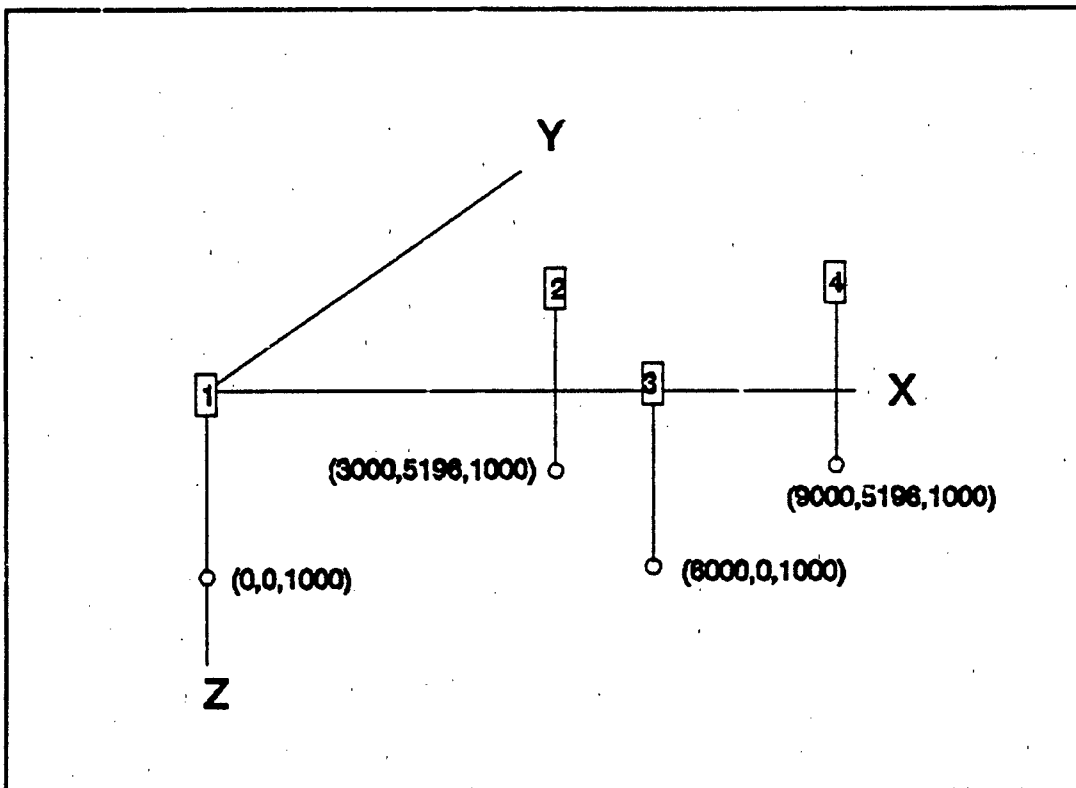


Figure 2. ATS Range Grid

With a relative grid established, the system now determines the positions of the targets on the range. The ATS has three distinct frequency bands to utilize, by incorporating a Shift Frequency, Shift Keying (SFSK) processor and transmitter. The high frequency will be used for the sing-around calibration already described, and the mid and low frequencies will be used to track the torpedo and the target. The SFSK processor and transmitter is similar to the system used on the Quinalt Shallow Water range at NUWES.

### III. SIMULATION DESCRIPTION

#### A. PROGRAM DESCRIPTION

A simulation program was written to determine the effects of a normal error on the transit times received at the computer site to investigate the accuracy of the ATS. The effects of shadow zones were not considered in the simulation due to the relatively short distances between any source and receiver pair. The simulation program has three main sections; solving for transit times, solving for positions, and collecting statistics.

##### 1. Simulation Inputs

The ATS simulation program requires three sets of inputs. The first set of inputs is the sound speed profile for the water mass. The program can accept up to 60 data points for the profile. The second set of inputs is the actual positions for the four buoys, the four suspended transducers and the two targets. The inputs are cartesian coordinate with buoy one being at the origin and buoy three establishing the X-Z plane. The third set of inputs is for the number of replications desired and the standard deviation of the noise for the systems. The standard deviation is a function of the distance between the source and receiver, and within the program is modeled by changing the travel times in

each of three groups; buoy to transducer, transducer to transducer, and target to transducer.

## 2. Solving for Times

Once the inputs have been entered, the program solves for the actual transit time between each source and receiver pair. This is done by taking the slant range between each source and receiver (Equation 3.1) and dividing by the

$$\text{Range} = \sqrt{(X_s - X_r)^2 + (Y_s - Y_r)^2 + (Z_s - Z_r)^2} \quad (3.1)$$

effective sound speed between source and receiver. The effective sound speed is calculated by solving for the travel time for a vertically propagating wave in each layer. The travel times are summed between the source and receiver depths and the difference in depths is divided by the travel time to yield the effective sound speed between the source and receiver. The derivation of the equation is shown below and starts with the definition of the travel time (Equation 3.2).

$$t = \int_{z_s}^{z_r} \frac{ds}{c(z)} \quad (3.2)$$

The ray path within a constant gradient is defined as the arc of a circle of radius equal to  $\sigma$  (Equation 3.3 and 3.4)

[Ref 1:p. 402].

$$ds = \sigma d\theta \quad (3.3)$$

$$\sigma = \frac{c(z)}{g \cos \theta} \quad (3.4)$$

Substitution of Equation 3.4 into Equation 3.2 yields Equation 3.5 and 3.6. The solution of the integral is shown in Equation 3.7

$$t = \int_0^{\theta} \frac{d\theta}{g \cos \theta} \quad (3.5)$$

$$t = \frac{1}{g} \int_0^{\theta} \sec(\theta) d\theta \quad (3.6)$$

$$t = \frac{1}{g} [\ln |\sec(\theta) + \tan(\theta)|] \quad (3.7)$$

Separation of the terms yield Equation 3.8. Using snell's law [Ref 1: p. 401], as shown in Equation 3.9, and making the assumption that the sine terms cancel for a vertically propagating wave, Equation 3.8 can be reduced to Equation 3.10.

$$t = \frac{1}{g} \ln \left| \frac{1 + \sin \theta}{\cos \theta} \frac{\cos \theta_0}{1 + \sin \theta_0} \right| \quad (3.8)$$

$$\frac{\cos \theta_0}{\cos \theta} = \frac{c(z_0)}{c(z)} \quad (3.9)$$

$$t = \frac{1}{g} \ln \frac{c(z_2)}{c(z_1)} \quad (3.10)$$

By summing the travel times within each layer, the propagation time is found. If within a layer, the gradient is equal to zero, the program takes the vertical distance within the layer and divides by the sound speed within the layer to determine the time  $t$ . The effective sound speed is now found (Equation 3.11).

$$effspd = \frac{Z_2 - Z_1}{t} \quad (3.11)$$

Knowing the slant range and the effective sound speed between each source and receiver pair, the transit times for all pairs are determined (Equation 3.12).

$$Time = \frac{Range}{effspd} \quad (3.12)$$

### 3. Adding Noise

When all of the transit times have been calculated and stored, the program begins the iteration cycle. The first step is the addition of the noise value to the transit times. This is done by taking a standard normal random variable and multiplying it by the transit time and the percentage value for the standard deviation. This results in a normal random variable with mean equal to zero and standard deviation equal to the given percentage of the transit time. This method was chosen because the transducer to transducer ranges and times

are typically 5 times greater than the pinger to suspended transducer times, and the error should be a function of range.

#### 4. Solving for Transducer Locations

After the noise has been added to each of the transit times, the location of each transducer is calculated. The depth of each transducer is found first using the transit time from the buoy pinger to the transducer suspended below (i.e. buoy pinger one to transducer one). From this transit time and using the length of the cable as a starting point, the depth is determined through an iterative process by calculating the effective sound velocity between the pinger and the estimated depth of the transducer. The solution is then found by multiplying the transit time by the effective sound velocity. The resulting depth is then compared with the estimated depth, and when the difference between the two values is less than one foot, the program continues, otherwise the resulting depth is used for the estimated depth and the calculation is repeated. Once the four transducer depths are established, the range coordinate system is established using transducer one as the origin of the X-Y grid and transducer three as the intersection with the horizontal axis (X-axis). There are two transit times for each range calculation made (transit time from transducer one to three and from transducer three to one), and the times are averaged. The slant range (SR) is then found by calculating the effective sound velocity

between the two depths and multiplying by the average transit time between the two transducers. The horizontal distance (H) is calculated using Equation 3.13. The position of transducer

$$H = \sqrt{(SR)^2 - (Z_1 - Z_2)^2} \quad (3.13)$$

two is found by using the horizontal ranges from transducers one and three and using the GPSS position of buoy two to determine which of two unique solutions is correct (the intersection of two circles). Transducer four is then located the same way using the positions and ranges from transducers two and three.

#### 5. Solving for Target Locations

With the range coordinate system established and the location of all transducers found, we are positioned to calculate the location of the two targets. It is assumed that all four transducers receive the signal from each target. The location of the target is then calculated through a least squares method similar to one used by Larry Anderson at NUWES. The detailed procedures for the algorithm are presented below.

Given the location of each transducer as  $(X_i, Y_i, Z_i)$  and the solution range between transducer  $i$  and the target ( $R_{\text{sol}}$ ) from the transit time, the location of the Target  $(X_T, Y_T, Z_T)$  is calculated.  $R_m$  is the measured slant range between target and transducer  $i$ , and  $R_c$  is the calculated slant range between target and transducer  $i$  as given by Equation 3.14. The

$$R_i = \sqrt{(X_T - X_i)^2 + (Y_T - Y_i)^2 + (Z_T - Z_i)^2} \quad (3.14)$$

location of the target is then calculated with respect to minimizing the Sum of Squares of errors (SSE), where the SSE is defined by Equation 3.15. The calculated slant ranges ( $R_i$ )

$$SSE = \sum_{i=1}^4 (R_i - R_{mi})^2 \quad (3.15)$$

are linearized around the trial value ( $X_{T_0}$ ,  $Y_{T_0}$ ,  $Z_{T_0}$ ), shown in Equation 3.16, where  $|_o$  means evaluated at point "o". The

$$R_i - R_{i_0} + \left. \frac{\partial R_i}{\partial X_T} \right|_o (X_T - X_{T_0}) + \left. \frac{\partial R_i}{\partial Y_T} \right|_o (Y_T - Y_{T_0}) + \left. \frac{\partial R_i}{\partial Z_T} \right|_o (Z_T - Z_{T_0}) \quad (3.16)$$

partial derivatives are listed in Equations 3.17 through 3.19.

$$\left. \frac{\partial R_i}{\partial X_T} \right|_o = \frac{X_{T_0} - X_i}{R_{i_0}} \quad (3.17)$$

$$\left. \frac{\partial R_i}{\partial Y_T} \right|_o = \frac{Y_{T_0} - Y_i}{R_{i_0}} \quad (3.18)$$

$$\left. \frac{\partial R_i}{\partial Z_T} \right|_o = \frac{Z_{T_0} - Z_i}{R_{i_0}} \quad (3.19)$$

The linearized model is substituted into Equation 3.15 and the SSE is minimized with respect to ( $X_T$ ,  $Y_T$ ,  $Z_T$ ). The resulting normal equations are put in matrix form as shown in Equation

3.20. The individual matrices are shown in Equations 3.21 through 3.23. Equation 3.20 is solved for the correction matrix (Equation 3.22) which when added to  $(X_{T_0}, Y_{T_0}, Z_{T_0})$

$$AX=B \quad (3.20)$$

$$A = \begin{vmatrix} \sum \left. \frac{\partial R_i}{\partial X_T} \right|_0^2 & \sum \left. \frac{\partial R_i}{\partial Y_T} \right|_0 \left. \frac{\partial R_i}{\partial X_T} \right|_0 & \sum \left. \frac{\partial R_i}{\partial Z_T} \right|_0 \left. \frac{\partial R_i}{\partial X_T} \right|_0 \\ \sum \left. \frac{\partial R_i}{\partial X_T} \right|_0 \left. \frac{\partial R_i}{\partial Y_T} \right|_0 & \sum \left. \frac{\partial R_i}{\partial Y_T} \right|_0^2 & \sum \left. \frac{\partial R_i}{\partial Z_T} \right|_0 \left. \frac{\partial R_i}{\partial Y_T} \right|_0 \\ \sum \left. \frac{\partial R_i}{\partial X_T} \right|_0 \left. \frac{\partial R_i}{\partial Z_T} \right|_0 & \sum \left. \frac{\partial R_i}{\partial Y_T} \right|_0 \left. \frac{\partial R_i}{\partial Z_T} \right|_0 & \sum \left. \frac{\partial R_i}{\partial Z_T} \right|_0^2 \end{vmatrix} \quad (3.21)$$

$$X = \begin{vmatrix} X_T - X_{T_0} \\ Y_T - Y_{T_0} \\ Z_T - Z_{T_0} \end{vmatrix} \quad (3.22)$$

$$B = \begin{vmatrix} \sum (R_{mi} - R_{i0}) \left. \frac{\partial R_i}{\partial X_T} \right|_0 \\ \sum (R_{mi} - R_{i0}) \left. \frac{\partial R_i}{\partial Y_T} \right|_0 \\ \sum (R_{mi} - R_{i0}) \left. \frac{\partial R_i}{\partial Z_T} \right|_0 \end{vmatrix} \quad (3.23)$$

yields the improved target position  $(X_T, Y_T, Z_T)$ . If the sum of the squares of the corrections is less than some value epsilon, Equation 3.24, the iteration is stopped. Otherwise,

$$(X_T - X_{T_0})^2 + (Y_T - Y_{T_0})^2 + (Z_T - Z_{T_0})^2 < \epsilon \quad (3.24)$$

the target position  $(X_T, Y_T, Z_T)$  is used for the next iteration in place of  $(X_{T_0}, Y_{T_0}, Z_{T_0})$  and the procedure is repeated until 50 iterations have been completed.

#### 6. Collecting Statistics

When the positions of the targets have been solved for, the errors are calculated. The distance between the actual and solution location of each target (Equation 3.25), and the distance in the relative position of the targets with respect to each other (Equation 3.26) are calculated.

$$TE_i = \sqrt{(X_{oi} - X_{si})^2 + (Y_{oi} - Y_{si})^2 + (Z_{oi} - Z_{si})^2} \quad (3.25)$$

$$RE = \sqrt{((X_{o1} - X_{o2}) - (X_{s1} - X_{s2}))^2 + \dots} \quad (3.26)$$

$X_{oi}$  is the X-value for the true position of the  $i$ th target,  $X_{si}$  is the X-value for the solved position of the  $i$ th target,  $TE_i$  is the True error for the  $i$ th target, and RE is the relative error between the two targets. The values for  $TE_i$  and RE are summed over the iteration loop and the programs final output is the mean and standard deviation of the true position error for each target and the relative position error between the two targets.

#### B. SIMULATIONS CONDUCTED

Three factors are considered as to the influence of the relative accuracy: Magnitude of the noise in the

measurements, the proximity of target one to target two, and whether the transducers are at equal or staggered depths.

### 1. Noise Values

Noise values are entered into the simulation by the standard deviation being a percentage of the true value. Values examined range between 0.1 and 1.0 percent.

### 2. Target Locations

The simulations were conducted for targets at close range (100 ft separation) and long range (3000 ft separation) to investigate the effects of target separation on the relative accuracy.

### 3. Transducer Depths

Some discussion has taken place as to the effects of staggering the transducer depths or having them all at an equal depth with the thought being would accuracy be gained by having the suspended transducers staggered at varying depths. Would this allow for better target resolution given the four slant ranges from the target to the transducers? Simulations were also conducted to draw a conclusion on the selection of transducers depths; equal depths or staggered depths with intervals of 100 feet.

#### IV. DATA ANALYSIS

Each of the four following cases were run using the simulation program with the noise values ranging from 0 to 1 percent. The performance goal for the ATS is 20 yards relative accuracy. The specifics of the four cases are as follows:

1. Case One: Transducers at equal depth (1000 feet) and targets at close range (100 feet).
2. Case Two: Transducers at equal depth and targets at long range (3000 feet).
3. Case Three: Transducers at staggered depths (100 foot intervals) and targets at close range.
4. Case Four: Transducers at staggered depths and targets at long range.

The results for the four cases are shown in Figure 3. The limit for the noise varies from 0.3 percent for cases two and four (targets at long range) to 0.4 percent for cases one and three (targets at close range).

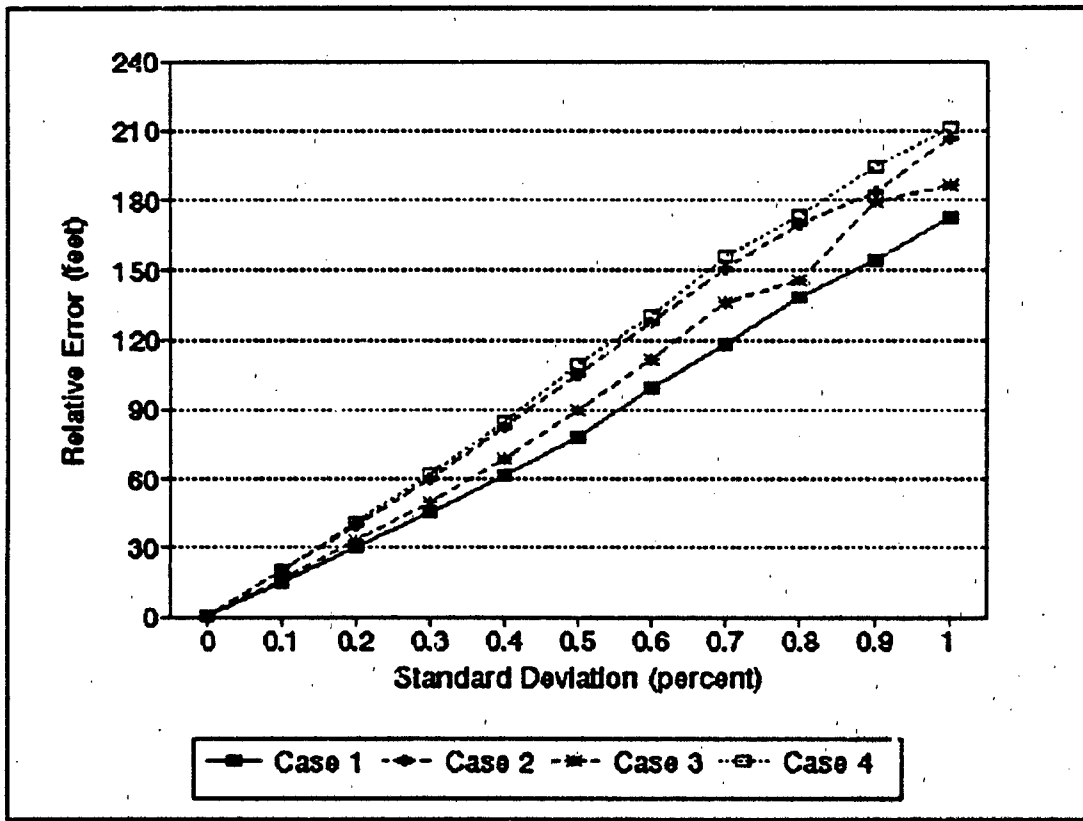


Figure 3. Relative Error Plot

## V. CONCLUSIONS AND RECOMMENDATIONS

### A. CONCLUSIONS

The results from the simulation show that the system can not handle a lot of noise as currently designed. The staggering of the transducer depths did not appear to have an effect on the accuracy of the system. All four cases were relatively close for noise value where the relative accuracy exceeded 20 yards.

### B. RECOMMENDATIONS

The accuracy assessment for the ATS is a very complex problem. This study has only focused on a few areas and a complete assessment of the system will require further study. From the initial results on the engineering development model, the outlook is very promising for the Navy to receive substantial benefits from its continued funding. Analysis of the data from the prototype buoys should reveal the magnitude of the noise, and the expected accuracy can then be determined. An additional area that should also be considered is to use telemetry data from the targets in the tracking problem. This could be utilized to provide the depth of the target and the velocity. By incorporating a Kalman Filter into the algorithm, it may be possible to reduce the impact

from a bad ping cycle. This would also necessitate looking at the accuracy of the depth sensors currently available.

The Auxiliary Tracking System should continue to be developed. Potential benefits for the Navy warrant the investment now, as current ranges are taxed to keep up with the demands placed upon them by the many users. As new weapons systems are developed, the ATS will allow more realistic operational testing to be conducted by allowing the weapons systems to be evaluated in various ocean types.

## APPENDIX A

```

CC ATSSIM.FOR
CC SIMULATION PROGRAM TO EVALUATE AUXILLARY TRACKING SYSTEM
CC ABSOLUTE AND RELATIVE ACCURACY ASSESSMENTS BASED UPON A
CC RANDOM NOISE WITH A GIVEN MEAN AND VARIANCE.
CC
REAL*8 SEED
REAL*4 XBUOY, YBUOY, ZBUOY, XPHONE, YPHONE, ZPHONE, XTGT, YTGT, ZTGT,
+ MEAN1, VAR1, MEAN2, VAR2, MEANR, VARR, SRANGE, RANGE, NOISE,
+ TTIME1, HTIME1, BTIME1, TTIME, HTIME, BTIME, A, B
INTEGER*4 BUOYS, MAXSSV, NCOUNT
DIMENSION XBUOY(4), YBUOY(4), ZBUOY(4), XPHONE(4), YPHONE(4),
+ ZPHONE(4), SRANGE(6), BTIME1(4,4), HTIME1(4,4),
+ PHONEX(4), PHONEY(4), PHONEZ(4), DEPTH(40), SSPVEL(40),
+ XTGT(2), YTGT(2), ZTGT(2), TGTX(2), TGTY(2), TTIME1(2,4),
+ TGTZ(2), BTIME(4,4), HTIME(4,4), TTIME(2,4),
+ TERROR(2), TESQ(2), TESUM(2), TRANGE(2,4)
MAXSSV = 40
BUOYS = 4
ZCABLE = 1000.0
CALL INPUT (NCOUNT, BTN, STN, TTN, SEED)
CALL PROFILE (MAXSSV, NUMSSV, DEPTH, SSPVEL)
CALL POSITS (XBUOY, YBUOY, ZBUOY, XPHONE, YPHONE, ZPHONE,
+ XTGT, YTGT, ZTGT)
CC CALCULATE TRANSIT TIMES FOR BUOYS
DO 20 I = 1, 4
DO 10 J = 1, 4
RANGE = SQRT((XBUOY(I)-XPHONE(J))**2+(YBUOY(I)-YPHONE(J))**2 +
+ (ZBUOY(I) - ZPHONE(J))**2)
CALL HMVELOC(ZBUOY(I), ZPHONE(J), NUMSSV, DEPTH, SSPVEL, HMVEL)
BTIME(I,J) = RANGE/HMVEL
10 CONTINUE
20 CONTINUE
DO 50 I = 1, 4
DO 40 J = 1, 4
IF (I .EQ. J) GOTO 30
RANGE = SQRT((XPHONE(I)-XPHONE(J))**2+
+ (YPHONE(I)-YPHONE(J))**2+(ZPHONE(I)-ZPHONE(J))**2)
CALL HMVELOC(ZPHONE(I), ZPHONE(J), NUMSSV, DEPTH, SSPVEL, HMVEL)
HTIME(I,J) = RANGE/HMVEL
30 CONTINUE
40 CONTINUE
50 CONTINUE
DO 70 I = 1, 2
DO 60 J = 1, 4
RANGE = SQRT((XTGT(I)-XPHONE(J))**2+(YTGT(I)-YPHONE(J))**2+
+ (ZTGT(I) - ZPHONE(J))**2)
CALL HMVELOC(ZTGT(I), ZPHONE(J), NUMSSV, DEPTH, SSPVEL, HMVEL)
TTIME(I,J) = RANGE/HMVEL
60 CONTINUE
70 CONTINUE

```

```

DO 900 KOUNT=1, NCOUNT
79 CONTINUE
CC ADD NOISE
DO 71 I = 1, 2
  J = I + 2
  CALL URAND(A,B,SEED)
  BTIME1(I,I) = ETIME(I,I) + (A*BTN*BTIME(I,I))
  BTIME1(J,J) = BTIME(J,J) + (B*BTN*BTIME(J,J))
71 CONTINUE
DO 73 I = 1, 4
  DO 72 J = 1, 2
    K = J + 2
    CALL URAND(A,B,SEED)
    HTIME1(I,J) = HTIME(I,J) + (A*STN*HTIME(I,J))
    HTIME1(I,K) = HTIME(I,K) + (B*STN*HTIME(I,K))
72 CONTINUE
73 CONTINUE
DO 75 J = 1, 4
  CALL URAND(A,B,SEED)
  TTIME1(1,J) = TTIME(1,J) + (A*TTN*TTIME(1,J))
  TTIME1(2,J) = TTIME(2,J) + (B*BTN*TTIME(2,J))
75 CONTINUE
CC CALC BUOY POSITS
DO 80 I = 1, 4
  PHONEX(I) = XBUOY(I)
  PHONEY(I) = YBUOY(I)
80 CONTINUE
  CALL HYDEPTH (ZCABLE, ZBUOY, NUMSSV, DEPTH,
+ SSPVEL, HMVEL, BTIME1, PHONEZ)
  CALL RPHONE (SRANGE, HTIME1, PHONEZ, NUMSSV, DEPTH, SSPVEL, HMVEL)
  CALL TWOD (SRANGE, PHONEX, PHONEY, PHONEZ, YBUOY)
CC CALC TARGET POSITS
DO 100 J = 1, 2
  TGTZ(J) = 400
  TGTX(J) = 2000
  TGTY(J) = 2000
  CALL TGTRANGE (TTIME1, TGTZ, ZPHONE, NUMSSV, DEPTH, SSPVEL, HMVEL,
+ TRANGE, J)
  CALL THREED (J, TGTX, TGTY, TGTZ, PHONEX, PHONEY, PHONEZ, TRANGE)
100 CONTINUE
CC CALC TRUE ERRORS
ERFIX = 0.0
DO 150 J = 1,2
  TERROR(J) = SQRT((XTGT(J)-TGTX(J))**2+(YTGT(J)-TGTY(J))**2+
+ (ZTGT(J)-TGTZ(J))**2)
  IF (TERROR(J) .GT. 1000.0) ERFIX = 1.0
150 CONTINUE
  IF (ERFIX .EQ. 1) THEN
    GOTO 79
  ELSE
    DO 200 J =1,2
      TESQ(J) = TESQ(J) + TERROR(J)**2
      TESUM(J) = TESUM(J) + TERROR(J)
200 CONTINUE
CC CALC RELATIVE ERRORS
  RERROR = SQRT((XTGT(1)-TGTX(1)-XTGT(2)+TGTX(2))**2+
+ (YTGT(1)-TGTY(1)-YTGT(2)+TGTY(2))**2+
+ (ZTGT(1)-TGTZ(1)-ZTGT(2)+TGTZ(2))**2)
  RESQ = RESQ + RERROR**2
  RESUM = RESUM + RERROR
ENDIF

```

```

900 CONTINUE
CC  CALC STATS ON TRUE ERRORS
CC  TGT1 RESULTS
    MEAN1 = TESUM(1)/NCOUNT
    VAR1 = SQRT(ABS(NCOUNT*TESQ(1)-TESUM(1)**2))/(NCOUNT*(NCOUNT-1))
CC  TGT2 RESULTS
    MEAN2 = TESUM(2)/NCOUNT
    VAR2 = SQRT(ABS(NCOUNT*TESQ(2)-TESUM(2)**2))/(NCOUNT*(NCOUNT-1))
CC  CALC STATS ON RELATIVE ERRORS
CC  RELATIVE RESULTS
    MEANR = RESUM/NCOUNT
    VARR = SQRT(ABS(NCOUNT*RESQ-RESUM**2))/(NCOUNT*(NCOUNT-1))
    CALL OUTPUT (MEAN1, VAR1, MEAN2, VAR2, MEANR, VARR,
+              BTN,STN,TTN,NCOUNT)
    END
*****
*   INPUT SUBROUTINE TO ENTER IN SIMULATION VALUES   *
*****
SUBROUTINE INPUT (NCOUNT, BTN, STN, TTN, SEED)
REAL*8 SEED
OPEN (UNIT = 1, FILE = 'INPUT.DAT')
READ (1,*) NCOUNT, BTN, STN, TTN, SEED
CLOSE (UNIT = 1, STATUS = 'KEEP')
RETURN
END

*****
*   PROFILE SUBROUTINE TO ENTER SOUND VELOCITY PROFILE *
*****
SUBROUTINE PROFILE (MAXSSV, NUMSSV, DEPTH, SSPVEL)
REAL*4 DEPTH, SSPVEL
INTEGER*4 MAXSSV, NUMSSV
DIMENSION DEPTH(40), SSPVEL(40)
OPEN (UNIT = 1, FILE = 'SSPROF.DAT')
READ (1,*) NUMSSV
IF (NUMSSV .GT. MAXSSV) THEN
    WRITE(*,*) ' MAXIMUM NUMBER OF SSP DATA POINTS EXCEEDED '
ENDIF
DO 10 I = 1, NUMSSV
    READ (1,*) DEPTH(I), SSPVEL(I)
10 CONTINUE
CLOSE (UNIT = 1, STATUS='KEEP')
RETURN
END

*****
*   POSITS SUBROUTINE TO ENTER BUOY, TRANSDUCER AND TARGET *
*****
SUBROUTINE POSITS (XBUOY, YBUOY, ZBUOY, XPHONE, YPHONE, ZPHONE, XTGT,
+                YTGT, ZTGT)
REAL*4 XBUOY, YBUOY, ZBUOY, XPHONE, YPHONE, ZPHONE
DIMENSION XBUOY(4), YBUOY(4), ZBUOY(4), XPHONE(4), YPHONE(4),
+          ZPHONE(4), XTGT(2), YTGT(2), ZTGT(2)
OPEN (UNIT = 2, FILE = 'BUOYLOC.DAT')
DO 10 I = 1, 4
    READ(2,*) XBUOY(I), YBUOY(I), ZBUOY(I), XPHONE(I), YPHONE(I),
+          ZPHONE(I)
10 CONTINUE
OPEN (UNIT = 1, FILE = 'TARGET.DAT')
DO 20 J = 1, 2

```

```

READ(1,*) XTGT(J), YTGT(J), ZTGT(J)
20 CONTINUE
RETURN
END

*****
*   HMVELOC SUBROUTINE TO CALCULATE MEAN SOUND VELOCITY   *
*****
SUBROUTINE HMVELOC (ZPING, ZRCVR, NUMSSV, DEPTH, SSPVEL, HMVEL)
REAL*4 ZPING, ZRCVR, DEPTH, SSPVEL, HMVEL, GRADNT, HMV1, HMV2, T
INTEGER*4 I, J, K, INIT, FINAL, NUMSSV
DIMENSION DEPTH(NUMSSV), SSPVEL(NUMSSV)
C ORDER THE DEPTH OF THE RECEIVER AND HYDROPHONE SO THAT THE
C RECEIVER IS THE DEEPER OF THE TWO DEPTHS.
T = 0.0
INTE = 0
IF (ZPING .GT. ZRCVR) THEN
    TEMP = ZPING
    ZPING = ZRCVR
    ZRCVR = TEMP
    INTE = 1
ENDIF
C INTERPOLATE THE SOUND SPEED AT THE PINGER DEPTH
DO 1 I = 2, NUMSSV
    IF (ZPING .GT. DEPTH(I)) GOTO 1
    GRADNT = (SSPVEL(I) - SSPVEL(I-1))/(DEPTH(I) - DEPTH(I-1))
    HMV1 = SSPVEL(I-1) + GRADNT*(ZPING-DEPTH(I-1))
    INIT= I
    GO TO 2
1 CONTINUE
C INTERPOLATE THE SOUND SPEED AT THE HYDROPHONE DEPTH
2 DO 3 J = 2, NUMSSV
    IF (ZRCVR .GT. DEPTH(J)) GOTO 3
    GRADNT = (SSPVEL(J) - SSPVEL(J-1))/(DEPTH(J) - DEPTH(J-1))
    HMV2 = SSPVEL(J-1) + GRADNT*(ZRCVR-DEPTH(J-1))
    FINAL = J-1
    GO TO 4
3 CONTINUE
C CALCULATE THE HARMONIC SOUND SPEED BETWEEN THE PINGER AND THE
C HYDROPHONE
4 IF (FINAL .LT. INIT) THEN
C
C SOURCE AND RECEIVER IN SAME GRADIENT
C TAKE AVERAGE OF TWO SOUND SPEEDS OF SOURCE AND RECEIVER
C
    GRADNT = (HMV2 - HMV1) / (ZRCVR - ZPING)
    IF (GRADNT .NE. 0.0) T = LOG(HMV2/HMV1)/GRADNT
    IF (GRADNT .EQ. 0.0) T = (ZRCVR - ZPING)/HMV2
    HMVEL = T/(ZRCVR-ZPING)
ELSEIF (FINAL .EQ. INIT) THEN
C
C SOURCE AND RECEIVER SPERATED BY ONE DEPTH GRADIENT
C
    GRADNT = (SSPVEL(INIT) - HMV1)/(DEPTH(INIT) - ZPING)
    IF (GRADNT .NE. 0.0) T = LOG(SSPVEL(INIT)/HMV1)/GRADNT
    IF (GRADNT .EQ. 0.0) T = (DEPTH(INIT)-ZPING)/SSPVEL(INIT)
    GRADNT = (HMV2-SSPVEL(FINAL))/(ZRCVR - DEPTH(FINAL))
    IF (GRADNT .NE. 0.0) T = T + LOG(HMV2/SSPVEL(FINAL))/GRADNT
    IF (GRADNT .EQ. 0.0) T = T + (ZRCVR-DEPTH(FINAL))/HMV2
    HMVEL = ABS((ZRCVR-ZPING)/T)
ELSE

```

C  
C  
C

SOURCE AND RECEIVER SEPERATED BY MORE THAN ONE DEPTH

```
GRADNT = (SSPVEL(INIT) - HMV1)/(DEPTH(INIT) - ZPING)
IF (GRADNT .NE. 0.0) T = LOG(SSPVEL(INIT)/HMV1)/GRADNT
IF (GRADNT .EQ. 0.0) T = (DEPTH(INIT)-ZPING)/SSPVEL(INIT)
DO 5 K= INIT + 1, FINAL
  GRADNT = (SSPVEL(K)-SSPVEL(K-1))/(DEPTH(K)-DEPTH(K-1))
  IF (GRADNT .NE. 0.0) T = T+LOG(SSPVEL(K)/SSPVEL(K-1))/GRADNT
  IF (GRADNT .EQ. 0.0) T = T+(DEPTH(K)-DEPTH(K-1))/SSPVEL(K)
5 CONTINUE
GRADNT = (HMV2-SSPVEL(FINAL))/(ZRCVR - DEPTH(FINAL))
IF (GRADNT .NE. 0.0) T = T + LOG(HMV2/SSPVEL(FINAL))/GRADNT
IF (GRADNT .EQ. 0.0) T = T + (ZRCVR-DEPTH(FINAL))/HMV2
HMVEL = ABS((ZRCVR-ZPING)/T)
ENDIF
IF (INTE .EQ. 1) THEN
  TEMP = ZPING
  ZPING = ZRCVR
  ZRCVR = TEMP
ENDIF
RETURN
END
```

\*\*\*\*\*  
\* HYDEPTH SUBROUTINE TO CALCULATE TRANSDUCER DEPTHS \*  
\*\*\*\*\*

```
SUBROUTINE HYDEPTH (ZCABLE, ZBUOY, NUMSSV, DEPTH,
+ SSPVEL, HMVEL, BTIME, PHONEZ)
CC SUBROUTINE TO CALCULATE THE DEPTH OF THE HYDROPHONE BELOW THE
CC BUOY.
REAL*4 ZCABLE, ZBUOY, DEPTH, SSPVEL, HMVEL, BTIME, ZOLD, PHONEZ
INTEGER*4 NUMSSV
DIMENSION DEPTH(40), SSPVEL(40), PHONEZ(4), BTIME(4,4), ZBUOY(4)
DO 5 I = 1, 4
  ZB = ZBUOY(I)
  ZOLD = ZCABLE
  DO 3 KOUNT = 1, 10
    CALL HMVELOC(ZB, ZOLD, NUMSSV, DEPTH, SSPVEL, HMVEL)
    ZNEW = HMVEL * BTIME(I,I) + ZB
    IF (ABS(ZNEW-ZOLD) .LT. 1.0) GO TO 4
    ZOLD = ZNEW
  3 CONTINUE
  4 PHONEZ(I) = ZNEW
  5 CONTINUE
RETURN
END
```

\*\*\*\*\*  
\* RPHONE SUBROUTINE TO CALCULATE RANGES BETWEEN TRANSDUCERS\*  
\*\*\*\*\*  
SUBROUTINE RPHONE (RANGE, HTIME, PHONEZ, NUMSSV, DEPTH, SSPVEL,  
+ HMVEL)

```
CC RANGE(1) = PHONE 1 TO PHONE 2
CC RANGE(2) = PHONE 3 TO PHONE 2
CC RANGE(3) = PHONE 1 TO PHONE 4
CC RANGE(4) = PHONE 3 TO PHONE 4
CC RANGE(5) = PHONE 2 TO PHONE 4
```

```

CC  RANGE(6) = PHONE 1 TO PHONE 3
    REAL*4 RANGE, HTIME, PHONEZ, DEPTH, SSPVEL, HMVEL, T
    INTEGER NUMSSV
    DIMENSION RANGE(6), HTIME(4,4), PHONEZ(4), DEPTH(40),
+     SSPVEL(40)
    DO 1 I = 1, 4
1  CONTINUE
    T = (HTIME(2,1) - HTIME(1,2)/3.0)*1.5
    CALL HMVELOC(PHONEZ(1), PHONEZ(2), NUMSSV, DEPTH, SSPVEL,
+     HMVEL)
    RANGE(1) = T * HMVEL
    T = 0.5*HTIME(2,3) + 0.5*HTIME(3,2)
    CALL HMVELOC(PHONEZ(2), PHONEZ(3), NUMSSV, DEPTH, SSPVEL,
+     HMVEL)
    RANGE(2) = T * HMVEL
    T = 0.5*HTIME(1,4) + 0.5*HTIME(4,1)
    CALL HMVELOC(PHONEZ(1), PHONEZ(4), NUMSSV, DEPTH, SSPVEL,
+     HMVEL)
    RANGE(3) = T * HMVEL
    T = (HTIME(3,4) - HTIME(4,3)/3.0)*1.5
    CALL HMVELOC(PHONEZ(3), PHONEZ(4), NUMSSV, DEPTH, SSPVEL,
+     HMVEL)
    RANGE(4) = T * HMVEL
    T = 0.75*HTIME(2,4) + 0.25*HTIME(4,2)
    CALL HMVELOC(PHONEZ(2), PHONEZ(4), NUMSSV, DEPTH, SSPVEL,
+     HMVEL)
    RANGE(5) = T * HMVEL
    T = 0.25*HTIME(1,3) + 0.75*HTIME(3,1)
    CALL HMVELOC(PHONEZ(1), PHONEZ(3), NUMSSV, DEPTH, SSPVEL,
+     HMVEL)
    RANGE(6) = T * HMVEL
    RETURN
    END

```

```

*****
*   TWOD SUBROUTINE TO CALCULATE TRANSDUCER POSITIONS   *
*****
SUBROUTINE TWOD (RANGE, XP, YP, ZP, BUOYY)
REAL*4 RANGE, BUOYY
REAL*4 XP, YP, ZP, DX, DY, ANS, XSQR1, XSQR3,
+ YSQR1, YSQR3, RSQR1, RSQR3, RHS, DISCRIM, THETA, PHI
DIMENSION BUOYY(4), XP(4), YP(4), ZP(4), RANGE(6),
+ ANS(2,2)
XP(3)=SQRT(RANGE(6)**2 - (ZP(1)-ZP(3))**2)
YP(3)=0.0
DX=XP(1)-XP(3)
DY=YP(1)-YP(3)
RSQR1=RANGE(1)**2-(ZP(1)-ZP(2))**2
RSQR3=RANGE(2)**2-(ZP(2)-ZP(3))**2
XSQR1=XP(1)**2
XSQR3=XP(3)**2
YSQR1=YP(1)**2
YSQR3=YP(3)**2
RHS = (XSQR1 + YSQR1 - XSQR3 - YSQR3 +RSQR3 - RSQR1)*0.5
IF (DY .EQ. 0.0) THEN
    THETA = RHS/DX
    A = 1
    B = -2 * YP(1)
    C = (THETA)**2 + XSQR1 + YSQR1 - (2 * THETA * XP(1)) - RSQR1
    DISCRIM = B**2 - (4 * A * C)

```

```

ANS(1,2) = (-B + SQRT(ABS(DISCIM)))/(2*A)
ANS(2,2) = (-B/A - ANS(1,2))
ANS(1,1) = THETA
ANS(2,1) = THETA
ELSE
THETA = RHS/DY
PHI = DX/DY
A = 1.0 + PHI**2
B = 2*(YP(1)*PHI-THETA*PHI-XP(1))
C = XSQR1 + (THETA)**2 + YSQR1 - RSQR1 - 2.0 * THETA * YP(1)
DISCRIM = B**2 - (4 * A * C)
ANS(1,1) = (-B + SQRT(DISCIM)))/(2*A)
ANS(2,1) = (-B/A - ANS(1,1))
ANS(1,2) = THETA - PHI*ANS(1,1)
ANS(2,2) = THETA - PHI*ANS(2,1)
ENDIF
IF (ABS(ANS(1,2) - BUOYY(2)) .LT. 1000) THEN
XP(2) = ANS(1,1)
YP(2) = ANS(1,2)
ELSE
XP(2) = ANS(2,1)
YP(2) = ANS(2,2)
ENDIF
DX=XP(2)-XP(3)
DY=YP(2)-YP(3)
RSQR1=RANGE(5)**2-(ZP(2)-ZP(4))**2
RSQR3=RANGE(4)**2-(ZP(3)-ZP(4))**2
XSQR1=XP(2)**2
XSQR3=XP(3)**2
YSQR1=YP(2)**2
YSQR3=YP(3)**2
RHS = (XSQR1 + YSQR1 - XSQR3 - YSQR3 +RSQR3 - RSQR1)*0.5
IF (DY .EQ. 0.0) THEN
THETA = RHS/DX
A = 1
B = -2 * YP(2)
C = (THETA)**2 + XSQR1 + YSQR1 - (2 * THETA * XP(2)) - RSQR1
DISCRIM = B**2 - (4 * A * C)
ANS(1,2) = (-B + SQRT(DISCIM)))/(2*A)
ANS(2,2) = (-B/A - ANS(1,2))
ANS(1,1) = THETA
ANS(2,1) = THETA
ELSE
THETA = RHS/DY
PHI = DX/DY
A = 1.0 + PHI**2
B = 2*(YP(2)*PHI-THETA*PHI-XP(2))
C = XSQR1 + (THETA)**2 + YSQR1 - RSQR1 - 2.0 * THETA * YP(2)
DISCRIM = B**2 - (4 * A * C)
ANS(1,1) = (-B + SQRT(ABS(DISCIM)))/(2*A)
ANS(2,1) = (-B/A - ANS(1,1))
ANS(1,2) = THETA - PHI*ANS(1,1)
ANS(2,2) = THETA - PHI*ANS(2,1)
ENDIF
IF (ABS(ANS(1,2) - BUOYY(4)) .LT. 1000) THEN
XP(4) = ANS(1,1)
YP(4) = ANS(1,2)
ELSE

```

```

      XP(4) = ANS(2,1)
      YP(4) = ANS(2,2)
    ENDIF
    RETURN
  END

```

```

*****
*   TGTRANGE SUBROUTINE TO CALCULATE RANGE TO TARGETS   *
*****
SUBROUTINE TGTRANGE (TTIME,TGTZ, ZPHONE,NUMSSV,DEPTH,SSPVEL,
+   HMVEL, TRANGE, J)
REAL*4 TGTZ, ZPHONE,DEPTH,SSPVEL,HMVEL,TRANGE,TTIME
INTEGER*4 J, NUMSSV
DIMENSION TGTZ(2),ZPHONE(4),DEPTH(40),SSPVEL(40),TRANGE(2,4),
+   TTIME(2,4)
DO 10 I = 1, 4
CALL HMVELOC(TGTZ(J), ZPHONE(I), NUMSSV, DEPTH, SSPVEL, HMVEL)
TRANGE(J,I) = TTIME(J,I) * HMVEL
10 CONTINUE
RETURN
END

```

```

*****
*   THREEED SUBROUTINE TO CALCULATE TARGET POSITIONS   *
*****
SUBROUTINE THREEED (J,TGTX,TGTY,TGTZ,PHONEX,PHONEY,PHONEZ,RM)
REAL*4 TGTX,TGTY,TGTZ,PHONEX,PHONEY,PHONEZ,PRPX,PRPY,PRPZ,
+   XTO,YTO,ZTO,A1,A2,A3,A4,A5,A6,A7,A8,A9,RO,DR,RM
INTEGER*4 J, IN
DIMENSION TGTX(2),TGTY(2),TGTZ(2),PHONEX(4),PHONEY(4),
+   PHONEZ(4),RO(4),RM(2,4)
IN = 0
5 CONTINUE
XTO=TGTX(J)
YTO=TGTY(J)
ZTO=TGTZ(J)
A1=0.0
A2=0.0
A3=0.0
A4=0.0
A5=0.0
A6=0.0
A7=0.0
A8=0.0
A9=0.0

DO 10 I= 1, 4
RO(I) = SQRT((XTO-PHONEX(I))**2+(YTO-PHONEY(I))**2+
+   (ZTO-PHONEY(I))**2)
DR = RM(J,I) - RO(I)
PRPX = (XTO - PHONEX(I)) / RO(I)
PRPY = (YTO - PHONEY(I)) / RO(I)
PRPZ = (ZTO - PHONEZ(I)) / RO(I)
A1 = A1 + PRPX*PRPX
A2 = A2 + PRPY*PRPY
A3 = A3 + PRPZ*PRPZ
A4 = A4 + PRPY*PRPY
A5 = A5 + PRPY*PRPY
A6 = A6 + PRPZ*PRPZ
A7 = A7 + DR*PRPX
A8 = A8 + DR*PRPY

```

```

      A9 = A9 + DR*PRPZ
10 CONTINUE
      DETAO = A1*(A4*A6-A5*A5)-A2*(A2*A6-A5*A3)+A3*(A2*A5-A4*A3)
      DETA1 = A7*(A4*A6-A5*A5)-A8*(A2*A6-A5*A3)+A9*(A2*A5-A4*A3)
      DETA2 = A1*(A8*A6-A9*A5)-A2*(A7*A6-A9*A3)+A3*(A7*A5-A8*A3)
      DETA3 = A1*(A4*A9-A5*A8)-A2*(A2*A9-A5*A7)+A3*(A2*A8-A4*A7)
      TGTX(J) = XTO + DETA1/DETAO
      TGTY(J) = YTO + DETA2/DETAO
      TGTZ(J) = ZTO + DETA3/DETAO
      IF (((DETA1**2+DETA2**2+DETA3**2)/DETAO) .LT. 1.0 ) THEN
        GO TO 900
      ENDIF
      IN = IN + 1
      IF (IN .GT. 25) THEN
        GO TO 900
      ENDIF
      GOTO 5
900 RETURN
      END

```

```

*****
*   OUTPUT SUBROUTINE TO OUTPUT DATA RESULTS   *
*****
      SUBROUTINE OUTPUT (MEAN1,VAR1,MEAN2,VAR2,MEANR,VARR,
+      BTN,STN,TTN,NCOUNT)
      REAL*4 MEAN1,VAR1,MEAN2,VAR2,MEANR,VARR,BTN,STN,TTN
      INTEGER*4 NCOUNT
      OPEN (UNIT = 8, FILE = 'OUTPUT3.DAT')
      WRITE(8,*) '          MEAN      STAND DEV '
      WRITE(8,1000) MEAN1, VAR1
      WRITE(8,1001) MEAN2, VAR2
      WRITE(8,1002) MEANR, VARR
      WRITE(8,*) ' NUMBER OF ITERATIONS, BUOY      TRANS      TARGET '
      WRITE(8,1003) NCOUNT, BTN, STN,TTN
1000 FORMAT (' TRUE ERROR FOR TARGET 1 = ',F8.3, F8.4)
1001 FORMAT (' TRUE ERROR FOR TARGET 2 = ',F8.3, F8.4)
1002 FORMAT (' RELATIVE ERROR          = ',F8.3, F8.4)
1003 FORMAT (' 3X,I6,15X, F8.4, F8.4, F8.4)
      RETURN
      END

```

```

*****
*   URAND SUBROUTINE TO GENERATE RANDOM NUMBERS   *
*****
      SUBROUTINE URAND(A,B,SEED)
      REAL*8 SEED, PI, R1, R2
      PI=3.14159265358979
      R1=(SEED+PI)**504.D-2
      R1=R1-DINT(R1)
      SEED=R1
      R2=(SEED+PI)**504.D-2
      R2=R2-DINT(R2)
      SEED=R2
      R=SQRT(-2*LOG(R1))
      T=2*PI*R2
      A=R*SIN(T)
      B=R*COS(T)
      RETURN
      END

```

## APPENDIX B

The following is the output data from the simulations  
conducted for each of the four cases discussed in Chapter IV.

Case number 1:

### BUOYLOC.DAT

0.0,	0.0,	5.0,	0.0,	0.0,	1000.0,
3000.0,	5196.0,	5.0,	3000.0,	5196.0,	1000.0,
6000.0,	0.0,	5.0,	6000.0,	0.0,	1000.0,
9000.0,	5196.0,	5.0,	9000.0,	5196.0,	1000.0,

### TARGET.DAT

2036.0,	2036.0,	400.0,
1965.0,	1965.0,	400.0,

### OUTPUT.DAT

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	.002	.0000
TRUE ERROR FOR TARGET 2 =	.001	.0000
RELATIVE ERROR =	.001	.0000
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0000	.0000

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	19.829	.0122
TRUE ERROR FOR TARGET 2 =	19.695	.0122
RELATIVE ERROR =	14.982	.0084
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0010	.0010

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	39.791	.0247
TRUE ERROR FOR TARGET 2 =	39.564	.0248
RELATIVE ERROR =	30.101	.0169
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0020	.0020

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	60.054	.0380
TRUE ERROR FOR TARGET 2 =	59.780	.0383
RELATIVE ERROR =	45.545	.0260
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0030	.0030

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	80.887	.0530	
TRUE ERROR FOR TARGET 2 =	80.616	.0537	
RELATIVE ERROR =	61.654	.0362	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0040	.0040	.0040

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	102.065	.0688	
TRUE ERROR FOR TARGET 2 =	102.172	.0718	
RELATIVE ERROR =	78.586	.0486	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0050	.0050	.0050

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	123.875	.0910	
TRUE ERROR FOR TARGET 2 =	123.837	.0939	
RELATIVE ERROR =	98.655	.0726	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0060	.0060	.0060

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	145.096	.1044	
TRUE ERROR FOR TARGET 2 =	146.658	.1133	
RELATIVE ERROR =	118.392	.0931	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0070	.0070	.0070

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	164.285	.1207	
TRUE ERROR FOR TARGET 2 =	165.526	.1290	
RELATIVE ERROR =	138.519	.1075	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0080	.0080	.0080

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	183.286	.1335	
TRUE ERROR FOR TARGET 2 =	179.448	.1264	
RELATIVE ERROR =	154.021	.1197	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0090	.0090	.0090

	MEAN	STAND DEV	
TRUE ERROR FOR TARGET 1 =	198.663	.1406	
TRUE ERROR FOR TARGET 2 =	199.931	.1478	
RELATIVE ERROR =	172.593	.1288	
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET	
1000	.0100	.0100	.0100

Case number 2:

BUOYLOC.DAT

0.0,	0.0,	5.0,	0.0,	0.0,	1000.0,
3000.0,	5196.0,	5.0,	3000.0,	5196.0,	1000.0,
8000.0,	0.0,	5.0,	6000.0,	0.0,	1000.0,
9000.0,	5196.0,	5.0,	9000.0,	5196.0,	1000.0,

TARGET.DAT

1000.0,	2000.0,	400.0,
3000.0,	4236.0,	400.0,

OUTPUT.DAT

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	.001	.0000
TRUE ERROR FOR TARGET 2 =	.002	.0000
RELATIVE ERROR =	.001	.0000
NUMBER OF ITERATIONS, BUOY		
1000	.0000	.0000 .0000

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	23.314	.0147
TRUE ERROR FOR TARGET 2 =	12.332	.0058
RELATIVE ERROR =	19.779	.0111
NUMBER OF ITERATIONS, BUOY		
1000	.0010	.0010 .0010

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	46.881	.0300
TRUE ERROR FOR TARGET 2 =	24.694	.0116
RELATIVE ERROR =	39.783	.0226
NUMBER OF ITERATIONS, BUOY		
1000	.0020	.0020 .0020

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	71.010	.0467
TRUE ERROR FOR TARGET 2 =	37.106	.0175
RELATIVE ERROR =	60.300	.0355
NUMBER OF ITERATIONS, BUOY		
1000	.0030	.0030 .0030

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	96.323	.0673
TRUE ERROR FOR TARGET 2 =	49.592	.0236
RELATIVE ERROR =	81.926	.0521
NUMBER OF ITERATIONS, BUOY		
1000	.0040	.0040 .0040

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	122.966	.0913
TRUE ERROR FOR TARGET 2 =	62.178	.0299
RELATIVE ERROR =	104.788	.0721
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0050	.0050 .0050

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	148.598	.1136
TRUE ERROR FOR TARGET 2 =	74.547	.0364
RELATIVE ERROR =	127.339	.0906
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0060	.0060 .0060

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	174.871	.1362
TRUE ERROR FOR TARGET 2 =	87.047	.0428
RELATIVE ERROR =	150.839	.1110
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0070	.0070 .0070

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	194.483	.1489
TRUE ERROR FOR TARGET 2 =	99.075	.0498
RELATIVE ERROR =	169.387	.1218
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0080	.0080 .0080

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	209.383	.1497
TRUE ERROR FOR TARGET 2 =	111.316	.0572
RELATIVE ERROR =	183.449	.1207
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0090	.0090 .0090

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	232.755	.1665
TRUE ERROR FOR TARGET 2 =	123.187	.0622
RELATIVE ERROR =	206.640	.1412
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0100	.0100 .0100

Case number 3:

BUOYLOC.DAT

0.0,	0.0,	5.0,	0.0,	0.0,	1000.0,
3000.0,	5196.0,	5.0,	3000.0,	5196.0,	900.0,
6000.0,	0.0,	5.0,	6000.0,	0.0,	800.0,
9000.0,	5196.0,	5.0,	9000.0,	5196.0,	700.0,

TARGET.DAT

2036.0,	2036.0,	400.0,
1965.0,	1965.0,	400.0,

OUTPUT.DAT

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	.002	.0000
TRUE ERROR FOR TARGET 2 =	.001	.0000
RELATIVE ERROR =	.001	.0000
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0000	.0000 .0000

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	21.890	.0139
TRUE ERROR FOR TARGET 2 =	21.668	.0138
RELATIVE ERROR =	16.342	.0095
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0010	.0010 .0010

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	44.028	.0283
TRUE ERROR FOR TARGET 2 =	43.639	.0283
RELATIVE ERROR =	32.941	.0193
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0020	.0020 .0020

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	66.771	.0445
TRUE ERROR FOR TARGET 2 =	66.268	.0445
RELATIVE ERROR =	50.214	.0303
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0030	.0030 .0030

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	90.263	.0629
TRUE ERROR FOR TARGET 2 =	89.303	.0620
RELATIVE ERROR =	68.667	.0436
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0040	.0040 .0040

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	114.024	.0834
TRUE ERROR FOR TARGET 2 =	114.166	.0862
RELATIVE ERROR =	89.502	.0640
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0050	.0050 .0050

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	137.825	.1066
TRUE ERROR FOR TARGET 2 =	136.027	.1048
RELATIVE ERROR =	111.802	.0864
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0060	.0060 .0060

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	164.585	.1340
TRUE ERROR FOR TARGET 2 =	159.147	.1289
RELATIVE ERROR =	136.492	.1275
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0070	.0070 .0070

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	178.254	.1318
TRUE ERROR FOR TARGET 2 =	174.554	.1306
RELATIVE ERROR =	146.033	.1085
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0080	.0080 .0080

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	201.941	.1519
TRUE ERROR FOR TARGET 2 =	198.101	.1477
RELATIVE ERROR =	178.767	.1563
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0090	.0090 .0090

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	217.521	.1554
TRUE ERROR FOR TARGET 2 =	212.118	.1509
RELATIVE ERROR =	186.845	.1463
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0100	.0100 .0100

Case number 4:

EUOYLOC.DAT

0.0,	0.0,	5.0,	0.0,	0.0,	1000.0,
3000.0,	5196.0,	5.0,	3000.0,	5196.0,	900.0,
6000.0,	0.0,	5.0,	6000.0,	0.0,	800.0,
9000.0,	5196.0,	5.0,	9000.0,	5196.0,	700.0,

TARGET.DAT

1000.0,	2000.0,	400.0,
3000.0,	4236.0,	400.0,

OUTPUT.DAT

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	.001	.0000
TRUE ERROR FOR TARGET 2 =	.001	.0000
RELATIVE ERROR =	.001	.0000
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0000	.0000 .0000

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	24.415	.0156
TRUE ERROR FOR TARGET 2 =	13.655	.0068
RELATIVE ERROR =	20.218	.0114
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0010	.0010 .0010

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	49.162	.0319
TRUE ERROR FOR TARGET 2 =	27.372	.0136
RELATIVE ERROR =	40.721	.0233
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0020	.0020 .0020

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	74.694	.0504
TRUE ERROR FOR TARGET 2 =	41.198	.0208
RELATIVE ERROR =	61.921	.0372
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0030	.0030 .0030

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	102.194	.0764
TRUE ERROR FOR TARGET 2 =	55.192	.0283
RELATIVE ERROR =	84.955	.0585
NUMBER OF ITERATIONS, BUOY	TRANS	TARGET
1000	.0040	.0040 .0040

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	130.319	.1024
TRUE ERROR FOR TARGET 2 =	69.366	.0364
RELATIVE ERROR =	109.312	.0842
NUMBER OF ITERATIONS, BUOY      TRANS      TARGET		
1000	.0050	.0050      .0050

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	154.690	.1222
TRUE ERROR FOR TARGET 2 =	83.145	.0447
RELATIVE ERROR =	130.410	.0952
NUMBER OF ITERATIONS, BUOY      TRANS      TARGET		
1000	.0060	.0060      .0060

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	183.675	.1501
TRUE ERROR FOR TARGET 2 =	97.235	.0547
RELATIVE ERROR =	156.063	.1203
NUMBER OF ITERATIONS, BUOY      TRANS      TARGET		
1000	.0070	.0070      .0070

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	202.344	.1559
TRUE ERROR FOR TARGET 2 =	112.773	.0695
RELATIVE ERROR =	173.353	.1238
NUMBER OF ITERATIONS, BUOY      TRANS      TARGET		
1000	.0080	.0080      .0080

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	221.332	.1593
TRUE ERROR FOR TARGET 2 =	126.445	.0794
RELATIVE ERROR =	194.134	.1413
NUMBER OF ITERATIONS, BUOY      TRANS      TARGET		
1000	.0090	.0090      .0090

	MEAN	STAND DEV
TRUE ERROR FOR TARGET 1 =	239.836	.1740
TRUE ERROR FOR TARGET 2 =	140.192	.0861
RELATIVE ERROR =	210.705	.1459
NUMBER OF ITERATIONS, BUOY      TRANS      TARGET		
1000	.0100	.0100      .0100

## LIST OF REFERENCES

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