



US Army Corps
of Engineers
Waterways Experiment
Station

AD-A276 924



Miscellaneous Paper GL-94-2

January 1994

2

A Computer Program for Evaluation and Overlay Design of Roads, Streets, and Open Storage Areas Using Nondestructive Testing and Elastic Layered Method—WESROAD

by Yu T. Chou
Geotechnical Laboratory

DTIC
ELECTE
MAR 15 1994
S E D

WESROAD

Approved For Public Release; Distribution Is Unlimited

3200 94-08214



DTIC QUALITY INSPECTED 1

94 3 11 152

Prepared for Headquarters, U.S. Army Corps of Engineers

The contents of this report are not to be used for advertising, publication, or promotional purposes. Citation of trade names does not constitute an official endorsement or approval of the use of such commercial products.



PRINTED ON RECYCLED PAPER

A Computer Program for Evaluation and Overlay Design of Roads, Streets, and Open Storage Areas Using Nondestructive Testing and Elastic Layered Method—WESROAD

by Yu T. Chou

Geotechnical Laboratory
U.S. Army Corps of Engineers
Waterways Experiment Station
3909 Halls Ferry Road
Vicksburg, MS 39180-6199

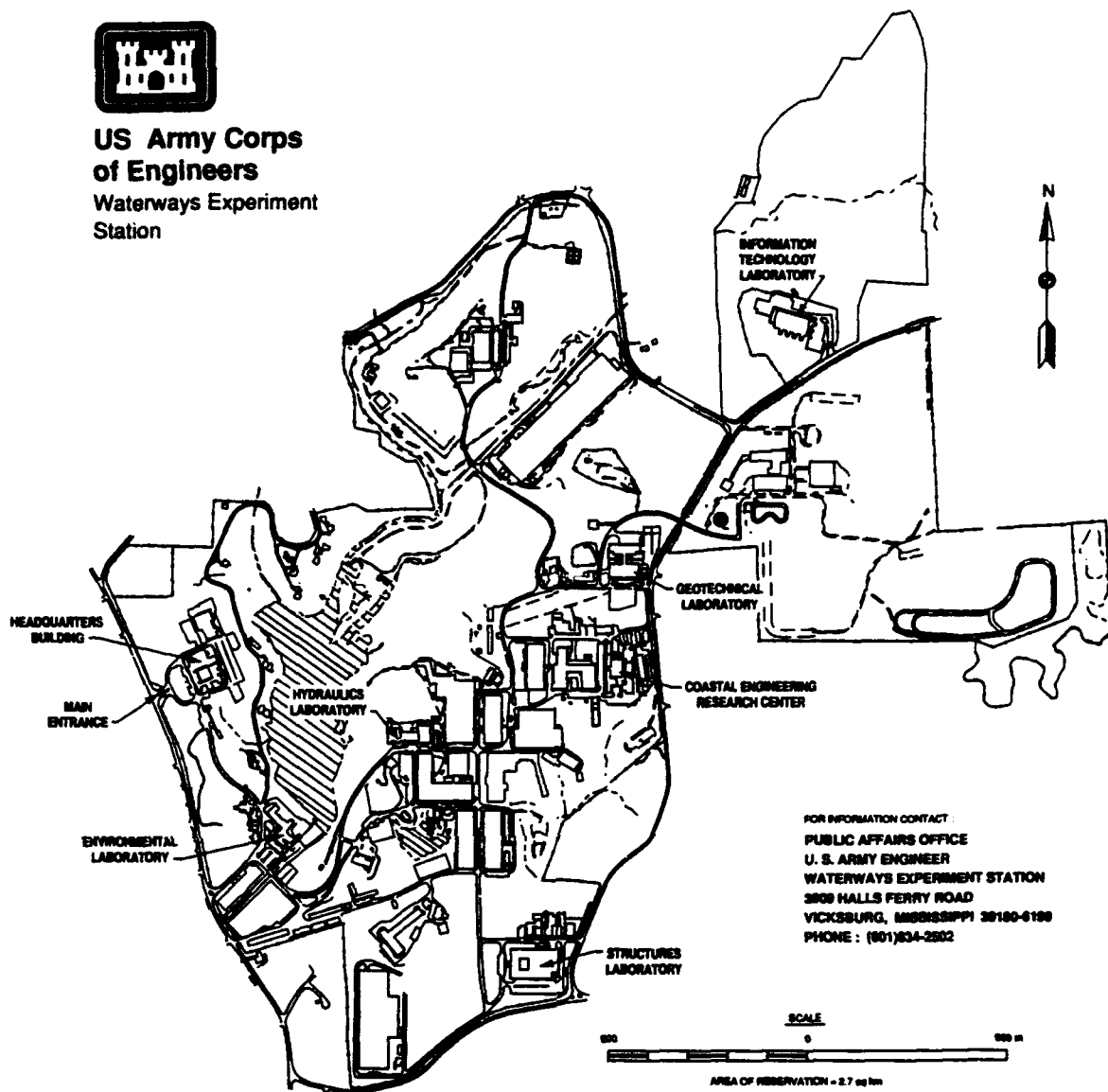
Accession For	
NTIS	CRA&I ☒
DTIC	TAB ☐
Unannounced	☐
Justification	
By	
Distribution /	
Availability Codes	
Dist	Avail. and/or Special
A-1	

Final report

Approved for public release; distribution is unlimited



**US Army Corps
of Engineers**
Waterways Experiment
Station



Waterways Experiment Station Cataloging-in-Publication Data

Chou, Yu T.

A computer program for evaluation and overlay design of roads, streets, and open storage areas, using nondestructive testing and elastic layered method—WESROAD / by Yu T. Chou ; prepared for U.S. Army Corps of Engineers.

31 p. : ill. ; 28 cm. — (Miscellaneous paper ; GL-94-2)

Includes bibliographical references.

1. Pavements — Overlays — Data processing. 2. WESROAD (Computer program) 3. Roads — Design and construction — Data processing. I. United States. Army. Corps of Engineers. II. U.S. Army Engineer Waterways Experiment Station. III. Title. IV. Series: Miscellaneous paper (U.S. Army Engineer Waterways Experiment Station) ; GL-94-2.

TA7 W34m no.GL-94-2

Contents

Preface	iv
Conversion Factors, Non-SI to SI Units of Measurement	v
1—Introduction	1
Background	1
Purpose and Scope	1
2—Program Logic and System Requirements	2
Program Logic	2
Concept of evaluation	4
Principle of overlay design	4
System Requirements	4
3—User's Instructions	5
Input data, INPAVE	5
Interface condition	5
Joint condition	5
Pavement condition	6
Evaluation criteria	7
Stress and Strain Computation, INLEA and WESLEA	7
Pavement Evaluation and Overlay Design, WESROAD	7
4—Example Problems	8
INLEA and WESLEA	8
INPAVE and WESROAD	11
Rigid pavement evaluation and overlay design	11
Flexible pavement evaluation and overlay design	18
5—Recommendations	24
SF 298	

Preface

The work reported herein was developed under the Headquarters, U.S. Army Corps of Engineers PCASE program. Mr. Greg Hughes, U.S. Army Corps of Engineers, was the Technical Monitor.

The study was conducted from June 1989 to February 1992 at the U.S. Army Engineer Waterways Experiment Station (WES), Geotechnical Laboratory (GL), by Dr. Yu T. Chou, Pavement Systems Division (PSD). The work was performed under the general supervision of Dr. W. F. Marcuson III, Director, GL, and Dr. George Hammit II, Chief, PSD, and Dr. Al Bush, Chief, Criteria Development and Applications Branch. This report was written by Dr. Chou.

At the time of publication of this report, Director of WES was Dr. Robert W. Whalin. Commander was COL Bruce K. Howard, EN.

Conversion Factors, Non-SI to SI Units of Measurement

Non-SI units of measurement used in this report can be converted to SI units as follows:

Multiply	By	To Obtain
inches	2.54	centimeters
kip (force)	4.448222	kilonewtons
pounds (force)	4.448222	newtons
pounds (force) per square inch	6.894757	kilopascals
tons (2,000 pounds, mass)	907.1847	kilograms

1 Introduction

Background

An engineering technical manual entitled "Evaluation of Roads, Streets, and Open Storage Areas Using Nondestructive Testing" has been prepared.¹ A user-friendly computer program, WESROAD, was prepared for the evaluation of the load-carrying capacity and overlay thickness requirements of existing military roads and streets.

Purpose and Scope

The purpose of this report is to provide users with necessary information for running the WESROAD computer program. The report contains the programming logic, computer system requirements, user instructions, and the input and output for example problems. The overlay design includes both concrete and flexible overlays.

¹ Headquarters, Department of the Army. "Evaluation of roads, streets, and open storage areas using nondestructive testing," TM 5-826-8/AFM 32-8009, Vol 2, Washington, DC.

2 Program Logic and System Requirements

Program Logic

WESROAD is a modification of WESPAVE, an evaluation program for air-field pavements that uses nondestructive testing (NDT) and the elastic layered method developed at the U.S. Army Engineer Waterways Experiment Station (WES). The program has two separate parts, which are presented below.

INPAVE is a user-friendly computer program creating input files for running WESROAD. The necessary information includes pavement layer thicknesses and moduli (backcalculated from NDT tests), interface slip conditions, pavement surface conditions, joint conditions in concrete pavements, and traffic data. Traffic data include the type and frequency of design vehicles traveling on the pavements. When running WESROAD, the WESLEA computer program is used to compute stresses and strains in the pavement.

The design vehicles are divided into axle groups for computation of pavement stresses, strains, and damage. A passenger car has two axles, which are both single axle, single wheels. A medium weight truck usually has two axle loads: the front is single axle, single wheels, and the rear is either tandem axle, dual wheels, or single axle, dual wheels. An 18-wheeler has three axles: the front is single axle, single wheels, and the middle and back axles are tandem axle, dual wheels. For track vehicles, such as military tanks, each track load is converted into eight circular loads and is considered as one axle load. Table 1 shows 19 axle loads based on the wheel configuration and weight category, which covers a wide range of loads for designing military roads and streets. The background of the group classification is presented in Technical Report No. 3-582.¹

¹ U.S. Army Engineer Waterways Experiment Station. (1961). "Revised method of thickness design for flexible highway pavements at military installations," Technical Report No. 3-582, Vicksburg, MS.

Table 1
Design Load Axles

<u>Configuration</u>	<u>Load Range, kips</u>
<u>Passenger cars, trucks, buses, etc.</u>	
Pneumatic tires	
1. Single axle, single wheels	0-5
2. Single axle, single wheels	5-10
3. Single axle, dual wheels	0-10
4. Single axle, dual wheels	10-20
5. Single axle, dual wheels	20-30
6. Tandem axle, single wheels	0-10
7. Tandem axle, single wheels	10-15
8. Tandem axle, dual wheels	10-15
9. Tandem axle, dual wheels	15-20
10. Tandem axle, dual wheels	20-50
<u>Forklift truck</u>	
Pneumatic tires	
11. Single axle, dual wheels	10-35
Solid rubber tires	
12. Single axle, single wheels	0-5
13. Single axle, single wheels	5-10
14. Single axle, single wheels	10-20
<u>Tracked vehicles</u>	
15. solid rubber grousers	0-20
16. solid rubber grousers	20-35
17. solid rubber grousers	35-50
18. solid rubber grousers	50-70
19. solid rubber grousers	70-120

Note: A table of factors for converting non-SI units of measurement to SI is presented on page v.

For example, if a road is to be designed for the following traffic:

- 10,000 passes of passenger cars, 9 kips for each axle
- 5,000 passes of truck, 9-kip front axle and 32-kip rear axle
- 1,000 passes of 60-ton M1 tank

The design axle loads, according to Table 1, will be:

- 25,000 passes of No. 2 axle load ($2 \times 10,000 + 5,000$)
 - 5,000 passes of No. 10 axle load (5,000)
 - 1,000 passes of No. 19 axle load (1,000)
- (Note: Axle numbers refer to the axles in Table 1.)

WESROAD is also a user-friendly computer program which first evaluates the load-carrying capacity of the existing pavement. If the pavement is capable of carrying the design traffic, the program will terminate; otherwise, the overlay design will proceed. The design includes both asphalt and concrete overlays. For concrete overlays, thicknesses of partial-bond and no-bond designs are given.

Concept of evaluation

The stresses, strains, and deflections in the pavement structure under the axle loads are computed by computer program WESLEA based on the Burmister layered elastic solution. The allowable passes on the pavement under each axle load are computed according to the failure criteria. The pavement damage under each axle load is then computed and summed. If the total damage exceeds 1.0, the pavement requires an overlay. Damage is defined as the ratio of the design passes to the allowable passes.

Principle of overlay design

Overlay design is based on a single axle load of the selected axle loads which induce the most severe damage to the pavement. An equivalent pass determined from the relationship shown below is calculated and a required new concrete thickness is determined. The overlay thickness is determined from overlay equations based on the required new concrete thickness.

$$\text{Total damage} = \frac{\text{Equivalent pass}}{\text{Allowable pass of the critical axle}} \quad (1)$$

It should be noted that WESPAVE adopts the allowable load concept in air-field pavement evaluation. The allowable load approach is feasible because WESPAVE evaluates a pavement for one aircraft loading. For road evaluation using WESROAD, various vehicles of different axle loadings and of different frequency are involved. The damage approach is therefore used to account for the mixed effects of the axle loadings.

System Requirements

The computer program was compiled using the Microsoft FORTRAN 5.0 compiler and was designed to operate on an IBM or compatible machine under the DOS 3.0 operating system or a later system. Although not required, an IBM AT class computer or better with a math co-processor and 640 KB of main memory is recommended.

3 User's Instructions

Input data, INPAVE

INPAVE can be activated by typing INPAVE at the DOS prompt and following the instructions shown on the screen. An input file name is required. A file name with the extension .INP is suggested for easy retrieval. Special attention should be paid in selecting interface slip conditions and joint conditions explained in the following paragraphs.

Interface condition

One drawback of every elastic layered computer program is that the interface condition between total adhesion and total slip cannot be quantified. In the WESLEA program, an interface condition of 1 indicates total adhesion, 0 indicates full slip, and 2-1,000 indicates partial slip. For an interface condition from 2 to 1,000, the physical meaning cannot be identified except it is known as a partial slip case in which the higher number means greater slip. In other words, the exact value of interface condition between a Portland cement concrete slab layer and the supporting clay subgrade is not known. It is suggested that a value of 1,000 be used for this case and that total adhesion be used for flexible pavements, i.e., total adhesion between the asphalt concrete and the granular or stabilized layers and total adhesion between the granular or the stabilized layer and the subgrade. It is important to know that WESLEA is fixed for five layers and if full slip is used at the interface, the program is fixed so that the first and second interfaces have full slip and the remaining interfaces have total adhesion.

Joint condition

For concrete roads, the free edge loading condition is the most critical and should be used for design. However, the failure criteria on which the design is based were established in test tracks where good load transfer was provided, and the test data were analyzed using the elastic layered method (interior

loading). The failure criteria are presented in TM 5-822-13/AFM 32-8007¹ and the development of the criteria is explained in Chou (1989).² To account for the more critical edge loading condition, a scheme was developed by Chou (1989)² to multiply the concrete stresses computed using the elastic layered method (WESLEA) by 1.33 to increase the concrete thickness.

In INPAVE, the user is asked to input the joint efficiency for the concrete pavement. The joint efficiency is the ratio of the deflection of the unloaded slab to the deflection of the loaded slab. A factor is computed based on the equation:

$$\text{FACTOR} = 0.7557 + 0.2058 \cdot \text{RATIO} + 0.1505 \cdot \text{RATIO}^2$$

for RATIO less than 0.75

$$\text{FACTOR} = 1.0 \quad \text{for RATIO greater than 0.75} \quad (2)$$

The computed stresses are then divided by this factor to account for the joint condition. Note that the smallest value of FACTOR is 0.7557. In other words, when there is no load transfer across the concrete pavement joints, the computed stresses will be increased by a factor of 1.323.

Since the computed concrete stresses are increased by a factor of 1.33 to account for the more critical edge loading effect as discussed above, it can be argued whether or not joint condition should be considered in pavement evaluation. In the WESROAD program, users are requested to input a measured deflection ratio (i.e., equal or less than 1.0). If the user feels that the joint condition should not be considered, the deflection ratio can be input as 1.0. Note that a deflection ratio less than 1.0 will increase the computed stresses and make the evaluation on the safer side. If the user does not have a strong feeling on this matter, either a measured deflection ratio or a value between 0.75 and zero should be used, preferably zero.

In WESROAD, an answer of "NO" to the question "DO YOU HAVE JOINT EFFICIENCY MEASUREMENTS" will automatically set the value of FACTOR to 1.0 in Equation 2.

Pavement condition

If the pavement surface is severely cracked, the "poor" option should be answered in INPAVE. In doing so the computed stresses are multiplied by a factor of 1.33 for both flexible and rigid pavements.

¹ Headquarters, Department of the Army. "Pavement design for roads, streets, and open storage areas, elastic layered method," TM 5-822-13/AFM 32-8007, Vol 1, Washington, DC.

² Yu T. Chou. (1989). "Development of failure criteria of rigid pavement thickness requirements for military roads and streets, elastic layered method," Miscellaneous Paper GL-89-9, U.S. Army Engineer Waterways Experiment Station, Vicksburg, MS.

Evaluation criteria

In WESROAD, users are asked to select the evaluation criteria of either initial failure or extended traffic. Initial failure refers to the failure condition that 50 percent of the slabs to be evaluated are cracked into two or three pieces at the end of the design pass level. Extended traffic refers to the condition that at the end of the design pass level, 50 percent of the slabs are cracked into approximately six pieces due to the design traffic.

Stress and Strain Computation, INLEA and WESLEA

Computer program INLEA creates input files for stress and strain computations in WESLEA. It should be noted that INLEA is different from INPAVE which creates input files for WESROAD for pavement evaluation and overlay design. INLEA inputs only pavement dimensions and loads, while INPAVE inputs not only these data but also pavement surface and joint conditions, traffic data, and many others. INLEA can be activated by typing in INLEA at the DOS prompt and following the instructions on the screen. An input file should first be prepared in INLEA to run WESLEA. The input file may be copied, manually modified, and renamed to expedite the input process, but care should be exercised not to alter the format of the file. Otherwise, run-time errors will be encountered in running the WESLEA program. WESLEA can be activated by typing in WESLEA at the DOS prompt and following the instructions shown on the screen. WESLEA is fixed at five layers. In other words, for a concrete slab on subgrade soil, the subgrade should be divided into four layers having any layer thicknesses but having identical material properties and full adhesion at the interfaces. However, a reasonable layer thickness should be used, such as 10 in., except the bottom layer, which is a half space. An extremely small layer thickness may cause a solution convergence problem.

Pavement Evaluation and Overlay Design, WESROAD

WESROAD can be activated by typing in WESROAD at the DOS prompt and following the instructions shown on the screen. An input file should first be prepared using INPAVE. The input file may be copied, manually modified, and renamed to expedite the input process, but care should be exercised not to alter the format of the file. Otherwise, run-time errors will be encountered in running WESROAD.

4 Example Problems

This chapter presents the results of computer problem runs which the user may use to check his own computer results to ensure the correctness of the computer runs.

INLEA and WESLEA

Pavement and load conditions are as follows:

a. Loads (Number 10 axle in Table 1):

Two dual-tandem axle loads spaced at 72 in. side by side

Axle load: 32 kips

Dual-tandem wheel dimension: 13.5 by 48 in.

Contact area radius: 4.265 in.

Selected computational points:

$x = 6.75$ in. $y = 0$ in. $z = 6$ in.

$x = 13.5$ in. $y = 0$ in. $z = 6$ in.

b. Pavement section:

Concrete slab thickness: 6 in.

E modulus of the concrete: 4,387,500 psi

Poisson's ratio of the concrete: 0.15

Slip condition under the concrete slab: Partial slip, 1,000

Subgrade modulus: 6,000 psi

Poisson's ratio of the subgrade: 0.4

The input data WESLEAR1.INP is shown in Table 2. The subgrade is divided into four layers.

When WESLEA is run, output is stored in the file WESLEAR1.OUT as shown in Table 3.

Table 2
Input Data File of WESLEA, WESLEAR1.INP

```

NO. OF PROBLEMS
*****
      1
                                     TITLE
*****
Input file for WESLEA, rigid slab under one 32-k dual tandem axle load
E, PSI      NU      THICK., IN      SLIP
*****      *      *      *      *
4387500.    .15      6.0      1000.
6000.       .40      10.0      1.
6000.       .40      10.0      1.
6000.       .40      10.0      1.
6000.       .40
NO. OF LOADED AREAS
*****
      8
LOAD, LBS   RAD., IN   X, IN   Y, IN
*****      *      *      *      *
4000.       4.265      .00      .00
4000.       4.265     13.50      .00
4000.       4.265      .00     48.00
4000.       4.265     13.50     48.00
4000.       4.265     72.00      .00
4000.       4.265     85.50      .00
4000.       4.265     72.00     48.00
4000.       4.265     85.50     48.00
NO. OF EVALUATION POSITIONS
*****
      2
LAYER X, IN   Y, IN   Z, IN
*****      *      *      *
1      13.50      .00      6.00
1       6.75      .00      6.00

```


Table 3
Output File of WESLEA, WESLEAR1.OUT

*****WESLEA DRA-07.90.18*****
 P R O B L E M N U M B E R = 1
 *****EXECUTED: 12- 2-1991 @ 15:19*****

Input file for WESLEA, rigid slab under one 32-k twin tandem axle load

STRUCTURE INFORMATION

MODULUS PSI *****	POISSON RATIO *****	THICKNESS IN *****	INTERFACE 1=NO SLIP >1=PARTIAL SLIP *****
4387500.	.15	6.00	
6000.	.40	10.00	1000.
6000.	.40	10.00	1.
6000.	.40	10.00	1.
6000.	.40		1.

INTEGRATION STEP : .004

LOAD INFORMATION

LOAD NO. ****	RADIUS IN *****	LOAD LB *****	CO-ORDINATES, IN X Y ***** *****	
1	4.27	4000.	.00	.00
2	4.27	4000.	13.50	.00
3	4.27	4000.	.00	48.00
4	4.27	4000.	13.50	48.00
5	4.27	4000.	72.00	.00
6	4.27	4000.	85.50	.00
7	4.27	4000.	72.00	48.00
8	4.27	4000.	85.50	48.00

POSITION: 1
 CO-ORDINATES, IN

LAYER *****	X *****	Y *****	Z *****
1	13.50	.00	6.00

(Continued)

Table 3 (Concluded)

	X	Y	Z
	*****	*****	*****
NORMAL STRESS, PSI	-188.2	-226.8	2.2
SHEAR STRESS, PSI	-.1	.0	6.1
NORMAL STRAIN, IN/IN	-.3522E-04	-.4533E-04	.1469E-04
DISPLACEMENT, MILS	.189	.497	-33.872

	POSITION: 2		
	CO-ORDINATES, IN		
LAYER	X	Y	Z
*****	*****	*****	*****
1	6.75	.00	6.00
	X	Y	Z
	*****	*****	*****
NORMAL STRESS, PSI	-156.6	-220.2	2.2
SHEAR STRESS, PSI	-.1	-.1	10.8
NORMAL STRAIN, IN/IN	-.2823E-04	-.4491E-04	.1338E-04
DISPLACEMENT, MILS	.407	.482	-33.160

INPAVE and WESROAD

Rigid pavement evaluation and overlay design

The existing pavement has the following characteristics and design traffic:

a. Pavement characteristics:

Concrete thickness: 6 in.

E modulus of the concrete backcalculated from NDT testing:
4,387,500 psi

Flexural strength of the concrete: 675 psi

Pavement surface condition: Poor with cracks

Subgrade modulus backcalculated from NDT testing: 6,000 psi

Frost code of the subgrade: zero

Interface condition under the concrete slab: Partial slip value of 1,000

Joint deflection ratio: 0.9

Pavement condition CB = 0.75

Pavement condition CR = 0.50

Evaluation criteria: Initial crack

Complete output: Yes

Compute overlays: Yes

b. *Traffic:*

100,000 operations of No. 1 axle, 1.5 kips
 200,000 operations of No. 2 axle, 9.0 kips
 700,000 operations of No. 10 axle, 32.0 kips
 (Note: Axle numbers refer to Table 1.)

After INPAVE is run, the input file EXAMPR1.INP is created as shown in Table 4. Axle coverages on the table are converted from input operations based on the operation per coverage values shown in Table 7 of WES Technical Report 3-582.

Table 4
Input File of WESROAD for Rigid Pavement, EXAMPR1.INP

```

NO. OF PROBLEMS
*****
1

                                TITLE
*****
Example Problem, Rigid Base Pavement, Three axle loads.
PAVEMENT TYPE          PAVEMENT          CONDITION      COMPUTE OVERLAYS
R=RIG/F=FLEX/C=COMP          G=GOOD/P=POOR          Y=YES,N=NO
*****
'r'          'S'          'P'          'Y'
NO. OF LAYERS  LAYER FOR SURFACE CRITERIA  LAYER FOR SUBGRADE CRITERIA
*****
2              1              2
TYPE  FROST CODE  E, PSI  THICK, IN  NU  SLIP
****  *****
2      0          4387500.  6.0    .15  1000.
6      0          6000.    .40    0.
*****RIGID & COMPOSITE PAVEMENTS ONLY*****
COMPLETE * PCC      JOINT      I=INIT FAILURE * OVERLAYS ONLY *
OUTPUT  * FLEX STR  DEFL RATIO  E=EXT TRAFFIC * CB      CR      *
*****  * *****  *****  *****
'y'      675.      .90      'I'      .75      .50
NO. OF AXLES CONSIDERED
*****
3
AXLE      AXLE      AXLE      AXLE
CODE      LOAD, KIPS  OPERATIONS  COVERAGES
****      *****
1          1.5      .100000E+06 .104275E+05
2          9.0      .200000E+06 .320000E+05
10         32.0     .500000E+06 .242718E+06
  
```

After WESROAD is run, the complete output is stored in EXAMPR1.OUT as shown in Table 5. The complete output is explained as follows:

Table 5
Output File of WESROAD for Rigid Pavement, EXAMPR1.OUT

 *****"WESPAVE" VERSION DRA-09.89.12*****
 *****EXECUTED: 11-19-1991 @ 13:44*****

PROBLEM NUMBER 1

Example Problem, rigid base pavement, three axle loads

PAVEMENT INPUT PARAMETERS

LAYER NO	MATERIAL TYPE	FROST CODE	MODULUS, PSI NDT	FROST	THICK. IN.	POIS RAT.	SLIP VALUE
1	PCC	0	4387500.	4387500.	6.00	.15	1000.
2	SUBGRADE	0	6000.	6000.	10.00	.40	1.
3	SUBGRADE	0	6000.	6000.	10.00	.40	1.
4	SUBGRADE	0	6000.	6000.	10.00	.40	
5	SUBGRADE	0	6000.	6000.	SEMI-INF	.40	

PAVEMENT EVALUATION SUMMARY
 (ALLOWABLE LOAD NOT APPLICABLE)

DESIGN AXLE ID	DESIGN LOAD KIPS	DESIGN COVERAGE LEVEL	ALLOW-ABLE LOAD KIPS	ALLOWABLE COVERAGES OF DESIGN AXLE	REQ'D OVERLAY, IN.		
					PCC	AC BOND	NO BOND
10	32.0	.244876E+07			13.4	7.6	8.4

(Sheet 1 of 5)

Table 5 (Continued)

BLIST FOR PROBLEM NUMBER 1

01:VEHICLE-PNEUM SA-SW 0-5

*****STRESSES FROM WES-5*****

EVALUATION POSITION	*****LOCATION*****			ADJUSTED TENSILE STRESS AT BOTTOM OF PCC LAYER, PSI
	X, IN.	Y, IN.	DEPTH, IN.	
1	.0	.0	6.00	.550253E+02

STRESSES HAVE BEEN MULTIPLIED BY 1.773

RIGID PAVEMENT EVALUATION

LAYER 1 THICKNESS= 6.00 OVERLAY THICKNESS= .00
 ALLOWABLE STRESS= 284.84 COMPUTED STRESS= 55.03
 STRESS RATIO= 5.18
 NO. OF COVERAGES= 104275.0 STREET PAVEMENT AREA
 DESIGN AXLE LOAD(KIPS)= 2. ALLOWABLE LOAD=NOT APPLICABLE
 MODULUS OF SUBGRADE REACTION, k (PCI) = 69.3
 EFFECTIVE k (PCI) = 69.3 PCC FLEXURAL STR (PSI)= 675.0
 DEFL. RATIO= .90 LOAD REDUCTION FACTOR = 1.000
 IMPACT FACTOR= 1.00 EVALUATION FOR: INITIAL FAILURE
 CONDITION= POOR CONDITION FACTOR= .75

02:VEHICLE-PNEUM SA-SW 5-10

*****STRESSES FROM WES-5*****

EVALUATION POSITION	*****LOCATION*****			ADJUSTED TENSILE STRESS AT BOTTOM OF PCC LAYER, PSI
	X, IN.	Y, IN.	DEPTH, IN.	
1	.0	.0	6.00	.324207E+03

STRESSES HAVE BEEN MULTIPLIED BY 1.773

(Sheet 2 of 5)

Table 5 (Continued)

RIGID PAVEMENT EVALUATION

LAYER 1 THICKNESS= 6.00 OVERLAY THICKNESS= .00
ALLOWABLE STRESS= 265.48 COMPUTED STRESS= 324.21
STRESS RATIO= .82
NO. OF COVERAGES= 320000.0 STREET PAVEMENT AREA
DESIGN AXLE LOAD(KIPS)= 9. ALLOWABLE LOAD=NOT APPLICABLE
MODULUS OF SUBGRADE REACTION, k (PCI) = 69.3
EFFECTIVE k (PCI) = 69.3 PCC FLEXURAL STR (PSI)= 675.0
DEFL. RATIO= .90 LOAD REDUCTION FACTOR = 1.000
IMPACT FACTOR= 1.00 EVALUATION FOR: INITIAL FAILURE
CONDITION= POOR CONDITION FACTOR= .75

10:VEHICLE-PNEUM TA-DW 20-50

*****STRESSES FROM WES-5*****

EVALUATION POSITION	*****LOCATION*****		DEPTH, IN.	ADJUSTED TENSILE STRESS AT BOTTOM OF PCC LAYER, PSI
	X, IN.	Y, IN.		
1	6.8	.0	6.00	.391407E+03
2	6.8	24.0	6.00	.226994E+03
3	13.5	.0	6.00	.405058E+03

STRESSES HAVE BEEN MULTIPLIED BY 1.773

RIGID PAVEMENT EVALUATION

LAYER 1 THICKNESS= 6.00 OVERLAY THICKNESS= .00
ALLOWABLE STRESS= 236.44 COMPUTED STRESS= 405.06
STRESS RATIO= .58
NO. OF COVERAGES= 2427180.0 STREET PAVEMENT AREA
DESIGN AXLE LOAD(KIPS)= 32. ALLOWABLE LOAD=NOT APPLICABLE
MODULUS OF SUBGRADE REACTION, k (PCI) = 69.3
EFFECTIVE k (PCI) = 69.3 PCC FLEXURAL STR (PSI)= 675.0
DEFL. RATIO= .90 LOAD REDUCTION FACTOR = 1.000
IMPACT FACTOR= 1.00 EVALUATION FOR: INITIAL FAILURE
CONDITION= POOR CONDITION FACTOR= .75

10:VEHICLE-PNEUM TA-DW 20-50

(Sheet 3 of 5)

Table 5 (Continued)

*****STRESSES FROM WES-5*****

EVALUATION POSITION	*****LOCATION*****		DEPTH, IN.	ADJUSTED TENSILE STRESS AT BOTTOM OF PCC LAYER, PSI
	X, IN.	Y, IN.		
1	6.8	.0	10.28	.212674E+03
2	6.8	24.0	10.28	.149693E+03
3	13.5	.0	10.28	.213897E+03

STRESSES HAVE BEEN MULTIPLIED BY 1.773

RIGID PAVEMENT EVALUATION

LAYER 1 THICKNESS= 10.28 OVERLAY THICKNESS= 4.28
ALLOWABLE STRESS= 236.33 COMPUTED STRESS= 213.90
STRESS RATIO= 1.10
NO. OF COVERAGES= 2448760.2 STREET PAVEMENT AREA
DESIGN AXLE LOAD(KIPS)= 32. ALLOWABLE LOAD=NOT APPLICABLE
MODULUS OF SUBGRADE REACTION, k (PCI)= 69.3
EFFECTIVE k (PCI)= 69.3 PCC FLEXURAL STR (PSI)= 675.0
F-FACTOR FOR AC OVERLAY= .95 CB= .75 CR= .50
DEFL. RATIO= .90 LOAD REDUCTION FACTOR = 1.000
IMPACT FACTOR= 1.00 EVALUATION FOR: INITIAL FAILURE
CONDITION= POOR CONDITION FACTOR= .75

ESTIMATED NEW THICKNESS= 9.61

10:VEHICLE-PNEUM TA-DW 20-50

*****STRESSES FROM WES-5*****

EVALUATION POSITION	*****LOCATION*****		DEPTH, IN.	ADJUSTED TENSILE STRESS AT BOTTOM OF PCC LAYER, PSI
	X, IN.	Y, IN.		
1	6.8	.0	9.61	.229757E+03
2	6.8	24.0	9.61	.158448E+03
3	13.5	.0	9.61	.231785E+03

STRESSES HAVE BEEN MULTIPLIED BY 1.773

RIGID PAVEMENT EVALUATION

(Sheet 4 of 5)

Table 5 (Concluded)

LAYER 1 THICKNESS=	9.61	OVERLAY THICKNESS=	3.61
ALLOWABLE STRESS=	236.33	COMPUTED STRESS=	231.78
STRESS RATIO=	1.02		
NO. OF COVERAGES=	2448760.2	STREET PAVEMENT AREA	
DESIGN AXLE LOAD(KIPS)=	32.	ALLOWABLE LOAD=	NOT APPLICABLE
MODULUS OF SUBGRADE REACTION, k (PCI)=	69.3		
EFFECTIVE k (PCI)=	69.3	PCC FLEXURAL STR (PSI)=	675.0
F-FACTOR FOR AC OVERLAY=	.95	CB=	.75
DEFL. RATIO=	.90	CR=	.50
IMPACT FACTOR=	1.00	LOAD REDUCTION FACTOR =	1.000
CONDITION=	POOR	EVALUATION FOR:	INITIAL FAILURE
		CONDITION FACTOR=	.75

ESTIMATED NEW THICKNESS= 9.45

THICKNESS OF LAYER 1 = 9.45

(Sheet 5 of 5)

- a. Page 1 of Table 5 shows the pavement information. Since the computed damage was greater than 1, overlay design was started. The axle load chosen for the overlay design was the 32-kip No. 10 axle with an equivalent coverage of 2,448,760. The design overlay thicknesses are:

Asphalt concrete = 13.4 in.

Concrete, partial-bond = 7.6 in.

Concrete, no-bond = 8.4 in.

- b. Page 2 of Table 5 shows the computed stresses in the 6-in.-thick concrete slab under the three axle loads. The stresses were multiplied by a factor of 1.773 (1.33×1.33) accounting for the edge load effect and poor pavement surface condition. Stresses were not adjusted for joint condition as the input deflection ratio was 0.9.
- c. The remaining part of the table shows results for the selected axle load at different stages of the overlay design iterations. In the first iteration, the thickness of the trial concrete was 10.28 in., resulting in a stress ratio of 1.10. The stress ratio is the ratio of the allowable stress to the computed stress. The concrete thickness was reduced to 9.61 in. with a stress ratio of 1.02. A new concrete thickness of 9.45 in. was thus selected for a stress ratio of 1.0. Overlay thicknesses were computed from overlay equations based on the new concrete thickness of 9.45 in. New concrete thickness is defined as the required concrete thickness on the same subgrade.
- d. Bonded concrete overlay is not allowed for existing concrete slabs which are in poor condition. The required bonded concrete overlay thickness will be the difference {~} between the new concrete thickness and the existing concrete if the latter is in good condition.

Flexible pavement evaluation and overlay design

The existing pavement has the following characteristics and design traffic.

a. Existing pavement:

Asphalt concrete thickness: 4 in.
E modulus of the asphalt concrete: 200,000 psi
Poisson's ratio of the asphalt concrete: 0.35
Interface condition under the asphalt: Total adhesion value of 1.0
Granular base layer thickness: 8 in.
E modulus of the granular layer: 40,000 psi
Poisson's ratio of the granular layer: 0.35
Interface condition under the granular layer: Total adhesion of 1.0
E modulus of the subgrade: 10,000 psi
Poisson's ratio of the subgrade: 0.4
Complete output: Yes
Surface condition: Poor
Overlay design: Yes

b. Traffic:

20,000,000 operations of No. 4 axle load, 18 kips

After INPAVE is run, the input file EXAMPF1.INP is created as shown in Table 6. After WESROAD is run, the output is stored in EXAMPF1.OUT as shown in Table 7. Table 7 shows that the required asphalt concrete overlay thickness is 7.0 in.

Table 6
Input File of WESROAD for Flexible Pavement, EXAMPF1.INP

```

NO. OF PROBLEMS
*****
1

TITLE
*****
ROAD EVALUATION AND OVERLAY DESIGN, FLEXIBLE PAVEMENT
PAVEMENT TYPE          PAVEMENT          CONDITION    COMPUTE OVERLAYS
R=RIG/F=FLEX/C=COMP    G=GOOD/P=POOR    Y=YES,N=NO
*****
'F'                    'R'                    'P'                    'Y'
NO. OF LAYERS          LAYER FOR SURFACE CRITERIA  LAYER FOR SUBGRADE CRITERIA
*****
3                      1                      3
TYPE  FROST CODE      E, PSI      THICK, IN  NU  SLIP
****  *****
1      0      200000.    4.0      .35  1.
5      0      40000.    8.0      .35  1.
6      0      10000.    .40      .40  0.
*****RIGID & COMPOSITE PAVEMENTS ONLY*****
COMPLETE * PCC      JOINT      I=INIT FAILURE * OVERLAYS ONLY *
OUTPUT   * FLEX STR  DEFL RATIO E=EXT TRAFFIC * CB      CR      *
*****
'Y'      -----
NO. OF AXLES CONSIDERED
*****
1
AXLE      AXLE      AXLE      AXLE
CODE      LOAD, KIPS  OPERATIONS  COVERAGES
*****
4          18.0      .200000E+08 .757576E+07

```

Table 7
Output File for WESROAD for Flexible Pavement, EXAMPF1.OUT

 *****"WESPAVE" VERSION DRA-09.89.12*****
 *****EXECUTED: 11-19-1991 @ 14: 8*****

PROBLEM NUMBER 1

ROAD EVALUATION AND OVERLAY DESIGN, FLEXIBLE PAVEMENT

PAVEMENT INPUT PARAMETERS

LAYER NO	MATERIAL TYPE	FROST CODE	MODULUS, PSI NDT	FROST	THICK. IN.	POIS RAT.	SLIP VALUE
1	AC	0	200000.	200000.	4.00	.35	1.
2	BASE OR SUBBASE	0	40000.	40000.	8.00	.35	1.
3	SUBGRADE	0	10000.	10000.	10.00	.40	1.
4	SUBGRADE	0	10000.	10000.	10.00	.40	
5	SUBGRADE	0	10000.	10000. SEMI-INF		.40	

PAVEMENT EVALUATION SUMMARY
 (ALLOWABLE LOAD NOT APPLICABLE)

DESIGN AXLE ID	LOAD, KIPS	COVERAGE LEVEL	ALLOW- LOAD KIPS	ALLOWABLE COVERAGES OF DESIGN AXLE	REQ'D OVERLAY, IN.
4	18.0	7575760.			7.0

(Sheet 1 of 4)

Table 7 (Continued)

BLIST FOR PROBLEM NUMBER 1

04:VEHICLE-PNEUM SA-DW 10-20

*****STRAINS FROM WES-5*****

EVALUATION POSITION *****	X, IN. *****	Y, IN. *****	ADJUSTED VERTICAL STRAIN AT TOP OF SUBGRADE, IN/IN *****	DEPTH, IN. *****	ADJUSTED RADIAL STRAIN AT BOTTOM OF AC LAYER, IN/IN *****	DEPTH, IN. *****
1	6.8	.0	.9885038E-03	12.00	.3238798E-03	4.00
2	13.5	.0	.9432652E-03	12.00	.4011891E-03	4.00

STRAINS HAVE BEEN MULTIPLIED BY 1.333

FLEXIBLE PAVEMENT EVALUATION

LAYER 1 THICKNESS= 4.00 OVERLAY THICKNESS= .00
ALLOWABLE ASPHALT STRAIN= .216E-03 COMPUTED STRAIN= .401E-03
ASPHALT STRAIN RATIO= .54
ALLOWABLE SUBGRADE STRAIN= .420E-03 COMPUTED STRAIN= .989E-03
SUBGRADE STRAIN RATIO= .43
NO. OF COVERAGES= 7575760.0 ROAD PAVEMENT AREA
DESIGN AXLE LOAD(KIPS)= 18. ALLOWABLE LOAD=NOT APPLICABLE
CALCULATED SUBGRADE CBR= 6.7 IMPACT FACTOR= 1.00
CONDITION= POOR CONDITION FACTOR= .75

MINIMUM RATIO= .43

04:VEHICLE-PNEUM SA-DW 10-20

*****STRAINS FROM WES-5*****

EVALUATION POSITION *****	X, IN. *****	Y, IN. *****	ADJUSTED VERTICAL STRAIN AT TOP OF SUBGRADE, IN/IN *****	DEPTH, IN. *****	ADJUSTED RADIAL STRAIN AT BOTTOM OF AC LAYER, IN/IN *****	DEPTH, IN. *****
1	6.8	.0	.4963186E-03	17.41	.2092720E-03	9.41

(Sheet 2 of 4)

Table 7 (Continued)

2 13.5 .0 .4614246E-03 17.41 .2044041E-03 9.41

STRAINS HAVE BEEN MULTIPLIED BY 1.333

FLEXIBLE PAVEMENT EVALUATION

LAYER 1 THICKNESS= 9.41 OVERLAY THICKNESS= 5.41
ALLOWABLE ASPHALT STRAIN= .216E-03 COMPUTED STRAIN= .209E-03
ASPHALT STRAIN RATIO= 1.03
ALLOWABLE SUBGRADE STRAIN= .420E-03 COMPUTED STRAIN= .496E-03
SUBGRADE STRAIN RATIO= .85
NO. OF COVERAGES= 7575760.0 ROAD PAVEMENT AREA
DESIGN AXLE LOAD(KIPS)= 18. ALLOWABLE LOAD=NOT APPLICABLE
CALCULATED SUBGRADE CBR= 6.7 IMPACT FACTOR= 1.00
CONDITION= POOR CONDITION FACTOR= .75

MINIMUM RATIO= .85

ESTIMATED THICKNESS TO MEET ASPHALT CRITERIA= 9.14
ESTIMATED THICKNESS TO MEET SUBGRADE CRITERIA= 10.72

MAXIMUM ESTIMATED THICKNESS= 10.72

04:VEHICLE-PNEUM SA-DW 10-20

*****STRAINS FROM WES-5*****

EVALUATION POSITION	X, IN.	Y, IN.	ADJUSTED VERTICAL STRAIN AT TOP OF SUBGRADE, IN/IN	DEPTH, IN.	ADJUSTED RADIAL STRAIN AT BOTTOM OF AC LAYER, IN/IN	DEPTH IN.
*****	*****	*****	*****	*****	*****	*****
1	6.8	.0	.4318432E-03	18.72	.1836207E-03	10.72
2	13.5	.0	.4031153E-03	18.72	.1767300E-03	10.72

STRAINS HAVE BEEN MULTIPLIED BY 1.333

FLEXIBLE PAVEMENT EVALUATION

LAYER 1 THICKNESS= 10.72 OVERLAY THICKNESS= 6.72
ALLOWABLE ASPHALT STRAIN= .216E-03 COMPUTED STRAIN= .184E-03
ASPHALT STRAIN RATIO= 1.18
ALLOWABLE SUBGRADE STRAIN= .420E-03 COMPUTED STRAIN= .432E-03
SUBGRADE STRAIN RATIO= .97
NO. OF COVERAGES= 7575760.0 ROAD PAVEMENT AREA
DESIGN AXLE LOAD(KIPS)= 18. ALLOWABLE LOAD=NOT APPLICABLE
CALCULATED SUBGRADE CBR= 6.7 IMPACT FACTOR= 1.00

(Sheet 3 of 4)

Table 7 (Concluded)

CONDITION= POOR CONDITION FACTOR= .75
MINIMUM RATIO= .97
ESTIMATED THICKNESS TO MEET ASPHALT CRITERIA= 9.09
ESTIMATED THICKNESS TO MEET SUBGRADE CRITERIA= 10.98
MAXIMUM ESTIMATED THICKNESS= 10.98

THICKNESS OF LAYER 1 = 10.98

(Sheet 4 of 4)

5 Recommendations

Computer program WESROAD should be used for the evaluation and overlay design of roads, streets, and open storage areas that have been evaluated using the NDT method. Computer program WESLEA is used for computing pavement stresses and strains. Although the programs are user-friendly, this report will be beneficial for users when questions arise. To ensure the correctness of the computer run, first-time users should run the programs using the input data provided in the example problem and check the computer results with those provided in Tables 2-7.

REPORT DOCUMENTATION PAGEForm Approved
OMB No. 0704-0188

Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.

1. AGENCY USE ONLY (Leave blank)

2. REPORT DATE

January 1994

3. REPORT TYPE AND DATES COVERED

Final report

4. TITLE AND SUBTITLE

A Computer Program for Evaluation and Overlay Design of Roads,
Streets, and Open Storage Areas Using Nondestructive
Testing and Elastic Layered Method - WESROAD

5. FUNDING NUMBERS

6. AUTHOR(S)

Yu T. Chou

7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES)

U.S. Army Engineer Waterways Experiment Station
Geotechnical Laboratory
3909 Halls Ferry Road, Vicksburg, MS 39180-6199

8. PERFORMING ORGANIZATION
REPORT NUMBER

Miscellaneous Paper
GL-94-2

9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES)

U.S. Army Corps of Engineers
Washington, DC 20314-1000

10. SPONSORING / MONITORING
AGENCY REPORT NUMBER

11. SUPPLEMENTARY NOTES

Available from National Technical Information Service, 5285 Port Royal Road, Springfield, VA 22161.

12a. DISTRIBUTION / AVAILABILITY STATEMENT

Approved for public release; distribution is unlimited.

12b. DISTRIBUTION CODE

13. ABSTRACT (Maximum 200 words)

A user-friendly computer program, WESROAD, is presented for the evaluation and overlay design of roads, streets, and open storage areas using the elastic layered method. The program is designed to operate on an IBM or compatible machine under the DOS 3.0 operating system or a later system. This report provides users with necessary information for running WESROAD, including the programming logic, computer system requirements, user instructions, and the input and output of an example problem. The pavements to be evaluated include flexible, concrete, and composite (asphalt over concrete) pavements. The overlay design includes flexible and concrete overlays.

14. SUBJECT TERMS

Pavements--Overlays--Data processing

WESROAD (Computer program)

Roads--Design and construction--Data processing

15. NUMBER OF PAGES

30

16. PRICE CODE

17. SECURITY CLASSIFICATION
OF REPORT

UNCLASSIFIED

18. SECURITY CLASSIFICATION
OF THIS PAGE

UNCLASSIFIED

19. SECURITY CLASSIFICATION
OF ABSTRACT

20. LIMITATION OF ABSTRACT