

AD-A279 338



**Spatial Contrast Sensitivity
Through Aviator's Night Vision Imaging System
(Reprint)**

By

Jeff Rabin

Aircrew Health and Performance Division

DTIC
ELECTE
MAY 18 1994
S G D

94-14820



404 578

DTIC QUALITY ASSURED 6

April 1994

94 5 17 102

Approved for public release; distribution unlimited.

**United States Army Aeromedical Research Laboratory
Fort Rucker, Alabama 36362-0577**

Notice

Qualified requesters

Qualified requesters may obtain copies from the Defense Technical Information Center (DTIC), Cameron Station, Alexandria, Virginia 22314. Orders will be expedited if placed through the librarian or other person designated to request documents from DTIC.

Change of address

Organizations receiving reports from the U.S. Army Aeromedical Research Laboratory on automatic mailing lists should confirm correct address when corresponding about laboratory reports.

Disposition

Destroy this document when it is no longer needed. Do not return it to the originator.

Disclaimer

The views, opinions, and/or findings contained in this report are those of the author(s) and should not be construed as an official Department of the Army position, policy, or decision, unless so designated by other official documentation. Citation of trade names in this report does not constitute an official Department of the Army endorsement or approval of the use of such commercial items.

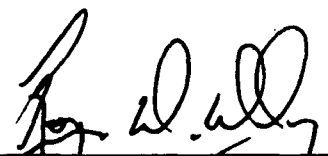
Human use

Human subjects participated in these studies after giving their free and informed voluntary consent. Investigators adhered to AR 70-25 and USAMRDC Reg 70-25 on Use of Volunteers in Research.

Reviewed:


RICHARD R. LEVINE
LTC, MS
Director, Aircrew Health and Performance Division

Released for publication:


ROGER W. WFLEY, O.D., Ph.D.
Chairman, Scientific
Review Committee


DAVID H. KARNEY
Colonel, MC, SFS
Commanding

REPORT DOCUMENTATION PAGE

Form Approved
OMB No. 0704-0188

1a. REPORT SECURITY CLASSIFICATION Unclassified			1b. RESTRICTIVE MARKINGS		
2a. SECURITY CLASSIFICATION AUTHORITY			3. DISTRIBUTION/AVAILABILITY OF REPORT Approved for public release; distribution unlimited		
2b. DECLASSIFICATION/DOWNGRADING SCHEDULE					
4. PERFORMING ORGANIZATION REPORT NUMBER(S) USAARL Report No. 94-19			5. MONITORING ORGANIZATION REPORT NUMBER(S)		
6a. NAME OF PERFORMING ORGANIZATION U.S. Army Aeromedical Research Laboratory		6b. OFFICE SYMBOL (if applicable) SGRD-UAS-VS		7a. NAME OF MONITORING ORGANIZATION U.S. Army Medical Research, Development, Acquisition and Logistics Command (Provisional)	
6c. ADDRESS (City, State, and ZIP Code) P.O. Box 620577 Ft. Rucker, AL 36362-0577		7b. ADDRESS (City, State, and ZIP Code) Fort Detrick Frederick, MD 21702-5012			
8a. NAME OF FUNDING/SPONSORING ORGANIZATION		8b. OFFICE SYMBOL (if applicable)		9. PROCUREMENT INSTRUMENT IDENTIFICATION NUMBER	
8c. ADDRESS (City, State, and ZIP Code)		10. SOURCE OF FUNDING NUMBERS			
		PROGRAM ELEMENT NO. 0602787A		PROJECT NO. 3M16278 7A879	
		TASK NO. PE		WORK UNIT ACCESSION NO. 164	
11. TITLE (Include Security Classification) (U) Spatial Contrast Sensitivity Through Aviator's Night Vision Imaging System					
12. PERSONAL AUTHOR(S) Jeff Rabin					
13a. TYPE OF REPORT Final		13b. TIME COVERED FROM _____ TO _____		14. DATE OF REPORT (Year, Month, Day) 1994 April	
15. PAGE COUNT 5					
16. SUPPLEMENTARY NOTATION Printed in Aviation, Space, and Environmental Medicine, August 1993, pages 706-710					
17. COSATI CODES			18. SUBJECT TERMS (Continue on reverse if necessary and identify by block number)		
FIELD	GROUP	SUB-GROUP	Spatial contrast sensitivity, night vision devices, night vision goggles		
17	05				
14	04				
19. ABSTRACT (Continue on reverse if necessary and identify by block number)					
Visual acuity is often used to assess vision through image intensifying devices such as night vision goggles (NVG). Fewer attempts have been made to measure contrast sensitivity through NVGs. Such information would be useful to better understand contrast processing through NVGs under various stimulus conditions. In this study, computer-generated letter charts were used to measure contrast sensitivity through third generation NVGs for a range of letter sizes. The red phosphor of a standard color monitor proved to be an effective stimulus for third generation devices. Different night sky conditions were simulated over a 3 log unit range. The results illustrate the profile of contrast sensitivity through third generation NVGs over a range of night sky conditions. Comparison of measurements through NVGs to measurements obtained without the device but at the same luminance and color distinguish between effects of luminance and noise on contrast sensitivity.					
20. DISTRIBUTION/AVAILABILITY OF ABSTRACT ☒ UNCLASSIFIED/UNLIMITED ☐ SAME AS RPT. ☐ DTIC USERS			21. ABSTRACT SECURITY CLASSIFICATION Unclassified		
22a. NAME OF RESPONSIBLE INDIVIDUAL Chief, Scientific Information Center			22b. TELEPHONE (Include Area Code) (205) 255-6907		22c. OFFICE SYMBOL SGRD-IAS-VS

Spatial Contrast Sensitivity Through Aviator's Night Vision Imaging System

JEFF RABIN, O.D., Ph.D.

Accession For	
NTIS	CRA&I ☒
DTIC	TAB ☐
Unannounced	☐
Justification	
By _____	
Distribution /	
Availability Codes	
Dist	Avail and/or Special
A-1	20

RABIN J. *Spatial contrast sensitivity through Aviator's Night Vision Imaging System*. Aviat. Space Environ. Med. 1993; 64:706-10.

Visual acuity is often used to assess vision through image intensifying devices such as night vision goggles (NVG's). Fewer attempts have been made to measure contrast sensitivity through NVG's. Such information would be useful to better understand contrast processing through NVG's under various stimulus conditions. In this study, computer-generated letter charts were used to measure contrast sensitivity through third generation NVG's for a range of letter sizes. The red phosphor of a standard color monitor proved to be an effective stimulus for third generation devices. Different night sky conditions were simulated over a 3 log unit range. The results illustrate the profile of contrast sensitivity through third generation NVG's over a range of night sky conditions. Comparison of measurements through NVG's to measurements obtained without the device but at the same luminance and color distinguish between effects of luminance and noise on contrast sensitivity.

VISUAL ACUITY has been used extensively to evaluate and to describe vision through image intensifying devices (night vision goggles). These studies determined the resolution limit of night vision devices under various conditions of ambient illumination and contrast (5,6,10,14). Fewer attempts have been made to measure contrast sensitivity through image intensifying devices. Such information would be useful since acuity provides only the limit of resolution, while contrast sensitivity can provide a more comprehensive index of visual function over a range of stimulus sizes. Wiley and Holly (15) used sinusoidal gratings to measure contrast sensitivity through second generation image intensifiers over a range of spatial frequencies. Their results defined the limits of human contrast sensitivity for a range of night sky conditions.

It has been technically more difficult to quantify contrast to third generation image intensifiers. This is because third generation devices have a spectral sensitivity in the near infrared, which is largely outside the

visual range. Thus, one must have quantitative control over intensity and intensity differences (contrast) in the near infrared (600-900 nm) to activate third generation devices with meaningful stimuli. In a recent study of visual acuity Kotulak and Rash (5) provided an effective stimulus to third generation devices by using a light source with spectral characteristics which simulated different night sky conditions.

In the present study a simpler approach was used to measure contrast sensitivity through third generation image intensifiers contained in the Aviator's Night Vision Imaging System (ANVIS). The red phosphor of a standard color monitor provided a spectrally narrow stimulus within the ANVIS sensitivity range. Computer-generated charts consisting of letters of different contrasts were used to measure contrast sensitivity through ANVIS over a range of letter sizes. Neutral density filters were used to produce larger changes in intensity to ANVIS to simulate different night sky conditions over a 3 log unit range. The results provide an index of contrast sensitivity through ANVIS over a range of night sky conditions. In addition, measurements through ANVIS were compared to measurements obtained without the device, but at the same luminance and chromaticity. Regression equations were derived from these data to estimate effects of luminance and noise on contrast sensitivity through ANVIS.

METHODS

The stimuli for measuring contrast sensitivity through ANVIS were letter charts software-generated on a VGA color monitor. Only the red phosphor of the monitor was used to limit the spectral composition of the stimuli to the spectral range of ANVIS. Although ANVIS has maximal sensitivity in the near infrared (750 nm), little infrared radiation is emitted by the red gun of the color phosphor (P22) such that its output between 600-720 nm constitutes the primary stimulus for ANVIS. Because neutral density (ND) filters are fairly flat over this spectral range, it was possible to introduce large reductions in monitor intensity with ND filters. Smaller intensity

From the Sensory Research Division, U.S. Army Aeromedical Research Laboratory, Fort Rucker, AL.

This manuscript was received for review in November 1992 and accepted for publication December 1992.

Address reprint requests to: MAJ Jeff Rabin, USAARL, Attn: SGDR-UAS-VS, P.O. Box 620577, Ft. Rucker, AL 36362-0577.

CONTRAST SENSITIVITY & ANVIS—RABIN

differences necessary to generate letters of different contrast were produced by software control.

The letter charts were patterned after the Pelli-Robson contrast sensitivity chart (8). This chart consists of letters of constant size but progressively lower contrast as one reads down the chart. The measurement is designed to provide an index of sensitivity for spatial frequencies near the peak of the contrast sensitivity function. In the present study, a series of four charts was generated, each consisting of letters which differed by a $2\times$ factor in size. Assuming that recognition of letters at threshold depends primarily on spatial frequencies of 1.5–2.5 cycles/letter (4), then the dominant spatial frequencies of the four letter charts used in this study were 0.5, 1.0, 2.0, and 4.0 cycles/degree at a test distance of 40 cm. Each chart consisted of six rows of letters with five letters per row. Due to the larger size of the 0.5 cycle/degree letters, only three letters were included in each row. Contrast was varied by altering the intensity of the letter by software control, while the background was held constant at the maximum level used (letters portrayed as decrements relative to a fixed background). Contrast was computed using the Michelson (7) equation, defined as the luminance difference between letter and background over the sum of these values, and decreased in $2\times$ steps from 64% at the top of each chart down to 2% at the bottom. Photometric measurements of the ANVIS display in response to software-controlled steps in monitor intensity revealed excellent agreement between changes in monitor luminance and ANVIS display luminance. Thus, for uniform field stimulation, differences produced by software control of the stimulus produced equivalent differences in the ANVIS display luminance.

ND filters were used to introduce larger changes in effective stimulation to ANVIS in order to simulate different night sky conditions. The irradiance of the night sky in the spectral range of ANVIS (600–900 nm) decreases by approximately 3 log units between full moon and overcast starlight conditions (5,9). To simulate this reduction in effective stimulation to ANVIS with decreasing night sky illumination, measurements were obtained with 0, 1, 2, and 3 log units of stimulus attenuation relative to the full moon condition. These four conditions were designated full moon, $\frac{1}{4}$ moon, starlight, and overcast. The amount of monitor attenuation (3.5 log units) necessary to achieve full moon stimulation was determined by several criteria. First, the luminance of the stimulus to ANVIS (0.01 cd/m^2) was equal to the value specified for night sky luminance under full moon conditions (5,9). Second, photometric measurement of the ANVIS display with different amounts of stimulus ND attenuation revealed an intensity range over which the ANVIS display luminance remained constant and then began to drop with further decrements in stimulus intensity. This eventual decline in ANVIS display luminance presumably reflects the point at which the automatic gain control of the device stops operating. Inspection of the display with small increases in intensity (0.1 log steps) above this point revealed a second region at which visual noise (scintillations) appeared minimized, and further increases in intensity revealed no further improvement in perceived image qual-

ity. This, again, corresponded to 3.5 log unit attenuation of the red screen producing a stimulus with a luminance of 0.01 cd/m^2 . This condition corresponded to our simulation of full moon illumination.

Contrast sensitivity was measured at a distance of 40 cm from the monitor to the halfway point of the ANVIS tube. All measurements were performed monocularly using the subject's right eye and the right tube of a binocular ANVIS mounted on a table. The left tube was occluded. Except for the monitor, all sources of illumination were extinguished, and the monitor intensity was reduced by placing ND filters in a filter holder directly against the objective side of the ANVIS tube. The tube was initially focused by the experimenter, and then rechecked for each subject by inspection of a small patch of vertical square wave grating centered in the monitor screen. Each chart was then displayed at the full moon condition, and the subject was asked to read as far down as possible. Guessing was encouraged and the subject was advised to take ample time to perform each letter recognition (3). The measurements were then repeated with 1, 2, and 3 log units of stimulus attenuation corresponding to our simulation of $\frac{1}{4}$ moon, starlight, and overcast conditions. Scoring was performed by letter in log contrast sensitivity units (1). Because there were 5 letters per row, and each row changed by 0.3 log units, each letter represented $0.3/5 = 0.06$ log units contrast sensitivity. The largest letters had only three letters per row making each letter worth 0.1 log units. Five subjects (age 21–40; mean = 29.5 years) with normal vision and visual acuity corrected to 20/20 participated in this study.

In separate sessions, contrast sensitivity was measured on the same subjects with a stimulus that simulated the ANVIS display at each night sky condition. The same charts were used, but modulated in contrast using only the green phosphor of the color monitor to simulate the green phosphor of the ANVIS display. To determine the display luminance for each night sky condition to use in the simulation, the luminance of the ANVIS display was measured over a range of intensities produced with a series of ND filters. As noted above, this revealed a region at which the display luminance was initially constant (measured as 1.8 fL) and then declined as the automatic gain control stopped functioning. The relation between log ANVIS luminance and ND filter attenuation is shown in Fig. 1 for decreasing portion of the curve. The simple linear equation derived from these data enabled us to estimate the display luminance for each night sky simulation (1.8, 1.2, 0.2, and 0.03 fL for full moon, $\frac{1}{4}$ moon, starlight, and overcast conditions, respectively), and these values were used to simulate the ANVIS display under each condition. Contrast sensitivity was measured on each subject under these simulated conditions in the same manner described for the ANVIS measurements.

RESULTS

In this study spatial contrast sensitivity was measured as a function of letter size, night sky illumination level, and viewing condition (ANVIS vs. simulation). A repeated-measures three-way analysis of variance re-

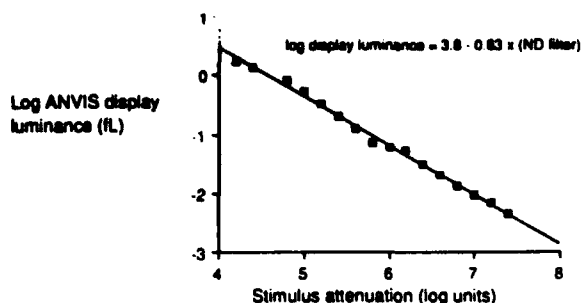


Fig. 1. Photometric measurements of ANVIS display luminance are plotted against log stimulus attenuation produced with ND filters of different amounts. The regression equation allowed us to estimate display luminance for simulated night sky conditions which encompassed 3 log unit range.

revealed significant main effects of letter size ($F_{3,64} = 122.64$, $p < 0.0001$), night sky ($F_{3,64} = 206.96$, $p < 0.0001$), and viewing condition ($F_{1,64} = 595.54$, $p < 0.0001$), and a significant interaction between letter size and night sky for the ANVIS condition ($F_{9,64} = 6.42$, $p < 0.0001$). We will first consider contrast sensitivity through ANVIS, and how it depends on letter size and night sky. ANVIS measurements will then be quantitatively compared to simulated ANVIS measurements to estimate effects of display luminance and electro-optical noise on contrast sensitivity.

Contrast Sensitivity Through ANVIS

Fig. 2 shows mean (± 1 S.E.) contrast sensitivity plotted against the four dominant spatial frequencies tested. Separate plots are shown for each simulated night sky condition (full moon, $\frac{1}{4}$ moon, starlight, and overcast). As shown in many previous studies (2,11,12,13), contrast sensitivity peaks at moderate frequencies and then declines with increasing spatial frequency. The absence of low spatial frequency attenuation in these plots suggests that recognition of the largest letters depends on both low and moderate spatial frequency components in these letters. Measurements with a spatially less complex stimulus (sinusoidal gratings) would probably show a decline in sensitivity at frequencies < 2 cycles/degree.

In view of problems noted above with describing letters in terms of spatial frequency, the data from Fig. 2

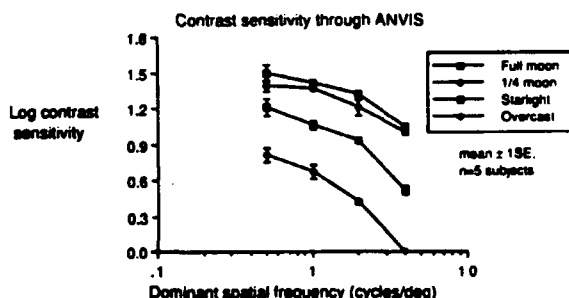


Fig. 2. The mean (± 1 S.E.) log contrast sensitivity is plotted against the dominant spatial frequency of the four letters tested. Separate plots are shown for each night sky condition.

were replotted in Fig. 3 as contrast sensitivity vs. Snellen letter size for each night sky condition. It is of interest that the peak of the function under optimal, full moon conditions (log contrast sensitivity = 1.5) corresponds to a Michelson contrast threshold of about 3.2%. This threshold is 2–3 $\times$ higher than values reported without image intensifying devices (2,3,13). Thus, the best contrast sensitivity through ANVIS is about 2 $\times$ less than one would predict from the assumed luminance and contrast of the ANVIS display. Another important feature illustrated in Fig. 3 is the reduction in contrast sensitivity with decreasing night sky illumination. Similar contrast sensitivity findings have been reported for second generation image intensifiers (15) and for visual acuity through both second and third generation devices (5,6,10,14). The present results complement and extend these findings by showing that contrast sensitivity through ANVIS decreases over a range of letter sizes with decreasing night sky illumination.

Whereas the reduction in contrast sensitivity with decreasing night sky illumination was observed over a range of letter sizes, this effect increases somewhat with spatial frequency (decreasing letter size). Fig. 4 shows mean (± 1 S.E.) contrast sensitivity plotted against the four night sky conditions for the largest (20/1200) and smallest (20/150) letters used in this study. As indicated in this figure, the total reduction in contrast sensitivity with decreasing night sky illumination was greater for the smaller letters (1.1 vs. 0.6 log units), and this difference was significant ($t = 7.32$, $p < 0.005$). Hence, the reduction in contrast sensitivity through ANVIS with decreasing night sky illumination is greater for objects of smaller size.

Noise and Luminance Effects On ANVIS Contrast Sensitivity

To determine factors which govern the decline in ANVIS contrast sensitivity with decreasing night sky illumination, measurements through ANVIS were compared to measurements made without the device, but at the same luminance and chromaticity as the ANVIS display. These comparisons between actual ANVIS contrast sensitivity and simulated ANVIS revealed higher contrast sensitivity in the simulated condition at all night sky illuminations. However, because we were

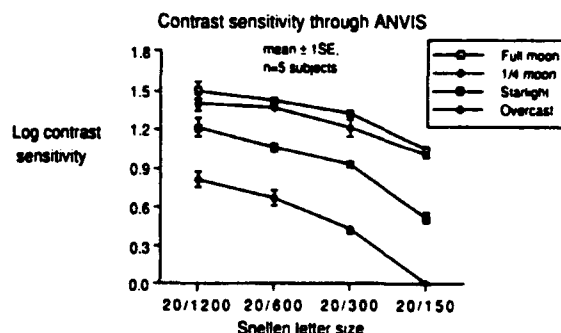


Fig. 3. The mean (± 1 S.E.) log contrast sensitivity is plotted against Snellen letter size for each of the four night sky conditions.

CONTRAST SENSITIVITY & ANVIS—RABIN

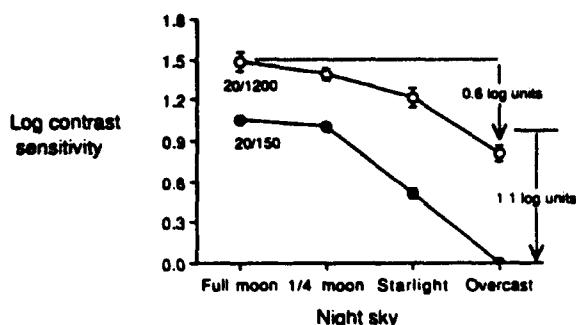


Fig. 4. Mean (± 1 S.E.) log contrast sensitivity is plotted against each night sky condition for the largest (20/1200) and smallest (20/150) letters tested. The total reduction in contrast sensitivity with decreasing night sky illumination is indicated for each letter size (0.6 log units for 20/1200 letters; 1.1 log units for 20/150 letters).

unable to generate contrasts low enough to reliably measure simulated ANVIS thresholds for the larger letters (20/1200 and 20/600), direct quantitative comparisons were not possible in these cases. Our comparisons were thus limited to the 20/300 and 20/150 letters which approximate spatial frequencies of 2–4 cycles/degree. Inasmuch as the simulated thresholds were obtained at the same luminance and chromaticity as ANVIS, any difference between simulated and ANVIS thresholds could not be explained by luminance differences, but could reflect electro-optical "noise." To quantify this noise effect as a function of ambient stimulation, all within-subject contrast sensitivity differences (simulated ANVIS-real ANVIS) for 20/300 and 20/150 letters were plotted as a function of night sky illumination. Different night sky levels were assigned quantitative values of 0, 1, 2, and 3 corresponding to full moon, 1/4 moon, starlight, and overcast conditions. These values are not arbitrary since each corresponds to about 1 log unit difference in stimulation to ANVIS. The least squares linear regression of the difference in contrast sensitivity plotted against night sky is shown in Fig. 5 and described by the relation:

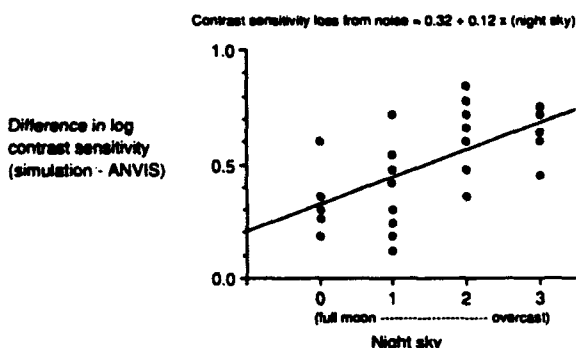


Fig. 5. The within-subject difference in log contrast sensitivity for ANVIS and simulated ANVIS is plotted against night sky illumination where 0, 1, 2, and 3 correspond to full moon, 1/4 moon, starlight, and overcast conditions, respectively. The data are for 20/300 and 20/150 letters. The least squares regression line and equation are shown.

$$\text{Difference in log contrast sensitivity} = 0.32 + 0.12 \times (\text{night sky}) \quad \text{Eq. 1}$$

This regression model is statistically significant ($F_{1,38} = 34.13$, $p < 0.0001$), and accounts for about 50% of the variability in contrast sensitivity differences between the simulated and ANVIS conditions ($r^2 = 0.47$). If we assume that scintillation noise effects are present only at lower light levels (night sky = 1, 2, or 3), then the noise term is given by the product:

$$0.12 \times (\text{night sky}) \quad \text{Eq. 2}$$

and this term drops out under full moon conditions. Nevertheless, the model indicates that even under optimal stimulation to ANVIS there is, on the average, a 0.3 log unit (2 $\times$) difference in contrast sensitivity unexplained by display luminance. Decreasing illumination below optimal levels reduces contrast sensitivity 0.12 log units per log unit reduction in stimulation.

In order to extract the effect of luminance on ANVIS contrast sensitivity, all ANVIS contrast sensitivity values for the letter sizes 20/300 and 20/150 were plotted against night sky stimulation in the manner described above. The best-fitting function to describe this relation was a second order polynomial illustrated in Fig. 6. This model of total contrast sensitivity as a function of ambient illumination was also significant ($F_{2,37} = 85.09$, $p < 0.0001$) accounting for 82% of the variation in ANVIS contrast sensitivity ($r^2 = 0.82$). Because the second coefficient in the polynomial expression was not statistically significant ($p > 0.9$), it was omitted from the equation such that total ANVIS contrast sensitivity is related exponentially to night sky illumination:

$$\text{Total contrast sensitivity} = 1.20 - 0.11 \times (\text{night sky})^2 \quad \text{Eq. 3}$$

Because in our model night sky was zero under full moon conditions, the total loss in contrast sensitivity with decreasing ambient illumination is given by the relation:

$$\text{Total contrast sensitivity loss} = 0.11 \times (\text{night sky})^2 \quad \text{Eq. 4}$$

By subtracting the effect of noise from total contrast

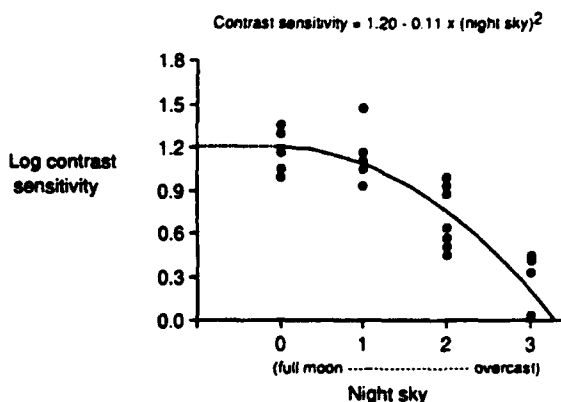


Fig. 6. Log ANVIS contrast sensitivity for 20/300 and 20/150 letters is plotted against night sky condition as described in Fig. 5. The least squares polynomial regression function is shown with the corresponding equation. The second coefficient was omitted since it lacked statistical significance.

CONTRAST SENSITIVITY & ANVIS—RABIN

sensitivity loss at each night sky condition, the influence of decreasing display luminance can be extracted. Table I shows the impact of electro-optical noise and luminance on ANVIS contrast sensitivity for various levels of stimulation.

DISCUSSION

This study illustrates the profile of contrast sensitivity through ANVIS over a range of letter sizes. Maximum contrast sensitivity is about 2× less than sensitivity tested without the device under comparable conditions of stimulation. This suggests that, even under optimal ambient levels of illumination, contrast sensitivity is slightly attenuated through ANVIS over a range of spatial frequencies. Similar findings were reported by Wiley and Holly (15) for second generation image intensifiers, and can also be inferred from inspection of visual acuity measurements through second and third generation devices. The etiology of this small attenuation in contrast sensitivity under optimal stimulus conditions is unclear, but could reflect limiting electrical or optical properties of the device.

Contrast sensitivity decreased substantially with decreasing night sky illumination, and this reduction was observed for a range of letter sizes. These findings are consistent with previous measures of contrast sensitivity through second generation tubes (15), and with visual acuity measurements through second and third generation devices under different night sky conditions (5,6,10,14). While the sensitivity loss with decreased ambient illumination included large letters (lower spatial frequencies), the effect was somewhat greater for smaller letters (higher spatial frequencies).

A comparison of measurements through ANVIS to measurements made without the device at the same luminance and chromaticity revealed consistently lower contrast sensitivity through ANVIS over the range of night sky conditions. Since luminance was equated in the ANVIS and simulation conditions, other factors, such as electro-optical noise, impair contrast detection through ANVIS under reduced levels of illumination. Regression equations were derived from the data to quantify effects of noise and luminance on ANVIS contrast sensitivity. The reduction in sensitivity with decreasing night sky illumination was found to be a com-

bined effect of lower display luminance and increased electro-optical noise. The development of image intensifiers which provide greater display luminance and lower noise at starlight and overcast levels of illumination will improve visual performance and enhance aviation safety. This study provides initial quantitative estimates of the impact of noise and luminance on ANVIS performance under low light levels.

It is noteworthy that the red phosphor of a standard color monitor can be used as an effective stimulus for third generation image intensifiers. Software-controlled steps in phosphor intensity provided quantitative control over contrast to ANVIS. Different night sky conditions were simulated by reducing monitor intensity with neutral density filters. This expedient approach will prove to be a useful tool for further assessment of vision through image intensifying devices in laboratory settings.

REFERENCES

1. Bailey IL, Bullimore MA, Raasch TW, Taylor HR. Clinical grading and the effects of scaling. *Ophthalmol. Vis. Sci.* 1991; 32: 422-32.
2. De Valois RL, De Valois KK. *Spatial Vision*. New York: Oxford University Press, 1988.
3. Elliot DB, Sanderson K, Conkey A. The reliability of the Pelli-Robson contrast sensitivity chart. *Ophthalm. Physiol. Opt.* 1990; 10:21-4.
4. Ginsburg A. Visual information processing based upon spatial filters constrained by biological data. [Dissertation] Cambridge Univ. 1978; Reprinted as AFAMRL Tech. Rep. 78-129, Library of Congress 79-600156.
5. Kotulak JC, Rash CE. Visual acuity with second and third generation night vision goggles obtained from a new method of night sky simulation across a wide range of target contrasts. Fort Rucker, AL: U.S. Army Aeromedical Research Laboratory, 1992; USAARL Report No. 92-9.
6. Levine RR, Rash CE. Attenuating the output of the AN/PVS-5A night vision goggles and its effects on visual acuity. Fort Rucker, AL: U.S. Army Aeromedical Research Laboratory, 1989; USAARL Report No. 89-24.
7. Michelson AA. *Studies in optics*. Chicago: University of Chicago Press, 1927.
8. Pelli DG, Robson JG, Wilkins AJ. The design of a new letter chart for measuring contrast sensitivity. *Clin. Vis. Sci.* 1988; 2:187-99.
9. RCA Electro-Optics Handbook. *Electro-optics handbook technical series EOH-11*. Lancaster: RCA Corp, 1974.
10. Riegler JT, Whiteley JD, Task HL, Schueren J. The effect of signal-to-noise ratio on visual acuity through night vision goggles. Wright-Patterson Air Force Base, OH: Armstrong Laboratory, 1991; AL Report No. AL-TR-91-0011.
11. Robson JG. Spatial and temporal contrast sensitivity functions of the human visual system. *J. Opt. Soc. Am.* 1966; 56:1141-2.
12. Schade OH. Optical and photoelectric analog of the eye. *J. Opt. Soc. Am.* 1956; 46:721-39.
13. Sucs FE, Uvjijs A. Contrast sensitivity in retinitis pigmentosa at different luminance levels. *Vision Res.* 1992; 7:147-51.
14. Wiley RW. Visual acuity and stereopsis with night vision goggles. Fort Rucker, AL: U.S. Army Aeromedical Research Laboratory, 1989; USAARL Report No. 89-9.
15. Wiley RW, Holly FF. Vision with the AN/PVS-5 night vision goggle. Neuilly-sur-Seine, France: AGARD 1976; 191:C7.1-C.12.

TABLE I. EFFECTS OF NOISE AND LUMINANCE ON ANVIS CONTRAST SENSITIVITY.

Night Sky	Reduction in Log Contrast Sensitivity		
	Total	Noise	Luminance
full moon	0.00	0.00	0.00
¼ moon	0.11	0.12	0.00
starlight	0.44	0.24	0.20
overcast	0.99	0.36	0.63

Initial distribution

**Commander, U.S. Army Natick Research,
Development and Engineering Center
ATTN: SATNC-MIL (Documents
Librarian)
Natick, MA 01760-5040**

**Library
Naval Submarine Medical Research Lab
Box 900, Naval Sub Base
Groton, CT 06349-5900**

**Chairman
National Transportation Safety Board
800 Independence Avenue, S.W.
Washington, DC 20594**

**Executive Director, U.S. Army Human
Research and Engineering Directorate
ATTN: Technical Library
Aberdeen Proving Ground, MD 21005**

**Commander
10th Medical Laboratory
ATTN: Audiologist
APO New York 09180**

**Commander
Man-Machine Integration System
Code 602
Naval Air Development Center
Warminster, PA 18974**

**Naval Air Development Center
Technical Information Division
Technical Support Detachment
Warminster, PA 18974**

**Commander
Naval Air Development Center
ATTN: Code 602-B
Warminster, PA 18974**

**Commanding Officer, Naval Medical
Research and Development Command
National Naval Medical Center
Bethesda, MD 20814-5044**

**Commanding Officer
Armstrong Laboratory
Wright-Patterson
Air Force Base, OH 45433-6573**

**Deputy Director, Defense Research
and Engineering
ATTN: Military Assistant
for Medical and Life Sciences
Washington, DC 20301-3080**

**Director
Army Audiology and Speech Center
Walter Reed Army Medical Center
Washington, DC 20307-5001**

**Commander, U.S. Army Research
Institute of Environmental Medicine
Natick, MA 01760**

**Commander/Director
U.S. Army Combat Surveillance
and Target Acquisition Lab
ATTN: SFAE-IEW-JS
Fort Monmouth, NJ 07703-5305**

**Director
Federal Aviation Administration
FAA Technical Center
Atlantic City, NJ 08405**

**Commander, U.S. Army Test
and Evaluation Command
ATTN: AMSTE-AD-H
Aberdeen Proving Ground, MD 21005**

**Naval Air Systems Command
Technical Air Library 950D
Room 278, Jefferson Plaza II
Department of the Navy
Washington, DC 20361**

**Director
U.S. Army Ballistic
Research Laboratory
ATTN: DRXBR-OD-ST Tech Reports
Aberdeen Proving Ground, MD 21005**

**Commander
U.S. Army Medical Research
Institute of Chemical Defense
ATTN: SGRD-UV-AO
Aberdeen Proving Ground,
MD 21010-5425**

**Commander
USAMRDALC
ATTN: SGRD-RMS
Fort Detrick, Frederick, MD 21702-5012**

**Director
Walter Reed Army Institute of Research
Washington, DC 20307-5100**

**HQ DA (DASG-PSP-O)
5109 Leesburg Pike
Falls Church, VA 22041-3258**

**Harry Diamond Laboratories
ATTN: Technical Information Branch
2800 Powder Mill Road
Adelphi, MD 20783-1197**

**U.S. Army Materiel Systems
Analysis Agency
ATTN: AMXSYP-PA (Reports Processing)
Aberdeen Proving Ground
MD 21005-5071**

**U.S. Army Ordnance Center
and School Library
Simpson Hall, Building 3071
Aberdeen Proving Ground, MD 21005**

**U.S. Army Environmental
Hygiene Agency
ATTN: HSHB-MO-A
Aberdeen Proving Ground, MD 21010**

**Technical Library Chemical Research
and Development Center
Aberdeen Proving Ground, MD
21010-5423**

**Commander
U.S. Army Medical Research
Institute of Infectious Disease
ATTN: SGRD-UIZ-C
Fort Detrick, Frederick, MD 21702**

**Director, Biological
Sciences Division
Office of Naval Research
600 North Quincy Street
Arlington, VA 22217**

**Commander
U.S. Army Materiel Command
ATTN: AMCDE-XS
5001 Eisenhower Avenue
Alexandria, VA 22333**

Commandant
U.S. Army Aviation
Logistics School ATTN: ATSQ-TDN
Fort Eustis, VA 23604

Headquarters (ATMD)
U.S. Army Training
and Doctrine Command
ATTN: ATBO-M
Fort Monroe, VA 23651

IAF Liaison Officer for Safety
USAF Safety Agency/SEFF
9750 Avenue G, SE
Kirtland Air Force Base
NM 87117-5671

Naval Aerospace Medical
Institute Library
Building 1953, Code 03L
Pensacola, FL 32508-5600

Command Surgeon
HQ USCENTCOM (CCSG)
U.S. Central Command
MacDill Air Force Base, FL 33608

Air University Library
(AUL/LSE)
Maxwell Air Force Base, AL 36112

U.S. Air Force Institute
of Technology (AFIT/LDEE)
Building 640, Area B
Wright-Patterson
Air Force Base, OH 45433

Henry L. Taylor
Director, Institute of Aviation
University of Illinois-Willard Airport
Savoy, IL 61874

Chief, National Guard Bureau
ATTN: NGB-ARS
Arlington Hall Station
111 South George Mason Drive
Arlington, VA 22204-1382

Commander
U.S. Army Aviation and Troop Command
ATTN: AMSAT-R-ES
4300 Goodfellow Bouvelard
St. Louis, MO 63120-1798

U.S. Army Aviation and Troop Command
Library and Information Center Branch
ATTN: AMSAV-DIL
4300 Goodfellow Boulevard
St. Louis, MO 63120

Federal Aviation Administration
Civil Aeromedical Institute
Library AAM-400A
P.O. Box 25082
Oklahoma City, OK 73125

Commander
U.S. Army Medical Department
and School
ATTN: Library
Fort Sam Houston, TX 78234

Commander
U.S. Army Institute of Surgical Research
ATTN: SGRD-USM
Fort Sam Houston, TX 78234-6200

AAMRL/HEX
Wright-Patterson
Air Force Base, OH 45433

Product Manager
Aviation Life Support Equipment
ATTN: AMCPM-ALSE
4300 Goodfellow Boulevard
St. Louis, MO 63120-1798

Commander and Director
USAE Waterways Experiment Station
ATTN: CEWES-IM-MI-R,
CD Department
3909 Halls Ferry Road
Vicksburg, MS 39180-6199

Commanding Officer
Naval Biodynamics Laboratory
P.O. Box 24907
New Orleans, LA 70189-0407

Assistant Commandant
U.S. Army Field Artillery School
ATTN: Morris Swott Technical Library
Fort Sill, OK 73503-0312

Mr. Peter Seib
Human Engineering Crew Station
Box 266
Westland Helicopters Limited
Yeovil, Somerset BA20 2YB UK

U.S. Army Dugway Proving Ground
Technical Library, Building 5330
Dugway, UT 84022

U.S. Army Yuma Proving Ground
Technical Library
Yuma, AZ 85364

AFFTC Technical Library
6510 TW/TSTL
Edwards Air Force Base,
CA 93523-5000

Commander
Code 3431
Naval Weapons Center
China Lake, CA 93555

Aeromechanics Laboratory
U.S. Army Research and Technical Labs
Ames Research Center, M/S 215-1
Moffett Field, CA 94035

Sixth U.S. Army
ATTN: SMA
Presidio of San Francisco, CA 94129

Commander
U.S. Army Aeromedical Center
Fort Rucker, AL 36362

Strughold Aeromedical Library
Document Service Section
2511 Kennedy Circle
Brooks Air Force Base, TX 78235-5122

Dr. Diane Damos
Department of Human Factors
ISSM, USC
Los Angeles, CA 90089-0021

U.S. Army White Sands
Missile Range
ATTN: STEWS-IM-ST
White Sands Missile Range, NM 88002

U.S. Army Aviation Engineering
Flight Activity
ATTN: SAVTE-M (Tech Lib) Stop 217
Edwards Air Force Base, CA 93523-5000

Ms. Sandra G. Hart
Ames Research Center
MS 262-3
Moffett Field, CA 94035

Commander
USAMRDALC
ATTN: SGRD-UMZ
Fort Detrick, Frederick, MD 21702-5009

Commander
U.S. Army Health Services Command
ATTN: HSOP-SO
Fort Sam Houston, TX 78234-6000

U. S. Army Research Institute
Aviation R&D Activity
ATTN: PERI-IR
Fort Rucker, AL 36362

Commander
U.S. Army Safety Center
Fort Rucker, AL 36362

U.S. Army Aircraft Development
Test Activity
ATTN: STEBG-MP-P
Cairns Army Air Field
Fort Rucker, AL 36362

Commander
USAMRDALC
ATTN: SGRD-PLC (COL R. Gifford)
Fort Detrick, Frederick, MD 21702

TRADOC Aviation LO
Unit 21551, Box A-209-A
APO AE 09777

Netherlands Army Liaison Office
Building 602
Fort Rucker, AL 36362

British Army Liaison Office
Building 602
Fort Rucker, AL 36362

Italian Army Liaison Office
Building 602
Fort Rucker, AL 36362

Directorate of Training Development
Building 502
Fort Rucker, AL 36362

Chief
USAHEL/USAAVNC Field Office
P. O. Box 716
Fort Rucker, AL 36362-5349

Commander, U.S. Army Aviation Center
and Fort Rucker
ATTN: ATZQ-CG
Fort Rucker, AL 36362

Chief
Test & Evaluation Coordinating Board
Cairns Army Air Field
Fort Rucker, AL 36362

Canadian Army Liaison Office
Building 602
Fort Rucker, AL 36362

German Army Liaison Office
Building 602
Fort Rucker, AL 36362

French Army Liaison Office
USAAVNC (Building 602)
Fort Rucker, AL 36362-5021

Australian Army Liaison Office
Building 602
Fort Rucker, AL 36362

Dr. Garrison Rapmund
6 Burning Tree Court
Bethesda, MD 20817

Commandant, Royal Air Force
Institute of Aviation Medicine
Farnborough, Hampshire GU14 6SZ UK

Defense Technical Information
Cameron Station, Building 5
Alexandra, VA 22304-6145

Commander, U.S. Army Foreign Science
and Technology Center
AIFRTA (Davis)
220 7th Street, NE
Charlottesville, VA 22901-5396

Commander
Applied Technology Laboratory
USARTL-ATCOM
ATTN: Library, Building 401
Fort Eustis, VA 23604

Commander, U.S. Air Force
Development Test Center
101 West D Avenue, Suite 117
Eglin Air Force Base, FL 32542-5495

Aviation Medicine Clinic
TMC #22, SAAF
Fort Bragg, NC 28305

Dr. H. Dix Christensen
Bio-Medical Science Building, Room 753
Post Office Box 26901
Oklahoma City, OK 73190

Commander, U.S. Army Missile
Command
Redstone Scientific Information Center
ATTN: AMSMI-RD-CS-R
/ILL Documents
Redstone Arsenal, AL 35898

Director
Army Personnel Research Establishment
Farnborough, Hants GU14 6SZ UK

U.S. Army Research and Technology
Laboratories (AVSCOM)
Propulsion Laboratory MS 302-2
NASA Lewis Research Center
Cleveland, OH 44135

Commander
USAMRDALC
ATTN: SGRD-ZC (COL John F. Glenn)
Fort Detrick, Frederick, MD 21702-5012

Dr. Eugene S. Channing
166 Baughman's Lane
Frederick, MD 21702-4083

U.S. Army Medical Department
and School
USAMRDALC Liaison
ATTN: HSMC-FR
Fort Sam Houston, TX 78234

Dr. A. Kornfield, President
Biosearch Company
3016 Revere Road
Drexel Hill, PA 29026

NVESD
AMSEL-RD-NV-ASID-PST
(Attn: Trang Bui)
10221 Burbeck Road
Fort Belvoir, VA 22060-5806

CA Av Med
HQ DAAC
Middle Wallop
Stockbridge, Hants S020 8DY UK

Dr. Christine Schlichting
Behavioral Sciences Department
Box 900, NAVUBASE NLON
Groton, CT 06349-5900

Commander, HQ AAC/SGPA
Aerospace Medicine Branch
162 Dodd Boulevard, Suite 100
Langley Air Force Base,
VA 23665-1995

Commander
Aviation Applied Technology Directorate
ATTN: AMSAT-R-T
Fort Eustis, VA 23604-5577

Director
Aviation Research, Development
and Engineering Center
ATTN: AMSAT-R-Z
4300 Goodfellow Boulevard
St. Louis, MO 63120-1798

Commander
USAMRDALC
ATTN: SGRD-ZB (COL C. Fred Tyner)
Fort Detrick, Frederick, MD 21702-5012

Director
Directorate of Combat Developments
ATTN: ATZQ-CD
Building 515
Fort Rucker, AL 36362