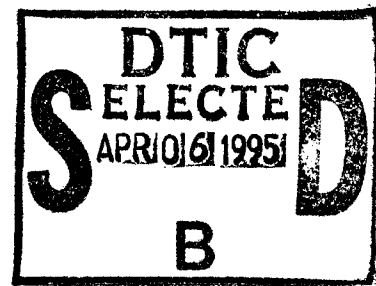




**US Army Corps
of Engineers**
Hydrologic Engineering Center

HEC-6: Reservoir Sediment Control Applications



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HEC-6: RESERVOIR SEDIMENT CONTROL APPLICATIONS¹

Caveat: "... the choice of a model at this time is arbitrary, and the choice of a modeler is probably more important than the choice of a model." (Dawdy and Vanoni 1986)

1. Some History of HEC-6 Development and Applications.² The following list summarizes efforts of the Corps' Waterways Experiment Station (WES) and Hydrologic Engineering Center (HEC) to improve HEC-6. Note that numerous research and project applications of HEC-6 have been performed by other Corps' offices, government agencies, private consultants, universities, and foreign countries that are not reported here.

- ▶ The "Time Sequencing Method" of scour and deposition calculations was developed at the Little Rock District of the Corps of Engineers in 1967 by Tony Thomas; it led to the development of HEC-6. The motivation for that effort was to confirm land acquisition requirements for Ozark Reservoir on the Arkansas River, recognizing potential future (50-year) sedimentation.
- ▶ The next major development to the numerical model that was to become HEC-6 was made at HEC for the Walla Walla District in the early 70's. The need was to predict future water surface elevations for levees at Lewiston ID on Lower Granite Reservoir. The incorporation of bed material sorting and armoring and expansion of the transport of grain sizes up to 64mm was done at this time.
- ▶ First complete documentation published by HEC for "Scour and Deposition in Rivers and Reservoirs", 1973.
- ▶ First HEC "Sediment Transport" training course presented, 1973.
- ▶ The third major development was made in 1974 for the Corps of Engineers' Fort Worth District. They needed to predict future maintenance dredging on the proposed Trinity River Navigation Project which consisted of 22 locks and dams in series. Silt and clay were the dominant sediment classes. The numerical model was modified to handle a system of locks and dams and to transport, deposit, and consolidate clays and silts.
- ▶ Comparison of model results with laboratory flume data published in ASCE Hydraulics Division Journal (Thomas and Prasuhn 1977).

¹ Prepared by D. Michael Gee, Senior Hydraulic Engineer, Hydrologic Engineering Center, 609 2nd St., Davis, California 95616. Published by the Federal Energy Regulatory Commission in *Notes on Sediment Management in Reservoirs: National and International Perspectives*, Edited by Drs. Shou-shan Fan and Gregory Morris, 31 December 1993.

² Contributions to this section by Tony Thomas of the U.S. Army Corps of Engineers Waterways Experiment Station are gratefully acknowledged.

- ▶ Use of the model for analysis of scour of sediment deposits after removal of a dam is demonstrated (HEC, 1977).
- ▶ "Scour and Deposition in Rivers and Reservoirs" is designated as "HEC-6". HEC publishes a user's manual and makes a public release of the model, 1977.
- ▶ The next major development was made for the Walla Walla District in 1978 to deal with a dendritic network of streams. This led to the "Network Version" of HEC-6 developed by WES.
- ▶ Addition of gravel mining capability at HEC, 1980.
- ▶ Addition of graphics using HEC-HGP (Hydraulics Graphics Package), 1980.
- ▶ The next major development was devised for studies of the Toutle and Cowlitz rivers responses to the Mt. St. Helens eruption in 1980. This work was performed for the Corps' Portland District during 1980-1985. Several transport functions were added to the model and the capability of including the effect of high concentrations of fines on the transport of sands using Colby's correction factor was added. A normal depth approximation to supercritical flow was developed. These enhancements were made to the Network Version which was given the name "TABS-1" and became the research version of the model at WES.
- ▶ Publication of HEC Training Document No. 13, "Guidelines for the Calibration and Application of Computer Program HEC-6", 1981. ▶ Application of HEC-6 to the Arkansas River, CO. This included simulation of irrigation diversions and use of HEC-DSS for hydrologic data management (Gee 1983).
- ▶ Release by HEC of a microcomputer (PC) version of HEC-6, 1985.
- ▶ Addition of cohesive sediment erosion algorithms. This was initially made to TABS-1 for Vicksburg District studies of the Red River Navigation Project in 1986.
- ▶ Implementation of a commercial vendor system by HEC for software distribution and support outside of the Federal Government, 1988.
- ▶ The next major development of TABS-1 was made for studies of the Richard B. Russell Reservoir pump-back hydropower project by the Savannah District. This modification changed geometry files from sequential storage to random access storage.
- ▶ A major enhancement was made to TABS-1 for dredging studies in the lower Mississippi River for the New Orleans District in 1991. The rate of dredging could be prescribed as well as the location of the out-fall discharge.
- ▶ Documentation and public release of a network version, based on TABS-1, of HEC-6 by HEC, 1991.
- ▶ Major update of TD-13, 1992.
- ▶ Update of user's manual, 1993.

- ▶ Ongoing work at WES with TABS-1 involves coupling of the sediment transport algorithms with the UNET unsteady flow program. It is planned to include the results of this work in the HEC NexGen River Analysis System currently undergoing design and development.

2. HEC-6 Description.

HEC-6 (HEC 1991) is a one-dimensional movable boundary open channel flow and sediment movement model designed to simulate changes in river profiles due to scour and deposition over fairly long time periods (typically years, although applications to single flood events are possible). The continuous flow record is broken into a sequence of steady flows of variable discharge and duration (see Figure 1). For each flow a water surface profile is calculated (using steady flow standard-step backwater computations) thereby providing energy slope, velocity, depth, etc. at each cross section. Potential sediment transport rates are then computed at each section for the given bed material grain size distribution. These rates, combined with the duration of the flow allow for a volumetric accounting of sediment for each reach. The amount of scour or deposition at each section is then computed and the cross section shape adjusted accordingly (Figure 2). The computations then proceed to the next flow in the sequence and the computation cycle is repeated beginning with the updated geometry. The sediment calculations are performed by grain size fraction thereby allowing for the simulation of hydraulic sorting and armoring. Features of the model include: capability to analyze networks of streams (Figure 3), automatic channel dredging, various levee and encroachment options, and several options for computation of sediment transport rates.

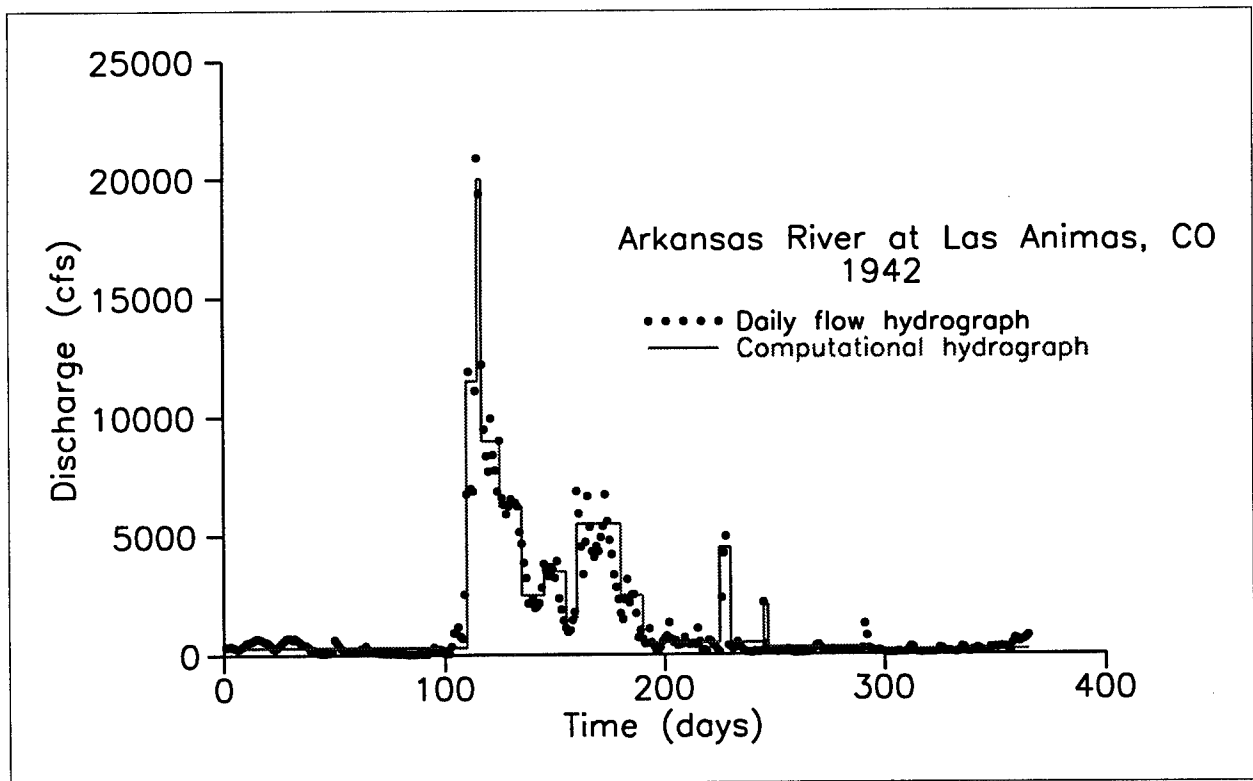


Figure 1 Flow Data Compression

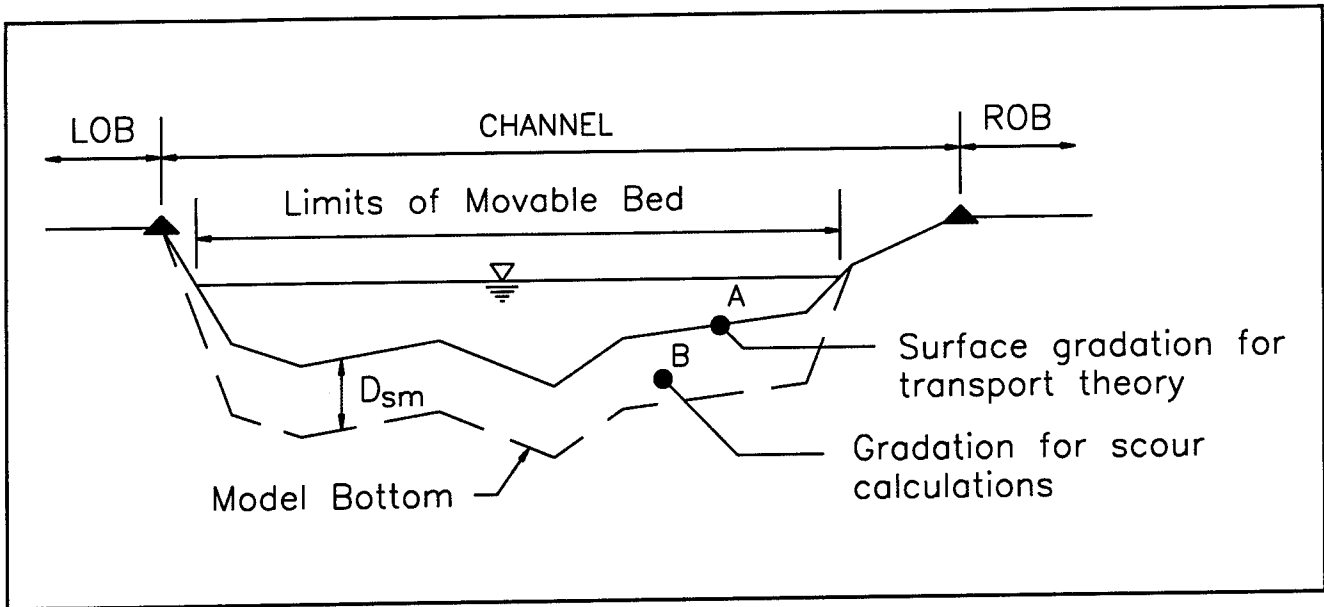


Figure 2 HEC-6 Cross Section Adjustment

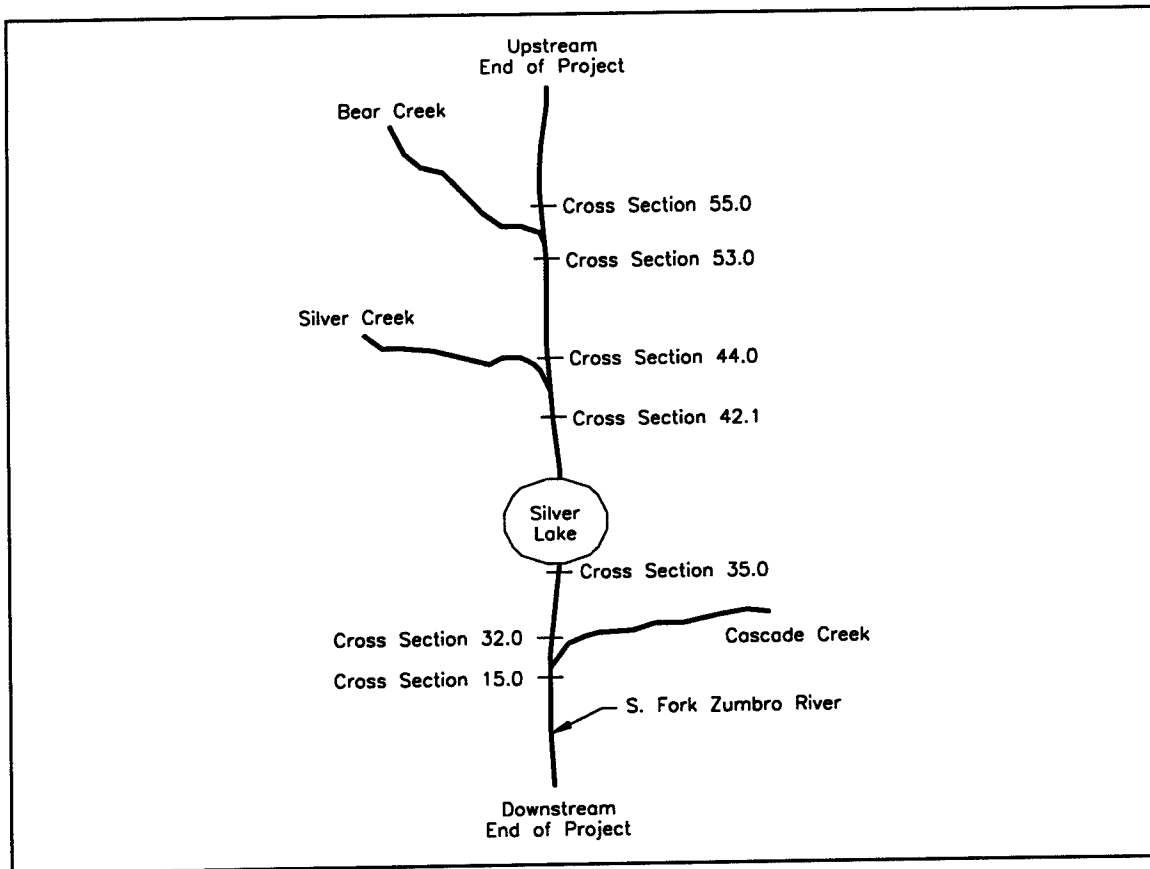


Figure 3 Example Stream System Network

HEC-6 (HEC 1991) is a movable boundary model. It was formulated around Einstein's basic concepts (Einstein 1950) of sediment transport; however, it is designed for the non-equilibrium case. Einstein did not address the non-equilibrium condition, but his "particle exchange" concept was extended in HEC-6 by noting that when sediment is in transport there will be a continual exchange between particles in motion and particles on the bed surface. The residue in the bed may be measurable, as in the case of the "bed material load", or it may be unmeasurable, as in the case of "wash load". The stability of particles on the bed surface may be related to inertia, as in the case of non-cohesive particles; or that stability may be primarily electrochemical, as in the case of cohesive particles. Energy forces acting to entrain a particle may be primarily gravity induced, as in the case of flow in inland rivers; or the forces may be combinations of energy sources such as gravity, tides, waves, and density currents, as in the coastal zone. Different types of sediment require different entrainment functions depending upon the propensity of the sediment to change hydrodynamic and physical properties of the flow and upon the sensitivity of the sediment type to water temperature and chemistry.

a. Equations of flow. The equations for conservation of energy and water mass are simplified by eliminating the time derivative from the motion equation which leaves the gradually varied steady flow equation. It is solved using the standard-step method for water surface profiles. The following terms are included:

$$\frac{\partial h}{\partial x} + \frac{\partial(\alpha U^2/2g)}{\partial x} = S_e \quad \text{(conservation of energy) (1)}$$

where

g	=	acceleration due to gravity
h	=	water surface elevation
S _e	=	slope of energy line
U	=	flow velocity
x	=	distance in the direction of flow
α	=	correction for transverse distribution of flow velocity

$$Q = UA + Q_1 \quad \text{(conservation of water) (2)}$$

where

A	=	cross-sectional area of flow
Q ₁	=	lateral or tributary inflow
Q	=	main stem water discharge downstream from Q ₁
U	=	main stem mean water velocity upstream from Q ₁

b. Friction and form losses. Both friction and form losses are included in S_e; bed roughness is prescribed with Manning *n* values. *n* values may vary with water discharge, location, or be related to bed material size (Limerinos 1970).

c. Equation of sediment continuity. The Exner equation is used for conservation of sediment:

$$\frac{\partial Q_s}{\partial x} + B_s \frac{\partial Y_s}{\partial t} - q_s = 0 \quad \text{(conservation of sediment) (3)}$$

where

B_s	=	width of bed sediment control volume
Q_s	=	volumetric sediment discharge rate
q_s	=	lateral or tributary sediment discharge rate
t	=	time
Y_s	=	bed surface elevation

d. Equation of sediment transport. Einstein's (Einstein 1950) work is definitive and presents a complete view of the processes of equilibrium sediment transportation; it, however, has been more useful for understanding those processes than for application, partially because of the numerical complexity of the computations. Many other researchers have contributed sediment transport functions - always attempting to develop one which is reliable when compared with a variety of field data. The resulting functions are numerous, yet no single function has proved superior to the others for all conditions. Therefore, the following functional form is presented here to show the importance of various parameters.

$$G = f(U, d, S_e, B, D_{eff}, SG_s, G_{sf}, D_{si}, P_i, SG_f, T, \dots) \quad (\text{Sediment Transport}) \quad (4)$$

where:

B	=	effective width of flow
d	=	effective depth of flow
D_{eff}	=	effective particle diameter of the mixture
D_{si}	=	geometric mean of particle diameters in each size class i
G	=	total bed material discharge rate in units of weight/time (e.g., tons/day)
G_{sf}	=	grain shape factor
P_i	=	fraction of particles of the i^{th} size class that are found in the bed
S_e	=	slope of energy grade line
SG_f	=	specific gravity of fluid
SG_s	=	specific gravity of sediment particles
T	=	water temperature
U	=	flow velocity

Sediment transport rates are calculated for grain sizes up to 64 mm (soon to be expanded to 2000 mm). Sediment sizes larger than 64 mm, that may exist in the bed, are used for sorting computations but are not transported. For deposition and erosion of clay and silt sizes up to 0.0625 mm, Krone's (1962) method is used for deposition and Ariathurai's (1976) adaptation of Parthenaides' (1965) method is used for scour. The default for clay and silt allows only deposition using a method based on settling velocity.

The sediment transport function for bed material load is selected by the user. Transport functions available in the program include the following:

- a. Toffaleti's (1966) transport function
- b. Madden's (1963) modification of Laursen's (1958) relationship
- c. Yang's (1973) stream power for sands
- d. Duboys transport function (Vanoni 1975)
- e. Ackers-White (1973) transport function
- f. Colby (1964) transport function
- g. Toffaleti (1966) and Schoklitsch (1930) combination
- h. Meyer-Peter and Müller (1948)
- i. Toffaleti and Meyer-Peter and Müller combination
- j. Madden's (1985, unpublished) modification of Laursen's (1958) relationship
- k. Parthenaides (1965), Ariathurai (1976) and Krone (1962) for cohesive sediments

- l. Copeland's (1990) modification of Laursen's relationship (Copeland and Thomas 1989)
- m. User specification of transport coefficients based upon observed data

e. *Computational methodology.* Descriptions of the computational methodology used in HEC-6 and application of the program are presented in the HEC-6 user's manual (HEC 1991).

Experience has shown that successful application of movable boundary models may require substantial effort to reproduce field observations, i.e., calibration. The general topic of application and calibration of numerical river models is thoroughly covered in Cunge, et al. (1980).

3. Specific Reservoir Simulation Capabilities.

- ▶ User can specify water surface elevations (internal boundary conditions) to simulate operation and control of reservoir pool elevations as functions of time.
- ▶ Allows for deposition and compaction of cohesive sediments with time.
- ▶ Provides for reentrainment of cohesive sediments based on equations presented by Parthenaides (1965).
- ▶ Can simulate deposition at various pool levels and, therefore, compute impacts of reservoir deposits on upstream water surface profiles.
- ▶ Has a "parallel flow" capability, which means that several discharges in the time series of flows can be modeled without updating boundary geometry - achieves computational efficiency.
- ▶ Can compute trap efficiencies and perform volumetric accounting of sediment by grain size.

4. Some Limitations of HEC-6 with Regard to Reservoirs.

- ▶ It is a **one-dimensional** model.
- ▶ Density variations due to thermal stratification or sediment concentrations are not included in the hydraulics.
- ▶ Modeling of the structure is limited by what the user can do with cross sections and water surface elevations.

5. Some Additional HEC and Corps of Engineers Software for Reservoir Analysis.

- ▶ HEC-5 "Simulation of Flood Control And Conservation Systems" (HEC 1982).
- ▶ HEC-5Q "Simulation of Flood Control and Conservation Systems - Appendix on Water Quality Analysis" (HEC 1986).
- ▶ HEC-PRM "Prescriptive Reservoir System Analysis Model - Missouri River System Application" (HEC Technical Paper No. 136 Nov. 1991).

- ▶ HEC NexGen project.
- ▶ TABS-2 "Open Channel Flow and Sedimentation," two-dimensional flow and sediment modeling system (vertically averaged).

a. Purpose. The purpose of the TABS-2 system (Thomas and McAnally, 1985) is to provide a complete set of generalized computer programs for two-dimensional numerical modeling of open-channel

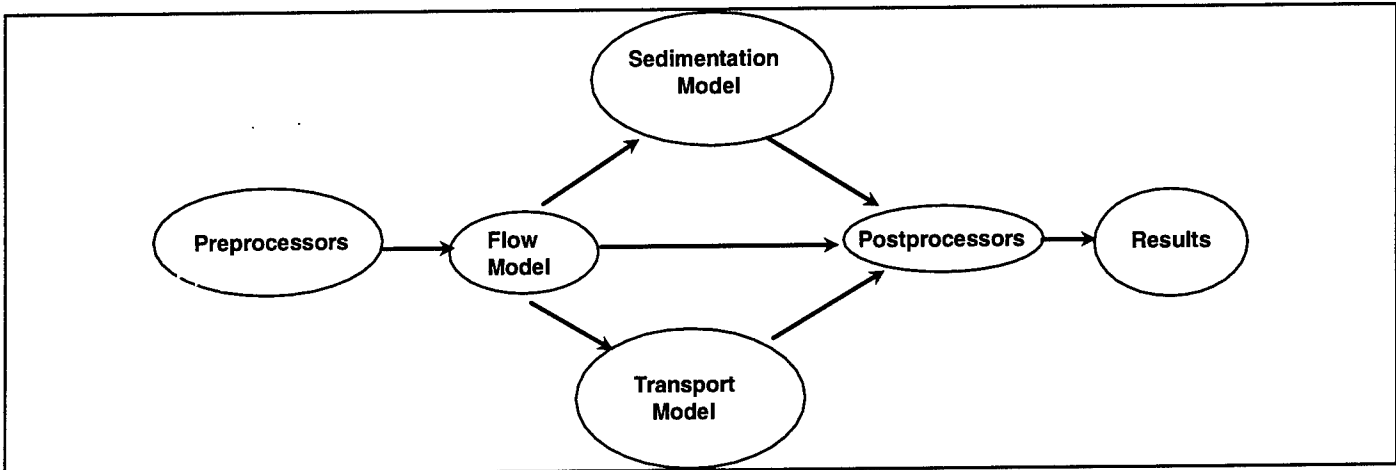


Figure 4 TABS-2 Schematic

flow, transport processes, and sedimentation. These processes are modeled to help analyze hydraulic engineering and environmental conditions in waterways. The system is designed to be used by engineers and scientists who need not be computer experts.

b. Description. TABS-2 is a collection of generalized computer programs and utility codes integrated into a numerical modeling system for studying two-dimensional hydraulics, transport, and sedimentation processes in rivers, reservoirs, bays, and estuaries. A schematic representation of the system is shown in Figure 4.

c. Uses. It can be used either as a stand-alone solution technique or as a step in the hybrid modeling approach. The basic concept is to calculate water-surface elevations, current patterns, dispersive transport, sediment erosion, transport and deposition, resulting bed surface elevations, and feedback to hydraulics. Existing and proposed geometry can be analyzed to determine the impact of project designs on flows, sedimentation, and salinity. The calculated velocity pattern around structures and islands is particularly useful.

REFERENCES

Ackers, P., and White, W. R., "Sediment transport: new approach and analysis," *Journal of the Hydraulics Division*, ASCE, Vol. 99, No. HY11, pp. 2041-2060, 1973.

Ariathurai, R., and Krone, R. B., "Finite element model for cohesive sediment transport," *Journal of the Hydraulics Division*, ASCE, pp. 323-338, March 1976.

Colby, B. R., "Practical computations of bed-material discharge," *Proceedings*, ASCE, Vol. 90, No. HY2, 1964.

Copeland, Ronald R., and Thomas, W. A., *Corte Madera Creek Sedimentation Study*, Technical Report HL89-6, USACE, Waterways Experiment Station, Vicksburg, MS, April 1989.

Copeland, Ronald R., *Waimea Sedimentation Study, Kauai, Hawaii, Numerical Model Investigation*, Technical Report HL90-3, USACE, Waterways Experiment Station, Vicksburg, MS, May 1990.

Cunge, J. A., Holly, F. M., and Verwey, A., *Practical Aspects of Computational River Hydraulics*, 1980, Pitman, London.

Dawdy, D. R. and Vanoni, V. A., Modeling Alluvial Channels, *Water Resources Research*, Vol. 22, No. 9, pp 71s-81s, August 1986.

Einstein, Hans Albert, "The Bed-Load Function for Sediment Transportation in Open Channel Flows," U.S. Department of Agriculture Technical Bulletin No. 1026, Soil Conservation Service, Washington, D.C., 1950, 71 pp.

Gee, D. M., "Prediction of the Effects of a Flood Control Project on a Meandering Stream," 1983, *Proceedings of the ASCE Conference Rivers '83* (also published as HEC Technical Paper No. 97).

Krone, R. B., *Flume Studies of the Transport of Sediment in Estuarial Shoaling Processes*, Hydraulic Engineering Laboratory, University of California, Berkeley, CA, 1962.

Laursen, E. M., "The total sediment load of streams," *Journal of the Hydraulics Division*, ASCE, Vol. 84, No. HY1, p. 1530-1 to 1530-36, February 1958.

Limerinos, J. T., "Determination of the Manning Coefficient from Measured Bed Roughness in Natural Channels," Water Supply Paper 1898B, 1970, U.S. Geological Survey.

Madden, E. B., "Channel Design for Modified Sediment Regime Conditions on the Arkansas River," Paper No. 39, *Proceedings of the Federal Inter-Agency Sedimentation Conference*, Miscellaneous Publication No. 970, Agricultural Research Service, U.S. Government Printing Office, 1963, pp. 335-352.

Meyer-Peter, E., and Müller, R., "Formulas for bed-load transport," *International Association of Hydraulic Research*, 2nd Meeting, Stockholm, 1948.

Parthenaides, E., "Erosion and Deposition of Cohesive Soils," *Journal of the Hydraulics Division*, ASCE, March 1965, pp. 755-771.

Schoklitsch, A., *Handbuch des Wasserbaues*, Springer, Vienna (2nd ed.), English Translation (1937) by S. Shulits, 1930.

Thomas, W. A. and Prasuhn, A. L., "Mathematical Modeling of Scour and Deposition," *Journal of the Hydraulics Division, ASCE*, Vol. 103, No. HY8, 1977 (Aug.), pp. 851-863.

Thomas W. A. and McAnally, W. H., "Open-Channel Flow and Sedimentation TABS-2," User's Manual, U.S. Army Corps of Engineers Waterways Experiment Station (WES), Instruction Report HL-85-1, 1985.

Toffaletti, F. B., *A Procedure for Computation of Total River Sand Discharge and Detailed Distribution, Bed to Surface*, Committee on Channel Stabilization, U.S. Army Corps of Engineers, November 1966.

U.S. Army Corps of Engineers, Hydrologic Engineering Center (HEC), "Effects of Dam Removal: An Approach to Sedimentation," Technical Paper No. 50, 1977, Davis, CA.

U.S. Army Corps of Engineers, Hydrologic Engineering Center (HEC), "HEC-5, Simulation of Flood Control and Conservation Systems, User's Manual," April 1982, Davis, CA.

U.S. Army Corps of Engineers, Hydrologic Engineering Center (HEC), "HEC-5, Simulation of Flood Control and Conservation Systems, Appendix on Water Quality Analysis," Sept. 1986, Davis, CA.

U.S. Army Corps of Engineers, Hydrologic Engineering Center (HEC), "HEC-6, Scour and Deposition in Rivers and Reservoirs, User's Manual," August 1993, Davis, CA.

U.S. Army Corps of Engineers, Hydrologic Engineering Center (HEC), "Prescriptive Reservoir System Analysis Model - Missouri River System Application," Technical Paper No. 136, Nov. 1991, Davis, CA.

U.S. Army Corps of Engineers, Hydrologic Engineering Center (HEC), "Guidelines for the Calibration and Application of Computer Program HEC-6," Oct. 1992, Davis, CA.

Vanoni, Vito A., ed., "Sedimentation Engineering," American Society of Civil Engineers Manual No. 54, 1975, New York, NY.

Yang, C. T., "Incipient motion and sediment transport," *Journal of the Hydraulics Division, ASCE*, Vol. 99, No. HY10, Proc. Paper 10067, pp. 1679-1704, October 1973.

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TP-86 Training the Practitioner: The Hydrologic Engineering Center Program
TP-87 Documentation Needs for Water Resources Models
TP-88 Reservoir System Regulation for Water Quality Control
TP-89 A Software System to Aid in Making Real-Time Water Control Decisions
TP-90 Calibration, Verification and Application of a Two-Dimensional Flow Model
TP-91 HEC Software Development and Support
TP-92 Hydrologic Engineering Center Planning Models
TP-93 Flood Routing Through a Flat, Complex Flood Plain Using a One-Dimensional Unsteady Flow Computer Program
TP-94 Dredged-Material Disposal Management Model
TP-95 Infiltration and Soil Moisture Redistribution in HEC-1
TP-96 The Hydrologic Engineering Center Experience in Nonstructural Planning
TP-97 Prediction of the Effects of a Flood Control Project on a Meandering Stream
TP-98 Evolution in Computer Programs Causes Evolution in Training Needs: The Hydrologic Engineering Center Experience
TP-99 Reservoir System Analysis for Water Quality
TP-100 Probable Maximum Flood Estimation - Eastern United States
TP-101 Use of Computer Program HEC-5 for Water Supply Analysis
TP-102 Role of Calibration in the Application of HEC-6
TP-103 Engineering and Economic Considerations in Formulating
TP-104 Modeling Water Resources Systems for Water Quality
TP-105 Use of a Two-Dimensional Flow Model to Quantify Aquatic Habitat
TP-106 Flood-Runoff Forecasting with HEC-1F
TP-107 Dredged-Material Disposal System Capacity Expansion
TP-108 Role of Small Computers in Two-Dimensional Flow Modeling
TP-109 One-Dimensional Model For Mud Flows
TP-110 Subdivision Froude Number
TP-111 HEC-5Q: System Water Quality Modeling
TP-112 New Developments in HEC Programs for Flood Control
TP-113 Modeling and Managing Water Resource Systems for Water Quality
TP-114 Accuracy of Computed Water Surface Profiles - Executive Summary
TP-115 Application of Spatial-Data Management Techniques in Corps Planning
TP-116 The HEC's Activities in Watershed Modeling
TP-117 HEC-1 and HEC-2 Applications on the MicroComputer
TP-118 Real-Time Snow Simulation Model for the Monongahela River Basin
TP-119 Multi-Purpose, Multi-Reservoir Simulation on a PC
TP-120 Technology Transfer of Corps' Hydrologic Models
TP-121 Development, Calibration and Application of Runoff Forecasting Models for the Allegheny River Basin
TP-122 The Estimation of Rainfall for Flood Forecasting Using Radar and Rain Gage Data
TP-123 Developing and Managing a Comprehensive Reservoir Analysis Model
TP-124 Review of the U.S. Army Corps of Engineering Involvement With Alluvial Fan Flooding Problems
TP-125 An Integrated Software Package for Flood Damage Analysis
TP-126 The Value and Depreciation of Existing Facilities: The Case of Reservoirs
TP-127 Floodplain-Management Plan Enumeration
TP-128 Two-Dimensional Floodplain Modeling
TP-129 Status and New Capabilities of Computer Program HEC-6: "Scour and Deposition in Rivers and Reservoirs"
TP-130 Estimating Sediment Delivery and Yield on Alluvial Fans
TP-131 Hydrologic Aspects of Flood Warning - Preparedness Programs
TP-132 Twenty-five Years of Developing, Distributing, and Supporting Hydrologic Engineering Computer Programs
TP-133 Predicting Deposition Patterns in Small Basins
TP-134 Annual Extreme Lake Elevations by Total Probability Theorem
TP-135 A Muskingum-Cunge Channel Flow Routing Method for Drainage Networks
TP-136 Prescriptive Reservoir System Analysis Model - Missouri River System Application
TP-137 A Generalized Simulation Model for Reservoir System Analysis
TP-138 The HEC NexGen Software Development Project
TP-139 Issues for Applications Developers
TP-140 HEC-2 Water Surface Profiles Program
TP-141 HEC Models for Urban Hydrologic Analysis
TP-142 Systems Analysis Applications at the Hydrologic Engineering Center
TP-143 Runoff Prediction Uncertainty for Ungauged Agricultural Watersheds
TP-144 Review of GIS Applications in Hydrologic Modeling
TP-145 Application of Rainfall-Runoff Simulation for Flood Forecasting
TP-146 Application of the HEC Prescriptive Reservoir Model in the Columbia River System
TP-147 HEC River Analysis System (HEC-RAS)
TP-148 HEC-6: Reservoir Sediment Control Applications