

FINAL REPORT

30 September 91 - 29 September 94

for

***Harmonic Gyrotron Amplifiers
and
Phase-Locked Oscillators***

AFOSR Grant AFOSR-91-0390

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**Submitted to
Dr Robert J. Barker
AFOSR/NE**

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MARYLAND HIGH POWER SOURCES

THEORY GROUP

*** Faculty**

T. Antonsen Jr.

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C. Liu

*** Undergraduate Students**

S. Rajapatirana

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Research Area

Mode Competition and Multi-Frequency effects in high power fast wave devices

Specific Applications:

1. High power gyrotrons for plasma heating
2. Parametric Mode interactions in harmonic gyrotrons
3. Multi-frequency effects in fel oscillators
4. Modeling of harmonic gyroklystrons, phase locked gyro oscillators, and gyro-twystrons

NONLINEAR SIMULATION OF HIGH POWER GYROTRONS

RESEARCH TOOL:

- *Time dependent multi-mode simulation code (MAGY)

CODE FEATURES:

- *Axial RF field profile determined self-consistently
- *Time dependent
- *Multi-Mode (frequencies are equally spaced)
- *Realistic boundary conditions
- *AC space charge
- *DC space charge (voltage depression)
- *Energy and Pitch angle distributions for incoming beam
- *Window reflection and delay
- *Non zero beam rise time
- *Mode coupling due to non uniform wall radius

THEORETICAL APPROACH

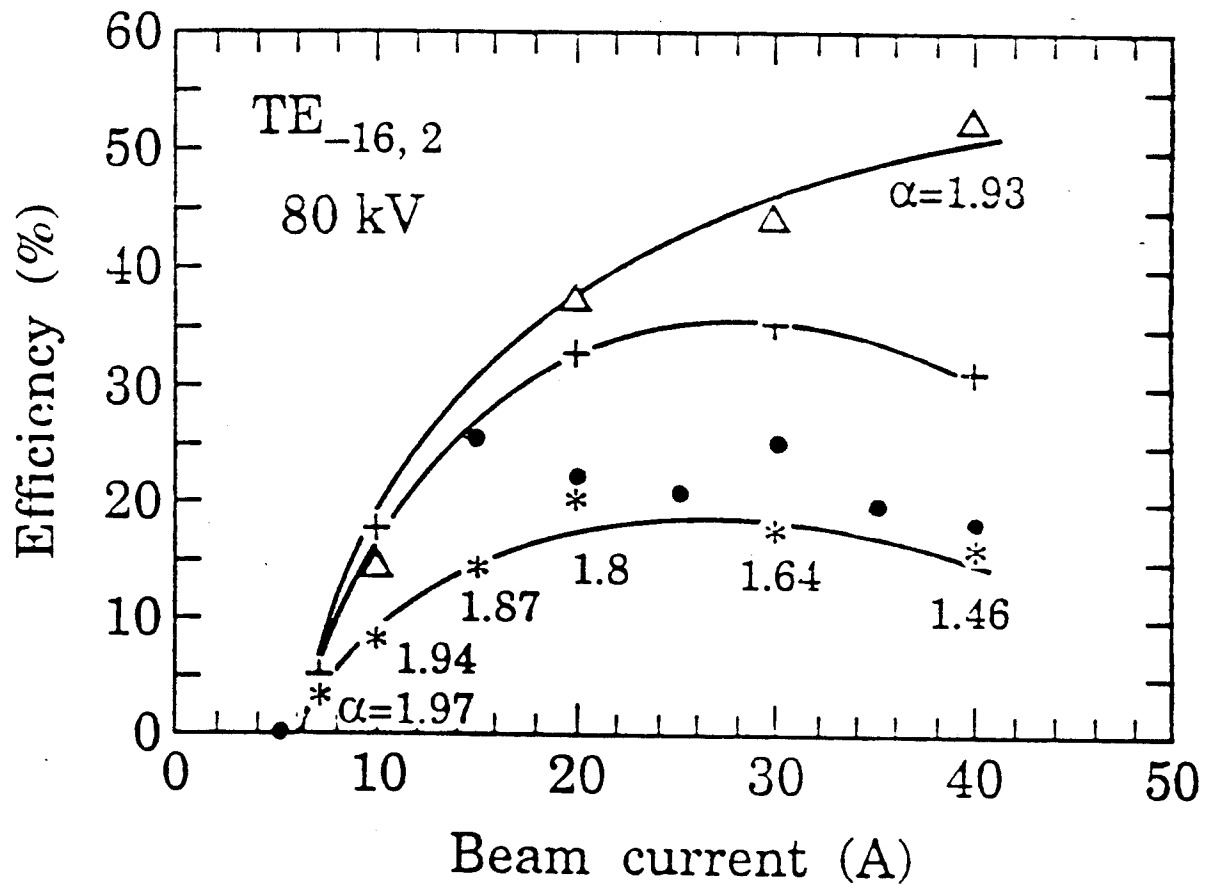
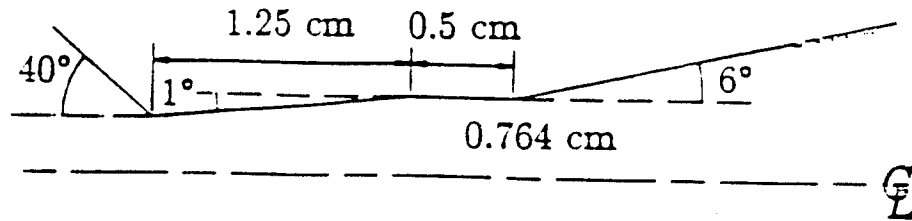
- Radiation field is expanded in transverse modes $\text{TE}_{\ell p}$

$$E(r, \phi, z, t) = \sum_{\ell p} \frac{c}{\omega_{\ell p}} E_{\ell p}(z, t) \exp(-i\omega_{\ell p}t) \hat{e}_z \times \nabla (J_{\ell}(k_{\ell p}r) e^{i\ell\theta}) + c.c.,$$

- Particle trajectories are followed in prescribed fields,
AC beam current calculated

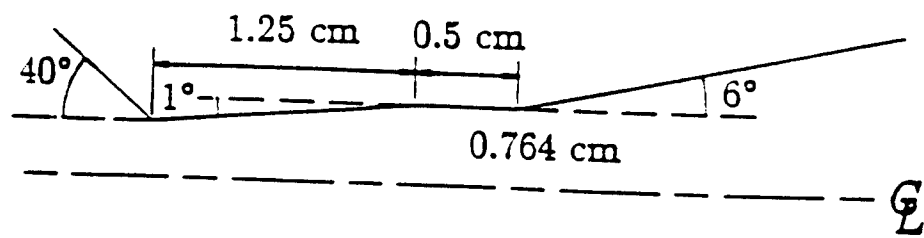
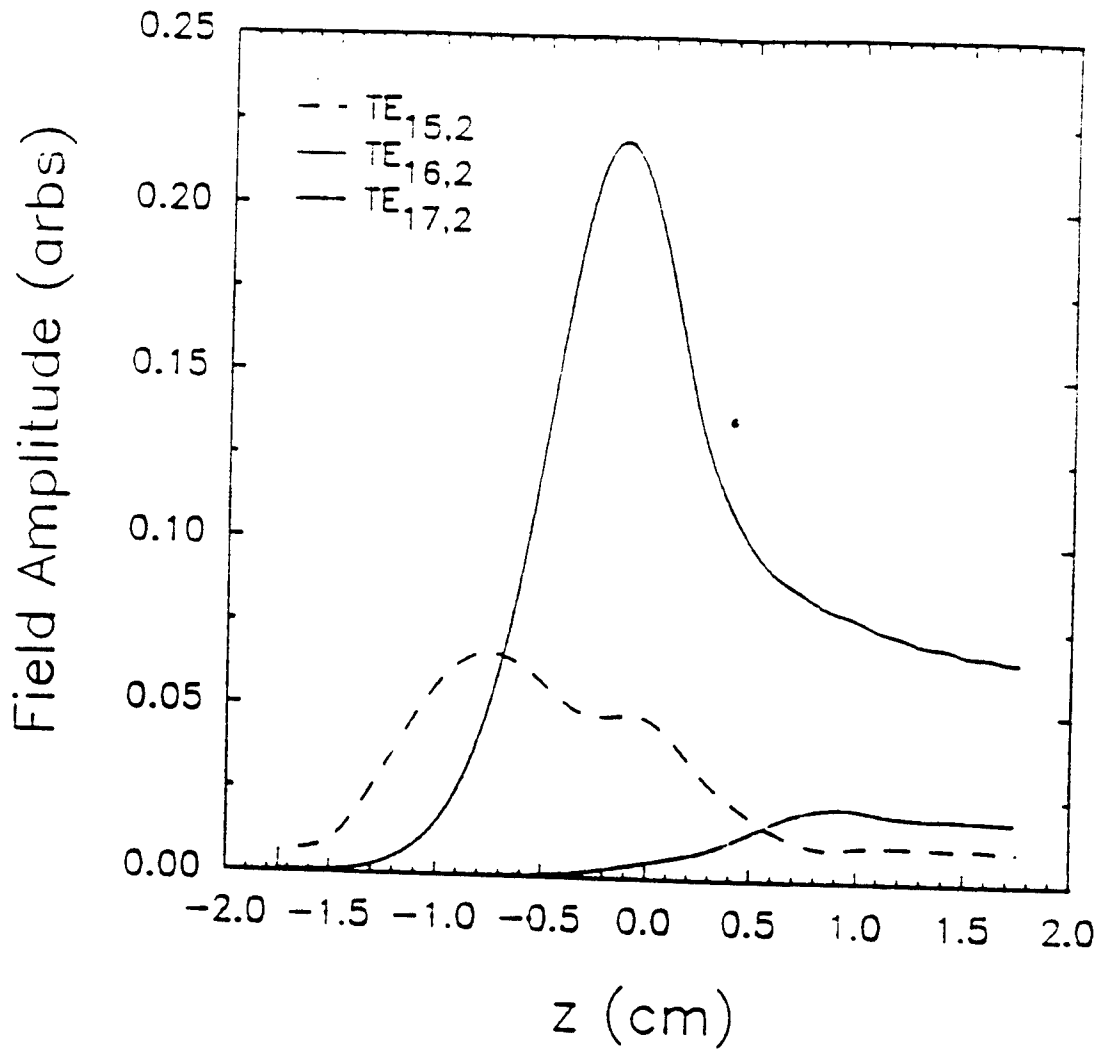
- Axially dependent field profile $E_{\ell p}(z, t)$ advanced in
time.

SIMULATION OF MIT SHORT CAVITY



- Δ : Single mode simulations with fixed α ($=1.93$).
- +
- : Experimental measurements.

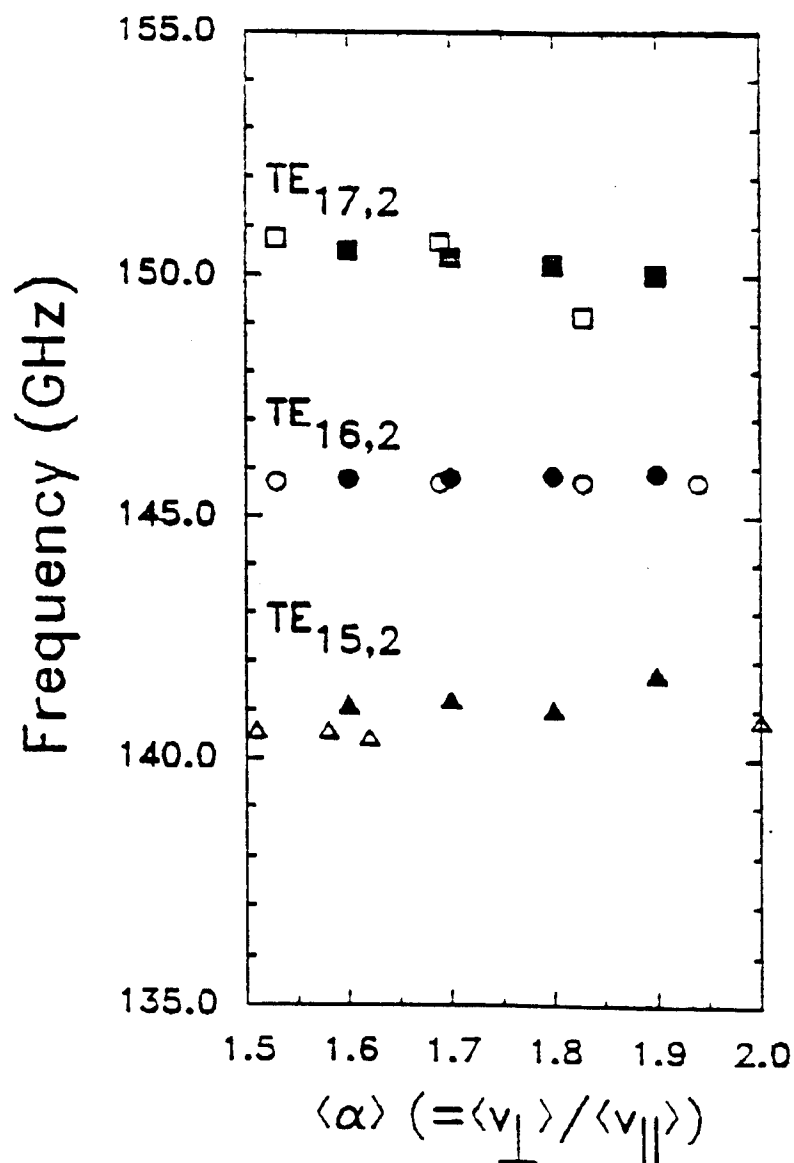
AXIAL FIELD PROFILES



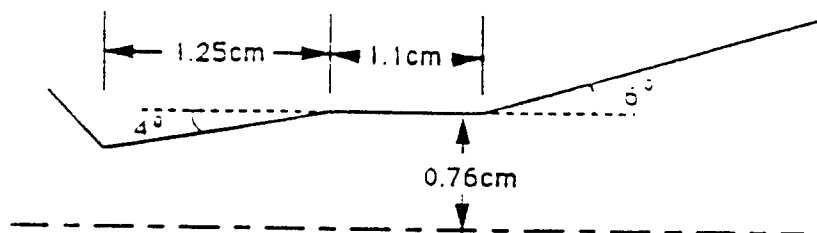
EXPERIMENTAL MEASUREMENT OF SIDEBANDS AT MIT

W.C. Guss, M.A. Basten, K.E. Kreischer, R.J. Temkin,
T.M. Antonsen Jr., S.Y. Cai, G. Saraph, and B. Levush

PREDICTED AND MEASURED MODE FREQUENCIES

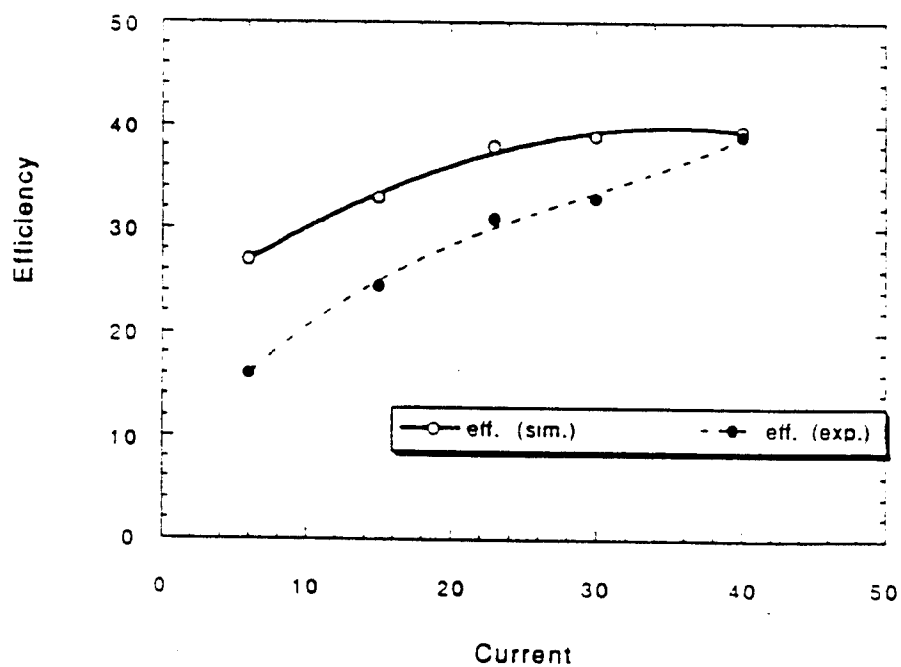


MARYLAND LONG CAVITY



EFFICIENCY VS. CURRENT

Maryland Long Cavity



Guss, Basten, Kreischer, Temkin, Antonsen, Cai, Saraph, and Levush, to be published in proceedings of IRMW

PARAMETRIC MODE COUPLING
IN HARMONIC GYROTRONS

Ph. D. Thesis

Girish Saraph

PARAMETRIC INSTABILITY

Three cavity modes: $TE_{l_1 p_1}$, $TE_{l_2 p_2}$, and $TE_{l_3 p_3}$

The cyclotron resonance criteria is given by,

$$\frac{\omega_1}{s_1} \approx \frac{\omega_2}{s_2} \approx \frac{\omega_3}{s_3} \approx \frac{\Omega_0}{\gamma}$$

The resonance criteria for the parametric instability are as follows:

- (a) For the harmonic numbers: $s_3 = s_1 + s_2$.
- (b) For the azimuthal mode indices: $l_3 = l_1 + l_2$.
- (c) For the angular frequencies: $\omega_3 \approx \omega_1 + \omega_2$,

Two characteristic features of the parametric instability are as follows:

- (a) Three modes are phase-locked together ,
- (b) When only one mode has high amplitude then the small signal gains of the other two modes match.

When the three modes are parametrically coupled, then different types of mode interactions can take place, viz. parametric excitation, decay of one or two modes, co-existence of three modes, or cyclic mode hopping between the three modes.

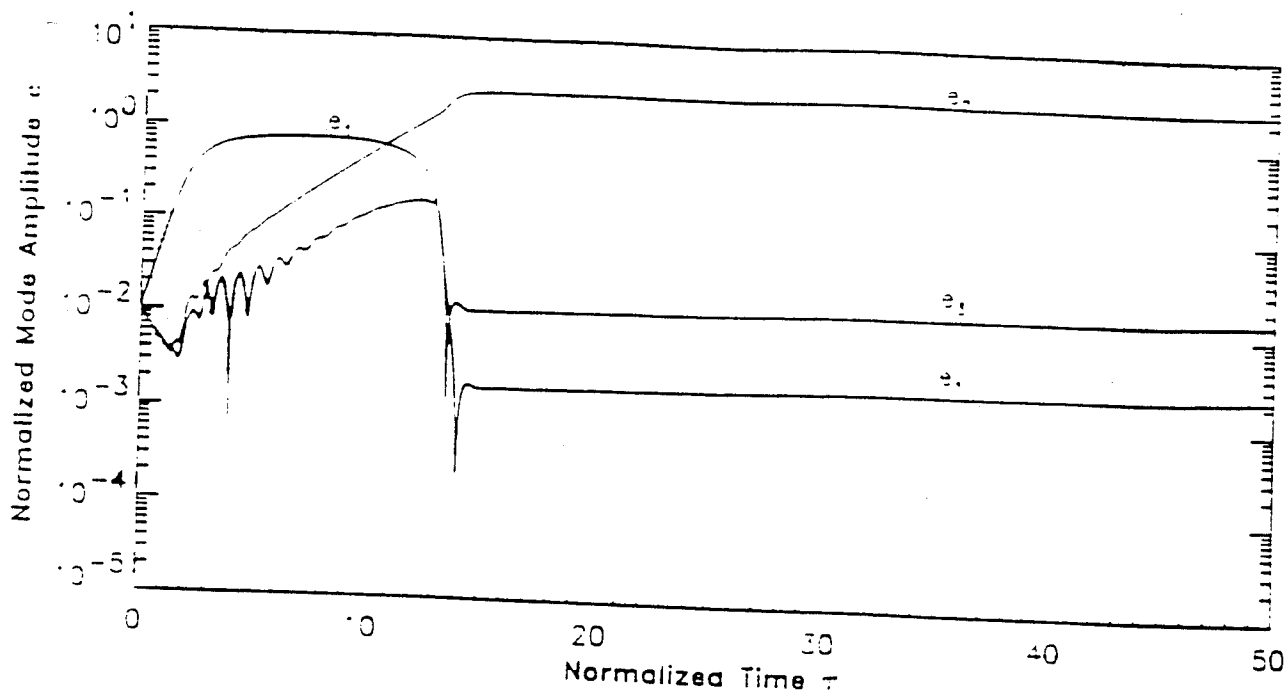
Notation used:

Mode 1 : $TE_{l_1 p_1}$ at the fundamental frequency ($s_1 = 1$)

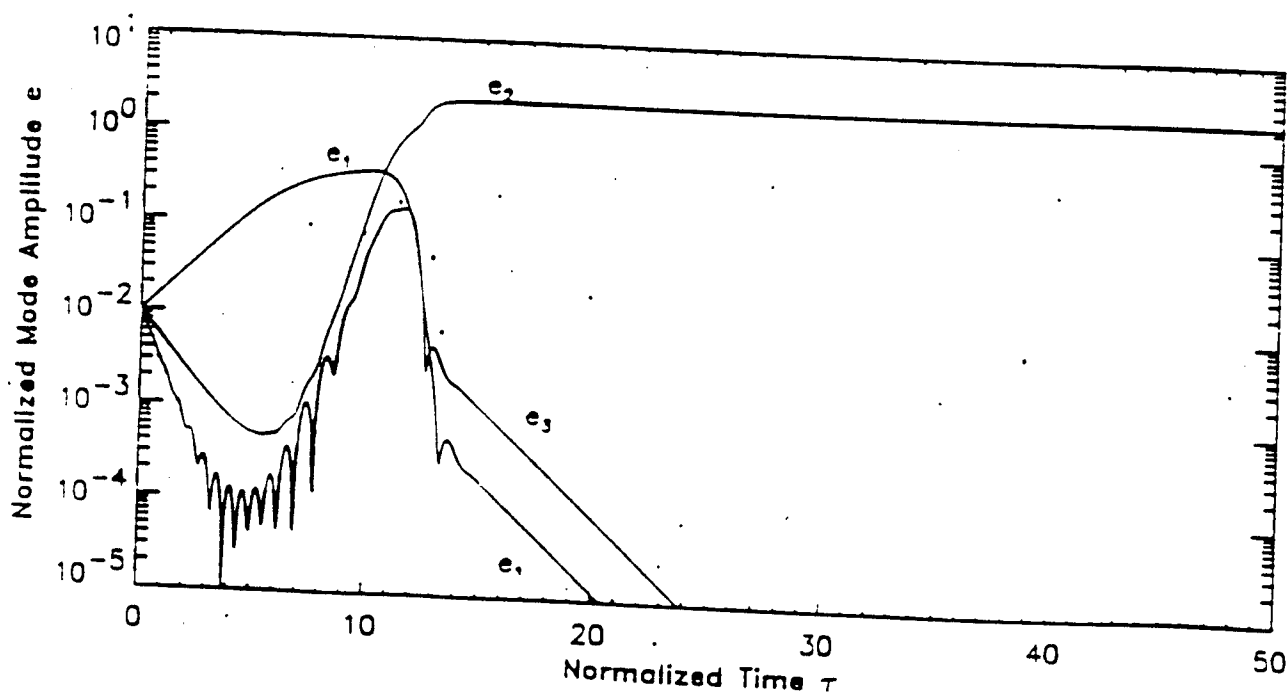
Mode 2 : $TE_{l_2 p_2}$ at the second harmonic frequency ($s_2 = 2$)

Mode 3 : $TE_{l_3 p_3}$ at the third harmonic frequency ($s_3 = 3$)

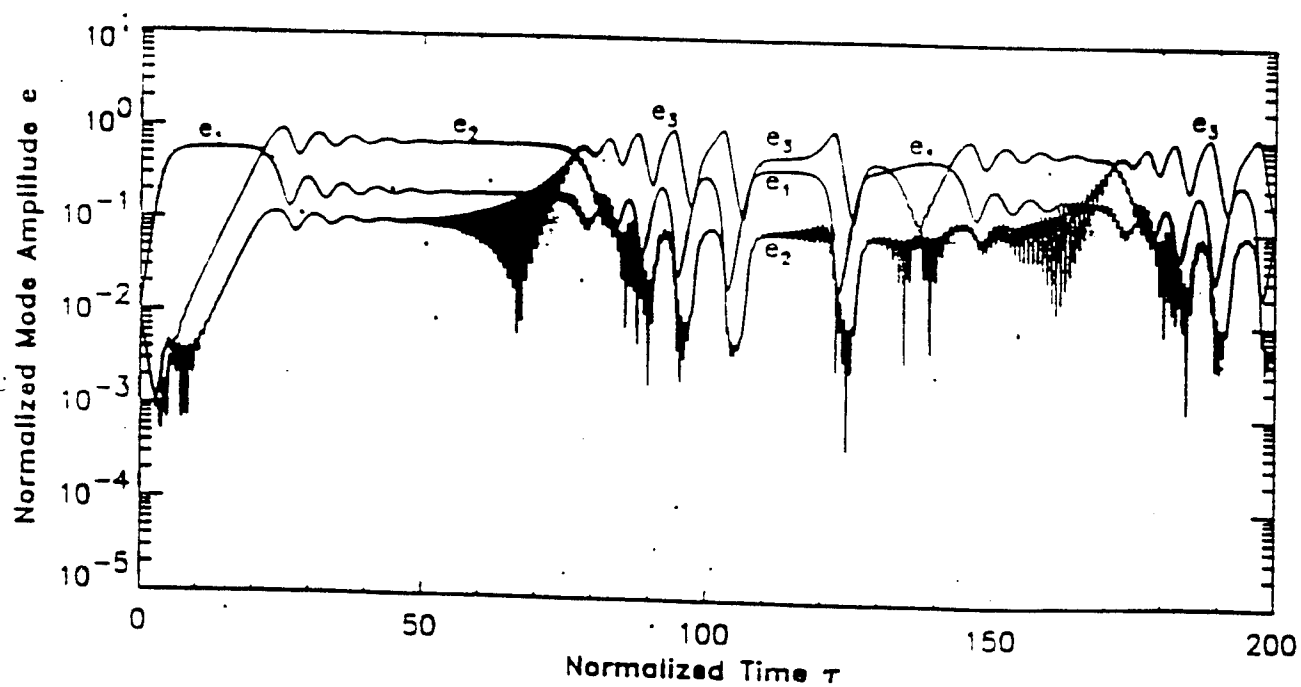
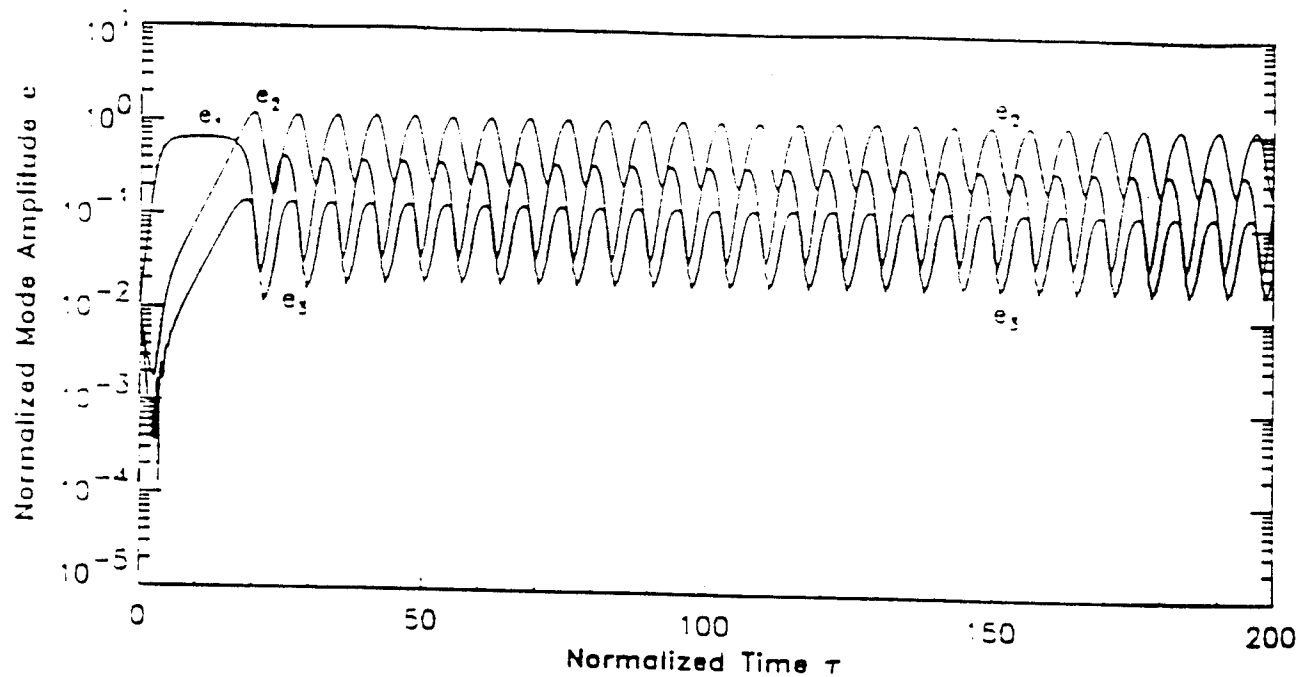
CO-EXISTENCE OF THREE MODES



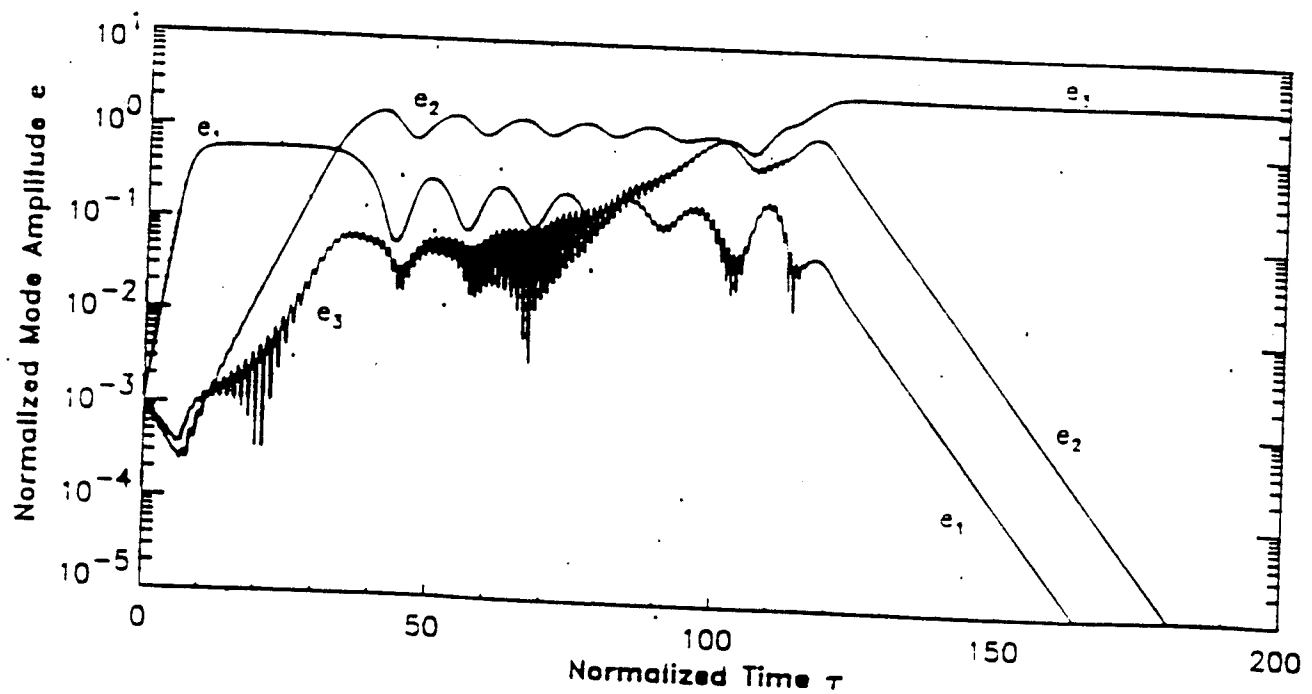
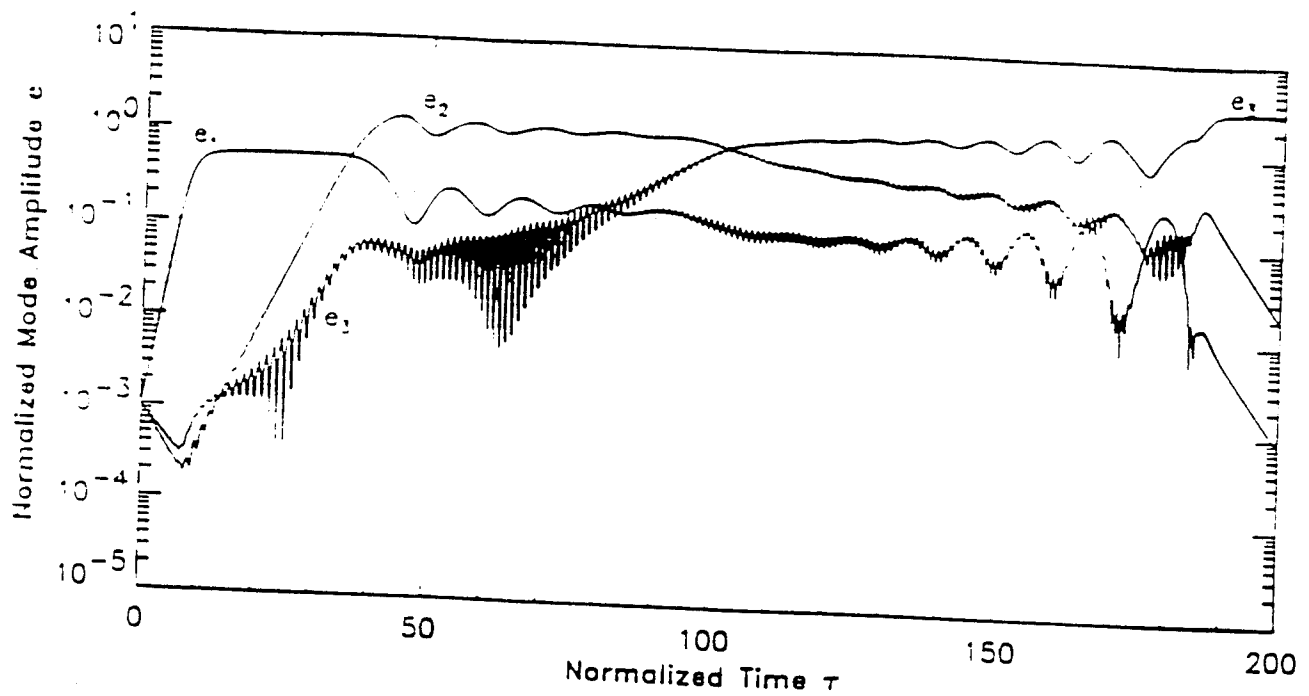
PARAMETRIC EXCITATION OF SECOND HARMONIC



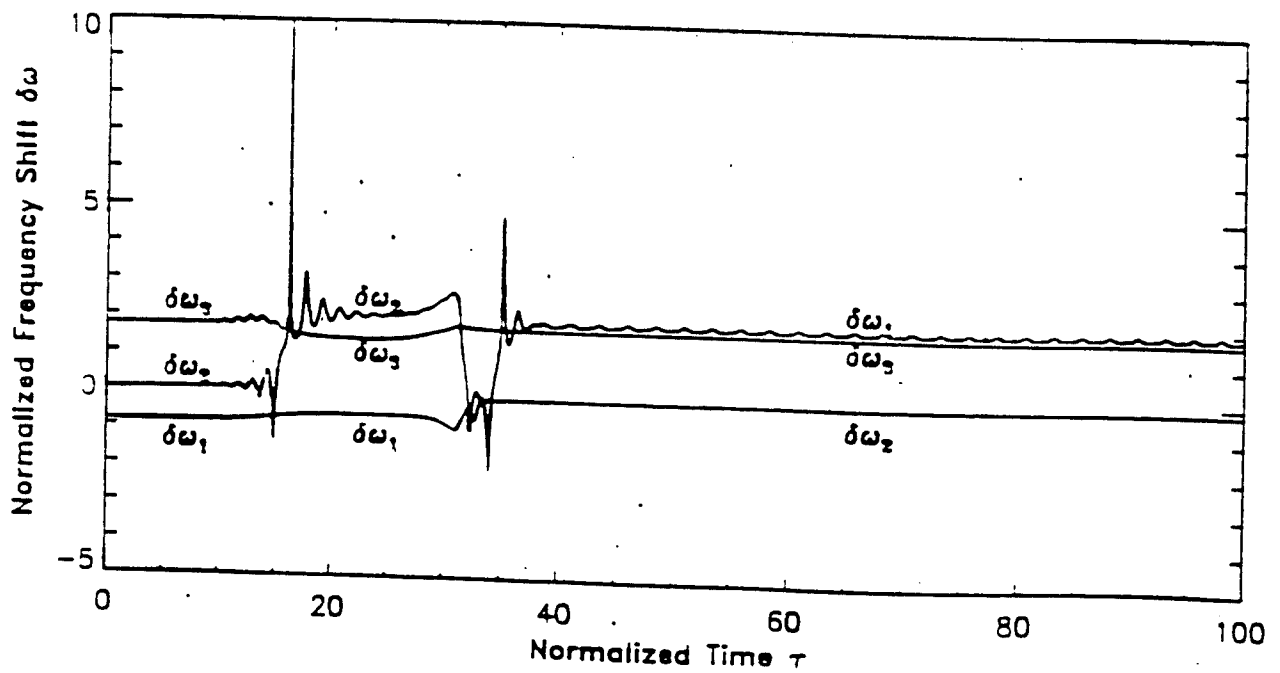
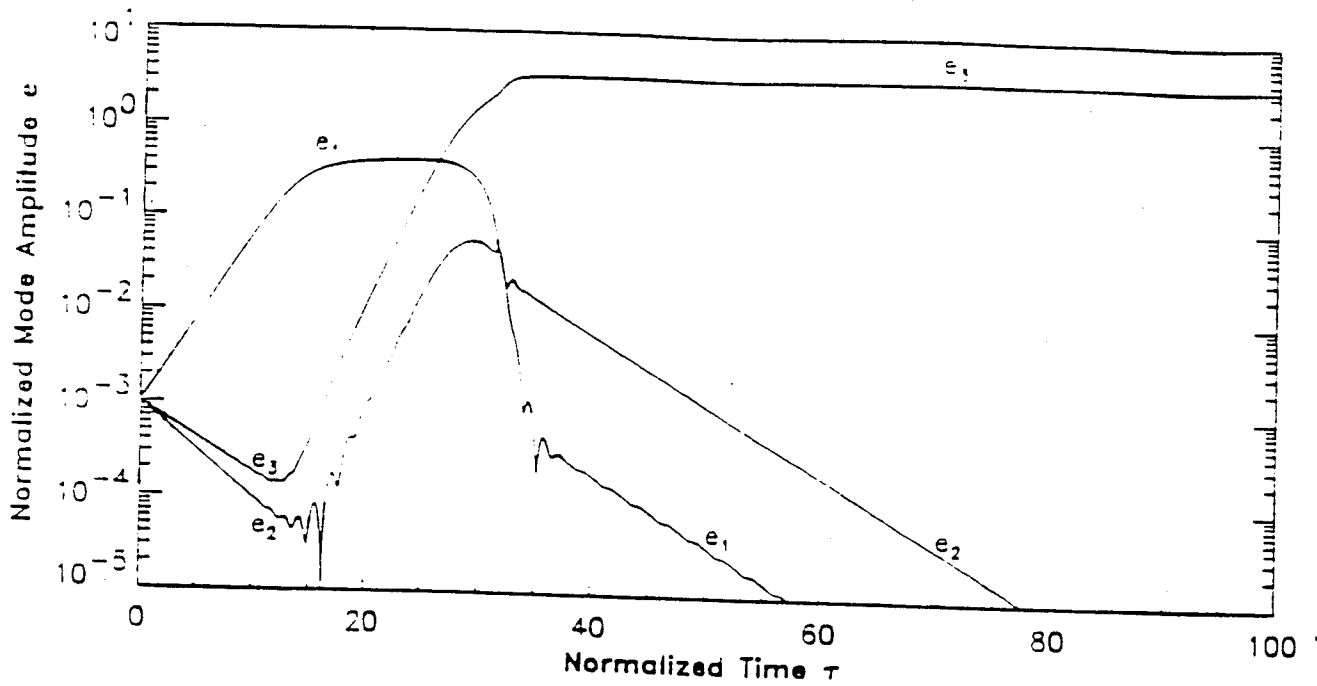
CYCLIC MODE HOPPING



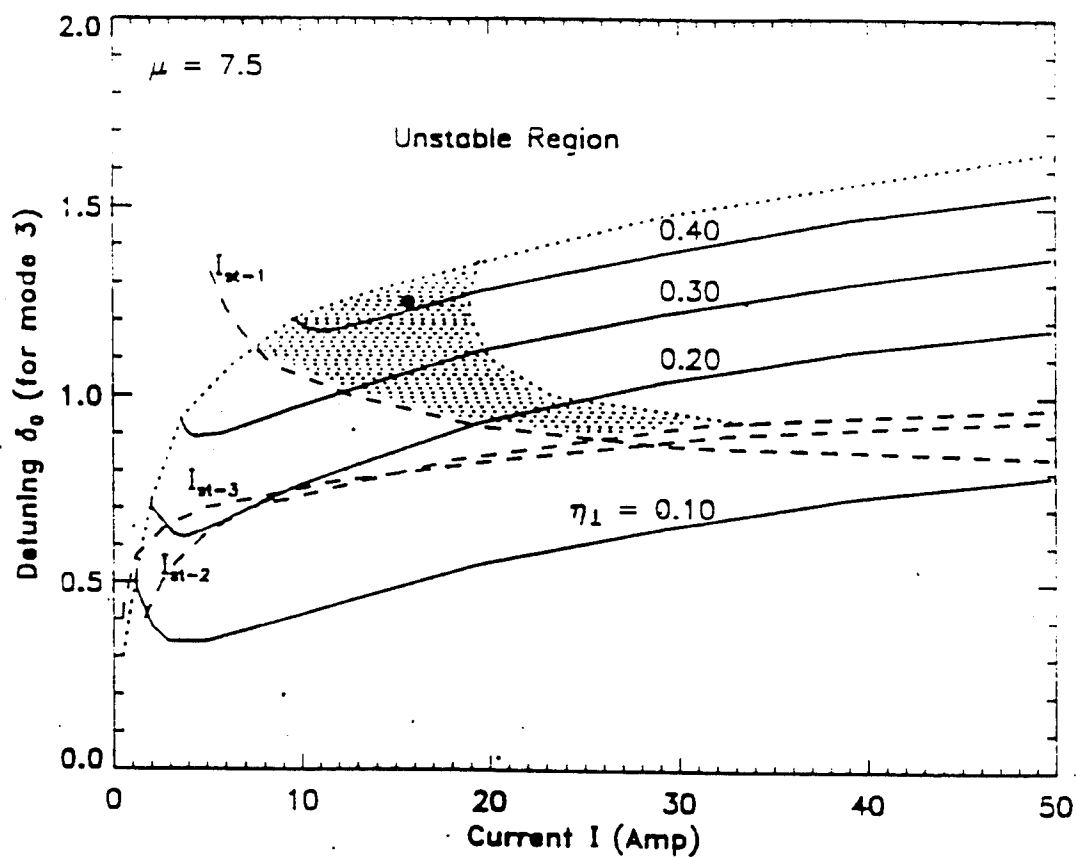
PARAMETRIC EXCITATION OF THIRD HARMONIC



PHASE-LOCKING OF MODES



REGION OF PARAMETRIC EXCITATION OF A THIRD HARMONIC AT 94 GHZ



DESIGN OF A THIRD HARMONIC GYROTRON

AT 94 GHZ

Mode 1 : $TE(3.1)$ at $s_1 = 1$

Mode 2 : $TE(1.3)$ at $s_2 = 2$

Mode 3 : $TE(4.3)$ at $s_3 = 3$

Selected Quantities:

Wall Radius $r_w = 0.65 \text{ cm.}$

Beam Radius $r_b = 0.42 \text{ cm.}$

Quality Factors: $Q_1 = 300.$

$Q_2 = 1200.$ $Q_3 = 2700$

Normalized Parameters:

$\mu = 7.5.$ $t_p = 86.$ $\hat{I}_1 = 230.$

$\delta = 0.7.$ $e_3 = 3.18.$ $\eta_{\perp} = 0.412$

Corresponding Physical Quantities:

Interaction Length $L_c = 4.14 \text{ cm}$

Operating Frequency $f_3 = 94 \text{ GHz}$

Magnetic Field $B_0 = 1.15 \text{ T}$

Beam Voltage $V = 31 \text{ kV}$

Beam Current $I = 15.75 \text{ Amp}$

Pitch Angle $\alpha = 1.9$

Net Efficiency $\eta = 32.3 \%$

Total Power Output $P_0 = 158 \text{ kW}$

Multi-frequency simulation of high gain fel oscillators

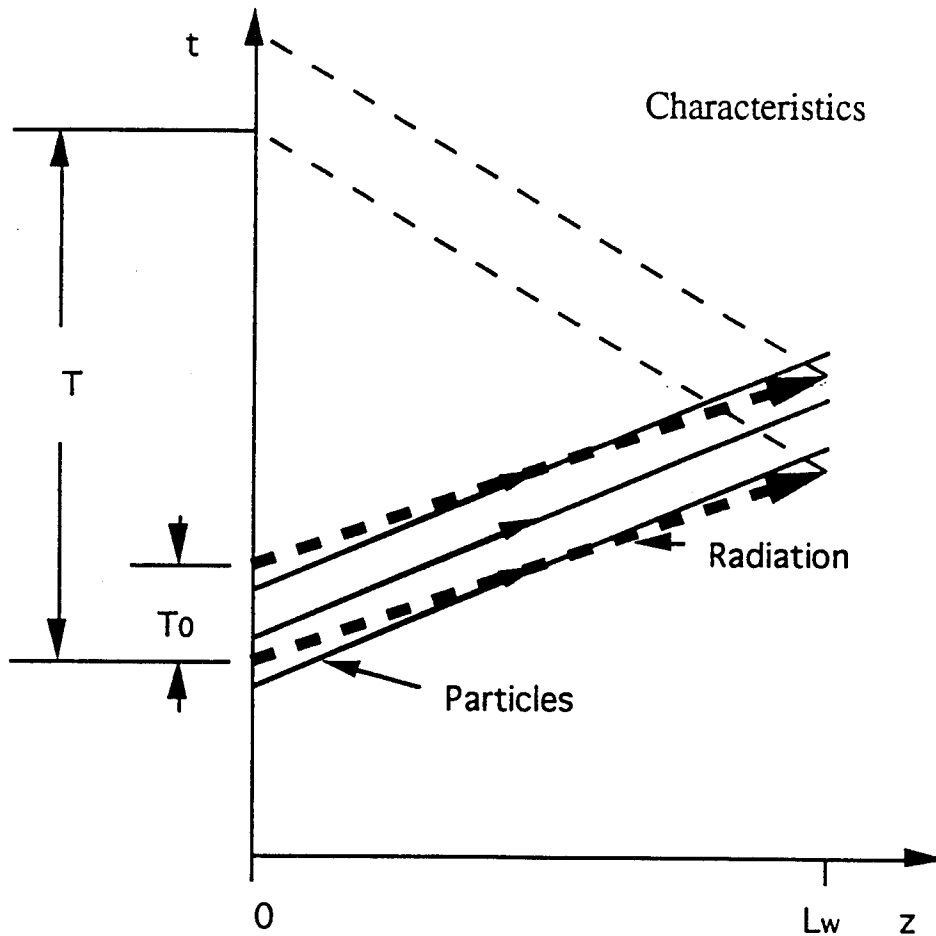
Radiation

$$\left[\frac{\partial}{\partial t} + v_g \frac{\partial}{\partial z} \right] \delta a(z,t) = - \frac{\pi I v_g v_w(z) \mathbf{e}_y \cdot \mathbf{e}_r^* C}{I_A k_0 A_{eff} v_z} \langle \exp(-i \psi) \rangle$$

Electrons

$$\left[\frac{\partial}{\partial t} + v_z \frac{\partial}{\partial z} \right] \gamma = i \frac{k_0}{2} \delta a(z,t) v_w(z) \mathbf{e}_y \cdot \mathbf{e}_r C \exp(i \psi) + \text{c.c.}$$

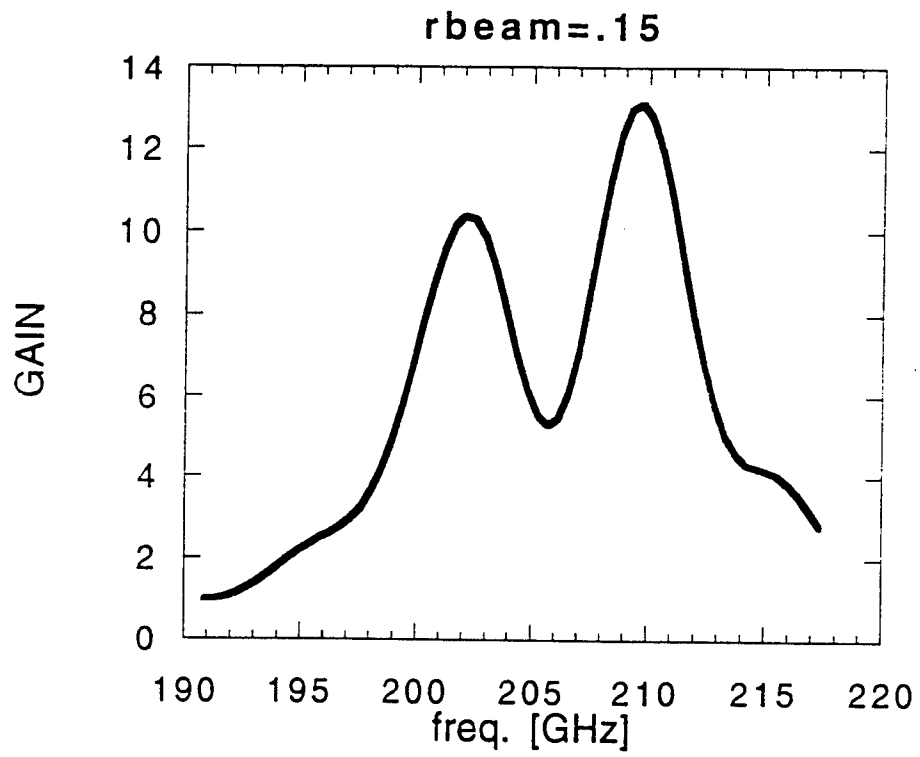
$$\left[\frac{\partial}{\partial t} + v_z \frac{\partial}{\partial z} \right] \psi = (k + k_w) v_z - \omega$$



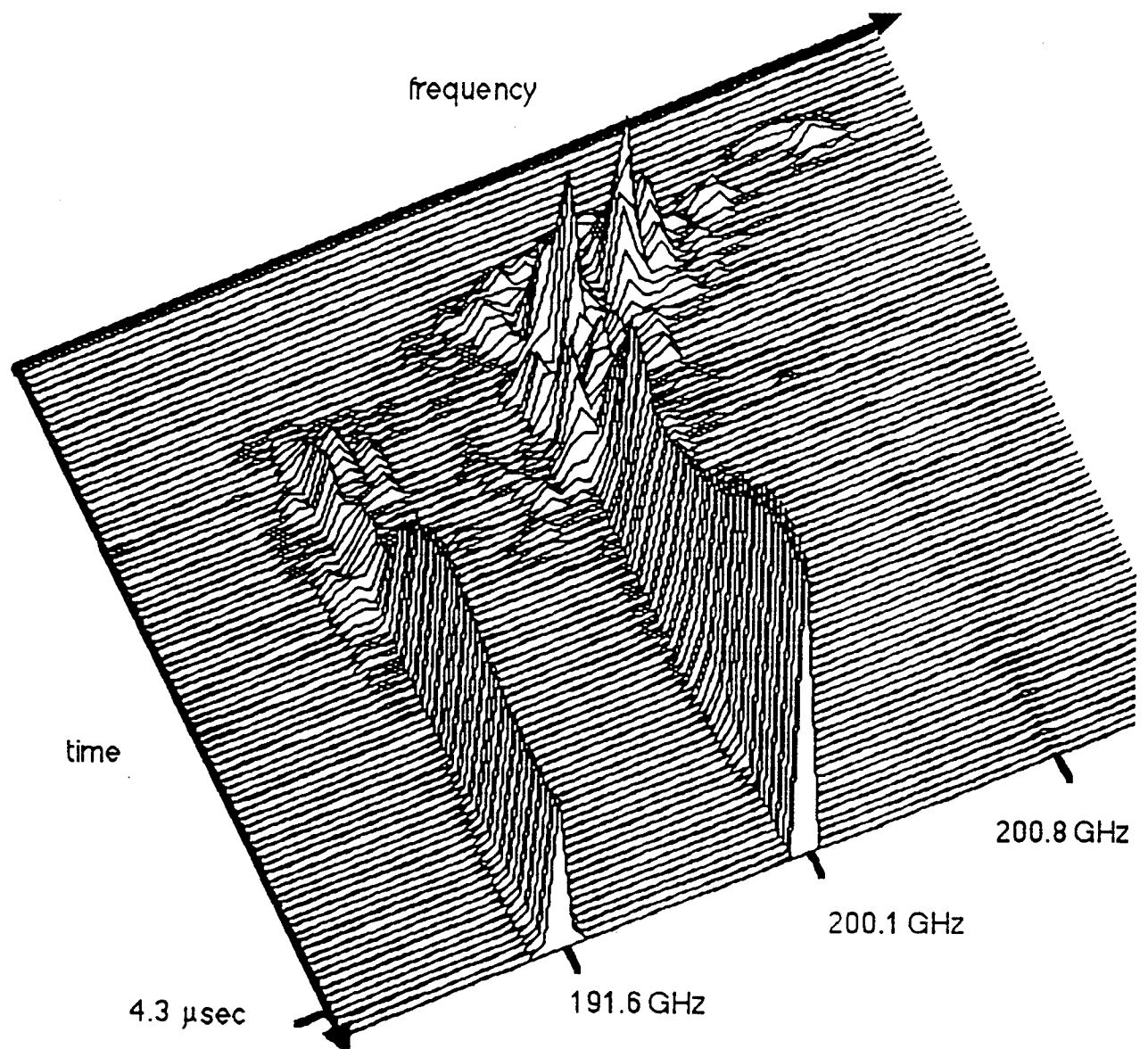
Proposed FEM design

Beam voltage	1.75 MV
Beam current	12 A
Beam emittance	0
Beam radius	.15 cm
Wiggler period	4 cm
Peak field wiggler section 1	2 kG
Peak field wiggler section 2	1.7 kG
No. periods wiggler section 1	25 (23 full periods)
No. periods wiggler section 2	19 (17 full periods)
Inter wiggler gap	6 cm
Waveguide mode	HE ₁₁ rectangular
Waveguide width	1.5 cm
Waveguide height	2.0 cm
Cutoff frequency	12.49 GHz
Cavity length	382 cm
Power reflection coefficient	.21

Linear Gain



Output Spectrum versus Time



Modeling of harmonic gyroklystrons, phase locked gyro-oscillators, and gyro-twystrons

Recent Topics

1. Theory of the relativistic gyrotwystron

input: cavity

output: travelling wave amplifier

2. Two harmonic prebunching of electrons in multi-cavity gyrodevices

input cavity: fundamental

second cavity: fundamental/second
harmonic

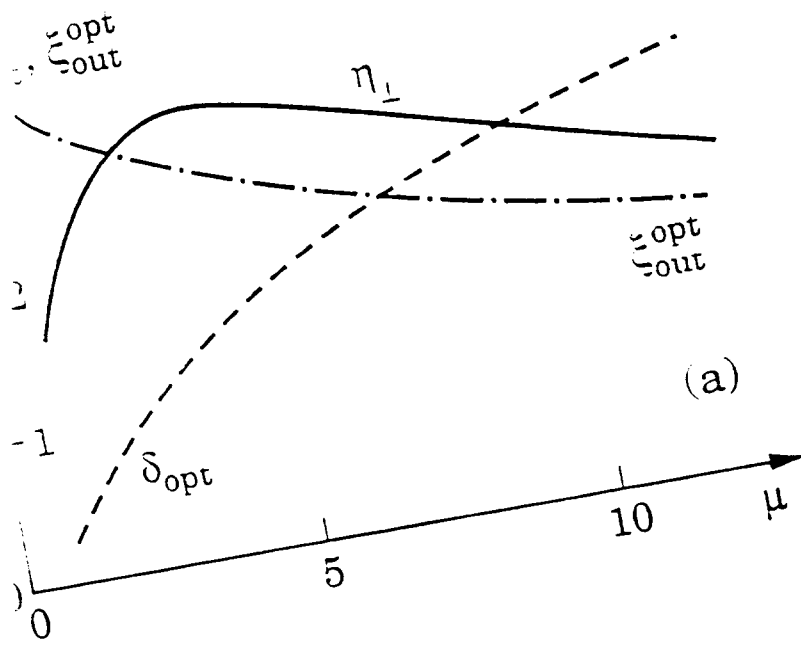
output cavity: fundamental-fourth harmonic

3. Theory of phase-locked gyrotrons operating at cyclotron harmonics

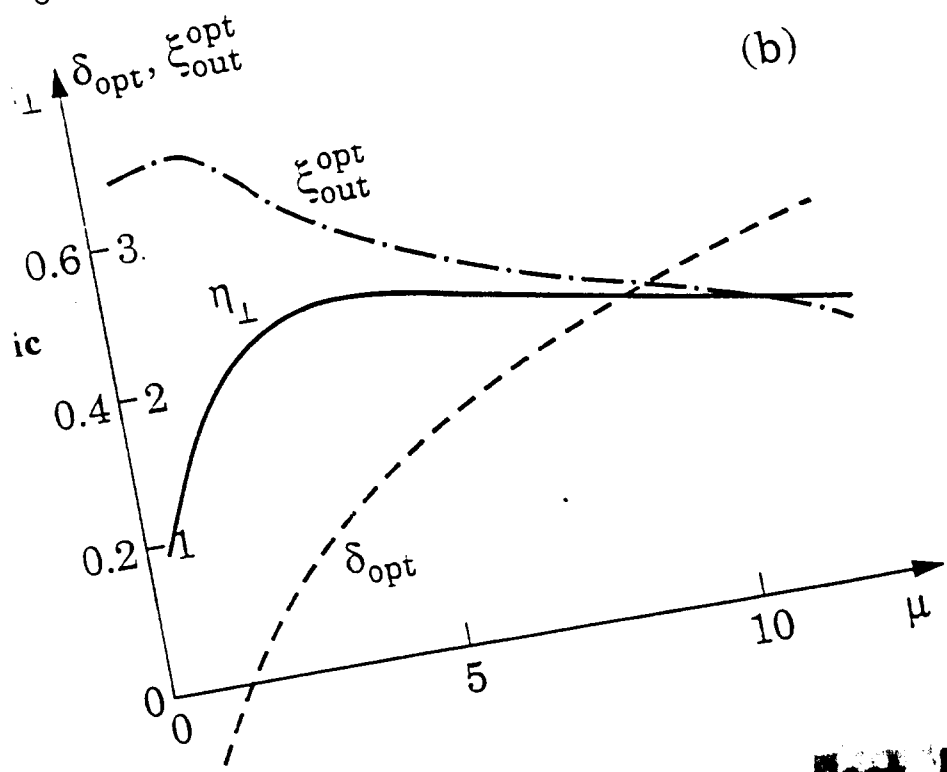
input cavity: fundamental

output cavity: second harmonic

relativistic gyrotwyston versus Output Cavity Length



(a)

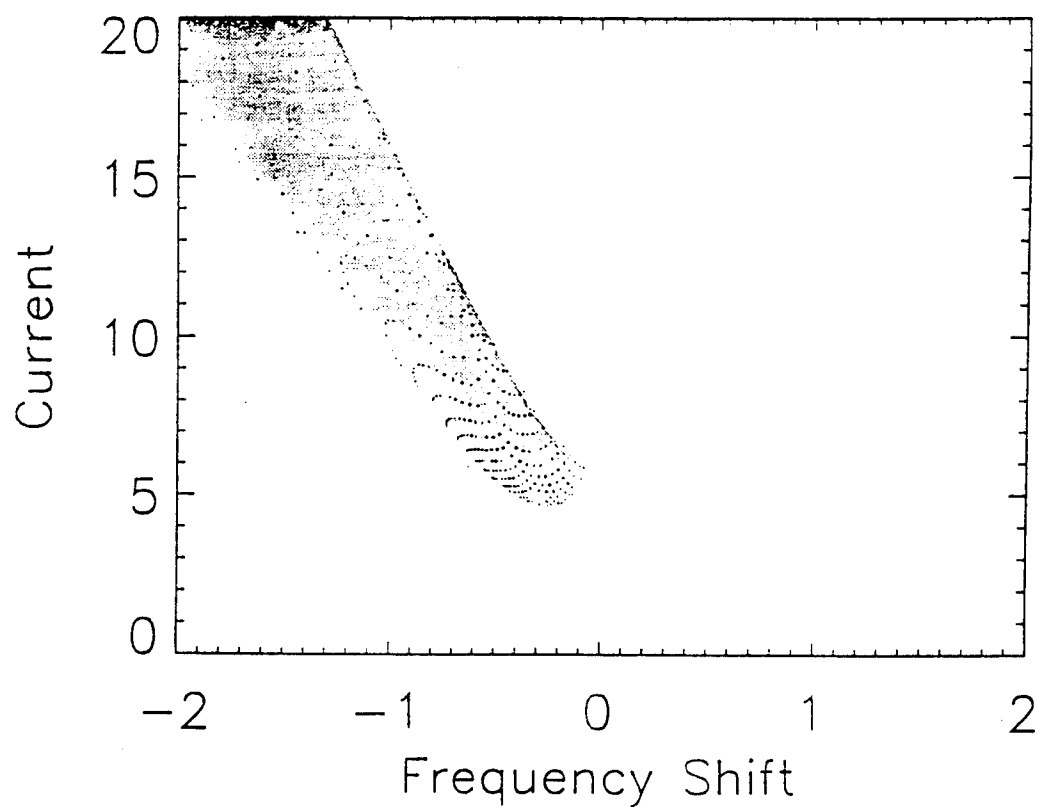


(b)

3. Theory of phase-locked gyrotrons operating at cyclotron harmonics

Locking Bandwidth versus Beam Current

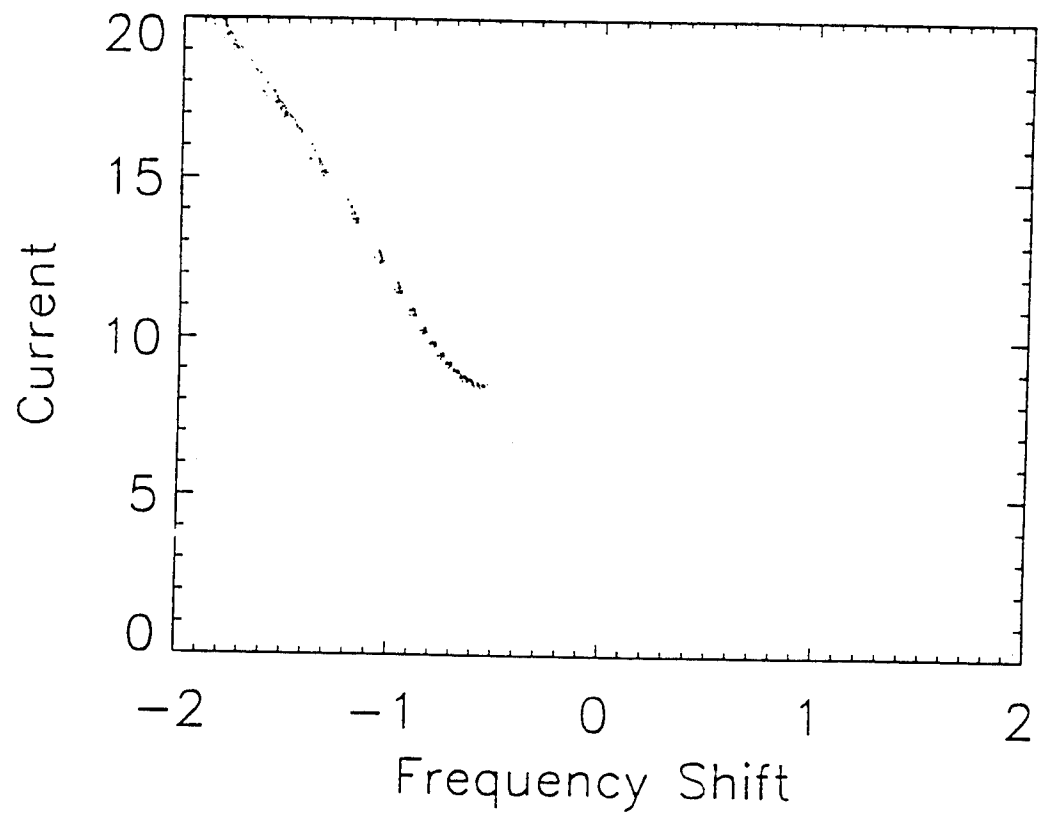
cold beam



3. Theory of phase-locked gyrotrons operating at cyclotron harmonics

Locking Bandwidth versus Beam Current

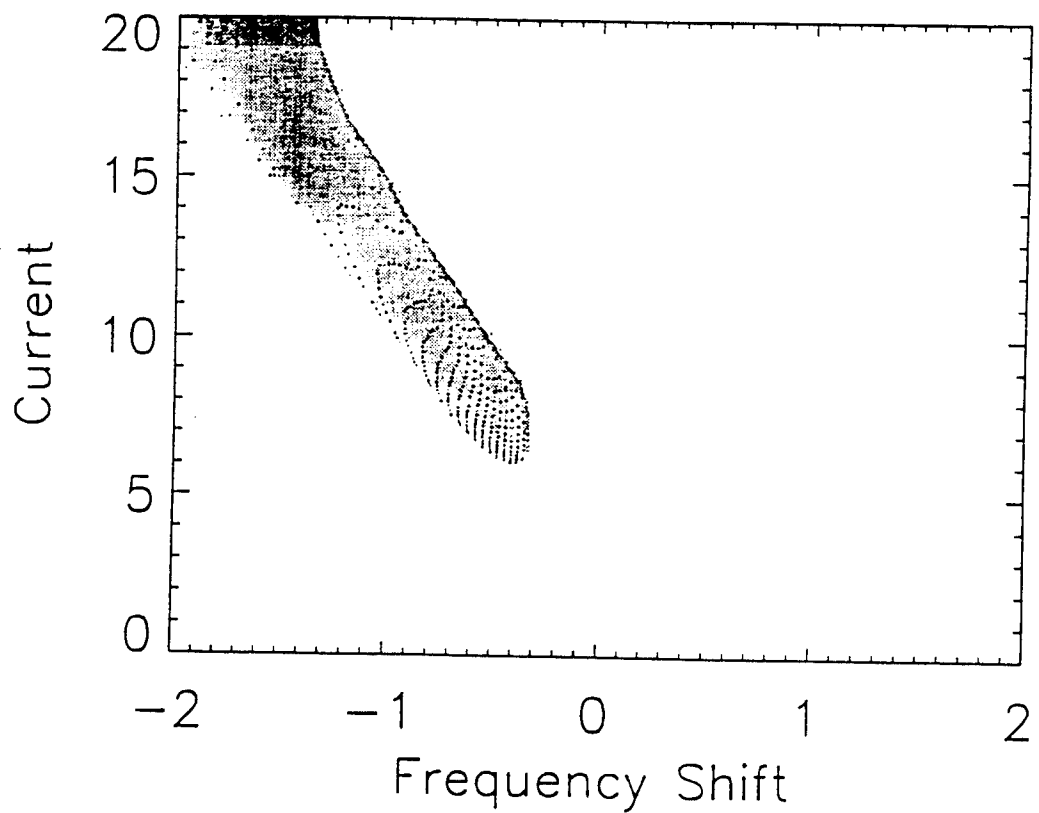
$$\delta\alpha/\alpha = .2$$



3. Theory of phase-locked gyrotrons operating at cyclotron harmonics

Locking Bandwidth versus Beam Current

$\delta\alpha/\alpha = .2$ with compensation



Current Efforts

Adapt individual models into a flexible simulation code for design and analysis of

Phase-locked harmonic gyrotron oscillators

Gyro-klystrons

Gyro-twistrons

Phigtrons

Included effects

Frequency multiplication

Multiple sections

Backward waves

NUMERICAL SIMULATION OF SLOW WAVE DEVICES

MODELING OF

vacuum backward wave oscillators

plasma filled backward wave oscillators

EXAMPLES

homogeneous slow wave structure

effect of the finite pulse duration

cyclotron absorption effect

effect of the non-synchronous harmonic

effect of plasma

non-homogeneous slow wave structure

efficiency enhancement

THEORETICAL MODEL

- representation of the field

$$E(x,t) = \{\varepsilon_{-}(z,t)e^{i(k_{-}z - \omega t)} E_p(x,k_{-}) + \varepsilon_{+}(z,t)e^{i(k_{+}z - \omega t)} E_p(x,k_{+})\} + c.c$$

$$B(x,t) = \{\varepsilon_{-}(z,t)e^{i(k_{-}z - \omega t)} B_p(x,k_{-}) + \varepsilon_{+}(z,t)e^{i(k_{+}z - \omega t)} B_p(x,k_{+})\} + c.c$$

$\varepsilon_{\pm}(z,t) \rightarrow$ slowly varying envelope

$$E_p(x, k_{\pm})$$

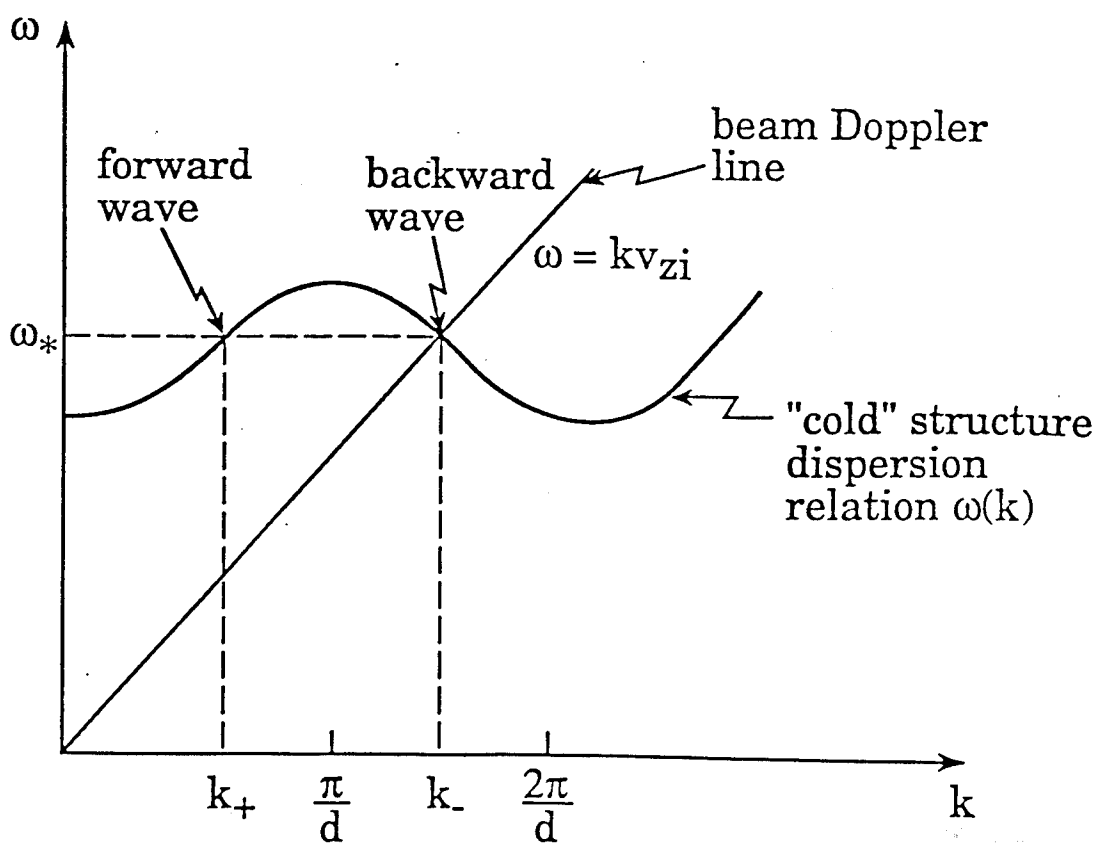
periodic functions

$$B_p(x, k_{\pm})$$

$$E_p(x, k_{\pm}) = \sum_n E_n(x_{\perp}, k_{\pm}) e^{ink_0 z}$$

$$k_0 = \frac{2\pi}{d}$$

$$B_p(x, k_{\pm}) = \sum_n B_n(x_{\perp}, k_{\pm}) e^{ink_0 z}$$



$$\frac{\partial \epsilon_-}{\partial t} + v_{g,-} \frac{\partial \epsilon_-}{\partial z} = - \int_0^d dz$$

$$\int_0^{2\pi/\omega} dt \int d^2 \mathbf{x}_\perp \mathbf{E}_p^*(\mathbf{x}, k_-) \cdot \mathbf{j} e^{-i(k_- z - \omega t)} / U, \quad (9)$$

- electromagnetic energy per $|\epsilon^2|$ contained in one period

$$U = \int_0^d dz \int d^2 \mathbf{x}_\perp \frac{|\mathbf{E}_p|^2 + |\mathbf{B}_p|^2}{4\pi} \quad (10)$$

- group velocity for the vacuum backward electromagnetic wave

$$v_{g,-} = \int_0^d dz \int d^2 \mathbf{x}_\perp \frac{c}{4\pi} \vec{z}_0 \cdot (\mathbf{E}_p(\mathbf{x}, k_-) \times \mathbf{B}_p^*(\mathbf{x}, k_-)) / U \quad (11)$$

- particle motion

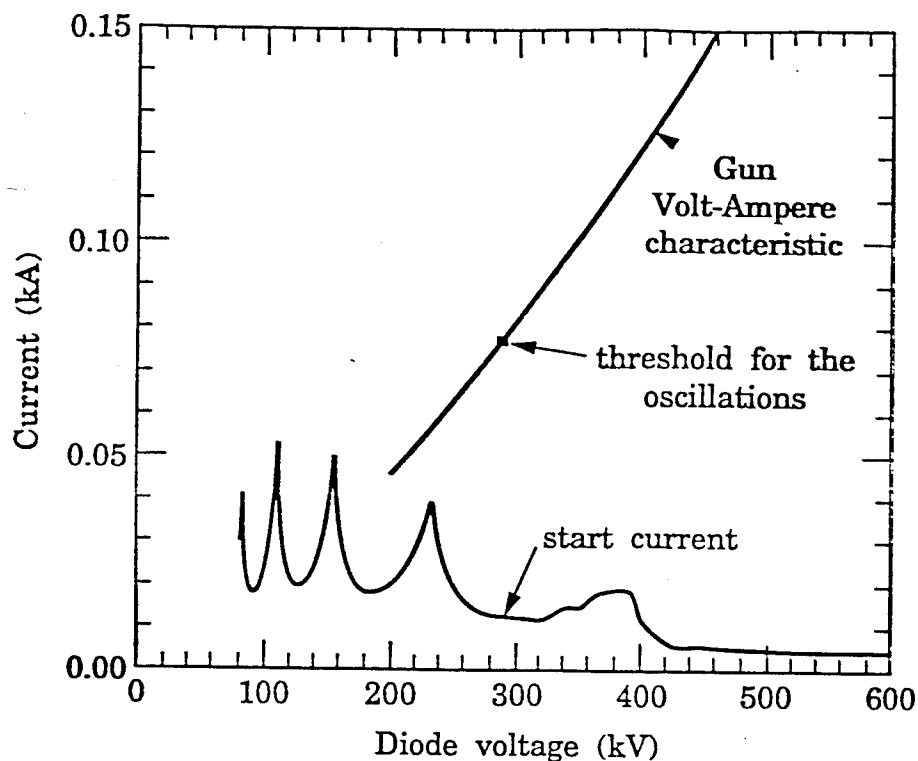
$$\frac{dp}{dt} = q \left[E + \frac{\mathbf{v}}{c} \times (B + B_{ext}) \right]$$

$$\frac{d\mathbf{x}}{dt} = \mathbf{v}$$

- assume that only two spatial harmonics of the backward wave can interact strongly with the beam

$$E(x,t) = \varepsilon_- e^{i(k_- z - \omega t)} \left[a_0 E_0(x, k_-) + a_{-1} E_{-1}(x, k_-) e^{-i(k_0 z)} \right] + c.c$$

$$B(x,t) = \varepsilon_- e^{i(k_- z - \omega t)} \left[a_0 B_0(x, k_-) + a_{-1} B_{-1}(x, k_-) e^{-i(k_0 z)} \right] + c.c$$



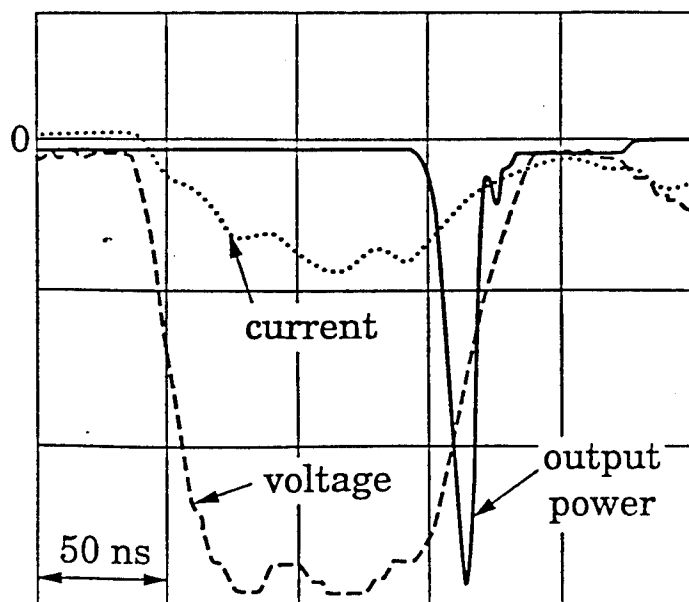
$$d = 1.67 \text{ cm}$$

$$L = 8d$$

$$r_{\text{max}} = 1.9$$

$$r_{\text{min}} = 1.1$$

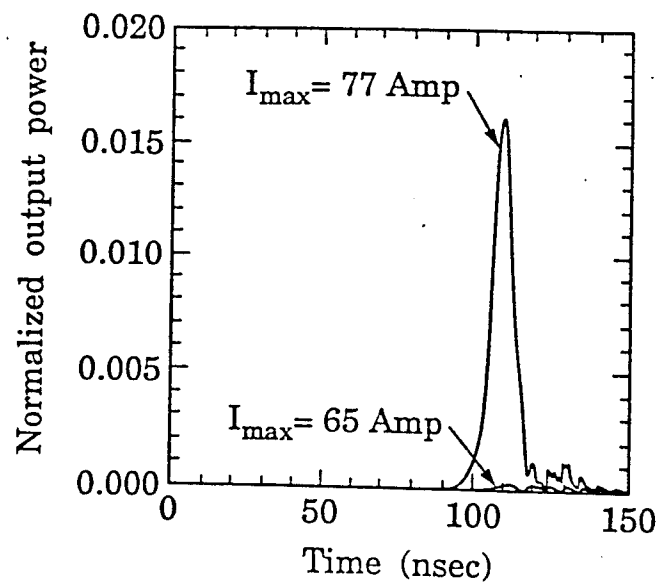
experiment

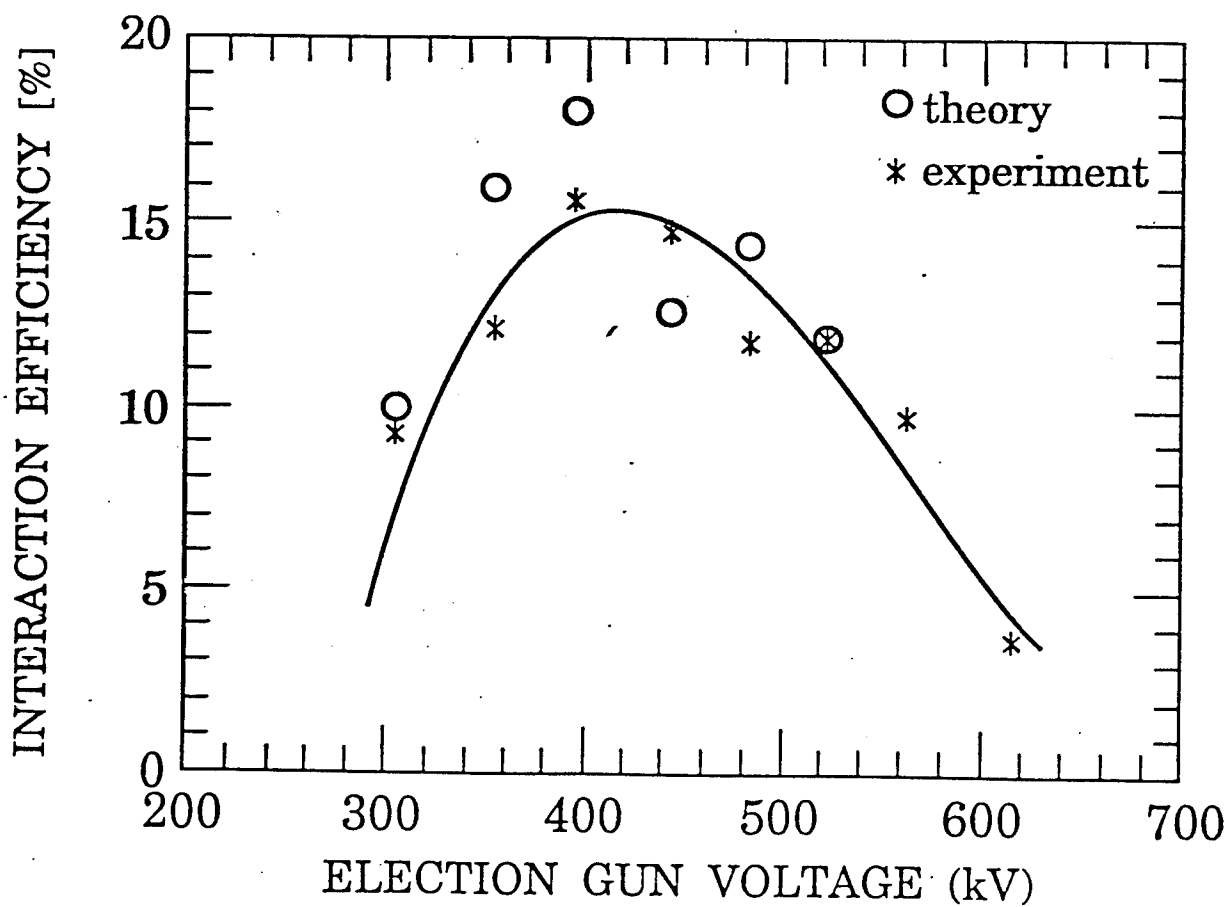
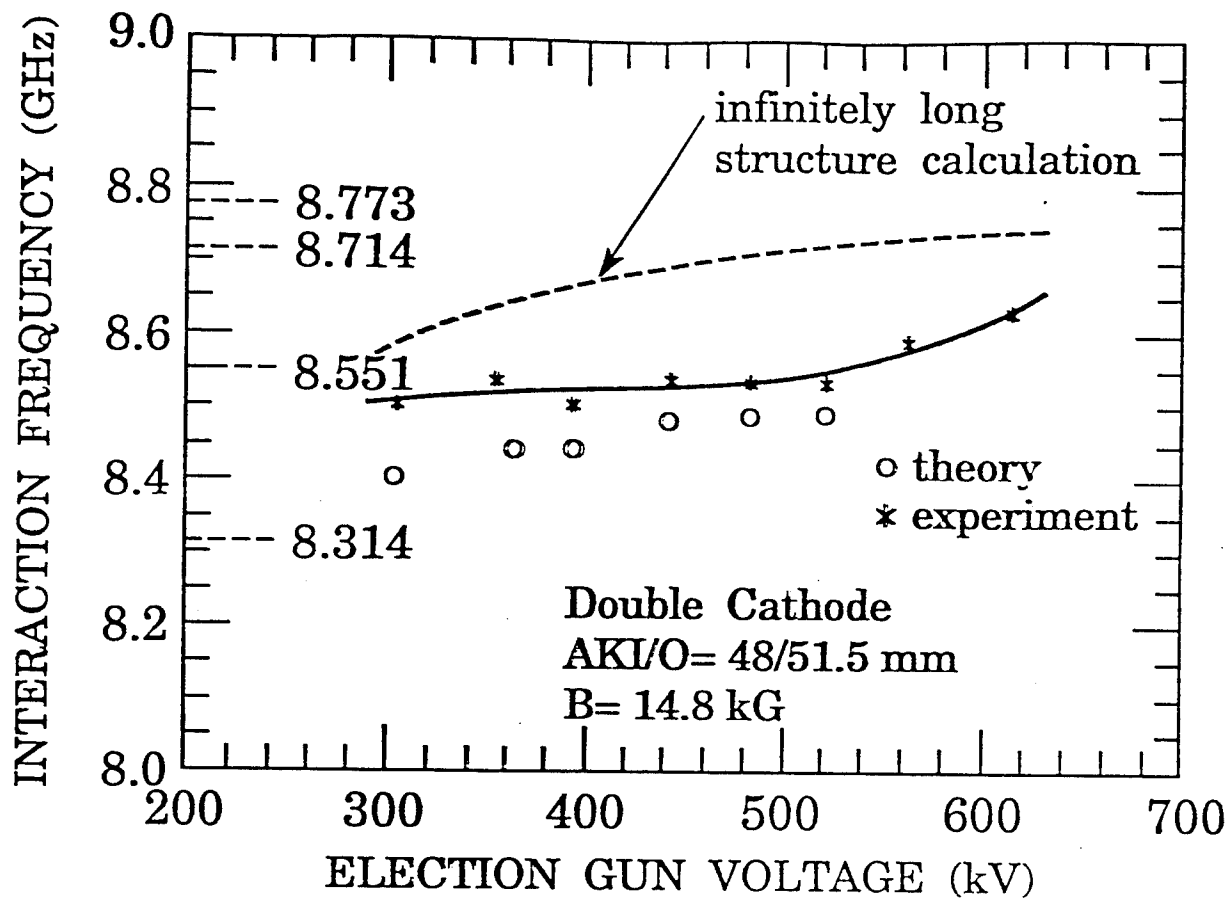


$$V_{\text{max}} = 289 \text{ kV}$$

$$I_{\text{max}} = 77 \text{ A}$$

theory

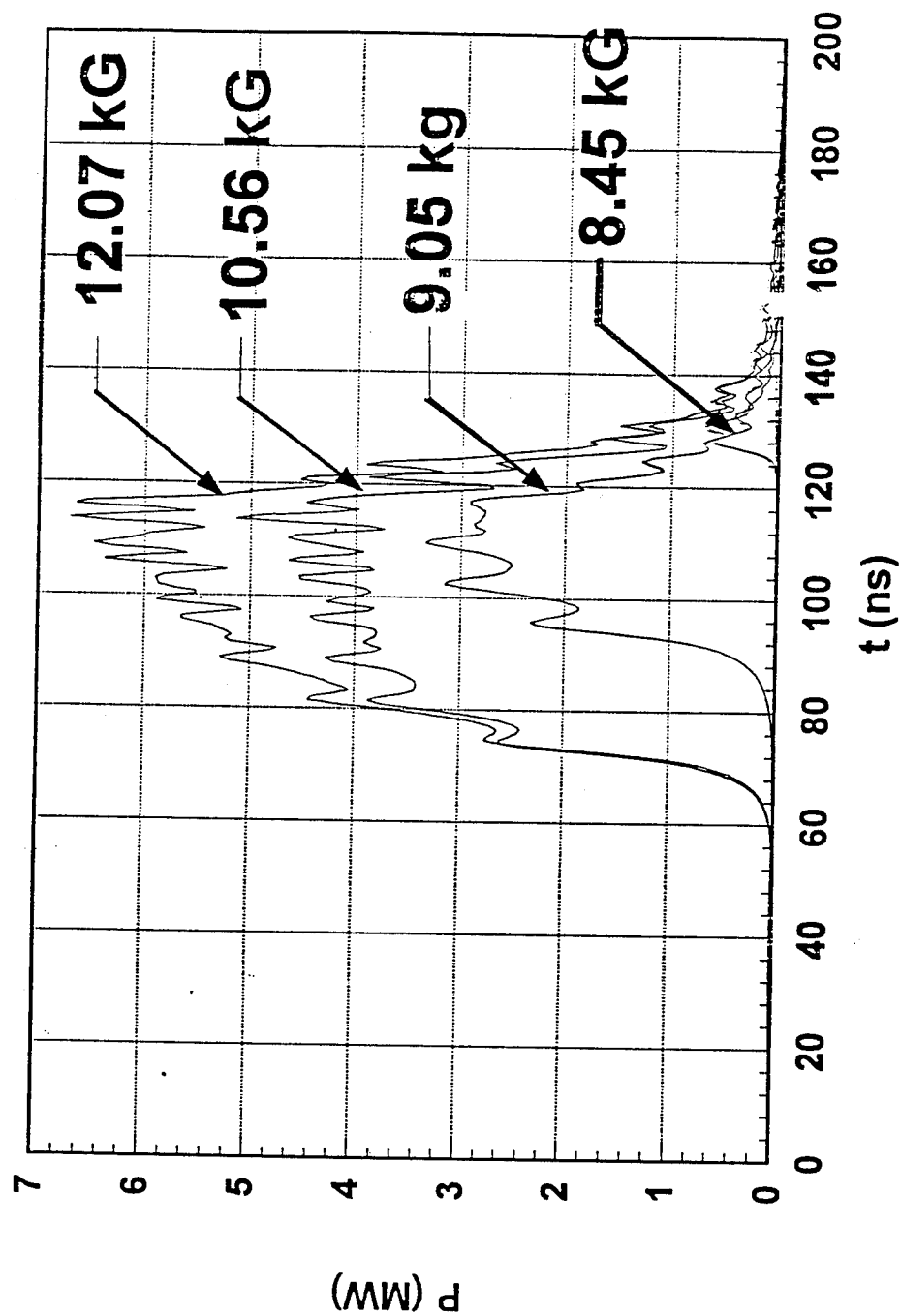




$$I = 110 \text{ A}$$

$$V = 412 \text{ kV}$$

Cyclotron Absorption Effect

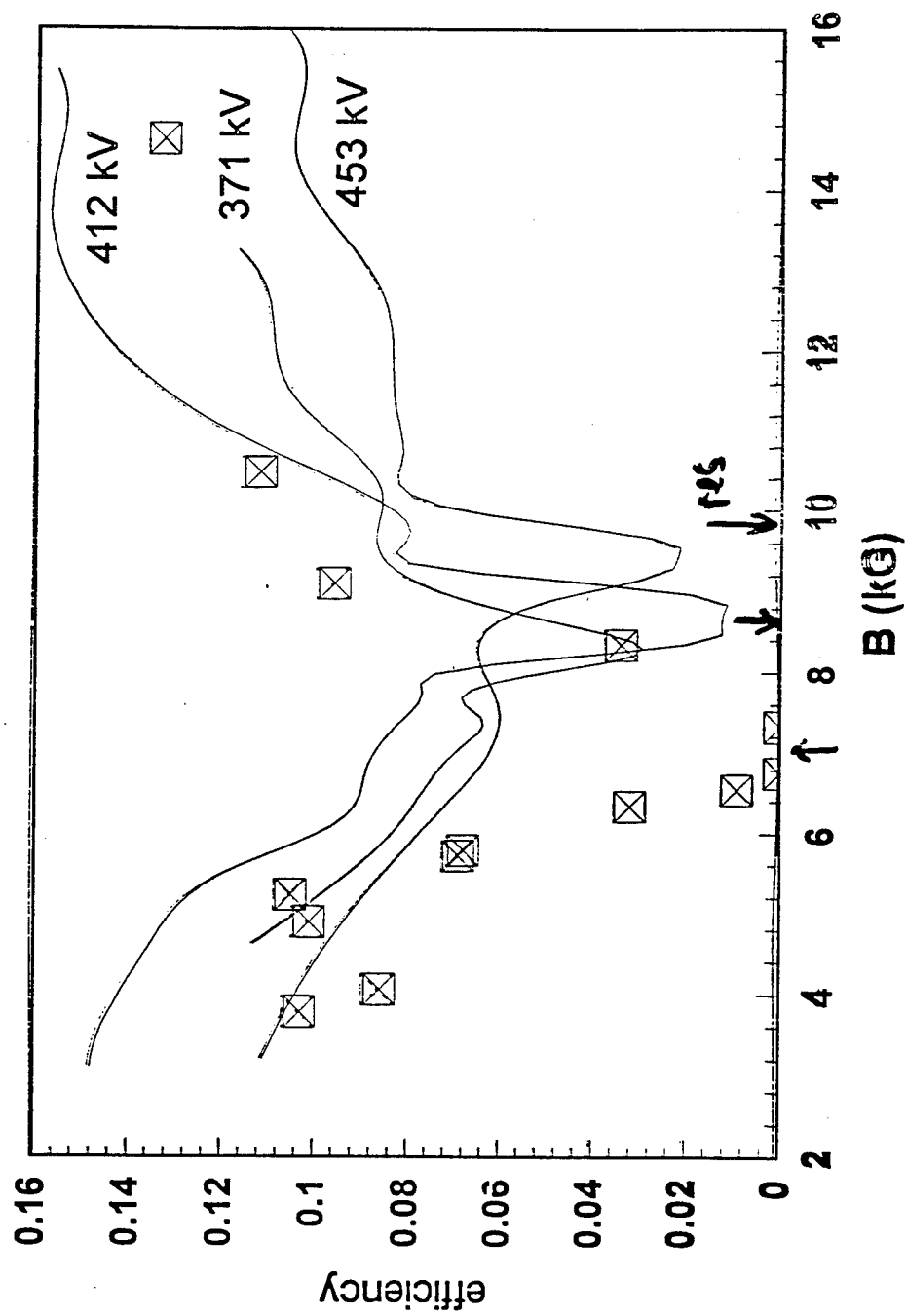


$$\beta_{res} \approx 9.6 \text{ kG}$$

$$\beta_{sim} \approx 8.5 \text{ kG}$$

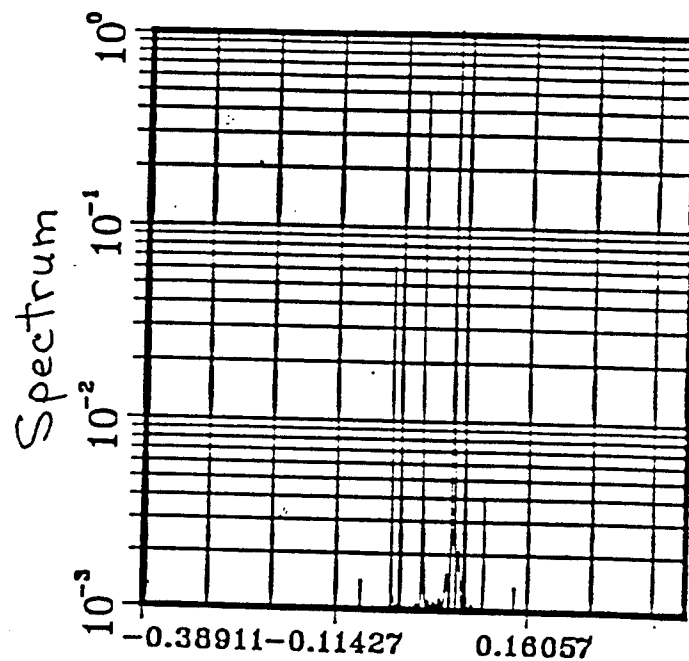
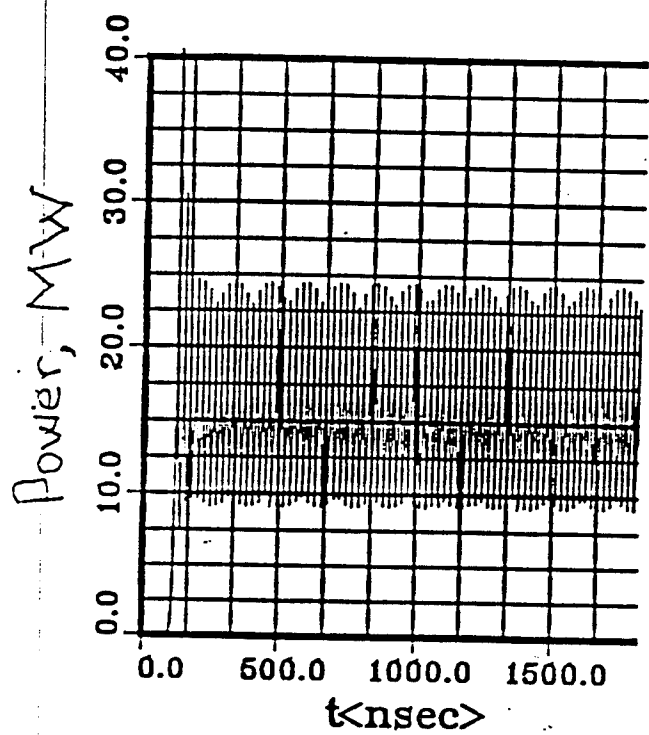
$$\beta_{exp} \approx 7.3 \pm 0.3$$

Cyclotron Absorption Effect

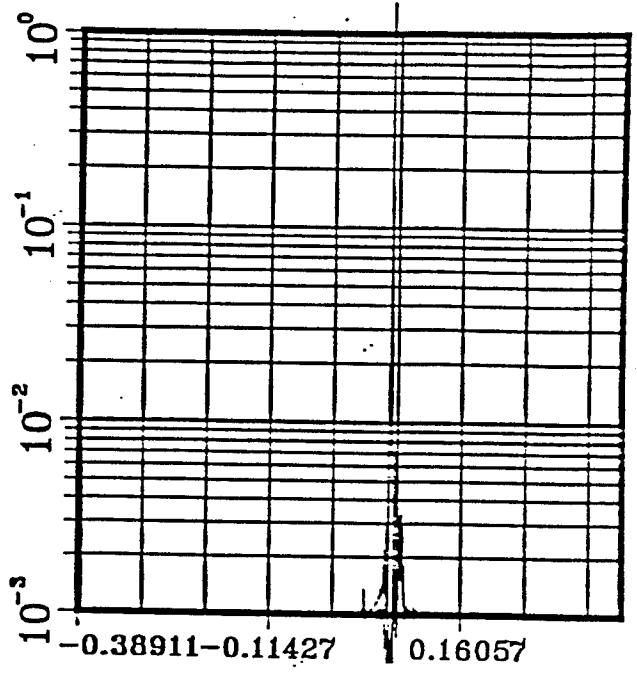
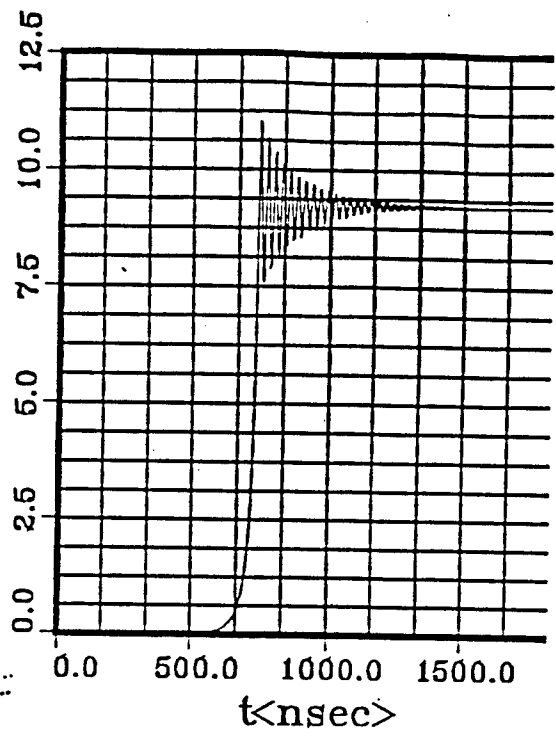


$$\theta_{ws} = \frac{mc}{q} \frac{2\pi}{d} (\alpha\beta)$$

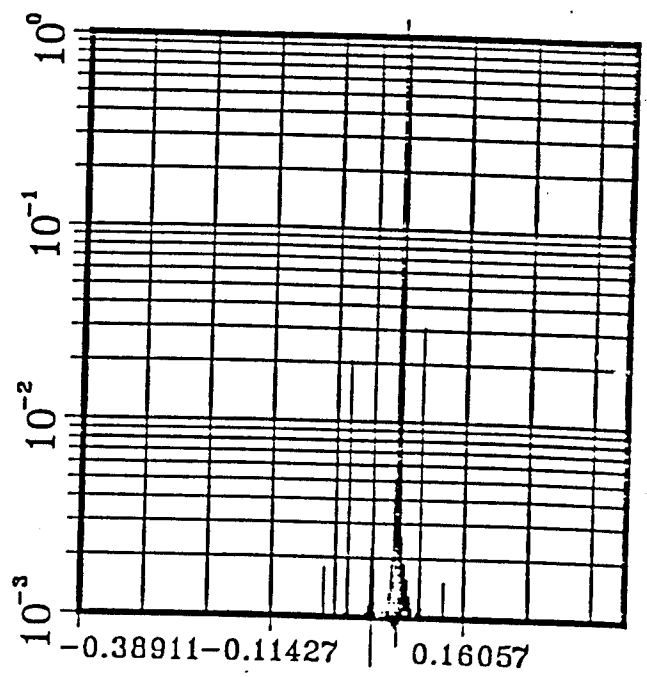
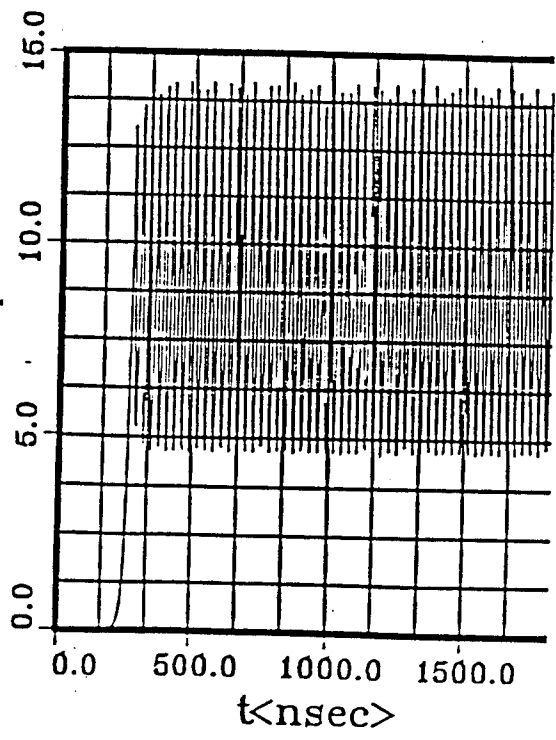
Only the synchronous harmonic



$$\psi = 0$$



$$\psi = \frac{\pi}{6}$$



Modeling of plasma filled Backward Wave Oscillator

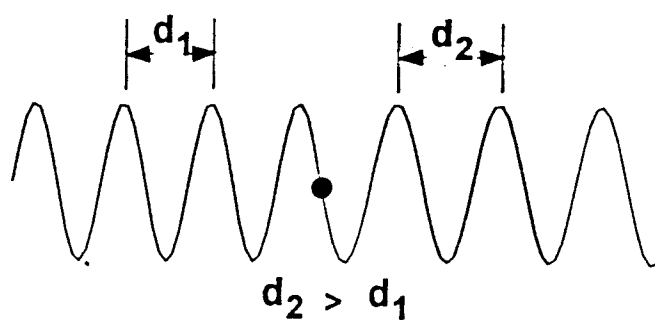
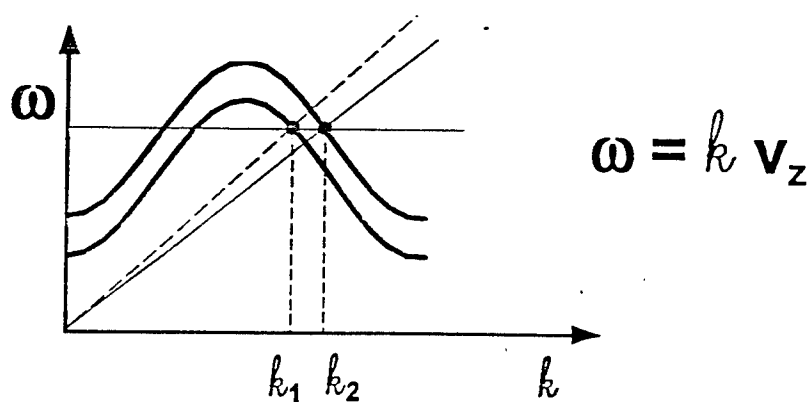
Ph. D. Thesis

Susan Miller

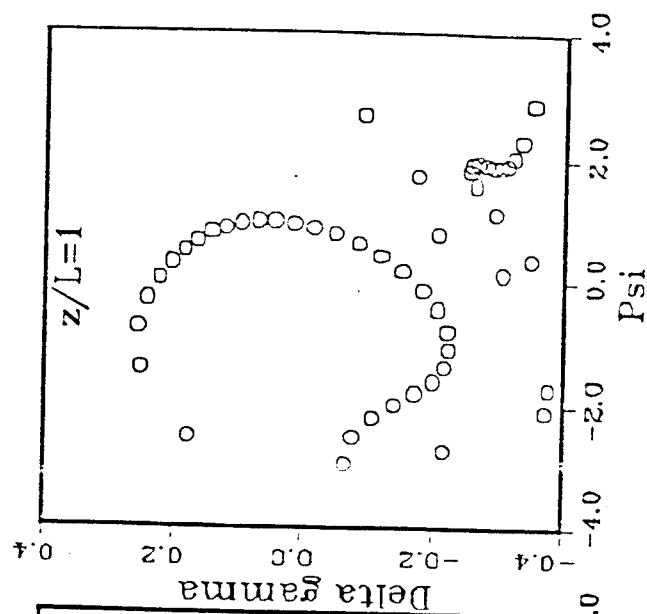
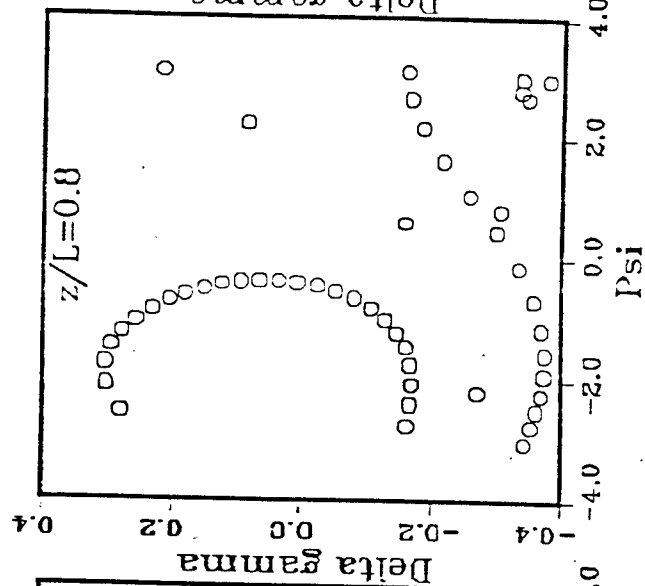
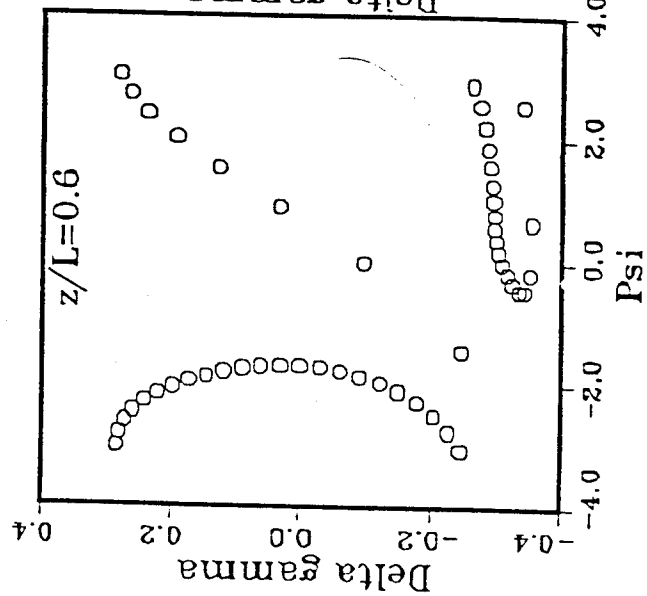
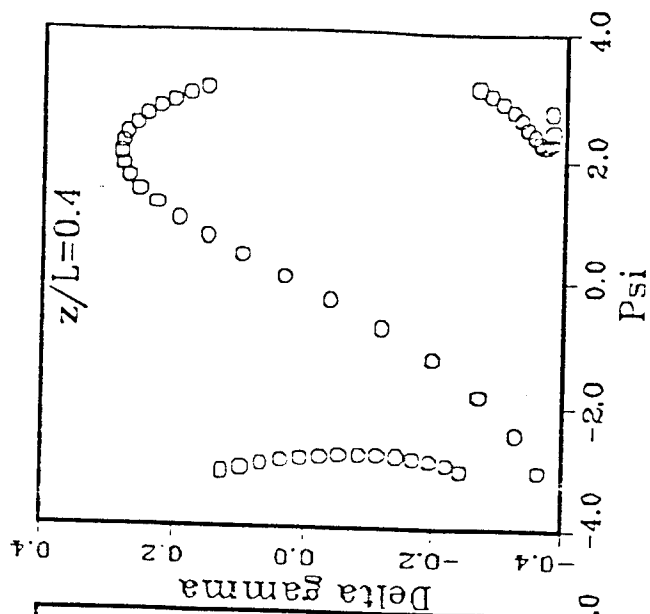
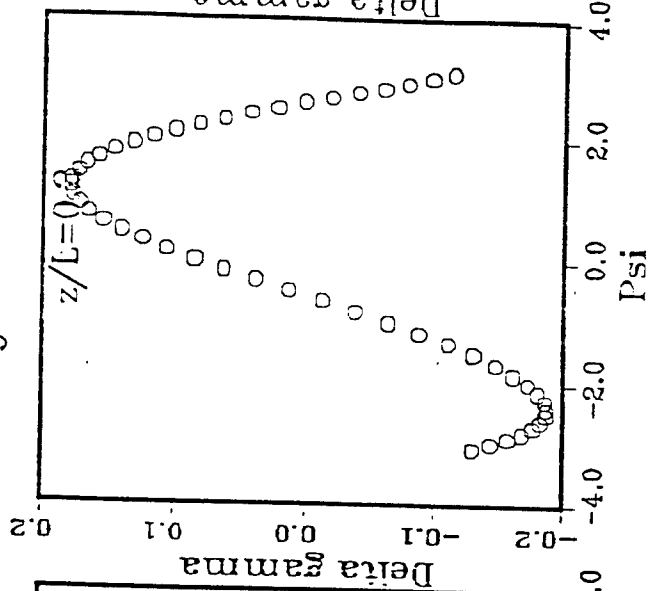
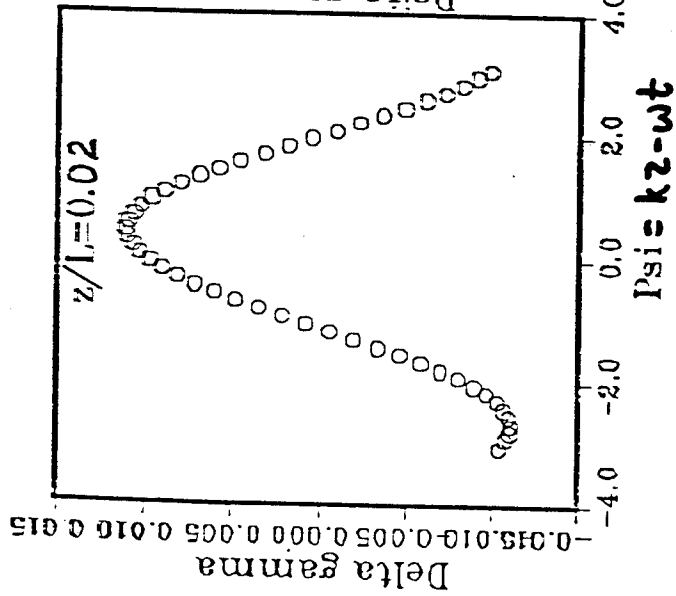
Efficiency enhancement of relativistic backward wave oscillator

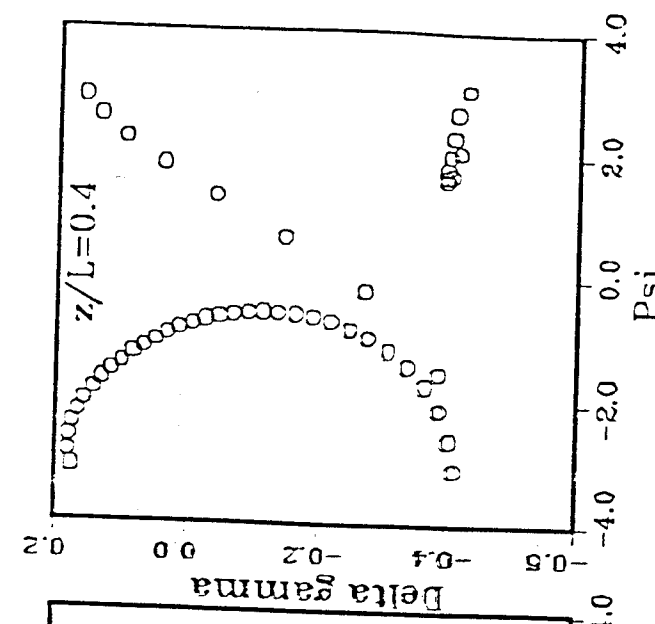
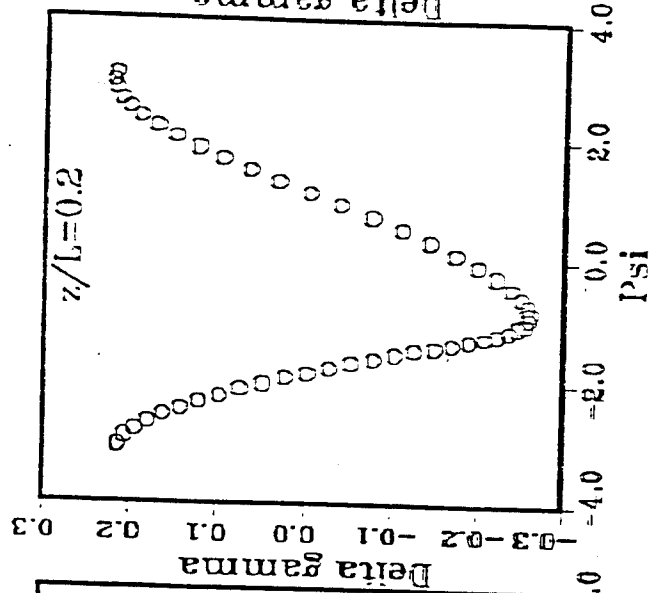
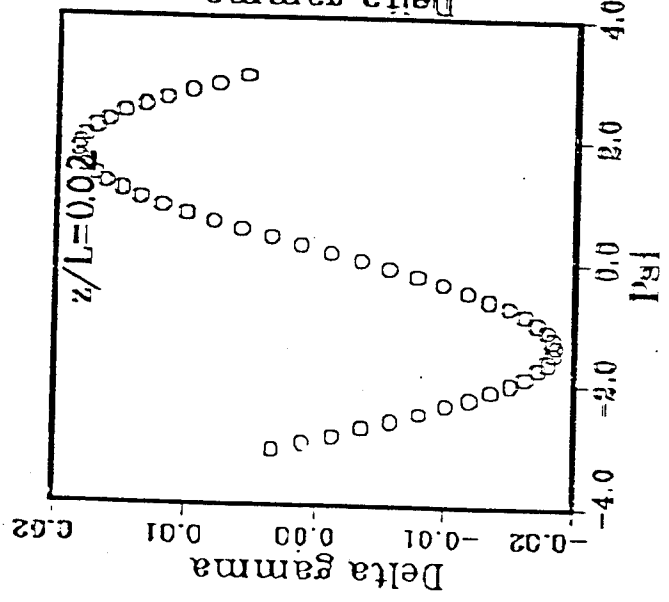
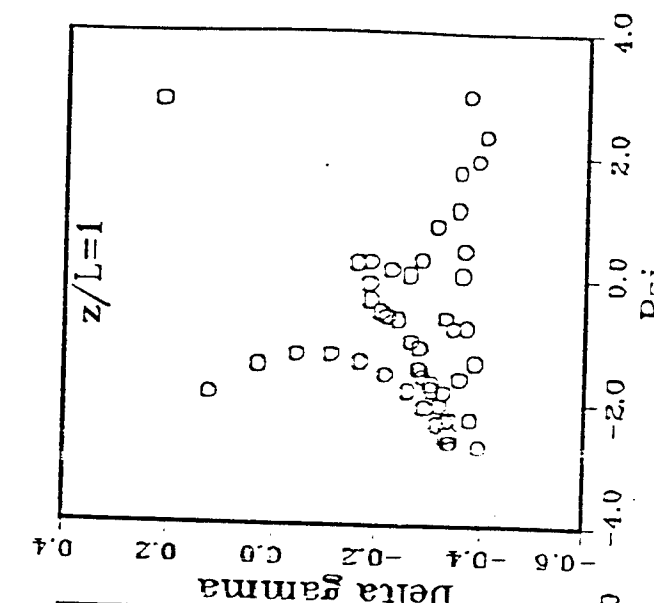
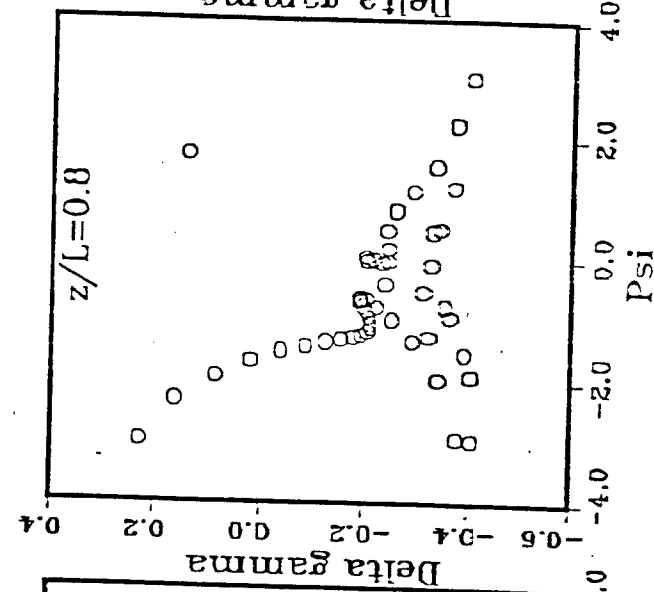
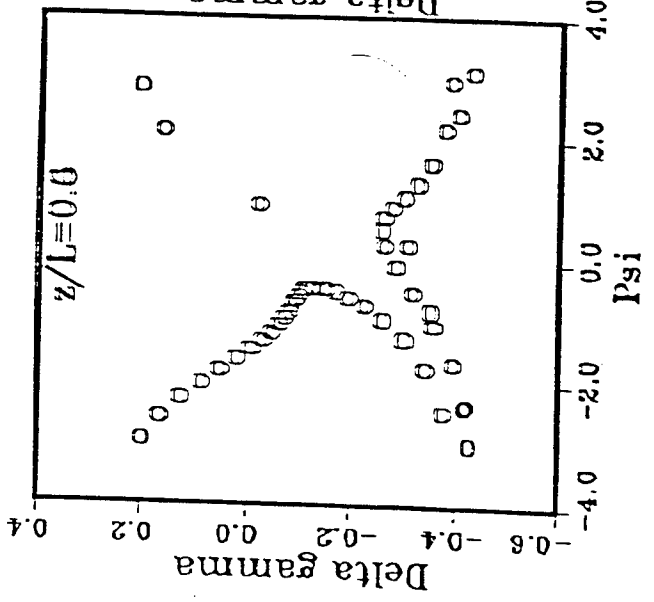
- **vary coupling impedance
along the interaction region**
- **sudden increase in phase
velocity of the synchronous
wave.**

Efficiency enhancement of high power relativistic backward wave oscillator

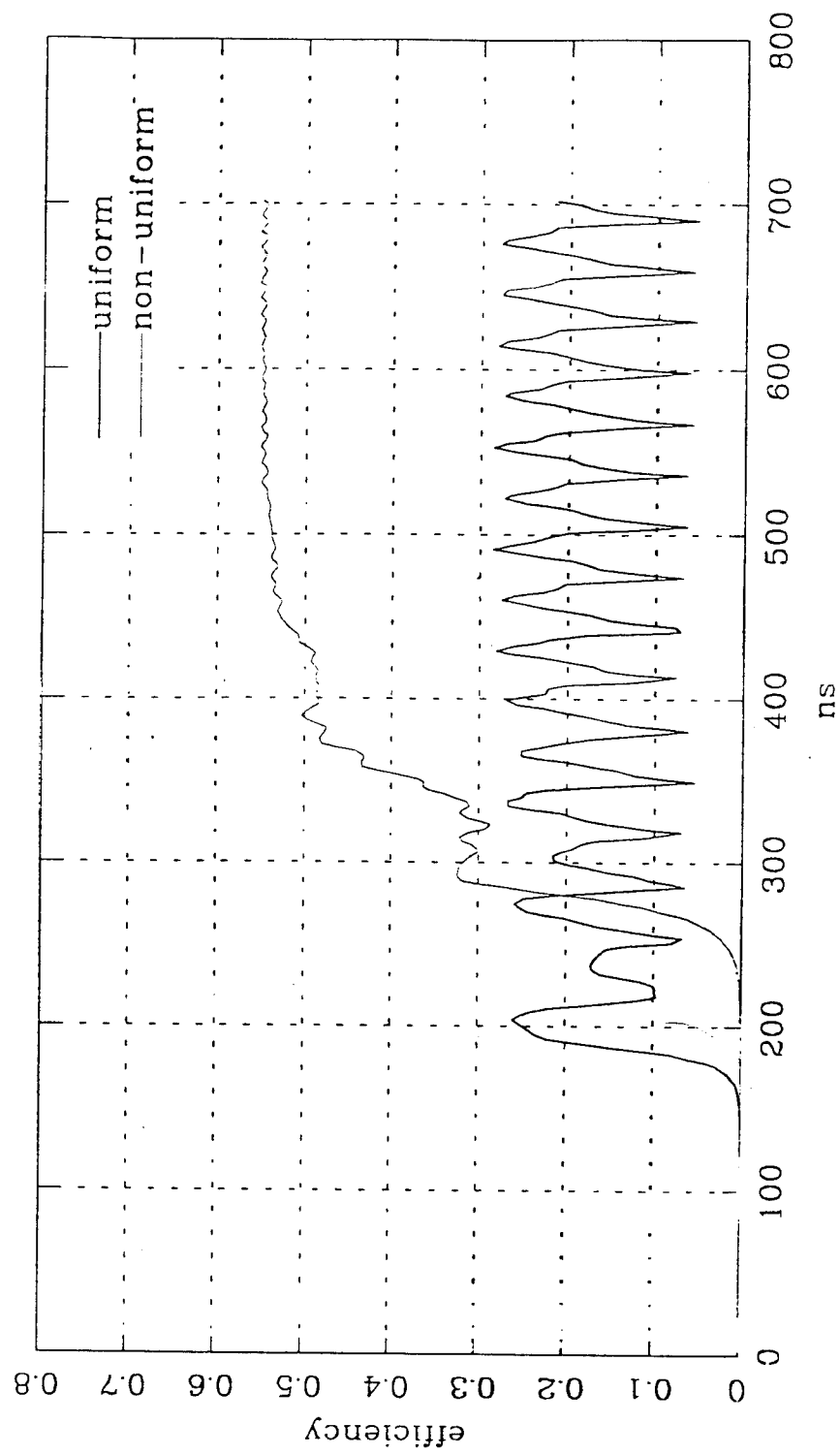


$$(\delta(z) - \delta_i)/\delta_i$$

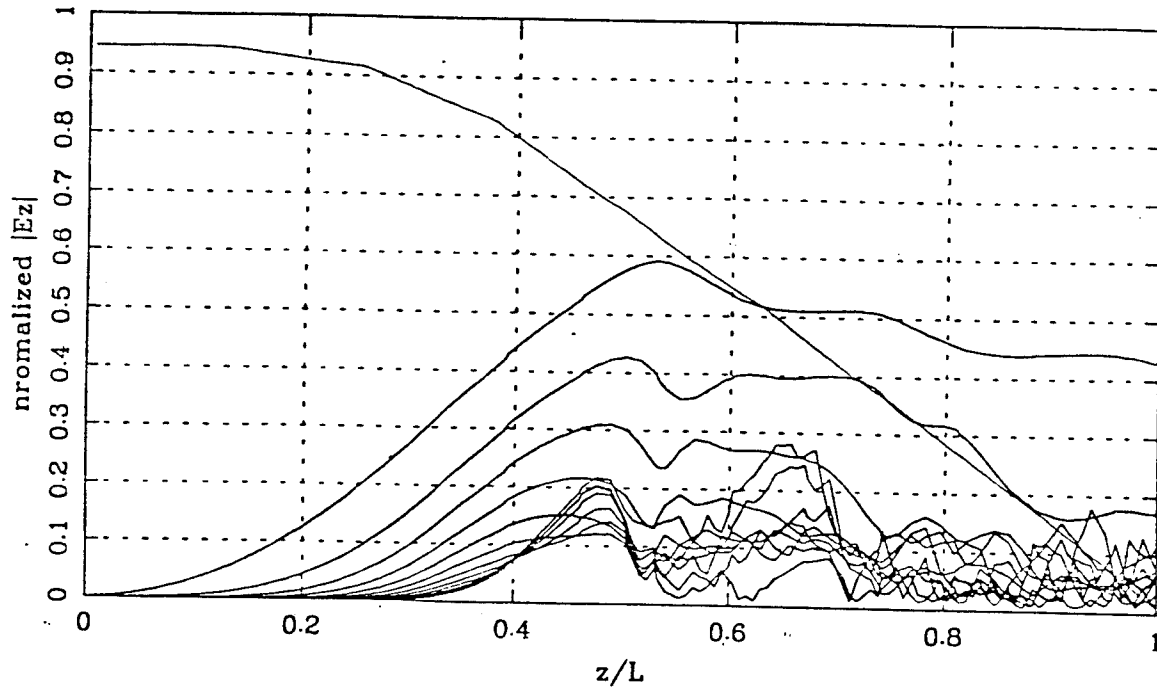




Efficiency vs. time (500 keV & 100 A beam)
with space charge neglected for uniform
and non-uniform structures



Amplitude of synchronus field (red) and
space charge harmonics fields (black)
vs. axial distance
(500 keV & 5 kA uniform sturcture)

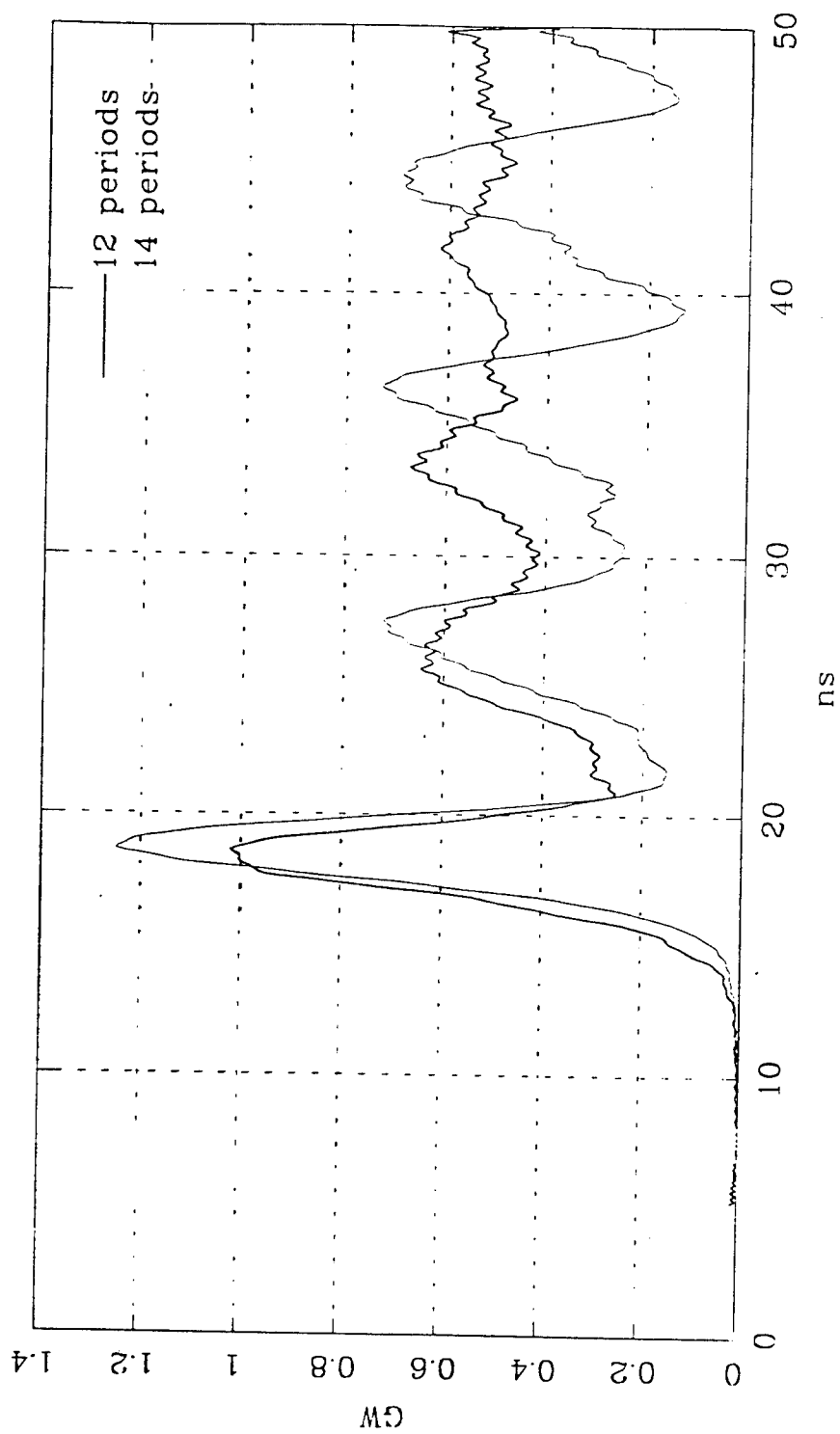


$$\frac{\partial \gamma}{\partial z} = \text{"radiation term"} - \frac{8I}{I_A k_0 r_b^2} \operatorname{Re} \left\{ \sum_{n=1}^N R_n e^{i n \psi} \langle e^{-i n \psi} \rangle \right\},$$

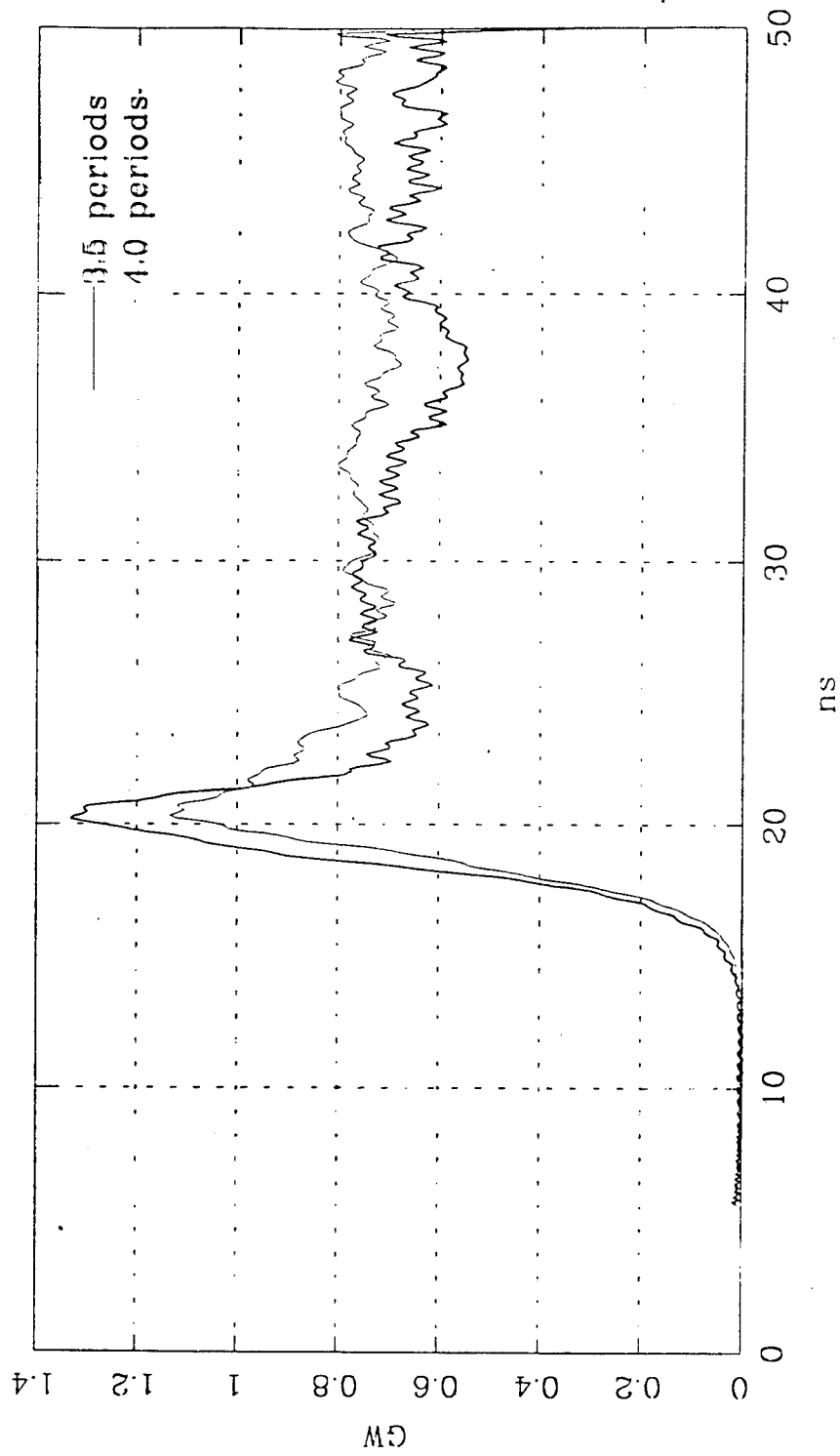
particle phase: $\psi = k \cdot z - \omega t$

R_n = geometric space charge reduction factor

MAGIC simulation of S-band BWO
with uniform structure
(12 and 14 periods long)
Output power vs. time



MAGIC simulation of S-band BWO
with non-uniform structure
(transition at 3.5 and 4.0 periods)
Output power vs. time



Current efforts

PIC modeling of non-homogenous structures

modeling of plasma filled backward wave oscillator

Possible new efforts

adopting our models to simulate multi-frequency phenomenon in slow wave devices such as TWT's

- 1. self-excitation of spurious oscillations**
- 2. simultaneous amplification of a number of signals at different frequencies**