



Mechanical Properties of Ferroelectric Composite Thin Films Fabricated by the Pulsed Laser Deposition Method

by Costas G. Fountzoulas
and Somnath Sengupta

ARL-TR-1673

May 1998

19980714 064

Approved for public release; distribution is unlimited.

The findings in this report are not to be construed as an official Department of the Army position unless so designated by other authorized documents.

Citation of manufacturer's or trade names does not constitute an official endorsement or approval of the use thereof.

Destroy this report when it is no longer needed. Do not return it to the originator.

Army Research Laboratory

Aberdeen Proving Ground, MD 21005-5066

ARL-TR-1673

May 1998

Mechanical Properties of Ferroelectric Composite Thin Films Fabricated by the Pulsed Laser Deposition Method

Costas G. Fountzoulas, Somnath Sengupta
Weapons and Materials Research Directorate, ARL

Approved for public release; distribution is unlimited.

Abstract

Barium strontium titanium oxide (BSTO) ferroelectric films of various nominal thicknesses were deposited by the pulsed laser deposition (PLD) technique on single crystals of sapphire at substrate temperatures varying from 30° C to 700° C. X-ray analysis showed that the thin films were amorphous up to 500° C, while at 700° C, they were polycrystalline. The microstructure of the thin films was columnar at all substrate temperatures. The film microhardness increased with increasing substrate temperature. While the cohesion failure load of the films remained fairly constant, the adhesion failure load increased with increasing substrate temperature.

Table of Contents

	<u>Page</u>
List of Figures	v
List of Tables	v
1. Introduction	1
2. Experimental Procedure	2
3. Results and Discussion	3
3.1 SEM Analysis	3
3.2 Microhardness	5
3.3 Cohesion and Adhesion Failure Load	5
4. Conclusions	7
5. Future Plans	8
6. References	9
Distribution List	11
Report Documentation Page	13

INTENTIONALLY LEFT BLANK.

List of Figures

<u>Figure</u>	<u>Page</u>
1. Thornton's Structure Zone Model for Coatings Produced by Sputtering	2
2. SEM Photomicrograph of Fracture Cross Section of a BSTO Film ($T_s/T_m = 0.15$)	4
3. Column Size of BSTO Films vs. T_s/T_m	5
4. Knoop Microhardness of BSTO Films vs. T_s/T_m	6
5. Cohesion Failure Load of BSTO Films vs. T_s/T_m	6
6. Adhesion Failure Load of BSTO Films vs. T_s/T_m	7

List of Tables

<u>Table</u>	<u>Page</u>
1. Column Size, Cohesion and Adhesion Failure Load, and Knoop Microhardness of BSTO Films vs. T_s/T_m	4

INTENTIONALLY LEFT BLANK.

1. Introduction

The concept of electronic thin film deposition at lower temperatures is desirable because it enables the integration of several device fabrication steps. However, the inherent material properties required for any application have to be maintained at the lower deposition temperatures. In the case of electronic thin films used for tunable dielectric applications, these properties include dielectric constant, voltage tunability, and the electronic loss tangent. However, the mechanical integrity of the thin film (i.e., the adhesion and cohesion) is just as important.

It is well known that the substrate temperature T_s , the ambient gas pressure, and the energy of any incoming ions influence the growth conditions and, therefore, the film structure produced under low-pressure conditions (Movchan and Demchishin 1969; Thornton 1977; Fountzoulas and Nowak 1991). A structural classification system that has gained the broad acceptance for thin films produced by the physical vapor deposition (PVD) process has been presented by Movchan and Demchishin (1969). They proposed three zones to describe the microstructures that can develop in deposits produced by vacuum evaporation as a function of T_s/T_m , where T_s is the absolute substrate temperature and T_m is the absolute melting temperature of the deposited material. Thornton (1977) elaborated on the approach of Movchan and Demchishin, extending it to typical sputtering conditions. Thornton also concluded that the structure and physical properties of films produced by sputtering could be represented as a function of T_s/T_m , in terms of four zones as shown in Figure 1, each with its own characteristic structure and physical properties. The general features of Thornton's model were based on the examination of 25- to 250- μm -thick coatings deposited at argon pressures 1.33×10^{-4} (1 mTorr) to 3.9×10^{-3} Pa (30 mTorr) using cylindrical-post and hollow cathode magnetron sputtering sources. Fountzoulas and Nowak (1991) further elaborated on the approach of Movchan and Thornton, extending it to ion plating.

We have initiated an investigation of the cohesive and adhesive properties of dielectric thin films of barium strontium titanium oxide (BSTO) deposited on single crystal substrates by the pulsed laser deposition (PLD) method (Sengupta et al. 1996; Brennan 1992; Lee, Ramesh, and Keramidas 1995).

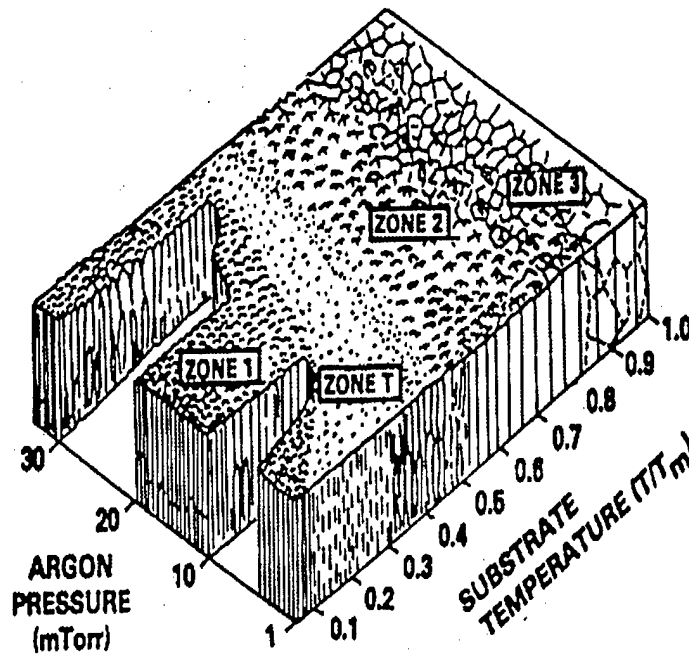


Figure 1. Thornton's Structure Zone Model for Coatings Produced by Sputtering (Thornton 1977).

This report presents the initial results of this study of these mechanical properties of BSTO thin films as a function of deposition temperature.

2. Experimental Procedure

In this work, thin films of BSTO were deposited by the PLD technique on single crystal sapphire substrates at room temperatures varying from 30° C to 700° C. The details of this deposition technique are given in Sengupta and Green (1998).

The fracture cross sections of the films were observed by scanning electron microscopy (SEM). Crystallinity, crystal orientation, and composition of the films were determined by FT-RAMAN spectroscopy and glancing angle x-ray diffraction (GAXRD). The adhesive and cohesive failure

loads of the films were evaluated with the aid of a CSEM-Revetest instrument (Centre Suisse d' Electronique et de Microtechnique, CSEM, CH-20007, Neuchâtel, Switzerland).

In the specimen evaluation, the material properties of the BSTO thin films deposited at various substrate temperatures were evaluated by FT-Raman spectroscopy (Sengupta and Green 1998).

The Knoop microhardness of the coatings, uncorrected for substrate hardness effects, was measured using a 0.25-N applied load and a dwell time of 15 s. Even at this low load, the maximum indenter penetration far exceeded the critical value of 1/10 of the coating thickness considered sufficient for the substrate not to have a significant effect on hardness values.

The cohesion and adhesion values of the various coatings were evaluated primarily with a CSEM-Revetest automatic scratch apparatus. This apparatus, with a diamond stylus radius of 20 μm , and the testing procedure are described in Kattamis et al. (1993); Bhansali and Kattamis (1990); Kattamis (1993); and Steinmann, Tardy, and Hintermann (1987). The sample translation speed was held constant at 5 mm/min, and the loading rate at 5 N/min; hence, the load gradient was $dL/dx = 1 \text{ N/mm}$. The cohesion failure load (L_C) is the minimum crack initiation load within the coating, and the adhesion failure load (L_A) is the minimum load at which the crack causes massive delamination at the coating/substrate interface.

3. Results and Discussion

3.1 SEM Analysis. The microstructure of the BSTO thin film, at various substrate temperatures, was evaluated by SEM photomicrographs (Figure 2). It became apparent from the SEM photomicrographs that the Thornton structural zone 1 (Thornton 1977) was not observed. Our films can be classified in the Thornton transition (T) and structural zone 2. The column size measurements as a function of the ratio of the absolute substrate temperature (T_s) and absolute film melting temperature (T_m) (2,004 K) are shown in Table 1 and Figure 3. For T_s/T_m between 0.15 and 0.19, the average column size increased from 190 nm to 230 nm. For T_s/T_m between 0.19 and 0.39,

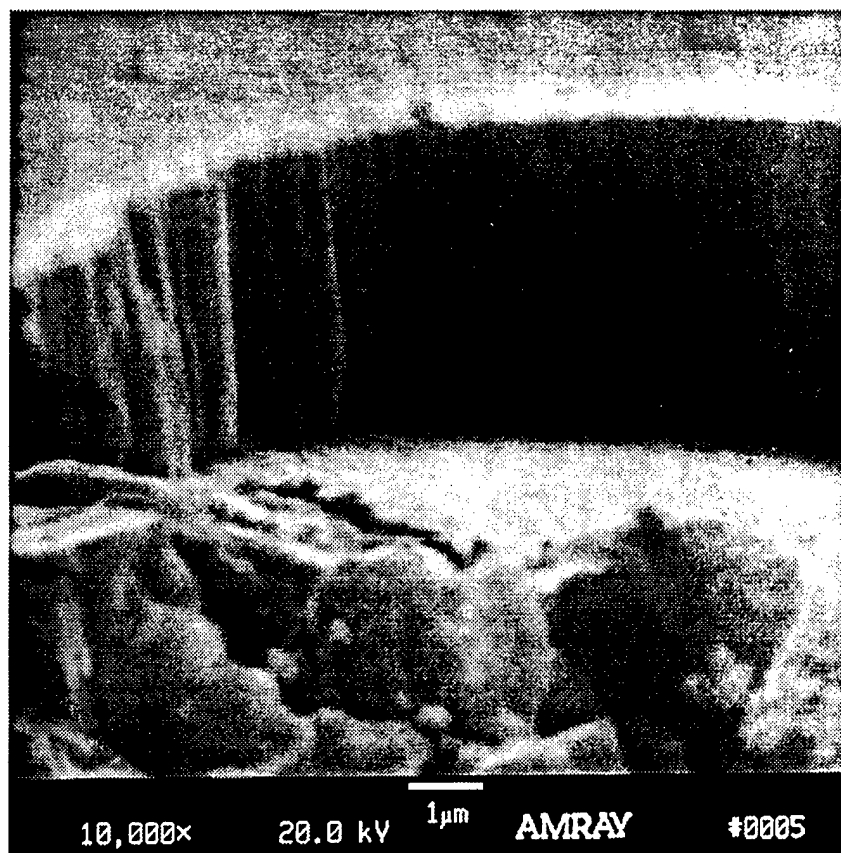


Figure 2. SEM Photomicrograph of Fracture Cross Section of a BSTO Film ($T_s / T_m = 0.15$).

Table 1. Column Size, Cohesion and Adhesion Failure Load, and Knoop Microhardness of BSTO Films vs. T_s / T_m

T_s / T_m	Thickness (nm)	Column Size (nm)	L_C (Cohesion Load) (N)	L_A (Adhesion Load) (N)	Knoop Microhardness (GPa)
0.15	1,000	190	11.63	16.06	1.3
0.19	2,200	230	13.75	18.75	1.5
0.29	1,000	250	13.65	38.22	5.7
0.39	1,000	220	12.96	22.68	6.6
0.49	3,000	2,007	12.32	24.08	7.0

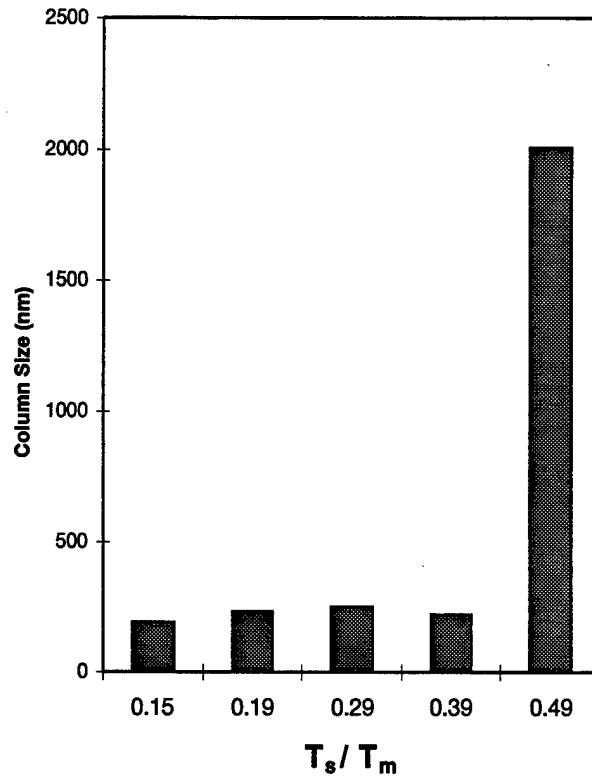


Figure 3. Column Size of BSTO Films vs. T_s / T_m .

the average column size remains practically constant. At $T_s / T_m = 0.49$, where the film is fully crystalline, the column size increases dramatically to 2,007 nm.

3.2 Microhardness. The Knoop microhardness of the BSTO films, uncorrected for the substrate hardness effect, ranged between 1.3 GPa and 7 GPa. Table 1 and Figure 4 show Knoop microhardness values as a function of T_s / T_m . The film microhardness increased with increasing T_s / T_m ratio and increasing film crystallinity. The highest Knoop microhardness was obtained at the highest temperature ($T_s / T_m = 0.49$).

3.3 Cohesion and Adhesion Failure Load. Measured average values of cohesion failure load (L_C) and adhesion failure load (L_A) are listed in Table 1. The cohesion failure load of the films remained fairly constant, independent of the substrate temperature (Figure 5). The average cohesion failure load of the film was about 13 N. The adhesion failure load of the films increased with

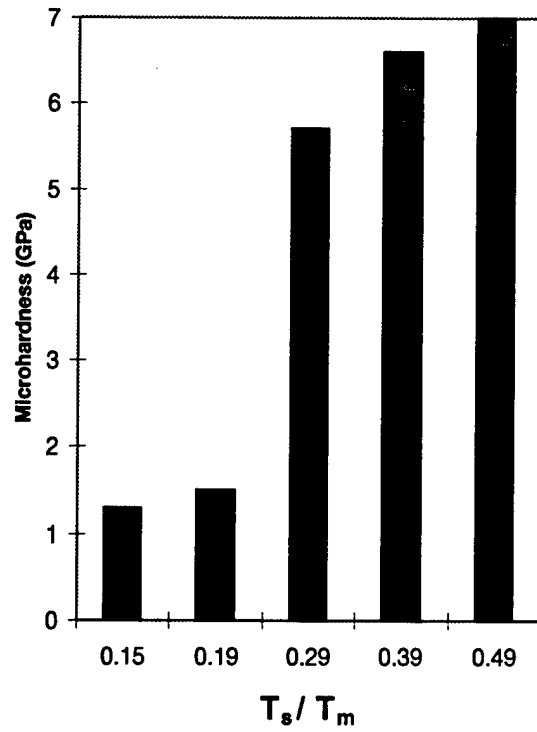


Figure 4. Knoop Microhardness of BSTO Films vs. T_s / T_m .

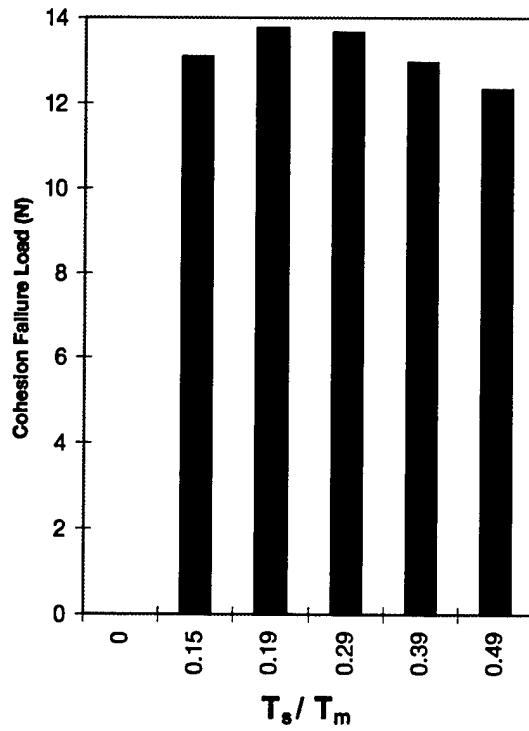


Figure 5. Cohesion Failure Load of BSTO Films vs. T_s / T_m .

increasing T_s/T_m ratio (Figure 6). However, for reasons currently not understood, for $T_s/T_m = 0.25$, the adhesion failure load exhibited a peak at a ratio of 0.29.

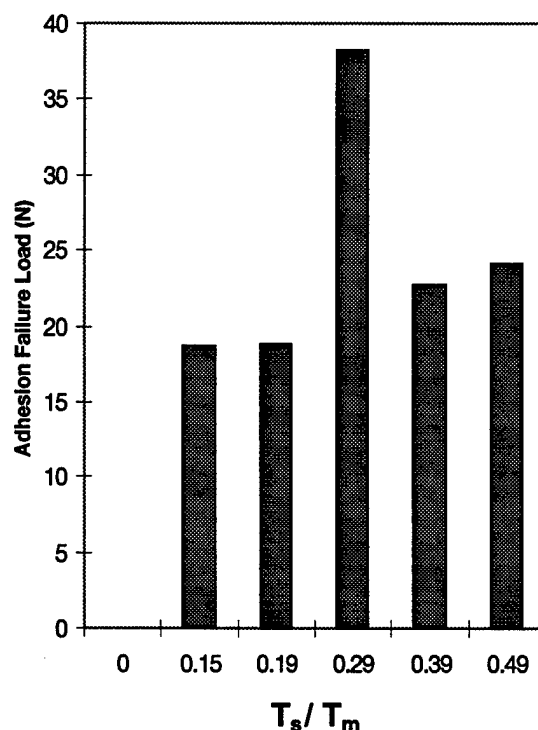


Figure 6. Adhesion Failure Load of BSTO Films vs. T_s/T_m .

4. Conclusions

The structure, crystallinity, cohesion and adhesion failure loads, and microhardness of BSTO thin films produced by PLD were correlated with the substrate temperature. For the entire temperature range, 278–973 K, the films were columnar and the column size increased with increasing substrate temperature. For $T_s/T_m \leq 0.29$, they could be categorized as being in the transition (T) Thornton structural zone, while for $T_s/T_m > 0.29$, they corresponded to the Thornton structural zone 2 category. The film was amorphous up to 373 K, partially crystalline from 573 to 973 K, and fully crystalline at 973 K. The cohesion failure load was constant for the entire substrate temperature range. The

adhesion failure load and microhardness increased with increasing thin film crystallinity and substrate temperature.

5. Future Plans

The microstructure evolution of the BSTO films as a function of the substrate temperature, laser pulse energy, and oxygen pressure will be further studied in order to construct a more comprehensive structure zone model for PLD BSTO films produced by the technique.

6. References

- Bhansali, K. J., and T. Z. Kattamis. *Wear*, vol. 141, p. 59, 1990.
- Brennan, C. J. *Integrated Ferroelectrics*, vol. 2, p. 73, 1992.
- Fountzoulas, C., and W. B. Nowak. *Journal of Vac. Sci. Technol.*, vol. A 9, no. (4), p. 2128, July/August 1991.
- Kattamis, T. Z. *Journal of Adhesion Sci. Technol.*, vol. 7, p. 783, 1993.
- Kattamis, T. Z., K. J. Bhansali, M. Levy, R. Adler, and S. Ramalingam. *Mater. Sci. Eng.*, vol. A 161, p. 105, 1993.
- Lee, J., R. Ramesh, and V. G. Keramidas. *MRS Symposium Proceedings*, vol. 361, p. 67, 1995.
- Movchan, B. A., and S. V. Demchishin. *Phys. Met. Metallogr.*, vol. 28, p. 653, 1969.
- Sengupta, S., L. C. Sengupta, D. P. Vijay, and S. B. Desu. *Journal of Integrated Ferroelectrics*, vol. 13, pp. 239–245, 1996.
- Sengupta, S., and S. M. Green. *Journal of Applied Surface Science*, in print, 1998.
- Steinmann, A., Y. Tardy, and H. E. Hintermann. *Thin Solid Films*, vol. 154, p. 333, 1987.
- Thornton, J. A. *Annual. Rev. Mater. Sci.*, vol. 7, p. 239, 1977.

INTENTIONALLY LEFT BLANK.

NO. OF COPIES	ORGANIZATION
2	DEFENSE TECHNICAL INFORMATION CENTER DTIC DDA 8725 JOHN J KINGMAN RD STE 0944 FT BELVOIR VA 22060-6218
1	HQDA DAMO FDQ DENNIS SCHMIDT 400 ARMY PENTAGON WASHINGTON DC 20310-0460
1	DPTY ASSIST SCY FOR R&T SARD TT F MILTON RM 3EA79 THE PENTAGON WASHINGTON DC 20310-0103
1	OSD OUSD(A&T)/ODDDR&E(R) J LUPO THE PENTAGON WASHINGTON DC 20301-7100
1	CECOM SP & TRRSTRL COMMCTN DIV AMSEL RD ST MC M H SOICHER FT MONMOUTH NJ 07703-5203
1	PRIN DPTY FOR TCHNLGY HQ US ARMY MATCOM AMCDCG T M FISETTE 5001 EISENHOWER AVE ALEXANDRIA VA 22333-0001
1	DPTY CG FOR RDE HQ US ARMY MATCOM AMCRD BG BEAUCHAMP 5001 EISENHOWER AVE ALEXANDRIA VA 22333-0001
1	INST FOR ADVNCD TCHNLGY THE UNIV OF TEXAS AT AUSTIN PO BOX 202797 AUSTIN TX 78720-2797

NO. OF COPIES	ORGANIZATION
1	GPS JOINT PROG OFC DIR COL J CLAY 2435 VELA WAY STE 1613 LOS ANGELES AFB CA 90245-5500
1	ELECTRONIC SYS DIV DIR CECOM RDEC J NIEMELA FT MONMOUTH NJ 07703
3	DARPA L STOTTS J PENNELLA B KASPAR 3701 N FAIRFAX DR ARLINGTON VA 22203-1714
1	US MILITARY ACADEMY MATH SCI CTR OF EXCELLENCE DEPT OF MATHEMATICAL SCI MDN A MAJ DON ENGEN THAYER HALL WEST POINT NY 10996-1786
1	DIRECTOR US ARMY RESEARCH LAB AMSRL CS AL TP 2800 POWDER MILL RD ADELPHI MD 20783-1145
1	DIRECTOR US ARMY RESEARCH LAB AMSRL CS AL TA 2800 POWDER MILL RD ADELPHI MD 20783-1145
3	DIRECTOR US ARMY RESEARCH LAB AMSRL CI LL 2800 POWDER MILL RD ADELPHI MD 20783-1145
	<u>ABERDEEN PROVING GROUND</u>
4	DIR USARL AMSRL CI LP (305)

INTENTIONALLY LEFT BLANK.

REPORT DOCUMENTATION PAGE			Form Approved OMB No. 0704-0188	
Public reporting burden for this collection of information is estimated to average 1 hour per response, including the time for reviewing instructions, searching existing data sources, gathering and maintaining the data needed, and completing and reviewing the collection of information. Send comments regarding this burden estimate or any other aspect of this collection of information, including suggestions for reducing this burden, to Washington Headquarters Services, Directorate for Information Operations and Reports, 1215 Jefferson Davis Highway, Suite 1204, Arlington, VA 22202-4302, and to the Office of Management and Budget, Paperwork Reduction Project (0704-0188), Washington, DC 20503.				
1. AGENCY USE ONLY (Leave blank)	2. REPORT DATE May 1998	3. REPORT TYPE AND DATES COVERED Final, January 1992 - April 1998		
4. TITLE AND SUBTITLE Mechanical Properties of Ferroelectric Composite Thin Films Fabricated by the Pulsed Laser Deposition Method		5. FUNDING NUMBERS 1L162618AH80		
6. AUTHOR(S) Costas G. Fountzoulas and Somnath Sengupta				
7. PERFORMING ORGANIZATION NAME(S) AND ADDRESS(ES) U.S. Army Research Laboratory ATTN: AMSRL-WM-ME Aberdeen Proving Ground, MD 21005-5069		8. PERFORMING ORGANIZATION REPORT NUMBER ARL-TR-1673		
9. SPONSORING/MONITORING AGENCY NAME(S) AND ADDRESS(ES)		10. SPONSORING/MONITORING AGENCY REPORT NUMBER		
11. SUPPLEMENTARY NOTES				
12a. DISTRIBUTION/AVAILABILITY STATEMENT Approved for public release; distribution unlimited.		12b. DISTRIBUTION CODE		
13. ABSTRACT (Maximum 200 words) Barium strontium titanium oxide (BSTO) ferroelectric films of various nominal thicknesses were deposited by the pulsed laser deposition (PLD) technique on single crystals of sapphire at substrate temperatures varying from 30° C to 700° C. X-ray analysis showed that the thin films were amorphous up to 500° C, while at 700° C, they were polycrystalline. The microstructure of the thin films was columnar at all substrate temperatures. The film microhardness increased with increasing substrate temperature. While the cohesion failure load of the films remained fairly constant, the adhesion failure load increased with increasing substrate temperature.				
14. SUBJECT TERMS mechanical, properties, ferroelectric, thin film		15. NUMBER OF PAGES 15		
		16. PRICE CODE		
17. SECURITY CLASSIFICATION OF REPORT UNCLASSIFIED	18. SECURITY CLASSIFICATION OF THIS PAGE UNCLASSIFIED	19. SECURITY CLASSIFICATION OF ABSTRACT UNCLASSIFIED	20. LIMITATION OF ABSTRACT UL	

INTENTIONALLY LEFT BLANK.

USER EVALUATION SHEET/CHANGE OF ADDRESS

This Laboratory undertakes a continuing effort to improve the quality of the reports it publishes. Your comments/answers to the items/questions below will aid us in our efforts.

1. ARL Report Number/Author ARL-TR-1673 (Fountzoulas) Date of Report May 1998

2. Date Report Received _____

3. Does this report satisfy a need? (Comment on purpose, related project, or other area of interest for which the report will be used.) _____

4. Specifically, how is the report being used? (Information source, design data, procedure, source of ideas, etc.) _____

5. Has the information in this report led to any quantitative savings as far as man-hours or dollars saved, operating costs avoided, or efficiencies achieved, etc? If so, please elaborate. _____

6. General Comments. What do you think should be changed to improve future reports? (Indicate changes to organization, technical content, format, etc.) _____

CURRENT
ADDRESS

Organization

Name

E-mail Name

Street or P.O. Box No.

City, State, Zip Code

7. If indicating a Change of Address or Address Correction, please provide the Current or Correct address above and the Old or Incorrect address below.

OLD
ADDRESS

Organization

Name

Street or P.O. Box No.

City, State, Zip Code

(Remove this sheet, fold as indicated, tape closed, and mail.)

(DO NOT STAPLE)