

ARMY RESEARCH LABORATORY



Shielding Effectiveness Measurements on Hardened, Transportable Facilities Using Transmission-Line Techniques

Robert Atkinson

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September 1998

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Sensors and Electron Devices Directorate

Reference: The Master Data Exchange Agreement between
the Government of the United States of America
and the Government of France
Annex No. DEA-A-80-F-1265
Title: Nuclear Weapons Effects

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Abstract

As part of science and engineering efforts between U.S. and French personnel, a testbed was devised that demonstrated an alternative approach to evaluating radio-frequency doors. The methods used multiwire transmission lines of the type generally used to perform radiated immunity measurements. Analysis of the results has provided a unique method of determining the electromagnetic susceptibility and long-term hardness-maintenance/hardness-surveillance status of critical command, control, communications, computers, and intelligence (C⁴I) facilities.

Contents

Acknowledgement	v
1. Introduction	1
1.1 Objectives	2
1.2 Personnel	2
2. Background	3
3. Impact of Study	3
4. Methodology	4
4.1 Overview	4
4.2 Transmission-Line Construction and Checkout	5
4.3 Measurement System	8
4.4 Facility and Test Environment	9
4.5 Microstrip Line Construction and Checkout	10
5. Data and Analysis	12
5.1 Environment Within Shield	12
5.2 Microstrip Measurements	13
6. Synopsis	16
Appendix A. Typical Response Data	17
Appendix B. Data File Names and Information	21
Distribution	29
Report Documentation Page	37

Figures

1. DEMOSTHENE	1
2. Schematic representation of transmission line	6
3. Initial TDR response curves for transmission line with six- and seven-wire geometries	8
4. Test and measurement setups	9
5. Typical knife-edge door seam construction	10
6. Microstrip line characteristics	11
7. Measured current on vertical wire	12
8. Measured current on a horizontal wire	13
9. Aperture response characteristics	14
10. Strip line response at six aperture positions	15

Tables

1. List of personnel	2
2. Aperture SE (approximate)	15

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C'est notre très agréable devoir de présenter les plus vifs remerciements à nos collègues scientifiques du CEG pour leur aide, direction, et amitié, sans lesquels le travail ici décrit n'aurait pu avoir lieu. Nous leur dédions ce rapport.

1. Introduction

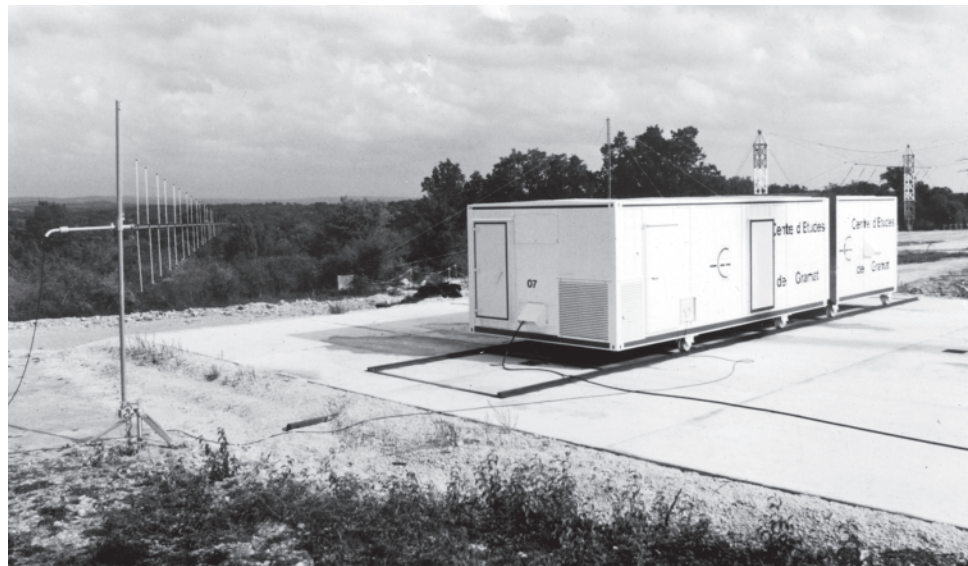
A feasibility study was undertaken by the U.S. Army Research Laboratory (ARL) and the Centre d'Etudes de Gramat (CEG) to evaluate the impact of degradation in radio-frequency (rf) shielded door systems that are typically found on tactical, nuclear-survivable command, control, and communications (C³I) shelters. This study took place under Annex DEA-A-80-F-1265, *Nuclear Weapons Effects*, of the Master Data Exchange Agreement (DEA) between the Government of the United States of America and the Government of France.

The study combined a unique approach to electromagnetic, free-field illumination with standard methods for measuring shielding effectiveness (SE) attenuation and degradation for ground-based command, control, communications, computers, and intelligence (C⁴I) facilities. The experiments were conducted at the CEG's DEMOSTHENE facility.

DEMOSTHENE is a French prototype of a mobile C³I facility. It is a modular, shielded structure, designed to ensure the survivability of critical communications equipment to high-altitude EMP (HEMP) effects. DEMOSTHENE (shown in fig. 1) was designed to be transportable by rail and typifies rear-echelon C³I equipment needs. Generally, it would not be found close to the forward edge of the battle area.

Presently, the prototype is set up near CEG's Horizontally Polarized Dipole (HPD) test facility, which is used to evaluate high-altitude electromagnetic pulse (HEMP) effects. Analysis of the experimental results was conducted by ARL personnel at the CEG testbed site and at ARL's Adelphi Laboratory Center, as well as by CEG personnel in France.

Figure 1.
DEMOSTHENE.



1.1 Objectives

This recent feasibility study focused on an experimental method to evaluate the impact of degradation in rf shielded door systems typically found on tactical, nuclear-survivable C³I shelters.

1.2 Personnel

The personnel responsible for the supervision, conduct, and engineering and technical aspects of these efforts are identified in table 1.

Table 1. List of personnel.

Name	Title	Function
CEG personnel		
Dominique Serafin	Chief	EMP analysis
Michel Bourzeix	Engineer	EMP analysis
Yves Daudy	Engineer	EMP analysis
Jean-Marie Lagard	Technician	EMP analysis
ARL personnel		
Joseph Miletta	Branch chief	EM physics
Robert Atkinson	Engineer	EM physics
John Stewart	Technician	EM physics

2. Background

The Centre d'Etudes de Gramat (CEG) is located in south central France near the town of Gramat, approximately 150 km (92 miles) north of Toulouse. Of the 350 people employed at this 700-acre site, about half are scientists, engineers, and technicians. The CEG Electromagnetic Pulse (EMP) Analysis Group, composed of about 30 people, acted as host for the DEA studies reported here.

The Army Research Laboratory (ARL) is dispersed across three principal locations in the United States, at the Adelphi Laboratory Center (ALC) in Maryland, at the U.S. Army's Aberdeen Proving Ground in Maryland, and at White Sands Missile Range in New Mexico. Members of the Electromagnetic Effects Physics Branch, located at the ALC site, participated with the CEG personnel, both in the performance of the experiments in France and in the follow-on analytical efforts in the United States.

The DEA provides a forum for the technical exchange of nuclear weapons EMP effects, as well as other detrimental electromagnetic effects found on the modern battlefield. In the past, generic studies have been performed by the CEG and ARL groups, both individually and working together under the DEA, to develop techniques, databases, and analytic approaches that support each country's survivability activities.

3. Impact of Study

Although this was not a final study, the findings from the experimental testbed could substantially influence the U.S. Army's present methods for assessing the long-term nuclear hardness maintenance/hardness surveillance (HM/HS) of tactical and strategic systems. Further, the methods developed are applicable to sheltered systems that extensively use lightweight, composite structures to obtain the necessary levels of EMP survivability.

4. Methodology

4.1 Overview

The experimental efforts centered around the design and construction of a testbed demonstration fixture with a large transmission line on the exterior of, and electrically connected to, the DEMOSTHENE facility. The transmission line was placed so that it enclosed one shielded entrance door at the center of the ground plane. The study team easily performed physical adjustments on the transmission line to achieve a 50- Ω geometry (a standard requirement for measurement purposes).

When construction and assembly were complete, the transmission line was energized, and the team characterized the electromagnetic environments within the transmission line and within DEMOSTHENE:

- a. Electric and magnetic (E and H) fields were measured (internal to DEMOSTHENE and within the working volume of the transmission line).
- b. Electric current levels were measured on the return plane of the transmission line; the team used these levels to evaluate the magnitude of injected current and the frequency response of the transmission line, and to provide a reference level for analytical calculations.
- c. Coupling was measured on simple electrical geometries within DEMOSTHENE, such as single wires positioned both horizontally and vertically within the facility at several distances from the shielded door.
- d. Coupling was measured on typical ac power supply lines within the sheltered (and filtered) facility.
- e. Coupling was measured on communications equipment racks in both electrically grounded and ungrounded situations.
- f. Coupling was measured on complex electrical geometries such as those that are typical of equipment interfaces (coaxial cables, general-purpose interface bus (GPIB) cables, and computer ribbon-type cables).

Included in the last group of measurements were both shielded and unshielded cables, loaded (50 Ω) and unterminated, and having both vertical and horizontal cable runs. Measurements were performed for two basic situations: In the first, no degradation to the shielded door gasket was present. In the second, the team simulated degradation by interfering with the electrical connections at the shield door knife-edge interface.

The team constructed a second microstrip line inside the DEMOSTHENE facility to allow for study of the effects of changes in the seam impedance due to degradation in the shielding door gaskets. The microstrip line was positioned vertically over one of the door's long-axis seams.

With the large (exterior) transmission line energized, the voltage response of the microstrip line was measured for various degrees of gasket degradation at several positions along the door seam.

4.2 Transmission-Line Construction and Checkout

A parallel-plate transmission line was selected to be part of the experimental methodology for several reasons: First, the electromagnetic and mathematical theory related to the response characteristics of these devices is widely understood. Second, parallel-plate transmission lines are relatively easy to build and implement. Third, measurements can be made with commercial, off-the-shelf (COTS) equipment using standard, well-documented (and relatively easy to perform) procedures. Combined, these facts implied that if the experiments were successful, the methods could be employed by military maintenance personnel in the field.

Generally, the electrical response of a transmission line is determined by the various aspects of its geometry that affect the characteristic impedance of the line. These aspects include such factors as the length and width of the line, the separation distance between the parallel plates, and how the transitions between the two plates at each end of the line occur. The characteristic impedance of a parallel-plate line can be effectively approximated by

$$Z_0 = \frac{377}{\sqrt{E_r}} \frac{h}{a} \quad , \quad (1)$$

where

$$\begin{aligned} Z_0 &= \text{line impedance,} \\ h &= \text{separation distance between plates,} \\ a &= \text{height of the line,} \\ 377 &= \text{"free-space" impedance, and} \\ E_r &\approx 1. \end{aligned}$$

The formula assumes that one of the two plates acts as an infinite ground plane. It is therefore important to note that as the width of the other plate tends to decrease, the overall line impedance tends to increase.

Since it was desirable to construct a transmission line that could easily propagate radiated signals in a transverse electromagnetic (TEM) mode, the following electrical criteria must also be satisfied:

$$\frac{2\pi h}{\lambda} \ll 1 \quad \text{and} \quad f = \frac{c}{h} \quad , \quad (2)$$

where

$$\begin{aligned} h &= \text{separation distance,} \\ c &= \text{constant speed of light,} \\ f &= \text{frequency of the propagated signal, and} \\ \lambda &= \text{wavelength.} \end{aligned}$$

Initial design considerations for the parallel-plate line included all the pertinent factors that have been previously described, as well as other factors associated with the implementation of the line, such as its physical size and location. As a result, it was determined that placement of the transmission line must necessarily include one of the shielded entrance doors.

The location for the transmission line was selected to be along the long-axis wall of the DEMOSTHENE facility. That exterior wall, which included both the EMP shield and the shielded entrance door, would act as the electrical ground plane for the line. The door was at the center of this ground plane.

The rest of the line was to be constructed primarily of multiple strands of 14-gauge copper wire, laid out in planar fashion, elevated, and parallel with the ground plane. The ground plane and parallel plane of wires were to be electrically connected at the door frame. Further details are shown in figure 2.

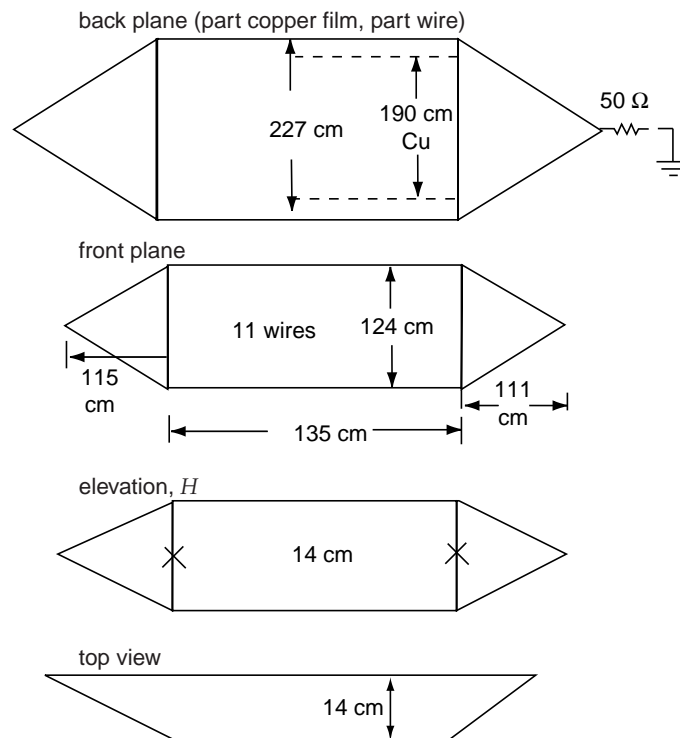
Since most measurement equipment requires 50-Ω inputs, it was desirable to achieve a geometry as close to that impedance as possible. However, physical factors such as the necessity of opening and closing the shielded entrance door with the transmission line in place would tend to make a 50-Ω geometry difficult to achieve.

Before construction was begun, the team determined the approximate dimensions for the width of the transmission line ($a = 1.5$ m) and for the separation of the plates ($h = 0.3$ m). Based on those dimensions, the following approximation for the line impedance was calculated (per eq (1)):

$$Z_0 = 377 \times (0.3/1.5) = 75.4 \Omega .$$

Rough estimations for the impedance of the transition areas (e.g., the area where the parallel line begins to taper) were difficult to make. However, by using curvature tables for such geometries, we determined an approximate value of about 100 Ω.

Figure 2. Schematic representation of transmission line.



In order to support the transverse electromagnetic (TEM) mode, the following calculation was performed (per eq (2)):

$$f \ll (c/2\pi h) = 159.2 \text{ MHz.}$$

Therefore, the line could theoretically support TEM propagation up to approximately 160 MHz.

Further, if a factor of 10 was assumed as the maximum limit for cutoff, it was reasonable to assume that the bandwidth of the line would be approximately 16 MHz.

Once the basic calculations had been performed and the selection of materials for construction had been determined, the transmission line was assembled on the exterior wall of the DEMOSTHENE. Following this, the team performed a series of experiments to assess the quality of construction and to compare the measured response of the line with the predictions.

Time-domain reflectometry (TDR) measurements provided data that were used to assess the electrical impedance of the line at various locations along that line. Initially, the line's general response was not as expected. The electrical impedance of the center portion of the line was approximately 100 Ω , much greater than predicted by the calculations. Although this impedance value was expected at the transitional areas (i.e., where the line tapered to a point), it was not desirable for several reasons.

First, from a measurement standpoint, the impedance mismatch between the transmission line and the measurement system (100 versus 50 Ω) would make it difficult to obtain reasonably accurate data.

Second, from the standpoint of power delivery, the transmission line was inefficient. Because of the high impedance, as well as the impedance mismatches at the transition areas, much more power would need to be delivered to the line than was previously anticipated.

As a result, the design and construction of the transmission line came under close scrutiny, and various design modifications were considered. There were initially two concerns, both having to do with the use of the copper wire.

When the line was first constructed, seven wires were used to create the transition areas and the center portion of the line parallel to the ground plane. (The center portion of the ground plane was almost entirely the shielded entrance door.)

The first modification to the design was to replace the copper portion of the ground plane with solid sheets of laminated copper foil. This was done in an attempt to reduce the electrical impedance of the transition areas.

Then TDR measurements were again performed. The overall response of the transmission line was much better and began to approach the predicted 75 Ω . We also performed the TDR measurements while varying the

number of wires used, so that we could determine how to improve the electrical response.

As an example, figure 3 displays the observed impedance values for the line when seven- and six-wire geometries were used. Shown on the figure are (1) the beginning of the transmission line and the initial transition, (2) the center of the transmission line and its characteristic impedance, and (3) the termination transition and reflection.

Based upon these measurements, wires were added until physical construction constraints would allow no more. The final geometry used 20 wires and had an electrical impedance of approximately 60Ω along the center section. The termination end of the line was necessarily matched with that resistance value.

4.3 Measurement System

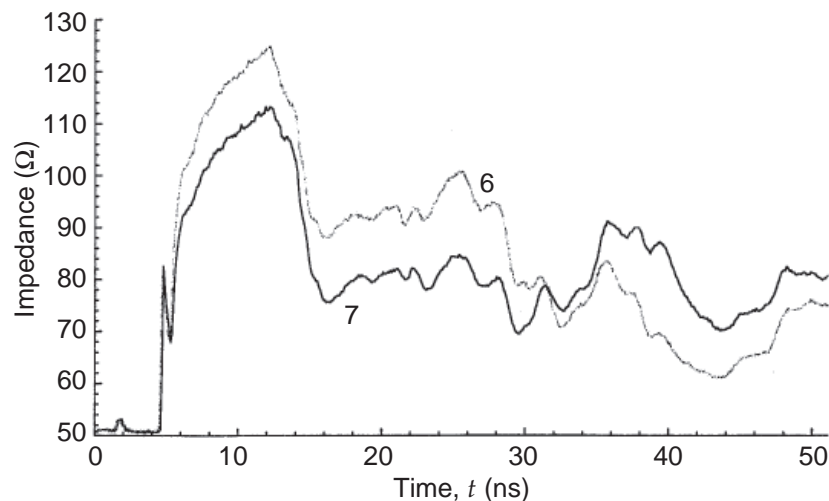
The TDR measurements described above were made on a Hewlett Packard 9573 network analyzer with attached 9753 TDR S1-S2 interface. The test configuration used is shown in figure 4.

Figure 4 also details the test setup used to monitor the electrified conditions of the transmission line, the electromagnetic environment within DEMOSTHENE, and current coupled to the interior wires and cables.

As shown in figure 4, the excitation source used was an Armexel pulse generator with the capability of delivering a 1-ns pulse with approximately 10 W of power. The output of the generator was fed directly into the "drive" end of the transmission line. A low-voltage output from the Armexel was used to synchronize and trigger the HP 5920 oscilloscopes during the data collection process.

Current measurements on a single wire of the transmission line were made with a CT-1 current probe. The output of the probe was transmitted to the oscilloscopes through a wideband fiber-optic link. Further, current coupling data (from both CT-1 and bulk current probes) and E - and H -

Figure 3. Initial TDR response curves for transmission line with six- and seven-wire geometries.



field sensor data were transmitted to the oscilloscopes through a similar fiber-optic system.

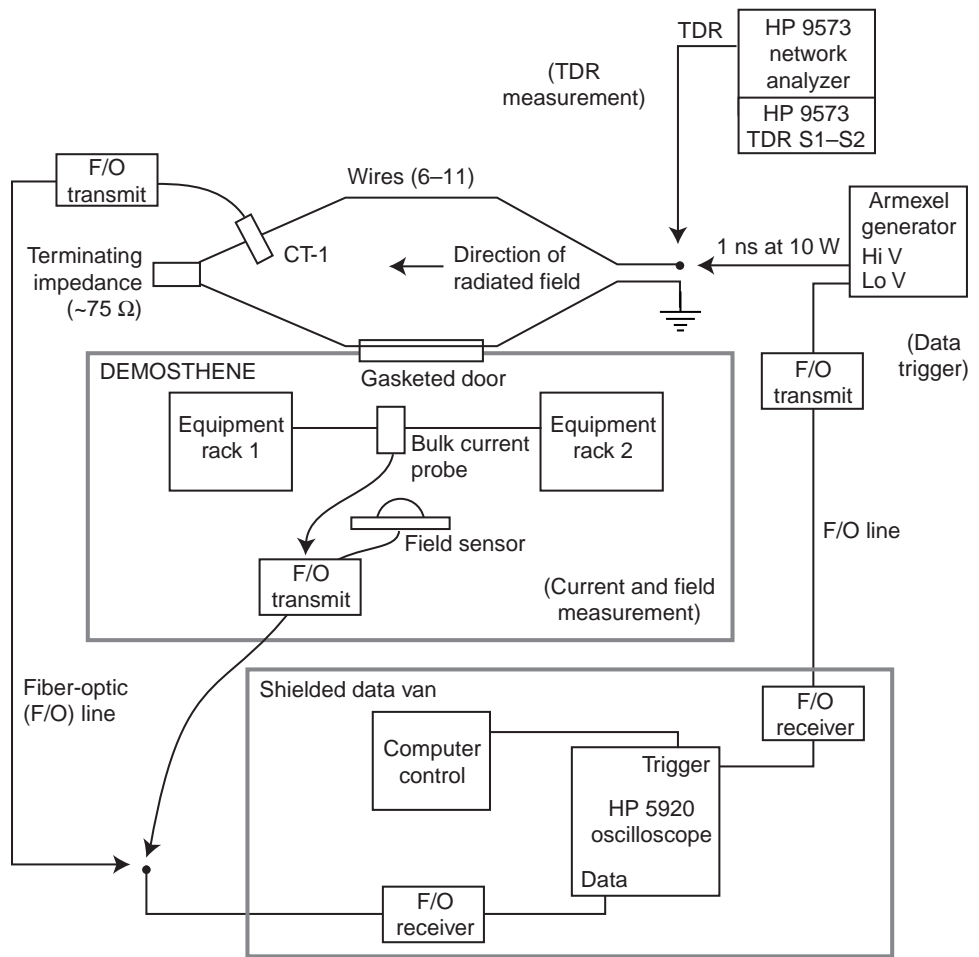
Data collection, instrument control, and some basic analytic functions were provided by a computer in an adjacent structure.

4.4 Facility and Test Environment

Of principal concern to the test engineers was the change in the EM environment within the DEMOSTHENE facility caused by flaws and other forms of degradation in the EMP shield.

The facility consisted primarily of two welded structures, joined together by bolts and rf gaskets in a more or less permanent configuration. By welding the structures, the design team ensured that the EMP shield at those areas were of high quality. Although the two sections were joined at a bolted seam, careful planning resulted in a design that maintained the same high-quality shield. Clearly, the areas that would suffer the highest degree of degradation were the entrance doors.

Figure 4. Test and measurement setups (TDR measurement setup and current and field data test setup).



Typically, these features tend to degrade quickly from constant usage. The “finger-stock” type of gasket becomes brittle with age and breaks. The mating edges oxidize with exposure to air. Multiple openings and closings cause the hinge systems to wear out and the doors to seat improperly within the door frame. As a result, the shield could become imperfect and, when excited by an external source, would not provide the necessary SE to protect the internal environment (and equipment) from the most severe external environment.

Because the shielded entrance door was included as part of the parallel-plate transmission line, it was possible to investigate the discontinuities in the EMP shield due to the door as a function of the line’s time-domain response. Also, it was possible to measure the internal environment and to study the changes in that environment when various degrees of door degradation were introduced.

Door degradation was simulated by the insertion of paper (nonconductive) into the door seam interface so that electrical continuity between the knife-edge and the “finger-stock” gasket could not exist (see fig. 5).

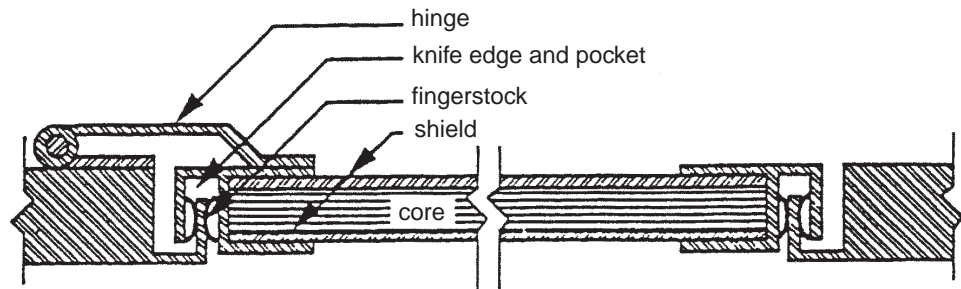
As a result, electromagnetic parameters such as the electric field and the magnetic field within the DEMOSTHENE facility could be measured directly with the proper sensor positioning. Indirectly, internal cable coupling could be estimated by measurement of the pickup response on various cables and wires through the use of current probes. These measurements were made on both shielded and unshielded cables. Some of the cables were terminated with $50\ \Omega$ (simulating electrically loaded conditions), and some were not terminated (simulating unloaded conditions). Further, some cables were vertically polarized, and some were horizontally polarized.

The positioning and number of electrical discontinuities indicate changes in the line impedance; one can study these changes by observing the TDR response of the transmission line. We performed additional experiments using a microstrip line within DEMOSTHENE and observing its response to the changes in the externally generated fields.

4.5 Microstrip Line Construction and Checkout

The microstrip line structure was chosen for the experiment because its response characteristics could be easily predicted. As with the larger transmission line, aspects of the smaller line’s geometry (the width and

Figure 5. Typical knife-edge door seam construction.



the separation distance from the shield) would determine its characteristic impedance.

What could not be predicted, however, was the reactive response of the line when subjected to different levels of electrical excitation caused by the large, external transmission line. Also unpredictable was the change in the microstrip line response when the area of degradation changed.

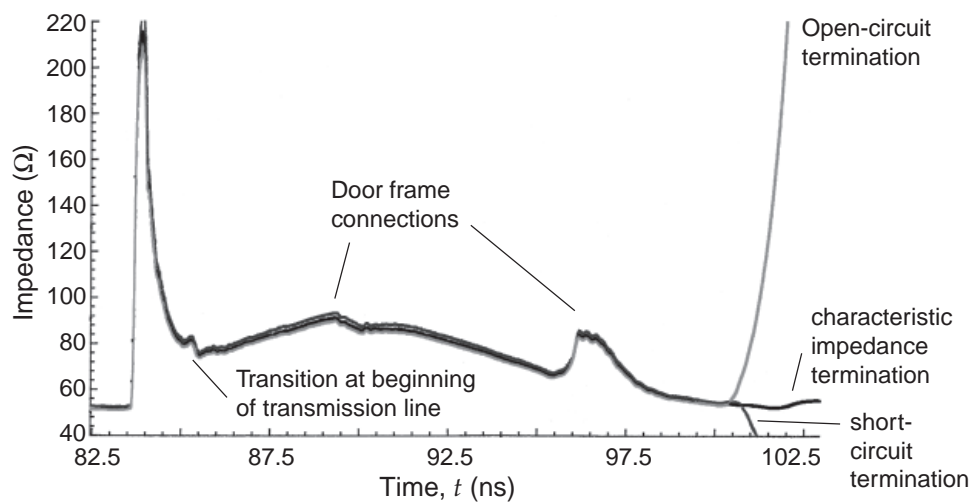
Strip-line construction was simple and consisted of nothing more than 5-cm-wide copper tape-foil, elevated above one entrance door seam by nonconductive stops, and terminated to the door frame at one end. The overall length of the strip line was approximately 176 cm. Because of the nonconductive stops, the separation distance between the strip line and the metallic door seam varied greatly along the length of the line. As a result, predicting the impedance for the strip line was difficult.

The separation distance was measured at six positions along the length of the strip line. The distances varied from approximately 1.4 to 2.7 cm. The average separation distance between these two parallel plates was approximately 2.5 cm.

Consequently, the predictions for the line impedance (calculated from eq (1)) yielded about 106Ω at the smaller distance and 204Ω at the larger distance. However, the predictions were inaccurate.

As can be observed from figure 6, the impedance of the line generally varied between 60 and 90 Ω . Most noticeable at the beginning of the TDR on figure 6 is the sharp transition (approximately 210 Ω). This was caused by poor electrical transitioning at the ends. Three termination conditions are also shown in the figure. These include the open-circuit condition (line not terminated), the short-circuit condition (line directly connected to the door frame), and the loaded condition (with 50 Ω). Also indicated on the figure are the approximate positions of the six measured distances.

Figure 6. Microstrip line characteristics.



5. Data and Analysis

5.1 Environment Within Shield

To assess the contributions to the interior electromagnetic environment due to the leakage of radiated energy, we examined two test configurations.

In the first configuration, a horizontal copper wire was extended vertically from the ceiling to the floor of the shield. The wire was electrically connected at both ends, and a CT-1 current probe was placed on this makeshift circuit.

The vertical wire was positioned at two locations relative to the door and degraded seam: the first location was 0.5 m from the center of the door; the second position was 1 m from the center of the door. The measured results are shown in figure 7.

Generally, the distance location of the vertical wire had little effect on the amount of signal coupled to the wire. Signal levels indicated an approximate loss of 40 dB in SE between 10 kHz and 10 MHz.

In the second configuration, a horizontal wire was extended across the room, 175 cm away from the shielded door. We simulated degrees of gasket degradation by introducing various lengths of paper into the door seam. Three different lengths were used: 60, 120, and 180 cm.

As before, the wire was electrically connected to the shield at both ends. Current coupled to the wire was again measured with a CT-1 current probe.

As shown in figure 8, the results of increasing the apparent amount of degradation are obvious: as the degraded area was extended, more radiated energy coupled onto the wire.

Figure 7. Measured current on vertical wire.

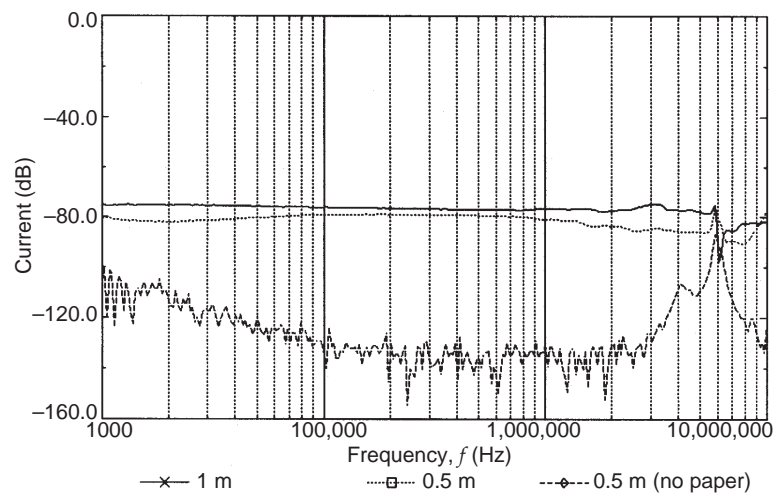
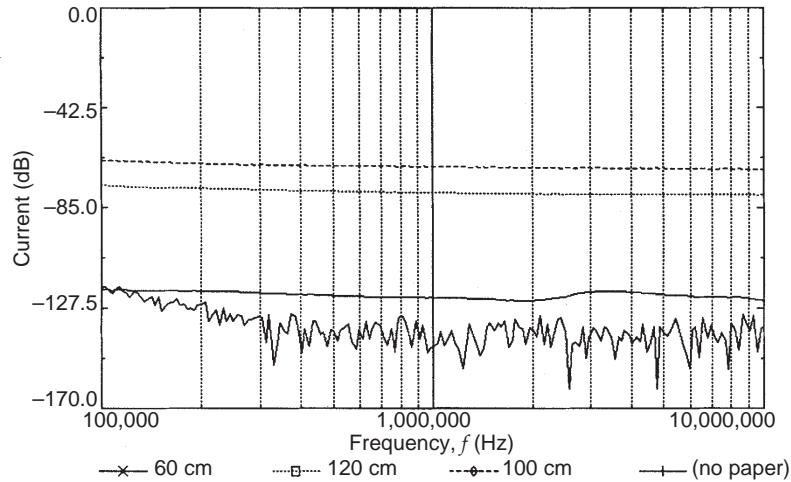


Figure 8. Measured current on a horizontal wire.



5.2 Microstrip Measurements

Before the microstrip line's response was measured, three assumptions were made: First, it was assumed that the external radiated field was uniform across the working volume of the large transmission line. Second, any aperture that was within the working volume would allow the external field to be re-radiated inside the shielded volume. Finally, the locations of the re-radiated field would be detected by the microstrip line.

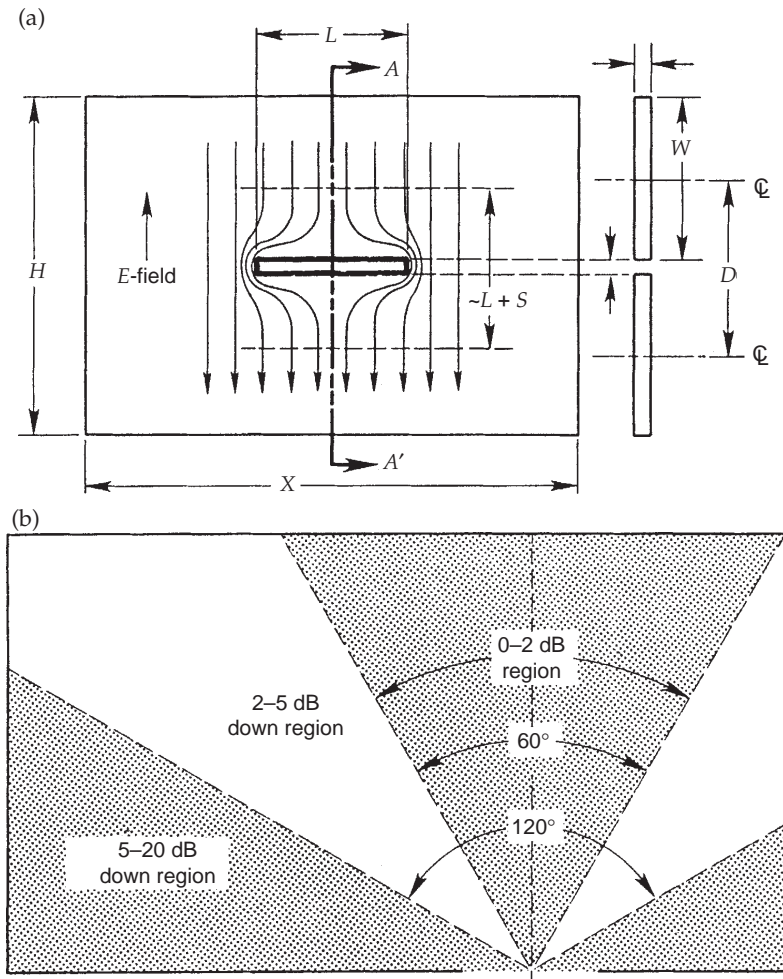
Since the parallel line was not a single, solid metallic sheet but was composed of 20 wires, slight fluctuations in the radiated field strength were expected. However, the wires were spaced close enough together so that the test engineers were reasonably confident that any fluctuations in field strength were minimized.

If this was the case, then it could be expected that the radiated field strength from the large transmission line, which was at a right angle to the shield, would be equal along the entire length of the door seam. If the door were removed, for instance, the microstrip line would then be subjected to a uniform field along its entire length.

Concerning the second assumption, discontinuities in the transmission line's ground plane (especially at the door seams) should tend to create aperture-like leaks in the EMP shield. Therefore, radiated energy would come through the aperture in a predictable way: generally, the exterior field would be polarized in various ways with the aperture. As shown in figure 9, surface currents that would result from the external field would be interrupted by the aperture.

At low frequencies the currents would tend to flow around the aperture. This would be particularly true if the length of the aperture (L) were much less than the wavelength (λ) of the radiated field. At higher frequencies, the aperture would begin to respond like a coplanar, parallel-plate transmission line. Radiation patterns would begin to occur on the interior of the door seam, which would, in turn, excite the microstrip line. Also, SE corresponding to the slot leakage would result.

Figure 9. Aperture response characteristics: (a) current flow at aperture and (b) internal radiated field.



Predictive values for SE at various frequencies were approximated by

$$S_{\text{approx}} = S_{\text{enclosure}} - 10 \log_{10} (LHf_{\text{MHz}}^2) \quad , \quad (3)$$

where

- S_n = SE of DEMOSTHENE (100 dB)
- L = aperture length in millimeters,
- H = aperture height in millimeters, and
- f_{MHz} = frequency in megahertz.

If the length of the aperture was 28 cm (approximately the length of an 8½ × 11 in. piece of paper) and the height of the aperture was 2.5 cm (approximately the thickness of the shield door, or 1 in.), then approximate values for the SE of the aperture would be as shown in table 2.

Therefore, inhibiting the electrical contact along the seam by creating an aperture with the size previously specified, one would expect to see the resulting effects on the response of the microstrip line.

As can be observed from figure 10, the aperture effects were characterized by changes in voltage levels on the strip line. Further, the levels predicted

for the various frequencies closely matched the measured response of the strip line.

Since the strip line was itself a transmission line, it was expected that fields radiating through the aperture might affect the response of the strip line differently as the position of the slot changed. However, this result was not demonstrated by the data.

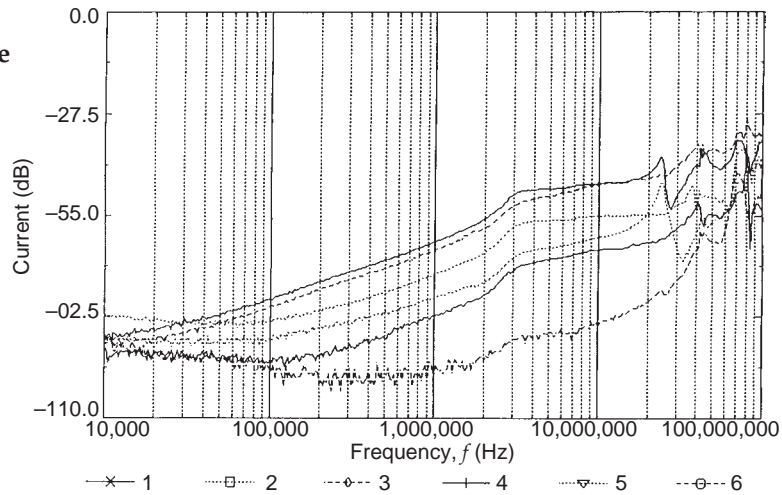
Figure 10 shows that as the position of the slot changed, changes could be detected in the measured response at the end of the strip line. Unfortunately, the changes were not consistent with the change in location of the aperture.

Table 2. Aperture SE (approximate).

Frequency (MHz)	SE ^a (dB)
0.18	1.5
1.0	61.5
10.0	41.5
100.0	21.5

$$^a[100 - 10 \log_{10} (280 \times 25 \times f_{\text{MHz}}^2)]$$

Figure 10. Strip line response at six aperture positions.



6. Synopsis

This testbed demonstrated a new approach to evaluating the SE of rf-tight doors similar to those typically found on critical ground-based C⁴I facilities. Through analysis of the results of the shielding degradation, both U.S. ARL and French CEG personnel gained insight into the modes and levels of EM coupling resulting from the various degrees of degradation.

In the past, multiwire transmission lines have generally been used to perform rf radiated immunity measurements over a generally wide frequency band. The type, size, and construction of the transmission lines described herein could generate both electric (*E*) and magnetic (*H*) fields. Significant *E*-field propagation, which was predicted before construction and later calculated from internal field measurements, generally ranged between approximately 100 and 200 MHz.

These limitations were, for the most part, due to the physical geometry of the lines. However, additional limitations were imposed by the source generators used to electrically excite the large external lines. Provided a more perfect transmission line were constructed, *E*-field propagation could have extended from approximately 10 kHz to 200 MHz. Hypothetically, *H*-field propagation could have extended up to approximately 1 MHz also. The strength of the fields would have remained dependent on the source voltages.

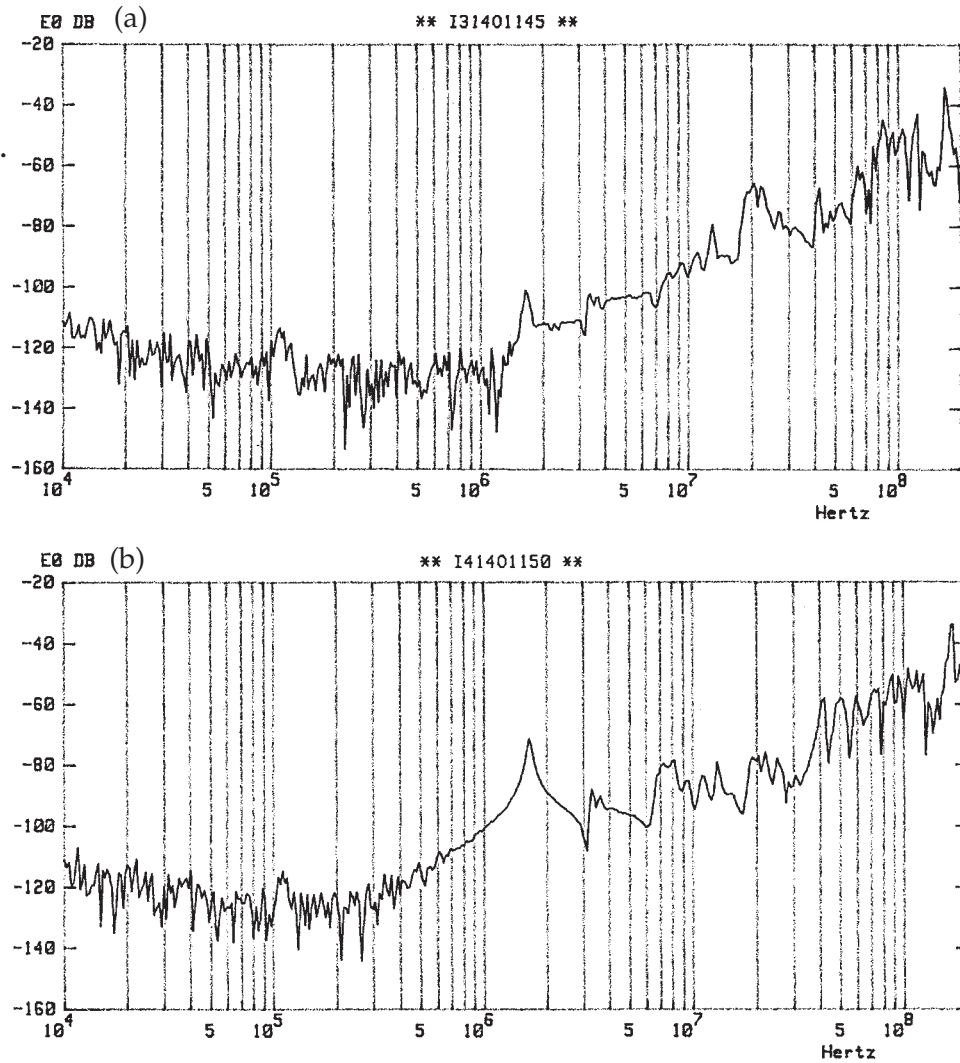
Despite the limitations, analysis of the transmission-line results has provided a unique approach to determining the long-term nuclear EMP HM/HS status of such facilities. Additionally, the methods used for construction and implementation of the external line could be modified for making radiated immunity measurements to EM fields, such as those described in MIL-STD-462D, *Measurement of EMI Characteristics*.

The internal microstrip line techniques need more investigation. Initial results have indicated that with some modifications these techniques could, as a minimum, be successfully used to verify compliance with regulations such as IEC 801-3, *Electromagnetic Compatibility for Electric and Electronic Equipment—Part 3, Immunity to Radiated RF EM Fields*. Further, the recorded data have supported the idea that areas of rf leakage can be detected with some accuracy, particularly along door seams.

Appendix A. Typical Response Data

Displayed in the following data graphs are various examples of induced currents measured within the DEMOSTHENE facility. These results, obtained inside the shielded volume, were typical examples of data collected during periods when the shielded door was energized by the large transmission line.

Figure A-1. Current on power cord:
(a) horizontally polarized and
(b) vertically polarized.



Appendix A

Figure A-2. Current on coaxial cable:
(a) horizontally polarized and
(b) vertically polarized.

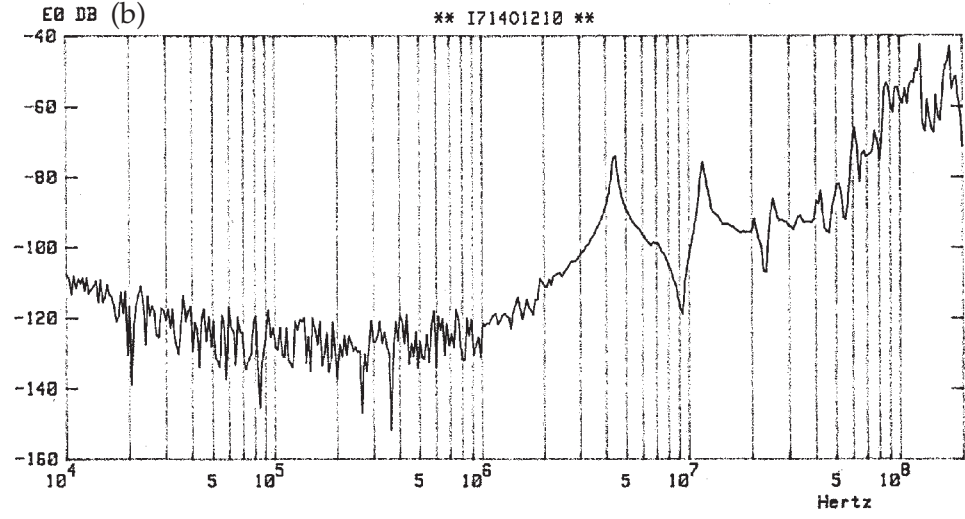
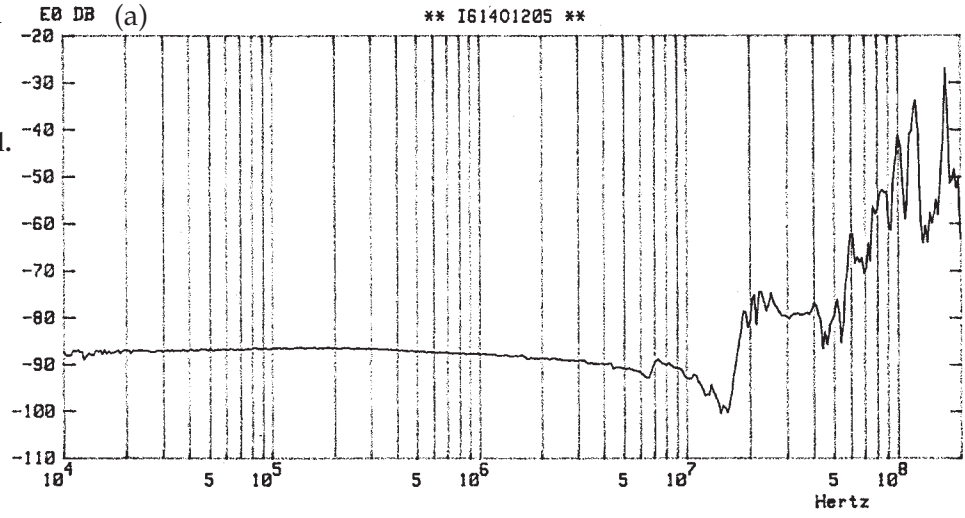


Figure A-3. Current on GPIB cord:
(a) horizontally polarized and
(b) vertically polarized.

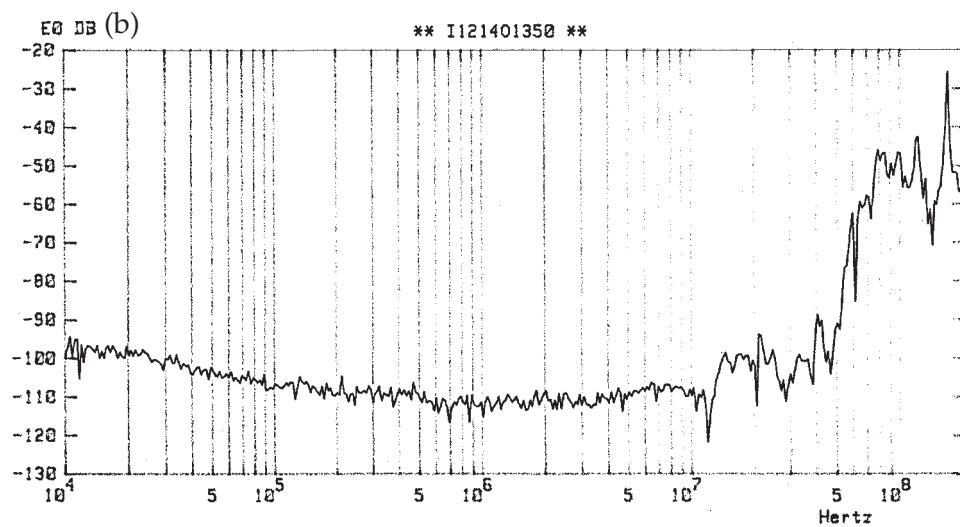
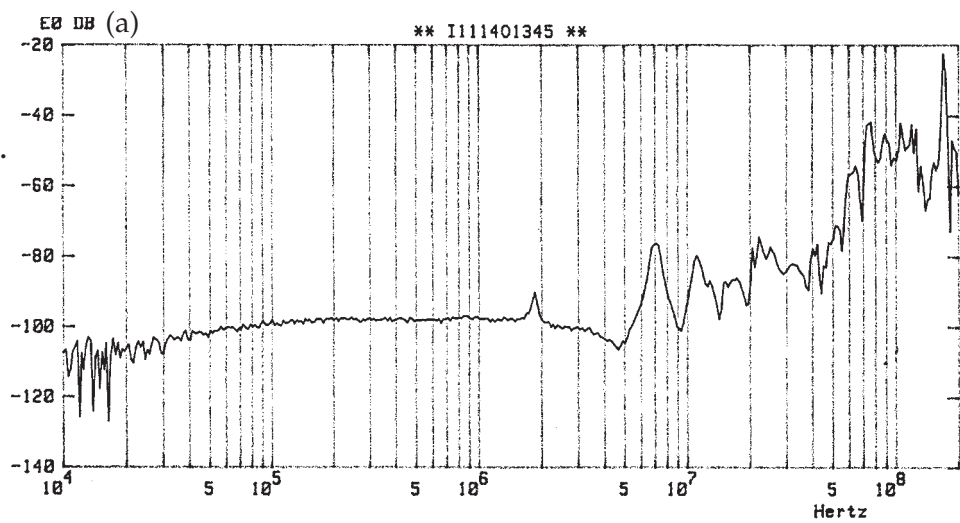


Figure A-4. Current on telephone cable.

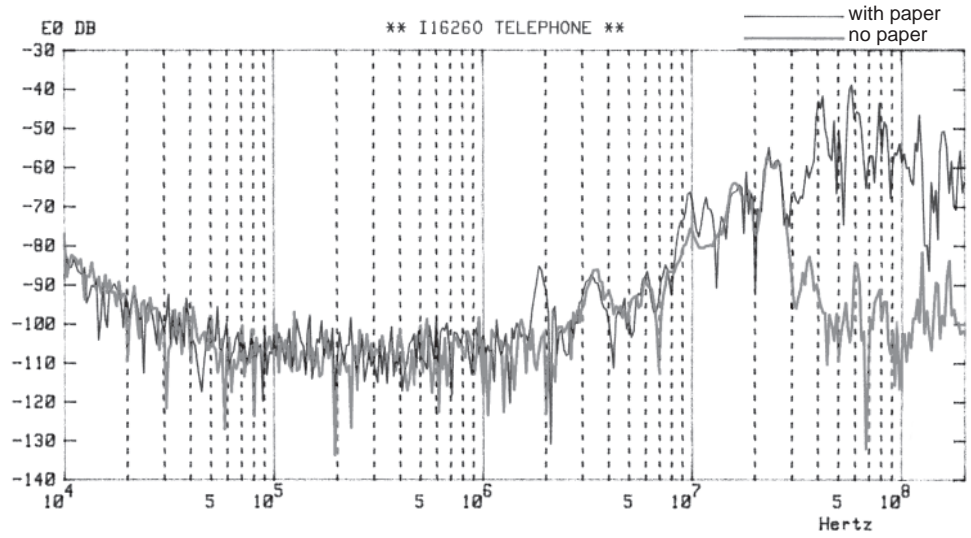


Figure A-5. Current on inter-rack horizontal coaxial cable.

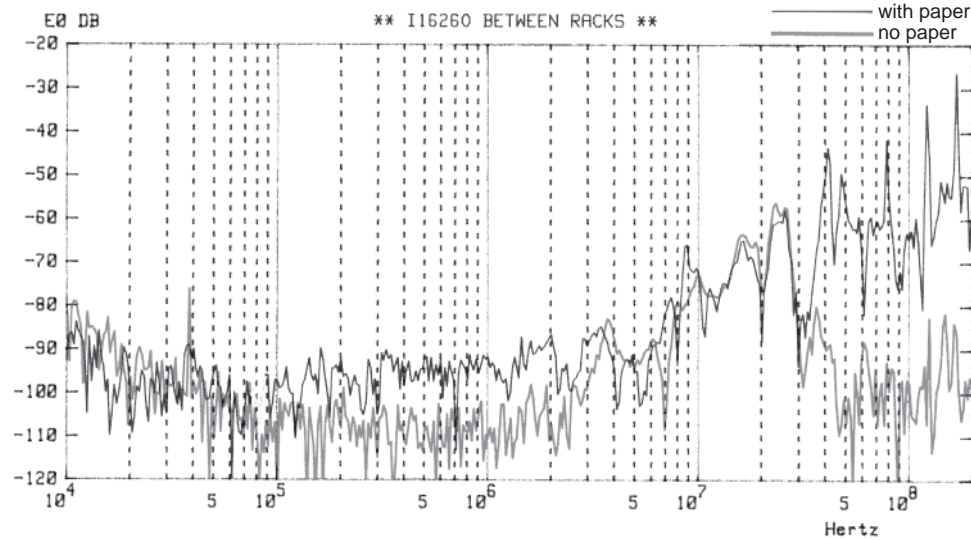
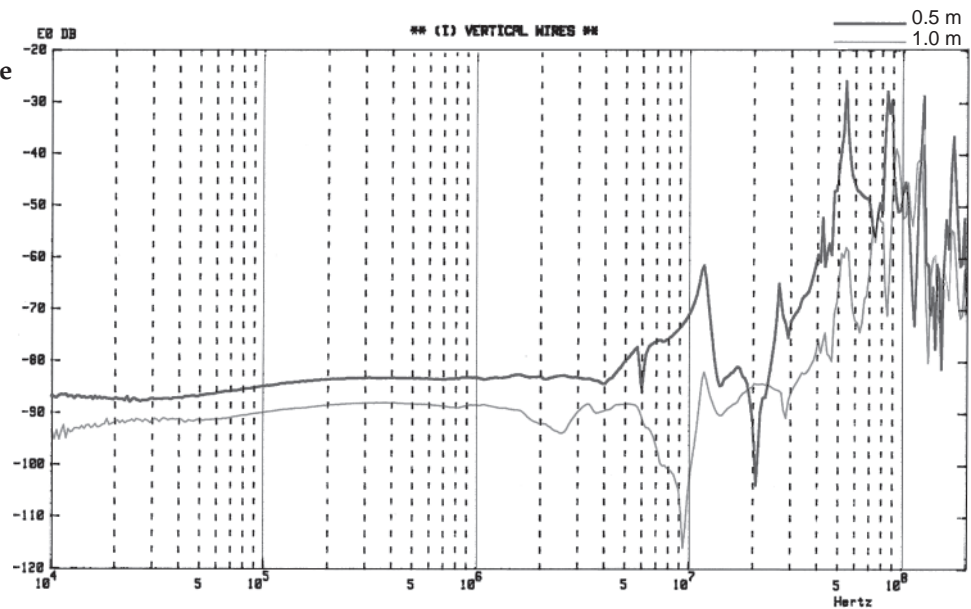


Figure A-6. Current on elevated, vertical single wires at 0.5 and 1.0 m from door.



Appendix B. Data File Names and Information

The following lists the data collected during the experiments at the DEMOSTHENE facility investigating shielding effectiveness. Also included are test-point designations and comments about the physical configurations of test items, personal observations by the test engineers, and the like.

= RECAPITULATIF FICHIERS (données standard AEM) =
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=====
FICHER | TITRE | XMAX | UNITES | YMIN / YMAX | UNITES |
=====
50OHMTERM | 50OHMTERM | 5.110E-08 Seconds | 4.675E+001/ 1.180E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE 50 Ohms ON RIGHT SIDE OF DEMOSTHENE |
DOOR |
-----
OPENTERM | OPENTERM | 5.110E-08 Seconds | 4.828E+001/ 6.641E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE OPEN CIRCUIT RIGHT SIDE OF DEMOSTHE |
NE DOOR |
-----
SHORTTERM | SHORTTERM | 5.110E-08 Seconds | 6.832E+000/ 1.226E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE SHORT CIRCUIT RIGHT SIDE OF DEMOSTH |
ENE DOOR |
-----
75OHMTERM | 75OHMTERM | 5.110E-08 Seconds | 4.831E+001/ 1.205E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE 75 Ohms RIGHT SIDE OF DEMOSTHENE DO |
OR |
-----
50TERMOD00 | 50TERMOD00 | 5.110E-08 Seconds | 4.242E+001/ 1.194E+002 Ohms |
TEK11801 | TDR STRIP-LINE TERMINATE 50 Ohms RIGHT SIDE OF DEMOSTHENE DOORWITH DO |
OR OPEN |
-----
50OHMTERM6 | 50OHMTERM6 | 5.110E-08 Seconds | 5.035E+001/ 1.134E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE 50 Ohms LEFT SIDE OF DEMOSTHENE DOO |
R |
-----
OPENTERM6 | OPENTERM6 | 5.110E-08 Seconds | 4.967E+001/ 1.845E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE OPEN CIRCUIT LEFT SIDE OF DEMOSTHEN |
E DOOR |
-----
SHORTTERM6 | SHORTTERM6 | 5.110E-08 Seconds | 3.028E+001/ 1.154E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE SHORT CIRCUIT LEFT SIDE OF DEMOSTHE |
NE DOOR |
-----
75OHMTERM6 | 75OHMTERM6 | 5.110E-08 Seconds | 5.049E+001/ 1.133E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE 75 OHMS LEFT SIDE OF DEMOSTHENE DOO |
R |
-----
75OHM6WG | 75OHM6WG | 5.110E-08 Seconds | 5.069E+001/ 1.248E+002 Ohms |
Mesure / TEK11801 | TDR STRIP-LINE TERMINATE 75OHM LEFT SIDE OF DEMOSTHENE DOOR |
6 WIRES |
-----
129S50R1 | 129S50R1 | 5.110E-08 Seconds | 4.659E+001/ 1.148E+002 Ohms |
Mesure / TEK11801 | TDR 50 OHMS RIGHT 7 WIRES FOR 2 PLANES |
=====

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Appendix B

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-----
|29S50R2  |29S50R2  | 5.110E-08 Seconds  | 4.425E+001/ 1.071E+002 Ohms
|Measure / TEK11801|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 7WIRES FOR NAPPE 7+2(
|1/2) WIRES FOR GROUND
-----
|29S50R3  |29S50R3  | 5.110E-08 Seconds  | 4.066E+001/ 9.267E+001 Ohms
|TEK11801|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 7WIRES FOR NAPPE,7+2 WIRES FOR
|GROUND H=15CM
-----
|29S50R4  |29S50R4  | 5.110E-08 Seconds  | 4.986E+001/ 8.963E+001 Ohms
|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 7WIRES FOR NAPPE 7+4 WIRES FOR GROUND H
|=15CM
-----
|29SE_V   |29SE_V   | 2.000E+08 Hertz    | -1.243E+002/-5.212E+001 dB
|Measure 3577A/P:B/R|IE/V WITHOUT CALIBRATION (JUST TO SEE THE SHAP)
-----
|29STRANS |29STRANS | 2.000E+08 Hertz    | -6.252E+000/ 4.840E+000 dB
|Measure 3577A/P:B/R| TRANSMISSION STRIP LINE |WITHOUT CALIBRATION (JUST TO SEE T
|HE SHAP)
-----
|29SI_V   |29SI_V   | 2.000E+08 Hertz    | -8.517E+001/-2.555E+001 DB
|Measure 3577A/P:B/R| CURRENT WITH CT1 ON 1 WIRE WITHOUT CALIBRATION (JUST TO SE
|E THE SHAP)
-----
|S11_500HMS|S11_500HMS| 2.000E+08 Hertz    | -4.846E+001/-2.864E+000 dB
|Measure 3577A/P:F2|S11 STRIP-LINE TERMINATE 50 Ohms RIGHT 7WIRES FOR NAPPE 7+4
|WIRES FOR GROUND H=15C
-----
|30S50R5  |30S50R5  | 5.110E-08 Seconds  | 4.899E+001/ 9.127E+001 Ohms
|Measure / TEK11801|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 7WIRES FOR NAPPE 20 W
|IRES FOR GROUND H=15CM
-----
|30S50R6  |30S50R6  | 5.110E-08 Seconds  | 4.427E+001/ 8.498E+001 Ohms
|TEK11801|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 13 WIRES FOR NAPPE 20 WIRES F
|OR GROUND H=15CM
-----
|30S50R7  |30S50R7  | 5.119E-08 Seconds  | 4.811E+001/ 9.000E+001 Ohms
|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 11 WIRES FOR NAPPE 20 WIRES+SHEET 1 PAR
|IT FOR GROUND H=15
-----
|30S50R8  |30S50R8  | 5.119E-08 Seconds  | 4.452E+001/ 9.030E+001 Ohms
|SAME THAN 30S50S7 BUT DOOR OPEN
-----
|01050R9  |01050R9  | 5.119E-08 Seconds  | 4.585E+001/ 8.231E+001 Ohms
|TEK11801|TDR STRIP-LINE TERMINATE 50 Ohms RIGHT 9 WIRES FOR NAPPE 20 WIRES+SH
|EET 2 PART FOR GROUND
-----
|010S11R9 |010S11R9..| 2.000E+08 Hertz    | -5.024E+001/-5.761E+000 dB
|Measure 3577A/P:F2|S11 ON 50 Ohms NAPPE:9 WIRES GROUND:2 CUPPER SHEETS H=15CM
-----
|040R50R11|01050R11 | 5.115E-08 Seconds  | 4.602E+001/ 8.415E+001 Ohms
|TDR TERMINATE 50 Ohms RIGHT 9 WIRES FOR NAPPE 20 WIRES+SHEET 2 PART FOR GROUND
|PAPER ON GASKET
-----
|04050R10 |04050R10 | 5.115E-08 Seconds  | 4.621E+001/ 8.211E+001 Ohms
|TDR TERMINATE 50 Ohms RIGHT 9 WIRES FOR NAPPE 20 WIRES+SHEET 2 PART FOR GROUND
|SAME THAN 01050R9

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|CT1REF7dB |CT1REF7dB| 2.000E+08 Hertz      |-4.520E+001/-1.932E+001 dBvolt
|Measure REFERENCE I WITH CT1 ATT FOL1000=28-21=7dB
-----
|HREF1_CT1 |HREF1_CT1 | 1.000E+07 Hz          | 3.817E+000/ 1.588E+001 A/M
|H=Vs/FT_MGL5(Vs=Mo*Aeq*j*W*H) STORED H/B(B is Vs REF CT1)
-----
|HREF2_CT1 |HREF2_CT1 | 2.000E+08 Hz          | 4.513E-001/ 1.378E+001 A/M
|H=Vs/FT_MGL5(Vs=Mo*Aeq*j*W*H) STORED H/B(B is Vs REF CT1) 2nd BAND
-----
|HREF_CT1  |HREF_CT1  | 2.000E+08 Hz          |-7.791E+000/ 2.569E+001 DBA/M
|Merging HREF1_CT1 AND HREF2_CT1 MAX ERROR ABOUT 1dB AFTER 9MHz
-----
|CT1601020 |CT1601020 | 2.000E+08 Hertz      |-4.339E+001/-1.795E+001 dBvolt
|Measure 3577A/P:A|CT1 REFERENCE FOL1000=28-21=7dB NOTE: NOT SAME AS 5 OCT
-----
|M652601020|M652601020| 2.000E+08 Hertz      | 8.488E-004/ 2.287E-001
|Measure 3577A/P:B/A|MGL5 INSIDE DEMOSTHENE 1M-200MHz WITH PAPER IN GASKET
-----
|M651601020|M651601020| 1.000E+07 Hertz      | 5.788E-003/ 6.595E-001
|Measure 3577A/P:B/A|MGL5 INSIDE DEMOSTHENE 10K-10MHz WITH PAPER IN GASKET
-----
|M651601100|M651601100| 1.000E+07 Hertz      | 8.298E-006/ 1.211E+000
|Measure 3577A/P:B/A|MGL5 INSIDE DEMOSTHENE 10K-10MHz WITH OUT PAPER IN GASKET
-----
|M652601100|M652601100| 2.000E+08 Hertz      | 3.214E-007/ 4.846E-003
|Measure 3577A/P:B/A|MGL5 INSIDE DEMOSTHENE 1M-200MHz WITH OUT PAPER IN GASKET
-----
|CT1601100 |CT1601100 | 2.000E+08 Hertz      |-4.389E+001/-1.931E+001 dBvolt
|Measure 3577A/P:A|CT1 REFERENCE FOL1000=28-21=7dB NOTE: NOT SAME AS 5 OCT
-----
|CT1601145 |CT1601145 | 2.000E+08 Hertz      |-4.468E+001/-1.882E+001 dBvolt
|Measure 3577A/P:A|CT1 REFERENCE FOL1000=28-21=7dB NOTE: NOT SAME AS 5 OCT
-----
|I162601145|I162601145| 2.000E+08 Hertz      | 2.838E-007/ 1.125E-002
|Measure 3577A/P:B/A|I94430_2 I ON TELEPHONE WIRE WITH PAPER IN GASKET
-----
|I162601200|I162601200| 2.000E+08 Hertz      | 1.029E-006/ 4.775E-002
|Measure 3577A/P:B/A|I94430_2 I ON WIRE FROM EQ IN RACK 2 TO EQ IN RACK 3
-----
|CT1601200 |CT1601200 | 2.000E+08 Hertz      |-4.596E+001/-1.827E+001 dBvolt
|Measure 3577A/P:A|Measure 3577A/P:A|CT1 REFERENCE FOL1000=28-21=7dB NOTE: NOT SA
|ME AS 5 OCT
-----
|HIN_CT160 |HIN_CT160 | 2.000E+08 Hz          |-6.409E+001/-5.289E+000 DBA/M
|H INSIDE/Ict1 HALF SLOT WITH PAPER
-----
|I162601530|I162601530| 2.000E+08 Hertz      |-1.339E+002/-5.718E+001 DB
|Measure 3577A/P:B/A|SAME AS I162601145 WITH NO PAPER
-----
|CT1601530 |CT160153  | 2.000E+08 Hertz      |-4.987E+001/-2.140E+001 dBvolt
|Measure 3577A/P:A|REFERENCE FOR I162601530

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Appendix B

CT1601600	CT1601600	2.000E+08 Hertz	-5.076E+001/-2.171E+001 dBvolt
Mesure 3577A/P:A REFERENCE FOR I162601600			
I162601600	I16201600	2.000E+08 Hertz	4.625E-007/ 1.531E-003
Mesure 3577A/P:B/A Mesure 3577A/P:B/A SAME AS I162601200 WITH NO PAPER			
INOISE1630	INOISE1630	2.000E+08 Hertz	5.166E-009/ 2.871E-006 volt
Mesure 3577A/P:B AMBIENT INSIDE DEMOSTHENE			
CT1801200	CT1801200	2.000E+08 Hertz	-5.852E+001/-1.744E+001 dBvolt
Mesure 3577A/P:A CT1 REFERENCE FOL1000=28-21=7dB NOTE: NOT SAME AS 6 OCT			
IHH801200	IHH801200	2.000E+08 Hz	-7.748E+001/ 5.998E+000 DB
H FIELD POLAR HORIZONTAL MGL6 .5M WITH PAPER (/REF)			
IHN801330	IHN801330	2.000E+08 Hz	-7.619E+001/ 1.105E+001 DB
H FIELD POLAR NORMAL MGL6 .5M WITH PAPER (/REF)			
IHV801345	IHV801345	2.000E+08 Hz	-5.283E+001/ 8.140E+000 DB
H FIELD POLAR VERTICAL MGL6 .5M WITH PAPER (/REF)			
IHV801400	IHV801400	2.000E+08 Hz	-5.946E+001/ 7.168E+000 DB
H FIELD POLAR VERTICAL MGL6 1M WITH PAPER (/REF)			
IHV801415	IHV801415	2.000E+08 Hz	-8.726E+001/ 5.304E+000 DB
H FIELD POLAR VERTICAL MGL6 2M WITH PAPER (/REF)			
IHN801430	IHN801430	2.000E+08 Hz	-7.519E+001/ 1.097E+001 DB
H FIELD POLAR NORMAL MGL6 1M WITH PAPER (/REF)			
IHH801445	IHH801445	2.000E+08 Hz	-8.418E+001/ 6.107E+000 DB
H FIELD POLAR HORIZONTAL MGL6 1M WITH PAPER (/REF)			
IEV801500	IEV801500	2.000E+08 Hz	-4.660E+001/ 4.717E+001 DB
E FIELD POLAR VERTICAL ACD4 1M WITH PAPER (/REF)			
IEN801515	IEN801515	2.000E+08 HZ	-3.248E+001/ 5.533E+001 DB
E FIELD POLAR NORMAL ACD4 1M WITH PAPER (/REF)			
IEH801530	IEH801530	2.000E+08 Hz	-4.443E+001/ 5.063E+001 DB
E FIELD POLAR HORIZOTAL ACD4 1M WITH PAPER (/REF)			
IEH801540	IEH801540	2.000E+08 Hz	-5.875E+001/ 1.305E+001 DB
E FIELD POLAR HORIZONTAL ACD4 .5M WITH PAPER (/REF)			
IEV801545	IEV801545	2.000E+08 Hz	-4.127E+001/ 5.218E+001 DB
E FIELD POLAR VERTICAL ACD4 .5M WITH PAPER (/REF)			
IEN801550	IEN801550	2.000E+08 Hz	-3.146E+001/ 5.254E+001 DB
E FIELD POLAR NORMAL ACD4 .5M WITH PAPER (/REF)			
IEN801600	IEN801600	2.000E+08 Hz	-6.402E+001/ 5.146E+001 DB
E FIELD POLAR NORMAL ACD4 .5M WITHOUT PAPER (/REF)			

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-----
|CT11200945|CT11200945| 2.000E+08 Hertz      |-4.754E+001/-1.729E+001 dBvolt
|Mesure 3577A/P:A|MESURE REF WITH CT1 FOL 1000 AT 28dB==>28-21=7dB ATTENUATION
-----
|EN1201000 |EN1201000 | 2.000E+08 Hertz      |-6.285E+001/ 2.768E+001 DB
|Mesure 3577A/P:B/A|E NORMAL WITH THOMSON SYSTEME (/CT1) AT 1M
-----
|EV1201010 |EV1201010 | 2.000E+08 Hertz      |-8.097E+001/ 2.188E+001 DB
|Mesure 3577A/P:B/A|E VERTICAL WITH THOMSON SYSTEME (/CT1) AT 1M
-----
|EH1201020 |EH1201020 | 2.000E+08 Hertz      |-5.977E+001/ 3.075E+001 DB
|Mesure 3577A/P:B/A|E HORIZONTAL WITH THOMSON SYSTEME (/CT1) AT 1M
-----
|EH1201030 |EH1201030 | 2.000E+08 Hertz      |-5.734E+001/ 3.497E+001 DB
|Mesure 3577A/P:B/A|E HORIZONTAL WITH THOMSON SYSTEME (/CT1) AT .5M
-----
|EN1201035 |EN1201035 | 2.000E+08 Hertz      |-6.044E+001/ 3.390E+001 DB
|Mesure 3577A/P:B/A|E NORMAL WITH THOMSON SYSTEME (/CT1) AT .5M
-----
|EV1201040 |EV1201040 | 2.000E+08 Hertz      |-7.274E+001/ 2.572E+001 DB
|Mesure 3577A/P:B/A|E VERTICAL WITH THOMSON SYSTEME (/CT1) AT .5M
-----
|HN1201115 |HN1201115 | 2.000E+08 Hertz      |-6.323E+001/-2.315E+001 DB
|Mesure 3577A/P:B/A|N NORMAL WITH THOMSON SYSTEME (/CT1) AT .5M
-----
|HH1201120 |HH1201120 | 2.000E+08 Hertz      |-6.996E+001/-2.451E+001 DB
|Mesure 3577A/P:B/A|H HORIZONTAL WITH THOMSON SYSTEME (/CT1) AT .5M
-----
|HH1201130 |HH1201130 | 2.000E+08 Hertz      |-6.946E+001/-3.821E+001 DB
|Mesure 3577A/P:B/A|H HORIZONTAL WITH THOMSON SYSTEME (/CT1) AT 1M
-----
|HN1201135 |HN1201135 | 2.000E+08 Hertz      |-6.504E+001/-2.698E+001 DB
|Mesure 3577A/P:B/A|H NORMAL WITH THOMSON SYSTEME (/CT1) AT 1M
-----
|HV1201420 |HV1201420 | 2.000E+08 Hertz      |-4.958E+001/-1.305E+001 DB
|Mesure 3577A/P:B/A|H VERTICAL WITH THOMSON SYSTEME (/CT1) AT 1M 265mA/m et H3
|H0 NOT CORRECTED
-----
|HV1201445 |HV1201445 | 2.000E+08 Hertz      |-4.848E+001/-9.109E+000 dB
|Mesure 3577A/P:B/A|H VERTICAL WITH THOMSON SYSTEME (/CT1) AT 0.5M 265mA/m et
|H30 NOT CORRECTED
-----
|CT11201625|CT11201625| 2.000E+08 Hertz      |-1.039E+002/-2.583E+001 DB
|Mesure 3577A/P:B/A|CURRED ON WIRE 0.5M FROM DOOR EXTENDED VERTICAL WITH PAPER
|IN DOOR
-----
|CT11301010|CT11301010| 2.000E+08 Hertz      |-4.587E+001/-2.004E+001 dBvolt
|Mesure 3577A/P:A|REF WITH CT1 FOL 1000 AT 28dB
-----
|CT11301020|CT11301020| 2.000E+08 Hertz      |-9.790E+001/-3.604E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON VERTICAL WIRE AT 1M WITH PAPER IN DOOR
-----
|CT11301045|CT11301045| 2.000E+08 Hertz      |-9.141E+001/-2.975E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON VERTICAL WIRE AT .5M WITH PAPER IN DOOR

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Appendix B

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|CT11301100|CT11301100| 2.000E+08 Hertz      |-9.313E+001/-2.783E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON VERTICAL WIRE AT.5M WITH PAPER IN DOOR CT1 ELEVATED
|TED
-----
|CT11301115|CT11301115| 2.000E+08 Hertz      |-8.246E+001/-3.258E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON CT1 CLOSE TO GROUND
-----
|CT11301130|CT11301130| 2.000E+08 Hertz      |-1.153E+002/-1.534E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON CT1 CLOSE TO GROUND WITH 120CM OF PAPER
-----
|CT11301135|CT11301135| 2.000E+08 Hertz      |-1.481E+002/-4.542E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON CT1 CLOSE TO GROUND WITH 60 CM OF PAPER
-----
|CT11301140|CT11301140| 2.000E+08 Hertz      |-1.545E+002/-8.722E+001 DB
|Mesure 3577A/P:B/A|CURRENT ON CT1 CLOSE TO GROUND WITHOUT PAPER
-----
|CT11301405|CT11301405| 2.000E+08 Hertz      |-1.620E+002/-8.866E+001 DB
|B/A|CURRENT ON CT1 CLOSE TO GROUND WITHOUT PAPER ON HORIZONTAL WIRE 175 CM FROM DOOR
-----
|CT11301420|CT11301420| 2.000E+08 Hertz      |-1.536E+002/-8.968E+001 DB
|B/A|SAME AS "CT11301405" WITH CABLE GENERATE THE SIGNAL NOT AT THE GROUND
-----
|NOI1301430|NOI1301430| 2.000E+08 Hertz      |-1.417E+002/-7.237E+001 DBvolt
|Mesure 3577A/P:B|NOISE CABLE GENERATE THE SIGNAL NOT AT THE GROUND
-----
|CT11301445|CT11301445| 2.000E+08 Hertz      |-8.761E+001/-7.868E+000 DB
|B/A|CURRENT ON CT1 CLOSE TO GROUND 180 CM PAPER ON HORIZONTAL WIRE 175 CM FROM DOOR
-----
|CT11301450|CT11301450| 2.000E+08 Hertz      |-1.023E+002/-1.969E+001 DB9dB
|Mesure 3577A/P:B/A|CURRENT ON CT1 CLOSE TO GROUND 120 CM PAPER ON HORIZONTAL WIRE 175 CM FROM DOOR
-----
|CT11301455|CT11301455| 2.000E+08 Hertz      |-1.676E+002/-8.282E+001 DBvolt
|Mesure 3577A/P:B|CURRENT ON CT1 CLOSE TO GROUND 60 CM PAPER ON HORIZONTAL WIRE 175 CM FROM DOOR
-----
|CT11301515|CT11301515| 2.000E+08 Hertz      |-1.325E+002/-3.695E+001 dB
|Mesure 3577A/P:B/A|SAME AS "CT11301135" BUT NO CABLE NOISE
-----
|CT11301540|CT11301540| 2.000E+08 Hertz      |-1.161E+002/-3.886E+001 DB
|Mesure 3577A/P:B/A|SAME AS CT11201625 BUT WITH WIRE AT 1.0M
-----
|I11401125 |I11401125 | 2.000E+08 Hertz      |-1.181E+002/-3.081E+001 DB
|Mesure 3577A/P:B/A|BULK(I) ON AC POWER LINE HORIZONTAL NEAR FLOOR SHIELD 6m LENGTH
-----
|I21401140 |I21401140 | 2.000E+08 Hertz      |-9.364E+001/-3.094E+001 DB
|Mesure 3577A/P:B/A|BULK(I) ON GROUND STRAP BETWEEN TWO RACKS
-----
|I31401145 |I31401145 | 2.000E+08 Hertz      |-1.535E+002/-3.399E+001 DB
|Mesure 3577A/P:B/A|BULK(I) ON POWER CORD HORIZONTAL BETWEEN 3 RACKS 2m LENGTH

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| I41401150 | I41401150 | 2.000E+08 Hertz | -1.441E+002/-3.396E+001 DB
| Mesure 3577A/P:B/A|BULK(I) ON POWER CORD VERTICAL 1RACK 1m LENGTH
-----
| I51401155 | I51401155 | 2.000E+08 Hertz | -1.433E+002/-4.267E+001 DB
| Mesure 3577A/P:B/A|I ON SINGLE CONDUCTOR OF RIBBON CABLE VERTICAL 1RACK .5m LE
| NGTH
-----
| I61401205 | I61401205 | 2.000E+08 Hertz | -1.004E+002/-2.688E+001 DB
| Mesure 3577A/P:B/A|BULK(I) ON HORIZONTAL COAX BETWEEN 3 RACKS h=1m - 2m LENGTH
-----
| I71401210 | I71401210 | 2.000E+08 Hertz | -1.517E+002/-4.243E+001 DB
| Mesure 3577A/P:B/A|BULK(I) ON VERTICAL COAX 1 RACKS 1m LENGTH
-----
| I81401215 | I81401215 | 2.000E+08 Hertz | -1.158E+002/-2.929E+001 DB
| Mesure 3577A/P:B/A|BULK(I) ON "L"SHAPE COAX 2 RACKS 1m LENGTH
-----
| I91401330 | I91401330 | 2.000E+08 Hertz | -1.098E+002/-3.478E+001 DB
| Mesure 3577A/P:B/A|BULK(I) ON HORIZONTAL COAX 2 RACKS 1m LENGTH
-----
| I101401335 | I101401335 | 2.000E+08 Hertz | -1.381E+002/-2.238E+001 DB
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-----
| I111401345 | I111401345 | 2.000E+08 Hertz | -1.270E+002/-2.230E+001 DB
| Mesure 3577A/P:B/A|BULK(I) ON HORIZONTAL GPIB BETWEEN 3 RACKS 1.5m LENGTH
-----
| I121401350 | I121401350 | 2.000E+08 Hertz | -1.217E+002/-2.575E+001 DB
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-----
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-----
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-----
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-----
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Appendix B

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-----  
| POS6180CT | POS6180CT | 2.000E+08 Hertz      | -9.025E+001 / -2.713E+001 dBvolt  
| Measure 3577A/P:B |  
-----  
| POS1180CT | POS1180CT | 2.000E+08 Hertz      | -9.597E+001 / -3.654E+001 dBvolt  
| Measure 3577A/P:B |  
-----  
| POS5R180CT | POS5R180CT | 2.000E+08 Hertz      | -9.067E+001 / -3.621E+001 dBvolt  
| Measure 3577A/P:B | REPEAT OF POS 5  
-----  
| FT_91550_5 | FT_91550_5 | 2.000E+08 Hertz      | 1.999E-001 / 1.520E+000  
| Measure 3577A/P:B/R/D | TRANSFERT FONCTION OF CURRENT PROBE (IMPEDANCE)  
-----  
| TDRMSL_50 | TDRMSL_50 | 1.029E-07 Seconds    | 5.150E+001 / 2.156E+002 Ohms  
| Measure / TEK11801 | 50 OHMS TDR  
-----  
| TDRMSL_OC | TDRMSL_OC | 1.029E-07 Seconds    | 5.099E+001 / 2.473E+002 Ohms  
| Measure / TEK11801 | OPEN CIRCUIT TDR  
-----  
| TDRMSL_SC | TDRMSL_SC | 1.029E-07 Seconds    | 3.654E+001 / 2.253E+002 Ohms  
| Measure / TEK11801 | SHORT CIRCUIT TDR  
-----  
| FT_94430_2 | FT_94430_2 | 2.000E+08 Hertz      | 8.175E-002 / 1.029E+000  
| Measure 3577A/P:B/R/D | IMPEDANCE OF CURRENT PROBE USED FOR TELEPHONE AND COAX(9  
| 4430_2 )  
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