

REPORT DOCUMENTATION PAGE

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	5b. GRANT NUMBER
	5c. PROGRAM ELEMENT NUMBER

Please see
attached

6. AUTHOR(S)	5d. PROJECT NUMBER 2302
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9. SPONSORING / MONITORING AGENCY NAME(S) AND ADDRESS(ES) Air Force Research Laboratory (AFMC) AFRL/PRS 5 Pollux Drive Edwards AFB CA 93524-7048	10. SPONSOR/MONITOR'S ACRONYM(S)
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12. DISTRIBUTION / AVAILABILITY STATEMENT
Approved for public release; distribution unlimited.

13. SUPPLEMENTARY NOTES

14. ABSTRACT

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15. SUBJECT TERMS

16. SECURITY CLASSIFICATION OF:			17. LIMITATION OF ABSTRACT <div style="text-align: center; border: 1px solid black; border-radius: 50%; width: 40px; height: 40px; display: flex; align-items: center; justify-content: center;">A</div>	18. NUMBER OF PAGES	19a. NAME OF RESPONSIBLE PERSON Leilani Richardson
a. REPORT Unclassified	b. ABSTRACT Unclassified	c. THIS PAGE Unclassified			19b. TELEPHONE NUMBER (include area code) (661) 275-5015

MEMORANDUM FOR PRS (In-House Publication)

FROM: PROI (STINFO)

22 May 2002

SUBJECT: Authorization for Release of Technical Information, Control Number: **AFRL-PR-ED-VG-2002-130**
C.T. Liu (PRSM); F.P. Chiang (NYSU), "Investigating the Deformation and Failure Mechanisms in Bi-Material Systems Under Tension"

ASME Winter Meeting
(Blacksburg, VA, 24-28 June 2002) (Deadline = 23 June 2002)

(Statement A)

- 1. This request has been reviewed by the Foreign Disclosure Office for: a.) appropriateness of distribution statement, b.) military/national critical technology, c.) export controls or distribution restrictions, d.) appropriateness for release to a foreign nation, and e.) technical sensitivity and/or economic sensitivity.

Comments: _____

Signature _____ Date _____

- 2. This request has been reviewed by the Public Affairs Office for: a.) appropriateness for public release and/or b) possible higher headquarters review.

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Comments: _____

Signature _____ Date _____

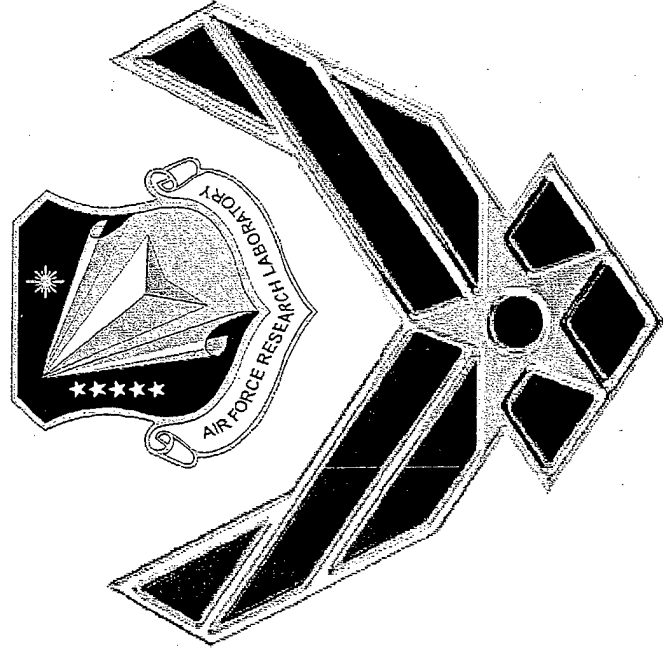
- 4. This request has been reviewed by PR for: a.) technical accuracy, b.) appropriateness for audience, c.) appropriateness of distribution statement, d.) technical sensitivity and economic sensitivity, e.) military/national critical technology, and f.) data rights and patentability

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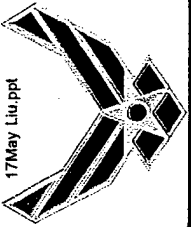
PHILIP A. KESSEL Date
Technical Advisor
Space and Missile Propulsion Division

Investigating the Deformation and Failure Mechanisms in Bi- Material Systems under Tension



C.T. Liu
AFRL/PRSM 10 E. Saturn Blvd.
Edwards AFB CA 93524-7680

Fu-Pen Chiang
Department of Mechanical Engineering
State University of New York
Stony Brook, N. Y. 11790



Objectives



≠ Investigate the Local Strain Distribution and Failure Mode in a Bi-Material Bonded

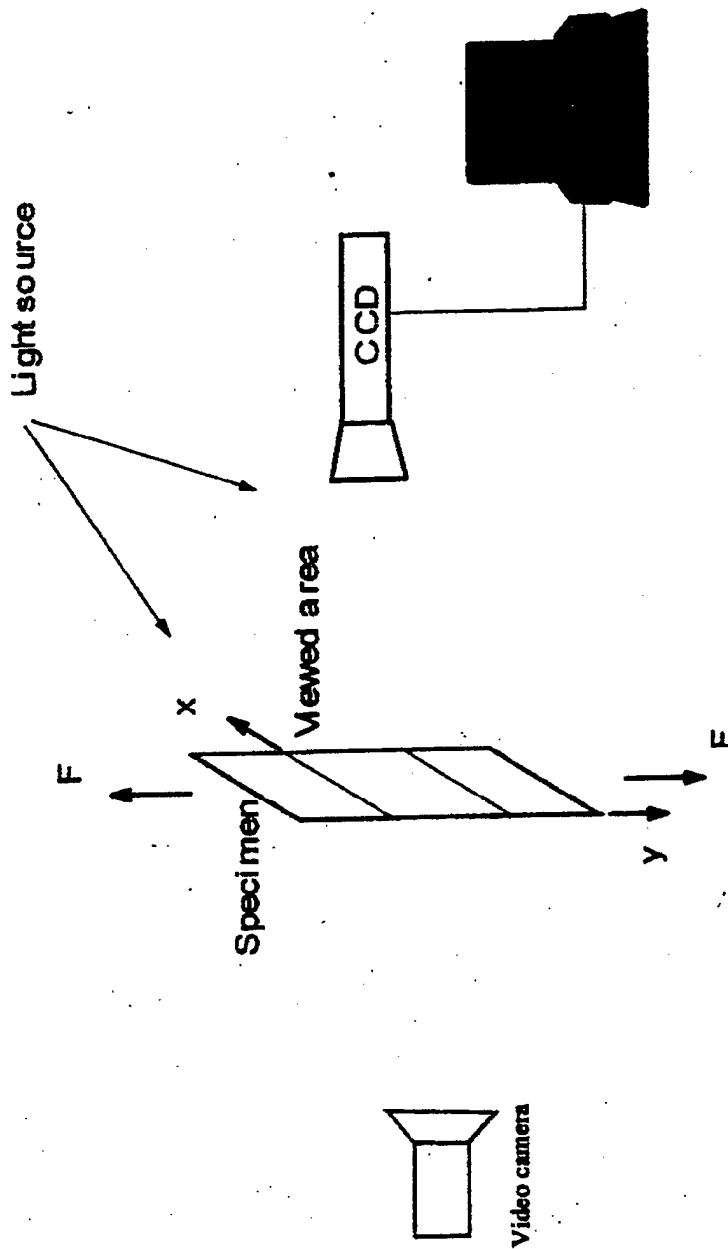
—Specimens under a Constant Displacement Rate Condition.

* Displacement Rate = 0.02 in/min

≠ Determine the Critical Strain for Debond at the Interface between the Two Materials.



Experimental Set-Up



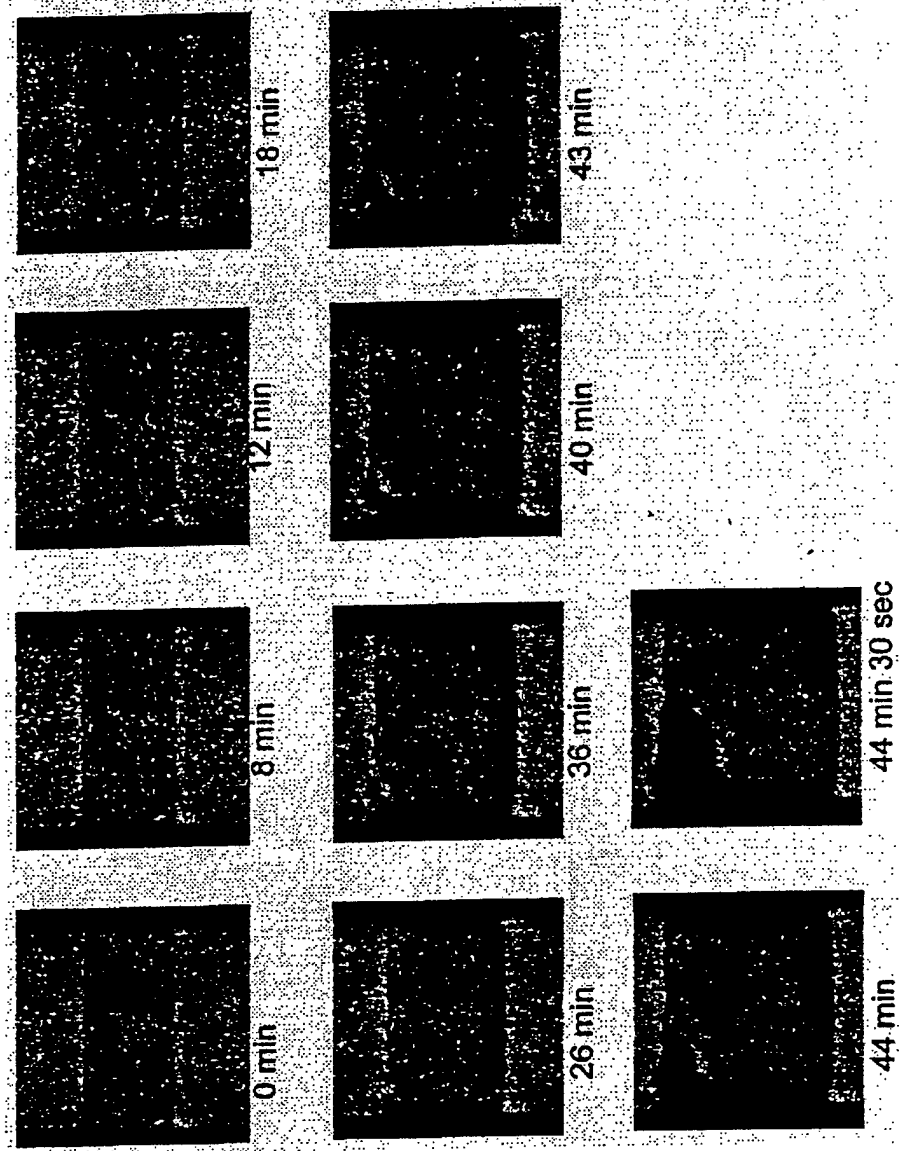


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The Mechanism of Debonding



Thickness to Width Ratio: 1:1:00

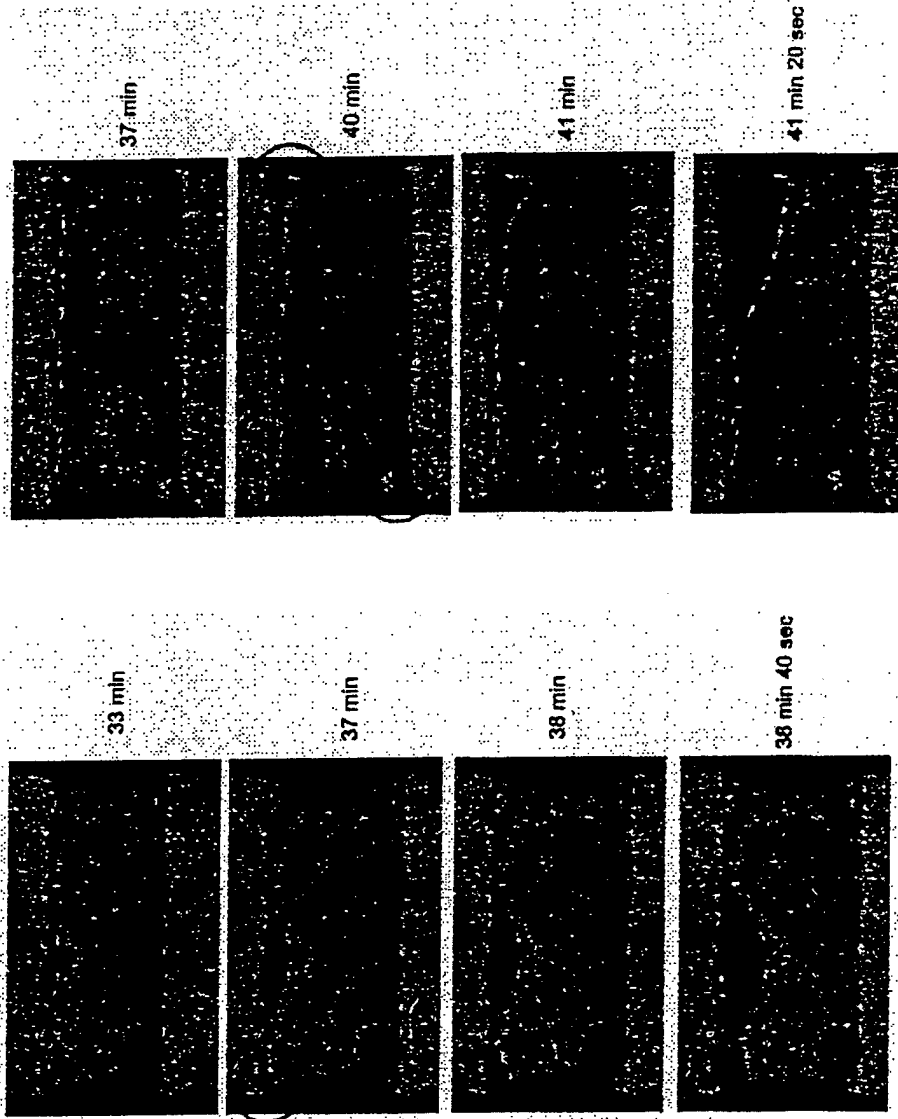




The Mechanism of Debonding



Thickness to Width Ratio: 1:2.25

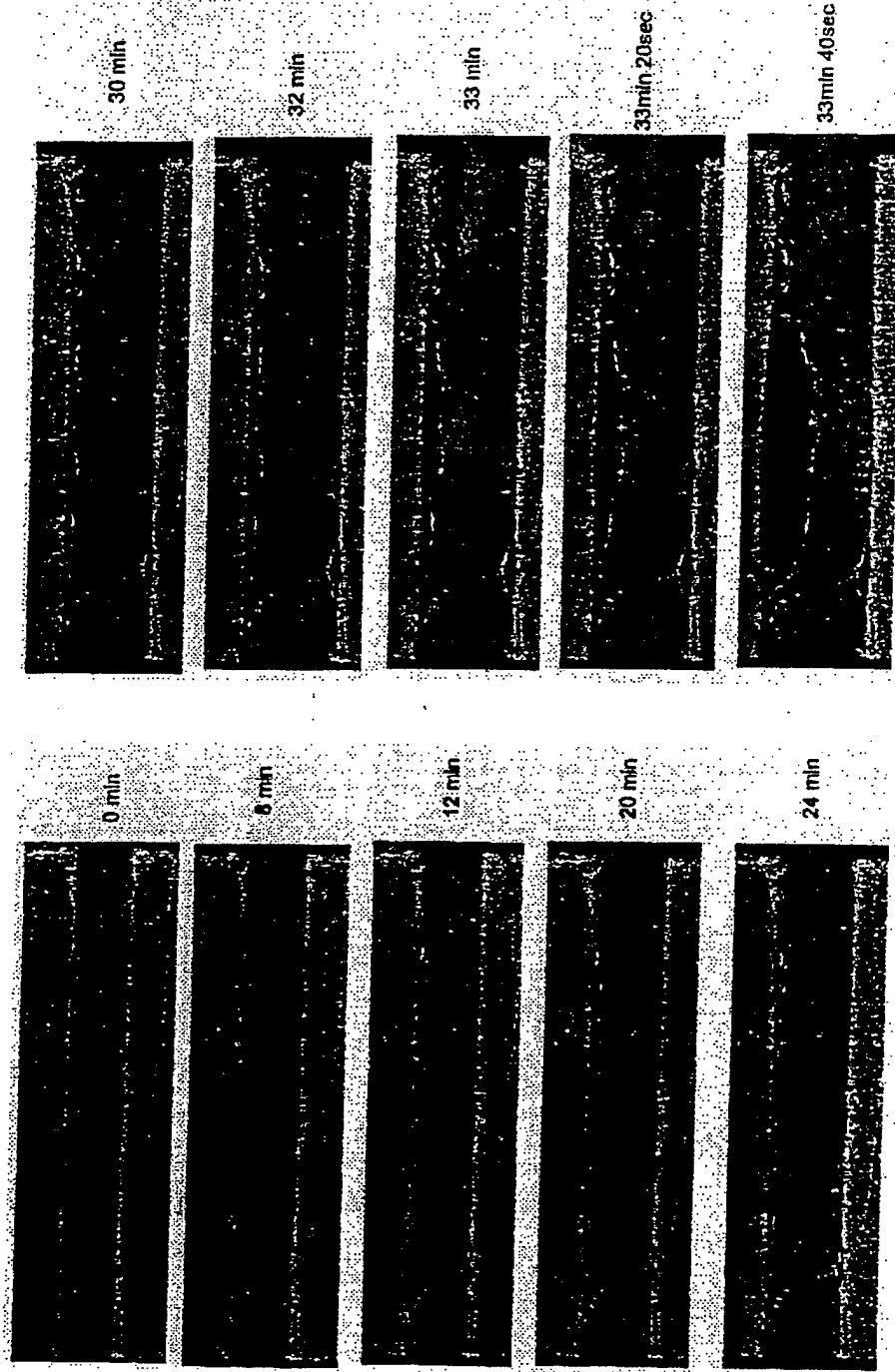




The Mechanism of Debonding



Thickness to Width Ratio: 1:5.00





AI071 DHR

The Debonding Modes



Size: t x w (in)	Ratio: t:w	Number of Specimens	Debond at center	Debond at corner
0.2 x 1	1:5	2	2	0
0.2 x 0.5	1:2.5	3	3	0
0.2 x 0.4	1:2	4	1	3
0.2 x 0.2	1:1	2	0	2

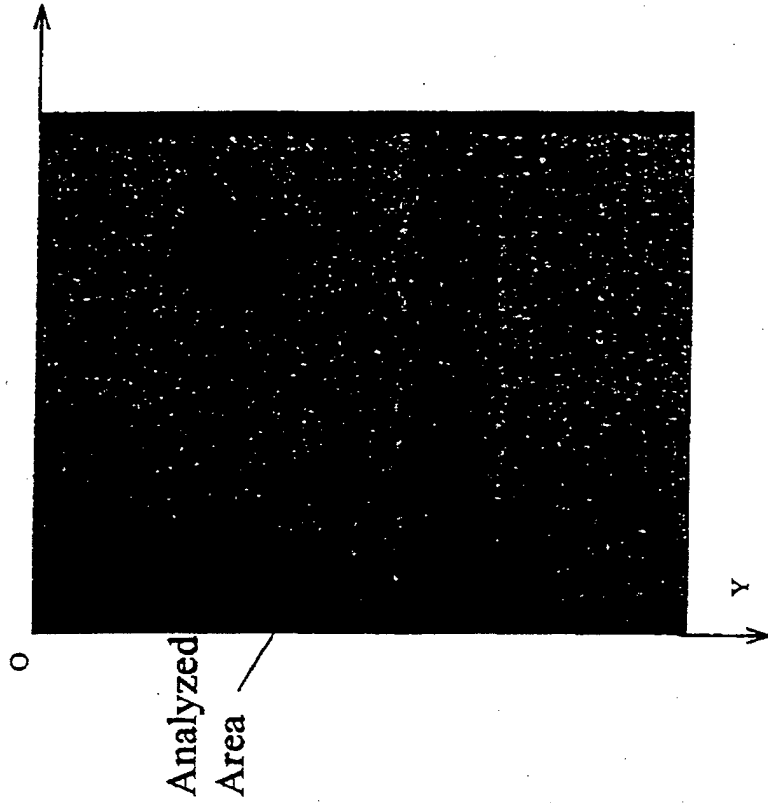
H ~ 4 in
h ~ 0.1 in

Critical ratio: ~ 1:2.25; either mode may prevail

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Analysis of Deformation

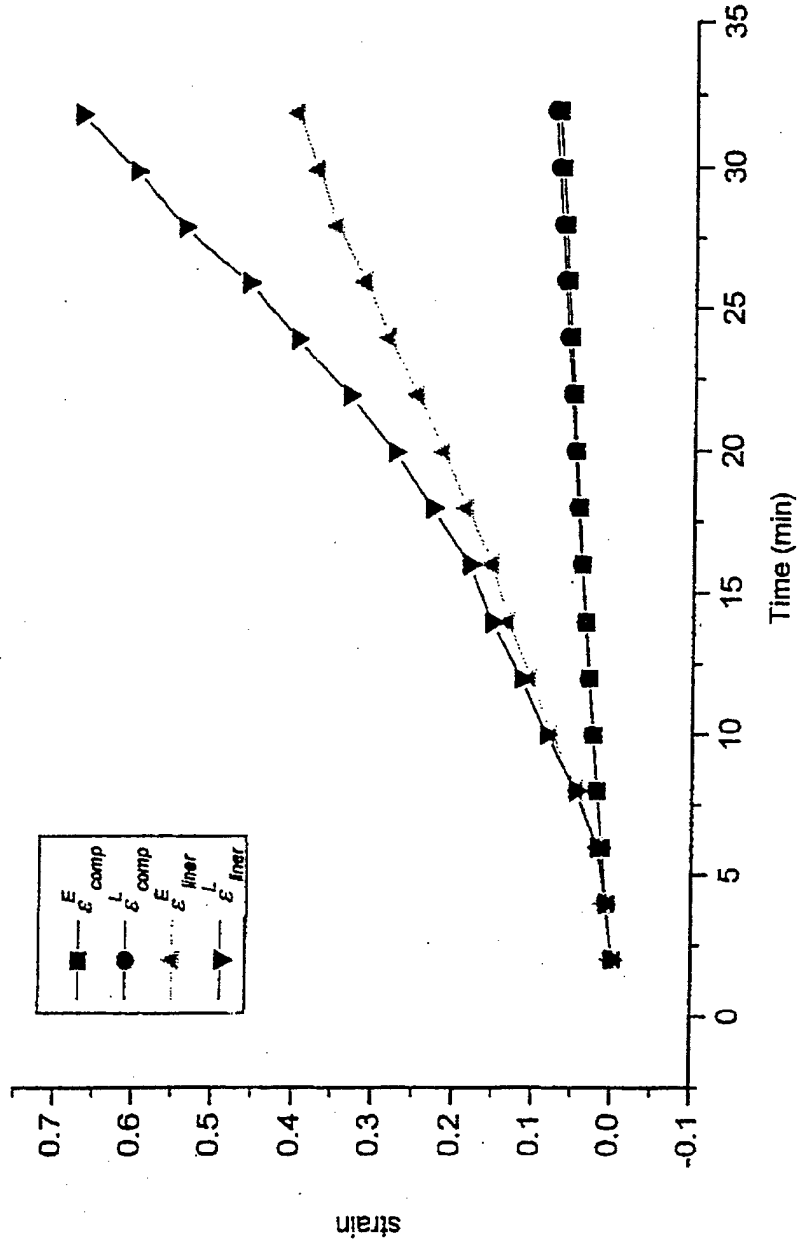




Average Strain Versus Force Curves



Thickness to Width Ratio: 1:5.00



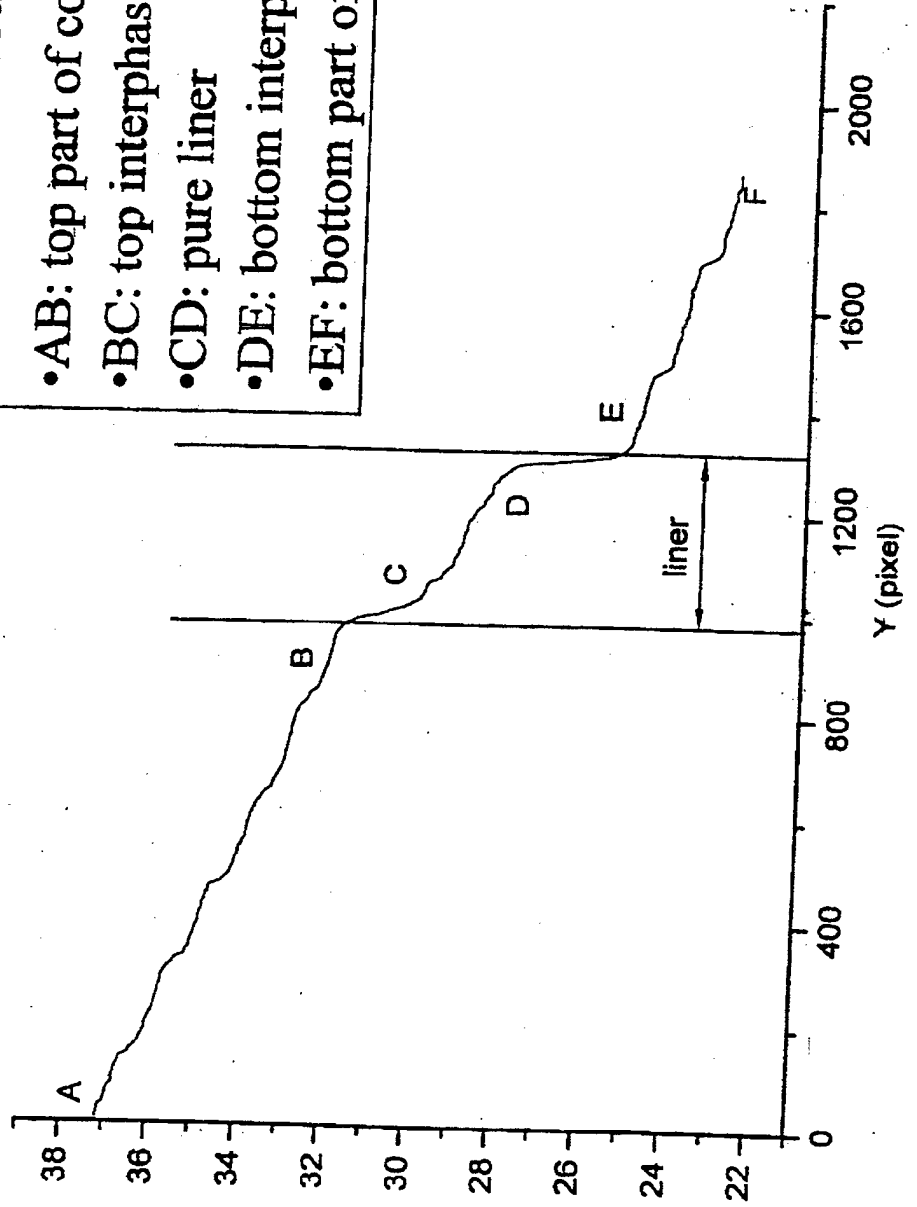


Displacement Increment Distribution along y



Direction

displacement increment between 8 and 10 min
 Δv (pixel)



Five linear sections:

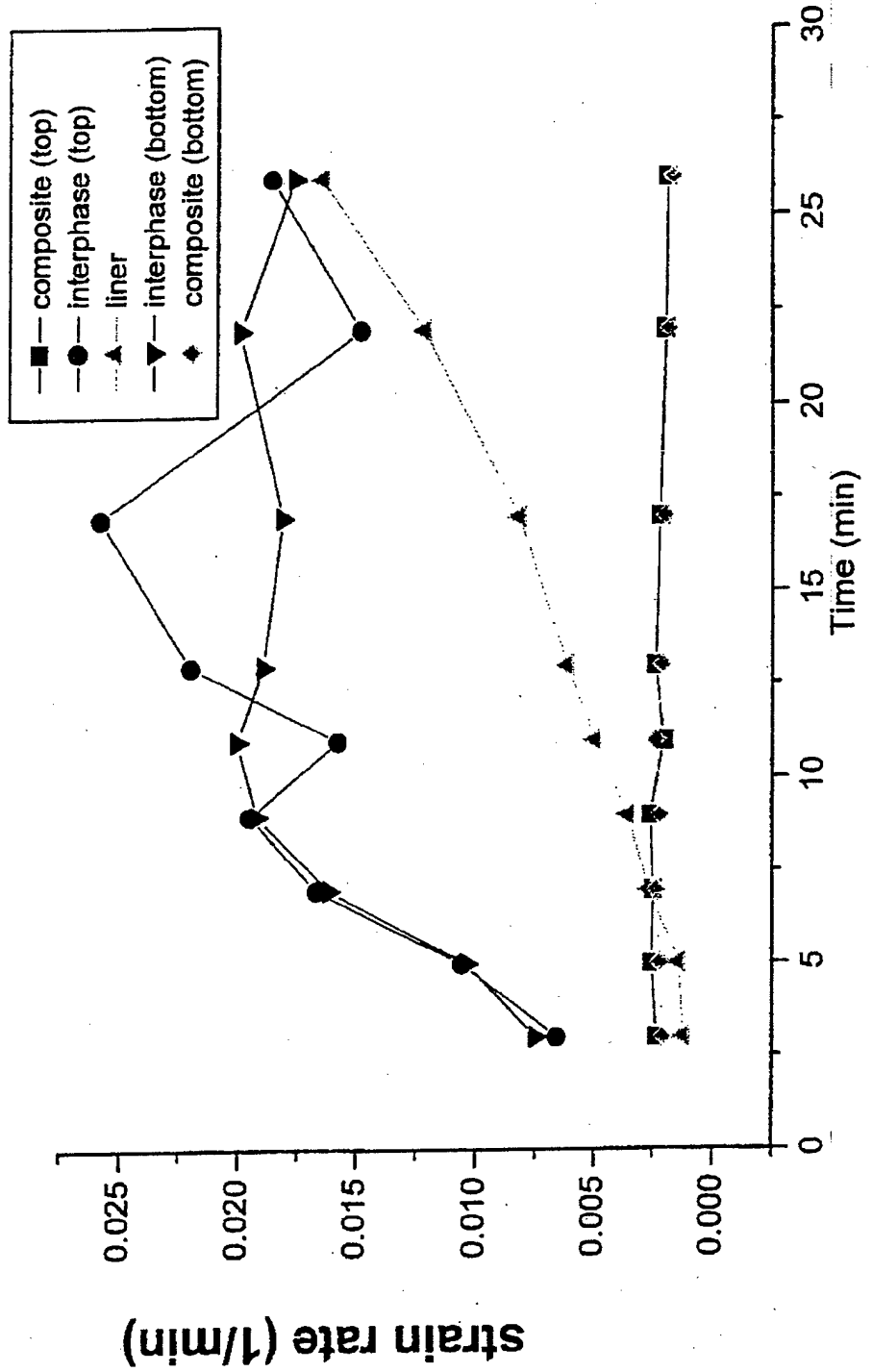
- AB: top part of composite
- BC: top interphase
- CD: pure liner
- DE: bottom interphase
- EF: bottom part of composite



Strain Rate versus Time Curves



Thickness to Width Ratio: 1:2.25



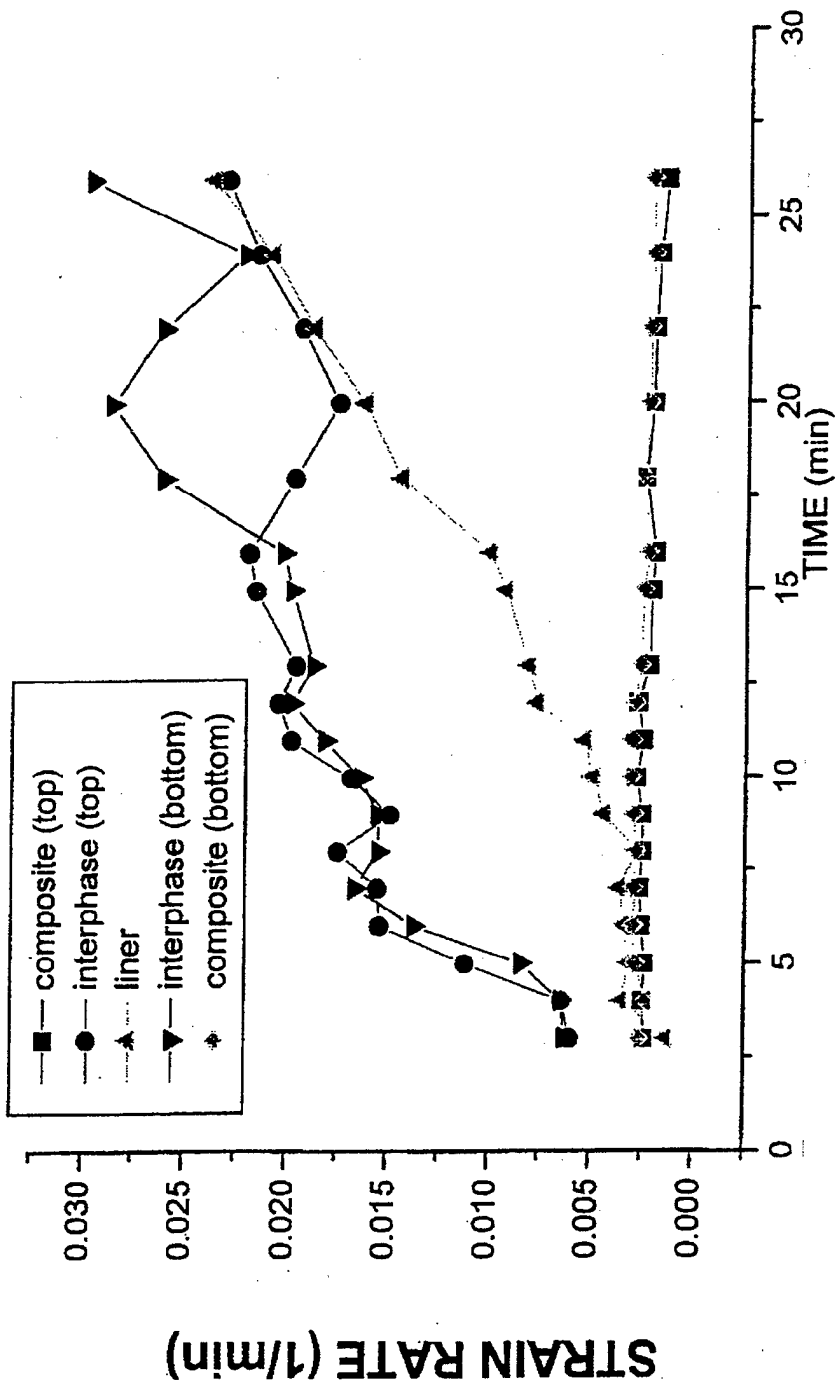


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Strain Rate versus Time Curves

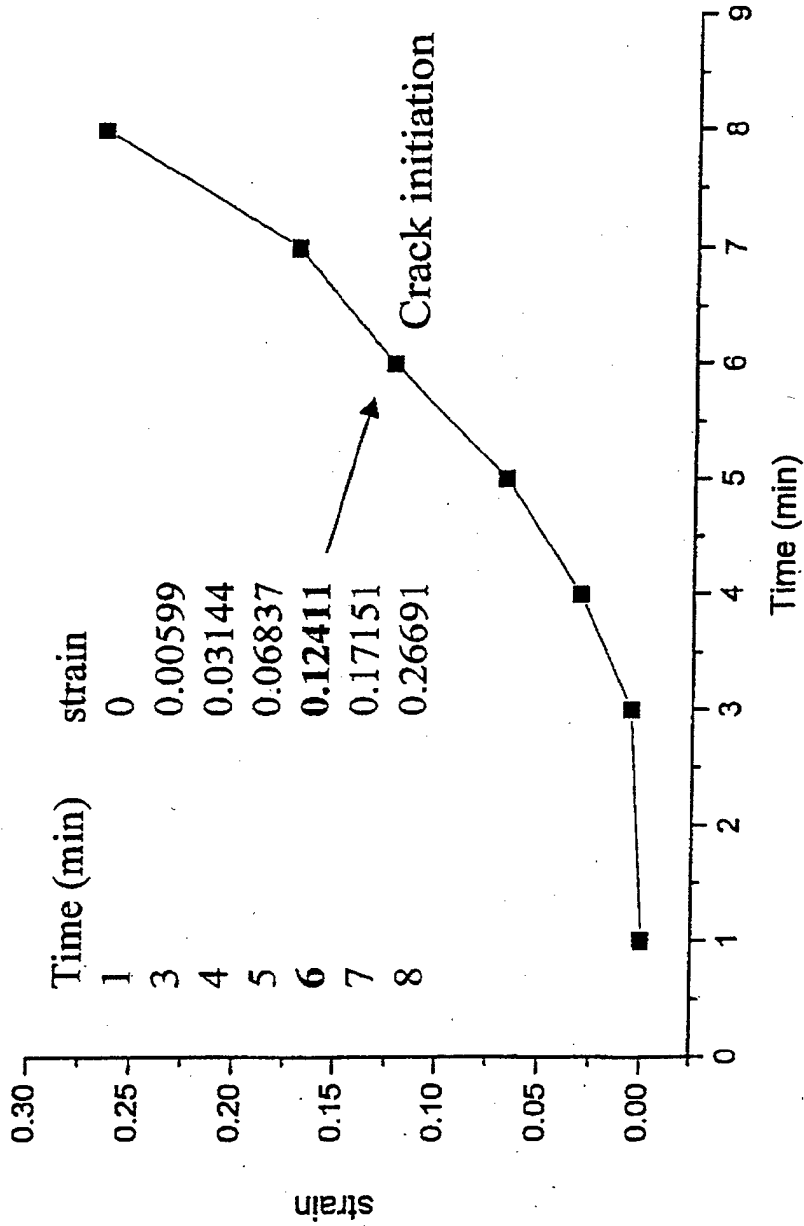


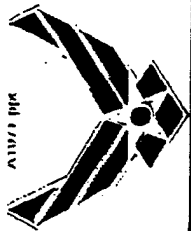
Thickness to Width Ratio: 1:5.00





The Time History of Local Strain near Interface

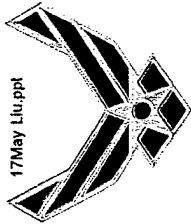




Summary of Debonding Initiation Strain



Specimen #	Size: t x w (in)	Ratio: t:w	Crack initiation strain
k	0.2 x 1	1:5	0.12
n	0.2 x 0.5	1:2.5	0.14
w	0.2 x 0.45	1:2.25	0.13
o	0.2 x 0.2	1:1	0.13



Conclusions



- ✘ The Failure location depends on the geometry of the specimen.
- ✘ There are interphase regions near the interfaces of the specimen.
- ✘ The strain rates in the rubber layer and the interface region change with time.
- ✘ The strain rate in the interphase region is significant higher than that in the rubber and the composite layers.
- ✘ The average critical local debond strain is 13%, which is independent of specimen geometry.