



ASAP 2003 WORKSHOP
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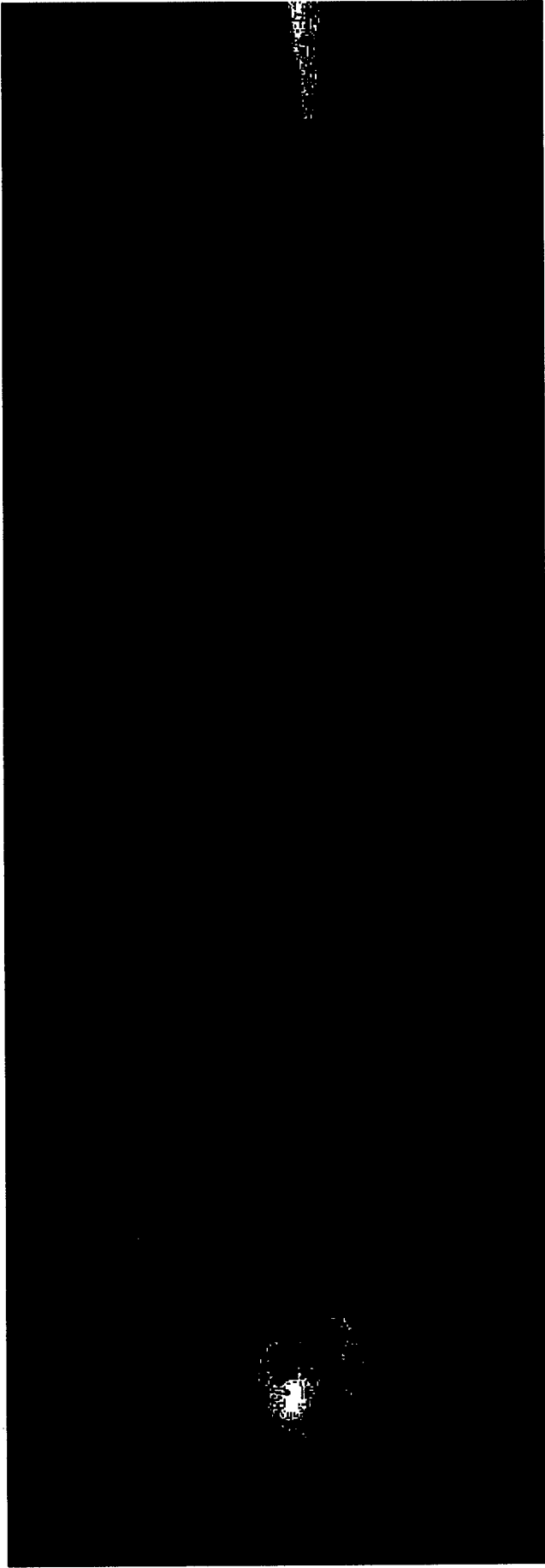
**REGISTRATION-BASED SOLUTIONS
TO THE RANGE-DEPENDENCE PROBLEM
IN STAP RADARS**

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INTRODUCTION



- **GOAL: TARGET DETECTION FOR ARBITRARY, POSSIBLY UNKNOWN
BISTATIC CONFIGURATIONS**
- **DIFFICULTY: COMPLEX NATURE OF RANGE-DEPENDENT BISTATIC CLUTTER**




OUTLINE

- INTRODUCTION
- CONFIGURATIONS AND SIGNALS
- RANGE-DEPENDENCE PROBLEM
- SNAPSHOT AND SPECTRUM
- STAP PROCESSOR
- EXISTING COMPENSATION METHODS
- NEW REGISTRATION-BASED METHODS
- SUMMARY

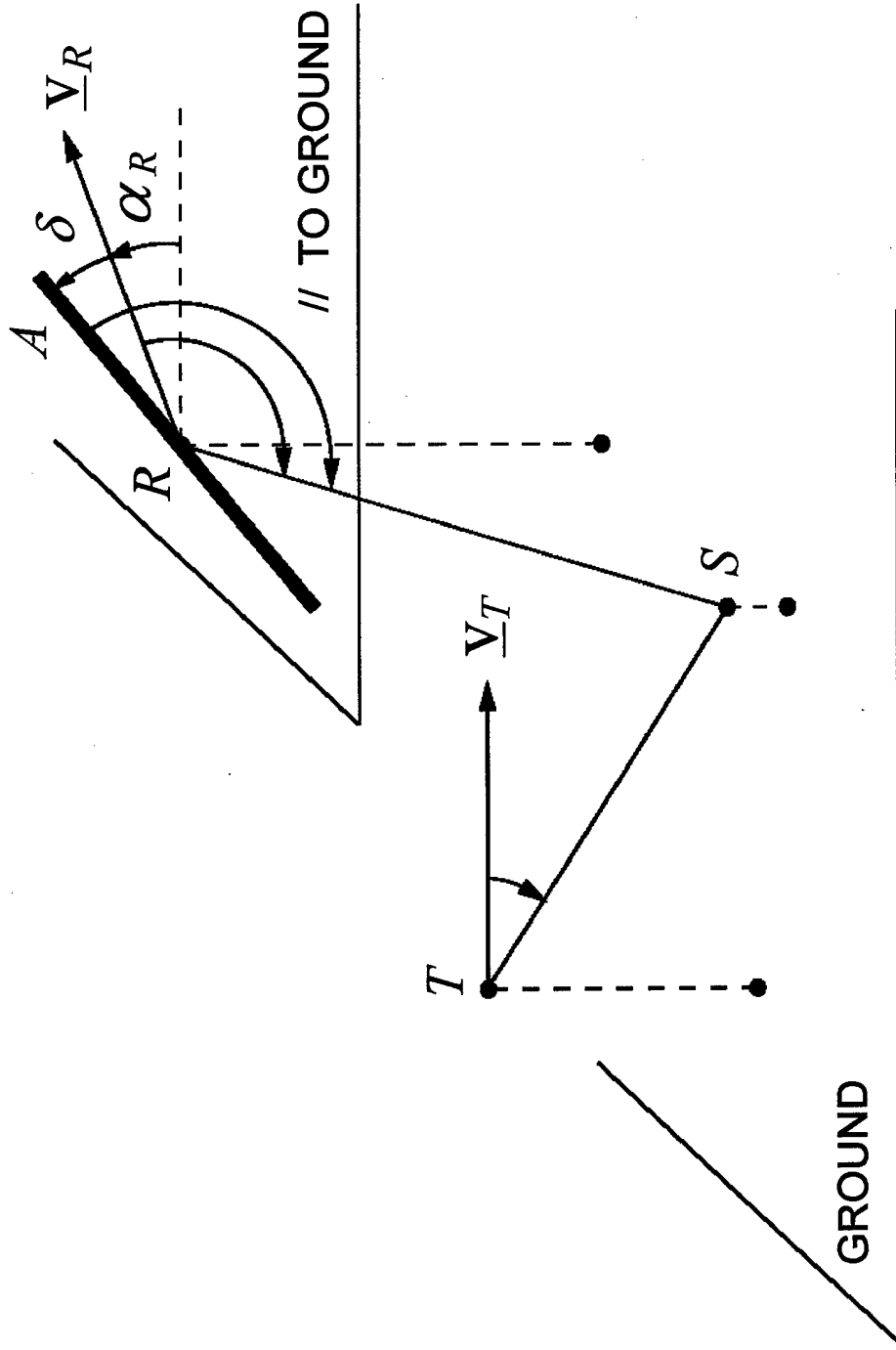


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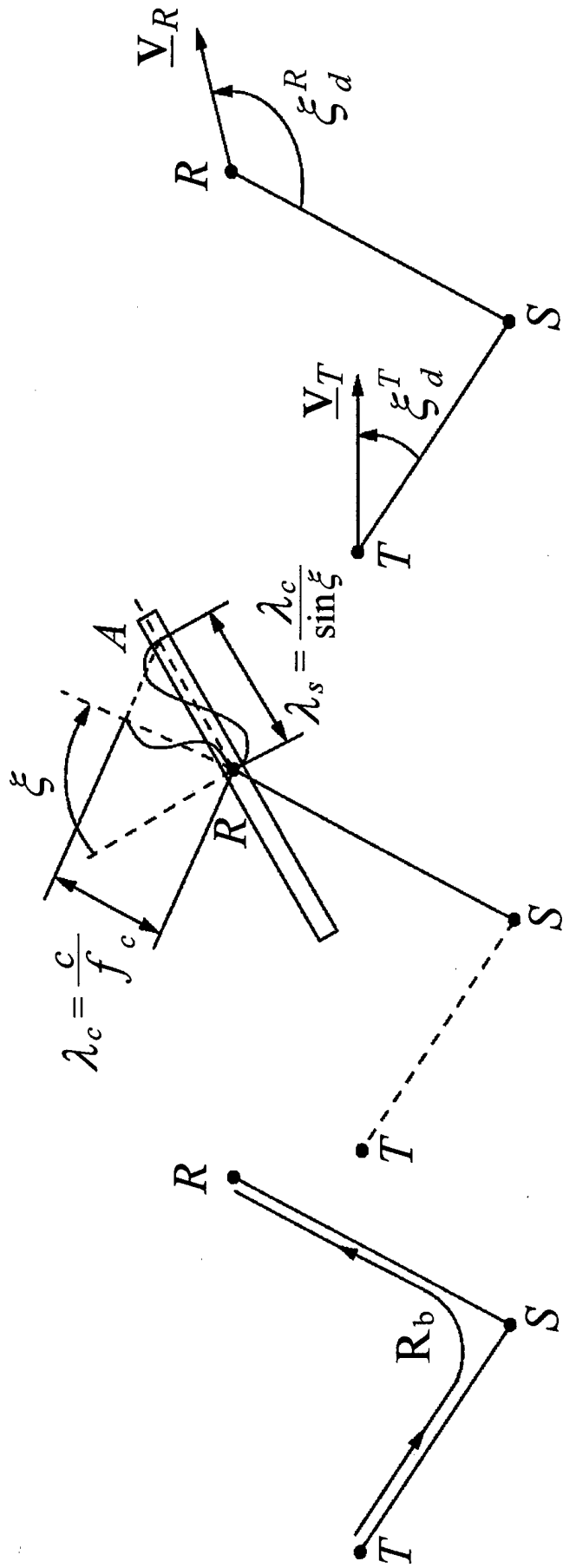
RADAR-MEASUREMENT CONFIGURATION: BISTATIC



GROUND IS ASSUMED TO BE A FLAT (HORIZONTAL) PLANE



WHAT DOES THE RADAR MEASURE ? DUAL VIEW



$$\tau_{rt} = \frac{R_b}{c}$$

“ROUNDTRIP” DELAY

τ_{rt}

$$f_s = \frac{1}{\lambda_s} = \frac{\sin \xi}{\lambda_c}$$

SPATIAL FREQUENCY

$f_s \rightarrow V_s$

$$f_d = \frac{V_T \cos \xi_d^T}{\lambda_c} + \frac{V_R \cos \xi_d^R}{\lambda_c}$$

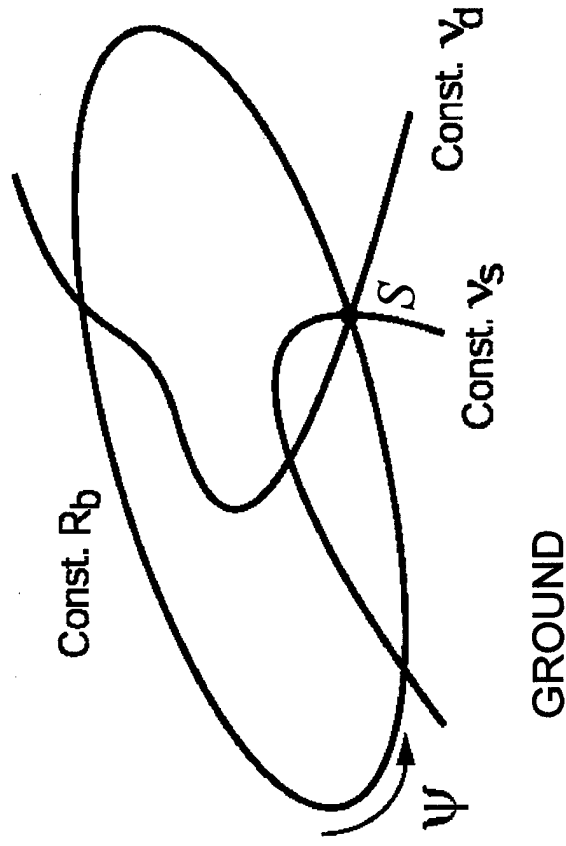
DOPPLER FREQUENCY

$f_d \rightarrow V_d$

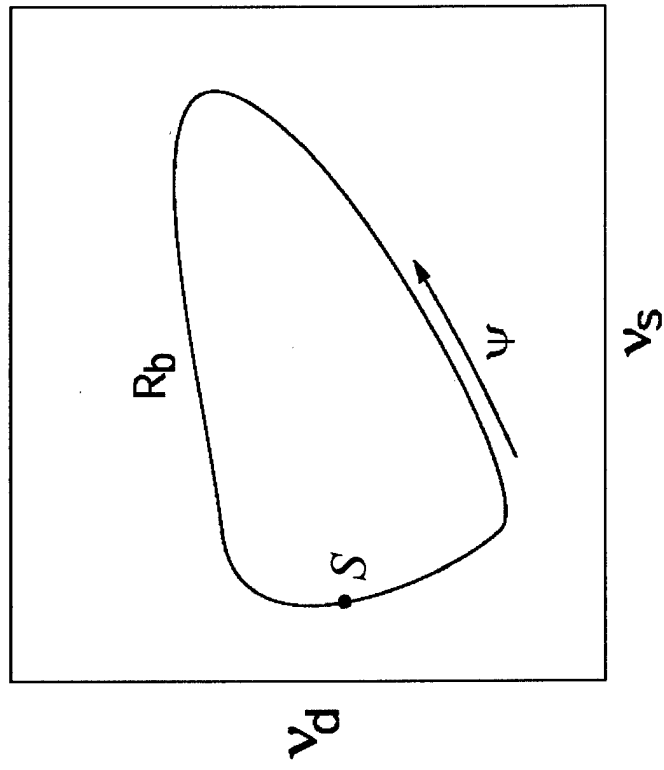


ABSTRACTING CONFIGURATIONS AND SIGNALS: DIRECTION-DOPPLER (DD) CURVES

ISOCURVES
(R_b, v_s, v_d)



DIRECTION-DOPPLER (DD) CURVES
(for a given R_b)



WHAT HAPPENS WHEN R_b CHANGES ?



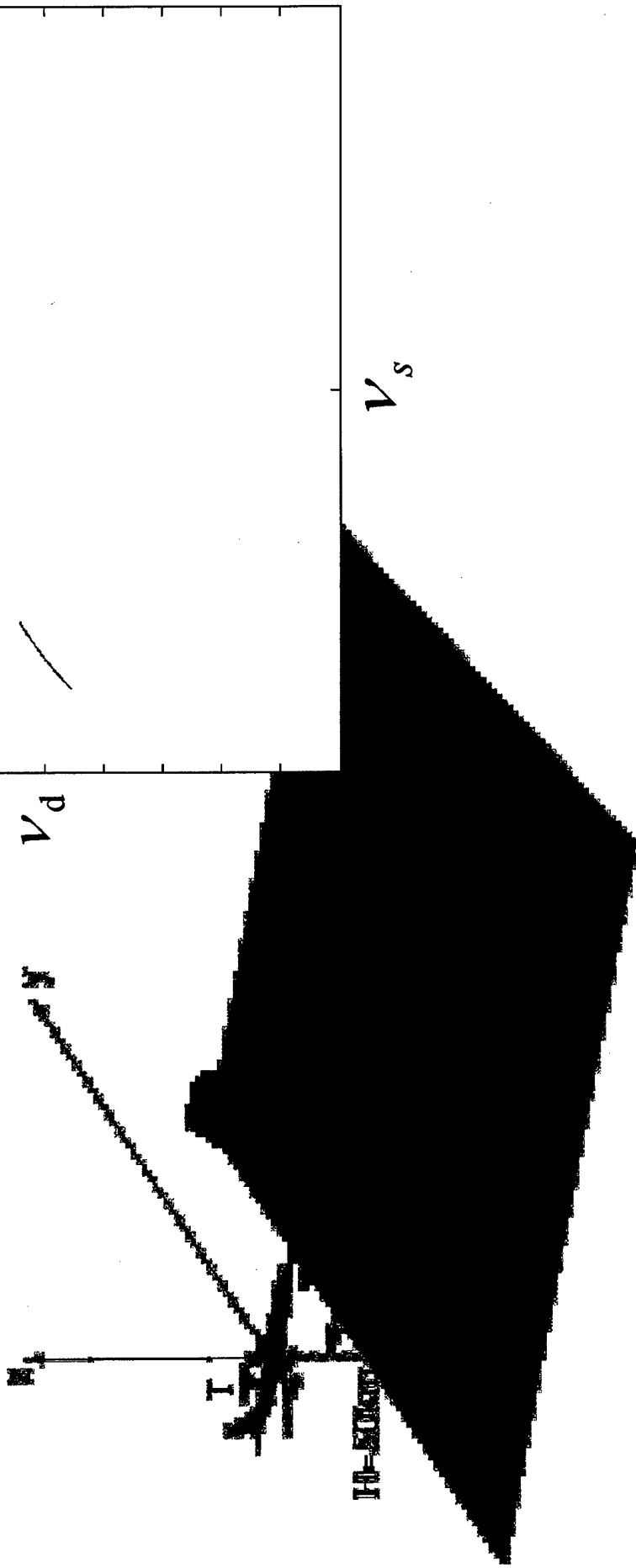
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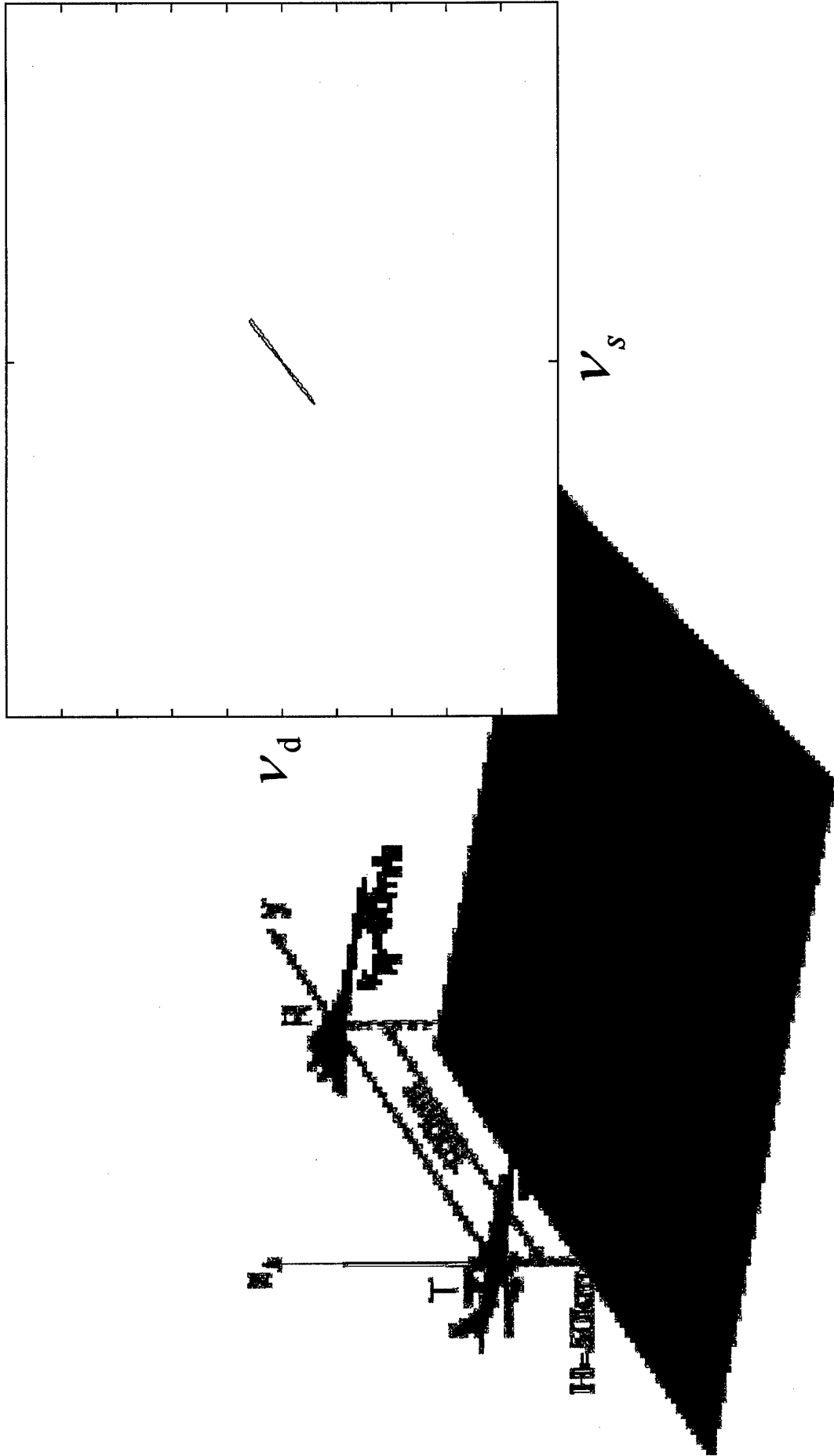


EXAMPLE DD CURVES: BISTATIC, IN-TRAIL, SIDELOOKING



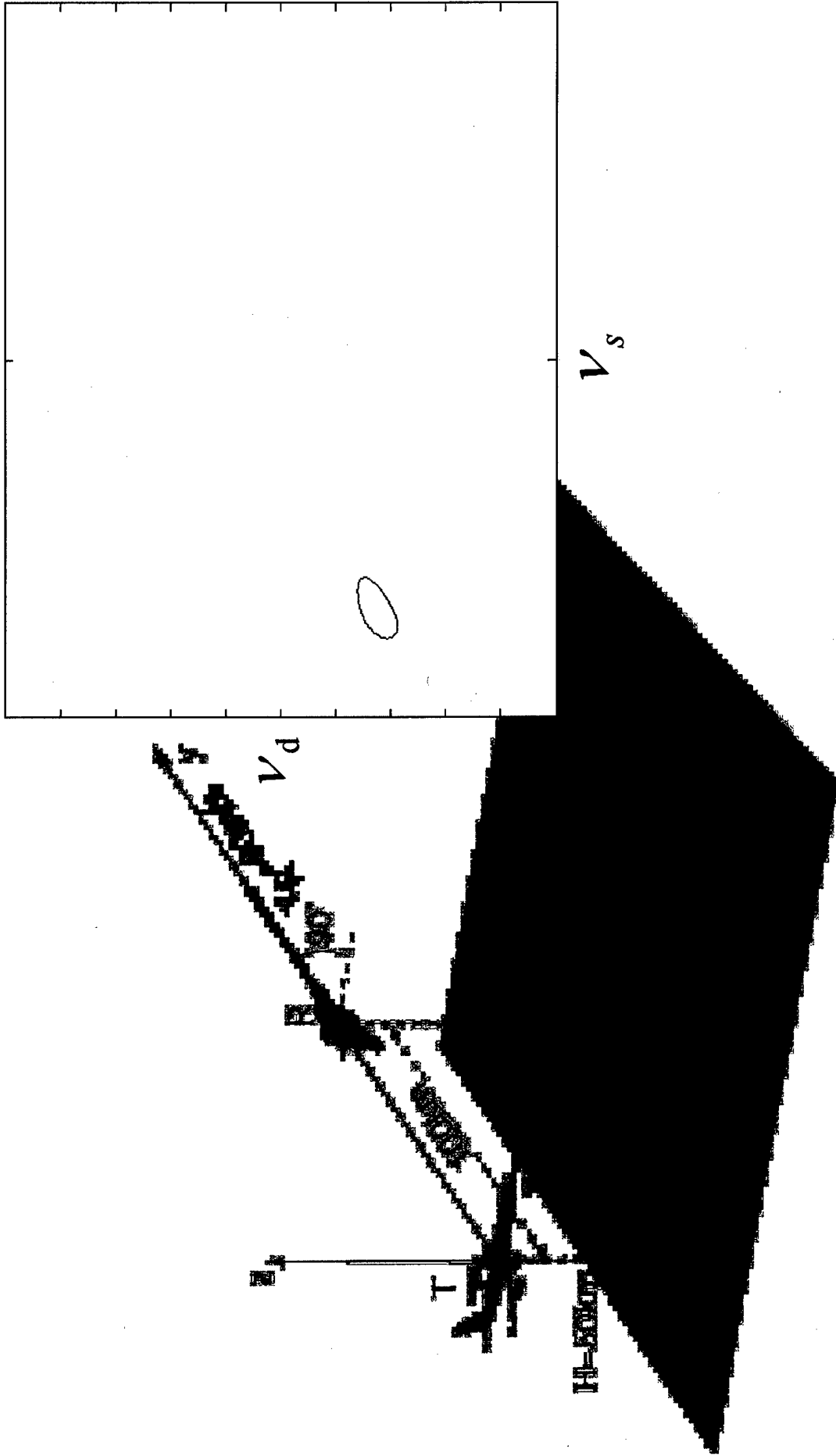


EXAMPLE DD CURVES: BISTATIC, WING-TO-WING, SIDELOOKING

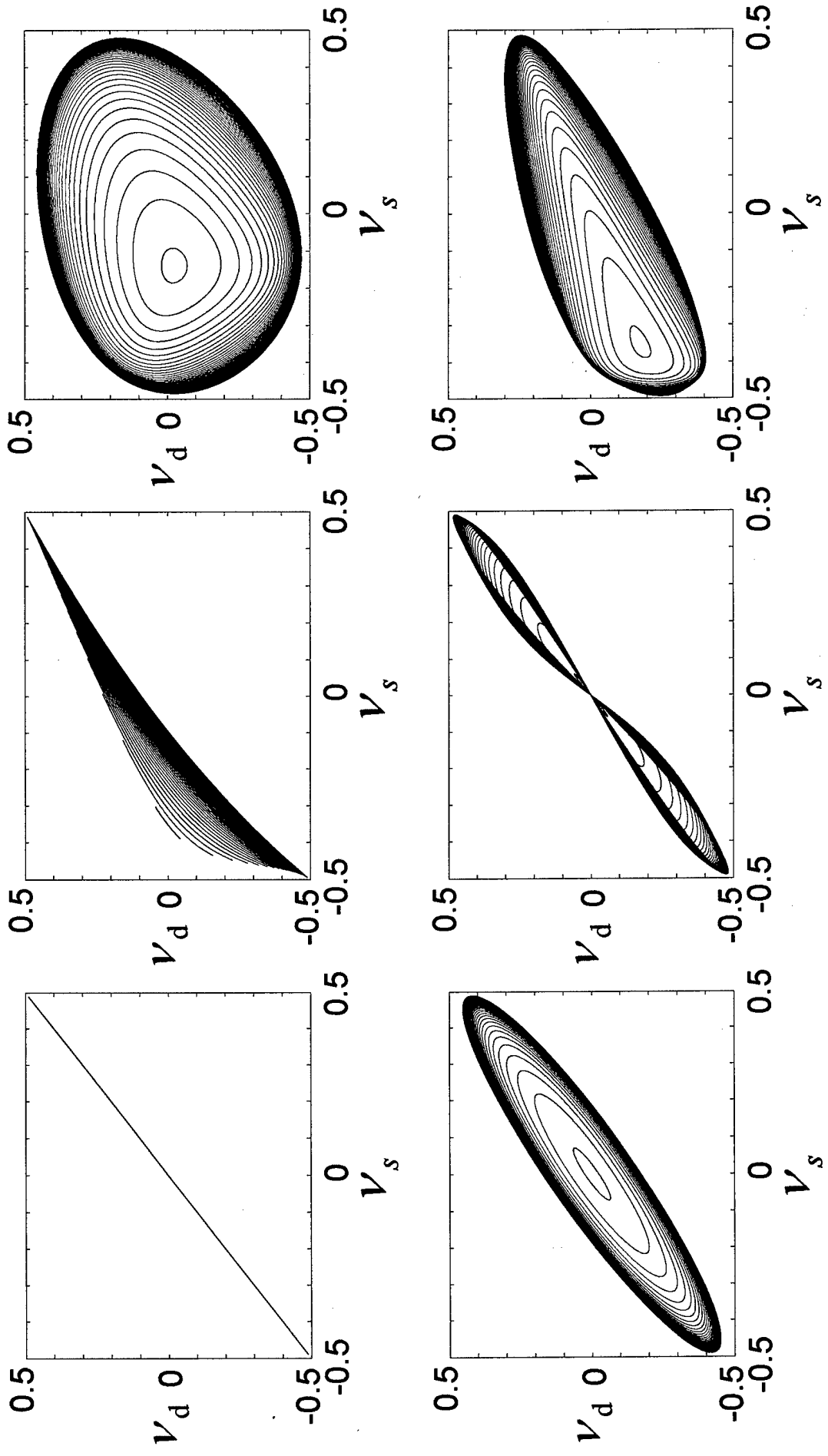




EXAMPLE DD CURVES: BISTATIC, WING-TO-FUSELAGE, SIDELOOKING

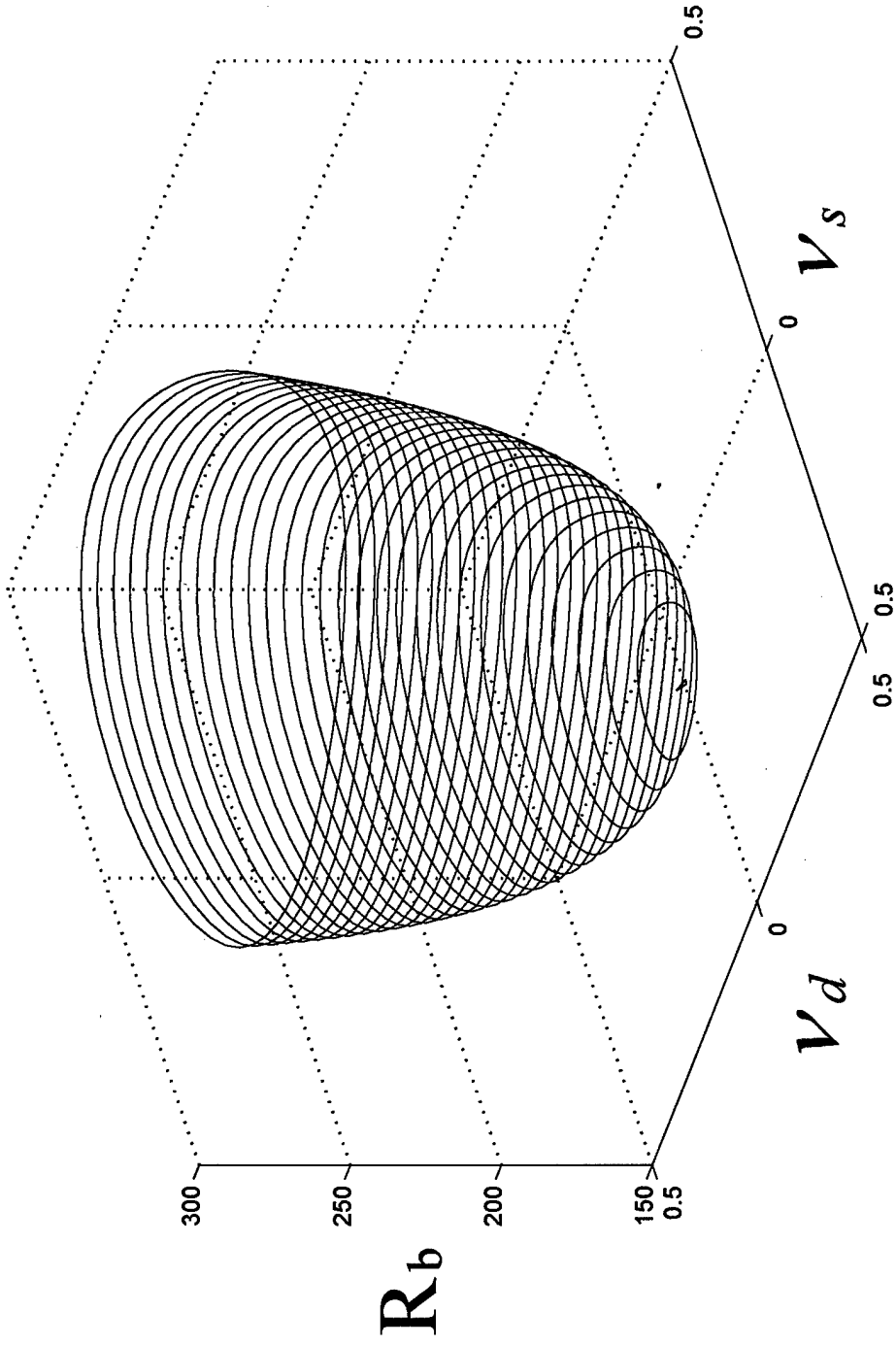


**PROBLEM: DD CURVES ARE RANGE-DEPENDENT!
(EXCEPT FOR MONOSTATIC-SIDELOOKING CASE)**






USEFUL CONCEPT: DD SURFACE



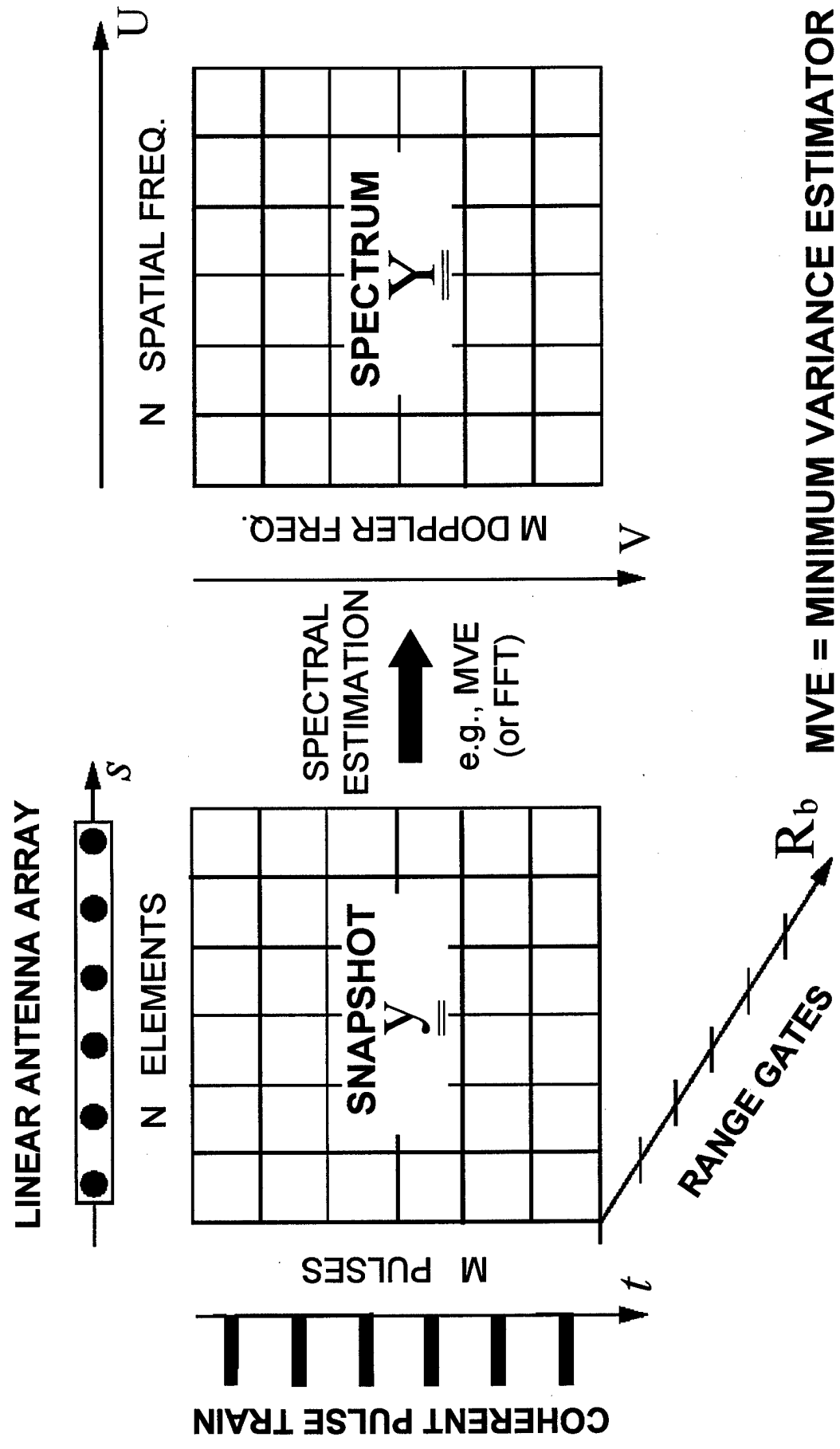


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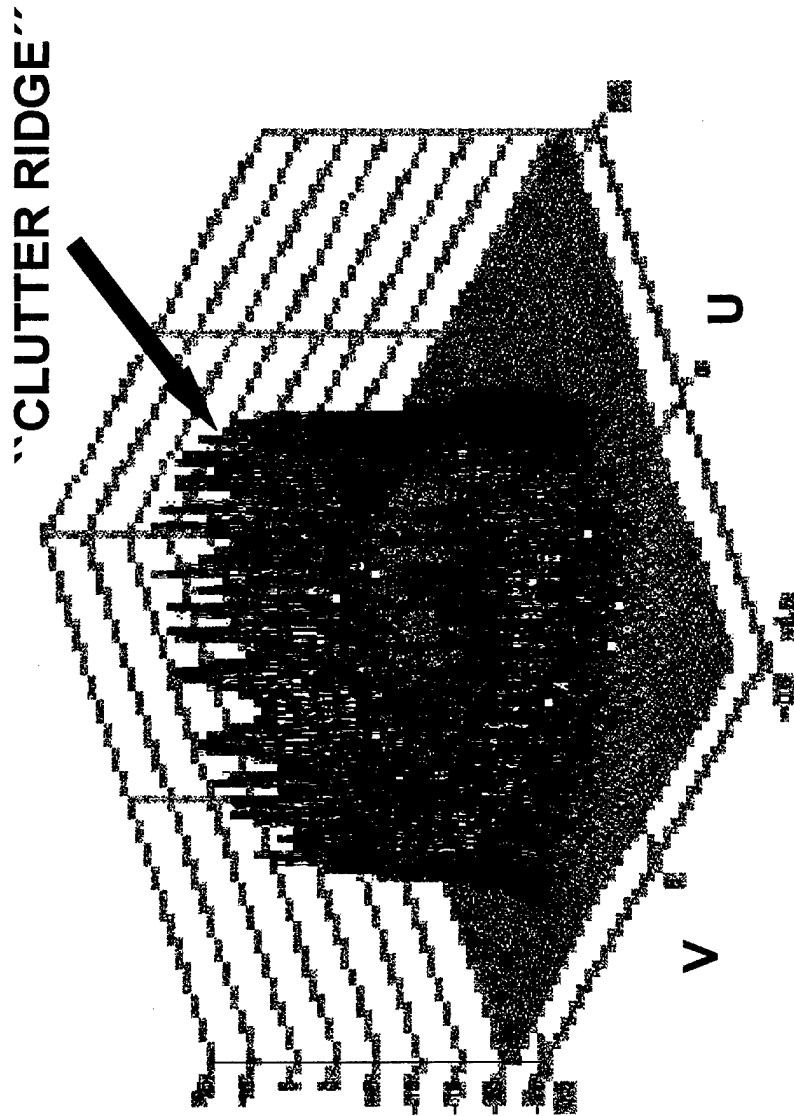
RADAR SNAPSHOT AND POWER SPECTRUM



MVE = MINIMUM VARIANCE ESTIMATOR



EXAMPLE POWER SPECTRUM: CLUTTER ONLY

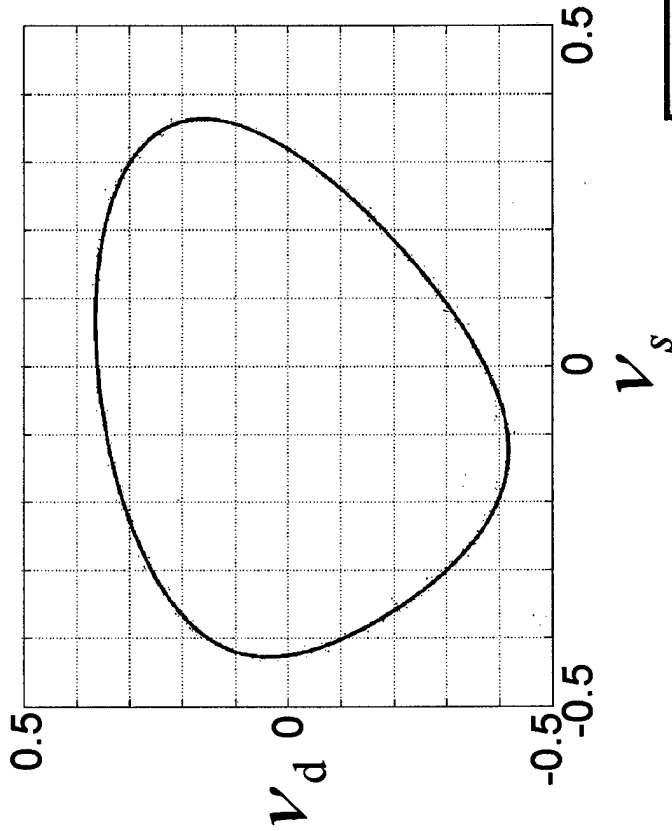


DOES THIS GRAPH TRIGGER ANY THOUGHT ?

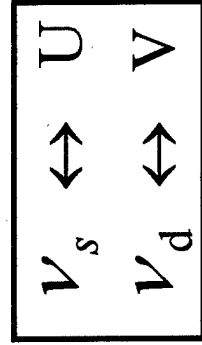
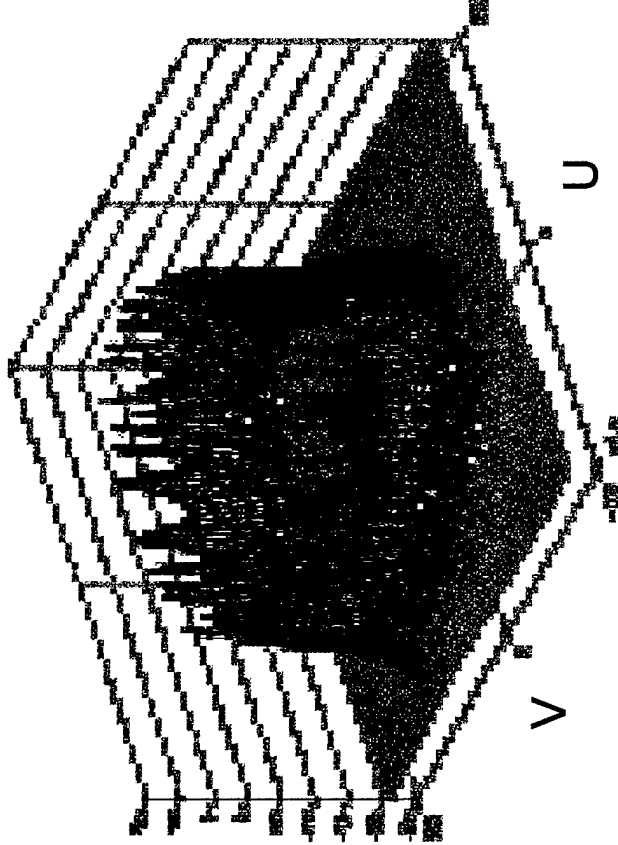


THE KEY LINK BETWEEN THEORY AND MEASUREMENT

DD CURVE
(THEORETICAL !)



CLUTTER RIDGE
(MEASURED!)





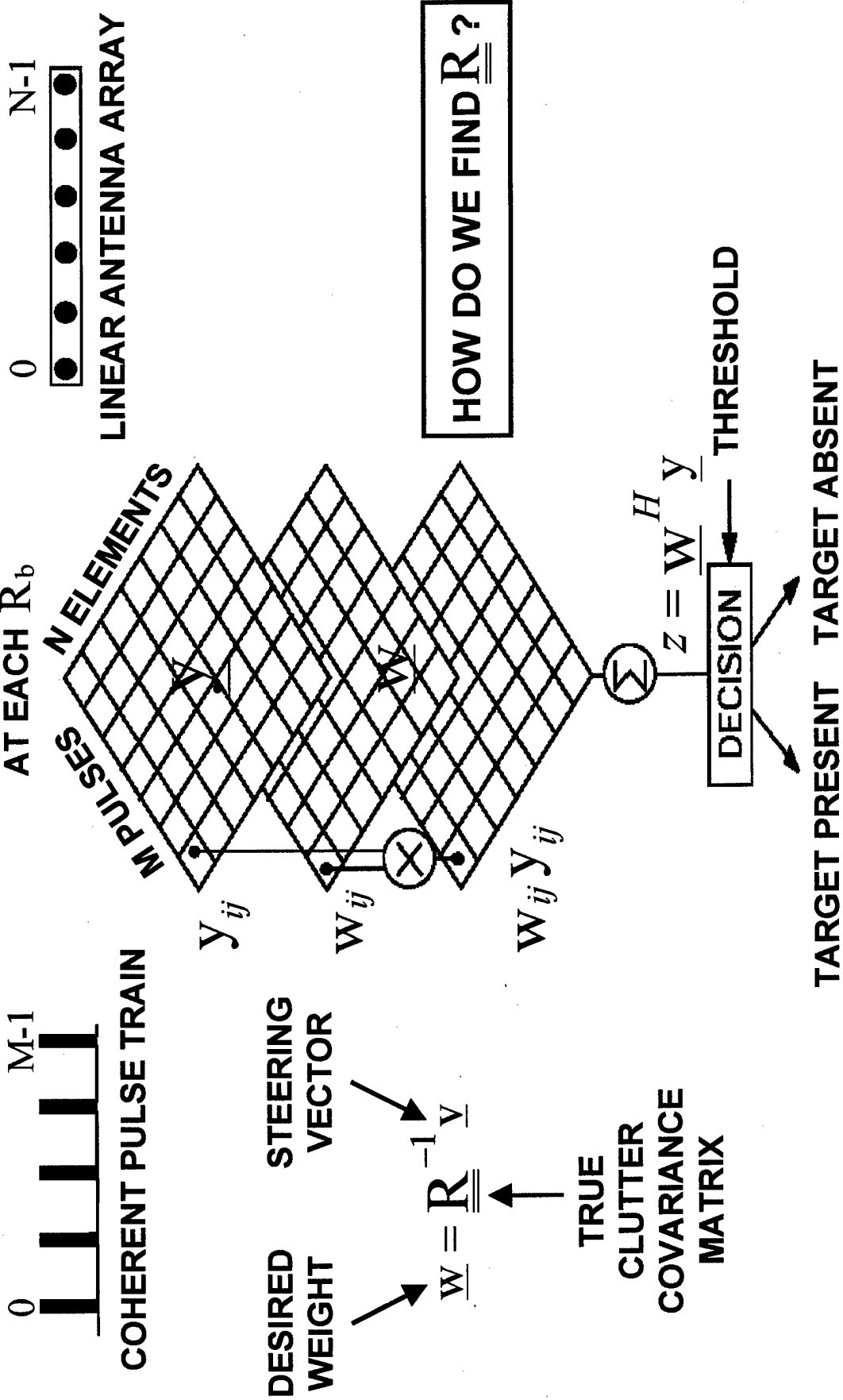
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THE OPTIMUM STAP PROCESSOR





WHAT VALUE DO WE USE FOR $\underline{\underline{R}}$ IN

$$\underline{\underline{w}} = \underline{\underline{R}}^{-1} \underline{\underline{v}} \text{ ?}$$

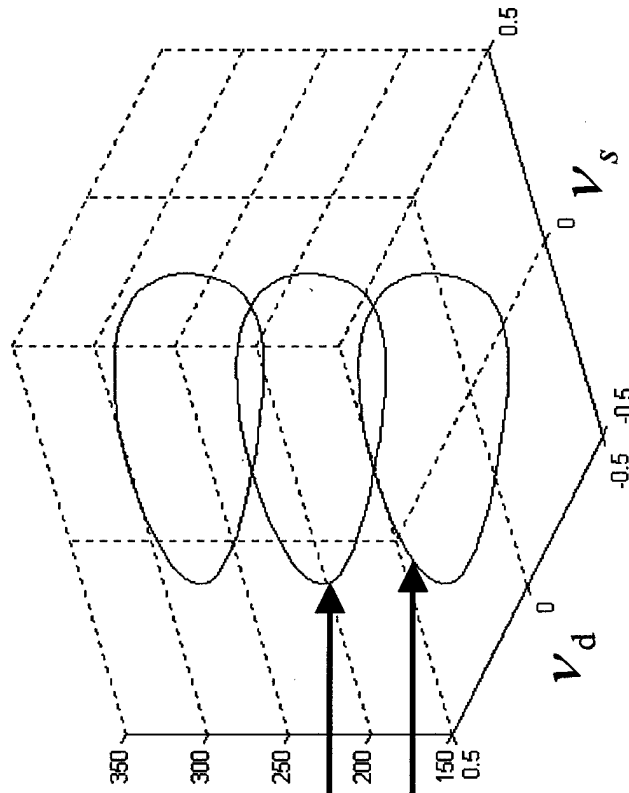
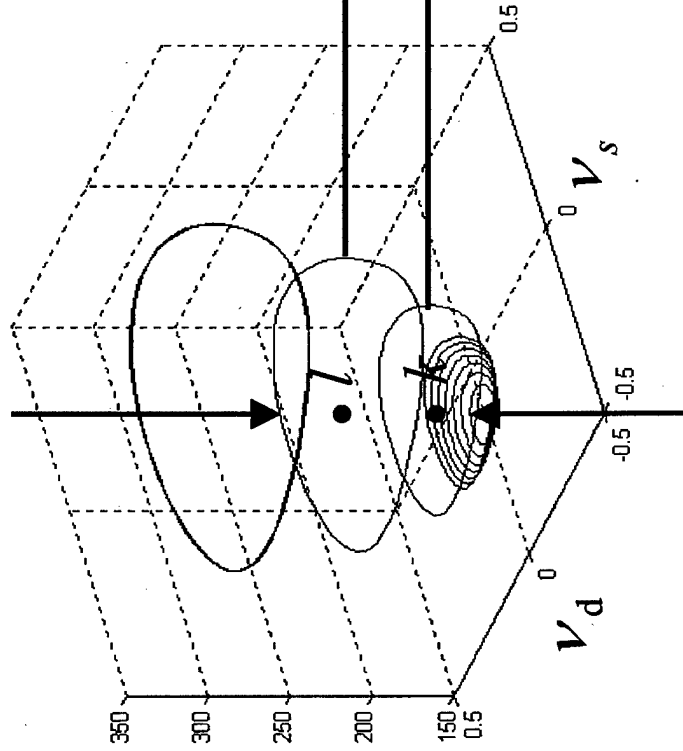
<p>COVARIANCE MATRIX $\underline{\underline{R}}(l)$</p>	<p>THEORETICAL & BEST</p>	<p>PRACTICAL & WORST</p>
<p>TRUE ESTIMATE</p> $\underline{\underline{R}}(l) = E\{ \underline{\underline{y}}_k \underline{\underline{y}}_k^H \}$	<p>BIASED ESTIMATE</p> $\hat{\underline{\underline{R}}}(l) = \frac{1}{N_l} \sum_{k \in S_l} \underline{\underline{R}}(k)$ $\underline{\underline{R}}(k) = \underline{\underline{y}}_k \underline{\underline{y}}_k^H$	<p>STRAIGHT-AVERAGING PROCESSOR (SA)</p>
<p>PROCESSOR</p>	<p>OPTIMUM PROCESSOR (OP)</p>	<p>STRAIGHT-AVERAGING PROCESSOR (SA)</p>

TO GET UNBIASED ESTIMATE OF $\underline{\underline{R}}(l)$, WE MUST ALIGN CLUTTER RIDGES OF $\underline{\underline{R}}(k)$'s !



THE CRUX OF STAP: ALIGNING CLUTTER RIDGES, i.e., DD CURVES

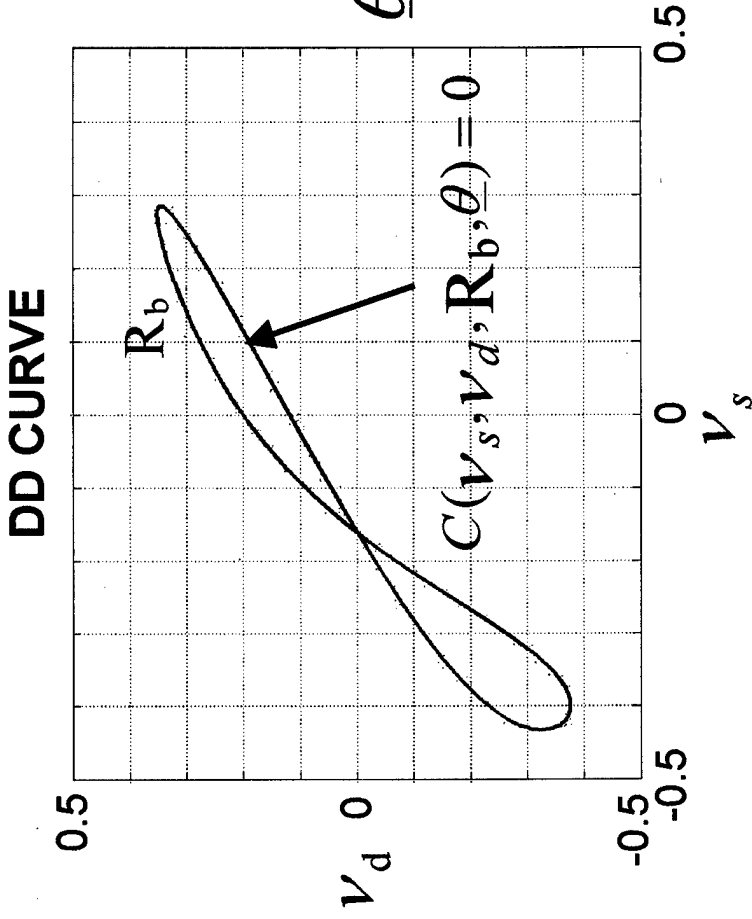
FIXED CURVE AT l (REFERENCE)



MOVING CURVE AT k

HOW DO WE ALIGN DD CURVES ?

AN ABSOLUTE MUST: A MATHEMATICAL THEORY OF DD CURVES



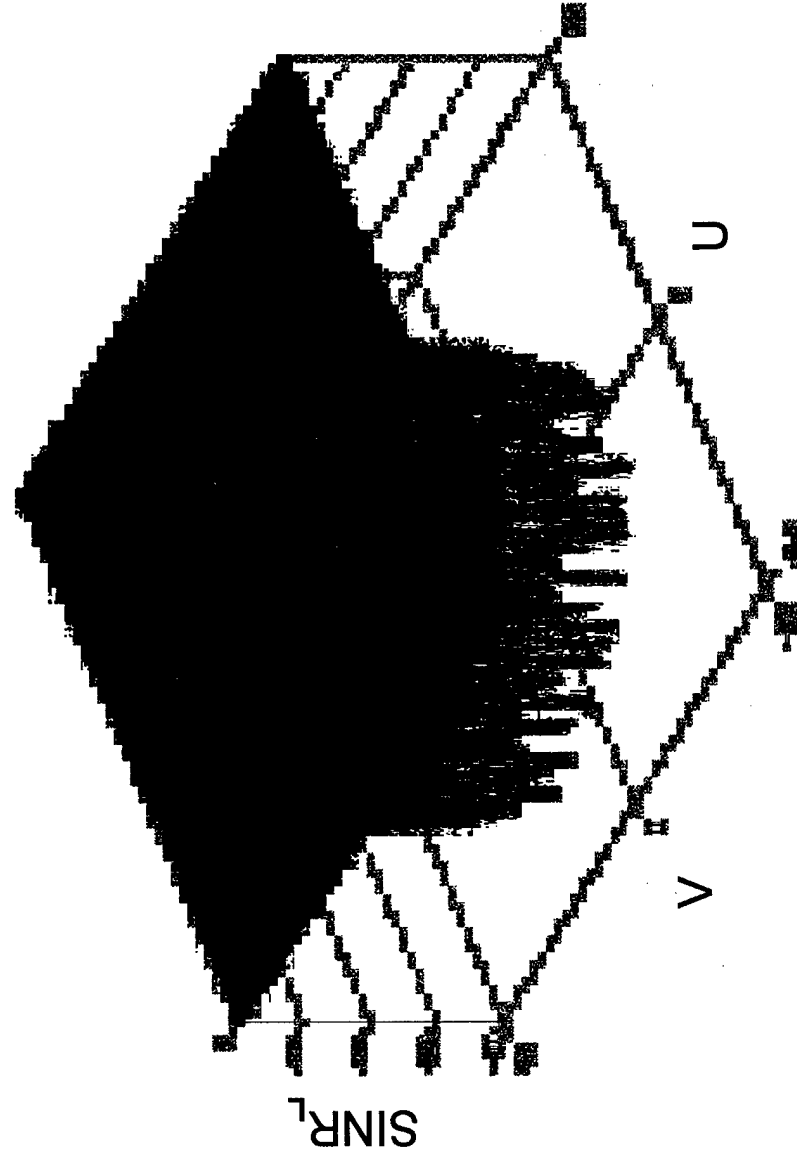
(X_R, Y_R, Z_R) = RECEIVER POSITION
 α_R = RECEIVER VELOCITY ANGLE
 δ = ANTENNA ANGLE
 V_R = RECEIVER VELOCITY
 V_T = TRANSMITTER VELOCITY

$\theta = \{$

**WE HAVE DEVELOPPED FORMULAS FOR ARBITRARY DD CURVES:
ONLY FOR THE MATHEMATICALLY-INCLINED !**

HOW TO QUANTIFY PROCESSOR PERFORMANCE ?

SINR LOSS



$$\begin{aligned} \text{SINR}_L &= \frac{\text{SINR}}{\text{SINR}_0} \\ &= \frac{|\bar{\mathbf{w}}^H \bar{\mathbf{v}}|^2}{(\bar{\mathbf{w}}^H \bar{\mathbf{R}} \bar{\mathbf{w}})(\bar{\mathbf{v}}^H \bar{\mathbf{v}})} \end{aligned}$$

$\bar{\mathbf{v}}(\mathbf{v}_s, \mathbf{v}_d)$

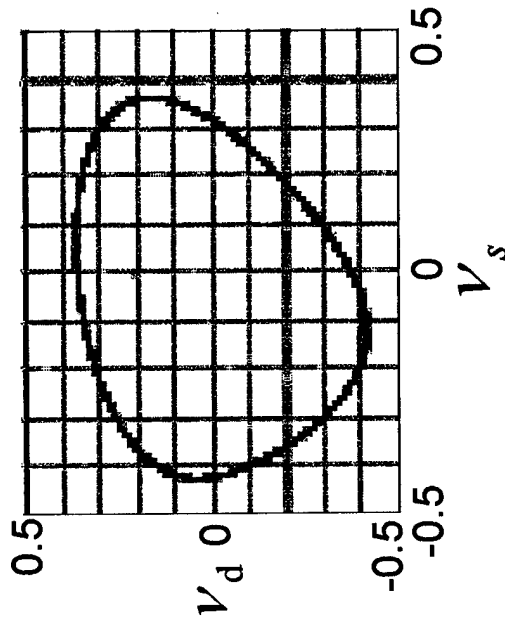


$\text{SINR}_L(\mathbf{v}_s, \mathbf{v}_d)$

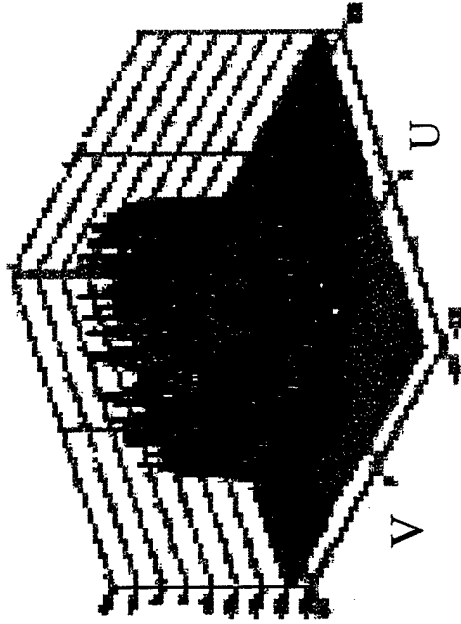


THE LINK BETWEEN THEORY, MEASUREMENT AND PERFORMANCE

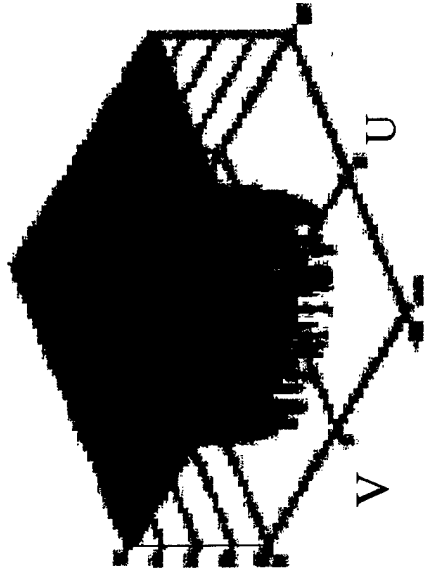
DD CURVE



CLUTTER RIDGE
(POWER SPECTRUM)



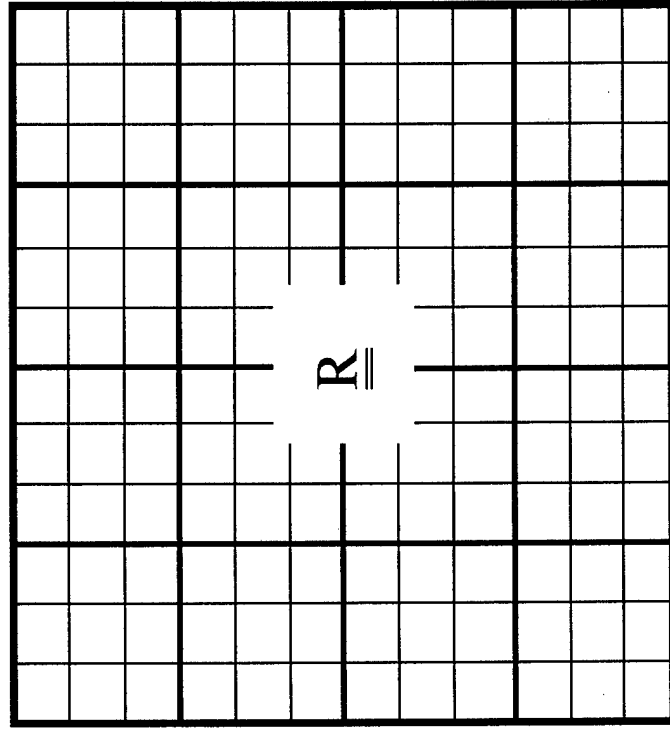
CLUTTER NOTCH
(SINR LOSS)





ASSUMPTION OF STATIONARITY: REDUCTION OF DIMENSIONALITY OF CLUTTER COVARIANCE MATRIX

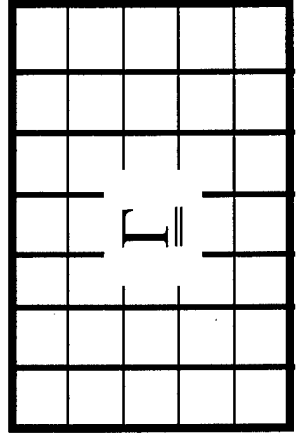
N
ELEMENTS



M PULSES

STATIONARITY
↑


2M - 1



2N - 1

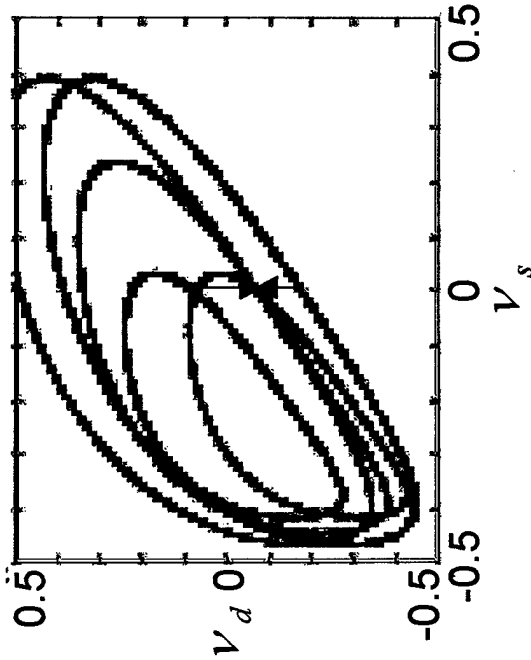


OUTLINE

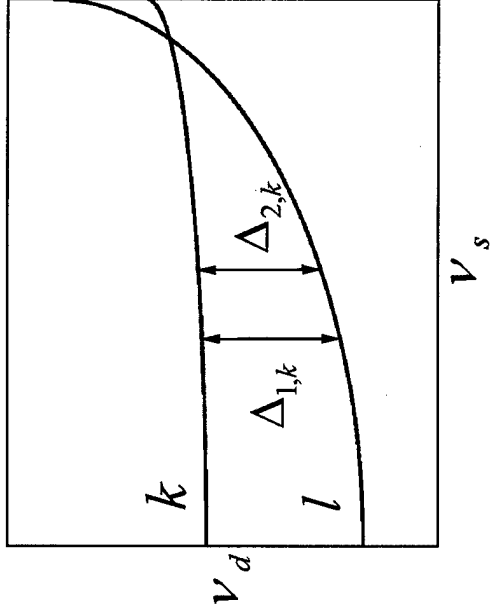
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EXISTING RANGE-COMPENSATION METHODS: (1) PRINCIPLE

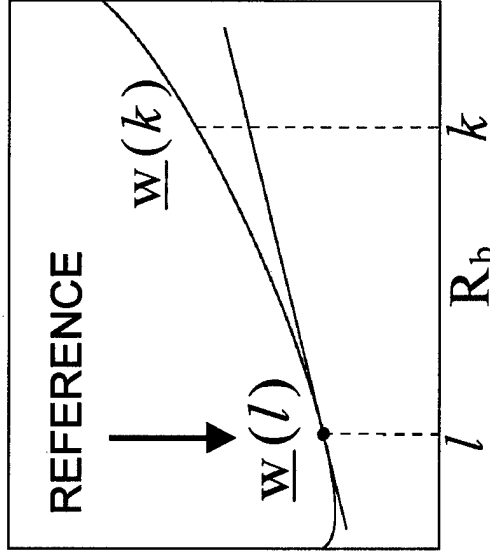
**DOPPLER WARPING
(DW)**



**HIGH-ORDER DOPPLER
WARPING (HODW)**



**DERIVATIVE-BASED
UPDATING (DBU)**



**WEIGHT CONSISTS IN A RANGE-DEPENDENT
DOPPLER SHIFT**

INDEPENDENT OF v_s | | | DEPENDENT ON v_s

**WEIGHT GIVEN BY
1st-ORDER TAYLOR SERIES**

$$\underline{w}(k) = \underline{w}(l) + (k - l) \dot{\underline{w}}(l)$$

Borsari, IEEE Radar Conf. (1998)

Pearson & Borsari, ASAP (2001)

Haynard (1996), Zatman & Kogon (2000), Zatman(2001)

University of Liège


EXISTING RANGE-COMPENSATION METHODS: (2) COMPARISON

	DW	HODW	DBU
+	<ul style="list-style-type: none"> • SIMPLE IMPLEMENTATION 	<ul style="list-style-type: none"> • NEARLY-PERFECT COMPENSATION 	<ul style="list-style-type: none"> • PARAMETERS NOT REQUIRED
-	<ul style="list-style-type: none"> • POOR PERFORMANCE FOR BS CONFIGURATION • PARAMETERS REQUIRED 	<ul style="list-style-type: none"> • COMPLICATED DOPPLER FILTERING • PARAMETERS REQUIRED 	<ul style="list-style-type: none"> • GOOD PERFORMANCE FOR SOME BS CONFIGURATIONS • TWICE AS MANY DOF REQUIRED

**OUR GOAL : GENERAL BS CONFIGURATIONS, UNKNOWN PARAMETERS,
LOW COMPLEXITY WITHOUT ANY INCREASE IN NUMBER OF DOF**

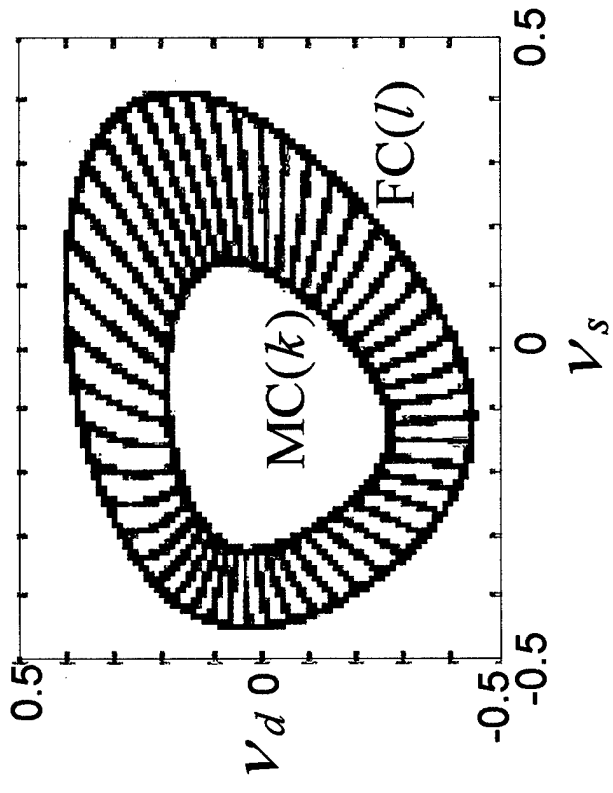
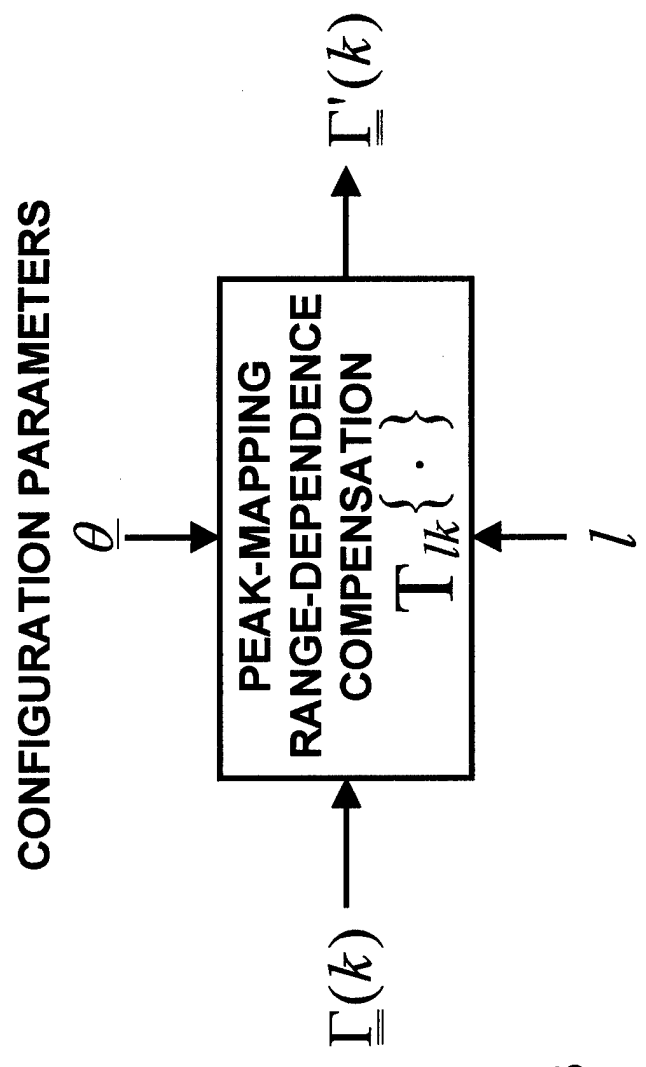


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PEAK-MAPPING RANGE-DEPENDENCE COMPENSATION: (1) Principle



$MC(k)$ = MOVING CURVE AT RANGE GATE k

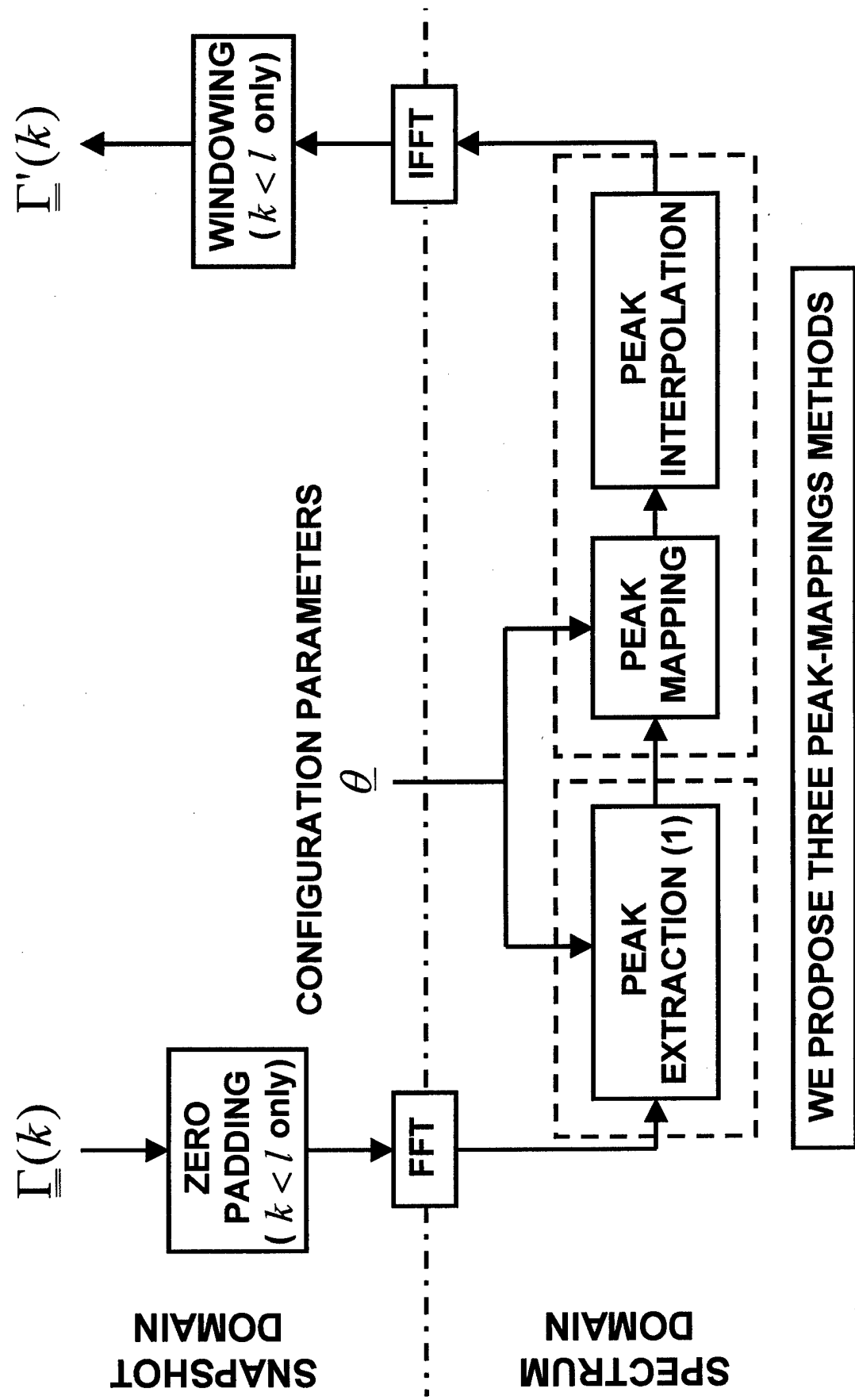
$FC(l)$ = FIXED CURVE AT REFERENCE RANGE GATE l

$$\hat{\Gamma}(l) = \frac{1}{N_l} \sum_{k \in S_l} T_{lk}^{\Gamma} \{ \Gamma(k) \}$$

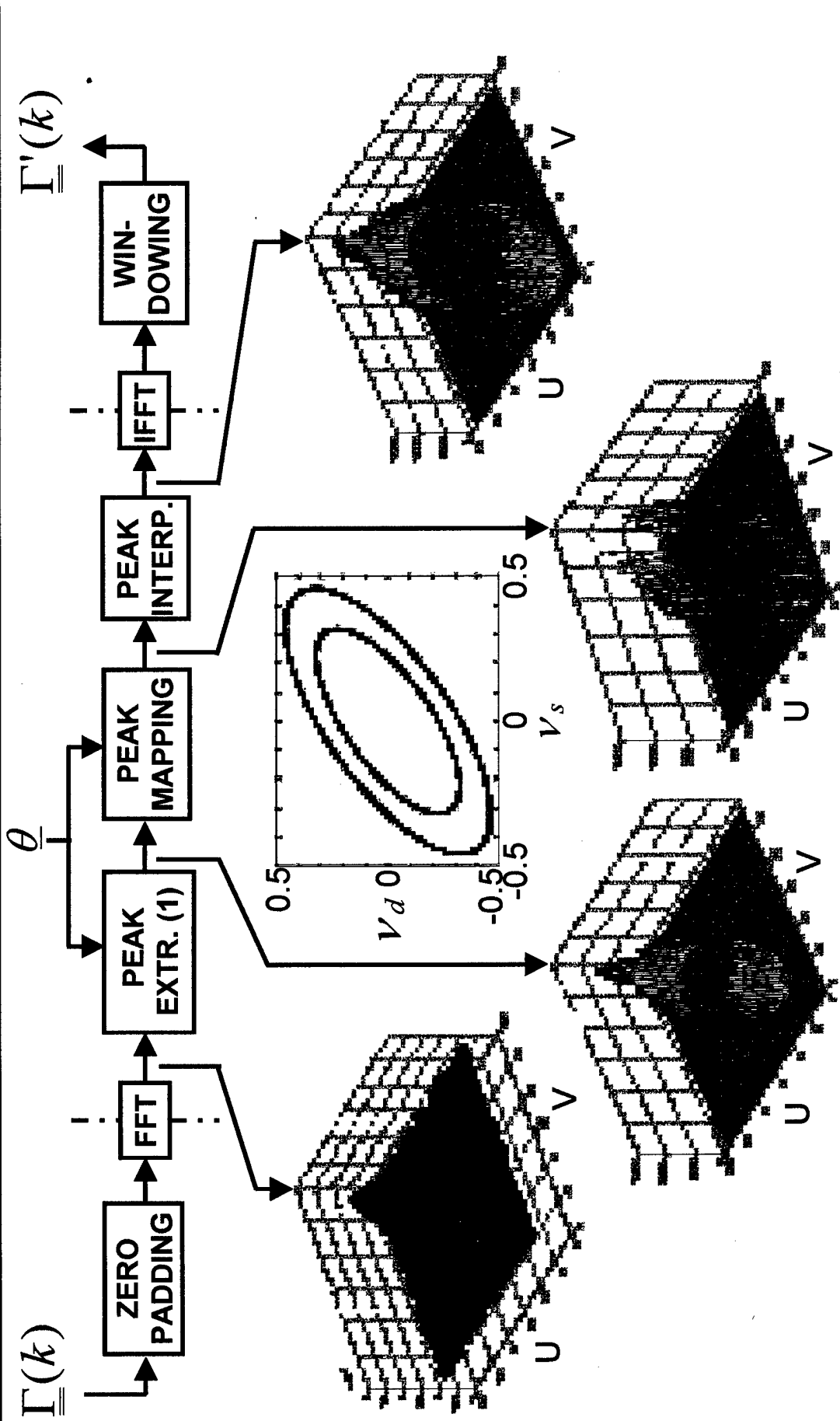
HOW DO WE FIND T_{lk}^{Γ} FOR ALL k AND l ?



PEAK-MAPPING RANGE-DEPENDENCE COMPENSATION: (2) System

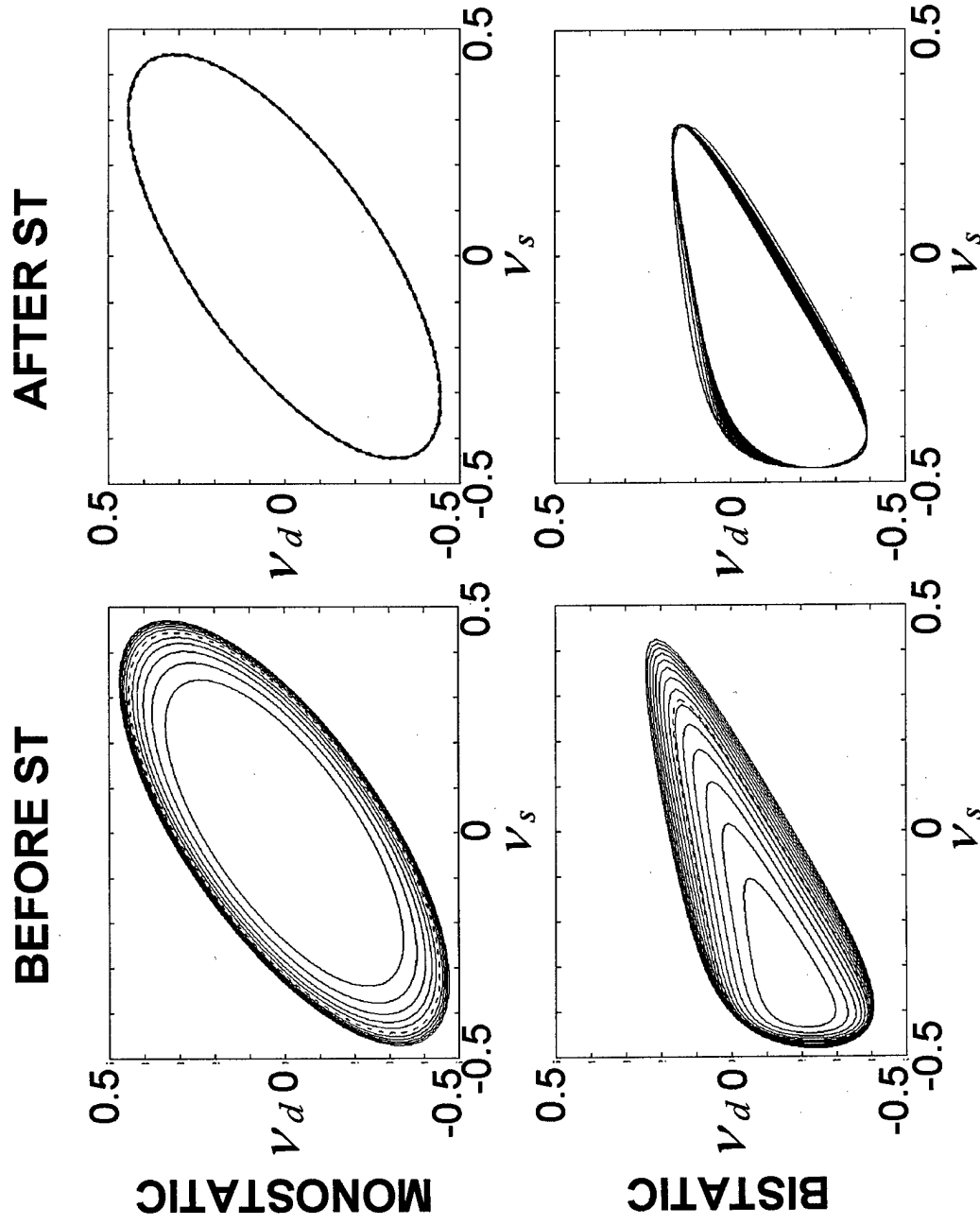


PEAK-MAPPING BY SCALING TRANSFORMATION (ST): (1) PRINCIPLE





PEAK-MAPPING BY SCALING TRANSFORMATION (ST): (2) PERFORMANCE



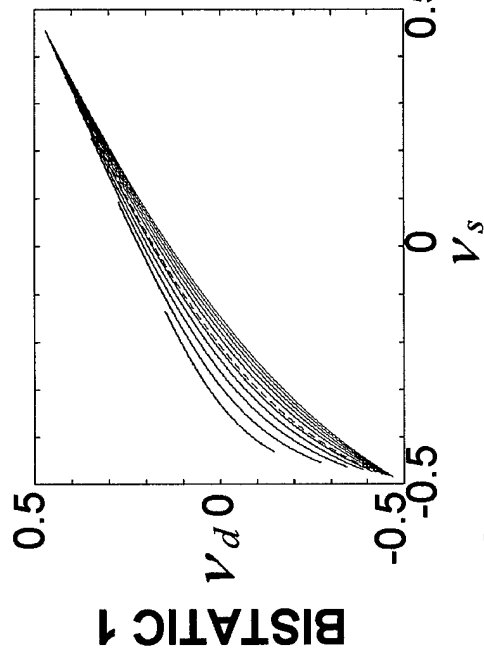
WORKS ONLY FOR
MONOSTATIC
CONFIGURATIONS

HOW DO WE
EXTEND
RANGE OF
APPLICABILITY ?

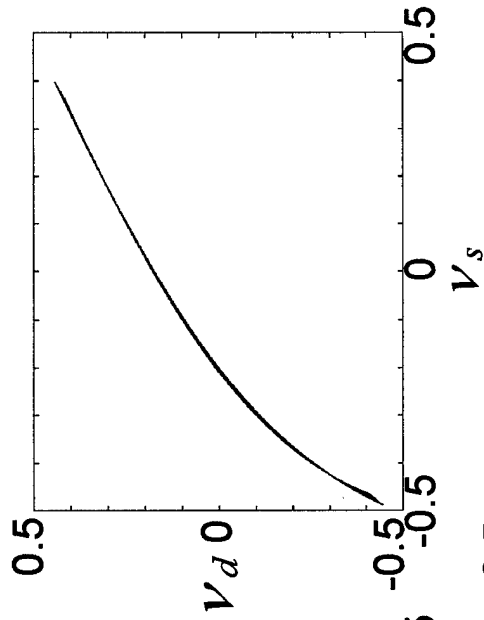


PEAK-MAPPING BY AFFINE TRANSFORMATION (AT): PRINCIPLE

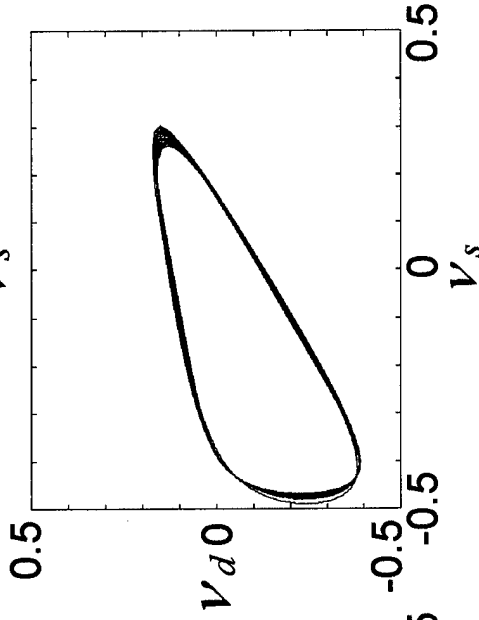
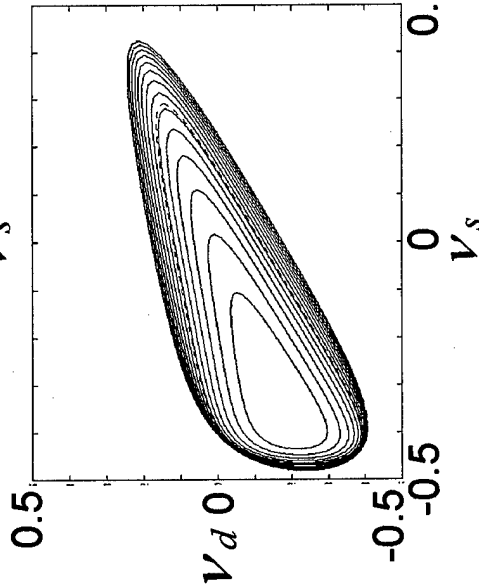
BEFORE AT



AFTER AT



BISTATIC 2



WORKS ONLY FOR
MONOSTATIC AND
SOME BISTATIC
CONFIGURATIONS

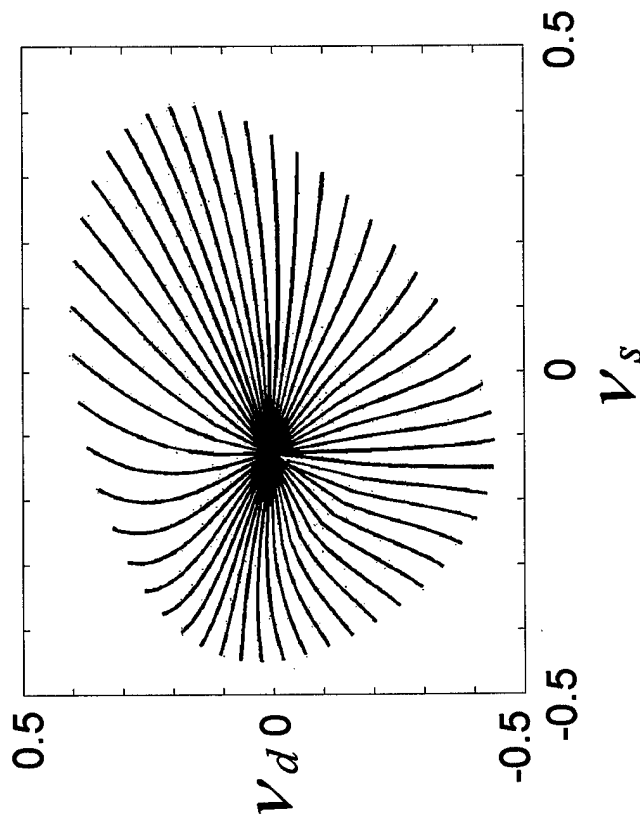


HOW DO WE
EXTEND
RANGE OF
APPLICABILITY ?

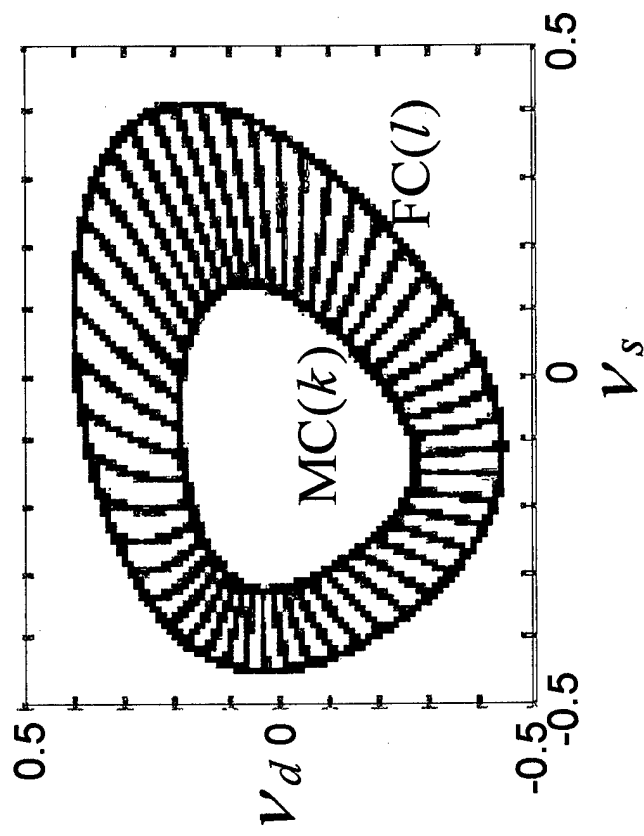


PEAK-MAPPING BY WARPING TRANSFORMATION (WT): (1) PRINCIPLE

EXAMPLE FLOW LINES

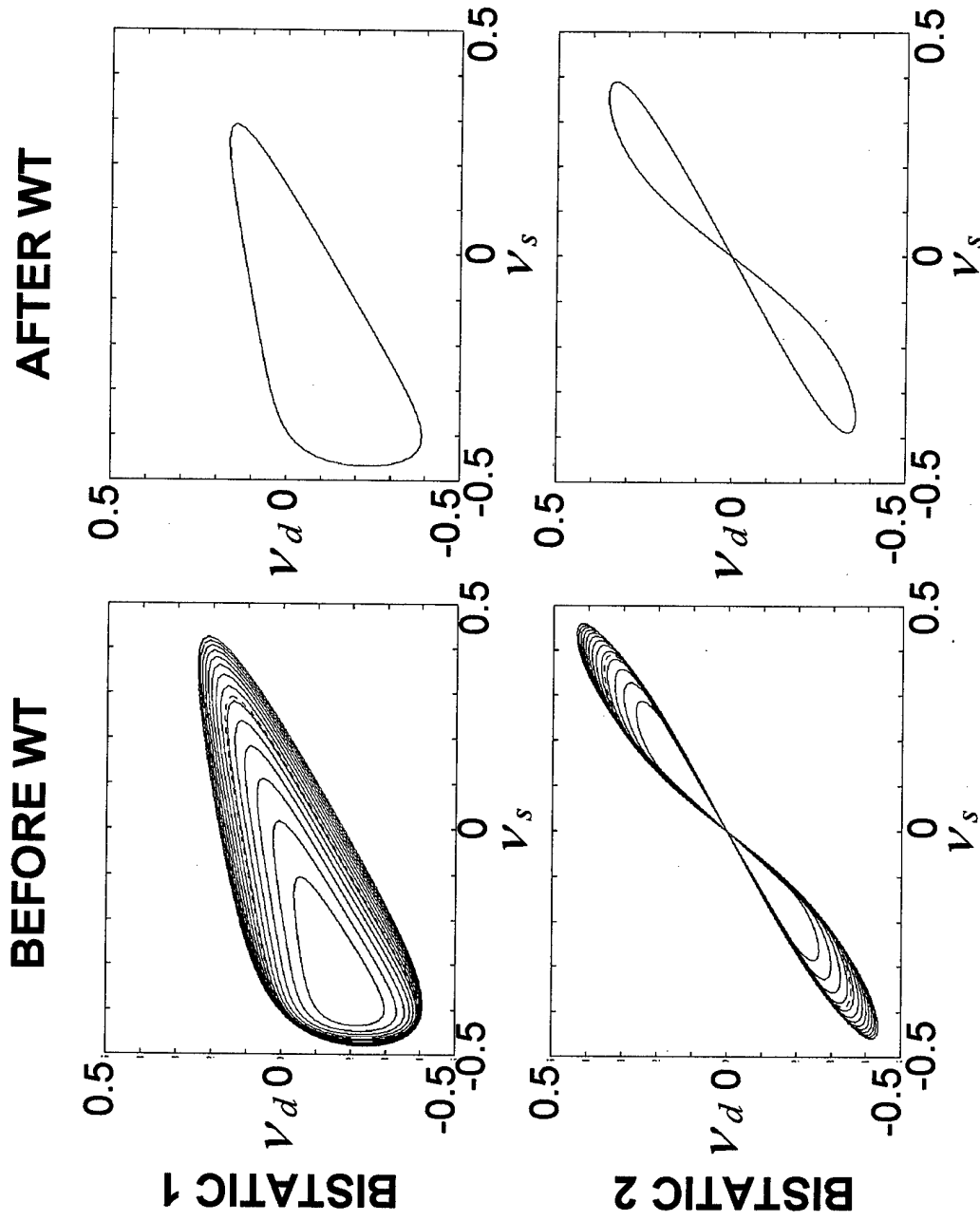


WARPING TRANSFORMATION



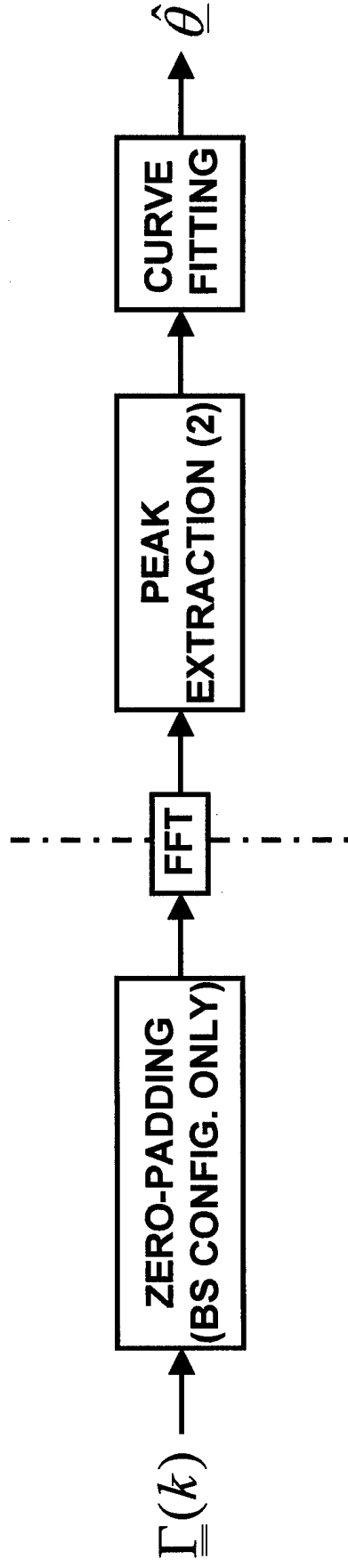


PEAK-MAPPING BY WARPING TRANSFORMATION (WT): (2) PERFORMANCE





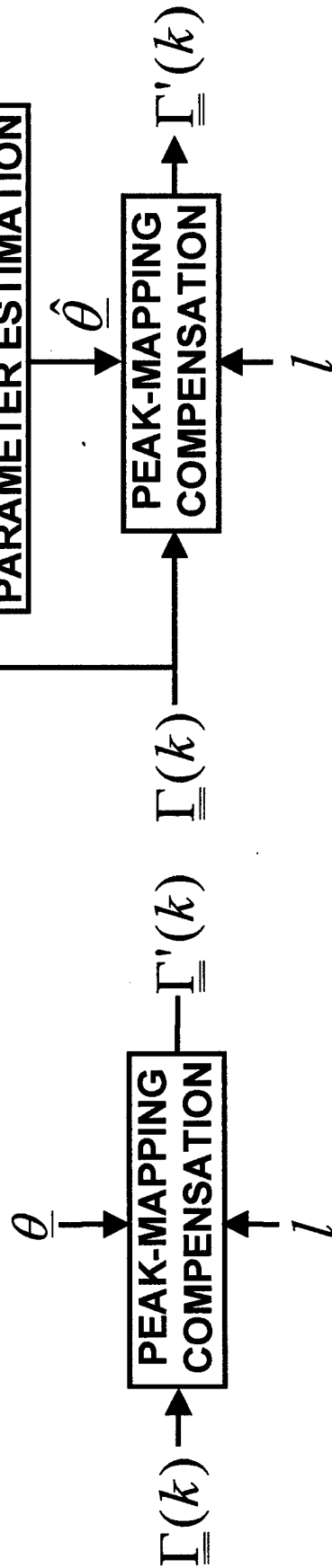
HOW DO WE FIND THE CONFIGURATION PARAMETERS ?



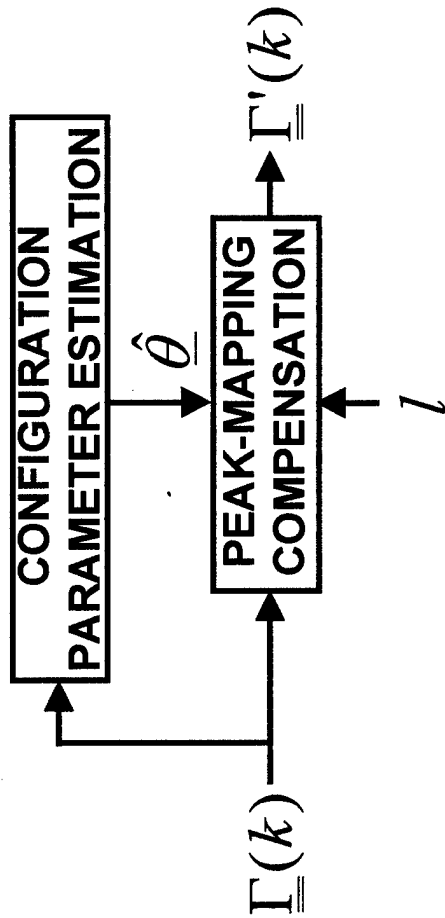
CONFIGURATION	PEAK EXTRACTION (2)	CURVE FITTING
MS	THRESHOLDING	SIMPLE MMSE
BS	WATERSHED SEGM. (Image processing)	DIFFICULT MMSE (Theory of DD curves)

RANGE COMPENSATION METHODS COME IN TWO TYPES AND SIX FLAVORS!

OPEN-LOOP (OL)



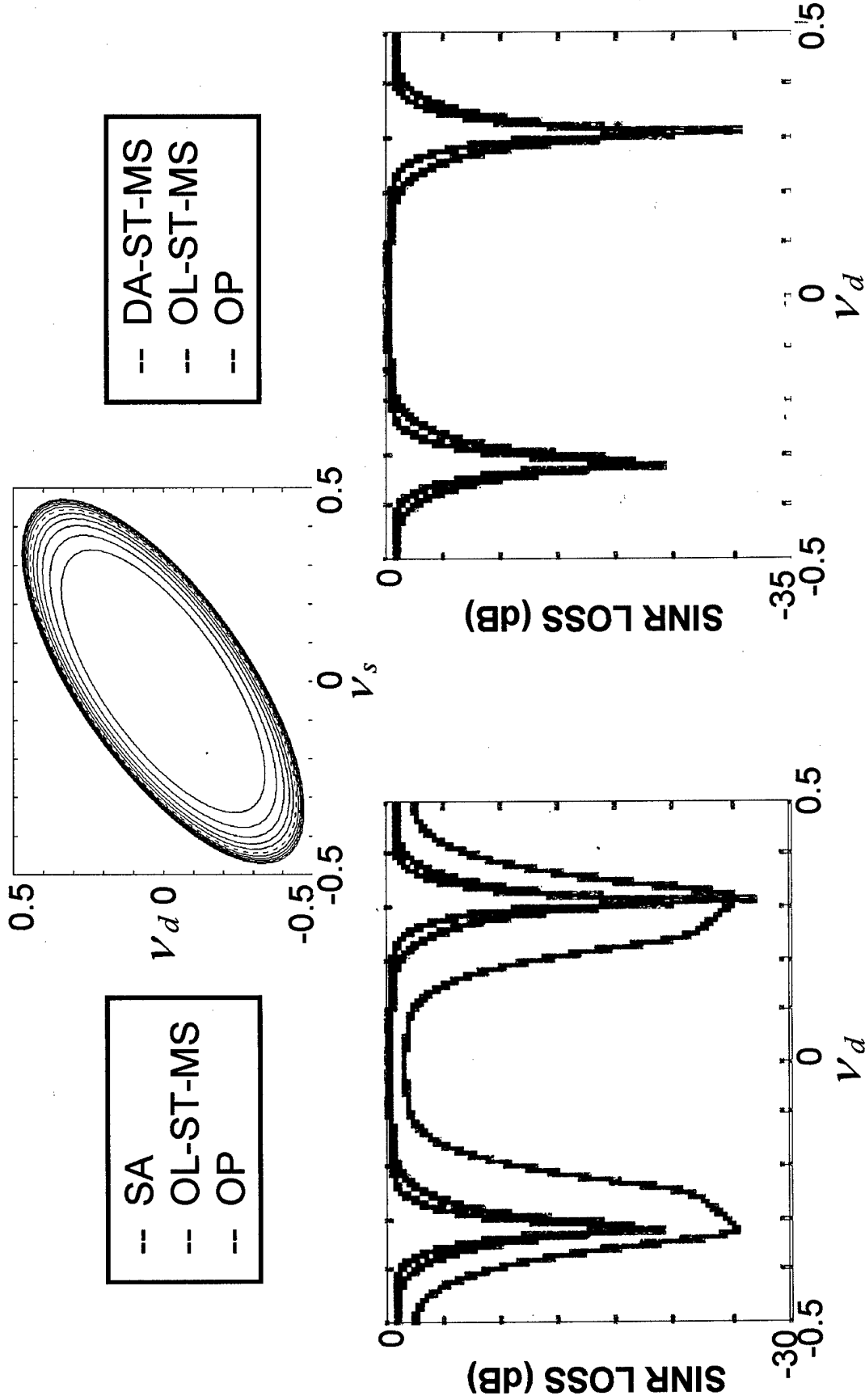
DATA-ADAPTIVE (DA)



PEAK-MAPPING COMPENSATION	OPEN-LOOP (OL)	DATA-ADAPTIVE (DA)
SCALING TRANSFORMATION (MS)	OL-ST-MS	DA-ST-MS
AFFINE TRANSFORMATION (BS)	OL-AT-BS	DA-AT-BS
WARPING TRANSFORMATION (BS)	OL-WT-BS	DA-WT-BS

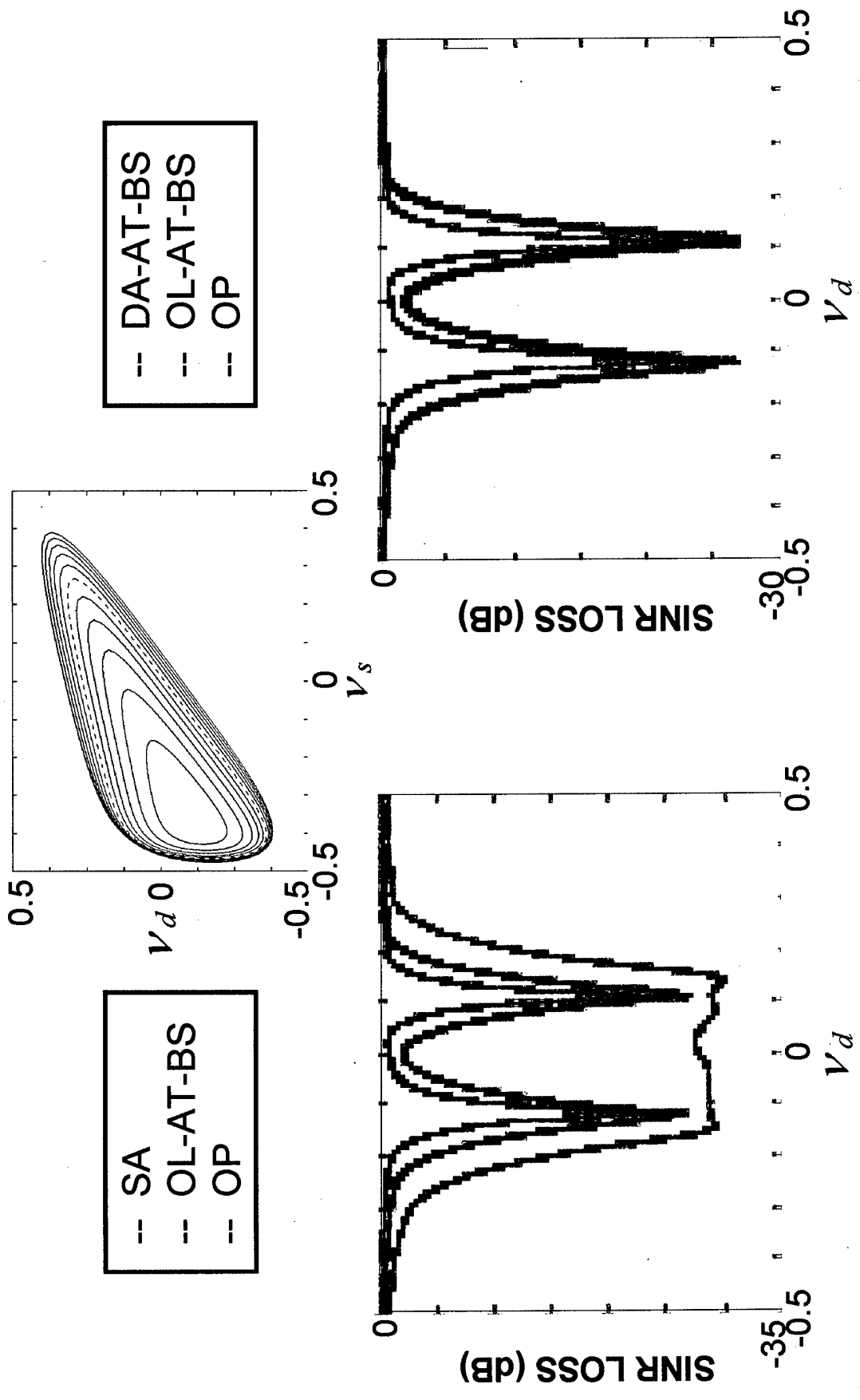


PERFORMANCE COMPARISON: (1) ST-MS



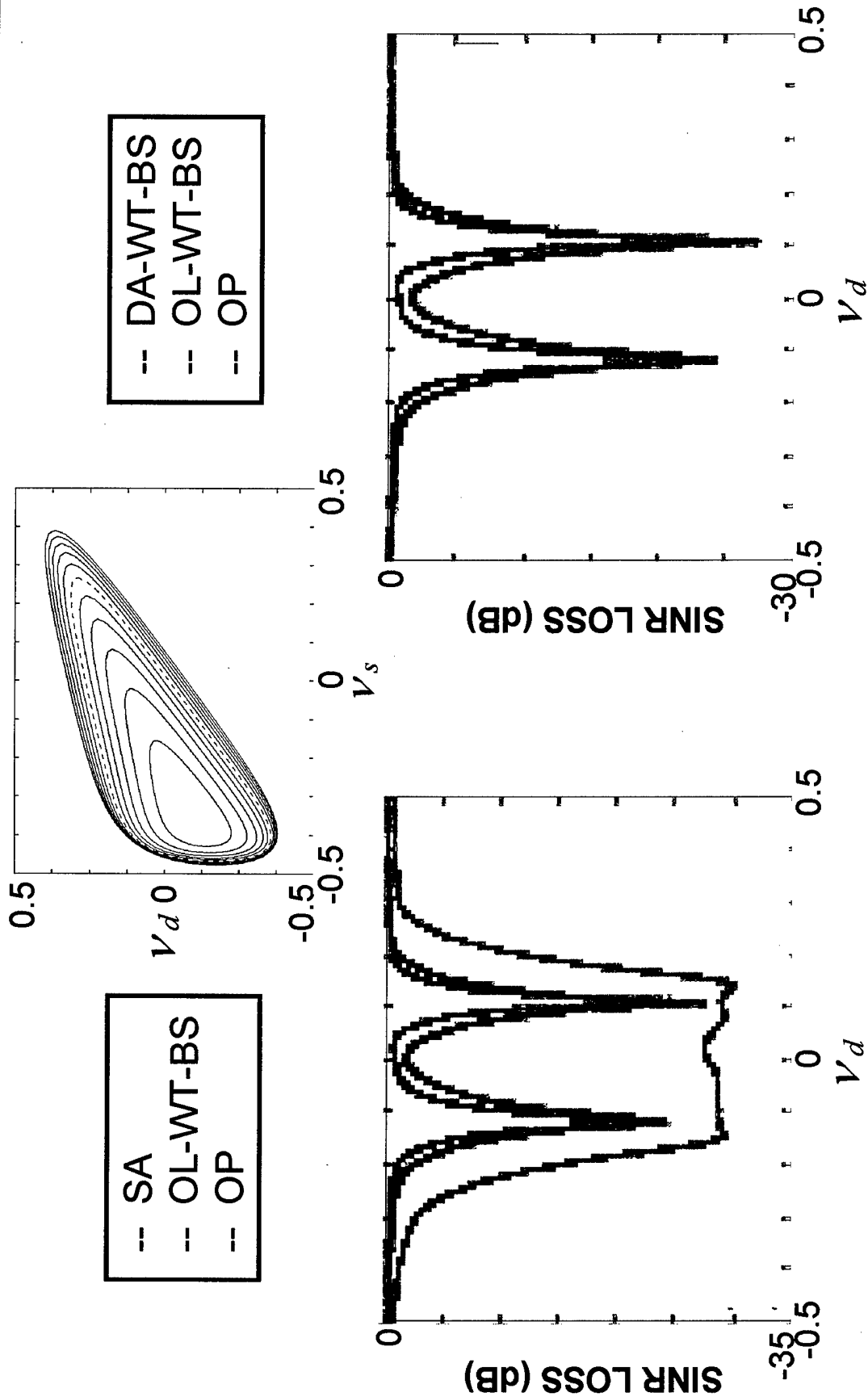


PERFORMANCE COMPARISON: (2) AT-BS



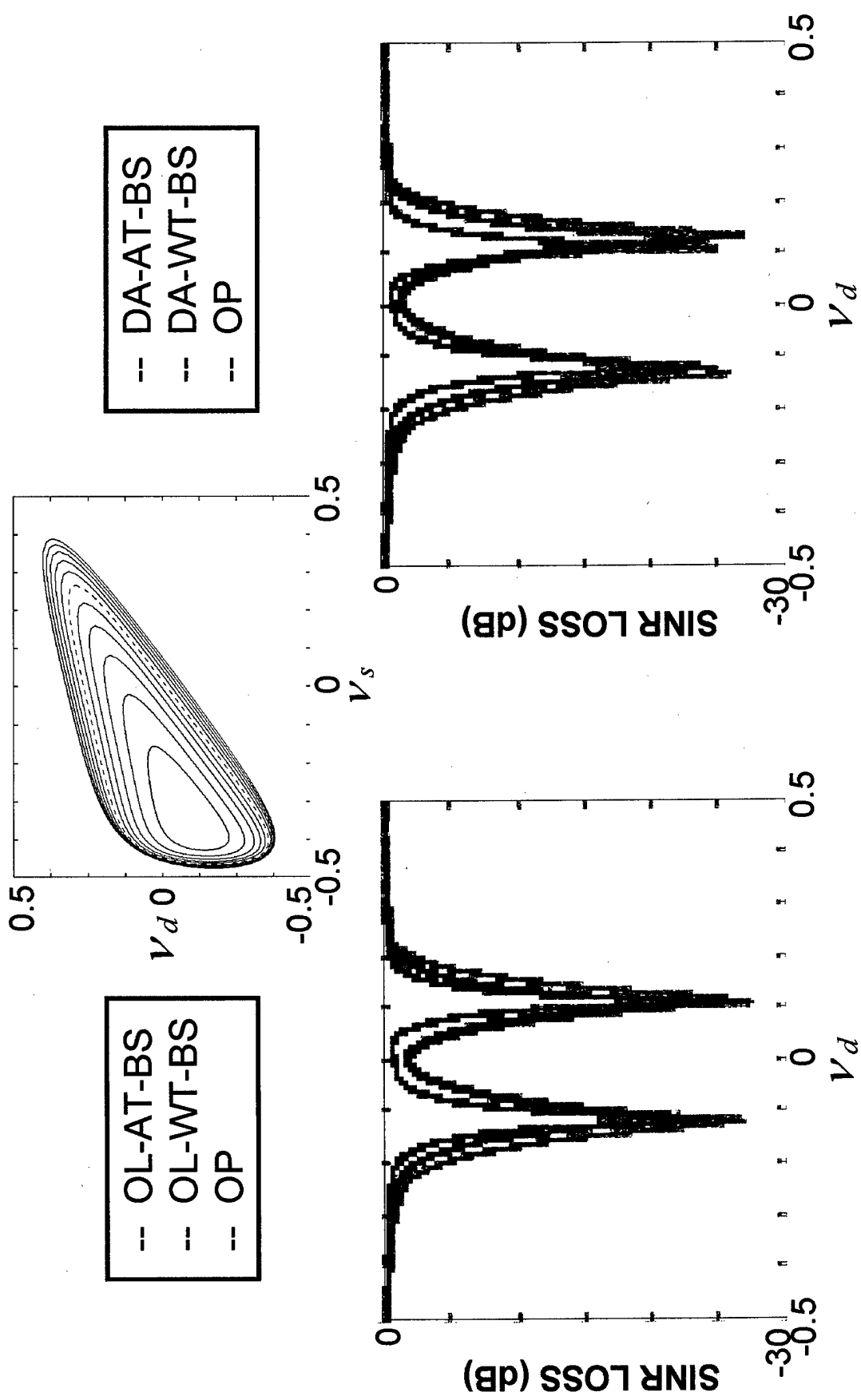


PERFORMANCE COMPARISON: (3) WT-BS



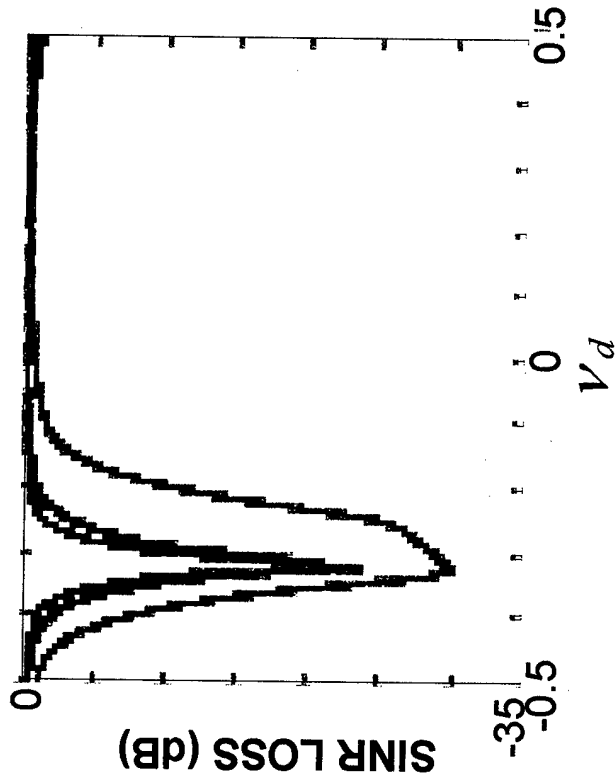
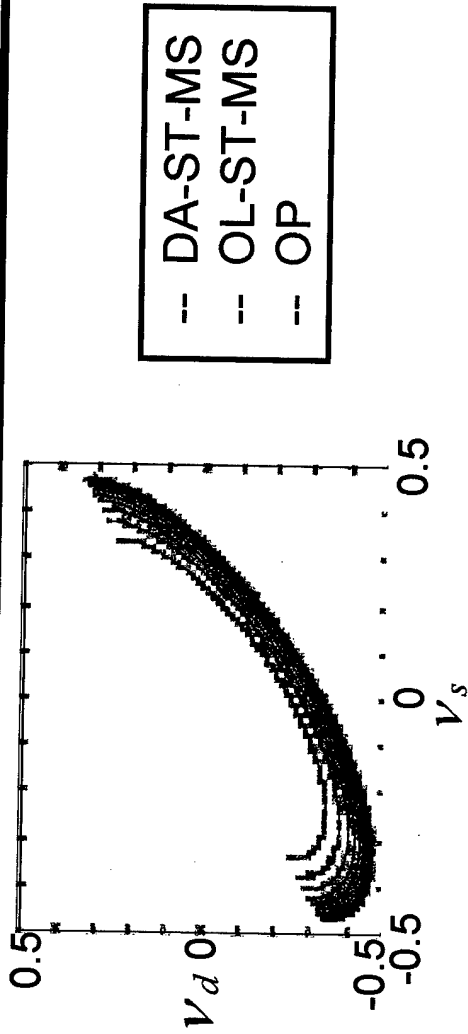


PERFORMANCE COMPARISON: (4) AT vs BT





PERFORMANCE COMPARISON: (5) DIRECTIVE SENSORS, MONOSTATIC



- SAME RESULTS FOR BS CONFIGURATIONS WITH DIRECTIVE SENSORS
- POOR PERFORMANCE FOR BS DA METHODS WITH DIRECTIVE SENSORS



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SUMMARY

- RANGE-DEPENDENCE OF BS CLUTTER SPECTRUM MAKES BS CLUTTER REJECTION A CHALLENGE IN STAP
- WE REVIEWED EXISTING COMPENSATION METHODS
 - DOPPLER WARPING (DW)
 - HIGH-ORDER DOPPLER WARPING (HODW)
 - Configuration parameters required
 - DERIVATIVE-BASED UPDATING (DBU)
 - Doubling of number of DOF

• WE PROPOSED NEW REGISTRATION-BASED COMPENSATION METHODS

- + Nearly perfect compensation for all MS and BS configurations
- + Configuration parameters not required
- + No increase of number of DOF
- High computational load
- Complex implementation
- Robustness