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# Space-Time Adaptive Processing Using Sparse Arrays

**Michael Zatman**

**11<sup>th</sup> Annual ASAP Workshop**

**March 11<sup>th</sup>-14<sup>th</sup> 2003**

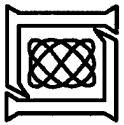
This work was sponsored by the DARPA under Air Force Contract F19628-00-C-0002.  
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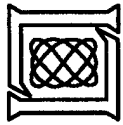


# Application: Space Based Radar

Fast orbital velocity  
(Large aperture ~  
GMTI performance) →

Long range to target  
(Large aperture ~  
location accuracy)

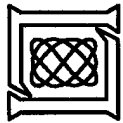
Launch cost  
~low weight  
and size (folded)



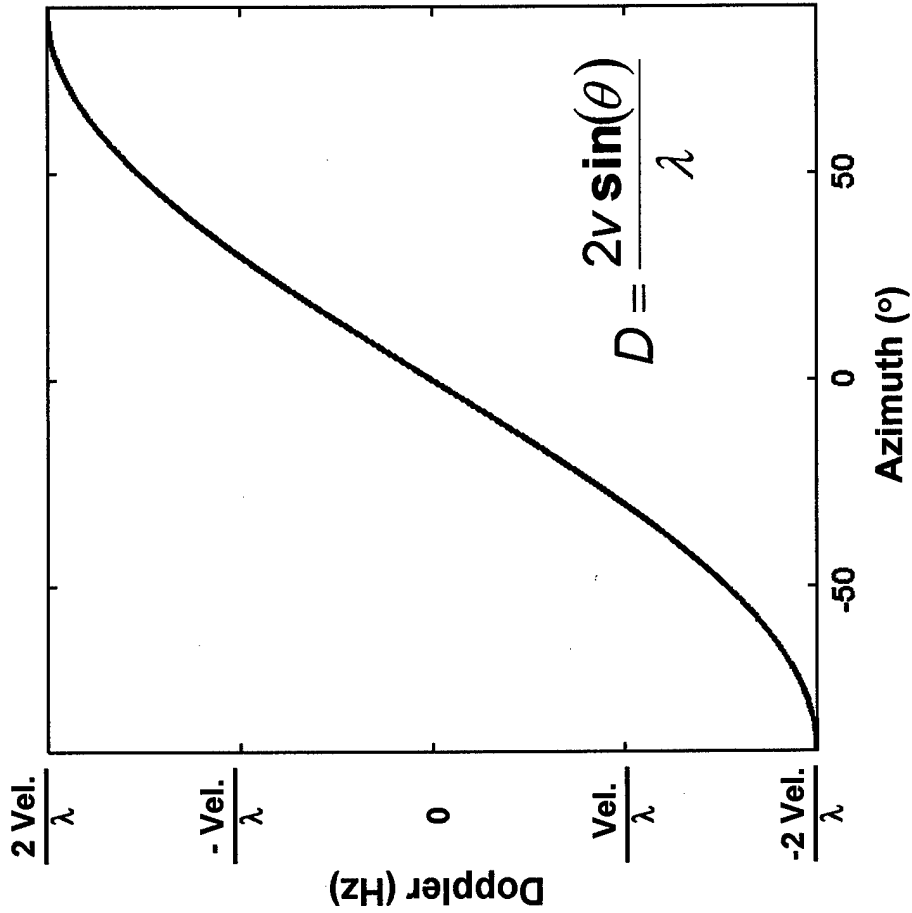
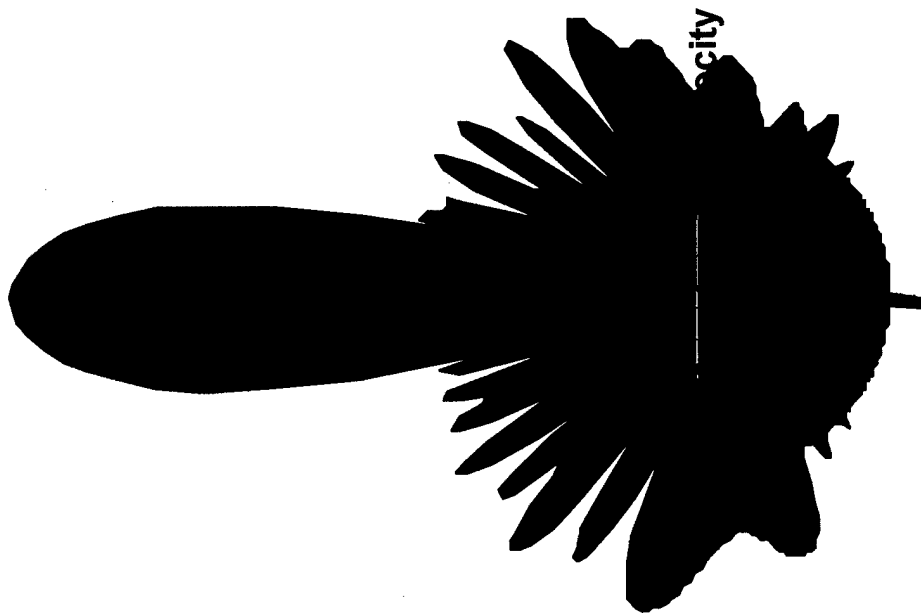
# Outline

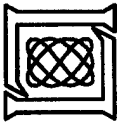
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- **Introduction**
- **Theory**
- **Performance**
- **Summary**

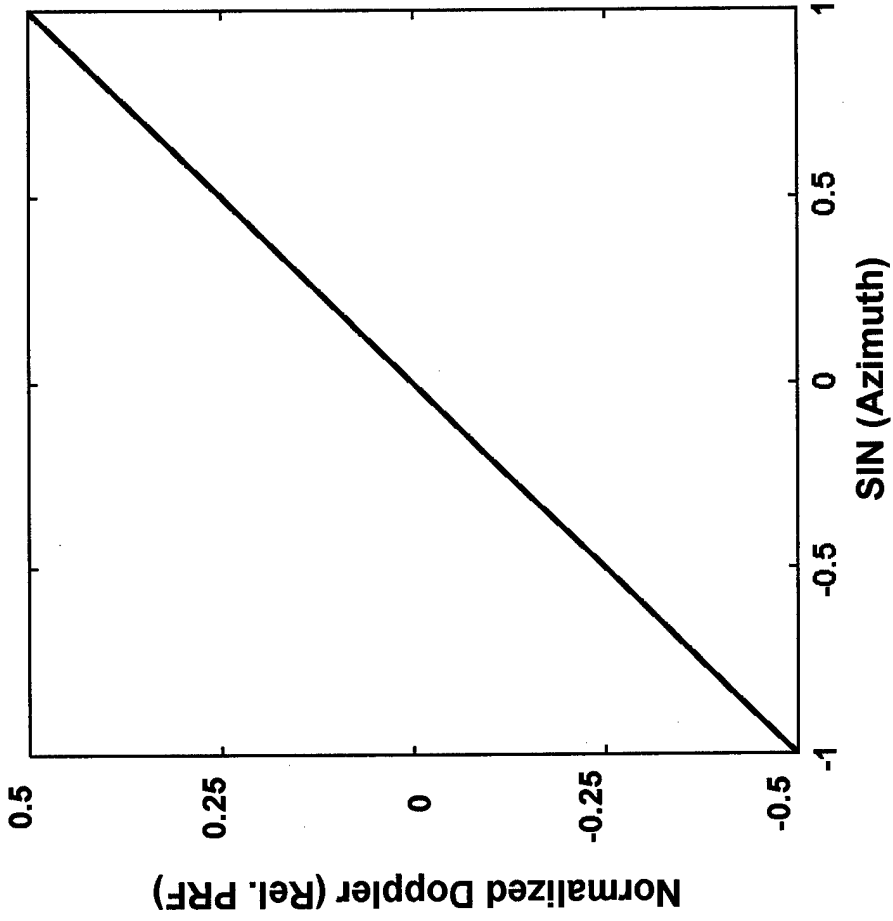
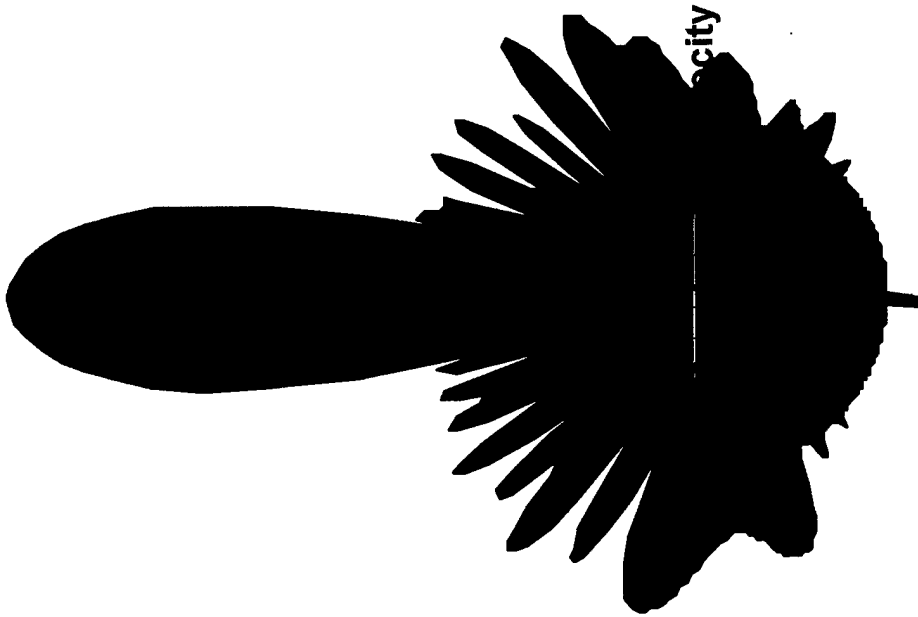


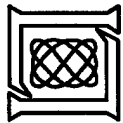
# STAP Units



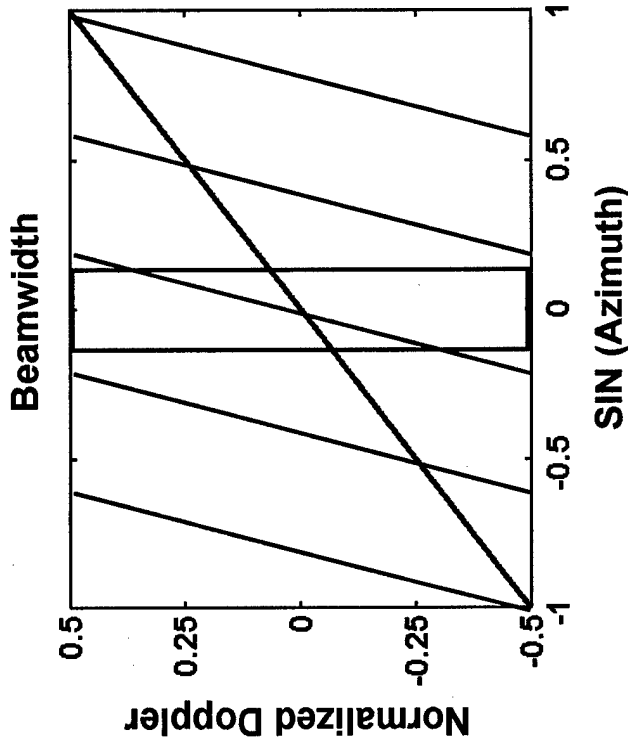
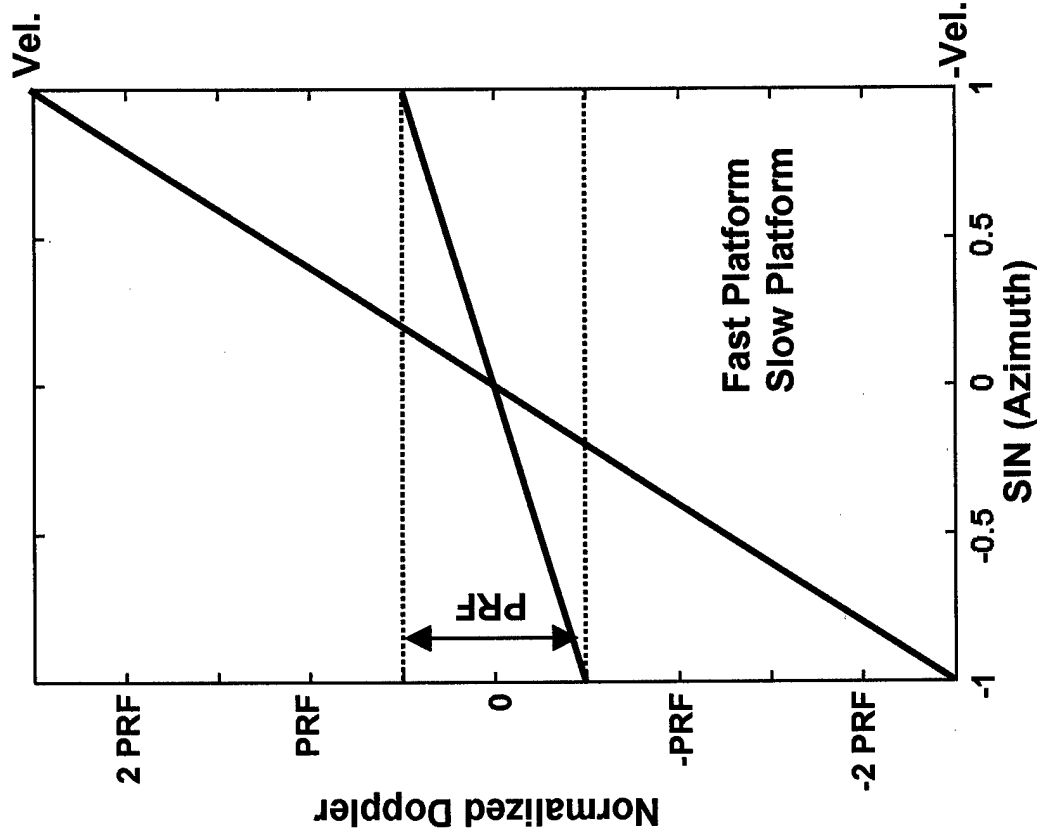


# STAP Units



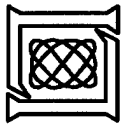


# Doppler Ambiguous Clutter

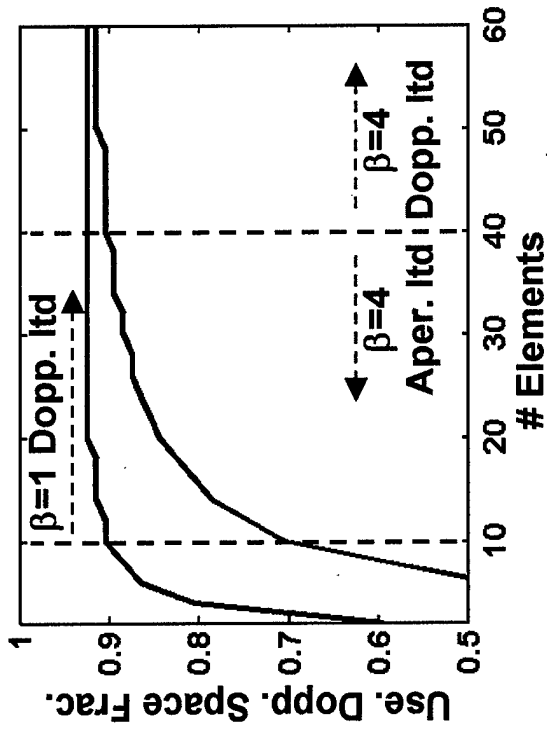
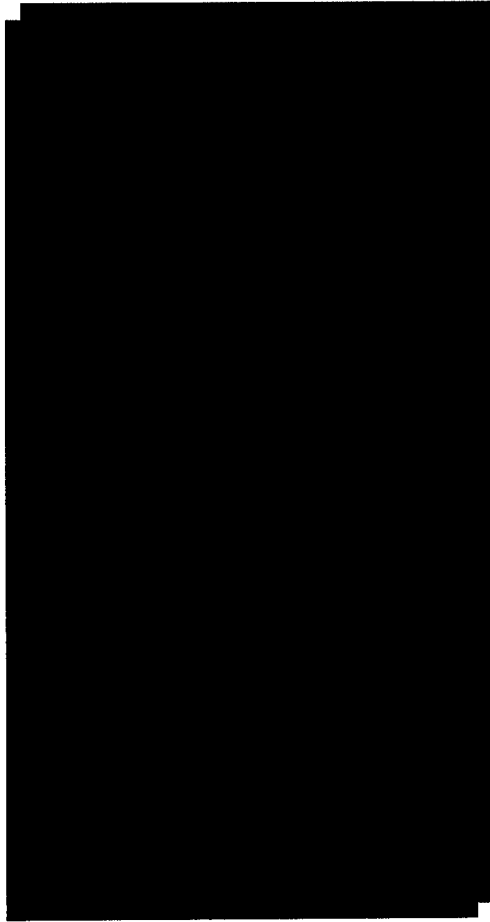
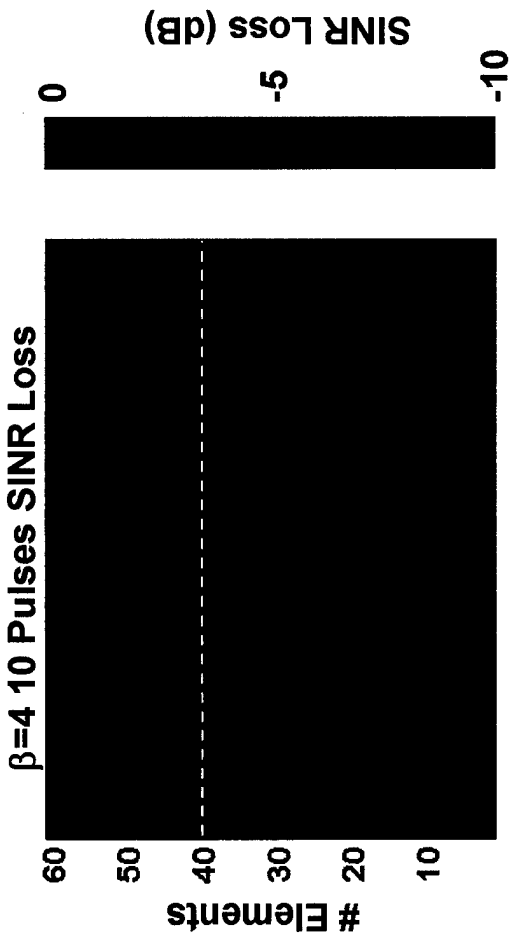
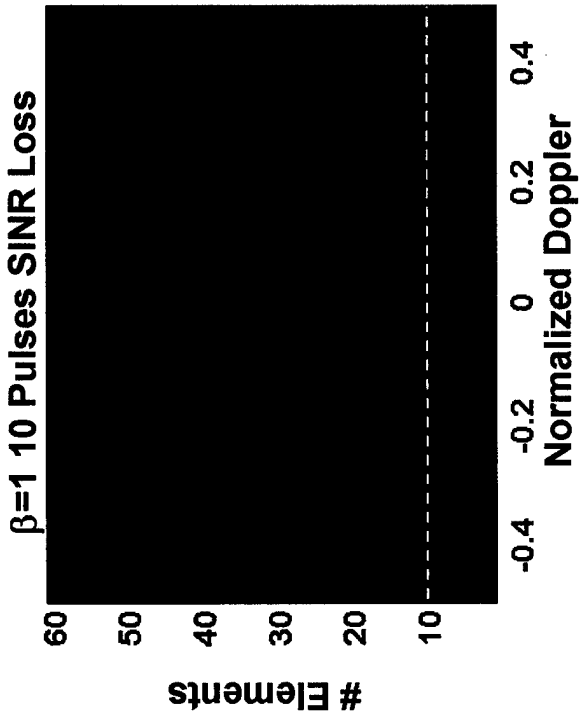


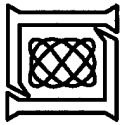
$$\beta = \frac{4V}{\lambda PRF}$$

$$\begin{aligned} \text{Main Beam} &= \frac{\lambda 2V}{L} \text{ (m/s)} = \frac{4V}{L} \text{ (Hz)} \\ \text{Clutter Width} &= \frac{4V}{L} \end{aligned}$$

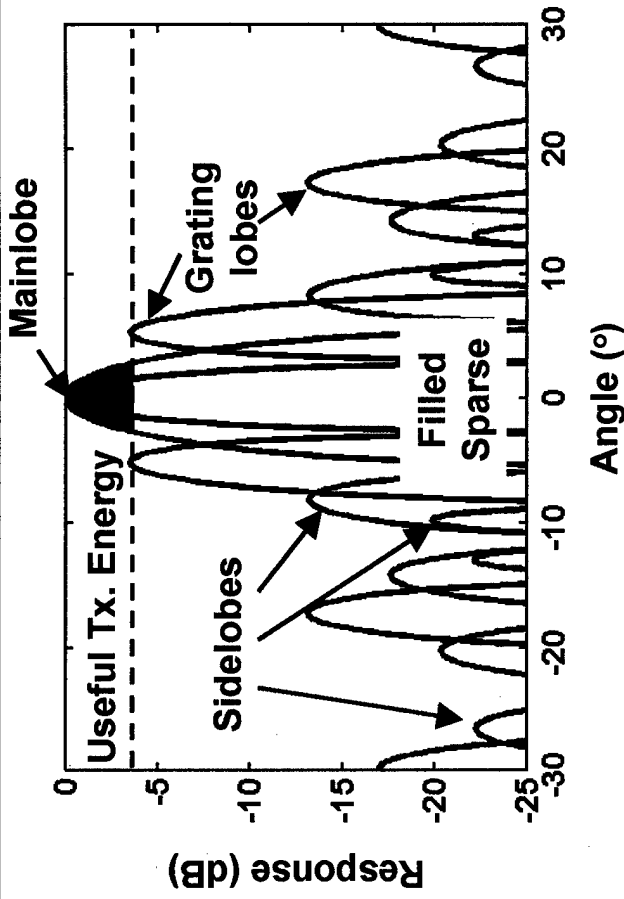
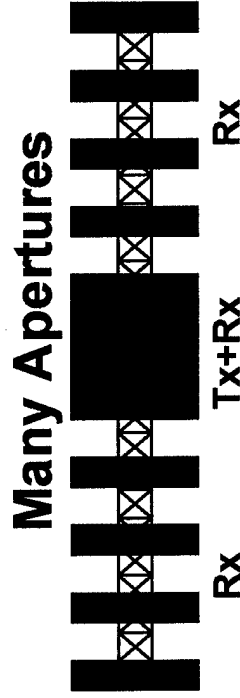
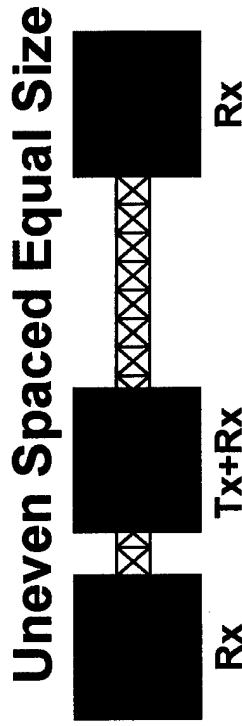
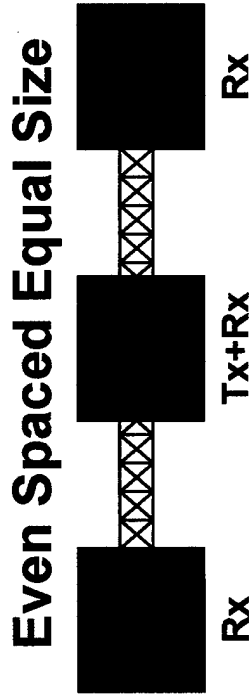
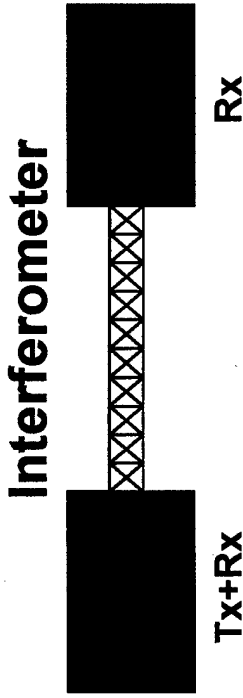


# Aperture and Doppler Limited Performance

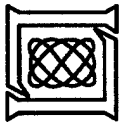




# Some Sparse Array Concepts



- Sparse arrays trade mainlobe width against grating lobe height to find the optimum sparseness
- Energy transferred from the mainlobe to the grating lobes is useless for Tx.
  - Use a filled section of the sparse array for Tx. And form multiple Rx. beams



# Sparse Array Issues

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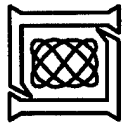
- **Angle estimation performance**
  - Improved accuracy due to narrower beamwidth (CRB)
  - Non-local errors due to grating lobes (WWB, ZZB, AB, ...)
  
- **SAR performance**
  - Multiple spatial samples per pulse
  - Tight PRF constraints
  
- **Hardware and cost**
  - Sparse arrays require less hardware
  - Cheaper & lighter
  
- ...



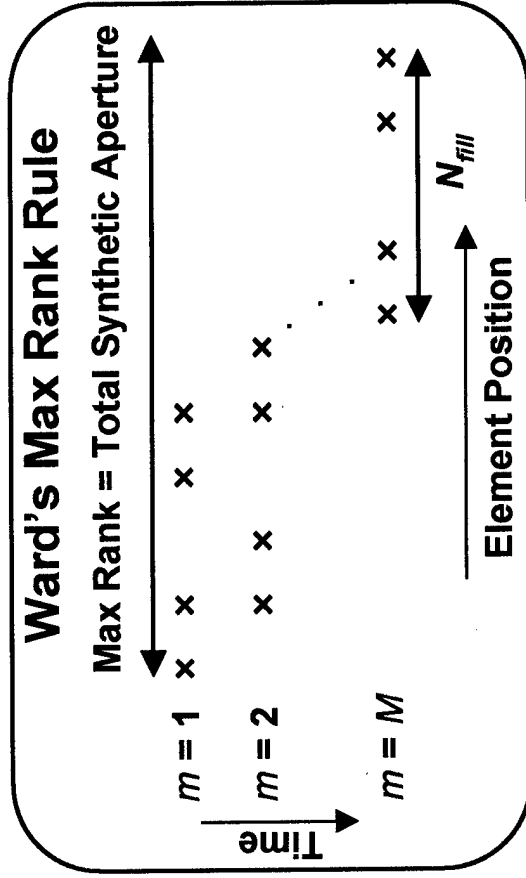
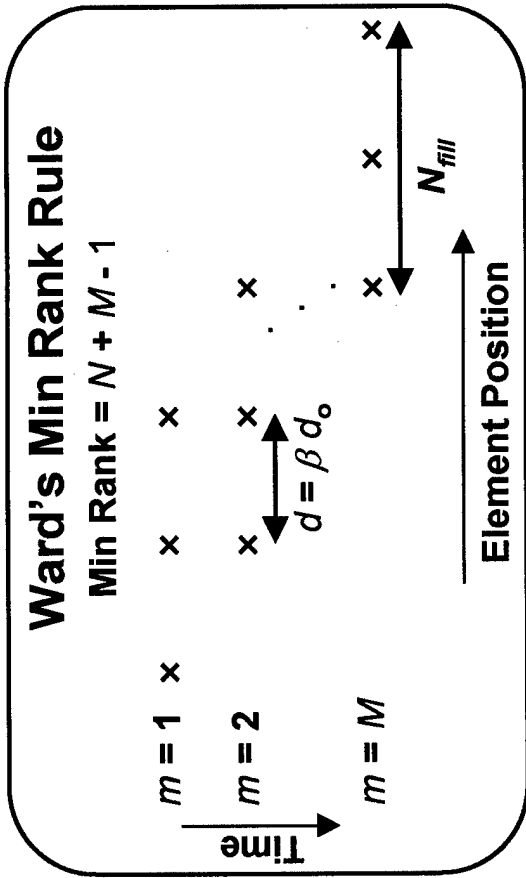
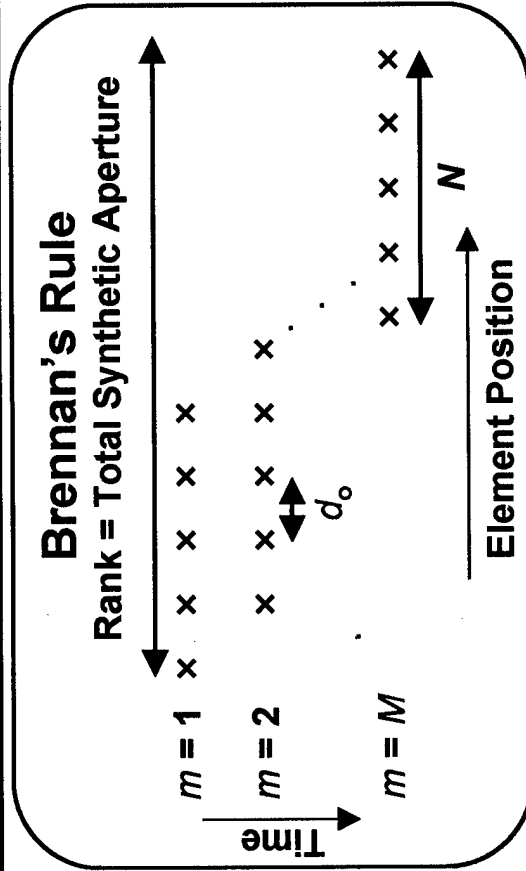
# Outline

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- **Introduction**
- **Theory**
  - **Clutter Rank**
  - **Waveforms**
  - **SINR Loss**
- **Performance**
- **Summary**



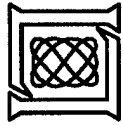
# Brennan's Rule & Ward's Rules\*



\*J. Ward, Asilomar 1998

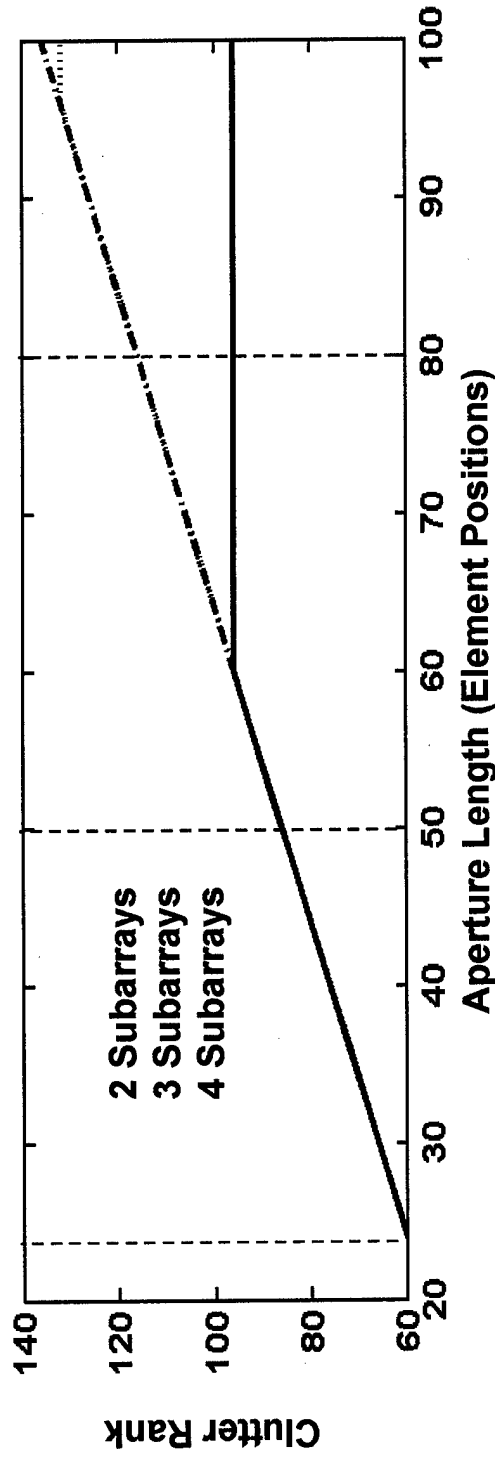
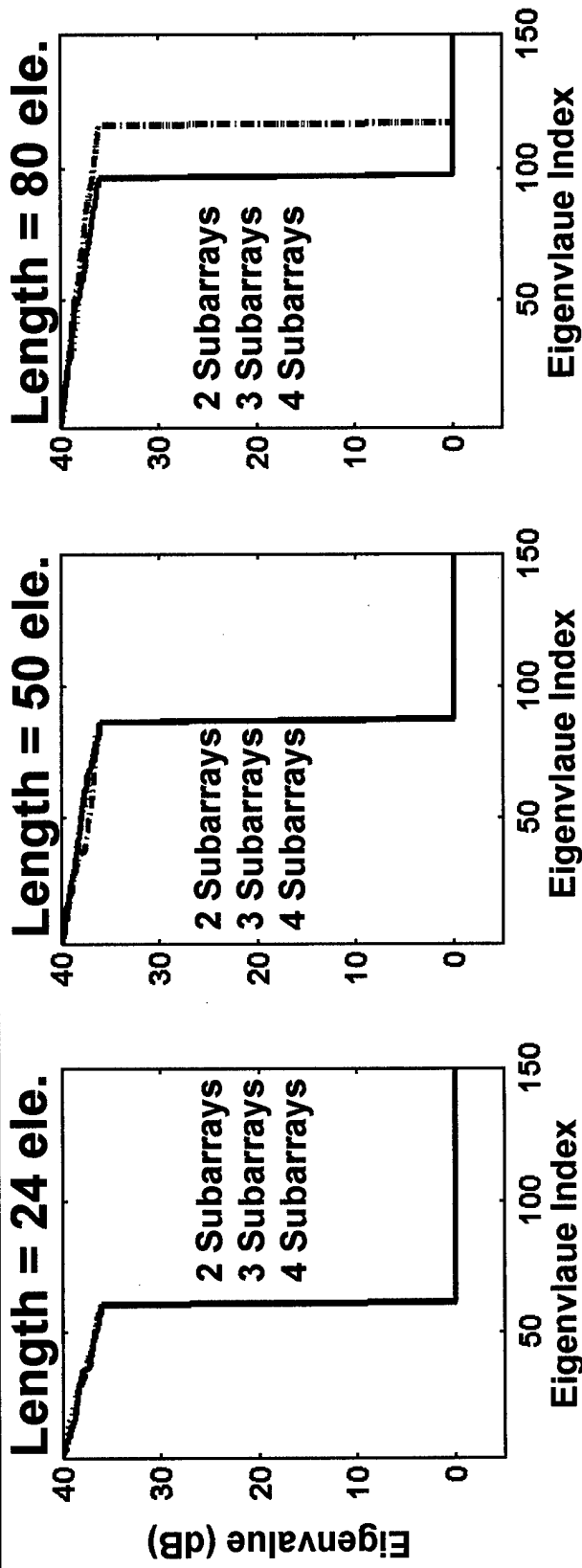
$N$  = Number of elements,  $M$  = Number of pulses,  $\beta = 2 \nu T d_0^{-1}$ ,  $N_{fill}$  = Number of elements in filled array

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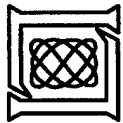


# Additional Sparse Array Behavior

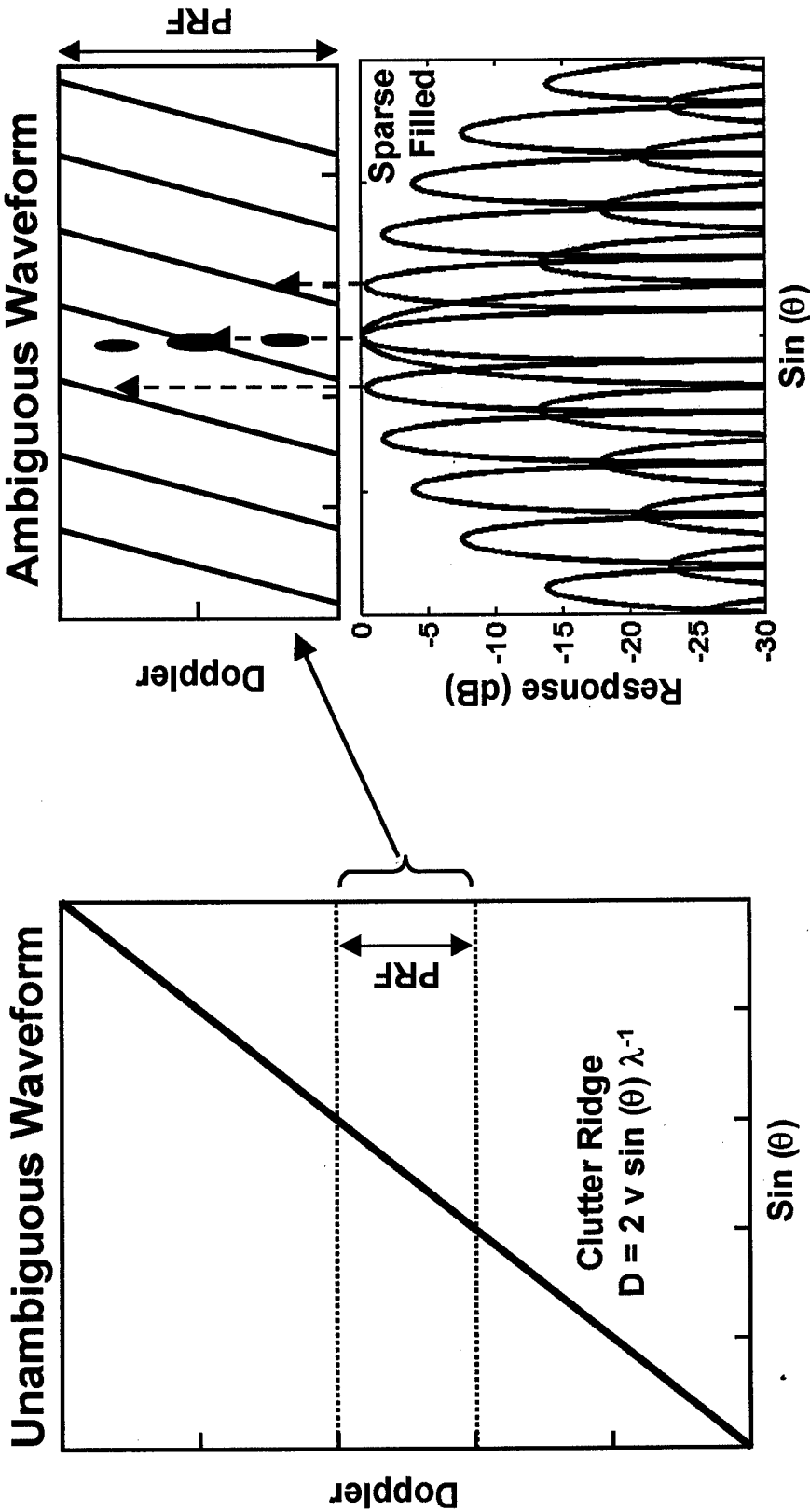
$N = 24, M = 10, \beta = 4$  Example



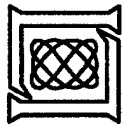




# Sparse Aperture Waveforms

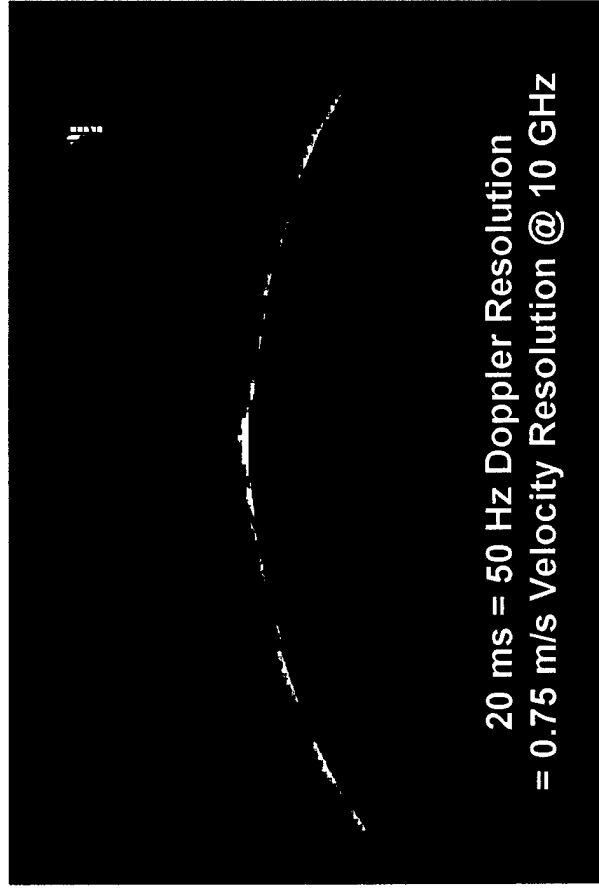


- Ambiguous waveforms (e.g., pulse-Doppler) and sparse (ambiguous) apertures lead to multiple clutter nulls
- Unambiguous waveforms preferable

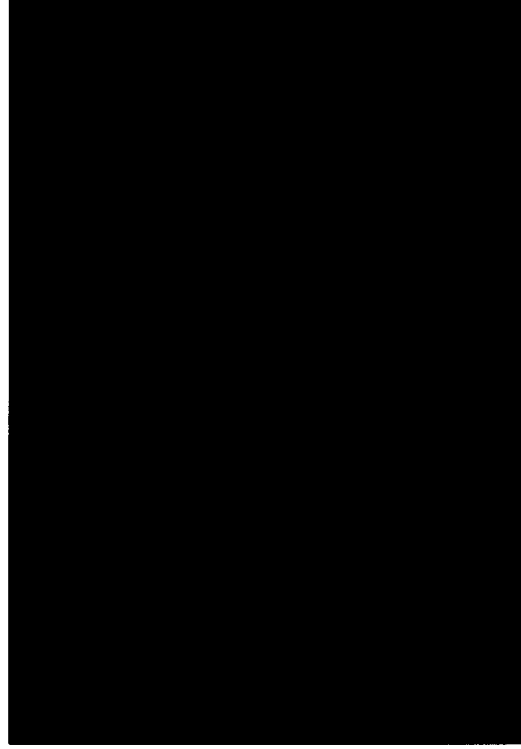


# Long Single Pulse Waveforms

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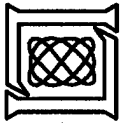
## Phase Encoded Waveform



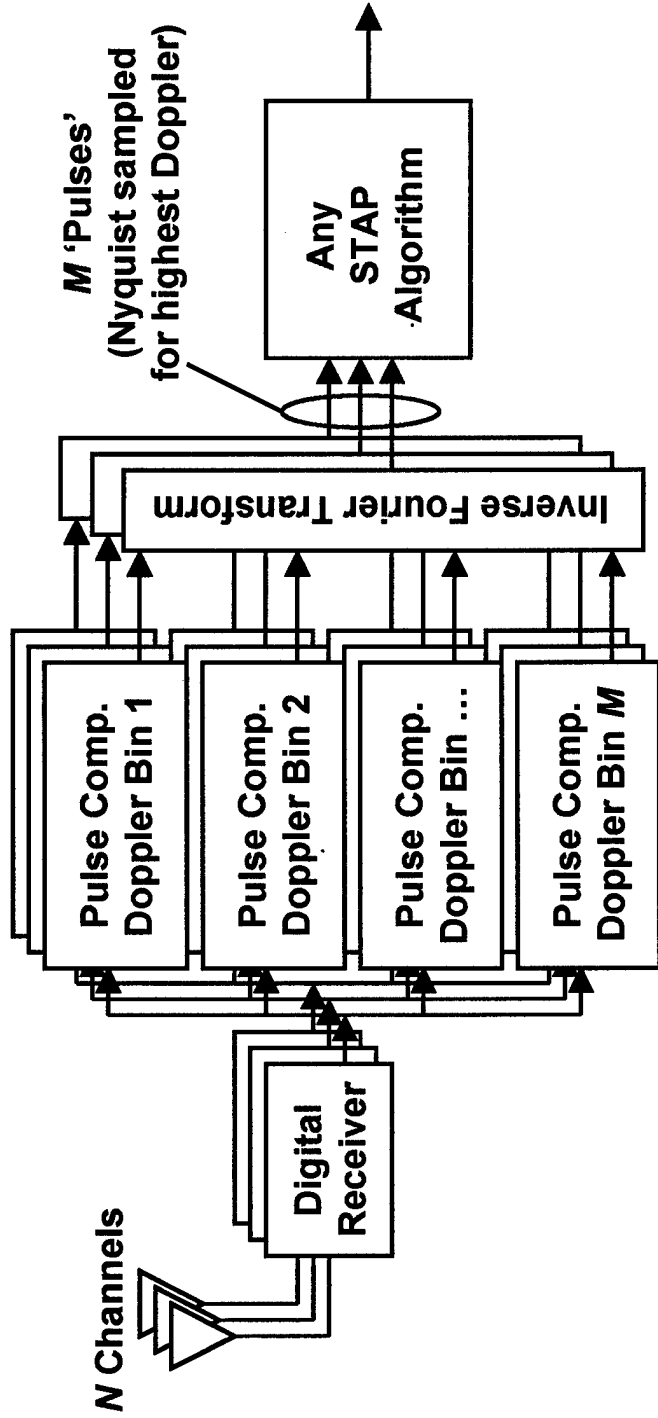
Doppler

Range

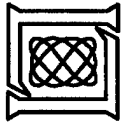
- **Single pulse means no range or Doppler ambiguities**
  - High chip rate sets Doppler ambiguities
- **Must pulse compress each Doppler bin separately**
  - More computation than pulse-Doppler waveforms
- **Concern about strong sidelobe clutter > noise floor**
  - Wide bandwidth & narrow antenna beam patterns



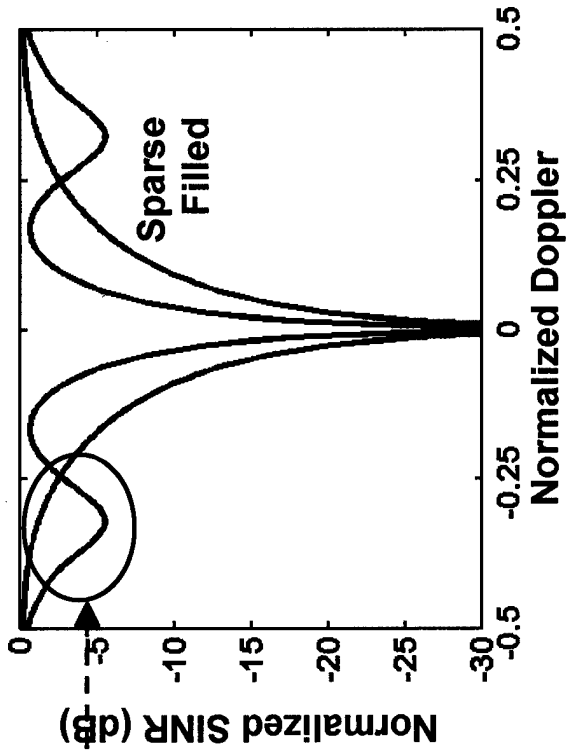
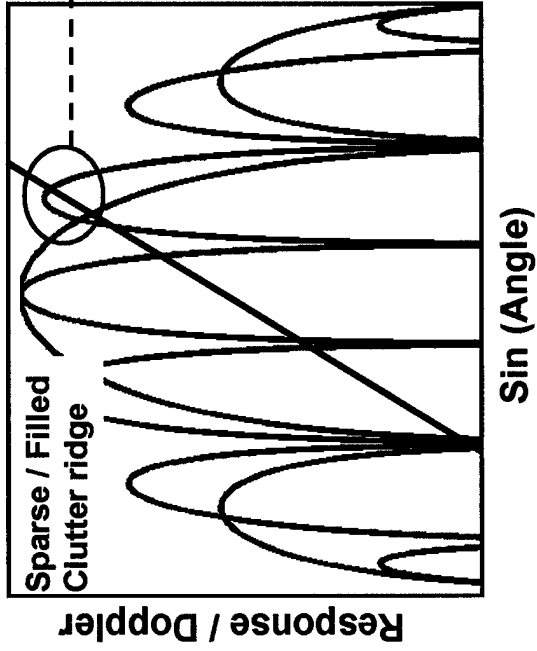
# Processing Long Single Pulse Waveform



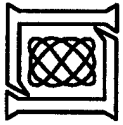
- Long single pulse radar can be made to 'appear' like a regular pulse-Doppler radar
- Looks like high PRF radar without the range ambiguities



# Space Time Adaptive Processing



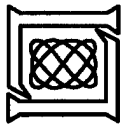
- Grating lobes lead to reduced detection performance at particular Doppler frequencies
- $$\text{SINR}_{\text{Loss}} \approx \mathbf{v}^H \mathbf{v} - |\mathbf{v}^H \mathbf{e}|^2 = 1 - \frac{\text{GratingLobeGain}}{\text{MainbeamGain}}$$
- Should not make the array too sparse
  - For <3 dB SINR loss grating lobe gain must be 3 dB less than main lobe gain ( $\Sigma$  grating lobes for pulse-Doppler waveforms?)



# Outline

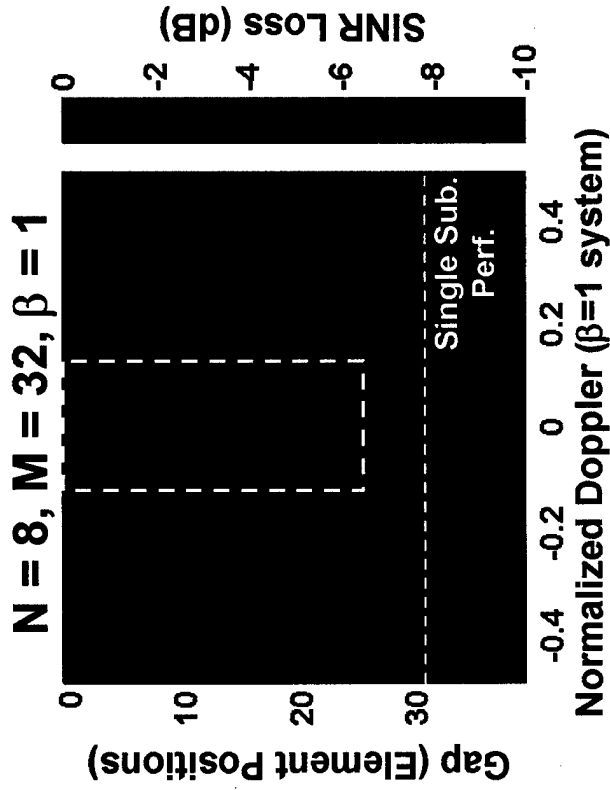
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- **Introduction**
- **Theory**
- **Performance**
  - **Dependence on waveform**
  - **SBR Design Example**
- **Summary**

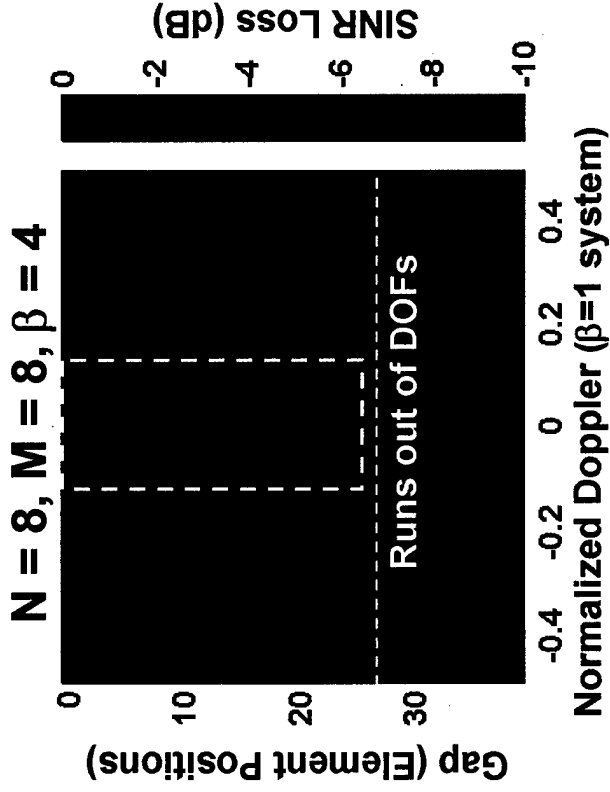


# Unambiguous vs. Ambiguous Waveforms

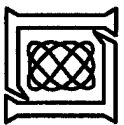
## Interferometer Example



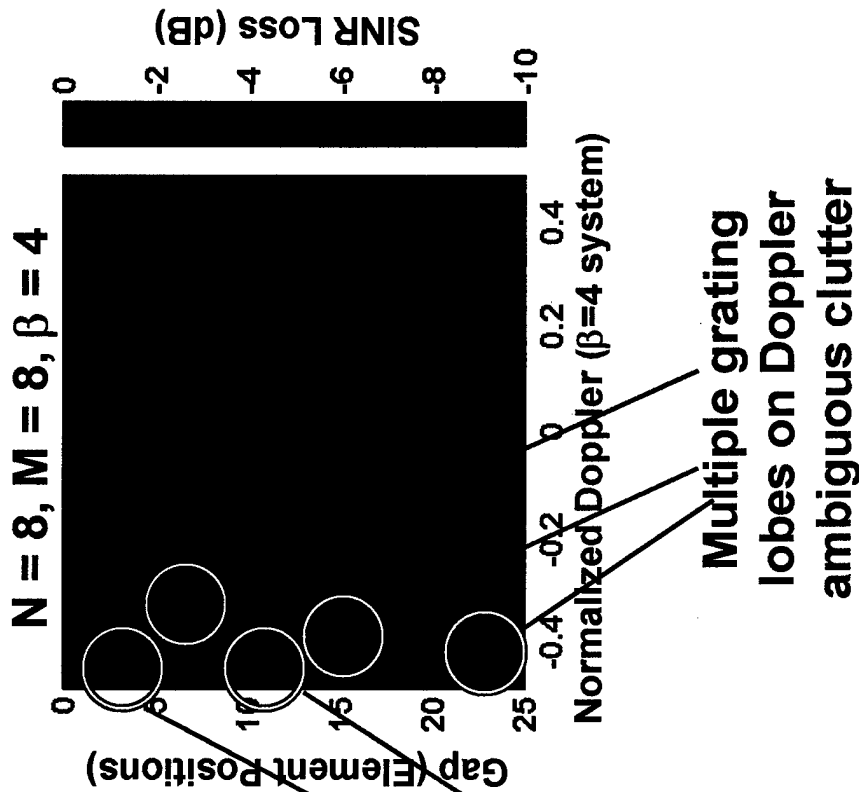
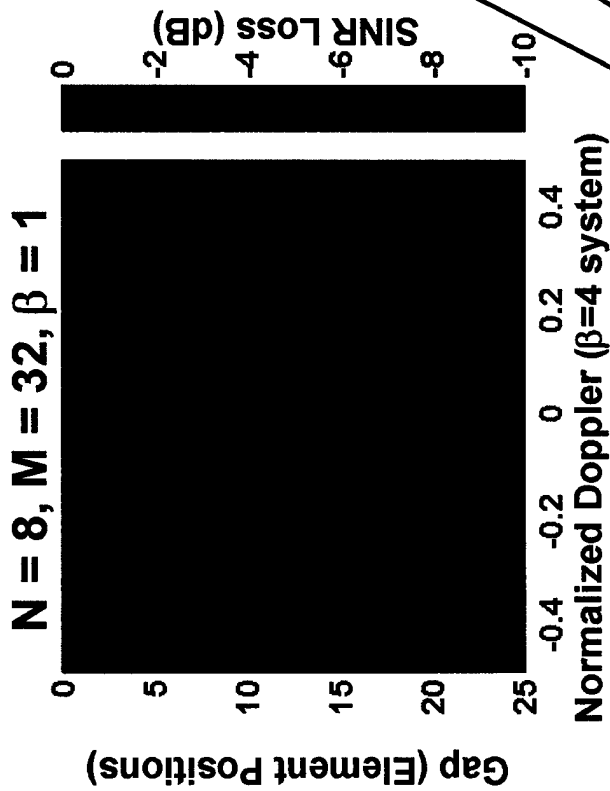
- Filled rank =  $8+1(32-1)$   
= 39
- Max. sparse rank =  $8+2(32-1) = 70$  (reached with a 31 element gap)

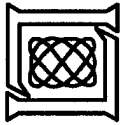


- Filled rank =  $8+4(8-1)$   
= 36
- Runs out of DOFs with a 27 element gap  
 $8+27+2(32-1) = 63$



# Unambiguous vs. Ambiguous Waveforms



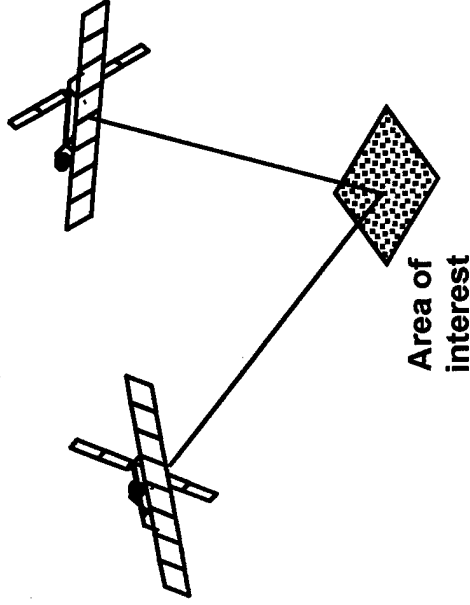


# Space Based GMTI Radar Examples

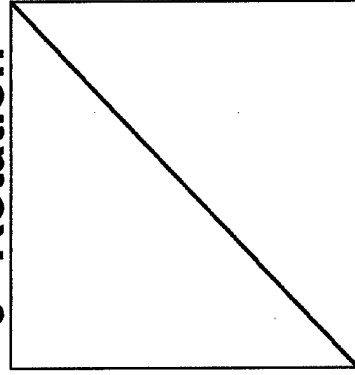
## Parameters

- 32m x 2.5m filled aperture
- 10 GHz operating frequency
- 1000 km orbit
  - 7282 m/s orbital velocity
- 1 kw peak transmit power
- 200 MHz bandwidth
- Unambiguous waveform
- -12 dB const.  $\gamma$  clutter model
- 2500 km range
  - 16.67ms CPI length
  - Travel ~120m in a CPI

## Scenarios



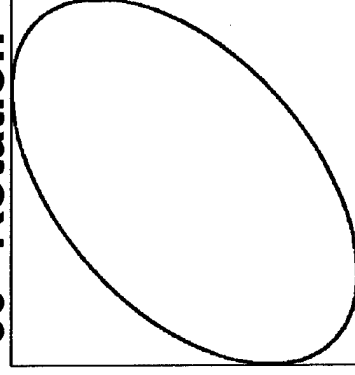
0° Rotation



Doppler

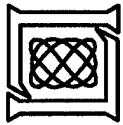
SIN (Angle)

60° Rotation



Doppler

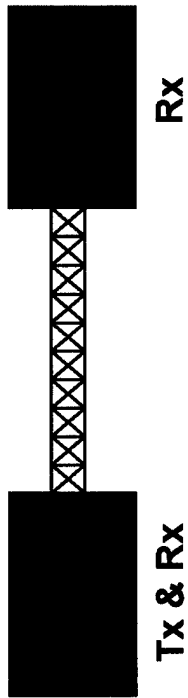
SIN (Angle)



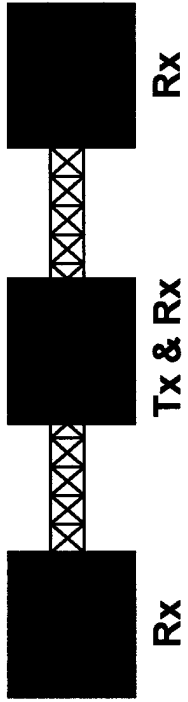
# Space Based Radar GMTI Designs

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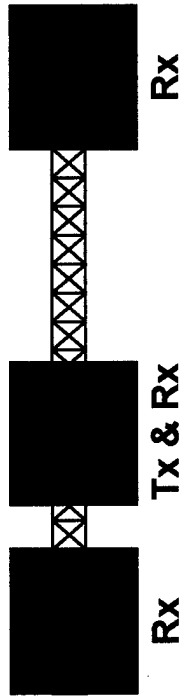
## Interferometer Array



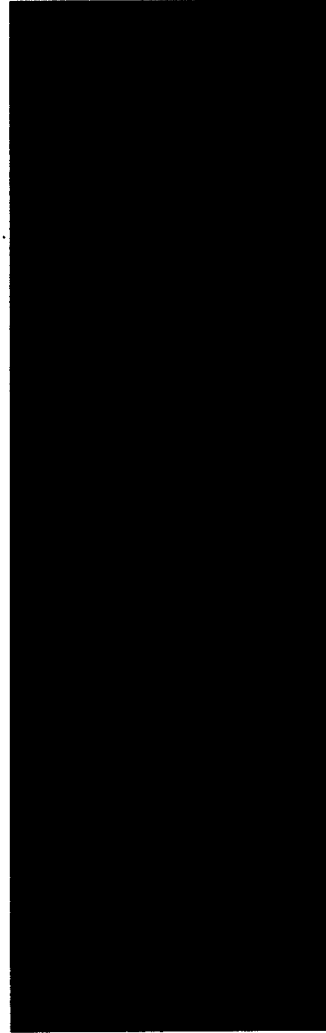
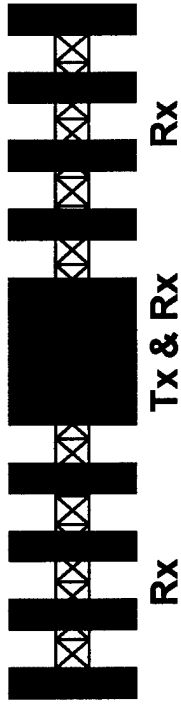
## Even Spaced Equal Size



## Uneven Spaced Equal Size



## Many Apertures

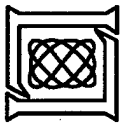


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\* Issues being addressed by Aerospace Corporation

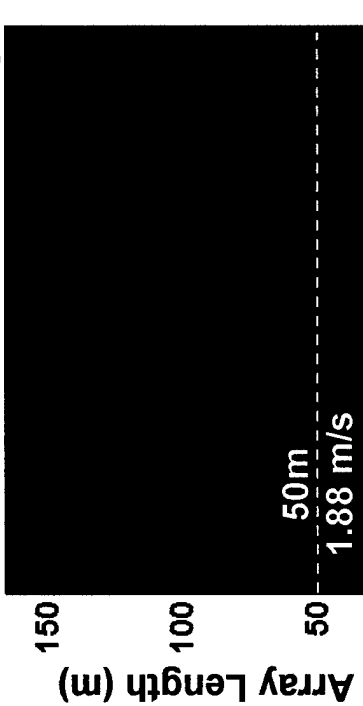
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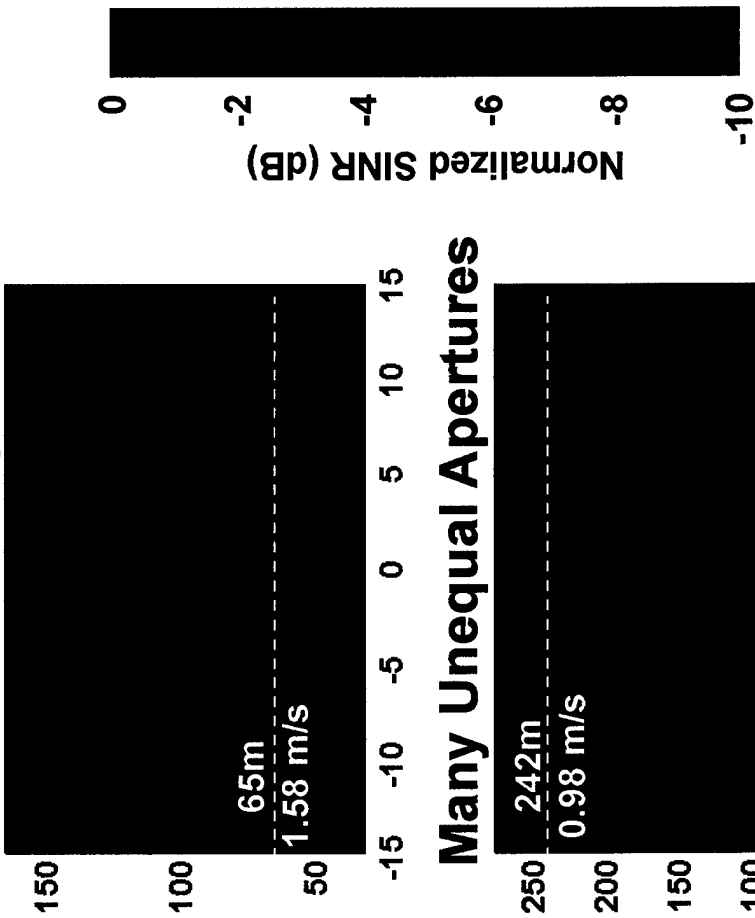


# 0° Rotation Scenario

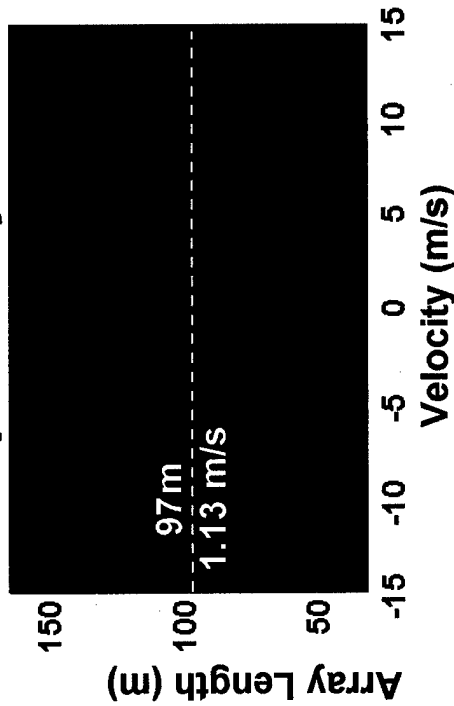
### Interferometer Array



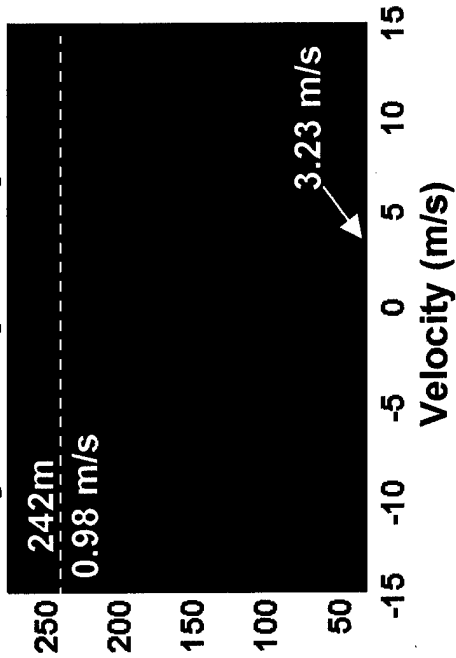
### Three Equal Arrays - Even



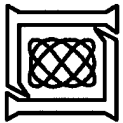
### Three Equal Arrays - Uneven



### Many Unequal Apertures

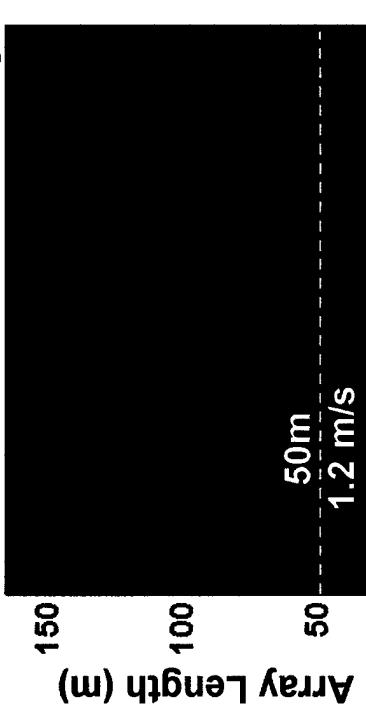


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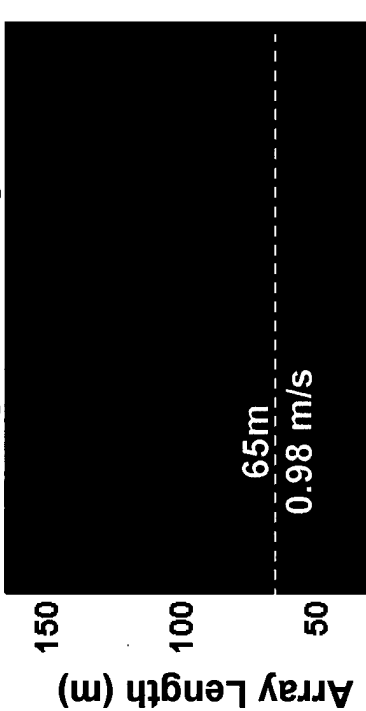


# 60° Rotation Scenario

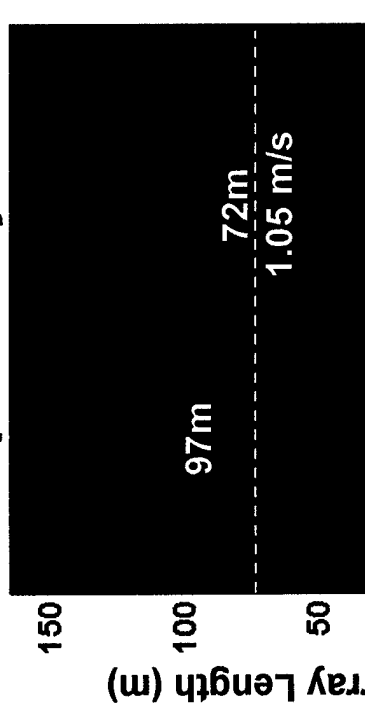
### Interferometer Array



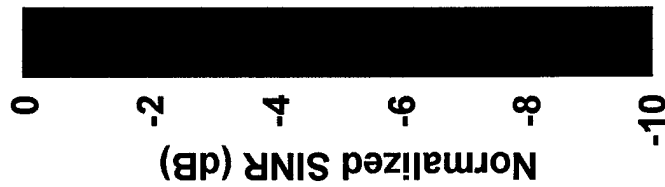
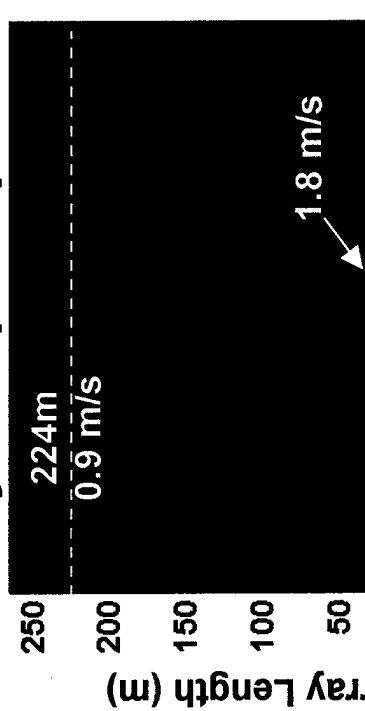
### Three Equal Arrays - Even

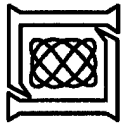


### Three Equal Arrays - Uneven

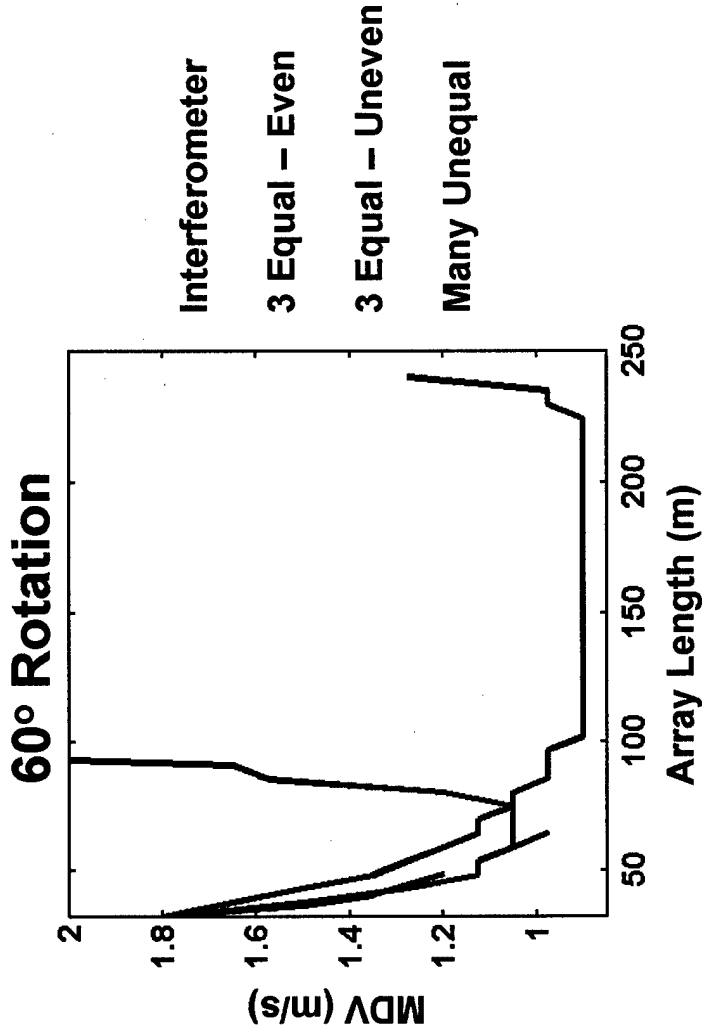
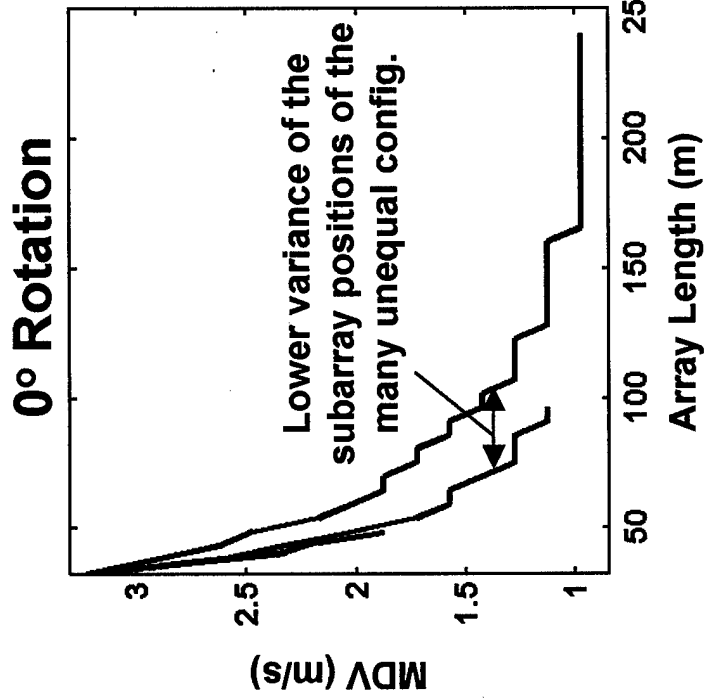


### Many Unequal Apertures

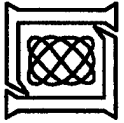




# -3 dB MDV vs. Array Length



- Many unequal subarrays configuration needs a larger baseline to obtain the same performance as the other configurations, but ultimately provides the best MDV
  - 165m aperture optimizes MDV for 2500 km range
  - Longer apertures improve angle metrics



# Summary

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- **Sparse arrays potentially improve the minimum detectable performance of space-based radars**
  - Approach the MDV performance of a large filled aperture much with lower size, weight and cost
- **Sparse arrays and sparse (pulse-Doppler) waveforms do not mix well**
  - Sparse arrays perform well with Doppler unambiguous waveforms
  - Sparse waveforms (pulse-Doppler) perform well with filled arrays
- **Long single-pulse waveforms provide range and Doppler unambiguous operation and are compatible with current STAP algorithms**
- **Sparse arrays with many unevenly sized unevenly spaced subarrays provide the best GMTI performance**

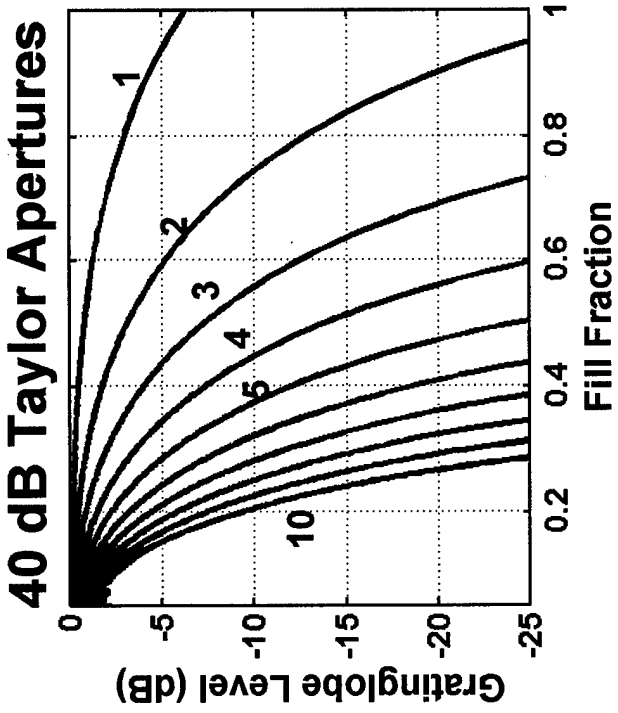
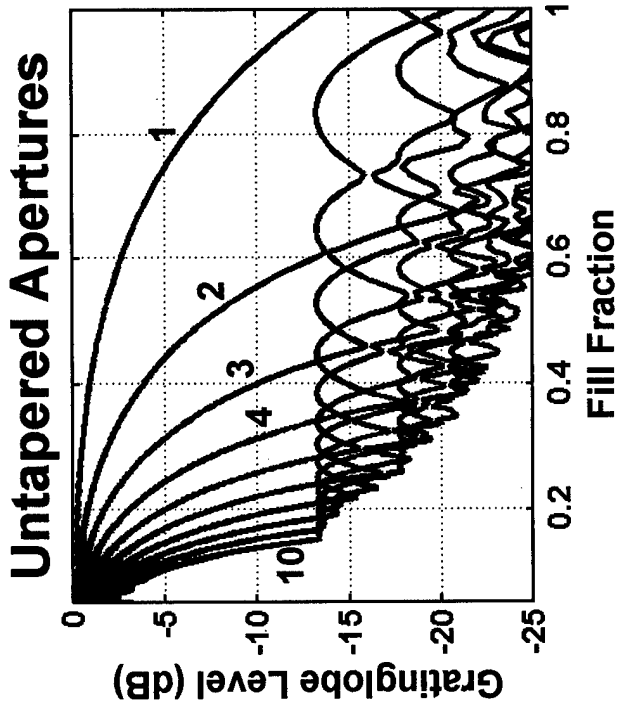


# Backup Viewgraphs

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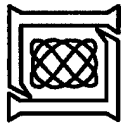


# Interferometer Array Grating Lobes

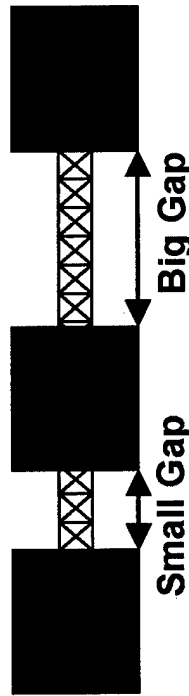
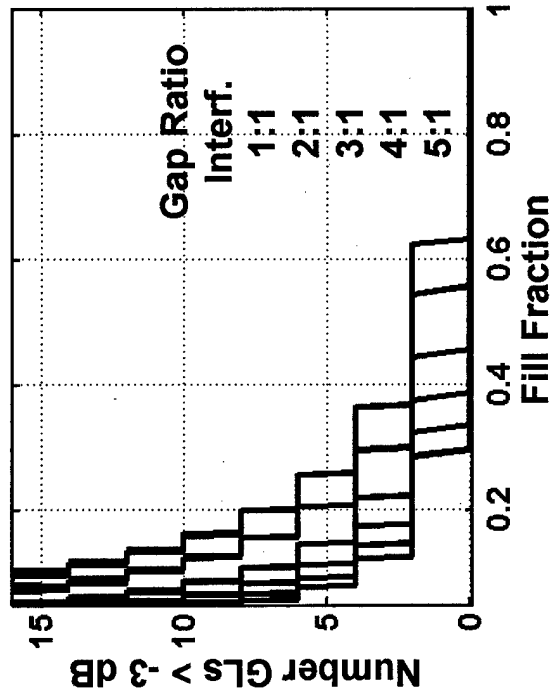
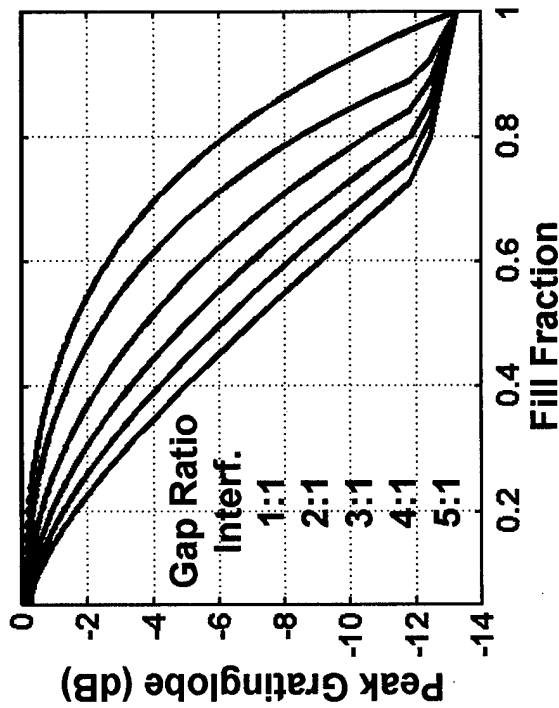


$$\text{Fill Fraction} = \frac{\text{Filled Aperture}}{\text{Total Aperture}}$$

- Grating lobes quickly appear for interferometer array
- $\sim 2/3$  fill fraction -3 dB grating lobes untapered apertures

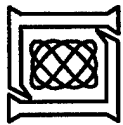


# Grating Lobe Distributions 3 Equal Arrays

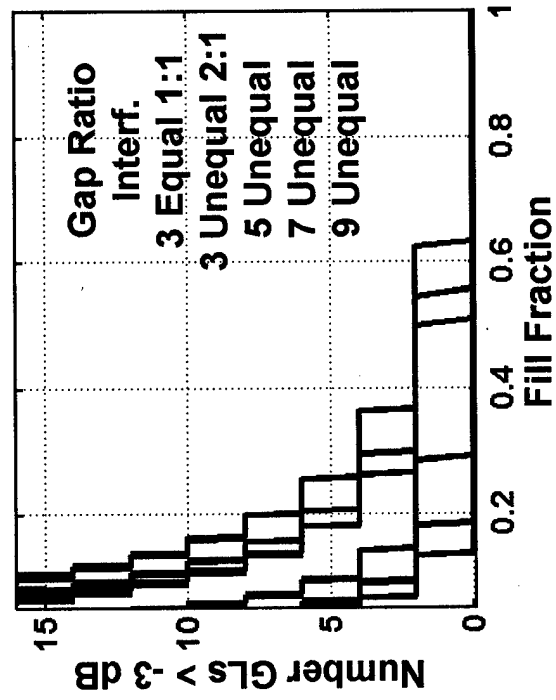
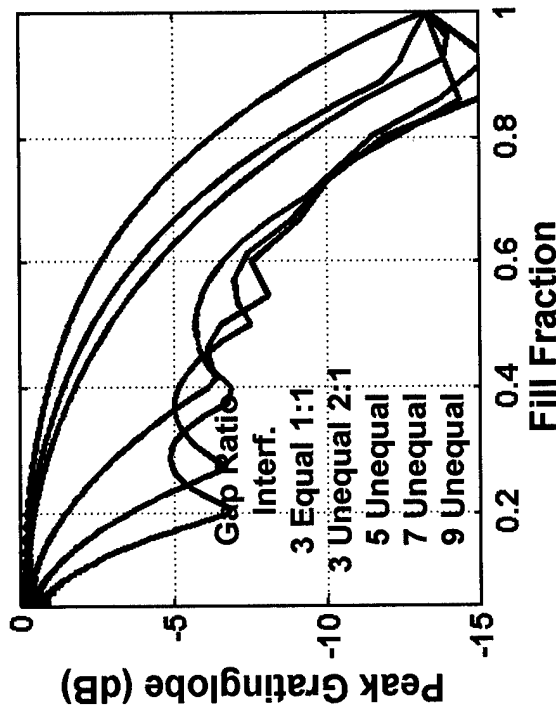


Gap Ratio = Big Gap : Small Gap

- Lower grating lobes than interferometer
- Higher gap ratios lead to lower grating lobes
  - Also poorer MDV performance

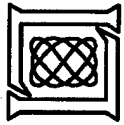


# Grating Lobe Distributions Unequal Arrays



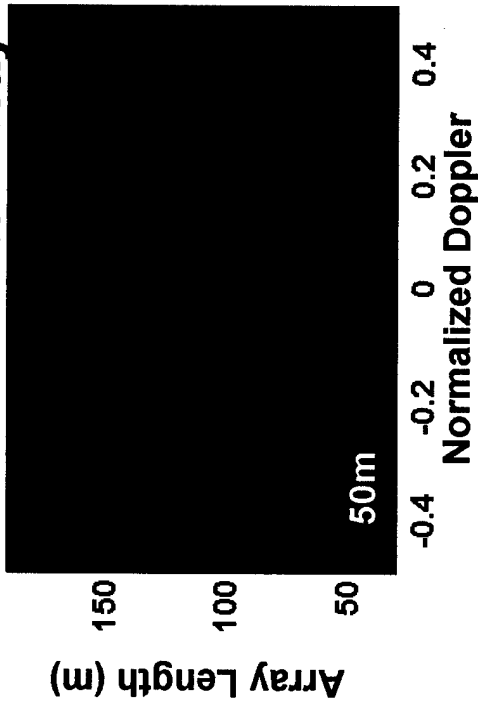
50% filled aperture in center subarray



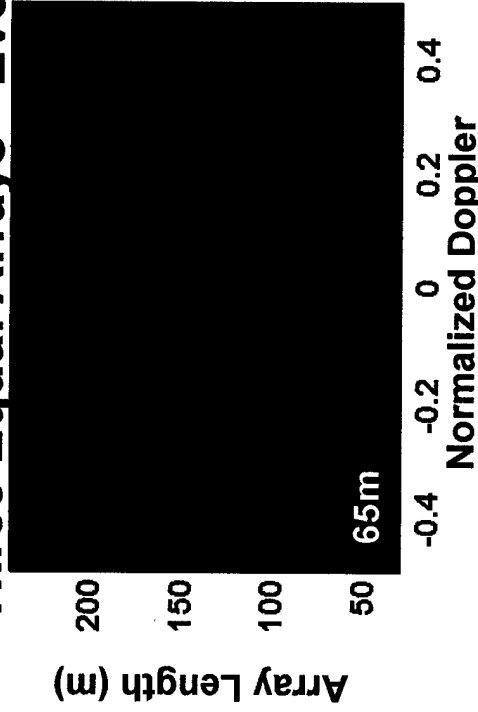


# 0° Rotation Scenario

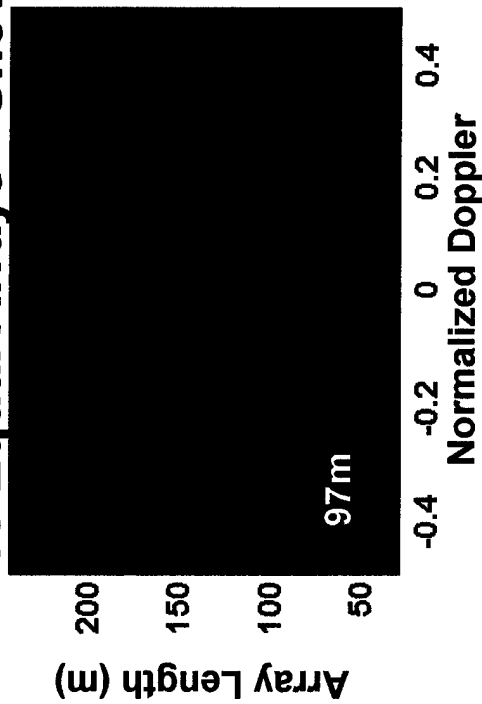
### Interferometer Array



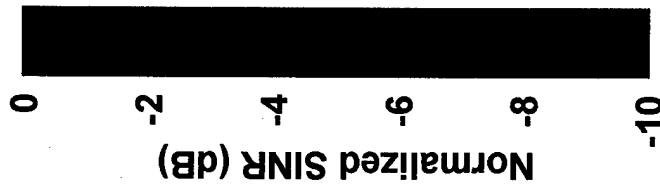
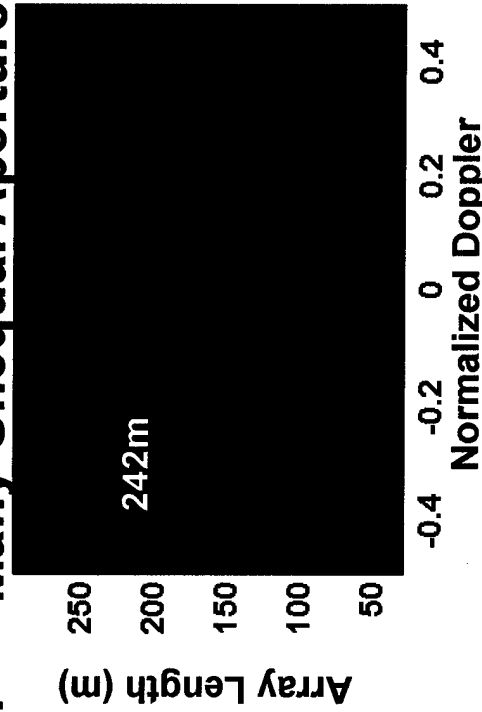
### Three Equal Arrays - Even



### Three Equal Arrays - Uneven

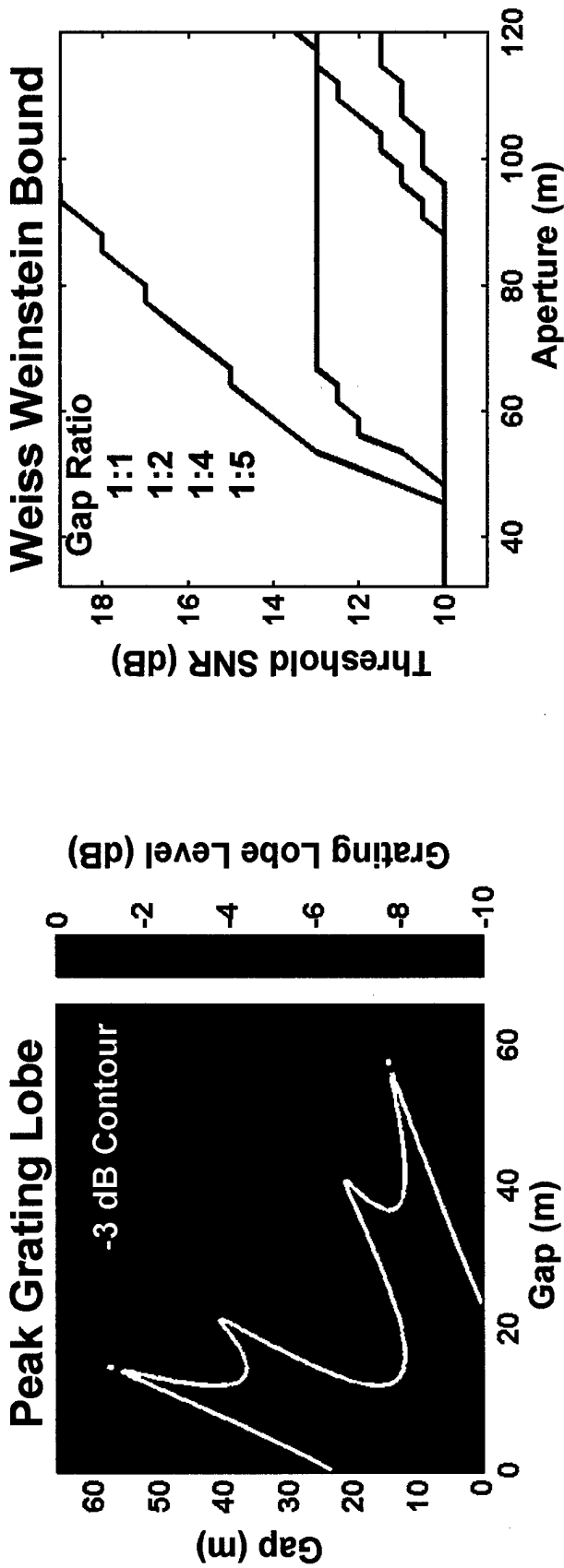


### Many Unequal Apertures

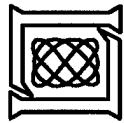




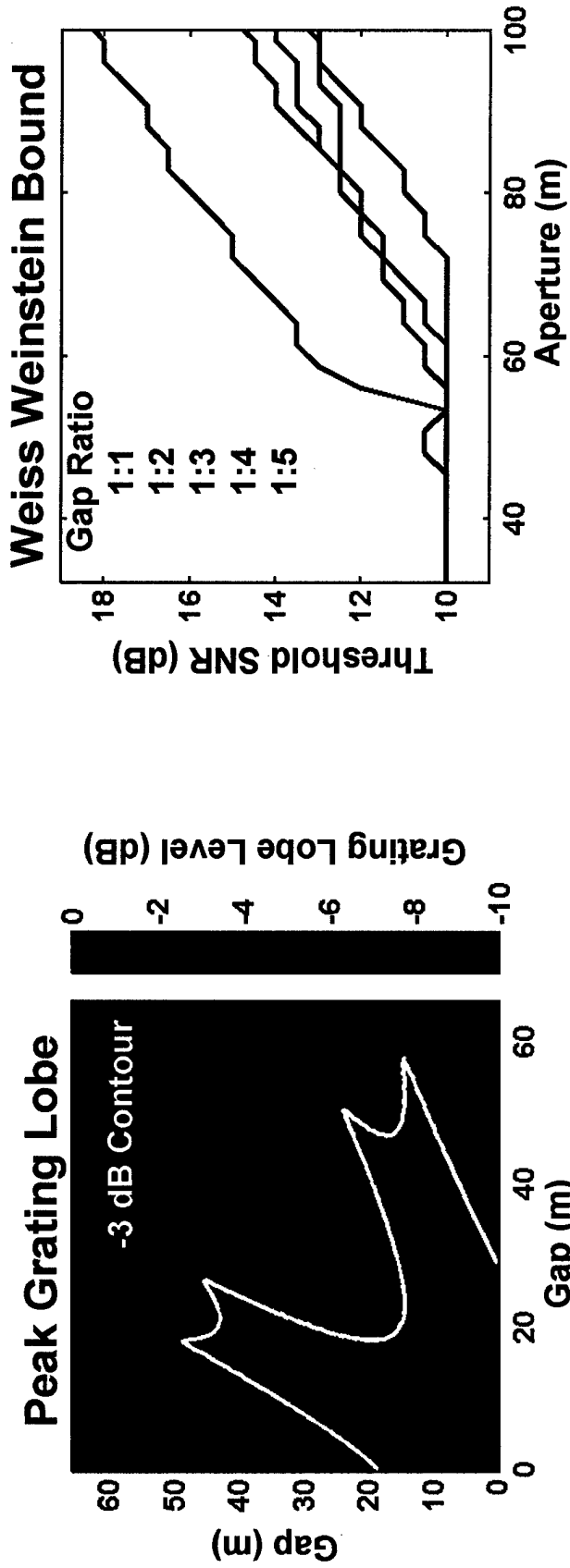
# Three Equal Apertures Target Location



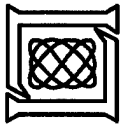
- 96 m aperture largest possible without increasing the threshold SNR
  - Provides 89 m rms error at 6° grazing
  - 82 m gives 107 m rms error



# Three Unequal Apertures Target Location

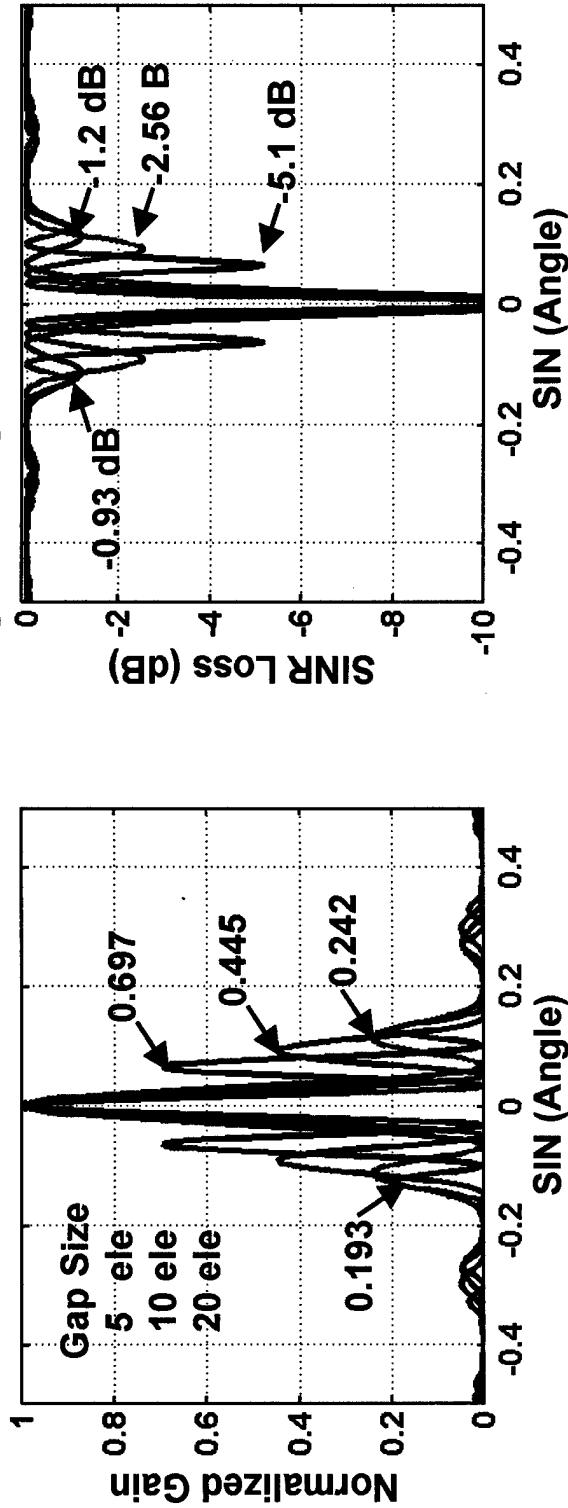


- 72 m aperture largest possible without increasing the threshold SNR
- 72m aperture Provides 119m rms error at 6° grazing



# SINR Loss Due To Grating Lobe (Spatial Only Example)

20 Element Array Example



- Under the high INR assumption:

$$\text{SINR Loss} \approx \mathbf{v}^H \mathbf{v} - |\mathbf{v}^H \mathbf{e}|^2 = 1 - \frac{\text{Grating Lobe Gain}}{\text{Mainbeam Gain}}$$

- i.e., for 3 dB loss grating lobe gain (sum grating lobes for pulse-Doppler?) must be 3 dB less than main lobe gain